## JUNE 1986



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## BACK NUMBERS

Some back issues published during the last six months are available from the Editorial Office at $£ 140$ inclusive of postage and packing. Address as above.

## QUERIES

We regret that we cannot answer technical queries over the telephone nor supply service sheets. We will endeavour to assist readers who have queries relating to articles published in Television, but we cannot offer advice on modifications to our published designs nor comment on alternative ways of using them. All correspondents expecting a reply should enclose a stamped addressed envelope.
Requests for advice on dealing with servicing problems should be directed to our Queries Service. For details see our regular feature "Service Bureau". Send to the address given above (see "correspondence").

## this month

485 Leader
486 Modern Receiver Circuitry, Part 3 J. LeJeune
-The way in which the signals at the output from the vision detector are separated and processed, including an account of the operation of a modern single-chip PAL decoder and a look at RGB output circuits.

## 488 Next Month in Television

489 Grundig's Satellite TV Receiver Steve Beeching, T. Eng. A preview of Grundig's approach to satellite TV reception.
490 Letters
494 Servicing the NordMende F10/F11 Chassis Christopher Holland This major European CTV chassis features some novel circuitry, specifically a step-up chopper power supply and a thyristor field output stage. An account of the operation of these circuits and guidance on fault finding.
498 Teletopics
News, comment and developments.
500 The Development of Colour Tubes, Part 1 Eugene Trundle
This initial instalment outlines the evolution of the
different types of colour tube from the earliest delta-gun type to the 45AX - via the Trinitron, PIL, 20AX and 30AX types.
504 Servicing Teletext Decoders, Part 5
Mike Phelan
How to go about fault finding, with specific reference to the initial Philips/Mullard chip set. Interpreting display errors and using an ASCII table to relate errors to data lines and memory locations. Notes on the effects of LSI chip faults.
510 VCR Clinic
Reports from Christopher Holland, Les Harris, Philip
Blundell, Eng. Tech., Steve Illidge and Mick Dutton.
512 LCD TVs from Citizen
How Citizen's pocket TV set produces a picture on its 18,000 pixel liquid-crystal display.
513 TV Fault Finding
Reports from Alan Shaw, Michael Dranfield and Philip
Blundell, Eng. Tech.
514 Long-distance Television
Roger Bunney
Reports on DX reception and conditions, news and a
review of the Fringe Electronics f.m. radio preamplifier.
517 Other things and other places Les Lawry-Johns
Les takes a break from TV matters and heads for far off
Dersingham - in a rather roundabout way.
518 Servicing Sinclair Microcomputers, Part 2
Ken Taylor
Complete circuit for the ZX81, along with a detailed
fault-finding procedure and data on chip pin conditions.
An easy way to get acquainted with microcomputer servicing techniques.
Service Bureau
524 Test Case 282

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## CAN YOU HELP?

A friend of ours requires a volume-on/ off knob and a turnlock-tuning knob for a Philips RM712 car radio. Can anyone supply these? Does anyone know the agents or a source of spares for Tensai TVs?

## CORRECTION

A correction to the c.r.t tester/booster circuit published last month appears on page 493.

## FRONT COVER

This month's cover photograph shows a close up of a test pattern displayed on the screen of a PIL type tube.

## More on Spares

No apologies for returning to the subject of spares so soon: it's likely to be an increasing headache for all concerned - setmakers, stockists, repairers and customers. Let's look at it first from the setmaker's point of view, prompted once more by Ferguson who have just announced that spares for the 14in. colour portable Model 3787 will no longer be supplied by them - nor will any repair work be undertaken. That's the popular little Movie Star portable fitted with a NordMende chassis, dating from the period in the early seventies when thryristor line output stages were all the rage amongst Continental setmakers.

The fact that these sets are now some ten years old highlights the problems. A setmaker of any size will have introduced a vast range of models over such a time scale. Just think of some of the permutations - different tube sizes and tuning arrangements, remote control, teletext and more recently stereo sound capability. Dealers and their customers expect to be able to order spares of every description: not just droppers, LOPTs and various safety specials but knobs that fall off and various bits of trim. Anything in fact that might be required to restore a set in for service to its original condition. This implies the need to stock thousands and thousands of different TV spare parts - spares also for a wide range of VCRs, radio and audio equipment. In terms of storage space and handling the costs involved are enormous. It's no use saying reorder when necessary from component manufacturers. They too alter their ranges, while the cost of ordering small quantities is prohibitively high even for the largest setmakers. Then there's the fact that many components are supplied to meet the specification for a particular model/chassis. We're thinking not just of safety components but of items shaped to fit particular PCB assemblies, cabinet mouldings and so on. There have been jokes in the past about computers running the show and part numbers as long as your arm: they just serve to emphasise the difficulties.

The vastly increased reliability of modern chassis hasn't helped in this respect. Cool running and low power consumption mean that sets can be expected to give years and years of service with comparatively few breakdowns. It's also a fact that a ten or fifteen year old set can still look quite new. But failures are inevitable from time to time and then the hassle starts. Just what is a fair time after which to put up the no longer available sign? Ten years sounds a nice round figure and seems to be the sort of time scale manufacturers now have in mind. After all if you've had ten years' service from a set you've not done badly, particularly in view of the modest initial price of consumer electronics equipment. But one has to admit that though this sounds reasonable it's not likely to assuage the customer who can't get his set repaired for want of some perhaps fairly minor item.
The repairer doesn't have to go back to the original maker for parts of course, though special items, whether to meet a safety requirement or an exacting performance specification - flyback tuning capacitors, the chopper and line output transistors used in some sets, and so on - are likely to cause problems. Increasingly, setmakers are farming out the supply of spares to specialist distributors. This ensures that spares are readily available around the country and has the advantage from the stockists point of view that he's not obliged to hold stocks of any and everything that might be required. He knows that a good range of tuners, LOPTs, triplers, droppers, electrolytics and transistors will meet the vast majority of calls for parts. Experience will provide a guide to what to stock for particular models and the independent distribulor has no obligation to search for an obscure item for an unusual set. For the most part repairers can, as they've always done, rely on various standard component lines. We hope that doesn't sound too complacent, being all too well aware of the frustrations that can arise when a customer can't be provided with the sort of service you aim to give.
When you come to think of it the service nowadays being provided by specialist component suppliers is remarkably cheap and efficient. While a setmaker buys components in bulk to feed to his computer-controlled production lines the stockist has to locate, pack, despatch and invoice items on an individual basis. It's amazing how they manage to do it and not surprising that a special screw, belt or plastic moulding can bring with it quite a hefty bill. This all reflects the incredibly tight costing that modern mass production brings with it: what costs the setmaker pennies must cost you pounds.
The problems all too lightly touched upon above are likely to involve us all in increasing problems of one sort or another. A year or so back some readers were contemplating the idea of providing computerised fault finding and data services, but no computer will solve the problem of the missing part. Anything for which there's an obvious need is likely to be made available by someone or other - think of the universal tripler and the solid-state PL802 for example. Alternatives for most electronic components could probably be found - if only one could lay hands on the original performance specification and they could be made to fit the bracket, board or other mounting requirement!

## INDEX TO VOLUME 35

Copies of the index to volume 35 (November 1984 - October 1985) of Television are now available from the editorial office at 75p each. The index includes full lists of VCR Clinic and TV Fault Finding items. Would readers please note that indexes are not available until approximately six months after the last issue concerned. We've already had a number of requests for the index to volume 36 - despite the fact that four issues have still to be written, prepared and printed . . .

# Modern Receiver Circuitry 

Part 3: Video Signal Processing

## J. LeJeune

The use of integrated circuits has enabled some sophisticated techniques to be adopted in TV receivers, techniques that might not have appeared had the use of discrete component circuitry continued. For a good few years now video signal processing in TV sets has been carried out in i.c. form: while RGB output chips have been devised, the advantage at the end of the video chain still lies with discrete component circuitry, due to the dissipation and high voltages involved.

## Filtering the Video Signal

The output obtained from the vision detector of a colour receiver consists of the baseband luminance signal $(50 \mathrm{~Hz}-5.5 \mathrm{MHz})$, the chrominance signal on its 4.43 MHz carrier with sidebands extending some $1 \cdot 1 \mathrm{MHz}$ on either side, and the 6 MHz intercarrier sound signal which is a beat frequency between the vision and sound i.f. carriers ( 39.5 MHz and $33 \cdot 5 \mathrm{MHz}$ ). We'll return to the sound signal in a later article. The chrominance subcarrier and its sidebands are interleaved with the upper luminance signal frequencies: because of the line structure of the TV picture, there are gaps in the luminance signal spectrum into which the chrominance signal is slotted.
The various components of the vision detector's output have to be separated for individual processing. Filtering arrangements vary from chassis to chassis but a typical way of going about this is shown in Fig. 1. The composite video signal is fed to the base of transistor Q1 via the bridged-T notch filter L3/C6/C7/R10 which removes the 6 MHz intercarrier sound signal. The chrominance signal feed is via $C 2$, the attenuator $R 8 / R 7$ and $C 4$ to the following signal processing i.c., with the series rejector circuit C3/L2 included to remove the l.f. video components - this arrangement is used in preference to a lossy bandpass acceptor circuit. C2 is of low value to contribute to the filtering. Q1 provides the sync and luminance feeds. It's made unresponsive to signals at the 4.43 MHz chroma subcarrier frequency by the inclusion of the parallel tuned circuit $\mathrm{L} 1 / \mathrm{C} 1$ in its emitter circuit: this introduces frequency selective negative feedback, reducing the stage gain at $4 \cdot 43 \mathrm{MHz}$. The unbypassed resistor R5 provides overall negative feedback - Q1 has low gain but good linearity and is primarily used as a buffer to prevent interaction between the sound and chroma subcarrier rejectors. Delay line DL1 is incorporated in the luminance signal path to compensate for the different bandwidths of the chrominance and luminance signal circuits.

## Luminance-chroma Processing Chip

Today's sets generally use a single chip to process both the chrominance and luminance signals. A good example of this type of i.c. is the Mullard TDA3560. Fig. 2 shows a block diagram of this widely used i.c.

Processing of the luminance signal is straightforward: amplification with d.c. clamping to restore the correct conditions following a.c. coupling ( C 5 , Fig. 1), d.c. contrast control, then matrixing with the colour-difference
signals to provide $R, G$ and $B$ signals for the output stages.

Before we look at the processing of the chrominance signal let's just recap on its composition. Two colourdifference signals, $B-Y$ and $R-Y$, are transmitted. At the transmitter these signals amplitude modulate two 4.43 MHz subcarriers which have a phase difference of $90^{\circ}$ - this means that when one subcarrier is at its peak the other is at zero. The two signals are then added to give the composite chroma signal - the technique is known as quadrature amplitude modulation. There's further complication with the PAL system since the phase of the R Y signal is shifted by $180^{\circ}$ on alternate lines. About ten cycles of 4.43 MHz subcarrier (the colour burst) are transmitted during the post line sync pulse back porch period to act as a reference for the decoding process. The only modulation on this carrier is the $180^{\circ}$ PAL signal swings, as a result of which the phase of the burst swings $\pm 45^{\circ}$ on alternate lines.

Within the TDA3560 the chroma signal is fed first to a gain-controlled amplifier (a.c.c. - automatic chrominance control). The control potential is obtained by rectifying the colour burst since this is not amplitude modulated. The burst signal has to be separated from the chroma signal for this purpose: this is done by using a suitably timed line pulse to open a gate. The separated burst signal is also applied to a phase detector which is part of a phase locked loop controlling the phase and frequency of a reference oscillator. In earlier decoders this oscillator operated at 4.43 MHz : for reasons that will become clear shortly in the TDA3560 and similar chips the frequency is 8.86 MHz .
Returning to the chroma channel itself, the signal is next subjected to saturation and contrast control - the latter so that the correct luminance to chroma ratio is maintained. The control stage is gated by the burst gate pulse so that operation of the contrast and saturation controls does not affect the amplitude of the burst. The chroma signal then leaves the i.c. for application to the delay line circuit which serves two purposes: it separates the $B-Y$ and $R-Y$ components of the signal and, by averaging the signal over pairs of lines, converts any phase error to slight desaturation. The separated signals are then


Fig. 1: Separating the outputs from the vision detector.


Fig. 2: Block diagram of the TDA3560 luminance and chroma signal processing chip.
applied to two synchronous demodulators. These require inputs from the reference oscillator, which takes us back to the a.p.c. loop.

The main purpose of the colour burst is to synchronise the reference oscillator which drives the synchronous demodulators. These operate on the sample-and-hold principle, sampling the modulated colour-difference signals at the peaks of the carriers to detect their amplitudes. The reference signal drives to the demodulators must have a phase difference of $90^{\circ}$ - the same as the original carriers at the transmitter. In earlier decoders this was achieved by incorporating a $90^{\circ}$ phase shift network in one of the reference signal feeds. The use of an 8.86 MHz oscillator avoids the need for this and provides more accurate results: its output is fed to two flip-flops which provide


Fig. 3: Obtaining quadrature reference signals to drive the $R$ - Y and B - Y demodulators by using two flipflops to divide by two the output from an 8.86 MHz oscillator. FF2 is positive-going edge triggered to produce an in-phase $4 \cdot 43 \mathrm{MHz}$ signal; FF1 is negative-edge triggered to produce a signal with a $90^{\circ}$ phase difference.


Fig. 4: Principle of the chroma delay line circuit.
division by two. By taking opposite polarity outputs from the flip-flops two drive signals with an exact $90^{\circ}$ phase difference are obtained. See Fig. 3.

It's also necessary to invert the drive to the $\mathrm{R}-\mathrm{Y}$ demodulator on alternate lines to counter the effect of the $180^{\circ}$ switching at the transmitter. This must be synchronised with the switching at the transmitter. The burst swings provide an identification signal for this purpose: the 7.8 kHz (half line frequency) ident signal synchronises the PAL switch (inverter) which is driven by line frequency pulses.

The presence of the burst/ident signals is a convenient way of establishing that the transmission is a colour rather than a monochrome one. No burst means no colour: the colour-killer then switches off the chroma delay line driver stage. If this is not done the a.c.c. circuit will operate the chroma amplifier at maximum gain and the monochrome display will be marred by colour noise.

Fig. 4 shows the operation of the delay line circuit. The composite chroma signal is fed directly and via the oneline duration delay line to add and subtract networks. Because of the $R-Y$ signal inversion ( $180^{\circ}$ shift) on alternate lines the $\mathrm{R}-\mathrm{Y}$ signal cancels out in the adder circuit while the $B-Y$ signal cancels out in the subtract circuit.

## Matrixing and Data Insertion

The third colour-difference signal $(G-Y)$ is obtained by matrixing the demodulated $\mathrm{R}-\mathrm{Y}$ and $\mathrm{B}-\mathrm{Y}$ signals. The luminance signal is then added to obtain RGB signals. These pass to the data insertion circuit which consists of three fast electronic changeover switches - they can operate at 10 MHz . The state of all three switches is controlled by the voltage at the insertion control pin 1.5 V at this pin changes the switches from off-air RGB to external inputs, the mode generally used for teletext. For mix-mode teletext a monochrome version of the text is fed

## next month in



## - SERVICING THE PANASONIC NV7000

Though a fairly early VCR, dating from 1981-2, this machine was of advanced design. It had directdrive motors, Dolby noise reduction, full cable remote control, slow motion and back-space edits. David Botto has handled large numbers of these machines and provides servicing notes and advice based on this experience.

## - COLOUR TUBE DEVELOPMENTS

Eugene Trundle continues his series with a detailed look at colour tube electron gun technology and the developments that have taken place in this area over the years. Just about everything has changed, from the heaters to the electron lens arrangements. Tube neck magnet systems are also considered: did you know why a combination of two-, four- and six-pole magnets is required?

## - MODERN RECEIVER CIRCUITRY

The line output stage, which does so much more than just provide horizontal scanning, has always been a bit of a mystery to those not versed in TV technology. The need for EW modulation with $110^{\circ}$ tubes has further complicated matters. Tuning is a key to line output stage operation but more than one frequency is involved - the line scan, flyback and harmonic frequencies in fact. J. LeJeune provides an account of the various things that go on in the line output stage.

## - SERVICING SÖNATELMR MONO PORTABLES

Sonatel monochrome portables were distributed by House of Carmen and were amongst the first to break the $£ 50$ price barrier. They were widely sold through the big retail chains and via mail order catalogues. When House of Carmen took over Morphy Richards the sets were sold under this well known brand name. Ian Rees provides detailed information on common faults and how to deal with them, also on adding a.g.c. to some models.

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Fig. 5: How long video leads and a tube's input capacitance form a low-pass filter that attenuates h.f. components of the signal.


Fig. 6: Basic class $A B$ video output circuit.


Fig. 7: Video output circuit used in the Thorn TX100 chassis.
to the insertion control pin. From the data insertion section the RGB video signals pass to the i.c.'s output stages where line and field flyback blanking is carried out.

## Video Output Circuits

The external RGB output stages drive the tube's cathodes. For optimum results the tube's heater-cathode and cathode-grid capacitances must be charged and discharged in the shortest possible time. It helps to mount the RGB output stages on the tube base panel. This eliminates the long leads otherwise required - these long leads, in conjunction with the tube's input capacitances, form lowpass filters that affect the set's h.f. performance - see Fig. 5.

The problem with a simple class A output stage of the type shown in Fig. 5 is that while the tube's input capacitance is quickly discharged on a negative-going signal transition, when the output transistor is rapidly driven to saturation, on a positive-going transition when the transistor is switched off the capacitance has to charge via the load resistor, which is typically about $12 \mathrm{k} \Omega$ in
value. Class AB output stages are favoured as a way of overcoming this disadvantage. Fig. 6 shows the basic circuit. Adding the emitter-follower transistor Tr2 in Tr1's collector circuit provides a method of rapidly charging the tube's input capacitance on positive-going transitions. Another advantage of the circuit is reduced dissipation.

Fig. 7 shows one of the RGB output stages used in the Thorn TX100 chassis. The pnp transistor Tr 60 is used to hold the emitters of all three output transistors at 2.5 V . Video from the chroma-luminance processing i.c. is applied to the base of the output transistor Tr65 via RV63: negative feedback via R609 sets the gain of the amplifier and stabilises the d.c. operating conditions. No adjustment of the grey-scale black level is required because the stage is designed to operate with the later TDA3562A
processor i.c. which incorporates automatic black-level control. If such adjustment was required, R610 could be made variable. Tr65 provides a peak-to-peak drive of 150 V at the base of the emitter-follower transistor Tr69. Up to this point the circuit follows a similar arrangement to that shown in Fig. 6. The final transistor Tr66 serves a dual function. It provides signal coupling to the tube via its base-emitter junction, acting as an emitter-follower on negative-going transitions - diode D603 provides coupling on positive-going transitions. The other function is to provide feedback from its collector to the beam current sensing (in the TDA3562A chip) and beam limiting circuits. The feedback to the chip is part of the black-level correction system. The power consumption of the stage is around 600 mV .

## Grundig's Satellite TV Receiver

Steve Beeching, T. Eng.

Grundig will be launching a new satellite TV receiver during the May trade shows in London. I was pleased to be present at a prelaunch appraisal with a friend of mine who has already looked at a number of satellite receiver systems.

The receiving dish was pointed at Eutelsat-1 F1 (ECS-1). Various programmes are available from this satellite. All were very well received - with the exception of scrambled transmissions for which at the time decoders had not been made available.

The main television set was a Grundig Model M70 with a 28 in. FS tube and a CTI decoder - this is an automatic PAL/NTSC/Secam decoder with a variable luminance delay line for correct luminance-chrominance registration (to put the red back on top of the snooker balls).

The pictures from the Italian channel RAI were stunning - not only because of the scantily clad ladies running about but also due to the shots being live from the studio and the wide TV bandwidth being used.

The satellite receiver itself is the size of a midi hi-fi unit $-320 \times 70 \times 270 \mathrm{~mm}$ - which is quite compact. It's a 29 station programmable receiver with the capability to tune each programme through the full $950-1,750 \mathrm{MHz}$ bandwidth in 99 channel steps. Channel selection is by means of an IR remote control unit.

The range of controls and inputs is comprehensive. There are two dish aerial inputs at the rear, X and Y . While the inputs can be from separate dishes the intended use is with a dual head end at the dish, i.e. a dish with two low-noise converters fitted, one for vertical and the other for horizontal signal polarisation. Selection of either is programmable via each input.

There are two scart connectors and a six-pin AV DIN socket. One scart socket is for use with a VCR and the other for connection to the main TV set (with the AV DIN socket as an alternative). Through connection via a relay is available when the satellite receiver is off. When in operation the VCR can record the channel currently being received: so you can watch a terrestrial programme (BBC-1, ITV etc.) on the main TV set while recording a satellite TV broadcast.

The low-noise converters at the dish are each fed with 15 V at 250 mA via the connecting cables: the power supply to them can be switched off by a small switch at the rear -of the unit. There's also a switch to select only input X in
the event of a single low-noise converter being used.
The unit uses a standard VCR type modulator and combiner amplifier - there's an audio level preset mounted below the modulator. The terrestrial TV aerial can be plugged in and the output next to it connected to any standard u.h.f. TV set. The additional satellite TV outputs are modulated on to u.h.f. channels in the region ch. 31-39, adjustable. We found that the modulator was good enough to be able to decode Italian teletext on a standard receiver.

There's a four-state voltage output for dish switching: 0 V dish 1 , horizontal; 3 V dish 1 , vertical; 6 V dish 2 , horizontal; 9 V dish 2 , vertical. The switching is done at the head end by h.f. relays.

Each programme (1-29) can be set not only to the required satellite channel (1-99) but also for input X or Y , for de-emphasis d1 or d2 and for deviation h1 or h2. The inputs from the low-noise converters are in the band 950 $1,750 \mathrm{MHz}$ (first i.f.). X or Y input selection is by switching voltages of +5 V or -5 V to bias on or off two pin diodes in the signal paths. After signal selection an a.g.c. stage caters for a range of between $47 \mathrm{~dB} / \mu \mathrm{V}$ to $75 \mathrm{~dB} / \mu \mathrm{V}$. A second mixer then produces an output at 480 MHz which, after two stages of i.f. amplification, is converted to baseband video by the f.m. demodulator. An a.f.c. output is fed to the microcomputer as a reference: the tuning is microcomputer controlled, using a phase-locked loop synthesiser. The input to the loop is from the local oscillator and the frequency of operation is set by the microcomputer: tuning drift is thereby eliminated, the range of control being sufficient to accommodate any drift in the low-noise converters.

The sound circuit caters for carriers at 4.5 MHz or in the range $6-7 \mathrm{MHz}$. A wideband phase-locked loop is used. Any channel can be set for 4.5 MHz or 6.5 MHz and stored in the memory. The 6.5 MHz carrier can be in the range 6 6.5 MHz : the phase-locked loop is arranged to demodulate within these limits without need for adjustment. The carrier is mixed to produce a $10 \cdot 7 \mathrm{MHz}$ sound i.f. signal which is demodulated by a standard TBA120 chip with an error signal fed back to the mixer - all this path is within the PLL.

The ECS-1 satellite at present carries eleven channels. Two of these are on east spot beams and were thus very faint, two were scrambled and the others were received
with excellent pictures - albeit a 2 m dish was being used. No adjustments to the TV set or the satellite receiver were necessary - reception of the whole band was simply by changing channels via the remote control unit. Different signal polarisation, de-emphasis, sound carriers and colour systems were all taken care of. My friend remarked how good it was - and he's not easily impressed.

## Letters

## WHY NO TEST CARDS?

Despite following the normal TV engineer's traditionally moderate line, after the events this week I really feel it's time to put pen to paper in a letter of complaint to the broadcasting authorities. I hope it will in no small way be supported by your good selves and the majority of Television's readers. In a nutshell, where have all our test cards gone? Since their disappearance from the BBC channels in what seems an age ago I've noticed little complaint or comment in these pages. Why hasn't anyone questioned the need for two channels of text consisting of repeated information every ten minutes or so on most days of the week? Apart from the occasional "glimpse" on Channel 4 it seems that test cards are now considered to be pointless.
Anyone involved in front line servicing will know this situation is far from ideal. At the time of writing a typical morning's programmes consist of BBC-1 text, BBC-2 text, ITV black-and-white film, Ch. 4 text. This situation doesn't allow the engineer let alone the customer evaluate the performance of a TV set or VCR.
So please BBC reconsider your policy and bring back our Effy at least on one channel. A display even every half hour would help, but please don't consider her redundant. I and many other engineers will tell you that this is far from the truth.
Keith Lane,
Southsea, Portsmouth.
Editorial comment: Whenever this comes up the broadcasting authorities tend to comment that it's not their job to provide a pattern generator that's expensive in terms of power consumption. But a portable pattern generator doesn't allow the complete transmission path to be assessed. There seems to be no reason why the broadcasters shouldn't oblige the trade in the way suggested: the present situation is unsatisfactory indeed.

