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 ELUIPMPNI．Ali requited parts，point to point $Q_{\text {Carr．idut }}$ wiring diagrams and detailed instructions． OGNS．$_{\text {GN }}$
If required printed circuits can be supplied wth appropiste components assombied，soldered and lested or 2 ens．extra Or unit completely assembled ready or use． 73 GNS． Or 2906 Carr． 151 Total 296．12．0．


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## R.S.C. STEREO 20/HIGH FIDELITY AMPLIFIER

 PROVIDING IO/I4 WATT ULTRA LINEAR PUSH-PULL OUTPUT ON EACH CHANNEL EUITABLE for "MIKE", GRAM.. HADIG OR TAPE. INTENDED FOR THE HOME OR STUDIO BUT X OTABLE PUR LALGE HALLS OR CLLBE* Four-position tone compensation and Output transinmers are high-quality sectlonally wound Input Seleetor switeb.
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* Separate Bass "Lift" and "Cut" and treble "Lul" and "Cut" controls.
* Neon panel indicator.
* Handsome Persper Frontplate.

Based on a current Mullard desien and employ-

to required apectication Uut put matchings for 3 end 15 mom speakpre ai each chanuetors Complote et of parts with poututo ponat wiring diazrans and witruc13 gns. fons, or Facto $y$ assembled. tested and sur or 19EPOXIT $5 \% /$ and 9 monthi payment., of $39 / 10$ total $£ 20.15 .6$ ). 18 Gns. A protective womien cabinet corered in a pleasin shade ni leatherelinth and hitted carrying hapdies ant feet can he supphed for $59 / 6$ extra. Varr. $5 / t$. Terous:
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(Trital 6 n/6).
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rempde. OUTPUT SOCKET PROVIDES L,T, aul H.T ior

 Complete kit of warte with mils puth hed chavis asid pont-to-pont wring diaurame and


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HIGH FIDELITY 12-14 WATT AMPLIFIER TYPE A11 PUSH-PULL ULTRA LINEAR OUTPUT "BUILT-IN" TONE Two mixing of "mike" and gram.. as in Alo. Iing EL84. EL8f, EZ81. High Qualıty sectionaliy wound output transtormer specrally designed for Ultra Linear oneration and reliable small condensers of FOR BASS AND TREBIE "N AN M, Frequency response $\pm 3 \mathrm{~dB} 30-20$, mit" and tive feedhack loonse $\pm 3$ dB $30-2$, , Six neya23 millivolts input required for FULL OUTPUT.
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12 B .3 W WTI IITFII.OL DSPEAKERS M CABINETs, Size 18 x $\pm 7.19 .6$ Terms: Deposit $17 / 9$ and 9 monthly pay-
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 AUBIOTRINE CORNER CONSOLE CABINETS Sirorgh made. Boantimit inith. Plrasung desun JTNIOR MODEL
Aprirax. $29 \times 1149 / 9$ standard model. To

## 5 Gns.



SENIOR MODEL. To take ut to 1210 . praker abd Kecommented for use with Audiotrme speaker arstum). Carr. 8/6. 8 GnS.
Tumus avaliable.
IUISOTHIXE III-FI SIPEAKER sySTLNA Consisting of matched $12 i n$ 12,000 line, IJ ohm high qualsty speaker cross-over unit choke, condenser, etc. and

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ensure surnrismshy realistic reproduction.
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## R.S.C. BASS-REGENT 50 WATT AMPLIFIER <br> AN EXCEPTIONALLY POWERFUL HIGH QUALITY ALL-PURPOSE UNIT For lead, rhythm, bass guitar and all other musical instruments For vocalists, gram, radio, tape and general public address <br> CKlsually puwerffut EOLDSPEAKER



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only 89/6. carr. 5i/. Ready for use, G ens. R.S.C. BATTER Y TO MINC CONVER-


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ASSEMBLED Fitted Ammeter and selector plug for 2 v Louvred metal cast finshed attractive hammer blue. Fused, ready for use with mains 39.9 Carr. /I2v. 1 nmp $27 / 9$

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## |ASON FMTI V.H.F./F.M. RadierTuner

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 a high quality tadio Tuner (specialls sullable for use with our Amplifiers). Lelayed A.V./C. Controls are Tuning. W/Ch. and vol. Only 250 v . 15 mA H.T. and L . T. of 6.3 v .1 amp required from arnplifter. Size approx. $9 \times 6 \times 7$ 7n. high. Simple aligro ment procedure. Point-to-point wiring diagrams, instructions and priced parts 1tst with illustrations, $2 / 6$. Total buildine COSt5 85.5.0. S.A.E. for jeaflet. OC45 3/11, OC44 3/11, 0C722/21, OC81 2/11. 0 Cl 171 S/9. AF17 6/9. Ediswan XA101 3/0. XA112 3/9. XC101A 3/9. Postare 6d. for up XA112 3/9. XClolto 3 transistors.

INTEREST CHARGES REFUNDED ON H.P. ACCOUNTS SETFLED IN 6 MONTHS R.S.C.


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dresses Page 749 freved in two-tone Rexine! Public Address. Normally supplied tor 15 ohm marching but or 351 - exvar Tuw (os, b-x0 walls. Fitted Overall size apptox. $42 \times 10 \times 51 \mathrm{n}$ $12 \frac{1}{2}$ Gins. Carr. Ur deposit morthiv. pa. Tybe dis, th watt: Fitted speakers Overul din. aporox $19 \frac{1}{2}$ Gins. Or jeposit ef 3 gn- and 9 mthly

30 WATT HI-FI AMPLIFIER FOR LEAD, RHYTHM BASS GUITAR and for VOCAL or INSTRUMENTAL GROUPS
 Four Input, trol Hi-Fi uni with separate Cut' and 'Treble controls. signed for vocal or instrumental Lead or Rhythm. outar Mullard or Brimar latest type valves. Housed 17 strons Rexine covered cabinet with cwin carrying handles. Attractive black and gold Perspex fascla plate. For $200-250$ V. A.C. mains. Output for sor 15 ohm speakers. 17 GNS. or payments of and mo monthly

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## F.

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to 30 Mcis rule tuning dial 'S meter. intermal lerrite aertal tor medium wave. Telescopic whip aerial 58 in .10 section fol short waves. Fitted sockets for optional outdoor aerlal. Headphones, extermal speatier socket. Other iea tures are electrical bandspreaci tuning. Noise limiter, A.V.C. B.F.O.: sand by switch size approx. 124 x $x$ gin. Handsome With full instructiuns mannal 19 Gns.

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## practical WIRELESS

## BEGINNING AND END

AN interesting fellow was Janus. A principal divinity in Roman mythology, he was primarily the god of All Doorways and, being blessed with two faces, could observe both the interior and exterior of a house. This handy physiognomical duality also enabled him to obtain the jobs of god of Beginnings and god of Departure. He also played an important role in the creation of the world. The first month of the year-Januarius-bore his name. In fact, a very versatile and busy lad.
Even so, he also held the position of god of All Means of Communication and it is a sobering thought that if we were still in the days of the Roman Empire he would not only be Minister of Transfort and Postmaster General, but President of the RSGB and Governor-General of the BBC.
We shall never know what he would have thought about the RAE, the virtues of SSB or the prospects of $14 \mathrm{Mc} / \mathrm{s} D \mathrm{X}$, but we can be sure he would have quickly dealt with pirate radio stations, licence dodgers, Party Political Broadcasts and other ills of our time. He might even have got together with his buddy Jupiter (President of the Board of Trade) and banned the import of $27 \mathrm{Mc} / \mathrm{s}$ walkie-talkies!

Reluctantly, returning to earth let us, like the double faced Janus, simultaneously look backwards and forwards by thanking you all for your interest during the past year and wishing you

| $\mathcal{A}$ Thappe CBristmas and Successfuf Mew Vear from the exitor and Gafaff. |
| :---: |
|  |  |

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An Economy Two-Band Receiver
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Short Wave Data in the Pull-Out Supplement

[^0]
## M.W.-D.X.

I feel I must compliment you on an excellent article called "M.W.-D.X." in the November issue of Practical Wireless. This is just the kind of text to encourage DXers against the streams of, "What's the point?" . ., Why bother? . . . So what? ..." people who just can't understand why we should stay up to 0400 for a few $\mu$ V's from New York.
A. Peake.

> Great Yarmouth, Norfolk.

## Batteries Offer

About this time last year, you printed in Practical Wireless my offer of free h.t. batteries. You may be interested to know that the response was very good. 1 despatched 109 to 71 applicants and still get the odd letters from people who have been reading back numbers. I had to turn down a further 20 requests as I had exhausted my supplies. However, the main purpose of this letter is to make an offer of 6 V dry batteries. The size is approximately 5 in, $x 4 \frac{1}{2} \mathrm{in}$. $x ~ 2 \frac{1}{4} \mathrm{in}$. and the weight $3 \frac{1}{3} \mathrm{lhs}$. Each battery contains eight cells wired in series/parallel to give 6 v , and they can easily be rewired for 3 or 1.5 V operation. Connection is by PVC covered wires. I can most easily send these in batches of four at 6s. post. ( 5 s . 6d. plus 6d. packing). Please send Postal Orders and do not cross.
These batteries are ex-U.S. Forces, thrown away due to the elapse of the makers' life expectancy. However, they are really as good as new. One person who tried one of these told me that it ran his transistor set for 14 months.
H. Humphries.

Old Rectory,
Gazeley, Newmarket, Suffolk.

## Mr. Methven Please

I wonder if Mr. Methven (June 1965 issue. page 148) would get in touch with me, please, as I would like to communicate with him.
H. Seaton.

The Presbytery, Foundry Hill, Hayle, Cornwall.

NEWS AND

## SLEEP-LEARNING EQUIPMENT



A number of researchers in America have laid great claims to the sleep learning method. It is particularly useful when a large number of facts have to be committed to memory, such as formulae, foreign languages etc.

The four simple basic requircments are a tape recorder, time switch, under-pillow speaker and a genume destre to lcarn.

If you possess the lacter requrement, then the first three can easily be obtamed from R.C.S. Products, Led., $\|$ Oliver Road, London. E. 17. $£ 45 \mathrm{~s}$. Od. buys the time switch with 14 day Swiss movement. The modified tape recorder complete with mic. and pre-recorded conditioning tape costs £23, and the pillow speaker 27s. 6d. The complete outfit may be obtained from R.C.S. Products at a cost of $£ 2910 \mathrm{~s}$.

## PRACTICAL WIRELESS AND PRACTICAL TELEVIEION FILM SHOW

The P.W. and P.TV. Fiimshow is to be held on February 4th. 1966. For more details see the notice on page 783.

## MASTERTAPE CHRISTMAS GIFTS

Mastertape (Magnetic) Ltd., announce that with every reel of Mastertape purchased over the Christmas period an empty spool of equivalent size will be provided free of charge.

The full reel and the empty spool will be packed together in a sealed polythene bag attractively over-printed with a Christmas motif.

## BRITISH ELECTRONICS FOR AMERIGAN AIRGRAFT

More British electronic equipment has been ordered by the Ministry of Aviation for the R.A.F.'s American Lockheed C-130 Hercules long-range transport aircraft.

Marconi Sixty Series transistorised airborne radio communications and navigation aids which are to be fitted, are already standard equipment in the majority of aircraft currently flying with the R.A.F.

Equipment specified includes the AD260 v.h.f. navigation system and the AD 360 automatic direction finding system. The AD260 provides full v.f.f. navigation facilities and provides the instrument landing outputs used in the automatic landing system in the BEA Trident and also in the BOAC VC-10 aircraft. The AD360 is the standard Marconi airline automatic direction finding system. It features fully automatic crystal controlled tuning which was pioneered by the Company, and is still only
available in Marconi ADF's. available in Marconi ADF's.

# COMMENT 

## EQUIPMENT FOR UK3 SATELLITE

UK3, the first all-British satellite, is being designed and built by the Guided Weapons Division of the British Aircraft Corporation.
At the Glenrothes, Fife, plant of Hughes International (UK) Ltd., microglass diodes are welded on to printed circuit boards to be used in the telemetry ground equipment of the project. These diodes form part of the microminiaturisation of the decoding matrices used in the telemetry ground equipment.

## EMBOSSED PLASTIG CALLSIGN PLAQUES

We have received from F. W. Harris \& Ca. Ltd., Town Hall Chambers, Lydney, Gloucestershire, a specimen callsign plaque. Inch-high letters are heat embossed into the white plastic background which measures $4 \mathrm{in} . \times 2 \mathrm{in}$.
The plaque, which is washoble and easily drilled for fixing, costs 3 s . inciusive. A free-standing version is priced at 4 s .

## CIVIL SERVICE RADIO SOCIETY

The Civil Service Radio Society will be pleased to welcome members of H.M. Civil Service and associated organisations to their meetings at the Science Museum, South Kensington. The meeting on 7 th December featured films on amateur radio. and on the 2lst there will be an informal meeting and a Christmas party. For further details, please contact the Secretary, Mr. G. Lloyd-Daiton, 2 Honister Heights, Purley, Surrey, or H. E. Reeve, G3JXZ, 284a Barking Road, East Ham, London, E.6.

## SOLID STATE AMPLIFIER

Messrs. Henry's Radio Lid., 303 Edgware Road, London, W.2., are fost making a name as being one of the transistor people as for as the constructor is concerned.

Their latest offering is a ready built audio amplifier with a frequency response $30 \mathrm{c} / \mathrm{s}$ to $16 \mathrm{kc} / \mathrm{s}$. The sensitivity is 6 mV into $1 \mathrm{k} \Omega$ for a push-pull output of 5 W r.m.s., IOW peak with less than $1 \%$ distortion.

Despite the output, and the s!x transistors plus diade, the unit measures only $2 \frac{7}{g} \mathrm{in}$. $\times 2 \mathrm{in} . \times 1 \frac{1}{2} \mathrm{in}$. and is avalable ready built and tested at £3 19s. 6d. plus 2s. post and package.

It uses a transformerless design, with outputs for 3,4 or $5 \Omega$ speakers. An optional mains unit is available at 54s., and for the hi-fi enthusiasts, o full-function preamplifier ot 79 s . 6 d .

more News and Comment

## To Make, or To Buy?

When reading the 'Editorial' and 'News and Comment' in the December 1965 issue of Practical Wireless, I felt that one point had been missed; the factor of technical advances in radio.

When most Amateurs were building their own equipment. the circuits and techniques were very elementary compared with the complexity of knowledge and highly advanced techniques of today. In the old days very good results were possible with simple equipment, since this equipment was norm. Today, however, one has to build modern firstclass equipment to compete with the commercial product. This requires a great deal of knowledge and skill of the sort which is available to the professional. For the Amateur who does not earn his living in the radio or electronic indusiry these techniques are sometimes felt to be far too difficult to master, and who is to blame him for buying the commercial article?
B. Otter.

Durham City.

## Thank-you Letter

In reply to the request for the "Regency" blueprint which youl kindly published for me, many readers sent copies. Some even enclosed the relevant issues of Practical Wireless, and one gentleman not only sent these but also enclosed the "Citizen" blueprint with the oscillator section completely wired and tested!

Will you through the medium of your columns thank all readers who helped me?
J. Owens.

Dolgellau, N. Wales.

## Correspondent Wanted

I AM interested in most branches of electronics. I would like to correspond with anyone who has the same interests and who is about the same age as myself (17).
David Higgins.
3 Woolgreaves Drive.
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on page 784


Push-Pull ELL80 Amplifier

## 3 VALVES * 8 WATTS

ALTHOUGH it uses only three valves and a minimum of other components this amplifier has an output of 8 W and will reproduce records and radio programmes, etc., at high quality.

## The Circuit

Referring to Fig. 1 it will be seen that the output stage employs only one valve, ELL80, which contains two pentode assemblies with a common cathode. Although rather expensive at present it is not unduly so when it is remembered that it takes the place of two and eliminates the problem of finding a matched pair of valves for the conventional push-pull circuit. The valve has a slope of $6 \mathrm{~mA} / \mathrm{V}$ and with 250 V on anodes and screens and a bias resistor of $180 \Omega$ it provides a power output of 8.5 W in return for a signal of

24 V peak grid to grid. The signal currents through the two halves of the valve cancel out at the common cathode and the bias resistor does not have to be by-passed. Resistor R14 is included in the supply to the screens to ensure that, taking into account the voltage drop in the output transformer primary, the screen voltage will not exceed that at the anode.

The optimum load for the ELL80 is $11,000 \Omega$. The specified output transformer is advertised for use with 6 V 6 or EL84 output valves but the manufacturers state that it is designed for a load of $10,000 \Omega$ and it is therefore suitable for the ELL80.

## Phase Inversion

The valve V2 is a double triode, ECC83, one half of which is used to provide the two signals of opposite phase required by the output stage. Allowing for the decoupling provided by resistor R11 and capacitor C10 the supply voltage to the stage is 245 V and with a total load of $200 \mathrm{k} \Omega$ $(R 12+R 13)$ the valve has an output capability of 27 V r.m.s. This meets the requirement of the output stage with something in hand.

It will be noted that the cathode of V 2 b is about 120 V above earth, which permits the grid to be directly coupled to the anode of V2a, so saving a coupling capacitor, grid and bias resistors. With this circuit the voltage across R13 is a little higher than that at the anode of $V 2 a$, thus providing working bias for the valve, a state of affairs which is automatically maintained irrespective of variations in supply voltage, etc. A further advantage is that direct coupling eliminates phase shift at extreme frequencies, which can be troublesome when feedback is applied over several stages as it is in this amplifier.

Heavy negative current feedback due to the large un-bypassed cathode load gives excellent linearity but the gain, as might be expected, is low, 0.9 each side or 1.8 times overall. For full loading the inverter therefore requires a signal of


Fig. 1: Circuit diagram of the amplifier.

## Voltage Amplifier

This signal is provided by V2a arranged as a conventional resistance coupled amplifier with decoupling provided by resistor R8 and capacitor C9. The bias resistor R10 is not by-passed, which saves a component and provides a convenient point for the injection of negative voltage feedback derived through resistor R18 from the secondary of the output transformer. This feedback compensates for deficiences in the transformer, reduces harmonic distortion and improves loudspeaker damping.

The values of resistors R10 and R18 are so chosen that in parallel they provide the correct bias for the valve, while in series, they cause the* desired percentage of the output voltage to be fed back. It will be seen that V2a operates with both current and voltage feedback and consequently with excellent linearity.

## Preamplifier and Tone Contro's

The gain of the amplifier from the grid of $V 2 a$ onwards is insufficient for most purposes, especially when the losses due to the introduction of tone controls are taken into account. A fairly high gain preamplifier stage is therefore needed.

The valve V 1 , in a conventional resistance coupled circuit with anode load of $100 \mathrm{k} \Omega$, gives a stage gain of 120 times. A gain of 180 can be had here by increasing R4 to $220 \mathrm{k} \Omega$. R. 1 to $1 \cdot 2 \mathrm{M} \Omega$ and R 5 to $2 \mathrm{k} \Omega$. but if this is done the s ,nal handling capacity of the valve will be reduced and it will be necessary to replace the grid resistor R 2 by a $1 \mathrm{M} \Omega$ potentiometer so that overloading with large inputs can be avoided.

With the circuit of Fig. 1 overloading will not occur with any normal gramophone or radio tuner input. The radio signal input is taken from a coaxial socket through the closed circuit jack It to the grid. Insertion of the jack plug disconnects the radio input and connects any other desired input.

The preamplified signal from V1 is fed into a Mullard-type tone control network consisting of the potentiometers VR1 and VR2 and their associated resistors and capacitors and thence to the volume control VR3. which incorporates the mains switching. Insertion of the controls at this point in the circuit ensures that thev are not liable to electrostatic hum pick-up and that any noise voltages originating in the first stage are reduced along with the signal when the volume is turned down. The values of the capacitors C5, C6, C7 and C8 gave a good range of control in the prototype but tone control is verv much a matter of individual preference and the capacitor values can be varied as desired.

## Power Supply

The amplifier requires an h.t. supply of 75 m A at 265 V under full load conditions and 2 A at 6.3 V for the valve heaters and indicator lamp. This is provided by a double-wound mains transformer and two silicon rectifiers. SR1 and SR2. Fuses are included to protect the transformer winding in

## COMPONENTS LIST

Resistors (all $\frac{1}{2} \mathrm{~W}$. unless otherwise stated)

| RI | 390 k S |
| :---: | :---: |
| R2 | 1 M $\Omega$ |
| R3 | 33ks, |
| R4 | 100 k s |
| R5 | lks |
| R6 | 150 k ¢ 2 |
| R7 | 150 k S |
| R8 | 27kS |
| R9 | $560 \mathrm{k} \Omega$ |
| R10 | 2.7k』 |
| RII | 27 kS |
| R12 | 100ks2 Matched |
| R13 | 100ks Sor 1\% |
| R14 | 2.2k』 |
| R15 | 470k $\Omega$ Matched |
| R16 | 470 k ) \} or 1\% |
| R17 | 18092 w . |
| R18 | 6.8 k S |
| R19 | 270s. iw. |
| VRI | $2 M \Omega$ log. (Treble) |
| VR2 | 2 MS log. (Bass) |
| VR3 | 1 MS log , with 5 witch |
| Valves |  |
| V1 | EF86, B9A base. |
| V2 | ECC83, B9A base. |
| V3 | ELL80, B9A base. |
| Capacitors (350v. working unt |  |
| Cl | $0.1 \mu \mathrm{~F}$ |
| C2 | $50 \mu \mathrm{~F} 25 \mathrm{v}$. electrolytic |
| C3 | $8_{\mu} \mathrm{F}$ electrolytic |
| C4 | $0.05 \mu \mathrm{~F}$ |
| C5 | 68 pF |
| C6 | 680 pF |
| C7 | 270 pF |
| C8 | 3,300 pF |
| C9 | $8 \mu \mathrm{~F}$ electrolytic |
| C10 | $8 \mu \mathrm{~F}$ electrolytic |
| CII | $0.1 \mu \mathrm{~F}$ |
| Cl 2 | $0.1 \mu \mathrm{~F}$ |
| Cl 3 | 16 \% F electrolytic |
| C14 | $16 \mu \mathrm{~F}$ electrolytic |

## Transformers

Mains $250-0-250 \mathrm{v} .80 \mathrm{~mA} .6 \cdot 3 \mathrm{v} .2 \mathrm{amp}$.
Output Push-pull, $10 / 12$ watts, 6 V 6 or EL84 to 3 and 15 ohms. R.S.C. (Manchester) Ltd.
Rectifiers
SR1, SR2—Silicon, BY 100 or similar
Fuses
FI, F2 150 mA .
Indicator Lamp
6.3 v .0 .3 amp . and holder.

## Miscellaneous

co-axial socket, closed circuit jack socker, aluminium for chassis, mains cable and plug, 22 s.w.g. tinned copper wire, sleeving, hardware, etc.
event of a rectifier breakdown. The reservoir capacitor is virtually C14+C13: resistor R19 has little smoothing effect and is included only to reduce the h.t. line voltage to the required figure of 265 V . Each of the earlier stages is provided with separate decoupling and smoothing, while in the output stage hum is alnost completely cancelled out by push-pull operation. What little
is left is very effectively suppressed by negative feedback and cannot be detected 12 in . from the speaker.
There is, of course, no reason why a valve rectifier should not be used if preferred and the fuses F1 and F2 need not then be fitted. The onlv requirements are that the valve should be capable of passing the required current and that a heater supply for it is available on the mains transformer. The advantage of the silicon rectifiers is that they do not generate heat, which is a consideration if the amplifier is to be installed in a cabinet with limited ventilation.

## Construction

The amplifier is constructed on a chassis of 16 s.w.g. aluminium sheet, 12 in . $x$ 5in. $x \quad 1 \frac{1}{2} \mathrm{in}$.. details of which are shown in Fig. 2. This allows plenty of room for everything, simplifies the construction and wiring and enables the constructor to make use of some of the older and bulkier components from the spares box. The wiring. for which 22 s.w.g. tinned copper covered with sleeving is suitable, is shown in detail in Fig. 3.
Note that in this diagram the positions of the components are approximate and the wiring has been opened out to make the connections clear. In construction all wiring should be kept to a reasonable length, particularly in the early stages, and if this is done no screening will be necessary anywhere in the amplifier. The positioning of the components is not critical.

## Components

If silicon rectifiers are used the h.t. voltage will come on before the valves are warmed up and
ready to receive it and all capacitors except C2 must therefore be 350 V working.
The accuracy of balance in the inverter stage depends entirely on the values of the resistors R12 and R13. Close-tolerance components are not necessary but the two must be balanced as closely as possible to ensure that their values are identical. Alternatively $1 \%$ resistors can be used. These remarks apply also to resistors R15 and R16 in the output stage. The wattage rating for resistors is given in the components list.

## Testing

First check that the valves are in the correct positions. The connections to V2 and V3 are such that if the valves are accidentally transposed a dead short will appear on the h.t. line. Next check with a meter on a high-resistance range between C14 and chassis to see that there are no shorts. The lead carrying the positive voltage from the meter battery should be applied to C14, when a large deflection should be observed, dropping back slowly to a reading of $1 \mathrm{M} \Omega$ or more as the capacitors become charged from the meter battery. Now connect a speaker and apply power. If as the valves warm up there is instability, reverse the connections from the output transformer primary to the ELL80 anodes to make the feedback negative.

The following voltages should be found at the points indicated using a 20,000 o.p.v. meter. Any substantial departure from these figures should be investigated.
C3 to chassis
C9
C10..................... 230 V
C13
C13
"


Fig. 2: Chassis drilling dimensions.


Fig. 3: Wiring diagram of the amplifier-underside view.

| V3 | anodes | screens ........... 255 V |
| :---: | :---: | :---: |
| $V 1$ | cathode | 1.8 V |
| V2a |  | $1 \cdot 4 \mathrm{~V}$ |
| V2b | , | 122 V |
| V3 | " | 12.2 V |

## Operation

A good amplifier is of little use without a good speaker and it is equally important that the
speaker should be suitably housed. The prototype gave excellent results with an 8 in. column speaker fitted in a 9 in . glazed ceramic drainpipe. Domestic objections to the pipe can be overcome by painting it with metallic paint. Another point to note is that while the tone controls have a good range they cannot be relied upon to compensate for large deficiencies in the input signal. The output from a pick-up, for instance, must be corrected for recording loss if the best results are to be achieved.

## BUMPER ISSUE THIS MONTH!

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# UNDERSTANDING F.M. 

by W. Groome

RADIO is a progressive hobby. Sooner or later you will turn to frequency modulation for high quality. interference-free reception and will want to build your PW design with an understanding comparable with your knowledge of amplitude modulation. The main difficulty seems to be that of visualising the behaviour of the carrier and this impedes the study of the discriminator. Despite technical and mathematical proof most of us like to have a mental image of what goes on; we like to "get the picture" first and then proceed to advanced details. In this article much of the picture is aimed at your imagination. but there is no childish simplification and nothing that will conflict with any contemplated further study.

The basis of all signalling is change. Something must wave, wag. flash, flicker, hoot-there must be some noticeable or detectable change of a normally steady state. A radio carrier alternates at a high frequency but can be said to have a steady state when the frequency and radiated power are constant, producing-by rectification in the receiver-an unvarying voltage. It is easy to appreciate that changes in the transmitted power will produce corresponding changes in the rectified voltage and that such changes can follow the waveform of the audio signal.

This is amplitude modulation. with which we can take the carrier frequency for granted (as we do with most dependable things) and regard the easy relationship between carrier amplitude changes and rectified signal amplitude changes. With frequency modulation the carrier power is constant; the waveform and dynamic range of the mudio signal are represented by changes of carrier frequency. Here lies one of the problems. The audio signal begins in the studio as a current or voltage varying in amplitude and it must emerge at some stage of the receiver in the same form. How can these changes of energy be conveyed by a carrier of constant power? A quick answer, which we shalil develop later, is that they are not
conveyed, they are represented. Another question arises from a glance at transmitter characteristics. How can we relate carrier frequency swings as wide as $150 \mathrm{kc} / \mathrm{s}$ with the frequency and amplitude of audio signals in the region under $20 \mathrm{kc} / \mathrm{s}$ ?

