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PRACTICAL WI \\ R \\ JANUARY 1965 \\ $\square$ \\  \\ $\square$ \\ "Baty
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#### Abstract

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| TAPE AMPLIFIER FOR STUDIO DECK with ready wired printed circuit, confrol and input panela, mains |  |  |  | The uew MARTIN alf tranisior TEN WATT AMPLI- <br> FIER kits tepresent excellent value for money. Fach |  |  |  |
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Finished in polished veneered walnut. Ideal for vocalists and Public Address. Normally supplied for 15 ohm matching but can be supplied for 100 v . line for 35/- extra. Type C57, 10-15 watts. Fitted five $6 \times 4$ elliptical speakers. Overall size ${ }_{26 \times 9 \times 4 i n s .} 9$ Gns. Carr. Type Ca8. $15-20$ watts. Fitted five 8 in . high flux speakers. Overall size ${ }_{\text {approx. }} 4212$ GnS. Carr.
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(Half-day
Tuesday)

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250 m $\begin{array}{lll}450-0-450 v, 250 \mathrm{~mA}, 6.3 v, 4 a . \mathrm{C} . \mathrm{T} .5 \mathrm{v}, 3 \mathrm{a} & 59 / 9\end{array}$ Midset Battery Pentode 66:1 for 354 Mide
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S-33

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## Practical Wireless



Vol. XL No. 695 JANUARY, 1965

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## Is C.B. the answer?

FOR some years, a Citizens' Band has been authorised in the U.S.A. An operator does not have to pass technical or morse tests, but simply obtains a special licence from the F.C.C. This permits operation of low power equipment on $27 \mathrm{Mc} / \mathrm{s}$.

The introduction of a similar licence in this country has been sometimes mooted as a possible means to siphon off many wouldbe and actual pirates into more legitimate channels.

Superficially, it would seem that a good case can be made out for such a Citizens' Band, on its own merit, disregarding the question of piracy. Those in favour often quote the C.B. radio of the U.S.A. But what, in actual fact, is the situation in America? A recent report from the American Correspondent in a national newspaper is revealing:

Young radio hams are ruining television reception for thousands of viewers in New York, says the Federal Communications Commission. Their chatter causes jiggling lines on the picture tube. Their bad language is coming over loud and clear on the sound tubes. "We're getting 900 complaints a month-the situation is serious and is getting worse" said a spokesman.
Allowing for the rather quaint phraseology, this report lays bare the way C.B. radio has gone. It shows that even with power limitations, inexperienced and/or irresponsible operators can play havoc with their fellow citizens' pleasures.

In setting up C.B. radio, the F.C.C. have created a kind of electronic Frankenstein. And in view of the widespread abuses have now found it necessary to tighten up considerably on the issue of licences and to insist on restrictions in operating conditions.

Perhaps one mistake was to allow the Citizens' Band to degenerate into a sort of third rate amateur band. This was not the original intention. And, far from easing any problems caused by illicit transmitting, the so-called Citizens' Band has only served to aggravate the problem. It is clear then that C.B. is no magic formula, no panacea.

Going back to that report, note that the opening words are "Young radio hams". Now, we all know that C.B. operators are not radio hams, but nothing will convince the general public (and newspaper writers) that they are not. Thus the good name of amateur radio gets linked with the bad boys of C.B.

We feel therefore, that although the basic idea of a British C.B. may seem attractive, it could well rebound on us and worsen existing problems. But if we ever do get a C.B., the authorities must learn from the lesson of the U.S.A. and clamp down from the start on those who only want the facility as an easy way to play at being radio amateurs.


Our next istue dated February will be publighed on January 7th


## NEWS AT HOME AND ABROAD

13RITAIN'S newest cableship, the C.S. Cable Enterprise, arrived at Singapore during October at the end of her maiden voyage from Britain. She was joined there a day later by the cablelayer C.S. Mercury, and from here the two ship, left a few days after to make the final lay of the South East Asia section of the Commonwealth telephone cable (SEACOM).

## R.S.G.B. COMPETITION AWARDS

A $^{\text {S }}$ usual at this year's. International Radio Communications Exhibition, a number of trophies for equipment construction ability were awarded 10 winners of the various competitions.

The "Home Constructors' Plaque" this year was awarded to H . Rogers, G3NHR, for his 1.8 and $144 . \mathrm{Mc} / \mathrm{s}$ transmitter. The "Manufacturers' Plaque" went to T. Withers (Electronics) Lid.., for their T.W. Communicator and Sven Weber won the "Horace Fremman Trophy" with his audio frequency peak level meter and $435 \mathrm{Mc} / \mathrm{s}$ tunnel diode amplifier. The "Amateur" Amateur Award-open to contestants having no professional connections with the electronics industry-was presented to L. J. Hodgkinson, G3LLJ.

Other awards (for nlembers of the RSGB outside Region 7) went to M. D. Mason, G6VX and Basil O'Brien, G2AMV whose entries were a linear amplifier and an electronics keying unit respectively.
Apart from the constructional contests, a Hammerlund HO 170A receiver was awarded to the holder of a lucky entry card, who this year was Mr. Horace Freeman. late RSGB Adverticement Manager.
The winner of the RACAL RA. 71 receiver competition, the proceeds of which were donated to the Imperial Cancer Research Fund. was Mr. Buckby of 62 Wheater Avenue, Corby, Huntingdonshire. His guess of 1911 as the number of solder joints in the receiver was the nearest made to the actual number of 1910 .

## "Practical Wireless" Film Show

IN order to give readers every opportunity of obtaining entry to the annual Practical Wireless Film Show, those interested in attending this year are invited to send for their free tickets now.

As in previous years, the Film Show will be held in collaboration with Mullard Limited at the Caxton Hall, Westminster. It will be held on 'February 5th.

Although the programme has been arranged to interest the amateur radio enthusiast, the selection will make it an entertaining as well as informative evening, with refreshments provided.

Films to be shown include "Electromagnetic Waves" and "The New Panorama Tubes".

Last year the P.W. Film Show attracted more readers than ever, attendance being well over the 400 mark. This year as many if not more are expected to attend and so only immediate application to the Practical Wireless offices, enclosing a stamped addressed envelope can guarantee a seat.

Both these ships belong to Cable and Wireless Limited, whose task it has been to lay the 2.000 nautical miles which form SEACOM. During final operations, C.S. Cable Enterprise provided navigational cover and marked the route with buoys which C.S. Mercury followed to lay the last 700 miles of cable.
Terminal points on the cable are at Singapore, Jesselton and Hong Kong and because of the monsoons of the South China Sea, operations had to be completed before November.
With the completion of SEACOM and its inauguration at the beginning of February, communication facilities will be greatly improved throughout the area and with the eventual extension of the link to Australia and thence via COMPAC and CANTAT to international telephone circuits, the region will be further opened up to the world.

## New R.S.G.B. President

THE Council of the Radio Society of Great Britain has appointed Mr. E. W. Yeomanson to the office of President of the Society for 1965.

Mr. Yeomanson has been a member of the Council since 1958 and until this appointment was Executive Vice-President.

Mr. Yeomanson, who holds an amateur transmitting licence with the callsign G3IIR, has been in the telecommunications industry for 30 years.

## DEMONSTRATION OF MICROWAVE POWER TRANSMISSION

$\mathrm{A}_{\text {of }}^{\mathrm{N}}$ impressive demonstration of microwave power transmission was recently staged by the Raytheon Company at their laboratory in Burlington, Massachusetts.

During a demonstration for visiting officials of the U.S. Air Force's Rome Air Development Centre ( RADC ), the 6 ft . rotorspan "helicopter" shown under
inspection in the accompanying photograph, climbed 50 ft . into the air under the power of invisible energy provided by a microwave generator on the ground. (The vertical wires in the photograph are merely guide lines.)

The microwave energy was heamed towards the helicopter by a saucer-shaped transmitting aerial situated directly beneath it.


Raytheon's "helicopter" used in a recent demonstration of microwave power transmission.

## I.E.E. Christmas Holiday Lecture

THE annual Christmas Holiday Lecture for older school children arranged by the Institution of Electrical Engineers will be delivered this year by Dr. D. H. Parkinson, D.Phil., of the Royal Radar Establishment. The lecture, which is intended for boys and girls of the fifth and sixth forms. will be given in the lecture theatre at Savoy Place on Wednesday, December 30th, at 2.30 p.m., and will be repeated the following day at the same time.

Dr, Parkinson will talk on "Superconductivity" (an electrical condition appearing in certain elements, compounds and alloys when cooled to temperatures nearing absolute zero) and will illustrate his lecture with slides, films and demonstrations.

Admission to the lecture is free, and application for tickets stating for which afternoon they are required should be made to the Secretary, the Institution of Electrical Engineers, Savoy Place, London, W.C. 2

The helicopter's square platform, mounted under the rotor, is in fact the " receiving" aerial, mado up of thousands of tiny diodes, each less than half-an-inch long. This array collects the transmitted beam and the diodes rectify the microwave energy into an immediate source of direct current electricity. This electricity is then used to power the small motor which turns the rotor blades of the helicopter.
This demonstration served to provide an intermediate indication of Raytheon's progress with an RADC commission to develop a helicopter device using power transmitted continuously from the ground without the use of wires. Apart from the academic interest in wireless power transmission raised by the demonstration, it seems as though practical applications for "flying platforms" on the lines of the experimental helicopter, could be developed and used for television transmissions, missile detection, aviation beacons, navigational and weather aids, and surveillance. Continued development will, of course, be necessary to make it possible for a flight vehiclo to keep itself continuously in the path of the microwave power without the use of guy linea

## AIRLINES ORDER MORE EQUIPMENT

TWO recent orders for Marconi radio equipment have come from two of the world's leading airlines, Qantas of Australia and British United Airways.
The equipment to be supplied to Qantas is the latest Marconi doppler navigator. This equipment will be installed in their fleet of Boeing 707 aircraft operating their new trans-Pacific route. The doppler equipment is transistorised and forms part of the widely-used Marconi Company's Sixty Series of aircraft radio equipment.
The other contract also involved Sixty Series equipment, and Vickers VC-10 aircraft, currently operating B.U.A.'s flights to South America, are provided with navigation and communication facilities by this Marconi equipment for the 7,900 mile flight.


## for 1-5-3 Mc/s

BY F. C. JUDD

THE basic principle of finding the direction and ultimately the location of a radio station was discovered early in the history of radio and has since remained almost unchanged.

The different applications are far too numerous to mention here, but in addition to straightforward location of radio stations the " loop" system of direction finding is now widely used by yachting
and motor cruising enthusiasts on open sea and to this end there are several types of ferrite loop d.f. sets available for operation in conjunction with the longwave coastal beacon stations. These beacons are extensively used for position location and homing.

The loop aerial can also be used very effectively for reducing interference from unwanred radio signals or electrical noise and is equally effective in locating electrical noise sources.

The interest in radio direction finding is also quite prominent with members of various radio societies and R.S.G.B. groups who annually sponsor direction finding contests. These are usually for the 160 m amateur band, for which the d.f. aerial described in this article was designed.

Earlier types of d.f. loop usually consisted of several turns of wire on a square frame, the number of turns depending on the frequency of operation. The loop was therefore tuned to resonance at the required frequency.

An unscreened loop of this kind was quite favourable for general reception, but not very accurate for d.f. For this purpose it was better to "screen" the loop so as to neutralise the self capacity of the winding. This type of loop is, however, large and not greatly sensitive.

Nowadays the ferrite rod aerial is used almost universally for domestic receivers because of its much greater sensitivity. This type of aerial also has highly directional properties and can be made to operate in exactly the same way as a wire loop type aerial. Even an unscreened ferrite rod aerial will provide a reasonably accurate bearing so long as it is not influenced by other conductors or by poor balancing within its own circuit.

Any loop aerial behaves somewhat like a half wave dipole aerial, i.e., it has a polar response like a figure of eight. In the case of the ferrite aerial maximum pick up is broadside to the rod with minimum pick up at each end. These are referred to as the maxima and minima (null) respectively and will be explained in more detail later.

Ferrite rod d.f. aerials are very easy to make and consist of the rod. a tuned winding and a coupling winding. The ferrite rod should be as long as possible. 8 to 10 inches. and of a grade suitable for the highest frequency of operation. The diameter is not greatly critical but should be tin. to tin. for best results.


COMPONENTS LIST
Resistors:
R1 $10 \mathrm{k} \Omega$ R3 Ik $\Omega$
R2 $68 \mathrm{k} \Omega$
All $10 \% \frac{1}{2} \mathrm{~W}$ carbon.
Capacitors:
C1 ${ }^{0.01 \mu \mathrm{~F}} \quad \mathrm{C} 2 \quad 0.01 \mu \mathrm{~F}$
VCI 50pF variable
VC2 300 pF maximum variable
Miscellaneous:
LI, 2 Aerial coil, see text. L3, 4, 5, Transistor tuning coil (Denco range 3, yellow). TrI OC44. SI Single-pole on/off switch. Ferrite rod. $70 \Omega$ coaxial cable.
Fig. I: The circuit of the transistor r.f. amplifier with the ferrite rod aerial arrangement on the left.

Fig. 2: Here the mechanical construction of the d.f. loop is illustrated. Few dimensions have been given as neither these nor the general layout are critical.

Mullard Ferroxcube grade B2 is suitable for medium and longwave with B3 for below 200 metres or, of course. for either of the three bands. Direction finding below about $3 \mathrm{Mc} / \mathrm{s}$ is not very practicable with loop or ferrite rod aerials.

The ferrite direction, finding aerial shown in the photograph on the cover was designed for operation from 1.5 to $3 \mathrm{Mc} / \mathrm{s}$ in order to cover the 160 metre amateur band of 1.8 to $2 \mathrm{Mc} / \mathrm{s}$. It is intended for use with any receiver covering the same frequency range.

The aerial, its attendant r.f. amplifier and turning box, etc., are mounted on a collapsible tripod as shown in the photograph. The circuit of the ferrite d.f. aerial and its r.f. amplifier is shown in Fig. 1. Although the

Fig. 3i Winding details of the ferrite rod aerial.
loop alone would operate directly with a sensitive communication receiver, the transistor r.f. amplifier does provide a very useful gain.

General constructional details are shown in Fig. 2 but aside from continuity of the screening, etc., the actual electrical layout is not critical. It is important, however, to wind the aerial coils as shown in Fig. 3 and to screen the tuning capacitor $\mathrm{VC1}$.

It is equally important to completely screen the r.f. stage because any direct signal pick up here would result in inaccurate bearings. On no account use steel or tinplate in the construction of the screening tube or the r.f. amplifier box. Only aluminium dural, brass or copper can be used. Details of the slotted ferrite aerial screen are given separately in Fig. 4.

Fig. 4: A detailed construction diagrom for the slotted ferrite aerial screen and its support.



Fig. 5: Fixing a map position from two stations of known locations.

The tuning gear consists of various Meccano parts as shown in Fig. 2 although, if desired, the worm and gear etc., could be dispensed with and the aerial turned by hand.
The aerial coil L1 should be tightly wound and the winding secured with cellotape or a cellulose fixative. The link coupling coil L2 is wound over the exact centre of the main winding. Each leg of the link winding is screened as shown and the screening braid bonded to earth at either end.

The tuning capacitor VCl is isolated from earth and must therefore be mounted on an insulating bush or small panel let into the side of the screening box.
The compass used for the prototype was a small aircraft type although any small hand compass or car compass could be used. The compass will not be affected by the ferrite rod providing it is mounted as shown in Fig. 2.

The aerial and the r.f. stage tuning canacitors are separate and are therefore tuned separately. Initial tests should be carried out on strong sienals from local stations because the tuning of both.'e aerial and r.f. stage is very sharp. It will be found advantageous to use a changeover switch so that the receiver can be switched to the normal receiving aerial or the d.f. aerial.
It is easier to find and tune a station on an open aerial first, but remember that when taking a bearing all other aerials must be disconnected and not connected to earth or any other equipment.

## Checking the Accuracy of the Loop

There are numerous causes of inaccuracies and of these other aerials, in fact any conductors that


Fig. 6 (o): The co sine pattern of the normal ferrite aerial; (b): the cardioid pattern obtained when a sensing aerial is coupled to the d.f. aerial.
can re-radiate are most likely to produce them.
Don't forget that the compass can also be affected by nearby magnetic metals such as drainpipes and even more so by loudspeaker magnets etc. For this reason the co-axial line between the d.f. aerial and the main receiver should be about six feet long so as to keep the compass clear of magnetic fields etc.

One important check is to make sure that the receiver and co-axial line etc., are not picking up signals when the r.f. amplifier of the d.f. aerial is switched off. Any pick up except from the d.f. aerial itself will result in inaccurate bearings.
Make initial tests by taking " fixes" on stations whose locations are accurately known. A.d.f. is taken on the null or minimum signal. Check these with a map and protractor and see that the reciprocal of the bearing obtained comes back to your own position.

Don't forget to add approximately $10^{\circ}$ to the compass reading to allow for the difference between magnetic North and true North. The diagram of Fig. 5 shows how a fix on your own position is taken.

For finding the true position of a station whose location is unknown it is necessary to take a fix at each of two different places. The distance between these two places will denend on the distance of the station and its general direction.
This is where a sensing aerial can be useful although it is not absolutely necessary. A sensing aerial is coupled to the d.f. aerial so as to alter the pick up pattern from co-sine (figure of eight) to cardinid as shown in Fig. 6.
Signals from the sense aerial are added in phase to those from the d.f. aerial so that when this is tuned only one maxima and one null is obtained. Either can be used to determine the general direction of the station.

The sense aerial is then disconnected and a minima obtained on the station. This will not show

Separate oscillator and aerial tuning makes alignment of this circuit easy.

## BEGINNER'S SUPERHET SXX



IHIS receiver is designed to avoid the difficulties which often arise in aligning aerial and oscillator stages. It is usual to employ a ganged capacitor for aerial and oscillator tuning and efficiency falls off badly if tracking of these circuits is not correct.
This difficulty, which can be particularly troublesome for an inexperienced constructor, is overcome by using separate oscillator and aerial tuning capacitors. This arrangement gives maximum efficiency and the trimming and padding capacitors otherwise required are eliminated.
in the long wave position Cl and. $\mathrm{C4}$ are added and this allows tuning to $1,500 \mathrm{~m}$ for the Light Programme. This system avoids the need for separate aerial windings, etc., and gives yery good signal strength.

The remainder of the circuit is of straightforward type and neutralising is not used in the intermediate frequency stages. This fiuther

## by R. F. Graham



Fig. 1: The complete superhet circuit.

The circuit is shown in Fig. 1, VC1 being the aerial tuner and VC2 the oscillator tuner. The aerial is wound so that the whole medium wave band is covered. When the wavechange switch is
reduces the number of components. Antomatic volume control is applied to Tr2 through F6\%in the normal way. Tr4 is an QC81D, followedr- by a matched pair OC81s for Tr5 and Tr6.

rig. 2: Connections between the front panel (controls and aerial) and the chossis, and the layout of components.

## Ferrite Aerial

This is shown in Fig. 2. Paper is wound round the rod and the $26 \mathrm{~s}, \mathrm{w} . g$. enamelled wire is fixed lin. from the rod end at point "A". This can be done with adhesive tape. Seventy-four turns are then wound on side by side and the small loop "B" is made. Another 12 turns are wound on in the same direction and the wire is secured at "C" with tape.

End " A" goes to the stator (fixed plates) tag of VCl. Tapping " $B$ " is extended by a lead soldered to $C 2$. End " $C$ " is taken to the rotor (moving plates) tag of $\mathrm{VC1}$ and to metal panel earth line.

The rod is mounted on two pieces of wood about $1 \frac{1}{2} \mathrm{in} . \mathrm{x} \frac{1}{2} \mathrm{in} . \mathrm{x} \frac{1}{\mathrm{t}} \mathrm{in}$. These are cut to fit the rod (Fig. 2) and are held by countersunk wood screws through the metal panel. String or thread through small holes binds the rod to the mounts.

## Construction

The receiver is wired on a paxolin board 8in. x $2 \frac{1}{2}$ in. and $\frac{1}{16}$ in. thick. Aluminium 8 in. $x 3 \frac{1}{2}$ in. has a flange about $\frac{3}{\text { in }}$. wide bent along one edge. The flange is bolted to the paxolin board. The variable capacitors, volume control and switch fit to the aluminium panel and the finished receiver is fitted in its cabinet by two screws through the panel into the cabinet front.
Space under the paxolin accommodates the speaker and battery. A $3 \frac{1}{2}$ in. unit (overall) can be fitted or an oval unit A very small speaker is not recommended.

If a suitable cabinet is to hand the positions of VC1, VC2, volume control and wavechange switch may be adjusted to suit. No changes to wiring on the paxolin panel will be needed.

