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aparto nio 111 0, DISS 0, EF92 3/- 10005	8/9	ŪC92	6/9
(DIN) EI 1001 11/- DE00 1/0 EF180 8/- 1000	0/0	UCC85	7/3
0 1000 1000 1000 DE00 1/- EF184 8/- F0104	8/3	UCF80	8/6
	8/6	UCH21	9/3
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full description

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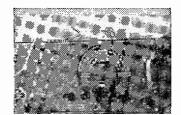
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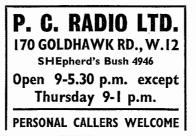
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SPECIAL 24 HOUR SERVICE OBSOLETE TYPESTA SPECIALITY Set of 24 Hour QUOTATIONS FOR ANY VALVE NOT LISTED Special 24 Hour DAF90, DF96, DF96, DL96 Set of 4, 19/- Postage 6d. per Valve C.W.O. No C.O.D. Express Mail AF114 9/- OC33 9/6 OC638 6/- Send S.A.E. for list Order Service Order Service AF116 9/- OC35 16/- OC812 4/- OC838 6/- Manufacturers and Export Inquiries Welcome Order Service OC25 11/- OC75 6/- OC812 6/- PLEASE NOTE OUR NEW ADDRESS Id/- OC75 6/- OC82 6/-						

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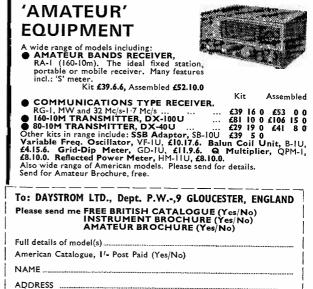
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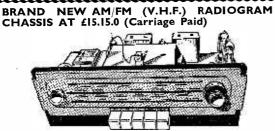
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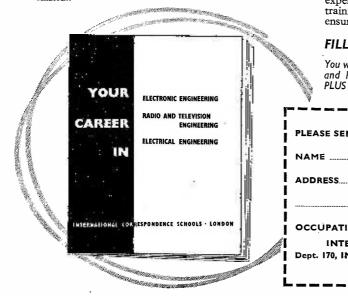
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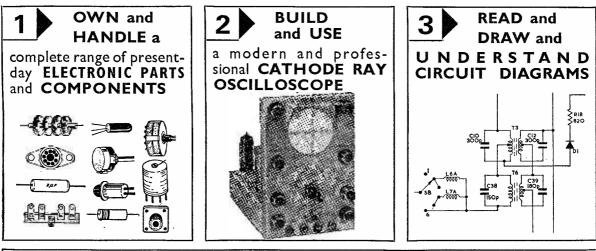


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SEPTEMBER 1966

issue 715

TOPIC OF THE MONTH

The Right Formula?

Nº a few weeks from now, the doors of the Earls Court Exhibition building will swing open and the turnstiles will begin clicking as the first visitors to the 1966 Radio Show pass into the halls.

After several years of travail and controversy, it may well be that at last some stability has been introduced into this important event in the calendar of the radio trade.

'Trade" is the key word. No longer have the organisers attempted to effect a compromise between a public exhibition and a trade show, a marriage in which incompatibility became increasingly manifest and has led to the inevitable divorce.

Changing patterns and balances dealt a death blow to the type of show which had prospered for so many years without much radical alteration, although many attempts were made to check the slide and to inject new zest into the enterprise. Either the signs were misread or the changes inadequate, for the Radio Show degenerated into the shambles of recent years with many companies mounting their own splinter exhibitions throughout London's hotel-land.

It emerged, however, that (1) Exhibitors found it more economical and profitable to restrict their shows exclusively to the trade, and (2) Foreign manufacturers could no longer be excluded. Arising from this, springs the 1966 Exhibition—a trade-only exhibition, with British and overseas manufacturers, under the same roof.

But although the conclusion is inevitably reached that a combined trade/public show is economically unviable is it, in fact, desirable or wise to abandon the traditional show?

Figures for attendances steadily declined. The public could see little more at the shows than they could in the radio shops and stores. Elaborate displays and entertainments were a financial luxury for the broadcasting organisations. And genuine radio enthusiasts found dwindling technical and hobbyist interest.

It seems, therefore, that the right solution has been found in dealing with the problem child of the industry. A few weeks hence, we will probably know.

W. N. STEVENS, Editor

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OCTOBER ISSUE WILL BE PUBLISHED ON SEPTEMBER 8th

All correspondence intended for the Editor should be addressed to: The Editor, "Practical Wireless", George Newnes Ltd., Tower House, Southampton Street, London, W.C.2. Phone: TEMple Bar 4363. Telegrams: Newnes Rand London. Subscription rates, including postage: 36s. per year to any part of the world. © George Newnes Ltd., 1966. Copyright in all drawings, photographs and articles published in "Practical Wireless" is specifically reserved throughout the countries signatory to the Berne Convention and the U.S.A. Reproductions or imitations of any of these are therefore expressly forbidden.

RACTICAL VOL 42 No 5

An Explanation

In response to my letter entitled "Any Offers?" in the February issue of PRACTICAL WIRELESS, I have received innumerable offers from readers all over Great Britain.

However, I have received an anonymous letter admonishing me of alleged misdemeanour and advising me not to live on others' gift subscriptions! If readers would carefully peruse my letter, they will note that I never expected anything free, and my proposition was strictly reciprocal. In fact, I have so far spent a little over the cost of a year's subscription in answering my correspondents and if anyone still thinks that this is a hell of a way of living on others' free gifts, he must surely be an imbecile.

Incidentally, I have since been authoritatively informed that contrary to my belief, technical publications are exempted from exchange restrictions. B. G. Kamath.

Bombay-52, India.

Rahble ?

IN reply to S. Peat on UHF and VHF Designs (P.W. March 1966).

A G8 licence may be an easier way to get a callsign, but to design, construct and operate equipment on u.h.f. is much more of a challenge.

At these frequencies, a hairpin can be a coil, two metal discs with an air gap a capacitor and the amateur has to be a highly proficient metalworker besides being able to solder.

This is the frontier of amateur radio communications and those of us who operate here are not following the wellworn pattern of proven design but are experimenting in the true spirit of amateur radio.

T. C. Challis, G8ALC.

Hull. East Yorkshire.

Transistor Solo Organ

I SHOULD like to thank you for publishing the above-mentioned article. Having built this organ, I then rearranged the circuitry by the addition of another oscillator taking the range to $4\frac{1}{2}$ octaves and added several other tonal effects, feeding each oscillator to a channel of a stereo amplifier, producing the bass section from one speaker and the treble from another. The result is startling with two hand playing-even if with only one finger of each hand.

J. C. Mitchell,

Wallasey, Cheshire.

NEWS AND ..



THE DUKE OF EDINBURGH VISITS MARCONI TEST SITE

The Duke of Edinburgh flew by helicopter the other week to Marconi's test site at Rivenhall. Essex, where he saw Britain's "break-through" in space communications overseas. He inspected the Cable and Wireless Ltd.'s satellite earth station undergoing tests at Marconi's and which has since been dismantled and shipped to Ascension Island, where it is to be used for Apollo "man-on-the-moon" communications. The photograph shows the Duke of Edinburgh chatting to engineers at the site. In the background can be seen the satellite earth station.

LOUDSPEAKER FROM RANK WHARFEDALE



First shown at this year's Audio Fair, Rank Wharfedale Ltd. have introduced a new 12in. bass unit to their range,

Retailing at £11 15s. the W12/FRS replaces the W12/PST and is the first chassis using Flexiprene cone surround to be offered to the public.

Bass units with Flexiprene are used in the Linton and Dovedale systems. When mounted in a suitable enclosure the W12/FRS will produce clean firm bass down to 25 c.p.s.

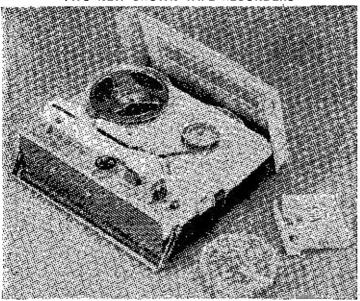
Bass resonance is 23/28 c/s. Flux density, 14,000 oersteds; total flux, 156,000 maxwells; baffle opening, 10% in.; chassis diam., 12% in.; pole size, 1≩in.; frequency range, 30–4,000 c/s and weight, 12 lbs.

RADIO TRADERS MOVE PREMISES

Radio Traders Ltd. (radio, electronic and electrical wholesalers) formerly of Tudor Place, W.1, have now moved to 8 Stephen St., Tottenham Court Rd., W.1 (Mus 4666). Radio Traders Ltd. have for many years served the trade with a wide variety of components. Enquiries for bulk and manufacturing quantities are invited.

...COMMENT

TWO NEW CROWN TAPE RECORDERS



Two new Crown portable tape recorders, model CTR 5450 and model CTR 3000 are introduced by the Heddon-Smith Group Ltd.

Model 5450—shown in the photograph—operates from four U2 cells or a.c. mains, is twin track, and has two speeds $1\frac{7}{8}$ and $3\frac{3}{4}$ i.p.s. Incorporating 5 transistors it takes up to 5in. spools and has 700mW output. It weighs 7.9 lbs. and measures $11\frac{1}{4} \times 8\frac{7}{8} \times 4\frac{3}{16}$ in. Price, complete with remote control dynamic microphone and magnetic earphone, is $29\frac{1}{2}$ guineas.

Model CTR 3000 incorporates 5 transistors, takes up to $3\frac{1}{4}$ in. spools and has an output of 800mW. It is twin track, has two speeds ($1\frac{1}{6}$ and $3\frac{3}{4}$ i.p.s.), weighs 5 1 lbs. and measures $8\frac{11}{16} \times 8\frac{9}{16} \times 3\frac{7}{16}$ in. Price complete with remote control microphone, magnetic earphone, 3in. reel and 3in. tape is 19 guineas.

UNISIL-CORED TRANSFORMERS AND CHOKES Belclere Company Limited, 385/387 Cowley Road, Oxford, have for the past few years produced a range of Transformer Design Kits. Up to the present, this range has consisted of three types of core: Mumetal, Radiometal and Silicor. Belclere have now added a fourth material—Unisil—to this range.

For power transformers the use of Unisil allows for an increase in output of approximately 25% compared with the Silicor equivalent.

Two leaflets have been printed describing the full range of sixty-two Transformer Design Kits available. These include full dimensional details and necessary design data. Should any reader require copies of these leaflets or details of "one off" transformers, write to Belclere direct.

WEATHER SATELLITE STATIONS

An order for five satellite receiving stations has been placed with Hawker Siddeley Dynamics Ltd.

The stations will be used at meteorological offices around the world to collect information transmitted from American weather satellites. The receivers will pick up television-type pictures of the earth and cloud formations as seen by the satellites' cameras 875 miles up.

International Short Wave Club

WE shall be pleased to send any readers a copy of "International Short Wave Radio" if they make application to the Secretary of the International Short Wave Club at the address below. Arthur E. Bear.

> 100 Adams Gardens Estate, London, S.E.16.

The Meaning of Amateur

YOUR correspondent Mr. R. Hasler has missed one point, and that is that amateur radio is still to a very large extent a "creative" hobby.

It is agreed that followers of other hobbies must of necessity purchase, say for example, a camera to enjoy the results to the full but nevertheless they get the creative end-product that they have set out to achieve.

I have never built a bike, nor knitted my own football socks (spare the thought!) but there are those amongst us who are unfortunately not in a position to enjoy the process of building their own equipment through some physical handicap but this does not detract from their "status" if you like, of amateur.

So, let us enjoy our QSO's during the coming years irrespective of whether our contact owns a "super XYZ at £2,000" or a "one-lung perker", meanwhile scanning the advertisement columns for hand-made bicycles and second-hand socks!

E. W. Bonson, G3JHY.

London, E.12.

Mobile Registration

MAY I be permitted to wonder if any of your readers are the owners of distinguished motor vehicle registrations, for example, EF 86, ECC 83 or even perhaps, now that 1966 is with us, OC 81D? **C. P. Finn.**

Tamworth, Staffordshire. Well, has anybody a distinguished registration number? We would be interested to hear of any.—Editor.

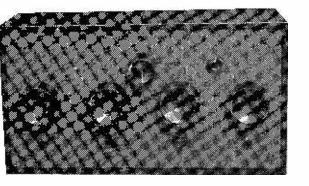
Correspondent Wanted

I WOULD like to correspond with somebody of my own age (14) who is interested in transistors and Hi-Fi. **Roger Murphy.**

203 Bills Lane, Shirley, Solihull, Warwickshire.

More News and Comment on Page 344





NE item that is essential in any audio workshop is a good quality audio mixer, this item enabling a number of individual sound sources to be "mixed" or added together to give a single, composite output; the volume level of each of the input channels can be individually controlled, to emphasise or minimise the presence of each channel on the final output, as required.

In practice, audio mixers vary considerably in quality and price, ranging from the simple "passive" types at a couple of pounds each, to the higher quality "active" types, having seven or more transistors, at prices in the order of £17 or more. The unit to be described fits into this latter category as far as quality is concerned, although, being home built, it can be constructed for a fraction of the "normal" retail price.

TYPES AVAILABLE

In view of the diversity of mixture types that are available, it is worth while digressing a little and explaining the basic principles of mixer circuitry, before dealing with the constructional aspects of the actual mixer that forms the basis of this article.

An example of the so called "passive" mixer circuit is shown in Fig. 1 and, as might be expected, the unit consists of a purely resistive network. For the sake of simplicity, only a 2-channel circuit is shown, one input being applied across R1 and the other across R5, while the output is taken from across R3.

The input that is applied across R1 is also connected across the series combination R2-R3, and causes a current to flow in both resistors. If the input equals 1 volt, the resultant current in each of these two resistors will be 10μ A since they total $100 \text{ k}\Omega$. Similarly, the input that is applied across R5 is also connected across the series combination R3-R4 and, if a 1 volt

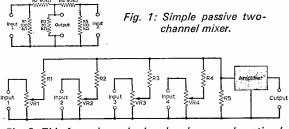


Fig. 2: This four-channel mixer has been made active by adding an amplifier.

Fig. 3: Block schematic diagram of the mixer described in this article shown on the right.

input is applied, a current of 10μ A will result through these two resistors. Thus, each input causes a current to flow in the common resistor, R3, and the total current through this resistor is proportional to the *sum* of the input signals. In the above example, the total current through R3 will be approx. 20μ A. It may be noted that, although this circuit is referred to as a "mixer", it is in fact an adding circuit.

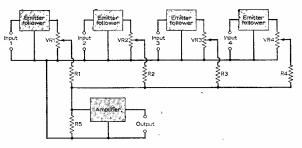
INTERACTION

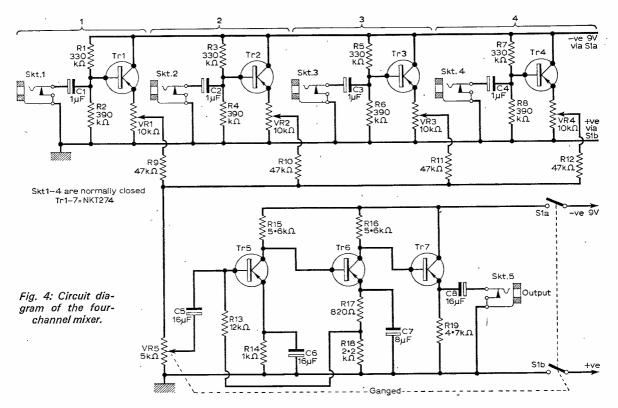
A certain amount of interaction takes place in these simple circuits, but can be minimised in a number of ways. The attenuation factor between input and output could for example, be increased by reducing the value of R3, and thus reducing the interaction between inputs at the expense of loss of signal strength at the output. Alternatively, the attenuation factor can be increased by increasing the values of R2 and R4, but in this case the reduction in interaction is obtained at the expense of an increase in the unwanted "noise" generated by the circuit. Again, the interaction can be reduced by reducing the values of R1 and R5, so that the attenuation factor between (say) input 1 and the output is unchanged, but the attenuation between the output and input 2 is increased, the reduction in interaction being obtained, in this case, at the expense of a reduction in input impedance to the mixer circuit.

Either of these methods may be used to reduce the interaction between inputs but each has its own particular disadvantages, and all practical designs are a compromise between the different "evils". Never-the-less, this "passive" mixer circuit is widely used in electronics, and forms the basis of *all* audio mixers, including "active" types, in general use.

ACTIVE MIXERS

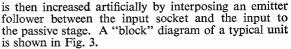
The next step up from the purely "passive" mixer involves adding an amplifier, using either valves or





transistors, connected between the output of the passive network and the output terminal of the complete unit, the amplifier being used merely to make up for the attenuation that normally occurs between the mixer input and output. A simplified diagram of a 4-channel active type of mixer is shown in Fig. 2. As can be seen, each input is applied to a variable resistor, giving individual volume control, and the required proportion of input signal is fed, via a series resistor (R1-R4) to the common resistor, R5, where the signals are added or "mixed". The resulting complex signal is then fed to the amplifier, which compensates for the loss of signal strength that occurred in the mixing stage, and the final compensated signal is fed on to the output terminal.

Finally, we come to what may be called the "high quality" types of mixer. Here, the "passive" section of the circuit is designed to give minimum noise, attenuation, and interaction, at the expense of reduced input impedance, and the actual input impedance to the unit



CIRCUIT DESCRIPTION

Each of the four emitter followers are identical. Taking input 1 as an example the signal is fed via blocking capacitor C1 to the base of Tr1, which is held at 4.5V by resistors R1 and R2 enabling input signals of up to approx. 8 volts peak-to-peak to be accommodated. The input impedance to each emitter follower is approx. $150k\Omega$, irrespective of the settings of the volume controls.

Each of the signals from the emitter follower stages is fed to the passive mixer, the "mixed" signal appearing across VR5. Transistors Tr5 and Tr6 are wired as common emitter amplifiers, using direct coupling to minimise the number of components. To give good d.c.

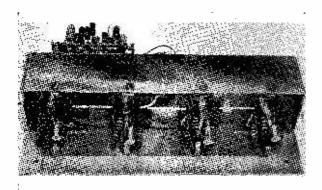
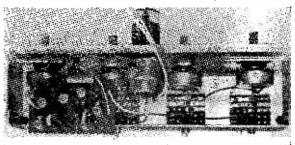


Fig. 5: Two views of the mixer. These should help the constructor locate the position of the major items.



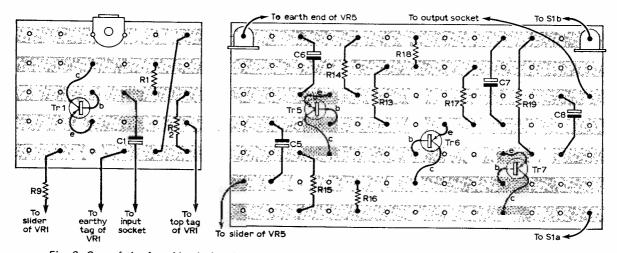


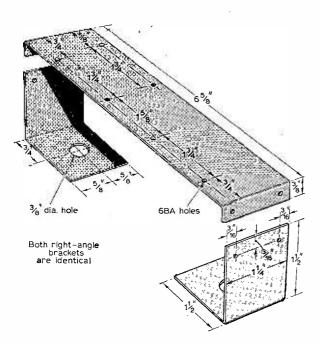
Fig. 6: One of the four identical emitter follower panels shown left along with the main amplifier panel.

and temperature stability, the base-bias to Tr5 is derived from the emitter circuit of Tr6, resulting in a d.c. negative feedback loop. Should the mean emitter current of Tr6 increase for any reason (such as a increase in ambient temperature), the negative voltage at the R17-R18 junction will increase, causing the mean emitter current of Tr5 to increase and the base voltage of Tr6 to fall.