## TELETEXT TROUBLES

I have some further news concerning XM11 teletext decoder problems. Suddenly, about three weeks before Easter, the problem I'd had with missing rows of data on BBC-2 vanished. Text has been fine on this channel ever since. The period of malfunction was about three months. A problem with ITV text, i.e. not getting it right first time, still comes and goes but I've now noticed that this occurs only with networked information - locally generated text from TVS is always right first time. Throughout this period of difficulty BBC-1 and Ch. 4 text have always been o.k.
So what can I conclude from this? First I don't believe anything has changed locally, neither do I think the receiver was ever suspect. The broadcasters assured me
that everything was o.k. at their end, which prompted me to look into the possibility that something might be wrong at my end. I believe, from what I've heard, that the XM11 may be less tolerant of variations in transmission parameters than later designs. I feel that this is the root of the problem, even though the broadcasters would deny it.
The original fault showed every fourth row missing. Later this changed to every fifth row, before the problem disappeared altogether. Perhaps something changed as a result of a three-monthly maintenance schedule somewhere. I doubt whether l'll ever find positive proof of my suspicions and will just have to be thankful that the fault has gone away.

## Keith Cummins,

Southampton.

## MICROCOMPUTER FAULTS

Further to my letter in the March issue, here's some more information on microcomputer faults.
The Sinclair Spectrum's power supply seems to be responsible for a number of faults. The main item that fails is, as I stated, a ZTX450 transistor (TR4). On later versions of the board it's a ZTX650. TR5 (ZTX213), diode D15, the 7805 regulator chip and even the inductor itself have been known to fail. With all these failures there's no buzzing noise from the inductor. A screen full of horizontal black-and-white lines can be caused by failure of the Z80A microprocessor chip or the ROM. These components should be available from advertisers in the pages of Sinclair User magazine.
The BBC computer has a strip of stiff conductors that link the keyboard to the main board. Repeated movement of this strip due to the addition of ROMs to the expansion sockets located beneath the keyboard can lead to failure of areas of the keyboard.
VIC20 computers have given us the following faults. Every other numeral not working ( 1 o.k., $2 \mathrm{w} / \mathrm{s}$ etc.): the 6522A chip in position UBA1 faulty. Poor or no colour: suspect the modulator or the Commodore chip. Intermittent loss of picture at switch-on: the 7402 chip in position UB9 sensitive.
G. Jackson,

Hyde, Cheshire.

## COMMODORE 64 TIP

Problems with home computers have been featured in recent issues. Here's one relating to the Commodore 64. It may save other readers a small fortune. The trouble is loading problems, with the computer not waiting for the play key to be pressed before going into the play or save mode. The I/O port for the cassette unit is in the 6510 CPU, along with the data direction registers. If you type in this one-line program:
10 print peek (1): GOTO 10
the computer should, if working properly and with no cassette keys depressed, respond with a solid row of 55 s . What you're more likely to see is a row of continuously changing numbers. Obviously something weird and wonderful is going on inside the chip. Next shock, phone Commodore and ask the price of a replacement chip: twenty four pounds!
A small modification (bodge) has so far proved very successful however. R1 ( $3 \cdot 3 \mathrm{k} \Omega$ ) is connected to pin 25 of the chip: it's a pull-up resistor connected to the cassette sense line. Wire a $47 \mathrm{k} \Omega$ preset in series with this resistor

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and adjust it until the row numbers stabilise at 55 (again all cassette keys up). The trick is also worth knowing since with many 64 s this 40 -pin chip is soldered in. It not only saves a fortune in chip, also a fortune in solder!
D.C.J. Tilley,

London E2.

## RC HANDSET CHECK

Here's a tip I've been using for the past three years when servicing remote control handsets. If you have a suspect handset in a customer's house and would like to check that it's the unit and not the TV set take a radio - if you have a car radio this will do - and tune it to an MW station with no modulation. Press the buttons on the handset: if the unit is working you'll hear a whistle as you do so. If you use a car radio the handset must be near the aerial.
William G. Lockitt, Eng. Tech.,
Rhyl, Clwyd.

## GRUNDIG SPARES

In the April Service Bureau column two possibilities were given for the problem of increasing sound with the Grundig 6010TD. These answers (manual control paddleswitches becoming leaky or a faulty SB2 memory module) were absolutely correct. You went on to say however that spares for these 13-14 year old sets are becoming difficult to obtain.

Well, a quick phone call to Grundig, using the number given in your TV/VCR spares guide, revealed that both the paddle-switch (part no. 29501.110.01) and the SB2 memory module (correct part no. $9.47041,1101$ ) are available ex stock, as is the complete remote control receiver module (part no. 29301.012.01) for those who need the "module exchange" repair system.

Alternatively anyone requiring Grundig TV parts would be pleasantly surprised if he consulted your classified advertisement columns. Our company has had a small but regular advertisement for a number of years. We can supply any part for the 6010 and have a fairly comprehensive module exchange scheme for many sets from 1970 to the current chassis.

Grundig thyristor line timebase sets such as the 6010 tend to lead a healthy existence, with excellent colour, superb picture and decent sound - provided they are carefully treated for the dry-joint syndrome at intervals of about five years. They are far too good to pension off in the prime of life because of fears of scarce spares.
Les Austin, Ochre Mill Technical Services Ltd.,
Lower Moddershall, Stone, Staffs.

## CRT BOOSTER CORRECTION



Please note an error in the simple c.r.t. booster/tester circuit shown in my article last month. The

Fig. 1: Correction to the simple c.r.t. tester/booster circuit featured last month (see page 450). An extra pole on S1 switches off the first anode supply in the boost position.
'boost/test switch S1 should be a three-pole two-way switch, the third pole removing the 90 V supply to the first anodes during reactivation (see Fig. 1).
Jim Littler,
Wigan, Lancs.

## HITACHI NP81CO CHASSIS

In the April TV Fault Finding column fellow sufferer Les Grogan mentioned top cramp on these sets due to C608 going open-circuit. We've also had this fault. Another top cramp fault in this chassis and in the CPT2051 (not the E variety) also produces gross nonlinearity in the middle part of the raster. This is due to $\mathrm{R} 614(150 \mathrm{k} \Omega)$ in the feedback network going open-circuit - a clue is given by the fact that the collector voltage of the top field output transistor is far too high. In one chassis (which one I forget) the set will be left tripping due to the guard circuit if R614 is removed to see whether this leaves the fault unchanged. Some chassis in this family use what looks like a half-watt job which usually doesn't fail: other sets use smaller resistors which do fail.

## J.R. Armagh,

Portadown, Craigavon.

## NORDMENDE FV/SK2 CHASSIS

I've had a couple of these sets in for repair lately. My patience was more than severely tried during the hours spent fixing them: perhaps some of the faults and symptoms may be of interest to others.
(1) Barrel distortion, i.e. bowing in from both sides. The trouble is in the EW modulator panel P. Check for open-circuits in resistor RP36 ( $1 \Omega$ safety type), coil LP30 or the EW modulator driver transistor TP04 (BD544B or 2N6107). The transistor has to be one of these two types. I tried several similar silicon pnp power transistors but they all broke down after a short period, taking the safety resistor with them. (Editor's note: some sets have a fuse in the RP36 position.)
(2) Dead set. This had me for a long time until eventually the second set came in and I was able to do some panel swapping. I'd originally thought that the trouble lay in the thyristor line output module U and had taken out every thyristor and tested it, all to no avail. The set just sat there dead until the horizontal line generator module Z was swapped. In went a new TDA2590 i.c. and the set sprang to life. I gritted my teeth.
(3) After a few minutes the set would lose tuning with jumping neons and hum on the field scan. Tapping hard in the bottom right-hand corner of the main PCB (track side) would restore normal operation for a few minutes. I eventually found that $\mathrm{CA} 30(2,200 \mu \mathrm{~F})$, the 36 V supply reservoir capacitor, was coming adrift - the ring making contact for the negative side of the capacitor had parted from the main body.
(4) Touch tuning trouble with intermittent and jumping tuning (neons varying) was inevitably the SAS580/SAS590 pair. Correct tuning was obtained when these i.c.s were replaced.

It seems that the NordMende SK2 chassis is reliable but tricky to repair if you're not familiar with the circuitry Both the faulty sets have now been working normally for some time, fortunately. Ploughing through has given me the confidence to work on the chassis again!
Des Walsh
Carrigaline, Co. Cork.

# Servicing the NordMende F10/F11 Chassis 

Christopher Holland

Despite its prominence in several West European markets the NordMende brand name has made relatively little impact in the UK, though NordMende chassis have appeared in sets sold with other names on the cabinet most notably the Ferguson 3787 colour portable. This lack of market impact has not been helped by the fact that different firms have acted as importers/agents at various times. In addition NordMende TV sets have traditionally been v.h.f./u.h.f. receivers, which means extra complication and cost in the UK market. NordMende is a leading brand in Ireland however and it's interesting that their colour chassis have always been at the forefront of TV receiver technology - some of the circuit techniques used in these chassis will be new to many TV technicians.

## Chassis Specification

The F10/11 series chassis have been in production since 1981. They are to be found in other makes of set, notably Thomson and Saba. Hitachi have also used the F11 chassis in some of their sets for markets where v.h.f./u.h.f. receivers are required. The design brief was to produce an international chassis with a single mother board on to which colour decoder, tuner and sound decoder panels could be fitted to suit the requirements of individual countries. Remote control sets can be converted for teletext use by fitting the relevant panel. All sets have a scart socket for direct connection of composite video, RGB or audio signals.

The F10 chassis was designed for use with $90^{\circ}$ tubes in sizes from 14 to 22 in., the F11 for $110^{\circ}$ tubes in sizes from 20 to 27in. The F11 thus requires a higher output from its power supply and an EW correction circuit. Otherwise it's essentially the same as the F10. There's a later version of the F11, the F11B: more on this later.

The notes in this article will be based on the F10 chassis, with F11 chassis differences noted in brackets as they arise. Most of the circuitry is fairly conventional, particularly the signal stages, and can be quite easily understood by referring to the appropriate circuit diagram. The only areas where these chassis vary greatly from normal practice are in the power supply and field output stages. We'll look at these in greater detail.

## Power Supply Circuit

The power supply is of the step-up chopper type: the voltage level supplied to the chopper circuit by a mains transformer and bridge rectifier is raised to and stabilised at a level suitable for the line output stage which then produces other d.c. lines. Line flyback pulses provide the necessary switching. The principle of the chopper arrangement is shown in Fig. 1: the complete circuit is shown in Fig. 2.

The bridge rectifier delivers a d.c. level of 80 V (F11 100 V ) to coil LP01. When the chopper transistor TP01 is switched on current flows through the transistor and this coil. Consequently energy builds up in the coil in the form of an electromagnetic field. When the chopper transistor is switched off by a flyback pulse from the line output
transformer the voltage at its collector will swing positively due to the collapsing field around LP01. This positivegoing pulse is rectified by DP14 which charges CP14 to produce the 109 V h.t. line (F11-140V). As is usual with W. German sets, this is referred to as the U1 rail. Note that the h.t. obtained in this way results from a combination of the $80 \mathrm{~V}(100 \mathrm{~V})$ d.c. supply and the switching action of TP01.

The centre-tapped secondary winding on the mains transformer supplies a bridge rectifier which provides a 24 V line (F11-31V) to power the audio output stage. The centre-tap is used to provide an 11.5 V line for startup purposes. This feeds the emitter of TP21 via diodes DP21, DP24 and DP03, with a chassis return via RP26, RP24 and RP21. The current flowing through RP26 develops a voltage to switch TP21 on, as a result of which CP10 charges via DP12. This line starts up the TDA1950 sync/line oscillator chip via RP27. During the start-up period the collector of the line driver transistor TL01 is fed from the centre tap via DP13. Once the line output stage comes into operation a line output transformer derived 13 V supply takes over from the 11.5 V line, via diode DP15. RP25 is included in series with CP10 to provide a slow-start action.

When CP10 has charged sufficiently transistor TP05 will switch on, charging CP12 via RP23. The positive-going voltage developed across CP12 will eventually switch on TP06, and in turn TP02 and the chopper transistor TP01 will switch on. Positive-going line flyback pulses are fed to the base of TP04, which is thus switched on once per line scan, discharging CP12. Drive to the chopper transistor is thus provided by the sawtooth waveform generated across CP12. The charging of CP12 is controlled by TP05 whose base samples the h.t. voltage whilst its emitter is held at a constant voltage by zener diode DP20 and DP19. Regulation is thus achieved since TP01's switch-on time is determined by the conduction of TP05: TP01 is switched off by negative-going line flyback pulses which are applied to its base via diodes DP43 and DP42. Note that this power supply arrangement is very tolerant of varying mains supply voltages. The mains level is monitored via the 11 V start-up tap on the mains transformer: diodes DP21, DP24, DP03 and resistor RP07 provide a d.c. bias at the base of TP04 proportional to the level of the mains


Fig. 1: Principle of the step-up power supply. (a) Chopper transistor on. (b) Chopper transistor off. (c) Waveform at the collector of TPO1.

input. The line flyback pulses thus switch TP04 on sooner or later as the mains input is varied over the range 150 260 V .

There are a couple of other points to note in this power supply. First, in remote control sets TP21 is used to switch the set to the standby condition: in this condition resistor RP21 is not connected to chassis, so there's no voltage developed across RP26 and TP21 is switched off.

Secondly, transistor TP18 and zener diode DP18 provide excess voltage protection. The emitter of TP18 monitors the line output transformer derived 21 V supply: should this rise above about 24 V TP18 switches on and diode DP25 conducts. TP21 then switches off, removing the supply to the TDA1950 i.c. with the result that the line timebase closes down.

## The Field Timebase

The field output stage uses a form of pulse-width modulation with a thyristor for the switching. It has great reserve of amplitude, which enables essentially the same circuit to be used with tubes from 14 to 27 in . It also uses very little energy as the output switching is carried out at line frequency - note that no heatsinks are required.

The complete field timebase circuit is shown in Fig. 3. Field sync pulses from the TDA1950 sync/line oscillator i.c. are inverted by transistor TF02 and applied to the base of TF04. The field sawtooth waveform is produced by the charging circuit RF12/CF04: when the voltage across CF04 exceeds that at the slider of the hold control TF04/03 switch on to discharge CF04, producing the flyback. Transistors TF05 and TF09 simply act as amplifiers for the field sawtooth waveform, which appears inverted (nega-tive-going) at the collector of TF06. Line pulses via DF06 and RF13 are added to this waveform. The result of adding these two waveforms is to produce a form of pulsewidth modulation at the base of TF07 (see Fig. 4). TF07 in turn triggers thyristor DF08. When DF08 conducts, current flows via the thyristor, coil LP01, winding 4-7 on
the diode-split line output transformer, the field scan coils and resistor RF21 to the U3 line. CF10 with the inductive components form a filter to integrate the pulse waveform. DF08 is switched off by the negative-going line flyback pulses applied to its anode by winding 4-7 on the line output transformer. DF09 is incorporated to ground the circuit during the field flyback. The power consumption is low since DF08 switches on for relatively short intervals of time.

## Later Chassis

As mentioned earlier, the F11 $110^{\circ}$ chassis has been superseded by the F11B. The basic changes are that a different EW correction i.c. is used (a TDA4950 instead of a TDA4610) while much of the circuitry is now incorporated in a TEA2026 i.c. This device contains the line oscillator, the field timebase with the exception of the thyristor and the step-up chopper power supply circuit with the exceptior of the chopper transistor itself. The i.c. uses a 500 kHz crystal oscillator with internal divider circuits, eliminating the need for line and field hold controls. If the chassis is fitted with a PAL/NTSC decoder panel in place of the standard PAL panel the presence of an incoming NTSC signal will be detected and the field frequency will be automatically switched to 60 Hz .

In addition to the new version of the $110^{\circ}$ chassis, the F10 is being replaced by the F12 for non-remote control 14in. sets and the F14 for remote control sets with 14-20in. tubes. Also the $\mathbb{F} 15$ was introduced recently, designed with the new generation of square tubes in mind. No F13 chassis you'll notice: I never realised before that the Germans are superstitious!

## Servicing Aspects

As with other modern TV chassis designs the reliability of these sets is good. Stock faults are not something one can list. A few faults have occurred on several occasions
however and the following notes should prove helpful.
Any line output stage problems that cause the d.c. supplies derived from the line output transformer to rise in value will result in TP18 conducting, thus switching off the line oscillator via TP21. In this condition the full U1 value of $109 \mathrm{~V}(\mathrm{~F} 11-140 \mathrm{~V})$ is not developed due to the absence of line pulses. As there's no load on the power supply the U8 80 V supply will rise to almost 90 V . Note also that if there's a power supply fault that prevents the step-up switching taking place, e.g. transistor TP01 opencircuit, the 80 V present on the U1 line is enough to allow the line output stage to operate. The result is a small raster with a severe hum bar. These symptoms are a sure sign that the line timebase is operating correctly and that the fault is in the power supply.

## Fault Notes

The following is a comprehensive list of the problems most likely to be encountered when working on sets fitted with these chassis.
Set dead, fuse FP02 blown: Check whether the chopper transistor TP01 is short-circuit. If it has to be replaced, check the other transistors in the power supply and resistor RP06 before switching on. A short-circuit line output transistor will also blow this fuse (the F10 chassis uses a BU208D, the F11 a standard BU208 and the F11B a BU508AV).
Set dead, fuse FP02 intact: Check for 80-90V (F11 100110 V ) at the collector of the line output transistor. If absent check for broken tracks around the diode-split line output transformer - it's heavy and in early sets the PCB was not very well supported in this area. Check for 11 V at the collector of the line driver transistor TL01. If there are no line pulses at pin 2 of the TDA1950 chip IL01 check the d.c. level at pin 14 . This is normally 12 V but 8 V will enable the line oscillator to start up. The start-up voltage is obtained from the 11 V tap on the mains transformer via transistor TP21. If sufficient voltage is present at pin 14 but there's no output at pin 2, change the i.c.
Set dead, remote control models: Check whether transistor TP21 is being switched off by the front remote control decoder panel. If so, suspect the 400 kHz crystal first with microcomputer controlled systems.
Set puising on/off: Remove the field scan coil plug (connector BF01). If the set now starts up with field collapse there's no field sawtooth for modulation by the line flyback pulses so the line output stage is being loaded down. Check resistors RF12 and RF15 followed by the transistors in the field timebase. The culprit could also be thyristor DF08 loading the line output stage via winding $4-7$ on the transformer.

If the set continues to pulse with the field scan coils disconnected check resistor RP11 in the power supply. If this is open-circuit the h.t. line will be too high. The supplies derived from the line output transformer will also be too high with the result that transistor TP18 will switch on. A fault of this type can be seen by monitoring the U1 line with an analogue meter: the voltage will flick between $80-130 \mathrm{~V}$ as the set pulses on and off (F11-100-160V). If the power supply appears to be all right check for something in the line output stage causing TP18 to operate the trip circuit. The line output stage can be checked by disconnecting the base of the chopper transistor TP01: if the set now starts up, albeit with a reduced raster size and a hum bar, the line output stage is all right. Line tearing with excessive h.t. ripple: Check the U8
supply reservoir capacitor CP11 - it could be dry-jointed. Also check CP12.
Field collapse: The usual field collapse symptom of a thin horizontal line across the centre of the screen is not often encountered with the type of circuit used in these chassis. If experienced check for something open-circuit between the anode of thyristor DF08 and the field scan coils via coil LP01 - this coil is a separate winding on the same former as the coil used in the switch-mode power supply and the PCB tracks to its pins should be checked.
Picture shifted upwards, with field roll: This is the most common field fault with these sets: it's caused by transistor TF09's d.c. biasing being incorrect. Check RL52 (15 $\Omega$ - this is the U3 supply surge limiter resistor), RF20, RF21 and RF10, also the height preset control PF02. In earlier chassis PF02 was a $100 \Omega$ preset: it was changed to $47 \Omega$ with a fixed $47 \Omega$ resistor in series.

The transistors used in the field timebase seldom give trouble: unfortunately when they do they often appear to be good when checked with an ohmmeter, so substitution is the only effective test.
Uncontrollable field roll: Check transistor TF02 and capacitor CF01.
No raster except for a wide horizontal band near the bottom of the screen: Check whether the U4 (200V) supply surge limiter resistor RL51 (39 ) is open-circuit.
E.H.T. but no raster: Check RL54 if the tube's heaters are out. If the tube's first anode voltage is absent or low (should be $350-400 \mathrm{~V}$ ) check the adjustment of the lower preset on the diode-split line output transformer: if adjustment is not possible the transformer will have to be replaced. Otherwise check transistor TV81 (BC557B) and resistor RV82 (10 2 ) on the tube base panel. Note that a fault in any of the three RGB output stages on the tube base panel can cause the TDA3506 RGB matrixing i.c. IV02 to cut off all three guns, thus giving a blank raster.
Excessively bright raster with flyback lines and no luminance: Check for excessive first anode voltage. If this cannot be adjusted, or adjusts to the correct level then drifts again, replace the diode-split line output transformer. This fault can also be caused by failure of the TDA3506 RGB matrixing i.c. IV02: first check whether its d.c. supply resistor RV23 (10 2 ) is open-circuit. In the unlikely event of IV02 failing after replacement check whether CV91 $(0.001 \mu \mathrm{~F})$ on the tube base panel is shortcircuit.
One primary colour weak: Check CV38, CV39 or CV40 $(0.68 \mu \mathrm{~F})$ associated with the TDA3506 chip as appropriate. Could also be caused by the chip itself.
Excess of one primary colour: Check CV47, CV48 or CV49 $(0.022 \mu \mathrm{~F})$ associated with the TDA3506 i.c. as appropriate.
No colour: Suspect the 4.43 MHz crystal QC02 or the AN5620X colour decoder chip IC01 on the PAL decoder panel. If the positive-going line flyback pulses are missing at pin 7 of this i.c. check transistor TL41 (BC548B).
Raster but no noise spots: Suspect the combined tuner/i.f. block which produces a composite video signal at pin 23, but first check the d.c. supply to the tuner. Can also be caused by the TEA2014 video switching chip IV03 - this i.c. is used to switch off the video signals from the tuner/ i.f. block and switch in the signal from the scart connector when the correct switching level is connected to pin 8 of this connector.
No tuning: Before changing the tuner block, check that the U1 supply is reaching the front panel where it feeds the 33 V zener diode (the circuit reference number for this


Fig. 3: Complete field timebase circuit, F10 chassis. RF12 is $3.3 \Omega$ in the $F 11$ chassis - there are other minor variations.
diode varies with different models). If the U1 supply is not present at the front panel check RL53 (100 $\Omega$ ) and CP24 $(0 \cdot 01 \mu \mathrm{~F})$. Check the 33 V zener diode itself, also the u.h.f./v.h.f. band selection circuit on the front panel. The usual culprit however is the tuner block itself. Note that it is also almost the only cause of tuning drift.
No sound: These sets all have a sound mute system which operates when no video signal is received. It compares the composite video signal with line flyback pulses within the TDA1950 chip: if the sync pulses in the video signal don't coincide with the flyback pulses pin 7 of this i.c. goes to 0 V (it's normally at 11 V ) and the sound is muted via pin 2 of the TBA120UB intercarrier sound i.c. This muting circuit should be kept in mind when fault finding: for example, on a set with no sound and a video fault don't chase a sound fault as the muting circuit will operate due to the absence of the video signal. The muting circuit can also give clues however: for example, a set with no video but good sound means that the fault is in the latter part of the video channel, certainly after pin 6 of the TEA2014 switching chip IV03 (this is the take-off point for the video feed to the muting circuit).

Where there's no sound and the muting is not in operation, i.e. pin 7 of the TDA1950 chip is at 11 V , check the TDA2006 audio output chip IS01. Note that many of these sets have been built with stereo use in mind: a second audio output chip is often fitted but not connected up - this is a convenient source of a replacement if you do


Fig. 4: Showing the way in which adding line pulses (three only shown) to a field sawtooth waveform gives pulse width modulation at the collector of TF07 so that DF08 is switched on progressively earlier as the field scan progresses.
not have one readily to hand.

