A COMPREHENSIVE PRE-AMP PRACTICAL (6) MARCH WIRELESS

TRANSISTORS FOR P.A.

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CONTENTS TRANSISTORISED WOLTMETER SWITCH-TUNED T.R.F. IMPROVING THE "19 SET" TRANSISTORISED TIMING UNIT "MAGIC NEEDLE" ETC. ETC. ETC.

PRACTICAL WIRELESS

March, 1960

PORTABLE TRANSMITTER RECEIVER No. 18

Entirely self-contained 6-valve Transmitter Receiver for voice and C.W. Frequency: 6-9 Mc/s (50-33 metres). The Transmitter signal is generated by a master oscillator circuit foilowed by a power amplifier. The aerial is auto-coupled to the power amplifier by aerial taps to a parallel tuned output circuit. The Receiver is a 4-valve superhet, comprising signal frequency amplifier, frequency changer, I.F. amplifier 2nd det. -A.V.C.-A.F., Stage, Selectivity: The resonance curve of the I.F. amplifier has a width of 7 kc/s, with

an average cut-off of 5 db/kc/s. Full netting facilities. circuit set for full modulation. operated by standard dry batteries, range approximately 10 miles. Incor-porates Test Meter for aerial loading. K.T. & L.T. readings. Supplied Brand New complete with Power Microphone. Headphones. Morse Key, Aerials. Webbing and full in-struction book all for only 80%. Carriage 10%- 18 Set as above less attachments 60/-, Carriage 10%-.

60/-. Carriage 10/-



meter, circuit and instruction book. (American manu-facture.) In used condition, 65/-, carr. 10/-.

MONITOR **TYPE 28.**

Consists of VCR138. 6-SP61, 1-5U4, 1-VU120: 3-EA50. 1 m/a meter scaled 100-0-100 volts. Incorporates Y shift. X shift in u/secs. Focus. sync. Bias. Input to X plates switched X 20, X 5 and direct, requires only suitable power pack for use as oscillo-70/scope. carr. 10'-.

PORTABLE TRANS/RECEIVER SET



NJARCLEIVER JEI Consisting of trans receiver covering 7.49 Mois, range up to 10 miles adphones, micro-pelescopic aerial. Only re-tuites 120 v & 3 v. dry bat-tery. These magnificent trans/receiver sets (as used by H.M. Forces) arr ideal for any application and can be operated with ease.

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POCKET MULTIMETER **BRAND NEW**

2.500 o.p.v. Multi range 6/30/120/ 300/1.200 v. A.C., ditto D.C. 0-1 K., 0-1 megohm : 400 Micro-A., 12 mA. 300 mA. -00 to +64 db 5 ranges : 3in. x 4im. x 1im. Large clear dial Leads supplied. List Price £6.19.6. OUR PRICE £4.7.6. Saving you £2.12.0. P. & P. 28.





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-B.C.602





2500 imp. using soft rubber miniature ear moulds for maximum music and voice reproduction of the finest quality. Supplied free is a small transformer unit with cord and plug which steps impedance up to 4.000 n. ONLY 15'. P. & P. 26.

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R.F.26. covers 50-65 Mc/s. vernier calibrated tuning. 20/-. R.F.26.

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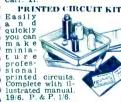
CRYSTAL DIODES 6/- per doz. P. & P. 1/-.

MICROPHONES - BRAND NEW. Throat magnetic 4/6; Throat carbon 3/6; No. 8 carbon with switch 6/6; No. 7 moving coll 6/6. Tannoy power mikes only 5.

U.S.A. WHIP AERIALS, 12ft. 12/6. P. & P. 2/6.

V.H.F. MOBILE AERIAL and base. as used by Taxis, Police, etc., 7/6. P. & P. 2/6.

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15/-. S.A.E. for further details. HI-FI CO-AX SPEAKERS BRAND NEW-U.S.A. MADE. 12in. Co-axial Speaker. The wooler uses 6.8 oz. Alinco 5 magnet. Has 3in. tweeter and an electronic crossover network to separate the speaker functions. Frequency response: 40-17,000 cycles. Output 12 watts, im-pedance 8 ohms. ONLY 160/-8in. 2in. tweeter, 10 watts, etc.. 90.- P. & P. 4/- on each.

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wiring diagram.

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A complete set of parts to construct a Stereo amplifier with an undistorted output total 6 watts. For A.C. mains input of 200-250 v. **63-19-6** Outputs for matched 2-3 ohm speakers. Sensitivity 130 m. C. Ganged Vol. and Tone Controls. Preset balance control. Full instructions and point-to-point wiring diagrams supplied. Only good quality Carr. and pkg. 5/-components and latest high grade valves used. Exceptionally realistic reproduction can be obtained at ample volume for the home, as can be demonstrated in typical surroundings at our County Arcade premises. A really sensational offer.

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LINEAR 'DIATONIC' 10-14 WATT HIGH FIDELITY PUSH-PULL ULTRA LINEAR MPLIFIER. FOR 200-250 v. A.C. mains. Valves ECC83. ECC83. EL84. EL84. EL84. EL84. ECC94. ECC83. EL84. EL84. EL84. ECC95. FOR The Controls. Independent 'Mike 'and Gram input sockets. Outputs for 3 and 15 ohm speakers. Only 12 GNS.' or Deposit 22/3 plus 10- carr. and 12 monthly payments of 22/3. Send S.A.E. for leaflet.

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Boost controls. Twin separately controlled high gain inputs so that two mstruments such as Guitar and String Bass can be used at the same time. Two loudspeakers are incorporated, a high Flux 12 in. for Bass notes and a 7 x 4 m elliptical for Treble Cabinet is well made and finished satin walnut. Size approx. 18 x 18 x 8 in. H.P. Terms. Deposit 23/6 and 12 monthly payments of 23/6. Both models for 200-250 v. A.C. Carr. 10/-Carr. 10/main



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UNESS: CASH WITH ORD VALUE £3 UPWARD FROM THE WORL	ER OR C.O.D. O 8 POST FREE. D'S FINEST MA	NLY. POST/PACKING C ALL VALVES BOXEI NUFACTURERS. PERSO	450 v. 3/9 8 x 16 mfd., 450 v. 3/9 HARGES 6d. PER ITEM : C.O.D. 2/6 D. FULLY GUARANTEED, AND DNAL SHOPPERS WELCOME FROM VALVES, WITH FULL TERMS OF

CED FIGM THE WORLD'S FINEST MANUFACTURERS, PERSONAL SHOPPER'S WELCOME FROM S 1 p.m. CATALOGUE OF OVER 1.000 DIFFERENT VALVES, WITH FULL TERMS OF LASE ENQUIRE FOR ANY ITEM NOT LISTED WITH S.A.E.



'TESTGEAR' SCOPE 3in, D.C. OSCILLOSCOPE



8-WATT PUSH-PULL AMPLIFIER COMPLETE WITH CRYS TAL MIKE AND 8in LOUDSPEAKER 8in.

Guitars, etc. Or 20/- deposit Plus P. & P. 7/6, and 4 monthly payments of 23/-.

2-TRANSISTOR POCKET RADIO

Plus Germanium diode, fully tuneable over medium and long waves. Size 31in. x 41in. x 4in. Complete set of components including case. 2 transistors and earpicce (less batteries).

19/6 Plus P. & P. 1/6. Point to point wiring diagram 1/6, free with kit.

PUSH-FULL OUTPUT STAGE Inclusive of transistors with input and output transformers to match? ohms steech coil, suitable for use with the above kit. Complete kit of parts including transistors.

 $\frac{19/6}{P \& P.1/6} \frac{P \ln s}{P \& P.1/6}$ Point to point wiring diagram 1/6, free with kit.



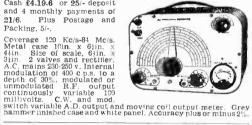
SIGNAL GENERATORS



Cash £6.19.6 or 25/- deposit and 6 monthly payments of 21'6. Post and Packing 5/- extra.

Coverage 100 Kess 100 Mess in tundamentals and 100Mess to 200 Mess on harmonics. Metal case 10in x Clin. x 5Hn., grey hammer finish incorporating three miniature valves and Metal Rectifer. A.C. Mains 200'250 v. Internal Modulation of 400 e.p.s to a depth of 20%; Modulated or unmodulated R.F. output continuously variable 100 milivolts. C.W. and mod. switch, variable A.F. output. Incorporating magic eye as output indicator. Accuracy plus or minus 2%.

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B.S.R. MONARCH 4-speed plays 10 records 12in. 10in or 7in. at 16. 33. 45 or 78 r.p.m. Intermixes 7in., 10in. and 12in. records of the same speed. Has manual play position : colour brown Dimensions: 123in. x 10%in. Space required above baseboard 41in.. below baseboard 23in. Fitted with Full-Fi turnover crystal head.

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Will tune to all Band I and Band III stations. BRAND NEW by famous manufacturer. Complete with PCC84 and PCF80 valves (In series) I.V. 16-19 or 33-38. Also can be modified as an aerial convertor (instructions supplied). supplied).

Complete with knobs. **22/6** Plus 3/6 P. & P. HEATER TRANSFORMER to suit the above. 200-250 v., 6/*. Plus 1/6 P. & P.

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All with tapped primaries. 200-250 volts. 0-160, 180, 200 v., 60 ma., 6.3 v. 2 amps. $10^{-6},$ 220-0-320 v. 75 ma., 6.3 v. 2.5 amp., 5 v. 2 amp., 10^{-6}, 230-0-200, 60 ma, 6.3 v. 2 amp., 6.3 v. 1 amp., 10^{-6}, Postage and packing on the above 3/-

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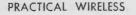
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** 5-10 ** MAIN AMPLIFIER which an undistorted power optiput of up to 10 watts is bian is thoroughly recom-mended to ** Hi-Fi ** en-thusiasts who contemplate a versatile and very high omitoners AND NEW MULLARD VALVES including PARMEKO MAINS TRANSFORMER including PARMEKO MAINS TRANSFORMER function of the latest Ultra-Linear Tumer) and the choice of the latest Ultra-Linear Tumer) and the choice of the latest Ultra-Linear PRICE COMPLETE KIT (PARMEKO £10.0.0 Alternatively we supply ASSEMBLED output Trans AROVE INCORPORATING PARTRIDGE OUTPUT TRANSFORMER, \$1.6.0 EXTRA.

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Comprises two "3-3" M MULLARD on HARN AMPLIFIERS on one enassis and is designed to operate with our DUAL CHANNEL FRE-AMP-LIFIER for both STEREDPHONIC or MONAURAL operation.

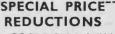
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March, 1960

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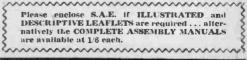
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This model incorporates two 2-valve Pre-Amplifiers (described above) combined into a Single Unit enabling it to be used for both STERFEO-HONIC Or MONAUK RAL operation. It is designed primarily to operate with our range of MULLARD MAIN AMPLIFIERS but will also operate equality well with any make of Amplifiers requiring an input of 250 mivolts. of Amplifiers requiring an input of 250 mivolis. COMPLETE KIT \$12,10.0 ASEMPLED \$15,0.0 OF PARTS \$12,10.0 AND TESTED \$15,0.0 It will operate equality well for MONAURAL only operation with one "5/10" Main Amplifier to which the second Main Amplifier can at any time be added, thus very easily providing for both STEREO operation . (a) The DUAL CHANNEL PRE-AMPLIFIER together with the Dual "3" "MAIN AMPLIFIER. (b) The DUAL CHANNEL PRE-AMPLIFIER with two "5/10" MAIN AMPLIFIER. THE ASSEMBLY MANUAL is available for 3'-.



RADIOL



"5-10" MAIN



PRACTICAL WIRFLESS



Carriage and Insurance 12/6 EVACUUMED RE CRM02, MW22-7, MW22-14, MW22-14C, $\]$ £2/15/- SZ/15/- CRM121, CRM121A, CRM122, MW31-14C, $\]$ £3/-/- £3/-/- £5 WW31-17, MW31-18, MW31-16C, $\]$ £3/10/- £5 £3/10/- £5 I21K, I41K, AV36-21, C14FM, CRM122, CRM124, MW36-24, MW36-44, MW36-44, MW36-44, MW36-44, MW36-44, MW36-44, MW36-46, MW36-46, MW36-36, CRM1528, CRM1548, CRM1548, CRM1548, CRM1548, CRM1548, CRM1548, CRM1548, CRM154	RANTEED 12 EGUNNED 5/10/- 5/15/- £ 5/15/- £ 5/15/- 15/- 15/- 15/- 15/- 10/- FFER : £ STORS : STORS : 0 ontput up to 8 8/- doz. GEX 8/- doz. GEX 8/- doz. GEX 15/- 16/-	MONTHS. NEW 27/19/- 28/19/- 28/19/- 22/19/- 22/19/- 22/19/- 22/19/- 22/19/- 22/- 23/- 23/- 23/- 23/- 22/- 23/- 23	ALSO A/6 - cuch - c	ARRIAG ARRIAG ARRIAG ARRIAG REE TR/ ARRIAG REE TR/ CARRIAG CONTINUES	AKES, Comp are unavualled are unavualled are unavualled are unavualled are unavualled are the area are the area area area area area area area are	tin value di in va
COLLARO "CONQUEST" H:F: 4 spl. 10 record Auto. $\pounds 6/19/-1$ Ioo CONDENSERS 10/- 100 CONDENSERS 10/- A must for your sparks box. A vell-balanded southenest of miniatres there mica and ceramic southenest of animatres there mica and ceramic southenest of a southenest. 1-2 watts VALVES ALL GUARANTEED 3 MONTES PL81 SOULED AMAZING 5/- EV51 ENDS 5/- U25 ENDS 8/- talaxy dulu sapphire crystal turnover pick-up head. Amazing value. $\pounds 3/10/-$ Carr. 3/- TO CONCOUNT SO PURCHASERS In dozens). Post 1 valve, dd.; 2-11, 1/- DYA 5/6-017 6/6-01767 7/9 4536 5/6 1/2070 6/-1900. AGG T 8/6-0176 7/9 4536 5/6 1/2070 7/-1900. AGG T 8/6-0176 7/9 1/255 1/26 1/26 1/2947 7/6 1548	STORS: Ontput up to 8 /HITE SPOT. - per dozen XA 10/-; GETL5, 2 General purpos 8/- doz. GEX HERS: For 10, 10, 7 /5/-, RM1, 6/6 (GLT RECORD wed 4/54 meed 4HF XORD AUTOCC X55A Senior	SPOT SPOT 800 kc/a. (4' R.F. and 1. A103, 15/-; .) 25/- 26/- 26/- 26/- 25/- 26/- 25/-	I'e cach. with 1.8; 2.5 POW XA104, We gi XA104, OUTP ake. 9d. stransf .8;9, selen- bridge, I'll doz. Af .17/-; I.20- .17/-; I.20- .17/-; F .319 0 STEIG .2 7 B	event manufactur F& I avit ontpu- ice free the corp UT BLANSFOR Una and 4 Transl form your existin NFRA RE Iall Price. 80 00w. £3/5/- PICK-UP ACOS 22/6. G AND REUTER	rere matched po put. Transiston recet Push-Puil MERS of Hill Bistor Angilther og receiver or me "outfit. ED HEA DO W. \$; - 2,000w CARTRIL POWER POI a 15/~, SON	air of GUT re, price 50 INPUT AN the Grade co- circuit. W amplither the TERS 3/-/- £3/10/ DGES INT 18/6. OTONE 17/6
VALVES SPECIAL OFFER PURCHASERS NEW 0% DISCOUNT SPECIAL OFFER PURCHASERS NEW 0xy SIX VALVES marked In black type (15%) NEW 0xpens). Post: 1 valve, 6d.; 2:11, 1/ NEW GUARAAI 24 5/6, 015 8/6, 015/07CT 7/9, 045:04 5/6, 129/07 6/-159/07 AGCT 5/-0B8c 3/6, 05K 05T 6/6, 015 05T 6/6, 128/07 6/6, 128/07 AGGT 5/-0B8c 3/6, 05K 05T 7/9, 0155 12/6, 0128/07 6/-050/0	C120D MKII C121/4 MKII Carr. and Pack	2HANGERS £7 £9 £9	3 19 0 POR 7 15 0 POR 7 19 0 amplif 7 19 0 amplif	RTABLE RI	ECORD P changer, 21 wa	att high gai
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	RET I LOW PI NTEED 3 <i>AGT 9(3) DP96</i> I U 10/6 DH85 I U 10/6 	FUGES MONTH B B B B B B B B	RN FREE or of (tee op 92 6(6 E493 7.6 E493 7.6 E493 7.8 E484 8.9 B484 8.2 B4	OFF OFF 2 TRANSIT INSUI (oily cummittee) Saliafact b goods If return Saliafact b goods If return Saliafact 9/8 Pid Saliafact Saliafact 9/8	PCO RANCE. All v ex-Government Lon or Money I et unuset wit - T41 7/6 (5 TH30C 12/6 (6 TH30C 12/6 (6 U14 8/- (7 U22 6/9 (0 U22 6/9 (0 U23 13/6 (0 U23	ST alves are or to rear-equi- back Guneral UCH81 & UCH81 & UCH82 & UCH82 & UCH82 & UCH84 & UCH85 & U

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 5/6 eD2
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 4/- EB41
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 USA
 HLAIDD9/6 PL22
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 G7
 6/8 GFG
 6/3 0B7G
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The new. excitins De ket Radio in beautifur moulded plastic case. This noted is a highly sensitive, self-contained set covering all medium waves. Uses modern miniature button-base valve and specially designed high efficiency coil. Excep-to-stor plans-the case is supplied ready drilled! Size of radio only 4 in x ready drilled! Size of radio only 4 in x and bat-treites fit inside. We all a supplied



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Our engineers have designed a novel Wrist-Watch Radio using latest Transistor Tech-niques. Size only lin, x lin, i !: -"Feather-weight"--yet gives clear, crisp-personal-phone reception over all medium waves. Tiny hattery inside lasts months-costs 5d. No Snags, anvone can build it in an hour or two using our pictorial step-by-step simple plans. All parts supplied (including case and strap) for only 29'6 (add 2:6 Post etc.). C.O.D. 2- extra. (All parts sold separately, priced parts list 1/6.) Send Now !

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Rhowledge whatever in the minutes. Handsome black and crackle steel case with specially made black and gold dial with stations printed. Size of radio only 611n. X 51n. X 51n. Covers all medium and long waves. H.T. consumption only 1 to 1.5 mÅ. Ideal for Bedroom. Garden. Holiday, etc. BUILD THE "SKY.ROMA" NOW! Total building cost-everything down to the last nut and bolt. 476 (Postage. etc., 2'-)- with full set of clear, easy-to-follow plans. (Parts sold separately. Priced parts list and plans 1/6.) C.O.D. 2.- extra.



The sensational "Silvertone "model 'A highly compact self-contained minia-ture "button-base" valve pocket radio at absolute "rockbottom" building cost. Covers all the medium waves with the very latest circuitry bringing at . with the very latest circuitry bringing in stations from all over Europe-with-out luss. Easy as A.B.C. to assemble, using our step-by-step instruction manual. Size only 4] in, x 2in, x 1in, -a fa-cinatinr little pocket radio. We can sumply all the parts including beautiful two-lone case, detachable acrial. Instruction book screws, wre. etc., toronly 29 6 plus 2/- post and packing). C.O.D. 2. extra. (Parts sold separately, priced parts list 19.)

THIS TRANSISTOR SET Can Be Built For Only 296. The Sky-Scout Pocket two-29/6 Scout " Pocket, two-stage transistor set, size only lin, x din, x filn. Covers all medium waves and works entirely oil tiny "penlight" battery which costs 64, and fits inside case. All parts tested before despatch. Can be built for 29.6, plus 2- Post and Packing. INCLUDING CASE. TRAN-SISTOR. STEP-BY-STEP PI.ANS FOR ABSOLUTE BEGINNERS, nuts, bolts, etc. (C.O.D. 2- extra.) Parts sold separately, priced parts list and plans 1.6. VERY SIMPLE TO BUILD.

This amazing "Tiny-Tim" model-no larger than a match-box-costs nothing to run-ever. We batteries : No Valves : No electricity ! Will meter run down or burn out. Uses the latest TRANSISTOR TYPE GER-MANIUM DIODE, receives local stations any-where-without extra aerial. Clear. Crisp Tone. No snags. anyone can build it within an hour using our step-by-step instruction book. etc., for only 15 - plus 2 - Post and Packing (C.D. 2'- extra). (Parts sold separately, priced parts list 1'9.)

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March, 1960

NO DEPOSIT - INTEREST FREE - 20 or 36 WEEKS TO PAY !



916

Balance at 2/11 per week for 19 weeks.

A beautifully styled cabinet. Made by a famous manufacturer. In polka dot cloth with clipped lid and carrying handle. Size 16 x 141 x 81in. deep. Will take B.S.R. Monarch 4-speed Autochanger and 7 x 4in. elliptical speaker and most of the modern portable amplifiers. Carr. & Ins. 4/6. Cash Price. 59/6.

AMPLIFIERS 12 Months Guarantee ALL PORTABLE AMPLIFIER Mk. D.1. 59/6

Brand new. Latest design with printed circuit. Dimensions 7 x 24 x Sin. A.C. only. Mains isolated 2-3 watts output. Incorporating EL84 as high gain output valve. Volume and tone controls. Knobs 2/6 extra. P. & P. 3/6.

AMPLIFIER Mk. D.2 79/6 Printed circuit. Latest design, Dimensions 7 x 2 \pm x Sin. A.C. only. Mains isolated. 3-4 watts output. Incorporating the latest ECL82 triode pentode output valve giving higher undistorted output. Volume and tone controls. Knobs 2/6 extra. P. & P. 3/6.

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Continental style cabinet including extra clip-on speaker cabinet. $15\frac{3}{2} \times 10\frac{3}{2} \times 24\frac{3}{2}$ in. deep Takes B.S.R. 4-speed stereo Autochanger. Printed circuit amplifier. Two Bin, speakers, Carr. & Ins. 6/6.