The mixed and amplified signal that appears at Tr6 collector is directly coupled to the base of Tr7, another emitter follower stage, which gives a low impedance output.

CONSTRUCTION

Start construction by cutting the front panel to size. Then drill the holes for mounting the volume controls,



sockets, etc., as shown in Fig. 7. When this has been done, the panel can be finished off by covering it with Fablon or a similar self-adhesive plastic decorative material. At this stage, the five small jack sockets can be secured in place, the size and type being chosen to suit individual tastes.

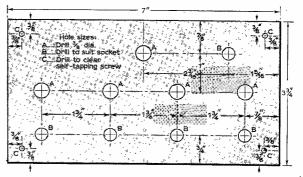
Next, cut the three small brackets to size, and bend and drill them as shown. Screw the three brackets together, and secure the resulting assembly to the front panel by means of VR1 and VR4, after first cutting the spindles of all five variable resistors to the lengths required by the front panel control knobs that are to be used. The remaining three volume controls can also be secured in place at this stage.

Make the four small emitter follower panels, as shown in Fig. 6a, first cutting the panels to size, then breaking the copper strips as shown with the aid of a small drill or the special cutting tool, and finally soldering the electronic components in place. When complete, bolt these panels in place on the main bracket.

Similarly, make up the main amplifier sub-panel, as shown in Fig. 6b, and, when complete, bolt it in place on the main bracket by means of the two modified solder tags.

Now complete the circuit by wiring up the interconnecting links, etc., as shown in Fig. 8, first soldering each of the input capacitors on the emitter follower panels to its respective input socket, and each of the

Fig. 7: Constructional details for the front panel and the brackets.



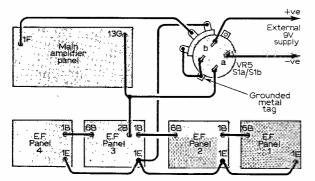


Fig. 8: Exploded view showing the internal connections.

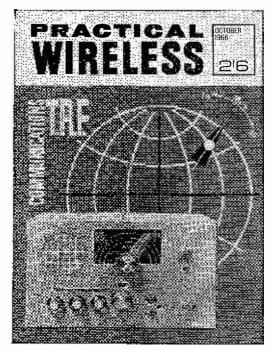
 $47k\Omega$ series resistors to the centre tag of its respective volume control. When the interconnecting leads have all been soldered in place, finish off by soldering a positive supply lead to the grounded metal tag on VR5, and solder one side of the negative line from the ON/OFF switch on VR5 to the relevant connections on the main amplifier panel and the emitter follower panel, and solder the external negative supply lead to the remaining tag on the ON/OFF switch.

The case can be made from either wood or metal, but must be provided with corner brackets to which the front panel can be screwed. When complete, the case may be covered with Fablon or a similar material.

comnonents list

<u> </u>	sompononto n	<u> </u>				
Resist	ions (all Lungth 100/					
RI	ors (all ¼ watt 10% 330kΩ	carbon	i): 47kΩ			
		RI2	47kΩ			
R2 R3	330kΩ	D 12	1240			
R4	390kΩ		l2kΩ lkΩ			
R5		RIS	5·6kΩ			
	390kΩ		5·6kΩ			
R7	330k Q	RI7	820.0			
R8	330kΩ 390kΩ	RIS	820Ω 2·2kΩ 4·7kΩ			
R9	47kΩ	RI9	4.7k Ω			
	47kΩ					
CI C2 C3 C4 C5 C6 C7 C8 Poten	$I_{\mu}F$ 12V electrolyt $I_{\mu}F$ 12V electrolyt $I_{\mu}F$ 12V electrolyt $I_{\mu}F$ 12V electrolyt $I_{6\mu}F$ 12V electroly $I_{6\mu}F$ 12V electrolyt $I_{6\mu}F$ 12V electro	ic ic ic rtic rtic ic rtic	10kΩ log 5kΩ log with switch			
Trans	istors (Newmarket):					
Trl	NKT274		NKT274			
	NKT274	Tr6	NKT274			
Tr3	NKT274	Tr7	NKT274			
Tr4	NKT274					
	Miscellaneous: SKTI)					
	2 Normally closed i	miniatu	re types to suit			
SKT	Gindividual require	ments	ie types to suit			
SKT4	SKT4					
SKT5. 9 volt battery, Veroboard, wire, solder, tags, etc.						

NEXT MONTH'S



COMMUNICATIONS T.R.F.

A highly selective and super-sensitive 6-stage unit covering 1.6-30 Mc/s. continuous in 3 switched bands. Receives 6 amateur bands, plus all short waves down to 10 metres and up to M.W. Light Programme. Completely self-contained, 12 x 8 x 7in.

GETTING GOING ON V.H.F.

This introduction to v.h.f. bands and techniques begins a new v.h.f. series.

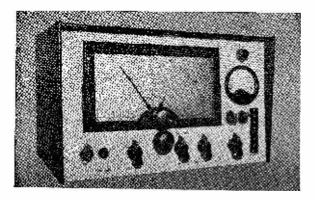
IMPROVING TRANSISTOR RADIOS

How to improve the cheaper transistor set. Covers better a.g.c.; adding diode output socket; extra r.f. amplifier and audio amplifier stage; battery economy.

FIVE-WATT AMPLIFIER

A compact 5-transistor 5-watt transformerless amplifier, built on a single board, measuring only $3\frac{1}{2} \times 2\frac{1}{4} \times 2\frac{1}{4}$ in., with constructional details for preamplifier and mains power supply unit.

OCTOBER ISSUE ON SALE SEPT. 8th ORDER YOUR COPY NOW !



THE "Ten-Five" was described initially in the October and November, 1964, issues of PRACTICAL WIRELESS. A further article suggesting minor changes appeared in the April, 1965 issue and in the November, 1965, constructional details were given for converting the "front end" to a much more efficient band-switched system.

Tr1 and Tr2 form, with their associated components, a tunable front end converter, producing a 1.6Mc/s output. One coil transformer only for each stage is shown, but fuller details relating to the section may be found in the November, 1965, issue.

After amplification by Tr3, the signal passes to the second mixer/oscillator, the 470kc/s output being fed to a two-stage i.f. amplifier Tr5, Tr6. The i.f. signal is demodulated by D2. The diode D3 acts as a series noise limiter, while D1 is an a.g.c. damping diode. Tr7 is a feedback oscillator, functioning as b.f.o. The audio amplifier consists of driver Tr8 and push-pull output Tr9, Tr10.

I.F. MODIFICATIONS

The new double-tuned i.f. transformers are fitted at i.f.t.1, i.f.t.2, i.f.t.3 and i.f.t.4. Transformers



A.S.CARPENTER G3TYJ

i.f.t.5 and T5 remain unchanged. Other circuit changes are made to the S-meter arrangement, the a.g.c. switching and the noise limiter circuitry. As far as possible, components bear their original references and most are identical. Some minor changes have been made, however, and a complete check is advisable. i.f.t. base connections are shown in the circuit diagram inset.

I.F. transformers 1 and 2 are tuned to 1.6Mc/s to feed transistor Tr4 and it may be noted that the fine tuner (TC4) which was previously connected to the front-end oscillator has now been moved and now may be used to vary the tuning of T4 slightly. T4 is normally fixed-tuned by means of C16, but TC4 proves additionally useful in cases where interference is experienced; it is also an aid to making c.w. and s.s.b. transmissions readable.

Damper diode, D1, is arranged to be non-conductive under weak or no signal conditions, its anode being held slightly negative with respect to its cathode by about 0.4V. If, with the a.g.c. switch set to "In" a strong transmission is tuned in, the base of Tr5 is driven in the positive direction and its collector current falls.

The resultant voltage change across R18 permits

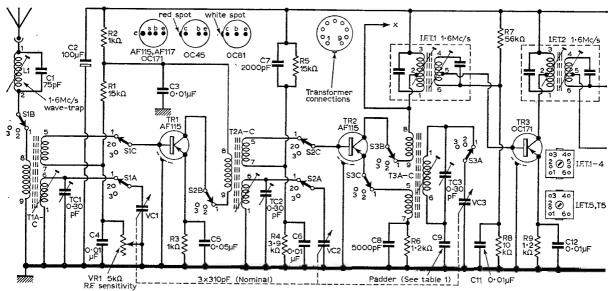


Fig. 1: Circuit of the bandswitched front end model. Only one transformer coil is shown in each stage in the interests of clarity.

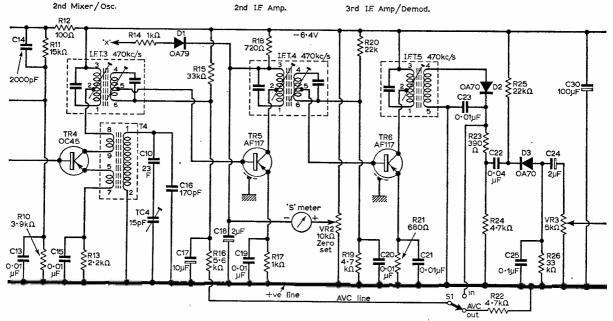


Fig. 2: The complete i.f. amplifier including second frequency changer/mixer.

the diode to conduct to damp the primary of the first i.f. transformer; the "S" meter balance as set by VR2, is also upset and the meter pointer moves across the scale in a forward reading direction by an amount depending on the strength of the received signal. The a.g.c. may be switched in and out irrespective of whether the b.f.o. is in circuit or not, switch S1 being in fact the item originally used in connection with the limiter. Here the revised limiter is left in circuit at all times diode D3 normally being conductive.

In the b.f.o. stage the pitch control is connected between the collector of Tr7 and the positive line yet is effectively across the main winding of T5when S2 is closed due to C30.

Demodulated output is available at the slider of gain control VR3.

AUDIO STAGES

These are almost unchanged. R38 value is increased. C30 and C31 are transposed. Sockets for use with a monitor volt-meter are provided across C34 and are essential when the receiver is to be run from a healthy 12V car battery—which might easily provide up to 14V under certain conditions.

The voltage reading will also be governed to a certain extent by the position of S3 since when on phone considerably less current is demanded; 10V maximum should be allowed. No meter need be used if the receiver is to be powered by a dry battery—a PP9 for example—which may be connected to the pole of S5 and earth, in which case the remainder of the circuitry can be omitted.

MAINS/BATTERY

By adding the circuitry shown in Fig. 3, optional a.c. mains or car battery powering becomes possible. In the latter case the voltage must be monitored as described above and kept under control by means of VR4. Great care to obtain correct polarity is required and connections should be in the sense shown.

When S5 is moved to position 2 the receiver may be powered from the domestic mains supply when S4 is closed to bring the panel-fitted neon to life. A d.c. potential of 9V is fed to positive and negative lines respectively and is obtained via mains transformer T8 and diodes D4 and D5 connected in a full-wave rectification circuit.

The receiver is prevented from functioning, however, if the rectifier diode cathodes are lifted from the positive line and this suggests a suitable muting circuit. No muting is necessary when the receiver is to be used purely for listening but when it is to work in conjunction with a transmitter some form of disabling circuit must be fitted to the front end or the r.f. transistors will be damaged.

In the prototype a flying lead is taken from pin 2 of the muting link socket to switch SF which is one section of a ganged Function switch contained within the transmitter. Pin 2 of the link plug is automatically grounded when SF is in the "Receive" and "Net" positions and as a result the receiver is made operative.

the receiver is made operative. Immediately "Transmit" is selected, however, the receiver supply is "killed" by breaking the +ve connection. To enable the receiver to remain operative when no transmitter is in use the muting link plug may be moved to connect points 1 and 3.

It should be noted that this muting system will not function when S5 is at "Battery" although it might be possible to achieve it by lifting the +ve terminal of SK1 and connecting it to pin 2 of the link socket. To date, however, the "Ten-Five" has not been used with a transmitter under /M or /P conditions, mainly due to laziness!

ALIGNMENT

Alignment has been dealt with previously and consists mainly of getting the i.f. stages "on the nose". Use of a signal generator with its output

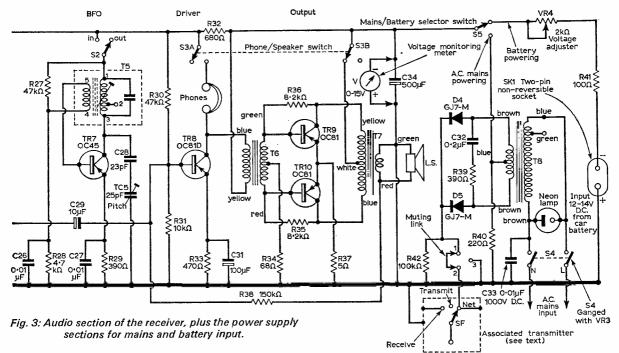


TABLE I Front end coverages

	Blue/Yellow transformers		White tran	nsformers
Maker's	Covera	ge	C9	Padder Pin No.
Range No.	Mc/s	Metres	00	
3	1.67–5.3	57–180	340pF	3
4	5.0-15.0	2060	960pF	4
5	10.5-31.5	9.5–28	2000pF	6 ¹

¹Automatic 2nd harmonic mixing occurs on this range

well attenuated is recommended, whereupon i.f.t.5, i.f.t.4 and i.f.t.3 in that order are peaked for maximum output at 470kc/s.

In the case of i.f.t.5 only one winding is tuned, whereas for all others two cores require adjustment. The core tuning the secondary—or base winding should be the first one attended to in each case and as small differences will occur the operation should be repeated several times to make certain no improvements can be made.

Reset the signal generator to 1.6Mc/s and inject this to the base circuit of Tr4, with TC4 set to half capacity. The core of T4 is then adjusted to resolve the signal, after which i.f.t.2 and i.f.t.1 may be attended to; the generator output being fed to the collector circuit of Tr2. At all times the signal generator output must be kept as low as is possible.

The b.f.o. is then switched in and the modulation switched out at the generator. TC5 is set to half mesh and the core of T5 adjusted until oscillation is heard. Careful manipulation of the core will now produce the desired zero beat, when the trimming tool may be removed. Subsequent rotation of TC5 slightly either side of centre should result in a beat

TABLE II Front end Tracking Points in Mc/s

Range	LF	LF	HF	HF
	Band	Tracking	Band	Tracking
	end	Point	end	Point
3	1·67	1·83	5·3	4·5
4	5·0	5·50	15·0	13·5
5	10·5	11·50	31·5	28·5

note of adjustable pitch being heard.

Normally the a.g.c. should be switched out when the b.f.o. is in use as it will be when receiving c.w. and single sideband transmissions.

FRONT-END ADJUSTMENT

Referring to Fig. 1, three transformer coils are required for each stage and these are coded blue in the case of T1A-C, yellow in the case of T2A-C and white for T3A-C. These are supplied by Denco and conform to the maker's range numbers 3, 4, 5. Trimmers (TC) are adjusted at the h.f. tracking points and the coil cores are adjusted at the l.f. tracking points on each range. Details are given in Tables I and II, with the full frequency ranges made available on each band. The core of coil L1 should be adjusted to produce minimum output at 1.6Mc/s.

Should overloading or blocking result on receipt of strong signals, exchange the $5k\Omega$ sensitivity control (VR1) for a 3.9k Ω fixed value resistor and fit instead an r.f. gain control in the form of a 100k Ω potentiometer wired as a variable resistor between one end of R1 (15k Ω) and pin 7, T₁A-C.

	ms not found in the original asign
Resistors:	-
R1 15kΩ	R22 4·7kΩ
B2 1kQ	*R23 390Ω
R3 $1k\Omega$	*R24 4·7kΩ
R4 $3.9k\Omega$	*R25 22kΩ
R5 15kΩ	*R26 33kΩ
R6 1·2kΩ	R27 22kΩ
R7 56kΩ	R28 4·7kΩ
R8 10kΩ	*R29 390Ω
*R9 1·2kΩ	R30 47kΩ
R10 3-9kΩ	R31 10kΩ
R11 15kΩ	R32 680Ω
R12 100Ω	*R33 470Ω
R13 2·2kΩ	R34 68Ω
R14 1kΩ	R35 8·2kΩ 5%
R15 33kΩ	R36 8·2kΩ 5%
*R16 5.6kΩ	R37 5Ω
R17 1 kΩ	*R38 150kΩ
R18 720Ω	R39 390Ω
R19 4·7kΩ	R40 220Ω
R20 22kΩ	*R41 100Ω
R21 680Ω	*R42 100kΩ
Capacitors:	
C1 75pF mica	
C2 100 μ F electrolytic 1	12V
C3 0.01μ F ceramic or	
C4 $0.01 \mu F$ ceramic or	
C5 0.05μ F paper	
C6 0.01 µF ceramic or	paper
C7 2000pF ceramic	
*C8 5000pF ceramic	
C9 See Table I	
*C10 23pF mica	
C11 0.01µF ceramic or	paper
C12 0 01 µF ceramic or	paper
C13 0.01µF ceramic or	paper
C14 2000pF ceramic	
C15 0.01 µF ceramic or	paper
*C16 170pF mica	
C17 10 μ F electrolytic 6	
*C18 2μ F electrolytic 6V.	
C19 0·01μF ceramic or	
C20 0.01μ F ceramic or	
C21 0.01μ F ceramic or	paper
*C22 0·04μF paper C23 0·01μF ceramic or	
*C24 2μ F electrolytic 6V.	
*C25 0.1μ F paper	,
C26 0.01μ F ceramic or	naner
C27 0.01μ F ceramic or	paper
C28 23pF mica	paper
C29 10µF electrolytic 6	V
*C30 100µF electrolytic	12V.
*C31 100µF electrolytic	
C32 0.2μ F paper	`
C33 0.01 µF paper 1000	DV.
C34 500 μ F electrolytic	
Variable capacitors:	· · · · · · · · · · · · · · · · · · ·
VC1/2/3 310pF (nom	inal) 3-gang tuning capacitor
Jackson ty	
*TC 0-30pF Beehive tr	immers (9)

*TC4 15pF variable "Air Tune" TC5 25pF variable "Air Tune" **Coils and Transformers:** *IFT1 I.F. transformer. Denco IFT18/1.6Mc/s *IFT2 I.F. transformer. Denco IFT18/1.6Mc/s *IFT3 I.F. transformer. Denco IFT18/470kc/s *IFT4 I.F. transformer. Denco IFT18/470kc/s *IFT5 I.F. transformer. Denco IFT14 The following are Miniature dual-purpose transistor coils by Denco. Range No. 3. Code Blue T1A Range No. 4. Code Blue T1B Range No. 5. Code Blue T1C T2A Range No. 3. Code Yellow T2B Range No. 4. Code Yellow T₂C Range No. 5. Code Yellow **T**3A Range No. 3. Code White тзв Range No. 4. Code White Range No. 5. Code White T3C Other Transformers: BFO I.F. transformer, Denco IFT14 **T**5 т6 Driver transformer, Ardente D3053 Τ7 Output transformer, Ardente D3027 Mains isolating transformer. MT9. (Norcol or Т8 Osmor) L1 Miniature dual-purpose valve type coil. Denco. Range 2. Code Red. Semiconductors: $\left. \begin{matrix} \text{OC81} \\ \text{OC81} \end{matrix} \right\} \text{matched}$ Tr1 AF115 Tr9 Tr10 Tr2 AF115 **OA79** Tr3 OC171 D1 **OA70** D2 OC45 Tr4 Tr5 AF117 **D**3 **OA70** D4 GJ7-M Tr6 AF117 GJ7-M Tr7 OC45 D5 OC81D Tr8 Switches:* *S1 Single-pole changeover *S2 Single-pole changeover *S3 2-pole, 2-way *S4 D.P. On/Off with VR3 *S5 Single-pole changeover **Potentiometers:** VR1 $5k\Omega$ VR3 5k Ω with switch S4 VR2 10kΩ VR4 2kΩ *Switch *S1A/B/C (Front-end). 3-wafer, 3-pole, *S2A/B/C 3-way rotary (Radiospares, etc.) Miscellaneous: *Meter (Miniature panel type, 200µA f.s.d) G. W. Smith & Co. Tag strips (10) Lektrokit LK-2231. Aerial socket. Non-reversible 2-pin socket. Phone and L.S. sockets. Transistor mounting clips for OC81's (2). Jackson "Caliband" dial and drive. Epicyclic reduction drive. Control knobs, *3-way muting link socket, sockets for monitoring voltmeter, *Neon warning lamp,

250V, Paxolin sheet 91 x 6 x 1 in., panel and cabinet

material. *Oddment aluminium 4 x $3\frac{1}{4}$ in. for coil pack,

solder tags, etc.