## Spares

The agents for NordMende sets in Ireland are Reynolds Electronics Ltd., Finnabair Industrial Park, Dundalk, Co. Louth (042 31281 ). The UK agents are Hayden Laboratories Ltd., Hayden House, Chiltern Hill, Chalfont St. Peter, Gerrards Cross, Bucks SL9 9UG (0753 888 447).

| NE OUTPU | RANSFORMER <br> \& CARRIAGE |
| :---: | :---: |
| Delivery by return of post. |  |
| BAIRD: 8290, 8752, 8773 | ITI: VC200 to VC402 CVC1, CVC2 (FORGESTONE) |
| RANK BUSH MURPHY | CVC5, CVC7, CVC8, CVC9, CVC20 10.35 |
| A774 with stick rectifier $\quad 9.78$ | CVC25, CVC30, CVC32, CVC45 9.20 |
| A816, T16, T18, 2712,2715 | CVC880, 1100, 1150 P.0A |
| T20, T22, T26, Z179, A823 | CVC1200, 1204, 1210, 1215, 2600 P.0A. |
| 2718 Basic unit | PYE: 169, 173, 569, 368 |
| DECCA: 1210, 1211, 1511 | CT200, СТ200/1, CT213 $\quad 10.35$ |
| 1700, 2001,2020, 2401,2404 9.20 | $725-731,735,737,741 \quad 9.78$ |
| $\begin{array}{ll}\text { CS1730, 1733, 1830, } 1835 & 920 \\ 30,70,80,90,100,120,130 & 9.20\end{array}$ | PHILPS: $170,210,300$ series $\quad 9.20$ |
|  | 320 series $\quad 9.78$ |
| FERGUSDN, THORN: 1590, 1591 9.20 TX, T8, TX2, TX3 mono P.0A <br> 1690, 1691. built in rect. 9.78 G8 and G9 Series £9.20 |  |
| $\begin{array}{ll}1600,1615,1700,1790 & \text { P.OA } \\ 3000,3500,8000,8500,8800 & \text { P.OA }\end{array}$ | $\begin{array}{lr} \text { G8 and G9 Series } & \mathbf{£ 9 2 0} \\ K T 2 \text { KT3. series } & 9.20 \end{array}$ |
|  | $\begin{array}{lr} \text { KT2. KT3. series } & 9.20 \\ \text { G11. K30. split diode } & \text { P.O.A } \end{array}$ |
| 9000, 9200, 9300 series 12.00 <br> $9500,9600,9650$ series 10.99 <br> 9800, TX9, TX10 series PDA. <br> MOVIESTAR 3781, 3787 12.00 <br> TX10 focus unit 1025 | BINATONE: 9909, 9860, 9488 P.OA. <br> DORIC Mk3, Mk1 11.50 <br> RNLUX 9560, 9670 P.0A. <br> GRUNDIG: most models in stock  |
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| FDELUT: FTV12 mono 10.35 <br> OX2000 XX3000 P.DA. | SANYO: 5101, 5103, 7118 P.0A. |
|  | SHARP: C1851H, C2051H P.OA. |
| G.E.C. 2047 to 3135 mono $\mathbf{9 . 2 0}$ TOSHIBA: C800, C800B P.OA <br> 1201H, $1501 \mathrm{H}, 2114,3133,3135$ 9.20 TANDBURG: 190, CTV2, CTV3 P.0A <br> TELERUNKEN: most models in stock    |  |
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| INDESTT: 24EGB, 12LGB, 12SGB 10.35 | Tidman Mail Order Ltd., 236 Sandycombe Road, Richmond, Surrey. <br> Approx. 1 mile from Kew Bridge. <br> Phone: 01-948 3702 <br> Mon-Fri 9 am to 12.30 pm \& $1.30-4.30 \mathrm{pm}$ <br> Sat 10 am to 12 noon. |
| WINDINGS 6 |  |
| TYNE: main winding  <br> RBM: T20, $22, \mathrm{~T} 26, \mathrm{Z179}$ 6.80 <br> 1.33  |  |
| WALTHAM: W125 eht winding 237 |  |
| WALTHAM: W190, W191 eht coil 5.00 |  |
| KORTING: hybrid winding 5.90 |  |
| THORN: 8000, 8500, 8800 eht 6.70 |  |

## Teletopics

## Agreed uk stereo TV Standard

The BBC has been carrying out tests on a digital stereo sound system of its own design since late 1983 - we last reported on the subject in this column in August 1984, after tests to confirm the system's compatibility with nonstereo receivers had been carried out. The system that's been evolved is called 728 -Nicam (near instantaneous compansion) and has been agreed by the IBA. It's at present awaiting approval by the Department of Trade and Industry. Since transmitters are already installed at Crystal Palace a London area service could be started in a matter of weeks: it would take some years to convert all the BBC/IBA transmitters. It's understood that Thorn EMI Ferguson has a decoder chip set at an advanced stage of development and that incorporating stereo sound would add about $£ 30$ to the cost of a receiver.

The system uses a single carrier spaced at 6.55 MHz above the vision carrier, with four-phase shift-key modulation: the transmitted data rate is $728 \mathrm{Kbits} / \mathrm{sec}$. The original analogue sound signal is sampled at a rate of 32,000 times a second, the samples being converted to 14 -bit words. To get the signal into the spectrum space available 10 bits are transmitted along with a signal to indicate to the receiver the compansion that has taken place. As a result the receiver can reconstruct and decode the original 14 -bit samples. One advantage of the system is its compatibility with the MAC standard proposed for satellite TV transmissions.

## DBS PROGRESS

The IBA has now advertised for contractors to provide three new TV services by satellite transmission, to be receivable throughout the UK. Applicants have been invited to submit proposals by August 29th with a view to the IBA selecting and appointing contractors by the end of the year with services coming into operation by 1990 . Applicants have been invited to apply for a contract to provide all three services - with a variety of programming between the three channels - to be financed either by advertising, by subscription or a combination of the two. Those proposing to provide fewer than three services are asked to indicate what forms of co-operation they would plan with other contractors. Applications have also been invited for contracts to provide teletext DBS services, both from those applying for the programme contracts and others. The government intends to introduce legislation so that the contracts would last for up to fifteen years, under the terms of the Cable and Broadcasting Act 1984.

Meanwhile the election of a new government in France has called into question the Maxwell group's plans (see last month) to provide programmes on two of the French TDF-1 satellite's channels. Mr. Maxwell maintains that he has a binding contract but the new government has indicated that it plans to cancel this, with six months' notice, and open the allocation of TDF-1's DBS channels to competitive tendering.

## INTERNATIONAL TRADE

The effects of the rise in the value of the yen, mentioned in our leader last month, are already showing through. Matsushita has reported the first fall in sales and profits
for eleven years, during the first quarter of its financial year which ended on February 20th. Consolidated profit fell by 19.3 per cent and sales by 8.7 per cent. Domestic sales fell by only $1 \cdot 1$ per cent while overseas sales recorded a decline of 16 per cent - sales of video/TV equipment fell by 17.2 per cent. Reduced colour receiver exports to China and a sluggish demand for components were given as contributory factors. Matsushita proposes to increase overseas selling prices and transfer some production to other south east Asian countries.
Sanyo is increasing the prices of its VHS VCRs in the UK by between $£ 30$ and $£ 50$ depending on model and predicts that other Japanese manufacturers will be doing the same.
The Thomson group is to cut its workforce in European colour receiver plants by between 20 and 25 per cent about 1,000 jobs in W. German plants will go, 550 jobs in France and 300 in Spain. Last year Thomson's consumer electronics group made a loss of $£ 30$ million on sales of some $£ 2 \cdot 1$ billion. The overall proposal is to cut the workforce from 8,500 to around 7,000 . Thomson, whose brands include NordMende, Saba and Telefunken, is one of Europe's two largest CTV manufacturers: colour TV accounts for roughly fifty per cent of Thomson's estimated annual consumer electronics output. Europe's other major consumer electronics manufacturer, Philips, plans to close a number of TV manufacturing plants.
Matsushita has announced the development of a 1 Mbit video DRAM. Mass production is expected to start by the end of the year. Two such chips are required to store a TV field.

## THORN-JVC DEAL

An agreement has been reached between Thorn EMI Ferguson and JVC for the manufacture at Ferguson plants of colour receivers to meet JVC's requirements in the UK and continental European markets. Under the terms of the agreement a range of products incorporating JVC's newly developed BX chassis will be manufactured by Ferguson with technical and production support from JVC: the new manufacturing operation will be managed by Ferguson and will require substantial additional equipment and dedicated production facilities. A new production line to be installed at Gosport will be able to produce over 200,000 sets a year. Enfield will supply PCBs and High Wycombe cabinet mouldings.

## ORION's UK PLANT

The Orion Electric Corporation of Japan is to set up a VCR/TV manufacturing plant at Kenfig Hill, South Wales - the 50,000 square feet factory was previously used by computer manufacturer Dragon Data. The first phase of the operation will be the installation of a production line for VHS VCRs: production is expected to be running at a rate of 10,000 machines a month by the end of the year. A CTV line will probably be added next year to produce sets for sale in the UK and continental Europe. Assistance tied to the number of jobs created will be provided by the Welsh Development Agency. Orion products will continue to be distributed in the UK by L and M Raymond of Watford. Sales are mainly to major retailers - Orion VCRs are sold by Dixons under their Saisho brand name.

## TV SYSTEMS TESTED

With the co-operation of Swindon Cable Ltd. IBA engineers recently demonstrated for the first time successful distribution of full-capacity MAC TV signals via a mod-
ern, operational cable system. Full-resolution MAC-encoded vision with digital sound at a data rate of $20 \cdot 25 \mathrm{Mbits} / \mathrm{sec}$ were inserted at the head end of Swindon Cable's multichannel system, using the EBU's "cut and rotate" scrambling system. A receiver connected to an existing domestic socket outlet produced pictures without any significant degradation.

A demonstration of the MUSE system has been carried out by RAI and NHK at Turin. The Japanese MUSE (multiple subnyquist sample encoding) system has been developed to enable high-definition TV signals to be transmitted using standard satellite TV channel bandwidths. Reception of MUSE-encoded signals via a noisy satellite transmission path is said to have produced pictures virtually identical to the original HDTV ones.

## NEW FILM CABLE CHANNEL

British Telecom is to offer cable operators a new film channel, with material sourced from MGM/UA, Paramount and Universal initially. It will compete with Robert Maxwell's Premiere channel, with which MirrorVision was recently amalgamated. Distribution of the new channel to cable operators will be via cassette rather than satellite transmission.

## VCR SERVICING VIDEOCASSETTES

Flintdown Ltd. (Mountauban Chambers, 339 Clifton Drive South, Lytham St. Annes FY8 1LP) has produced a series of seven cassettes on servicing domestic VCRs. The series consists of (1) an overview of VCR systems, (2) servo control systems, (3) colour recording systems, (4) frequency modulation, (5) VHS, Betamax, V2000 and Video 8, (6) component video and (7) VCR faults. Each cassette is available in any standard format and costs $£ 35$ plus VAT - a discount of 10 per cent is given on a complete set of seven cassettes.

## VIDEO EQUIPMENT

JVC has launched a midi-sized hi-fi VCR, Model HRD470, which is expected to retail at around $£ 600$. The tape deck has been rotated through $180^{\circ}$ to give frontloading of the cassette end first.

Kodak is test marketing some electronic still picture systems in the USA. A disc recorder-player enables 50 TV fields from a TV set or other video source to be recorded on a standard 2 in . floppy disc. Recording is triggered by remote control. A companion printer produces prints of any recorded field on instant colour film. There's also a film to disc transfer service which enables 35 mm colour film negatives to be recorded on disc for playback via the recorder-player.

Grundig has introduced a combined colour receiver/ VCR unit, Model TVR5000, which is expected to sell at around $£ 950$. The VCR incorporated is the new VS300 which features auto tape time select, electronic locking and can record two programmes up to a year ahead.

## AMSTRAD TAKES OVER SINCLAIR'S COMPUTER INTERESTS

Amstrad has bought the world-wide rights to Sinclair Research's current computer interests. Sinclair is now a research organisation without marketing operations. A computer under development by Sinclair will be offered to Amstrad at a later date.

Amstrad is to continue production of the Spectrum computer in the UK for the present. Sales of the QL will
continue while stocks last but this machine will probably be phased out. Interesting that Amstrad decided not to take on Sinclair's pocket monochrome TV set. Amstrad paid $£ 5$ million for the right to use the Sinclair brand name and current stocks.

## TV/VCR SPARES GUIDE

Some corrections and an addition to the spares guide published with our April issue. Spares for recent NEC products are available from NEC Business Systems (Europe) Ltd., NEC House, 164-166 Drummond Street, London NW1 3HP or from SEME Ltd., Unit 2E, Saxby Road Industrial Estate, Melton Mowbray, Leics. Models include CTVs 12T311, 20T772, 20T773, 14T412, 14T1406, CT1404, FS1901, FS1902, CT1416 and FS1502 and VCRs PVC744E and PVC746E (Beta) and N830EK, N831EK, N833EK, N9013 and N9014 (VHS). Spares for earlier NEC models distributed in the UK by Cap Ten are available from Tech Semco.

The address we gave for Tensai was the last known one. It appears that this company is no longer represented in the UK. Don't use the phone number we gave - it's been transferred to a domestic user.

Spares for three Gold Star monochrome portables, Models VW300, VR317 and VR700, are available from Uni-Com Electronics, Station Road, Edenbridge, Kent TN8 6EW (0732 865 238).

CPC of Preston was mentioned in the Letters column last month as a supplier of spares for Sinclair microcomputers. The full address is CPC Electronic Component Distributors, 194-200 North Road, Preston, Lancs (0772 555 034). CPC are also official spares stockists for Fidelity, Ferguson, Philips, Pye and Sony.

## TVRO EQUIPMENT

Megasat's new top-of-the-range satellite TV receiving system is said to be the only totally automatic remotecontrolled system on the market with a computer-generated "menu" of programmes presented on the screen for user selection. Any programme can be selected by remote control without the user leaving his chair. The remote control system includes the motorised dish and automatic polarisation. Price is $£ 2,645$ including VAT (plus installation). The Megasat system is available from Harrods, Wallace Heaton and Lasky's Tottenham Court Road and Brent Cross stores.

NEC's NESAT satellite TV receiver system is now available with an automatic aerial tracking system. The actuator motor is linked by cable to a microprocessor controlled tracker unit which can be located anywhere in the vicinity of the TV set. An LED display shows the dish position.

Sat-Tel has developed a battery-operated satellite TV signal meter to simplify dish installation. The meter, called the Skyhound, plugs directly into the LNC's output and in addition to the meter display has a variable audio pitch indicator.

A new transistor from Mullard, type BFG195, has a transition frequency of typically 7.5 GHz and a unilateral power gain of 12 dB at 2 GHz . It can handle a power dissipation of 0.5 W and is said to have the highest presently available power handling capability for this category of transistor. The four-lead, dual-emitter transistor is intended for applications in high-gain wideband systems up to 2 GHz , e.g. in the first i.f. section of a satellite TV receiver.

# The Development of Colour Tubes 

Eugene Trundle

The picture tube is the very heart of a colour set or monitor, its characteristics dictating not only the shape and size of the set but the design of every other section of the receiver apart from the tuner, the i.f. amplifier and the control system. Even the sound system is related to the tube in that the loudspeaker usually has to be accommodated alongside and its shape, size and magnetic field must conform, while the audio amplifier is (or should be) tailored to the type of loudspeaker in use.

## The Early Days

Colour picture tubes have been with us since late 1949, when Dr. Harold B. Law made the first shadowmask tube at the RCA company's Princeton, New Jersey laboratories. The picture was small, about 11 cm in diameter, and the resolution and convergence performance were very poor by today's standards. Most of the ingredients of subsequent tube technology were there however: three guns, one for each primary colour; a tri-colour phosphor screen; and above all the shadowmask. In one form or another the shadowmask has been present behind our screens ever since.

The original RCA design was based on an idea by A. C. Schroeder, patented by him, for a delta-gun/mask/ triad-phosphor-dot screen configuration. A much earlier patent for a colour display tube, filed in Germany by Werner Flechsig in 1938, proposed the shadowmask in an aperture-grille form: this uncannily anticipated the Trinitron tube introduced by Sony of Japan some thirty years later.
The first delta-gun tubes had an internal phosphor-dot screen which was flat, as was the shadowmask mounted some 1.2 cm behind it: the curved glass faceplate acted merely as a clear window. It wasn't until 1954 that tubes with the phosphors deposited on the rear of the curved faceplate went into production. These had a deflection angle of $70^{\circ}$, a circular 21 in . ( 53 cm ) screen, a huge 51 mm diameter neck and a metal cone. An all-glass version went into production three years later.

## Tube Evolution

Gradual improvements in the phosphors, mask and faceplate light transmission characteristics were introduced before the next big step in 1964, the $90^{\circ}$ deflection tube with a rectangular 25 in . ( 63 cm ) screen. This was followed shortly after by a 19 in . ( 49 cm ) version. The popular 22in. ( 56 cm ) $90^{\circ}$ tube came in 1967.

1968 was a significant year. In April the Sony Trinitron tube was released, initially in a 33 cm (13in.) rectangular format with $90^{\circ}$ deflection. With its in-line gun assembly and striped phosphor screen it was the precursor of all the current tube designs: a grille with slots from top to bottom performed the same function as the shadowmask. The rest of the world followed: RCA's PIL (precision in-line) tube with its slotted shadowmask and striped screen was introduced in 1972 and was followed over the next few years by many variants. The great advantage of the PIL tube was the elimination of the need for the convergence
circuitry required with delta-gun tubes.
The first $110^{\circ}$ shadowmask tube was introduced in 1969 - especially for Europe, as the US market wasn't at that time into wide-angle colour tubes. It was a delta-gun tube with a thick neck ( 36.5 mm ). $110^{\circ}$ tubes with 29 mm neck diameters appeared as early as 1970 . The seventies saw a succession of developments: saddle-toroidal yokes in 1973; internal magnetic shields, quick-heat cathodes and the Philips 20AX tube in 1974; "soft flash" in 1977; the Philips 30AX system with no need for setmaker or service technician adjustments in 1978, along with pincushiondistortion free (pin-free) tubes from Japan. In 1979 the mini-neck tube ( 22.5 mm diameter) came from Japan and in 1982 Toshiba introduced the FST (flat square tube) screen. To bring us up to date, the Philips 45AX tube was introduced in 1984 and in 1985 Sanyo demonstrated small, prototype beam-indexing tubes - this type of tube has a single gun with switched RGB inputs and no shadowmask (the idea is not new but its realisation has always proved difficult, mainly because of the problem of switching the video signals at the high frequency required).

## The Delta-gun Tube

Since we're going to describe the components and techniques used in colour tubes in some depth it's important that their basic operation and principles are understood. Although delta-gun tubes are now obsolete as far as domestic TV sets are concerned they are still in production for use in monitors and advanced computer displays since they are capable of giving very high definition displays when fitted with a fine-pitch shadowmask. Let's start then with a brief rundown on delta-gun tubes.

The virtue of all types of direct-viewing colour displays (as opposed to multi-tube projection systems) is that the tube used simultaneously produces on its screen light in the three primary colours red, green and blue. This implies the presence on the screen of three different phosphors, and the trick is to ensure that the electron beam from each gun strikes only the appropriate phosphor material. Hence the shadowmask which, for each beam, casts a shadow over the phosphors the beam shouldn't reach. The delta-gun tube has three electron guns arranged in equilateral triangular formation in the tube's neck - see Fig. 1. The guns are each tilted towards the tube's major axis so that their electron beams converge at the shadowmask. Because the beams come from three different "aiming points" their approach angles differ: this is the key to the operation of the mask (see Fig. 2). The beams cross over at the shadowmask and diverge beyond it, each to strike its correct phosphor dot.

## Colour Purity

So far as the mask and screen are concerned the origin of the beams is not the delta-gun assembly itself but a point in space in the tube neck, at the centre of the deflection yoke, called the deflection centre. By fitting a lamp at the apparent source of each beam in turn the positions of all the phosphor dots for each colour can be


Fig. 1: The thick-neck, delta-gun arrangement. (a) Positions of the three guns in the tube neck. (b) Configuration of the gun electrodes and convergence pole-pieces. (c) Axial view of the pole-pieces mounted at the end of the guns: the polepieces guide the magnetic fields from the adjacent radial convergence coils.


Fig. 2: Trajectories of the beams in a delta-gun tube. In practice each beam is larger than one shadowmask hole.


Fig. 3: The inherent raster geometry errors with a delta-gun tube.
fixed photographically with reference to the perforated shadowmask. This is done during manufacture and ensures that provided each beam is correctly aligned at the deflection centre perfect colour purity will be produced in operation, with no overshooting of the electron beams on to phosphor dots of the wrong colour at any point on the screen. Purity setting is easy to adjust: we manipulate a pair of ring magnets to align the beam trajectories through the deflection centre, then adjust the position of the deflection centre itself by sliding the deflection yoke along the tube's axis.

## Convergence

The problem with the delta-gun picture tube configuration is its inherent registration errors. The three rasters, red, green and blue, are traced out by separate electron beams coming through the deflection centre at three different angles - each is subject to different aberrations in the scanning process. This results in the complex raster geometry errors shown in Fig. 3. Each colour raster has a different combination of trapezium and pincushion distortion. To pull these odd and divergent rasters into registra-


Fig. 4: Principle of the Trinitron tube.
tion, i.e. to overlay them, calls for individual and close control over the positioning of all three beams as they enter the deflection field. A static magnetic field will suffice to pin together the raster centre points (static convergence) but to make the edges of the three individual rasters register each beam must be subjected to a continuously varying magnetic field (dynamic convergence). A parabolic correction waveform is required to iron out the pincushion distortion while a sawtooth correction waveform will cancel trapezium distortion. Hence the "tilted sawtooth" current waveforms in the radial dynamic convergence correction yoke. These are required at both line and field rate, and must be adjustable in amplitude and tilt - and in shape in the case of the blue horizontal correction waveform for $90^{\circ}$ tubes and for most functions with $110^{\circ}$ tubes.

The difficulties, the compromises necessary, the expense of providing the convergence hardware, the skill needed in aligning the many presets, the power loss in the entire convergence network and its vulnerability to drift prompted the tubemakers to investigate different arrangements for the picture tube. The goal was to produce a tube that has an inherent self-converging characteristic. So long as there are three beams travelling along the tube on different paths this is very difficult! The solution adopted was to mount the guns in line so that the three beams travel abreast and to build correction into the tube and its yoke, something that calls for a very high degree of manufacturing accuracy. Before we come to the selfconverging PIL tube however we should look at the first in-line tube to be mass produced, the Sony Trinitron.

## The Trinitron Tube

The principles of the Trinitron tube are shown in Fig. 4. The tube has several advantages over the delta-gun type of tube. These spring from its use of a single in-line electron gun assembly and an aperture-grill form-of shadowmask. The electron gun has three separate cathodes arranged side-by-side: all the other electrodes are common to the three beams. This facilitates the use of a single, large-diameter electron lens (see later) in the centre of which the beams cross over, making for minimum aberration and a reduction of the scanning spot size (in comparison with the delta-gun tube) of about 25 per cent. The two diverging outer beams are redirected by an electronic prism (a set of electrostatic deflection plates) so that they converge and cross over at the aperture grille.
The aperture-grille shadowmask consists of a metal sheet with a large number of evenly-spaced vertical slits to provide shadowing for groups of three (RGB) phosphor stripes. This form of construction has little stiffness in the vertical direction and has thus to be kept under considerable tension to prevent sag or buckle. One consequence is that a parabolic faceplate contour cannot be used Trinitron faceplates have a cylindrical contour with the
vertical profile straight. The transparency of the aperture grille was about 33 per cent greater than that of the shadowmasks used in contemporary delta-gun tubes, giving a brighter image for a given beam current. This and the 25 per cent smaller spot diameter gave the Trinitron tube a considerable advantage, which was widely acclaimed.

Having the three beams in the same horizontal plane brings two benefits: first the purity is virtually unaffected by horizontal magnetic fields such as the Earth's; secondly the need for vertical convergence correction disappears because the deflected beam trajectories remain in a single horizontal plane. The fact that the three beams are very close together on their journey through the deflection field also minimises horizontal misregistration of the three rasters. Total errors are reduced to those shown in Fig. 5. The standing voltage on the prism electrodes is adjusted to achieve correct static convergence on the vertical centre line, leaving a relatively simple dynamic convergence correction problem which can be solved by applying a parabolic waveform to the prism electrodes, see Fig. 6. Minor trimming is carried out by tilting the deflection yoke and adjusting the line-rate (and, in large-screen versions, field-rate) sawtooth current in a single four-pole convergence coil associated with the deflection yoke. These are purely trimming adjustments to take up tube and yoke manufacturing tolerances, not correction for inherent geometrical errors as in delta-gun tubes.

