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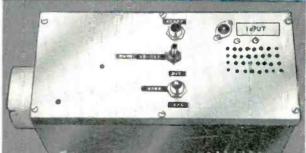
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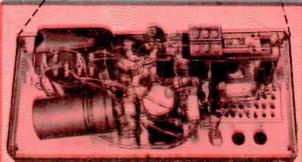
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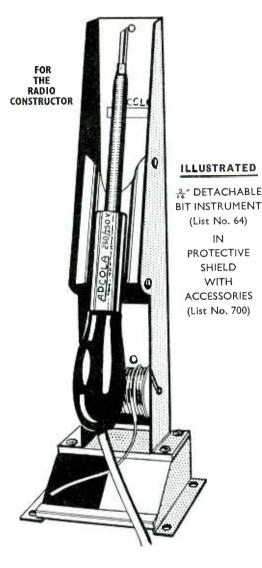








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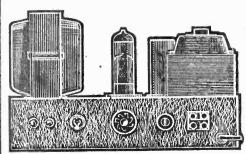
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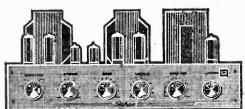
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FIVE-TEN AMPLIFIER

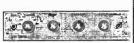
One of the most inmous amplifiers ever made—thousands are in service as the nucleus of high quality installations throughout the world. Check the phenomenal performance, unmatched by any other amplifier obtainable in this price range; Freq. response 5 c/s. to 30 kc/s. flat ± 1 db. Distortion 0.1% at full 10 watts output. Noise -65 db. below 10 watts. Imput signal 40 mV. for 10 watts. Out. Imp. 3 or 15 ohms. Valves E281. E785, ECC83, 2× E184. Size overall: 10 x 7 x 6 ihn high. Incorporates mains outlet for gram and anx. supply of 250 v. at 35 mA. and 6.3 v. at 23 amps. for pre-amblituders. To full Mullard specification. Assembled and tested 213.100 there, etc. To full Mullard specification. Assembled and tested 213.100 Kit 15 cm. All 16 corriege.

AMPLIFIER AND THREE-VALVE PRE-AMPLIFIER. Assembled and tested 225.10.0. Kit 219.10.0. Add 8/6 corriege.



TEN PLUS TEN STEREO AMPLIFIER

Basically two Five-Ten amplifiers with design variations that exploit the exceptional qualities of the Mullard ECLS6 Triode/Peatode. Add Stern engineering to a very exacting specification and the result is Stereo performance of the highest quality at astonishingly low cost. Freq. response 5 c/s. to 60 ke/s. fat \pm 3 db. Sens. 23 mV. for full 10 watte output each channel. Noise -65 db. below 10 watts. Cross talk -60 db. Distortion 0.2% at 10 watts. Out. Imp. 3.75, 8 and 16 ohms from sectionalized secs. of special Utra Linear output trans. Valves 2 x EFS6, 4 x ECLS6, G234. Size 14 x 64 x 64 in high. Aux. output for pre-amp. 300 v. at 6 mA. and 6.3 v. at 15 amps. Illustration shows amplifier fitted with Passive Control Unit (see right). Assembled and tested £20,0,0. Kit £16.0.0. Add 8/6



TWO-VALVE PRE-AMPLIFIER

Specially designed for use with the Muliard series of 3, 10 and 20 watt amplifiers but entirely sultable for all Bi-Fi power units not requiring input of more than 250 mV for full output. Features include inputs for crystal and Features include inputs for crystal and variable reductance pick-ups with RIAA equalization, plus radio, sensitive microphone, and tape replay direct or from pre-amp. Controls include or position selector, volume and widerange bass and treble boost. Vaives 2 x EF86, size 9½ x 4½ x 2½ in. high. Panel 10½ x 2½ im. Requires 300 v. at 3 mA and 6.3 v. at 0.6 amps. Assembled and tested \$9.10.0. Kit \$6.6.0. 4dd 6f-cerriage.



THREE-VALVE PRE-AMPLIFIER

Specially recommended for use with the 5-10 amplifier, but also suitable for use with all Mullard series mono amplifiers and any high quality unit requiring an input of up to 250 mV. for full output. Features include: wide range Bass and Treble controls, high and low pass diters, auxiliary input and record output sockets, switched inputs for crystal or magnetic pick-ups, radio tape playback and auxiliary. Power required 250 v. at 6 mA. and 6-3 v. at 1 ample Valves 2 x EF86 and ECCSS. Section 1 x 4 x 4 m. high. Panel 12 x 4 in. Assembled and tested 213.13.0. Kit £10.10.0. Add 51-carriage. Specially recommended for use with the



A really versatile instrument that makes a handy, pocket size tool. Measures AO or DC voltage in three ranges of 0-15-160-1000 v. Resistance 0-100,000 ohms, and Current 0-150 mA. D.C. Size only: 3½ x ½ x ½m, with ingenious dial design, providing a clear, easily read scale. Complete with battery and test leads.

PORTABLE NEW TAPE RECORDER

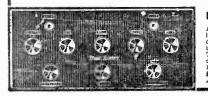


Exceptionally low-priced, but actually a robustly made reliable instrument which can be used anywhere for note which can be used anywhere for how taking, idea recording, dictation, etc. Mechanism solidly built onto rigid steel chassis and housed in tough grey plastic case with carrying strap and clear plastic tape deck cover. Fitted with single multi-selector function switch and volume control. Hand microphone has Stop/Start thumbswitch for remote control of record and playback trans-scription. Complete with tape and spare spool, mike and miniature ear-piece. Size only: 8 x 7\frac{1}{2} x 2\frac{1}{2} in. bigh. £6.19.6. Carriage 4/6.

VANDAL PROOF CAR AERIAL Automatically locks below wing when pushed down—withdraws only with special key. 5-draw telescope aerial extends to 4ft. Retracts into concaled plastic tube. Fits any wing contour. With fitted lead, standard plug, 2 keys, keyring, fitting instructions. 39/6. P. & P. 2/6.

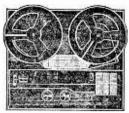
PASSIVE CONTROL UNIT

Specially designed, self-contained unit for use with the Ten plus Ten, either fo Specially designed, self-contained unit for use with the Ten pins Ten, either for direct attachment to chassis or for remote fitting. Incorporates switched inputs for crystal or ceramic pick-up, radio and tape replay together with Vol., Bass, Treble and Balance controls on an attractively styled and finished front panel. Sens. 230 mV. for 10 watts, Imp. 500 K. Size 14 x 2 x 2in. Fanel 15; x 2/m. For dynamic or low output pick-ups, use Dual Channel pre-amplifier described below. Passive Control Unit assembled and tested and complete with Ten plus Ten Amplifier 284.0. & kit 220.0.0. Add 10; corridge.



DUAL CHANNEL PRE-AMPLIFIER

Actually twin Two-Valve Pre-amplifiers which together provide an extremely versatile and sensitive imput arrangement for the Ten plus Ten amplifier in place of the Passive Control Unit. Features include, dual inputs for mono and stereo Magnetic, Variable Reluctance, Crystai and Ceramic pick-ups, dual inputs for direct and pre-amplified tape playback and radio; separate continuously variable Bass, Treble, and Volume and Balance controls. Switching permits Mono or Stereo operation, equalization conforms to BIAA on discreplay, Power input \$20,505 v. at 6 m. A and 6.3 v. at 1 amp. Size 11 x 5 x 4 in. high. Panel 12 x 44, Assembled and tested and supplied complete with Tan plus Ten Amplifier 234.0.0 Kit \$27.0.0, Add 10/6 carriage. Dual channel pre-amplifier only. Assembled and tested \$15.0.0 Kit \$12.10.0



DUVIDAL TAPE SPLICER



14/6

Essential for editing and making immaculate joins in broken tape. Twin clamps hold broken ends in perfect alignment; integral eatting tool makes diagonal spice and trims away surplus splicing tape when join as complete. Size only 3 x 2 x 1 jim.

HF/TR3 TAPE **AMPLIFIER**



Easily the best complete tape amplifier available to the home builder. Supplied already matched for the Magnavox 363

Features include: switched equalization for all speeds (CCIR standards at 7½ i.p.s.) Treble boost incorporated during Record; Bass beaut. incorporated during Record; Bass boost during playback, speakers output matched for 3, 7.6, and 15 ohms, additional outputs for extension speaker, bone monitoring on Record and Hi-Fi playback through existing systems, inputs for Mic. Pick-up, and VHF Radio. Valves: EPs6, ECC83. EL94, EMM, EZS1. Size overali: 11 x 6 x 6in. (Panel 13½ x 3in.). Power pack on separate chassis size 7½ x 3 x 4½n. Amp. & power pack kit of parts 213.13s. Assembled and tested £19. Add 7/6 carriage.

MAGNAVOX 363 TAPE TRANSPORTER(Left)

Manufactured to precise limits that permit recording and tape playback to the highest standards set by the Music Industry. Simple, reliable design employs a single high-duty motor with heavy fiywheel, Fratures include fast wind on and rapid rewind, pause control, 3-speed selection with interlock, built-in revolution indicator, plano key controls. Streeds 12. interlock, butli-in revolution indi-cator, plano key controls. Speeds 18, 3? and 7½ i.p.s. Wow and flutter 0.10% on 7½ i.p.s. Max. spool size 7in. Playing time up to 120 min. per track from 1,2000tt. standard tape. Size 13½ x 11m. plus 5½in. below mounting board. With 4 track heads, 210,100. With ½ track heads, 213 19,6. Add 10½ curriage and insurance.

TAPE HEAD **DEMAGNETIZER**

A must for serious tape users! Tape headsbecompermanentlymagnetized with constant use; effect is enumbative and leads to background noise that prevents the achievement of perfect recordings. Highly effective, mans operated device is simply applied to be a made and the same arrive magnetic condition things are sufficiently applied to design the same arrive magnetic condition things are sufficiently applied to design of infunishing a mortivation of the same arrives magnetic condition of infunishing a mortivation of the same arrives are sufficiently as the same arrives and the same arrives are sufficiently as the same arrives are sufficiently as the same arrives are sufficiently as a same arrives are sufficiently as a sufficient as a same arrives are sufficiently as a sufficient as a suffic loops of diminishing amplitude, leaving head substantially free of magnetism. Cleans any tape head in seconds. 29/6 P. & P. 2/-.

TAPE PRE-AMP TYPE 'C'



Specially developed by Mullard Laboratories for use with high quality replay systems, and supplied specifically matched for use with the Magnavox 363 tapedeck Features include: ferrovacule pot core inductors include ferrovacule pot core inductors oscillator incorporation of the feature of the feature of the feature ferrovacule for matching to existing high-quality amplifier systems, inputs for Miller processed in case size 11½ x 6½ x 3½in. Ferrovacule feature f

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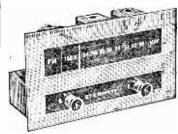
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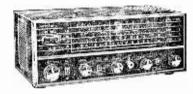
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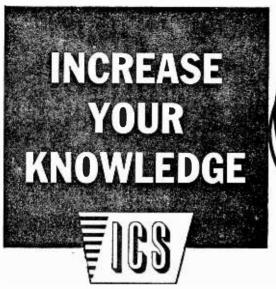
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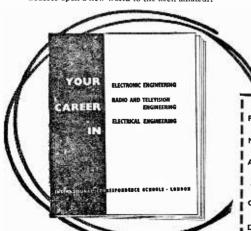
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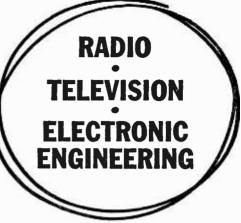
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Size only 10½ x 5½ x 7½in. Rating 8
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c.p.s. Cabinet beautifully finished
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OUTPUT 10 WATTS R.M.S. into 15 ohms. OUTPUT 15 WATTS R.M.S. into 3-4 ohms. Maximum Instantaneous Peak Power Out-

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ILITUS:
SENSITIVITIES: Magnetic P.U. 4
mV. Crystal or Ceramic P.U. 400 mV.
Microphone 45 mV. Tape Head
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FREQUENCY RESPONSE: 20-20,000 c.p.s.
TREBLE CONTROL: +15dB to -14dB at

THEBLE CONTROL: +13dB to -14dB at 10 Kcls.

10

WE PROUDLY INTRODUCE TWO COMPLETELY NEW UNITS WITH TECHNICAL SPECIFICATIONS COMPARING MORE THAN FAV-OURABLY WITH SIMILAR AMPLI-FIERS AT 2-3 TIMES THE COST,



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CONTROLS:5 position Input Selector, Bass Control, Treble Control, Volume Control, Balance Control, Stereo/Mono Switch, Tape Monitor Switch, Mains Switch, INPUT SOCKETS (Matched Pairs) (1) Magnetic P.U. (2) Ceramic of Crystal P.U. (3) Radio/Aux. (4) Tape Head/Microphone.

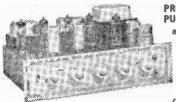
Operation of the Input Selector Switch assures appropriate equalisation.

oper admit the fight selector switch assures appropriate equalisation. The fight of the control of the control of the the control of the control of the control Attractive Facia and the control of the Knobs. Neon Panel Indicator. Above facilities, etc., except for Gang-ing and Balance Control, apply also to Super 15.

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Based on a current Mullard design and employ-ing valves ECC83, ECC83, ECL86, ECL86 ECL86, ECL86, EZ81. Send S.A.E. for leaflet.

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PROVIDING 10/14 WATT ULTRA LINEAR PUSH-PULL OUTPUT ON EACH CHANNEL

SUITABLE for "MIKE", GRAM, RADIO or TAPE.

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 Four-position tone compensation and
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 Will amplify direct from Tape Heads.

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 Separate Bass "Lill" and "Gut" and trable
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5 Gns. Carr. 7/6. SENIOR MODEL

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AUDIOTRINE HI-FI LOUDSPEAKER

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HI-FI



A highly sensitive Push-Pull high output unit with self-contained Preamp./Tone Control Stages. Performance figures compare equally with most expensive amplifiers available. Hum level—708E. Frequency response ± 3dB 30-20,000 c/s. A specially designed sectionally wound ultra linear output transformer is used with 807 output valves. All first grade components. Valves EF86, ECC83, 807, 807, GZ34. Separate Bass and Treble Controls. Minimum input required for full output 12 millivolts so that any kind of Microphone or Pick-up is suitable. The unit is designed for Cubs, Schools, Theatres, Dance Hails or Outdoor Functions, etc. For use with Electronic Organ, Tor Radio Tuner, Two inputs with associated volume controls so that two separate inputs such as Gram and "Mike" can be mixed, 200-250v. 50 cfs. A.C. Mains. Output for 3 and is ohm speakers. Complete kit of parts with fully punched chassis and point to point wiring diagrams and instructions. 12 Gns. 10/1- valves, 12 months' guarantee for 16 gus. for leaflet. TERMS: Deposit 48/- and 9 monthly payments of 33/3 (Total 217.7.5).

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PUSH-PULL ULTRA LINEAR OUTPUT "BUILT-IN" TONE CONTROL PRE-AMP



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A complete set of parts for the construction of a stereo amplifier giving 5 watts high quality output on each channel (total 10 watts) Sensitivity is 50 millivoits. Suitable all crystal or ceramic stereo heads. Ganged Bass and Treble Control give equal variation of "lift" and "cut". Provision is made for use as straight (monaural) 10 watt amplifier. Valve line-up ECC83, ECC83, ELS4, ELS4, ELS4, EZ44, ED44, EZ54. Outputs for 2-3 ohm speakers. Point to point wiring diagrams and instructions supplied. Send S.A.E. for leaflet. Full constructional details and price list 2/6.

Or supplied factory assembled with 12 months' guarantee for £11.7.6.

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12in. HIGH QUALITY LOUDSPEAKERS

In wainut veneered cabinet.
10 WATT MODEL. Gauss
12,000 lines. Speech coil 3 or 15 ohms £4.19.6

15 ohms.

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Size 18 x 18 x 10in.

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Any of above in artra heavy Rerine covered Cabinets, 21 extra.

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consisting of choke, conden-ser, etc.) and Tweeter. Smooth res-Smooth response and extended frequency range ensure surprisingly realistic reproduction. Standard 10 watt rating. £4.19.9 Car. Senior 20 week.

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For lead, rhythm, bass guitar and all other musical instruments



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especially suitable for Bass Guitar
Incorporating massive 15in. high flux loudspeaker. Rating 25 watts. Individual bass and treble controlled. Substantial cabine and
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High-fidelity output. Separate bass and treble
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Manufacturers' discontinued Model. Push pull output. Latest high efficiency valves. Dual separately controlled Inputs for 'Mike' and gram. Separate Bass and Treble Controls. High Sensitivity. Out-put for 3 or 15 ohms speaker. Guaranteed tested and in perfect working order

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Or deposit of 3 gns. and 9 mthly pymts of 43/2 (Total 214 gns.).

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Consisting of Mains Trans., Metal Rectifier, Electrolytics, smoothing choke, chassis and circuit. 200/250v. A.C. mains, Output 250v. 60 9/1 A.C. mains. mA, 6.3v. 2a.

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Carr. 15/make. Normal price over 17 Gns. £25. Very limited number 17 Gns. to clear with full guarantee. Terms available.

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All the above amplifiers are for the STUDIO deck which is no longer available. The Martin Recordakits will be modified for the new Magnavox deck in due course. Details will be forwarded to enquirers when to hand.
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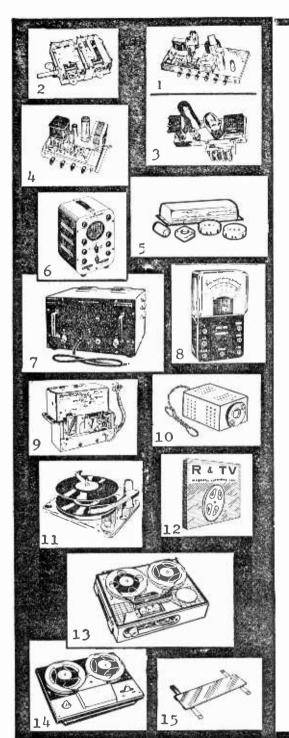
Special versions of the P50 Series are now available for the AF.117 or OC.170 Transistors. Details of the simple modifications to our standard receiver are given in the latest edition of the Constructors Booklet which is priced at 21-.

The new components and their original equivalents are listed below:

		F	or OC4	5	For	AF1 17	Price
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2nd I.F. Transformer	***	P	50/2C0	2	P51	/2	5/7
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PRACTICAL WIRELESS

MARCH 1966 Vol 41 NO 709

MOUNTAIN OF MAIL

ONTENTO

THE size of our post bag seems to increase month by month. Whether in fact this is more apparent than real we have not had the nerve to check upon. We do know, however, that each week we have to clear a mountain of mail.

Mind you, we are not really complaining. It might often appear that we are becoming engulfed in an avalanche of letters, but we undertake the task of clearing them in a spirit of (relatively) cheerful acceptance. For without such response, we would not be able to keep in such close contact with the opinions, aspirations, thoughts, wishes and (we must admit) occasional grouses, of readers. And a hobby magazine without a lively participating readership is dead.

As might be anticipated by connoisseurs of this page, all this is leading up to a few things that have been niggling away in the dark recesses of our minds. The obvious kick-off is to regret that it is impossible always to provide a quick reply. Our policy for users of the Query Service, for instance, is to channel specialised enquiries to members of a panel of experts who operate outside our normal editorial staff. In this way, the best possible advice is obtained, but delays are sometimes inevitable.

It must also be remembered that sometimes a seemingly simple enquiry (which may take only a single line of writing) could require a considerable time in checking references, or in obtaining information when it is not on file.

So, in the interests of everyone, please keep letters concise and clear. Always quote our Reference number on follow-up letters. Do not write for blueprints we do not list. If you want technical advice, always enclose a query coupon and SAE. In fact—if in doubt—read the notes printed each month on the inside back cover page!

Meantime, keep the letters coming and we will do our very best for you!

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-www.americanradiohistory.com

R.A.E. Success

I HAVE recently sat and passed the R.A.E., after following the course in Practical Wireless. I am now practising Morse, to bring my present 6—7 words per minute up to the required 12.

I should like to add that I found John Colley's remarks in "The Morse Bogey" very en-

couraging.

L. R. Tennant.

East Cowes,

Isle of Wight,

A Challenge

A FEW years ago a quite ordinary commercial 6-valve set costing about £15 had three wavebands, and pushed out two or three watts through an 8in. speaker, which was very pleasant to listen to. No present-day transistor set can compare with this,

I have constructed many of your own designs and several commercial kits; I have also listened to quite a few fairly expensive commercial sets. NONE of them is capable of reproducing music to my satisfaction and I have gone back to listening to my ancient mains radio (5-valve superhet, circa 1935).

I can imagine that some of your technical staff will disagree with me. In which case I offer P.W. a challenge! This is to publish a design—for readers to construct—of a transistor radio to the following specification:—

Mains operated. Medium and long wave bands. Output at least 3W. To operate a fair-sized speaker of 15Ω. Tone control that really works. Capable of GOOD music reproduction. Output for tape recorder. (If a separate v.h.f./f.m. circuit could be incorporated, so much the better).