Beautifully made for portable stereophonic record players. Latest design with printed circuit. Dimensions $3 \times 5^{\frac{1}{2}} \times 9^{\frac{1}{2}}$ in A.C. only. Mains isolated. Twin amplifiers each side giving 3-4 watts output, incorporating ECL82 triode pentode valve. Full tone, volume and balance controls. Complete and ready to fit. Knobs 3/6 per set extra. Carr. & Ins. 3/6.

Cash price £7.19.6.

B.S.R. MONARCH U.A.8 4-SPEED AUTOCHANGER



4-speed Autochanger. Incorporating auto and manual control complete with turn-over crystal P.U. and Sapphire stylus. A.C. Post & Ins. 5/6, or Initial Payment 8/1, plus post and & Ins. and 19 weekly payments of 6/11.

T.U.9, B.S.R. 4-speed single player, £4.9.6. Collaro Conquest 4-speed Autochanger, £6.19.6. Collaro Conquest Stereo Autochanger, 11 gns. P. & P. on all the above 5/6.

STURDY CASE, 12/6

 $8\frac{1}{2} \times 7\frac{1}{2} \times 3\frac{1}{2}$ in. deep. Covered in burgundy and grey washable rexine. Strong clasp, hinges and handle. Ideal for portable radio chassis or transistor set. Can be adapted as a record carrying case to hold 18 seveninch long-playing records. P. & P. 2/6.



Balance at 3/5 per week for 19 weeks.

A delightful looking cabinet 14 $\frac{3}{4}$ x 17 $\frac{3}{4}$ x 8 $\frac{3}{4}$ in in 2-tone leatherette. Will take a B.S.R. Monarch 4speed Autochanger and 6m. round speaker. Carr. & Ins. 4/6. Cash Price, 69/6.



Polished oak cabinet of attractive appearance. Fitted with 8in. P.M. speaker W.B. or Goodmans of the highest quality. Standard matching to any receiver (2-5 ohms.) Switch and flex included. ins. carr. 3.9.

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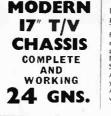
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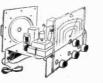
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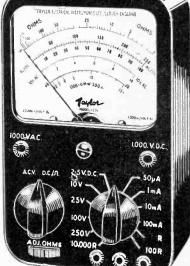
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2 Pole 8 way		 1.01	36
2 Pole 11 way			36
2 Pole 12 way			46
3 Pole 3 way		 	16
3 Pole 6 way			36
4 Pole 4 way		 	
1 Pole 4 way			5.
6 Position shorting	g		30.
6 Pole 3 way			26
6 Pote 3 way ceran	nte		3/6
8 Pole 2 way			21-
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9 Pole 3 way	*** *	 	26
12 Pole 2 way		 	21-

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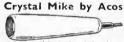
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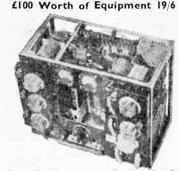


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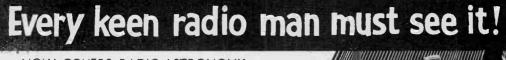
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March, 1960



Practical Wireless

VOL. XXXV, No. 637, MARCH 1960

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RADIO TELESCOPES

D URING the course of this year, wireless will play an important part when the first practical steps are taken to

try to discover whether or not life exists elsewhere in the universe. The radio telescope at Green Bank, U.S.A., will be used by scientists who will listen for radio signals coming from other solar systems. Ever since scientists first made optical telescopes and probed the heavens, the great size of the universe has become more and more apparent, and now it is realised that its enormity cannot be comprehended. It has been supposed that there must be many other worlds similar to our own in which live intelligent beings similar to ourselves, and it is reasonable to assume that any signals transmitted from such worlds would aim at establishing contact with others and therefore would consist of definite sequences.

Naturally, it would be difficult to monitor more than one specific frequency and it is assumed that the wavelength used for the transmissions would be 1,420Mc/s. This frequency is known as the hydrogen line frequency and could be called the most popular frequency in creation since most of the matter in space is neutral hydrogen. Once the frequency of transmission has been assumed, the problem of monitoring becomes easier, although the difficulty now arises of detecting any deliberate modulation at that frequency. Owing to inter-galactic noise and other sources of signals, the detection of pulses may not prove easy. If, therefore, any of the other radio telescopes in the world were tuned to this frequency during their normal programme of work it is unlikely that signals would be detected, even if they were being transmitted. It is unlikely that the Jodrell Bank radio telescope will be used for monitoring space signals in the near future as it is heavily committed to its programme of research in radio astronomy and the tracking of earth satellites and moon probes. Jodrell Bank has a much larger range than the Green Bank telescope and will receive signals from at least 700 light years away and perhaps more and may be at present less suitable than Green Bank for the purpose in mind. The Green Bank telescope will be focused first on the nearest suitable stars. These are some 11 light years away-about 66 million million miles from us.

If there is intelligent life elsewhere in the universe it is reasonable to assume that radio will be the medium used for communication, although the speed of communication will not be as great as might at first be thought. Radio waves travel at 186,000 miles per second but even at this speed it might take 11 years for the signal to reach us and we might have to wait 22 years before we would receive a reply to any signals which we might transmit. In view of the delays involved, the transmission of signals at this juncture seems hardly worthwhile unless a very far-sighted policy is envisaged. The programme at the moment must be one of passive reception and the most that can be expected in the near future is the confirmation that some form of life exists elsewhere in the universe.

Our next issue, dated April, will be published on March 4th

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PRACTICAL WIRELESS

Round the World of Wireless

POTENTIAL AND CURRENT NEWS

Broadcast Receiving Licences THE following statement shows the approximate number of Broadcast Receiving Licences in force at the end of November, 1959, in respect of wireless receiving stations situated within the various Postal Regions of England, Wales, Scotland and Northern Ireland. The numbers include licences issued to blind persons without payment.

Region	Total
London Postal	
Home Counties	
Midland	
MI. I. F.	691,772
Minush Mile	558,805
South Western	485,796
Wales and Border Cou	
Total England and Wa	les 4,305,314
Scotland	
Northern Ireland	
Grand Total	4,960,788

British Equipment for Peru

THE Smethwick (Staffs) firm of Hadley Telephone and Sound Systems Ltd., is providing a staff location installation for a new hospital in Mollendo, Peru. The equipment, which consists of an amplifier, a moving coil microphone, 16 cabinet and 15 spherical type loudspeakers has been ordered from the British firm by Sociedad Relojera SA, of Lima, and will go into the Arequipa Hospital in Mollendo.

British Standard 448

THE B.S.I. announces the publication of another two Sections (BSG/F and B7E/F) to B.S. 448, "Electronic valve bases, caps and holders." The new sections specify the base and bulb outline dimensions of the BSG/F and B7E/F subminiature valves with flexible connecting leads. Gauges for checking the lead spacing and the bulb outline dimensions are also specified. Copies of this Standard may be obtained from the British Standards Institution, Sales Branch. 2, Park Street,



This Kowa Microrecorder is claimed to be the smallest tape recorder in the world. Developed by the Kowa Optical Works of Japan, and produced by the Kowa Electric Laboratory in Nagoya, it can be used for 30 minutes uninterrupted recording on a double-track tape, which is reversed automatically when recording on one track has been completed. It is an all-transistor recorder with playback, and weighs 780 grams. Accessories include a telephone pick-up, "secret" wristwatch microphone, earphones and speaker.

W.1. Price 2/- each. (Postage U.H.F. Systems for S.A. Navy extra to non-subscribers.)

Electronic Computing for B.P.C.

A N order for one of the largest electronic computing systems in the United Kingdom has been placed with Ferranti Ltd. by the British Petroleum Company Limited. The system, costing over £4 million, will also be one of the fastest in the United Kingdom for processing data as it is based on the Ferranti Mercury computer, at present the fastest machine manufactured in Western Europe. The extensive ancillary equipment includes a converter unit which transfers information from magnetic tape to punched cards and vice versa, and facilities for printing data from magnetic tape or: very high speed printing units. The system will be used by the British Petroleum Co. for both scientific and commercial applications. It is anticipated that the system will be installed in one of the company's head office buildings in London around the turn of the year 1960/61.

A SUBSTANTIAL order for multi-channel medium and high power communication equipment has been placed with Plessey International Limited by the South African High Commissioner in London. The equipment will be installed on South African Navy fighting ships for ship-to-ship and shipto-shore communication. The placing of this important order follows the success of similar Plessey U.H.F. sets on ships of the British and Commonwealth navies. The order was negotiated in South Africa by representatives of Plessey International Limited.

Radio Trades Examination Board

A the annual general meeting of the board on December 30th last, Mr. Edwin Arthur William Spreadbury. M.Brit.-I.R.E., was elected chairman in succession to Mr. E. M. Lee, B.Sc., M.I.E.E. (Belling and Lee Ltd.). Mr. Spreadbury has been associated with the R.T.E.B. since June, 1943, when he was appointed an examiner and a

member of the examinations committee. Subsequently, he became a member of the committee which drafted the scheme of examination in television work, the first examination being held by the board in 1950. In recognition of this work Mr. Spreadbury was elected to the council of management of the board in 1947.

By reason of his technical articles and books. Mr. Spreadbury is well known to the industry and the trade for his interest in promoting higher standards of servicing efficiency. He has been connected with the radio industry since 1922. He joined the staff of the Wireless Trader in 1937 and is now the technical editor.

Radio-telephones for Mexico two-way units and fixed station equipments. Many of these radio-telephones will be used for the extension of the existing public correspondence scheme. whilst others will be used for new private radio-telephone systems. It is anticipated that 1.000 mobile units will be required by Mexico this year. to a total value of £100,000. Pye has already supplied over 3,000 mobile radio-telephone units to Mexico.

Electrical Engineers Exhibition

THE Ninth National Electrical Engineers Exhibition will be opened by the President of the Board of Trade, the Rt. Hon. Reginald Maudling, M.P., at 12 noon on April 5, 1960, at Part of the Earls Court. " Marine Electrics " feature will be devoted to electrical and electronic equipment from aircraft Britain's renowned carriers, H.M.S. Victorious and H.M.S. Hermes. Also featured will be equipment as used in the S.S. Canberra, the largest liner built in British shipyards since the war. Exhibits will include the latest navigational aids, radar and radio communications equipment. An electrolier. believed to be the world's largest, will be suspended from the 110ft, high roof of the Exhibition Hall. It is built by William McGeoch & Co. and measures 75ft, in circumference. Its total loadings will be around

18.500W. Visitors will walk on the world's largest electrically heated carpet. Made by Thermalay Ltd., it covers over 1,000 sq. ft. and will have a loading of more than 11,000W. For the first time there will be a feature of outdoor electrical equipment. An area of over 5,000 sq. ft. will be devoted to heavy transformers built by the English Electric Co. Ltd.

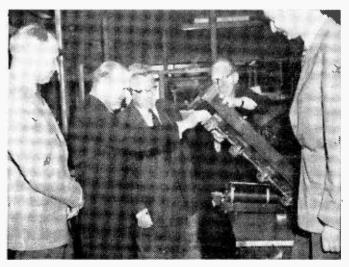
East Pakistan Contract

THE Commissioners of the Port of Chittagong, East Pakistan, have placed an order with Marconi's for the establishment of a V.H.F. radio-telephone network to improve ship-toshore communications within the port area and the Kharnaphuli river. Besides the installation of duplicate V.H.F. transmitters and

equipped to enter or leave the port in full radio communication with the port authorities.

Change of Name

N the 1st January, 1960, the British Thomson-Houston Company, Metropolitan-Vickers Electrical Company and Siemens Edison Swan Ltd. changed their names to Associated Electrical Industries (Rugby) Ltd., Asso-Electrical Industries ciated. (Manchester) Ltd., and Associated Electrical Industries (Woolwich) Ltd., respectively. At the same time five new product divisions of Associated Electrical Industries were announced. They are as follows: (1) Cable Division: (2) Construction Division: (3) Telecommunications Division; (4) Radio and Electronic Components Division: (5) Instru-



Marconi's Wireless Telegraph Co. Ltd., are designing and supplying the electronic equipment for a new air defence system for Sweden, Contracts worth approximately £1,500,000 have already been placed with the company, Recently a delegation of senior officials of the Royal Swedish Air Board visited the Marconi Works at Chelmsford and the Research and Development Laboratories at Great Baddow, in connection with the contract. Photograph shows (L. to R.) Colonel Hamilton and General Rapp of the Royal Swedish Air Board, Dr. E. Eastwood (Chief of Research, Marconi's), Mr. Keall (Marconi's) and Colonel H. Lindgren (Royal Swedish Air Board),

receivers in the shore stations at the port office and at the signal station at Juldia, the order also includes the supplying of mobile stations for use in two harbour tugs and a pilot launch. This installation will enable all visiting ships which are suitably mentation Division. From the 1st January the total of A.E.I. Product Divisions to be established became 12, and the famous companies whose names are to change will cease to trade, but will manage a number of A.E.I. Product Divisions.

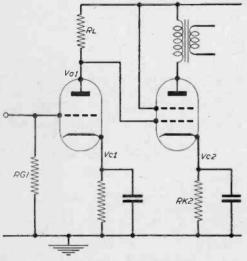
The D.C.2. Stereo Amplifier

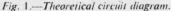
PRACTICAL WIRELESS

A DIRECTLY COUPLED CIRCUIT

By J. S. Kendall

THE power required for listening in the average room is not great—in fact 2W is usually more than enough and even then this is only required on peaks. This stereo amplifier, the D.C.2, is directly coupled with negative feedback and an output of just over 3W per





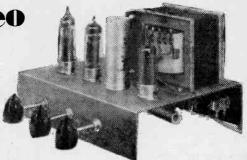
channel. The distortion and noise levels are low. Three controls are provided: volume, tone and stereo/mono. This latter allows one single input to be fed to both channels so that they act in parallel.

Circuit

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For this circuit twin direct-coupled amplifiers have been chosen. There are several reasons for this, one of the main being that from the grid of the input section to the anode of the output valve there is negligible phase shift from the lowest frequency to the highest. There is thus only one component in which phase shift can occur: the output transformer. Again, this phase shift has been reduced by the use of negative feedback. The total number of components is also low and construction for the beginner is simplified.

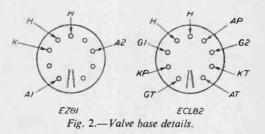
The basic circuit of each amplifier is shown in Fig. 1. It is drawn as a separate triode and pentode, which is correct although they are in the same glass envelope. The anode of the triode is strapped across to the control grid of the pentode section, and no stopper is used—the lead



March, 1960

is only about $\frac{1}{6}$ in., so none is required. Thus the anode voltage of the triode appears at the grid of the pentode.

If the reader is thinking of constructing his own directly-coupled amplifier, he should be warned not to attempt to work the drive valve at too low a voltage to allow it enough swing to drive the output valve correctly, and then attempt to clear up the matter with very heavy negative feedback. Allow an anode voltage of at least twice the r.m.s. drive voltage required by the output valve-within reason, the higher the better. but not so much that the output valve is starved of voltage. The average power supply unit with a 250-0-250V transformer will give about 300-320V smoothed. Remember that the anode voltage of the drive valve and the normal bias voltage of the output valve have to be substracted from this figure. A good figure for the anode voltage of the drive valve is 25 to 50V. The voltage at the cathode of the voltage output valve has to be the anode voltage of VI plus the bias voltage of V2, i.e., Vk2=Va1 + (bias for V2). For example, H.T. line voltage is 300, the anode resistor for VI is 220k and the anode current of VI is 1.2mA. Thus, the voltage dropped across RI would be 260. Thus, at the anode of VI we would have 300-260=40V. To this we have to add the value of the bias for the output valvesay, 6V which gives 46V. This, to the nearest 10 per cent., is 50V. Looking up the valve, we find, say, Va = 250V., Ia = 36mA, Vg2 = 250V, Ig2=4mA. We add the currents together: 36 + 4 = 40mA and we can now, by a further



simple calculation, calculate the value of the cathode resistor of V2 (Rk2). We have the voltage as 50V and the current at 40mA. Therefore, Rk2=1.25k. Now, 1,250 ohms is not a preferred value of resistor. Therefore, we must

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find the nearest 5 per cent. preferred value, which is 1.2k. The wattage rating is next to be found. In this case W=EI is the formula to use. We have found E to be 50 and I as 0.04A (converting mA to amperes), so $50 \times 0.04=2W$. In this instance, as in all others where low drift is required, use a resistor that is well within its rating, say, 5W 5 per cent. wire wound. Next, having built the unit we have to test it. The

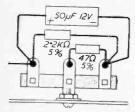


Fig. 3.—Wiring of the sub-assemblies for the triode stage.

critical reading is the one at the cathode of the output valve. The reading here is very rarely just as calculated even if we have made all our calculations correctly. The currents through the valves vary from valve to valve by quite a large amount, and also the conditions of the first valve circuit are reflected into the circuit of the second valve. It is the current through the output section of the valve that we have to watch, and bear in mind that we can expect a change in bias of 10V on the output valve for every 8mA change in Ia. Calculate the voltage drop across the valve and work out the power dissipated by it and check that this is not outside the ratings given by the manufacturers. If the errors are large, then corrections can best be made at the cathode resistor of the drive valve. To increase the resistance here will have the effect of increasing the cathode voltage of the output valve, a decrease will also cause a decrease in the output cathode voltage.

Readings

When taking voltage readings on direct-coupled amplifiers, remember always to have the volume control set at the same point. All valves take a minute amount of grid current by what is known as secondary emission. This minute current, so small that it can usually be ignored, gives a voltage across the input resistor of the amplifier-usually the volume control, and is amplified by the first valve. Thus, say, the

current is one-hundred-millionth of an ampere, and we use a 1M volume control, then the voltage is 1/100th and this amplified, say. 50 times by the valve gives $\frac{1}{2}V$. With a modern output valve that can cause a definite change in current. However, with a new valve, it can be ignored, but with a valve that is older and softer, the figure will be ten times as high.

Construction

First the valveholders should be fitted to the chassis. Then as all the transformers are also

associated with tag strips, next fit the mains transformer, and under the two nuts of the fixing bolts at the valveholder side, fix a three-way tag strip. The transformer should be fixed so that the H.T. and heater windings are at the valveholder side, and the mains tags to the rear of the chassis. Shake-proof washers should be used under the tag strips in order that a good connection to the chassis is made—simple, but important. The H.T. and heater wiring may now be made. Fig. 2 shows the base of the EZ81 rectifier valve. Run two wires (twisted for preference), one from each of the 300V secondary to one of the anodes of the EZ81-i.e., one 300V to A1 and the other to A2. Next, take a pair of wires from the 6.3V heater winding (top righthand set of tags on the transformer) to the heater tags of the valveholder; ignore the tag marked 5V and use the common and the 6.3V tags.

Next, take a wire from pin 3 to pin 4 of the valveholder, and solder all the leads so far wired except the wire to pin 3. Next come the heaters of the other two valves—the ECL82s. The base wiring is shown in Fig. 2. Run a pair of twisted wires from the centre tapped 6.3V on the transformer to the heater tags of the valveholders pins 4 and 5—then solder them. Next solder a wire on the mains transformer from the centre tag of the 300-0-300V winding to the centre-tap tag of the 6.3V winding and then on and solder to one of the fixing bolts of the mains transformer.

Sub-assemblies

Next make up two small sub-assemblies—these consist of a three-way tag strip, with an electrolytic and two resistors. They form the bias and negative feedback resistor for the triode sections of the ECL82 valves. 50μ F, 12V electrolytics have

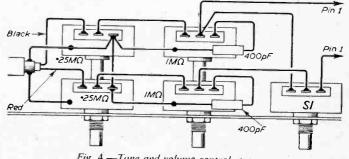
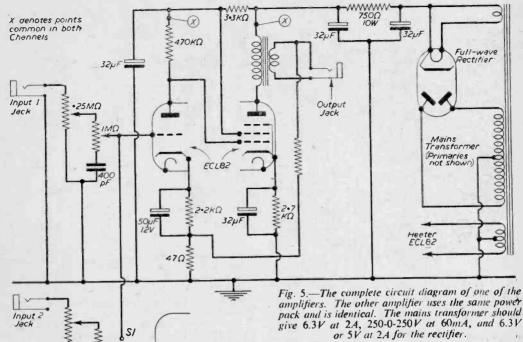


Fig. 4.—Tone and volume control stages.

been chosen and the resistors are of 5 per cent. tolerance. The reason for the use of 5 per cent. resistors has been explained earlier. The method of wiring the tag strips is shown in Fig. 3. A very neat job can be made of these if the wires are kept short—the view is as seen from the front edge of the chassis and the earthing tag is to the rear. At the right-hand end—the end with only the 2.2k and the electrolytic—solder a short length of wire—2in. is ample and it should be insulated. Next fix the four jacks in place, one in each of the four $\frac{1}{2}$ in. holes at the rear of the chassis.



tors are soldered to pins 7 of the same valveholders. A wire is connected between the two pins 7 and a capacitor of 32µF and of 350VW joined between this point and the common earth line. A further resistor of 3.3k, 5 per cent., 3W is joined between the same point (+ve side of electrolytics, two 470k resistors and two tags 7 on the ECL82 valves) and one of the pins of the $32 + 32\mu F$ block electrolytic. Do not solder this last wire vet. At the inner side of the inner output transformer, the tag of a double $32\mu F$ capacitor is joined and soldered to the common earth line. It is simplest to follow if the two tags are placed in a horizontal plane so that one can be referred to as the left and the other as the right. To the left and nearly touching the capacitor is a threeway tag strip. From the right-hand tag of this, fix a wire to the left-hand tag of the $32 + 32\mu F$, and between the same tag and the earth line fix a 2.7k wire-wound 5 per cent. resistor of 7W rating. Strap pin 2 of the nearest ECL82 to the junction of the resistor and capacitor and solder. Between the right-hand tag of the same capacitor and the centre (earthed tag) of the adjacent tag strip join a 2.7k, 5 per cent., 7W wire wound resistor, and from the junction of the 2.7k and the capacitor join a wire to pin 2 of the other ECL82 and solder. To complete the H.T. circuit wiring, take a 750Ω 10W wire wound resistor and join one end of it to the right-hand tag of the extreme left tag strip, run a wire to the cathode of the EZ81 and a further wire from the same cathode to the unoccupied tag of the $32 + 32\mu F$ 450VW electrolytic. Then solder these. The other end of the 7502 10W resistor should be against

(Continued on page 944)

Grid of other Channel It is best to have the tags pointing in the same direction as the flange of the chassis. We can now fix the two output transformers in place.

