## PRACTICAL WIRELESS <br> JANUARY 1968

## Special

 INTEAMITTENT FAULT LOCATOR OLEABNING MOREE- SIMPLE BUESTTHUTION EOX

IN THIS ISSUE



THE gTVEMAN

STEP BY STEP GENERAL PURPOSE RECEIVER

SOLDERING EQUIPMENT


FOR CATALOGUES APPLY DIRECT

17in.-£11.10.0

* Components Carr. 30/-

TWO-YEAR GUARANTEE EX-RENTAL TELEVISIONS
$\star$ -
free illustrated
LIST OF TELEVISIONS $17^{\prime \prime}-19^{\prime \prime}-21^{\prime \prime}-23^{\prime \prime}$
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TWO-YEAR GUABANTEED TUBES $100 \%$ REGUNNED 14in.-69/6 17in.-39/6
211n. and ALL SLIMLINE TUBES 99/6 EXCHANGE BOWLS. Carr. $10 / 6$
EX MAINTENANCE TESTED TUBES

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\text { 17in }-35 /-14 \mathrm{in}-15 / \text { - Carr. } 5 / \text { - (not slimline) }
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We offer you lally tensilised polyester／mylar and P．V．C．tapes of identical quality hi－fl，wide range recording characteristics as top grade tapes Quakity control manufacture．They are truly worth a few more coppers tham TRY ONE AND PROVE IT YOURSELF．

| Standard Play |  |  | Long Play |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3 in ． | 150 ft ． | 2／3 | 3in． | 225 ft ． | 2／9 |
| 4 in ． | 300 ft ． | 4／6 | 4in． | 450 ft ． | $5 / 6$ |
| 5 in． | 600 it ． | $7 / 6$ | 5 in ． | 900 it ． | 10／6 |
| 5 l in． | goort． | 10／6 | 51 in ． | 1，200ft． | 13／－ |
| 7in． | 1，200ft． | 12／6 | 7 in ． | 1，800ft． | 18／6 |
|  | Double Play 300 ft |  | 4in． | Triple Play 900 ft ． | 13／－ |
| $3 i n$. $4 i n$. | 300 ft ． denft． | $87-$ | 5 in ． | 1．800it． | 25／－ |
| 5 in ． | 1，200 fl ． | 15／－ | 5 in ． | 2.400 ft ． | 341－ |
| $5{ }^{3} \mathrm{in}$ ． | l．Niogit． | $19 / 6$ | 7 in ． | $3,606 \mathrm{ft}$ ． | 44／－ |
| 7 in ． | $2,400 \mathrm{t}$ ． | 271－ | 3 in | adruple Pla fionft． | 8／6 |

Post Free leas $5 \%$ on three recls．
Qusntity and Trade enquiries invited．

## MAINS－BATTERY

Microsonic 7
7 TRANSISTOR RADIOS Superbet，full medium wave coverage amazing volume．clarity and sensitivity from built－in PM speaker．Solid leathe poedet wallet．Fabulous present．Huge purchase enables us to onter at a fraction o and performance your moner will be refunded，il returned within 29／－ 14 days）．
2 SETS of rechargeable Cadmium Cells to at．Only 10／－extra．
CHARGER：200／250V A．C．tor Cldmium Cells．Charges 2 batteries at once，Cumplete with 5 amp plug．10／－extra．

## 100 HI－STABS

CO－AX，low loss．Bd．yd．， 25 yds $11 / 6$ 50 yds．22／－： 100 yds ．42／6．Plu⿷s $1 / 3$ 100 RESISTORS 8IZES－L－3 watt．
MICROPHONE CABLE．Highest quality black，grey，white，9d．per Fard．
100 CONDENSERS
Miniature Ceramic，Silver．Mica，etc．．3pF to $5 \mu \mathrm{~F}$ ．LIST VALUE OVER 84 ．
25 ELECTROLYTICS
Assorted 2 to 500 mFd 6 to 4 volt．LIST VALUE OVER 85.

## Transistorised FM Tuner

## 

## SRP12 <br> AT5 Model 1.000 <br> Model 2.000

£4．7．6
12．15．0

Model 3.000
ATB
401
Mono dual cartridges ：$\quad$ \＆27．10．0 $\begin{array}{ll}\text { Stereo ceramic cartridges } & 19 / 6\end{array}$
PLINTHS
Universal fitting de luxe Teak 10r SP25． $1.000 .2 .000,59 /=$
3.000. AT60 Ditto Perspex Cle
Ditto Perspex Clear
View Cover，Complete 5.15 .0 LAB80，401，Superb Teak／Pers－ $\begin{aligned} & \text { pex top finish plinth } \\ & \text { Normally } 212.10 .0\end{aligned} \mathrm{f} 9.19$.

This beautifully compact 6 transistor machine（size $6 \times 4 \mathrm{x}$ 2tin．）will give quieter，more interference free reception．Months of use from a standard 9 volt battery or its small power requirements can be
drawn from any amolifier．Low noise draw changer．Smooth 2 gang tuning Ireq．ebanger．Smooth 2 gang tuning
feeding no less than three I．F．stages feeding no less than three I．F．stages terminating in an L．F．stage giving smple obligation at all


## REDUCED PRICE DUE TO HUGE SALES <br> <br> E6．10．0 <br> <br> E6．10．0 <br> （3 FOR E18）

a－BAND AM／YM RADIOS
Well－known Caroline Portable covering L．W．，M．W． and F．M．Bands．Gets all the BBC prorrammes． complete with leather case and accessories， 8 Gns．
amazing value． amazing value．
radiogram chassis
With Coramic $10 \times 5 i n$ ． 1 all range speaker，All wave． current manulacture，heavy A．C．type with large Complete valves．De luxe wovo

12 Gns．
With two $10 \times 5 \mathrm{in}$ ．speakers． plinth record players
ype AM80 4－watt smplifer．Garrard SRP12 Deck with dual cartridge，with eliptioal
speaker．Dust cover，worth double．
$\quad \frac{1}{2}$
Gns． 2－SPEAKER VERSION－As above in Vyanide，dove grey fnish with 2nd speaker in detach－ $9 \frac{1}{2}$ Gns．
able cover．Wonderful present．

## BARGAIN PARCELS

neluding variable condensers，i．t．coils，loudspeaker plus／sockets．Knobs，pots，oondensers，resistors，nuts bolts，cabinet fittings，switches，transformer choke rectifier，transistors at a amall Iraction of list value Due to heavy demand we now pack them in several sizes－be amazed－try one now
tbs．（post 3／－）
14 lbs．（post $6 /-$ ）
$17 / 6$

50 TAG STRIPS Mixed sizes 2 to 15 way

## 25 POTENTIOMETERS

 Including with switch，long and short spindle，pre－sets，log and lin unased． $1 \mathrm{k}-2 \mathrm{~m} \Omega$ ，
## CONNECTING WIRE

## PV．C．Bright Colours．Five 25tt．

 P．V．C．Brigcoils only．

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 VALVES
## $\star$

BY RETURN OF POST—GUARANTEED 3 MONTHS Satisfaction or Money Back Guarantee on goorls if rethrned unused within 14 days． TRANSIT INSURANCE．POSTAGE 1 valve 日d．2－11 6d．per valve．＇Free over 12

 | $1 \mathrm{L4}$ | $2 / 3$ | 6 Q 7 AT | $7 /-30015$ | $11 / 6$ | ECC81 | $4 / 9$ | EZ81 | $6 /-$ | PY88 | $8 / 8$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1S4 | $4 / 9$ | 6 Q 7 GT | $8 / 9$ | 30017 | $10 / 6$ | ECC82 | $5 / \mathrm{F}$ | $\mathrm{FC4}$ | $8 /$ | PY800 | $7 /-$ |




 |  | Z4G | $6 / 9$ | 6 V 6 G | $4 / 9$ | $30 \mathrm{P4}$ | $11 / 6$ | ECC88 | $9 / 6$ | $\mathrm{KT68}$ | $5 / 9$ | TDD4 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| ECF80 | $7 / 9$ | KT68 | $19 / 6$ | U14／18 | $7 / 6$ |  |  |  |  |  |  |






 $\begin{array}{ll}\text { 6BW6 } & 7 / 1 \\ \text { BBW7 } & 51\end{array}$ ${ }^{C 6}$ C8 $41 /-$ $\begin{array}{ll}8 \mathrm{CD} 6 \mathrm{G} & 17 \\ 6 \mathrm{D} 6 & 4\end{array}$ 6F1 BF23
BJ5G

 | JK7G | $2 / 8$ | 1487 |
| :--- | :--- | :--- |
| $19 A Q 5$ |  |  | BK8GS L1 1



## TRANSISTORS

GUARANTEED TOP QUALITY Mullard Matched Output $12 / 6$
Kits OC18D and 2－0C81


| 3F118istirs． |  |  |  |
| :--- | :--- | :--- | :--- |
| AF114 | $6 / 6$ | OC44 | $5 /-$ |
| AF115 | $6 /-$ | $0 C 45$ | $4 / 6$ |
| AF116 | $8 /-$ | 0072 | $5 /-$ |
| AF117 | $5 / 6$ | $0 C 81$ | $5 /-$ |
| AF127 | $5 / 6$ | $0081 D$ | $4 / 6$ |
| OC26 | $7 / 6$ | 00170 | $6 /-$ |
| OC85 | $9 /-$ | OC171 | $6 /-$ |

GERMANIUM DIODES General Purpose miniature 8 d． detector or $8 / 6$ doz gold Bonded Top Grade $1 /=$
（9／6 doz．）． SILICON RECTIFIERS （inaranteed performance．Top


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Factory fresh less Cartridges
SRP12 110／230v
59／－
AT6 мк．ІА $\quad 9 \mathrm{ghs}$
Mono first－grade Cartridges．．．．．．．．．12／6 Stereo Ceramic Cartridges．．．．19／－extra．

4 －spd heavy turntable player E／M1 $200 / 250 \mathrm{~V}$ with lightweight pick－up（dual cartridges
10／－extra） 49／－
$C O L \angle A R O \quad \begin{aligned} & \text { 4－speed Battery } \\ & \text { Model worth £7 }\end{aligned}$ with lightweight pick－up
（matching dual cartridge 49／－ $10 /$－extra）．Postage 5／－（extra all mode／s）

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LP－ACOS GPB5／B7 LP－RONETTE BF40／LP－GARRARD GC2 LP
SPEAKERS．［2im．Tound high quedly British hitecs twetter come， 6 witio，in $3 \Omega$ or

 MICROPHONES．LAPEL／HAND MIKE－1／in．dia．Lapel Clij，ideal for Lape record－ ing．With leat．Very вensitive．7／6．P．\＆P．
CRYSTAL HAND MIKE．Robust and sensitive．Cream plastic case．Just the thing
STUDIO CRYSTAL MIKE．Professional，Omni－directional，providing features usually
only available at many thmes the price．Sensitivity－50dB．Reaponse－50－12，000 only a wailable at many threes the price．Sensitivity－ 50 dB ．Respotise－ $50-12,000$ c．p．s．Black Plaktle with punched chromium case，sulvels．stand huliler and ghielded
cable．Onis $48 /-$ ．P．\＆P．2／．The stand below fits this mike ss（well as many others）． ACOS MIC 40 －World fimous Desk Mike．13／9 plus P，if $1 / 3$. ACOS MIC 45 －splendjd Curved Hand Grlp Crystal Mike， $14 / 6$

TELESCOPIC FLOOR STAND．HEAVY BASE．Standird thread，ext．to 4 ft .7 in ． 48／6，Carriage and Packing 4／6．
TELEPHONE PICK－UP COIL．For recording or amplifying both sifes of telephone INTER－COMM．DE－LUXE 2－WAY．Highly efficient．Bafe BABY ALARM．Works INTER－COMM．DE－LUXE 2＂WAY．Highly effetent．sail BABYAL batiery， $55 /-$ P．dP． $2 / 6$ ．
 Over 5 W per channel．Size $121 \times 6 \times 47 \mathrm{n}$ ．Controls for Gram，rablio，tape，basa，ireble， AMPLIFIER．Compmet for use in mains portable grams 61 x 24 x 5 in．，printed circult，vol．
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4 TRANSISTOR 3W AMPLIFIER，slize $2 \% \pi 28 \times 1 \neq \mathrm{in}, 3,8$ or $15 \Omega$ output． 9 volt irattery operated．Hishly sensitive．Price（less batters）52／B．P．\＆P．1／6 RECORD PLAYER DECKS．GARRARD．
Autoehangers 4 apeed
MODEL 1000
$\begin{array}{llll}\text { MODEL } 1000 & £ 8.6 .0 \\ \text { MOL } \\ \text { MODEL } \\ 2000 & \text { £6．16．6 }\end{array}$

A 70 MK ．II
Single Players
SP25 4 speed Light T／Table 29．19．6（less cartridge）
All latest models complete wlithnono cariridge（except 81²5）．Stereo 10／－extra．
P．© P．all nodela $7 / 6$ ．Price SP25 4 speed Heary T／Table
SRP22 3 вpeed
£10．19．6（less cartridge）
£4．19．6
B．S．R AUTOMATIC RECORD－CHANGER DECES．LATEST MODELS UA25－Very popular－4 \＆peed．Cap．six 7in．， $10 \mathrm{in} . .12 \mathrm{in}$ ．records 2518
26 UA ${ }^{2} 5$ SS slim deajgn－tirst class 4 epeed，two－tone grey

MAGNAVOX＂383＂TAPE DECKS．LATEST MODELS．WORLD FAMOUS． $131 \times 11 \times 5 / \mathrm{n}$ ，below hoard，t＇or $200 / 250 \mathrm{~V} 50$ eycles A．C． 3 speed，digit counter piano key controls，Jin．reels．Fercy modern feature．Speeds $17,3 \%$ and 7 i i．p．s． With $\frac{1}{\text { track Braimatic heads，} £ 10.10 .}$

PICK－UP CARTRIDGE REPLACEMENTS（Standard Fitting tor all Record Players ACUB GP／B7－2 MONO 12／8．ACO8 G1／73．2 BTEREO 25／－．ACOS GP／O1－1 MONO Finest Quality British made MYLAR Recording Tape．Fully Guaranteed．In Carions
 $5_{4}^{3} \operatorname{in}$ ．R501t．Standard Play 7 in．I200f，Standard Play 5in， 9001 t ．Tong Play $\quad 12 / 6 \quad 57 \mathrm{in}$ ． 1800 ft ．Double Play \＆P．Four reels and over post paid． 1＇\＆P．I／－per reel．Four reels and over post paid．
POCKET MULTX－TEST METER． $1000 \Omega$ per volt．Volts 0／10／50／250／500／1000 A．O． abd D．C．Current： $0-1-100-500 \mathrm{~mA}$ ．Resiatance： $0-100 \mathrm{~K} \Omega$ ．Complete with test
 （ $20,000 \Omega \mathrm{l}^{\prime}$ ．V．） $0 / \overline{5} / 25 / 250 / 500 / 2500 \mathrm{D}$ ．C．Cursent $0-50$ micro amy $/ 2 \cdot \overline{\mathrm{~b}} \mathrm{~m} \mathrm{~m} / 250 \mathrm{Am}$
 with batiery．instructions，jeads $72 / 6$ ．
TRANSISTORS：Some popular typer from our range：OC44 ami OC4 $3 / 6$ each． OC71 2／9．UC72 3／8，OC81 and OC41D 3／－each．OC1693／9．OC1703／6．AF1174／－ OG26 \％／6．GET8 5／8．General purpase（Approx．OC71）1／－each
NEW HIGH FREQUENCY TRANSISTORS．Sinclair STI 40 4／－；ST141 8／－．both capable of operating up to $700 \mathrm{Mc} / \mathrm{B}$ ．ALSO MAT1007／8．MATIO1 8／6．MAT1207／9． MAT121 8／6．ADT140 15／－．High speed switching transistors：BSY26，BSY28， 73SY $65,5 /$－each．
THYRISTORS．
THYRISTORS． $100 \mathrm{PIV} 5 \mathrm{~A}, 12 / 6$.
up to 3.
R．F．FIELD INDICATOR．For use with redio controlled models．Checks radiation from existing antenna．Tunes 1 to 250 Mc in 5 banda．Senaitive 200 mA meter move－ ment． 5 section plug－in aerial．Phone jack and cryatal earpiece for monitoriug． No bathery required．Pourerif magne
TERMS．Cish with order．No C．O．D．Orders total \＆5 atsd over gent carriage paid （excenting record player deck where earriage is shown）．Guaranteed money refunded if goods returned purfect within $\bar{y}$ days of despatch．

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| :---: | :---: | :---: | :---: | :---: | :---: |
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| RX60N | Communication Receiver | E27 15 | 0 | f23 12 | 0 |
| PA539 | 30 Watt Mains P．A．Amplifier | £29 10 | 0 | f25 | 6 |
| AFM200 | Hi－Fi AM／FM Tuner | E29 10 | 0 | £25 | 6 |
| SA200 | 15 Watt Integrated Stereo Amp | £27 15 | 0 | f23 1？ | 0 |
| FMT640 | Hi－Fi FM Tuner | E24 17 | 6 | £21 12 | 6 |
| SA100 | 10 Watt Integrated Stereo Amp | £1818 | 0 | f16 | 6 |
| VTA40 | All Transistor Stereo Amp．． | £39 10 | 0 | £33 11 | 6 |
| VFM40 | All Transistor FM Tuner | £12 19 | 6 | £11 2 | 0 |
| TSA10 | 10 Watt Transistor Amp | E1319 | 6 | f11 19 | 6 |
| FMT10 | All Transistor FM Tuner | E13 19 | 6 | £11 19 | 6 |
| TSA20 | Transistor 20 Watt Amp | £23 2 | 0 | f19 16 | 0 |
| MS80 | 15 Watt Rosewood Speaker System | £14 14 | 0 | E12 12 | ， |
| HT20 | Rectangular Horn Tweeter | f4 2 | 6 | f3 10 | 6 |
| DM18HL | Dual impedance Dynamic Mike | ¢6 6 | 0 | f5 | 0 |
| FMT41 | Battery operated FM Tuner | ¢8 10 | 0 | f7 4 |  |
| FMT51 | LW／MW／FM Tuner，battery operated | £13 19 | 6 | f11 19 | 6 |
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| D12 | Car Defroster | ¢1 8 | 6 | £1 | 6 |
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| 1A7GT | 716 | 134 | 11177 | $4 /$ | 76 | CL84 77－ |  | 8／3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 \mathrm{H6GT}$ | $7 / 3$ | 10 Fl 9／8 | DH81 | 12／6 | EF＇183 6／6 | PCL．85 8／3 | UCH2＋2 | $8 / 9$ |
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| 1 R 5 | 5／6 | 124T7 3／9 | DK9 | $5 / 6$ | EH90 6／6 | PENA4 $6 / \theta$ | tCIm | 7－ |
| 184 | 4／9 | $12 \mathrm{AU6} 4 / 9$ | DKY | 81－ | Ela3 6／6 | PEN36Cl5／－ | UCL | $8 / 9$ |
| 185 | $3 / 9$ | 12AU7 $4 / 9$ | DK96 | 6／6 | EL41 8／6 | P1PL300 13／－ | L＇H | $8 / 9$ |
| 1 T 4 | $2 / 9$ | $12 \mathrm{AX7} 4 / 0$ | DL33 | 6／9 | ELJ84 4／9 | P1 336 9／－ | U178 | $71-$ |
| 3 A 5 | 71. | 12K8GT 7／8 | DL35 | $5 /-$ | LL90 5／－ | PL81 8／9 | U F＇8 | ／9 |
| ＋ | 5／6 | $20 \mathrm{~F} 210 / 6$ | 1L92 | $4 / 9$ | EL95 5／－ |  | U1．4 | $8 / 9$ |
| 384 | $4 / 9$ | 80LL 14／8 | DL94 | 5／6 | EM80 5／9 | PL83 6／3 | U14 | 20／－ |
| 3 V 4 | 516 | 24 Pl 9／－ | DL9 | 6／－ | EM81 8／9 | PLR4 6／3 | UL8 | 6／－ |
| $5 \mathrm{U4G}$ | $4 / 6$ | ${ }^{20} \mathrm{P} 314 / 9$ | DY86 | $5 / 9$ | EM84 8／3 | PL500 13／－ | UY゙1 | 16 |
| 5 V 40 | 8／－ | $20 \mathrm{P}_{3}$ 17／－ | UY8？ | $5 / 9$ | EM87 6／6 | PX25 719 | UY8 | 4／9 |
| 5Y3G＇1 | 5／－ | 25 U －${ }^{\text {T }}$ T11／6 | EABC8 | 6／－ | EY51 6／3 | PY32 8／6 | $V^{1}+13$ | 10／6 |
| 574G | $7 / 6$ | $30 \mathrm{Cl} 511 / 6$ | EAF4： | 8／6 | RY86 6／－ | PY33 8／6 | YP132 | 211－ |
| 6／30L2 | 11／9 | 30 Cl 7 12／6 | EB91 | 2／8 | EZ40 6／9 | PY80 5／3 | W7\％ | $3 / 6$ |
| 6A． | $2 / 3$ | 30C18 11／8 | EBC33 | 71. | EZ41 6／9 | PY81 5／3． | 27 | 3／6 |
| 6Ast | $3 / 6$ | $30 \mathrm{F5}$ 12／－ | E13C41 | 8／－ | E780 4／6 | PY82 5／－ | Transis |  |
| 6A45 | 4／9 | 30ドLI 13／9 | E，BFx0 | 8／－ | E781 4／8 | PY83 5／9 | ACLO | 10）－ |
| 6ATt | 4／－ | $30 \mathrm{FLL14} 12 / 6$ | \＆BF＇R9 | $5 / 9$ | GZ322 81－ | $\begin{array}{ll}\text { 1 P88 } & 7 / 3\end{array}$ | ACI27 | 6！－ |
| 68A6 | $4 / 6$ | $30 \mathrm{Ll} \mathrm{S}^{3} \mathrm{12/-}$ | ECU81 | $3 / 9$ | KTfi 6／8 | PY800 6／－ | A11440 | 15／6 |
| 6 BE 6 | 4／3 | 301.17 13／－ | ECC＇82 | 4／9 | $\mathrm{K}^{\text {T81 }} 12 / \mathrm{F}$ | PY807 6／－ | AFl02 | 18／－ |
| Babc | 15／－ | $30 \mathrm{P} 412 /-$ | CC83 | 71. | N18 5／6 | R19 7／－ | AF115 | 61 － |
| 615．J6 | $6 / 9$ | 30 P 12 11／－ | CC8 | 6／3 | N78 14／9 | R20 12／9 | AF11 | $8 / 6$ |
| 6 Bl | 719 | $30 \mathrm{P19}$ 12／－ | ECC8 | 5／6 | N108 14／6 | U25 11／8 | AFII | 5／－ |
| 60．st | 8／6 | 30 PlL 14／6 | ECF80 | 71 － | PC8H 8／－ | U25 11／6 | AFlı | $8 / 6$ |
| 6 F 1 | $7 / 9$ | 30PLI314／6 | ECF82 | $8 / 8$ | 1＇C88 81－ | U47 13／6 | AF12． | 7／6 |
| $6{ }^{61} 13$ | $3 / 6$ | $30 \mathrm{PLI+14/6}$ | ECF86 | 9／－ | PC97 5／8 | U49 13／6 | AF12． | $7 / 6$ |
| 6 F 1 | 9／－ | 35LAUT 7／6 | ${ }_{3} \mathrm{CH} 35$ | 6／－ | P6900 7／8 | U52 4／6 | AF＇12 | 7／－ |
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| 6 K | 1／6 | 3524Q＇T 4／6 | ECH81 | 5／3 | PCC89 9／8 | U191 11／－ | OC22 | 19 |
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(Normal) : this effect. INPUTS AND CONTROLS-CHANNEL ${ }^{2}$ (Normal): this contains two high gain input jack sockets controlled by Volume Control 2 , which is mounted directly above the sockets marked Normal. TREBLE: gives a controlied boost to the treble frequencies on Channel 2 only. GAINS VOLTAGE: fully adjustable, $200-250$ volts, A.C. 50 cycles. distortion. OUTPUT IMPEDANCE: 3 ohms. Price 21 gns , plus $£ 1$ postage and packing.
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| 185 | 4／－ | 6C5G | 4／－ | 61．6G； | $71-$ | 10LI | 8／－ | 2586  <br> 28 D 7 $5 / 6$ | 866 A | $13 / 6$ | DL96 | \％－ |  |  | GZ30 | 10／－ | PGFP80811／6 | U19 | 35／－ |  | 5／－ |
| 1 T 4 | 3／－ | 606 | $3 / 9$ | L18 | 51－ | 10LD11 | 15／－ | $\begin{array}{ll}2807 & 5 / 3 \\ 30 \mathrm{Cl} & 6 / 3\end{array}$ | ${ }^{854}$ | 4／6 | DM70 | 51－ |  | $301-$ | GZ ${ }^{5}$ | 9／6 | PCL8：7／－ | U－55 | 13／6 | YR1 | 0 |
| 3A4 | 3／8 | 8 B | 61－ | 7G | 81 | 10P13 | 15／6 | $30 \mathrm{Cl5}$ 13／6 | 1625 | $5 / 6$ | DY86 | 6／－ | E | $201-$ | \％ 234 | $10 \%$ | PCL83 8／6 | U26 | 13／6 |  | 5／－ |
| 3Q4 | 6／6 | 6CD6G | $201-$ | 6Q7GT | $8 / 6$ | 11 E 3 | 421－ | $\begin{array}{ll}30 \mathrm{Cl15} & 13 / 8 \\ 30\end{array}$ | 40242 A | $50 \%$ | DY87 | $61-$ | $\mathrm{EF3}_{7}$ | 2 | KT36 | 17／6 | PCL84 $\%$ | U78 | $3 / 6$ | －T 2 \％ | 15／－ |
| $3 \mathrm{Q5}$ | $6 / 6$ $4 / 9$ | W4 | 5／9 | ${ }_{68 \mathrm{SC}}{ }^{684}$ | $7 /-$ | 12AT6 | $4 / 6$ $3 / 9$ | $\begin{array}{ll}30 \mathrm{Cl7} & 14 /- \\ 30 \mathrm{C18} & 13 / 6\end{array}$ | 4763 | $101-$ | F888CC | 121－ | EF339 | 61－ | T61 | $12 / 6$ | PCL85 $8 / 6$ | U191 | $12 / 6$ | －T31 | 801－ |
| 384 384 | 4／9 | 60W4 | 12／8 | 68G7 | $5 /-$ | 12AT7 | 3／9 | $30 \mathrm{F5}$ 14／－ | 7193 | $2 /-$ | EA50 | 21－ | EF41 | $8 / 6$ | 66 | $181-$ | PCL86 8／6 | U251 | $12 / 6$ | VU111 | 7／8 |
| $5 \mathrm{F4GY}$ | 8 | 6E5 | $7 / 6$ | 6887 | 3／3 |  |  | 30 FLA 16／－ | 7475 | 4／－ | EABC80 | 6／6 | EF50 | $2 / 6$ | KT81 | 351－ | PENA4 201－ | U301 | 15／－ | VU120 | 12／6 |
| 5U4G | 4／－ | 6F1 | $9 /-$ | 68， 7 | 5／－ | 12 |  | 30 FL12 18／－ | ATP4 | $2 / 3$ | EAfr42 | $8 / 6$ | EF＇80 | 5／－ | KT81 | 7C5） | PENB4 20］－ | U403 | 6／6 | YU508 | $35 /-$ |
| 5V4G | 81 － | 6F6G | 8／－ | 6SK7GT | 4／9 | A6 |  | 30FL14 13／6 | ATP5 | 71. | LB41 | 4／6 | EF85 | 6／6 |  | 107－ | PEN45 7／－ | U404 | $10 / 9$ | W81m | － |
| 5 Y3＠T | 5／－ | $6 \mathrm{F6G}$ | 4／－ | 6＊L7GT | 4／9 |  |  | $30 \mathrm{L15} 1513$ | ATP7 | $5 / 8$ | EB91 | 3／－ | EF86 | 6／3 | KT8 | 251－ | PEN46 $2 / 9$ | U801 | 17）－ | － | － |
| 5749 | 6／9 | 6F8G | 4／6 | 68N7GT | 4／8 | 12C8GT |  | L0L17 14／3 | AU2 | 801 | EBC33 | 71 | 12F89 | 5／－ | KTW61 | （1） | PLas | UA |  | \％ | － |
| 6／301，2 | 13／－ | 6 F 11 | 71 － | 68Q7 | 6／－ | 1208G | 17／6 | 30 P 12 12／－ | AUS | 7／6 | EBC41 | $8 / 3$ | $\mathrm{FiP91}$ | $3 / 6$ | KT2 | 61－ | PLSL $7 / 6$ | AF42 | 8 | － |  |
| 6 A7 | 15\％． | 6 F 13 | $5 /$ | 6U4CT | 12／－ |  | $2 / 6$ | 30 P 19 13／－ | AZ1 | 8／－ | EBC90 | 4／－ | LF92 | $2 / 6$ |  | 17 | P | B | 8 － | XSG | － |
| 6 AB \％ | 12／6 | F14 | 12／6 | 6U5G | 7／6 | 12J5GT | 216 | 30PL1 15／－ | AZ31 | 9／－ | EB1880 | ${ }^{6 / 6}$ | E．1988 | $9 / \mathrm{-}$ |  |  | PL83 6／－ | UC81 |  |  | 7／8 |
| 6AC7 | 3／－ | $6 \mathrm{~F}^{2} 23$ | 13／8 | 6V6M | 81－ | T |  | 30 PL13 15／－ | CBL31 | 15／－ | EBP83 | 7／6 | KF183 | 8j－ | MUP4 |  |  | U8F89 | 8 |  |  |
| 6 AK 5 | 4／6 | $6 \mathrm{~F}^{2} 4$ | 12／－ | 8VtG | 4／6 |  |  | $30 \mathrm{PL14} 15 /-$ | $\mathrm{CCH}^{\text {Cla }}$ | $21 /=$ | EBF89 | ＋6／6 | EF184 | 6／－ |  | $7 / 8$ $12 / 6$ |  | CCCs | $8 / 8$ $8 / 6$ | E（1） | 50／－ |
| 6．45 | 3／－ | $6 \mathrm{~F}^{2} 25$ | 12／－ | 6V6G | $8 / 6$ |  |  | 35А馬 12／6 | CL．33 | 201－ | EBEL |  | E1．32 | $3 / 6$ | N37 | $10 / 6$ | PY：33 $14 /-$ <br> 18  | UCC85 | 8／6 | P | 19／－ |
| AM5 | $2 / 8$ | 6 F 28 | 11／6 | 6. | $3 / 6$ |  |  | $\begin{array}{ll}35 \mathrm{~L} 6 & 5 / 8 \\ 354 & 4 / 6 \\ 3574\end{array}$ | ${ }_{\text {CY31 }}$ | 10／－ | EBLL21 | 27／6 | ELi3 | 12／6 | N78 | 15／－ | PYB1 6／－ | UCF80 | $8 / 6$ | 5CP1 | 35／－ |
| 6AM6 | 3／6 | 6 6．16 | $2 / 8$ | $6 \times 56$ | 4／8 | 128A7 |  | $\begin{array}{lr}35 \mathrm{~F} & 4 / 6 \\ 3583 & 10 \%\end{array}$ | Dacriz | 7\％－ | EBL30 | $2 / 9$ | E1，34 | 9／6 | N N 108 | 15／－ | ${ }^{\text {PY8 } 215}$ | UCH 42 | 8／6 | C以1520 | 40／－ |
| 6AQ5 | 5 ／6 | ${ }_{6}^{655}$ | 2／6 | 6X5GT | $5 / 8$ | H7 |  | ${ }_{35 \mathrm{Fa}}^{35 \mathrm{GT}}$ 10／－ | Dar91 | 6／3 | ECC81 | $3 / 9$ | EL41 | 8／6 | NuTI | $3 / 6$ | 1Y83 6／－ | UCH81 | 6／3 | ACR1 |  |
| 6AB7G | 15\％ | 6.55 M | 6 | $7 \mathrm{B6}$ | 10／－ |  |  | $\begin{array}{ll}35 \mathrm{Z4GT} & \text { b／8 } \\ 35 \mathrm{Z} & 5 / 6\end{array}$ | DCC90 | $7 /$ | ECC82 | $4 / 9$ | EL4： | $8 / 6$ | NGT7 | 55／－ | PY800 7／－ | UCL82 | 71 |  | 85，0，0 |
| 6AT6 | 4／－ | $6 \mathrm{JJ5G}$ | 4／6 | 7117 715 | 70\％－ | 12 sk 7 | $4 / 8$ | $\begin{array}{ll}3520 & 51 \\ 37 & 5 /-\end{array}$ | DF33 | 8 F | ECC83 | $5 / 9$ | EL84 | 4／3 | OZ4 | 4／6 | 1＇Y801 7／－ | UCL83 | $8 / 9$ | CR | 35／－ |
| 6 BrBa | $2 / 8$ | 6.56 | 3／－ | 7 C 0 | 6／－ | 12sR7 | 5－ | 42 6f－ | DF70 | 71 | ECC84 | 61－ | EL90 | 5／8 | ${ }^{12} \mathrm{CB6}$ | $8 / 6$ | 12276 | UF41 | 8／－ | C |  |
| $6 \mathrm{B4G}$ | 15／－ | 6．57M | 7／6 | 7 D 5 | 8／－ | $14 \mathrm{H7}$ | 91－ | $50135 \quad 6 / 6$ | DF91 | $3 \%$ | ECC85 | $5 /-$ | EL95 | 5／－ | P＇C88 | $8 / 6$ | 1219 7／＊ | UF89 | 81－ |  | 48／－ |
| 6BA6 | 4／6 | 6J70 | $4 / 9$ | 7 H 7 | 6／－ | 19AQS | 5\％ | $50 \mathrm{C5} 519$ | DF92 | $2 / 6$ | ECC88 | $7 \%$ | ELLS 80 | $201-$ | PC97 | 7／8 | RG匂／500 | U1，41 | $8 / 8$ | C | C |
| 6BE6 | $4 / 6$ | 6 J 7 GT | 8／ | 7R | 17／6 | 20D1 | 10／－ | 50CD6G31／－ | DH＇96 | 6／3 | ECF80 | 6／6 | EM80 | $7 \%$ | PCC84 | 5／8 | 80／ | UL84 | 6\％－ |  | 46／－ |

