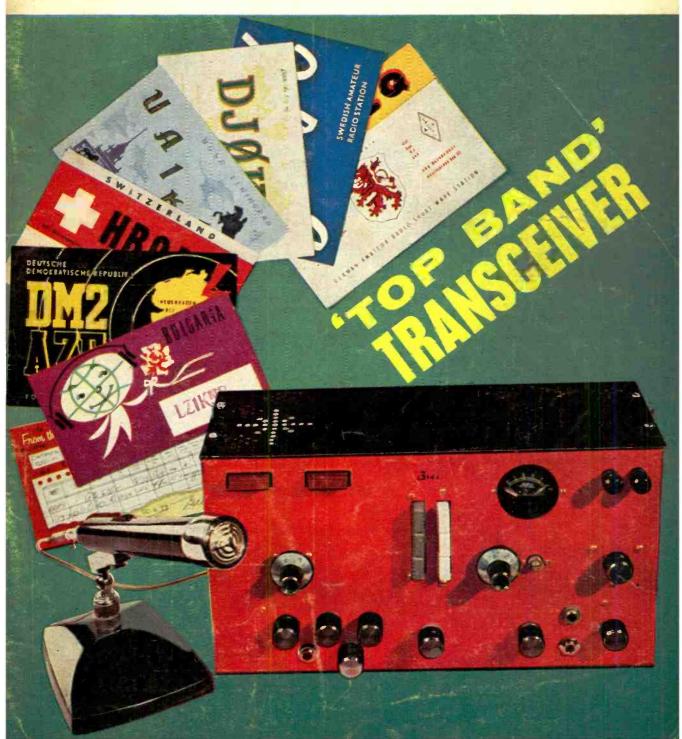
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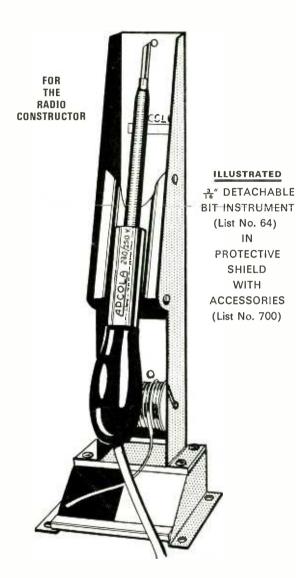
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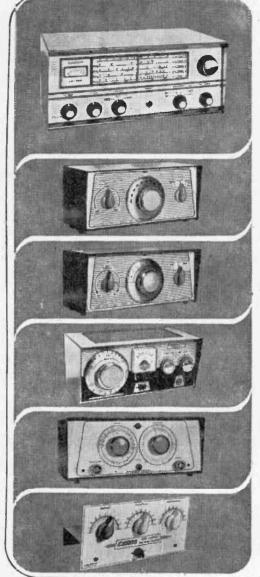
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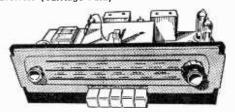
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EF184	6/4	UCH81	6/3		11/-		2/6		12/6	OC202	13/6
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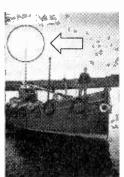
Throughout the development of radio communication the keen private experimenter has contributed largely to the advance of our science. The amateurs of the thirties pioneered reliable shortwave transmission and reception. Basic theories and their practical application are to this day hatched in the fertile minds of ingenious men who are the leading amateurs of our time.

The Joystick Aerial System can now be regarded as the perfect example of a purely amateur development "turning professional". Thousands of Joystick variable frequency aerial systems have been sold. The enormous number of enthusiastic testimonials that have accumulated at the Joystick factory are now in themselves calling for a separate filing room! The continuing success of the VFA has not only spread right round the world but has finally penetrated the barrier of professional and official circles. Professional bodies in the USA, Europe, Africa and the Far East have ordered VFA systems for operational use and for experimental work. Security forbids the whispering of names but clearance has been given to mention the Nigerian Police and an Australian fire control organisation.

In the Scottish fishing boats which have installed the system, communication with other ships and shore stations has become considerably more reliable over difficult paths.

This VFA system is a remarkable invention and its unique quality of high performance at any selected frequency from 1 M/c to 30 M/cs—particularly from difficult locations—has radically changed the attitude of both the licensed amateur and the shortwave listener towards their aerial problems.

Each Joystick VFA system is complete with a Joymatch matching unit suitable for each type of operation.

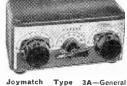


Scottish Fishing Boats Aerial Problems solved!

The Joystick aerial was successfully subjected to the most rigorous tests under appalling weather conditions aboard the MFV Crystal Sea OB104 and the MFV Margaret Ann OB79 out of Mallaig. Previously the old-fashioned wires had to be lowered every time the ships' derricks were used. Communication with shore stations and other ships was consistently good.



Joymatch Type 2A—General medium wave coverage extending over short wave spectrum.



Joymatch Type 3A—General short wave coverage for SWL. Bandswitched for amateur bands. Joymatch Type 4—(similar to Type 3A). For transmission and reception. Bandswitched on 160—10 metres.



Joymatch Type 4RF—For transmission and reception on 160— 10 metres. Includes RF meter for peak efficiency.



Joymatch Type 3—General shortwave coverage SWL (Junior model).

You cannot afford to ignore the potential of the Joystick VFA. The system is simple to use—the Joystick VFA will clip to a chimney, tree or mast, can be laid upon a pelmet, stood in the corner of a room, will even give a good account of itself in a basement.

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You are strongly recommended to contact the Joystick factory immediately (or one of our agents) for a brochure with full details.

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15 watt HI-FI TRANSISTORISED AMPLIFIER TYPE A15



HIGH FIDELITY LOUDSPEAKER UNITS Cabinets of latest styling Satin Teak or Walnut, acoustically lined (and ported where appropriate). Credit Terms available on all units.

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8 WATT rating. 3 or 15 ohm. Frequency response 50-13,000 c.ps. Specially designed high flux 5in. speaker with low fundamental resonance. Handsome Teak veneered cabinet. £6/19/11

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Cross-over unit
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Rating 10 watts.

Smooth response

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12 Gns.

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R.S.C. STEREO/TEN HIGH QUALITY AMPLIFIER

Carr. 15/-.

A complete set of parts for the construction of a unit giving 5 watts high quality output on each channel (total 10 watts). Sensitivity is 50 millivolts. Suitable all crystal or ceramic stereo heads. Cansed Bass and Treble Controls. Provision is made for use as straight (monaural) 10 watt amplifier. Valve line-up ECC83. ECC83. EL84. EL85. Outputs for 2-3 ohm speakers. Point to point wiring or supplied factory assembled with 12 months' guarantee for 11 kns. f8.15.0 Terms: Dep. 36/- and 9 monthly payments 25/5 (Total £13.4.9).

AMPLIFIER TYPE A15
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R.S.C. TFM1 TRANSISTORISED VHF/FM RADIO TUNER

Total cost of parts with detailed wiring diagrams and instructions. Carr. 10/- 12 Gns. Carr. 10/- 2 Or factory built 154 Gns. Or in Teak finished cabinet as illustrated 194 Gns. Terms: Deposit £5 and 9 monthly pay-ments 39/-



* High-sensitivity * 200-250v. A.C. Mains operation. * Sharp A.M. Rejection. * Drift-free reception. * Output ample for any amplifier (approx. 500 m.v.) * Simple alignment instructions. * Output available for feeding tuning meter. * Output for feeding Stereo Multiplexer. * Tuner head using Silicon Planar Transistors. * Designed for standard 80 ohm co-axial input standard of performance and reliability. The pre-wired tuning head facilitates speed and simplicity of construction. Printed circuitry. Only first grade transistors and components used. Our latest product giving you the best at half the cost of comparable units. Stereo Multiplexer available.

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HF811D 8in. 10 WATT 4 Gns. HF101D 10in. 12 WATT 5 Gns. HF100D 10in. 15 WATT £5.15.0 HF121D 12in. 20 WATT £6.15.0 HF127D 12in. 30 WATT 9 Gns.

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FULLY TRANSISTORISED 200/250v. A.C. Mains,
15 WATTS R.M.S. cont. into 3-4 ohms.
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Maximum instantaneous Peak power output 28 watts.
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BY ALISATION TO Standard R.L.A.A. and C.C.I.R.
Characteristics for Gram and Tape Heads.
FULL TRIE MCNITORING FACILITIES.
SENSIT WITHINS Magnetic P.U. 4 mV. Crystal or
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TREBLE CONTROL: +126B to -146B at 10 Kc/s.
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ALL COMPONENTS ETC. ARE OF A HIGH STANDARD AND SUPPLIED BY LEADING BRITISH MANUFACTURERS.

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R.S.C.SUPER 30 STERED AMPLIFIER

A DUAL CHANNEL VERSION OF THE SUPER
I5. Employing Twin Printed Circuits. Close tolerance
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CROSS TALK: -52dB at 1.000 cp.s.
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Treble Control, Volume Control. Balance Control, Stereo/
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(2) Ceramic or Crystal P.U. (3) Radio/Aux. (4) Tape Head/
Microphone. Operation of the Input Selector Switch
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Rigid 18 s.wg, Chassis, Size approx. 12in. Wide, 3in. High

Rigid 18 s.w.g. Chassis. Size approx. 12in. Wide, 3in. High and 8in. Deep. Neon Panel Indicator, Attractive Facia Plate and Spun Silver Matching Knobs. Above facilities, etc., except for Ganging and Balance Control. apply also to Super 15.

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Carr. 13/9 18 1/2 Gns.

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Incorporating the latest Magnavox Tapedeck. The Audiotrine High Quality Tape Amplifier with switched equalisation for each of 8 speeds. High Flux P.M. Speaker, empty Tape Spool, a Reel of Best Quality Tape and a handsome Portable Cabinet of latest styling finished dark grey leathercloth. Size 144 x 17 x 81 in. and circuit. Purchased separately would total approx. 234 Performance equal to units in the £50-£60 class. Deposit 262 Gns.

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A highly-sensitive 4-valve quality amplifier for the home, small club, etc. Suitable for all crystal or ceramic P.U. heads and practically all "mikes". Separate Bass and Trehle controls giving "lift"

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R.S.C. A10 30 WATT ULTRA LINEAR HI-FI AMPLIFIER

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Highly sensitive. Push-Pull high output, with Pre-amp./Tone Control
Stages. Performance figures equal to most expensive amplifiers
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Specially designed-sect ionally wound ultra linear output transformer
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Sensitivity 12 millivolts so that any kind of Microphone or
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Reserve L.T. and H.T. for Radio Tuner. Two inputs with associated
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PUSH-PULL ULTRA LINEAR OUTPUT "BUILT-IN"
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AN EXCEPTIONALLY POWERFUL HIGH QUALITY ALL-PURPOSE UNIT For lead, rhythm, bass guitar and all other musical instruments. For vocalists, gram, radio, tape and general public address

** UNUSUALLY POWERFUL LOUDSPEAKER COMBINATION consisting of a FANE HIGH FLUX 15in. 30 watt unit PLUS a FANE 12in. 20 watt unit with extended frequency response. ★ 4 Jack Inputs and two Volume Controls for simultaneous use of up to 4 plck-ups or "mikes". ★ Cabinets covered in two-tone Rexine/Vynair with gold trimming. Fitted carrying haddles. ★ Separate Bass and Treble Controls giving "lift" and "cut".

49½ Gns. Send S.A.E. for leaflet. Or call at one of our many branches and compare the Bass-Regent with units at three times the cost.

Carr. 30/- Or deposit£7.17.6 and 9 monthly payments of £5.10.10. (Total 55 gns.)

G15 15 WATT AMPLIFIER for Lead or

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Type BM1. An all-dry battery eliminator. Size 5\(\frac{1}{2}\) x\(\frac{4}{2}\) x\(\frac{1}{2}\) x\(\frac{1}

SELENIUM RECTIFIERS F.W. (Bridged) All 6/12 v. D.C. output. Max A.C. input 18 v. 1a. 3/11, 2a. 6/11, 3 a. 9/9, 4 a. 12/9, 6 a. 15/9.

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Rhythm Guitar, Mike, Gram or Radio

High-fidelity output. Separate bass and treble controls. Twin separately controlled inputs so that two instruments or "mike" and pick-ups can be used at the same time. Heavy Duty 12in. 20 watt Speaker. Cabinet covered in attractive Rexine/Vynair. Size 18 x 18 x 8 in. Deposit 3 gns. 19½ Gns. 15/-. and 9 monthly payments of 43/7. (Total £22.16.3). S.A.E. for leaflet.

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POWER PACK KIT Consisting of Mains Transformer, Metal Rectifier. Electrolytics, smoothing choke, chassis and circuit. 200/250v. A.C. mains. Output 250v. 60vm 4.6.3v. 28 Supplied with case in lieu of chassis 28/11. Or assembled 39/11.

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R.S.C. COLUMN SPEAKERS

Covered in
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Type C58, 15-20 watts. Fitted flwe 8in. high flux
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30 WATT HI-FI AMPLIFIER

for Guitar, Vocal or Instrumental Group

A Four Input. two volume control Hi-Fi unit with separate Bass and Treble "cut" and "boost" controls. Latest type valves. Housed in strong Rexine covered cabinet carrying handles. Attractive black and gold perspex facia plate. For 200-250v. A.C. mains. Output for 3 or 15 ohm speakers. Send S.A.E. for leaflet. Deposit 23 and 9 monthly payments of 37/5 (Total 21s.16.9).

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In walnut veneered cabinet. 10 Watt Model, Gauss 12,000 lines. 3 f4.19.11 or 15 ohms. Carr. 7/6

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Terms available on both. Carr. 10/6 FANE HEAVY DUTY HI-FI SPEAKERS

5 Gns 12in. 20 watt. Type 122/10.

12in. 30 WATT HEAVY DUTY 15 ohm LOUDSPEAKERS

Flux Density 17,000 lines, Fully Guaranteed.
Outstanding value at normal price of approx. 2 carr. 1 £12. Or deposit 23/10 and 9 monthly payments 7 GNS. of 15/8 (Total £8.3.4).

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425.0-425v. 200mA. 6.3v. 4a, 6.3v. 4a, 5v. 3a 450.0-456v. 250mA. 6.3v. 4a, c.t., 5v. 3a TOP SHROUDED DROP-THEOUGH TYPE 526.0-256v. 70mA. 6.3v. 2a, 0.5-6.3v. 2a, 250.0-256v. 100mA. 6.3v. 2a, 6.5-6.3v. 1a, 350.0-350v. 80mA. 6.3v. 2a, 6.5-6.3v. 1a, 350.0-350v. 100mA. 6.3v. 4a, 0.5-6.3v. 3a, 300.0-300v. 100mA. 6.3v. 4a, 0.5-6.3v. 3a, 300.0-300v. 130mA. 6.3v. 4a, 0.5-6.3v. 1a, Suitable for Mullard 510 Amplifier 300.0-350v. 100mA. 6.3v. 4a, 0.5-6.3v. 1a, Suitable for Mullard 510 Amplifier 300.0-350v. 100mA. 6.3v. 4a, 0.5-6.3v. 3a, 350.0-350v. 100mA. 6.3v. 4a, 0.5-6.3v. 3a, ELLAMENTO TRANSISTOR POWER PACK

32/9

350-0-350v. 150mA. 6.3v. 4a. 0-5-6.3v. 3a. 39/11 FILAMENT or TRANSISTOR POWER PACK Types 6.3v. 1.5a. 6/9, 6.3v. 2a. 7/9, 6.3v. 3a. 9/9, 6.3v. 6a. 19/8, 12v. 1a. 8/9, 12v. 2a. or 24v. 1.5a. 19/9, 0-9-18v. 1½a. 16/9, 0-2-36-42v. 2a. 27/9. CHARGER TRANSFORMERS 0-9-15v. 1½a. 13/11 2/ja. 16/11, 8a. 18/11. 6a. 21/11. 6a. 25/11, 8a. 31/11 AUTO (Step UP/Step DOWN) TRANSFORMERS 0-110/120v. 200-230-250v. 50-80 watts, 14/9 150 watts, 29/11, 250 watts, 49/9, 500 watts. 99/9 UTTPUT TRANSFORMERS

OUTPUT TRANSFORMERS
Standard Pentode 5,000 to 30 or 7,000 0

to 3Ω Push-Pull 8 watts EL84 to 3Ω or 15Ω ... Push-pull 10-12 watts 6V6 to 3Ω or 15Ω ... Push-pull 10-12 watts to match 6V6 to 3, 5, 8

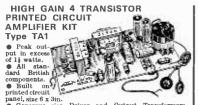
Push-pull 10-12 watts to match 6V6 to 3, 5, 8 or 15Ω
Push-pull EL94 to 3 or 15Ω 10-12 watts.
Push-pull Utra Linear for Mullard 510, etc.
Push-pull 10-18 watts, sectionally wound 6L6.
KT96, etc., for 8 or 15Ω
Push-pull 20 watt high quality sectionally wound, EL34, 6L6. KT66, etc., to 3 or 16Ω fully shrouded.

SMOOTHING CHOKES 150 mA, 7-10H, 250 Ω 12/9. 100 mA, 10H, 200 Ω 9/11. 80 mA, 10H, 350 Ω 7/9. 60 mA, 10H, 400 Ω 4/11.



11/9

21/9 22/9



printed circuit panel, size & x 3in.

Generous size Driver and Output Transformers.

Output transformer tapped for 3 ohm and 15 ohm speakers.

Transistors (GET 114 or 31 Mullard OC81D and matched pair of OC81 o/p).

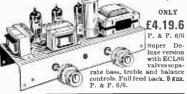
Everything supplied, wire, battery clips, solder, etc.

Comprehensive easy to follow instructions and circuit diagram 1/6. (Free with Kith. All parts sold

SPECIAL PRICE 45/-. P. & P. 3/-.
Also ready built and tested, 52/6. P. & P. 3/-.
A pair of TAls are ideal for stereo.

STEREO AMPLIFIER

Incorporating 2 ECL86s and 1 EZ80, heavy duty, double wound mains transformer. Output 4 watts per channel. Full tone and volume controls. Absolutely



6 TRANSISTOR AND DIODE **SUPERHET**

A first-class 2 waveband transistor superhet. • Printed circuit panel (size 8‡ x 23in.). • 3 pre-aligned IF transformers. • High-gain Ferrite Rod Agrial. • All First-grade transistors. • Car aerial winding. • Pushpull output • All parts supplied with simple instructions. All parts sold separately, Set of parts if purchased at one time ONLY \$4.5.0, P. & P. 2/6 (Circuit diagram 2/-Free with set of parts.)

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Suitable for use with above. 2in. Goodmans. Ideal replacement for most pocket portables, 8/6; 3im. 12/6; 7 x 4in., 21/-; P. & P. 2/- per speaker. Portable CABINET

Size approx. 91 x 61 x 31in. Suitable for above using 31in. speaker, 25/-. P. & P. 2/6.

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FOR TRANSISTOR SUPERHET

3 IF transformers one oscillator coil one driver transformer and wound Perrite aerial (med. long and caraerial coupling), 32/6 complete post 2/. 6 transistor printed circuit board to match 8/6. Post 1/-. Circuit diagram 1/6 extra.

MINIATURE PRECISION AIR-SPACED TWO GANG TUNING CONDENSER, 176+176 p.F. size 1½"w x ½"d x 1½"h with vanes open. Built in trimmers 5/-. P. & P. 1/-

BRAND NEW TRANSISTOR BARGAINS
GET 15 (Matched Pair) 15/-; V15/10p, 10/-; OC71
5/-; OC70 6/-; AF117 7/6.
Set of Mullard 6 transistors OC44, 2—OC45 OC81D

Set of Mullard 6 transistors OC44, 2—OC45 OC81D matched pair OC81 25/-, ORP12 Cadmium Sulphide Cell 10/6.

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B.S.R. MONARDECK (Single speed) 3\(\frac{1}{4}\)in. per sec., simple control, uses \(\frac{1}{2}\)in. spools, \(\frac{2}{6}\). 5.0 plus 7\(\frac{6}{6}\) carr. and ins. (Tapes extra).

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Beautifully made and expensively finished in dark grey heavy grade rexine. Satin Chrome metal grille front and chrome fittings. Speaker aperture 9° x 4° Overall Size 15½° w. x 15° d. x 7½° h. Will take any standard tape deck or single record player. Limited number only. Worth at least £5, OUR PRICE 49/6. P. & P. 5/-. Brand new and unused.

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A top-quality record player amplifier. This amplifier (was used in a 29 gn. record player) employs heavy duty double wound mains transformer, ECC83, EL84, EZ80 valves. Separate Bass, Treble and Volume controls Complete with output transformer matched for 3 speaker. Size 7in. w. x 24in. d. x 54in. h. Ready

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Uncut motor board. Will take above amplifier and B.S.R. or GARRARD Autochanger or Single Record Player Unit. Size 18 x 14 x 8½ in.

Price 23.9.6. Carr. 7/6.

4-SPEED PLAYER UNIT BARGAINS All brand new in maker's original packing.
SINGLE PLAYERS

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44.18.8 AUTO CHANGERS

AUTO CHANGERS

GARRARD 1000 with special Hi-Fi cartridge. \$6.2.6
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All the above units are complete with t/o mono head
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Suitable for use with Medium or High Impedance mikes,
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200/300 volt H. T. rail or 9 volt battery. Gain approx 14:1.
Fully isolated input by Mu-Metal screened transformer.
Size 4\frac{1}{2} \times 1\frac{1}{2} \times 1\frac{1}{

Dual Purpose Bulk Tape Eraser and Tape Head Demagnet-

TWIN TELESCOPIC AERIAL. Comprising two 3-section heavily chromed rods. Closed 12-in. each extending to 32in. Completely adjustable from vertical to horizontal. Supplied complete with universal mounting bracket, coax lead and plug. Suitable for F.M. or TV. 12/8. $P_{\perp} \& P_{\perp} ? P_{\perp} \& P_{\perp}$

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with twin .0005 tuning condenser for AM connection. Prealigned FM section .Complete with ECCS5 (6L12) valve and full circuit diagram of tuner head. Another special bulk purchase rabbles us to offer these at 27/6 each, P. & F. 3/-. Order quickly! Limited number also available with precision geared 31 reduction drive, 30/-. P. & P. 3/-.