Now and again, some journalist "does a Gower", usually citing the involved clauseology of politico-legal regulations, and thundering "How is the man in the street expected to understand this?"

The short answer, of course, is that the man in the street can jolly well stay there—leaving legal arguments to those trained in the unravelling of complexities. But sometimes the charge comes nearer home, as when technical writers are accused of making their contributions too specialised and their language too introvertive.

The fun really begins when these specialists deliberately set out to confuse. An hilarious example occurred recently in "Systems and Communications", where readers were invited to provide their descriptions of a "Yack-Yack". They were assured it was a genuine device and given



Yak-Yak or baby alama

a single-sentence hint of its construction and use—deliberately vague.

The response was amazing! Some believed it to be a walkietalkie set, used in Tibet. Others said it was a "widget designed to

330

produce at the user's ears a sound field which exactly cancels unwanted external noise—such nagging wives". Many as plumped for a two-way telephone system for housewives, or even more way-out, mini-mothers-in-One brilliant inventor law. announced it to be a balanced Yaw-Assisted Cranium Kicker, which tended to keep the inebriated wanderer upright working on rectified brain waves.

The real Yack-Yack is almost as way-out as some of the inventive descriptions. It is an "undercom" for underwater communications between skin divers. It has a face mask with microphone and sound diffuser "to eliminate bubble noise", and a non-corrosive plastic case containing amplifier, battery and speaker. Range, 50 feet. Produced by Raytheon Ltd.

All very fine, but the absolute gem of a letter from S. E. Dinwiddy must be quoted in its entirety to prove my point:

"The information transponder receives dynamic aerial disturbance which it transduces into an electrical analogue which may be propagated along a conducting path to a corresponding installation. The device also contains the complementary transducer which re-transmits, providing conditions are acceptable, a recognisable imitation of the excitation presented to the remote installation.

The transducers are housed in a single module which rests on the second module of the installation when dormant. This second module contains an electro-acoustic transducer employed to attract attention in the event of a request for communication from a distant installation. It also contains a rotating perforated disc by the manipulation of which electrical impulses are transmitted to the complex intermediate apparatus by means of which communication may be effected to any one of a large number of similar apparatus in other locations.'

The example shows clearly what can be done to render a commonplace object practically unidentifiable by a straightforward factual description, using "plain" technical language. No gobbledygook; no copywriters' garblese. Yet the technical man, at whom other technical writers



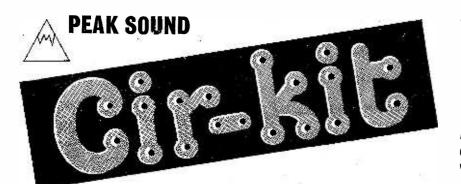
Down from their high horses

are aiming their contributions, finds it quite clear. Hence the stupidity of those who complain of the unintelligibility of technical articles, when they have not taken the trouble to learn the vocabulary.

We may mention that articles in *Practical* group magazines are deliberately written to be clear to both the technical man and the beginner, without boring the one by babytalk or confusing the other by unexplained terms. It often astounds me that some writers, whom I know personally, can get down so nimbly from their high horses of erudition and meet us common mortals elbow to elbow at the bar.

As a final note—the latest issue of S & C asks for descriptions of "A Whirley"—which is agile, weighs 833 tons and can be swept into position effortlessly. Henry can hardly wait for the answers.

Garblese



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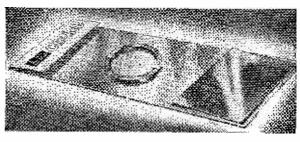
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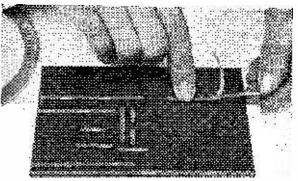
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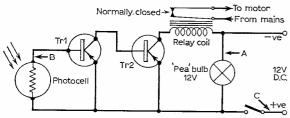
MODIFICATIONS

To add autostop facilities to a BSR tape deck . . .

PHOTOCELL plus a couple of inexpensive transistors, a lamp and a relay are all the components needed to add autostop facilities to a BSR tape deck. None of the components are critical and most readers should already have the items at hand. The relay will probably cause the most difficulty as it has to disconnect the power (mains voltage) to the tape motor.

Almost any photocell will do (the ORP12 is an example) and can be anchored by one of its lead wires to the pinch wheel assembly—see the accompanying illustrations. The lamp (a tiny "pea" bulb) is also anchored to the pinch wheel assembly, but in a position which puts the tape between it and the photocell.

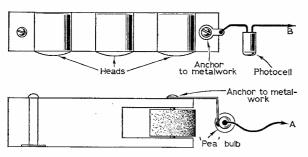
With the tape running from one spool to the other, the light to the photocell from the "pea" bulb is blocked by the tape and the circuit is



Circuit diagram of the autostop.

inoperative. When the leader portion of the tape (the translucent part at either end of the tape) passes between the photocell and lamp there is sufficient light to fire the photocell. This will switch on the control transistor Tr1, which in turn switches the other transistor on, allowing maximum current to flow through the relay coil which causes it to operate and break the power supply connections to the tape motor.

Since the pinch wheel is not brought up to the tape on fast wind, the sensitivity of the circuit is not so high as the lamp is further away from the photocell and the circuit will not operate until all the tape has passed the photocell.

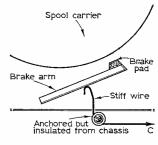


Location information for the photocell and the "pea" bulb.

The transistors are not at all critical and almost any p-n-p device can be used in the Tr1 position. In the other position, a power transistor is needed since it has to be able to draw enough current to operate the 12-volt relay. You may find it necessary to include another transistor to increase the sensitivity to the desired level. If this is the case, it should be inserted between Tr1 and Tr2: connecting the base to the collector of Tr1 and the emitter to the base of Tr2. The author used an OC72 in the Tr2 position.

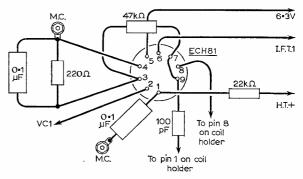
Power for the circuit is taken from a 12-volt battery, via a simple switch on the brake arm on the right-hand s p in d le which isolates the circuit when the control lever is in the central position.

C. R. Marflow



Alternative Frequency-Changer for the Progressive Short Wave Receiver

Since publishing the Progressive Short Wave Receiver in the February issue, the 12AH8 triode/ pentode valve specified for the front end has become difficult to obtain. An ECH81 may, however, be used in the V1 position, but the valve base wiring has to be modified and R1 has to be altered to $22k\Omega$.



The wiring alterations to the valve base are as follows: remove the chassis connection to pin 5 and connect to the 6.3V heater line: disconnection pin 9 from the heater line and connect it with a short lead to pin 7 on the same base. The diagram shows valveholder V1 modified for an ECH81.



THE receiver to be described was designed to provide efficient but inexpensive reception of the short wave bands without the use of cumbersome batteries which sooner or later (and usually at a most inconvenient time) require replacement.

The disadvantage of any basic $\hat{t}.r.f.$ is that it is relatively insensitive and not very selective, and ways and means have had to be sought to improve both state of affairs. The universal method is by feeding a portion of the amplified signal back to the grid and reamplifying it ad nauseum! In Fig. 1 this function is performed by L3 which is the reaction coil, and which must be connected so that the feedback is positive; i.e., in phase with the signal at the grid of V1.

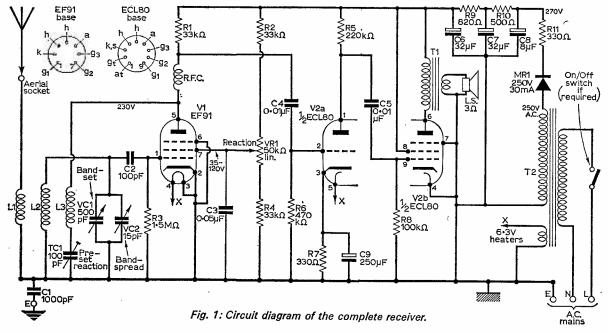
The feedback must be made variable so that it can at all times be kept just, and only just, below the point of oscillation at which point both sensitivity and selectivity are at optimum. There are two ways of performing this function, one is by making the trimmer TCI a variable and using it to adjust the reaction, and the other (which is used in this design) in which TC1 is adjusted initially and then subsequent reaction is controlled by the potentiometer in the screen grid of V1. By varying



the potential applied to the screen of V1 we can vary the gain much more smoothly.

Referring to VC1, the greater the band-width covered and the smaller the separation between adjacent stations for every degree of rotation, making it extremely difficult to separate stations who may be separated by only a few kc/s or so. Fortunately, the addition of another tuning capacitor connected in parallel with the main tuning capacitor (VC1), and having a total capacity much less than the former, can considerably assist tuning. The frequency shift is therefore related to the difference in capacity between the main or bandset capacitor and the ancillary or bandspread capacitor.

The anode load of V1 is composed of an r.f. choke and a resistor R1 in series. R.F.C. forms the r.f. anode load across which the feedback voltage is developed. Its inductive reactance is very high to







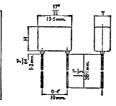
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Cap. μF	н.	т.	Type No.
0.01	<u>;</u> ;,″ 9mm	32 ″ 5.5mm	PM XI
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0.047	<u>₩</u> 9mm	7/32 5.5mm	РМХЗ
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Insulation Resistance:

Terminations:

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Finish:

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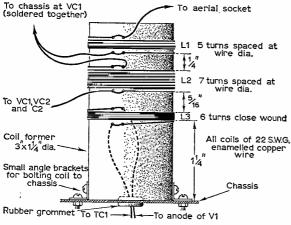
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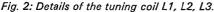


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r.f. signal but negligible at a.f. and so R1 is included across which the a.f. voltage is developed. This a.f. voltage is derived from the rectification of the modulated r.f. voltage by the grid and cathode of V1 acting as a diode in parallel with the tuned winding L2. This type of detector is commonly called the grid leak detector.

From the junction of R1 and r.f.c. the a.f. voltage is passed, via C4, to the grid of V2a which is the triode portion of the ECL80 triode pentode audio amplifier. V2b is the power output stage, having as its anode load the primary of the output





transformer, the secondary of which feeds a small loudspeaker.

As far as valves are concerned, we need only consider V1 because on its characteristics will depend the ultimate performance of the receiver. An EF91 was chosen for this position because it has an excellent r.f. performance and can be purchased very cheaply indeed. Identical replacements are Z77, 6AM6, 6F12, CV138 and 8D3.

All the components to be used should be to hand before any attempt is made at constructing the chassis and front panel so that any changes necessary due to a difference in component size can be allowed for. Both the chassis and front panel were made from 18 s.w.g. aluminium, although brass or tinplate could be used with the advantage that all earth connections could be soldered directly to the metalwork. After all the holes have been made the chassis and panel may either be paint sprayed or given a crackle finish. Suitable transfers may be fitted to the front panel giving the unit a really smart finish.

COIL WINDING

The aerial coupling, tuning and reaction windings are all wound on the same former which should be 3in. long with an outside diameter of $1\frac{1}{4}$ in. The wire used was 28 s.w.g. enamelled wire, but this is not critical and other gauges not too far removed from 28 would prove acceptable.

L3 should be wound first and in order to do so two small holes should be pierced in the coil former about 1/8in. apart as in Fig. 2. The end of the wire is threaded through the two holes two or three times to hold it firm and then six complete turns are wound tightly on side by side or "close wound". Two further holes are pierced and the wire threaded through as before. About 6in. should be left at both ends to connect to anode of V1 and to TC1.

L2 is next to be wound and to do this a further pair of holes should be pierced 5/16in. away from L3. The winding is wound in the same direction as L3, but the turns are spaced from each other by the diameter of the wire. Seven complete turns are wound tightly on and a further pair of holes pierced through which the end is threaded. The ends of this winding can be about 4in. long.

L1 is wound in the same manner as L2 but is spaced from it by 1/4in. The start of L1 can be left about 4in. long but the finish should be left some 8in. long so that it can be soldered directly to the aerial input socket. Results comparable to those obtained with the prototype will only be obtained when the coil is wound exactly as the original, but, and this is an important but, results will still be obtained if individual coils vary in diameter, coil spacing, wire diameter and wire spacing.

Actual construction can commence with the fitting of all major components except the coil which should be left until last. The coil is bolted coaxially about a grommet through which

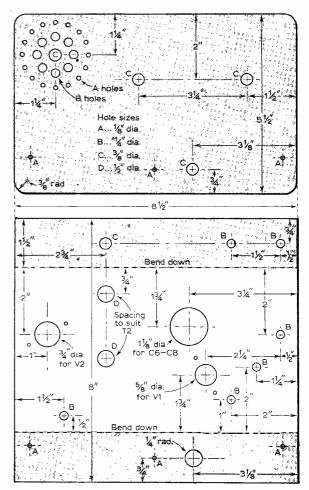


Fig. 3: Layout and drilling details of the front panel and chassis.

the lead out wires from L3 only are passed, thus separating the inputs and outputs and permitting the feedback to be closely controlled. This reaction winding L3 must be correctly wired otherwise feedback will be out of phase or degenerative. The other end of L3 is soldered to TC1 which is bolted to the chassis using one of the 6BA nuts and bolts that are used to bolt the coil above chassis.

The power supply section should be completed first and to this end one side of the heater winding and one side of the h.t. winding should be connected to chassis. It is important to connect the metal rectifier correctly because the application of an incorrect *negative* voltage to the positive side of the reservoir and smoothing capacitors will cause damage. The metal rectifier will also be damaged.

If the front panel and chassis have been sprayed, it is essential to carefully scrape the paint away, leaving bright clean metal before the earth tags are bolted on, as faulty earth connections can give rise to a host of troubles ranging from failure to weak signals or incipient instability, this latter effect manifesting itself as a host of minor whistles where transmissions ought to be.

WIRING OF V2

With the completion of the power supply and r.f. stage wiring, attention can be turned to the audio stages as represented by V2. Pins 4 and 7 of V2, together with its centre skirt, are earthed to a separate earth tag bolted under one of the transformers securing 4BA nuts and bolts. This helps to reduce congestion round V2. The anode of V2b is connected to the primary of T1 by a short length of insulated wire, passing it through the same grommet as the h.t. feed to the other side of the primary. Pin 8 is the screen grid of V2b and makes

a convenient tie point for the h.t. lead to the primary of T1 and R5. Above chassis wiring is simple,

but as it is all "tuning" wiring some extra care is worth while. 20 s.w.g. tinned copper wire was used on the prototype covered with sleeving except where the coils' lead out wires were concerned. These were carefully scraped free of enamel and thoroughly tinned with solder and then connected as follows. The "start" of L1 was taken through the grommet, suitably sleeved, and soldered on to the aerial socket. The "finish" of L1 and the "start" of L2 were scraped carefully free of enamel, twisted together, tinned, and soldered to the earth tag or rotor tag of VC1. The "finish" of L2 is soldered to the stator tag of VC1 from which point a short length of sleeved s.w.g. tinned copper wire is soldered to the stator tag of VC2. L3 has been already

Fig. 4: Underchassis wiring diagram showing positioning of the main wiring. Important. Note the polarity of the midget contact-cooled rectifier MR1.

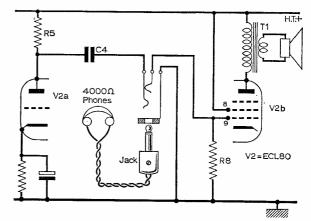
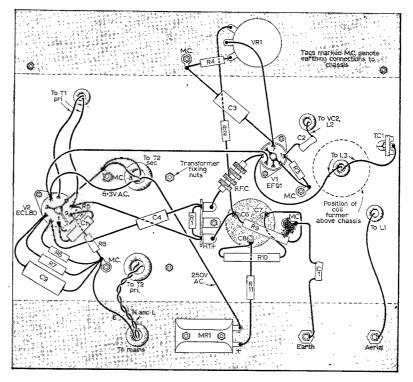


Fig. 5: Simple modification for the inclusion of a jack socket for headphone reception. Phones should be high impedance.

dealt with and need not concern us any further. The importance of making sound soldered joints cannot be over emphasised if the r.f. section is to work at maximum efficiency, and this it will be unable to do if "dry" or high resistance joints are present.

Following completion, a close recheck of all wiring is essential, particularly round the h.t. line, and an ohmmeter check between all "line" points and chassis is very desirable. The initial reading will be a very low resistance one due to the current drawn by the smoothing capacitors, but this should gradually increase to a reading of about $100k\Omega$.

Once the set has been checked and found satisfactory, the mains can be connected and preliminary tests initiated. Prior to the mains being connected, TC1 should be fully unscrewed so that its capacitance is at minimum. VC1 and VC2 should



be set at maximum capacity and VR1 rotated anticlockwise so that its wiper is at the tag connected to R4. The mains can now be connected and a short while after a rustling noise and possibly a faint amount of hum should be heard from the loudspeaker. VR1 should now be advanced slowly towards its fully clockwise position at which point some signals may be heard, assuming, of course, that an aerial has also been plugged into the aerial socket. If signals cannot be heard by rotating VC2, the bandspread capacitor, TC1, should be slowly screwed in to increase its capacity until signals can be heard on rotating VC2. VR1 should now be backed off slightly and TC1 again slowly screwed in until signals can be heard. The screen grid voltage of V1 should now be in the region of 120Vand TC1 can be assumed to be finally adjusted and all subsequent reaction controlled by VR1. As the frequency is increased by unmeshing VC1, the reaction control VR1 will require adjusting in an anticlockwise direction. The ideal range of VR1 is from excessive reaction at the low frequency end of the band to the high frequency end, at its most clockwise or maximum position, to insufficient reaction at its anticlockwise or minimum position. If reaction cannot be obtained with VR1 fully clockwise and TC1 fully tightened up, the coil connections are wrong and the leads from L3 to V1 anode and TC1 will have to be transposed. The mains should be disconnected for this operation and VR1 and TC1 returned to minimum. Upon reconnecting the mains, the reaction circuit should function normally.

FREQUENCY CHECKING

Unless it is desired to cover a particular bandwidth, the receiver can be considered as being fully operational. If a signal generator is available, dial calibration can be checked easily and quickly. If not, reliance will have to be placed on transmissions for calibration. One of the greatest disadvantages common to all simple t.r.f. receivers employing reaction is that the feedback voltage varies with frequency, necessitating an adjustment to the reaction control every time the frequency is changed. This is a fundamental difficulty and one the individual will have to accept if he is to make the most of his own set. The point of optimum sensitivity is when the set is just, and only just, below the point of oscillation. If the reaction is advanced to the point where the set actually oscillates all that will be heard is a high pitched hiss and whistles wherever there is a transmission. If the reaction is not sufficiently advanced only very strong transmissions, or perhaps no transmissions at all, will be heard. The point of correct reaction can be easily determined by slowly advancing the control until a "plop" is heard followed by a hiss and whistles. This is excessive reaction and the control should be "backed off" to a point where the set does not go "plop", and transmissions of voice, music and morse should be heard naturally. The reception of morse is often improved by employing fractionally excessive reaction.