As it is impossible to buy a commercial set approaching this specification, I am certain that many of your readers would be only too delighted to construct a quality radio.

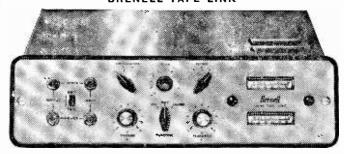
L. Welch.

Hillingdon, Middlesex.

[How about it?-Editor]

NEWS AND..

BRENELL TAPE LINK



The Brenell Hi-Fi Tape Link contains twin recording amplifiers, "Push Pull" Bias/Erase oscillator, twin playback preamplifiers and is designed for use with a three-headed stereophonic tape deck, i.e. separate Erase, Recording and Playback heads of either the half track or quarter track types of the following types:

Erase Record Playback
2/2 TRACK (half track)BL210 or UL290 UK202 UK200
2/4 TRACK (quarter track) ...BL216 or UL296 UK207 UK205

Any make of High Fidelity amplifying equipment capable of supplying a signal level from Radio Tuners, Microphones, Gramophone Pickups, etc., of at least 75 millivolts (the output from a Hi-Fi preamp usually ranges

from 125 to 500 millivolts).

Mono and Stereo recording facilities are provided and whilst recording is in progress one may listen to the recorded material a fraction of a second after recording has taken place or to the signal being fed to the recording amplifier (comparison of the recorded and original signals may be undertaken). Two edgewise scaled illuminated meters indicate the recording signal level and dual concentric gain controls give individual control of the two recording amplifiers. Variable Bias enables the recordist to obtain optimum results at all tape speeds with all brands of tape. Frequency correction for 4 tape speeds, both for recording and replaying, is incorporated.

To ensure elimination of hum, the amplifiers are completely enclosed in a strong metal case, valves are D.C. heated and the power unit is on a separate chassis in order that it may be mounted where it cannot introduce hum into the system.

Price including power unit—£46.0.0. For further details contact Brenell Engineering Co. Ltd., 231 Liverpool Road, London N.I.

A BOOKLET FROM MULLARD

A booklet entitled "Quick-Heating V.H.F. Tetrodes and Double Tetrodes" is now available from Mullard.

The booklet provides designers with information on the techniques associated with the use of quick-heating v.h.f. tetrodes and double tetrodes. It gives abridged data on each type, a selection of practical circuits and recommended valve line-ups for different types of transmitter.

Requests for copies should be made to the following address: Industrial Markets Division, Mullard Limited, Mullard House, Torrington Place, London, W.C.I.

"PUSH-BUTTON MULTIMETER"

Planet Instrument Co., 25 Dominion Avenue, Leeds, 7, are able to supply most of the non-standard resistors, and low value resistors used in the "Push-Button Multimeter," published in the January, 1966, issue of Practical Wireless.

.. COMMENT

NEW POWER TRANSISTOR FROM MARCONI

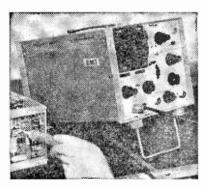
A new transistor, type 203-03, one of the types that has made the Marconi MYRIAD computer possible, has just been placed on the general market by the Microelectronics Division of The Marconi Company.

This new transistor is an n.p.n. silicon planar transistor mounted in a standard (3 lead) TO-5 encapsulation. The combination of high breakdown voltage and current handling capacity with low saturation voltage and fast switching times are believed to be unique.

In a typical circuit, the total time taken to switch ON is 14 nanoseconds, and the total time taken to switch OFF is 90 nanoseconds. The collector-emitter saturation voltage is of the order of 0.3V and maximum collector-base leakage is $0.1\mu\text{A}$. Minimum collector-base and collector-emitter breakdown voltages are both 45V with a minimum emitter-base breakdown voltage of 4V.

Ratings (Limiting Values). Storage temperature —65 to +150°C. Maximum power dissipation at 25°C. case temperature, 3.0W. Maximum power dissipation at 25°C. ambient temperature, 0.8W. Maximum power dissipation at 25°C. mum power dissipation at 75°C. ambient temperature 0.5W. Maximum emitter-base voltage 4.5V. Maximum collector-emitter voltage 50V. Maximum collector-base voltage 50V. Peak emitter current I-OA.

TRANSISTOR OSCILLOSCOPE FROM EMI



A new, low price, solidstate measuring oscilloscope with high performance characteristics has been announced by EMI Electronics Ltd.

Known as the Oscilloscope 101, its advanced circuitry provides stable triggering up to 30 Mc/s. The Y-amplifier bandwidth of 15 Mc/s, coupled with a maximum sensitivity of 50mV/cm, ensures that waveforms are faithfully displayed on the new 3in. c.r.t., type MX54. Specification as follows:

Y AMPLIFIER—bandwidth: d.c. to 15 Mc/s (-3dB); sensitivity range: 50mV/cm to 60V/cm; measurement accuracy: better than \pm 5%.

SWEEP GENERATOR & X AMPLIFIER—bandwidth: d.c. to 4 Mc/s (-3dB): sensitivity: 300mV/cm to 1.5V/cm; sweep speeds: 40ns/cm to 100 ms/cm; measurement accuracy: better than \pm 5%. TRIGGERING—bandwidth: 5 c/s to 15 Mc/s: sensitivity: 0.2 cm internal,

0.2V external; modes: a.c. (level control operative) automatic (level control inoberative).

VOLTAGE CALIBRATION—produces 7 kc/s square waves of amplitudes from 200mV to 40V accurate to 2%.

CATHODE RAY TUBE—EMI type MX54, 3in. diameter operated at 2·6kV. POWER SUPPLIES—95 to 130V, 50 to 60 c/s or 190 to 260V, 50 to 60 c/s or 12V d.c. nominal (11 to 14V absolute), positive earthed.

The power consumption is 25W a.c. or 20W d.c.

The height is 9in., width 8.5in. and depth 15in. The weight is approximately 17 lbs. and the case is finished with silk screen printed front and rear panels and plastic faced covers. The price is £170.

more News and Comment on page 968

The Meaning of Amateur

On READING the item on "The Meaning of Amateur" in the January, 1966, issue I find myself rather puzzled. To purchase a commercially made Tx and Rx and use same if licensed I am wondering what the operator would be an "amateur" of, not having constructed any equipment himself. I have always had the impression that an amateur was a person who used his initiative and produced an article entirely on his own, not having been professionally trained in the subject. The reference sportsmen does not amateur apply in any way and I am rather surprised that such a letter was printed. The difference professional between amateur sportsmen is that the latter are not paid for their activities.

If our Birmingham friend hasn't sufficient interest in radio to enable him to brew his own gear I would suggest he looks to some other hobby where a little energy and initiative is not required.

Long live amateur radio as we know it, with appreciation to P.W. in that field.

J. R. Davidson, G3FG.

Carshalton. Surrey.



Your correspondent on "The Meaning of Amateur" (page 692, December issue) asks people buy expensive equipment rather than "roll their own". The simple answer to this is that the trade has cottoned on to this and almost all components are priced against published circuits. so that the home-made job will cost as much as-and sometimes more than-an on-the-shelf product.

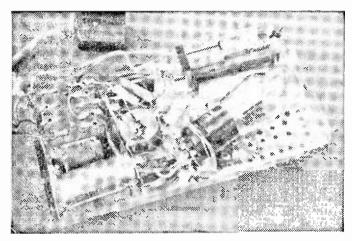
If one wants proof of this one has only to take any good circuit and price the components available on the market-then compare the total with the price of a proprietary item. In addition, how many of us can afford the test equipment, etc., to set up a home-made job?

D. A. Snoad.

Haslemere, Surrey.



A SIMPLE PROXIMITY DETECTOR



by H. Wagner

HERE have been several proximity detectors described in technical magazines over the last few years; most of them rely on the change in anode (or collector) current as a result of change in oscillatory state of a simple feedback r.f. oscillator. This type of detector can be made very sensitive; in fact a true proximity detector and, as such, can be employed in cases where it is important for an operator not to get too close to a piece of machinery, etc. As a burglar alarm it would seem that great sensitivity is not so much required as reliability of operation the moment the guarded article is touched or tampered with.

The little gadget described here is less complex than the oscillator type of detector but, once set, will give reliable service.

Modes of Operation

From the circuit diagram in Fig. 1 it can be seen that in one mode of operation the thyratron is operated on a.c.; by throwing a switch the circuit will run on d.c. This choice of operation is deliberate. If one intends to leave the house unattended for only a short time—to pop around the corner—it is better to select a.c. operation. The

intruder, having had his warning, is now faced with one of two courses of action: (i) Clear off, muttering invectives, (ii) sit down and think out his next move.

If you're out for a short time you'll foil his second course and you will not have unduly annoyed your neighbours.

If you're off for the weekend, switch to d.c. operation. Once triggered the device will not let up until the police get the Electricity Board to disconnect your supply and then it is the duty of the force to protect your property until your return.

If one of these devices is hooked up to each external door, you might ask, how are you going to explain away the shocking noise you make each time you re-enter your own dwelling? The circuit in Fig. 2 shows how one door is provided with a

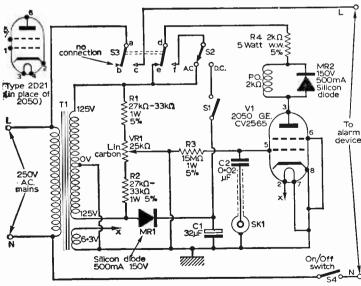


Fig. 1: Circuit diagram of the proximity detector. The relay is a P.O. type, 2-pole, 2-way, $2k\Omega$. Resistors should be high stability types for optimum circuit reliability. T1 is a Radiospares midget type, 125-0-125V and 6·3V secondaries.

touch detector having a bi-metal relay in the output circuit. The 30-40 second delay on this is long enough for a sober man to get his key in the lock, open the door and switch off the device before it starts the bell ringing. The remaining detectors in the house are switched off in the normal manner.

Layout Uncritical

There is very little to mention concerning the circuit. Layout of the components has been suggested in Fig. 3 but need not be adhered to so long as the valve is kept away from the other portions of the circuit such as the transformer, silicon diode and the 5% resistors. If the 2050 valve is used it will be found to run much cooler than the miniature 2D21. If the miniature valve is used, plenty of cooling holes should be drilled in the box within which the device is housed. One of the writer's detectors was built in a larger biscuit tin and one in a somewhat smaller one. Both tins were cleaned with spirit and then sprayed with aluminium paint to improve their appearance.

The valve socket is soldered directly into a small piece of biscuit tin and a lip is bent on the under side so that this can be soldered directly to

the inside of the lid of the box.

Switch S2 can be a more fancy one-pole, two-way one, but an ordinary two-way type is satisfactory. A jumper wire is soldered as shown in the diagrams. S1 is not absolutely necessary since, once the device is operating correctly, the armature in the relay can be made to throw out by setting the switch S2 over to the a.c. position. S1 was left out in the second model. The type of relay used was not very suitable but with the $2k\Omega$ wire-wound resistor in series and a little fiddling with the contact tensions no more trouble was experienced. A $1\mu F$ paper capacitor was tried instead of the silicon diode but this is not recommended. If a $5k\Omega$ relay is available, or even a $4k\Omega$ one, there should be no difficulty at all.

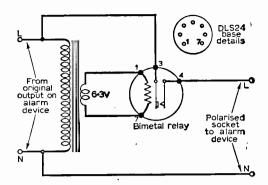


Fig. 2: Connections from unit to provide one door with touch detector.

In the prototype ordinary resistors were used after first using $50k\Omega$ potentiometers to find the correct values in the resistor string across the secondary of the power transformer. Ordinary 20% resistors were useless; 10% were still unstable over a long period; 5% high-stability resistors provided complete reliability.

Mains Voltages

The house voltage in the writer's area is approximately 250V. Where this differs adjustments can be made so that the actual voltage on each side of the centre tap is around 120V. The most important thing is to get the two voltages—a.c. and d.c.—in agreement. The valve data book says the maximum grid resistor should be $10 M \Omega$. With the low voltages and currents used here $15 M \Omega$ was found to be better. An interesting thing about the two valves is that whilst the 2D21 seems more sensitive its action does not appear to be so decisive as that of the 2050. It also runs very much hotter.

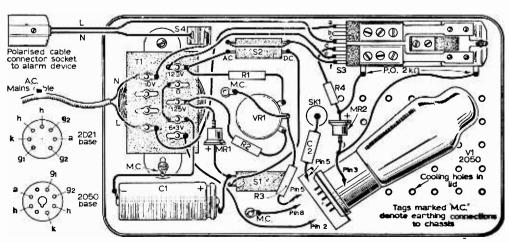


Fig. 3: Layout of components—from the 2050 unit shown in the heading photograph.

Testing the Unit

After the unit has been built it should be tested for positive action of the relay. Allow the set to warm up for about four or five minutes and then turn the $25 k\Omega$ potentiometer until the relay drops out. On touching the core of the coaxial cable at the end remote from the unit the relay should pull in smartly. If it is found that the relay prefers to operate the other way, i.e. prefers to stay pulled in and drops out smartly when the cable core is touched, the remedy is to change over the leads to the primary of the transformer. If this has to be done do not forget to change the leads over at the other end of the cable connectors to keep the polarities correct.

If preferred the delay unit can be built inside the same box as the alarm device. The way described in this article is quite useful as the delay section can be transferred from one unit to the other without in any way upsetting the rather

critical setting of the units.

Once positive action has been obtained the final adjustment should be put off for about four days, during which time the unit should be left on in its assigned position. This will age the valve sufficiently and it is quite extraordinary how the unit will settle down after this initial cooking.

The proximal end of the cable shield will be grounded automatically through the coaxial plug and socket. The other end of the cable—and this should not exceed 4ft in length—has a crocodile clip soldered to the core and the braiding should be trimmed off and taped out of the way.

The mains cable should have a ground wire so that proper grounding of the unit may be effected

through the house grounding system.

Exactly how the crocodile clip is connected to the door has to be found out by trial and error. Too close coupling will virtually short out a.c. hum on which this unit depends for its action.

In the writer's case it was found that a nail driven into the wood about \(\frac{1}{2}\)in. from the "lock" gave just about the right coupling for one unit, whilst the other unit required the nail to be placed about \(\frac{4}{2}\)in. away from the lock.

Field Intensity

One point should be mentioned; make this unit is that it depends upon the a.c. field intensity in its vicinity. If this is altered by switching on lights in the same room—the hall—or, shall we say, using any lights carrying current along wires in the vicinity of the alarm unit, then the unit will have had its sensitivity altered.

In other words, final adjustment must be done with lights out and only the usual things working in the house such as the frig. and water heater. Once this is understood, and the unit adjusted under these conditions, one will be agreeably

surprised at its reliability.

One point should be mentioned: make sure the d.c. output is about the same at the relay contact as the a.c. Otherwise sensitivity will not be the same and results disappointing.

Two of these units have been operating continuously for many months without any sign of

instability.

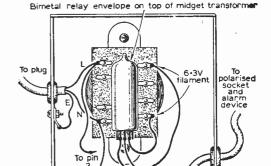


Fig. 4: Physical layout of the unit of Fig. 2.

Tin box :- 45 x 35 x 23 deep

In our area power failures are far more common than elsewhere and it was very necessary to make sure that the unit did not "play up" after the power had been returned. It was found that what really happened was that the unit lost its sensitivity for about ten minutes after "returning" the power and this whether the mode switch was set at "one shot" or "warning".

The third unit operating in the house is the one described by R. Bebbington in the November, 1963, issue of this magazine. This one gave a few false alarms, to my embarrassment, but settled down quite happily when its sensitivity was suitably reduced. Its only weakness is its power output—in noise. A push-pull class B maximum gain, maximum distortion amplifier(!) using two 61.6s in the output stage raised the noise level to a very nice 30W.

The a.c. hum field units drive a G.E.C. burglar alarm bell of very generous proportions, plus two powerful lights directed on to "the right places". The noise and bright lights are quite awe-

inspiring!

PRACTICAL WIRELESS BINDERS

The Practical Wireless Easi-binder is designed to hold normally 12 issues. Please state volume number required otherwise a blank cover will be sent.

A new version of the Easi-binder with a special pocket for storing blueprints and data sheets is now available. The price is 11/6d inclusive of postage.

Order your binder from: Binding Department, George Newnes Ltd., Tower House, Southampton Street, London, W.C.2.



Aerial Tuning Methods

GORDON J. KING

N aerial is possessed of distributed inductance and capacitance. This makes it equivalent to a transmission line and thus in many respects it, behaves like a tuned circuit. An aerial is said to be tuned when its length equals a half wavelength or a multiple of half wavelengths of the signal and when the aerial is "unearthed". With an "earthed" aerial tuning occurs when its length equals a quarter wavelength or a multiple of quarter wavelengths of the signal. Here, then, we have the fundamental conception behind half-and quarter-wave aerials.

Tuned Aerials

An aerial abstracts signal energy from a passing radio wave. If the aerial is of a length equal to the wavelength of the signal, then a complete wave of electrical current is induced into it, as shown in Fig. 1. Here it will be seen that wave A-B is identical to wave B-C but of opposite sign. Thus, a complete current change can be accommodated in an aerial whose length is half that of the aerial in Fig. 1. This is shown in Fig. 2 and is representative of the half-wave aerial. The aerial is unearthed in this case.

An earthed quarter wave aerial works in a similar manner, but the missing second quarter-

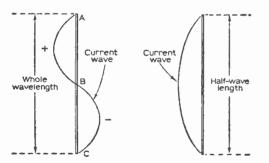


Fig. 1 (left): A current wave of the nature illustrated here is induced into an aerial which is adjusted in length to suit the wavelength of the signal.

Fig. 2 (right): Since a complete change of current occurs both at A-B and B-C in Fig. 1, an aerial tunes when its length accommodates a half of a whole wave, as this diagram shows.

wave section is produced by a reflection in the earth of the first quarter-wave section. This is called an "image" aerial. The joint action of a quarter-wave aerial and its image is the same as that of an unearthed half-wave aerial. The image

effect is depicted in Fig. 3.

V.h.f. aerials for radio and television are usually of the half-wave variety, since they are not normally earthed. This means that the overall length of the aerial corresponds to half the wavelength of the v.h.f. signal. In practice, the length of the aerial is not exactly half the wavelength of the signal because the velocity of the radio wave on being induced into the aerial is reduced slightly. This is corrected by arranging for the physical length of the aerial to be about 95 per cent of the signal half wavelength. That is, by making the aerial 5 per cent shorter than the signal half wavelength. Thus, to tune to a wavelength of, say, 10 metres, a half-wave aerial would need to have a physical length of about 9.5 metres.

Simple Calculations

Radio waves in free space have a velocity of 186,000 miles per second, equal to 300,000,000 metres per second. The signal wavelength then, is really a measure of the distance that a full radio wave travels in one second. Since we know the wave velocity, therefore, we can easily find the wavelength by dividing 300,000,000 by the signal frequency in cycles per second (c/s). The answer is in metres.

We can ease the calculation at v.h.f. by crossing off six noughts at the top of the equation and working in megacycles per second (Mc/s) at the bottom instead of in c/s. Remember, here we are dealing in whole wavelengths. The length of a tuned unearthed aerial is 95 per cent of half the wavelength value so calculated. Let us try a simple example

Say the signal frequency is 150Mc/s (in the v.h.f. spectrum). The wavelength of that signal is thus 300/150, or 2 metres, Half is 1 metre, and 95 per cent of this is 0.95 metre, which is the length of a half-wave aerial that would tune 150Mc/s. Easy?

Incidentally if we want to work in feet we should multiply the length in metres by 3.281 or in inches multiply by 39.37. Thus, the 0.95 metre aerial illustrated above is equal to 3.117ft. Using

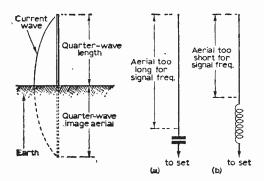


Fig. 3 (left): A quarter-wave aerial which is effectively "earthed" at one end behaves as a half-wave aerial by virtue of the quarter-wave "image" of the real aerial reflected by the ground.

Fig. 4 (right): The inductive element of an aerial which is too long for the signal can be tuned out by series capacitance, as shown at (a), while the capacitive element of an aerial which is too short for the signal can be tuned out by series inductance, as shown at (b).

the above arithmetic, a formula for calculating the length of an aerial in feet direct is length in feet equals 468/frequency in Mc/s. Of course, it follows that a quarter-wave aerial is exactly half the length of a half-wave one.

Just one more thing here and that is since the wavelength of a signal is equal to the wave velocity divided by the frequency, the frequency of a signal is equal to the wave velocity divided by the wavelength. This simply means that by dividing 300 by the wavelength in metres we are given the frequency in Mc/s, or by using 300,000,000 at the top the answer is in c/s.

Tuning Artifices

So far so good but what if one wants to operate an aerial over a range of signal frequencies? The obvious solution is to arrange for the aerial to be adjustable in length so that it can be tuned accurately to any particular signal frequency or

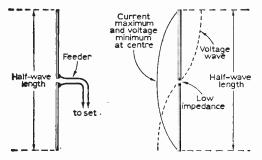


Fig. 5 (left): A half-wave aerial is generally split in the centre to take the feeder, as shown here.