## Circult Board

The positions of holes can be found by placing the paxolnn under Fig. 3 and marking with a sharp-pointed tool. All the small holes are then made with a $\frac{1}{\delta} \mathrm{in}$. drill. A $\frac{1}{8}$ in. drill can be used for the three $6 \mathrm{~B} . \mathrm{A}$. bolts and to clear the oscillator coil and i.f. transformer pins. Each of these components has two can tags which pass through holes.
T1 is held by its wire ends. T2 is secured by lugs which pass through slots and are bent over. These slots can be made by drilling $\frac{1}{1}$ in. holes side by side.

It is best to drill all holes before mounting any parts and to clear away dust and fragments. When all holes have been made from Fig. 3, components can easily be inserted.

The volume control, switch and variable capacitors are mounted on the panel as in Fig. 2. The slide switch needs a slot, made by drilling holes and cleaning up with a small file.

The flange on the panel is drilled to match the paxolin board and three 6B.A. bolts hold these items together. A tag is placed under each bolt head and under the nuts. Construction is easier if the ferrite rod VRI and the variable capacitors are left off until last.

## Top of Circuit Board

This is shown in Fig. 2. All the resistors except R3 may be added first. The colour coding is given in the components list to avoid any errors here. The wire ends are bent to pass through the circuit board holes. The bend should not be immediately against the resistor body. R16 and R18 must be 5\% tolerance.

Capacitors C5, C10, C11, C12 and C13 are electrolytic and their positive and negative ends are placed as in Fig. 2. All the other capacitors can be inserted either way round.

The oscillator coil has a coloured spot between pins 1 and 6 and this must face transistor Trl, Fig. 2. The transistors are left off until other wiring is completed.

## Under the Circuit Board

A 22s.w.g. (or similar) bare tinned copper wire is soldered along the three tags and provides an earth return for numerous leads. For connections elsewhere 26 s.w.g. tinned copper wire with 1 mm sleeving is most convenient. Connections are shown in Fig. 3.

The oscillator coil and i.f.t. can tags should first be earthed. The resistor and capacitor ends can then be bent over, cut and soldered. Insulated sleeving is only required where wires cross. R3 is soldered from pin 5 of the oscillator coil to pin 3 of IFT1.

As leads are placed and soldered they can be marked with coloured pencil. If this is done systematically there is no danger of overlooking any connection.

## Transistors and Diode

With the transistors specified a red spot shows the collector lead. The base lead is centrally placed and the remaining lead is emitter. In Figs. 2 and $3 \mathrm{C}, \mathrm{B}$ and E show collector, base and emitter connections.

All transistors may be mounted with their leads quite long and this reduces chances of damage due to heat while soldering. Trl has a $\frac{3}{4}$ in. piece of sleeving on its base lead. The wires are then


The chassis and panel completed, ready for mounting in the cabinet.
pushed through the holes shown, bent over and soldered. Excess is snipped off. Radio-type cored solder is used and a small electric iron is best. It should not be necessary to hold the iron in contact with the joint for more than about a second or so.

Transistors $\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ each have a $\frac{3}{3} \mathrm{in}$. pieco of sleeving on the base lead. With $\operatorname{Tr} 4, \operatorname{Tr} 5$ and


Fig. 30: The underside wiring $t$ driver and output stages.

Tr6 the leads can be left full length if wished. Sleeving is needed on each base lead to prevent shorts to emitter or collector leads.

The negative end lead of diode D1 is about $\frac{3}{4} \mathrm{in}$. long and is soldered to pin 1 of IFT3. The positive end goes to C9.

## Panel Wiring

This is shown in Fig. 2. A lead passes from pin 4 of the oscillator coil, through hole "X" in Fig. 3, to the fixed plates tag of VC2. C4 is also soldered on here. VCl fixed plates go to " A " on the aerial and C1.

The slider (centre tag) of VRI is wired to R11. One outer tag goes to the on/off switch, wavechange switch and chassis, Fig. 2. The other outer tag is connected to the junction of diode DI and C9.
Thin red fiex provides the positive battery connection from the on/off switch. Black flex from the negative end of C13 is for battery negative. These leads are about 9 in. long and are taken into the pins of a non-reversible $7 \frac{1}{2} \mathrm{~V}$ battery twin plug and are soldered. Correct polarity is absolutely essential.

A length of thin twin flex is soldered to the secondary tags of T2 and to the speech coil tags of the speaker. Best reproduction is not to be expected until the speaker is fitted in a cabinet.

## Controls

A piece of thin card about 3 in. $\times 8$ in. is secured to the aluminium panel by means of the nuts holding the capacitors and volume control.

Viewing the set from the front, medium waves are tuned with the slide switch knob to the left (switch open). The other position brings in Cl and C 4 for 1,500m.

Botn variable capacitors are set fully open and the knobs are secured with their pointers to the left. When tuning, both knobs are moved approximately in step. However, VC2 is the more critical, so it is easier to tune with this, then adjust VCl for best volume. When tuning positions for a few stations have been marked it will be clear how tuning operates and adjustment will be found very simple. No aerial and oscillator circuit alignment has to be undertaken as with ganged tuning.

When a station has been tuned in, the cores of IFT1, IFT2 and IFT3 are adjusted for best volume. This is best done with a weak station. The i.f.t.s are intended for $470 \mathrm{kc} / \mathrm{s}$ but results will be similar if they are by chance adjusted to some other frequency.

No neutralising is used in the i.f. amplifier. As a result oscillation may arise when the i.f.t.s are exactly in tune. If so, slightly "stagger" them until this is cured. That is, screw one core in slightly and another out slightly.

It may be preferred to add neutralising later. If so, connect a $1 \cdot 2 \mathrm{k} \Omega$ resistor to pin 1 of IFT1. Take a 56 pF ( $2 \%$ ) capacitor from the free end of the resistor to pin 1 of IFT2. Also solder a $3.9 \mathrm{k} \Omega$ resistor to pin 1 of IFT2. Solder a 18 pF $(2 \%)$ capacitor to the free end of the $3.9 \mathrm{k} \Omega$ resistor and to pin 1 of IFT3. These components are best under the circuit board. The i.f.t.s can


Fig. 3b: The wiring; mixer, if. and detectar.

## COMPONENTS LIST

| Resistors: |  |
| :---: | :---: |
| RI | 56k $\Omega$ green-blue-orange-silver |
| R2 | $10 \mathrm{k} \Omega$ brown-black-orange-silver |
| R3 | 390s2 orange-white-brown-silver |
| R4 | $3.9 \mathrm{k} \Omega$ orange-white-red-silver |
| R5 | $56 \mathrm{k} \Omega$ green-blue-orange-silver |
| R6 | $8 \cdot 2 \mathrm{k} \Omega$ grey-red-red-silver |
| R7 | $680 \Omega$ blue-grey-brown-silver |
| R8 | $4 \cdot 7 \mathrm{k} \Omega$ yellow-violet-red-silver |
| R9 | I $k \Omega$ brown-black-red-silver |
| R10 | $22 \mathrm{k} \Omega$ red-red-orange-silver |
| RII | $1 \cdot 2 \mathrm{k} \Omega$ brown-red-red-silver |
| R12 | $68 \mathrm{k} \Omega$ blue-grey-orange-silver |
| R13 | $680 \Omega$ blue-grey-brown-silver |
| R14 | $22 \mathrm{k} \Omega$ red-red-orange-silver |
| R15 | $1 \mathrm{k} \Omega$ brown-black-red-silver |
| R16 | $82 \Omega$ grey-red-black-gold |
| R17 | $4.7 \Omega$ yellow-violet-gold-silver |
| R18 | $4.7 \mathrm{k} \Omega$ yellow-violet-red-gold |
| All 10\% (last band silver) $\frac{1}{2}$ W carbon, except RI6 and RI8 which are $5 \%$ (gold band) |  |
|  |  |



A rear view inside the cabinet of the finished receiver.
then be readjusted for best results.
If the receiver is wanted for medium waves only omit the wavechange switch, C1 and C4. If a vehicle aerial or other outside aerial is ever used a 25 -turn coupling winding can be placed on the ferrite rod about $\frac{1}{2}$ in. from " C ". One end of the winding is taken to the external aerial and the other to the nearest earth return tag.

A capacitor of $0.1 \mu \mathrm{~F}$ or $0.2 \mu \mathrm{~F}$ may be wired from Tr4 collector to earth return to reduce the hiss and heterodynes sometimes heard with some medium wave transmissions after dark.

## VCI and VC2

These may be air spaced or solid dielectric. The former is better for VC2 because it is likely to be smoother in action. A 150 pF short wave miniature variable capacitor is ideal. A 100 pF capacitor will cover to about 500 m if the oscillator coil core is well in. If to hand a 300 pF capacitor may be used with a 300 pF fixed capacitor in series.

If VC 1 is 300 pF this covers medium waves with a little to spare. If to hand a miniature ganged capacitor could be used for either VC1 or VC2

Capacitors:
Cl 1,000pF silver mica l\%
C2 $0.04 \mu \mathrm{~F} 150 \mathrm{~V}$
C3 $0.01 \mu \mathrm{~F} 150 \mathrm{~V}$
C4 200 pF silver mica $5 \%$
C5 $10 \mu \mathrm{~F}$ electrolytic 6 V
C6 $0.25 \mu \mathrm{~F} 150 \mathrm{~V}$
C7 $0.1 \mu \mathrm{~F} 150 \mathrm{~V}$
C8 $0.25 \mu \mathrm{~F} 150 \mathrm{~V}$
C9 $0.01 \mu \mathrm{~F} 150 \mathrm{~V}$
$\mathrm{C} 10 \quad 2 \mu \mathrm{~F}$ electrolytic 6 V
C11 $100 \mu \mathrm{~F}$ electrolytic 12 V
$\mathrm{C} 1250 \mu \mathrm{~F}$ electrolytic 6 V
$\mathrm{Cl} 3100 \mu \mathrm{~F}$ electrolytic 12 V
VCI 300pF variable (Jackson 2094)
VC2 150pF variable (Jackson C804)
Potentiometer:
VRI $5 \mathrm{k} \Omega$ with single-pole switch ( $\$ 2$ )

## Semiconductors:



Inductors:
IFTI, 2 I.F. transformers (Osmor PW/2)
IfT3 I.F. transformer (Osmor PW/3)
LI Aerial coil-see text
L2 Oscillator coil (Osmor PW/I)
T1, T2 Driver and output transformers suitable for OC8I's and a $3 \Omega$ loudspeaker (Osmor QXDI and QXO2 respectively)

## Miscellaneous:

SI 2-pole slide switch or any other small changeover type
S2 Single-pole on/off switch, on VRI
26 s.w.g. enamelled copper wire for LI. Ferrite rod 6 in . $\times \frac{3}{8} \mathrm{in}$. diameter. $3 \Omega$ loudspeaker, $3 \frac{1}{2} \mathrm{in}$. in diameter. Piece of aluminium $3 \frac{1}{2} \mathrm{in} . x 8 \mathrm{in}$. Piece of paxolin $2 \frac{1}{2} \mathrm{in} . \times 8 \mathrm{in}$. Two knobs $1 \frac{1}{2} \mathrm{i}$ n. in diameter, one lin. in diameter.

## Cabinet

This is made from $\frac{3}{16} \mathrm{in}$. or $\frac{1}{4} \mathrm{in}$. wood. Internal dimensions are $8 \frac{1}{5} \mathrm{in}$. wide, $6 \frac{3}{4} \mathrm{in}$. high and $2 \frac{3}{6} \mathrm{in}$. deep. An opening $6 \frac{3}{4} \mathrm{in}$. wide and $2 \frac{1}{2} \mathrm{in}$. high is cut in the front to clear switch and knobs.

The speaker opening may be circular, covered with speaker gauze. Or several rows of 3 in . or similar holes may be drilled. The battery is a H1187 or equivalent.
Joining edges of wood are smeared with adhesivo and the pieces are fixed together with panel pins. When the adhesive is hard the cabinet can be cleaned up with glasspaper and it may then be varnished, painted or covered with one of the popular fabric materials. A small carrying handle can be screwed to the top. The receiver is fixed by screws through the aluminium panel into the front. Tuning positions can be marked on the card.
Current drain is about 7 mA to 10 mA with very low volume, rising to 15 mA to 25 mA or so with good volume. If a heavy current flows when first connecting the battery, switch off and look for a short-circuit or other defect.

## Audio Volume Control with the K42

ALTHOUGH a photoconductor is essentially a non-linear device in that its resistance even at constant illumination decreases slightly with increasing applied voltage, at low voltages the departures from non-linearity are so slight that the cell can be used to control small-signal audiofrequencies without introducing distortion.

The basic circuit of a light-operated volume control is shown in Fig. 10. The photoconductor forms the lower leg of a potential divider across the signal voltage. When illuminated it has a resistance of about $100 \Omega$ and there is an attenuation of 1,000 times of 60 db -when in darkness it has a resistance greater than $10 \mathrm{~m} \Omega$ and the attenuation is negligible. If this arrangement is to be used as a volume control it is required that the photoconductor should change logarithmically when a control is advanced linearly (as in the usual " $\log$


Fig. 10; The basic circult of a light-operated volume control.


Fl. Ils A practical remote volume control circuit.
pot'), because the ear responds to stimuli in this way.

A plot of the resistance of a K42 illuminated by a 6.3 V 60 mA lamp bulb close to its glass window in a light-proof box is shown in Fig. 12, the resis. tance-scale being of the logarithmic or decibel form. The voltage across the lamp was varied by a resistor VR1 in series with the 6 V supply. Curve J shows the variation of photoconductor resistance with lamp voltage, and curve K shows the variation with the lamp series resistance. To get a "log pot" law a control would have to give a straight line on this diagram, and it will be seen that the lamp-voltage curve departs greatly from linearity. The lamp series-resistance curve K however, is much straighter because of the "constant current" characteristic of incandescent lamps, hence a linear series resistor provides the required control.

## Remote Volume Control

A practical circuit for a remote volume control is shown in Fig. 11. VR2 is the normal volume control in the amplifier and is set so that with the lamp off the signal is at the maximum required level. VR1 is the remote control: decreasing the resistance of this allows more current to flow


Fig. 12: Resistance graph of the K42 Illuminated by on incondescent lamp.

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| 1 D 5 | 6／6 | 7 C 5 | $7 / 9$ | DF91 |  | ＇EF41 | 8／6 | $1 P \mathrm{C}$ | $\epsilon$ | U49 |  |
| 1H5GT | $8 / 3$ | 7 C 6 | $7 / 6$ | DF＇96 | 6／－ | EF42 | $4 / 6$ | 8 PCP80 | 819 | U50 |  |
| 1NagT | $8 /-$ | $7{ }^{7} 7$ | $5 / 9$ | DH76 | $3 / 6$ | EF80 | 4／3 | 3 PCH 82 | 6／9 | U52 |  |
| 1 R 5 |  | 7Y4 | $5 /$ | 11177 | $3 / 6$ | EF85 | $5 /-$ | PCF84 | 7／9 | U5 |  |
| 185 | 8／9 | Izats | 4／3 | D H 81 | 12／6 | Erse | $8 / 3$ | 3 PCF86 | 9／6 | U7 | 8 |
| 1 T 4 |  | －12AT7 | $3 / 9$ | DK32 | $81-$ | EF89 | 4／3 | PY800 | 6／ | U191 | $8 / 6$ |
| 2 P | $19 / 6$ | 12AU7 | 4／9 | DK91 | 4／9 | EF91 | $2 / 9$ | PGF805 | 9／6 | U281 |  |
| $3 \mathrm{A5}$ |  | 12 AX | 4／9 | 1） 692 | 6／9 | EF92 | $2 / 6$ | 6 PCL82 | 8／6 | U291 | 寿 |
| 3 Q 4 | 4／10 | 12K7GT | 4／3 | DK96 | $8 / 6$ | EF＇183 | $7 / 6$ | ${ }^{\text {PCL } 83}$ |  | U301 |  |
| 384 | 4／9 | $12 \mathrm{K8G'T}$ | 8／9 | DLa3 | 7／3 | EL38 | 11／9 | $9 \mathrm{PCL84}$ | 7／6 | U801 | 15／9 |
| 3 V 4 | 5／6 | 1297GT | 4／3 | DL35 | $8 / 9$ | EL41 | $7 / 3$ | 3 PCLL85 | 8／G． | U4020 | 5／9 |
| 5 U 40 | 4／6 | $19 \mathrm{BG6G}$ |  | DL92 | $4 / 9$ | F1， 4 | $4 / 9$ | PENA4 | 8／9 | UAB | 80519 |
| 5 Y 3 G | $5 /$ | －20L1 | 12／6 | DL94 | 5／6 | EL95 | 5／6 | Pren 14 |  | UAF42 |  |
| 58，4G |  | 20 P 4 | 13／6 | Ll96 | $6 /$ | EM34 | $7 / 11$ | 1 PEN 383 | 9／6 | UBCAI | 8／6 |
| 6 L 5 |  | 20P5 | 11／9 | EABC80 | $8 /$ | EM80 | 6／8 |  |  | UBC81 |  |
| $6 \mathrm{AQ5}$ |  | －25L6at |  | EAF42 | 8／－ | Emsi | $7 / 9$ |  | 15／－ | UBF80 |  |
| 6AT6 | 3／8 | $3{ }^{300118}$ | $9 / 6$ | Ebs1 | $2 /-$ | EM84 | $6 / 3$ |  |  | UBFR9 | 8／8 |
| 6Ba6 |  | $30 \mathrm{FL1}$ | $9 / 6$ | EBC33 |  | EM87 |  |  |  | UCC84 | 8 j |
| 6BE6 | $5 / 3$ | 301． 30 | 9／6． | EBC41 | 7／3 | EY51 |  | C |  | UCC85 | 8／9 |
| 6BG6G | 12／6 | $3{ }^{31} 4$ | 13／6 | ERFx0 |  | EY86 | $5 / 6$ |  |  | UCF80 |  |
| ${ }_{6} 6 \mathrm{BH} 6$ | 5／－ | －30P19 | 13／6 | EBF83 | 7／6 | L2．40 | $5 / 6$ | PL36 | $8 / 8$ | UCE42 | 7／6 |
| 6 B |  | 30 P L1 | 8／－ | EBF89 | 6／－ | E／41 | $7 / 6$ | 1 181 |  | UCH81 |  |
| 6F1： | $3 / 6$ | $301^{2} \mathrm{~L} 13$ | 9／－ | EBL21 | 10／6 | Ez80 |  | 1＇L82 | $5 / 6$ | UCL82 | $7 / 6$ |
| 6 F 14 | － | 30 PL 1 | 12／3 | bce40 | 8／9 | EK81 | 4／6 | ${ }^{\text {P }}$ L ${ }^{\text {a }}$ |  | UCL83 |  |
| 6.179 | 4／6 | 35 A | 14／－ | ECCr 1 | $3 / 9$ | ＇1W4／50 | $006 / 3$ | PL84 | $5 / 8$ | UF4 | $7 / 3$ |
| 6K74 | 1／6 | 3 Lb | 6／3 | ECCs2 | 4／9 | CZ333 | 14／6 | $8 \mathrm{P} \times 5$ | $7 \%$ | UF42 |  |
| 6 K 7 GT | 4／－ | 35\％46 | 4／11 | Hir | 71. | （\％237 | 819 | 1 P 32 | 8／－ | UF89 | 613 |
| 6 K 86 | $4 / 3$ | 53 KU | 8／6 | 120．n4 | 6／3 | KT32 | $5 /-$ | $\mathrm{Pl}^{13}$ | － | U1．t1 |  |
|  | $7 / 8$ | AC／V1＇2 |  | Ful 85 | 613 | КTiti | 8／－ | PY80 | $5 / 3$ | UL44 |  |
| ${ }^{68}$ | $9 / 6$ |  | 12／B | ECF80 | 8／3 | ME140 | 15／ | PY81 | $5 / 9$ | UL84 |  |
| $6 \mathrm{6Ta}$ | $4 / 9$ | AZ31 | $8 / 6$ | ECF\％ | 8／3 | MU14 | 5／－ | 1 Y Y | $5 /-$ | UU7 | $8 / 6$ |
| 6 G 7 GT | $7 / 8$ | B30 | 9 | ECF86 | 10／8 | M | ENB | PY83 | $5 / 9$ | UY21 |  |
| 68LTGT | 5／－ | CL33 | 9／6 | LCH35 | 6／－ |  | 12／6 | 1＇Y88 | $7 / 3$ | UY41 | $4 / 9$ |
| 68 NTG | 3／9 | CY1 | 12／6 | ECH42 | $8 / 3$ |  | $4 / 10$ | TDD | 719 | UY85 |  |
| 6V6G | $3 / 9$ | DAC32 | 8／3 | ECH81 |  |  | 16／6 | TH21 | 9／6 | VP4B |  |
| $6 \mathrm{V664}$ | 8／6 | DaF91 | $3 / 9$ | ECL80 | 6／3 | OD3 | 4／8 |  | 4／9 | － | $3 / 6$ |
| 6x4 | 318 | DaF90 | 6／－ | EC182 | $7 /$ | PC95 | $6 / 9$ | U25 |  |  | 2／8 |
| 6EJGT | 8／6 | DCC90 | 8／8 | ECL | 8／－1 | PC97 | \％／－ | ， |  | 72 | 16／6 |

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through the lamp making it brighter, thus decreasing the resistance of the photoconductor and hence the signal voltage to the amplifier. If VR2 is not to be used it should be replaced by a $500 \mathrm{k} \Omega$ fixed resistor to limit the output resistance of the divider when feeding directly into a valve grid. This circuit has the advantage that switching off the lamp leaves the amplifier in its normal operating state. so that power is taken from the battery only when the volume is turned down by remote control.

