ELECTRONIC & RADIO ENGINEER

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In this issue

Magnetic Tape Recording Amplifier for Decimicrosecond Pulses Super-Gain Aerial Beam Electromagnetic Wave Problems

Three shillings and sixpence

SEPTEMBER 1959 Vol 36 new series No 9

high efficiency with low cost

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BICC / downleads

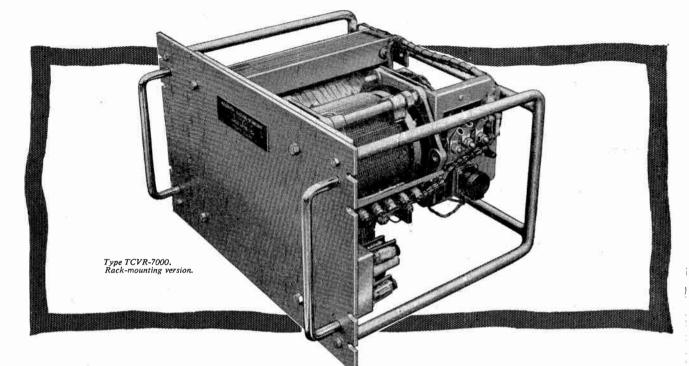
BRITISH INSULATED CALLENDER'S CABLES LIMITED, 21 Bloomsbury Street, London, W.C.1

Electronic & Radio Engineer, September 1959

ii

40 VOLTS/SEC AUTOMATIC CORRECTION

-with the type TCVR voltage regulator



The TCVR is a servomechanical automatic voltage regulator having the very high speed of correction of FORTY VOLTS PER SECOND. It provides an *undistorted* output, maintained constant within very close limits (normally $\pm 0.5\%$) from no-load to full-load, for wide variations in frequency and power factor.

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For high-speed, accurate stabilisation without distortion—specify TCVR.

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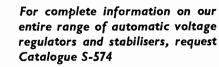
BMVR: Motor-driven laboratory and industrial regulators ranging from 1.6 to 29 kVA single-phase, and 4.8 to 87 kVA three-phase. Constancy of output normally \pm 0.5% from no-load to full-load. No distortion. Speed of correction 1 Volt/Sec. A great variety of models, standard, tropical and militarised, for all applications.

BAVR: Electronic stabilisers of very high accuracy, and very rapid response, with no moving parts. Input range: -10% to +5%, output constancy $\pm 0.15\%$. Three sizes: 200, 500 & 1000 VA. Exceptionally useful for control of chemical processes, heating, tighting, etc.

ASR: Automatic step regulators, small, inexpensive, and with sinusoidal output waveform. Two sizes: 1.15 kVA and 2.3 kVA. Input range -10% to +5%: output constancy, $\pm 2\frac{1}{2}\%$.

ATC: Automatic Tap-Changing Transformers — a development of ASR. Two sizes: 575 VA and 1150VA. Input range -20% to +10%: output constancy, $\pm 5\%$. Provide adequate stabilisation for many types of apparatus, at low cost. Also useful as pre-regulators, e.g. in conjunction with BAVR.





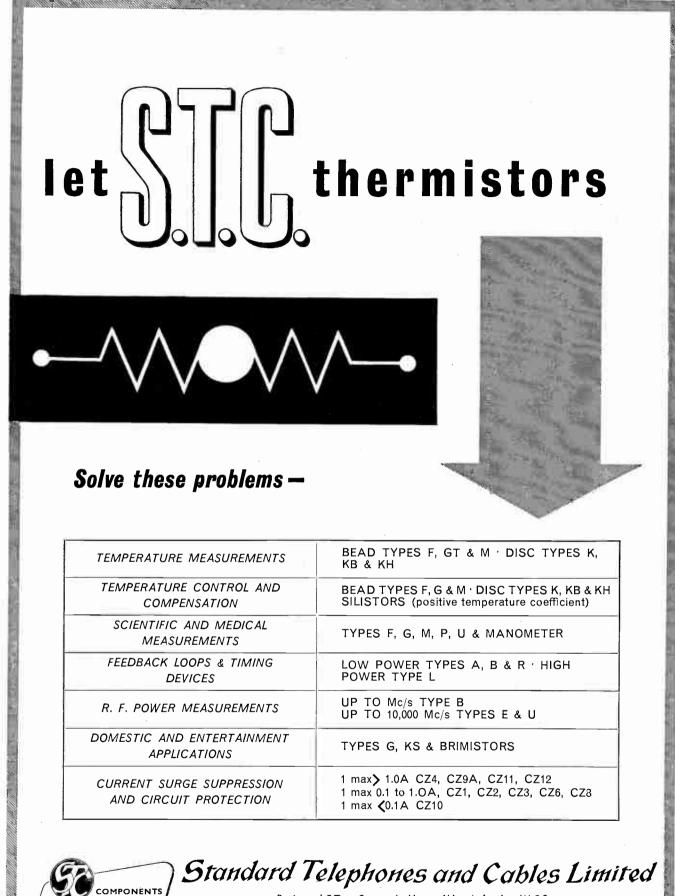
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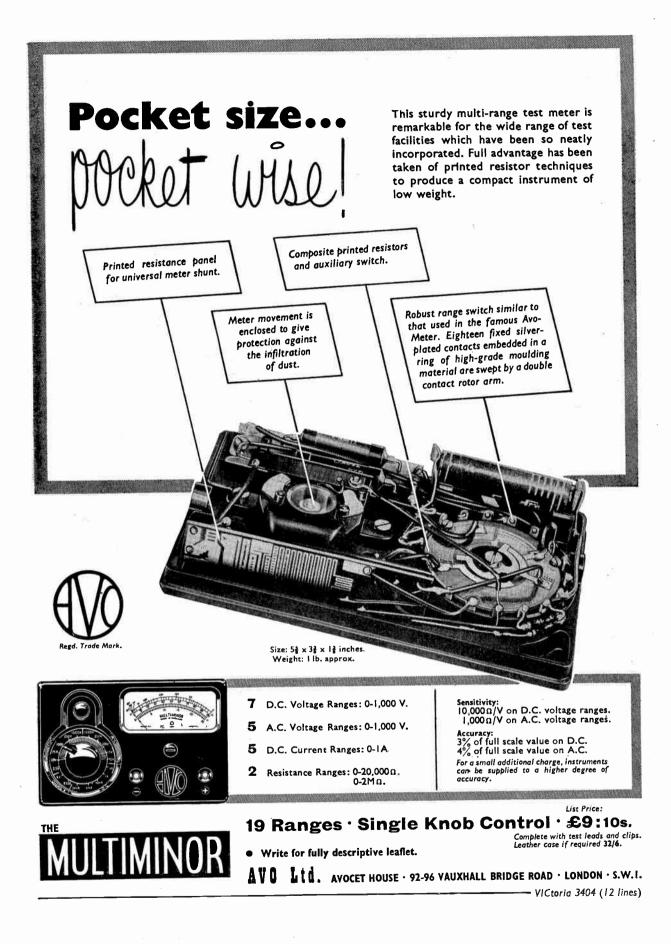
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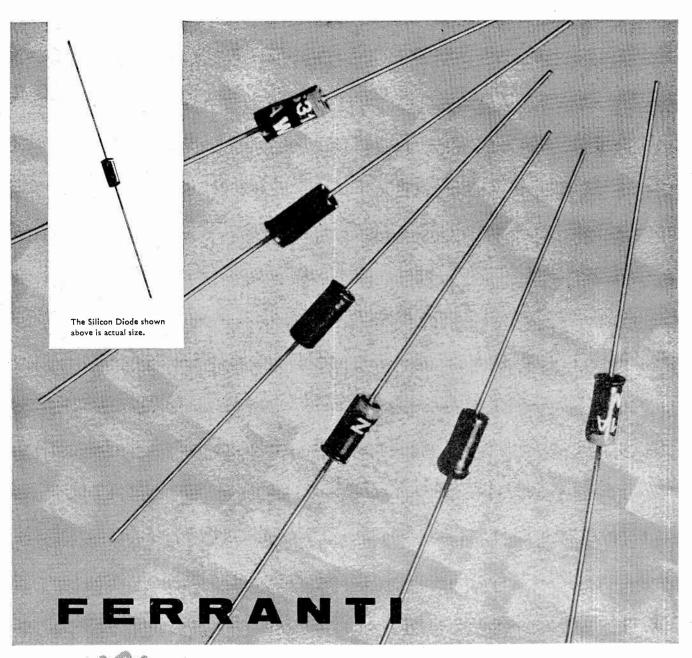
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BRIEF SPECIFICATION OF	'999' DIGITAL VOLTMETER TYPE LM901
Voltage ranges:	0 to 0.9999V; 0 to 9.99V; 0 to 99.9V.
Range extension:	An 'add 10' button extends the digital count to 1099.
Input impedance:	1 megohm; 100 kilohms on 0.999V range.
Accuracy of indication:	Absolute 0.25% long term. Short term 0.1% .
Reading time:	280 milliseconds for any change of indication.
Polarity & decimal display:	Both the polarity and decimal point position are clearly displayed.
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Silicon Diodes ZS30 series

for **MINIATURIZED** Circuitry

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● AUTOMATIC WIRING TECHNIQUES ● HIGH POWER TO SIZE RATIO HIGH TEMPERATURE OPERATION HIGH FORWARD CONDUCTANCE HIGH RECTIFICATION EFFICIENCY RUGGEDISED CONSTRUCTION

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Grade | (Aero Engines) > 500 g. Class HI Temperature Range -70° C to $+ 135^{\circ}$ C.

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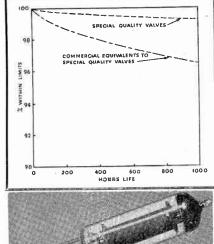
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TESTS PROVE M-O.V. SPECIAL QUALITY VALVES ARE SEVEN TIMES MORE RELIABLE THAN COMMERCIAL EQUIVALENTS

"Percentage within limits curves for M-O.V. special quality valves and for commercial valves."



In his article (given at the 4th National Symposium of Reliability and Quality Control in Electronics in New York). Mr. R. Brewer* describes the tests carried out on M-O.V. Special Quality valves. In comparing the reliability of these Special Quality valves with that of their commercial equivalents, he states:—"the Special Quality valves are about *seven times better* than their commercial equivalents."

*Research Laboratories of the General Electric Co. Ltd., Wembley. Reprints of Mr. Brewer's article, which first appeared in the April 1958 issue of "British Communications and Electronics", are available on request from the M-O. Valve Co. Ltd.

The table shows in detail the results obtained by the comparative lifetesting of special quality valves and their commercial equivalents. Of this and the vibration-fatigue test, Mr. Brewer writes:— "... tests carried out on four types of Special Quality valves have shown a high order of reliability in both types of test. The development of these valves has benefitted from the study of the causes of failures occurring in the life tests of commercial valves. This study has shown how valve assembly, processing and design faults can affect life, and it has thus provided an important feedback path by which improvements in valve reliability have been made."

"Comparison between Special Quality valves and commercial equivalents on 500-hour electrical life test."

Type r	eferences		Reliable		Commercial			
Reliable	Commercial	No, run	No. outside limits	% outside limits	No. run	No. outside limits	% outside limits	
CV4005 CV4014 CV4062	U78 Z77 N78	1,185 1,245 185	2 4 2	0.17 0.32 1.1	474 991 960	9 22 22	1.9 2.2 2.3	
	Totals	2,615	8	0,31	2,425	53	2.2	

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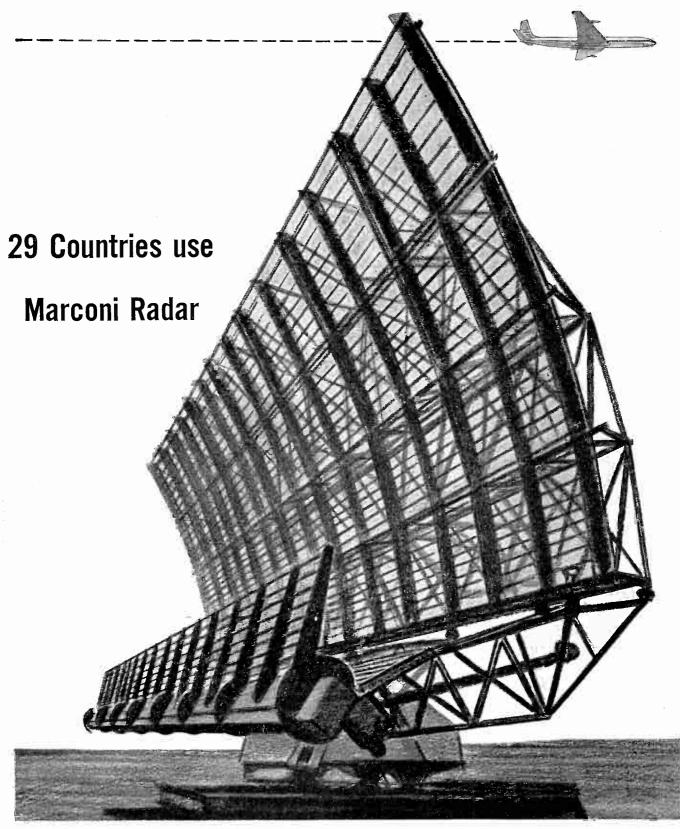
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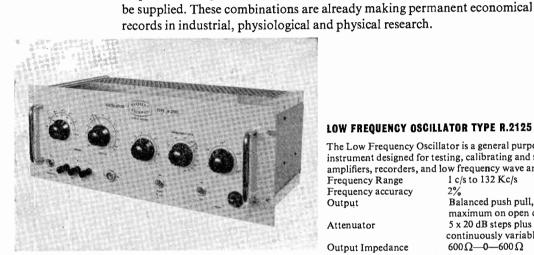


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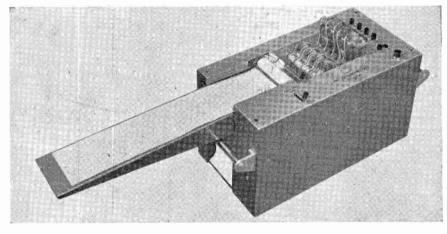
The Low Frequency Oscillator is a general purpose R.C. instrument designed for testing, calibrating and setting up amplifiers, recorders, and low frequency wave analysers." Frequency Range

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Attenuator

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8 CHANNEL PEN RECORDER UNIT

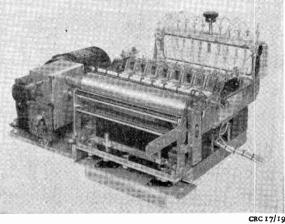
The pen motors incorporated in this unit are identical to those used in the 4 channel pen oscillograph. The unit includes 8 pen motors fitted into a magnet block, two time markers, ink system and paper drive mechanism. Three speeds of 1.5, 3 and 6 cms/sec. are available. The unit is offered as shown in the photograph and is intended for incorporation into the users own equipment. A 16 channel version of the above unit is also available.

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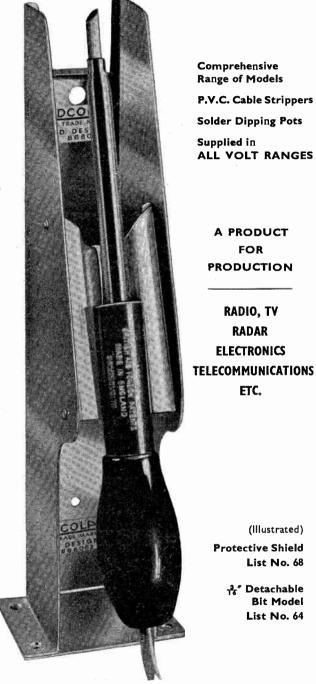
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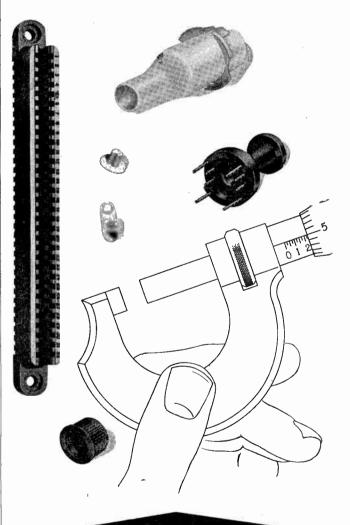
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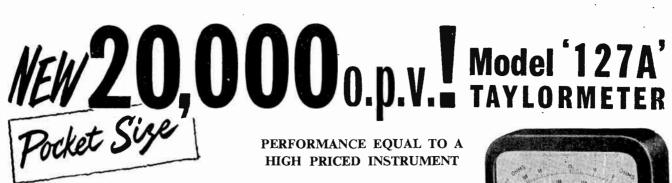
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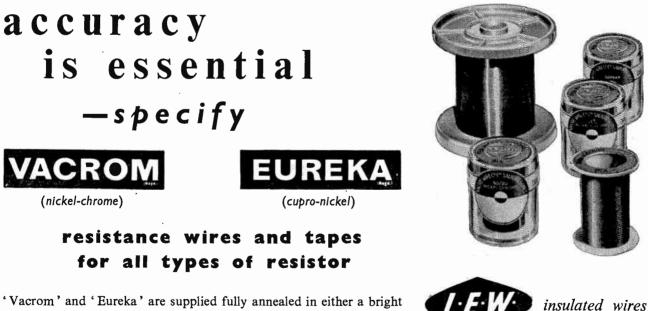
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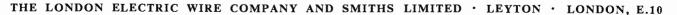
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Band width \dots D.C. to 40 Mc/s (-3dB)

Rise time \dots 9 mµsec.

Sensitivity 1 cm. per 100 mV.

By switch control the sensitivity can be increased to 1 cm. per 10 mV over a bandwidth of 2.5 c/s to 20 Mc/s. A nine-step attenuator and a fine gain control extend the sensitivity range to approximately 1 cm. per 12 V. An RC probe is available with 10-1 reduction factor, extending the range to a minimum of 1 cm. per 120 V. A balanced signal delay is incorporated in the amplifier enabling the observation of pulse leading edges.

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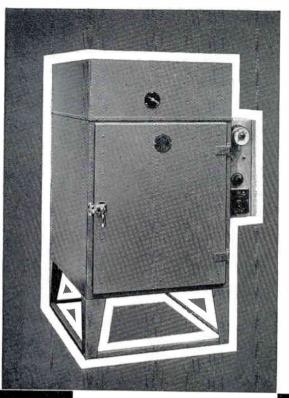


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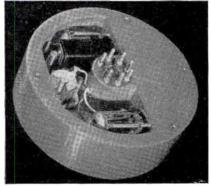


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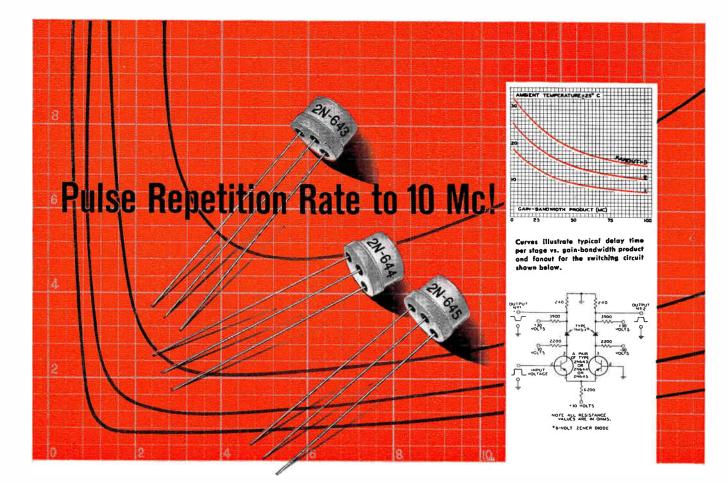
- ★ for producing patterns, models, jigs and tools
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The photograph, showing the Venner Mark II Whaling Buoy, is reproduced by courtesy of Venner Electronics Limited



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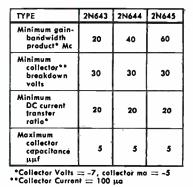
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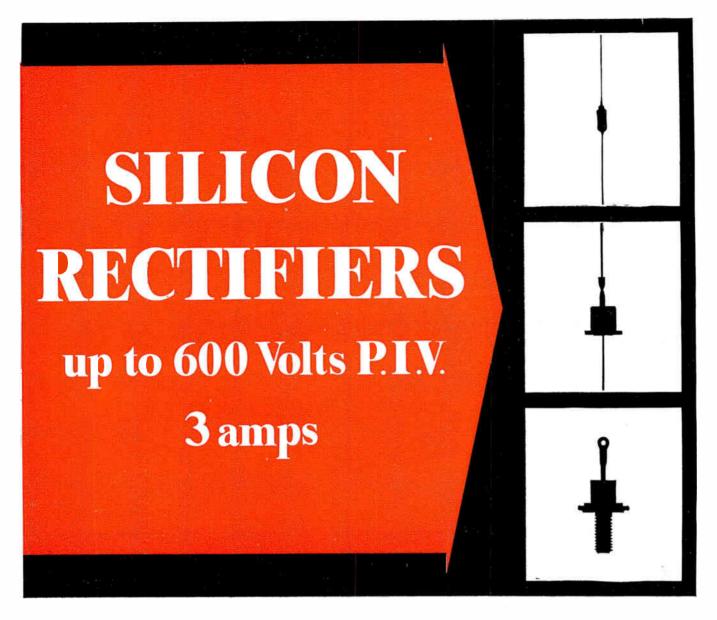




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Peak Inverse Voltage at -65°C to +150°C	PIV	200V	600 V	200V	600V	200V	600V
Average Rectified Forward Current at +50°C	I.	750mA	750mA	† 400mA	†400mA	*3A	*3A
Average Rectified Forward Current at +150°C	Ĩ.	250mA	250mA	150mA	150mA	*1A	*1A
Recurrent Peak Forward Current at +50°C	i,	† 2.5A	† 2.5A	† 1·25A	† 1.25A	*10A	*10A
Surge Current for 10 Milliseconds	IPK	16A	16A	6A	6A	33A	33A
Operating Temperature, Ambient	Ť	65°C to +150°C					
SPECIFICATIONS							
Minimum Breakdown Voltage at +150°C		240V	720V	240V	720V	240V	720V
Maximum Reverse Current at P.I.V. at +25°C	Llb	10µA	10µA	0.2µA	0-2µA	10µA	10µA
Maximum Forward Voltage Drop at +25°C	Eb	1.0V	1.0V	1.0V	1.0V	1.1V	1.1V
	5	(I _o =500mA)		(I ₀ =400mA)		(Ib=1Amp)	
* Rectifier mounted on 2" x 2" x it" aluminium Heat Sink † @ 25°C							

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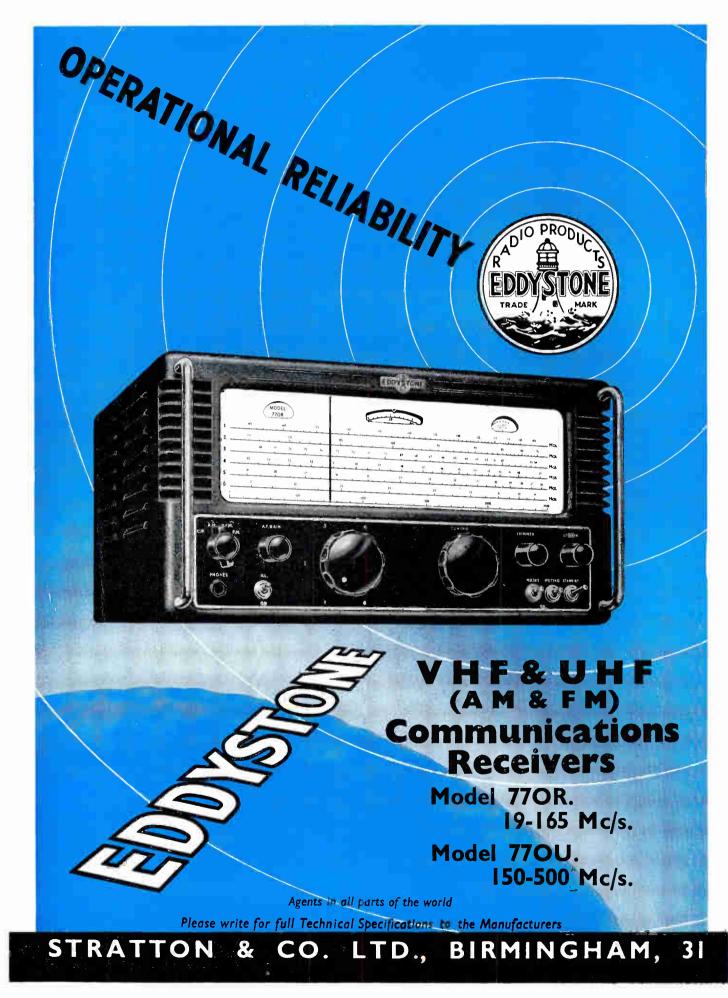
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CONTENTS VOLUME 36 NUMBER 9 SEPTEMBER 1959

ANNUAL SUBSCRIPTION

Parametron	319	Editorial
Magnetic Tape Recording	320	by L. H. Bedford, C.B.E., M.A.
Linear Amplifier for Decimicrosecond Pulses	323	by J. F. Golding and L. G. White
The Fringe of the Field		by Quantum
Electromagnetic Wave Problems	332	by J. D. Lawson
Super-Gain Aerial Beam	338	by R. F. Kyle
Transistor High-Frequency Parameter f1	341	by L. G. Cripps, B.A.
Mathematical Tools	347	by Computer
Coaxial Cable Performance	349	by W. A. Cameron, B.Sc.
Correspondence	352	
New Books	353	
Standard-Frequency Transmissions	355	
New Products		
Abstracts and References A137-A	154	

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ELECTRONIC & RADIO ENGINEER

VOLUME 36 NUMBER 9

SEPTEMBER 1959 incorporating WIRELESS ENGINEER

Parametron

I N our field, strange new words crop up almost daily and few people will be startled by this one. Some may guess that it is a device operating on the principle of the parametric amplifier, and they will be right.