A headphone jack can be easily incorporated between V2a and V2b as shown in Fig. 5 so that with the jack withdrawn the signal from V2a is fed normally, via C4, to V2b when the jack is inserted the connection is broken and the signal is fed to

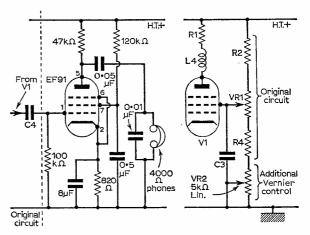


Fig. 6 (left) One way to run headphones only. The EF91 replaces V2.

Fig. 7 (right) Modification for Vernier reaction control.

the headphones instead of V2b thereby muting the speaker (and output stage).

An essential requirement is that the grid leak of V2b, which is R8, must be wired as originally, that is on to the grid pin.

The last modification is a somewhat unusual one and concerns the incorporation of a vernier reaction control; Fig. 7 shows how this can be done.

It makes the adjustment of optimum reaction quite easy, a feature that will be much appreciated when very weak stations are being sought.

Every receiver from the very simple to the very complex benefits from the use of a really first-class aerial and earth system, though both do not, unfortunately, receive the attention they deserve.

★ components list

R1	0% <u>‡</u> W exc 33 kΩ	ept where s R7	33	0Ω			
R2	33 kΩ	R8					
R3	1·5 MΩ	R9	82	0Ω 3W wire wound			
	33 kΩ	R10	50	0 Ω3W wire wound			
R5	220 kΩ	R11	- 33	0Ω wire wound			
R6	470 kΩ	VR1	50	$k\Omega$ wire wound			
	itors:						
C1	1000pF		C9				
	100pF			500pF			
C3	0∙05µF	,	VC2	15pF			
C4	0·01µF		TC1	100pF Pre-Set			
	0·01µF						
C6	$32\mu F$ $32\mu F$ Co	mmon					
C7	$32\mu F \succ Co$		~				
C8	8μF J ^{Ca}	n electrolyti	C				
Misce	lianeous:						
T1 40: 1 o/p transformer, 3 ohms Sec'							
T2	T2 PRi. 240V Sec. 250V at 30mA 6.3V at 1A.						
L1 L	L1 L2 L3 See Text.						
MR1 Contact Cooled rectifier 250V at 30mA.							
L.S.	L.S. 3 ohms 23 in. square.						
R.F.	C. Short Wa	ave R.F. Ch	oke.				
Valve	s:						
V1	EF91. 6A	M6 V2	ECI	_80			

*A.C. PROBE *AUDIO MONITOR

HREE items of test gear are described in this article—an a.c. probe with a 100mV sensitivity in the frequency range 3kc/s to 30Mc/s, a simple audio frequency monitor that will respond to 1mV signal level changes and a 16 to 64Mc/s receiver-oscillator. None of these instruments require expensive components such as moving coil meter movements and all use cheap transistors. A little ingenuity is, however, required in the construction, particularly when putting the r.f. probe together, since part of an old gas lighter refill holds most of the components.

A.C. PROBE

This general purpose instrument is designed to indicate visually the presence of audio or radio frequency voltages in a circuit under test. The sensitivity is such that a clear response can be obtained from signals of less than 100 millivolts in the frequency range 3kc/s-30Mc/s.

Unlike the familiar signal tracer, which relies on audible detection of the signal, unmodulated r.f. may be checked by this probe. The input is deliberately attenuated at low audio frequencies to enable much higher voltages to be inspected without overloading the instrument; even mains supplies can be tested.

A typical application of the instrument is to check if the oscillator of a superhet receiver is functioning. If the probe needle is touched on the oscillator section terminal of the tuning capacitor the torch bulb should glow brightly if all is well. Similarly, the glow of the bulb can give a useful indication of the comparative output of a radio control transmitter, and will check the quench action of a super-regenerative receiver. To achieve minimum circuit loading and self-capacitance, the torch may be held in the fingertips by its plastic reflector holder, instead of by the metal barrel.

Circuit Description

From the circuit diagram, illustrated in Fig. 1, it can be seen that two transistors are d.c. coupled in a Darlington Pair configuration, with the bulb load in the common supply line, providing a degree of negative feedback. Additional thermal stability results from the diodes D1 and D2 across the baseemitter junctions of the transistors. These diodes

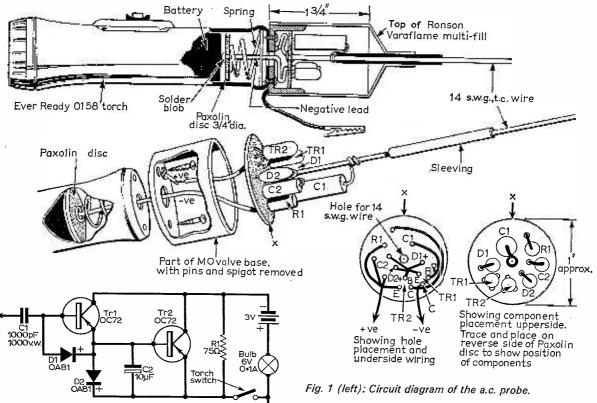


Fig. 2 (above): Constructional details of the a.c. probe.



also rectify the signal. Resistor R1 is selected to bias the bulb so that it will just glow faintly with no input applied. In the original circuit a resistor of 75 ohms was used, but variations between individual bulbs may necessitate a slightly different value.

The earth return lead can be dispensed with when measuring r.f., and also when testing mains supplies, but it should be brought into use for low level audio checks. The bulb specified was found to give the best all round results and is of the type normally used in bicycle dynamo front lamps.

Probe Construction

Constructional details of the probe are given in Fig. 2. The torch is drilled at the battery end to take self-tapping screws and the negative battery lead. A paxolin disc is placed between the battery spring and battery case. This is fitted with a flexible lead and retained by a generous blob of solder which makes contact with the negative end of the battery. The centre spigot and pins are removed from a Mazda octal valve base—taken from an old valve of the ARP 12 variety—and this is retained on the end of the torch by self-tapping screws.

A used Ronson lighter refill is first shaken to ensure that no liquid fuel remains inside. If not, the contents may be emptied into a lighter. Residual pressure in the refill is released by inserting a 1/16in. drill into the rubber valve and twisting until the hissing stops. BE VERY CAREFUL AS THIS OPERATION CAN BE DANGEROUS. The drill's grooves provide a gap for the gas to escape freely and the operation should be performed well away from naked flames. When the refill is completely de-pressurized, the alloy body may be cut with a fine saw to form a cap. After the burr has been removed with sandpaper or a file, the cap should be found to be a good force fit on the valve base. If it is too tight the base may be lightly sanded. The valve portion of the refill is finally drilled out to take the probe needle insulating sleeve.

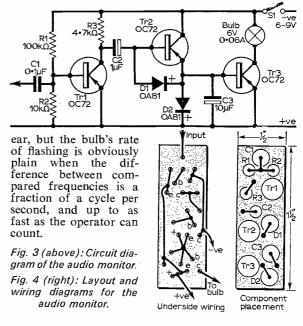
A disc of paxolin, approximately 1in. in diameter, is cut and filed to suit the inside of the valve base and is then drilled as shown in the placement diagrams in Fig. 2. If desired, the disc could be copper clad on one side and etched to make a circuit, but with the prototype the component's leads were inserted in the holes, bent over and soldered together. To ensure correct positioning of components, a tracing may be made from the placement diagram and pasted on the upperside of the drilled disc. This can be torn away after construction is completed.

One must ensure that Cl has an adequate voltage rating, and that the insulation of the probe needle is impeccable if the instrument is to be used at mains voltages. The value for Cl, 0.001μ F, represents a reactance greater than 3M Ω at 50c/s, reducing to about 30k Ω at 5kc/s. If a flat response is required down to the low audio frequencies Cl may be increased in value to, say, 0.1μ F, but the instrument must not then be used for mains checking as the high voltage input would severely overload the circuit.

AUDIO MONITOR

The circuit shown in Fig. 3 is a straightforward development of that given in Fig. 1. Here the bulb is employed as the collector load of Tr3 and a stage of a.f. amplification has been added. The monitor may be used as a modulation peak level indicator in tape recorders and portable transmitters; the complete unit occupying much less space than a meter. Other possible applications are as a null detector in a c.r. bridge, and as a pulse rate monitor in a simple Geiger counter. Response to a signal is unambiguous and changes of less than **1mV** in signal level are discernible. As a rough indication of sensitivity, when a crystal microphone insert is connected directly to the input of the monitor the bulb will flash brightly in response to a human whistle five yards away. Standing current is around 10mA, rising to approximately 100mA on signal peaks.

When comparing close audio frequencies, both may be simultaneously fed into the monitor and the slow resulting beats counted and timed with a stopwatch, giving an exact determination of frequency when one of the inputs is a closely controlled standard, such as the 1000c/s tone radiated by the BBC at commencement of transmissions. This is more positive than aural methods since beats of only a few cycles per second are not easily resolved by either ordinary amplifying equipment or the human



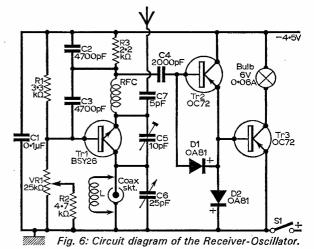
On 9 volts the bulb will be overrun at high input levels. This was not thought to be critical as such levels would seldom be sustained for lengthy periods and bulb replacement could hardly be termed expensive. However, when running with large inputs Tr2 and Tr3 tend to warm up and, with d.c. coupling, their leakage current increases. Under such conditions the bulb will not extinguish completely when the signal is removed, until the transistors have had a chance to cool. To minimise this effect, Tr2 and Tr3 may be fitted with heat sinks, when the application demands continuous illumination of the bulb.

In this case, construction is almost certain to be a matter of individual preference as the unit would normally be incorporated with some larger item of equipment. As a guide the layout of the prototype, on a paxolin panel measuring $1\frac{1}{2}$ " x $\frac{1}{2}$ ", is given in Fig. 4.

If a light dependant resistor is coupled to the bulb this can be used as a noiseless, remote volume control in an amplifier or radio receiver. A small a.c. voltage injected into the monitor will control the effective resistance of the LDR, and a feedback loop can be arranged to provide volume compression.

RECEIVER-OSCILLATOR

Anyone who has tried winding their own coils will appreciate the usefulness of an instrument which confirms that n turns on a d diameter former do, in fact, produce the required value of inductance. When a radio control receiver is first constructed its tuned circuit, or circuits, may peak many megacycles above or below the allotted band. Without a signal generator or grid-dip meter, much time can be spent screwing cores in and out, in the hope that at a certain stage in the proceedings the receiver will respond to a nearby transmitter, assuming that the transmitter is on frequency also. The major problem with most types of home-built frequency standards is that of initial calibration, and the same applies to conventional short-wave receivers. Although a dial marked 0-100 may look good, it is better to know what the divisions represent in terms of megacycles or metres.



With little more than a simple 1Mc/s crystal marker and a length of wire, the Receiver-Oscillator may be accurately calibrated for use as a frequency sub-standard, to check the resonance of both passive and active tuned circuits. In other words, the instrument has more uses than can be listed here. Sufficient to say that it may be utilized to test field strength meters; receivers, oscillators, TV, many instruments, and will stand-in as a signal generator. Even if a signal generator is already available, together with a wide range communications receiver, it is often quite useful to have a means of duplicat-

Circuit Description

piece of equipment to another.

The super-regenerative detector offers a convenient and simple way of arranging for twoterminal plug-in coils, with one end of the winding earthed. It is also highly sensitive, and with careful design will cover a wide frequency range without complicated switching and adjustments.

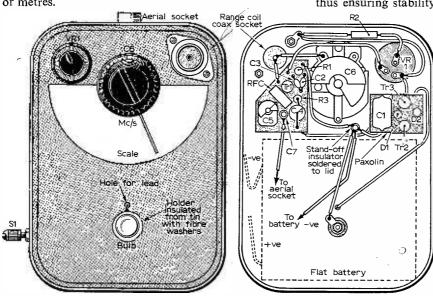
ing their functions, or to transfer a signal from one

The circuit, Fig. 6, gives the salient details. An n-p-n epitaxial transistor is used for Tr1, allowing the coil L to be connected directly to the earth rail, thus ensuring stability and ease of operation. These

transistors are now readily a v a i l a b l e at moderate prices and give excellent results.

The unusual point about the circuit is that the quench frequency, arising from the mode of operation, is used to bias the bulb amplifier; via C4 from the emitter network of Tr1, and is controlled by VR1, which also determines the operating point of the detector, and hence its sensitivity. If VR1 is fully advanced to its minimum resistance position

Fig. 5: Constructional diagrams of the Receiver-Oscillator. Range scale and coilwinding details are included in Fig. 7.



the quench disappears and the circuit oscillates only at r.f. The feedback trimmer C5, once set, can be left alone and the instrument will operate quite successfully over the entire frequency range-with or without quench-covered by adjustment of the main tuning control C6 and non-critical rotation of VR1. The choice of range, 16-64 Mc/s, may appear arbitrary, but this covers those frequencies not normally to be found on ordinary short-wave receivers, to link up with the lower television bands, and also embraces model control, two amateur bands and the Industrial, Scientific, and Medical allocation at 40.68 Mc/s. If switched values for C5 can be tolerated then the instrument could be made to cover 10-150Mc/s, but tests indicate that operation at those limits would tend to be critical. Many circuits claim to cover a wide range but this desirable end is seldom achieved without complexity or unreliable operation.

It will be noted that the electrolytic capacitor, shown in the previous circuits, across the baseemitter junction of the output transistor, has been omitted. This is to allow a pair of low-impedance headphones to be connected in place of the bulb for the purpose of identifying certain signals when calibrating the instrument. Without the electrolytic capacitor, the bulb current consists of rectified a.c., resulting in slightly less brilliance, but this has no important effect on performance.

The circuit is not at all critical where component spreads are concerned. The r.f.c. may be pile wound, with one or two hundred turns of 40 s.w.g. wire on the body of a miniature resistor, or can be a pi winding taken from a small medium wave coil or an i.f. transformer, as in the original. Provision for an aerial is made, feeding via 5pF capacitor C7 into the low impedance side of Tr1. Even if the aerial socket is shorted to earth no resetting of the dial is necessary to compensate for frequency variation with load, hence this socket may be confidently used both as an input and output without impairing the instrument's accuracy.

Construction

A 2oz. tobacco tin is not the most ample of all-metal containers, even if it is easy to come by, consequently a slightly unconventional mode of assembly was resorted to when building the instrument, allowing for the fact that most of the internal space was taken up by a large long-life battery. The 25pF capacitor, C6, could just be accommodated without packing under its bush so a thick paxolin panel was out of the question; C6, VR1, coaxial coil socket, and bulb holder were mounted as shown in Fig 5. After a certain amount of brooding and twiddling of spindles it was realised that the only space left for wired components were two disconcertingly small areas of bare metal on either side of C6, squeezed between the battery, VR1 and socket. In response to this challenge, two pieces of paxolin were cut and drilled and after the components were mounted, soldered, and tested, these panels were glued to thin pieces of foam plastic which were then, in turn, glued to the tin-lid in the positions shown in Fig. 5. With the battery in place there was not even enough room for the most miniature of switches so S1 was made up with a 6BA screw and nuts, soldered to the side of the tin, so that when screwed in it shorts the positive terminal of the battery to the instrument's case.

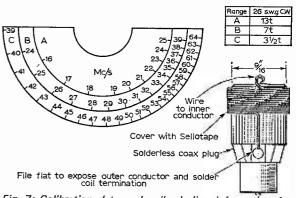


Fig. 7: Calibration data and coil-winding information for the Receiver-Oscillator.

Three coils were wound, according to Fig. 7, on a modified Radiospares 'Normal' coaxial plug, with 26 s.w.g. enamelled wire. Part of the plug outercasing is filed away to expose the outer conductor and the end of the enamelled wire-after being scraped clean-is soldered to this before winding the coil. Also, a length of insulated 20 s.w.g. wire is fitted to the centre conductor by means of the solderless connector supplied with the plug, as a winding anchorage. The prototype's scale is given as a guide and may be referred to when calibrating the instrument. The rest of the construction and link-up wiring should be plain from the diagrams. C5 is a miniature solid-vane printed-circuit trimmer, but if its replica cannot be found, two insulated wires, twisted together, may be used in place of C5 as the value of capacitance required is only a few pF. C2 and C3 are very small high K ceramic subminiature capacitors. All resistors used were also subminiature types.

Calibration and Use

The battery may be temporarily connected to negative lead and tin-lid, and coil 'A' inserted in its socket. Rotation of VR1 should cause the bulb to glow. If not, the wiring must be re-checked, and a signal can be applied from an audio oscillator to the base of Tr2 to ensure that bulb and associated amplifier are working. C5 is set to the midcapacitance position and can be used later to shift the dial calibration points so that the ranges meet or overlap slightly. Even with the vanes fully out of mesh, however, the original circuit oscillated reliably.

When the bulb lights, back off VR1 to approximately half brilliance and then couple the aerial socket to a 1Mc/s crystal marker. The bulb's glow should peak up sharply at each 1Mc/s division as C6 is slowly rotated. If a piece of paper is lightly glued to the lid, the points of maximum brilliance may be marked with a pencil.

Repeat the procedure for coils B and C, slightly re-adjusting VR1 to maintain maximum sensitivity at different dial settings. The resulting scale should consist of a number of regular pencil marks, with a taper towards closer spacing at the high frequency end of the dial, representing 1 Mc/s intervals. To identify the marks numerically, plug in coil C and about two yards of aerial. Replace the bulb with a

-continued on page 351

In answer to Henry

ON opening my copy of PRACTICAL WIRELESS this month, I was shattered to find that Henry had done me the honour of bringing his big guns to bear on me and my "polite reprimand". Did I really stick my neck out that far? Rallying from the shock however, I take my courage in both hands and a pen in one and set out to defend myself.

Given Henry's fuller explanation of the more sophisticated uses to which synthesisers may be put. I see where the misunderstanding has arisen. In his first article, Henry said: "By transmitting a great number of channels simultaneously" whereas, in his second, he modifies the description to "both transmitter and receiver can be continually changing frequency"—a very different thing since "simultaneously" implies that the channels are all being used at the same instant in time, as in the simultaneous broadcasting system of the BBC where the same programme is radiated on various frequencies by several transmitters throughout the country. Incidentally, channels are not transmitted, surely it is information which is transmitted on channels.

All this, of course, only serves to underline the difficulties which a columnist faces when he attempts a general description of apparatus or technique; inevitably, absolute accuracy must be sacrificed to the limitations of space.

Pax Henry!—our differences are semantic, not technical.

John Niven Douglas.

Glasgow, N.W.

Roding Boys Society folds

WE would like to inform your readers that, following the resignation of the leader of the Roding Boys' Society, this Society has been disbanded. However, some of the ex-members have now formed the Redbridge Scientific Society, meeting at the same premises: Wanstead Community Centre, The Green, E.11.

We would be obliged if you would print this letter as an announcement to those earlier members of the Roding Boys' Society, who remained loyal to the Society although distant from its core.