Here I call upon your imagination. Fig. 1 represents the dial of a receiver. It is calibrated vertically in $\mathrm{kc} / \mathrm{s}$ and has a pointer driven by the usual knob (not shown). A certain frequency is marked at the middle of the scale ( fc ) and others are shown by the amount by which they are higher or lower than fc . The receiver is selective and has a visual indicator (not shown) to tell you when a carrier is tuned in.

Imagine that a carrier has been located at fc but it seems wayward: it is drifting and you have to retune. Still it drifts and as you manipulate the knob to follow it the pointer is driven up to $+30 \mathrm{kc} / \mathrm{s}$, then you have to tune downwards to follow the carrier to $f c$ and then further down as far as $-30 \mathrm{kc} / \mathrm{s}$. Here it drifts up again until the pointer finally returns to $f c$.

Let us check what happened. The carrier drifted by a large amount - from fc up to $+30 \mathrm{kc} / \mathrm{s}$. then down to $\mathrm{f} c$ and beyond to - $30 \mathrm{kc} / \mathrm{s}$, finally returning to fc. One whole cycle of change. Yes, just one cycle of change. Despite all the $\mathrm{kc} / \mathrm{s}$ your pointer moved up and down in only one cycle. and if you like to go over it again in imagination you will find that the pointer movement agrees well with the rise and fall of a sine wave. You will also realise that the pointer, following deviations of frequency, had a certain amplitude of movement. which suggests the possibility of such conversion although not normally by a mental-mechanical process!


If the response of the imaginary receiver is broadened to cover the entire bandwidth of $150 \mathrm{kc} / \mathrm{s}$ a frequency meter scaled as in Fig. 1 can indicate the deviations directly without knob-twiddling. Now we watch the pointer go through the same change of plus and minus $30 \mathrm{kc} / \mathrm{s}$ five times in one second. If the pointer had a pen over a moving band of paper the five cycles would be recorded as in Fig. 2.

Rolling the paper back for one further imaginary experiment we find that the deviations are much wider-the pointer swings $60 \mathrm{kc} / \mathrm{s}$ each way instead of $30 \mathrm{kc} / \mathrm{s}$-but still at the same rate of five cycles per second. These are drawn in broken line in Fig. 2.

From all this it is clear that the rate of change

Fig. 1: You can follow the explanation of frequency deviation with this diagram.


Fig. 2 (above): Carrier frequency deviations converted into modulation wave form.
Fig. 3 (below): Slope of LC circuit produces amplitude modulation from frequency modulated carrier.

of carrier frequency is the modulation frequency (five cycles per second in our slow-motion picture. audio frequencies in reality) while the amount of deviation represents the amplitude. Unlike the a.m. signal, frequency modulation does not transmit real amplitude changes ready-made. It represents them, it provides their patterns, it supplies signal designs from which the receiver must recreate the amplitude changes of audio tones. There must be built into the receiver some means of "knowing" what the frequencies "mean", some way of recognising that it must supply amplitude changes of voltage or current as instructed by the swinging carrier.

A tuned LC circuit does "know" this, for it is inherently frequency-sensitive, having a response that is maximum at the resonant frequency but falls away gradually to frequencies on either side. Fig. 3 shows one side of the kind of response we would like to have. A carrier arriving with constant amplitude will suffer varying losses as its frequency swings between the resonant peak and the point of lowest response, and will therefore
emerge with an amplitudo modulation. An ordinary $d \mathrm{~m}$. detector will then demodulate the amplitude changes and lose the residual (and now unwanted) f.m. content in its r.f. filter.

This arrangement, the "slope" detector is merely a mis-tuned a.m. circuit. The straight slope of Fig. 3 is not attainable in practice and the normal curve brings serious distortion. For this reason, and because the degree of off-tuning is critical, the arrangement is rarely used.

If we broaden the response of a tuned transformer sutficiently it will no longer be frequencysensitive within the flat bandwidth and will therefore fail to act as a slope detector. It will, however, be phase sensitive.

There is some difficulty in describing the action of phase discriminators without assuming the reader is familiar with the nature and effects of phase relationships. The subject is worthy of an article to itself but for the present we must settle for the statement that phase means the positions of a.c. cycles in time. For example, two trains of cycles may have the same frequency but the cycles of one may commence earlier or later than those of the other. Their result would depend on the amount (expressed in angular degrees) of "lead" or "lag".

The Foster-Seeley discriminator works by comparison of a signal after it has passed through two routes. of which one introduces phase shift and the other does not. In Fig. 4 the direct route via capacitor C1 produces no phase shift. The transformer secondary conducts it equally to the diodes for rectification and it appears in opposition across the total load R1 R2. In the absence of aid or opposition from elsewhere the two outputs would cancel.

In addition to this reference the signal also arrives via the tuned transformer with changes of phase dependent upon frequency. At the central. resonant frequency it is a quarter of a cycle ahead of the reference signal at one diode-it leads by


Fig. 4: Foster-Seeley discriminator.
$90^{\circ}$-and at the other it lags by $90^{\circ}$. It can be shown by vector diagram that this combination in exact quadrature produces diode inputs greater than those of the reference signal alone, but they are still equal and therefore the diode outputs still cancel. This condition exists only for the resonant frequency:At all other frequencies the phase of the tuned transformer signal changes increasing the angle at one diode input and decreasing it equally at the other. The balance that produced equal aid to the reference signal is now disturbed and the total signal is now shared unequally between the two diodes. The rectifier outputs cannot cancel but must leave a difference. This difference voltage. varying as changing phase angles bring changing unbalance, is the a.f. signal.

The circuit is sensitive to amplitude modulation (which for practical purposes includes interference) and must therefore be preceded by a limiter. This is usually an over-driven i.f. stage which clips the tops and bottoms of the carrier waves to a uniforrn level, removing interference "spikes" in the same process.
This additional stage can be eliminated by rearranging the circuit to make the diodes serve the dual roles of rectifiers and dynamic limiters. Fig. 5 shows a simple version of the ratio detector, the most popular system today. Although the reference signal is derived from the tertiary transformer winding instead of via a capacitor the signal conditions are much the same as in the Foster-Seeley circuit as far as the rectifiers. The diodes, you will notice, are connected to make their outputs additive across the load instead of subtractive. As the unbalance produced by phase shifts brings an increased input to one diode and an exactly corresponding decrease to the other the sum of the two outputs is always the same. The difference voltage is therefore due to the changing ratios by which the diodes contribute their shares to the total sum, and can be taken as an a.f. signal across either of the capacitors C2 C3 or either of the resistors R1 R2.

We have established the total diode-to-diode voltage as being (ideally) constant, and it can be



Fig. 6: Pulse-counter discriminator.
stabilised by a large capacitor C4, which charges to a level set by the average carrier amplitude and also absorbs some of the spurious signals that may be riding above the carrier. The diodes are tied to this steady bias and variations of carrier strength (and these include interference that "lifts" the carrier level) change the working points, varying their resistance inversely with the changes of carrier level. The diode resistance damps the tuned circuit, therefore a rise of carrier amplitude is countered by heavier damping and is unable to attain more than about $15 \%$ of its true worth.

The ratio detector is now seen to be a phase discriminator in which unbalanced diode output resulting from the phase shifts of frequency deviations in a tuned transformer provide an a.f. signal by their voltage differences and, by their sum voltage, a bias that enables the diodes to serve also as dynamic limiters. Although limiting is less effective than that of a separate stage it is adequate for most ordinary needs, and is achieved with economy.

Both discriminators depend upon accurate alignment of tuned transformers and upon the maintenance of this alignment once it has been attained. The conversion of frequency deviations to phase-shifts, thence to diode unbalance and difference voltages is reasonably accurate and distortion is variously claimed as being between $1 \%$ and $3 \%$, which is below the standard required for transmitter monitoring and certain other high quality needs. For such purposes there is a system which gives a more direct and linear conversion of frequency deviations to a.f. voltages. The system is aperiodic-it has no tuned network-therefore the alignment problem does not exist and there is no long-term deterioration of the performance.

The receiver gives each carrier cycle a fixed value and adds them to obtain an output that is continuously proportional to their number. At the higher deviations the number of carrier cycles per given small period of time is obviously larger than the number arriving with the lower deviations and in an additive circuit these varying numbers of cycles will produce varying voltages. These constitute the a.f. signal. To give each cycle the same value regardless of frequency the carrier (i.e., i.f.) sine waves are converted into pulses, and this can be achieved in a simple overdriven limiter stage. In Fig. 6 clipped waves from the preceding limiter are passed through the differentiator network C1 R1 through diode DI which passes pulses of one

Fig. 5: Ratio detector.

# onthe <br> Short Weves MONTHLY NEWS FOR DX LISTENERS 

All times are in G.M.T.

All frequencies are in $\mathrm{kc} / \mathrm{s}$.

## The Broadcast Bands-by John Guttridge

0N November 7 most international stations introduced their winter schedules. Details of some of these are amongst this month's information.

Japan: Nippon Hoso Kyokai (Radio Japan, Tokyo) is using new frequencies for some General Service transmissions in English and Japanese. Between 1200 and $17309,505 / 9,560 / 11,815$ are used. The 1800 and 1900 transmissions are on $9,505 / 9,560 / 9,605$. From 2000-2030 9,560/9,605/15,195 are used.

Philippines: Far East Broadcasting Co. (Box 2041, Manila) replaced 15,385 by 11,850 for the 2330- 0100 section of its English transmission on December 1. This transmission is also carried on 17,810 . Other portions of the English service with new frequencies are $0830-09009,715 / 11,920 / 15,440 / 15,300 / 17,810$ and 0900-1145 15,440/17,810. Full QSL.

Ryukyu Islands: Voice of America relay on Okinawa, can be heard in London until 1600 on 7,235 in Chinese. Station identification is given at 1600 in English.
Australia: Radio Australia (P.O. Box 428G, G.P.O., Melbourne) now transmits in English to British 1sles from 0815-0915 on 9,570/11,710.

Canada: Canadian Broadcasting Corporation (P.O. Box 6000, Montreal) now uses $15,320 / 11,720$ for the 1055-1315 segment of its European Service.
U.S.A.: Voice of America (U.S. Information Agency, 330 Independence Avenue, S.W., Washington 25, D.C.) now has following European English schedule: On 1,196 Munich 0400 0430, 0500-0730, 1600-1830, 2200-2345; 3,980 Munich 0300-0700, 1400-2345; 5,965 Tangier, 5,995 Greenville, 7,200 BBC and $7,2500300-0730 ; 5,995$ Tangier $1630-$ 2245; 6,040 0500-0730; 7,205 Thessaloniki 15002300; 9;540/9,740 0430—0730; 9,760 1430-2245; 9,565/9,710 1900-2245; 11,760 1800-2215; 15,205 Greenville 1400-2215; 15,290 Tangier 1400-1800; 15,295 0600-0730; 17.780 Greenville 1400-1800.

Radio New York Worldwide (4 West 58th Street, New York City 19, N.Y.) has following new English schedule: $1200-140015,290$ or $15,295 / 17,710$ (plus 15,385 Saturdays and Sundays); 1400-1500 17,845/ 15,440 (plus 15,385 Saturdays and Sundays); 1500$190017,845 / 15,440 / 17,730 ; 1900-200015,440 / 11,970 /$ $17,845 / 17,730 ; \quad 2000-2100 \quad 15,440 / 11,970 / 11.880 /$ 17,730: 2100-2145 11,970/9,740 or 9,570/11,880/ $17,730 / 15,440 ; 2145-22009,740$ or $9,570 / 11,725$ or 11,790. A new QSL card is now being issued. The Dx programme is now at 1330 and 2130 on Saturdays.

Cuba: Radio Habana (Apt. Postal 7026, Habana) transmits to Europe in English from 2010-2040 on 11,735.

Mexico: Radiodiffusora Comerciales (Quemada 40, Col. Narvarte), can be heard during the evening over

XEWW on 15,110 with interference from Radio Iran on 15, 112 .

Netherlands Antilles: Trans World Radio (Bonaire), has been heard with English test transmissions at 0140 on 11,$825 ; 1430$ on 11,820 and 1825 on 15,180 .

Brazil: Radio Farroupilha (Rua Vigario José Inacio 263, Porto Alegre, Rio Grande do Sul) has been heard as early as 1900 with excellent signal over ZYU60 on 15,335 .

Austria: Osterreichischen Rundfunk (Wien IV, Argentinierstrasse 30a) transmits to Europe from $0500-2200$ on 6,$155 ; 0900-19007,245$; and 06001700 on 9,770.

Bulgaria: Radio Sofia (Sofia) has an English transmission to Africa from 1905-1930 on 11,715/15,320.

Denmark: Radio Denmark (Shortwave Department, Radio House, Copenhagen $V$ ) has now returned to 15,165 for its transmission from 0900-1000.

France: O.R.T.F. (116 Avenue du Président Kennedy, Paris 16) has English for the U.K., Monday-Saturday on 6,175 at 2000-2015.

Germany: Deutsche Welle (Bruederstrasse 1, Postfach 344, $5 \mathrm{Köln}$ ) has now brought its Kigali, Rwanda, 250 kW relay into full service. English transmissions are 0630-0715 on 11,905; 1215-1300 17,765; 1745-1830 17,805; 0430-05006,045; 101510459,$735 ; 1545-16159,695$. The new schedule for English programmes transmitted from Julich, Germany, is $0300-03405,980 / 7,175$ : 0845-0940 17,845/ $11,925 / 15,275$; $2110-2200$ ' $5,980 / 7,175$; $1550-1620$ 7.175/9,735; 0645-0715 9,605/11,785/15,275; 10151030 11,930/15,280/17,870; 1555-1630 9,610/11,890; $0130-02506,075 / 9,640 ; 0500-0540$ 6,145/9,735: 1510-1550 9,545/9,640/11,795. A new QSL card is being issued.

Greece: Radio Athens (Mourozi Street 16, Athens) may be heard on 9,605 during its 1030-1300 transmission except for 1045-1100 when there is a special transcription broadcast for North America on this channel from Deutsche Welle. Although all prom grammes from Athens are in Greek, the station (a rare catch) may be identified by its flute and bel interval signal.

Holland: Radio Nederland Wereldomroep, P.O.B. 222, Hilversum, how has six English transmissions (daily except Sundays). Details are 0730-0820 9,715/ 11,730/11,790 and 19m.b.; 1430-1520 17,810/15,425 6,$020 ; 1900-1950$ 9,590/6,020 and $25 \mathrm{~m} . \mathrm{b} . ; 2000-$ 2050 19,25 and $31 \mathrm{~m} . \mathrm{b}$. and 6,$020 ; 2100-2150$ 9,590/6,085; 0130-0220 9,600 (Bonaire relay). Happy Station programmes on Sunday are 0600-0720 $11,730,9,715 ; 0730-08509,525 / 11,970$ and 19 m. b.; $1030-1150$ 9,710/5,980/6,020; 1430-1550 17,810/ $15,425 / 6,020$; $1800-172019$ and $25 \mathrm{~m} . \mathrm{b} . ; 1900-$
 $25,31 \mathrm{~m} .6 . ; 2200-2320$ i $5,220 / 9,715$.

Portugal: Radio Lishon (Rua Sao Marcal IA, Lisbon) has the following new English transmissions 0300-0345 5,975; 0730-0815 and 0815-0900 7,130/9,645; 2015-2100 6,025/7,225.

Switzerland: S.B.C. ( 3000 Berne 16) has completely new schedule. English to the U.K. is now at I145-

1315 on $9,665 / 11,865$. Full details of the other English transmissions will be given next month.

Thanks this month go to John Sawyers (ilford), J. W. Smith (Anstruther), Roy Patrick (Derby). Brian Burling (Rotherham), R, J. S. Gilchrist (E3rstol). Radio New York Worldwide, S.B.C.. and the International Short Wave Club.

## The Amateur Bands-by David Gibson G3JDG

ANOTHER excellent month for the DX fans. especially on the h.f. bands. Twenty-one " megs" has opened with a real vengeance at times and the majority of logs received this month were for this band.

Yours truly was operating in the "Jamboree on the Air" event using the call G3GJX/A from Leverstock Green, At 0700 hours $21 \mathrm{Mc} / \mathrm{s}$ proved a hive of industry and no trouble was experienced in raising JA stations in Tokyo and Osaka. It must be confessed that this was with 400 W p.e.p. of s.s.b. to a two-band cubical quad.

My best on 20 m from the home QTH was VK3ATN. Imagine my feelings when an s.w.l.'s report contained the same call-only the s.w.l. was using a t.r.f.! Brethren I am choked.

If you hear 3A2DA then you are listening to a pirate. Geoff Haynes, the real 3A2DA, would like any reports on this call. -Time, band, etc. Greoff's address is Sans Nom, Fir Tree Road, Leatherhead, Surrey.

## The L.F. Bands

Eighty looks very promising for the winter months. James Brown (Llandaff), 19 set, a.t.1. dipole, reports hearing some 20 W stations and 23 VE's, including VEØMS//MM (Baffin Is.). Others heard include K2GO, UA2KAN, ZB2AO. ZD8HL, 4X4AS. 7X2AH. Peter Hickey (Pinner), t.r.f. hooked K2KPM, K8HIR, TI2IO (Costa Rica), VEIIE. W-2ZPO. 3WJO. 3WPG, 4BW, YV5BMR ZL2BCG, ZL4LM, ail around $0600^{\circ}$ hours G.M.T. A4238. QTH unknown: RX107+ PR30, 132ft long wire running SE/NW, DL, EA, HA5. HB9, HV1 (Vatican City). LX1. LZ, OH, OK, ON, SM, VE, VO, W4/P, YU, YV, 4U1, all on sideband. D. M. Howarth (Bolton). PCR3. 20 ft vertical on $7 \mathrm{Mc} / \mathrm{s}$, DJ, LA5. OK. ON. PAØ. plus two nice ones. SV1CC, VK5V4.

## $14 \mathrm{Mc} / \mathrm{s}$ and Higher

Dennis Goh using a transistor receiver with the P.W. add on b.f.o. raised DU, JA. KA. KG6. VK. VS6. VS9, XW8. 9M6. Not DX to him because Dennis is in Singapore. Chris Freeman (Nuthall). $\mathrm{HE} 80+\mathrm{PR} 30$, a.t.u. ground plane. CN8. FM7 (Martinique), FP8 (St. Pierre and Miavelon), KG4. LA2/MM. OD5, UI8, VK3, VK4, VP7. YS1. ZD8. 4X4, 5Z4. Dave Hidmore (Belper). HE40, dipole. CN8, CR4, CR6. EP2, FG7. HI8. HK, IØ. K7/VO2, KZ5. LU. OD. PY-1. 2. 5. 7. SVØ. TG9 (Guatemala), VP6, VP9, XE, YV3, ZB. All these logs are for 20 and the last $14 \mathrm{Mc} / \mathrm{s}$ report comes
from Bernard Hughes (Worcester), $840 \mathrm{C}+\mathrm{Codar}$ preselector, dipole, KL7. K X6 (Marshall [5.), MP4 SVQ, UA9, VP9, VK-2, 3. 4. YV. ZL. Stephen Beal (Muswell Hill). P.W.. May, i964. t.r.f. 66 ft long wire, $21 \mathrm{Mc} / \mathrm{s}$. AP3 (Pakistan), OD, SV, UB, VE, VP2 (St. Vincent), K1,W-1, 2, 3, ZB2, 4X4. S. Barnes (Newthorpe), PCR2, 30ft long wire, W-1. 2. 3. 4. 8. 9. K-2. 4. WA. WB, 4X4. A. Smith (Highbury Barn). HE30, Joystick, G3, Ki OD5. UA3.VE3, W-1, 3, 8, 9, Ø. 6W8 (Senegal).

## 28Mc/s

Paul Baker (Pontypool). HE30, 45ft long wire plus 14 ft whip, CR6CZ. CR7FR. DJ, DL, GW5XN, Il, K2, LUIDAB, SM, SVIDB, W2AZD. ZSIBV, 9G1DM. 9J2DL. R. Ibali (Worksop). SX28 + PR30, 80ft long wire end fed with 35 ft coaxial. CR7FR. CR7IZ. ZSIBV, 7S2CB, ZS2ND. ZS6MM. Christopher Clarke (Farnham), 10 -valve $\mathrm{s} / \mathrm{het}$. 33 ft wire around picture rail. CR7, CT1, DJ, DI., EA. ET3, G's. II 1U. OD5, OE, OH. SV1. UQ2. VK2NN. W1, YV5, ZC4, 7S1, 5A1. 7X2. 9J2, all a.m. or s.s.b.

## In General

Listen to the low end of 160 for W1BB/1. On 20 m phone KW6 (Wake Is.). KM6 (Midway Is.), KJ6 (Johnson Is.). KR6 (Okinawa). all very active. $\mathrm{K} / \mathrm{ZBR} / \mathrm{MM}$ is the U.S.S. Calcaterra cruising around the Antarctic, whilst a VK9 is reported operating from Papua Territory.

One piece of news perhaps not generally known is the RSGB news bulletin broadcast on Sunday mornings. The London area has a transmission on $3.6 \mathrm{Mc} / \mathrm{s}$ at 0930 hours.

The Severn area at 1000. Belfast 1015. North Midlands 1030. North West England 1100, South West Scotland 1130, North East Scotland 1200. All these on $3.6 \mathrm{Mc} / \mathrm{s}$.

For the two metre enthusiasts the news is also broadcast on Sunday mornings as follows:$145 \cdot 1 \mathrm{Mc} / \mathrm{s} 0930$ beaming North from London. $145.1 \mathrm{Mc} / \mathrm{s}$ beaming West from London. $145.8 \mathrm{Mc} / \mathrm{s}$ 1015 beaming South from Belfast. $145 \cdot 3 \mathrm{Mc} / \mathrm{s} 1030$ beaming North West from Sutton Coldfield. $145 \cdot 3 \mathrm{Mc} / \mathrm{s} 1100$ beaming South West from Sutton Coldfield. $145 \cdot 5 \mathrm{Mc} / \mathrm{s} 1130$ beaming North from Leeds. $145 \cdot 5 \mathrm{Mc} / \mathrm{s} 1200$ beaming East from Leeds.

That's it for this year. Thanks to all who sent in logs. Please keep them coming. Best 73, Mri Christmas es cuagn next year.

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Use of whips or very short wires.
Increased signal strength and proper loading are often a matter of securing an impedance match between aerial or feeder and receiver or between transmitter and aerial or feeder. This is easily arranged for the impedances likely to be encountered.

Reduction of harmonic output may be incidental with the use of the tuner for other purposes or may be sought to alleviate television interference. Transformation from unbalanced to balanced feeders is necessary when working a transmitter pi-output into balanced feeders-ihat is, open wire tuned or untuned lines and $300 \Omega$, $75 \Omega$ and similar twin-lead feeders. The balanced system may also reduce TV1 or BCl . The change from twin balanced feeders to coaxial feeder may also be needed for best working of a receiver not having twin or dipole aerial sockets.

For multi-band working with the usual types of aerial a tuner is almost essential. It allows best results from a simple wire.

As the tuner of ten matches impedances ( $Z$ ) it is sometimes called a Z-match. In general any tuner can be made to perform satisfactorily with any aerial, receiver and transmitter if the inductance and capacity values are suitable. The construction and components can be varied enormously with no significant change in results.

Fig. 1 shows the method adopted to investigate tuners used with various aerials and transmisters. The transmitters had pi-output (unbalanced


Fig. 1: Equipment to test tuner and coupling efficiency.
coaxial) circuits of usual type. A standing wave bridge indicates what is happening between transmitter and tuner but is otherwise often relatively unimportant. The r.f. meter indicates aerial current. A useful field strength indicator is a pick-up aerial very remote from the transmitting aerial with diode rectifier and giving readings through a long, buried feeder, a microammeter being visible from the operating position.

It was generally found that field strength was the same with any tuner provided it was correctly adjusted. Also that the standing wave ratio on a short coaxial line from the transmitter to the tuner might have no significance from the point of view of maximum radiated signal strength. (This is expected because the transmitter pi-tank can handle high standing waves.) It was also noted that maximum field strength coincided with maximum aerial current through the r.f. meter provided nothing was done to change the feed point impedance. So tuning for maximum aerial current corresponds to tuning for maximum radiated signal strength.

fig. 2: Operating directly from the transmitter.

## Single Wire Feed

The end of the aerial or its downlead is the feed point with an end-fed aerial. In the simplest possible system the aerial is taken directly to the transmitter pi-tank (Fig. 2a). This allows correct loading of the p.a. only. if the aerial presents an impedince within the pi-tank range.

| TABLE |  |  |  |
| :---: | :---: | :---: | :---: |
| Band | Coil | Capacitor | Purpose |
| 160 | 40 turns. 20 swg. $1 \frac{1}{2} \mathrm{in}$. dia. Link 11 tur | 300pF | Fig. 7A, 7B. |
| 80 | 26 turns. 16 swg. <br> $2 \frac{1}{2} \mathrm{in}$. dia. $3 \frac{1}{2} \mathrm{in}$. long. 3 -turn link | $\begin{aligned} & 150 \mathrm{pF} \\ & 150+150 \mathrm{pF} \end{aligned}$ | $\begin{aligned} & \text { Fig. 4, 5A } \\ & \text { Fig. 5B, } 8 \end{aligned}$ |
| 40 | 7 turns each side centre tap of above | 150 or 100 pF $150+150 \mathrm{pF}$ $150+150 \mathrm{pF}$ | $\begin{aligned} & \text { Fig. } 4,5,6 \\ & \text { Fig. } 5 B, 8 \end{aligned}$ |
| 20/15 | 3 turns each side centre tap of above | 100 or 50 pF or $100+100 \mathrm{pF}$ | Fig. 4, 5, 6 |
| 10 | 7 turns. 14 swg . $1 \frac{1}{2} \mathrm{in}$. dia. 2 in . long. Link I or 2 turns | 50pF or $100+100 \mathrm{pF}$ | Fig. 4, 5, 6 |
| 80 | 28 turns. 14 swg. $4 \frac{1}{2} \mathrm{in}$. dia. 4in. long | - | Base loading loft. Whip Fig. 7C |
| $\begin{aligned} & 80 / 40 / \\ & 20 / 15 / \\ & 10 \end{aligned}$ | 26 turns. 18 swg. $2 \frac{1}{2} \mathrm{in}$. dia. $3 \frac{1}{2} \mathrm{in}$. long. Clip tap any turn. | 150 pF optional. | Fig. 28 |
| $\begin{aligned} & 80 / 40 / \\ & 20 / 15 \end{aligned}$ | 30 turns. $265 w g$ enam. side by side. $\frac{3}{4} \mathrm{in}$. dia. Tapped at 3, 5, 7, 12 and 20 turns. | 150 pF | Receiver only Fig. 4, 5, 7B |
| $\begin{aligned} & 80 / 40 / \\ & 20 / 15 / \\ & 10 \end{aligned}$ | 30 turns. 14 swg. <br> 2立in. dia. Clip tap any turn | Optional in parallel, 150 pF for $80,50 \mathrm{pF}$ for $40 / 10$ | Whip or short wire. Fig. 5A, 7C |
| 80/40 | 30 turns, 14 swg . 4 in . dia. $5 \frac{1}{2} \mathrm{in}$. long. Tapped 7 turns each side centre | $\begin{aligned} & 200+200 \mathrm{pF} \text { or } \\ & 100 \mathrm{pF} \end{aligned}$ | Fig. 5, 6 |
| 20/15 | 14 turns. 14 swg . 2in. dia. 3in. long. Tapped 4 turns each side centre | . $100+100 \mathrm{pF}$ or 50pF | Fig. 5, 6 |

If the aerial is resonant at the working frequency the impedance is resistive because current and voltage are in phase. The impedance $\mathbf{Z}=\mathrm{V} / \mathrm{I}$ (voltage divided by current). Fig. 3 shows the distribution of current and voltage on a $\lambda / 2$ (half-wave) aerial. At each end current is small and voltage high. At the centre current is large and voltage small. Therefore the end impedance is high and the centre impedance is low. Typically the end impedance may be some thousands of ohms while the centre impedance is about 70n. If the aerial is a $\lambda / 2$-wave fed at $X$, the feed impedance into which the pi-tank must operate is high. If the aerial is $\lambda / 2$ and the feed point is Y , then the impedance is low. At interme-


Fig. 3: Distributian of current and voltoge on an aerial.
diate lengths such as $\mathbf{Z}$ the impedance has some intermediate value.
When the aerial is not resonant at the working frequency its feed point has capacitive or inductive reactance. If the reactance and impedance values fall within the range of the pitank, then the transmitter can be loaded directly into the aerial, Fig. 2a.
The usual pi-output circuit can be adjusted to work into impedances from about 50 to 300 or 500』, actual limits depending on component values. Therefore a transmitter will quite often work into a random length of wire. If the impedance falls outside the range of the pi-tank. the transmitter cannot be loaded correctly, and if the feed impedance is high the voltage across VC2 is large, and it may spark over, especially on modulation peaks.