Even though the cells have a fairly slow response time they are still sufficiently sensitive to $50 \mathrm{c} / \mathrm{s}$ to pick up the slight ripple on mains-driven bulbs and a d.c. supply to the bulb must be used. The photoconductor must also be protected from ambient lighting so that it responds only to the light of the lamp. They may be mounted close together in a light-proof box or the lamp may be taped to the glass window of the K42 with black p.v.c. tape and the whole unit cocooned in this tape If ambient light leaks into the photocell its resistance will fall and full volume will not be ohtained

Obviously this circuit has a disadvantage over the usual volume control in that it requires a lamp dissipating some 200 mW to control audio-voltages of negligible power. This is inefficient but has the great advantage for purposes of remote control that the controlline leads carry no cienal voltage and may be as Inng as required since hum pick-up and h-ief suviteting tonnsients on these leada do not get into the audio side. Also the slow response of light bulh and cell provides freedom from potentinmeter noise.

## Volume Compressor

It is often required to produce a constant output sienal from a source which is fluctuating greatlv in intensity. e.g. to reduce output variations in a public address system due to differentes in the placing or vocal intensity of speakers. There are valve volume compression circuits which achieve this. but they are generally very complicated and difficult to set up. By driving the volume control lamp from the output of the power amplifier it is controlling (Fig. 13) a volume compressor par excellenere can be constructed such that a thoucand to one change of input voltage causes only a threc to one change in output voltage. at any power from 60 mW upwards.

The reason for this great compression of dynamic range may be seen by reference to curve J of Fig. 12 which shows the variation of photoconductor resistance with lamp voltage. Suppose R1 is $1 \mathrm{M} \Omega$ and the input signal to the amplifier via the volume control is such that there. is 2 V output across the lamp, then the photoconductor resistance is $1 \mathrm{k} \Omega$ and the volume control is attenuating by 1,000 .

Now suppose the input signal falls so that the output across the lamp is 1 V , then the photocon-
ductor resistance is $100 \mathrm{k} \Omega$, and the volume control is attenuating by only 10 . Thus an input voltage swing of 200 has produced an output voltage swing of only 2 !

The circuit of Fig 13 stabilises the output at about 1 V which represents 60 mW into a $15 \Omega$ load or 300 mW into a $3 \Omega$ load. To make the circuit capable of stabilising any level of output above this figure a variable resistor (VR1) is placed in series with the lamp bulb (Fig. 14). The greater this resistor the greater the output from the amplifier necessary to maintain IV across the bulb. Thus this control acts as the volume control determining the stabilized output; the normal volume control on the amplifier performs a different function which will be explained in the next paragraph.


Fig. 13: A volume compressor circuit.
The table below gives the approximate values of VRI for various maximum output powers into $3 \Omega$ and $15 \Omega$ loads.

| Power | Load |  |
| :---: | :---: | :---: |
| 60 mW | $3 \Omega$ | $15 \Omega$ |
| 300 mW | 0 | 0 |
| 1 W | $40 \Omega$ | $60 \Omega$ |
| $3 W$ | $100 \Omega$ | $150 \Omega$ |
| 10 W | $250 \Omega 2$ | $300 \Omega$ |
|  |  | $600 \Omega$ |.



Fig. 14: A volume compressor for variable output levels,

In setting up the final circuit (Fig. 14) the constructor must decide what is the lowest signal which must give full output from the amplifier. The latter must then itself have the sensitivity to give the required output on this signal before all the control circuits are added, since these circuits only attenuate large signals and do not amplify smaller ones. The control VR2 is used to adjust the amplifier sensitivity so that it just gives the required output power on this minimum signal; it controls the range of compression not the output volume.

To set up the circuit the lamp is switched off, the minimum signal fed in and VR2 adjusted to give the required output into the loudspeaker. Then the lamp is switched on, a signal near maximum fed in and VR1 adiusted to give about the same output. Any signal below the minimum will not be compressed and will be amplified normally at maximum sensitivity. Any signal above minimum will come out at the pre-set volume. Since the gain of the system is greatest on low inputs the signal to noise ratio will be increased on these by the volume compression achieved. This trading of noise for compression limits the range of compression which is realisable in practice.

## Automatic Attack/Decay Control

Automatic volume controls which when switched on "swell up" the sound at a pre-determined rate, and when switched off allow the sound to decay at some pre-determined rate, are used in electronic musical instruments to control the "attack/decay" envelope of the notes: variations of this on a sound of given pitch make all the difference between gentle bowing of a violin and the percussive "ting" of a bell. Also in sound studios similar automatic controls are used to fade sound effects in and out gradually rather than suddenly switching them on.

This type of control is of great help to the amateur tape-recordist trying to mix several inputs with only one pair of hands-instead of having to turn a volume control by hand when he wants to bring in a sound effect, he can just flip a switch and the automatic control will do the rest. As with the volume compressor there are valve circuits to perform this task. but they are complex and generally introduce distortion-here again the K42 circuit scores in simplicity and versatility.

The volume control of Fig. 10 is used again but with the lamp driven by an automatically controlled voltage from a d.c. power amplifier. The output from this amplifier is an almost exponentially rising or decaying voltage which compensates for the non-linearity in the lamp/photoconductor system and produces a constant rate of change of sound in decibels per second - this giving the required audio effect. The rates of rise and fall of this voltage may be pre-set and determine the time taken for the sound to attack and decay.


Fig. 15: A circuit for automatic attack/decay control.

The circuit of the automatic attack/decay control may be considered in three stages (Fig. 15):
(1) The lamp-driven volume control which is the same as that of Fig. 10 and needs no further explanation.
(2) The two transistor d.c. power amplifier which consists of two emitter followers in cascade. This configuration gives no voltage gain, but matches the very low resistance of the lamp to the high output impedance of the control circuitry.
(3) The control voltage circuit which provides a varying voltage whose rates of rise and fall can be pre-set as required.
The d.c. amplifier circuit is very simple and should present no difficulty in construction provided the correct types of transistors are used. Tr2 provides the power for the lamp and must be capable of dissipating $150 \mathrm{n}, \mathrm{W}$, any audio transistor with this power rating and medium to high gain is suitable, e.g. NKT223, NKT224, OC81, etc. Tr2 should be in good condition and highgain, NKT223, NKT224. OC71, etc. - a poor transistor will work but the longest attack/decay times will be unobtainable. When the input to the amplifier is disconnected the output voltage should be less than 0.3 V and the lamp should not glow. When the input is connected to the 6 V negative rail the lamp should glow brightly.

The control voltage is provided by alternately charging a large capacitor C 1 through resistors VR1 and VR2 by means of the changeover switch S1. The resistors are made variable so that the time taken for the sound to swell up or die away may be pre-set. From Fig. 12, curve J, it may be seen that the photoconductor attains its maximum resistance with a lamp voltage of 0.7 V and is not affected by voltages below this. Therefore the control voltage must vary above 0.6 V and to ensure this Cl is returned not to earth but to a potential divider cnnsisting of R1 and R2 whose junction is about $0 \cdot 6 \mathrm{~V}$ negative to earth.

Consider the switch S1 switched to VR2 and C1 completely discharged: the input voltage is then

# SIMPLE TIMING, DEVICE 

## By S. W. Andrew

below are the approximate value of Rx for various timing durations:
$\begin{array}{lllllllllllll}\text { sec. } & 1 & 2 & 3 & 4 & 6 & 8 & 10 & 12 & 15 & 20 & 25 & 30\end{array}$ Rx (kת) 1630506182100115127150175200230 Longer durations are not practical as the charging current is quite small, i.e. not much greater than the leakage current in C1. Since the leakage current is dependent on temperature and past history of the capacitor it can vary quite a lot, causing great inaccuracies in the duration.

The unit was constructed in a die-cast instrument box but any suitable chassis can be used. The layout is not critical but if a metal chassis is used it should be earthed. The components list is given only as a guide. The values of R2, R3 and R4 may have to be changed to suit individual relay requirements. S1 can be replaced with a $0.25 \mathrm{M} \Omega$ potentiometer and a calibrated scale.

## COMPONENTS LIST

Resistors:

| RI | $220 \Omega$ | R4 | $220 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: |
| R2 | $3.3 \mathrm{k} \Omega$ | R5 | $6.8 \mathrm{k} \Omega$ |
| R3 | $5 \mathrm{k} \Omega 5 \mathrm{~W}$ | Rx | See text |

All $10 \%+W$ unless otherwlse stated.

## Capacitors:

$\mathrm{Cl} 50 \mu \mathrm{~F}$ electrolytic 100 V
C2 $64 \mu \mathrm{~F}$ electrolytic 100 V
Valves:
VI OA3 V2 Small pllot neon
Switches:
SI SIngle-pole, I2-way rotary
S2 2-pole, 2-way toggle
Miscellaneous:
TI Mains transformer, converter type. Primarles, 240V. Secondaries, 200V 20 mA
RLI Single-pole change-over relay. Ik $\Omega$ coll reslstance
DI, 2 Sllicone power diodes, 200 V 100 mA SKI Output socket
0.5 A fuse and holder. Pllot lamp holder. international Octal valve-holder. Chassls, wire, etc.


Fig. 1: In this circuit of the timer unit, all switches are shown in the "unit off" position.


SOME technical information has recently come to hand on the transmitting facilities of the Canadian Broadcasting Corporation at Sackville on the Canadian Atlantic coast.

Here there are three 50 kW transmitters which can -qperato on any of the short wave bands from 6,000 to 21,000 . Special variable frequency oscillators maintain the operating frequency within $25 \mathrm{c} / \mathrm{s}$ : The transmitters are capable of full modulation by any audio frequency in the 30 to $10,000 \mathrm{c} / \mathrm{s}$ range.

Each transmitter can be tuned to any one of 13 aerial systems. The directional properties of these antennae can be reversed to cover different areas:" For example, the European beam is reversible to cover New Zealand, Central America and-Mexico.

Some of the antennäo are of a dual-frequency type which enable two transmitters operating simultaneously in adjacent short wave bands to be coninected to the same antenna through a common trat mission line.

Tho whole antenna system is designed to with wind fivelocity of $120 \mathrm{~m} . \mathrm{p} . \mathrm{h}$. and an ice coating tin. thick on all members.

Three stations from which I have recently received verifications aro Radio Nacional de Espana (General Yague 1, Madrid, Spain), Radio Varician (Vatican City, Vatican State) and Radio Tirana: (Rue Conference de Peza 3, Tirana, Albania).

That from the Vatican was best, giving date, time and meter band. The Spanish card gave the frequéncy and date only. Radio Tirana simply sent a carbon copy letter saying the report was correct English transmissions from this station are ffog 2000-2030 and 2130-2200 on 9,390/ 7,090 and 1,088 medium wave.
$A_{i}$ cateck on stations operating in the 31 m band brougtit the following results. On 9,450 the home servide of Radio Moscow was heard with station identification at 1615. The Moscow home service was allso heard at 2100 on 9.615. Between 17001730 :there was an unidentified language transmission on 9,480 from Moscow and between 1730-1800 Arabic was being transmitted on 9,500.

At 1615 Cairo Radio (Maspero, Cairo) uses 9,475 for its transmission to the Sudan. Reception was slightly better on this frequency than the 25 m band alternative of 11,915 . Cairo was also heard in Arabic on 9,495 around 1730. The programme appeared to be the Voice of the Arabs service end, although the signal was strong, suffered from c.w. interferenca

Radio South Africa can be heard throughout the evening until close down at 2115 on 9,525 . Reception is variable, mainly because Radio Moscow also has a transmitter on this frequency.

Well known as the home of the European service of the Swiss Broadcasting Service, Berne, Switzerland, is 9,535 . From 2100 this channel begins to fade out, although the alternative outlet of 6,165 gives a first-class signal. News in French can be heard at 2130 .

Several transmitters make use of 9,540 . After 1900 the Voice of America puts in a very good signal in its Russian service, Around 2200 Radio Free Europe is the dominant station, although there is strong interference from another station, as yet unidentified.

During the evening Radio Sofia, Bulgaria, uses 9,560 for several of its European transmissions, including the half-hour English transmissions at 1930 and 2130. During the 1930 transmission a 54,444 SINPO rating is not unusual. Most of the Sofia transmissions on 9,670 are also carried on 6,070.

Five kilocycles further on-9.565-the Voice of America Tangier transmitter comes through well, although Sofia occasionally splashes over to spoil the signal. During the evening the Voice of America transmitter carries the English programme with Music, U.S.A., at 1915 and news at 2000 .

At 2000 two stations clash on 9.575 . These are R.A.I., Via del Babuino 9, Rome, Italy, and Radio Mayrink Veiga (Rua Mayrink Veiga 15, Rio de Janciro, Brazil). By 2100 the Italian station has closed down, with the result that the Brazilian may be clearly heard. Radic Mayrink Veiga, by the way, asks those wanting a QSL verification of their report to enclose the return postage.
The European service of the BBC uses 9.580 at 2100 for a news broadcast and commentary in English.
On weekdays and Saturdays 9.590 is used hy the English service of Radio Nederland (P.O.B 222, Hilversum). Reception is variable and the alternative frequency of 11.730 is more reliable.
Up to 2115 the General Overseas Service of the BBC can be heard on 9,625. A good frequency to try after 2115 is 9.410 .
From 2000-2145 the Canadian Broadcasting Corporation transmits in English and French to Europe on 9.630 . This is the best of the three frequencies used. Of the others 11.720 is quite good but 15,320 is often inaudible, especially after 2100.

Radio Nacional de Espana has a Spanish language broadcast from 1620-2120 on 9,695. Reception is good, spoilt only by a weak jamming transmitter. Fair reception is given also on the alternative frequencies of $6,140 / 7,105$.
Finally a note about Radio Australia (P.O. Box 428G, G.P.O., Melbourne). This station now
comes crashing in during the afternoon on $9,570$. Signal strength on the SINPO rating is usually 4.

This month I have mentioned a few of the stations coming through well in the 31 m band. Don't be surprised if you get different resultsthat is the nature of short wave. I shall be interested to hear of any changes you find.

## The Amateur Bands-by David Gibson G3JDG

ASOMEWHAT disappointing month on the l.f. bands, which should have yielded better things considering the activity which was about in the form of contests. There was the VK/ZL c.w. contest, VU2/4S7 contest phone and c.w., the RSGB $7 \mathrm{Mc} / \mathrm{s}$ DX phone contest, $C Q$ world wide DX contest on phone, and the YL/RL party on c.w. Yet, in spite of all this activity things didn't come through at all as planned, at least not at this QTH.

On Top band $1800-2000 \mathrm{kc} / \mathrm{s}$ many G stations were monitored on both phone and c.w., some quite a distance i.e. Somerset, but the furthest one to arrive was GW3HUM 579. Another very loud signal signed itself G3LYW and was using SSB. It is surprising really that more stations don't use this mode of transmission on Top band, especially in view of the power limit of 10W. A point of interest is that RTTY is not permitted. Eighty metres seems to be getting more like Forty as regards noise. One or two excursions into this band proved very frustrating and the only stations who managed to filter through at this QTH were SM5BX, DJ9TN, OK2PS and G3BZU. DJ9PB/P (the $\mathbf{P}$ signifying portable) put in a very creditable signal, and was going great guns. After this, Eighty was given a rest, but a chance listening early one morning at 0500-0630 hours G.M.T., was rewarded by some real DX from ZL4BX and ZL4LM, both SSB about 5 and 6 . Needless to say, the big rig was hurriedly switched on, but alas no success in raising either of these stations.

With so much more activity on Twenty the usual procedure at G3JDG is to listen for about half an hour on Forty and then either switch off in disgust or switch to Twenty. However, this month it was decided to stick at it and see if there really was anything about. The result was a battle royal to nurse through a VK call sign, which after much effort turned out to be VK4SS. Having now got the hang of it, other signals were sorted out from the QRM (commercial type prominent) which included VQ2SD, OK 1 AFM, YU3ABZ, OK100, SM5BOU, SP6OQ and IT1AGA on Sicily. A new one for the bciok OX3LP (Greenland).

## The H.F. Bands

Twenty metres, always good for DX somewhere didn't quite live up to it this time, although much activity is nearly always in evidence. At the time of writing, the band starts to open up at about 0400 hours GMT and returns to graveyard like conditions at around 2000 hours GMT. W's were plentiful and many were received, far too many to mention. Those who were 5 and $8 / 9$ were K3VAB. W4HZI, W2WY, W4AF, WB2CPW and WA8FQU.

The VK/ZL contest was very disappointing as regards logging anything, the only VK other than VK4SS heard at all at any time was VK2ADE. Much of Europe came in and another Greenland station on phone was OX3HM. Looks like the polar regions are hotting up-as far as Ham radio is concerned of course.

My remarks in this column about the Fifteen metre band have not gone unnoticed, and even if I can't hear anything it doesn't mean to say that everyone else if afflicted with $21 \mathrm{Mc} / \mathrm{s}$ deafness. A "G3" colleague in Watford writes to say that on Sunday, 18th October, from 1625 to 1707 hours GMT, the following stations were in evidence: WA2KRM, W1CHG, W4SJT, PY5RB, WA4UEJ/ MM, CN8AK, VQ2JM and CR4AB.

## Ten Metres

A terrible confession this month! The cubical quad, which gave such sterling service during the summer months was brutally dismantled and a two element wire beam (rotatable) was put up in its place at the same height ( 12 ft ). This gives less gain but nevertheless seems to work quite well. $G$ stations worked with it were G2CZM, G3FIB, G3GXJ (SSB), G3MXQ, G3RRK, G3JDB, G3SFZ, G3AYC, G3EUJ, G3PAO, G3AEQ. G6FS was heard many times and called without success. DX-wise on this band it's been a poor month with only four stations to report. ZE1AN, ZE1JD, ZE1EV and ZC4AK, all on the same Sunday morning. ZE1AN in Bulawayo was a very FB signal and Tom made it a three-way with himself, G3JDG and G3TMI in Canterbury. The interesting thing is that although G3TMI was completely inaudible ZE1AN literally hundreds of miles away was a good 5 and 6/7.

Perhaps an explanation about the ZC4 station is necessary since last month I reported that all ZB4 (Cyprus) callsigns had been withdrawn. This is perfectly true, but this does not affect the sovereign base areas, they merely change their callsigns from ZB4 to ZC4.

## Here and There

Many stations classified as rare DX, often are small portable rigs operated on some remote island so small that they may not even be shown on some maps. A round-up to check which islands are inhabited by a box emitting r.f. and which are not, revealed the following. On Jan Mayen Island, LA2QJ/P and LA9PI/P are fairly active. The South Shetland Islands are put on the radio map

## a simple Two-band Phone



Transmitter

## BY G30GR

1HIS transmitter has been found very satisfactory, and can be built almost entirely from receiver type components. Change-over switching is included, so that it is only necessary to add an aerial, receiver, and microphone. Many transmitters in the power range up to 10 W cover the 160 m band only, but in the present circuit 80 m is also included. As end-fed aerials are often used on 160 m , the same aerial will be even more effective on 80 m , while with the latter band greater ranges can usually be covered.

Fig. 1 is the circuit, and the method of working is straightforward.

## Switching

The control switch has three positions, for transmit, receive and net. Section Sla applies h.t. to the oscillator in both transmit and net positions. With the switch at net, only the oscillator is working, so that the signal can be tuned in on the receiver, to find if the channel is clear. (This position is also used for tuning-up if a variable frequency oscillator or VFO is employed with the transmitter as described later.)
With the switch in the central position, the serial is connected to the receiver by section Slb, so that the same wire may be used for both reception and transmission. R14 is a bleeder, to discharge C10 and C11 when the equipment is awitched off.