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3-VALVE AUDIO AMPLIFIER



MODEL HA34
Designed for Hi-Fi reproduction of records. A.C. Mains operation. Ready built on plated heavy gauge metal chassis, size 7 jin. w. x in. d. x 4 jin. h. hoorporates ECCS3, EL34, EZ50 valves. Heavy duty, double would mains transformer matched for 3 ohm speaker, separate Bass, Treble and volume controls. Negative feedback line. Output 4\[\psi \text{watta} \], Front panel can be detached and leads extended for remote mounting of controls. MODEL HA34

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This kit although similar in appearance to HA34 employs entirely different and advanced circuitry.

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Stylishly finished monaural amplifier with an output of 14 watts from 2 EL84s in push-pull. Super reproduction



push-pull. Super reproduction of both music and speech, with negligation of the public public

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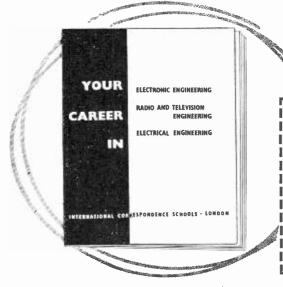
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MAGNAVOX 363 TAPE DECKS

TAPE DECKS

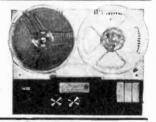
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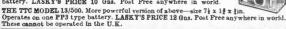
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Metal case size 3\frac{1}{2} (plus spindle) \times \frac{1}{2} \times 1 \ti

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In metal case size 4 x 6 x 1\frac{1}{2}in. Fully tunable—complete with PC86 and PC88 valves. LASKY'S PRICE 29/6 Without valves 12/6 TRANSISTORISED VHF TUNER

Bub-Ministure turret type fitted with 12 sets of cols and 3 Min In metal case size 3 x 1½ x 2½ in. LASKY'S PRICE 37/6 and 3 Mullard AF102 transistors

TREMENDOUS BARGAIN!

TV UHF TUNER AND IF AMPLIFIER PANEL

IF AMPLIFIER PANEL

Model No. 89384 made by famous manufacturer as standard conversion unit to 625 line reception (BBC 2) for 18° and 23° 406 line (convertible model) Cossor, Philips, Scott and Stella television receivers. The units are the standard conversion of the units with detailed convers and fully guaranteed, complete with detailed conversion on the sets mentioned above to meet only a pair of pilers and a screwdriver! The units are fitted with 7 Mullard valves—PCF 80 x2, EF188, EF184, ECC82, PC86, PC88. Size of units; tuner 71 x 4 x 81n. 18° panel on 9 x 44in. printed circuit board x 24in. deep. Complete with all leads, screws, washers etc. Original Price 210.10.0. Price £10.10.0.

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Incorporating the very latest circultry to provide high sensitivity and good quality in conjunction with extreme small size and compactness. High quality Newmarket transistors used throughout. All designed to operate on by ... miniature battery. Add 1/- on each lor Post and Packing. TTPE LRPC 1. 8 transistor. Input sens. 80mV. output 150mW. output 150mV. output 150mV. 400.

2 x 1 x ½in. PRICE 27/6

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PRICE 59/6 5 t x lix x lin. PRICE 59/6
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Special function modules—all one size $1 \nmid x \mid x \mid 1$ in. Complete with detailed function and installation instructions. Send S.A.E. for specification sheets. TFPE PA-1, Public address amp. for use with carbon, crystal or Dynamic microphones, TYPE CO-1. Morse code practice oscillator-for use with morse key and 3 \Omega nd 3Ω speaker. PRICE 20/-

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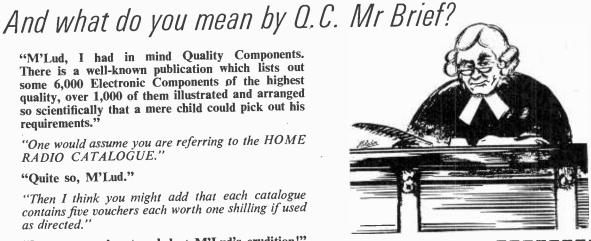
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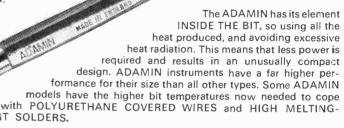
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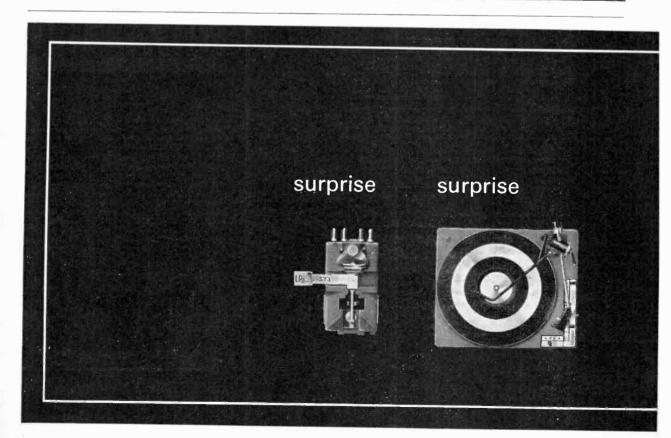
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P. A.P. 3/6 Circuit diagram 2/6

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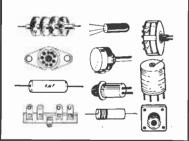
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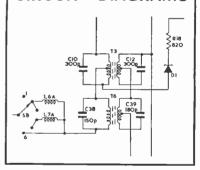


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WIRELESS

VOL 42 No 11

issue 721

MARCH 1967

TOPIC OF THE MONTH

More 'Pop' & Local Radio

The White Paper issued recently on Broadcasting has done a jolly good job of whitewashing and it is difficult from this document to comprehend the Government's attitude towards broadcasting in the United Kingdom. It has denied Independent Television the right to broadcast in colour (which would not cost the general public an extra penny), yet has permitted the BBC to start a popular music programme in the medium wave band and to run an experimental chain of local radio stations in the v.h.f. band.

"It has of course been the Government's duty," the White Paper explains, "to consider what the proposals for further extending the broadcasting services should seek to serve, and what organisation could best promote these purposes. The Government have also had to consider to what extent it would be in the national economic interest to allow the extensions. It is not enough that they should be desirable in themselves. The overriding consideration is whether the country can afford them."

What a lot of rubbish! The "pirate" radio stations have clearly shown that there is a need for "pop" music and that in general, listeners are not offended by the accompanying advertising. The Government have totally disregarded public opinion in deciding to set up a "popular" music station of a character which will not replace the "pop pirates".

Nine experimental local radio stations operating in the v.h.f. band are to be set up by the BBC in different parts of the country during the year. Locations have not yet been decided, but the stations are hoped to offer a full-scale local service and to be financially supported from local sources. Commercial advertising will not be accepted, yet the BBC will be prepared to accept financial support from local authorities, Chambers of Trade and Commerce, local Councils of Churches, arts associations and other representative bodies active in the social and cultural life of the community. The BBC will not, however, take a direct grant from the local rate fund, but will accept money from local authority departments, such as education. Thus, it would appear that this scheme is just another burden upon the ratepayer.

W. N. STEVENS—Editor

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APRIL ISSUE WILL BE PUBLISHED ON MARCH 3rd

All correspondence intended for the Editor should be addressed to: The Editor, "Practical Wireless", George Newnes Ltd., Tower House, Southampton Street, London, W.C.2. Phone: TEMple Bar 4363. Telegrams: Newnes Rand London. Subscription rates, including postage: 36s. per year to any part of the world. © George Newnes Ltd., 1967. Copyright in all drawlings, photographs and articles published in "Practical Wireless" is specifically reserved throughout the countries signatory to the Berne Convention and the U.S.A. Reproductions or imitations of any of these are therefore expressly forbidden.

Power supplies

I was unable to follow the reasoning in the article by H. T. Kitchen that appeared in the January 1967 issue.

Obviously $\frac{250}{25}$ x $\frac{60}{230}$ is not equal to 38

ohms as he states. Of course $\frac{250}{25} \times \frac{230}{60}$ is equal to 38 but what happened to the milliamps, that 10^{-3} bit, and how on earth did he come by the equation $\frac{E^1}{1} \times \frac{E^2}{1^2} = R$ (internal) and then confuse the product IR as being internal resistance?

P. Murphy.

Aldermaston, Berkshire.

The author replies:

I admit guilt in committing the sin of confusing my multiplication and division signs. The error is undoubtedly mine, and as the perpetrator thereof I must, bravely smiling, take the consequences.

It is, I regret, yet another example of the fallibility of human nature; of how a temporary loss of sync between brain and pen can virtually ruin much otherwise painstaking and accurate work.

As I see it, however, the bone of contention is the ultimate equation for calculating IR. Here, of course, I was well and truly up the creek when I used a multiplication sign instead of a minus one. The equation should

have read $\frac{E^1 - E^2}{I^2 - I^1}$

Using the new set of rules the IR for my power supply works out at 571 "point something" ohms. And as for forgetting our little milliamp friends, I hang my head in shame.—H. T. Kitchen.

THE P.W. FILM SHOW

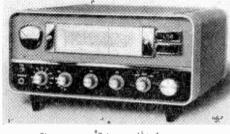
The annual film show, organised jointly by Mullard Ltd. and Practical Wireless, is to be held, as before, at Caxton Hall, Caxton Street, Westminster, London, S.W.1. The date is Friday, April 14th, and the show will start at 7.30 p.m. prompt.

The programme will include a film *Electrons in Harness* and a topical talk on *Transistors and Television*. Refreshments will be served in the interval.

Applications for tickets—which are free—should be made now to Film Show, Practical Wireless, Tower House, Southampton Street, London, W.C.2. A stamped addressed envelope must be included with all applications.

NEWS AND..

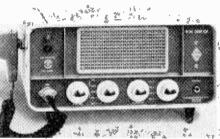
TWO NEW MODELS FROM K.W. ELECTRONICS



KW201 Amateur Band Receiver

11 ranges, 1·8—30 Mc/s. Crystal mixer. Crystal BFO. Q Multiplier.

Sens: $1\mu V/500 \text{mW}$. S/N: $1\mu V/20 \text{dB}$.



KW2000CA SSB

Transceiver
3—19 Mc/s. 180W
p.e.p. (SSB), 75
watts (CW), 25 watts
(AM). Mains or
Battery.

Transceiver—18 lb. A.C. p.s.u.—23 lb. D.C. p.s.u.— $6\frac{1}{2}$ lb.

The KW201 incorporates a mechanical filter which gives an i.f. selectivity of 3.1 kc/s at 6dB and 6 kc/s at 60dB. The Q multiplier (optional extra) gives a range of 3.1 kc/s to 200 c/s selectivity. The slide-rule vernier dial is accurate to 1 kc/s. The KW201, designed for optimum performance on single sideband, measures $13\frac{3}{4} \times 6 \times 12\frac{1}{2}$ in. and weighs 19 lb. Power supply is 200-240V, but a 115V version is available. The price is £105, complete with 13 crystals.

The KW2000CA is a commercial long range unit with a frequency stability of 1 part in 10^6 in ambients between $+700^\circ$ to -10° C. Enquiries to K.W. Electronics Ltd., 1 Heath Street, Dartford, Kent.

SILICON PLANAR TRANSISTORS—NEW TYPES

Mullard have added seven new p-n-p types to their range of silicon planar transistors. Because of their linear gain/current characteristics they are all suitable for both switching and linear applications.

The BCY70 and BCY72 are both 350mW type, the former having a high Vceo of 40V and low saturation voltage and intended for mediumspeed switching applications. The BCY72 is a general purpose type.

Low leakage current, low saturation voltage and high cut-off frequency (in excess of 200 Mc/s) are features of the new 600mW transistors 2N2904, 2N2904A and 2N3133 (high speed switching and driving) and 2N1131, 2N1132 (medium speed switching).

Mullard also announce new additions to their range of miniature and sub-miniature glass-encapsulated quartz crystal units. An AT-cut unit is available for a range of 1.6—87 Mc/s. There is also a special 10 Mc/s unit for secondary frequency standards (QX3100). A data book with full specifications is available on request.

IMPROVED SURFORM TOOLS

Stanley Works announce a completely redesigned range of their well-known Surform tools which have replaceable blades and can be used on materials from balsa wood to mild steel. Most readers will be familiar with these tools and will be interested to hear that an additional heavy duty blade specifically recommended for use on harder materials such as metals is now available for the first time.

... COMMENT

NEW YORK STATE LAW ENFORCEMENT FACSIMILE SYSTEM

Recently Governor Nelson A. Rockefeller, and Mayor John Lindsay and Commissioner Howard Leary, inaugurated a new communication system to aid New York State criminal justice agencies in fighting crime.

The equipment being supplied by Western Union for New York State Identification and Intelligence System is manu-

factured by the Muirhead Group of Companies.

Prior to the installation of this equipment when a suspect was fingerprinted, identification could take 7 to 10 days, it now takes 2 to 3 hours.

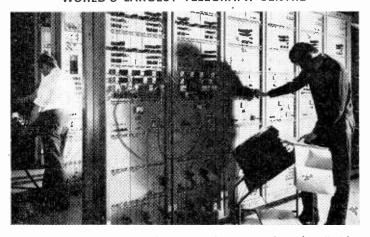
The suspect's fingerprint card is placed on a photographic transmitter and within 14 minutes is sent over a telephone circuit to an automatic photographic facsimile recorder. The received copy is automatically processed within the machine to produce a finished photographic copy of the original fingerprint card. This automatic processing takes approximately 12 seconds.

Once the suspect's identity is verified, a copy of his criminal history is transmitted by a rapid message facsimile system to

the originating agency in 4 minutes.

The installation is one of some 105 similar systems to be installed during the next 18 months, linking the various criminal justice agencies throughout the State with the State's Division of Identification in Albany.

WORLD'S LARGEST TELEGRAPH CENTRE



Automatic error-correcting telegraph equipment has been installed by The Marconi Company at the GPO's Fleet Building Telegraph Centre, the largest of its kind in the world. Situated in the heart of London, the equipment will provide for a substantial increase in the traffic handling capacity of radio telegraph services. Already the telex calls through Fleet Building exceed the total overseas telephone traffic from the whole of the United Kingdom, and the telex service is still expanding.

The photograph shows the Marconi equipment, which is known as Autoplex, undergoing final acceptance tests at the GPO's Telegraph Centre.

Autoplex is completely transistorised and housed in tall slim racks. At Fleet Building, 36 of these have been installed, increasing the centres radio-telegraph capacity to 296 circuits, each capable of carrying four separate telegraph links.

No news is good news

Your editorial and four-column article on the prosecution of pirate radio stations was a waste of space. Everyone interested had heard the outcome on radio, TV and read it in newspapers long beforehand.

I'm not against editorial comment about such issues, after all that is what maintains a magazine's individuality, but a full account and a promise of another detailed case is too much. The space could have been put to better use as constructional articles.

If this is going to be the future policy of P.W. how about the prosecutions of "ham" pirates, not to mention a sound version of Underneath the Dipole (from

P.T.)?

A far better policy would be to refuse advertised non-convertible 27 Mc/s walkie talkie spreads unless boldly indicated as such.

I.N.R.W. Newport. New Marston, Oxford.

[Although we cannot obviously compete with newspapers in reporting news items we feel it is reasonable to devote some space to important happenings in the radio world. A newspaper is usually thrown away after reading, whereas most readers retain their copies of hobby magazines. This provides a useful reference source for the future.

With regard to 27 Mc/s walkie-talkies, readers can be left in no doubt of our feelings on this point. Advertisers are asked to state that such equipment cannot be used in the U.K. (for P.W. has a worldwide circulation, including countries where C.B. facilities are available). For the benefit of those who may still be unaware of the facts may we again point out that the use of 27 Mc/s walkie-talkies for communications purposes (however limited the range) is strictly illegal and renders the user liable to prosecution]—Editor.

Club spot

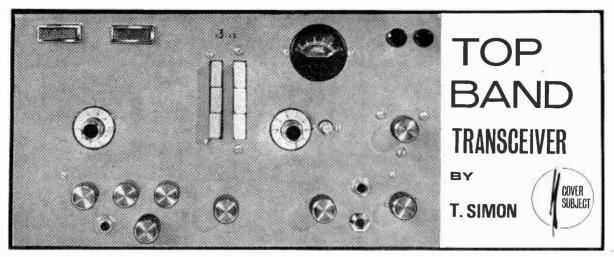
I would like to say how much I enjoy reading the Club Spot feature in this magazine. It is very useful to members of other clubs as it shows the activities that can be enjoyed from club membership and gives club committees ideas for their own organisations.

Brian Smith.

Ilford, Essex.

[We are pleased to hear that you enjoy the Club Spot feature. We would like to take this opportunity to appeal to clubs to send in information about themselves together with one or two photographs of QTH's and or members and equipment. All will be considered for publication.]—Editor.

More News and Comment on Page 844



HE trend in amateur circles these days is toward compact units as opposed to the huge rack and panel arrangements of earlier years. In a multi-band transmitter running 150W, it becomes necessary to "loose" 140W if topband is to be included and the 10W power limit observed. The unit to be described is based on observing the first statement above, while avoiding all the complications implied by the second.

The cheapest commercial topband transmitter on the market sells at around £15 and then requires the additional expense of a power supply. The unit described here cost less than £15 to construct and is not merely a transmitter. This price included the power supply unit; built-in frequency marker including crystal; and a receiver to boot. Briefly, the unit comprises a complete self-contained phone/ c.w. station for the 1.8-2.0Mc/s amateur band, occupying a space $12 \times 6\frac{1}{2} \times 4\frac{1}{2}$ in. It is based on economy and simplicity and uses only six valves, two in the transmitter, one in the modulator, and three in the receiver.

The circuit diagrams of the complete unit are divided into two sections; transmitter, and receiver plus power unit. Thus just the transmitter could be built, this would form the basis of a useful miniature topband rig, or just the receiver portion might be constructed, this being of particular interest to s.w.l's., and again the unit could be very small indeed.

Receiver Circuitry

This section of the unit employs three valves all Mullard type EFC82/6U8. The aerial input circuit ignores the coupling winding on L1 and the coil is top-capacity coupled to the transmitter tank circuit via C49 and S1e on the T/R switch. In this way the extra stage of selectivity afforded by the tank circuit is utilised on receive. In the writer's area there is strong break-through from the BBC at Brookmans Park (908kc/s 2nd harmonic). This is entirely eliminated by the tank circuit which peaks quite sharply.

V1 is a standard frequency changer circuit but with the inclusion of an extra potentiometer in the cathode of the pentode section. The original idea was to provide variable mute on transmit in order

to monitor one's transmissions on the receiver, but due to the very close proximity of the transmitter this does not function quite as well as was hoped. and the substitution of a fixed resistor of some $10k\Omega$ should prove adequate. An alternative would be complete screening of the receiver section—a complication which did not justify the effort required since the simple arrangement shown does work tolerably well. On receive, the T/R switch shorts the muting resistor to earth via S1a and the circuit functions as a normal frequency changer.

The pentode sections of V2 and V3 are used as i.f. amplifiers at 465kc/s whose gain is effectively controlled by VR2. These stages are quite stable providing the anode and screen volts are not too high, hence the larger than usual values of the screen resistors R7, R12. In the prototype the optimum valves for R7/R12 were found to be $82k\Omega$, however to allow for different layouts, etc., it was considered safer to specify the values shown in Fig. 1. The values quoted are for maximum gain consistent with stability, however, if it is found that on peaking the i.f.t. cores the circuit becomes unstable, then it is better to drop the h.t. to the i.f. stages rather than leave the i.f.t's. slightly off tune. If this latter procedure is adopted the receiver will work but the selectivity will suffer.

The triode of V2 is a straightforward audio amplifier fed from the diode detector D1. The triode section of V3 functions as a b.f.o. with VC2 as a pitch control for resolving s.s.b. and c.w. while S2 switches the b.f.o. out for a.m. reception. The high value decoupling and load resistors R10/R11, and the consequent low volts on the anode of V3b were found to be a necessity. Even with two $47k\Omega$ resistors here there was still too much b.f.o. injection. Also note there is no b.f.o. coupling capacitor as such. This proved to be superfluous presumably due to the coupling afforded by the inter-electrode capacity within the valve V3 itself.

Transmitter Circuitry

This section utilises the remaining three valves in which the first stage comprises another ECF82/6U8 as a Clapp v.f.o. and tuned buffer-amplifier/crystal oscillator (V5).

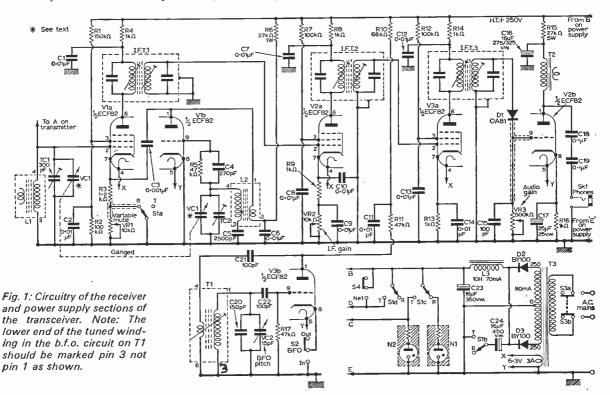
The v.f.o. is cathode coupled to the buffer stage

via the v.f.o. crystal switch S6. With this switch depressed the v.f.o. output is disconnected and the pentode section reasonates at 1.9Mc/s thus forming a frequency meter giving a marker right in the centre of the band. It might be possible to use a 100kc/s crystal and get a 1.9Mc/s point plus two very useful band-edge points on 1.8 and 2.0Mc/s but this idea has not been tried.

The p.a. V6 is a 5763, this valve merely because it happened to be in the junk box. Other suitable valves would be the 6BW6 or 6AQ5. Note alternative valves might require adjustment of circuit values, and some are B7G bases not B9A as for the 5763.

Departure from the time honoured pi-tank might shock some, since this has become almost an accepted standard. However the present system does permit odd lengths of wire presenting all sorts of impedances to be matched quite precisely and accurately. Those who still prefer a pi-tank might p.a. valve to limit the anode current to a safe value during the key-up periods, when there would otherwise be no bias (due to there being no drive) on the 5763 or p.a. valve used. If the v.f.o. were keyed, the buffer amplifier would also require cathode bias, or some means of protection during key-up.

