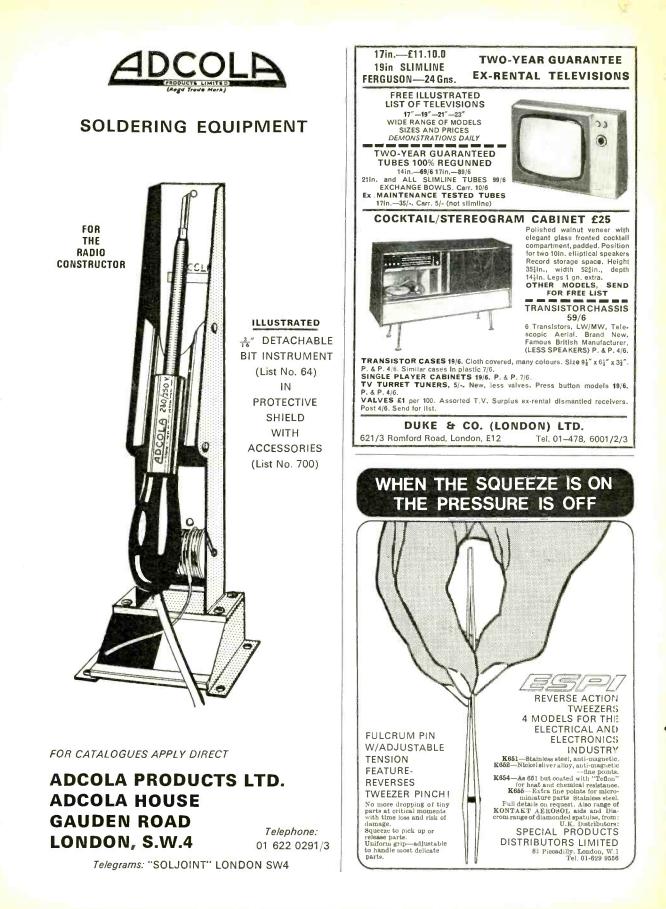
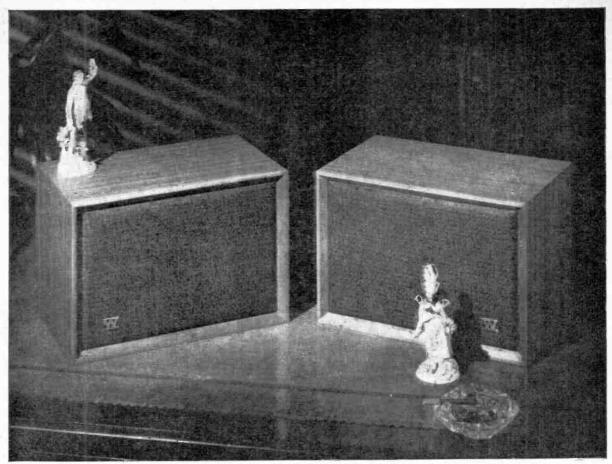
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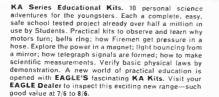
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Attractive case with red speaker grille. Size 62 x

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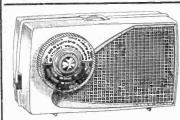
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An extremely reliable general purpose valve amplifier. Its rugged construction yet space age styling and design makes it by far the best value for money. TECHNICAL SPECIFICATIONS

TECHNICAL SPECIFICATIONS 4 electronically mixed channels, with 2 inputs per channel, enables the use of 8 sep-arate instruments at the same time. The volume controls for each channel are located directly above the corresponding input sockets. SENSITIVITIES AND INPUT IMPEDANCES Channel 1 4mV at 470K] These 2 channels (4 inputs) are suitable for Channel 2 4mV at 470K] These 2 channels (4 inputs) are suitable for Channel 3 200mV at Im } [gram, tuner, organ etc.]. Input sensitivity relative to 10w output. TONE CONTROLS ARE COMMON TO ALL INPUTS Bass Boost + 12dB at 60 Hz/s. Bass Cut - 13dB at 60 Hz/s.

Bass Boost +12dB at 60 Hz/s. Treble Boost +11dB at 15 KHz/s. Treble Cut -12dB at 60 Hz/s. With bass and treble controls central -3dB points are 30 Hz/s and 20 KHz/s. POWER OUTPUT

For speech and music 50 watts rms. 100 watts peak. For system and music 50 watts rms. 100 watts peak. For systemined music 50 watts rms. 90 watts peak. For sine wave 38.5 watts rms. Nearly 80 watts peak. Total distortion at rated output 3.2%Total distortion at 20 watts 0.15% at 1 kHz/s Output to match into 8 or 15 ohms speaker system. **NECATIVE FEED BACK** 20dB at 11kHz/s.

SIGNAL TO NOISE RATIO 60dB. MAINS VOLTAGES

Adjustable from 200-250v A.C. 50-60 Hz/s A protective fuse is located at the rear of unit. VÁLVE LINE UP Double purpose ECC83 x 3, EL34 x 2 and GZ34



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put). 4 watts r.m.s.

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SPECIFICATIONS Elegant styled cabinet (sizes 16" wide 5" high 8½" deep) in black rexine and woodgrained sides. Brushed aluminium front panel with contrasting black / silver knobs

CONTROLS

Stereo/Mono switch. Gram/Aux switch. Volume left. Volume right. Treble (cut and lift). Bass (cut and lift). Separate on/off switch. Neon pilot indicator. INPUTS AND OUTPUTS

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Size: 9" x 6" x 1³". A.C. Mains, 200-250V, 4 valves. For use with Std. or L.P. records, musical instruments, all makes of pick-ups and mikes. Output 8 watts at 5 per cent of total distortion. Separate

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600 mW FOUR TRANSISTOR AMPLIFIER

Features N.P.N. and P.N.P. complementary symmetrical output stage, $2\frac{1}{4}$ x $\frac{3}{4}$ " Speaker. Output impedance 12 ohms frequency response 3dB points 90 c/s and 12 Kc/s. Price 15/- plus 1/- P. & P. 7 x 4" Speaker to suit, 19/6 plus 2/- P. & P.

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AC mains 240V. Size 7" x 44" x 13". Frequency response 100 c/s-10 Kc/s Semi conductors, two OC 75's two AC 128's and two stabilizers AA129. Tone and volume controls on flying leads. £2.10.0 plus P. & P. 3/6. Suitable 8" x 5" 10,000 line high flux speaker, 18/6 plus 2/- P. & P.

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Size 5 $\frac{1}{2} \times 3\frac{1}{4} \times 1\frac{1}{4}$ in. For IF and RF alignment and AF output 700 o/s frequency coverage 460 kc/s to 2 mc/s in switched frequencies. Ideal for alignment to our Elegant Seven and Musette. Built and tested. 39/6 P. 8, P. 3/6.



BSR TAPE DECKS 200/250V A.C. mains

Type TD2 Tape speed 3[‡] twin track, £6.19.6. Type TD10 2-track, 3 speed, plus rev. counter-£7.19.6.

£7.19.0. Type **TD10** 4-track, 3 speed, plus-rev. counter---**£9.5.0.** P. & P. on each 7/6.





6" x

8





P. & P. 3/-



at 1 KHz. Negative feedback 13dB at 1 KHz. Mains supply 220-250V A.C. 50-60 Hz.

TECHNICAL SPECIFICATIONS

Gram sensitivity 40mV at 1 KHz. Aux sensitivity 50mV at 1 KHz. (Sensitivities are given for rated out-

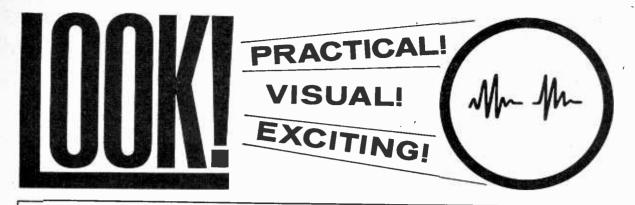
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27 <u>gns</u>

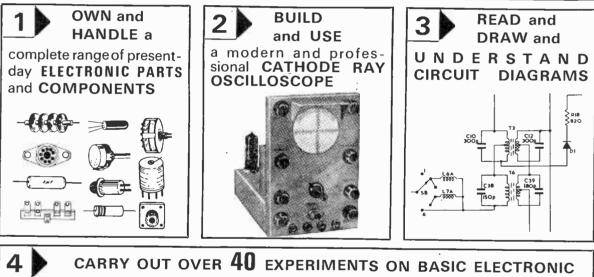
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MAY 1968

IRELESS

TOPIC OF THE MONTH

End of the Road

WE hope that just because the manufacture and import of certain radio equipment became illegal as from April 1st, owners, or prospective owners, of such equipment will not be tempted to become April Fools!

RACTICAL

P.W. long campaigned for some action on the question of illicit walkie-talkies and last year, at long last, the Postmaster-General introduced a Bill covering the situation.

Under Section 7 of the Wireless Telegraphy Act, 1967, importers and manufacturers must seek the authority of the PMG to make or import apparatus designed to transmit between 26·1–29·7 and 88–108 Mc/s. Most of the trouble was caused by 27Mc/s walkie-talkies which created interference with other (legitimate) services and since 27Mc/s is not available for amateur use their operation was in any event illegal.

A curiosity of the law is that it is *still* not illegal either to *sell* or to *buy* such equipment, but only illegal to *use* it. Thus unscrupulous dealers could sell the units to innocent purchasers; or buyers, knowing the risks, could buy them over the counter with no questions asked.

One suggestion we made (*) to end this anomaly was that any transmitting equipment should only be sold to purchasers able to produce a transmitting licence for the frequencies covered. The PMG chose to tackle the problem by tightening up on the manufacture and import side. At the same time, the 1967 Act raised the maximum fine for operating such equipment without a licence to £400, while retaining the maximum penalty of three months' imprisonment.

Readers, particularly newcomers, should bear these facts in mind if they are tempted to buy, or use, such equipment from any source whatsoever! The only licences issued to use walkie-talkies and other small radio transmitters are for such users as police, fire and other public services, organisers of sporting events, yachtsmen, the press, schools, entertainers and various business (factories, building sites, etc.). Even so, a condition is that the equipment must meet performance requirements and operate on specified frequencies.

Amateur licences and frequencies, of course, remain unaffected by the provisions of the Act.

W. N. STEVENS---Editor

All correspondence intended for the Editor should be addressed to: The Editor, "Practical Wireless", George Newnes Ltd., Tower House, Southampton Street, London, W.C.2. Phone: TEMple Bar 4363. Telegrams: Newnes Rand London. Subscription rates, including postage: 36s. per year to any part of the world. (c) George Newnes Ltd., 1968. Copyright In all drawings, photographs and articles published in "Practical Wireless" is specifically reserved throughout the countries signatory to the Berne Convention and the U.S.A. Reproductions or imitations of any of these are therefore expressly forbidden.

*see p97 June 1967, p276 August 1967, p437 October 1967 for comments and details of the Bill.

NEWS AND COMMENT

	17
Leader	18
News and Comment	10
Practically Wireless	
by Henry	35
On the Short Waves	
by Christopher Danpure and	
David Gibson, G3JDG	44
Your Questions Answered	46
The MW Column	
by Alistair Woodland	57
Letters to the Editor	61
New Books	62
COI COI COI COI COI	66

CONSTRUCTIONAL

TRF5 Pocket Portable by R. F. Graham	20
Simple Automatic Switch by J. E. Kasser	23
Modulated Crystal Marker by Hugh Wagner	28
End Fed Aerial Tuner by F. G. Rayer, G30GR	31
Midget I.C. Amplifier by L. McNamara, B.Sc.	38
A Comprehensive Checker by C. R. Bradley	40
The "Clubman" Part 5 by J. Thornton-Lawrence,	40
<i>GW3JGA</i> Simple Musical Toy	48
by J. M. Watt	65

OTHER FEATURES

Repairing Radio Sets, Part 2	
by H. W. Hellyer	24
Five Steps to Hi-Fi	
by Iain Smith	36
The Semiconductor Diode	
by Barry C. Francis	50
A Method of Repetitive Morse	
Broadcasts	
by J. McCarthy	58
	VAY 10th

VOL 44 No 1

issue 735

NEWS AND COMMENT...

"BETTER SOUND"

There will be four programmes in a new series "Better Sound" which will be broadcast on Fridays at 7.00-7.30 p.m. in Study Session, Radio 3 from May 3 to 24. Listeners will be invited to send questions of general interest, or requests for more information on particular topics covered in the series and these will be dealt with in two extra programmes which will follow the repeat of the series later in the year.

The series will be repeated on Radio 4 on Saturday mornings at 11.00-11.30 a.m. from August 17 to September 14. There will be no programme on August 31 (Bank Holiday weekend), but there will be two additional programmes on Saturdays, September 21 and 28.

The series is planned for home enthusiasts and those who use sound equipment as a teaching aid, or in amateur dramatics and so on. The aim is to help them to get the best out of their hi-fi equipment, tape-recorders and radios. This will be done by giving information about the basic principles involved in the transmission, recording and reproduction of sound, and practical advice on the choice and use of different types of equipment. Advice on particular makes cannot be given and the construction and repair of equipment will not be dealt with.

Speakers will include Donald Aldous, technical editor of *Audio Record Review*, John Borwick, technical editor of *The Gramophone*, John Crabbe, editor of *Hi-Fi News* and members of the BBC's staff.

Each programme will focus attention on one area of this wide field. A number of topics (e.g. microphones, loud-speakers, stereo) will therefore be treated in more than one programme.

Programme 1: Transmission and reception of radio, including stereophonic broadcasting. Explanation of a.m. and f.m., etc. Programme 2: The nature of sound, and room acoustics, with demonstrations of the effect of different placings of microphones and loudspeakers. Programme 3: The reproduction of music in mono and stereo; hi-fi equipment. Programme 4: Tape-recording for the amateur.

The diagrams in the *Study Notes* (BBC Publications, 2s. 6d. plus 5d. postage) will be helpful in following the broadcasts and the explanations in the text of the basic principles of the transmission, recording and reproduction of sound in mono and stereo will be useful for reference, particularly for the less knowledgeable listeners.

GB2LO AT CITY OF LONDON FESTIVAL

An unusual feature of the 1968 City of London Festival, July 8–20, will be the Amateur Radio station installed and operated by the RSGB.

The location is still under negotiation, but the station will be in a very prominent place within the 1 03 square miles of the City of London, and easily accessible to the public.

The GPO have granted the use of the callsign, GB2LO.

Equipment will be loaned by Messrs. K. W. Electronics Ltd. and will be operated by volunteers on the amateur frequencies in the 10, 15, 20, 40 and 80 metre wavebands. The society's public relations personnel will be on hand to explain the station and its function to visitors. Operation will be on single sideband only.

SPRING IS HERE !

We were delighted to snip the following from the price list of a well-known semiconductor manufacturer:

1N34A-C Geranium Diode 4s 6d Zenobia diodes, of course, cost more !

RADIO SPEEDS UP RAIL MAINTENANCE

With increased efficiency as the prime objective, British Rail Eastern Region have introduced a new system of v.h.f. communication between their London Area Electric Traction Engineer's mobile maintenance units and the overhead line depots at Romford, Cheshunt, Pitsea and Colchester, via a control at Romford, Essex.

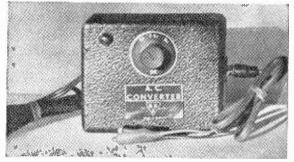
This system operates over an area bounded by London, Bishop's Stortford, Colchester, Walton-on-the Naze and the Essex Coast.

There are two fixed radio stations and aerials at Danbury in Essex and Highgate in Middlesex. Any signal transmitted from a mobile unit, all of which are on a common frequency, is received simultaneously at each aerial and, after automatic comparison for strength, the station receiving the stronger signal feeds it direct to Romford Control.

Here the switchboard operator can communicate with all mobile maintenance units and extend calls between selected extensions in overhead line depots to such units.

Each mobile unit is equipped with a receiver/transmitter which is operated by the car-starter battery carried by the vehicles. Incoming calls are heard on a loudspeaker mounted in the cab and a telephone handset is used for carrying on conversations.

VERSATILE POWER UNIT FROM R.C.S.



R.C.S. Products Ltd., 11 Oliver Road, London, E.17, announce the latest in their range of power units. It is called the "Plus Three" and provides three separate switched voltages of 6V, 7.5V and 9V d.c. at 250mA.

It is ideal for most types of transistor equipment including record players, tape recorders and radio receivers, and makes a good test bench power supply. It is housed in an attractive rexine-covered wooden cabinet measuring $4\frac{1}{4} \times 3\frac{1}{2} \times 2\frac{1}{2}$ in.

An indicator lamp is standard fitting to ensure that the unit is not left running when the equipment has been switched off, and an optional extra is a lead fitted with a din plug so that the unit can be used in conjunction with the Philips battery operated tape recorders. Also, the makers state that connection leads can be made up to individual specifications.

The "Plus Three" costs 57s. 6d, p.p. is 2s. 6d.

NEWS AND COMMENT...

THE R600 FROM ROBERTS' RADIO



The R600 is a f.m./a.m. transistor portable. A transformerless audio amplifier is employed and press-button switches are provided for waveband selection, automatic frequency control for the v.h.f. band and treble cut.

The circuit employs 11 transistors and 5 diodes and the output stage delivers power in excess of 1W to a 7 x $3\frac{1}{2}$ in. elliptical speaker.

A hinged and rotatable telescopic rod aerial is provided for f.m. reception, and a built-in ferrite rod aerial for the a.m. bands. Sockets are provided for use with a car-type aerial and an earpiece.

The receiver is housed in a wooden case covered with black leathercloth set off with silver trim and natural teak end-panels and is mounted on a ball-bearing turntable.

Approximate size is $11\frac{1}{4} \times 6\frac{1}{8} \times 3\frac{1}{2}$ in., weight is 5 lb. and the recommended price, including battery and purchase tax is 23 guineas.

HEATHKIT AT IDEAL HOME EXHIBITION

The feature of the Heath stand was a presentation in a domestic setting of music in the home. Items from their Hi-Fi range were demonstrated under simulated home conditions.

Hi-Fi audio equipment on view included a.m./f.m. tuners, both mono and stereo, amplifiers and speaker systems for reproducing sound from these sources and from record and tape decks: portable and car radio receivers, stereo record players and stereo tape-recorders were also shown.

BBC RADIO DURHAM

The BBC has placed an order with Bovis Ltd., of Harrow, Middlesex, for building work at the headquarters of BBC Radio Durham, Park House, Durham. Studio and ancillary accommodation will be formed here for this new local radio station, which is expected to be brought into service early this summer.

Radio Durham will transmit on 96.8 Mc/s in the v.h.f. band, from a transmitter at the BBC's Pontop Pike station. The area served will cover most of the County of Durham, except the western part, and will include the City of Durham, Sunderland, Bishop Auckland, Chester-le-Street and the greater part of Consett.

INDUSTRIAL TRAINING FILMS

A comprehensive catalogue of audio visual material for industrial and other training uses has been published by Rank Audio Visual Limited. In its sixty-four pages it lists a wide range of audio visual material on a multitude of training applications in industry, commerce and education.

It includes a total of 346 titles of 16mm. films, 8 mm. concept loop films, 35mm. filmstrips, and sound filmstrip kits. The catalogue is available free of charge from Rank Audio Visual Limited, P.O. Box 613, Woodger Road, Shepherd's Bush, London W.12.

NEWS FROM THANET

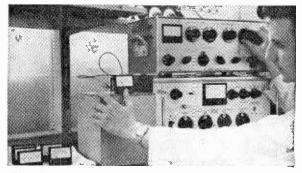
GB2MHE will be operated by the Thanet Radio Society at the Hobbies Exhibition run by the Rotary Club of Margate at the Lausanne School April 24–27. A.M. Phone on 80-40-20-15-10m 4 and 2m. Special QSL's. Contacts and reports will be appreciated. Dick Trull, G3RAD.

BBC RADIO STOKE-ON-TRENT

So that the start of the local broadcasting service for the Stoke-on-Trent area, on March 14, would not be delayed, the BBC brought into service a temporary low-power transmitting installation. This was on the site of the permanent transmitter, at Alsagers Bank, near Newcastle-under-Lyme.

Radio Stoke-on-Trent transmits on 94.9 Mc/s in the v.h.f. band. The local programmes are originated from the new BBC premises at Conway House, Cheapside, Hanley.

SIFAM METERS FOR AMPEX TAPE RECORDERS



The picture shows special "VU" meters for use in a new, portable professional tape recorder being tested at the Torquay factory of Sifam Electrical Instruments Co. Ltd.

Sifam have received a large initial contract from Ampex Electronics Ltd., Reading, Berks., for these meters for fitting to the new Ampex AG–20 battery-operated audio recorder. Built into a modified Sifam "Director 24" instrument case, the meter movements have specially designed ballistics based upon the stringent USA Standards Institute specification for volume measurement of electrical speech and programme waves.

The meters were subjected to severe tests both in the UK and by the Ampex parent corporation in the United States. The most dramatic of these was an environmental test of the recorder in which an interview was taped by skydivers from the British Green Jackets Parachute Club during free fall from an altitude of 12,000 feet.



HE t.r.f. type of receiver avoids the more complicated circuits and alignment difficulties of the superhet, yet will normally give good loudspeaker volume plus a reasonable selection of stations. This circuit has five transistors in a 6-stage reflexed arrangement which is sensitive, easy to build, and provides excellent volume from an economical single-ended push-pull output stage.

Figure 1 shows the circuit, and a personal phone or headphones may be used to test it in three sections, during construction. This ensures that progressive wiring is correct. Tr1 acts as r.f. amplifier, with regeneration through TC1 controlled by the potentiometer VR1. R.F. is blocked by the r.f. choke and passes to diodes D1 and D2, the demodulated signal passing through L1 to Tr1, which furnishes audio signals across R1, taken through C6 to Tr2. When the circuit is wired as far as C6, phones from C6 to battery positive give moderate phone volume from some local stations, while tuning and regeneration will be found in order if this section is working correctly.

Tr2 and Tr3 are audio amplifiers, connected to obtain d.c. stabilisation of their working conditions.



For example, assume Tr2 collector current is too high. The voltage drop across R4 rises, moving Tr3 base positive and Tr3 emitter current falls, reducing the voltage drop across R6, and moving Tr2 base positive through R3, to restore working conditions. Should Tr2 collector current be too low, the reverse arises. With Tr3, excess collector and emitter current increases the voltage drop across R6, shifting Tr2 base negative, increasing Tr2 collector current and the voltage drop across R4, which in turn moves Tr3 base slightly positive, to restore conditions.