Basically, the parametron is a resonant circuit in which either the inductance or capacitance varies periodically. When an exciting current of a certain frequency is applied to the inductance, say, an oscillation of one-half the frequency builds up in the circuit and this oscillation has one of two possible phase relations with the exciting current. These two phases can be used to represent 0 or 1 binary digits and so the parametron finds application in computers.

It appears to be widely used in this way in Japan and the parametrons employed have ferrite cores to furnish non-linear inductances. Exciting frequencies up to 6 Mc/s are used. Logical operations can be carried out and binary counters, adders and multipliers obtained without the use of valves or transistors. Even diodes are said to be unnecessary, since limiting effects are obtained by core saturation.

Quite an extensive literature on the subject exists, going back to 1954, and mainly in the Journal of the Institute of Electrical Communication Engineers of Japan. A recent article in Control Engineering (April 1959) gives a good deal of general information on the subject.

Devices of the type described do not appear to be electronic at all, any more than a magnetic-core memory is electronic. Parametric principles are being applied, however, with the capacitance of junction diodes as non-linear capacitance elements, and these are certainly electronic. It is rather uncertain whether or not these devices should be called parametrons. We ourselves think not and suggest that the term be reserved for non-electronic elements.

Is it being pedantic to point out that parametric, which is actually used in the sense of 'variable parameter', is really quite the wrong word?' A parameter is a quantity which is constant in the case being considered, but which may vary in different cases. Inductance, capacitance and resistance are all parameters of a circuit; more strictly, they are parameters in the describing equation. As soon as one of them is made a variable, surely it ceases to be a parameter!

Magnetic Tape Recording

HOW IS TAPE MAGNETIZED?

By L. H. Bedford, C.B.E. M.A.*

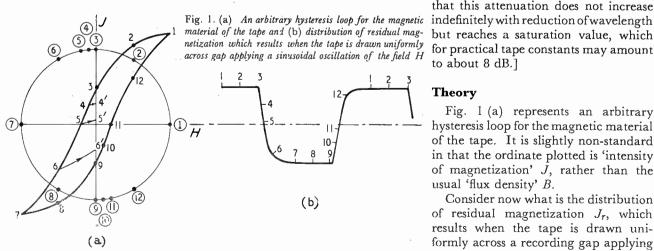
In view of the highly developed state of the taperecording art and of the existence of a number of advanced analytical papers on the subject, the writer has been puzzled for some years by the apparent absence of a clear and convincing account of the basic mechanism of the process. That such is indeed the position is confirmed by the fact that much questioning on the subject has invariably produced a negative answer and, further, by the following quotation from a recent comprehensive account of the subject¹:

"Three interpretations of the mechanism of h.f. bias have been given. Either through a suspicion of oversimplification or through unavoidable complication none is thought to be completely satisfactory". The writer would go further by saying that all are highly unsatisfactory.

This state of affairs is somewhat surprising in view of the fact that the introduction of the h.f. bias method was the 'break-through' on which the useful development of magnetic recording is based.

The situation is somewhat analogous to that in television in which the break-through occurred with the introduction of the storage camera tube, the Iconoscope, by Zworykin. The mechanism of the Iconoscope, however, proved to be quite different from what Zworykin imagined when he first conceived this epochmaking tube. Similarly, in the case of magnetic recording, the writer suspects that the h.f. bias method was tried out on the basis of a loose or inaccurate theory, and that its immediate success caused practical application to go ahead on an empirical basis, and to hell with the theory.

Some two years ago the writer, in desperation, * English Electric Aviation Ltd.



formulated for his own use a half-baked theory of the recording process. Recently the baking operation has been continued to a stage where, although incomplete, the theory seems to offer a sufficiently coherent picture to be worth presenting. It is accordingly given below but, as the conclusions are rather striking, it may be desirable to state these in advance:

Conclusions

1. What is fundamentally written on the tape is a distorted version of the bias waveform, consisting of alternately polarized quarter-cycles of constant magnetization separated by quarter-cycles of transition.

2. In the case of saturation bias, a possible but unusual condition, the signal is written as a variation of the mark : space ratio of this distorted bias waveform.

3. In the case of normal bias, the above mechanism also applies, but to it is added a variation in the relative magnitudes of opposite quarter cycles of constant magnetization.

Axiom

Recording takes Place at the Trailing Edge of the Recording Gap.

This is to say that the length of the recording gap is not of primary importance; it is possible to write a pattern whose wavelength relative to the length of the recording gap is indefinitely short. This means in particular that the bias frequency is recorded on the tape in toto though subject to attenuation in the permanent record by the mechanism of 'self-demagnetization of short magnets'. [Daniel², has shown

that this attenuation does not increase for practical tape constants may amount to about 8 dB.]

Theory

Fig. 1 (a) represents an arbitrary hysteresis loop for the magnetic material of the tape. It is slightly non-standard in that the ordinate plotted is 'intensity of magnetization' J, rather than the usual 'flux density' B.

Consider now what is the distribution of residual magnetization J_r , which results when the tape is drawn uniformly across a recording gap applying

a sinusoidal oscillation of the field H. The frequency of this oscillation is not important, but to fix our ideas let us suppose that this frequency is the bias frequency, whose wavelength on the tape is small compared to the gap length. Then any one element of tape finds itself cycled round the hysteresis loop some finite number of times during its passage through the gap until it arrives at the trailing edge where the field collapses abruptly from its current value to zero. (We here discount fringing effects.)

Points 1-12 have been numbered round the hysteresis loop and we consider the value of J_r corresponding to the collapse of the field to zero from each of these points in turn. Consider the conditions corresponding to point 1, that is to say the state of affairs for an element which arrives at the trailing edge when H is a maximum. The residual condition of the tape thereafter is that corresponding to point 3. The same applies to any point 2 intermediate between 1 and 3. It follows that the whole of this quarter cycle writes as constant intensity of magnetization, the remanence corresponding to H_{max} .

The next quarter cycle is more difficult to analyse because we do not 7. know to what values of remanent magnetization the points 4, 5 and 6 collapse. They are arbitrarily shown as the points 4', 5' and 6'.

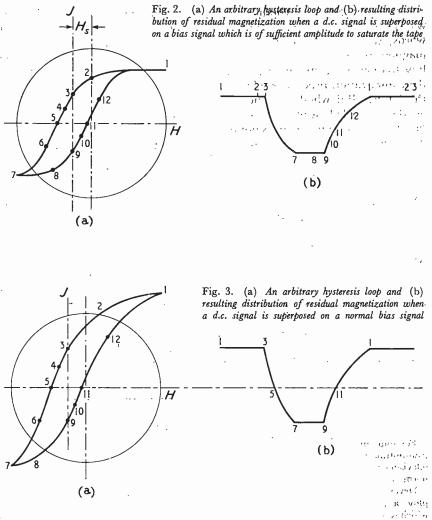
The following two quarter cycles are repeats of the . above in mirror image.

This figure allows us to plot the distribution of residual magnetization. For clarity, we introduce a circle whose radius describes H in vector fashion, and points (1) to (12) on the circle correspond to points 1 to 12 on the hysteresis loop. The distribution pattern then follows as Fig. 1(b). [The careful drawing out of this waveform is recommended as far more instructive than any amount of reading!]

As already remarked, the frequency is not of primary importance. If we regard it as signal frequency then the nature of the distortion revealed by Fig. 1(b) would indicate the uselessness of any attempt at direct (unbiased) recording. Note that the main feature of this distortion, namely the quarter-cycle flats, is quite unavoidable.

Now turn attention to Fig. 2, in which we regard the oscillation of H as occurring at bias frequency, and consider the effect of superposing a *signal* of relatively low amplitude and frequency—in fact we consider a d.c. signal. To simplify the discussion, and also to bring out the point that this is a perfectly possible mode of operation, we also consider initially the case of saturation bias; i.e., a bias amplitude sufficient to take the tape material well into saturation.

Again, points 1-12 are numbered around the hysteresis loop and again the circle indicates the magnetizing



field in vector fashion. The centre of the circle is now off-set from the zero of H by the amount H_s , the d.c. signal field.

Fig. 2(b) plots the resultant distribution of remanent magnetization. Note now that the regions of opposite constant magnetization are now of unequal length. The waveform thus contains a d.c. component of remanent magnetization. Thus it is that the signal is, written in a form which is most conveniently described as a variation of mark : space ratio.

Finally, in Fig. 3, we revert to the bias conditions relevant to Fig. 1 and indicate the effect of superposing a d.c. field H_s . It is clear that we now have two effects:

- (a) The unequal mark: space ratio as before, and
- (b) A difference of magnitude of the opposite values of constant magnetization.

Both effects co-operate to produce a d.c. signal component in the written waveform.

At this stage, it may be well to introduce a distinction between the terms 'written' and 'recorded'. By the former we mean the state of magnetization occurring immediately after the geometrical and magnetic discontinuity at the trailing edge; by the latter, whatever magnetization may finally result after any self-demagnetization has occurred.

It has already been indicated that vanishingly short magnets; e.g., of $\frac{1}{4}$ bias-wavelength, may be expected to decay in magnetization to the extent of some 8 dB.

What is not clear is whether or not the long-signal wavelengths are exempt from such decay; in other words, whether it is legitimate to resolve the written magnetization into a low-frequency component and bias-frequency components, and to consider the demagnetization process as selective to the detriment of the latter. But whether or not the signal components of the recorded waveform survive better than the bias-frequency components is not of ultimate importance since the latter are subsequently lost in the reproducing system in at least two other ways. First they are attenuated by the usual 'aperture effect' of the reproducing gap, which is several bias wavelengths long. Secondly, bias frequencies are well attenuated in the normal audio circuits of the reproducing amplifier.

In a very simplified experimental approach, whose unexpected results gave rise to the above theory, the writer examined the waveform resulting from a lowfrequency sinusoidal signal without bias. The immediate and striking observation was that the waveform changed very little *in shape* over a wide range of amplitudes. 'Flats' on the waveform were a prominent feature and these retained a constant proportion of the cycle with increase of amplitude. However, in other respects, the actual waveform differed markedly from what is predicted above. The discrepancy can be explained by assuming a phase error in the reproducing amplifier, this being compensated only for amplitude. Alternatively, the discrepancy may turn on the fact that the recording gap is short compared to the audio wavelength so that the tape elements are not subject to their normal cycling exercise³.

The above theory is aimed at clarifying the basic process of recording, and does not cover the more subtle points. Further, it has the following shortcomings:

1. Although it renders plausible the linear amplitude characteristic of a biased recording, it does not give a quantitative treatment of this.

2. Fringing effects, which may have serious repercussions, are ignored.

3. It is still not impossible that some minority effect (such for example as fringing) may over-ride the mechanism here described.

If the above theory has any value this may rest less on either novelty or mode of expression than on the fact that it is expressed at all.

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¹ H. G. M. Spratt, "Magnetic Tape Recording", Heywood & Co. Ltd., 1958.
 ⁸ E. D. Daniel, Proc. Instn elect. Engrs, Pt. III, 1953, Vol. 100, p. 168.
 ⁸ P. E. Axon, Proc. Instn elect. Engrs, Pt. III, 1952, Vol. 99, p. 109.

MOTION PICTURE FACSIMILE EQUIPMENT

For some months the B.B.C. has been using a special system for transmitting brief television news-picture sequences and other short television films over a circuit of the transatlantic telephone cable normally used for sound.

Developed by the B.B.C. Engineering Division, the process employs a slow-speed flying-spot film scanner, the video signal from which is used to modulate a carrier for transmission over the cable. At the receiving end the signals are demodulated and used to operate a slow-speed film telerecording equipment.

Transmission is over a normal cable which has a nominal bandwidth of 6.4 kc/s but, in order to limit the variation in the group delay/frequency characteristic to a value which can be corrected, it is necessary to restrict the usable video bandwidth to 4.5 kc/s. It has therefore been necessary to effect as many economies in the bandwidth of the video signal as are compatible with acceptable picture quality. These economies are : restriction of the horizontal definition to that corresponding with a bandwidth of 1.75 Mc/s in the 405-line system; a reduction to 200 lines using sequential scanning, and the scanning at the transmitting end of only alternate film frames with each frame-scan reproduced on two adjacent film frames at the receiving end.

These measures result in reducing the 3-Mc/s bandwidth of the British system to approximately 450 kc/s, the remainder of the bandwidth reduction is obtained by decreasing the scanning speed until the maximum video frequency corresponds with the available $4 \cdot 5$ -kc/s upper limit. The time required to scan the film is approximately 100 times the normal and thus a half-minute news flash takes approximately 50 minutes to transmit.

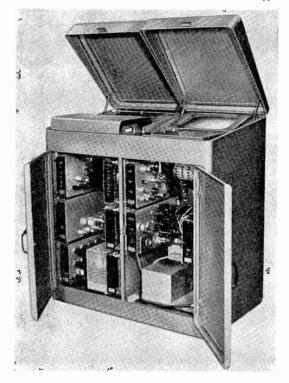
The effective picture repetition frequency of $12\frac{1}{2}$ per second results in satisfactory reproduction of most material excepting that in which rapid movement occurs.

Vestigial-sideband transmission is used with a special form of negative-going amplitude modulation. The carrier frequency is 5 kc/s and the whole of the lower sideband is transmitted, the vestige of the upper sideband extending from 5 kc/s to $5 \cdot 5$ kc/s.

A special form of modulation has been used in which the maximum depth of modulation considerably exceeds 100%. This method results in an increase in the effective depth of modulation and thus also in the signal-to-noise ratio of the system—a necessary improvement, particularly as volume-range compressors and expanders are not used. In order to achieve the synchronous detection needed, a regenerated carrier at the receiving terminal is used and is locked in phase to the original transmitted carrier.

The full amplitude of the video signal is used for the triggering edge of the synchronizing signal. The full synchronization signal consists of four similar pulses and protection is provided against these pulses interfering with the bursts of reference carrier which are used for oscillator locking.

Film-scanning equipment with doors open to show the electronic apparatus



Electronic & Radio Engineer, September 1959

Linear Amplifier for Decimicrosecond Pulses

By J. F. Golding* and L. G. White*

SUMMARY. This article deals with a novel linear amplifier for pulse signals where rise times of the order of $0 \cdot 1$ microsecond are required into fairly large capacitive loads. The conventional method of amplifying such pulses is by the use of low value anode load resistors or by the application of negative feedback to obtain the required bandwidth. In the system described, the bandwidth is increased by increasing the output power of the amplifier for the duration of the leading and trailing edges of the pulse.

he conventional methods of designing pulse amplifiers devolve upon the analysis of a step function into its constituent frequency components; the amplifier is then designed to have a frequency response of such a form as to produce minimal degradation of the pulse shape. The aspects of the design of such amplifiers have been dealt with very comprehensively by Brockelsby and others^{1,2,3,4}. The amplifier described in this article, however, was devised after considering its action from a rather different viewpoint.

In any amplifier intended for use with pulse waveforms the limit to the steepness of the edges of the output pulse is imposed by the charging time of the output capacitance. This charging time can be reduced by making the source impedance of the amplifier (when regarded as a voltage generator) as low as possible. And this is normally done either by the application of negative feedback or by the reduction of the value of the anode load resistor.

A brief quantitative analysis of the behaviour of a simple amplifier may be illuminating as an introduction to the line of reasoning adopted by the authors. Fig. 1(a) shows a typical pentode output stage with the stray output capacitance C indicated by dotted lines. The equivalent circuit of this amplifier is shown in Fig. 1(b).

The value is regarded as a constant-current generator in which I is equal to $g_m e_g$. Now, if e_g takes the form of an instantaneous step function, the voltage developed across the load will be equal to RI only after the capacitance C has fully charged; that is to say, when the charging current has dropped to zero. Theoretically, of course, the capacitor takes infinite time to charge completely; but it will charge to a given proportion of the final output voltage in the time t given by

$$t = CR \cdot \log_{e} (I/i_{c}) \qquad \dots \qquad \dots \qquad \dots \qquad (1)$$

where I is the output current of the value, i_c is the instantaneous charging current.

If the time of rise is to 90% of the pulse height, time t is given by

$$t = CR \log_{e} (I/0.1I) = 2.3026CR \qquad .. \qquad (2)$$

Now, C is determined by the stray capacitance. So, in order to achieve a specified time of rise, R must be adjusted accordingly. If, then, a particular pulse

Electronic & Radio Engineer, September 1959

height is required, the necessary current will be given by V/R; where V is the required pulse height.

Apart from the large valve required to handle this current, the total current drawn from the power supply becomes uneconomically high. Furthermore, it can be reasoned from the above argument that the rise time of the output pulse is inversely proportional to the

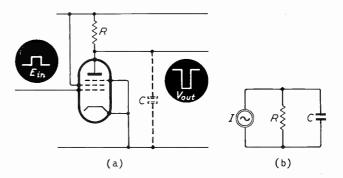


Fig. 1. (a) Typical pentode output stage; (b) equivalent circuit regarding the valve as a constant-current generator having negligible shunt conductance

available output current from the valve regardless of any conventional means of achieving wide frequency bandwidth, such as negative feedback.

As an example, consider an amplifier for supplying a 100-volt pulse to a capacitive load which, together with circuit strays, amounts to 100 pF. And let us suppose that a rise time of $0.1 \ \mu$ sec. is required.

From (2) we can calculate R.

 $R = t/2.3026C = 10^{-7}/(2.3026 \times 10^{-10}) = 460 \ \Omega.$ Therefore, for 100 volts pulse height

I = 100/460 = 0.2176 A.

If the amplifier is to handle positive and negativegoing pulses, the valve must be operated under class A conditions, and this implies a standing anode current of the order of half an amp.

The difficulty can be overcome by the use of a separate valve which supplies the charging current for the output capacitance. Such an arrangement is shown in Fig. 2. Valve V_1 is the pulse amplifier. The total capacitance shunting the output is represented by capacitor C_{s} , shown dotted. The current in the shunt capacitance is sampled by inserting a low-value resistor in series with part of it. This is done by means of the

^{*} Marconi Instruments Ltd., St. Albans, Herts.

network C_1 and R_1 , where the capacitance of C_1 actually forms part of the shunt capacitance. Providing the time constant of this network is small compared with the rise time of the output pulse, the instantaneous voltage across R_1 will be directly proportional to the instantaneous current in the total shunt capacitance.

The differentiated voltage pulse developed across R_1 is amplified and inverted by valve V_2 ; and the output from the anode of this valve is fed to the grid of a class B amplifier V_3 connected in parallel with V_1 .

If, then, a sharp positive-going step voltage is applied to its grid, valve V_1 will immediately begin to draw an increased current, discharging C_8 and C_1 . The pulse output voltage, however, will not increase—in the negative direction—to its peak until the shunt capacitance has fully discharged. But, due to the amplified differentiated pulse appearing at its grid, valve V_3 will conduct very heavily during the discharge period, giving a very rapid leading edge to the output pulse.

Quantitative Analysis

The circuit shown in Fig. 2 can be represented as that shown in Fig. 3(a). Valve V_1 is a constant-current generator, its output *I* being equal to $g_m e_g$. The current i_{α} is equal to the product of the voltage developed across R_1 and the effective mutual conductance of the auxiliary boost amplifier (V_2 and V_3); i.e.,

 $i_a = A \cdot i_{C1}R_1$... (3) where i_{C1} is the current in capacitor C_1 , A is the effective mutual conductance of the auxiliary amplifier; i.e., the current output of V₃ divided by the voltage input to V₂ and

 $i_{C1} = i_{Cs}[C_1/(C_1 + C_s)]$... (4) where i_{Cs} is the current flowing in the total shunt capacitance. N.B. The total shunt capacitance includes C_1 .

Therefore

$$i_{\alpha} = i_{Cs}[A \cdot R_1 \cdot C_1/(C_1 + C_s)] \cdot \dots \cdot (5)$$

For convenience let us call the factor within the large brackets k. So i_{α} then becomes $k \cdot i_{Cs}$.

The circuit in Fig. 3(a) is, in turn, equivalent to that

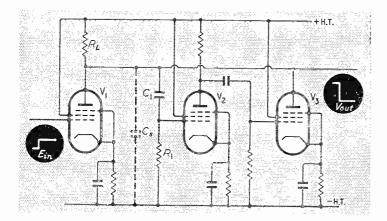


Fig. 2. Basic arrangement of auxiliary boost circuit

shown in Fig. 3(b). If the input voltage to the grid of V_1 is assumed to be an instantaneous step function, we can say that *I* is equal to V/R_L , where *V* is the height of the output pulse.

It will readily be appreciated that ideally k should be equal to unity. For, if this is so, the whole of the charging current will be supplied by the boost amplifier $(V_2 \text{ and } V_3)$ so that the pulse output voltage rises instantaneously with the input voltage. This is, of course, not a practical possibility; but it is interesting to analyse the action of the circuit in order to assess how nearly the ideal condition can be approached.

The current in R_L is given by the expression

 $i_R = I + k \cdot i_C - i_C = I + i_C(k-1) \dots$ (6) where i_R is the current in R_L ; i_C is the current in C_s .

From basic energy-transfer theory we can derive an expression for the instantaneous voltage as follows:

$$I = i_R + i_C(1-k) = \frac{q}{CR} + \frac{dq}{dt}(1-k)$$

where q is the charge in C_s . This can be rewritten

$$\frac{dq}{q - CRI} = \frac{dt}{CR(1 - k)}$$

Integrating both sides,

$$\log_{e} (q - CRI) = \frac{-t}{CR(1-k)} + K$$

where K is the constant of integration.

To evaluate K, take the condition when t = 0; then q also equals 0.

Therefore

 $K = \log_e \left(-CRI \right)$ so that

 $(q - CRI) / -CRI = e^{-t/CR(1-k)}$

This can be rewritten $1 - (q/CRI) = e^{-t/CR(1-k)}$

But RI is the pulse height V; and q/C is the instantaneous voltage v.

Therefore

$$v = V [1 - e^{-t/C_s R_L (1-k)}]$$
 ... (7)

It would appear from the above that, if k = 1, the voltage across R_L will be equal to the pulse height and independent of time. So long as k is less than unity

the circuit will remain stable; but, if k is allowed to exceed unity, the factor within the large brackets becomes negative and the circuit will tend to ring. Taken to extremes, of course, if the gain of V₂ and V₃ is increased sufficiently the circuit will oscillate.

It must be remembered, however, that the derivation of expression (7) is based upon the assumption that the time constant C_1R_1 is negligible. This approximation simplified the reasoning and is virtually true for most practical pulses. But it is obvious that it is not possible to make v equal to V unconditionally. To establish the ultimate limitations it is necessary to take all the circuit parameters into consideration. This may not be entirely possible because it is difficult to account for all the stray impedances. Nevertheless, a close approximation can be made because by far the most important limitation is due

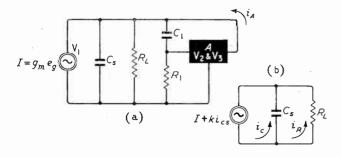


Fig. 3. Equivalent circuits of Fig. 2

to the time constant C_1R_1 ; and, if this parameter is taken into account, it can be shown that the fastest rise time obtainable is given by the expression

$$v = V \left[1 - \left\{ 1 + \left(\sqrt{x} - 1\right) \frac{t}{T} \right\} e^{\frac{-t\sqrt{x}}{T}} \right] \qquad \dots \tag{8}$$

where x is $C_8 R_L / C_1 R_1$; T is $C_8 R_L$

It can also be shown that the ultimate condition of stability is given by the expression

$$k \leq 1 + [C_1 R_1 / R_L (C_1 + C_s)] \qquad \dots \qquad (9)$$

As the time constant C_1R_1 tends to zero so the limiting value of k tends to unity; but, so long as the value of C_1R_1 is not negligible, k can exceed unity slightly without producing instability.

The mathematical derivations of expressions (8) and (9) are given in the appendix to this article.

The Positive-Going Edge of the Output Pulse

The circuit shown in Fig. 2 provides for negligible deterioration of the negative-going edge of the output pulse. It does not, however,

pulse. It does not, nowever, operate when the input voltage to the grid of V_1 is a negative-going step. The complete circuit of a system suitable for linear amplification of positive-going and negative-going pulses is shown in Fig. 4.

Two additional valves, V_4 and V_5 , form a second boost circuit which provides the charging current for the shunt capacitance during the positive-going output step. The operation of valves V_4 and V_5 is similar to that of V_2 and V_3 . Since the second pair of boost valves operates in the reverse direction from the first pair, it is necessary to connect them between the output line and a separate 500-volt h.t. line.

The circuit shown in Fig. 4 is of an experimental

Fig. 4. Practical circuit of amplifier

Electronic & Radio Engineer, September 1959

amplifier designed to use type EF91 valves. This amplifier was designed to provide a 50-volt output pulse with a rise time and fall time of 0.1 μ sec across a capacitive load of the order of 100 pF.