If difficulty arises with a given length, the addition of a loading coil Fig. 2b may cure this. Tappings allow the feed point impedance to be adjusted until the pi-tank can operate into it successfully. The variable capacitor VC3 (additional to aerial capacity) is optional. It allows fine adjustment with few tappings, coil and capacitor forming an $L$ network.

The use of this type of tuner will allow any
ordinary pi-tank to work into any aerial length from a few feet up to long wires which are many multiples of a $\lambda / 2$. It is thus quite a convenient circuit to employ.

## Parallel Tuned Circults

An end-fed aerial or single wire feeder can be worked from a parallel tuned circuit (Fig. 4). LI is a coupling link, usually two or three turns, connected by coaxial feeder to the pi-tank. L2 is tuned to the working frequency by VC1. Point X or point $Y$ is earthed. The aerial tapping is near earth on L2 for low impedances and far from earth (near the coil top) for high impedances. Almost any impedance can be fed, the tapping being moved from the earthed point a turn or so at a time until correct loading is obtained.


Fig. 4: Parallel tuner for end-fed aerials.
Fig. 4 has the advantage that L1 is grounded to the transmitter chassis and the p.a. h.t. can never reach the aerial, even if the anode blocking capacitor failed. L2 tuned by VC1 gives some suppression of harmonics.

The use of a tapped coil, L1 in Fig. 5a, gives similar results. With medium and high power the voltage across VC1 will be very high. Fig. 5 b has the advantage that the voltage across sections of the two-gang capacitor VC2a and VC2b is halved. Point X may be earthed instead of the coil centre tap. If X in Fig. 4 or Fig. 5 b is earthed the link is wound on the centre of the main coil.

With receivers the same circuit can be used. Adjustment is then for maximum signal strength. Where the aerial impedance was a bad match for the receiver input impedance at some frequency the tuner may-increase signal strength some $S$ points at this frequency.

Single wire feeders include the end of Marconi
$(\lambda / 4)$ and end-fed Hertz $(\lambda / 2)$ aerials and the downlead of systems such as the Windom. All random length end-fed aerials also terminate in a single feed point.

## Coaxial to Balanced Feeder

Most transmitters have a coaxial output socket. This can be transformed to balanced feeder by using a tuner as in Fig. 6. L1 and L.2 can be the same as in Fig. 4 or 5 . If the single capacitor VCl in Fig. 4 is used it should be operated through an insulated extension. The two-gang capacitor (Fig. 6) helps to maintain balance.

The twin feeder may be $75 \Omega$ flat twin, $300 \Omega$ flat twin or an open wire line. The coil centre tap Y may be earthed or the capacitor at $X$. The feeder taps are near $Y$ for low impedance and farther from $Y$ for high impedance. With an open wire tuned line having high impedance the feeders may be connected to the ends of the coil.

A $\lambda / 2$ centre-fed dipole can be used in this way with a balanced twin feeder instead of having a coaxial feeder from the pi-tank. Harmonic output is reduced and the balanced system may help avoid TVI.

## Series Tuning

Low-impedance feed points can be handled by tappings near the earthed point of a parallel tuned coil. For very low impedances the tapping becomes critical and may be awkward. So series tuning is then of ten employed.

This is quite popular with a $\lambda / 4$ Marconi and similar short aerials. The capacitor VCl in Fig. 7a is in series with the coil L2. L1 is a coupling link from the transmitter. Using a tap on L2 b gives similar results. The aerial is series tuned against ground and a good earth is required for best results.

It will be seen that the circuits in Figs: 4 and 5 can be used for series tuning by placing the capacitor in series with the main coil. Series tuning is often employed on 160 m where it is impracticable to erect a $\lambda / 2$. Whips and short aerials can be fed by this means. The capacitor may sometimes be omitted, Fig. 7c. The tapping positions are then more critical as there is no other means of adjustment.

When a Zepp or tuned doublet is used and has a low impedance feed point, series tuning is often used (Fig. 8a). The centre tap Y may be earthed. One capacitor is sometimes omitted. Occasionally the coil is divided by cutting the centre turn and a single capacitor is placed here, Fig. 8 (B). This maintains the balanced system with a single capacitor. A coaxial line can also be fed by series tuning (C, Fig. 8).

## Other Circuits

Most tuners are derived from the circuits given. The coil may have tappings for multi-band operation. Tests made with an efficient 80 m coil, tapped for 15 and 20 m , showed no measurable

Fig. 5: Alternative systems of coupling and tuning.


Fig. 6: Coupling to twin feeders.
loss in signal strength compared with a coil wound for 15 and 20 m only.
In any of the circuits a capacitor is sometimes included in series with the link so that the reactance of this may be tuned out.

Various particular circuits are seen and aim to avoid band switching or secure some other advantage. One is shown in Fig. 9a. VC. and VC2 allow series tuning of L.2, VC3 being set at minimum. If parallel tuning is required VC3 is used. Another circuit is that at B. VC3 and VC4 are in series across L3, L4 being high impedance at this frequency. When the frequency is that covered by L4, VC4 is effectively in parallel with VC3, the few turns of L3 having little effect. The aim is to cover two or more bands without switching. In general the circuits shown earlier give at least equivalent results.


Fig. 7 above): Series tuning for Marconi aerials. Fig. 8 (below): Circuits using series tuning.


## Adjustments

For receiving only, adjust ments are directed towards securing the best signal strength. A tuning or signal strength meter should be fitted to the receiver if not present. Adjustments can be


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| :---: | :---: |
| 7 in ，Long play， $1,800 \mathrm{ft}$ ． | 19／8 | 5 in ．Double play， 1,200 t．男哖，Double play，1，800t n．Doable play，2，400ft 3in．Triple play，450ft．（Plain＇white boxes） 8in．Triple play，600ft．（Pisin white boxea） In．Triple play， 900 ft ．（Plain white boxes） Sin．Triple play，1，800ft．（Plain white boxea） in．Triple play， $3,600 f$ ．（Unboxed） in Stand bhie

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on a strong signal in the band, the tuner then being left alone. If tappings are marked or selected with a switch this allows easy resetting for a band in conjunction with a variable capacitor with numbered dial.

The benefit secured from a tuner may be

(a)

(b)
he adlousted for maximum aerial current on the r.f. meter if fitted. If a field strength meter is available this naturally offers a means of tuning up.

It will probably be found that the transmitter pi-tank can be operated into a wide range of impedances which may be available by different adjustments of the tuner. All these may result in a similar radiated signal. though some produce high standing waves on a coaxial line from transmitter to tuner. If this line is short losses are negligible and the tramomitter pi-tank can return the reflected power as if operating directly into an aerial. On these grounds the presence of a low standing wave ratio in the position in Fig. 1 indicates power is flowing from the transmitter to the tuner and aerial; but a high standing wave ratio does not mean there is necessarily any measurable loss in radiated signal strength.
The readings of the r.f. meter will depend on frequency, aerial and power and will thus change from one band to another or if modifications are made to the aerial-earth system. However, the meter is useful to check that usual output is obtained and because more current here corresponds to more power radiated provided frequency and aerial-earth system are unchanged.

With average wire aerials the length in feet for a $\lambda / 2$ at any particular frequency is:

$$
\begin{gathered}
468 \\
\hline \mathrm{Mc} / \mathrm{s} .
\end{gathered}
$$

The length for a $\lambda / 4$ is:
234
$\overline{\mathrm{Mc}} / \mathrm{s}$.
It is thus easy to calculate the length needed for a $\lambda / 2$ or $\lambda / 4$ aerial for any band.

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## A Transistorised L.C.R. Bridge - Part Two By Mike Fisher

CONSTRUCTION of the basic bridge circuitry is quite straightforward but care should be taken to keep the connecting leads fairly short and a reasonably heavy gauge wire should be used. The inevitable resistance of the circuit wiring will necessitate the adjustment of the $1 \Omega$ standard resistor on test. The $0.1 \mu \mathrm{~F}$ standard capacitor will be difficult to obtain to a high standard of accuracy but this snag can be overcome by using a normal type of component and adjusting its value by wiring additional capacitors in parallel on test. The procedure for adjusting these two
components is as follows:
$1 \Omega$ resistor. Build the complete bridge unit and calibrate the main balance control by its resistance against a suitable test instrument. If no test instrument is available the dial can be set up by placing $1 \%$ test resistors across the " $X$ " terminals and adjusting the bridge to balance. The scale is then marked at the balance point with the appropriate value. This calibration is best carried out on the $0-1,000 \Omega$ to $0-100 \mathrm{k} \Omega$ ranges. When the dial calibration is complete connect a $1 \%$ or better resistor of value between 2 and $10 \Omega$ across


Fig. 10: Circuit diagram of the complete unit.


Fig. I: : Component layout of Veroboard circuit.
the "X" terminals, set the range switch to the $0-10 \Omega$ range and set the dial to the point at which balance should be obtained. The value of the $1 \Omega$ standard resistor is then adjusted until a true balance is obtained at this point.
$0 \cdot 1 \mu F$ standard capacitor. A close-tolerance test capacitor, preferably of either 0.05 or $0.005 \mu \mathrm{~F}$ value, is connected across the " $X$ " terminals and the instrument switched to the required range. The dial is set to the point at which balance should be obtained, as above, and the standard capacitor is then adjusted until a balance is obtained at this point. Calibration, etc., is now complete.

The detector circuit. Component values and layout are not critical. OC7I transistors were used for the simple reason that they were at hand but it will probably be found that OC70, etc., types will work quite well in the circuit.

The oscillator circuit. Considerable variation of component values and working voltages is permissible with this circuit: it will continue to function at voltages of less than 1.5 V .

The ratio of the transformer seems to be of little real importance. 3:1 ratio was used on the test circuit but it was found that a far too powerful feedback signal resulted and the $470 \mathrm{k} \Omega$ resistor to the base of the transistor had to be introduced to stop squegging which resulted. The
value of this resistor should be adjusted as follows to suit the particular transformer used (it will probably be found that the circuit will still work even if $d$ transformer with a ratio of $40: 1$ is used).

Wire up the circuit, leaving the $470 \mathrm{k} \Omega$ resistor shorted out, and connect the $0.05 \mu \mathrm{~F}$ capacitor across the transformer primary (connected as the collector load). A pair of headphones is now connected via a blocking capacitor to the transistor collector and the negative rail. A strong audio signal should be heard. This signal will probably seem to be fairly pure in tone but this may be a delusion caused by the high volume level. The tone frequency should be about $1 \mathrm{kc} / \mathrm{s}$; if not the frequency may be adjusted by changing the value of the capacitor in parallel with the primary winding. When this adjustment has been completed a fairly high value resistor should be connected in series with the phones, resulting in a very low volume level to them. It will probably be found that at this low level the frequency of the signal seems to be considerably different from that formerly heard: in fact it may even sound like a motor-boat running at low speed. This is symptomatic of "squegging", caused by too high a feedback factor. The short across the $470 \mathrm{k} \Omega$ resistor should now be removed. Should oscillation now cease completely reduce the value of the resistor until oscillation starts again. The resistor effec-
tively reduces the magnitude of feedback and it will be found that as the resistor value is increased so the squegging frequently rises until. finally, when the correct degree of feedback has been obtained, only the pure tone of the oscillator will remain. It may be necessary to readjust the frequency of oscillation during the setting up.

If it is found to be necessary to use a very high value of R4, such as the $470 \mathrm{k} \Omega$ shown in Fig. 7, it will be found that the base bias chain, R1 and R2, will have no effect on circuit operation. R1 and R2 can therefore be removed from the circuit. Inspection of the waveform on a scope will show, in the above case, that distortion is taking place; as long as squegging is not taking place, however, the oscillator may still be used to energise the bridge.

It is felt that ideally the transformer T 1 should have a ratio of about $20: 1$ if a pure sinewave is to be obtained from the circuit.

It should be noted that if the above adjustments are not made poor detector response and faulty balance reading may be obtained.

A suitable front panel layout for the instrument is shown in the heading and the final circuit of the complete instrument.

## Components List

The $50 \mu \mathrm{~A}$ meter is available from Radio and TV Components (Acton) Ltd., price 25 s .

If difficulty is experienced in obtaining S1, the two-pole, seven-way switch, an alternative would be a two-pole, ten-way type modified as follows: Drill and tap a 6BA hole in the switch front plate in such a position as to fall between the seventh and eighth position locator recesses. A. short 6BA screw can then be inserted in the hole and will act as a stop, reducing the number of a vailable switch positions to seven.

S2 the seven-pole three-way switch, may be adapted in similar fashion from an eight-pole, four-way switch, available from Radio Component Specialists, of 337 Whitehorse Road, West Croydon, price 6 s . 6d. Alternatively a Wearite 12 -pole, three-way switch, price 7s. 6d. may be. used with the five unwanted poles left blank. This switch can be obtained from L. Wilkinson (Croydon) Lid., Longley House, Langley Road, Croydon, Surrey.


Fig. 12 (above): General layout of metalwork.

Fig. 13 (below): Wiring diagram of front panel etc.



Fig. 14: Wiring of S2 (mode).
Fig. 15: Wiring of SI (range).


| Position of <br> SI (Fig. 10) | Range |  |  | R |
| :---: | :--- | :--- | :---: | :---: |
| 1 | $0-100 \mu \mathrm{H}$ | $0-100 \mu \mathrm{~F}$ |  |  |
| 2 | $0-1 \mathrm{HH}$ | $0-10 \Omega$ |  |  |
| 3 | $0-10 \mathrm{mH}$ | $0-10 \mu \mathrm{~F}$ |  |  |
| 4 | $0-100 \mathrm{mH}$ | $0-1 \mu \mathrm{~F}$ |  |  |
| 5 | $0-0.1 \mu \mathrm{~F}$ | $0-1 \mathrm{k} \Omega$ |  |  |
| 5 | $0-1 \mathrm{H}$ | $0-0.01 \mu \mathrm{~F}$ |  |  |
| 6 | $0-10 \mathrm{H}$ | $0-100 \mathrm{k} \Omega$ |  |  |
| 7 | $1-100 \mathrm{H}$ | $0-1000 \mathrm{pF}$ |  |  |

## Front Panel and Chassis Assembly

The prototype instrument was designed, from the mechanical point of view, to fit into an instrument case that was available at the time and no effort was made to miniaturise. While it is unlikely that the same mechanical dimensions will be used in any instrument built by the reader the general constructional details used in the proto-

| COMPONENTS LIST |  |  |  |
| :---: | :---: | :---: | :---: |
| Resistors |  |  |  |
| RI | 10k $\Omega$ 10\% |  | $1 \Omega$ |
| R2 | $1.5 \mathrm{k} \Omega 10 \%$ |  | $10 \Omega$ |
| R3 | $1.2 \mathrm{k} \Omega 10 \%$ |  | $100 \Omega$ |
| R4 | $470 \mathrm{k} \Omega$ see text |  | 1k $\Omega$ |
| R5 | $15 \mathrm{k} \Omega 10 \%$ | R15 | $10 \mathrm{k} \Omega\}^{\text {see text }}$ |
| R6 | $15 \mathrm{k} \Omega 10 \%$ |  | $100 \mathrm{k} \Omega$ |
| R7 | $1.2 \mathrm{k} \Omega 10 \%$ |  | $1 M \Omega$ |
| R8 | $1.2 \mathrm{k} \Omega 10 \%$ |  | 100s2 |
| R9 | 390 $10 \%$ |  | $9 \mathrm{k} \Omega 10 \%$ |
| $R 10$ | 4.7k $20 \%$ |  |  |
| All re | esistors $\frac{1}{\text { d }} \mathrm{W}$ minim |  |  |
| Potentiometers: |  |  |  |
| VRI Ik $\mathbf{w} / \mathbf{w}$ linear 1\% $\%$ large diam |  |  |  |
|  |  |  |  |
|  | 10k $\Omega$ Carbon Li | ear |  |
| Capacitors: |  |  |  |
| CI $0.05 \mu \mathrm{~F}$ (see text) |  |  |  |
| $\mathrm{C}^{\text {2 }}$ 2014 F |  |  |  |
| C3 | $0.1 \mu \mathrm{~F} 1 \%$ (see te |  |  |
| Semiconductors: |  |  |  |
|  |  | DI |  |
| Tr2 |  | D2 | Any |
| Tr3 | Red Spot, |  | Germanium |
| Tr4 | OC71, etc. | D4 | Diode |
| Tr5 |  |  |  |
| Miscellaneous: |  |  |  |
| T1 20:1 to 3:1 (see text) |  |  |  |
| T2 1:1 Veroboard |  |  |  |
| SI 2P 7W $3 \frac{1}{4} \times \mathrm{lin}$. |  |  |  |
| S2-7P 3W |  |  |  |
| S3 IP 2W self return |  |  |  |
| S4 2P 2W |  |  |  |
| MI $0-50 \mu \mathrm{~A}$ |  |  |  |
|  |  |  |  |
|  |  |  |  |

type may be of interest.
The dimensions of the front panel are $11 \frac{1}{4} \mathbf{x}$ $6 \frac{7}{8} \mathrm{in}$. This panel may be cut from sheet aluminium, plywood or hardboard.

The two side members are cut from aluminium, and bolted to the front panel as shown in Fig. 12. The securing screws should be countersunk flush into the front panel. The right-hand side member has the meter bolted to it as shown. Clinch nuts are secured to the rear flanges of the side members and holes cut in the rear of the case to line up with them; the chassis can then be held secure in the case by screws at the rear, leaving the front panel free from unsightly screws.

Resistors R11 to R17 should be soldered directly to the contacts of switch S1.

## HIGH WATTAGE LOADS

by C. L. Jones, B.Sc.

THE most common types of resistors used in electronics are designed to dissipate a comparatively small quantity of energy. Occasionally higher voltage components are required, for example as "loads" when testing equipment. The problem resolves itself into two categories-that of comparatively small currents at high voltages and that of high current at low voltages.

## Low Current-High Voltage

The original need for such a load occurred when the voltage-current curve for a power pack of maximum power output, about $30 \mathrm{~W}(300 \mathrm{~V}$ at 100 mA ), was required. A rheostat to cope with this would be expensive and so the circuit given in Fig. 1 was used.


Fig. 1: This circuit eliminates the use of a rheostat. The transformer is optional as heater supplies can be obtained from the tronsformer under test.

Almost any output valve can be used but the original rig employed a 6 L 6 which had been discarded because of a broken spigot. The current taken by the valve is varied by means of R1, the fixed resistor R2 limiting the current when R1 is at minimum.

The values of R1 and R2 will depend on the use to which the circuit is put. R1 limits the current when R2 is at minimum. When assessing the value of R 2 the following points should be borne in mind:
(a) If R2 is too low then the minimum current taken by the valve is high.
(b) If R2 is too high adjustment of the current is difficult, especially when the current is high.

The maximum current for the valve has been exceeded by as much as $50 \%$ but only for short periods. Since valves which are past their best are used the risk is felt to be justified. Readings can be taken very quickly so that prolonged overloading can be avoided.


Fig. 2: The graph obtained by using the circuit of Fig. I.

Fig. 2 shows a graph obtained using the circuit. It could be used to provide data to stabilise the power pack. The power pack in question is used with different pieces of test equipment which are used too infrequently to make it worth while providing each with its own power supply. The test instruments have widely different h.t. requirements and the graph is used to find a suitable resistor to put in series with the supply. Thus each piece of equipment has a built-in h.t. dropper and a decoupling capacitor which enables it to be phigged directly into the power pack and provides additional smoothing.
A second unit has been built employing a 6 V 6 to test the regulation of a power pack designed to operate an amplifier and a tuner, the latter being switched off when the amplifier is used for records. The effect of switching one load off or on can be determined by setting $R 2$ so that the valve takes
the same current as the equipment it is simulating. The circuit can be wired up when required or built into a small self-contained unit. The transformer shown in Fig. 1 is optional as heater supplies can be taken from the transformer under test.

Multi-range meters can be used to measure the current and voltage. They provide a "fixed" load; R2 can be adjusted until the milliameter registers the required current, then the meter can be replaced by a "short" across $X$ and $Y$.

Details of R1 and R2 are given below but should only be used as a rough guide as the exact current depends on the h.t. voltage and individual requirements may enable more suitable values to be used. The last two columns were determined using the power pack from which Fig. 2 was drawn.

|  | R 1 | R 2 | Current | Current |
| :---: | :---: | :---: | :---: | :---: |
| 6V6 | $100 \Omega$ | 10 ks | 6 mA | 130 mA |
| 6 V 6 | $500 \Omega$ | 10 kS | 6 mA | 60 mA |

The maximum power dissipated by $R 2$ in the case of 6 V 6 is just over 1 W . An old standard size (l) $\frac{1}{2}$ in. diameter) wire-wound potentiometer should be used rather than the more modern miniature type.


Fig. 3: Graph showing how resistance of metallic conductors increases with rise in temperature.

## High Current-Low Voltage

Testing power amplifiers can be a noisy business if the outputs are fed into a loudspeaker, so that dummy loads are required if the family or neighbours are not to be disturbed. Further, if feedback loops are connected the wrong way round sensitive speakers can be damaged, so that some less delicate load is required. Resistors as described below have also been used in series with a power supply when charging small accumulators at a constant current.

There are several different types of "resistance" wire avalable, each with properties suited to


Fig. 4: Method of connecting resistonce wire.
particular applications. Convenient sources of resistance wire are electric fire elements, especially the type obtaned as tight coils, which are then stretched backwards and forwards over a rectangular ceramic former. A 1 kW element of this type is made from about 10 yd of $25 \mathrm{~s} . \mathrm{w} . g$. " nichrome " wire. This is a nickel-chromium alloy which can stand up to high temperatures. The resistance of tha particular gatuge of wire is almost exactly 5!) per yard at room temperature. Thus the length for any particular resistance is easily calculated.

The resistance of metallic conductors increases with increase in. temperature and a sample has been tested to determine the heating effect of current passing through it. The results are shown in Fig. 3. The length of wire can be adjusted to give correct resistance at any particular current. For these tests the wire was kept stretched out horizontally and it should be remembered that if it is coiled tightly heating will increase.


Fig. 5: Method of eliminating "kinks" in wire.

The temperature of the uncoiled wire rises above the melting point of solder with currents as low as 2 A . so that connections are best made as shown in Fig. 4. In any case it is difficult to solder this type of wire. The ends of the wire can be clamped between washers under 4BA brass terminals: these help to dissipate the heat generated in the wire. Large diameter coils should be made and if housed in a container this must have well-ventilated sides.

Resistors made in this way are not "noninductive ", but at low frequencies this should not be much of a problem. The wire may be freed from kinks by looping one turn around the shaft of a large serewdriver and pulling the wire as shown in Fig. 5.


## PUSH—BUTTON MULITMETER

D. FANSHAWE

IWE meter was primarily designed for use in transistor experiments connected with the design of apparatus. It is often required to monitor base and collector currents, and also collector voltage. These three jobs can be done with only one meter provided three switched inputs are available. The total cost of the instrument is around $£ 3$.

## INPUTS

This meter has three pairs of input sockets on the front panel (marked 1,2 and 3) and each input can be selected in turn simply by pressing the appropriate input push button.

The basic meter movement is an ex-government meter of $50 \mu \mathrm{~A}$ f.s.d., available from one of the advertisers in this magazine, price 25 s . The switch-
ing is by push-buttons, three banks of three-way units are used. When the meter is being used as a general purpose multimeter, the test leads can be used in any input; but if it is desired to monitor two currents and a voltage in turn, the current inputs should be plugged into inputs 1 and 2. The voltage input should be plugged into input 3. The reason for this is that inputs 1 and 2 are both short circuited when they are not selected so that the circuit under observation will not be broken. Fig. 2 shows the meter being used in this way.

## RANGES

The meter ranges are: $50 \mu \mathrm{~A} ; 1 \mathrm{~mA}: 25 \mathrm{~mA}$; 500 mA ; (all d.c.). $1 \mathrm{~V} ; 10 \mathrm{~V} ; 50 \mathrm{~V} ; 500 \mathrm{~V}$ (all d.c.). $1 \mathrm{k} \Omega ; 100 \mathrm{k} \Omega ; 10 \mathrm{M} \Omega$.


Fig. I: Complete circuit of the multimeter.


49 m band: During daylight, stations up to about 1,000 miles distant should be well received. During darkness, reception will be excellent for DX stations-in fact during the winter it may be one of the best bands for after-dark reception.

41 m band: Similar to 49 m but noisier-although both bands will suffer interference due to the extensive use of these bands, particularly after dark.

31 m band: This will provide good short distance (up to 1,000 miles) reception during daylight. During darkness, good long distance reception will often be possible, notably during the summer months.
25 m bond: Excellent for daylight reception of stations up to around 2,000 miles. Late afternoons and early evening will produce long distance reception but it may fade out during hours of darkness, particularly in the winter.

19 m band: During hours of daylight this band will produce excellent DX reception from all over the world. Conditions should normally hold up to early evenings, but will then fade out.

16 m bond: Capable of producing strong DX signals, this band is best between autumn and spring during daylight hours but the summer may be relatively bleak.

13 m band: Of little use at present, though the winter may bring a few stations in.
IIm band: Until the sunspot cycle swings back there will be very little activity on this band.

## Station Information

Various lists of short wave broadcasting stations are available, but the most comprehensive is the World Radio TV Handbook, published in Denmark but obtainable in the U.K. through booksellers at 23 s . Od. Apart from a complete listing of stations, it contains notes on programmes, identification and other essential information.

## WHEN AND WHERE TO LISTEN

It is impossible to more than generalise in the space available. Conditions may change from day to day, month to month. Generally speaking, the high frequency bands are best during daylight and the low frequency bands during darkness. In any given year, conditions will vary from season to season,

## LISTENING TO SHORT WAVE STATIONS

The newcomer to the short wave bands may understandably become rather confused; strange jargon, unpredictable reception, and other frustrations. It is not the intention of this pocket guide to present a treatise on the mysteries of the short wave bands but rather to collect in a handy form much of the basic essential data and reference material useful in day-to-day short wave listening.

## The A mateur Bands

Here is a brief summary of what to expect from.the amate ur bands most likely to be tuned by the newcomer:
$1.8 \mathrm{Mc} / \mathrm{s}$ ( 160 metres). "Top Band" is used mainly for local communications between stations up to about 100 miles apart during daylight hours but for British Isles coverage after dark. During winter months, European contacts are possible and under very favourable conditions British stations have worked Transatlantic stations and even the Antipodes.
$3.5 \mathrm{Mc} / \mathrm{s}$ ( 80 metres). This band is favourable for hearing all the British Isles and Europe. During the hours of darkness, particularly in the winter, stations further afield are not uncommon.
$7 \mathrm{Mc} / \mathrm{s}$ ( 40 metres). Much patience is needed in listening on this band due to interference from broadcasting stations and other intruders. Though basically a "local" band, much longer distant reception is possible, notably on morse, and particularly during the winter after darkness.
$14 \mathrm{Mc} / \mathrm{s}$ ( 20 metres). The most popular " DX " band of all. It is open for world-wide reception most of the year, though it sometimes "closes" early in the evening during the winter. Sometimes, according to conditions, European stations are heard at outstanding strength.
$21 \mathrm{Mc} / \mathrm{s}$ ( 15 metres). Potentially a good band for long distance signals, much patience is required. It is best during summer months and when sunspot activity is high. Openings may be of comparatively short duration, but they are often very productive.
$28 \mathrm{Mc} / \mathrm{s}$ ( 10 metres). Much the same as $21 \mathrm{Mc} / \mathrm{s}$. When the band is really "open", stations from all over the world are often heard at remarkable strength; at other times the band may appear to be completely "dead".