With Tr2 and Tr3 added, phones from Tr3 collector to battery negative should give more than enough volume, with good quality of reproduction, thereby showing this section is in order. Transformer T1 drives Tr4 and Tr5 in a popular and economical push-pull circuit, operating directly into a 75Ω speaker.

Components

There is some latitude in transistors and some other items, but miniature transistor receiver type components have to be used throughout. All resis-

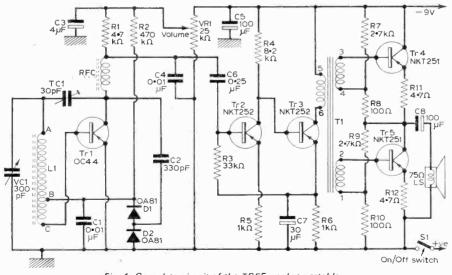


Fig. 1: Complete circuit of the TRF5 pocket portable.

tors are 10% (silver band) except R7, R8, R9 and R10, which must be either 5% (gold band) or selected with a reliable meter for accuracy. VR1 is a midget pot with switch and actual results are the same with $10k\Omega$ or 20k Ω . VC1 is a midget solid-dielectric (300pF) but there is space for a midget air-spaced capacitor, if to hand, and 365pF or other larger value can be fitted.

Various transformers for single-ended pushpull, for use with OC71 and 2xOC72, or OC81D and 2xOC81, or similar transistors, are satisfactory for T1. The ratio is generally about 7:1 + 1, to 3.5:1+1. Tags are numbered in Fig. 1 and a wiring plan shows location of tags or pins and must of course be for the actual transformer, if different from that listed.

The speaker is a 75-80 Ω 2in. or similar unit, but 35 Ω units are also in order, while a 25 or 35 Ω speaker is particularly suitable for 2xOC81 or similar transistors. The receiver is easily accommodated in a plastic case which is approximately $5\frac{1}{2} \times 3\frac{1}{4} \times 1\frac{3}{4}$ in. external dimensions.

Chassis and Case

This is 5 x 3in., $\frac{1}{16}$ in. paxolin, with all components except VR1 and the speaker mounted on the back as in Fig. 2. Cases of the type mentioned have three projections inside, tapped 6 B.A. Bolts in holes X, Fig. 2, secure the finished receiver in its case. These three holes can be positioned by cutting thin card 5 x 3in., placing it in the case, piercing over the tapped holes, then using the card as a template for drilling the paxolin. Should any holes

be inaccurately placed, they can be elongated with a small round file. The two holes marked S are for bolts with extra nuts, which secure the speaker. Somewhat similar cases are made with tapped holes to fix a speaker inside, and two flexible leads can then run from speaker to receiver.

The speaker opening, Fig. 2, is about 1[‡]in. in diameter, to clear the speaker. As many holes as possible should be drilled before fitting any components to the panel.

Ferrite Rod Aerial

This has 88 turns of 26s.w.g. enamelled wire,

side by side on a $5 \times \frac{3}{8}$ in. ferrite rod. Glued paper is wound round the rod, and the wire fixed at A with tape, adhesive, or cotton. After winding 76 turns, the small loop B is made, and winding continued in the same direction for a further 12 turns, the wire being fixed at C.

A loop of some insulating material, such as cardboard, leather or plastic is cut to go round the rod, and drawn tight with a bolt, which also goes through the panel. Extra nuts or a spacer lifts the rods so that the winding clears the trimmer TC1. Note that a wire also passes from the moving plates of VC1 through the panel to the "earth" of battery positive circuits the other side.

If the receiver is to be tested in sections as mentioned, insert components up to C6.

The underside of the panel (or front when the receiver is in its case) is shown in Fig. 3. VR1 is fixed with a small bolt. The simplest method of wiring is to use 26s.w.g. or similar bare tinned

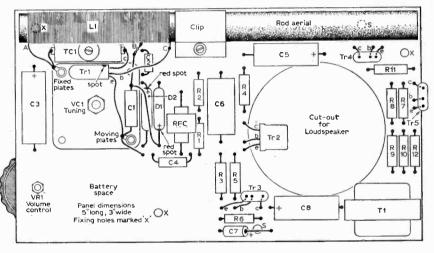


Fig. 2: Component layout. The volume control VR1 is mounted on the reverse side (see Fig. 3).

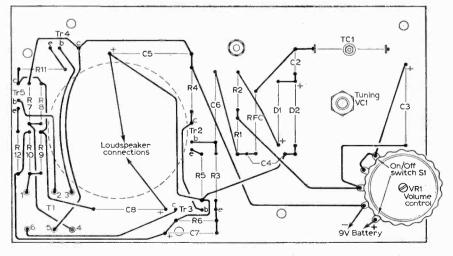


Fig. 3: Underside wiring of the paxolin panel.

copper wire, with 1mm red sleeving for "earth" and black sleeving for negative line. Joints (especially for transistors and diodes) are soldered rapidly, the iron being removed immediately the joint is formed.

To test the first stage, connect phones from the free end of C6 to battery positive and unscrew TC1. Set VR1 at about half its travel. Tune in a signal with VC1 and screw down TC1 until the receiver just begins to oscillate, backing off VR1 slightly should then control regeneration. A meter in one battery lead should show a current of about 1-1.5mA, falling by about 0.2mA on tuning in a strong signal, due to increased base bias from the diodes. Regeneration becomes less easy towards the low frequency end of the waveband, so TC1 can be readjusted slightly later, for best over-all reception.

During normal use, VR1 must be adjusted as a regeneration control, not as a simple audio volume control. Rotating VR1 towards maximum builds up volume, until oscillation begins. Sensitivity is very high just below this oscillating point. Should no results be obtained, connections in this part of the circuit should be checked.

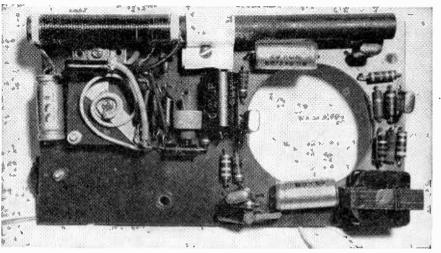
When Tr2, Tr3, and associated components

have been added, it is worth checking results by connecting phones between the collector of Tr3 and the battery negative line. This corresponds to points 5 and 6, Fig. 1. Volume on local signals should be very great, and more stations may be heard. There should be no audio distortion. If results are poor or distortion has arisen since adding Tr2 and Tr3, check resistor values and connections here.

Current drain with Tr1, Tr2 and Tr3 in use depends somewhat on transistors, but can be ex-

🖈 components list

Resiste	ors:	Capa	acitors:	
R1	4·7kΩ	C1	0·01µF 150V	
R2	470kΩ {	C2	330pF 150V	
R3	33kΩ 4.000	C3	4µF 25V electrolytic	
R4	$8 \cdot 2k\Omega$ 10%	C4	0·01µF 150V	
R5	1kΩ	C5	100µF12V electrolytic	
R6	1kΩ	C6	0·25µF 150V	
R7	2·7kΩ)	Ç7	30µF 6V electrolytic	
R8	100Ω 5%	C8	100µF 12V electrolytic	
R9	2·7kΩ (^{> 3} %	VC1	300pF miniature	
R10	100Ω]		variable	
R11	4.7Ω 10%	TC1	30pF trimmer	
R12	4.70			
VR1	25kΩ pot. with			
switch		Indu	ctors:	
		L1	see text	
Semico	onductors:	RFC	miniature 7.5mH r.f.	
Tr1	OC44		choke	
Tr2	NKT252	T1	Single ended push-pull	
Tr3	NKT252		transformer 7:1 + 1	
Tr4	Tr4 NKT251 matched		(Fotiphone L442 or	
Tr5	NKT251 ∫ 111att	sneu	similar) see text	
D1	OA81			
D2	OA81			
Miscellaneous:				
Ferrite rod, wire, solder, paxolin 5 x 3 x $\frac{1}{16}$ in., 75 Ω speaker, case to suit, knob, dial, 9V battery.				



Internal view of assembled receiver (less loudspeaker).

pected to be around 3-4mA. Should there be any fault, correct this before wiring the output stage.

Output Stage

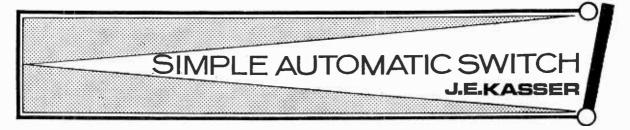
As mentioned, connections to T1 in Fig. 3 are for the listed transformer, and tag 1 is red. Other transformers have tags in different positions, but are equally suitable.

Resistor values R7 to R12 are suitable for OC72's, OC81's, and many similar transistors, in addition to those listed. The output transistors are best purchased as a matched pair. It should then be found that the voltage at the junction of R8 and R9 is about half the supply voltage. This will not be so with unmatched transistors in Tr4 and Tr5 positions or with an error in value in R7, R8, R9 or R10. In practice, it is usually found that results are satisfactory if transistor voltages lie within about 20% of each other, if the transistors are otherwise matched.

Current taken by the whole receiver should be about 8-10mA, rising to 12-20mA peaks with good volume. Should current be around 8-10mAbut extreme distortion spoil results after adding the output stage, check connections to T1. In particular, leads to one half secondary may need to be reversed. Should current be much under 8mA, with weak, distorted reception, check that a mistake is not made in reading the values of R7-R11. Should current be much over 10mA, with no signals tuned in, but reception nevertheless good, R8 or R10 may be too high in value, or R7 or R9 too low. This is not expected with 5% resistors.

Loudspeaker Mounting

There is space for the usual 9V miniature battery, and receiver leads should have correct positive and negative clips. If the speaker is bolted to the paxolin panel, a piece of thin felt, thick blotting paper, or similar 'material with a central hole can be placed between speaker and cabinet, to prevent vibration sounds. The tuning scale is drawn on card, afterwards cemented to the case front. A knob of fairly large diameter is most suitable for tuning.



HIS simple but useful device is an all solid state switch, i.e., it has no moving parts to go wrong, such as relays etc., although it can easily be made to utilise a relay if desired. However, the unit as described here may be used without a relay to control load currents of up to 2.5 amps. The unit can be used with a variety of input circuits for a wide range of applications requiring a switch which is not self-latching, i.e., is only activated as long as the original trigger input lasts.

No signal

The circuitry is very simple, but a brief description might prove useful for those not familiar with this type of device. When there is no signal applied to the input (i.e., the base terminal of Tr1) Tr1 is switched off and is in a non-conducting state. Current flows through the potentiometer formed across the supply lines by R1, R2 and R3. Because of this flow of current, the base terminal of Tr2 is forward biased due to the voltage drop across R3, and thus Tr2 is conducting, or is switched on. The collector current of Tr2 is controlled by VR1, while R4 functions as a limiting resistor to set the limit for maximum current through the transistor. Since Tr2 is conducting and the emitter drawing current, and because of the direct connection to the base of Tr3, Tr3 is conducting also and thus current flows through the load, its maximum value being approximately $h_{fe} \times I_b$.

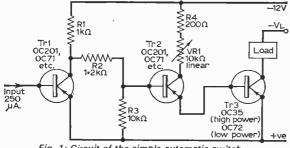


Fig. 1: Circuit of the simple automatic switch.

The choice of transistor for Tr3 is made according to the power dissipation required. In the prototype it is an OC35 for high power applications, The prefix VL is the load supply voltage and this can be made any value within the V_{MAX} of the transistor Tr3. It can, in fact, be connected to the 12 volt negative rail if required.

Signal applied

If an input signal is applied to the base of Tr1 the transistor will conduct, and the potentiometer network (R1, R2 and R3) is now starved of current, the current now flowing through the transistor Tr1. The effect on Tr2 base is that it drops to a potential of

practically zero volts and thus, being robbed of its forward bias, transistor Tr2 cuts off and ceases to conduct. Since Tr3 base potential is more or less dependent upon whether Tr2 conducts, i.e., it is connected directly to Tr2 emitter, it (Tr3) now ceases to conduct and thus cuts off. Obviously if Tr2 is not conducting then the potential presented at Tr3 base by virtue of the current flowing through Tr2 emitter is removed. Since it was this bias which caused Tr3 to conduct, once Tr2 cuts off and ceases to draw current, then Tr3 also will cease to conduct and will become cut off. It is plain that with Tr3 not passing any current, the load will be robbed of

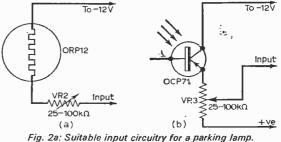


Fig. 2a: Suitable input circuitry for a parking lamp. Fig. 2b: The same circuit using a photo-transistor.

current too and will thus switch off the device to which it is attached. This means that current is flowing in the load circuit as long as there is no input to the base of Tr1. Directly a signal is applied, Tr3 will cut off, and thus no current will flow in the load.

Transistors

Silicon transistors were used in the prototype mainly because they were to hand, however, there is nothing really critical about the circuit and most transistors should work. It should be borne in mind, however, that changing the transistors could easily vary the switching sensitivity.

Parking light

This type of circuit would be ideal as a parking light if the load was furnished by a suitable lamp and the input circuit triggered by a photocell or photo-transistor as suggested in Fig. 2. The potentiometer regulates the sensitivity of the device and, if preferred, Trl might be replaced with a photo-transistor direct, such as the OCP71.

Burglar alarm

The photo-transistor will also prove very useful if a burglar alarm is envisaged, since the breaking of the light beam will switch on the alarm. Other uses include any sort of alarm or level detector, and the unit will replace a relay but only with one set of terminals. The actual switching speed is dependent only on the characteristics of the transistors used.

repairing radio sets

PART 2 H. W. HELLYER

Last month we dealt with the basic operation of the transistor. We go on to discuss their identification, handling and replacement

Handback the trouble of servicing transistorised equipment lies in the difficulty of handling small and often unfamiliar parts. It is all very fine for the professional to whom experience has given confidence and who, let it be whispered, may have access to an immediate replacement for the part he damages by haste or clumsiness! For the ordinary chap, however, transistor radio repairs pose a very real problem.

IDENTIFICATION

The first requirement is identification. There are literally hundreds of different sorts of semiconductor devices already in use. Components, likewise, have proliferated; and in doing so have shrunk to very

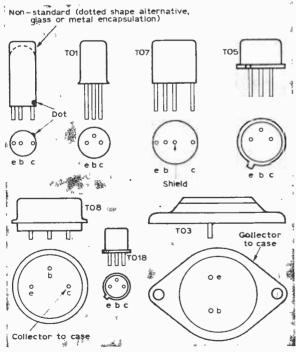
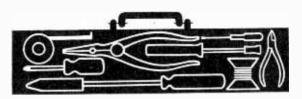


Fig. 11: Popular encapsulation shapes, with bottom view of electrode connections. Examples: Non-standard; OC71, OC74, OC81, OC82, TO1; OC45M, OC81M; TO7; OC170; TO5: 2G401, NKT162; TO18: AF127; TO3: OC26, AD140; TO8: NKT303.



small proportions. A magnifying glass, tweezers and a pencil-bit soldering iron are obligatory. no longer optional, servicing aids.

Because of this problem of identification much of the space available for this article has been taken up by diagrams which may seem superfluous to our more experienced readers. Figure 11 shows the actual shape and size (to scale) of the more popular transistors, with the electrode arrangement of their bases. The code is c collector, b base, and e emitter, with the letter s denoting screen where this applies. On some of the power transistors the collector is internally connected to the outer casing, which forms the collector connection, and some care must be taken when dealing with these for the mounting is often arranged so that the maximum heatsink operation takes place. A very thin film of insulant is fitted between the outer casing and the plate on which the transistor is mounted, giving maximum heat transference, but electrical insulation. Obviously this must be treated with great care. A split, a crease, or even a slight sideways movement during reassembly, may cause a shorted electrode and irrevocable damage.

Similarly, insulating sleeves, bushes and washers will be found that serve the same purpose. to keep the wire pins away from the main chassis while permitting electrical connection. When removing one of these power transistors always take great care to retain the bits and pieces as these *must* not be omitted later.

REFITTING TRANSISTORS

When refitting such a transistor a smear of silicon grease on the mica, porcelain or other insulant will aid heat transference and help prevent cracking. Remember that there is often a good deal of heat to be transferred. A finger on the casing of the output transistors of a car radio, for example, will soon convince one that these are not "cold-running" devices. The important factor is the ambient temperature. In the specifications for transistors one finds the power output given for a particular ambient temperature, with the symbol T_{amb} denoting this figure and perhaps a symbol T_{case} or perhaps twice as much denoting the temperature at which the outer casing is designed to operate. The other relevant operating currents depend on this rating and will be drastically altered if it changes.

To emphasise this point Fig. 12 shows some of the heatsink mountings in common use. Note the insulating bushes, etc., and always remember that good thermal contact *must* be made. Even a bit of swarf, or a dirty surface beneath the mounting, will be enough to raise the operating temperature perhaps beyond safety limits. In Part 1 last month Gordon J. King dealt with the phenomenon of thermal runaway and I need only add that in some receivers it is a very real threat so that all efforts must be made to keep operating temperatures within the design limits.

An example would be the modification of a receiver to use perhaps a transistor preamplifier stage. If this is fitted near a heat-generating source such as a valve or power transformer great care is needed to remove the heat before it can do any damage to the vulnerable semiconductors.

WATCH SPECIFICATIONS

I apologise for this Jeremiah-like note, but bitter experience of certain car radios which had their output transistors mounted on the back of the case inviting fitting methods that put them in areas of a very poor ventilation—sometimes right in the air-stream of the heater of the car—taught the author that makers' parameters must be respected if breakdown is to be avoided.

Even the simple heatsink, the brass or copper clip that apparently floats in mid-air, is a vital part of the design and should not be omitted. A popular trap is the temptation to "open" these with a knife or screwdriver blade to facilitate removal of the transistor. When the new transistor is fitted, the case is loose within its heatsink, and if a little extra trouble is not taken to tighten this thermal contact operating conditions may be altered. Pinch the curl of the heatsink slightly before re-insertion of the transistor, but make sure that the pinching is even, i.e. over the whole length of the casing, so that no heat spots are caused. If the original was bolted to the chassis, then do the same with the new fitting, even if it is a little more trouble.

Always remember that manufacturers work to very tight costing schedules. The fraction of a penny that the heatsink costs may be a significant figure when multiplied by mass-production quantities. It was not put there for fun!

LEAD-OUT WIRES

Another point is the lead-out wires on some semiconductors. For r.f. and i.f. transistors, particularly in frequency-modulated receivers, the length of the lead can be important. When fitting a new transistor try to keep to the original dimensions even if this is a bit more trouble to do. In particular try to simulate the routing of the wire ends, do not cross collector and base leads just because it makes a neater fitting, do not bend wires too close to the capsule, and avoid running screen connectors to the nearest convenient place. The specific point that comes to mind is that of mounting a transistor on the opposite side of a printed circuit board from which it was removedoften easier to do. Nine times out of ten you may get away with it; the tenth time, however, there will be an increase in noise level or the chance of instability.

Microphonic transistors may seem a contradiction in terms. But longer leads than necessary on replacement transistors can cause this trouble, which again emphasises the need to keep leads to the right length.

On the other hand, the mounting lead is some-

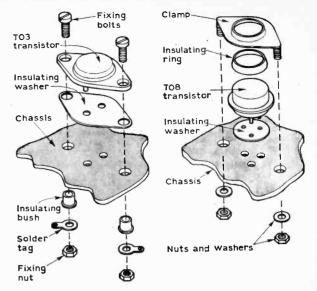


Fig. 12: Power transistor heat-sink mountings. It is important that the electrode pins do not touch sides of clearance holes and that good contact of the transistor with insulating washer and the latter with chassis is ensured.

times employed as a primitive sort of heatsink. This was a popular technique in fitting semiconductors in some television receivers. The wire ends of silicon rectifiers and other diodes were twisted into small loops and the components wired to tag strips. So cutting leads shorter simply invited overheating. The curl was to provide a mechanically stable mounting and had nothing to do with inductance!

Mechanically stable mountings—how important that phrase can be. The encapsulation of tiny components often means delicate leads in confined spaces, and to succumb to temptation and bend these leads sharply is to ask for trouble. Sharp bends should be avoided. Once again, the emphasis is on the proper tool for the job. A good pair of fine-nosed pliers or strong tweezers are part of the standard equipment of anyone wanting to work on transistorised equipment.

SOLDERING

Soldering transistor leads is perhaps the most difficult part of the job. To attempt this task with a clumsy bit is to invite disaster. We have already pointed out that heat is a danger—both in operation and in handling. A fine bit, just enough heat exactly where it is wanted, and the use of some form of heat shunt should be standard procedure. In emergency quite simple heat shunts can be made. Even a twist of wire around a transistor lead, between iron and component can be of some help.

Correct preparation of the job is more important with transistorised equipment than with receivers using valves. The joint to be soldered should be cleaned, the printed circuit board prepared, and any fixing hole thoroughly cleared (a match-stick inserted into the hole to clear it immediately the solder is molten is most useful) before the transistor itself is brought anywhere near the board. Soldering should be quick, direct and efficient. The greatest mistake is to use an inadequate iron for a greater length of time than is desirable. You will melt the solder, true, but you could possibly melt a few components also in the process!

SMALLER ITEMS

Some of the problems of repair arise from the disparity between the original components and whatever replacements are available. There has been a steady shrinking of components—and, despite oldfashioned opinion, a steady increase in quality. This is underlined by the current attention given to integrated circuits. Fortunately my brief stops short at the discrete bits and pieces more often associated with the common transistor radio.

Removing these smaller items very often means damaging or destroying them. It is a hard fact, but one that must be faced. It is thus more than ever important to make *in situ* tests rather than to remove components. This procedure was stressed by Gordon J. King and the theoretical tests need not be repeated here. Some of the practical points arising from them are, however, worth a few lines.

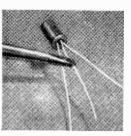
First—servicing transistor radios needs a totally different approach from previous methods used for dealing with valved equipment. Careful diagnosis and correct measurement are much more important. While it is easy and the common practice to remove and replace a valve for test, and often quicker than taking the measurements that would prove its failure, the opposite situation holds with transistor radio testing. Therefore it is vital to know what we are testing, what readings to expect, and how to prove the fault without unnecessarily disturbing the circuit.

But there is a catch here. Suppose a transistorised circuit has broken down and preliminary inspection reveals a burnt-out resistor, what then? A logical approach is needed. We must ask ourselves Why? and indulge in a little theoretical conjecture before grabbing the tools. What could cause the failure; what secondary symptoms would we expect to find; what "cold" measurement tests will help us to prove the fault before we switch on again?