With a 10,000- Ω anode load and an h.t. of 250 V, valve V₁ has a dynamic g_m of 2.5, giving a stage gain of 25. The shunt capacitance having been set artificially at 100 pF, the value 10 pF was chosen for capacitor C_1 . Then, if the time constant of the sampling network is to be small compared with $0 \cdot 1 \mu$ sec, a series resistance of the order of 500 Ω can be used for each of the boost circuits, giving an overall time constant of 0.01μ sec. In practice, a pair of 1,000- Ω variable resistors (VR_1 and VR_2) were used.

The figure for k can then be obtained by substituting the constants given above in (5).

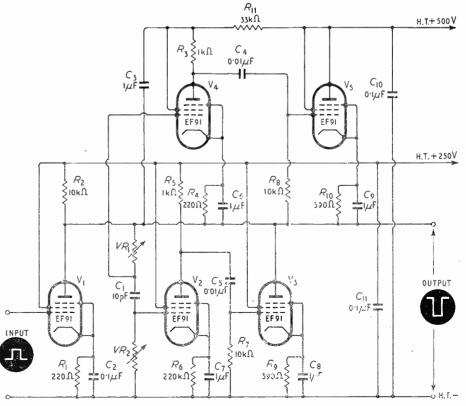
Thus

$$k = A \frac{5 \times 10^2 \times 10^{-11}}{11 \times 10^{-10}} = 50.A$$

Therefore, if k = 1, A = 0.02.

This means that 1-V input at the grid of V_2 or V_4 must give an anode current of 20 mA in V_3 or V_5 . This figure is only about three times the g_m of the valve so that the voltage gain of V_2 and V_4 need only be of the order of 4. This gain is easily achieved with the use of a 1,000- Ω anode load. The stray capacitance shunting the anode loads of V_2 and V_4 should not exceed 10 pF even allowing for wiring strays. This gives a time constant for the anode circuits of these valves of the order of 0.01 μ sec so that there will be negligible deterioration of the differentiated pulse if the rise time of 0.1 μ sec is adequate.

In order to obtain linear amplification of the pules



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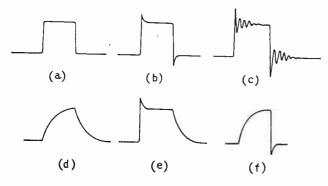


Fig. 5. Output pulses for various settings of linearity controls for positive output pulse; i.e., negative input pulse.

(a) VR_1 and VR_2 correctly adjusted;

(b) VR_1 and VR_2 too high;

(c) VR_1 and VR_2 very much too high, causing ringing;

(d) VR_1 and VR_2 too low;

(e) VR_1 too low and VR_2 too high;

(f) VR_1 too high and VR_2 too low.

 $N.B.-VR_1$ controls negative-going edge; VR_2 controls positive-going edge

signals it is, of course, important that the circuit should be so adjusted that k is in fact equal to unity. This adjustment is made by means of the variable resistors VR_1 and VR_2 . These resistors control the voltages applied to the respective boost circuits, and thus they control the effective gain of each of these circuits.

The amplifier is set up by empirical means. A pulse signal having a rise and fall time of less than 0.1 μ sec is fed to the grid of V₁. The output pulse is monitored by means of a suitable cathode-ray oscilloscope. With the desired capacitive load connected, variable resistors VR_1 and VR_2 are adjusted for the sharpest obtainable output pulse with no overshoot on the leading and trailing edges. Overshoot indicates that k is greater than unity. Fig. 5 indicates the forms of oscillograms of the output pulse for various settings of the variable controls. It will be found that the settings of the controls are interdependent, and that it is necessary to adjust both controls simultaneously.

If the value of k is adjusted to exceed unity by an appreciable amount, the circuit becomes unstable. This instability takes the form of damped oscillation superimposed upon the pulse or upon the baseline following the pulse.

The EF91 is not by any means the ideal valve for this purpose; it was used because it was the most suitable valve available to the authors when the experimental amplifier was constructed. The maximum instantaneous cathode current of this valve is of the order of only 300 mA. With a valve such as the 6F17, which is specially designed for exceedingly heavy instantaneous currents, a very high standard of performance should be obtainable with large capacitive loads.

Conclusion

The circuit described has several advantages over the conventional feedback type of amplifier. The most important of these is probably the fact that both positive-going and negative-going transients are amplified by driving a valve into conduction.

When a positive-going step voltage is applied to the

grid of a feedback amplifier, the valve will conduct very heavily due to absence or reduction of feedback during the transient period. But, when the negative-going step is applied to the grid, the anode current will be reduced—perhaps to cut-off—and the stray capacitance will charge through the load resistance at a rate determined by the time constant $C_s R_L$. This means, of course, that R_L must be a comparatively low value to produce a steep edge with the result that the standing current of the feedback amplifier will probably be very little different from that of the simple amplifier in Fig. 1. For, even if the amplifier is required for positivegoing input pulses only, it cannot be run fully in class B; it would be driven beyond cut-off during the negativegoing trailing edge of the pulse.

To the best of the authors' knowledge, the system devised, using a boost amplifier to provide the charging current for the stray capacitance, is original. The system is perhaps related to the shunt-regulated amplifier devised by Cooper^{5,6}, in which a boost valve is connected in series or in parallel with the output valve in order to compensate for a load which varied with voltage applied to it.

Also, the method of sampling the charging by means of a small RC circuit in parallel with the stray capacitance is not unlike the system used by Gouriet⁷ for compensating for frequency distortion in a transmitted signal.

APPENDIX

Mathematical Analysis of the Amplifier

Referring to Fig. 3(a), let i_{cs} be the current in C_s , let i_r be the current in R_{L_s} and let i_c be the current in C_1 and R_1 . Then

$$g_{m}e_{g} + AR_{1}i_{c1} = i_{r} + i_{cs} + i_{c1}$$

$$v = i_{r}R_{L} = i_{cs}/p_{r}C_{s} = i_{c1}(R_{1} + 1/pC_{1})$$

where v is the instantaneous output voltage; p is the Heaviside operator.

$$\therefore g_m e_g = v \left[\frac{1}{R_L} + pC_s + \frac{(1 - AR_1)}{(R_1 + 1)pC_1} \right] \dots (10)$$

Then

$$\frac{v}{e_g} = g_m R_L \frac{p/C_s R_L + 1/C_1 R_1 C_s R_L}{p^2 + p[1/C_1 R_1 + 1/C_s R_L + (1 - AR_1)/C_s R_1] + 1/C_1 R_1 C_s R_L}$$
(11)

Let $C_s R_L / C_1 R_1 = x$ and $C_s R_L = T$ So that

$$\frac{v}{e_s} = g_m R_L \frac{p/T + x/T^2}{p^2 + \frac{p}{T} \left[1 + x + \frac{R_L}{R_1} (1 - AR_1) \right] + \frac{x}{T^2}} \qquad \dots (12)$$

$$= g_m R_L \frac{p/1 + \omega_0^2}{p^2 + 2\alpha p + \omega_0^2} \qquad \dots \qquad \dots \qquad \dots \qquad (13)$$

This is a standard form which is readily interpretable as a time function by means of a table of Heaviside transforms. There are three solutions, depending on the relative values of α and ω_0 . The condition for stability is that both roots of the denominator must be negative and real or have negative real parts. The roots are :

$$p_1, p_2 = -\alpha_z^2 \pm \sqrt{\alpha^2 - \omega_0^2} \qquad \text{if } \alpha^2 > \omega_0^2$$

 $p_1, p_2 = -\alpha \pm j\sqrt{\omega_0^2 - \alpha^2} \quad \text{if } \alpha^2 < \omega_0^2$ In both cases stability demands that α be a respectively of the state of the

In both cases stability demands that $\boldsymbol{\alpha}$ be a positive number, and this requires

$$1 + x + \frac{R_L}{R_1} > AR_L$$
 (14)

If α^2 is less than ω_0^2 the step response will be oscillatory. In order to avoid this α^2 must be equal to or greater than ω_0^2 . For circuits having this form of characteristic equation, the fastest rise time for a

non-oscillatory response is obtained with $\alpha^2 = \omega_0^2$. For this condition

$$\frac{v}{e_g} = g_m R \left[\frac{t}{T} e^{-\alpha t} + 1 - (1 + \alpha t) e^{-\alpha t} \right]$$

$$= g_m R \left[1 - \left\{ 1 + (\alpha - 1/T) t \right\} e^{-\alpha t} \right] \qquad \dots \qquad \dots \qquad (15)$$
Since $\alpha^2 = \omega_0^2$, we can write $\alpha = \sqrt{x}/T$; so that
$$\frac{v}{e_g} = g_m R_L \left[1 - \left\{ 1 + (\sqrt{x} - 1) \frac{t}{T} \right\} e^{-\sqrt{x}t/T} \right]$$
The condition for $\alpha^2 = \omega_0^2$ amounts to
$$\left| \frac{\sqrt{x}}{T} \right| = \left| \frac{1}{2T} \left[1 + x + \frac{R_L}{R_1} (1 - AR_1) \right] \right|$$
or $2\sqrt{x} = 1 + x + \frac{R_L}{R_1} (1 - AR_1)$

$$\therefore \quad 0 = (1 - \sqrt{x})^2 + \frac{R_L}{R_1} (1 - AR_1)$$
or $AR_L \doteq \frac{R_L}{R_1} + (1 - \sqrt{x})^2 \qquad \dots \qquad \dots \qquad \dots \qquad (16)$

From (14) we can find the limiting value of k for stability.

$$k = AR_1 \cdot \frac{C_1}{C_1 + C_s} = AR_L \cdot \frac{R_1/R_L}{1 + C_s/C_1}$$

But stability demands
$$AR_L \ge 1 + x + \frac{R_1}{R_L}$$

So the limiting value of k
$$= \left[1 + x + \frac{R_L}{R_1}\right] \cdot \frac{R_1/R_L}{1 + C_s/C_1}$$
$$= 1 + C_1R_1/R_L(C_1 + C_s) \qquad \dots \qquad \dots \qquad \dots \qquad (17)$$

However, the limiting condition for a non-oscillatory step response is given in (16), and this can be interpreted as a lower value of k as follows :----

$$k < \left[\frac{R_L}{R_1} + (1 - \sqrt{x})^2\right] \cdot \frac{R_1/R_L}{1 + C_s/C_1}$$

= $\left[\frac{R_L}{R_1} + 1 - \frac{2\sqrt{C_sR_L}}{\sqrt{C_1R_1}} + \frac{C_sR_L}{C_1R_1}\right] \cdot \frac{C_1R_1}{R_L(C_1 + C_s)}$
= $1 + \frac{C_1R_1 - 2\sqrt{C_1R_1C_sR_L}}{R_L(C_1 + C_s)} \dots \dots \dots (18)$

It is evident that the limiting values of k as determined in (17) and (18) tend to unity as the time constant C_1R_1 tends to zero. But, whereas the limiting value for circuit stability exceeds unity when C_1R_1 is not negligible, the limiting value for a non-oscillatory step response is slightly less than unity for values of C_1R_1 less than $C_s R_L$.

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ELECTROCHEMICAL RELAY

A recent discovery by Stanford R. Ovshinsky of Ovitron Corporation, U.S.A., promises a new and interesting control componentthe electrochemical relay.

It comprises two large electrodes immersed in an electrolyte and a third central control electrode. Initially, the a.c. resistance between the two large electrodes is high but, when a direct current is passed through the control electrode, it falls to a very low value. When the direct control current is interrupted, the relay reverts to its initial condition.

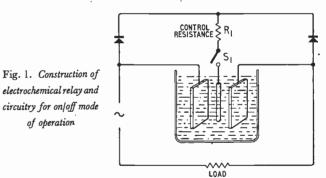
The schematic diagram of Fig. 1 shows the necessary circuitry for the on/off mode of operation and the component parts of the relay. The relay chamber contains a solution of acid and free ions, immersed in which are the load electrodes which are made of a film-forming material such as tantalum. The control electrode is an acid-resistant platinum rod, located half-way between the load electrodes. The large electrodes are connected to the load and the a.c. supply in series. Two rectifiers are connected back to back to the large electrodes to provide the d.c. bias for the control electrode. With the switch S_1 open there is no energizing voltage applied to the control electrode and, therefore, the relay is 'open' and presents a high resistance between its load terminals.

With S1 closed, the control electrode becomes positive with respect to the load electrodes and the resistance between the main electrodes falls to a low value. The alternating current then depends mainly on the magnitude of the load resistance.

One prototype model is completely sealed in an inert plastic case measuring 1.5 in. high by 1.5 in. diameter, with a plug-in base termination. It has a contacts rating of 4 A, 70 V r.m.s. The peak voltage that can be handled is 140 V; if the supply voltage exceeds this, the electrolyte conducts regardless of whether or not the control electrode is energized. The minimum supply voltage is 3 V.

Typically, with an applied voltage of 30 V a.c. and a load resistance of 65 Ω , the alternating load current is 450 mA and the direct control current 18 mA. The load current remains a true sine wave and is apparently unaffected by passage through the electrolyte. When the relay is energized and current is flowing, the

Eléctronic & Radio Engineer, September 1959



impedance between the electrodes is approximately 2Ω . At the instant of make the impedance is higher but it stabilizes at a constant value after a short time.

The impedance changes slightly with variations of load current, but this characteristic is less marked for high values of load current.

The load current varies with the magnitude of its control current. In consequence, the electrochemical unit will function not only as a relay but also as a power-modulating device. The design of a given relay can be modified to provide any one of a wide range of ratios between the load current and control current; at present, typical values range from 10:1 to 50:1 and, as would appear logical, the speed of response is greater at the lower ratios.

The speed of response of load current to control current of the electrochemical relay is somewhat similar to the magamp in that the response is definitely related to the frequency of the applied voltage. During tests, the load circuit has been opened within $\frac{1}{2}$ to 3 c/s of the 60-c/s applied voltage. The magnitude of the applied voltage does have a slight effect on the speed of de-energization but varying the load current, within limits, has no measurable effect.

Initial tests of the electrochemical unit show that the rated temperature rise is 50 °C and the operation is relatively stable over ambient temperatures from -10 °C to 150 °C. These tests also show that the units are unaffected by vibration, moisture, mounting position, external electrostatic or electromagnetic fields.

^{*} Based on an article "The Electrochemical Relay: A kemarkable New Switching Form", by John. D. Cooney, Control Engineering, July 1959, p. 121.

NEWS FROM NEUTRONS

Some of the matters to be mentioned here recapitulate what was said about strong and weak interactions earlier this year. Be patient about this. It is not an easy sort of subject, and it is something even to get the vocabulary straight. I do not profess to be able to follow the details of the theory of β -decay, but I began to be worried when the mere volume of experimental information about it (or the fraction that has come my way, to be honest) got beyond me to sort out at all. Then a bit of sense broke in, and I realised that I was trying to do things the hard way. For the main principles are, I think, laid bare by some not over-involved experiments on one particle only—the neutron.

Since the article on Glasstone 1958 that appeared in this journal in April, two very good articles on elementary particles have been published. The first of these. "Elementary Particles-the Present Situation", by P. E. Hodgson, appeared in Science News, Vol. 52. May 1959. The author concentrates on the experimental side of the production and classification of the thirty-odd named particles. He gives a table of the various modes of formation and decay of the charged and neutral K-mesons; magnificent bubble-chamber pictures of typical events-mentioning incidentally that results are pouring out from the high-energy machines so abundantly that the bottle-neck appears to be in scanning the pictures, for which automatic processes have been devised. He refers to the new conservation laws, and to the new 'strangeness' quantum number attaching to certain hyperons which, so to speak, outlive their welcome, and gives a table of the particles with their spins, isotopic spins, strangeness (where applicable), Q-values for decays, and energies of decay products. But he does not say much about what some of these attributes mean.

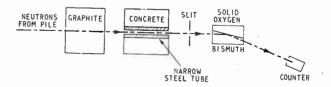
The second, a contribution by Prof. D. H. Wilkinson to the most admirable book, "Turning Points in Physics" (North-Holland Publishing Co., 1959), approaches the matter from the other side. His article, "Towards New Concepts-Elementary Particles", explains the ideas that have emerged from the experimental work. He does go very fully into the origin of the terms isotopic spin and strangeness, and also mentions the matters of parity conservation (which amounts to the assumption that space is symmetrical towards events) and time-reversal (which amounts to saying that if we could run time backwards, a process would be expected to happen in the reverse order). The importance of the latter is quite considerable, for the uncertainty principle shows that there are 'holes' in observable time in which virtual processes can occur; if it doesn't behave itself when we are standing over it with a stop-watch, where are we? Fortunately it appears that time does

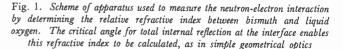
behave symmetrically as far as experiments go; it seems to stand the test of time.

He also explains the difference between strong and weak interactions, a point taken up in the next section of this article. If you take together Mr. Hodgson's account and that of Prof. Wilkinson, you have a good picture of the theoretical and the practical sides, both expressed lucidly in simple terms. For those of you who would look further, there is an article on "The New Particles" by Prof. O. R. Frisch in the June 1959 number of the Bulletin of the Institute of Physics, which discusses schemes for correlating slow decay processes and predicting those that might be found. And I should mention also the publication in June of J. Hamilton's book, "The Theory of Elementary Particles" (Clarendon Press: Oxford University Press), which is on the scale of Heitler and Dirac, and which at a first glance I found far too difficult for me. I shall have to try to do my duty by you and get round to this in time if I can. It confirmed my belief that the best way to start on this sort of topic at my level is to take on something relatively simple like a single solitary neutron.

Strong and Weak Interactions

The most familiar particle-particle interaction is the electrostatic action between a proton and an electron. It is also the easiest for the mathematician to handle, as the figure which can be taken to represent its size is $2\pi e^2/hc$, which is the fine-structure constant 1/137 whose square and higher powers can be neglected. Actions between nucleons-n, n; n, p; p,p-appear to be independent of charge, to involve a high energy, to happen very quickly, and to be represented on the same scale by a figure of the order 1 to 10. They are called strong interactions. The third class, of which the β -decays of the π -meson and the μ -meson and the neutron are typical, involve very much less energy, take place more slowly in the sense that the excited particle has a relatively long half-life (that of the neutron, for example, is about 10³ seconds though the





others mentioned come nowhere near this) and are represented by a figure more like 10^{-12} . They are called weak interactions. The Λ° hyperons and other 'strange' particles were given this name originally because their decay releases a great deal of energy, but their half-life is consistent with a weak interaction. Any kind of β -emission, such as that of 60 Co, is weak.

Now, once the meson had been introduced as the means by which strong interactions occurred, it was a more or less straightforward task to frame a theory which seemed to fit them. The weak interactions gave, and are giving, all the difficulty. It was realized that they probably involved some hitherto unsuspected principles, or departures from accepted ones.

Strong interactions treat all directions in space alike, and have always been regarded as conforming admirably with the laws of conservation of energy and of angular momentum. Weak interactions did not fit in with these conservation laws, and the suspected reason, namely the neutrino (or antineutrino), was eventually found. Weak interactions do not treat all directions in space alike, or need not necessarily do so. In seeking a reason for this, it may be that the ground shifts somewhat from the properties of particles and the nature of their interactions by means of fields to the properties of space—which may amount, I suppose, to the same thing in the end.

The β -decay of the neutron,

$$n \rightarrow e + p + \nu$$
,

which releases about 1 Mev of energy, of which the antineutrino and the recoiling proton take an unpredictable share, is the simplest weak interaction for experimental study.

Optics of Neutrons

The optics of neutrons is a much less geometricaloptics affair than that of electrons. They cannot be focused by electric and magnetic fields, or made to do Newtonian-particle tricks. On the other hand, their Compton or de Broglie wavelength $\lambda = h/mv$ can be altered by moderating their speed, and beams of a homogeneous velocity (monochromatic neutrons) can be obtained by reflecting them at nearly grazing incidence from a crystal. The analogue of the X-ray 'Bragg angle' depends on v (or on λ), so that those coming off in a given direction are monochromatic. Collimation is done, as with X-rays, by using a long thin tube; and, indeed, the whole job is much more like X-ray optics than electron optics.

With this difference, that the neutron's magnetic moment is a major significant property. X-rays are undeviated by a magnetic field, and electrons go round in circles; but neutrons tend to set with their magnetic axes in line with the field (either parallel or antiparallel), and so can be polarized by it.

Study of Weak Interactions

In the classical Lorentz electron theory of optical refraction and dispersion, the electron is considered as an oscillator with a natural frequency which responds as a sort of forced oscillation to the electromagnetic waves; and the refractive index for electromagnetic waves of a given frequency is worked out in terms of the number of electrons per unit volume and the coupling between the oscillators and the waves. For 'waves' read 'neutrons', of wavelength $\lambda = h/mv$ if you like; and for 'forced oscillation' read 'weak interaction between neutrons and electrons'. The picture is then translated into neutron-optics terms. Neutrons passing from a vacuum to a medium should thus be refracted; the refractive index will depend on the extent of the interaction between the neutrons and the electrons in the medium, and on the number of electrons per unit volume. If we know the latter and can measure the refractive index, then the magnitude of the neutronelectron interaction can be calculated.

Things are not so simple really, because the nuclei of the atoms in the medium have their say in things,

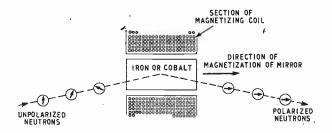


Fig. 2. Production of polarized neutron beam. The diagram is in a sort of semi-perspective, and the mirror is surrounded by a magnetizing solenoid, and also attached to a voke (not shown) completing the magnetic circuit. The direction of magnetization is from left to right. Unpolarized neutrons striking the surface at a suitable angle are reflected with their magnetic axes parallel to the direction of magnetization of the mirror

and scatter the neutron beam. So the refractive index is, in fact, measured by determining the critical angle at a boundary between two solids which have approximately the same scattering effect but widely different electron densities, such as bismuth (Z = 83, density 8.9 gm/cc) and solid oxygen (Z = 8, density of the order 1.1 gm/cc). The critical angle then gives the relative refractive index between the two media. The apparatus is shown in Fig. 1. It should be noted that this experiment measures the strength of the action between a neutron and an electron, not that of the action of β -decay.

Polarization of Neutrons

You remember all about Malus and reflection at a dielectric or transparent surface, and the Brewster angle in the production of polarized light. Something rather similar in appearance is done to obtain a polarized beam of neutrons (Fig. 2) by reflection at the surface of a smooth sheet of magnetized iron or cobalt. The magnetic axes of the neutrons are aligned either parallel or antiparallel to the direction of magnetization of the mirror, and we have the same situation as in optics, where we never really get one beam of polarized light, but always two which often conveniently separate themselves. Here it appears that the mirror acts not only like a Malus reflector, but also like a calcite crystal, as the refractive index is different for the two directions of polarization. Total reflection can occur at the surface, but the critical angle is different for the two directions of polarization, and a beam in which one polarization

predominates can be obtained by arranging the direction suitably.

With a beam of polarized neutrons undergoing β -decay as they travel, it was possible to see whether this orientation of their axes conferred any preferential direction on their decay products.

Symmetry Properties in the Decay of Polarized Neutrons

This series of experiments was performed by M. T. Burgy and his collaborators at the Argonne National Laboratory, and V. L. Telegdi of the University of Chicago, and published in the Physical Review, Vol. 110, p. 1214 (1958). A very narrow vertical-strip beam of slow ('thermal') neutrons with their spins setting horizontally in one direction (or about 87% of them doing so) was obtained by scattering a collimated beam, that had been previously moderated and rendered monochromatic, at a very small grazing angle from a vertical mirror of magnetized cobalt, about 12 cm high by 120 cm long. While the half-life of a neutron is about a quarter of an hour, sufficient individuals decay while traversing a 15-cm length of the evacuated detector chamber (Fig. 3) for the event to be recorded, first by a pulse in the electron detector due to the β -particle, and then after the proper short interval by a pulse in the proton detector. The two together check that this is indeed a genuine β -decay event. With the mirror magnetized one way, the neutron spins were

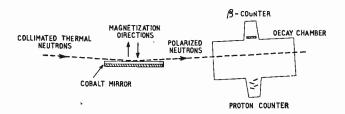


Fig. 3. Scheme of apparatus for testing symmetry in β -decay, viewed in plan. The cobalt mirror, set vertically, could be magnetized horizontally in either of the directions shown by the arrows, so that the beam of neutrons entering the decay chamber was a thin vertical wafer with the neutron spins setting horizontally in the appropriate arrow direction, pointing either towards or away from the β -counter. The β -counter used a scintillator in conjunction with a photomultiplier, and the proton counter a system of dynodes

polarized towards the electron detector, while with its magnetization reversed, they were polarized with the spin-axes pointing away from it. It was found that 20% more electrons were emitted in a direction opposite to the spin direction than along the spin direction. In order to check that this was attributable solely to differences in the neutron polarization, each observation was repeated with the neutron beam depolarized by passing it through a very thin steel sheet at the entrance to the chamber.

The foregoing account may be a little misleading, in that it seems to suggest that the electrons had to go one way or the other. The point is, that a symmetrical distribution *might* have been expected, but that there was instead an emission in all directions, but with that against the spin favoured. There is an analogy in the events of the cricket field. You might think that somebody like Lock or Laker would get people dismissed from catches in any part of the field in equal proportions; actually a high proportion of them fall to catches on one particular side due to playing against the spin. Do not think, by the way, that I am implying that cricket is nothing but a form of weak interaction nowadays. It is a noble instrument of instruction, without which no schoolboy would ever believe in Newton's laws of motion, and no true Briton ever be reconciled to the principle of glorious Uncertainty; if it did not exist, it would be necessary to invent it in the interests of physics.