General: Space does not permit a comprehensive survey of the various bands but a very good idea of current reception conditions can be obtained from reading the monthly notes On the Short Waves published in each issue of Practical Wireless.
but an influencing factor is the sunspot cycle. Years of high sunspot activity favour the high frequency bands, years of low sunspot activity (we are in a "trough" at the moment) favour the low frequency bands. Thus, whereas the $28 \mathrm{Mc} / \mathrm{s}$ amateur band is relatively poor this year, in several years' time it may be excellent. With these reservations in mind, the following notes should be accepted as a guide to reception. Times in GMT.

## North America/Caribbean

Best times are 1500-2300, peaking in winter around 1800 and in summer around 2030. Western N. America is more difficult but try around $1500-1800$ and breakfast time. Broadcasting stations: 19 m afternoon, 25 m after dark (winter), in summer 19 m band is best. Amateurs: 20 m most reliable throughout the year-East Coast possible all through the day. After dark, 40 and 75 m bands and in winter $1.8 \mathrm{Mc} / \mathrm{s}$.

## Central America

On broadcast bands, try 49 m around dawn, or late night in winter (when the $60,75 \mathrm{~m}$ bands may also be productive). Amateur bands: 20 m is best bet after dark and around dawn.

## South America

Best times are 0900-1100 and 1700-0100. On broadcast bands (except summer) 19 m is best for morning period, 25 and 31 m evenings. Also try the $60-75 \mathrm{~m}$ section. In summer, this area is more difficult to hear- 25 and 31 m is usually best, evenings. Amateur bands: again 20 m and 40 m after dark. Also 15 m early evenings.

## Central/South Africa

Best general times are between 1300-2200. On broadcast bands, 19 m during daylight hours and 25 / 31 m after dark especially during winter. On amateur bands try 20 m around $1700-2000$. Usually good when $28 \mathrm{Mc} / \mathrm{s}$ is "open".

## Asia

For S and SE Asia, best times are $1100-1700$, starting off with 16 and 19 m bands, then 25 m . During winter, the best period may hold till around 2100 on 31 and 41 m bands. For amateurs, 20 m is again about the best bet. Best times for Northern Asia 0600-0900 and again around 2000 . The 19 m and 25 m broadcast bands are best.

## The Antipodes

Peak times are $0600-1000$, with $1400-1700$ and around 2200 during winter. New Zealand is best

## Modes of Operation

The main system used by amateurs is amplitude modulation. The beginner will listen mainly to stations using a.m. telephony ("phone") which is receivable in the normal way on any receiver. However, thousands of stations operate on telegraphy (Morse code, "cw"), because (a) the language barrier is reduced owing to the use of internationally understood codes and abbreviations, and (b) under comparable reception conditions a faint c.w. signal can be copied easily whereas a phone signal would be unintelligible. To receive c.w. signals it is necessary to have a receiver with a beat frequency oscillator (b.f.o.) which heterodynes with the incoming signal, thus making it audible. Much of the more exotic DX is heard on c.w., particularly on the lower frequency bands and the newcomer is urged not to overlook the facilities to receive c.w. stations.
To overcome the severe crowding on the amateur bands, various forms of a.m. single sideband telephony are gaining popularity. To receive such transmissions properly, the receiver should have a product detector. Frequency modulation is also permitted, but is not used extensively.

## the ham language

## Callsigns

For identification purposes, every amateur station has a callsign, issued by the licensing authority. This consists of a prefix (establishing the country of origin) followed by a suffix (establishing personal identity). Sometimes a numeral indicates regional significance; for example-VE2AAA is in Quebec, because VE is the Canadian prefix and 2 is the identification for the Province of Quebec.

The competitive element is strong in both listening and transmitting. Most societies issue certificates for DX achievements-mainly on the basis on the number of countries, counties, "zones", etc. The prefix list on pages $10-13$ is that currently recognised by our national society, the RSGB, for country "scoring" purposes.

## Abbreviations

In order to avoid ambiguity and to save time, the pioneer operators gradually devised a system of codes and abbreviations still used today. These comprise (a) signal reporting systems, (b) the Q Code, (c) general abbreviations. The greatest benefit is felt by c.w. operators who are able to convey intelligent messages to any other station regardless of nationality. In the pages that follow, the basic ingredients of this international "ham language" are outlined.
around $0900-1100$. Summer is poor compared with other seasons. Best broadcast bands are 25 and 31 m in morning, 31 and 41 m in afternoon, and 19 m for evening. For amateurs 20 m is best, though 40 m can be good during winter mornings.

## Pacific Area

A difficult area to hear. Best time is between $0600-1100$ on the 19 and 25 m broadcast bands and 20 m amateur band.

## Europe/North Africa/Near East

Little need to elaborate as it is possible to hear all these areas almost around the clock.

## THE "Q" CODE

One of the ingredients of the "ham language" is the Q Code, adapted from the professional communications code. Each set of symbols can be used as a question or as an answer, or in general context. For example, QTH? means "what is your location?" and QTH London means "my location is in London". An operator may also say, e.g., in conversation: "My QTH is poor for reception". Here are some of the more commonly used Q signals.

| QRA | Full address |
| :--- | :--- |
| QRB | Distance (miles) |
| QRG | Frequency $(\mathrm{kc} / \mathrm{s})$ |
| QRJ | Weak signals |
| QRH | Your frequency varies |
| QRK | Signal strength |
| QRL | Busy |
| QRM | Man-made interference |
| QRN | Atmospheric |
|  | interference; static |
| QRO | High power |
| QRP | Low power |


| QRQ | Send faster |
| :--- | :--- |
| QRS | Send slower |
| QRT | Closed down |
| QRU | Nothing further to say |
| QRV | Ready to operate |
| QRX | Wait |
| QSA | Readability of signal |
| QSB | Fading |
| QSL | Acknowiedgement of <br>  <br>  <br> receipt; confirmation <br> of contact |


| QSO | Contact |
| :--- | :--- |
| QSP | Pass on a message |
| QSV | Send series of V's |
| QSX | Listen for |
| QSY | Change frequency |
| QSZ | Double sendiag |
| QTC | Telegram, mesmage |
| QTH | Location |
| QTR | Time check (exact |
|  | time) |

## QSL Cards

Two stations which have maintained a two-way contact may exchange "QSL" cards. These prominently display the call sign and contain data on the equipment used and confirmation details of the contact. The QSL card is the proof, normally required in claiming certificates.

Short wave listeners may also attempt to obtain QSL cards from transmitting stations by sending reception reports. But whereas in the early days most amateurs welcomed such unsolicited reception reports the fact must be faced that with such high activity on the bands today most amateurs already know how they are getting out and many SWL reports are virtually useless. In fact many stations will not even send cards to stations they have "worked" unless they are specifically requested.

We would therefore advise prospective QSL collectors to concentrate on sending reports mainly to genuinely unusual stations, such as long distant signals on the harder bands ( $1 \cdot 8,3 \cdot 5$ and $7 \mathrm{Mc} / \mathrm{s}$ ). Also, in any case, it is only courtesy to enclose return postage in the form of reply coupons obtainable from any Post Office.

## THE BROADCASTING BANDS

Many broadcasting stations have regular programmes andjor announcements in English; indeed more and more countries are establishing "international" services, with propaganda programmes beamed to all parts of the world. There are, however, a large number of stations which never, or rarely, give English announcements. Some use call signs for identification, though these are being dropped by many broadcasters. Luckily, most of the "local" stations, particularly Latin Americans, still retain the callsign in the prominent station announcements, together with the various station slogans.

Regular readers of Practical Wireless can obtain monthly news of broadcast band happenings in the feature On the Short Waves. The newcomer may, however, find the following summary of the various bands of great use in learning what to expect.

60 and 75 metres: These bands are used almost exclusively for local regional broadcasting. The 60 m band (in fact it ranges from approx. 50.63 m ) is a happy hunting ground for Latin Americans. Between $50-140 \mathrm{~m}$ are several "tropical" bands, used for local broadcasting, and there is something of interest all through this range. Reception should be good on these frequencies for several years (being-as we are in a period of low sunspot activity) and the Latin Americans should be plentiful during hours of darkness, notably during the winter months. Static interference may be troublesome during the summer.

## SIGNAL REPORTING SYSTEMS

Of the various signal codes evolved through the years, the RST system is the only one to have gained universal acceptance.

## Readability:

RI Unreadable
R2 Only just readable, and only occasional words heard
R3 Readable, but with considerable difficuity
R4 Readable with almost no difficulty
R5 Perfectly readable
Signal Strength:
SI Signals only just perceptible

S2 Very weak signals
S3 Weak signals
S4 Fair signals
S5 Fairly good signals
S6 Good signals
S7 Moderately strong signals
S8 Strong signals
S9 Extremely strong signals

## Tone:

TI Extremely rough note
T2 Very rough note

T3 Rough, low pitched note T4 Rather rough note
T5 Musically modulated note T6 Modulated note, slight whistle
T7 Fairly good note, smooth ripple
T8 Good note, slight ripple T9 Pure DC note
(If the note seems to be crystal controlled, an " $x$ " is added, if the note is chirpy, a " $c$ " is added.)

Thus an extremely strong, perfectly readable c.w. signal with a pure d.c. note would be reported as RST 599. On telephony the a ccepted form is R5 S9, but the same signal could be reported as QSA5 R9 (or Q5 R9) owing to the persistence of an earlier system with a QSAI-5 readability scale and an RI-9 strength scale. Quality of modulation scales have been evolved but are never used.

The readability/strength code can be used for reporting to broad casting stations, but a better system for this purpose is the SINPO code. This has five scales, each of 1 to 5 , as indicated by the letters $S$ (Signal Strength), 1 (Interference), N (Noise, i.e. static), P (Propagation Disturbance, i.e. fading) and O (Overall quality of reception).

The scale for signal strength is: 1-barely audible; 2-poor; 3-fair; 4-good; 5-excellent. The scales for Interference, Noise and Propagation Disturbance are: 1-extreme; 2-severe; 3-moderate; 4 slight; 5-nil. The scale for overall quality is: 1-unusable; 2-poor: 3-fair; 4-good; 5-excellent. Thus, in the SINPO code, a perfectly received signal would be given 55555 .


## AMATEUR ABBREVIATIONS

In order to save time; the pioneer operators gradually evolved a series of abbreviations which have now become an accepted part of amateur radio operating. Most of these were devised to reduce the number of morse code characters but some are still used verbally and in written characters. Their derivation is fairly obvious; contraction by omitting vowels (i.e., HRD=HEARD, RPT=REPORT), by phonetics (i.e., $S E D=S A I D, G U D=G O O D$ ), by using initials (i.e., SWL=SHORT WAVE LISTENER), by general contraction using first and last letters or by using an $X$ as termination (i.e., $V Y=V E R Y$, TX $=$ TRANSMITTER). Here are some of the more common abbreviations in use.


## FREQUENCY AND TIME CHECKS

A number of stations operate in order to provide accurate time and frequency checks, mainly on $2500,5000,10,000,15,000,20,000$ and $25,000 \mathrm{kc} / \mathrm{s}$. Many of these stations operate continuously with audio tones and interruptions in morse and voice. WWV also gives radio propagation forecasts.

ATA, New Delhi, India, $10,000 \mathrm{kc} / \mathrm{s}$.
BPV, Peking, China, $5000,10,000$ and $15,000 \mathrm{kc} / \mathrm{s}$.
CHU, Ontario, Canada, 3330, 7335 and $14,670 \mathrm{kc} / \mathrm{s}$.
DCF77, Mainflingen, Germany, $77 \cdot 5 \mathrm{kc} / \mathrm{s}$.
FFH, Paris, France, $2500 \mathrm{kc} / \mathrm{s}$.
HBN, Neuchatel, Switzerland, $5000 \mathrm{kc} / \mathrm{s}$.
IAM, Rome, Italy, $5000 \mathrm{kc} / \mathrm{s}$.
IBF, Turin, Italy, $5000 \mathrm{kc} / \mathrm{s}$.
JJY, Tokyo, Japan, 2500, 5000, 10,000 and
$15,000 \mathrm{kc} / \mathrm{s}$.
LOL, Buenos Aires, Argentina, 5000, 10,000 and $15,000 \mathrm{kc} / \mathrm{s}$.

MSF, Rugby, England, 2500, 5000 and $10,000 \mathrm{kc} / \mathrm{s}$. OMA, Prague, Czechoslovakia, 50 and $2500 \mathrm{kc} / \mathrm{s}$. OLB5, Prague, $3170 \mathrm{kc} / \mathrm{s}$.
OLD2, Prague, $18,985 \mathrm{kc} / \mathrm{s}$.
RWM, Moscow, U.S.S.R., 5000, 10,000 and $15,000 \mathrm{kc} / \mathrm{s}$.
WWV, Washington, U.S.A., 2500, 5000, 10,000, $15,000,20,000$ and $25,000 \mathrm{kc} / \mathrm{s}$.
WWVH. Hawaii, $5000,10,000$ and $15,000 \mathrm{kc} / \mathrm{s}$.
ZLFS, Lower Hutt, New Zealand, $2500 \mathrm{kc} / \mathrm{s}$.
ZUO, Johannesburg, South Africa, 5000 and $10,000 \mathrm{kc} / \mathrm{s}$.

Apart from the above-mentioned stations, the following transmitters can be used as accurate frequency check; since the frequencies are maintained within a tolerance of better than $\pm 1$ part in 10 GBR, Rugby, $16 \mathrm{kc} / \mathrm{s}$; Droitwich, 200kc/s; GRO, Skelton, 6180kc/s; GSB, Daventry, $9510 \mathrm{kc} / \mathrm{s} ; ~ G S V$, Daventry, $17,810 \mathrm{kc} / \mathrm{s}$. (GSV, GSB and Droitwich are broadcasting stations).

## HOW TO BECOME A RADIO AMATEUR

Having acquired experience in listening on the amateur bands, many SWL's aspire to owning and operating their own amateur station. In the interests of all users of the air space, and to provent absolute chaos, it is necessary to control the conditions under which amateur transmitting stations must operate.

In the U.K., applicants for an amateur licence must (a) be over 14 years of age, (b) be a British subject, (c) pass the Radio Amateur Examination, (d) pass the Post Office Morse Test. The R.A.E.

| WKD Worked | XTAL Crystal | YL | Young lady |  |
| :--- | :--- | :--- | :--- | :--- |
| WL | WiH | XYL | Wife $($ ex-YL $)$ | 73 |
| WUD | Would | YF | Wife | 88 |
|  |  | Love and kisses |  |  |

## AMATEUR CALL SIGN PREFIXES

The following list of call sign prefixes is arranged to indicate where a common prefix is shared by areas which can be counted as separate "countries" for scoring purposes. This list has been prepared by the Radio Society of Great Britain, our national radio society.

| AC3 | Sikkim | CT1 | Portugal | FH8 | Comorols. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AC4 | Tibet | CT2 | Azores | FK8 | New Caledonia |
| AC5 | Bhutan | CT3 | Madeirals. | FL8 | French Somaliland |
| AP | W. Pakistan | CX | Uruguay | FM7 | Martinique |
| AP | E. Pakistan | DJ, DL, DM | Germany | FO8 | Clipperton ls. |
| BV | Formosa | DU | Phillipine Is. | FO8 | French Oceania |
| BY | China | EA | Spain | FP8 | St. Pierre and |
| C9 | Manchuria | EA6 | Balearic Is. |  | Miquelon |
| CE | Chile | EA8 | Canary Is. | FR7 | Reunion ls. |
| CE9, VP8 | Antarctica | EA9 | Ifni | FR7 | Gloriseuses is. |
| CE® | Easter Is. | EA9 | Rio do Oro | FR7 | Juan de Nova |
| CEO | Juan Fernandez | EAO | Spanish Guinea | FS7 | French St. Martin |
| CM, CO | Cuba | El | Eire | FU8 | New Hebrides |
| CN8 | Morocco | EL | Liberia | FW8 | Wallis and |
| CP | Bolivia | EP | Iran |  | Futuna ls. |
| CR4 | Cape Verde is. | ET2 | Eritrea | FY7 | French Guiana |
| CR5 | Portuguese | ET3 | Ethiopia |  | and Inini |
|  | Guinea | F | France | G | England |
| CR5 | Principe, Sao Thome | FB8 | Amsterdam and St. Paul Is. | $\begin{aligned} & \text { GC } \\ & \text { GC } \end{aligned}$ | Jersey <br> Guernsay and |
| CR6 | Angola | FB8 | Kerguelen Is. |  | Dependencies |
| CR7 | Mozambique | FB8 | Tromelin is. | GD | Isle of Man |
| CR8 | Portuguese Timor | FC | Corsica | GI | $N$. Ireland |
| CR9 | Macao | FG7 | Guadeloupe | GM | Scotland |

requires a knowledge of fundamental receiving and transmitting theory and a knowledge of amateur licence regulations. The Morse Test is at 12 words per minute.

## Sources of Information

How to Become a Radio Amoteur: This is an invaluable pamphlet giving details of the R.A.E., licence conditions, etc..It can be obtained on request from: Radio Services Department (Radio Branch), General Post Office, Headquarters Buildings, St. Martins-le-Grand, London, E.C.I.

Pamphlet No. 55 (Radio Amoteurs' Examination): This contains the syllabus upon which the examination is set and can be obtained, price $1 /$-, from The City and Guilds of London Institute (Publications), 76 Portland Place, London, W.I. Also obtainable from the same address, price $2 /-$, are copies of the question papers set during the last three years.

The Radio Amateurs' Examination Manual: This is designed for those studying for the R.A.E. and covers the whole syllabus. Price is 5/6 from Radio Society of Great Britain, 28 Little Russell Street, London, W.C.I. Other useful publications by the RSGB include A Guide to Amateur Radio (price 4/-) and Morse Code for Radio Amateurs (price 1/9).

## PHONETIC ALPHABET

In order to convey a call sign or other information through interference, amateurs may resort to phonetic words. This may lead to confusion with newcomers since a popular phonetic alphabet uses geographical locations (such as $A=$ America, $H=$ Honolulu)! Although there is no compulsion, U.K. operators are encouraged to use the alphabet contained in the Radio Regulation, Geneva 1959, and adopted by NATO Services and other bodies, viz.:

| A | Alfa | H | Hotel | O | Oscar |
| :--- | :--- | :--- | :--- | :--- | :--- |
| B | Bravo | I | India | P | Papa |
| C | Charlie | I | Juliet | Q | Quebec |
| D | Delta | K | Kilo | R | Romeo |
| E | Echo |  | L | Lima | Sierra |
| F | Foxtrot |  | M | Mike | Sier |
| G | Golf | $\cdots$ | N | November | U |

$\checkmark$ Victor<br>W Whisky<br>$X$ X-ray<br>Y Yankee<br>Z Zulu

| GW | Wales | KC6 | E. Caroline Is. | M1 | San Marino |
| :---: | :---: | :---: | :---: | :---: | :---: |
| HA | Hungary | KC6 | W. Caroline Is. | MP4B | Bahrain ts. |
| HB | Switzerland | KG1 | see OX | MP4Q | Qatar |
| HC | Ecuador | KG4 | Guantanamo Bay | MP4T | Trucial Oman |
| HC8 | Galapagos Is. | KG6 | Mariana ls. | MP4M | Muscat and Oman |
| HE | Liechtenstein | KG6 | Guam | OA | Peru |
| HH | Haiti | KG6 | Marcus Is. | OD5 | Lebanon |
| HI | Dominican Rep. | KG61 | see KA® | OE | Austria |
| HK | Colombia | KH6 | Hawaii | OH | Finland |
| HKD | San Andres and | KH6 | Kure Is. | OHD | Aaland Is. |
|  | Providencia | KJ6 | Johnston Is. | OK | Czechoslovakia |
| HKD | Malpelo Is. | KL7 | Alaska | ON4, 5, 8 | Belgium |
| HKD | Bajo Neuvo | KM6 | Midway Is. | OX, KG1 | Greenland |
| HM | Korea | KP4 | Puerto Rico | OY | Faeroe Is. |
| HP | Panama | KP6 | Palmyra Group; | OZ | Denmark |
| HR | Honduras |  | Jarvis is. | PA®, Pl1 | Netherlands |
| HS | Thailand | KR6 | Ryukyu Is. | PJ | Netherlands |
| HV | Vatican City | KS4 | Swan Is. |  | W. Indies |
| HZ | Saudi Arabia | KS4B | Serrana Bank and | PJ2M | Netherlands |
| 11, IT1 | traly |  | Roncador Cay |  | St. Martin Is. |
| IS1 | Sardinia | KS6 | U.S. Samoa | PK | Indonesia |
| JA. KA | Japan | KV4 | Virgin Is. (U.S.) | PX | Andorra |
| JT1 | Mongolia | KW6 | Wake Is. | PY | Brazil |
| JY | Jordan | K×6 | Marshall Is. | PYס | Trinidade and |
| K | see W | KZ5 | Canal Zone |  | Vaz. Is. |
| KA | see JA | LA | Jan Mayen | PYס | Fernando de |
| KAØ, KG61 | Bonin and | LA, LB | Norway |  | Noronia |
|  | Volcanols. | LA | Svalbard | PZ | Netherlands |
| KB6 | Baker, Howland | LH | Bouvet Is. |  | Guiana |
|  | and American | LU | Argentina | SL, SM | Sweden |
|  | Phoenix ls. | LU-Z | see CE9 |  | Poland |
| $\mathrm{KC4}$ | see CE9 | LX | Luxembourg | ST2 | Sudan |
| KC4 | Navassa ls. | LZ | Bulgaria | SU | Egypt |


| AMATEUR BANDS (U.K.) |  |  |
| :---: | :---: | :---: |
| Frequency Band (Mc/s) | Classes of Emission | Maximum d.c. Input Power |
| 1.8-2.0 |  | 10 watts |
| $\begin{aligned} & 3 \cdot 5-3 \cdot 8 \\ & 7 \cdot 0-7 \cdot 10 \\ & 14 \cdot 0-14 \cdot 35 \\ & 21 \cdot 0-21 \cdot 45 \\ & 28 \cdot 0-29.7 \end{aligned}$ | $A 1, A 2, A 3,$ A3A, | 150 watts |
| 70.2-70.4 |  | 50 watts |
| $\begin{gathered} 144-145 \\ 142-146 \\ 420-450 \\ 1,215-1,325 \\ 2,300-2,450 \\ 3,400-3,475 \\ 5,650-5,850 \\ 10,000-10,500 \\ 21,000-22,000 \end{gathered}$ |  | 150 watts |
| $\begin{gathered} 2,350-2,400 \\ 5,700-5,800 \\ 10,050-10,450 \\ 21,150-21,850 \end{gathered}$ | $\begin{aligned} & \text { PID, P2D, } \\ & \text { P2E, P3D, } \\ & \text { P3E } \end{aligned}$ | 25W (mean), 2.5kW (peak) |
| Note: A-classes of emission are forms of amplitude modulation, F-frequency modulation and P-pulse modulation. |  |  |


| SV | Greece | UM8 | Kirghiz | VPS | Turks and |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SV | Crete | UO5 | Moldavia |  | Caicos is. |
| SV | Dodecanese | UP2 | Lithuania | VP6 | Barbados |
| TA | Turkey | UQ2 | Latvia | VP7 | Bahamas |
| TF | Iceland | UR2 | Estonia | VP8 | see CE9 |
| TG | Guatamala | VE, VO | Canada | VP8 | Falkland is. |
| TI | Costa Rica | VK | Australia | VP8 | S. Georgia |
| T19 | Cocos ls. | VK | Lord Howe Is. | VP8 | S. Orkney is. |
| TJ | Cameroun | VK | Willis Is. | VP8 | S. Sandwich is. |
| TL8 | C. African Rep. | VK9 | Christmas is. | VP8 | S. Shetland Is. |
| TN8 | Congo Republic | VK9 | Cocos is. | VP9 | Bermuda is. |
| TR8 | Gabon Republic | VK9 | Nauruls. | VQ1 | Zanzibar |
| TT8 | Tchad Republic | VK9 | Norfolk is. | VQ7 | Aldabra is. |
| TU2 | Ivory Coast Rep. | VK9 | Papua Territory | VQ8 | Cargados Carajos |
| TY | Dahomey Rep. | VK9 | New Guinea | VQ8 | Chagos Is. |
| TZ | Mali Republic | VKO | see CE9 | VQ8 | Mauritius |
| UA1, 3, 4, 6, |  | VK® | Heard Is. | VQ8 | Rodriguez is. |
| UNI | European S.F.S.R. | VKO | Macquarie Is. | VQ9 | Seycheiles |
| UA1 | Franz Josef Land | VP1 | British Honduras | VR1 | British Phoenix Is. |
| UA2 | Kaliningradsk | VP2 | Anguilla | VR1 | Gilbert and Ellice |
| UA9, 0 , |  | VP2A | Antigua, Barbuda |  | and Ocean Is. |
| UW9 | Asiatic S.F.S.R. | VP2V | British Virgin Is. | VR2 | Fiịi ls. |
| UBS, UTS, |  | VP2D | Dominica | VR3 | Fanning and |
| UY5 | Ukraine | VP2G | Grenada and |  | Christmas Is. |
| UC2 | White Russian |  | Dependencies | VR4 | Solomon Is. |
|  | S.S.R. | VP2M | Montserrat | VR5 | Tonga is. |
| UD6 | Azerbaljan | VP2K | St. Kitts, Nevis | VR6 | Pitcairn is. |
| UF6 | Georgia | VP2L | St. Lucia | VS5 | Brunei |
| UG6 | Armenia | VP2S | St. Vincent and | VS6 | Hong Kong |
| UH8 | Turkoman |  | Dependencies | VS9 | Aden and Socotra |
| U18 | Uzbek | VP3 | British Guiana | VS9 | Maldive Is. |
| UJ8 | Tadzhik | VP4 | Trinidad and | VS9 | Sultanate of Oman |
| UL7 | Kazakh |  | Tobago | VS9K | Kamaran Is. |

These ranges are selected by pressing a function button ( $\mathrm{mA}, \mathrm{V}$ or $\Omega$ ) and also a range button. Each of the three range buttons will select a current range, a voltage range or a resistance range. Thus the left-hand range button will give ranges of $0-1 \mathrm{~mA} ; 0-1 \mathrm{~V}$ or $0-1 \mathrm{k} \Omega$, depending on which function button is depressed. Thus three range buttons allow us to select 3 current ranges, 3 voltage ranges and 3 resistance ranges. The fourth current range $(0-50 \mu \mathrm{~A})$ is obtained by pressing the mA function button and releasing all the range buttons. (This can be done by slowly pressing a button half-way in until it unlocks the other buttons, and then releasing it.)

## V FUNCTION BUTTON

The fourth voltage range $(0-500 \mathrm{~V})$ is obtained by pressing the $V$ function button and releasing all the range buttons. It is suggested that the buttons be colour coded, using red for current, green for voltage and yellow for resistance. Thus buttons "input 1 ", " input 2 " and " mA " will be coloured


Fig. 2: Checking transistor performance.
red; buttons "input 3 " and "V" will be coloured green; and button " $\Omega$ " will be coloured yellow. The three range buttons are each divided into three equal areas which are coloured red, green and


Fig. 3: Wiring and layout diagram.
yellow respectively. Thus for each button the appropriate current, voltage and resistance range can be written on the red, green and ycliow panels. When all the function buttons are released the meter movement is short circuited, and the meter should be left like this when not in use.