Fig. 6 (right): The voltage and current distribution in a tuned half-wave aerial. The impedance at the centre is low and at each end high.

wavelength. This is done in fact, where optimum radiation (in the case of a transmitting aerial) or signal pickup is demanded. Often, however, a number of aerials are used which can be switched to the transmitter or receiver to suit the sending or received signal frequency.

There is another way of handling the problem which is based upon the fact that if an aerial is not exactly the correct length for resonance, it can be resonated by adding series inductance if it is too short or by adding series capacitance if it is too long. The idea is shown in Fig. 4. This tuning idea is derived from the fact that a signal voltage applied to an aerial will encounter a capacitive reactance at frequencies just below resonance and an inductive reactance at frequencies just above resonance. Thus, the series inductance neutralises the capacitive reactance of too short aerials, while the series capacitance neutralises the inductive reactance of too long aerials. When an aerial is correctly tuned its loading point looks like resistance.

An aerial resistance or impedance stems from the fact that, apart from a current component of the abstracted signal, it also has induced into it a voltage component. Thus, the resistance or impedance is given by the voltage at any given point divided by the current at the same point. This means that the resistance or impedance is low when the voltage is low and the current high and high when the voltage is high and the current low.

An unearthed half-wave aerial is often disconnected electrically at its centre, at which point a connection is made to the feeder as shown in Fig. 5. This is known as the half-wave dirole. Dirole because the aerial is then in two sections "di" (two) "pole" (sections). When an aerial is so arranged the impedance at the centre is low because the current is at maximum and the voltage at minimum as shown in Fig. 6.

Impedance

The actual impedance offered by an aerial to a series voltage is influenced by various factors, including frequency ground losses, type of aerial, length and so forth. However, the impedance at the centre of a tuned half-wave dipole is in the order of 75Ω . This point thus represents a good match to 75Ω coaxial feeder or twin feeder. The transference of signal to or from an aerial is governed by the matching, the closer the match the better the transference. A serious mismatch loses signal power because the signals are then reflected up and down the feeder and tend towards cancellation.

The impedance at the end of a tuned aerial is high, in the order of thousands of ohms, because here the voltage is high and the current low. The impedance at the "earthed" end of a ovarter-wave "earthed" aerial is also low, comparable to that at the centre of an "unearthed" dipole. Quarter-wave aerials are often used with mobile radio communication systems on cars. Here the metal body of the car, represents the earth and it is in this that the aerial image is reflected.

An "earthed" aerial should not be taken to

imply that one end is really connected direct to earth. It simply signifies that the missing quarterwave section is made up either by the earth itself or by the mass of metal (such as the metal body of a car) by virtue of the image effect described earlier. Connection to a so-called earthed quarterwave aerial is shown in Fig. 6.

Ordinary car radio aerials are not normally tuned in terms of length. Car radios and transistor sets operated in cars tune over the l.w. and m.w. bands. Of course it would be impossible to employ a half- or quarter-wave aerial tuned by length to such long wavelengths. The loss of efficiency by the use of an aerial of considerably shorter length than the signal half or quarter wavelength in such cases is countered by the use of high gain r.f. and frequency changer stages in the sets themselves.

The same really applies to domestic radios which work from short lengths of aerial wire. There is no real tuning in the aerial itself but sometimes "loading coils" are used in the aerial circuit particularly on the l.w. band, to enhance the signal transference from the aerial to the first stage in the set.

Tuning by Inductance

It is possible dramatically to improve the performance of a car radio or transistor set working in a car from a short, outside car-type aerial by loading or tuning the aerial with series inductance and then adjusting the length of the aerial to resonance at the required frequency. This gives the condition depicted in Fig. 4b.

For m.w. applications such a coil can be wound on a length of ferrite rod and then introduced between the bottom of the aerial and the set as shown in Fig. 8. A practical coil of this nature can consist of 120 turns of 20 s.w.g. enamelled covered wire close wound on a 4in, ferrite rod of When connected in the aerial in. diameter. circuit as shown in Fig. 8 the length of the telescopic aerial should be adjusted with the set tuned to a weak m.w. station at the top of the band

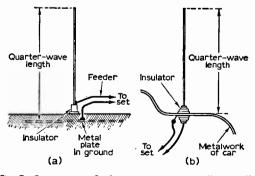


Fig. 7: Connecting a feeder to a quarter-wave "earthed" aerial. At (a) a connection is made to a metal plate in the ground, beneath the aerial, while at (b) the metal body of a car, for instance, is used instead of an earthed plate.

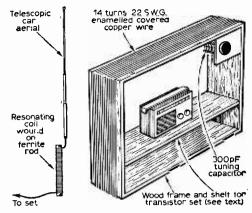


Fig. 8 (left): An inductor connected at the end of a telescopic aerial can be used to improve reception. The system is then tuned by adjusting the length of the telescopic gerial when the set is tuned to the required station. Details of the "resonating coil" are given in the text.

Fig. 9 (right): Greatly improved performance of small transistor portables on distant or weak stations is possible by placing the set in a tuned loop, as shown here. Details are given in the text.

(round Radio Luxembourg area) for maximum pick-up.

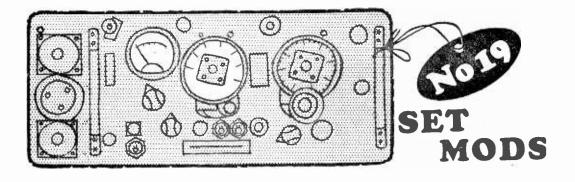
On the s.w. bands a too long aerial can be peaked on any particular station by connecting a variable capacitor of 300pF in series with the aerial at the set end, giving the condition as shown in Fig. 4a. The capacitor should be adjusted for maximum response.

Tuned Loop

Transistor sets feature ferrite rod aerials of high efficiency the coils on which are tuned by the r.f. section of the two-ganged canacitor There are times, however, when a greater signal pick-up would be desirable, especially at the high-frequency end of the m.w. band. This can often be achieved without the use of an external aerial or amplifier by running the set itself within a tuned loop as shown in Fig. 9. The loop is wound on a wooden frame with a shelf inside upon which the transistor set can be stood. For normal m.w. reception the loop should consist of 14 turns of 22 s.w.g. enamelled covered copper wire the ends of which are connected across the tags of a single section 300pF tuning capacitor. This can be mounted on a small wooden panel in one corner of the frame as shown in the diagram. A suitable overall size for the frame is 18in, x 18in, x 6in, though the width is really governed by the dimensions of the transistor set, for the 14 turns of wire take up very little space.

The set is placed in the loop as shown and both the loop and the set orientated for maximum The loop tuning capacitor is then pick-up.

adjusted for maximum boost.



by S. Simpson

.S.19, Mk. 3, now widely available from dealers in Government surplus equipment, was employed by the Army as communications equipment for use in tanks. It is of rugged construction and contains an intercom amplifier, a v.h.f. transceiver, an h.f. transmitter, and a corresponding five-valve superhet receiver. This receiver is the subject of the following modifications; when modified, it becomes a nine-valve (including rectifier) receiver comprising two r.f. stages, mixer, two i.f. stages, detector/avc/first a.f. stage (which can be tapped for head-set operation), output stage and beat-frequency oscillator. The frequency ranges, 2Mc/s to 45Mc/s and 45Mc/s to 8Mc/s, are unchanged. Power is obtainable from 240V a.c. mains.

This article is not suitable for a novice, unless he is prepared to "write off" the cost of his W.S.19 as "gained experience" if he fails to cope with the job. It is written for the amateur who has built one or two receivers and other equipment using valves, and has overcome the snags which perhaps arose. He must have access to a fine-pointed soldering iron, a comprehensive test meter, a reasonable workbench with adequate light on which the receiver can be left undisturbed (this is not a "one-evening" job) and a power supply giving 6.3V at about 3A, and 200V at about 50m.A. An existing a.c.-operated receiver can be put to use, as described later.

Components

One or two additional components will be required. These are:—

- (1) Mains transformer giving 250/0/250V, 50mA, 6:3V at 3A, 5V at 2A. The transformer should have above-chassis mounting facilities.
- (2) Smoothing choke, approximately 10 Henries at 50mA. Under-chassis mounting and of small dimensions as space is limited.
- (3) 8 + 16μF, 300V working, electrolytic capacitor. Under-chassis mounting; space is limited.
- (4) 5Z4 or 5Z4G rectifier.
- (5) Approximately twelve resistors.
- (6) Two single-circuit telephone jacks; one sockets.

Part 1

(7) One 3Ω impedance permanent-magnet loud-speaker.

Quantity insulated single-lead flex (nine different colours are very desirable); quantity twin p.v.c. flex; approximately 3ft. coaxial lead.

The Procedure

The procedure adopted by the author was:

- (1) an initial check of the receiver as found;
- (2) carry out one of a series of modifications, then check that the receiver is still operational:
- continue with the next modification, check, and so on.

The reader will find that he covers some ground more than once; the reason is apparent when one studies the complexity under the W.S.19 chassis. If a lot of the work is attempted at one go, only an experienced amateur will extricate himself from the tangle of snags he will probably set up. "little and often" is a much better policy when dealing with W.S.19.

The Modifications

The series of modifications is carried out in the following order:—

- (1) Conversion of valve heaters circuit; initial check.
- (2) Removal of send/receive relays and restoration of affected h.t. circuits: check receiver.
- Inclusion of headset output; check.
- 4) Restoration of a.v.c. | Carried out as one modifi-
- (5) Restoration of b.f.o. note control.
- (6) Inclusion of additional r.f. stage; check.
- (7) Inclusion of loudspeaker output stage; check.
- (8) Inclusion of band-spreading; check.
- (9) Inclusion of mains power supply; no check possible at this stage.
- (10) Modification to A SET, B SET, and I/C switch assembly to provide "mains on" and "h.t, on" control, also headset sockets check.
- (11) Inclusion of monitoring system; check,

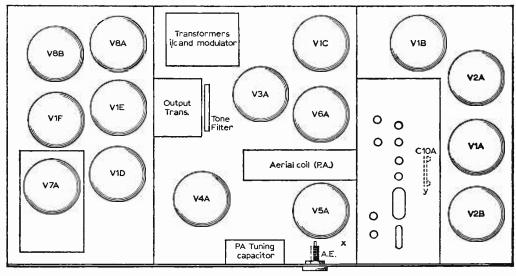


Fig. 1: Topside chassis layout before modification.

Illustrations

The reader should study the illustrations provided in this article in conjunction with the W.S.19 as found. No attempt has been made to produce an accurately-dimensioned drawing of the topside of the chassis, nor to include all of the assembly, but identification of the parts concerned should be quite easy.

The underside view (Fig. 2) shows all valve sockets concerned and their orientation, also the locations of certain terminal strips and existing components mentioned in the modifications. It also shows as shaded rectangles, the positions of additional components. An overall circuit diagram of the modified receiver is not given. The original heater circuit is given in Fig. 3 and compared with the modified version.

Time Involved

One is often asked, "How long will the job take?". The answer can only be based on certain assumptions. Given a fairly intelligent amateur possessing more than basic knowledge and the necessary tools, and working two hours nightly, he should complete the work in approximately ten days. The individual reader must apply this "yardstick" to his own ability.

Making a Start

The work begins by checking the "found" condition of the receiver, and the valves,

- Remove the securing screws and remove the chassis from its outer case.
- (2) Remove all valve screens, including the cover over the v.h.f. section; note that the cover carries a valve-location plan and check it agrees with Figs. 1 and 2.

(3) Remove all valves; check the following starred valves are present and usable:—

★V2B	6K8	*V3A	6Q7	V8B
★V1A	6K7	V6A		VIE
★V2A	6K8	★V5A	6K7	V1F
★V1B	6K7	V4A		V1D
*V1C	6K7	★V8A	6V6	V7A

(4) Check that the general mechanical condition of the receiver (controls, switches, etc.) is apparently sound.

Initial Check: Heaters

The initial check involves changing the heater circuit from the original (Fig. 3a) to that shown in Fig. 3b; thereafter, an external power supply is used to check that the receiver, as found, is operational.

- Study Fig. 3a, then, by a zero ohms check, ascertain which heater pins are, in fact, earthed. Note these on Fig. 2.
- (2) Proceed with interconnections shown in Fig. 3b.
- (3) At the "A SET, B SET I/C" switch assembly (hereafter "3-switch assembly"), loosen the securing nut at each switch.
- (4) Remove four 6BA ch.hd. screws passing through the assembly plate. Undo the switch securing nuts completely, then remove the plate. The DPDT switches and associated wiring are now accessible. (This procedure is necessary because of the very limited wiring to these switches.)
- to these switches.)

 (5) Check A SET is switched off (toggle upward). Check for zero ohms between pin 3 on PL2 (lower plug on left front of panel) and the upper contacts of A SET. (Pin 3 carries LT+).
- (6) Switch A SET on and check for zero ohms

between PL2, pin 3 and the appropriate lower contact on A SET. If the switch is erratic replace it and wire as found. (One of these wires is cut away at the next operation; read the step below before wiring).

(7) Having found the appropriate l.t. contact, sever the wire (lead "a" in Fig. 3a). Solder a new lead ("b", Fig. 3b) between the l.t. contact and the "live" pin on V5A. The lead should be capable of carrying 3A without undue loss.

Initial Check: H.T. Supply

Check the h.t. line as follows:-

- (1) Check for zero ohms between PL2, pin 6 (h.t. input) and the remaining unchecked contact on the upper side of A SET, with the switch "off".
- (2) Check for continuity across the switch to the relevant contact with A SET switched "on".
- (3) Check for zero ohms between PL2, pin 6 and tag 9 on TS1 (Fig. 2). Disconnect the meter and refit the 3-switch assembly.

Initial Check: Power Supply

A 6.3V 3A a.c. supply, together with approximately 200V h.t., are required. Sources will, of course, vary, but it is assumed the reader has the knowledge and ability to adapt the power supply in an existing a.c.-operated radio, radiogram, etc., to his needs. The chassis of the adapted source should be connected to W.S.19 chassis, the h.t.+ line to Pl.2, pin 6, one 6.3V line to Pl.2, pin 3, and the remaining line to W.S.19 chassis. Caution must

be taken to guard against crossed earths short-circuiting the 6:3V supply; if the adapted source carries dial lamps, crossed earths will be shown up by failure of the dial lamps to light.

The W.S.19 will withstand 280V, but an attempt should be made to reduce h.t. to approximately 200V by use of a voltage dropper; the W.S.19 end of the dropper will require at least $8\mu F$ bypass capacitance to W.S.19 chassis.

Initial Check: Operation

With the adapted power source switched off, proceed as follows:—

- Temporarily fit two crocodile clips to the headset-cord connections. Clip one to W.S.19 chassis and the other to one lead of a 0·01µF, 300V capacitor. Connect the free lead of the capacitor to the white lead of the output transformer (Fig. 1).
- (2) Fit the starred valves (referred to earlier) to the relevant sockets.
- (3) Connect a reasonably efficient aerial to the A set AERIAL plug. An earth is helpful but not essential. Turn up A.F. GAIN and R.F. GAIN.
- (4) Connect a voltmeter to read 300V maximum between W.S.19 chassis (negative) and PL2, pin 6.
- (5) Don the headset. Switch on A SET. Switch on the adapted power source.
- (6) Check that the valves in W.S.19 are alight. Watch for h.t. at the voltmeter; before this rises to a maximum the output of the receiver should be audible. If it is not, check that the M.C.W., C.W., R.T. switch (hereafter

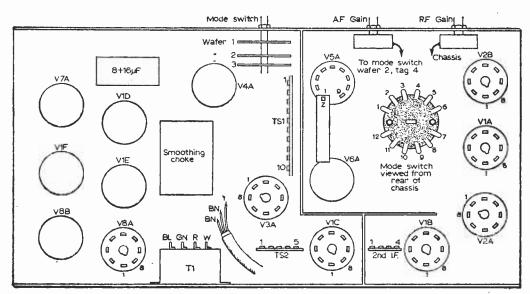
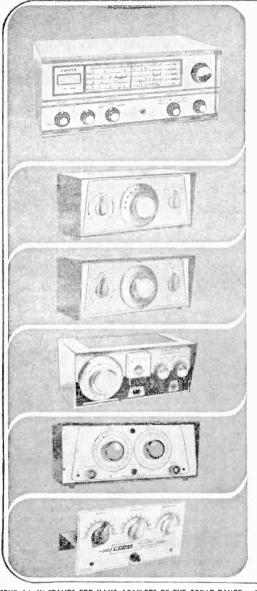


Fig. 2: Layout of valve sockets (underside). The additional components are the 8+16uF capacitor, smoothing choke and T1.

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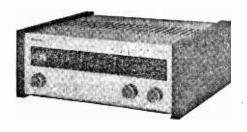
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"mode" switch) is at R.T. If the headset is still silent, transfer the 0.01 µF capacitor lead from "white" to "blue" on the output

transformer.

(7) Check A.F. GAIN and R.F. GAIN are operational. Check for noisy valves. Set the mode switch to C.W. and check that the beatfrequency oscillator (b.f.o.) is operational. (Note that maximum R.F. GAIN can swamp the b.f.o.; reduce R.F. GAIN if this trouble is found). Check the b.f.o note-shift control is operational (the change of note in the author's version is very slight).

(8) If all is well, switch off the adapted power source, then A SET. Disconnect the headset from the capacitor and chassis; leave the capacitor in position. Disconnect the power supply leads but do not discard the arrangement as it will be necessary in further checks.

Modification can now begin.

Removal of Send/Receive Relays

These are two relays mounted on a common bracket under the chassis. These are removed to provide room for power supply components. Since these relays carry certain h.t. leads to the receiver section, elimination of the relays is followed by restoration of necessary h.t. circuits, and a receiver serviceability check. Proceed as follows.

Cut away all wiring to the relays; soften the locking varnish at the bracket holding screws by wetting with methylated spirit. Remove the screws.

Switch on A SET. Check for zero ohms (approximately) between PL2, pin 6, and TS1, tag 9 (Fig. 2). Switch off A SET.

- (3) Connect one ohmmeter lead to pin 6 on V1C (occupied by junction of two resistors). Connect the ohmmeter free lead in turn to each red or orange lead in the group coming from the vicinity of V1C (these leads were cut away from the relays) and check for zero ohms.
- (4) Connect the lead so found to TS1, tag 9. Connect the ohmmeter to tag 9 and on high ohms range check for continuity at the screen grids (pin 4) of VIA, VIB and VIC. Restore cut connections, if any, by checking backward from the affected valve.

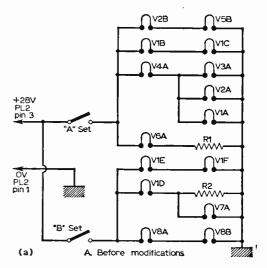
(5) Restore R.F. GAIN by earthing the central contact to an adjacent tag in the screened compartment of the waveband switch.

Recheck the receiver, at present operational without A.V.C. and B.F.O.

Inclusion of Headset Operation

This modification converts V3A, into an A.F. amplifier to drive an output valve. From its anode, a feed to a headset is provided.

- (1) Cut all wiring away from the modulator transformer, intercom transformer, and output transformer. Remove these components; keep the output transformer handy.
- (2) Remove all wiring to V4A socket; remove



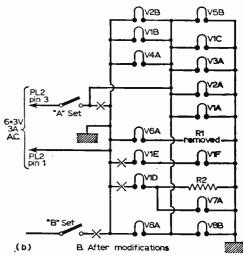


Fig. 3: The heater circuitry (a) before modifications (b) after modifications.

the socket (secured by two 4BA screws into stand-off pillars).

- On the mode switch, wafer 2, pin 4 (Fig. 2), locate a screened lead passing to V3A control grid. Extend the connection from pin 4 to include pin 3, also on wafer 2.
- (4) At A.F. GAIN control, connect the centre contact to wafer 2, pin 4, mode switch.
- (5) Connect a $47k\Omega$, 1W resistor between TS1 tags 5 and 9. Cut short the existing mauve wire on tag 5.
- A tubular 0.01μF capacitor exists at tag 5. The other lead of this capacitor terminates on a tag below tag 4. (TS1 is a double-row connector strip). To this tag, 4A, connect one lead of a 4in. piece of flat, twin flex.

Earth the remaining lead on tag 3. This twin lead will eventually carry phone output.

(7) Remove the 3-switch assembly. Cut the wiring to the 1/C switch and remove the switch. In its place, fit a single circuit phone socket (not self-shorting).

(8) Connect the phone output lead to the socket, then refit the switch assembly (hereafter "2-

switch assembly").

(9) As found, the mode switch, when set to "C.W.", disconnects h.t. from V3A screen grid. To prevent this, connect TS1 tag 7A (lower row, under tag 7) to TS1 tag 9.

(10) Connect the headset clips to a phone jack, insert the jack into the phone socket, then recheck the receiver which is at present without A.V.C. and B.F.O.