They are bolted in place with the tags pointing to The small subthe centre of the chassis. assemblies are bolted one under each of the fixing bolts of the output transformers at the end nearest to the valveholders. We can now take the wiring a few steps further. Join the running wires from the sub-assemblies to pin 8 of the nearest ECL82. Join a wire from the inner tag of an output jack to the tag at the valve end of the nearest output transformer, and a 1009 resistor from the same transformer tag to the junction on the sub-assembly of the capacitor, the 2.2k and the 47Ω resistor. Solder and repeat with the other transformer.

Final Wiring

400

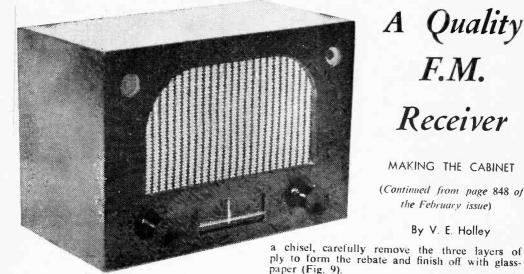
Next, run a length of tinned copper wire through the four sleeve tags of the jacks (those are the tags at the fixing end of the jacks) and solder. Join the two nearest tags of the output transformers to this common earth line and solder. Take two 470k, 5 per cent. resistors and bend the wires sharply back about 1in. from the body of the resistors and solder the bend to pin 9 of the two output valves-one on each-the free end of the wire is taken to pin 3 and soldered. This fixes the resistors in position and joins pins 3 and 9. The wires from the other ends of the resis-

A Quality

F.M.

Receiver

MAKING THE CABINET (Continued from page 848 of the February issue) By V. E. Holley



S stated in the previous article, a suitable cabinet for this receiver may be made from five-ply wood. fin. thick, having an oak, walnut or similar facing.

Procedure

First mark out and cut the front, $13\frac{1}{2}$ in. \times 9in. (Fig. 8) and cut the apertures for the speaker, tuning scale, etc. Those for the tuning indicator and panel light should first be cut from the faced side of the wood with a $\frac{1}{4}$ in. centre bit to a depth of about $\frac{1}{4}$ in. and completed from the other side with a $1\frac{1}{4}$ in. bit. The larger holes can be cut with a fret saw or hacksaw blade, working from the faced side. Sand the edges of all the

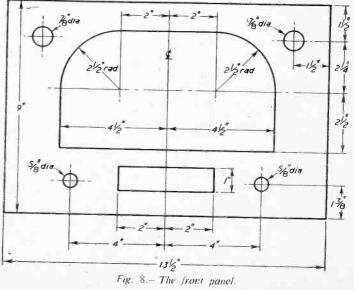
holes smooth and flat, apply a coat of matt black paint and set aside to dry. Keep the paint off the faced surface.

Cut next two pieces for the sides, 9in. \times 7¹/₂in. each. Check that they are exactly rectangular and of correct and identical measurement-the fit of the joints and consequently the strength of the cabinet depend on it. The top and bottom of each side must now be rebated to receive the top and bottom of the cabinet. On the unfaced side of the wood draw lines very slightly more than 3 in. from the edges and with a tenon saw cut carefully along the lines to a depth of three layers of ply, keeping the saw at right angles to the surface. If the constructor is not too confident with a tenon saw, it is a good idea to tack a strip of wood with a straight edge along the line of cut to act as a guide for the saw. With

Assembly

An exactly similar rebate must now be formed all round the four edges of the front of the cabinet, on the unfaced surface. Now assemble the front and two sides and measure the exact length of top and bottom required to fit into the rebates. Cut the top and bottom to this length and 71in. wide; no rebating is required.

The top, bottom and sides should now be assembled temporarily on a flat surface, front downwards, using three lin. panel pins, driven not more than half-way home at each corner. The rebated front should be a good push fit. Dismantle, apply a good resin glue to all mating surfaces and reassemble, driving the panel pins



right home. Glue alone is sufficient to secure the front. Place the cabinet front up with a weight on top to keep the front firmly in position till the glue is hard.

Polishing

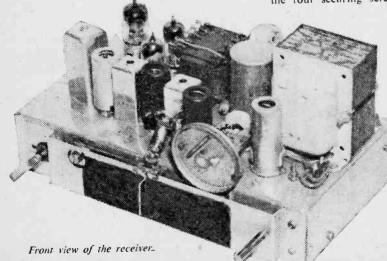
First punch in the panel pins till the heads are below the surface. A small wire nail with the point sawn off flat makes a good punch. Fill in the holes and any other blemishes with plastic wood of a suitable colour and when the filling is hard, give the whole cabinet a good rub down with No. 2 glass-paper, squaring off the corners and removing any old polish. Finish off with No. 0 glass-paper. The final result depends very largely on this preparation so make sure that no scratches or blemishes remain. Wood dye of the desired colour may now be rubbed in with a rag wad

There are three methods of obtaining the final finish. The first and best is french polish, which is also the quickest. There is no need to view this with alarm as there are plenty of french polishes to be had which are specially compounded for amateur use and nothing more is required of the operator than that he should follow the comparatively simple instructions enclosed with the polish.

Another Method

The second method is to apply three or four coats of clear varnish, rubbing down with No. 0 glass-paper between each. A period of 24 to 48 hours must be allowed for the hardening of each coat. Varnish does not darken the wood. It should be applied and allowed to dry in a dustfree atmosphere.

Another alternative is shellac, which is an ingredient of most french polishes. Dissolve an ounce or so of gum shellac in methylated spirits to produce a liquid about the consistency of paraffin and apply rapidly with a brush. Do not



Finally, a back should be made for the cabinet. This may be of \$in. plywood with suitable openings for connections and ventilation. To secure it, two \$\frac{1}{2}\$in. panel pins may be driven into the bottom edge so that they project \$in. The heads

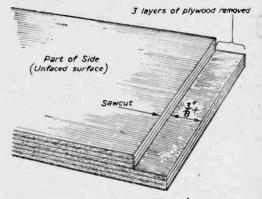


Fig. 9.-Forming the rebate.

can then be sharpened and pressed into the bottom of the cabinet. The top may be secured to small brackets or wood fillets fitted in the top corners of the cabinet.

Fitting the Receiver

Glue a piece of Tygan or other suitable material over the speaker aperture and cut a piece of thin plywood to shape and size to cover the aperture with $\frac{1}{2}$ in. to spare all round. In the plywood cut a 5in, diameter hole for the speaker in such a position that when fitted, the speaker will lie at the right-hand end of the aperture, looking from the rear, and three of the four securing screws will pass through the

ply into the front of the cabinet. Attach the speaker to the ply at the fourth securing point, using a 4B.A. countersunk bolt, and fit the assembly into the cabinet with wood screws of suitable length.

The tuning indicator should be fitted to a bracket in the top lefthand corner, looking from the rear, and the panel light similarly in the opposite corner, a piece of coloured plastic being fitted into the hole through which the lamp is viewed.

The receiver may be secured in the cabinet by means of four self-tap-(Continued on page 970)

An Inductance Measuring Instrument

A D.C. BIAS SUPPLY IS INCLUDED

I NTERSTAGE, and output transformers for use in transistor circuits are not difficult to make. The A.C. voltage applied across their primary winding is very much smaller than those used in valve circuits. and consequently the number of turns on the core is very much fewer than for a similar transformer used in valve circuits. If an output stage transistor is, say, working Class B from a 6V battery supply, the maximum collector voltage swing will be from 0 to -6 (see Fig. 1),

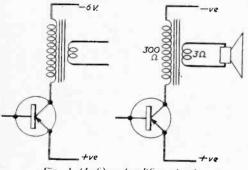


Fig. 1 (Left).—Amplifier circuit. Fig. 2 (Right).—Transformer matching.

a total of 6V peak swing. This would correspond to a signal output of 6×0.707 —a little over 4V r.m.s. In practice, an output stage would not work Class B single ended, but in push-pull, but this example does serve to show the low voltage swing in transistor applications compared with similar valve circuits where the anode voltage swing may be of the order of 200 or more.

There are two main considerations in the design of such an output transformer:---

(a) The correct matching of the transistor impedance to the, lower, loudspeaker impedance.

(b) The shunt impedance of the transformer windings must be sufficiently high in order not to shunt the lower frequency output signals past the speaker.

These two latter points require expanding.

(a) Impedance Matching (A.C. Conditions)

Consider an OC72 output transistor working, single ended, Class A, into a 3Ω speaker (Fig. 2). The equivalent circuit as far as the transistor

The equivalent circuit as far as the transistor is concerned is as shown in Fig. 3.

So, looking into the primary from the transistor. 300 Ω should be seen. However, looking into the secondary from the speaker 3 Ω should be seen.

This condition is achieved by impedance matching with a transformer of the correct turns ratio, which is given by By D. Saull

Turns ratio =

Load impedance Speaker impedance = $\sqrt{\left(\frac{300}{3}\right)} = \sqrt{\left(100\right)} = 10$

The primary must, therefore, have ten times more turns than the secondary, or, another way of putting it, the secondary winding requires ten times less turns than the primary. But, how many turns must the primary winding have in the first place? The answer to this question brings us to expansion (b).

(b) Shunt Inductance

An output transformer has a bandwidth, that is a range of frequencies which it will pass with

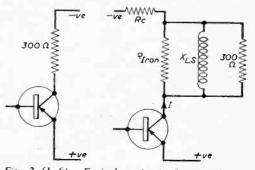


Fig. 3 (Left).—Equivalent circuit for transformer coupling. Fig. 4 (Right).—Simplified equivalent circuit for transformer loading.

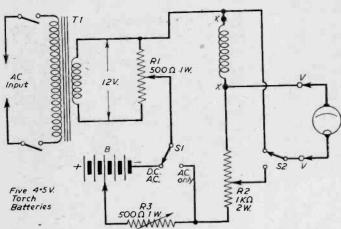


Fig. 5.-Complete circuit of the instrument.

equal attenuation. A moderate general purpose amplifier with single speaker will have a frequency range of approximately 100c/s-4kc/s.

The frequency response falls off at the higher end owing to leakage inductance and capacity between windings. At the lower frequency end this frequency fall off is due to shunt inductance.

The leakage inductance may be reduced by ensuring tight coupling between the windings and the core.

The shunt inductance effect may be reduced by ensuring that the primary inductance is high as possible.

Consider the simplified equivalent circuit for a transformer (Fig. 4) in the OC72 output stage being considered.

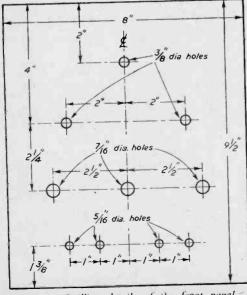


Fig. 6 .- Drilling details of the front panel.

The copper losses (D.C. refistance of the transformer windings); Rc. waste the signal output power (l^2/Rc). The resistance R_{IRON} (the iron losses in the transformer laminations) waste power also

The power delivered to the 3000 resistance represents the useful power that is delivered to the speaker.

XLS represents the shunt inductance, the current which by-passes the 3002 resistance and is not available for transfer to the speaker. This value requires to be kept as high as possible, and it will be noticed that XLS is lowest for the lower frequencies of the signal (i.e., XLS= 2π fL). In practice XLS should not be less than twice the load impedance. For the transformer we have been considering about 250mH (this

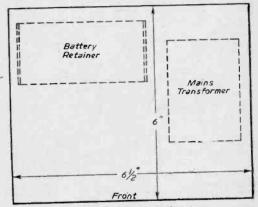


Fig. 7.-Chassis details.

gives about 6dB down at 100c/s).

It should be remembered that the inductance of an iron-cored winding may vary considerably with the A.C. applied voltage although it is nearly independent of frequency over the audio range.

Besides the A.C. component in the primary of a transformer, there may be a steady value of D.C. which will tend to lower the inductance of the winding.

Circuit of Inductance Measuring Instrument

Difficulties arise when measuring the impedance of iron cored windings on conventional inductance bridges, for the following reasons:—

(a) The A.C. applied voltage to the test component is usually unknown.

(b) There is usually no provision for any D_aC. component.

The circuit of the instrument (shown in Fig. 5) does measure reasonably accurately the reactance of iron-cored windings with a D.C. component flowing in the windings, up to 1k (3H) at 50mA D.C.

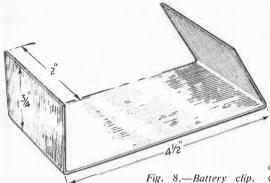
The circuit values may be amended if desired to cover other ranges.

The mains transformer T1 is a 12V filament transformer. Resistor R1 regulates the required A.C. voltage appearing across terminals X to

A.C. votage appearing across terminals x to which the unknown winding is connected. ' The battery "B" provides the D.C. component and is made up of five 4.5V torch batteries in series (22V). The 500 Ω resistor R3 is the fine control of the D.C. component, and should be kept at a low value, the coarse control of current being achieved by altering the battery tapping.

Switch S1 throws the measuring conditions from A.C. only to A.C. plus D.C. component. Resistor R2 is a 1k wire-wound potentiometer

which is calibrated in ohms against an ohmmeter. Switch S2 is used alternately in the measure-



ment of the A.C. voltage drop across R2 and the test winding. The voltmeter connected to the terminals "V" ideally should be a value voltmeter (an ordinary voltmeter may be used if of high resistance).

The accuracy of the instrument is dependent upon the calibration of R2.

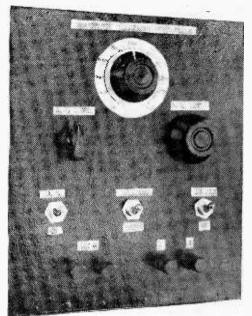
Use of the Instrument

The inductance required to be measured is connected to terminals "X"; SI is switched to A.C. plus D.C. position and the required battery tap selected to give the appropriate D.C. current. This value is measured by a current meter inserted in one of the battery leads.

The main switch is closed and with a value voltmeter connected to terminals "V." switch S2 is thrown from one position to the other and RI and R2 adjusted until the value voltmeter gives the same reading in both positions of switch S2, and the voltmeter reading is at the voltage at which the component under test will normally operate under circuit conditions. The reactance of the winding is then read off the calibrated scale on R2.

Practical Layout and Construction

> The material used for the panel and base was hardboard, the marking out being shown in Fig. 6. The base was secured to the panel by means of a strip of $\frac{1}{2}$ in. $\times \frac{1}{2}$ in. wood glued and pinned to the base.



The front panel.

The panel after cutting to size and drilling, etc., was painted black. A suitable hardboard case could be made to enclose the instrument and covered with an adhesive-backed plastic material.

Radio Trades Examination Board Fifteenth Annual Report

THE Council of Management has pleasure in presenting this report which covers the work of the board for the year ended 31st August. 1959.

The main object of the board, which is to promote technical courses in radio, television and electronic servicing, has met with considerable success-measured in terms of the number of candidates entering for the board's examinations. In 1959 a total of 2,310 candidates sat the radio and television servicing examinations and this represents an increase of 33 per cent. on the number of candidates sitting the same examinations in 1958.

Unfortunately, this larger number of candidates did not provide the same increase in the number of successes, and in fact, in the Radio Servicing Examination there was a drop in the number of candidates qualifying for a certificate.

The relatively poor results in the Radio Servicing Examination have, however, been the cause of much discussion.

The written papers were very much below the normal standard and we're the main cause of failure, and this inability to cope with theory undoubtedly resulted in many candidates failing the practical examination.

A Novel Circuit Technique

936

AN ALTERNATIVE TO PRINTED CIRCUITS

By J. D. Ingleby

TTH the coming of "Hi-Fi" and the transistor, the home constructor is finding that the only stage at which he can exercise his skill and experience is in the assembly of a given circuit. Whether for better or worse, the art of improvising one's own circuit and components is rapidly becoming outdated, and the focus is increasingly on a neat and compact circuit. The printed circuit is the answer to this trend, and indeed most transistor superhet kits use this technique. However, making one's own printed circuit is an expensive and elaborate



Another view of the transistorised amplifier.

This article describes a technique procedure. which retains the advantages of printed circuits, their economy of size and weight, strength and neatness.

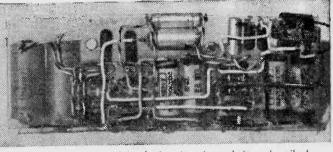
Circuit Materials

This circuit technique uses, in place of a printed circuit board, ordinary celluloid or trans-parent plastic sheeting. This is obtainable at reasonable prices from model shops, hardware stores, radio dealers, or motor-cycle repair shops. It has the advantage that wiring can be done with the components in view, and furthermore that the components can be inserted simply by pushing the bent wire ends through the sheet with the tip of a hot soldering iron. This method of fixing is quite rigid, as the celluloid sets hard round the inserted end.

Method of Assembly

The transparent sheeting may be of any kind, with the following limitation: it must be rigid enough to hold the components firmly, but thin enough to allow them to pass through easily, 1/32in celluloid or "Corbex" sheeting is ideal. Most dealers have conveniently-sized offcuts, but large sheets are more economical in the long run.

The next step is to work out the layout of components from the circuit diagram. In doing this a compromise must be made between comconvenience, for the most and pactness



A transistorised amplifier built using the technique described.

symmetrical layout is seldom the easiest to wire. However, one advantage of transistorised equipment is that the components have all a more or less equal size, and thus a neat design is often practicable. The layout should be worked out on a piece of paper, which can be slipped under the board during construction.

When the celluloid has been cut to the required shape, using scissors, the components are shaped for insertion. This is done with a small pair of pliers, taking care not to damage the components. Transistor leads should not be bent too close to

the seal, and resistors can crack if not handled carefully. Light pressure should be applied until the component sinks into the board: hold it in place until the celluloid sets firm. This may be done by using the plan as a guide underneath the board. It may be necessary to heat-shunt transistor

er. leads with pliers or a crocodile clip. but with experience only a moment's heat be either glued or bolted on. When all the com-ponents have been fixed on, turn the board over and trim all wire ends down to about 1/16in. long.

(Continued on page 948)

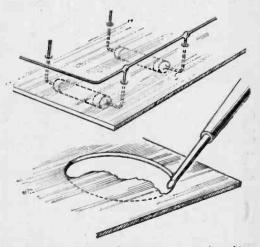


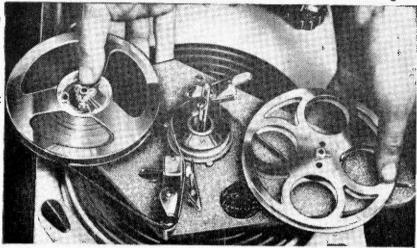
Fig. 1.-Method of fixing resistors and making holes in the plastic sheeting.

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TURNS

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Personal Callers Welcome



ANY of my friends who are radio amateurs construct items of radio gear in their spare time. The majority, to ensure domestic harmony, perform their operations in a shed outside the house. in a cellar or in a spare room. Most of the sheds and cellars used are damp and cold and although much of the apparatus built is for use on the domestic mains supply, few constructors appreciate the dangers encountered when working in such surroundings. Now the pundits among my readers will say that the remedy for this state of affairs is simple; all exposed metalwork including the chassis under construction should be earthed and 3-pin plugs should be used with all gear. This procedure is not easy to carry out, however, and if the earth wiring is not perfect, dangers may be created, as well as removed.

Some amateurs do not appreciate that there is a danger of shock when working in damp surroundings with apparatus connected to the domestic mains. One side of the mains (the neutral) is earthed at the source of supply and the other side is therefore at a potential of some 200-250V above earth. Thus, if it is possible during the constructional work to touch the live side of the mains and at the same time to make contact with the earth, either directly or indirectly. an electric shock will be experienced. The severity of the shock and its effects upon the recipient naturally depend upon the degree of electrical contact. Metal chassis can easily be electrical contact. Metal chassis can easily be connected by accident to the live side of the mains and would constitute a grave danger in workplaces such as sheds and cellars. However, if the chassis were earthed and inadvertently the live side of the mains made contact with it there would be, in effect. a short across the supply which would blow the fuses (always provided that the fuses had not been replaced with 18 gauge copper wire!).

If the constructor works in a room at, for instance, the top of the house where there are no earthed objects, it may not be necessary to earth the apparatus being used. In fact it may be an advantage to leave all chassis "floating"; when chassis are earthed the mains potential appears between the live mains lead and the chassis and it is all too easy to hold the chassis with one hand to steady it and touch live leads— H.T., mains, etc.—and receive a shock. My own practice as I do most of my constructional work In the topinost room of the house nowadays, is to leave all metalwork "floating." I have removed all earthed objects from the room; the floor is wooden and is covered in duck boards and I make a point of wearing rubber-soled shoes. There is no risk of shorting the H.T. when making wiring adjustments with a soldering tron while the apparatus is switched on: if the iron body and the chassis were earthed, contact between the iron and any part of the H.T. line would cause a partial or total short. No doubt this procedure of mine will be frowned upon by those who set themselves up as technical authorities, but as far as I can see there is less danger of shock with this system, if one can be quite sure that there are no earthed objects within reach of the test bench. Of course, the finished apparatus is fitted with a 3-wire mains lead and a 3-pin plug for safety.

The hazard of electric shock has come to be looked upon as something to ridicule. It is not. All electric shocks can be prevented if due attention is paid to the installation and the procedure employed. The commonest cause of workshop shocks is holding the chassis with one hand and touching a live point with the other, thus receiving a shock across the chest—one of the most dangerous paths for the current. The remedy is obvious.

A press notice from the Institution of Electrical Engineers was printed in the previous issue and I think it is worthwhile to reprint the most important parts of it which concern imported electrical apparatus and the dangers of misconnection.