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# PRACTICAL WIRELESS 

TOPIC DF THE MDNTH

## Dear Santa .....

AND what, dear reader, would you like Santa Claus to bring you this Christmas--assuming that the old gentleman can negotiate your array of TV aerials, break out of your converted chimney-piece speaker enclosure, avoid falling over your junk box and, if he does, choke back the cries of anguish to avert operating your audio switch and turning on the telly? Apart, that is, from a gadget to stop editors committing sentences like the above to print.

We made a few enquiries. Messrs. Guttridge and Gibson plumped for sockfuls of exotic DX, Henry and Pax wanted an exclusive interview with the man (no doubt as an excuse to work in a Santa Claus and reindeer sketch) and although many readers would ask for the secret of $100 \%$ success in constructional projects Messrs. King and Hellyer wanted more and better failures, obviously to justify some more fault finding articles.

The P.W. staff, when pressed, came up with a number of startling (though somewhat predictable) requests which we are glad to forget. But every individual reader would find no trouble in drawing up a splendid list of gifts.

Well, fasten your safety belts, for we have bad news. We learn, on the best authority, that there just ain't no Santa Claus! You will just have to carry on without his help and make the best of it under your own steam. Maybe it's just as well, really. You'll get much more fun and satisfaction working things out on your own. The only sure way to success is in learning by mistakes, building up experience gradually and trying things out.

But if you're still not convinced about Santa Claus, why not ask him for an annual subscription to Practical Wireless? You never know your luck! Or, better still, play Santa yourself and solve that difficult Christmas problem with a subscription to your friend - or, if you have no friends, to yourself!
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[^2]
## news And comment...

## "SATELLITE JOURNALISM'

The Post Office made journalism history on October 17th when it provided facilities for the intercontinental transmission of a newspaper page over a $48 \mathrm{kc} / \mathrm{s}$ satellite circuit.

A Muirheads Page Facsimile'Transmitter in the London office of the "Daily Express" was connected with a Muirheads Page Facsimile Receiver installed in the plant of the "El Mundo" newspaper in San Juan, Puerto Rico.

The $48 \mathrm{kc} / \mathrm{s}$ circuit, involving the use of cable and micro-wave systems connecting the "Daily Express" with the GPO's Goonhilly Earth Station, was extended to Mill Village, Canada, through the COMSAT Organisation's "Early Bird" satellite. The link from Mill Village to San Juan was afforded over the facilities of the AT \& T and IT \& T companies.

This demonstration was undertaken on behalf of the Inter-American Press Association whose annual general conference took place in San Juan during the middle of October.

## V.H.F. STEREOPHONIC TRANSMISSIONS

(Extension to the Midlands and North)


Reproduced by courtesy of the BBC Engineering Information Department.

Work is in hand to extend the stereophonic transmissions, at present radiated from Wrotham, Swingate and Brighton, to Sutton Coldfield and Holme Moss and certain relay stations fed from them, early in 1968. The unshaded part of the map above indicates the areas in which satisfactory stereophonic reception should normally be obtained. In places where the field strength is low, increased background noise may be heard on stereophonic programmes; improvements to the receiving aerial should enable the noise level to be reduced.
"KNIGHT KITS" ${ }^{\prime \prime}$

FROM MESSRS.

## ELECTRONIQUES

KG-275 Exposure Meter


Messrs. Electroniques have entered the "Kit" market with a vengeance. Their latest catalogue lists a host of units to suit all tastes. Signal generators, Hi-Fi, Oscilloscopes, Power Units and Receivers to mention just a few.

Readers will be pleased to hear that Electroniques claim a near foolproof system of guaranteed satisfaction with all their "Knight-Kits". They run a postal service for any advice needed. They will service the unit if required, and if, after building the Kit, difficulty is encountered, they will get it working too. There is also a money-back guarantee.

The above photograph illustrates the KG-275 Exposure Meter. It is possible to construct this in an evening and it is claimed that "It responds to light so weak-you can't see to read the meter".

The photograph below is their "Star Roamer" all band receiver which covers from 200 to $400 \mathrm{kc} / \mathrm{s}$ and from $550 \mathrm{kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ continuous thus covering long, medium and short waves both commercial and ámateur.

The instruction manuals are laid out in such a manner that Electroniques are able to claim that anyoneregardless of their knowledge of radio and electronics, can build any of these kits. The wiring is taken a step at a time and each manual is generously illustrated. Even the wires are colour-coded and cut to length too. They even tell the constructor when to take a break for coffee!

It is pleasing to note in the catalogue, that against most of the kits is a recommended book to assist the constructor gain the fullest advantage of the unit he has constructed.

A catalogue of the new "Knight-Kits" is available free from Messrs. Electroniques (Prop. STC Ltd.), Edinburgh Way, Harlow, Essex.


## NON-STOP POP BATTLE

The BBC may face a big clash with the pop record companies if it increases the broadcasting time for playing records. The companies fear that continuous radio pop will stop people buying records.

The BBC chiefs are under pressure from Mr. Robin Scott, controller of Radio 1, who wants record time increased from the present 82 -hours-a-week limit.

His plea is backed by young people who have been writing to the BBC complaining about the broadcasting of quiz shows and plays instead of continuous pop "like the pirate stations".

Opposition to an increase of needle time (the broadcasting term for the playing of records) comes from the Musicians' Union and Phonographic Performances, a consortium of record firms.

They claim an increase would mean less work for musicians and "over-exposure" of records, with transistor radios being used as "portable juke boxes".

## LONG-RANGE COMMUNICATIONS IN AUSTRALIA

The building of a long-range cable connection is to be commenced in Western Australia early in 1968, involving a cable almost 600 miles long with four co-axial conductors which will connect the towns of Perth and Carnarvon. A $12 \mathrm{Mc} / \mathrm{s}$ system will simultaneously transmit 1,200 longdistance calls and a TV programme along two conductors; the other two lines are being equipped with a $4 \mathrm{Mc} / \mathrm{s}$ system comprising 960 telephone circuits. Siemens will be supplying and installing the line amplifiers for both systems. The transistorised wideband amplifiers conform with the latest state of the act, require no maintenance whatever and can be fed with d.c. via the inner conductors of the associated coaxial conductors. These wideband amplifiers are accommodated in more than 200 intermediate repeater points mainly in underground containers.

## FREE FIELD STEREO CARTRIDGE

Goldring Manufacturing
 Co. (GB) Ltd., 486-488 High Road, Leytonstone, London. E.11, announce their new stereo magnetic cartridge, No. 800. In this unit, a very lightweight tube of magnetic material lies in a "free field" generated by a fixed source and is made to follow the record groove modulation by its coupling to a low mass diamond point. Due to the low mass, the mechanical impedance of the moving system has been reduced, pushing the resonance up to a frequency of over $20 \mathrm{kc} / \mathrm{s}$.

A significant by-product of this "free field" system is that the cross-talk separation is maintained at a very high level, never falling below $15 d B$ even at the highest frequencies and averaging over $20 d B$ at the midfrequencies.

Sensitivity is 1 mV per $\mathrm{cm} / \mathrm{sec}$.; separation is 25 dB at $1 \mathrm{kc} / \mathrm{s}$; load is $100 \mathrm{k} \Omega-47 \mathrm{k} \Omega$; effective point mass is 1 mg and stylus point, 0.0005 in . diamond. Tracking weight is 8 grams. The price is 1127 s . 6d. which includes P.T.

HEADPHONES WITH TONE CONTROL A new headphone, from the USA claims to reproduce full bass sound to surpass any headphone made, plus the special "Adjustatone" feature which allows response up to the limits of human hearing yet provides for scratch and hiss elimination.

Frequency response is from 10 to $15,000 \mathrm{c} / \mathrm{s}$. Weight 12 oz. Operation
 is on outputs from 3 to $16 \Omega$ and requires less than 1 W . Distortion is less than $1 \%$ at levels below the threshold of pain (130dB SPL). Sensitivity is $100 \mathrm{~dB} \mathrm{SPL} / \mathrm{mW}$ at $400 \mathrm{c} / \mathrm{s}$.

Price is $9 \frac{1}{2}$ gns. Transatlantic Music Tapes (Distributors) Limited, Bristol \& West House, High Street, Salisbury, Wiltshire.

## BBC RADIO LEICESTER

The first of the BBC's local radio stations was brought into service at Leicester on November 8. Transmission is on $95.05 \mathrm{Mc} / \mathrm{s}$ in the v.h.f. band, with horizontal polarisation, from a transmitter at Anstey Lane. Regular trade test transmissions are radiated daily from 09.30 to 18.00 and started on Friday, October 27.

The local programmes are originated from the headquarters of BBC Radio Leicester at Epic House, Charles Street.

Radio Leicester serves Leicester and its immediate surroundings including Arnesby, Cosby, Desford, Woodhouse Eaves, Burton-on-the-Wolds, Hungerton and Gaulby. The transmissions are on v.h.f. only. Listeners who may not have a v.h.f. receiver should consult their radio dealers who will be able to advise about reception.

Receivers for Radio Leicester are also suitable for reception onv.h.f. of Radio 2 (Light Programme), Radio 3 (Third Network) and Radio 4 (Home Service). The BBC's v.h.f. sound services provide improved reception which is much less susceptible to noise and interference than is reception on medium and long waves.

## L. W. Roche

It is with deep regret that we have to announce the death of L. W. ROCHE. "Lew', as he was known to all his many friends and acquaintances, did a great deal of pioneer work in the field of electronic music. Many of his electronic organ designs in ''kit form" currently enjoy wide popularity. He was associated at various times with a number of companies who specialised in this field, and at the time of his death was chief design engineer for Henry's Radio Ltd. 'Lew' had been failing in health for a number of years. To his family we express our sympathies in their great loss.


THE simple crystal receiver has many advantages to offer. It is cheap to construct, easy to build and doesn't require any form of power either from the mains or batteries. It can be left switched on without waste, and requires only an aerial and an earth lead to provide hours of inexpensive entertainment. This is an ideal project for the beginner and also provides a very acceptable present for the Christmas stocking for a youngster.

## LAYOUT

The layout of the receiver is very uncritical and the components can be laid out in almost any style to suit the container or case. The prototype was built in a two-ounce tobacco tin merely because this


Fig. 1 (left): Simple longwave crystal set.
Fig. 2 (right): Adding a switch for m.w. and l.w.
was to hand and a wooden container would be just as good.

## CIRCUIT

The complete circuit diagram is shown in Fig. 1. Only three components are used: a coil, a capacitor, and a crystal diode. An aerial is connected to point A, the earth to point B, and a pair of headphones to points C and D . If a mistake is made in the wiring no damage will be done, the set just will not work until the fault is rectified.

The prototype receives three programmes in Hertfordshire at headphone strength--Radio 1, Radio 4, and on long waves Radio 2. As it stands the circuit in Fig. 1 will receive only long waves and thus only one station, Radio 2. If a piece of wire is connected to points B and X this will short out the lower part
of the coil and the receiver will work only on medium waves. In this condition it receives two stations, Radio 1 and Radio 4 . For simplicity this latter connection would be ideal, but if we were to wire-in a simple switch between points $B$ and $X$ we could have a two-band set for either medium or long waves dependent upon the position of the switch. This modification is shown in Fig. 2. Any on/off type of switch will do but in order to ensure that it will fit in the case, one of the small slide switches, mounted on the side of the case, would be best.

## CONSTRUCTION

There are only four holes to drill. Three are 6BA-two for the coil and one for the small tag strip. The fourth hole is $\frac{3}{8} \mathrm{in}$. diameter for the tuning capacitor. Mount the tuning capacitor first, then the tag strip and finally the coil. The 6BA bolts will make their own thread in the coil former but these should be tightened gently otherwise the coil former might split.
The thick double tag on C1 is the tag to connect to earth, the other tag being the aerial connection. It must now be decided whether a switch is to be used. If not, then now is the time to decide whether long or medium wave is to be selected. Since the


Fig. 3: Adding a $4: 7 \mathrm{k} \Omega$ resistor to make a tuner.
prototype was wired for medium wave only, this wiring will be described first.

Take a length of wire and connect it to the red and blue tags on the coil L1. From here the same wire is taken to the large double tags on the tuning capacitor C 1 and from this point to tags 1 and 2 on the tag strip.

Next, a wire is connected from the remaining tag on C1 to tag 4 on the tag strip. Now solder another wire from the same point (tag 4 on the tag strip), to the black tag on the coil. The last step is to connect the diode between tags 3 and 4 on the tag strip. The diode should be connected with its positive end to tag 4 and the negative end to tag 3. This completes all the wiring for the medium wave only set.

To test the receiver, connect a pair of high resist-
ance headphones $(4,000 \Omega)$ to tags 2 and 3 on the tag strip, the aerial to tag 4 and the earth lead to tag 1. By rotating the tuning capacitor it should be possible to hear a station, possibly two stations. The set should receive a station quite well if it is within 40 to 50 miles from the transmitter.
In some cases it might be difficult to separate the two stations and here it would pay to experiment with the length of the aerial. Alternatively, another variable capacitor, the same value as Cl , could be connected between the aerial and point A on Fig. 1.

If long wave only is required it is only necessary to break the wire which shorts the red and blue tags on the coil together. In this case the red tag is left unconnected and only the blue tag is wired up.

## DUAL WAVE

For the reception of both long and medium waves a switch is required as explained. The set is wired as for long waves only and two wires are taken to the switch. One wire from the blue tag, this is the wire which goes from the blue tag to the double tags on the tuning capacitor and tags 1 and 2 on the tag strip. This wire is continued to one terminal on the switch. Another wire is taken from the red tag on the coil to the other terminal of the switch. Note, this will be the only wire on the red tag of the coil.
The aerial should be as long and as high as possible. A length of 70 ft . of bell wire was used on the prototype with the earth taken to a length of copper pipe driven into the ground just outside the window. However, quite good results were obtained using only the bedsprings as an aerial and no earth, although this produced considerably less volume and no stations could be heard on long waves with this set-up. A length of wire around the picture rail should also produce results.
The front of the case was masked with adhesive tape and then sprayed with a paint aerosol, after which the tape was removed. The dial was made from

## components list

```
C1 500 pF variable capacitor (Jackson Dilecon).
L1 Dual range crystal set coil (Repanco type DRX1).
D1 Diode. OA81 (or OA70, OA79). Almcst any diode
    will do.
Four-tag tag strip, 6BA bolts and nut, scraper board, pointer knob, two-ounce tobacco tin, high resistance headphones ( \(4,000 \Omega\) ), aerial and earth wire, wire for wiring up, solder, \(4.7 \mathrm{k} \Omega \frac{1}{4}\)-watt fixed resistor if required.
```



View of the completed receiver wiring. Component positioning is not critical as there is plenty of room. Note the bottom tag of coil has no connections
black scraper board which is easily obtainable from most stationers and art shops. It costs 2 s . 6 d . for a small packet. This is a black-coated card which, when scratched or scraped, will produce a white image. The dial could easily be made from a piece of white card or paper and the marking made in ink.

The photograph shows the inside of the case and the wiring of the prototype wired for medium waves only. The inside of the tin is not normally black. It was painted this colour purposely, but only so that the wiring and components would show up better on the photograph.

The crystal set may be used as a tuner in conjunction with an amplifier. Good results were obtained using the prototype with a small commercial transistor amplifier. To use the set in this way one extra component is required-a $4.7 \mathrm{k} \Omega$ fixed resistor. This component is wired across on tags 2 and 3 on the tag strip. A length of screened lead is then taken from these two tags to the amplifier. The braiding or screening of this lead goes to tag 2, and the other wire to tag 3. Similarly, at the amplifier end, the screening goes to the earth line and the other wire to the amplifier input. When the set is used in conjunction with an amplifier the phones are, of course, disconnected from the circuit.

## WIDE RANGE PULSE GENERATOR

A precision unit which, when used in conjunction with an oscilloscope, is extremely useful for television circuit and response testing. It also has important applications in the fields of CCTV and colour television.

## CAPACITANACE DIODE TUNING

Junction diodes are becoming increasingly used for a wide range of applications, from a.f.c. to tuning by means of a potentiometer at v.h.f. and u.h.f. How and why they do this, and elementary basic principles of semiconductor diodes are examined in this article.

## THE PROFESSIÔNAL*SERV̂ICE ENGINEER

## SEMTEDNOURTOR NODTU

## PART 3

IN power amplifiers transistors are required to work at levels that leave only a small margin of safety against thermal runaway. The maximum temperature has to be kept within the limit permissible by the efficient removal of the heat being produced, which is concentrated mainly at the collector junction. Conduction of this heat into a larger area of metal enables it to be radiated and convected at a faster rate, and the power is increased for a given junction temperature.

Germanium transistors in Class B output stages require heat sinks at outputs above a fraction of a watt, and small silicon transistors similarly above a watt or two. In a high-power amplifier the driver stage transistors, when germanium, may also need to be mounted on a heat sink.

A number of transistors of TO-3 or similar construction make thermal contact with the heat sink through a thick copper mounting-plate with twoscrew fixing. Small power transistors of TO-5 construction can be fixed on a heat sink by a method that presses the rim of the transistor casing on to the heat sink, so producing metallic contact over the flat area of the transistor. A washer with holes for screws can be used. For other small-output transistors it is necessary to fit a copper clip that is bolted to the heat $\sin k$, or which at low power can itself serve as a heat sink.

Any surface unevenness on the heat sink under the transistor should be avoided. Burrs at holes have to be removed, and a special silicone grease is applied to reduce the thermal contact resistance.

## INSULATION

The collector in power transistors is connected internally to the metal case of the transistor. There are, however, small output transistors, e.g. of TO-1 construction, which are electrically isolated from their case, or in which it is the base that is connected to the container.

In general, therefore, both transistors of an output stage can only be mounted on the same heat sink if 0.002 in . mica and insulating bushes are used to insulate one or both transistors. Instead of mica a $\frac{1}{8}$ in. thick anodised aluminium insulator can be used, and its very low thermal resistance is an asset when the transistor and heat sink also have very low thermal resistances. The heat sink itself can be anodised to insulate it and improve radiation from it, but the separate insulator provides a double insulating layer.

Heat sinks in direct contact with the transistor can be mounted on insulators inside an amplifier cabinet provided that effective cooling is maintained. The area of a heat sink creates a risk of capacitive feedback to earlier
R. LEYLAND
stages, and the preamplifier may have to be screened from it.
There is no harm in merging a number of heat sinks into a single large one providing that the transistors are spaced out and electrically insulated. A metal cabinet or chassis can be used as the common heat sink, or two large heat sinks insulated from each other can serve as the sides of a cabinet. With these methods precautions may be necessary to avoid short-circuits from accidental contact with external metal objects.

## HEAT SINKS

The surface of a heat sink, except at the point where the transistor is mounted, can be blackened to improve radiation. This reduces the thermal resistance by about $30 \%$ as compared with bright metal. Convection is assisted by mounting the heat sink vertically, and an improvement of possibly $20 \%$ can in this way be obtained. The thermal resistance of a rectangle of blackened 16 s.w.g. aluminium measuring 7 in . x 4 in . is approximately 3.5 deg . C/W.
In determining the thermal resistance necessary for a heat sink from the derating characteristic of the transistor it is usual to assume an ambient temperature of 45 deg . C.
Sometimes a heat sink is chosen that is adequate for music but not for continuous sinewave testing. The lower the thermal resistance of a heat sink the better, as there will be less variation in quicscent current with signal level, but there is little advantage in making it very much lower than the interna! thermal resistance of the transistor. For example,


Fig. 10: Packaged 800 mW a.f. amplifier type PC7+ (Newmarket Transistors). Dimensions: 3 in $\times 1.75 \mathrm{in}$.
a small transistor with a thermal resistance of 50 deg. C/W junction-to-case would probably not be fitted on a heat sink with a thermal resistance lower than $15 \mathrm{deg} . \mathrm{C} / \mathrm{W}$ (possibly a 2 in . square of metal) but if a power transistor of 1.5 deg. C/W thermal resistance was fitted on this heat sink there would be considerable room for improvement.