Each button operates a $4-$ pole 2 -way switch. The circuit diagram is given in Fig. 1 and the layout in Fig. 3. The case is made from plywood bonded with epoxy resin (Araldite etc). The resistances are nearly all non-standard valves. If you are on good terms with your dealer he may let you go through his stock of $10 \%$ resistances with his meter until you find ones near enough. This way means that your meter will be slightly innacurate on some ranges, but it should not be enough to worry about.


Fig. 4: Cabinet drilling and constructional details.

## SPECIAL RESISTORS

The very low value resistances are best made from lengths of electric-fire element. Pull out a few feet of element to remove the kinks, measure this length accurately (in inches) and borrow an ohmmeter to measure its resistance. Divide the length by the resistance and you will get a number which represents the length which has a resistance of $1 \Omega$. Multiply this by the resistance you want. This will give you the length of wire you will need (in inches). Remember to cut off a piece slightly

## COMPONENTS LIST

## Resistors:

All selected from 10\%, $\frac{1}{4}$ watt

|  |  | Nearest <br> Resistance |
| :--- | :--- | :--- |
| Value | standard value |  |
| R1 | $524 \mathrm{k} \Omega$ | $560 \mathrm{k} \Omega$ |
| R2 | $4.944 \mathrm{k} \Omega$ | $4.7 \mathrm{k} \Omega$ |
| R3 | $49.45 \Omega$ | $47 \Omega$ |
| R5 | $384 \Omega$ | $390 \Omega$ |
| R6 | $15.8 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ |
| R7 | $9 \mathrm{M} \Omega$ | $8.2 \mathrm{M} \Omega$ or $10 \mathrm{M} \Omega$ |
| R8 | $800 \mathrm{k} \Omega$ | $820 \mathrm{k} \Omega$ |
| R9 | $180 \mathrm{k} \Omega$ | $180 \mathrm{k} \Omega$ |
| R10 | $19 \mathrm{k} \Omega$ | $18 \mathrm{k} \Omega$ |
| R11 | $53 \Omega$ | $56 \Omega$ |

The following resistors are made from resistance wire:

Length of $230 / 250 \mathrm{v}$
500 watt fire element
(Wellco Ltd)
202 mm
130 mm
6.5 mm
longer than this to allow for the soldered ends. The $0.1 \Omega$ resistance may be best made out of copper wire. If you use fire element for this one, it will be about $\frac{1}{4}$ in. long and may be a bit too small to handle easily. If you use Weilco spiral element. $230 / 250 \mathrm{~V} 500 \mathrm{~W}$. a 6.5 mm length has a resistance of $1 \Omega$, and you will find the suggested lengths for each resistance in the components list. The wire should be insulated with a varnish.

## CONSTRUCTION

Construction should be started around the banks of switches, leaving leads about 6 in . long for connecting to the meter, the batteries, the potentiometer and the input sockets. The four screws at the back of the meter are removed and the cover can then be lifted off. The existing scale should be

## Other Components

VRI $1000 \Omega$ linear w.w. pre-set potentiometer
BI Two 15 V batteries in series (Ever Ready BI54)
B2 One 1.5 V baby cell battery (Ever Ready LPU 11)
Three 3 -way pushbutton units, each operating a 4-pole, 2-way switch (Broadway Electronics Ltd., Tooting).
$50 \mu \mathrm{~A}$ meter, ex-government (Radio \& TV Components (Acton) Ltd.).
Six sub-miniature sockets and plugs.
One piece of $\frac{1}{8}$ in. plywood, $12 \frac{1}{8}$ in. $x \mid l i n$.
Two pieces of leathercloth for covering $18 \mathrm{in} . x$ 5in.; $15 \mathrm{in}, \times 4 \mathrm{in}$.

Fig. 5: Scale calibration for the new dial (see text).
removed, and the scale shown in Fig. 5, copied on to thin card, mounted in its place. The pointer can be lengthened, if desired, by gluing a short length of very fine wire to the end of it. If this is done, it must be counterbalanced very carefully so that the position of the pointer does not change when the meter is horizontal and vertical.

The wooden case can be covered with leathercloth.


## UNDERSTANDING F.M.

-continued from page 762
polarity only. The pulses " pile up" additively in C2, but not indefinitely because there is a drain into the following a.f. circuit through C4. Allowing for the smoothing effect of C2 C3 and the time constants of the network it will be realised that the pulses lose their separate identities but set up voltages that change with their rate of arrival. The smoothing network includes the adjustment required for de-emphasis. D2 eliminates pulses of opposite polarity.

To produce distinct pulses the carrier must be converted to a very low intermediate frequency between 100 and $500 \mathrm{kc} / \mathrm{s}$ and the gain of the receiver is consequently low. Nevertheless, it provides a simple system of the highest quality and a successful valve version appeared in the April 1965 issue of this journal. It is well suited to transistor circuitry and a design is in development at the moment.
As the object of this article has been to explain the nature and behaviour of the f.m. carrier in order that the discriminators likely to be encountered can be understood, such matters as the relationship between frequency modulation and phase modulation, pre-emphasis and de-emphasis, limiter circuitry, and interference, have not been included because these can be pursued after the information in these pages has been understood.

## ECONOMY FM TUNER (October 1965 P.W.)

Fig. 1 shows the screen grid (pin 8) of V 2 connected to the junction of R2/C2. This should have been shown connected to the junction of RI/CI only.

## MINIATURE OSCILLOSCOPE (November 1965 P.W.)

Henry's Radio Limited, 303 Edgware Road, London, W.2. have informed us that they are able to supply new, from stock, the ACRIO (VCR139A) c.r.t. We understand that this will replace the VCR139 without any changes to the circuitry. The price is 25 s . 0 d . plus 2 s . 6 d . post and packing.

## BUILT-IN TUNER FOR TAPE RECORDERS (September 1965 P.W.)

The H402 coil kits are now being supplied with two different codings. The colour coding of the cores given in the article is correct where the transformers have part numbers viz: E360-S301-S203 etc., and where the ferrite rod aerial has only three leads.
Where the ferrite rod aerial has four leads, the GREEN and BLACK leads should be joined together and taken to chassis ( + ve). Also where the transformers do not have part numbers, the colour coding of the cores are as follows: OscillatorBlack. Ist i.f.t.-Yellow. 2nd i.f.t.-Red. 3rd i.f.t.Grey.
A circuit diagram supplied by the coil kit mannfacturers, is included with each set of coils, and reference to this before construction will clarify the connections.

## PRACTICAL WIRELESS AND PRACTICAL TELEVISION FILM SHOW

The Film Show, which is held annually, is to be held as before, at Caxton Hall, Caxton Street, Westminster, London, S.W.I. The ciate of the Show, which is arranged in collaboration with Mullard Limited, is Friday, 4th February, 1966, at 7.30 p.m. sharp. The films to be shown are "Electromagnetic Waves, Part II" and "Thin Film Microcircuits" and the illustrated talk will be on "Transistor Topics". Refreshments will be provided. The talk will be given by Mr. I. Nicholson of Mullard Limited, and in the chair will be Mr. W. N. Stevens, Editor of "Practical Wireless" and "Practical Television". Applications for free tickets should be made to FILM SHOW, "Practical Wireless", Tower House, Southampton Street, W.C. 2 and not to Caxton Hall. A stamped addressed envelope must be enclosed.

## Dealings with the G.P.O.

I ENCLOSE part of recent correspondence between myself and the G.P.O. Radio Services Branch.

From the University of Sheffield Amateur Radio Society:

Q1 . . . Can Sound 'B' licensees operate on any amateur frequency provided that they use a Sound 'A' callsign, the holder of which is present?

A1... The holder of an amateur (Sound) licence ' $B$ ' is permitted to operate an 'A' station under the direct supervision of the licensee on all amateur frequencies. Operation, however, is restricted to telephony only.

Q2 . . . Can Sound 'B' licensees operate a club (Sound ' $A$ ') station as authorised operators, unsupervised, on frequencies bigher than $420 \mathrm{Mc} / \mathrm{s}$ ?

I appreciate that the use of Morse is not allowed when a Sound ' B ' licensee is transmitting.

A2...The holder of an Amateur (Sound) licence 'B' cannot be authorised to act as an additional operator of an ' $A$ ' olub station.

I feel that these answers could be of sufficient significance for comment in Practical Wireless. J. P. Billingham.

Ardsley, Barnsley.

## Tape Terminology

The remark in Mr. Read's letter (November 1965 issue) has been somewhat anticipated. On the 20th of October, George Newnes published a short work, "Questions and Answers on Radio and Television ", putting technical matters into language that, I hope, will be both instructive to the layman and helpful to the accomplished. Also published on that date was my more ambitious work on the subject that appeals to Mr. Read, "Tape Recording Service Manual". Although this is a volume costing three guineas and containing technical data on a great many tape recorder mechanisms and circuits, it also contains a seotion dealing with the principles of tape recording and general servicing procedures in which Mr. Read may be interested.
H. W. Hellyer.

Bargoed, Glamorgan.

## NEWS AND..

## THE WORLD'S MOST PRECISE "RADIO EYE"



A new 140 ft . diameter radio telescope is now operational in Green Bank, (West Virginia) USA. It is being used by astronomers to detect sources of noise in outer space. Unique feature of the telescope is a Westinghouse metal bearing which pivots 2,600 tons on a film of oil only the thickness of a hair.

Built at a cost of $\$ 13$ million the station, known as National Radio Observatory, is designed to be the world's most precise instrument for pinpointing waves from outer space.

## THE COLDEST PLACE ON EARTH

In a recent issue of the Mullard Outlook, details were given of the Mullard Cryomagnetic Laboratory located at Oxford, England. This forms part of the internationally known Clarendon Laboratory which has become famous for its contributions to research in the field of magnetic fields at very low temperatures.

Mullard scientists in their new laboratory with its source of very high power magnetic fields have recently been testing many new types of semi-conductor material. This may, in time, lead to revolutionary methods of generating, transforming and distributing electric power. In the course of studying aspects of solid state physics, the scientists have been able to achieve temperatures as low as a millionth of a degree above absolute zero-almost as cold as the conditions found in outer space.

The Mullard Cryomagnetic Laboratory is believed to be the only one in the world to have reached so far down the temperature scale and thus earned for itself the title of "The Coldest Place on Earth".

## LASER TELEPHONE LINE IN MOSCOW

The first laser telephone communication system linking two districts in Moscow is being put into operation. Special transmitting equipment converts telephone signals into impulses which are superimposed on a laser ray. The receiving equipment directs the ray to a large parabolic mirror which reflects it into a system of filter and photo transformers where it becomes a telephone signal again.

# ..COMMENT 

## INTERNATIONAL RADIO COMMUNICATIONS EXHIBITION

Now fairly established as a regular event in the radio calendar, this year's exhibition at the Seymour Hall fully lived up to the reputation of its predecessors.

The home-constructed units bore witness to the very high standard attained these days by Amateurs, and with some exhibits it was difficult to define the borderline between these units and some of the commercial items. Of particular note was the solid state mobile equipment built by G3LOK and the superb s.s.b. transceiver constructed by G3SBA.

The British Amateur TV Club displayed an impressive array of gear with a triple-turret TV camera with built-in monitor screen televising the exhibition from the balcony.

In the professional field, K.W. Electronics displayed their KW2000A s.s.b. transceiver while across the hall Brian J. Ayres \& Co. were showing a range of National equipment. Highlight here was the much talked of solid state receiver, the HRO-500 costing about 4705 . Needless to say, this is not a t.r.f.!

The manufacturers award this year was presented to Tom Withers of T.W. Electronics for their solid state v.f.o. for $144 \mathrm{Mc} / \mathrm{s}$. Messrs Imhofs offered an impressive display of cabinets of all shapes and sizes, and Electroniques offered their very excellent coils and receiver front-ends for the serious amateur. I. Beam aerials showed a number of their time proven v.h.f. and u.h.f. arrays, plus the able assistance of Vic. Hartopp to answer the numerous queries.

The accent this year was clearly two things-the increase in solid state circuitry, and s.s.b. Next year might even see greater marriages between these two.

## MARCONI SOLID SWITCHES

The photograph shows the final stage in the production of one of the new range of Marconi highspeed solid-state switches.

Hard black Araldite, an extremely tough epoxyresin, is being poured into the body of the switch to provide complete encapsulation. This technique provides the maximum possible protection for solid-state electronic circuits. After curing at $60^{\circ} \mathrm{C}$, the switch becomes an entirely solid unit which is capable of operating under extreme environmental conditions.

These new switches are fully transistorised and can be used as direct replacements for electromechanical relays. They are virtually indestructible and will operate almost indefinitely.


Thumbnail History of Radio
I would like to thank the many old-timers who have helped me in my researches for the above-mentioned article. Most of this information has been passed on to me by the old operators on 80 m whose tanks are sadly diminishing all the time. I feel that it is especially important to collect all this information before it is lost.
R. F. Farley, G3SSJ.

> Mytchett,
> Nr. Aldershot, Hampshire.

## The Meaning of Amateur

Do your correspondents think that amateur foothallers should knit their own jerseys and socks, or that amateur cyclists should construct their own cycles?

So why should amateur radio enthusiasts be any different? Why should they not have the benefit of commercially-made equipment as much as amateurs in any other field?
R. G. Hasler.

Birmingham, 28.
I Do not think we should take too seriously the letter on this subject from Mr. Heathfield in the December issue-he generalises too much on only a few observations. Will he now do us the favour of visiting those of his friends whose hobby is photography and then tell us how much of their apparatus (cameras, lenses, light meters, rangefinders, print-driers, etc.) they have made for themselves, and if he considers it a bad thing that they should buy commercial gear.

Has it escaped his notice that a commercial-looking piece of equipment may in fact have been built from a kit of parts such as those offered by K. W. Electronics, or Heathkit?

Our hobby is perhaps unique in that so much of the apparatus used in it can be built at home to save heavy outlays if one is so inclined; that so much is published to enable this to be done, and that so many people (despite what Mr. Heathfield would Jike us to belicve) still do "roll their own" and enjoy doing it.
W. E. Thompson, G3MQT.

St. Leonards-on-Sea, Sussex.

# TAPE TAPE TAPE TERMINOLOGY TAPE 

## PART SIX

## THREE-HEAD SYSTEM

Using separate Erase, Record and Play Heads.

## TONE CONTROL

Used during playback to "tailor" the response of the tape recorder to suit listening conditions. Can consist of a simple top-cut network or a more complicated bass and treble constant-control, using feedback networks and balanced controls.

## TRACK

The magnetised path of the recording after it has passed the recording head. Trackwidth depends on the gap length. Fig. 19 shows actual and proposed track dimensions on standard quarterinch (average) tape. Figures given are in inches, and some tolerance is allowed for most measurements, depending on head manufacture. The diagram is not to scale.
(a) Half-track operation, BS. 1568.
(b) International half-track standard.
(c) Original Continental quarter-track standard, now discontinued.
(d) Proposed "compatible" standard.
(e) American MRIA quarter-track standard.

Note that various standards have been proposed. and the latest attempt is to ensure compatability, i.e. the replaying of two-track recordings through a four track machine for stereo reproduction, without losses and also to be able to replay quarter-track recordings on a half-track machine, which is at present not satisfactory. Spaces between tracks and at edges are called "safety lanes".

by H. W. Hellyer

## TWIN TRACK

Correctly referring to a stacked head with two gaps, one above the other, for simultaneous recording and playback of two tracks. (As opposed to two-track, where a single gapped head is used for recording and replay of two tracks by tape inversion at the end of the reel.) Similarly, quartertrack recording is made on a four-track machine having two gaps, and employing the tape inversion principle. Track numbering is normally 1 and 4 for the outer tracks and 2 and 3 for the inner tracks, giving a numbering 1 to 4 from top to bottom. But some manufacturers favour different numbering systems.

## transoucer

A device which is actuated by waves from one transmission system and supplies related waves to other media. Practically, a microphone or loudspeaker which converts sound waves to electrical impulses, or vice versa.

## TWEETER

Small loudspeaker specially designed to handle the higher audio frequencies. Normally connected via a filter which cuts off tones below about $2,000 \mathrm{c} / \mathrm{s}$.

## ULTRASONIC FREQUENCY

A frequency lying above the audio frequency range; usually employed to indicate the frequency range of the bias oscillator. This is not strictly accurate, bias frequency is usually in the radio frequency part of the spectrum.

Fig. 19: Track dimensions on standard $\frac{1^{\prime \prime}}{4}$ tape.


## VARIABLE BIAS

Method of altering bias gradually to obtain good tone balance, usually during superimposition when the action of cutting out erase power can affect bias conditions, and when reduced bias is needed for the later signal to prevent overriding the original.

## variable speed wind

In some machines (professional types mainly) the speed of winding can be potentiometer controlled for special applications.

## EXCLUSIVE TO PRACTICAL WIRELLSS READERS

## TRANSISTOR POCKET RADIOS



ONLY $\quad 28 / 6$
NO MORE TO PAY

BULK PURCHA8E ENABLES OS TO MAKE THIS FAN MAND WITH GUARANTEE : :
The "BAN REMO" Brings tuned that it brings the voices of and vocalists drainer and rocalists dra in your home, oftice in your home, offtce,
etc. Only $4 \%$
$2 i n$ $\underset{\text { etc. in } 1 \text {. Fite easily }}{ }$ into your pocket or haudbag. Works for months off $1 / 2$ battery shnuld last a lifetime, anyone can assemble itionan
hour or two with our easy plan. Minature speaker. carrying case-everything only $28 / 6$ 2/f P. \& P. (Parts can be bought separately.) Inmited period-so rush your order before it $^{\circ}$ too late. DEMONGTRATIONB DAILY.

## DON'T WALK-


 OUTFIT \& baby alarm

LIMITLD QUANLITY SAVE £3.13.1 ONEY Robustly made, brand new 49/ I separate, fully transistorised - each can speak or ifsten to the other - complete with 60 ft . connecting wire. Fixed in a flash. Ends babycrying worries. Ideal for Workshop to House, Sickroom. hundreds of uses Hangs on wall or stands up. our absurd 3/7. Money refunded if not 6 gns. value

## MAKE 5 DIFFERENT

 TRANSISTOR RADIOS FOR 35/NO EXPER LENCE NEC
ESSAY. No soldering.
Only 8 connections con first radio to work A.B.C. Plans, Gabinet Loudspeaker (alone 1\%/6). Earphone 4 Semi-conductors. Coils. Condensers, Resistors, Tuner, Switch. Screws, etc Fnglish plied and Foreign reception. As supForces, etc TESTIMONIALS GALORE Mr Ik t'I of Lomionjerry, writas:". I received your components and 1 must sau that I am very satisfied with them' I have RA ADIO COETKSE: Originally E6 SEND OXIV $35 /=$ plus $3 / 6$ posit, ete,


Well-known brand Transistor Rsdio Kits-YOU SAVE e3,10.6. Covering all medium/long ware with parts including Mullard Bem Conductors. 48 page instruction manual. Entertaining sind educational No soldering, just phu
Radios in a few mins.


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## FABULOUS

## ST. TROPEZ MK. 6

## The Sensational Pocket Radio



This fantastic offer will ama

- the beautifully compact -the beautifully compact ST TROPEZ, measuring $4 t$ I 3 I 1 tin
recelves perfectly in bedroom recelves perfectly in bedroom
oftice or gardens-over all medium waves including Luremboarg. Un waveg including Lurembonig. Un
der Id. per hour running eost
ANYONE can agsemble it in AN YONL can assemble it in on
 extra). Case extra. Parts can be bonght separately,

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Fig. 20 depicts (a) original circuit of wind-on and re-wind motors of typical three-motor machine. with loading resistor used to balance torque during Record or Playback. (b) Modified circuit using variable resistor to form bridge. (c) Motor torque varies as resistance (and hence applied voltage) is varied. Suitable for single-phase induction motors with no electrical connection between stator and rotor. Speed of motor is less than synchronous speed, the difference being the "slip" which increases as rotor speed decreases. The circuit allows relative torque variation. At point of intersection of curves. which depend on motor characteristics, motors are balanced and at standstill.

## VARIABLE RELUCTANCE MICROPHONE

Older types of moving iron microphone come into this category, and are rarely used for present purposes. (See Microphones.)

## VELOCITY MICROPHONE

A microphone in which the electric output substantially corresponds to the instantaneous particle velocity in the impressed sound wave. An example is the ribbon microphone, in which pressure gradient principle is employed, the difference in pressure between the two faces of the ribbon causing movement and electrical output. (See Microphones.)

## VIDEO TAPE RECORDING

Method of recording television pictures on magnetic tape for subsequent replay. Problems involved are caused by the need for large band-width-at least $2 \mathrm{Mc} / \mathrm{s}$-which calls for high speed of tape past heads. This can be achieved either by fast tape speed or by rotating a sequence of switched heads as the tape is moved. Fig. 21 shows basic rotating head system used for video tape recording. Two-inch Mylar tape is used at 15 in/ sec. Headwheel spins at 15,000 r.p.m., giving relative head-to-tape speed of $1570 \mathrm{in} / \mathrm{sec}$. Vision track is modulated on to an f.m. carrier from 42.2 to $6.8 \mathrm{Mc} / \mathrm{s}$ before recording and demodulated after replay. There are four heads, and four channels, with each head having a 120 degree arc of tape contact- 30 degrees of overlap. Each head is switched electrically during contact, and "killed" during out of contact period to reduce stray responses. Synchronising is supplied from servo control of motor and sync pulses are recorded on tape. Switching gate is controlled by photocell from motor into switching module.
The multiple head system scans the tape vertically with the tape at relatively slow speed. A tape speed of $7 \frac{1}{2}$ in/sec. will produce a track speed of $200 \mathrm{in} / \mathrm{sec}$. or greater with rotating heads. As the tracks are nearly vertical, and in rotation, the tape must be wider than standard, and mechanical problems of speed regulation, head wear and synchronisation are encountered. Two such machines recently marketed have tape speeds of 12.6 and $19 \mathrm{~cm} / \mathrm{sec}$, and tape width of 50.8 mm and 25.4 mm respectively.
The alternative technique, of a stationary head


Fig. 20: Circuits of wind-on and rewind motors and motor torque graph.
and fast-moving tape, uses speeds of up to $150 \mathrm{in} /$ sec., and a standard $\frac{1}{4}$ in. tape, on which one track of video and another of f.m. sound are recorded. Typical head gap sizes are less than micron. (One example is the American Fairchild V-5000, using a tape speed of $120 \mathrm{in} / \mathrm{sec}$., a standard tin. tape. and movable heads to scan four tracks. A single track is used with multiplexed video and audio signals. The record head has a relatively wide gap but the playback head gap is only 0.000039 in. wide. Instrumentation tape is used, of $9,000 \mathrm{ft}$. length on a $10 \frac{1}{2} \mathrm{in}$. standard NAB spool.)

Later developments include thermoplastic video recording, first developed for radar equipment. A tape is prepared with a positively charged thermoplastic layer, which has a low-melting point. The
basic negatively charged tape has a higher melting point. Thermoplastics soften when heated and return to normal condition on cooling.
The principle involves heating the whole tape to the melting point of the charged thermoplastic layer by passing it through a vacuum and applying a dielectric heater. Ripples are formed on the tape in proportion to the moving electron beam of the cathode ray tube through which it passes, the beam being modulated by the video information. The dielectric process causes the thermoplastic layer to "freeze" temporarily in its ripple formation as it passes through and this modulated tape is replayed by passing light through a condenser lens, the transparent tape and an apertured plate, using the Schlieren optical system. A very wide bandwidth (up to $50 \mathrm{Mc} / \mathrm{s}$ ) is possible. The drawback is the elaborate vacuum pumping equipment, but development of a special tube with a mosaic of fine wires in place of the normal phosphor screen is still taking place. The wires are embedded in the glass and pass right through, forming a virtual extension of the electron beam, and eliminating the complication of vacuum sealing of the tape at the point of modulation.

Recently announced was a video-disc method of recording with parallel principles, but using a method of repeated "stills" instead of a moving picture, stored on dise. The great advantage of such a system, if it can be developed beyond the slow-scan 25 frames per second limitation, is the simplicity of the playback conversion equipment.

## VOLUME

Correctly, an acoustic, rather than electrical term. Measurement refers to the pressure of the sound wave in terms of dynes/square centimetre. The louder the sound, the greater the pressure, but
loudness, as a term, depends also on the frequency and waveform. Convenient form of volume expression is in decibels, this scale being nearer to the aural range than any linear form.

## VOLUME COMPRESSION

System of sound recording where the level of the signal passing through an amplifier is arranged to control the gain in such a way that high sound levels are amplified less than low sound levels.

## VOLUME UNIT (VU) METER

Type of modulation level indicator which measures electrical signal voltages and records relative levels of sound. This type of meter responds to average values but does not indicate peaks. Professional recording authorities favour peak programme meters for correct setting of modulation levels. American machines favour VU meters, the British and many Continental machines have various forms of peak reading meters or indicators (such as the magic eye) or modified forms of these, with rise times flattened slightly by charge circuits to give a compromise system.

A typical VU meter would be a rectifier-fed, moving-coil meter with a low total series resistance so that the non-linear forward characteristic of the rectifier makes it almost a square-law instrument, measuring energy or power rather than voltage or current. The scale is marked in volume units, each being approximate to one decibel with the instrument measuring a pure steady tone. But peaky waveforms will produce only the "averaged" response, sometimes referred to as the r.m.s. reading (not quite accurately, except with pure sine waveforms).


Fig. 21; Basic rotating head system for video recording.

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## WATT

The unit of electrical power. Defined as the energy expended per second by an unvarying electric current of one ampere across a potential difference of one volt. For audio purposes, both the peak power and the average power must be considered. Electro-acoustic efficiency is less than purely electrical measurement may indicate. Electro-acoustic efficiency ratio may be as much as $30: 1$ with commercial equipment. A speaker efficiency is only some 3 to $5 \%$ under normal domestic conditions, so that an amplifier with an average audio output of 10 watts is adequate for domestic purposes, even if transient peak powers are as much as 40 watts. Most domestic tape recorders with inbuilt speakers are only intended to give about $2-5$ watts audio output. which is quite sufficient for normal purposes.

## WAVELENGTH

In tape recording, directly related to the speed and frequency of the medium: i.e. the frequency of signal and the speed at which the tape passes the head gap, which determines the physical wavelength of the recorded "magnet" on the tape. Wavelengths become shorter as the frequency of the applied signal increases, but longer as the speed of tape transport increases. This is important during playback, where the higher speed permits use of a wider gap for a given frequency due to the extended wavelength, or, conversely, allows a higher frequency response for the same gap when the tape is recorded and replayed at a higher speed.

## wow

Distortion caused by periodic variation of tape speed. Although there is no standard, variations of up to twenty times a second in pitch of the sound are generally considered as "wow" while variations in the band $20-200 \mathrm{c} / \mathrm{s}$ are called "flutter". Wow is more evident with sustained notes and music with "dying tones" such as piano and organ music. It is usually caused by eccentricity in moving parts. Regularity of the wow may be a clue to its origin. Flutter has the effect of making the tone harsh. and is often more difficult to determine. Its resuits sometimes sound like an overloaded amplifier due to frequency modulation of the recorded signal. Wow and flutter figures are stated as an R.M.S. measurement. typical specification being "less than $0.2 \%$ total r.m.s.". More than 0.5 is poor.

In Tahle I reel sizes in inches, tape length in feet, playing times in minutes and seconds for principal types of tape in general use. There are variations of tape length, and playing time between manufacturers. Figures given are common to the largest number of companies. Playing time is for a single track at $3 \frac{3}{3} \mathrm{in} . / \mathrm{sec}$ For alternative speeds divide and multiply by factors of 2 . For complete tape playing time on more than one track multiply by number of recorded tracks (except for stereo).


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## ELECTRONIC PITCH-PIPES

## by

R. Bebbington

Grad. I.E.R.E.

ANYONE who has had anything to do with training or conducting choirs will appreciate the value of a set of pitch-pipes. Pianos are not always situated conveniently adjacent to the choir and to pitch the notes of the initial chord for unaccompanied singing can be something of a problem. The author knows from bitter experience that the notes you play on the piano and the notes you sing to the choir on your return-after knocking over a few music stands and negotiating several rows of seats-are not always the same. Usually the tenors will be quick to point this out to you, that is if the effort of reaching a top $A$ that should only have been a top $F$ has not permanently strained their vocal chords. The eloctronic pitch-pipes to be described have been used nuccessfully for male voice singing and have been particularly aseful for open-air activities.

