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# All Valves Brand New and Fully Guaranteed - Obsolete valves a speciality. 

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| AC2/P | $21 \%$ | ECC85 | $\begin{array}{r} 716 \\ 12 / 6 \end{array}$ | $\begin{array}{cc} \text { EY83 } & 1218 \\ \text { EY86 } & 7! \end{array}$ | $\begin{array}{ll} \text { PCC84 } & 816 \\ \text { PCC85 } & 916 \end{array}$ | TDDI3C ${ }_{17 / 6}$ | UU9 $7 / 6$ <br> UYIN 12.6 | 6AK8 | $\begin{aligned} & 716 \\ & 410 \end{aligned}$ | $\begin{aligned} & 6 P 28 \\ & 6 Q 7 \end{aligned}$ | $\begin{array}{r} 12 / 6 \\ 9 / 6 \end{array}$ | $\begin{aligned} & 12 S J 7 \\ & 12 S K 7 \end{aligned}$ | $\begin{aligned} & 81 . \\ & 6 \% \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AC2/P |  | ECC91 | $3 /$. | EY91 31. | PCC88 1216 | TH41 2716 | UY2I 1516 | 6AM5 | 5\%. | 6Q76 | 616 | $12 \mathrm{SL7}$ | 8\% |
| DD | 21\% | ECF80 | 716 | EZ35 61. | PCC89 816 | TY86F 1216 | UY41 716 | 6AM6 | 41. | 6Q7GT | 816 | 12SN7 | 101 |
| AC/TP | 321. | ECF82 | 816 | EZ40 7\% | PCF80 91. | U10 91. | UY85 7\% | 6AQ5 | 816 | 6SA7 | 71. | 12 SQ 7 | 816 |
| AC/VP | -5-7 | ECH3 | 2116 | EZ41 71. | PCF82 71. | U12 9\% | VMS4B 1216 | 6A | $9 / 3$ | 6SC7 | 816 | $14 \mathrm{H7}$ | $0 \%$ |
|  | $17 / 8$ | ECH2I | 21\% | EZ80 616 | PCF84 1216 | U14 91. | VP4 15/. | 6 AT6 | $6 \%$ | 6SF5 | 10\% | $14 \mathrm{R7}$ | 1016 |
| AZI | 15\%. | ECH35 | 101/ | EZ81 616 | PCF86 12's | U22 81- | VP4A 15\% | 6AU6 | 91. | 6SG7 | 71. | 1457 | 16\% |
| AZ31 | 10\% | ECH42 | 916 | EZ93 71. | CL82 91. | U24 21\% | VP4B 151. | 6B8G | 31. | 6 SH 7 | 61. | $19 \mathrm{AQ5}$ | 81/ |
| B36 | 91. | ECH81 | 81. | Ell48 2\%- | PCL83 11/6 | U25 12'6 | VR105/3071. | 6BA6 | $6 \%$ | 6SJ7 | 616 | 19 B | 51. |
| CIC | $10 \%$ | ECH83 | 816 | FC2 15\% | PCL84 1016 | U26 1216 | VR150/307\% | 6BE6 | 61. | 6SK7 | 516 | 2001 | $10 \%$ |
| CBL3I | 2116 | ECL80 | $8 \%$ | FC2A 1716 | PCL85 1016 | U31 91. | W61 IIt | 6BG6G | 151. | 6SL7GT | 61. | 2002 | 211. |
| CCH35 | 2110 | ECL81 | 10\% | FC4 151. | $\begin{array}{ll}\text { PCL86 } & 12 / 6\end{array}$ | U35 17'6 | W76 5\% | 6BH6 | 81. | 6SN7GT | 516 | 20 F 2 | 1716 |
| CL33 | 15\% | ECL82 | 916 | FCl3 15\% | PENA4 1716 | U37 17'6 | W77 4\% | 6BJ6 | 61. | 65Q7 | 816 | 20 LI | 24\% |
| CYI | $15 \%$ | ECL83 | 1076 | FCI3C 17/6 | ENB4 17/6 | U43 8'6 | W81 6\% | 6BQ7A | 1216 | $6 \cup 4 G T$ | 101. | 20P1 | 15\% |
| CY31 | 151. | ECL86 | 1016 | FW4/500 91. | N4DD | U47 12'6 | W8IM 6\% | 6BR7 | 1016 | 6U5G | 716 | 20P3 | 24. |
| D77 | 41. | EF6 | 211. | FW4/800 91- | $24 /$ | $\cup 50 \quad 7{ }^{\prime}$ - | $\times 41$ 15\% | 6BS7 | 12/6 | 6V6G | 416 | 20P4 | 2316 |
| DAC32 | 916 | EF9 | 2116 | GZ30 1016 | PEN4VA | U52 4' | $\times 61 \mathrm{M}$ 10\% | 6BW6 | 81. | 6V6GT | 81. | 20P5 | 24/m. |
| DAF91 | 616 | EF22 | 141. | GZ32 1016 | 1776 | U76 7'6 | $\times 65 \quad 1216$ | 6BW7. | 51. | $6 \times 4$ | 416 | 25A6 | 8/- |
| DAF96 | 81. | EF36 | 41. | GZ33 1913 | PEN36C 20\% | U78 4 4'6 | $\times 76 \quad 1216$ | $6 \mathrm{C4} 4$ | 316 | $6 \times 5 \mathrm{G}$ | 61. | 25L6 | $8 \prime$ |
| DCC90 | 1216 | EF37 | 81. | GZ34 13/6 | PEN45 10\% | U145 10'6 | $\times 76 \mathrm{M} \quad 1216$ | 6C5GT | 81. | $6 \times 5 \mathrm{GT}$ | 816 | 25Y5 | 81 |
| DF33 | $10 \%$ | EF37A | $8 \%$ | GZ37 19/3 | EN45DD | U191 15'6 | $\times 78$ 241- | 6C6 | 616 | $6 / 30 \mathrm{~L} 2$ | 101. | 25Y5G | 81. |
| DF91 | 4/2. | EF39 | 4\% | HABC8610\% | 25 | U251 15.6 | $\times 794216$ | 6C9 | 1276 | $7 \mathrm{B5}$ | 1216 | 25Z4 | 716 |
| DF92 | $7 / 2$ | EF40 | 15t. | HL41 8/. | PEN46 5\% | U281 15' | $\times 81$ 10\% | 6CD6G | $27 / 6$ | 786 | 1015 | 25Z5 : | $81-$ |
| DF96 | 81. | EF41 | 81. | HL4IDD $8 / 6$ | 3DD | U282 19'6 | Y61 10\% | 6 CH 6 | 10\% | 787 | 816 | 25Z6 | $8 / 6$ |
| DF97 | 1176 612 | EF42 | 1018 | $\mathrm{HL92}^{\text {HL/6 }}$ | 20\% | U301 $22^{\prime \prime} 6$ | Y63 101. | 6D2 | 4/2 | $7 \mathrm{C5}$ | $81 /$ | $275 \cup$ | $19 / 6$ |
| $\begin{aligned} & \text { DH63 } \\ & \text { DH77 } \end{aligned}$ | $6 /$. | EF50A | 316 | HLI33DD | PENDD4020 | U329 12'6 | Z63 716 | 6D6 | 516 | $7 \mathrm{C6}$ | 816 | 30 Cl | 916 |
| DK32 | 1116 | EF80 | 51. | HN309 2616 | 201. | U403 101. | Z77 4! | 6 FI | 10\% | 7 D 5 | 1. | 30 C 15 | 216 |
| DK91 | 713 | EF85 | 51. | IW4/350101. | $\begin{array}{ll}\text { PL33 } & \text { 1512 } \\ \text { PL } 36 & 1216\end{array}$ | U404 101. | Z152 5\% | 6 F 6 | 619 | 7D8 | 15\% | L | 1016 |
| DK92 | 816 | EF86 | 91. | $1 W 4 / 50010 /=$ | PL38 211 | $\cup 801$ 1919 | OZ4 5\% | 6 F 12 | 4\% | 7H7 | $7 / 6$ | 30LI | 816 |
| DK96 | 816 | EF89 | 9\% | KT33C 81- | $\begin{array}{ll}\text { PL38 } & 211 \\ \text { PL81 } \\ \text { PL }\end{array}$ | $\cup A B C 8071$. | 1 A 71116 | 6F13 | $10 \%$ | $7 \mathrm{R7}$ | 1010 | 30 LI 15 | 1116 |
| DL33 | 816 | EF91 | 41. | KT36 1716 | $\begin{array}{lr}\text { PL81 } & 116 \\ \text { PL82 } & 8 / 2\end{array}$ | UAF42 816 | $1 C 51016$ | 6 FI 4 | $10 \%$ | 757 | 101. | 30 P 4 | 201. |
| DL35 | 1016 | EF92 | 41. | $\begin{array}{ll}\text { KT55 } & 1716\end{array}$ | PL82 8\% | UB41 716 | 1058 | 6 F15 | 1216 | 7Y4 | 718 | 30 PI 2 | $10 \%$ |
| DL91 | 810 | EF95 | 5\% | $\begin{array}{ll}\text { KT61 } & 916\end{array}$ | $\begin{array}{rr}\text { PL83 } & 1076 \\ \text { PL84 } & 816\end{array}$ | $\cup B C 41816$ | ID6 101. | 6 F 19 | 1216 | 8D3 | 416 | 30 PI 16 | $9 \%$ |
| DL92 | 616 | EF93 | 1018 | KT66 15\% | $\begin{array}{lr}\text { PL84 } & 816 \\ \text { PL820 } & 1816\end{array}$ | $\cup B C 81$ I01- | $1 H 5916$ | $6 F 23$ | $10 / 6$ | 9 BW 6 | 1216 | 30P19 | $21 \%$ |
| DL93 | 710 | EFI83 | 1016 | KT76 101- | $\begin{array}{ll}\text { PL820 } & 18 / 6 \\ \text { PM24M } & 1316\end{array}$ | UBF80 816 | IL4 51. | 6 F 25 | 1616 | 10 Cl | 1216 | 30 PLI | 15! |
| DL94 | 716 | EF184 | 1016 | KT部 15\% |  | UBF89 716 | ILN5 416 | $6 F 26$ | 1316 | 10C2 | 1716 | 30PLI 3 | 1216 |
| DL96 | 810 | EK32 | 88 | KTW61 8i- | PX25 25\% | UBL21 20\% | IN5 916 | $6 F 33$ | 516 | 10FI | 10\% | 30PL14 | 1816 |
| EA50 | 21. | EL2 | 2516 | L63 51- | $\begin{array}{ll}\text { PX25 } & 25 \% \\ \text { PY31 } & 151\end{array}$ | UCC84 1016 | IR5 713 | $6 \mathrm{H}_{6}$ | $2 \%$ | 10 F 3 | 1216 | 35 A5 | 1716 |
| EABC80 | 51. | EL3 | 2116 | LNI52 81. | $\begin{array}{lr}\text { PY31 } & 1512 \\ \text { PY } 32 & 1216\end{array}$ | UCCB5 716 | 154 8\% | 615 | 516 | 10F9 | 1216 | 35L6GT | 816 |
| EAC91 | 41. | EL6 | 211. | LN309 1116 | 3312 | UCF80 $13 / 6$ | 155 | 615 G | 416 | 10LDI1 | 15\% | 35 W 4 | 716 |
|  | $9 / 6$ | EL32 | 416 | LZ319 1216 | $\begin{array}{lr}\text { PYY3 } & 1216 \\ \text { PY } & 716\end{array}$ | UCH21 2015 | $1 \mathrm{l} 4{ }^{1}$ | 6.J5GT | $51 /$ | 10P13 | 15\% | $35 Z 3$ 。 | 1616 |
|  | 216 |  |  | MKT4 1716 | $\begin{array}{ll}\text { PYY81 } & 716\end{array}$ | H42 9/6 | IU5 519 | 617 | 716 | 10 Pl 14 | 191\% | 35 Z4 | 716 |
|  |  |  |  | MS4B I716 | PY82 7\% | $\begin{array}{rr}\text { UCH81 } \\ \text { UCL82 } & 810\end{array}$ | 2419 | $6 J 7 \mathrm{G}$ | 5\% | 1105 | 2316 | 3575. | 816 |
| EBC3 | 211. | EL37 | 1716 | $17 / 6$ | PY83 8\% | $\begin{array}{ll}\text { UCL82 } & 101 \\ \text { UCL83 } & 1315\end{array}$ | $\begin{array}{rr}3 A 4 & 51 / \\ 3 A 5 & 1016\end{array}$ | 617 G $6 \mathrm{K7}$ | 716 | 12 A 6 | 616 | 40SUA | 51. |
| EBC33 | 4/8 | EL33 | 1916 | MVS/PENB | 38 101. | UF41 716 | 304 8\% | 6 K 7 G | $2 \%$ | 12AT6 | $7 / 6$ | $42$ | $12 / 6$ |
| EBC41 | 816 | EL4I | 10\% | 1716 | $30010 \%$ | UF42 715 | 3Q3 91. | 6 K 7 G | 716 | 12 AT7 | 51. | 50 C 5 | $10 \%$ |
| EBCB1 | 101. | EL42 | 101. | MUl4 9\% | PZ30 151- | UF33 71. | 354 7\% | 6 K 8 | 916 | $12 \mathrm{~A} \mathrm{l}^{\text {a }}$ | 1716 | 50CD6 | 2716 |
| EBF30 | 816 | EL81 | $12 / 6$ | M $\times 40 \quad 15 /$. | Q5150115 | UF85 715 | $3 \vee 4$ 7/6 | 6K8G | 51. | $12 \mathrm{AU7}$ | 5\% | SOL6 | $8 / 6$ |
| EBF83 | 816 | EL84 | 619 | N13 81- | QSI50/15 | UF3S 12\% | $5 \cup 4$ 4 | 6K8G | 916 | $12 \mathrm{~A} \times 7$ | 51. | 53KU | 1216 |
| EBF89 | 81. | EL85 | $10 \%$ | N37 14/\% | 10\% | UF89 616 | $5 V 4 \mathrm{G} \quad 719$ | 6K25 | 18\% | $12 \mathrm{BA6}$ | 716 | 75 | 8 F |
| EBLI | 21\% | EL90 | 816 | N78 1716 | R2 10\% | UL41 8\% | $5 Y 36$ 7I. | 6LI | 1015 | 12BE6 | 716 | 78 | $7 / 6$ |
| EBL2I | 21\% | EL91 | 41. | N108 151. | R3 10\% | UL44 20/\% | 5Y3GT 816 | 6L6 | 716 | $12 \mathrm{BH7}$ | $10 \%$ | 80 | 91. |
| EBL31 | $21 / 6$ | EL95 | 1016 | N308 20\% | R16 17/6 | UL46 1416 | 5Z4G 916 | 6 L 7 | $10 \%$ | 12 C 8 | 816 | 85 | 1716 |
| ECC35 | $8 \%$ | EM80 | 816 | N339 30\% | R19 16/. | UL84 71. | 5Z4GT 12/6 |  | \% | 12 JGT | 41. |  |  |
| ECC40 | 15\% | EM81 | 816 | N369 1016 | R20 16\% | UL85 716 | 6A7 91- | 6119 | $10 \%$ | 12 J 7 GT | 816 | 85A2 | 30\% |
| ECC81 | $5 \%$ | EM84 | 916 | OD3 5\% | SP41 316 | UM39 10'6 | 6A3G 816 | $6 \mathrm{LI9}$ | 916 | $12 \mathrm{K7GT}$ | 51. | 185BT | 30\% |
| ECC82 | 51. | EM85 | $10 \%$ | OZ4 516 | SP61 36 | URIC 15\% | 6A3GT 13'5 | 6L34 | 916 | 12K8G | $0 \%$ | 305 | $13 \%$ |
| ECC83 | 716 | EY5I | 816 | P2 10\% | T41 151. | UU6 I! | $6 \mathrm{AC7}$ 6' | 6N7GT | 916 | 12Q7GT | 616 | 807B | $5 \%$ |
| ECC84 | 816 | EYOI | 816 | PABC80 13\%. | T004 12'6 | UUd isfor | $6 A_{i} \leqslant 5 \quad 5 / 2$ | 6P25 | $10 / 6$ | $125 A 7$ | 816 | 807A | 6/2 |


| S |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| RMI | 513 | 14A86 | 1716 | 16RD-2-2-8-1 12'- |
| RM2 | 716 | 14 A 97 | 251. | 16RE 2-1-8-1 816 |
| RM3 | 719 | 14A100 | 271. | 18RA 1-1-8-1 416 |
| RM4 | 14' | I4RA I | 1716 (FC301) | I8RA I-1-16-1 616 ( $\mathrm{FCl\mid 6)}$ |
| RM5 | $19 / 6$ | I4RA | 191-(FC31) | I8RA 1-2-8-1 11' |
|  |  | IGRC I- | 1816 | 18RD 2-2-8-1 15/- (FC124) |

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312 PACKING CHARGE ON ALL C.O.D.
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| OC44OC45 | 61. | OC75 | 61. |  | C82 | 81- |
|  | 71. | OC77 | 61. |  | C82D | 81. |
| OC71 | 51. | OC8। | 61. |  |  |  |
| OC74 | 61. | OC8ID | 61. |  |  |  |
| $400 \text { volt: }$ | SILICON R |  | RECTIFIERS |  |  |  |
|  | ts 350 m | A |  |  |  |  |

## SETS OF VALVES

IR5, IS5, IT4, 3S4, 3V4 ... ... ... Set of 4, 1916
DAF91, DF91, DK91, DL92, DL94 ... Set of 4, 1916
DAF96, DF96, DK96, DL96

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 The popular complete " 5 -10" incorporating Control Unit providing up to 10 watts high quality reproduction. Specified components and new MULLARD VALVES. fncludes PARMEKO MAINS TRANS-FORMERS and cholce of PARMEKO or FORMERS and cholce of PARMEK COMPLETE \&11.10.0 Dep. \&2.6.0
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A HIGH QUALITY AMPLIFIER DEVELOPED FROM THE VERY POPULAR KIT OF PARTS $£ 7.10 .0$ ASSEMBLED
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A six Transistor (plus two Diodes) Portable covering the Medium Waveband. Small enough to slip into Handbar or Pocket ( $4^{\circ} \times 24^{x} \times 1$ )
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For Stereophonic or Monophonic Operation. Beaulifully styled with Finger Tip Conirols. Conslsting of Tape Deek incorporating High Quality Preampliffer. List Price is $£ 94.10 .0$ Deposit $£ 9.18 .8$ and 12 months at $\$ 49.10 .0$ Deposit
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A completely self contained, self powered Unit designed to add full TAPE RECORDING facill-
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MULLARD'S 2-VALVE PRE-AMPLIFIER TONE CONTROL UNIT
Employing two EF86 valves and designed to operate with the Mullard MALN AMPLIFIER but also perfectiy suitable for other
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* Input for Crystal Plck-ups and variable reluctance magnetic types.
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Total cost of complete Kit. $\mathbf{\$ 1 6 . 1 0 . 0}$ carr. CR 66 Cabinet less Cabinet and Indicator
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Signal strength indi-
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## THE NEW CR45 $\star$ NEW STYLING TOP PERFORMANCE



* Tunes $10-2000$ metres (5 Coils).
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$\star$ Miniature I valve, all band receiver,
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HIGH GUALETY In walnut vencered oabinct veneered oabinet. Gause
12,000 lines. Speech 12,000 lines. Speech
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A hichly-sensitive 4 -valve quallty ampllfier for the home, small club, etc. Onyy bit mililvolts lnput is required for full outputso that if ts sultable for use with the tatest himb fidelity piek-ub heads, in adclition to alt other types of pick-ups ind pracuically nll "mikes: separate lass and Treble Controls are providra. These Heve rull long-playing record ediadisation. Rumi level is newhed. used. T. or 300 v . 25 mA . and L . T. or 6.3 v . 1.5 n . is available for the mupply of a Radio Feeder Unit, or $230-250$ v. 50 c/a. Output for $2-3$ ohm speaker. Chassis is not allve. Kit is complete in every detnil and includes fully punched chassis (wlth base plate) with 13 iue
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3 and 15 ohm speakers, Complete K1t of

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Suitable microphones and speakers avallable at competitive prices.

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SUPERHET FEFDER UNIT. Design of a high quality Radio Tuner (spectally suitable for use with our Amplifiers), Delayed A.V./C, Controls are Tuning
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## R.S.C. PORTABLE GUITAR AMP. <br> LIFIERS NOW ON PAGE 883.

AUDIOTRINE HIGH FIDELITY REPRODUCERS THE DUO/10. Consisting of a 12 in .12 .000 line Speaker with heavy four layer volce coll. the Audiotrine oross-over unit. and a 41n. Dlameter Tweeter Unit Incorporated in the extremely attractive Audiotrine Senior Corner Console Oabinet as desorlbed bolow. Matching Impedance 15 ohms. Power handling 10 watts nominal. 14 watts peak. Frequenoy ONLY 2719 and nine montbly pay- 12 Cns.
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impedance 15 ohms. Fre- ONLY quency range $40-15,000$ c.p.s. Power handling 6 watts Inominal Ideal for Stereo.
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Carr. 4/6

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STANDARD MODEL. AS above but for 124. Speakgrs. Sike $20 \times 15 \times 1810$. ESpe claliy recommended for Audlotrine Loud. speaker systems. For vertical or horizontal use, 25.19.6. Sultable legs with brass ferrules, $19 / 6$ per set of 4.

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 TliME. Consjating of matohed 12in. 12,000 line. 15 ohm high quality speaker: cross-over unit (consisting of choke condenser, otc.) and Tweeter. The smooth response and extended irequency range ensure surprising yreaing £4.19.9. Ourr. 5 Standard 10 watt rating £4.19.9, 76 .Or Senior 15 Wa
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Incorporating the latest Collaro Studio Tape Transcriptor. The Audiotrine High Quality Tapo Amplifer with negative feedback equalisation for each of 3 apeeds. High Flux P.M. Speaker, empty Tape Spool, a Reel of Best quality Tape and a Handsome Portable carrying Cabinet with latest attractive two-tone polyohrome finish. size $143 \times 15 \times 8 i \mathrm{in}$. high, and circuit. Total cost if purchased individually approximately £40. Performance equal to units in the f60-880 class. S. A. E, for leaflets. TERMS. Deposit 22.13 .9 and 12 monthly payments of $44 /$-. Cash price if settied in 3 months.

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All for A.C. Mains 200-250v., 50c/s. Guaranteed 12 months.

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| :---: | :---: |
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| Consisting of Mains Transformer |  |
| 0-200-230 |  |
| Solenium Rectifler: Ammeter, |  |
| Variable Charge Rate selector |  |
|  |  |
| and circuit. 59/9. Carr. 4/6. |  |
| CHARGER KIT, 12v. 14 AMP or |  |
| 24 v .7 amp. Consisting of mains trans. |  |
| 200-230-250 \%. F.W. (Bridge) selenium |  |
| Rectifier. F Ammeter, Fuses. Vari- |  |
| $6 \mathrm{gns}$. Carr. 15/-. Please state if 12 v . |  |
|  |  |
| or 24 v . kit required. |  |
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| Watts. First quality. For Radio |  |
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Assembled 4-5 amps. 6/12 v. Fitted Ammeter and selector. Also seleotor selector. Also
plug for
6 charging. Louvred stee] case in stoved blue, hammer finlshed. Fused with mains and $69 / 9$ output leads. Carr $5 /$ 5 monthly payments $13 / 3$. $0 / 12$ v. 3a, all facilities
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ASGEMBLED 12 V .10 Amb with varlable charge rate adiust ment, ammeter and strong louvred, stove enamelled case.

BATTERY CHARGER KITS Consiating of Mains Transformer, F.W. Bridge, Metal Rectifler, well ventiated steel case. H . Groms Cv. or 12 v . 1 amp ............ 22/9 As above, with Ammeter $28 / 8$ 6 v .2 amps .................. $19 / 9$ 6 v . or 12 v .2 amps. 6 v. 12 \& 2 amps iöclu 25/9 sive of Ammeter............ 35/9 6 v . or $12 \mathrm{v}_{\mathrm{i}} 4$ amps $\ldots \ldots \ldots .45 / 9$ Armine 12 V. ${ }^{2}$ amps. wirs rate selector ...............52/8 CHARGER AMMETERS $0-1.5$ a.. $0-3$ a.. $0-4$ a.. $0-7$ a. 0-25 a., 0-60 a., 8/9.