Restoration of AVC and BFO

Removal of the relays interrupted the A.V.C. and B.F.O circuits. Restore them as follows.

(1) Locate a severed 3-wire cableform (Brown, Brown Yellow) passing close to the left of TS2 (looking from rear of the inverted chassis).

(2) Check for zero ohms between TS2, tag 4 (Fig. 2) and one of the brown leads.

- (3) Extend the brown lead so found to wafer 3, tag 11 on the mode switch (include unused tag 8 when counting). Cut away any WS19 wiring existing on tag 11.
- (4) Check for zero ohms between the yellow lead of the severed cableform and tag 3 on the 2nd i.f. transformer connection strip (Fig. 2).
- (5) Extend the yellow lead to wafer 3, tag 2 of the mode switch, first cutting away existing wiring.
- Strap wafer 3, tags 12 and 1 and earth at TS1, tag 2.

The receiver can now be checked if desired, but B.F.O. is still absent. To restore B.F.O., continue as follows.

- (1) Locate A NET switch on the extreme right of the panel face. Ensure the dolly is *upward* to prevent misleading results of ensuing checks.
- (2) Set the mode switch to C.W., then unship the mode switch (held by two 4BA ch. hd. screws passing through the panel).
- Locate a mauve wire on wafer 2, tag 8. Check for zero ohms between this tag and V2B, pin
- (4) Also leaving tag 8 is a second mauve wire, part of a cableform including two whites, one yellow, one green, one red. All but the mauve lead will have been cut in earlier steps. Locate the red lead and check for zero ohms to TS1, tag 9.
- Solder the red lead to wafer 2, tag 10. With the A NET switch still dolly upward, check for zero ohms between TS1, tag 9 and V2B, pin 1. Set the mode switch to RT and check continuity between TS2, tag 9 and V2B, pin 1 is broken.
- Refit the mode switch; check the receiver for RT and C.W. operation. Note that M.C.W. position now behaves as C.W. position.

(Note... The A NET switch can bring in B.F.O. if switched dolly downward, independently of the mode switch. If this is considered undesirable, one lead to the A NET must be cut, but the switch is difficult of access).

I.F. Stages

Some receiver i.f. transformers have been modified by the services to give increased i.f. bandwidth, $100 \mathrm{k}\Omega$ resistors were wired across both primary and secondary windings, and if visible on the underside of the i.f. transformers they should be removed.

Inclusion of Additional R.F. Stage

The receiver, as it now stands, has one r.f. stage. An additional stage can be obtained by making use of V5A (originally a buffer stage in the transmitter section and which is tuned to signal frequency by one section of the four-gang variable capacitor). Proceed as follows.

- Cut out all of the transmitter power amplifier wiring and remove all components other than the P.A. TUNING capacitor; a later modification involves this item. (See Fig. 1).
- (2) Remove V5A. At point x, drill the chassis to pass a 15in. length of thin coaxial cable. Solder one end of the coaxial to the contact on AERIAL A plug (now freed by removal of wiring).
- (3) Thread the coaxial up and between the A.F. GAIN control and chassis, over the threaded bush of the waveband switch, past the B.F.O. note control, under the adjacent pre-set capacitor, and terminate on a 100pF mica dielectric capacitor to be soldered to V2B, pin 3. If uninsulated cable is used, take precautions against short circuits where necessary.
- (4) A similar coaxial lead is required between V6A, pin 5 and tag y on a 2-way strip fitted to the 4-gang capacitor (the tag-strip is located directly under the reference "C10A"). A route for the lead can be obtained through a screw-hole formerly used in supporting the P.A. tuning inductor; access to tag y is available at a grommet on the side of the 4-gang capacitor. Earth the coaxial sheath at pin Z on the inductor adjacent to V6A (see Fig. 1).
- (5) The h.t. supply to V5A was severed at the relays. Restore it by connecting a lead to T51, tag 9, pass the lead through a hole in the screen near to pin Z (see sub-para. 4) and connect it to the second tag clockwise from pin Z (looking along the inductor towards the panel). Be careful not to damage the inductor.
- (6) Refit V5A. Do not fit V6A. Check the receiver as before and note that it is now possible to overload the receiver if the R.F. GAIN is set to maximum.

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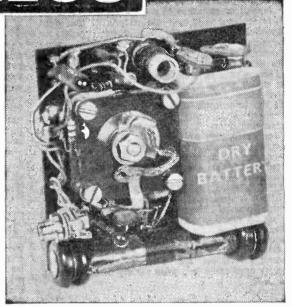
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BOOKS REVIEWED

NIFIED CIRCUIT THEORY IN AND ENGINEERING ANALYSIS.

By J. W. Head, M.A., Cantab., F.Inst.P., A.M.I.E.E., F.I.M.A. and C. G. Mayo, M.A., B.Sc., M.I.E.E.; published by Iliffe Books Ltd.

174 pages, 83 in. x 51 in. Price 42s.

THE purpose of this book is to show how the output or response of a linear system may be formulated whatever the nature of the input may be. Steady state conditions present no mathematical difficulties but decidedly more advanced techniques are required when dealing with the non-steady state.

The authors have a very easy style and, taking the reader gently by the hand, they show that the basic ideas associated with operational calculus and the impedance concept are extremely simple to grasp and, once understood, have a high

resolving power".

The early part of the book is concerned with electrical circuits having lumped elements; the latter part is more theoretical and extends the circuits which are still linear but contain

distributed elements.

UNIFIED CIRCUIT THEORY has been written by practical mathematicians in simple, straightforward language with the purpose of providing practising engineers and students with a powerful tool for evaluating linear circuit responses irrespective of the input. Although the examples are expressed mainly in terms of electrical systems the methods employed are equally applicable to a wide variety of other fields.

NON-LINEAR AND PARAMETRIC PHENOMENA IN RADIO ENGINEERING. By A. A. Kharkevich--edited by Keats A. Pullen, Jr., Eng.D., published by lliffe Books Ltd. Eng.D., published by Iliffe Books Lo 190 pages, 83 in. x 53 in. Price 35s.

INHIS book was originally published in Russia, where the author is currently Professor of Theoretical Radio Engineering at the Moscow Electrotechnical Institute of Communications, the book was subsequently translated, edited and

brought up to date in the USA. It is an extremely clear and interesting introduction to the theory of non-linear systems and its practical application to typical electronic problems. It opens with a chapter on non-linear circuits and fundamental non-linear processes, and amongst other things deals with voltage and current stabilisation, frequency multiplication, rectification, detection, and non-linear methods of amplitude modulation. The second chapter deals with the generation of oscillations, stability criteria, and various types of oscillator including those for micro-waves. The third chapter is concerned with the response of non-linear systems to external signals: rectifier operation, locking, the regenerative receiver, pulsed synchronisation and synchronisation of a relaxation oscillator.

The final chapter, which discusses circuits with variable, time-dependent, parameters, is of particular interest at the present time when variable-

parameter devices having high quality characteristics have opened up new vistas in solid state electronics.—C.R.R.

TRANSISTORS IN LOGICAL CIRCUITS. By J. Ph. Korthals Altes, published by Iliffe Books Ltd. 117 pages, 8\(^2\)in. x 5\(^1\)in. Price 16s.

ERE is another addition to the Philips paperback series (P11). It covers in a basic form the field of modern switching techniques, starting whenever possible with known relay switching techniques and introducing those using semiconductor devices. The various chapters deal with concepts of switch algebra, the binary system, transistor switching, and-or-not operation, counting switch circuits, arithmetical operations, applications and practical hints. For those becoming interested in computors or measuring and control techniques this book offers a useful introduction. -W.N.S.

PICK-UPS: THE KEY TO HI-FI. By J. Walton, published by Sir Isaac Pitman & Sons Ltd. 100 pages, 74in. x 5in. Price 10s.

MHOUGH small physically this is a most useful little book, packed with information, advice and guidance. Writing is concise, making the most of the space available. The preliminary chapters cover material to be found elsewhere to be sure (fundamentals of recording and playback, principles of pick-ups, etc.), but the second half of the book deals exclusively with practical aspects of pick-up ills and cures and outlines in a very readable and lucid manner tests, causes and cures for these ailments.

Without a doubt anyone about to invest in a new pick-up, or who has trouble with his existing one, or-indeed-anyone interested in more than a casual way with hi-fi reproduction will find the price of this book a "sound" proposition.— W.N.S.

CIRCUITS USING DIRECT CURRENT RELAYS. CIRCUITS USING DIRECT CONNECT.

(Philips Paperbacks Series). By A. H. Bruinsma; published by Iliffe Books Ltd.

86 pages, 8½in. x 5½in. Price 13s. 6d.

N modern electronics the technician looks for simple and yet reliable circuits to solve his switching and amplifying problems. The relay still plays an important role in the solution of such problems, for although new devices now exist for replacing relays new opportunities for their use have also arisen during the past decade.

This book gives an insight into a number of uncommon circuits which have already proved themselves in practice and the possibility of applying d.c. relays in commanded or programmed sequence circuits is fully explained. The circuits are dealt with in such a way that the reader may obtain a great understanding of the properties of the relay without the use of complicated mathematics,—C.R.R.

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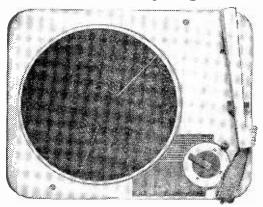
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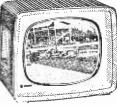
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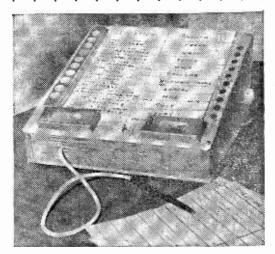
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PART TWO-WIRING

THE wiring procedure for the quiz machine will vary a little according to the type of relays used, and it is recommended that if relays different from those used by the author are resorted to, a rough wiring diagram be drawn up before any wiring is commenced. Fig. 9 shows the underside pin connections for the relays used in the prototype.

As said previously, the sockets for the relays were mounted in banks; one bank of ten, holding RLA to RLJ, and second bank of two, RLR and

Fig. 8 shows how the banks of relays are interconnected. To save time, and to speed up the soldering operation, it is quicker to cut all the lengths of jumper wires in one operation, and bare all their ends before starting to solder. The colour coded flying leads to the panel should be

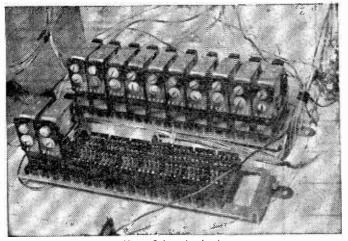
left at least 18in. long; these will be cut to length

on connecting them to the tag strips.

The wiring on the underside of the front panel is shown in Fig. 10. If colour coding is adopted, it is imperative that the correct wires go to the correct tags otherwise there may be great diffi-culties in sorting out faults, for instance if a relay sticks it can be readily found by referring to the coding and the question position (A piece of paper containing the code should be stuck in side the instrument in case servicing is necessary).

The flying leads to the answer contacts can go either direct to the contacts in a random order, or can be routed via the programme switch. For the small extra cost, it is well worth while incorporating this switch as it broadens the scope of

the instrument considerably.



View of the relay banks.

Programme Switching

The number of programmes available is limited only by the capacity of the switch (there are 3.268,800 different possible combinations), but in the prototype it was decided that three different arrangements would suffice.

The switch required will be ten pole three way for a triple programme, and Fig. 7 shows one suggested wiring system There are, of course, many possible wiring arrangements, but the one shown here is simple in that it has a symmetry by grouping consecutive questions in threes.

The switch used in the prototype was of the wafer type, as this was the most convenient way of obtaining the ten poles. Four,

three pole three way wafers were ganged on one spindle.

The wiper contacts (numbered from 1 to 10) are connected to the corresponding "Answer" positions of Fig. 4, and the output connections labelled A to J are connected to the answering contacts on the front panel.

If the wiring of Fig. 7 is strictly adhered to, the following table shows the position in the answer column of the correct answer to each question for each of the three programmes. As with the colour code, it is useful to keep a record of the combinations shown below.

The relays used in the prototype were all 50

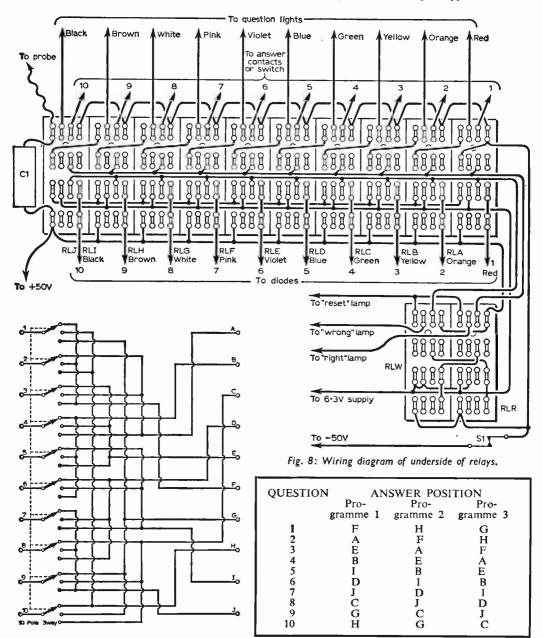


Fig. 7: Suggested wiring of programme switch.

Positions in answer columns to questions.

Question

Diodes

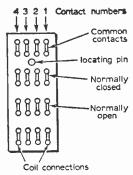


Fig. 9: The underside pin connections of relays used in the prototype.

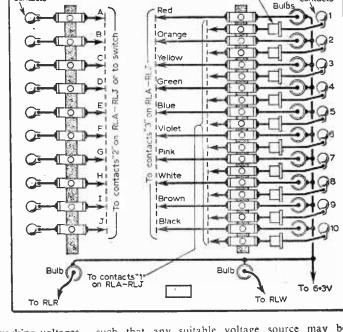


Fig. 10: The underside wiring of the front panel.

volt working, and as most of the working voltages are exposed at the contacts, it is worth bearing in mind that children may use the machine. The author is of the opinion that 50 volts can be regarded as comparatively safe, but other people's opinions may vary on this point, therefore it is worth bearing this matter in mind before using some of the high impedance relays that are available which require quite high voltages.

No details are given in this article about a suitable power supply, but the requirements are

such that any suitable voltage source may be used; good smoothing is not required, therefore a conventional R-C pi network will be sufficient for the supply to the relays, and the output from a heater transformer will be more than adequate for the bulbs. This unit can be incorporated in the same cabinet.

It should, however, be noted that if the instrument is run from a mains power supply, the supply should be isolated via a transformer for the same reasons as stated above.

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- ★ SOUND CHANNEL PROBLEMS
 TV audio troubles discussed with emphasis
 on noise and/or impulse limiters.
- ★ EFFECTS OF FAULTY RESISTORS
 Examines effects of faulty carbon, wirewound and variable resistors in TV receivers.

On Sale 24th February Price 2/-

A COMMENTARY BY HENRY

ACTICALLY RELESS

No. 19 Oh. but it Hertz!

ONE of these days, the term "cycle" will merely denote that contraption you keep folded in the boot of your inter-city car to beat the Barbara-ban on parking.

Already, leading technical journals in the United States have adopted standard European symbols. From henceforth c/s becomes Hz and kc/s is (or are) kHz. Even one of our own specialist magazines admits to keeping a watching brief on the situation.

The term "Hertz" derives from Heinrich Rudolph Hertz, who transmitted the first radio wave across a room in Frankfurt in 1888. Yes, I looked it up. And in the course of doing so was intrigued by the time-scale between discoveries and inventions. For example-it hardly seems possible that the theory of electro-magnetic waves had already been expounded (from a purely mathematical premise, admittedly) by James Clerk Max-well nearly 25 years earlier!

Hardly seems possible in these days, when every post brings news of fresh techniques, and what the Press Officer of each electronic giant insists on calling

"break-through". This telescoping of the timescale was brought home to me forcibly the other day when reading a piece about "mechanised h.f. systems". Briefly, the argument was for machine tele-



Every post brings news of fresh techniques.

graphy, using low-power h.f. networks with programmed instructions and remote control, taking away much of the operators' chores of locating and locking on to a weak and distant signal.

It seemed strange that there was no reference to the "frequency synthesiser". After all this now-popular plaything of the Defence Departments of several countries is the answer to continuous tuning and signal-locking. By transmitting a great number of channels simultaneously, and locking the receiver to the desired one by a process of division and phaselocking, using reference oscillators and a voltage-controlled oscillator energised by the incoming signal, completely private and accurate tuning is effected. So why did the writers of the other article not mention it?

Looking up the dates provided the clue—the first article was published about a year ago. Not that the principle of frequencysynthesis is all that new. Like Mr. Maxwell's ideas, it gave birth to erudite argument some twenty years earlier. In fact, there was a description of the technique in IEE Proceedings of

But when one remembers the cumbersome man-packs of those days and considers that the system requires some thousands of transmitters instead of just one, it can be seen that the theory had to await the development of micro-miniaturisation and the solid-state device to become practice.

The time-lag seemed even more pronounced when this innocent explorer stumbled upon the subject of fibre-optics. Here, it seemed, was something well worth further research. Bending light around corners has long been a kind of alchemist's dream to the experimenter. Now, by directing the light to the end of a glass fibre, coated with a slightly more opaque glass to



A handy toy for finding the gas-meter.

give the required refractive characteristics, the light can be obtained at the other end of the fibre, practically undiminished. The ray simply goes along the fibre, bouncing along the walls

gaily, undeterred by bends.

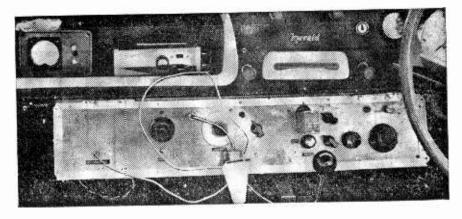
A handy toy, you'd say, for finding the gas-meter at the back of the boot cupboard. But there's more to it than that, for the fibres can be spun so thin that 150,000 of them would not exceed the diameter of a match, and their ends can be scanned by the light beam so that the emitted result follows the same pattern. You see where we are leading? Yes, the flat cathode ray tube, picture on the wall television, and all that. Exciting breakthrough, you would think.

So did Henry, till he discovered that the original patent was taken out by-John Logie Baird! He would have had to wait 30 years to see the progress in glass tube drawing perfected to the state needed to make use of his ideas

But the time lag can hardly have been so well demonstrated as in the case of Patent 997,670, Peter Gilhead, UK. A transistor oscillator and amplifier with output electrodes sensitive to low resistance paths, for locating pressure-sensitive points on the

The pay-off line is that this is. for use in the healing process of Acupuncture. Practised by the Chinese 3,000 years ago.

TRANSISTOR MOBILE TX



Ten watts on Top Band

F. C. JUDD, G2BCX

NOR the past six months or so the writer has been carrying out research and development in high-efficiency transistorised mobile (or fixed high-efficiency transistorised mobile (or fixed station) transmitters the result of which is the circuit shown in Fig. 1. It should be carefully noted that the r.f. amplifier shown in Fig. 1 employs a Texas 2N1907 power transistor and that no other should be used. The p.a. circuit operates at an efficiency approaching 100%, which is impossible to achieve with any conventional class C valve amplifier. In other words, for 10W d.c. power input as rated by the GPO licence for 160m operation the 2N1907 p.a. stage will deliver very nearly 10W of r.f. power to the aerial. A class C valve amplifier would deliver only 6 to 7W of r.f. power for a d.c. input of 10W. Mobile operators will at once realise the value of this and the fact that the transistor transmitter of Fig. 1 will modulate to 100% as any normal transmitter. The transmitter consumes no power from the car battery unless one is actually transmitting and when fully operational consumes less current than the heater circuits alone of any valve transmitter of comparable power. The total drain from a 12V car battery, including the transistor modulator, is only $1\frac{1}{2}A$.

High Efficiency P.A.

Firstly then how is the high efficiency of the p.a. stage maintained? The answer is simple, for the transistor is pulsed or switched at the operating frequency (1.8 to 2Mc/s) but the duty cycle—the time during which the p.a. transistor conducts—is very short. The duty cycle is only a small portion of the negative part of the drive signal. A current meter connected in the 12V h.t. rail will therefore only read the average d.c. current consumed by the p.a. stage.

It should be noted that a v.f.o.-controlled version of this transmitter has been designed and used with equal success. The only reason for presenting the crystal-controlled version is the simplicity of the circuit. The v.f.o.-controlled

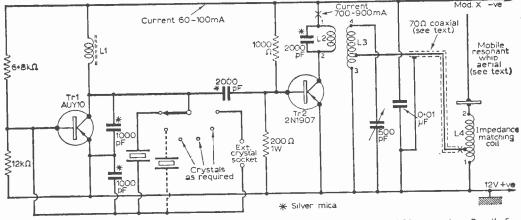


Fig. 1: Circuit diagram of the transmitter. L1 is a Vinkor pot core LA2105 with 6 turns of 20s.w.g. wire. Details for L2, 3, 4—see Figs. 3 and 4.