With the switch in the last position, Sla applies h.t. to the oscillator. SIb takes the aerial to the power amplifier tank coil L1, while Slc shorts the receiver aerial circuit to earth. Section S1d applies h.t. to the modulator and p.a. stage V2.

The single pole on/off switch connected to L1 is for $160 / 80 \mathrm{~m}$, half the coil being shorted out for 80 m working.

## Metering

This is reduced to the simplest possible method, by including a 100 mA or similar meter in the cathode circuit of V2. With the transmitter switched to net, grid current through R3 from the cathode is indicated, and should be between 1 mA and 2 mA . The reading at this current is small, but the 807 operates well over a wide range of grid currents.
When the 3 -way switch ( S 1 ) is on transmit, grid, screen grid, and anode currents all pass through the meter, thus showing the total d.c. input.

## Oscillator

V1 is employed as a Pierce oscillator, and thus needs no coils or tuning. The crystal holder is to the right of the panel, so that crystals can be plugged in easily. C 1 isolates h.t. from the crystal, while the trimmer TC1 allows oscillation, and thus the drive to $V 2$, to be adjusted.

V1 may be used as a buffer when operating the transmitter with a VFO.

## Modulator

This consists of the high gain twin triode V3, followed by a single 6 V 6 . No audio gain is included, because modulation was fourd satisfactory with a crystal microphone at a normal distance. The modulating power can be adjusted by moving the microphone nearer or farther away.
The 6 V 6 has an audio output of about 4.5 W and good modulation is obtained. The audio choke L2 is actually the primary of a speaker matching transformer, the secondary being ignored. This transformer should be rated at $80-100 \mathrm{~mA}$, and is of the type intended for use with mains output pentodes.
With modulation of this kind, the anode of V 4 cannot swing negative, so that over-modulation (and consequent splatter) is avoided. If excessive modulation is attempted, audio distortion will become severe, and this is a sign that the audio input should be reduced.

## RFC2 and LI

RFC2 is an anti-parasitic choke, made by winding six turns of 20 s.w.g. enamelled wire on $100 \Omega$ $\frac{1}{2} \mathrm{~W}$ carbon resistor, the winding being stretched out to about $\frac{5}{8} \mathrm{in}$. long. This is then soldered by short leads to the cap clip of V2.

LI is 60 turns of $26 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. double cotton covered wire, on a $1 \frac{1}{2}$ in. diameter former. This is close wound, and the ends pass through small holes. The centre turn is prised up, a piece of card is slipped under it. and it is scraped so that a lead can be soldered on. The coil is supported by a bracket screwed to the frame of the twin-gang capacitor VC2.


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## Power Supply

The 5 U 4 G rectifier valve requires a 5 V 3 A secondary, but a $5 V 4 G$ may be used and run from a 5 V 2 A secondary. If a $100-125 \mathrm{~mA}$ smoothing choke of low d.c. resistance is to hand, this can replace R15.

With a $250 / 0 / 250 \mathrm{~V}$ transformer, the hit. line voltage dropped to $210-220 \mathrm{~V}$, at 100 mA . so a 275 V transformer is preferable. though the 250 V type is satisfactory. The h.t. drain is around 90 mA with a crystal, or about 110 mA with the VFO. As
resting intervals follow periods of transmitting, a 100 mA secondary can be used, though a $125-150 \mathrm{~mA}$ secondary would be better if available.

The 6.3 V winding should be able to deliver 2 A , for crystal operation, or 3 A if the VFO is to be added.

## Above Chassis

A chassis approximately $13 \frac{1}{2} \mathrm{in}$. $x \quad 5 \frac{1}{2} \mathrm{in}$. is suitable, with an aluminium, hardboard, or ply-


Fig. 1: The complete circuit of the transmitter.


Fig. 2i The above-chassis layout of components.


Fig. 3: The underchassis wiring of the transmitter.
wood panel about $13 \frac{1}{2}$ in. $x 8 \mathrm{in}$. bolted to the front runner. The layout of components is shown in Fig. 2, and is not critical.

The variable capacitors may be attached to the panel, or fixed to the chassis with brackets. Both are electrically connected to the chassis. The two sections of the gang capacitor are wired in parallel. A lead is soldered to one bottom tag, and passes through a hole to Sib.

A pillar or strip with an insulated tag supports the RFC1 choke. C6. RFC2 and R5 are held by the wiring. RFC2 and R5 should not be omitted.

The meter is bolted in a hole cut in the panel, An adjustable washer cutter is useful for this.

Though a 100 mA instrument is convenient, other meters can be perfectly satisfactory. If $V 2$ anode receives 250 V , an anode current of 40 mA indicates 10 W input, which is the maximum permitted on 16 m . (Input $=\mathrm{E} \times \mathrm{I}$. or $250 \times 0.04 \mathrm{~A}$.) A 0.50 mA meter is thus suitable, if included in the anode circuit. To do this, wire pin 4 of V2 to chassis, and connect the meter in the lead passing from RFCl to R4. Connect C4 or a similar value capacitor across the meter.

A 1 mA or other sensitive meter can be shunted to read $0-50 \mathrm{~mA}$, or $0-100 \mathrm{~mA}$. It is thus often possible to use an instrument to hand.

A mains voltage switch $\$ 3$ is used in the mains
circuit. The $160 / 80 \mathrm{~m}$ switch is a single pole twoway rotary type.

## Under the Chassis

Wiring etc., can be seen from Fig. 3. The heater circuit is completed first, with the connections run near the chassis. Both sockets of the crystal holder need clearance holes. Crystals may have $\frac{1}{2}$ in. or 3 in. pin spacing, with a holder to suit, or a 3 -socket holder which will take either type may be used.

The centre pin of the trimmer TCl is soldered 10 an earthed tag of the valveholder. A screened lead is required from the microphone socket. Points marked MC go to tags bolted to the chassis.

For mains supply, a 3-core flexible cord is used. Equip the cord with a 13A type plug fitted with a 3A or sinilar fuse. Green is for carth, and goes from the large pin to chassis. Red is the live conductor, from plug fuse to transmitter mains switch. Black is the neutral circuit, from plug neutral to transformer primary. A tag strip anchors the leads, if necessary, and also provides a chassis connecting point for Cl 1 .

All leads should be short and direct, and approxinately in the positions shown. Tag 7 of the rectifier valveholder is merely used as an anchor point for R15 and C10.

## Function Switch

This is 4-pole, 3-way and may have two wafers, or be a double sided single wafer. Fig. 4 shows connections to a two-wafer switch, viewing hoth wafers from behind. Sla applies h.t. to R2 in positions 1 and 3 . Sib takes the aerial to the transmitter in position 1, and to the receiver in


Fig. 4: Connections to the switch, SI.
position 2. S1e earths the receiver aerial lead in position 1. S1d applies h.t. to the transmitter in position 1, and to the bleeder R14 in position 2. Positions are:-1 Transmit. 2 Receive. 3 Net.

If a 4 -pole 2 -way switch is to hand, this can be used for transmit/receive. An on/off toggle switch is then fitted to the panel and connected to apply h.t. to RI only, for net operations. This switch is returned to its off position, for transmitting and receiving.

If a double sided wafer is used, check that this is wired correctly, becalise tags will appear reversed when viewing part of the circuit from the front of the wafer.


## Oselliator Adjustment

With a crystal inserted, and the transmitter switched on, furn the function switch to net. Comniencing from the open position, screw down TC1 until the meter shows between 1 mA and 2 mA grid current. If preferred, a test-meter may be temporarily inserted between R3 and chassis, for this test. If so, meter positive goes to chassis. A check should be made with any crystals to be used, so that TCl can be adjusted to suit all crystals.

## P.A. Loading

A first test is best made by connecting a 15 W $200 / 250 \mathrm{~V}$ household lamp from aerial lead to transmitter chassis. Close the gang capacitor fully. Check with the net position that grid drive is obtained. then turn the switch to transmit. The offtune current may be very heavy, and VC1 is quickly rotated until current dips to a low valueprobably $10-15 \mathrm{~mA}$ or so. The gang capacitor is then opened, to increase loading, VC1 being readjusted as necessary for minimum current, as shown by the metcr. As this progresses, the input will rise. and the lamp light with increased brilliance.

With the valve employed, the screen grid current was about 5 mA so that the screen and grid currents together total about $6-7 \mathrm{~mA}$. In these circumstances. loading is increased until the meter shows roughly 6 mA more current, than the required anode input. An anode input of about $8-9 \mathrm{~W}$ is most suitable.

If prepared. the meter can be included in the h.t. circuit from L2 to RFC1 as mentioned. It then indicates anode current only.

For 160 m band working, crystals in the 160 m band are necessary, and the $160 / 80 \mathrm{~m}$ switch (S2) is open. For 80 m , close this switch, and use 80 m
crystals. Those 160 m crystals whose 2 nd harmonics fall in the 80 m band may be used for 80 m and 160 m operation.

## Testing Modulation

If wished, the modulator section can be tested by temporarily connecting a loudspeaker to the unwanted secondary of L2. Keep microphone and speaker separated, to avoid howling.

Modulation may be checked by connecting phones, to a loop consisting of a few turns of insulated wire, with a crystal diode in one lead. With the transmitter loaded into the lamp, bring this loop near to L1. Speech should sound clear and distinct.

The station receiver may also be used. To avoid overloading, the r.f. gain should be turned back, and it may be necessary to short circuit the aerial socket to chassis. Tune in the signal on the receiver, again ?keeping the microphone clear of the loudspeaker.

## Interconnections

The 'function switch provides single control sendreceive working. Receiver and aerial connecting sockets can be fitted to the panel. Or a length of co-gxial cable can be connected to the switch, and taken to the receiver aerial socket.

Transmitter and receiver are best side by side, and the aerial lead should run clear of other equipment.

Before transmitting, the function switch is turned, to net, and the oscillator signal is tuned in on the receiver. This shows the position which the radiated signal will occupy. The switch is then turned to transmit, a call made, and the switch returned to receive for replies.

## Aerial

And end-fed wire, with a total length of about 45 ft : ' upwards, is often employed for 160 m . The transmitter is loaded into the wire in the way describedifor the lamp test. The transmitter pi output tank coil can work effectively into a wide range of impedances.

Loading conditions can only be anticipated with any accuracy with $\frac{1}{4}$-wave and $\frac{1}{5}$-wave aerials. ©. 80 m , a $\frac{1}{4}$-wave is roughly 64 ft . This will have low impedance, so that the gang capacitor is well closed. On this band, a $\frac{1}{2}$-wave is about 128 ft , which has a high end impedance, so that the gang capacitor (VC2, VC3) will have to be set at a lower-capacity. The $128-132 \mathrm{ft}$. or so would be about a $\frac{1}{4}$-wave on 160 m , and thus low impedance on this band, while high impedance on 80 m .

With intermediate lengths, perfectly satisfactory working is generally possible, the gang capacitor being adjusted to suit. If a particular aerial length will not load the transmitter, the solution is to use an aerial tuner, or change the aerial length.

A'dipole is very satisfactorv, for one band only. For 80 m , it can be abouit 128 ft . with a centre $75 \Omega$ co-axiall or twin feeder. The feeder brading. or one lead of the twin, is taken to the chassis of the tranșituter. The remaining conductor is the aerial connection.
Satisfactory results have been obtained with short indoor wires, spirals suspended vertically,

and other aerials which can be erected in a limited space. Aerial tuners have appeared in past issues.

The following measurements were taken with the transmitter and VFO. Some variation from the figures given is not important. A $2 \mathrm{k} \Omega / \mathrm{V}$ meter was used on its 300 V range.

Mains transformer output 250/250V on net and receive.

Mains transformer output $240 / 240 \mathrm{~V}$ on transmit. Current consumption on receive: 6 mA .
Current consumption on net (crystal) 5 mA .
Current consumption on net (VFO) 25 mA . 6 J 5 a node, 200 V .
6 AG 7 anode, 150 V . S.G. 110 V . (VFO).
807 grid current $1 \frac{1}{2} \mathrm{~mA}$.
Loaded to 45 mA (cathode) input, 807 anode (at R FC) 200 V .

Loaded to 45 mA (cathode) input, 807 screen 165 V .5 mA .

6 V 6 anode current 38 mA .6 V 6 cathode 10 V .
807 total input, 9 W.
807 anode input, nearly 8 W .
H.T. drain on trancmit (crystal) 88 mA .
H.T. drain on transmit (VFO) 108 mA .

# ADDING A "MAGIC EYE" tuning INDICATOR 

By W. J. Holdsworth

ATUNING indicator of the magic eye type is a refinement easily added to a receiver by the home constructor, and the type used. a Y63, is readily obtainable from advertisers in this magazine.

The indicator consists of a triode amplifier valve with an extended cathode which allows electrons to strike a visible target electrode causing it to glow green. A V-shaped black shadow decreases as the signal is tuned in. The shadow is the result of a deflection of the electron flow by a field around the cathode ray electrode, introduced between the cathode and the target anode and joined to the triode anode.

Fig. 1: The circult arrangement necessary for the inclusion of the magic eye tuning indicotor in a receiver circuit.


The grid is connected to the a.v.c. line in an a.m.. receiver; or to the negative end of the discriminator stabilising capacitor in an f.m. receiver.

The anode current will be high in the no signal condition, and a large voltage drop will be produced across the anode load resistor. The triode anode and c.r. electrode will be at a much lower potential than the target anode.

There is a considerable effect on the electron flow and there will be a wide shadow.

As a station is tuned in the a.v.c. voltage rises and anode current decreases, causing an increase in the anode and c.r. electrode potential.

The shadow decreases in area and minimum shadow indicates correct tuning. Components may be mounted close to the valveholder. The indicator can be fitted to the front and panel by means of a capacitor clip or in any way which appeals to the constructor.

A hole $1 \frac{1}{32}$ in. will have to be cut for the Y63. A picce of sponge rubber may be placed around the valve under the clip.

An escutcheon, Bulgin type E8, may be utilised on the front to complete the finish.

COMPONENTS LIST
RI $1 M \Omega \frac{1}{2} W$
R2 IM $\Omega \frac{1}{2} W$
Cl $0.05 \mu \mathrm{~F} 350 \mathrm{~V}$
Y63 valve. One international octal valveholder. $1 \frac{1}{2} \mathrm{in}$. capacitor clip. Piece of sponge rubber. Nuts, bolts, etc.


## a pair of



PHYSICAL size is of some importance to constructors when items are built for "add on" application, i.e. are to be inserted or attached to equipment already operative. The pair of preamplifiers presented here are each quite small physically as may be seen from the illustrations and either, or both, may be added to a v.h.f./f.m. tuner to increase its output. Both units make use of a simple "printed circuit" construction easily duplicated.

## A Base for the "Printed Circuitry"

One of the aids available to constructors nowadays is a specially prepared "printed circuit type" board. This comprises thin plain paxolin with parallel copper strips each $0 \cdot 1 \mathrm{in}$. wide spaced apart by a similar distance on one side.
A matrix of small holes spaced evenly over the *urface at 0.2 in to coincide with the copper strips enables conventional wiring to be largely dispensed with and a circuit may be interlinked via the strips and the resistors and capacitors, etc., of which it is made. The board may go under various


Fig. It The type of commercially available "printed board" used for the units.
names but that used for the prototype is named "Verohoard" and is easily obtained.

A representative section of "Veroboard" (conductor side) is shown in Fig. 1, and as will be appreciated the material enables small items to be neatly constructed in a surprisingly short time. It is not thought likely that the board could withstand the application of high potentials but here no danger results since the h.t. voltages chosen are hardly lethal.

## Why Boosting is Required

Not all users of v.h.f./f.m. tuners are fortunate enough to reside close to a transmitter and results sometimes prove disappointing due to a poor loca-tion-which might also be one where traffic interference constitutes a further hazard.

Considerable distortion can be present in the output of v.h.f./f.m. equipment operated with insufficient aerial input because the limiter and discriminator stages are unsaturated. Furthermore, even if a tuner confers a reasonably high output this might not be comparable to that afforded by ancillary aparatus such as a crystal pick-up, a tape recorder outlet, etc.

One can, admittedly, attenuate these other sources to obtain a levelling overall but this might not always be desirable and in these cases it is better to increase the output of the tuner instead.

There are various ways in which the tuner output can be raised. (1) By improving the aerial system. (2) By amplifying the v.h.f. signal before it reaches the tuner. (3) By amplifying the outpur afforded by the tuner (audio amplification). (4) By using all the systems simultaneously.

# preamplifiers 



Fig. 2 : (a) A simple r.h.f./f.m. system and (b) with the addition of "booster" units.
A. S. CARPENTER

G8ABG
Construction is equally simple for either unit.

## The Signal Preamplifier

(Unit "A")
The circuit of Unit "A" is shown in Fig. 3, a cascade configuration being adopted. V.H.F./F.M. signals from the aerial are fed to T1 and appear amplified at T2 where they may be injected into the original aerial circuit of the tuner. The first triode (VIA) functions in grounded cathode mode but V1B operates as a grounded grid stage, the overall result being comparable to a pentode but without its noise.

Anyone wondering how V1A anode derives a potential for its anode should note that the two trindes are connected in series across the d.c. supply lines. each anode receiving one half of the available voltage, due to current flow.
The valve chosen is specially designed for the work and the potentials are adequate; the 180 V

It should be noted, however, that on no account should the cores of the i.f. transformers in a v.h.f./ f.m. tuner be "peaked" to obtain greater output.

A typical set-up is illustrated in Fig. 2 (a) where a conventional tuner feeds an audio amplificr. In many cases the first valve in such a tuner will be a ECC85 or similar type. Fig 2(b) shows a rearrangement to accommodate the proposed pair of preamplifiers and, of course, the resulting output will be much greater.
In the test assembly both units were easily accommodated within the tuner itself but other arrangements are possible. Both units need not necessarily be used, however, but if one is omitted it should, if possible, be Unit "B"-in a weak signal area at any rate.
Unfortunately, although Unit " A" is likely to be most suitable under such conditions it is less easily set up than Unit " B" since it contains tuned circuits. Current demands must also be considered and Unit "A" requires 8 mA at 150 V d.c. plus 0.33 A at 6.3 V a.c., whilst Unit "B" although more economical consumes some 2 mA at 150 V d.c. and 0.3 A at 6.3 V a.c.

This means that when both units are incorporated at least 10 mA and 0.63 A must be available from the existing d.c. and a.c. feed lines respectively.


Ag. 3i The circult of $\operatorname{IJ}!\mathrm{I}^{\text {a }} A^{n}$, the signal presmplifier.
limit should not be exceeded, however. Resistors R3 and R4 merely split the supply potential to bring the grid of V1B to a suitable voltage with respect to its cathode.

The input and output transformers are hand-made, both being air-cored. No variable tuning is fitted, the transformers being adjusted to give maximum output at the middle frequency. viz., the Third Programme. The overall bandwidth is restricted slightly by fixed capacitors C2 and C5. Details of transformer construction will be given later.

C1 and C3 are neutralising eapacitors and were not found to be unduly critical, although if a very low noise level is desired C1 may be replaced by a 15 pF (max) concentric trimmer. The r.f. choke is also hand-made and can materially affect the gain of the unit; in practice it is adjusted experimentally. With careful adjustment an overall gain of 18 dB can be secured.

## Constructing Unit "A"

The first step is to take a piece of "Veroboard" and with a hacksaw or fretsaw cut out a piece to the size shown in Fig. 4 so that it has seven conductor strips-which may be imagined to have numeral designations as shown. The ten rows of "holes" are given imaginary letter designations.

Next a cut-out should be made exactly as shown (in Fig. 4) just large enough to accommodate a ceramic noval valveholder. The two holes at " $x$ " and " $y$ " are then enlarged to 6BA clearance and a slot cut in the appropriate copper strip at " $z$ " with a file.

In this state the board is rather fragile but rigidity is regained immediately the skirted valveholder is bolted down. For the valveholder tag


Fg. 5: Wiring of Unit " $A$ " on the plain side.


Fig. 4: Wiring of Unit " $A$ " shown from the conductor side.
orientation it must be emphasised that a ceramic valveholder with tags placed in a like position with respect to the locking holes as that shown must be selected.

Fig. 4 also shows the wiring of the conductor sizc although with regard to the valveholder this mostly consists of bending over the contacts and soldering them where marked.

Resistors R3 and R4 are deliberately placed on the conductor side to simplify transformer adjustments later on the plain side.

At this stage four stout copper wires each about 1 in . long of, say, 22 s.w.g. are located and soldered in holes B2, B5, 12 and 15 to stand upright on the plain side of the board. These are later shortened to form "pillars" to accept the T1 and T2 main winding endings. The choke can be left until later.

Various differently coloured flying leads for supplics, etc.. are also required and may be soldered where shown. Depending on the final usage the negative line-and also perhaps lead "C"-will not be needed, as for instance if either strips " 1 " or " 7 " are in some way finally connected to the actual tuner chassis.