"The attention of vendors and users of imported domestic electrical apparatus, photographic and projection equipment, tape recorders, etc., is urgently directed to the risks which may ensue if the colour coding of the cores of the flexible cord with which such apparatus is furnished differs from the established British coding set out in The Institute's Regulations for the Electrical Equipment of Buildings, that is to say:

Green-earth connection.

Red-phase (live) connection.

Black-neutral connection.

"The risk is most acute if the flexible cord provided with the apparatus has a core coloured red which serves as its earth connection; because if the user, following established British practice, connects this core to the terminal of a British connecting plug which may itself be marked red, and then inserts the plug into a normal British socket, the result will be that any exposed metal parts of the imported apparatus connected to the red core will be charged at mains voltage, and represent a serious hazard."

Measurements with Multirange meters

ACCURACIES TO BE EXPECTED

THE most common voltmeter used for normal circuit measurements is undoubtedly the moving coil type. There are many manufactured and home-made instruments in daily use. Unfortunately the operation of this type of movement draws current from the circuit under test. This may alter the true circuit conditions and give misleading results. A study of the effects which are caused is both interesting and instructive and may save time normally wasted in trying to interpret a seemingly impossible result.

The errors caused by connecting the voltmeter to the circuit depend mainly upon two facts.

(a) the resistance of the meter or the "ohms per volt" figure.

(b) the source impedance of the voltage at the circuit test points.

"Ohms per Volt" (Ω/V)

This term is used for calculating the resistance that the connection of the meter effectively places in parallel across the test points. Normally, the lower this value of resistance, the more severe the effect of connecting the meter becomes. Basically the moving coil voltmeter is a milliammeter, or microammeter, with an externally added, high value series resistor. The Ω/V figure is proportional to the value of the added resistor which in turn depends upon the sensitivity of current required for f.s.d. (full scale deflection) of the meter. The more sensitive the meter, the less the current required for f.s.d. and the higher the value of the added series resistor. The higher the value of the series resistor the higher the Ω/V figure. Thus the Ω/V figure is indirectly related to the sensitivity of the meter.

Practical examples will make this clear. supposing the basic meter movement has an f.s.d. of ImA and it is required to use the meter in conjunction with a series resistor to measure voltage up to 100, i.e., f.s.d. is to represent 100V. The value of series resistor is found to be 100V/ImA=100k. Or, in other words, when a 100k resistor is connected across 100V it will pass a current of ImA and with the meter connected in series with the resistor it will indicate ImA or if the scale is calibrated in volts, 100V. Now if the series resistor of value 100k is divided by the f.s.d. voltage of 100V we get 100k/100V= 1,000. This is the ohms per volt figure for the particular meter in the example. As stated above, this figure is governed by the basic current required for f.s.d. and is not altered by the value of D.C. voltage chosen for f.s.d. For example, supposing a value of 250V was chosen for f.s.d. Then the added value of series resistor required to limit the current to ImA is 250V/ ImA=250k. Dividing this value by the f.s.d. By B. Sexton

voltage of 250 gives 250k/250V=1,000. Thus the Ω/V figure is the same as that for an f.s.d. of 100V.

Meter Movement

It should be noted that when obtaining the value of series resistor in previous examples the inherent resistance of the basic meter movement has not been taken into consideration. The resistance is usually so small in comparison with the large value of series resistor that it may safely be disregarded unless the meter is to be used with an f.s.d. of a very low voltage.

Now consider a more sensitive meter movement, one which requires, say, only $50\mu A$ for f.s.d. or is 20 times more sensitive than one requiring lmA for f.s.d. To use this meter as a voltmeter with f.s.d. of 100V will require a series resistor of $100V/50\mu A=2M$. The Ω/V figure would then be 2M/100V=20,000. If the meter is used with an f.s.d. of 250V then calculations will give the

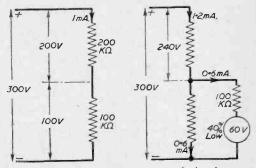


Fig. 1 (Left).—Simple circuit and calculated current and voltages. Fig. 2.—(Right).—The result of connecting a $1,000\Omega/V$ meter on the 100V range.

value of series resistor as 5M and the O.P.V. figure as 20,000. Thus, using a meter which is 20 times more sensitive has increased the Ω/V figure by 20.

Thus the higher the sensitivity of the meter the higher the Ω/V figure. The Ω/V figure of any movement can quickly be found by dividing 1V by the f.s.d. current of the basic meter movement. A meter of f.s.d. 1mA has an Ω/V figure of 1V/1mA=1,000 and a meter of f.s.d. $50\mu A$ has a Ω/V figure of $1V/50\mu A=20,000$. These figures agree with those found by the longer method in the previous examples.

Normally the Ω/V figure is stated on the instrument, but if not then simply divide by the lowest direct current range. This assumes, of course, that the lowest direct current range is the basic, unshunted, meter movement.

Readings

Fig. 1 illustrates a simple circuit consisting of two resistors in series across a 300V supply. The true, calculated circuit conditions of current and voltage are shown. It is desired to measure the voltage of 100V across the junction of the two resistors and H.T. negative. The separate use of two meters with different Ω/V figures will be considered and illustrates the errors introduced by meter connection to the circuit. It should be noted that two resistors are shown for simplicity. The bottom resistor could represent the static D.C. resistance of a valve and the top resistor the anode load. The 100V would then represent the anode voltage.

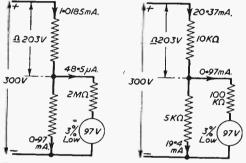


Fig. 3 (Left).—Result of using a meter of $20,000\Omega/V$. Fig. 4 (Right).—Effect of $1,000\Omega/V$ meter on accuracy when the source impedance is low.

The result of connecting a multi-range 1,000 Ω/V meter, switched to the 100V range, is shown in Fig. 2. The resistance of the voltmeter is represented by the series resistor and will be $100 \times 1,000 = 100$ k. Note that the meter movement resistance is considered so comparatively small that it is neglected. The meter will appear as a 100k resistor in parallel with the 100k circuit resistor giving a resultant value of 50k. The 300V supply now "sees" a 200k resistor in series with an effective value of 50k. The circuit conditions, calculated from Ohm's Law. will adjust accordingly and are as shown. The original voltage of 100V will now be measured as 60V; the reading error is 40 per cent. low. The meter is drawing 0.6mA and the fixed 100k resistor is passing 0.6mA. This total current of 1.2mA is flowing through the 200k resistor causing a drop of 240V across it. It is interesting to note that although the meter is drawing 0.6mA, the original current has increased by only 0.2mA. It is this extra 0.2mA flowing through the 200k resistor which increased the volts drop by 40 thus subsequently decreasing the voltage across the bottom resistor.

Increased (Ω/V)

q

Fig. 3 shows the result of using a meter with $_{J}$ a higher Ω/V figure of 20,000. On the 100V range the meter appears as a 2M resistor in parallel with the 100k circuit resistor giving a resultant value of 95.5k. Circuit conditions are as shown. The voltage can be calculated and now 97V will

be measured, i.e., the reading is now only 3 per cent. low. The meter draws only 48.5μ A, the 100k resistor passes 0.97mA and the total current is 1.0185mA or an increase of 18.5μ A. This increase in current is much less than the increase caused by the $1.000\Omega/V$ meter and consequently the voltage drop across the 200k resistor is increased by approximately 3. The calculated percentage errors show the superior accuracy obtainable with the higher Ω/V meter.

It must be emphasised that the errors obtained apply only to the circuit considered in Fig. 1. The impedance of the circuit at the test point also has an effect, as mentioned earlier; this effect will vary with different circuits.

Source Impedance

Consider the circuit shown in Fig. 4. Note that the resistors are now 10k and 5k. Before connecting the meter a calculation will show that the true voltage across the 5k resistor was 100V and the current 20mA. The meter connected is $1.000\Omega/V$ and switched to the 100V range. As in Fig. 2 the meter appears as a 100k resistor, but is now in parallel with a 5k resistor giving a resultant value of 4.76k. The circuit conditions adjust as shown, the voltage is now measured as 97. i.e., the error is 3 per cent. The current drawn by the meter is 0.97mA and that passed by the 5k resistor is 19.4mA. The total current of 20.37mA flows through the 10k resistor. The extra 0.37mA causes the increased voltage to drop across the 10k resistor.

Thus comparing the circuits of Fig. 2 and Fig. 4 it will be seen that in both cases a $1,000\Omega/V$ meter, switched to the 100V range, was used to measure a potential of 100V, but with widely differing results. This illustrates the importance of source impedance. When a voltage is being measured via a high resistance the current drawn by the meter can cause large errors owing to the voltage drop that this current produces. As the source impedance decreases, so does the voltage drop, and consequently the measurement becomes more accurate.

H.T. Battery

A practical example of this is the H.T. battery. A new battery, in perfect condition, has a low internal resistance and when measured with a low Ω/V meter will indicate correct voltage, but after use towards the end of its working life, the internal resistance will have increased and then there may be a marked difference between the measured voltage and the actual, no-load, voltage.

The higher the Ω/V figure of the meter the less important the effect of source impedance becomes. This point is illustrated by comparing Fig. 3 and Fig. 4. The voltage of Fig. 3 may be considered to have a high source impedance, but by using a meter of $20.000\Omega/V$. the accuracy is the same as that obtained in Fig. 4 where the voltage has a low source impedance, but is measured with a meter of only $1.000\Omega/V$. The accuracy could further be increased by using the $20.000\Omega/V$ meter to measure the low source impedance voltage of Fig. 4. 942

Thus the high Ω/V meter is far superior to the low \$1/V meter, but owing to the use of a more sensitive meter movement it is usually more expensive. By switching to a higher range, greater accuracy can be obtained with the low Ω/V meter although the reading of the scale becomes more difficult. Fig. 5 shows how the original circuit conditions of Fig. 2 would change if the meter is merely switched to a higher range. Assuming the meter has a 1,000V range it will then appear as a 1M resistor which, in parallel with the fixed 100k, gives a resultant of 91k. Note that the original current has increased by only 0.034mA. This increases the voltage drop across the 200k resistor to approximately 206. Thus the meter will indicate 94V. The reading rnus the filter will indicate 94V. The reaching error is then only 6 per cent. Compared to the original error of 40 per cent., this is a large increase in accuracy and illustrates the fact that it is always best to make a voltage reading on the highest convenient range. It must be realised, of course, that to read 94V accurately on a 1.000V scale may present difficulty. The number of divisions on the scale will be governed by the width of the scale and probably each division will represent 10V on the 1,000V range. Thus accurate interpolation is required. Whilst this becomes easier with experience it is obviously not so accurate as reading on the 100V scale where each division would then represent IV.

This change in voltage reading when changing meter ranges of a low Ω/V meter can be used as an indication of the source impedance at the test point. If the reading changes drastically when the meter range is switched then a high source impedance is evident and obviously affecting the accuracy of the readings. If the meter reading changes only slightly with range switching, then the source impedance is low and readings are then much more reliable.

Measurement Methods

It is possible to read the voltage of Fig. 1 without causing any effect on the circuit conditions as no current is drawn from the circuit under test. Fig. 6 illustrates the method. Two meters and a potentionneter are required. The potentiometer is connected in parallel with the two original resistors. Note that connecting the potentiometer across the original 300V supply may cause the 300V supply to decrease slightly due to the extra load. This effect has, for simplicity, been ignored. If in practice it could not be ignored, then a separate power supply for the potentiometer would be required. negative side of each supply would be joined. The voltage between the slider and H.T. negative Voltmeter is measured by the voltmeter VM2. VM1 is connected between the slider of the VM1 is connected between the slider of the potentiometer and the junction of the two resistors. The position of the slider is varied until VM1 reads 0V. The voltage at the junction of the two resistors is then given by the reading of VM2, this will be the true voltage of 100. Although VM2 will be drawing current it will all pass through the added potentiometer circuit and not through the

original circuit. It should be noted that VM2 is not reading the true voltage at the slider of the potentiometer, i.e., if VM2 was removed the true voltage at the slider would be higher than 100V. This is of no consequence as all we are interested in is obtaining a voltage which we can read easily that will be the same voltage as that at the junction of the two resistors. That it is the same is shown by the fact that the voltmeter VM1 indicates OV thus proving that the two points are at the same potential.

The accuracy of reading then depends only on the calibration accuracy of VM2. This method, of course, can be applied to the measurement of almost any high impedance point where meter current would give a false impression of the true reading.

Changes

Another difficulty sometimes encountered is the measurement of the change in a high potential. An example of this would be the change in output voltage of a power pack between no load and load conditions. With good regulation the change may be very small and consequently difficult to read on the high voltage range of the meter. Assume a practical example of a power pack which has a no load output voltage of 300. When a certain load is connected the output voltage may drop to say 299. If the output voltage was measured on the 1.000V meter range this change of 1V would be difficult to discern

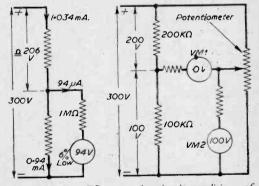
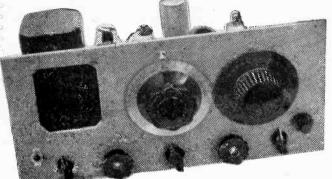


Fig. 5 (Left).—Effect on the circuit conditions of Fig. 2 when the meter is switched to a higher range. Fig. 6 (Right).—Making the measurement without drawing any current.

and practically impossible to read to any real degree of accuracy.

Fig. 7 (page 984) shows a simple but accurate method. The 300V no load output can be switched on load as shown. A second H.T. supply and resistor network are required. The voltage of this second H.T. supply must be within a volt or two of 300. The resistance of the potentiometer should be low, so that only a few volts are developed across it. Between the slider of this potentiometer and the original 300V supply is connected a voltmeter, the full scale reading of which is only a few volts. In the diagram 0-2.5V is shown. Note that the negative sides of the voltage supplies are common. Now by (Continued on page 984) An Experimental S.W.



THE number of turns in the coils used in this receiver were given in the previous article. The detector coils are shown in Fig. 4. In each case the primaries can be wound with 26 to 30s.w.g. wire, with turns side by side, about 4in. space being left between this winding and the earthed end of the tuned section, as in Fig. 4.

In the diagrams "G" indicates the grid end of the tuning coil, "C" the cathode tap, and "E" the chassis or earth connection. "A" is the R.F. anode connection, and "H.T." the high tension line lead. The circuit will work well with no R.F. stage, "A" then being taken to the 50pF aerial condenser, and "H.T." to chassis.

Aerial Coils

These can be wound, or be ready-made S.W. coils. Using 4in. diameter formers, seven and a-half turns of 20s.w.g. wire, spaced to occupy 1in, winding length on the former, will do for 10 to 20m. For 18 to 30m 20 turns of 24s.w.g. will be satisfactory, with 30 turns of 26s.w.g. for 30 to 60m, and 50 turns of 30s.w.g. for 60 to 100m. The three larger coils are fitted with dust cores, and the tuning range can be adjusted with these to match the appropriate plug-in coils in the detector stage.

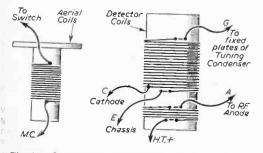


Fig. 4.—Construction of the aerial and detector coils.

Three

943

OPERATING THE RECEIVER

By F. G. Rayer

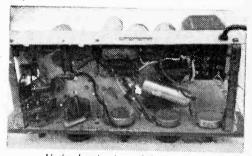
(Continued from page 858 of the February issue)

For single band tuning, the aerial coil can be wound to match the detector coil. Leads should be short and direct in both tuned circuits.

Switch connections are shown in Fig. 5. In one position, the 470k resistor is in circuit from valve grid to chassis, and the 150pF tuning condenser is disconnected. The other four switch positions bring in the tuning condenser and one coil.

Operating the Set

Though distant reception is easily possible with a poor indoor aerial, an outdoor aerial will improve results. The aerial circuit switch is normally left at the untuned position. The detector regeneration control should be so operated that the valve is just on the point of oscillation. This position is easily found as increasing

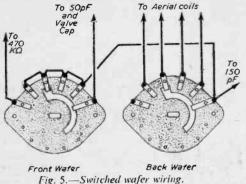


Underchassis view of the receiver.

the screen grid voltage with this control will build up volume until the set oscillates when tuned through a station. The control knob should then be turned slightly back. With weak signals the correct setting of this control becomes very important.

Tuning is normally carried out with the 15pF condenser. The 100pF condenser can be moved 10degrees at a time, this breaking up each waveband into many smaller bands, each of which is covered with the 15pF condenser, with some overlap. Provided the 100pF condenser is set accurately, as described, it will be quite easy to find any particular station logged against the 15pF condenser dial. When necessary, an aerial coil can be switched in, and it is then quite easy to find the correct tuning position for the 150pF condenser. Selectivity in this circuit can be increased, when needed, by turning the 50pF aerial condenser to a low capacity. The R.F. gain control can best be set at about three-quarters full gain, but this can be adjusted as circumstances require.

Amateur stations will be heard on the 10, 15, 20, 40 and 80m bands, USA and other non-local

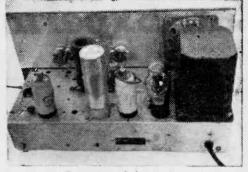


D.C.2. STEREO AMPLIFIER

(Continued from page 930)

the free tag of the next tag strip. Run two wires from this tag—securing the 10W resistor to it at the same time—one to the tag of the $32 + 32\mu$ F 450V with the 3.3k wire wound on it, and the other to the two tags on the output transformers that are situated second in from the rear of the chassis, then solder. We now have three of the four tags of the output transformers soldered. Between the remaining one and the last ones soldered, solder a 0.01μ F 400VW paper capacitor, and join the same tag—free before the fixing of the 0.01μ F—to pin 6 of the nearest ECL82. This should now leave both EC1.82 valves with pin 1 free and a tag on each of the two left-hand (power unit end) jacks free.

We can now fix the volume control, tone control and the stereo/mono switch in position. With the chassis still inverted, the left-hand socket is for the volume control-a twin bank 250 + 250k log. The centre hole is for a similar type, but is 1M + 1M. The other control is the stereo/ mono control, and is made by Kendall and Mousley Ltd. It is a single-pole two-position switch. The actual wiring of the tone and volume control circuit is shown in Fig. 4. Note that the wires from the input jacks are in screened twin cable and that the braiding is joined at one end to the common earth at the rear of the chassis. and at the other end to the various cases of the pots (four points) to two tags on the volume control, and also the two tone control capacitors are joined to the cases of the tone control pot. The colour of the wires in the screened twin is important, as if they are reversed the channels will be reversed in the amplifier.



Rear view of the receiver.

stations coming in best on 10, 15 and 20m bands. Long distance reception of commercial broadcast stations will often be best on 19 and 25m bands, until evening, when 31 and 41m bands will often give very good reception of African. American, and Far East stations. Conditions vary according to the season and time of day, but very many transmissions are made in English, from localities all over the world, and it will generally be reasonably easy to log a number of these.

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T is essential that when soldering or making good any dry or loose connections, that the

heat applied is carefully controlled, the reason being that excessive heat will result in the base material blistering, thus causing the metallic conductors to lift from it. Such base materials comprise phenolic impregnated papers, epoxy impregrated fabrics, or woven glass cloth treated with silicones or epoxy resins. The use of any particular base material depends mainly upon its final use, an important factor being the maximum working temperature.

As in the conventional type of radio circuit dry joints will result in poor electrical connections, not forgetting any break in the metallic conductor. Such breaks, however, in the printed circuit, may be only a very small crack, resulting in intermittent operation. Such faults can best be traced by continuity checks, but in doing so it is advisable to bend the printed circuit to assist in tracing the break or dry joint in the conductor.

It is as well to mention, however, that when soldering new connections, or making good any dry joints, it is necessary to ensure that no splashes of surplus solder short-circuit the metallic conductors or components, bearing in mind that with this type of circuit miniature components are used.

The insulation resistance between the conductors is usually fairly high, something in the order of 50,000M, but this value will be greatly reduced if the printed circuit is allowed to become damp, oily or dirty. Any dust collecting between the conductors will eventually result in tracking or electrical leakage.

944

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A 6K7 Superhet

ALIGNMENT OF THE RECEIVER

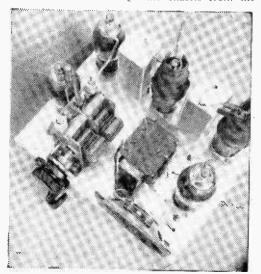
By J. Heath

(Continued from page 837 of the February issue)

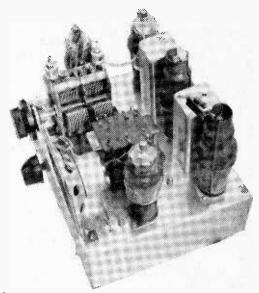
WHEN wiring up the I.F. transformers, note that leads or tags are often marked according to the points to which they are normally connected. If so, then "anode" and "H.T. positive" leads will be the primary, with both transformers, and they are connected to anodes and H.T. positive line. With the first transformer, the bottom secondary lead or tag will often be marked "A.V.C." and this is taken to chassis, as in Fig. 3. With the second transformer, this lead is often marked "diode load" and it is also taken to chassis, as shown.

Coils

Aerial and oscillator coils are fitted to a small piece of aluminium, as with some types the core adjusting screws are otherwise inconveniently situated under the gang condenser. Coil tags are numbered in, Figs. 1, 3 and 4. With the aerial coil, tag 3 is wired to the rear fixed plates of the gang condenser, marked "Y" in Fig. 2. A lead also passes down through the chassis from the



Plan view of the seceiver.



front plates "X" to tag 7 of the oscillator coil. The tag connections shown in Fig. 4 are for the coils given in the components list (Astral Radio Products). The aerial and oscillator coils produced by other manufacturers will be equally satisfactory, but the maker's tag data must then be followed, as connections will not be the same as those in Fig. 4. The padder indicated in Fig. 1. must also be of the value specified by the coil maker. If long waves are also provided, a separate padder will be, needed with the long wave oscillator coil, and will often be 150pF. Correct ganging of the tuned circuits will be impossible if the padder is omitted, or of the wrong capacity.