R. J. Lipscombe.

187 Markhouse Road, Walthamstow E.17.

Wrong address

THANK you for printing my request in the Sell or Loan section of August PRAC-TICAL WIRELESS. Unfortunately the address is wrong; it should be:---Mr. D. Mines, 41 Sandringham Road, Bitterne Park, Southampton,

NEWS AND ..

"CIR-KIT" FROM PEAK SOUND

From Peak Sound (Harrow) Limited, 10 Asher Drive, Off Mill Ride, Ascot, Berkshire, comes "CIR-KIT", 0.002in. copper-coated on one side with a special heat-resistant adhesive which in turn has a protective paper backing. It can be used for modifying existing printed circuits, building up prototype or experimental circuits, small quantity production runs on simple circuits or as flexible connectors, etc.

"CIR-KIT" is available in kit form. Kit No. 1 consists of 1ft. of 6in. wide CIR-KIT; three 6 x 12in. Bakelite E.10 laminate boards; 25ft. of $\frac{1}{8}$ in. wide CIR-KIT and 25ft. of $\frac{1}{16}$ in. wide CIR-KIT. Kit No. 2 contains 4ft. of 6in. wide CIR-KIT; five 6 x 12in. Bakelite E.10 laminate boards; 100ft. of $\frac{1}{8}$ in. wide CIR-KIT; 200ft. of $\frac{1}{16}$ in. wide CIR-KIT; one Craft knife and a spare blade. There is also a trial kit, which contains 4 x 6in. sheet of CIR-KIT; one piece of 12 x 6in. Bakelite E.10 laminate board, and 15ft. of $\frac{1}{8}$ in. wide CIR-KIT.



FI-CORD INTERNATIONAL RELEASE THE "300"

A new pocket-sized batteryoperated dictating machine, the Fi-Cord 300 has recently been introduced. It is a compact lightweight Swiss precision-built fully transistorised unit, complete with all transcribing facilities for the office. Fitting into the palm of the hand, the 300 measures $6\frac{3}{8} \times 3\frac{1}{4}$ x $1\frac{1}{8}$ in. and weighs 25 ounces. It provides simple and rapid 1-2-3 operation for recordrewind-listen in addition to fast forward and stop.

Tape speed is $1\frac{7}{8}i.p.s.$ and tapes recorded on this machine can be played back on any tape recorder having the same speed and using $\frac{1}{4}in$. tape. A digital counter is employed and a warning buzzer indicates the end of the tape.

The exclusive Fi-Cord accessory socket for both input and output accepts a choice of accessory microphones, stop-start (remote control) and lapel types, either for reducing background noise or for general purpose.

Price of the Fi-Cord 300 is £63 retail. For further details contact Fi-Cord International, Charlwoods Road, East Grinstead, Sussex.

FIRST INTERNATIONAL TV & RADIO SHOW

For the first time London will be the centre for a major international trade exhibition of audio and video electronic equipment—including colour television receivers—when The Television and Radio Show is at Earls Court, London from August 22 to 26, 1966. As well as many thousands of retailers and wholesalers and their salesmen and service technicians, attendance will include hundreds of traders from abroad.

Unlike previous national public radio shows at Earls Court, this year's is international and trade-only. Organised with the backing of the distributing side of the trade and British and foreign manufacturers and import agencies, it is timed to enable the home trade prepare for an exceptionally vigorous sales drive this winter.

The show will highlight the way in which compact transistor equipments and small but good loudspeakers are making good quality reproduction available to everyone, not just the comparatively small group of hi-fi music/electronic enthusiasts.

...COMMENT

STEREO AT LAST !

Regular stereo transmissions started from the BBC on July 30. At present, the ration is two to three stereo programmes each day, using the fully compatible pilot-tone system (as used in the U.S.A., Germany, France, Italy and Holland) which was previously tested in the Music Programme,

The stereo service is broadcast from the Third Network v.h.f. stations at Wrotham and Dover, but it is planned to increase coverage to Sutton Coldfield within a year and then to Holme Moss some months later.

Emphasis will, naturally, be on music—both recorded and live—and it is hoped to cover the Promenade Concerts during the forthcoming season. All stereo programmes will be identified in the *Radio Times*.

Further extensions of the service, both in relation to coverage and character of programmes, will be considered in the light of public reaction and the economic resources available.

MINI SOLDERING IRON

Rawlplug Co. Ltd., Rawlplug House, 147 London Road, Kingston, Surrey, are marketing a miniature soldering iron for light use. Its copper alloy tip is ready for use in 2 minutes, and it reaches 750°F in less than 4 minutes. The cork handle is a good insulator which is also very comfortable to hold over long periods, and which enables the soldering iron to be laid on the bench without the danger of the tip touching the surface. Obtainable from Ironmongers and Hardware shops, the Mini iron costs 19s. 6d.

R.S.G.B. NATIONAL MOBILE RALLY

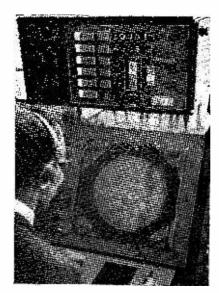
The R.S.G.B. National Mobile Rally is to be held by kind permission of His Grace the Duke of Bedford, at Woburn Abbey, Bedfordshire, on Sunday, September 11, 1966. The park opens at 11 a.m. There are ample car parking facilities and there is a children's playground, pets' corner and a boating lake for the youngsters.

The talk-in stations will be GB2VHF and GB3RS on 2m (144.86 Mc/s), 4m (70.260Mc/s), 80m s.s.b. (3.75Mc/s) and 160m (1940kc/s).

SECAR SECONDARY RADAR SYSTEM

This photograph shows the prototype Marconi/Thompson SECAR control and indicator unit, mounted above a standard radar (PPI) display. The display screen shows secondary radar responses with a video-map of the airways and coastline of southern England and parts of France, Belgium and Holland.

Secondary radar is a ground-to-air data link designed to provide the radar controller with the identity and height of any aircraft, to supplement the "plan position" information given by the normal, or "primary" radar.



Station interference

WITH reference to N. D. Mugford's letter in July 1966 PRACTICAL WIRELESS.

It's not only the Communist Bloc that is responsible for the chaos on the short waves.

The Voice of America with its excessive bandwidth caused through deliberate misoperation as a counter to jamming is responsible for a lot of interference. There is not a single Missionary radio station that beams to the U.K. that does not suffer either the whole time, or part time from V.O.A. or A.F.R.S. interference. Even the 260 kW Bonaire station suffers.

Radio Free Europe and Radio Liberty also offend as they attract jamming. HCJB was coming through the best for some time on 15.115 Mc/s. until one of the latter opened up nearby, causing HCJB to shift to 15.325 Mc/s, where reception is not so good.

The BBC also is not wholly blameless. Despite protests the interference at critical times to the transmissions of Transworld Radio Monte Carlo on 7.26 Mc/s is notorious.

Lastly, some commercial operators of communication transmitters are also to blame. I'm certain that while the bulk of such interference is image reception, some is not.

Present day high power transmitters have taken the interest out of the hobby, and the shortwaves are being misused for a verbal slanging match between East and West. Missionary radio stations together with the stations belonging to some of the smaller nations are an oasis in an otherwise dry and uninteresting territory.

D. O. French.

Stroud Green, London, N.4.

Can anyone help?

I WOULD like to purchase a copy of PRACTICAL WIRELESS for October 1964 and wonder if any of your readers could oblige, I will gladly refund the postage with the price of the book. **G. E. Newman.**

G. E. Newman.

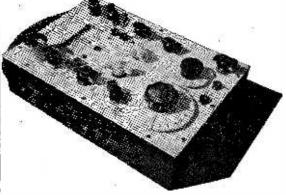
4 Laburnum Grove, Hayling Island, Hants.

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I SHALL be grateful if any reader will sell me a copy of "Amplifiers, Design and Construction" by F. J. Camm since all efforts to purchase through normal trade channels have failed. Cyril H. Rowe.

> 16 Ty Fry Road, Rumney, Cardiff.





Part II

R.D.OWEN

CIRCUIT details of the multimeter section of this instrument were given last month along with details on how to work out the various shunt and load resistor values. In this part, the bridge section is discussed and constructional information is given on the complete instrument.

An important point to remember when constructing measuring equipment is that the accuracy of the instrument can only be as good as the components that are used in it. The author specifies highstability 1% resistors for the bridge section and has achieved an overall accuracy of $\pm 3\%$ on most of the resistance ranges. He has achieved the same accuracy on the two lowest capacitance ranges, but has sacrificed accuracy on the higher capacitance ranges owing to the cost of the necessary components. This is not too serious as accuracy is not all that important on the higher ranges as often one only requires to know if a component is serviceable and not its precise value.

BRIDGE

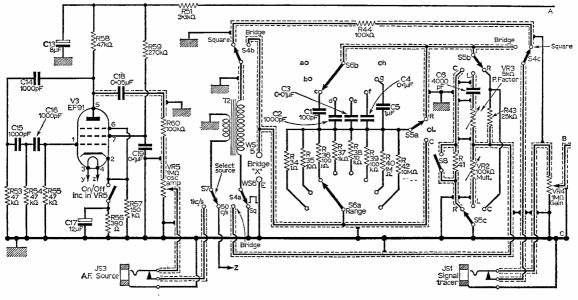
A circuit diagram of the bridge section of this instrument appears in Fig. 6. Also included in this diagram are the three valve stages which are also associated with the signal injection and tracing circuits. The bridge itself is fairly straightforward, making use of a single direct reading scale which carries all nineteen ranges. Null indication is by means of a magic eye (V2).

A full list of the bridge ranges was given in Part I (Fig. 2), but recapping there are eight resistance ranges from 400 pF to $40 \text{ M}\Omega$, five capacitance ranges from 400 pF to $4\mu\text{F}$ and six inductance ranges from 40 mH to 4000 H. All ranges are in multiples of 10.

CIRCUIT DESCRIPTION

The basic bridge circuits for resistance, capacitance and inductance are shown in Figs. 7a, 7b and 7c. Depending upon the range selected, one of the resistors R34 to R40, or R42, is used as a standard for one arm of the bridge on the inductance and resistance ranges. The standard in the other arm is then R43 for resistance, or C6 for inductance.

The $2.5k\Omega$ potentiometer VR3 is the power factor control. This gives an idea of the efficiency of the inductance being tested. D.C. resistance or leakage in the inductance causes a phase change relative to the phase of the a.c. if a pure inductance were present. The power factor control VR3 in effect



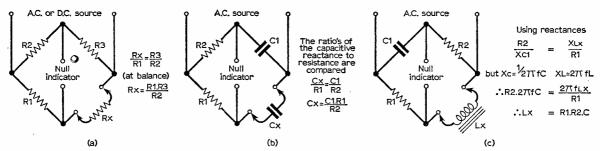


Fig. 7: Basic resistance (a), capacitance (b) and inductance (c) circuits as used in the bridge section. Circuit component references in these diagrams do not tie-in with those given on the main circuits.

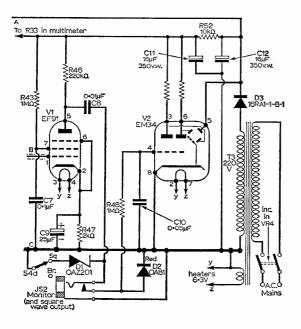
varies the efficiency of the standard C6 and hence can be adjusted to produce the same phase shift as the inefficiency in the inductance being measured. In the author's unit the power factor control was only calibrated in resistance, since the actual power factor corresponding to a particular resistance depends upon the range to which the bridge is switched. If, for best null point, the power factor control is set at low resistance, then the power factor is obviously good, and vice-versa.

On capacitance ranges, C1 to C5 are standards in one arm of the bridge and R43 in the other. The positions of VR2 and the one standard are interchanged on the capacitance ranges so that the direction of the calibrations on VR2 scale remain constant.

The bridge circuit is arranged so that one "X" connection is in fact earth, to minimise external pick-up.

The 50c/s bridge source is derived from the heater winding of the mains transformer and is isolated and stepped up by T2; a three-to-one transformer. The 1kc/s source is derived from a phase shift oscillator employing an EF91 (V3) and is fed to the bridge via a switched jack JS3. This permits the 1kc/s supply to the bridge to be cut-off and used as a signal injector.

The null indicator part of the bridge circuit



consists of a pentode amplifying stage V1, coupled to a magic eye indicator V2. The connection with the actual bridge is via a switched jack, JS1, which serves to disconnect the bridge and allow the null indicator to be used as a signal tracer when a jack plug is inserted.

SIGNAL INJECTOR

The phase-shift oscillator V3 is switched on and off by the switch included in the amplitude control, VR5. When the switch closes it connects R56 and C17 in parallel with R57, which is left in circuit when the oscillator is switched off to avoid cathode poisoning of the valve.

If a square wave output is desired S4 is switched to "square" and the output taken from the monitor socket. In this position V3 is then connected to V1 via step-up transformer T2 (bridge is disconnected) which gives a very large voltage swing at the grid of V1. The valve "bottoms" when the grid voltage exceeds 2V positive, and the valve cuts off when it goes more than 2V below the zero line. The output of the oscillator is thus squared by the limiting action. Further squaring is achieved by zener diode D1, which is in the output side of V1. This shorts out all negative and positive excursions in excess of 6V.

The 50c/s square wave output can also be used for synchronising purposes, testing amplifiers in conjunction with an oscilloscope and for signal injection into r.f. circuits since it has a high harmonic content.

SIGNAL TRACER

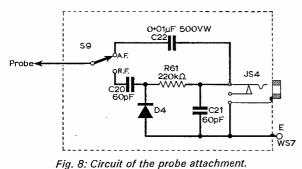
The pentode amplifying stage, V1, has a gain of about 350. For visual null indication or visual indication in signal tracing the output of V1 is rectified by D2, and the resulting negative voltage is smoothed by R48 and C10 before being applied to the grid of the magic eye. Null point (maximum "opening" of the magic eye) corresponds to minimum negative grid voltage.

An external amplifier or a crystal earpiece are advised for signal tracing, whereas the magic eye gives the better null indication.

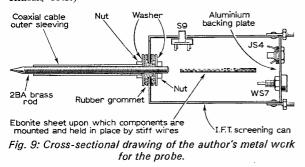
Fig. 6: Circuit diagram of the bridge section of the multitest. Only one connection has to be made to the multimeter section of this instrument and that is to R33 from the h.t. rail—the junction of C11 and R52. The circuit for the multimeter section was given in Part I, Fig. 1 (last month).

R.F./A.F. PROBE

S9 is the r.f./a.f. selector switch. On a.f. it simply connects the probe tip, via isolating capacitor C22 (500VW) to the output jack JS4. This is connected by a screened lead (terminating in jack



plugs at both ends) to the "signal tracer" input, JS1. When switched to r.f. the signal is fed via a 60pF capacitor to diode D4 which functions as a detector. The output is "smoothed" (to remove the r.f. component) by R61 and another 60pF capacitor and then fed to jack JS4. WS7 is the earth connection to the probe and should be connected to the chassis of the set being tested. (Beware of live chassis sets!)



CONSTRUCTION

No difficulties should arise in constructing this instrument, particularly if readers use one of the universal chassis with the separate sides and top. One can, of course, do the "tin bashing", but the author found the manufactured chassis to be more robust than the home-built units. Also, one can purchase one with a hammer finish which gives the finished job the professional touch. These chasis are available through most dealers: the author's unit, which measures $10 \times 7 \times 3in$, came from Home Radio Ltd., 187 London Road, Mitcham, Surrey.

The completed unit is rather compact and the author recommends the instrument should be constructed in the following sequence: multimeter section, bridge section, power supply, power feed lines, etc., and finally mounting the separately constructed sub-chassis for V1 and V3. Following this sequence will minimise disturbance to wiring already done.

The switch layout used by the author is illustrated in Fig. 3 and the position of the main under-chassis components is shown in Fig. 5: both of these illustrations appeared in Part I of this article. Layout is not critical and can be varied to suit individual readers' needs. One should, however, be careful to ensure that the major components (including the switches) all go in without touching one another before drilling any holes.

MARKING THE CONTROLS

Several methods are available to the constructor for marking the front panel controls nowadays, including the instant, self-adhesive lettering. The range switch S6 will probably cause the most difficulty as nineteen ranges have to be included. A close-up of this switch is illustrated in Fig. 10. This gives the information that has to be written on the card which can be covered with a varnish or some perspex before it is glued to the control knob.

The companion control VR2 may also cause a little trouble, as again one has to prepare a card.

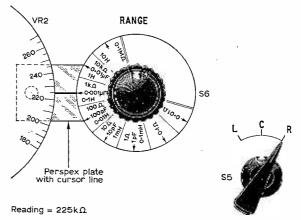


Fig. 10. Close-up of the range switch and the multiplier.

One should first find the electrical maxima and minima, using a ohmmeter. This will give you the total angle of rotation, which has to be divided into 80 equal divisions; every second division being drawn longer than the rest since it corresponds to tens. The scale is thus calibrated in fives and tens from zero to four hundred.

It is extremely important that the calibration markings are accurately drawn since the accuracy of the bridge depends upon it. Reference to the front panel illustration shows how the two scales are arranged. The perspex cursor is simply glued to the front panel.

To read the value of a component under test, one simply adjusts for null indication and then multiplies the reading on the range scale (S6) by the reading on the multiplier scale (VR2).

COMPENSATION RESISTOR VALUE

To obtain the correct value for R41, the bridge section should be switched to the 0-400 pF range, switch S8 closed and the 1 kc/s bridge source selected (with maximum gain). The null indicator gain is then reduced until the course section of the magic eye is about three-quarters closed. The multiplier is then rotated until the null point is found; the null indicator gain being increased as necessary to provide a more sensitive indication. The correct value for R41 in k Ω is one quarter of the indicated capacitance.