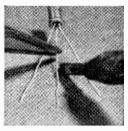
EXAMPLE

To take an example, the output stage burnout of a high quality and expensive tape recorder. The obvious signs were blackening of two emitter resistors, indicating that the output transistors had been passing heavy current. These were low-ohm components and their exact value had to be observed. But preliminary tests could be made with temporary resistors, all "cold" measurements giving readings that appeared normal. By hooking up several seriesparallel "christmas-tree" arrangements, the working values were simulated. (This is where a good resistor/ capacitor substitution box is a very handy workshop aid. The actual components do not need to be fixed into place; flyleads serve the temporary purpose.)

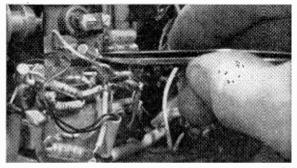
Applying power and taking measurements of current and voltage we found that the output transistors had indeed been damaged. Input conditions, at d.c., were apparently normal.



A simple pair of tweezers aids in the handling of small parts, such as transistors.



A suitable heat-shunt such as a pair of long-nosed pliers between capsule and solder joint prevents damage.



Removing transistor from congested circuit board is made easier by tweezers with blade end.

Now comes the trap. If we replace the output transistors and damaged components, then resume operation, all seems to be in order. But in a short while the equipment is returned to us with the selfsame components burnt out. Why? The answer, in this particular case, was failure of a small-signal transistor some *five* stages earlier. This was permitting larger signal current swings than the design parameters should have allowed. The intermediate stages could handle this overload, which gradually increased toward the output section. The output pair handle quite heavy currents, and the large input signal swing drove them way beyond their limits on a strong signal. The trouble was cumulative and until we got to the root of it by more careful measurements under dynamic rather than static conditions the fault could not be proved. Now we fly straight toward the known culprit and replace the AC128 with an AC153.

CARE NEEDED

This example is given only as a warning that testing needs to be more careful than we may have been accustomed to in previous times. A valve voltmeter is now an accepted part of the bench rig, in general rather than intermittent use. An oscilloscope is even more useful for taking spot measurements of incoming signals without disturbing the circuit. But even where the only gear one has is a multimeter, the need to use this diligently becomes obvious. If a manufacturer says there is $2 \cdot 1V$ at the base of a transistor he means this—and the difference of even point one of a volt can be significant. Gordon J. King is treating the important subject of signal testing more fully in the next part. His advice is well worth studying.

From the practical point of view, and even at the risk of repetition, we must stress the dangers to transistorised equipment in making the tests themselves. A careless probe can damage a transistor irrevocably in less time than it takes to curse one's clumsiness. If we accidentally slip and short-circuit a transistor's base to collector, or, in some cases, its emitter to chassis, we can write off that transistor almost immediately. If we apply too great a signal from our generator or other source, small-signal stages in the earlier part of the circuit will suffer, and again transistors may saturate on negative peaks (assuming p-n-p types with positive chassis). Thermal runaway can occur when leakage current rises, a rise in junction current causing more heat, causing more current, and so on.

HIGH IMPEDANCE

It is essential that we do not bring about these conditions by our tests. The volt-meter, for example, should be at least 20,000 ohms/volt to give accurate readings down to one-tenth of a volt or even less without disturbing the circuit. This is because to read these voltages one must switch to a low-voltage range, and the meter imposes a greater load on the

lower ranges. Hence the very obvious advantages of the valve volt-meter, which has a very high impedance.

A.C.

But the valve voltmeter is often a main-powered item, and here another snag arises. Leakage currents can be caused if unearthed test equipment is used or if earthed equipment and test gear is used with phase-change differences in wired connections. Figure 13 shows the connection of a signal generator to an a.c. operated radio or amplifier. Both the chassis of the signal generator and the set should be earthed, and this means properly bonded from the metal parts, not just from the earth connector of a threewire lead.

One reason is that the dotted capacitor shown is actually a distributed capacitance between the windings of the transformer and the core, and perhaps across any r.f. filter that may be included in the mains circuit of the test gear. Connecting the test gear to the set, even via the isolating capacitor C2 whose job is to prevent transients that can also damage transistors, does not remove the danger as the coupling is electrostatic. If we now apply a soldering iron to the set, even with the set switched off, and if the metal bit of the soldering iron itself is not adequately earthed, a fairly large current can flow from the iron to earth via the transistor. Soldering a base connection of a radio with an unearthed iron is simply inviting trouble. So the prime rule, before commencing, is to make sure that all the equipment is earthed to a common point. Five minutes extra in setting up before starting work can save quite a bit of trouble later.

Any output meter used should be of correct load

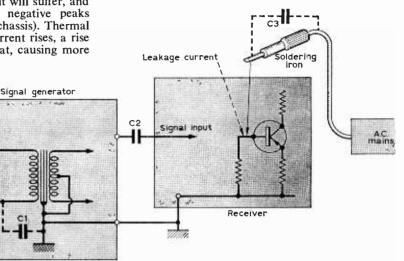


Fig. 13: Leakage currents due to electrostatic charges between mains wiring and chassis can be transmitted to the receiver from test gear, despite isolating capacitors. The great danger is the use of an unearthed soldering iron, which can cause heavy leakage current to pass through transistors to chassis and back to earth.

impedance. Conditions with transistor output stages in respect of possible damage are virtually opposite to valve stages. A short-circuit across the output will cause breakdown. A load lower than that required in the design will draw extra power from the output circuit. Hence the need to observe correct loading when fitting extension loudspeakers. Hence also the reason that some amplifiers are rated at higher power output for lower impedance loudspeakers.

Finally, any ohmmeter used will be powered by a small battery. On the \times 100 ranges, this can be several volts more than the circuit may handle. This is a point that should be considered when testing.

TO BE CONTINUED

★ FAULT FINDING CHART No. 2

The fault finding chart presented with this issue is to be used in conjunction with last month's chart. This month the chart, however, deals with diagnosis. The two charts together form a comprehensive guide to fault diagnosis and tracing, and will be found useful either on their own or used in conjunction with the new series of Repairing Radio Sets.



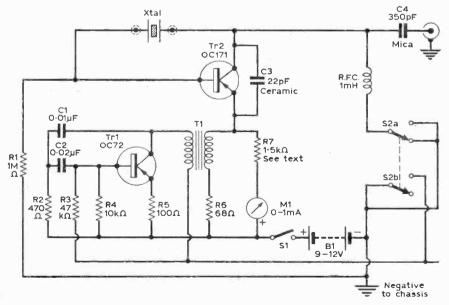
DURING odd sessions of experimentation in the workshop, the writer came across some stubborn crystals that would not easily oscillate in conventional valve circuits, but would sometimes do so in transistorised circuits. Accordingly, an attempt was made to put together a simple transistorised oscillator, using the minimum of parts, that could be used for sub-standard crystals. The circuit shown works well in spite of the fact that no tuned circuits are used.

For prolonged use a fairly large 9 volt battery should be used since the drain of the oscillator alone is about 10 milliamps, whilst it is double this when the modulator is in use. A 12 volt battery may be used provided attention is paid to the dissipation of the audio transistor used.

It is preferable to use a meter, which may be either a 1 or 2mA unit. A meter does give one an idea if the crystal is functioning, and some indication of its activity. To set up the meter, use, initially, a $2k\Omega$ potentiometer and set this to give almost f.s.d. with the hottest crystal in stock. A fixed resistor of that value (R7) is then soldered into the circuit. The type of modulation is simple and the low level; nevertheless it is very effective. The wave shape should ideally be sinusoid, and if the constructor is keen on this he can insert, temporarily, a $15k\Omega$ potentiometer in place of the 470Ω resistor shown in the circuit diagram, and adjust it to give a good wave shape. However, the note produced may not be as distinctive and pleasing as that obtained at a sacrifice in wave-shape. In the prototype, and a copy that was built later, the most suitable note (to the writer's ear) was one of a little less than 1800c/s.

Construction

A glance at the circuit diagram shows that, contrary to usual practice in p-n-p transistor circuitry, positive is not at ground potential. Battery negative is grounded to the chassis and covering box, and the on-off switch is in the positive line. It is worth while cutting the three holes for the commonest valveholders, as this enables most crystal types to be



accommodated.

The two-pole switch shown in the diagram was a two-pole six-position wafer switch, as it happened to be handy. The unused tags are used for supporting components. If this system is copied, make sure the stop lugs on the switch are bent into position, so that the switching range is restricted to two positions only. Likewise, the unused pins on the valve-holders may also be put to good use. Quite apart from driving the first stage of a transmitter. there are other uses for this useful unit, and most

Fig. 1: Circuit diagram of the modulated crystal marker.

-continued on page 32

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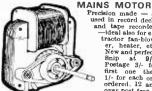
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Each kit comprises seven items-Choke, 2 tube ends, starter, starter holder and 2 tube clips, with wiring instructions. Suitable for normal fluorescent lubes or the new "Gro-lux" tubes for fish tanks and indoor plants. Inx" tubes for fish tanks and indoor plants. Chokes are super-silent, mostly result, mostly result, filled, Kit A-15.20 w. 19/6, Kit B-30.40 w. 17/6, Kit C-80 w. 12/6, Kit D-125 w. 22/-Kit D-65 w. 12/6, Kit MF1 is for fill, Sin, and 121n, miniature tubes. 19/6, Poetage on Kits A and B 4/6 for one or two kits then 4/6 for each two kits ordered. Kits C, D and E 4/6 on first kit then 3/6 for each kit ordered. Kits MF1 3/6 on first kit then 3/6 on each two kits ordered.

MAINS TRANSISTOR POWER PACK

PACK Designed to operate transistor sets and amplifiers, Adjustable output 6 v., 9 v., 12 volts for up to 500 mA. (class B working), Takes the place of any of the following batterise; PP1, PP3, PP4, PP6, PP7, PP9, and others. Kit comprises: mains transformer rectifier, smoothing and load resistor, condensers and Instructions. Real snip at only 16/6, plus 3/6 postage.



Precision made — as used in record decks and tape recorders —ideal also for ex-first one then 1/- for each one ordered, 12 and over post free.

RELAY SWITCHES. These enable micro switches, RELAY SWITCHES. These enable micro switches, delicate thermostate or other low current devices to control up to 30 amps.—ideal to switch thermal storage heater— motors, etc., made by the famous A.B.I. group these are listed at 220 each—you can buy if yoourry at a very keen price or 330/6 each and we will include diagrams and data. Mounted on panel size approximately 6 x7 x2 in. deep.

THERMOSTATS



By the second second

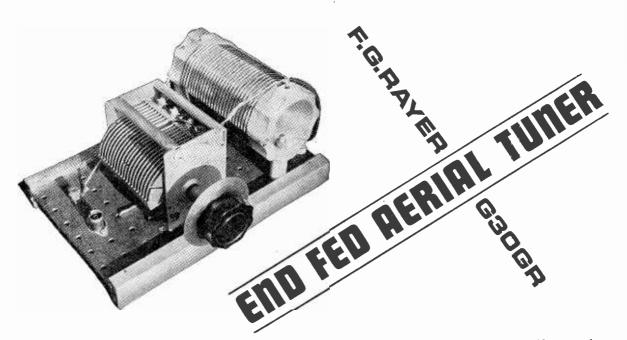
(Dept. P. W.) 102/3 TAMWORTH RD., CROYDON, SURREY (Opp. W. Croydon Stn.) also at 266 LONDON ROAD, CROYDON, SURREY S.A.E. with enquiries please



30



BATTERY OPERATED TAPE DECK With Capstan control. This unit is extremely



COUNT of amateur stations contacted on 80 metres shows that over half are using some form of end-fed aerial, and that a large percentage of these aerials are near a $\frac{1}{2}$ -wavelength long, that is, roughly 125-130ft. Many kit and commercial transmitters have a pi output circuit which should work into a fairly low impedance circuit, and it is commonly found that a $\frac{1}{2}$ -wave end-fed aerial cannot be operated from these transmitters unless a tuner is added. The tuner described here is extremely simple and can be assembled in a very short time. It is suitable for 150 watts, but could be scaled down for lower powers.

The circuit is shown in Fig. 1. L1 is tunable to 80m, and can be 26 turns of 18s.w.g. enamelled wire, on a ribbed former $2\frac{1}{2}$ in. in diameter, the winding being spaced to occupy about $3\frac{1}{2}$ in. (An easily obtainable Eddystone former of this size can be purchased.) Other coils of about equal inductance should be equally satisfactory. The coupling loop L2 is 3 turns of stout, well insulated wire, overwound on the earthed end of L1.

For tuning, a 150pF or similar capacitor is used, and it should have plate spacing at least equal to that of the transmitter p.a. anode tuning capacitor. The capacitor actually fitted was a 2-gang component with sections wired in parallel. Non-miniature receiver type capacitors will do for low power only. If the capacitor sparks over in use, this shows its spacing is too small, for the power and aerial employed.

LAYOUT

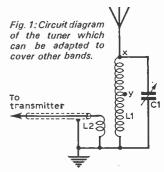
The tuner can be built on a piece of varnished hardboard or pegboard about $5\frac{1}{2} \times 9in$, with wooden runners to give clearance for fixing bolts etc., with components placed as in Fig. 1. A coaxial socket was used for connecting up the transmitter. A standoff insulator or insulated terminal is provided for the aerial. The aerial lead itself should be well insulated, by passing it through sleeving, if necessary.

Many transmitters have a coaxial socket for output. The connection between the transmitter and tuner can then consist of a piece of 75Ω transmitter grade coaxial cable with a coaxial socket each end. It is as well to place the tuner near the entry point of the aerial, but within reach, so that it can be adjusted.

AERIAL LENGTH

An aerial which is a $\frac{1}{2}$ -wave at about the middle of the 80m band is approximately 128ft. long, although the actual length is often increased to as much as 138ft., because this is a multiple of $\frac{1}{2}$ -waves on some higher frequency bands, and may be convenient for multi-

band operation. This includes the section. horizontal down lead, and connection to the tuner. Height, bends, and other features also modify the effective length. The aerial may be 14s.w.g. hard-drawn, or 7/26 or similar covered aerial wire. All joints should be soldered. Signal strength is



increased by having the whole as far from earthed objects as possible.

If the receiver has a 75Ω input and a signal strength meter, the aerial tuner can be adjusted by observing the strength of some station tuned in. It should then be possible to load the transmitter pi output circuit into the tuner, without changing the tuning of the latter. In other cases, it may be found that the tuner has to be adjusted, as the setting of C1 considerably modifies loading on the transmitter. If a 75Ω non-inductive dummy load is available, a check can be made by loading the transmitter into it. Then connect the aerial tuner instead, and adjust it for similar loading, with the transmitter tuning untouched.

Another method is simply to adjust the aerial tuning and pi output capacitor of the transmitter until the p.a. anode current is at the wanted loaded figure, with the p.a. capacitor dipped for minimum current. If this is done, the same loading can be achieved with a number of settings of the aerial tuning capacitor and pi output capacitor. These correspond to different impedance conditions in the coaxial line from transmitter to tuner, but have no practical result on efficiency, as can be checked with a field strength meter.

OTHER BANDS

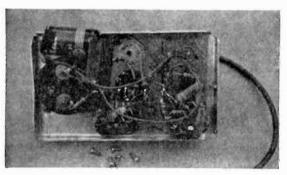
As an end-fed wire is easily used for other bands, the top half of L1 may be shorted out, for 40m. (Join X and Y in Fig. 1.) A comparison of signal strength showed no difference if the 80m coil were used in this way, or a coil wound for 40m only was substituted.

For still higher frequencies, relatively few turns are needed, so it was decided to employ a separate coil and capacitor. Using the same size former, a 15/20m tuner had 8 turns of 14s.w.g. wire, occupying $2\frac{1}{2}$ in., for L1, and 2 turns for L2. A 100pF capacitor was sufficient to tune the coil to resonance.

The tuned circuit naturally provides some harmonic suppression. In addition, the transmitter pi output circuit can now work into the low impedance

MODULATED CRYSTAL MARKER

-continued from page 28



Internal view of the modulated crystal marker.

constructors interested in this type of unit will already have thought of them.

If the valveholders are used for both crystal and components, it is mandatory that the vacant sockets be plugged with sealing-wax or plastic cement. HowFig. 2: Layout of the tuner used in the prototype. This is uncritical and other should prove equally satisfactory.

coaxial line, and this further reduces any harmonics which may be present. If a standing wave indicator or harmonic filter should be available, these can be included in the coaxial line. Tuner adjustment can then be for the minimum s.w.r., and this is also necessary to match the harmonic filter impedance, if used. When a filter or s.w.r. indicator is not used, the presence of standing waves in the coaxial line has no practical result on the signal radiated from the aerial. This is because the line is short, and the transmitter pi output can always perform satisfactorily with some standing waves present.

Should available space result in the aerial being rather more or less than a $\frac{1}{2}$ -wave, or multiple of $\frac{1}{2}$ -waves or some bands, then its end impedance will no longer be very high. As a result, it should be tapped down L1, until loading is satisfactory.

\star components list

Resist	ors:	Capaci	tors:
R1	1MΩ	C1	0·01µF
R2	470Ω	C2	0.02µF
R3	$47k\Omega$	C3	22pF ceramic
R4	10kΩ	C4	350pF mica
R5	100Ω		
R6	68Ω	Inductors:	
R7	1·5kΩ	T1	1:1 miniature driver transformer (Radio-
Transistors:			spares)
Tr1	OC171	RFC	1mH r.f. choke
Tr2	OC72		
Miscel	laneous:		
Mete	r 0–1mA	f.s.d.; valveh	olders-one of each

Meter 0–1mA f.s.d.; valveholders—one of each, B7G, B9A and I.O.; co-ax socket; 2-pole 2-way switch—S2; 1-pole 2-way switch—S1.

ever, this treatment should not be given to the B7G socket.

PRACTICAL TELEVISION — ON SALE APRIL 19th

X-RAY RADIATION METER

Because of the high e.h.t. necessary with shadow—mask tubes, very large X-ray dose rates are produced, hence the importance of being able to detect X-ray radiation in experimental work.

The meter described in this article has been designed to fulfil this requirement.

TELEVISION RECEIVER TESTING

The first part of a new series on television receiver testing techniques, concentrating on the test procedures adopted by the professional service technician.

IMAGE INTENSIFIERS AND CONVERTERS

An interesting group of devices ensures that today no scene is "untelevisable". The image intensifier produces brilliant images by light amplification so that we can see in the dark.







THEN Henry began indulging his penchant for airing his views, the long period some between submission of journalistic gem and the almost inevitable thud of its rejection on the doormat was hardly endurable. Offering a crumb of comfort, Mrs Henry used to say: "I'll bet they have taken your ideas and published them under someone else's name." Something of the same idea must haunt those who design some electronic wizardry and then try to take out a patent.

Between the final flourish of the soldering iron and the yacht off the Bahamas and sports car with built-in blonde there lies a tedious, obstacle-strewn road that is enough to deter all but the most diligent Blumlein. Looking at some of the conditions and restrictions recently to check the amazing resemblance between two colour-TV circuits, convinced this experimenter that it would be better to stick to garden-shed hook-ups and leave the breakthroughs to those more adequately equipped. But let us follow the fortunes of a humble back-alley inventor. We will call him Bill Smith; after all, his parents did!

Bill had been tinkering with a relaxation oscillator when the thought of the musical mousetrap occurred. Unlike Prof. Geiseling and his zoological researches on animal response, he had no



A musical mousetrap.

notions of lulling the rodents to sleep, or measuring their responses. He was more concerned with trap clearance.

In short, Bill had a disposal problem. All very fine setting the coiled wire mechanism with the best Double Gloucester. All very fine bribing the laziest cat in New Malden not to pinch said D-G. All very fine triumphantly removing the mangled remains of some pathetic Mickey and burying it where said lazy cat would not bother to dig it up. But Bill was not always on hand, and mice, though nocturnal creatures, did not always conveniently make their rendezvous with the Big Spring when they heard his flat feet approaching. Then, it was as likely that Mrs Bill Smith would come across said mangled etc., and dissolve in a fit of the vapours. Women are like that.

So it was necessary to organise some form of warning that would alert Bill, and only Bill, when the poor mus domesticus tripped the catch. A buzzer was out of the question; a bell might have been mistaken for the telephone; chimes were the front door early warning system and the construction of a voice-pulsed gadget that shouted "Hey You" was, Bill felt, somewhat beyond the resources of PRACTICAL WIRELESS Advisory Service. (Not according to some readers!-Ed.)

The solution came as he tried to attract his wife's attention from the kitchen transistor radio. She was oblivious, lost in a world of Jimmy Young—probably waiting for the telephone to ring! He snapped the switch and she blinked to the surface like a cod coming into warm waters. That was the answer: a transistorised alarm on her deaf side, to beat out a rhythmic signal, preferably in discordant tones. He would leap with jarred nerves; she would never notice!

Soon he was off to the Patents Office to register the unique, unPat. Pending



"Show us a working model."

paralleled musical mousetrap, only to be met with a frosty-faced glare and the remark: "You cannot simply patent an idea. Show us a working model."

More midnight oil, more curious noises behind the wainscot, more wailing protestations from Mrs S and Bill had his "vendible product"—a new process of doing something. He was ready to file his patent.

Sixteen years is the protection period, and then even the best musical mousetrap becomes public property. And during that time, the renewal fee has to be paid. Just to apply, and then write Pat. Pending, or Pat. Applied For and a string of fancy numbers, can be quite meaningless, as Bill discovered. Moreover, just because a device does not bear that magical six or seven figure number, it does not signify the patent is invalid, or does not exist.

Bill gave up the day his wife came back from the supermarket humming *The Sound of Music*. Somewhere there must be a sale for musical mousetraps, Patent Applied For—1/432.666. Perhaps if Bill had fitted a d.f. loop and a homing device, he could have interested some party behind the Iron Curtain, or in the Common Market or somewhere . . .

Five to hi-fi

PART ONE PICK-UPS

IAIN SMITH

A HIGH fidelity sound system can be considered as a chain with the pick-up, turntable, amplifier and loudspeaker each being the individual links making up the chain. It is often said that the amplifier is the strongest link in the chain, which is true. It is also said that the loudspeaker is the weakest link in the chain. This is not true. The loudspeaker is suspect for several reasons; one being that the average loudspeaker is between 5 and 10 per cent efficient, another being the loudspeaker's tendency to produce Doppler distortion (more of this later in the series).

There is, however, a far weaker link producing far more distortion, namely, the pick-up. The pickup transducer itself does not produce any significant distortion. Most distortion is produced at the point of contact between stylus and groove, the stylus mounting and cantilever with pick-up arm construction providing another distortion factor. An important feature of any pick-up head is its "compliance".