Work on the plain side of the board is illustrated in Fig. 5 and is quite straightforward. Remember, however, that when the valve can is placed over the valve it could short-circuit nearby component wires if care is not taken.

## Making the Transformers

The aim is to obtain an inside winding diameter of $\frac{3}{8} \mathrm{in}$. and reasonably thick wire-say 22 s.w.g. -should be used for the main windings.

Experimentally select a suitable capacitor, fountain pen or other "dummy former" that will permit the required final diameter and taking a length of wire together with another length of thin single strand PVC wire wind on seven full turns of both wires together, remembering that it is casier to remove a turn later than to add one.

Next unwind the PVC length urail only two turns remain and cut off unwanted lengths as necessary. With the dummy former, still in position
solder the transformer under construction as shown in Fig. 5, the main winding endings being soldered to the shortened wire lugs already fitted.

When the ends of the PVC insulated winding have been soldered as shown, carefully slide out the dummy former, when a self-supporting and neat transformer should be seen with the main winding turns spaced at about wire thickness from each other.

The other transformer is similarly constructed. To make the self supporting choke wind six turns of fine enamelled copper wire on to a $\frac{1}{4} \mathrm{~W}$ resistor then slide off.

The valve is next inserted into its holder and the screening can fitted. Check to see that no component lead-out is fouled. Check the unit with an ohmmeter to ensure no h.t. short circuit exists.

## Locating and Testing

The actual location of the unit in a given set-up will depend on the type of apparatus in use. If the preamp can be fitted in the tuner itself so much the better and one simple way of fixing it is to locate 1 in . long threaded spacers at each valveholder bolt so that the board is held stilt fashion.

With h.t. and l.t. fed lines connected it is merely necessary to remove the aerial leads to the tuner and re-connect to winding (a) on T1. A short length of screened cable is then connected between the tuner input and points (c) and (d) on T2.

At switch-on the h.t. voltage should immediately be checked and if in excess of 180 V d.c. the apparatus should be switched off and a 1 W dropper resistor inserted in the lead to the preamplifier h.t. To determine the approximate value needed use the simple formula:

$$
R=\frac{E \times 1.000}{8}
$$

where $R=$ the value of resistor required in ohns, and $\mathrm{E}=$ voltage to be dropped.

Therefore, if the measured h.t. line voltage is 244 V this is in excess of 180 by 64 , and so
$64 \times 1,000$

$$
\mathrm{R}=\frac{}{8}=8,000 \Omega
$$

A 1 W resistor of $8.2 \mathrm{k} \Omega$ would be suitable in this case. If such a resistor is used, however. connect the red end of a $4-8 \mu \mathrm{~F}, 250 \mathrm{~V}$ electrolytic capacitor to hole C 2 and its negative end to hole C 7 using a wire ended item.

## Setting Up

Tune in the Third Programme then adjust T1 and T2 for maximum output aurally, or visually by employing a suitable indicator and a signal generator. If it is found that when holding the dust iron cored end of a tuning wand inside either transformer the output increases, then the inductance value is too low and the turns should be squeezed together.

If on the other hand, as is more likely, introduction of the brass end of the wand causes output to increase then the inductance value is too large and if slightly increasing the turns spacing does not allow "peakiness" then a turn must be removed and the spacing readjusted.

## COMPONENT LIST

```
For Unit ' \(A\) '
\begin{tabular}{lll} 
RI \(220 \mathrm{k} \Omega\) & Cl & 10 pF \\
R2 \(100 \Omega\) & C 2 & \(4 \cdot 7 \mathrm{pF}\) \\
R3 \(100 \mathrm{k} \Omega\) & C 3 & 2 pF \\
R4 \(100 \mathrm{k} \Omega\) & C 4 & 2000 pF \\
\(\frac{1}{4} \mathrm{~W}\) & \(10 \%\) & C \\
VI-ECC84 & \(4 \cdot 7 \mathrm{pF}\) \\
CI-E6 & C7 & 2000 pF
\end{tabular}
T1, T2, RFC (see text) All ceramic
Miscellaneous-Noval valveholder (ceramic and skirted) with can, aerial lead, small piece
'Veroboard', wire, nuts and bolts, etc.
For Unit 'B'
\begin{tabular}{llll} 
R1 & \(470 \mathrm{k} \Omega\) & Cl & \(32 \mu \mathrm{~F}\) electrolytic 250 V \\
R2 & \(100 \mathrm{k} \Omega\) & C 2 & \(25 \mu \mathrm{~F}\) electrolytic 6 V \\
R3 & \(1.8 \mathrm{k} \Omega\) & C 3 & \(10,000 \mathrm{pF}\) ceramic \\
R4 & \(1 \mathrm{M} \Omega\) & C 4 & \(10,000 \mathrm{pF}\) ceramic \\
R5 & \(1.2 \mathrm{k} \Omega\) & & \\
R6 & \(22 \mathrm{k} \Omega\) & \\
R7 & \(10 \mathrm{k} \Omega\) & \(\mathrm{VI}-\mathrm{ECC}\) \\
All \(\frac{1}{4} \mathrm{~W} 10 \%\) & &
\end{tabular}
Miscellaneous-Noval valveholder (skirted) with can, small piece 'Veroboard', wire, nues and bolts, etc.
```

Fortunately this is fairly easy to accomplish, due to the layout, without completely removing the transformer. Supplies should be switched off whilst such adjustments are made.

When the transformers have been attended to the choke can be experimented with and slightly spacing the turns, using an insulated tool will indicate what is needed. If gain falls off the inductance of the choke is insufficient and vice versa.

On completion the transformers and the choke should be "doped" to keep the turns correctly positioned. The only other items capable of affecting gain are R3 and R4 and although some small amount of experimenting can be done here the values should not be made widely dissimilar.

## Other uses for Unit "A"

By modifving the transformers and the choke the preamplifier could be made to act similarly at different frequencies-for the $144 \mathrm{Mc} / \mathrm{s}$ amateur band or for Band III TV perhaps. The number of turns required must be found experimentally but for $144 \mathrm{Mc} / \mathrm{s}$ tuned windings of 4 turns are suggested with 2-3 turns for Band III TV. The input and output windings should also be reduced to about $1 \frac{1}{2}$ and 1 turn respectively.

## THE AUDIO PREAMPLIFIER (UNIT "B")

This unit is so simple as to need little description. The circuit is shown in Fig. 6 where V1A functions as a conventional audio amplifier feeding ViB operative as a cathode follower.

Leads associated with the input need to be kept short and might need screening but the output leads may be quite long if necessary since these

points are at low impedance. In this section the load resistor is R6 in the cathode circuit, R5 merely being a bias fixing item.

Low note response might possibly be improved by increasing the value of C4-and perhaps C3although sub-miniature specimens . might not be available at values ten times greater than the specified value.

The anode of VIB is made "earthy" due to Cl which further confers decoupling for the whole unit in conjunction with R7. The h.t. current demand (less than 2 mA ) is light indeed.

## Constructing Unit " $B$ "

Here again a small piece of "Veroboard " is cut and prepared to agree with Fig. 7, and although its length is identical with that used for Unit " A", it is wider by one conductor strip. "Wiring up " is very simple as may be seen from Figs. 7 and 8. Note, however, that some items are mounted verti-cally-as shown inset.

Again is it ncessary to select a valveholder with tags orientated as shown; it is also necessary to

Fig. 6: The circuit of Unit " $B$ ", the audio preamplifier


C1-ve to $\mathrm{H}_{2}$


Mount R1,R3,R5.
R7, C1and C2 upright

C2-ve to ©8

Fig. 7: Wiring of Unit " $B$ " shown from the conductor side.
select physically small compo nents.

Normally $\mathrm{C}_{\mathrm{in}}$ (Fig. 6) will be integral with the apparatus with which the unit is to be used and a volume control might also exist at this point. Should it do so, pin 2 of VIA could be connected to the slider and R1 omitted. The output at C4 (point m ) would then be joined to the wire originally in connection with the volume control slider but if this is done a $470 \mathrm{k} \Omega$ to $1 \mathrm{M} \Omega$ resistor should be wired between holes $B 1$ and $B 2$ or the valve following may receive no biąs.

A simpler method is to allow the top end of the volume control to be fed from C4 whereupon $C_{i n}$ which originally connected there, is wired directly to hole A7 as shown in Fig. 7 and RI retained.

Supplies are picked up similarly as for Unit "A" but in this case the h.t. voltage is not too critical; the board is not overstressed due to the preparation. A check for h.t. short circuits should be made on completion and before switch-on.

Fig. 8: Wiring of Unit " $B$ "-ploin side.

## Other Uses for Unit "B"

These are fairly obvious and if required an ancient receiver can be "pepped up" by the addition of a low power audio amplifier made to give really " meaty" output. Care should be taken to see that no overloading can occur though.

## Conclusion

Earlier it was stated that one way of improving reception of weak v.h.f./f.m. signals was to improve the aerial system. Actually this should be dealt with first of all, for a good aerial is greatly to be preferred to any preamplifier. It is easy to make a suttable aerial which should be mounted as high as is possible. If an outdoor location is not possible try using the loft, or a safe place under the eaves. If results are then inadequate the preamplifier(s) can be tried.

The dimensions and essential details of a suitable aerial can be seen in Fig. 9; the material being $\frac{1}{4} \frac{3}{8}$ in. dural or copper tube and connected to coaxial cable as illustrated. If possible the aeriak should be wholly in the horizontal plane but in difficult situations length " A" may be bent downwards.


Fig. 91 The dimensions and connections of a v.h.f./f.m. dipole.

Although such an aerial is not very directive it should be orientated for maximum pick-up of the area transmission. Directors or a reflector would increase the gain but are not usually desirable as excessive "beaminess" is introduced which limits the choice of stations considerably. If trouble is likely from passing traffic keep the aerial as far away from the roadway as is practicable.

## A FERRITE ROD D.F. AERIAL

 -continued from page 838the true position, however, so a second fix will still have to be taken from another point.
For example we have taken a fix from point A as in Fig. 7. The actual direction could be to X or $\mathbf{Y}$ as outlined above, a sensing aerial would determine the direction but since another fix must be

fig. 7: Plotting the true position of the unknown location of a transmitter.


Fig. 8: Another typical direction finding arrangement.
taken from another point (B) to find the true position, the direction would become known anyway.
Supposing the location of the transmitter were as shown in Fig. 8, i.e., in the direction of X (we will assume the d.f. receiver is already at point A as before). The second fix, taken at point $\mathbf{B}$ would now show the transmitter's true position somewhere along the line in the direction of $\mathbf{X}$.
One must obviously avoid taking fixes along the same line of direction. Always take the second fix at as wide an angle as possible from the first.

# some experiments with A.M. INTERFERENCE SUPPRESSION <br> <br> BY <br> <br> BY <br> <br> G. R. WILDING 

 <br> <br> G. R. WILDING}

PURPOSEFUL experiment must surely be one of the most engrossing aspects of amateur radio and one of the avenues in which the writer has carried out exploration is a.m. interference suppression.

In this article some original and interesting circuits are given for individual experiment and development, but first a recap on the only system used in pre-war receivers, apart from special aerials, when some attempt was made to remove this background noise.

The detector diode was negatively biased so that unless any signal first overcame this bias it could not be rectified, therefore this meant that inter-station noise and weak station signals failed to break through and left the entire waveband silent except for the really strong signal.

This method not only removed entirely weak signals but distorted any on the edge of the cut-off voltage as well as failing to remove heavy interference present with the strong signals and was by no means a good approach to the problem and, therefore, such systems are not now used.

The basic idea in the author's system is graphically shown in Fig. 1, where it will be seen that a high-mounted aerial in a static free zone has a dummy downlead running parallel to its own and being terminated at opposite ends of a standard medium wave coil whose centre tap feeds the receiver's aerial socket.
Equal value signal and noise microvolts are picked up by the real and dummy downlead,

cancelled out by the coils' magnetic field, leaving only the signal picked up by the actual aerial for amplification.
This is a sound and simple scheme which works well in practice. but while it ensures that the downlead does not contribute to the general. noise level, fails to remove what interference may be picked up directly by the aerial.
Then again, many listeners will he unable to have good outdoor aerials of any type in a staticfree zone.
The next step is to accept that an inferior indoor or outdoor aerial may have to be used and feed in anti-phase at the other end of the coil, a signal composed of equal noise level but much lower still signal level.

In other words, as poor an aerial as possible.
The most obvious snlution is a connection via a blocking capacitor to the neutral side of the mains, using the mains as an aerial, or the use of a threecore mains lead whose third wire will then comprise the "poor" aerial.

But here we strike snags. To get the two inputs to cancel out their noise content when fed to the inductance and leave only the strong station signal minus some quite unavoidable weak station signal from the mains aerial requires that both inputs must he of equal phase and voltage.

Variations in voltage amplitude can be levelled in various ways. perhaps the simplest being a sliding ferrite core to the coil which can vary the relative inductance of each half so that the magnetic fields can cancel out.

To get the phasing similar is much more difficult as the phase of each input is dependent on the LC values of the source.
Probably the best way, although here there is much opportunity for experiment, is to tune both aerial and mains aerial to the same frequency, when. of course, on resonance both circuits must be in phase.

Such an arrangement is shown in Fig. 2 and when correctly set up background noise will be found to diminish as adjustment of the core and canacitors produces almost a $100 \%$ noise cancellation.

Unfortunately the background noise pattern on both medium wave and long wave varies in character and intensity over the tuning range of the set so that the capacitor settings must be varied as one tunes up or down the dial.
This, of course, is a disadvantage and again calls

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## 3: CAPACITANCES CONTINUED AND BASIC A.C. THEORY

### 3.1 Capacitances Connected in Parallel

WHEN capacitances are connected in parallel, the total capacitance of the group is given by adding together the capacitances of the individual components. For example-in Fig. 23a,

$$
\begin{aligned}
C & =C_{1}+C_{2} \\
& =1+5=6 \mu \mu
\end{aligned}
$$

and in Fig. 23b,

$$
\begin{aligned}
C & =C_{1}+C_{2}+C_{3} \\
& =1+2+3=6 \mu \mathrm{~F}
\end{aligned}
$$



Fig. 23: Capacitances arranged in parallel.
When capacitances are connected in parallel, the highest voltage which can be applied to the combination is equal to that which can be applied to the capacitance with the lowest working voltage.

### 3.2 Capacitances in Series Connections

If two capacitances are connected in series, as shown in Fig. 24a, the total capacitance will be given by-

$$
\begin{aligned}
C & =\frac{C_{1} \times C_{2}}{C_{1}+C_{2}} \\
& =\frac{3 \times 6}{3+6}=\frac{18}{9}=2 \mu \mathrm{~F}
\end{aligned}
$$



Fig. 24 : Copacitances in series.
In Fig. $24 b$ the total capacitance will be given by-

$$
\begin{aligned}
\frac{1}{C} & =\frac{1}{C_{1}}+\frac{1}{C_{3}}+\frac{1}{C_{3}} \\
& =\frac{1}{1}+\frac{1}{2}+\frac{1}{3}
\end{aligned}
$$

$$
\begin{aligned}
& =\frac{6}{6}+\frac{3}{6}+\frac{2}{6} \\
\frac{1}{\mathrm{C}} & =\frac{11}{6} \\
11 \mathrm{C} & =6 \\
\mathrm{C} & =\frac{6}{11} \\
\mathrm{C} & =0.545 \mu \mathrm{~F}
\end{aligned}
$$

It must be remembered that the same units must be used throughout in any calculation of this type.

The total capacitance when two or more capacitances are connected in series is always less than the value of the lowest capacitance used.

The voltage appearing across a capacitance in a series connected arrangement can be found in the following way:
$1,000 \mathrm{~V}, \mathrm{E}$, is applied to three capacitances connected in series and having values of 1,2 and $3 \mu \mathrm{~F}$. C is the total capacitance and from Fig. 24 b it can be seen that $\mathrm{C}=0.545 \mu \mathrm{~F}$. Let the voltage across $\mathrm{C}_{1}$ be $\mathrm{E}_{1}$, that across $C_{2}$ be $E_{2}$ and that across $C_{3}$ be $E_{3}-$

$$
\text { then } \begin{aligned}
\mathrm{E}_{1} & =\frac{\mathrm{C}}{\mathrm{C}_{1}} \times \mathrm{E}=\frac{0.545}{1} \times 1,000=545 \mathrm{~V} \\
\mathrm{E}_{2} & =\frac{\mathrm{C}}{\mathrm{C}_{2}} \times \mathrm{E}=\frac{0.545}{2} \times 1,000=273 \mathrm{~V} \\
\mathrm{E}_{3} & =\frac{\mathrm{C}}{\mathrm{C}_{3}} \times \mathrm{E}=\frac{0.545}{3} \times 1,000=182 \mathrm{~V}
\end{aligned}
$$

-the sum of $E_{1}, E_{2}$ and $E_{3}$ being equal to $E$. Therefore in serles connected arrangements care must be taken to ensure that the voltage appearing across a capacitance does not exceed its Working Voltage.

### 3.3 Alternating Current

An alternating current is one which commences at zero, rises to a maximum positive value, falls to zero, reaches a maximum negative value and finally rises to zero once more. This whole process represents one complete cycle in an alternating current flow. This is shown graphically in Fig. 25, and it can be seen that the time taken for one complete cycle is called the period of the alternating current.


Fig. 25ı An a.c. waveform.
The amplitude of an alternating current is the maximum value of current reached-whether positive or negative. The frequency of an alternating current is the total number of complete cycles which take place
tn one second or $\mathrm{f}=\frac{1}{\mathrm{~T}}$ where t is in seconds and f is in cycles per second. Two examples of the frequencies of alternating currents are (1) The mains supply$50 \mathrm{c} / \mathrm{s}$. (2) The Light Programme- $200,000 \mathrm{c} / \mathrm{s}$.

### 3.4 Phase Differences in Alternoting Currents

A complete alternating current (a.c.) cycle is divided into 360 degrees, as shown in Fig. 26.


Fig. 26: Phase differences in alternating currents.
The a.c. cycle drawn as a dotted line has the same frequency and amplitude as I, but it LAGS $90^{\circ}$ behind I-or it has a phase lag of $90^{\circ}$ compared with I.
Although the above work is concerned with alternating currents, exactly the same conclusions are reached when dealing with alternating voltages or a combination of the two.

### 3.5 Alternating Currents Applied to Resistances

When a.c. is applied to a (pure) resistance, the current flowing in the resistance varies completely in step with the voltage appearing across the resistance. This means that there is no phase difference between current and voltage. Because there is no phase difference, Ohm's Law can be applied directly when a.c. is applied to a resistive circuit.


Fig. 27 t A.C. applled to a resistance.

### 3.6 R.M.S. Values for Alternoting Currents

If a voltage of 250 d.c. was applied to a resistive circuit and the amount of heat which was dissipated was noted and then 250 volts a.c. was applied for the same length of time, it would be found that the heating effect of the a.c. would be more than that of the d.c. The value of the a.c. voltage which would give the same heating effect as 250 volts d.c. is

$$
250 \times 0.7=175 \mathrm{~V}
$$

This voltage is called the Root Mean Square (r.m.s.) value of the a.c. voltage and it is equal to $\frac{1}{\sqrt{2}}$ of the


FIg. 28: A.C. applied to a capacitance.
peak voltage.

$$
\begin{aligned}
\text { or } & \text { Vpeak }=\sqrt{ } 2 \times \text { Vr.m.s. } . \\
\text { also } & \text { Vr.m.s. }=\frac{1}{\sqrt{2}} \times \text { Vpeak } \\
\text { or } & \text { Vr.m.s. }=0.7 \times \text { Vpeak }
\end{aligned}
$$

### 3.7 Alternating Current Applied to o Capacitance

When an alternating current is applied to a capacitance the voltage which is being used to push the current through the capacitance lags $90^{\circ}$ behind the current or the current leads voltage by $90^{\circ}$. This is shown graphically in Fig. 28.

### 3.8 Capocitive Reactance

When a.c. is applied to a capacitance the current flowing depends on the frequency of the a.c., the value of the capacitance and the applied voltage. The frequency of the a.c. and the value of the capacitance affect the current flow in much the same way as resistance affects the current flow in a d.c. circuit. The name of the component, derived from the frequency and the capacitance, is the capacitive reactance and it is measured in ohms and is represented by $\mathrm{X}_{0}$.

$$
X_{0}=\frac{1}{2 \pi \mathrm{fC}}
$$

where $X_{c}$ is in Ohms, $f$ is in cycles per second, $C$ is in farads and the constant $\pi=3 \cdot 14$. It is however much easier to use microfarads for $C$ and megacycles for $f$, in which case the capacitive reactance will still be in ohms.
e.g. Find the reactance of a capacitance of $0.005 \mu \mathrm{~F}$ at 0.5 megacycles ( $\mathrm{Mc} / \mathrm{s}$ ).

$$
\begin{aligned}
& \mathrm{X}_{\mathrm{c}}=\frac{1}{2 \pi f \mathrm{C}} \\
&-\frac{1}{2 \times 3.14 \times 0.5 \times 0.005} \\
&=63.7 \Omega
\end{aligned}
$$

For a circuit containing only capacitive reactance,


Fig. 29: A.C. applied to an inductonce.