## The PIL Tube

The Trinitron design showed the advantages of the inline gun configuration. It was not long before the PIL tube came along. The main differences between the two tubes are as follows: in the PIL tube there are staggered crossties in the mask assembly (see Fig. 7) to provide sufficient mechanical rigidity to enable a conventional parabolically curved faceplate to be used, and the elimination of all need for dynamic convergence correction. This is achieved by a very special deflection yoke design in which the density of the magnetic flux in the tube's neck is not homogeneous, as in a monochrome or delta-gun tube, but astigmatic.
The degree of deflection applied to an electron beam is proportional to the deflection field's magnetic flux density. To scan a picture tube horizontally and vertically both deflection field strengths change continuously according to a sawtooth law, but at any given instant the total flux density present is proportional to the distance from screen centre to the point at which the beams strike the screen. If the magnetic field required is carefully distributed in the tube's neck it's possible to achieve good convergence all over the screen area. Fig. 8 shows the effect of a uniform deflection field in a tube cross-section: the three beams converge at the screen centre and since each is affected equally by the deflection field they will converge at a point along a circular line (the image field) whose radius is the deflection centre to screen centre spacing. Beyond this crossover point the beams will diverge, striking the relatively flat tube screen at points a, $b$ and $c$.
The operating principle of the PIL tube depends on a special deflection yoke design which produces magnetic flux lines distributed in the tube's neck in the manner shown in Fig. 9, which is again a tube cross-section drawn looking from above the tube to show horizontal deflection. In this astigmatic field the deflection force acting on


Fig. 5 (left): The Trinitron tube's basic convergence errors. The absence of crossover with the $R$ and $B$ verticals is due to the use of an astigmatic vertical deflection field.

Fig. 6 (right): Voltage and waveform applied to the prism electrodes to correct the misregistration shown in Fig. 5.

Fig. 7: Configuration of the slots in a PIL shadowmask.


Fig. 8 (left): An in-line gun array projecting three beams through a homogeneous deflection field.

Fig. 9 (right): With careful distribution of the deflection field flux density, convergence is automatically achieved over the entire screen area.


Fig. 10 (left): Errors arising from vertical deflection of in-line beams by a homogeneous magnetic field.

Fig. 11 (right): Opposing astigmatic line and field deflection fields in a fully self-converging yokeftube system.
a given beam depends on the path taken by the beam through the deflection field. The centre beam, taking this first, passes through the relatively weak field in the middle of the deflection centre and is deflected to point $A$ on the screen. The right-hand beam will start to turn left as it enters the deflection field. It then passes into an area of reduced flux. As a result the deflection force acting on it is reduced and it turns through a lesser angle than the centre beam. If the flux density in the deflection field is tailored to be just right the beam will converge with the centre beam at point A instead of crossing the centre beam's path to strike the screen at some point B. As the left-hand beam starts to turn left it encounters an increasingly strong magnetic field. This bends it farther to the left with the result that it's aimed precisely at point $A$ on the screen


Fig. 12 (left): Earliest form of toroidal deflection yoke for a PIL tube.

Fig. 13 (right): Saddle-wound yoke for a $110^{\circ}$ 20AX selfconverging tube, showing the horizontal deflection coils.

- if it passed through a homogeneous field it would strike the screen at some point C . The same principle applies when the three beams are deflected to the right instead of to the left.
Now for vertical deflection. As the beams are deflected upwards or downwards from screen centre the yoke-toscreen beam path becomes progressively longer, which would lead to horizontal displacement of the three images due to crossover of the beams before they reach the screen, see Fig. 10. To counter this the horizontal lines of magnetic flux, which produce the vertical deflection, are given an increasing vertical component away from the tube's axis - the field is increasingly barrel shaped.

The horizontal and vertical field patterns required are shown in Fig. 11. These astigmatic fields are achieved by the deflection yoke's winding pattern: the configuration of the toroidally-wound yoke is shown in Fig. 12. The effective field pattern (and hence dynamic convergence trimming) can be adjusted by tilting the front (screen) end of the deflection yoke to achieve optimum registration of the three rasters. In the original PIL tube design this was carried out at the tube factory, using a yamming jig (YAM $=$ Yoke Alignment Machine), after which the yoke was wedged and sealed to the tube with a thermosetting adhesive. The tube and yoke thus became effectively a single assembly and replacement tubes came with sealed on yokes. In subsequent designs the yoke and tube were treated as separate components, with alignment left to the setmaker or TV technician.

Purity (initial alignment of all three beam paths) and static convergence (individual control of the effective point of origin of the two outer beams) is provided by a combination of two-, four- and six-pole magnets mounted on the tube's neck behind the deflection yoke. These were sealed in the original type of PIL tube but can be adjusted in later in-line tube designs.

To summarise, the PIL type tube trades the complications of delta-gun tube convergence for very tight manufacturing tolerances in both the tube and yoke design. We'll return to both of these later, but before doing so we must examine the approach taken by Philips/Mullard in their 20AX in-line tube design.

## 20AX System

This was the first European successor to the delta-gun tube. It has three separate guns mounted in-line in a thick tube neck ( 36.5 mm diameter). The deflection angle is $110^{\circ}$ (the deflection angle with the original, smaller screen size PIL tubes was $90^{\circ}$ : the later larger screen tubes have $110^{\circ}$ deflection). With the 20AX tube the manufacturing tolerances are sufficiently tight not to require any tilting of the yoke assembly. Instead, manufacturing tolerances are taken up by introducing adjustable sawtooth currents at
line and field rate in a four-pole convergence correction coil built on to the deflection yoke and by differential adjustment of the sawtooth scanning currents flowing in the separate halves of each deflection coil pair. These current controls are provided by half a dozen preset potentiometers or links. Static convergence and purity are catered for by a cluster of two-, four- and six-pole ring magnets of similar design and working on the same principles as those used with the PIL tube.

## The 30AX Design

All the adjustments required with the 20 AX tube were eliminated when the next Philips design, the 30AX, came along some four years later. This is similar in principle to its predecessor but with such close yoke design tolerances that dynamic convergence trimming adjustments are no longer necessary. The cluster of ring magnets on the tube neck was replaced by a special magnetic ring mounted inside the tube, on the top of the triple-gun assembly. This has a combination of two-, four- and six-pole fields printed into it during manufacture, using a computercontrolled external magnetising jig. These fields are "customised" for each tube, which is thus brought to design centre tolerance in respect to picture geometry, purity and static convergence: the magnetic characteristics of the ring do not drift during the tube's life. With the 30AX system any tube will work with any yoke (for a given tube size) without need for setting-up adjustment the yoke is precision located by three bosses moulded into the tube's glass flare.

20AX and 30AX tubes use saddle-wound yokes with the distribution of the wires controlled by the precision mandrel on which they are wound. Fig. 13 shows the winding pattern for the 20AX tube: it's the "bunching" of the individual wires that provides the astigmatic deflection field required.

## FS Tubes

The next significant change in tube design came in 1982 with the FST glass envelope. This was pioneered by Toshiba of Japan and involved increasing the radius of the faceplate to make it flatter while squaring off the corners in order to approach the rectangular shape of the transmitted picture more closely. The reduced bracing effect of the flatter faceplate necessitated an increase of around 30 per cent in the thickness of the front glass and a corresponding increase in tube weight. Benefits of the new design include reduced reflections from the tube screen, a greater angle of legibility and less pattern distortion in the picture. The characteristics of the FS tube were described in an article in the June 1985 issue of Television.

## The 45AX

The latest example of an FS type tube is the Philips/ Mullard 45AX design, in which the triple-gun assembly and thick neck have finally been abandoned in favour of single-gun, narrow-neck technology.
This article has briefly set the scene in outlining the main developments in colour tube technology over the years. Next month we will start to look in greater detail at the individual components that go to make up a picture tube and its deflection system. This will give greater insight into design philosophy and the continuing quest for better performance with lower power consumption.

# Servicing Teletext Decoders 

Part 5: Fault Finding

In this concluding article in the present series we'll examine methods of tackling faults that affect teletext reception. By now many readers will be well versed in servicing digital circuitry since this is becoming more and more common in consumer electronics equipment. An indepth knowledge of this is not essential for teletext servicing however. There are two main reasons for this. First the use of LSI chips means that we cannot go down to gate-level fault-finding: most decoder faults are caused by failure of one of the LSI or memory chips. Secondly there's the advantage that since teletext is basically a display function the screen usually tells us what's happening. Thus many faults can be diagnosed without even removing the set's back cover.
It must be said at the outset that many of the faults that affect teletext reception are not caused by a decoder malfunction. Ignoring for the moment faults with the power supplies, earths etc. we should emphasise that the digital signal obtained from the vision detector must be of good quality with few errors: thus everything from the transmitter to this point must be working reasonably well.
Faults in the early stages of the set show up as text display errors, such as wrong characters or graphic blocks, possibly not on all channels and possibly very intermittent. Incorrect characters can be caused by a decoder fault but in his case the errors repeat themselves, i.e. either the fault occurs at the same screen position, the same character or group of characters are wrongly displayed or maybe rows or columns are repeated. More on this later.
Starting at the front, the aerial must provide a ghostfree signal. It's difficult laying down any hard and fast rules here: various things affect reception and the type of set is also relevant. It's true to say however that signal
strength is not the most important thing: excessive patterning due to beats with other transmissions, i.e. crossmodulation, and ghosts - especially those close to the original signal - can wreak havoc with teletext reception.

The tuner and i.f. strip must have good h.f. performance. In general this means that if we were to look at the reprodúction of a perfect staircase signal, using a perfect oscilloscope, there would be slight overshoot on each step but it would be possible to tune the vision detector to obtain square corners. Every stage from the aerial socket to the vision detector has a bearing on this. To return to teletext versions of the Philips G11 chassis, which we took as our basic example of a teletext receiver, in these the i.f. panels (incorporating the tuner) were selected for teletext performance and so labelled. This doesn't mean that an i.f. strip not so labelled won't work it probably hasn't been tested for text performance.

## G11 Teletext Conversion

We'll digress here for a moment to mention, for the benefit of anyone wishing to make up a teletext G11, that the other differences lie in the colour decoder, the text power supplies and the additional remote control circuitry. The colour decoder has the RGB interfacing panel described. in Part 1 added - this can be done on a nonteletext panel by removing the links to the bases of the RGB output transistors.

## Power Supply Arrangements

In early models with ultrasonic remote control there's a separate power supply panel that lives in the bottom of


Fig. 1: The teletext decoder/remote control power supply arrangement used in early teletext versions of the Philips G11 chassis. The circuit is shown in basic outline only.

the cabinet - a simplified circuit is shown in Fig. 1. The mains transformer feeds a bridge rectifier which produces 19 V across C12. IC19 provides a regulated 12 V supply from the 19 V supply: this voltage is used to power the remote control receiver and is also passed to the VIP chip in the decoder. R25 drops this supply to 5V for the M911 remote control decoder chip. The 19 V supply is also fed to the emitter of the chopper transistor T50. This is part of a series chopper circuit with L54 the reservoir inductor and D51 the "efficiency diode". The 11 V output developed by the chopper is applied to the 5 V regulator IC61 whose output powers the rest of the teletext decoder. At least it does once the line timebase has started up. The delay is necessary to allow C 12 to become fully charged before the chopper starts. Note that the supply for the 18 kHz astable multivibrator $\mathrm{T} 41 / 43$ comes from the set's main 12 V line, which is derived from the line output transformer. So T50 is without drive until the line output stage is operative. There's elaborate over-voltage protection - teletext decoders were worth a fortune at that time!

Later models with infra-red remote control have a simpler arrangement - the decoder's 5 V supply is derived from an extra winding on the line output transformer, making the line output panels non-compatible. The pulses from the line output transformer are fed to a small panel at the bottom of the cabinet. This panel contains a large diode, a 5 V regulator and a few other bits. The teletext decoder's 12 V supply comes from the set's main 12 V line via the remote control receiver.

Servicing either of these power supplies should pose no problems, but we'll mention the effect of either teletext decoder supply being absent: no 5 V rail produces a bright blank raster, no 12 V supply gives absence of text only.

Needless to say any voltage change or defective decoupling can cause some very strange faults indeed! The moral is to check both lines, preferrably with a scope, when presented with an inexplicable fault symptom.

## Misadjusted Clock Coil

An odd effect occurs when the 6.93 MHz clock coil is incorrectly adjusted: the errors increase towards the righthand side of the screen. This shows up clearly when the clockcracker page is selected. Don't forget that adjustment will have no visible effect until the page is reselected. Leave any adjustments on the decoder alone unless absolutely necessary.

## Memory Faults

Most of the faults on the G11's teletext decoder panel are due to the 2102 memory chips. If wrong characters are persistently displayed at a particular row/column position one of the memory cells is stuck at one or zero. Many characters wrong but always the same errors means that one of the data bits is stuck. This may occur during read or write but this makes no practical difference. If row or column address pins are shorted to either rail groups of text will be repeated.

A "hard" RAM failure means the device is permanently damaged. This sort of thing usually occurs during the initial test period - the so-called burn-in. There are on the other hand "soft" failures that recover or occur only once. Soft failures can be caused by mains noise, static, c.r.t. flashovers or cosmic particles. No, we're not entering the realms of science fiction: it's a fact that our seven

Table 1: ASCII code for the SAA5050.

| Dec. | Binary | Means | Dec. | Binary | Means | Dec. | Binary | Means | Dec. | Binary |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0000000 |  | 32 | 0100000 | Space | 64 | 1000000 |  | 96 | 1100000 | - |
| 1 | 0000001 | Red* | 33 | 0100001 | ! | 65 | 1000001 | A | 97 | 1100001 |  |
| 2 | 0000010 | Green* | 34 | 0100010 | " | 66 | 1000010 | B | 98 | 1100010 | b |
| 3 | 0000011 | Yellow* | 35 | 0100011 | f | 67 | 1000011 | C | 99 | 1100011 | c |
| 4 | 0000100 | Blue* | 36 | 0100100 | \$ | 68 | 1000100 | D | 100 | 1100100 | d |
| 5 | 0000101 | Magenta* | 37 | 0100101 | \% | 69 | 1000101 | E | 101 | 1100101 | d |
| 6 | 0000110 | Cyan* | 38 | 0100110 | \& | 70 | 1000110 | F | 102 | 1100110 | f |
| 7 | 0000111 | White* | 39 | 0100111 |  | 71 | 1000111 | G | 103 | 1100111 |  |
| 8 | 0001000 | Flash | 40 | 0101000 | ( | 72 | 1001000 | H | 104 | 1101000 | h |
| 9 | 0001001 | Steady | 41 | 0101001 | ) | 73 | 1001001 | 1 | 105 | 1101001 | , |
| 10 | 0001010 | End box | 42 | 0101010 | * | 74 | 1001010 | J | 106 | 1101010 | j |
| 11 | 0001011 | Start box | 43 | 0101011 | + | 75 | 1001011 | K | 107 | 1101011 | k |
| 12 | 0001100 | Normal height | 44 | 0101100 | , | 76 | 1001100 | L | 108 | 1101100 | k |
| 13 | 0001101 | Double height | 45 | 0101101 | - | 77 | 1001101 | M | 109 | 1101101 | m |
| 14 | 0001110 |  | 46 | 0101110 |  | 78 | 1001110 | N | 110 | 1101110 |  |
| 15 | 0001111 |  | 47 | 0101111 | 1 | 79 | 1001111 | O | 111 | 1101111 | - |
| 16 | 0010000 |  | 48 | 0110000 | 0 | 80 | 1010000 | P | 112 | 1110000 | o |
| 17 | 0010001 | Redt | 49 | 0110001 | 1 | 81 | 1010001 | Q | 113 | 1110001 | p |
| 18 | 0010010 | Greent | 50 | 0110010 | 2 | 82 | 1010010 | R | 114 | 1110010 | a |
| 19 | 0010011 | Yellowt | 51 | 0110011 | 3 | 83 | 1010011 | S | 115 | 1110011 | s |
| 20 | 0010100 | Bluet | 52 | 0110100 | 4 | 84 | 1010100 | T | 116 | 1110100 | $t$ |
| 21 | 0010101 | Magenta $\dagger$ | 53 | 0110101 | 5 | 85 | 1010101 | $\cup$ | 117 | 1110101 | u |
| 22 | 0010110 | Cyant | 54 | 0110110 | 6 | 86 | 1010110 | $\checkmark$ | 118 | 1110110 | v |
| 23 | 0010111 | White $\dagger$ | 55 | 0110111 | 7 | 87 | 1010111 | W | 119 | 1110111 | w |
| 24 | 0011000 | Conceal | 56 | 0111000 | 8 | 88 | 1011000 | X | 120 | 1111000 | x |
| 25 | 0011001 | Norm. graphics | 57 | 0111001 | 9 | 89 | 1011001 | Y | 121 | 1111001 | Y |
| 26 | 0011010 | Sep. graphics | 58 | 0111010 | : | 90 | 1011010 | Z | 122 | 1111010 | Y |
| 27 | 0011011 |  | 59 | 0111011 | ; | 91 | 1011011 | $\leftarrow$ | 123 | 1111011 | $1 / 4$ |
| 28 | 0011100 | Black backg'd | 60 | 0111100 | $<$ | 92 | 1011100 | 1/2 | 124 | 1111100 | 1/4 |
| 29 | 0011101 | New backg'd | 61 | 0111101 | = | 93 | 1011101 | $\xrightarrow{ }$ | 125 | 1111101 | 3/4 |
| 30 | 0011110 | Hold graphics | 62 | 0111110 | ? | 94 | 1011110 |  | 126 | 1111110 | - |
| 31 | 0011111 | Release graphics | 63 | 0111111 | ? | 95 | 1011111 | \# | 127 | 111111 |  |

* Alphanumerals. $\dagger$ Graphics.

Notes: Graphics see Fig. 2. ASCII = American Standard Code for Information Interchange.

2102 s, innocently sitting there, are occasionally hit by charged particles from space or from other sources - even i.c.s emit them! The result can simply be that one of the cells is flipped over without damage. More often however one of the gate layers is punctured: this is not always permanent.

Êquipment for fault-finding can consist of just a meter (or logic probe) and, most importantly, an ASCII table (see Table 1 and Fig. 2). It's important to know which memory chip deals with which bit. We refer to the bits of a byte by number, starting with the left-most bit which is also referred to as the most significant bit (MSB) as it represents 64 . This is bit number one. The least significant bit (LSB), the right-most one, is equal to one. This is bit seven (our character set is a seven-bit one so we don't use a full-sized byte, i.e. one with eight bits). The RAM chips in this decoder are numbered IC6671-IC6677: IC6671 is


Fig. 2: Graphics characters are from 33 to 127 (ASCII code) and are built of six blocks. To ascertain the ASCII value of a graphic, add together the blocks and add 32 to the total. These are displayed if preceded by attribute 30 (hold graphics).
for bit seven, IC6672 for bit six, etc.
In the event of wrong characters note at least two wrong characters and decide what they should have been. Then see what the difference is in the binary ASCII code. You should find that only one bit differs between the correct and incorrect versions, and that this applies to all the wrongly displayed characters. Note that some characters will be correct despite the presence of the fault: these correspond to the ones in which the stuck cell or data line is stuck at the correct level. For example, bit seven stuck at one means that the even numbered codes can't be displayed. The displayed alphabet will consist of AACCEE etc. At the other end, bit one stuck at zero will make it impossible to count above 63 , so that codes from 64 to 127 will be displayed as zero to 63 . This means that the alphabet cannot appear. All you'll get is numerics, attributes and some punctuation marks. Clearly the possibilities are legion. For example, bit two stuck causes all letters to be in upper or lower case: bit two stuck at zero makes an attribute of anything with bit one low - this gives a very strange display, with psychedelic colours everywhere - whereas if bit two is stuck high the display is in monochrome with everything in lower case and no graphics.

The way in which the errors are displayed depends on whether a memory cell or data line is stuck. If a memory cell is stuck, one location only will show errors. A stuck data line will affect the whole screen. Returning to our earlier example of bit seven stuck high, if say row six column two shows D when it should show C one memory cell is defective and will produce display errors only when
it should contain an even code. If the bit seven data line is high however no even codes will be displayed anywhere on the screen.

When row or column address lines are stuck the effect is that groups of rows or columns are repeated depending on which bit is stuck or missing. The addresses can count only in steps of $2,4,8,16$ or 32 , remembering the bit of wizardry carried out in this decoder to make the RAMs compatible with the screen format. Problems here are usually due to faults in either one of the three 74LS chips in the row/column address decoder or because one of the five little white chokes in the column address lines is opencircuit. A logic probe with a pulse indication is useful here. The chokes can safely be shorted out.

There are many other fault possibilities. When two pins of one of the 2102 memory chips short together internally there will be all sorts of weird effects, the usual one being an almost blank screen with just one character repeatedly displayed at random. Check by removing each RAM i.c. in turn, followed by reselecting a page: when the faulty i.c. has been removed the display will return to the one byte missing condition, as when a data line is stuck low.

So this part of the decoder is not too bad after all - a little thought and detective work will sort out any problems.

## LSI Chip Faults

The various LSI chips can fail. The VIP and TIC chips usually give a blank screen with no text and the TAC chip incbility to select text or pages. An interesting variation occurs when an SAA5040 is fitted instead of an SAA5040A. The only difference is that the status displays

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for channels two and three (BBC-2/ITV) are transposed the converse is also true of course.

The TROM chip is first in the firing line in the event of any c.r.t. flashovers, so the output pins are prone to getting stuck. The funny one is when pin 16 (TLC transmitted large characters) which is connected to the TIC chip gets stuck, either due to a duff TIC or TROM chip: the RACK stops and the header row is repeated all down the screen. Remember that the outputs can be high, low or open-circuit. No luminance output affects only the mix mode: the result is not too obvious - the picture can be seen through the text. No blanking output (pin 25) gives mix mode instead of text; if this pin is stuck high there's text only, with no picture; if stuck low the text in the mix mode is faint. The results of the RGB oatputs packing up should be fairly obvious.