Compliance

The compliance of a pick-up transducer as used in record reproduction can be defined as "the ability of the stylus to trace accurately the pattern of modulations of the recorded groove without damage to the groove walls". Compliance is measured as the distance in centimetres that the stylus will move for a thrust of 1 dyne. This distance is usually very small and normal compliances are in the order of units $x 10^{-6}$. Two compliances are usually stated for stereo pick-ups; a lateral and a vertical compliance. All pick-ups have a lateral compliance but for safe tracking of stereo records, a vertical compliance is the one and only essential factor. This is because stereo records have modulations on each groove wall, which are at forty-five degrees to the vertical, therefore, some vertical motion is unavoidable.

By the above definition a good compliance is one which allows the pick-up to track the record without damage to the grooves. A figure of $5 \times 10^{--}$ cm/ dyne laterally and 2×10^{-6} cm/dyne vertically is about the minimum acceptable to meet this condition. Obviously, higher figures than this are better. The compliance of a pick-up determines, to some extent, the output from the pick-up. With high compliance pick-ups there is so much flexibility in the stylus cantilever or coupler that a movement of the stylus by the groove only produces a small movement of the transducer hence a smaller output. This is why high output crystal pick-ups used with low sensitivity amplifiers, found in portable record players, have a low compliance. Because of the low compliance a high tracking weight, around the 10 gramme mark, is usually necessary which is not very healthy for records.

Stylus Tip Mass

Another factor affecting the wear on records by pick-ups is the stylus tip mass. It is thought by some authorities to be the most important factor and experiments carried out so far confirm this. Tip mass is the mass of the stylus as seen by the groove of the record. This is not related to tracking weight, as mass is effective in all directions not just vertically. Many expensive pick-ups have a tip mass of 3 milligrammes. Experiments have shown that this, even when combined with a high compliance, produces measurable record wear. It is thought that something less than $1\frac{1}{2}$ to 2 milligrammes is desirable. The Decca Deram ceramic stereo pick-up has a tip mass of 0.6 milligrammes. This pick-up shows no measurable record wear after 250 playings under a 400 times magnification. Its compliance 9.0×10^{-6} lateral and 5.0×10^{-6} vertical is also somewhat less than some expensive pick-ups with a 3 milligramme tip mass, whose performance cannot compare.

Other factors affecting performance are tracking weight and electrical impedance. Tracking weight should be as low as the compliance allows but within the manufacturer's specification. Too little tracking weight causes more record wear, slightly more than is necessary.

Impedance

The electrical impedance required by the pick-up as a load should be matched by the input impedance of the amplifier. If the impedance, presented as a load to the pick-up, is too low, then a loss of the lower frequencies will result. Little effect will be noticed by putting a larger load than required across the pick-up. The minimum voltage required by the amplifier to drive it should also be matched by the maximum output of the pick-up.

Pick-up heads should be mounted in a lightweight shell coupled to a lightweight arm. This is to reduce the effective mass of the arm as seen by the stylus, thereby reducing lateral forces which cause record groove deformity. Friction in vertical and lateral pick-up arm bearings should be as low as possible, again to reduce lateral and vertical forces. Certain bearings such as brass bush and spindle types have limitations in this respect. Bearings should at least be of the small ball type.

The type of pick-up arm material affects pick-up performance. Plastic is notorious for causing resonance and die-cast aluminium is only one step better. Best materials are tubular aluminium or low resonance wood.

Another way in which pick-up arm construction affects performance is the angle at which the head is offset. Unless the stylus cantilever is tangential to the portion of the groove beneath it, distortion in the output waveform will be set up (see Fig. 1). The

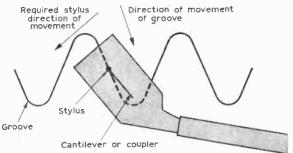


Fig. 1: An illustration of how tracking error occurs through the pick-up being incorrectly offset.

reason for the distortion is that it is direct lateral movement of the stylus that creates the output and the resultant movement of the stylus in the diagram would not conform to the recorded pattern.

A method of checking for tracking error is as follows. Take an old disused 78 r.p.m. disc and draw a line across the diameter. Mark a point on this line $2\frac{1}{2}$ in. from the record centre. With the stylus placed on this point the pick-up head should be at right angles to the diameter. If there is more than a three degree error, this should be corrected if the arm is of sufficient length. Correction can be made by either moving the pick-up head along the arm or by adjusting the arm length. Distortion caused by tracking error will be more noticeable towards the centre of the record.

Buying Guide

To sum up here are the main points to look for when purchasing a pick-up.

1. The pick-up should have a high compliance.

2. The tip mass should be less than two milligrammes.

3. The electrical impedance and output should be matched to the amplifier.

4. The pick-up arm bearings should be of the low friction type.

5. The pick-up arm construction should be of low resonance material.

6. The pick-up arm construction should be of such a length as to avoid tracking error.

Obviously a book could be written on this subject but the points outlined in this part should prove helpful.

to be continued

SATELLITE EARTH TERMINALS

APRIL ISSUE, PAGE 915

We regret that due to a printers error, the power of the signals referred to in the 28th line, second column, was given incorrectly.

This should read ".... 10⁻¹⁸watts" and not 10 watts as stated.



Starting a brand new Beginner's Construction Series on simple radio receivers. Full details for building the first project—a single transistor receiver. A compact, easy-to-build, economical to run midget. Ideal for the novice.

+

I.C. PREAMPLIFIER

+

Build this high impedance miniature preamp. Uses the very latest integrated circuit techniques and printed circuitry.

Typical circuits for use as an amplifier/detector stage for a.m. receivers, and for stereo applications.

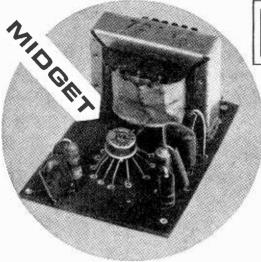
PORTABLE KEYLESS ORGAN

Solid state musical organ with unique "keyless" notes. Has built-in vibrato, its own preamp and output stage. Full instructions including tuning-up, playing techniques etc. . . and Building a variable frequency oscillator; Five steps to hi-fi; Repairing radio sets . . . **plus** all the regular features and news.

ALL IN NEXT MONTH'S



ON SALE MAY 10th



HE great controversy in the world of electronics at the moment concerns the present L status of the integrated circuit. No one really queries the assertion that over the next few years these devices will win for themselves a considerable share of the components market. Inevitably, as costs of conventional assembly increase, while the manufacturers become more expert in the design and production of semiconductor devices, use of the latter must become the approach dictated on terms of economy for more and more applications. It is the purpose of this article to point out that this breakthrough has already occurred for small audio amplifiers, and describe one particular design in which an integrated circuit is used to economic advantage. The circuit diagram of Fig. 1 which illustrates the equivalent of the I.C. in discrete circuitry, should be sufficient to prove that for the

I.C.AMPLIFIER L.M.C.NAMARA B. Sc.

sum for which this device can be obtained, it is certainly money well spent. In all, it contains the equivalent of seven functional transistors (a word about the diodes D1—D3 in due course), with nine resistors, arranged to provide the functions given in the block diagram, Fig. 2. We find five separate functions—a high impedance buffer amplifier, a voltage regulator, a phase splitter, and a pair of power output transistors, all n-p-n silicon planar epitaxial types, with identical characteristics except for Tr6 and Tr7 which are specially designed and fabricated for the higher currents they carry as output transistors.

The Integrated Circuit

The operation of this rather complex unit deserves fuller attention. The first block in Fig. 2 represents the transistor Tr1, which functions as a single emitter follower amplifier stage. With a higher input impedance than the conventional common emitter stage, it provides a better match to the output of a signal source such as a crystal gram cartridge. In a practical circuit, there is an emitter load resistor external to the I.C. (R13 in Fig. 3), and the signal developed across it is applied to the following differential amplifier type phase splitter, with its two transistors Tr2 and Tr3. The chain of diodes D1, D2 and D3 are actually further silicon transistors with their collectors unconnected; it would therefore be expected that the voltage developed across each would be the characteristic emitter-base voltage of a good silicon transistor, about 0.7 volts. Con-

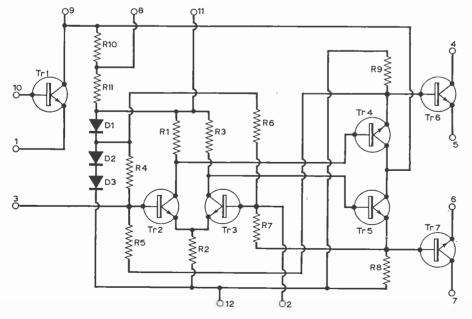


Fig. 1: Complete theoretical circuit diagram of the CA3020 integrated circuit. Component values are not listed, as these are not included in the manufacturer's data (see text).

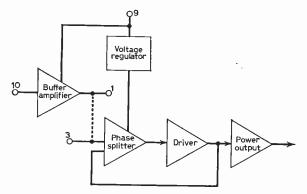


Fig. 2: Block diagram showing the functions of the I.C.

sequently these diodes perform the voltage regulator function, setting the base and collector voltages of the transistors of the phase splitter stage. The driver and output stages are therefore controlled also, as they are direct-coupled to the phase splitter. As for the operation of the differential amplifier, Tr2 produces out-of-phase signals in the collector and emitter load resistors, R1 and R2. As the base of Tr3 is by-passed by an external capacitor, this transistor acts as a common base amplifier, producing a signal at the collector in phase with that applied at the emitter. It follows that the audio signal in R3 will be equal in amplitude but opposite in phase to that in R1. The driver transistors Tr4 and Tr5 are directly coupled across these resistors, and act as emitter follower amplifiers; although in this mode they do not provide as much gain as in a common emitter amplifier, they are also performing an impedance matching function which eliminates the need for a transformer to drive the output pair. They are also responsible for providing a suitable level of base bias for these transistors.

Performance

Now that the operation of the I.C. has been considered, it is possible to devote some attention to the performances which could be expected from the unit. The values of the resistors and parameters of the transistors in the monolithic chip of the I.C. are not given in the supplier's data on the unit. This is perhaps because the tolerance to which a resistor can be fabricated by epitaxial diffusion is not yet as great as that expected in discrete components, and should any values be quoted, they could be no more than typical values. On the other hand, the ratios of resistances are very closely controlled in this type of manufacture, and the circuits are such that this ratio is more important than any absolute values of components. As a result, while the resistances found in individual circuits may vary, all samples will give a maximum power output of 550mW, and a power gain of 58dB. As the components within the chip are all direct coupled, there are no components to limit the bandwidth of the unit; the figure quoted of 6Mc/s is probably set by the structures of the higher power output transistors. As a result there can be no loss of fidelity at audio frequencies due to phase distortion in the I.C., and it will be the components external to the chip which will provide the frequency limitation, e.g. the inductance of the output trans-

★ components list

	ors: 470kΩ 4·7kΩ		4·7Ω % 1 ₩
Capaci	tors:		
C1	0·1µF	C3	0·1µF
C2	0.01µF	C4	5µF electrolytic
all m	iniature, 12V i	minimum wkg	
Miscol	lanoouer		

Miscellaneous:

Output transformer Ardente D3027; RCA* integrated circuit type CA3020; VR1 500k Ω with s.p. switch; VR2 50k Ω .

*RCA Great Britain Ltd., Lincoln Way, Windmill Road, Sunbury, Middlesex.

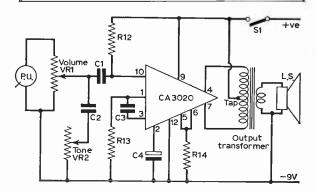


Fig. 3: Complete circuit of the I.C. gram amplifier.

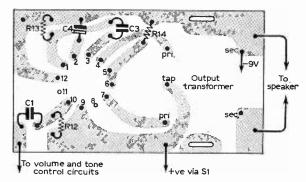
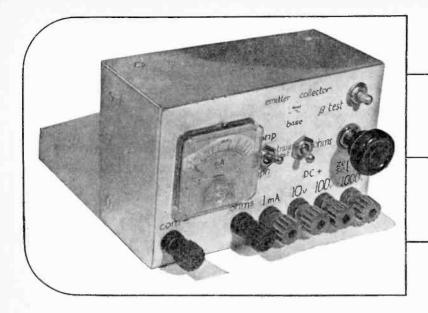


Fig. 4: The printed circuit. When viewed from the underside the tab on the I.C. can indicates lead 12.

former used to couple the output transistors to a loudspeaker. The transistors themselves are high quality types, as would be expected from silicon epitaxial units, and this contributes to the good noise figures claimed for the I.C., typically a signalto-noise ratio of 70dB. The input impedance of, typically, $50k\Omega$ ensures that the loss of signal in feeding a CA3020 amplifier from a gram pickup is minimised. However, perhaps the most striking aspect of the performance of the unit is in the efficiency of the voltage regulator system, which ensures efficient running of the circuit over a wide range of supply voltages and thermal and load conditions. The CA3020 will operate at line voltages

-continued on page 43



A COMPR CHECKE C.R. BRADLEY

An economical instrument which tests p-n-p and n-p-n transistors for relative BETA (current gain) and leakage. It will also test diodes and give useful voltage, current and resistance measurements.

USING new parts and an easily obtainable surplus ImA meter movement, this simple instrument was built for less than $\pounds 2$. It is designed to fill the needs of servicing home-built and commercial transistor equipment and will give a positive good/bad test for commonly used low voltage transistors. It will also prove its worth in weeding out the "junk box" which, in the author's case, provided most of the components.

Before the transistor testing circuit can be considered one must have a basic understanding of the operation of a transistor. The basic properties of a typical small p-n-p transistor are illustrated in Fig. 1. Here it is seen that a small current (e.g. $50\mu A = 50 \times 10^{-6}$ amps) is drawn out of the base of the transistor (I_b) while a larger current (e.g. $2mA = 2 \times 10^{-3}$ amps) is drawn from the collector (I_c). The sum of the currents (I_b+I_c) is the emitter current (I_e) which flows in the direction indicated by the arrow inside the transistor symbol.

The amplifying properties of the transistor depend on the fact that a large change in I_e may be produced by a small change in I_b . The graph in Fig. 1 shows a signal with a current swing of $25\mu A$ applied as input to the

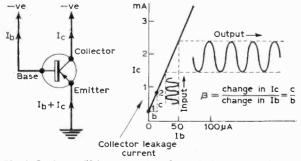


Fig. 1: Basic amplifying properties of a typical p-n-p transistor. The graph shows how Ic depends on Ib and is for a fixed collector voltage. base producing an output signal from the collector with a current swing of ImA. Thus a *current amplification* has taken place. The amount of amplification depends on the *current gain* of the transistor or the steepness of the I_c/I_b graph. The current gain or BETA (β) of the transistor is defined mathematically by: $\beta = \frac{\delta I_c}{\delta I_b}$ where δI_c

 $\frac{\delta r_e}{\delta I_b}$ is merely calculus notation for the ratio:

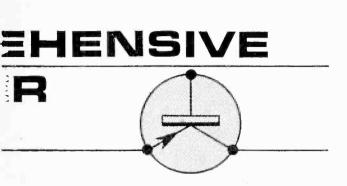
change in 1c corresponding change in I_b . In our example (see graph), $\beta = ImA/25\mu A = 40$.

Note that when $I_b = 0$ there is still a small collector leakage current. In a small germanium transistor this should not exceed 0.15mA and will generally be much less; certainly so for silicon transistors. For a useful listing of values of I_{ebx} see the article "In-circuit Transistor Tester" (P.W. Dec. 1967, p. 605).

Transistor tests

The transistor testing circuit is shown in Fig. 2. When S1 is open the base and emitter of the transistor under test are at earth potential and no current should flow across the reverse biased base-collector junction. What does flow is a small leakage current which is indicated on the meter; we are at point 1 on the graph in Fig. 1. Discard the transistor if this exceeds 0.15mA. The leakage current may be too small to indicate on the meter at all.

When S1 is closed ("BETA TEST") a small emitterbase current flows (assuming this junction is good) and a substantial collector current should result. Remember that a transistor's action is as follows: a small increase in the emitter-base current produces a large increase in the emitter-collector current. The meter reading should rise by about 0.5mA, the amount depending on the BETA of the transistor. We are now at point 2 on the graph. If the current does not rise, or only slightly, the transistor is faulty. But the budget-minded user will not discard it yet as either the emitter-base or collector-



base junctions may be usable as a diode!

As a low battery voltage (1-5 volt cell) is used, small transistors cannot be damaged by excessive currents. This does however limit the tester's use to common low voltage transistors. It will be found that even new transistors of the same make and type have widely varying BETAS; the tester makes it possible to select high gain transistors for critical circuits and find matched pairs for push-pull output stages. The same circuit is used for testing n-p-n transistors with the battery polarity reversed. The low voltage means that incorrect setting of the p-n-p/n-p-n switch in the final circuit is unlikely to damage the transistor under test.

Additional ranges

The 1mA meter used in the transistor testing circuit may also be used for simple voltage, current and resistance measurements. For d.c. voltage tests a resistor is placed in series with the meter as in Fig. 3 and by

Ohm's law:
$$\mathbf{R}_v$$
 (OHMS) = $\frac{\text{(voltage for f.s.d.) (volts).}}{1/1000 \quad (amps)}$

In this instrument the voltage ranges shown in Table 1 were obtained.

Ordinary 10% resistors were used for R_v by the author as the simplicity of the instrument and the small ImA meter used did not seem to justify closer tolerance (and more expensive) resistors. However 5% or even 1% components can certainly be used for greater accuracy. The 1,000 volt range is optional and if it is built into the tester then proper insulated terminals and test prods *must* be used and great care taken in making

TABLE 1

R _v *	f.s.d. volts
1 0k Ω	10V
$100 \mathrm{k} \Omega$	100V
$1M\Omega$	1,000V

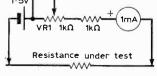


Fig. 5a: Resistance measurement circuit.

high voltage measurements. A 500 volt range ($R_v = 500 \text{ k} \Omega^{\dagger}$) might be thought more useful although this range would not match the existing 0–1.0 meter calibrations so easily.

Only the basic ImA d.c. current range is provided as this will suffice for many transistor circuit measurements. Higher current ranges are obtained by the use of "shunts" or resistors in parallel with the meter as shown in Fig. 4 where $R_c(OHMS) = R_i/(current for$ f.s.d. (*milliamps*)—1). The internal resistance (R_i) of the meter *must* be known and will probably be 100 Ω . Shunts may be built into the instrument to give additional ranges or wired externally when required. The author finds a 10mA range obtained with an 11 Ω shunt (near enough to 11·11 Ω given by the formula for $R_i = 100\Omega$) occasionally useful.

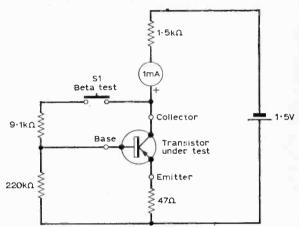


Fig. 2: Circuit of transistor leakage and beta tester. Close S1 for "BETA TEST"...

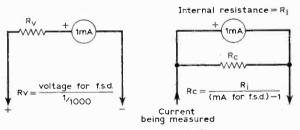


Fig. 3: Voltage measurement Fig. 4: Current measurement circuit. circuit.

A single resistance measurement range is obtained by the circuit in Fig. 5. The two test leads are first shorted together and the potentiometer VR1 adjusted for full scale meter deflection (zero ohms). The leads are then connected across the test resistance and a reduced current flows. The resistance may then be calculated

from the formula:
$$R(ohms) = 1500 \left(\frac{1-I}{I}\right)$$
 where

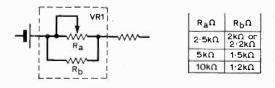


Fig. 5b: Use of alternative potentiometer values.

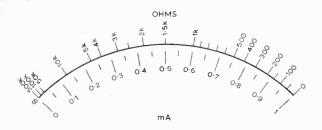


Fig. 6: Additional calibration of the 1mA meter for resistance measurements using formula in text.

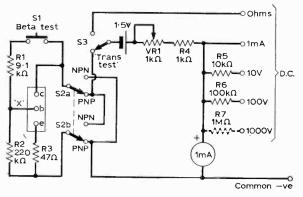
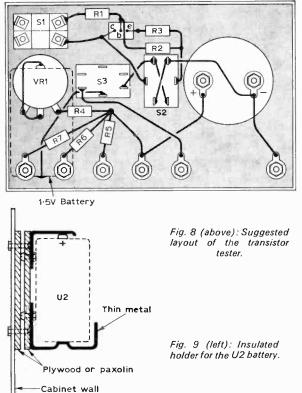


Fig. 7: Complete circuit of the instrument. The 1000V range is optional.



I(mA) is the meter reading. It is more convenient to have an ohms calibration on the meter. This will be a nonlinear scale ranging from infinity to zero ohms as in Fig. 6. To make the calibration, open the meter carefully and remove the scale taking great care not to damage the hairspring or pointer or let dust into the movement. The ohms scale is drawn carefully with indian ink and should not be calibrated too closely, particularly towards the high end, or legibility will be lost.

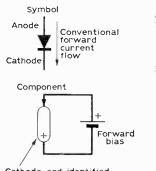
🖈 components list

Resisto	ors:	Swi	tches:
R1	9·1kΩ	S1	push button type
R2	220 kΩ	S2	DPDT toggle
R3	47 Ω	S3	SPDT toggle
R4	1kΩ		
R5	$10k\Omega$	Met	ter:
R6	100kΩ	0—	1mA d.c.
R7	1 M Ω		
VR1	1kΩ potentio	meter	
Termina	laneous: ls; 1·5V batte wire, solder et		lder; transistor socket;

Construction

The complete circuit of the instrument is shown in Fig. 7. A transistor socket is provided for transistor tests while other functions are selected by connection to the appropriate terminal. COMM is the common negative terminal for all ranges.

The non-standard value of R1 may be obtained by wiring $10k\Omega$ and $100k\Omega$ resistors in parallel. If a $1k\Omega$ potentiometer is not available for VR1 other values may be used as detailed in Fig. 5(b). The layout of the instrument is not critical and is left to the constructor. The meter, switches, terminals and transistor socket need only be mounted on a panel and the remaining few components wired in behind. A suitable layout is shown in Fig. 8. The cabinet could be built with a hinged back for test lead stowage. If a metal cabinet is used it should be left electrically "floating", i.e. not connected to any part of the circuit. The author used the $6 \times 4 \times 2\frac{1}{2}$ in. size of a popular range of four-sided aluminium chassis as a neat cabinet. The battery (a U2 size cell) is held in a simple home-made holder as in Fig. 9.