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## Interleaved and Impregnated. Prim-

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 Midget type $24-3-3 \mathrm{in}$. $250-0-250 \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a} .0-5-6.3 \mathrm{v} .3 \mathrm{a} 27 / 9$ $300-0-300 \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 0-5-6.3 \mathrm{v}, 3 \mathrm{a} 2$ la, for Mullara Amplifier
$350-0-350 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a} .5 \mathrm{v}, 3 \mathrm{a} \quad 27 / 11$

FULLY SHROULED (continued)-$425-0-425 v .200 \mathrm{~mA} .8 .3 \mathrm{v}, 4 \mathrm{a}, \mathrm{C}, \mathrm{T}, 5 \mathrm{v} .3 \mathrm{a}$
$425-0-425 \mathrm{v}, 200 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, \mathrm{C} . \mathrm{T}, 3 \mathrm{v}$.
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Midget Battery Pentode $66: 1$ for 354, atc.
Small Pentode. 5000 n to $3 \Omega$
Small Pentode $7 / 8,0000$ to $3 \pi^{\circ}$ Standard Pentode $5,000 \Omega$ to $3 \Omega$ Standard Pentode 7,000 $\Omega$ to $3 \Omega$ $10.000 \Omega$ to $3 \Omega$
ush-Pull 8 watts, ELBi, or 6V6 to Push-pull $10-12$ watts to match 6 V 6 or EL84 to 3-5-8 or $15 \Omega$ Fush-Pull types for 3 and 150 speakers: Push-Pull 10-12 watts 6V6 or EL84 .. 18/9 Push-Pull Mullard 510 Ultra Linear $29 / 9$ wound, 6L6. KT66. EL34, otc. $\quad 49 / 8$

ASSEMBLED $6 / 12$ v. 2 ambos. FItted Ammoter andselector plug tor 68 . or 12 v Louvred metal case finshed attractive hammer beady for Fused, ready and ontput leads
$49 / 9{ }_{3 / 19}^{\text {Carp }}$
6/12v. 1 amp. $27 / 8$
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MIDGET MAINS Primarios 200-250 $V_{\text {, }}$
 Both above size $24 \times 21 \times 2 \frac{1}{2}$ ns FILAMENT TRANSFOR MERS All with $200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$, primaries 6.3 v . 1.5a. 5/9; 6.3 \%. 2a. 7/6; 0-4-6.3 \%. 2a, 7/9: 12 v. 1 a, $7 / 11 ; 6.3$ v. 3 a, 8/11; 6.3 v. 6 a,
$17 / 6 ; 12$ v. 1.5 a. twice. $17 / 6$. 17/6:12 V. 1.5 \& twice, $17 / 6$.

$150 \mathrm{~mA} .7-10 \mathrm{H}$ H 250 ohms
100 mA .10 H 200 Ohms
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$11 / 9$
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All with $200-230-250$ V. $50 \mathrm{c} / \mathrm{s}$ Primaries; 0-9-15 V. 1t a. 12/8; 0-9-16 \%. 2a, 14/9; 0-9-15 6 a. $23 / 9: 0-9-15$ v. 8 \&., $28 / 9$
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SB-10U May be used with most A.M. transmitters. Less than 3W R.F. input power required for 10 W output. Operation on $80,40,20,15$ and 10 m bands on USB, LSB or DSB
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S-99


AM/FM Tuner


TA-IS


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A first-clase 2 waveband transistor superhet in kit form. Printed circuit panel (slze 81 $x$ 2gin.) 3 pre-aldgaed. I.F, transformers. aerial. First-grade $A$ E tranalatora Car aeral trendling. Purall wut eng All with almple instructions.

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24 ln 35 obms speaker, 10/6;
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Two valve. UY85, UL84 O.P. trads., use with 80 volt tap of motor. $38 / 6$. P.P. $2 / 6$ on above. Dropper res. for filuments if required. $2 / 6$.
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$\underset{\text { speaker }}{\text { Goodnans } 10 \mathrm{in} \text {. } x}$ min
E.M.I. $13 \sqrt[3]{\operatorname{jin} .} \mathrm{x}$ Btin. hlgh tlux

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# BDDOSTRUTOTOR LEADS THE WORLD in Electronics training 


 OME readers might feel that this month's cover subject is a little unusual. Without wishing to be facetious, we agree that it strikes a somewhat unusual note and can, in fact, be described as slightly off beat!
There must be many enterprising readers who have built up similar unconventional pieces of equipment, for there is obviously a limit (physically, at least!) to the number of radio sets one can, or wishes to, build.

While the description of radio sets is one of the main features of Practical Wireless constructional articles, we are fully, aware that the advanced constructor may well be satiated with radio sets or has become capable of designing his own.

There is, of course, the associated audio field and it is our policy to provide plenty of material of this kind. But although there is a considerable range of designs to draw upon in radio sets (from the transistor pocket receiver to the multi-stage communications receiver) and a number of new circuit features (such as reverberation-one system is described in this issue and others will follow), it is, perhaps, on the "electronics" side that there is potentially the greatest scope.

So far as the home constructor is concerned, this potential is still largely untapped, but can range from geiger heads to gimmickry. Some of these gadgets, admittedly, may be of more value as construction and design exercises, but many could have very practical applications.

One of these is the metronome shown on the front cover and described in this issue. Most people build or buy radio sets, amplifiers and tape recorders largely for the reproduction of music. And, due partly to the upsurge of interest in hi-fi, there is a growing cult of musical appreciation.

This is reflected in the returning to favour of the erstwhile irreplaceabie piano and other instruments. And since many readers of Practical Wireless are no doubt amateur musicians, an electronic metronome is one useful way of combining interests.

If you have constructed any practical "off beat" items you feel would interest other readers, we would like to hear about them.

## Last Chance

Just a final reminder that this is your last chance to obtain tickets for the Practical Wireless Film Show which has been arranged in collaboration with Mullard Ltd. and will be held at Caxton Hall, Westminster, London, on February 1 st, starting at 7.30 p.m.

Tickets for this show are free and may be obtained simply by writing to us and enclosing a S.A.E.
 Our neaz isewe dated March will be published en Fabriary Tth.

will be 10 a.m. to 7 p.m. daily except Thursday March 19th when it will be extended to 9 p.m.

For the first time overseas manufacturers will be invited to exhibit, and although a certain amount of additional space has been made available it is anticipated that it will all be taken before the end of 1963.

## Acoustic Fault-finding Apparatus

A NEW acoustic fault-finding apparatus which incorporates an AEI type BK24 ignitron is now being used by the North Western Electricity Board.

Previously a mechanical contactor was used to discharge two $2 \cdot 25 \mu \mathrm{~F}$ capacitors, connected in parallel and charged to 25 kV , into the faulty cable. This method proved quite successful, but the high-voltage contactor, being very noisy, made detection difficult when the fault was close
to the equipment. Furthermore, approximately half of the stored energy was dissipated at the contacts and did not reach the fault.

By using an ignitron instead of the contactor, both these disadvantages have been overcome. The ignitron is an inherently noiseless device and its characteristics are such that the are voltage drop, and consequent energy loss, is very small.

## New Organisation Headquarters in London

THE wholly owned British subsidiary of US General Electric, International General Electric Company of New York Ltd., has announced the formation of an Industrial Electronics Division to market many General Electric industrial electronics products in Europe.

International General Electric Company of New York, Ltd. has


This photograph shows a high-power three-dimensional radar made by C.S.F. of France, who have recently, opened their first London office.
been marketing the products of US General Electric in the United Kingdom for many years. The complexity of modern industrial electronics equipment, however, has led to the establishment of this new organisation of much broader scope and capability

This new organisation will have have headquarters in London at 31 John Street, WC1, and will establish additional facilities in the United Kingdom and on the Continent to meet market requirements.

## British Equipment at Milan Exhibition

FrOLLOWING demonstrations of electric equipment during past months in Germany and Switzerland, EMI Electronics Ltd. exhibited equipment in Italy, at the Automation and Instrumentation Exhibition held in Milan.

Chief among the exhibits was a Robotug driverless truck, fitted with electronic guidance equipment, which follows a magnetic field surrounding a wire buried just below the surface of the ground.

Also on show was EMI's oscilloscope type WM16 with a range of plug-in pre-amplifiers. Other exhibits included nuclear health monitoring equipment, the EMlac II analogue computer, and a wide range of special electronic valves and tubes.

## I.E.E. Membership reaches $\mathbf{5 0 , 0 0 0}$

$\mathrm{A}^{\mathrm{T}}$T a recent meeting the I.E.E.'s Council admitted to membership of the Institution the man who brings the total to 50,000.

Starting in 1871 with about 70 founder members of the then Society of Telegraph Engineers, numbers grew rapidly to 3,660 in 1900. By the beginning of the second World War, the figure was approaching 20,000 , and the striking advance in technological developments in the last 20 years has contributed largely to the fact that the membership since then has more than doubled.

The " 50,000 th member" is William R. Matthews, admitted as a student.


At the microphone of this 6kW transmitter, which was installed at the Marconi works at Chelmsford in 1920, is W. T. Ditcham, whose voice was the first to span the Atlantic from Europe to Nova Scotia.

## Transport Minister Opens Medway Scheme

## New British Railways Testing Station

THE Right Hon. Ernest Marples, M.P. recently opened a new radar and radio control centre for the Medway Conservancy Board. The ceremony was carried out in the new control room and was seen by visitors in the reception centre on a closed-circuit television chain.

A well planned operation room, built on top of Garrison Point Fort at Sheerness, houses the control consoles for the three viewing units of the Decca Harbour Surveillance Radar and the Pye v.h.f. radiotelephone equipment. The Pye radio transmitters, which are sited on the Southdown Hills two miles from the operations room, give the best possible coverage to shipping in the Medway.

The Medway Port and Information Service has now been extended to include harbour surveillance radar and the radiotelephone system has been improved and enlarged.

International radiotelephone channels recommended by the Hague Convention are used and two-way v.h.f. radio communication between the Port Authorities and Ships' Masters help in the safe and fast movement of ship ping in the Medway

BRITISH Railways Eastern Region has placed a contract with Associated Electrical Industries Ltd. covering electrical loading equipment and a communication system for the new diesel-electric locomotive testing station now being built at Doncaster. When completed this station will be capable of testing a range of twenty-one different locomotives, from small shunters to 3,300 h.p. "Deltics".

Testing will be carried out from two control desks mounted in a control room overlooking the interior of the station. The desks will control the contactors on the fan-cooled loading resistance banks and will also carry test instrumentation.

An AEI type RP loading resistor, in which the resistance strip is edgewise wound and ceramic insulated from the central steel mounting strips, will be mounted on two banks, each with a dissipating capacity of 2,000 h.p. Tappings can be varied on-load by means of contactors mounted on the resistor banks which, in conjunction with the changeover switches and links in the termination cubicles, will enable either one Deltic locomotive to be tested alone, or two locomotives of 2,000 h.p. maximum, by using, both resistan Bankstseparately.


## Electronic

By K. Berry

टSSENTIAL to someone learning to play the piano and useful to anyone (hi-fi enthusiast or not!) with a keen interest in music is the metronome. This article describes a cheap, easy-tobuild electronic metronome. The beat note is continuously variable over the range $45-200$ beats per minute. Should this range seem rather large it must be pointed out that this is appröximately the range found in a proprietary clockwork metronome.

## Circuit

The circuit of the unit is shown in Fig. 1. It will be seen that it is basically a transistor version of the well-known multivibrator circuit.

The rate of operation is altered by varying the time constant C1, VR1, R2. When VR1 is set for zero resistance $C 1, V R 1$ is equal to R3 and the circuit operates at its fastest rate with $\operatorname{Tr} 1$ and Tr2 "bottomed" for equal periods of time (i.e., with a $1: 1$ mark-space ratio). When VR1 is set for maximum resistance, C1, VR1, R2 is about eight times as large as C2, R3 and the circuit operates at a lower rate with $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$ being bottomed for unequal periods of time (the approximate mark-space ratio in this case is $6 \cdot 5: 1$ ).

The audio output is obtained by connecting a loudspeaker from the collector of $\operatorname{Tr} 2$ to ground via a capacitor.

## Components

The components required for this metronome are given in the component list. The timing capacitors C 1 and C 2 are ordinary $50 \mu \mathrm{~F} 12 \mathrm{~V}$ etched aluminium foil electrolytic capacitors. Now since the capacity marked on these is subject to a tolerance of some $+100 \%$ or $-50 \%$ one 'can obviously get into difficulties here. The capacitors used in the prototype equipment were $47 \mu \mathrm{~F}$ and $48.5 \mu \mathrm{~F}$ respectively and measurements made of other electrolytic capacitors would suggest that although electrolytics can vary by $+100 \%$ or $-50 \%$ they do not often do so. The best solution is to check the capacitors on an impedance bridge if one is available. Failing that, go ahead with


Fig. 1-The circuit of the unit.


Fig. 2-A suitable power-pack.
standard electrolytics and, if the correct speed cannot be obtained from the metronome at first, substitute fresh $50 \mu \mathrm{~F}$ capacitors first for C 1 , then for C2. If this dodge fails the " $50 \mu \mathrm{~F}$ " capacitors can be shunted with some small value electrolytics (if the metronome runs too fast) or replaced with a parallel configuration of small values, say two $20 \mu \mathrm{~F}$ capacitors plus a $5 \mu \mathrm{~F}$ capacitor. This may sound rather formidable and in fact one probably won't be faced with having to do this but, since the possibility exists, it is best to bring it out rather than conveniently forget about it!
The transistors used in the prototype . unit were Mullard, type OC41. This type is a p-n-p germanium junction switching transistor, but most types of audio p-n-p transistors should serve just as well and a list of possible alternatives has been included in the component list.

The loudspeaker which was incorporated in this unit was marked as having an impedance of $10 \Omega$. Also tried was a loudspeaker with a speech coil impedance of $2-3 \Omega$ and this was


This photograph shows clearly the wiring of the unit.

## COMPONENTS LIST

## Resistors:

| R1 | $1 \mathrm{k} \Omega$ | R3 | $3.3 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- |
| R2 | $3 \cdot 3 \mathrm{k} \Omega$ | R4 |  |
|  | All $\frac{1}{4} W$ carbon |  | $l k \Omega$ |

VRI $25 \mathrm{k} \Omega$ carbon potentiometer, log

## Capacitors:

CI $50 \mu \mathrm{~F}$ electrolytic 12 V
C2 $50 \mu \mathrm{~F}$ electrolytic 12 V
C3 $8 \mu \mathrm{~F}$ electrolytic 150 V
C4 $250 \mu \mathrm{~F}$ electrolytic 25 V
C5 $250 \mu \mathrm{~F}$ electrolytic 25 V
Semiconductors:

## Trl, Tr2 Transistors Mullard OC41 (alternatively OC71, OC72) <br> MR1-4 Rectifiers S.T.C. RS20

DI Zener diode Mullard OAZ207

## Miscellaneous:

LSI Loudspeaker, 2-15 $\Omega$ impedance
SI Single-pole switch
S2 Double-pole switch
TI Mains transformer: input $240 \mathrm{~V} 50 \mathrm{c} / \mathrm{s}$; output 12 V 30 mA

## Power Supplies

The prototype was self-powered by means of a dry (primary) battery. This was a layer-type battery intended for use with transistorised equipments of size $1 \frac{1}{\mathrm{i}} \mathrm{in}$. $\mathbf{x} 1 \mathrm{in}$. x 2 in ., but any type of 9 V battery may be used. The normal current consumption of the metronome is $12-15 \mathrm{~mA}$ at 9 V .

There is no reason why the unit should not be run off the d.c. mains supply if portability is not important. A suitable power unit is shown in Fig. 2. The use of a Zener diode to regulate the output voltage is necessary because of the fluctuating nature of the current drawn by the metronome

## Calibration and Use

When the unit has been wired all that remains is to calibrate it. This can most easily be accomplished by using an electronic or electromechanical counter, but since these are not readily available the practical method is to count the number of beats whilst observing a watch or clock with a sweep second hand. This is quite easy up to about 150 beats per minute and with a little practice one can count up to 240 beats per minute.

H. W. Hellyer

9HE story of the radio enthusiast who progressed from the crystal set to a high-powered transmitter with nothing but a keen, wet finger is probably apocryphal. But during the short and crowded history of radio a surprising amount of good work has been done with the minimum of test equipment.

Partly this may have been due to high capital costs, partly because of a lack of information on the capabilities-and, indeed, the limitations-of individual items of test gear. Today we find a very wide range of equipment at our disposal, both surplus and commercial, in kit form and brand, spanking new. The advertisement columns of Practical Wireless abound in tantalising offers.

The problem is to know what to buy or make.
This series of articles aims to reduce the problem by outlining the scope and purpose of test equipment and presenting some of the applications. It does not set out to be a catalogue and specific items of equipment will not be described except where they illustrate a particular test sequence.

Circuits and methods are the result of practical experience at the bench and in the field. Many articles on the modification and adaptation of test gear have appeared in these pages and it is not intended to tread the same ground: additions to commercial test equipment will be mentioned only where such circuits extend the scope and versatility of the basic instrument.

However, queries are welcomed; novel ideas that readers may suggest will be laboratory tested and passed on. In this way it is hoped that these articles may prove a useful source of reference to those who study the advertisements and wonder whether particular instruments are suitable or will fulfil the desired purpose.

Information on test gear is singularly scarce. Of the few books available on the subject perhaps the best, and certainly the most up to date, is "Radio and Television Test Instruments ", by Gordon J. King, published by Odhams Press, 25s. Mr. King is no stranger to readers of Practical Wireless; his help and guidance in the preparation of this series is gratefully acknowledged.

## The Bosic Meter

The fundamental item of equipment in any workshop, amateur or professional, is the test
meter. Without it other, more complicated, instruments are just so much expensive decoration. A good deal of testing can be done with a trustworthy meter and plenty of time and ingenuity.

Unfortunately modern receivers and other electronic circuitry are much more complex than those of previous "wet-finger" days. Closer tolerances demand a higher standard of testing and more precise instruments.

This does not mean that the most expensive meter is necessarily the best for any particular purpose. There are multimeters ambitious enough to knock a hole in any wage packet with many ranges and functions that the owner never useseven if he has found out how.

But if the only measurements required are voltages and currents met during receiver repair, plus the general purpose resistors of no closer than 5 per cent tolerance, a good "standard" meter should be sufficient. Such factors as robustness, ease of scale reading, foolproof overload and


Fig. I-A typical meter movement.
simple connection may be as important as the movement sensitivity.

## Sensitivity

Nevertheless it is the sensitivity of the basic movement that ultimately determines how good or bad a meter can be. Remembering that a metel connected to a circuit for measurement becomes part of the circuit under test, it is obvious that the less effect the meter has upon the circuit the
greater the accuracy of readings.
The sensitivity of a meter depends upon the current needed for FULL-SCALE DEFLECTION and the fundamental resistance of the meter. The latter important factor is stated as the OHMS PER VOLT rating. General purpose meters for measuring voltage and current and, by the addition of a voltage source, indicating resistance, are usually MOVING COIL instruments. There are other types, having special purposes, which we shall discuss later.

A typical basic moving coil assembly is illustrated in Fig. 1. In this the coil $\mathbf{A}$ is wound on a rectangular former and mounted on jewelled bearings in a magnetic field provided by polepieces N and S . The field is carefully determined and there are wide variations in the polepiece conformation between different manufacturers.

In our example a brass section is seen, $B$, between the poles with an iron flux adjustor; F , which should not be altered. Indeed when servicing or cleaning meters take care not to disturb the mechanical assembly: clamps and brackets may, in fact, be acting as magnetic shunts.

Note the flux compensator, C , the cylinder on which the coil is mounted. This serves to maintain a radial field and to reduce the reluctance effect between the moving arms of the coil assembly and the inner surface of the polepieces. On some types advantage is taken of this effect for additional damping.

## Even Movement

Others have an aluminium plate fixed to the pointer arranged to operate in a magnetic field. The flux opposes the actuating current and, by Faraday's Law, increases with the acceleration of the pointer movement. This tends to produce an even movement of the pointer across the scale.
On the model shown in Fig. 1 additional balance to the movement is afforded by the weights, $W$, near the lower end of the pointer. These should not be confused with the gravity balance weights fitted on some of the cheaper models.

Current is fed to the coil by a pair of springs, $P$, wound in opposing spirals, also assisting in movement balance, particularly in return action of the pointer when the actuating current is removed. An important function of these springs, generally made of a non-magnetic material, phosphor bronze, which has the added advantage of a lower coefficient of linear expansion than spring steel, is the temperature compensation they afford.

## Refinements

Other refinements may be found: a transverse bar for extra balancing, a light piston or vane in a virtually closed air chamber for braking action, a mirror backing to part of the scale to assist visual alignment--an anti-parallax device. And the zeroing set screw, $\mathbf{Z}$, which adjusts an eccentric thread to move a fine wire in an inverted U-piece at the lower end of the pointer.
From the foregoing it can be seen that the lighter and more perfectly balanced the meter movement is the less current needed to operate the pointer. Other things being equal, the more sensitive the instrument. By winding the coil with a high number of turns of very fine wire a meter
can be constructed having a high resistance and needing a very small current for full-scale deflection.

Nowadays meters of 20,000 ohms per volt having an f.s.d. of 50 microamps $(0.00005$ of an ampere) are quite common and at least one wellknown meter available to radio engineers has a sensitivity of $100,000 \mathrm{ohms} / \mathrm{volt}$. This means that on the 100 -volt range of such an instrument the load presented to the circuit is in the region of 10 Megohms, comparable with the standards of many an electronic meter, about which more later.

The importance of this factor of high $\Omega / V$ can be seen by reference to Fig. 2. Here we have an identical pair of $100,000 \Omega$ resistors. cannected across a 100 -volt d.c. supply. We know by simple


Fig. 2-These diagrams illustrate the importance of high $\Omega / V$ foctor in meters.
calculation that 50 volts is dropped across each and would be indicated by an ideal voltmeter.
But if we put a meter with a sensitivity of 1,000 ohms/volt across R2 the actual reading is as low as $33 \cdot 3$ volts. This is because a 1,000 ohms/volt meter on its 100 -volt range has a resistance of 100,000 ohms. In parallel with the resistance of R2 this reduces the total resistance across the section $B C$ to 50,000 ohms, giving a $2: 1$ ratio of AB to BC and a voltage drop of $66 \cdot 6+33: 3$ instead of the $50+50$ in the former instance.
Similarly a $20,000 \mathrm{ohms} /$ volt instrument would read 47.5 volts across $R 2$, which is better, while a 100,000 ohms/volt instrument would indicate the near-accurate voltage of $49 \cdot 9$ across the same point.
This serves to illustrate one practical point. Greater accuracy is obtained by using the voltmeter on its higher ranges. However, from the point of view of mechanical accuracy, antiparallax reading and an aid to interpolation (the assessment of readings between the divisions of the scale) it is often better to adjust the range so that the pointer lies in the middle third segment of the scale.

A further practical point to note is that most of scale of 110 deg. or more, while there are less useful models with an 80 deg. scale.

## Linear Scale

Moving coil meters have the advantage that the torsion, and thus the arc of travel, is proportional to the actuating current so that the scale is linear. They can be made accurate to 1 per cent for

## Keep this for reference

## FACTS, FIGURES \& FORMULAE

During this series, various references will be made to electrical and magnetic properties. Before we can employ test gear efficiently, we must know what the quantities are that we are measuring. The following notes contain definitions that may be familiar to many readers-but their collection and statement at the outset will save time and space in digressing explanations later.

## Valve Characteristics

Amplification factor $(\mu)=$ Anode impedance $\left(r_{\mathrm{a}}\right) \times$ Mutual Conductance (gm)
where $\mathrm{r}_{\mathrm{g}}$ is in thousands of ohms and $\mathrm{g}_{\mathrm{m}}$ in $\mathrm{mA} /$ volt.

$$
\text { Stage Gain, } A=\frac{\mu \times R_{a}}{R_{a}+r_{a}}
$$

(where $R_{a}$ is the anode load, in the same unit as $r_{a}$ ).