## Cireuk Theory

The transistorised version of the well-known Hartley oscillator is employed as a high degree of stability can be obtained. Even with battery ageing there is no discernible variation in pitch,


Fig. I: Tones selected by switched capacitors.
a pitch or frequency standard for other purposes.
The output of the oscillator is fed straight into a bigh-impedance miniature loudspeaker which serves as the collector load. Sufficient volume is obtained to allow the unit to be operated inconspicuously in a coat pocket and still be heard. Should extra volume be required an output stage can easily be added and a resistor substituted for the oscillator collector load. In its simplest form the unit can be really compact, the prototype measuring 4 in . $x 3 \mathrm{in}$. $x 1 \frac{1}{2} \mathrm{in}$. The frequency determining components are the tapped coil, the capacitors across it and, in the simplified version, the series variable resistor.

For accurate pitch control a capacitor for each note is preferable and this requires a single-pole, 12-way switch to cover every semitone in a complete octave or musical scale. It is extremely


Fig. 2: Tones selected by potentiometer (see fig. 4).
unlikely that exact values of capacitors will be found to tune each note in the scale and padding by smaller values will have to be done. If you are incapable of doing this, even with the aid of a piano, borrow the ear of a musical friend. If extreme accuracy is not so important the variable resistor is an easier and cheaper method of frequency control and can be quickly calibrated.

With the components listed in Fig. 2 the $2 \mathrm{k} \Omega$ variable control has a frequency range of one octave from $E$ flat to E flat.
Choice of coil will obviously influence the precise location of the frequency range, but this is immaterial as long as a complete octave is covered, since this is bound to embrace all the notes in any musical scale. However, as the coil is the only item that is not standard some details are perhaps called for at this stage. Many tapped coils have been tried and the circuit oscillated freely with most of them. These included inter-valve transformers, television blocking oscillator transformers, the tapped primary of a standard output transformer,

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 Test Prods，2／9．Set Trim Tools，3／－ Multicore Solder，6d．yd．Dispuenser， $2 / 6$ ．

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| 5 Y 3 | 6／－12aU7 | 6／－ECL82 | 10／－ 3 P61 | 8\％ |
| 574 | 8／－124x7 | 7／－ECLS6 | 10／－U 22 | 71. |
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| 6AT6 | 6／－112K9 | 14／－EF86 | 10\％UBC81 | 6／－ |
| 6BA6 | $7 / \mathrm{F} 12 \mathrm{Q7}$ | $6 / \mathrm{m}$ E89 | 8／\％UBF89 | 5／． |
| ¢BE6 | 5／－35 26 | 9／－EL84 | $7 /$ UCHel | 9\％ |
| ${ }^{5} \mathrm{H} 6$ | $3 /-35 \mathrm{Z4}$ | 5／－EY51 | 9／－UCL82 | 10／＝ |
| 855 | 5／－954 | 2／－EY86 | $9 \%$－UF89 | 7／6 |
| \＄3． 6 | 5／－DAF96 | 8／－EZ40 | 5／－\ULat | $8 \%$ |
| 6JTG | 6／－DF96 | 81 E280 | 7－ULS4 | $8 \mathrm{8} \mathrm{\%}$ |
| 6Kg | $5-\text { DK90 }$ | $8 /-E Z 81$ | \％／－UY41 | 51－ |
| いK76 | $5 /-D L 96$ | 8／－MC14 | 7 7 － 185 | 7／． |
| 6K84 | 5／－EABC80 | 7／61PC97 | 7／－lUU9 | \％\％ |
| 6 V 7 M | 5j－EB91 | 4／－PbC84 | 8i－W81 | 6\％． |
| $\begin{aligned} & \text { B.T } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { TAPE } \\ & \text { 2/6 pair } \end{aligned}$ | MOT01kS for 200－250 | $\begin{aligned} & 115 \text { v. } A \\ & \text { v. (in } \operatorname{ser} \end{aligned}$ |  |

RETURN OF POST DESPATCH

\section*{NEW ELECTROLYTICS FAMOUS MAKES} TUBULAR TUBULAR CAN TYPES | $1 / 350 \mathrm{v}$ | $2 /-$ | $100 / 25$ | $2 /-$ | $8 / 600 \mathrm{~V}$ |
| :--- | :--- | :--- | :--- | :--- |

 | $6 / 3507$ | $2 / 8$ | $600 / 157$ | $2 / 6$ | $16+16 / 500 \%$ |
| :--- | :--- | :--- | :--- | :--- |
| $8 / 4507$ | $2 / 8$ | $1000 / 16 \%$ | $9 / 6$ | $29+6$ |

 \begin{tabular}{llll|ll}
$82 / 450 v$ \& $8 / 9$ \& $8+8 / 460 \mathrm{v}$ \& $3 / 8$ \& $32+82 / 450 \mathrm{v}$ \& $8 /-$ <br>
$82 / 4 / 450 \mathrm{v}$ \& $8 / 9$ \& $60+50 / 350 \mathrm{v}$ \& $7 /-$

 

$25 / 20 \mathrm{v}$ \& $2 /-$ \& $82+32 / 350 \mathrm{v}$ \& $4 / 6$ \& $100+200 / 275 \mathrm{v}$ <br>
\hline \& $12 /-$
\end{tabular} PAPER TURULARS

$350 \mathrm{v} .0 .19 \mathrm{~d}, ; 0.51 / 901 \mathrm{mFd}, 3 / 4 ; 2 \mathrm{mFd}, 150 \mathrm{v} . \mathrm{S} /=$ S00v． 0.001 to $0.019 \mathrm{H}_{\mathrm{o}} ; 0.11 /-; 0.251 / 8 ; 0.52 / \mathrm{B}$ $1,000 \mathrm{v} .0 .001,0.002,0.005,0.01,0.021 / 8 ; 0.05$ ， $2,000 \mathrm{v} .0 .005,0.01 /$
$2,000 \mathrm{v} .0 .005,0.01,0.02,2 / 6 ; 0.05,8 / 6$.
Sab－min． $0.001,0.005,0.01$
Sub－Min． $0.001,0.005,0.01,0.02,0.04,0.05,0.1,1 /-$

SILVER MICA（tolerance 1pF）， 2.2 to 47 pF ， $1 /$ ditto $1 \% 50$ to $800 \mathrm{pF}, 1 /-1,000$ to $2,000 \mathrm{pF}, 1 / 9$ CERAMIOS $500 \mathrm{v}, 1 \mathrm{pF}$ to 0.01 mFd ． 9 d ．ench． TWIN GANGS．＂O－O＂ $208 \mathrm{pF}+178 \mathrm{pF}, 10 / 6$ ； 365 pF min．， $10 / \mathrm{c} ; 500 \mathrm{pF}$ standard with trimmer 9／6；midget with trimmers， $9 /-: 500 \mathrm{pF}$ slow motion atandard， $9 /-$ ；small $3-\mathrm{gang} 500 \mathrm{pF}, 19 / 9$ ．Single ＂O＂ $365 \mathrm{PF}, 7 / 6 \mathrm{SHORT}$ WAVE，Stogle 10 pF $25 \mathrm{pF}, 50 \mathrm{pF}, 75 \mathrm{pF}, 100 \mathrm{pF}, 150 \mathrm{pF}, 5 / 6$ each． Can be ganged together．Couplers 9i，each．
TUNING AND REACTIOR $100 \mathrm{pF}, 300 \mathrm{pF}, 500 \mathrm{pF}$ ． 3／8 each，solid dielectric．TRIMMERS Compresaion $205 \mathrm{pF}, 1 / 8$ ； $800 \mathrm{pF} 750 \mathrm{p} .9100 \mathrm{pF}, 150 \mathrm{pF}, 1 / 3$ ； HEADPHONES 2，000 ohms， $12 / 8$ ．
ELS4 Traneformer 0 ohma， $12 / 6 ; 4,000$ ohms， $16 / \%$ EL84 Oltra EL84 Ultra Linear Push－Pall， $10 \mathrm{w} ., 49 / 6$ ．
Standard Pontode S／6
TRANSISTOR MAINS
ELIMINATOR PPl＝6v．PP9－9v．2／96 DOUBLRS CE／B，PPI （4 4＋4）．Bive as batterien Aso min．9v．19／8．
Fermt Werrad P50 COILS
and 2nd I．F． $\mathrm{F} 50 / 2 \mathrm{CC}, 5 / 7$ Osc．P50／1AC，5／6；1st P50／3CC，6／；Driver Trans－LFDT4， $8 / 6$ Printed Circuit $9 / 6 ; 35$ ohm Speakers， $5 i n$
$17 / 6 ; 6 \times 41 \mathrm{n} .21 /$ Book $2 /$ ． 3 ohm OPT $10 / 8$ 17／6：6x4in．21／－Book 2／－． 3 ohm OPT 10／6 NEW MULLARD TRANSISTORS Koldart $1 / 8 ; 0671,6 / 5 ; 0078,7 / 6 ;$ OA810，9／6 OC81，7／6；AF115，10／6；AF114，11／\％；0044，8／
 ginicon Riccilpizers．OAS10 500mA，900v．8／6； BY100 560mA， $400 \mathrm{v} .10 \%$ ．
MAINS TRANEFORMERS Postag＊2／－ach STANDARD $250-0-250 \quad 80 \mathrm{~mA}, 6.3 \mathrm{~V}_{\mathrm{E}} \quad 8.5$
 MA．，or 4v，2A，22／6；ditto 350－0－360
MNLATURE $200{ }^{7}$ ．， $20 \mathrm{~mA} ., 6.3 \mathrm{v}$ ．，1／
8MDGEL $2207 ., 45 \mathrm{~mA}, 6.8 \mathrm{~T} ., 2 \mathrm{~m}$
$29 / 6$
$10 / 6$
$\begin{array}{ll}\text { E，MLL } 300-0-30070 \mathrm{~mA}, 6.3 \mathrm{v}, \text { ，} 4 \text { 复 } & 16 / 6 \\ 19 / 6\end{array}$

 GENERAL PURPOSE LOW VOLTAGE 2 amp． $3,4,5,6.8,9,10,12,15,18,24,30 \mathrm{~F}$ ． ATmp．vergion，taps and 4 taps up to 60 p ． 0\％．29／6 0－116，200，230，240\％150w，22／6；500w， $82 / 6$ TRANSIBTOR，9v．， 80 mA ．， $1+ \pm 1+ \pm 1$

## BEST BRITISH P．V．C． RECORDING TAPES


 Volume Controls 180 ohm 0 CABLE Lnear or Log Tracks Lang spindles，Midget $\begin{array}{ll}\text { LS．} 8 /= & \text { D，} 2, ~ M e g ~\end{array}$ Semb－air spaced tin
 Ideal 625 iines U．H．F Stereo L／S 10／6；DP． $14 / 6$
$\mathrm{~lm} \log +\operatorname{lmA} / \log .7 / 6$ Low loss $\mathrm{KdB} 1 / 6 y \mathrm{~d}$. TELDPCOPIC CHROME TELESCOPIC CHROME AERLALS， 12 to 33ıu．，6／B， TRIPLEXERS Bande I．I1，III，12／B，COAX PLUGB 1／－ OUTLET BOXES（Aurisce or tugh）4／－
BRLANCED TWIN FEEDERS，6d．yd．， 80 or 300 ohm TWIN SCREENED， $1 /$－per 7ard， 80 ohmo only．

THE＂INSTANT＂BULK TAPE ERASER AND RECORD HEAD DEMAGNETIZER $200 / 250 \mathrm{~V}$ A．C． $35 \%$

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 finin， $16 / 6 ; 10 \mathrm{in} ., 30 /-; 12 \mathrm{in}, 30 / \mathrm{m}$ ；（ $15 \mathrm{ohms}, 85 / \mathrm{m}$ ）；
 EMI 13 ₹ $81 \mathrm{l}^{2}$ ，ceramic，donble cone， 3 or $150,45 / \mathrm{m}$ WAVE－CHANGE SWITCBES， 2 p． $2 \cdot$ ซay or 4 P． 3．way， $8 / \mathrm{g}$ esch 8 or 1 p ． 12 －way； 4 p ． $2 \cdot$ ．was or 4 p ． WATE－CHAYGE＂MA
WAVE－CHANGE＂MAKITS＂available， 1 p ．12－why， 2 p．6－way， 3 p．4－way， 4 p．3－way， 6 p．2－way．K Price， 1 wafer 8／6；2－wafer 12／6； 3 waier 16／－，Extm wafers 3／4 each，extra long shafts 2／－extra，
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JACKS Standand open－ciredt 2／6，closed Grundis type 3－pho 1／3．gitan Grundig type $3-\mathrm{pho} 1 / 3$ ；Standard Lead Type $6 / a$ Phone Plogg 1／－．Bocket $1 /=$ ．Hanana Plugs $1 /-$ BULGIN HON－REV PLOGS and SOCKITG 2－pin 4／8；P73 3－pin 4／8；P194 6－pin B／6；Pit 12／B
 H W．
10 ohms to 10 meg．
5 watt 0.5 to 8.2 ohm 3 W
10 watt 15 wLRE－WOUND RESISTORS
15 watt 10 ohms－ 6,800 obus
MAINS DROPPERS Midget
$1 \mathrm{~K} ., 0.2 \mathrm{~s} ., 1.2 \mathrm{~K}$ ．， 0.15 s, ， Wirewonnd Ext．Spearer Controls $10633 /-; 25 \Omega 6 / 6$ WIRE WOUND POTS 3 WATT．Pre－set Mia．，TV Types，All valuea 10 ohms to 25 K ．， $8 / \mathrm{m}$ each， 30 K． W／－（Carbon 30K to 2 meg．， $3 / \mathrm{F}$
Wharew SPEAKER IREPT Tygan various culours，52in．Fide EXom $10 /=\mathrm{ft}$ ．；26in．wide from $5 /-\mathrm{ft}$ ．samples A．A．R． ARDENTE TRANSISTOR TRANSFORME日g $8 f$－ Da085 7.3 CT． 1 Push－Puy to 3 ohms output $11 /=$ D3058 11．5：1 Output 3 ohms， $11 / \mathrm{D}$ D001， $18 / \%$ D238 4．5；1 Driver，11／6：D240 8．5：1 Driver， $11 / 6$ TRANSISTOR POTS 5 K Switched VC1545 $\quad 5 / 3$ UB MIN EARPIECE Xtal or Masnetio

JIN JACE AND PLUG 2.6 or 3.5 min ．， $3 / 6 \mathrm{pr}$
TV REMOTE CONTROL for Philips 19TG111A， 121A，125A．142A，23TG111A，113A，121A，131A， Pug－in，with 11tt，7way eable，a DP switohes，dual pot，volume and brightaess．OA81 diode ete．．etc．
List 3 gns，New，boxed．OUR FRICE $19 / 6$ post tree． Blank Aluminium Chassis， 18 s．w．g．， 4 bldes，riveted $9 \times 7 \mathrm{~m}, \mathrm{~b} / 6 ; 11 \mathrm{xin} ., 7 / 6 ; 13 \times 9 \ln ., 9 / 8 ; 14$ I 11 inn



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ampess


[^4]etc. The latter was used successfully without laminations and a tapping was soldered on after exposing the primary layers by bending back one of the end cheeks. The exact position of the tap was not found to be critical.

## Practical Layout

No hard and fast rules are given as regards size of unit as this will be dictated $\mathrm{b}_{j}$ the components available to the constructor. If a $2 \frac{1}{4} \mathrm{in}$. loudspeaker is used an extremely portable unit may be built around it, particularly if resistance tuning is employed. Readers who are used to working from a theoretical diagram will no doubt have their own ideas about the practical layout and this should not present any problems. However, for the less experienced constructor and those who prefer to work from a wiring diagram a suitable layout is given.

A small tin box was used to house the experimental model, the loudspeaker and tuning control being attached to the lid. Construction was simplified as the tagstrip and the "earthy" side of components could be soldered directly to the case. One slight drawback was that initial tuning and calibrating had to be carried out with the lid closed as the proximity of the metal lowered the pitch about a semitone by increasing the inductance of the coil. With a plastic case the problem of hand capacity might arise.

A 9 V battery such as the Vidor VT3 was chosen because these are physically small but there is no reason why external batteries should not be used. Where space is no criterion a larger speaker may be utilised and this may have the more usual lowimpedance speech coil if it is connected through a transistor output matching transformer.
Advantage was taken of the case being metallic to solder one of the push-switch contacts to it, the other contact being soldered to one of the adjacent points on the tagstrip. A halt-men length of thick copper wite soldered to the "earthy" contact and fitted with a small length of sleeving serves admirably as a push button. A hole should be suitably drilled, as indicated in the diagram. for this to protrude slightly through the side of the case.
 Approximate values of the switched capacitors for the scale of A Major
( 3 sharps). The values for the chromatic semi-tones lie approximately
half-way between adjacent notes. half-way between adjacent notes.


Fig. 4: Dial for the $2 k \Omega$ potentiometer in Fig. 2.

## Calibration

Once the capacitors have been selected in the switched version a permanent scale can be accurately scribed as the 12 semitones will be equidistant on the positions of the switch. If the simpler resistor method of tuning is used, then there will be cramping towards the lower notes which could result in some slight pitch inaccuracies due to difficulties in reading the scale. Generally these would be too small to be serious.

Should the frequencies covered be too high in the musical range these may be lowered by increasing the fixed capacitor across the coil or, alternativelv, inserting an iron core in the coil.

## A COMMENTARY BY HENRY <br> practically <br> WIRELESS

## No. 17 Illogical Conclusions

THAT hilarious pantomime "The March of Progress" has earned a few deft sideswipes from Henry's bladder. Any jester worth his cap and bells could hardly miss a target so wide.

In the field of telecommunications it would seem that Progress -with a capital-is marching onward with the relentless determination of a hungry rhinoceros. Every trade magazine we pick up heralds new approaches, developments, devices and even ideas. Editors delight in crystal gazing or, unforgivably, reminding us how accurate their predictions of a half-century ago have turned out to be.

Bofins-not to be outdonebrush up their syntax and publish the intimate details of their experiments. Scribes like me absorb the gist and breathe out hot air about "The Sets of Tomorsow" or less precisely, "New Concepts". The innocent bystander may be forgiven for thinking us all a dynamic class of citizens, leading the backward plodders of Industry and Commerce into some brave new world beyond the horizon.

One has only to read the dismal history of Colour TV to see what is meant. In the November issue of Practical Television the Editor recounted his remarkable dream-which ended with a delegate to one of those interminable Colour Television Standards Conferences crying: "But do we really need colour TV?"

Mr. Sidney Bernstein and Lord

. . the relentless determination of a hungry rhinoceros.

Thomson, chairmen of Granada and Scottish Television respectively, have come out against premature launching. This does not mean that either of inese extremely astute gentlemen is a reactionary diehard. Their kick is not against progress, so much as against the effect mistiming of decisions may have upon their profits.

And to be sure, decisions are not likely to be timed at all if the last breakdown of talks, following hard on a hasty "final" SECAM demonstration, is indicative.

The ironic fact that Henry is trying to wrinkle out and lay before you, dear Reader, is that technical magazines were running series of articles on Colour TV Principles, or Servicing Colour Receivers as much as ten years ago.

These were based on American experience, to be sure. Yet it is worth remembering that it is only as lately as 1964 that the larger companies in the States were able to make Colour TV pay. Last year, for the first time, colour TV sales overtook black-and-white receivers. What price Progress?

Getting away from radio's foundling, let's ask each other: "What sort of wireless signal are you getting?" Short of stringing the surrounding rooftops with piano-wire pigeon traps and digging below plastic water-main level for the earth return, can you pick up interference-free programmes?

I thought not. Then, am I being naive in suggesting that a logical conclusion is some form of communal aerial system? To indulge in another Progress Prediction, the future should bring all communication services. radio, TV, what-have-you to the house via a single pipeline. Water, Gas, Electricity. Telecoms, each with its inaccessible stop-cock and horrible quarterly bill.

Rather like the Editor's dream, you may say. And after


Digging for the earth return.
reading of the furore at Cwmbran New Town last autumn, I'd be inclined to agree. There, the Corporation decided to be in the van of progress by wiring their beautifully planned houses for all services and putting a one-andsixpenny charge on the rates. But the concession was given to a relay company and the local traders came out strongly in protest to the local press. One can hardly blame them when the pipeline people are also their greatest rivals in the set retail business. There's not much living left in selling radiograms and tape recorders. Even if (see last month) Dame Progress hands us videotape on a plate.

The joke is that BBC? had just then opened in the area and both radio dealers and pipeline technicians were chasing madly up and down the Welsh Mountains in search of the u.h.f. signals. Considering the ban on rooftop aerials that is imposed in the New Town, developments should be of some interest to followers of the pantomime called Progress.
When colour TV does come along, we wonder what the residents who voted against the levy on the rates will say. Possibly : "I don't care about the bloke down the road, Jack, My 'Coronation Street' comes through OK".

That should please Mr. Bernstein, at least.