But this analogy runs away with me, and could be pursued to the point of infinite tedium. As compared with football, which is a highly-energetic strong interaction of short half-life (45 min), cricket is indeed a low-energy interaction of long half-life. The various decay modes can usually take anything up to three days, and 'strange' encounters which take an unconscionable long time dying have been observed by many reporters in various Commonwealth centres. Footballers are symmetrical in their play-like Wodehouse's man with two left feet most of the time, and craftily ambidextrous when the referee isn't looking; the cricketer is consistently either left-handed or right-handed. In football, time and space treat both sides more or less impartially; not so in cricket, where one side or the other is usually trying to beat the clock and there is no precedent for any spatial symmetry involving both sides batting at once. And, of course, there is this odd twocomponent business in cricket; the ball may be accompanied by an anti-particle, the no-ball-which cannot exist until it is detected. The impatient among you may be fidgeting, and murmuring about bats that get stored in belfrys; but I am plodding through the drowsy sun-drenched summer afternoon to the stage at which I intend to declare.

This is the point. Put yourself in the position of an intelligent footballer seeing a cricket match for the first time and trying to interpret it in familiar terms, and you are somewhere near the problem that the theoretical physicist found in weak interactions. The most difficult part is really in absorbing the vast array of apparently unco-ordinated events, and in finding out what the pattern really is. So far as I can understand things, this side is pretty well under control now. Next, to try and find out why it all happens, the sensible footballer would probably seek to isolate the simplest type of interaction, that of a single bowler and batsman at the nets. Once he understood what each was trying to do, he would then have some hope of sorting out the many-body interactions of a full-dress match. And this, of course, is where the neutron experiments come in; they are, to end this analogy for good, a study of weak interactions practising at the nets.

To return to business. In the action $n \rightarrow e + p + \nu$, the antineutrino flies off in one direction and the proton recoils in the other. The antineutrino itself cannot be detected, but the recoil proton can and is. Going through the experiment again, but this time noting the relative numbers of protons for the two orientations of the neutron spin, it was found that there is a strong preferential emission of antineutrinos *in* the neutron-spin direction.

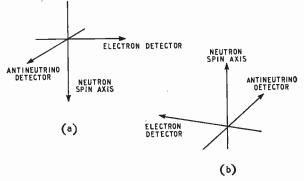


Fig. 4. Time-reversal simplified: (a) the relative directions of antineutrino (or proton) detector and electron detector as we would see them, (b) as the same situation would appear to an observer for whom time was running backwards and who sees all the timeable things—the momenta of electron and proton, and the neutron spin, reversed. As can be seen by rotating (b), this differs only from (a) in that the direction of the neutron spin relative to the other two arrows is reversed. In this experiment, to see whether reversal of the neutron spin affected the counts in the two detectors, they were shifted from the positions of Fig. 3 to those shown here

What symmetry really means in this connection is that a process involving certain spatial directions, and the process obtained by imagining the whole thing reflected in a mirror, should, if symmetry obtained, have the same relations between the relative directions. That is, the same result should be obtained in equations in which x, y, and z are replaced by -x, -y, and -z. The experiments, in showing that symmetry of this kind breaks down in β -decay, help to discriminate between types of equation which might be used to describe the process.

An Experiment with Time

So much for x, y, and z. But what about the fourth co-ordinate, t? Well, there is no question of making time run backwards, but it is possible to forecast the result of putting -t for t in the equations by taking up the view-point of an imaginary observer for whom time was running in reverse. Fig. 4 (a) shows the directions of emission of antineutrino and electron (the proton is omitted) with respect to the neutron spin. A timeinverting observer would meet this as it is, but would *record* this same event with the direction of the spin and of the momenta of the electron and antineutrino reversed. Now, this second point of view is related to the first like the Fleming left-hand motor rule, and the right-hand dynamo rule.

In Fig. 4(a), with your left hand say to yourself, "forefinger electron, second finger neutron-spin, thumb antineutrinos". And apply the same incantation to Fig. 4(b) with your right hand. If you now superpose the forefingers and thumbs of the two hands, you see that this amounts only to the direction of the neutron spin being reversed.

Reading, of course, recoil-proton detector for antineutrino detector, it is only necessary to preserve the two directions of these fixed, and to note their respective particle counts for the two opposite orientations of the neutron spin in order to check whether time is operating symmetrically. These experiments showed that it did.

The significance of these results is rather harder to explain. I can only say, as the Burgy-Telegdi paper does, that they help to discriminate between some four possible processes that might account for β -decay. Until the experts can get round to putting things a little more simply, that is about the best that I can do. Meanwhile, it is interesting to reflect that after about twenty years of serving nuclear physics as a piece of furniture rather like your own trusty electron, and after a rather shorter career in nuclear power as (in the words of O. R. Frisch) an industrial commodity to be consumed by the ton, the neutron has been promoted to a post of special responsibility in the attack on the mysteries of weak interactions.

THE OPHITRON

A compact microwave generator embodying a new focusing principle has been developed by the General Electric Co. Ltd.

This value is an electrostatically focused backward-wave oscillator which has been named the 'Ophitron'. The name is derived from a Greek word meaning a serpent and is suggested by the undulating path of the electron stream flowing along the structure. The main advantages of this oscillator are: small size (6 in. long by $\frac{3}{4}$ in. diameter), low weight (7 oz.) and its simple construction.

A single stamped-out periodic structure and two flat focusing plates form the propagating path for the r.f. wave, and set up the periodic electrostatic field which focuses the electron beam. The system has the fundamental advantage that the crests of the undulating electron beam are brought into the region of the maximum r.f. field. This feature gives good coupling between beam and wave and gives a large bandwidth. The present Ophitron tunes electronically over at least a 40% band in the 10,000-Mc/s region.



G.E.C. electrostaticallyfocused backward-wave oscillator

The complete artificial

larynx showing the com-

bined on/off switch and

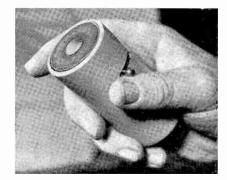
inflection control

TRANSISTORIZED ARTIFICIAL LARYNX

A new artificial larynx, for persons who have lost their voices through surgical removal (laryngectomy) or paralysis of their vocal cords, has been developed by Bell Telephone of America.

Still in the experimental stage, it is completely self-contained in a unit $3\frac{1}{4}$ in. long by $1\frac{3}{4}$ in. diameter. The underlying principle is a vibrating driver (transducer) which is held against the throat. By means of a finger-operated combination push-to-talk switch and inflection control, the user can control the frequency of the driver and, therefore, the pitch of his artificial voice. Users of this 'larynx' can, with practice, achieve a sentence intelligibility of 97%. In this unit, two transistors are used in a relaxation oscillator

of variable frequency and pulse width. The frequency is variable between 100 to 200 c/s for men and 200 to 400 c/s for women.



Electromagnetic Wave Problems

A SYNTHETIC APPROACH

By J. D. Lawson*

S UMMARY. A number of wave problems encountered in physics and electrical engineering are related in ways which may not be immediately apparent. In this article a number of such problems are discussed in such a way as to bring out their common features. First, the plane electromagnetic wave in a loss-free medium is described in some detail; the physical distinction between the normal uniform plane waves and slow or 'inhomogeneous' waves, in which the amplitude varies exponentially in one direction, is emphasized. This is followed by a discussion of some diffraction problems in which the fields may be readily synthesized as a spectrum of plane waves. Cylindrical systems are then introduced by the imaginary operation of 'rolling up' planar systems; thus a corrugated surface guide supporting a slow wave becomes a linear accelerator or a magnetron according to whether it is rolled up in a direction perpendicular or parallel to the corrugations. Radiation from an electron moving in a straight line (Cerenkov radiation) and in a circle (synchrotron radiation) are studied by considering the electron as a δ -function of current which can be resolved by Fourier analysis into a spectrum of sinusoidal currents, each associated with a travelling electromagnetic wave. In this case analogies are drawn with surface waves on wires and with corrugated surfaces rolled up in such a way that the corrugations are on the outside. Also discussed are the properties and limitations of 'super-gain' aerials, and their relation to phenomena associated with the wave-mechanical description of neutron scattering.

The solution of the time-independent wave equation $\nabla^2 + (2\pi/\lambda)^2 = 0$ has a wide variety of forms, each with its appropriate mathematical description. Sometimes this mathematical description tends to obscure the essential simplicity of the physical situation, and does not reveal features common to a number of systems. A physical description of the field distribution often depends essentially on the topology and scale (the ratio of a characteristic dimension of the system to λ), whereas a mathematical description is very sensitive to the actual geometry. Thus, the difference between the

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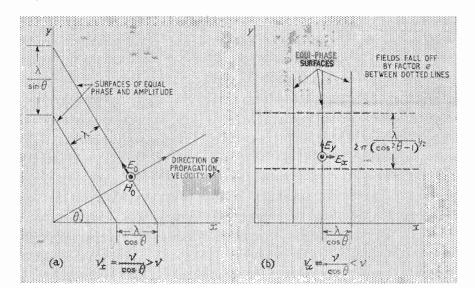


Fig. 1. Two forms of plane wave in a lossless medium

wave propagation in a circular waveguide and a hexagonal waveguide is physically trivial, but a mathematical description of the fields looks very different in the two cases. In this article some common features of topologically similar problems are discussed in terms of physical ideas obtained from the study of the two forms of the simple electromagnetic plane wave in a loss-free medium.

The method is descriptive rather than deductive, and the object is merely to show a few underlying physical features common to a number of phenomena which may not appear at first sight to be closely related.

> Simplifications are made, and intuitive reasoning is sometimes used; it is felt that this is justifiable in an article designed to present familiar ideas in a slightly unorthodox way, rather than to obtain new results. Adequate treatments of the subjects under consideration will be found in the references, which are to articles which are readily available rather than to original sources.

Two Forms of Plane-Wave Solution

The plane-wave solution of Maxwell's equations in a lossless medium will now be described. Co-ordinates are chosen such that the magnetic field is in the z direction, then if the direction of propagation of the wave makes

an angle θ with the x axis the field components are given by the real part of the expression:

$$H_{z} = H_{0} \exp \left\{ 2\pi i (ft - x \cos \theta | \lambda - y \sin \theta | \lambda) \right\}$$

$$E_{x} = -Z_{0} H_{z} \sin \theta$$

$$E_{y} = Z_{0} H_{z} \cos \theta$$
(1a)

 Z_0 is the intrinsic impedance of the medium, and the wavelength and frequency are related to the velocity of propagation v by the equation:

$$v = f\lambda$$
 (2)

A diagrammatical representation of such a plane wave is given in Fig. 1(a). It will be seen that the apparent wavelengths measured along the x and y axes are $\lambda/\cos\theta$ and $\lambda/\sin\theta$ respectively. The phase velocity of the disturbance is therefore $v \sec \theta$ along the x axis and $v \csc \theta$ along the y axis. These velocities vary between v and ∞ as θ varies, so that in such a wave they are always greater than v. This result is quite familiar in the theory of rectangular waveguides in which the simplest mode in a guide of width a consists essentially of two interfering plane waves at angles $\pm \sin^{-1} (\lambda/2a)$ to the direction of propagation.

It is of interest also to consider the impedance of the wave system defined by Equ. (1a). In a wave system referred to cartesian co-ordinates the impedance Z_x measured in the x direction is given by $Z_x = E_y/H_z$, provided that there are no other components of field in the yz plane^{1,2}. The significance of this quantity is that it is continuous across boundaries parallel to the yz plane. For the plane wave under consideration, Fig. 1(a), $Z_x = E_y/H_z = Z_0 \cos \theta$. Similarly $Z_y = -E_x/H_z = Z_0 \sin \theta$.

In deriving the solution of the wave equation given in Equ. (1), the only restriction placed on $\cos \theta$ and $\sin \theta$ is that $\cos^2\theta + \sin^2\theta = 1$. It is therefore necessary to investigate solutions in which $\cos \theta$ is greater than unity and $\sin \theta = \pm i(\cos^2\theta - 1)^{\frac{1}{2}}$ is pure imaginary. Writing the solution in terms of $\cos \theta$ and choosing the negative imaginary value of $\sin \theta$ yields

$$H_{z} = H_{0} \exp \left\{-2\pi y (\cos^{2}\theta - 1)^{\frac{1}{2}} / \lambda\right\} \times \exp \left\{2\pi i (ft - x \cos\theta / \lambda)\right\}$$

$$E_{x} = i Z_{0} H_{z} (\cos^{2}\theta - 1)^{\frac{1}{2}}$$

$$E_{y} = Z_{0} H_{z} \cos \theta.$$
(1b)

In such a wave the fields decrease exponentially away from the x axis, and since $\cos \theta > 1$, the phase velocity

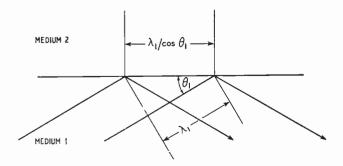


Fig. 2. Reflection at an interface; the wave in medium 2 is a slow wave if λ_1 cos $\theta_1 < \lambda_2$

Electronic & Radio Engineer, September 1959 C

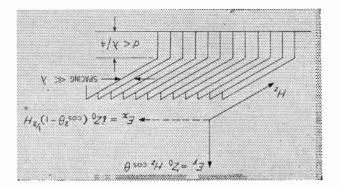


Fig. 3. Inductive corrugated surface

along the x axis is less than v. The x component of electric field is pure imaginary, this means that it is $\pi/2$ out-of-phase with the other fields. Consequently the impedance Z_y is also imaginary, $Z_y = -iZ_0(\cos^2\theta - 1)^{\frac{1}{2}}$. A negative imaginary value denotes that the magnetic field 'leads' the electric field, and hence that the impedance is capacitive. Such a wave is shown diagrammatically in Fig. 1(b).

Waves of this type are known as surface waves, or sometimes as slow waves or inhomogeneous plane waves. They occur, for example, at the surface of a slab of optically-dense material at which total internal reflection is occurring; under these circumstances Snell's law gives a value greater than unity for $\cos \theta$, the angle between the 'refracted' ray in the less dense medium and the surface. Evidently the phase velocity along the interface is less than the velocity of light in the less dense medium (Fig. 2).

Such surface waves may also be produced on corrugated surfaces. A surface structure such as that shown in Fig. 3 is purely inductive, since it appears as a system of short-circuited transmission lines of length less than $\lambda/4$. Provided that the fine structure of the surface can be neglected, its impedance may be matched to that of a capacitive surface wave. The impedance $Z_{(-y)}$ looking into the surface is $iZ_0 \tan 2\pi d/\lambda$ where d is the depth of the slot, and the impedance looking away from the surface into the surface wave Z_y is $-iZ_0$ $(\cos^2\theta - 1)^{\frac{1}{2}}$. Now the condition for a match is that these should be equal numerically but opposite in sign, so that

$$Z_0 \tan 2\pi d/\lambda = Z_0 (\cos^2\theta - 1)^{\frac{1}{2}} \qquad \dots \qquad (3)$$

whence

$$\cos \theta = v/v_x = \sec 2\pi d/\lambda \qquad \dots \qquad \dots \qquad (4)$$

As d increases from 0 to $\lambda/4$, the phase velocity drops from v to zero.

A Spectrum of Plane Waves

So far, only single waves have been considered; some problems however can be very conveniently treated by considering an angular spectrum of plane waves, in which $\cos \theta$ takes all values between $-\infty$ and $+\infty$. As an example, a somewhat idealized solution of the problem of two-dimensional diffraction through an aperture in a screen will be outlined. A more complete and rigorous treatment of this method may be found elsewhere^{3,4}.

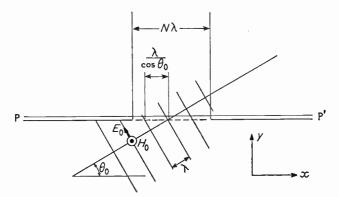


Fig. 4. Diffraction by aperture

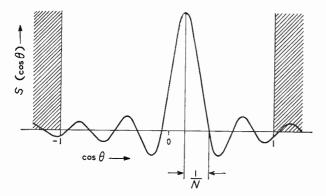


Fig. 5. Spectrum of plane waves through the aperture plane in Fig. 4. The values of $\cos \theta$ in the shaded region correspond to slow waves

The situation to be analysed is shown in Fig. 4. A plane wave in which H is perpendicular to the paper falls on a screen at an angle θ_0 ; there is an aperture of width $N\lambda$ in the screen, and it is required to find the distribution of fields in the space beyond the screen.

Before doing this, the concept of an aperture plane PP' will be introduced. This plane is just beyond the screen (Fig. 4), and divides the space into two halves, one of which contains the source of radiation and the screen, whereas the other is empty. These will be referred to as the 'source region' and 'free region' respectively. The screen will be assumed to be conducting, and edge effects will be neglected. By this we mean that the distribution of electric field in the aperture plane is assumed to be uniform with a phase gradient of $2\pi \cos \theta_0$ radians/wavelength opposite the aperture $(N\lambda/2 > x > - N\lambda/2)$, and zero elsewhere $(x > |N\lambda/2|)$.

By means of the Fourier integral this field may be analysed into a spectrum of fields in the aperture plane each extending from $-\infty$ to $+\infty$, each component of the spectrum being characterized by a particular value of cos θ . This procedure is formally similar to the resolution of a single rectangular pulse into a frequency spectrum. Furthermore each of these component fields may be consistently regarded as belonging to a plane wave travelling into the free half of space at an angle θ from the aperture.

Omitting the term exp. $(-2\pi i ft)$ expressing variation

334

with time (since this is a constant factor throughout) the aperture field may be written :

$$E_x = E_0 \sin \theta_0 \exp(-2\pi i x \cos \theta_0 / \lambda),$$

where $N\lambda/2 > x > - N\lambda/2.$

Denoting the spectrum of fields by $S(\cos \theta)$

$$E_x = \int_{-\infty}^{\infty} S(\cos \theta) \exp((-2\pi i x \cos \theta / \lambda)) d(\cos \theta)$$

whence by the Fourier inversion theorem

$$S(\cos \theta) = \int_{-N\lambda/2}^{N\lambda/2} E_x \exp \left(2\pi i x \cos \theta/\lambda\right) dx/\lambda$$

= $E_0 \sin \theta_0 \sin\{N\pi(\cos \theta - \cos \theta_0)\} \div \pi (\cos \theta - \cos \theta_0) \ldots \ldots \ldots (6)$

Fig. 5 shows the shape of the spectrum; values of $|\cos \theta|$ greater than unity correspond to slow waves travelling along the aperture plane, with amplitude decreasing in a direction measured perpendicular to the plane. It is interesting to note that changing $\cos \theta_0$ merely changes the origin in the figure. It is possible to show that the angular spectrum of waves is identical to the distant 'polar diagram' of the aperture considered as an aerial^{3,4}. This might be expected from the form of Equ. (6), which is that of the well-known polar diagram of a continuous linear array of length $N\lambda$ and phase gradient $2\pi \cos \theta_0$ radians per wavelength⁵.

It is possible to set up a field in which $\cos \theta_0$ is greater than unity in the aperture plane by placing a material of high optical density behind the screen, and making the angle of incidence in this medium (measured to the surface) less than the critical angle. If this is done the 'main beam' at $\theta = \theta_0$ disappears, and only radiation corresponding to the secondary maxima occurs. The importance of this apparently trivial example will be apparent later.

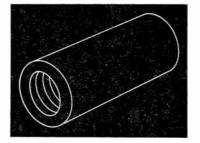
Some Applications to Particle Accelerators

Some characteristics of particle accelerators will now be discussed in the light of concepts so far developed.

Since surface waves have a phase velocity less than that of light, and a field component in the direction of propagation, they are clearly suitable for accelerating particles. For example, the corrugated surface of Fig. 3 could be rolled into a tube about a horizontal line (Fig. 6), and the phase velocity of the wave varied by varying the depth of the corrugations. This is essentially what is done in the travelling-wave electron accelerator⁶. The mathematical representation of the fields looks different, exponentials are replaced by Bessel functions, but the essential physical situation is the same.

Another system worthy of consideration in this

Fig. 6. Corrugated waveguide formed by rolling up the surface of Fig. 3



Electronic & Radio Engineer, September 1959

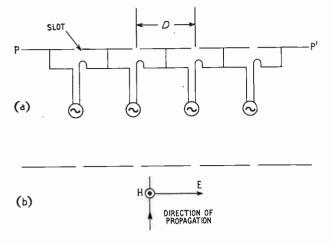


Fig. 7. Array of slots in a conducting metal sheet fed by (a) resonators; (b) a plane wave

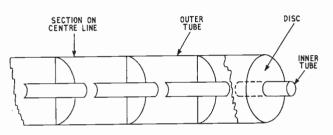


Fig. 8. The slot system of Fig. 9 (a) rolled up to form a standing-wave linear accelerator

connection is that of an infinite array of slots in a metal sheet, fed either by resonators which are in turn fed by generators all in phase, Fig. 7(a), or alternatively by an incident plane wave normal to the sheet, Fig. 7(b). The polar diagram of the radiation from the slots can be found in a manner similar to that used to calculate diffraction through a single aperture. Since, however, the function E_x in the aperture plane is periodic and infinite in extent, the form of the function $S(\cos \theta)$ is that of a 'line spectrum'. Lines will occur at values of $\cos \theta$ given by $\cos \theta = n \lambda / D$, where D is the slot spacing and n may be any integer positive or negative. The envelope of the lines will depend on the slot width, and will be broad if the slots are narrow. There will only be a finite number of lines for which $n \lambda/D$ is less than unity; these will correspond to plane waves travelling away from the aperture at angles $\cos^{-1}(n\lambda/D)$, as in a diffraction grating. For $n\lambda/D$ greater than unity however, there is an infinite set of slow waves travelling in both directions along the aperture plane. (A detailed study of a very similar problem, the reflection of a wave at a grid of wires, has been made by Macfarlane⁷).

If now, as before, the system of Fig. 7(a) is rolled up about a horizontal axis into a small enough tube the radiated waves may be suppressed while the slow waves are retained. The system then becomes virtually a resonant type linear accelerator (Fig. 8). The amplitude of the very slow waves (n large) falls off rapidly with inward radial distance from the walls, so that these

Electronic & Radio Engineer, September 1959

waves do not interact strongly with the particles. An alternative way of interpreting this effect is to say that particles moving at these slow speeds $(vD/n\lambda)$ spend many cycles in the field of each gap, and thus do not receive a large net acceleration. In the notation of klystron theory this is expressed by saying that the gap factor, β , is small.

If the accelerator of Fig. 8 is split into separate resonator units, and the whole rotated about a vertical axis, the type of accelerating system used in synchrotrons is obtained (Fig. 9).

Cylindrical Waves Moving Axially

In the discussion on accelerators, cylindrical waves were introduced. Another form of cylindrical wave which has been studied both theoretically and experimentally may be obtained by effectively turning the corrugated waveguide inside out, and replacing the corrugations (if desired) by a dielectric, so that the system consists of a metal tube or wire surrounded by a cylindrical shell of dielectric⁸. The radial dependence of the field for such a system can be expressed in terms of the Hankel function⁹. At large distances from the wire however the field is indistinguishable from that of a plane wave if observed over small ranges of r and ϕ where r is the distance from the wire and ϕ the angle measured in a plane perpendicular to the wire with the wire at the origin. Furthermore the value of $\cos \theta_0$ (which is greater than unity) associated with the wave is just that given by the velocity of light divided by the velocity of

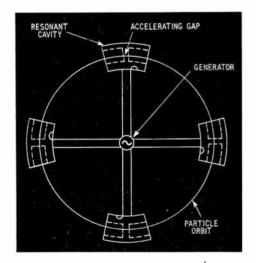


Fig. 9. R.F. system for synchrotron

the wave along the wire, as in the case of the plane wave. This can be verified quite simply by writing down the asymptotic expression for the Hankel function solution, as given for example in reference 9.

In such a guided wave the power flux is of course entirely in a direction parallel to the wire. An alternative way of supporting such a wave would be to use an infinite array of Hertzian dipoles placed end to end, each fed in such a way that the phase gradient along the array is $2\pi \cos \theta_0$ per wavelength. If such a system is used there is no reason why $\cos \theta_0$ should not be less than unity. If this is so, the Hankel function changes its character, and the solution remote from the dipoles becomes a travelling wave, moving outwards at an angle θ_0 to the axis.

The radiation from an array of finite length can be found in an analogous way to the radiation through a finite aperture, by Fourier analysis of the current distribution along the array into a spectrum of current waves each extending all the way along the axis. Analogous to Equ. (6), for an array of length $N\lambda$,

$$S(\cos\theta) = I_0 \sin \{N\pi (\cos\theta - \cos\theta_0)\}/\pi (\cos\theta - \cos\theta_0)$$
...(7)

The angular distribution of radiation, $P(\cos \theta)$, is not, however, given by Equ. 7. It is nevertheless related to it by the expression

$$P(\cos\theta) \propto \sin\theta \cdot S(\cos\theta) \quad \dots \quad (8)$$

Even if $|\cos \theta| > 1$ some radiation occurs when the array is of finite length; this may be compared with diffraction through a finite aperture when $|\cos \theta| > 1$ discussed in the section on 'A Spectrum of Plane Waves'. Of particular interest is the case when $\cos \theta = 1 + 1/2 N.^{10}$

Radiation from an Electron Moving in a Straight Line

The main interest of the previous section is the insight it gives into the problem of radiation from an electron. Fourier analysis has already been used to analyse the current function into components with different spatial periodicities $\cos \theta/\lambda$, but a single temporal periodicity fhas always been assumed. In the radiation problem, however, use is made of Fourier analysis in time also.

