# PRACTICAL WRRELESS <br> <br> OCTOBER 1964 

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IOTRANSISTOR DOUBLE CONVERSION RECEIVER S-Meter B.F.O. Mains Power Unit

## ADCOLA

## SOLDERING INSTRUMENTS AND EQUIPMENT



> DESIGNED FOR THE AMATEUR'S RADIO STATION

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| TAPE AMPLITLRR FOR STUDIO DECK with ready |  |  |  |
|  |  |  |  |  |  |
| and output trannformers, knoba, plans, serews etc. EF86, ECX83, EZ80, EM85 and 2 EL84. 3 wath output. Magic eye. Radio snd Mic. inputa, ext. speaker |  |  |  |
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| socket, tone and monltor controls, Can be used an an |  |  |  |
| Collaro studiódeck Very latest model, 3 bpeds, |  |  |  |
| 9 motors, 7-tnch spooly . . ................ $£ 10.18 .6$ | 44/- | 8 | 24/6 |
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| TAPE AMPLIFIER FOR STUDIO DECE a described |  |  |  |
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|  |  |  |  |  |  |
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| CASE with spesker, two tome grey $\cdots$. . . . . 55.8 .0 |  |  |  |
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| TAPE PRE-AMPLIFIERS |  |  |  |
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 DOMPLETE KIT with tope and microphone .. 229.19.6

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TAPE AMPLIFIER FOR
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HIGH QUALITY AMPLIFIER


Kit can be supplied assembled and

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A complete set of parts 4 Gins． to construct of a good avality stereo amplifier with an undistorted output total 6 watts． For A．C．mains input of 200－250 v． Sensitivity $130 \mathrm{~m}, \mathrm{v}$ ，Ganged Vol． und Tone Controls．Preset balance ontrol．Full Instructions and t＇lck－up Head 19／日 extra with above flck－up Head 19／0 extra with above
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$250-0-250 \mathrm{v}, 100 \mathrm{~mA} .5 .3 \mathrm{v} .4 \mathrm{a}, 0-5 \mathrm{c}$ $300-0-300 \mathrm{w}$ $300-0-300 \mathrm{v}, 130 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{4a}$, C．T． 6.3 V la，for Mullard Amplifier
$350-0.350 \mathrm{v} .10 \mathrm{~mA}$ ． $6.3 \mathrm{v}, 4 \mathrm{a} .0-5-6.3 \mathrm{v} .3 \mathrm{a}$
$350-0-350 \mathrm{v}, 150 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 0-5-6.3 \mathrm{v}, 3 \mathrm{a}$
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$4 / 6$
$4 / 6$
$4 / 6$
$4 / 6$
$5 / 9$
$5 / 9$
$5 / 8$
9／9
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$80 / 9$
49／9
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[^2]
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OUTLET BOXES（Suriace or flush）， $4 /-$ ea，
TWIN SCREENED DAT Yd Yd．8d． 80 or 300 ohms． Wirewound Ext．Bpeaier Control． 100 3／－． 250 e $/ 6$. WIRE－WOUND POTS． 3 WATT．Prefet Min． TV Types．All values to 10 ohma to $25 \mathrm{~K}, 3 / \mathrm{e}$ es． $30 \mathrm{~K}, 4 / \mathrm{F}$ ，（Carbon 30 K to 2 meg．， $8 / \mathrm{c}$ ）
WIRE－WOUND 4 WATTS Pots．Long spindle． Value， 50 ohms to $50 \mathrm{~K} ., 6 / 6: 100 \mathrm{~K}$ ．， $7 / 6$ ．
PEILIPS TRIMMERS． $0.10 \mathrm{pF}_{3}, 3 \cdot 30 \mathrm{pF}$ ．， $1 / \mathrm{m}_{\text {。 }}$
TRIMMERS，Ceramio． $30,30,70 \mathrm{pF} .9 \mathrm{~g}$ ．； 100 pF ． $150 \mathrm{pF} . \mathrm{I} 1 / 8 ; 250 \mathrm{pF} ., 1 / 8 ; 500 \mathrm{pF} ., 750 \mathrm{pF} . \mathrm{pig}$ ． TV etc．TRIMMER， 1000 pF ．，with knob， $2 /$ ． RESISTORS．Preferred values． 10 ohms to 10 meg．
 High Stability．$\frac{1}{2}$ ．i $1 \%$ 2／－Preferred values $10 \Omega$ to 10 meg．Ditto $5 \% 10 \Omega$ to 22 meg．， 9 d.
BRIMISTORS CZ1， $3 / 6 ; \mathrm{CZ}, 2 / 6 ; \mathrm{CZ3}, 1 / 6$ ． BRIMSTORS CZ1，3／6；CZ2，2／6；CZ3，1／6．
5 watt $\}$ WIRE－WOUND RESISTORS $\quad\left\{\begin{array}{l}2 / 3 \\ 2 / 6\end{array}\right.$ 10 Watt $\left.\begin{array}{l}15 \text { watt }\end{array}\right\} \quad 10$ ohms－ 10,000 ohms $\quad\left\{\begin{array}{l}2 /= \\ 2 / 6\end{array}\right.$ 12.5 K to 25 K 10 w ． $9 /-$
$5 /-$
$12 /-$
$7 / 6$
$6 / 6$
$5 /-$
$8 /-$
$7 /-$
$7 /-$
$11 / 6$
$12 / 6$
$8 / 6$.

## MAINS TRANGFORMER 200／250 V．A．C．

 ETANDARD，$\because 30-0-250,80 \mathrm{~mA}, 6.3$ v． 3.5 a tapped 4 v .4 a．Hectitier d．J v． 1 a．，I v ． $20 / 8$ Ma．or 4 ． 2 a．，22／6，ditto， $300-0-350$ 29／8 MIDGET RE 200 V． 20 IDA， 8.8 ． 1 A ． $10 / 6$ SMALL， $250-0250,45 \mathrm{~mA}, 16.3$ v．2 a．．． $17 / 6$ 8TD．250－0－250，$\$ 5 \mathrm{~mA}, 6.3$ v． 3.5 ¿．$\quad \cdots \quad 17 / 6$ HEATER TRANS．，ti．3 v． $1 \frac{1}{6}$ \＆．．．．$\quad . \quad 7 / 6$ Ditto，tapped 1．4．2．3，4，5．6．3 Ditto，sec． 6.3 F .4 gmp ． GENERAL PURPOSE LOW VOLTAG\＆ $10 / 6$ $3,4,5,6,8,9,10,12,15,18,24,30 \mathrm{Y}$ AUTO TRANSFORMERS， 150 w ． $0,116,{ }^{2} 200,{ }^{2} 230,{ }^{2} 50$ v． $500 \mathrm{w} .{ }^{2}$ 22／6． MAINS POWER PACK8．Heady built with Transformers，Rectifiers，Condensers，providing H．T．and L．T．outputs． 200 v． 20 ma．D．C． 6.3 v． 1 a．A．C．．．25／6

INTERVALVE TRANSFORMERS． $3: 1$ or $5: 1,9 /-$ O．P．TRANSFORMERS．Heavy Duty．\＄／6．Multi－ ratio，7／6．Multiratio heavy duty push－puli， 10 w 10 w ．O．P．matehing trans．， $3, \mathrm{~T}_{,} 15 \Omega, 12 / 8$ L．F．CHOKES． $15 / 10 \mathrm{H} .60 / 65 \mathrm{~mA} .5 / \% 10 \mathrm{H} .85 \mathrm{~mA}$ ． L．F．CE， 10 H ． 150 uIA． $14 /-$ ．

## C．R．T．BOOSTER TRANSFORMERS

 for heater cathode short circuit or tubes with failing emission．Full instructions supplied．mains input． Type A optional $25 \%$ and $50 \%$ hoost Zv．or fv．or $6.3 v$ or $10.8 v$ or 12.6 y.State Volitage required．PRICE $10 / 6$ ．

TINNED COPPER WIRE 16 to 22 gwg．$\frac{1}{2} \mathrm{lb} ., 3 / 6$ ． ENAMEL COPPER WIRE $16-22$ ．2／9： $24-30,8 / 6$ ；
 2,6 or $12 \nabla_{0}, 1 \neq 8 m p, 8 / 9 ; 2 \mathrm{a}_{0} 11 / 8 ; 4 \mathrm{~s}, 17 / 6$ ． CHARGER TRANSFORMERS．T＇apped input 200 ， 250 v．for charging at 2,6 or 12 $\nabla ., 1 \neq$ amps．， $16 / 6$ ； 4 AMP CAR BATTERY CHARGER with Bm－
meter，Leads．Fuse Case，etc．，for 6 v ．or 12 v ．， $58 / 6$.
BOOKS list S．A．E．
Boys＊Book of（rystal Sets．
2／6
Hieh widelity Speaker Enclosure $5 / 6$
High Fidelity Sueaker Gilciosure $5 / 6$
TV Fault Finding
Mullard Amplifier Manual．
Radio Valve finide，Books 1．2， 3

| 4 or 5 |  |
| :--- | :--- |
| Practleal ifadio Inslife Ouit | 0ach |

5／－each
Master Colour Code Chart
Trakgistor Controlled Models

## 4 TRANSISTOR PUSH－PULL

$\mathrm{Size}_{\mathrm{f}}^{\mathrm{sin}}$ ．AUDIO AMPLIFIER
$A$ ready built miniature pugh $\cdot$ puli amplitier with Driver and output transformers， 4 transistors． deal for use with record players，intercoms．， BABY ALARM末，etc，Complete with full Price $47 / 6_{9 v .}$ instructions and circuit． $2 / 3$ ．2fin．Speaker $15 /-$

## 1964 RADIOGRAM CHASSIS



THREE WAVEBANDS S．W． $16 \mathrm{~m} .-50 \mathrm{~m}$.
M．W． $200 \mathrm{~m} .-5 \tilde{0} 0 \mathrm{~m}$.

PIVE VALVE Lat＇EST MULLARD H． 00 ECH81．EF89，EBCR1，

A．C．200／250 $\quad$ ．Short－Medium Long／Gram． Ferrite Aerial A．C．V． 3 ohm output of wate Tepe Sockets．（ilass diai，borizontal wordiug size 13 in ．$x 7 \mathrm{in}$ ．Aligned and callibrated，isolatied Chassls size likin．x 7in，high x ylin．deep． 29．15．6 Carr．\＆Ins．4／6．


8 in ．JUNIOR SPECIAL 8 w ．
5821
－20．000 c．p．s．
12in．STALWART HEAVY DUTY 16w． 5 gnt $45-13,000$ eps． 3 or 15 ohm poice coils．Unlimited Applioations．Response 45 to 13,000 epm magnet 12，000 lines．it uality unbeatable．

12in．STANDARD HEAVY DUTY 20w．${ }^{2}$ gns． Hore powerlu！magnet 14,000 Jinen epecial uag－ pension．40－14．500 opl．Recommended where－ over a high atandard of reproduction is dasired
12in．BASS HEAVY DUTY 25 m ．
12 gna．
ew ormer with msgnetic demping 25－16，000 cps Ideal lor all electric guitara．

15in．AUDITORIUM MODEL 35w． 18 gni ． Improved magnet alcomaz with heavy plated 0．000 ops solud heat prooted Perolin Cout Former．Ideal for all Eleotrio Guitara．

LOUDSPEAKERS P．K． 8 OHM．21，3，4，5in． x 4 iu．． $15 / 6 ; 6 / i n$ ．Rola， $16 / 6 ; 8 \mathrm{in}$ ．Plessey， $17 / 6$ ； I Gin．， $8 \times$ Bin．， $21 /-$ ； $10 \times 13 \mathrm{n} ., 22 / 6 ; 10 \mathrm{in}$ ．Rola 30／－； 12 in K A．30／－；EM1，Louble Cone Ceramic nagnet $10 \mathrm{~m} 13 \times 8 i n, 45 / \mathrm{F}$ ．Horn Tweeter，29／6． TEATORLAN HF1012．10in． 3 to 15 ohun 10 w．， 92／－；Bin．HFS1\％，76／－；Crossover CX3000，88／＊： 6tin．，18／6；8in．19／6；10in．，29／6；1火in．，60／－． TWIN GANG TUNING CONDENSERS． 365 pF
 with triumers， $9 /-$ ；inidget，7／6；with trimmers， $9 /-$ 500 pF glow motion tuting standard， $9 /$ ．Transistor gang $208+176 \mathrm{pF}$ with trimmers，10／6．SmaLL． 3 gang $500 \mathrm{pF}, 17 /$ ，8INGLE 365 pF ，7／6．SINGLE $10 \mathrm{pF}, 25 \mathrm{pF}, 50 \mathrm{pF}, 75 \mathrm{pF}, 100 \mathrm{pF}, 150 \mathrm{pF}, \mathrm{\delta} / 8$. solid dielect ric $100,300,500 \mathrm{pF}$ ． $3 / 6$ ．
CONDENSERS．New stock． 0.001 mid 7 kV ． T．C．C．， $5 / 6 ;$ Ditto， 20 kV ．， $9 / 6 ; 0.1$ mid．， $7 \mathrm{kV} ., 9 / 6$ ； Tubular 500 ₹． 0.001 to 0.05 mid．， $8 d$ ； $0.1 .1 /-$ $0.25,1 / 6 ; 0.5 / 350 \mathrm{v}$ ．， $1 / 9 ; 0.1 / 350 \mathrm{v} ., 9 \mathrm{c} . ; 0.01 / 2,000 \mathrm{v}$ ． $0.1 / 1,000$ v．， $1 / 9 ; 0.1$ mfd． 2,000 volte， $8 / 6$
CERAMIC CONDS． 500 V． 1 pF to 0.01 mfd ．， $0 d$ ． IIVER MICA CONDENSERA， $10 \% 5 \mathrm{pF}^{+}$to $500 \mathrm{pH}^{2}$ Od： 600 pF to $3,000 \mathrm{pF} .1 \quad 1 /$ ．Close tolerance $+1 \mathrm{pF}) 2.2 \mathrm{pF}$ to $47 \mathrm{pF}, 1 \%$ ．Ditto $1 \%$ to 50 pF to $815 \mathrm{pF}, 1 /-1.000 \mathrm{pF}$ to $\delta, 000 \mathrm{pF}, 1 / 9$.

## FERGUSON QUALITY AMPLIFIER 4 watts

Bize 6t x $5 \times 4 i n$ ．Mains Trangiormer， 200 f 250 V ．Volume and tone controls，Sengitivity $200 \mathrm{~m} . \mathrm{v}$ ．Response 25 to $20,000 \mathrm{cps}$ ．Price $49 / 6$. or 2 unite ntatched for Stereo，89／6．

WAVECHANGE SWITCHES
8 p． 4 －way 2 wafer long spindle
2 p． 2 －way or 2 o． 6 －way lons spindie $\quad . \quad 8 / 8$ 2 p．2－way or 2 p． 6 －way long apindle $\quad .8 / 6$ 4 p． 2 －way or 4 p． 3 －way long spindle $8 / 6$
$3 / 6$ Wavechange＂MAKITS＂．Wafers＂avail－ able： 1 p． 12 way． 2 p． 6 way． 3 p． 4 way． 4 able： 1 p． 12 way， 2 p． 6 way． 3 p． 4 way． ${ }_{2}^{4}$ p． 3 way． 6 p． 2 way， 1 wafer switch． $12 / 6: 3$ wafer switch， $16 / 6$ ： additional wafers up to 12 ．3／6 each extra Valveholders．EA50，6d．B12A．CRT，1／3 Engl．and Amer．4， 5 and 7 pin， $1 /=$ B8A．B8G，B9A． 9 ：Ceramic EFSO，B7G，B9A， int．oct．$/ /=$ B7G．B9A cans $1 /=$ each．Valve
plugs B7G．B9A．Int．octal．，2／3．

> HIGII GAIN TV PRE－AMPLIFLERS B．B．C．Channel 1 to 5．Gain 18dB． ECC84 valve．Kit price $29 / 6$ or $49 / 6$ with power pack，Details 6d．（PCCB4 valve if preferred）．Coils only $9 / 6$ ． ISAND III I．T．A．－Same prices． Tunable channels 7 to 13 ．Gain 17 dB Circuit and colls only．9／6．Chassis 4／9．

Post 1／－（unless otherwise stated）
C．O．D．2／－extra．


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Double Play Tin．reel，：2，4ntit．42／－Spare Пйи．recl， 1,2 애t． $25 /-$

Plastic
 Reels
 $\begin{array}{ll}3 \mathrm{in.} & 1 / 6 \\ 4 \mathrm{in.} & 2 /-\end{array}$ Standard $7 \mathrm{in}, \mathrm{rac} . \mathrm{A}, 2001 \mathrm{t} .17 / 6$ $5 \mathrm{im} .2 /$
$61 \mathrm{in} .2 /=$ 7in．2／6 ＂INANINILICP＂，Tapu Sulicer $5 /-$
Leader tape $4 / 6 ;$ Splicing tape $3 /-$ CKYKTAL sET BOOALE $1 /$
CRYSTAL DIODE G．E．C．2／－，GEX34，3／－，OA81，3／－ HIGH RES．PHONES， 4 ，（U01 ohllt，15／－， 2,000 ohms 12／6．MOVING COIL PHONES， 100 ohme， $10 /-$ SWITCH CLEANER．Flula squirt spout， $4 / 6$ tin


#### Abstract

＂6＋1＂TR．ANSiNTOR H．JIDO First class components to make a 6 transistor 2 waveband supernet chassis． parts including BVA transistors，ferrite aerial．with car ueridl coil．printed circuit，ginin．x 2 inin．but ExCLUDING Speaker and cabinet． Speakers． 35 ohms． $6 \times 4$ in． 21 £4．5．0 5in．．1\％／6：3！in．．15／6．


BULGIN PLUGS AND SOCKETS
 JACKS．Kizglish uphn wirautn，2／B．Closed circuat， 4／3，Grundig ty ke，3－pin，1／3．4irmulig lead jack， $3 / 6$ ． JACK PLUGS．tinglish，3／－：Noreened，4／－；tirundig 3－pin，3／6，Phowo Phess．1／－；Shekets．6d，
 11.314 ．Formers， 5937 or $x$ cans TVL or $2, \% i u$. Eq． SLOW MOTFON DRIVES．6：1，4／3．30：1，10／6．
 ANTEX SUB－MIN IRON， 15 w ． 6 ，spares in stock．


 RM4，RMS．14A100，14A116，10／－each．FC3I RMA，RMS．14A100，14A16，10／－eacin．Fieri， $200 \mathrm{~V} 450 \mathrm{~mA} .10 /-: 250 \mathrm{~V}$ 150mA， $5 / 6$.
 Priar 1o／6，ready made with valve $1 \$ 5$. MOKCH＇NIZF $2!\times 4!x 1 i n$ ．One resistor to change，full instructions supplied
Battery $8 / 6$ extra．
Details Free．
Colls Wearite＂p＂＇Type，4／－each．
Wminor Midget＂$Q$＂type．adj．dust core， trom $4 /$－each．All ranges．List S．A．E
Rtwhnco bisis．s．IJ．and Med．T．R．F． with reaction．4／6．Med．wave D．H．． $3 / 6$ Frrite Arrialu，M．，8／9：M．and L．．． $12 / 6$ ． Ommor Ferritu ikod irrialm．L．and M ． for transistor circuits， $10 /$ each．
 \｜F．Cokes，2／6．Onmor（WCI，6／9．
I．If，r ctils，A／HF，7／－pair：HAX 3／6．
 Neoside＇Trimming Tool， $1 / 9$.


Blank Numirifum thatils， 18 S．W．g． 4 sides，riveted corners，lattice fixing holes． 2 inn．sides． $7 \times 41 n ., 4 / 9: 9 \times 7 \mathrm{~m}$. 5／9： $11 \times 7 \mathrm{in} .6 / 9: 13 \times 91 \mathrm{n} ., 8 / 6 ; 14 \times 11 \mathrm{n}$ 10／6： 15 x 14in．， $12 / 6$.
Almminium Pantlo， 18 s．w．g．． $12 \times 12 \mathrm{in}$. 4／6： $14 \times 91 n . .4 /=; 12 \times 8$ in．．$_{3} /-; 10 \times 71 n .$. 2／3： $8 \times 6$ in．， $2 /-6 \times 4$ in．， $1 / 6$ ．

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Collaro stiodia eratik ellolis， 0

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MAINS DROPPERS．Midget aljumtatle widers
 LINE CORD，$s-w a y 100$ ohut $1 t ., 1 /-11$ ． MIKE TRANSFORMERS．5U－1， $3 / 9$. P．V．C．Covered Wire，kingle or sirambed，2d．yit Sleeving． 1 ur： 2 mm．．2d．： 4 thm．．3d．：t min．，5d．

B．T．H．TAPE MOTORS． 115 v．A．C．． $12 / 6$ ea． or pair for $230 \mathrm{v.}$. （in series） $12 / 6$ ．
SPEAKER－FRET， ：old Whroou of lireen deth
 5in．wide from $10 /$－it． 2 fin．wide irath $5 /-\mathrm{ft}$



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 All leading mahem，volumbe contzots，


## WEYRAD P50

（O）ILA AND）IURI VNIFIRMIEIKS FOMR
 Long and Medium terial－RA2W 6in．rod 208 pF tuning，with ear aerial coil 12／6 Osc．Coil P50／1AC 176 pF tuning $5 / 4$ 1st and 2 nd I．F，P50／2CC $470 \mathrm{k} / \mathrm{es} 5 / 4 \mathrm{each}$ 3rd I．F．P50／3CC 6／－，Spare Cores 61. Driver Transtormer－LFDT4 $9 / 6$ Wavechange Slide Switch d．p．d．t． $3 / 6$ Printed Circuit－PCA1．Size $21 \times 8$ x $1 n$ ． Ready drilled and printed
35 ohme Sontrol． 5 －DI＇ $15 / 6$ ： 5 in ． $4 / 6$ 35 ohm speakurs， 3 im $15 / 6: 5 i n, 176$ ： $6 x 41 n . .21 /-$
J．B．Tuning Gang with trimmers $10 / 8$ Constructor＇s Booklet Constructor＇s Booklet
3 ohm O．P．Trans．O．P．T． 10／6
 UC71 6／－，QC72 \％／6．OCA1D \％／6．（1C81 N／6． OC44 8／－．OC15 8／－，OC171 10／6．AF117． $9 / 6$.
Sull Miniature＂ondlensire． $0.1 \mathrm{mF} \mathrm{F}^{2}$ $30 \mathrm{~V} . .1 / 3,1,2,4,5,8,16,25,30,50,11 \mathrm{~mm} \mathrm{md}$ 15 volt． $2 / 6$ ca．Transistor Holders，1／3．
 Med．wave kit， 2 transistors， 2 diodes． earphone，icrrite aerial．Cablnet ＂r＇ransisiur $\overline{4}$（hammel Nixer with 4 separate input／output controls $59 / 6$.