## Equivalences

$$
\begin{gathered}
R(\text { ohms })=\frac{E(\text { volts })}{I(\text { amps })} \\
W(\text { watts })=I^{2} R=\frac{E^{2}}{R}=E I \\
F(\text { in Mc/s })=\frac{3 \times 10^{2}}{\lambda \text { in metres }}=\frac{300}{\lambda} \\
\text { Where } \lambda \text { is wavelength). } \\
\left.X_{0} \text { (ohims }\right)=\frac{10^{4}}{2 \pi f C}
\end{gathered}
$$

(Capacitor reactance, where $f$ is frequency in cycles/second and $C$ is capacitance in microfarads).
$X_{\mathrm{L}}(\mathrm{ohms})=2 \pi \mathrm{~L} \mathrm{~L}$
(Inductor reactance, where $L$ is inductance in henries.)
(N.B. 2ff often designated $\omega$ (omega).)

$$
\text { At resonance, } X_{C}=X_{L} \text { and } f_{r}=\frac{1}{2 \pi \sqrt{L C}}
$$

(Where $f_{r}$ is resonant frequency in kilocycles, $L$ in microhenries, $C$ in microfarads).
Magnification factor of tuned circuit: $Q=\frac{2 \pi f L}{R}$

## Decibels

The Bel is the common logarithm of the ratio of two powers.
One-tenth of a Bel, the decibel (dB) is used for convenience.

$$
\text { Thus } \mathrm{dB}=10 \times \log \frac{W_{1}}{W_{2}}
$$

(where $W_{1}$ and $W_{2}$ are the two power levels).

$$
\text { and } d B=20 \times \log \frac{V_{1}}{V_{2}}
$$

(where $V_{1}$ and $V_{g}$ are the two voltage levels)
(this supposes equal impedances to be employed).
Typical dB ratios are:
Power ratio of $2=3 \mathrm{~dB}$, of $10=10 \mathrm{~dB}$ of $100=20 \mathrm{~dB}$.
Voltage ratio of $2=6 \mathrm{~dB}$, of $10=20 \mathrm{~dB}$,
of $100=40 \mathrm{~dB}$, of $1000=60 \mathrm{~dB}$.

## Meter Calculations

$$
\text { Shunt } R_{s}=\frac{R_{m}}{n-I}
$$

(where $R_{m}$ is internal resistance of meter, and $n$ is the factor of multiplication)

$$
\text { Multiplier } R_{v}=\frac{(E \times I, 000)}{I}-R_{m}
$$

(where $E$ is the required full-scale voltage, $R_{m}$ the internal resistance of the meter, and I the full-scale current of the meter (mA)).

A unit of reciprocals is given on the following page. Other factors, figures and formulae will be defined where applicable in the articles.

## ABBREVIATIONS AND PREFIXES

| Abbr. | denotes |
| :--- | :--- |
| $M$ | Mega, or Meg |
| $\mathbf{k}$ | Kilo |
| $d$ | Deci |
| $\mathbf{m}$ | Milli |
| $\mu$ | Micro |
| $\mu \mu$ or P | Pico |
| v.l.f. | Very low frequency |
| l.f. | Low frequency |
| m.f. | Medium frequency |
| h.f. | High frequency |
| v.h.f. | Very high frequency |
| u.h.f. | Ultra high frequency |
| s.h.f. | Super high frequency |

## meaning

"millions of", as in Megohm $=10^{6}$ ohms.
"thousands of", as in kilohm or kilocycles, $=10^{3}$ ohms or cycles per second.
"tenths of", as in decibel $(\mathrm{dB})=10^{-1} \mathrm{Bel}$.
"thousands of", as in milliampere $(\mathrm{mA})=10^{-3}$ amperes.
"millionths of"' as in microfarad $=10^{-6}$ Farad.
"million-millionths of", as in picofarad (pF) $=10^{-12}$ Farad.
$0-30$ kilocycles per second $(\mathrm{kc} / \mathrm{s})$, or above 10,000 metres wavelength.
$30-300 \mathrm{kc} / \mathrm{s}$, or $10,000-1,000$ metres.
$300-3,000 \mathrm{kc} / \mathrm{s}$, or $1,000-100$ metres.
$3,000-30,000 \mathrm{kc} / \mathrm{s}(3-30 \mathrm{Mc} / \mathrm{s})$, or $100-10$ metres.
$30-300 \mathrm{Mc} / \mathrm{s}$, or $10-1$ metre.
$300-3,000 \mathrm{Mc} / \mathrm{s}$, or $100-10 \mathrm{~cm}$.
$3,000-30,000 \mathrm{Mc} / \mathrm{s}$, or $10-1 \mathrm{~cm}$.

| Reciprocals |  |
| :--- | ---: |
| Conductance $(G)$ is the reciprocal of resistance, | $=\frac{1}{R}$ |
| Susceptance $(B)$ is the reciprocal of reactance, | $=\frac{1}{X}$ |
|  | 1 <br> Admittance is the reciprocal of impedance, <br>  |

general work (sub-standard models are accurate to 0.2 per cent) and are not liable to interference from external fields.

Their principal disadvantage is that a reversal of energising current results in a reversal of torque and thus they are basically suitable for d.c. only and polarity must be observed. A.C. ranges are obtained by rectification of the applied current, usually by small metal rectifiers.

These have a non-linear characteristic in the conductive direction and therefore the sensitivity and accuracy of a.c. ranges is less than of d.c. ranges. Calibration is in r.m.s. values and the readings should be multiplied by 1.414 to obtain peak values, but this applies only when a sinu-


Fig. 3-Methods o; decoupling moving coil instruments
soidal waveform is applied. Other waveforms will give misleading indications.

This makes it necessary to provide decoupling for a standard moving coil instrument when it is used to take readings where, for example, signal voltages may be present. Fig. 3 indicates such a method and also shows that the correct place at which a meter should be applied is where the signal voltages have the least effect or, alternatively, are least affected by the presence of the meter.

Thus in Fig. 3a a reading of anode current of an audio amplifier stage is made by inserting the meter on the h.t. side of the load resistor and decoupling the meter for signal voltage by a suitable capacitor. And in Fig. 3b the meter is
inserted in the anode lead of an i.f. amplifier at a point of low signal potential and similarly decoupled. Do not insert the meter between the anode of the valve and the load.

## Current Testing

Current testing is done by the insertion of the meter in series with the circuit. From our former statement we can see that a meter with a small f.s.d. current needs a smaller value of shunt resistance for a greater total measured current. Thus the meter plus shunt presents less disturbance to the circuit.

It is not intended to give details of shunt calculation and construction at this point, nor the details of multipliers for extending voltage ranges -this has been done many times before in these pages. We shall assume that we are using the meter within its designed limits.

Practically, however, there are several points to note. Before inserting a meter for current testing switch off the apparatus. In addition to safeguarding the circuit under test this also protects the meter from unnecessary transients which can upset a delicate movement.

## Polarity

Observe polarity-a meter which has the reverso connection at high loading can suffer mechanical damage because of the attempt of the pointer to force against the lower stop.

If the current to be tested is not known, always try first on the highest range. Actually it may be better to make some alternative test first to ensure that the current does not exceed the range of the meter. This can sometimes be done by making a voltage reading across part of the circuit and doing a quick calculation.

In a similar way always test at the highest voltage range first and do not switch ranges with the meter in circuit. Overload protection is generally provided; some instruments have a mechanical trip that is operated by the pointer over-riding the upper stop, some use a shunting rectifier which bypasses harmful currents from the moving coil. But there are limits and meters are expensive items to repair or replace.

## Maintenance

When attempting meter maintenance, care must be taken not to employ magnetic tools or, indeed, ferrous tools of any kind. Metallic particles can be transmitted to the polepieces and movement very easily and are extremely difficult to eradicate. Getting magnetic particles from the gap in $a$ movement is best done by' removing the coil assembly altogether and cleaning the pole faces with a soft cloth. Take great care not to damage the flat spiral springs or pointer. Pivots can be cleaned with jeweller's rouge applied with a sharpened matchstick.

A good deal of space has been used in this introductory article for the purpose of laying the ground. In the next part we shall take a look at other kinds of meter and capacitance resistanco testing.
(To be continued)


SIMPLE

## TRANSISTOR

TWO
By F. G. Rayer

JHIS receiver is of extremely simple construction, and is thus particularly suitable for beginners who may be looking for an easy, straightforward circuit. There are three stages-a crystal diode detector, followed by an audio amplifier, and a Class A output stage. The set is intended to run from a L5048 or similar $7 \frac{1}{2} \mathrm{~V}$ battery, though a 9 V battery may be used.

The circuit is shown in Fig. 1. A receiver of this kind is not intended for reception of distant or overseas stations, and it requires some kind of aerial and earth. For local station reception, for which it is intended, an indoor aerial should
loudspeaker may be connected directly, with no transformer.

## Paxolin Pane

The receiver is built and wired on a paxolin panel 4 in . $x 8 \mathrm{in}$. Material $\frac{1}{16} \mathrm{in}$. thick is sufficiently strong, though $\frac{3}{32}$ or $\frac{1}{8}$ in. paxolin could be used. All the holes are drilled as indicated in Fig. 2. Holes for leads can be made with a ${ }^{\frac{1}{1}}$ in. or similar small drill. Holes for the speaker bolts, and L. 1 mounting, should be about $\frac{1}{8} \mathrm{in}$. diameter, while VCl is secured with three short 4B.A. bolts.

If any changes are made, such as to the speaker or VC1, these holes should be modified to suit. Tl had lugs, which are passed through slots. usually be sufficient. The aerial
may be taken to tappings $B$ and D , or to the beginning of the coil (A) according to conditions.

Holders are used for the transistors. This avoids possible damage due to overheating, and allows any audio frequency transistors which are to hand to be tried. The transistor in the Tr 1 position can best be an OC71 or similar type, while the Tr2 transistor is an OC72 or similar output type. Results obtained with spare transistors can easily be compared by inserting them in the holders.

For optimum amplification, resistor values are quite important. It is easy to check the working of each stage, with phones and a
 meter, as described later.

Capacitor values are not particularly critical VC1 is a midget air-spaced capacitor of about 380 pF , but the value is not important, and a 500 pF solid-dielectric tuning capacitor could be used instead. Alternatively, a 500 pF air-spaced capacitor. or similar component. C 1 may be $0.1 \mu \mathrm{~F}$ to $0-5 \mu \mathrm{~F}$. C2 may be $32-100 \mu \mathrm{~F}$, while C3 may be $4-8 \mu \mathrm{~F}$.

The output transformer T 1 is a non-miniature transistor type component, such as would be used with a pair of transistors in push-pull. The speaker unit shown is a highly sensitive one, but there is no actual need to use this particular size. Many speakers have a 2 to $3 \Omega$ speech coil, and these require a 2 to $3 \Omega$ secondary on the transformer T 1 . Speakers of other impedance may be used, with their particular matching transformers. A 758
then twisted. These slots can be made by drilling two or three small holes close together.

There is no reason why a ready-made coil should not be used. If so, the ferrite slab. with winding, is not required. The coil should be wired to agree with its maker's data. The receiver will also be found to work well on long waves, in those areas where the Light Programme on 1500 m is available, so a small rotary switch can replace the on/off switch, for dual-wave tuning. In this case coil wiring should be taken from the coil maker': instructions leaflet.

All holes are drilled before mounting any parts The transistor holders are a tight push fit in thei holes. and are held with a touch of cement. The speaker can be left off until wiring is otherwist finished.


Fig. I-The circuit.

## Rear of Panel

All the components are fitted to the panel, at the back, as in Fig. 3. C2, C3 and C4 have positive and negative ends, so their leads are inserted through the holes as indicated. There should be no possibility of wiring or component value errors, f care is taken to insert the resistors and capasitors as shown.
The tuning coil is wound with 28 s.w.g. d.c.c. wire, on a ferrite slab about $\frac{1}{8}$ in. $x \frac{8}{8}$ in. $x 3$ in. Referring to Figs. 1 and 3, there are 20 turns from A to $B$, six turns from $B$ to $C$, six turns from $C$ to $D$, and 20 turns from $D$ to $E$, making a total of 52 turns. All turns are wound in the same direction, zlosely side by side, and some nodification to the number of arns, or gauge of wire, or the size of the slab or ferrite rod, will not $x$ very important.
The tapping points $\mathrm{B}, \mathrm{C}$ and D :an be made by twisting small oops, during winding, and a dab of cement will hold the ends $A$ ind $E$, which are long enough to each VCl. A is taken to the ixed plates tag, and $\mathbf{E}$ goes to the rame, which is also connected to he battery positive line, on the ther side of the panel.
Two small blocks of hardwood or other insulating material are :ecured to the paxolin by neans of small screws. The errite slab rests on top of these locks, and is held with elastic ,ands passed through holes, und tied.
All wiring is on the front of he panel, and is very simple. _eads can be of any thin, nsulated wire, and all connecions are kept flat against the ,axolin. Wiring is shown in Fig. 4. Point + ve joins a tag leld by one of the bolts ecuring the variable capacitor.「hese bolts must be short, or lave washers, so that they do


Fig. 2-Drilling details of the paneh


Fig. 3-Component layout on the rear of the panel.

With any reasonably effective aerial, and an average earth, quite good, phone volume should be obtained, from local stations.

The 'phones may then be wired in parallel with R6, and Tr1 may be inserted. There is no need to cut the transistor leads, but thin sleeving should be placed over them, to avoid shorts. It is essential that the collector, base and emitter leads are inserted in the correct sockets, as in Figs. 3 and 4.

Volume should be very much increased. Current consumption of Tr 1 will depend on the transistor, but can be expected to be around 1 mA . If the stage does not amplify, or if results are distorted, suspect the transistor, or wiring, etc. If Tr 1 is of a type much different from that mentioned, the values of R1 and R4 may need changing.
The 'phones can then be removed, and Tr 2 inserted. Consumption should be around 18 mA to

## COMPONENT LIST

Resistors:

|  |  | $1 \mathrm{k} \Omega$ | R7 | $39 \Omega$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R1 | $65 \mathrm{k} \Omega$ | R 4 | $1 \mathrm{k} \Omega$ | R |  |
| R2 | $10 \mathrm{k} \Omega$ | $\mathrm{R5}$ | $12 \mathrm{k} \Omega$ |  |  |
| R3 | $3.9 \mathrm{k} \Omega$ | R6 | $2.2 \mathrm{k} \Omega$ |  |  |

Capacitors:
R6 $2 \cdot 2 \mathrm{k} \Omega$
VCI Approx. 380 or 500 pF variable capacitor
CI $\quad 0.25 \mu \mathrm{~F}$ paper
C2 $50 \mu \mathrm{~F} 3-6 \mathrm{~V}$ or similar
C3 $8 \mu \mathrm{~F}$ 6-9V or similar
C4 $100 \mu \mathrm{~F} 3-6 \mathrm{~V}$ or similar
Semiconductors:
Two transistor holders
TRI OC7I or similar
TR2 OC72 or similar
GD9 Crystal diode
Miscellaneous:
On/off switch. Control knob. Ferrite slab and wire as described, or transistor set coil. W/B HF. $3.573 \frac{1}{2} \mathrm{i}$. 3 ohm speaker, or similar unit. Non-midget type transistor output transformer, ratio about 8 : I. Paxolin panel approx. $8 \times 4 \mathrm{in}$., etc.

25 mA , with average loudspeaker volume. If current is over about 25 mA , with the values shown and a particular transistor of different type, RS may be increased in value, until the set draws about 20 mA or so. If current is low, with lack of volume, RS may be reduced in value, until the set draws about 20 mA . An L5048 or similar battery will have a long life, with this current drain.

## Cabinet

The receiver is not intended for portable use so the smallest possible cabinet is not required


Fig. 4-The wiring diagram.
If no cabinet is to hand, one can be constructe from thin wood.

The receiver front consists of a piece of paxolir or any other thin material, with holes to agres with VCl , switch, and the speaker aperture Silk or other fabric is stretched over the front, ans cemented round the edges. Holes are cut in th fabric to clear the switch, and the spindle of VC1
The securing nut of the switch is removed, ans washers are placed on the switch, so that the fron panel will just clear the receiver wiring. The tw panels are then locked together with the switcl nut, and a control knob is placed on the tunin. capacitor spindle.


These capacitors are ideal for miniaturised transistor circuits such as in pocket radios. Each is available with wires at opposite ends for horizontal mounting (' $H$ '"), or at one end for vertical mounting (" $V$ ").
Connection wires are welded for low resistance contact and solder coated for ease of assembly. The standard length is $1 \frac{1}{2}^{\prime \prime}$ for the horizontal range, cropped to $\frac{3}{16}$ " for the vertical range.


The capacitors are in insulated seamless aluminium cases and sealed with a synthetic rubber burig.
Capacitance and Tolerance Standard tolerance is $-20 \%+100 \%$ of the rated capacitance. Operating Temperature Range: $-20^{\circ} \mathrm{C}$ to $+60^{\circ} \mathrm{C}$.

| T.C.C. TYPE | CASE SIZE IN INCHES |  |  | MAXIMUM D.C. WKG. VOLTAGES AND CAPACITANCE ( $\mu$ F) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | D | L. | C | 3V. | 6 V . | 10 V. | 15 V. | 25V. | 50V. |  |  |  |
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# Quality Amplifier <br> (Continued from page 823 of the January issue) <br> pre-amp 

By A. Cole

ЭHE author ended last month by mentioning a method of tone control by connecting a $10-50 \mathrm{k} \Omega$ potentiometer and $0.1 \mu \mathrm{~F}$ capacitor in series from the anode of the output valve to chassis. This cuts treble by shunting actually produced power to earth instead of through the loudspeaker, and introduces effectively lower impedance at high frequencies to mismatch the output valve, leading to "distortion and cross modulation. The "bass" in the "top-cut" setting of such a tone control is muffled and woolly, and the application of a shrill-toned signal can lead to severe overloading even though the actual volume finally present in the loudspeaker may be quite small.

The ideal position for a "top cut" control is right at the grid of the input stage; since then the above named disadvantages do not apply. Accordingly, VR2 and C6 constitute a treble-cut tone control of this kind, at the input grid of V1. This is ahead of the negative-feedback loop, and does not in any way limit the available output power, as there is linear treble response within the amplifier proper.

A treble cut control is more useful than a balanced treble lift/cut. In the same way, a bassboost is more useful than a balanced bass boost/ cut. VR 3 and C9 vary the amount of bass negative feedback, so that the gain at bass frequencies may be raised above that at other frequencies, when VR3 is at high resistance setting.

Naturally, the degree of bass-boost available cannot exceed the degree of negative feedback employed, and is thus adjustable by means of VR4. If the completed amplifier howls or squeaks, reverse connections to the secondary of the output transformer.

Amplifiers overload much more easily on bass than on treble, because the human ear is less sensitive to bass sounds and considerably more power is required. Thus many arrangements which simply pump the necessary bass voltage into an amplifier, without further considerations, give a very rough bass response. because of overloading before the necessary sound-intensity is reached.

The arrangement here adopted is much purer, because any would-be distortion consists of higher harmonics for which the negative feedback reduction is much less, so they are still strongly eancelled by the negative feedback, in spite of its
bass reduction for bass-boost tone control.
This form of tone control is an interesting exception to the otherwise normal rule saying "tone and volume controls should not be placed within a negative feedback loop".

Finally, as far as tone is concerned, one of the most effective methods of getting very clean dis-tortion-free reproduction is to use an output stage with a generous power reserve, so that one does not need to drive it to the end if its tether for normal usage.

## Checking for Balance

On completion, an oscilloscope check can be made. First of all, after checking the wiring, ensure that in the absence of a signal there is 10 V drop across R25 and equal voltages at V2 and V3 anodes.

Connect the oscilloscope Y-amplifier to the loudspeaker terminals (with a resistor of correct value and power rating as load). There should be no extraneous audio or supersonic signals present at any combination of settings of the controls, apart from slight residual hum.

Feed in a sine wave signal from an oscillator to the input and turn up the volume gradually. If the $Y$-amplifier is voltage calibrated, the r.m.s. voltage across the load resistor when visible distortion just starts can be read off and by dividing its square by the load resistance in ohms, the maximum power output under prevailing conditions obtained.

Turning the volume up still more, distortion should commence symmetrically on both half cycles. This is a sensitive criterion for balance throughout the amplifier and if serious asymmetry on onset of distortion is experienced this must be cured. Possible reasons could be wrong value of R8, R16/R18 unmatched, wrong value of R17, V2/V3 emission grossly different, and parasitic oscillation.

The oscilloscope method of testing can be used to determine the power output at various frequencies throughout the entire audio range, and to determine the necessary input voltage for full output by transferring the oscilloscope probe to the input, after adiusting the input signal for full output as observed when the probe is connected to the output load. The effect of the tone controls can also be studied this way (Table 2).

## Power Supply

Separate rectifier bridges are used for the amplo
fier and the tuner supply. There is no great objection to using a single bridge ( 300 V a.c., 200 mA rating) if available. C 2 will then appear in parallel with the first section of Cl , which should then be about $64-100 \mu \mathrm{~F}$. However, the design of Fig. 1 gives good decoupling and better smoothing.

The arrangement of R3, R4, R5, C3, C4, C5, gives three well decoupled separate supplies for the different sections of the tuner.

R3, R4, R5, C3, C4, C5 are located on the power-pack chassis instead of the tuner chassis, otherwise the return paths for a.c. through C3, C4, C5 would run between the two chassis and the interconnecting cables would carry a.c. components at high mains harmonics, resulting in increased stray hum injection into the circuits.
direct galvanic injection through stray "earthloops". If one makes haphazard earth-connections between the various items and the screenings of signal cables, a chassis inter-connection lead or a signal-cable screening may share some of the a.c. components of power flowing between the two units.

By virtue of the always-present pure resistance of the cable or screening concerned, there will be a resulting a.c. voltage drop along the connection concerned, so that all parts of it are no longer at the same a.c. potential. The result is that proper earthing or screening cannot then be present because the a.c. voltage drops along the supposed earthing or screening are injected directly in series with the signal proper, such effects being called


Fig. 2s The under-chassis wiring diagram.

## Double Smoothing

Note the arrangement of $\mathrm{R} 14, \mathrm{R} 15, \mathrm{C} 10, \mathrm{Cl1}$. The ripple from a fullwave bridge rectifier from the $50 \mathrm{c} / \mathrm{s}$ mains is at $100 \mathrm{c} / \mathrm{s}$. A capacitor of $32 \mu \mathrm{~F}$ has an impedance of roughly $50 \Omega$ at $100 \mathrm{c} / \mathrm{s} ; 8 \mu \mathrm{~F}$ roughly 200 . R14 and C10 thus reduce ripple in the ratio $300: 1$ and $\mathrm{R} 15, \mathrm{C} 11$ reduce the remainder in the ratio 75:1. The total reduction is thus in the ratio $22 \cdot 5$ thousand to one.

## Earth Connections

Hum induced by capacitive coupling of grid circuits to a.c. potentials is less of a danger than
"hum-injection on earth-loops".
Such effects also take place to a slight exten over stray capacities, which also present a finit impedance to a.c., and thus can never be avoide absolutely, yet one can do a great deal to reduc stray hum by a properly-conceived arrangement o earthing connections.

## Earthing of Signal-cable Screens

The purpose of a signal cable screen is $t$ prevent the amplifier at the output end of th cable seeing anything else but what is fed in a the input end of the cable. Therefore the cabl


Fig. 3i The above-chossis layout of components.
screening must be at the potential of the "prevailing earth" for the following amplifier stage.

The proper place for earthing the screen of the signal cable is thus at the following amplifier which it feeds, and nowhere else. If the signal input to the cable is from another chassis, it is better to use a separate earth-wire connecting the two chassis, and earth the cable screen only at the following amplifier end, rather than use the screen itself as only, or additional, earth connection between the two chassis.
Furthermore the separate earth connection between the two chassis concerned must be such that no a.c. power components flow along it.