An electron or assemblage of electrons moving in a straight line with velocity u may be considered as a current, I = g(ut-x). This may now be Fourier analysed into frequency components of the form exp. $\{2\pi i(ft-fx/u)\}$, so that if h(f) is the distribution of frequencies

$$I(x,t) = \int h(f) \exp\left\{2\pi i \left(ft - x\cos\theta_0/\lambda\right)\right\} df \dots \qquad (9)$$

where
$$\cos \theta_0 = f \lambda / u = v / u$$
 (10)

In free space $\cos \theta_0$ is always greater than unity, and no radiation occurs. In a dielectric medium, however, u can exceed v, and in this case radiation occurs at an angle $\cos^{-1}v/u$. This is Čerenkov radiation¹¹. If wavelengths large compared with the linear dimensions of the electron bunch only are considered, then $g(ut-\delta)$ is proportional to $\sigma(ut-x)$, h(f) then becomes independent of f, and it is readily seen from Equ. (9) that the spectral distribution varies as 1/f. It was stated above that in free space $|\cos \theta_0|$ is always greater than unity, and that no radiation occurs. If, however, the track is of finite length, by analogy with the finite aperture in the section on 'A Spectrum of Plane Waves' $\cos \theta_0$ has to be replaced by a spectrum in which all values of $\cos \theta$ are present, and some radiation does therefore take place. This radiation is normally associated with the acceleration of the charge at the beginning and end of the track. The angular distribution of a single frequency component of the radiation from an ideal point electron in free space which moves with uniform velocity over a finite track of length L is given by Equs. (7) and (8), with $N = L/\lambda$ (λ being the freespace wavelength of the frequency component under

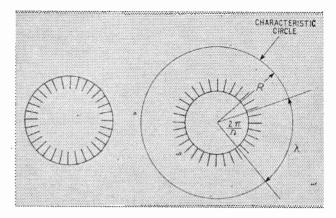


Fig. 10. The corrugated surface of Fig. 3 rolled up about an axis perpendicular to the paper

consideration). If the track of the particle is many wavelengths long, an overall picture of the radiation polar diagram can be obtained by replacing the oscillatory term in the numerator of Equ. (7) by its envelope, Equ. (8) then becomes

 $P(\cos \theta) \propto \sin \theta / \pi (\cos \theta - \cos \theta_0) \dots$ (11) The divergence at $\theta = \theta_0$ is in the region where $\cos \theta > 1$, and is therefore not important.

For a relativistic electron travelling at nearly the speed of light an interesting substitution can be made. If γ is the ratio of the total energy of the electron to its rest energy then for $u \approx c$

$$u/c = (1 - 1/\gamma^2)^{\frac{1}{2}} \approx 1 - 1/2 \gamma^2 \qquad \dots \qquad (12)$$

whence for θ small equation (11) becomes

 $P(\cos \theta) = p(\theta) \propto 2 \theta/\pi (\theta^2 + 1/\gamma^2)$.. (13) It is seen that the radiation is directed more strongly forward as the electron energy increases. The angle at which the maximum emission occurs can readily be shown to be $\theta = 1/\gamma$.

This method of calculating the radiation from an accelerated electron is not, in general, the most useful or convenient; it is, however, sometimes useful for discussing the behaviour of low-frequency components¹².

Cylindrical Waves Moving Circumferentially

In Fig. 3 a plane guiding surface is shown. It is os interest to consider what happens when the surface if curved into a cylinder with its axis perpendicular to the paper. If the surface is rolled up with the corrugations on the inside, a magnetron structure is obtained. The magnetron operates when the magnetic field and applied voltage are adjusted so that the electron cloud moves with an angular velocity equal to that of the slow waves, Fig. 10.

When the corrugations are on the outside, the situation is rather more interesting. If the phase velocity of the wave is u at the surface of the corrugations, it will be equal to v the velocity of light at a radius equal to v/u times the radius of the cylinder. This radius and the associated circle will be called the characteristic radius R and the characteristic circle respectively. If the total change of phase round the cylinder is $2n\pi$, then it may

easily be verified that $R = n \lambda/2\pi$. The solution of the wave equation for this case can be expressed in terms of a Hankel function of the second kind of order $n.^{13}$ Fig. 11 shows the variation of the circumferential component of E for the special case where n = 4. An examination of the form of the solution shows that the wave changes character at the characteristic circle; it varies monotonically outwards to the circle, and is oscillatory outside it. Well inside the characteristic circle the components of E and H are nearly $\pi/2$ out-ofphase, at large distances outside they are in phase. The whole solution is rather like that of a plane wave in which $\cos \theta$ varies with radius r according to the relation $\cos \theta = R/r$. Inside the circle the wave is predominantly an evanescent wave, and outside it is a predominantly travelling wave, so that power gradually leaks away from the corrugated surface into the radiation field. For small values of u or of the surface curvature the characteristic circle is a long way from the surface, and the power leaks out very slowly.

Analogy with Wave Mechanics

The region between the circle and the surface is analogous to a potential barrier in wave mechanics. In the scattering of neutrons by a nucleus for example, partial waves associated with an angular momentum $\{l \ (l + 1)\}^{\frac{1}{2}}$ only interact weakly with a nucleus of radius less than $l\lambda/2\pi$. The reason for this is that such a nucleus lies inside the characteristic sphere and a potential barrier (the centrifugal barrier) has to be crossed in order to reach it. Under these circumstances, the wave function decreases monotonically inwards from the characteristic sphere.

'Super-Gain' Aerials

If two waves of equal amplitude and rotating in opposite directions are present on a cylindrical guiding surface, the angular dependence of the components of the field becomes proportional to exp. $i (2\pi ft - n\phi) +$ exp. $i (2\pi ft + n\phi) = 2 \cos n\phi \exp (2\pi i ft)$. If the system is considered as an aerial, the distant radiation pattern then has the form $p(\phi) \propto \cos n\phi$. A more practical aerial could be made from a slotted cylinder fed by generators; c.f., the system shown in Fig. 7 rolled up about an axis perpendicular to the paper. If the slots are sufficiently close, any arbitrary field distribution round the circumference can ideally be obtained by suitable adjustment of the amplitude and phase of the generators. This field distribution can be written as a Fourier series

$$E_{\phi} = \Sigma E_n \cos n\phi \qquad \dots \qquad \dots \qquad \dots \qquad (14)$$

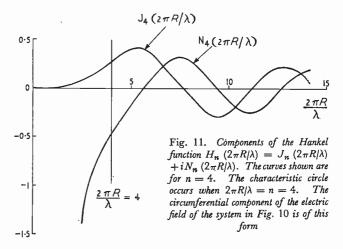
The distant radiation field can similarly be written

$$E'_{\phi} = \Sigma E'_n \cos n\phi \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (15)$$

where E_n'/E_n is a function of the radius r of the aerial. From Equ. (15) it is clear that from an aerial of given size, an angular distribution of any arbitrary shape can be obtained by taking enough terms of Equ. (15) and adjusting the values of E_n accordingly. However, as nis increased beyond a value such that the characteristic circle has a larger radius than that of the aerial $(n>2\pi r/\lambda)$ the value of E_n'/E_n drops very rapidly indeed, due to the presence of the 'potential barrier'¹⁴. In order that an appreciable amount of power can leak out, therefore, the fields E_n (when *n* is greater than $2\pi r/\lambda$) must be extremely large at the radius *r*. These fields are predominantly reactive and represent a considerable amount of stored energy in the neighbourhood of the slots. Thus it is difficult to produce a beam narrower (between zeros) than π/n , where $n = 2\pi r/\lambda$; that is, narrower than $\lambda/2r$. This may be compared with the angle between zeros from a uniformly illuminated aperture of width 2rof $\sin^{-1}\lambda/2r$, or $\lambda/2r$ when $r > > \lambda$. The difficulty of producing a beam substantially narrower than that from a uniformly illuminated plane aperture is well known³.

Radiation from Electrons Moving in a Circle

When electrons move in a circle, power is radiated. This fact is well known to designers of particle accelerators, and is important in the design of large electron synchrotrons. That such radiation will occur can easily be seen by Fourier analysis of the current pulse (due to the electron) as a spectrum of sinusoidal current distributions running round the circle with a phase velocity equal to the electron velocity u. Since u is less than v(the velocity of light), the field due to a component with



wavelength λ will fall off in a direction away from the orbit, being substantially reduced in a distance $\lambda/2\pi$ $(\cos^2\theta - 1)^{\frac{1}{2}}$ where $\cos\theta = v/u > 1$; c.f., the plane wave in Fig. 1 (b). If then the characteristic circle is nearer to the circle on which the electron moves than this, radiation will occur freely, if it is further away, little radiation will occur. A 'cut-off' therefore occurs at a wavelength given by

$$\lambda = \Delta R/2\pi (\cos^2\theta - 1)^{\frac{1}{2}} \qquad \dots \qquad \dots \qquad (16)$$

where ΔR is the radial distance between the two circles; this argument is only valid when the electron velocity is nearly equal to v, so that $\Delta R \ll R$. From geometrical considerations

$$\lambda/2\pi (\cos^2\theta - 1)^{\frac{1}{2}} = \Delta R = R (1 - u/v)$$
 ... (17)

Now from Equ. (12),

 $u/v = \sec \theta \approx 1 - 1/2\gamma^2$

whence Equ. (17) becomes

$$\lambda = \pi R / \gamma^3 \quad \dots \quad \dots \quad \dots \quad (18)$$

This is, therefore, the critical wavelength below which little radiation occurs. A full mathematical treatment of

this problem has been given by Schwinger¹⁵. Because of this cut-off, classical theory is a good approximation unless the circle is so small that its radius is of the same order as the de Broglie wavelength of the electron. Under these conditions, quantum mechanics must be used.

Conclusion

The aim of this article has been to show how a physical understanding of the two forms of plane electromagnetic wave can give insight into a number of wave and radiation phenomena. Although it may appear trivial to some readers, it is hoped that it may be of value to those who think visually rather than in terms of formal relationships.

Acknowledgement

I should like to thank Professor A. L. Cullen for several helpful suggestions and criticisms.

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Super-Gain Aerial Beam

DERIVATION OF A CYLINDRICAL APERTURE DISTRIBUTION

By R. F. Kyle*

SUMMARY. This article describes a method of deducing the distribution of field on a cylinder of any prescribed radius from a given distribution on a cylinder of infinite radius.

Lt has been the dream of designers for some years to produce an aerial with more gain than that obtained from an aperture with uniform illumination and constant phase. It has been demonstrated theoretically that aperture distributions to produce such super-gain aerials exist, but it has also been shown that the difficulties of feeding such an array are great and that the value of Qbecomes very large. For apertures which are a fraction of a wavelength long, some degree of super gain is certainly practicable, as shown in the case of certain television aerials; however, this has not been demonstrated in the case where the aperture length is considerably in excess of one wavelength.

This article develops a method by which the amplitude and phase distribution around a cylinder of arbitrarily small diameter can be deduced from a radiation pattern of given shape. It was suggested by the late Dr. O. Bohm that the simplest theoretical approach to the problem of working back from the radiation pattern to the distribution over an aperture, is to consider the conditions around a closed surface. This eliminates the diffraction methods which are necessary when a line source is considered. A circular cylindrical surface is the simplest case to analyse and an expression for the field on any

radius can be deduced for the required radiation pattern at infinity.

Theory

The horizontal radiation pattern of a circular cylinder whose axis coincides with the z-axis of the co-ordinate system is given by an expression of the form $F(\theta)$. The case considered in this note is where $F(\theta) = \cos^2 m \theta$ and $F(\theta)$ is taken as zero outside the range $\theta = \pm \pi/2m$. This represents a beam with no side-lobes and the voltage beam width is given by $\phi = \pi/2m$. The pattern is assumed to be uniphase.

The above expression can be expanded in the form of a Fourier series.

$$F(\theta) = \sum A_n \cos n \, \theta \qquad \dots \qquad \dots \qquad \dots \qquad (1)$$

where
$$A_n = \frac{\phi}{\pi} \frac{\sin n \phi}{n \phi} \frac{1}{1 - \left(\frac{n \phi}{\pi}\right)^2}$$
 and $\phi = \frac{\pi}{2m}$

Any electromagnetic wave can be represented in cylindrical co-ordinates by

$$\psi = \sum a_n \exp(in\theta) H^{(1)}{}_n \left(r \sqrt{k^2 - h^2} \right) \exp\left(\pm ihz - i\omega t\right)$$
(2)

Electronic & Radio Engineer, September 1959

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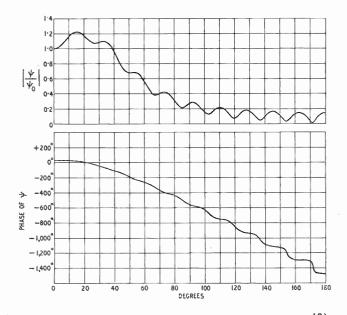


Fig. 1. Variation γf amplitude and phase around cylinder of radius $\frac{i0\lambda}{2\pi}$

This represents a wave travelling outwards¹. If it is assumed that h = 0, then the problem becomes a twodimensional one and the radiation is purely radial. If it is further assumed that the distribution is symmetrical about $\theta = 0$ and the term exp $(-i\omega t)$ is neglected then expression (2) reduces to

$$\psi = \sum a_n \cos n\theta \ H_n^{(1)} (kr) \qquad \dots \qquad (3)$$

where $k = \frac{2\pi}{\lambda}$

It now remains to determine the coefficients a_n by identifying the expression (3) for large values of r with the assumed radiation pattern.

The asymptotic expression for $H_n^{(1)}(kr)$ is

$$H_n^{(1)}(kr) = \sqrt{\frac{2}{\pi kr}} \exp(ikr) \exp\left[-\frac{2n+1}{4}\frac{\pi i}{4}\right]$$

As it is only the variation with θ which is considered in the expression for the radiation pattern the terms in r and the constants which do not vary with the terms of the series can be neglected.

$$\therefore H_n^{(1)}(kr) = \left[\sqrt{\frac{2}{\pi kr}} \exp(ikr) \exp\left(-\frac{\pi i}{4}\right)\right] \exp\left(-\frac{n\pi i}{2}\right)$$

From this we get $a_n \exp\left(-\frac{n\pi i}{2}\right) = A_n$ $\therefore a_n = i^n A_n$ Therefore for any value of $r, \psi = \sum i^n A_n \cos n\theta H_n^{(1)}(kr)$

Particular Case

If the particular case of m = 5 is taken in the above expressions the half-voltage beam width is 18°. The Fourier series is an infinite one but if it is terminated at the 11th term it is found that, instead of a main beam with no sidelobes, there are sidelobes approximately 19 dB down from the main beam and that the main beam is widened by about 5°.

It is obvious by considering this Fourier series that, in general, small changes of a few per cent in the amplitude

Electronic & Radio Engineer, September 1959

of one mode on the finite cylindrical surface will change the radiation pattern by a negligible amount.

The expression for the field amplitude and phase derived above have been computed around cylinders of circumference 10λ and 5λ , for the particular case m = 5 and n = 0 to 10; these are shown in Figs. 1 and 2. It is clear from these curves that the variations of amplitude which have to be set up around the smaller cylinder are extremely rapid and violent. The phase variation is steeper on the smaller cylinder.

Impedance Considerations

If the case of a transverse magnetic field is considered and, as before, only the purely two-dimensional problem is taken, then there are two impedances in the directions of the transverse axes which can be defined.

$$Z_r = -\frac{E_z}{H_{\theta}} \text{ and } Z_{\theta} = \frac{E_z}{H_r}$$

where $E_z = k^2 \psi$; $H_r = -\frac{ik^2}{\omega \mu} \frac{1}{r} \frac{\delta \psi}{\delta \theta}$; and $H_{\theta} = \frac{ik^2}{\omega \mu} \frac{\delta \psi}{\delta r}$

Hence
$$Z_{\theta} = \frac{\omega\mu}{n} r$$
, $Z_r = \frac{i\omega\mu}{k} H_n^{(1)}(\rho) / \frac{\delta}{\delta\rho} H_n^{(1)}(\rho)$
= $iZ_0 H_n^{(1)}(\rho) / \frac{\delta}{\delta\rho} H_n^{(1)}(\rho)$

It is the radial impedance Z_r which is of practical significance and when

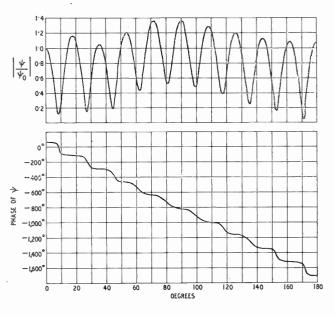
$$r \to \infty, H_n^{(1)}(\rho) \Big/ \frac{\delta}{\delta \rho} H_n^{(1)}(\rho) \to \frac{1}{i}$$

Hence $Z_r \rightarrow Z_0$

The values of Z_r for the separate modes on cylinders of circumference 10λ and 5λ are shown in Fig. 3. The most significant aspect of these graphs is that the resistive component drops to very low values for the higher modes on the smaller cylinder.

An estimate of the frequency sensitivity of the

Fig. 2. Variation of amplitude and phase around cylinder of radius $\frac{5\lambda}{2\pi}$



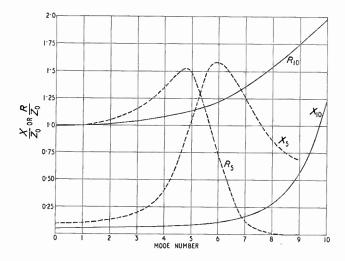


Fig. 3. Resistance and reactance of cylindrical modes

impedance has been calculated as being an alternative to the calculation of the Q and, as is to be expected, the variation is most for the higher modes. The percentage changes of resistance and reactance for a 1% change of frequency are given in Table 1.

TABLE 1

 Percentage Change of Resistance and Reactance of the Individual Modes for a 1% Frequency Variation.
 (A) Cylinder of Radius 10λ/2.

		2π
	$\frac{\Delta R}{R} \times \frac{100}{\%}$	$rac{\Delta X}{X} imes rac{100}{\%}$
Z ₀ Z ₁ Z ₂ Z ₃ Z ₄ Z ₅ Z ₆ Z ₇ Z ₈ Z ₉ Z ₁₀	Zero - 0.0003 - 0.03 - 0.083 - 0.16 - 0.28 - 0.46 - 0.70 - 1.02 - 1.13 + 0.77	$ \begin{array}{r} -1.0 \\ -1.01 \\ -1.12 \\ -1.33 \\ -1.65 \\ -2.12 \\ -2.82 \\ -3.80 \\ -5.17 \\ -6.78 \\ -7.01 \\ \end{array} $

	$\frac{\Delta R}{R} \times \frac{100}{\%}$	$\frac{\Delta X}{X} \times \frac{100}{\%}$
Z ₀ Z ₁ Z ₂ Z ₃ Z ₄ Z ₆ Z ₇ Z ₈ Z ₉ Z ₁₀	Zero 0.008 0.1 0.29 0.45 0.9 8.0 13.2 15.5 17.9 20.3	$ \begin{array}{r} - & 0.9 \\ - & 1.3 \\ - & 1.5 \\ - & 2.4 \\ - & 3.6 \\ - & 4.0 \\ 0.44 \\ 2.5 \\ 2 \\ 1.6 \\ 1.4 \end{array} $

(B) Cylinder of Radius $\frac{5\lambda}{2\pi}$

Conclusions—Further Problems

The problem of relating the properties of the individual dipoles or sources to the overall field round the cylinder has not been resolved. It is considered that any system of sources will be backed by a metal cylinder and the modifications which this produces in the field remain to be calculated, as does also the effect of considering a finite source system in place of the field independent of the z direction.

Acknowledgement

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STEPPING TRANSISTOR

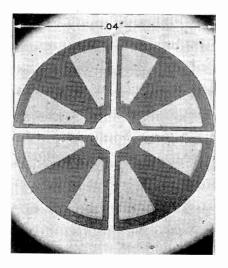
The development of a p-n-p-n semiconductor element that can serve as the basic building block of a silicon stepping transistor was recently announced by Bell Telephone Laboratories, U.S.A.

The four-terminal device acts as a pulse-controlled on/off switch and may be used as a basic stage in building certain logic circuits in digital computers. By using one element to drive two others, versatile decoders can be made.

A more complex device, which is fabricated from a single piece of silicon, can also perform the logic functions. An experimental prototype stepping transistor with four stages has been made.

The original object of the development was to produce a semiconductor device that would function in a similar way to a gas stepping tube (such as a Dekatron). The gas stepping tube utilizes the bistable voltage-current characteristic of a gas discharge for its operation. Unidirectional transfer of voltage between one anode and several cathodes is obtained by the non-symmetrical geometry of its construction.

The stepping transistor uses a p-n-p-n transistor as the bistable element. The design of the structure results in a bistable voltage-



A four-stage stepping transistor fabricated on a single piece of silicon.

current characteristic between a single common electrode and a set of multiple electrodes. Non-symmetrical geometry is employed to obtain a uni-directional transfer of voltage. Also, unlike the gas stepping tube, close proximity is not basically required in the stepping transistor.

The current level at which these devices are operated can be designed within the range 1 to 100 mA with supply voltages of 10 to 100 V.

Experimental models have been operated at speeds up to 10^{6} pulses per second and it is expected that, with improved designs, they will operate even faster.

ITS MEASUREMENT AND IMPLICATIONS

By L. G. Cripps, B.A.*

SUMMARY. The frequency at which the earthed-emitter short-circuit current gain has fallen to unity is a parameter of use in defining high-frequency characteristics of transistors. In this article the idea is discussed and the significance of the parameter explained. A method of measurement of use up to frequencies of the order of 200 Mc/s is also given. It is concluded that the parameter is sufficiently important for it to replace, at least partially, the alpha cut-off frequency, as a means of specifying the frequency performance of a transistor.

parameter which gives a qualitative idea of the high-frequency performance of a junction transistor (Fig. 1) is the frequency at which $|\alpha'| = 1$. It has not been widely used in the past since its connection with equivalent circuit parameters and other characteristics has not been well understood. The purpose of the present article is to discuss its more precise use as a means for obtaining quantitative results, in the way that the alpha cut-off frequency has been used in the past. The relations between the new parameter and quantities such as the alpha cut-off frequency are first considered, and a brief explanation is given of the effects of emitter depletion-layer capacitance. A method of measurement, alternative to one discussed by Pritchard¹ is also described. Certain of the results are shown to be virtually independent of any (constant) drift field which may be present in the base region of the transistor. Two papers have appeared recently which are related to the present article. Thomas and Moll² have given a general discussion of transistor current gain, and certain of their results are in accord with the ideas presented below. Appendix II of the paper by Thornton and Angell³ compares a quantity f_T (almost identical with f_1) with the alpha cut-off frequency.

Before proceeding with the main discussion it is convenient to prove a basic theorem, remarkable for its simplicity and for the fact that it does not seem to be very widely known. If we assume the internal alpha of a transistor to be represented by

 $\alpha = a - jb$, ... (1) where a and b are both real, then the quantity $\alpha' (= \alpha/(1 - \alpha))$ will be given by

$$x' = \frac{a - ib}{(1 - a) + jb}$$

If we then consider the particular condition

$$a = 1/2$$
 \cdots \cdots \cdots \cdots \cdots \cdots $(2$

$$\alpha' = \frac{1/2 - jb}{1/2 + jb}$$
 so that $|\alpha'| = 1$. (3)

Thus (2) and (3) are equivalent conditions, and we * Mullard Research Laboratories.

Electronic & Radio Engineer, September 1959

may assert the theorem : the frequency at which $|\alpha'| = 1$ is identical with the frequency at which $\operatorname{Re}(\alpha) = 1/2$.

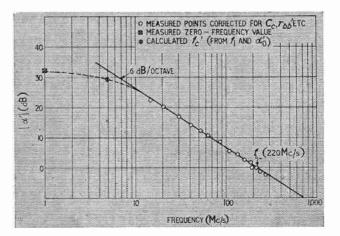
It should be noted that this result is quite general, and will apply to any device for which the quantities α and α' may be defined. It is independent of the form of the functions representing the behaviour of *a* and *b* with frequency, and is also independent of the lowfrequency value of alpha (α_0). It will thus hold for the alpha of a transistor with a 'built-in' drift field, whatever the characteristics of that field.

The Parameter f₁

We define $f_1 (= \omega_1/2\pi)$ to be the frequency at which the real part of the internal alpha of the transistor has fallen to 6 dB below its low-frequency value: $\operatorname{Re}(\alpha)/\alpha_0 = 1/2$. By the theorem just proved, f_1 is almost, but not quite, the frequency at which $|\alpha'| = 1$ (since α_0 is normally close to unity) and, for many practical purposes, the two frequencies may be taken to be the same; a discussion of the relation between them is given in the section describing the measurement of f_1 .