The modulator section V4, provides frequency modulation and uses the two triodes of a 12AX7 in cascade. Doubtless one section might prove sufficient, but with two stages the QSO can be conducted in a confidential whisper with the mike gain half way up. Frequency modulation was chosen mainly because of the modest requirements both in circuitry and components, not to mention its tendency not to aggravate t.v.i. as opposed to, say, amplitude modulation. A class A audio amplifier suitable for a.m. would be required to produce around 5 watts of audio with attendant consumption of some 40-50mA of h.t. current plus the heavy and somewhat bulky modulation choke or



substitute a 500 + 500 pF variable capacitor, both sections in parallel, for the tank coil tapping switch S7. Due allowance for this should be made in the layout and size of chassis when planning. If this procedure is adopted then VC4 would also benefit from being a higher value, say 200-300pF. In the event of very short antennas such as whips being used, then the 500 + 500pF suggested for the pi-tank modification would benefit from being increased by the inclusion of a 1,000pF capacitor wired in parallel.

The transmitter is keyed in the cathode of the p.a. since this method has proved satisfactory in the past. If keying is inserted in the buffer or v.f.o. then a bias resistor and decoupling capacitor should be included in the cathode return of the

transformer. The 12AX7 on the other hand consumes but a few mA, thus one gets a bonus of being able to use a much smaller mains transformer, less complex circuitry, and fewer components. There has, to date, been no sign of t.v.i. at any time with the prototype.

The input circuit is intended for a crystal mike and although the input impedance is not matched, the $500k\Omega$ pot. VR4 being an abnormally low value for a crystal mike, there is sufficient gain and the speech quality is quite good. The 100pF capacitor across the mike input is included to avoid the BBC being re-radiated due to the mike lead acting as an aerial. The $500k\Omega$ audio gain control is really a luxury, as once set for a particular mike it requires very little adjustment, thus a fixed resistor

could be substituted if desired. The value will depend on the particular mike used, but around $330k\Omega$ would be a good starting point for most crystal mikes.

The modulator receives its h.t. supply whenever

In the prototype design the place now occupied by the crystal held two 85A2 stabiliser valves wired in series to provide 85 volts stabilised to the v.f.o. and buffer screen, and 170 volts stabilised to the buffer anode. The v.f.o. tuned 900kc/s-1Mc/s,

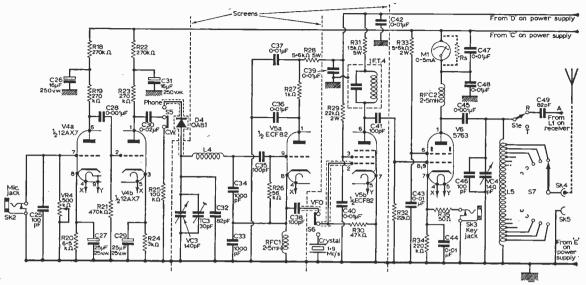


Fig. 2: Circuit of the transmitter and modulator sections. Note complete screening of the modulator diode.

the T/R switch S1c is in the transmit position, but it is not coupled to the transmitter until the phone c.w. switch S5 is depressed.

Although the p.a. tuning capacitor and the modulator section are in the same compartment and are not screened from each other, there is no interaction nor any trace of feedback.

Power Supply Circuitry

This scarcely needs any comment since it boasts well proven circuitry with little originality, consisting of standard full-wave rectification with choke or capacity input.

and its anode load consisted of a 1.6Mc/s i.f.t. modified to form a wide-band coupler. The buffer anode also had one of these and the system worked extremely well. However once the p.a. was brought in, there was so much r.f. in so small a space that the p.a. just could not be tamed. Those who prefer this arrangement might consider using a slightly larger case to allow better screening and improved layout. The stability of the present v.f.o. tuning 1.8-2.0Mc/s was found quite adequate without any stabilisation, thus the 85A2's were omitted.

The two neons in the power unit illuminate to show immediately on the front panel whether the station is on transmit or receive. For those build-

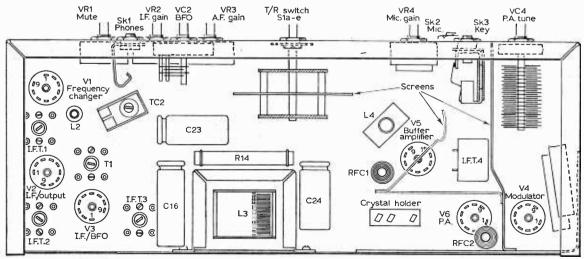


Fig. 3: Under chassis view showing positioning of main components and screens.

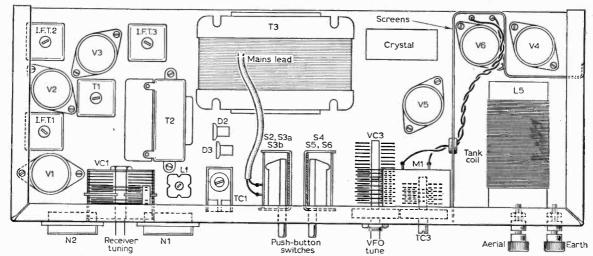


Fig. 4: Layout of the main components above chassis. Smaller items omitted for clarity

ing the rig, a fuse from the mains transformer centre tap to earth is strongly recommended, perhaps on the front panel in place of the variable mute control or the mike gain pot. VR4.

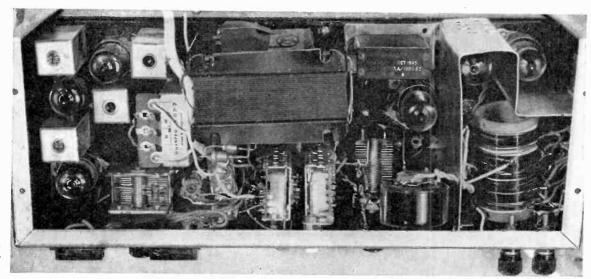
None of the components in the power section are unduly critical, for example any choke that will fit in will suffice from 8-20H providing it is capable of passing some 70mA. A 60mA component might tend to run a little warm.

It is not advisable to use a larger value electrolytic for C24, $16\mu F$ being considered rather high by some and $8\mu F$ is perhaps a safer value. It will be noted that on receive the power unit uses choke input, whereas on transmit, capacitor input is used by switching in C24 via S1b on the T/R switch in order to obtain a higher h.t. voltage. This is optional and if preferred choke input can be successfully employed on both functions. In addition to switching the neons the T/R switch also provides h.t. to the p.a. and modulator via S1c, and

h.t. to the v.f.o./b.a. via S1d. When the T/R switch is in the receive position, the Net switch, when depressed, supplies h.t. to the v.f.o. and buffer stages. This allows the operator to zero beat the v.f.o. with an incoming signal on the receiver without radiating a note which could annoy others. (V.F.O. swishers please note.) This facility also allows the crystal oscillator to be used to line up the receiver dial. Also, if the transmitter is now zero beat with the note from the crystal oscillator, it is possible to line up the transmitter dial at the same time.

Next month, the layout and constructional details will be given, and would-be constructors are urged to wait for these before attempting construction as certain snags could arise which can be avoided if they are known in advance.

to be continued



Photograph of the top chassis. Compare this with Fig. 4 above. Receiver section is on the left, transmitter and modulator on the right, power supply in the centre,

BALANCE CONTROLS

for stereo amplifiers

By J. B. Willmott

DDING a stereo balance control unit to a hi-fi installation often improves the end product. It is not readily appreciated that a pair of amplifiers of the same make and type do not necessarily have the same gain characteristics. Nor, for that matter, do the other links in the chain (such as loud-speakers, preamplifiers, microphones, etc.) of the same make and type always match up. In order to overcome this difficulty, one can adjust the individual controls of the main amplifiers, but this is retained a clumsy way of doing things when it is relatively simple to add a balance control which will increase the gain of one amplifier and at the same time reduce the gain of the other.

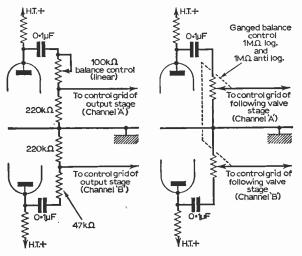
Nine different circuits are touched upon in this article. This is by no means all, but should fire the imagination of the serious constructor and give

the novice a good insight.

Before considering the various circuits, one must also appreciate that environment is important. Most hi-fi installations are accommodated in rooms that are not acoustically perfect, and the positioning of the loudspeakers in relation to the furnishings can have a marked effect on the end product. Also it is worth considering your own hearing; possibly that is not perfectly balanced. So to obtain the best results, why not let your ears be the judge?

SUGGESTED CIRCUITS

Possibly the simplest system of all is that shown in Fig. 1, in which the the gain of channel "A" is made variable by the insertion of a $100 \mathrm{k}\Omega$ potentiometer, in place of the $47 \mathrm{k}\Omega$ fixed resistor used in the same position in channel "B". However, it may be found that there is insufficient variation of gain of channel "A" to achieve balance under certain conditions. In Fig. 2 use is made of a twin-gang potentiometer wired up so



that channels "A" and "B" are controlled in reverse (i.e., as the gain of one channel is increased, that of the other is correspondingly decreased). This, however, requires the use of a specially designed twin potentiometer, known as "log./anti-log."; obtainable from most component suppliers. The advantage of this system is that either channel can be reduced to "zero" (with a corresponding rise to maximum gain in the other channel) so that even the most widely differing output requirements can be met, the only drawback is that at no setting of the control can both channels be working at full gain simultaneously.

Figure 3 depicts a very simple but effective interstage control of balance, in which only a single linear law $1M\Omega$ potentiometer is used. The slider of this control is connected to earth (chassis) line, and the control grids of the following valve stages

are fed from the "top" and "bottom" of this same potentiometer. Note the inclusion of $47k\Omega$ resistors in the grid leads to each of the subsequent valves. These should be connected as close as possible to the valveholder grid tag; the components serve as grid stoppers (reducing the danger of instability) and prevent the control grid of the succeeding valve from being connected directly to chassis (and thus cutting off grid bias) should the

(and thus cutting off grid bias) should the balance control be adjusted to the limit of its setting in either direction. Component values of the cathode bias resistor and capacitor are not shown, as these will depend on the type of valve employed in the output stages. With the popular EL84,

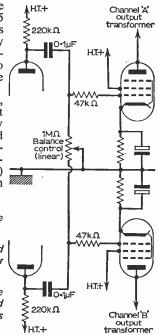
suitable values would be 150Ω and $25\mu\text{F}$ (25 VW). The previous valve stage can be any high or medium impedance triode (or the two halves of a double triode such as an ECC83).

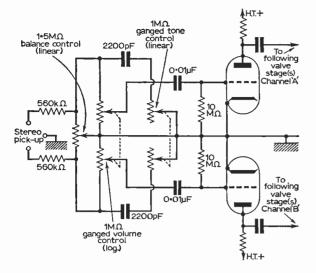
By way of a change, Fig. 3 shows a circuit for incorporation directly across the pick-up, and for sake of completeness, the associated volume and tone (top cut) controls are included in

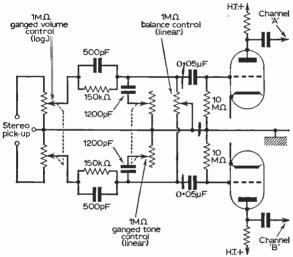
Fig. 1 (far left): Simple form of balance control.

Fig. 2 (near left): A ganged log./anti-log. potentiometer is needed for this circuit.

Fig. 3 (right): A single linear potentiometer is used in this circuit to vary the bias to the p.a. valves.







the circuit diagram. The system would be ideally suited to a simple inexpensive two stage amplifier. Note that the grid bias for the first valve stage is provided by the voltage resulting from the minute grid current flow through the high value grid leak resistor ($10M\Omega$). No cathode bias components are then required for this stage, and this system works very well indeed in stages where the signal level is quite low. The component values suggested have been used by the author in an amplifier fed from a crystal pick-up in a B.S.R. "Monarch" autochanger unit, and should suit any of the popular crystal pick-ups in the modest price range.

A further circuit suitable for insertion directly across the pick-up is shown in Fig. 4. In this circuit, the tone controls, either a simple "top cut" or more elaborate separate Bass and Treble, would be incorporated in the coupling between the valve stage shown and that following.

As in the previous circuit, bias for the first valve is obtained through a high value grid leak resistor. The component values of the anode load resistors and coupling capacitors to the following stage are not given, as these will vary according to the type of valve employed. Practically any

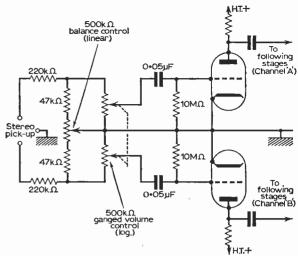


Fig. 4 (top left): Tone and volume controls are inclu-HIT ded in this circuit which μF balances the signals at 0•1µF the pick-up. To control grid of following Fig. 5 (top right): Another circuit in which the signals \$470 kΩ (Channel A) are balanced before being 100kΩ amplified. balance control (linear) Fig. 6 (lower left): In this circuit the tone and volume controls are also ÅH.T.+ directly connected across 470kΩ 0•1 uF the pick-up. Fig. 7 (lower right): Part

triode or pentode valve can be used, but for convenience, the use of one half of a double triode (such as an ECC83 or 6SL7) in each channel is recommended.

of the signal is shunted

through the h.t. rail to

achieve balance.

Another design eminently suitable for two stage audio amplifiers is shown in Fig. 6. In this arrangement the volume and "top-cut" tone controls are connected directly across the pick-up (which with the component values suggested, should be of the high output crystal type referred to earlier), followed by the balance control, which is a $1M\Omega$ linear potentiometer. The 500 pF capacitor paralleled by a $150 k\Omega$ resistor (in between the volume control slider and the coupling to the grid of the first valve in each channel) are inserted to provide a degree of frequency correction from the pick-up.

Figure 7 and the following two circuits, represent a less conventional approach to the control of balance. In the first circuit, the $0.1\mu F$ capacitor connected to the slider of the balance control $(100k\Omega \text{ linear})$, shunts a proportion of the audio signal away from the following stage to the h.t. line, and eventually via the power supply smoothing capacitor, to "earth". The proportion of signal so by-passed depends on the position of the balance control slider; movement of this decreases the signal passed on from channel "A", for example, at the same time as increasing that passed on from channel "B", or vice versa. Whereas all the

To control grid of following stage (Channel'B')

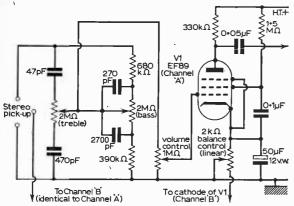


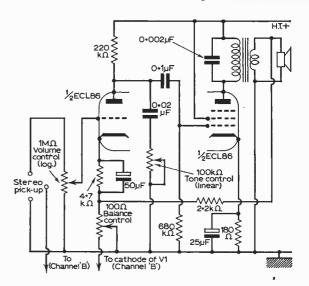
Fig. 8 (above): This circuit shows how it is possible to vary gain using vari-mu valves.

Fig. 9 (right): The level of negative feedback is varied to achieve balance in this circuit.

Note: The Channel 'B' circuits to match those given in Figs. 8 and 9 are identical, with the volume and tone controls ganged with those of Channel 'A'.

previous circuits have made use of potentiometers varying the signal strength fed between one valve and the next, or between pick-up and first amplifier valve stage, Fig. 8 shows how it is possible to vary the gain of an amplifier with vari-mu valves. This is, of course, common practice in r.f. and i.f. circuitry in radio receivers; it is not always realised that vari-mu valves can, in certain circumstances, be used in audio frequency circuits. The main proviso is that the signal level should be fairly low, as any attempt to deal with large swings of signal voltage in a vari-mu valve will introduce an intolerable level of distortion. However, if such a valve is used at low signal level, quite satisfactory control of gain can be secured by varying the grid bias. In the example shown, the author used EF89 valves, with very satisfactory results. Bass, treble and volume controls are shown and the circuit will give all the necessary controls for an inexpensive stereo amplifier. A valve such as the popular EL84 could follow the EF89's in each channel, and would provide some 4 watts output. The actual control of balance is provided by the $2k\Omega$ linear wirewound potentiometer, which should have a rating of about 5 watts. The slider is connected to chassis, and variation of its setting will vary the bias between wide limits. One word of warning, operation of the amplifier with the balance control set at the extreme ends of its track will leave one valve with zero bias, and if operated for any length of time in this position, will damage the valve. This can be avoided, if thought necessary, by inserting a fixed value resistor of say 100Ω between each valve cathode and the balance control.

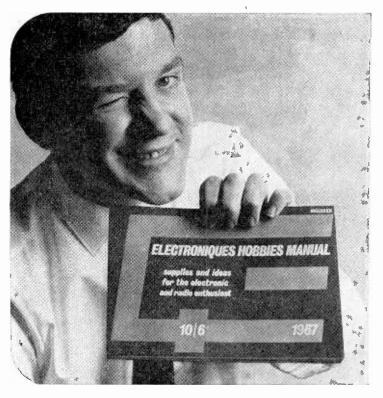
There is another method of varying the gain of an amplifier, Fig. 9, and that is by adjusting the amount of negative feedback. In the example shown, the balance control is a 100Ω wirewound potentiometer inserted between the junction of the negative feedback line (the $2.2k\Omega$ resistor from output transformer secondary to the lower end of the cathode bias resistor of the first valve stage) and chassis. Variation in the setting of this control

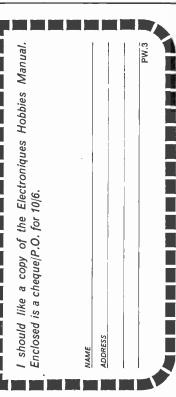


changes the amount of negative feedback applied; it will be seen that both channels are controlled simultaneously, but in an inverse manner, i.e., increased feedback in channel "A" would be accompanied by simultaneous decreased feedback in channel "B", and vice versa. The purist will no doubt exclaim that variation in negative feedback not only varies the gain of an amplifier, but also affects the frequency response; a greater degree of feedback giving a better low frequency response, so that relative volume levels will be controlled. This does not appear to have any serious effect in practice, at any rate in amplifiers in the inexpensive class. Indeed a system similar to this has been used by a number of commercial manufacturers of stereograms. The circuit diagram represents one complete channel of a stereo amplifier, using the two halves of an ECL86 valve; the second channel is identical, and only a power supply is needed to complete the equipment. As in all circuits using negative feedback, it is important to ensure that the feedback is correctly phased, otherwise positive feedback, resulting in uncontrollable oscillation, will result. The amplifier should be first constructed with the connections to the secondary of the output transformer (other than the speaker speech coil of course) omitted, and once tested and found to be working satisfactorily, the earth and feedback connections can be made temporarily to the output transformer secondary. If an uncontrollable howling results, the connections to the output transformer should be reversed.

One word of warning, the control potentiometers used should be of first class manufacture, and in the case of "ganged" components, must be properly matched during manufacture. Cheap surplus, or salvaged, potentiometers just will not do; they will lead to more annoying intermittent faults and noisy operation and can ruin the enjoyment of reproduction from an otherwise impeccable amplifier system.

Finally, don't let your enthusiasm for straining your ears to hear every grain of "movement" hamper your enjoyment of listening to stereo recordings. Get your tone and balance controls adjusted to your liking, and then leave them well alone.



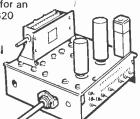


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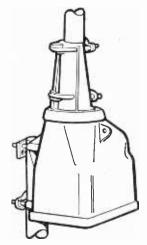
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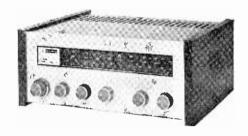
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MONTHLY NEWS FOR DX LISTENERS

THE BROADCAST BANDS

GUTTRIDGE JOHN bν

EUROPE

ENMARK: Radio Denmark (Shortwave Department, Radio House, Copenhagen V) now transmits on 15,165 to South America in Danish at 1600-1645 and Spanish at 1645-1715.

German Federal Republic: Deutsche Welle (Bruederstrasse 1, Postfach 344, 5 Köln) has made changes recently:—the following English transmissions: 0300-0345 7,160/9.530; 1550-1630 11,765/9,535; 0130-0250 9,735.

German Democratic Republic: Radio Berlin International (116 Berlin Nalepastrasse 18-50) now uses 1,430 / 6,080 / 6,115 / 7,185 / 7,300 for the 2200-2230 English transmission.

Radio Volga (Menzelstrasse 5, Potsdam) is now using shortwave as well as the 263 long wave outlet. Has

been heard in Russia in evening on 9,680.

Italy: R.A.I. (Via del Babuino 9, Rome) now uses following outlets for English transmissions: 2115-2135 (Europe) 7,240/6,050; 2205-2225 9,710/6,010; 2020-2040 7,265/5,990; 0100-0120 9,630/6,010. New languages introduced are Maltese 1225-1230 on 9,575/7,235 and Amharic 2020-2040 15,150/11,810/9,570.

Norway: Radio Norway (Oslo) now using two Schedule is 0300-0430 9,550/9,610/ 11 m.b. outlets. 11,850/1,578; 0700-0830 21,670/11,850/9,610/17,825/ 25,900; 1100-1230 9,610/11,850/21,730/25,730/25,900; 1300-1430 21,670/21,630/17,825/25,730/25,900; 1500-1630 21,670/15,175/17,825/25,730/21,730; 1700-1830 21,670/15,175/17,825/11,850; 1900-2030 11,850/15,175/ 9,610/21,670/21,730; 2100-2230 11,850/9,610/11,735; 2300-0030 11,850/9,550/9,610.

Poland: Radio Warsaw (Al Niepodleglosci 75/77, Warsaw) now transmits in English as follows: To Europe 1830-1857 7,145/6,135; 1930-2000 9,540/7,145/6,135/1,502; 2030-2100 7,125/5,950; 2130-2155 7,145/6,135; 2230-2300 5,950/9,540/1,502; 2303-2330 818; To Africa 1200-1230 and 1300-1330 7,145/11,840/ 15,275; to Australasia 0730-0800 and 0830-0900 9,675/ 11,840/15,275.