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the current flowing in the circuit, I, can be found by using the expression:

$$
I=\frac{E}{X_{c}}
$$

which is purely a modification of Ohm's Law.

### 3.9 Alternating Current Applied to an Inductance

If an alternating current is applied to an inductance, the voltage in this case leads the currem by $90^{\circ}$. This is the opposite to the case when a.c. was applied to a capacitance. The flow of current through an inductance, compared with voltage, is shown graphically in Fig. 29.

### 3.10 Inductive Reactance

When a.c. is applied to an inductance the current flowing through the inductance depends on the applied voltage, the frequency of the a.c. and the value of the inductance in henrys. The current flow does in fact vary directly as the frequency and inversely as the inductance. Once again, the frequency and the inductance affect the current flow in the same way as does resistance in a d.e. circuit. The component, which is derived from the frequency and the inductance, is called the inductive reactance and it is measured in ohms and represented by $X_{L}$.

$$
\mathrm{X} L=2 \pi \mathrm{fL}
$$

where $X_{L}$ is in ohms, f is in cycles per second and $L$ is in henrys.

In radio frequençy circuits however, the inductance can be expressed in millihenrys ( mH ) and the frequency in kilocycles ( $\mathrm{kc} / \mathrm{s}$ ).
e.g. What is the reactance of an inductance of 0.2 henrys at $500 \mathrm{c} / \mathrm{s}$.?

$$
\begin{aligned}
\mathrm{X}_{L} & =2 \pi \mathrm{fL} \\
& =2 \times 3.14 \times 500 \times 0.2 \\
& =628 \Omega
\end{aligned}
$$

For a circuit containing only inductive reactance, the current flowing in the circuit, I, can be found by using the expression:

$$
\mathrm{I}=\frac{\mathrm{E}}{\mathrm{X}_{L}}
$$

which is once more purely a modification of Ohm's Law.

## Question

What is the reactance of a capacitance of $2 \mu \mathrm{~F}$ at $50 \mathrm{c} / \mathrm{s}$ and what current would flow through it if 250 V a.c. were applied to it? What value of inductance would have the same reactance as the above capacitance, when the frequency remains at $50 \mathrm{c} / \mathrm{s}$ ?

## Answers to Last Month's Problem

1. To convert to a Voltmeter reading to 250 V .

$$
\begin{aligned}
R & =\left[\frac{\mathrm{E}}{\mathrm{I}} \times 1,000\right]-\mathrm{Rm} \\
& =\left[\frac{250}{10} \times 1,000\right]-50 \\
& =25,000-50 \\
& =24,950 \Omega
\end{aligned}
$$

or Voltage across meter

$$
\begin{aligned}
=E & =1 R \\
& =0.01 \times 50 \\
& =0.5 \mathrm{~V}
\end{aligned}
$$

$\therefore$ Voltage across shunt

$$
\approx 250-0 \cdot 5=249 \cdot 5 \mathrm{~V}
$$

Current through shunt

$$
\begin{aligned}
& =\frac{E}{I} \\
& =\frac{249 \cdot 5}{0 \cdot 01} \\
& =24,950 \Omega
\end{aligned}
$$

2. To convert to an ammeter reading to 2 amps.

$$
\begin{aligned}
\mathrm{R} & =\frac{\mathrm{Rm}}{\mathrm{n}-1} \\
& =\frac{50}{200-1} \\
& =\frac{50}{179} \\
& =0.252 \Omega
\end{aligned}
$$

or Voltage across meter $=0.5 \mathrm{~V}$ (see above)
$\therefore$ Voltage across shunt $=0.5 \mathrm{~V}$
Current through meter $=0.01 \mathrm{~A}$
$\therefore$ Current through shunt $=1 \cdot 99 \mathrm{~A}$

$$
\begin{aligned}
\therefore R & =\frac{E}{\frac{1}{0.5}} \\
& =\frac{1.99}{} \\
& =0.252 \Omega
\end{aligned}
$$

Part 4 Next Month

## A.M. INTERFERENCE SUPPRESSION

## -continued from page 866

for experimental work to eliminate.
However, to remove the noise from one particular station, or over an 80 to 120 m waveband sector, the unit described will be found most effective, although for best results it should all be enclosed in an earthed metal case.

The same principle of feeding two noise-bearing signals in anti-phase so that the unwanted interference cancels out, leaving only the pure signal, can be employed with two ferrite rod aerials.

One is positioned in the usual manner for maximum signal strength while the other is placed for maximum interference pick-up consistent with minimum signal pick-up.

The two aerial windings are connected in series anti-phase and as both will be of identical construction no centre-tapped coil will be needed, for cancellation will not be achieved magnetically but by the subtraction of the two opposing e.m.f.s in exactly the same manner as the equal but opposite voltages in a frame aerial cancel out when placed facing the station.

Unfortunately as the two aerial windings are in series it will be essential to halve the number of turns on each rod to maintain the correct inductance and this will halve the induced e.m.f.

However. in strong cases of local interference it may be found that sufficient noise voltage can be picked up by a one-third winding on the static rod, leaving two-thirds for the signal rod, thus keeping station strength to a maximum.

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## PI: AUDIO QUALITY, by G. Sloz

156 pp. Price 13s. 8 d .

THIS is not a book for those requiring circuit diagrams or other specific information of that kind. It is, however, a storehouse of facts, figures and design ideas. Some measure of this can be illustrated by the fact that it contains 26 tables within the twelve chapters.

This does not mean that the book is academically "dry"; on the contrary the author tackles his subject matter in a readable (dare we say "chatty"?) spirit. Experiments made by the author are used to illustrate points, and throughout the book, one has the feeling that one is in the hands of the authoritative, yet "human" writer.

The opening chapter is full of interest and sets the pace and style for the rest of the book. In dealing with the question "what is hi-fi?", the author approaches the subject with wisdom and common sense and should be required reading by anyone interested in this subject. As a brief example, he states that "Technically perfect reproduction leads to uncertainty about the musical quality. Musically perfect reproduction leads to uncertainty about the technical specification."

The main chapters are Power Requirements, Non-linear Distortion, Frequency Response, Pitch Deviations, Background Noises, Stereophony, Other chapters include one entitled Experimental Evidence and the opening sentence "When theory and experiment agree, one is naturally suspicious" gives a lead to the entertaining approach of the whole book. Not to be missed by audio-philes.-W.N.S.

## * P2: THE TAPE RECORDER, by C. G. Nijsen 틀 142 pp. Price 13. 6d.

WE have two quarrels with this one. Firstly the sub-title is "A complete handbook on magnetic recording". This is not quite true since it is written mainly for the user of tape recorders and does not delve into details of the mechanics (or the electronics). Secondly, and this must bo correlated to the first comment, the section on faults only occupics $4 \frac{1}{2}$ of the 142 pages of the book; even then the information given is extremely basic and has appeared elsewhere many times.

Having said this, one cannot carp any more.

And, in any case, the criticisms given are really relative to the aims of the author. We will even forgive him such extravaganza as ". . . this most ingenious product of Man's imagination set out on what was to prove the triumphant globe-encompassing path" in the Introduction!

In all fairness, this is good value. Chapters include introductory ones on the nature of sound and a potted history of sound recording. A third of the book covers The Tape Recorder (Principles, Speeds, Sound Tracks, Electromagnetic Process. Recording and Reproducing Processes, Sound Quality, The mechanism, Microphones, Loud-speakers)-42 pages.

The next largest section (29 pages) is Advice on Making Recordings, and this is, perhaps, the one which will appeal most to the type of reader at which the book is aimed. Other sections are quite brief, but deal with a wide range of subjectStereophony, Acoustics, Choosing a Recorder, Connections and. Accessories, to name the most important.

This book is not for the technical genius or advanced tape enthusiast, but at the price it can hardly be bettered as an introduction to the suhject for newoomers requiring an essentially nontechnical treatment of how to get the best from a tape recorder.-W.N.S.

## 三 P3: AERIALS, by D. Stobbame <br> $\equiv 110 \mathrm{pp}$. Price 10s. 6d.

IHIS is a practical book, with little mathematics, and is particularly designed for those who have to tackle the problems of siting and erecting aerials. It is not a treatise on all manner of aerials, but confines itself to considering TV and f.m. aerials only and although this may at first seem to detract from the value of the book, on reflection it seems a good idea. For here we have the information in a concise form with no extraneous information to detract.

The book takes a more or less predictable form -a first chapter dealing with the theoretical aspects of energy transfer from transmitter to receiver, followed by descriptions of dipole aerials (the book confines itself, of course, to dipoles and elaborations thereof, such as the Yagi) and then chapters on the choice and installation of aerials, connections to the receiver, attenuators and multiple installations. The book rounds off with an appendix of useful data, including a host of British, CCIR and RTMA channel numbers and frequencies.

One criticism is that nothing is said at all about preamplifiers, except for a valve unit for use in collective aerial systems. It is a pity that some mention could not have been given of transistor aerial preamplifiers. Nevertheless, the book has much useful information and merits a place on the bookshelf.-W.N.S

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# Bread-board Wiring 


W. Groome

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TTHE object of bread-board wiring is not to imitate printed circuitry but to achieve similar compactness by methods familiar to the homeconstructor and more suitable for single hand-made products. As in printed circuitry the usual metal chassis is replaced by a thin plastic panel-today's descendant of the plywood bread-board of early radio days. Bare tinned copper wires are firmly attached by simple methods and with more freedom in arrangement than is possible with printed stripes.

## Some Advantages

With no earthed metal to worry about live components can be fixed anywhere on the panel, conserving space by using head-room necessary in any case to clear valves, coil-cans and other fixed items, and allowing short connections above or below. This arrangement, with the wires secured neatly along the panel surface, is comparable with printed circuitry and is particularly suitable for small transistor equipment. However, we can improve the seope of the system in a way that is denied to the printed circuit designer by allowing a small clearance beneath the board in which snall components and short wires can be suspended. This amounts to a two-layer wiring capable of conserving considerable panel area, which is a worth while exchange for a small depth of $\frac{1}{2}$ in. that is often needed in any case for panel stiffeners or mounting arrangements.

A four-valve experimental push-pull amplifier shown in the photograph on the following page, is housed comfortably on a 9in. $x$ 6in. panel of which almost one-third was necessary for the large output transformer. Although the underside wiring looks slight compared with the conventional style of wiring the amplifier is of full specification and is used later in this article as an example of practical work. The abolition of groupboards and the arrangement of the components in logical positions has led, as we shall see later, to a lay-out having a distinct resemblance to the theoretical circuit.

Plain plastic laminate (not metallised) is available in several grades from radio quality " Paxo-
lin " to the cheap "backing vencer" seen in the photographs. Use $\frac{1}{6}$ in. thick material for valve circuits and about half this thickness for little transistor sets.

## Interconnections

Ignoring components for the moment Fig. 1 shows how wire can be safely attached to the panel by "stiches" passed through small holes. A change of direction is initiated by a single hole or a two-hole stitch. Note particularly the way the wires can be shifted from one side of the panel to the other. This is of the utmost value in allowing "wires to dodge each other at crossings, for the "leap" that clears them without danger of electrical contact also anchors them to the panel. This is the feature that makes it possible to complete a complex circuit mainly with bare wire-entirely


Fig. 1! The method of "stitching" connecting wires between holes made in a paxolin chassis.
with bare wire if one is determined to push the system to the extreme.

Fig. 1 gives several variations of the method and it will be obvious that wires can be made to emerge through the board at any point convenient for the connection of components on either side. This surface wiring is an important part of the system but there is no need to make a fetish of it simply to achieve some resemblance to printed circuitry, for it is possible to make the work even easier by using here and there a few of the more useful tricks of chassis wiring. For short point-topoint connections 20 to 22 s .w.g. wire is stiff enough to be reliably self-supporting and there is no


A amplifier constructed by the author which shows the clean layout obtainable using bread-board wiring.
wiring is completed the screws can be removed for re-use. Self-threading screws can be obtained from engineer's stockists; the No. 39 drill is a suitable size for making stitch holes.

Fig. 2 also shows another way of anchoring components. Here the panel wiring ends at a couple of stitch holes and is threaded through them twice before being snipped off. The "groove" between the two turns accommodates the component wire snugly and provides an anchorage area for solder, which converts the anchorage into a tiny composite metallic block virtually incapable of movement or fracture in any normal conditions. The last method in Fig. 2 again uses a two-turn stitch, this time to bind the component wire down to the board. The end is then doubled back over

The absence of a metal chassis is no problem even at v.h.f. Indeed, it is an advantage because wiring capacitance is virtually eliminated. As a screen the chassis was never wholly effective, while its ability to circulate hum and interference currents had long ago led to a preference for busbar earthing. This, or a near equivalent, is the earthing method used in bread-board wiring. If conventional metalcollared valveholders are used (they are quite suitable, and easier to obtain than the printed-circuit type) put tags under the fixing screws so that a continuity wire can be run
reasom why this well-known idea should not be used with a bread-board, with the wire either pressed close to the surface or suspended clear of it (and other items) by the tags to which it is coldered. This is one advantage of the underside clearance already suggested. Stiff air-spaced wires form another safe way of crossing without contact.

Very often, in this underside space, small capacitors and resistors can be point-to-point connected, as in chassis wiring. Using conventional valveholders (which are as well suited to the system as the printed circuit surface type) and again drawing from chassis experience, common-earth connections with small components soldered across the tags demand no extra panel area and provide the technically correct short, direct leads.

## Anchoring Components

Instead of the group-boards necessary with a metal deck the non-conductive bread-board permits wire-ended components to be fixed direct to its surface. Solder tags (Fig. 2) are a handy method of anchorage. Ordinary BA screws can be used, of course, but I find it quick and convenient to fit No. 4 type " $Z$ " self tapping screws. These can be driven like wood-screws into holes made with a No. 39 drill and no nuts are required. I usually put a dab of "Araldite" adhesive under each tag and when this has hardened and the
along the panel from holder to holder. With two tags per valveholder it is possible to branch the earth lead for convenient connection of components anywhere on the board, or to duplicate it


Fig. 2: Methods of anchoring components to the panel.


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Fig. 3: The push-pull amplifier circuit used in the practical example.
an awl. Screwed tags will generally seem too large for this miniature work, therefore the alternative anchorage illustrated in Fig. 2 should be scaled down for this purpose. All components can go on top and the wire can run on either side; the underside clearanco can be reduced to as little as tin. Remember that plastic materials are poor conductors of heat and that power transistors must be mounted on the area of metal recommended by the makers to avoid thermal run-away.

## A Practical Example

The amplifier shown in the photograph is used for a description of practical work because most of its circuit (Fig. 3) is familiar. It was built to test a number of unconventional output transformers that will not be described here, and as the photograph shows signs of the rough experimental treatment a little "tidying up" has gone into the wiring diagram, Fig. 4. To achieve the utmost clarity the drawing is purposely out of scale and the components have been spaced much more widely than in
when it is desirable to halve its r.f. inductance. Near to the tags small holes enable short wire connections to be dropped through to the valveholder tags. Other underside leads and components can be earthed at the valveholder common point or fed through the panel to any point on the bus-bars.

Heater, h.t., a.v.c. negative feedback and other long lines should be stitched to prevent them from drooping and touching other parts. Although all wiring can be bare it would be ridiculous to spurn an insulated lead if this could help to achieve the speed and simplicity that is the aim of the system. Centre-tapped heater wiring is an example. The twisted pair for this must obviously be of insulated wire. The single lead for an unbalanced heater supply, however, is often more conveniently arranged with bare stitched wire.

With a thin bread-board and fairly fine wire transistor circuits present no problems. Wire-holes can be pierced with


Fig. 4: The bread-boord wiring diagram of the amplifier circuit of Fig. 3.
the photographs. although their relative positions are unchanged. This is for the purpose of illustration and the practical version would be compressed to the scale of the photograph.
Fig. 4 is an underside view and everything visible on that side is depicted in bold line (double to indicate air-spaced wires), while top-side wires and components are "ghosted" in broken line. I suggest the following procedure which will be suitable for wiring the majority of circuits. Beginning at a tag screwed to the flange of the input socket run an earth line on to the top side to all valveholders and to the negative terminal of the power supply. Drop wires through to connect earth to the appropriate tags on the valveholders. Connect the insulated and twisted heater wiring, pressing it close to the surface of the panel. Alternatively, this pair can be laid on top and fed through where needed for connection. The heater wiring is not shown in Fig. 4, which does, however, indicate tags in places where none are to be seen in the photograph in order to make clear indication of certain connections. The constructor will quickly learn where tags are essential and where they can safely be omitted.

Begin the signal circuit with an air-spaced connection from the input socket to V1 grid and solder R1 at the valveholder. Strap cathode and suppressor across the valveholder with a short insulated wire and from here talre a bare wire through to the top where C1, R2 and R3 are supported on tags in positions very similar to those in the theoretical circuit. These three components have a common point to which the feedback lead is connected. C2, quite small, is supported on top of the panel by stitches with its wire ends fed through to the screen-grid and common cathodesuppressor tags. R4 makes a point-to-point connection to the decoupling network.
This first valve stage illustrates very distinctly the way that wires in crossing directions can be kept safely apart by separating them to opposite sides of the panel, and even with the deliberate " expansion" of the drawing the shortness and directness of the wiring is noticeable. Wire the anode to a tag supporting the load resistor R5 and the grid components of V2. Although an insulated wire was used for the direct grid connection during the experiments this can be left bare in a normal job not subject to frequent alteration. R7 makes a point-to-point connection to the other grid of V 2 , from which a wire feeds through to C5 on top of the panel. Strap the cathodes with insulated wire across the valveholder and connect R 8 to earth. Connect the anodes to R9, R10 supported on three tags.

The decoupling components for these two stages have resistors on the underside and the double electrolytic capacitor above; the correct wiring for this network is as indicated in Fig. 4 and not as used for a special purpose in the prototype.

Again following circuit sequence and avoiding the unrelated positioning of ten needed with groupboards, connect the coupling capacitors C6, C7 convenient to the anode resistors and to the grid components of the output stage. Fit the four bias components on the top with the resistors R16 R 17 raised well clear so that their heat may be dissipated in air. With many output transformers it may
be best to use flexible insulated connections from the anodes and screen-grids, as shown in the diagram.
This is not intended as a final amplifier design, for readers of this journal are already well served in that respect, but it is familiar enough to enable the bread-board version to be studied without difficulty. The layout shown could be used for any similar circuit provided the design differences (in feedback arrangements, for instance, or added phase-correction networks) are incorporated. The amplifier was particularly well behaved in the high frequency end of the audio range, and this was undoubtedly due to the absence of stray capacitance which, with a metal chassis, can be high enough to influence feedback stability.

## Layout Planning

Perhaps the most welcome virtue of the breadboard is the elimination of metalwork, for the construction and assembly work is delightfully easy with laminated plastic. As always, the best results will be the outcome of a little advance planning. Shuffle your components on the bench until you arrive at a layout that is compact and suitable for the circuit and physical connections, deciding which shall go on top and which below. For a start in planning you could begin with positions similar to those of the circuit diagram, but be practical about this when some variation is obviously preferable. Measure the area required, sketch your final plan, and then go to work on the panel.

You will not find edge stiffeners necessary with small panels and light components, but the addition of the $\frac{1}{2}$ in. square hardwood strips does aid cabinet installation and heavy parts like transformers do need this extra support. I have compared this panel system with the old bread-board, but, curiously enough, the edge stiffeners actually convert it into a shallow box not unlike the (genuine) cigar boxes used for crystal sets in even earlier radio times!

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# A COMMENTARY BY HENRY PRACTCAIMY WIRELESS <br> No. 5 Bring in the New 

THE turn of the year is the time for three things: resolutions, diaries, and wild, wicked speculations about the year to come.

Take a look at any daily paper; any weekly periodical; any monthly magazine. You will find the sages and the pundits solemnly pontificating on the prospect that lies before us. Never a word, you'll note, about the equally emphatic predictions of yesteryear. Unless, by some twist of chance, the random shaft of prophecy hit the mark and became fact.

This column has learned its lesson about resolutions. Wilde observed accurately that the fatality of good resolutions is that they are always too late. He might have added that the fatuity of the bad ones is that they are always too easy to keep. Like the resolve made to wrap each joint firmly before applying the solder:later regretted when one discovers the component was fastened to the wrong tag. Or the determination to build and test all those coveted pieces of equipment: usually reculting in a heap of half-completed junk in the corner of the outhouse.