It should be noted that by 'internal alpha' in the above definition is meant the alpha for the base trans-

Fig. 1. Measured curve of $|\alpha'|$ against frequency for an experimental transistor



mission process, after the effects of parasitic elements such as collector capacitance and series resistance, base resistance, etc., have been removed.

In the following, we shall consider the relation between f_1 and the earthed-base and earthedemitter cut-off frequencies, and the capacitance $C_{b'e}$ in

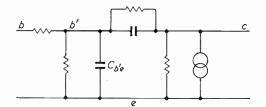


Fig. 2. Earthed-emitter hybrid- π equivalent circuit for alloy junction transistors

the earthed-emitter hybrid- π equivalent circuit circuit (Fig. 2). Stephenson⁴ has related f_1 to physical rather than electrical quantities in a paper concerned with the effect of d.c. collector voltage. te Winkel⁵ has given a more complete discussion of the equivalent circuit of a drift transistor using f_1 .

It has been shown⁶ that the following expression is a good approximation for the alpha of a transistor with no drift field:

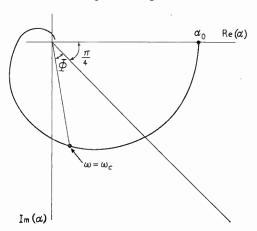
$$\alpha = \frac{\alpha_0 \exp\left(-j \, \Phi f | f_c\right)}{1 + j f | f_c} \qquad \dots \qquad \dots \qquad (4)$$

Here Φ is the phase angle (in radians) at the cut-off frequency $f = f_c$, referred to the radius $\theta = -\pi/4$ (Fig. 3). It has a value $\Phi = 0.22$.

te Winkel⁵ has shown that Equ. (4) is also a good approximation if a uniform drift field is present, provided an appropriate value of Φ is employed [see his equation (25) loc. cit.]. The range of validity of the equation is approximately $0 \leq f \leq 2f_1$, and Φ takes values $0.22 \leq \Phi \leq 1$.

From Equ. (4) it is possible to obtain the relation between f_1 and f_c , for various values of Φ . If this is done it is found that, to a good approximation,

 $f_1 = f_c (1 + \Phi)$ (5) Equation (5) can also be inferred from te Winkel's⁵





analysis, and the degree of approximation estimated. Calculation of the behaviour of α' from expression (4) for alpha gives

$$\alpha' = \frac{\alpha_0'}{1 + j \frac{f}{f_c} \cdot (1 + \Phi) (1 + \alpha_0')} \qquad \dots \qquad \dots \qquad (6)$$

where

$$x_0' = \frac{\alpha_0}{1 - \alpha_0}$$

The derivation of this equation has been given by te Winkel, together with an indication of its range of validity. Crudely, it breaks down at frequencies of the order of f_1 .

Two important results emerge. First, α' follows the simple law, implying that $|\alpha'|$ falls with increasing frequency at a rate asymptotically approaching 6 dB per octave, whatever the value of drift field. Experimental confirmation of this fact is given in Fig. 1. Secondly, the 3-dB down point is seen from Equ. (6) to occur when $f/f_c (1 + \Phi) (1 + \alpha_0') = 1$, so that, with $f = f_c'$ at this point, we have, firstly

$$f_c' = \frac{f_c}{1 + \alpha_0'} \cdot \frac{1}{1 + \Phi} \qquad \dots \qquad \dots \qquad (7)$$

and secondly, using (5),

$$f_{c}' = \frac{f_1}{1 + \alpha_0'}$$
 ... (8)

in which the unpleasant quantity $(1 + \Phi)$ has been removed. The value of f_c' calculated according to Equ. (8) is shown on the experimental curve of Fig. 1.

For alloy transistors it is well known that neglecting emitter depletion-layer capacitance, the capacitance $C_{b'e}$ (see Fig. 2) is given by

$$C_{b'e} = 1 \cdot 21/\omega_c r_e \qquad \dots \qquad \dots \qquad \dots \qquad (9)$$

If a uniform drift field is present, this expression becomes

 $C_{b'e} = (1 + \Phi)/\omega_c r_e$... so that, using (5) we may write

.. (10)

and again the quantity $(1 + \Phi)$ has been removed. If there is appreciable emitter depletion-layer capacitance, this expression must be modified to

$$C_{b'e} = C_{ed} + 1/\omega_1 r_e \qquad \dots \qquad \dots \qquad (12)$$

where ω_1 is an 'internal' quantity which differs from the measured value due to the presence of C_{ed} . An indication of the effect of C_{ed} on the measured f_1 may be obtained by the following heuristic argument. We may equate the actual $C_{b'e}$ to that which would be calculated from a measurement:

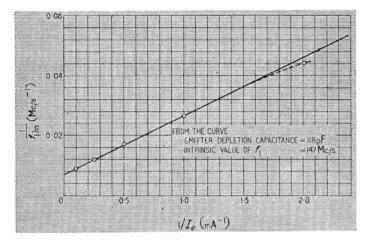
$$1/\omega_{1m}r_e = C_{ed} + 1/\omega_1r_e \qquad \dots \qquad \dots \qquad (13)$$

Writing $r_e = kT/qI_e$

we have

$$1/\omega_{1m} = 1/\omega_1 + (C_{ed} k T/q) (1/I_e) \dots \dots \dots (14)$$

Thus a graph of $1/\omega_{1m}$ against $1/I_e$ should be a straight line of intercept $1/\omega_1$ and slope $C_{ed} kT/q$. An experimental curve is shown in Fig. 4, which indicates that Equ. (14) is at least of the correct form. From the curve, values of f_1 and C_{ed} were deduced.



Measurement of f₁

The quantity actually measured by the apparatus to be described is the frequency at which the modulus of the earthed-emitter current gain falls to unity. Correction for the effects of collector capacitance, base resistance and the external measuring circuit must be applied to the result to obtain the corresponding quantity for the 'intrinsic' transistor; that is, for the base transmission process. The corrected quantity then corresponds to the true value for $|\alpha'| = 1$, and therefore, for $\operatorname{Re}(\alpha) = 1/2$, by the basic theorem proved To obtain f_1 , for which by definition earlier. $\operatorname{Re}(\alpha) = \alpha_0/2$, a second correction is necessary. The two corrections are discussed in detail in the Appendix. They correspond to similar corrections when measuring f_c by methods which yield the frequency at which $|\alpha| = 1/\sqrt{2}$ rather than $|\alpha| = \alpha_0/\sqrt{2}$.

The basis of the method is shown in Fig. 5. A signal is fed to the emitter, and the voltages V_1 and V_2 developed across two small and equal resistors R_1 and R_2 included in series with the base and collector are observed by a single voltmeter which is connected alternately across the two resistors. The frequency of the generator is adjusted until the voltages V_1 and V_2 are equal in magnitude. Since $R_1 = R_2$, the generator setting corresponds to the frequency at which $|i_c| = |i_b|$. This measured frequency will be called f_{1m} .

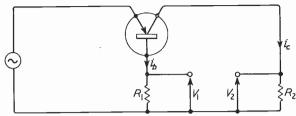
The method has the advantage of being independent of the calibration accuracy of the voltmeter and is, in principle, capable of operation up to very high frequencies, provided the reactive parts of the impedance of R_1 and R_2 are balanced and are not too large. An amplitude-modulated signal generator may be employed, so that a wide-band voltmeter can be obtained by using a diode detector followed by amplification at the modulation frequency. Non-linearity of the detector at low levels is unimportant.

It should be noted that the equipment easily lends itself to the measurement of $|\alpha'|$ at frequencies other than f_1 , so that a curve of $|\alpha'|$ against frequency may be obtained. The procedure is as follows. The detector is connected across R_1 and the voltage V_1 observed. The detector is then transferred to R_2 and the input signal attenuated until the observed voltage V_2 is the same as the voltage V_1 observed in the first

Electronic & Radio Engineer, September 1959

Fig. 4. Measured curve of $1|f_{1m}$ against $1|I_e$ for an experimental transistor

[Fig. 5. Basic method of measuring f_1



position. The change of attenuator reading is then $|\alpha'|$. The curve of Fig. 1 was obtained by this technique.

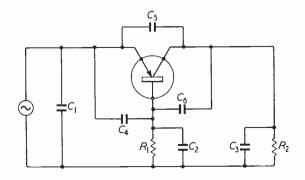
Before considering the detailed circuit, a number of factors affecting accuracy will be considered.

The requirements for the generator are twofold. First, its frequency calibration must clearly be accurate or should be checked against a standard. Secondly, the output waveform should be pure. This factor may be easily overlooked in this type of measurement, but results can be nullified if harmonics or audio frequency are presented, since the transistor will behave differently for these frequencies and for the fundamental.

As in all measurements of this type, the signal level employed must be small enough for transistor non-linear effects to be negligible. This condition can be achieved by reducing the signal level until no change of answer is obtained.

Ultimate accuracy depends upon the ease with which a small difference between the two signals V_1 and V_2 (Fig. 5) can be detected. Thus the detector used for these voltages must have good noise performance or the difference will be lost. Since the resistors R_1 and R_2 are only of the order of 10 Ω and therefore develop only small voltages, high sensitivity is also important. A receiver would be an obvious choice for the detector, but has the severe disadvantage of requiring retuning each time the generator frequency is adjusted. However, sufficiently good performance can normally be combined with the advantage of wide-band detection, by using

Fig. 6. Stray capacitances



a modulated signal, as described above, provided the amplifier following the detector is narrow-band.

The behaviour of the two measuring resistors R_1 and R_2 is of importance. It is easy to satisfy the condition $R_1 = R_2$ at low frequencies (to an accuracy of 1 part in 1000, say), and the use of high-stability resistors ensures a reasonable permanence of the equality (occasional checking of the resistors is, of course, desirable). However, stray components become important at high frequencies and, since the resistances are low, series inductance becomes important at a much lower frequency than shunt capacitance. By using similar and similarly-arranged resistors the inductive effects of the loops associated with the resistors may be approximately balanced. Minor adjustment at high frequencies to the loops then allows a more accurate balance to be obtained. This may be done, with no transistor in circuit, by connecting a suitable impedance alternately between emitter and base terminals, and then emitter and collector terminals, and adjusting for equality of V_1 and V_2 .

The stray capacitances in the circuit are shown in Fig. 6. C_1 may be neglected completely since it will not normally be high enough to limit the generator output. As explained above, C_2 and C_3 only become important at frequencies outside the range of the apparatus since the series inductance of R_1 and R_2 predominates. C_4 , C_5 and C_6 must be made small by screening the circuits associated with the three transistor terminals from each other.

Finally, there are the corrections which must be applied to the measured frequency to allow for the effects of resistors, and for the fact that $\alpha_0 \neq 1$. The derivation of the correction formula is given in the Appendix, the result being

$$f_1 = f_{1m} \left[1 + \omega C_c (r_{bb'} + R_1 + R_2) + \frac{2}{\alpha_0'} \right] \quad \dots \quad (15)$$

This correction formula is based on a simple equivalent circuit and the assumption that the correction is small. It may be necessary under some circumstances to use a more exact expression.

Complete Measuring Circuit

The complete circuit is shown in Fig. 7 and will operate over the range 5-200 Mc/s. The signal is fed to the emitter via a d.c. blocking capacitor (1000 pF) and the emitter supply is connected via a decoupling circuit (1.5 k Ω , 1000 pF, 1.5 k Ω). A path for the base direct current is provided by a $1.5-k\Omega$ resistor, across which the 10 Ω measuring resistor is connected by a 1000-pF capacitor; a.c. coupling is used to avoid applying d.c. to the detector. A similar arrangement is used for the measuring circuit (1000 pF and 10 Ω) at the collector, and the collector d.c. supply is connected through a decoupling network (1.5 k Ω , 1000 pF, 1.5 k Ω) similar to that at the emitter. The 1.5-k Ω resistor in the base, and the 1.5-k Ω resistor in the collector decoupling network shunt the measuring resistors, but the shunting is small (less than 1%) and in any case the two effects almost cancel. The coupling capacities (1000 pF) to the 10 Ω measuring resistors are almost certainly inductive at the high-frequency

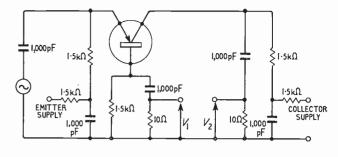


Fig. 7. Complete circuit of apparatus for measuring f_1 over the range 5-200 Mc/s

end of the range, but their impedance will still be low and the effect small. Accuracy of measurement is probably better than 2% over most of the range [provided the correction formula (15) is applied] but the errors may rise slightly above, say, 180 Mc/s. The inductances associated with the two measuring resistors are balanced at 220 Mc/s and the balance then holds over the entire range of the apparatus. The curve of Fig. 1 was obtained using the apparatus described. It should be noted that the application of the correction formula (15) changed the observed value of f_1 for the particular transistor used by about 10%, and altered the slope of the curve from 6.4 dB/octave to 6.0 dB/octave.

Conclusions

The two conditions $|\alpha'| = 1$ and $\operatorname{Re}(\alpha) = 1/2$ are equivalent, and the equivalence is independent of the behaviour of alpha. The result is thus independent of any drift field which may be present. The frequency at which these conditions are satisfied may be called f_{1m} .

A more convenient parameter for analysis is f_1 , which is the frequency for $\operatorname{Re}(\alpha) = \alpha_0/2$. It may easily be obtained from f_{1m} [for which $\operatorname{Re}(\alpha) = 1/2$] by applying a small correction. f_1 is related to wellknown parameters by the expressions

$$f_1 = f_c/(1 + \Phi)$$

$$f_1 = f_c'(1 + \alpha_0')$$

$$C_{b'e} = 1/\omega_1 r_e$$

Emitter depletion capacitance may be related to $C_{b'e}$ and ω_1 by the expression

 $C_{b'e} = C_{ed} + 1/\omega_1 r_e,$

which leads to a simple means of measuring C_{ed} .

Measurement of f_1 may be easily carried out, to an accuracy of about 2%, up to frequencies of the order of 200 Mc/s.

The conclusion from the work described here is that f_1 is a more attractive parameter than f_c for many purposes, in that it is convenient to measure, and has more direct application to equivalent circuits. It is therefore desirable that f_1 should replace, or at least supplement, f_c wherever possible.

Acknowledgements

The author is indebted to several of his colleagues for suggestions and assistance. In particular, Mr. L. P. Morgan first suggested the basic method of measuring f_1 ; Mr. J. B. Rodgers designed, constructed and checked the measuring equipment; Mr. M. J. Gay carried out the original calculations of errors in roduced by C_c , $r_{bb'}$, and external resistors; and Mr. W. L. Stephenson pointed out the method of estimating ω_1 and C_{ed} from measurements at various currents. The author also wishes to thank the Directors of Mullard Ltd., and the Director of the Mullard Research Laboratories for permission to publish this paper.

APPENDIX

Calculation of a Correction Formula for the Effects of C_c , r_{bb}' , Measuring Resistors, and α_0 .

The analysis will be carried out in two parts, the effect of α_0 being treated separately from the remaining effects.

Assuming the equivalent circuit of Fig. 8, in which the section enclosed by a dotted line represents the transistor and writing $1/j\omega C_c = -jX_c$, then we have

 $I_b [r_{bb'} + R_1] = [I_c (1 - \alpha) - \alpha I_b] [-jX_c] + I_cR_2$

If suffix m is used to denote a measured quantity we thus have, after rearrangement,

$$\begin{aligned} |\alpha'|_{m} &= \left| \frac{I_{c}}{I_{b}} \right| = \frac{|r_{bb}' + R_{1} - j \alpha X_{c}|}{|R_{2} - j X_{c} (1 - \alpha)|} \dots \dots \dots (16) \end{aligned}$$

With $\alpha = a - jb_{a}'$ this becomes
$$|\alpha'|_{m} = \frac{|\omega C_{c} (r_{bb} + R_{1}) - ja - b|}{|\omega C_{c} R_{2} - j (1 - a) + b|}$$

$$= \sqrt{\frac{\omega^2 C_c^2 (r_{bb'} + R_1)^2 + b^2 - 2b \ \omega \ C_c (r_{bb'} + R_1) + a^2}{\omega^2 C_c^2 (R_2^2 + b^2 + 2b \ \omega \ C_c \ R_2 + (1-a)^2}}$$

The true value is given by

$$|\alpha'| = \left|\frac{\alpha}{1-\alpha}\right| = \left|\frac{a-jb}{1-a+jb}\right| = \sqrt{\frac{a^2+b^2}{(1-a)^2+b^2}}$$

Hence

$$\frac{\left|\frac{\alpha'}{\alpha'}\right|_{m}}{\left|\frac{\alpha'}{\alpha'}\right|} = \sqrt{\frac{1 - \frac{2b}{a^{2} + b^{2}} \cdot \omega C_{c} (r_{bb}' + R_{1}) + \frac{\omega^{2} C_{c} (r_{bb}' + R_{1})^{2}}{a^{2} + b^{2}}}{1 + \frac{2b}{(1 - a)^{2} + b^{2}} \cdot \omega C_{c} R_{2} + \frac{\omega^{2} C_{c}^{2} R_{2}^{2}}{(1 - a)^{2} + b^{2}}}}$$

We now assume that the effect of C_c etc. is small so that $\omega \ C_c \ (r_{bb'} + R_1) \ll 1$

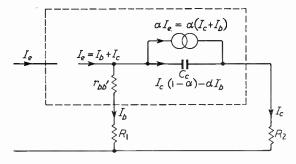
 $\omega C_c R_2 \ll 1$

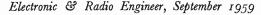
Expanding by the binominal theorem and neglecting second-order terms we have

$$\frac{|\alpha'|_m}{|\alpha'|} \simeq \left[1 - \frac{b}{a^2 + b^2} \cdot \omega C_c (r_{bb}' + R_1)\right] \left[1 - \frac{b}{(1 - a)^2 + b^2} \omega C_c R_2\right]$$
$$\simeq 1 - b \,\omega C_c \left[\frac{r_{bb}' + R_1}{a^2 + b^2} + \frac{R_2}{(1 - a)^2 + b^2}\right]$$

To obtain a true correction factor it is necessary to know the values of both a and b. We know a is of the order of 0.5 and it is a reasonable approximation to take the same value for b. Thus we assume a = b = 0.5

Fig. 8. Circuit for analysis of effect of C_c, r_{bb}' and external resistors





so that

$$\begin{aligned} \frac{|\alpha'|_m}{|\alpha'|} &\simeq 1 - \omega \ C_c \ (r_{bb}' + R_1 + R_2) \\ \text{or} \quad |\alpha'| &\simeq |\alpha'|_m \ [1 + \omega \ C_c \ (r_{bb}' + R_1 + R_2)] \\ &= 1 + \omega \ C_c \ (r_{bb}' + R_1 + R_2) \qquad \dots \qquad \dots \qquad (17) \\ \text{f} \quad |\alpha'|_m &= 1 \end{aligned}$$

Taking the approximation

$$\alpha' = \frac{\alpha_0}{1 + j f_i f_c'}$$

then $|\alpha'| = \frac{1}{\sqrt{1 + (f/f_c')^2}}$

At frequencies of the order of f_1 , we have $f_!f_c' \gg 1$. Hence, $|\alpha'| \simeq \alpha_0'f_c'/f$

so that

$$\frac{d\left[\alpha'\right]}{df} = -\alpha_0' f_c'/f^2 = -\left|\alpha'\right|/f.$$

Thus, since

$$\Delta |\alpha'| = \frac{d |\alpha'|}{df} \Delta f$$

we have

$$\frac{\Delta |\alpha'|}{|\alpha'|} = -\frac{\Delta f}{f}$$

Thus if $|\alpha'|$ is measured to be x% too high, the frequency is x% too low. Hence, using Equ. (17), the correction formula is

$$f_1 = f_{1m} \left[1 + \omega C_c \left(r_{bb'} + R_1 + R_2 \right) \right] \qquad \dots \qquad \dots \qquad (18)$$

A more accurate result requires a knowledge of a and b so that a bridge or other method of measurement is necessary enabling the real and imaginary parts of α to be found.

The effect of α_0 may be calculated as follows. Provided α_0 is not too different from unity, only a small correction is necessary to obtain the true value of f_1 . Thus, an approximate expression for α is justified:

0 0

$$\alpha = \frac{\alpha_0}{1+jf_c} \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (19)$$

Then Re(
$$\alpha$$
) = $\frac{\alpha_0}{1 + (f/f_c)^2}$
Hence
 $d \operatorname{Re}(\alpha) \qquad \alpha_0$

$$\frac{\frac{d}{df}}{\frac{d}{f}} = -\frac{\frac{\alpha_0}{[1+(f/f_c)^2]^2} \cdot \frac{2f}{f_c^2}}{\frac{Re(\alpha)}{1+(f/f_c)^2} \cdot \frac{2f}{f_c^2}}$$

Now

$$\Delta \operatorname{Re}(\alpha) = \frac{d\operatorname{Re}(\alpha)}{df} \cdot \Delta f$$

Thus

$$\frac{\Delta \operatorname{Re}(\alpha)}{\operatorname{Re}(\alpha)} = -\frac{\Delta f}{f} \cdot \frac{2(f/f_c)^2}{1 + (f/f_c)^2}$$
$$= -\frac{\Delta f}{f} \cdot \frac{2\left[\frac{f}{f_1(1+\Phi)}\right]^2}{1 + \left[\frac{f}{f_1(1+\Phi)}\right]^2}$$

Thus, at $f = f_1$

$$\frac{\Delta \operatorname{Re}(\alpha)}{\operatorname{Re}(\alpha)} = -\frac{\Delta f}{f} \cdot \frac{2\left[\frac{1}{1+\phi}\right]^{2}}{1+\left[\frac{1}{1+\phi}\right]^{2}}$$

If
$$\Phi = 0.2$$
,
 $\frac{\Delta \operatorname{Re}(\alpha)}{\operatorname{Re}(\alpha)} = -\frac{\Delta f}{f} \cdot 0.82$
If $\Delta = 1.0$
 $\frac{\Delta \operatorname{Re}(\alpha)}{\operatorname{Re}(\alpha)} = -\frac{\Delta f}{f} \cdot 0.40$

Thus a reasonable compromise, approximately valid for all values of Φ , would appear to be

$$\frac{\Delta \operatorname{Re}(\alpha)}{\operatorname{Re}(\alpha)} = -\frac{\Delta f}{f} \cdot \frac{1}{2} \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (20)$$

[Of course, if the value of Φ is known, a more accurate figure can be taken, but there would be little point in doing this since the initial equation (19) is not accurate in any case.]

Equ. (20) means that a small change x% in $\operatorname{Re}(\alpha)$ corresponds to a change (-2x)% in frequency. The percentage change in $\operatorname{Re}(\alpha)$ in passing from the measured point $\operatorname{Re}(\alpha) = 1/2$ to the required point $\operatorname{Re}(\alpha) = \alpha_0/2$ is a decrease of $(1 - \alpha_0) \times 100\%$. Thus the change in frequency, by Equ. (20), is an increase of $2(1 - \alpha_0) \times 100\%$. Thus the correction formula is

$$f_{1} = f_{1m} \left[1 + 2(1 - \alpha_{0}) \right]$$

$$\simeq f_{1m} \left[1 + \frac{2}{\alpha_{0'}} \right] \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (21)$$

The approximation breaks down at high values of Φ since Equ. (19) is then no longer valid. However, since the correction is small, Equ. (21) may be sufficiently accurate for most purposes. Combining Equs (18) and (21), neglecting second-order corrections, gives

$$f_1 = f_{1m} \left[1 + \omega C_c (r_{bb'} + R_1 + R_2) + \frac{2}{\alpha_{0'}} \right] \quad .. \quad (22)$$

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Hydrogen-Oxygen Fuel Cell

For over one hundred years, engineers and scientists have been endeavouring to produce a practical fuel cell. First envisaged in the early part of the nineteenth century by Sir William Grove, a form of fuel cell was produced by the end of that century, but lack of materials and technology prevented its further development.

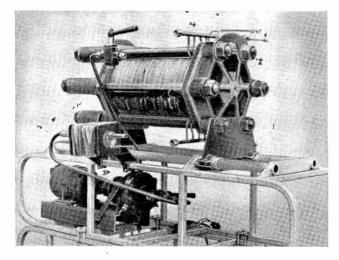
Now, a team working in Cambridge under the sponsorship of the National Research and Development Corporation and led by F. T. Bacon, M.A., A.M.I.Mech.E., has produced a cell capable of delivering an output of 5 kW at 24 V.

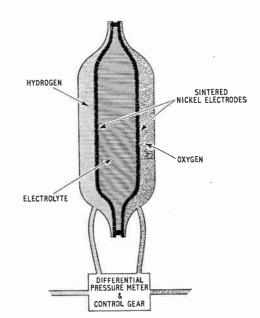
A 'Fuel Cell' is an electro-chemical device in which the free energy of combustion of a fuel is converted directly into electrical energy. It operates by a simple reversal of the process of electrolysis of water.

The one now produced consists of 40 cells, 10 in. diameter and approximately 30 in. long; each cell consists of two porous sinterednickel electrodes, one for hydrogen and the other for oxygen, separated by an electrolyte. The oxygen electrode is treated with lithium and pre-oxidized to prevent corrosion. The electrolyte is a strong caustic potash and working conditions are around 200° C and 400 p.s.i. The electrolyte soaks into the porous electrodes but, on the application of gas under pressure from the back of the plate, is expelled from the larger pores; the gas cannot bubble through the smaller-pored surface due to the surface tension of the liquid. Thus, there is a very large surface of wetted metal in contact with gas in each electrode (about forty square metres).