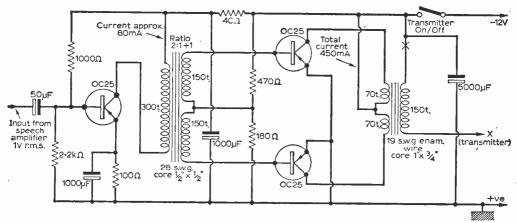


Fig. 2: Circuit of the modulator unit.

transmitter required a rather more elaborate drive stage and transistor v.f.o.s are not the most stable devices to use.

Points to Note

The construction of the transmitter is not critical, i.e. no particular screening is required (a photograph of the completed transmitter mounted in the writer's car is shown in the heading. What is important is that the following are strictly adhered to:

- Mica capacitors of good quality must be used where shown.
- Paper capacitors must not be used in the oscillator or p.a. stage.
- 3. The tuning coils L1, L2 and L3 must be constructed exactly as described.
- The impedance matching unit L4 must be used in conjunction with the transmitter and the aerial if the whip aerial as shown is used.
- The p.a. stage will not drive from a valve or other type v.f.o. Instant destruction of the p.a. transistor could result by attempting to do this.
- 6. On no account should the p.a. transistor collector current be allowed to exceed 1A.

The circuit has been carefully designed and thoroughly tested and modifications to component values could result in destruction of either one of the transistors or at least poor operation of the circuit.

Modulation

A suitable modulator is shown in Fig. 2 and may be operated with any small transistor microphone preamplifier such as those made by Walgain or a home-constructed type with an output of about IV r.m.s. It is advisable to operate the speech preamplifier from its own dry battery.

Details of the modulator transformer are given in Fig. 2 but some idea of its working power can be ascertained by connecting a dummy load across the secondary. The dummy load may consist of

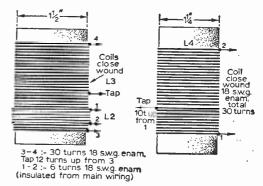


Fig. 3 (left): Details of L2/3. Fig. 4 (right): Details of L4.

a 6.3V 0.3A flashlight bulb, which should light to full brilliance on modulation peaks. It would, of course, be more ethical to check with an audio generator and oscilloscope plus a dummy load of about 1Ω .

Tuning and Impedance Matching

The crystal oscillator collector coil consists of six turns of 20 s.w.g. enamelled wire wound on the bobbin of a Vinkor pot. core type LA2105. The coil resonates to the approximate centre of the 1.8 to 2Mc/s amateur band. (Note that none of the coils are suitable for other bands and details for other band operation cannot be given.) The p.a. coils L2 and L3 are wound on a paxolin or other type former as shown in Fig. 3. The impedance matching unit L4 is most important when using the whip antenna shown in Fig. 5. The coupling line between the p.a. tuning coil L3 and the impedance matching unit must be not less than 6ft of 70Ω coaxial line if using this whip. may be longer, up to 12ft if necessary, which is more than sufficient to cover the length of a car from the transmitter inside to an aerial mounted at the back,

Construction

No constructional details have been given as most mobile operators will wish to make up the transmitter to fit into some convenient part of the car, usually under the dashboard. The photograph shows the transmitter in a case which was tailor made of dural, aluminium or mild steel. The diagram of Fig. 6 may serve as a guide to constructors.

An important item is the heat sinks for the various transistors. The heat sinks for Tr1 and Tr2 of Fig. 1 must be not less than 6in. x 5in. and made of dural, aluminium or mild steel. The transistors may be insulated with the usual mica washer arrangement but if mounted directly on to the heat sink then the heat sinks themselves must be insulated from the chassis. Much the same comments apply to the heat sinks for the driver and modulator OC25 transistors.

Suitable Mobile Aerial

Details of the aerial actually used with the high-efficiency transistor transmitter are given in Fig. 5. The major part of the coil is double wound to reduce coil r.f. resistance losses, but remember, slight adjustment of the lower part of the coil and/or the aerial section above the coil may be required, i.e. a few turns on or a few turns off. Such adjustment should be carried out with a 6V 0.5A lamp in a two-turn link coupled around the lower part of the coil. The lamp should light to almost full brilliance when the transmitter is developing full power and the aerial is correctly adjusted to resonance at the centre frequency of the band, namely 1,900kc/s. The tuning circuit L3 will automatically tune the aerial to other frequencies within the band. Current through the 70Ω coaxial line should be 0.3 to 0.4A when the transmitter and aerial are properly tuned. A

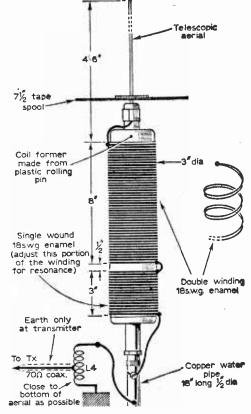


Fig. 5: Details of 160m aerial.

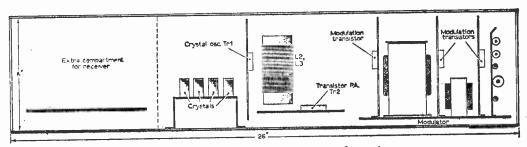


Fig. 6: Layout of prototype, with compartment for receiver.

means of monitoring the current to the p.a. is desirable and, of course, very useful for the initial tune up. The circuit diagrams indicate typical readings and indeed an ammeter, say 0-1A, connected at point X in Fig. 1 would be very useful in ensuring that the current here did not rise above, say, 900mA. (Note: Under no circumstances should this current exceed 1A.) At present 2N1907s are expensive and attempting to squeeze out the last watt of r.f. could easily prove a very costly process.

The modulator and driver transformers were

made from a couple of audio transformers which were to hand. The core sizes and winding details are given in Fig. 2.

The writer has been using both a v.f.o. and the crystal-controlled version (as in Fig. 1) for some time and ranges of over 200 miles have been obtained using the transmitter and aerial as

described.

The transmitter has been used with equal success for "fixed" station as well as portable operation and is probably the most efficient yet most economic mobile transmitter design available.

F. L.THURSTON

RECEIVER was required by the lady of the house for use in the kitchen. The most popular stations, in this particular case, were Caroline and Luxembourg, but it had been found, however, that these two stations were often difficult to locate on the more conventional type of receiver. The solution to the problem was to make these stations switch-tuned.

It was eventually decided to make up a receiver that was switch tuned to the following four stations: Home, Light, Caroline, and Luxembourg. These last two stations are often subject to fade and adjacent channel interference, as well as being very weak in many areas. When designing the receiver, therefore, a superhet was indicated.

One of the major disadvantages of the conventional superhet is that the oscillator section is subject to a fair amount of drift, and the circuit is thus generally not suitable for use as a switch tuned receiver, unless exceptional care is taken to obtain the required stability. The t.r.f., on the other hand, is not subject to drift of this kind

and so is ideal for use as a switch tuned receiver of fairly powerful stations, such as Home and Light, but it does not have the required selectivity or a.g.c. that is essential for good results on the weaker stations.

When designing the receiver that forms the basis of this article, a superhet was deemed essential, but with the following five outstanding characteristics: Very high gain, low noise, good selectivity, good a.g.c., and excellent stability, the last of these characteristics being the most important.

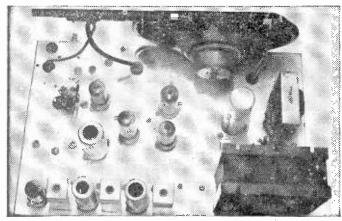
CIRCUIT DETAILS

In the final circuit, all five of these characteristics have been obtained. In view of these characteristics, the resulting circuit is ideal for adaptation, by substituting a variable tuning gang and range selection facilities in place of the switch tuning used in the prototype,

The full circuit diagram of the receiver in its

final form is shown in Fig. 1. The r.f. signal is picked up by the ferrite rod aerial which has provision for the coupling of an external aerial, if required. The ferrite aerial is tuned by one of the trimmer capacitors, C21—C24, and the selected signal is fed to the grid of V1, the preselector stage. A radio frequency transformer is used as the anode load of V1 with its secondary winding tuned by one of the trimmers, C25—C27, and the tuned signal is fed to the grid of V2, the mixer.

An EF91 pentode is used as the mixer, with its screen grid held at a fixed potential by the divided chain R3—R4, and decoupled by C3. The local oscillator voltage is injected into the mixer cathode via C18. The



Showing the general layout of above-chassis components.

mixer generates exceptionally low noise.

The local oscillator uses one half of a doubletriode (V3a) in a conventional circuit. The output of the local oscillator is fed to the grid of a cathode follower (V3b) via C15. With its high input and low output impedance the cathode follower acts as a buffer between the mixer and oscillator, and eliminates any "pulling" of the oscillator frequency which might otherwise occur via the mixer. The h.t. to the oscillator and cathode follower is stabilised by V4, the regulator valve. Exceptional oscillator stability is obtained due to this stabilising and buffering. A small trimmer capacitor, C32, is mounted on the front of the receiver, and was fitted so that any drift that did occur in the oscillator could be counteracted. Drift has proved to be so low in practice, however, that, although at the time of writing the receiver has been in use for over six months, operating under adverse temperature conditions, the trimmer has not so far needed adjustment.

It should be noted that the range switching

It should be noted that the range switching is so arranged that, on any given tuning coil, certain of the trimmer capacitors are switched in parallel, so that their capacitances are additive for station changing. When aligning the receiver, then, these trimmers must be adjusted in the correct

sequence,

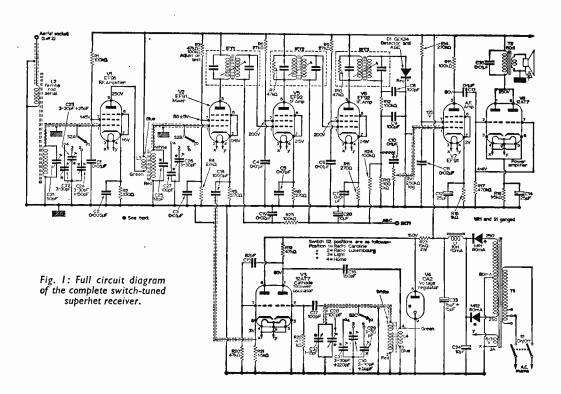
The 465kc/s output of the mixer is selected by i.f.t.1, and passed on to the i.f. strip. Two stages of i.f. amplification follow, via V5 and V6 (EF92 var-mu pentodes), which have a.g.c. applied. Each of these valves has an i.f. transformer as its anode load (i.f.t.2 and i.f.t.), respectively), and in each case the transformer primary winding is damped by a 47kΩ resiston, the gain of each transformer, and results in vastly, improved circuit stability (no screening is used in the prototype receiver). As three i.f.'s are used in all, no adverse loss of selectivity results, and μ is in fact necessary to de-tune the i.f.'s if approximately acceptable quality of telephony is to be received. The amplified i.f. signal is detected by diods.

The amplified i.f. signal is detected by diod, D1, and the r.f. component is filtered out by the network C8, R12, C9, and R13, and the a.f. component is passed to the audio amplifier stag, via C10 and RV1. The a.g.c. voltage is obtained via the above filter network plus an additional time constant network, comprising R24 and C20. In this circuit, the a.g.c. line has an impedance of about 200kΩ, which is less than one fifth of the value obtained in most circuits; this comparatively low impedance results in far greater stability than is obtained in the conventional home-built radio. The a.g.c. line is wired to an output socket to facilitate the lining up of the tuned circuits if a multimeter is available.

The a.f. section comprises an EF91 amplifier and a double-triode, with the two sections wired in parallel, as the power output stage. About half a watt of a.f. is available, which is considered to

be adequate for normal domestic use.

continued overleaf



THE CHASSIS

The switch-tuned receiver uses a standard 12in. x 8in. x 2½in. chassis, the main drilling and cutting dimensions of which are shown in Fig. 2. The chassis has corner brackets fitted, as shown in the photographs, and these are employed as securing points when the chassis is mounted in the cabinet. The speaker is bolted directly to the chassis, and a cut-out must be provided, as shown.

As the wiring is fairly complex, it is considered that the best approach to the construction is to build the receiver in a number of distinct stages. As well as having the advantage of simplifying construction, this procedure also has the advantage that the set can be built as a "progressive", in which valuable experience in

superhet practice can be obtained. The oscillator and mixer sections can be built in a number of versions, to show experimentally the advantages and disadvantages of these types.

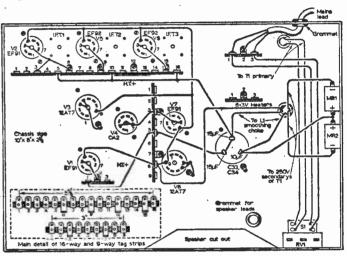
CONSTRUCTION: STAGE I

Cut and drill the chassis as shown in Fig. 2. Bolt the mains transformer in place (T1), with the mains winding facing to the rear of the chassis. Bolt the smoothing choke, L1, in place. Bolt the loud speaker in place in the cut-out provided at the front of the chassis. Drill three holes, approximately \(\frac{3}{2}\)in. diameter, for grommets, one to the left of the speaker, and one in front and

the other behind the mains transformer, as shown in the photographs and diagrams.

Secure the large triple value capacitor, C33—C34, in place. The particular type and order number of this component is shown in the components list; a near value to this may be fitted, however, if difficulty is found in obtaining the recommended type.

Fit the eight valveholders, taking care to note the correct orientation, as shown in Fig. 3. Also note that V3, V5, and V6 valveholders must be provided with screens. Fit variable resistor RV1, with its built-in 2 pole, 2 way mains switch, in place on the front left of the chassis. Secure the three 3-way tag strips in the positions shown. Fit the 9-way and 16-way tag strips EXACTLY as shown in the diagram (Fig. 3), this is most important. Both of these tag strips are cut from



AGC STTE Administra

Fig. 3 (above): Constructional details for Stage 1.

Fig. 2 (left): Drilling and cutting details for the chassis.

standard types, and the position of the tags is considered to be so important in the construction of the receiver that sketches of the two types, showing positions of insulated and earthed tags, as well as major dimensions, have been included in Fig. 3.

In the prototype set two 250V, 80mA half wave rectifiers, of the old "finned" type were used, mounted to the left-hand side of the chassis. Any other type of rectifier may be used, however, provided it is suitably rated. A full wave type may be used in place of the two half-wave ones. The rectifiers should, however,

COMPONENTS LIST Resistors: Valves: RI 100kΩ R2 330Ω R3 47kΩ to 100kΩ RI4 270k Ω RI5 100k Ω VI EF91, 6AM6 V6 EF92 V2 EF91, 6AM6 V7 EF91, 6AM6 RI6 IkΩ V8 12AT7, ECC81 V3 12AT7, ECC81 R17 470kΩ V4 OA2 (Adjust on Test) DI GEX 34 or similar R4 22kΩ R18 1.5kΩ V5 EF92 R5 270Ω R6 27kΩ R7 47kΩ R19 47kΩ R20 $47k\Omega$ R21 $1.5k\Omega$ Rectifiers: MRI, MR2 250 volt, 80mA (see text) R8 270Ω R22 47kΩ R9 $27k\Omega$ R23 15kΩ, 2W Transformers: R24 100kΩ R25 100kΩ RVI 250kΩ log RIO $47k\Omega$ TI Mains transformer RII 270Ω 250-0-250 v., 80mA 6.3 volt, 3A R12 100kΩ T2 Output transformer RI3 100kΩ + 2p. 2w switch (SI) Ratio 60: I for 3 ohm speaker. See text All carbon, ½ Watt, 10%, Sockets, etc.: unless stated otherwise 2 off B7G valve-holders, with screens (V5, V6) Capacitors: CII $0.02\mu\text{F}$ 250 volt CI2 $25\mu\text{F}$, 25 volt Ċ1 0·01μF 350 volt 4 off B7G valve-holders, C2 0.005µF 350 volt without screens (VI, V2, V4, V7) C3 0.01 µF 350 volt C4 0.01 µF 350 volt C5 0.01 µF 350 volt C6 0.01 µF 350 volt C7 0.01 F 350 volt C13 0·1 µF, 350 volt C14 25µF, 25 volt C15 82 pF I off B9A, with screen (V3) I off B9A, without screen (V8) I off Radiospares 2-way aerial socket C16 150pF (see text) C7 0.01 µF 350 volt C17 100pF 100pF CI8 1000pF CI9 0·02μF C8 Switches: Č9 SI see RVI S2 3 pole, 4 way. See text 100pF C10 0·1 μ F, 150 volt C20 10 μ F, 25 volt C21 50pF postage stamp trimmer C22 3-30pF C23 3-30pF + 25pF C24 3-30pF + 150pF Coils: LI 10H, 80mA smoothing choke L2 Ferrite rod aerial. See text C25 18pF Mica L3 Weymouth HH3 C26 3-30pF C27 100pF C28 100pF postage S C29 3-30pF see L4 Weymouth HO4 IFTI, IFT2, IFT3 "MAXI-Q", type IFTI 1/465 text C28 100p; C29 3-30pF C30 3-30pF + 56pF C31 3-30pF + 220pF C32 1-15pF (see text) Front Panel Trimmer C33 15 + 15µF Triple type Electrolytic C10 NTS, type K553 Misc. Components: Chassis, $12 \times 8 \times 2\frac{1}{2}$. Aluminium, with corner brackets I off Ferrite rod, 10" x 3". 3 off 3-way tag strips I off 9-way tag strip

be mounted in roughly the position shown.

Mount the three i.f. transformers in place. A miniature type MUST be used, and the "MAXI Q" type IFT11/465 is recommended. Mounting instructions are included in the instructions provided with the i.f.t's.

** 3-30pF = Philips 'beehive' type trimmers

Finally, wire-up the mains connection, power supply and l.t. to all valves (except V4), as shown in Fig. 3. When this has been done, check over the wiring and switch on. If a multimeter is available, check that the h.t. is available; it should be over 300 volts. Plug-in all valves, except V4, and check that their heaters are working correctly. This concludes Stage 1.

STAGE 2. THE A.F. SECTION

Secure the output transformer, T2, in place

below chassis to the left-front, as shown. In the prototype, a 60:1 ratio was used for the 3Ω speaker, the precise ratio is not critical, however, and almost any output transformer of roughly this ratio may be used.

Wire, screened wire, solder tags, grommets, etc

See text

I off 16-way tag strip

I off tag board

Wire-up the circuit as shown in Fig. 4 using screened leads between the grid of V7 and the volume control, and between the volume control and C10. The loose end of C10 may be temporarily secured to a spare tag.

Check the wiring and switch on, after first making sure that the speaker is connected to T2 secondary. With the volume control turned full up, touch a finger to the loose end of C10; a strong 50c/s hum should be heard. If a multi-

-continued on page 993

U.H.F. and V.H.F. Designs

DESIGNS frequently appear in PRACTICAL WIRELESS for the construction of equipment suitable for the h.f. bands, i.e. 160m, 80m, 40m and 20m.

Why are there no articles on equipment for the v.h.f. and u.h.f. bands? Surely these represent more of a challenge. From memory I can recall but one design for receiving transmissions above 50Mc/s (other than f.m. bro..dcast sets) and that was for building a simple t.r.f. set.

Several times one read: of amateurs holding a G3 licence condemning the G8 licence as providing "an easy way out", but is it such an easy way out?, but is it such an easy way out? Perhaps that is why no designs for v.h.f. and u.h.f. equipment appear—it is below the fully licensed ham who has passed his Morse test to use these bands—leave them for the rabble who are too lazy to pass the Morse test and provide us with designs or information for them.

S. Peat.

Frodsham, Cheshire.

Can Anyone Help Please?

SOME time ago in PRACTICAL WIRELESS a reverberation unit consisting of springs, was published.

My huge collection of PRACTICAL WIRELESS surprisingly, does not contain this issue. Would any kind readers please lend me this issue? It would be highly appreciated.
W. F. Wright.

9 Priory Road Caravan Site, Ruskington, Sleaford, Lincolnshire.

* * *

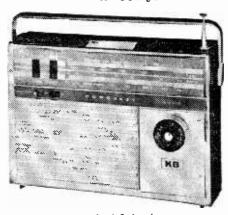
On behalf of Bury and Rossendale Radio Society, I should like to appeal to your readers for any surplus literature relating to amateur radio. We would welcome back numbers of P.W., and handbooks relating to both commercial and ex-govt. equipment. Postage costs etc, will be refunded.

A. Cooper.

58 Spring Street, Bury, Lancashire.

NEWS AND.

A "CONQUEST" FOR KB



A development of the KR 016, the KR 026 "Conquest" transistor radio, is the newest model from KB.

The "Conquest" has long, medium, short, and v.h.f. wave-bands.

Attractively styled in a shock resistant black plastic cabinet, with chrome speaker grille and trim, the "Conquest" has nine transistors and seven diodes.

The speaker is 5in. x 3in. and there is a ten-section telescopic

aerial for short and v.h.f. bands.

The illuminated scale and wave-band selection are push-button operated and there are thumb-edge controls for volume and tone.

Other features include separate on/off switch, concentric tuner and fine tuner, sockets for car and external v.h.f. aerial and ear-piece.

Price: 23 guineas (including p.t.).

"LIFELINE" FOR SHERPA HOSPITAL

The world's most remote hospital, 13,000 ft. up the slopes of Everest, is to have two powerful radiotelephones to provide a "lifeline" with civilization.