Cathode end identified with '+' or red mark

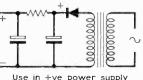


Fig. 10: Diode polarity. When using the tester, the positive end must go to the "COLLECTOR" test point. Before making a resistance or transistor test the "OHMS" terminal must be shorted to the "COMM" and VR1 adjusted for full-scale deflection (zero ohms) with S3 in the "OHMS" position. This adjustment compensates for the voltage drop of the battery with time although for accurate readings the battery should be fresh.

Diodes and rectifiers may be tested as follows: connect the diode between "EMITTER" and "COL-LECTOR" on the transistor socket. Try both settings of the p-n-p/n-p-n switch. In one direction the diode will be forward biased and a substantial current should flow (0.6mA or more); in the other direction no more than a tiny leakage current should flow. If the diode fails this test it is faulty. There often seems to be confusion in people's minds about which end of a diode is which; this can be cleared up by reference to Fig. 10. On this instrument the cathode (red or "+ve" end of the diode is

MIDGET I.C. AMPLIFIER

-continued from page 39

of as low as 3V, though at a reduced power level, and as high as 9V, though here a heat sink is advisable to hold down the temperature of the transistor junctions in the chip. Such sinks are commonly available as the I.C. is supplied mounted in a standard transistor-type format, according to the accepted TO-5 specification, and push-fit heat sinks are supplied for these transistors. Incidentally, although this property is unlikely to be of great advantage to the designer of amplifiers for entertainment and domestic purposes, the fact that the regulator keeps operation stable over the temperature range -55 deg. to + 125 deg.C. is certain to be of interest to industrial and military users. In the past, too. it would have been expected that the efficiency of the circuit would be lower than that of a discrete-component amplifier of the same output power, due to the loose tolerance of integrated resistors biasing the transistors. In this circuit, however, maximum power is obtainable with a current drain of no greater than 22mA.

Constructional Details ·

Now for an actual prototype amplifier using the RCA type CA3020 integrated circuit audio amplifier. The circuit of Fig. 3 was found to be a satisfactory competitor with typical discrete-component transistor amplifiers when used in a portable record player. Construction could not be simpler, and without any crowding it is possible to mount the whole amplifier on a printed circuit board less than 3 x 2in. As is clear from Fig. 1, all connections to the output transistors with the exception of the bases must be through external circuitry. This allows for an emitter resistor which introduces a slight degeneracy or negative feedback at that stage of the amplifier. It also allows a selection of the operating conditions for the output stage, as both the idling current, that is, the current drawn by the unit under no signal conditions, and the power output, depend on R14. Lowering it allows a greater output but increases this idling current and the dissipation in the I.C. In the prototype a value of 4.7Ω was selected; the power output dropped to about 350mW, which, however, is sufficient to enjoy the

the one connected to the "COLLECTOR" test point if forward conduction is obtained with S2 in the p-n-p position.

Footnote

This instrument is intended to give a relative indication of transistor BETA only. Accurate BETA measurements are possible however if a 100μ A meter is placed at "X" in Fig. 7 to measure I_b when S1 is closed. Hence BETA is calculated from the definition given.

• Rv actually includes the internal resistance of the meter which is usually about 100Ω . This is negligible compared with these values.

 \dagger Or two $1m\Omega$ resistors in parallel.

reproduction of recordings on a portable gram deck. Under these conditions a heat sink was not required. The printed circuit shown in Fig. 4 contains all the necessary interconnections between the components of the amplifier except C2 and the volume and tone controls, which are mounted separately and connected to the amplifier by screened flying leads. The output transformer whose tapped primary serves as a load to the output transistor pair, coupling them to the loudspeaker, is the only other major component on the board besides the I.C. I will not go into the details of the production of the printed circuit board by the conventional method of applying a paint pattern over the areas which are to form the conductors, and etching off the remainder of the copper foil coating of a section of clad paxolin using FeC1₃ solution; this process has been described repeatedly, to that the experimenter capable of working with integrated circuitry will be familiar with such a basic operation. The common alternatives, Veroboard and Cir-Kit, are also acceptable, but rather more difficult to use than is common with these methods, due to the close spacing of the 12 leads from the TO-5 can of the I.C. If these techniques are chosen, the leads of the I.C. must be carefully "spidered" or bent apart close to the seals in the base of the I.C. can so that they can reach the spacing of the Veroboard. Care is necessary in this operation, lest the leads or the seals of the can are damaged by bending too close. It must be remembered that a damaged I.C. can't be disregarded like a broken transistor—it represents almost a complete amplifier, and costs a lot more than an OC72!

Of course, the amplifier described is only one of the applications of this versatile circuit, and the imagination of inventive readers will find further applications for an effective and economical unit such as this one. The writer, for one, expects to hear a lot more about it in the future, and hopes it will find the commercial success the ingenuity of the design deserves. Perhaps such success will lead its manufacturers and their competitors to follow it up with more of the same, and perhaps even more exciting developments.

Full constructional details of an integrated circuit preamplifier (I.C. Preamplifier) with an input impedance of $10M\Omega$, will be published next month.



Times GMT Frequencies in kc/s

MONTHLY NEWS FOR DX LISTENERS

THE BROADCAST BANDS by CHRISTOPHER DANPURE

W ITH the spring schedules halfway through the operation period, and DX-ing conditions good, you should now be logging the world. With sunspot prediction of 132 for April, all the broadcast bands are open at different times of the day. So first off, here are the propagation predictions for April.

West and East Africa: 0600-1800 GMT 25, 21, 17 and 15Mc/s are the best bands, after 1800 and up to 2000 GMT 21, 17, 15, 11 and 9Mc/s, and 2000-0600 GMT 15, 11, 9, 7 and 6Mc/s bands.

South Africa: 0800-1400 GMT the best bands are 25 and 21Mc/s, 1400-1800 GMT 25, 21, 17 and 15Mc/s, 1800-2400 GMT 21, 17, 15, 11, 9, 7 and 6Mc/s, 2400-0400 GMT 11, 9, 7 and 6Mc/s, 0400-0800 GMT 15, 11 and 9Mc/s.

South Asia: 0800-1200 GMT use 25, 21 and 17Mc/s, 1200-1800 GMT up to 1600 GMT 25, 21, 17 and 15Mc/s, 1600 GMT drop 25 and 21Mc/s and add 11 and 9Mc/s, 1800-0200 GMT 11, 9, 7, 6 and 5Mc/s, 0200-0800 GMT 11 and 9Mc/s.

South East Asia: During morning hours 25 and 21Mc/s, in the afternoon 21, 17 and 15Mc/s, evening hours up to 2200 GMT 15, 11, 9 and 7Mc/s, 2200-0800 GMT 15 and 11Mc/s.

North East Asia: 0800-1400 GMT 21, 17 and 15Mc/s are the only bands open, 1400-1600 GMT 17, 15 and 11Mc/s 1600-2400 GMT 15, 11 and 9Mc/s, 2400-0400 GMT 11Mc/s only, 0400-0800 GMT 15 and 11Mc/s.

Australia via Asia: 0800-1200 GMT listen on 25 and 21Mc/s, 1200-1600 GMT 21, 17 and 15Mc/s, 1600-2000, GMT 15, 11, 9 and after 1800 GMT 7Mc/s, 2200-2400 on 11Mc/s only, 2400-0800 GMT this circuit is closed most nights, but signals may come through on 15Mc/s.

South America (North of the Amazon): From 1200-2000 GMT 25, 21Mc/s after 1800 GMT 17Mc/s as well, 2000-2200 GMT 21, 17, 15 and 11Mc/s, 2200-0400 GMT 17, 15, 11 and 9Mc/s, 0400-0800 GMT 15, 11 and 9Mc/s, 0800-1200 17 and 15Mc/s.

North America: During mornings on 17 and 15Mc/s, after 1200 GMT 25, 21 and 17Mc/s, evenings 17, 15 and 11Mc/s, night hours and early mornings on 15, 11 and 9Mc/s.

Those were the propagation conditions for April, listing the various shortwave bands which are "open" to different parts of the world.

ASIA

Rep. of Korea: The Voice of Free Korea has now the following schedule for its English programmes all over 50kW transmitters, 0500-0530 on 9,640 General Service to Asia, 0600-0700 on 15,130 to North America, 0800-0830 on 9,640 and 6,035 to South East Asia 1030-1100 on 9,640 General Service to Asia, 1430-1500 on 15,430 to South East Asia, 2100-2130 on 9,640 General Service of Asia, 0300-0400 on 15,430 to North America. The only transmission to Europe from *The Voice of Free Korea* is one in French from 0700-0730 on 15,130.

Thailand: *R. Thailand* is now using a 100kW transmitter on 11,910 at following times: 0415 0515 to North America in English; 0530-0600 to Europe in French; 0930-1020 to Far East in Thai, Vietnamese and Cambodian; 1025-1157 to Asia in English, Małay and Kuoyu; 1300-1400 to S.E. Asia in Thai.

EUROPE

Federal Republic Germany: The Voice of Germany is now as follows for its English Services transmitted from Jülich. 0300-0340 to South Asia oh 11,945 and 9,640; 0445-0545 on 11,945 and 9,640 to West North America; 0600-0630 on 17,845 15,275 and 11,785 to Africa; 0845-0940 on 21,650, 17,845 and 15,275 to Far East, Australia and New Zealand; 1045-1050 on 21,560, 17,875 and 15,275 to Africa; 1045-1055 on 11,905 and 9,605 to North America; 1550-1620 on 17,875 and 15,275 to South Asia; 1900-1910 on 17,790 and 15,405 to North America; 2110-2200 on 9,765 and 7,290 to East Asia and Australia; 2145-2205 on 15,275 and 11,925 to Africa; 0130-0250 on 11,945 and 9,640 to East North America.

Norway: *R. Norway* transmits daily in Norwegian and on Sundays the last 30 minutes of each transmission is in English, 0700-0830 on 25,900, 25,730, 21,730, 21,655 and 15,175; 1100-1230 on 25,900, 25,730, 21,730, 21,655 and 7,240; 1300-1430 on 25,900, 25,730, 21,730, 21,655 and 17,825; 1500-1630 same as at 1300-1430; 1700-1830 on 25,900, 25,730, 21,730, 21,655 and 15,175; 1900-2030 on 25,730, 21,730, 21,655, 17,825 and 15,175; 2100-2230 on 21,730, 21,655, 17,825 and 15,175; 2300-0030 on 15,345, 15,175 and 11,850; 0300-0430 on 11,860, 11,850 and 9,610.

AFRICA

South Africa: R.R.S.A. has altered the frequencies for the following English transmissions, now as follows; weekdays only 0415-0427 11,900 and 9,525; 0430-0442 11,900 and 9,525; 0500-0512 7,270 and 5,980; 0515-0527 15,220 and 11,900. Daily 1700-1750 21,535 and 17,805; to North America from 2326-0020 on 15,220 and 11,875; 0026-0320 on 11,875 and 9,705.

Many thanks for the *Radio R.S.A.* schedule to Mr. A. J. Jenkins, and items for the July issue please send them in by April 20th, 73's and good listening.

DEFINITE stirring down in the r.f. forest this past month. The sunspots are perking nicely and all the little peaks on those propagation prediction charts are getting better and better. All six bands from 1.8 to 30Mc/s are buzzing and, if trends continue, it could well be a bumper year for DX. There should be something somewhere on one of the bands whatever time you listen at present.

Derek Pearson (Worcs), proves that you don't have to be rich to qualify as an s.w.l. His set cost one shilling at a jumble sale but he has already logged VE3, VE6, YV4 and 3V8 on 14Mc/s.

SEVEN AND DOWN

F. McVerry (Lanarkshire), 7 valve s'het, 40ft., indoor antenna heard these on 160 metres c.w.— EI9J, GM3OXX, GI3OQR, GW3FSP, HB9TTH, OK1AHZ, OK1KP, OK2BKW, OK2RZ, PAØPN. On 3.5Mc/s s.s.b. his best were—CN8AW, EP2GI, HA2KRB, K2RBT, W1HKK, W1FZJ/KP4, 5Z4KL, 7XØAH, YU2HDE. On 7.0Mc/s c.w.—CT1MU, EA8UC, HB9AHC, HK7XI, IT1AGA, K2OTC, K3JH, PY7ARW, SL3AW, UA6KLA, UA9BN, VO2AW, WB4CIB, and on s.s.b.—EA4DO, ET3FMA, HC2AM, LX1BW, YV4UA.

M. Higgins (Sussex), 19 set, 132ft., l.w., bagged goodies on forty—CT1LN, F5TA, XE1CCW, ZL1HEO, ZL2BCG, 8P6BH.

J. East (Worcs), R1475, dipole, reckons 8 a.m. for the Pacific and evenings for Africa and S. America. He also informs that the 8P6 callsign is a new one for VP6 (Barbados). On 80 s.s.b.— CN8AW, CT1JH, K3UZE, VE1—ADA, AFI, IE, PL, UG, VE2XO, VE3ALX, VO1GL, VP2AA, WB2YFY/MM, ZB2A, ZB2AP/MM, ZC4MO, ZC4RB, 4U11TU, 7XØAH. While on 40 s.s.b.— CM2DC, CR6AD, CT1LN, EA3JE, ET3FMA, HB9RC/P/HP1 (in Panama City), IS1EP, IT1LTF, W1FZJ/P/KP4, PY2AST, UB5KAW, W3ZKH/P/3, WB4CPW, ZS1JA, ZS1NR, 4U11TU.

R. Miller (Essex), SR150, 30ft. l.w. plus an a.t.u. (good lad), logged these on 80 s.s.b.—CT1LN, CT2AA, F2RD, HB9MQ, ON5EL, OY7S, OY4OV, OZ6AE, SL3ZV, TF2PL, T12NA, VE1— AX, APZ, IE, VO1CE, W1FZJ/KP4, W2LX, W4BVV, W8MMC, W9ARV, YV1PW, YV2GK, ZB2A, ZC4MO, ZD3F, 3A2MJC, 4X4WN, 7XØAH, plus one query—OR9SN.

FOURTEEN AND UP

K. Weston (Wales) has been an s.w.l. since Santa unobtrusively popped a Trio 9R59 in his sock. He reports hoards of W's invading 28Mc/s.

H. E. Thornton (Surrey) started radio in the 1920s with an Experimental *Receiving* licence (not easy to get). With his "Portable One" he was permitted to ".... conduct experiments in the open air but not within two miles of a Government Station". His latest receiver to date is an Eddystone 940 complete with 100ft. I.w. On twenty he reports sigs. from—CR4AJ, KP4DCP, LU7DH, PY2ALE, TF2WKW, ZL4BX. On ten metres—CO2HQ, PJ2CQ, UN1CP, UA3AYN, VE1ATV, ZS1BV, 9J2WR. He also

reports a regular sked between the Science Museum station GB2SM and ZD9BE on Tristan da Cunha.

R. Dinning (Ayrshire), HA-350, PR-30, dipole, heard s.s.b. emanating from—CN8AB, CR61K, CR7JA, CT2AA, ET3REL, HS1AF, HS3DR, HV3SJ, KL7EBK, KR6BD, OD5BN, OX3YK, PZ1BD, PY7YN, TF2WKI, VE8RCS, VK2ON, VP8HZ, W6VPH, YV5CID, ZB2BM, ZL1AH, ZL4BX, 6Y5CB, 9Y4VT, W's 1-Ø.

M. Crawshaw (Lancs.), SR600 (triple conversion s'het), 80 metre dipole at 20ft. A peep at 28Mc/s revealed—CT3AO, EI5AL, F9CT, IIAIG, K3AFO, K8GLL, ON4VT, OZ1LO, VE1AKC, VE2AJV, VE3FWG, XE2BBO, ZE1BR, ZS1BV, ZS6OI all a.m. and on s.s.b.—CP1LN, CT1BH, DJ5RR, K1CTQ, OE5ARL, SV1AB, VE2LY.

P. Pollak (S.W.15), 840A plus Q multiplier, 60ft. end fed, states the case for twenty metres in no uncertain terms with-CE3ZN, CE6FK, CN8GE, CR4AJ, CR6GQ, CR7IC, CT2AA, ET3ZU, HI5BK, HKØBKW, HK3BLF, HK4PX, HS1AF (Thailand), JA1HMJ, KL7GDS, KP4BKF, KR6KN, LU5AQ, OY2H, OD5EJ. PJ4AC, PZ1BW (Surinam), TG5HC, TI2JCC, VE4SA, VE7AAF, VE8IY, VK2BK, VK1PL VK3HW, VK4SD. VK6CF, VP2GAI, VK7TR, VP2AA (Antigua), VP8JD, W6HVN, W7HEU, XEIKV, XP1AA, ZD7KH, ZD9BE, ZLIAHD, ZL2KC, ZL3OY, ZL4BX, ZP3AB, ZSIJU, ZS2EV, 4X4RW, 5H3JL, 5N2AAS, 5Z4KL, 6W8DY, 6Y5RA, 7Q7BN, 7XØAH (Algeria), 9L1DW, 9Y4VT. All these on s.s.b. and a very neat log too.

M. Guest lives in Mousehole (so help me that's the address) . . . (thereby hangs a tail). Anyway, it's in Cornwall and he has a CR100 and almost has a dipole for ten metres. Logged on this band—CR6QK, CX2CO, CX2BR, CX6BA, K2DPA, K9PPX, OA1MKA, OA7RP, OX3KM, VK6TXI, WØBQL, W8CIQ, W91UO, YV1WX, ZS1FH, 5N2LF, 9G1KM, 9G1FF, 9H1BA, 9J2DT, all on s.s.b.

M. Pasek (Notts.), HRO, 150ft. l.w., logged these on ten—CR4BC, CT3AH, UV3ACI, UW1DB, VK2OXB, VK3DL, VK3AGX, VK4PJ, VK5XV, VK5NY, ZE2JA, 9J2BC.

J. Preece (Cheshire), PCR3 modified as per P.W., Jan. 1968, accuses me of having printed his logs twice before. Guilty Sir ! and just to prove there's no hard feeling, here's what you heard on twenty s.s.b.—CN8GE, CR6AR, CR7CR, LA9TI/MM (17°S 4°E—go on, look it up), LU5AQ, LX1AJ, OZ9DX, PY4ATG, PY7CP, TR8AJY, UA9KDL, UT5KTH, VE3AA, VK3SK, YV4QG, ZC4MO, 5Z4KL, 6Y5GB. Also reported—7P8AB located at Maseru in Basutoland.

COMPOTE DE CONTEST

Are you sitting comfortably? Then I'll begin—6th —7th April, one I haven't heard of before but it's down as c.w. only from 3.5 to 30Mc/s; 20th—21st, 4 metre contest; 27th—28th, VERON—all bands every man for himself; 4th—5th May, 70 and 20cms. contest; 4th—5th May, another 3.5 to 28Mc/s c.w. special.



Interference

In my living-room I have a fluorescent light which gives interference on high frequencies, especially 2 to 4Mc/s. Can you suggest what and how I can fit something to this light to suppress this interference?—P. McKay (Leeds).

First, check the contacts at the ends of the tube to make sure that they are clean and making good contact with the holders. Then try rotating the tube through 180deg., and reversing it end for end. Renew the suppressor capacitor, using one of, identical ratings. Earth the metalwork of the fitting and if possible, feed the unit via metal-clad cable with the cladding earthed. Suitable cable is M.I.C.C. but you will need an electrician to install it unless you know how to do it.

Also, buy two 5nF (0.005 μ F) capacitors 500V a.c. working and connect them in series. Connect this combination across the tube. In fitting, connect a capacitor of 0.1 μ F 500V a.c. working across the mains supply cable. Connect two 0.5 μ F 500V a.c. capacitors in series across the mains cable, wiring the junction of these components to earth i.e., to the frame of the unit which will be earthed as above.

Rechargeable Cells

I would be obliged if you could tell me where I can obtain a charging set for mercury cells RM640 and E640.—E. Stuart (Edinburgh).

It is not possible to recharge cells of the mercury type since these are primary cells and not secondary cells. The only type of cell which looks rather like a mercury cell and which can be recharged is the nickel-cadmium cell.

Pulse Counter

With reference to the pulse counting f.m. circuit in the February, 1967, issue of P.W., and to one published a couple of years ago, I would like to know if either is suitable for use with a standard multiplex decoder. Also if the bandwidth of any pulse counting detector is sufficient, does it need a special decoder?—D. Webb (London, N.W.9).

A pulse-counting descriminator is not really suitable for use with a Multiplex decoder. There are several reasons for this, the main one being the use of a low i.f. in the receiver. If you wish to obtain really good results from stereo programmes, we would suggest you make a small tuner of a more conventional type especially for this type of reception.

Radio Teletype

On a visit to the last R.S.G.B. exhibition I noticed an exhibit by a teleprinting society.

Can you tell me if there is a society for radio teletype (R.T.T.Y.) enthusiasts, and the name and address of the secretary?—H. Beaumont (Margate).

Yes, there is a very active society, the name and address to write to is as follows: British Amateur Radio Teletype Group, D. J. Goacher, G3LLZ, 51, Norman Road, Swindon, Wilts.

Speaker Impedances

Is there any way of finding the impedance of speech coils in loudspeakers? I have two unmarked speakers but only a voltmeter for making tests.— T. Cropper (Middleton).

Loudspeakers normally have impedances of 3, 7 or 15Ω . These impedances are measured at 1kc/s. To find the impedances of a loudspeaker, the simple way (although it is approximate) is to measure the d.c. resistance of the speech coil. The d.c. resistances of speech coils of 2, 5 and 10 Ω will correspond to impedances of 3, 7 and 15 Ω respectively.

Short Wave Conversions

Could you please say whether there is a simple way to convert an existing receiver for short wave reception?—L. Ballard (Reading, Berkshire).

It is possible to convert short wave signals to a frequency on the medium waves in order to receive them on a normal receiver. A suitable converter for this purpose was described in our "Keybook" entitled "More Simple Radio Circuits" which you can obtain for 3s. 6d. from your local bookseller.

Transmitting Licence

I am keen to own and operate my own transmitting station. I understand that I will need a special licence. Can you tell me how I get a licence and what is involved?—E. Ledger (St. Albans).

We suggest that you write to Radio Service Branch, GPO Headquarters Buildings, St. Martin's le Grande, London, E.C.1, and ask for a free copy of their pamphlet "How to become a Radio Amateur".

Interference Suppression

Could you please let me have any information on any publication or literature regarding the suppression of electrical interference to a car radio from a car engine?—H. Wilkinson (Willington, Derby).