## Avoiding A.C. Power Currents

There is only one solution to this problem. If one has to send a.c. power between two chassis of equipment (heater supplies, mains), then one should provide separate outward and return wires for the a.c. from the chassis supplying this power. In other words, earth connections for the a.c. supply concerned must, be made on the consumer chassis ONLY. (See Fig. 5.)

## The Present Amplifier

Ln Figs. 2 and 4 cables A, B, C are screened
signal cables. Cables A and B may be combined as a single screened cable with two insulated "inners" not individually screened from each other, but it is essential that C remains separateotherwise serious interference with the negativefeedback characteristics can result.
Cable E is a substantial four-core 15 A mains power type cable, carrying the three h.t. supplies for the tuner and the negative/inter-chassis connection. This cable is entirely for d.c., and the "d.c. loops" thereby resulting, giving slight d.c. differences of potential between the two chassis, are unimportant. They certainly cannot introduce hum! Cable D is another four-core power cable, for all a.c. connections. Note that none of its wires have any direct earth connection to the amplifier chassis nor to the control-panel chassis.
The grey wire, which will be the subsequent earth side of the tuner heaters, will receive an earth (chassis) connection only on the tuner-chassis, where the heater power is consumed.
Note that the black lead of the d.c. cable E, used as a.c.-free inter-chassis earth connection, also picks up mains earth on the control panel, yet is not connecied to the chassis plate of the control panel. The control panel is earthed via the signal cable screenings, and is thus merely a part of the main amplifier/power-pack chassis.

## Hum Injection via Valve-heaters

With modern valves there is only a very small hum-contribution from this source, which can be compensated by connecting a centre-tapped potentiometer across the heater supply.

Such measures were not found necessary in the


Fig. 4: The wiring diagram of the flying control panel.
prototype, the residual hum at zero-setting of VR1 being such that one can just hear that the amplifier is operating in a quiet room. Also as far as r.f. and i.f. stages are concerned-particularly at v.h.f.-it is definitely of advantage, for stability, if one side of the heater supply can be earthed directly.

From amplifier-power pack chassis

## COMPONENTS LIST

Resistors:

| RI | $100 \Omega$ | R2 | $100 \Omega$ |
| :---: | :---: | :---: | :---: |
| R3) |  |  |  |
| $R 4\} 5 k \Omega 10 \mathrm{~W}$ w.w. |  |  |  |
| R5 |  |  |  |
| R6 | $22 \mathrm{k} \Omega$ | R10 | $5.6 \mathrm{k} \Omega$ |
| R7 | $4.7 \mathrm{M} \Omega$ | RII | $68 \mathrm{k} \Omega$ |
| R8 | $1 \cdot 8 \mathrm{k} \Omega \pm 5 \%$ | R12 | $22 \mathrm{k} \Omega$ |
| R9 | $100 \Omega$ | R13 | $1 \mathrm{M} \Omega$ |
| R14 ${ }^{\text {R15 }}$ \} $15 \mathrm{k} \Omega$ |  |  |  |
| R15 ${ }^{\text {R }}$ / $5 \mathrm{k} \Omega$ |  |  |  |
| R16 | $47 \mathrm{k} \Omega$ matched with R18 |  |  |
| R17 \|.5k $\Omega \pm 5 \%$ matched pair |  |  |  |
| R18 $47 \mathrm{k} \Omega$ |  |  |  |
| R19 | $10 \mathrm{k} \Omega$ | R20 | $10 \mathrm{k} \Omega$ |
| R2I $560 \mathrm{k} \Omega$ ] |  |  |  |
| R22 | $560 \mathrm{k} \Omega\}$ mat |  |  |
| R23 | $100 \Omega$ | R24 | $100 \Omega$ |

R25 $90 \Omega 2 \mathrm{~W}$ w.w. $\pm 2 \%$
All resistors $\pm 20 \%$ iW carbon, unless otherwise stated.
Variable Resistors:
$\begin{array}{ll}\text { VR2 } & 500 \mathrm{k} \Omega \\ \text { VR3 } & \text { lin. } \\ \text { VR }\end{array}$
$\begin{array}{ll}\text { VR2 } & 500 \mathrm{k} \Omega \text { lin. } \\ \text { VR3 } & 50 \mathrm{klog} .\end{array}$
VR4 $500 \Omega$ l.n. w.w. preset

## Capacitors:

Cl Electrolytic Can, $50+50 \mu \mathrm{~F} 450 \mathrm{~V}$, high ripple rating
$\mathrm{C} 2 \quad 32 \mu \mathrm{~F}$
$\left.\begin{array}{ll}\text { C3 } & 16 \mu \mathrm{~F} \\ \mathrm{C} 4 & 16 \mu \mathrm{~F}\end{array}\right\}$ Tubular Electrolytics 350/385V
C5 $16 \mu \mathrm{~F}$
C6 200 pF Paper, 500 V
C7 $\quad 50 \mu \mathrm{~F}$ I5V electrolytic
C8 1000pF Paper, 500V
C9 $0.1 \mu \mathrm{~F}$ Paper, 500 V
ClO $32 \mu \mathrm{~F}$ Tubular Electrolytics $350 / 385 \mathrm{~V}$

## VRI $500 \mathrm{k} \Omega$ log

lytic $\qquad$

.

CI $8 \mu \mathrm{~F}$ Tubular Electrolytics 350 '385V
Cl2 $0.056 \mu \mathrm{~F}$ Paper, 500 V
C13 $50 \mu \mathrm{~F}$ I5V electrolytic
$\left.\begin{array}{ll}\text { CI4 } & 0.056 \mu \mathrm{~F} \\ \text { CI5 } & 0.056 \mu \mathrm{~F}\end{array}\right\}$ Paper, 500 V , matched pair
Cl6 $50 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic
Valves, Transformers, etc.:
VI ECC83
$\left.\begin{array}{ll}\text { V2 } & \text { EL84 } \\ \text { V3 } & \text { EL84 }\end{array}\right\}$ matched pair
D1 Selenium Bridge Rectifier B250C80
D2 Selenium Bridge Rectifier B300CI 50
TI Mains Transformer, $250 \mathrm{~V} 200 \mathrm{~mA}, 6.3 \mathrm{~V} 2 \mathrm{~A}$, 6.3 V 4 A

T2 Smoothing Choke $10 \mathrm{H} / 125 \mathrm{~mA}$
T3 Hi-Fi Output Transformers for $2 \times$ EL84 in Class A Secondary for $7 \frac{1}{2}$ ohms, push-pull
Switches:
SI 2 pole On/Off Toggle Switch, Mains 2A rating
S2 Ceramic 2-way rotary switch, 8 pole 2A, 500 V

## Loudspeakers:

WB "Stentorian" HFIO16

## Miscellaneous:

Panel Pilot Lamp, Red. Insulated Panel Fuse (Mains). Four knobs. Three Noval Valveholders, Ceramic, I with screening-hood (steel). Thirteen Rubber Grommets, $\frac{1}{3}$ to $\frac{1}{2}$ in. diameter. Two pairs insulated Wanderplug Sockets (Red/Black). Approx. 3 yards 4 -core Power Cable, 15A. Approx. $4 \frac{1}{2}$ yards flexible thin coaxial screened cable, PVC outer coating (quality microphone cable). Tagstrip, bolts, connecting wire, solder, etc. Aluminium sheet, $\frac{1}{16}$ in., for Chassis, Panel Plate and Cleats. (Approx. $16 \times 10 \mathrm{in}$. piece, total needed.) $\frac{3}{16} \mathrm{in}$. plywood, approx. $4 \times 10 \mathrm{in}$. raw, for Control Panel. Insulating tape.


Fig. 5: The correct and incorrect methods of connecting chassis earths.

In general, the author is of the opinion that one need not be hypercritical in striving to get the hum-level in an amplifier so low that it is inaudible even under the most exacting circumstances, for as soon as any ordinary programme is playing at normal volume, slight residual hum is normally quite unnoticeable.

## Final Remarks on Wiring

Note the spaced arrangement of R3, R4 and R5 in Fig. 2. This is important, as these resistors will generate considerable heat. Note also the "grid" of bare earth wires strung between chassis-con-

## TABLE 2


necting tags (marked MC) under component fixing bolts. This is a very effective and convenient component earthing system, giving very high contact reliability.

In Fig. 3 and Fig. 4 can be seen the method of anchoring the cables, to prevent destruction of connections by pulling.

Note carefully the layout of components on the chassis, as shown in Figs. 2 and 3.

The mains'transformer and the output transformer are mounted as far apart as possible, and with the cores at right angles to each other. The amplifier components are mounted huddled-up in the opposite corner of the chassis to the mains transformer. The major heat-producers, V2, V3 and the mains transformer. are not placed in the immediate vicinity of each other. The input valve V1 is situated furthest of all from the power supply components.

It is advisable to operate the input valve V1 in a screening can, but this is very inadvisable for V2 and V3, as ventilation of these valves is thereby impaired, leading to overheating of the electrodes and early failure.
The radio/gram switch, $\mathbf{S} 2$, should preferably be a ceramic type with good contacts rated at 2 A each. It is 8-pole, 2-way, normally on two wafers; the depiction in Fig. 4 is as one wafer only for clarity. Those sections remote from VR3 should be used for the five a.c. switching functions. Three sections are wired in parallel for switching the heaters, to give ample surge rating when switching on the cold heaters of the tuner.

The four tagstrips on the panel are mounted on brass stand-off bolts on the plywood overlap, countersunk from the front. Those of the signal input tagstrip are earthed to the chassis plate, to prevent hand-capacity hum effects from the front. Others may be treated the same way, but this is an unnecessary complication. Note the positioning of tags for higher voltages towards the centre of the strips, for safety.

The amplifier/power-pack chassis and flying panel form an inseparable unit. The panel is intended for mounting with four bolts through the corners to the back of the cabinet top-panel, so that the controls appear through a suitable (smaller) cut-out in the latter.

The gram motor, tuner power supplies and signal from the tuner are connected with soldered joints on the flying panel tagstrips, removable for servicing. Mains input is also wired to the appropriate tagstrip on the flying panel. The pickup output goes to a socket on the tuner chassis. If the final stage of the tuner requires to be used as audio pre-amplifier, this valve must take h.t. and heaters ahead of S2.

## NEXT MONTH THE PRE-AMP WILL BE DESCRIBED

# ECHO CHAMBER FOR MICROPHONE OR ELECTRIC GUITAR 

By B. M. Jeffery


#### Abstract

In this instrument, reverberation is achieved by delayed playback from a continuous loop of magnetic tape. Details are given for constructing a special tape deck, together with details of a suitable amplifier and mixing circuit.


7HE amplifier used in this echo chamber is a modified Mullard type amplifier, but there is no reason why any other tape amplifier and record oscillator should not be employed if preferred. It should be noted that the amplifier and oscillator is used only for amplifying the input signal and for recording on to the tape; no playback switching or erase switching is needed. To obtain the correct echo an attenuator circuit is needed and is described later. A switch for selecting the playback heads is required. Output from the selected playback head is fed to a separate power amplifier, together with the original signal.

In the constructional diagrams all holes have to be drilled to take 4B.A. bolts, unless otherwise stated.

## Main Deck Plate

The main deck plate is made from a piece of立in. thick steel plate or a similar metal, size 10 in . x 8 in . The plate is drilled as Fig. 1. All holes marked " A", are drilled to take 2B.A. bolts, holes marked "B" are drilled to take tin. rubber grommets. The hole marked " C " is drilled to take the $\frac{1}{2} \mathrm{in}$. brass bush. The corners of the deck plate can be rounded slightly as shown in Fig. 1. The holes marked "A" on each corner are used for fixing the plate to the cabinet.

## Head Mounting Plate

This plate is made from $\frac{1}{6} \mathrm{in}$. thick brass size


Fig. 1: Dimensions of the main deck plate.

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| :---: |

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Fig. 2: The head mounting plate.
6in. $\times 1 \frac{3}{4} \mathrm{in}$. Brass was chosen because it is nonmagnetic and easy to drill. The plate is drilled as shown in Fig. 2. All holes marked " $A$ " are drilled to take 6B.A. bolts. The corners on this plate should preferably be rounded.

## Head Covers

These head covers are made from $\frac{1}{16}$ in. thick brass size 2 in . $x \frac{t}{5} \mathrm{in}$. (four required). The covers are drilled and then bent as in Fig. 3. It may be noted that if heads other than the ones stated are used the measurements of the covers will differ slightly. The heads are placed approximately 1 in . apart.


## The Erase Magnet

The mounting for the erase magnet is made from two pieces of $\frac{1}{\text { in }}$. thick brass lin. $x \frac{1}{2}$ in. These are drilled and assembled as in Fig. 4.


Material $1_{16}{ }^{4}$ thick brass 4-required

Fig. 3 (above): The heod covers.

Fig. 4 (right): The method of mounting the erose magnet.

Fig. 5 (below): The pressure pod arms.


At this stage one small brass pulley wheel is required, and this acts as a tape guide. Fig. 6(a) shows the size of the pulley wheel and how it is mounted. Fig. 6(b) shows an alternative type of tape guide which can be used in place of the pulley wheel. This is a fixed mounting, but it will be found that the pulley type is better as it allows the tape to be pulled through the heads more smoothly than this fixed type guide. At this stage the heads, erase magnet, tape guide and pressure pads are assembled on the head mounting plate as in Fig. 11.


Fig. 6 (above): a: Tape guide pulley assembly; b: alternative fixed-type guide.
Fig. 7 (below): Tension pulley assembly.



Fig. 8 (above): Motor drive wheel assembly.
Fig. 9 (below): Drive wheel and bush assemblies.



1 dia. brass bush drilled
$\because$ to clear $1 / 4$ dia spindle .

$I^{\prime \prime}$ dia brass drive wheel drilled to fit tight on spindle

## rension Pulley Assembly

This is made from $\frac{1}{5} \mathrm{in}$. thick steel, drilled and issembled according to details given in Fig. 7. A econd pulley wheel is used here, the size being he same as the tape guide pulley. A medium trength string is attached to one end and provides he tension necessary to keep the tape tight. All toles are drilled to take 4B.A. bolts.

## Motor Drive Wheel Assembly

This piece is made from 1 in. thick steel cut and Irilled as shown in Fig. 8(a). The rubber used is $\frac{1}{2}$ in. diameter. Another medium spring is used to eep the rubber drive wheel in contact with the notor and flywheel. Fig. 8(b) shows the completed ssembly.

## Drive Wheel and Bush Assembly

This bush is made from a piece of brass rod cut and drilled as in Fig. 9(a). The bush used in the prototype was obtained ready made from a light engineering firm. Fig. 9(b) and Fig. 9(d) show the construction of the drive wheel with the main spindle fitted. The drive wheel is made from a piece of lin. diameter rod. The wheel is made to fit tight on to the main spindle. A small screw can be fitted through the wheel to keep it tight, but this screw must be set well into the brass wheel to avoid scratching the tape. Fig. 9(c) shows the plane view of the brass bush. The holes marked "A" are drilled to take 4B.A. bolts which secure the bush to the main deck plate. The main spindle is cut from $\frac{1}{2}$ in. steel rod as in Fig. 11 (a).

## The Pressure Wheel Assembly

This is made from $\frac{1}{8} \mathrm{in}$. thick steel, cut and drilled as Fig. 10(b). All holes are drilled to take


Fig. 10 (above): Pressure wheel assembly.
Fig. II (below): Drive wheel and flywheel assemblies.


4B.A. bolts. A standard rubber pressure wheel size lin. diameter by $\frac{1}{2}$ in. thick is used. This is mounted as in Fig. 10(a). A medium spring at one end of the metal provides the tension against the drive wheel for the tape motion through the heads. At this stage the whole drive assembly and motor are mounted to the main deck plate. The completed assembly is shown in Fig. 11(b). Next the pressure wheel is mounted. Fig. 11(c) shows the flywheel, motor and drive pulley in position.

## Completing the Deck

The tension pulley wheel is now added to the deck together with the spring. Then the leads from the heads are connected to a small piece of tag panel mounted on the underside of the deck. The holes marked " D" in Fig. 12 are for the mounting feet which support the deck when it is in the cabinet. Three supporting feet are required and are made from $\frac{1}{4} \mathrm{in}$. steel rod, 4 in . long. The hole marked " $E$ " is used for mounting a twin connector or a piece of tag panel for the mains supply to the motor. Fig. 12 shows the completed deck with the tape in position. The tape used is the standard tin. type, and is joined by a piece of splicing tape to make a continuous loop.

## Adjustments

The adjustments for the bias level are carried out in the normal way. Other adjustments to the completed echo chamber can be made as required. The bias current through the record head should be 1 mA constant.


Fig. 12i The completed deck.

## The Amplifier

This amplifier is built in the normal way. Care should be taken when wiring the valve grids and heater chain, and these should be kept well away from each other to prevent hum pick-up. Three valves are used: EF86, ECC83 and EL84 (see Fig. 13). The EF86 low noise pentode is used for amplifying the input signals. The first section of the ECC83 double triode valve is used in the equalising stage, and the second section is used as the output stage when recording. The EL84 output pentode is used as the oscillator. An EZ8C full wave rectifier is employed in the power pack

## Input Stage

The EF86 acts as a voltage amplifier. It i possible to record from either microphone o.


Fig. 13: The main amplifier circuit.


Fig. 14 (above): Attenuator and playback circuits.


Fig. 15 (above): Power pack circuit.
Fig. 16 (below): Above-chassis layout.

guitar input sources. Both input are fed to the grid of the valve. Input two being attenuated by R1. The two inputs can be used at the same time if required.

## Equalising Stage

The first section of the ECC83 (V2A) is used only for equalisation purposes. The component values used in this part of the circuit may need to be varied to give the correct bass and treble response, according to the type of head used. Switches S1, S2 and S3 select the desired equalisation circuit. A low level output is taken from the anode load of this stage and is taken to the attenuator circuit (Fig. 14).

## Recording Stage

The output from the anode of the equaliser stage is taken to the grid of the section of the ECC83 via the gain control VR1. Further high frequency boost is added to the recording signal by C14 and R20, in the cathode circuit of V2B. The recording signals are taken from the anode of this stage via a parallel-T network to the recording head. Bias is fed to the recording head immediately after the $T$ network.

## H.F. Oscillator

The bias signal is fed to the recording head via the 82 pF capacitor C22. The valve of this capacitor determines the bias current flowing in the head. The bias voltage is obtained from the anode of the EL84. The oscillator coil and oscillator component values will depend on the type of recording head used. The record head used in' the author's model had an impedance of $300 \Omega$.

## Attenuator and Playback Circuit

The attenuator is a straightforward circuit using three resistors and a capacitor (Fig. 14). The input to this circuit is taken from the anode of V2A (junction of R16, R17). The original signal is thus attenuated and then combined with the output from the playback heads to form the echo required. Switches SI-S4 allow the playback heads to be switched simultaneously as required. Switches A and B are closed with the switch in S4 position. The playback signals and the orginal signals are fed to the main power amplifier.

## Power Pack

This is an ordinary power-pack and is wired as shown in Fig. 15. The transformer used is a standard type with a $300-0-300 \mathrm{~V}$ 250 mA h.t. winding and two 6.3 V heater windings.

so I suggested four $15 \Omega$ new models, and suggested that the slight mismatch would not be noticeable, and I pointed out that I thought that the removal of a single point source of sound, and the new distribution of sound might give. him an improved performance.

I have not yet ceased to hear what a miracle this has performed in the set. It certainly has improved reproduction, giving a much rounder tone without the "hole in the wall" effect, and the top definitely sounds much brighter. Probably ideas on this line might be tried in other vintage models with advantage, but I certainly did not expect it to have worked such an improvement in reproduction on an old set.

## A Future Trend

I recently read a news item (from America!) that a new infra-red camera had been developed which could photograph the immediate pastduring a test some cars were driven from a car park, the camera was set up, and took pictures of the cars which had vacated the site!
Some years ago a technician, also from America, decided (and I believe proved-or was it in a radio play?) that when a transmission is sent out it goes round and round the earth gradually attenuating, but never completely dying out. Will we next hear that a radio or circuit has been demonstrated which can pick up yesterday's signals from the jumble which must be whirling round our earth?
Probably if the transmitter closed down immediately the signal had ceased, a very sensitive set could pick up a weak signal, say after two or three circuits of the earth, but surely next time round it would mix with the outgoing signal on the wavelength.

Come to think of it, perhaps this is the cause of some of our distortion-some of yesterday': signals modulating those of today. Who woulc like to bet how long it will be before a set is announced which receives old signals?

## Modern Music

It is a long time since I mentioned anythin! about modern music, as I fully realise that thi modern generation "have much different ideas ol this subject than us "old 'uns", but I have becom. increasingly appalled at the incessant repetitious ness of modern music-not only the melody (i) you can call it that), but the words.
In addition to constant repetition of notes o short themes, the words, too, seem to go on and or line after line. Have the writers taken an easy wa; out, or is this some modern trend? I will not dea with the splitting-up of a single-syllable word int many-syillables-You-who-who-who etef


HAVING become interested in 8 mm cine hotography last summer I found that there was 10 commercial amplifier available on the market which provided the facilities that' were needed for Idding sound commentaries at a reasonable cost. The amplifier to be described was therefore lesigned and built primarily for this purpose, but $t$ has many other uses as a compact, good quality undio amplifier and mixer. The main requirements hat were needed are as follows:
I. Good quality output of 3 to 4 W suitable for use at home or occasionally in a small hall.
2. Microphone input with its own independent volume control.
3. Music input (from gram or tape-recorder) with its own independent volume control.
4. Ability to "mix" these two inputs as required. This enables a background of music to be fed into the amplifier while at the same time a spoken commentary can be super-imposed.
5. A simple but effective tone cohtrol to cater for different room conditions.
6. The final design had to be sturdy and compact for transporting, have a smart appearance, and be readily accessible for any maintenance that might be required.
One additional feature was added during the actual building and this provides a bonus item. A tape outlet socket was fitted so that music from records or other source, together with a superimposed spoken commentary, could be recorded.
Considerable care has been taken in designing the layout of the amplifier and the wiring to give the best results together with a clean, neat, work-


Fig. I: The circuit.

# ne-movie amplifier 

By S. COLLINS

## 2AL PURPOSE 4W AMPLIFIER WITH AND OTHER SPECIAL FACILITIES

manlike appearance. This has also made for an easy 'straightforward sequence of assembly and wiring up:
The chassis is constructed from 18 s.w.g. aluminium, which was found to be quite rigid enough when formed into the two-sided channel section as shown. The dimensions and drilling details are given in Fig. 6 and these should be closely adhered to.
The next step is to mount the main components
on to the chassis, starting with the three valveholders, noting that the special anti-microphonic holder is fitted in position V1 and a solder tag is fitted under the fixing nut nearest to the edge of the chassis. These holders are mounted from above the chassis and careful reference should be made to the wiring diagram to ensure that the gap between pins 1 and 9 on each one corresponds exactly with the drawing.
Next fit the mains transformer, making sure by the coloured wires that it is the correct way round, and at the same time secure a seven-way tag strip under the two inner nuts. Before these fixing nuts and bolts are fully tightened it may be advisable to fit the clip for the $50+50 \mu \mathrm{~F}$ electrolytic as the fixing screw for this comes quite close to the lower edge of the transformer. The flying leads from the transformer should be passed through their respective holes in the chassis and, to protect them, a rubber grommet should be slipped over them and fitted into the chassis.