## ＂THE POWER MITE＂45／－

 Ratios．Same size as ⺊．P． 9 （200／250V． Miniature L＇1＇3 model

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 ＂Performs aqreeably woll＂（The Gramophone

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 Juthate deala as below
AUTOCHANGE KITS COMPLETE（ 23 above） B．S．K．Monarch ．．．．211．10．0 P．Y．चith Garrard Autoslim 11.10 .0 P． SINGLE PLAYER KITS．Complete tas above
 OR SEPARATELY 43．8．6．1．P． 34 Cabine with our choice iz．Q．6．P．P． 3 is
cut out to your Amplitier with \％ 4 In

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Complete with ACOS LP－78 Turnover Head．got－ Replacement sapphire styli $5 /-$ ．tiamond $15 /-$ Mono GP59 Xtals $15 /$－：Stereo Ronnette 301 －
BARGAIN SINGLE PLAYER KIT 20G250 v．A．C

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With 2－stage Amplifter： 3 watt： 2 va；wes，UCLS 2 UY85，High－flux 5 in speaker；4－speed E．M．I． for LP／STD．Records．7in．，10in．．12in．．，Cut out Mounting Boards $12 \times \times 9$ ：in．

ARDENTE TRANSISTOR TRANSFORMERS
D3035， 7.3 CT；I Push－pull to 3 ohms output D3034 1．74：1，C．T．Push－puli Driver D3058，11．5：1 Output to 3 ohms，eto． D3058，11．5：1 Output to Dims ，eto．
 ARDENTE TRANSISTOR VOLUME CONTROLS VCI545， 5 K with switch dia．． 0 in．
SUB－Min．EARPIECE Xtal or marnetis SUB－MIN．JACK AND PLUG



 mammerals ami tine point＂rs．zerro adifumbnont serew on iront mi metor． | 1 min | $\cdots$ | $27 / 6$ | 5011 | $\cdots$ | $39 / 6$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| mII | - | $2 / 6$ | $.00 / \mathrm{L} .1$ | $\cdots$ | $32 / 6$ |


 －1000 V．A．C．A）．C．onnis 0－100t．etc．． $49 / 6$.

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Migh output．Size 11m．dia．x in．


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## Practical Wireless


Vol. XL No. 692 OCTOBER, 1964


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## Contents



## Good Response

T10 trim, or not to trim? That is the question that must have been asked a million times in radio shack or workshop. or the corner of the kitchen table.
A lot of nonsense has been talked about the unforgiveable sin of "iwiddling the trimmers". The imputation is that the average radio enthusiast is quite incapable of making tuning adjustments. Such critics need an answer.

It would be foolish to ignore the fact that in the course of every year, many receivers find their way to the professional's service bench. hopelessly out of alignment due to inexpert and haphazard trimmer and core twiddling. Or that many gloony hours are spent annually by home constructors in futile attempts to peak and calibrate newly constructed sets.

However, those that sulfer in this way are usually raw novices, those with no contact with other amateurs, or those who with iron resolve refuse to put themselves out to learn a few elementary facts.

The majority of amateurs are unquestionably more competent and intelligent, and even if they do not have access to the proper test instruments they are able, under certain circumstances, to make adjustments to tune circuits without dire consequences.

When a receiver is known to be aligned-when it has been working, but a fault has developed-there is no objection to an exploratory movenent of iron-dust cores and trimmers, provided a few obvious basic rules are observed.

First, cores or trimmers should be moved one at a time. If no improvement is noted, they should be returned to the original position before proceeding to the next. Second, a visual indication of output is very much better than trusting to the ear; more delicate adjustment is possible.

Third, where a set is completely out ol alignment, the correct sequence of adjustments should be followed-and the possibility of an alternative fault should be investigated before re-tuning. A receiver that is known to be out of alignment, such as a newly-built model. should be aligned "according to the book".

Now the critics must be well aware that most readers of magazines such as Practical. Wireless are quite conversant with the above homespun rules. Why, then, their spleen?

It seems to be based on one main bad fault-the chewed-up slug or the trimmer with the crached insulating washer. This is generally the result of using makeshift tools. Very seldom is it caused by the true enthusiast.

The only real restriction on trimming should be the neces: sity for test equipment when aligning those circuits that must be tuned to an exact response curve. A smail movement of any one core of a TV or an f.m. receiver i.f. strip may seem to make little difference. but its eflect on the overall response could be deceptively damaging.

We are sure that regular readers will know not only how but when to adjust a tuned circuit. And we hope that the trimming tools presented with this issue may prevent a few more slugs becoming chewed uo or cracked!

Our next issue dated November will be published on October 7th
 when radio amateurs in different countries achieved communication via the moon. Pairs of amateur stations have been using signal bounce off the moon to relay radio transmissions in the 2 m and 70 cm ham bands.

These experiments were undertaken with the new giant 300 m radio telescope in Puerto Rico, soon after its completion. (This installation is from time to time being made available for such anlateur experiments.) Several contacts have already been logged using this somewhat spectacular amateur set-up. the first being on 13th June, 1964. when KP4BPZ (Puerto Rico). using the giant telescope aimed at the moon as receiver antenna. received signals from a group of Swiss and German amateurs in Hedingen. near Zurich, and. some time later, signals beamed at the noon by the British station G3LTF (Peter Blair) running 80 W into a parabolic aerial.

A further successful contact with Puerto Rico via the moon was established by the German station DJ3EN (Hinterzarten/ Black Forest) on June 14th. On this occasion, DJ3EN ran 500 W on the 2 m band into a conventional tenelement Yagi aimed directly at the moon. By the time his signals had been received in Puerto Rico. they had travelled a distance of roughly half a million miles.

## ELEGTRONIC GOMPONENTS CONFERENCE

A ONE-WEEK conference on components and materials used in electronic engineering will be held at the Institution of Electrical Engineres in London from 17th to 21st May next year. concurrent with the 1965 Radio and Electronic Component Show at Olympia.

Subjects to be discussed are recent developments in active and passive components, including integrated circuits, and in the materials of which they are made.
"Resistors", "dielectrics". "capacitors"." microwave ferrites". "electro-mechanical devices", "semi-conductor devices" are a few of the categories for which contributions have been invited for inclusion in the programme.

The conference is being organised jointly by the I.E.E. Electronics Division, the Institution of Electronics and Radio Engineers and the United Kingdom and Eire Section of the Institute of Electrical and Electronics Engineers.

## 450 Motorcycle Transceivers Ordered

FOLLOWING their successful introduction last year. an order for 450 Ultra 4A5 motorcycle transceiver sets for use by British Police Forces has been received by the Telecommunications Division of Ultra Electronics Limited from the Home Office.

The 4A5 set provides two-way communication on four channels with a standard spacing of $25 \mathrm{kc} / \mathrm{s}$. The single superhet receiver design is fully transistorised and uses a $10.7 \mathrm{Mc} / \mathrm{s}$ i.f. crystal filter. The transmitter, now further transistorised. incorporates quick-heating valves to eliminate standby battery drain. It operates on 6 or 12 V supplies.

Ultra have also received an initial order for 26 of their f.m. 4B6 Packsets for use by the Metropolitan Police.

## Computer for Scottish University

A LARGE general purpose analogue computer, type 247, costing approximately $£ 19.000$, has been ordered by the University of Strathclyde, Glasgow, from the Solartron Electronic Group Ltd.. of Farnborough. Hampshire.

This is the fourth 247 computer to be ordered this year, the others having already been installed at the University of Sheffield and two technical colleges. The Glasgow computer will be installed in the Electrical Engineering Department and will be used for the investigation of automatic control systems and general research.

ARECENT innovation from Mullard Lid.. which could have the probable effect of standardising more than ever before the design of transistor receivers. is a range of transistor eircuit modules for a.m. radios being made available to manufacturers, having the obvious advantages of faster. easier production and greater freedom in cabinet styling.

With these devices a manufaeturer will be able to build a receiver around two modulesone constituting the r.f./i.f. section. the other the complete atudio amplifier -- instead of assembling individual components.

The r.f./i.f. module, type LP156, is a fully-screened i.f. amplifier and mixer stage (see photograph on this pagel covering the short. mediam and long wavebands using external oscillator coils. (Other versions are available for medium and long wavebands only, using internal oscillator coils, but all versions measure the same: 2.44 in . $x$ 1.19in. x 0.64in.) The mixer stage uses an AF115 transistor and the two stages of i.f. amplification use AF117's. followed by a diode detector (O.A90).

The whole module is designed to operate from a $7 \cdot 6 \mathrm{~V}$ suppiy line derived from the audio module.

## V.H.F. RELAY STATION IN FORFAR

 '】HE BRC"s new television and v.h.f. sound relay station for Forfar, which was brought into service earlier this year, is situated at Harecairn. near Monikie. Dundee. From here it serves an area including southern Angus, northern Fifechire and small areas of eastern Perthshire and southern Kincardineshire. with transmissions of $\mathrm{BBC}-1$ television and the three v.h.f. sound programmes.The television transmissions, are on channel 5 (vision $66.75 \mathrm{Mc} / \mathrm{s}$, sound $63.25 \mathrm{Me} / 5$ with vertical polarisation. with the Scottish Home Service on $92.7 \mathrm{Mc} / \mathrm{s}$, the Light Programme on $88 \cdot 3 \mathrm{Mc} / \mathrm{s}$ and the Third Programme/Network Three on $90 \cdot 5 \mathrm{Mc} / \mathrm{s}$, all with horizontal polarisation.

## mullard introduce circuit MODULES FOR TRANSISTOR SETS

This latter. type LP1153, is an a.f. amplifier giving an output of 500 mW into a 10 s loudspeaker. It is designed to operate from a 9 V supply and it measures 2.01 in . $x \quad 1 \cdot 27 \mathrm{in}$. x $1 \cdot 08 \mathrm{in}$.

The eircuit uses an LFK4 transistor package and comprise's a d.c.-coupled preamplifier stage and a complementary output stage. Overall d.c. fectbach of 10dB is applied to stabilize the working condition and approximately 10 dB of a.c. feedback
reducer distortion and gain spreads.

To simplify manufacture further, the r.f./if. module comes pre-aligned, so reducing the alignment procedure of the complete receiver. In addition fallt-finding by the set maker is virtually climinated since both types of module are given stringent quality control tests during manufacture. Servicing is also simplified. the replacement of a module taking a few minates only.


Mullard's new r.f./i.f. circuit module.

A

New Radio Station in British Honduras NEW h.f. radio station is to built in British Honduras for Cable and Wireles LId.. near the city of Belize. It will cost in the region of 8100.000 to huild and take about 18 months to complete.

The station will be built on a site at Pine Ridge and when finished will comprise two separate buildings, about 800 yards apart. for housing fransmitters and receivers, the transmitters being remotely controlled from the receiver building

Belize is one of the youngest branches in the worid-wide telecommunications network of Cable and Wireless Lid.. and its associated companies. Opened in Anill, 1962, it faced many difficulties as a result of the devastation caused by hurricane "Hattie". which struck Belize on October 31si. 1961.

A temporary wircless station set un in 1958 was destroyed and much of the equinment lost. An emergency station was set up while negotiations for the company to take over the external telecommunications of British Hondur continued with the Govemment.

The damage calsed by fooding during hurricane "Hattie" emphasised the vulnerability of sites in the city of Belize and it was decided that the new station would be erceted further inland on higher ground.

Four transmitters of 1 kW each, and five receivers will be installed in the station. A link between the new station and the Central Telegraph Office in Cattouse Building. Belize, will be established by a mutli-channel v.h.f. link.

# THE <br> "TEN-FIVE" 



## A 10-transistor

## double-conversion

communications receiver

\author{

- s-meter <br> - b.f.o. <br> - mains powered
}


## IBT A S. CATRPコMNTコIR GBAIEG

NOW that suitable ready-made coils are available it is possible to construct an excellent Short Wave transistorised receiver possessing a high degree of sensitivity.

The receiver to be described was built primarily to provide signals in the various Amateur bands: it requires no valves and may be run either from a standard 9 V dry battery or from the domestic mains supply at $220-240 \mathrm{~V}$ a.c.. The semi-conductor complement comprises ten transistors and five diodes, two of which are used for a.c. rectification purposes in the mains power supply section.
The receiver is not inexpensive to construct and a fair amount of work is also involved since the design is moderately complicated. Other requirements in the workshop are: A suitable signal generator, a soldering iron fitted with a pencil bit, time, patience-and a pair of strong iweezers!

## Sections of the Receiver

The block diagram of Fig. 1 shows the various sections and it will be observed that the "double
conversion" principle is employed, for as is well known this technique proves most beneficial on the higher frequency bands. A tuned r.f. stage is also included and this ensures high gain whilst also acting as a buffer stage against oscillator radiation, via the aerial system.

The primary coverage afforded by the tuned section is $1 \cdot 67-31 \cdot 5 \mathrm{Mc} / \mathrm{s}$ (9.5-180 metres) with additional optional coverage of $0.175-1.545 \mathrm{Mc} / \mathrm{s}$ (194-1700 metres.) These additional ranges are rarely likely to be needed here, however. since they are more easily and conveniently covered using a conventional portable domestic medium/ long waveband transistor receiver.

Mechanical handspreading is provided for the tuned sections via the familiar Jackson "Caliband " drive. this providing by means of its two pointers reduction ratios of 6 and $48: 1$. Although adequate bandspreading is achicved even on the highest frequency ranges a small panel fitted device-to be described later-is also included, this being most useful for minimising interference caused by an adjacent station.


Fig. 1: Block diagram representation of the "Ten-Five" circuit.

It may be noted too that a beat frequency oscillator (b.f.o.) is also fitted together with a "pitch" control to vary the bast note. In addation, the b.f.e. may also usefully be employed in conjunction with the "Pitch" control to make single sideband (s.s.b.) transmissions intelligible.

A signal/tuning meter is litted and operated by the receiver a.ve system and because the a.v.e is made inoperative when the b.f.o. is in use the meter pointer reads full scale. In a permanent battery-powered construction it might then be beneficial to arrange for the meter to monitor the applied battery potential but this service was not needed in the prototype due to use of an a.c. mains power unit.

## Outlets

Both phone and speaker outlets are provided on the front panel and nay be selected as required by means of a switch. The phone outlet is high impedance whilst the "L.S" outct is low impedance and assumes use of an externally connected 302 unit. Some 500 mW of audio is available under normal circumstances via the loudspeaker. The
ats is ustal in push/pull systems of the type employed. The consumption can easily rise to 45 mA or more on peaks so the mains transformer supply is obviously preferable on both regulation and replacement counts. The output stage could then be advantageously allowed a larger quiescent current drain. For general phone use, however. a hattery is quite satisfactory and a reasomable life can be expected.

## Bandchanging

The simple "plug-in" method is employed and becaluse the converter section is fitted with an r.f. stage three coils have to be changed for cach band. A cotal of three sets (nine coils) covers the ranges envisaged so the problem is not very scrious.

Each coil is clearly colour coded and tits a standard noval 9 -pin valve holder. "Padder" connections present no problem either, for on each coil this connection is brought out to a different pin so that if the holder is aporopriately wired the correct padding capacitance is atutomatically conneeted for each oscillator coil. Details relating to this and to ranges covered, etc., are given below.

TABLE I

| Blue and Yellow Coils |  |  |  |  | White coils |  |  | T3 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maker's | Ls | Coverage |  | "Q" | Lo | C9 | pin | Cto | Copi |
| No. |  | $\mathrm{Mc} / \mathrm{s}$ | Metres |  |  |  |  |  |  |
| 1 | 2350 | 0.175-0.525 | 570-1700 | 60 | 156 | 50 | 6 | 35 | 20 |
| 2 | 271 | 0.515-1.545 | 194-580 | 100 | 66 | 110 | 2 | 20 | 10 |
| 3 | $27 \cdot 2$ | 1-67-5.30 | 57-180 | 60 | 13.6 | 340 | 3 | 11 | 10 |
| 4 | 2.9 | 10.5-15.6 | 20-60 | 90 110 | 2.22 2.35 | 960 2000 | 4 | 4.5 1.5 | -* |
| 5 | 0.65 | 10.5-31.5 | 9.5-28 | 110 | $2 \cdot 35$ | 2000 | 6 | $1 \cdot 5$ | -* |

Aerial Coils-Blue, TI. Interstage Coils-Yellow, T2. Oscillator Coils-White, T3.
Ls -Nominal inductive value of tuned winding. (Approximately $15 \%$ variation obtainable via dust core).
' $Q$ ' -Approximate ' $Q$ ' value of tuned winding--mid scale tuning point.
Lo -Nominal inductive value of oscillator tuned winding.
$\mathrm{C}_{q}$-Padder capacitance value required.
Cto -Oscillator pF trimmer capacitance extra to 39 pF assumed circuit capacitance.
Copi - Additional fixed capacitance recommended across tuned winding as appropriate using plug-in band changing method. Note: panel fitted TC4 accomplishes this.
*Harmonic mixing used on this range, the second harmonic being automatically present at alignment.
Note that Table I shows all coils available although only ranges $3-5$ are likely to be required here.
phones may be leli connected or may be removed as required without in any way alfecting the receiver.

## Consumption

The total quiescent current drain from a 9 V supply is 12 mA when the snaker outlet is in use but falls to 5 mA on phone because the output stages are switched out. Bringing in the b.f.o. adds $0.6 \mathrm{~mA}(600 \mu \mathrm{~A})$ and may be considered negligible. Current consumption changes very litile at any time when on phone but if the sneaker is in use the demand varies with the signal strength and volume

## CIRCUIT DESCRIPTION

## Converter and Ist $1.6 \mathrm{Mc} / \mathrm{s}$ I.F. Amplifier

The converter, intermediate frequency stages, a.v.c.. demodulating and limiting sections are shown in Fig. 2. (a) and (b).

The first two transistors. Tri. Tr2 (AF115) are the active elements of the converter. Trl being the r.f. amplifier feeding Tr2 as mixer oscillator. Signals from the aerial are here converted to the 1 st intermediate frequency, viz., $1 \cdot 6 \mathrm{Mc} / \mathrm{s}$ and since no direct pick-up at this frequency is required a simple wavetrap is inserted in series with the acrial.


Fig. 2 (a): The r.f. amplifier, first frequency changes and $1.6 \mathrm{mc} / \mathrm{s}$ i.f. stages of the circuit.


Fig. 2 (b): The second frequency changes, $470 \mathrm{kc} / \mathrm{s}$ i.f. amplifier and detector.

The coil (L1) used here is a range 2 (Denco) valve type, the quoted inductance value of which is $129 \mu \mathrm{H}$ for the main winding. This is roughly resonated at $1.6 \mathrm{Mc} / \mathrm{s}$ by C 1 , fine adjustments being made using the variable core. A single winding high " $Q$ ", $1.6 \mathrm{Mc} / \mathrm{s}$ filter coil could be used as an alternative.

The sensitivity of the r.f. stage is controllable to some extent by means of VR1 which is brought
out to the panel. The control normally needs to be retarded when s.s.b. transmissions are being received but it has also been noted that the gainas indicated by the signal meter-does not necessarily increase when VR1 is turned fully up. Sometimes the reverse is the case depending on the band in use and might be due to the transistor characteristics.

Coils T1, T2 and T3 are the plug-in types
already referred to, each being tuned by a section of the 3 -gang capacitor VC1/2/3 fitted with trimmers. The tuned sections of each transforme: are coupled to the appropriate circuit by mutual inductance.

Signals at $1 \cdot 6 \mathrm{Mc} / \mathrm{s}$ appearing at $\operatorname{Tr} 2$ collector are next applied via a transformer to the base of Tr3 (OC171) for further amplification at this frequency, so increasing the need for the aerial trap.

## Converter Trimming

Although variable r.f. trimmers, panel mounted, are feasible to compensate for errors due to bandchanging, the first oscillator is controlled by means of TC4, labelled (Osc. Trim). In use it is assumed that the first stuge is damped by the aerial so that it remains either to trim the interstage circuit to fit the oscillator or vice versa, the oscillator adjustment being preferred here since it helps compensate for $C_{\text {to }}$ and $C$-opi, Table I.