We suggest that you incorporate the following suppression measures in your car: 0.5μ F from D terminal of dynamo to chassis; 0.5μ F from D terminal of regulator to chassis; 2μ F from B terminal of regulator; 2μ F from outer terminal of coil; 0.5μ F from "live" side of any interfering accessory such as clock etc.; $5k\Omega$ cut-lead suppressors at each end of each plug lead; $5k\Omega$ cut-lead suppressors at each distributor-end of lead to centre of distributor; special non-capacitive filter in F lead of regulator. You can obtain all of these components from garages and radio component stockists.

If when driving along, you switch off the ignition, and the interference continues, it may be due to static electricity. If so, paint rubber conducting-paint on the walls of the tyres (the walls not visible from the road) and use a conducting grease such as a graphite-based type in the wheel bearings.

Earthing

I have just installed a shortwave receiver and I have been told that I should take the earth lead to one of the metal pipes in the house which will be a better earth. Is this in order please?—F. J. Mc-Donald (Walsall, Staffs.)

We strongly advise against earthing any electrical apparatus to metal pipes in the house. Many water pipes are now of the plastic variety outside the building and thus would be a poor earth. On no account should a metal gas supply pipe be used as an earth.



J. THORNTON-LAWRENCE GW3JGA

continued from the April issue

 Π HE Clubman Mk IV is a further development of the Mk III version, previously described and includes an output stage with built-in loudspeaker. The complete circuit is shown in Fig. 30.

The Output Stage

тне

This stage consists of a single transistor, Tr9, operating in class A and providing approximately 30 milliwatts of audio power to a $2\frac{1}{2}$ in. loudspeaker mounted at the left-hand side of the cabinet.

The input to Tr9 is taken from the headphone jack socket J1 and may be replaced with a closed circuit type, if preferred, so that the output stage is disconnected when the headphone jack is inserted, as shown in Fig. 30. With the jack plug removed, input signals are passed to Tr9 base and amplified a.f. signals appearing in the collector circuit are passed through T1 to the loudspeaker. D.C. biasing of Tr9 base is provided by the potential divider R29 and R30, the emitter stabilising resistor is R31. C25 provides extra decoupling of the -9 volt supply.

Two forms of negative feedback are incorporated in the output stage to improve the quality of reproduction. Negative series current feedback is provided by omitting the usual by-pass capacitor across R31, in this way the output signal current develops a signal voltage across R31 and this voltage appears in phase and in series with the input signal. Negative shunt voltage feedback is provided by connecting R29 to the collector of Tr9 instead of to the -9volt line. The a.f. voltage across the primary of T1

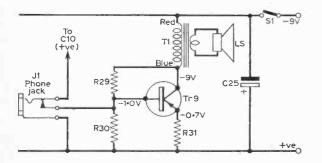


Fig. 30: Theoretical circuit of the output stage.

produces an a.f. current through R29 and this is out of phase and in shunt with the input signal.

The output stage is constructed on a small Veroboard panel which is fixed to the chassis by a bracket, identical to those used for fixing the i.f./a.f. panel in the Mk II receiver. The Veroboard panel is $2\frac{1}{8} \times 1\frac{1}{4}$ in. and the layout of components is shown in Fig. 31. To fix T1 to the panel, it is necessary to make a slot between two pairs of holes, so that the mounting tags on the transformer may be passed through the slots and bent over on the reverse side of the panel.

The output stage panel is fixed near to the b.f.o. box, as shown in Fig. 33. The three connecting leads may be connected as follows, chassis to J1 earth, J1 to J1 live and -9V to S2.2.

Loudspeaker Mounting

The loudspeaker is mounted at the left-hand side of the chassis near to the output stage as shown in Fig. 33. It is necessary to make a clearance hole in the chassis, to allow the loudspeaker to sink through, until the magnet is resting on the top of the chassis. With a little care, it is relatively easy to cut out the required shape using an Abrafile and finally finishing off the edge with a small flat file.

The vertical edge of the chassis is left intact and

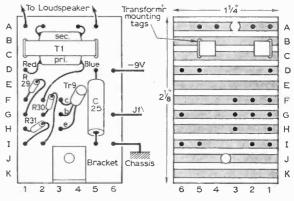
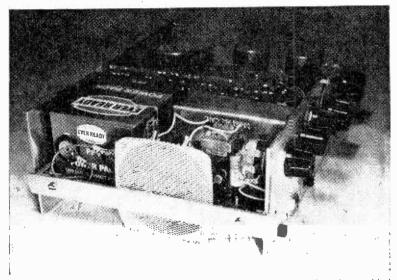


Fig. 31: Veroboard panel layout and connections.

appears across the front of the loudspeaker as shown in Fig. 32. The speaker is fixed to this edge using two clips, fixed with two countersunk 6BA screws and nuts. A piece of speaker fret material is fastened over the front of the speaker to complete the external appearance. Two wires connect the loudspeaker to the output stage panel. It is necessary to cut a $2\frac{3}{8}$ in. diameter hole in the end of the cabinet to "let the sound out" and this is done partly in the top cover.

To mark out the hole, the covers should both be fitted normally to the receiver, the centre of the hole is marked, as shown in Fig. 32. A circle of $2\frac{3}{8}$ in. diameter is then marked on the covers, using a pair of compasses or dividers. The covers are then removed and the



Photograph of the Mk. IV Clubman. A loudspeaker and output stage have been added.

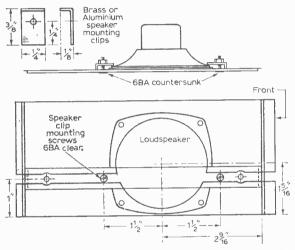


Fig. 32: Sketch showing method of mounting the loudspeaker.

★ components list

R30	ors: 15kΩ 2·2kΩ 100Ω	carbon, ½W, 10%
Capaci C25	tor: 100μF, 15V	electrolytic
Transfo T1	ormer: 9·2:1 ratio	T/T4 Radiospares
000000	onductor: OC82	
Loudsp 2½in.		
Jack: J1	Jack (insul	ated) closed.
Verobo 2 ¹ / ₈ x		2in. matrix

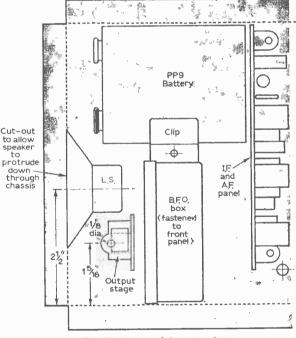


Fig. 33: Layout of the extra stage.

shapes cut away using an Abrafile. The edges should then be smoothed off using a fine half-round file.

Where the covers have previously been covered with plastic Contact or Fablon material, it will probably be necessary to re-cover them completely, as once the plastic material has been stuck to the metal for some time, it cannot easily be removed and re-fitted. Care should be taken to get a good finish when trimming the material around the speaker cut-outs.

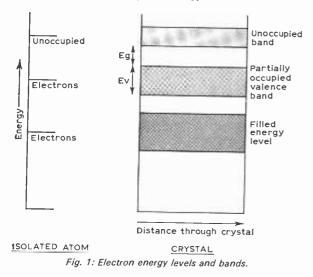
This completes the Mk IV version of the Clubman.

TO BE CONTINUED



KNOWLEDGE of semiconductors can be traced back as far as Michael Faraday who noticed the negative temperature coefficient of silver sulphide. But it was not until the second world war that the semiconducting properties of silicon and germanium were properly realised. Silicon and germanium occur in group IVB of the periodic table along with tin and carbon, and are similar in that they both possess four electrons in the outer, valence band of their atoms.

An atom consists of a centrally placed nucleus, positively charged, surrounded by negatively charged particles known as electrons. These electrons orbit the nucleus and although they exist in the space outside the latter they are not able to occupy just any old place. They are only permitted to rotate around the nucleus at certain discrete distances which correspond to certain energy levels. Thus to an isolated atom there is assigned a fixed number of energy levels at which its electrons can exist. But atoms do not exist in isolation, and as a result of this the picture is complicated by the fact that the electrons and energy patterns of adjacent atoms influence each other. This means that instead of an electron occupying an energy level associated only with its own nucleus, its energy level is modified



by the presence of neighbouring atoms. The result of this is that an electron can occupy a band of energies (Fig. 1).

CRYSTAL STRUCTURE

Germanium is a crystalline material, which means that its atoms are arranged in a regular fashion

throughout in a lattice-like structure. Each germanium atom has 32 electrons, of which four are valence electrons. These are the ones that are of importance because it is they that contribute to the electrical properties of a substance. The valence electrons form bonds with the valence electrons of adjacent atoms and it is these bonds that hold the lattice together. The valence electrons occupy the partially filled energy band shown in Fig. 1. Above this band is an energy gap where electrons cannot remain and a conduction band that they can enter if given sufficient energy to surmount the energy gap Eg, Fig. 1. The conduction band is an unoccupied band of energies into which electrons may pass. Obviously an electron at the top of the valence band requires an amount of energy equal to Eg to just scrape into the bottom of the conduction band, while an electron at the bottom of the valence band requires (Eg + Ev)energy in order to scrape into the bottom of the conduction band.

On its own germanium is not a good conductor since in the pure substance (at absolute zero temperature) there are no free electrons available to produce a flow of current. If, however, an impurity that possesses either three or five valence electrons —remember germanium has four—is introduced into germanium during its preparation its conductivity is greatly improved. We must next see how this happens.

DONOR IMPURITY

Consider the situation when a pentavalent atom (i.e. one with five valence electrons) such as antimony has been added. Since the antimony atom has five valence electrons and only four can form valence bonds with the adjacent germanium atoms one is left "unpaired". This is free and can move about the lattice and thus contribute to conduction. One small point here: an atom with all its electrons present is electrically neutral, the charge on the positive nucleus being exactly balanced by the collective negative charge of the electrons. Thus if an electron leaves its parent atom the result is a positively charged atom since the charge on the positive nucleus is greater than the collective negative charge of its electrons. In the above case with antimony when the fifth valence electron leaves the atom it leaves behind a positively charged atom.

An impurity that contributes electrons to a semiconductor in this way is called a donor impurity, since it donates electrons, and because the electrical conduction thus made possible is by means of electrons the doped germanium is referred to as n-type, the n denoting the presence of negative carriers.

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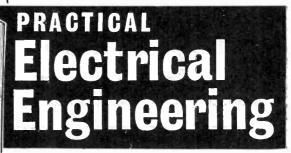
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ACCEPTOR IMPURITY

An impurity material the atoms of which have three valence electrons will also increase the conductivity of semiconductor material if introduced into the crystal lattice structure. In this case, however, instead of there being a free electron as in the case of the n-material there appears a gap or hole in the crystal lattice structure since germanium atoms, having four valence electrons, form four valence bonds with adjoining atoms in a complete lattice. The hole thus introduced into the crystal lattice structure represents a positive charge-equal to the negative electrical charge which an electron carries-and in fact will attract to it any free electrons that happen to be present. For this reason a trivalent impurity material is termed an acceptor impurity-since it will accept an electron to complete its electron pairing with adjacent atoms in the crystal structure and, since the holes introduced by it represent a positive charge, semiconductor material doped with an acceptor impurity is called p-type semiconductor material.

EFFECT OF IMPURITIES

We must now relate these impurity introductions to the energy diagrams previously described. In the case of the donor impurity the spare electrons contributed have energies just below the conduction band. This means that with a small "push" (in this case a quantity of energy) they will move into the

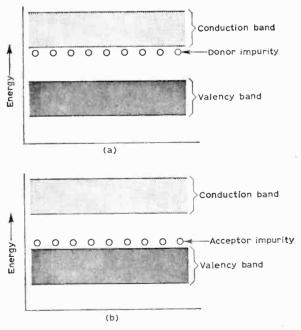


Fig. 2: Energy level diagrams for (a) donor and (b) acceptor impurities.

conduction band and be able to take part in electrical conduction (Fig. 2a). In the case of the alternative acceptor impurity the energy of the holes contributed lies just above the valency band (Fig. 2b). This means that electrons can be easily moved from

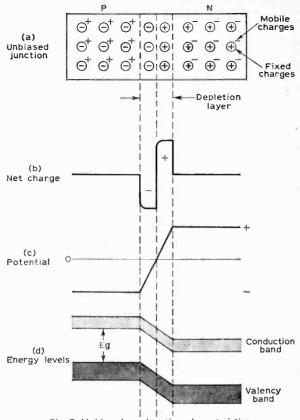


Fig. 3: Unbiased p-n junction characteristics.

the valency band into this level to take part in conduction.

THE P-N JUNCTION DIODE

A diode allows current to flow easily in one direction but not in the other. A semiconductor diode consists of two regions of oppositely doped germanium formed together (Fig. 3). In the pregion we have mobile positive carriers and stationary negative charge centres and in the n-region mobile negative carriers and stationary positive charge centres.

On forming the two regions mobile negative carriers from the n-region travel across the junction and combine with the positive holes in the p-region, while mobile positive carriers move in the other direction to combine with the electrons of the nregion.

This occurs in the region very close to the junction. As can be seen from Fig. 3a all the mobile charges in this region have been eliminated leaving only the fixed positive and negative charges associated with the donor and acceptor atoms. This region next to the junction containing only fixed positive and negative charges is called the depletion layer.

Thus the charge in the depletion layer on the p and n side is as shown in Fig. 3b falling to zero through the rest of the crystal. Fig 3c shows the potential throughout the crystal and it is this that is of importance when considering diode action. In the n-region the potential gradually rises to some positive

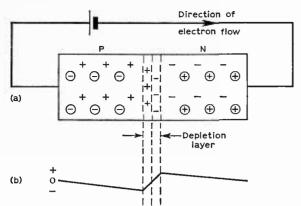


Fig. 4: (a) Forward biased junction. (b) Potential barrier.

value because of the positive charges in the depletion layer, but increases no further than the end of the depletion layer. In the p-region the reverse occurs and a negative potential is set up across this half of the depletion layer.

The energy diagram (Fig. 3d) is interesting: associated with both halves of the depletion layer are conduction and valency bands but these vary across the width of the depletion layer as shown. Notice that the energy gap Eg between conduction band and valency band remains constant. We must next consider the flow of electrons that occurs across the whole crystal if a potential difference is placed between opposite faces of the semiconductor, bearing in mind that (a) the crystal is neither an insulator nor a conductor and (b) a potential difference already exists between its ends (see Fig. 3c).

If the negative terminal of a battery is connected to the n side and the positive terminal to the p side and the voltage is sufficient it will reduce the potential barrier across the junction as shown in Fig. 4. In this case electrons will flow from the negative terminal of the battery via the semiconductor diode to the positive terminal with very little hindrance from the semiconductor. In this condition the diode is said to be forward biased and acts as a

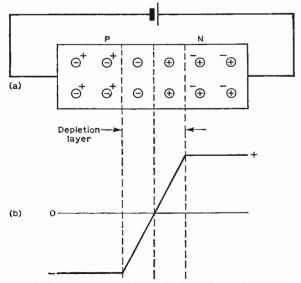
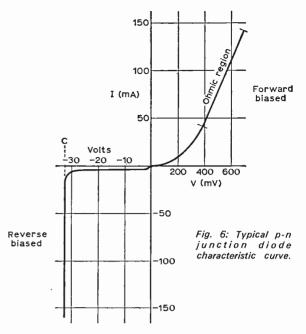


Fig. 5: (a) Reverse biased junction. (b) Potential barrier.



conductor. The application of the battery in this way drives the free electrons and holes nearer the junction, thus decreasing the size of the depletion layer and making easier the passage of current across the junction.

If, however, the negative terminal of the battery is connected to the p-region and the positive terminal to the n-region, the situation will be reversed and the potential barrier increased as shown in Fig. 5. This means that before electrons can travel from the p to the n-region they have to acquire sufficient energy to surmount this considerable potential barrier and thus under normal conditions no flow of current occurs. The diode is said to be reverse biased, and acts as an insulator obstructing the flow of current.

Thus the diode is a conductor with the applied voltage in one direction and an insulator with the applied voltage in the other.

DIODE CHARACTERISTICS

A typical diode characteristic is shown in Fig. 6, and may be obtained by using the arrangement shown in Fig. 7. With switches A and B in the position shown the diode is forward biased, and in the other position the diode is reverse biased. The variable resistance is used to alter the voltage applied across the semiconductor diode, this being measured on the voltmeter. The corresponding current flowing through the diode is recorded on the ammeter.

Taking first the forward biased case shown in Fig. 6 we see that the relationship between voltage and current is initially curved so that only small increases in voltage are required to produce quite substantial changes in current. This curve is exponential in shape. In the reverse direction it can be seen that a very large voltage has to be applied before any appreciable current will flow, so that up to this point (C) the device can be said to act as an insulator. What happens beyond this point is known