Rumania: Radio Bucharest (P.O.B. III, Bucharest) now has six new QSL cards which may be obtained by sending six reception reports numbered one to six.

Sweden: Radio Sweden (Box 955, Stockholm 1) has completely revised English schedule which includes use of 13 m.b. for first time. Times and frequencies are 0900-0930 6,065/21,690; 1100-1130 6,065/9,705; 1230-1300 9,705/21,690; 1400-1420 11,810/17,840; 1600-1630 11,705/17,840; 1900-1930 6,065/11,705; 2245-2315 7,270 11,705; 0030-0100, 0200-0230, 0330-0400 5,990; 0515-0545 11,705; 2015-2045 6,065/11,705; 2330-2400 1,178.

U.S.S.R.: Radio Moscow. There is a new service entitled "Radio Station Peace and Progress, the Voice of Soviet Opinion". Programmes are English 0900-1000 and French 1000-1030 on 12,060/15,200/15,360/15,450/ 17,710/17,795.

Radio Minsk (Minsk) may be heard in Bielorussian from 2130-2200 on 5,940.

Yugoslavia: Radio Belgrade (2 Hilendrarska, Belgrade) now using 6,100/7,200 only for the 1830-1900 English transmission.

AFRICA

Cape Verde Islands: Radio Clube de Cabo Verde (Casilla Postale 26, Praia) gives good reception on 3,883 in Portuguese 2000-2200.

Ethiopia: Radio Voice of the Gospel (P.O. Box 654, Addis Ababa) has changed the following English transmissions recently: 1345-1400 15,315; 1900-1910 9,705; 0430-0455 11,810; 0530-0555 11,785; 1655-1710 6,065; 1900-1945 15,115; 1630-1645 11,925; 1755-1810 9,565.

Morocco: Radiodiffusion Television Marocaine (1 Piere Paient, Rabat) now transmits English at 1800-1900 over 15,408.

Voice of America relay, Tangier (Washington 25, D.C., U.S.A.) now using the new outlet of 9,660 to Eastern Europe.

Nigeria: Nigerian Broadcasting Corporation (Broadcasting House, Lagos) now carrying foreign service from 1300-2200 over 7,275/9,690/11,900. English is at 1500-1600, 1700-1900, and 2100-2200.

Rwanda: La Voix de l'Iem Fé (Kigali) broadcasts from 2000-2200 over 9,575/11,715 in French.

South Africa: Radio South Africa (P.O. Box 8606, Johannesburg) has replaced 15,205 by 15,215 for the 2200-2255 European English transmission. frequencies are 9,720/11,785.

Tanzania: Radio Tanzania (Box 9191 Dar es Salaam). Test transmissions over a 240kW transmitter have been reported as follows 0930-1000 21,600; 1000-1300 15,435; Reports are wanted. It is believed a 1530-1600. regular service may now be in operation.

Saudi Arabia: Saudi Arabian Broadcasting (Ministry of Information, Airport Road, Jeddah) is now using 9,670 after the scheduled 2100 close down time.

Ceylon: Radio Ceylon (Department of Broadcasting, P.O. Box 574, Colombo 7) broadcasts in its External Service as follows: 0700-0815 to Europe, West Africa and Middle East on 15,330; 0915-1030 to South Asia The station is considering changing the on 17.850. times of its broadcasts and would appreciate listeners' views. QSL cards for the station commercial service may be obtained from Radio Advertising Services (Radio Ceylon) Cecil Court, Lansdowne Road, Bombay, India.

News was received this month from J. D. Ashworth, T. Ibbitson, D. Hobro, S. L. Brunt, A. B. Thompson, World Communications Club of G.B., P, Quin, International Short Wave Club, J. N. Newport, Radio New York Worldwide, Swiss Broadcasting Corporation W. E. Bartlett J. W. Smith S. Ormerod.

NE puzzling question posed to experts and laymen alike is "Where do all the flies go in the wintertime?". Variations on a theme now prompt me to enquire "Where do all the s.w.l.'s go at Christmas?". Either nobody listened, or else you've all gone shy and are not going to confess to Auntie Dave what you got up to in the festive season. Only a handful of letters in the postbag this month (sobs quietly into dirty hanky), so let's hope you are all saving those lovely logs for next month.

Top band has been surprisingly good at times and GDX has been about at quite good signal strength. GM stations and the North and Midlands have been heard near London at 5 and 6 on a.m. phone. Topband addicts might be interested to hear that G31DG is now mobile /M on 160 and many Northern stations have been received on the loaded

whip.

Frank Videan (St Albans) AR88, long wire, listened on 160 in the wee small hours. His log for the period 0103-0630 however is certainly neither wee nor small—DJ4SS, HB9CM, OK2KHF, OL9-KRA, PAØPN, VP6TK, W1HGT, W1BTK, W8A-NO, ZD8J, 9H1AE. Who said 160 has had it? When one considers that these stations were received through fish-phone, Loran, v.f.o. swishers and all the other noise on 160, it's a very fine effort indeed.

Mc/s Mixture

Often an s.w.l. will send in a log for several bands, and in order to get in as many logs as possible I usually take one or perhaps two bands from each report. This month however, I thought I'd put in the complete log, just to show how serious-

ly and diligently some s.w.l.'s listen.

Robert Iball (Notts), AR88D, 80ft. top and 35ft. of 72Ω co-ax feeder running S/N. Bob skimmed just the cream from his logs and offers—1·8 Mc/s—K8CRJ, K8HKB, K8RRH, K9PAW, OE5KE, VE3-BWY, VO1FB, W1BHQ, W1HGT, W1WY, W2FYT, WA8EMJ, W8GDQ, W8HGW. 3·5Mc/s—VE2BZL, W4YWX, W8JMC, W9BGX, YV2GC. 14Mc/s—KL7EB, LA2NK/MM, TN8AA, VE5US, VE8BB, VP9FK, VP9DH, YV5ALK, 5Z4SS. 28Mc/s—CR-7CZ, CX2CO, H18XAL, HKØAL, KP4CQZ, KZ5-TW, LA2MA/MM, UA9EU, UA9WJ, VK5DS, VK7SM, 4X4DH, VS9AJC.

N. Henbrey (Sussex), EA12, 20 metre dipole at 25ft. Offers a five-band log starting with 80—HI8X-AL, K2DXV, K2ISP, K2RBT, K8YWG, UAØBP, VE1ABZ, VE2KC, VE3XK, VO1FX, VO2AW, VS-9AJC, W1FZJ/KP4, W3BMS, W4GFW, YV5BTS. 40—CN8AW, EP2BV, IS1DMN, K5HWA, PY6WA, PY7KOG, UA9BE, UW9AF, VK2AVA, VP2AA, VP6KL, W3BMS, W4AZK, ZD8ARP, 5A3TW, 5N2AAS, 9H1AL, 9H1AM, 9X5MH. 20—CE6EZ, CR5SP, HP9FC/MM, KR6CO, KL7EBK, OD5AR, U5ARTEK, UA9YO, ZP3AB, ZS3XG, ZD8L, 3A-2CQ. 15—K2UTC, K3TGS, K4DI, K8RHK, K9HCG, MP4BBA, UF6FE, UL7JA, VE1AIT, VE2BDT, VE3FJZ/SU, VP5RB, WA1FDU, W5PMZ, YA1FV, ZS4MZ. 10—FH8CD, OD5CN, VE3-WQ, VK6CF, ZC4CI, ZC4CN, ZC4RM, ZE5JS, 4U1SU.

J. Farrer (Herts), HMV domestic receiver, 90ft.

l.w. says W6 and W7 are now breaking through on 28Mc/s, while down the other end John remarks on the increase in s.s.b. stations on topband. His log for 3·5Mc/s reads—CN8AW, CTIEE, DJ1SU, EA-2FF, EI4J, F2MO, HI8XAL, K3UZE, K4YGU, K8YWG/P (using 50 watts), LA2PM/MM, MP4T-BO, OZ1SF, SV2MB, UA3TN, UC2LVK,UP2OJ, UR2REK, VE1AIJ, VE2AUU, VE3DMU, VO1FG, VS9AJC, W1DRS, W2ZPO, W3AQH, W4RNG, W4UHA/P, ZL1BDW, ZL3AKJ, ZL3JC, ZL3RK, ZL4KE, ZL4OD, 4X4OV.

Higher up

I did wonder, some little while ago, if 14 and 21 were dying or losing their popularity. Not so, as

some logs prove a different story.

Paul Baker (Mon.) HE30, 45ft. l.w. sends in a log for 14 and 21 of stations heard at various hours. 20—FB8YY, HL9TH, HS4AK, UAØEH, VK9AG, VP8CW, VS9OC, YK1AA, 4S7PB. 15—CO8RA, CR3KD, CR4BC, FL8RA, KL7CSR, KV4CX. MP4BBA, OH2BBF/MM, PX1PA, ST2SA, TF2WK, VEØMB, K4OMM, VK9XI, W7ETD, YA5RG, ZL1AFN, ZL2AJV, ZL2KP, 5N2AAR, 6Y5RS, 7XØWW, 9M2DQ. Paul reckons to hear Australia, New Zealand and Japan on 15 metres between 0830—0930 and very often from 1200—1500 during a second opening.

J. Dunnett (Singapore), Racal 17, 7Mc/s dipole at 70ft. for all bands writes in with a report on 14 and 21Mc/s from way out East. All that lovely sunshine and he has to pinch my best DX too! On 14 c.w. Jim logged—EA8FG, EA9EO, FK8AH. FM7-WP, MP4MAW, VP6PJ, ZD8J, 5R8AW, 6W8CQ. While on 14 s.s.b.—CN8CB, CT2YA, CT3AU, G5A-AV/K5ZKN, KJ6BZ, KG6IJ, KL7FRY. KW6EG, U5ARTEK, VK9XI (Christmas Is.), 3W8AD, 7Q-7EC, 9Y4AR. On 21Mc/s c.w.—HP1RP, PZ1BX, VS6FS, 5N2AAW, 5Z4JW, 9G1RW. With a b.f.o. in, s.s.b. stations heard were CR7AN, CT3AU, GB3MM, VK9CJ, (Papua), 6O6BW, 9M1AF. Jim says "We also hear lots and lots of G's here".

Mumblings

News and natterings from here and there. First, for those trying to brush up their c.w. The RSGB organise slow c.w. most evenings on topband. The ARRL station has set sessions on most bands most days and does a special run at up to 35 w.p.m. for those who really reckon they can take c.w. Ten metres, still going strong. An interesting letter from Barry Tew (G8AVW). Barry says he tuned his CR150 down below 28 and heard American Citizens Band Stations between 27 and 28Mc/s. He thinks these stations are restricted to 5 watts and a 60 inch antenna. Anyone else heard anything? Mind you don't pick up 28Mc/s image if it's a single conversion superhet. Contests for the chilly 4 weeks called February: 4th.-5th., ARRL phone contest; 12th., First 70Mc/s contest; 18th.—19th., First 1.8Mc/s c.w. contest; 18th.—19th., ARRL c.w. contest; March 4th.—5th., Second 2 metre contest. The deadline for reports this month is the 20th. How about an epistle from you?

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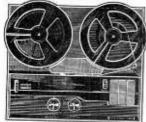
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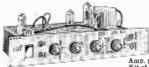
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TENSILIZED POLYESTER			
3½in. 600ft. Double Play	 	11	6
5in. 1,200ft. Double Play	 	15	0
5½in. 1,800ft. Double Play	 	22	6
57in. 2,400ft. Triple Play	 	37	6
7in. 2,400ft. Double Play	 	25	0
7in. 3,600ft. Triple Play	 	50	0
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practically wireless HENRY commentary by

To Kit Or Not

E began this series—so long ago, it seems-with a passing glance at the kitmaker. From time to time we have taken a harder look. Now, with the glittering commercial confections of the Radio Show behind us, and our corns beginning to heal, we may return to glare more closely at the subject. Recently, the need arose for an inexpensive portable amplifier. Inexpensive, for Henry's relations all appear to be touchingly impecunious. Portable, because the thing had to be lugged around the country as an aid to illustrated lectures.

Obviously, a transistorised version was called for. Equally obviously, the various commercial products had to be ruled out—first because their prices indicated the parts were at least gold-plated, and second because no manufacturer considered that mono production was worthwhile. The answer—build it yourself.

But the particular kit that seemed appropriate for the purpose, and remarkably cheap, was from a firm a little less illustrious. A preliminary (unofficial) glance



An old Caxtonian duplicator

at the circuit showed it to come from a fairly trustworthy stable. The advertisement showed an attractive finished job. So Henry showed his money and plunged . . . up to his top-knot in trouble!

The kit came in a tatty cardboard box, each piece wrapped in a screw of crumpled paper. Careless unpacking could easily have whittled away half the contents. But the greatest disappointment was the literature that pretended to be a guide to construction.

Apparently run off by a shell-shocked operator of an old Caxtonian duplicator, on Government surplus blotting paper, pinned in a Chinese order of page numbering, it should have deterred us from the start.

Between us we managed to make some sense of the hieroglyph and laid out the parts for checking against the list. (My typewriter nearly wrote 'lost'—and it would have been more appropriate.) Several components were missing, and remained so, despite a ferreting amidst the packing. Others had been substituted, which only became confirmed as we ploughed through the barely legible text. We made up the missing quantity-secretly commiserating with some innocent not blessed with a pretty full spares box. Then we amended the given list, if only for the sake of posterity.

The actual building was not too bad, provided one already had a fair knowledge of the techniques. The absolute beginner, despite what the advertisements claimed, would have been bogged down before the third page. The selector switch was physically different from the diagram, and connections had to be worked out. One or two unexplained wires appeared, and the proiected colour coding could not be followed because different lengths of different colours had been included. Again, no obstacle to the experienced, but . . .

We shall skate mercifully over some other points—vital paxolin spacers missing; too many nuts of one size, not enough of another; an extra switch on the



The thing refused to work

diagram, not mentioned in the text; no flats on the control spindles; no spigot holes drilled, and chassis holes out of alignment. And, incidentally, no solder!

The important point was that the thing refused, pointblank, to work. At this stage, the novice slings it back to his supplier and pays the fee he could have laid out before his hair went grey, to have his pet rebuilt. We reverted to first principles and cast aside the instructions, checked the diagram against the original design in an old technical magazine, made due allowances for the alterations that had obviously been done more with a view to economy than efficiency, and eventually got results.

An unlucky case? Maybe, but we would like to hear of other experiences. We would even like to see a Constructors' Guide to Kits. Henry reckons he knows which firms would top the list as 'Best Buys'.



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IMPROVING THE NOTE IN THE NOTE

C. MOLLOY

LMOST twenty years have gone by since the first R1155 communications and direction finding receiver became available to the public through the surplus market. Since that time a lot of useful information has been published on this R.A.F. aircraft h.f. receiver in the technical journals, but often in issues that are now out of print. This article does not include a complete circuit diagram, but gives general information plus details of improvements that the author has made to his own receiver.

The standard model covers the range 75kc/s to 18.5Mc/s in '5 bands, with a gap from 500kc/s to 600kc/s and another from 1.5Mc/s to 3.0Mc/s. A second, less common version, designated L or N, omits the lowest range, 75kc/s to 200kc/s, but covers the Trawler Band, 1.5Mc/s to 3.0Mc/s. The two types are otherwise identical, having a single r.f. stage, mixer, two i.f. stages, a b.f.o. and a triode output stage feeding high impedance phones. An external power unit is used.

REMOVAL OF D.F. COMPONENTS

As the R1155 is a dual purpose receiver, many of the d.f. components can be removed without affecting the performance of the communications section leaving space for additional items to be added and, incidentally, reducing the total power consumption. A circuit diagram of the R1155 together with notes, is available from an advertise-iser in Practical Wireless. From this the readers can locate the d.f. components and decide which of them he would like to remove. The associated valves are V1, V2 and V8 and these are shown in Fig. 1. The meter balance control, meter amplitude control, meter deflection switch, aural sense switch, and associated wiring also can be taken out, to give extra front panel space.

The job of removing the d.f. components should

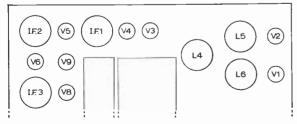


Fig. 1: Top view of the receiver showing position of the major components.

be tackled systematically, removing one item at a time and checking in each case that the receiver's performance is unaffected. If a mistake is made it should then be easy to pin point where it occurred. Care should be taken, especially at valve bases, not to break the continuity of the heater and h.t. lines.

DECOUPLING CAPACITORS

At this stage a check of all paper decoupling capacitors is advisable. There are two types, both of which are metal cased. Those mounted above the chassis are easily found, being cylindrical (3in. diameter, 3in. high) and secured to the chassis by a large nut. Age may have brought about leakage and an easy method of checking is to use a voltmeter set to a range suitable to measure the h.t. supply. Connect the meter positive lead to the receiver's h.t. positive line and the negative to the capacitor to be tested after electrically removing it from the h.t. line. A good capacitor will make the meter needle kick and then return to zero; this is caused by the charging current flowing into the capacitor. A faulty capacitor will either give a steady reading or the needle will gradually fall to a low value. Any faulty capacitors should, of course, be replaced. The lot had to be changed on the author's receiver (using modern components of the same value).

A number of smaller cylindrical decouplers can be found in several places within the coil compartment. These seem to be less prone to leakage and can probably be left alone. But it is well worth checking all the paper decoupling capacitors, as a defective one can make a considerable difference to the performance of the receiver.

LINING UP

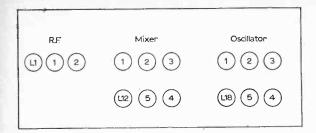
No difficulty should be experienced lining up the i.f. stages. Figure 1 shows the position of the three i.f. transformers and the dust cores are readily accessible through the screening cans. The i.f. frequency is 560kc/s.

Disconnect the top cap of the frequency changer valve V4 and apply 560kc/s to the valve from a signal generator. The magic eye can be used as a peaking indicator, but make sure the a.v.c. is inoperative by turning the master switch to either the OMNI or O position. Set the volume control to maximum (reducing signal generator output as necessary) and adjust the cores of each i.f. transformer in turn, starting at the last stage (number 3) and working towards the front end.

The r.f., mixer and oscillator circuits can be lined up on each band in turn by choosing alignment points near the ends of the bands and inject-



Fig. 2: Layout of the trimmers, viewed from the front of the receiver.



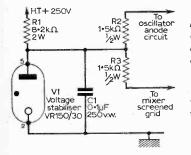


Fig. 3 (above): Side of the coil compartment viewed from front of the receiver.

Fig. 4 (left): Simple stabiliser, see text for details.

ing an appropriate signal to the aerial input. If a signal generator is not to hand tune to a broad-casting station of known frequency and use it instead. This is not really a satisfactory method owing to the difficulty of obtaining a steady signal, but at a pinch it will do. Switch off the a.v.c., turn the gain control to maximum and use the tuning indicator. The trimmers are adjusted at the h.f. end of the band and the dust cores at the other. It will not be necessary to touch the oscillator section unless the scale calibration is out of adjustment: often peaking the r.f. and mixer trimmers will suffice. The location of all trimmers is shown in Fig. 2. A 4BA box spanner will be required to adjust the majority of them. The layout of the coils is shown in Fig. 3. The cores can be adjusted without removing the cover of the coil compartment

L18 comprises 2 tuned chokes which assist in maintaining a constant oscillator voltage throughout ranges 1 and 2. They should not be adjusted.

L12 is an i.f. rejector and is connected to the mixer grid circuit on ranges 3 and 4. To adjust, inject 560kc/s to the r.f. circuits, then tune the receiver to the l.f. end of range 3 or the h.f. end of range 4 and adjust the core for minimum output. L1 is only used on d.f. and can be ignored.

L4, L5 and L6 are the r.f. coils for ranges 3, 4 and 5 respectively. These are located above the chassis inside large cylindrical cans (see Fig. 1) and the cores are accessible from the top.

AERIAL TRIMMER CONTROL

A simple but very useful addition to any receiver is an aerial trimmer. A small variable capacitor of 50pF will do, connected in parallel with the r.f. section of the main tuning capacitor. It is used to counteract any loading effect the aerial may have on the first tuned circuit. The capacitor can be mounted on the front panel in the space vacated by the meter deflection or aural sense switches. The moving vanes are connected to chassis and a short length of coaxial cable is run from the fixed vanes to the rear section of the main tuning capacitor; the cable braiding should be earthed. The r.f.

trimmers will now have to be re-adjusted on all bands and this is done with the aerial trimmer set to minimum capacitance (vanes out). The aerial trimmer is used to peak signals after they have been tuned in and the effect will be most apparent at the h.f. end of each band.

BANDSPREADING

Although the slow motion drive, especially the later type, is excellent, a bandspread control is a definite advantage on the higher frequencies. It can also be used for dial setting to counter the effects of oscillator drift on lower frequencies. Ideally, a twin-gang variable capacitor of about 20pF per section can be used, mounted below the chassis underneath the main tuning capacitor. One section should be connected in parallel with the oscillator (front section) and the other to the mixer (centre section) of the main tuning capacitor. The writer was unable to obtain a twin-gang capacitor of suitable dimensions and as two single variable capacitors were to hand, decided to use these instead. It was found advantageous to have two controls instead of one, though of course they were less convenient to use. After making this modification, the oscillator and mixer trimmers have to be repeaked and this should be done at the h.f. end of each band with the vanes of the band spread control fully open.

Care should be taken when drilling through the front panel as it is of double thickness at this point. Swarf may fall between the inner and outer sections and later find its way into other parts of the receiver. It is not too difficult to remove the outer panel including the scale cover, if the slow motion drive is taken off first.

VOLTAGE STABILISER

Frequency drift, especially on the higher frequencies, can be a nuisance and a considerable improvement can be obtained by stabilising the voltage at the oscillator anode. A type VR150/30 voltage stabiliser was used (Fig. 4 shows the connections). This stabiliser has an octal base and can be plugged into the valveholder previously used for V8. All the d.f. wiring should, of course, be removed from this valveholder including the heater supply. The $22k\Omega$ resistor (R28) in the oscillator anode circuit has to be replaced with a $1.5k\Omega$ ½ watt resistor. Resistor R28 is located inside the coil pack on a small tagboard which is mounted on the chassis at the left hand side as viewed from the rear of the receiver. One side of this resistor is connected to h.t. positive and the other side goes to a common lead which runs between L15, L16, L17 and L18. Remove the strap to the h.t. positive line and run a wire to pin 5 on the base of the stabiliser.