No, the only resolutions your scribe will impose are the few he


A heap of half-completed junk.
expects olfars to adacia w Writing legible letters, enclusing stamped, addressed envelopes, keeping strictly to the point . . . especially when writing to the Editor.

He could add also some optimistic hopes: that manufacturers of radio equipment would resolve (a) to be a little less enthusiastic when applying the power screwdrivers to those dinky-headed self-tapping screws; (b) to eschew the plastic knob that disintegrates when threatened with removal, and (c) to provide some sort of service data on the tangled mystery their clever advertising has sold us.

Or, to be even more optimistic. to hope that the radio trade would regard the questing amateur as a friend and not a potential rival. Would supply, not necessarily at less than full profitmaking prices, the asked-for spares across the counter. But that would imply a revolution rather than a resolution.

Diaries: what of them? There is no lack of exemnlary material. But the famous diarists of the past do not seem to have included a radio pinncer among their ranks. Pepys was, it is true, well versed in the art of communication: but mainly on the wavelength of serving-maids. Dampier had something of the right idea, stuffing his rolled manuscripts up his hollow. bambon rods for posterity to find. And as for John Fvelyn, though he was a Fellow of the Royal Society, it is hardly likely he could whip up much information on electronics at the end of the seventeenth century.

Nowadays, we are all too busy to bother with more than the cryptic ideograms that may once have been meant as reminders about those standard faults and useful formulae. Pages are covered with strange suippets of circuits and figures that bear no relation to anvthing, least of all


Pepys was well versed in the art of communication.
the date at the head of the page. Interspersed with odd shopping lists, telephone numbers now exdirectory, and addresses of bankrupt firms that were once the source of our bargain lines in spares. I can trace the progress from a Short-wave Two to a Communications Double-Super that never did reach completion.

Leafing through old diarles, which one dare not throw away in case the information comes in handy, is a pleasure akin to browsing through the musty back numbers of P.W. But some of the entries seem completely foreign. Wilde was right to observe that everyone should keep someone else's diarv. It certainly looks as if someone else was keeping Henry's during the stereo upsurge of '58. How else to account for those enthusiastic entries:
" Double amp - try feedback over balance . . ." or
"Speakers - $Z^{2}+Z_{0}=$ ???. Match Trans. 8 mf series
"Back-to-back cardioid-sound cancellation? What price Blumlein?"

Perhaps the most interesting part of the modern diary is the "specialist" section. We find ranks of these handy pocket compendiums in the bookshops. Whether you are a Boy Scout, an engine-driver, a rose-grower, a radio fanatic or a plain and
-continued on page 898

## PART 4-FEEDBACK IN TRANSISTOR CIRCUITS

# Understanding SEMICONDUCTORS ${ }_{\text {вуцгин шоовв }}$ 

CONTINUED FROM PAGE 774 OF THE DECEMBER ISSUE

TRANSISTOR amplifier gain also depends on the interstage coupling. This consists of the emitter - collector capacitance, impedance matching between stages and the working frequency.
The gain of an amplifier may be altered by taking some of the amplifier output and feeding it back to the input. This method is known as applying feedback.
Feedback may be split generally into two main categories: Positive feedback, negative feedback.
When positive feedback is applied to the input terminals of an amplifier it is additive to the input signal and therefore it can be said that the amplitude of the input signal is effectively increased. The gain of the amplifier stage itself is constant; the amplitude of the input has increased, hence the output amplitude will also increase. The apparent gain of the amplifier has then become greater with the application of positive feedback.
Fig. 25 shows the input signal, the signal fed back and the effective value of input due to feedback. The input and feedback signals are in phase.


Fig. 25: The effect of positive feedback on the input signal.



Fig. 26: The input signal with negative feedback applied.

Negative feedback is that feedback which, when applied to an amplifier, makes the effective input signal smaller; the output signal is then also made smaller. Stage gain will then appear to decrease by applying negative feedback.

Fig. 26 shows diagramatically the effective value of input signal due to negative feedback.

Input and feedback signals are in opposite phaso or $180^{\circ}$ out of phase.
The application of feedback to a circuit may have several other effects on the functioning of that circuit, otherwise there would be little need to ever apply negative feedback.
A most important effect is on the working frequency range or " bandwidth".
Although positive feedback increases amplifier gain the bandwidth is made smaller. If an amplifier is required for small frequency ranges only, or even for a fixed frequency, positive feedback would be ideal.
Negative feedback increases amplifier bandwidth. This would be used in a circuit which required a stable gain of a wide frequency range such as an audio amplifier used for both speech and music.

Unintentional feedback in the circuitry may take place due to component positions. Two resistors connected in the circuit, side by side, will act as a small value capacitor. Component positions are of more importance in valve circuitry than in transistor circuitry due to the larger component sizes but are still of some importance.
Too much positive feedback could drive a transistor into cutoff or saturation. whereas negative feedback may dampen the input to such a degree that no output is obtainable.

Feedback is also used extensively in a series of electronic circuits known as oscillators.

A pendulum is an analogy to the oscillator.

The mechanical movement of the pendulum is such that if some force is not present to sustain the swinging action the sweep angle decays due to friction losses at the fulcrum and a minute amount of windage.

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Left hand side movement

Fig. 27 (left): Plotting the movement of a pendulum against time produces a sinusoidal graph.

Fig. 28 (below): The parallel LC arrangement for oscillator circuits.


Suppose a pendulum were to be set in motion but, instead of leaving the movement to die away, a small force is used at the end of each swing to make up for the friction and windage losses. it would be seen that the pendulum would swing indefinitely.
If the length of the pendulum were shortened the pendulum would swing to and fro more quickly. Conversely if the pendulum were to be made longer the number of swings per second or swing frequency would decrease.
Considering one swing of the pendulum. starting from the centre and plotting the vertical movement of the weight against time. a sinusoidal wave is produced as shown in Fig. 27.
Several types of osciliators exist using either inductors and capacitors (LC) or resistors and canacitors (RC) to produce oscillation.
If a capacitor and inductor were connected together in parallel as in Fig. 28 and a battery applied across them for a moment, allowing the canacitor to charge up to the voltage of the battery and then (thè battery) withdrawn. the capacitor would discharge into the inductor, producing a magnetic field around the inductor. This would then be converted into energy to recharge the capacitor.
It is impossible to obtain an inductance with zero resistance. therefore a certain amount of energy would be lost on each oscillation.
This parallel circuit would act similarly to the pendulum in that the oscillations would fall away, also the oscillations would be of a sinusoidal form.

It was explained that. by applying a battery across a capacitor and inductor in parallel and then withdrawing it current in the parallel circuit moved to and fro sinusoidally with an amplitude decreasing in size with time due to resistive losses in the inductor. To enable the parallel circuit to produce an oscillation of constant amplitude, feedback must be applied. The type of feedhack must be additive to the oscillation, therefore positive feedback must be used.

A transformer or two inductors in magnetic coupline has an inductance due to factors contained by both coils. A transformer may also produce a $180^{\circ}$ phase shift in currents fowing through the coils.
A grounded emitter amplifier produces a $180^{\circ}$ phase shift between base current and collector current: $360^{\circ}$ phase shift may be taken as no phase shift as one cycle of oscillation spans $360^{\circ}$. One
winding of the transformer in the collector circuit of the transistor would produce a $180^{\circ}$ phase shift between the collector current and that flowing in the second transformer coil. The base current would then be in phase with the current in the second transformer coil. If the second coil were to take the place of the inductor in the LC jaralled circuit the induced current in the second coil would be of such a nature so as to aid the natural oscillations. Providing this feedback is of sufficient magnitude to overcome losses the circuit would oscillate at a constant amplitude.
The basic iclea of this system is shown in Fig. 30.
Fig 31 shows a circuit diagram of such an oscillator. $R_{1}, R_{2}, R_{3}$ and $C 3$ provide biasing between base and emitter. The value of inductance


Fig. 29: Explanatory diagram of the LC oscillator.


Fig. 30: Circuit of an LC oscillator. CI prevents the base from shorting to earth.
is a combination of factors in L1 and L.2. Frequency of oscillation depends on this combined value. known as mutual inductance, and the value of capacitor C1.

On application of the voltage source a voltage is seen across C1 and L2 in parallel. C1 will charge and begin to discharge through L2. This will change the voltage difference across C 1 , thus changing the potential at the base. A change $180^{\circ}$ out of phase with this will be seen in coil L1 due to amplifier action and hence fed back into the coil L2 with a further $180^{\circ}$ phase displacement. Energy would normally be lost in the coil L2 but due to the feedback via $\operatorname{Tr} 1$ and L1, oscillation is able to continue at a fairly constant amplitude.

There are two main methods of obtaining an output from this type of oscillator; normal amplifier output may be taken from the collector (point A in Fig. 30) but very small values of current only may be drawn. otherwise oscillation will cease due to lack of feedback. A more common method is to use a third winding on the transformer ( B in Fig. 30) from which slightly larger values of current may be drawn but whose presence changes the mutual inductance value of the transformer and hence the frequency output.

There are other types of LC oscillators using feedback in a similar manner to the one in Fig. 30 but there is not space to deal with them here.

RC oscillators are also of several types and again only one shall be dealt with here-the "phase-shift" oscillator.

The phase-shift oscillator is allowed to oscillate at one frequency only, which is determined by the values of capacitance and resistance used in the " phase-shift network".

Similar to the LC oscillator, a grounded emitter amplifier is used to amplify the oscillations but an RC network is used to provide feedback in place of the inductive method.

The circuit shown in Fig. 31 provides a current

Fig. 31 (right): A CR circuit giving $60^{\circ}$ phase shift.


Fig. 32 (below):

phase shift of $60^{\circ}$ between input and output, therefore three of them connected in series would give a $180^{\circ}$ phase shift.

Fig. 32 shows the diagram of a phase-shift oscillator.
$R_{3}, R_{4}, R_{6}$ and $C 4$ provide the base-emitter biasing. $\mathbf{R}_{3}$ is also a part of the phase-shift network. Obviously there are several losses in the CR network and to overcome these the amplifier stage should have a gain of at least 29 times.

The output is taken from the collector of the transistor.

Part 5 follows next month

## PHOTOCONDUCTORS

## -continued from page 848

0.6 V and the lamp is off so that the volume control is up at maximum output. Now S1 is switched to VR1 the "decay" control: C1 slowly charges up through VR1. the voltage across the lamp rises and the resistance of the photoconductor falls so that the volume control output decreases, reaching its minimum when C 1 is fully charged; the volume control is now off.

Now S1 is switched back to VR2: C1 slowly discharges through VR2, the lamp voltage falls etc.- the whole cycle being repeated in reverse until the initial state with C 1 completely discharged and the volume control at maximum is reached.

With the values of C1, VR1 and VR2 given, the attack and decay times can be varied from several seconds. down to practically instantaneous. If Jonger times are required Cl may be increased to $1,000 \mu \mathrm{~F}$ or more.

In this article the writer has described only a few of the possible applications of photoconductive cells. They are a comparatively recent
device and many manufacturers in Great Britain and the U.S.A. are working on improved forms and new applications. Their use to replace relays in switching circuits has perhaps the greatest potential at present: a neon lamp or electroluminescent panel can control several photoductors, switching them from virtually opencircuit to virtually short-circuit by means of its light output. The most important improvement to be made in these devices is a great decrease in their response time, at present over one tenth of a second. Cadmium Selenide cells can bring this down to one hundredth of a second and other compounds may bring it much lower. Other photosensitive devices of entirely different principles are also becoming available and the ultimate value of the photoconductor cannot yet be judged, but it is safe to say that it will be with us for many years, assuming greater importance as improved forms become available.

Acknowledgement is made to Ericcson Telephones Ltd. for permission to use their published data on the K42.

The K42 is available from Service Trading Co. at 8 s .6 d . It is not available direct from the manufacturers in quantities less than 500.


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「YHE surprising thing about such records as these is that they were not thought of sooner. As a commercial proposition they have not been going for more than six to nine months-at the most. The guitar. on the other hand, has been the foremost instrument in the popular music field for a good ten years.

However, such a record as this certainly fills a need. For no matter how many books, booklets and advice may be read on the subject, there is nothing like coming to grips with somethong in practice for rapid learning.

Side 1 is split into two parts. The first half describes the techniques of tuning the gustar-i.e., pitch-pipes, tuning fork. etc., and gives full details on how once one striry $y$ is correctly tuned, the rest can be adjusted in unison. This section is perhaps the most important on the whole record. For as is rightly stated, the hallmark of the good guitarist is an accurately tumed instrument. which applies even more so to the beginner, because at the outset the ear too easily accepts any sounds-whether the right or wrong ones.

The second half of track 1 deals with basic chords and their formation, the common key of C being chosen. Simple accompaniment is also touched upon.

Side 2 is the more difficult to master and one gets the impression that things are pushed along a little too quickly. But the trath is that the newcomer has only to lift the pick-up from the record and start again, so that he learns at his own rate in any case. The key of Am is dealt with and an explanation of picking out on the bass strings in conjunction with chord work is given.

Part $B$ of side 2 concentrates on the right hand and the use of the plectrum, with a little more on the use of hass notes. Lastly, part C is concerned with rhythm and in addition to the electric guitar a bass guitar is brought in to illustrate the effects of various beats and times.

While it would be naive for any wolld-be guitarist to expect to be able to play like Segovia simply by hearing this record, it is a great help for a beginner to be able to make direct comparisons of his own playing with that on the record, which of course he can do. In short. a record such as this justifies its expense to the learner by its help in the all-imporant initial. formative. stage of playing, and even on that score alone would stand recommended.
"Learn To Play The Guitar" by Johnny Bennett. retails at $25 /$, and comes complete with a sheet of simplified chord forms. Recorded Tuition Ltd.., 174/176 Marbank Road, South Woodford. London, E.I8.

## SINCLAIR X-10—TRADE NEWS, DECEMBER P.W. (P.786)

WE have been asked to make clear that T.S.L. are the sole distributors for this amplifier so far as the wholesale and retail trade are concerned. This company does not supply the public direct.


ACTON, BRENTFORD AND CHISWICK RADIO CLUB Hon. Sec.: W. G. Dyer, G3GEH, 188 Gunnersbury Avenue, London, W. 3.

At the meeting on 8th December at Club H.Q. at 66 High Road, Chiswick, there will be a demonstration arranged by Ad. Auriema Led., of eransceivers, including the National NCX5. The meeting commences at $8 \mathrm{p} . \mathrm{m}$.
BASILDON AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: C. Robertson, Milestone Cottage, London Road, Wickford, Essex.

Peser Blair, G3LTF, who is well known for his acsivities on 2 m ., 70 cms . and 23 cms . will be giving a talk on v.h.f. $/ \mathbf{u} . h . f$. . at the Ballroom of the Bullseye, Southernhay. Town Centre, Basildon. ,The meeting will be held on Wednesday, 9th December at 8 p.m. Admittance is free and there are ample car-parking facilities. CHESTER AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: P. J. Holland, Field House, 19 Kingsley Road, Great Boughton, Chester.
On 3 rd November there was a net night on 160 m , and 2 m . The following week there was a film show when several technical films ware shown. On 17th Novamber. Mr. J. Butler, G3FNV. gave a report on the International Radio Communications Exhibition held at the Seymour Hall, London, and on 24th November there was a sale of members' surplus equipment. All meetings are held at 8 p.m. in the Y.M.C.A., Chester.
DERBY AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Littloover, Derbyshire.

On th November members held a surplus sale and a week later saw a demonstration of communications receivers. 14th November brought the Short Wave Magazine contest and on the l8th there was a technical film show. On 25th November there was an open evening with a juniors' meeting, and the following week, the second R.S.G.B. Top-Band contest.
GUILDFORD AND DISTRICT RADIO SOCIETY
Hon. Sec: D. H. Mead, G30×1, 41 Egley Road, Woking. The lecturer on 13th November was A. Birt, G3NR, who gave a talk on the Racal R.A. 17 Receiver. On the 27th P. H. Jones, Esq., gave a talk on the Decca Navigation System.
MELTON MOWBRAY AMATEUR RADIO SOCIETY Hon. Sec.: D. W. Lilley, G3FDF, 23 Melton Road, Asfordby Hill, Melton Mowbray, Leicestershire.

At the meeting on 26th November hold in the St. John Ambulance Hall, Asfordby Hill, members brought and discussed leems of gear recencly built, or that were in the course of construction.


NORTHERN HEIGMTS AMATEUR RADIO SOCIETY Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

On loth November members saw a Muliard Film Show, at the King's Hall. Bradford, and on the II th three young SWLs gave a talk on their hobby. This was followed on the 25 th by Mr. L. M. Dougherty, B.SC., F.R.A.S., who gave a talk and demonstrations on transmitter alignment.
READING AMATEUR RADIO CLUE
Hon. Sec.: R. G. Nash. G3EJA, "Peacehaven", 9 Holybrook Road, Reading, Berkshire.
The meeting hald on 28th November was concerned with the conversion and use of government surplus gear. All entries had to be in by this meeting for the Trophy Competitions held by the Club, which will be judged at the meeting to be held on lith December.
SLADE RADIO SOCIETY
Hon. Sec.: D. T. Wilson, 177 Dower Road, Four Oake, Sutton Coldfleld, Warwickshire.
On 13th November, Mr. R. Palmer (G5PP), well known for his potent signals on top band and two maters, tave a talk on "Mobile Operation". The Society's A.G.M. was held on 27 th November. SPEN VALLEY AMATEUR RADIO SOCIETY
Hon. Sec. ${ }^{2}$. Pride, 100 Ralkes Lane, Birstall, Mr. Leeds.
Members visited the Home Office Wireless Depot on 12 th November, and on 26th November, A. W. Walmsley, G3ADQ, gave a lecture on SSB.
WELLINGEOROUGH RADIO CLUE
Hon. Sec.: J. Baker, 34 Eseex Road, Rushden, Northamptonshire.

On 12th November, Mr. D. Slater gave a lecture on "Electrochemistry", The following weok, members saw a fim entitled, "Super Grid Construction", and on 26th November, D. Britton spoke on "Model Aireraft and Radio Control".
WEST KENT AMATEUR RADIO SOCIETY
Hon. Sec.: H. F. Richards, 17 Reynolds Lane, Tunbridse Wells, Kent.
Ar the meeting on 13th November, members heard an illustrated talk entitled "Componenss", given by a representative of Messrs. Erie Resistors L.td. A week later, H. Turner spoke on "Dual Standards TV Cireuiery".

There will be an Exchange and Mart on Ilth December, where members may offer their surplus gear for sale or exchange.

## ON THE SHORT WAVES

-continued from page 85!
by LU1ZC and LU8ZI around $1400 \mathrm{kc} / \mathrm{s}$. ZL1ABZ on Kermadec Island is now QRT having gone home to New Zealand so at the moment no r.f. emanating from Kermadec. This also applies to Campbell Island. The Andaman lslands are on the map with the callsign VU2NRA. Norfolk Island VK9RB and VK9DR. Christmas Island is still with us, and KG6IF on Marcus Island. Deception Island has three or four operators, and the callsign to listen for here is LU4ZI. Heard Island is out of the running at present, but plans are reported to be afoot to remedy this, the callsign will probably be VK0PK. Finally Aaland Island boasts the call OH 0 -and is a fairly easy one to hear. (This one is big enough to be shown on the map.)

In case you can't believe your ears then be assured that a W callsign is emanating from Russia. If you $\log$ W8NRB/UA then it really is W8NRB who has special permission to work/UA from Kussia until about the second week in January.

My thanks to those who pointed out that GB3LER the beacon is on $29.005 \mathrm{Mc} / \mathrm{s}$ and not $29.000 \mathrm{Mc} / \mathrm{s}$ as I claimed last month. There must be some real accurate frequency metres about amongst our readers!

## National Field Day

Congratulations to the winners of NFD. The two-station winners made 2,185 points and the single station winners 1,067 . One thing emerges from NFD which is both surprising and interesting. These are the high scores made amongst the bedlam on $7 \mathrm{Mc} / \mathrm{s}$ Considering the low power limit for NFD and the conditions usually prevailing on Forty this is really quite some achievement. The two station and single station scores respectively for $7 \mathrm{Mc} / \mathrm{s}-610$ points and 422 points.