Place the $.50+50 \mu \mathrm{~F}$ electrolytic capacitor into

## COMPONENTS LIST

## Resistors:

| RI | 4.7M $\Omega$ 1 W 5\% high stability |  |
| :---: | :---: | :---: |
| R2 | $390 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 5 \%$ | high stability |
| R3 | $100 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 5 \%$ | high stability |
| R4 | $15 \mathrm{k} \Omega 2 \mathrm{~W} 10 \%$ |  |
| R5 | $470 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 10 \%$ |  |
| R6 | $470 \mathrm{k} \Omega$ i ${ }^{\text {W }} \mathrm{W} 10 \%$ |  |
| R7 | $470 \mathrm{k} \Omega \stackrel{1}{2} \mathrm{~W} 10 \%$ |  |
| R8 | $3 \cdot 3 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 10 \%$ |  |
| R9 | $220 \mathrm{k} \Omega$ / W 10\% |  |
| R10 | $390 \Omega 2 \mathrm{~W} 10 \%$ |  |
| RII | $470 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 10 \%$ |  |
| R12 | l.5k $\Omega$ IOW 5\% | wire wound |

## Capacitors:

| Cl | $0.05 \mu \mathrm{~F} 500 \mathrm{~V}$ |
| :--- | :--- |
| C 2 | $0.25 \mu \mathrm{~F} 500 \mathrm{~V}$ |
| C 3 | $4 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic |
| C4 | $0.05 \mu \mathrm{~F} 500 \mathrm{~V}$ |
| C5 | $25 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |
| C6 | $25 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |
| C7 | $0.05 \mu \mathrm{~F} 500 \mathrm{~V}$ |
| C8 | $0.05 \mu \mathrm{~F} 350 \mathrm{~V}$ |
| C9 |  |
| C10. | $50 \mu \mathrm{~F} \times 50 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic |

## Controls:

VRI $500 \mathrm{k} \Omega \log$. (microphone volume)
VR2 $500 \mathrm{k} \Omega \log$. (gramophone volume)
VR3 $50 \mathrm{k} \Omega$ lin. with D.P. switch (tone control)

## Miscellaneous:

Three coaxial sockets. One Bulgin Dl 80 signa! lampholder. One Bulgin J2 open jack socket.

One Belling Lee L575 miniature fuse-holder. One Belling Lee L562 IA mini-fuse. One Bulgin P360 mains plug and socket. Three Eddystone 841 knobs and dials. One 12 -way Radiospares group board. (std.). One backing plate for above. Two $\frac{1}{2} \mathrm{in}$. grommets. Two $\frac{3}{8} \mathrm{in}$. grommets. One $1 \frac{3}{8} \mathrm{in}$. condenser clip (vertical $\mathrm{mtg})$. One tag strip, 2 insulated, earth, 2 insulated. One tag strip, earth, 3 insulated, earth, I insulated. One tag strip, earth, 5 insulated, earth. Twelve 6BA nuts, $106 B A \frac{1}{4} \mathrm{in}$. screws, 2 6BA $\frac{1}{2}$ in. screws. Twelve 4BA nuts, II 4BA $\frac{1}{4}$ in. screws, I 4BA $\frac{1}{2}$ in. screw. Two 6BA solder tags. One 6.3 V 0.3 A mes pilot lamp.
Valves:
VI EF86 V2 ECL82 V3 EZ80
Chassis:
18 swg aluminium, size $10 \times 3 \times 2 \frac{1}{2} \mathrm{in}$.
Valve-holders:
One B9A anti-microphonic
Two B9A plain moulded
Mains Transformer:
Electro Voice No. I04F
H.T. $\quad 250-0-250$ volts at 65 mA
L.T.I $\quad 6.3 \mathrm{~V}$ IA
L.T. 2 6.3V IA

Output Transformer:
Electro Voice No. II7E
Primary $5000 \Omega$
Secondary. 3 and $15 \Omega$
Additional items:
Solder, wire, sleeving, 3 -core mains•leads, ete.


Fig. 2: The front of the group board wiring.
the clip and press well down on to the chassis. Before tightening check that the position of the tags corresponds with the diagram and if necessary slightly bend them to give good clearance from the edge of the hole.
The output transformer can now be mounted by means of four 4B.A. nuts and bolts, and here also care should be taken to see that this is the correct way round according to the coloured leads. A sixway tag strip is secured under two of the fixing nuts as shown in the wiring diagram and this will accommodate the transformer secondary connections, allowing an easy adjustment from 3 to $15 \Omega$ output impedance.

Turning now to the front panel of the chassis, these components can be fitted. First the three coaxial sockets (not forgetting the 6B.A. solder tag


Fig. 3 (obove): Rear of group board wiring.


Fig. 4 (left).: Loudspeaker/output transformer connections for $15 \Omega$ speaker.
Fig. 5 (right): Loudspeaker/output transformer connections for a $3 \Omega$ speaker.
under one nut of the first one which is for the microphone). Next fit the pilot light, fuseholder, output jack socket and the mains input connector as shown in the diagram.
(To be continued)


Fig. 6: Chassis drilling details.

(Continued from page 800 of the January issue)

$\checkmark$HE m.w. coil for the r.f. stage is L4, and the aerial trimmer is mounted directly on the front runner. Other components are located as in Fig. 3. The anode lead of V1, from tag 3, passes directly through the screen, to wafer 4.

C 1 is connected to a tag near the screen and L4, and a tag is fitted to this bolt above the chassis, and is wired to the rotor contacts adjoining VC1A. C1 is positioned as in Fig. 3, to give a short lead to the smallest coil, L1.

The aerial lead from the coaxial socket SK1 on the chassis is screened, and brought to wafer 1.

## Jther Wavebands

The other coils may now be added. Four sands are provided:

Band 1, $19-8 \cdot 5 \mathrm{Mc} / \mathrm{s}$, or approx. $16-35 \mathrm{~m}$.
Band 2, $9-3.5 \mathrm{Mc} / \mathrm{s}$, or approx. $33-85 \mathrm{~m}$.
Band 3, $4-1.4 \mathrm{Mc} / \mathrm{s}$, or approx. $75-210 \mathrm{~m}$.
Band 4, $1.55 \mathrm{Mc} / \mathrm{s}-550 \mathrm{kc} / \mathrm{s}$, or approx. 200 550 m .
The coils are so positioned as to obtain short viring for the smaller coils, and particularly for 3and I coils. Referring to Fig. 3, the coils are:

|  | Aerial | Frequency changer | Oscillato |
| :--- | :---: | :---: | :---: |
| Band 1 | L1 | L5 | L9 |
| Band 2 | L2 | L6 | L10 |
| Band 3 | L3 | L7 | L11 |
| Band 4 | L4 | L8 | L12 |

If the coils are positioned with their flat sides s in Fig. 3, much of the wiring to one coil will e a duplicate of that to the others. Leads to L1, 5 and L9 must be short and direct. C5 is wired lirectly to L5, L6 and L7, and is taken to a tag olted to the chassis. A lead passes from this oint to the rotor contact adjoining VC2A.
Short leads pass from the coils, to chassis. If referred, coils for one band may be inserted at time, and the receiver may be tested. This will void any possible confusion in wiring.

## econd I.F. Amplifier

This is V4, and can be wired up complete. A ining meter can be used with the receiver, or the no sockets provided for this item can be shorted ith a length of wire.
The automatic volume control circuit leads re run close to the chassis. The h.t. positive line ires are also kept near the chassis. It is elpfal to use sleeving of suitable colours, such as :d for the h.t. positive line, and brown or some

# General Purpose COMMUNCATIONS RECEVER 

other colour for the a.v.c. line. Circuits can then be identified more easily.
The IFT's are appropriately wired. Those used had coloured leads, but some have tags or pins. The maker's data will show anode, h.t. a.v.c. and grid connections, which should be followed.

## I.F. Filter

This is formed by IFT1 and IFT2, these two transformers being mounted on a small chassis made from aluminium, as in Fig. 1. C11 is of very low capacity, and can be made by twisting together insulated wires, if preferred.

The primary of ITF1 is taken to $V 2$ anode and h.t. line (R7) as shown for an ordinary circuit. The secondary of IFT2 goes to a.v.c. line and V3 between the "grid" tag of IFT1 and the "anode" tag of 1 FT2. The a.v.c. tag of IFT1 and h.t. tag of IFT2 are joined, and taken to chassis.
C16 is wired from IFT2 to chassis, and R10 is also included in the i.f. filter. A lead from R10 passes through the receiver chassis to the a.v.c. line.
The filter assembly is bolted to the chassis, and holes are required so that the lower cores of the IFT's may be reached by means of a long insulated blade. A plastic knitting needle, suitably shaped. will do for this purpose.

## Screening

Adequate screening is required, or the receiver will oscillate when VR1 is adjusted to maximum sensitivity. All valve cap leads are screened, as in Fig. 1. The braiding is taken to the chassis, or other direct earthing point.

When clear glass valves are used, it will be found necessary to fit valve cans round V2, V3 and V4. Valves of many types can be used in the receiver, and they may be of dissimilar size, shape, or may differ in the screening arrangements. The suffix "G" and "GT" indicates glass, and glasstubular valves, while the omission of this indicates a metal valve. For example, 6 K 7 G valves are of the usual glass shape, while 6K7GT valves are the shorter tubular type. These valves, and a metal type $6 \mathrm{K7}$, are otherwise the same.

Underneath the chassis, anode and grid leads


Fig. 3.-The layout of components on the underside of the chassis


An underchassis view of the recelver
should be short and direct, and clear of each other, to avoid back coupling. If oscillation tends to begin when the IFT's are aligned, this shows that screening in these stages is inadequate, or that wiring is too long.

In the audio circuits, the grid lead (cap) of V5 must be screened and also the leads from V9 to the noise limiter switch, and C25. If this screening is omitted, some hum may be heard on signals.

## B.F.O.

The beat frequency oscillation is required only for the reception of c.w. morse, and it is built in a screening can, as in Fig. 5. An unused can, as obtained from a fairly large surplus i.f. transformer, is satisfactory. A piece of aluminium forms a bracket, to hold the coil to the variable capacitor VC4. as in Fig. 5. The unit should be tested before fitting it in the screening can, as it is secured by the nut holding the variable capacitor. Leads pass down through the chassis, to V8.

As the IFT's are aligned to $470 \mathrm{kc} / \mathrm{s}$, the b.f.o. can best tune from about $467 \mathrm{kc} / \mathrm{s}$ to $473 \mathrm{kc} / \mathrm{s}$, to give an audio beat note of up to $3 \mathrm{kc} / \mathrm{s}(3,000$ cycles) with the b.f.o. placed either side of the intermediate frequency.

The b.f.o. coil can be a surplus $470 \mathrm{ks} / \mathrm{c}$ IFT winding, in which case C36 will generally be present, and a suitable range should be achieved by adjusting the coil core. The variable capacitor VC4 only needs to be of small value, and 15 pF should suffice. Exact results depend on the value of C36. Provided the b.f.o can be tuned to produce a good audio note, the exact value of the variable capacitor is not important.

To obtain oscillation, a cathode tap is used, marked B. With some coils, a turn can be prised up, bared, and a thin lead can be soldered to it. If this is impossible, extra turns can be added, wound in the same direction. The tap is then the junction between the existing winding and the new turns, while $A$ is the beginning of the existing winding, and C is the end of the new winding. Only a few turns are required. This, again, depends on the coil, but ten turns should be adequate.

To test the b.f.o, an ordinary broadcast station can be tuned in. The b.f.o. is then switched on, and VC4 and the coil core can be adjusted until an audible beat note is heard.

Any other coil tunable to $470 \mathrm{kc} / \mathrm{s}$ (about 640 m ) is also suitable. If the coil does not have an adjustable core, C36 should be a preset trimmer, alternatively the total capacity needed can be made up by means of preset and fixed capacitors in parallel.

The coupling capacitor C39 is of very small value, and can be made from twisted insulated wires. If so, tune in a fairly weak c.w. signal, and adjust the coupling or twist, until a good audio note is obtained. The value is in no way critical.

## D.D.T. and Output

Wiring to the double-diodetriode V5, and output stage V6, will be quite straightforward.

As a loudspeaker with suitable output transformer fitted to it was used, no output transformer was included in the receiver. Two sockets, as shown in Fig. 3 allow the loudspeaker to be connected. The receiver should not be switched on with V6 inserted, unless the loudspeaker with transformer is connected. If a loudspeaker without transformer is to be used, the transformer can be incorporated in the receiver, near the mains transformer. In this case, the transformer primary is wired to tags 3 and 4 of V6, and the secondary is taken to the loudspeaker sockets on the rear chassis runner. The transformer ratio for a $2-3 \Omega$ loudspeaker is approximately $45: 1$.

## Noise Limiter

This is V9, and the switch shorts pins 3 and 4 when the limiter is not in use. The marker/limiter


Fig. 4-Details of the switch wiring.
switch is shown in Fig. 4 and one section of the switch is connected as indicated. Leads to the associated resistors should be short and direct, and all wiring here should be clear of the heater circuit. When the limiter is out of action, results should be normal. This setting of the switch is employed for general reception.

Noise of a static nature will often be encountered, especially on some short-wave bands, and the limiter switch may then be turned to the central position. There should then be a considerable reduction in noise level.

## Tuning Meter

The tuning meter can be plugged into the sockets provided, which must be shorted when no meter is used. A satisfactory meter of simple type can be arranged by taking the leads to a 1 mA instrument, with a shunt which will allow the meter to read full-scale, with VR1 at maximum sensitivity, and no signal tuned in. The shunt can be made from a length of resistance wire, or a preset wirewound resistor or potentiometer may be employed. The actual type of meter is of no importance, provided its full-scale reading is less than the a node current of V 4 , so a 5 mA instrument is also suitable.
When a signal is tuned in, the meter reading will fall. Correct tuning is therefore that giving the lowest reading. When trimming and aligning, adjustments can be directed towards obtaining the lowest meter reading, as this gives a more accurate indication than can be achieved by ear.
Any modification which changes signal strength will alter the meter reading, so it is easy to compare the results obtained with different aerials, and so on.

A test meter set to its 10 mA or a similar range, may be employed as a temporary tuning meter. Readings will depend on the aerial and other factors, but a change in current of some 5 mA should be expected, with a strong signal.

A bridge circuit meter can also be used. This is rather more complicated, and by no means essential. A typical circuit is shown in Fig. 6. Here, the meter reads zero, with no signal. and the reading rises in proportion to signal strength.

## Crystal Marker

The crystal used was a $100 \mathrm{kc} / \mathrm{s}$ type, with octal base, to fit an octal valveholder. If crystals with a different pin arrangement are used, the holder should be chosen to suit.

V7 is the marker valve, and Fig. 4 shows the marker switch wiring. TC2 is an air-spaced 100 pF trimmer, totally insulated from the chassis. An air trimmer can be held with 6B.A. bolts. A small air-spaced variable capacitor of ordinary type can be mounted on a strip of paxolin. which is in turn held to the chassis by long bolts having extra nuts. or spacers. The spindle should be slotted, so that it can be adjusted with an insulated blade.
If the receiver has a long-wave band, obtained by wiring in three l.w. coils, to spare switch contacts, the BBC Light Programme on $200 \mathrm{kc} / \mathrm{s}$ $(1,500 \mathrm{~m})$ may be used to check the crystal frequency. If there is no l.w. band, the standard frequency transmissions radiated on $2.5 \mathrm{Mc} / \mathrm{s}$ ( 120 m ) may be used for this purpose. For most easy choeking, the signal obtained from the
marker should be of somewhat similar strength to the signal of the station used as a frequency standard. It may thus be necessary to disconnect C34, and probably use a short, temporary aerial, if receiving the Light Programme. This depends on the signal strength, and is not critical, except that adjustment is difficult if signals are not of somewhat similar power.
With a $100 \mathrm{kc} / \mathrm{s}$ crystal, the marker signal will appear at $100 \mathrm{kc} / \mathrm{s}$ intervals throughout the tuning ranges, growing weaker as higher harmonics are used. To check crystal frequency, tune in the station chosen, and switch the marker on. Any difference between the marker harmonic and tation frequency will be heard as a low audio


Fig. 5 (above)-The beat frequency oscillator.
Fig. 6 (below)-The bridge tuning meter.

tone, and it may be only a few $\mathrm{c} / \mathrm{s}$. TC2 is adjusted to bring the marker crystal to zero beat, or nearly so. No further adjustment is required.
In normal use, the marker provides exact calibration points. For example, the 80 m amateur band extends from $3.5 \mathrm{Mc} / \mathrm{s}$ to $3.8 \mathrm{Mc} / \mathrm{s}$ and marker harmonics will appear on $3 \cdot 5 \cdot 3 \cdot 6,3 \cdot 7$ and $3.8 \mathrm{Mc} / \mathrm{s}$. A bandspreading scale will show this smaller divisions being equally spaced.
The bandsetting scales can be marked at $100 \mathrm{kc} /$ s intervals, with bandspread capacitor pointel vertical. To calibrate the scales, remove the aerial On the s.w. bands, markings at $500 \mathrm{kc} / \mathrm{s}$ points will suffice. High $100 \mathrm{kc} / \mathrm{s}$ harmonics become very weak, and closely spaced. A $500 \mathrm{kc} / \mathrm{s}$ or $1 \mathrm{Mc} / \mathrm{s}$ crystal avoids this, but is not suitable for lowel frequency calibration. If required, $500 \mathrm{kc} / \mathrm{s}$ check
(Continued on page 950)

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No. I-D.C. Stabilisation of Transistors

ONE hears a good deal from time to time about the troubles experienced by people experimenting with transistors.

There is no lack of information about the technical aspects, for those whose maths are up to it. But one aspect appears to have been neglected; that is: the precise know-how of how to handle them in practice.

This is not altogether a simple matter. Transistors pose problems which are not quite the same as valves. It can be even less simple if the theory of their operation is incompleteiy apprehended and, indeed, most of the literature on this subject pre-supposes a technical knowledge at least up to H.N.C. standard.

In consequence, one hears complaints about transistors "ruined in soldering them"; or already defective when bought; of circuits which don't work, or which " run hot".

These problems are not limited to amateurs. As an example we know of at least one commercial firm manufacturing transistorised apparatus which complained that $50 \%$ of its diodes were defective when supplied-there was, of course, nothing wrong with the diodes but there was a great deal wrong with the firm's "experts", trained, no doubt, on valve circuitry, who hadn't a clue when it came to transistors and whose own methods of testing them were in fact causing the damage.
Really there is nothing mystifying about transistors once you get used to handling them. But you do have to know your way around and it is probably true that the "way around" is only now beginning really to be understood even by the people making them.

## SOLDERING METHODS

For instance, this question of soldering. Transistors will stand up to the iron, properly applied. What they will not stand is too much heat applied for too long a time. They should be "spotted" on; a quick, clean joint made first time and finished with. (Tin the terminal and sweat the transistor lead to it quickly and cleanly.)

Transistors are made with long leads-leave them long. Sleeve the leads so they won't short to the rim of the capsule. If the joint is made quickly and the iron removed before it has time to damage the transistor there will be no trouble.

Huld the transistor lead close to the iron with a pair of long nosed pliers during the operation, the pliers will draw off the heat and stop it running up the lead to the transistor. But speed is the essence of the job.

In fact far fewer transistors are ruined in solder. ing than is generally supposed.

But they won't stand up to being put in, taken out again, put in again, on that score howeverwhat will? With all electronic soldering the secret is "once only", and finish!
Diodes are often soldered with a spring in them again a precaution against heat. That is, a loop is made in the lead and this loop is held in the nose of the pliers while soldering.
A final point, transistors can be spoiled by light. too ... if the capsule is glass it will be painted


Fig. I (left)t Here the moin flow of current is fronpositive to negotive.
Fig. 2 (right): Here there are two currents flowing
to exclude light. Don't scratch the paint. If the capsule is metal that problem does not arise.
In order to handle transistors properly it is essential to understand how they work.

The transistor is basically a development of the old cat's whisker crystal except that hertzite or galenium crystals would not amplify, whereas the transistor does. Its properties are those of a solid

The basis of the thermionic valve is that current passing through it from anode to cathode can be made a function of the grid, that is, it can be controlled in amplitude by conditions on the grid In the transistor, current passing through it in one direction can be made a function of current passed through it in another-can be controlled ir amplitude by varying the conditions of the seconc current.

But here the analogy between valve and $\operatorname{tr} \boldsymbol{n}$ sistor ends. The valve is a voltage device, controlled and operated by volts. The transistor is a
current device, controlled and operated by current. One finds that it is here that people seem to meet with the greatest difficulty in understanding how a transistor functions. It must be admitted that the majority of technical literature is not very easy to understand on this issue.

## BIAS ARRANGEMENTS

A transistor must be biased just as a valve is. But not by volts. A transistor is biased by the amount of current put through it. An understanding of this process is an absolute necessity if you are going to do anything with transistors at all. Most of the phenomena which cause so much trouble to the inexperienced spring from this factor; most of the peculiarities of the transistor are rooted in it, so are the difficulties that probably arise when trying to find out what is wrong with a piece of transistorised apparatus which refuses to work properly.

Consider Fig. 1. There is a collector, an emitter and a base. For the nonce these may be regarded as analogous to the anode, the cathode and the grid of a valve provided it is always remembered that in transistors the anode (or collector) is negative; that its voltage is likely to be of the order of only some 4.5 instead of the two or three hundred you would find on the anode of a valve and that, whereas varying the voltage on the anode of a valve would have a considerable effect upon the amount of current which would flow in the anode-cathode circuit, in the case of the transistor, once you have exceeded the minimum rated voltage-somewhere around half a volt perhapsit does not matter how many volts you put on the collector up to the rated maximum, the current flow in the collector-emitter circuit will be substantially the same whatever the collector volts.

In Fig. 1 the main flow of current in the battery circuit will be through the emitter, into the transistor, out of the collector and back to the battery $\ldots$ from positive to negative, that is, using the normal terminology. This current will be of an order of milliamperes or even amperes.
It has already been said that this current does not depend upon the voltage on the collector. On what, therefore, does it depend? Returning to the valve analogy again for a moment, it depends upon conditions on the base, which functions here as the control grid of a valve.
How does it control? In the valve the control grid would be a few volts negative or positive to the emitter (cathode), thereby causing the collector-emitter (anode-cathode) current to be greater or less as the case might be. Not so with the transistor!

## BASE CURRENT

Consider next Fig. 2. Here is included a second battery, B2, sensed so as to make the base. while remaining positive in relation to the collector, slightly negative in relation to the emitter. Current will now flow through the transistor through a second path-namely, from emitter (positive) through the transistor and out of the base (negative). There are now two currents flowing through the transistor simultaneously. Rather as there would be in a valve if grid current was allowed to flow.
It is this second current which biases the transistoc.


Fig. 3: The battery, B2, of Fig. 2 is replaced here by o resistor.

The value of the current which will flow in the collector-emitter circuit is a function of the value of current flowing in the base-emitter circuit. Varying the current in the base-emitter circuit will cause proportionate but greatly amplified changes in the collector-emitter circuit.

This may still appear to be voltage biasing . . . since there needs to be volts on the base to obtain it, obviously. Avoid thinking that way . . . it is the current through the base which operates the transistor; with no current there would be no bias.

So far the picture presents no particular difficulty. In order to obtain the standing quiescent d.c. current in milliamperes or amperes required in the collector circuit then all that needs to be done is to pass a definite value of current through the transistor via the base-emitter circuit. Having stabilised the d.c. or quiescent conditions by selecting the correct base-emitter current to give the quiescent collector current wanted, if now an a.c. signal is fed in between emitter/and base the r.m.s. variations on the base will vary the base potential. thus vary the base current, which will in turn vary the collector-emitter circuit current. Owing to the resistance of the transistor in the collector-emitter sense being greatly more than its resistance in the base-emitter sense the variations in the output will be greater, that is amplified, than those in the input. As the base-emitter current/collectoremitter current transfer characteristic is substantially a straight line over the operating part of the curve the amplification will be substantially linear.
From here the picture complicates somewhat. To begin with, while the current in the collectorcircuit will be of the milliampere order, the current required in the base-emitter circuit to procure it is only of the order of microamperes. In order to obtain a current of microamperes, obviously the voltage required on the base to produce it will be microvolts.
This presents one of the difficulties experienced by the trial-and-error experimenters. To obtain a bias of, say, 200 microvolts on the base (in relation to the emitter, which in the diagrams is shown taken direct to earth, which is positive) is not quite the same thing as getting, say, 3 V on the grid of a valve!