## ECONOMIC DEVICES, PO BOX 228, TELFORD TF2 8QP

| 1580 H | 330 | 2SA940 | 1.9 | $25 C 535$ | 0.79 | AF180 | 0.55 | BA656 | 159 | BC560C | 0.14 | 80X63A | 156 | BPF2 | 07 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15885R | 330 | 2SA940-2 | 214 | 2 SC 536 | 029 | AF181 | 0.53 | BA7100 | 10.5 | B6635 | 0.35 | B0Y20 | 1.21 | ${ }_{8 F}{ }^{\text {F79 }}$ | 0.96 | ${ }^{8 \times 1 \times 94}$ | 0.14 |
| 16039 | 0.79 | ${ }^{254950}$ | 0.12 | ${ }^{25 C 537}$ | 0.51 | AF186 | 0.53 | BA841A | 16.72 | BC536 | 0.2 | BDY81 | 1.18 | BrY90 | 0.6 | BM56 | 120 |
| 16181 | 1.0 | 2SA951 | 126 | 2 SC 505 L | 1.16 | AF239 | 0.13 | bAB43 | 356 | ВС637 | 024 | BF115 | 0.40 | BLY49 | 220 | BZY93c30 | 1.26 |
| 16182 | 1.04 | 2SA996-Y | 1.16 | $2 \mathrm{SC620}$ | 1.46 | AF279 | 0.0 | BAB54 | 5.76 | BC639 | 020 | BF117 | 0.56 | BROO | 022 | BZYBE RANGE | 0.10 |
| 16334 | 0.88 | 2SA999 | 136 | 2Sc6a3A | 159 | AL13 | 1.36 | bavis | 021 | BC540 | 024 | BF118 | 0.6 | BR01 | 0.75 | BZX61 RANGE | 0.18 |
| 16335 | 0.9 | 2 2S874 | 1.15 | ${ }^{2 S C 658}$ | 0.67 | ANH15 | 3.98 | BAV19 | 0.11 | BC879 | 0.39 | 8F121 | 0.25 | BROS | 0.75 | BZX79 RANGE | 0.10 |
| 16446 | 0.98 | 2SB185 | 1.13 | 2 2C681 | 4.40 | AN155 | 1.29 | bavzo | 0.31 | BC880 | 0.31 | BFi23 | 0.13 | ${ }_{\text {BROS }}$ | 125 | ${ }_{\text {Closd }}$ | 0.45 |
| 16600 | 138 | ${ }^{258375}$ | 3.7 | ${ }^{25 C 688}$ | 188 | AN206 | 250 | BAV21 | 0.34 | ВСхз | 0.40 | BF127 | 0.13 | BRC116 | 0.67 | C106M | 0.76 |
| 16802 | 17 | 2 284400 | 0.40 | ${ }^{2 S C 684}$ | 1.05 | AN208 | 35 | BAW62 | 0.19 | вCryo | 0.30 | BF137 | 0.20 | BRC300 | 201 | C1129 | 0.58 |
| 17052 | 5.51 | 2 288405 | 1.03 | $2 \mathrm{SC693}$ | 0.50 | AN210 | 278 | BAX12 | 0.4 | BC71 | 021 | ${ }_{\text {BFF }} 153$ | 0.58 | BRC5296 | 0.7 | CA3046 | 206 |
| 17053 | 5.51 | 2SB407 | 324 | $2 \mathrm{SC710}$ | 0.50 | AN211 | 325 | BAX13 | 0.11 | BC72 | 020 | BF154 | 0.25 | BRC6109 | 0.83 | CA3099 | 0.83 |
| 17074 | 9.30 | 2S84498 | 6.93 | 2SC711A | 0.50 | AN2140 | 275 | BAX16 | 0.11 | BD115 | 0.46 | BF157 | 0.33 | BRC82 | 1.08 | casosala | 325 |
| 17089 | 5.35 | ${ }^{288511}$ | 250 | ${ }^{2 S C 717}$ | 128 | AN231 | 14.65 | BC107 | 0.13 | 80116 | 0.70 | BF158 | 0.18 | BRC83 | 219 | Ca3094 | 220 |
| 17127 | 3.51 | ${ }^{2 S 854}$ | 139 | $2 \mathrm{SC734}$ | 1.43 | AN234 | 5.58 | bCiola | 0.11 | 80124 | 131 | BF159 | 0.18 | BRCO4 | 208 | CA3131EM | 3.12 |
| 17376 | 1.58 | ${ }^{288546}$ | 375 | ${ }^{2 S C 761-Y}$ | 0.55 | AN236 | 378 | BC1078 | 0.18 | 8D124P+KIT | 0.09 | BF160 | 0.31 | BRX44 | 0.90 | CBF16848N-071 | 1.56 |
| 17523 | 132 | ${ }^{258565}$ | 200 | ${ }^{25 C 7783}$ | 3.98 | AN239 | 589 | BC108 | 0.15 | ${ }^{80131}$ | 0.42 | ${ }^{\text {BFF167 }}$ | 0.30 | ${ }^{\text {BRXX49 }}$ | 0.53 | CD4000 | 0.38 |
| 17524 | 1.32 | 2S86184 | 22 | ${ }^{25 C 730 \%}$ | 1.64 | AN240P | 1.52 | ${ }^{\text {BC1 } 1888}$ | 0.15 | 80132 | 0.2 | ${ }^{\text {BFI73 }}$ | 0.34 | BRY39 | 0.59 | CD4002 | 0.7 |
| in400 | 0.06 | ${ }^{2588631}$ | 325 | ${ }^{25 C 828}$ | 0.28 | AN241 | 1.7 | BC109 | 0.12 | ${ }^{80133}$ | 0.53 | BF1T | 0.35 | BSS38 | 0.87 | CD4008 | 135 |
| 1 14002 | 0.06 | ${ }^{258643}$ | 0.54 | 25 C887A | 3.05 | AN245 | 4.49 | BCL1098 | 0.15 | 80135 | 0.36 | BF178 | 0.60 | BSTB0140G | 525 | CD4011 | 029 |
| 1 1 4003 | 0.06 | ${ }^{258659}$ | 3.7 | ${ }^{25 C 876}$ | 0.56 | AN253 | 297 | ${ }^{\text {BCI } 109}$ | 0.12 | ${ }^{80136}$ | 0.25 | BF179 | 0.35 | BSTCO246 | 725 | CD4012 | 024 |
| ${ }^{1} \mathrm{~N} 4004$ | 0.05 | 2S8681 2S8695 | 3.96 158 | ${ }_{2}^{2 S c} 5838$ | 0.54 | AN260 | 336 | ${ }^{\text {BCII }} 13$ | 0.14 | ${ }^{80137}$ | 0.35 | ${ }^{\text {BFIP0 }}$ | 0.36 | BSTCO233 | 725 | CD4013 | 0.47 |
| ${ }^{1} \mathrm{~N} 4005$ | 0.08 |  | 19 | ${ }_{2 S}{ }^{25 c 935}$ | 4.13 | AN262 | 1.98 | BC119 | 0.35 | ${ }^{80138}$ | 0.45 | BF181 | 0.32 | ${ }^{\text {BSTCCOOL43 }}$ | 307 | CD4016 | 0.46 |
| 1/2006 iN4007 | 0.09 | $\left\lvert\, \begin{aligned} & 2 S B 75 \\ & 2 S B 774 \end{aligned}\right.$ | 1.04 | ${ }^{2 S C 336}$ | 8.56 | AN272 | 7.98 | BC126 | 020 | ${ }^{80} 139$ | 0.3 | BF182 | 0.34 | BSTD1043 | 28 | CO4017 | 0.92 |
| 1N4007 iN4148 | 0.07 | $\begin{aligned} & 2 \text { 2SB774 } \\ & 2 S B 819 \end{aligned}$ | 0.08 | ${ }^{2 S C 940}$ | ${ }_{2} 4.90$ | AN281 | ${ }_{50} 6$ | BC132 | 0.14 | 80140 | 0.37 | ${ }^{\text {BFIP3 }}$ | 039 | BSV578 | 3.48 | CO4420 | 123 |
| ${ }^{\text {N4, }} 148$ | 0.04 | ${ }_{2}{ }^{2 S} 881924$ | 0.89 | 2SD1128 | 230 | AN295 | 559 | BC135 | 0.14 | 80144 | 1.70 | BF184 | 0.6 | BSW58 | 0.50 | CD4021 | 0.39 |
| (1N4488 | 0.005 | $\begin{array}{\|l} \text { 2SC1034 } \\ \text { 2SC1050 } \end{array}$ | 6.75 5.06 | ${ }^{\text {2SD1138 }}$ | 0.95 | AN301 | ${ }_{359} 5$ | ${ }^{\text {BCI37 }}$ | 0.18 | 80150 | 125 | ${ }^{\text {BFIP5 }}$ | 0.39 | ${ }^{\text {BSX1 }} 19$ | 0.34 | CD4023 | 028 |
| 1 N5402 | 0.15 | ${ }^{2 S C 1096}$ | 1.16 | ${ }^{2 S D 1453}$ | 0.75 | AN303 | 4.39 | ${ }^{8 \mathrm{BC}} \mathrm{BC} 389$ | 031 | ${ }_{80150}$ | 1.60 | ${ }_{\text {BFIOs }}$ | 0.14 | BSX20 | 03 | C04022 | 0.64 |
| 1 N 403 | 0.16 | 2SC1104 | 3.8 | 2SD152K | 251 | AN305 | 9.7 | BC140 | 0.45 | BD163 | 0.7 | BF196 | 0.17 | ${ }^{\text {BSY79 }}$ | 0.51 | CD40408 | 0.85 |
| iN5404 | 0.15 | 2SC1106 | 4.5 | 2SD198 | 3.7 | AN315 | 245 | BC141 | 0.3 | 80165 | 0.62 | BF197 | 0.16 | BT100A | 1.6 | C0.4047 | 1.06 |
| 1 N 5408 | 0.35 | ${ }^{2 S C 1114}$ | 6.75 | 2 2SD234 | 0.49 | AN316 | 553 | BC142 | 0.3 | 80166 | 0.42 | BF198 | 0.17 | Вт 106 | 1.55 | CD4049 | 0.45 |
| $1 \mathrm{NO14}$ | 0.04 | 2SC1116 | 4.95 | 2 2S235 | 0.60 | AN318 | 6.71 | BC143 | 0.3 | BD168 | 0.3 | BF199 | 0.17 | ВT108 | 1.65 | CO4052 | 0.75 |
| IR3403 | 5.00 | ${ }^{2 S C 1124}$ | 120 | ${ }^{2 S D 24}$ | 229 | AN320 | 5.47 | BC147 | 008 | 80175 | 0.60 | BF200 | 0.37 | BT119 | 1.76 | C04066 | 0.38 |
| ${ }_{\substack{1 \\ 1 \\ 1 \\ 1 \\ 1545}}$ | 0.20 | ${ }^{2 S C 1129}$ | 0.30 | ${ }_{2}^{2 S D 257}$ | 29 | AN321 | 225 | BC1488 | 0.10 | 80179 | 0.49 | ${ }^{85218}$ | 0.36 | BT120 | 217 | C04069 | 029 |
| 1 155012A | 0.81 | ${ }^{2 S C 1158}$ | 330 | ${ }_{2 S}{ }^{\text {2S313 }}$ | 259 | AN331 | 4.59 |  | 0.13 0.11 | ${ }^{80181}$ | 0.99 | ${ }_{8 F 237}^{8 F 24}$ | 0.17 | ${ }^{8 T 121}$ | 24 | CD4070 | 0.65 |
| 15921 | 0.10 | 2SC1162 | 1.05 | 2503250 | 1.95 | AN37 | 5.37 | BC149 | 0.11 | BD183 | 0.99 | BF240 | 0.17 | TBA970 | 3.06 | ${ }^{\text {co4093 }}$ | 0.35 |
| 2 N 1303 | 03. | 2SC1172 | 22 | 2SD348 | 16.13 | AN340P | 1.17 | BC1498 | 0.13 | 8D184 | 121 | BF241 | 0.17 | BT151-800R | 1.15 | CDS511 | 1.10 |
| 2 22219A | 0.40 | ${ }^{2 S C 1195}$ | 37 | ${ }^{2 S D 350}$ | 520 | AN355 | 5.59 | BC153 | 0.14 | 80187 | 0.53 | BF245 | 0.50 | В 1 ¢5018 | 20 | CD4528 | 204 |
| ${ }^{2}$ N2223 | 0.38 | ${ }^{2 S C 1212 A}$ | 1.5 | ${ }^{2 S} 2$ DJ35a | 200 | AN362 | 1.75 | BC154 | 0.14 | 80189 | 0.80 | BF245A | 0.37 | BT8124 | 4.89 | CD4556 | 3.4 |
| ${ }^{2} \mathbf{N} 2646$ | 0.80 | ${ }^{\text {2SC1213 }}$ | 0.89 | ${ }_{2 S 03535}$ | 7.50 | AN370 | 338 | BC159 | 0.35 | 8D190 | 0.80 | BF245B | 0.49 | BU106 | 248 | CRO2AM-8 | 1.50 |
| 2N2905 | 0.6 | 2SC1280 | 0.90 | $2 S 0401$ | 255 | AN5111 | 29 | BC160 | 0.0 | 8020 | 0.53 | BF246A | 252 | BU108 | 1.50 | CV12E | 307 |
| 2N2906 | 0.38 | ${ }^{2 S C 1306}$ | 1.98 | 2 SD 14 | 1.98 | AN5120N | 4.50 | BC168 | 0.36 | BD203 | 050 | ${ }_{8 F 256}$ | 03 | ${ }^{\text {BU10 }}$ | 50 | Cx0950 | 3.14 |
| 2N2926 | 0.15 | 2SC1316 | 4.10 | 2SD471 | 213 | AN5132 | 4.39 | BC169C | 0.16 | 80204 | 098 | BF256L8 | 0.2 | BUIIIY | 4.16 | Cx104 | 9.64 <br> 10.50 |
| 2 N 3053 | 027 | 2SC1317 | 0.87 | 2 25560 | 295 | AN5250 | 209 | BC170 | 0.16 | BD207 | 1.79 | BF256ic | 0.2 | BU125 | 240 | Cx109 | 785 |
| 2 N 3054 | 0.98 | ${ }^{2 S C 1364}$ | 0.48 | 2S5588A | 1.98 | AN5435 | 308 | BC171 | 0.11 | BD208 | 123 | BF257 | 0.3 | BU126 | 1.5 | Cx130 | 8.76 |
| 2N3055 | 0.61 | 2SC1383 | 120 | 2SD600 | 30 | AN5610 | 7.6 | BC172 | 0.13 | BD22 | 0.49 | BF258 | 0.36 | BU137 | 925 | Cx134 | 11.04 |
| 2N3442 | 1.14 | ${ }^{2 S C 1391}$ | 205 | 2SD601R | 0.65 | AN5612 | 3.81 | BC1728 | 0.27 | 8023 | 0.49 | BF259 | 0.34 | 8U205 | 1.08 | Cx136 | 11.49 |
| ${ }^{2133702}$ | 0.14 | ${ }^{25 C 1398}$ | 0.4 | ${ }^{2 S D 613}$ | 1.03 | AN5613 | 380 | BC173 | 0.17 | B0278 | 0.03 | BF262 | 0.57 | BU206 | 17 | Cx139 | 11.83 |
| ${ }^{2133703}$ | 0.14 | ${ }^{2 S C 14134}$ | 3.05 | ${ }^{2} 2$ S6621 | 1257 | ans630 | 3.55 | BC1748 | 027 | ${ }^{80239}$ | 1.05 | ${ }^{\text {BF223 }}$ | 0.57 | BU207 | 1.65 | CX157 | 4.84 |
| 2N3705 2N3706 | 0.16 | 2SC1446 | 120 | ${ }_{\text {2SO636 }}^{\text {2SD }}$ | 0.55 | AN5701N | $\underline{1.65}$ | ${ }^{\text {BC1717 }}$ | 020 | ${ }^{80232}$ | 050 | ${ }_{\text {BF271 }}$ | 0030 |  | 1.12 | ${ }^{\text {Cx1 }} 58$ | 4.10 |
| 2N3707 | 0.16 | ${ }^{2 S C 1475}$ | 0.31 | 2S0655 | 0.98 | ANG300 | 700 | ${ }^{\text {BC179 }}$ | 0.25 | ${ }^{80237}$ | 0.4 | ${ }^{\text {BF274 }}$ | 0020 | ${ }^{\text {Bu }}$ | 1.12 | Cx187 | ${ }_{5}^{675}$ |
| 2 N 3711 | 0.11 | 2SC1505 | 1.00 | 2 20657 | 285 | AN6310 | 8.74 | BC182 | 0.09 | B0238 | 0.45 | BF324 | 023 | BU2080 | 1.95 | CX755 | 1205 |
| 2N3771 | 204 | ${ }^{2 S C 1514}$ | 13 | 2SD661A | 0.80 | ANG320N | 428 | BC182L | 0.10 | 80239 | 0.6 | BF336 | 0.33 | BU209 | 128 | CX885A | 689 |
| ${ }^{2} \mathrm{~N} 372$ | 1.71 | ${ }^{2 S C 1553}$ | 125 | 2 2SD731 | 255 | AN6340 | 6.46 | BC182LB | 0.14 | 80240 | 0.51 | BF337 | 0.40 | BU228 | 295 | DEC1 | 220 |
| 2N373 | 229 | 2SC1578 | 8.74 | $2 \mathrm{SD773}$ | 0.33 | AN6341 | 4.00 | BC1834 | 0.11 | BD241 | 0.39 | BF338 | 0.40 | BU326 | 200 | DEC2 | 220 |
| 2N3819 | 0.42 | 2SC1583 | 1.17 | 2 2SD811 | 559 | angzar | 1.51 | BC183LB | 0.25 | BD242 | 0.39 | BF355 | 0.49 | BU328A | 220 | DS3486 | 433 |
| ${ }^{2} 133823$ | 1.17 | ${ }^{25 C 1617}$ | 388 | ${ }^{250823}$ | 1.98 | Ang333 | 16.00 | BC184 | 0.13 | ${ }^{\text {B2a } 234}$ | 037 | BF362 | 0.56 | BU326S | 220 | DS3487N | 4.33 |
| ${ }_{2}^{2}{ }_{2} \mathbf{N} 39394$ | 0.02 | 2SC675 2SC1678 | 1.41 | ${ }_{2} 2 \mathrm{SDO837}$ | 120 | AN6371 | ${ }_{7}^{650}$ | BC184L | 0.14 | ${ }^{80213 C}$ | 0.79 | ${ }^{\text {BFF333 }}$ | 0.00 | ${ }^{\text {B44 }}$ | 1.19 | E1222 | 0.40 |
| 2N4101 | 1.33 | ${ }^{2 S C 1741}$ | 125 | ${ }^{2} 250856$ | 225 | ANA383 | 195 | ${ }_{\text {BCI86 }}$ | 028 | 80244 | 0.51 | ${ }^{85} 8391$ | 0.50 | 8U4060 | 1.78 | E5024 | 028 |
| 2 N 240 | 330 | 2SC1810 | 1.70 | 2 SD 8570 | 1.54 | AN6551 | 1.35 | BC187 | 028 | BD245C | 0.95 | BF417 | 0 O | ${ }_{\text {B44 }}$ | 1.00 | E9003 | 0.45 |
| 2 N 444 | 0.90 | 2SC1815 | 0.65 | 250882 | 1.50 | AN6552 | 0.65 | Вс204 | 0.16 | BD246C | 0.30 | BF418 | 1.87 | BU412 | 9.15 | E9005 | 0.50 |
| ${ }^{2}$ N5239 | 0.50 | ${ }^{2 S C 1828}$ | 0.05 | ${ }^{2 S 0894}$ | 1.50 | AN6610 | 240 | 8C207 | 0.14 | BD253 | 1.05 | BF422 | 029 | BU426A | 1.5 | ESM310BP | 4.15 |
| 2N5294 2 2N5296 | 0.50 | 2SC1829 2SC1875 | 22 | ${ }^{\text {2SOB98 }}$ | 25.4 | AN667\% | ${ }^{6.50}$ | ${ }^{8 C 212}$ | 0.11 | ${ }^{\text {B20 278A }}$ | 0.80 | ${ }^{\text {8F423 }}$ | 0.52 | BU500 | 1.95 | FND500 | 5.78 |
| 2N5297 | 0.50 | 2SC1881K | 298 | ${ }_{2 S k}{ }^{\text {2Sk }}$ | 295 | ANT114E | ${ }_{59} 1$ | ${ }_{\text {BCl }}^{\text {BC2128 }}$ | 0.10 | BD317 BD318 | 200 | ${ }^{87450}$ | 0.3 | 8U508A | 158 | GC374 | 1.55 |
| 2N5298 | 0.61 | 2SC1893 | 302 | 2SK34 | 0.76 | AN7115 | 1.75 | BC213LB | 0.15 | BD375 | 0.9 | BF457 | 0.41 | ${ }^{\text {BU }}$ | 265 | ${ }^{60243}$ | 4.85 |
| 2N5771 | 1.18 | 2SC1906 | 0.98 | 2SK41 | 1.07 | AN7120 | 4.65 | BC214 | 0.10 | BD380 | 0.76 | BF458 | 0.39 | BUT05 | 4.07 | ${ }_{6}$ | 18 |
| ${ }^{2}$ N6109 | 1.58 | ${ }^{2 S C 1921}$ | 137 | 2SK79 | 298 | AN7145 | 280 | BC214L8 | 0.25 | 8D410 | 0.52 | 8F459 | 0.52 | Bu806 | 1.79 | HA11215 | 5.06 |
| ${ }^{\text {2N6130 }}$ | 0.72 | ${ }^{25 \mathrm{SC}} 1923$ | 1.07 | 40408 | 0.50 | AN7146 | 4.35 | BC25 | 0.40 | BD433 | 0.47 | 8F460 | 156 | BU807 | 0.80 | HA11211 | 2.53 |
| 2 N 6133 | 125 | ${ }^{2 S C 1929}$ | 225 | 40594 | 1.53 | AN7151 | 225 | BC237 | 0.10 | BD434 | 0.49 | BF469 | 0.31 | BU828A | 215 | HA11225 | 429 |
| ${ }^{\text {2N6 }}$ N6292 | 0.95 | 2SC1945 | 5.50 | 4EX581 | 1.13 0.90 | AN7156 | 285 | ${ }_{\text {BC238 }}{ }^{\text {BC273J }}$ | 0.12 | ${ }^{80435}$ | 0.69 | ${ }^{85470}$ | 0.05 | BUW84 | 138 | HA11226 | 8.7 |
| 2N696 | 0.43 | 2SC1959 | 0.31 | 741 | 0.30 | AN7218 | 1.64 | BC238A | 0.13 | ${ }^{80437}$ | ${ }_{0}^{0.60}$ | ${ }^{\text {Bra72 }}$ | 0.33 | BUX84 | 1.00 | HA11229 | 288 |
| 2N698 | 0.43 | 2SC1957 | 0.55 | 7805-T022 | 0.63 | AN7223 | 425 | BC2388 | 0.13 | BD438 | 0.40 | B5479 | 0.61 | BUY69a | 204 | HA11124 | 2438 |
| 2SA1006 | 1.50 | 2SC1953 | 193 | 7806 | 0.3 | AU107 | 350 | BC239 | 0.12 | BD441 | 1.0 | BF480 | 0.60 | ${ }^{\text {BY126 }}$ | 0.13 | ${ }_{\text {HA11244 }}$ | 280 |
| 2SA1011 | 1.05 | ${ }^{25 C 1962}$ | 198 | 7808 | 0.5 | AU110 | 225 | вс2398 | 025 | BD442 | 0.66 | Br491 | 0.38 | BY127 | 0.13 | HA11251 | 4.47 |
| ${ }_{\text {2SA }}$ SA1015 | 0.0 | 2SC198939 | 310 | ${ }_{7815}^{7812-1022}$ | 1.16 | ${ }_{\text {AU }}{ }_{\text {Al13 }}$ | 525 | ${ }^{\text {BC2531a }}$ | 0.12 | ${ }^{\text {BD509 }}$ | 1.0 | ${ }^{\text {BF495 }}$ | 0.54 | ${ }^{\text {BY133 }}$ | 0.11 | HA1125 | 429 |
| 2SA1020Y | 0.85 | 2SCIges | 0.55 | ${ }_{7818}$ | 0.58 | ${ }_{\text {AYıOS }}$ | 208 | ${ }^{8 .} 8$ | 0 | ${ }^{\text {BD5 }} 10$ | 1.0 | BF506 | 0.6 | ${ }^{8 Y 164}$ | 0.47 | HA137W | 287 |
| 2SA1027R | 0.45 | 2SCron9 | 0.34 | 7824 | 0.54 | BA524 | 82 | BCOO1 | 0.6 | ${ }^{\text {BD529 }}$ | 1.30 | ${ }_{8}{ }_{5} 23$ | 024 | ${ }^{817179}$ | 0.92 | HA1138 |  |
| 2 2SA73 | 0.75 | $2 \mathrm{SC2029}$ | 233 | 7905 | 0.80 | 8250 | 205 | BC302 | 0.58 | 80530 | 1.10 | BF532 | 0.45 | BY182 | 1.05 | HA1144 | 7.7 |
| ${ }^{2 S A 7665}$ | 4.58 | ${ }^{\text {2SC72028 }}$ | 211 | 9358 | 10.70 | 840 | 1.5 | BC303 | 1.04 | ${ }^{\text {BD5 } 533}$ | 0.67 | $\mathrm{BF}^{596}$ | 0.18 | BY184 | 0.47 | HA1156 | 1.16 |
| ${ }^{2 S C 1173 Y}$ | 125 | $2 \mathrm{SC2ab3}$ | 0.98 | AA133 | 0.12 | BA130 | 0.14 | BC307 | 0.18 | BD534 | 0.53 | BF597 | 0.27 | BY197 | 0.7 | HA1160 | 4.78 |
| ${ }_{2 S}^{2 S C 1474}$ | 12 | ${ }^{2 S C 20778}$ | 239 | ${ }^{\text {ACI33 }}$ | 0.12 | ${ }^{\text {BAA } 1310}$ | 1.98 | BC307A | 0.14 | ${ }^{80555}$ | 0.78 | $8 \mathrm{Bf694}$ | 02 | BY189 | 1.79 | HA1166 | 525 |
| ${ }^{\text {2SCLI }}$ 2S09 ${ }^{\text {S }}$ | 1.35 3.95 | ${ }_{\text {2SC2073 }}{ }^{2 S}$ | 1.54 | AC123k ACin | 0.43 | BA1320 BA132 | 138 395 | BC308 BC308A | 0.18 | ${ }^{805536}$ | 0.91 | ${ }^{87757}$ | 005 | ${ }^{\text {BY198 }}$ | 1.20 | HA1166X | 5.36 |
| 2SA1095 | 4.10 | $2 \mathrm{SC2091}$ | 130 | ${ }^{\text {ACC128 }}$ | 0.34 | BA1330 | 275 | ${ }_{\text {BC309 }}$ | 0.17 | ${ }^{80} 5538$ | 1.18 | ${ }_{\text {BF761 }}$ | ${ }_{0}^{0.4}$ | BY2012 | 1.50 | HA1167 | 5.35 |
| ${ }_{2}$ SA11103 | 8.5 | ${ }_{2 S C 2141}$ | 1.56 | ${ }^{\text {A Cl138 }}$ | 024 | BA145 | 0.19 | BC317A | 0.13 | BD544 | 0.38 | BF762 | 0.75 | ${ }_{\text {BY207 }}$ | 027 | HA11705 | 800 |
| ${ }^{2 S A 329}$ | 0.00 | ${ }^{2 S C 2156}$ | 198 | AC141 | 020 | BA148 | 0.30 | 8c327 | 0.15 | 8 C 588 | 125 | 8F869 | 0.65 | BY208 | 0.45 | HA11703 | 9.56 |
| ${ }^{2 S A 351}$ | 1.17 | ${ }^{25 C 2} 216$ | 0.00 | ${ }^{\text {ACLI42K }}$ | 0.43 | ${ }^{\text {BA154 }}$ | 0.0 | BC328 | 0.11 | ${ }^{80677}$ | 0.53 | 8 F 780 | 0.30 | BY210-400 | 0.18 | HA11701 | 9.56 |
| 2SA489 2SA490 | 1.17 | 2SC2333 $2 S \mathrm{Cz236}$ | 220 | ${ }^{\text {AC151 }}$ | 0.03 | ${ }^{\text {BA }}$ B4155 | 0.12 | ${ }_{\text {BC3 }}{ }_{8}$ | 0.09 | ${ }^{8 D 679}$ | 0.57 | ${ }^{\text {BFFS59 }}$ | 0.02 | ${ }^{\text {Br }}$ B10-600 | 027 | HA11710 | 9.50 |
| 2 SA493 | 225 | 2 SC 2778 | 1.14 | AC179 | 028 | ${ }^{\text {BA159 }}$ | 0.12 | ${ }_{\text {BC3 }} \times 8$ | 024 | ${ }_{80681}$ | 1.4 | ${ }_{\text {BF970 }}$ | ${ }_{0} 0.9$ | ${ }_{\text {BY218 }}$ | 1.64 | HA1713 | 8.13 20.15 |
| ${ }_{2} 254562$ | 0.57 | ${ }_{2 S \mathrm{~S} 2314}$ | 217 | ${ }^{\text {ACI } 183}$ | 0.72 | BA182 | 029 | BC440 | 1.08 | BD696 | 27 | BFF39 | 0.44 | $8 Y 23$ | 123 | HA11715 | 8.13 |
| 2SA564 | 0.58 | ${ }_{2 S C 2}^{2 S 535-11}$ | 10.41 | ${ }^{\text {ACC187 }}$ | 0.39 | BA232 | 1.12 | ${ }^{\text {BC441 }}$ | 0.4 | ${ }^{\text {BDG999 }}$ | 3.49 | BFP61 | 0.50 | BY224-600 | 1.88 | HA11714 | 7.76 |
| 2SA614 | 4.88 1.14 | 2SC2551 | 123 | AC187K AC188 | 0.43 | ${ }_{\text {BA3311 }}^{\text {BA32 }}$ | 1.24 | ${ }_{\text {BC454 }}$ | 036 | ${ }^{\text {BDOT00 }}$ | 3100 | Bff62 | 0.50 | BY2z-100 | 1.13 | HA11716 | 13.10 |
| 2546995 | 1.50 | 2SC2570 | 1.5 | ${ }^{\text {AC1 } 188-01}$ | 0.49 | BA312 | 0.97 | ${ }_{\text {BCA61 }}$ | 0.4 | ${ }^{\text {BDO }}$ 809 | 1.12 | ${ }_{\text {BFRP81 }}$ | 0 | ${ }^{8 Y} 827$ | 0.05 |  | 1826 1600 |
| 2SA659 | 0.19 | 2SC257 | 1.75 | AC188K | 0.4 | BA313 | 0.75 | ${ }^{\text {BC462 }}$ | 1.15 | BD710 | 0.20 | BFR26 | 1.0 | ${ }^{81}$ | 0.60 | HA11725MP | ${ }_{6}^{16.00}$ |
| ${ }^{25 A 573}$ | 17 | ${ }_{2 S \mathrm{C} 2578}$ | 6.5 | AC193k | 0.55 | bA317 | 0.05 | BC463 | 0.61 | BD809 | 0.75 | BFP89 | 1.63 | 8Y229-1000 | 1.12 | HA11781 | 8.50 |
| ${ }^{254656}$ | 1.61 | ${ }^{2 S C 22771}$ | 1.90 | ${ }^{\text {ACL }}$ S 14 K | 0.55 | BA318 | 0.09 | ${ }^{\text {BC47 }}$ | 037 | B0810 | 0.09 | BFFPsa | 130 | ${ }^{8 Y 229500}$ | 0.98 | HA1180 | 5.15 |
| 2SA697 2SA699 | 10.82 | ${ }_{\text {2SC2828 }}$ | 207 | ${ }_{\text {AD }}$ AD 143 | 1.06 | ${ }^{\text {BA328 }}$ | 4.7 | BC478 | 0.38 | BD879 | 0.74 | 8F42 | 0.43 | BY255 |  | HA1198 | 7.03 |
| 2 2SA715 | 0.95 | ${ }^{2553153}$ | 5.26 | ${ }_{\text {AD }}{ }^{\text {AD }} 145$ | 1.50 | ${ }_{\text {BA33 }}$ | 6.17 | ${ }^{\text {BC539 }}$ | 0.28 | ${ }_{\text {BD895 }}$ | 207 | 8F743 8 FF 84 | 0.03 | ${ }^{\text {BYY295 }}$-600 | 1.03 | HA13301 HA1306 | ${ }_{225}^{625}$ |
| 2 2A747 | 826 | $2 \mathrm{SC372}$ | 1.40 | AD161 | 0.56 | BA5102A | 37 | BC546 | 0.17 | ${ }^{81899}$ | 24 | BFW10 | 0.00 | ${ }_{\text {BY299 }}$ | 0.00 | ${ }_{\text {Hal }}$ | 220 |
| 2SA748 | 1.08 | ${ }^{25 C 373}$ | 1.16 | AD162 | 0.6 | BA511 | 232 | 8C547 | 0.10 | BD901 | 0.79 | $8 \mathrm{Br} \times 29$ | 0.34 | BY407 | 0.84 | HA1339 | 230 |
| ${ }_{2 S A B 17}$ | 0.65 | 2 SC 333 | 1.35 | AD262 | 125 | BA514 | 225 | BC548 | 0.10 | 8D932 | 085 | 8fx84 | 0.31 | ${ }^{8 Y 409}$ | 1.49 | HA13402 | 787 |
| 2SAB18 2SAB35 | 180 250 | ${ }_{2 S c}{ }^{2 S c 39898}$ | 0.00 | ${ }_{\text {AFP }}^{\text {AF1 }}$ A 14 | 247 | ${ }_{\text {BA524 }}$ | 200 | ${ }_{8}^{8 C 549}$ | 0.10 | BDWB3C BDW | ${ }_{1} 15$ | - ${ }^{8 \times 1} 885$ | 0.41 | ${ }^{8 Y 448}$ | 0 | HA13342 | 205 |
| 2SAB36 | 009 | ${ }^{2 S C 4} 43 \mathrm{C}$ | 039 | AF118 | 120 | ${ }^{\text {BA526 }}$ | 79 | ${ }^{\text {BC555 }}$ | 0.16 | BD×32 | 1.75 | ${ }_{8 \times 8 \times 8}$ | 0.55 | BYW19/1000 | 1.10 | HA13365 HA1356WR | ${ }_{180}$ |
| ${ }^{2 S A B 44}$ | 0.30 | ${ }^{25 C 41}$ | 219 | AF127 | 0.50 | BA527 | 298 | BC557 | 0.10 | B0X53A | 4.93 | BFX88 | 0.34 | Brws | 0.34 | HA1367 | 4.38 |
| ${ }^{\text {2SABAB7 }}$ | 0.70 215 | 2SC458 | 0.39 | ${ }_{\text {AFP139 }}^{\text {AFF }}$ | 0.53 | ${ }_{\text {BAF32 }}$ | 207 | ${ }^{8 C 558}$ | 0.10 | ${ }^{80 \times 538}$ | 335 | BEX89 | 0.40 | ${ }^{\text {BYX10 }}$ | 029 | HA1388R | 245 |
| ${ }^{2 S} 2$ SAB37\% | 20.9 | ${ }^{\text {2SC55s }}$ | ${ }_{2} 8$ | ${ }_{\text {AF179 }}$ | 0.55 | ${ }_{\text {BA6 } 209}^{\text {BA3 }}$ | 2.75 | ${ }_{8}^{8 \mathrm{C} 55998}$ | 0.10 |  | 216 215 | ${ }^{\text {BFY50 }}$ | 0.38 | 8Yイ55.600 | 0.19 125 | HA13588 HA1370 | 1.90 30 |
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# VCR Clinic 