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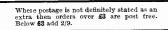
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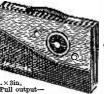
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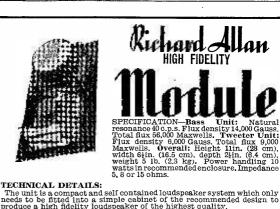
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·02μF ·02μF ·1μF ·1μF ·25μF ·5μF ·5μF ·5μF SILVER : RESISTO cards of 1 Resistors	350 vol 600 A.(350 vol 350 vol 350 vol 350 vol 500 vol 500 vol MICA, CI DRS. 1 wa 0. Fanta for Trans	t 6d. 1. 1/3 t 7 ¹ /2d. t 9d. t 10d. t 1/3 t 1/8 t 1/6 ERAMIC, 1 tt to 3 was stic valuel sistor Worl	4/6 11/8 5/8 6/9 7/6 9/~ 11/3 13/6 POLYSTY tt. Close Only 50/ c. Low va	25/- 62/6 31/3 37/6 41/8 50/- 62/6 75/- VRENI Tolera /- per 1 dues. ‡	£6/5/0 £15/12/6 £7/16/3 £9/7/6 £10/8/0 £12/10/0 £15/12/6 £18/15/0 E, Mixed types, , nnce. Mixed valu	\$3/070 p values 10/- ies. Polyth st and pack	per 10 per 10 ene wi	90. rapped on
·02µF ·02µF ·1µF ·1µF ·1µF ·5µF ·5µF ·5µF SILVER : RESISTO cards of 1 Resistors quality. !	350 vol 600 A.C 350 vol 750 vol 350 vol 500 vol 500 vol MICA, CI BRS. ± wa 10. Fanta for Trans 50 for 10	t 6d. 1. 1/3 t 7½d. t 9d. t 10d. t 1/- t 1/3 t 1/6 ERAMIC, 1 ttto 3 wa stic value! / Our se	4/6 11/3 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close Only 50/ ., Low va	25/- 62/6 81/3 87/6 41/8 50/- 62/6 75/- YRENI Tolera /- per 1 tlues. <u>1</u> only.	f6/5/0 f15/12/6 f27/16/3 f9/7/6 f10/8/0 f15/12/6 f15/12/6 f15/12/6 f18/15/0	\$3/0/0 p values 10/- nes. Polyth st and pack ance. Long]	per 10 per 10 ene wi ing. eads.	90. rapped on Excellent
02μF 02μF 1μF 1μF 1μF 5μF 5μF 5μF 5μF SILVER RESISTO cards of 1 Resistors quality. {	350 vol 600 A.C 350 vol 350 vol 350 vol 500 vol MICA, C DRS. 1 wa 10. Fanta for Trans 50 for 10. TORS. U	t 6d. 1. 1/3 t 7½d. t 9d. t 10d. t 1/- t 1/3 t 1/6 ERAMIC, 1 tt to 3 was stic valuel sistor Worl Our see Untested, 1	4/6 11/3 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close Only 50/ c. Low va election countarked	25/- 62/6 81/3 37/6 41/8 50/- 62/6 75/- YRENI Tolera /- per 1 dues. ‡ only. d. Exc	#6/5/0 #15/12/6 #57/16/3 #9/7/6 #10/8/0 #12/10/0 #15/12/6 #15/12/6 #15/12/6 #15/12/6 #15/12/6 #15/15/0 E. Mixed vapes, watt. 5% tolera ellent value at :	\$3/0/0 p values 10/- nes. Polyth st and pack whee. Long J 12/6 for 50,	per 100 per 10 ene wi ing. eads. £1/0/	90. rappad on Excellent 10 for 100.
02μF 02μF 1μF 1μF 5μF 5μF 5μF SILVER RESISTO cards of 1 Resistors quality. 1 TRANSIS L.B.M. CK	350 vol 600 A.C 350 vol 750 vol 350 vol 350 vol 500 vol 850 vol 985. ± wa 10. Fanta for Trans 50 for 10 500 vol 985. ± wa 10. Fanta for Trans 50 for 10 500 vol 985. ± wa	t 6d 1. 1/3 1. 7 ³ d. t 7 ³ d. t 9d. t 10d. t 1/- t 1/3 t 1/6 ERAMIC, 1 tt to 3 was stic values with Worl / Our sec Untested, r Switching	4/6 11/3 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close Only 50/ c. Low va election of inmarket Transist	25/- 62/6 81/3 87/6 41/8 50/- 62/6 75/- YRENI Tolera f- per 1 dues. ‡ only. d. Exc ors. Vo	46/5/0 415/12/6 47/16/3 29/7/6 410/8/0 412/10/0 415/12/6 415/12/6 418/15/0 5, Mixed types, unce. Mixed valu 1,000 plus 5/- po watt. 5% tolers ellent value at ery small. NPN	\$3/0/0 p values 10/- nes. Polyth st and pack whee. Long J 12/6 for 50,	per 100 per 10 ene wi ing. eads. £1/0/	90. rappad on Excellent 10 for 100.
02µF 02µF 1µF 1µF 5µF 5µF 5µF 5µF SILVER RESISTO cards of 1 RESISTO cards of 1 RESISTO cards of 1 RESISTO cards of 1 RESISTO cards of 1 RESISTO	350 vol 600 A.C 350 vol 750 vol 350 vol 500 vol 500 vol 500 vol 500 vol 60 vol 500 vol	t 6d. 1. 1/3 t 7 ³ d. t 9d. t 9d. t 10d. t 1/- t 1/3 t 1/6 ERAMIC, 1 tt to 3 was stic value? / Our see Intested, 1 Switching Trans	4/6 11/3 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close POLYSTY tt. Close Only 50/ c. Low va lection c unmarker Transist sistors. 6	25/- 62/6 81/3 87/6 41/8 50/- 62/6 75/- YRENI Tolera /- per 1 dlues. <u>1</u> only. d. Exc ors. Vo for 10	26/5/0 215/12/8 215/12/8 29/7/6 210/7/6 210/7/6 210/7/6 215/10/0 215/10/0 215/12/8 2	\$3/0/0 p values 10/- nes. Polyth st and pack stand pack stand pack st and st and	per 100 per 10 ene wi ing. eads. £1/0/	90. rappad on Excellent 10 for 100.
02µF 02µF 1µF 1µF 5µF 5µF 5µF 5µF SILVER RESISTO cards of 1 RESISTO cards of 1 RESISTO cards of 1 RESISTO cards of 1 RESISTO cards of 1 RESISTO	350 vol 600 A.C 350 vol 750 vol 350 vol 500 vol 500 vol 500 vol 500 vol 60 vol 500 vol	t 6d. 1. 1/3 t 7 ³ d. t 9d. t 9d. t 10d. t 1/- t 1/3 t 1/6 ERAMIC, 1 tt to 3 was stic value? / Our see Intested, 1 Switching Trans	4/6 11/3 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close POLYSTY tt. Close Only 50/ c. Low va lection c unmarker Transist sistors. 6	25/- 62/6 81/3 87/6 41/8 50/- 62/6 75/- YRENI Tolera /- per 1 dlues. <u>1</u> only. d. Exc ors. Vo for 10	46/5/0 415/12/6 47/16/3 29/7/6 410/8/0 412/10/0 415/12/6 415/12/6 418/15/0 5, Mixed types, unce. Mixed valu 1,000 plus 5/- po watt. 5% tolers ellent value at ery small. NPN	\$3/0/0 p values 10/- nes. Polyth st and pack stand pack stand pack st and st and	per 100 per 10 ene wi ing. eads. £1/0/	90. rappad on Excellent 10 for 100.
·02µF ·02µF ·1µF ·1µF ·25µF ·5µF ·5µF SILVER SILVER RESISTO Cards of 1 Resistors quality. 4 TRANSIS I.B.M. C. NKT 124 Diodes 1/	350 vol 600 A.C 350 vol 750 vol 350 vol 550 vo	t 6d. 1. 1/3 t 7 ² d. t 9d. t 10d. t 1/- t 1/3 t 1/- t 1/3 t 1/6 ERAMIC, 1 /- Our see Untested. 1 Switching hing Trans	4/6 11/8 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close Only 50/ c. Low va lection c. Ilection c. Ilection c.	25/- 62/6 31/3 37/6 41/8 50/- 62/6 75/- YRENI Tolera /- per 1 lues. ‡ only. d. Exc ors. Va for 10 per 100	\$6/5/0 \$15/12/6 \$7/16/3 \$9/7/6 \$10/8/0 \$12/10/0 \$12/10/0 \$15/15/0 \$15/15/0 \$15/15/0 \$15/15/0 watt.5 % tolers watt.5 % tolers watt.5 % tolers watt.3 % tolers 0, \$12/10/0 per	\$3/0/0 p values 10/- ies. Polyth st and pack where. Long J 12/6 for 50, or PNP. 6 1,000.	per 10 per 10 ene wi ing. eads. £1/0/ for 10	90. rappad on Excellent 10 for 100.
021LF 021LF 11LF 12LF 525LF 52LF 52LF SILVER SILVER SILVER Cards of 1 Resistors quality. TRANSIS L.B.M. CX N.KT 124 Diodes 1, SIGNAL 3 REV. CO	350 vol 600 A.C 350 vol 750 vol 350 vol 150 vol 500 vol 500 vol 70 RS. 4 wa 0. Fanta for Trans 50 for 10 (TORS. C 70 mputer : (> Switcl - each, 9 INJECTO UNTER.	t 6d 1. 1/3 1. 7 24 t 7 24 t 9d. t 10d. t 1/3 t 1/3 t 1/8 t 1/6 ERAMIC, 1 tt to 3 was stic valuel istor Worl /- Our se Switching Transit Transito R. Transis	4/6 11/3 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close Only 50/. t. Low va lection c inmarket Transist sistors. 6 en, 50/- I tors, compo	25/- 62/6 81/3 87/6 41/8 50/- 62/6 75/- WRENI Tolera /- per 1 bolly. d. Exc ors. Vo for 10 per 10 nponei onents	26/5/0 21/6/2/6 27/16/3 29/7/6 21/2/6/3 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6	\$3/6/6 p values 10/- nes. Polyth st and pack unce. Long I 12/6 for 50, or PNP. 6 1,000 . nake, 10/-	per 10 per 10 ene wi ing. eads. £1/0/ for 10 only.	90. rappad on Excellent 10 for 100.
021LF 021LF 11LF 12LF 525LF 52LF 52LF SILVER SILVER SILVER Cards of 1 Resistors quality. TRANSIS L.B.M. CX N.KT 124 Diodes 1, SIGNAL 3 REV. CO	350 vol 600 A.C 350 vol 750 vol 350 vol 150 vol 500 vol 500 vol 70 RS. 4 wa 0. Fanta for Trans 50 for 10 (TORS. C 70 mputer : (> Switcl - each, 9 INJECTO UNTER.	t 6d. D. 1/3 t 7 ² d. t 9d. t 10d. t 1/- t 1/8 t 1/6 ERAMIC, 1 tt to 3 wa stic value! J.tt to 3 wa stic value! J Our se Jntested, 1 Switching hing Transis R. Transis	4/6 11/3 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close Only 50/. t. Low va lection c inmarket Transist sistors. 6 en, 50/- I tors, compo	25/- 62/6 81/3 87/6 41/8 50/- 62/6 75/- WRENI Tolera /- per 1 bolly. d. Exc ors. Vo for 10 per 10 nponei onents	26/5/0 21/6/2/6 27/16/3 29/7/6 21/2/6/3 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6/2 21/2/6	\$3/6/6 p values 10/- nes. Polyth st and pack unce. Long I 12/6 for 50, or PNP. 6 1,000 . nake, 10/-	per 10 per 10 ene wi ing. eads. £1/0/ for 10 only.	90. rappad on Excellent 10 for 100.
-02(μF -02(μF -1μF -1μF -1μF -25(μF -5μF -5μF -5μF -5μF -5μF -5μF -5μF -5	350 vol 600 4.0 550 vol 350 vol 350 vol 350 vol 500 vo	t 6d 2. 1/8 t 7 ² ₂ d. t 9d. t 10d. t 1/- t 1/- t 1/8 ERAMIC, 1 t 1/8 ERAMIC, 1 t 1/6 ERAMIC, 1 t 1/6 ERAMIC, 1 t 1/6 ERAMIC, 1 t 1/6 ERAMIC, 1 t 1/6 ERAMIC, 1 t 1/6 ERAMIC, 1 t 1/6 t 1/3 t 1/6 ERAMIC, 1 t 1/6 t	4/6 11/3 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close Only 50/, c. Low va lection c lection c lection c lection c sistors, com rs, compo h, or 5in Lapel. 10	25/- 62/6 81/8 87/6 41/8 50/- 62/6 62/6 75/- YRENI Tolera /- per 1 lues. ‡ only. d. Exc for 10 per 100 nponet onents , 10/- 0/- eac	\$6/5/0 \$15/12/6 \$7/16/3 \$9/7/6 \$10/18/0 \$12/10/0 \$18/15/0 \$18/15/0 \$18/15/0 \$00 plus 5/- po wast. 5% toler- ellent value at: eny small. NPN 0, \$12/10/0 per nts, circuit, to r (excluding met e ach. h with plug and	\$3/0/0 p values 10/- nes. Polyth st and pack ance. Long 1 12/6 for 50, or PNP. 6 1,000. nake, 10/- ter), 10/- o	per 10 per 10 ene wi ing. eads. £1/0/ for 10 only.	90. rappad on Excellent 10 for 100.
-02(μF -02(μF -1μF -1μF -1μF -25(μF -5μF -5μF -5μF -5μF -5μF -5μF -5μF -5	350 vol 600 4.0 550 vol 350 vol 350 vol 350 vol 500 vo	t 6d C. 1/3 C. 1/3 C. 1/3 C. 1/3 C. 1/3 C. 1/3 t 7 ² / ₂ 4 9d. t 1/3 t 1/3 t 1/3 t 1/3 t 1/3 t 1/6 ERAMIC, 1 C. 1/6 ERAMIC, 1 C	4/6 11/3 5/8 6/9 7/6 9/- 11/3 13/6 POLYSTY tt. Close Only 50/, c. Low va lection c lection c lection c lection c sistors, com rs, compo h, or 5in Lapel. 10	25/- 62/6 81/8 87/6 41/8 50/- 62/6 62/6 75/- YRENI Tolera /- per 1 lues. ‡ only. d. Exc for 10 per 100 nponet onents , 10/- 0/- eac	\$6/5/0 \$15/12/6 \$7/16/3 \$9/7/6 \$10/18/0 \$12/10/0 \$18/15/0 \$18/15/0 \$18/15/0 \$00 plus 5/- po wast. 5% toler- ellent value at: eny small. NPN 0, \$12/10/0 per nts, circuit, to r (excluding met e ach. h with plug and	\$3/0/0 p values 10/- nes. Polyth st and pack ance. Long 1 12/6 for 50, or PNP. 6 1,000. nake, 10/- ter), 10/- o	per 10 per 10 ene wi ing. eads. £1/0/ for 10 only.	90. rappad on Excellent 10 for 100.

CONDENSER BARGAINS! ELECTROLYTIC

-UP HEADS. MONO 14/-. STEREO 21/-, DIAMOND STEREO 28/9 ACOS MAKE. G. F. MILWARD, 17 PEEL CLOSE, DRAYTON BASSETT, Nr. TAMWORTH, Staffs. Phone: Tamworth 2321. Orders Under 10/- please include 1/- post and packing.



TECHNICAL DETAILS: The unit is a compact and self contained loudspeaker system which only needs to be fitted into a simple cabinet of the recommended design to produce a high fidelity loudspeaker of the highest quality. The unit consists of a sin, bass sunit, 4in. tweeter and crossover network mounted on a duralumin plate which forms the front panel of the com-plete enclosure. The method of assembly of the module is unique in that the cone and synthetic rubber surround of the 5in. bass unit are mounted directly on to the duralumin front panel and the ceramic magnet is supported on sub-stantial pillars attached to the panel. The conventional chassis with all its disadvantages is thus eliminated. The tweeter is a special version of the 460T unit with a doped cambric surround and extremely light suspension system. The crossover network is a five element circuit using ferrite cored inductors and reversible electrolytic capacitors mounted on a printed circuit board.

inductors and reversible electrolytic capacitors mounted on a printed circuit board. Free constructional details of the recommended cabinet are readily available from us. Where larger power handling is required several units may be mounted in a larger cabinet, multiple units may also be mounted in a column enclos-ure to form a high power handling, high quality line source. The unit may also be mounted directly into existing equipment or in cavities in walls etc.

The unit forms the drive system of the 'Minette' enclosure, for details see separate leaflet. Patents applied for. Price £8 plus £1.5.9 tax





-continued from page 348

Insertion of R41 should transfer the null point to 0pF when switch S8 is opened. If it does not, slight adjustment should be made to its value until it does. With R41 set correctly, capacitances as low as 2pF can be measured.

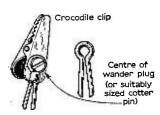
OPERATION

While it is not worth laying down strict operating details, it is probably worth pointing out that the 1kc/s source is best for low capacitance and inductance measurements and the 50c/s source for measuring low value resistors. Generally speaking, for all other values either a.c. source may be used, although one or the other usually gives a better null point.

When making insulation tests it is necessary to bridge the negative terminal to earth with a "jumper" and connect the test leads to WS3 and WS4.

Although the switch incorporated in the "ohms

Fig. 11: This crocodile clip come wander plug is ideal for capacitance measurements since it keeps the stray capacitance to a minimum.



set zero" control has no effect on most ranges, one must be careful to ensure that it is left open while measuring a.c. voltages as if closed it would shunt the meter through R16, T1 and R17. The control must, however, be closed for alternating current measurements.

The circuit diagram of the multimeter section given last month is incorrect. The lead at present shown connected to the 2.5V position of S1a should, in fact, go to 0.1mA position on the same switch wafer; the 2.5V position is blank (no 2.5V range on a.c.).

Transistorised Indicators

-continued from page 343

pair of low impedance headphones soldered to an old bulb screw. It should be possible to hear, at good strength, a local Band I television transmission, sound and vision. The frequencies for these are given in the table. Obviously, given the 1Mc/s points, a single known identification of any point on

★ components list

A.C. Probe:	Receiver-Oscillator:			
RI 75Ω	RI 3·3kΩ			
CI $0.001 \mu F_{1,000VW}$				
$C2 I0\mu F9VW$				
DI, D2 OA81	VRI $25k\Omega$ miniature			
Trl, Tr2 OC72 or near	Cl 0.1µF			
equivalent	C2, C3 4,700pF sub-min			
Torch Ever-Ready 0158,	ceramic			
with battery	C4 2,000pF tubular			
Bulb 6 volt, 0 IA	C5 10pF Oxley			
Misc. Empty Ronson	SMT9/10-9			
Multi-fill refill,	printed circuit			
paxolin, Mazda	C6 25pF Jackson			
octal valve base.	C804			
14 s.w.g. wire	C7 5pFtubular			
	ceramic			
	Trl BSY26			
	Tr2, Tr3 OC72 or near			
	equivalent			
Audio Monitor:	DI, D2 OA8I			
R1 100kΩ	Bulb 6 volt 0.06A			
R2 Ι0kΩ	RFC See text			
R3 4·7kΩ	SI See text			
CI 0.1µF 100VW	L See text and			
C2 ΙμΕ΄ 9VW				
C3 10µF 9 VW	Fig. 7			
DI, D2 OA81	Misc. Three Radio-			
Trl, Tr2, Tr3 OC72 or	spares 'Normal'			
near equivalent	type coax plugs,			
SI On-off, single	one coax socket,			
pole	bulb holder,			
Bulb 6 volt, 0.06A	aerial socket,			
Misc. Bulb holder,	knobs, 4.5 volt			
paxolin, 6 or 9	1289 battery,			
volt battery	paxolin.			

the scale will enable the whole range to be calibrated.

The C range can be used as a reference for the other two ranges. The 2nd harmonic of a 27Mc/s signal will be heard, or will cause the bulb to glow brighter, at precisely 54Mc/s on scale C, and will correspond to a pencil mark on range B representing 27Mc/s. If the signal is 27.5Mc/s, the harmonic will then coincide with 55 on range C, and will be

BAN	ID I TI	ELEVISION FREQUENCIES
м	1c/s	
Vision	Śound	
· 45	4I ·5	Crystal Palace, Divis.
51.75	48·25	Holme Moss, North Hessary Tor, Truleigh Hill and Dover, London- derry, Rosemarkie.
56.75	53·25	Kirk O'Shotts, Norwich, Row- ridge, Blaen Plwyf.
61.75	58·25	Sutton Coldfield, Sandal, Meldrum, Folkstone and Les Platons.
66.75	63.25	Wenvoe, Pontop Pike, Douglas, Orkneys.

half way between divisions on Range B. A 16Mc/s signal will appear at 16, 32, 48 and 64Mc/s. It is possible also, with a good length of aerial, to pick up several short-wave transmissions on ranges A and B, as further frequency checks. If a calibrated shortwave receiver is to hand, it may be tuned to the self-radiated characteristic hiss of the instrument's super-regen, as added confirmation of calibration points.

Finally, when satisfied that all dial markings are correct, the piece of paper may be removed, traced, and an inked scale made. When in use, a passive tuned circuit brought near the instrument's coil will cause bulb brilliance to dip, and a nearby oscillator will increase the brilliance of the bulb. The aerial socket can be utilized for very weak input signals, and for injecting a signal into other apparatus when the instrument is employed as a signal generator.