It was thought worthwhile to stabilise the voltage at the screened grid of the frequency changer too. Voltage changes on the screen grid can cause small changes to the oscillator frequency. Since the screen grid voltage can vary in sympathy with the a.v.c. voltage it is possible for some kinds of fading to produce variations in the oscillator frequency which will give rise to objectionable distortion. The majority of receivers do not apply a.v.c. to the mixer valve, probably for this reason. An obvious solution is to disconnect the mixer from the a.v.c.

line, however, the a.v.c. on the R1155 is very efficient and rather than disturb it, it was thought better to stabilise the screen grid voltage. Only one additional resistor is required to do this and it is shown in Fig. 4 connected between pin 5 of the stabiliser valve and pin 4 of V4. The two resistors connected to pin 4, a $22k\Omega$ and a $27k\Omega$, should be removed but the connection to the decoupler should be left.

R.F. GAIN CONTROL

The volume control on the R1155 is a little unusual as it consists of a twin-gang potentiometer. One section $(0.5 M\Omega)$ is an audio volume control while the other $(50 k\Omega)$ controls the gain of V3, V4, V5 and V6 by applying a steady controllable voltage to the a.v.c. line. When the master switch is in the a.v.c. position only the audio gain control is effective, V3 to V6 being controlled by the normal a.v.c. voltage. When the master switch is in the OMNI postition, the $0.5 M\Omega$ section is out of circuit allowing maximum audio gain. Also, the a.v.c. line is disconnected from the a.v.c. diode load and joined to the $50 k\Omega$ section which then forms part of a biasing network situated between h.t. negative and the chassis.

In short, when the a.v.c. is on, the receiver output is controlled manually by the audio gain control. When the a.v.c. is off, the audio gain is fixed and the combined r.f./i.f. gain control is effective. This is a sensible arrangement and is more or less how one woud use a receiver with separate r.f. and audio gain controls. There are occasions though when one wants to reduce only the r.f. gain to avoid overloading the frequency changer with a strong signal. However, to do this with the R1155,

the i.f. gain has to be reduced too.

A separate r.f. gain control will solve this problem and one can be installed quite easily by placing a 5kΩ potentiometer between the chassis and pin 8 of V3. The potentiometer can be fitted underneath the chassis so that the shaft projects through the front panel below and to the right of the main tuning capacitor, maintaining symmetry of control layout (including the two bandspread controls). Alternatively, the potentiometer can be fitted in one of the spaces along the top of the front panel which were previously occupied by d.f. components.

The left hand terminal of the potentiometer as viewed from the rear, is connected to chassis. The strap from V3 pin 8 to chassis is removed and a

R1 10kΩ i 1155 Input Output Tape 100Ω recorde Fig. 5 (top left): Simple R1 10kΩ attenuator. 1/2W Fig. 6 (top right): Germanium diode noise limiter. Fig. 7 (left): Silicon diode OAŽOZ limiter.

wire is run to the central terminal of the r.f. gain control. A 0·1µF decoupling capacitor must be connected from pin 8 to chassis and it is essential to connect this component direct to pin 8 and not to the centre terminal of the potentiometer, otherwise instability will occur.

TAPE OUTLET

The phones output from the R1155 is suitable for direct connection to a tape recorder. In a previous article a description was given of how to fit a front panel phones socket. Adjacent to this, a second socket can be fitted for use as a tape outlet. A $0.1\mu F$ 350VW capacitor was used to isolate the headphones from the input of the tape recorder and it was wired between the line terminals of the phones and tape socket, at the rear of the front panel. The second terminal of each socket was connected to the chassis which should be earthed.

An attenuator may be required for some recorders. Figure 5 shows a simple attenuator which, if it is required for permanent use, can be wired between the tape and phones socket.

NOISE LIMITER

A subject that is almost certain to start a discussion among radio enthusiasts is that of noise limiters. Many circuits have appeared: some are good, others not so good; the method of operation of some is simple, of others it is obscure; some operate on the i.f. stages of the receiver, others are used on the audio; some automatically adjust themselves to the signal level, others have to be set manually; and so on. Unfortunately there are snags of one sort or another connected with many noise limiters. To be effective, some of them have to be set so that they tend to clip the signal causing distortion, which may, of course, be acceptable. It is obviously better to have a partly distorted signal that is audible, than one which is lost in noise.

It was finally decided that a simple audio limiting circuit applied to the phones output of the R1155 would probably be as good as any. Figure 6 shows the circuit of a parallel type of audio limiter. Either valve or semiconductor diodes can be used but in each case the main drawback of this circuit is the same. The diodes have to be reverse-biased so that they will only conduct when the bias voltage is exceeded. If 1.5V dry cells are used, the limiter will not act until 3V peak-to-peak is applied to it, which is ample to drive a pair of headphones.

It is possible to throw away the biasing batteries and use silicon diodes in the noise limiter circuit; since these devices do not conduct in the forward direction until a forward bias is applied (the level of which varies according to type). Figure 7 gives details of such a circuit using 0A202 diodes. Germanium diodes were tried, but discarded as

they distorted the output.

The limiter is connected between the output transformer and the phones socket; it is convenient to mount the components at the rear of the socket itself. The effect of the limiter is immediately apparent, removing the usual clicks, bangs and static crashes. As the volume is turned up a point is reached where no further increase in output is obtained. Any further advance of the volume control only brings about distortion.

a two-transist 'ERSONAL POR

EFLEXING in this personal radio makes two transistors do the work of four. Often it is not easy to carry out successfully, but works reasonably well in this circuit, even over an output stage feeding an earpiece. The quality depends upon using a good earpiece and the type specified is Ardente ER250.

Alignment problems do not exist in a receiver that has only one tuned circuit. On the other hand, as it takes as many as four tuned circuits to suppress a powerful transmission and enable a weak signal to be heard, it is mainly a local station receiver. Reaction could be added to sharpen selectivity, but risks instability, and there is probably some r.f. feedback already. It is almost unavoidable when a t.r.f. circuit is put into miniature form, since the input and output of the r.f. amplifier are working at the same frequency, and are close

With a ferrite aerial, an r.f. amplifier is essential, because a detector can only respond effectively to strong signals. At low signal levels the detector is insensitive and produces increased distortion. A.F. amplification cannot, in general, make up for a lack

of r.f. amplification.

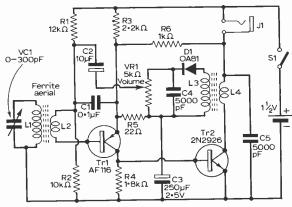


Fig. 1: Circuit diagram of the two-transistor radio.

A 1.5V battery is capable of providing all the volume needed in an earpiece. The low voltage, however, accentuates the non-uniformity of gain over the medium waves, and sensitivity decreases towards the high-frequency end. Improved sensitivity

and increased volume could have been obtained on a 3-volt supply, but this would have involved extensive modification. Most of the difficulties of a t.r.f. circuit would disappear if it were designed to recieve a single frequency like the i.f. amplifier of a superhet. Instead it has to be tunable over a wide frequency band, and conditions vary considerably over the tuning range. Here the circuit is aperiodic except for the input, although L3 with only 20 turns should assist in maintaining the r.f. gain at the high-frequency end.

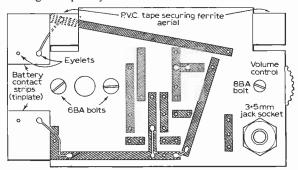


Fig. 2: Mounting board using "Cir-kit".

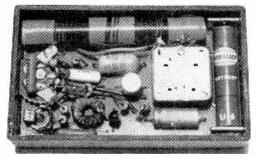
Tuning is effected by a 300pF miniature plastic dielectric capacitor across a 70 turn winding on the ferrite aerial, and this is coupled by a coil of five turns to the base-emitter input of Trl. The two transistors serve first as r.f. stages feeding the detector via a small step-up transformer, and then as a.f. stages amplifying the a.f. from the detector. The overall a.f. gain is about 40 times with negative feedback applied by means of R5 to reduce distortion in the output stage. A step-up ratio to the detector is possible because the detector is working at a rather low signal level at which its impedance is fairly high. Ideally there would be a further step-up to a tuned circuit, but this, though desirable, would involve the complication of ganged tuning.

R.F. TRANSFORMER

The r.f. transformer is wound on a $\frac{1}{2}$ in. ferrite ring because this has very little external field and avoids r.f. instability through magnetic feedback to the ferrite aerial. It is more compact than a ferrite pot core, and can be wound fairly easily. Very little of the a.f. at the collector of Tr2 can reach the detector via this transformer, although winding the coils L3 and L4 on separate rings coupled by a

BLE

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capacitor of about 200pF might be a better arrangement, and would still give a step-up to the detector. The r.f. at the collector of Tr2 is passed via the transformer to the detector, but after the modulation is extracted, it too must be filtered out, and only the resulting a.f. is passed back to the base of Tr1 so that the transistors can now function as a.f. amplifiers.

The success of reflexing depends upon this sequence of filtering, and r.f. current must also be kept out of the earpiece leads in order to prevent re-radiation and hand-capacity effects when tuning. This is the purpose of the bypass capacitor C5.

TRANSISTORS

A direct-coupled circuit requires fewer components, and a complementary arrangement of a p-n-p transistor followed by an n-p-n can take a form which does not require any adjustment. D.C. feedback to overcome drift is applied via R6 to the emitter of Tr1. The potential divider consisting of R1 in series with R2 provides a "reference voltage". The resistance R3 is necessary mainly because of the low supply voltage. D.C. stability would be somewhat better on a higher supply voltage, because the base-emitter potential drops of the transistors would be a smaller part of the total voltage.

A silicon transistor 2N2926 is deliberately chosen for Tr2 because of its large base-emitter drop. This permits a larger current in Tr1 for a given load resistance R4. The total current of the receiver is under 2mA and of this about one-third of a milliamp flows in Tr1. The first transistor could also be

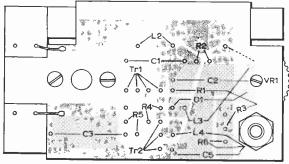


Fig. 3: Printed circuit as alternative to Fig. 2.

a silicon transistor, but of the p-n-p type, such as 2N3702. However it was found that the germanium r.f. transistor AF116 gave a larger output. Complementary circuitry can be confusing, and the lead

arrangements of the two transistors should be studied carefully before insertion into the circuit. The lead arrangements of the silicon and germanium transistors are depicted in Fig. 5 which also shows the positions of the corresponding holes in the mounting board.

The detector diode DI is connected with the red end towards the volume control. The polarities on the electrolytic capacitors should also be carefully observed, otherwise the circuit will stop working in a short time. The metal case of C2 is connected to the junction of R1 and R2, while that of C3 is connected to the negative side of the battery. The battery itself must be correctly inserted, although no damage appears to occur from an accidental reversal when the rest of the circuit is in order.

CONSTRUCTION

The components are assembled on a small mounting board of 1/e in. insulating material. "Cir-Kit" strip on the underside is an alternative to a printed circuit, although rather close spacing is involved. Holes for component leads are drilled with a No. 60 drill. Guide marks are then made

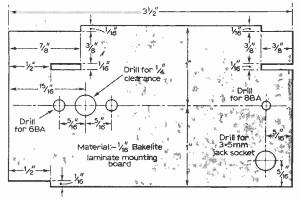


Fig. 4: Details of the mounting board.

with a scriber for the edges and ends of the strips. The "Cir-Kit" strip is cut to length, then the paper backing is prised off with the point of the scriber, holding the end of the strip with small forceps or tweezers. When all the strips have been pressed down in position, the mounting board is placed with the copper side downwards on a flat wooden surface, and the holes can then be drilled through the strips, smoothing them afterwards where necessary. Joins between adjacent strips can be made by soldering short pieces of 24s.w.g. tinned copper wire across them, and in one or two instances, gaps between the strips can be widened by cutting away some of the strip.

FERRITE AERIAL

The 3 x $\frac{3}{8}$ in. ferrite rod is a piece broken off from a longer rod. A method of doing so is to wind two turns of $\frac{1}{2}$ in. Sellotape tightly round at the point where the break is required. Place the rod on a hard surface and position a metal chisel at the edge of the Sellotape. A sharp tap with a hammer will usually produce a clean break at this point. The ferrite rod is then covered with p.v.c. tape and wound with 70 turns of 24s.w.g. enamelled wire. The ends of the wire are fixed with a strip of of p.v.c.

tape. A piece of the tape is then applied around the middle of the winding and the five-turn coupling is then wound on top. Owing to the shortness of the aerial the winding has to be in the middle for maximum signal. The ferrite aerial is fastened on to the

applied around the perimeter of the ring and folded inwards. It can be pushed into the centre from each side to cover the ring completely. The 40-turn winding requires 27in. of 36 s.w.g. wire. Double silk-covered may be used, but should be waxed

before winding since the wire has to be threaded through the core 40 times and this can impair the insulation. The 20-twin winding may consist of 15in. of 30s.w.g. wire.

Battery contacts may be formed by folding strips of tinplate to the shape shown in Fig. 6, and are attached underneath the mounting board by small eyelets. smallest eyelets obtainable are the type made for insertion in Veroboard, are thus suitable and material. In for $\frac{1}{16}$ in. assembly, the component leads are passed through respective bent over, clipped, and

for the inmaterial. In assembly, the component leads are passed through their respective holes, bent over, clipped, and soldered to the copper strips with printed circuit solder. Ease of construction is more important than the ultimate in compactness. Resistors stand vertically on the board. A heat shunt, e.g., the Antex type, can be used when soldering the transistors and diode. Special care is needed as the leads are made very short so that the transistors project no higher than the variable capacitor. Although it takes longer, the best method is perhaps to apply the soldering iron for a second

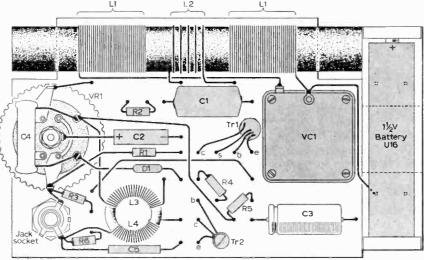


Fig. 5: Component arrangement above circuit board.

mounting board by strips of p.v.c. passed through slots in the board. It is raised above the surface by $\frac{1}{8}$ in. squares of the $\frac{1}{16}$ in. material cemented to the mounting board under the ends of the rod.

TUNING CAPACITOR

The round-head screws supplied with the 300pF Dilemin capacitor are too short for mounting on the $\frac{1}{16}$ in, material and can be replaced by similar 6BA screws $\frac{1}{4}$ in, long. The washers supplied are

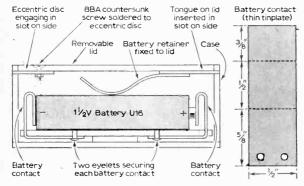


Fig. 6: Sectional elevation showing battery contacts.

placed between the capacitor and the board, as it requires to be raised slightly to clear a ridge around the tuning shaft. A check should be made on the length of the screws projecting through the board, as the capacitor will be damaged if these screw in too far. It should also be kept in mind that the end stops of the capacitor will be damaged if the shaft is turned beyond its normal range, especially as it is a little stiff to turn at first.

Before winding the two single-layer windings on the ferrite ring (type FX1593), ½in. Sellotape is

CABINET

adequate precautions.

The case is made from Rain. material glued at the edges with Bostik clear adhesive. A strip of leather-cloth is glued round the sides of the box and trimmed with scissors. A piece is glued over the top and trimmed neatly round the edge so that the join is almost imperceptible. The back, too, is covered with leathercloth, and is removable by giving a small screw half a turn with a screwdriver. The locking device consists of an eccentric disc which enters a slot in the side. The three slots required in the sides are made before assembly by drilling series of holes with a No. 60 drill. These can then be merged by inserting the tapered end of a nail file.

at a time, followed by an adequate cooling interval.

The high frequency performance of transistors seems often to be impaired by soldering without

There is an opening in the end of the case for the edge-type volume control, which also incorporates the on-off switch; and to enable the chassis of the receiver to drop into place, the hole in the case for the tuning shaft is elongated slightly. This can be done by using the ‡in. drill in the manner of a saw.

A combined tuning knob and dial is constructed from three discs as shown in Fig. 8, and is fixed on the shaft by a piece of wire through a hole drilled in

* components list

Resistors:	Capa	acitors:			
R1 12kΩ	C1	0·1μF 125V polyester			
R2 10kΩ	C2	10μF 15V electrolytic			
R3 2·2kΩ	C3	250μF 2.5V electrolytic			
R4 1·8kΩ	C4	5,000pF tubular ceramic			
R5 22Ω	C5	5,000pF tubular ceramic			
R6 1kΩ	VC1	300pF Jackson "Dilemin"			
Coils:					
L1 70 turns 24swg enam. wire					

L2 5 turns 24swg enam. wire | see text

L3 20 turns 30swg dsc wire

L4 40 turns 36swg dsc wire

Miscellaneous:

Earpiece, Ardente type ER250 with cord and 3.5 mm jack plug. Jack socket 3.5 mm. Ferrite rod. Ferrite ring core type FX1593. Battery, 1.5V type U16. Edgewise pot. (Volume and on/off switch) $5k\Omega$ with switch.

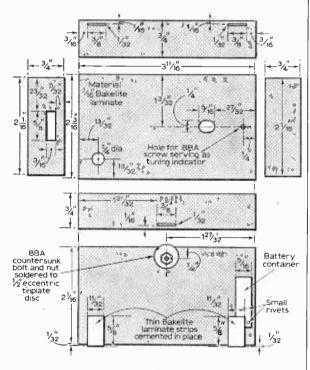
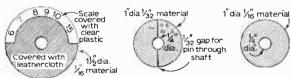


Fig. 7: Constructional details of the case.

Fig. 8: Individual parts for the tuning scale.



the shaft with the No. 60 drill. The knob is covered with leathercloth to match the case, except for the end of the shaft exposed in the centre for decorative effect. The scale round the edge is marked approximately in hundreds of kilocycles and is covered with clear plastic.

THE COLUMN

THIS month we will take a look at the Americas. The prolific stations of South America are usually best heard in the spring, when North America is less favourable. Some of the most consistent are PRG3 (1280kc/s), PRA3 (860); YVQO (650), HJED (820), LR4 (910), LR1 (1070), PRF4 (940), PRA2 (1040), ZFY (760).

Central America and the Carribean are usually more difficult to hear except for a few outstanding ones such as Radio Americas, Swan Island (1157, but frequency varies) and PJB Bonaire (800). Others to look for include CMBC Havana (690), CMCA (830), Jamaica (650), St. Lucia (840), Guadeloupe (640), ZBM1 Bermuda (1235—together with spurious pop pirate signal!), HOL55 (1315), TGRB (1120) TIRICA (625), PJD2 (1295), Belize (834) and the regular St. Pierre et Miquelon on 1375. A consistent one last season was XEW Mexico City, now suffering from splash from Milano; however it is often strong from 0500.

The east coast USA and Canadian stations, of course, can be heard very early in the evening when conditions are good, long before the Europeans sign off and loggings have occurred as early as 1730! With peak conditions they can be heard as late as 0900. Early arrivals to look for include WHDH (850), CJCH (920), CJON (930), WAVY (1350), WINS (1010), CBA (1070), CJCB (1270). Even mid-West stations have been heard comparatively early— WOAI (1200) and KMOX (1120) both before 2300.

Some channels are known as "graveyards" because they are occupied by dozens of lowpowered local stations and no dominant station is apparent—just one weak signal on top of another. 1240, 1340 and 1400 are examples. Some stations make use of two frequencies (shared time), e.g. WFAA and WBAP both operate on 570 and 820. Other stations operate during daytime only. Also remember that on many channels both USA and Canadian stations operate. Which makes it important to take care in identification.

Some easy ones are WNBC (660), WCBM (680), WABC (770), WCBS (880), WBZ (1030), WHN (1050), WBAL (1090), WNEW (1130), WCAU (1210), WKBW (1520), WQXR (1560). More difficult high power stations include WFAA/WBAP (820), WCCO (830), WJR (760), WSB (750), WOWO

(1190), WLS (890), WHO (1040). You should add a few Indian stations to the log this month in the early hours between 0030—0200. Most have some English programmes (mainly newscasts). Most likely ones are Rajkot (910), Lucknow (760), Sangli (1250), Ajmer (600), Ahmedabad/Baroda (in parallel on 850), Delhi (1070), Bombay (1040). Several others have been logged. Radio Pakistan is more difficult but look for Lahore (630), Quetta (750), Rawalpindi (1150).

Japan is heard only rarely in Britain (but often in Sweden due to polar paths reflection). But try around 1500 on 1250 for Vladivostok, a good catch.

Alistair Woodland

Cycles for ever

What a strange point of view Mr. Covington has (Practical Wireless, January, 1967). Surely, the only sane outlook is to have descriptive terms wherever possible. Everyone who can remember back must realise the difficulty a beginner has in memorising a multitude of non-descriptive terms. If all Mr. Covington is worried about is verbal speed, what can be quicker than the usual "cycles"?

Regarding written speed, surely the three letter m.p.h. is simpler than the

five letter plus oblique mile/h.

I think that the answer to the change for changings' sake group is to simply ignore them—I shall certainly continue to write c/s and say cycles for cycles per second.

W. Lee. Hu

R1155 information

RECENTLY there have been letters in this magazine concerning the R1155, from Mr. Tye and myself. I would like to state that although I said I would get copies made of any information I received, I cannot get them done free. Many readers have written asking for the information and only one has sent the money for the copying. The charge for this is 1s. per page.

A. R. Preston. London, S.E.8.

Phonetics again

I AGREE entirely with the letter of Charles Mitchell (November 1966 issue). Most amateur radio operators operate fairly powerful transmitters. They are fully competent to operate their equipment or else they wouldn't be licensed amateurs. The one quality they lack, is use of codes and abbreviations. Mr. Mitchell says he had heard a ham on 80m using very different phonetics when repeating his callsign in the same transmission. I have listened to hams doing this many a time. Sometimes the callsign is given without the use of phonetics, and we, the S.W.L. fraternity and the amateur who he is in QSO with, are subject to "garbled" call signs. I think that before licences are granted the applicants should be tested on their knowledge of abbreviations, etc., set down in the Geneva Radio Regulations, 1959. It would be interesting to hear what other readers think of my idea. Grimsby, S. Haagensen.