In practice TC4 is initially set to about haif capacity and the tuning mechanism operated in the -usual way to resolve a signal. Should this seem
" pruned " away. C 10 may also be made to limit maximum circuit capacitance as required.

## Second Converter and $470 \mathrm{kc} / \mathrm{s}$ I.F. Amplifier

When the $16 \mathrm{Mc} / \mathrm{s}$ signals from Tr3 are applied to Tr4 a second frequency conversion takes place. The second i.f. amplifier operates at $470 \mathrm{kc} / \mathrm{s}$ and because T4 can be fixed tuned the oscillator may operate at a frequency lower than that of the signal, i.e., at $1.13 \mathrm{kc} / \mathrm{s}$. The coil (code red-range 2) must be screened, using the can provided; it has a tuned winding, quoted inductance value of $129 \mu \mathrm{H}$ and so requires a capacitor of approximately 170 pF across it, although in practice accurate setting is accomplished with its core. This second converter could be operated at $2.07 \mathrm{Mc} / \mathrm{s}$ if preferred, but use of a different coil would be advisable to allow adequate shunt capacitance to be added whilst Tr4 would need to be an OC44.

The $470 \mathrm{kc} / \mathrm{s}$ i.f. amplifier is conventional except that transistors from the Mullard "AF" range are used instead of the more usual OC45 types which would necessitate additional items in the form of neutralising components. All the i.f. transformers


Fig. 2 (c): The b.f.o. and audio sections, plus the power supplies.
weak. the pointer mechanism is moved a fraction to one side of the transmission and TC4 experimentally adjusted. It is quickly evident which way the main pointer must go by watching the signal meter. TC4 is also useful for piching out a single transmission from a clutter. for losing adjacent c.w., etc.. quality being unimportant. Sometimes a "returning" station is very slightly off frequency and TC4 is then particularly useful. for the main dial needs no alteration, both stations being heard in turn merely by moving TC4 to and fro. A large value capacitor must not be used for TC4 and the total number of vanes should be four, others being
are single tuned and selectivity is quite good. The circled figures associated with all coils and i.f. transformers refer to their basing connections for which a key is provided (Fig. 2).

The signal meter in the collector circuit of Trs reads in reverse but this is not important. (It coull. however, be mounted upside down to give a left to right needle mavement but would require a new scale.)

As the bias varies at the base of Tr 5 due to demodulator action. a large rectified signal tends to cut oft the follector current thereby causing the meter pointer to fall back. The meter records

## COMPONENTS LIST

## Resistors:

| Ris |  |  |  |
| :---: | :---: | :---: | :---: |
| RI | 15 k , | R21 | 680, |
| R2 | IkS | R22 | $4.7 \mathrm{k} \Omega$ |
| R3 | $1 \mathrm{k} \Omega$ | R23 | $1 \cdot 2 \mathrm{k} \Omega$ |
| R4 | $3.9 \mathrm{k} \Omega$ | R24 | $22 \mathrm{k} \Omega$ |
| R5 | $15 \mathrm{k} \Omega$ | R25 | 47kS |
| R6 | $1.2 \mathrm{k} \Omega$ | R26 | 100 kS |
| R7 | $56 \mathrm{k} \Omega$ | R27 | 22 k S |
| R8 | $10 \mathrm{k} \Omega$ | R28 | $4.7 \mathrm{k} \Omega$ |
| R9 | IkS | R29 | $1 \mathrm{k} \Omega$ |
| R10 | $3.9 \mathrm{k} \Omega$ | R30 | $47 \mathrm{k} \Omega$ |
| RII | $15 k \Omega$ | R31 | $10 \mathrm{k} \Omega$ |
| R12 | $100 \Omega$ | R32 | $680 \Omega$ |
| R13 | $2 \cdot 2 \mathrm{k} \Omega$ | R33 | $1 \mathrm{k} \Omega$ |
| R14 | $1 \mathrm{k} \Omega$ | R34 | 68, |
| R15 | $33 \mathrm{k} \Omega$ | R35 | $8 \cdot 2 \mathrm{k} \Omega 5 \%$ |
| R16 | $6.8 \mathrm{k} \Omega$ | R36 | $8 \cdot 2 \mathrm{k} \Omega 5 \%$ |
| R17 | $1 \mathrm{k} \Omega$ | R37 | $5 \Omega$ |
| R18 | $720 \Omega$ | R38 | $100 \mathrm{k} \Omega$ |
| R19 | $4.7 \mathrm{k} \Omega$ | R39 | $390 \Omega$ |
| R20 | $22 \mathrm{k} \Omega$ | R40 | $220 \Omega$ |

    wise stated.
    Potentiometers:
VRI $5 \mathrm{k} \Omega$
VR2 $150 \Omega$
VR3 $5 k \Omega$ with double-pole on/off switch (\$4).
Coils and Transformers:

| IFTI | I.F. tr |
| :---: | :---: |
| IFT2 | I.F. transformer. Denco IFT16 |
| IFT3 | I.F. transformer. Denco IFT\|3 |
| IFT4 | I.F. transformer. Denco IFT13 |
| IFT5 | I.F. transformer. Denco IFT14 |
| TI | See Table I; plug-in transistor coil. Denco (blue) |
| T2 | See Table I; plug-in transistor coil. Denco (yellow) |
| T3 | See Table 1; plug-in transistor coil. Denco (white) |
| T4 | Miniature valve-type coil. Denco range 2 (red) |
| T5 | B.F.O. transformer. Denco IFT14 |
| T6 | Driver transformer. Ardente D3053 (with clamps) |
| T7 | Output transformer. Ardente D3027 (with clamps) |
| T8 | Mains isolating transformer. Norcol or Osmor MT9 |
| LI | Miniature valve-type coil. Denco range 2 (red) |

Variable Capacitors:
$\mathrm{VCl}, 2,3310 \mathrm{pF}$ (nominal) 3 -gang tuning capacitor with feet and trimmers (TCl, 2, 3). Jackson "F'".
TCl, 2, 3 Trimmers on $\mathrm{VCl}, 2$ and 3.
TC4 See text. Jackson "Air Tune".
TC5 25pF. Jackson "Air Tune".

Capacitors:

| C | 75 pF mica |
| :---: | :---: |
| C2 | $100 \mu \mathrm{~F}$ electrolytic |
| C3 | $0.01 \mu \mathrm{~F}$ ceramic or Pa |
| C4 | $0.01 \mu \mathrm{~F}$ ceram |
| C5 | $0.05 \mu \mathrm{~F}$ |
| C6 | $0.01 \mu \mathrm{~F}$ ceramic |
| C7 | 2,000pF mic |
| C8 | $0.01 \mu \mathrm{~F}$ cerami |
| C9 |  |
| C10 | 6 pF |
| CII | $0.01 \mu \mathrm{~F}$ ceramic or pa |
| 12 | $0.01 \mu \mathrm{~F}$ ceramic or pap |
| $\mathrm{Cl}^{2}$ | $0.01 \mu \mathrm{~F}$ ceramic or pape |
| Cl4 | 2,000 pF mica |
| C | $0.01 \mu \mathrm{~F}$ cerami |
| C16 | 175pF mica |
| $\mathrm{Cl}_{17}$ | $10 \mu \mathrm{~F}$ electrolytic 6 V |
|  | $5 \mu \mathrm{~F}$ electrolytic 12 V |
| C19 | $0.01 \mu \mathrm{~F}$ ceramic or |
| C20 | $0.01{ }^{\text {F }}$ ceramlc or pape |
| C21 | $0.01 \mu \mathrm{~F}$ |
| C22 | $100 \mu \mathrm{~F}$ |
|  | $0.01 \mu \mathrm{~F}$ |
| C24 | $0.1 \mu \mathrm{~F}$ pap |
| C25 | $0.01 \mu \mathrm{~F}$ ceram |
|  | $0.01 \mu \mathrm{~F}$ ceramic or |
| C27 | $0.01 \mu \mathrm{~F}$ ceramic |
| 8 |  |
| C29 | $10 \mu \mathrm{~F}$ electrolytic |
|  | $100 \mu \mathrm{Felectrolytic} 6 \mathrm{~V}$ |
|  | $100 \mu \mathrm{~F}$ electrolytic 12 V |
| C32 | $0.2 \mu$ |
| 33 | $0.01 \mu \mathrm{~F}$ paper 1,000 |

Semiconductors:

| Tri | AFII 15 | Tr5 | AF117 |
| :---: | :---: | :---: | :---: |
| Tr2 | AFIIS | Tr6 | AFII7 |
| Tr3 | OC171 | Tr7 | OC45 |
| Tr4 | OC45 | Tr8 | OC8ID |
| Tr9 | OC81 Matched |  |  |
| Trio | OC81 \} pair |  |  |
| DI | OA79 | D4 | GJ7-M |
| D2 | OA70 | D5 | GJ7-M |
| D3 | OA70 |  |  |

Switches:
Sla, b 2-pole, 2-way
S2a, b 2-pole, 2-way
S3 Single-pole change-over toggle
S4 Double-pole on/off switch on VR3

## Miscellaneous:

Meter $500 \mu \mathrm{~A}$ f.s.d. movement. $9 \frac{1}{2} \mathrm{in}$. $\times 6$ in. $\times \frac{1}{16} \mathrm{in}$. piece of paxolin. Nine tag strips. Lektrokit LK-2231. Aerial socket. 16 s.w.g. aluminium for flanges and screen. Two transistor mounting clips. Battery connectors. Phones/speaker outlet sockets. Jackson "Caliband" dial and drive assembly. 3 Noval low-loss valve-holders. Tags, wire, etc.
all changes of signal strength and can thus be used usefully as a tuning indicator and alignment aid. A $500 \mu \mathrm{~A}$ meter movement shunted by a preset variable resistor enables accurate f.s.d. setting as required, at the same time temporarily removing the a.v.c. bias, i.e., by rotating SIA to "Out". Small panel type meters are easily obtainable.

## The A.V.C. System

Diode D1 in connection with Tr 5 collector circuit is arranged to be non-conductive on small or moderately strong signals, the reverse bias applied being in fact 0.6 V . When a very strong signal is tuned in, however, a proportionately
greater bias is applied to Tr5 due to D2 which provides bias at all times. whereupon the potential at ( 18 changes sufficiently for D1 to conduct and thereby damp the first i.f. transformer to reduce gain still further. Simple undelayed a.v.c. thus initiates a delayed a.v.c. characteristic.

## The B.F.O. and Audio Sections

The audio content of the demodulated signal appears across VR3 and is available as required via the slider. S3 determining whether the signals are extracted direct or via the simple series limiter circuit associated with D3. Carrier level maintains D3 in a condacting state but a sudden burst of noise results in cut-off so that the signal path is broken when the switch is set to "In". Distortion occurs particularly at high volume seftings and there is heavy attenuation although the circuit proves useful when listening on 'phones.

The audio stages proper plus the b.f.o. are shown in Fig. 2(c). The b.f.o. calls for little comment since it is a conventional feedback-type


A rear view of the finished receiver.
oscillator operated close to the intermediate frequency, the precise value being controlled by panelfitted TC5. labelled "Pitch". CW signals may then be conveniently heterodyned and in addition s.s.b. transmissions may be read. Sufficient b.f.o. injection results due to stray couplings: it may be noted that C 28 is not required if a 15 pF maximum capacity air-spaced variable trimmer is available for use at TC5.

The audio signal is fed via C29 to Tr 8 , this being a conventional audio driver transistor stage (OC81D) feeding the push/pull output pair. Try/ 10. Fitment of the phone outlet in the collector circuit of Tr8 has no adverse effect on performance for R32 is in series with the phones across the driver transformer when this function is in use. Signals of moderate phone strength are actually available at points "D" and "Y" but the amplification afforded by Tr 8 is worth while using.

The output transistors bias arrangement calls for some comment. As is well known forward bias for a pair of output transistors worked in push/ pull is frequently achieved by connecting the
driver transformer secondary winding centre tap to a fixed potentiometer connected across the supply battery. etc. Here the lower member of such a potentiometer is R 34 but the upper section (normally approximately $4 \cdot 7 \mathrm{k} \Omega$ ) is not connected to the -9 V line. Instead two resistor's are used (R35/36) and connected between base and collector on each of the output pair. This arrangement not only simplifies phone/hs. switching (Try)/10 are completely disconnected at phone) but also introduces some degeneration due to a.c. feedback and this materially assists the overall performance in several ways. at the expense of a small amount of gain. A small portion of the output at T7 is also fed back degeneratively across the amplifier via R38 but apparent increased sensitivity results if the resistor is omitted. It may be noted that the driver and output transformers used in the prototype are Ardente, but there is no reason why equivalent types by other manufacturers should not be used.

## Powering the Receiver

Power requirements were detailed earlier and although the prototype uses an internal mains unit this is by no means essential for the construction is such that a PP9 battery will stand neatly in the area here occupied by the mains components, rectifiers, etc. Expense may be minimised initially by using the battery and adding the mains items required later. In the main. however, battery powering is uneconomical for in common with all transistor receivers batteries have to be discarded when their potential has fallen by some $30^{\circ} \mathrm{j}$ and many volts are thrown away.

As may be seen from the illustration the mains transformer. T8, is quite small physically and is only about one quarter the size of a conventional heater transformer! The promary winding is appropriately tapped and a single secondary supplies $9-0-9 \mathrm{~V}$ which is rectified by a pair of sub-miniature GJ7M diodes. These require no heat sinks due to low current demands. The resultant d.c. potentials are fed to the positive and negative receiver rails. R 40 being included to astist in some degree voltage stabilisation in assochation with C31. An automatic "earth" results from fitting C33. No heating has oceared in the prototype even after allowing the receiver to run continuously for several hours. Constructors who do not wish to include this section should omit all items to the right of the broken line in Fig. 2(c) yet retaining "On/Of" " facilities via the switches integral with the volume control. Care must be taken to check that polurity is correct.
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# INEXPENSIVE INTERCOM SYSTEM by P. D. de Lacey and A. T. Chattaway 

T1HE intercom described here was designed to be built at low cost and to use, as far as possible, existing equipment. It provides a means of speech communication between house and workshop, and may also be used as a private telephone link between adjacent houses. It has the advantage that the sound is reproduced at sufficient volume to be heard throughout an averagesized room, leaving the user at the "slave station" free to continue his work while holding a conversation with his counterpart at the " master station ".

## Construction of the Master Station

The use of a loudspeaker as the microphone,
"gram-input" sockets. The switch should then look like Fig. 2.

## Construction of the Slave Station

The slave station consists of a loudspeaker, as nearly as possible identical with that at the master station: a battery suitable for operating the bell (or buzzer) at the master station; and a push-button switch.

The circuit diagram is given in Fig 3. No constructional details are given since these will vary according to the cabinet used. The push-button $\mathbf{S}^{2}$ is to ring the bell at the master station, which should then call up the slave station.


Fig. 1: Circuit of the master stotion.

## Completion of the Intercom

The wires marked A, B and C in Fig. 1 are joined to the sockets marked A. B and C in Fig. 3 respectively. Suitable wire may be purchased for about 10 s . per half-mile. A valuable saving can be made by using the earth connection of the mains power supply for the connection marked C. This cannot, of course, be done where the "two-pin" fixtures are in use. DO NOT USE THE MAINS EARTH FOR A OR B AS IT WILL INTRODUCE A LOUD HUM.
whilst not giving an ideal frequency response. simplifies the construction to a great extent. Most enthusiasts will have at least one amplifier suitable for this purpose, the only features required being that (a) it will give a loud output using, as a microphone, a loudspeaker similar to that for which its output is matched, and (b) it has one terminal (earth or chassis) common to the input and output circuits (this avoids unnecessary complications in the switching arrangements). Most radiograms come into this category. The circuit of the master station is shown in Fig. 1.

Two sockets and a double-pole double-throw switch are screwed to the case of the amplifier. One of the sockets is connected to the earth or "common" lead of the amplifier, and the other to two diagonally opposed end terminals of the switch. The remaining two end terminals are connected to the side of the loudspeaker which is not earthed. The connection which formerly went to this terminal of the loudspeaker is now joined to one of the centre terminals of the switch. and the other centre terminal to the non-earthed side of the


Fig. 2: Wiring of 51 .


Fig. 3: Slave station circuit.


Fig. 4 (a) and (b): These show, respectively, the receiver volume control before and after the incorporation of a gram input socket and 53.

## Transist orisation of the Unit

A valve amplifier needs to warm up before use and hurried calls may be delayed because of this A transistor amplifter is therefore recommended. If a transistor ratio is owned the chances are that it is not litted with sockets for "gram input".

| COMPONENTS LIST |  |  |  |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { RI } \\ & \text { All } \end{aligned}$ | 100ks R2 IMS <br> $\therefore-20 \% \cdot \frac{1}{4} \mathrm{~W}$ miniature | R3 | 3 k ! |
| Cl C 2 | $2 \mu \mathrm{~F}$ electrolytic 12 V <br> $2 \mu \mathrm{~F}$ electrolycic 12 V |  |  |
| Tri | OC71 |  |  |
| S1 | D.P.D.T. switch |  |  |
| S2 | Bell-push switch |  |  |
| S3 | S.P.D.T. switch |  |  |
| S4 | D.P.D.T. switch |  |  |

These can be fitted very simply by connecting the sockets across the volume control (in most radios). A switch should be litted to disconnect the radio while using the amplifiel. Fig. 4 (a) shows the volume control before alteration and Fig. 4 (b) shows it afterwards.

If this gives insulficient volume a pre-amplifier is needed. This will follow the circuit of Fig. 5. The transistor is a "red spot" or OC71.

The resistors in Fig. 5 may be $\frac{1}{2} \mathrm{~W} .20^{\circ}$ tolerance types. The capacitors should have a voltage rating of at least 12 V . The simplest method of construction is to solder the transistor. 100:? and 1 M ! resistors, and the capacitor direct to the sockets and the 3kse resistor and other capacitor direct to the swith.

## Using the Intercom

After everything has been correctly commected up. the master station should be switched on. the "gram-radio" switch should be put in the "gram". position. the "send-receive" switch in the "send" position, and the volume control adjusted to about half its maximum value. The user should then make some suitable announcement and switch the "sund-receive" switch to the "reccive" position. when he should hear suitable comments from his.


Fig. 5: Circuit of the preamplifier.


Fig. 6: Construction details of the preampififier.
colleague at the slave station. The best position to mount the "send-reccive" switch is on the lefthand side of the cabinet, as it can then be operated with the left hand. leaving the right hand free to take notes if necessary. The volume condrol, if it incorporates the "on-off" switeh. should be marked to enable the most convenient position to be selected each time it is switched on. The user soon acquires the hnack of switching over the " send-reccive" switen to lisien or speak.

# The PRACTICAL WREEESS TRIMMER and ALIGNMENT SET 



TRIMMING tools are not only essential to anyone undertaking serious constructional work on receivers, but they are expendable. This is not to say they necessarily get broken. but like the canteen spoon they are liable to become elusive at the critical moment-usually becuuse someone else has borrowed them.

Many readers, no doubt. already have a set of trimming tools. in particular those who obtained the set we presented with the April issue this year. Others make do with improvised trimming tools fashioned from plastic knitting needles or other suitable materials. We are certain. however, that all readers will welcome the new set of tools being presented with this issue-whether they already have trimming lools or not.

The new set is based on the first set but is designed in a diflerent way. Thus the two sets may be, in some ways. complementary. One great inprovement is the material from which the new tools are made: this is a new very tough plastic, admirably suited for such applications.

The photograph in the heading shows the tools assembled. and a description of their uses follows:

No. 1 has a wide " screwdriver " blade (though it should not be used as such!) and is used to adjust mica and ceramic trimmers, ferrite pot cores. and slotted hex-nut compression trimmers.

No. 2 has a fine. narrow blade for the adjustment
of slotted cores widely used in transistor radio receivers. The slots are often carried right through the core and the correct method of adjustment is to insert the trimming tool as far as possible before turning. to reduce torsion. Since this is a very popular size. two of these are provided in this kit. No. 3 being a duplicate.

No. 4 has a blade suitable for the majority of iron dust cores employed in radio and television receivers (except transistor radios).

No. 5 has a slotted end which may be used for turning the flattened shank (usually brass) which is used to move a ferrite core in the coil of many radio sets and television turret tuners.

No. 6 is for adiusting tuning slugs with hexagonshaped holes. This has a long shank so that it may be used with transformèrs fitted with wo such slugs one above the other. The trimming tool is inserted through the upper slug without disturbing its selting. then inserted into the lower slug which can then be adjusted independently, the diameter of the shank is small enough for it to rotate in the hexagon hore of the upper slug.

Nos 7 and 8 are extension shanks. Each has a hole in the top for receiving the spigot of any of the other trimming tools. No. 7. in addition to the hole, also has a spigot, so that it may be inserted into the end of No. 8. thus exending even further the length of the composite tool.

## DOES YOUR BBC-2 PICTURE SUFFER FROM NOISE?

If so, you should get the September issue of Practical Television (on sale now, 2s.) in which C. H. Banthorpe describes a u.h.f. amplifier designed to overcome this problem. There's much more beside in every issue, to interest, inform and instruct.

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# PART I <br> Understanding SEMICONDUCTORS <br> BY LESLIE MOORE 

'IHE series aims to give the reader a basic knowledge in the use of semiconductors and the principle of operation of several different types of circuit. It also aims to give the amateur ability to design these basic circuits with a minimum knowledge of mathematics. A knowledge of Ohnis law and the basic operation of components such as inductors, capacitors. etc., will be taken for granted.