—continued on page 57



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TITIMPERS. Compression service de la control solo 20, 70 (2), 20, 20, 20, 20, 20, 20, 20, 20, 20, 20	TWIN GANG. "0-0" 208 pF. + 176 pF., 10/6; 865 pF., minia- ture 10/6; 500 pF standard with trimmers. 8/8: 500 pF.	
TITIMPERS. Compression service de la control solo 20, 70 (2), 20, 20, 20, 20, 20, 20, 20, 20, 20, 20	midget less trimmers, 7/6; 500 pF, slow motion, standard 9/-; small 3-gang 500 pF, 18/9, Single "0" 365 pF 7/6, Twin 10/-	$\frac{12\text{in.}}{25\text{w}}$ 5 gns. $\frac{12\text{in.}}{35\text{w}}$ 8 $\frac{1}{2}$ gns. $\frac{16\text{in.}}{50\text{w}}$ 18 gns.
TITIMPERS. Compression service de la control solo 20, 70 (2), 20, 20, 20, 20, 20, 20, 20, 20, 20, 20	SHORT WAVE. Single 10 pF., 25 pF., 50 pF., 75 pF., 100 pF., 160 pF., 5/6 each. Can be ganged. Couplers 9d. each.	"BONDACOUST" CABINET WADDING 18in. wide, 2/6 It.
	TUNING. Solid dielectric. 100 pF., 300 pF., 500 pF., 5/- each. TRIMMERS. Compression ceramic 30. 50, 70 pF., 9d.;	E.M.I. Cone Tweeter 31" square, 3-20kc/s, 10w. 17/6. Quality Horn Tweeters 2-18kc/s, 10w 29/6 Crossover 16/6.
CURTACT UNDERLIS + were domand 7 dr. 5 som A 106. Torent, own Low Charles and charles and the second secon		LOUDSPEAKERS P.M. 3 OHMS. 23in., 3in., 4in., 5in., 7in. × 4in., 15/6 each: Sin. 22/8: 64in. 18/6: 10in. 30/-:
SUNUCULUAR CINE NECURUNUS TAPE	CONTACT COOLED wave 60mA 7/6; 85mA 9/6.	12in. Double cone 3 or 15 ohm 35/-; 10 × 6in. 30/-; 8 × 5in. 21/-; E.M.I. Double Cone 13i × 8in., 3 or 15 ohm models 45.
Base Spools 2/6. Tape Splices 3/-, Leader Tape 4/2. Reales Tape Basels for Collars models 2 lines 41: 9/16. MAINS TRANSFORMER Post Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 200 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.0. v. 100 v. 1		SPECIAL OFFER! 8 ohm, 21in., 5in.; 80 ohm, 21in., 21in. 15/6 25 ohm, 5in., 6×4in. 35 ohm 3in., 7 × 4in.
Base Spools 2/6. Tape Splices 3/-, Leader Tape 4/2. Reales Tape Basels for Collars models 2 lines 41: 9/16. MAINS TRANSFORMER Post Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 200 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.0. v. 100 v. 1	5" reel, 900' LP with strobe markings also cine light	JACK SOCKET Std. open-orcuit 2/6. closed direntit 4/8:
Base Spools 2/6. Tape Splices 3/-, Leader Tape 4/2. Reales Tape Basels for Collars models 2 lines 41: 9/16. MAINS TRANSFORMER Post Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 200 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.0. v. 100 v. 1	corders and cine projectors. List 28/	Chrome Lead Socket 7/6. DIN 3-pin 1/8, 5-pin 1/6; Lead 3/6. Phono Plngs 1/ Socket 1/-, JACK PLUGS Std. Chrome 3/-:
Base Spools 2/6. Tape Splices 3/-, Leader Tape 4/2. Reales Tape Basels for Collars models 2 lines 41: 9/16. MAINS TRANSFORMER Post Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 200 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.0. v. 100 v. 1	OUR PRICE 14/-	2.5mm.; 3.5mm, 1/9; DIN 3-pin 8/6; 5-pin 5/ WAVE-CHANGE SWITCHES WITH LONG SPINDLES.
Base Spools 2/6. Tape Splices 3/-, Leader Tape 4/2. Reales Tape Basels for Collars models 2 lines 41: 9/16. MAINS TRANSFORMER Post Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 200 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.0. v. 100 v. 1	NEW B.A.S.F. LIBRARY BOXED TAPE	2 p. 2-way, or 2 p. 6-way, or 3 p. 4-way 4/6 each. 1 p. 12-way, or 4 p. 2-way, or 4 p. 3-way, 4/6 each.
Base Spools 2/6. Tape Splices 3/-, Leader Tape 4/2. Reales Tape Basels for Collars models 2 lines 41: 9/16. MAINS TRANSFORMER Post Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each Sch-2500 600.A. 6.3. v. 3. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 200 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.5. each MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.3. v. 1. 4. or 5 v. 2. 6. 0.0. MIDDET 200 v. 400 A. 6.0. v. 100 v. 1		Wavechange "MAKITS" 1 p 12-way, 2 p. 6-way, 3 p. 4-way, 4 p. 3-way, 6 p. 2-way. Prices include click spindles, adjustable
MAILS SCALESTS Post 6/-exch. Sign-Cased Stand, 63.9, 55.4, 63.9, 14. or 59, 74.8, 59.7, 57.5, 510/300-C-3009, 120mA, 63.8, 43.6, 85.7, 84. Post 6/-exch. MINATCRE SON 20 mA, 63.9, 15.4, 63.8, 74.8, 59.7, 84. Post 6/-exch. Post 6/-exch. MINATCRE SON 20 mA, 63.8, 14.8, 65.8, 14.8, 59.7, 84. Post 6/-exch. Post 1966 MINATCRE SON 20 mA, 63.8, 14.8, 65.7, 28. Post 1967 Post 1967 Post 1967 MINATCRE SADE SON 20 mA, 63.7, 18. Post 1968	Spare Spools 2/6. Tape Splicer 5/ Leader Tape 4/6.	stops. spaces, etc., 1 wafer, 10/6; 2 wafer, 15/-; 3 wafer, 19/6. TOGGLE SWITCHES, sp. 2/6; sp. dt. 3/6; dp. 3/6; dp. dt. 4/6
WHING THRUSTORING 50-each 30-30 Sum A. 63 v. 13. 63 v. 14. or 5 v. 24. 357-360-430-400 m.A. 63 v. 13. 63 v. 14. or 5 v. 24. 357-360-430-400 m.A. 63 v. 13. 63 v. 14. or 5 v. 24. 357-360-430-400 m.A. 63 v. 13. 63 v. 14. or 5 v. 24. 357-360-430-400 m.A. 63 v. 13. 63 v. 14. or 5 v. 24. 357-360-400 m.A. 63 v. 14. a. 69(c. 33 v. 43. 1176) WINATURE 200 v. 20 m.A. 63 v. 14. a. 69(c. 33 v. 44. 1176) WINATURE 200 v. 20 m.A. 63 v. 14. a. 69(c. 33 v. 44. 1176) WINATURE 200 v. 20 m.A. 63 v. 14. a. 69(c. 33 v. 44. 1176) DENERAL 200 v. 20 m.A. 63 v. 14. a. 69(c. 33 v. 44. 1176) DENERAL 200 v. 20 m.A. 63 v. 14. a. 69(c. 33 v. 44. 1176) DENERAL 200 v. 20 m. 200 v. 20 m.A. 63 v. 44. 30 v. 412		
1500-0300.400 m. 200.4.8.3 v. 3.a. 1.a. of 5 v. 2a. 35/- MIRIATURE 200 v. 300 m.A. 6.3 v. 1.a. 0.5 v. 2a. 17/6 MIRIAL 200-6.300 v. 100 m.A. 6.3 v. 1.a. 0.5 v. 2a. 12/6 MIRIAL 200-6.300 v. 100 m.A. 6.3 v. 1.a. 0.5 v. 2a. 12/6 MIRIAL 200-6.300 v. 100 m.A. 6.3 v. 1.a. 0.6 v. 1.a. 0.7 v. 100 m.2 v. 100 m.	WAINS INANSFURINERS 5/- each	
MINIATURE 200, 200 m.A. 6.3 v. 1 a	350-0-350-80 mA. 6.3 v. 3.5 a, 6.3 v. 1 a, or 5 v. 2a MT 510/300-0-300v 120mA. 6.3 v. 3.5 a, 6.3 v. 2a, 6.3 v. 2a, 45/-	Superhet. Ferrite Aerial etc.
HEATEX TRANS. 13. 4. 40 (0: 63. 7.42	MINIATIRE 200 v 20 m A . 8 3 v 1 a 12/81	joins for editing and repairs. With 3 blades. 17/6
 b. 9, 8, 10, 12, 15, 15, 24 and ov. At £ 8, 40, 50, 60, 80, 15, 10, 10, 10, 12, 10, 18, 24 and ov. 188, 10, 10, 10, 10, 10, 10, 10, 10, 10, 10	SMALL 250-0-250 50 mA, 6.3 v. 2 a	EAGLE 4 CHANNEL TRANSISTOR MIXER. Add
 b. 9, 8, 10, 12, 15, 15, 24 and ov. At £ 8, 40, 50, 60, 80, 15, 10, 10, 10, 12, 10, 18, 24 and ov. 188, 10, 10, 10, 10, 10, 10, 10, 10, 10, 10	Ditto tapped sec. 1.4 v., 2, 3, 4 5, 6.3 v. 1 [±] amp. 12/6 GENERAL PURPOSES LOW VOLTAGE. Outputs 3, 4, 5,	mix Microphone, records, tape and tuner with GO / G
CRYSTAL MIKE INSERTS11 × lin. 8/6: BM3 lin. dia. 9/611 × lin. 8/6: BM3 lin. dia. 9/611 × lin. 8/6: BM3 lin. dia. 9/612 × lin. 8/6: BM3 lin. dia. 9/613 × lin. 8/6: BM3 lin. dia. 9/614 × lin. 8/6: BM3 lin. dia. 9/615 × lin. 8/6: BM3 lin. dia. 9/616 × lin. Y = 1000 ohms17 × lin. 8/6: BM3 lin. dia. 9/618 × BEAPHONES 2000 ohms Super Quality 10/619 × lin. 3/6: BAM19 × lin. 3/6: SA19 × lin. 3/6: SA10 × lin. vin. vin. vin. vin. vin. vin. vin. v		
CRYSTAL MIKE INSERTS11 × lin. 8/6: BM3 lin. dia. 9/611 × lin. 8/6: BM3 lin. dia. 9/611 × lin. 8/6: BM3 lin. dia. 9/612 × lin. 8/6: BM3 lin. dia. 9/613 × lin. 8/6: BM3 lin. dia. 9/614 × lin. 8/6: BM3 lin. dia. 9/615 × lin. 8/6: BM3 lin. dia. 9/616 × lin. Y = 1000 ohms17 × lin. 8/6: BM3 lin. dia. 9/618 × BEAPHONES 2000 ohms Super Quality 10/619 × lin. 3/6: BAM19 × lin. 3/6: SA19 × lin. 3/6: SA10 × lin. vin. vin. vin. vin. vin. vin. vin. v	AUTO TRANSFORMERS 0-115-230 v. input/Output. 60w. 18/6; 150w. 30/-; 500w. 92/6; 1000w. 175/	dance 600 ohm/50K. 70-12,000 cps. Universal LU.IU.U mounting. stick, hand or stand. Professional quality.
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ALL PURPOSE HR. HEADPHONES H.R. HEADPHONES 2000 ohms Super Quality 38/5 LOW RESISTANCE HEADPHONES, 3-5 ohm 35/- LOW RESISTANCE HEADPHONES, 3-5 ohm 35/- LOW RESISTANCE HEADPHONES, 3-5 ohm 35/- 1968 GRAM CHASSISTANCE HEADPHONES, 3-5 ohm 1968 CHASSISTANCE HEADPHONES, 3-5 ohm State and the state of the sta	11 × žin. 6/6; ACOS 12 × žin. 8/6; BM3 1in. dia. 9/6. MOVING COIL MIKE with Remote Control Switch. 19/6	tuning. Size 6 × 4 × 24 in.
H.E. HEADPHONES 3-5 ohm 35/- LOW RESISTANCE HEADPHONES 3-5 ohm 35/- LOW RESISTANCE HEADPHONES 3-5 ohm 35/- LOW RESISTANCE HEADPHONES 3-5 ohm 35/- LIGHT ALL ADPHONES 3	ALL PURPOSE HEADPHONES	EAGLE 3 WATT AMPLIFIER. 4 Transistor 69/6
 * K RADIO BOOKS * (Postage 96.) * Radio Audio Amplifer Manual Book 1, 3/6; Books 1, 2, 3 or 5	H.R. HEADPHONES 2000 ohms Super Quality 85/-	
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GRAM CHADSIS: Post 5/ Five Valves: ECH81, EF89, Cons, Med., Short, Gram. EBC6. EL34, E280, Long, Med., Short, Gram. EBC6. EL34, E280, Sum out, Su	and the second se	
GRAM CHASSIS Det 5/ Three Wavebands: Five Valves: ECHSI: EF89, EBCS, EL84, E280, I3-month guarantee. A.C. 200-250 v. Perrits Aerial ia nin. × 4in. Two Pilot Lamps. Four Knobs. EDCS, L184, E280, EBCS, EL84, E280, I3-month guarantee. A.C. 200-250 v. Perrits Aerial ia nin. × 4in. Two Pilot Lamps. Four Knobs. EDCS, L184, E280, I3-month guarantee. A.C. 200-250 v. Perrits Aerial ia nin. × 4in. Two Pilot Lamps. Four Knobs. EDCS, L184, E280, I3-bom. SW 00-180m. Markite exp. push buttons. File International Radio Stations List 2/8 Modern Transistor Crouits for Bestinners. 6/- Visues. VEROBOARD 0.15 MATRIX 294 v5 in. 3/8d 21 × 31 in. 3/8d. EDCE CONNECTORS 16 war 4/-; 24 way 3/- in. wide 40, per Lin.; in. wide 1/- per 1in. (up the IT) in. Ia. wide 40, per Lin.; in. wide 1/- per 1in. (up the IT) in. Ia. wide 40, per Lin.; in. wide 1/- per 1in. (up the IT) in. TALMK ALUMINIUM CHASSIS. Is s.w. 8, 29 in. 3/8d. 200 (State 9) × 50m. 3/8(14 × 11in., 16/6; 11 × 11n., 7/6; 13 × 8im. 9/6; 14 × 11in., 18/6; 15 × 12in., 6/6; 14 × 9in., 5/e; 12 × 8in., 4/6; 10 × 7in., 3/6; 8 × 6in. 2/6; 6 × 4in., 1/6/- Xatum Mick TAPE ERASER AND RECORDING HEAD DEMAGNETISER WIRE-WOUND 3WATRIX 200/250 v. A.C. Laadets A.E. 200/250 v. A.C. Laadets A.E. 200/250 v. A.C. Laadets A.E. 200/250 v. A.C. SPECIALISTS Wirelew CULDED 9d.; CERAMICS 1/- EACH. SCHEENING CANS 1/- VALVE BASE PLUGS 2/3. Sum Post and Packing charge 2/6. C.O.D. 5/- extra. Full list 1/ CALLERS WELCOME COMPOSULATIONS Sum Condent Canser 2/6 × 23. 337 <whitehorse croydon<="" road,="" td="" west=""></whitehorse>	1968	
Three Wavebands: Five Valves: ECH81. EP89. Long, Med., Short, Gram. EBC8 EL84, E280. Labor, Med., Short, Gram. EBC8 EL84, E280. Laine de allibrated. Chassisolated from mains floating transistor. Receivers. floating transistor. Receivers. floating transistor. Beeelvers. floating transistor. floating transistor. floating transistor. Beeelvers. floating transistor.		Transistor Audio Amplifler Manual Book 1, 3/8: Book 2, 6/-
Three Wavebands: Five Valves: ECH81. EP89. Long, Med., Short, Gram. EBC8 EL84, E280. Labor, Med., Short, Gram. EBC8 EL84, E280. Laine de allibrated. Chassisolated from mains floating transistor. Receivers. floating transistor. Receivers. floating transistor. Beeelvers. floating transistor. floating transistor. floating transistor. Beeelvers. floating transistor.	ALL	Transistor Communication Sets
12-month guarantee. A.C. 200-250 v. Ferrite Aerial 10 13 watts 3 ohm. Chassis 131in. × in. × isin. iai size 13in. × din. Two pilot Lamps. Four Knobs. f10.19 14:scd.calibrated. Chassis isolated from mains f10.19 19-50m. SW 60-180m. Mastic exe, push buttons. f10.15 110.st (56 4) 4/-31 m. s/d6, 10-7 f11.9 111.m. st (66, 11 × 71n., 766, 11.8 f11.9 112.st (56, 9 × 71m., 6(6; 11 × 71n., 766, 14 × 91n., 766, 12 × 81n., 4(6; 10 × 71n., 3(6; 8 × 61n., 166; 11 × 91n., 766, 12 × 81n., 4(6; 10 × 71n., 3(6; 8 × 61n., 166; 14 × 91n., 766, 12 × 81n., 4(6; 10 × 71n., 3(6; 8 × 61n., 166; 14 × 91n., 766, 12 × 81n., 4(6; 10 × 71n., 3(6; 8 × 81n., 166; 14 × 91n., 166, 14 × 91n., 766, 12 × 160., 48 × 91n., 50 × 160., 600 × 100. 112 × 81n., 4(6: 10 × 71n., 3(6; 8 × 61n., 166; 14 × 91n., 166, 12 × 100., 800 × 100., 100 × 100., 100 × 100. <	Three Wavebands: Five Valves: ECH81, EF89,	Sub-Miniature Transistor Receivers
Iaim. × 4in. Two pilot Lamps. Four Knobs. f10.19 Aligned calibrated. Chassisiolated from mains f10.19 DE JUXE STEREO GRAM CHASSIS V.H.F., MW, SW State of alignment of the state of th	12-month guarantee, A.C. 200-250 v. Ferrite Aerial	At a glance valve equivalents
19:50m. SW 60-180m. Marke eve. push buttons. £19.19 VEROBOARD 0.15 MATRIX 21:50m. SW 60-180m. Marke eve. push buttons. £19.19 VEROBOARD 0.15 MATRIX 21:50m. SW 60-180m. Marke eve. push buttons. £19.19 VEROBOARD 0.15 MATRIX 21:50m. SW 60-180m. Marke eve. push buttons. £19.19 21:50m. SW 60-180m. Marke eve. push buttons. £10m. 216d. 21:50m. SW 60-180m. Marke eve. push buttons. £10m. 216d. 21:50m. SW 60-180m. Marke eve. push buttons. £10m. 216d. 21:50m. SW 60-180m. Marke eve. push buttons. £10m. 216d. 21:50m. SW 60-180m. Marke eve. push buttons. £10m. 216d. 21:50m. SW 60-180m. Market eve. push buttons. £10m. 216d. 21:50m. SW 60-180m. Market eve. push buttons. £10m. 216d. 21:50m. SW 60-180m. Market eve. push buttons. £10m. 216d. 21:50m. SW 60-180m. 210m. 21	13in. × 4in. Two pilot Lamps. Four Knobs. £10.19	valves, Transistors, Diodes equivalent manual10/6
10 table jud vertices 10 table jud vert	DE LUXE STEREO GRAM CHASSIS V.H.F., MW, SW 19-50m SW 60-180m, Mazic eve, push buttons, £10 10	1 w. 1 w. 1 w. 20% 3d.; 1 1 w. 8d.; 2 w. 1/-; 1 w. 10% 6d.
 VERDORAL OLD MILLING 31 × 391:n. 3/84. VERDOR DOWNED CONNECTORS 16 way 61. VERDE VOLTERS 7/6d. VERDE VOLTERS 7/6d.	o valve plus tect. Size to a ri a olu. digu.	Ditto 5 %, Preferred values 10 onms to 22 meg., 9d.
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THE SEMICONDUCTOR DIODE

----continued from page 54

as the avalanche effect, but for the moment it can be seen that provided the diode voltage is kept below point C it will perform as required.

The fact that a small current flows in the reverse biased condition before point C is reached may seem to conflict with the theory outlined earlier concerning potential barriers. However there is quite a simple explanation. In order for an electron to take part in conduction it has to enter the conduction band and to do this it has to obtain an amount of energy (Eg, Fig. 1) to lift it out of the valency band. Sufficient energy is provided for a few electrons to do this by heat that is transferred to them from outside the crystal. Ordinary room temperature is enough to impart sufficient energy to allow a few electrons to cross into the conduction band, and this gives rise to the small amount of current that flows even when a semiconductor diode is reverse biased.

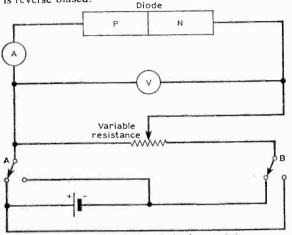


Fig. 7: Circuit for plotting diode characteristics.

The reason for the sharp change that occurs at point C in the reverse characteristic is that at this point—usually known as the zener voltage or reverse breakdown voltage—the potential is such that the electrons forming the "reverse current" are travelling at very high velocity. The result is that a considerable number of electron collisions occur, resulting in a rapidly increasing number of electrons being separated from their parent atoms—in short, an avalanche effect takes place.

As light is a form of energy its effect on a pn junction is similar to that of heat, i.e. exposure of a biased pn junction to light gives rise to a flow of current proportional to the strength of the illumination. This effect, known as photoconduction, is made use of in photocells and phototransistors.

Another feature of the pn junction that is of practical use is the junction capacitance. Since the depletion layer in the reverse biased condition has very few charge carriers while the p and n regions on either side are conductors, the device is akin to a capacitor; and since the width of the depletion layer is proportional to the bias applied across it this junction capacitance is inversely proportional to the bias. Consequently we have a device that can be used for frequency stabilisation in oscillator circuits.

MW COLUMN

HERE is little DX news this month since the generally poor conditions of this season L have continued. But readers should note that the seasonal change in propagation which might well help occurs around March-April conditions should and, in particular matters be more favourable for signals coming from South and Central America. This could well provide an opportunity to log a few of the more difficult ones from these parts and the chances can be assessed by the reception of the more likely ones to come through. Some to look for are CMCN (550kc/s); HJHJ Radio Libertad (610); La Voz de la Victor, Costa Rica (625), HJBJ La Voz de Sania Marta (640); YVLH Radio Giradot (650); CMCH Havana (770); CMCA Havana (830); HJKC Emisora Nuevo Mundo (850); YVLW Radio America (890); YVRO Radio Aeropuerto (910); YVNZ Radio Calendario (1020); 4VEF Haiti (1035); YVQJ Radio Barcelona (1080); WUNO Rio Pedras P.R. (1320); WIVV (1370).

Reception from Asia sometimes improves around this time of year, notably from the India/Pakistan region, so keep an ear open for stations such as Lahore (630), Quetta (750), Indore (650), Vijayawada (840), Ahmedabad (850), Sambalpur (860), Lucknow (910), Raipur (980), Rajkot (1070), Sangli (1250) and others. The North Regional stations sign-on at 0130, 0200 and 0330, West Regional stations at 0130 and 0230. East Regional stations 0130 and 0200, South Regional stations 0130, most of them starting off with news in English.

The fact that GMT has now disappeared completely is rather unfortunate for MW work, since it now means that everything starts an hour later *all* the year round instead of only during the summer months. This has been taken care of in the above times for the Indian stations. (Note: I have sometimes heard Indian stations on the air *before* the scheduled sign-on times, so it is still worth while listening around on their frequencies earlier than the times listed—*Editor*.)

Among the oddments of news this month is a report that Malta on 1241 has stopped transmitting. CJRS is a new Canadian on 1510 with 10kW. CKOC on 1150 has pushed up its power to 10kW.

Some of the items noted this month have been Tanzania on 638, Dakar on 764, *Radio Carve* Montevideo (850), LR3 *Radio Belgrano* Buenos Aires (950), CKBW Bridgewater (1000), LR1 *Radio el Mundo* (1070), YVQT *Radio Carupana* (1110). Glyn Morgan has a tentative logging of Saudi Arabia on 647 and Johannesburg on 1286 at 0220.

ALISTAIR WOODLAND



J. McCARTHY

describes

HIS article describes a circuit which can be used to send automatic Morse transmissions of a repetitive nature. For example, to transmit manually: CQ CQ CQ de G3ABC several times and receiving no reply is not only frustrating but tiring. Using the circuitry to be described, the "CQ" calls may be automatically broadcast, leaving the operator completely free during the period of transmissions. The equipment used would probably be readily available in the "ham's" shack, and the small amount of additional circuitry required can be built in an evening. The equipment required is: a tape recorder; transmitter, preferably with automatic break-in facilities (when the key is up, the receiver is automatically un-muted); a simple two-transistor switch; a controllable tone source.

PICK-UP

In the author's case, hum was picked up using a conveniently available metal bed. The Morse key's back-contacts shorted the tape recorder's input to earth when the key was released. When, however, the key was depressed, the hum from the bed was fed into the recorder's input. If a less barbarian method is preferred, a tone source may be constructed, but this is left to the amateur's choice. The equipment is used as follows:

SOURCE

The call, for example as above, is recorded on the tape recorder using the tone source and the Morse key. The call is thus recorded on tape. The call is then played back when required into the switch, which keys the transmitter. At the end of the call, the receiver is automatically activated, and

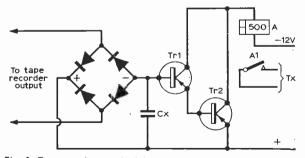


Fig. 1: Two transistors wired in a super-alpha configuration receive impulses from the tape recorder via the bridge rectifier made up from the four diodes.

the tape can be either wound back, or turned over in order to use the other track which would be recorded in the same way. Another possibility with a $1\frac{7}{8}$ in recorder would be to use an endless tape spilling into a conveniently positioned rubbish bin. This, too, is left to the individual constructor.

If the transmitter lacks break-in facilities, a modi-

A METHOD OF REPETITIVE MORSE BROADCASTS

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fication can be made to the transistor switch. The circuit of the switch is given in Fig. 1. As will be seen, the tape recorder's loudspeaker is muted, and a suitable resistor (3 or 5Ω) wired across the input of the switch. The smoothing capacitor, Cx, is dependent on the speed of Morse required; it must be great enough to prevent relay chatter, but not so great as to blur the Morse characters. The value should be found by experiment, 0.1μ F being a reasonable starting value. The two transistors, which

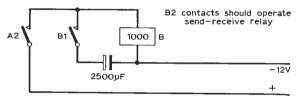


Fig. 2: Using an extra relay to facilitate break-in working. The electrolytic used to slug the relay might need to be varied in value dependent upon morse speed.

were two red-spot surplus types, are connected in a "super-alpha" configuration, and operate the switch's own relay, which should be a high-speed type. The contacts on the relay are used to key the transmitter. The four diodes are ordinary germanium "crystal" diodes.

The chassis used for the construction of the switch was a piece of paxolin— $1\frac{1}{2} \times \frac{3}{4}$ in., to which the wiring was actually stitched, using a large needle, thin wire, and a sewing machine (no kidding). More conventional methods, such as Veroboard are, of course, suitable. The whole was constructed within a metal box roughly 3 x 3 x 2in.

BREAK-IN

If a transmitter is used which does not have break-in facilities, then an extra relay is used which is switched on by the A relay, but is rendered slow-to-release by the large electrolytic in parallel with it. This second relay, the B relay, should be connected to the transmitter in such a way as to switch on the transmitter at the first Morse character, and to hold on the transmitter till shortly after the last character. If the Morse is excessively slow, trouble will probably arise due to this relay energising, and releasing, between each letter, and the value of the electrolytic should be increased.

The supply for the switch is 12 volts which was obtained in the author's case from a transistor radio power supply unit. Alternatively, the tape recorder or transmitter may be persuaded to supply the required voltage.

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AVAILABLE FOR IMMEDIATE EXPORT General Information. This set is normally carried in the life jackst of Airmen. It is a complete miniature light-reight radio Truncific effective, rompilete miniature light Beacon plus two way speech communication of give and of finding themselves in the sea. It comprises a Trans-mitter-Receiver, a speech unit, a coding unit and a power supply elther Battery or Transistor. These three items are permanently interconnected and all units are completely scaled and water tight using a combined speaker/mike. Press to talk or listen buttons. fold up actial, a total of three valves are used, power required 6.3 volta LT 90 volta and 435 volta D.C. HT. Frequency 243m/cs. Transmitter output pulse power. Beacon 15 wats, Talk 3 waita. SUPPLIED IN MAKER'S BOXES in Grade 1 condition sinkly at 43-. post 5/- with circuit. New batteries if available 7/6 each.