Lincolnshire.

Price correction

The price of the Electronics (Croydon) Ltd., "Supertone G.C.V." radio, as advertised on page 779 of February issue, should be £3 19s. 6d. and not as printed.

NEWS AND..

COBRA AND THE COMMODORE FROM K-B



The latest in the K-B range of portable radios are the Cobra (left) and Commodore (right). Both models feature modular construction which makes servicing a very easy job—the r.f., i.f. and a.f. sections being three plug-in units. The transistor complement is the same in both receivers: 2 × AF117, OC70, 2 × AC127 and 2 × OC81.

The Cobra embodies a 5in. speaker and cabinet dimensions are $5\frac{5}{8} \times 10\frac{1}{16} \times 2\frac{3}{8}$ in. and the Commodore having a $7 \times 3\frac{5}{8}$ in. speaker, measures $7 \times 12\frac{5}{8} \times 2\frac{3}{4}$ in. Both receivers cover long waves and have bandspread on the medium wave band and have provision for an earpiece which is provided as an optional extra and both sets have a car aerial socket. Tape recordings can be made from the Commodore.

The cabinet of the Cobra is Arabian blue plastic with a chrome plated fascia and satin finished aluminium fold-down handle. The Commodore is in a wooden cabinet covered in grey leathercloth with chrome finished knobs and trim. The Cobra costs 12½ gns. plus 3s.8d. surcharge and the Commodore 18 gns. plus 5s.3d. surcharge.

CHRISTMAS MAYDAY CALL FOR RARE DRUG

A ham radio broadcast from Vienna promptly translated into action by a Swedish newspaperman resulted in the emergency despatch from the Wellcome Chemical Works, Dartford, on Christmas Day of 100 tablets of a rare drug which may be the last hope of prolonging the life of a patient in Zagreb, Yugoslavia.

The emergency call, put out on behalf of Dr. Otto Schinkler of Vienna, was for the drug Alkeran needed by his sister, a doctor at the 1st Polyclinic in Zagreb, to treat Eviord Storjok, a 35-year-old patient suffering from cancer. With pharmacies closed and continental telephone lines jammed with Christmas goodwill messages, Dr. Schinkler enlisted the help of Friedrich Stobel, a ham whose Mayday call was picked up by a fellow ham in Stockholm.

Action began when Fred Bramberg, on duty at the Stockholm newspaper "Expressen", received news of the broadcast by telephone. At about 4 p.m. Bramberg was able to reach by telephone Dr. Fred Wrigley, Overseas Director of The Wellcome Foundation Ltd.

With the aid of Mr. W. L. Jeffrey, general manager in the overseas unit and Mr F. G. Rundall, General Works Manager, the tablets were located in the Wellcome Chemical Works. They were handed to Mr. Alan Stubbs, head of the Works despatch section who, despite having one leg in a plaster cast delivered them to B.E.A. Export Cargo Unit to be put on the first connecting plane for Zagreb.

...COMMENT

THE BRITISH ACOUSTICAL SOCIETY

A significant milestone in the history of British Acoustics has been the formation of the British Acoustical Society. This resulted from meetings arranged by the Royal Society between representatives of architecture, engineering, medicine and pure science.

Appropriately, in view of its importance to large sections of the community, the first meeting was a two-day symposium on aircraft noise. Subsequently, symposia have been held on such diverse subjects as underwater acoustics and acoustical investigations of defects in solids.

For full particulars of membership apply to Dr. R. W. B. Stephens at the Physics Department, Imperial College, London, S.W.7.

RADIO 390 LOSE APPEAL BUT BACK ON THE AIR An order of *certiorari* to quash the convictions against Radio 390 and two Company directors (see last month's issue for court report), was dismissed by a two-to-one majority in the High Court of Justice on 13th December. Estuary Radio Ltd., who own Radio 390, switched their transmitter on again New Year's Eve in open defiance of the Post Office, and are now broadcasting as before from the former anti-aircraft fort on Red Sands in the Thames Estuary. The other 'pirate' radio station BBMS, which was also prosecuted for illegally broadcasting from another fort in the Thames Estuary, is still, as far

GRUNDIG SV80 POWER AMPLIFIER

as we know, operating in the medium wave band.



Grundig announce a range of high quality Hi-Fi units, amongst which is the SV80; a fully transistorised mains powered stereo amplifier with a transformerless output stage. Provision is made for the connection of a radio tuner, tape recorder and record player and there are output sockets for loudspeaker assemblies and headphones. Finished in light walnut or teak the cabinet matches other items in their Hi-Fi range.

Technical specification: Mains voltage, 110-130-220-240V 50/60c/s; Power Consumption, 120W max.; Transistors. $14 \times BSY76-4 \times BSY51-2 \times BSX40-AD152-8 \times 2N2148$; Diodes, $2 \times ZF27-2 \times GF580-2 \times ECO1106-8 \times ECO3390-DZ62$; Channel Separation, better than 46dB; Frequency Response, $20-20.000c/s \pm 1dB$; Damping Factor 20 at 5Ω , 60 at 15Ω ; Input Sensitivities, Mic $7\cdot5mV/100k\Omega$, P.U. (Magnetic) $4mV/47k\Omega$, P.U. (Crystal) $220mV-3V/1M\Omega$, Radio/Tape Recorder $250mV/470k\Omega$; Output Sockets, Speaker $2 \times 5\Omega$ (4— 16Ω), Headphones $2 \times 300\Omega$; Output Power is $2 \times 40W$ (Music Power) and Controls are: Volume, Stereo Balance, Bass and Treble; Distortion Factor is less than 0.5%; Power Bandwidth, 10-50,000c/s-18 distortion; and Balance Regulation, up to 10dB.

Starting a club

I was glad to read the letter from G3VLJ last month, and I would like to encourage any young reader in that area to contact him. There may be older readers who know young beginners and who could tell them of the proposed club. Mr. Hansen and I have corresponded earlier on the topic, and I know he is keen.

I have always thought and hoped that the next move in the youth service would be a growth of radio and science clubs, so best wishes to the Croydon area

By the way, if there are any interested young people in the Holloway/Camden Town area who would like to contact me, I would be very pleased to hear from them.

Ken Smith, G3JIX. 82 Granville Road, Walthamstow, E.17.

Foreign equipment

From time to time I have observed letters published in your journal from readers who have purchased foreign-made receivers and equipment which have broken down and been left inactive due to requirement of special parts which the suppliers are unable to supply or have a "I couldn't care less" attitude when letters are written to them requesting data and availability of parts in the country the product is marketed in.

I am surprised to see, why persons in Great Britain who have such an abundant source to draw from in their own country, purchase products made abroad. It could be in my opinion, the price at which they are sold. A similar product made at home (Great Britain) does cost more, I agree, but there is always the dependability of the manufacturer being able to supply the necessary parts if they are of a special nature to the instrument concerned.

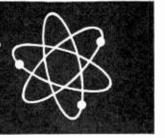
I have had similar experiences with American - made products, which I ordered from New York. Certain parts in an oscilloscope purchased in kit form were missing when the parcel arrived, and after a correspondence that lasted over a period of years, I was told that the kit-maker had gone out of business and they were sorry they couldn't supply parts; would I be interested in ordering another kit?!!! The result has been that I have a white elephant in the house.

I have, however, experienced that the British manufacturers are most cooperative in supplying technical information of their products, and any special parts for many of the test equipment that I own, and service has been very prompt.

S. M. Sharifi.

Teheran, Iran.

EXPERIMENTERS CORNER



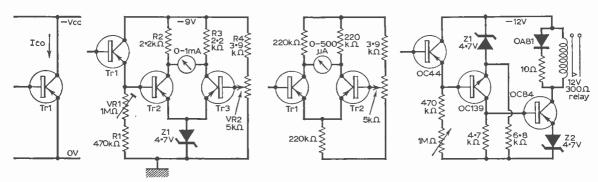
SOLID STATE THERMOMETERS AND THERMOSTATS

K. T. WILSON

OST textbook descriptions of transistor action pay a fair amount of attention to the effect of varying temperatures on the operation of transistor circuits. As far as the normal operation of circuits is concerned, the temperature dependence of all the transistor parameters is a problem which must be taken care of in the design of equipment. If we wish to use transistors as temperature detectors, however, we must find a way to obtain the maximum temperature sensitivity in order to make the thermometer action as sensitive as possible.

The most temperature dependent parameters of any transistor are the leakage currents, and of the two leakage currents of importance, the more sensitive is the collector leakage current in the common emitter connection with the base open cirone milliamp flows in the collector of Tr2 at room temperature. VR2 is then adjusted so that the meter reads zero at room temperature.

The circuit as drawn provides a range of ten degrees centigrade (eighteen degrees Fahrenheit) for full scale deflection. It is therefore very suitable for interior use where temperatures fall within this range (15-25 degrees centigrade). The experimenter can readily devise methods of extending this range; for example the collector loads of Tr2 and and Tr3 could be dropped to 680Ω and a 5mA meter used. Alternatively, the circuit of Fig. 3 could be used. Here the temperature sensitive transistor forms one of the long-tailed pair of the meter circuit, and the Zener diode has been replaced by a resistor. It should be noted that these circuits are entirely unsuitable for car radiator measurements,



Left to right, Fig. 1: Path of leakage current I'co. Fig. 2: A simple thermometer circuit using I'co to record temperature fluctuations. Fig. 3: Alternative circuitry using a long tailed pair. Fig. 4: Circuit of a simple thermostat. (Tr1, Tr2, Tr3—OC70, 71, 44 etc).

cuited. This mouthful is usually shortened to I'co. For most germanium transistors, the value of I'co approximately doubles for every ten degrees centigrade rise in temperature; or, to put it another way, the I'co increases by about ten per cent per degree centigrade.

A thermometer circuit using this principle is shown in Fig. 2. Tr1 is the temperature sensitive transistor with the base open-circuited. VR1 is adjusted so that the leakage current at room temperature produces a voltage I'co. (R1 + VR1) which is slightly greater than the stabilising voltage of the Zener diode Z1 (4-7 volts in this case). This voltage produces a current in the base of Tr2, and hence an amplified current in the collector of Tr2. The value of VR1 should be adjusted so that

as the temperatures encountered may be destructive to the transistors.

Finally, Fig 4 shows a sensitive thermostat using the same principle. In this case the resistance in the emitter of the sensing transistor is high for the maximum sensitivity. To enable the first stage to be coupled directly to the second, Tr2 is an n-p-n type. In some cases where great sensitivity is not required and a low-current relay is available, the n-p-n transistor can operate the relay directly. As shown, the output of Tr2 is directly coupled to a power transistor Tr3 which operates the relay. This arrangement is capable of controlling temperature very closely, the only backlash being due to the relay.

HI-FI - COMPONENTS - TEST EQUIPMENT

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EAGLE FMT41. FM TUNER

Sub-ministure 6 transistor 3 diode F.M.
Tuner. Covers 88-108 Mc. Operates
from 9-volt battery, micro ministure
circuit giving brilliant FM reception.
Ready to use, simply connect to your Hi
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REMOTE CONTROL STEREO HEADPHONE STATION LS.2.

A junction box for connecting stereo headphones to a stereo or monaural system. Separate controls for each channel. On/off switch. Stereo sockets allow two sets of headphones to be used. With instructions and 20ft. of 5 conductor cable. 5 conductor cable.



PROJECT CONSTRUCTIONAL KIT This advanced educational kit is excellent for hegimers as well as the more advanced experimenter. Not even a soldering Iron is needed. Complete with 60 page booklet giving full details 60 page booklet giving of suggested circuits.



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to handle. Will remove magnetism from tape heads per-

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MAGNETIC STEREO CARTRIDGES M1007F. SILVER
Response: 20-18,000 cps
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5cm/Sec.
Stylus: 0.7 Mil diamond
Tracking Pressure

2-4 grai

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5cm/Sec. Stylus: 0.5 Mil diamond Tracking Pressure 1-2.5 grams.

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As reviewed in $Hi\ Fi\ News\ Sept.\ 1965.$ Both feature singularly smooth reproduction and incisive separation of stereo channels

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a compact, versatile integrated unit for monaural or stereophonic reproduction from record player, tape recorder and tuner. Power output 5 watts per channel. Frequency response 40-20,000 c.p.s. £18.0.0

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The perfect answer for the music lover who wants full range The perfect answer for the music lover who wants full range fidelity in a compact system. Features an 8lin full range high compliance speaker with an output capacity of 20 watts RMs. Frequency response: 30-40 c.p.s. Sensitivity: 97 db/w. Flux density: 90-40 c.p.s. Sensitivity: 97 db/w. Flux density: 90-40 c.p.s. densite: 16 ohm. Size 14jin high \times 10^{6} /_{1s} in. wide x 8lin. deep. £14.14.0

As well as this beautifully designed speaker there are two other models MS65. 10 watts RMS at £12.12.0 and MS40 5 watts RMS £8.10.0.

5 watts RMS £8.10.0. All three speakers are finished in magnificent rosewood and the entire cabinet filled with acoustic damping material.

UD40H CARDOID DYNAMIC MICROPHONE



Features a pop-proof diaphragm and superior anti feed-back proper-ties, reduces feed-back and room re-verberation. O/p: -42 db. Res-ponse: 60-12,000 cps:

ponse: 6 12,000 cps; 50K ohm impedance £6.6.

MININE.

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DM31C. CARDOID DYNAMIC MICROPHONE

Superb quality with ball head for distri-buted cardoid front-al pick-up. Output: -52db. Response: 40-13,000 cps. Impedance 50 Kohm. £7.7.0.



DM24HL



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FUTURE BROADCASTING PLANS

HE Postmaster General, Mr. Edward Short, has at last presented Parliament with the long overdue White Paper dealing with broadcasting. Although the contents of this Paper (Cmmd. 3167, obtainable from Her Majesty's Stationery Office, price 1s. 6d.) will not affect many readers directly, it is interesting to note the Govern-

ment's views on broadcasting.

"The Government have under review various major aspects of broadcasting policy," the White Paper states. "First among them was the question of the BBC's finances. Besides this, there were various proposals for the further extension of the broadcasting services; that there should be a fourth television service; that a service of local sound broadcasting should be introduced; and that there should be an extra service of sound broadcasting entirely given over to music . . .

"In reaching the conclusions announced in this review, it has of course been the Government's duty to consider both what purposes the proposals for further extending the broadcasting services should seek to serve, and what organisation would best promote those purposes. The Government have also had to consider to what extent it would be in the national economic interest to allow these extensions. It is not enough that they should be desirable in themselves. The overriding consideration is whether the country can afford them.

FINANCES OF THE BBC

The first thing the White Paper looks at in detail is the finances of the BBC. Reference is made to the fact that the BBC have already started another television service (BBC-2); that they are providing self-contained television services for Scotland and Wales; that they have greatly increased the number of hours of broadcasting on the Third Programme and in Network Three; that more time has been allocated to adult education on television; that a colour service is to start on BBC-2; and that the BBC are developing stereophonic broadcasts in the v.h.f. transmission of the Third Programme.

To carry out these improvements, it is recorded in the review that the BBC now receive the full proceeds of the £5 combined sound and television licence and of the sound only licence, which now costs £1 5s. In mentioning that the Government have completed their enquiry into the BBC's finances, the review continues, "Practically speaking, the only possible ways of providing finance for the BBC are: by direct Government subvention, by the sale of advertising time in the Corporation's

services, or by the licence fee system.

"A Government subvention would be liable to expose the Corporation to financial control in such detail as would prove incompatible with the BBC's independence. The money would, of course, have

to be found from general taxation.

"Under their Licence and Agreement (Cmmd. 2236) the BBC are not allowed to broadcast commercial advertisements without having sought and obtained the Postmaster General's permission. Because of the probable long-term effect on the character of their services, the BBC have never sought this permission. The BBC have reported that, by making special economies they will—on certain assumptions—be able to do so until 1968 when they would need an increase of £1.

"In order to make these special economies, the BBC will restrict activities which they have hitherto considered well justified but which, against the background of continued financial stringency, can be sacrificed to the overriding national need for economy. The Corporation have conducted a searching examination of all their ancillary services and operations, with a view to making the maximum retrenchment in detail. By itself, however, this will not suffice. Some larger scale projects, desirable in themselves, for enlarging and modernising the Corporation's programme production capacity, will be foregone for the present. But the BBC will be able to maintain their present level of programme output and to proceed with extensions and developments of their services already authorised or about to be authorised.

"One assumption on which the BBC have based their undertaking to manage without an immediate increase in the licence fee is that counter measures against licence evasion will prove effective. It has been reliably estimated that, of the gross revenue amounting to some £80M, payable in a full year, some £10M is lost through evasion. This is far too much to be tolerated. Honest viewers and listeners are, in effect, paying for the dishonesty

of the evaders.

"Steps have already been taken by the Postmaster General to tighten up counter evasion measures, but, by themselves, they will not suffice. Further measures are required. The Government are reviewing the penalties which Magistrates may impose on convicted evaders, and are discussing with the associations representing retailers and the rental companies ways in which dealers could help in the enforcement of the licence system. The Government will announce their proposals as soon as these discussions have been completed; and legislation will be brought before Parliament in the current session. The Government recognise the effort which the Corporation are making . . . and are satisfied that no increase in the fee will be required before 1968.

A FOURTH TELEVISION SERVICE

Explaining the Government's decision not to alter the present number of television services, the White Paper suggests that there is room for only one more television service in the next ten years or so, since two of the allocations in the u.h.f. bands will be needed for the changeover of the two present 405-line television services to 625 lines. The review continues, "When the Television Act 1963 was before Parliament, the Government of the day stated their intention to allocate this service [the vacant channel in the u.h.f. bands] to a second programme of independent television during 1965 unless the financial or other obstacles were insurmountable. However it were allocated, a fourth

television service would make large demands on resources. The three main services of television already provide a large volume of programmes of various kinds and the Government do not consider that another television service can be afforded a high place in the order of national priorities.

"Moreover, before deploying the last frequencies certainly available for television for many years to come, the Government would need to be satisfied that the case for committing them to any new service had been fully established. The Government have decided that no allocation of frequencies to a fourth television service will be authorised

for the next three years at any rate.

"Besides the claim of independent television to the frequencies required for a fourth television service network, there is also the possibility that the network would be required for a specialised service of educational television, forming part of the structure of the Open University. The decision to reserve the fourth network would enable the requirements of the Open University to be appraised more closely in the light of practical experience."

COLOUR TELEVISION

The White Paper restates the Government's intentions to start a colour service on BBC-2 during 1967. "It is the Government's view that the cost of colour programmes, which are likely at the outset to be available only to a small minority of viewers because of the cost of the receivers, should not fall upon viewers in general. Accordingly a supplementary licence fee of £5 will be required from those equipped to receive colour programmes."

POPULAR MUSIC PROGRAMME

Introducing a new popular music programme, the White Paper claims the fact that there is a ready-made audience for continuous popular enter-tainment is not new. "What is new is that, by appropriating wavelengths allotted to other countries and by largely disregarding copyright in gramophone records, the pirate stations have been able to exploit the fact. Legislation to end the activities of these stations has been introduced. The Government recognise that there is, however, a need for a new service devoted to the provision of a continuous popular music programme. The question is how the need can legitimately be met: legitimately in that it would be broadcast only on wavelengths available under international agreement to this country, and in that it would respect the rights of performers, composers and others in the material broadcast.

"It is necessary to weigh also any implications for present services to the listening public generally; and, in particular, whether the need to provide frequencies on which to transmit a popular music programme would involve an unacceptable curtailment of the present services of sound

broadcasting.

"Because a popular music programme does not need to differ from place to place, the most economical way of broadcasting it will be by relatively few stations, each with a large transmission area. The characteristics of wavelengths in the medium wave band suit them to this objective. But, as the medium wavelengths available to this country are already intensively used, room for an extra service can only be found by redeploying them. There is not room enough in them for all the present sound radio services and for a popular music programme with anything like sufficient coverage.

"The Government have therefore discussed with the BBC what rearrangement of their services they would need to make in order to find room for the additional service. In the past, the Corporation have considered that they could best serve their various audiences by providing the Light Programme on both long and medium wavelengths, in order to attain the widest possible coverage at an acceptable standard of reception. Now, however, that the long wave transmission of the Light Programme is reinforced by the BBC's v.h.f. transmissions, which have themselves attained virtually complete population coverage, and now that portable v.h.f. transistor sets, at reasonable cost, are available, the Corporation feel free to devote the medium wave channel of 247 metres to a popular music programme.

"The BBC have informed the Government that, on weekdays, the programme would broadcast popular music continuously from 5.30 a.m. to 7.30 p.m. and again from 10 p.m. to 2 a.m., and on Sundays, for most of the day's broadcasting. Over six hours of music each day would be played from gramophone records. The remainder would be either live broadcasts or BBC recordings of popular music especially made for the service. The programme would provide each day a blend of output to meet the needs of the audience for

popular music.

"In the Government's view, the provision of a popular music programme on the medium wavelength, 247 metres, would, on an overall appraisal, provide an extension of choice to the listener. They will authorise the BBC to provide the new service at an early date."

LOCAL SOUND RADIO

"No general service of local sound broadcasting, which would be available during the hours of darkness as well as in daylight, can be provided only on medium wavelengths allotted to the United Kingdom," the White Paper states. "The only possibility for such a service lies in v.h.f. In practical terms, some 150 towns and cities could be served. Of the proposals put to the Government for the provision of a service, some advocate that it should be provided by commercial companies, others that it should be provided by the BBC.

"In a worthwhile service of broadcasting a local station should, the Pilkington Committee concluded, transmit for a sufficient part of the broadcasting day (material) of particular interest to the community served by that station rather than to other localities. In their White Paper of July 1962 (Cmmd. 1770) the Conservative administration agreed that the justification for local sound broadcasting would be the provision of a service genuinely 'local' in character. The Government share this view.

-continued on page 854

PSE QSL

Will You Please QSL . . .