A tag board with two tags joined is used for H.T. positive connections, as in Fig. 3. A second small tag strip provides an aerial connection, the 500 pF condenser and 10k resistor forming 'a modulation hum filter. Trouble from modulation hum is unlikely, but in localities where this is severe, a 0.05μ F 750V condenser can be wired in parallel with the primary of the mains transformer. The 500pF aerial condenser must also be of good make, and 500V or 750V rating, as it prevents mains voltages reaching the aerial.

Using and Adjusting the Set

If clear glass valves with no external or internal screening are fitted in the mixer and I.F. positions, instability is likely when the I.F. transformers are correctly aligned, and when the volume control is turned towards maximum. Valves of this kind should thus be provided with screening cans, of ready-made type, or bent up from aluminium. The cans are connected to the chassis.

Alignment is carried out as with a standard superhet. If a signal generator is available, set this to give a 465kc/s modulated output, and place the output lead near the anode connection of the mixer. The LF, transformer cores are then adjusted for maximum response. The aerial and oscillator trimming condensers are then adjusted for best volume with a signal around 230m, and the cores are adjusted for best volume with a signal of about 500m.

Another Method

If no generator is available, it should be possible to tune in the local station. The I.F. transformers can then be adjusted for best volume, taking care that no core is at the limit of its travel. A station of fairly low wavelength is

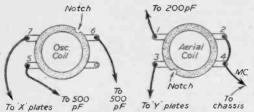


Fig. 4.-Aerial and oscillator coils.

then tuned in, and the gang condenser trimmers are adjusted for best results. The set is then tuned to a station of fairly high wavelength, and the coil cores are adjusted.

The procedure should be repeated two or three times, until no further improvement is possible. An insulated blade is most suitable, because the presence of a metal blade in the coil or trans-

former windings will upset adjustments. A baffle board or cabinet is required if the loudspeaker is to give best reproduction. cabinet is recommended, and can easily be made from in. thick or similar wood, with a 3-ply front. An aperture to match the speaker cone should be cut in the front, and covered with silk or speaker gauze. A clearance hole for the com-

A NOVEL CIRCUIT TECHNIQUE

(Continued from page 936)

Wiring

Do not use thick or multi-strand wire for wiring up the circuit. A diagram is often helpful, though most transistor circuits are relatively A fixed order should be straightforward. followed, starting, for example, with earth points, negative points, etc. Although transistor circuits are generally free from stray wire pick-up troubles, wires should be quite short.

Fig. 1 shows how to connect up the wire ends Time spent on good underneath the board. soldering pays dividends later on !

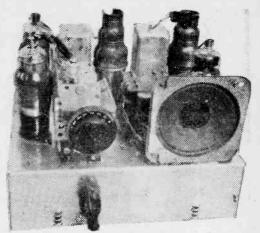
Installation

The completed circuit can be glued or bolted into place. Avoid looseness in equipment like car radios, which must be firmly constructed.

Removal of components for replacement is effected by melting the joint and levering out the loosened part.

Other Applications

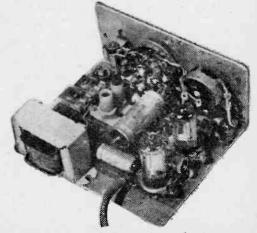
Of course, transistor circuits are not the only application of this technique: many valve circuits can be constructed using celluloid sheeting, though large components often need to be more



Front view of the receiver.

bined switch and volume control, and an opening to suit the dial used, are also required. The completed receiver can then be placed in the cabinet from behind. If a back, with rows of holes for ventilation, is screwed on, this will protect the receiver and prevent chassis or other parts being touched, and thereby avoid the chance of mains shocks from this cause. For the same reason there should be no exposed metal, such as the volume control bush or spindle, or knob grub screws, which might be touched. This can be arranged by using a knob which covers the bush and nut, and having the grub screw well recessed. or filling the grub screw hole with an insulating compound such as sealing wax. Similar precautions should be taken with the tuning control.

firmly secured. However, celluloid is an obvious replacement for tag boards, for components can be arranged as required, and the board bolted where it is most convenient. Fig. 1 shows how to cut out large holes for valveholders, which are then bolted on in the usual way.



A receiver built on plastic sheeting.

948



A DEVICE FOR CHECKING FREQUENCIES By G. Tomassett

HIS instrument, with its somewhat presumptuous name, is intended to facilitate frequency measurements. The accuracy obtainable, even at 200Mc/s, is of the order of ± 5 c/s or so. These figures are relative. Explicitly, you can evaluate an unknown frequency with the mentioned accuracy relative to your R.F. signal generator.

Uses

The Magic Needle is operated in conjunction with a reliable R.F. generator. A sensitive A.F. amplifier may, sometimes, be dispensed with. Obviously, if you work on a tape recorder, you should not need a sensitive external audio amplifier. The same applies if you are dealing with a radio or TV set. The use of an external separate amplifier does, however, simplify things. particularly for the beginner.

The instrument has been successfully used for:---(a) Radio sets, when, because of a defective component or because of a serious misalignment, the frequency has departed from its correct value. Its use has been of invaluable help with faulty transistor sets.

(b) TV sets. particularly in instances of channel changes. In these cases, the instrument is really indispensable. The line frequency can be measured utilising the harmonics produced in the output stage.

(c) Tape recorders to determine the erase frequency which can be of some significance. In this connection, owing to the relatively low frequency, the harmonics must be used. In one instance, where the frequency was 60kc/s, the 15th harmonic still gave an audible signal. (Zero beats were found in this succession: 600, 660, 720, 780, 840kc/s.)

(d) Experimental oscillators of any kind.

Operating the Test Gear

This is the sequence of the operations to be carried out in order to determine the value of an unknown frequency:

Coil "C"

(a) Connect cable Y to input of A.F. amplifier and cable X to output of R.F. generator.

(b) Switch on all components, Allow five minutes or more for warming up.

(c) Set R.F. generator to maximum output and internal modulation to "off."

(d) Set A.F. amplifier to full volume.

(e) Pick up the needle, holding it where the cables are clamped together and, as a first attempt, put the tip of the needle as near as possible to the coil of the oscillator under test. Often, however, this proximity is not necessary; it can some-times be detrimental, especially when high accuracy is required.

(f) Move the generator, operating both range and dial until the typical approximation of the zero beat is heard. If the sound produced is very loud, reduce the coupling by drawing the tip of the needle away from the circuit. When zero beat is obtained, the frequency sought will be within the region of $\pm 5c/s$ compared with the frequency recorded by the R.F. generator. It must be realised that both the R.F. oscillator

under test and the R.F. generator produce harmonics which might be misleading. As a rule, when more than one zero beat is heard. the loudest will be the right one (the one to be taken into account).

The Circuit

The R.F. current set up in Rg (internal resis-tance of generator) will flow through coil "C," diode D1 which rectifies it and, finally, return to

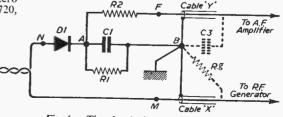
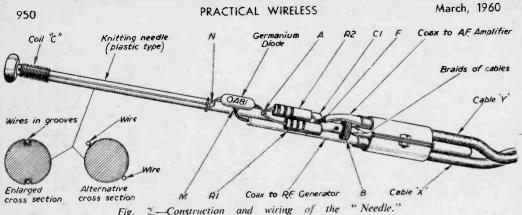
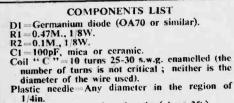


Fig. 1.-The circuit diagram.



2.-Construction and Fig

Rg passing through the R1-C1 group. If any audible signal were superimposed on this current, the audible part would be taken from point A by R2, filtered by C3 (which is not physically present) and, finally, amplified by the A.F. amplifier. Obviously, if the R.F. generator is not internally modulated, nothing will be heard at the amplify-ing end. When, however, the tip coil "C" is



Coax cables = Two short lengths (about 2ft.).

immersed in an electromagnetic field, an induced current will circulate in it. Through the rectification process of D1, the two currents (the induced one and the one delivered by the generator) are mixed so that at point A there will appear as many as four currents of the following frequencies:

(1) (fg)=frequency of generator; (2) (fx)= value of unknown frequency; (3) (fg + fx); (4) (fg $-f\mathbf{x}$).

As (fx) is likely to be a radio frequency (not audible) and as (fg) is definitely a radio frequency, it is clear that only the term (fg-fx) can give an audible frequency. Further, from (4), if (fx) equals (fg) the result of the subtraction will he zero or zero beat which is, in fact, the principle upon which this instrument works. The aim, then, is to find a frequency in the range of the R.F. generator which, because of its being equal to (fx), gives a zero beat through the Magic Needle.

The "difference" current of frequency (fg-fx) or (fx-fg), feeds the audio amplifier and is carried there by means of the low-pass filter R2-C3 (C3 is not physically present but represents stray capacitances). The low-pass filter will convey to earth the other three components, namely (fg), (fx), (fg+fx). The incoming R.F. signal and the outgoing audio signal are both carried by coax cables not longer than about 2ft.

Assembly of the Parts

All the components are attached to the needle through small holes (see Fig. 2). The distance in between the holes is not given because it is dependent upon and varies according to the length of the components used. Some five holes are needed and two extra ones are advisable to fix the ends of coil "C," thus preventing turns from slipping.

The wire used for the coil is also used for its connection to the rest of the circuit. In order to carry the two terminal wires of the coil to the components, it would be advisable to make two grooves along the needle (see cross section).

The coax cables are clamped together around the end of the needle by means of a bracket or simply by adhesive tape.

Transistorised Mixer Unit

IN the article by A. M. Shafford which appeared on page 765 of the January issue no definite details were given of the type of microphone for which the mixer is suited. The author assumed that it would normally be used with the crystal microphones supplied with popular tape recorders, that is, high impedance types. The method of gain control employed has given rise to a certain amount of criticism, but although it is not ideal, it is the simplest which can be achieved when only one transistor stage is employed and in practice gives very satisfactory results. The low amplification of the mixer makes it unnecessary to control gain after amplification; no significant improvement in signal-tonoise ratio would be achieved and a separate transistor amplifier would be needed in each channel before mixing. This procedure would complicate the design of the pre-amplifier which was aimed at simplicity and low power consumption.

The value of 10µF for the output coupling condenser may seem rather high, but it ensures that the unit is suitable for coupling into all valve amplifiers and as in the writer's case a fully transistorised amplifier. There is no point in choosing (say) a 0.01µF coupling condenser unless the unit is always to be used with amplifiers having high input impedances.

Versatile V.F.O.

FURTHER CONSTRUCTIONAL DETAILS

(Continued from page 844 of the February issue)

By R. H. Wright

THE original V.F.O. unit was constructed on au 8in. \times 8in. \times 2 \pm in. chassis. not because such a size was necessary, but rather because such a size was at hand. Actually, the whole unit, including the buffer valve, could be con-

March, 1960

I.

structed easily on a 4in. \times 8in. chassis, Eddystone have a chassis measuring 8½in. \times 5¼in \times 2½in. and this is designed to

fit inside their type No. 644 metal cabinet. Use of this cabinet would give a very professional finish to the unit. Paxolin group panels can be used with

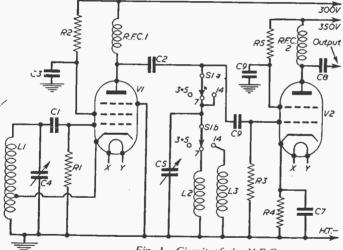


Fig. 1-Circuit of the V.F.O.

definite advantage for the mounting of many of the individual capacitors and resistors and apart from making construction actually easier (since much inter-component wiring can be carried out on the panel itself) neaten the final unit and does away with the "spiders' web" of resistors and capacitors radiating out from each valveholder.

Operation of the V.F.O.

The writer has found that, generally speaking. it is bad policy to key the V.F.O. together with the main transmitter and such action makes a chirpy note very hard to eliminate. A better method is to fit a switch in the cathode line of the oscillator valve so that the oscillator can be switched on without operation of the full transmitter. This permits the oscillator to be adjusted to the required frequency without radiating a full Front view.

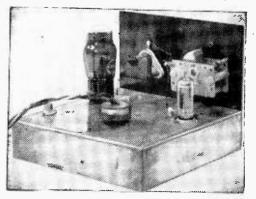
signal and so causing interference. When the key is finally pressed it is only a moment's operation to make any final adjustment to the transmitter

tuning before commencing a call. If the full transmitter circuit suggested in the first section of the article has been built up, incorporating the V.F.O. and amplifier sections (Figs. 1 and 3) the following tuning procedure should be followed.

(i) Set the V.F.O. to the required frequency and tune the grid circuit of the buffer (C5/L2 or L3) to the second or fourth harmonic of 3.5 Mc/s if final output is required on 7 or 14Mc/s. Correct tuning of this circuit would produce maximum grid current in the final amplifier circuit.

(ii) With the key pressed and the V.F.O. in operation, set C5 of the amplifier section to full capacitance value and, with the correct coil in the L1 (amplifier) position,

(Continued on page 957)



Rear view.

March, 1960

A THREE-VALVE CIRCUIT WITH TREBLE, BASS, VOLUME AND FILTER CONTROLS

By R. Taylor

N ideal pre-amplifier may be stated to fulfil the following requirements : (a) to accept an electrical input from a gramophone pick-up, radio or other similar source; (b) to correct this input for amplitude and frequency, and (c) to supply a suitably amplified voltage to the main amplifier.

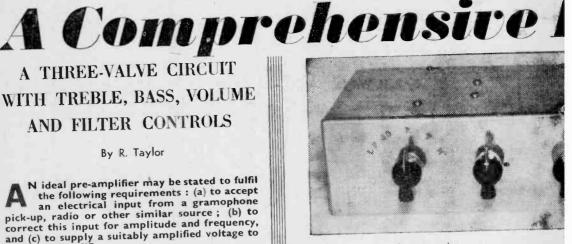
The main audio amplifier usually supplies low impedance loudspeaker. Very few loudspeakers have an entirely satisfactory frequency response. and dimensions, shape and furnishing of a room may again influence and colour the sound issuing from the loudspeaker. It is thus often possible to improve the overall result by the judicious use of variable tone (or frequency) correcting networks which are most conveniently situated in the pre-amplifier.

The pre-amplifier about to be described is designed to fulfil as many of the essentials tabulated above as possible, while retaining the advantage of compactness and reliability.

Specification

952

Three coaxial inputs are shown in the theoretical diagram (Fig. 1) for gramophone pick-up, radio and tape, but constructors not possessing a tape recorder may choose to omit the third. It must be stressed that this pre-amplifier does not contain correction networks to enable direct replay



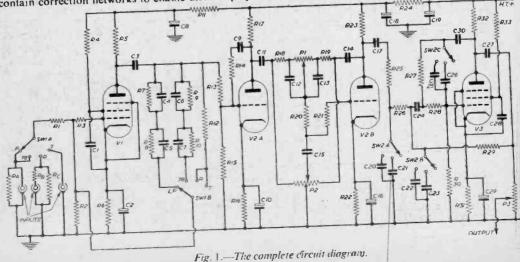
The front panel.

from the tape deck playback head, and the input should be taken from a signal source after the frequency correction stage of the tape recorder pre-amp.

The inputs are taken via a selector switch to the grid of the first valve (6BR7) for voltage amplification. The load resistance R_A of the pick-up input as shown in Fig. 1 will only be suitable for a magnetic type of pick-up, with an output of less than 50mV, such as the Goldring 500/600 cartridges, etc. For magnetic types of pickup with greater output, or crystal types, alternative input networks are recommended (Fig. 2).

Equalisation

A negative feedback resistance/capacity network in the anode/grid circuit of the first stage provides the necessary frequency correction for most L.P.





and 78rev/min recordings, while a resistance negative feedback circuit in combination with the potential divider Rb and Rc, attenuates the radio tuner signal sufficiently to avoid overloading the first valve stage.

The second stage (12AX7) incorporates a well known variable tone control circuit with independent cut and boost in both treble and bass frequencies, as referred to a frequency of 1kc/s.

This stage feeds into the final stage (6BR7) which includes both high- and low-pass filters. The high-pass, or "rumble," filter is useful for attenuating the irritating low frequency rumble associated with so many turntables, and has a cut-

off frequency of about 35c/s with a slope greater than 12dB/octave, and is permanently in circuit. The low-pass filter can be switched from level response to frequency cuts at 7.5kc/s or 5kc/s with a slope approaching 18dB/octave.

Construction

The chassis is formed from a sheet of aluminium, preferably of 3/32in. thickness, to make a box 12in. $\times 5in$. $\times 2\frac{1}{2}in$. Apart from the input power supply junction box and coaxial sockets mounted on the rear of the chassis, the only projections are the controls on the front. As the valves run very cool, they are mounted with all the other components within the chassis, which makes a very neat, yet efficient unit.

To make construction easy, most of the resistors and capacitors are soldered on to group boards and tag strips, which can be assembled outside the chassis, with lengths of wire for connections

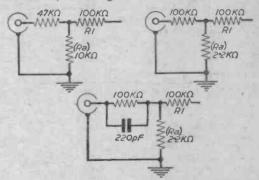
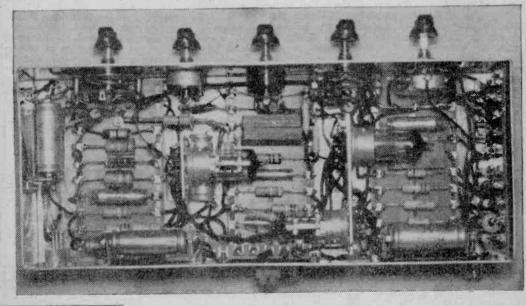


Fig. 2 .--- Alternative pick-up input circuits.



This view shows the compact layout employed

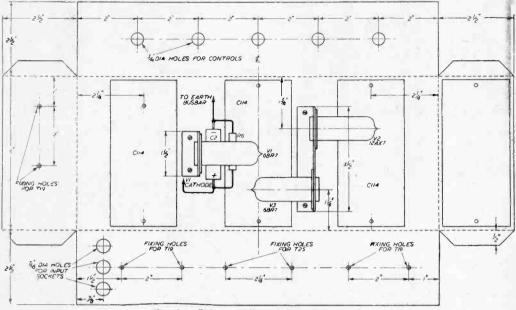


Fig. 3.-Chassis drilling details and layout.

to other units attached, before bolting into position.

Only one earthing point to chassis is used, and all connections to earth in the circuitry are made to this one point, via a heavy gauge copper busbar, the farthest end of which is insulated from chassis by connecting it to a spare terminal on a group board.

Chassis

The plan of the chassis, and approximate disposition of group boards, tag strips, etc., is shown in Fig. 3. The valveholder brackets should be made of aluminium of similar gauge to the chassis, with a $\frac{1}{2}$ in. to $\frac{1}{2}$ in. width right angle to bolt to the chassis. The valve sockets should be positioned to allow reasonable clearance between the valve and the components mounted on the group boards, and a distance of approximately I_s^{\pm} in. from the floor of the chassis to the valve centre line will be found suitable. The group boards are raised slightly from the chassis by a spacer nut, which enables the passage of insulated wiring between board and chassis, thus making a neater appearance.

It is suggested that the assembly and wiring of the pre-amplifier be undertaken very carefully to minimise the possibility of any mistake. If care is taken in following the diagrams and instructions. no difficulty should be found. It should be noted, however, that the construction of such a compact unit demands care and patience, and the use of a pencil bit soldering iron is almost an essential. (To be continued)

	COMPONENTS	LIST
Resistors : R1 100k R13 100k R25 68k	C7 470pF ceramic C8 8 µF electrolytic 350VW	C27 0.02 µF paper 350VW C28 0.1 µF paper 350VW
R1 100K R15 100K R25 08K R2 2.2M R14 270k R26 68k R3 3.3k R15 470k R27 3.3M	C9 0 .01 µF 350VW	C29 25 / F electrolytic 25VW
R4 1.5M R16 2.7k R28 100k R5 220k R17 100k R29 390k	C11 0.05#F paper 350VW C12 4,700pF ceramic	Sundries :
R6 1.5k R18 100k R30 470k R7 470k R19 470k R31 560	C13 4,730pF ceramic C14 0.05 //F paper 350VW	SW1 2-pole, 4-way switch SW2 3-pole, 3-way switch
R86.8M R20 470k R32 100k R9 3.3M R21 1k R33 470k	C15 100pF ceramic C16 25 µF electrolytic 25VW	B9A valve bases Coaxial sockets P1 1M pot. (linear)
R10 3.3M R22 2.2k Ra R11 22k R23 100k Rb (see	C17 0.05 µF paper 350 VW C18 8 µF electrolytic 350VW	P1 Try pot. (tinear) P2 500k pot. (linear) with tap at 50% rotation
R12 330k R24 22k Rc text	C19 8 #F 350 C19 8 #F electrolytic 350VW	P3 250k pot. (log.) Group boards (Bulgin C114))
Capacitors : C1 0.1 #F paper 350VW	C20 680pF ceramic C21 470pF ceramic	Tag strips (Bulgin T19 and T25)
C2 25 µF electrolytic 25VW C3 0.05 µF paper 350VW	C22 1,500pF ceramic C23 1,000pF ceramic C24 4,700pF ceramic	Valves :
C4 220pF ceramic C5 830pF ceramic	C25 15pF ceramic	V1 6BR7 V2 12AX7
C6 50pF ceramic	C26 10pF ceramic	V36BR7

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PRACTICAL WIRELESS

for P

ADEQUATE OUTPUTS CAN BE OBTAINED FROM SIMPLE CIRCUITS

By J. Gray

TRANSISTOR amplifier can be used to work a loudspeaker for sports, outdoor events, and similar functions, and this type of equipment can be independent of the need for mains or accumulator supplies. It is not practicable to obtain volume equalling that of a large mains-operated public

address amplifier,

which may deliver

useful output can

nevertheless

In general, one of two purposes will be

in view. First, it may

be necessary to work loudspeaker situ-

ated some distance

from the microphone,

se that the person

using the latter can

be at the best obser-

vation point. Or it

may be necessary to obtain a good, easily

many

а

be obtained.

watts, but a

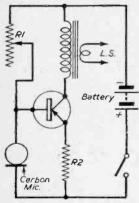


Fig. 1.-Directly coupled

audible signal without circuit. the person having to raise his voice. Transistor equipment will easily meet these needs, but ordinary transistor circuits will not give sufficient output for several loudspeakers, or very high volume coverage over a wide area.