## CONTENTS OF SERIES

The principle of operation of the crystal dinde with a brief explanation of their atomic structure. the circuit symbol of the diode and an illustrated explanation of the junction diode as a half-wave rectifier.

Reasons for full-wave rectification. introduction to power supplies. rectification, smoothing, stabilisation. An explanation of the smoothing circuit will be given. The zener diode and its use as a stabiliser and the conversion of thermionic rectifiers to semiconductor rectifier circuits.
An explanation of the principle of operation of the transistor. its use as an amplificr and an explanation of the derivation of a formula for current gain. The grounded emitter amplifier, input impedance, output impedance, impedance matching between stages. Frequency response of the amplifiers. negative feedback, the emitter follower. Summary of amplifier.

Oscillators-comparing the oscillator to an amplifier with feedback: the Wein bridge, phaseshift oscillators: an L.C. oscillator.

The free-running multivibrator with a brief explanation of the other multivibrators that exist ( $\div 2$ ctts, etc.).

No circuits will be given as typical example, of working models. It will not be possible to include the whole of one subject in one article except that of the explanation of the principles of operations of single articles, e.g. introductory passage.

## the operation of the crystal diode

Since the introduction of crystal diodes as an electronic device an amazing revolution has taken place. The semiconductor has now become a part of the modern way of life; to enable a greater understanding of their uses and applications this series of articles has been written.
A basic knowledge of atomic structure is necessary to enable the understanding of the operation of semi-conductors.

An atom. the smallest obtainabie particle of an element, consists basically of a nucleus encom-
passed by orbiting particles known as electrons.
The nucleus contains several different sized particles the largest of which are the neutron. an electrically neutral particles. and the proton, which is of equal mass to the neutron but holds a positive electrical charge. The number of protons in the nucleus is equal to the number of orbiting electrons. Electrons orbit the nucleus in a set manner as can be seen in Fig. 1.


Fig. 1: The germanium atom.

The germanium atom has 32 orbiting electrons set in fixed paths known as shells. The first shell contains two electrons. the second eight. the third 18. the fourth four, but in other atoms is capable of holding as much as eight electrons.

Copper has only 29 orbiting electrons. hence it has only one electron in its outer sheil. The nucleus has little influence over the single electron because of the comparatively large distance between the two: on the application of an external electrical force the single electron can be easily attracted away from the atom. This enables copper to be a good conductor of electricity, clecitricity being the flow of electrons.

Germanium, however. has four electrons in the outer shell. so that a greater attraction between the outer shell and the nucleus is established. making the attraction of electrons from the atom difficult. Because of this characteristic gernanium is known as a semiconductor.
The atoms in a germanium crystal form themselves in such a manner so that each atom shares each one of the electrons in its outer shell, with another atom making it appear that each atom has a full outer shell of electrons. The formation is hnown as the crystal "lattice".

If small quantities of (a) arsenic and (b) gallium are added to germanium crystals the following will occur:
(a) Arsenic has five electrons in its outer
shell and an arsenic atom will take place in the lattice as a germanium atom; this will leave a single atom to orbit the arsenic atom. As electrons hold a negative charge this material is known as " $n$ " type.
(b) Gallium has three electrons in the outer shell and if a similar occurrence happens as before, neighbouring atoms in the lattice will share their electrons with the gallium atom but


Fig. 2: Make-up of the semiconductor. The bar of the circuit symbol is equivalent to the cathode of the thermionic diode.
in return can only share three atoms with the germanium. Between two atoms, therefore, there will be a space, one electron missing, which is called a "hole". Because the electrons have a negative charge and the holes indicate a lack of negative charge the holes are said to have a positive charge; this material is called "p" type.

If an alternating voltage were to be applied to the diode the action previously described and as shown in Fig. 3 would occur.
It has been explained how a semiconductor diode could be used as a half-wave rectifier. The problem with this method is one of power consumption; the half-wave not seen in the output is returned back to the supply, so that half the current drawn from the supply is wasted. If the diode were to be connected as shown in Fig. 4. on the half-cycle which is not seen at the output, no current would be drawn from the supply.

The application of rectifying circuits in electronic circuitry is most prominent in power supply units.

For reasons of economy the vast majority of mains supplies in this country are alternating current (a.c.) rather than direct current (d.c.).

The majority of electronic equipment requires a direct current supply and to produce this an a.c. to d.c. power supply unit is used as shown in Fig. 5.

The rectifying circuit produces a pulsating direct voltage from an alternating voltage. A half-wave rectifier may be used for this purpose but the average output voltage is low compared with the


Fig. 3: The action of half-wave rectification: (a) obtaining a positive pulsating direct current; (b) a negative pulsating direct current.

When a junction is made by joining a " $p$ " type crystal to an " $n$ " type crystal the additional electrons in the " $n$ " type begin to flow into the "p" type for a short period and form a barrier at the junction, preventing any further flow of electrons.


Fig. 4: Arrangement for drawing no current from the supply.

The junction barrier so formed is of such a manner to allow electron flow to take place when an external voltage source is applied to the junction, making the " $p$ " type of positive potential with respect to the "n" type. When the voltage or "bias" is reversed the junction will not conduct.
peak voltage of the input. A more efficient but more expensive arrangement is the full-wave rectifier which is a combination of a number of semiconductor diodes. This is shown in Fig. 6.
(1) On the application of a positive half-cycle of alternating voltage it is seen that diode (a) will


Fig. 5: Block diagram of a power supply.
conduct current but diode (b) will not, so that the positive half-cycle will appear at point A .
(2) On the negative half-cycle the signals will be seen by diodes (c) and (d). Diode (d) will not conduct current under this condition but diode (c) is biased to enable it to conduct current. The negative half-cycle will therefore appear at point $B$.

If the output terminal $B$ is held at a steady voltage. usually zero voltage or "earth". the second half-cycle will appear as a positive voltage at A with respect to B.


Fig. 6: The full-wave rectifier.


Fig. 7: The waveform obtained when terminal $A$ is held at steady voltage instead of B.

If a "negative voltage" is required it is in order to hold terminal $A$ at a steady voltage, instead of $B$, and the voltage at $B$ will appear to be a pulsating negative direct voltage (see Fig. 7).

It is obvious that the full-wave rectifier produces an average voltage greater than that produced by the half-wave rectifier for the same input voltage.

Another advatntage of the fullwave rectifier will become apparent when smoothing circuits are dealt with.

The basic component of a smoothing circuit is a vapacitor as depicted in Fig. 8.

As the first input pulse is applied the capacitor draws current from the rectifier circuit and charges to the peak voltage. If a normal load (or a current drawing circuit) is placed across the capacitor. after the first pulsc is applied, the capacitor will then supply current to the load.

Because current is being drawn from the capacitor the voltage across it will drop: the rate at which the voltage across the capacitor falls is much less than the rate at which the voltage from the rectifier falls. The voltage supplied to the load will begin to rise after the rising voltage of the second pulse from the rectifier coincides with the falling voltage across the capacitor.

The waveform due to the changing voltage difference across the capacitor is known as voltage ripple.

There are numerous types of smoothing circuits used, all of them employing the charging of one or several capacitors.

For very good smoothing a filter network. as shown in Fig. 9, is used.

The inductance or choke. 1.. opposes alternating voltages without dissipating excess power. The capacitor $C^{\prime}$ functions in a similar manner in
capacitor $C$, reducing even more the voltage ripple.
A less expensive method is to replace the inductance by a resistor. The resistor opposes direct and alternating voltages equally. The effectiveness of smoothing in this ease is less than the first.

The type of smoothing ined for a circuit is entircly dependent on the degree of d.c. the circuit is required to product.

The stabilising circuit involves more complex components and will be dealt with later in the series.

In many commercial radio receivers, etc., it would be uncconomical to stabilise the output from the smoothing circuit, so the stabilising cirenit is omitted.

The resistor R is placed in the circuit (Fig. 10) to limit the peak rectifier current. If the peak current became excessive the semiconductor diodes


Fig. 9: A filter network.


Fig. 8: The basic smoothing circuit and its action.

# BOORS REVIEWED 

EXPERIMENTAL RADIO ENGINEERING
By E. T. A. Rapson. Published by Sir Isaac Pitman \& Sons Ltd.
214 pages, $8 \frac{1}{2} \times 5 \frac{1}{2}$ in., boards. Price 14 s .

THIS is a fifth edition of an old favourite which dates back to the war years. It will be remembered by many old hands and in its up-to-date edition will, no doubt, be welcomed by newer students of radio.
A new chapter has been added which is devoted entirely to transistors, measurement of parameters, ett.
This book is not intended for the general reader and has. obviously, been written with the technical student in mind.

The entire volume consists of a series of experiments in radio engineering which range from the characteristics of attenuators and filters to electroacoustic tests.

This volume would. as the preface rightly points out, be suitahle for a student attending a three year course in radio engineering at a technical college. Would-he students and prospective radio engineers are referred to Mr. Rapson for further details.

At the price, this is extremely good value. - D.L. ${ }^{\text {G. }}$

## COMPUTER CIRCUIT PROJECTS

By Lee Boschen. 144 pages. Price 21 s.

THERE are many men in the realms of electronics. be they professional or amateur, who are bonded by one common tic-they are practical people. While they no doubt enjoy the odd spate of technical literature they are never more happy than when there is a trusty soldering iron in one hand and a recl of "resin cored" in the other.
This group should find Computer Circuit Projects of great interest, since it eaters for just such tastes. It takes the terrifying and grand name of "computer" and transforms it into 143 pages of practical and interesting circuitry. There are 14 such projects ranging from a single stroboscope to a Rally Computer. Some of these circuits are "Very similar, to others already published. The "Logic Lock" and the "Automatic Signal Flasher" for instance. However, there are numerous ideas to suit all tastec.
It should not be thought that this book is merely a collection of circuit diagrams printed on a fow pages. Fach project has photographs of it together with other illustrations. and with each there is a discussion of circuit action. The circuitry as a whole is right up to date, some using transistors. some diodes or valves. and in some cases an alternative circuit transistor and/or valve is offered.
For those who are tired of t.r.f.'s and audio amplifiers and would like to build something diffcrent but not too difficult, then you are advised to visit your local bookshop with 21s.-D.L.G.

ABCs OF COMPUTERS
By Allan Lytel. 128 pages. Price 16 s.

THE word computer conjures up many things in the mind. Huge grey steel monsters with staring, winking eyes, rows of meters pulsing, and memory mechanisms buzzing. To the average man and to many electronic enthusiasts the word often means huge consoles and thousands of diodes. transistors and/or valves, and quite unconventional and frightening circuitry. Rumour even has it that the grids are taken direct to h.t. + and that transistors are connected the wrong way round -on purpose.
For those who profess to be impartial. and prefer to think for themselves, together with those readers who would like to know some basic facts about computers, it is suggested that an outlay of 16 c . of the realm be made. This modest sum will enable the "enquiring" to ohtain a tome of knowledge aptly tifled ABCs of Computers, and as this title implies it is a book which supplies the basic facts on this fascinating subject. Its 128 pages are generously sprinkled with illustrations and the text is well written and concise.

In a book of this size it is obviously not possible to enter deeply into the subject and the would-be reader. therefore, need not fear that he will be dragged into heavy technical discussions. The chapters 4 and 5 on "Numbers for computers" and "Arithmetic Opcrations" are a pleasure to read. The binary system seems casy enough. once it is understood, hut understanding it in the first place can prove very tricky. Some writers never seem to present this binary business very clearly and often gloss over it in a few words.

However, it would not he true to say this of Allan Lytel. It would have been even more useful had values been given to all circuit diagrams. even more so in this case since the novice would not have any idea of values in these types of circuits shown.

Also, perhaps. having educated the reader to a certain standard it would have been helpful to have provided a list of suggested books for further reading. Howevcr. for the person wishing to scratch the surface of this fascinating fieldABCs of Computers-is recommended.-J.D.G.

## ABCs OF ELECTRICITY

Howard W. Sams Editorial Staff. 96 pages. Price ifs.
These three books, originally published in the USA by Howard W. Sams \& Co. Ine., and now published and distributed in this country by W. Foulsham \& Co. Ltd. Each book has a preface for British readers written by $W$. Oliver $G 3 \times T$. The common format is $8 \frac{1}{2} \times \sin$., stiff covers.

I$N$ any technical field there is one segment of learning more vitally important than any other-the ground work. It is essential that the basic theory be fully understood. and although this may prove a long "slogging" effort it is well worth while in the long run.

ABCs of Electricity is obviously written for the raw beginner and offers five chapters-Electricity (batteries), Magnetism, A.C. Theory and A.C. Theory and

- continued on page 535


HAVING gleaned and logged all the information we can about a station's signal we come to the business of sending off a reception report, and if possible getting it confirmed by a QSL card.

An ordinary piece of notepaper can be used for the actual report but a much neater report can be made on quarto lined paper. Neatness and simplicity are important because (except at the bigger stations) it will probably be in a language of which the evaluating engineers only have a limited knowledge.

As a general rule all stations except those in South America will accept a report in English. With South Amcrica, unless you are dealing with a station which you know to have an English section, the report should be in the local language

Spanish or Portuguese. A suitable translation is contained in "How to listen to the World ".

The first thing a report should contain is your name and address. Great care (block capitals) should be taken to see that this is legible. If the station can't even read your address it is unlikely to persevere with the rest of the report!

To start off you should say something to the effect that recently you were very pleased to heat the station concerned and are enclosing a report on its signal, mentioning the reporting code you are using e.g. SINPO. SINFO. RSI. After this you should ask the station to verify the report. if it finds it to be correct, with its QSL card.
The final part of your letter should deal with your receiving equipment. Details stations are interested in are the type of your receiver (domestic or communications) and the sort of aerial you are using-dipole or end fed, indoor or outdoor.
You shouid then set out your report. It should take a similar form to your log with columns for date, time (stating the zone you are using. Greenwich Mean Time being the most common), frequency (stating whether kilocycles or megacycles), the report (SINPO) and remarks.
Two items go in the last column. The first of these is interference details. These should include the type (jammer, broadcast, c.w.) of the interfering station and its frequency. The second item consists of details of the programme heard. The purpose of giving these details is to prove absolutely to the station that you really heard it. Unfortunately there are some unscrupulous QSL collectors who invent reception reports in the hope of gaining QSL cards. Some stations will waive the programme details after you have proved yourself if you report regularly to them.

Ideally your report should cover at least half an hour's listening time though this need not all be at the same time. Stations that use more than one frequency for a transmission especially appreciate
comparative reports on the frequencies used. You can end your report with such thangs as a programme schedule request. Record jequests or questions for special programmes are best sent in a special letter.

Finally there comes the question of return postage. With large and government stations this is normally unnecessary. Smaller stations, however, often appreciate it. A full list of stations requiring return postage is given in the " World Radio and Television Handbook ". Postage if sent should be in the form of an International Reply Coupon which you can obtain at your Post Office. Don't forget. incidentally, that your report will usually require more than a threepenny stamp.

## DX NEWS

News has just arrived from Radio Japan of its plans for broadcasting the Olympic Games to the world. An unenviable task this, as the games are taking place at about the worst time possible as far as reception conditions go. Recause of this two new 100 kW transmitters are being linked together to give an output of 200 kW .

From October 10th to 24 th when the games are in progress there will be special programmes during Radio Japan's normal transmissions and the general service will be especially extended. Normal transmissions to Europe in English will be at $0800-0820$ GMT on $11.780 / 15.135 \mathrm{kc} / \mathrm{s}$. English broadcasts in the General Service consisting of both live and recorded items are as follows: On $9.505 / 15.195 / 15.310 \mathrm{kc} / \mathrm{s}-0645-0700,0745-0800$, 0845-0900. $0945-1000$ and 1045-1100: on 9.505/ $9.740 / 11.815 \mathrm{kc} / \mathrm{s}-1245-1300$. 1345-1400. $1445-$ 1500. 1545-1600. 1645-1700. 1745-1800 and 18451900: on 11.815/11.940/15,195-2145-2200; on 11.940/15.105/15.425kc/s-2345-0000: on 15,105 ! $15.195 / 15.310 \mathrm{kc} / \mathrm{s}-0245-0300$. 0345-0400.
On October 10th the opening ceremony will be broadcast live from 0450/0700 and on October 24 the closing ceremony will be broadcast live from 0800-0900. Programme schedules giving full details are available free of charge from Radio Japan. Tokyo. Jadan.

Radio Australia has been coming through well in the late evening recently. Two transmissions recently logged around 2245 in London were an Indonesian programme on $11.760 \mathrm{kc} / \mathrm{s}$ and an English programme to Southern Asia. This station's U.K. transmission in English is from 0630-0730 on $9.570 / 11.710 \mathrm{kc} / \mathrm{s}$ but is not coming through too well at present.

A Middle Eastern station presenting quite a challenge is the Kuwait Broadcasting and Television service. It is sometimes audible after 1930 through heavy CW on $4967 \mathrm{kc} / \mathrm{s}$.

For more DX news see page 573

# UTILITY 

## POWER PACK

A Compact Power Supply for the Workbench

by V. E. HOLLEY

MANY constructors have need from time to time of a bench power supply which usually tahes the form of a self-contained pack from which h.t. and l.t. voltages can be taken by leads to the equipment to be supplied. The unit here described is somewhat different, being designed so that it can be fitted in a few minutes to any chassis with only three connections to be made and may remain there permanently if desired.

The basis of the pack is a mains transformer of the three-way mounting type. on to which are fitted all the components of the circuit shown in Fig. 1. Outputs of $250 \mathrm{~V} \quad 80 \mathrm{~mA}$ and heater voltages of $6 \cdot 3,5$ and 4 are provided.

Apart from bench use. the pack is especially suitable for compact equipment. The transformer selccted for the prototype measures 4in. $x 3 \frac{1}{2}$ in. $x 2 \frac{1}{2} i n$. and the addition of the rectifying and smoothing components increases the $2 \frac{1}{2}$ in. measurement by less than a quarter of an inch. The total heating effect is noticeably less than that of a pack using a valve or metal rectifier and this is an important advantage in equipment where temperature rise must be limited.

## Rectifiers and Fuses

Silicon rectifiers are used. These have a very low forward resistance, 15 to $25 \Omega$ being typical. so that the protection against overload afforded by the relatively high resistance of a vacuum valve or metal rectifier is absent. If a large current rating is selected, say 500 mA , the rectifiers do not require any protection against the accidental short circuit that may occur on the bench, but the transformer winding does. Fuses F1 and F2 are therefore included in series with the rectifiers. This arrangement is to be preferred to the more usual single fise in the h.t. secondary centre tap because it gives protection against breakdown of a rectifier.

It will be seen from Fig. 1 that if such a breakdown occurred and there were no fuse, a very large current would pass around the h.t. secondary winding which would quickly be destroyed. The fuse ratings must be selected not with reference to the load current but to the larger value of the surge current which passes into the capacitors C1 and C2 when power is first applied. This is not


Fig. 1: The simple circuit for the power pack.


The finished power pack.

## COMPONENTS LIST

TI Mains transformer, 3-way mounting, $250-0-250 \mathrm{~V} 80 \mathrm{~mA} .6 .3 \mathrm{~V} 3 \mathrm{amps}$, tapped $4 \mathrm{~V}, 6 \cdot 3 \mathrm{~V} 2 \mathrm{amps}$, tapped 5 V and 4 V
MRI, 2 Silicon rectifiers, BYI00 or similar, 800 V p.i.v., 500 mA
RI Resistor-lk $\Omega$, low
$\mathrm{Cl}, \mathrm{C} 2$ Capacitors- $16+32 \mu \mathrm{~F}$ electrolytic, 350 V working in lin. diameter can
F1, F2 Fuses rated at 150 mA each
Fuseholders-two
LPI Pilot lamp-2.5V 0.3A bulb
SI Double pole on/off switch
Length of tag strip
Perspex for cover, self-tapping screws, wire and sleeving, etc.

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easily measured but with the values of $\mathrm{R}, \mathrm{Cl}$ and C2 shown. 150 mA fuses are satisfactory.
It is important that the rectifiers should have adequate peak inverse voltage rating. Referring again to Fig. 1, when the right hand side of SR 1 is 250 V rms above earth, the peak voltage dt this point will be 1.414 times as great, i.e., approximately 350 V .
Capacitor C2 and the left hand side of SR2 will also be at this potential: but the right hand side of SR2 will at the same instant be 350 V peak negative to earth so that the peak voltage across it in the non-conducting direction will be 700 V . In practice. this theoretical figure may be increasedsomewhat by the effect of line surges. wave form distortion and such-like disturbances. so the rectifier peak inverse rating should not be less than 800 V .

## Construction

Fig. 2 shows the positions of the components and the connections to be made. The wiring should be no longer than necessary and if $20 \mathrm{~s} . \mathrm{w}$.g. tinned copper is used. it can be laid neatly in position and will stay there. The tag strip holding the smoothing resistor etc.. must be soldered to the transformer frame. using a large iron. and the rectifiers tucked neatly beneath it as shown in the illustration.

Take care not to use the earthed tags for any of the connections. The outer metal bodies of the rectifiers are "live" so they must be firmly positioned clear of the transformer frame. The indicator lamp is considerably under-run and so is not likely to need replacement: it can therefore be soldered permanently into circuit without a lamp holder. The fuse holders are secured with impact adhesive.