Heat sinks of finned design in extruded aluminium alloy are obtainable with specified values of thermal resistance. For example, one measuring 5 in . x 4 in . $x$ lin. deep (over the fins) has a thermal resistance of 2 deg . C/W.

## NEGATIVE FEEDBACK

Unvarying amplification of varying signals is the ideal, and fidelity amplification implies an amplification that is linear up to the maximum output. It is the effectiveness of negative feedback in promoting linearity that makes fidelity amplifiers possible. Distortion occurs mainly at high signal levels in the driver and output stages and, subject to some reservations, can be reduced to any desired extent, relative to signal, by applying sufficient negative feedback.
A.C. negative feedback stabilises amplifier gain, according to the values of resistances in the feedback network, making it insensitive to changes within the amplifier, and less dependent on the characteristics of the transistors. Since distortion is reduced to the same extent as gain is reduced, the more amplification within the feedback loop the better, and high-gain transistors will result in a lower distortion figure. It is also more effective to apply the negative feedback over a number of stages. Modifications to stages within a negative feedback loop may appear to have no effect until the feedback is disconnected. For example, when negative feedback is in action. bootstrapping does not produce any very noticeable increase of gain.

It is only worthwhile reducing low basic distortion to a small fraction of $1 \%$ by negative feedback if the loudspeaker itself produces little distortion. In a portable radio the quality improvement resulting from the use of 10 dB of negative feedback, reducing the gain about three times, could be considered adequate, while in a fidelity amplifier as much as 50 dB of negative feedback, reducing the gain over 300 times, might be applied. More usual amounts are $20-40 \mathrm{~dB}$ with gain reductions of 10 to 100 times. Some gain must be retained in the power amplifier however to avoid the need for a highlevel output from the preamplifier, which would tend to reintroduce distortion.
D.C. negative feedback used to stabilise the quiescent midpoint voltage can be applied to a much greater extent than a.c. feedback. A single feedback path can be used for both with a decoupling capacitor included, e.g. at the emitter of the driver stage or at a point in the feedback path, to reduce the amount of a.c. feedback applied. It is preferable that the amount of feedback should not depend too much upon the value of the capacitor, as it can when a feedback voltage is developed across the capacitor in series with a low resistance.

Negative voltage feedback from the output reduces the output impedance. Values of output impedance of less than an ohm can be obtained for good loudspeaker damping.

## FREQUENCY RESPONSE

Tone controls are usually incorporated in the preamplifier stages, a completely uniform response, obtained by means of a resistive negative feedback network, being aimed at in the power amplifier over the a.f. range. In some amplifiers, however, the negative feedback network is modified and made frequency-dependent to provide a bass or treble control.
Even with negative feedback the maximum power response is not usually maintained with germanium power transistors at a frequency of $10 \mathrm{kc} / \mathrm{s}$ and above due to a decrease of efficiency. There is an increased risk of thermal runaway in testing with a continuous sinewave signal at high frequency, but little effect on the reproduction of music. Silicon power transistors. made by the newer diffusion process, do not have this limitation of h.f. output. It is usually necessary, however, to limit the response beyond the a.f. range, i.e., above $15 \mathrm{kc} / \mathrm{s}$.

Although in a fidelity amplifier the response will extend down to -3 dB at $20 \mathrm{c} / \mathrm{s}$, with a small loudspeaker a -3 dB response at $200 \mathrm{c} / \mathrm{s}$ is more suitable to avoid the distortion produced by a small loudspeaker at low frequencies. This allows a loudspeaker coupling capacitor much smaller than the $1,000 \mu \mathrm{~F}$ or more used with a loudspeaker of low resonant frequency. A disadvantage of the smaller capacitor is its higher series resistance, which could put as much as an ohm in series with the loudspeaker.

When negative feedback is applied via a resistor as a current to the base of the driver stage it lowers the effective input impedance, and the amount of negative feedback depends on the collector load resistance of the predriver stage, being greater if the value of the load is high. If instead the negative feedback is applied as a voltage across a small resistor at the emitter of the predriver stage it raises the input resistance of the predriver stage, and the amount of negative feedback is then maximum when the predriver input comes from a low-impedance source.

## H.F. STABILITY

Feedback is a stabilising factor when phased negatively to reduce the effective input. Instability is produced however when amplifier phase shift is sufficient at some frequency to transform negative into positive feedback. This phase shift accompanies the usual decrease in amplifier response outside the a.f. range, at low and high frequencies, and may cause a peak in the amplification. If the loop gain exceeds unity at this frequency, oscillation occurs.

With no transformers to restrict the performance phase shift in a transformerless amplifier is reduced, allowing more negative feedback to be applied without oscillation. Direct coupling of amplifier stages overcomes low-frequency phase shift, but there is still risk of oscillation above the a.f. range, especially with a reactive loudspeaker load. Even when continuous oscillation does not occur there may still be bursts of oscillation following any abrupt transition in the waveform. This shows up in tests with a square waveform, or when the signal is increased to the point where clipping occurs on peaks, or in the presence of some crossover distortion.


Fig. 11: Bridge rectifier power supply type PC101, for use with amplifier type PC7 (Newmarket Transistors).

To avoid high-frequency instability a number of precautions are taken. Transistors made by the diffusion process, with high cut-off frequencies, can be used to reduce phase shift at high frequencies. A small capacitor of suitable value can be connected across the negative feedback resistance, and is often placed between the collector and base of the driver stage. This improves the pulse response of the amplifier by removing overshoot, i.e. the commencement of an oscillatory response.

Another precaution against h.f. instability is to connèct a passive network, consisting of a suitablychosen resistor and capacitor in series, at some point in the amplifier to reduce the h.f. response. A network of this type is often connected across the loudspeaker.

## POWER SUPPLIES

Distortion in an amplifier is less when it is working at only a fraction of full output, and there should be ample output power available in reserve in a quality amplifier to cope with sudden increases in signal. A power capability of several watts is therefore desirable except in small portable radios. A 40or 50 -volt supply enables an amplifier to develop this amount of output power without currents so heavy as to make earthing problems difficult. These currents flowing in earth links or chassis can produce potentials that can be fed back to the input and cause increased distortion.

A mains type power unit will usually be required for a high-wattage amplifier, and involves introducing a mains transformer, but this is able to supply the two amplifier channels of a compact integrated stereo system.

One type of transformerless amplifier, the $\pi$-mode Class AB, takes a constant supply current and there


Fig. 12: Diode-decoupled power supply for two amplifier channels of a stereo system.


Fig. 13: Stabilised power supply for a Class B amplifier.
is no problem of supply regulation. With Class B amplifiers, however, the power unit must have good regulation to avoid large voltage variations caused by the varying current demands of the Class B output stage. These can restrict the maximum output from the amplifier especially on a test signal consisting of a continuous sinewave, making the sinewave rating less than the power rating on music, which on average takes only a third of the current required for the sinewave signal. Series resistance in the supply must therefore be minimised, and smoothing is sometimes omitted except for a reservoir capacitor of possibly $2,500 \mu \mathrm{~F}$.

## REGULATION

Full-wave bridge rectification (Fig. 11) has the advantage of better regulation, and makes the ripple frequency $100 \mathrm{c} / \mathrm{s}$. When the current drain is small the voltage nears the peak value, so hum is reduced on quieter signals where it would be more noticeable.

Inductance-capacitance filters are practicable if the chokes are of very low resistance. A 50 mH choke with a $2,000 \mu \mathrm{~F}$ capacitor will reduce ripple 36 times.

Diode decoupling (Fig. 12) offers some advantages. A forward-conducting junction diode takes the place of the choke as the series element of the ripple filter. Its voltage drop is less than a volt and becomes constant at high currents, where the diode has little effect. At low currents, the a.c. resistance of the diode increases, and provides ripple suppression where it is most necessary. Separate diode decoupling for two channels of a stereo system provides very satisfactory separation between them.

A stabilised power supply can have a very low output impedance and there should then be no difference between the amplifier ratings for sinewaves and for music. An extra power transistor is involved, with a heat sink, and a zener diode reference. The best type of circuit will probably include two other transistors (see Fig. 13). Amplification in the regulator circuit enables the mains unit to have an output impedance of only a fraction of an ohm, and also ensures very effective ripple suppression.


EVERY day, thousands of messages are transmitted in morse or c.w., from ships, aircraft or commercial stations. Many news broadcasts from all over the world are in morse and offer interesting listening for keeping up to date with the international situation. Again, amateur radio enthusiasts or Hams can be heard chatting across thousands of miles. If you can't read morse you are missing a lot of interesting fun.
Learning to send and receive c.w. is not difficult, though some will learn quicker than others. There are numerous methods of learning too, but whichever way you finally decide upon, one factor will be far more dominant than the actual method itself-your determination. If you are really determined to learn morse, then you will, no matter how you go about it.


Fig. 1: Circuit for a simple oscillator.
One point is important and agreed by practically all c.w. men. DO NOT think of the code in terms of dots and dashes, if you do, and you are determined to learn then you will succeed, but it will be more difficult and will almost certainly take longer. For example, the letter $U$ is thought of as di-di-dah and not dot-dot-dash, while F would be di-di-dah-dit.

Memorising the code can be done in a number of ways. Some people learn the characters containing only dots-E, I, S and H , and then those with dashes-T, M and $O$. These are quite easy to remember and this takes care of seven characters. Some then proceed to learn all the remaining characters which begin with a dit, and finally those beginning with a dah. Others advocate memorising the five vowels first since these are in common usage.


Fig. 2: Correct spacing and character length.
Another method, which the writer can recommend, is to start by learning the first seven characters of the alphabet. When these are memorised, make up little groups using only these seven characters in different sequences. This is to ensure that they are thoroughly committed to memory. The next seven letters are then memorised and the
process repeated, after which, jumbled groups using the first fourteen letters are practised. This procedure divides the alphabet roughly into four easy bites and with just fifteen minutes practice every day it should not take longer than two weeks to completely memorise the code. The length of each practice session is a matter of individual preference. However, several short sessions are better than a few long ones.

## ESSENTIALS

The first essential is a morse key and an audio oscillator. Failing this a buzzer will do but an oscillator is preferred. Circuitry for a suitable unit is shown in Fig. 1. It is very simple and easy to make up either on Veroboard, printed circuit or a tagstrip.

Hold the key lightly, resting the first and second fingers on the knob. The morse code is sent with the arm, the wrist acting as a pivot, and NOT by pecking at the key with the fingers. The fingers shourld not leave the key, and above all-relax. Send slowly and concentrate on accuracy, speed will come with practise. Remember that-one dah is equal in length to three dits, the spacing between two letters of the same word or group is three dits, the spacing between individual characters of the same letter is one dit, and finally the space between words or groups should be equal to five dits. (See Fig. 2.).

| AMZFR | GOLMM | THEFP | QCMOA | IIFMZ |
| :---: | :---: | :---: | :---: | :---: |
| YOOVB | TFORO | HXCEF | ENJNJ | LWUAF |
| REDER | TPEKQ | LAKSJ | MCUOI | AIOSH |
| QLWPS | ODKRU | THNVG | ALOUE | IEOUA |
| MZNXB | BVGFH | JDKSL | APQOW | IEURY |

Fig. 3: Example of some five-letter groups.
Practise sending slowly and accurately, if you develop a sloppy style or a bad fault it will be almost impossible to correct after a time. Guard against clipped characters, incorrect length of characters and spacing. Most important, guard against tension in the hand, wrist and arm muscles. A good c.w. operator can send for a very long time without any apparent effort. If your hand, wrist or arm are tensed up in any way, you will find that you are unable to send for more than a few minutes, so relax, take your time and hold the key very lightly with the fingers just resting on the key.
A tape recorder is a great asset because you can send some morse at a very slow speed, concentrating on well-formed, properly spaced characters, and then play it back thus getting valuable practice at receiving, and at just the right speed too. Receiving
morse is always harder than sending. This is mainly because in sending you can think ahead, you know what's coming next, in receiving you must take it as it comes and while you're writing down one character you must already be listening and concentrating on reading the next.

## PRACTISE

One excellent way of practising is to write out some mixed groups of characters as shown in Fig. 3. Using five figures to the group you can then count each group as a word. In this way you can time yourself and thus find out your speed in words per minute. In the case of the Ham licence you will need to be able to send and receive at 12 w.p.m. so it would be prudent to aim at 15 w.p.m. It might prove easier to write out the groups on graph paper, this makes division easier. Groups are excellent practise, particularly in receiving. With plain language there is a tendency for the brain to cunningly try to guess the next letter. Thus if the letters come out T-H- the brain might guess E making the word THE. However, the word might easily be THAT or THIS or THESE etc. In five-figure mixed groups this is eliminated and the brain can't cheat. It is very tempting to try and read sense into the code, i.e., make out the words, but this should be avoided at all costs in the early stages. When you can receive comfortably at 25 w.p.m. all well and good, but when you're just starting to learn morse remember, while you are trying to read the message, you are not concentrating on the next character and thus your concentration will be divided and you will lose characters and have to pick up again. This is also a bad thing as it is rather demoralising to keep missing characters.

## MISTAKES

If you miss a character leave a blank space and carry on. Don't ponder on the character you missed or you'll miss others while you are thinking. If, on checking, you find that a particular character(s) is causing bother, make up some mixed letter groups using the difficult character(s) interspersed with some you know well. Half an hour's practice will soon sort things out, or better still, three or four ten-minute sessions.

Once you have learnt the code, a very good way of practising is to mentally send the code in your head. When you travel on a train or a bus look at the adverts and send these mentally. This exercise will help enormously in improving your speed, while in the early stages it affords a very good exercise in familiarity.

## LISTENING

The amateur bands are an excellent hunting ground for practice. Even stations sending very fast will send their callsigns two or three times. If a country's list is obtained, then, by hearing the callsign, it is easy to determine the country where the particular amateur is located. To add to the interest, a world map might be purchased, and coloured pins pushed in when a particular country is heard. This is simple because amateurs in a particular country have their callsigns beginning with the same prefix, only the last few letters differ. Amateurs in Sweden all have callsigns beginning SM, those in Peru all

| ALPHABET |  |
| :---: | :---: |
| A didah | N dah dit |
| B dah dididit | O dah dah dah |
| C dah di dah dit | P di dah dah dit |
| D dah di dit | Q dah dah di dah |
| E dit | R di dah dit |
| F dididah dit | S dididit |
| G dah dah dit | T dah |
| H didididit | U dididah |
| 1 didit | $\checkmark$ di di di dah |
| J di dah dah dah | W di dah dah |
| K dah didah | X dah di di dah |
| L di dah di dit | Y dah di dah dah |
| $\mathbf{M}$ dah dah | Z dah dah di dit |
| NUMERALS |  |
| 1 di dah dah dah dah | 6 dah di di di dit |
| 2 di di dah dah dah | 7 dah dah di di dit |
| 3 didididah dah | 8 dah dah dah didit |
| 4 dididididah | 9 dah dah dah dah dit |
| 5 dididididit | 0 dah dah dah dah dah |
| miscellaneous |  |
| Question mark | di di dah dah di dit dah di di dah dit |
| Oblique stroke |  |
| End of Message | di dah di dah dit |
| Error | di di didididididit |
| Invitation to transmit | dah di dah |

start with OA. Thus if the callsign DU1FFZ was heard, the station would be in the Philippine Islands because DU is the amateur prefix for the Philippines. A list of prefixes for the different countries is obtainable from the R.S.G.B., 28 Little Russell St., London, W.C.1, and costs 9 d .

The Radio Society of Great Britain has many members all over the country who send slow c.w. (morse) specially for the benefit of those starting to learn and who wish to improve their speed. The main band on which these transmissions take place is topband $1.8-2.0 \mathrm{Mc} / \mathrm{s}$ or 160 metres. The Society publish a monthly bulletin (free to all members) and this gives details of the times, dates and frequencies of these transmissions together with the callsign and location of the station.

You can learn morse-anyone can. Get yourself a key and an oscillator or buzzer. If you have a tape recorder all the better, if not borrow one. A cheap one will do fine and you will be able to practise without an instructor. All you need now is determination and you're in business.

## IMPORTANT

DON'T BUY PRACTICAL WIRELESS and then allow it to become torn and dirty. Don't search frantically through your back issues for that particular article either.

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v． $\qquad$ $\begin{array}{ll}\text { LECTROLTTICS CAN } \\ \text { 100／25 ₹．} & 21-81600\end{array}$
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32＋32／350 v． $4 / 6^{4} / 100+200 / 275$ v．12／6
 CERAMIC， $500 \mathrm{\nabla} .1 \mathrm{pF}$ ．to 0.01 mid ．， 9 d ．Discg $1 / \mathrm{m}$ ．

## PAPER TUBULARS


$500 \mathrm{v},-0.001$ to 0.05 gd．$; 0.11 /-; 0.251 / 6 ; 0.53 /-$
$1.000 \mathrm{v},-0.001,0.0029,0.0047 .0 .01,0.02,1 / 6 ; 0.047,0.1,2 / 6$ ． $1,000 \vee .-0.001,0.0029,0.0047 .0 .01,0.02,1 / 6 ; 0.047,0.1,2 / 6$.
E．H．T．CONDENSERS． 0.001 m／d． $7 \mathrm{kV} ., 6 / 6 ; 20 \mathrm{kV} .10 / 6$. SILVER MICA．Close tolerance（plas or minus pF．）， 5 to $47 \mathrm{pF} .1 /-;$ ditto $1 \% 50$ to $800 \mathrm{pF} .1 / 1-; 1,000$ to $5,000 \mathrm{pF}, 2 /-$ ． TWIN GANG．＂0－0＂ $208 \mathrm{pF}+17 \mathrm{ApF}, 10 / 6 ; 365 \mathrm{pF}$. minia－ ture $10 /-$ ； 500 DF standard with trimmers， $9 / 6 ; 500 \mathrm{pF}$ ． midget less trimmers，7／6； 500 pF ．slow motion，standard $9 /-$ ； small 3 －gang 500 pF ．18／9．Single＂ 0 ＂ 385 pF ．7／8．Twin $10 /-$ SHORT WAVE．Single 10 pF ．， $25 \mathrm{pF}, 50 \mathrm{pF}, 75 \mathrm{pF}$ ．， $100 \mathrm{pF}, 160 \mathrm{pF}, 5 / 6$ each．Can be ganged．Couplers 9 d ．each．
TUNING．Solid dielectric． $100 \mathrm{pF} ., 300 \mathrm{pF}, 500 \mathrm{pF}, 3 / 6$ eaoh． TUNING．Solid dielectric． $100 \mathrm{pF}, 300 \mathrm{pF}, 500 \mathrm{pF}, 3 / \mathrm{B}$ eaoh．
 250 v．RECTIFIERS．Seleniam t wave $100 \mathrm{~mA} 5 /-$ ；BY100 $10 /-$ CONTACT COOLED \＆wave $80 \mathrm{~mA} 7 / 6 ; 85 \mathrm{~mA} 9 / 6$ ． Full wave $75 \mathrm{~mA} 10 /-$ ； $150 \mathrm{~mA} 19 / 8$ ；T．V．reots． from $10 /-$
NEW B．A．S．F．LIBRARY BOXED TAPE 7 in．L．P．1，800 ft．45／－； 7 in．D．P．2，400 ft．70／－ 60 min．Cassette C60（For Philips，otc．）17／6 Spare Spools 2／6．Tape Splicer $5 /$－．Leader Tape $4 / 6$ ．
Tape Heads：Coliaro 2 track $28 / 6$ pair．B．S． 4 track $99 / 6$.
MAINS TRANSFORMERS

## AS

 MT． $510 / 300-0-300 \mathrm{v} .120 \mathrm{~mA}$, B． 3 v． 4 a MINIATURE $200 \mathrm{v}$.20 mA．， 6.3 v ．
MLDGET 220 v． $45 \mathrm{~mA} ., 8.3 \mathrm{v}$.2 a ． SMALL $250-0-25050 \mathrm{~mA} .6 .3$ ч． 2 B
HEATER TRANS． $6.3 \mathrm{v} .1 \frac{1}{2} ., 8 / 6 ; 6.3$ v． 4 s ． Ditto tapped gec． 1.4 v．， $2,3,4,5,6.3 \mathrm{~F} .1$ it amp ． GENERAL PURPOSE LOW VOLTAGE．Outputs $3,4,5$ $6,8,9,10,12,15,18,24$ and 30 F ．at 2 a ．． 1 amp．， $6,8,10.12,16,18,20,24,30,36,40,48,60,291$ AUTO TRANSFORMERS $0-115-230$ v．Input／Output，
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H．R HEADPHONES 2000 ohms Saper Quality
 TAPE DECK AMPLIFIERS FOR B．S．R．T．D． 2 ETC． With Pre Amplifier，Oscillator，all valves，＂magic eye＂tuning
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# practically wireless commentary by IEINII 

IT is Mr. Mendit, isn't it? The wireless man? You may not remember me, I'm Smith. Smith, that's it, with an "I", "but one eye, although popular prejudice runs in favour of two", as Charlie Dickens said. Yes, I know there are a lot of Smiths, biggest family in the phone book, eh? But I was in your shop the other day.

Sorry, didn't quite get that it's a bit noisy-bit of a party going on here. Yes, you can hear it, can you? Can't pick you up loud and clear, as you wireless chaps say. . . Atmospherics, eh? that's a laugh. The atmosphere here you could cut with a chopper, man, ninety-five per cent proof, ha, ha,

No, I say, don't ring off. I know it's late. . . well, Christmas and all that. Yes, Merry Christmas to you, too, Mr. Mendit. I just wanted to ask you. .

Important? Well, you judge, you just ask Mrs. Smith if it is important-see what she says. No, I know you don't want to talk to Mrs. Smith-tell the truth, I don't much, either, ha, ha. No, I'm the one who was in your shop the other day. Yes, we met. I was looking at that SuperSpecial Goldbrick Stereoplex Radiogram, remember?

I thought you would. Yes, the gentleman with the dog, that's right. Listen, I'm sorry about that


Bit of a party going on here
lamp standard. Yes, rather flimsy, wasn't it. And Rover is a big fellow. No, I didn't ring you up to talk about that

The Goldbrick? Well, yes, I was very interested. Yes, I know it has-yes, and what-d'ye-callit feedback, too. I know I heard you. Quite a bargain, I'm sure. Mrs. Smith was saying . . . yes, that's her you can hear in the background. Well, she always sings Shenandoah at family parties. She needs a bit of relaxation since that shock she had from the vacuum cleaner - no, no, I'm not complaining, honest. Not unless it is that the shock should have been a bit bigger!

No, really, I was joking, Mr. Mendit. Yes, I know you've got your code of ethics. Me too. . . what's that? Does it include ringing up in the middle. . . oh, come, friend, it is Christmas. Yes, I know you are opening the shop tomorrow-good luck. Me, I'll be dead-oh, if tonight goes on like this! No time to call around. I wondered if you would be coming out this way-you or one of your engineers? Always a drop of tiddley on hand.

No, I don't suppose you can afford to drink on duty, not with these breathalysers and things. It doesn't bother me, not since I was disqualified last Bank Holiday.
What's that? No, I don't suppose it is easy to fit in deliveries at holiday times-as the midwife said, ha, ha. Oh, really, would you? Make a special case of it. Well, I do declare, that's big of you, I mean, considering we only met the once. . . Previous customer? Well, you could say that. We have had a few bits and pieces. . . ha, ha. Perhaps I am being modest. You've got a sense of humour, Mr. Mendit. It is very good of you. I don't like to bother you really, not with the weather like it is. Look, perhaps I could get the boy to pop round, if I can tear him away from his train set.


Rover is a big fellow..
No, train set. . . electric? but of course, what else! Well, no, not actually from your shop-we got it wholesale. Yes, like the fridge, and the telly, yes.
Hallo, you there, Mr Mendit? Bad line, this. All I could hear was a sort of heavy breathing. I said, I could send the nipper. . . Big van, what big van? Do you do all your rounds in a big van? that's not what I would call economic. . . oh, well, I suppose if you sell a lot of big stuff. No, not every day you sell a Super-Special Goldbrick I guess. Good luck to you. Nice bit of profit for the holiday.

What's that? Cash? Well, ha, ha, you're still joking - that's funnier than that noise Mrs. Smith is making behind here--I must say. Not much of a purchase to run up a contract for, Mr Mendit. I reckon I can scrape up a couple of bob, even after what this party is setting me back. Enough for a dry battery anyway. . .

Goldbrick, what Goldbrick? I thought you said you'd sold it! ME? You're joking again. . . I was just asking if you could drop by with a battery for the kid's transistor radio.

What's that, I don't hear you very well. I know it's late, yes, I know, but it is Christmas. I say, Mr. Mendit, hallo-hallothis is a bad line. I thought I heard you say.

Funny, the line's gone dead.

## adaptable LOWCOST hi-fi 5Y5TEm

w. CAMERON

PART 2

IN THIS PART A PRE-AMPLIFIER STAGE IS ADDED TO THE BASIC AMPLIFIER DESCRIBED LAST MONTH, TO enable a comprehensive tone control circuit TO BE INCORPORATED.

AN OC45 is used in the pre-amplifier stage and is shown as Trla in the pre-amplifier circuit diagram (Fig. 4). It will be seen that it replaces R2 $(4 \cdot 7 \mathrm{k} \Omega)$ in the basic circuit, as a bias element for $\operatorname{Tr} 1$. Thus these two transistors are directly coupled.

The bias for the first stage is a.c. bootstrapped to the emitter via C2a; this virtually eliminates the shunting effect of the bias elements and gives a relatively high input impedance, about $30 \mathrm{k} \Omega$ in this case.

An h.t. decoupling resistor and capacitor $R 4 a$ and C3a have been added to reduce mains hum to negligible proportions when used with a mains power unit. R1 now goes to the other side of the collector load R3. Feedback is provided by the treble control VR la. C4a serves to increase the negative feedback and hence reduce the gain at higher frequencies, by an amount determined by the setting of VR1a.


Fig. 4: Pre-amplifier and tone control circuits: additional components are suffixed a.

Bass boost and cut is provided by VR2a and its associated network.

The frequency response characteristics of the tone control circuits plotted against that of the basic amplifier is shown in Fig. 5.

## INPUT IMPEDANCE \& SENSITIVITY

Due to the higher input impedance, the sensitivity into the base direct (via Cla) is less than previously at 30 mV , but whereas the basic amplifier required a series resistor of $100 \mathrm{k} \Omega$ to give a sensitivity of 1 V , in this case the series resistor must be $1 \mathrm{M} \Omega$.