A further difficulty arises in that this voltage is critical. If the base is a couple of hundred microvolts more negative than it should be the current in the collector circuit rises above the safe limits and the transistor may be ruined; 200 microvolts less than it should be and no current flows at all -the transistor is "cut off". There are other phenomena, too, which we will leave for the moment. First let us go ahead and see how we get that microvolt bias on the base.
In Fig. 3 the battery B2 is replaced by a

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Fig. 4: Here RI is extended, thus making a potential divider.
resistor (R1) from the negative line of the supply. Now, on the assumption that we want a current of $200 \mu \mathrm{~A}$ through the base-emitter path and we have a voltage of -9 V on the supply line (with the emitter at 0 V positive), and the published data for the transistor in question tells us that in order to get a base current of $200 \mu \mathrm{~A}$ we need a negative potential on the base of, say, $200 \mu \mathrm{~V}$, it is a simple matter to calculate what value of resistor, R1, will be needed to drop -9 V to $-200 \mu \mathrm{~V}$. That is, to drop the whole nine volts except the odd $200 \mu \mathrm{~V}$.

Provided the resistor is accurate-and it will have to be accurate within $1 \%$-the correct conditions will be obtained. Also provided the resistor is high stability and does not vary under load the conditions will remain stabilised. The correct d.c. base current will flow to produce the correct required collector current-somewhere in the centre of the output curve probably. If we feed an r.m.s. signal in at the points $X-X$ across base and emitter it will swing the base current and an amplified and linear copy of it will result in the collector circuit. Provided, of course, that it does not swing the base so far negative as to cause the collector current to exceed its maximum or too far positive so as to stop collector current flowing altogether - "clipping" and "bottoming", which will be dealt with later.

## DOWN TO MICROVOLTS

For the sake of the experts who may be reading this we will not complicate matters by considering "leakage currents" at this stage.

Sufficient should have been said to make this matter of current bias clear to those who may not completely have understood it and also to point what is one of the first hurdles to the man who wants to experiment with transistors ... that we are dealing with microvolts on the base, not volts, and they must be precise! It is not very easy to obtain microvolts within fine limits by a process of trial and error. With transistors, therefore, the thing is to make precise calculations first, then make sure that all one's components, especially resistors, are accurate and will remain so under operating conditions. If calculations are correct there is no reason why apparatus should not work for the first time of asking-which will be a great deal easier than trying to find out why it doesn't work, as may be the case if trial-and-error methods are used.

The values given here are, of course, only approximations, nor do they include leakage currents, but all the essential information is in the published data for any actual transistor, although there are many circuits in which the bias is obtained in the manner just explained; this method
is wholly unsatisfactory in practice! If anything goes the slightest degree wrong there will be more transistors burned out-without the aid of the soldering iron.

Which leads to a consideration of certain peculiarities of transistors. These are: impedances, temperature effects, transistor spreads . . . the whole question of d.c. stabilisation.

## IMPEDANCE EFFECTS

Consider again the circuit in Fig. 3. The value of volts dropped by the biasing resistor R1 must depend upon the amount of current through the base, which will be the sum of the leakage current for that particular transistor and the actual current at the bias volts. The leakage current can be taken as the current which would flow if the collector were open circuited, but at this stage that may be ignored. The amount of current flowing through the base will depend upon the resistance or impedance of the base-emitter internal path through the transistor.

Now a transistor is not resistive- that is, it does not obey Ohm's law. Therefore this impedance is not stable. In fact it varies with frequency (considering d.c., we are at zero frequency, of course), it varies in sympathy with the output impedance, which is also not stable. It varies under load. Also it varies from transistor to transistor due to production spreads, which can be considerable, hard though the manufacturer tries to keep them within close limits.

This means that the input impedance is going to vary during operation and is unlikely to be identical between different transistors. Therefore the base biasing potentials are going to vary during operation and,- if a transistor has to be changed, the conditions set up for one may be miles out for the new one. One cannot afford to be miles out with transistors.

A reasonably stable bias is needed on the base, one which will not vary greatly from transistor to transistor and one which is as little dependent upon the varying impedance of the base itself under load as possible. This cannot be obtained by using the series resistance shown. Every variation in base impedance, and therefore in current, is going to cause considerable variation in the voltage dropped across the resistor, which must be large in order to drop the necessary volts at a current of only microamps.

There are a number of recommended ways of obtaining a reasonably stable condition on the base each with its own particular merits or demerits for certain applications ... but we are going to confine ourselves to the preferred method.

The resistor R 1 is extended by means of a second leg, R2, to earth (emitter), thus making it into a potential divider (see Fig. 4). Consider this condition: if the impedance of the divider is made sufficiently low it will swamp the impedance of the transistor under drive and the voltage at the base tapping will remain reasonably constant regardless of the current taken by the base or, more properly, regardless of variations in it, which will be small in comparison to the current taken through the divider as a whole.

That is, the potential at the tapping point can be made more dependent upon the total current through the divider than it is upon the amount drawn by the base. Changes in transistors will also have much less effect. Thus there is a reason-
able degree of d.c. stabilisation of conditions on the base!

## TEMPERATURE EFFECTS

A transistor is not stable against heat. Transistors are rated at a temperature of round about $45^{\circ} \mathrm{C}$.

There are two ways in which temperature can be considered. One is the room temperature, or ambient temperature, which will determine the lowest temperature these components can operate at. But in actual operation they will heat up according to the value of the current passing through them. Unless steps are taken to limit the rise in temperature within the safety value there will be more destroyed transistors.

Consider what may happen in the circuit of Fig. 3 with the series base resistor and the emitter down to earth. If the transistor is allowed to take too much current, perhaps by fault conditions on the base or because calculations were wrong in the first place, it will heat up. The hotter it gets the more current it takes... until by a process analogous to internal combustion and termed "thermal runaway" it exceeds the safety value and destroys itself.
This will not be prevented by using mica washers, heat sinks and so on, which merely increase the amount of current the transistor can take without getting too hot.

Consider, however, the circuit of Fig. 5, in which there is now an emitter resistor, Re. Under normal operating conditions the volts dropped across this resistor by the emitter current will be, say, IV at quiescent current value.
The base bias will have been calculated so that the base potential is some 1.2 V to earth-that is, $200 \mu \mathrm{~V}$ to emitter as before.
Now in the event of a rise in quiescent collector current through any cause-temperature or other-wise-the volts dropped by the emitter resistor will also increase; the voltage at the base tap on the potential divider remaining substantially unaffected. Thus the emitter moves more negative to base, which is the same as saying the base


Fig. 5 (above): An emitter resistor, Re, is included in this circuit.
Fig. 6 (below): This circuit should remain stable under most conditions.

moves positively to the emitter, so tending to reduce the current in the collector circuit to its original value and thus prevent thermal runaway. Remembering, of course, that moving the base negatively increases collector current, whereas moving it positively decreases it. (If the base becomes positive to the emitter then the collector current will cease entirely, the transistor enters cut-off condition and the flow of base current reverses and now flows in to the base and out of the emitter. This gives rise to some interesting phenomena.)

This final circuit, which is the preferred circuit for d.c. stabilisation, gives substantial protection against thermal runaway effects as well as compensating for transistor spreads and impedance variations.

Once d.c. stabilised a transistor stage can be used in any sort of a.c. configuration. The emitter or the collector can be grounded to a.c. even though not earthed to d.c.

So the rule is: establish the conditions of d.c. stabilisation before you do anything else. If the hook-up does not work, check the d.c. conditions. The collector current can be read by checking the voltage drop through the collector load; the emitter voltage can be checked by reading the volts dropped across the emitter resistor. As a transistor obeys Kirchoff's Law the base current could be read as the electrical difference of collector and emitter currents were that difference large enough to measure, which normally it will not be. But the value of the collector current, in milliamps, will enable the base biasing current to be ascertained by making reference to the published data for the transistor.
The base voltage to earth can be read if there is an emitter resistor; this should be slightly more negative than the emitter itself.
This is by no means the whole story. A glance at the circuit (Fig. 5) will suffice to show that the potential divider R1, R2 is not quite what it appears to be on the surface. In practice the biasing potential is almost wholly determined by R1 because the input impedance of the transistor itself is in effective shunt with R2 and, as seen, this is of a low order, some $100 \Omega$ perhaps. Thus R2 is really only a bleeder.
Nevertheless with this circuit for d.c. stabilisation, if calculations have been accurate having regard to the published data on the transistor in use, the stage should work-as far as d.c. is con-cerned-first go off.
Trouble shooting with transistors has its own problems. The impedances are far lower than those associated with valves, so are the voltages; on the base you are dealing with micro values. If the value of a resistor is taken in situ it will probably only read the impedance of a transistor in shunt with and, as the whole set-up is critical within fine limits, transistors can be wrecked when trying to find out why they won't work.
Once d.c. conditions have been established go ahead to the next stage and consider the a.c. applications.
If the circuit shown in Fig. 6 is used, and in addition arrange that the collector load is of a value which drops at least half the supply voltage (in this case 4.5 V , which is half of 9 V ), it will result in a set-up which should work and remain stable under almost any conditions.


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# THE AUDITRON 



By M. L. Michaelis, M.A.
indicators, because this is normally by far the easiest to achieve. A phase-indicator normally requires a cathode-ray oscilloscope, which would involve costs and complications out of all proportion if one merely desired to build a bridge alone. However, it is well worth while if matters lie the other way, namely that an oscilloscope exists, and we want to modify this to include a bridge function, as here. Phase-Null indication has, namely, some advantages in sharp definition of the Null (Balance), as it involves the closure of an ellipse to a straight line at true balance, opening up again beyond, which is a visually very distinctive action. The human eye is very sensitive to any departures from the straight line!

The actual bridge itself is one of the conventional arrange-
(Continued from page 842 of the January issue)

$\mathcal{J}$HE shift controls have a time-lag of about one second before the trace fully follows movement of the controls VR3 and VR4. This is due to the charging time of C28 and C38. It could be avoided by returning R15 and R16 to the final anode (pin 8) of the c.r.t., and applying the shift voltages in the same manner to the other two plates. This was round to worsen the hum level on the trace slightly, and to worsen astigmatism slightly, yet should by all means be tried, as conditions could easily be different with individual Auditrons, whether the specified tube is employed or not.

## The Bridge Circuit

Fig. 3 (page 514, October issue) shows the arrangements for measuring capacities of from about $1,000 \mathrm{pF}$ to $30 \mu \mathrm{~F}$, and inductances from about 1 to 20 H , by means of the " bridge" arrangements built as an integral part into the Auditron.

It is a fact that, in a.c. bridge arrangements of conventional type, not only are the voltages equal, but also the phases are equal, for the two pints' between which the null-indicator is connected, once the point of balance has been reached. Thus, in principle, a null-indicator can be used to react to voltage or to phase differences, though almost always voltage indication is used in normal null-
ments for a.c., though novel in detail. R17 and R18 form an a.c. bleeder on the 110 V a.c. line, tapping off sufficient amplitude to give about 2 cm deflection on the $X$ plates, using the mains sinewave. C13 and R12 form the "standard" arm of the bridge, giving a definite phase shift (in fact, $45^{\circ}$, because the impedances of C13 and R12 have been chosen to be approximately equal at mains frequensy) for the bridge $X$ deflection, compared to the incoming mains voltage. It is seen that Sle and Sif, two wafers of the function switch, cut off the a.c. supply to R17 and short R12, in all positions except "three", which is the " bridge" setting.

The other arm of the bridge is given by the unknown capacitor or inductor to be measured. connected between the terminals "LT AC" and "Pot" of the "bridge" connections on the panel. This is fed from the a.c. heater line, which is in phase with the 110 V a.c. line feeding the other bridge arm. The completion of the second arm is given by the fixed and variable resistors selected on S3a, a wafer of the bridge range switch S3.

## Normal Use of the Auditron Bridge

The normal use of the Auditron Bridge is for checking and measuring capacities larger than $1,000 \mathrm{pF}$. The capacitor is first of all checked for leakage before making a capaciry measurement, because leaking capacitors would ctill wive a capa-
city reading, apparently, i.e., a phase balance may still be found, but at the wrong point. Thus it is first necessary to make sure that the insulation is reasonable. This is done by first connecting the capacitor with one end to the bridge terminal labelled "h.t.", and the other end to the prod of the signal amplifier probe, having turned the signal amplifier gain to zèro beforehand, because only the valve-voltmeter function is needed at this stage of proceedings. If the capacitor insulation is reasonable, the valve-voltmeter in the signal amplifier of the Auditron should, as soon as the above connections are made, give a sharp kick to about +250 V (for all except the smallest capacities), and thereafter return to zero at once, or within a short time, according to the capacity.

Leaks having resistances of $20 \mathrm{M} \Omega$ or less will have been shown up by this method, and a capacitor passing this test should be suitable for most normal purposes. Note that the applied test voltage in this test was about 250 V which should be permissible for most normally used condensers. If the capacitor is of lower voltage rating, then adopt a modified procedure described later in this discussion.

## Copacity Measurement

The capacitor undergoing tests is next connected between "LT AC" and "Pots", and the prod of the probe is connected also to "Pots". The signal amplifier gain is turned up until an oblique ellipse of reasonable size is observed on the c.r.t. screen.

S3 is switched to that range including the nominal (or estimated) value of the test capacitor. The corresponding potentiometer then in circuit, VR5, VR6 or VR7 is turned until the ellipse exactly closes up to a pure straight line going obliquely across the c.r.t. screen, and the capacity value is then simply read off from the scale attached to the potentiometer. If one has no previous idea of what value the capacity might have, one has to search through the various ranges, yet there is a right and a wrong way of doing this. If, even at full signal amplifier gain, the oblique ellipse is lying very flat, giving little departure from a horizontal trace, it is a sign that the capacity of the test capacitor is much less than the bridge range set at the time. If the ellipse is large and distinct, yet makes no attempt to close to a line over the entire range set, then the capacity of the capacitor is much greater than the range set. Always adjust the signal amplifier gain (VR13) such that the figures are as large as possible, yet still do not fold over at the ends (distortion in the signal amplifier due to overload).

## Arrangement of Potentiometers

When making the calibration scales to be attached to the "bridge" section of the Auditron panel, the five positions of S3 should be marked clearly with the capacity range covered in each case, and an arrow pointing to the potentiometer knob operative for each position. Position 1 operates with VR5, and will cover about 1 to $30 \mu \mathrm{~F}: \mathrm{R} 19$ is here a safety resistor, to avoid shortcircuits if the test condenser has a dead-short fault and VR5 is turned to minimum. In such a case, without R19, a total short would be present on the heater line, which would most likely burn out the bottom end of VR5.

Position 2 operates with VR6, and should cover about 0.1 to $1 \cdot 0 \mu \mathrm{~F}$. R28 here serves the double function of safety resistor as above, and limits the high capacity end of the range to reasonable overlap with the next range.

Positions 3, 4. 5 all operate with VR7, which thus carries three scales. In position 3 coverage is about 0.02 to $0.25 \mu \mathrm{~F}$. Position 4 merely switches in an additional series resistor, 'changing the range from about 0.01 to about $0.02 \mu \mathrm{~F}$. Finally, in position 5 , the same range of $0.01-0.02 \mu \mathrm{~F}$ is still operative, but a standard capacitor of $0.01 \mu \mathrm{~F}$ is placed in parallel with the unknown one, so that the actual range, as far as the external capacitor on test is concerned, has become zero to $0.01 \mu \mathrm{~F}$. Balance clarity is too weak for anything except very rough indications below $1,000 \mathrm{pF}$, thus this


Banana plug/crocodile clips of the type used by the author (See page 942)
range is calibrated 1,000 to $10,000 \mathrm{pF}$. Capacities smaller than $1,000 \mathrm{pF}$ should be measured by resonance methods with a coil, using a grid-dip meter, or by other standard methods. For ranges 3, 4, 5 R21 performs the functions of safety resistor and scale range limiter.

## Paper Capaeitors rated at less than 250V

To obtain test voltages less than the full h.t. of 250 V , the "H.T." and "Pots" terminals should be shorted together. VR6 carries a voltage scale, in addition, from about 12 to 100, giving the indicated voltages at the shorted terminals, for the relevant slider positions. VR5 carries a similar additional scale from about 1 to 12 V .

For the initial leakage test, therefore, S3 should be switched to the desired voltage range, and the potentiometer adjusted to the rated voltage of the condenser, after shorting "H.T." and "Pots". One end of the capacitor is then connected to "H.T." as before, and the other end to the prod of the probe, and the same procedure used as before.

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test components or mistaken connections.
After checking the insulation of a low voltage paper capacitor in this way (or any other nonelectrolytic type of capacity within the ranges covered), a capacity measurement may be made in the same way exactly as for higher voltage ratings, because the applied voltage is then only 6.3 V a.c. maximum. Naturally, the shorting lead between "H.T." and "Pots" must be removed again prior to the capacity measurement.

## ©uantitative Insulation Measurement

As will have been made clear in another article which appeared in past months in this magazine, dealing with noisy volume controls, those capacutors used for coupling from the anode circuit of a stage of amplification to the grid of the next stage can sometimes give trouble if the insulation is not better than $500 \mathrm{M} \Omega$. The Auditron can be used, in the "bridge" setting, to check whether a capacitor satisfies this condition.

After successfully completing the above described "reasonable" insulation check the capacity measurement, multiply the observed capacity (in $\mu \mathrm{F}$ 's) by 500 . This gives the shortest tolerable time-constant (in seconds) of the selfdischarge rate of the capacitor across its own leakage, for the purposes envisaged, and the Auditron can now be used to check that this timeconstant is with certainty exceeded.

For this purpose, proceed exactly as for the "reasonable". insulation test. Now set the signal amplifier gain, by means of the Zener diode calibrator to give a vertical-deflection sensitivity of two-thirds as many volts per centimeter as the test voltage used. Now touch the prod of the signal probe on to the free end of the test capacitor in the normal way, and wait until the initial valve-voltmeter deflection has died away to invisibility. Then remove the prod of the probe, leaving the capacitor hanging with one end free, and wait the calculated "minimum-time-constant" period (e.g. for a typical coupling capacitor of $0.05 \mu \mathrm{~F}$, this would be 0.25 seconds). Then immediately touch the prod on to the free end of the capacitor again. If the jerk of the trace on the c.r.t. screen (upwards) is then less than one centimeter, the capacitor has insulation better than $500 \mathrm{M} \Omega$, and is thus satisfactory. If the jerk is greater, the capacitor is of doubtful quality for coupling purposes.

## Insulation Tests for Electrolytic Capacitors

All tests and measurements on electrolytics nust use a polarising voltage of the correct sense, and this is automatically provided in the "reasonable insulation" test here. Thus leakage checks for electrolytics can be performed in the same way exactly as for other types of capacitor. Observe that the test voltage does not exceed the rated voltage (though it may be less, but not less than half of the rated voltage), and observe correct polarity. The positive lead of the electrolytic should go to the "H.T." terminal, and the negative lead to the prod of the probe.

The "reasonable insulation" test, showing leaks of about $20 \mathrm{M} \Omega$ or less resistance, is normally adequate, and represents all that can be expected in the way of insulation from many large capacity
electrolytics. However, there is nothing against applying the above described time-constant observation method to test for even better insulation. This is desirable in those cases where electrolytics are to be used for coupling purposes, such as in certain types of frame-timebase circuits in television circuits.

## Capacity Measurements for Electrolytics

It is not possible to use the normal bridge operation and calibration for capacity measurements on electrolytics, because no d.c. polarisation is then available. A different method is thus to be used, which is particularly possible because of the high capacity of electrolytics.

This method proceeds in the same manner as the "reasonable insulation" test, and may be performed simultaneously with the latter right at the start. Apart from observing that the valvevoltmeter deffection should return fully to zero if the insulation is satisfactory, the time it needs to halve its initial deflection should be noted, in seconds, with the switch marked "C" on the probe set to position "time". This time, in seconds, gives the capacity of the electrolytic, in $\mu \mathrm{F}$ 's.

The same procedure is to be used for nonelectrolytic types with capacities exceeding $30 \mu \mathrm{~F}$, i.e. not covered "by the highest bridge range.

The switch "C" should be left at position " scope" for all other uses of the Auditron.

Capacitors found in modern transistorised equipment are often electrolytics of about 6 to 12 V rating and have capacities of hundreds or thousands of $\mu \mathrm{F}$ 's. The above described method of capacity measurement (primarily intended for h.t. smoothing capacitors) would thus take too long with these components, apart from insufficient sensitivity on the valve voltmeter at the low working voltages.

These capacitors should thus be charged from a suitable tap on a grid-bias battery, observing polarity and keeping to within the voltage rating. Allow about 15 seconds for charging. Then connect the charged capacitor to a suitable range on a good multimeter, i.e. a voltage range of about 5 or 10 V f.s.d., and having at least $4,000 \Omega / \mathrm{V}$.

The time in seconds should be noted, required for the initial meter deflection to recrease to one third of its value. Dividing this by the meter resistance for the used range, expressed in $\mathrm{M} \Omega$, gives the capacity of the capacitor in $\mu \mathrm{F}$. Thus. for example, if a 6 V working capacitor is charged to 6 V and 110 seconds are needed for the initial. meter deflection of 6 V to fall to 2 V , using the 10 V d.c. range of total resistance $40 \mathrm{k} \Omega(0.04 \mathrm{M})$, the capacity is clearly $2,500 \mu \mathrm{~F}$. Insulation should be tested in these cases by first touching the charged capacitor on to the meter terminals, long enough to observe the deflection, then disconnecting the capacitor again, and after a time-long compared to the capacity-measurement time, i.e. at least ten minutes-re-connecting and noting that the reading should not have changed appreciably.

The fact that tests on low-voltage high-capacity electrolytics can be performed in this simple manner with an ordinary multimeter explains why no attempt has been made to cover this function on the Auditron, it being thus superfluous there. All the other numerous capacitor test facilities embodied in the Auditron, as described above, are seen, however, to be far more convenient there
than with other arrangements, justifying their incorporation.

## Choke-Coil Inductance Measurements

Inductances cause a phase shift in the opposite sense to capacitors thus, when connected between the "LT AC" and "Pots" terminals on the Auditron bridge, they will increase the phase difference between the two points of the bridge diagonal, instead of compensating it to zero as in the case of capacitors at balance.

The criterion here to be used for "balance" is when the phase difference has thereby been augmented to $90^{\circ}$, manifested by an erect or horizontal positioning of the ellipse on the c.r.t.-screen, according to the $Y$-amplifier gain set. In other words, the ellipse ceases to be oblique. In this condition, a suitable setting of the $Y$-amplifier gain enables a perfect circle to be produced on the c.r.t.-screen, which is the final true indication of "balance" with a choke.

The only setting of S 3 giving a useful range here is position 1 , which was for 1 to $30 \mu \mathrm{~F}$ and here covers about 1 to 20 H . This range of inductance is useful for checking smoothing chokes, audiooutput transformers, etc.

## Moasuring Small Inductances

The bridge-facilities on the Auditron have been designed to cover those capacity and inductance measurements normally required and not conveniently covered by employment of the grid-dip meter mentioned in an earlier article.
All r.f. coils, for anything from long waves down to v.h.f., r.f. chokes, i.f. transformers, etc. should be measured with a grid-dip meter.

## Callbrating the Bridge Controls

The bridge controls should be calibrated against capacitors of accurately known values. As standard inductances, a number of chokes and transformers as different as possible should be selected, their total impedance at mains frequency determined by measuring the current they take when connected to a suitable low voltage a.c. supply, and using Ohm's Law. The inductance is then given by the following formula:-
$Z=$ Total impedance at $50 \mathrm{c} / \mathrm{s}$ mains frequency (ohms).
$\mathrm{L}=\frac{\sqrt{\mathrm{Z}^{3}-\mathrm{R}^{3}}}{314}$ Henry
$\mathrm{R}=$ d.c. resistance of windings (ohms) (use ohmsrange of multimeter).
The voltage calibrations of VR5 and VR6, for test-voltages for low rating capacitors, should be made as follows. For each scale mark desired, the potentiometer resistance needed to give the corresponding voltage with R2 as bleeder from 250 V input should be calculated by direct proportion. The multimeter should then be connected between "Pot" and chassis (Auditron disconnected from the mains), and the knob of VR5 or VR6 turned until the desired resistance is noted on the meter. The voltage mark concerned is then made against the pointer position of the potentiometer knob.
Alternatively a valve-voltmeter can be used for direct calibration of the voltage between "Pot"
and chassis when "H.T." and "Pot" terminals are shortened, and the Auditron switched to "bridge". The built-in valve voltmeter can be used for this purpose for the higher range 12 V to 100 V , but is not sensitive enough for the lower range.
The three bridge terminals on the panel of the Auditron are coloured wander plug sockets of the insulated type. Three miniature insulated crocodile clips with a banana plug at one end and the jaws at the other, made as small integral units (see photograph) were purchased. These can be plugged into the wander plugs, and the test capacitor held between the respective jaws.