## Safety Precautions

In view of the exposed h.t. connections it is advisable. if the unit is for bench use. to fit some sort of cover over both sides of the transformer. This was done in the case of the prototype by bending two pieces of $1 / 16 \mathrm{in}$. perspex to the required rectangular shape and securing them to the sides of the transformer frame with selftapping screws.

The bending can be accomplished quite easily after clamping the perspex between two pieces of plywood along the line of bend and dipping the assembly in very hot water.

The cover should be about half an inch shorter than the height of the transformer so that an opening can be left at the bottom for through ventilation which the smoothing resistor at the top will promote by convection. The double pole on-off switch, S1, S2, is fitted to the cover on the


Fig. 2: Construction details of the unit.
mains input side of the transformer. If desired, an additional fuse can also be fitted here in the a.c. supply line as a protection against heater line short circuits etc.

A suitable rating, allowing for surge is 250 to 500 mA .

## BOOKS REVIEWED

-continued from page 530
Generators and Alternators. Although there is no question that this book offers a great number of basic facts there are one or two puzzling aspects of $i t$.

In Figs. 1-13 and 1-14 the battery mysteriously reverses polarity and the voltages in Fig. 13 are given with respect to reference point $D$. The voltage then would be minus 6 V and minus 5 V and not just 6 V or 5 V as stated. In Fig. $1-17$. page 24 , we are told to note that 4 amps of current flow toward point $A$. but there is. in fact. no suc' reference point marked $A$ in the Fig. 1-17 at all. In the photographs, Figs 2-4 and 2-6. the same battery is shown twice, and perhaps a different
photograph would have been more educational. It would certainly prove more interesting.

A graph appears on page 62 and the vertical axis is marked in gausses. yet the word gauss does not appear to be included in the text at all. These points may appear small, but since the book is intended for beginners it is felt they should be mentioned
Vecior diagrams start to appear on page 73 and it is regrettable that no clear explanation of them appears. particularly as their importance is very great. as anyone who has studied a.c. theory will know.

The book is priced at 16 s . and it is suggested that any reader conemplating pu-chasing it should be in a position to examine it first rather than send money "blindly" through the post. -D.L.G.

# The "Spectreuphon" 

# SOME IDEAS FOR EXPERIMENTS WITH CHROMASONIC DISPLAYS 

## BY I. J. KAMPEL

DESCRIBING a unique device, which from an existing audio source, improves mono or stereo reproduction, and provides a visual conception of the music, by means of changing colours, to match the mood of the music.
There are many examples of how sound and colour can be subtly merged to produce an unparalleled emotional effect-producing not only extreme pleasure, but a pleasing relaxation of mind. This is offered as a supplement to all hi-fi and audio fans-so much more than the 'flat' sound from a single-speaker mono system. and much more pleasing than the simpler two-speaker stereophonic system.

The Spectrcuphon provides a visual conception of the music to be provided from an existing audio source.


Fig. Ia (above): The basic layout of a mono system using the "Spectreuphon".
Fig. Ib (right): The arrangement for stereo.

Direct coupling to most modern radios, taperecorders, record-players, is simply made through extension speaker sockets. It will be necessary, however, to fit a switch on the audio unit. if one does not exist, to cut out the internal speaker.

Before describing the unit in detail. a brief description of the effect would be in order.

## Effect of Mono Spectreuphon

The author has previously described a unit for feeding two loudspeakers from an existing audio source (mono), giving an effect not unlike stereophonic sound to the unexperienced, average listener. No owner of a stereo set-up would mistake it for stereo. but if suitable speakers are used, he would be forced to admit there was a fair comparison. Some listeners to the system were in fact convinced that it was stereo, and found it
just as satisfactory! (The original unit-the Euphon-appeared in the October, 1963, P.W.) The mono version of the Spectreuphon contains the original Euphon circuit. (Section 2, Fig. 2.)

The Spectreuphon should be listened to-and viewed-in a darkened room:

Let us suppose that the unit is connected to a record-player, and a record has just been put on. Until the record begins there will be complete darkness-then comes the music-and light. The coloured light thereafter faithfully follows the pitch. volume beat, and general mood of the music. As the volume increases so the light becomes more intense; it follows visually if there is a distinct beat; if there is a predominance of treble. mid-range, or bass, so there is a predominance of one particular colour, and as the ranges merge together so do the colours, mixing, diffusing together. giving subtle intermediate shades and hues. If the record ends in a fade-out, so the light dies down to darkness with the sound.


## Effect of Stereophonic Spectreuphon

Two inputs are required for this unit. these being taken from the sockets to which left-hand and right-hand channel speakers are usually connected. The audio to these speakers is then fed via the Spectreuphon unit. This is neccssary, as the unit must have a volume level on it.

The left-hand audio channel then controls the left-hand side of the display unit-consider it as a screen for now-whilst the right-hand audio channel covers the other half. This means that beside the visual effects described in the mono version, the stereo version provides left and right emphasis according to speakers, and also a colour shift if there should be an audio movement shift.
The stereo Spectrcuphon does not improve sound reproduction in itself. If, as later diagrams
indicate, two crossover networks are employed. and a four-speaker system set up, then there will be a great improvement. Many stereo systems have, however, these networks built in, with twin woofer and tweeter.

## Single Speaker Spectreuphon

If for one reason or another, only a single speaker may be employed, or a single speaker
view. it consists simply of a number of lights.
There are three groups of lights, each group controlled by a different filter network and channel of the Spectreuphon. One set of bulbs responds to bass, one to treble, and the third to mid-range.

Fig. 2 is the complete mono Spectreuphon, which includes a two-channel audio tuetwork to feed two loudspeakers. to give an effect similar to stereophonic sound. This circuit diagram is divided


Fig. 2: The complete circuit of the mono "Spectreuphon".
unit. slight adaptions will have to be made to the circuit of the mono unit. Details of this will be given later. It is possible to use only the one existing speaker.

## The Spectreuphon Circuit (Mono)

Fig. Ia is a block diagram of the basic principle and lay-out of the mono system. Actual visual units will be described later, but whatever type is used, basically. and from the electronic point of
into five sections so that reference to this circuit is simpler.
Section $\mathbf{1}$ is the three-channel filter network which separates treble. mid-range, and base, and so controls a group of lights on each of these channels. An increase in one range, and the consequent additional transistor bias. increases the collector current, and consequently the lights brilliance. being connected ciirectly in the collector line.

Section 2 is the two-channel audio network, which feeds J2 a low frequency output, and 13 a high frequency output, so the speaker connected to $\mathbf{1 2}$ produces mainly bass, and the speaker to J3 mainly treble. Coil and cap. details are to be found in Table 1.
Section 3 is simply a switching unit on the three outputs of Section 1. Each of these outputs feeds a different set of lights, of a different colour. Hence, the six-way, three-pole switch, allows any combination of colours and channels to be obtained, so giving a greater varicty.
Section 4 is simply the smoothed power supply. There is little to say about this, as any suitable

| TABLE I |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| C | L | Speaker Impedance | C | L |
| 6-9 | 1-2 | $3 \Omega$ | $\begin{aligned} & 30-32 \mu \mathrm{~F} \\ & \text { electrolytic } \end{aligned}$ | $3 \Omega 0.135 \mathrm{mH}$ |
|  |  | 158 | $\begin{gathered} 5-8: \mathcal{F} \\ \text { electrolytic } \end{gathered}$ | $15 \Omega 0.675 \mathrm{mH}$ |
| X | $Y$ | $3 \Omega$ | 30 2 F paper | $3 \Omega 20.135 \mathrm{mH}$ |
|  |  | 1592 | 6uF paper | $15 \Omega 0.675 \mathrm{mH}$ |


| Suitable makes | LI-L2 |  | as below |
| :---: | :---: | :---: | :---: |
| $X \& Y$ | Hunts <br>  <br>  | Denco <br> D54/I-WP44 <br> divider |  |

full-wave bridge rectificr and transformer are satisfactory.
Section 5 indicates the form the lights will take. Only one of six bulbs on each channel is indicated. It will be seen that they all have a common negative-the only contact with the negative side of the rectifier-except the smoothing capacitor.

## Controls

VR1, VR2, VR3, are sensitivity controls, and require some patience to set for best performance from the visual unit.
VR4, is an audio volume control. The volume control on the existing audio unit is turned up until a suitable level is obtained in the lights unit. VR4 is then used to turn down audio to a comfortable level.
VR5. is a balance control, and with this it is possible to shift the treble-base emphasis, according to individual requirements.

## Details of Construction

It will be seen from the circuit diagram (Fig. 2) that resistors $R 4, R 5$, and $R 6$, have no value indicated on them. The reason for this is that they tend to vary according to particular transistors. To find the right value resistor. the method indicated in Fig. 3 should be employed. Here a variable resistor and a set resistor are connected, in serics, collector to base. The six bulbs should he in circuit for this test, on each channel. Sct this system up on each of the three transistors. For this test, the audio part of the circuit need not be operational. but it will probably be found that the level required to operate the unit will be too high for listening to, and hence the speaker on the audio unit will have to be cut out.

Firstly, in daylight, adjust each of the three 3 K potentiometers until the filaments of the bulbs on each of these channels have just gone out. When this has been carried out on all channels, start the audio unit up. The lights should then light up and


Fig. 3: Determining the values for $R 4, R 5$ and $R 6$, see text.
fluctuate in brilliance. Adjustment of VR1. VR2 and VR3 may be necessary. but if the lights are working as described, it is pointless at this stage, to try and adjust them for optimum treble-mid-range-bass performance.

In Fig. 3 the Ik resistor is in series with the potentiometer as a safety measure, and should not be omitted. If it is. a collector-base short could occur, causing permanent damage to the transistor. When the correct level has been found, the resistance then across the collector-base of cach transistor should be measured, and replaced by a resistor of the same value. If space will permit, leave the potentiometers in circuit. These potentiometers should be mounted inside the unit,

## COMPONENTS LIST

| Number required |  |  | Euphon Circuit (Sect. 2 Fig. 2) |
| :---: | :---: | :---: | :---: |
| Mono | Stereo |  |  |
|  |  |  |  |
| 2 | 二 | LI, L2 | See Table I |
| 4 | - | $\mathrm{C} 6-\mathrm{C} 9$ | See Table I |
| I | - |  | $25 \Omega$ wirewound pot. |
|  |  |  | LIGHTS FILTER NETWORK Ete. (Sect. I) |
| 3 | 4 | J1-J3, Jx | Jack plugs and sockets |
| 3 | 6 | VRI-VR3 (x2) | $100 \Omega$ wirewound pots |
| 1 | 1 | $\checkmark R 4$ | $50 \Omega$ wirewound pot |
| - | 1 |  | Twin-ganged 50 ohm wirewound pot |
| 2 | 4 | R1, R2 (x2) | $15 \Omega \frac{1}{2}$ watt res. |
| 1 | 2 | $\text { R3 }(x 2)$ | $100 \Omega^{2} 1$ watt res. |
| 2 | 4 | C1. ${ }^{\text {C4 ( }}$ (2) | $2 \mu \mathrm{~F} \text { elec. } 25 \mathrm{~V}$ |
| ! | 2 | $\mathrm{C} 2(\times 2)$ | $10 \mu \mathrm{~F}$ elec. 25 V |
| I | 2 | C3 $3(\times 2)$ | $50 \mu \mathrm{~F}$ elec. 25 V |
| 1 | 2 | C5 (x2) | $25 \mu \mathrm{~F}$ elec. 25 V |
| 4 18 | 7 |  | Wander plugs and sockets |
| 18 2 | 24 |  | 6.3 V 150 mA bulbs |
| 2 | 2 | S1, 52 | D.P. S.T. toggle switches |
| 1 | - |  | 6 W .3 P . rotary switch (mono) 6W. 6P. rotary switch (stereo) |
| 3 | 6 | Tr1-Tr3 (x2) | or as required $0 \subset 20$ |
| 3 3 | 6 |  | Test Requirements $1 \mathrm{k} \Omega$ res. <br> $3 \mathrm{k} \Omega$ wirewound pots |
|  |  |  | POWER SUPPLY <br> (Sect. 4 Fig. 2) |
| One 3A | One 4A | TI Transform 15 V | mer: primary to suit; secondary |
| 1 | I | C10 $1000 \mu \mathrm{~F}$ | elec. cap. 25 V |
| I | 1 | R7 \| $\Omega$ \| wa | att res. |
| I | I | Full-wave | e rectifier 3A/4A |
| 1 | I | 3A/4A Fu | use |

Fig. 4: Connections to an OC28 transistor.

so that they are only disturbed when required. The response of the lights is far more sensitive if adjusted as described.

Fig. 5 indicates the mounting of the power transistor.

Oversize holes are drilled in the chassis to ensure that the connections do not short to chassis. The transistor rests on a lead heat-sink. and underneath this us a mica washer to insulate the collector from the chassis.

Should it be found that the lights will not dim, then a higher value potentiometer or resistor should be fitted in place of the original.

SkI, Sk2. Sk3, are the positive contacts of the three sets of bulbs. Six bulbs, in parallel, are connected to each of these sockets, their common negative on all sets, going to Sk4.


Fig. 5: Mounting details of the power tronsistor.

When ready for the final test of audio and visual unit, each of these sets of bulbs will be a different colour.

## The Spectreuphon Without Additional Speaker Cabinet

If it is required to have the visual unit with original sound (mono), and it is found on test that the volume is not too high when turned up high enough to operate the Spectreuphon light-control unit, then you have no problem. Forget Section 2 and just plug in to extension speaker sockets for light control. If, however, as expected, it is too high, then the audio level has to be brought down by another control.

In Fig. 6, a two-way, iwo-pole switch is inserted between the speaker and output transformer. In one position there is a straight path through and in the other position, the path is through to socket. JA.

A lead is then taken from this, preferably
screened, to JB or Jl on Fig. 2.
The $50 \Omega$ potentiometer is then used to turn the volume down to a suitable level, and the signal is fed back to the original unit, and speaker, via JC on the Spectreuphon unit, and JD on the audio source.

If this is the method that is to be employed. because of reasons of expense or space, sound could be improved by the addition of a small tweeter in the record-player or what-have-you, in which the speaker is contained.

The circuit of Fig. 7, the usual crossover network, should then be employed. The coil and capacitor values given in this table are also suitable for the Euphon circuit.


Fig. 6: Incorporating a two-way, twa-pole switch between the speaker and output transformer.


Fig. 7: A crossover network for the "Spectreuphon".

Unless the audio source is of the standard known to-day as hi-fi. the addition of this network is pointless. This also applies to some extent in the audio circuit of the Spectreuphon. If there is not any response below say $10 \mathrm{kc} / \mathrm{s}$, or a cut-off before it reaches the higher frequencies, little will be gained by the use of this unit.

If there is room for a single cabinet, a large woofer and small tweeter mounted logether in the same cabinet, if large enough, will produce far superior audio to that previously experienced with a single-perhaps small-speaker, in a cabinet which did not allow the required resonance. The cross-over network of Fig. 7 should be used for this. connected across $Y Z$ on the original circuit (Fig. 2).


I1 HIS transistor tester was developed to facilitate rapid transistor testing in the workshop. The main purpose of this tester is to make what are primarily "go"-"no-go" tests, by measuring the transistor collector leakage current and current amplification factor in the common emitter configuration. i.e. Ico and $ß$. Experience has shown that a tester of this type is all that is required to tell whether a transistor is working or not or to measure or compare "Beta" for matching transistors etc. Furthermore testers of this type are generally used in preference to the more accurate and comprehensive transistor parameter test sets.
The basic tester is suitable for testing only low power receiving type transistors.

## SPECIFICATION

Collector Leakage Current ( 1 co ) $0-1 \mathrm{~mA}$
Current Amplification Factor (B) 0-100 $\}$ two 0-250 $\int$ ranges
Transistor Type
pnp or npn

## CIRCUIT AND THEORY

The circuit of the tester is shown in Fig. I. ^ $4 \frac{1}{2} \mathrm{~V}$ dry hattery is used as the power source. one of quite small capacity being suitable since the maximum drain is 10 mA and that only for the few seconds required to take a reading.

Switch SI selects the supply polarity required

## A SIMPLE Irinsi

for either npn or pnp transistors with a central "off" position. whilst switch S2 is used to measure either Ico or "Beta." When switched to Ico the base circuit of the transistor is left open circuit and a $4.5 \mathrm{k} \Omega$ resistor is connected in series with the meter to prevent it being damaged if a transistor having a short circuit between collector and emitter is tested. When the tester is switched to read lco a check on battery voltage may be made by shorting the collector and enitter terminals, the meter should then read full scale or thereabouts, since the meter is connected as a voltmeter reading 4.5 V full scale. It may, incidentally also be used as a continuity tester or ohmmeter! There are two positions of S2 for measuring "Beta," the first giving a full scale

## COMPONENTS LIST

## Resistors:

R1 $45 \mathrm{k} \Omega(33 \mathrm{k} \Omega+12 \mathrm{k} \Omega) \frac{1}{4} \mathrm{~W}$ h.s.
R2 $112 k \Omega(100 k \Omega+12 k \Omega) \frac{1}{4} W$ h.s.
R3 $4 \cdot 5 \mathrm{k} \Omega(3 \cdot 3 \mathrm{k} \Omega+1 \cdot 2 \mathrm{k} \Omega) \frac{1}{4} \mathrm{~W}$
R4 390s:

## Switches:

SI 2-pole 3-way rotary (or 4-pole 3-way, see text).
S2 3-pole 3-way rotary
\$3 Bell-push type: push to make

## Miscellaneous:

MI ImA moving coil meter
$4 \frac{1}{2} \mathrm{~V}$ battery. Case. Knobs, terminals, crocodile clips, etc.


reading of 100 and the second of 250. The measurement of "Beta" is effected by injecting a known current into the base of the transistor and measuring the resultant collector current. Thus when the meter is switched to the "Beta" range giving a full scale reading of 100 , a current of $\underline{4.5} \times 1,000 \mathrm{~mA}=0.1 \mathrm{~mA}$
45.000
is injected into the base of the transistor. Now $\Delta \mathrm{Jc}$
" Beta" $=\frac{\Delta \mathrm{Ic}}{\Delta \mathrm{Ib}}$
hence, assuming a linear characteristic, Ic
$"$ Beta $"=\frac{-}{\mathrm{Ib}}$ (approx.).
If Ico is small compared with the collector current, lc, this is a reasonable approximation. So if the meter reads 3 mA " Beta" $=\frac{3}{0 \cdot 1}=30$.
With the meter having a full-scale deflection of 10 mA the reading of 3 mA so obtained will correspond to a " Beta" of 30 , which is the correct result.

When S2 is switched to read "Beta" a $390 \Omega$

## By K.BERRY

resistor is connected in series with the meter to protect it from damage should a transistor having an internal short circuit be connected to the tester. This resistor may be removed by pressing a push button. S3, which then shorts the 390 resistor, though in practice the value of "Beta" indicated varies very little whether the resistor is in or out of circuit.

In the circuit shown, the metcr reads the collector current plus the base current, but since the latter is so small it makes very little difference to the indicated value of "Beta." This slight error can be overcome by moving the meter cirsuit from its present position to one where it is in the collector circuit. The only drawback is that S 1 then becomes a four pole switch since the meter must be reversed as well as the battery when changing from pnp to npn transistors. The modified circuit is given in Fig. 2.

## CONSTRUCTION AND COMPONENTS

The prototype tester made by the author is illustrated in Fig. 3 and was made as small as


Fig. I (left): The basic circuit of the transistor tester.

Fig. 2 (right): The circuit modified to incorporate a 4-pole switch in the SI position to give the instrument a slightly better degree of accuracy.

possible. It is housed in a small proprietary diccast box measuring $7 \frac{1}{2} \mathrm{in}$. $\times 2 \frac{1}{\mathrm{k}} \mathrm{in}$. $\times 4 \frac{3}{3} \mathrm{in}$. (Eddystone Cat. No. 845 ). Small rubber feet are fitted to the underside of the instrument to prevent it scratching polished surfaces.

The meter used originally was a $2 \frac{1}{2}$ in. diameter moving coll meter with a resistance of 1800, but any 1 mA meter will suffice. It will be seen that in the components list the value of Rs, the meter shunt, is not given. This is because the value of this resister will depend on the resistance of the meter used. Its value may be calculated from the
expression: $\mathrm{Rs}=$ meter resistance $\times \frac{-}{90}$.


Fig. 3: A view of the finished instrument showing the front ponel layout of controls, etc.

Hence in the original transistor tester, which used a meter with a resistance of $180 \Omega$, the shunt

$$
10
$$

Rs has a value of $180 \times \underset{90}{-}=20 \Omega$.
The type of components used is unimportant, though it is suggested that the resistors controlling the base current $100 \mathrm{k} \Omega+12 \mathrm{k} \Omega$ and $33 \mathrm{k} \Omega+$ $12 \mathrm{k} \Omega$ should be $1 / 4 \mathrm{~W}$ high stability types. Fig. 4 shows the internal layout of components and the wiring.

## TEST CONNECTORS

The connections to the transistor under test are brought out to the front panel via sockets which take "wander" plugs such as are used for the older type of h.t. battery. To facilitate connecting : transistor to the tester. the standard "wander" plugs have been modified by cutting off their heads and soldering "crocodile" clips to them as shown
in Fig. 5. The plug portion of the plug/crocodile clip assembly is then inserted in the tester socket.