To make this clearer it will be remembered that the input impedance of the basic amplifier was about $300 \Omega$ with a sensitivity of 3 mV . It can be said therefore that the sensitivity is $3 \mathrm{mV} / 300 \Omega$ or $30 \mathrm{mV} / 3 \mathrm{k} \Omega$ if a series resistor of $2.7 \mathrm{k} \Omega$ is inserted, or $1 \mathrm{~V} / 100 \mathrm{k} \Omega$ with a series resistor of 99,700 ( $100 \mathrm{k} \Omega$ in practice). In other words $1 \mathrm{mV} / 100 \Omega$ above 3 mV .

Compare this with the base sensitivity/impedance now of $30 \mathrm{mV} / 30 \mathrm{k} \Omega$, or $100 \mathrm{mV} / 100 \mathrm{k} \Omega$ with a series resistor of $70 \mathrm{k} \Omega(68 \mathrm{k} \Omega$ in practice) or $1 \mathrm{~V} / 1 \mathrm{M} \Omega$ with a series resistor of $970 \mathrm{k} \Omega$ (1M $\Omega$ ) i.e. $1 \mathrm{mV} / 1 \mathrm{k} \Omega$ above 30 mV , or 10 times better than previously at an input impedance of $30 \mathrm{k} \Omega$ or more.

Matching the source impedance to the input impedance is not difficult, as it is not particularly critical provided the source impedance is equal to or less than the input impedance. For example a tuner might have an output of 100 mV and output impedance of $10 \mathrm{k} \Omega$, this would then be fed into the 100 mV input even though the impedance at this input is $100 \mathrm{k} \Omega$.

The only difficulty might be when it is desired to use a device with a very low source impedance, with an output of less than 30 mV and an impedance of considerably less than $30 \mathrm{k} \Omega$, such as a dyn-

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\hline OA2 \& 5/- \& 6CW4 \& 12/- \& 12AH7 5/- \& 90AG 67/6 \& DM71 9/9 \& EF97 8/- \& MHLD6 \& \(8130 \quad 25 /-\) \& \(\begin{array}{ll}\text { VP41 } \& 5 /- \\ \text { VR75 } \& 21 /-\end{array}\) \& \[
\begin{array}{ll}
\text { BA } 129 \& 2 / 6 \\
\text { BA130 } \& 2 /-
\end{array}
\] \& \[
\begin{array}{ll}
\text { OA79 } \& 1 / 9 \\
\text { OA81 } \& 1 / 9
\end{array}
\] \\
\hline OB2 \& 81. \& 6 D 3 \& 7/6 \& 12AT6 4/6 \& 90AV 67/6 \& DW4/350 \& EF48 9/- \& 12/8 \& SP4I3 \({ }^{\text {SP13C }}\) 19/6 \& \(\begin{array}{ll}\text { VR75 } \& 21 /- \\ \text { VR105 } \\ \text { SR }\end{array}\) \& \[
\begin{array}{ll}
\text { BA130 } \& 2 /- \\
\text { RCY10 }
\end{array}
\] \& \begin{tabular}{ll} 
OA81 \& \(1 / 9\) \\
OAB5 \& \(3 /-\)
\end{tabular} \\
\hline \(\mathrm{OB4}^{1}\) \& \(4 / 3\) \& 6156 \& \(3 / 7\) \& 12AT7 \(3 / 6\) \& 900G 34/- \& (1) \(8 / 6\) \& EF183 6/3 \& MLs 8/- \& \(8 \mathrm{BP13C}\) 12/6 \& VR105 5/- \& BCY10 5/- \& OAB5 \\
\hline 1 A3 \& \(2 / 6\) \& \(6 \mathrm{E5}\) \& \(9 / 6\) \& 12AU6 4/9 \& 90CV 33/6 \& DWF4/500 \& EF184 \(5 / 9\) \& \(\begin{array}{ll}\text { M } 4 \text { S } \& 20 / 5 \\ \text { MSP4 } \& 12 / 8\end{array}\) \& \(\begin{array}{lr}\text { SP'42 } \& 12 / 6 \\ 8 P 61 \& 8 /-\end{array}\) \& VT61A 7/- \&  \& OA90 \(2 / 6\) \\
\hline 1 A 4 \& 12/6 \& 6 Fl \& \(9 / 6\) \& \(12 \mathrm{AD7}\) 4/6 \& \(90 \mathrm{Cl} 16 /-\) \& DY88 \(8 / 6\) \& EHY0
EL32
E/6
E/- \& MSP4 12/8 \& 8P6I
TDD \(2 / 812 / 0\) \& VT61A
VT501
3/- \& \(\begin{array}{ll}\text { BCY33 } \& 5 /- \\ \text { BCY } 34 \& 5 /-\end{array}\) \& \(\begin{array}{ll}\text { OA90 } \& \text { OA91 } \\ 1 / 9\end{array}\) \\
\hline 145 \& \(5 /-\) \& 6F6G \& 4/- \& 12AV6 5/9 \& 150B2 14/6 \& DY86 5/9 \& EL32

3/- \& MXIto 12/6 \& TDD2A ${ }^{\text {TDD }}$ 7/6 \& VUl11 6/- \& BCY38 5\%- \& OA95 1/9 <br>

\hline 1A7GT \& $7 / 6$ \& ${ }_{\text {f }} \mathbf{F} 12$ \& 3/3 \& $12 \mathrm{AX7} 9 / 6$ \& $1500251 /$ \& DY87 5/9 \& $\begin{array}{cc}\text { EL33 } & \text { 12/- } \\ \text { EL34 }\end{array}$ \& | MX40 |
| :--- | :--- |
| N 37 |
| $23 / 3$ |
| 28 | \& TH4B $10 \%$ \& VU120 12/- \& $\begin{array}{ll}\text { BCY38 } \\ \text { BCY } 39 & 5 /- \\ \text { 5/- }\end{array}$ \& | OAB |  |
| :--- | :--- |
| OA182 | $1 / 9$ | <br>

\hline 101 \& $4 / 9$ \& (iF13 \& 3/6 \& 12AY7 9/8 \& 161 15/- \& $\begin{array}{ll}\text { E80F } \\ \mathrm{E83F} & \text { 24/- }\end{array}$ \& $\begin{array}{ll}\text { EL34 } & 9 / 6 \\ \text { EL35 } & 10 / \mathrm{c}\end{array}$ \& $\begin{array}{ll}\text { N37 } \\ \text { N78 } & 38 / 4\end{array}$ \& TH21C 10/6 \& VU120A12\%- \& BCZ11 3/6 \& OA200 3/- <br>

\hline 1 C 2 \& $7 / 6$ \& 6F14 \& 151- \& 12BA6 5/- \& 185BT 34/11 \& | E83F |  |
| :--- | :--- |
| E88CO | $24 /-$ |
| $12 /-$ |  | \& $\begin{array}{ll}\text { EL35 } \\ \text { EL36 } & \text { 10/9 }\end{array}$ \& $\begin{array}{ll}\text { N108 } & 28 / 7\end{array}$ \& TH30C 14/6 \& VUl33 \%/- \& BC107 4/2 \& O4202 2/- <br>

\hline $1 \mathrm{C8}$ \& $8 / 6$ \& 6 F15 \& $10 / 9$ \& 12BE6 $5 / 3$ \& 301 20/- \& ${ }_{\text {E18806 }}{ }_{\text {E180 }} 12 / 6$ \& $\begin{array}{lr}\text { EL36 } \\ \text { EL37 } & \text { 18/8 }\end{array}$ \& N339 25/- \& TH233 6/9 \& W42 11/- \& BC108 3/日 \& OA210 9/6 <br>
\hline $1 \mathrm{C5}$ \& $4 / 8$ \& $6{ }^{1} 17$ \& 12/6 \& 12BH7 6/- \& $\begin{array}{ll}302 & 16 / 6 \\ 303 & 15 /-\end{array}$ \& $\begin{array}{lrr}\text { E180F } & \text { 17/6 } \\ \text { E1148 } & 1 / 9\end{array}$ \& $\begin{array}{cc}\text { EL37 } & \text { 16/6 } \\ \text { ELA1 } \\ 8 /-\end{array}$ \& P41

P/6 \& TP22 5/- \& W61M $24 / 6$ \& B0109 4/6 \& OA211 13/6 <br>

\hline $1 \mathrm{C6}$ \& 10/6 \& 6 F 18 \& $8 / 6$ \& $\begin{array}{ll}\text { 12E1 } & 17 / 6\end{array}$ \& $\begin{array}{ll}303 & 15 /- \\ 305 & 16 / 6\end{array}$ \& | E1148 |  |
| :--- | :--- |
| EA50 | $1 / 8$ |
| $1 / 6$ |  | \& ELA2 $7 / 6$ \& $\mathrm{P}^{\text {¢ }}$ 1 1 2/6 \& T'P25 5/- \& W63 10/8 \& BC113 5/- \& OAZ20012/- <br>


\hline 105 \& $8 /$ \& $6 \mathrm{~F}^{23}$ \& 11/6 \& | 12J5GT |
| :--- |
| $1277 G 7$ |
| $8 / 6$ | \& $\begin{array}{ll}305 & 16 / 6 \\ 306 & 13 / \%\end{array}$ \& $\begin{array}{cr}\text { EA50 } \\ \text { EA76 } & 1 / 6 \\ \text { 13/- }\end{array}$ \& EL421 8/- \& PA13C80 7/6 \& TP2620 $7 / 6$ \& W76 3/6 \& BC115 3/- \& OAZ20110/6 <br>

\hline 1 D 6 \& 9/6 \& 6 F 24 \& $10 /-$ \& \[
$$
\begin{array}{ll}
1257 \mathrm{GT} & 8 / 6 \\
12 \mathrm{~K} 5 & 8 / \mathrm{F}
\end{array}
$$

\] \& | 306 |  |
| :--- | :--- |
| 807 | $11 / 9$ |
| $11 / 2$ |  | \&  \& $\begin{array}{cc}\text { EL81 } & 8 / 7 \\ \text { EL83 } & 6 / 9\end{array}$ \&  \& TY86F \& W77 2/6 \& $13 \mathrm{Cl16}$ 5/- \& OAZ202 9\%- <br>


\hline 1 1FD1 \& $6 / 7$ \& 6 F 25 \& 10/- \& $\begin{array}{ll}12 \mathrm{~K} 5 \mathrm{rat} \\ 12 \mathrm{~K} 7 \mathrm{GT} & 8 / 6\end{array}$ \& $\begin{array}{ll}807 \\ 856 & 11 / 8 \\ 2 /-\end{array}$ \& | FABC80 $5 / 9$ |
| :--- |
| FAC91 $3 / 3$ | \& EL83 4 cha \& $\begin{array}{ll}\text { PC88 } & 8 / 6\end{array}$ \& 11/10 \& W81m 6/- \& BC118 $4 / 6$ \& OAZ203 9/6 <br>

\hline 1 1119 \& $3 / 3$ \& 6 F 28 \& 10/6 \& 12 K 7 GT
12KGGT
$7 / 9$ \& $\begin{array}{lr}\text { 956 } & 2 /- \\ 1821 & 10 / 6\end{array}$ \& $\begin{array}{ll}\text { EACAC91 } \\ \text { EAF42 } & 3 / 3 \\ 7 / 6\end{array}$ \& EL85 7/6 \& PC95 6/9 \& UABC80 5/8 \& W101 26/2 \& BD119 9/\% \& OAZ204 9/- <br>
\hline 166 \& $61 /$ \& $6 \mathrm{~F}^{2} 2$ \& 3/- \& 12K8GT $7 / 8$ \& $\begin{array}{ll}1821 & 10 / 6 \\ 5768 & 10 \%\end{array}$ \& $\begin{array}{ll}\text { EAF42 } & 7 / 6 \\ \text { EB4L } & 4 / 9\end{array}$ \& EL86 8/- \& PC97 5/9 \& UAF42 7/9 \& W107 10/6 \& BFY50 5/- \& OAZ205 9/- <br>
\hline 1H5GT \& 7/- \& 6G6G \& 2/6 \& 12Q7GT $3 / 6$

$128 A 7 G T$ \& $\begin{array}{cc}5768 & 10 /- \\ 7475 & 2 / 6\end{array}$ \& | EBil |  |
| :--- | :--- |
| EB91 | $2 / 3$ | \& EL91 $2 / 6$ \& PC900 818 \& UB41 10/6 \& W729 101- \& BFX51 $4 / 6$ \& OAZ20710/8 <br>

\hline 114. \& $2 / 6$

$5 \%$ \& 6H6at \& 1/6 \& $\mathrm{l}^{28 \Delta 7 G T} 819$ \& | 7475 |  |
| :--- | :--- |
| 1834 | 201 |
| 20 |  | \& ${ }_{\text {EBC3 }}$ 20/6 \& EL95 5/- \& PCC84 5/6 \& UBC41 8/6 \& X24 18/6 \& BFY52 5f- \& OAZ210 7\%- <br>

\hline 1LD5 \& 5/6 \& 6.550 \& 3/9 \& $12 \mathrm{SC7}$ 4/- \& $\begin{array}{ll}\text { A1834 } \\ \text { ACO44 } & \text { 14/- }\end{array}$ \& EBC33 6\%- \& ELL80 13/- \& PCC85 619 \& UBC81 $6 / 6$ \& $\times 41$ 101- \& BF154 5/- \& OAZ22413/- <br>
\hline 1N5GT \& 7/6 \& 6 J 6 \& $3 /=$ \& 12 BH 78 3/- \& AC2PEN \& EBC41 713 \& EM71 14/= \& PCC88 10/6 \& UBF80 $5 / 6$ \& $\times 61$ 6/- \& BF159 5/- \& OCl8 25/- <br>
\hline 1 Pl \& 8/- \& ${ }^{6 J 76}$ \& 4/8 \& 128577 51- \& 19/6 \& EBC81 6/8 \& EM80 5/8 \& PCC89 9/9 \& UBF89 5/8 \& $\times 63$ \& BF163 4/- \& $\mathrm{OCR2}^{\text {OC2 }}$ 5/- <br>
\hline 1 P 10 \& $4 / 8$ \& 6JJ6GT \& $8 / 6$
$5 /$ \& 128 K 7 3/- \& AO2PEN/ \& EBC90 3/9 \& EM81 6/9 \& PCC189 8/3 \& UBL21 91- \& X64 $5 / 6$ \& BF167 $2 / 8$ \& 0623 \% <br>

\hline $1 \mathrm{Pl1}$ \& $5 / 8$ \& 6K7G \& 1/3 \& $\begin{array}{ll}128 Q 7 & 8 /- \\ 12987 & 5 /-\end{array}$ \& DD $18 / 8$ \& ${ }_{\text {EBF80 }}$ EBC91 $5 / 9$ \& EM84 $\begin{gathered}\text { 6/- } \\ \text { EM85 } \\ \text { 11/- }\end{gathered}$ \& $\begin{array}{ll}\text { PCF80 } & 8 / 3 \\ \text { PCF82 } & \text { 6/- }\end{array}$ \& $\begin{array}{ll}\text { UC82 } & 5 / 6 \\ \text { UCC84 } & 8 / 6\end{array}$ \& $\begin{array}{ll}\times 65 & 5 / 6 \\ \times 66 & 7 / 8\end{array}$ \& $\begin{array}{ll}\text { BF173 } & 2 / 6 \\ \text { BF184 } & 2 /-\end{array}$ \& | 0 CO |  |
| :--- | :--- |
| $\mathrm{OCL25}$ | $5 /-$ | <br>