## Reports from Christopher Holland, Les Harris, Philip Blundell, Eng. Tech., Steve Illidge and Mick Dutton

## JVC HRD140 - Ferguson 3V44/45

The latest generation of JVC VCRs have been around for about a year. Though proving to be reliable a fair number have appeared in our workshops in recent months. I'd hesitate to describe the following as stock faults: we've nevertheless encountered most of them more than once.
First a note about the circuit protectors used in the power supply. These look like two-legged transistors and appear to go open-circuit for little or no reason. Different sets of symptoms occur when the various d.c. lines produced by the power supply panel are absent. With any VCR that appears to be non-functional or has all the motors spinning at switch on, first check the unswitched 12 V line and the switched 5 V and 12 V lines. Replacement of the appropriate circuit protector will normally provide a complete cure. Note that it's also easy to cause them to fail while you're working on a machine. The unswitched 12 V line remains throughout the machine even when the front operate switch is at off, and there's no on-off switch at the back. Don't let the meter's probe slip while checking the output at plug CN3 of the power supply. Absence of the switched 5 V line with the relevant circuit protector intact can be caused by Q10 and D3 on the power supply panel.

The use of resistors in place of circuit protectors is not recommended. Even very small value resistors will produce a voltage change that can interfere with normal working. Here's an example. The problem with the machine was that the drum motor would not spin when the tape loaded to the heads. This was eventually traced to someone having used a $4.7 \Omega$ resistor in place of a circuit protector in the switched 12 V line.

Some other problems. The tape loading half way to the heads then returning to the cassette is due to the absence of drum pickup head pulses. I've had the lead open-circuit at the head, also a defective head where the pin fell out of the head body. If the machine plays for a few seconds then unloads, with fast forward or rewind for only a few seconds, the take-up pulses are missing: I've twice had Q1 on the deck terminal faulty - on both occasions the transistor checked o.k. on an ohmmeter.

The symptoms associated with absence of the switched 12 V line are that the operate indicator comes on as soon as the machine is plugged in, the drum and capstan motors turn, the machine switching itself off after a few seconds. Should these symptoms continue after replacing the appropriate circuit protector, or if the protector is intact, check the outputs from the two loading sensors. These should give d.c. levels of 0 V and 12 V at pins 34 and 35 of the main microcomputer chip. If either level is wrong yet both loading arms are back in the cassette housing the timing of the gear train from the loading motor has slipped. Ideally you'll need a second open VCR to see how to put it all back together again. Why does the timing slip? Check that the back-tension arm is not fouling the left-hand loading arm during the unloading procedure.

Two problem areas with the previous generation of JVC machines were the cassette housing and a tendency for the video heads to clog with dirt very easily. The latest machines do not suffer from these problems to the same extent. If you have to remove the screening plate over the heads for any reason, take care when replacing it - it's
very easy to dry-joint Q1 on the head motor driver amplifier panel but very difficult to resolder this properly. There speaks the voice of experience!

On one occasion when I thought I had an instance of dirty heads the culprit turned out to be IC102, which is really a luminance subassembly soldered in at right-angles to the main PCB. Each to his own way of removing it. I've also had this assembly cause picture overloading after a few seconds of play, a squirt of freezer putting things right again for a further few seconds.
A case of failure to record was caused by the 9 V line to pin 2 of IC101 being absent: Q111 had gone open-circuit.

An unusual problem was a VCR with no tuner channel change, being stuck on number one. A few preliminary checks failed to bring anything to light so as I'd a similar machine already on the bench I swapped the front panels. This didn't cure the fault. Back went the original front, whereupon I inadvertently discovered that the timer indicator wasn't responding to the timer switch. Deciding to follow this lead instead took me to pin 51 of the main microcomputer chip. Due to some form of corrosion there was a leak to pin 52 , the 5 V supply line. Cleaning the print provided a cure. A few weeks later another machine came in with the same fault symptoms and the same cause as well.

Another unusual problem was poor playback pictures with the machine's own recordings. The f.m. waveform at TP106 was continually varying in amplitude, with the output from one head occasionally disappearing altogether. The effect on the screen was that the pictures would fade into noise maybe twice or three times a minute. Examination of the record f.m. signal showed that nothing was amiss and the odd thing was that the noise appeared at different points when the same recording was played again. The answer was that no control pulses were being recorded. The cause: R438 was missing - it had never been fitted. This would have been easy to miss during a quick visual check as the picture was stable for up to twenty seconds at a time. Very good these digital servos!

There we have it then. All in all the best machine developed by JVC to date, and by quite a margin. The only design problems from a servicing point of view appear to be the bottom cover retaining screws, which can be awkward to remove, and the relatively inaccessible motor driver amplifier panel. There's also a knack to removing the bracket which holds the combined aerial amplifier/r.f. modulator unit. A weak point here appears to be the external aerial connection centre pins. We've found them to be broken on a greater number of machines than we would expect - potentially a very expensive repair. Otherwise these machines will in years to come greatly lighten the workload of harassed video engineers.
C.H.

## Ferguson 3V29/30 - JVC HR7200/7300

There have been various comments in these pages in recent months concerning the problem of loading motor belt slippage in these very popular machines. Perhaps the following notes will help. We've had a large number of
these machines through our workshops over the years and have found that a contributory factor seems to be dust on the motor and worm pulleys - the fault often occurs with VCRs that have a dusty interior, though not exclusively so. Before replacing the belt clean both pulleys and examine the two cogs that protrude into the upper part of the chassis and engage the loading rings - clean out any grit that's become embedded in hardened grease. Take care not to get any of the grease from the worm drive on the replacement belt.

Another point I've noticed is that belt slippage can occur as the machine warms up: on many occasions I've left a VCR on soak test while trying to trace a servo fault or whatever and after playing a three hour tape once or twice have found that the machine refuses to load. Most customers don't put their machines to this sort of extended use, but a case could perhaps be made for belt changing whenever one of these VCRs is brought in for service. Don't ask me how a belt stretches as a VCR warms up. Maybe the motor would be a more likely candidate for suspicion. Changing the belt however has always in my experience provided a complete cure.

Finally, I see a lot of VCRs that have been "looked at" elsewhere. A few intriguing solutions to this problem have been noted. I cannot comment on belt boiling as it's difficult to tell when a belt has been boiled, but bending the contacts of the after-loading switch is very popular: it doesn't work. Neither does replacing D3, an 11V zener diode on the mechacon panel, with a higher voltage type the loading arms will come out of the cassette housing like greyhounds out of their traps but the belt will still slip. What will work is removing the loading motor from its bracket and elongating the bracket mounting holes using a needle file. I did this once with a local customer's machine when we'd no spare belts and told him to come back when the problem recurred: that was over a year ago, and I've not seen him since. Maybe he just didn't want to return to someone who confessed to carrying out a temporary repair. It's quicker of course to replace the belt. C.H.

## Sharp VC581

This was a good one! At stop the capstan rotated backwards and when play was selected the capstan stopped . . . Investigation started at the capstan forward/reverse switching i.c. (IC701) where the reverse select pin 2 was found to be high all the time. The track was traced back to D7018 via wire link J20 which was shorting to link J25. These links are at the right-hand side of the mother board.
P.B.

## Panasonic NV7000

The fault with this machine was no sound in the E-E mode. Checks in the sound section revealed that the audio mute circuitry was operating: pin 1 of connector P4009 was high at approximately 5 V . The cause of the trouble was the quad, two-input nand gate chip IC6010. Replacing this provided a complete cure.
S.I.

## Panasonic NV333

The capstan wouldn't lock in the playback mode. Both the reference and capstan FG signals were present and on checking the d.c. voltages around the capstan servo chip IC2003 the voltage at pin 16 was found to be low at about half the correct level. Tracing this voltage back to its
source we found that the 9 V supply to connection E on the system control board was missing. The cause was Q6003 being open-circuit: this transistor acts as a switch, supplying 9 V except when the machine is in the record mode.
S.I.

## Hitachi VT8000

On pressing the play button the drum motor would creep up to speed slowly, in an irregular manner. The capstan motor would then start, again in a very erratic manner. The 9 V supply at PG502/6 and the 12 V supply at PG502/7 were both low. The cause was traced to R054 on the system control board being high in value. S.I.

## Sharp VC8300

We had two of these in during the same day. The first wouldn't switch off, with the operate light always on. Q902 was found to be short-circuit. The second machine would lose the playback picture - the screen intermittently became a blank white raster. This was traced to dry-joints on plug/socket connector CD on board PWB-C. M.D.

## Sharp VC7700

The complaint was no play. The machine would lace up then unlace after about three seconds. We checked the inputs to the microcomputer chip and found that the source of the trouble was a false signal from the slack sensor mounted on the pinch roller bracket. Replacing this cured the problem.
M.D.

## Panasonic NV370 with TX5500

We delivered a new Panasonic NV370 VCR and TX5500 colour receiver. This set employs a budget-type search tuning system that's difficult to fine tune exactly. We tuned in the TV channels, but when the VCR was tuned in there was loud intercarrier buzz on the ITV channel (41) in the E-E mode. We tried shifting the modulator frequency but this didn't help. It was possible to cure the problem by fine tuning the set but when the video channel was reselected the buzz returned. The problem remained even when both the TV set and the VCR were exchanged. As Panasonic had no suggestions we resorted to opening the VCR's modulator in the customer's house and adjusting the sound coil and video level potentiometer for no buzz. This cured the problem but means that the VCR is no longer compatible with other TV sets (low sound).
M.D.

## Hitachi VT33

The problem with this machine, which had been faulty from new, was a ringing on playback of its own recordings. I replaced IC201 but the fault remained: this meant I had to think! A check through the recording signal path revealed that R222, which damps L204, was $270 \mathrm{k} \Omega$ instead of $150 \Omega$. Replacing this resistor produced correct operation.
L.H.

## Philips VHS VCR with Thorn TX9

A Philips VHS machine would work all right with any other set but on playback of some recordings via a set fitted with the Thorn TX9 chassis the top of the picture pulled and there was a white band at the top. The
problem was cured by fitting a 10 dB attenuator between the TV set and the VCR.
L.H.

## GEC V4004/Hitachi VT33

The problem with this machine was intermittent loss of colour on playback. After a few checks I suspected the
colour processing chip IC203 as I've had this fail before, but the fault remained when a new HT4239 was fitted. On making voltage checks at Q217 and Q358 I found that the 9 V collector supply was only 5 V , due to choke L215 in the supply line being open-circuit - the 5 V was coming from pin 27 of IC203 via the base-collector junction of Q217! Normal operation was restored after replacing L215. L.H.

## LCD TVs from Citizen

Pocket TV sets using liquid-crystal panels to produce the picture have been on sale in Japan and the USA for some time. Late last year Casio released an LCD set in the UK and the 1985-6 Tandy catalogue lists two such sets, one by Casio and another by Citizen. Citizen are now marketing the set themselves in the UK and we have been lent one to see how it performs.

The present model has a 2.7 in . (diagonal) screen with just over 18,000 pixels (picture elements). A model with 3.5 in . screen, more pixels and incorporating $\mathrm{f} . \mathrm{m}$. radio is due for release shortly and a colour set is expected by the end of the year. The current model measures just $7.5 \times$ $135 \times 23.6 \mathrm{~mm}(15 / 16 \times 53 / 8 \times 3$ in. $)$ and weighs approximately 230 g ( 270 g with batteries). It consumes 0.4 W and can be operated from four size AAA batteries, an a.c. adaptor, a car battery or an optional NiCd rechargeable battery pack. Battery life is approximately ten hours with continuous use of four AAA alkaline batteries. There's a video input jack, earphone jack, external acrial jack and a.c. adaptor jack.

The LCD panel is illuminated from the rear and produces the picture by either allowing the light through or blocking it to a greater of lesser extent. Natural light (outdoors), a back-lighting attachment or other light source can be used. The panel consists of two sheets of glass with a gap of about 0.3 mil between them: the twisted nematic (TN) liquid crystal material fills the gap between these sheets. Two sheets of polarising material cover the rear and front surfaces of the panel. Inside the


Fig. 1: Block diagram of Citizen's LCD TV receiver.
panel are 122 horizontal row elements backing one glass sheet and 148 vertical column elements backing the other sheet. The intersections of the row and column elements produce the pixels.

Light entering the rear of the panel is first polarised, i.e. only light waves polarised in one direction are allowed through by the rear polarising sheet (ordinary light has random polarisation). The effect of the TN liquid crystal material is to change the polarisation of the light by $90^{\circ}$. The second polarising sheet at the front allows this light through. Control of the panel's light transmission is achieved by applying an electric field to each row/column intersection, i.e. pixel, in turn. The fields alter the alignment of the liquid crystal molecules with the result that the light transmission characteristic changes.

A block diagram of the Citizen receiver is shown in Fig. 1. The top part is conventional - a tuner, i.f. strip and audio amplifier - the rest is not. The LCD panel requires row and column drive, and there are 122 rows not 625 lines. The heart of the set is the control i.c. which provides synchronised timing for the display drives and converts the analogue video signal to a four-bit digital signal. This signal is then processed in the column driver i.c., using shift registers, latches and pulse-width modulation. The digital video signal is alternately stored in two shift registers, the switching being at $0.3 \mu \mathrm{sec}$. When a complete line of video signal has been stored it's read out at a rate that conforms with the row timing. It's then converted to pulse-width modulation to drive the column electrodes. The row drive circuit addresses the row electrodes in sequence: when a row is switched on, the column electrodes apply the pulse-width modulation to the pixels in that row.

The brightness of the display is varied in two ways, by the pulse-width video modulation and by the brightness control which sets the amplitude of the pulses applied to the column electrodes. Note that the brightness control has to vary several voltages so that its operation does not affect the pixel address switching.
It's necessary to generate higher voltages than the 6 V input: the varicap tuning system requires 38 V while the row address system requires up to 19 V . An $L C$ oscillator and two rectifier circuits produce these higher voltages.
Some sophisticated electronic technology is used in the set and the construction is a masterpiece of miniaturisation - the PCBs use surface-mounted component technology. We found the set to be sensitive, using its built-in rod aerial, and easy to tune. What of the picture? We feel that any attempt at lengthy viewing would not be easy on the eyes. But then the set is not meant as a main TV picture source, rather as a portable picture source to refer to as and when the user wishes to do so. The limited resolution unfortunately makes most: lettering illegible.

# TV Fault Finding 

Reports from Alan Shaw, Michael Dranfield and Philip Blundell, Eng. Tech.

## Thorn TX100 Chassis

This is the best TV chassis produced to date by Thorn-EMI-Ferguson. It's used in sets fitted with various types of tube, certain component values being changed to suit. As with most new TV chassis there's no such thing as a common "stock" fault. Anyone with experience of the later TX9 and the TX10 chassis will be at ease with the TX100. I hope the following notes will be of interest to those who are not too familiar with Ferguson colour sets.

One interesting feature is the automatic grey-scale adjustment. If you reduce the height of the picture you'll see three test lines above the picture area. These test lines ( 23,24 and 25 ) are used to produce a beam current of $10 \mu \mathrm{~A}$ to set the c.r.t. cut-off point for each gun. The only variable controls are for the highlights. A start-up delay circuit (TR3 etc.) earths pin 18 of the colour decoder chip when the set is first switched on to prevent the rapid warm-up c.r.t. producing a bright picture that drifts down to black level.

The power supply is built around the popular TDA4600-2 self-oscillating chopper control chip. A replacement must have the suffix -2: the early TDA 4600 will not work in the chassis. Start up is via a thyristor (SCR1) which provides a supply to pin 9 of this chip - around 56 V at this pin is sufficient to get the circuit going. D10 stops SCR1 working once the chopper circuit comes into operation. When the h.t. voltage rises so does the voltage across pins $10-8$ of the chopper transformer: this voltage controls the mark-space ratio of the output from the chip. The chopper circuit's normal operating frequency is 20 kHz , rising to 60 kHz with remote-control versions in standby and dropping to 4 kHz when there's a heavy load on the 119 V line, e.g. a short-circuit line output transistor.