Sir Edmund Hillary will lead a New Zealand expedition into Nepal this year to begin construction of a six-bed hospital for 4,000 Sherpas in the Khumbu area of the Himalayas. The expedition will carry with it two compact single-sideband transmitter-receivers, manufactured by Pye of Cambridge, which will give hospital staff a vital link with Katmandu, 160 miles away. The sets, which are Pye SSB 125's, have been presented to Sir Edmund by Mr. G. A. Wooller, managing-director of Pye (New Zealand), Limited.

COIL FORMERS FROM CAMBION

Cambion Electronic Products Ltd., Castleton, Nr. Sheffield, announce the new printed circuit solid pin flangeless coil formers 3618 and 3619. Well suited for use with "pi-"wound coils, these two new coil formers from Cambion incorporate all standard Cambion features including a moulded diallyl phthalate base and a polypropylene liner. Both are engineered with unique flangeless construction to facilitate greater use of the winding space area.

Engineered for vertical mounting on ·200in. centres in printed circuit applications, these new coil formers can be used wherever an r.f. coil is required. The 3618 coil former measures ·325in. above the board, while the 3619 former measures ·480in. Both formers have a ·375in. square base with solid brass pins (hot solder dip) integrally moulded. Cambion coil formers 3618 and 3619 come with standard powdered irons in yellow, red, green, white, purple and blue. These cover the frequency ranges ·2 to 1·5 Mc/s through to 40·0 to 300 Mc/s.

.. COMMENT

SALON INTERNATIONAL DES COMPOSANTS **ELECTRONIOUE**

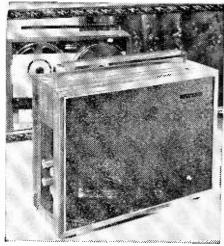
English Electric Valve Company are exhibiting on Stand 160 Allee 2 at the Paris Components Exhibition, where the display will show a selection from the very wide range of specialised electronic valves and tubes made in England at either the Chelmsford or Lincoln production plants.

Special prominence is being given to the new generation of High Power Klystrons, with output powers ranging up to 40kW and utilising water vapour cooling with the collector uppermost. These tubes have been developed for high efficiency operation in u.h.f. television transmitters or translators and have a perveance

figure of 2.

Another large display will feature the range of X and S-Band TR and TB Cells and Microwave switching devices. These have been developed to meet the needs for reliable and inexpensive units in microwave duplexers. The range includes types developed for marine, airborne and land based equipments.

HIGH QUALITY TAPE RECORDER



the newlyformed company of Van Der Molen, comes the VR.4 three-speed, four-track tape recorder. It has Italian motors specially designed for vertical operation, and instead of incorporating a mains transformer, an overwind on the motors provides the

Wow and flutter is not greater than 0.35% at $l_{\frac{7}{8}}$ i.p.s., 0.25% at $3\frac{3}{4}$ i.p.s. and 0.15% at $7\frac{1}{2}$ i.p.s. Frequency response at $7\frac{1}{2}$ i.p.s. is 40 c/s to 15 kc/s \pm 3dB, at $3\frac{3}{4}$ i.p.s., 40 c/s to 10kc/s

 \pm 3dB and at 1 $\frac{7}{8}$ i.p.s., 60 c/s to 5 kc/s \pm 3dB. The amplifier output is 5W and the signal to noise ratio is better than 40dB. The loudspeaker is an 8in. round unit mounted in the back of the recorder. A three digit tape position indicator is featured.

The amplifier has three inputs (1) microphone 2mV at $50k\Omega$ (2) pickup or tuner 30mV at $IM\Omega$ (3) mix 200V at $IOOk\Omega$. Outputs are (1) internal amplifier or headset 2-4V r.m.s. at $10k\Omega$ (2) extension speaker-8 Ω (3) alternative head output average 2mV at 1 kc/s.

The amplifier controls are volume, mixing, treble, base and track selector and ten semiconductors are employed in the circuitry.

Record monitoring facilities are provided, by means of the internal speaker. Dimensions are $15\frac{1}{4}$ in. x $12\frac{1}{4}$ in. x $7\frac{3}{4}$ in., the weight 16 lbs. and the price 59 guineas.

The makers say that VR.4 is the first in a line of high quality products. The photograph shows the VR.4 in a vertical position facing a mirror to show the deck.

Hawaiian Guitar

HAVING built the Hawaiian guitar (June, 1965, issue), amplification did not come up to expectations when plugged into the pick-up sockets of a radio-

Here I found an ideal application for the small three-transistor amplifier which appeared in PRACTICAL WIRELESS, May, 1965.

When this amplifier was connected between the guitar preamplifier and the pick-up sockets on the radiogram the volume resulting was more than ample.

It was a simple matter to arrange the input, output or both jack plugs on the transistor amplifier so that current was being drawn only when both plugs were in position.

A. Cunningham.

Liverpool 5.

The Cost of Radin

Amateur radio today is a very Indeed two complex hobby. amateurs in the same town may not know that the other is on the air.

Most emateurs, if they use ready-made gear, are not pleased with it and they will try and improve and make it just that bit better. Amateur radio is much like yesteryear, only today it is much more expensive.

F. Rose, G2DRT.

High Wycombe. Bucks.

Sir, I would be grateful if any reader could sell or loan me . . .

...any part for the "Soundmirror" tape recorder produced by Thermionic Products Ltd. If anyone can help, could they please write to me. All letters will be answered.—John Wills, St. Helier, Bovey Tapens South Dayon Tracey, South Devon.

... circuit diagram of 3 or 4 transistors to manufacture a transistor set to receive 2 or 3 broadcasting stations from a distance of about 200 miles with an output of 50mW minimum on loudspeaker, with a short aerial and no earth connection. I shall send Indian Gifts.—Pramod Prakash Pyar, c/o Dr. Bachna Ram Goel, near Jain Mandir, Dhuri, Dt. Sangrur, Punjab, India.

a.m.fi.m. receiver.—T. F. Jones, Flat 2, Block 3, Wychbury Court, Highfields Estate, Halesowen, Birmingham.

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* DISTORTION

* MAXIMUM POWER OUTPUT

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21.5 Watts

THE article to be described was built to fulfil a dual purpose. Namely, to provide high-fidelity reproduction from records, microphone or guitar, etc., at the lowest reasonable cost. As the two most expensive single items in a high quality

amplifier are the mains and output transformers, attention was given primarily to the design of the output stage. After studying many valve specifications the author formed the opinion that a pair of 6L6's functioning with an 8,0000 load in

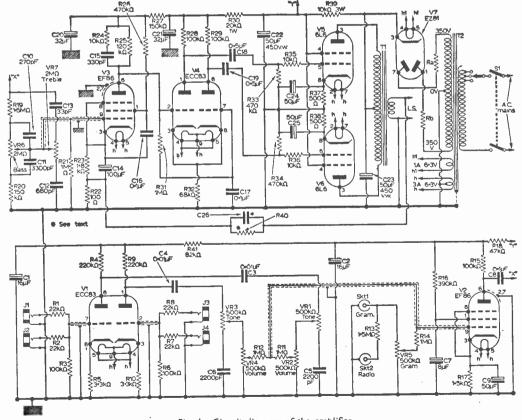
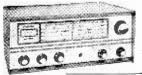


Fig. 1: Circuit diagram of the amplifier.



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20mA	22/6	50V. DC		22/6
50mA	22/6	100V. DC		22/6
100mA	22/6	150V. DC		22/6
150mA	22/6	300V. DC		22/6
200mA	22/6	500V. DC		22/6
300mA	22/6	750V. DC		22/6
500mA	22/6	15V. AC		22/6
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	7/2	EZ40	5/6	PY80	6/-	U25	10/3	30C17	11/6
EBC41		EZ41	5/6	PY81	71-	U26	10/6	30C18	10/-
EBC81	6/6	EZ80	5/6	PY82	5/6	U191	9/9	30F5	10/-
EBF80	7/- 7/-	EZS1	5/6	PY83	9/6	U 193	7/-	30FL1	10/8
EBF89		EZ90	5/-	PY88	7/-	U251	11/8	30L15	13/8
ECC81	7/4	GZ32	11/-	PY800	7/-	U281	13/9	30L17	11/6
ECC82	7/4	GZ34	11/-	PY801	7/-	U282	13/9		
EOC88	7/4	HBC90	6/4	UABC80	7/-	U301	13/9	30P12	9/6
BCC84	7/8	PABC80	7/6	UBC41	7/-	U801	19/-	30P4	12/-
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Class AB₁, push-pull, would give the desired performance. For a total current consumption of 93mA with a h.t. of 360V, an undistorted output of 15W is obtainable while, assuming that a fairly efficient output transformer is used, an output of over 20W can be expected. The output transformer used was an obscure make but gave surprisingly good quality. However, various output transformers are available, from less than thirty shillings to more than four pounds, and the reader is left to decide to borderline between quality and economy.

It will be noticed that there are four tone controls. Two provide tone control over the whole power amplifier, giving more than ample compensation. To keep the gram or radio response as set, these controls must not of course, be interfered with. Thus, simple treble cut controls (VR1, VR3) were provided after the two channels. These channels each have jack inputs (J1—J4) with sensitivities of around 2mV. The gram input (Sk11) thas a sensitivity of approx. 50mV and the radio (Sk12) a sensitivity of approx. 300mV. The rest of the amplifier is of conventional design and will be described below.

The Main Amplifier

The tone controls in the main amplifier provide a lift and cut of +10dB and -10dB at 10kc/s (VR7) and lift and cut of + 11dB to -5dB at 20c/s (VR6). From the sliders of these controls the signal is fed to the EF86 (V3). This stage provides a gain of about 150 times. Overall negative feedback is also introduced in this stage. The r.c. network in the anode circuit comprising R24, C15, reduces any tendency towards high-frequency instability. High-stability resistors are used to reduce noise. Direct coupling is employed between the anode of V3, and the phase-splitter, V4.

A word of advice here. The difference between the anode voltage of V3 and the cathode voltage of V4, provides bias for the phase splitter. It is important that this bias is correct, i.e. the grids of V4 must be at a potential 2.5V less positive than that of the cathode with respect to chassis. If the bias is too low, grid current will flow on peak signals causing distortion. If it is too high, distortion will be caused because the phase splitter will operate on a non-linear part of its characteristic. The phase splitter is the commonly used cathode coupled type.

The Output Stage and Power Supply

The output stage being relatively simple, there is little left to say except that separate cathode resistors are used to compensate for unequal d.c. in the two output valves. It is an interesting point to note that the same configuration of output stage employing a 3·8kΩ load will produce a maximum output of 40W. However, this power was not needed and the cost incurred by the larger output transformer would ruin the whole reason for using 6L6's, i.e. economy. The power supply utilises a transformer with a secondary rating of 350—0—350V at 100mA. There are many transformers of this type on the market, most under thirty shillings in cost, The rectifier used was an EZ81.

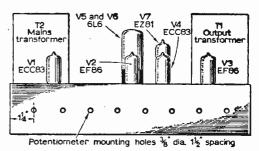


Fig. 2: Front view showing position of components.

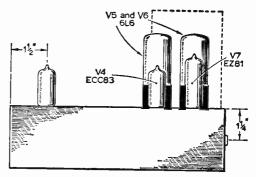


Fig. 3: Side view of chassis.

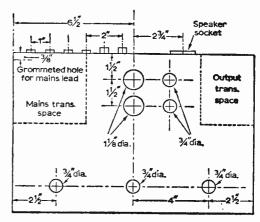


Fig. 4: Top view of the chassis.

There are two resistors shown in the circuit diagram, namely RA and RB. These should be used to bring the resistance of each half of the h.t. secondary winding, to at least 190Ω per section. There must be two heater supplies one of 6.3V 3A and one of 6.3V 1.0A.

Construction

The unit was constructed upon a chassis of the measurements 13 x 9 x 2½in. A matching base plate was constructed to fit. Sketches of the

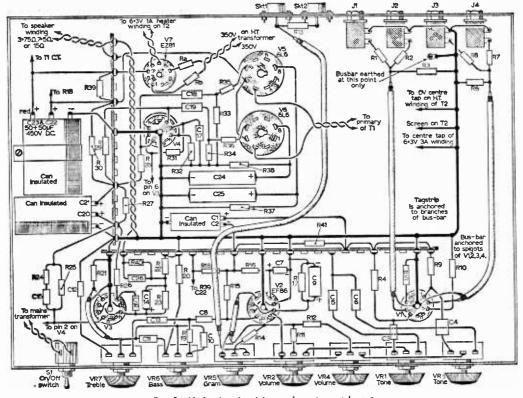


Fig. 5: Underchassis wiring and component-layout.

author's amplifier are shown to give the reader some idea of construction. The layout is not critical but attention should be given to the following details:—

- (i) screening of signal leads either more than one inch long or near to other signal leads.
- (ii) leads, especially those of grid circuits and tone controls, should be as short as possible.

Table I

	hecks with Ω/V meter
Point	Reading
VI Ist Anode VI 2nd Anode V2 Anode C2I C22 C23 V4 each Anode V4 Cathode V4 Grid VI Anode V2 Screen	60V ± 15% 60V ± 15% 90V ± 15% 220V ± 15% 280V ± 15% 380V ± 15% 200V ± 15% 61.5V ± 15% 61V 61V See text

(iii) heaters should be placed as shown.

The author purchased a piece of perspex for the front panel for about 1s. 6d., and this imparted a very professional finish. Jack sockets and coaxial sockets were mounted on the rear. The author used the type of sockets that fitted flush and did not protrude. This was merely for reason of compactness. The mains transformer used had the voltage adjuster fixed in the shrouding but as others may not, space was left in the sketch for a voltage adjustment panel. The speaker output was a normal two-pin socket, to take split pin wander plugs. Figs. 2, 3 and 4 front, side and top views show the layout of main components and drilling dimensions. Fig. 5 shows the basic position of components on the underside of the chassis. The list of voltage readings are guides to the reader when testing the amplifier. When construction is finished, testing should take place.

Testing

The unit is inverted and switched on with a voltmeter connected across C23. After a few seconds the needle should swing to approximately 380V. The reading should not be less than 360V. If an abnormally low reading is obtained, the anode and screen grid currents of the output valves

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RECORDING TAPE—Reduced Prices

Famous American Columbia (CBS) Premier Quality Tape at REDUCED PRICES. A genuine recommended Quality Tape—TRY IT. Brand new, boxed and fully guaranteed. Fitted with leader and stop foils.

4/9., 3in. D.P. 30 1 6/6. Plastic Tape Reels Plastic Spool Containers .. 3in. 1/3; 5in. 2/-; 5fin., 2/-; 7in., 2/3 .. 5in., 1/9; 5fin., 2/-; 7in., 2/8

Alumin, Chassis, 18g, Plain Undrilled, folded 4 sides, 2° deep, 6° x 4°, 4/6; 8° x 6°, 5/8; 10° x 7°, 6/9; 12° x 8°, 7/6; 12° x 8°, 8/-, etc.
Alumin, Sheet, 18g, 6° x 6°, 1/-; 6° x 9°, 1/6; 6° x 12°, 12/-; 12° x 12°, 4/6, etc.

 Jack Plugs
 Standard
 24" Igranic

 Type, 2/6.
 Sereened Ditto, 3/3.

 Miniature ser.
 14", 2/3.
 8ub min, 1/3.

 Soldering Irons.
 Mains 206/220V or

 230/250V.
 Solon 2.3V tuct.
 24/6.

 Spare Elements.
 5/6.
 Ets., 1/3.

 65W 29/16
 Bits., 1/3.

6 VALVE AM-FM TUNER UNIT



Condensers—Silver Mica, All values 2pF to 1,000pF, 6d, each. Ditto Ceramics 9d, Tub 450V T.C.C. c. 0.001 mFd to 0.01 and 0.1/350V, 9d, 0.02-0.1/500V, 14, 0.25 Hunts 1/6, 0.5 T.C.C. 1/9, etc., etc. Close Tol. S/Micas—10%, 5pF-500pF 8d, 600-5,000pF, 1/-, 1%, 2pF-100pF, 9d, 100pF-500pF, 1/d, 755pF, 5,000pF, 1/6, Resistors—Full Range 10 ohms-10 meg, ohms 20%, 4 and 4 W, 3d, 1, W, 5d, (Midget type modern rating) 1W, 5d, 2W, 9d, Hi-Stab. 5%, 4W, 6d, (100 ohms-1 omeg). Other values 9d, 1%, 4W, 1/6 etc., etc.

Volume Controls—5K-2 Meg. ohms. 3in. Spindles. Morganite Midget Type 14in. diam. duar. 1 year. LOG or LIN. ratios less Sw. 3/-. DP. Sw. 4/6. Twin Stereo less Sw. 7/6 100k to 2M ohms with DP Sw. 9/6.

WAVECHANGE SWITCHES, 1 p 12-way 2p. 2-way 2 p. 6-way, 3 p. 4-way, 4 p. 2-way, 4 p. 3-way, long spindle, 3/6 ea.

EXPANDED ANODISED METAL. EXPANDED ANODISED METAL, Attractive gilt finish 4in. x fin. diamond mesh 4/6 sq. ft. Multiples of fin. cut. Max. size 4ft. x 3ft. 47f6, plus carr. Do., finer pattern mesh 4/6 sq. ft., multiples of 12in, max. size 3 ft. x 2 ft., 27/6 sheet.

ENAMELLED COPPER WIRE— ½1b. reels 14g-20g, 3/-; 22g-28g, 3/8; 36g-38g. 4/9; 39g-40g, 5/-, etc.

JASON FM TUNER UNITS.
Designer-approved kit of parts.
FMT1. 5 gns. 4 valves 20/FMT2. 67.10. 5 valves 35/MERCURY 10 gns. 3 valves, 22/6.
JTV2 £13.19.6 4 valves, 22/6.
NEW JASON FM HANDBOOK 2/6.
8 br Alogment Service 7/6. TUNER 48 hr. Alignment Service, 7/6, P. & P. 2/6,

10B-ELECTROLTIICS-CAN \$1/25v. 50/12v. 1/9; 8 + 8/450v. 4/6; 50/50v. 100/125v. 2/-: 32 + 32/275v. 4/8. 8/450v. 4/350v. 2/3; 50/50/350v. 6/6; 16 + 16/450v. 5/6; 60/250/275v. 12/6; 82 + 32/450v. 6/6; 100 + 200/275v.12/6



MULLARD "3-3" & "5-10" HI-FI AMPLIFIERS 3 ohm & 15 ohm output

"3-3" Amp. 3 valve, 3 watt hi-fi quality at reasonable cost. Bass Boost quanty at reasonable cost. Sase Boost and treble controls quality sectional output transformer 40 c/s-25 kc/s + 1 dB, 100mV for 3W, less than 1 % distortion. Bronze escutcheon panel. Complete Kit only 7 gna. Carr. 7/8. Wired and tested £8,10.0.

Basic amplifier kit price Ready built 11; gns.

(COMPDO: COMPON: COMPO

CONTROL PANEL KIT. Bass. Treble and Volume controls with 4-position selector switch for radio tape and llin. x 4in. escutcheon panel. AMPLHIFIER KIT AND CONTROL PANEL KIT, \$1,1,1,96. Ditto, ready wired.

\$14.19.6.
2-Valve PRE-AMP. UNIT. Based on Mullard's famous 2-valve (2xRF86) circuit with full equalisation, with volume, bass, treble and 5-position selector switch Size 9x6x24in. Ready Built £7.19.6. Carriage 3/6.



Incorporating
4 Sp. Garrard
Auto-Slim unit and Mullard latest 3 watt

Auto-slim unit and Mullard latest 3 watt printed circuit amplifier (RCL 86 and EZ 80), vol., bass and treble controls, with 8" x 5" 10,000 line speaker.

Contemporary styled 2-tone cabinet, charcoal-grey and off-white with matching blue-relief, 81ze 17# x 16" x 8". A stylish unit capable of quality reproduction. Circuit and const. details 216 (free with kit).

COMPLETE KIT Carr. and ins. 12/6 Ready wired 30/cextra. Illuminated perspex control panel escutcheon, 7/6 extra. Four contemporary mounting legs 6in. 10/6; 9in. 11/6; 12in. 12/6 extra.

TRANSISTOR **COMPONENTS**

2/-, 12V. Wkg.

2/-, 12V. Wkg.
Condensers 150 v. working:
01 mFd., 02 mFd., 03 mFd.,
04 mFd. 96; 05 mFd., 1 mFd., 1/-;
25 mFd., 1/3; 5 mFd., 1/6, etc.
Midget Tuning Condensers.
"00" 208 pF and 176 pF, 8/6,
ditto with trimmers, 9/6. J.B.
220 pF and 105 pF conc. slow
motion 10/6. 365 pF single 7/6.
Sub. min. [1. Dilemin 100 pF,
300 pF, 500 pF, 7/- each.
"FERRITE ARRIALS. M. A. L.W.

FERRITE AERIALS, M. & L.W. car aerial coil 9/8.