ANY newcomers must have looked at John Guttridge's page and asked themselves, "How do they pick up so-and-so, when I only hear the same stations over and over again?" This article is not intended to teach old-hands new tricks or newcomers old tricks but is simply an account of one man's methods of receiving, and obtaining verification from some of the less common stations heard on the shortwave broadcasting bands.

First of all, it is necessary to have the kind of receiver and aerial which give one a sporting chance of receiving the less common station. The depth of one's pocket and personal choice influence the selection, as does the question whether one should build or buy. What is important is that the receiver should have adequate selectivity and sensitivity to enable the weak signal to be heard through the strident blasts of the major broadcasters on both sides of the Iron Curtain, and also it should have reasonably accurate tuning calibration.

Secondly, the idea should be laid to rest that one person hears all the DX that is going whilst another just does not have the luck. The real answer is that the "lucky" man is usually the one who sets a trap for the DX and then waits for his quarry to appear in it. This is the purpose of this article—to suggest a way in which the trap may be baited, without moving from the fireside, and even without the receiver being switched on. If the "shack" is in an uncomfortable location it makes a pleasant way of pursuing the hobby when the fireside, slippers and background tele are more inviting.

Another myth is that one must speak—or at least understand—a number of languages. This just is not so. What is important is that one should be able to recognise a number of languages, and this ability comes with practice. Very soon one finds that one has a working knowledge of the words which make up station identifications in a number of languages, and as this knowledge is gained it becomes easier to identify stations using languages other than English.

So far as reporting to DX stations is concerned, English is almost universally acceptable, and only a small number of stations ask for reports in other languages. Several short-wave clubs issue QSL report forms in a number of languages, and these help to overcome the language difficulty.

The first 20 or 30 overseas stations can be logged and reported without any difficulty—even if the

A QSL card is a written confirmation of either a contact with, or the reception of, a Radio Station. On the Medium and Short Wave bands, broadcasting stations will often send their QSL cards on receipt of a report. This also applies to "Ham" Stations. However the reports received must be of some use to the station concerned, merely to inform briefly that "I heard you Thursday at 0745 hrs" is virtually useless. The following article is split into two sections. Alan Thompson describes some techniques for the 'commercial' enthusiasts, and David Gibson, G3JDG writes from the amateur's point of view.

receiver and aerial fall far short of the ideal. As the QSL cards for these begin to come in, you will begin to notice some significant—and surprising—gaps in your list. The answer is likely to be that they are countries—not necessarily difficult to receive in themselves—which either do not use English, use low-powered transmitters or only broadcast for a short time each day. It is now that the fireside work begins and perhaps an actual example of the writer's method will best illustrate what is

An essential tool is the "World Radio TV Handbook". This is published in Denmark annually, but is written throughout in English. It can be obtained through all booksellers, but any good reference library should have a copy. The Handbook lists all the radio stations of the world and gives details of their programme schedules and frequencies.

Another invaluable publication is the "Kurzwellensender Frequenzliste" which is issued free by Sender Freies Berlin two or three times a year. This list is in German—with English notes—and gives, in frequency order, brief transmission details of the main radio stations heard in Europe (excluding Radio Moscow, Radio Pekin and Radio Free Europe). Armed with one, or preferably both, of these publications one can settle down and set the "trap".

Let us say that one is anxious to hear Saudi Arabia. A glance at the WRTH will show that the foreign service is carried in a group of Middle Eastern and Indian languages and is clearly not destined for the U.K. Since transmitters are normally beamed to the area in which reception is intended such services are not likely—as a general rule—to be heard or heard well in a totally different direction. (This is a dangerous generalisation, but the exceptions are outside the scope of this article).

There is, however, a Saudi Arabian General Service in Arabic which is clearly intended for the Middle East and North Africa—an area much nearer the U.K. Both the WRTH and the "Frequenzliste" publish tables showing the broadcast bands which are most likely to give good reception in a particular area at any time, and these show that the Middle East is likely to be best heard in the U.K. on the 9Mc/s band in the evening.

Reference back to the WRTH shows that Saudi Arabia uses two frequencies in the 9Mc/s

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3μF ..

4μF ..

10µF

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25 volt

25 volt

25 volt

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band in the evening—9,670 and 9,720kc/s. The WRTH will also show that the Swiss Broadcasting Service utilises 9,665kc/s for its evening service to the U.K. from 1845 to 2015 G.M.T. in English.

This transmission can hardly be missed and it then becomes a question of finding the Swiss programme, waiting for the close down and then listening for a station using Arabic as its main language on a channel only 5kc/s away. With the bandwidth of the average receiver, as S.B.C. leaves the air so Jeddah will (one hopes) be heard, and the tuning knob will only need to be moved a fraction to bring it in at maximum strength.

It should be mentioned that S.B.C. uses the same channel again at 2030 G.M.T. for its Spanish and Portuguese service, so one must look snappy and get the pencil recording details of the Saudi Arabian programme if one is to submit a report and ask for a QSL.

The instance mentioned is an actual case history, and the same method has been used on numerous occasions to locate the less familiar countries. At the time this article was written the frequencies mentioned were in use by the stations concerned but they may, of course, be changed when this article appears.

A "scientific approach often pays off, but luck can also play a part. The author, while on holiday, was determined to find four elusive countries. The approved method produced not a flicker of the "S"-meter, not a sound. A fortnight later, idly tuning the bands, not looking for anything in particular, three of the countries concerned were logged and the fourth followed, on a similar occasion, a week later. The best laid schemes of DX listeners often fail to trap the quarry, but when they do succeed (or even if it is just luck) it is nice to write "Will you please QSL?"

Finally a word regarding reception reports. Most of the world's broadcasting stations require a minimum of 10 minutes programme details before they will verify a report, and some require longer. Essential information in a report is:

(a) the date and time (in G.M.T.).

(b) the frequency or wavelength of the broadcast.

(c) details of the receiver and aerial used and

(d) a report in the SINPO code, or else a general indication of the strength of the signal, the interference and noise level (identifying the source of interference, if possible) together with an estimate of the overall quality of reception.

In addition brief programme details should be given together with the times of the various items—for example:

1955 G.M.T.: Station identification in French and News (give items if possible).

2000 G.M.T.: Time signal (pips) and station identification.

2001 G.M.T.: Announcement—Frank Sinatra song (give titles of musical items if possible).

Before sending off a report—indeed, before even writing it, if only to save the cost of Air letters—it is essential to consider whether you have given all the information one can to enable the station to be certain that you have received their programme. You must provide sufficient definite data to permit a check against the station log.

Making SWL Reports . . .

VER the past years, the writer has received a large number of s.w.l. reports. It is an unhappy fact that out of every hundred received only about two are of any real use and warrant the sending of a QSL card. This startling figure (2%) is borne out in conversations with other amateurs who also appear to be inundated with useless scraps of paper.

If a station receives a useful report from an s.w.l., it is highly probable that a QSL card will be sent. The following notes are intended as a general guide for those s.w.l's. who don't get replies, or for those just starting to listen on the

amateur bands and short-waves.

1. First, the report should be legible. About 10% fail on this count. Remember that amateurs in other countries may not speak or read fluent English, so legibility is of paramount importance.

2. The time should be specified in G.M.T. using the 24-hour system and the letters G.M.T. written

after to avoid any misunderstanding.

3. Your QTH or locality. If you live in a small village, then a reference to the nearest large town should be included i.e. Harpenden—6 miles N.W. of St. Albans. Also if possible the height a.s.l.

4. Equipment in use. Don't just put "superhet" for the receiver. It might be a simple 3 valve job

or a 16 valve triple-conversion unit.

5. Aerials are very important. The type of aerial, and the length in the case of a longwire should be noted. Also, most important, the direction it points, that is looking straight down the wire. The height is also a useful item to put down, too. An example of this, for a longwire might be—68ft. end fed running N.E./S.W., 30ft. high. Again if a dipole is used this fires broadside to the direction of the wire, i.e., 90° to it and this should be remembered when giving a report.

6. The following are the standard items and are usually the only things put down. Those s.w.l's. who only include these items and nothing else can be congratulated on producing a near useless report in most cases. By themselves they aren't much use, but with all the other information

referred to they are vital.

(a) RST. Readability, Signal strength, and (in the case of c.w.) Tone.

(b) QRM. Interference.

(c) QRN. Atmospherics.(d) QSB. Fading.

(e) QRG Frequency.

Relevant reports on other signals received during the same period are very useful too, especially from the same area if the station happens to be either very strong, very weak, or perhaps fading compared with the other signals on the band.

7. The frequency should be given accurately. If possible a simple crystal frequency standard should be fitted to the station and the receiver dial calibrated against it. At each session of listening, after the receiver has warmed up, the dial should be checked and adjusted to ensure that the receiver dial reads accurately.

8. S-Meter readings should be qualified. Many S-meters are included in the receiver in such a

way that they are affected by different settings of the various controls. Perhaps the best way is to set the controls to a particular setting and feed in a signal of known strength, i.e. so many microvolts and mark this on the meter as say S9 plus 40dB.

Or perhaps a signal with an S9 carrier could be used to make some form of calibration. This reference, however the meter is set up, should be put in the report. The signal level of the other station in the QSO together with callsign should also be included, if it can be heard.

The above notes are not rigid. However a report based on these would stand a very much greater chance of a QSL than the more usual "Heard you 5 and 7 here on a superhet, please QSL".

An example report is given below in order to show the general pattern. Compare this with the classic "Heard you here 5 and 7" etc.

M. Jenkins, 38 Malsen Road, Menton, Bedfordshire, England. Six miles S.W. Bedford. Latitude Longitude Approximately 300 ft. a.s.l.

Equipment.

Seven valve single conversion superhet. One r.f., f.c., two i.f., two a.f., b.f.o. Headphone reception.

Antenna.

Half wave dipole co-ax fed plus balun, 40ft. high running N.E./S.W.

Date/Time/Frequency.

Monday 28th March, 1966. 0022 G.M.T. 14155 kc/s.

Signal Report.

W6ZZZ/P. Your a.m. signals RST 58. In QSO with—AP2XXX. His a.m. signals RST 55.

QRN/QRM/QSB.

QRN: Nil. QRM: Slight/moderate from local G 5 kc/s h.f. QSB: Slight from 57/58.

S-Meter.

S-Meter calibration, $1\mu V$ in reads S9.

Remarks

Also heard W6XXX/M at 5 and 5 but no QSB. W1/W2's received 0001-0130 all average 5 and 7, no QSB. Heard you on March 20th, 1966 in QSO with ZL9XXX when you were 559, conditions about the same as above.

Would very much appreciate a QSL card. Stamps/IRC's enclosed.

PRACTICAL TELEVISION

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U.H.F. AERIALS

Details of aerial design—including constructional details

HUM IN TV RECEIVERS

How to locate and cure this common fault **February issue on sale now 2s.**

FUTURE BROADCASTING PLANS

-continued from page 849

"They consider that this objective would prove incompatible with the commercial objectives of companies engaging in local sound broadcasting; and that, in result, the former would be likely to suffer. While the Government do not, in principle, rule out advertising as a means of financing broadcasting stations in public ownership, it is in their view of first importance to maintain public service principles in the further development of the broadcasting services; and accordingly they reject the view that a service of local sound radio should be provided by commercial companies.

"Evidence of the expertise and professional enthusiasm which the BBC could bring to local sound broadcasting is to be found in the 'trial programmes' they have prepared. They lend much support to the view that, properly organised, local radio would provide a valuable service to the local community; and, by giving a new means of expression to its particular interest and aspirations, serve to reinforce its distinctive character and sense

of identity.

"The Government believe that local radio organised and produced as a public service, would be most likely to realise those social purposes to the full; and would at its best prove an integrating and educative force in the life of the local community. But it is, they consider, important to establish how far the claim for a local station is likely to rest on genuinely local initiative having these purposes as its objectives; and how far local sources of finances are likely to be available to meet the expenditure required by such an initiative. In sum, not only is it important to establish that a local service of high quality could be maintained, monthin, month-out. There is also the question whether it would command enough support, including financial support, to justify the development of a service on a widespread and permanent footing . . .

"In considering how an experiment should be conducted, the Government have had regard not only to the need to avoid an excessive diversion of resources for the purpose but also the undesirability of entering into a commitment at this stage to any permanent form of constitution and organisation. They conclude that these various requirements will best be met if the experiment is conducted by the BBC as a venture in co-operation with local interests; and they have therefore decided to authorise the BBC to go ahead with a ninestation project in v.h.f. The stations would offer a full-scale local service. They would come into operation after about a year; and after a year or so of operation, should have provided the information on which to found the final solution . . .

"The Government reserve until the conclusion of the experiment any decision on the question whether a general and permanent service should be authorised, and, if so, how it should be constituted, organised and by whom provided, as well as how it should be financed. The decision that the BBC should conduct the experiment implies no commitment that the Corporation should provide a permanent service; if it were decided to authorise one."



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Complete kit as described

With coils tested \$\frac{F}{2}\$ \$\frac{F}{4}\$ \$\frac{A}{4}\$ \$\frac{C}{2}\$ \$\frac{C}{4}\$ \$\f

f4.19.6 With coils tested and pre-aligned and pre-aligned for circuit and data.

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Designed and made by Mullard, these inductors are as used in T.R.S. Decoder above. TYPE WF2949 and WF2951, each 25/-. Per pair 49/6. Post free.

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33m. 37-; 33m. x bin. 512; 34m. x 34m. 39; 33m. x 17m. 129.
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WIREWOUND RESISTORS, 25 ohm to 10 K 5 w, 1/3, 10 w.

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CONDENSERS Silver Mica. All values 2 pt to 1,000 pt. 6d. ca.
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and 1/350 v. 10d. .02 MF to 0.1 MF, 500 v. 1/-. .25 T.C.C. 1/9. 5 T.C.C. 2/-.
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6 VALVE A.M./F.M. TUNER UNIT

In Kit Form with or without Power Pack

Med. 190 m., 550 m., V.H.F.—86 Mc/s-103 Mc/s., 6 valves and metal rectifier. Self - contained power unit. Magic-eye, 3 push-button



eye, 3 push-button controls, on/off, Med., V.H.F. Diodes and high output sockets with gain control. Illuminated 2-colour perspex dial 11½n. x 4 in. chassis size 11½n. x 4in. x 5½n. Strongly recommended for use with Mullard amplifiers. For A.C. mains 200/250 v. Unbestable value. Complete kit, Inc. Power Pack as illustrated, 11 gns, Carr. 7/6. Ditto less Power Pack, 10 gns, Carr. 7/6. Circuit and Construction details, 4/6. Free with kit.

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3 WATT TRANSISTOR AMPLIFIERS—(Newmarket PC5+). 6 Transistor, 3 ohm Output. Size 5½ x 1½ x ½in. 5-8 mV sensitivity. Excellent High Gain Med. Imp. Audio Amp.75/-. Post 1/-. 9 v. PP3 battery 2/6 and 3 ohm speaker cxtra.

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FULLY TUNABLE ON ALL WAVEBANDS

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Covers Medium and Long Waves, Trawler Band and three Short Waves to approx. 15 metres.

Push-pull output for room filling volume from rich toned 7 x 4in. speaker. Air spaced ganged tuning condenser,

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The perfect portable and the ideal car radio. (Uses PP7 batteries, available anywhere.) 9 stages—7 transistors and 2 diodes

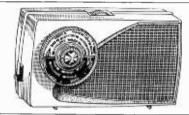
EXTRA BAND FOR EASIER TUNING OF LUXEMBOURG, etc.

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Parts Price List and easy build plans 31- (Free with kit)



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P. & P. 3/6

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7 stages—5 transistors and 2 diodes

Fully tunable over Medium and Long Waves and Trawler Band, Incorporates Ferrite rod aerial, tuning condenser volume control, new type fine tone super dynamic 3in, speaker, etc. Attractive case. Size 6 ½ 4 ½ x 1 ½ in, with red speaker grille. (Uses 1289 battery, available anywhere.)

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POCKET FIVE Now with 3in. Speakerl ● 7 stages—5 transistors & 2 diodes

■ 7 stages—5 transistors £ 2 dic Covers Medium and Long Waves and Trawler Band, a feature usually found in only the most expensive radios, on test flome, Light, Luxembourg and many Continental stations were re-ceived loud and clear. Designed round supersensitive Ferrite Rod Aerial and fine tone 3in. moving coil speaker. built into attractive black and gold case. Size 5¼ x 1½ x 3½in. (Uses 1289 battery available anywhere.)

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TRANSONA SIX



STOP PRESSI Pocket 5 med. and long wave version with miniature speaker. P. & P. 29/6

NEW ROAMER SIX

NOW, WITH PHILCO MICRO-ALLOY R.F. TRANSISTORS

6 WAVEBAND ! !

8 stages—6 transistors and 2 diodes
Listen to stations half a world away with this
6 waveband portable. Tunable on Medium and
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Top grade transistors. 3-inch speaker, handsome case with gilt fluings.
Size 7i x 5i x 1iin. (Carrying strap 16 extra.)

EXTRA BAND FOR EASIER TUNING OF LUXEMBOURG, ETC.
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13.19 6 P.&P. Parls Price List and asev build 8 stages—6 transistors and 2 diodes

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plans 2/-

This is a top performance receiver covering full Medium and Long Waves and Trawler Band. High-grade 3in. speaker makes listening a pleasure. Push-pull output. Ferrite rod aerial Many stations listed in one evening including Luxembourg loud and clear. Attractive case in grey with red grille. Size 6‡ x 4‡ x 1‡in. (USes PP4 battery available anywhere.) Carrying Strap 1/- extra. Total cost of all

59/6 P. & P.

Parts Price List and easy build

MELODY SIX ·

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Our latest completely portable transistor radio covering Medium and Long Waves. Incorporates pre-tagged circuit board. 3in. heavy duty speaker, top grade transistors, heavy duty speaker, top grade transistors, vave change slide switch, sensitive sin. Ferrite rod aerial. Push-pull output. Wonderful reception of BBC, Home and Light, 208 some leather-look pocket size case, only 61 x 34 x 1911, approx. with gilt speaker grille and supplied with hand and shoulder straps.

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9 stages-7 transistors and 2 diodes

Covers Medium and Long Waves and Trawler Band. The ideal radio for home, car, or can be fitted with carrying strap for outdoor use. Completely portable—has built-in Ferrite rod aerial for wonderful reception. Special circuit incorporating 2 RF Stages, push-pull output, 3in. speaker (will drive large speaker). Size 7½ x 5½ x 1½in. (Uses 9V battery, available anywhere.)

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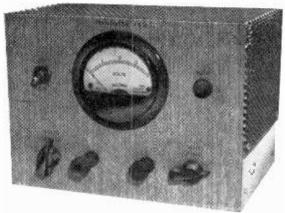
N professional laboratories, considerable use is made of stabilised power supply units for experimental and development work, since these units have a low output impedance and give a constant output voltage over a very wide range of current demands.

To be really useful, a variable voltage power supply unit should have an output impedance, or effective internal resistance, that is comparable to that of a conventional battery, and should be reasonably well stabilised against changes in mains supply voltage, etc. The unit that forms the basis of this article has been designed with these points in mind.

Simplest form

The simplest way of obtaining a variable voltage power supply is to wire a variable resistor across a normal power supply, and take the output from across the slider, as shown in Fig. 1a. This, however, is rather wasteful of power, gives a high effective internal resistance, and does not guard against changes in the supply voltage. An improvement over this basic system is shown in Fig. 1b. Here Tr1 is wired as an emitter follower, with its base connected to the slider of VR1, and the output voltage is taken from across R1 in the emitter line of Tr1. The emitter voltage of this transistor "follows" very closely the voltage on the base. Taking very little power from VR1, the transistor presents a high input impedance while at the same time giving a low output impedancy, and thus presenting a low effective internal resistance.

A further improvement which is shown in Fig. 1c, increases the effective gain of the transistor. Here, Tr1 and Tr2 are connected as a Darlington (or Super-Alpha) pair, the emitter current of one transistor feeding directly into the base of the other, with a current gain equal to the product of the individual gains of Tr1 and Tr2.



For example, if both transistors have current gains of 50, the effective current gain of the combination "transistor" will be 2,500 and the output impedance of the circuit will be correspondingly low.

Both of these transistor circuits give a variable voltage output with little power wastage and have reasonably low effective internal resistance, but neither circuit is stabilised against changes in supply voltage. This problem can be overcome by modifying the circuit as shown in Fig. 1d. Here, the voltage that is used to feed VR1 and the base of Tr1, is stabilised by the Zener diode, D1, the actual supply that is connected across the transistor circuit is not. However, the output voltage is approximately the same value as that at the slider of VR1 and is thus stabilised against changes in the mains voltage. This circuit (shown in Fig. 1d) is very useful, but its power handling requirements are limited by the output transistor, Tr2. If the unit is to give output voltages up to 18 volts, it is necessary to use an unstabilised input supply of at least 22 volts. If an output of 6 volts is required, 16 volts must be dropped across the output transistor. This means Tr2 will have to dissipate 16 watts with a 1A output current.

Finalised circuit

These problems are overcome in the circuit of the finished power supply unit, as shown in Fig. 2. Here, the output voltage is varied in three ranges, and the unstabilised input voltage is varied to suit the range in use, thus ensuring that a minimum of power is lost across the output transistor Tr3. A complete description of the circuit follows:

The mains supply is connected to transformer T1 via switch S1. Switch S2a selects either the 5, 11, or

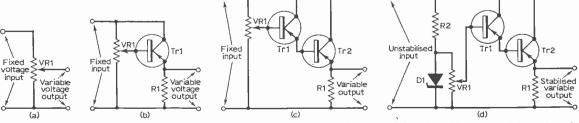
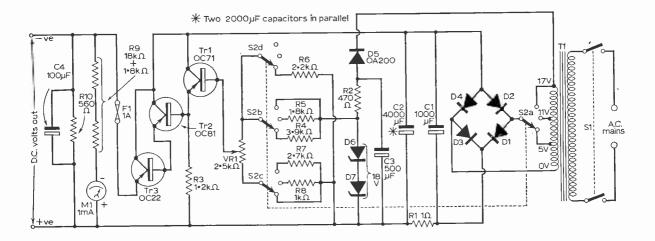


Fig. 1: (a) Basic circuit, (b) improvement by the addition of an emitter follower, (c) replaced by super-alpha pair emitter follower, (d) the Zener diode stabilises the circuit against changes in the supply voltage.