Important servicing note: the 15 V regulator chip IC9, the sound channel chip IC5 and the field output chip IC6 are all temperature conscious - never apply freezer to any of them under fault conditions. IC6 will automatically turn off when the temperature exceeds $175^{\circ} \mathrm{C}$. If you apply freezer you'll turn it back on, with possibly alarming results - the i.c. can literally explode, with consequent damage to the board.

Faults we've had to date are as follows. (1) Blown mains fuse due to the chopper transistor TR6 being leaky or short-circuit. Check the TDA4600-2, R121 (27 $\Omega$ ) and R114 ( $0.47 \Omega$ or $0.39 \Omega$ depending on chopper transformer), also R115 ( $330 \mathrm{k} \Omega$ or $270 \mathrm{k} \Omega$ depending on chopper transformer) - repeated failure of TR6 is likely if this latter resistor is out of tolerance. (2) Grainy picture due to the r.f. amplifier transistor in the tuner or the SL1432 i.f. preamplifier chip IC1 being faulty. (3) Intermittent field collapse due to $\mathrm{C} 95(0.01 \mu \mathrm{~F})$ being intermittently leaky. (4) A small picture due to D28 (BY299) being leaky - this diode is present only in $110^{\circ}$ models.
A.S.

## Some Quickies

Ferguson TX90 chassis: We've had a couple of these portables in with the mains fuse blown due to one of the c.r.t. fixing screw washers trapping the degaussing coil and shorting it to the earthed c.r.t. rimband.
ITT CVC32 chassis: Blank raster, sound o.k. Check
whether R28 ( $820 \Omega, 1 / 2 \mathrm{~W}$ ) on the mother board is opencircuit.
Amstrad CTV1400/Orion 14PC portable: Intermittent flashing and drifting is usually caused by faulty eight-way channel selection switches but can also be due to a faulty tuning potentiometer bank. Note that while they look the same the potentiometers in non-remote control models are $100 \mathrm{k} \Omega$ each while those in remote-control versions are $20 \mathrm{k} \Omega$ each.
Pye 725/737 chassis: For weak field sync check C941 ( $4.7 \mu \mathrm{~F}$ ).
Thorn 9000 chassis: Line off speed. C715 ( $22 \mu \mathrm{~F}, 275 \mathrm{~V}$ ) open-circuit.
Philips KT4/K40 chassis, remote control versions. Unable to tune any stations, on-screen line not moving and no channel display - the 5 V regulator on the VST panel is open-circuit. Remote receive light permanently lit, channel change slow to react - D6103 (BA317) on the VST panel leaky.
A.S.

## Thorn TX90 Chassis

A few of these sets have been in for repair with the same fault - intermittent collapse of the bottom half of the field scan and height variations from the bottom upwards. This is caused by dry-joints around the field output transistors. As there aren't many components in the field output stage we generally resolder the lot.
M.D.

## GEC C2110 Series

Some quickies on these sets.
Field collapse: Check the voltage at the collector of the discharge transistor TR452. If abnormally high (33V) change R455 ( $470 \mathrm{k} \Omega$ ).
Slight field jitter at the top of the picture: Replace the midpoint voltage preset P 454 ( $470 \Omega$ ).
Height shrinks as the set warms up: Change the field driver transistor TR453 (AC188).
Picture only ten inches high, with unlocked colour and distorted sound: Replace the 40 V supply rectifier D601 on the line timebase panel. A BY210-800 is suitable.
Loss of one primary colour with a dark picture, the relevant first anode voltage being low: Replace the tube base spark gap associated with the missing colour. M.D.

## Thorn 1790 Chassis

We've had a lot of these sets in for repair lately, all with the no results symptom. In every case the cause has been bad cracking around the mains transformer. One set came in with an intermittent fault: no signals, no video and a jumping picture. When the fault eventually appeared we found that the 90 V rail was missing. This was traced to a crack around one of the line output transformer's pins.
M.D.

## Philips G9 Chassis

There was a very odd fault on this set. The top quarter of the field scan was missing: it wasn't compressed or folded
over, and the rest of the picture was normal. The set was left on and after ten minutes the scan had filled more of the screen, leaving a circular patch at the top left. A quick timebase panel swap proved that the fault was in this area and a number of electrolytics in the field timebase were changed: the fault was cleared when $\mathrm{C} 22(10 \mu \mathrm{~F})$ and C 51 $(47 \mu \mathrm{~F})$ were replaced. Surprisingly if either one of these capacitors was replaced the fault remained: the two capacitors had to be replaced as a pair and we couldn't find anything wrong with the originals. M.D. (Editorial note: In this chassis changes in the conditions in the field timebase affect the line blanking.)

## Philips KT3 Chassis

This set led me a merry dance: there were intermittent black lines at the top of the picture. As usual the fault disappeared as soon as the chassis was disturbed. Over a
period of time the decoder panel and the blanking transistor were replaced to no avail. Then one day the test card was on when the fault appeared and I noticed that the top of the picture was bending over to the right. Examination of the soldering on the sync separator and i.f. modules revealed that C2148 at the input to the TDA2540 chip, inside the i.f. can, hadn't been soldered in.
P.B.

## Philips K35 Chassis

This set had no colour till you turned up the brightness. Then along with the colour came flashing horizontal lines. Substitution proved that the fault was in the decoder module. A new TDA3560 decoder chip stopped the flashing lines but a replacement for $\mathrm{C} 66(100 \mu \mathrm{~F})$ was required to bring back the colour - this electrolytic decouples the 12 V supply to the chip.
P.B.

## Long-distance Television

Roger Bunney

March was another relatively quiet month but now that April is here there should be increasing Sporadic E activity - mid-April SpE openings usually indicate a good season ahead. A brief outline of SpE signal propagation is given later in the column for the benefit of new readers. -

The repeat performance 27 days after the massive Aurora on February 8th produced little by way of reception here in the south - I noted only heavy patterning from the north on chs. E2/R1 on March 6th. Iain Menzies, well placed in Aberdeen, logged AR signals on the 6th, 7th and 9th, but only NRK (Norway) chs. E2/3 and TSS (LISSR) ch. R1, during the later evening periods. NRK/ TSS signals were again logged via AR on March 17th, $20 \mathrm{th}, 22 \mathrm{nd}, 23 \mathrm{rd}$ and 26 th . Further information on the February aurora has come to hand. On the 8th a Swedish amateur (SM6PU) heard a US amateur (K1TOL) operating at $50 \cdot 11 \mathrm{MHz}$ (time $0050-0052$ ). SM's aerial was aimed at $279^{\circ}$. During the midnight period K1TOL heard the UK 50 MHz beacon on Anglesey (GB3SIX). This shows that transatlantic DX-TV reception must have been possible in Band I, though it would have been of poor quality.

There was minimal SpE propagation during March. The best days were the 18 th with TVE (Spain) ch. E3 and TVP (Poland) ch. R1, both at 1220-1230, and the 27th with SR-1 (Sweden) ch. E3.

Tropospheric propagation matched the poor weather conditions. There was a slight lift on the $14 / 15$ th, giving enhanced reception from France. Dave Shirley at Hastings and Tim Anderson at St. Leonards claim the first reception in the UK of the new French local stations. Dave logged TV5 from Lens on ch. E51 at 0200 on the 15th, with a PM5544 pattern carrying the identifications "TDF" and "RES 5". On the following night he received the Lens TV6 signal on ch. E54, this time on programme with a "TV6" insert at the top right corner, then the PM5544 pattern with similar identifications though "RES 6". The signals were not visible until stronger main network TDF transmitters came on air.
Not an exciting month then, but by the time this is read things should be happening. During the strong gales over the weekend of the $22 \mathrm{nd} / 23$ rd Cyril Willis's aerial system collapsed: repairs are in hand.

## News Items

UK: Gloomy news concerning Band III. It appears that up to five mobile radio networks are to be established in the London area with up to twenty channels each. Regional networks with up to nineteen channels are to be established in Birmingham, Merseyside, Nottingham, Leeds and Central Scotland. National Radiophone should be in operation by the end of the year, covering the London area to the M25 with four transmission sites using twenty channels each.


Left: The FUBK test pattern in use by Copenhagen on ch. E56 at 200W - a French signal transmitted during the October tropospheric opening. Centre: An unusual test card received from Hamburg, ch. E9, in early 1985. Right: A Danish regional identification on ch. E7. Photographs of reception by Ryn Muntjewerff in Holland.

Ireland: The Republic is permitting an experimental amateur radio allocation at $50-51.75 \mathrm{MHz}$, on a limited basis about twenty operators will be allowed to operate in the first phase, provided there's no interference to cable TV and the RTE-1 outlet at Maghera.
France: A seventh TV network (TV7) is expected to start operations in mid-1987, with programme linking by satellite.
Spain: Full daytime transmissions are planned. We understand that Breakfast TV will be via the TVE-1 transmitters.
In brief: China is to launch a TV/communcations satellite . . . RTM (Morocco) is now testing all day on chs. E25/6, using the PM5544 pattern . . . SBS-TV (Australia) started services from Hobart (Tasmania) and Perth during March, on ch. 28: a new ch. 10 commercial service is planned for Perth.

## Satellite TV News

There's been a severe fall off in sales of satellite TV receiving equipment in the USA, mainly because of uncertainty caused by the increased use of scrambling. There have been redundancies in at least two equipment manufacturers - Amplica and Birdview Satellite Communications have announced redundancies approaching forty per cent. The latter company says advances in equipment technology mean that fewer manufacturing personnel are required. There's also a general move to Ku band (11-7$12 \cdot 2 \mathrm{GHz}$ ) operation by cable programme originators in the USA in order to avoid their material being received without payment by those with C-band TVROs. Major NBC feeds have recently been transferred to the SBS-3 satellite at $95^{\circ} \mathrm{W}$ (transponder 1) in preference to adopting scrambling in Band C. Anderson Scientific has produced a "low-cost video stabiliser" which will unscramble VideoCipher 2 and Oak-Orion transmissions - the former has digitally encrypted sound, which is likely to pose a problem.

The AUSSAT satellite is now relaying ABC-TV (Victoria) TV programmes on a full-time basis. Interesting that Tony Dunnett in North Island, New Zealand has received the C-band downlink at his company's NZ location. Tony's company (SAT-TEL - no connection with the UK firm of the same name) makes dishes in sizes up to 3 m and LNAs down to $50^{\circ} \mathrm{K}$.

## Fringe Electronics FM Radio Preamplifier

Fringe Electronics Ltd. (Fringe House, 50 Mansfield Road, Clipstone, Notts NG21 9EQ) has introduced a mains-operated, set-back preamplifier intended for use with f.m. radio equipment: the noise figure quoted is 1.9 dB and the claimed gain is typically 20 dB . I've recently had one for assessment. Internally the single stage of amplification, using a bipolar transistor, has bandpass input tuning and a tuned collector load circuit. A voltage stabiliser is incorporated and the circuitry is built on a high-quality, low-loss PCB. I've no criticism of the construction. The noise could be checked only subjectively but measurements of gain were made. Over the 88 108 MHz band the gain varied from 22 dB to 23.5 dB , comfortably exceeding the claimed figure. Gain was also checked at various frequencies outside the band to assess the response to known or possible sources of high-level interference. These tests indicate that the unit should minimise if not eliminate all but the strongest local sources of interference. At 41 MHz the gain was -25 dB , at $50 \mathrm{MHz}-18 \mathrm{~dB}$, at $65 \mathrm{MHz}-5 \mathrm{~dB}$, at $75 \mathrm{MHz}+7 \cdot 5 \mathrm{~dB}$, at


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$146 \mathrm{MHz}-17 \mathrm{~dB}$, at $160 \mathrm{MHz}-28 \mathrm{~dB}$ and at 170 MHz -43 dB : 50 and 146 MHz were chosen in view of current or pending amateur radio operations while 75,160 and 170 MHz were chosen since they relate to PMR activity.

Checks with weak signals above 100 MHz in all instances gave a very clean improvement to a signal that had previously been just above the noise level. In general a weak signal at the noise level was raised to give acceptable, "cleanish" mono reception. I found no evidence of overloading at the bottom end of the band despite the presence of very strong signals locally - this was when listening to weak commercial/BBC stations between strong local ones. It's possible however that the gain could be too great for use with inferior tuners/receivers with bipolar front ends (and thus more susceptible to overloading). My own receiver, a mid-range Sanyo with MOSFET front end, gave no problems. I tested the amplifier thoroughly with a view to DX-FM use and the results were excellent.

The unit comes blisterpacked and sells for $£ 15.75$ plus VAT. With appropriate splitters it could also be used in a distribution network.

## Old Sets for Disposal

Two elderly sets have recently been passed on to me they'll be dumped if no one wants them! The first is a midfifties Ekco mains/battery portable, Model TMB272. It was working when put into store many years ago. The other is a set I know better - a Bush TV62 in a Bakelite cabinet. I used this type of receiver for many years and can recommend it despite it being made back in 1957: it works, the screen lights up and the cabinet is uncracked -
it'll be a collector's item in years to come! These sets are free but must be collected (Southampton area). If interested, drop us a line with s.a.e. The TV62 can be converted to 625 -line operation but it would be nice to see it left as a memorial to 405 lines.

## New Book

The latest publication from the BATC (available from 14 Lilac Avenue, Leicester LE5 1FN) is "The Best of CQTV". It contains the more important and innovative articles that have appeared over the last five years in the BATC journal CQ-TV - interest in amateur TV has increased greatly in recent years and back copies of the magazine are now generally unavailable. The articles cover operation at both $70 \mathrm{~cm}(435 \mathrm{MHz})$ and 23 cm $(1.3 \mathrm{GHz})$, f.m. and a.m. video, test equipment and even a vision mixer, with full circuit diagrams and with some PCBs offered to members. I truly recommend this $100-$ page (A5 format) book: it's well worth the $£ 3.50$ (including UK postage) price, being packed with information. Overseas readers should send a London based bank draft and include sufficient extra postage.

## Australian Channel Allocations

Robert Copeman (Melbourne) has sent us an up-todate listing (May 1986) of the Australian v.h.f. and u.h.f. TV channel allocations (see Table 1). The B/G system applies, i.e. with $5 \cdot 5 \mathrm{MHz}$ sound-vision spacing and also PAL colour. Note that the use of Band II for TV is being gradually phased out as the number of f.m. radio stations using the band increases.

## From our Correspondents . . .

First a couple of corrections. In the December 1985 column we showed a Tele Malta Corporation test pattern received by Mel Thurlbourn whilst he was in the area and suggested that the power of the ch. E10 transmitter was 10 kW . Edmond Friggiere tells us that the power is less than 2 kW . In the April issue we showed a slide received by Marios Colocassides in Cyprus and captioned it as being from Tunisia. We got the channel right (ch. E33) but the transmission was from Beirut.

In the April column we mentioned a query about reception of an AFRTS signal in Rastanura, Saudi Arabia, on ch. E27. A London-based reader has solved this mystery for us. The source of the signal is a 100 W transmitter owned/operated by the Omani Prime Min-

Table 1: Australian TV channel allocations.

| Ch. | Freq. (MHz) | Ch. | Freq. $(\mathrm{MHz})$ | Ch. | Freq. $(\mathrm{MHz})$ |
| ---: | :---: | :---: | :---: | :---: | :---: |
| 0 | $45-52$ | 33 | $561-568$ | 53 | $701-708$ |
| 1 | $56-63$ | 34 | $568-575$ | 54 | $708-715$ |
| 2 | $63-70$ | 35 | $575-582$ | 55 | $715-722$ |
| 3 | $82-92$ | 39 | $603-610$ | 56 | $722-729$ |
| 4 | $94-101$ | 40 | $610-617$ | 57 | $729-736$ |
| 5 | $101-108$ | 41 | $617-624$ | 58 | $736-743$ |
| $5 A$ | $137-144$ | 42 | $624-631$ | 59 | $743-750$ |
| 6 | $174-181$ | 43 | $631-638$ | 60 | $750-757$ |
| 7 | $181-188$ | 44 | $638-645$ | 61 | $757-764$ |
| 8 | $188-195$ | 45 | $645-652$ | 62 | $7641-771$ |
| 9 | $195-202$ | 46 | $652-659$ | 63 | $771-778$ |
| 10 | $208-215$ | 47 | $659-666$ | 64 | $778-785$ |
| 11 | $215-222$ | 48 | $666-673$ | 65 | $785-792$ |
| 28 | $526-533$ | 49 | $673-680$ | 66 | $792-799$ |
| 29 | $533-540$ | 50 | $680-687$ | 67 | $799-806$ |
| 30 | $540-547$ | 51 | $687-694$ | 68 | $806-813$ |
| 31 | $547-554$ | 52 | $694-701$ | 69 | $813-820$ |
| 32 | $554-561$ |  |  |  |  |

ister. It's of Acrodyne manufacture and is fed with signals from an 11 m Scientific Atlanta Intelstat (B standard) earth station. Apparently there are several such receiveonly stations dotted around the Gulf area, privately owned by prominent people. The Omani transmitter broadcasts the AFRTS-Southern Europe service for the benefit of local residents, taking the feed (without censorship) from transponder 9 on Intelstat V F-02. There were plans at one stage for a similar service in Abu Dhabi. Interesting that in Turkey the AFRTS relay is delayed for 24 .hours for censorship purposes - even for US Forces!

## Sporadic E Propagation

The "season" for Sporadic E propagation normally extends from about the second week in May to midAugust, with sometimes a minor spell of activity in midApril and another period in mid-December. The ionosphere's E layer is some 70 miles above the Earth during the day and though reflective to short-wave signals is generally transparent to v.h.f. signals. M.W. signals are normally absorbed by the D layer during the day, though reflection from the $E$ layer occurs after dark when the $D$ layer disperses. Reflection of v.h.f. signals from the E layer occurs when ionised clouds are present. These occur at random and cannot be forecast. Incident Band I signals can be reflected over great distances, typically $500-1,500$ miles in a single hop. The higher the intensity of the ionisation the higher the signal frequency that can be reflected. Reflection of Band III signals occurs only rarely: reflection of Band II radio signals is rather more common.

During an opening the reflective clouds vary in number and may be stationary or move at some speed. As a result the signal reflections will vary: the skip conditions change and alternative signals may appear on a channel. With widespread reflection the result is severe interference. Reflective conditions can last for minutes or hours. There's a greater chance of SpE activity when the weather is humid and thundery.

Since SpE signals can be very strong a simple wideband dipole will often suffice for reception: two fixed dipoles mounted at right angles will allow switched coverage of all directions. Alternatively a two-element wideband system with a rotator can be used. Aerial height need not be high - the signals tend to arrive at an angle relative to horizontal - but it's best to have the aerial at 20 ft or so to clear nearby objects. Most signals start off horizontally polarised, but a propagation shift tends to occur. The general rule however is to mount the aerials horizontally. We hope to feature shortly a wideband Band I/III design as a DIY project.

Double-hop reflection will bring in signals from 2,000 miles or beyond, signals from the Middle East often being seen in the UK. Use of an indoor preamplifier will often help with weaker signals. Local interference tends to occur in Band I and is best filtered out before amplification: provided premium quality coaxial cable is used there will be little loss and the optimum signal/noise ratio will be maintained.

A 625 -line receiver with v.h.f. coverage can be used or alternatively a u.h.f. receiver, preferably with single-knob, slow-motion tuning, can be used in conjunction with an upconverter. Improved results will be obtained by using a narrow i.f. bandwidth to reduce adjacent channel interference. Finally a commercial: my DX-TV book, published by Babani publications, is at present out of print - a new edition is expected shortly.

## Other things and other places

Les Lawry-Johns

There's more to life than TV sets, though there are times when this is none too obvious. Anyway, I thought you wouldn't mind if for a change I told you about some other things and places.

## The Coat

One of these things is my overcoat. It was made to measure in 1938 by M. Burton and cost $37 / 6 d$. For those of you who want that in present day money it comes to one pound thirty seven and a half pence (I think). That coat is as good as new and still fits. It's double breasted and waisted. I've worn it twice during the last thirty years, which all goes to show how many funerals I've attended. Not quite true that, because an overcoat isn't needed in summer. Jealousy will get you nowhere. Oh yes, black melton.

## The Journey

Next places. A couple of weeks ago the phone rang during the evening. HB answered it. She sounded a bit excited and I heard her say "We'll come up and get it". Since her daughter Colleen was with us at the time she didn't say anything more about the conversation. After Colleen had left I was told all about it. Colleen had always wanted a small Dachsund and we'd sent out signals a month or two back in the hope of getting one for her birthday. One of the signals had now been answered: there were three puppies ready to leave their mother and we could have our pick. All we had to do was to hang up the Closed sign and pop up to Dersingham. Lovely, but where's that?

I consulted my AA New Book of the Road. It's just up from Kings Lynn, near the Wash. My eye wandered down the A10 to Ely, thence to Cambridge and Theydon Bois to pick up the M25 to Dartford Tunnel. Not far. Any idiot could do it with a full tank of petrol.

On the following Tuesday the tank was full, the oil was checked and we were ready to go. Colleen arrived at nine thirty and we were off. First to the Dartford Tunnel which is practically on our doorstep. I missed it. We circled round and after a slight detour through Bexley we got there. Never mind, we were on our way in my safe and strong hands. Straight up the M25 towards Theydon Bois, steer to the right and up the M11 and on our way to Cambridge. On and on like the brave six hundred my Grandad used to sing about. Harlow came and went, then Bishop's Stortford. Flashing along the motorway while other cars flashed past as though we were standing still.

Undeterred we fought our way up past Cambridge and on to Ely, my eyes like diamonds behind my new specs (first time wearing them for two years), though I must admit they were getting tired. King's Lynn loomed up and we went round a roundabout and took the A149 past Castle Rising on the left and finally hit Dersingham. By now the Ouse was ousing all over the place and had been
for some time: waterways to the right of us, waterways to the left. On we went, past the fish and chip shop, slowly now, looking for the flags. At last we found them and turned into our destination. A man was waiting at the gate. He'd been waiting for a long time.

HB jumped out and greeted him profusely. I was amazed. Then Colleen did the same. I got out and we shook hands like gentlemen.
"This is my Uncle Roy" said HB.
"Well I'm buggered" said I.
"This is my husband."
"Well I'm buggered" said Roy.
HB hadn't even said we were going to relatives.
Into the house where Roy's wife greeted us warmly. Colleen looked at the large box on the floor from which some wimpering issued. "Goodness, aren't they beautiful!" she cried. One had a black patch on its back. She leaned over and picked him up, then realisation dawned. "He's yours" we told her.

We had lunch and gossiped. I finished off my whisky and started on some wine. They'd a lovely garden where the birds were well catered for. While we were admiring its features we saw a bag containing a marrow and some beans being passed over the wall on a rope. Roy took the bag in and came out with a bottle of home-made wine. It was tied to the rope and and pulled over the wall. Nary a word was said.
"Does that happen often?" I queried.
"Several times a week - the wife makes good wine."
"So I'd noticed."
By now it was almost two and I was beginning to wonder how long it would take to get back. So with Dacksy in a box and plenty of food for him we took our leave and departed, heading for King's Lynn. Somehow I took the wrong road and we went through miles and miles of country. There wasn't much sun but what there was I kept to the right of me so I knew we were going south. Eventually we arrived at Ely. HB glanced at the petrol gauge. "We're half empty."

I'd also been looking at it. "We're half full" I said.
We were well on the way to Cambridge now, but instead of bypassing it I found myself in the town centre. So many bikes, I've never seen so many. We went round the market square just for fun and headed out of town, eventually finding the M11. Down we hurtled while cars flashed by in the outer lane. The petrol gauge by now read very low. It suddenly occurred to me that there are no filling stations on these motorways. I didn't want to go off and get lost again; I also knew that an empty reading meant that there were still two gallons on board. But at the speed we were going they wouldn't last very long. So I gritted what teeth I had and slowed down. We crept along the M25 and under the Dartford Tunnel. Then along the A3 till we were able to fill up just three miles from home. We were glad to be back. Dacksy had slept all the way and even Douggie (Colleen's husband) likes him.

So much for the trip and its confusions. I don't know how ET manages it: from one end of England to the other about twice a week. But I'm not that bad at navigation. JAR gets lost trying to find his way from one side of London to the other (almost) on a good day with the light behind him . . .

## Oven Problem (Microwave)

You remember HB's sister Dot - her with the brown eyes? Well Dot has a microwave oven with two bulbs in it.

These are in series which means they are rated at 125 V (20W). One went so they both went out. HB brought the good one down so that we could match it. We couldn't. Not only becuase we don't have any 125 V bulbs but also because the base is slightly larger than the normal SES.

So HB trudged around the town, getting the same
response. One shop assistant gave her detailed instructions on how to get to our own shop, which pleased her no end. Our wholesalers don't seem to have them either, so Dot's going to have to make do with a one lamp (240V) oven with the other lamp shorted out. If we can find a 240 V lamp with that unusual base.