THE BROADCAST BANDS

by JOHN GUTTRIDGE

Times in GMT Frequences in kc/s

Austria: Osterreichischen Rundfunk (Wien IV, Argentinieistrasse 30a) now has a regular overseas service which follows the schedule pattern established during a long period of test transmissions. The station has been noted in Europe at 0900—1100 on 6,155/7,245/17,755 and 1500—1700 on 9,770/11,785/ 17,750.

Brazil: Radio Bandeivantes (Casilla Postale 372, Sao Paulo) has been sending out silk World Cup shields. Radio Jornal do Comercio (Rua Marquez do Reife, Pernambuco) may be heard after 2100 on 9,565. Agencia National (Setor Radio and TV, Casilla Postale 95, Brasilia) is believed to be using 14,730 instead of 14,690 for the 2230–2330 transmission over PSF.

Bulgaria: Radio Sofia (4 Bd. Dragan Zankov Street, Sofia) now uses 9,560 in addition to 6,070 for its European English transmissions at 1930–2000 and 2130–2200.

Colombia: Radio Sutatenza (Accion Cultural Popular, Aereo 1770, Bogota) heard at 2300 over HAGC, 5,075.

Cuba: Radio Habana Cuba (Apartment Postal 7026, Habana) now transmits in English at 0100—0330 9,525; 0330—0600 6,135; 1800—1900 17.735; 2010—2140 15,155 (Europe) and 2050—2150 15,300/15,340.

Czechoslovakia: Radio Prague (2 Vinohradska 12) has English at 0330–0430 on 5,930/7,120/7,345/9,795 and at 0100–0200 on same frequencies plus 11,910. There is a further English transmission at 1730– 1830 on 5,930.

Denmark: Radio Denmark (Shortwave Department, Radio House, Copenhagen V) is now using 15,165 for its 1945–2015 and 2145–2215 transmissions.

Ecuador: La Voz de los Andes (HCJB) (Casilla 691, Quito) is now using 15,325/17,880 for the 1800-2400 transmission to Europe. English is at 1845-2000, 2100-2130 and 2330-2400. The morning European transmission is 9,645/11,910 and the new frequency of 6,025 between 0430-0630.

Finland: Finnish Broadcasting Company (Unioninkatu 16, Helsinki) has a DX programme on 9,555/11,805/15,185 at 1600—1700 on Fridays, 1215—1315 on Saturdays and on 6,120 at 2100—2200 on Fridays.

German Federal Republic: Deutsche Welle (Bruederstrasse 1, Postfach 344, Skoln) is now using 11,945/9,530 for the 0300–0340 English transmission. Other English transmissions affected by changes include 0845–0940 11,925/15,275/17,845; 1550–1630 17,875/15,295; 0130–0250 11,945/9,640; 0500–0540 11,890/9,735; 1510–1555 9,675/15,405/11,925. Holland: Radio Nederland Wereldomroep (P.O. Box 222, Hilversum) now has one of the most attractive QSL cards. A special Spanish vocabulary for use when reporting on Spanish stations is available on application. Frequencies for English transmissions are 0020-0110 800 (Bonaire); 0130-0220 9,590 (Bonaire); 0730-0820 11,730/9,715/ 9,525; 1430-1530 17,810/15,425/6,020; 1900-2000 11,730/9,590/6,020; 2000-2050 11,730/9,590/6,020; 2100-2150 15,425/11,730; 2130-2220 15,220 (Bonaire).

Monaco: Trans World Radio (Rue de la Poste 5, P.O. Box 141, Monte Carlo) is now using the Radio Monte Carlo transmitter on 1,466 in the early morning and evening. English is at 2130–2230. The new frequency of 11,760 is being used for the Russian programme from 1805–1840 when it swamps the Voice of America transmitter on the same frequency.

Netherlands Antilles: Trans World Radio (5c Zootpannenweg, Bonaire) now has English 2115—2130 instead of 2115—2145 on 15,245. On Sundays there is a DX programme at 0330 on 11,820.

Radio New York Worldwide has moved its offices and studios to 485 Madison Avenue, New York, N.Y., 10022, U.S.A., and has changed its call sign from WRUL to WNYW. New transmitters are expected to be on the air next year.

U.S.A.: WWVH (Box 578, Puunene, Maui, Hawaii) has been heard at between 1150—1210 on 15,000 under the more powerful WWV. Both these stations are standard frequency time signal stations. Positive identification was possible due to the split second difference between signals at the receiver because of the different transmission paths.

Voice of America (U.S. Information Agency, 330 Independence Avenue, S.W., Washington 25, D.C.): Frequency usage for English to Europe is now 3,980 0300-0730, 1400-2345; 5,965 0300-0730, 1630-2200; 5,995/7,200/7,250/9,540/9,635/9,740, 0300-0730; 7,210 1500-2245; 9,565 1700-2245; 9,760 1700-2215; 11,760 0500-0730: 11,790 0300-0730, 1700-2200; 15,205/17,780 1400-2215; 15,290 1400 -2245; 15,295 0600-0730; 1,196 0400-0415, 0500-0730, 1600-1830, 2200-2345.

A special word of thanks this month to the Swiss Broadcasting Corporation which is now supplying "On the Short Waves" with the script of its broadcast band Dx News programme. Help has also come this month from S. Shaw, J. W. Smith, S. Ormerod, M. Goodwin, A. B. Thompson, J. Clark, G. Roberts, P. de Lacey and Sweden calling Dx-ers.

*



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His and 30Mc/s. Reports coming in from all over the country bear the same story as that told by the G3JDG rx, incidentally now an HA-230. To sum-up the month and conditions at the time of writing would sound rather like the usual weather forecast—variable with occasional showers of DX. One "Colin", 840A and a bent nail, informs that 20 was a hive of activity around 1 a.m. BST, yet on one recent late session at '3JDG the only signals which stirred any excitement in the 130 ft. l.w. were numerous Boris's and Vlads happily chirping to each other with T3 notes. (Needless to add T9's were being exchanged.)

Fifteen metres has been wide open to the Far East at times and JA's running 20 watts have romped in at 5 and 7.

Ten metres is becoming more and more interesting with a bit of DX showing up now. The 28Mc/s logs this month are from people with modestly priced receivers and straightforward wire antennas. If you want to be with it "like I dig 10 man" then take 16 ft. 8 ins. of wire, cut it in the middle and feed it with co-ax (any length). Try Sundays for a first listen.

7 Mc/s and Down

A horrible state of affairs this month, almost too terrible to relate but alas I must. Out of all the piles of logs that arrived only two were for the l.f. bands. (Pauses, dries eyes on dirty hanky, and continues). The first log from **E Goonan** (Manchester), 19 set plus a.t.u., 30 ft. end fed, logged some forty odd stations on 7Mc/s. Mostly Europeans (EU's) but from further out came Ul8KNA, HM4CS and HM2AXU. Another log from **M Pemberton** (Bucks) CR150, 66 ft. end fed heard G, GC, GW, and DJ, DL, F2, ON5, on eighty, while on forty DJ, DL8, EI, G, GM, LA3 ON5, OZ6, and PY8QM (Brazil). No reports for top band although several EU's are about down the l.f. end. How about an 1.f. month? $1\cdot8/3\cdot5/7Mc/s$ only. I know this is quite a task and much more difficult than 20 and 15 where the DX just falls like ripe plums. To request someone to listen on 40 metres is like asking them to walk through a pack of mad dogs with a pork chop on each ear—nevertheless, I'm asking! One hour on 40 for each hour on the h.f. bands. Go on live dangerously—I dare you. (No—I will not provide the pork chops!)

The Aitch Eff Bands

Never any shortage of logs for these bands particularly 20 and 15. So many at times that I sort them into those who took the trouble to put the log in alphabetical order and those who did not. Here are reports from those who did. **Chris Claydon** (Fife) 840C, 60 ft. l.w. had a brief listen on 20 and heard BV1USA (Taipei), CR3KD (Bissau, Port Guinea) CR4BC, HI8LC (Santa Domingo), KH6FRI (Hawaii), LU1ZC (Deception Is. Antarctica) UAØ KAE, UWØIF, VP2AZ, VP8IN (Base F, Grahamland Antarctica). **D. Skidmore** (Belper), HE40, 100 ft. end fed, 20 metres all s.s.b.—CN8BB, CR66C, CX9AAK, EA8AH, EL3C, ET3WH, HV3SJ, IS1VAZ, JA4BJO, JA6AD, KL7EBK, KM6SEN (Midway Is), KR6DI, PY2BEH, SVØWV, TF3EA, UA9TE, UL7BF, VE2ABJ/SU, VE8MP, VK5MS, VP6KL, WA6EKD, W6EDB, XE1FFW, XW8BJ, YV1EC, YV3CN, ZB2AK, ZD7RH, ZD9BE, ZE3MV, 4X4AM, 5N2AAW. Ian Haworth (Preston) CR100, 33 ft. end fed, 20—BV1USA, CR6BX, CX2CO, HI7ATM, HK3RQ, HP1FR, JA1,2,6, MP4BBA, KZ5PW, OA3PZ, OX3BF, PY1,2,3,4,5,7, ST2SA, TI8LN, VK1,2,3,4,6,7, 9VW, VP2GR, YV5BIG, ZL5AA (Antarctica), 4X4VH, 5A1CV, 9Q5HF, all phone. On 15 a log from F. Le Blancg (Jersev, C.I.), Pye

On 15 a log from F. Le Blancq (Jersey, C.I.), Pye domestic rx 50 ft. end fed, CR5CA, CR6GL, CX8PS, HB9GR/P, KP4AXC, LU5DJV, LX1DC (Luxembourg), OD5ET, PY2CDY, PZ1BO, SV1BL, TR8IAD (Gabon), TU2BA, XE1RC, ZC4MO, ZS1DV, 5A1TK, 6W8DD (Senegal), 9H1R, 9Q5CB. Michael Leck (Lancs) 87OA, 66 ft. end fed, CR6KR, CR7FM, CT1CJ (Portugal), EAØJM, EP3RO, JA2GDT, JA7DTF, K1FZS, K2YXY, K4DI, LX1YL, MP4BBA, P11HTG, SV1CX, SV1DL, VE3FRV, ZC4HR, ZE2JA, ZE6JL, ZSBD, 4X4KX, 5A1TK, 5A5TE, 5N2AAR, 5X5JK, 9J2K, 9N1JP, 9O5IA.

Colin Morris (see Ten Metres), found twenty busy with FM8CD, FL8AC, HC8JG, HM9DL, HR1SO, HS1AK/P2, KH6FMS, KW6EJ, KX6BU, OA5W, PJ2MI, PJ3CR, ST2BSS, TI3AA, VP2KD, XE1FFW, YK1AA, 3A2CP, 9M6WQ. M. Levy (Kirkella), runs a "not so very good receiver", an S38E. With 66 ft. of wire twenty yielded EP2GF, HC1SM, HS1AK/2, HV3SJ, JA3HF, KL7EBK, KR6MM, LU1CM, MP4BCC, OX3KI, VK2PP, VP6KL, ZD9BE, 5Y3GT, 5Z4IR.

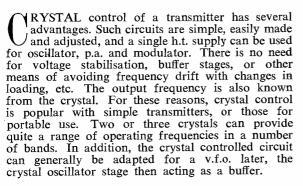
Ten Metres

Yes a separate heading again. Brazil coming in 59, Cyprus 57, Venezuela 59, half Africa at 58 average, this is the story now. **Colin Morris** (Tenbury Wells), double s/het homebrew, dipole-DJ7RD 1852, EL2AK 1724, OD5BU 1853, PY1BYK/P7 1814, PY2BYI 1816, YV5BPJ 1812, YV5AGM 1755, ZC4MO 1747, 5H3JJ 1746, 5Z4AA 1726, 7X2AH 1340, 9H1A 1748, 9J2VX 0825, 9J2MM 1806. Times g.m.t. **Paul Baker** (Pontygasseg) (Fancy sending that on c.w.!) HE30 60 ft. end fed, CT1, DJ, DL, DM, EA4, F, HB9, I1, IT1, OE, ON, OZ, SM, SP, UA2, UB5, UC2, UR2, YO, CR6GP, CR7IZ, K4DI, PY1CRC, ZC4MO, ZS1BV, 4X4IH, 5N2AAR, 9J2VX, 9Q5GW.

News and Notes

Little items of gossip passed my way and now offered for your discerning palates includes VP8IK (Antarctica) bottom end of 7Mc/s (still no pork chops—not even if you hear him!) VS9OC back in business again on the h.f. bands on s.s.b. Kure Island at it on 20 metres look for a /KH6. Also Japanese amateurs, at present JA's are also to include JH call signs shortly. A reminder that now is the time to check the local schools and technical colleges for R.A.E. classes, enrolment usually being early September. Contests for sunny August—alas just one, the WAE c.w. section contest. September 3-4th VHF-NFD. Deadline for next month is the 25th, how about a log from you?

HERYSTAL CONTROLLED OSCILLATORS and TRANSMITTERS



Triode Oscillators

These are not much used, but are worth considering for a very small or simple transmitter. Two circuits are shown in Fig. 1. The "a" circuit requires no coil, output being at the crystal frequency. A 6C5, 6J5, 6C4 or other triode can be used, or the triode section of a triode-pentode. With the latter, the pentode serves as p.a., allowing very small size in the 5W-1OW input range. Most valves and crystals require some capacity from grid to cathode. The 30pF trimmer is adjusted from zero capacity until all crystals oscillate well. About 100-150V will be sufficient for the anode, so the anode resistor can be adjusted or replaced by an r.f. choke, if only a low voltage is available.

Fig. 1b uses a coil L1, tuned to near crystal frequency. If a meter is included in the h.t. circuit, a dip in current is found when oscillation commences. Tune for nearly minimum current, which gives nearly maximum r.f. output. Normally, L1 is not tuned *exactly* to resonance, because the circuit will then not start oscillating when switched on.

by F.G. RAYER G3OGR

With these circuits, output is generally at crystal frequency. This does not matter with single-band operation, but is rather a limitation for multi-band working.

Crystal Harmonics

Various tetrode and pentode oscillators allow output to be obtained on the crystal frequency, and multiples of this frequency. It is necessary that the harmonic falls within the higher frequency band in view. This will be so with some crystals, but not with others. As example, a 3520kc/s crystal would allow working on 3.52, 7.04, 14.08 and 21.12Mc/s. But a 3650kc/s crystal has harmonics (multiples) falling outside the 7, 14 and 21Mc/s bands. The circuit in Fig. 2 is particularly easy to adjust.

The circuit in Fig. 2 is particularly easy to adjust. L1 is tuned to the crystal frequency, or the wanted harmonic. A fixed or plug-in coil can be used, or coils can be selected by switching. A single fixed coil can sometimes be used for two adjacent bands.

At high multiples, output falls off, until sufficient grid drive for the following stage is no longer obtained. With values shown, a 3.5Mc/s crystal should provide enough grid drive for a 6146, 807, or similar p.a., on 3.5, 7, 14, and 21Mc/s. The 6CH6 requires about 25mA. Grid current in the following stage can be adjusted by slightly detuning L1.

When first setting up an oscillator or transmitter of this kind, check that the correct harmonic is being used. This is most readily done with a wavemeter. Wrong harmonics can then be avoided.

It is helpful to prune L1, or have an adjustable core, so that only one correct harmonic is tunable

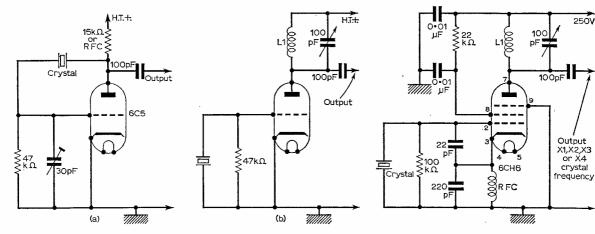


Fig. 1 (a and b): Two simple triode oscillators.

Fig. 2: Oscillator with output on fundamental and harmonics.

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with each coil. If this is done, the capacitor can be reduced to 25pF. Wrong harmonics cannot then be reached.

When obtaining maximum grid drive to the next stage, with a high frequency multiplication, L1 should be chosen so that the parallel capacity is small. This is not important on $3\cdot5$, or 7Mc/s, and may not matter on 14Mc/s, but may make all the difference on 21 and 28Mc/s. With switching, absorption by unused coils can also cause losses which reduce grid drive.

Crystal Switching

It is often convenient to have the crystal holder on the front panel or fit a switch for easy changes in frequency. Fig. 3 shows a suitable circuit for three crystals, X1, X2 and X3.

Fig. 3 also allows the input from a v.f.o. to drive the crystal stage. Even with a v.f.o. available, it is sometimes convenient to have a crystal or two for frequency checks.

A co-axial lead takes the v.f.o. output to the socket shown. To avoid instability or frequency pulling it is generally better to use the crystal stage as a doubler. So the v.f.o. can be on 1.8 Mc/s for 3.5 Mc/s, or 7 Mc/s for 14 Mc/s (doubling). The crystal stage can also triple (21 Mc/s operation with 7 Mc/s v.f.o.) with good results. A v.f.o. giving outputs on 1.75 Mc/s and 7 Mc/s bands will permit working all frequencies from 3.5-28 Mc/s.

Crystal Holders

Crystals have a wide range of bases, with holders to suit. It is best to have all with similar pins. If some different crystals are to hand, an adapter can be made as in Fig. 4. This has two pins to fit the normal crystal holder, mounted on a paxolin strip. Two "sockets" bent from brass receive the pins of the crystal. The adaptor allows a small crystal to be used in a large holder, or the reverse, according to construction. Holders can also be purchased which take either $\frac{1}{2}$ in. pin spacing or $\frac{3}{4}$ in. pin spacing crystals, but some of these will no longer be satisfactory with small pin crystals once a large pin crystal has been inserted.

An ordinary octal holder will take FT243 type crystals. Other sockets can be used for heater and h.t. circuits, as in Fig 4. This allows a crystal or v.f.o. to be plugged into the same panel mounted octal holder.

The $\frac{3}{4}$ in. spacing type of crystal will fit a UX5 (807 type) holder. Again, spare sockets can be used

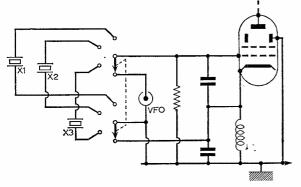


Fig. 3: Crystal switching and v.f.o. input circuitry.

to supply power to an optional v.f.o. It is also possible to have crystal/v.f.o. switching, with power for the v.f.o. from a separate power pack, or taken from the transmitter by means of a separate multiway plug.

Multi-Band Transmitter

Fig. 5 is a transmitter circuit allowing multi-band working with a minimum of difficulty. L1 is tuned to the crystal frequency, or required multiple. About 3mA to 4mA grid current is usual for the 807, and a 3.5Mc/s crystal should give 5mA drive on 14Mc/s and lower frequency bands.

For a single band, L1 and L2 can be fixed. This simplifies building when interest is mainly in one band. For multi-band work, plug-in coils or switching is required. Normally, the p.a. (807) is always driven on the same frequency as the output, because doubling here reduces efficiency.

H.T. for the crystal oscillator can be drawn from the same pack as supplies the p.a. If so, add a series resistor so that about 250-300V is obtained. A single meter, with switching, can be used for p.a.

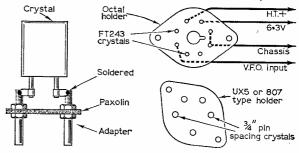


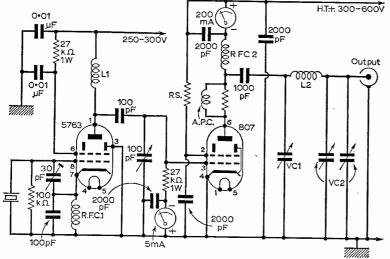
Fig. 4: Crystal adapter and plug-in holder for v.f.o.

grid and anode, but separate meters are an added convenience. A switch to apply h.t. to the oscillator only is also very useful indeed, so that grid current can be checked and operating frequency noted with the receiver.