\hline $1 \mathrm{R5}$ \& $4 / 9$ \& 6 K 7 GT \& 4/6 \& $\begin{array}{ll}12627 & 5 /- \\ 12 \mathrm{~V} 4 & 2 /\end{array}$ \& AC6PEN $4 / 9$ \& EBF80 ${ }_{\text {ESF83 }}$ 7/9 \&  \& PCF84 8\%- \& UCC85 8/6 \& $\times 76 \mathrm{M}$ 7/8 \& BY100 $3 / 6$ \& 00285 <br>
\hline 184 \& 4/9 \& 6 K 8 G \& $3 /-$ \& $\begin{array}{ll}12 \times 4 & 2 j- \\ 13 \mathrm{D} 1 & 5 /-\end{array}$ \& AC/PEN (5) \& EBF889 $5 / 9$ \& EY51 5/6 \& PCF86 8/- \& UCF80 818 \& $\times 40 / 8$ \& BY101 11/8 \& OC29 16/6 <br>
\hline 185 \& 3/3 \& 6 K 8 GT \& $7 / 6$ \& 13D1 \& AC/PEN (7) \& EBL21 10/3 \& EY81 7/- \& PCF801 8/6 \& UCH21 9/- \& X81M 29/1 \& BY105 1016 \& $0 \mathrm{C30}$ 7/- <br>
\hline 172 \& 34/11 \& 6K25 \& 24/- \& $\begin{array}{ll}1303 \\ 1447 & 9 / 6\end{array}$ \& AC/PEN $19 / 6$ \& ${ }_{\text {EC52 }}$ \& EY83 9/- \& PCF802 9/6 \& ЈCH42 $8 / 6$ \& X101 29/1 \& BY114 8/- \& OC35 10\%- <br>
\hline ${ }^{1 T 4}$ \& $2 / 6$
$5 / 6$ \& 6 L 1 \& 101 \& $\begin{array}{lr}1487 \\ 1487 & 19 / 6\end{array}$ \& AC/THI10\% \& ${ }_{\text {EC53 }}$ 12/6 \& EY84 9/6 \& PCF805 9/8 \& UCH81 6/- \& X109 26/- \& BY234 4/- \& OC36 $\quad 7 / 6$ <br>
\hline 1U5 \& 5/8 \& 6L6GT \& 718 \& 18 12/6 \& AC/TP 19/6 \& EC54 6/- \& EY86 5/9 \& PCF80611/6 \& UCL8'2 7- \& Y63 5/- \& BY236 4/- \& $0 \mathrm{C38} 11 / 8$ <br>
\hline $2 \mathrm{D130}$ \& $7 \%$ \& 6 L 18 \& $7 / 6$ \& 19 10/6 \& AC/VP1 12f- \& EC70 4/9 \& EY87 518 \& PCFP08 12/6 \& UCLA3 819 \& Y65 51- \& BY238 4/- \& $0 \mathrm{OC4} 1$ 10/- <br>
\hline 2 D 21 \& $5 / 8$ \& 6 L 19 \& 19\%- \& 19AQ5 5/- \& AC/VP2 11/- \& EC86 11/6 \& EY88 7/6 \& PCL81 9/- \& UF41 $7 / 9$ \& Z63 4/9 \& BYZ12 5\%- \& $0 \mathrm{C42}$ 6/9 <br>
\hline 2X2 \& 3/- \& 6 LD 20 \& 6/8 \& 20 D 1 13/- \& $\begin{array}{ll}\text { ATP4 } 4 & 2 / 8\end{array}$ \& EC88 10/6 \& EX91 3/- \& PCL88 6/3 \& UF42 $4 / 9$ \& 2868 \& BYZ13 5/- \& OC43 12/6 <br>
\hline 3 A 4 \& $3 / 6$ \& $6 \mathrm{CP7GT}$ \& ${ }^{71}$ \& $20 \mathrm{D} 4 \quad 2015$ \& AZ1 81- \& EC91 4/- \& EZ35 5/3 \& PCL83 8/6 \& UF80 \& 777 \& CG12E 4/- \& $0 \mathrm{C44}$ 2/- <br>
\hline 3A5 \& 8f. \& 6 Pl \& 12/- \& $20 \mathrm{~F} 211 / 6$ \& AZ31 7/9 \& EC92 6/6 \& EZ40 6/- \& PCL84 7 \& 85 \& 2329 11/6 \& CG4\% $4 /$ \& $0 \mathrm{C44PM} 8 / 3$ <br>
\hline 3B7 \& $5 /-$ \& 6 P 25 \& 12\% \& $20 \mathrm{LI} 15 / 6$ \& AZ41 6/6 \& ECC31 15/6 \& EZ41 6/6 \& 85 \& UF86 91 \& 2729 6/3 \& GD3 $\quad 8 / 6$ \& OC45 $1 / 8$ <br>
\hline 3D6 \& 3/9 \& 6 P 26 \& 121- \& $20 \mathrm{Pl} 17 / 8$ \& B36 4/9 \& ECC32 $4 / 6$ \& EZ80 3/9 \& 8 \& UF89 5/8 \& 23 \& GD4 6/6 \& 0646 <br>
\hline 3Q4 \& $5 / 3$ \& 6 P 28 \& $251-$ \& 20P3 17/- \& BL63 10/6 \& ECC33 20/1 \& EZ81 4/3 \& PCL88 15/- \& $\begin{array}{ll}\text { UL41 } & 8 / 8 \\ \text { UIA6 } & 9 / 6\end{array}$ \& Transistors \& GD6 $5 / 6$ \& OC65 22/6 <br>
\hline $3 \mathrm{C5GT}$ \& 6/6 \& 6476 \& $5 / 0$ \& 20P4 17/6 \& CK506 8/6 \& EGC34 $29 / 6$ \& EZ90 \& PEN45D ${ }^{\text {P }}$ \& UL84 5/8 \& and diodes \& GD8 4/- \& OC66 25/- <br>
\hline 384 \& 4/8 \& 607GT \& $8 / 9$ \& $20 \mathrm{P5}$ 171- \& CL4 19/6 \& ECC35 4/9 \& 006 \& 19/6 \& UM80 5/- \& $2 \mathrm{C} 22510 / 8$ \& GD9 4/- \& 0070213 <br>
\hline 3 V 4 \& $6 / 6$ \& 6R7G \& 5/6 \& $25 \mathrm{A6G}$ 7/8 \& CL33 19/6 \& ECC40 $0 / 6$ \& GZ30 7/6 \& \& URIC 6/6 \& 2N404 6/- \& G110 4/- \& 0 C 71 2/- <br>
\hline 4D1 \& 3/9 \& 6 6 7 GT \& 11/- \& $25 \mathrm{LG6}$ 4/9 \& CV6 2/6 \& ECC81 3/6 \& $\begin{array}{ll}\text { G230 } & 7 / 6 \\ \text { GZ32 } & 0 /-\end{array}$ \& PEN383 $9 / 8$ \& UU5 7/- \& AA120 3/- \& GD11 4\% \& 0072 2/- <br>
\hline SR4GY \& 8/9 \& 68A7GT \& $7 /$ \& 25 Y 5 6\%- \& CV63 10/6 \& $\mathrm{ECC8}^{4 / 6}$ \& $\begin{array}{ll}\text { GZ32 } & \text { G233 } \\ \text { G2/8 }\end{array}$ \& PEN384 \& UU8 16/6 \& AA129 3/- \& GD12 4/- \& 0c73 16/- <br>
\hline 6U4G \& $4 / 8$ \& $68 \mathrm{C7}$ \& 616 \& $25 Y 50$
$25 \mathrm{Z} \mathrm{SG}^{8 / 6} 86$ \& $\begin{array}{ll}\text { CV271 } & 12 / 6 \\ \text { CV428 } & 19 /-\end{array}$ \& $\begin{array}{ll}\text { ECC83 } & 4 / 6 \\ \text { ECC84 } & 5 / 6\end{array}$ \& $\begin{array}{ll}\text { G233 } & \text { 1234 } \\ \text { 10/- }\end{array}$ \& PEN $3811 / 6$ \& UU12 $4 / 3$ \& AC107 3/6 \& GD14 10/- \& $0 \mathrm{C74}$ 8/- <br>
\hline 5 C 4 G \& 81- \& 68677 \& 7/9 \& 2524G 8/3 \& CV428 19/- \& ECC84 5/6 \& $\begin{array}{ll}\text { G234 } & 14 / 6\end{array}$ \& PEN453DD \& UY1N 10/3 \& AC113 5/- \& GD15 81- \& $0 \mathrm{C75}$ 2/- <br>
\hline 6Y3GT \& $51 /$ \& $68 \mathrm{H7}$ \& $3 /-$ \& $\begin{array}{ll}2525 & 7 / \% \\ 25869\end{array}$ \& $\begin{array}{lr}\text { CY1 } & 18 / 4 \\ \text { CY1C } & 8 / 6\end{array}$ \& ECO88 7/- \& H30 5/- \& PEN4.19/6 \& UY21 8/- \& AC114 8i- \& GD16 4/- \& $0 \mathrm{C76} 3 /-$ <br>
\hline 5 53 \& $7 / 6$ \& ${ }_{6857}$ \& $5 / 8$ \& $\begin{array}{ll}25260 & 8 / 6 \\ 30 \mathrm{Cl} & 6 / 3\end{array}$ \& $\begin{array}{ll}\text { CY1C } & 6 / 6 \\ \text { CY31 } & 6 / 6\end{array}$ \& ECC189 9j- \& HABC80 9/3 \& PENA4 19/6 \& UY41 5/6 \& ACl26 2/- \& GET102 8/6 \& $0 \mathrm{CJ} 73 / 4$ <br>
\hline 5Z4G
$6 / 30 \mathrm{~L} 2$ \& $7 / 6$ \& 68K7
68N7GT \& 4/6 \& $\begin{array}{ll}30 \mathrm{Cl} & \text { 6/3 } \\ 30015 & 12 /-\end{array}$ \& $\begin{array}{ll}\text { D131 } & 1 / 3\end{array}$ \& ECC804 12/6 \& HL:2 7/8 \& PEN/DD \& UY85 4/9 \& ACl27 2\%- \& GET103 4/- \& OC78 3/- <br>
\hline 6/30L2 \& $12 / 6$
$7 / 6$ \& 68N7GT \& 4/8 \& $\begin{array}{ll}30 \mathrm{Cl15} & 12 /- \\ 30 & 13\end{array}$ \& D15 15/6 \& LCO807 19/9 \& HL13C 4/- \& $4020 \quad 17 / 6$ \& U10 9/- \& AC128 2f- \& GET10518/- \& OC78D 3/- <br>
\hline $6 A 80$
$6 A C 7$ \& $7 / 6$
$3 /-$ \& $68 Q 7$
6887 \& $61-$
$2 /-$ \& $\begin{array}{ll}30 \mathrm{Cl18} & 13 / 6 \\ 30 / 6\end{array}$ \& D63 5/- \& ECF80 $7 /$ - \& HL22 10/6 \& PFL20013/6 \& U12/14 7/6 \& ACIS4 5/- \& GET111 \& $0 \mathrm{C79}$ 8/- <br>
\hline 6AC7 \& 3/6 \& 6887
687 \& 12/6 \& $30 \mathrm{F5}$ 11/6 \& 1777 2/3 \& ECF82 $6 / 9$ \& HL23DD $5 /-$ \& PL33 9/- \& U16 15/- \& ACl0 6/B \& 15/6 \& OC81 . 21- <br>
\hline 6Ag7 \& $2 / 6$
$5 / 9$ \& 68T7
6 U 4 GT \& $1 / 6$
$9 / 6$ \& $30 \mathrm{FL1} \mathrm{15/6}$ \& DAC32 7/- \& ECF86 8/6 \& HLal 3/9 \& ${ }^{\text {Pl36 }}$ 9/- \& U17 5/- \& ACl56 4/- \& GET113 4/0 \& OC81D 2/- <br>
\hline 6AJ5 \& $8 / 6$ \& 6U5G \& $5 /-$ \& $30 \mathrm{FL12} 15 /-$ \& DAF91 3/3 \& ECF804 $24 /$ - \& HL410D \& PL38 19/9 \& U18/20 $6 / 6$ \& $\begin{array}{lll}\text { ACl5 } & 5 /-\end{array}$ \& GET114 $1 / 8$ \& $0 \mathrm{Ocs1m} 5 /-$ <br>
\hline 6AK5 \& 4/9 \& 6U7G \& 710 \& $30 \mathrm{FL14} 12 / 6$ \& DAF96 6/- \& ECF80512/6 \& $18 / 6$ \& PL81 6/9 \& U13 40/- \& Ac165 b/- \& GETI1517\%- \& OC82 $2 / 3$ <br>
\hline 6AK6 \& 6/- \& 6V6G \& 3/6 \& $30 \mathrm{LL} \quad 5 / 6$ \& DCC90 8/- \& ECH3 23/3 \& HLA2DD8\% \& PL81A 6/9 \& U22 5/8 \& ACl66 5/- \& QETI16 $7 / 8$ \& 00820 <br>
\hline 6AK8 \& $5 / 9$ \& $6 \times 4$ \& $3 / 6$ \& $30 \mathrm{L15}$ 14/- \& DD4 10/6 \& ECH21 9/8 \& $\mathrm{HLl33DD}_{9 / 6}$ \& PL82 5/9 \& U25 12/6 \& ACl67 12/ \& GET118 4/6 \& 0 Ocs 3 2/- <br>
\hline 6 611.5 \& $2 / 3$ \& 6X5GT \& 5/3 \& 301.17 13/- \& DD41 $12 / 6$ \& ECH33 $22 / 8$ \& HN309 26/6 \& PL83 8/- \& 426 11/- \& AC168 \& GEF119 4/6 \& Ocrs 3/- <br>
\hline 6AM4 \& 18/8 \& 6Y7G \& 12/6 \& $30 \mathrm{P} 4 \mathrm{MR}^{11 / 6}$ \& ${ }_{\text {DF33 }}{ }^{\text {D/6 }}$ \& ECH35 8/- \& HN309 $26 / 6$ \& ${ }^{\text {PLL84 }}$ P150 ${ }^{\text {P/3 }}$ \& U33 13/6 \& ${ }^{\text {ACl }}$-69 $11 \%$ \& GET573 8/6 \& 0 Cl 39 121- <br>
\hline 6AMb \& $2 / 6$
$3 / 3$ \& 7A7 \& 12/6 \& M ${ }_{13 /-}$ \& ${ }_{\text {DF66 }}$ 151- \& ECH81 5/- \& HYR2A ${ }^{\text {H/9 }}$ \& ${ }^{\text {PLL504 }} 15 /$ 1- \& U35 16/6 \& $\begin{array}{ll}\text { ACli7 } & \text { 5/6 }\end{array}$ \& GET872 10\% \& 0 Cl 40 19/- <br>
\hline 6AM6 \& $4 / 8$ \& $7 \mathrm{B6}$ \& $10 / 9$ \& 30 P 12 11/- \& DF72 301- \& ECH83 \% \& IW3 5/6 \& Pw84 9/3 \& U37 34/11 \& ADl40 8/- \& GET873 4/- \& OC169 3/9 <br>
\hline 6AR8 \& 20\%- \& 787 \& 71. \& 30 P 19 11/- \& DF91 $2 / 6$ \& ECE84 $6 / 6$ \& IW4/350 5/6 \& PX4 14/- \& U45 15/6 \& AD149 8/- \& GET874 \& OC170 2/6 <br>
\hline 6AT6 \& 3/9 \& $7 \mathrm{7C5}$ \& 401- \& 301 L1 15/- \& DF96 6\%- \& ECL80 6/- \& IW $15006 /-$ \& PY80 5/- \& U50 5/- \& AF102 18/- \& 23/6 \& 00171 3/4 <br>
\hline 6AU6 \& $5 / 6$ \& 7C6 \& 6/- \& 30PL13 15/- \& DF97 10/- \& ECL82 6/3 \& K BC32 20/5 \& PY81 5/- \& U52 4/9 \& AF114 4/- \& GET882 10/ \& $0 \mathrm{OC172}$ 4/- <br>
\hline 6AV6 \& 5/- \& $7 \mathrm{H7}$ \& 5/- \& 30 PL14 15/- \& DH30 15/6 \& ECL83 9/- \& KF35 12/6 \& PY82 5/- \& U76 4/6 \& AF115 3/- \& GETP877 4/6 \& OC200 8/6 <br>
\hline 6B8G \& 2/6 \& $7 \mathrm{N7}$ \& 12/6 \& 30 PL 15 15/- \& DH63 5/- \& ECL84 12\% \& KL35 11/6 \& PY83 5/6 \& U78 3/6 \& AF'116 3/- \& GET889 4/6 \& OC201 23/- <br>
\hline 68A6 \& 4/6 \& 7 V 7 \& $51-$ \& 35 A5 15/- \& DH76 3/6 \& ECL85 11/- \& K LL32 21/7 \& PY88 7/3 \& U101 19/8 \& AF117 8/4 \& GET890 4/6 \& $0 \mathrm{O} 202 \mathrm{5} / 6$ <br>
\hline 6BE6 \& 4/3 \& 7 Y 4 \& $8 / 6$ \& 35L6GT 8/3 \& DH77 8/9 \& ECL86 $7 / 9$ \& KT2 51- \& PY800 6/- \& U107 17/6 \& AF118 3/- \& GET896 4/6 \& OC203 5/6 <br>
\hline 6BG6G \& 2015 \& 9BW6 \& $9 / 6$ \& 35 W 4 4/6 \& DH81 $10 / 9$ \& ECLL800 \& KT8 15/- \& ${ }^{1} \mathrm{Y} 801$ 6/- \& U191 12/- \& AF119 3/- \& GET897 4/6 \& OC204 10/6 <br>
\hline 6 BH 6 \& 6/6 \& $9 \mathrm{9D2}$ \& $3 / 8$ \& $35 \mathrm{Z3}$ 101- \& DH101 25/- \& $23 / 9$ \& KT32 4/9 \& PZ30 9/6 \& U251 12/6 \& AF124 $7 / 8$ \& OET898 $4 / 6$ \& 002061016 <br>
\hline $6 \mathrm{BJ6}$ \& $7 /$ \& $9 \mathrm{D7}$ \& 7/6 \& 35Z4GT 4/6 \& DH107 ${ }^{\text {d }} 11$ \& $\mathrm{EF}^{2} 26 / 6$ \& KT36 2918 \& QP21 5/- \& U281 819 \& AF125 3/6 \& GEX13 $3 / 6$ \& OC812 87- <br>
\hline 6BQ5 \& $4 / 6$ \& 10 Cl \& 9/- \& 35Z5GT 5/6 \& 16/11 \& EF36 3/- \& KT41 18/6 \& QQVO3/10 \& U282 12/3 \& AF126 $7 /-$ \& GEX 35 4/6 \& OCP7 $27 / 6$ <br>
\hline ${ }_{68 \mathrm{BP7A}}$ \& 7/- \& $10 \mathrm{C2}$ \& 12 J \& 42 5/- \& DK32 716 \& EF39 5\% \& KT44 519 \& $120{ }^{30 /-}$ \& U309 12/6 \& AF128 3/6 \& GEX3 10, \& ORP12 19/6 <br>
\hline $6 \mathrm{BR7}$ \& 9/- \& 1012 \& 11/8 \& 43 101- \& DK40 10/6 \& EF39 8/0 \& KTf3 4 ¢ $/$ - \& $10 / 6$ \& U403 6/6 \& AF139 10/- \& GEX45010 \& T82 12/6 <br>
\hline 6B78 \& 8/8/8 \& 10F1 \& 15/- \& 50A5 21/10 \& DK92 \& EF41 9/- \& $\begin{array}{lll}\text { KT66 } & 16 / 6\end{array}$ \& Q8150/15 \& U404 6\% \& ${ }_{\text {AF179 }}$ AF13/6 \& 15/- \& 8X641 10j- <br>
\hline 6887 ${ }_{\text {63W }}$ \& 18/6 \& 10 FP \& 15/- \& 50C5 $5 / 8$ \& DK96 8/6 \& EF42 3/6 \& КТ74 12/6 \& Q816 \& U801 18\%- \& AF180 $9 / 6$ \& CEEX64 11/6 \& V10/15A <br>
\hline 63W6 \& 7/\% \& 10 Fl 18 \& $9 /-$ \& 5006D6G40/9 \& DL33 6/6 \& EF50 $2 / 6$ \& KT76 7/6 \& R10 15/- \& U4020 6/- \& AF181 14/- \& GEX66 15/- \& 12/- <br>
\hline 6BX6 \& 4/6 \& 10LD3 \& 6/6 \& 50L8GT 61- \& DL35 4/8 \& EF54 6/- \& K'T88 $27 / 6$ \& R11 19/6 \& VMP4G 17/- \& AF'186 10\% \& GT3 5/- \& XA102 19/6 <br>
\hline 6 C 4 \& $2 / 3$ \& 10LD11 \& 10\% \& 52 KU 14/6 \& DL72 15/- \& EF80 4/6 \& KTW61 4/8 \& $\mathrm{R12} 516$ \& VP2 $3 / 6$ \& AFZ12 5/- \& M1 $2 / 10$ \& XA103 15/- <br>
\hline 6G5GT \& 6/- \& 10P13 \& 14/6 \& 53 KU 14/6 \& DL75 30/- \& EF83 $9 / 9$ \& KTW62 $12 / 6$ \& R16 34/11 \& VP2B ${ }_{\text {VP4 }} 9 / 8$ \& A8Y27 10/- \& M3 2/10 \& MAT100 7/9 <br>
\hline 6C6 \& $3 / 9$ \& 10P14 \& 15/6 \& $72 \quad 6 / 6$ \& DL92 4/9 \& EF85 4/6 \& KTW63 4/- \& R17 17/6 \& VP4 14/6 \& A8Y28 8\%- \& OA5 5/6 \& MAT101 8/6 <br>
\hline 6 CP \& 10/9 \& 12A6 \& $5 /-$ \& 77 5/- \& DL94 5/6 \& EF86 6/3 \& KTZ41 8/- \& R18 9/6 \& VP4A 14/6 \& A8Y29 10/- \& OA10 B/6 \& MAT120 $7 / 9$ <br>
\hline $6 \mathrm{CD6G}$ \& 19/6 \& 12AC6 \& 81- \& 78 4/9 \& DL96 6/- \& EF89 4/9 \& 163 4/6 \& R19 6/9 \& VP4B 11/- \& AY100 261- \& OA47 2/- \& Mati21 8/6 <br>
\hline 6CD7 \& 9/6 \& 12AD6 \& $9 \%$ \& 80 5/3 \& DLE10 10/8 \& EF91 3/3 \& LP2 9/6 \& R52, 7/8 \& VP13C 7/- \& BA115 $2 / 8$ \& OA79 31- \& P3464 2/- <br>
\hline 6x, 6 \& 6/- \& 12AE6 \& 7/6 \& 85A2 $2 / 6$ \& M70 6/- \& EF92 $2 / 6$ \& MHD4 7/6 \& RK34 7/6 \& VP23 2/6 \& BA116 \%\% \& OA73 3/- \& ZE12V7 1/9 <br>
\hline
\end{tabular}

MATCHED TRANSISTOR SETS 1-OC44 and 2-OC45 8/6; 1-OC81D and 2-OC81 7/8; 10C82D and 2-0C82 8/6; Bet of three-OC83 (GET118/119) 8/6; 1-GET874P sleeved Fellow, 13a130) 17/G. Postage Ad, per set
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Fig. 5: Frequency response characteristics of the complete amplifier and tone control system.
amic microphone. This difficulty could be overcome by using a pre-set in place of R2a, with the slider taken to earth via a $100 \mu \mathrm{~F}$ capacitor. This would then give an input impedance range of $300 \Omega$ to $30 \mathrm{k} \Omega$, being $300 \Omega$ at better than 1.5 mV with the capacitor at the emitter end of R2a. Adjusting the slider will optimise the sensitivity for any value of source impedance up to $30 \mathrm{k} \Omega$, above which it has no advantage whatsoever, and robs the circuit of its very low noise properties.

## OVERLOAD CAPABILITY

The foregoing remarks concerning sensitivity for maximum output assume the volume control at maximum, but the overload capability of the stages preceding the volume control is about four times, so the maximum input into the 30 mV terminal can be 120 mV , and into the 100 mV terminal 400 mV and so on.

Even so, some crystal pick-ups will overload the first stage and result in distortion unless the series resistor is increased in value. An example is the TC8H cartridge which on loud passages has an output of about 6 V r.m.s., so in this case the series resistor could well be 2 to $4 \mathrm{M} \Omega$ to prevent overload distortion. However, with this type of input, with the load resistor in series, there is a noticeable loss of top response when the resistor exceeds $1 \mathrm{M} \Omega$, due to the capacitive nature of crystal pick-ups, and it is necessary to compensate for this by shunting the whole or part of the series resistor(s) with a small capacitor of 50 to 100 pF , the most suitable value being a matter of individual taste, found by trial.


Fig. 6: Wiring to the bass, treble and volume controls. Tags referred to are those in Fig. 8.


Fig. 7: Input and balance control arrangement for stereo operation. Suitable for use with a crystal or ceramic pickup.

Alternatively, an attenuator could be used in the input and its simplest form could be a $1 M \Omega$ pre-set across the input, with the slider taken via Cla to the base of Trla. The slider should at all times be near the earthy end of the control.

## STEREO OPERATION

Two of these amplifier units can be used to pro-


Fig. 8: Modified tagboard layout. The sensitivity/impedance matching network is not shown: this consists of a group of sockets mounted at the rear of the chassis.


Fig. 9: Simple mains power supply unit for the basic 1-watt amplifier

## components list

## Resistors:

| R1a | $10 \mathrm{k} \Omega$ |
| :--- | :--- |
| R2a | $1.2 \mathrm{k} \Omega$ |
| R3a | $10 \mathrm{k} \Omega$ |
| R4a | $1 \mathrm{k} \Omega$ |
| R5a | $1.5 \mathrm{k} \Omega$ |
| R6a | $1 \mathrm{k} \Omega$ |

## Capacitors:

| C1a | $25 \mu \mathrm{~F}$ electrolytic 6 V |
| :--- | :--- |
| C2a | $8 \mu \mathrm{~F}$ electrolytic 6 V |
| C3a | $25 \mu \mathrm{~F}$ electrolytic 12 V |
| C4a | $5,000 \mathrm{pF}$ paper or polyester |
| C5a | $0.1 \mu \mathrm{~F}$ paper or polyester |
| C6a | $0.47 \mu \mathrm{~F}$ paper or polyester |

Transistors:
Tria OC45
Tr1 2G371
vide stereophonic reproduction, simply by utilising dual controls for volume and tone control functions, and adding a balance control.

This is shown in Fig. 7. The 56 pF capacitors shunting the series resistors are optional and are to compensate for some loss of top due to the high series resistors.
A tweeter may be incorporated in the speaker system, provided the main speaker is not less than $15 \Omega$ impedance, and the tweeter, also $15 \Omega$, is fed via a reversible or non-polarised capacitor of not more than $4 \mu \mathrm{~F}$.

## OPERATION FROM THE MAINS

The power requirements are modest and a mains transformer rated at 9 or 10 V at 0.5 amp and a 0.5 amp 12 V selenium bridge rectifier are more than adequate to supply either a single amplifier or two amplifiers of a stereo pair.

A suitable power supply circuit is shown in Fig. 9, but constructors intending at some future time to proceed with the power amplifier described next will do well to obtain the larger mains transformer and rectifier specified with this, using one-half of the centre tapped secondary to obtain the 12 V required for the 1 watt unit.

## To be continued

## ADAPTABLE LOW COST HI-FI SYSTEM <br> (Part 1, December issue)

The text giving Chassis Details on page 614 should have appeared instead at the end of the article on page 572. The author has drawn our attention to the fact that the Texas range of transistors (i.e. 2 G 371 etc.) were used in the prototype. He recommends their use if the performance figures given are to be expected. If constructors experience difficulty in obtaining these semiconductors, and other components, they may be obtained from Messrs. C. \& D. Electronics, 17 St. Luke's Road, Pallion, Sunderland. They can supply the recommended transistor package (matched set of driver and output pair) at 12 s .6 d . per set.

## LETTER5

## Letter of thanks

I feel very flattered to think that fellow readers have responded to my appeal for help as they have. I am also grateful to you for publishing my letter.
Readers and yourself will therefore be pleased to know that I succeeded in getting results, after replacing the electrolytics, and repairing a broken joint on the L.S. mains windings.-W. M. Mackenzie (Gosport, Hamts.).

## Not only button pushing!

I would like to comment on the letter by R. T. Brown in the September issue of P.W. As a part-time commercial operator, I object to the statement that the only qualification to operate is the ability to push a button and speak into the microphone. The
ability to rig aerials and to maintain the equipment is essential in most cases.

I would like to see some of the "competent amateurs" working directed net with ten outstations under difficult conditions.
I personally do not want a licence because I could not stand the few poor amateurs to be found on the bands in this district. I am no anti-RAE or anti-Morse man, but I do consider myself a competent operator in my own field and would like to be treated as such and not as just a "button pusher".-M. Fisher (Huddersfield, Yorkshire).

## 19 Set Mods '"Mods'"

I have, with the assistance of Mr. S. Simpson's extremely good articles on 19 Set Mods, modified my own 19 Set. I found it
beneficial to earth the centre pin on the set's tone control pot, but I have gone one step further. I by-passed a $4,800 \Omega$ resistor fixed to the b.f.o. triode anode tag. I now find that s.s.b. signals are not saturated as was the case before. A further modification I attempted was for Top Band. Four 100 pF capacitors ( $1 \%$ silver mica) which were to hand, were fitted across the four ganged tuning capacitors and earthed through a four-pole two-way wafer switch when necessary.

I am pleased to say that this modification is successful and by moving the wavechange switch to the 4.5 to $8 \mathrm{Mc} / \mathrm{s}$ position, I find that Top Band appears between 2 and $2.5 \mathrm{Mc} / \mathrm{s}$. This is very convenient as it is on the same scale as 80 metres.-J. Scott (Newquay, Cornwall).

# RTM DATA RUC: 

THE Practical Wireless Data-Rule was originally presented free with the November issue of this magazine, together with complete summary of instructions. This is the second of a short series of articles explaining the use of the rule, especially aimed at the beginner. The rule is now available from the Practical Wireless Blueprint Department, price 5/-.

Last month's article dealt with the more general uses of the $L$ and $M$ scales, the component tolerance scale, the reciprocal scale, the decibel scale and the log scale. This article will now complete the instructions concerning the same side of the rule.

## DIRECT CONVERSION

The rule provides a means of ready conversion between many of the more common electrical units, or units closely associated with electrical engineering or electronics.

Conversion between two given units is straightforward given suitable $\log$ scales, such as the L and M scales on the rule. It is only necessary to place the significant figures of two equivalent units adjacent to each other, for the rest of the rule to then give direct conversion. Take, for example, conversion between metres and yards. Now it is known that $1 \mathrm{~m} .=1.09 \mathrm{yds}$., therefore, if the 1 of scale $L$ is placed adjacent to the 1.09 of scale M , direct conversion between the two units is now possible. Thus, if we wished to know the metric equivalent of 6 yards, this is found to be $5 \cdot 5$ metres, for $5 \cdot 5$ in scale $L$ is adjacent to 6 in scale M, i.e., scale $L$ reads in metres, scale M in yards.

The decimal point may be placed easily if a note is made of relative magnitude at the initial setting. In the previous example, with the rule set as indicated, since scales read 1-10, direct conversion between scales is possible, and thus if one scale was multiplied by some factor of 10 , the other scale must be multiplied by a similar factor. Thus had we wished to know the netric equivalent of 600 yards, we would call this $6.0 \times 10^{2}$ in scale $M$, giving the reading in scale $L$, as indicated, but also $\times 10^{2}$, i.e., $5.5 \times 10^{2}=550$ metres.

Take the point where the conversion falls off the scale, for example, find the distance in yards corresponding to 9.5 m . The rule must be reset, placing the 10 of scale $L$ opposite the 1.09 of scale M. The significant figures of


Fig. 9: Conversion to $k W$. hours of $72 \times 10^{6}$ joules.
the answer are then seen to be 1036, but this is known to represent the end of rule, in scale $M$, just above the 10 . Thus we can correct this to read the true answer, 10.36 yds.

It is thus possible to mark on the slider, marks indicating the conversion factors between various units, and this is done on the Data Rule in windows combining I and $\mathbf{J}$. When the slider is set so that the correct conversion factor is set on scales $L$ and $M$, the appropriate units are displayed in the window. Note that there are two windows. and any units conversion may only appear in one window at once.

It has been shown that when the I of scale $L$ has been set against the correct conversion factor in scale $M$, direct reading conversion is available, where the bottom scale is multiplied by the same factor as is required to be multiplied by the indicated value in scale L. A further conversion factor may be required to allow for differences in magnitudes. Now when the scale is reset to 10 in scale $L$, it is necessary to multiply by 10 on top of any other conversion factors. This factor consideration is taken into account automatically by the calculator, by means of the two small circular Conversion Factor windows in the two bottom corners of the rule. When the slider is pulled out to the left of the rule, units to be converted will only appear in the left-hand IJ window, and the conversion factor will appear in the left-hand small circular window, both right-hand windows remaining blank. The converse applies, i.e., with the slider pulled out to the right, the appropriate conversion factor appears in the right-hand small circular window, the units to be converted being in the right-hand IJ window, the left-hand windows being blank. Thus a diflerent conversion factor will appear for the same units conversion, according to the choice of two slider settings.

The procedure to convert between the units given on the rule is thus as follows. Expose the desired units conversion in one or other of the two units conversion windows. When this is done, as the black arrows indicate, the I portion of the window indicates the units described by the L scale, and the J portion of the window indicates the units described by the M scale. The conversion factor in the appropriate small circular window then indicates the multiplication factor of scale M for this to read correct conversion from scale L , where the units in scale $L$ refer to magnitudes of between 1 and 10 . Thus, if the indicated conversion factor is $10^{n}$, and if it is necessary to multiply a quantity in scale L by $10^{*}$ to give it in the form $\mathrm{N} \times 10^{\times}$, where N is between I and 10 , then multiply the read-off value in scale M by $\times 10^{n+x}$. Due to the space available in the conversion factor windows, a minus index could not be shown in the usual form $\times 10^{-n}$, and has instead been shown with.
a bar above the index, thus: $\times 10^{\bar{n}}$.
Example: Convert $72 \times 10^{6}$ joules into $\mathrm{kW} . \mathrm{hrs}$. (see Fig. 9). This must firstly be mentally converted to the form $7.2 \times 10^{7}$ joules, and a wise precaution is to jot down the factor $\times 10^{7}$. Now adjust the slider until joules appears in window I , and kW .hrs. in window J . The left-hand window is required for this example. Ensure that the positioning arrow in the window is correctly aligned. Now scale $L$ reads directly in joules, and scale M directly in kW.hrs., times the appropriate factor, and thus we see that 7.2 joules (scale L ) is equivalent to 2 (on scale M ) $\times 10^{-6}$ (left small conversion window) kW.hrs. But we wish to convert $7.2 \times 10^{7}$ joules, not 7.2 joules, therefore the answer is times the same factor, i.e., $2 \times 10^{-6} \times 10^{7}=2 \times 10^{1}=20 \mathrm{~kW} . \mathrm{hrs}$.

To convert from the units in the lower scale to those in the upper scale, the procedure is reversed, and the same example, $20 \mathrm{~kW} . \mathrm{hrs}$. would be approached thus :-

Convert to the form $2 \times 10^{1}$, and keep a note of the factor $\times 10^{1}$. Now with reference to the upper scale, the lower scale is times the factor $10^{-6}$. Thus the upper scale, relative to the lower, is $\times 10^{6}$. Thus, opposite 2 in the lower scale, we see $7 \cdot 2$ in the upper scale, and thus the answer is $7.2 \times 10^{6+1}=7.2 \times 10^{7}$, or, in the original form, $72 \times 10^{6}$ joules.


Fig. 10: Resonance example taken from the rule.
A method of simplifying this even further has been devised, eliminating thought about the sign of the conversion factor according to the direction of conversion, in the form of the "SIGN" symbols above the conversion factor windows. This indicates that when changing down, that is from the upper units in the window to the lower units, the units are unchanged, i.e. the units being converted to are times the indicated factor. If changing up, however, from the lower window units to the upper, the sign changes, i.e. scale $L$ is $\times 10^{-2}$, where $z$ is the indicated factor. From this it will be seen that $7 \cdot 2$ joules corresponds to $2 \times 10^{-6} \mathrm{~kW} . \mathrm{hrs}$., and $2 \mathrm{~kW} . \mathrm{hrs}$. corresponds to $7 \cdot 2 \times 10^{-(-6)}=7.2 \times 10^{6}$ joules.

If the reader wishes to add any other units conversions to the rule to suit individual needs this is easily achieved, provided that at least one equivalent is known. If the rule is set up to give the required conversion, provided that this particular conversion does not overlap one already shown on the rule, the new position arrow may be marked in the window, and the appropriate units entered together with the conversion factors.

As an example of this, let us say that it was desired to add on the yards-metres conversion. We know that $1 \mathrm{~m} .=1.09$ yds., thus set the 1 of scale $L$ against the 1.09 of scale M. If this is done, it is seen to be too near the Lux-ft. can. conversion, and it is not possible to mark the yards-metres conversion at this point.

The other point is the reciprocal of one of the units however, or more simply, set the 1.09 of scale $L$ against the 1 of scale $M$, and now we have the conversion, and also a blank window on the left, where we may fill in yards in the upper section of the window, and metres in the lower section of the window. Now 10 yards is equivalent to 9.17 metres, therefore no multiplication factor is required for the M scale to be correct, thus put the index 0 in the left-hand window $\left(\times 10^{0}=1\right)$, and by resetting the rule to place the newly-created units conversion in the right-hand window, insert the index $\overline{1}$ in the right-hand conversion factor window. This is so since 1 yard must correspond to the indicated $9 \cdot 17$, but $\times 10^{-1}$ metres. Thus the right-hand window conversion factor will always be one factor of ten lower than the corresponding left-hand window factor.