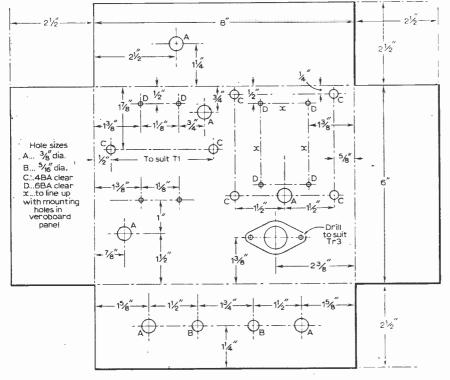
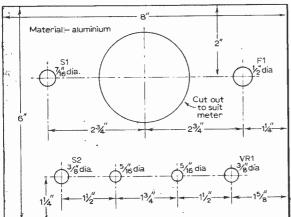


Fig. 2 (above): Complete circuit of the power supply unit. S2 is a four-pole, threeway wafer switch. D6-D7 could be a single $18V \ \frac{1}{2}W$ Zener diode.

Fig. 3 (left): The main chassis dimensions. Note that Tr3 is insulated from the chassis by the use of insulated washer and spacers.

Fig. 4 (bottom left): The front panel dimensions.



17 volt tapping on the secondary of T1 and connects it to the bridge rectifier, which comprises D1—D4. The rectified output is smoothed by the C1-R1-C2 filter network and passed to the control circuitry.

An additional line is taken from the 17V tap on the secondary of T1 to D5, and the resulting rectified a.c. is smoothed by C3 and fed to the R2-D6-D7 network, to give a final stabilised reference voltage across the Zener diodes. This stabilised voltage is applied across VR1, making a variable stabilised output available at the slider; the available voltage swing of VR1 is limited on each range by the R4—R8 series resistors.

The voltage from the slider of VR1 is fed to the base of Tr1, which is wired as an emitter follower with emitter load R3. The voltage at Tr1 emitter is fed to the Super-Alpha pair, Tr2—Tr3;



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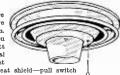
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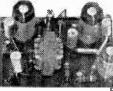
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674

7B7

7C5 7C6 7C7 7H7 7Q7 787 7V7

7Y4 7Z4

SD2 9D2

9D6 10F9 12A6 10P14

12AH7 12AT6 12AT7

12AV6 12AU7

12AX7 12AY7 12BA6 12BE6 12BH7

12C8 12E1

12E1 17/6
12H6 2/12J5GT 2/6
12J7GT 6/6
12K7GT 2/12K8M 10/12Q7GT 3/3
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10/-7/-8/-7/8 7/-18/-8/-8/-8/-2/6 3/-2/-9/-5/-5/-5/-5/-

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5/-7/-7/-

17/6

5/9 5/-2/-7/-18/-6/-15/-5/-18/-

6BR7 6BW6

6C5GT

6C6

6C6G 6C8G

6CH6 6C21 6CL6 6CW4

6D6 6E5

6F12 6F13 6F14

6G6G

6H6M

6J5 6J5G 6J6W

6J7G 6J7M

6K6GT 6K7G 6KJGT 6K8G

6K8GT

6K8M 6K25 6L5G 6L6GA 6L6M

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7/-2/-2/6 6C4 6C5G

6/-6/6 4/-5/-5/-4/-20/-2/6

10/-6/-2/-3/6 6/-5/-5/6 2/-4/9 3/-8/3 6/6

4/-45/-5/-14/-10/-4/7 2/6

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3FP7 3EG1 5PC1 5FP7

25D7 30 30C15

30FL1

30FL1 30L15 30L17 30P12 30P19 30PL1

30C15 10/-30C18 11/-30F5 8/6

30FL12 19/-

30FL13 6/-30FL14 13/-

30PL13 15/-30PL14 15/-

30 PL14 15/-3516GT 7/-35T 17/6 35W4 5/-35Z3 10/-35Z4GT 6/-37 4/-38 4/-

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50L6GT 8/-53A 7/6 57 6/-

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(c) 260-350 v. stabilised, adjustable, approx .45 mA.

(d) 450 v. approx, 30 mA.

(g) 430 v. approx. 30 mA. (g) 50 v. approx. 150 mA. (f) 4.5 v. A.C., 4.5 amp. common earth. (g) 6.3 v. A.C., 4.5 amp. common earth. 5 valves, 7 silicon rectifiers, 4 Solenium HV rectifiers. Brand new, £9.10.6. Carriage 12/..

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PERSONAL CALLERS WELCOME the final output voltage is taken from Tr3 emitter to the output terminals via fuse F1. R10 is a small permanent load resistor connected across the output terminals.

A voltmeter, comprising M1 and R9, is built into the unit and permanently wired across the output terminals for monitoring purposes. Although the prototype unit was found to give output voltages from zero to 18V in three ranges, at currents up to 1A, the maximum output voltage and available current can be increased simply by changing component values.

Construction

The prototype unit was built up on a standard 8in. × 6in. chassis, with angled corner brackets. Construction should be started by drilling this chassis as shown in Fig. 3. Next, drill and cut the front panel, as indicated in Fig. 4. The hole for the meter is best cut by first marking the panel and then cutting away the unwanted metal with the aid of a fret-saw fitted with a metal-cutting blade.

When the front panel is complete, it can be covered with one of the decorative self-adhesive plastic materials before it is secured to the main chassis. It should be noted that the actual front panel controls, VR1, S2, and the two output terminals, can be used to secure the front panel to the chassis, thereby eliminating unsightly bolt heads, etc. Grommets should now be fitted in all suitable holes in the chassis, and transformer T1 and all tag strips should be bolted in place.

* components list

Resistors: (all 5%, ½W except where otherwise stated)

R1	1Ω, 3W	R6	2·2kΩ
R2	470Ω, $10%$	R7	2·7kΩ
D2	1.21.0 100/	DO	11.0

R3 1·2κΩ, 10% R8 1κΩ R4 3·9κΩ R9 18κΩ + 1·8κΩ, 1% R5 1·8κΩ R10 560Ω, 10%, 1W

VR1 2.5kΩ, wire-wound, linear

Capacitors: (all electrolytic, 30VW)

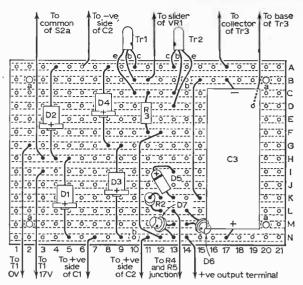
C1	1000μF	C3	500μF
C2	$2000\mu F + 2000\mu F$	C4	100µF

Semiconductors:

Tr1	OC71 or OC75	D5	OA200 or OA202
Tr2	OC81 or OC72	D6	9V, ½W, 10%, Zener
Tr3	OC22 or OC23	D7	9V, ¼W, 10%, Zener
D1—	-4 1A, 50 p-i-v, si	ilicon	

Miscellaneous:

Battery charger transformer with 1.5A output at 5V, 11V and 17V; two-way, two-pole on/off switch; 1A fuse and holder; 1mA meter movement (see text); two output terminals; $8in. \times 6in.$ chassis; strip of Veroboard (see Fig. 5); tag strips; rubber grommets; control knobs; wire; sleeving; and expanded metal speaker gauze.



 $a\!=\!drill$ mounting hole to clear 6B.A screw and cut back copper $b\!=\!b$ reak copper strip with small drill or special cut ting tool

Fig. 5: Veroboard assembly details.

Cut the small Veroboard sub-panel to size as shown in Fig. 5, and break the copper strips where indicated with the aid of a small drill or the special cutting tool that is available. Now assemble all components and leads to the board as indicated. It should be noted that on the prototype two Zener diodes have been used, but these can in fact be replaced by a single 18V Zener diode, if available. When complete, the Veroboard sub-panel should be bolted in place on the underside

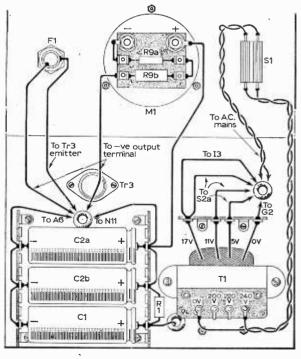


Fig. 6: Above-chassis wiring.

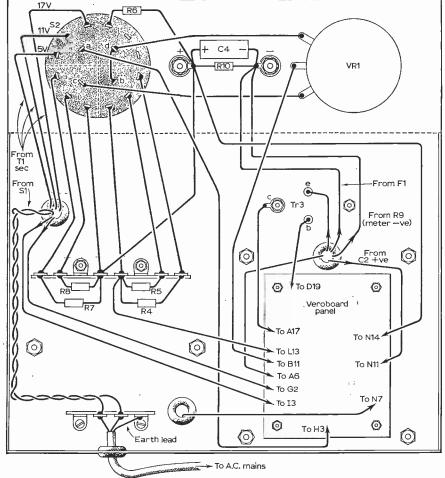


Fig. 7. Wiring of the under chassis.

of the chassis with the aid of small 6BA screws, taking care to use rubber grommets as spacers between the Veroboard and the main chassis to prevent short circuits occurring.

Now, using insulated washers and spacers, bolt transistor Tr3 in place on the top of the chassis, and complete the under-chassis wiring as shown in Fig. 7. Secure the F1 fuse holder, switch S1, and the moving coil meter to the front panel, and complete the wiring of the top of the chassis as shown in Fig. 6. When complete, double check all wiring and then carry out a functional test, checking the output voltages and currents on all ranges. With the component values shown, the voltage swings should be as follows: Range 1, 0.5—3.5V, Range 2, 3—10.5V, Range 3, 9—18V. These voltages are without external load.

The meter circuit

On the prototype, a 1mA moving coil meter was used as the monitor, wired as a 20V (f.s.d.) d.c. voltmeter. It is not essential to use a 1mA meter movement and in fact almost any meter may be used for this job, but one must know the sen-

sitivity of the movement. If it is not marked on the face of the instrument in ohms-per-volt, but the internal resistance is given, it is a simple matter of Ohm's law: $E=I \times R$. For example, a 1mA movement with an resistance internal $1,000\Omega$, will drop 1V and, thus, have a sensitivity of $1,000\Omega$ per volt. To increase the voltage range of the movement to 20V f.s.d. the total series resistance has to be increased by the same factor-twenty. Thus an external series resistor of 19,000Ω is required $(20,000\Omega)$ less the 1,000 Ω internal resistance).

Usually, the internal meter resistance will be indicated on the face of the meter, but if it is not it can be determined by connecting the meter in series with a 4.5 to 12V battery and a high value series resistor and variable resistor, and adjusting the values of these two resistors until the meter reads f.s.d. A variable resistor should now be connected in parallel with the actual meter and adjusted until the meter pointer falls to half f.s.d., at which point the values of the internal meter resistance and the

parallel resistance will be equal. Thus, the internal meter resistance can now be determined by removing the parallel variable resistor and measuring its resistance on an ohmmeter. It should be noted that, if any attempt is made to measure the internal meter resistance directly with the aid of the ohmmeter, severe damage may result.

The specified transformer is capable of supplying currents up to 1.5A. If higher currents are required, an alternative transformer should be used, and the four rectifiers, D1—D4, should have suitably increased ratings.

The transistor types used are not critical. Tr1 may be any small a.f. transistor capable of working with a collector voltage of approx. 25V or greater, but should preferably be a fairly high gain type. Tr2 may be any type capable of working with a collector voltage of approx. 25V, and able to handle powers of at least 100mW. Tr3 may be any power type capable of working at collector voltages of approx. 25V or greater, able to handle emitter currents of at least 1A, and dissipating powers of 16W or more on a large heat sink. If larger currents are required, the ratings of Tr3 should be suitably increased, or, alternatively, two or more power transistors wired in parallel.

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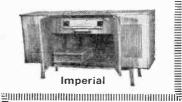


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■ NEWNES RADIO AND TELEVISION SERVICING (1965-66 Models) By J. P. Hawker and J. Reddihough. 496 pages, 9 × 6in. Now published by Buckingham Press Ltd. Price 85s.

VERY year a new edition of Newnes wellknown Radio and Television Servicing is published. Always in great demand, these annual volumes contain a wealth of circuits, data and repair hints for popular television and radio receivers, tape recorders and record reproducers. The new 1966 edition has just been published and deals with 1965-66 models, nearly 50 principal makes.

The publishers, Buckingham Press Ltd. who are the successors to S.B. Division of George Newnes Ltd. have asked us to mention that their address has not changed, it remains-15-17 Long Acre, London, W.C.2. Copies of Radio and Television Servicing are available on free trial, direct from Buckingham Press Ltd.—PEM.

THE LAW AND YOUR TAPE RECORDER By Andrew Phelan. Published by Print and Press Services Ltd. 30 pages. 7 × 5in. Paperback. Price 3s. 6d.

N these days of rules and regulations it is almost impossible to draw breath without breaking Lsome law or other; and ignorance is no excuse. Practically every time the enthusiast uses his tape recorder he is inviting prosecution-or so it would appear after a perusal of this interesting little booklet.

The author is a barrister-at-law, and the text occasionally betrays this, but otherwise, a lucid account of the pitfalls of the laws of copyright as related to tape recording will be found here.

It is perhaps unfortunate that amid all this frightening legal stricture we find no hint of aid. "This is the law"—says Mr. Phelan, in effect, without adding that application to the Performing Rights Society, or Phonographic Performances Ltd., would solve many of the immediate problems of the local impresario.

For the ordinary user, the problem seldom arises: one can take down broadcast material for one's private enjoyment so long as it is not covered by a separate copyright, but as this permission does not extend to gramophone records, whether broadcast or not, Junior is contravening the Acts of 1956, 1958 and 1963 every time he tapes down "Top of the Pops". Replaying his recording to someone else compounds the felony and accepting payment for the privilege is so reprehensible that we shudder to think of the consequences!

Whether one intends to make a business of tape recording or simply indulges in the hobby for pleasure, it is wise to know the legal limitations and this pocket book is a cheap and easy introduction.-MAQ.

SHORT WAVE LISTENING Published by Iliffe Books Ltd. By J Vastenhoud. Published by Illife Books L 107 pages. Size 8½in. x 5½in. Price 12s. 6d.

F the PRACTICAL WIRELESS feature "On the Short Waves" has given you an appetite for Listening to foreign radio stations this book will provide a meaty dish. All the beginners' questions-What frequency bands should I listen to and when? What is a QSL card? How do I send a reception report? Can I join the DX Club?-are well answered. Established DXers will not be surprised for the author is Jim Vastenhoud, regularly heard on Radio Nederland's DX programme.

As well as the chapters dealing with the practical side of DXing the book contains chapters on the principles of short wave transmission, the aerial and the correct choice of receiver, which seems to be a standard in any book dealing with radio these days. Other useful selections include comprehensive frequency prediction tables, an English-French-Spanish dictionary of commonly used DX terms, and DXing with a tape recorder.

I started by saying that this was the book for the newcomer. Old hands shouldn't be put off by this as they will find new ideas here. I certainly did. -JMG.

SILICON CONTROLLED RECTIFIERS ■ By Alian Lytel. Published by W. Foulsham & Co. Ltd. ■ 128 pages. Size 8½ × 5in. Price 16s.

HOSE who are not aware of the importance of silicon controlled rectifiers in power switching and control applications should find this book most rewarding. SCR's, or thyristors, operate in much the same way as gas filled thyratrons, but are much simpler to use and have many more applications. In fact, it is possible to control kilowatts of power with these four-layered semiconductor devices from extremely small signalsi.e., the output of a photocell or a thermocouple.

Silicon controlled rectifiers are comparatively new in this country—outside the professional and industrial fields-and it will not be too long before the majority of domestic electrical appliances and electronic equipment make use of them. They are ideal for controlling electric motors.

This book first deals with the theoretical aspects, of SCR's, then goes on to explain in detail how they work, with various types of triggering circuits.

necessary. As the book originates from the United States, the publishers have thought it necessary to include a specially written chapter for the English reader. It states, in three pages, that the mains supplies, are different and that American components are used throughout. It also gives an incomplete list of British suppliers to the home constructor.—JRC.

MAKING THE MOST OF TAPE POSITION INDIGATORS

By J. LOWRIE Grad I. E. E.

OST tape recording enthusiasts keep a detailed record of each tape with a list of the material recorded on it. In order to spot individual items some method of cataloguing must be used. Coloured indicators can be attached to the tape or note taken of the scale reading on the tape usually marked from 0 to 10. Most modern tape recorders are, however, fitted with a rev. counter



After one revolution the tape unwound at A is much longer than that at B. Length unwound = 2TR where R is radius from centre of tape spindle to outer layer of tape.

Dial reading	0	45	_92	145	208	279	370	420
Time (minutes)	0	5	10	15	20	25	30	32

Fig. 1: Diagram and Table showing why the relationship between dial reading and footage is not linear.

which is geared to the tape spindle and automatically records the number of revolutions. The disadvantage of this method is that dial readings do not correspond directly to the footage of tape which has passed the head. Why this is so can be seen from Fig. 1. As the tape runs off the spool the length of tape which unwinds gets less—length of tape unwinding= 2π x radius of outside of tape.

The person using the tape then faces an obvious difficulty: if the rev. counter shows a reading of say 400 at the end of the tape and after a recording has been made the reading is 200, how much recording time is left? At first sight it would appear that only half of the tape has been used whereas more than half has been run off as can be seen when the situation represented in Fig. 1 is considered. It is possible to time the first recording and subtract this from the total playing time but it becomes tedious if this has to be done for each tape; it is much better to compile a graph relating tape footage to dial reading and reference to this will show at a glance the time difference between various dial readings.

The procedure for making a graph is as follows; Take a full spool of tape and set it into position for playback.

Set dial readings to zero.

Start playing back at fastest speed on machine. Note time at start and take dial readings every five minutes. Note the time when all the tape has been used.

The results obtained will form a table similar to the table, Fig. 1, which was obtained using 1,200ft. of L.P. tape on a 5\frac{3}{4}\text{in.} spool running at 7\frac{1}{2}\text{in.}/sec. The results of Table 1 are plotted on a graph to give Fig. 2. It is easy to see at a glance the recording time represented by various dial readings. Thus for example, if recording started at 180 and ended at 310 the recording time would be 27-18=9 minutes.

If the relationship between recording time and dial reading had been direct the graph would have been straight as shown by the dotted line. Thus after reading 100 serious errors would arise if the correction supplied by the graph were not applied. The graph can be adapted for other speeds simply by multiplying the time scale by the correct factor (e.g. 3\frac{1}{2}\text{in./sec.} would require scale to be doubled) leaving the dial reading unchanged. The exact figures on the graph are affected by the spool size and whether L.P. or standard tape is used. Thus graphs should be drawn up for each spool size used, one for standard tape and one for L.P. tape.

Once armed with these graphs the enthusiast can

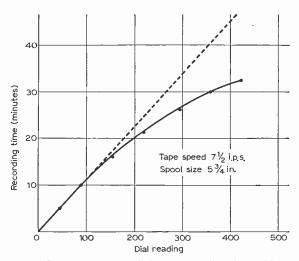
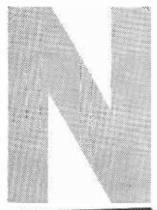


Fig. 2: Graph showing variation of recording time with dial reading.

safely record new material in between two sections which he wishes to preserve knowing exactly how much recording time is available and being certain that there is no danger of inadvertently erasing material which he wants to keep.









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COMBINED FM TUNER AND POCKET FM RECEIVER

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TECHNICAL SPECIFICATIONS Performance figures obtained using Stereo 25, two Z.12s and a PZ.3.

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Pick-up-3 mV into 50K ohms.
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FREQUENCY RESPONSE
(Mic. and Radio)-25 c/s to 30 kc/s ±1dB extending to 100 kc/s

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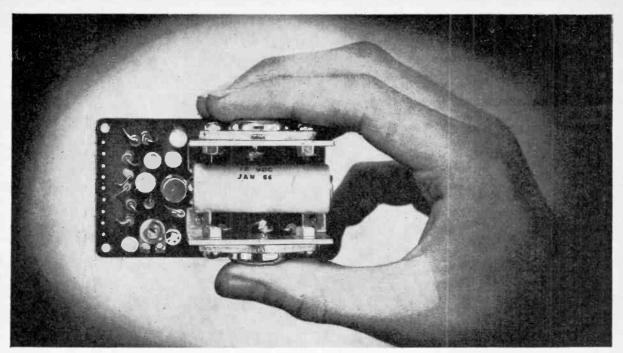
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make it possible to use just one

TECHNICAL SPECIFICATIONS

■ Size 3 in. × 13in. × 11in.

Class "B" ultralinear output.

RESPONSE 15-50,000c/s ± 1dB.

M Suitable for 3, 7.5 or 15 Ω speakers. Two 3 Ω speakers may be used in parallel.

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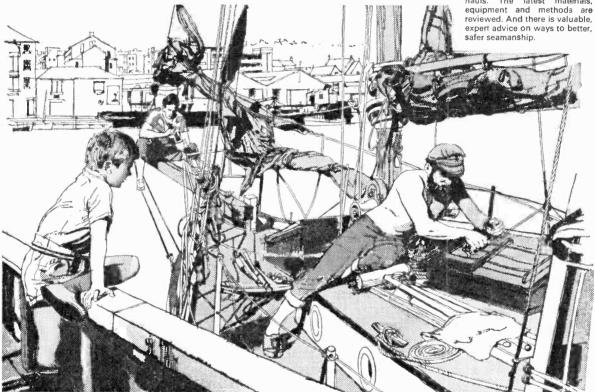
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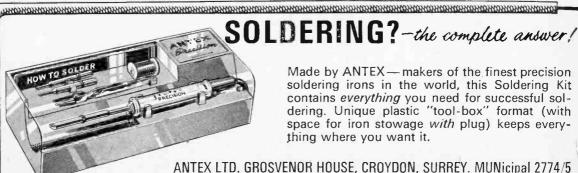
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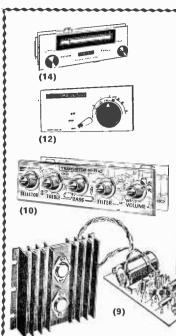
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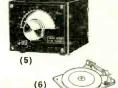
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