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We have a few of these V.H.F. 12 valve transreceivers operating on 3 switched channels between 60Me/s-95Me/s complete with all 6 crystals, headphones, mike, mobile aerial and dipole aerial, all connectors plus alloy tripod for mounting the set on. Power input 12V D.C., TX output 3 watts, internal speaker (all valves B67). All air tested O.K. Sipplield in good grade 2 condition at \$20,0.0 esch, carr. 30/-. Also available in matched pairs 255 per pair, carr. 30/-. tested.



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stage, frequency changer, two I.F. (465 Kc/s) signal detector, A.V.C. and output stage. A B.F.O. included for G.W. or single side-band reception. T.X. output waive 807, other valves octal bases. Many extras, e.g. netting switch, quick flick dial settings, squickh etc. Power re-time transmitter 500 with B.O. size septrox, 74 X J; X Hina. Every set supplied in new or as new condition in earton with book including circuits, only \$4,10.0, or Grade 2 slightly used 50/.. Grade 3, used but complete, 53/.. Garr. ALL 15/. WE MAKE A MAINS 200/250 VOLT POWER UNIT in louvred metal case to plug direct into set hower socket to run (1) receiver, 70/e, post 5/.. (2) TX and RX. \$6,100, post 7/6. (3) 12 volt D.C. P.U. (original). FAIR CONDITION, 40/-, Carr. 5/.. A charge of 10/. to unpack and test the receiver of these sets is made only if requested. Headphones and Mike 15/-, new and boxed.



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Oh, so slow!

Your March Editorial dealing with the warning of amateurs who transmit their call-signs faster than the prescribed maximum of 12 w.p.m. is a timely one. So far as I know no other periodical has spoken out on the subject, and 1 think I am right in saying that no official reason was ever given for lowering the acceptable maximum speed from 20 to 12 w.p.m. One club to which I belong has for some time been concerned at the seeming persecution of progressive c.w. operators and its newsletter has commented greatly on this.

From its membership it has been established that the following countries do *not* find it necessary to restrict the sending of call-signs to 12 w.p.m.: Australia, Belgium, Brazil, Bulgaria, Canada, Denmark, Finland, East and West Germany, Italy, Netherlands, Nicaragua, Norway, Poland, South Africa, Sweden Switzerland and USA.

Why, then, do the UK authorities see fit to impose such a backward step on British amateurs?

As for the reason some amateurs find themselves in trouble, perhaps the GPO has left us to our own devices for so long (my station has not been inspected for 15 years) we think they will never enforce *any* regulation. What a pity the station inspectors only show any interest when TVI or BCI are reported. An occasional, but unexpected visit would do much to keep the standard of equipment, operating and log-keeping up to scratch.

However, regulations are regulations, and it would be as well for all amateurs to re-read their licences, especially the sections limiting the operating of stations to qualified persons *only*, the sending of the station call-sign, at not more than 12 w.p.m., at the beginning and end of each "over", on changing frequency and every 15 minutes, when transmissions exceed that length of time and the ban on "Third Party" messages.

Until such time as the GPO readopt the more realistic 20 w.p.m., we c.w. operators can only hope that equal notice will be taken of "Joe", "Fred" and "Tom", all s.s.b. users, who seem to have forgotten they were ever issued with call-signs.—F. Allan Herridge, G3IDG (Hampshire).

A dig at Ed.

Your Topic of the Month for March refers to the fact that the Radio Services Department has been sending letters of complaint to amateurs who have been sending their call-signs faster than 12 w.p.m.

LETTERS. The Editor does not necessarily endorse the views expressed by correspondents.

You refer to this as "petty niggling by the GPO", and say you cannot understand "why it should suddenly become necessary to throw the book at operators."

Before you put your big feet any deeper in the mire let me invite you to read my AMATEUR (SOUND) LICENCE A which has been drawn up in accordance with the WIRE-LESS TELEGRAPHY ACT, 1949. Section 9(2) reads: "The call-sign, which may be sent either by morse telegraphy at a speed not greater than 12 words per minute or by telephony"

In short, you are knocking the GPO for insisting that amateurs operate within the terms of their licence.

Just watch it, Ed, or you'll end up in the Tower—and I don't mean the Post Office Tower!—John Mayall, G3VPH (Droitwich, Worcs.).

[Why should I read your amateur licence G3VPH—I have quite a few of my own, more than one of which says I can send call-signs at no more than 20 w.p.m. That, of course, was in the days before the GPO started to niggle and reduced it to the 12 w.p.m. crawl asked for today. As you say, I may well end up in some sort of tower but so long as it isn't the Tower of Babel occupied by some of the a.m. and s.s.b. boys I shall not complain. I'll just set up my rig and send out slow morse practice sessions for the benefit of the GPO!—Editor]

PCR mods

The "Trawler-band" coils mentioned in the article "Mods to the PCR" as used by the writer are Repanco Types RA3, RHF3 and RO3. The writer has made inquiries and confirms their availability at 3s. 9d, each through retail shops.

The PCR3 which does not have a Long Wave band, covers the ranges 13-43, 43-120 and 200-550m. The trawler band coils could be substituted for the middle range if the 160m band is desired or alternatively the existing coils could be padded up with trimmers.—G. L. K. Crawford, B.Sc. C.Eng. (Tonbridge, Kent).

The art of unsoldering

I was recently faced with the unenviable task of unsoldering numerous components from a printed circuit board, the job being further complicated as I had no "desoldering" tool.

To overcome my difficulties I made use of an old foot pump. After removing the original connector, I fastened a piece of rubber tubing to the outlet of the pump. To the other end of the tube was inserted an old ball-pen case. This provided me with an excellent tool with which to blow away molten solder from the joints.

l find a pair of arterial forceps (obtained from a local surgical shop) just the job for a heat sink, as they can be locked on a wire and left, thus leaving both hands free.— A. Parkinson (Grimsby, Lincs.).

Me too!

I wonder how many of your readers are being duped daily by the actions of firms advertising in your pages? Like Mr. Haworth (Letters, March issue) I too required a crystal for a project. I wrote to a firm whose name appears regularly in your magazine requesting a copy of their list of transistors, and their 24-page illustrated brochure on Valves and Quartz Crystals for which I enclosed a postal order for one shilling.

An envelope duly arrived in which were six mail-order forms, the list of transistors, a leaflet giving information and prices of components for a superhet receiver, and a coloured pamphlet extolling the contents of their new 1968 catalogue which could be obtained for eight shillings and six pence no Quartz Crystal list, and no postal order!

The mind boggles at the fortune these people must be amassing from the odd shillings pouring in from people like Mr. Haworth and myself!—Harry B. T. McLaren (Cheshire).

Members wanted

Would anyone be interested in joining a new Radio Club (Fulford & District Amateur Radio Club) Nr. York, with premises behind the Social Hall in School Lane, Fulford, please contact me.—G. B. Widnall, G8ATJ Hon. Secretary, 5 Heslington Croft, Fulford, York).



Books reviewed on this page are normally obtainable through any retail bookshop. In this instance, the information printed in heavy type should be auoted.

TRANSISTOR TECHNOLOGY

By Robert G. Middleton. Published by Foulsham Sams. 288 pages, $8\frac{1}{2} \times 5\frac{1}{2}$ in. Price 30s.

T HIS book appears to be originally intended for the American market and was reviewed with some trepidation. However, all fears regarding confusion proved groundless, and, like mathematics, the basic principles of semiconductors are the same in any language. There are four pages at the beginning which discuss any slight misunderstandings which might arise.

The book would be ideal for students taking telecommunications and who need a basic primer in the field of transistors and diodes. Others, whose knowledge of semiconductors is a little vague or needs brushing up, will also find this a very useful volume.

Starting with a brief coverage of solid state physics and the atomic concept, Transistor Technology goes into details of diode operation, describing the electrical and mechanical properties of solid state diodes, From here it explains the principle of transistor action, outlining the detailed physical construction techniques, electrical characteristics (gain and leakage, for example), and the use of various types of amplifiers. In addition, such useful information as feedback, equivalent circuits, bias stabilisation, and distortion is thoroughly presented.

A useful feature of the book is the questions at the end of each chapter forming a useful yardstick with which to measure how much information has registered. Model answers to these questions are included at the end of the book. Verdict-a useful addition to the bookshelf for the layman, and a handy volume for the student.-DLG.

HOW TO BUILD SPEAKER ENCLOSURES

HOW TO BUILD SPEAREN ENCLOSUNES By Alexis Badmaieff and Don Davis. Published by Foulsham-Sams Technical Books Ltd. 144 pages, 8≹ x 5≩in. Price 25s. Ξ

you find loudspeaker jargon infinitely 0 baffling? Are you likely to construct an exponential acoustical horn expansion, with $12\frac{1}{4}$ foot diameter mouth and 16 feet long? Or are you generally content with the humble radiogram, despised by the hi-fi-fanatic?

Whatever your audio interest, you are sure to find some of the answers to your questions in this stimulating book. What is more important, you will probably find, also, a number of new questions to which you may not have previously given much thought. It is that sort of volume.

The authors preach the need for a good enclosure, designed to suit the driver unit, if any serious listening is intended. The days of "bung it in a box" are far behind us. From the several detailed constructional designs, it should be possible to find an enclosure to suit most purposes, even though most of the driver units are transatlantic in origin. There are many similar units-and I submit, a few better designs-available in this country.

The book covers Infinite Baffles, Bass-reflex enclosures, Horn enclosures, Labyrinths, and Crossover networks, as well as discussing enclosure design and the theory of driver units. A few details of electronic and acoustical measurement are given, but this is primarily a practical book, amply illustrated, occasionally controversial and never dull. Recommended for all except those with cloth ears.-HWH.

THE PRACTICAL AERIAL HANDBOOK

By Gordon J. King. 8[‡] x 5[‡]in. Price 35s. Published by Odhams. 224 pages,

LTHOUGH Mr. King is an established writer, I regret that I am unable to review this book with much enthusiasm.

"Practical Aerial Guide" would be a more suitable title since handbook is usually the title for those works which delve deeply and often technically into a subject, far more so than the author. The inside flyleaf claims that "Expert guidance is given on choosing the best aerial system to suit any particular purpose". This is rather a sweeping statement and the book does not substantiate this.

The volume contains a great deal of useful information, of this there is no denying; however, many of the illustrations appear to have already made their debut in *Practical Television*. There are informative and useful chapters on propagation, feeders, signal combining and splitting, shared aerial systems and TV interference. A section on signal boosters is notable in including circuit diagrams with all component values given. But the chapter "Practical Aerial Systems", while containing plenty of theoretical material, stops short of providing actual practical constructional details.

One startling constructional detail is the use of a four-foot ferrite rod 3in. in diameter on which the reader is advised to wind a coil to "load" an aerial.

The book is, in general, well written and certainly well illustrated, but for my money it's a subscription to Practical Television every time.-DLG.

AMATEUR RADIO CALL BOOK (1968 Edition) Published by the Radio Society of Great Britain, 28 Little Russell Street, London, W.C.1. 104 pages. Size 9% x 7% in. Price 6s.

r HIS new edition, like its predecessors, lists in call sign order the addresses of licensed amateurs in England, Wales, Scotland, Channel Islands, Isle of Man, Northern Ireland and Eire. More than 1,800 changes of address, reissued calls and cancellations have been recorded, in addition to 900 new call signs since the 1967 edition. For the first time, a list of British amateurs holding reciprocal licences with other countries is given.

Miscellaneous information includes amateur prefixes (by both prefix and country order), Inter-national Q Code, Great Circle bearings from London, a list of R.S.G.B. affiliated societies and clubs, Zonal and Regional boundaries, etc.

If you are active on the air or as a SWL you will need a copy of the Call Book.—DC.



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64



A SIMPLE MUSICAL TOY

LTHOUGH it is easy to build an oscillator to function in the range 100-1,000c/s (middle C being about 260c/s), this signal, where heard directly from the loudspeaker is not very musical. In small electronic musical instruments the use of a small loudspeaker is another factor which contributes to a very poor tone being achieved. However, if the loudspeaker is used only as a source of vibrations which causes a larger structure to resonate, it is then acting like the reed in a clarinet which on its own has no great musical value. A clarinet relies on a change in the properties of a resonator in order to change the note, an electronic instrument can change the frequency at which the "reed" is vibrating.

The Circuit

The circuit used is shown in Fig. 1, it consists of a multivibrator, which is tuned to operate in the frequency range required, and a simple class A amplifier capacitively coupled to it. The frequency

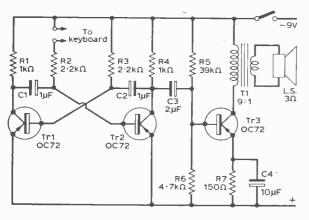


Fig. 1: Circuit for the simple musical toy.

at which the oscillator works is altered by the addition of resistances in series with R2. The methods of tuning and keyboard construction are discussed later.

Construction

The instrument was built on a base board 12 x 18in. of $\frac{1}{4}$ in. plywood. Square ($\frac{1}{2}$ in.) wood strip was used to mark the outline of the resonator box, and was glued into position on the base board (as shown in Fig. 2). The top of the box was made of $\frac{1}{8}$ in. plywood 12 x 4 $\frac{1}{2}$ in. A hole 2 $\frac{1}{2}$ in. in diameter was cut in the centre of the plywood with a fret-saw, so that a 2 $\frac{1}{2}$ in. miniature speaker could be fitted facing

J. M. WATT

into the box. The top was glued on to the box, and the speaker was glued into its position over the hole in the top. On one side of the speaker two 4in. lengths of $\frac{1}{2} \times \frac{1}{2}$ in. wood strip were glued 3in. apart to hold the 4in. square sheet of Veroboard on which the electronic circuit was mounted. On the other side of the speaker, two similar strips were mounted to steady the battery. Since a PP9 battery was used, these strips had to be $2\frac{1}{2}$ in. apart. The battery was secured by a strong rubber band stretched over it between panel pins half protruding from these blocks.

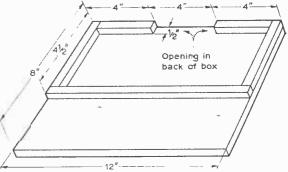
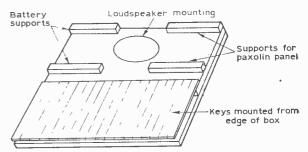
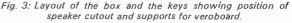


Fig. 2: Constructional details including relevant dimensions of the box on the base boærd.





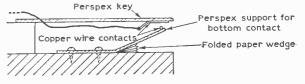


Fig. 4: Constructional details of suitable but simple keys showing positioning of keying contacts.

The keyboard consists of eighteen strips of $4 \times \frac{2}{3} \times \frac{1}{16in}$. Perspex. Each key has a thick gauge wire

contact on its underside, with a length of thinner wire soldered to it. The keys are pressed on to a common contact which is a thick copper wire supported on four flexible 1/16in. Perspex supports so that the key will give after contact is made, this gives the keyboard a more pleasant feel, and reduces noise from the keys. The copper contacts are glued to their Perspex supports.

When the keyboard has been completed, the electronic circuit may be screwed on to its supports. One of the terminals leading to the keyboard is connected to the common base contact of the keyboard. The second terminal is connected through a tuning resistance to the key, each key having a different tuning resistance for a different note.

Preferred Values

It is possible to tune an instrument using standard resistance, but this suffers from three main disadvantages:

1. Resistances are only available in standard values which may not coincide with any note required, although by combination of components it should be possible to obtain all the necessary notes.

2. Resistors are not made to high accuracy so may not give the required note.

3. Since other components are of doubtful accuracy experimentation with resistors is necessary, and this increases the expense of the instrument. If, however, it is decided to tune the instrument using standard resistors, values of 0-10k Ω will give a range of about three octaves, the higher resistances producing lower notes.

Simple Tuning

A cheaper and more accurate method of tuning the instrument is to make resistors of the correct value. This can be done quite simply by using a thin film of graphite. If a wire lead is taken from the keyboard terminals and laid along the base of the Perspex keys, it can be inlaid into the Perspex by putting a hot soldering iron on to it until the Perspex softens and the wires start to sink into it. The wire

should be held down with a pair of pliers until the Perspex resets around the wire; only short sections of wire can be done at a time, so the process should be repeated along the length of keyboard. The the wire from the contact

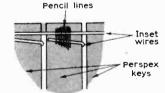


Fig. 5: How the wires are inset and tuned with the aid of a soft pencil.

on each key should be inlaid into the key in the same way so that the two wires tie parallel about 2mm. apart. The wires are then bared, and the Perspex between them roughened by sandpapering the area. With the key prepared in this way, it is now ready for tuning.

With the key depressed no note will be produced until contact is made by scribbling across and between the two wires with a soft pencil until enough graphite has been deposited between the two wires to create the resistance required to give the note wanted.

The keyboard consists of eighteen keys, but some may wish to extend the keyboard with a second one above it for "black" notes.

CO! CO! CO! CO! CO! CO!

ISSUES WANTED

... November 1964 issue of Practical Wireless.-A. Holmwood, 8 Dock Street, Pembroke Dock, Pembs. , a copy of the July 1967 issue of Practical Television .- M. Hews, 28 Oak Tree

Cose, St. Ives, Huntingdonshire.copies of *Practical Wireless* for the years 1964, 1965 and 1966.—R. James, 14 Hotblack Road, Norvich, Nortolk.

Hotblack Road, Norwich, Notion, ... issues of Practical Wireless containing details of VALVE version of a switched v.h.f. tuner (the transistor one was in August 1967). Issues required are believed to be April 1965 and possibly May and June 1965.—S. Fisher, 146 Hilton Street. Springfields, Wolverhampton, Staffordshire.

. Practical Wireless Issues between May 1964 and October 1966 Inclusive .-- S. V. Austen, Hamilton House, Stone Cross, Bilsington, Ashford, Kent. , the August 1960 Issue of Practical Wireless .-- J. Brown, 38 Muirfield, Perth,

Scotland. The September 1965 issue of Practical Wireless .- Tan Ke Huat, 19 Wolsket

Road, Singapore 13. , a copy of the January 1966 issue of Practical Wireless .--- J. Evans, Tyddyn Y Garreg, Glanrafon, Corwen, Merionethshire.

the November and December 1964 issues of Practical Wireless, covering "Preparing for the R.A.E." parts 1 and 2.-A. Givens, 41 Veronica Crescent, Kirkcaldy, Scotland.

. . Copies of the periodical "CQ" dated from August 1966 to April 1967 inclusive even loan for a week would be greatiy appreciated .-- D. Hule, Marieville, Campbeltown, Argyll.

town, Augur. ... the Issue of Practical Wireless containing details of the "Multipurpose Audio Switch" by F. L. Thurston.--I, Grewar, 55 Dens Road, Dundee, Angus, Scotland. ... the January 1957 Issue of Practical Wireless containing details of the "Explorer v.h.1. Receiver".--T. Cridland, "Whitworth", Zuyder Road, 60 Acres, Canvey Island,

Essex. . . . the copy of *Practical Wireless* dated November 1953 containing details of an electrically-operated coil winder.—A. Moat, 29 Dwyer Street, Toowoomba, Queensland, Australia.

... Issues of Practical Wireless, January 1967—June 1967 Inclusive.—A. Staneveld, "Hollingside", 127 Weildon Crescent, Harrow, Middlesex.

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LUF 50 volt	8µF		64µF	2.5 volt 9 volt
1.25µF 16 volt	8µF 8µF 8µF 8µF 8µF 8µF	350 volt	100µF	3 volt
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2µ1 10 voie	8μF 8μF	275 volt		12 volt
2μF 150 volt 2μF 350 volt	10μF 16μF	25 volt 150 volt	200µF 200µF 200µF	3 volt 4 volt
$2.5 \mu F$. 16 volt $2.5 \mu F$. 25 volt	10 μF 16 μF 20 μF 20 μF 20 μF 20 μF 25 μF 25 μF 25 μF 25 μF 30 μF 40 μF 40 μF	3 volt	200µF	16 volt
	20µF	6 volt 9 volt 15 volt	250µF 250µF 250µF 320µF 350µF 350µF 400µF 400µF	2.5 volt 9 volt
3μF 25 volt 3·2μF 6·4 volt	20µF	15 volt	320µF	2.5 volt 9 volt
3.211F 64 volt	25μF	6 volt 12 volt 15 volt	350µF	10 volt
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4µF 25 Von	30µF	6 volt	400μF 500μF 500μF 	4 volt
4µF 100 volt	30µF	10 volt 3 volt	500μF 640μF	6 volt 2-5 volt
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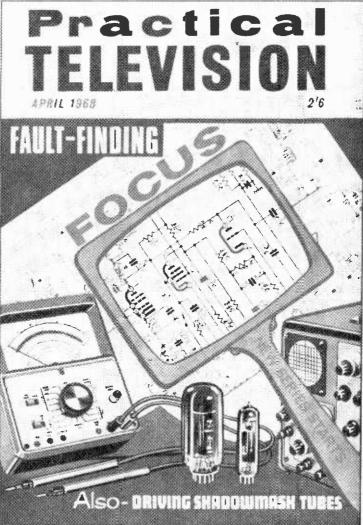
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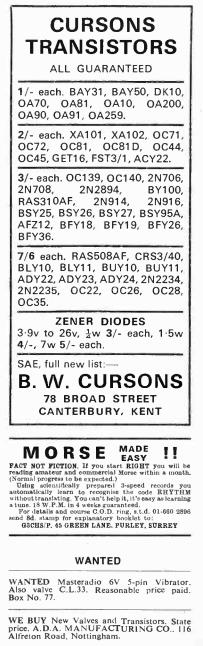
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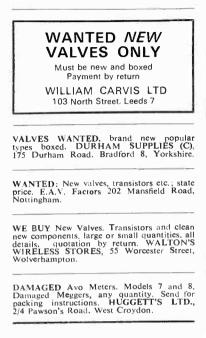
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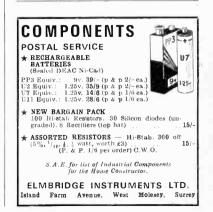
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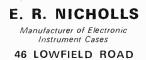
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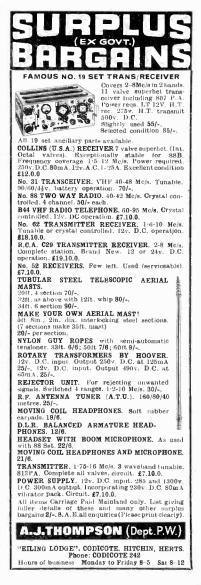
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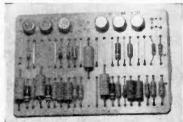


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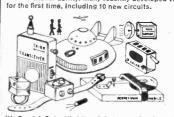
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