## RESONANCE

Resonance for an inductance and capacitance in a parallel circuit may be computed from the abac provided on the rule. The full formula for parallel circuit resonance is given as: $f_{\text {res }}=\frac{\sqrt{L / C-R^{2}}}{2 \pi L}$ In radio circuits, however, " $R$ " may nearly always be taken as negligible in comparison with $2 \pi \mathrm{fL}$, and therefore:$C \bumpeq \frac{1}{(2 \pi f)^{2} L}$ and the frequency expression may be simplified to read: $-\mathrm{f}_{\mathrm{res}}=\frac{1}{2 \pi \sqrt{\mathrm{LC}}}$ as in fact shown on the rule. The abac scales are based on this expression, and by relating the log scales by a straight-edge, given two of the three variables, the third may be fixed directly.

Let us consider the following example by calculation, and by evaluation by the rule. A capacitor is measured at 3.76 pF . What inductance is required for the circuit to resonate at $150 \mathrm{Mc} / \mathrm{s}$ ? Also, deduce the capacitor range required, if the above capacitor is a variable, to give the tuning range $100-200 \mathrm{Mc} / \mathrm{s}$ assuming a fixed inductance.

We shall evaluate the first part of this question mathematically, check on the rule, and then complete the question by the rule only. Now, $150 \times 10^{6}=$ $\begin{aligned} & \frac{1}{2 \pi \sqrt{3 \cdot 76 \times 10^{-12} \mathrm{~L}}} \cdot(150)^{2} \times 10^{12}=\frac{1}{4 \pi^{2} \times 3 \cdot 76 \times 10^{-12} \mathrm{~L}} \\ & \therefore \mathrm{~L}=\frac{1}{4 \pi^{2} \times 3.76 \times 10^{-12} \times(150)^{2} \times 10^{12}} \\ & \mathrm{~L}=\frac{1}{4 \pi^{2} \times 3.76 \times 22,500} \\ & \mathrm{~L}=0 \cdot 3 \mu \mathrm{H}\end{aligned}$

To check this on the rule, adjust the slider to expose V.H.F. in the frequency window (A), thus making the resonance panel correspond to Fig. 10. If a ruler is placed to cut the C scale at 3.76 pF , and the f scale at $150 \mathrm{Mc} / \mathrm{s}$, it is also seen to pass through $0.3 \mu \mathrm{H}$ on the L scale, agreeing with the far more complicated method of evaluation shown above. Note that the coloured scale markings on the ABAC represent significant figures only, and the decimal point, or rather the magnitude of the points, is defined by the windows above and below the scales, the windows defining the upper and lower limits of the scales.

To complete the question, refer to Fig. 10. In the figure, the line $A B$ indicates the straight line evaluation in the first part of the question, where point $O$ is the answer to the first part of the question. Since inductance is constant, all other lines drawn on the scales in this question must also pass through point $O$. The frequency range $100-200 \mathrm{Mc} / \mathrm{s}$ is asked for, thus line OC through the red 2 in the f scale, representing $200 \mathrm{Mc} / \mathrm{s}$, and the line $O D$ through the red 1 in the $f$ scale, representing $100 \mathrm{Mc} / \mathrm{s}$, define the limits of capacitance required on the C scale, and this is seen to be, approximately, $2 \cdot 1 \mathrm{pF}$ to 8.2 pF .

## PARALLEL RESISTOR CHART

The red numbers and lines on the chart represent preferred values of resistance which are normally obtainable. The right-hand numbers in black are specific values from 0 to 100. A problem often encountered is when a particular value of resistor is required which is not a preferred value. One way to overcome this problem is to use two other resistors of the appropriate value wired in parallel. The chart works out the required values at a glance without recourse to mathematical problems.
Let us assume that $490 \Omega$ is the required value (see Fig. 11). Firstly locate 49 on the right-hand black scale. On the chart, decimal points are placed by inspection, hence look at 49 for 490 . Now look across the chart, in line with the 49 , until the nearest intersection of coloured lines is seen to the 49 line. Reference to the chart on the rule will confirm that this is the intersection of the lines marked 120 and 82 in the left-hand column, and as shown in the figure. These two values represent the significant figures of the parallel resistors.

From the rule of thumb that when two resistors are in parallel, the combined resistance must be lower than the lowest of these resistors, and also remembering that two resistors of equal value in parallel will give a combined resistance of half their individual value, we can easily estimate the correct values. The reader will also realise that if one resistor is very much larger than the other, it will have little effect, and the combined resistance will be just slightly lower than the lower resistor value. Since we are evaluating for $490 \Omega$, common sense tells us that the two values must be $1.2 \mathrm{k} \Omega$ and $820 \Omega$. As


Fig. 11: Parallel resistors determined for a non-standard resistance. a quick check on this assumption, we could consider the case where the two resistors were both of the lower value, $820 \Omega$, and this would give a combined resistance of $410 \Omega$, too low. Thus, since the other resistor is a fair bit larger than this approximation, we can assume that it would lift the combined resistance to $490 \Omega$. If the value is required reallyaccurately, then multiply out:-
$\mathrm{R}_{\text {tot }}=\frac{820 \times 1,200}{820+1,200}=488 \Omega$. As described last month, we could then rapidly evaluate the percentage difference this is with the tolerance scale, by setting the central line to the required 490, and thus seeing that the chart has given a value better than $\pm 1 \%$.

In the practical case, do not overlook the actual resistor tolerances that will be used. Thus the chart
rapidly evaluates the resistance values, and the $L$ and $M$ scales provide the means of evaluating the check shown above accurately, having worked out that $820+1,200=$ 2,020 . To do this, divide 820 by 2,020 , then multiply the answer by 1,200 , to get the answer 488.

As indicated, the chart can also be used forseries capacitors, however it is really designed for parallel resistors, therefore the preferred resistor values are not really suit-


Fig. 12: Interpreting the resistor colour code. able for capacitors.

For capacitors it will serve as an approximate guide, but since capacitor tolerance is usually exceedingly wide, particularly in electrolytics, it can serve a purpose for capacitors as well.

## RESISTOR SELECTION

The two upper tables on the rule are designed to ease selection of resistors, the left-hand table gives the resistor colour code, and the right-hand table gives the preferred resistance values. Fig. 12 indicates how the coloured bands on the resistor should be interpreted. It should be noted that the bands start from one end of the resistor, leaving the far end of the resistor blank, and when reading the colour code, always start with the colour next to the nearest end of the resistor, and then work along taking colours in turn. The first colour indicates the first digit, and the second colour the second digit of the resistance value. The third colour indicates the number of noughts which should be placed after the previous two digits, or the factor " $n$ "' if the previous two digits are multiplied by $10^{\mathrm{n}}$. The last band, if there is one, indicates the resistance tolerance allowed. If there is no fourth band a tolerance of $\pm 20 \%$ is assumed.

As an example, take the following four colours, reading in from the end:-red, violet, orange, gold. Obtain the first digit by looking for red in the top lefthand table. This is seen to be 2 . The second digit, from the same table, is seen to be 7 , the code number for violet. We must then add on to this three noughts, due to the orange band, and the gold band at the end tells us the resistor's $\pm 5 \%$ tolerance. Thus the resistance value is nominally $27 \mathrm{k} \Omega$, and it is read as $27 \times 10^{3}$ from the code, or 27 with 3 zeros after this giving 27,000 2 .
Another example:-green, blue, black. This represents $56 \times 10^{\circ}$ i.e. $56 \Omega$.

A final example, the resistance $3 \Omega$ would be coded $03 \Omega$, i.e., black, orange, black.
The top right-hand table indicates the first two digits of resistance values that are usually obtainable. Thus, if a calculation calls for a resistance of say $5 \cdot 9 \mathrm{k} \Omega$, reference to this table tells us that the nearest preferred value to this will be $5.6 \mathrm{k} \Omega$.

Next month's issue will deal with the scales on the other side of the rule.

## To be continued

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# THE <br>  <br>  <br>  <br>  <br> <br> J. THORNTON-LAWRENGE GW3JGA 

 <br> <br> J. THORNTON-LAWRENGE GW3JGA}

FOLLOWING the formation of a local Amateur Radio Club, many junior members expressed the desire to purchase or build a receiver but either lacked the finances or felt that building a receiver was beyond their capabilities. With these and other requirements in mind, the Clubman MK I receiver was designed to provide:

1 Satisfactory reception of a.m. signals on Top Band ( 160 m ), Trawler Band and the 80 metre amateur band.

2 Easy construction from readily available parts.
3 Minimum cost.
4 Pleasing appearance.
5 Facility for adding extra stages and refinements at a later date.

## Basic Circuit

The basic circuit is that of a 5 -stage superhet receiver, as shown in Fig. 1. In order to economise on transistors and components, a reflex circuit is employed as shown in Fig. 2. In this circuit the i.f. amplifier transistor is also used as an a.f. amplifier. Only one double-tuned i.f. transformer is used providing a reasonable degree of selectivity which is in keeping with the general performance of the receiver. The complete circuit is shown in Fig. 3.

## Frequency Changer Stage

Incoming signals pass through the r.f. gain control VRI to the coupling coil LI. VRI is connected so as to provide to LI an impedance which varies as little as possible with the setting of the control. L2 is the tuning coil which, with VCl and TCl , is tuned to incoming signal. L3 is the coupling coil to Trl base. Trl and its associated components comprise a self-oscillating mixer stage which follows standard practice. The local oscillator frequency is determined primarily by L6 and VC2. TC2 is the oscillator trimmer and C 4 is the padding capacitor. The feedback required for oscillation is provided by the collector coupling winding L4 and the emitter coupling winding L5. D.C. biasing for Trl base is provided by the potential divider R 1 and R 2 , while R4 is the emitter stabilising resistor. Decoupling of the various circuits is provided by $\mathrm{C} 1, \mathrm{C} 2$, and C3. The purpose and value of R3 is discussed later.

## The I.F. and Detector Stages

Signal, local oscillator and resultant sum and difference (i.f.) frequencies appear at the collector of $\operatorname{Tr} 1$. Thè i.f. frequency only is accepted by the i.f. transformer i.f.t.l., the primary and secondary of which are tuned to 470 $\mathrm{kc} / \mathrm{s}$. I.F. signals at this frequency are passed to the base of Tr2. Amplified i.f. signals at $\operatorname{Tr} 2$ collector are developed across the choke L7 and passed by C7 to the demodulator.

The demodulator consists of a voltage doubling rectifier circuit comprising D1 and D2, the signal load resistor is R7 and decoupling is provided by C6. The audio frequency signal is developed across R7 and is returned to the base of Tr 2 by the coupling capacitor C8.
$\square$

* STEP BY STEP GENERAL RECEIVER


Fig. 3: Circuit diagram of the "CLUBMAN" MK I receiver.
components list

Resistors:
All 10\% watt Carbon.

| R1 | $10 \mathrm{k} \Omega$ | R5 | $1 \cdot 2 \mathrm{k} \Omega$ | R9 | $1.5 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R2 | $2 \cdot 7 \mathrm{k} \Omega$ | R6 | $8 \cdot 2 \mathrm{k} \Omega$ | R10 | $470 \Omega$ |
| R3 | see text | R7 | $5.6 \mathrm{k} \Omega$ | VR1 | $5 \mathrm{k} \Omega$ |
| R4 | $1 \mathrm{k} \Omega$ | R8 | $100 \mathrm{k} \Omega$ | VR2 | $250 \Omega$ |

Capacitors:
C1 $\quad 0.01 \mu \mathrm{~F} 20 \mathrm{~V}$ disc ceramic
C2 $\quad 0.002 \mu \mathrm{FHi}$ K ceramic
C3 $\quad 0.01 \mu \mathrm{~F} 20 \mathrm{~V}$ disc ceramic
C4 1100 pF (1000 pF and 100pF in parallel) Mica
C5 $\quad 0.01 \mu \mathrm{~F} 20 \mathrm{~V}$ disc ceramic
C6 $\quad 0.01 \mu \mathrm{~F} 20 \mathrm{~V}$ disc ceramic
C7 $\quad 0.001 \mu \mathrm{FHi} \mathrm{K}$
C8 $8_{\mu} \mathrm{F} 15 \mathrm{~V}$ electrolytic
C9 $\quad 25 \mu \mathrm{~F} 15 \mathrm{~V}$ electrolytic
C10 $25 \mu \mathrm{~F} 15 \mathrm{~V}$ electrolytic
TC1 3-30pF concentric trimmers

TC2 $\quad 3-30 \mathrm{pF}$ concentric trimmers
VC1/VC2 365pF 2 gang Jackson type 02
Semiconductors:
TR1 OC170 Mullard
TR2 OC45 Muliard
TR3 OC71 or OC81 Mullard
D1 OA81 Mullard
D2 OA81 Mullard
Inductors:
$\left.\begin{array}{ll}\text { L1/L2/L3 } & 3 T \text { blue } \\ \text { L4/L5/L6 } & 3 T \text { red }\end{array}\right\}$ Denco
$17 \quad 2.5 \mathrm{mH}$ RFC type CH 1 Repanco
IFT1 $470 \mathrm{kc} / \mathrm{s}$ type T41/IE Weymouth
Miscellaneous:
Open jack socket, miniature slide switch, slow motion drive, knobs, terminals, 2 B9A valveholders, solder tags, battery clips, nuts, bolts and screws, materials for cabinet.

## A.F. Amplifier and Output Stage

Tr2 now performs as an a.f. amplifier, the amplified signal appears across the collector load R6 and is passed directly to the base of $\mathrm{Tr} 3 . \operatorname{Tr} 3$ is the a.f. output stage and the collector and load resistor R9 are coupled to the headphone jack by C10. D.C. biasing of Tr 2 and Tr 3 is rather unusual and is shown in Fig. 4. The coupling between Tr 2 and $\operatorname{Tr} 3$ is seen to be direct. The bias current for the base of Tr 2 is obtained from Tr 3 emitter. This means that there is a complete d.c. feedback loop. Starting at the base of Tr 2 , signals and d.c. level changes appear amplified and of opposite polarity at the collector and pass on to the base of Tr 3 . Corresponding d.c. changes appear at Tr 3 emitter and this is fed back to $\operatorname{Tr} 2$ base. As the changes fed back to $\operatorname{Tr} 2$ base are opposite to those originating there, the circuit is kept stable. A.F. signals existing at Tr 3 emitter find an easy path to earth via the decoupling capacitor C9, and are not fed back to the base of Tr2. Strongly amplified a.f. signals appear at Tr 3 collector.

For simplicity the a.f. gain control was omitted from the circuit in Fig. 4 and is now shown in its correct position in Fig. 5. As the a.f. gain control VR2 is increased in resistance (anticlockwise rotation) the a.f. currents flowing through C9 produce an a.f. voltage across VR2 and R10. This a.f. voltage provides negative series current feedback to Tr 3 and


Fig. 4 (upper): Biasing circuit Tr2, Tr3.
Fig. 5 (lower): Biasing circuit Tr2, Tr3, with a.f. gain control.
negative shunt current feedback via R7 and R8 to Tr 2 , thus reducing the a.f. gain of both stages. The feedback provides a variation of gain of about 100 to 1 , but will not reduce the output to zero.


Photograph shows internal view of the basic receiver.

## General Construction

The receiver is built on a simple aluminium chassis with front and rear panels, giving excellent accessibility for construction and adjustment. A two-part wrap-around cover provides neat appearance with easy fixing. Drawings of the chassis, covers and other items are given in Fig. 6.
If you have the usual metalworking tools and have some experience of metalwork, the chassis and panels should present no problems. If you are new to metalwork the following hints may help you.

1-The aluminium for the panels, chassis and brackets should be cut by a guillotine or metal saw, tin shears or snips leave a poor edge to the metal which is difficult to correct. A supplier of sheet metal will probably cut the metal to the required size for you. If you have to cut the metal with a saw, be sure to file the edges level and smooth afterwards.
2-Mark out centre lines on the chassis and panels as all dimensions are given from these lines. Mark out all the other dimensions from the centre lines, double check dimensions and use a small centre punch to mark the centres of all holes. Mark out the brackets etc., as shown in Fig. 6. The holes in the chassis, panels and brackets may now be drilled. It is advisable to run a pilot drill of $\frac{1}{8} \mathrm{in}$. diameter through the large holes first before drilling to the correct size. Holes over $\frac{3}{8}$ in. diameter should be made using a chassis cutter, the Q-Max type is ideal. The rectangular holes for the slide switches may be made by drilling a couple of holes within the markedout area and then opening up to size with a small flat or three-cornered file.


Fig. 6: Details of the main chassis drilling, front and rear panels, top and bottom covers, capacitor brackets, side trims and battery clip.

3-The bending of the chassis and covers is tackled next. If you do not have access to a bending machine, or suitable pieces of angle iron which may be clamped in a vice, an easy way of bending the chassis is as follows. Cut two pieces of $\frac{3}{4}$ in. thick blockboard, size $8 \frac{7}{8} \times 6$ in., make sure all the corners are square and the edges parallel. Sandwich the chassis between them so that the blockboard fits the $8 \frac{1}{8} \mathrm{x}$ 6in. area which will be the inside dimensions of the chassis. Screw the two pieces of blockboard together through two or more of the holes already drilled in the chassis. The whole assembly is now clamped in a vice and each edge of the chassis is gently tapped over, using a block of hardwood and a light hammer. Do not rush this operation as it is difficult to straighten any irregularities that may appear in the edge. Make sure the edges are folded in the correct direction. The covers and brackets may be made in the same manner as the chassis but without drilling holes.
4-The panels now require fixing to the chassis, and it will be seen that no holes exist on the edges of the chassis for this purpose, this is intentional. Cut four small blocks of wood having a distance of exactly $\frac{3}{4} \mathrm{i}$. between two opposite faces, for use as jig blocks. Turn the chassis folded-edge upwards and stand this on the four blocks so that the chassis is raised exactly $\frac{3}{3}$ in. Take the front panel and rear panel and stand these against the respective edges of the chassis as shown in Fig. 6. Make sure everything is square and mark through the panel fixing hole on to the chassis edge. Centre punch the centre of the markings and drill $\frac{1}{8} \mathrm{in}$. diameter holes. The panels may now be bolted to the chassis using 6BA bolts and nuts. The jig blocks should again be used to ensure the complete unit is tightened up squarely.


Fig. 7: The receiver dial-shown to scale.
5-The top and bottom covers are now placed in position. The rear panel should be set in about $\frac{1}{8}$ in. and the front panel about $\frac{1}{4}$ in.
6-To present a good appearance, the front and rear panels are covered with white Fablon or Contact plastic material.
7-The dial is made of an aluminium disc cut to shape and a calibrated paper disc attached. (See Fig. 7.)

To be continued

## THE

MW

## COLUMN



ONCE again we bring you some notes on the Medium Wave DX situation. The most interesting items to report are of West Coast North American reception. It must be pointed out that with the approach of the sunspot maximum these are liable to be more difficult to $\log$.

On August 28th KOMO (1000) was heard in Southport at 0430 GMT and in Bristol KOMO again plus KING (1090) (both in Seattle, Washington) on October 22nd-KOMO at 0520 and KING over WBAL, Baltimore, Maryland.

Another interesting catch from Charles Molloy in Southport, who with Pat Dobbs in Bristol are the only ones who have reported West Coast reception recently, is CBW (990) in Winnipeg on September 11th at 0515 with close down announcements followed by their all night programme. Of course the regular East Coast stations in Canada and the USA continue to be logged widely.

Looking to South America we have a report of a real rarity in the UK-CP4 (1020) Emisora del Estado, La Paz, Bolivia, which was heard in June and July by AI Slater in Southwick, Sussex. This was verified -sign off at 0400 . Other South Americans that you can look for are YVQQ (770) R. Puerto la Cruz, this is regular-also YVLH (660) $R$. Giradot, Maracay. HJED (820) La Voz de Cauca, Cali, and HJCT (1190) La Voz de la Costa, Baranquilla and there are Brazilians to be heard when conditions permit from midnight onwards. PRE8 (980) R. Nacional, Rio, PRB9 (1000) R. Pan-Americana, Sao Paulo, PRG9 (1100) R. Nacional, Sao Paulo. PRE3 (1180) R. Globo, Rio and PRG3 (1208) R.' Tupi. Rio. Also we must not forget our old friend I.RI (1070) R. El Mundo, Buenos Aires.

Now to Asia-under favourable conditions around 0030 to 0310 one may $\log$ All India Radio. We have reports of Ahmadabad (850). Delhi (1070), and you may look for Sangli (1250). Afternoon reception of the latter was known, but we feel it to be very difficult now. Others are Hopei (770) around 2220, Urumchi (1525) in Russian from around 1800 and Taiwan (750) from about 2100 .

On the African continent there are some excellent potential catches. Fairly often heard is Sao Tome (759) around 2000, also the high power R. Biafra, Enugu (620) at 0430 and R. Lourenco Marques (917) at 0100 . A good source of DX is South Africa and over the past year we have had reports of the S.A.B.C. Springbok Commercial Service, which is an All Night Service. As far as we know the earliest hour for this is about 0130 and the following channels should be carefully watched: 1286-in Johannesburg, East Rand, 1268 in Pretoria and 782 in Bloemfontein-if Deutschlandsender is off the air.

We hope that these notes are of interest. They have been compiled at very short notice upon an urgent request to help out due to the indisposition of Al Woodland.

KEN BROWNLESS


THE growing popularity of transistor portable receivers in recent years has resulted in large numbers of mains table receivers being discarded long before their useful life was over. Many of these sets have excellent short wave bands, others have push pull output and good quality speakers. Many dealers, having taken this type of receiver in part exchange against sales, are glad to get rid of them for a nominal payment.

Many of these receivers have only rectifier and smoothing faults but it is surprising how many different types of bases there are. The amateur has only a limited selection of valve rectifiers in his junk box. An attempt to find an interchangeable rectifier which could be used with base adaptors to test any set resulted in this universal rectifier.


Fig. 1: Full wave rectifier using two silicon diodes.
The problem of catering for different heater voltages has been overcome by the use of silicon diodes. Wiring the diodes and limiting components to a B9A base enables direct replacement of EZ80 and other current rectifiers. Base adaptors, as in Fig. 5 enable the basic unit to be adapted to International and Mazda octal, B7G, B8A and other


Fig. 2: Half wave rectifier circuits (left) and (right) full wave circuits. The $0.005 \mu \mathrm{~F}$ capacitors should be 1000 V wkg.
type bases. Most a.c. receivers using full wave rectifiers have heater supplies of 5 or 6 volts. Removal of the rectifier does not interfere with the heater supplies of the other valves in the receiver. A defective rectifier can. therefore, be removed and a diode replacement unit substituted.

Figure I shows the component parts of a full wave universal rectifier, namely two B100 silicon diodes, two $12 \Omega 6$ watt resistors, two $0.005 \mu \mathrm{~F} 1 \mathrm{kV}$ wkg., capacitors wired to a B9A pin base. Fig. 2 shows the comparative valve and diode circuits for both full wave and half wave rectifiers.

Many a.c./d.c. receivers are still in use despite the ever-growing popularity of the transsistor home radio. Using high voltage filaments for output and rectifier valves they make use of half wave rectification for h.t. supplies. Typical of this design are the Ultra U930 with UL41 output valve and UY41 rectifier, the Philco Model 104 with UL84 and UY85 rectifier and the Pilot Maestro with 35L6 and 35Z4 valves.

A common fault in a.c./d.c. rectifiers is a break in the cathode lead leaving the heater intact. Since half wave rectification is used only one silicon diode and associated components is required to replace the rectifier valve. In such a case the parts can be wired across the valve holder base as shown in Fig. 3.

Where, however, the heater is open circuit, it is necessary to bridge the gap in the heater circuit, in order to restore the current to the remaining valves in the set. The resistance value of the "bridge" must be chosen so that approximately the same voltage will be dropped across it as was developed across the rectifier valve filament.

Reference to a valve data booklet will give details of rectifier heater voltages and currents. The Ultra radio, Model U390, referred to above makes use of a UY41 rectifier. This is a valve with a 31 V 0.1 A heater and a B8A base. The value of the resistor required to replace the filament can be obtained from Ohm's Law-Resistor $\mathrm{R}=\mathrm{E} / \mathrm{I}$. The nearest resistor value would be $300 \Omega$ ( 5 watt rating) and this would be wired across pins 1 and 8 of the rectifier base and the diode, resistor and capacitor connected as shown in Fig. 4(a).

Fig. 3: Replacement silicon rectifier fon international octal base) for 3524 where filament is still intact.


The Philco radio uses a UY85 rectifier valve with a 38 volt heater at $0 \cdot 1 \mathrm{~A}$. Again from Ohm's Law the heater "bridge" resistor can be ascertained. The nearest commercial value would be $400 \Omega 5 \mathrm{~W}$. The valve has a B9A base and the resistor would be joined across pins 4 and 5. Fig. 4(b) shows the diode wiring.

For the Pilot Maestro which has a 35 volt rectifier a bridge resistor of $200 \Omega 6 \mathrm{~W}$ will suffice (see Fig. 4(c).

When a valve rectifier has been proved to be defective, the glass envelope and valve structure may


Fig. 4: (a) Complete rewire to replace UY41 with o/c filament; (b) ditto for UY85; (c) used where 3524 filament is o/c (also add Fig 3 details).
be removed, and the components wired on top of the base if it is thought undesirable to wire them under the chassis. This allows ventilation of the bridge resistor which will run warm. When wiring up diodes the full length of the wires should be used. Sleeve them and sheath the outer case of the diodes in plastic tape. If the case should contact the chassis the output will be short circuited.

Before fitting a replacement rectifier, the cause of failure must be ascertained; otherwise the diodes may in their turn be damaged. A short circuit in the reservoir capacitor is a typical cause of rectifier failure.

Referring back to Fig. 2 silicon diodes have a lower forward resistance than valve rectifiers. Replacement of a valve with a diode would result in a higher voltage across the reservoir capacitor.


Since there is no heater warm and smoothing up period the full voltage appears across the reservoir capacitors immediately the receiver is switched on. This could cause damage. To reduce these dangers a series resistor of $12 \Omega 6 \mathrm{~W}$ is connected to each diode. The $0.005 \mu \mathrm{~F}$ capacitors are connected across the diodes to protect them from voltage surges. Universal silicon diode rectifiers have given a new

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## Direct Reading Audio Oscillator and Frequency Meter

This is a compact dual-purpose instrument covering $20 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}$ in four ranges. Oscillator outputs are at $10 \mathrm{mV}, 100 \mathrm{mV}, 1000 \mathrm{mV}$ plus one which is continuously variable, and distortion is only $0.5 \%(100 \mathrm{c} / \mathrm{s}$ to $50 \mathrm{kc} / \mathrm{s})$, or $1 \%(40 \mathrm{c} / \mathrm{s}$ to $100 \mathrm{kc} / \mathrm{s})$. The frequency meter is accurate to $5 \%$. Monitor facilities are provided.

Full constructional details are given of this design, which uses 8 transistors and 5 diodes, together with helpful notes on calibration.