## USING THE TESTER

Having assembled and wired the tester it may now be given an initial test before being used. This may be done by switching to $n p n$ and Ico when once again the meter should read full scale, When this has been done a "known good" transistor should be tested as follows: First connect the transistor to the tester. Next select npn or pnp as required by S1. Then set S2 to Ico and note meter reading. Finally switch $\mathbf{S 2}$ to "Beta" 100 range and note reading. If reading is greater than 100 switch to "Beta" 250 .

It should be appreciated that when testing a transistor on this tester there is no thermal stabilisation and in consequence measurements of "Beta" should be made quickly, otherwise the junction will rise in temperature, with the result that lco will increase and thermal runaway might occur.


Fig. 4: The wiring inside the case. This diagram shows the wiring for the circuit of Fig. 2, i.e. with 4 -pole switch.


Fig. 5: The modified wander plugicrocodile cilp transistor connector.

# Miniature POWER Amplifier 

by J. Harrison



TIHIS small power amplifier was developed while converting a mono radiogram to stereo, but since making the unit many other uses have been found. among them as a centre channel amplifier for experiments in 3 channel stereo, as the output stage of a domestic radio and as a monitor during tests on cquipment when using an uscilloscope. No doubt the constructor will find plenty of other uses for this compact cool-running amplifier.

For constructors who are tired of the usual single-ended small amplifier designs (usually employing a valve of the ECL80, ECL82. ECL86 varietyl. this circuit makes an interesting and rewarding project, easily assembled in a few hours.

The two valves used are almost sure to be found in the spares-box and are 12AX7 (amplifier and phase-splitter) and 12AU7 (push-pull output). These can be bought for around 6s. 0d. each.

The advantages of push-pull operation are well known and $90 \%$ of all amplifiers with a hi-fi tag to them have push-pull output. The main advantage for an inexpensive amplifier is the fact that there is no d.c. flux in the output transformer and no signal currents flow around the power supply, which contributes greatly towards amplifier stability.

In a practical amplifier. due to slight unbalance of valve currents and signals. perfect cancellation is not achieved but even so there is a great improvement compared to single-ended working. The only disadvantage is. more signal drive is required because the signal is halved between the two output valves.

## The Circuit

One half of the first valve is used as a voltage amplifier directly coupled to the other half used as a phase-splitter. The
anode load of the first stage is large ( 470 kS ) and working into the high-impedance of the phasesplitter produces a greater than usual stage-gain.

Provision has been made in the cirait for a negative feed-back loop (if required) from the output transformer seconclary to the sathode of VIA.

The amplifier should be tried out at first without any fecdhack. tested and if satisfactory then it should be incorporated. The amount of n.f.b. will depend upon how much gain the constructor can afford to lose, however, even without any n.f.b. sound is clean and well-damped.

## Construction

Construction is quite simple and there is plenty of room on a $4 \frac{1}{2} \mathrm{in}$. $x 4 i n$. $x$ lin. chassis. The layout shown in the diagrams is definitely the best for


Fig. 1: The simple two-valve circuit.
short leads and constructors are recommended to follow it.

Most of the components are mounted on a small tag-board which has ten pairs of tags. These have been numbered for reference 1 to 20 in the wiring diagram. Some of the tags are linked together and wiring these first before mounting any components will make the job much easier.

There are three components not on the tag board:
(1) Input grid resistor RI between pin 7 on VIA and earth solder tag.
(2) Output valves bias resistor R10 from the commoned cathodes of V2 to the centre
-continued on page 566

## COMPONENTS LIST

Resistors:

| R1 | $270 \mathrm{k} \Omega$ | R7 | $22 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: |
| R2 | $470 \mathrm{k} \Omega$ | R8 | 470ks |
| R3 | $4.7 \mathrm{k} \Omega$ | R9 | $470 \mathrm{k} \Omega$ |
| R4 | $220 \Omega$ | R10 | 270』 IW |
| R5 | 100k $\Omega 1 \%$ h.s. | RII | $4.7 \mathrm{k} \Omega$ |
| R6 | $100 \mathrm{k} \Omega 1 \%$ h.s. |  |  |
|  | 5\% $\frac{1}{2} \mathrm{~W}$, unles | ther | state |

## Capacitors:

$\mathrm{CI} 16 \mu \mathrm{~F}$ electrolytic 350 V
C2 $100 \mu \mathrm{~F}$ electrolytic 6 V
C3 $0.05 \mu \mathrm{~F} 350 \mathrm{~V}$
C4 $0.05 \mu \mathrm{~F} 300 \mathrm{~V}$
Valves:
VI $12 \mathrm{AX7}$ (ECC83, CV4004)
V2 $12 \mathrm{AU7}$ (ECC82, CV4003)

## Miscellaneous:

TI Output transformer, to match $10 \mathrm{k} \Omega$ anode load (see text).
Two B9A valveholders. IO-way tag strip.
Coaxial socket.


Fig. 3: Above-chassis loyout and dimensions.


Fig. 2: The main wiring diagram; below is an underchassis view of the finished amplifier.


Fig. 4: Harmonic distortion plotted against output for the 12AU7 operated in Closs A push-pull.

NOME like circuses others prefer bread. The organisers of the Radio Show contrive to offer us both.

Some of the other exhibitions around town look with envy on the Earls Court Dichotomy. But radio and television are a natural gift to the show-hizminded organiser. After all free samples of synthetic butter. or a static, unreal room, or ceven a bevy of this year's winners of the nursemaid stakes can hardly compete with the Fiair of the Air.

Behind it all there is a pretly formidable feat of dovetaled planning. And not a little skullduggery.

It is the aim of many exhibitors to unveil a last-minute surprise. "You want a better set-we have it . . . at lest". they secm to say. This leads to a frenzied rushing around on preview and opening days of the gentlemen of the Press. Dashing the free gin from their lips, they converge on the suspected harbour of secrets and attempt to lift the veils-or at least those ugly dust covers that so many cxhibitions aflect. (Haven`t they heard of polythene?)

Hard on their heels come the rival representatives. They try to look unconcerned as they tecter on tiptoc. wondering whethe: that box behind the stand is going to turn out a trend-setter TV or merely contains the managing directors packaged chicken and champagne lunch.


Frenzied rushing around

Up in the Organiser* Office the headache grows yet more intense. Piles of statistics have to be sorted. analysed and sent to the corners of the world. The bloke with the late-entry surprise may find he has defeated himself hy missing the Press boys deadline. Or he may lose his impact entirely with the kind of oracle who sits in the Press Office and writes his report to the readers of Little Midmarsh from the wealth of exhibition handouts.

On the stands all is glitter and smiles. Bright new models look better than they ever will again. Silver and gold plated dissections revolve on their stands. Artycrafty scenes vie with the blatantly humorous displays. while here and there. as if in detance, some bold maker stachs his cxhibits like a row of cheeses. One expects the immaculately dressed vendor to bark: " Roll up, roll up. Every one a wimer".

The annoying thing to some hardened visitors is the lack of information available on their favourite hobby-horse subjects. The deferential gent at the front of the stand is not quite sure. He will have to ask Mr. Mumblegum. This elusive character is hidden behind a phalanx of broad backs, within the drapes and hardboard. like a Rugby forward changing his lattered shorts.

In the meantime there is much else to see. The special attraction. for example. of the XYZ demonstration. We concult the gulde, the official map. which even a child could understand. We are stupidly adult. We end up wandering in widening cireles between towering walls of brick. When we finally reach the Dem. Room a forbidding elockface. its hands leering toward some impossibic. future appointment. confronts us.

For the moment we must be satisfied with the information in the leaflets so lavishly displayed


Changing his shorts.
on every other stand save where we forage. Little boys with capacious satchels have long since skimmed the cream.

But there is still plenty to see. The designers of both the technieal innards and the fashionconscious cabinets and cases (for some modern sets can hardly be described as having cabinets) are at pains to cry their originality. Which makes it all the more surprising when we see the same styling on so many stands. Are we to believe that design has reached a saturation point of near-perfection? (Stand up that man who gave a hollow laugh!)

In our bemused wandering around this Aladdin's Cave of wonders we are likely to lose sight of the great amount of background work. The miles of specially laid cable, the carpentry, the decoration, the problem of assembling people and products under one roof at any given period.
Think of that next time you eurse the unexpected hump on the floor of the main aisle, the confusing layout of stands that always secms to lead you past the same eyc-catching display. the queues for lukewarm tea, the foot-wearying iron stairs, the heat. the draughts, the impassable crowd around the rostrum.

Whether your taste is for bread or circuses, remember we must have both.

## AN

# INDUCTANCE/CAPACLTANCE TESTER 

by H. Webster

Asumpie but versatile two terminal oscillator which enables inductance and capacitance measurements to be carried out with good accuracy is described. In addition, gang capacitor sections and inductances, whether screened or unscreened, can be matched to a high degree of accuracy. Further suggestions are given for the construction of a signal generator which is a novel departure from the usual type of instrument.

A problem which is frequently encountered by the constructor is the measurement of inductance. In particular, one is often faced with the task of matching inductances to fairly close tolerances. Even when two coils are wound as physically similar as possible, the inductances of the respective coils may well vary by as much as $2 \%$. In most cases the error will generally exceed this figure.

As a simple example consider an inductance of $100 \mu \mathrm{H}$ in parallel with a capacitance of 200 pF . The resonance frequency of the combination is $1125 \mathrm{Kc} / \mathrm{s}$. Replacement of the $100 \mu \mathrm{H}$ inductance with one of $99 \mu \mathrm{H}$ results in the new resonance frequency of $1131 \mathrm{Kc} / \mathrm{s}$. Since the miss match between the two inductances is a mere $1 \%$, the $6 \mathrm{kc} / \mathrm{s}$ error is somewhat astonishing. Nevertheless, a simple calculation wiil convince the experimenter of the truth of this statement.

Two such coils used in the radio frequency stages of a receiver would give extremely bad alignment. Since hand wound coils are less reproducible than machine wound coils, these errors are frequently much greater than in the foregoing example.
For some time past the author has employed a simple unit which can be used to match inductances to a high degree of accuracy. In addition, the inductances of coils can be measured, capacitances determined and tuning capacitor sections equalised. Slight modification of the oscillator is necessary if inductance and capacitance measurements are contemplated. The modified circuit diagram 1 . given in Fig. 1.

## Principle of operation

## Inductance measurement.

A simplified block diagram of the basic circuit for the measurement of inductance is given in Fig. 2.
The mode of operation is as follows. L, the unknown inductance, is placed in parallel with a standard capacitance $C$. The resonance frequency of the combination LC is determined by means of a calibrated receiver. A knowledge of this frequency enables one to determine the inductance utilising the formula

$$
\mathrm{L}=\frac{25,330}{\mathrm{C} \mathrm{f}^{2}}
$$

where $L$ is expressed in microhenries, $C$ in microfarads and $f$ in kilocycles/second. Since several


Fig. 2: The basic arrangement for making inductance measurements.
factors have been excluded, this method is only suitable for approximate measurements.

In the block diagram, the tacit assumption has been made that the capacitance $C$ is the


Fig. 1: The basic circuit of the instrument. only capacitance in circuit. Since circuit wiring and valve electrode capacitances are present these so called stray capacitances must be taken into account.
Consider the following argument:
Let $\mathrm{L}=$ inductance $\mu \mathrm{H}$.
$\mathrm{C}_{\mathrm{s}}=$ stray capacitance $\mu \mathrm{F}$.
$\mathrm{C}_{1}=$ maximum capacitance of $\mathrm{C} \mu \mathrm{F}$.
$C_{2}=$ minimum capacitance of $\mathrm{C} \mu \mathrm{F}$.
$\mathrm{F}_{1}=$ resonance frequency of combination $\mathrm{L}, \mathrm{C}_{1} \mathrm{C}_{\mathrm{s}} \mathrm{kc} / \mathrm{s}$.
$F_{2}=$ resonance frequency of combination.
$\mathrm{L}, \dot{C}_{2} \mathrm{C}_{3} \mathrm{kc} / \mathrm{s}$.
When $C_{1}$ is in circuit, total capacitance $=\mathrm{C}_{1}+\mathrm{C}_{\mathrm{s}}$.

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Fig. 3: Specimen graph of dial readings plotted agairst capacitance. The apparent zero capacitance at a dial reading of 16 occurs because of the arbitrary choice of 500pF as maximum capacity.
When $C_{2}$ is in circuit, total capacitance $=C_{2}+C_{s}$.

$$
\therefore \text { since } \mathrm{LC}=\frac{\mathrm{K}}{\mathrm{f}^{2}} \text { where } \mathrm{K}=25,330
$$

$$
\text { then } L\left(C_{1}+C_{5}\right)=\frac{K}{f_{1}{ }^{2}}
$$

Subtracting

$$
\text { and } L\left(C_{2}+C_{s}\right)=\frac{K}{\mathrm{f}_{2}{ }^{2}}
$$

$$
L\left(C_{1}+C_{s}\right)-L\left(C_{2}+C_{5}\right)=\frac{K}{f_{1}{ }^{2}}-\frac{K}{f_{2}{ }^{2}}
$$

$$
\text { or } \mathrm{LC}_{1}+\mathrm{LC}_{\mathrm{s}}-\mathrm{LC}_{2}-\mathrm{LC}_{\mathrm{s}}=\frac{\mathrm{K}\left(\mathrm{f}_{2}{ }^{2}-\mathrm{f}_{1}{ }^{2}\right)}{\mathrm{f}_{1}{ }^{2} \mathrm{f}_{2}{ }^{2}}
$$

$$
\text { or } L\left(C_{1}-C_{2}\right)=\frac{K\left(f_{2}+f_{1}\right)\left(f_{2}-f_{1}\right)}{f_{1}{ }^{2} f_{2}{ }^{2}}
$$

transposing

$$
L=\frac{K\left(f_{2}+f_{1}\right)\left(f_{2}-f_{1}\right)}{f_{1}{ }^{2} f_{2}{ }^{2}\left(C_{1}-C_{2}\right)}
$$

Hence, if the resonance frequencies, $f_{1}$ and $f_{2}$, are found and $C_{1}-C_{2}$ is known, then $L$ can be calculated. Two points arising from this expression are worthy of note. First, the stray capacitance term $\mathrm{C}_{5}$ is automatically cancelled out in the derivation. Secondly, the expression contains in the denominator the factor $C_{1}-C_{2}$. Since this is merely the difference. $\Delta \mathrm{C}$, between two quantities, the absolute value of C , the variable capacitor, is not required. What is required. however, is an accurate knowledge of $\Delta \mathrm{C}$.

## Practical considerations

An accurate calibration of the variable capacitor
is absolutely essential if reliable results are to be obtained. A method for the determination of $\triangle \mathrm{C}$ will now be given.

With the switch in position 2 the standard medium wave coil is brought into circuit. The variable capacitor is turned to maximum capactty. In the author's instrument this capacitor had a nominal value of 500 pF and was fitted with a dial calibrated from 0-100.

A table, divided into two columns, is drawn up. One column represents capacitance, the other column dial readings. The capacitance column is divided in 50 pF intervals, starting with 500 pF , corresponding to a dial reading of 100 .
The modulated r.f. signal emitted by the oscillator is picked up on the calibrated receiver which is tuned to the medium wave band and placed a suitahle distance from the oscillator. A knowledge of the frequency of the emitted signal is not necessary for calibration of the capacitor

The receiver setting is left undisturbed and a close tolerance $( \pm 1 \%)$ capacitor of $50 p \mathrm{~F}$ capacitance placed across the LC terminals. The variable capacitor is retuned until the signal is again picked up on the receiver. Since the inductance is constant, the reading of the variable capacitor must have decreased by 50 pF . The dial reading must therefore correspond to 450 pF . With the dial setting of the variable condenser unchanged the 50 pF standard is removed and the signal again picked up on the receiver. The 50 pF standard is replaced across L.C and the variable capacitor retuned as before. In this way a series of capacitance points, each differing by 50 pF can be obtained. The variable capacitor dial readings are then plotted against the appropriate capacitance readings on a sheet of graph paper as shown in Fig. 3. Reference to the graph will then enable the constructor to determine the capacitance difference between any two points on the dial.

The factors affecting the accuracy of the foregoing calibration will be apparent: First, the calibration is based on the accuracy of the fixed standard capacitor, and secondly, it is necessary to decide whether two signals are of equal magnitude. For all practical purposes a $\pm 1 \%$ silver mica capacitor is adequate for calibration purposes. The second source of error can be largely elliminated by fitting the receiver with an output meter. Alternatively, if a.v.c. is fitted, a $0-10 \mathrm{v}$. d.c. meter may be connected across the bias resistor of one of the controlled valves.

## Applications of instrument <br> Inductance measurements

The experimenter is often required to wind a coil to a given inductance value. In general the required number of turns can be obtained either by calculation, using some type of empirical formula, or b* graphical methods. After winding the coil with the appropriate number of turns it is frequently found that inductance is quite different from the nominal value.

Now let us suppose that a coil of inductance $170 \mu \mathrm{H}$ is required for medium wave band coverage. Reference to tables or formulae will indicate that approximately 98 turns of $34 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. enamelled wire close wound on a 1 in. diameter former will give this value of inductance. Starting at the grid end of the coil, wind on 5 turns and space this section from the remaining 93 turns by approximately $\frac{1}{8}$ in. Switch the oscillator to position 1 and connect the coil across the LC terminals. Set the variable capacitor
to 400 pF and tune in the resulting signal on the receiver. Note the frequency $f_{1}$. Reset the capacitor to 300 pF and again note the new frequency $f_{2}$. The values obtained in this way are substituted in the formula and the inductance calculated. Adjus tment of the inductance can be made either by spacing of the 5 turn section or by removal of turns.

As an example of an experiment by the author, a coil of nominal inductance $170 \mu \mathrm{H}$, was required. It was found that with 400 pF in circuit the resonance frequency was $600 \mathrm{kc} / \mathrm{s}$. With 300 pF in circuit the resonance frequency was $680 \mathrm{kc} / \mathrm{s}$. Substitution in the formula gives

$$
\begin{aligned}
& \text { nula gives } \\
& 25330 \times(680+600) \times(680-600)
\end{aligned}
$$


assures readers that this is extremely unlikely! In the more likely event of $f_{1}$ and $f_{2}$ being different, note whether $f_{2}$ is greater or less than $f_{1}$. If $f_{2}$ is greater than $f_{1}$ then $L 2$ is less than $L 1$ and conversely, if $f_{2}$ is less than $\mathrm{f}_{1}$ then L2 is greater than L1. Since it is more practicable to remove turns from a coil, inductance matching is carried out on the higher of the two inductances. The following procedure is adopted.
With the lower of the two inductances determine the frequency with the calibrated receiver. Without disturbance of the generator or receiver settings, remove the inductance and insert the inductance of higher value. The coil is then adjusted, either by placing or removal of turns until the emitted signal coincides with the receiver setting. The coils are then matched.

Although the arithmetic is simple, the working out is a little heavy and the use of logarithms is recommended. In the above case the inductance was increased by bringing the 5 turn section into closer proximity with the main coil.

A serious source of error in the preceding experiment can arise in reading the frequency on the receiver dial. Unless the receiver calibration can be relied upon a better procedure is as follows. Tune the receiver to a station of known frequency at the 1.f. end of the medium wave band. Adjust the oscillator variable capacitor until zero beat is obtained. With the aid of the graph note the capacitance corresponding to the dial reading. Retune the receiver to a station of known frequency near the h.f. end of the band. Adjust the variable capacitor for zero beat, again noting the capacitance reading. The inductance is calculated as in the preceding example.

When other inductance values are required a rough calculation will give the approximate frequency coverage and the receiver can be switched to the appropriate band.

## Inductance matching

Although the foregoing experiments are of interest, particularly where an exact knowledge of the inductance of a coil is required, in practice, the constructor is more interested in the matching of coils rather than in the determination of absolute values. It will now be shown how exact matching of two or more coils is possible.
Let us assume that two coils L 1 and L 2 , require matching. Insert L1 across the LC terminals and place the switch in position 1. Adjust the variable capacitor to any convenient value and the note the frequency $f_{2}$ of the resulting signal on the calibrated receiver. Remove L1 and insert L2 and again note the frequency $f_{1}$ of the signal. If $f_{1}$ and $f_{2}$ coincide the coils are perfectly matched. However, the author


Fig. 4: The underchassis wiring diagram.
If greater accuracy is required the coils can be matched by zero beating against a station of known frequency. With practice, a high degree of accuracy can be achieved.

It is important to note that after each adjustment of the coil, the hand or any other earthed object should not be in close proximity with the coil. Since it is inevitable that the panel is near to the coil, each determination is carried out at exactly the same distance from the panel.

## Gang capacitor matching

It is not generally realised that gang capacitor sections are rarely equal. In many cases the errors involved may be as great as $2 \%$. For exact ganging of circuits not only must the inductances be matched and stray capacitances balanced out but also the gang capacitor should have equal capacitance in each section at every setting of the gang capacitor. Too often this source of error is overlooked when poor receiver alignment is obtained, Provision is generally


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made for the adjustment of gang capacitor inequalities by the provision of split end vanes in each section. Using the oscillator, excellent matching of gang capacitor sections can be achieved in the following manner.