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| OBL | 8／－ | － $3 \mathrm{C4}$ | $2 / 8$ | $7 \mathrm{C5}$ 8／－ | $1-25 Z 60 \mathrm{~T} 8 /$ |  | $17 /$ | EB41 | 1／9 |  | $7 / 3$ | M1104 $7 / 6$ | RGl | 84 | +301 C329 |  | $\text { (11114 } 101-$ |
| OR4GT | －1818 | 6C5 | 4／－ | $7 \mathrm{Cb} \quad 8 / 8$ | 8 28177 $6 / 9$ | 9 － $\mathrm{C}^{\text {P }}$ |  | EB91 | $4 / 9$ <br> $2 / 3$ | EL91 | 2／6 |  | 6 EK34 | $65 /$ | U329 |  | QET103 \％／－ （iET 10410\％ |
| 1A3 | 2／6 | 1806 | $3 /-$ | $7 \mathrm{C7}$ 5／－ | －30Cl $6 / 6$ | 16 （7） |  | －EBC3 | $20 / 6$ | ELS 45 | $5 /$ | M10 $5 / 5$ | $9{ }^{\text {¢ }} 330$ |  | L14．3 | 9／6 | （iET 10410／－ （：ET＇据17／6 |
| TA4 1A5 | 12／6 | （608 | $3 / 6$ $10 / 8$ | $\begin{array}{ll}7 \mathrm{DH} & 15 / 8 \\ 715 & 14 / 6\end{array}$ | － $300 \mathrm{Cl5} 1010$ | $1-\mathrm{AC/BG}$ | G $22 / 6$ | EBC3\％ | 3i） $6 /-$ | Finsi60 | 2\％／－ | MS4B 20 | $9 \mathrm{sP4B}$ |  | 1404 | 9 | （：ET10円17／6 <br> （1ETH1112／＝ |
| 147 GT | 7／6 | 6010 | 10／8 | $\begin{array}{rrr}703 & 14 / 6 \\ 7 \times 7 & 7 /-\end{array}$ |  | 19 AC／s |  | EBC41 | $18 / 6$ | ELL20 | 16／4 | MnPl 12／－ | SP130 |  | USU1 | 15／2 | （＊ET113 6／9 |
| 101 | $4 /$ | 6C12 | 8／8 | 7H\％ $5 / 9$ | $\begin{array}{ll}30 \mathrm{Cl} \\ 30 \mathrm{~F} 5 & 9 / 3 \\ 3 / 3\end{array}$ | 3 AC／TH | Hl $10 /$ | EBC80 | 1 $6 / 3$ <br> 18  | EL822 | 2 22／6 | MU12／14 $4 / 8$ | 6 NP＇41 |  | V4020 | 6／6 | GFT114 6／8 |
| $1 \mathrm{C}_{2}$ | $81-$ | 5CD6\％ | 18\％ | 7R7 12／6 | 30 F 5 $7 / 2$ <br> 30 FL $9 / 8$ | 3 AC／TH | ¢1 $10 /$ | EBC90 | $\begin{array}{ll}1 & 3 / 8 \\ 1 & 5 / 6\end{array}$ | ELILS | （13／6 | $\begin{array}{lr}\text { MX40 } & 8 / 8 \\ \mathrm{~F} 37 & 10 / 8\end{array}$ | ${ }_{8 P 42}$ | 12 | VMP4 | $11 /$ | GETILIM\％ |
| 103 | 6／8 | 6CD 7 | 9／8 | 7 V 7 5／－ | 30FL | AC／ | 1 | EBFso | （ $5 / 6$ | EM34 |  | $\begin{array}{cc}\text { N37 } \\ \text { N73 } & 10 / 6 \\ & 281\end{array}$ |  |  | VMs | 12 | （E＇ГN73 9／3 |
| 105 | 5／－ | 6CH5 | $6 / 6$ | 7Y4 | 10 | AC | P2 121 | EBFS3 | （1） | E．a33 |  | $420 /$－ |  | 27 | $V \mathrm{PL}$ |  | GET\＆74 9／6 |
| 100 | 10／6 | 6CW4 | 24／－ | 8 D 2 | 301.151018 | ATP |  | LBF69 | 3 |  |  | K168 26／2 | T |  | VPeB | 9 | GEXI3 $3 / 6$ |
| 1 D 5 | 8／6 | 6D1 | $1 / 6$ | 9BW6 ${ }^{\text {d }}$ | $301.1711 / 6$ | 6 AZ1 |  |  |  | 71 | 15 | N339 25／－ | T1）${ }^{\text {a }}$ | 12 | VP4 | 14 | CEN：3）3／－ |
| 1DS | $9 / 8$ | 6D8 | 9／6 | $9 \mathrm{O}_{2} 3$ | $30 \mathrm{P} 412 / 2$ | －AZ31 |  |  |  |  | 3 | $3 / 6$ | 6 TlbL4 |  | VP4A | 14 | CEX ${ }^{\text {a }}$ 10／－ |
| 1FD1 | 6／ | 6156 | 3／－ | 9107 | $30 \mathrm{Pl2} \quad 7 / 6$ | 6 A 41 |  |  |  |  | 7 | P51 2／8 | TH4B | 10 | $\mathrm{V}^{2} 48$ | 12 | GEX45 8／6 |
| 1 FD 9 | $8 / 8$ | OE5 | $9 / 6$ | 10 C 1 | $30 \mathrm{Pl6}$ 5／8 | ${ }_{\text {B } 36}^{\text {A }}$ |  |  | 6 | EM884 | 81 | PABC80 6／ | THELC | C 10 | VP130 | へ | GEXis 11／6 |
| 196 | 6／－ | 6F＇1 | 9／8 | 10 C 2 12／ | $30 \mathrm{P19} 12 /$ | －B 349 |  |  | 4 | EM85 | 818 | PCs6 $9 / 8$ | TH300 | －14／0 | ypes | $2 / 6$ | GEX $6615 /=$ |
| 1H5GT | $7 / 6$ | 6F6G | $8 / 9$ | $101) 17$ | $30 \mathrm{PL1}$ 9／6 | $8{ }^{6}$ B719 | 10／8 | EC90 | $4 / 9$ $2 / 3$ | EM37 | 7／8 | $\begin{array}{ll}\text { Pe88 } & 9 /- \\ \text { Pe95 } & 6 / 8\end{array}$ | TH41 | 15／ | VP41 | 6／－ | MAT100 $7 / 8$ |
| 1L4 | 213 | 6F0GT | $7 / 6$ | $10 \mathrm{D} 211 / 8$ | 30PL13 10／6 | $6{ }^{\text {BLt } 3}$ | $10 / 8$ | EC91 | 2／3 | EN31 | 10／－ | PC95 $6 / 8$ <br> PC97 $6 / 8$ <br> 697  | TH233 | 3 6／ | VPl33 | 918 | MAT101 8／6 |
| 1LA4 | 17／6 | 6F76 | 5）． | $10 \mathrm{~F} 1 \quad 10 \%$ |  | $3{ }^{\text {a }}$ | 1 | HC91 | 4／6 | EN91 | 5／8 $5 / 6$ | PC97 PCO4 P／8 | TPロ： | 5 | VR75 | 21／－ | MA ${ }^{1} 1208 / 9$ |
| 1HA6 1 | 16／10 | 6 Fb | 51－ | $10 \mathrm{Fo} \quad 9 / 8$ | 30¢ L15 9／8 | 6 CK506 | 12／6 | ECO21 | $6 / 6$ $7 / 3$ |  | $5 / 6$ $7 / 3$ | ${ }_{\text {PCO }}$ | TP25 | －5／ | VR105 | $5 / 6$ | MATİ1 8／6 |
| 11D5 | 4／－ | 6F12 | 3／－ | 10 F 18 ll 9／9 | $\begin{array}{ll}35 / 51 & 12 / 6\end{array}$ | $6{ }^{6}$ | 19／8 | ECCS 2 | $7 / 3$ | FYol | $7 / 3$ $9 / 3$ | $\begin{array}{lr}\text { PCC83 } & 6 / 8 \\ \text { PCC88 } & 10 / 8\end{array}$ | TP＂520 | 2） $7 / 8$ | VR150 | $4 / 8$ | OA5 6／ |
| 11， 5 | $4 / 6$ | $6 \mathrm{~F}^{1} 13$ | $8 / 9$ | 10Lل3 6／3 | $35 A 52019$ | 0 CL33 |  | Lec3 3 |  |  |  | PCC88 10／8 | TYsibr | 11／8 | VT61． | 71 | OA10 6／6 |
| 1N5GT | $8 / 6$ | 6 Fl 4 | 28／5 | 10LD11 9／6 | 85L6GT 6／F | － $\mathrm{Cl}_{6}$ |  | ECCs 4 |  |  |  | ${ }^{\mathrm{PCCR}} \mathrm{PCO} 11 / 6$ | Uabç | 50 5／6 | VT501 | 8） | OA70 3／0 |
| 1 Pl | 8\％ | 6F15 | $6 / 9$ | 10 Pl 3 12\％． | 35W4 4／8 | －CV63 | 0／8 | EO |  |  | ， | PCCLs9 10／－ | UA1＇42 | $26 / 9$ | VL111 | $5 /-$ | OA73 3／－ |
| 1 1P10 | 4／9 | 6F16 | 6／8 | $10 \mathrm{P} 1411 / 6$ | $35 \mathrm{Z3}$ 16／2 | 2 Cver1 | 12／6 |  |  |  | $8 / 9$ | PCFAO 6／6 | UB41 | 1016 | V「120 | 10／－ | 0474 3／． |
| 1 P 11 | 5／－ | 6 F 17 | 12／6 | 1103178 | 35Z4GT 4／6 | CV429 | 19／－ | Eccal | 816 | L285 | 3／8 | $\begin{array}{ll}\text { PCFxy } & 8 /- \\ \text { Prbs }\end{array}$ | UBC＇41 | 1 6／3 | VU12 | 10／－ | $04813 \%$ |
| 1 RS | 4／m | 6Fl\％ | 18／5 | $115517 / 6$ | 35Z5GT 5／9 | CY | 16／4 | ECOs 2 | 4／6 | E2740 | $5 / 3$ | PuF84 8／6 | LBE＇d | 1 6／3 | VU133 | 7 I | OA85 3／－ |
| 184 | 5／－ | $6 \mathrm{~N}^{\circ} 2 \mathrm{~B}$ | $9 / 8$ | $11 \mathrm{ES} 1 \%$ | 40SUA 6／6 | CY10 | ＋6／6 | k0083 | 4／6 | E2，41 | $5 / 6$ $6 / 3$ | $\begin{array}{ll}\text { PUF88 } & 813 \\ \text { PC＇F801 } & 819\end{array}$ | UBF80 | 0 616 | W21 | $5 /-$ | OA86－／－ |
| 185 | 318 | 6F24 | 10／8 | 1246 8／3 | 41MTL 8／－ | －CY31 | 5／9 | ECC84 | 5 | E241 | $6 / 3$ $3 / 9$ | PCFrol ${ }^{\text {P（PF802 }} 10 / 9$ | UBF89 | 4 813 | W42 | 12／－ | OAy0 3／m |
| 1 T 2 | $291-$ | 6 F 32 | 3／－ | 12A8GT16／3 | 419TH 10\％－ | －D1 | 1／3 | ECC85 | $5 / 6$ $5 / 9$ | E2Z80 | $3 / 9$ $4 / 8$ | PCF802 PCF805 10／3 | UBL2I | $110 / 9$ | W61M | 24／6 | OA91 8／6 |
| 154 | 2／3 | 6 F 33 | $8 / 8$ | 12AC5 8／6 | 42 5／－ | － 15 | $15 / 6$ | ECu48 | 8／9 | EZ81 | $4 / 8$ $3 / 9$ | PCF805 $8 / 3$ | UC0： | $8 / 3$ | W63 | 10／6 | OA95 8／6 |
| 144 | 6／8 | $6 \mathrm{G6}$ | 2／6 | 12AD6 9／6 | $4310 /-$ | D42 | $10 / 6$ | ECC189 | 8／9 | EZ．90 | $3 / 9$ $14 / 6$ | PCF806 19／9 | UCus4 | $8 /{ }^{\circ}$ | W76 | $8 / 6$ | OA200 5／－ |
| $1 \mathrm{U5}$ | 618 | 6E6 | 1／6 | 12AR6 $8 /=$ | 45 17／6 | $1 \times 3$ | 10／6 | ECOC804 | 11／8 | FC2 | 14／6 | $\begin{array}{ll}\text { PCLEA } & 6 / 6 \\ \text { PCLS8 } & 9 / 6\end{array}$ | UCO85 | 6／6 | W77 | $8 / 6$ | OA211 18／6 |
| 247 | 12／6 | 6.55 | 3／－ | 12AH7 6 | 45260T $15 /$ | 1577 | 2／3／8 | ECC80 | 8／9 | $\mathrm{FCl}_{\mathrm{FCl}}^{\mathrm{FC}}$ | 8／9 | $\begin{array}{ll}\text { PCL88 } & 9 / 6 \\ \text { PCL44 } & 7 / 8\end{array}$ | UCF80 | 8／8 | W81M | 5／9 | OAZ20012／6 |
| 2028 | $2 / 9$ | OJSGT | $4 / 3$ | 12AH8 $10 / 0$ | 50A5 $21 / 10$ | DAC32 | 2／3 | ECF80 | 15／3－ | ${ }_{\text {FCl }}$ | 14／8 | $\begin{array}{ll}\text { PCLA4 } & 7 / 8 \\ \text { PCL85 } & 8 / 6\end{array}$ | CCH21 | $181 /$ | W101 | $26 / 2$ | OAZ：203 9／8 |
| 2D130 | 71. | 6J 6 | 3／－ | 12AT6 4／6 | 50B5 6／6 | DAF91 | 3／8 $3 / 8$ | ECF＇82 | 7／3 | FC130 | 1．1－ | PCL85 816 | UCH48 | 8／－ | W107 | 10／6 | OAT204 9／6 |
| 2 D 21 | 5／－ | 6J7G | 4／8 | 12AT7 $3 / 6$ | 50005 616 | DAF96 | － |  |  |  |  | L86 $\begin{array}{r}8 / 9\end{array}$ | UCH81 | 8／6 | W1729 | 17／6 | OAZ210 7／8 |
| 2 XQ | 3／－ | 6J7GT | 71 | 12AU6 $5 / 9$ | 50CD6G40／9 | DCe90 | － | ECFS04 | 4 24／－ | GT1C | 9／9 | PLLAR 12／8 | UCLA | $7 / 8$ | X14 | $7 / 8$ | OC16 W 35／ |
| 8 A 4 | $8 / 9$ | 6K80T | 5／6 | 12AU7 4／6 | 60L6QT 6／－ | D1）4 | $12 / 6$ | ECH3 | 424／3 | GU50 | 579 | 40D $84 \%$ | UF41 | 9／3 | X18 | $8 /$ | OC19 26／－ |
| 8A5 | $6 / 9$ | 6K76 | 1／8 | 12AV6 $5 / 9$ | $52 \mathrm{KU} 14 / 6$ | DD41 | $10 / 6$ | ECH21 | 10\％－ | G730 | 55／6 | PEN45 84\％＊ | CF41 UF4？ | 8／9 | X 24 | $18 / 8$ | OT 22 23／\％ |
| 3 B 7 | 5／－ | 6K7GT | 1／8 | 12AX7－ $4 / 6$ | 53EU 14／8 | DDT4 | $7 / 6$ | ECH33 | 22／8－ | ${ }^{4} 1832$ | 8／6 | PEN45 ${ }^{\text {PEN }}$ | UF43 | 4／9 | － 41 | 101－ | 0c23 87／－ |
| $3 \mathrm{H6}$ | $8 / 8$ | 6K86 | 8／3 | $12 A Y 7 \quad 9 / 9$ | 72 8／8 | UET＇25 | 716 | ECH3 | 6\％ | G1293 | 14／6 | 12\％． | TF80 | $8 / 3$ | X 61 | $8 /-$ | O（2）12\％ |
| 304 | $6 / 3$ | －K88TM | M8／6 | 12BA6 $5 / 3$ | 77 5\％ | DF33 | $8 / 6$ | ECH42 | 6／5 | G233 | 14／6 | PEN46 12／－ | C1F85 | $8 / 8$ | X 64 | 5／9 | OC26 8\％ |
| 300GT | 6／9 | 6 K 25 | 84\％ | J2BE6 $4 / 9$ | 78 4／9 | DF66 | 15／． | LCH81 | 5／9 | ${ }^{\text {a }}$（1837 | $14 / 6$ | PEN46 $4 / 7$ | CE86 | $9 / 6$ | $\times 64$ | $5 / 6$ | 642k 28／－ |
| 384 | 418 | 6 LI | 101－ | $12 \mathrm{BH} 78 /-$ | 80 5／3 | DF72 | $30 \%$ | ECH83 | 6／6 | H／237 H 30 | 14／8 | PEN38310／8 | UF89 | $5 / 6$ | $\times 65$ | $5 / 6$ | 0С29 18／6 |
| 3）4 | 5／－ | 6 L 50 | 12／6 | $12 \mathrm{El} 18 / 9$ | 83 V 81. | 1）F91 | 2／3 | ECH84 | 6／6 <br> 18 | HABC80 | 9／8 9 | PEN 4031） $10 / 6$ | UL4L | $7 / 6$ | د66 | 7／3 | 01433 9／6 |
| 4D1 | 819 | 6I6G＇T | 7／3 | 12H6GT $1 / 6$ | 85 A2 6／6 | DF＇96 | 6／－ | EOLR0 | 5／8 | HabCso HL2 | －9／3 716 | PENA $4^{10 / 6}$ | U1．4 | 8／6 | X 76 m | 8／8 | OC3is 21／6 |
| SR4GX | 8／8 | 6L7GTM | M 616 | 12J56T $2 / 6$ | 904G 67／6 | DF97 | 101－ | ECL82 | 8／8 | ${ }_{\text {HL2 }}$ | 7／6 | PENA4 ${ }^{\text {PEN／D }}{ }^{\text {7／－}}$ | ULX4 | 5／6 | $\times 78$ $\times 79$ | 28／2 | UC41 8\％ |
| 5T4 | $7 /$ | 6L18 | 101－ | 1237GT 7／8 | $\begin{array}{ll}\text { 90av } & 67 / 6\end{array}$ | DH30 | 15／6 | ECLS3 | $8 / 6$ $8 / 9$ | ${ }^{\text {HLis3 }}$ | 12／6 | PEN／DD <br> 4020 | CM4 | $17 / 6$ | ${ }^{\mathbf{X} 79}$ | 27／0 | OC4： $5 / \mathrm{L}$ |
| 3V4a | $4 / 6$ | 6119 | 19／． | $12 \mathrm{~K} 510 /$ | CG $49 \%$ | DH53 | ＋4／3 | ECL86 | 8／9 | HL23D | 12／6 | 4020 <br> PFL200 <br> 90／5 | UM34 | $17 / 6$ | X81M | 2911 | OC43 18／6 |
| 6V4G | 8／－ | 61．03 | 0／6 | 12K7GT 8／8 | 90 CV 42／－ | DH76 | 3／6 | EFs | $20 / 6$ | HL231 | 15／8 | PFL200 20／5 | UM80 | $8 / 8$ | $\times 101$ | 28／6 | OC4 4／9 |
| 5Y8GT | 419 | 6LD23 | $6 / 8$ | 12K8GT 8／6 | $\begin{array}{ll}90 \mathrm{Cl} & 16 \%\end{array}$ | UH77 | $3 / 6$ | EF9 | $20 / 6$ | HLA1以 | 13／8 | PL33 9／－ | UR1C | 6／6 | X109 | 206／ | OC44PM $8 / 8$ |
| 5Z3 | 6／6 | 6LD30 | 6／8 | 12476T 3／6 | 15082 18／6 | DH81 | 28／8 | EF22 | 20／6 | H1420 | D12／6 |  | UUS | 71／ | X 118 | $9 / 9$ | OC45 8／6 |
| $5 \mathrm{5C4}$ | 776 | 6N7CT | 7／－ | 129A7UT6／9 | $\begin{array}{rr}16082 & 18 / 8 \\ 10042 & 5 / 9\end{array}$ | DH101 | 25／－ | EF36 | $6 / 6$ $3 / 6$ | HL133 ${ }^{\text {H }}$ | D12／6 | $\begin{array}{ll}\text { PLi38 } & 16 /-\end{array}$ | UU8 | 11／． | X119 | $8 / 8$ | OC45 M 8\％ |
| $8 / 3019$ | 870 | $6_{61}{ }^{\text {P1 }}$ | 9／5 | 12907 4／－ | $\begin{array}{lr}161 & 15 / 8 \\ 161\end{array}$ | DH1071 | 16／11 | EFS374 | 3／6 | HN309 | 25／6 | PL81  <br> $\mathrm{PLS2}$ $6 / 9$ <br> 18  | UU78 | 11／－ | X 142 | 8／－1 | OC6s 22／6 |
| RA6G | \＄／9 | ${ }_{6} 8 \mathrm{P} 25$ | $6 / 6$ | 128 Cl \％$/ \mathrm{F}$ | 161 185\％34／11 | DH719 | 5／9 | EF39 | 8\％\％ | HN309 | 25／－ | $\begin{array}{ll}\text { PLC82 } & 5 / 3 \\ \text { PLB3 } & 8 /-\end{array}$ | UU8 | 14／2 | $\mathbf{Y} 63$ <br> $\mathbf{Y} 65$ | $5 /-$ | 0 O64 25／－ |
| 6489 | $5 / 9$ | 6P26 | 9／－ | 128178 | 185 BT  <br>   <br> 215 HG 3411 <br> $6 / 6$  | DK32 | 5／9 | EF40 | $8 / 8$ | HVR2 | $8 / 9$ $8 / 9$ | $\begin{array}{ll}\text { PLB3 } & 8 /- \\ \text { PLS4 } & 8 / 3\end{array}$ | UU9 | $5 / 6$ | Y65 763 | 5／8 | 0070 8／8 |
| $6 \mathrm{AB7}$ | 4／： | 6P28 | $11 / 8$ | 12857 8／－ | $\begin{array}{lr}215 N G & 6 / 6 \\ 220 B & 10 / 6\end{array}$ | DK40 | 15／6 | EF41 | $8 / 8$ | HVR2A | $8 / 9$ $5 / 6$ | $\begin{array}{lr}\text { PLS4 } & 6 / 3 \\ \text { PL500 } & 15 / 9\end{array}$ | UYYiN | 4／3／3 | Z63 | $4 / 6$ | OCT1 3／8 |
| $6 \mathrm{AC7}$ | $8 /-$ | 6Q7G | 4／8 | $129 \mathrm{K7} 3 /=$ | $\begin{array}{ll}220 B & 10 / 6 \\ 301 & 20 /-\end{array}$ | DK91 | 4／－ | EF4： | $6 / 8$ $3 / 8$ | 1W4／350 | －5／6 | $\begin{array}{cr}\text { PLL600 } & 15 / 9 \\ \text { PY84 } & 9 / 3\end{array}$ | UY1N | 10／3 | 766 | $7 / 3$ | Oc72 8／－ |
| 6 6as | 216 | 6870T | 7／8 | 12897 8／－ | $\begin{array}{ll}3(1) & 20 /- \\ 302 & 15 /-\end{array}$ | DK92 | $8 /-$ | ${ }_{\text {EFs0 }}$ | 2／9 | 1w4／350 | （ 5／6 | $\begin{array}{rr}\text { PY84 } & 9 / 3 \\ \text { PT15 } & 10 \%\end{array}$ | UY21 | 9／－ | 777 | $3 / 6$ | 0 O73 18\％ |
| 6AG7 | $5 / 9$ | 6 KTG | $5 / 8$ | 124887 | $\begin{array}{ll}302 & 15 /- \\ 304 & 15 \%\end{array}$ | DK96 | 6／6 | EF54 | 3／6－ | KBCes | 20／5 | $\begin{array}{cr}\text { PT15 } & 10 / \% \\ \mathrm{PX4} & 8 / \%\end{array}$ | UY41 | $5 / 8$ | $27 \div 9$ 7749 | 6／8 | Oc74 8\％ |
| ¢AJō | 8／6 | 6R7GT | 11／－ | $12056 \%$ | $\begin{array}{ll} \\ 05 & 15 / 7 \\ 16 / 8\end{array}$ | 1） | $6 / 6$ $8 / 9$ | EF3\％ | 3／－ | KEC35 | $20 / 5$ $12 / 6$ | $\begin{array}{ll}\text { PX4 } & 9 / 5 \\ \text { PX25 } & 8 / 6\end{array}$ | UY85 | 4／9 | 7749 | $9 / 8$ | $0 \mathrm{C75}$ 8\％ |
| 6AK5 | $4 / 9$ | 68A7 | $3 \%$ | 12 Y 4 2／－ | $18 / 6$ <br> $13 /-$ <br> 18 | 1）L35 | 5／－ | ${ }_{\text {EF80 }}$ | 5／8 |  | $12 / 6$ $11 / 6$ | $\begin{array}{ll}\text { PX25 } & 8 / 6 \\ \text { PY31 } & 6 / 9\end{array}$ | U10 ${ }^{\text {U12／14 }}$ | $9 / 8$ | 7759 | 36／－ | OC7E 8／8 |
| 6A K6 | 6／－ | 68C7 | 4／9 | 13115 | （13／－ | Llas | 5／8 | EF83 | $4 / 3$ $8 / 9$ | KL25 | 11／6 | $\begin{array}{ll}\text { PY31 } & 8 / 9 \\ \text { PY32 } & 8 / 9\end{array}$ | U12／14 | ${ }^{7 / 8}$ | Transis | fors | 0¢7\％12／ |
| GAK8 | 6／9 6 | 689\％ | 719 | 13D3 9／－ | 307 11／9 | DL72 | 15／－ | EF85 | $8 / 9$ $4 / 6$ | K LLL3 | 21／\％ | $\begin{array}{ll}\text { PY32 } & 8 / 9 \\ \text { PY } 31 & 8 / 9\end{array}$ | U16 | 15／－ | and diod | des | 0¢78 8／－ |
| 6ALS | 2／3 | 68G7GT | 4／9 | $14 \mathrm{H7}$ 9／8 | 956 2／－ | DL75 | 301－ | EF85 EF86 | $4 / 6$ $6 / 6$ | K ${ }_{\text {K }}$ | 5／\％ | $\begin{array}{ll}\text { PY3i } & 8 / 9 \\ \text { PY80 } & 4 / 9\end{array}$ | U17 U18／20 | 5／8 | AAl20 | 4／8 | OCb1 4／－ |
| 6AM5 | 2／6 0 | 68E7 | 3／－ | 15026 | ${ }_{1603}^{12031-}$ | DL92 | 3／9 | EF86 EF89 | 6／8 $4 / 3$ | ${ }_{\text {KT3 }}{ }^{\text {K }}$ | 15／\％ | $\begin{array}{ll}\text { PY80 } & 4 / 8 \\ \text { PY81 } & 5 /=\end{array}$ | U18／20 | 8／8 | AA129 | 4／6 | Gcisid 4／－ |
| 6AMB | 9／－ 6 | $68 J 7$ | 4／6 | 18 12／6 | $\begin{array}{ll}1622 & 18 / 8\end{array}$ | DL94 | 5／8－ | EF91 | $3 / 3$ | KT32 | 4／9． | $\begin{array}{ll}\text { PY81 } & 5 / 2 \\ \text { PY82 } & \text { 1／9 }\end{array}$ | ${ }_{\text {U19 }}$ | 48／6 | $\mathrm{A}^{(10} 10{ }^{\text {a }}$ | 14／6 | Ocxis 8／－ |
| 6AQ5 | 519 | 38K7 | $4 / 6$ | 18 10／6 | 2101 12／6 | DL96 | 6／－ | EF93 | 3／8 2／6 | KT33C | 29／1 | $\begin{array}{ll}\text { PY82 } & 4 / 9 \\ \text { PY83 } & 5 / 6 \\ \text { PY8 }\end{array}$ | U22 | $5 / 9$ | Ac－113 | $81-$ | 0682 10\％ |
| BARU 2 | $201-6$ | 68L7GT | $4 / 9$ | 19 AQS 713 | $408315 /-$ | DLs 10 | 10／6 | ${ }_{\text {EF97 }}$ | 2／8 | KT36 | 29／1 | $\begin{array}{ll}\text { PY88 } & 5 / 6 \\ \text { PY88 } & 7 / 3\end{array}$ | U45 | $8 / 6$ | ACl14 | $81 /$ | Oc8s 6\％ |
| 6AT8 | $8 / 6$ | 6aN7GT | 4／6 | 19BC6G80／5 | 4687 71／－ | DMM70 | 10／6 | EF98 | 10／－ | KT41 | $6 / 8$ $5 / 6$ | PY8R  <br> PY800 $5 / 3$ <br> 18  | U2H | $7 / 6$ | Acti ${ }^{7}$ | 9／6 | OC84 8／\％ |
| 6A U6 | $5 / 9$ | 6SQ7 | $6 /$ | $19 \mathrm{H1} 8 / \mathrm{c}$ | 5763 7／6 | UM71 | 9／9 | EF183 | 9／9 | ET44 KT （61 | 5／9 | PY800 <br> PY801 <br> 76 <br> 186 | U31 | 6／6 | A1140 | 25／6 | H1539 12\％ |
| 6A Y\％ | 516 | 48 T 71 | 12／8 | $20 \mathrm{D} 1 \mathrm{l}^{2} \mathrm{f}$ | 6067 10／－ | DW4／350 | $\begin{array}{r}\text { 9／9 } \\ \hline 8\end{array}$ | EF184 | $7 / 8$ $6 / 6$ | KT61 | 6／9 $3 / 9$ | $\begin{array}{ll}\text { PY801 } & 7 / 6 \\ \text { PY30 } & 8 / 6\end{array}$ | U33 | $13 / 6$ | A F＇tos | $27 / 6$ | $0 \cdot 140$ 19／－ |
| $6 \mathrm{B5G} 12$ | 216 | 6887 | 2／－ | 201228 | 71931 | DW4／500 | 08／6 | EF184 EH90 | $6 / 6$ $9 / 6$ | KT03 | $3 / 9$ $12 / 3$ | $\begin{array}{ll}\text { PY830 } & \text { 9／8 } \\ \text { Q1＇21 } & 5 /-\end{array}$ | U35 U37 | 18／6 | AF14 | $11 / 6$ | Or，170 8 8／8 |
| 83889 | 216 | 6U4GT | $8 / 6$ | $20 \mathrm{~F}^{4} 2 \quad 11 / 6$ | 7475 2／9 | DY86 | 6／8 | Ehis | 519 | KT74 | $12 / 6$ | $\begin{array}{ll}\text { Q121 } & 5 /- \\ \text { QP22B } & 12 / 6\end{array}$ | U47 | 29／－ | AFllio | 10／6 | OC171 0／\％ |
| 6 BA 6 | $4 / 8$ | 6U5G | $5 / \mathrm{m}$ | 20 L 119 | $9004 \quad 4 / 6$ | DY87 | $7 / 6$ | LL22 | 10／8 | KT88 | 12／6 | QP22B $12 / 6$ | U48 | $15 / 6$ $8 / 6$ | AFlif | 10／6 | $0620010 / 8$ |
| 6 BEG | $4 / 3$ | 6U76 | $71-$ | 20 P 11216 | 9006 216 | E80w | 24f－ | EL33 | 8／6 | KTW61 | 28／8 | QQVO3／10 $35 /$－ | U57 | 8／6 | ${ }_{\text {AF11 }}$ | 8／6 | OC201 29／－ |
| 6BL6 | $5 / 36$ | 6V6G | $8 / 6$ | 20P3 19／－ | 41834 20／－ | F83F | 24／－ | EL34 | $8 / 6$ $9 / 9$ | kTw61 | $4 / 8$ $5 / 6$ | Q ${ }^{\text {Q }}$（5180 $10 / 6$ | U50 | $4 / 9$ $4 / 6$ | AF118 | 20／－ | Oc203 14／\％ |
| ${ }_{6}^{68.6}$ | $5 / 66$ | 6V6GT | $5 / 6$ | 20 P 4131. | ACO44 9／－ | E684\％ | 18／6 | EL35 | 10\％ | KTW63 | $5 / 6$ $5 / 6$ | Q87520 10／6 | U52 | $4 / 6$ $4 / 6$ | A Fives | 11／－ | Occe ${ }^{2} 10 / 6$ |
| $6 \mathrm{B45}$ | $4 / 6$ | $6{ }^{6} 4$ | $3 / 8$ | $20 \mathrm{P5} \quad 11 / 8$ | AC2HL $10 / 6$ | E180F 1 | 19／6 | ELis6 | 8／9 | KTV41 | $5 / 6$ $5 / 6$ | QS150／159／6 Rio 15／－ | －7\％ | $4 / 6$ $3 / 9$ | AFI25 | 10／6 | OC206 10／6 |
| ${ }^{68 \mathrm{BP7A}}$ | 7／6 616 | 6×5 | 5／3 | 25ABG 7／8 | AC2PEN 11／6 | E1148 | $11 / 9$ | EL37 | 12／3 | LCB4 | 5／6 | $\begin{array}{ll}\text { Rio } & 15 /- \\ \text { Ri2 } & 5 / 6\end{array}$ | ［18 | $3 / 9$ $19 / 6$ | AFl26 AFl27 | 16／6 | OCP71 27／6 |
| $6 \mathrm{BR7}$ | $8 / 86$ | $6{ }^{67} 1$ | 12／6． 2 | $25 L 6$ | AC2PEN1 | EA50 | 1／6 | ELal | $12 / 8$ | LN152 | 5／9 | $\begin{array}{rrr}R 12 & 5 / 6 \\ \mathrm{R} 15 & 29 /-\end{array}$ | L101 V 107 | $19 / 6$ $17 / 6$ | AFlo | 98／6 | ORP12 $12 / 6$ |
| 6BR8 | 81－ 6 | 624／84 | $5 / .2$ | 25U4G＇T1a／7 | DD 12／6 | EA76 | 6／9 | EL．42 | 718 | LN152 | 5／9 $9 / 6$ | $\begin{array}{ll}\mathrm{R} 16 & 29 / 6 \\ \mathrm{R} 17 & 17 / 6\end{array}$ | प107 1191 | $17 / 8$ $9 / 6$ | AF7，${ }^{\text {d }}$ | 28／8 | ORPl2 $12 / 6$ |
| 6887 | 3／－ 6 | 6Z5G | 15\％－ | $25 \mathrm{y}{ }^{2} 719$ | AC5PEN $/$ | EABCSU | 6／9 | EL81 | $8 / 3$ | LN319 | $9 / 6$ $9 / 6$ | $\begin{array}{rr}\mathrm{R} 17 & 17 / 8 \\ \mathrm{R} 18 & 9 / 6\end{array}$ | 1.191 $C 551$ | $9 / 6$ $9 /-$ | 13 Y 10 y BY 105 | 8／． | TH2 12／6 |
| 68W6 | $7 / 67$ | 7471 | 12／6 2 | 25Y5G $7 / 9$ | DD 23／8 | EAAC91 | 3／3 | $\begin{aligned} & \text { EL8I } \\ & \text { ELS. } \end{aligned}$ | $8 / 3$ $6 / 9$ |  | $9 / 6$ $9 / 6$ | $\begin{array}{ll}1218 & \text { 9／8 } \\ \text { 1219 } & 8 / 9\end{array}$ | C451 | 9／－ | BY105 | 13／6 | TAS 15／－ |
| 6BW\％ | 51.17 | 786 1 | 12／6 | 2574G 6／6 | ACAPEN 4／9 | EAF42 | $3 / 8$ $7 / 8$ | $\begin{aligned} & \text { ELS3 } \\ & \text { ELo4 } \end{aligned}$ | $8 / 9$ $4 / 6$ | Ľ319 | $9 / 6$ $8 / 6$ | $\begin{array}{ll}1219 & 8 / 9 \\ \mathrm{R} 52 & 7 / 8\end{array}$ | U281 | $8 / 9$ | GD3 | 5／6 | V10／15A12／． |
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| 1 L | 51. | 6 CH | 1／9 | 64.7 | $8 /$ | 12A16 | $5 / 9$ | 301.17 | 12／8 | AZ1 | $8 / 9$ $7 / 18$ | 1；Brys | 519 | E1．41 | $7 / 3$ | PC | $8 / 3$ |  | 59／－ |  | 3／6 |
| IN5GT | 8／－ | 6456 | $41-$ | 6 H | 8／6 | IDA117 | 5／－ | 30 Pr | 141\％ |  | $12 / 8$ | EBLI | $17 / 6$ | E1．4： | $7 / 8$ | P！97 | $7 /-$ | 5130 | 10\％ | V7 | 10／6 |
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| 125 | 318 | bCDeat | $22 / 6$ | 68． 77 | 5／－ | ${ }^{2} \mathrm{RBE6}$ | 4／8 | 30 PL 13 | $12 / 6$ | C1，33 | $12 / 6$ | ECCMI | $3 / 3$ | E1．93 | 81 | Proses | 101－ | 8 Pr 1 | $1 /-$ | Y 41 | $4 / 6$ |
| 174 | 2／8 | 60hts | 81－ | ¢8K．：T | $4 / 9$ | 12 BH | $5 / 9$ | 301L14 | 12／6 | U431 | ${ }_{7 / 6}^{101-}$ | ECcest | $5 / 5$ | EMi34 | 91. | $\mathrm{p}^{\text {Proma }}$ | 8／6 | ${ }^{3465}$ | 19／6 | UY8， | 4／9 |
| 3 A 4 | 3／6 | 90．W4 | 14／－ | felatit | $4 / 9$ | 124.89 | $7 / 6$ | 35 A5 | 171－ | Dac32 | $7 / 6$ $3 / 3$ | Eccsa | 4／6 | EM801 | 6／－ | PTFs？ | $6 / 5$ | 862150 | $12 / 6$ | CR97 | 27／6 |
| 3 L 4 | 6／8 | 6L6 | $2 / 8$ | 68N76\％ | 4／－ | 12 N 1 | 19／8 | ${ }^{35} 5$ | $5 / 9$ 419 | TAF9L | 313－ | ECes 4 | $4 / 6$ 516 | EMB1 | $7 /-$ | PLWM | $8 \%$ | T＋L | 81. |  | B |
| 3Q5 | $6 / 6$ | 1） $\mathbf{E} 5$ | 519 | $6{ }^{6} 97$ | 81. | 195559 | $2 / 3$ | 35 W 4 | $\begin{array}{r}4 / 9 \\ \hline 101\end{array}$ | DAF96 | 6／－ | Ecres | 519 | EM8， | 61－ | PC1＊＊ | $8 / 6$ |  | $7 /$ |  | 30／－ |
| 384 | $4 / 8$ | －${ }^{\text {F＇1 }}$ | 9／－ | 6U4GT | 10／－ | 10376it | 7／3 | 3．）／4 | 101－ | Ince90 | 7／． | Lersy | $8 / 9$ | E8L1． | 2718 | Pr＇rayl | $9 / 8$ | TH41 | $201-$ |  |  |
| 361 | $81-$ | 5456 | 5＇ | 6U5（ | $7 / 6$ | 12ん70＇下 | 3／－ | 35\％40T | $3 / 9$ | ［ $\mathrm{F}^{3}$ 3， | 8／－ | ECuma | 8／8 | EY51 | $8 / 6$ |  | $9 / 9$ | －111 | \％ 7 |  | 30／－ |
| 5 R 44 | 8\％ | 6FGd | 4／－ | 6）M | 8／－ | 12K8けT | $8 / 3$ | $352 \overline{5}$ | $5 / 6$ | DF\％ | 51／ | ECFE＊ | $6 / \mathrm{C}$ | EY44； | $8 / 3$ |  | 1016 | U14 | 7\％－ | MP | 171－ |
| －U44 | $4 /-$ | －F\％ | 4／6 | 6Vb4 | 3／6 | 1．07， | $3 /-$ | 37 | 5／2 | 1）PGI | $2 / 6$ | Ecrex | 6\％－ | EZai | $4 / 9$ | PUESU0 | 12／－ | C19 | 30／－ | R105！ | $3051-$ |
| 5 V 44 | 8／－ | 6F11． | 12／6 | 6VmbT | 71. | 12AA7 | 6／6 | 42 | 4／8 | DF92 | $2 / 6$ | ECHES | $19 / 5$ | EZ40 | $5 / 6$ | PCFs | 12／6 | （025 | 101－ | V Rijol3 | 305. |
| 5Y3GT | 4／6 | 6F13 | $5 /=$ | $6 x^{4} 4$ | $3 / 6$ | $12 \mathrm{SG7} 7$ | $3 / 6$ | 50 B 5 | ${ }_{8 / 3}^{6 / 8}$ |  | 6／1－ | ECHH35 | 81－ | ERCX | 6／6 | PCLAz | 616 | U20 | 10／． | T＂45 | 12／6 |
| $5 \mathrm{Z}+\mathrm{GT}$ | 81 | 6 FL 4 | 12／6 | 6．259 | 4／9 | 1 LSH 7 | $2 / 9$ | $50 \times 5$ | 6／3 | DH7\％ | $8 / 6$ | ECHI81 | 8／6 | ELCB0 | $5 / 6$ | PCL88 | 8／－ | U7 | 3／6 | VT31 | 59／－ |
| 6／30L8 | 10／－ | EFU3 | $9 / 6$ | $6 \mathrm{C} 5+5$ | $7 / 8$ | 1：38．17 | $8 / 9$ | 5015 | 124／9 | DKさ2 | $7 / 9$ | ECHs | $8 / 6$ | EXZS1 | 3／8 | PCLS4 | 77 | U191 | 11／－ | ［111 | 6）－ |
| 6 A7 | 15／－ | $6{ }^{1} 16$ | $2 / 6$ | 786 | 11／－ | 12.8 K 7 | 2／9 | dir | 6／－ |  |  |  | $6 /$. | 4，230 | $8 / 6$ | PCL8： | $7 / 3$ | U231 | 11／6 | Vi20 | 101－ |
| 6 ABG | 6／6 | 6F5 | 1／3 | 787 | 7\％ | 128R7 | 3－ | 75 | $51-$ |  |  |  | $8 / 8$ | 1：733 | $91-$ | PuLats | 819 | U301 | 12／－ | C5518 | 251－ |
| 6 AC7 | $8 /$ | 6J5M | 6／6 | 7 C 5 | 101． | $14 \mathrm{H7}$ | 20／－ |  | 4／6 |  | 71 |  | $8 /$ | － | $9 / 8$ | PENA 4 | 201－ | U403 | 6／6 | W814 | 5 |
| 6 AK5 | 4／6 | 6.55 F | $2 / 6$ | $7 \mathrm{C6}$ | 8／－ | 19 AQ | $7 / 6$ |  | 0 |  | $4 / 9$ | ECLM | $8 / 6$ | KT3 | 22／6 | PENB4 | 20） | Uल61 | 18／6 | $\times 78$ | 28／6 |
| $6 \mathrm{AL5}$ | 31－ | 6J5GT | 4／3 | 7155 | $8 /-$ | 2011 | 10／－ | $8{ }^{\text {a }}$ A2 | 801 $8 / 8$ | $1) L 03$ | 4／8 | EF9 | 2015 | － | $17 / 6$ | EN4 | 6／－ | tabca | 5／6 | $\mathbf{X} 79$ | 25／－ |
| 6AM5 | $2 / 6$ | ${ }_{6}{ }^{3} 6$ | $\stackrel{*}{10}$ | $7 \mathrm{H7}$ | 5／－ | $20 \mathrm{~F}^{2}$ | $19 / 6$ | 80．20 | 818 | $1 \mathrm{DL93}$ | 6／6 | EF36 | 31－ | K T66 | 121． | EN | 2／9 | 1FAF42 | $7 /$ | X $111-5$ | 5／－ |
| 6AM6 | $2 / 9$ | 6．37M | \＄／6 | 7 F 7 | 18／－ | 20 LI | 12／6 | 150B2 | $11 / 6$ | ${ }_{\text {D1，}} \mathrm{DL} 9$ | $8 / 6$ | EFF37A | $9 / 6$ | K181 | 10\％ | PL36 | $9 / 6$ | U PC＇1 | $6 / 6$ | XP1－5 | 51－ |
| $6 \mathrm{AQ5}$ | 6／－ | $6 J 76$ | $4 / 3$ | $7 \mathrm{S7}$ | 18／6 | 20P4 | 14／－ | 150C4 | 12／8 | 101,96 | 81. | EF39 | $5 /-$ | KT＇48 | 20\％－ | ILB1 | 7. | UBC－ 1 | 71 | XSG1－5 | 10／－ |
| 6487 | 22／8 | 6J7GT | 71. | 7 Y 4 | 5／－ | 20 P 5 | 12／6 | 801 | $7 / 8$ | 10M70 | $51-$ | EF41 | $8 / 6$ | KTwi | 4／3 | $\mathrm{PLLS}^{\text {P }}$ | $5 /-$ | UBE80 | 5／9 | Y 63 | $7 / 6$ |
| 6AT6 | $3 / 6$ | 6K6GT | $5 /$ | 98W6 | 8／\％ | 25 Ab | $6 / 6$ $4 / 6$ | 807 | 10／－ | DY86 | 7／－ | EF50 | 21. | KTとき1 | 8／－ | PL83 | $6 /-$ | U EF59 | 6／3 | 3 ECl | $401-$ |
| 6AUB | 81. | ${ }_{6}^{6 K 7 M}$ | 5／8 | 10 Cl | 9／－ | ${ }^{2515 Y}$ | 6／－ | 806 9.54 | 101－ | DY87 | 718 | EPM0 | $4 / 6$ | mLa | 17／6 | PL®： | $6 / 3$ | UCC84 | 816 | 3FP7 | 12／6 |
| 6B8G | $2 /$. | 6K7 | 1／3 | 10 cz | 12／6 | ${ }^{25 Y 5}$ | 6／\％ | 16.25 | 5／－ | 2884C | 14／－ | EF85 | $4 / 8$ | MLO | $12 / 6$ | PL500 | 14／6 | UC085 | 616 | 5 CP 1 | $30 \%$ |
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| 6BE6 | $4 / 18$ | 6K8M | 8／6 | 10F3 | 12／6 | 3525 2586 | 8／6 | 4026AB | 10／6 | EABC80 | 8／6 | EF89 | 4／－ | MU14 | 4／－ | PY3\％ | $8 / 6$ | UCH42 | 71 | ACR13 |  |
| ${ }^{\text {6BH6 }}$ | 716 | 6 K 8 G 6 K 8 T | 8／8 | 10 Fr 18 | 9／－ | 2807 | 5／－ | 7198 | 1／6 | EAFter | $7 / 6$ | EF91 | $2 / 9$ | MX 40 | 12／6 | PY81 | 5／8 | UCH81 |  |  | 8.0 .0 |
| $6 \mathrm{BQ74}$ | 7／6 $7 / 8$ | 6K26 | $801 /$ | 10 Ll | 10／－ | $30 \mathrm{cl15}$ | 9／6 | 7475 | $2 / 6$ | EB41 | 4／6 | EF92 | $2 / 6$ | N37 | 10／－ | PY82 | $5 / 6$ | UCld |  |  |  |