# Servicing Sinclair Microcomputers <br> \section*{Part 2} 

Ken Taylor

Last month we considered some of the i.c.s used in microcomputers and ended with a block diagram of the simplest computer possible. It had just a Central Processing Unit (CPU - the microprocessor), a Read Only Memory (ROM) that contained the operating instructions, a Random Access Memory (RAM) for storing the program and data and an Uncommited Logic Array (ULA) for doing all the hardware jobs, including interfacing with the TV modulator and the tape input/output ports. Fig. 5 last month was in fact a block diagram of the Sinclair ZX81 microcomputer which is probably the simplest possible home computer design. We'll now examine this model as an introduction to computer servicing.

In producing such a simple computer Sinclair Research introduced several features which make both the circuitry and operation rather different from that of the more usual type of microcomputer. For instance, where have all the other chips one might expect to find gone? The ones that generate the TV display signals and the decoder chips that decide whether it's the ROM or RAM you want? Or the special that looks after the keyboard? They all seemed to be essential in the Amstrad machine described in this magazine last year. In the ZX81 these jobs are all shared between the CPU and the specialised circuitry in the ULA, the timing and decision making being carried out by the former. There's a penalty to be paid for doing things in this simplified way however: the time the CPU has available for processing the program is severely limited. In fact whenever there's a display present the CPU is free only for the period of the field flyback - for the rest of the time it's producing the line sync and display details!

## Sinclair ZX81 Circuit

So when you study the ZX81's circuit details (Fig. 1) remember that this is a very specialised machine with a component count unlike most other microcomputers, though it does have a standard CPU and a system that functions in the same way despite looking so different.
Further examination of Fig. 1 will help to explain some of the differences and clear up many of the problems described above. You'll see that the ULA chip is connected to the TV and tape circuits directly at pins 16 and 20. It can decode the address lines and then enable either the RAM or the ROM via one of the Chip Select (CS) lines at pins 12 and 13. It also assists the CPU in reading the keyboard, via the KBD0-KBD4 lines. These link the ULA to the keyboard via a five-pin socket (KB1) that's not shown in the diagram. This PCB-mounted socket connects the keyboard "tails" to these lines while an eightpin socket (KB2), also not shown, connects the other keyboard tails to diodes D1-8. The ULA also produces
the 3.25 MHz clock signal from the 6.5 MHz ceramic filter (X1) connected to pin 35.
The machine has only 1Kbyte of RAM fitted to the board. Provision is made for this to consist of either one 4118 memory chip or two 2114 chips. There's also provision for fitting a 2Kbyte RAM for the export model. The usual memory extension consists of a 16 K unit which plugs into the edge connector at the back of the machine. Fitting an extension memory disables the internal 1 K memory however - the following test procedure assumes that only the internal memory is in use.
The data lines to the ROM and RAM and some of the ROM address lines incorporate buffer resistors. These enable the lines to be used by more than one device without conflict. They are very useful in a fault situation for determining which device is still functioning satisfactorily. Lines downstream of these resistors are given an identifying accent, e.g. A1'. The edge connector also has these identifications on some of the contacts to show which side of the resistors link up with them.
There have been at least three versions of the PCB. Fig. 1 represents the issue one board but I've experienced no difficulty in identifying the circuitry on later boards. They vary a little in layout but the component numbers on the boards seem to be the same. One of the only differences on the issue three board is the use of individual resistors in place of packs RP1 and RP3 - R35-42 and R43-47 respectively. There's a photograph of an early version of the issue one board, without component numbers, on page 162 of the ZX81 BASIC Programming Book that was supplied with every machine. This photograph shows all the i.c.s mounted in sockets, which certainly isn't the case with later boards. Note also that the ULA is called the "Sinclair Computer Logic" which is a less standard but perhaps more sensible name.

The power supply unit is separate from the computer and connects to it via a 3.5 mm jack plug. It's not shown in Fig. 1 but is a simple d.c. unit that gives very little trouble - except for the moulded jack. If you have one that's been changed, make sure that the tip is positive.

## Initial Checks

When the computer is first switched on the display should consist of a white-on-black K (inverse K) cursor at the bottom left of the screen.

If it doesn't, carry out the following simple checks. Remove any extension memory plugged into the rear connector. Check the power supply - the plug should provide an open-circuit voltage of about 14 V , tip positive. If the plug has been changed for a solder-on type it's easy to check the on-load voltage which should be about 11 V . This will show whether an overload or open-circuit con-


Fig. 1: Basic circuit diagram for the Sinclair ZX81 microcomputer.
dition is present in the machine. In the latter case suspect that the plug has at some time been connected with reversed polarity - this often blows the 5 V regulator and saves the rest of the circuitry.

Check the tuning. The modulator is usually set to channel 36 quite accurately, but sweep the band in case the tuning has moved or been altered. If there's no output signal from the ULA the modulator's output will consist of carrier only, devoid of even sync signals. In this case the indication on the TV screen will be negligible.

## Dismantling the ZX81

If you haven't found the fault by now you'll have to make internal tests. This means dismantling the unit. First remove the four screws from the base. Three of these should be hidden under rubber feet - if these are still there (the two at the front and the one at back left). Lift
off the base and remove the two screws securing the PCB. If you turn the board over towards the front the keyboard tails can be removed from the two sockets. Treat these plastic strips with the utmost care - they are very easily damaged (more about this later).
With the board completely removed the TV and power supply leads can be reconnected. Initialisation of the computer to give the inverse K cursor display occurs without the keyboard being connected, so we can leave it disconnected until the fault has been found.

## Fault Finding

Table 1 provides a quick fault-finding sequence: the numbers refer to the following paragraphs which give details of the procedure. Remember that there can often be more than one fault present, so repeat the sequence if necessary.

Table 1: ZX81 fault-finding sequence.

(1) The power supply should provide about 11 V at 400 mA on load. Less than 7 V will be insufficient for the regulator to function correctly. An excessive current reading indicates a fault on the board.
(2) The regulator should deliver 5 V to each of the i.c.s on the board. Its heatsink normally runs hot to the touch, but not unbearably so.
(3) The signal from pin 16 of the ULA chip to the modulator should give a ' PH ' indication on the logic probe (see Table 2). An oscilloscope should display a signal of 2 V peak amplitude from the peak to the bottom of the sync pulses. Inverse K will produce a very faint signal near the end of the field trace.
(4) If the modulation signal is present but the TV output is absent check the modulator's supply voltage and the tuning adjustment screw - this should be approximately 3 mm down inside the former.
(5) If the cursor is present, connect one of the contacts of the small keyboard socket KB 1 to a contact on the large socket KB2. Check whether a character or keyword appears on screen. Don't worry about shorting more than one connector in either of the sockets as this won't cause any damage to the computer - but it won't produce a display either as the software checks that only one key (apart from the shift key) is being pressed before it produces a screen display.
(6) Two faults that can affect the keyboard circuit are shorts between the lines or open-circuit lines or diodes. They can be identified by their effect on the system. Open-circuits affect only the keys they connect (see Fig. 1). A short effectively holds one key on, disabling the whole keyboard. Faults can occur anywhere in the circuit, from the address bus side to the diodes to the ULA chip's KBD pins. Check for shorts where the PCB tracks run obliquely under socket KB1. The resistance between these KBD tracks should be a few thousand ohms.
(7) The keyboard connection tails are very vulnerable, so to avoid unnecessary work make a thorough check that the computer is working satisfactorily before reconnecting the keyboard. Connect each contact on the small five-pin socket KB1 to at least two contacts on eight-pin socket KB2, checking the screen entries. Finally make sure that the tails are not splitting across (see following paragraph) and that the metallised contacts at the ends are in good condition. Then reconnect the keyboard by turning the case face down, front towards you, with the PCB laid component side up on the case so that the edge connector is at the front left: loop the tails over and push them carefully into the sockets, with a slight rocking movement. Don't push too hard or the plastic will buckle and split. When both tails have been fitted turn the PCB over on to its screw pillars and secure with two short screws.
(8) Often one bank or row of the keyboard fails to operate. This is usually due to cracks across the plastic tails severing one or more of the tracks. If the crack is near the end of the tail a clean square cut can sometimes be made, removing the fault. If not too short the tail can then be refitted. As mentioned above the end contacts of the tails should be checked to make sure that there's a good contact for the connectors. If the ends look a little dirty don't be tempted to apply a liquid solvent cleaner some of these attack the plastic (they don't soften it, they completely disintegrate it!).

If a satisfactory repair proves to be impossible a new keyboard will have to be fitted. These are readily obtainable and are easy to fit to the case with the self-adhesive backing.
(9) Here's a simple ROM check to establish that all the

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bytes of memory are being read correctly. Although it's unlikely that a ROM fault could continue to be present at this point in the test sequence without being detected the check will set your mind at rest. Enter and run the program below - it takes just over a minute to run. Check that the answer printed out is 855106 . If the answer is 854885 the ROM is an early version. To prove this enter: PRINT SQR 25 (square root of a quarter). An answer of 1.359 instead of .5 proves that the ROM is an early type which has a few faults. Any other answer to the program indicates a ROM error. Here's the program:

| 10 | FAST |
| :--- | :--- |
| 20 | LET L $=0$ |
| 30 | FOR N $=0$ TO 8191 |
| 40 | LET L $=$ L + PEEK N |
| 50 | NEXT N |
| 60 | PRINT L |

(10) At this stage it remains only to check the tape save/ load operation and box up the computer. Put in a short program - the one above will do - and save it on tape. Switch off the machine to clear it, then restart and load the program. These operations are both described in Chapter 16 of the BASIC Programming Book supplied with the ZX81.

If the tape tests o.k. the case can be assembled, the four screws fitted and the rubber feet restuck in their sockets. (11) This is the stage you'll probably end up at if the computer has suffered major damage. You've proved that the fault lies in one or more of the chips or on the PCB.

First check whether the computer has been repaired previously. If you find evidence of modifications or soldering, check the board carefully for solder splashes, shorted
tracks etc. Where Sinclair Research fitted i.c. sockets originally I've found that they fitted them to all the i.c.s. So if you find a board that has sockets for some of the i.c.s treat it with suspicion - it's probably been modified.

I don't intend to tell you how to extract a suspect i.c. but let me tell you one of the pitfalls of the method I use in order to illustrate an elusive fault condition. I use a sucker on each pin of the i.c. and having removed most of the solder finally free each pin with a pair of pliers and if necessary the use of solderwick. This often leaves the odd pin still slightly secured in the hole: as the i.c. is carefully removed it's important to free any such pins before they lift and break the print. It's very easy to end up with a print crack on the top of the board and if undetected this crack will be covered when the socket is fitted. So if you have a particularly difficult fault, make sure that this hasn't happened. Check the signals at the i.c. pins and at the line end (the next component) to ensure track continuity.

## Checking the ICs

Next, i.c. checks. Table 2 lists the conditions at each pin of the i.c.s. The readings were taken using the Tandy Micronta logic probe featured in last November's issue of Television. The computer was at the inverse K cursor stage and the supply for the probe was taken from the 5 V rail - I always fit a short wire with a small loop to the 5 V plated-through hole near the regulator.

To simplify checking, the pins are listed in numerical order in Table 2 though quick checks at selected pins might speed up the testing. For example I always make an initial check on the 5 V and chassis pins of all the i.c.s, then the reset line and memory request pins of the CPU and the cell select and read pins of the ROM and RAM chips. But this is only my own view of what are the more important checks or those most likely to lead to a fault indication. All the pin signals are listed, even those directly connected to the pins of other i.c.s, as this makes for easier checking. As mentioned earlier when describing the circuit some data and address lines incorporate buffer resistors between the i.c.s. These can be very useful as failure of an i.c. at one end of a resistor won't affect the i.c. at the other end, so you can establish with certainty which i.c. is faulty.

It's often easy to locate a fault or anomaly in the signals on the lines but very difficult to establish the reason. The unnecessary removal of a 40 -pin i.c. is a non-profitable pastime to be avoided if possible. Other approaches can be adopted. One that has been with us since the earliest days of printed circuits is to cut the track. This is useful for tracing shorts, the computer equivalent of which is the loss of a logic signal. When deciding where to make the cut remember what was previously said about track cracks under sockets and try to avoid making any cut that would subsequently be covered by a socket. Another method of checking a suspect i.c. is to mount a good one on top piggy-back fashion: the legs should be sprung in and care taken to ensure that there's contact at all the pins of the suspect i.c. This doesn't always work but it's worth a try when you have two or three suspect soldered-in i.c.s. The method complements track cutting as it's particularly effective with open-circuit chips.

One last tip. When you suspect that ULA chip and don't have a spare - I usually suspect the item for which I don't have a replacement - remember that the TV screen will be bright if the ULA is all right, even if all the other

Table 2: Signals on the i.c. pins.

| Pin | N1 | IC2 | IC3 | $1 C 4 a / b$ |
| :---: | :---: | :---: | :---: | :---: |
|  | (ULA) | (ROM) | (CPU) | (RAM) |
| 1 | P | P | P | P |
| 2 | P | P | P | P |
| 3 | P | P | PL | P |
| 4 | P | P | P | P |
| 5 | P | P | P | P |
| 6 | P | P | P | P |
| 7 | PH | P | P | P |
| 8 | PH | P | P | P |
| 9 | P | P | P | L |
| 10 | P | P | P | P |
| 11 | P | P | H | P |
| 12 | P | L | P | P |
| 13 | P | P | P | P |
| 14 | P | P | P | P |
| 15 | PH | P | P | P |
| 16 | PH | P | P | P |
| 17 | P | P | PH | P |
| 18 | P | P | P | H |
| 19 | P | P | P |  |
| 20 | L | P | PH |  |
| 21 | P | P | P |  |
| 22 | OC | P | PH |  |
| 23 | P | P | H |  |
| 24 | P | H | PH |  |
| 25 | H |  | H |  |
| 26 | P |  | H |  |
| 27 | H |  | P |  |
| 28 | P |  | P |  |
| 29 | H |  | L |  |
| 30 | P |  | P |  |
| 31 | H |  | P |  |
| 32 | P |  | P |  |
| 33 | H |  | P |  |
| 34 | L |  | P |  |
| 35 | H |  | P |  |
| 36 | P |  | P |  |
| 37 | P |  | P |  |
| 38 | P |  | P |  |
| 39 | F |  | P |  |
| 40 | H |  | P |  |
| $\begin{aligned} & \text { P = pulse, high and low LEDs lit. } \\ & \text { PH = pulse and high LEDs lit. } \\ & P L=\text { pulse and low LEDs lit. } \\ & H=\text { high LED lit. } \\ & L \quad=\text { low LED lit. } \\ & O C=\text { no LED lit (open-circuit). } \end{aligned}$ |  |  |  |  |

chips are defective. So a bright screen without a cursor usually means that you should look elsewhere for the fault.

## Spares

The above paragraph reminds me that I mentioned in the introduction to this series last month that Sinclair spares are readily available. The supplier I use is PV Tubes, 104 Abbey Street, Accrington, Lancs BB5 1EE 025436521 or 025432611 . I find that when in a hurry a phone call quoting my Access card number will rush a spare to me - sometimes by the following morning. (Editorial note: the full address of CPC , mentioned in Roger Burchett's letter last month, is CPC Electronic Component Distributors, 194 North Road, Preston, Lancs - 0772555 034).

This concludes the notes on servicing the ZX81. Next month we'll start on the Spectrum and Spectrum Plus.

# Service Bureau 

Requests for advice in dealing with servicing problems must be accompanied by a $\mathbf{£ 1 . 5 0}$ cheque or postal order (made out to IPC Magazines Ltd.), the query coupon and a stamped addressed envelope. We can deal with only one query at a time. We regret that we cannot supply service sheets nor answer queries over the telephone.

## SONY KV2704UB

There are vertical stripes right across the screen, darker on the left-hand side and more noticeable on a plain raster. than a picture. There are also outlines to the left-hand side of verticals. These are more noticeable on faces and clothes. An outdoor aerial is in use, directly aligned with the transmitter.

For the striations we suggest you check the damping components in the line scan and EW modulator circuits R828 ( $10 \Omega, 2 \mathrm{~W}$ ), R831 ( $2 \cdot 2 \mathrm{k} \Omega$ ) and C834 ( $0 \cdot 01 \mu \mathrm{~F}$ ). If these are in order suspect ripple on a supply line - the 250 V supply reservoir capacitor $\mathrm{C} 825(22 \mu \mathrm{~F})$ is a strong possibility. Scope checks on the supply lines and at the c.r.t. electrodes should lead you in the right direction. If the ghosting effect is still present when the striations have been cleared, try the aerial with another set. If this gives ghost-free reception we would suspect the SAW filter SWF201.

## THORN 9000 CHASSIS

The problem with this set is mains fuse blowing. Replacing the Syclops transistor restores normal operation, but only for a few days or weeks.

The cause of this trouble is generally either latchety sockets on the base and emitter pins of the Syclops transistor, dry-joints on the Syclops and/or line output transformer, or intermittent failure of diode W702 or W704 in the Syclops circuit. These things should all be checked, the diodes preferably by substitution.

## PANASONIC NV366

The front panel controls frequently lock up - the cassette cannot be removed and all functions except for the clock and programmer are inoperative. Switching off the power for a lengthy period of time restores normal operation until the next lock-up.

Assuming that the supply lines are all present and correct, it sounds as if the syscon microcomputer chip is coming unhinged. Check first that its 5V supply (pin 39) is present and correct, with no ripple/hash. If all is well here you could try a mains "conditioner" before condemning the chip itself (MN1405VKK). A conditioner is likely to help only if you live in an area with a noisy mains supply. You'll most likely find one at the local computer shop - it goes between the VCR's mains plug and socket.

## GRUNDIG 8610

The picture is bright and sharp but there's a red background with red flyback lines. Interchanging the red and green drives changes the background to green with green
flyback lines. The effect is more noticeable with dark scenes and monochrome film.

Your R-G transposition check leaves little doubt that the problem lies on the RGB panel. Most often this inability to reach black level is due to a changed value component in the relevant $\mathrm{R} / \mathrm{G} / \mathrm{B}$ clamp/feedback circuit.' R1916 ( $100 \mathrm{k} \Omega$ ) and R1918 ( $470 \mathrm{k} \Omega$ ) are the first suspects. R1902 ( $220 \mathrm{k} \Omega$ ) which with R1901 biases the base of the pnp transistor in the red output stage is also well worth checking. Make sure that the red drive control R1911 is in order, then if necessary check C1912 $(4 \cdot 7 \mu \mathrm{~F}), \mathrm{C} 1914$ $(0.22 \mu \mathrm{~F})$ and the clamp pulse coupling capacitor C 1917 $(0 \cdot 1 \mu \mathrm{~F})$.

## RANK T20 CHASSIS

The channel indicator is stuck on 0 . All touch contacts seems to try channel selection but 0 remains.

We suggest you dismantle and thoroughly clean the touch contacts, the associated insulating surfaces and even the back of the touch pads. If the fault remains on reassembly it's likely that the SAS580/590 chips are faulty - we generally replace them as a pair (take precautions against static charges when handling them).

## THORN 9600 CHASSIS

Occasionally the set functions perfectly. Usually however after switching on it starts up then shuts down. In the shutdown condition voltages are still present at all major points.

The most common cause of this fault is dry-joints on the PCBs. Check the pins of the chopper transformer T512 carefully, then the pins of the line output transformer T801. If necessary check the line drive connecting pins of plug/socket 810 and the jointing and condition of the $0.47 \Omega$ series resistor R510.

## SANYO CTP7118

The set has an appetite for e.h.t. triplers - a replacement lasts for only about six months. This happened again recently and an examination showed that the casing had burnt through from the inside, near the fixing lugs. R764, which is in series with the EW driver transistor, also needed replacement. This time the new tripler lasted for only halr an hour however. The line output transistor, EW modulator diodes and small passive components in the line output stage all seem to be o.k. - we suspect the line output transformer. The h.t. is correct at 150 V though excessive demand from the line output stage pulls this down to about 70 V .

We would agree that the line output transformer T602 is probably faulty - we've had this happen with more than one of these sets. It's likely however that a faulty tripler ruined the transformer rather than the reverse. There

should be no more trouble when both have been replaced, but make sure that terminals D and M on the tripler are wired correctly (incorrect connection of these is a common mistake).


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Each month we provide an interesting case of TV/video servicing to exercise your ingenuity. These are not trick questions but are based on actual practical faults.

It's been a long and weary winter and on this spring day everyone in the workshop seemed to be out. Resident Workshop Sage (RWS) was gallivanting in Wales, RT (Real Technician) had taken a precious day's holiday to dig his garden while TS (Techno-Supersleuth) was out on the road fitting a teletext retrokit to a Sony TV set two villages away. The harassed Service Manager eyed the trainee with a beady eye: now was his chance to shine and put some of his college learning to practical use. Problem: his bench was equipped only for audio servicing. SM rigged up a portable 200W isolating transformer, then the mirror from the washroom, and supplied a conductive wristband - the latter a pointless if impressive gesture since there were unlikely to be any chips vulnerable to static in the motley collection of TVs in the waiting-repair queue.

The first of them was an ageing Pye colour set fitted with the 725 chassis. It was accused of intermittent low gain, the symptom being spasmodically snowy pictures. The trainee was in trouble from the moment he switched on! It took some time for the picture to appear, and when it did it was small and fluttering in size. Once tuned in the sound was present but was somewhat overwhelmed by a squeal from the area of the power supply circuitry on the right-hand panel. With these symptoms present the question of snowy pictures seemed somewhat irrelevant. Plainly the power supply department - a thyristor mains rectifier/regulator - was in pain. A circuit diagram was found and a brief study of the arrangements was made.

The trainee decided that a check on the 170 V h.t. line at fuse F971 would be a good start, especially as it's so accessible at the centre of the baseboard. The voltage here was found to be low and varying - its average level seemed to be around 140 V . The current passed by the fuse was less than 500 mA , so the trainee rightly concluded that the problem was not due to any excessive loading on the line. His next move was to squirt all the components in the PSU with freezer. This made the picture contract a little more. A few minutes of poking and prodding in the PSU was terminated when the phone rang. It was TS! He knew all about Pye TVs! Could he suggest anything for
the small, fluttering picture on the Pye 725 ?
TS was full of suggestions. Kick off by backing down the overvoltage trip potentiometer; if the picture still flutters check the trigger diac's $8 \cdot 2 \mathrm{M} \Omega$ bias resistor R 924 ; make sure that the feedback resistor R897 hasn't changed value; then suspect the diac (D892) and the thyristor (D888) said he. Magic thought the trainee as he walked back to his bench with a new spring in his step. Alas for pride! So much for experience! None of these things did any good at all. With a new BR100 trigger diac and BT116 thyristor, with the overvoltage trip transistor VT881 taken out of circuit, with replacement resistors in the R924 and R897 positions - and several others - the problem remained. The control transistor VT902 was changed, also its 7.5 V reference zener diode, but the fault remained.

Further thought led to a careful check on the huge $3 \cdot 3 \Omega$ surge limiter resistor R978. It measured $3 \cdot 21 \Omega$. A mighty muffer was procured and substituted for the h.t. reservoir and smoothing capacitors C880 and C877 in turn. It made little difference. An oscilloscope was brought into play and hooked to various points in the PSU, with confusing and inconclusive results. The main message provided by the waveforms was that the h.t. voltage was fluttering and that the conditions around the control transistor VT902 were also fluttering. The one crucial and revealing point in the power supply circuitry never saw the scope probe! What was it? Where did the fault lie? See next month!

## ANSWER TO TEST CASE 281 - page 452 last month -

The Hitachi VT33 VCR described last month was suffering from intermittent loss of drum servo lock, the effect being confined to the record mode. The fault condition was related to the white content of the off-air picture being received and recorded. The steps taken during the diagnostic procedure were logical and sensible - almost to the end! The cursory check of the video signal being received by IC202 on the Y/C board was inadequate. With a new i.c. fitted the symptoms remained the same. A more careful check was then made on the video waveform at the input to the Y/C panel. The field-rate display on the scope revealed that the video signal had a d.c. level that wandered wildly, with the field sync pulses on such a steep gradient that they fell across the same scope screen graticule as much of the video signal itself the effect of poor l.f. response.

The same sorry waveform was present at the i.f./ detector panel's video output, but not at the output from the video detector i.c. itself or at any of the three subsequent video amplifier transistors Q851/2/3. What had happened was that the video output coupling capacitor C859 ( $470 \mu \mathrm{~F}, 6.3 \mathrm{~V}$ ) had dried up and gone low in value, knocking off the l.f. response.

The simple test to prove all this? The technician should have injected a baseband signal at the video input socket. This would have produced consistently good drum servo locking during record.

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