## MEDIUM WAVE DX

Now that the MW/DX season is in full swing, "Medium Wave News" is again being published. For details drop a line, enclosing S.A.E., to K. Brownless, 7 The Avenue, Clifton, York

# 1 NOT BUILD ONE OF OUR PORTABLE TRANSISTOR RADIOS... 

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## ROAMER SEVEN Mk III

5 WAVEBAND PORTABLE OR CAR RADIO Amazing performance and specification Now with PHILCO MICRO-ALLOY R.F. TRANSISTORS Covers Medium and Long Waves. Trawler Band and stages- 7 transistors and 2 diodes Push-pull output for room flling volume from rich toned heavy duty 5 in. speaker. Air spaced ranged tuning condenser. Ferrite rod aerial for $M$ \& $L$ waves and telescopic aerial for $S$ waves. The perfect with gilt trim and shoulder and hand surt Pry battery available anywhere).

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## TRANSONA

 F\|V E Luome Light, A.F'N. at good volume; G.P. Durham - 7 stages- 5 transistore and 2 diodes
Fully tunable over Medium and Long Waves and Trawler Band. Incorpordenser, volume control, new type fine tone super dynamtc 24 in . speaker et.c. Attractive case. Size $6 \frac{3}{2} \times 4 \frac{4}{x} 1 \frac{1}{2}$ in.
With red speaker grille. (Uses 1289 battery available anywhere). Total cost of all 42/6 P. \& P. Parts Price hist and eosy build parts now only plans 2\%.
 Parts Price List and easy build plans 21 ..


## SUPER SEVEN

9 stages-7 transistors and 2 diodes
Covers Medlum and Long Waves and Trawler Band. The ideal radio for home, car, or can be fitted with carrying strap for outdoor use. Completely portable-has built-in reception Spectal cireudtincorporating 2 RF Stages push-pull output reception. Special dircuitincorporating 2 RFe Stages pushopulloutput. 3 in speaker (will drive large speaker). Size $7 \frac{1}{2} \times \frac{1}{2} \times 1 \frac{1}{2}$ in. (Uses 9 y $\begin{array}{lll}\text { Total cost of all } \\ \text { parts now only } & \mathbf{3 . 1 9 . 6} & \text { P. \& P. } \\ 3 / 6\end{array}$ parts now only 316 build plans 21 -.

All components used in our receivers may be purchased separately if desired. Parts price lists and easy build plans supplied free with sets of parts or available separately at prices stated. Overseas post 101\%.

... amazed at volume and dermann. has really come up to my expectations.

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Our latest completely portable transistor radro covering medium and long waves. Incorporates pre-tagged circuir board, 3in. heavy duty speaker, top grade transistors, volume control, tuning condenser, wave change slide switch, senslive Gin. Ferite Wonderful reception of B.B.C. Home and Lieht. Ros and many Continental stations, Handsome leatlier-lonk pencke size case. only bi $x$ 3i $x$ ifin. approx. whin filt speaker Ports Price List and Total cost of all \&3.9.6 P. \& P. easy build plons $2^{\prime}$ a parts now oriy $=3.3 .0$ 3\%


## POCKET FIVE

- 7 stages- 5 transistors and $\lambda$ diodes Covers Medium and Long feature usually found in only the most expensive radios. On test Home, LJght, Luxembourg and many Continental stations were received lond and clear. Designed round supersensitive Ferrite Rod Aerial and
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Joobas's Villy 12 Ghs.
"1rijaonr's
\&6.19.6
Carr. \& Ins. $7 / 6$ DIRICE


## USEFUL H.T. BATTERIES

SIR,-I have a number of h.t. batteries which I would be willing to give free of charge to readers of Practical Wireless.

Voltage is 138 V with taps at 67.5 V and 73.5 V . The size is $10 \mathrm{in} . \times 6 \frac{3}{3} \mathrm{in}$. $\times 2 \frac{1}{2} \mathrm{in}$. and the weight is 81 b . They were made in 1962 for U.S. Forces and have now been rejected for time limit on expected life. In fact they will give hours of running time.

As 1 have over 100 i will genainely be glad to let people have them. If sent by post I should need 4 s . per battery. - H. Humplirits (The Old Vicarage, Gazeley, Newmarkct, Suffolk).

## NATIONAL RADIO CLUB FOR BOYS

SR,-I was rather dinappointed to lind that there is no mational radio clob for hoys and I feel that many of the young readers of Praciocal Wireless may like to start such a club.

I fully realise the many difficulties that are involved but I would like readers under the age of 16 who are interested in starting such a clab to write to me expressing their views on the matter. - M. Overbury (9 Jerome Drive, St Albans, Hertfordshire).

## IMPROVED RECEPTION

SSIR,-Recently I was experimenting with a piece of ferrite rod to improve the reception on a domestic portable receiver. I tirst obtained a rod of ferrite about $3 \frac{1}{2} \mathrm{in}$. Jong and wound as many turns of plastic-covered copper wire on it as possible, keeping the turns in place with adhesive tape. Fixing one end to a good acrial and the other to a good earth. it was only necessary to place the wire-covered rod on or near the radio receiver to effect an amazing increase in volume. -R. A. Crane (Great Yarmouth, Norfolk).

## A READER'S THANKS

SIR,-As a result of a request through your columns a reader has sent me the circuit diagram of the Ekco car radio CR/61A.

This gentleman did not send his address--the postmark on the envelope was Sideup-and as 1 am unable to remburse him for his trouble may I thank him through your columns?

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative detaila for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELE. PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iil of the cover.
The Editor does not necessarily ogree with the opinions expressed by his correspondents.

I had quite given up hope of ever getting the circuit of the set and would like to say how grateful I am to him.-P. Hearne (Gossops Green, Crawley).

## CAROLINE AGAIN

SIR.-I would like to make the following points concerning " Radio Caroline" and her sister ships. Firstly, in some newspapers there can be found a Caroline "Radio Times"; secondly, a certain watch firm has agreed to supply watches as prizes in one of their competitions and thirdly, there are several land addresses which are read out over the air to which correspondence nay be sent.

Surely the people arranging such facilities are all assisting the ships and are therefore breaking the law. Since the Postmaster has done nothing about it does this mean that he is going to compete with them as Mr. D. Barrington suggests?-M. Ballance (Oxford).

## BROKEN COIL CORES

SIR.-Recently I was faced with the problem of removing a cracked iron dust core from a coil former, and I successfully adopted the following procedure.

Firstly, a small hole was drilled as deep as possible in the corc. A thin metal rod was then obtained and its end smeared with metal adhesive (Loy is a commercially available example). This rod was then inserted in the hole in the core and left there until the adhesive hardened. The broken core was then removed by rotation of the rod.-A. J. Mulley (Preston. Lancashire).

## HIGH SENSITIVITY BRIDGE

SIR.-My congratulations to Mr. M. A. Harris, contributor to your Practical Wireless periodical dated December, 1961, and January, 1962, for his clear and straightforward circuit. I have constructed the unit and found it most accurate.

Additional accuracy of reading, however, not envisaged by Mr. Harris, may be obtained by the adoption of a slow-motion cursor traversing a circilar protractor. The latter was fixed behind the ealendated scate and orientated to cormespond
to the maximum swing " $\theta$ " of the potentiometer. Accurate interpretation may be then undertaken using the formulae:

$$
R=\frac{S \emptyset}{\theta-\emptyset} \quad \text { and } C=\frac{S(\theta-\emptyset)}{\emptyset}
$$

when $R=$ test resistance, $S=$ standard $R$ or $C$, $C=$ capacitance, $\theta=$ total swing of potentiometer and $\theta=$ swing, degrees.

As Mr. Harris implies, the basic accuracy is limited by the standards obtainable, but these may be replaced with those of greater accuracy as they a ppear, on the market.

Precision $1 \mu \mathrm{~F}$ capacitors $0.1 \%-0.3 \%$ accuracy at $20^{\circ} \mathrm{C}$ are now available at G. W. Smith, Lisle Street, London. W.1.-G. W. Nixon (Epsom. Surrey).

## ELECTRONIC WALLHAPE:..

SIR,-I am looking for a wallpaper pattern with an electronic theme for my "shack/bedroom". Please can any of your readers help me.-C. P. Finn ("South Dene", South Kirkley, Pontefract, Yorkshire).

REQUESTS FOR INFORMATION ARE INSERTED IN THIS COLUMN ON THE UNDERSTANDING THAT READERS USING THE SERVICE UNDERTAKE TO REPLY TO ALL OFFERS RECEIVED AND TO RETURN ALL DATA NOT REQUIRED. BECAUSE OFTHELARGE NUMBER OF REQUESTS RECEIVED, ILLEGIBLE WRITING WILL AUTOMATICALLY DISQUALIFY LETTERS FROM PUBLICATION. FOR THE SAMEREASON, WE CANNOT GIVE SPACE FOR REQUESTS FOR PAST isSUES OF "PRACTICAL WIRELESS."

## Sir-l would be grateful if any reader could sell or

loan me . . .
circuit diagram and information on a.m. recejver unit 71 v.h. $\mathrm{Ci}^{\text {i }}$ It has a three push-bution system, with several EF50 and EF39 valves,-P. LAPwood, 16 Cheviot Drive, Melbourne Farm Estate, Chelmsford. Essex.
Victoria Sireopy of QSI for August 1940.-G. T. Dowson, 39 Victoria Street, Scarborough.
ST450. -H . . J. Hudsson, 1 Park for Stella tape recorder, Model ST450.-J. J. Hudson, 1 Park Terrace, Barnard Castle. Co. Durbam.
C.R. 100 . the service sheets, manual or any useful data on the London, N.W. 3 .
. service sheet, circuit diagram or any other information on the Perth "Clarissa" Mk. 1 Tape Recorder.-T. G. Wigmore, 73 Robertson Way, Malpas, Newport, Monmouthshire.
$\therefore$ an instruction manual for the R107 and any details on this receiver.-N. SUDRON, 1 Aiskew Grove. Fairfield, Stockton-on-Tees, Co. Durham.
.. the operating manual, circuit diagram or any usefui data on the Marconi Trans-Recelver. Type CNY2.-Donsid Macaulay, Police $\$$ ation, Cardross. Dumbartonshire, Scotland.
. any information on the No. $19 \mathrm{Sel}, \mathrm{Mk} .3$ version.K, R. Pegley, 68 Rarls Lane, Hayling Island. Hampshire.
... any information, circuil diagram, instruction manual. setting-up instructions on a Hallicralters Marine Radiophone Type HT11B.-EA1 F. Matmong, C.P.O.'s Mess. H.M.S. Osprey, Portland, Dorset.
.. information on converting the $38 \mathrm{Sel}, \mathrm{Mk} .2$, to top band operation.-S. Alderton, $2 a$ Goldings Road, Loughion. Essex.
... servicing data on "Claviolines"-all models. Would purchase or part exchange Univox servicing dath.-D. CAsserley. clo Mrs. E. Dudley, 27 George Street, Chesterion, Stoke-onTrent, Staffordshire.
$\cdots$ any intormation on working the R109A from a.c. mains.- A Corker, 3 West Crescent. Sunnyside. Nr, Rotherham Yorkstire.
circuit and any other data on the AP61357 Admiralty Type 62iH. Receiver.-H. A. Forrester, 58 Bede Avenue. Sherburn Road Estate, Durbam. 1116A. Ait expenses glady circuit for the Air Ministry Receiver Street, Greenock. Renfrewshire, Scotland.
.. the circuit and details of Wavemeter Type WII91A.L. Hall, 13 Werter Road, London, S.W. 15.
. instruction book or a circuit on the Type 3, Mk. 2 Iransceiver (i.e, circuit for transmitter, receiver and power supply).-L. O. Tully, 120 Victoria Street. Fairfield 53, Brisbane. Queensland, Australia.
Receive .. the handbook, instruction manual, etc., for the R107 Receiver.-G. E. Wesrwood, 114 Pettits Lane, Romford, Essex. R $\because$ the manual and any information on the Ex-Army Radio Set No. 18, Mk. 3T.-G. P. Mxart, 25 Lowshill Lane, Rednal, Birmingham.
No. 563 . the circuit diagram of the Marconi Radiogram, Model Norfolk.
Amplifier circuit or details of the Williamson High Power Amplifier. - "Monkroyd", Portsmouth, Todmorden, Yorkshire.
 M. J. COOPER, "The Lawns". Usk, Monmouthshire, Wales.
radiogram . the circuit and any information about the R.A.P. Middlesex.
Number $\quad$ information, instructions and circuits for Mierotimer Number 130) Built by R. K. Dundas Lid., Portsmouth.R. Sharland, 70 Hillcroli Crescent, Oxhey. Watiord. Hertfordshire.

## THE "TEN-FIVE"

In the circuit diagram, Fig. 2(a) on page 518 of the October issue, pin 1 of T2 should be taken direct to +ve line and not to the junction of C5/R3 as shown. Also in Fig. 2(c) the pole of S2B should be taken to the -ve line.

## TRANSISTOR PRE-AMP

When power is drawn from a conventional valve amplifier h.t. supply for the pre-amp, the coaxial output socket (Fig. 1) should not be connected to the + ve line, otherwise an h.t. short will occur.

## PRACTICALLY WIRELESS-continued from page 885

ordinary phillumenist, there is a diary aimed especially at you, with a wealth of listed information that often crowds the entry pages into a slim centre section. My last diary tells me how to calculate series and parallel combinations, what frequencies the radio stations of the world employ, the size of wire I must use to construct my own coils, the equivalents of long-forgotten valves, and the addresses of all
the technical institutes and societies I could have joined if : had been able to learn the above information by heart. Somewhere among the small print I should undoubtedly find a Greek alphabet, a decibel conversion table and a flurry of Abacs.
Also among my souvenirs is a so-called Radio Diary that some misguided relative gave me, knowing my hobby. Unfortunately, the compilers had concen-
trated on output rather than input, and I now have a fund of gen on the lives of the pop stars, and instead of valve curves there are photographs less useful, if more revealing. Cleavage in place of characteristics: fancy instead of fact.

Which brings us back to some of those wild speculations we began this column with - but more about them anon.

Don't Miss These Bargains Transigtor ferrite rod aerial with medium and long mave coils with circuit $7 / 8$.
Oacilustor Coil and set of 3 I.F. tranalormera Truing Condanser to suit sir-p.
Truning condenser to suit. air-spaced with trimmers. $\theta /$.
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T.C.C. of Dubilier Tubular Condensers

de nut :30 F .
. 0 mi 50 n v .
.0011 mi 1.000 v .
$.001 \mathrm{mf} 1.000 \%$.
$.002 \mathrm{mf} 1,000 \mathrm{~F}$
$.005 \mathrm{mff} 1,000 \mathrm{v}$

| .02 mf |
| :--- |
| .01 min |
| mi | $1.000 \mathrm{\nabla}$.

10/- doz. 6/- toz. Battery Charger Reotider $\quad . \quad 101$-do 5 amp. $8 / 8$.
Metal Chastis-pu Amplifer complenched for Mullard 510 Ampliner. complete with inner screening sertinns and atnre edamelled, $12 / 6$ set.
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which are in tilass B pusb-mull for hatiers eronomy. Ifeal liutle unit for baby alarin, cecond rilayer. intercom.. etc. etc. I日/B. Speaker $12 / 6$ catra.
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# Sinclair xio The only amplifier of its kind in 

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This high fidelity integrated power amplifier and preamp uses II transistors and has a transformerless output of 10 watts for feeding into a 15 ohm loudspeaker system. It requires only the addition of tone and volume controls and a 12 volt D.C. power supply to make it a complete mono high fidelity assembly of exceptional quality. Stereo is achieved by using $2 x-10$ amplifiers and ganged or separate controls. Input sensitivity is sufficient for all crystal, ceramic or magnetic pick-ups. The manual supplied with the $\mathrm{X}-10$ gives detailed instructions for connecting the controls and for using the amplifier in a wide variety of applications.

This radically new transistor amplifier (patents applied for) is the first to be marketed anywhere in the
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## Guarantee

The Sinclair $X-10$ os with everything purchased from Sinclair Radionics carpies our guarantee as shown on the fourth page of our advertising.

## Easiest of all to build

Not the least among the many important features of the $X+10$ is the elegant component layout. This together with the $X-10$ Manual and assembly instructions make building exceptionally easy. When assembled the amplifier, which measures only $6 \times 3 \times \frac{3}{2}$ in., can be placed in any convenient position with leads brought out to controls. input, output and power supply.


BLOCK DIAGRAM shows in simplified form the stages of function of this remarkable amplifier. Such design with its very much better standards of performance is made possible by use of the very latest transistors and high quality components.
 X-10 Power Supply Unit (ready built)
for A.C. Mains two $X$-10's if required.


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# 10 Watt litiegrated amplifer using pulse width modulation 

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With P.W.M. the audio signal modulates a high frequency square wave "carrier" by varying the mark-space ratio. These variations are converted to energy in the output stage. Being independent of the transfer characteristics of the output transistors, the output is an exact replica of the input signal. The improvement in the quality of reproduction from the loudspeaker is instantly apparent. Transient response is greatly improved, there is no falling off in the higher audio frequencies, no intermodulation distortion and the response curve is so flat that you could draw it with a ruler! A new type of output stage and P.W.M. plus many other refinements result in an amplifier which is compact, rugged stable, requires no heat sink-and costs so little. The $\mathrm{X}-10$ may be used with low-output pick-ups such as Decca Deram, Ortofon, etc., as well as with tape play-back heads. Used in pairs the X -10 brings new depth to stereo listening.
SINCLAIR X-10 MANUAL
Explains how the amplifier functions, how to add volume and tone controls to suit your precise requirements, and how to use the $X$ - 10 for stereo. A variety of systems is shown, none of which will add more than a few shillings to the original cost of your $X-10$. The Manual which is included with every $X-10$ is available separately for $1 \%$.
$\star$ Supply voltage- 12 volts D.C.

* Completely British Design
$\star$ Number of transistors-11
$\star$ Overall size- $6 \times 3 \times \frac{3}{4} \mathrm{in}$.
* Input sensitivity-ImV into IK. ohm.
* Total harmonic distortion-less than 0.1\%
$\star$ Output power-10 watts
$\star$ Frequency response-5-20,000 c/s $\pm 0.5 \mathrm{~dB}$
* Speaker impedance-15 ohms
* Damping factor-greater than 100
$\star$ Quiescent consumption- 75 mA


# THE SMALLEST AND MOST 

## The British designed SINCLAIR

MICRO-6

## SIX STAGE RECEIVER

NOW MORE THAN EVER IS THE TIME TO BUILD YOUR MICRO-6. With the days so short, the performance from this amazing 6-stage radio is proving sensational. Stations aimply pour in from the Continent with outstanding quality and again and again the Micro-6 is reported to be giving excellent results where other sets cannot be used at all. As the illustration shows, the set is smaller than a matchbox, yet overythins including batteries and ferrite rod aerial is contained in the tiny white, black and gold case. The Micro-6 has vernier-type tuning and is switched on by inserting the Micro-plug of the earpiece into the socket at the side. This remarkable British receiver cannot be too highly recommended both as an intriguing design to build and a most practical radio to use. It's a set you will be de lighted to build and use. IT PLAYS ANYWHERE.


* SIZE— $14 / 5 \times 13 / 10 \times 1 / 2$ in.
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BLOCK DIAGRAM OF MICRO-6

The Micro-6 uses three special Micro Alloy transistors in a new and original circuit. Two stages of R.F amplification are followed by an efficient double diode detector which drives a high-gain 3-stage A.F. amplifier. Powerlul A.G.C. applied to the firat R.F. stage ensures fade-free djstant stations tuned in.

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This amplifier makes a powerful car, portable or domestic radioused with the Micro-6 or Slimline receivers and a plus is included for connecting to these sets. With its own buils in volume control and on-off switch, the TR 750 has a full 750 milliwatt transformeriess output for 10 mV into lOK ohms and a irequency response from 30 to $20,000 \mathrm{e} / \mathrm{s} \pm 1 \mathrm{~dB}$. It will also make an efficient hi-fi record reproducer used singly or paired for stereo and there are many other uses for the TR 750 which is available for building or ready built.

All ports with instructions
come to
Ready built and tested

# EXCITING <br> SET ON <br> <br> EARTH 

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## THE MICRO-6 INCLUDES THE SMALLEST COMPONENTS EVER!


#### Abstract

We show here some of the components (apart from case, dial and earpiece) required for building the Micro-6, drawn to actual size. They include the smallest components ever to be made available to domestic set constructors. Being of the kind used in space and computer electronics, they have to be reliable. The tuning system has ingenious vernier control for easy station separation. The batteries (obtainable anywhere) are each smaller than an aspirin tablet and give upwards of 70 hours working life! The 8-page fully illustrated instruction manual shows very ciearly how to assemble the Micro-6 step by step making it easy for anyone to build.


All Darts required to build the Micro-6 incluaing tiohtweight earpiece. case and instructions come to
59/6
"Transrlsta" nylon strap for wearing the Micro-ti like a
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Build it in a single evening

SINCLAIR X-10

UNIQUE 10 WATT AMPLIFIER

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#### Abstract

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