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## ADDRESS


by J. B. WILLMOTT

IN a recent article in this magazine, describing the numerous uses to which the EF50 type valve, now so widely obtainabie from advertisers in this magazine at give away prices (freyuently as little as 1 s .6 d . each), the author made reference to a receiver designed and constructed over 10 years ago. This has given completely trouble free service, and accordingly a further prototype has now been constructed, using components currently obtainable. The receiver described here follows closely along the lines of the original design: it is capable of giving really good quality reproduction of local Medium and Long Waveband BBC programmes in good reception areas.

Obviously no "straight" (or superhet) receiver can give the same freedom from background noise or interference by Continental stations after dark.
as an f.m1. receiver; but in areas of good BBC reception, extremely good results are assured, at a fraction of the cost of purchasing or assembling an f.m. receiver. In areas where the Light Programme is strongly received on Medium Waves, such for example as London, the Long Wave tuning coils and the attendant complication of wavechange switching, can be omitted entirely.

A double-wound mains transformer is specified and thus the chassis of the completed receiver is completely isolated from the mains supply and therefore safe to handle. A direct earth connection is recommended and it is surprising how much improvement in performance and lowering of background noise results from this often neglected connection.

Layout is not unduly critical apart from the


Fig. 1: Complete theoretical circuit diagrom.
essential need to separate the r.f. and detector tuning circuits (achieved by mounting the respective tuning coils above and below chassis respectively) but it is suggested that the layout shown in Figs. 2 and 3 would be difficult to improve upon as it results in a neat and symmetrical disposition of components as well as ensuring shortness of wiring. A full list of all components required is given and there should be no difficulty in obtaining any of them from component stockists.

Briefly the circuit comprises an r.f. amplifier stage (V1), followed by an infinite inlpedance detector (V2), noted for its low distortion. Then follows an a.f. amplifier stage (V3), feeding into the power output stage (V4) power being supplied from the mains through a double-wound mains transformer with full-wave rectification provided by V5.


Fig. 2: Suggested underchassis layout.

## Preparation of Chassis and Component Mounting

A ready-made four-sided aluminium chassis, dimensions 10 in . $x 7 \mathrm{in}$. $\mathrm{x} 2 \frac{1}{2}$ in., which is a "standard" size, is specified and the details of drilling to be carried out are clearly shown in Fig. 3. The sizes of the various holes can be found by reference to the chart at the top of the diagram. The large valveholder cutouts are not all of the same size, a point which must be borne in mind, those for V1, V2 and V3 being $1 \frac{1}{2}$ in. diameter, V4 and V5 are $1 \frac{1}{8} \mathrm{in}$. diameter and the hole to accommodate C13 should be $1 \frac{1}{4} \mathrm{in}$. diameter. Established constructors will no doubt have the necessary range of screw-up-type hole cutters for the purpose but with patience these holes can be made by drilling a series of small holes around the circumference of each large hole, pushing out the centre blank and cleaning up with a file. This is admittedly somewhat tedious and investment in a set of hole cutters is strongly advised if any quantity of constructional work is envisaged in the future.
It will be noted that three of the holes marked "D" on the upper chassis surface and a further hole on the rear chassis should be fitted with rubber insulating grommets. It is through these holes that leads carrying mains supply or mains transformer connections will pass. The exact position of fixing holes for valveholders and the mainc transformer are best marked out on the chassis surface, using the actual components as a template. Make certain that the valveholders are positioned so that the locating spigots take up the direction indicated by the spigots in Fig. 2. The fixing holes for the two-gang tuning capacitor and the "I.B. Full Vision Dial Assemblv" are clearly shown. Obviously if any other make of tuning capacitor or dial assembly is used the position of these fixing holes will need to be amended. The
two holes " D " near the centre of the area occupied by the gang capacitor provide for connecting wires to the lower tags on the fixed plates of this component passing through the chassis to the wavechange switch.

Mounting of components can begin as soon as all drilling is completed and it is recommended that all valveholders be fitted first, using 6BA nuts and bolts. A solder tag should be secured under the chassis to the fixing bolt nearest pins 1 and 9 on V1 to V3 inclusive and nearest to pins 1 and 8 on V4. A further solder tag should be secured above chassis on the fixing bolt of V1 valveholder nearest the holes " E " midway between L 1 and L 2 positions and also to the fixing bolt of valveholder V5 nearest to the mains transformer.

Attention should now be turned to fixing the full vision tuning dial asserribly. This dial provides three-waveband indication but the short wave band is, of course, ignored in this design. The two-gang tuning capacitor is mounted on long 4BA bolts, using additional nuts (or brass spacers) to support it at the correct height above chassis for the spindle to accurately register with the driving boss on the drive assembly. Check to ensure that the drive operates smoothly and without strain before finally tightening the mounting bolts of the gang. It is advisable to solder a 6 in. length of connecting wire to each of the two-gang lower tags before mounting the component. these wires being fed through the appropriate holes "D". Ultimately they will be cut to length and covered by insulating sleeving when wiring-up is carried out.
Next mount the mains transformer. seeing that the primary winding tags are nearest the side of the chassis. This will ensure that mains supply leads coming up through the single hole " $D$ " are conveniently placed for connection to the primary winding, whilst secondary winding connections


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Fig. 3: Chassis drilling details.
utilise the two "D" holes to the right of this component. Now mount the electrolytic smoothing capacitor C 13 , using the clip specified in the components list, with its tags projecting through the hole " C ". Before wiring is commenced check that all components are in their correct position and firmly bolted down.

## Testing and Alignment

Before inserting valves and connecting to the mains supply the following check tests with an ohmmeter are highly desirable: First connect the meter across the receiver mains supply leads and check that when the on/off switch is turned to "on" the resistance of the primary winding of T2, some 20 to $50 \Omega$, is indicated. Now conneot the negative meter lead to chassis and the positive to pin 8 of V5, a momentary "kick" of the needle (indicating charging up the reservoir and smoothing capacitors), followed by a fall to almost opencircuit reading, should result. A reading of $50 \mathrm{k} \Omega$ or less indicates an unwanted path between h.t.
positive and chassis and must be investigated. before proceeding further.

Retaining the meter negative lead on the chassis, place the positive test prod on the cathode pins of V1 to V4 in turn and in each case a resistance indication corresponding to the value of the relative cathode resistor (see Fig. 1). Now remove the negative clip from the chassis, place the positive meter prod on the cathode (pin 8) of V5 and connect the meter negative in turn to the anode and screened grid pins of V4, the "anode" of V3 and V2 (comprising pins 2, 3 and 4 linked together in each case) and the anode pin of V1. In each instance continuity should be established and a resistance reading reflecting the value of the various dropping and decoupling resistors in circuit at the points tested.
If all the foregoing tests are carried out with satisfactory results the receiver can be connected to the mains with confidence. Remove test meter connections, ensure that on/off switch is in the "off" position. Insert all valves, conncut loud

## COMPONENTS LIST

Resistors:
RI 22 k
R2 $150 \Omega$
ik $\Omega$
$10 \mathrm{k} \Omega$
$47 \mathrm{k} \Omega$
$10 \mathrm{k} \Omega$
R7 $10 k \Omega$
All resistors $\frac{1}{2} W$ stated.

## Capacitors:

Cl $\quad 0 \cdot 1 \mu \mathrm{~F} 350 \mathrm{~V}$ paper
C2 $0.1 \mu \mathrm{~F} 350 \mathrm{~V}$ paper
C3 $0.1 \mu \mathrm{~F} 350 \mathrm{~V}$ paper
C4 $\quad 0.5 \mu \mathrm{~F} 350 \mathrm{~V}$ paper
C5 1000 pF mica
C6 200 pF mica
C7 $0.1 \mu \mathrm{~F} 350 \mathrm{~V}$ paper
C8 $8 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic
C9 $25 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic
Cl0 $0.1 \mu \mathrm{~F} 350 \mathrm{~V}$ paper
CII $8 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic
$\mathrm{C} 12 \quad 0.05 \mu \mathrm{~F} 350 \mathrm{~V}$ paper
$\mathrm{Cl} 3 \mathrm{a} / \mathrm{b} \quad 16+16 \mu \mathrm{~F} 450 \mathrm{~V}$ electrolytic
TCI 50 pF trimmer
TC2 50pF trimmer

TC3 50pF trimmer
TC4 50pF trimmer
$\left.\begin{array}{l}\mathrm{VCl} \\ \mathrm{VC} 2\end{array}\right\} 500 \mathrm{pF}$ J.B. 2 gang
Potentiometers:
VRI $500 \mathrm{k} \Omega$ carbon
VR2 $25 \mathrm{k} \Omega$ carbon with switch
Valves:

| $V 1$ | EF50 | $V 4$ | $6 V 6$ |
| :--- | :--- | :--- | :--- |
| $V 2$ | EF50 | $V 5$ | $6 \times 5$ |

V3 EF50
Miscellaneous:
LI Wearite PA2
L2 Wearite PAI
L3 Wearite PHF2
L4 Wearite PHFI
TI Mains Transformer "Douglas", 250-0-250V $80 \mathrm{~mA}, 6.3 \mathrm{~V} 3.5 \mathrm{~A}, 6.3 \mathrm{~V}$ IA.
T2 Output transformer $5000 \Omega: 3 \Omega$
Speaker $3 \Omega 8$ - 10 in . dia.
Chassis $10 \times 7 \times 2 \frac{1}{2} \mathrm{in}$.
J.B. "Full Vision" dial and drive assembly. SI 4 pole 2 way. 3 B9G valve holders. 2 . 10 . valve holders. Red "Pilot" indicator butb holder. 6.3 V 0.3 A bulb.
speaker and aerial (also earth if used) to appropriate sockets. Insert mains plug and switch on. After a few seconds the heater glow in V5 and V4 will be visible, then advance the volume control to maximum, when a slight breathing sound should be audible from the loudspeaker. Gently touch a screwdriver blade on the centre tag of VR1 and a loud mains hum should emanate from the loudspeaker, indicating that the a.f. stages are functioning. Removing and replacing the aerial lead should produce a loud "click" from the speaker indicating that the r.f. section is also functioning. Rotating the tuning capacitor should locate the local BBC transmitter. Clockwise position of the wavechange switch gives medium wave band coverage, anticlockwise gives long wave band.

As soon as a signal of some sort is heard adjust the trimmers on the appropriate aerial and h.f. coils (long or medium wave band, according to setting of SW1). With SW1 definitely in the m.w. position endeavour to tune in a station at the low wavelength end of the dial such as the BBC Light Programme on 247 m or Radio Luxembourg on 208 m , then adjust the trimmers (on L2 and L4) for maximum volume consistent with reasonably accurate station indication by the dial pointer. Slight adjustment of the pointer itself is permissible to obtain exact indication of station tuned to. Now swing the tuning capacitor towards the high wavelength end of the dial and the local regional and Third programmes should be received at the correct point on the dial as the J.B. "Full Vision" is designed to match accurately to Wearite " $P$ " type coils. Switch to long wave and, as the only station likely to be required will be the BBC Light


Fig. 4: PA2 coil connections
on $1,500 \mathrm{~m}$ set the pointer to this mark and adjust the trimmers on L1 and L3 for best results.

The receiver should be found to have more than adequate volume. even when used with a short " picture rail" aerial, within $30-50$ miles of BBC regional transmitters and a most pleasing standard of reproduction. Thanks to the employment of infinite impedance detection it will be particularly noticeable that transient sounds such as cymbals and other percussion instruments come through with especially realistic clarity, superior to all but the most expensive superhet or f.m. receivers. One final word: When inserting or removing EF50 valves a firm, straight pull (or push) is desirable. Any effort such as rocking from side to side in assist insertion or removal is liable to crack the glass seals around the valve base pins.


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1THE Basildon and District Amateur Radio Society was formed in 1962 by a number of licensed amateurs and short wave listeners living in the new town of Basildon and t'ie surrounding country area. The Club now has over fifty members of uhom twenty are licensed with a number of them. SWI 's sludying for the Radio Amateurs Examination or for the Post Ofice Morse tests. Club mombers cover a wide range of ages and professions, teenagers still at school and members in their sixties; firenien and chartered accountants.

Most of the licensed amateurs operate on the frequencies 160,80 and 40 metres. but there is strong interest in 70 and $144 \mathrm{Mc} / \mathrm{s}$ and 70 centimetres. G3EDM and G3ORT are keen mobile operators. G3PZZ and G3OIT are active on the DX bands. G3PGN and G3OQT can often be heard at weekends operating on $70 \mathrm{Mc} / \mathrm{s}$, while G3ASH and G3IJB are active on 144Mc/s.

The Club is affiliated to the Radio Society of Great Britain and each year enters for National Field Day. In 1963 and 1964 the Club won the Bristol Trophy, awarded for the highest score achieved by a single station entry.

The Club holds meetings twice a month: the first at the Bullseye Hotel, Town Centre, Basildon,
when wives and girl friends are cordially welcomed, and the second meeting, usually held in the thrd week of the nionth, is devoted to talks, junksales. lectures and film shows. This latter meeting is held in the Mayflower Restaurant, adjacent to the Van Gogh, Paycocke Road, Basildon. Members are advised of forthcoming activitues in a monthly newsletter.

Last year the Club visited the G.P.O. receiving station at Brentwood and later the transmitting station at Ongar, where great interest was shown in the equipment used by the Post Office. Envious eyes were cast on the masts supporting the transmitting and receiving aerials, but all cars were searched before leaving these stations by the chairman. Geoff Mills (G3EDM)!

In recent months visits have been arranged to the Marine Control Centre of Lathol Ltd., which controls the movement of all oil tankers entering or leaving the Thames: to the G.P.O. Telephone Exchange at Grays/Thurrock, and to the Communications Division of the Municipal Airport of Southend-on-Sea. For the winter months the Committee has planned a demonstration of portable and mobile equipment, a lecture on aerials. a film show. junk sales as well as an illustrated lecture on lasers.

The Society endeavours to look after the interests of those concerned with amateur radio, whether members or not, and is at present co-operating with the Company concerned regarding possible interference, from or to, the wired television system being installed in Basildon New Town.

The Club aims to bring the activities of the amateur world to the attention of residents in the district through the local press as well as the National magazines. It welcomes new members, whether licensed or not, and a letter to the Secretaries, B.D.A.R.S., Milestone Cottage, London Road, Wickford, Essex (Telephone: Wick ford 2462) will bring full details of membership. The subscription for those over 18 years of age is only 12 s . 6 d . per year-so come and join a really go-ahead Club.

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gutput ransi rroer, 40 e/g- $25 \mathrm{kc} / 9$ sutput 'ransi rracr, 40 e/e-25 kc/9,
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 cirut with ruli equalisation, with volurne, basa, trehbe and $\overline{5}$-pusition selector



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Illuminated peispex control pane: escutchega, $7 / 6$ extra. Fuur contemporary mounting lega tin. 10/0; 9 in. 11/6; orary mouning

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$2 / \mathrm{m}, 12 \mathrm{~V}$. WKG.
Condensers 150 F, working: $.01 \mathrm{mFrd} . .102 \mathrm{mPrd} ., 03 \mathrm{mFd}$. $.04 \mathrm{mFd} .0 \mathrm{~d}: 05 \mathrm{mF}, 1 \mathrm{mFd}, 1 / \mathrm{i}$ Midget Tuning Condensert. J.B. "OO" 208 pF and $176 \mathrm{pP}, 8 / 6$, ditto with trimmers, $9 / 6 . \quad \mathrm{J} . \mathrm{B}$. 220 pF and 105 pF conc riow Bub. miln. in. Dlemin 100 pF , Bub. miln. tin. Dlemin
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* Consumption 5 mA
* Audio respome- $10-20,000$ $d B|\mid d B$
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$16 \mathrm{Mc/s}$.
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