Oxygen molecules on the oxygen electrode combine with water to form negatively charged hydroxyl ions, each of which removes an electron from the oxygen electrode. The hydroxyl ions migrate through the electrolyte to the hydrogen electrode where they combine with the hydrogen to form water, depositing an electron in the process. Thus the hydrogen electrode becomes negative with respect

A forty-cell battery with the hydrogen circulator and condenser for water removal mounted underneath





Simplified schematic diagram of fuel cell

to the oxygen electrode and, if a load is connected, current flows in the external circuit.

In order to remove the water formed, the hydrogen is circulated past the back of the hydrogen electrodes and the mixture of hydrogen and steam is cooled externally, so that the condensate can be released as required.

The pressure of the two gases in the cell must be very evenly balanced; to ensure this, a control system is incorporated to keep the oxygen pressure constant and to control the hydrogen pressure against it by a very accurate differential pressure meter which actuates a power-operated inlet valve controlled by a servomechanism.

In its present form, the hydrogen-oxygen fuel cell has reached the second stage of development and is now approaching the commercial proposition of a completely automatic source of power. Before this can be accomplished there are several problems to be solved, including the reduction in size of the control gear and the pre-heating of the cell.

When operating, the cell generates heat that can be used to keep the cell at its optimum operating temperature but, for starting, it is necessary to supply heat from an external source.

In its commercial form the cell will have to be provided with some means of pre-heating. This could be supplied by a secondary source of power, such as an accumulator or, alternatively, on offload condition the cell could be made to 'tick over' by supplying current to a pre-heating element. Up to the present time this problem has not been solved.

MATHEMATICAL TOOLS

By Computer

Cancel with Care

Lig. 1 shows an equivalent circuit for a transformer which has unity ratio, at frequencies sufficiently high for the shunting effect of the primary and secondary inductances to be negligible. Leakage inductance is represented by L and the primary and secondary capacitances by C_1 and C_2 ; these represent internal as well as external capacitances. The resistances R_1 and R_2 are mainly the source and load resistances, but can be taken to include also shunt losses in the transformer.

A constant current I is supplied, and the resulting secondary voltage V_0 is easily obtained in the form

$$\frac{IR}{V_0} = 1 - \omega^2 T_1^2 (1+b) d + j\omega T_1 \left(\frac{1+ab}{1+a} + d - \omega^2 T_1^2 b d\right)$$

where

$$R = \frac{R_1 R_2}{R_1 + R_2}, \ T_1 = C_1 R_1, \ a = R_1 / R_2$$

$$b = C_2 R_2 / C_1 R_1, \ d = L / C_1 R_1 (R_1 + R_2)$$
(2)

The magnitude of IR/V_0 , say 1/G, is therefore given by 1 1 + 9779(7 + 1)9 = 0771 + 7)

$$\overline{G^2} = 1 + \omega^2 T_1^2 \{ (x+d)^2 - 2d (1+b) \} + \omega^4 T_1^4 \{ d^2(1+b)^2 - 2bd (x+d) \} + \omega^6 T_1^{6} b^2 d^2$$
(3)

where
$$x = \frac{1 + ab}{1 + a}$$
 (4)

For maximal flatness we require the coefficients of $\omega^2 T_1^2$ and $\omega^4 T_1^4$ to be zero, so that

 $(x + d)^2 = 2d(1 + b)$... $d^2(1 + b)^2 = 2bd(x + d^2)$ (5)

$$d^{2}(1+b)^{2} = 2bd(x+d)$$
 ... (6)

Now if b = d = x = 1 it is easily verified that Equs. (5) and (6) are both true, but when b = 1, Equ. (4) tells

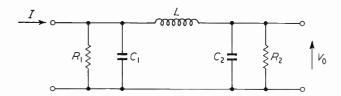


Fig. 1. An equivalent circuit for a unity-ratio transformer at high frequencies

us that x must be 1 whatever the value of a may be. Physically, b = 1 means that the time constants C_1R_1 and C_2R_2 are equal. In a practical case we might have $R_1 = 20 \text{ k}\Omega, R_2 = 5 \text{ k}\Omega, C_1 = 100 \text{ pF}, C_2 = 400 \text{ pF}$ and L = 50 mH; a then has the value 4 and b = d. _ - - • = 1, the time constants C_1

 R_1 and C_2R_2 being 2 μ sec.

Now let us consider the general case. In Equs. (5)

and (6) the quantities b, d and x are all real, positive and finite. The obvious way to proceed is to eliminate x[or rather (x+d)] by squaring both sides of Equ. (6) and substituting from Equ. (5); this gives

$$(1+b)^4 d^4 = 4b^2 d^2 \cdot 2d(1+b) \qquad \dots \qquad (7)$$

At this point we must note carefully that Equ. (7) could not only be obtained from Equs. (5) and (6) as they stand, but would also be obtained if Equ. (6) had been

$$d^{2} (1+b)^{2} = -2bd (x+d) \qquad \dots \qquad (8)$$

(1)

Equ. (8) is fortunately irrelevant to our present investigation, because b, d and x are positive, but when

squaring has to be done in order to solve equations, it is most important that all solutions obtained are checked in the original equations, because a solution of Equ. (7) could have been a solution of Equs. (5) and (8) instead of a wanted solution of Equs. (5) and (6).

Returning to Equ. (7), we can be quite sure that (1+b) and d^3 are different from zero, and therefore may be cancelled to give 012

$$d = \frac{8b^2}{(1+b)^3}$$
 (9)

Substituting from Equ. (8) to Equ. (5), we may also safely cancel a d and divide through by b to obtain

$$x = \frac{(1+b)^2 d}{2b} - d = \frac{4b \ (1+b^2)}{(1+b)^3} \qquad \dots \qquad \dots \qquad (10)$$

and we can easily verify that these values of x and dsatisfy the original Equs. (5) and (6), whatever the value of b may be. We have, however, already seen that although Equ. (4) is apparently a relation between x and a, it reduces to x = 1 (which is independent of a) when b = 1. Let us therefore try and express a in terms of x from Equ. (4) and see how the result is affected by putting b = 1.

Multiplying through Equ. (4) by the safely positive quantity (1 + a), we have

$$(1+a)x = 1+ab$$

Now provided that x is not equal to b, we can deduce from Equ. (11)

$$a = \frac{1-x}{x-b} \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (12)$$

Substituting from Equ. (10) for x, we can safely multiply numerator and denominator by $(1 + b)^3$ to clear cumbersome fractions, and we thus obtain

$$a = \frac{(1+b)^3 - 4b(1+b^2)}{4b(1+b^2) - b(1+b)^3} = \frac{1-b+3b^2-3b^3}{b\{3-3b+b^2-b^3\}} = \frac{(1-b)(1+3b^2)}{b(1-b)(3+b^2)}$$
(13)

Provided that b is not equal to 1, Equ. (13) yields

$$a = \frac{1+3b^2}{b(3+b^2)}$$
 (14)

by cancelling the factor (1 - b). If, however, b is equal to 1, we have already seen that x has the required value 1 whatever the value of a may be.

We have also noted that Equ. (12) is not valid when x = b; Equ. (11) in this special case tells us that x = 1. There is thus only one special case, when both x and b are equal to 1.

In order to understand the peculiarities of the special case, let us consider first what happens for a general value of b if we are content to allow a small tolerance in the value of x, so that we accept x_1 as sufficiently near the required value of x given by Equ. (10), where

$$x_1 = \frac{4b(1+b^2)}{(1+b)^3} (1+\lambda) \qquad \dots \qquad \dots \qquad (15)$$

If we think of λ as 0.01, this means that we are prepared to tolerate a 1% excess in x; if λ is -0.01, we are prepared to tolerate a 1% deficiency. When we allow x to be replaced by x_1 , we must correspondingly replace a by a_1 where

$$x_1 = \frac{1+a_1b}{1+a_1}$$
 (16)

Multiplying through Equ. (16) by $(1 + a_1)$ [which is positive in cases of practical interest] and rearranging, we have

In order to obtain a usable value of a_1 from Equ. (17), we must adjust λ so that x_1 is between b and 1 [if b = 1, Equ. (17) simply tells us that $x_1 = 1$ since a_1 cannot usefully be -1, and Equ. (15) then tells us that λ is necessarily zero. No tolerance is thus required, and a_1 reduces to a, which, as we have already seen, can have any value in this case]. If b exceeds 1, $(1 - x_1)$ and $(x_1 - b)$ will both be negative, so that a useful, positive value of a_1 is obtained; if b is less than 1, $x_1 - b$ and $(1 - x_1)$ will both be positive, so that again a useful value of a_1 is obtained. In either case we can find an explicit formula for a_1 from Equ. (17) by dividing through by $(x_1 - b)$. If we then substitute for x_1 from Equ. (15), we have

$$a_1 = \frac{1 - x_1}{x_1 - b} = \frac{(1 - b)(1 + 3b^2) - 4\lambda b(1 + b^2)}{b(1 - b)(3 + b^2) + 4\lambda b(1 + b^2)} \quad \dots \quad (18)$$

The position we have now reached is that if we require exact maximal flatness in the general case $(b \neq 1)$ we must make R_1/R_2 have the value *a* given by Equ. (14). Nevertheless, if we are prepared to tolerate a slight departure from maximal flatness (measured by the quantity λ defined in Equ. (15)) we can allow R_1/R_2 to have instead the value a_1 given by Equ. (18). λ must necessarily be small, or the variation of *G* with frequency [Equ. (3)] will be excessive. If therefore (1 - b) is not small, whether it is positive or negative, a_1 will not be very different from *a*. On the other hand, if (1 - b) is comparable with λ , a_1 can be very different from *a*. Suppose, for example, that b = 0.99. Then Equ. (18) reduces to $0.0394 - 7.8412\lambda$

$$a_1 = \frac{0.0394 + 7.0112\lambda}{0.0394 + 7.8412\lambda} \qquad \dots \qquad \dots \qquad (19)$$

and therefore if λ is just below +0.005, a_1 is small and positive, while if λ is just above (i.e. nearer zero than) -0.005, a_1 is very large. Hence although the value of *a* for maximal flatness is in this case very close to unity [from Equ. (14) with b = 0.99 or Equ. (19) with $\lambda = 0$] λ will not numerically exceed 0.005 for any value of R_1/R_2 , so that the error in *x* will not exceed $\frac{1}{2}\%$ and there will be very little change of G_1 with frequency whatever the value of R_1/R_2 may be. Correspondingly, if we put $(1 - \epsilon)$ for *b* in Equ. (18) and neglect ϵ^2 and $\epsilon\lambda$, Equ. (18) reduces to

$$a_1 = \frac{\epsilon - 2\lambda}{\epsilon + 2\lambda} \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (20)$$

and, therefore, although the correct value for maximal flatness is found from Equ. (14) to be unity, λ will only lie between $+\frac{1}{2} \epsilon$ [$R_1 \ll R_2$, a_1 small] and $-\frac{1}{2} \epsilon$ [$R_1 \gg R_2$, a_1 large] whatever the value of a_1 may be.

If $\frac{1}{2}\epsilon$ numerically exceeds the greatest value of $|\lambda|$ that can be tolerated, say λ_0 , then Equ. (20) shows that a_1 can only be varied between finite limits which include the value given by Equ. (14); in fact

$$\frac{|\epsilon| - 2\lambda_0}{|\epsilon| + 2\lambda_0} < a_1 < \frac{|\epsilon| + 2\lambda_0}{|\epsilon| - 2\lambda_0} \quad \dots \quad \dots \quad (21)$$

and, as we have already noted, if $|\epsilon|$ is large compared to λ_0 [though still sufficiently small to justify the neglect of ϵ^2 and $\epsilon\lambda$ in deriving Equ. (20)] a_1 differs little from the value unity obtained for a in Equ. (14) neglecting ϵ^2 . If ϵ^2 cannot be neglected, we must, of course, use Equ. (18) instead of Equ. (20), but the result is still essentially the same— a_1 does not differ appreciably from a if the error in x is to be kept within the prescribed tolerance.

Thus the apparently anomalous case when b=1 is now seen in its proper perspective as a limiting case. The value a_0 of a obtained from Equ. (14) after the factor (1 - b) is cancelled always gives maximal flatness, and if (1 - b) is not small (whether positive or negative) we cannot vary a appreciably from a_0 without seriously disturbing the constancy of G_1 with respect to frequency. If (1 - b) is small, but of the same order of magnitude as the maximum relative. discrepancy in x that can be tolerated, a_0 is still the correct value of a for maximal flatness, but considerable variation of a can be permitted without seriously disturbing the constancy of G. When (1 - b)is very small, even the variation of a from 0 to ∞ will have so little effect on the value of x, that the maximal flatness is virtually independent of a. When b is actually 1, we simply proceed to the limit so that the maximal flatness is completely independent of the value of a, and no tolerance in the value of x is required.

U.S. ELECTRONICS

The 6th National Symposium on Reliability and Quality Control in Electronics will be held at the Statler Hilton Hotel, Washington, D.C. from 11th to 13th January 1960. Information regarding the submission of papers and attendance at the Symposium may be obtained from Mr. R. Brewer of the Research Laboratories, The General Electric Co. Ltd., Wembley, Middlesex. (Arnold 1262).

Coaxial-Cable Performance

DETERMINATION OF SINE-SQUARED PULSE RESPONSE

By W. A. Cameron, B.Sc., A.M.I.E.E.*

he British Post Office has recently included in its specification for repeater sections of 0.375-in. coaxial cable, pulse measurements of impedance regularity, and has followed the C.C.I.T.T.† recommendations¹ governing the overall testing of television links, that the test pulse should be sine squared in shape. This specification is for a three-mile and six-mile repeater spacing and requires a test pulse of width **at** half height of $0.1 \,\mu$ sec.

The transmission of a transient waveform through a cable causes a decrease in amplitude of the waveform and an increase in its effective width. Thus the measurement of impedance regularity of a cable by pulse reflection requires a knowledge of the response of the cable to the impulse used. This can be measured experimentally using multiple reflections in a short length of cable, or calculated from a knowledge of the pulse shape.

Measurement of the Pulse Response of Coaxial Cable

Equipment essential for the pulse measurement of cable impedance regularity consists of a pulse generator and a high-speed oscilloscope with a fairly high sensitivity².

In order to measure the pulse response of the cable, the pulse generator, which is normally of low output impedance, is connected to a short length l of the cable under test through a series resistor of value R, and the output from the cable is connected to the oscilloscope input (which is of impedance R_0) through a similar resistor (as shown in Fig. 1). Due to the presence of the second resistor, a discontinuity will exist and, at this point, the input pulse will be reflected and an echo pulse will travel along the cable towards the pulse generator where it will again be reflected. At each point of discontinuity there will be a reflection factor of

$$\rho = \frac{R - R_0}{R + R_0} \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (1)$$

and a voltage transmission factor of

$$k = \frac{2 R_0}{R + R_0} \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (2)$$

where R_0 is the characteristic impedance of the cable. Thus, if R is chosen to be much larger than R_0 and the oscilloscope is of a sufficiently high gain to compensate for the factor k then, for each input pulse, a train of impulses will be displayed on the oscilloscope and the *n*th impulse of the train will be distorted due to trans-

Electronic & Radio Engineer, September 1959

mission along a length (2n-1) l of cable. Since the maximum value of R will be limited by the available gain of the oscilloscope amplifier, a correction to each pulse height will have to be made for the additional attenuation due to the factor $\rho^{2(n-1)}$. Fig. 2 shows a typical echo train and Fig. 3 the decrease of the pulse height with the length of cable traversed, as measured in the laboratory on 750 yards drum length of 0.375 in. coaxial cable using this technique. These results have been corrected for the additional attenuation due to the factor $\rho^{2(n-1)}$.

Calculation of the Response of 0.375 in. Trunk Coaxial Cable to a Sine-Squared Pulse

If a linear system is driven by a transient signal and if the transient is of sufficiently short duration then the output waveform from the system may be approximated by the impulse response of the system. The pulse response of a system is its response to a Dirac impulse $\delta(t)$ which has a Laplace Transform given by

$$\int_{0}^{\infty} e^{-st} \,\delta(t) \,dt = 1 \qquad \dots \qquad \dots \qquad \dots \qquad (5)$$

As is well known³, if i(t) is the system impulse response and f(t) the input waveform then, assuming zero initial values, the output will be given by the convolution integral

$$V_0(t) = \int_0^t i(\tau) f(t-\tau) d\tau \quad .. \qquad (6)$$

and by use of this integral one may compute the response

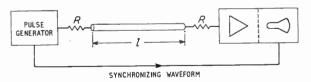
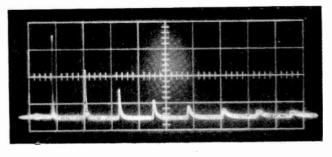


Fig. 1. Measurement of cable pulse response by multiple reflections

Fig. 2. Typical echo train



^{*} Research Laboratories, General Electric Co. Ltd., Wembley. † International Telegraph and Telephone Consultative Committee.

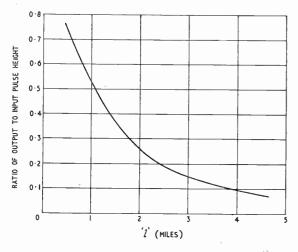


Fig. 3. Measured decrement in pulse height v. length of cable

of a linear system to any waveform from a knowledge of the system impulse response.

The transmission of a voltage wave along a correctly terminated transmission line is given by

$$P = j H f + (1+j) K \sqrt{f}$$

where H and K are constants depending on the cable dimensions. Putting $s = j\omega = 2 \pi j f$

$$Px = \frac{HXs}{2\pi} + \frac{Kx}{\sqrt{\pi}}\sqrt{s} \qquad \dots \qquad \dots \qquad (8)$$

where, for 0.375-in. trunk coaxial cable,

 $K = 4.375 \times 10^{-4}$.

In a transient analysis we may neglect the basic time delay due to exp $-(HX s/2\pi)$ and consider the response

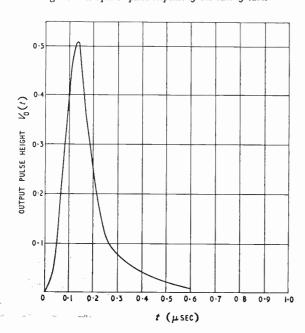


Fig. 4. Sine-squared pulse response of one mile of cable

of a network having the transfer characteristic

$$V_0(s,x) = V_i(S,0) \exp\left(\frac{-Kx}{\sqrt{\pi}}\sqrt{s}\right) \qquad \dots \qquad (9)$$

The impulse response of the cable is given by the inverse transform of

$$\exp\left(\frac{-Kx}{\sqrt{\pi}}\sqrt{s}\right)$$

which is given by Carslaw and Jaegar³ as

$$i(t) = \frac{Kx}{2\pi t} 3/2 \exp\left(\frac{-K^2 x^2}{4\pi t}\right) \qquad \dots \qquad (10)$$

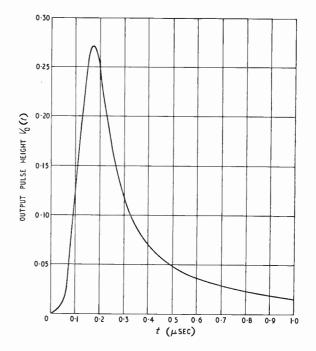


Fig. 5. Sine-squared pulse response of two miles of cable

Substituting Equ. (10) into the integral (6) and taking

$$\begin{cases} = \sin^2(\pi t/2T), \ 0 \le t \le 2T \\ = 0, \ t < 0 \ \text{and} \ t > 2T \end{cases}$$
(11)

we see that the output waveform from the cable is given by

$$V_0(t) = \frac{Kx}{2\pi} \int_0^t \frac{1}{\tau} 3/2 \, \exp\left(\frac{-K^2 x^2}{4\pi\tau}\right) \sin^2\frac{\pi}{2T} (t-\tau) \, d\tau$$

This integral has been evaluated over the relevant range of t for x = 1, 2, 3, and 4 miles using a Hollerith HEC 2M digital computer. Graphs of the output waveform for these lengths of cable are given in Figs. 4–7. Fig. 8 shows how the calculated height of the output pulse varies with cable length, and is in good agreement with the measured curve given in Fig. 3. Fig. 9 gives the pulse height attenuation in dB plotted against the cable length in yards. This is the curve which would normally be used in correcting a cable echo response to allow for pulse-height attenuation.

Electronic & Radio Engineer, September 1959

World Radio History

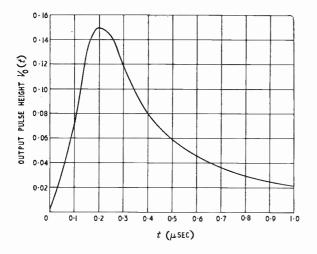


Fig. 6. Sine-squared pulse response of three miles of cable

Validity of the Impulse Approximation

It is of interest to know the minimum length of cable for which it is valid to consider the pulse as an impulse in computing the attenuation of the pulse amplitude and this question will now be considered.

The Laplace Transform of the sine-squared pulse is given by

$$V_{i}(s) = \int_{0}^{\infty} e^{-st} \sin^{2} \frac{\pi t}{2T} dt$$
$$= \left\{ \frac{1 - e^{-2st}}{2} \right\} \left\{ \frac{1}{s} - \frac{s T^{2}}{s^{2} T^{2} + \pi^{2}} \right\} \qquad ... (13)$$

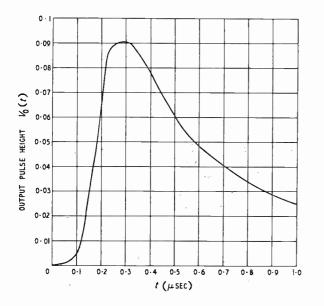
We may expand this in ascending powers of T as

$$V_{i}(s) = T - sT^{2} + s^{2}T^{3} \left\{ \frac{2}{3} - \frac{1}{\pi^{2}} \right\} - s^{3}T^{4} \left\{ \frac{1}{3} - \frac{1}{\pi^{2}} \right\}$$
... (14)

Now, $V_0(s) = V_i(s) Z(s)$, where Z(s) is the system function.

Thus from Equ. (14) we see that since, assuming

Fig. 7. Sine-squared pulse response of four miles of cable

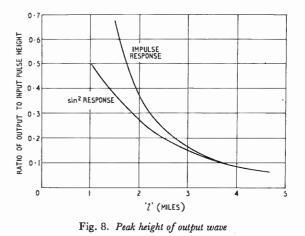


zero initial conditions, multiplication of the system function by s^n implies the *n*th differentiation of the system impulse response we may, by performing the requisite differentiations, expand $V_0(t)$ in ascending powers of T as

$$V_{0}(t) = T i(t) - T^{2} \frac{di(t)}{d(t)} + T^{3} \left\{ \frac{2}{3} - \frac{1}{\pi^{2}} \right\} \frac{d^{2}i(t)}{dt^{2}} - T^{4} \left\{ \frac{1}{3} - \frac{1}{\pi^{2}} \right\} \frac{d^{3}i(t)}{dt^{3}} \qquad ... \quad (15)$$

where $i(t) = \frac{Kx}{2\pi t} \frac{3}{2} \exp\left\{ -\frac{K^{2}x^{2}}{4\pi t} \right\} = \frac{b}{t} \frac{3}{2} \exp\left(-\frac{a}{t} \right) \frac{di(t)}{dt} = \left\{ \frac{a}{t^{2}} - \frac{3}{2t} \right\} i (t) \frac{d^{2}i(t)}{dt^{3}} = \left\{ \frac{a}{t^{2}} - \frac{3}{2t} \right\} \frac{di(t)}{dt} + \left\{ \frac{3}{2t^{2}} - \frac{2a}{t^{3}} \right\} i (t)$

Since we are interested in the peak response we shall



consider the validity of the approximation at the time when di(t)/dt = 0, that is when

$$t = \frac{2a}{3} \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad \dots \qquad (16)$$

Thus neglecting powers of T greater than the third we require that

$$\begin{vmatrix} T^{3} \left\{ \frac{2}{3} - \frac{1}{\pi^{2}} \right\} \frac{d^{2}i}{dt^{2}} \end{vmatrix} \ll \begin{vmatrix} T i(t) \end{vmatrix}$$

or
$$\begin{vmatrix} T^{2} \left\{ \frac{2}{3} - \frac{1}{\pi^{2}} \right\} \left\{ \frac{3}{2t^{2}} - \frac{2a}{t^{3}} \right\} \end{vmatrix} \ll 1$$

or substituting from Equ. (16) $1.89/a^2 \ll 1$. For an 0.1-µsec pulse on 0.375-in. trunk coaxial cable

$$a = 0.153 \times 10^{-7} x^2$$

 $T = 10^{-7} \sec x^2$

and our requirement becomes

$$x^4 \gg 80.7$$

or x > 3 miles ... (17) Substituting Equ. (16) into Equ. (12) we obtain

$$i(x)_{\text{peak}} = \frac{T \, 3\sqrt{6\pi}}{K^2} \frac{\exp}{x^2} (-1.5) = \frac{1.518}{x^2} \dots (18)$$

Electronic & Radio Engineer, September 1959

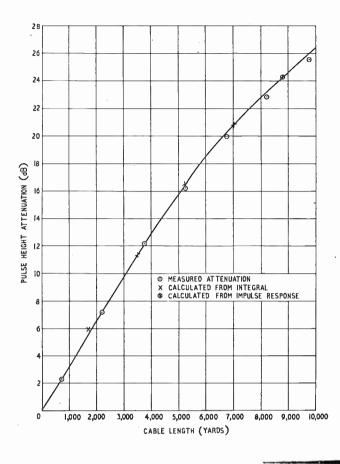


Fig. 9. Height attenuation of $0 \cdot 1$ µsec sine-squared pulse

where x is in miles and for 0.375-in. trunk coaxial cable $K = 4.375 \times 10^{-4}$ and $T = 10^{-7}$.