For the purpose of illustration the matching of a twin gang capacitor will be described. With the oscillator switch in position 3 the medium wave coil is brought into circuit and the variable capacitor switched out of circuit. Connect one section of the gang capacitor across the LC terminals of the oscillator. Turn the gang capacitor from maximum capacity to minimum capacity until the first segment of the split end vane is completely in mesh with the stator plates. Tune the receiver to the h.f. end of the medium wave band until the oscillator signal is heard. Remove the clip from the stator tag of the first section and replace on the second section tag. The end segment is then gently bent out from the vertical and auay from the other rotor vanes until the radiated signal coincides with the receiver setting

Naturally the choice of section for adjustment depends on which section has the higher capacitance value. The higher the capacitance, the lower the frequency, conversely the lower the capacitance, the

higher the frequency. The adjustment is always carried out on the section with the higher capacitance.

When equality has been obtained the process is repeated with the remaining segments until a perfect match is obtained at all settings of the gang capacitor.

## Capacitance measurement

Capacitors in the range $10-500 \mathrm{pF}$ can be measured with reasonable accuracy by means of the oscillator. The accuracy of measurement is limited only by the errors involved in the calibration of the oscillator variable capacitor. The principle of the method is similar to that employed in the calibration method.
With the variable capacitor set to maximum
capacity ( 500 pF ) the resultant frequency is observed on the receiver. The unknown condenser is placed across the LC terminals and the variable capacitor tuned until the signal is again heard. The capacitance reading of the oscillator dial is noted. For example, if the setting of $C$ without the unknown capacitance is 500 pF and 450 pF with the unknown capacitance in circuit, then the value of the unknown capacitance is $500-450=50 \mathrm{pF}$. This method is unsuitable for capacitances greater than 500 pF since the greatest measurable capacitance can never be greater than the capacitance swing of the variable capacitor.

## Constructional details

The oscillator is constructed on a $5 \mathrm{in} . \times 3 \mathrm{in} . \times 2 \mathrm{in}$. chassis, the relevant dimensions being given in Fig. 5. Wiring of the instrument is not critical and most of the components will probably be to hand. The variable capacitor is the most critical item and it is strongly recommended that a good specimen manufactured by a reputable firm is used. Since the current consumed by the oscillator is negligible a small midget transformer will sulfice for the power requirements. In the author's instrument the transformer is separate from the oscillator but there is no reason why other constructors should not make the transformer an integral part of the unit. A slightly larger chassis will of course be necessary if this is envisaged.

Fig. 5 (left): Principal chassis dimensions.


Fig. 6: An above-chassis view.
The connections of the unknown intuctance or capacitance to the LC terminals are of considerable importance. These connections should be constructed from thick copper wire so that the leads are sell supporting. The two leads terminate in crocodile clips which can be lirmly attached to the component under test. When testing gang capacitor sections it is important that the frame of the capacitor us connected to the terminal marked E . Similarly, if screened coils are being tested the screen and earthy end of the coil should be firmly earthed to the same terminal.

The oscillator switch performs three functions. Position I is used for inductance testing and matching, position 2 for capacitance testing and position 3 for gang capacitor matching.

When testing or matching inductances it is essential to ensure that the two coils are tested in the same
position relative to the instrument panel. To avoid undesirable screening! effects it is recommended that the test leads are not less than 3 in . in length.
The author has found that the instrument is greatly superior to the grid dip oscillator for the measurement of inductance and capacitance. If desired, the basic circuit could be embodied in a complete signal generator with the additional facilities of inductance and capacitance testing being incorporated. A suggested circuit for the experimenter who desires to elaborate on the test unit is given in Fig. 9.

## Appendix

For the sake of completeness and as a convenient reference for constructors the following data is included.

Several expressions are available for the calculation of the number of turns required for a given inductance The author has used two well known formulae which have proved satisfactory in practice. The first formula is applicable to single layer coils.

$$
N=L R\left[1+\sqrt{\frac{9}{a L R^{3}}}\right]
$$

Where $\mathbf{N}$ is the required number of turns
L is the inductance in microhenries
a is the radius in inches
and $R=\frac{20}{n d^{2}}$ where
$n$ is the number of turns per inch d is the diameter in inches

The second formula is applicabie to pile wound coils. See Fig. 8.

$$
L=\frac{0.2 \times a^{2} \times N^{2}}{3 a+9 b+10 c}
$$

where $a$ is the mean diameter
$b$ is the winding length
$c$ is the depth of winding
N is the number of turns
all dimensions being expressed in inches


Fig. 7: Front panel layout of controls.

Applications to coil winding
The frequency coverage of a given coil and variable capacitor is given by the expression
$\frac{f_{2}}{f_{1}}=\sqrt{\frac{\overline{C_{1}}}{C_{2}}}$ where $C_{1}$ is the maxinum capacity of the variable capacitor and $\mathrm{C}_{2}$ the minimum capacity. In practice, stray capacitances have to be taken into account. These extraneous capacitances have a bearing on the frequency coverage of the given combination of C and L . Now let us suppose that it is desired to cover the medium wave band with a given coil and a variable capacitor of 500 pF nominal capacity. Average values for the maximum and minimum capacitances of such a capacitor are 500 and 15 pF respectively. To these values must be added stray capacitances, which in general may be as high as 15 pF . The capacitance coverage is now $515-30 \mathrm{pF}$. The total minimum capacitance is now brought up to some predetermined value by the use of a trimmer capacitor. Let this excess capacitance be 20 pF . The capacitance coverage is now $535-50 \mathrm{pF}$. We can now calculate the frequency coverage using the previous expression. If we assume the lowest frequency we wish to cover is say $560 \mathrm{kc} / \mathrm{s}$ then

$$
\text { Since } \frac{f_{2}}{f_{1}}=\sqrt{\frac{535}{50}}=3.27
$$

then $f_{2}=560 \times 3.27=1753 \mathrm{kc} / \mathrm{s}$.
The inductance of the required coil may be calculated utilising the expression

$$
\mathrm{L}=\frac{-}{\mathrm{Cf}^{2}}
$$

Substitution of the previous values of C and F gives

$$
L=\frac{25,330}{.000535 \times 560^{2}}=165 \mu \mathrm{H}
$$

The required coil may now be weund to this inductance value using the first inductance formula. Let the diameter of the former be 1 in . and assume that the given enamelled wire occupies a winding length of 100 turns per inch. e.g. 34 s.w.g.

$$
\begin{aligned}
& \quad \text { Since } R=\frac{20}{n d^{2}} \text { then } R=\frac{20}{100 \times 1^{2}}=0.2 \\
& \therefore N=165 \times 0.2\left[1+\sqrt{1+\frac{9}{0.5 \times 165 \times \cdot 04}}\right]=97
\end{aligned}
$$

Hence the coil can be wound with 97 turns of 34 s.w.g. wire, close spaced and occupying a length of approximately 1 in .

An example of inductance calculation utilising the second formula will now be given. Assume that a coil of $2000 \mu \mathrm{H}$ inductance is required to be wound on a 1 inch former and using 34 s.w.g. wire. Any arbitrary value of $b$ may be chosen. Let this value be $\frac{1}{8}$ inch. The number of turns of wire occupying this length is approximately 12. It is now necessary to try several trial solutions. Assume that 100 turns are required. The number of layers is. therefore
100

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The depth therefore is $\frac{8}{100} \mathrm{in} .=\mathrm{C}$.
Substituting these values in the formula gives

$$
L=\frac{0.2 \times 1.08^{2} \times 100^{2}}{3.24+1 \cdot 11+0.8}=454 \mu \mathrm{H}
$$

thus giving one trial solution. The process is repeated for other values of N . A rough plot of N against


Fig. 8: Critical coil dimensions in inductance calculations.

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Fig. 9: Input circuit for combined signal generator and inductance/ capacitance tester. SI: pos. I inductance match and test; 2 capacitance test and $560-1600 \mathrm{kc} / \mathrm{s} ; 3$ gang capacitor match; $4180-600 \mathrm{kc} / \mathrm{s}$; 5 1.6-5 Mc/s; 6 5-15 Mcis; 7 $10-30 \mathrm{Mc}$ 's.

inductance is made, when the required number of turns for the given inductance may be read off from the curve.

Another and possibly less tedious method of computation may be carried out with this formula

$$
\frac{0 \cdot 2 a^{2} N^{2}}{3 a+9 b+10 c}
$$

Transposition gives

$$
N^{2}=\frac{L(3 a+9 b+10 c)}{0 \cdot 2 a^{2}}
$$

The preceding $2000 \mu \mathrm{H}$ inductance may now be calculated as follows.
Two arbitrary valves are assigned to $b$ and $c$. For the purpose of calculation let $b=\frac{1}{8}$ inch and $C=$ $\frac{1}{8}$ inch, then since $L=2000$ and $a=1 \frac{1}{8}$

$$
\text { Then } N^{2}=\frac{2000\left(3 \frac{1}{8}+1 \frac{1}{8}+1 \frac{1}{4}\right)}{0.2 \times 1 \frac{1}{8} \times 1 \frac{1}{8}}=49,400
$$

$$
\therefore \mathrm{N}=222
$$

The required gauge of wire is now calculated. Let
$n$ be the number of turns per inch.
Then the number of turns in length $b=b n$.
and the number of turns in depth $\mathrm{c}=\mathrm{cn}$
$\therefore$ Total number of turns $=b n \times c n=b c$
and this value is equal to N
$\therefore$ Since $N=222$
then $b c n^{2}=222$ and since $b=c=\frac{1}{8}$ in.
then $n=\sqrt{\frac{222}{\frac{1}{8} \times \frac{1}{8}}}=120$
From wire tables it is found that the nearest gauge which has a winding length of 120 turns per inch is 38 s.w.g. enamelled wire.

The required data is therefore 222 rurns of 38 s.w.g. enamelled wire, pile wound to a length of $\frac{1}{8} \mathrm{in}$. and a depth of $\frac{1}{8}$ in.

The required number of turns for the inductances given in the suggested circuit of Fig. 9 can be calculated by means of these formulae. These calculations are left as an exercise for the experimenter.

## TRADE NEWS•TRADE NEWS • TRADE NEWS TRADE NEWS•TRADE NEWS • TRADE NEWS

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This battery-operoted record player is made by W. H. Sanders (Electronics) Ltd.

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## THE "MULTIPHONIC"



# A I3-STAGE STEREO AMPLIFIER <br> BY MARTIN L. MICHAELIS 

CONTINUED FROM PAGE 421 OF THE SEPTEMBER ISSUE

PROVIDED that the points outlined last month regarding h.t. voltage for the output stages are observed, almost any reasonable arrangement with available components may be used as h.t. supply if the exact specified items are not to hand.

If a transformer with a centre-tapped full-wave h.t. winding $250-0-250 \mathrm{~V}$ (do not use a higher voltage one) is used operate one rectifier MR1. MR2 off each 250 V end. The value of R20 will almost certainly need to be raised somewhat under such circumstances. If valves type ECC88 are available in place of PCC88 all heaters may be run in parallel off a single 6.3 V winding, so that only one such winding (rating about 3 A ) is then needed. However, such valves are rarer than PCC88s. If a single heater winding used in this way has no tap earth one side and operate DI and D2 off the other end.

The resulting increased bias voltage may be applied to $V 4$ without further modification but C11 on each amplifier must now be shunted with a 5 V Zener diode (cathode to chassis). If a 4 V tap is present earth the " 0 " end and oper"ate D1, D 2 off the 4 V tap. Naturally, when using ECC88s R41-R44 are not required.

## Circuit Details of Input/Output Matrix

V4 and V5, on the one hand, and V3 on the other hand constitute two separate units, either or both of which may be omitted if not required. V3. with its function of splitting a monaural input into two channels, is the more important. It is hardly sensible to omit it if one is likely to operate with monaural signals in addition to pure stereo.

The output matrix section $V 4$, V5 may be
omitted if one never contemplates using outputs other than the two main speakers, and when the latter are substantial enough to give good bass reproduction themselves. not requiring the use of a common middle position bass amplifier and speaker operated off P4 when feeding a large audience in a large room with large baseline stereo signals.

The circuit arrangement of V3 is known as "anode-splitter". Both grids of the double triode are fed in parallel from the monaural input via separate grid-stoppers to prevent parasitic oscillation. The anode circuits are separate. giving two identical but electrically separate outputs.

The unbypassed cathode resistors both reduce gain (largely unwanted in this stage) and neutralise any would-be cross-talk between stereo signal channels due to this stage. R22/VRI/VR2 form an output voltage divider. coupling into the respective main amplifier channels: C14 is the normal h.t. voltage blocking capacitor.

This very high impedance voltage divider serves the purposes of further removal of unwanted gain of V3. thus not unnecessarily raising the hum and noise level. and it also prevents loading of the stereo input through the anode circuits of V3. R21 serves no electrical purpose, being merely a convenient anchorage point in the layout specified.

This sort of measure is a useful trick to remember: if a string of required components in serics requires anchorage at a junction a very high value resistor or very low value capacitor can be used as a dommy tie-point to chassis or some other convenient anchorage. One must merely be certain that the electrical side effects are in all cases truly negligible.


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V4 operates simultaneously as a pair of independent cathode-followers for the stereo output at P3 and as an additive anode amplitier developing a combined monaural signal across R34 from the stereo input to the two grids.

The monaural anode signal is passed on to V5 as output cathode-follower. R35 and R37 as voltage divider set an operating point of sufficient standing anode current for $V 5$ as the d.c. voltage across R37 is repeated by d.c. cathode-follower action across R38. Such a method of positive grid bias on an h.t. bleeder is not usable for V4 because it would pass d.c. into the track of VR3. making operation of that control scratchy.

The use of extra blocking capacitors would produce unnecessary bass loss and phase shift. detrimental to stereo reproduction with a central common bass speaker. Thus cathode bias is used here as an alternative.

## Speakers

The cabinet design used in the prototype for the complete unit aims at giving a complete selfcontained installation for "personal" stereo listening in a sma! room. Two small oval speakers of about $3 \times 5 \mathrm{in}$. are specified and housed in niches at each end of the amplifier cabinet. giving a baseline of about 2 ft . This gives a reasonable stereo impression when the unit is standing on the table in front of the listener athout a yard from his head.

A more intense eflect is obtained when the speaker units are removed from the niches and placed as far apart as the listener recedes from them. The room area-in which stereo effect obtain: is therehy also greatly increased. enabling larger audiences to be served.

However, with the small speakers specified the tone is likely to be very shrill and thir when they are moved apart, with a rather empty "middle ". Ihis defect may be combated either by using in addition. placed centrally, a third amplifier and large bass speaker, operated off P 4 . or simply by bsing an identical pair of much larger speakers in good cabinets.


Fig. 4: The amplifier power supply


The "Multiphonic" viewed irom the rear.


Fig. 5: Control layout on the front panel of the completed "Multiphonic".

Performance is very good indeed if a pair of 10 in . speakers with $15 \Omega$ speech coils are mounted in bass reflex corner cabinets, stood in adjacent corners of the room and operated directly off the two amplifier channels.

A general rule for stereo listening is that the lines from the ideally positioned listener to the respective speakers should be approximately at right-angles. Frequencies below about 200c/s do not contribute gratly to the stereo effect as the human ear is not able to distinguish direction of origin very clearly at low frequencies.

Thus a common central speaker, obtaining bass from both channels, may be used. It is even
possible to use passive cross-over networks for three speakers from the two amplifier outputs for this type of arrangement.

However, the use of two-channel speakers alone, both having adequate bass response, is generally preferable because-even though bass stereo contribution is negligible-the phasing is always purer in such an artangement. thus definitely improving performance.

If a central bass speaker is used it is essential that a top-cut filter is used, preventing frequencies above at the most $500 \mathrm{c} / \mathrm{s}$ reaching this speaker in audible amount. Otherwise the stereo effect is greatly weakened.

## Miniature Power Amplifier

-continued from page 544
spigot on valve-holder No. 2.
(3) Decoupling capacitor Cl from tag No. 20 to earth.
Use rubber grommets in the holes in the chassis where wires pass through to prevent the plastic insulation being cut by sharp edges. Wiring should follow normal audio practice. twisted leads for heaters and single earth connection to chassis. When wiring-up do not forget the centre spigot on the valve-holdera, which must be earthed. plus one side of the output transformer secondary.

## -

## Power Supplies

Almost any power unit will be able to supply the modest power necessary. smoothed h.t. of approximately $280 / 290 \mathrm{~V}$. at 20 mA and 6.3 V a.c. at 0.6 A . An h.t. supply of 300 V must not be exceeded.

## Components

Resistors of $1 / 2$ watt rating are adequate. Only two close-tolerance resistors are needed and these are the phase-splitter anode and cathode loads,
where signal balance depends upon equality of the resistors. $1 \%$ tolerance must be used here.

Resistors for the rest of the circuit are preferably high stability of 50 tolerance, these are only slightly more costly than normal $10 \%$ carbon types and are well worth the slight extra cost.

Do not use a midget-sized o.p. transformer, otherwise low-frequency power output will be severely limited. A $3 / 4 \mathrm{in}$. stack of laminations is the minimum for reasonable fidelity. The correct anode to anode load is $10 \mathrm{k} \Omega$ and the turns ratio of the transformer for different loud speaker impedances is as follows:

| Speaker Z | Ratio |
| :---: | :---: |
| 30 | 60 to 1 |
| $8!3$ | $35: 1$ |
| $15!2$ | $25: 1$ |

## Testing

When connected to a suitable power supply and correctly matched to the loudspeaker. feed in a signal from tape-recorder or radio tuner and if qatisfactory a test of voltages in the circuit can be made.

Voltages indicated are for no-signal conditions and should be within $5^{\circ}$ of the indicated values. If voltages across the cathode bias resistors are low this indicates low emission of the valve(s).

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ABSORPTION WAVEMETERS 3.00 to $35.00 \mathrm{Mc}^{\prime} \mathrm{s}$ in 3 switched bands． $3.5,7,14,21$ and 28 Mc s．Ham bands，marked on scale．Complete with indicator bulb．A MUST for any Ham shack， $22^{\prime} 6$ post free．
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THERMO， $2 \frac{1}{4} \mathrm{in}$ ．round $0-2.5$ amp， $7 / 6$ each．P．\＆P． $1 / 6$ ．

## I70－I72 CORPORATION ST． BIRMINGHAM 4

# The BUCCANEER 

# MULTI-BAND TRANSMITTER 

By J. E. Alban G3JEA

CONTINUED FROM PAGE 438 OF THE SEPTEMBER ISSUE

'HE transmitter is assembled on a standard 16 in . $x 9 \mathrm{in} . x 2 \frac{1}{2}$ in. deep chassis. and the valve base holes cut as shown in Fig. 4. If the Labgear unit is used. a drilling template is supplied by the makers and this should be positioned as indicated. The v.f.o. box is approximately 3 in . high. $2 \frac{1}{2}$ in. wide and 4 in . deep, but should this not be readily avaifable a small chassis could be used and a side cover fitted, access being made through the left hand side should repair be necessary. Alternatively, an Eddystone die-cast box can be used. The p.a. compartment is made rather on the
large side to allow for ample ventilation.
All wiring should be carried out in 20s.w.g. finned copper, covered with suitable insulated sleeving. Heater leads, h.t. leads other than those carrying r.f. must be screened. In each case the metal screening must be exposed and wherever leads cross one another or run parallel for more than 3 or 4 in., they should be bound together with a few turns of tinned copper wire and soldered and bonded to the chassis. The modulator section clamper wiring, and bias supplies should also be screened and decoupled with dise ceramic conden-


Fig. 4: Above-chassis layout of the major components.

MATERIALS FOR CHASSIS, PANEL, ETC. Rack panel, $19 \times 10 \mathrm{in}$., black crackle finish Chassis, $16 \times 9 \times 2 \frac{1}{2} \mathrm{in}$.
Chassis bottom cover, $16 \times 9 \mathrm{in}$.
Boxfor v.f.o., $4 \times 3 \times 2 \frac{1}{2}$ in.
V.F.O. box side cover, $4 \times 3 \mathrm{in}$.

All the above materials may be obtained from H. L. Smith \& Co. Ltd. as standard ready-made items.
Two p.a. box side covers, $8 \frac{3}{4} \times 5 \frac{3}{4}$ in. with $\frac{1}{2}$ in. flange.
P.A. box rear and front panels, $6 \frac{1}{2} \times 5 \frac{3}{4} \mathrm{i}$.
P.A. box top cover, $8 \frac{3}{4} \times 6 \frac{1}{2}$ in. expanded aluminium.
$32 \times \frac{1}{2} \mathrm{in}$. angle aluminium for top cover.
sers where indicated
When mounting the v.f.o. box on the chassis. care should be taken to see that the feed-through capacitors should be well clear of the holes drilled through the chassis, avoiding any possibility of short circuits or ineffectiveness of the condensers. Before any wiring is attempted, all holes indicated should be drilled in the front, rear, and top of the chassis. To avoid confusion, a Belling type of coaxial socket is used for the microphone. an Igranic socket for the key and ordinary banana-plug type of sockets for the station change-over relay connections. A Bulgin 5-way socket is used for the h.t. and 1.t. connection to the power supply, there being ample spacing across the pins to wire in the r.f. decoupling chokes and condensers.


Fig. 5: Design for the front panel of the "Buccaneer".


The completed chassis of the "Buccaneer".

When assembling the p.a. stage, a small circular screen 3 in. high and $2 \frac{1}{2}$ in. diameter should be affixed to the chassis with the valve-holder screws. In the writer's case. this is a small aluminium can. obtained for the asking from the local chemist's shop. and used for the bulk packaging of tablets. The metal frames of the variable capacitors in the pi-network and that of the harmonic trap should be bonded together with copper braid or 16 s.w.g. copper wire, and earthed to the chassis, as close to the cathode connection of the 807 as possible. Likewise, the 807 heater choke and decoupling capacitors should be soldered directly to the valve socket by the shortest lead possible.