Simple Circuit

A very simple circuit is shown in Fig. 1, using a microphone directly connected to a transistor. In this circuit, as in the others described later, a carbon microphone is essential to secure enough output. Various surplus microphone inserts and hand mikes may be used. Carbon microphones do not themselves produce any current, but present a varying resistance to a current obtained from a battery. When the switch is closed,

current flows through the microphone and R1. R1 and the microphone act as a voltage divider supplying the transistor base. To secure a satisfactory base voltage. R1 is thus best of variable type. It should be set to a fairly high resistance at first, this being reduced until best results are obtained.

Best output will be obtained with a microphone of low resistance, preferably not over 50ohms. A wire-wound resistor of some 250ohms can then be used for R1. If the microphone is of high resistance then R1 must be increased in value to suit. The total resistance of R1 and the microphone then becomes rather high, so that the current through the mike is small, and the signal obtained from it is much reduced. Enough output will not be obtained with a high resistance carbon microphone unit.

R2 limits current, and can be about 20hms for a power transistor such as the V30/20P. It is also wire-wound. A power transistor output transformer is essential, transformers intended for valve circuits being unsatisfactory. For the

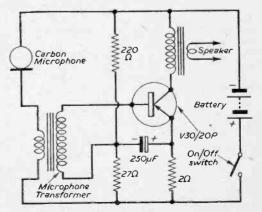


Fig. 2 --- Adding a coupling transformer.

V30/20P and a 30hm speaker, the transformer ratio should be about 3.2:1.

The battery voltage may be anything up to 12. Current is only drawn when the switch is closed. To save current, and let the transistor cool, a spring-loaded push switch may be used, and held down when announcements are being made. Dry batteries with large cells can be used, but for long periods of operation at best volume, an accumulator is recommended.

Transformer Coupling

The sensitivity of the circuit can be improved, especially with a microphone of fairly high resistance, by using an input transformer, as shown in Fig. 2. The base circuit of the transistor is completed through the secondary, and correct operating voltages can thus be maintained. Resistor values are for the transistor shown, but can be changed to suit other power transistors.

For maximum volume, the primary of the transformer should have about the same resistance as the microphone. If primary and mike are of rather dissimilar resistance, it will be found that no increase in volume is achieved. Best possible volume is obtained when both primary and microphone are of quite low resistance, so that a large microphone current passes through the primary. This is most easily assured by using one of the various "power" type microphone units. As with Fig. 1, any battery voltage

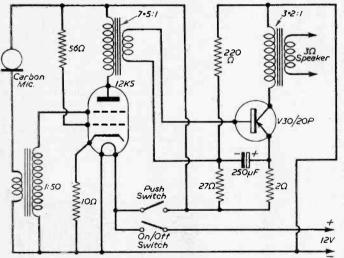


Fig. 3. - Circuit with valve pre-amplifier for 12V operation.

may be used, but a 12V supply from accumulator or large dry cells will be best.

A Value Pre-amplifier

A transistor requires power, in the form of current, to drive its base circuit. This means that a step-up transformer cannot be used from the microphone, because the transformer could only increase signal voltage at the expense of current. This difficulty does not arise with a valve, the grid of which requires an input voltage and negligible current. A valve pre-amplifier thus allows a high-ratio microphone step-up transformer to be used. This gives a very great increase in sensitivity, because the valve itself also provides more amplification.

A circuit of this kind is shown in Fig. 3, the valve being of a type intended for 12V heater and H.T. supply, so that only a 12V accumulator will be needed. Intermittent operation is, in fact, possible from a 12V dry battery made up of large cells.

Transformer Ratio

For best sensitivity, microphone transformer primary and mike should be of similar resistance, as explained. The ratio is not very important, 50:1 being average. A lower ratio may be needed with high resistance microphone units. Surplus microphone transformers of suitable type will do well, and will have a very high secondary resistance. Some speaker output transformers will function, with the low resistance winding used as primary.

The valve anode transformer is of the transistor coupling type, and this also applies to the output transformer. Both these transformers are wired so that the larger winding is primary, because a step-down ratio is necessary to match speaker to transistor, and transistor to valve. Wiring any of the transformers incorrectly will

result in little or no output at all.

A switch completes the valve heater circuit, so that the cathode can be maintained at operating temperature. Talking is then possible immediately the push switch is closed. With only one switch it would be necessary either to leave the microphone and transistor drawing current. or to wait for the valve to heat up.

Underchassis wiring for the circuit in Fig. 3 is shown in Fig. 4. The secondary of the output transformer goes to speaker. The exact layout of parts is of little importance, provided the transformers are some distance apart, and preferably with their cores at right angles, to avoid howling.

The 2200hm resistor is best of 1W rating. It can be made up by wiring two 4400hm $\frac{1}{2}W$ resistors in parallel, or two 1100hm $\frac{1}{2}W$ resistors in series. The low value

resistors are best wire-wound.

Transistor Mounting

When anything approaching maximum output is being obtained, the transistor will become hot. This heat must be conducted away. A metal plate, or the metal chassis, is thus used for this purpose. In Fig. 4, the transistor is bolted to the chassis, but is not in electrical contact with it. To obtain the required electrical insulation.

PRACTICAL WIRELESS

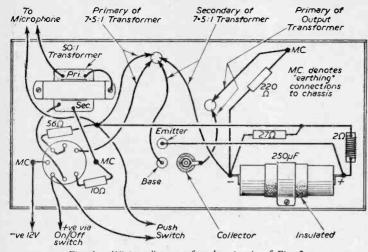


Fig. 4.-Wiring diagram for the circuit of Fig. 3.

while allowing heat to reach the chassis, the transistor makers provide a very thin mica washer. After drilling clearance holes for the transistor, burr or roughness must be carefully removed, so that the mica washer can lie flat on the chassis. The transistor is then bolted on, a paxolin or insulated washer being used to prevent contact between tag and chassis, on the underside. A "heat sink" can also be made by using a flat sheet of aluminium, of reasonably large size and stout gauge, if this is more convenient.

If an experimental circuit is made up, and a 12V supply used, an initial test with a meter is wise, to see that maximum ratings are not exceeded. This is not necessary when using specified values with the appropriate transistor. Some types of transistor are not intended for 12V, and this should be remembered.

VERSATILE V.F.O.

(Continued from page 951)

rotate C4 and watch for a dip in the meter connected in the cathode of the amplifier valve. C4 should be adjusted to the lowest current reading when a dip is registered on the meter.

(iii) Now decrease the capacitance of C5 (and as this is done the meter reading will rise again) and retune for the dip by means of further adjustment of C4. Repeat this operation—decreasing C5 and retuning C4 to the dip—until the dip occurs at about 45 to 50 milliamps of cathode current. The transmitter is now tuned. The V.F.O. may now be adjusted to any frequency in the band without any further transmitter tuning actually being necessary though if the V.F.O. frequency changes by any appreciable amount it may be found that slight retuning increases output. The correct method of setting C6/L2 was described in the first section of the article. This, ef course, can only be carried out in conjunction with a local TV receiver.

As mentioned previously, care must be taken to ensure that all sections of this transmitter, and, The size of the loudspeaket is of no importance, except that a reasonably large unit is best, because small speakers will give less output, and may not be able to handle the signal without overloading. In some instances the speaker may be mounted in the same case as the amplifier, or it may be more convenient to have the speaker in a separate box, or fixed to a baffle board hung at some suitable point.

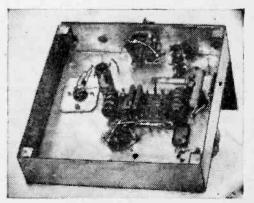
The layout of the various units (battery, microphone, amplifier, and speaker) is not of much importance, and depends on the purpose in view. With a small amplifier, as in Figs. 1 and 2, the mike, amplifier and speaker could be in a single case. Or

batteries and amplifier may occupy the case, with leads to microphone and speaker.

With the larger type of amplifier, such as that in Figs. 3 and 4, it is convenient to house the amplifier separately, so that microphone, speaker and accumulator may be attached. Or the microphone may be permanently wired, and the amplifier can then have terminals or sockets for speaker, and a flexible cable for accumulator connecting purposes.

The simpler circuits shown require a relatively large input to the microphone. Howling owing to feedback from the loudspeaker is thus unlikely. However, with the circuit in Fig. 3 it will be found that vibrations or sounds from the loudspeaker must not be allowed to reach the microphone at all strongly, or howling will be set up.

indeed, any transmitter, are correctly tuned to the required harmonic. For such a check, a wavemeter is very necessary and a suitable cheap, absorption type will be described in a future article.



Underchassis view.

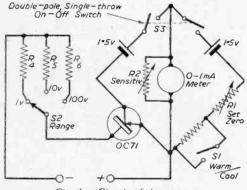
March, 1960

A Transistorised Voltmeter

HIGH INPUT RESISTANCE IS A FEATURE

THE meter described in this article is intended for the measurement of voltages in circuits where very small currents are to be found. If a conventional moving coil or moving iron instrument is connected to a circuit in which only a few micro-amps current flow, then the high current drawn by the meter will result in extremely inaccurate readings. To overcome this effect, it is necessary to use a voltmeter with a very high impedance. The valve voltmeter is an example of such a device.

It was decided that as transistors are cheap and need only a low voltage battery supply we would use them, therefore making the meter port-





able in all ways. When transistors are used in the common emitter configuration, it shows a high impedance between the base and emitter and this fact has been made use of in the design of this apparatus.

Circuit

The circuit shown in Fig. 1 may be considered as a bridge circuit with the meter in the centre arm. Once the circuit has been balanced by adjusting R1 and S1, any variation in the impedance between transistor collector and emitter will destroy the bridge balance and cause the meter to be deflected. The control R2 acts as a shunt to the meter and can be used as a sensitivity control.

The base of the transistor draws current from the supply to which the instrument is connected and since the emitter to collector impedance varies as the base current varies, then changes in the meter deflection occur. To increase the range of the instrument and to increase its impedance, series resistors are switched into the base circuit by S2. In the circuit a warm/cool switch has been provided, this is necessary owing to the dependence of the transistor operating conditions upon temperature. By the use of this switch, the

By G. Connor

instrument can be used over a wide temperature range.

The meter is adjusted initially as follows:

1. Switch on and after short circuiting the input adjust the set-zero R1 control for zero

	COMPONENTS
Transistor	OC71 or equivalent.
Meter	0-1mA.
RI	50k linear variable.
R2.	25k
R3	47k fixed carbon.
R4	22k
R5	220k
R6	2.2M
SI	Two-way, single-pole, toggle switch.
S2	Three-way, single-pole, rotary switch
S3	Two-way, two-pole, toggle switch.

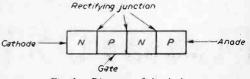
reading on the required range. If this proves difficult, it may be necessary to use the warm/cool switch.

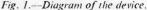
2. Connect the instrument to source of known potential and set the pointer of the meter by means of the sensitivity control.

Silicon Controlled Rectifiers By E. G. Bulley

THESE devices can be said to be a development from both the silicon transistor and rectifier. They are in fact neither transistor trolled rectifier or thyratron, and are p-n-p-n semi-conductors. They can, therefore, best be described as a controlled switching device. Such devices will, however, become more common and available to the constructor and experimenter as in the case of the transistor.

Silicon controlled rectifiers have a low forward voltage drop which permits high current ratings and high efficiency with low voltage requirements. Considering these devices, one will appreciate that they have three rectifying junctions, as can be seen from Fig. 1. The first "n" is known as the cathode, whereas the first "p" is known as the "gate." This termination acts as a grid as in thyratron practice and does not, therefore, need further explanation. The second "p" type is known as the anode and likewise, the reader will appreciate its use.





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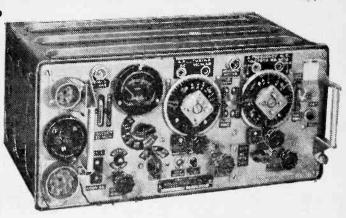
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FURTHER IMPROVEMENTS

The "No. 19"

March, 1960

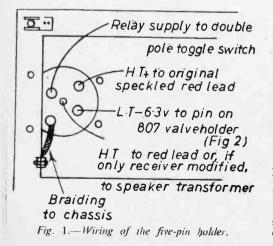
By D. W. Dillon

THE recent release of thousands of ex-army American-

built W.S. No. 19 Mk.2's has resulted in almost every enthusiast's shack in the country containing one. While they are generally used in their original condition, several major defects soon become apparent. The first and most important of these is a great lack of selectivity—the subject of a recent PRACTICAL WIRELESS article. The second fault is that too much associated equipment is necessary for the operation of the set: power unit, accumulators. junction box, microphone, headphones and heavy connectors! The AVC action is too heavy and sluggish and the signal to noise ratio is very poor. It is very difficult to transmit good CW because of the lack of sidetone facilities. On telephony the output power is very low, the modulation invariably downward, and the speech quality poor. It is therefore fortunate that by the removal of the "B" set and "LC." amplifier, much space is available for modifica-tions. Although several amateurs have modified the "B" set for local two-metre use, in the majority of sets, this space simply goes to waste.

Modifications

The first part of this article should be of interest to all 19 set owners, and the carrying out



of the simple modifications described results in transformation into a highly sensitive. selective and inexpensive mains-operated receiver. The second part of the article concerns the transmitter modifications and is of particular interest to licensed radio amateurs and those who hope to obtain a licence shortly. It should, however, be noted that, as with any radio transmitter, no matter how low the power, a Post Office licence is necessary before any attempt is made to transmit into an aerial.

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The transmitter modifications will allow fully automatic sidetone monitoring on CW. The original circuit allowed only 12W input at about 30 per cent. efficiency on telephony, which does not usually result in flattering signal reports ! This article will describe the addition of a 15W modulator stage requiring few extra components and which will allow 30W of good quality 100 per cent. modulated phone output to be run to the 807 P.A. Alternatively series-gate modulation is also described which gives carrier controlled output. The advantage of this method are the small space and few components required, but the disadvantages are lower efficiency and the necessity for $67\frac{1}{2}$ -90V negative bias on the modulator.

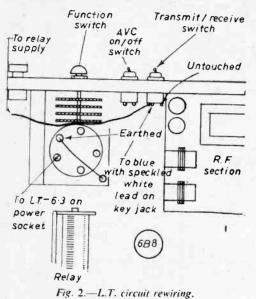
Testing

Having received the set, it is strongly recommended that it be tested in its original form, by obtaining the loan of the associated equipment. After it has been proved to be working satisfac-torily, the B set and LC amplifier are stripped out. All the components to the left of the abovechassis screen (when looking at the front panel) should be removed, as should also those to the left of the below-chassis relays, with the exception of the key jack leads, the leads to pin 4 (green) on the 12-way plug and those to pins 4 (red) and 6 (speckled red) on the six-way plug. The B set gain control also remains. The six- and 12-way plugs are removed, the 12-way one being dis-carded and replaced by a British five-pin socket. The inside "plug" part of the five-way plug is discarded, the outside casing being once again bolted on to the panel, with a Mazda octal valveholder bolted behind the panel to receive the speaker and remote control plug. The braided earth lead is connected to tag 3 on the holder.

while the original red (H.T.) leads are re-routed under the chassis, being connected to the five-pin socket as shown in Fig. 1. A closed circuit jack is substituted for the "quench control" grommet.

6V Operation

The 12V line is earthed at the 807 valveholder (Fig. 2), and a lead taken from the other heater tag to the five-way socket. This allows 6V operation of the heater chain. The green lead (ex-pin 4 is attached to the headphone jack socket. The



leads to the single-pole toggle switch on the front panel are removed, as are also the left-hand section leads on the double-pole toggle switch.

The green and blue leads on the other section should not be dis-turbed. The large 0.1μ F paper condenser fixed to the chassis beside the P.A. tuning condenser is replaced by a 750VW, 0.0005μ F type. The 10Ω variable resistor (het tone) is removed and the leads insulated. In its place is mounted, a 10k wire-wound potentiometer. The resistor between the cathode (pin 8) of VIA (6K7) and earth is disconnected from the chassis tag, and joined to the potentiometer slider. The left-hand tag of the potentiometer is earthed. This is the new R.F. gain control. The single-pole toggle switch on the front panel is used as the AVC on/off switch, being connected between chassis and the AVC line (white) on the tagboard near the 6B8 valveholder.

The bracket which originally

supported the B set tuning condenser is modified to support a miniature air-spaced 0.0005μ F variable condenser. This bracket is replaced in its original position, together with the calibrated knob. A 14in. diameter 3in. coil former 3in. long is wound with 18 turns 22s.w.g. tinned-copper wire, evenly spaced over 24in., is mounted directly on the old E1148 valveholder. One end is joined to a soldering tag on the tuning condenser frame, and the other to the fixed vanes. The B set aerial socket is removed and replaced by a small ceramic feed-through insulation. This is joined to the fixed vanes. A four turn insulated link is fixed around the earthed end of the coil, and connected to a short piece of 80 Ω coaxial cable, which passes directly under the condenser spindle and meter to the tank coil. The original screened box is replaced over the aerial tuning components.

Diode

A crystal diode is connected, with the black end to the fixed vanes and the red end to the small tagboard in the screened box. A wire is taken from this in the direction of the tank coil and marked for later described modifications. The lid of the box is fixed in position. The lead to the A set aerial socket is removed, together with the connection to C1A and the R.F. CL2B.

The tank coil L3A is removed, the connections being noted. The tapping point is ignored, and about three turns removed from the upper end. A four-turn insulated link is wound on the lower end and connected to the coaxial cable. The coil is replaced, the coaxial cable outer sheath being earthed to chassis at its base and all the original leads, with the exception of that to the tapped point, being reconnected to the coil. The set is now ready for testing.

(To be continued)

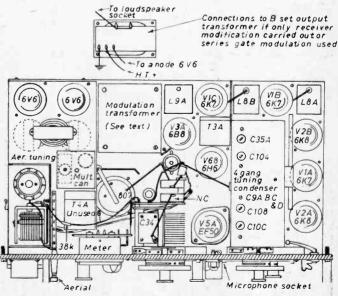


Fig. 3.-Top view of modified 19 set.

March. 1960

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Transistorised Timing Unit

AN INEXPENSIVE CIRCUIT

By L. Baker

THIS photographic process timer is simple to use, inexpensive to build, and small in size, making it a useful accessory in any amateur's darkroom. There are very few parts, and the average constructor will have many, if not all, of these already to hand. The circuit uses a single transistor of the red spot surplus type which makes possible the small size of the finished unit. The size of the case of the prototype is $3 \times 5\frac{1}{2} \times 2in$. This case was originally intended as a food box of the plastic type and is obtainable from all multiple stores. Other types of box or case can, of course, be used, but it is best to use insulating materials such as to prevent any possibility of electrical shock.

Relay

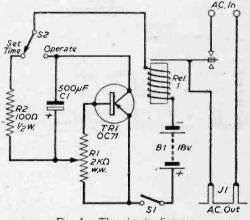
Generally, the size of the relay used will govern the actual size of the finished unit. The relay must have a coil resistance of $2,000\Omega$. In the original model, a surplus type of relay was used, although the P.O. type 3000 works just as well, as indeed will any relay having the required coil resistance. The contacts of the relay must be capable of carrying a reasonably large current dependent on the lamp type in the enlarger. The condenser C1 in the diagram (500μ F) is made up of two units of 250μ F each. However, any number of condensers may be connected in parallel in order to obtain the required 500μ F. The positive side of all the condensers used must be connected together as should the negative sides. The small transistor capacitors now on the market will suit admirably and any number of these connected in parallel to give the 500μ F will suit.

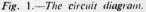
The 2k potentiometer should preferably be a wire-wound type in the interests of accuracy and long service. In the prototype the on/off switch is ganged with this potentiometer, but a separate on/off switch could be fitted if it is considered desirable. The tag strip fitted inside the case serves the useful purpose of providing anchoring points for the wiring and transistor. The resistor R2 in the diagram is 100Ω and rated at $\frac{1}{2}W$. A larger wattage component could be used here if $\frac{1}{2}W$ type is not to hand. The output socket mounted at the side of the plastic case in the prototype was taken from an old L.T. battery of the "dry" type. The writer used this socket as it was small and neat and easily mounted. Other two-pin sockets will suit just as well.

Other two-pin sockets will suit just as well. The relay should be mounted first and holes should be drilled in the case for the fixing bolts. Holes should be then drilled for the potentiometer, S2. the tagstrip, and the output socket. Having drilled the holes, all the parts should be removed from the case which should be covered with one of the thermoplastic materials now available. Alternatively, if a plywood case is used, this can be covered in rexine or similar material. Readers who are skilled in woodworking may care to sand and polish the case. All parts may now be mounted again and the wiring completed. It is best to wire in the transistor last and a heat shunt should be applied to the wires of this component while the iron is applied in order to avoid damage to this component. A pair of tags on the tagstrip are utilised to secure the mains flexible lead; one lead (neutral) from the mains is wired from the tagstrip directly to the output socket, the other lead being taken also to the output socket via the relay contacts.

Batteries

The batteries in the prototype unit were enclosed in the case of the unit. These batteries consisted of two transistor power supply batteries (each of 9V) wired in series to give 18V. One terminal of the on/off switch serves as the anchor point for the positive connection to the batteries. The negative connection to the batteries is taken from one terminal of the relay coil. The other parts are suspended in the wiring. Some of the tags on the strip are not used at all and some serve the purpose of





anchoring the tagstrip to the plastic case by means of small nuts and bolts. Good quality plastic insulation wire should be used throughout. All wiring on completion should be double checked with batteries disconnected, for possible mistakes or short circuits. It is a good idea to include a 0.5mA meter in series with the positive lead to the batteries as a temporary check. On switching on a small current should flow: approximately 1 to 2mA, certainly no more.