Midget Vol. Control with edge control knob, 5 K/ohms, with switch 4/9; Ditto less switch 3/9. Speakers: P.M.; 2in. Pleasey 75 ohms 15/6. 24 in. Continental 8 ohms, 13/6. 7 x din. Pleasey 35 ohms, 23/6.

Ear Ping Phones—Min. Continental type 3ft. lead, jack plug and socket. High Imp., 8/-, Low Imp., 7/6.

Phono Plugs, 9d. Phono Sockets (open), 9d. Ditto (closed), I/-, Twin Phono Sockets (open), 1/3.

7 VALVE AM/FM RADIOGRAM CHASSIS New 1965 Model now available

VALVE AM/FM
Valve line.np ECCS5 ECH81 EF89,
EABCSO, EL84, EM81, EZSO.
Three Weeband and Switched Gram,
positions.
1,000-2,000 m. VHF/FM 88-95 Mc/s.
1,000-2,000 m. VHF/FM 88-95 Mc/s.
Phillips Continental Tuning Insert with
permeability tuning on FM and combined AM/FM IF transformers. 400
Kc/s. and 10.7 Mc/s. Dust core tuning
all coils. Latest circuitry metuding
all coils. Sensitivity and reproduction
of a very high standard. Chassis size
13] x 6jim. Height 7jim. Edge illuminated glass dial 11½ x 3jim.
Vertical pointer. Horizontal station names.
AC. 200/2520v. operation. Magic-eye tuning.

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Vertical pointer. Horizontal station names.

Gold on brown background.

A.C. 200/250v. operation. Magic-eye tuning. Circuit diagram now avalable.

Aligned and tested ready for use £13,18,6. Carr. & Ins. 7/6.

Comp. with Tape. 0/F socket, ext. sp kr and F/U sockets and indoor F.M.

acrial and 4 knobs—walm tor ivory to choice. \$0 F.M. Speaker only required.

Recommended Quality Speakers 10° R.A., 27/6. 134° x 8° E.M.I. Fidelity, 37/6.

12° R.A. with conc. Tweeter, 42/6, Carr. 2/6.

BONDACOUST Speaker Cabinet Acoustic Wadding (1 in. thick approx.) 18 in. wide, any length cut, 2/3 per (t., 6/- per yard. TINNED COPPER WIRE, 16-22g, 4/- 4/1b. ERSIN MULTICORE SOLDER, 60/40 4d. per yard. Cartons 6d., 1/-, 2/6 etc.

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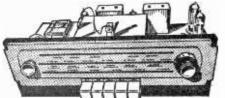


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BRAND NEW AM/FM (V.H.F.) RADIO GRAM CHASSIS AT £13.13.0 (Carriage Paid)



Chassis size 15 x'6½ x 5½h. high. New manufacture. Dial 1.½ x 4in. in 3 colours, predominantly cream. 200-250v. A.C. only. Pick-up. Ext. Speaker. Ac., E., and Dipole Socksta. Five push-buttons—OFF, L.W., M.W., F.M. and Gram. Aligned and tested. O.P. Transformer. Tone control. 1000-1900 M.; 200-550 M.; 85-98 Mc/s. Valves EZ80 rect.; ECH81, EF98, EABCOS. EL94, ECOSS, 5-chm speaker required. 9 x 6in. ELLIPTICAL SPEAKER, 20/- to purchasers of this chassis. TERMS: (Chassis), 83.10.0 down and 5 monthly payments of £2.4.0. Chesp Boom Dipole for V.H.F., LE/6. Feeder 6d. per yard. ALTERNATUE DEEI 278. Similar to above chassis. With addition of

ALTERNATUR DES 2M. Similar to above chassis. With addition of Shortwave 6-17 Moja. Price \$15.15.0 (carr. paid). TERMS: \$8.10.0 down and 6 monthly payments of £2.4.0. Total H.P. Price \$16.16.0. Circuit diagram 2/5. Carriage to N. Ireland 20/- extra.

NEW 6 FURH-BUTTON STEREGORAN CHASSIS LW.; 8.W.1; 8.W.1; V.H.F.; Grazz; Stereo Gram. Two separate channels for Stereo Gram with balance control. Also operates with two speaker on Radio. Chassis size: 15 x 7 x 64m. high. Dial cream and red, 15 x Stn. Price 517.17.0, carr. paid or \$4.9. deposit and 6 monthly payments of 50/-. Total H.P. price 510.0.0. Cream monified scoutcheon for dial, 7/6 avers.

BATTERY ELIMINATOR

CHARGE THE TUNER CHARGE

Covering 88-96 Mc/s. Dims. 8 x 6 x 6 ts. high. Valves ECOS5, EABCS0 and Fally wired and tested ONLY 88.17.5 (carr. paid). Room dipole, 12/6, Feeder 6d. par yard.



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TRANSISTOR RADIO



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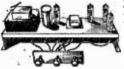
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PLUS 5/- POST. COMPLETE KIT ONLY OR FULLY BUILT 26.7.6. Tax & Carr. Paid

£4.0.0

AMPLIFIER WATT PUSH-PULL O.P. £5.5.0 (6/- Carr.)

200-240 A.C. mains. Bass, treble and vol. controls. EZ80, ECC83 and 2-EL84*s. Chassis 12 x 3½ x 3½in. With o.p. trans. for 2-3 ohm speaker. Front panel (normall) servewed to chassis) may be removed to the control of and used as flying panel. With Cream/Black control panel whole length of front chassis.



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The "BLAKE" 12in. Heavy Duty Cabinet. Size 241 x 18 x 9in. The Baffie is in. thick. Covered in Rexine and Vynair. 85/s. De Luxe model veneered with wood grain Formica and standing on smart 6in. legs. 25. Please add 10/- for postage.

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Rexine leather cloth 50il. wide, 10/6 yard. S.A.E. for samples.

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EARPIECES with cord and 3.5 mm plugs, 8 ohm magnetic 3/-; 250 ohm 4/-; 180 ohm magnetic with clip 6/6; Crystal 4/-.

BROADWAY ELECTRONICS 92 MITCHAM ROAD, TOOTING, S.W.17

Phone: BALham 3984

(four minutes from Tooting Broadway Underground Station)

	COMPONENTS LIST							
Resist		C7 8 μ F 250V.W. C9 50 μ F 250V.W						
RI	22kΩ 20% ¼W R8 22kΩ 20% ¼W	C8 0·1µF						
R2	22kΩ 20% ¼W R9 220kΩ 20% ¼W	C10 270pF 10% silver mica						
R3	100kΩ 20% ¼W R10 3·3kΩ 20% ↓W	C11 3300pF 10% silver mica						
R4	$220k\Omega 20\% \frac{1}{4}W$ RII $470k\Omega 20\% \frac{1}{4}W$	C11 3300pF 10% silver mica C12 680pF 10% silver mica						
R5		C13 33pF 10% silver mica						
R6	100kΩ 20% ¼W R13 1.5MΩ 20% ¼W	C14 100µF 12V						
R7		C15 330pF 5% silver mica						
R15	100K12 10% High Stab. (114)	C16 0.1μ F C18 0.5μ F						
		C17 0.1μ F C19 0.5μ F						
R17	1.5kΩ 10% ¼W R20 150kΩ 10% ¼W	C20)						
R18	47kΩ 20% IW R2I IMΩ 10% ±₩	$C21$ $32\mu F + 32\mu F 450V.W.$						
R19	1.5M 10% 1W	C22 3						
R22	100 O 50/ High Coah 1/4/	C_{23}^{22} > 50 μ F + 50 μ F 450V.W.						
R23	I-8kΩ 5% High Stab. 1W	C24 50µF 25V C25 50µF 25V						
R24	10kΩ 5% High Stab.‡Ŵ	$(15\Omega \text{ speaker} 150\text{pF})$						
R25	120kΩ 5% High Stab. JW	C26 { 7.5Ω speaker 220pF } 5%						
R26	470kΩ 5% High Stab. IW	3.75Ω speaker 330pF						
R27	1-8kΩ 5% High Stab. ½W 10kΩ 5% High Stab. ½W 120kΩ 5% High Stab. ½W 470kΩ 5% High Stab. ½W 150kΩ 10% IW	Valves:						
R28	$100k\Omega$ 5% High Stab. $100k\Omega$ 5% High Stab. $100k\Omega$	VI ECC83 VS 3						
R29	100kΩ 5% High Stab. ČŽ ^{VV}	V2 EF86 V6 \6L6						
K.30	20kO 10% IW R35 10L0 100/ 1\A/	V3 EF86 V7 EZ81						
R31	IMΩ 10% ±W R36 10kΩ 10% ±W	V4 ECC83						
R32	68kΩ 10% IW R37 500Ω 5% 3W	Transformers:						
R33	IMΩ 10% ¼W R36 10kΩ 10% ¼W 68kΩ 10% 1W R37 500Ω 5% 3W 470kΩ 5% ¼W R38 500Ω 5% 3W 470kΩ 5% ¼W R39 10kΩ 10% 3W	TI 8k Ω to 3.75, 7.5 or 15 Ω 20W rating						
R34	470kΩ 5% ±W R39 10kΩ 10% 3W	T2 350-0-350V 100mA						
R40	15Ω spkr-18kΩ, 7·5Ω spkr-12kΩ, 3·75Ω	6·3V c.t. 3A						
	spkr-8·2kΩ	6.3V 1.0A						
R41	82kΩ IW	Miscellaneous:						
RA	Can cour (EVA) analy	VR1, VR2, VR3, VR4, VR5—500kΩ log.						
RB	See text (5W each)	VR6, VR7—2M Ω log.						
		SI D.P.S.T.						
Capac	itors:	5 89A valve holders, 2 I.O. valveholders.						
Çİ	} 16μF+16μF 350V.W.	4 open circuit jacks. 2 coaxial sockets.						
C2	J * * *	I speaker socket. Chassis 13 x 9 x 2½in.						
C3	0.01μF C5 220pF	Base plate 13 x 9in. 7 control knobs.						
C4	0·01μF C6 220pF	Nuts, bolts, wire, grommets, etc.						
		,						

should be checked and should be 44mA and 2.5mA respectively. If the current readings are correct then the mains transformer and rectifier should be checked. High or low currents drawn by the output valves mean incorrect cathode loads and will lead to distortion and low output. R37 and R38 should be adjusted to give as near as possible equal currents through each valve. The correct phase of negative feedback can be decided aurally. The rest of the voltage checks should be made as per Table 1. Applying a 50c/s signal so as to overload the amplifier completely should

give about 19-20V across a 15Ω load.

Final Notes

If the constructor can afford to be really lavish, a beautiful job can be made of this unit and it could, if need be, be built on a larger chassis to accommodate the transformers etc. It will form the perfect basis for a hi-fidelity reproduction system and the constructor will be able to say truthfully that is as good as many commercial products.

EDITORIAL ASSISTANT

An opportunity occurs for a keen radio enthusiast to join the editorial team of "Practical Wireless".

An advanced technical knowledge is not essential, but some previous experience in journalism is desirable.

Salary will be related to qualifications and ability.

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on the Short Waves MONTHLY NEWS FOR DX LISTENERS

All times are in G.M.T.

All frequencies are in kc/s.

The Broadcast Bands-by John Guttridge

Holland: Radio Nederland Wereldomroep (P.O.B. 222, Hilversum) now uses 9,590 for the 0130—0220 English transmission.

Italy: R.A.I. (Casella Postale 320, Rome) transmits in English as follows: 1205—1230, 11,865/9,575; 2020—2040, 9.710/7,275/7,235/6,050/5,990; 0100—0120, 9,630/6,030; 2205—2225, 9,710/6,010; 2115—2135, 7,235/6,050.

Monaco: Trans-World Radio (Rue de la Poste 5, P.O. Box 141, Monte Carlo) has daily English transmissions, all on 7,260, from 0730—0800, and on Sundays at 0800—1100, 1230—1330 and 1600—1630.

Norway: Radio Norway (Oslo) now transmits as follows: 0300—0430, 1,578/6,185/7,240/9,610; 0745—0815, 9,610/21,730/7,240/15,175/17,825; 1100—1230, 7,240/21,730/25,900/9,610/15,175/17,825; 1300—1430, 9,610/21,730/25,900/11,850/15,175/17,825; 1700—1830, 7,240/9,610/11,850; 15,175; 1900—2030, 6,185/7,240/9,610/11,850; 2300—2230, 6,185/7,240/9,610/11,850; 2300—0030, 1,578/6,185/9,610/11,850. Home Service transmissions are relayed on 6,130. This station will also QSL its medium wave home service transmissions. Best outlets to try are 890/1,313/1,578.

Poland: Radio Warsaw (Al Niepodleglosci 75/77. Warsaw) transmits: English to Africa at 1900—1930 on 7,285/9,675 and 2200—2230 on 7,125/7,145/7,285/11,840.

Portugal: Radio Portugal (Rua S. Marcal 1A, Lisboa) has the following English transmissions: 0730—0815 and 0815—0900, 11,840/17,880 or 17,890; 1345—1430 and 1815—1900, 21,495/17,880 or 17,890; 2015—2100, 7,285/6,025; 2245—2330, 1,061/755; 0200—0245, 0400—0445, 6,185/6,025; 0300—0345, 5,985. A DX programme is broadcast every second and fourth Friday at 0745, 0830, 1400, 1830, 2030, 2300, 0215, 0315, 0400. Portuguese-by-Radio lessons are transmitted every Tuesday and Friday for the last quarter of an hour of all short wave transmissions. A special booklet for the lessons is available. A competition, "Make Your Dreams Come True", is being run until June 19. A new quarterly programme guide is available on request.

Rumania: Radio Bucharest (P.O.B. 111, Bucharest) has the following English trans-

missions: 1930—2030, 7,195/6,190; 2230—2300, 7,195/6,190/155; 0130—0230, 11,810/9,590/9,510/6,190/6,150/5,990; 0300—0330 and 0430—0500, 11,810/9,590/9,570/9,510/6,190/6,150/5,990; 1500—1530, 15,380/11,940/11,885/11,810.

U.S.S.R.: Radio Kiev (Ukrainske Radio, Radio Centre, ul Khreshchatik 24, Kiev) can just be heard in English from 1200—1230 on 11,925.

Radio Moscow (Moscow) has English for North America at 2200—2230 on 9,680/7,360/7,250/7,170/7,150 and 0000—0030 on 9,680/9,570/7,360/7,330/7,310/7,250/7,200/7,150.

Vatican: Radio Vatican is reported on 11,735 with English at 2230, Mondays, Wednesdays and Saturdays.

Egypt: Cairo Radio (Propagation and Monitoring Department, U.A.R. Broadcasting and TV, Maspero, Cairo), using the additional outlet of 9,675 to Europe from 1830—2330. Other frequencies are 9,475/11,915. An hour-long English transmission can be heard at 2130.

Ethiopia: Radio Voice of the Gospel, ETLF (P.O. Box 654 Addis Ababa) can be heard signing on at 1300 on 15,410. There is interference from a BBC World Service outlet on this frequency.

Liberia: Voice of America relay, Monrovia (Washington 25, D.C., U.S.A.), may be heard in English from 2200—2215 sign off on the new frequency of 7,130.

Mali: Radio Mali (B.P. 171, Bamako) can be around 2045 on 9,745.

Japan: N.H.K. (Tokyo) has changed frequencies for some General Service transmissions. Affected transmissions are 0100—0130, 15,105/15,300/15,425, and 0200—0230, 0300—0330, 0400—0430, 11,705/15,195/15,300.

Windward Islands: Windward Islands Broadcasting Service (St. George's, Grenada, W.I.) transmits to the British Isles from 2000—2145 on 11,895. Other short wave outlets are: 1545—2240, 5,010; 2155—0215, 3,280; 2245—0215, 2,420.

Ecuador: La Vos de los Andes, HCJB (Casilla 691, Quito), has two evening English transmissions to Europe. They are at 1845—2000 on 17,780/15,405 and 2100—2130 on 15,115/11,755.

Austria: Osterreichischer Rundfunk (Wien IV,

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Argentinierstrasse 30a) has a transmission on Saturdays and Sundays at 1700-2000 on 9.610.

German Federal Republic: Deutsche Welle (Bruederstrasse 1, Postfach 344, 5 Koln) now uses 17,830/11,890 for its 1555—1630 English transmission. The 2020-2050 and 0430-0500 English transmissions from the Kigali, Rwarda, relay have been dropped,

German Democratic Republic: Radio Berlin International (Berlin-Oberschoneweide, Nalepastrasse 18-50) is now using 6.115/6.080/7,185/1,430 for its 2200-2230 European English transmission,

Thanks for contributions go this month to the Middlesbrough Boys' High School Short Wave Club, S. Shaw, L. Sapiets, B. Burling, T. Black, S Ormerod and W. Finch.

The Amateur Bands-by David Gibson G3|DG

TEGULAR readers will be sorry to hear of the illness of your regular columnist G3DG, which has resulted in this emergency write-up by your editor. Latest news is that Dave is now recovering and we hope he will be able to resume his usual role by next issue.

The LF Bands

Coinciding with good m.w. DX conditions, Top Band has been producing some interesting calls including OK, SP, ZB2AM, VO1FB, VP9EU, 9M4LP, 6Y5XG, YVØAA, HK4EB, 2C4GC, EP21W and others. Best times to listen are from around midnight and around dawn. Australia has also been reported, as have plenty of W's.

"80 metres seems very busy with DX activity' says N. Bristow (Stafford), who reports VOIDD, YV5AGA, HKØKL, and HC5, ZB2 and others, all on s.s.b. between 0100-0200. On c.w. much of interest has been heard by members of the staff from late evening onwards and at "breakfast time". Samples—ET3USA, VP2SY, VK5NQ, EP2BQ, H13PC, 6Y5BB and many U's.

7Mc/s

For those who persevere, 40m. can still be rewarding. Best times are late evening and the early a.m.'s, at breakfast time and also early and mid afternoons. Much fine DX has been heard, notably on c.w. of course, such as: ET3USA, KR6DB, ZD8AR, KX6BX, VS6FF, VP5AR, VS9ADF, CR6DA. Japan has been heard in quantity from midday to late evening and VK/ZL during the same period UAO's have also been logged.

14Mc/s

It never fails! Although the band has been closed in the evenings, a lot has been happening during daylight hours, particularly the periods

0500-1000 and early evenings.

N. Bristow found 9M2SS, VK2MO, VK3UQ, VK3AHR, VK6NS all between 1300-1400 on s.s.b. A4378 of Cardiff pulled in VP2VE, PY9HL, PY7YS, VK3AHO, VK9DR, VK6GP, HK3AVE, YVION, HI3XEC, ZB2AJ, HRIJMF, KH6EDX/P, 6Y4DM, UA9KCF—all in three days, on s.s.b.

i. Black of Gillingham logged EA8CR, EA9IC (Ifni), HIISO, HIBJSM, HZIAT, MP4BCC MP4TBO, OD5BZ, 7Q7PBD, 7X2MD, 9GITF 9M6AP, 9Q5AA, OY2H, many VK's, VP5RB, VP9MK, XE2WH, ZC4JU, ZLIAOU, 6W8CW, 6Y5MG, 4X4DK etc—all on phone.

Those who can read c.w. might have heard some of these: VR2EW, YJ1DL, ZD7IP, ZD9BE, BVIUSA, CR3AD, CR8CA, FR7ZG, FB8XX, KX6SZ/Ebon.

21 and 28Mc/s

Well, as expected, 28Mc/s has been virtually dead, although a very few DX signals did struggle through between the hours of 1000-1500. 21Mc/s, however, has been a little more helpful, with some fine DX at times. Ouf friend A4378 of Cardiff logged 9H1R, SVIDB, EA8CR, ZS6RA, ZS6FJW. PY9HL, WAØHHX, KØGQG, VP9DL, ZE6JL and others, all s.s.b.

On c.w., these are some of the stations heard recently: ZD8AR, TT8AE, VQ8AW, FL8MC, JA3API, VS6FF, ZE3JJ, CR7IZ, TY3ATB, VS9AMD, VS6FO, XE1OE, XW8BD, ZD5M, ZD7IP, 9K2AD, 5R8CQ, 9M4MY, Also VK, ZL,

General

G3FNF is now on from St. Helena as ZD7RH, and ZD9BE is on from Tristan da Cunha on 14Mc/s c.w. If you want Ifni, try for EA91C (I. Black heard him on 14Mc/s). We hear that Nauru may be hearable by means of KG6SZ/VK9. Another VK9 to watch for is VK9PL—a rare one indeed (Papua), operation on 21Mc/s.

MEDIUM WAVE DX

The correspondence received following the article on m.w. DX in the November issue, clearly shows that there is a submerged section of the fraternity quietly working away in the background on this band.

If sufficient readers express interest we could well start a regular feature next season. Please write and let us know if you would welcome this move. In the meantime, serious m.w. DX chasers are advised to drop a line to Ken Brownless, 7 The Avenue, York, who, with Al Woodland and Bernard Brown, is collating m.w. DX information.