## A Probe for the Auditron

As mentioned earlier in this series, the Auditron should normally never be used without its specially constructed probe at the signal amplifier input, i.e. only in exceptional circumstances should a signal be fed direct from its source, via a screened or unscreened cable, into the signal-amplifier input.


Fig.13: Equivalent circuit showing the stray capacities operative if a signal source is connected directly to the input of an oscilloscope amplifier.

Also no oscilloscope should be operated without its proper test-probe at the signal amplifier input. Probes are generally not exchangeable between various oscilloscopes since these must be carefully balanced to suit the particular signal amplifier with which they are to be used.

Fig. 13 depicts the important aspects of the signal amplifier input circuit if it is attempted to feed in a signal direct, without using a probe. Ri represents the d.c. impedance of the amplifier input, which is $135 \mathrm{k} \Omega$ in the case of the Auditron. Ci represents the total effective internal stray capacity of the amplifier input, up to and including the coaxial input plug-socket $P$. The value of Ci is unknown and must be measured in a completed amplifier.

AB represents a length of cable, screened or unscreened, used to connect the signal source to the amplifier input $P$. Ce represents the stray capacity of the cable to earth. Cc and Ci , acting in parallel, can be lumped together as a single stray capacity, Cm, once it has been decided what length and type of input cable to use.
Two yards of good coaxial cable with a capacity not exceeding about 1 to 2 pF per inch can be used for the Auditron signal input. Choose a fairly thin, easily flexible, coaxial cable. With such a cable $\mathrm{Cc}+\mathrm{Ci}(\mathrm{Cm})$ comes out at around 150 pF .
(To be continued)

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SPECIAL AMERICAN MYLAR DUPONT. 5 in . 1,200 ft. D.P. Top quality Brand New $251-$ post free. Limited quantity only!
PLASTIC TAPE SPOOLS. Best quality
 TELEPHONE PICK-UP COIL. Designod to feed into the microphone input of elther a tape recorder or any high gain ampliser. Easily attached to telephone by rubber secshielded to positioned on telephone this model is more than adequate for a fully modulated tape recording. Brand new complete with 5 [t. shielded cable. ONLY 14/-. Post iree.

## MINISETS LTD Hatherley Mews London EI7

## THE IMPERIA

An aasy－to－build 6－Transistor Portable Superhet which can be builc by the constructor easy construction．All com－ easy oonstruction．All com－ ponents are new．5in．speaker Attractive case of exclusive design $8 \frac{1}{2} 55$ x 2lin．With gold－plated grifle． 2 kin ．With designed matching coil for use in car．Only first grade fully guaranteed matchedtransistors and diodes are used．Anyone can build this set for
£7．17．0
Everything supplied excep soldering tron．P．\＆P．3／－．Full instructions 1／6（free with order）．

## 6－Stage Transistor Pocket Portable

Can be £4．19．6 $\underset{2 i 6}{\mathrm{P} . \mathrm{P} .}$ bullt for $1.62 / \mathrm{b}$
$\star$ Completely self contained． no aerial or earth required． ＊Push－pull output， 250 milii－ watts．
$\star$ 3in．high fiux speaker．
＊Pre－assembled circult boser with simple instruc－ tions ensuring easy con－ struction．
$\star$ High Q Ferrite Rod Aerial．


Can be supplied with long－wave $6 /$－extra．
Full instructions，price list 1／6（Free with order）．

## 3－Transistor Radio（plus 2 diodes）

## Total building $70 /=\quad$ P．P． $2 / 6$

＊Pre－assembled circuit board，ensuring easy construction．
$\star$ Full medium－wave ooverage．
$\star$ Attractive case $5 \frac{1}{4} 3 \times 181 n$ ．
$\star$ All components including transistors are brand，new and direct trom manufac－ tarers．
＊Ferrite Rod aerial coll．no external aerial or earth required．
＊2kin．high fux speaker direct from manufacturer．
＊Arter－sales service．
Send 1／6 for instructions，circuit and price list．

## THE RIETI

6－Stage super sensitive Transis－ tor Portable．Easy to build． All components first grade．A real portable transistor radio， covering Medium wave recep－ tion．5in．speaker．high Q ferrite aerial especially de－ signed．Pre－assembled circuit board enables the complete set to be assembled and tested betore placing in case．
Attractive case $84 \times 54 \times 241 n$ ． with gold－plated grille．Total



Medilum and Long wave 8／－extra．Full instructions $1 / 6$（free with order）．

## The new NOMBREX

TRANSISTORISED WIDE－RANGE SIGNAL GENERATOR 27
$220 \mathrm{kc} / \mathrm{s}$ to $220 \mathrm{Mc} / \mathrm{s}$


RETAIL £7．10．0 $\begin{gathered}\text { Post and ins．} 3 / 6 \\ \text { Battery } 2 / 3\end{gathered}$ 36＂Screened Test Lead 6／3 extra CASH WITH ORDER．REGRET NO C．O．D． IMMEDIATE DELIVERY
Trade and Export Enquiries Invited

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THESE
FEATURES
COMPACT Only $6 \mathbf{t}^{\circ} \mathrm{x} 4 \mathbf{t}^{*}$ PORTABLE Weight 2 lbs．

ACCURACY！ Under $2 \%$

JCONOMYI 3v．Battery

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Send t2 deposit pay balance
21／－per month

NOMBREX LTD．（Instruments Division 45）
Estuary House，Camperdown Terrace，Exmouth，Devon， England．Tel． 3515.

## EXPRESS ELECTRONHCS ROSEDENE LABORATORIES KINGSWOOD WAY，SELSDON，SURREY

## VALVES NEW TESTED ANDGUARANTEED FOR THREE MONTHS

|  |  | ¢ B 6 6 |  | 12AX7 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | 6335 |  | 2日以女 |  | DH14 | 8／8 | E |  | PLas |  |
| 1 F1 |  | ¢ $\mathrm{BR7}^{\text {a }}$ |  |  | 10／6 | $1)$ | 10／－ | F | 9／6 | PY81 |  |
| 1F3 |  | ¿BWV0 |  |  | 11 |  | 7／6 | Et | \％ | PY82 | $7 /$ |
| 1 Fll |  | tbw7 |  |  | 716 | D | 8／－ | F | 10\％－ | $\mathrm{H}^{\prime} \mathrm{Y} \mathbf{S}$ | $7 / 6$ |
| 19 |  |  |  | 1 LSN 7 | 6／1 | $1{ }^{\text {L }}$ 92 | $5 / 9$ | HSIS5 | 101－ | R19 | 101 |
| 1 PL |  | ¢F |  | litas | $9 /$ | LLy 4 | $6 / 6$ | EY51 | $7 / 8$ | 85A1 |  |
| 1 P 10 |  | ¢Higl |  | 19AQS | $9 / 6$ | DL9\％ | $8 /-$ | EY81 | 101－ | U52 |  |
| 11 |  | dJ7c19 | $7 / 6$ | 25460 | $7 / 6$ | E15Y1 | 4／－ | EZ40 | $7 / 8$ | U7 |  |
| $1 \mathrm{R5}$ |  | ＇K67i | $5 / 6$ | 25 Ladat | $7 / 6$ | EBC | 10／－ | EZR | 8／－ | U78 |  |
| $1 \pm$ |  | 6 K 8 d |  | 25244 | 9 9－ | ABE8 |  | EZ8 |  |  |  |
| 4 |  | 6076 | 5／6 | 30 Cl | $7 / 6$ | ECX8 |  | HVR |  | UBC4 |  |
| U5 |  | 68LTGT | $61-$ | 30 L 1 | $7 / 6$ | ECC82 | $6 /$ | Кт330 | $8 /$ | UCH 42 |  |
| 24 |  | 68N7GT | 6／－ | 3 LbG | $7 / 8$ | ECC83 | 6／9 | KT66 | 11／8 | UF41 |  |
|  |  | AVGG | $7 / 6$ | 35 W 4 | $8 / 6$ | ECC84 | $7 / 8$ | N17 | $5 / 8$ | UL41 |  |
| 3 V 4 |  |  |  | $35 Z 46 T$ | 8／－ | ECF90 | $8 / 6$ | N18 | $8 /=$ | UY41 |  |
| 3GT |  | $6 \times$ ¢a |  | 5763 | $7 /$ | ECF82 |  | N 19 | 1 | W17 |  |
| 4 |  |  |  |  | 61－ | ECH 42 |  | N709 |  | W76 |  |
| 6．K6 |  |  |  | DAF91 | $7 / 6$ | FCH81 | 10\％－ | CC8 |  | W1＋2 |  |
| 6A Lat |  |  |  | DAF96 | 81－ | ECL 8 | $8 / 6$ | PCF80 | $7 / 6$ | X17 |  |
| 6AM6 |  | 12AD ${ }^{\text {d }}$ | 11／6 | DCO90 | 12／8 | ECI8 |  | PCE82 | 776 | X142 |  |
| 6AT6 |  | 12 AH 8 | 10／． | DF＇91 | 81－ | EF41 |  | PCL82 | $8 /-$ | X 150 |  |
| 3 6 |  | 12AT7 |  | DF96 |  | EF80 |  | PCL34 | $9 /=$ | Z77 |  |
|  |  |  |  |  |  |  |  |  | 12／6 | D |  |
| High Stability Resistors $1 \mathbf{W} 5 \% 50 \Omega$ to 1M，Od．Midget Cersmios 500 F．Qd Coax．Super quality tin．，8d．Fd．Pluge 9d．8ockete 日d．8ilicon H．T．Reets． 250v． 800 MA $\ddagger$ in．$x+i n .8 / 6$ ．Contaet Cooled $250 \mathrm{v} .50 \mathrm{MA} 6 / 6.85 \mathrm{MA} 8 / 6$. |  |  |  |  |  |  |  |  |  |  |  |
| NEW TRANSI8TORS BY MULLARD．OC19，OC26，OC66，25／－；OC44． OC45．9／－；OC70，OC71，6／－；0072，7／6；0C72 matched in pra．18／－； 0C74，OC75．0C78，OC81，7／6；OC82，0C170，9／6． |  |  |  |  |  |  |  |  |  |  |  |
| VALVES MATCHED IN PAIRS |  |  |  |  |  |  |  |  |  |  |  |
| ELL34 27／6，EL84 15／－，N709 15／－，6V6G 15／－，6BW6 14／－per pair．Pugh－ Pull O．P．Transformer for above $3-15 \Omega$ 14／6，P．\＆P．1／6，12im，P．M． |  |  |  |  |  |  |  |  |  |  |  |
| $\text { Modeh, } 87,7.0 .$ |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| DK91，DF91，DAF＇rg1，DL92 or DL94，19／8 ECH42，EF41，RBCA1， |  |  |  |  |  |  |  |  |  |  |  |
| DK96，DF98，DAF96．DL96．．．．．．．．．．27／6 ELA1；E240．．．．．． |  |  |  |  |  |  |  |  |  |  |  |
| 1C3，1F1，1FD1，1P1．．．．．．．．．．．．．．．．27／8 |  |  |  |  |  |  |  |  |  |  |  |
| 1RS，1T4，188，384，or 374．．．．．．．．．．．．19／8 |  |  |  |  |  |  |  |  |  |  |  |
| Post | e an | d packin | 8 |  | 21 | ost ire |  | C．O．D． |  |  |  |



## NEW STYLED HI-FI CABINET

A NEW radiogram cabinet has just been brought on to the market by G.K.D. Limited and which has been specifically designed to house Leak hi-fi units.
G.K.D. have called this new cabinet the "Southdown" and have managed to combine good styling and compactness with generous space allowance for any combination of Leak equipment. This has been achieved by incorporating a spring-loaded drawer which, when opened, reveals a panel for mounting tuner or pre-amplifier units.

The manufacturers are G.K.D. Limited, King Street, Houghton Regis, Bedfordshire.

(Right) Telonic 's new sweep generator.


This new transistor tester is made by Taylor Ltd.

## TRANSISTOR TESTER

A NEW transistor tester - model 44 - is announced by Taylor Electrical Instruments Ltd. This portable tester is capable of measuring accurately the characteristics and performance of modern transistors.

Several new features have been introduced in this model, including facilities for varying the collector voltage, base current and collector current independently.

The tester is made by Taylor Electкical Instruments Ltd., Montrose Avenue, Slough, Buckinghamshire.

## SWEEP GENERATOR

ANEW sweep generator is now' available covering a wide spectrum of r.f. frequencies with a sweep width over its entire range. The new instrument, model SP-1200. manufactured by Telonic Industries Inc. (U.S.A.), has a centre frequency range of $5 \mathrm{Mc} / \mathrm{s}$ to $1,200 \mathrm{Mc} / \mathrm{s}$ and a sweep width also 5 to $1.200 \mathrm{Mc} / \mathrm{s}$.

The English agents for Telonic equipment are Livingston Laboratories Ltd.; 31 Camden Road. London, N.W.1.


#  Club News  

## REPORTS OF CURRENT ACTIVITIES

AMATEUR RADIO SOCIETY OF CHESHAM AND DISTRICT

Hon. Sec.: Capt. C. G. Stephenson, G3CLJ/T, 21 Lynton Road, Chesham, Buckinghamshire.

Each Tuesday evening morse, first aid, practical construction and other subjects are taught and on Fridays the Society arranges RAE theory lectures. Sunday meetings are devoted to practical operating.

At the recent Annual General Meeting it was disclosed that the Sociery's membership had increased $600 \%$.

BRIDLINGTON AMATEUR RADIO SOCIETY
Hon. Sec: P. Cartwright, G3POC, 55 Hermitage Road, Bridlington, East Yorkshire.

This Society has recently moved into new premises in the centre of the town in North Street. Any persons interested in becoming a member would be most welcome.
On Wednesday evening the Society runs morse classes for those wishing to gain experience in this subject.
Arrangements are already going ahead for another mobile rally to be held in June.

## BURTON-ON-TRENT AND DISTRICT RADIO SOCIETY

Hon. Sec.: H. Marrison, 38 Baker Street, Burton-upon-Trent, Staffordshire.
Lectures have been arranged for members on the first Wednesday of each month, and on December 5th an RAE lecture was given.

The meeting on December 12th was devoted to a film show.

LOTHIANS RADIO SOCIETY
Hon. Sec.: W.T. Sutherland, GN3JWS, 47 Great King Streèt, Edinburgh 3.

On December 13th members attended an R.S.G.B. tape recorded lecture on "World Wide Telecommunications".
Later, in the month, on the 27th, members enjoyed a "Social evening".

## MITCHAM AND DISTRICT RADIO SOCIETY

Hon. Sec.: B. Blandford, I Biggin Avenue, MItcham, Surrey. A very successful Christmas Meetling was held on December 14th. A Christmas Draw was arranged with many inviting prizes.
During the evening judging for the annual Constructional Contest took place and the Society trophies were presented.

## PLYMOUTH RADIO CLUB

Hon. Sec.: R. Hooper, 2 Chestnut Road, Peverell, Plymouth, Devon.
In the recent competition for the "Ernie Hillyard" trophy, the winner was judged to be Colin Jones with his radio teletype converter. Second was John Fallen with a stereo amplifier, and third was Ted Fallen with a grid dip oscillator.
A party of members attended the opening night of the Torbay Radio Club on Saturday, December 9th.

Future Event:
January 19th-Dinner and social evening.

## CITY OF BELFAST Y.M.C.A. RADIO CLUB

Hon. Sec.: R. H. Payne, 25 Arundel Street, Belfast 12.
The club meets every Wednesday and Saturday and a varied programme of lectures and visits has been arranged. There are also constructional facilities available to mambers.

A slide show and Christmas party was en. ioyed by all who attended on Deccmber 19th.

## CLIFTON AMATEUR RADIO SOCIETY

Hon. Sec.: C. E. Godsmark, 211 Manwood Road, London, S.E.4.

The annual Constructional Contest was held on December 14th at the clubrooms.

The $1.9 \mathrm{Mc} / \mathrm{s}$ net on Christmas morning was controlled by G 3 GHN , the club station.

## COVENTRY AMATEUR RADIO SOCIETY

Hon. Sec.: A. J. Wilkes, G3PQQ, 141 Overslade Crescent, Coundon, Coventry.
This Society is now setcled at its new headquarters and the newly purchased l50W transmitter is also installed.

[^4]
## "CORONATION STREET OR CQ.ZL..."

4HE radio ham, perhaps more than any other hobbyist, needs to belong to a club to attain full enjoyment of his chosen pastime. To be a lone-wolf will not do, for the very act of listening or transmitting-which, after all, must be considered the fulfilment of whatever else he may decide is intimated in the title of "radio ham "-brings him into immediate contact with his fellow enthusiasts.

Yet in spite of this undeniable fact, the Practical Wireless offices receive many letters from readers who obviously do not belong to a radio club and whose particular problem could be solved simply by joining such a society.

For instance, we receive many queries about ex-government sets and, as most readers will know, information about this equipment is very hard to come by. In fact most information originates with the more ambitious enthusiasts who are prepared to service such equipment "blind". And where do these individuals gather and compare notes?-in the radio clubs of course, and it is in these clubs therefore, that the most comprehensive data on ex-government sets is to be found (except in government records, that is).

The radio clubs also offer unrivalled opportunities for instruction on the practical side of operating as a licensed amateur, and this is very important for any potential ham. Also important are the number of social events that take place from time-to-time, not to mention rallies, d.f. contests, lectures, construction competitions, etc., etc.

This time of the year is the busiest for all amateurs whether on the air or at the workbench, and so the choice is yours, "Coronation Street" or "CQ. ZL. .", but for those who do not belong to a radio society, we would suggest that you seriously consider joining your local club. if only for the ragchews and film shows! There are many clubs listed on this page and most secretaries will be pleased to give you details of their activities and also extend a welcome to go along to the next meeting to see "just what
goes on ".

# SURIBTON PARK <br> RADIOLTD. FOR POST HASTE-POST FREE SERVICE 



| HALF TRACK |  |
| :---: | :---: |
| TDE Monardeek, latert model 51 | 8.9.0 |
|  |  |
| ape Amplifier for B.S.R. deok, printed circuit ready wired, with |  |
| ECC83, ECL82, EM85 and EZ81. Couplete with all |  |
|  | 8.8.0 |
| Deposit 21.0.0 und s monthly .............. 21.1.0 |  |
| Case with 7in. 1 4in. spesker, in two tone grey...................., 84.4.0 |  |
| Complete Kit as above. . . . . . . . . . . . . . . . . . . . . . . . . . |  |
|  |  |
| The above recorder can be supplied assembled, tested and complete with tape and microphone for. Deposit 82.10 .0 and 12 monthly $\qquad$ i.i.1.6 |  |
|  Deposit 21.5 .0 and 12 monthy |  |
| Tape Amplifier for atudio deck, with ready wired printed circult control and input panela, mains and output transformers. Complete with valves, knobe, plans, screws, etc. EF86, ECC83, EM84, EZ81, OAB1 and 2 ELR4, 3 watta output. Magic eye, radio and mic. Inputa, EX L/B socket, tone and monitor controls. Can be used as an amplitter... $19 \%$ 811.11.0 Deposit 81.4 .0 and 12 monthly. . |  |
| Case for above iucluding 9in. $\mathbf{x} 5 \mathrm{5in}$. speaker. . . . . . . . . . . . . . . . . 5 . 5. |  |
| Total Kit as above <br>  |  |
|  |  |
| This Machine is listed et 39 gnil , by makers and in a very good buy. Building Instructions arailable at $2 / 6$ each kit (refunded it kit | ought) |


| QUARTER TRACK |  |
| :---: | :---: |
|  |  |
| Tape Amplifer as over, but quaster track | 89.9.0 |
| Deposi |  |
| se, two tone grey, | 82.4.4.0 |
| mplete Kit as atiove. |  |
| Collaro Studio Doek, $\begin{gathered}4 \text { track } \\ \text { Deposit } 11.18 .8 \\ \text { and } \\ \text { iz monthily }\end{gathered}$ |  |
|  |  |
|  |  |
| Complete Kit 4 track Collaro Deponit 88.10 .0 and $12 \ldots \ldots 0$ monthis <br>  Tape Pro-amplifier for Collaro deck, with power supplica, ECC8, ECL82, EZ80 and EM85, Radio and Moc sooketh, givem an equalised output of $400 \mathrm{~m} / \mathrm{Volta}$ |  |
|  |  |
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| Qaarter Track . .1...................................iio |  |
| Marriott Tape Heads. 4 track type L/RPS/7 and L/KS/9 Mecord/ Playback and Erase with mounting bracket loe Btadbo deck. |  |
|  |  |
|  |  |
| Hirriott 2 track type R/R P/I Record / Plas beik only witi briciet |  |
| for 8tud |  |
|  |  |
|  |  |
| Brenell Mr. 5 Amplifer, with power. |  |

## JASON F.M. TUNERS



## AMPLIFIERS (MONO)

|  | $812.12 .0$ |
| :---: | :---: |
| Dulci DPA15 Main amplifier, Five valve. Push-pull. ................. Deposit £1.11.6 and 12 monthly ............. $\quad$ E1.6.1 | \$15.15.0 |
|  | 29.9.0 |
|  | 218.18 .0 |
|  | 215.15.0 |
|  | 222.10 .0 |
| AMPLIFIERS (STEREO) |  |


812.12 .0

Dulel Stereo Five, Pre amplifer.........
218.18.0
£11.11.0 1eposit 21.4 .0 and 12 monthiy...............................
Leak Stereo 20, Main amplifier...............................................

Quad 22 Etereo Control Unit. Devosit $£ 2.10 .0$ and 12 monthiy....................................i. 6

## RADIO TUNER8

| ntrong T4 C. V.H.F. Tuner, seif powered Deposit 28.3 .6 and 12 monthly. $\square$ | 19.18. |
| :---: | :---: |
| antrong ST8 Mk. 2. AM/FM Tuner, nelf powered. <br> Deposit $£ 9.16 .6$ and 12 monthly <br> ............. 32.0 .1 | 127.18.0 |
| Armstronk AF208 AM/FM Radio chasela Bang and Treble controls, P.U. inputs, etc. <br> Deporit 82.8 .8 and 12 monthiy. |  |
|  |  |
| Armstrong Stereo 35 AM/FM Radlo Chamit, Boparath tore and volume controls | 282.15.0 |
| Armstrong Stereo 12, Mk. 2, AM/FM Radio Chande, Puik-pall output atage, both channels <br> Deposit $£ 4.7 .0$ and 12 monthly |  |
| e. | 7/6 |
| d, F.M. Tuner, ${ }_{\text {Den }}$ | 288.1.9 |

## GRAMOPHONE UNITS



Garrard TPA12 arm and shell less cartridge
Garrard Autoslim with mono cartridge. ㄴ…
Garrard Autoslim De Luxe with mono cartridge.................... $£ 12.14$.
Philitgs AGeposit $£ 1.5 .6$ and 12 monihly
11.1.1 212.15.
ii..3. 4
ci.0.io

с1.9.5
£17.15.5
Deposit. f1.19.6 and i2 monthly
Goldring Lenco GL 58, less cartridge ..
Garrard 4HF with mono and 12 monthly
ei.11.i
Depoosit \{2.1.6 and 12 monthiy
Garrard Lab,, Type "A" with mono cartridge Deposit 22.7 .4 and 12 monthly غi.18. 81.17.9 Garrard 301 301
peposit 22.8 .9 and 12 monthly

- 8.0 .0 .8

24.10 .3


## LOUDSPEAKERS

| Goodmsns Ariette 8 | £5.17.7 |
| :---: | :---: |
| Axiom 10 | £7.0.0 |
| $\begin{aligned} & \text { Ariom 201 } \\ & \text { Deposit \&i.i.o. and } \end{aligned}$ | 810.7.0 |
| 5K/20xL | 87.0 .0 |
| Wharledale Super 8/Fs/AL | 26.9.11 |
| Super 3 | 86.0.11 |
|  | £11.10.0 |

## New !-For you to build

## THE COROVER' 6 "

This superhet recciver uses the vory latest circuitry, 6 transisfors and two diodes and is fully tunable over tothmedium sind long Wavebands. First stage uses three Mullard AF. 117 alloy diffused transistors with
OA. 79 and OA. 91 diodes, outputOA. 79 and OA. 91 diodes, outputOC. 31 D and two OC. 81 's 1 n pushpull. I.F. frequency $470 \mathrm{Kc} / \mathrm{s}$. gives excellent reception aver all gives excellent reception over all Operates on four 1.5 v . pen torch batterles. All components are Operates on four 1.5 V . pen torch batteries. All components are case with carrying handle-fitted sockets for personal earpleces. tape recorder and car aerial. Size $6 t \times 4 \times 1 / 1 n$.
MAY BE BUILT FOR $\$ 5.19 .6$. All Parts sold separately. P. \& P. 4/- extra (Data and instructions $2 / 6$, free if all parts bousht).