## Tuning Up Procedure

The v.f.o. should first be set to cover the bands as required. By using the bandset condenser and

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the dust core of the inductance, some degree of variation is obtained in the bandspread coverage of the 15 pF capacitor, TC1.
When satisfied with the coverage, the exciter bandswitch should be set to $3.5 \mathrm{Mc} / \mathrm{s}$ and the main h.t. rail switched off. The drive control should be set at two-thirds open and key depressed. Some drive may be immediately apparent on the p.a.


Fig. 6: The receiver muting and antenna change-over switching circuit.
grid current meter, but whether or not current is indicated, the first trimmer on the multiplier, that is, the one immediately behind the panel, should be peaked up for maximum drive. These adjustments to the wide band multiplier unit should only be made with reference to the manufacturers'
details supplied with the unit. Reduce the level of the drive control by stages should the meter be overloaded. The v.f.o. should be set at $3.5 \mathrm{Mc} / \mathrm{s}$ for this adjustment. When satisfied that the first trimmer is peaked at maximum, the v.f.o. should be tuned to the h.f. end of the band and the trimming procedure repeated, this time using the other trimmer. Now, should the drive fall off badly to one end or the other, further trimming should be carried out. The final adjustment should be carried out on the v.f.o. output capacitor TC2, situated at the rear of the v.f.o. box. As the latter is brought into resonarice, it will be observed that the strength of the v.f.o. signal in the station receiver will decrease, allowing the oscillator to be left running all the time without hampering reception.
The other bands are then set up in turn, using the trimmers for $7 \mathrm{Mc} / \mathrm{s}$ and $14 \mathrm{Mc} / \mathrm{s}$, etc., until all bands have been adjusted and drive is fairly linear across them. Final peaking adjustments can be carried out on these bonds with the Philips trimmers underneath the chassis. It is only necessary to obtain around 4 mA with the drive control at maximum, to get more than sufficient power to drive the 807 to full input. In practice it is found that 1.5 mA is ample when running at 90W input on phone and c.w. For phone operation the t.x. is adjusted in the c.w. position first, then the switch turned to the other mode, also, the input level control should be adjusted to give approximately 12 mA standing anode current in the p.a. Using the mike gain control and speaking normally it should be adjusted until the anode current peaks reach the same level as when the key is pressed in the c.w. mode. The key is bypassed with a switch, so that it can be left in circuit if so desired.

The relay-control switching, shown in Fig. 6, is self-explanatory. Care should be taken to obtain a relay with reasonably wide spacing for the antenna change-over. Send-receive switching is a joy to use with just the one control to change over the antenna, mute the receiver, allow monitoring. and keep a snappy QSO going without the use of too many hands.

## Amateur Band DX by G3JDG

Top Band has been particularly disappointing. At one session only two stations were audible: G3SCP (RST599) and G3SVV (459) both calling CQ.

Eighty Metres has been rather "quiet" although some DX has appeared. Mostly Europeans in evidence, SM, DJ, OK, etc., and, of course, the usual G sideband net up the h.f. end discussing everything from rhombics to rhinoceros.

Forty Metres proves by far the noisiest band of the bunch and at times almost bedlam. The i.f. segment has been a hive (literally) of activity, but phone stations seem to be harder to find these days. For those who can stick at it the stations are there in amongst the noise, the commercials. and the many strange squeaks and whistles peculiar to the $7 \cdot 7 \cdot 1 \mathrm{Mc} / \mathrm{s}$ portion of the short-wave bands.

Twenty Metres is by far the best DX band at the moment in spite of its annoying habit of fading out for a time. On July 28 th 13 countries were heard in 14 minutes from $21 \cdot 27$ to $21 \cdot 41$ hrs. All Europe was in full swing: UT5, YO F2, I1, OE, ${ }_{579}$ DI, LZ, OH, UB5, UAI, DM, average report wa" 579. In the h.f. sector the "W's" were roaring in averaging 5 and 7 to 8 and easily readable in spite of the QRM and slight QSB. All these on an odd piece of wire for an aerial and no matching ATU.
Fifteen Metres rather dead and neglected. Rumours of exotic DX breaking through may well be true but they were not audible to your scribe. Anyone else hear anything on this band??
Ten Metres-Reputed to be dead as the proverbial Dodo-sunspot cycle at its lowest-waste of time-" Lucky if you hear a " G ". Friends you have been misied! Sunday morning 26.7.64 from 1030 to $1400 \mathrm{hrs}-\mathrm{OK}$. UA3. OKI. SP8. DJ8, DI. 7, G3. LA8, DM3/P, OZ5. EI, HB9 and GM. ALL ON AM PHONE. Clearly there's life in the band and no doubt SWL reports would be appreciated.


ACTON. BRENTFORD AND CHISWICK RADIO CLUB Hon. Sec.: W. G. Dyer, 3GEH, 188 Gunnersbury Avenue, London, W. 3.

At the September meating of this society, to be held on the 22nd, G3IGM will be giving a talk entitled "Application of Theory to Practice".

## BRADFORD RADIO SOCIETY

Hon. Sec: E. G. Barker, G3OTO. 63 Woodeot Avenua, Baildon, Nr. Shipley, Yorkshire.

Mombers of this sociecy who attended the August meeting on the 18th. heard a lecture on "Civil Defence".
The first meeting in September was on the Ist and was an informal evening.

## CHESHUNT AND DISTRICT RADIO CLUB

J. V. Beavan. G3GBL, 41 Albury Ride, Cheshunt, Hertfordshire.

This society meets on the first Friday of each month at the Civil Defance Centre, Turners Hill. Cheshunt. The mootings begin at 7.30 p.m. when visitors and prospective members will be welcomed.

On August 7th the Club met to hear a tape recorded lecture on test gear and other subjects.
This Saturday-Sth September-Club members will be operating a demonstration station in the playing field at Goffs Lane, Cheshunt, under the call-sign GB3CRC. Visitors to the site will be welcomed by the members and all communieations will be by telephony to ereate more interest for the less technical amongst them. The station will be on the air from $11.30 \mathrm{a} . \mathrm{m}$. to dusk on 160 and 80 m .
CHESTER AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec: P. J. Holland, Field House, 19 Kingaley Road, Gt. Boughton, Chester, Cheshire.
After the activity of Net Night held at the beginning of August, members settlad down to open discussion on the Ilth. An open night on the 18th once again provided the opportunity for quite a ragchew amongst members.

## CLIFTON AMATEUR RADIO SOCIETY

Hon. Sec. I. Rose, G3OGE, 63 Broomfield Road, Beckenham, Kent.

Recent additions and alterations to the Club's aerial array have made it possible to increase activity on $144 \mathrm{Mc} / \mathrm{s}$. and 70 cm .
On Auguse 16 th, members cook part in the second $3.5 \mathrm{Mc} / \mathrm{s}$. d.f. contest.

## DERBY AND DISTRICT AMATEUR RADIO SOCIETY

 Hon. Sec.: F. C. Ward, G2CVV, 5 Uplands Avenue, Littleover, Derby.This Soriery's mobile rally which is hold annually at Rykneld School, went off successfully on August 16th after preparations had been finalised a few days before at a meeting on the 12 th .

## GUILDFORD AND DISTRICT RADIO SOCIETY

Hon. Sec.: D. H. Mead, G3OX1, 41 Egley Road, Woking, Surpy.

Chobham Common was the venue for a group of members of this Society working portable gear on August 2 lst. At the meeting on the 2ath, members discussed plans for the demonstration station they are manning at chis year': Guildford Town Show, baing held the following weekend.

## NORFOLK AMATEUR RADIO CLUB

Hon. Sec.: A. W. Preece, G3TCO, School of Biological Sciences, Wilberforce Road, Norwich, NOR 77H.
Since its inception In January this year, membership of this society has risen to nearly 40 with Club activities likewise inereasing. Recently a regular series of lectures has begun, to be followed by R.A.E. classes and morse practice sessions.

New mombers will of course be welcomed at any of the meatings held each Monday, beginning at 8 p.m.
NORTHERN HEIGHTS AMATEUR RADIO SOCIETY Hon. Sec.: A. Robinson, G3MDW, Candy Cabin, Ogden, Halifax, Yorkshire.

Members of this Sociecy provided two demonstration stations during Augues, one being the Halifax Agricultural Show held

on the Sth, and the other at Crossleys Carpets Gala held on the ISth. On the l6th of the month, a group of members paid a visit to the radio telescope station at Jodrall Bank. Cheshire.
August ended with a ragehew night on the 19th, with no more elub activities until September 2nd, when Northern Heights A.R.S. played host to members of the Manchester Radio Society at a Pea and Pie Supper

READING AMATEUR RADIO CLUB
Hon. Sec.: R. G. Nash, G3EJA, "Peacehaven." 9 Holybrook Road, Reading, Berkshire.

The Club met on August 29th to hear several members describe various pieces of ancillary equipment made by them for use with typical transmitter rigs.

## WEST KENT AMATEUR RADIO SOCIETY

Hon. Sec.: H. F. Richards, 17 Reynolds Lane, Tunbridge Wells, Kent.

The main event of this Sociery during August proved to be a very enjoyable one for all who attended. It was held on August 30th and was in fact, a pienic at Sussex's Sheffiold Park.

## COURSES OF INSTRUCTION

## BIRKENHEAD TECHNICAL COLLEGE

It is expected that an R.A.E. course will be run ar this college on Thursday evenings. Enquiries for membership can be made either to the college or to $A$ Seed, 31 Withert Avenue, Bebington, Wirral, Cheshire.

## BRENTFORD EVENING INSTITUTE

Several courses of interest to the radio enthusiast are being run by this Institute this aurumn, including R.A.E. and morse. Enrolment for any of the classes may be made between 14th to 17th September at the Brentford Evening Institute. Clifden Road, Brentford, Middiesex.

## CENTRAL EVENING INSTITUTE

R.A.E. classes are being held at the Lea Mason Centre of the Central Evening Institute in Birmingham, starting on 14th September. Enrolment week commences 7th September.

## EAST HAM TECHNICAL COLLEGE

An R.A.E. course will begin at the East Ham Technical College, High Street South, London, E.6, on 2 lsc September. Candidates should enroll on the 14 th, 15th or 16th September.

## NORTHSIDE SCHOOL

On 2 /si September, an R.A.E. course begins at Northside School, Percy Road, Finchley, London, N.12. Morse instruction will also be given later in che course. Enrolment for the course can be made between 14 th and 17 th September,

## WEMBLEY EVENING INSTITUTE

At the Copland School of this Institute in Wembley High Road, R.A.E. classes will be held from $2 l$ st September. Enrolments will be accepted between 14th and 17th September.

## WESLEY EVENING INSTITUTE

A radio and television course will begin at this Institute on 21st September. Enrolment can be made at the Institute in Wesley Road, London, N.W.10, between 14th and 18th September

## AUDIO OSCILLATOR DESIGN

We wish to point out that the article "Audio Oscillator Decign ", which appeared in the August 1964 issue of Practical Wireless, was based on a chapter of the Mullard Reference Manual of Transistor Circuits, published by Mullard Limited.

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## AMERICAN LITERATURE

S
IR,-Recent issues of your journal have, more often than not, included a page of book reviews, and this, in my opinion, well reflects the state of the book market which is currently being flooded by technical publications both from home and abroad.

Many of the imported books come from the U.S.A. and while any additions to the amount of technical literature available is to be welcomed. much of the value of these books might be lost by an unwary reader in this country who does not allow for the very real language differences to be encountered in works of American origin. When reading books from the U.S.A. dealing with radio and electronics, I find it necessary to accustom myself to substitute automatically "earth" for " ground ", "anode" for "plate", etc., for to stop, think and translate every unfamiliar term as it occurred in the text would be disastrous for any reader trying to absorb the contents.

There is then, I suggest, a strong case for making available information to explain and clarify these differences, a sort of English/ American dictionary. It is probably true that English versions of technical works originally written in French, German or Russian suffer less from these difficulties than American books, as translators of foreign language books are aware of English expressions and take this into account, whereas books which come from the United States are left "raw" because officially both countries use the same language.

If it were just a matter of substituting one word for another, there would be little to worry about; however, very often the whole approach to a piece of theory differs in the U.S.A. and even circuit diagrams and symbols have a peculiar and confusing appearance to the British reader.James Goodwin (Scarborough, Yorkshire).

## PAST ISSUES OF P. W.

SIIR,-With reference to your "Sell or Loan" column, I have available every copy of Practical Wireless from 1950 to 1962, also every copy of Practical Television from No. 1 to 1962, and I am willing to give any of these issues, free of charge, to anyone who cares to write, enclosing postage sufficient to cover any issues they require, This is a genuine offer now that I find I am forced to dispose of these magazines as they take up more space than I can afford.--I. F. Hitchicock (86 Reigate Avenue, Sutton, Surrey).

Whilst we are always pleased to assist readera with their technical difficulties, we regret that we are unable to suppiy diagrams or provide instructions for modifying commercia or surplus equipment. We cannot supply alternative detail for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVER THE TELE PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of the cover.
The Editor does not necessarily agree with the opinions expressed by his correspondents.

## TRANSISTOR PREAMP

SR,-Regarding the Transistor Preamp on page 358 of the August issue of Practical Wireless. When used with the power supply unit for a valve amplifier (Fig. 3) the output should be laken from C4 and the negative line. This will avoid having a potential difference between the preamp output and valve amplifier input circuits. The input circuits should be isolated by a $25 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic in series with the + ve lead to the volume control and input sockets (negative to VR1 and sockets). This will prevent d.c. from reaching the tuners and gram p.u. if they are earthed to the amplifier chassis.

I would also like to correspond with any radio enthusiasts of my own age (13).-Alan Campbell (30 Barnsdale Road, St. Ninians, Stirling, Scotland).

## POCKET SIGNAL INJECTOR

SIR,-It would be interesting to know the variety of containers used by your readers to make the Pocket Signal Injector and also the Signal Tracer when they found that the specified pencil torches were in short supply. I see that in your August issue Mr. Raymond Cruise used a film cassette tin. Myself I turned to the little clear plastic boxes in which "Desogen" throat tablets are packed. They measure 3 in. $x 1 \frac{1}{2}$ in. $x \frac{1}{2}$ in., will contain a U16 1.5 V battery, but with difficulty, or Mallory cells very easily, and have the advantage that they do not need insulating for a.c./d.c. work. They enabled me to make neat jobs of both the Injector and the Tracer with which I am very satisfied. The printing on the boxes can be removed with metal polish and elbow grease!

Making the probe from 2B.A. threaded rod with a hand drill is by no means child's play. Unless the rod is supported very little filing effect is obtained from a file held on the rod and the file cannot be controlled and prevented from slipping all over the place. I found that I had to nail a thick block of soft wood to my bench and fix the hand drill in the vice so that the 2B.A. rod in the chuck lay flat on this block. Then I drove a goodsized staple into the block so that I could put the point of my file into it and utilise it to get pressure on the rod. Even then I found the file tended to be dragged into the staple so that it jammed and lateral movement of it was impossible. This meant another nail in the block for a file stop to prevent the jamming. Another nail near where the rod entered the chuck jaws
acted as a lateral stop and completed this Heath Robinson rig. After all this I had no difficulty in finishing two nicely tapered probes. I hope other readers will find this tip helpful for both of these neat and extremely useful instruments.-R. S. Welford (Sunbury-on-Thames, Surrey).

## SHAKE-PROOF WASHERS

SIR,-No one these days seems to know what the shake-proof washers on such things as potentiometers and air-spaced condensers are for.

They are supplied to prevent the whole component from turning when heavy-handed people twist the knob; not to prevent the screw from turning. Therefore the washer should be fitted to the spindle of the component before it is fitted to its chassis.

It is true that some of these types of components are fitted with positioning lugs, in which case the washer should be placed on the same side of the chassis as the locknut.-A. Martin (London, S.W.19).

## THE IMPORTANCE OF THE RAE

SIR,-While I am in favour of commercial broadcasting and think the BBC monopoly ought to be broken, I think the comments of W. Jenkins and A. Sidi, on Thermion's Caroline views should be put into proportion.

I would like to say that Caroline's operation outside Territorial Waters is merely a protest to the Postmaster General for his refusal to issue commercial broadcasting licences, and is not an advocate for the issue of licences to unqualified operators such as we would have in a "Citizen Band". The RAE is not an electronic wizard's examination. It merely tests one's knowledge of basic radio theory, and most important, the necessary knowledge to deal with any interference which may result from the operation of one's station.

If Mr. Jenkins or Mr. Sidi cannot be bothered to learn these few basic facts, then I suggest they try some other hobby. I can just imagine the answer they would give to their irate TVI-prone neighbours, to say nothing of the model enthusiast from down the street who has just lost a beautiful radio controlled plane. I should imagine it would be something to this effect, "Sorry mate, I don't know a thing about radio, I just operate it for fun ".A. Marnard, b.r.s. 26128 (Bognor Regis, Sussex).
(We endorse Mr. Maynard's remarks concerning the R.A.E.. The amateur transmitting licence is not a barrier to the real enthusiast. Readers interested in obtaining their "ticket" will find something of interest in the next issue-Editor.)

## Sir-l would be grateful if any reader could sell or loon me . . .

. . following issues of P.W.: Dec. 1961, Jant., Feb., Mar., Apl., May 1962, and Jan. 1963. I will pay full price for all copies in good condition.-J. J. BowYer, 2 Chichester Street, Chester.
. . . the circuit and booklet of Marconi Communications Receiver CR100.-WAH KHAI LiANG, Department of Radio, Radio Malasia, Penang, Malasia.

18 Green Park, Witton Lawn, Cork, Irish Republic. Tangney, ... the circuit and servicing data for the Deffant AF7.-R. W. Sheppard, 97 Hermitage Woods Crescent, St. John's, Woking, Surrey.
circuit diagram and any other information regarding the PCR3 receiver.-B. GIBSON (ZS2PG), 69 Firt A venue, Newton Park, Port Elizabeth, S. Africa.
W . . . details or handbook on the Lavoie Laboratory Micro Wave Frequency Meter Model 105SM Serial 2876, covering 375 to $725 \mathrm{Mc} / \mathrm{s}$. -F. B. Blake, 2 Fair View, School Lane, Seer Green, Beaconsfield, Buckinghamshire.
. . circuit or manual on the Super Skyrider Hallicrafter SX 16, also the data for the D.B. 20 Preselector,-R McLachlan, 66 Haigh St., Halifax, Yorkshire.
. $18^{\circ}$ circuit diapram and manual for Hallicrafter receiver SX 28 , and a circuit of about 60 W c.w./phone v.f.o. transmitter with a suitable s.s.b. adaptor for the same. I shall arrange payment through a friend in U.K-S. L. ANAND 3066/SA Street No. 10, Ranjit Nagar, New Delhi -12, India.
test instructions for Hansen Multimeter, Model T.S.-J. DunNett, 7 Lorne House, Kinlochleven, Argyll.
... the handbook, circuit or any other data on the R1132A communications receiver.-F. H. LADD, 4 Wellington Close, Meibourne Park, Chelmsford, Essex.

E, 45 the manual of the R. 107 ser ZA 3050.-B. Catchpole, 45 Balmoral Drive, Borehamwood, Hertfordshire. Ex.Government $\mathbf{R x} / T \mathbf{x}$ Model $3 / 11$ (also known as B11). -A. Parkin, 9 Dawsons Rough. Shawbury, Shropshire.
. . . circuit or any information as to the connections of the 12 pole outlet socket of the 38 a.f.v. transceiver.-D. K. Cooper. c/o R.E.C. \& Co., Lefkara, Cyprus.
list of valves or the circuit diagram for Philips Receiver, Type BX 516 A/10.-C. K. Ocran, P.O. Box 205 Takoradi, Ghana.
_S. Saether~․ . Roberg, Tonsberg, Norway.
any aerial details or the circuit for Communications Receiver P.C.R.3.-A. Gargett, 30 Dryden Road, West Cliff Est., Scunthorpe.
Tape Recorder.-. . Any information on the Roding Transportable don, Essex.
Presto . . . circuit and any other details of a Crosley Prestotune set.-J. Smart-Okuoka, 7 St. George's Road, Coventry.
the August 1962 issue of Practical Wireless. - J. B. White, i Lansdown Place West, Bath, Somerset.
issues of Practical Wireless dealing with modifications to the R109 A receiver.-T. R. SmITh, 50 b Aldershot Road, Guildford, Surrey.
circuit diagram and component values for the Ekco Car Radio CR61/A.-P. HEARNE, 1 Derwent Close, Gossops Green, Crawley, Sussex.

## CATALOGUE RECEIVED

MIESSRS. Henry's Radio have recently published a new 1964 edition of their comprehensive catalogue. It comprises 86 pages and is fully illustrated, covering a very wide range of electronic components.

Cadmium sun-cells, crystal owens. dosimeters, deccatrons, printed circuit etching kits. ferrite pot cores, geiger tubes, gamma probes and mercury cells, are but a few of the items listed.

A wide range of transistors and associated components are included, plus a transistor equivalent chart and connection details.

It is a well-produced book and much thought obviously has been given to its preparation. The price is 2 s . 6 d . post free and copies may be obtained from Messrs. Henry's Radio Lid., 303 Edgware Road, London, W.2.


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## SOME EARLIER DESIGNS

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