## Reclaiming Faulty Transistors

Faulty transistors are usually thrown away. But are they always really useless? Only one junction may be damaged and many such components can be reclaimed for use as diodes or zeners. This article shows how to build a simple test unit to check whether damaged transistors can be utilised for other purposes.

## Improving the PCR

How to improve the performance of the well-known PCR, PCR2 and PCR3 communications receivers by adding a transistor b.f.o. stage and incorporating variable selectivity.

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## 

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$\begin{aligned} & \text { List price } \\ & \text { was } 5 \text { gns. }\end{aligned} \quad S A L E \quad P R / C E \quad 35 /-\quad$ P.\& P. $2 /-8$ DUALIMPEDANCE VERSION OF ABOVE-for 600 and 50 ks ת $\begin{aligned} & \text { List price } \\ & \text { was } 6 \text { gns. }\end{aligned} \quad S A L E P R / C E 42 /-\quad$ P.\& P. $2 /$


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High quality 14 watt power amplifier with separate volume controls on each input. also bass and treble controls. Inputs $1.5 \mathrm{mV}: 2-40 \mathrm{mV}$. Output impedance 3 or EF86 EF86. ECC83 and EZ881. Frequency Response Hi Fi enthusiast, or as guitar amp. Gold hammer finish with distinctive perspex ront panel
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## ASIA

Afghanistan: Radio Afghamistan (Ansari Watt. Kabul) using the new outlet of 15,435 from 1100-1200 for a combined Pushta/Dari programme.

China: Radio Peking (Fu Hsin Men, Peking) has English to Europe at 2030-2125 and 2130-2225 on approximately 9,890 and also in the 25 and 42 metre bands. English for Africa is at 1930-2025 and 2030 2125 on 9,450.

Indonesia: Radio Republik Indonesia (P.O. Box 157, Djakarta) has left 9,865 for its Arabic, French, Indonesian and English programmes at 1615-2000 to Europe. Listed new frequency, on which the station has not so far been reported is 15,200 . However part of the Arabic programme at 1615 was heard on 9,588 before being blotted out by interference.

Japan: N.H.K. (Tok vo) latest schedule for the general service is: on $15,105 / 15,195 / 15,3000100-0130$, 0200-$0230,0300-0330,0400-0430,0500-0530$; on $9,505 /$ 15,195/15,300 0600-0630, 0700-0730, 0800-0830, 09000930; on 9,505/11,815/15,300 1000-1130; on 9,505 $9,560 / 11,815,1200-1230,1300-1330,1400-1530,1600$ $1630,1700-1730,1800-1830$; on $9,560 / 11,815 / 15,105$ $1900-1930,2000-2030,2100-2130$; on $9,700 / 15,195 /$ 17,785 2200-2230, 2300-0030.

Lebanon: R. Lebanon (Ministry of Information, Beirut) now using 15,180 at $1830-2030$ in English, Arabic and French to Africa.

## AUSTRALASIA

Australia: Radio Australia (P.O. Box 428G, G.P.O. Melbourne) now uses 11,810 from 1800-2115 in English. The 2230-0030 Indonesia programme now goes out over $21,680 / 15,330$. The UK English transmission is now at 0815-0915 on 9,560/11,710.

## NORTH AMERICA

U.S.A.: Radio New York Worldwide (485 Madison Avenue, New York, NY, 10022) now reported to have the following frequency usage to Europe. On 17,730 1600-1945; 21,530 1600-1700; 11,970 2000-2200; $21,5201700-1945 ; 17,7601945-2200 ; 15,4401600-2200$. A press release from the station says however that at 1700 it is using $17,760 / 17,845 / 21,465 / 21,530$.

## CENTRAL AMERICA

Cuba: Radio Habana Cuba (Apartado Postal 7026, Habana) has made the following changes: Spanish to Mediterrancan: 1630-1730, 0830-0930 11,735; 18552030 17,855/17,885. Arabic to Mediterranean 0800 0830, 1000-1030 11,735; 1810-1855, 2030-211017,855/ 17,885; English for the Americas 2050-2150 15,230. French to Mediterranean 0730-0800, 0930-1000 11,735; 1700-1810, 2110-2140 17,855/17,885.

Netherlands Antilles: Trans World Radio (Bonaire) reported on 15,255 to Europe at 2000-2130.

Windward Islands: Windward Islands Broadcasting Service (St. George's, Grenada) noted at 2015-2130 on 21,690

## SOUTH AMERICA

Chile: Radio Nuevo Mundo (Casilla 9255, Santiago) reported on the new outlet of 17,865 at 24000200 .

## EUROPE

Albania: Radio Tirana (Rue Ismail Quemal, Tirana) reported using new outlets $6,200 / 9,510$ for the $2200-$ 2230 English transmission to Europe.

Belgium: Radiodiffusion-Television Belge (18 Place Eugene Flajey, Brussels 5) transmits as follows at 1830-2100 over 6,010/11,615/17,860; 2115-2200 6,010/ 9,615/15,335; 2315-0100 6,010/9,615/11,895.

Denmark: Radio Denmark (Radio House, Rosenorasalle 22, Copenhagen 5) has retimed its South American service. New times arc Danısh 2000-2045 and Spanish 2045-2115 over 15,165.

German Federal Republic: Deutsche Welle (5 Koln 1, Postfach 344) has made the following frequency changes: Indonesian 1210-1320 15,300/17,830/21,650; English 0300-0340 9,640/11,945; 1550-1620 15,275/ 17,875. Spanish 0555-0635 9,545/11,945; 2240-2350 and Portuguese 2140-2240 9,545/11,795/15,435. Turkish 0610-0640 9,610/11,795.

German Democratic Republic: Radio Berlin International (116 Berlin Nalepastrasse 18-50) now transmits in English as follows at 1730, 2015*, 2200**, 2300** on 6,080/6,115/7,185/7,300/9,730 (also on *1.511; **1,430); 0100, 0230 on 9,730/11,890; 0345, 0445 9,560/9,650; $0345,11,795 ; 1215,160021,600 ; 061511,795 ; 1315$ 21,$655 ; 191517,785 ; 160017,805 ; 064517,700 ; 1200$, 131521,$610 ; 1415,15,125$.
Great Britain: $B B C$ (C EXB, Bush House, London, WC2) noted on 25,720 with Hindu 1500-1545; Urdu 1415-1500; Chinese 1200-1300; Indonesian 1030-1100; Japanese 1100-1130; Vietnamese 1130-1200.

Manx Radio (Loch Promenade, Douglas, Isle of Man) transmits as follows: 0600-0630 and 1730-1900, 1,594; 0630-1730 1,295. There is also a religious programme at 1015-1100 on 1,594.

Greece: Radio Athens (Mourouzi Street 16, Athens 138) noted with English and French during the 22002230 Greek transmission on $11,720 / 15,345$.

Hungary: Radio Budapest (Brody Sandor-S.U. 5-7, Budapest VIII) has English as follows: To Europe $2130-2230$ on 11,910/9,833/7,220/6,234 and 2330-2400 on 6,234/3,995/539. To Far East 0800-0815 Wednesday and 1015-1030 Friday $11,910 / 15,160 / 17,890$. To North America $0030-0130$ 6,234/7,220/9,833/11 910/15,160; $0300-0400$ and 0430 and $05006,2347,220 / 9,833 / 11,910$.

Thanks for help go this month to D. O. French, Roy Patrick, A. E. Roxburgh, M. A. Golics, Swiss Shortwave Service, Radio New York Worldwide and the International Short Wave Club.

THINGS are really hotting up now and if they get any hotter the shack at 3JDG will be growing orchids. Ten metres has burst its banks at times although still rather up and down. Twenty and fifteen have really been wide open and even noisy seven megs has reared its DX head. David Smith (Lancs.), has sent in a $\log$ for $1.8 \mathrm{Mc} / \mathrm{s}$ which shows that it is far from being just a " $G$ only" band. Incidentally W1BB has now worked 97 different countries on 160 metres, anyone beat that?

Best times to listen on the bands is always a good thing to know. At the time of writing topband is interesting after $10 \mathrm{p} . \mathrm{m}$., while twenty and fifteen seem to be at their best from $10 \mathrm{a} . \mathrm{m}$. to $4 \mathrm{p} . \mathrm{m}$. Ten is a daytime band too from 10 a.m. to 4 p.m. but has stayed open till 9 p.m. on occasions.

Many thanks to all those who sent in logs this month. Some were really fine business so let's take a peep at the postbag and see.

## L.F.

Brave men still shake at the knees and keen types hide in dark corners, that is if you happen to mention a listen on the l.f. bands. Only two souls came through unscathed this month each with a bag of goodies.
D. Smith (Lancs.), RX6ON, 35 ft . end fed scooped this lot on topband c.w.-OK2BOB, OK2BKH, OK2AKU, OL2AIO, OK 3 KAS , and from the Channel Islands-GC3ODE.
P. Baker (S. Wales), HE30, 150 ft . end fed listened on 80 s.s.b. and got-CN8AW, FP8CA, VE1UA, VO1AW, VS6FS, VS9MB, W3BMS, ZC4MO, then a good opening to the Pacific-ZL2FQ, ZL2KT, ZL2BCG, ZL2RJ, ZL4KE, ZL4LM. On 40 (I'm shaking already), Paul raised-CN8AW, CN8BV, EA6BC KIDRI, K8AWS, OA8NAM, PZ1CF, SV $\varnothing W V$, UJ8GW, VK2AVA, W3BMS, ZB2AP, ZC4AK, ZL2BDA.

## TEN METRES

The r.f. coming in on this band is quite devastating at times. Really worth a listen these days too so spin the dial round to $28 \mathrm{Mc} / \mathrm{s}$ and leave it there ready for the next session.
G. Coomber (Essex), HRO-MX, 15 metre dipole at 16 ft . hooked these on s.s.b.-W1HRN, W2QCR, W3GHF, W4MMD, W5TBH, W8OCT, W9LKJ, W $\varnothing$ AXE, $5 \mathrm{~N} 2 \mathrm{AAF}, 9 \mathrm{H} 1 \mathrm{~K}$.
P. Knowles (Cheshire), CR45 plus PR30, heard these, which is pretty good for a t.r.f.-DJ9HI, EA6BJ, IIKTS, K1FWK, UB5GTW, UB5SLF, VE3CTI, W1TAT, W2EIR, W3TUA, W4CNN, W8YCI, W9HLY, YO2QCA, ZE8JM, ZS1JH all on a.m. too.
L. Rowland (Cheshire), lurked with intent on $28 \mathrm{Mc} / \mathrm{s}$. Using a Trio $9 \mathrm{R}-59$ and a 150 ft . long wire as bait he captured-CE3TS, CN8PR, CR6IV, CR7FM, CX9PP, EA6BJ, EL2AI, EL2S, EP2BQ, ISIIUA, IT1BXX, JA1AG, JA1FGE, JA2GDF, K1YZW, K2QIL, K4KJN, K5DFZ, K6CCY, K6HAD, K8EQH, KøRCH, KG6ALY, KP4BJD, KR6TAB, KV4AD, KV4BW, KZ5MB, OD5BZ,

OX3BS, PY2DSE, PZ1BX, SV $\varnothing W M, ~ U A 3 A V V$, UF6ACR, VE3PWA, VE4GC, VE5LL, VK6BE, VK6CF, VK6XX, VK9DR, VK9DJ, VS6DO, VU2MWP, W2BZ, W3AEC, W4YYY, W5IOU, W6EPZ, W6VIO, WA6HXW, WB6RJG, W7PEY, W8AUE, W9RYX, W $\varnothing$ QDW, XE2IW, YVILA, YV5ANE, ZC4MO, ZE1AA, ZSIFH, ZS5DG (No relation), ZS6AOW, 3V8BZ, 4X4BL, 5N2AAF, 5R8AS, 9J2WR, 9LiGQ, 9LiJJ. All on s.s.b. (My kingdom for a b.f.o.).
II. Davies (Essex), homebrew double superhet transistorised (well done, Sir), 10 metre dipole, logged-OD5BZ, OX3BX, PJ2CQK, VE3BRC, YV6BV, 5N2AAF, 9H1AG, $9 \mathrm{H} 1 \mathrm{~K}, 9 \mathrm{G} 2 \mathrm{OK}$.

## TWENTY/FIFTEEN

D. Henbry (Sussex), HA500, 20 metre dipole, shows what's about on $21 \mathrm{Mc} / \mathrm{s}$ s.s.b.-CE3PY, CR6II, CR7DS, EL8H, HK3BLD, HK5ASA, HL9KB, HR 1 KAS , KV4CF/M, KZ5SF, LU8DB, LU8DKA, OA4JR, OA8V, TG7AV, VP2GBC, VP8JD, VS6BE, VS6FZ, VU2BK, W7MX, WA7CDM, WA7EVO, YN4WD, ZL1ABO, ZLIJN, ZP5JB, 601 GB , 9X5GC.
S. Herod (Suffolk), Two commercial sets, one as a b.f.o. On $21 \mathrm{Mc} / \mathrm{s}$ s.s.b. CE $\varnothing \mathrm{AE}, \mathrm{CN} 8 \mathrm{FV}, \mathrm{CR} 61 \mathrm{~A}$, CR7FG, FL8HM, HI8XBA, HRIKAS, JA1BZ, JA2JAA, JA3FSN, JA4COS, JA5CEU, JA $\varnothing B Q F$, K7NEQ, K3USL/AM $(23,000 \mathrm{ft}$. up off Sardinia), KG6AAY, OD5CN, VS9MB, W7LVI, ZE6JL, ZL2JSC, ZLIPZ, 5Z4IW, 7Q7EC, 9Q5AF, 9U5CM.
R. Dinming (Scotland), HA350, Joystick, loggedCR4CB, DUIFC, DU1FB, HIlMN, KL7SAY, KZ5WL, LUIDAB, JA $\varnothing$ PE, VK1GD, VK2AGW, VK3AMK, VK6ALY, VQ9CT, YAIHD, YSiJSL, ZLIIH, ZS6BFY, 9H1R. All $21 \mathrm{Mc} / \mathrm{s}$ s.s.b.
L. Bousher (Wales), R1155, 50 ft . end fed raised these on phone on twenty-CE6EQ, EL3C, H18LAL, HC6GM, HK3AUE, HK4AZX, JA1PIB, KP4AKB, KZ5NH, KZ5RJ, OA3CL, OX4AA, OY1WP, PX1NV, PYICLI, PY7GV, PZ1BW, TG9AD, UP2NV, VE3BZU, VK4PU, VO1HQ, VP8JB, YSIRCP, YV5BE, ZEICGF, ZS9H, 3A2DW, 5Z4IW, 6Y5GG, 8RIS, 9G1BS, 9Y4VT.
J. Edwards (S.E.20), SX24, 80ft. long wire switched in the b.f.o. for these on s.s.b. CR4BC, EP2BQ, ET3USA, HI8XMY, HK3AUE, JT1BB, KP4AKB, LU8DDI, PYITX, TI2ALG, UG6AW, VK2AVG, VK7RX, VP8HZ, VP8IU.
P. Leybourne (Glos.), HRO, 60ft. end fed listened from 0500 to 0700 and heard-EP9EP, HB9AA, HP1JC, KP4AST. PY2SO. VE3EWY, VK2WD, VOIFB, WB2RRR, W6ZKM, W9TFU, YV1EL, ZL1AIX, ZL2AAG, ZL2ANR, ZL2AZZ, ZL4GH, ZL4KL, ZL5KL., ZM7WMM.

## CONTESTS

Many a tear will be shed in the Christmas pud this month. Only one contest in my diary-3rd December $70 \mathrm{Mc} / \mathrm{s}$ c.w. contest.

Very best wishes for Christmas and the New Year to all r.f. lovers. Don't forget all those wonderful nets that go on on Christmas Day morning. CUAGN in 1968.

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Total building costs


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Total building costs


MELODY MAKER 6
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PART 6

## The R1155

The R1155 has always been popular. It was first manufactured for the R.A.F. in large numbers during the last war, and was used by Bomber Command. There are several versions but as the differences are minor they will all be dealt with in this section. The frequency range of the R1155 and R1155B (the most common versions) is as follows:-
$18.15-7.5 \mathrm{Mc} / \mathrm{s} ; \quad 7.5-3.0 \mathrm{Mc} / \mathrm{s} ; \quad 1,500-600 \mathrm{kc} / \mathrm{s} ;$ $500-200 \mathrm{kc} / \mathrm{s} ; 200-75 \mathrm{kc} / \mathrm{s}$.

The R1155L and the R 1155 N versions have the following frequency range:-
$18.0-7.5 \mathrm{Mc} / \mathrm{s} ; 7.5-3.0 \mathrm{Mc} / \mathrm{s} ; 3.0-1.5 \mathrm{Mc} / \mathrm{s} ; 1,500$ $-600 \mathrm{kc} / \mathrm{s} ; 500-200 \mathrm{kc} / \mathrm{s}$.

The i.f. is $560 \mathrm{kc} / \mathrm{s}$.
The circuitry includes an r.f. stage, two i.f. stages, a b.f.o., noise limiter, and a visual tuning indicator of the magic eye type. In its unmodified form, output is for headphones. The R1155 has a very large and distinctive tuning dial. In addition, the R1155B version has a superb high reduction tuning drive. This tuning drive is available separately, and can be fitted to the other versions.

The b.f.o. control is pre-set. This arrangement is quite suitable for c.w., but not quite so convenient for s.s.b.

The R1155 requires an external power unit. Output for headphones, and power input, are all provided for by one Jones socket, located on the front panel. A commercially manufactured power unit/output stage, inclusive of speaker, has been available. This unit will connect with the Jones socket thus enabling the R1155 to be used without modification.

In its original form, the RII55 was fitted with a direction finding device. This is of no use to the amateur, however.

Modifications: Although the magic eye funing indicator is quite suitable for the accurate tuning in of signals, an " $S$ " meter would be required for the accurate comparison of signals. In spite of the availability of a commercial power unit/output stage unit, many users prefer to modify the R1155 itself, and build a power supply and output stage into the set. There is room for this, if the unwanted D/F components are removed. For s.s.b. use, a fully tunable b.f.o. would be required, and this can be achieved simply by replacing the pre-set component by one with a longer spindle. Another possible modification is the stabilisation of the oscillator supply.

Availability: Quite a large number of R1155's were available before the period covered in this


Photograph by courtesy of The Marconi Company
report. A large number of the R1155B version were available in grade 2 condition between mid-1960 and mid-1961, and sold for prices ranging between $£ 8$ and $£ 10$. The commercial mains power supply/ output stage unit, mentioned earlier, was available for $£ 610 \mathrm{~s}$. Handbooks were not available, but a booklet of technical information was supplied.

Following the R1155B's, a number of R1155L's, or R1155N's (with the 1.5 to $3 \mathrm{Mc} / \mathrm{s}$ band) in grade 2 condition were available in mid-1961. They were only on sale for a month or two, at $£ 1219 \mathrm{~s} .6 \mathrm{~d}$., power/output units extra.

No Rll55's were released during 1962, 1963 and 1964. In mid-1965, however, a very small number of R1155B's in grade 2 condition were sold for $£ 6$ 19 s . 6 d . They are no longer available.
During 1960/61/62, the high reduction tuning drive, (fitted to the "B" version), was in plentiful supply for fitting to the other versions.

Although at the present time the R1155 is not available on the surplus market, and is unlikely to be in the future, they can be quite easily obtained on the secondhand market. Prices are from $f 10$ downwards, and most of them have been modified in various ways.

R1155 manuals are believed to be unobtainable, although a commercially produced booklet, containing technical information is available.

## The R1475

Designed by Marconi for the R.A.F., this is generally considered to be the receiver that replaced the R1155, although the authenticity cannot be
established. The R1475 certainly has a very fine performance, and is highly stable.

The receiver covers from 2 to $20 \mathrm{Mc} / \mathrm{s}$ in four bands. The i.f. is $600 \mathrm{kc} / \mathrm{s}$. The R1475 has 11 valves as follows:- $36 \mathrm{~K} 7,16 \mathrm{~K} 8,16 \mathrm{~J}, 36 \mathrm{Q} 7,16 \mathrm{H} 6$, 1 Y63 tuning indicator and a VR150-30 voltage regulator. The circuit includes one r.f. stage and two i.f. stages, a $600 \mathrm{kc} / \mathrm{s}$ crystal reference oscillator and a crystal controlled b.f.o. A voltage stabiliser is also incorporated. Other features include four-position selectivity with audio filters for c.w. reception; fast and slow a.g.c., and high and low noise suppression. Receiver sensitivity is of the order of 1 microvolt.
The tuning dial, which is of rather unusual design, is accurately calibrated and provides very adequate mechanical bandspread. The dial can be reset against the $600 \mathrm{kc} / \mathrm{s}$ oscillator by means of a special panel trimmer control.

A unique feature is that it is able to receive on two entirely independent frequencies simultancously. This feature is provided by means of a plug-in unit with an additional mixer, allowing the R1475 to receive on a guard channel in the range of 2 to $4 \mathrm{Mc} / \mathrm{s}$ or 4 to $7.5 \mathrm{Mc} / \mathrm{s}$.

The R1475 requires an external power supply, and the unit which is normally associated with this
receiver is the power pack type 360, which will operate from 200 to 250 V a.c. or 12 V d.c. The size is $16 \frac{1}{2} \mathrm{in}$. x 9 in . x 11 in . and the power pack is 8 in . x 9 in . x 1 lin .

Modifications: Modification is hardly necessary, but for the serious user, an " $S$ " meter might be considered more convenient than the tuning indicator that is fitted. It would be possible to replace the front-end valves with miniatures, but this is rather a drastic measure, and might not effect a great improvement.
Availability: A very few of these receivers came on the market in 1961. They were in grade 2 condition and were priced at $£ 12$ to $£ 14$, with power unit. A few grade 3 specimens were also available at a much lower price.
However, last year another batch arrived on the market, in varying conditions, the price ranging from $£ 10$ to $£ 15$. Some of these were in grade 3 condition. Power supplies were not available. The receivers were available over a reasonable period of time, and so it should not be too difficult to obtain one secondhand if they are no longer available from surplus dealers.

Information on the R1475 is very difficult to obtain, as it is a relatively scarce receiver. Manuals are not available.

## The TCS

This was made by Collins of the USA and it is deservedly popular. It is an exceptionally stable receiver, covering from 1.5 to $12 \mathrm{Mc} / \mathrm{s}$, It has seven valves, as follows:-1 12SA7, 1 12SQ7, 2 12A6, and 3 12SK7. The circuit includes one r.f. stage and a separate local oscillator. The i.f. is $460 \mathrm{kc} / \mathrm{s}$.
The TCS was originally designed for operation with a matching transmitter, but will operate entirely satisfactorily as an independent unit.

It has a vernier tuning system, fitted with antibacklash gears. Other panel controls are r.f. gain, a.f. gain, b.f.o. control, bandswitch, power switch, and a crystal local oscillator switch. The last control provides for reception on a crystal controlled frequency. In addition an output jack for 600 -ohm phones is provided. It does not have an internal power supply, and requires 250 V d.c. at 80 mA and 12 V a.c. at 1.25 amps .

Modifications: Although the TCS is exceptionally stable, making it eminently suitable for s.s.b. reception, the two main criticisms are the wide bandwidth and inadequate bandspread. The tuning drive can easily be modified by fitting an epicyclic drive; this will provide good mechanical bandspread. A Q-multiplier will improve the selectivity.

The r.f. gain controls both the r.f. and the i.f. stages. The provision of a separate r.f. gain control would doubtless improve the performance. Also, it is considered desirable to replace the 12A6 output and the 12A6 local oscillator with 12J5 valves. (These are a direct replacement.) This will give a more comfortable output for headphones and will reduce the output to the mixer which is considered to be excessive. By carrying out this modification, the h.t. current will be reduced by as much as 25 mA .

Availability: Unfortunately, the TCS has not been widely available in this country. It is almost certain that some were released prior to 1960, however. The one and only release in the period covered by


Photograph by courtesy of R.T \& I Electronics Ltd:
this report occurred in the summer of 1960. A number were released in grade 2 condition, at prices between $£ 8$ and $£ 11$. Power units were also available for about $£ 4$. It is believed that the sale of receivers from this release continued until late 1961 or early 1962. A few grade 3 specimens were available for a correspondingly lower price.

As this receiver is rather popular, and was probably released in larger numbers in the United States, it should be easy to obtain a manual.

## The No 52 Set

The 52 set is a Canadian receiver, and was manufactured by Marconi in large quantities. It was intended for operation in conjunction with a matching transmitter, but it is completely self-contained as a receiver. The frequency range is from 1.75 to $16 \mathrm{Mc} / \mathrm{s}$ in three bands, as follows:-
$1.75-4 \mathrm{Mc} / \mathrm{s} ; 3.5-8 \mathrm{Mc} / \mathrm{s} ; 7-16 \mathrm{Mc} / \mathrm{s}$.
The receiver contains 10 valves, and has the following stages:-r.f., mixer, separate oscillator, two

## E S V

## Stereo amplifier

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| 3000 less Cartridge |  | . |  |  | £9 | 13 | 0 |
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$\begin{array}{ll}0-5!\mu A & 2 \frac{t^{\prime \prime}}{2} \text { round proj. } \\ 200 \mu A & 2^{\prime \prime} \text { round panel s }\end{array}$
$200 \mu \mathrm{~A} \quad 2^{\prime \prime}$ round panel sealed Calibre-30 $\quad 22 /$ $\begin{array}{ll}200 \mu \mathrm{~A} & 3 \frac{1}{2}^{\prime \prime} \text { round panel } \\ 750-0-750 \mu \mathrm{~A} & 2^{\prime \prime} \text { round plug-in }\end{array}$
1 mA
$1 \mathrm{~mA} \quad 2 \frac{1}{2}$ round panel
$1 \mathrm{~mA} \quad 2^{\prime \prime}$ round panel sealed
$1 \mathrm{~mA} \quad 3 \frac{t^{\prime \prime}}{}$ round panel
$5 \mathrm{~mA} \quad 2^{\prime \prime}$ round clip fix panel or proj. .. 20/-
5-0-5mA $10-0-10 \mathrm{~mA}$ 1" round panel
$\begin{array}{ll}10-0-10 \mathrm{~mA} & 2 \frac{1}{2} \\ 0-30 \mathrm{~mA} & \text { round panel } \\ 2 \frac{1}{2}^{\prime \prime} & \text { round panel }\end{array}$

$\begin{array}{ll}75 \mathrm{~mA} & 2 \frac{1}{2} " \text { "plug } \\ 100 \mathrm{~mA} & 1 \frac{1}{4} " \text { proj. }\end{array}$
$100 \mathrm{~mA} \quad 1 \frac{1}{2}$ " round panel
$100 \mathrm{~mA} \quad 2 \frac{1}{2 \prime \prime}$ round panel
$2 \mathrm{Amp} \quad 2 \frac{1_{2}^{\prime \prime}}{} \quad$ round panel
5-0-5 A mp $2 \frac{1}{2}$ " round panel
8 Amp $2 \frac{1}{2}$ " round panel
25 Amp $\quad 3 \frac{1^{\prime \prime}}{2}$ round proj.
$50 \mathrm{Amp} \quad 2^{\frac{1}{2}}{ }^{\prime \prime}$ round panel
$\begin{array}{ll}20 \text { VDC } & 2^{\prime \prime} \text { square pane } \\ 150 \text { VDC } & 4^{\prime \prime} \text { round panel }\end{array}$
150 VDC ${ }^{4} 5 \mathrm{kV}$ with res. $2^{\prime \prime}$ round panel

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i.f.'s, detector/a.g.c., first audio. output and b.f.o. There is also a three-valve crystal calibrator to provide marker check points at $10 / 100 / 1,000 \mathrm{kc} / \mathrm{s}$ intervals. The set contains a valve check voltmeter which can also be used as an " $S$ " meter.