Beginners should note that conditions are still good. At the time of writing, East Coast Americans/Canadians are often at good strength from 2100 and at superb strength by midnight. Easy ones to try for include CBA Sackville (1070kc/s). Radio America, Swan Island (1157), CJCB, Sydney (1270), WINS New York (1010). CBM Montreal (940), CBT Grand Falls (540), WHDH Boston (850), WNBC New York (660), WOR New York (710), Transworld Radio Bonaire (800), WNFW New York (1130), CJON St. Johns (930). WCBS New York (880), WEZE Boston (1260). Latin Americans are also often good, from 2230 or so. Afternoons and evenings sometimes yield Asiatics, notably Anwhei, China (940), V.O.A. Okinawa (1078), Baghdad (760),

OSCILLATOR CIRCUITRY

R. Leyland

1-TRANSISTOR R-C OSCILLATORS

CIRCUITS that originated in a thermionic form can usually be translated into a transistorised version and this is so with phase-shift oscillators. The sine wave which these develop is indispensable for testing amplifiers and much better able to reveal any severe distortion than is the square wave produced by a multivibrator. Square waves have an application in showing the transient response, but in checks upon both frequency response and upon distortion, such as that due to incorrect bias conditions it is necessary to use sine waves.

The simplest sine wave oscillator is not much more complicated than a multivibrator circuit and its frequency stability may well be superior since it does not depend upon switching levels but upon

phase-shifting properties.

Limiting

Sine waves are also preferable as fundamental a.f. signals because square waves are more easily produced from sine waves by auxiliary limiting or switching stages than are sine waves from square

Fig. 1: Clipping of the output waveform in an overdriven stage.

ones. In fact uncontrolled excessive and amplification in a sine wave oscillator gives rise to squaring on the peaks, as also does a run-down battery. A multivibrator cannot generate a sine wave however the amplitude may be controlled and sine waves can only be extracted from square ones by suppressing the upper harmonics low-pass filters or tuned circuits, which is not a very convenient method and quite different from the principle of phase-shift oscillator.

It is possible by listening to a loudspeaker for variations in the tone produced by a sine wave (which as an audible tone resembles a continuous whistle) to detect the presence of harmonics caused by distortion, but a better method is to observe the waveform on an oscilloscope.

Squaring, or limiting on the peaks, is indicative

of an overdriven valve or transistor and, like other forms of amplitude distortion, is equivalent to the introduction of harmonics which might be described as ripples at higher frequency. Square waves on analysis, resolve into a very large number of these sine wave components, forming a harmonic series of 1, 3, 5, 7... times the fundamental frequency or first harmonic (with even harmonics missing).

A filter can reduce the proportion of upper harmonics relative to the fundamental, but when a pure sine wave is required it is preferable to reduce distortion at its source by restricting the waveform excursions of a sine wave oscillator to the linear part of its amplifying characteristic.

part of its amplifying characteristic

Input Waveform

Distorted waves are also produced in transistor oscillators (Fig. 3) if considerations of impedance level are ignored. The input impedance of a transistor is only about $1k\Omega$ in grounded emitter and may be only 200Ω in grounded base. What matters even more, however, is that this input impedance is non-linear, which implies that the waveforms of the input current and voltage are not alike except for very small inputs. The output

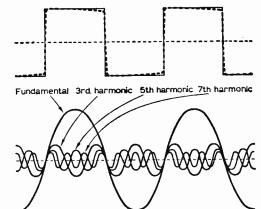


Fig. 2: Sine wave harmonics composing a square wave. Finite rise and sag times modify the square waveform as shown.

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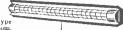
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PRINCESS 2 WAVE

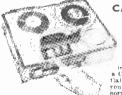
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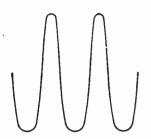


Fig. 3: Distortion of a sine waveform which occurs when the transistor input is fed from a low impedance source.

current reproduces the waveform of the input current, so the required sinewave has to be supplied in the form of a current. A voltage sine wave can only be used if the non-linearity of the transistor input is overcome either by a high series resistor or by negative feedback applied in such a way as to increase the effective input impedance. This "swamping" of the transistor input impedance by making it a small part of the total circuit impedance amounts to a mismatch of impedance levels, and a similar mismatch is required at the output of the amplifier section of the oscillator to ensure a constant input to the phase-shifting network, especially when variable tuning is employed.

Oscillation

Sine waves are produced through the action of the R-C network and stable oscillation involves reproducing the sine wave input for the amplifying section of the oscillator from its own output via the phase-shifting network. Oscillation occurs at the frequency where the overall phase-shift of the amplifier and network is zero provided that the loop gain is greater than unity. It also depends upon positive feedback, but sine waves cannot be generated in the absence of a frequency determining network. Under direct coupling the amplifier then merely acts as a trigger circuit, switching from one voltage level to another when an impulse is applied. With two a.c. couplings the circuit switches automatically as a multivibrator, the frequency depending upon the rate at which the coupling capacitors can charge and discharge between two levels.

Phase Reversals

Positive feedback implies an output in phase with the input. Feedback from the collector to the emitter of a single transistor would be positive, but as the collector current is less than the emitter current oscillation cannot occur without some further amplification. The same is true of feedback from the emitter to the base except that here it is because the emitter voltage is lower than the base voltage. Feedback from the collector to the base is negative feedback and cannot produce oscillation directly. However, a ladder network converts negative into positive feedback at one frequency and thus is able to produce sine wave oscillation if the gain of the transistor is adequate to overcome the attenuation.

When the oscillator contains two transistors a number of circuit arrangements can yield positive feedback. For example, a double phase reversal brings the output back into phase with the input. If there is a phase reversal in only one transistor, as in Fig. 4, a ladder network is used.

Phase reversal in a transistor does not depend upon frequency and is less a phase shift than inversion of the input waveform, but as the negative and positive peaks of a sine wave are alike it is indistinguishable from a phase shift of 180° or one half-cycle such as occurs in a ladder network at one particular frequency and with considerable attenuation. The inverted waveform at the collector is, of course, amplified with respect to the base input. Voltage movements at these electrodes are in opposite directions just as for the grid and anode of a valve.

Some additional internal phase shift occurs in a transistor at high frequencies and this departure from an exact anti-phase relationship is, of course,

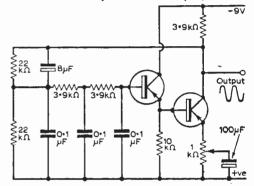


Fig 4: I kc/s oscillator for average transistors, with potentiometer amplitude control.

undesirable since the object is to concentrate all the frequency dependent phase shift into the R-C network. It can be minimised by using r.f. transistors in the oscillator, so enabling its performance to be extended into the lower radio frequencies.

Amplitude Control

Means must be provided of controlling the loop gain of a sine wave resistance capacitance oscillator since harmonics are not suppressed to anything like the extent possible with high-Q tuned circuits.

If the gain is insufficient oscillation will not occur, while if it is excessive there will be squaring of the peaks. Sometimes the amplitude or gain control can take the form of a potentiometer in the emitter circuit of a transistor with the slider grounded through a decoupling capacitor. Over a narrow range of gain adjustment a sine wave output is obtained of amplitude depending on the gain setting. Thus the oscillator is sensitive to small changes in initial gain and to make the amplitude less liable to variation it is desirable to stabilise the amplifier gain by means of negative

feedback, thus offsetting the effects of supply voltage variation and of decrease of gain at high frequencies.

The extra potentiometer for controlling the loop gain is no longer necessary when there is automatic control. Thermionic valve oscillators often incorporate a small lamp (3-15W), its resistance adjusting automatically to keep the amplitude at a constant level. A thermistor can be used instead and consists of a minute bead of temperature sensitive material mounted on wire leads in a glass envelope filled with an inert gas. The thermistor has a negative temperature coefficient, while the lamp is used as a series element in a positive feed-back loop, or as a shunt element in a negative feedback loop, while the thermistor is normally the series element in a negative feed-back path but could be used as a shunt element in a positive feed-back loop. A

blocking capacitor is included to keep direct current from passing through the thermistor, but this precaution is not always observed with a lamp which is sometimes placed in the cathode circuit of

a valve.

Good ventilation is required in a valve circuit as otherwise heat from the valves will reach the thermistor, causing a slow drift. This problem does not arise in a transistorised oscillator but the power in transistor circuits is small and special thermistors are necessary with the thermistor element in a vacuum instead of inert gas. These offer a sensitive means of control but the safe

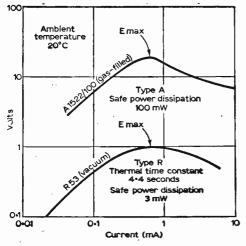


Fig. 6: Thermistor characteristics (S.T.C.). Power Sensitivity of R type is about X14 that of A type. Both obtainable in a range of E max values.

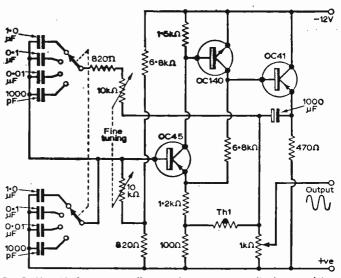


Fig. 5: Variable frequency oscillator with automatic amplitude control by a thermistor (acknowledgements Mullard Ltd.)

power dissipation is very much smaller. A further difference is the much longer thermal time-constant, which implies sluggishness of response. A readjustment to the tuning may cause the temporary cessation of oscillation and it may be a second or two before recovery takes place and the thermistor resumes control. This "amplitude hunting" is not an unusual occurrence in thermionic valve oscillators using lamps or thermistors for control, although to a lesser degree.

The effectiveness of control is increased when the thermistor is one arm of a bridge arrangement. Impedance variations exert more influence in a bridge circuit because some of the unvarying part of the voltage is balanced out. Although with a negative temperature coefficient the resistance of a thermistor decreases as the current is increased the voltage only falls after a peak has been reached at a certain value of current (see Fig. 6). This represents the largest r.m.s. voltage that can be maintained across the thermistor, and for larger currents the resistance decreases so rapidly that the voltage falls with rising current. The thermistor is therefore unable to absorb an excess voltage and passes it on to act as negative feedback. Thus the output of the oscillator will tend to stabilise at a value determined by the maximum voltage of the thermistor.

Alternative methods of amplitude control are sometimes used but are not always as satisfactory, e.g. a limiter followed by sharply selective circuits to remove harmonics or control of amplifier gain in a low-level stage by means of a d.c. bias developed by rectification of the output. Such methods are inherently non-linear, while the thermistor has a short-term kinearity, i.e. its resistance changes slowly and only varies during the cycle at very low frequencies.

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Miniature POWER Amplifier

by J. Harrison

THE miniature power amplifier described in the October, 1964, issue has attracted the attention of quite a number of readers of PRACTICAL Wireless who have since wrote and queried using the amplifier for record reproduction.

This small unit has proved excellent for this purpose and provides smooth music reproduction far above the standard provided by normal commercial record-player amplifiers.

Examining a volume containing servicing data and circuits for current commercial record players

provided the following statistics.

Of valve-driven gramophones 85% use only one valve usually a single high sensitivity output pentode type UL84; 10% use one double valve of the UCL82 variety and the remainder are expensive models which have amplifiers with two or more valves and give reasonable fidelity. sistor versions are usually equipped with three or four transistor amplifiers with class "B" output which produces peculiar distortions which make the sound quality unpleasant to the ear and soon brings about "listener fatigue". After listening with dismay to many new models and reviewing their circuits the miniature power amplifier was designed. The following notes will help constructors to get the best out of this and other small amplifiers.

Suitable Pick-ups and Controls

The amplifier requires 250mV r.m.s. input signal for full output. This is just right for medium to high-output crystal or ceramic pick-ups. For mono any of the Acos GP19 and HGP39 series are excellent, giving good quality with negligible record wear. For stereo working the superb Decca Deram gives just the right output and the BSRC1 at half the cost is good and gives double the output of the Decca.

manufacturers' data-sheets Pick-up quote the sensitivity of their products in millivolts per centimeter per second, which simply means the output signal is directly related to the velocity of movement of the stylus in the record groove. To enable constructors to estimate the output of a particular pick-up from the mv/cm/sec figure the following is a good guide:

Take the mv/cm/sec figure quoted by manufacturer and multiply it by the following factors:

For classical music recordings X5. For EP's and "pop" discs

This difference in output is because with "pop" discs the effective recorded velohigher. city is much Ceramic element pick-ups (Deram and BSRC1) require high value volume controls, $2M\Omega$ being recommended. For others $1M\Omega$ is satisfactory but to combat rumble from inexpensive turn tables a lower value can be tried.

Power Levels for Domestic Listening

This has been a subject for much discussion over the years and the recommendations of experts have varied between 10 W and 100W! The main factors affecting power requirements are:

1. Loudspeaker efficiency.

-continued on page 993

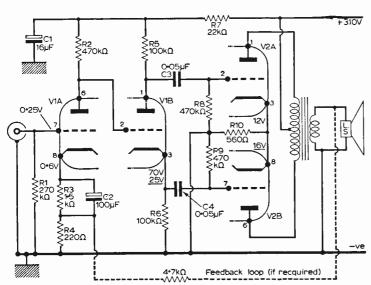


Fig. 1: The circuit. R3 is now $1.5k\Omega$ enabling the first stages to give a larger voltage swing to the output triodes.



No. 5

WELLINGBOROUGH RADIO CLUB

A LTHOUGH most people look on the meeting held in what was the Wellingborough YMCA as the original one, in fact, the nucleus of the Club members had met on the first occasion in a room at a local public house, and then in the workshop of an electrician.

However, it was September of 1952 that the inaugural meeting was held, and what a wonderful cross section of professions were there.

A police sergeant, electricians, teachers, a rail-wayman, and even a representative of a monumental mason! Sadly, however, virtually all the original members are no longer with us, all having left the district. However, on the brighter side their places have been filled by equally keen members.

After the inauguration a few meetings were held

After the inauguration a few meetings were held at the British Railways Sports Club in Wellingborough, but then in November of 1955 we were fortunate in obtaining the use of our present clubroom in Silver Street. This we obtained through one of our members who sadly passed away some years ago. With the use of the room available to us at all times we have been able to decorate it, and do alterations to the electrical side over the years, and so have made the room almost self contained. From this room all our varied projects have been thought up, talked about and brought

into being, and also some of the inquests on our

Throughout the Club's comparatively short history, raising funds for various local charities has always played a prominent part, and has always been a regular summer activity at local fêtes which we have attended, with the assorted electronic games devised by the members.

Perhaps the most memorable of these was the celebrated "Dam Buster". For several years this was very popular with the crowds and aven today people still ask after us not by our radio title but

as "... the dive bomber people".

Soon after we acquired our clubroom one member barely escaped with his life when just before Christmas fire ruined his flat.

The Club immediately went into action with the result that on Christmas Eve the Club Treasurer was able to hand over a cheque to ensure that "Reg", and his family were not without some of the trimmings of Christmas.

For some years the Club's transmitter G3KSX was to be heard frequently on the air from the clubroom. Sadly to relate, in the last two years interest in operating has virtually disappeared and the Club callsign has been put into abeyance, but at the time of writing there are not only plans

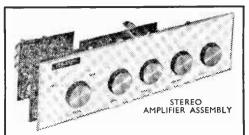
afoot to get the Club's transmitter on the air again, but there is sufficient interest being shown to warrant the starting up of a Morse class. With the arrival of the "overspill population" into the town more new members are appearing, and a confident atmosphere pervades the air as the future programme is planned.

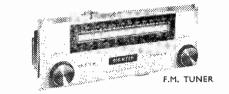
Apart from the talks and lectures to be given, a Club project is to be initiated which will enable members to actively participate in its construction. Over the years the Club has become quite well equipped-in fact at the time of writing members are busy reseating the Club's chairs. Amongst Club's possessions is a 16mm. projector, something we imagine few clubs possess. This enables



Members discuss a c.r.t. that has a modified electron gun for an Electron Difraction experiment.

-continued on page 993





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the Club to include quite a few technical films in its programmes.

So I think that the Wellingborough Radio Club, to which, incidentally, it changed to from its more lengthy title of Wellingborough and District Radio and Television Society some years ago, can look forward to a happy future.

Admittedly the last few years have been lean ones but there is no doubt that things are on the up and up. One has only to see the new faces in the clubroom on Thursday evenings, to which

anyone who is interested in ANY aspect of electronic or electrical work is most heartily welcome.

Do you live in the Wellingborough district? The fact that you read this magazine proves that you are interested, so why not pop in to see us or drop our secretary a line? We shall be very pleased to see you or to hear from you.

Meetings are held every Thursday evening at 7.45 p.m. in the clubroom, situated above the W.I.C.S. fruit shop in Silver Street, Wellingborough. The hon, secretary is Mr. J. Baker, 34 Essex Road, Rushden, Northants,

SWITCH-TUNED SUPERHET

-continued from page 967

meter is available, check the voltages as indicated on the circuit diagram of Fig. 1. Note that these voltages are obtained with an h.t. of 250 volts; the h.t. can be reduced to this level by loading the supply with a suitable resistor, although such accuracy is not strictly necessary.

The circuit can be given a functional check as an a.f. amplifier in a number of ways. Three of these are as follows:—

- (a) Feed the output of a transistor or valve radio directly between the loose end of C10 and chassis.
- (b) Connect microphone between C10 and chassis.
- (c) If a spare speaker and output transformer are available, connect the spare speaker to the transformer secondary, and the primary between C10 and chassis. The arrangement will now act as a microphone.

In the case of both (b) and (c) it will be found that if a "microphone" is placed within the vicinity of the receiver speaker, "howling" will

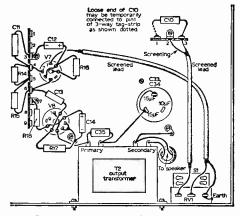


Fig. 4: Wiring details of the A.F. section.

take place due to feedback; howling may take place at ranges up to several feet.

A maximum output of about half a watt, with little distortion, should be available.

TO BE CONTINUED

MINIATURE POWER AMPLIFIER—continued from page 989

2. Size of room and furnishings.

3. Preferred listening level.

As a guide to the home constructor a test was made with a calibrated oscilloscope across the terminals of an 8in. speaker with 12,000-line magnet in a small cabinet in a well-furnished room of 2.000 cu. ft volume. The electrical power needed to generate more than adequate level of sound was as follows:

Average volume level power to speaker 0.085W. Peak volume level power to speaker 0.48W.

Static and Dynamic Tests

Testing and evaluating the performance of a finished project can be both interesting and instructive and it is always satisfying to know a piece of equipment is working correctly. Static (d.c.) and dynamic (a.c.) voltages are indicated in the circuit diagram. For constructors with limited test equipment measurement of the d.c. volts at V1 cathode and the junction of the output valves' cathodes gives a reliable indication that the amplifier is working correctly.

Circuit Improvement

Only one slight component change has been found to improve on the original circuit and that is reducing R3 to $1.5 \, \mathrm{k}\Omega$. This enables the first stages to give a larger voltage swing to the output triodes. Changing this resistor alters the static voltages applied to the anodes and cathodes of the voltage amplifier and phase-splitter. These voltages are shown on the circuit diagram; full-power signal voltages are underlined.

R10 was given as 270Ω in the original circuit. This was incorrect and should have been 560Ω .

Because of the small anode currents (9mA) and balanced working of the output valves a small transformer can give good response and the Elstone MR/T is recommended for 3Ω speakers.

Reliability Test

A 250-hour reliability test was given to one of the small amplifiers. It was driven continuously at full output at 1,500c/s and at the end of the test all resistors were found to be working well within their rated power and there was no measurable change in valve performance.

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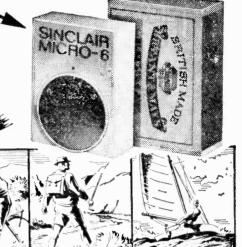
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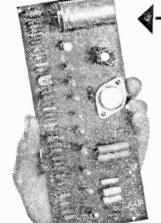
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7 TRANSISTOR SUPERHET FM TUNER/RECEIVER * TECHNICAL DESCRIPTION

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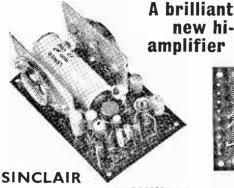
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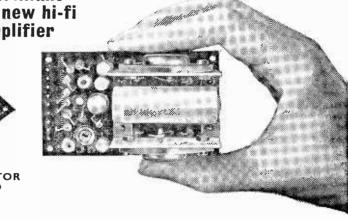
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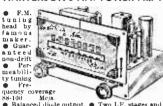
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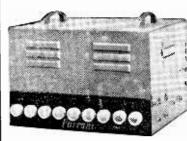
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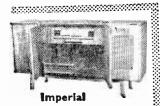
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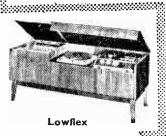
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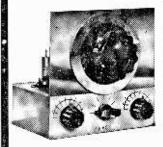
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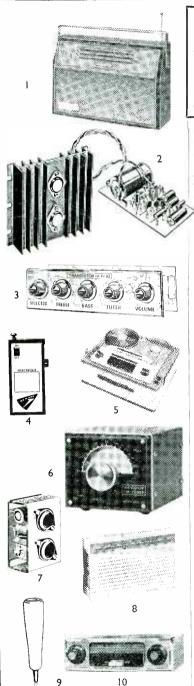
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