The p.a. anode anti-parasitic choke can be 5 turns of 20 s.w.g. wire in a coil $\frac{1}{2}$ in. long and $\frac{3}{8}$ in. The diameter, around a 1-watt 47 ohm resistor. The 807 works well with 100mA anode current. This is 30W input with 300V, 40W with 400V, and so on up to 60W with 600V. The screen resistor Rs is adjusted to obtain about 250-275V on the screen grid, measured with the transmitter working.

For c.w., any of the usual keying methods can be employed. Cathode keying is most simple. For phone, a push-pull modulator furnishing an audio output equal to about one-half the p.a. input gives excellent results. Fixed capacitors should have a voltage rating at least twice that of the h.t., or preferable 1.5kV or higher for 600V.

VC1 should be wide spaced. A 200pF capacitor is suitable for all bands, but for h.f. bands only 100pF is easily sufficient. VC2 is a 2-gang or 3-gang broadcast receiver type component, with a maximum total capacity of about 800pF to 1500pF in all. The p.a. should not be operated without a load—aerial, r.f. output meter, 60-watt domestic lamp, or other equivalent device. With VC2 closed, VC1 is dipped for minimum anode current. VC2 is then opened until the dip on VC1 corresponds to 100mA (or other chosen input).



The 30pF trimmer is only screwed down sufficiently to obtain enough grid drive with all crystals. Grid current is reduced, when necessary, by detuning the p.a. grid capacitor.

Oscillator Anode Coils

Very many different coils are suitable for L1 (shown in Figs. 2 and 5). Receiver type coils can often be used. A frequency check can be made with a grid dip oscillator, so that the coil core (or number of turns) can be adjusted, if necessary. Alternatively, apply h.t. to the oscillator only, tune the unknown coil for maximum p.a. grid current, then check the harmonic obtained with a wavemeter.

Two circuits for switch selection of various bands are shown in Fig. 6. Circuit "a" employs a single, tapped coil. This can be wound on a 1in. diameter paxolin tube. Section 1 is 35 turns of 26 s.w.g. enamelled wire side by side, followed by $\frac{1}{8}$ in. space. Section 2 has 15 turns side by side, also 26 s.w.g. enam. A $\frac{1}{4}$ in. space is left and sections 3 and 4 are wound so that there are $13\frac{1}{2}$ turns in all, of 20 s.w.g. enamelled or bare wire, occupying $\frac{2}{8}$ in. Section 3 is 6 turns, and section 4 is $7\frac{1}{2}$ turns. Connections must be short and direct, with C1 from coil to VC1 rotor, and C2 having short leads from anode and coil to VC1 also.

The "b" circuit uses separate coils and VC1 can be smaller, without causing difficult coil pruning, because 3.5, 7, and 14Mc/s band coils have adjustable cores. The 21Mc/s coil can be made out of self supporting, stout wire, and can be adjusted by compressing or stretching it. The 28Mc/s band coils can also be made in this way. The individual coils must be placed to avoid absorption by unused windings, or grid drive will be reduced badly.

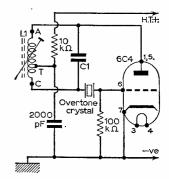
For 28Mc/s six turns of 18 s.w.g. wire in a coil $\frac{5}{8}$ in. diameter and $\frac{1}{2}$ in. long should prove suitable. The 21Mc/s coil can be nine turns of 20 s.w.g. wire $\frac{5}{8}$ in. diameter and $\frac{3}{4}$ in. long. For 14Mc/s, 17 turns of 20 s.w.g. $\frac{5}{8}$ in. diameter and 1 in. long may be used. On these bands, stray wiring and capacity greatly influence coverage, so turns may have to be adjusted.

It is not worth winding coils for the lower frequency bands. For 7Mc/s, a coil adjustable through

360

Fig. 5: Transmitter circuit for the 3.5–28 Mc/s bands.

Fig. 7: Overtone oscillator for h.f. or v.h.f. bands.



about 11μ H should suffice, with about 40μ H for $3\cdot5$ Mc/s. If VC1 is larger, there is much more latitude in coil inductance, but h.f. bands should be reached with VC1 nearly completely open for the reason described.

PA Coils

Individual coils, placed across terminals or plugged in, are very satisfactory here. For one band only, a fixed coil is used. For multi-band coverage, a coil can be wound on a $1\frac{1}{2}$ in. diameter former, with 16 s.w.g. wire for 21/28 Mc/s, and 20 s.w.g. for 7/3 5 Mc/s. Wind 25 turns of 20 s.w.g. and 10 turns of 16 s.w.g. in series, with a space of $\frac{1}{4}$ in. between them, separating turns so that the 25 turns occupy $1\frac{1}{4}$ in. and the 10 turns $1\frac{1}{4}$ in. Tap the larger winding at 16 turns for 7 Mc/s, and the smaller coil at six turns for 21 Mc/s. The whole 10 turns are employed for 14 Mc/s. Switching is the same as in Fig. 6 "a". Turns in circuit are thus 6 for 21 Mc/s, 10 for 14 Mc/s, 19 for 7 Mc/s and 35 for 3.5 Mc/s. Switch rotor goes to VC2.

A 28Mc/s coil can have five turns, $\frac{3}{4}$ in. in diameter and 1in. long, using 14 or 16 s.w.g. wire. It may need a little adjustment, depending on layout.

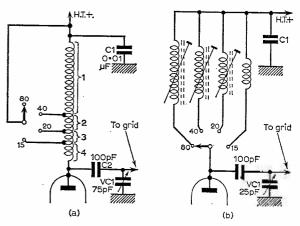
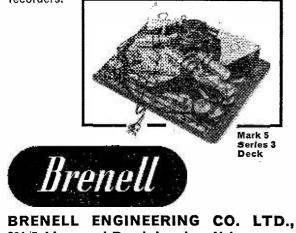


Fig. 6: Oscillator anode coil circuits.



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Construction

The construction of a transmitter with a circuit such as that in Fig. 5 is very straightforward and snags are unlikely. A normal layout permits L1 to be under the chassis, with L2 and all anode components in the p.a. above the chassis. Wiring is short and direct, with by-pass capacitors directly to the chassis.

When first using the transmitter, a test should be made that grid drive is in fact on the correct frequency, as mentioned. The tuning of the p.a. anode coil should be done on low power; by reducing h.t. or temporarily fitting a $47k\Omega$ screen grid resistor. Some change to grid current, with anode tuning, is normal, especially on the h.f. bands.

Adjusting VC1, Fig. 5, should cause a smooth dip in anode current. Changes in anode current at other settings are unlikely, but indicate parasitic or other unwanted oscillation. Stray back coupling from anode to grid, due to a poor layout, is a likely cause.

With the crystal removed, grid current should be zero, and no r.f. output obtained. For these tests, p.a. input (with an 807) should not exceed 20-25 watts.

Overtone Oscillator

For h.f. and v.h.f. bands, an overtone crystal oscillator has several advantages. A typical circuit is shown in Fig. 7. One or more stages of multiplication will be avoided, and the lowest frequency obtained is the overtone frequency (not the crystal frequency).

One application of this circuit is in a 144Mc/s transmitter. A 8Mc/s overtone crystal will provide a direct output on 24Mc/s, L1 being tuned to this frequency. A tripler stage then gives 72Mc/s, with a doubler providing the final conversion to 144Mc/s.

C1 may often be omitted, or is very small (say 2.5pF). If a number of crystals are used, a miniature variable capacitor, panel controlled by an insulated extension, is handy to obtain reliable starting and best output. The crystal should be an overtone type. Some are marked with the overtone frequency they produce (e.g., 24 Mc/s) while others have the fundamental (not used) specified.

When first testing the circuit, the tapping T on L1 may have to be moved. If this is too near the crystal end C, output may be poor, or no oscillation obtained. But if T is too near the anode end A, oscillation may arise on any frequency to which L1 is tuned, and is no longer crystal controlled. With T correctly placed, oscillation only arises as L1 is tuned through the overtone frequency, as with a conventional oscillator (shown in Fig 1b).

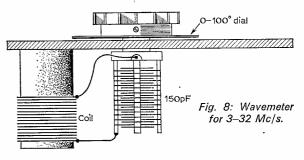
For 24Mc/s output with an 8Mc/s 3rd overtone crystal, 20 turns of 26 s.w.g. wire on a $\frac{1}{4}$ in. diameter cored former should be found suitable, using a 1.5pF fixed, or preferable 2.5pF pre-set or variable capacitor in the C1 position. The tapping T can initially be 7 turns from C.

Similar circuits can be used for 28Mc/s band working, to avoid multipliers. The overtone obtained by L1 should be checked with a grid dip oscillator or wavemeter. The coils needed may appear unusually large for the band, because of the extremely small capacity.

Wavemeter

A simple wavemeter for checking in the 3.5-28Mc/s range can be made from a coil and parallel variable capacitor. It can be calibrated from a grid dip oscillator, signal generator, or receiver. To calibrate from a receiver, loosely couple the wavemeter to a loop in the aerial connection, and tune it to produce a dip on the signal strength meter of the receiver, with transmissions for the wanted bands.

An easily made wavemeter is shown in Fig. 8. If made *exactly* as described, calibration should be of sufficient accuracy to allow the Amateur bands



to be identified, and a check on readings can be made, so that they can be corrected, if necessary. Two coils are required. In view of the few items needed, it is easy to make two complete wavemeters, one for each band.

Each coil is wound on 1in. diameter smooth paxolin, using 24 s.w.g. enamelled wire, with turns side by side. The small coil has seven turns, and the large coil 35 turns. The free ends of windings are 2in. long. The capacitor is 150pF, with semicircular vanes. The dial is 0-100, zero being with the plates unmeshed. The following calibration was obtained:

Smal	l coil	Large coil		
Frequency (Mc/s)	Dial Reading	Frequency (Mc/s)	Dial Reading	
10.0	8	32	8	
9.0	9	30	9	
8.0	12	28	10	
7.0	15	26	12	
6.0	20	24	14	
5.0	30	22	16	
4.5	38	20	20	
4.0	57	18	25	
3.5	62	16	31	
3.0	82	15	36	

To check the p.a. drive frequency, place the wavemeter coil near the oscillator anode coil L1, and tune the wavemeter until a dip is observed in p.a. grid current. The band (crystal harmonic) can then be seen on the wavemeter dial.

An initial check of p.a. anode tuning can be made with no h.t. applied to the p.a. If VC2 (Fig. 5) is closed a fairly steep rise in signal strength, as shown by a receiver signal strength meter, will be seen when VC1 is tuned to resonance. That is, L1, L2 and the receiver all tuned to the same frequency. Normally, a small dip in grid current can also be seen on the grid meter when L2 is tuned through resonance. This is extremely small on 3.5Mc/s, but may be 0.1mA or so on the h.f. bands.



The Science Museum Radio Society, founded in 1955 by a small group of Civil Servants on the Museum staff, widened its membership to take in all Civil Servants and those in allied occupations in 1957. At the same time the Society's name was changed to the Civil Service Radio Society. Today the Society is over one hundred strong and has a balanced membership about half holding transmitting licences.

REGULAR MEETINGS

Monthly meetings take place on the third Tuesday of the month throughout the year in the Demonstration Room, First Floor, Science Museum. Members may operate the well-known GB2SM transmitter and meet in the less formal atmosphere of a general gathering. These "informal" meetings are very popular and the evening PRACTICAL WIRELESS attended, two other visitors came along — Rev. Fr. Ray Sturzen-hecker DJ5SJ from Frankfurt, Germany, and David Jeanes VK2BSJ from Rockdale, NSW, Australia. Although neither visitor operated GB2SM, Dave spent all Sunday on-the-air at the chairman's home (John Stuart G3 TUM) before returning to Australia. Ray will be in Britain for some time lecturing at Wimbledon College, where he plans to start a boys' radio club.

UNLICENSED STATION

Station GB2SM listens out for members from 6 to 6.45 p.m. on club nights. This station is unique in as much as it is unlicensed (being on Crown property) and is extremely well equipped—most of the gear being on "permanent loan" from manufacturers.

The Society provides operators for station GB2SM for many of the amateur contests and their



No 12 EIVIL SERVICE RADIO SOCIETY GB2SM

Left to right: David Jeanes VK2BSJ (visitor), Peter Hearson G3SIU (treasurer), A. E. Roberts G3RUR, R. J. Pigou G3CRP, John Stuart G3TUM (chairman), E. K. Williams G8VY, George Herbert (assistant secretary), J. A. Payter G3GXA, Rev. Fr. Ray Sturzenhecker DJ5SJ (visitor) and Gordon Lloyd-Dalton (secretary).

skills (coupled with the first-class gear) can be seen from the premier awards displayed in the clubroom. The Society also runs a "ham" competition, open to all members, annually awarding a trophy known as the "Museum Key". John Springate G3CAZ, is the current recipient.

WORKSHOP FACILITIES

Later this year the Society will be able to offer workshop facilities to members, through the cooperation of the Civil Service Sports Council—at a Westminster address.

Beginners to radio and audio are already made welcome at the Society and most members are only too willing to loan technical publications and textbooks.

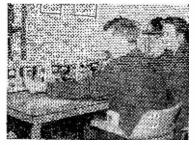
FORTHCOMING LECTURES

Although the 1966/67 winter season meetings have not yet been finalised, the society hope to include talks on the following subjects: relays, their uses, and practical circuits; short-wave listening; the Post Office Tower; general approach to aerials (by a consultant); building-up kits; a hi-fi demonstration by a noted manufacturer; and propagation, etc. These meetings will be additional to the "informal" meetings.

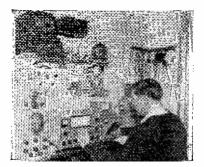
MEMBERSHIP

Full membership is only granted to members of H.M. Civil Service and their wives, whereas anyone in comparable employments (in the railway service, banking, industry, etc.) can become a ssociate members.

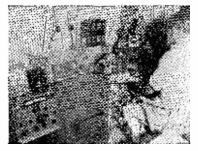
become as so ciate members. Readers interested in joining the Society should either go along to one of the "informal" meetings held at the Science Museum or drop a line to the secretary: G. Lloyd - Dalton, 2, Honister Heights, Purley, Surrey.



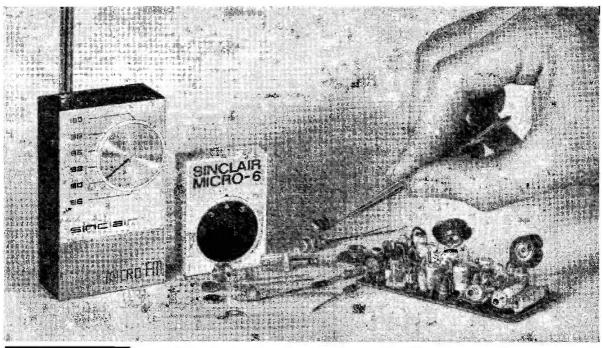
G3CRP and G3RUR operating the GB2SM s.s.b. transceiver.



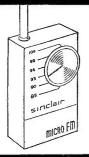
Peter Hearson G3SIU has just completed the s.s.b. transceiver (G2DAF, Mk.II) shown in centre of the photograph. It took him the best part of two years to build.



John Stuart uses two transmitters, a home-made top-band job with 10 watts output and a Heathkit DX 40U with v.f.o.



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★ TECHNICAL DESCRIPTION

THE SINCLAIR MICRO FM is a completely self-contained double-purpose F.M. superhet. It uses 7 tran-sistors and 2 diodes. The R.F. amplifier is followed by a self-oscillating mixer and three stages of I.F. amplification which dispenses with I.F. transformers and all problems of alignment. The final I.F. amplifier produces a square or aignment. Ine final I.F. ampiftier produces a square wave which is converted so that the original modulation is reproduced exactly. A pulse-counting discriminator ensures better audio quality. One output is for feeding to ampifier or recorder and the other enables the Micro FM to be used as an independent self-contained pocket portable. A.F.C. "locks" the programme tuned in. The telescopic aerial included is sufficient in all but the worst signal areas.

plete an FM set for himself have been completely eliminated in the Micro FM. It is ready to use the moment you have built it. The pulse counting discriminator ensures best possible audio quality; sensitivity is such that the telescopic aerial included with the kit assures good reception in all but the very poorest reception areas. The Sinclair Micro FM will give you all you want in FM reception and the satisfaction of building a unique design that will save you pounds.

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Complete kit inc. telescopic aerial, case, earpiece and instructions



SINCLAIR MICRO-6 — Build it in an evening Complete kit including case, aerial, lightweight earpiece & instructions

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amplifier of its size and power. At the same time its rugged construction and its amazing adaptability make it possible to use just ONE type of amplifier in an exceptionally wide variety of applications. Eight special H.F. transistors are used in a highly original circuit to achieve the characteristics demanded of any quality amplifier, irrespective of price, yet this Sinclair unit costs well under £5.0.0, including its own integrated pre-amplifier stage. It will function efficiently from anything between 6 and 20 volts, making it very battery, for example. Where it is re-quired to run the Z.12 from mains supply, the PZ.3 is recommended. The Z.12 accepts radio, microphone and pick-up inputs, and detailed instructions for connecting these in mono and stereo are given in the manual supplied with every unit, together with a variety of matching control networks. Those wishing to have the very finest preamplifier and control system can connect inputs via the Stereo 25, a new unit designed specially for use with the Z.12 to produce the very finest stereophonic hi-fi you have ever heard-and the saving to you in cost is fantastic.

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- + IdB **INPUT SENSITIVITY**—2 mV into 2 K ohms **SIGNAL TO NOISE RATIO**—better than 60dB **OUTPUT IMPEDANCE**—suitable for 3, 7:5 and 15 ohm loudspeakers. Two 3 ohm speakers may be used in parallel **POWER REQUIREMENTS**—6 to 20 volts D.C.
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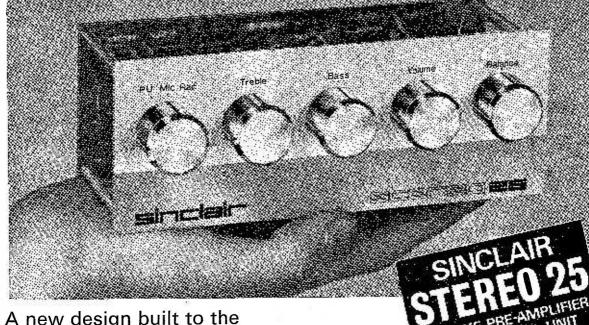
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TECHNICAL SPECIFICATION

Performance figures quoted here were obtained using the Sinclair Stereo 25 fed to two Z.12's and the entire assembly powered by a PZ.3 Mains Power Supply Unit.

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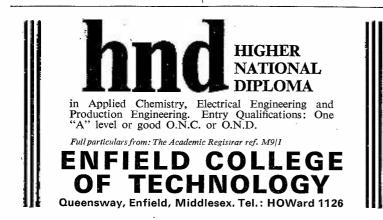
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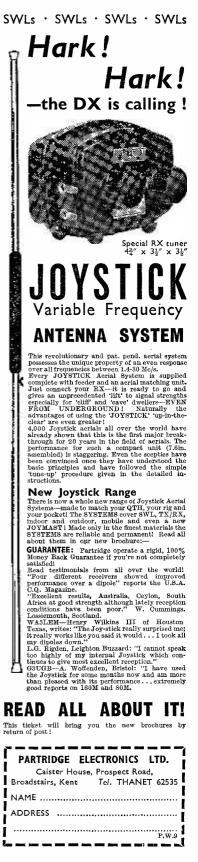
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