To test and calibrate the instrument, the dial must be marked out and attached to the face of the instrument temporarily. It is not possible to mark in the seconds time on the dial accurately without at first experimenting with the completed unit.

(To be continued)

Switch-tuned T.R.F.

HIGH QUALITY RECEPTION OF LOCAL TRANSMISSIONS

By J. Lanspeary

THIS set was designed and built to provide a small, robust "kitchen" radio to receive the local M.W. transmissions, which in the author's area include the BBC Light Programme on 247 metres. The circuit is extremely simple, being a T.R.F. without reaction, using an infinite impedance detector to provide at least one circuit which tunes sharply. Miniature valves were used because these were to hand, but there is, of course, no reason why octal types should not be used; they have the advantage of cheapness. It is

are aperiodic-type coils with dust-iron cores; they are very small and rather fragile, but the performance is very good. Tuning was carried out by a two-bank three-way Yaxleytype switch, and two banks of $3 \times 50pF$ trimmers. All wiring to trimmers and switch was made in screened wire. Grid and anode leads may also be screened to advantage.

When wiring up around the 12AX7 base it will be found that a piece of tagboard is useful to mount the detector cathode components, and also

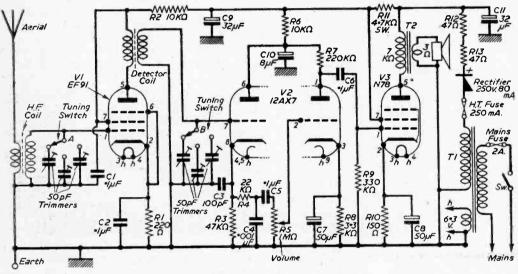


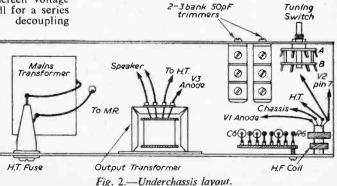
Fig. 1.-The circuit diagram.

recommended, however, to use the specified valve as detector/A.F. amplifier, as the writer has found that the infinite impedance detector is subject to microphony, especially when mounted near the loudspeaker.

The 6AM6 used as R.F. amplifier is one of few valves which may be run with a screen voltage of 250, and a change here might call for a series screen resistor and associated decoupling condenser.

the anode resistors. Wire up the power pack first, then the heaters, then the rest of the circuit backwards, beginning with the output stage and ending with the tuning switch.

The prototype used a 3in. deep chassis; this (Continued on page 969)



Tuning

Switch-tuning was employed as it does away with the need for a dial and drive assembly, surely one of the most trying parts of a receiver. Also, it takes up less room.

Since the Light Programme was available on medium wave, this simplified matters considerably. The coils chosen were Osmor types QA1th and QHF11. These

966

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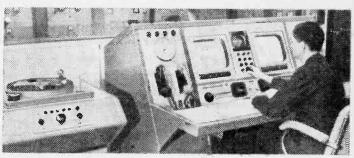
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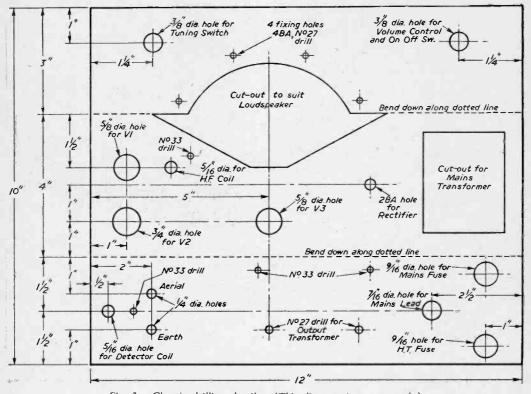


Fig. 3.—Chassis drilling details. (This diagram is not to scale.)

enabled the switch to be mounted underneath the valveholder wiring.

The Circuit

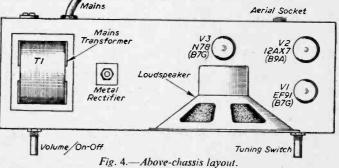
This is very simple. The first valve is connected as a tuned R.F. amplifier, feeding the first

section of a 12AX7, which is connected as an infinite-impedance detector. The advantage of this type of detector is the very low loading which it imposes on the tuned circuit which feeds it. The result is that this tuned circuit tunes sharply, resulting in a great increase in selectivity.

The A.F. output is developed across the 47k detector cathode resistor. Residual R.F. is removed by the filter C3, R4, C4, and the D.C. component blocked by C5.

Thereafter the signal passes to the second half of the 12AX7, which operates as a high gain A.F. amplifier, and to the output valve. This is an N78, rated to give 4W output into a 7k load, with 250V H.T.

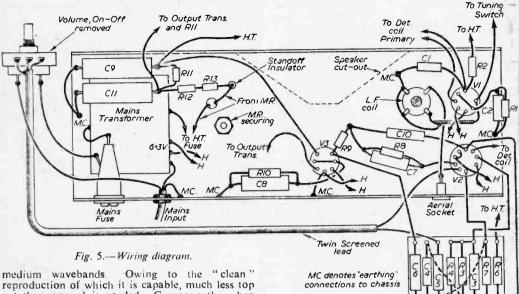
The power supply circuit is also very simple, consisting of a half-wave metal rectifier, resistancecapacity smoothing, and mains transformer. Two 47 Ω resistors are fitted in series with the rectifier; these can be of the $\frac{1}{2}W$ carbon type, and their function is to protect the rectifier from the initial surge which occurs when the electrolytic condensers charge up as the set is switched on. The main smoothing resistor is R11, and it is recom-



mended that this be a vitreous wirewound type, as it becomes quite hot.

Performance

As can be expected, this receiver is not particularly sensitive, being a T.R.F. without reaction. However, it does give very good reproduction of the stronger signals put out by the BBC in the



reproduction of which it is capable, much less top cut than normal is needed. Consequently, when listening to orchestral music, the fidelity of reproduction compares very favourably with most single-ended superhets. The speaker used in the prototype was an 8in. wafer type, measuring less than 2in. back to front, and it was mounted on the chassis.

The results quoted were with 3ft. of 18s.w.g. copper wire used as an aerial and the chassis connected to mains earth (a very desirable feature

A QUALITY F.M. RECEIVER

(Continued from page 932) ping screws passing through the bottom into the chassis flanges.

Although the values of the various components used in this receiver can be determined from the when the set is housed in a cupboard, not a cabinet!). With a picture-rail aerial, some 15ft. long, volume is much increased, but selectivity becomes a problem, the longer aerial damping the first tuned circuit.

To chassis

text and the circuit diagrams, some readers may find it easier to buy components from the list which is given below. When ordering, it may be found that some components are temporarily out of stock and if this is so the advice of the dealer should be taken concerning suitable equivalents.

COMPONENTS LIST								
$\begin{array}{l} Resistors: \\ (All $\frac{1}{4}W$ unless \\ R1-18k. \\ R2-4.7k $\frac{1}{4}W$ \\ R3-6.8k $\frac{1}{2}W$ \\ R3-6.8k $\frac{1}{2}W$ \\ R4-150 Ω. \\ R5-100k. \\ R6-47k $\frac{1}{4}W$ \\ R7-4.7k $\frac{1}{4}W$ \\ R9-47k. \\ R10-150 Ω. \\ R11-47 Ω. \\ R11-150 Ω. \\ R13-47 Ω. \\ R13-47 Ω. \\ R14-6.8k. \\ R15-6.8k. \\ R15-10.8k. \\ R15-2.7k. \\ R18-11M. \\ VR1-2.2k $pot. \\ VR2-1M $log. \\ Capacitors: \\ \end{array}$	otherwise stated.) R19—1M. R20—47k. R21—270k ±W R22—2.7k. R23—22 Ω. R24—10k ±W R25—47k. R26—1M. R27—2.2k. R28—47k. R30—470k. R31—600 Ω 1W R32—Sce text (p. 848 February issue). R33—100k. wire-wound.	C3-1,000pF ceramic. C4-1,000pF ceramic. C4-1,000pF ceramic. C5-1,000pF ceramic. C6-47pF ceramic. C7-47pF ceramic. C7-47pF ceramic. C9, C10-25+25pF ganged. C11-1,000pF ceramic. C13-10,000pF ceramic. C13-10,000pF ceramic. C14-10,000pF ceramic. C15-47pF ceramic. C16-10,000pF mica or ceramic. C17-Not used. C18-300pF mica or ceramic. C20-300pF mica or ceramic. C21-50 μ F electrolytic 25VW C23-50 μ F electrolytic 350VW C25-8 μ F electrolytic 25VW	 C29-0.01 //F 300VW C30-0.01 //F 300VW C31-16 //F electrolytic 350VW C32-16 //F electrolytic 350VW C33-See text (p. 848 February issue). Sundries : IFT1, IFT2, 10.7Mc/s I.F. transformers. RDT ratio detector transformer. L1-See text and Fig. 3a. L2-See text and Fig. 3a. L4-LF choke 10H 60mA. T1-Output transformer Wharfdale GP8. T2-Mains transformer 250-0-250V 60mA 6.3V 4A. Valves : V1, V2, V3, V4-EF91. V5-ECC81 or ECC83. V6. V7-EL91. 					
C1-1,000pF ce C2-1,000pF cer		C27-0.01 #F 300VW C28-8 #F electrolytic 350VW	V8—6X5. V9—EM34.					

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ub News

ALDERSHOT & DISTRICT AMATEUR RADIO SOCIETY Signals Wing, No. 4 Training Regiment, Royal Engineers, Gibraltar Barracks. Hon. Sec. : A. M. Laidler.

MEETINGS are held every Wednesday at the above address M at 7.30 p.m. with the exception of the second Wednesday in each month when the meeting is held at "The Cannon," Victoria Road, Aldershot.

A technical course of training to R.A.E. standards was started in January in readiness for the May examination. It is also hoped to run Morse training periods for those persons requiring this type of training.

type of training. The society requires instructors and lecturers to give instruction to R.A.E. standards and licensed amateurs who are willing to devote a little time to instruct new members. All correspondence should be addressed to the hon. sec. at "Pondside," Sandy Lane, Churt, nr. Farnham, Surrey.

BRIGHTON AND DISTRICT RADIO CLUB

Home Guard Club, British Legion, 76, Marine Parade, Brighton. Hon. Sec. : H. R. Henly (G3HR).

ON January 6th Mr. D. Hemsley gave a talk on "A Home-built Oscilloscope for TV Servicing," and on January 20th a filmshow was held at the H.Q.

Future events :

- February 10th.—Informal evening. February 17th.—Filmshow. February 24th.—" A Home-built Tape Recorder," by Mr. D.
- March 2nd.—Informal evening. March 2nd.—Informal evening. March 9th.—"The Design of Communication Receivers," by H. R. Henly. March 16th.—Filmshow. March 23rd.—Informal evening. March 30th.—Demonstration of the Geloso G209R Receiver,

by R. Smith.

BRITISH INSTITUTION OF RADIO ENGINEERS

Bedford Square, London, W.C.I. Meetings for February, 1960
 LONDON Section.—Meetings are held at the London School of Hygiene and Tropical Medicine, Keppel Street. Gower Street, W.C.I.
 There Explores With At 630 Computer aroup "Drift

Tuesday, February 9th.—At 6.30. Computer group. "Drift Correction of D.C. Amplifters," D. Leighton Davies. Wednesday, February 24th.—At 6.30 n.m. Medical electronics group. "The Unification of Electronic Clinical Instruments,"

Wednesday, February 24th.—At 6.30 p.m. Medical electronics group. "The Unitication of Electronic Clinical Instruments," Dr. F. D. Stott. Bristol, South-western Section.—Meetings are held at the School of Management Studies, Unity Street. Wednesday, February 24th.—At 7 p.m. "Industrial Magnetic Recording and Playing Machine Design," J. Elliot. Cardiff, South Wales Section.—Meetings are held at the Welsh College of Advanced Technology. Wednesday, February 10th.—At 6.30 p.m. "Low Noise Low Drift D.C. Amplifters." V. L. Devonald, B.Sc. Newcastle-upon-Tyne, North-eastern Section.—Meetings are held at the Institution of Mining and Mechanical Engineers, Neville Hall, Westgate Rd. Neville Hall, Westgate Rd.

Revuic Hall, Westgate Rd. Wednesday, February 10th.—At 6 p.m. "Instrumentation in Rocket Propulsion," Raymond E. Ross (Associate Member). Wolverhampton, West Midlands Section.—Meetings are held at the College of Technology, Wullruna Street. Wednesday, February 10th.—At 7.J5 p.m. "Electronic Reading," I. W. Merry.

BRITISH SOUND RECORDING ASSOCIATION

ONDON Meetings .- Meetings are held at the Royal Society of Arts, John Adam Street. Adelphi, London, W.C.2.

Future events: February 19th.—At 7.15 p.m. "The Sounds of Music," W. H. George, M.Sc., Ph.D., F.Inst.P. March 18th.—At 7.15 p.m. Talk by R. S. Roberts, M.Brit.I.R.E.

Sen.M.I.R.E.

Sen.M.I.R.E. April 22nd.—At 7.15 p.m. "Sound Radiation from Loud-speaker Cabinets," James Moir. M.I.E.E. May 21st.—Amateur competition display—annual general meeting to be held in the evening at the Overseas League, St James's S.W.I. South-western Centre.

Centre Organizer : D. W. Aldous, "Alderbourne," Greenways Road, St. Marychurch, Torquay, Devon. Meetings are held at Callards Cafe at, 7.45 p.m.

REPORTS OF CURRENT ACTIVITIES

March 3rd.—" High Fidelity Sound Reproduction," N. Mordaunt (Tannoy).

CALCOT RADIO SOCIETY

Hon, Sec.: C. Aldous, 3, Oliver Drive, Calcol, Reading, Berkshire. Future events :

FEBRUARY 18th.—Lecture and demonstration of Hi-Fi equipment by a representative of E.M.I. Sales. March 17th.—Lecture on the suppression of electrical inter-ference in TV and radio sets. by Mr. Richardson of the G.P.O. April 21st.—A lecture and demonstrations by a representative of Twardson and the supersentative of the set of t

of Truvox

May 19th.--Lecture and demonstration on the Design of Hearing Aid Equipment, by Mr. Williams, of Belclere Ltd.

CHILTERN AMATEUR RADIO CLUB

Hon. Sec. : R. Barton. 25, Hillside Road, Marlow, Bucks.

MEETINGS are held at the British Legion Club. St. Mary's Street, High Wycombe, on the last Thursday of each month. February : "Some Aspects of Aerial Design "-G3LSK. March : Mullard Film Show-G3INZ. April : Junk sale and Quiz. May : Mobile gear for the Amateur Band.

- DERBY AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec.: F. C. Ward (G2CVV), 5, Uplands Avenue, Littleover, Derby.
- MEETINGS are held in Room No. 4, 119, Green Lane, Derby. Future events

February 7th, at 7.30 p.m.: Proposed date for contest for G5YY. March 18th, at 7.30 p.m.: Proposed date for annual dinner

and dance August 14th, at 7.30 p.m. : Third annual mobile rally.

HALIFAX AND DISTRICT AMATEUR RADIO SOCIETY Hon. Sec. : A. Robinson (G3MDW), Candy Cabin. Ogden, Halifay

 O^N December 8th members heard a lecture dealing with radio astronomy by Mr. Doihty, of Halifax, and on February 2nd H. Makin (G3FDC) gave a lecture on the S.W.R. Bridge.

Future events :

February 16th : Informal meeting. March 1st : Film show.

NOTTINGHAM CO-OPERATIVE AMATEUR TAPE RECORDING SOCIETY

OWING to accommodation difficulties the meeting night has been altered to Thursday. A fairly detailed programme has been planned for the first few months of 1960 and, as several members have expressed the desire to know more about tape recorders, a series of informal discussions have been arranged technical aspects and this means that the club will have meetings every other Thursday on February 18th, March 3rd, 17th, 31st, April 14th and 28th, etc.

THE RADAR AND ELECTRONICS ASSOCIATION Hon. Sec. : C. W. Knight, 83, Portland Place, London, W.1.

MEETINGS are held at the Royal Society of Arts, John Adam Street, Adelphi, London, W.C.2, at 7.30 p.m. Future events :

February 9th Transistors--Today and Tomorrow." by E. Wolfendale, B.Sc.(Eng.), A.M.I.E.E. March 28th : "Computers—Some Design Problems of Large-scale Computers," by Peter D. Hall, of Ferranti Ltd.

THE READING AMATEUR RADIO CLUB

Hon. Sec. : R. J. Nash (G3EJA), " Peacehaven," 9, Holybrook Road, Reading. ON January 30th a meeting was held on morse instruction.

U following the discussion on field day activity for the new year. A junk sale was held atterwards. Future events :

February 27th : Film on the manufacture and application of transistors. SIC STRUKES

March 26th : Talk on the application of transistors to ham

gear, in particular receivers and transmitters. Meetings are held at Palmer Hall, West Street, Reading, at 7.30 p.m.

REIGATE AMATEUR TRANSMITTING SOCIETY

Hon. Sec. : F. D. Thom (G3NKT), 12, Willow Road, Redhill, Surrey.

MEETINGS are held at The Tower. High Street, Redhill, usually on the third Saturday in the month at 7.30 p.m. The club visited the BBC station at Tasheld on January 9th and the first annual general meeting was held on January 16th.

Future events :

February 7th : Annual dinner to be held at Laker's Hotel, Redhill. Tickets 15s. each. February 20th : "The Story of Paul Bates (G3MAC)," by

G2DVD, assisted by G3HCU. March 19th : "TVI" by G4ZU.

THE SLADE RADIO SOCIETY

Hon. Sec.: C. N. Smart, 110, Woolmore Road, Erdington, Birmingham, 23.

MEETINGS are held at the Church House, High Street, Erdington, at 7.45 p.m. The club station (G3JBN) at the Church House is available for the use of members for constructional purposes.

Future events :

Future events: February 12th: Sale of surplus equipment. February 26th: "Electronics in the Search for Oil," by \vec{G} , T, Peck, M.B.E. March 4th: Mullard film meeting to be held at the Bennett Hall, Y.M.C.A., Snow Hill, at 7.45 p.m. March 11th: Modern broadcast reception. March 25th: "Electronic Digital Computers," by M. D. Eventer (GACKZ) Fowler (G3GKZ).

THE TEESIDE AMATEUR RADIO CLUB

Hon. Sec. : A. L. Taylor (G3JMO), 12, Endsleigh Drive, Acklam-Middlesbrough.

MEETINGS are held at Settlement House, 132. Newport Road, Middlesbrough, every alternate Friday from February 5th until the Easter break.

WELLINGBOROUGH AND DISTRICT RADIO AND TELEVISION SOCIETY

- Hon. Sec. : D. J. Trusler, 87, Irchester Road, Rushden, Northants, Club room above W.I.C.S. fruit shop in Silver Street.
- MEETINGS are held in the club room every Thursday at 7,45 p.m. Future events

February 18th : Film ni March 3rd : Talk on Mitchell, B.Sc. Film night in the club room. alk on "Electronics and Radiation," by R.

Third Conference on Medical Electronics To be held at Olympia, London, 21st-27th July, 1960

THE human body is made up of a number of inter-related systems-brains and nerves. heart and blood vessels, stomach and intestines, lungs and windpipe-and different electronic techniques can be used for their measurement and control.

In the respiratory system, one of the things the physician may need to know is the velocity with which air flows through the windpipe, and the volume of air respired at each breath. This may be measured by a device called a pneumotachometer. In this, the airstream passes through a piece of metal gauze. This causes a change in pressure which is related to the rate of flow. The change in pressure is minute, but it can be measured by an electronic-pressure gauge. The electric signal obtained is passed through a "black box" which instantaneously computes the volume of air breathed in a given time, and records it as a line on moving paper.

The physician may need to know the amount of carbon dioxide which is being excreted as a waste product into the expired air. This information can be obtained by chemical analysis, but a single determination would take a skilled technician half an hour or more. The modern method uses infra-red rays which are passed through a sample of the breath. The carbon dioxide present abstracts some of the energy from the rays. The lost energy can be measured, and because of the terrific speed of electronic techniques the breath can be analysed in this way in a few hundredths of a second. Thus not only can the amount of carbon dioxide be measured, but also the concentration in each fraction of the expired air, and this can be very helpful in the diagnosis of respiratory disease.

In poliomyelitis, the breathing muscles may be partly paralysed, and the patient's respiration may then have to be assisted by a machine. Electronic devices can now measure the patient's disability. and control the degree of assistance provided by the machine. In this way the volume of breathing is automatically adjusted to suit the need of the individual patient.

During anæsthesia, drugs may be used which produce a temporary paralysis of the breathing muscles, and here again an electronically controlled machine may take over the patient's breathing and keep its volume at the right level.

Servo systems are common in electronics, and a "servo-anæsthetiser" has been devised at the Mayo Clinic. This is worked by the activity of the patient's brain. This activity is measured electronically. An increase in this measurement indicates that anæsthesia is becoming lighter. This increase sets off a relay which raises the rate at which the anæsthetic is being delivered. Conversely, deepening anæsthesia results in a decrease in the rate of delivery. In this way the depth of anæsthesia is automatically held at any desired level.

These are but a few examples of the impact of electronics on two aspects of medicine. New uses are continually being found, and so rapid is the progress, in a dozen different countries, that international conferences to exchange ideas and to tell of new techniques are needed every year.

The next such conference is being organised by the Electronics and Communications Section of The Institution of Electrical Engineers in London next July. Doctors, biologists and electronic engineers from all over the world are being invited to attend. The proceedings are designed to appeal not only to the medical and electronic experts but also to those who are not themselves specialists, but who wish to get a general background to the many new techniques. It is expected that from this meeting of British and foreign talent, new methods of measurement and control, of diagnosis and treatment, will emerge to heal the sick.