Panel controls are r.f. gain, a.f. gain, noise limiter, b.f.o. switch, heterodyne pitch control and wide or narrow bandwidth switch. Also, fast and slow tuning controls with additional oscillator control for fine adjustment. Other features include manual or automatic volume control on both c.w. and r.t., and there is also a c.w. filter. The set contains an internal 3 in . loudspeaker, and the whole receiver is housed in a steel carrying case, size 15 in . $\mathbf{x} 12 \mathrm{in}$. $x 15 \mathrm{in}$.

An external power unit is required for the 52 set, and must supply 12 V and 160 V h.t. Suitable power units are available which operate from 115/ 230 V a.c. or 12 V d.c.

Modifications: The 52 set does not require modification for satisfactory operation. One drawback to this receiver is the lack of bandspread on the $14 \mathrm{Mc} / \mathrm{s}$ amateur band, and modification details have appeared for this in the amateur radio press.

Availability: It first became available in small quantities in 1960 in grade 2 condition, for $£ 12$, power unit $£ 3$ extra. Early in 1961, they became more widely available, and the price was reduced
to $£ 9$, plus $£ 3$ for the power unit. They had all been sold, however, by the end of 1961.

In late 1962, more of them were released in grade 2 condition, and sold for prices between $£ 5$ and $£ 8$, or for $£ 910$ s. with power unit. These were quickly sold. Also, at this time, a few in grade 3 condition were available, and sold for $£ 210$ s.

In late 1963 , grade 2 receivers were available for $£ 7$, without case or power unit; and then a quantity of grade 152 sets, self-contained with power units, were available at $£ 13$ to $£ 14$. These latter were quickly sold out by the end of 1963. Some receivers in grade 2 condition were also sold for various prices at the same time. None were available in 1964.

During 1965, a quantity of the complete 52 set installation, comprising receiver, transmitter and power unit, came on the surplus market, and a few receivers were available separately for $£ 10$ without the power unit. There should be no difficulty in obtaining a 52 set on the secondhand market, owing to the large number released over the last five or six years.

The 52 set receiver handbook is difficult to obtain, although circuit diagrams were supplied with the receiver in some cases.

## END OF SERIES

## $?$ YOUR QUESTIONS ANSWERED

## SCRATCH FILTER

Could you give me any information about a scratch-filter for a record player? I believe there was a simple one published a few years ago in Practical Wireless but I have been unable to trace it.-E. Robins (Newport, Monmouthshire).

It is not easy to add scratch-filters to existing record-playing equipment. However, you could try connecting a 50 pF or 100 pF mica capacitor from each grid to chassis, and from each anode to chassis. The combined effect of these capacitors should reduce the high-frequency response.

If you want comprehensive control of tone, rumble, and hiss, you need a full-scale pre-amp. One such is described in the Mullard publication Mullard Circuits for Audio Amplifiers.

## LOG OR LINEAR?

Can you please tell me how and why we use log and linear potentiometers in circuits? I cannot find a rule which tells when and where to use these com-ponents.-F. Hardy (Hull, E. Yorkshire).

The type of potentiometer used in a circuit depends largely on whether or not the circuit handles audio frequencies. The human ear has what is termed a logarithmic response to sound volume. This means that, for instance, if an amplifier rated at 5 W were fully driven, and then compared with a 10 W amplifier fully driven with the same signal, then the second volume level would not sound anywhere near twice as loud as the first, even though the output power had been doubled. Thus, in audio gain-control circuits, $\log$ pots. are employed so that equal increments of rotation of the pots. result in equal increases in loudness.

If linear pots. were used, then to double a given
volume level, and then double it again, the two increments in rotation of the control would be far different. You will find more on this subject in books in your local library.

## / WANT TO LEARN

At the moment I know nothing about TV, radio, signs, terms, etc. and would like to learn, especially how to read wiring diagrams. Can you suggest any books which may help me?-M. Sabre (Wellington, Somerset).

Our book entitled Beginner's Guide to Radio would be of interest to you. We also publish a Keybook entitled More Simple Radio Circuits which contains a number of designs suitable for the beginner. We recommend that you start constructing units as soon as possible in order to gain experience. If you look through recent issues of P.W. you will find a number of simple designs and we suggest you select one which interests you and which you feel capable of constructing.

## REPLACEMENT AUTO-TRANSFORMER

I have been using an auto-transformer to drop the local voltage down from 220 volts to 110 volts in order to use a soldering iron of 110 volts 75 Watts. Unfortunately the auto-transformer has burned out so I am writing to inquire if some other means can be employed to do this, such as a resistor to drop. voltage, before purchasing another auto-transformer. -J. Macfarlane (Sunderland, Co. Durham).

It would not really be a good idea to use a dropping-resistor instead of your auto-transformer to power your 75 W soldering iron. If you were to use a resistor, then it would have to dissipate 75 W in order to drop the voltage to the correct amount, We recommend that you obtain another autotransformer for your iron. Such transformers are available from a number of our advertisers.

## Radio One v Radio Caroline

In a recent poll on the merits of "Radio 1" in our class, the results were as follows:
Two pupils admitted they didn't like either station. Another two pupils said they liked Radio Caroline and Radio One, but Radio One lacked something. And twenty-five pupils said Radio Caroline was great and Radio One was a flop.-K. Howes, 3T (The Latymer School, Edmonton, N.9).

## An early portable

As a reader of P.W. since No. 1 and having read and gained very much valuable information and advice from it over the years, I thought perhaps the construction for Christmas 1925 of a portable radio, may be of interest to readers.
This early set was of the I.H.F Detector, and two L.F. Stages with $2 V$ P.M. class valves. The frame aerial was mounted in the lid of the case and could be swung over 180 deg . for the best reception. Provision was also made for the connection of external aerial and earth. A twopin non-reversible plug for extension speaker ( $2 \mathrm{k} \Omega$ ) was fitted on the front control panel.
The weight of the 1.t. grid and h.t. batteries was approximately 28 lb . This just goes to show the progress of radio in 40 years.F. F. Towndraw (Newquay, Cornwall).


Mr. Towndraw with his early portable receiver.

## Radio alarm

I was interested to read in the August issue of P.W. re Patrick Highams "Radio Alarm".

It is some 30 years ago when I used to experiment with clocks for switching on and off of radios etc. You may be interested to know of my first one which was a chain driven clock and by fixing an ordinary switch to the wall in direct line with the trailing end of the chain and soldering a small hook to the knob it acted very effectively as an automatic switch. It was noted the speed of the chain was exactly 8 links per hour, therefore it was possible to divide the time by 8 and measure off the number of links for any given time; to my surprise the chain was always thrown clear and never prevented the clock from still carrying on.

Later on I progressed further and made one which would put the radio on and off 8 times in the 12 hours, and in addition to this it could be pre-selected to also change from one station to another. One could go to bed listening to dance music on the "Light" until a set time and be awakened at $7 \mathrm{a} . \mathrm{m}$. by the "Home News". It of course needed some planning when setting up for a full day's programme but once set it did the job and amused many of my visitors and friends.

Today I have a surplus to requirements cooker electric clock which switches my f.m. set on and off at pre-set times, and in addition the outlet socket can also be used for other purposes, electric fire, tape recorder, etc.

Still on the subject of clocks, some years ago I had what I thought was a good idea but it was turned down by a British firm as costing too much to make. When an electric clock fails due to a power failure, my idea was to bring into operation an ordinary movement automatically, to keep the clock on time, and when the power of the mains was again restored the spring-driven clock mechanism was automatically stopped until another failure presented itself.

Some of my Swiss friends
inform me a similar clock was tried out in Switzerland about 1938 but never came to anything due to the extra costs.

However, all our little ideas and whims seem very much outdated in this modern World of Electronics.

Anyhow, I was pleased to hear of Mr. Higham's idea, and seems he was thinking on the same lines as myself.-H. S. Barker (Lancashire).

## How's this for a shack?



Mr. Rowlinson's wireless cabin on board the S.S. City of Winchester.

I felt that you might like to publish this photograph of my wireless cabin on S.S. City of Winchester during the time I served on the ship, 1923-4, in the frozen meat trade on the New Zealand-UK run.
The transmitter was a $\frac{1}{2} \mathrm{~kW}$ job made by Marconi. In the picture, the old Jigger transformer and ATI with plugs to tap windings can be seen.
Also, one can see the Emergency Transmitting Set comprising a 10 in . induction coil, and the rotary converter starter and field regulator.

Of chief interest perhaps, is the 31 A crystal receiver and the then brand-new one valve amplifier for use with crystal receiver. Also the old sliding ATI for reception of Poldhu, Eiffel Tower and long waves around 2,000 metres.L. Rowlinson (Farnham Common, Buckinghamshire).

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# internittont fault locator 

IT has been said that necessity is the mother of invention. It was certainly necessity which caused the writer to build the following instrument.
To explain how this came about is quite simple. The writer was engaged in repairing and servicing car radios, and, as a result of the vibration to which car radios are subjected a number of in'termittent faults were encountered which to say the least were extremely irritating. The next question after deciding that such an instrument was necessary was the manner in which this was to be achieved?

The ideal instrument would be one in which the fault showed itself to be in some particular stage of the receiver. So far so good, but it was also necessary to decide which fault to locate on the instrument.

If one were to consider a voltage fault, then a number of voltmeters would be needed, each connected (a) to the anode or screen of the valvesin the case of valve car radios, or (b) to the collectors of each transistor-when servicing transistor car radios. However, such an arrangement would not locate an open inter-stage capacitor either r.f. or a.f., since such faults would hardly cause any indication on the voltmeters.

An oscilloscope is most useful in receiver servicing, but like other such instruments, may only be connected to one spot at a time. Hence, with such and instrument, luck would play an important part in having it connected to the faulty stage when the fault developed, and in servicing one does not have stores of luck in the same way as parts.



What was left? The answer to that was the actual signal passing through the various stages of the receiver, could something be carried out on those lines? It certainly cold, and what was more, the advantage of the oscilloscope and the voltmeter was employed to give further assistance. Therefore, it was reasoned that a signal indication was of far greater value when considering intermittent faults, however such faults occurred.

It was decided to employ eight magic eyes to provide the means of visual indication of the presence, or absence of a signal, eight r.f. amplifier valves, and eight diode detectors together with a rectifier valve meant 25 valves. This, of course, resulted in another problem, that of providing sufficient h.t. and most important, heater voltage and current.

The valves employed were, eight magic eyes EM80; eight r.f. valves EF92; eight detectors 6AT6; rectifier valve EZ81.

A mains transformer was obtained with the following secondaries, H.T. $350-0-350$ at 150 mA ; L.T. 16.3 volts 2.5 amps c.t.; L.T. 26.3 volts 3 amps c.t.; Rec. $6 \cdot 3$ volts 2 amps ; Primary, 200- 250 volts.

The heaters of the valves were connected in the manner shown in Fig. 1. Despite the advantage of transistors in the reduction of size when such an instrument is considered, the writer was of the opinion that, since most of the intermittent faults were on transistor receivers, he did not require the instrument to suffer in the same way with intermittent faults! Thus the plan to employ valves for those reasons was firmly decided at the start. Hence we have an instrument which has eight inputs, each having an EF92, a 6AT6, and an EM80 indicator, and may therefore be connected to eight points of a receiver providing visual indication of, or the absence of, signal at various parts in a receiver. The next step is to work a circuit around these valves and to incorporate such features as voltage readings, and also oscilloscope graphs at the eight points of connection.

## The Circuit

The circuit is shown in Fig. 2, with the exception that only one single stage is given, this being for olearness, and will be quite sufficient for the general function of the instrument to be seen. The other seven stages are exactly the same in all respects.

It will be seen from examination of Fig. 2, that


Fig. 2: Simplified circuit of the Intermittent Fault Locator (see text).
the input to the instrument is via the coaxial sockets, and in our own particular case to socket A. It is then fed to the volume control VR1 via the isolating capacitor C3, this capacitor being most necessary when connecting to the anode of valve receivers.

The control VR1 also plays an important part, since as the instrument is connected to the various stages of the receiver, the gain or signal strength is much greater. This would result in overloading of the target, thus making visual indication of the signal difficult, if not impossible. Hence the purpose of VR1 is to limit the signal fed to V1, and in consequence, to V3.

As the signal reaches the grid of V3, the area of the target fluorescent portion increases-in this instance green-and in the absence of a signal, a shadow results. This action is, of course, different to some indicators, where the reverse takes place. i.c., the signal causes the shadow on the target to become small.

The values of the components will be given at the end of this article, in particular, it is important to note that R3 and R4, must be equal in value, in order for maximum signal gain to the grid section of V3.

## Voltage Test

So that voltage checks may be carried out, eight "press to test" switches are provided, contact being made when the switches are pressed, and contact is automatically broken when the hand or finger is removed from the button. A d.p.d.t. SI switch is also provided to enable oscillograph readings to be obtained. This switch is actually a d.p.d.t. connected
to act as a s.p.d.t. as shown in the diagram.
This provision will be found very useful in the early stages of transistor receivers, where the signal gain is not very great. However, with the system of the press button, the oscilloscope, or the voltmeter may be quickly connected to eight points in the receiver, and in particular, to the stage where the magic eye has indicated that a fault exists.

With reference to the voltage test which may be carried out on the instrument, it is most essential that the meter used should be of good quality. Therefore, anything less than $20,000 \mathrm{ohms} / \mathrm{volt}$ should not be used, this requirement being for transistor receivers where the total voltage supply is extremely low, and from which the meter must draw its own supply to operate its movement, all of which can lead to errors in measurement.

## Voltmeter Range

With reference to Fig. 2, it will be seen that S3 is the voltage range switch, this allows voltage checks from 3 to 600 volts to be carried out.
With regard to transistor receivers it is essential that the low voltage ranges have accurate resistance values, to avoid serious errors in measurement. This means that the resistance of the meter must be at all times taken into account, even on the low range of 3 volts, a meter movement of 2,500 ohms can introduce an error of $4 \%$ at f.s.d. if its resistance is left out of the calculations.

The voltage ranges considered useful by the writer are, $0-3 \mathrm{~V}, 0-15 \mathrm{~V}, 0-30 \mathrm{~V}, 0-100 \mathrm{~V}, 0-300 \mathrm{~V}$, and $0-600 \mathrm{~V}$. The first three voltage ranges must be considered to be for transistor receivers, this of

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W．E．Wire Ended．
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| $8 \times 8 \mu \mathrm{~F}$ | 450 v | $1{ }^{\prime \prime} \times{ }^{\prime \prime}$ | T． 1 | 4 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $8 \times 16 \mu \mathrm{~F}$ | 450 v | $2^{\prime \prime} \times 1^{\prime \prime}$ | T． 1 | 4 | 6 |
| $16 \times 16 \mu \mathrm{~F}$ | 275 v | $2^{\prime \prime} \times{ }^{\prime \prime}{ }^{\prime \prime}$ | T． 1 | 4 | 0 |
| $16 \times 16 \mu \mathrm{~F}$ | 450 V | $2^{\prime \prime} \times 1^{\prime \prime}$ | T． 1 | 4 | 6 |
| $16 \times 32 \mu \mathrm{~F}$ | 275 v | $1^{3 \prime \prime} \times 1^{\prime \prime}$ | T． 1 | 4 | 0 |
| $32 \times 32 \mu \mathrm{~F}$ | 275 v | $2^{\prime \prime} \times 1^{\prime \prime}$ | T． 3 | 4 | 0 |
| $50 \times 50 \mu \mathrm{~F}$ | 300 v | $2^{\prime \prime} \times 1 \%^{\prime \prime}$ | T． 2 | 4 | 6 |
| $50 \times 150 \mu \mathrm{~F}$ | 300 v | $3 \frac{1}{2}{ }^{\prime \prime} \times 1$＂ | T． 2 | 6 | 6 |
| $60 \times 250 \mu \mathrm{~F}$ | 275 v | $4^{\prime \prime} \times 1$ 硈＂ | T． 2 | 9 | 0 |
| $80 \times 40 \mu \mathrm{~F}$ | 450 v | $4^{\prime \prime} \times 18^{\prime \prime}$ | T． 2 | 12 | 6 |
| $100 \times 100 \mu \mathrm{~F}$ | 275 v | $3^{\prime \prime} \times 1{ }^{\prime \prime}$ | T． 2 | 6 | 6 |
| $100 \times 400 \mu \mathrm{~F}$ | 275 v | $4 \frac{1}{\prime \prime}^{\prime \prime} \times 1 \frac{1}{2 \prime}^{\prime \prime}$ | T． 2 | 13 | 6 |
| $200 \times 200 \mu \mathrm{~F}$ | 300 v | $4^{\prime \prime} \times 1{ }^{\prime \prime}{ }^{\prime \prime}$ | T． 2 | 12 | 6 |
| $300 \times 300 \mu \mathrm{~F}$ | 300 v | $4^{* *} \times 1{ }^{\prime \prime}$ | T． 2 | 14 | 0 |

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course taking into consideration coach radio which require 24 volts. After the 30 volt range has been worked out, the meter resistance may be neglected, since an error of $4 \%$ means only an error of 4 volts in 100 volts.

The switch S2, allows the meter movement to have its leads reversed, this for transistor car radios, which may have the chassis either negative or positive polarity. It will also be seen that a speaker is provided with a balance control, so that the output stage is always loaded to avoid damage to the output transistor, and to reduce the signal should the phone ring. The receiver`s volume control must always be at maximum in order that the magic eyes show the presence of the signal, any change in the volume control would give false indication not only to the magic eye display, but also to the oscilloscope, where perhaps, reference voltages have been used to set the Y amplifier to a certain gain which will prove of no use of the gain of the receiver is changed, or the input to the receiver from the signal generator.

## Instrument Front Panel

Figure 3 shows the front panel of the instrument with all its main control positions cut out. The measurements here are very approximate, the volume controls and switches etc. should be of the midget type, or else difficulties will be met when it is desired to fix the front panel to the chassis.

The top row of holes are for the magic eye display, and it is essential that these coincide with the "windows" of the EM80, close working between the top chassis and the front instrument panel clearly being necessary.

The lower rows of holes must also "coincide" when drilling of the panel and chassis are undertaken.

These holes include those for the pilot lamp,



Fig. 3: Front panel of the instrument showing cut outs for the main controls etc.
on/off switch (d.p.s.t.), the polarity switch for the meter, the voltage range selector, and the switch for bringing in either the voltmeter or the oscilloscope.

## Wiring Points

The leads to the valves such as V1 in Fig. 2, must be kept apart from each other, in no circumstances must they be made into a neat 8 -core cable, for to do so would introduce capacity between them. This would result in a signal input to say point " $A$ " Fig. 2, causing the other magic eyes to indicate the same signal, even if there is no other input to the coaxial sockets.
It has been previously stated that the press buttons were mounted very close to the coaxial sockets, the reason for this being again one of capacity effect. It will be seen that the lead from the centre of the coaxial socket up to the press button switch, is constantly present. That is to say, its capacity-with the other leads-are added to the receiver under test. It is, of course, necessary to reduce excess capacity, hence these connections must be kept very short. The press buttons are indicated in Fig. 2 by Pl/P8.
In the general construction of the instrument, the heaters were wired first, different colour wiring being used for each section of valves, it is vital that these do not get mixed up!

The next stage is to wire the resistors to the magic eye display, completing one step at a time for instance, one would complete the anode connections of all the EM80 valves before they went on to the grid connections. In this way nothing is left to chance and so on with the other valves.
Perhaps the next step will be to describe the manner in which the instrument is employed to locate either (a) an intermittent fault, or (b) a fault which makes the receiver output low after it has been switched on for some time.
Take a typical five transistor car radio, including a germanium diode detector (DI).

We shall assume that we have
an intermittent fault, and to employ the instrument in its location, the socket " $A$ " would be connected to the collector of Trl (frequency changer), socket " $B$ " to the collector of $\operatorname{Tr} 2$ (st i.f. stage), socket "C" to the collector of $\operatorname{Tr} 3$ (2nd i.f. stage), socket " D " to the secondary of the 2 nd i.f. transformer, socket "E" to the a.f. side of D1, socket "F" to the collector of $\operatorname{Tr} 4$ (1st audio stage), socket " $G$ " to the base of Tr5 (output transistor - single ended), and socket "H" to $\operatorname{Tr} 5$ collector.

We may also obtain voltage readings at the various points so that we can check them, when the receiver cuts out, against those reading when the receiver was working, this would show up on the meter when the press buttons were operated.

In a like manner the oscilloscope, but before we may do this we shall require a signal input to the aerial socket, this being supplied from a signal generator. The car radio is tuned to this signal, and the aerial trimmer adjusted for maximum gain. It will, of course, be necessary to reduce the input to the coaxial sockets so as to prevent overloading of the "magic cye display", this being achieved by the volume controls under each of the windows. The gain of the receiver will become greater as we progress towards the output stage as expected.

As soon as we have a good indication of the signal on each of the magic eyes, the oscilloscope can be connected to each of the points and the various gains noted. This may be recorded, reference voltages from the front of the oscilloscope being used to measure the gain of the "Y" amplifier at any point. For instance, at the a.f. side of D1 the gain of the scope may be set to show 10 divisions on the graticule, for a reference voltage of 1 volt.

If the signal at this point is 0.3 volts, this would be equal to 3 divisions on the graticule; at other points in the circuit, the gain of the " $Y$ " amplifier will be changed, but, if it is necessary to return to the a.f. side of DI, we only need to bring the trace up to

## * components list

| R1 $100 \mathrm{k} \Omega$ R 4 $1 \mathrm{M} \Omega$ <br> R2 $15 \mathrm{k} \Omega$ R 5 $1 \mathrm{M} \Omega$ <br> R3 $1 \mathrm{M} \Omega$ R 6 $1 \mathrm{M} \Omega$ <br> VR1 $2 \mathrm{M} \Omega$   <br> Meter resistances vary according to mete All capacitors in Fig. 2 with the exception is 100 pF are $0.01 \mu \mathrm{~F}$. The balance contro for the speaker is 25 ohms. <br> The smoothing capacitors are $8 \mu \mathrm{~F}$ at 600 vo the smoothing resistance two $2 \cdot 2 \mathrm{k} \Omega$ resistors in parallel. |  |  |  |
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Internal view of the complete instrument.

10 divisions for a reference voltage of 1 volt switch in the scope to D1, where the gain should show 0.3 volt if all is in order.

Let us assume that the magic eye " $D$ " reduced to a shadow instead of producing an area of green. If "C" shows that a signal is reaching the magic eye, then the secondary is $\mathrm{o} / \mathrm{c}$, or a capacitor $\mathrm{o} / \mathrm{c}$ or even $\mathrm{s} / \mathrm{c}$.

On the other hand, if no signal is heard from the speaker, but the magic eyes up to "D" show that a signal is reaching those points, the scope should be connected to either "C" or "D", to see if the waveform is modulated, if not, this will point to the frequency changer stage being at fault.

Thus it is possible to locate the stage at fault, however, some faults cause the output to reduce after the receiver has been on for some time, this will be shown by the magic eyes after the stage at fault, to indicate a reduction in area of fluorescence. The fault being between the last good magic eye indication, and the first poor magic eye display.

It is also possible to use a probe for signal tracing, one amplifier stage of the instrument being used. The writer has used the instrument with good results in locating sources of intermittent faults, or the reduction of gain after the receiver has been on for some time.

It will be obvious to some readers that a single germanium diode could perform the function of V2. This is true, but the author had the valves and components to hand and to avoid extra expense these were used instead.

## REPLACEMENT RECTIFIERS

-continued from page 678

lease of life to a number of old sets for which replacement valve rectifiers have long since disappeared. Perhaps the oddest was replacement of the
rectifier section of a 117 L 7 valve. This was a combined output valve and rectifier with 117 V 0.09 A heater from a pre-war American receiver. The heater was still intact but the rectifier cathode had collapsed. Substituting a diode unit left the output section functioning and restored the radio to a new lease of life.



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## 12 WATT INTEGRATED HIGH FIDELITY AMPLIFIER AND PRE-AMP



## 12 watts R.M.S. output continuous sine wave (24W PEAK) 15 WATTS MUSIC POWER (30W PEAK)

- $3 \times 1 \frac{3}{4} \times 1 \frac{1}{4} \mathrm{in}$.
- IDEAL FOR

BATTERY OPERATION

- 15-50,000c/s $\pm 1 \mathrm{~dB}$

PZ. 3 Mains Supply Unit for Z. 12 and Stereo 25 users.

79/6

The embodiment of power, efficiency, reliability and economy. Nothing could be better than this fine amplifier for use with space-saving plinthmounted motor and pick-up assemblies. Equally, its light weight makes the $\mathbf{Z . 1 2}$ ideal for guitar amplifier or electronic organ. It operates efficiently on any power supply between 6 and 20 V . D.C. The pre-amp of this 8 -transistor master piece will accept the outputs of pick-up, radio and microphone, etc. Full details for matching control and selector switching circuits are in the manual supplied with each unit. The $Z .12$ is now in use all over the world and is the accepted standard for all hi-fi needs.


TECHNICAL DETAILS
Class "B" ultra-linear output.
RESPONSE $15-50,000 \mathrm{c} / \mathrm{s} \pm 1 \mathrm{~dB}$.
Suitable for $3,7.5$ or $15 \Omega$ speakers. Two $3 \Omega$
speakers may be used in parallel.
INPUT- 2 mV into $2 \mathrm{k} \Omega$.
Signal to noise ratio better than 60 dB .
Use two for stereo.
BUILT, TESTED AND
GUARANTEED.

SINCLAIR STEREO 25 For use with two Z.12s or any hi-fi stereo system. Frequency response $25 \mathrm{c} / \mathrm{s}$ to $30 \mathrm{kc} / \mathrm{s} \pm 1 \mathrm{~dB}$. Switched inputs for P.U. Radio, Microphone, etc. Equalisation correct to within $\pm 1 \mathrm{~dB}$ on RIAA curve from 50 to $20,000 \mathrm{c} / \mathrm{s} 6 \frac{1}{2} \mathrm{in}$. $\times 2 \frac{1}{2}$ in. $\times 2 \frac{1}{2} \mathrm{in}$. plus knobs. Built, tested and
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