## THE 'SPRITE'



A six transistor superhet Mintature pocket Radio of Commercial Quality. Funly tunable over Long and Medium wavebands. Uses printed circuit and High sensitivity internal ferrite rod aerial. I.F. frequency 470 Kc/s. Translstors: 3-Philco
 battery. Supplied with the complete RF battery. Supplied with the complete RF ready built and mounted on the printed circuit; for final assembly you only have to fit the wave-change switch, tuning condenser and drive, volume control, earphone socket and aerial rod. In very attractive plastic case, size $4 \times 2 \downarrow$ xin.
COMPLETE AS ABOVE 89/6 All parts sold sebarately. Real Calf Leather Case, wrist strap and Personal Earphone with case. $10 /-$ extra.
case. $\mathbf{P}^{10 /-3 / 6 \text { extra. (ra. (Data and instructions } 2 / 6 \text {, free if all parts }}$ bought.)

## Wirecomp's Finest Ever Value Offer-

 THE 'REALSTIC 7'
## FULLY <br> TRANSISTORISED PORTABLE RECEIVER

This super set-made to the highest professional standards-1s now available to the home constructor. Comprises Mullard Trans. OC44. OC45 s, OC71. OC81D, and 2 OC8I's, plus OA70 Crys. milliwatt output Ders 350 high flux speaker- F hrequency speaxer-1.F.
 irequency $470 \mathrm{Kc} / \mathrm{s}$.ully tunable over medium and long wave-bands. All components mounted on single printed circuit board, size $51 \times 51 \mathrm{in}$. Attractive two-tone plastic cabinet with carrying landle-size $7 \times 10 x$ Red/Gres, Blue/Grey or all Grey. Complete with full chotce of tions. Ail barts sold separately. Complete with full instruc-
WIRECOMP'S PRIGE
$\Varangle 6.19 .6$
Inciuding Free P.P. 9 sattery - Value 3/8 P. \& P. 4/6 extra. (Circuit diagram $2 / 6$, free if all parts bought.)

## WIRECOMP ELECTRONICS 378 HARROW ROAD, LONDON, W9.

 TEL: CUNNINGHAM 9530Hours of husiness: 9 g.m. to $6 \mathrm{p} . \mathrm{m}$. Open all day Saturday, Opposite Paddington General Hospital Buses $18 B$ and 36 pass the door.


## ERSIN MULTICORE SOLDERS

## for a first class joint every time

Wherever precision
soldering is essential, manufacturers, engineers and handymen rely on multicore. There's a multicore solder just made for the job you have in hand. Here are some of them.

## HOME CONSTRUCTORS 216 PACK

In addition to the well-known Home Constructors Pack (containing 19 ft . of $18 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. 60/40 alloys) a simllar pack is now avallable contalning 40 ft . of 22 s.w.8. 60/40 alloy especially suitable for printed circults.


## THE NEW HANDY DISPENSER

Easy to find in the tool box-simple to use. The solder is in a continuous coll which can be used direct from the handy free-standing dispenser-in fact. It is virtually a third hand for those tricky soldering Jobs. Containing 15 feet 5 -core 18 s.w.g.
Ersin Multicore Savblt alloy.
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#### Abstract

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDERTAKE TO ANSWER QUERIES OVERTHE TELE PHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page lil of the cover.


## SAVE OUR STYLUS?

SIR,-In reply to Mr. Davenport's letter in the December issue, may I respectfully suggest that if he were to study microphotographs of record grooves, he would soon realise the serious damage caused by the dirt and dust which adheres to fingermarks on a long playing record. This dirt not only causes excessive surface noise on a lightweight pick-up, which has been specially designed to give the highest quality with the lowest record wear, but also damages the stylus. This in turn deforms the grooves of every record which is afterwards played by it, therefore causing over $£ 50$ of unnecessary damage to even a modest collection of 30 records.

If Mr. Davenport cannot tell the difference in quality between the average " 3 W -or-bust " record player with a cheap multi-purpose sin. loudspeaker, and a 30 W hi-fi stereo system whose tweeters and bass reflexes alone can do credit to frequencies ranging from cascading strings down to a deep organ diapason, then I am afraid that he is missing a great deal of enjoyment and pleasure indeed. - J. D. Maitland (Preston, Lancashire).

S
IR.-In answer to Mr. Davenport's letter in the December issue, I would have thought that, although he is obviously not an hi-fi enthusiast, he would not have condemned his friend's disc and stylus cleaning activities. In addition to the effect of dust on the quality of reproduction obtained, it can also be very damaging to the surfaces of modern microgroove records, and the expense of 30 s. or $£ 2$ for replacing records carelessly damaged in this way is, in my opinion, considerable.-D. L. Miller (Plymouth, Devon).

## HI-FI FANATICS

$\mathrm{S}^{18}$IR.-How right your correspondent D. R. Davenport is to criticise these self-styled hi-fi fanatics.

From such contact as I have had with these people, I am convinced that it is not an appreciation of music that drives them to buy expensive record reproducing equipment, but rather a very juvenile type of pleasure in showing off audio setups to friends. Their wariness of people touching their records and equipment I am sure arises from nothing more than a desire to reserve the pleasures and mvsteries of hi-fi for selective cliques.

Recording and equipment manufacturers must bless this gullible section of the public who so readily buy their products, just so long as they can impress their friends with "frequency response", "rumble filters", "negative feedback tone circuits" and all the other little non-committal technical terms which clever salesmanship dictates shall be tagged to these products.-N. L. Nicholls (Northampton).

## THE QUANTUM THEORY

SIR,-With reference to Mr. Robbins' letter in the October issue. I suggest that he, as well as Mr. Craske has misconstrued the Quantum theory entirely.

Mr. Robbins' statement that photon sirnultaneously exhibits wave and particle properties is entirely erroneous. The term photon, from the Greek meaning "light", came into general use around 1928. It is frequently regarded as synonymous with energy quantum, but is strictly the quantity, or quantum of radiation associated with a single quantum of energy. It may in fact be described as an "atom" or "particle" of radiation. By Max Plank's equation,. a photon of radiation of frequency, $V$, carries an amount $h V$, of energy: h being the Plank constant.

Also, the wave and particle conceptions are not as Mr. Robbins states, analogies used to explain certain phenomena. They are in fact fundamental characteristics of nature. The diffraction and interference properties of radiation necessitate a wave structure, whereas photo-electric phenomena and the Compton Effect imply that radiation consists of particles.

The fact is that everything exhibits wave character or particle character depending on the circumstances. But as such, they do not exhibit simultaneously, as shown by Heisenberg's "Uncertainty Principle".

Electromagnetic radiation is definitely a wave motion, covering the enormous range from about $10^{-10} \mathrm{~cm}$ for Gamma rays to $10^{8} \mathrm{~cm}$ for the longest known radio waves. These radiations are fundamentally the same, all travelling at the speed of light, differing only in their wavelength. Also their energy content is calculated by the Quantum theory; the energy Quantum being proportional to the frequency.

Further by means of Plank's constant and the mass-energy equations of Albert Einstein, DeBroglie showed that a particle of mass $M$, moving with a velocity V , is associated with a h wavelength $\lambda$, given by $\lambda=\frac{-}{\mathrm{MV}}$; where h is the Plank constant. Therefore wave-particle duality of matter, is an inherent cancept of nature.

To enunciate an example: positron electron annihilation results in a loss of mass and a liberation of energy. This energy appears in the form of Gamma radiation. The rest mass of an electron is close to $9.11 \times 10^{-88}$ gram, the positron presumably being the same, consequently positron electron annihilation results in a loss of $2 \times 9.11 \times 10^{-28}$ gram. Using Einstein's mass-encrgy equation, the accompanying liberation of energy will be $E=9.11 \times 10^{-28} \times$ $2 \times 8.99 \times 10^{20}=1.64 \times 10{ }^{-6}$ $\mathrm{erg}=1.02$ million electron volts. Hence the total energy accompanying annihilation is 1.02 million electron volts. From the Quantum theory equations, the resulting wavelength equals $1.24 \times 10^{-10}$
1.02
which is $0.0121 \times 10-{ }^{8} \mathrm{~cm}$ or $0.0121 \AA$. To conserve momentum as required by laws of mechanics. two equal Quanta are expelled in opposite directions. The energy of each Quantum 1.02
is then $\frac{2}{2}$ million electron volts and the corresponding radiation wavelength is $0.024 \AA$. The mass-equivalent of a photon of wavelength $0.024 \AA$ treated as a particle moving at the speed of light can be calculated from the DeBroglie equation in the form $M=\frac{h}{\lambda V}$ and equals 9.11 x $10^{-28}$ gram.
Hence when a positron and electron annihilate one another, the photons produced have the same effective mass, so that mass in the broadest sense is conserved.-A. Redman (Shipley, Yorkshire).


Fig. I: See Modified T.R.F.

## MODIFIED T.R.F.

SIR,-I wonder if this circuit (Fig. 1) of a receiver I have just built would interest any of your readers. The original design was by J. G. Ransome and was published in the December 1961 issue of P.W. under the title of "Transistor T.R.F. Receiver". However, I am using only two transistors instead of three and headphones instead of a loudspeaker. A few feet of thin flex serves as a throw-out aerial.
Reception on medium waves is amazing, with several Home Service transmitters coming in at good strength. After dark, Athlone and many foreign stations are received exceedingly well.H. E. Chamberlain (Newark-on-Trent, Nottinghamshire).

## GENERAL PURPOSE COMMUNICATIONS RECEIVER

(Continued from page 926)
calibration points can be obtained by temporarily taking the b.f.o. output to the aerial circuit. and tuning the b.f.o. to $500 \mathrm{kc} / \mathrm{s}$, by means of the $100 \mathrm{kc} / \mathrm{s} 5$ th harmonic.
The $160,80,40$ and 20 m amateur bands are covered, and commercial 49, 40, 31, 25, 19 and other bands, including ship-to-shore, etc. The marker signal is c.w., and operates the tuning meter, but is only able to produce an audible signal if the b.f.o. is on.

To tune a narrow band of frequencies accurately, the bandspreading pointer is placed on a $100 \mathrm{kc} / \mathrm{s}$ marking (pointer vertical) and the bandsetting capacitor is adjusted to the marker harmonic, as this gives more accurate setting than possible by visual means. Harmonics beyond the 40 th or 50 th ecome difficult to locate. Normal reception is of Irse possible with the marker stage omitted. 7 image frequencies become apparent on vavelengths (these are $940 \mathrm{kc} / \mathrm{s}$, i.e., 2 x i.f. Ty, above the tuned frequency) they should
be relatively weak unless the trimmers are adjusted to them in error.

The receiver should give very good results on all bands, and the iron dust cores of the coils may be adjusted with an insulated blade for best results. Initially, set TCI nearly open, and tune in a low wavelength station. The panel trimmers $\mathrm{VC1C}$ and VC2C should tune quite sharply, for best reception. If best results are obtained with either of these trimmers fully open, screw TC1 up slightly, to increase its capacity.
A station of fairly high wavelength in the band is then tuned in, the panel trimmers being left untouched, and the coil cores are adjusted for best results, and to secure the required band coverage. Actual coverage depends to some extent on the positions of the cores. It will be found that at other parts of the tuning range, slight re-adjustment of the panel trimmers will improve reception, especially with very weak signals, and on the short-wave ranges. If TC1 is at a suitable capacity, and the coil cores are correctly positioned, little re-adjustment of the panel trimmers will be needed, throughout the tuning range. Alignment should be undertaken as carefully as if preset trimmers were fitted, but any slight errors will not result in lost efficiency, as the panel trimmers can be adjusted finally to suit.

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| ARPI2 | 31. | EBC33 | 71. | EZ40 | 71. | P×25 | 91. | Y66 | $8 /$. | 6C6G | 31. | $7{ }^{7} 4$ | 51. | 2507H | 49 | CV1596 |  |
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| ATP4 | 219 | EC90 | $20 \%$ | G1/236G | 91. | PY83 | 713 | IO8GT | 61. | $6 \mathrm{F7}$ | 51. | 12 AH 7 | 51. | 715B | 60\% | 5BPI | 351. |
| ATP7 | 516 | EC91 | 31. | G120/1B | 91. | PZI-35 | 91. | IE7G | $7 / 6$ | 6F5GT | 5/9 | 12AT7 | 516 | 717A | 816 | 5CPI | 42'6 |
| AUI | 51. | ECC81 | 516 | GL450 | $10 \%$ | QP21 | $6 \%$ | IG6GT | 61. | 6F8G | 51. | 12 A U | 91. | 801 | 61. | 5FP7 | 45\% |
| AU4 | 51. | ECC82 | 616 | GL464A | $10 \%$ | QP25 | 51. | ILA | 31. | 6F12 | 416 | $12 \mathrm{Cu7}$ | 616 | 803 | 2216 | 5FP7A | 25'. |
| AW3 | 41. | ECC83 | 71. | GU20/21 | 401. | QS95/10 |  | ILDS | 51. | 6 Fl 3 | 51. | $12 \mathrm{AX7}$ | 71. | 805 | 301. | 78P7 | 401. |
| AZ31 | 71. | ECC84 | 71. | GZ32 | 91. | QV04/7 | 7 I | IR5 | 61. | 6F33 | 316 | 12 C 8 | 31. | 807 (sel | c- | 120P7 | $60 \%$ |
| BS4A | $5 / 6$ | ECC85 | 81. | H63 | 71. | R3 | 81. | 154 | 51. | 6G6G | 216 | 12 El | $20 \%$ | ted) | 516 | VCRX2 | 253 |
| BT45 | $15 \%$ | ECC91 | 41. | HK54 | 51. | R3/10 | 4/. | 155 | 516 | 6H6M | 116 | 12H6 | 21. | 807BR | 51. | (with | scann- |
| BT9B | $20 \%$ | ECF80 | 1016 | HL23 | 61. | REL21 | 251. | $1{ }^{1} 4$ | 41. | 615 | 316 | 12J5GT | 316 | 808 | 81 | ing coil) | (1) 45\% |
| BT83 | 2216 | ECF82 | 816 | HL230D | 61. | RK34 | 216 | IW4 | 61. | 6J5G | 31. | 12 J 7 GT | 81. | 810 | 801. | VCR138 | $830 \%$ |
| CV54 | 51. | ECH81 | 716 | HVR2 | 1216 | R×235 | $10 \%$ | 2 A 3 | 51. | 616 | 316 | 12K7GT | 416 | 813 | 60\% | VCRI39 | 9 A |
| CV71 | 31. | ECL80 | 716 | KRN2A | 191. | SP2 | 316 | 245 | 61. | 6J7G | $5 \%$ | 12K8M | 716 | 815 | 40\% |  | 35'- |
| CV102 | 11. | ECL82 | 816 | KT32 | 81. | SPI3C | 416 | 2A6 | 71. | 6K6GT | 61. | 12Q7GT | 414 | 816 | 30\% |  |  |
| CV264 | 20\% | EF36 | 316 | KT8 | $22 / 6$ | SP41 | 216 | 2C34 | 216 | 6K7G | $2{ }^{1}$ | $125 A 7$ | 71. | 829A | 301. | Pho |  |
| CV4014 | 81. | EF37A | 71. | KT33C | 41. | SP61 | 21. | 2 C 42 | 251. | 6K7GT | 419 | $125 C 7$ | 41. | 832 | 151. | Tub |  |
| CV4015 | 71. | EF39 | 41. | KT44 | 613 | STV280/40 |  | 2 C 46 | 301. | 6K8G | 519 | $125 G 7$ | 3/. | 832 A | 351. | CMG8 | 91. |
| CV4025 | 10\% | EF50 | 116 | KT63 | $5 \%$ |  | $12 / 6$ | $2 \times 2$ | 41. | 6K8GT | 813 | $12 \mathrm{SH7}$ | 31. | 843 | 714 | GS16 | $12 / 6$ |
| CV4046 | 40\%. | EF54 | 313 | KT76 | 10\% | STZ280/80 |  | 3A4 | 5). | 6K8M | 816 | 12SJ7 | 51. | 866A | 141. |  |  |
| CY31 | 61. | EF55 | 51. | KTW61 | 6\% |  | 50\% | 3B7 | 51. | 6L5G | 61. | 12SK7 | 316 | 930 | 81. | Special |  |
| DI | $1 / 6$ | EF70 | 41. | KTW62 | $6 \%$ | SU2150A4'9 |  | 3B24 | 51. | 6L6 | 91. | $12 \mathrm{SL7}$ | 519 | 954 | 41. |  |  |
| D41 | 313 | EF73 | 61. | KTW63 | 616 | T41 | $7{ }^{1 .}$ | 3 E 29 |  | 6L6G | 61. | 12 SN 7 | 519 | 955 | 216 | 2 3 31 | 451. |
| 077 | $4 / 3$ | EF80 | 516 | KTZ41 | 61 | TP25 | 151. | (829B) | $80 \%$ | 6L7G | 416 | 12SR7 | 51. | 956 | 21. | 3A/1481 | $145{ }^{2}$ |
| DA30 | $12 / 6$ | EF85 | 616 | KTZ63 | 81. | TTI | 31. | 3Q4 | 61. | 6L34 | 416 | 12 Y 4 | 21. | 957 | $5 \%$. | 3J170/E | 438 |
| DAF70 | 351- | EF86 | 71. | MH4 | 316 | TT15 | 25\% | 354 | 51. | 6N7G | 519 | $14 \mathrm{L7}$ | 71. | 958A | 41. | 3192/E |  |
| DAF91 | 61. | EF89 | 71. | MH4I | 51. | TZ20 | 16\% | 3 V 4 | 61. | 6N7GT | 61. | ISD2 | $6 \%$ | 1616 | $3 \%$ |  | 37.10 |
| DAF96 | 716 | EF91 | 316 | ML4 | $4 \%$ | U12/14 | 8\% | 5R4GY | 91. | 6Q7G | $6 \%$ | 2042 | 1716 | 1619 | $5 \%$ | 4J31, | 435 |
| DD41 | 41. | EF92 | 31. | ML6 | 61. | U17 | 51. | 5 T 4 | 91. | 6R7 | 61. | 21B6 | 91. | 1625 | $6 \%$ | $4150^{\circ}$ | 435 |
| DETS | 151- | EF95 | 51. | MS/PEN | 6\% | U18 | 616 | 5U4G | 51. | 6SC7 | 516 | 25L6GT | 719 | 1626 | 416 | 5D21 | 63 |
| DET19 | 316 | EL32 | 319 | OB3 | 71. | U27 | 81. | 5 F 4 G | 81. | 65C7GT | 51. | 30 | 51. | 1629 | 416 | 723A/B | $50^{\prime}$ |
| DET20 | 21. | EL33 | 71. | OC3 | 516 | U52 | 51. | 5Y3G | 31. | 65G7 | 5/. | 35L6GT | $8 \%$ | 4043C | $13 / 6$ | 725A | 30\% |
| DF39 | 41. | EL35 | $6 \%$ | OD3 | 61. | UCH42 | 716 | 5Y3GT | 61. | 6SH7 | 31. | 35 T | 1716 | 4063 | $8 \%$ | 726A | $27 / 6$ |
| DF72 | 716 | EL4I | 81. | OZ4 | 41. | UBF80 | 816 | 5Z4 | 816 | 65J7GT | 419 | 35Z4GT | 71. | 6064 | 10\% | ACT6 | 160\% |
| DF91 | 41. | EL42 | 81. | PCC84 | 71. | ULII | 51. | 5Z4G | 71. | 6SJ7Y | 616 | 37 | 41. | 6065 | 81. | CV193 | $30 \%$ |
| DF96 | 716 | EL84 | 71. | PCC85 | 81 - | UL12 | 51. | 6AB7 | 41. | $65 K 7$ | 51. | 38 | 41. | 6120 | $4!$. | CV239 | 70\% |
| DK96 | $7 / 3$ | EL91 | 416 | PCF80 | 71. | UL41 | 71. | 6AC7 | 31. | 6SL7GT | 616 | 42 | 51. | 6516 | 81 | CV980 | 31. |
| DL92 | 61. | EM80 | 81. | PCF82 | 81 | UL84 | 716 | 6AG5 | 31. | 65N7GT | 416 | 58 | 61. | 7193 | 119 | KR6/3 | $\underline{4}$ |
| DL94 | 61. | EM84 | 1. | PCL82 | 816 | Uu9 | 516 | 6AG7 | 61. | 6SQ7 | 61. | 59 | 61. | 7475 | 31. | L57B | $30 \%$ |
| DL96 | 716 | EN31 | 101. | PCL83 | 10\% | UY41 | 61. | 6AJ7 | 3/- | 6557 | 31. | 75 | 516 | 8013A | 25'. | WL417 | A |
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49/6

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 Model PT340/10/50/250/500/1,000 volts A.C./D.C. $0 / 1 / 100 / 500 \mathrm{~mA}$ D.C. Resistance $0 / 100 \mathrm{k}$ ohm.

Ideal pocket sized multi-tester for all radio and domestic work.
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| $\times C I 4 I$ | 101 |  |  | $\times A 151$ 51- XCl63 71- XCl42 151$\begin{array}{llllll}\times A 152 & 51- & \times C 181 & 71 & \times C 155 & 201- \\ \times A 161 & 916 & \times C 1014 & \\ \times C 156 & 221\end{array}$

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## New Transistor Catalogue with

 Connection Diagrams, Equivalents and Details included in New 44 Page Catalogue, 11 .| A | 2716 |  | 201- | OC78D | 71- |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AFII 4 | 111- | OC29 | 20'- | OC82 | 10'- |
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| AFII6 | $101-$ | OC41 | 91. | OC84 | 816 |
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| C107 | $14 / 6$ | OC44 | 716 | OC171 | 1016 |
| CY21 | 61- | OC45 | 616 | OCP71 | 291- |
| AFZ 12 | 35 ${ }^{-}$ | OC71 | 51. | ORPI2 | 1216 |
| C16 | 201- | OC72 | 71. | MATIOO | 719 |
| C22 | 231- | OC75 | 71- | MATIOI | 1816 |
| C23 | 3316 | OC76 | 71- | MATI20 | 7/9 |
| C24 | 291- | $0 \mathrm{C78}$ | 71 | MATI21 | 1816 |
| C25 | 121- | OC81 | $71_{11}$ | SB305 | 816 |
| C26 | 251- | OC8ID | 71- | SB231 | 1216 |
| $\begin{aligned} & \text { Spe } \\ & \text { Mat } \end{aligned}$ |  | $\begin{aligned} & \text { Very Lo } \\ & \text { Sets_L } \end{aligned}$ |  | us Quot |  |
| SIL | CO | N RECTI | FIE | 500 mA |  |
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[^4]:    DERBY AND DISTRICT AMATEUR RADIO SOCIETY

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    Probably the most enjoyable meeting for many members was the Christmas Party held on December 19th. There were no more meetings for December but a club net on 160 m was operated on Christmas Eve and New Yoar's Eve.

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