PRACTICAL WIRELESS



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PRACTICAL WIRELESS

SOLDERING IRON STAND

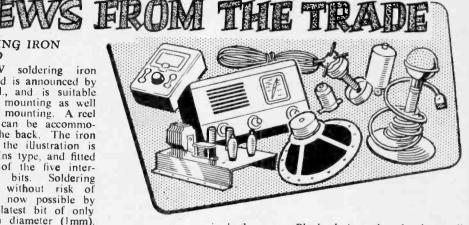
NEW soldering iron stand is announced by Antex Ltd., and is suitable for bench mounting as well as for wall mounting. A reel of solder can be accommo-dated on the back. The iron shown in the illustration is of the mains type, and fitted with one of the five interchangeable bits. Soldering transistors without risk of damage is now possible by using the latest bit of only 0.040in. in diameter (1mm).

It is necessary to touch the lead of a transistor for only a few seconds with this needle-type bit to solder or unsolder. The stand retails at 12s. 6d. Antex Ltd., 7/8 Idol Lane, London, E.C.3.

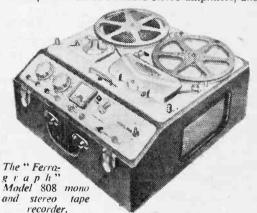
NEW TAPE RECORDER

A NEW tape recorder, Model 808, has been announced by Ferrograph. The purpose of the machine is to give both mono and stereo recording and reproduction on conventional tracks. There are complete recording amplifiers

The " Antex " soldering iron stand.



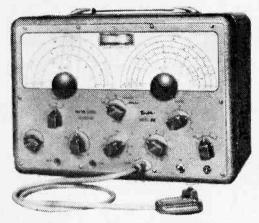
in both cases. Playback is at low level on all output channels: 1.5V across 5,000 ohms. The reason for this is twofold; in the first instance. it would not be possible to include two audio amplifiers in an already full portable case, and, secondly, the majority of serious users would be in possession of standard stereo amplifiers, and



would have no need of further amplifiers of this type. In a two-tone, grey transportable cabinet, this model retails at 105 guineas. British Ferro-graph Recorder Co., Ltd., 131, Sloane Street. London, S.W.1.

A.M./F.M. Signal Generator

A SIGNAL GENERATOR designed mainly for the servicing of A.M. and F.M. high frequency receivers and the intercarrier I.F. stages of television receivers was released in January by Taylor Instruments. This model (61A), provides in conjunction with an oscilloscope complete facilities for the sweep alignment of the R.F., I.F. and discriminator or ratio detector stages of A.M. and F.M. receivers. The A.M. generator covers the range 4-120Mc/s in five bands, all on fundamentals. The F.M. and sweep bands cover the frequencies 4-12Mc/s and 70-120Mc/s in three bands. Deviation on F.M. is variable up to 100kc/s from the mean carrier frequency at a modulation rate of 400c/s. All the facilities offered in the 61A model may be selected by



The "Taylor" A.M./F.M. signal generator.

internal switching. Taylor Electrical Instruments Ltd., Montrose Avenue, Slough.

"THERMONIC OSCILLATORS"

THE second of the new series of filmstrips introduced recently by the Mullard Educational Service to assist the teaching of electronic engineering in technical colleges and similar establishments has now been completed. The first strip in the series, parts 1 and 2, dealt with the basic principles of oscillation and the various forms of sinusoidal oscillators. Thermonic Oscillators-parts 3 and 4" resumes the story with an exposition of non-sinusoidal oscillators. It explains the generation of pulses, square-waves, and sawtooth waveforms for television and oscilloscope timebases, and describes in detail the various forms of relaxation oscillator, blocking oscillator and multivibrator. The filmstrip comprises 22 frames in colour and may be obtained from the distributors. Unicorn Head Visual Aids Ltd., 42. Westminster Palace Gardens, London, S.W.1. price 25s.

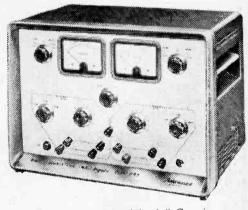
" RADIO AMATEURS' HANDBOOK"

THE 27th edition of the Radio Amateurs' $T_{Handbook}^{HE}$ is to be published in 1960 and will remain the same price as the previous edition. which is 32s. 6d. For further information readers should contact Arthur F. Bird. 66, Chandos Place, Strand, London, W.C.2.

TRANSISTORISED STABLE D.C. SUPPLY

TRANSISTORISED dual stabilised D.C. unit which provides two 0-30V. 1A stabilised supplies from a single instrument has been produced by "Advance." Both sections of the supply are floating and may be operated separately, or connected in series to provide a maximum output of 60V A.C. at I A. Similarly, both positive and negative voltage supplies may be drawn simultaneously up to a maximum of 30V each. The range of 0 to 30V in each section

is covered in three 10V steps by means of a variable control directly calibrated in volts and the output is monitored by an ammeter and voltmeter which can be independently switched to either circuit as required. Four terminal output networks are incorporated which enables the effects of resistance of the connecting leads to the load to be virtually eliminated and overload protection is afforded by an electronic circuit which provides complete protection against both progressive overloads and short circuits. Protection against internal failure or excessive mains surges is provided by a panel-mounted fuse in the mains circuit. Advance Components Ltd., Roebuck Road, Hainault, Ilford, Essex.



The " Advance" stabilised D.C. unit.

TV SET FOR DESIGN CENTRE

C.W.S. Defiant television set has been chosen by the Council of Industrial Design for exhibition in the Design Centre. Slimline model V101, it is a 17in, table model with 12 valves and a wide angle 110deg, tube.

CAREERS IN RADIO AND TELEVISION SERVICING

AREERS, for boys about to leave school, in U the repair and maintenance of radio and television receivers, are described in *Radio and Television Servicing* (H.M. Stationery Office, No. 66. price 1s. 6d. net), a revised booklet in the "Choice of Careers" series published by the Central Youth Employment Executive.

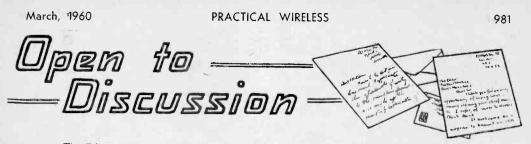
A systematic approach is the basis of good servicing, and the booklet shows how the young trainee learns to identify the many different radio components, and to use hand tools and special test equipment, developing his knowledge of electrical theory at the same time.

The most common form of training in the industry is apprenticeship, and details are given of the national apprenticeship scheme drawn up by the trade and of the schemes operated by the Airways Corporations and the Service departments. Among the qualities needed for this occupation are dexterity, patience, perseverance and resourcefulness.



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The Editor does not necessarily agree with opinions expressed by his correspondents.

Whilst we are always pleased to assist readers with their technical difficulties, we regret that we are unable to supply diagrams or provide instructions for modifying commercial or surplus equipment. We cannot supply alternative details for receivers described in these pages. WE CANNOT UNDER-TAKE TO ANSWER QUERIES OVER THE TELEPHONE. If a postal reply is required a stamped and addressed envelope must be enclosed with the coupon from page iii of cover.

Interference

SIR,-I think you are right in your comment in the December, 1959, issue, by saying that interference on A.M. medium and long waves can only be stopped (or partly stopped) by closer control of frequencies and number of stations operating. All this deserves a conference of all countries concerned and must include the USSR (which has hundreds of stations). The chance of any agreement is very small, I think. What is needed is as follows: each country should be given three or four channels to broadcast highpowered transmissions. The main part of listening to home transmissions should be done on V.H.F. which at present is cheap. The medium wave perhaps could be made larger say 165-700m and each country should do its part to stop interference from morse, etc. We can only hope that something will be done sooner or later about the problem which grows worse each year.-M. **REYNOLDS** (Nailsea).

The "Old Days"

SIR,—It is obvious that amateur radio is not all that it used to be. This is because all "modern" components have to be soldered. In many cases there is very little of anything left, to solder on to! Many amateurs have no facilities for soldering. Many are not allowed to solder.

Again, modern components are dull and uninteresting in appearance. An article is described as a "capacitor" and has much wonderful scientific data tagged on. The latter no doubt is correct. But it will appear to be just a plain common roll, covered in paraffin wax, and with a wire sticking out of each end.

a wire sticking out of each end. "Condensers" used to be well designed and interesting-looking pieces of apparatus. They had screwing-down holes, efficient terminals, and soldering tags. They were brand new in appearance, wrapped in tissue paper, and packed in attractive cartons. Therefore they sold well! Resistances had metal cones at each end. To

Resistances had metal cones at each end. To change a resistance, one had only to remove one from its clips and replace it with another. What magnificent iron-shrouded transformers there were. Variable condensers were veritable masterpieces. Coils were composite and shielded triumphs ! In those days there was also the sense of the marvellous to attract the amateur. I well remember the excitement which reigned when he "giant" 5XX station, with its 14kW, was about to take the air. I listened in with a crystal set, based on a 12 \times 4in, cardboard former wound with 24 gauge D.C.C. wire. I think we half expected loud speaker results! I was gratified, however, to receive loud and clear telephone signals; much better than those previously received from the London station.

Valves were quite good in those days. Especially when the new "dull-emitters" were introduced.

The experimenter with battery and transistor sets, who does not wish to solder, should obtain some small oblong electrical connectors. These have a central hole, which enables them to be bolted to the chassis with small gauge bolts. They completely obviate the need to bend wires on condensers and resistances and can also be removed and replaced at will.

Use a larger chassis! One with components widely spaced gives a set a quite impressive appearance. Far more so than does a small chassis, containing all the wires and components. in more or less a jumbled heap.—A. TROWBRIDGE (Staines).

Capacitors

 $S^{IR,-I}$ am a beginner to radio and I would like somebody of your readers to help me. Suppose that I need an $8\mu F$. 600VW condenser and that nothing of the kind is available. Can 1 put two $16\mu F$, 300VW condensers in series so that I will obtain an $8\mu F$ 600VW condenser from them? In my opinion 1 am right and 1 wonder of any of your readers will agree.—JOSEPH MIFSUD (Flat 1, Block XI, Hubbard Flats, Cospicua, Malta, G.C.).

Radio Sound

S1R,—There have been numerous letters about radio sound on A.F. amplifiers. The radio sound in most cases is due to the fact that anode bend rectification is taking place. This is most probably due to the fact that the bias resistor in one stage has deteriorated so that the valve is biased up to nearly cut off point and is hence acting as an anode bend detector. It could also be due to wrong choice of bias resistor value in the first case. The fact that different stations are received can only be due to the fact that the "mike" head is acting as a tuned circuit and with difference in the length of cable there will be a difference in frequency received. If any other SWL of my own age (14) could take the trouble to correspond with me I should be pleased to hear from him.—W. J. WHITE (14, Pollard Close, Chigwell, Essex).

27Mc/s Transmitter

SIR,—I constructed the 27Mc/s pocket transmitter as published in the December edition of PRACHCAL WIRELESS, and found it to work quite satisfactory. I then converted the transmitter for mains use, using an R.F. pentode triode connected, cathode keying. I found that a 50c/s mains hum was being transmitted, so I included an A.F. choke in the anode circuit. This worked extremely well, but when I was working the transmitter I noticed that another signal was behind my own. I then sent out a continuous signal, and found that when my transmitter was in operation other stations transmitting speech and music came in behind, but when I switched my transmitter off they stopped. This did not only occur on 27Mc/s but on many frequencies. Can any reader give an explanation of this ?— C. GODDARD (Wallington, Surrey).

Using the RF24

SIR,—Several queries have been received regarding the coil data of the RF24 unit. Several of the RF24 and RF25 units on the surplus market have been modified to cover the frequency ranges of the RF26 and RF27 units. The coil details required are as follows:

R.F. grid coil. $14\frac{1}{2}$ turns 22s.w.g. tinned copper with three turn link interwound at earth end

Mixer coil: 8[±] turns 2²s.w.g. tinned copper.— D. PRATT, G3KEP and D. NOBLE, G3MAW (Yorkshire).

Mains Polarity

SIR,—With reference to G. F. Watt's letter on mains polarity (December, 1959, issue). I should say that there would be no possibility of the Supply Authority changing the phases over at the Power Station or Sub-station, for that matter, as this would have disastrous effects, such as three-phase motors being reversed. Also on a single-phase supply the polarity of the switching of lights, also plugs, would be reversed; this also would result in the neutral being broken at the switch positions instead of the live side.

There is a possibility of the mains round G. F. Watt's area being out of balance; this could be caused by too many consumers on the same phase, causing a leakage on the neutral, which could have a potential of several volts between neutral and earth. depending on this out of balance. This may be the explanation for the ripple of which Mr. G. F. Watts complains.

I was also interested in Mr. G. Y. Kingdon's letter in the November issue, and fully agree with him regarding earthing and more stress being placed on the correct connections of live and neutral and earth terminals of plugs. as all modern three-pin plugs and socket outlets are marked "L." "N" and "E." It is always advisable to test the socket outlet to find the polarity, as

quite often these are connected the wrong way round, even when the job has been done by a socalled electrician.

I was also interested in Mr. W. Pascoe's comments on earth connections, and he makes a rather interesting point where miniature circuit breakers are employed on some modern installations. Where the radio set is an A.C. type with the three core lead connected to a mains earth system and also an independent outside earth, it does appear that this would create a parallel earth depending on the resistance of the two earths, therefore, affecting the working of the miniature circuit breaker. 1 intend taking this matter up with someone who is an authority on circuit breakers.—A. DEARDEN (Johannesburg, S. Africa).

Transistors v. Valves

SIR,—Being an ardent supporter of the valve, I would like to make a few points in its favour.

Transistor sets cannot beat F.M. mains valve sets as far as reproduction and good tone are concerned, because as yet transistors do not work so well at high frequencies, and it would be difficult for a transistor set to beat the tone and volume of an ordinary five-valve superhet.

Although mains sets do not work as soon as they are switched on. one should not compare transistor sets with mains superhets. Battery sets, on the other hand, work instantaneously like transistor sets.

Although transistors have many points in their favour, such as small size and low power consumption, valves are being made smaller, and are taking less current. Perhaps a power supply to heat the cathode could be completely eliminated by further research into "cold-cathode" valves. If there was no need for a filament battery, there would be few advantages for transistors.—D. C. HAIGH (Bradford, York).

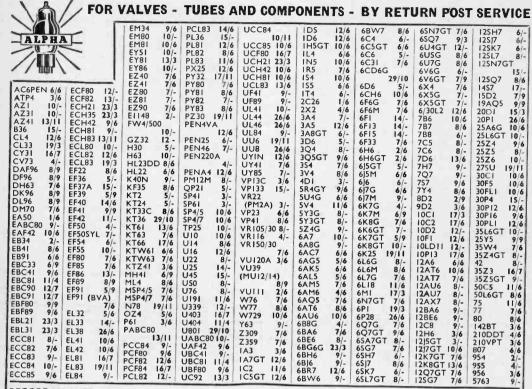
S1R,—Recent letters from readers prompt me to offer a few remarks. On transistors. I would say that I have experimented with them for the past three years, having always tried to get a lot from the least, and like them.

I have achieved a certain success, being able to receive stations from all over Europe, plus Tangier, on all wavelengths down to 30m; this on a crystal and transistor circuit with a 75ft. aerial about 20ft, high, and a counterpoise type earth, as I find it very much better than a "grounded" earth. Tapped coil and switch are employed in both aerial and tuned circuits and output is boosted by a transformer.

I have tried many of the circuits which have been published in previous issues of PRACTICAL WIRELESS and have made many very good receivers—some without resistors.

The volume from the two circuits is terrific. But, like Capt, Graham and others remark, break-through persists from powerful stations, and in my area the local Third tries to swamp everything.

PRACTICAL WIRELESS



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4-speed 10 records .capacity, Ful-Fi turnover crystal cartridge. £6.19.6.

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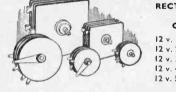
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983

For "Thermion's" information, until last week when I had a check and change, I was using as long wave coupling, a coil I wound by hand in 1923 and I have more components of that vintage. I also held one of the 15s. experimental licences of that time, and I listen to ships on a one valve circuit using a very old 2V valve and can log every ship, shore station including Scottish.— W: M. MACKENZIE (Gosport, Hants).

Correspondents Wanted

SIR,—I am 21 years of age and I am a qualified radio engineer. I am also working in the Police Radio Office as a radio engineer. I want to correspond with any boys of any age who

MEASUREMENTS WITH MULTI-RANGE METERS

(Continued from page 942)

adjusting the potentiometer the voltmeter should be set to read full scale, i.e., 2.5V. The potential between the slider and H.T. negative then has a reference value of 297.5V. The resistance value of the potentiometer is made low so that the adjustment is fine otherwise a slight movement of the slider would represent many volts and the voltmeter could not be accurately adjusted.

The load is now switched on and if the change in voltage is from 300V to 299V then the meter reading will decrease from 2.5V to 1.5V. This change can then easily be read to a high degree of accuracy.

A.C. Measurements

The basic moving-coil instrument may be modified to measure A.C. by first rectifying the A.C. before passing it through the meter movement.

Unfortunately the resistance of the rectifier varies with the amount of current flowing; at low values of current, low scale readings, the forward resistance of the rectifier is greater than at high scale readings. This effect is unimportant when using high voltage ranges as then the required high value of series resistor "swamps" the resistance variations of the rectifier. On low voltage ranges the rectifier resistance variation become proportionately greater when compared

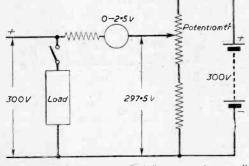


Fig. 7.—An accurate method for measuring small changes in voltage.

are interested in radio subjects.—ASHAK KAPUR (Ph. Police Radio Office, Simla—2).

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to the total circuit resistance and result in a nonlinear shape of the low end of the scale.

With the better, and subsequently more expensive, instrument the difficulty is overcome by using a voltage transformer on the low ranges. The low input voltage is stepped up and then the higher value of series resistor is large enough to swamp rectifier resistance variations,

Quoted Accuracies

In the cheaper instruments the inaccuracies are tolerated but are indicated by quoting the calibra-

Voltage	Accepted Variation	Error
80	76V to 84V	5% 10%
40	36V to 44V	
20	16V to 24V	20%
8	4V to 12V	50%

tion accuracy of the meter as a percentage of *full* scale reading. Consider a meter, the accuracy of which is quoted as, say. 4 per cent. of full scale reading. On the 100V range this means a reading may vary by $\pm 4V$. At f.s.d., the percentage error is, of course, only 4 per cent, but the table above shows how the percentage error increases at voltages less than f.s.d.

This point should be borne in mind before wasting time trying to make a too accurate reading. The accuracy cannot be better than the accuracy of the instrument.

Another point to remember is that the moving coil instrument measures the mean value of the rectified A.C. The value normally required is the r.m.s. The average value when multiplied by the form factor gives the r.m.s. value. The form factor for a sine wave is 1.11 so during calibration all mean values are multiplied by 1.11 and scale readings are then read as r.m.s. values.

If the waveform of a measured voltage is not a pure sine wave, the form factor will not be 1.11 and the meter calibration will not be maintained. Two vastly different waveforms may have the same mean value but as the form factors would be different the r.m.s. values would be different although the meter deflection would be the same in each case. In practice the error is not very great but is mentioned mainly to emphasise the errors present when the waveform is not a pure sine wave.



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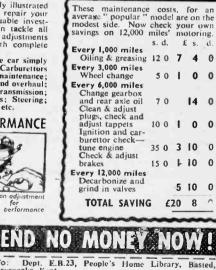
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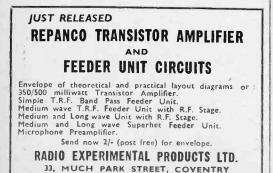
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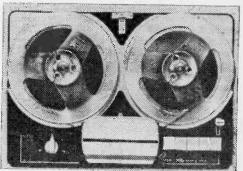
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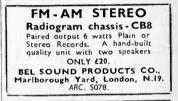
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PRACTICAL WIRELESS

March. 1960



Practical Wireless

-BLUEPRINT-

ALL OF these blueprints are drawn full-size and although the issues containing descriptions of these sets are now out of print, an asterisk in the list below denotes that constructional details are available free with the blueprint.

The index letters which precede the Blueprint Number indicate the periodical in which the description appeared. Thus PW refers to PRACTICAL WIRELESS; AW to Amateur Wireless and WM to Wireless Magazine.

Send (preferably) a postal order to cover the cost of the Blueprint (stamps over 6d. unacceptable) to

Title		Number	Price
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Junior Crystal Set		PW94*	2/-
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Modern One-valver	• • •	 PW96*	2/6
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PRACTICAL WIRELESS, Blueprint Dept., George Newnes, Ltd., Tower House, Southampton Street, Strand, W.C.2.

SPECIAL NOTE

THE following blueprints include some pre-war designs and are kept in circulation for those constructors who wish to make use of old components which they may have in their spares box. The majority of the components for these receivers are no longer stocked by retailers.

Title		Number	Price	
A.C. Fury Four	• • • •	PW20*	2/6	
Experimenter's Short Wave		PW30a*	2/6	
Midget Short Wave Two	••••	PW38a*	2/6	
Band-Spread Three (Battery)		PW68*	2/6	
Crystal Receiver	<u>)</u>	PW71*	2/-	
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Simple S.W. One-valver		PW88*	2/6	
Pyramid One-valver	•••	PW93*	2/6	
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BBC Special One-valver Short-Wave Two	•••	AW387*	2/6	
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Short-Wave World Beater	•••	AW436*	3/6	
Standard Four Valve S.W.		WM383*	3/6	
Enthusiast's Power Amplifier	• • •	WM387*	3/6	
Standard Four Valve	• • •	WM391*	3/6	
Listener's 5-Watt Amplifier	•···	WM392*	3/6	
TELEVISI	ON			
Argus Television Receiver	•••		3/	
Simplex Television Receiver	•••	<u> </u>	3/6	
QUERY CO			<u> </u>	
This coupon is available until 5th March, 1960 and must accompany all queries in accordance with the notice on our "Open to Discussion" page.				

PRACTICAL WIRELESS, MARCH, 1960

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-SERVICE-

PRACTICAL WIRELESS

March, 1960



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