Thus we see that for cable lengths of greater than three miles the pulse height is decaying according to the inverse square of the cable length. That is, doubling the length of cable traversed will produce an additional attenuation of 12 dB.

This function is shown in Fig. 8 where it is compared with the peak height of the response of the cable to an 0.1- μ sec sine-squared pulse.

Conclusion

Methods have been described for the calculation and measurement of the response of a length of cable to a transient waveform of given shape. In particular, a curve has been derived for the attenuation of the peak amplitude of an 0.1- μ sec sine-squared pulse propagating through 0.375 in. diameter coaxial cable of the type used for trunk telephony.

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 H. S. Carslaw and J. C. Jaegar, "Operational Methods in Applied Mathematics" Oxford University Press, 1948.

Correspondence

Letters to the Editor on technical subjects are always welcome. In publishing such communications the Editors do not necessarily endorse any technical or general statements which they may contain.

Comparison of Four Television Standards

SIR,-Dr. Haantjes and Mr. Breimer of Philips' Research Laboratories, have pointed out the existence of an error in the Appendix of my article, "Comparison of Four Television Standards", which appeared in Electronic & Radio Engineer, November 1957. The formula for the group delay, $\tau(x)$, given in the caption of Fig. 6, is too small by a factor n and this means that the scale of group-delay ordinates in Fig. 6 requires multiplication by 40 for the U.K., U.S. and West European television systems, whilst the French system requires a multiplication by 15. The same remarks apply to the ordinate scale of Fig. 7, whilst in Fig. 8 each ordinate corresponding

to a given abscissa, n, must be multiplied by that value of n. Also, the formula for $\phi(x)$ must be multiplied by *n*.

The result of this correction is to make the group-delay errors caused by the Nyquist slope in the receiver no longer negligible, as was suggested in the original article.

The last column of the attached table gives a measure of the group-delay error as a proportion of the duration of a picture element. It will be seen from this that the U.K. system suffers very little degradation, but that the West European 625-line system, employing negative modulation, gives rise to an error across the video band of nearly three picture elements. It is, of course, true

Television system	Parameter, n determining steepness of Nyquist slope in receiver	Picture Element duration τ_0 (μsec)	Group delay at vision carrier .f., $\tau (\omega_0)$ (μsec)	Group delay at cut-off frequency of main sideband $\tau (\omega_0 + \omega_c)$ (µsec)	Difference : $\tau(\omega_0) - \tau(\omega_0 + \omega_c)$ (μsec)	$\frac{\tau(\omega_0) - \tau(\omega_0 + \omega_c)}{\tau_0}$
U.K	40	0.167	0 · 52	0.36	0.16	0.96
U.S	40	0.125	0.52	0.30	0.22	1.76
West European neg. mod. 5-Mc/s video	40	0.100	0.52	0.24	0.28	2.80
French	15	0.048	0 · 142	0.073	0.069	1 · 44

that much greater errors than these may arise in practice and, furthermore, the modulation depth has an effect upon the way in which these group-delay errors are translated into distortion of the response of a receiver to transient excitations.

D. MAURICE.

B.B.C. Research Department, Kingswood Warren, Surrey. 9th September 1959.

Echo-Distortion in Frequency Modulation

SIR,—Mr. Medhurst's article in the July issue, p. 253, is a valuable contribution to the study of multichannel radio systems, and has been read with interest. Some of the results given have been compared with measurements made in this Laboratory, and good agreement has been found.

It may be of interest to mention a further approximate result

when θ_0 is large, derived from a consideration of the f.m. noisepower spectrum. This approximation neglects the effect of the carrier phase and therefore gives only the mean distortion power ratio; it is,

$$\frac{1}{r^2} \frac{D}{S} = \frac{1}{2\sqrt{\pi A^3} \left(1 - \frac{\sin\theta_0}{\theta_0}\right)^{\frac{1}{3}}} \exp\left(-\frac{1}{4A^2 \left(1 - \frac{\sin\theta_0}{\theta_0}\right)}\right)^{\frac{1}{3}}$$

where Mr. Medhurst's symbols are used. The result is valid only for large values of A; it closely follows the mean-power curves derived from Figs. 1 and 2 for $A \theta_0 > 2$ and A > 1.

It may also be noted that the mean-power curves lie 3 dB below the corresponding curves in Fig. 1 over the region where Equation (7) is valid (approximately $A \theta_0 < \frac{1}{2}$).

the publication of this translation, there are at least three eminently practical aspects which ought to be stated. First, this book is widely

quoted in publications, but access to it was difficult until now.

Secondly, even after nearly two decades this is an invaluable

reference book for the serious research worker in this field; as an

R. HAMER

Cardiff.

Post Office Engineering Dept.,

18th September 1959.

New Books

Synthesis of Linear Communication Networks

By WILHELM CAUER. Pp. 866 + xxxvi. McGraw-Hill Publishing Co. Ltd., 95 Farringdon Street, London, E.C.4. Price \pounds 7.17s.

This is not a 'new' book. The first edition of this classic of German and international circuit theory was completed in 1940 and published in Germany in 1941 (under the title "Die Theorie der linearen Wechselstromschaltungen"). A new, much enlarged, edition was originally planned and prepared by Cauer himself. After his tràgic and early death in 1945 a second edition was prepared by Klein and Pelz and published (again in German) in 1954. This edition contains some additions based on various Cauer manuscripts and a number of explanatory comments and notes by the editors. Now an English (or rather American) translation, based on the second German edition, has been prepared by Knausenberger and Warfield. Some of the material has been re-arranged, and some notes and comments by the translators and "a commentary of latest developments in network theory together with a bibliography of pertinent English-American literature" have been added.

Cauer is one of the pioneers and architects of modern network theory. One of his first important contributions was the generalization of Foster's reactance theorem, on the one hand by means of continued fraction expansions leading to ladder structures, and on the other hand by extending it to RC and RL two-terminal networks. This was followed by the application of elliptic function theory to approximation ('interpolation') problems in network design (combined with a modern treatment of lattice filters). He continued to contribute to all problems of modern network synthesis, always with originality and mathematical rigour, his fundamental aim being the creation of 'exact mathematical' synthesis methods.

Modern synthesis methods are characterized by three stages.

- 1. General types and structures of 'physically possible' networks are studied and corresponding classes of network performance characteristics are determined.
- 2. The performance characteristics required in a particular design or synthesis problem (which originally do not exactly correspond to those of a physically possible network) are *approximated* by suitably chosen characteristics which do correspond to such a network.
- 3. A network is *realized* which corresponds to the chosen approximating characteristics.

Until less than two years ago there were no text books in English dealing in a comprehensive way with such modern synthesis methods. Today the situation is different, and this is chiefly due to the publication of Guillemin's latest book "Synthesis of Passive Networks" (which has to be considered together with his well-known previous books).

Thus the question arises :---What purpose is served by the publication of another book which deals basically with the same subject and which in its essential parts is now nearly 19 years old? To this reviewer the answer seems clear :---Quite apart from the historical interest with which many research workers in this field will greet

example it may be mentioned that some derivations of important formulae, given without proof in Darlington's famous publication on insertion-parameter filters, will be found in Cauer's book. Thirdly, the treatment and style in Cauer's book are quite different from those in Guillemin's book. Where Guillemin always seems to remain the teacher, passionately interested in making matters easy for the reader—without in any way lowering the standard—Cauer's main interest seems to lie in mathematical rigour and in the generality of results. This difference in the two authors' styles and methods of approach increases by their very contrast the attraction and value of the appearance of Cauer's book in an English edition. The book begins with four prefaces of various kinds, a short biographical note by his widow and an extract from an obituary, written by K. W. Wagner. After a list of Cauer's publications and patents and a detailed list of contents there is an Introductory

written by K. W. Wagner. After a list of Cauer's publications and patents and a detailed list of contents there is an Introductory Chapter which has been added in the second edition and is based on an original monograph by Cauer. Its value appears doubtful, as it is in many parts difficult to understand unless the reader is already familiar with the book or at least with the subject matter. On page 28 the characteristics function ψ (where ψ is defined by the expression $A = \log_e \sqrt{1 + |\psi|^2}$ for the 'operating loss' A) is discussed. Here the statement "..., if the operating loss is prescribed, ψ can be found except for its sign" is wrong (the corresponding statement on p. 27 in the second German edition "if the operating loss is prescribed, ψ can generally be chosen in various different ways, even apart from its sign" is correct). The following chapters are: 1. Statement of the Problems and Examples; 2. Circuit Analysis; 3. Two-Terminal-pair Networks; 4. Positive-real Functions and Positive Matrices; 5. Reactance Theorems; 6. Image Parameter Theory of the Low-pass Reactance Filter; 7. Generalized Image-parameter Theory. Then there are two appendices (1. Two-terminal-pairnetwork Formula Collection, and 2. Practical Filter-design Techniques Based on the Image-parameter Theory) which complete the first part of this book. In the English edition there are two parts (designated as 'volumes 1 and 2'), though the book is published like its two German predecessors in one single volume, and though the German editions do not show any division into two parts. This sub-division of the English edition, involving a re-arrangement of appendices, is regrettable as it may cause confusion, particularly as Dr. Glowatzki, a pupil of Cauer, is preparing a 'second volume' for the German edition, containing so far unpublished Cauer manuscripts (announced in the second German, but not in the English edition).

The chapter headings of part II of the English edition are: 8. Reactance Two-terminal-pair Networks with Prescribed Operating Conditions; 9. Frequency Band-separating Networks; 10. Equivalence of Reactance Networks. They are followed by five appendices (1. Aids in Linear Algebra; 2. Elements of the Theory of Analytic Functions; 3. Solution of Some Chebyshev Extremal Problems; 4. Practical Filter Design Techniques Based on the Operating-parameter Theory; 5. Recent Advances; Supplementary References) and by an Index. Appendix 5 represents an attempt to bring the book up to date.

Summarizing, it may be said that the editors and translators of this book had a very difficult task and the result can be criticized, and could probably be improved, in many details. However, this is rather unimportant. It should also be said that this is emphatically not a book for a first study of the subject, and even for a specialist it would not serve as the only book on synthesis. However, "Cauer" should be studied and consulted by, and be accessible to, everybody working in the field of modern network synthesis and design. The publication of this translation will make the attainment of this aim very much easier. W.S.

Noise in Electron Devices

Edited by LOUIS D. SMULLIN and HERMANN A. HAUS. Pp. 413 + xvi. Chapman & Hall Ltd. (for John Wiley), 37 Essex Street, London, W.C.2. Price 96s.

The 'electron devices' with which this book is concerned might be summarized as active network devices, since they are gridcontrolled thermionic valves, electron-beam tubes and transistors. This is further emphasized by decorating the cover with a pattern of " $2eI_0\Delta f$ ", and the impression on the reader is almost that pains have been taken to seclude mention of $4RkT\Delta f$ from the book as far as possible. This is unfortunate, because the minimum noise of most thermionic devices is proportional to cathode temperature.

Of the authors contributing to this book, Haus, Quate and Peter are known to all who are interested in electron-beam tubes, and Van der Ziel is known as an authority on flicker noise and semiconductors. Noise in multi-electrode valves is covered by Talpey (who has published work on elastically-reflected electrons in relation to induced grid noise), and noise in practical transistors and transistor amplifiers by Fonger of R.C.A. Laboratories, Princeton. The book contains a great deal of information which hitherto has been scattered in the literature and thus will be a valuable introduction for anyone intending to specialize in one of the three fields which it covers. It claims to its credit thorough mathematical analyses, but at times one feels a lack of that physical interpretation which would assist in transferring the theory to new applications.

The book is based on a vacation course given at M.I.T. in 1955, and unfortunately for the authors the intervening years have been exceptionally fruitful in the development of amplifying devices. The maser and the (variable-capacitance) parametric amplifier appear only by way of apology in the preface, and the book includes neither the most recent work on low-noise guns for conventional travellingwave tubes nor the recent work on 'fast-wave' low-noise beam amplifiers.

The reader who has followed this book will have no difficulty in following the subsequent literature on electron-beam amplifiers, but he may feel the lack of guidance in approaching the noise properties of the maser. D.A.B.

Television Servicing

By ALEX LEVY and MURRAY FRANKEL. Pp. 534 + vii. McGraw-Hill Publishing Co. Ltd., 95 Farringdon Street, London, E.C.4. Price 43s.

This should be a useful book to anyone concerned with American television receivers. Its application to British receivers, however, is limited by the difference between the two television systems, for these have led to big differences in receiver circuitry. W.T.C.

Basic Electricity

By VAN VALKENBURGH, NOOGER & NEVILLE Inc. Pp. 596 in 5 parts. The Technical Press Ltd., 1 Justice Walk, Chelsea, London, S.W.3. Price 55s.

These books form a course of training developed for the U.S. Navy and adapted to British and Commonwealth usage by a special electronics training investigation team of R.E.M.E. They are of a very elementary nature, starting with the electron and frictional electricity and ending with circuit breakers.

Anyone examining these books is apt to be misled by the form of the illustrations. Many are of a pictorial character, which will undoubtedly help the real beginner, but most are far too big, creating an impression almost of a child's picture book. The text, however, is clearly written and the material is, in the main, well presented.

The books form a first course of an unusual character and one which is worth studying by anyone interested in elementary training. W.T.C.

Radio Circuits (4th Edition)

By W. E. MILLER, M.A. (Cantab.), M.Brit.I.R.E. Revised by E. A. W. SPREADBURY, M.Brit.I.R.E. Pp. 172 + ix. Published for *Wireless & Electrical Trader* by Iliffe & Sons Ltd., Dorset House, Stamford Street, London, S.E.1. Price 15s.

BRITISH STANDARDS

Fixed Electrolytic Capacitors (Aluminium Electrodes) Pp. 10. B.S. 2134, Part 2: 1959. Price 5s.

Year Book 1959

Pp. 543. Contains information about the Institution and the services it offers. It lists the British Standards current at 1st January 1959. Price 15s.

These publications can be obtained from British Standards Institution, 2 Park Street, London, W.1.

NATIONAL BUREAU OF STANDARDS

On the Theory of Fading Properties of a Fluctuating Signal imposed on a Constant Signal By H. BREMMER. Pp. 32. Price 32 cents.

, _____ xp. oz. x1/0 02 00110.

Standards Materials issued by the National Bureau of Standards

Pp. 27. Price 44 cents.

Tables of Osculatory Interpolation Coefficients By H. E. SALZER. Price 38 cents.

Tables of the Exponential Integral for Complex ArgumentsApplied Mathematics Series 51. Price \$5.65.

Fractional Factorial Experiment Designs for Factors at Three Levels

Pp. 37. Price 38 cents.

Maximum Permissible Body Burdens and Maximum Permissible Concentrations of Radionuclides in Air and Water for Occupational Exposure

Pp. 95. N.B.S. Handbook 69. Price 44 cents.

These publications can be obtained from the Superintendent of Documents, U.S. Government Printing Office, Washington 25, D.C., U.S.A.

MANUFACTURERS' LITERATURE

Brimar Valve and Teletube Manual No. 8. A 374-page catalogue including details of recent additions to the ranges of products available, as well as comprehensive information on many current equipment valves. The catalogue also includes: new rating charts for rectifiers, data on "Replacement and Obsolete" types and a revised circuits section. Price 6s.

Standard Telephones & Cables Ltd., Valve Division, Footscray, Sidcup, Kent.

Advance Components Catalogue. This revised edition includes comprehensive details of all current products : a.f. and r.f. generators, v.h.f. and f.m./a.m. generators, 'Q' meters, standard inductors, crystal calibrator, a.c. valve voltmeter, attenuator casting and switch, attenuators and coaxial switches.

Advance Components Ltd., Roebuck Road, Hainault, Ilford, Essex.

How to use Araldite Epoxy Resin Adhesives. A booklet produced as a guide to the materials which can be successfully bonded by Araldite.

CIBA (A.R.L.) Ltd., Duxford, Cambridge.

Electrical Insulation. A 24-page booklet describing electrical insulating materials produced by Langley London Ltd. Includes

ⁱ nformation on mica and mica products and the range of Lantex laminates of paper-fabric and glass with bonds of phenolic, polyester, ethoxylene, silicone and other resins. Langley London Ltd., Kelvin Way, Crawley, Sussex.

Permanent Magnets Summarized. This 48-page booklet was written by F. G. Tyack, A.M.I.E.E., of James Neill & Co. (Sheffield) Ltd., and gives practical information on design and application of permanent magnets.

James Neill & Co. (Sheffield) Ltd., Magnet Department, Napier Street, Sheffield 11, Yorks.

Regalox Alumina Ceramics. Booklet containing information on high-grade sintered alumina ceramic materials produced by *Royal Worcester Ceramics Ltd., Tonyrefail, Glamorgan.*

Beryllium Products. Illustrated technical brochures available on beryllium copper wrought alloys and beryllium metal. Beryllium Smelting Co. Ltd.,

36-38 Southampton Street, London, W.C.2.

Mullard Photomultiplier Tubes. A 6-page folder giving characteristics, constructional details, etc., of photomultiplier tubes for scintillation counting.

Mullard Ltd., Torrington Place, London, W.C.1.

Copper Cables. Pp. 62. Contains chapters on the properties of copper and some of its alloys, the manufacturers of copper wire, power, transmission and other types of insulated cables. An appendix, bibliography and list of applicable British Standards, together with numerous diagrams and illustrations, are also included. *Copper Development Association*, 55 South Audley Street, London, W.1.

MEETINGS

I.E.E.

27th October. "Future Trends in Memory Stores for High-Speed Digital Computers", discussion to be opened by W. Renwick, M.A., B.Sc.

28th October. "Development of Eurovision", by M. J. L. Pulling, C.B.E., M.A.

2nd November. "Some Comments on the Classification of Waveguide Modes", by A. E. Karbowiak, B.Sc.(Eng.), Ph.D., and "Some Comments on Quasi-Optical Methods at Millimetre Wavelengths", by L. Lewin.

3rd November. "An Analogue Electronic Multiplier using Transistors as Square-Wave Modulators", by P. Gleghorn, B.Sc. (Eng.).

6th November. Medical Electronics Discussion Group. Subject not announced, to commence at 6 o'clock.

9th November. "Theory of the Travelling-Wave Parametric Amplifier", by Prof. A. L. Cullen, Ph.D., B.Sc.(Eng.); "The Gain of Travelling-Wave Ferromagnetic Amplifiers", by P. J. B. Clarricoats, B.Sc.(Eng.), Ph.D.; "Some Properties of Travelling-Wave Resonance", by J. R. G. Twisleton, B.Sc., and "Saturation Effects in a Travelling-Wave Parametric Amplifier", by A. Jurkus, B.Sc., and P. N.Robson, B.A.

These meetings will be held at the Institution of Electrical Engineers, Savoy Place, Victoria Embankment, London, W.C.2, and will commence at 5.30, except where otherwise stated.

The Television Society

22nd October. "New Television Standards: Their Effect on British Television". Discussion.

6th November. "Deflection Techniques for 110° Picture Tubes", by B. Eastwood, B.Sc.

These meetings will commence at 7 p.m. at the Cinematograph Exhibitors' Association, 164 Shaftesbury Avenue, London, W.C.2.

The Society of Instrument Technology

14th October. "An Automatic Analogue Computer for Missile Homing Investigations", by J. G. Thomason, B.Sc., to be held at Manson House, 26 Portland Place, London, W.1, at 7 o'clock.

Brit. I.R.E.

28th October. "Radio-Its Impact on Shipping", by Captain J. D. F. Elvish, C.B.E., and "A Historical Survey of Radar and

Electronic & Radio Engineer, September 1959

Radio Aids to Aircraft Navigation", by Air Marshal Sir Raymund G. Hart, K.B.E., C.B., M.C. 4th November. "Input/Output Devices", half-day symposium;

4th November. "Input/Output Devices", half-day symposium; meetings commencing at 3 and 6 p.m.

11th November. "Physiological and Acoustical Aspects of Hearing" by R. P. Gannon, B.Sc., M.B., Ch.B.

These meetings will be held at the London School of Hygiene and Tropical Medicine, Keppel Street, Gower Street, London, W.C.1, and will commence at 6.30, except where otherwise stated.

NEW DIRECTOR FOR S.I.M.A.

The Scientific Instrument Manufacturers' Association of Great Britain have recently announced the inauguration of S.I.M.A.'s new Director—Captain Robert Alexander Villiers, C.B.E., A.M.I.E.E., R.N. (Retired).

OBITUARY

It is with regret that we learn of the sudden death of a well-known personality in the radio industry, Thomas Edward Goldup, C.B.E., M.1.E.E., aged 65.

Mr. Goldup joined Mullard Valve Co. in 1923, and in 1928 was responsible for the formation of their Technical Service Department. In 1938 he was made a director of Radio Transmission Equipment Ltd., now Mullard Equipment Ltd. and, in 1951, he was appointed a director on the main Mullard board.

In addition to his work for Mullard Ltd., Mr. Goldup was known throughout the industry for his active participation in matters relating to technical education. He was a member of many committees, including the British Standards Institution and Radio Industry Council, and he was Chairman of the Ministry of Supply at Malvern.

Mr. Goldup was appointed C.B.E. in 1954 and elected President of the Institution of Electrical Engineers for the year 1957/58.

STANDARD-FREQUENCY TRANSMISSIONS

(Communication from the National Physical Laboratory) Deviations from nominal frequency* for July 1959

$\begin{array}{c c c c c c c c c c c c c c c c c c c $			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1959	1500 G.M.T.	1030 G.M.T.
	 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	NM 18 · 3 18 · 3 18 · 4 18 · 3 18 · 0 NM 18 · 0 18 · 5 18 · 5 18 · 2 18 · 1 18 · 0 18 · 2 18 · 1 18 · 0 18 · 3 18 · 3 18 · 4 18 · 3 18 · 1 16 · 8 16 · 1	- 7 - 7 - 8 NM NM - 10 - 11 - 12 - 13 NM - 11 - 9 - 9 - 9 - 9 - 9 - 9 - 9 - 9

* Nominal frequency is defined to be that frequency corresponding to a value of 9 192 631 770 c/s for the N.P.L. caesium resonator.

 \uparrow At 2400 G.M.T. on this day the phase of the seconds pulses was advanced by 20 milliseconds. NM = Not Measured.

New Products

Transistor Beta Tester

Siemens Edison Swan have announced a new low-priced battery-operated transistor tester.

Its purpose is to provide a quick run-ofthe-mill test on all p-n-p transistors; current gain and collector leakage being measured under common-emitter conditions.

Current gain (β or α') within a range 10–150 can be read directly on a dial by adjusting the control until an audible note just ceases. This measurement can be



carried out at a collector current of 0.5-4 mA, the set collector current being read on a meter.

Leakage current is measured on the meter at a fixed voltage of 9 V. Accuracy of measurement \pm 5% or \pm 5, whichever is the greater.

Siemens Edison Swan Ltd.,

155 Charing Cross Road, London, W.C.2.

Space '30' Analogue Computer

Solartron Electronic Group have announced the introduction of a new general-purpose analogue computer designed for the solution of linear and non-linear simultaneous or single differential equations.

It includes 30 operational amplifiers (with computing components), 60 coefficient potentiometers, 4 diode bridges, 4 relay amplifiers, 2 diode function generators, 4 servo multipliers, \pm 100-V 200-mA reference supply, a digital voltmeter (5 digit), 816-way detachable patch panel, control and monitoring panel with automatic timer, a.c. mains stabilizer and all the necessary power supplies.

All the computing passive elements incorporated are of 0.1% accuracy. Solartron Electronic Group Ltd.,

Thames Ditton, Surrey.

Pulse Monitoring Oscilloscope

Mullard Equipment Ltd. have introduced a new pulse monitoring oscilloscope with the exceptionally fast rise-time of 2 m μ sec, equivalent to a bandwidth of d.c. to 220 Mc/s.

The Instrument, type L362, has been designed for the display or measurement of



pulses between 3-mµsec and 3-µsec duration.

It has been developed from a design of the Atomic Energy Research Establishment, Harwell, and makes use of the sampling principle; the complete c.r.t. trace is builtup, as a low-frequency replica of the input, from a series of dots, each of which corresponds to a sample taken from successive repetitions of the input. A charge storage circuit maintains the position of a dot until the succeeding sample is taken.

Details from the makers' specification include:

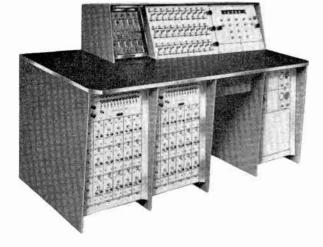
Y System	
Sensitivity	150 mV/cm.
Voltage measure-	
ment range	1·5–0–1·5 V.
Input impedance	1 kΩ, 2 pF approx.
Noise level	10 mV peak-to-peak at
	probe input.
X System	
Time-base ranges	0.03, 0.1, 0.3, 1 and
	3 μsec.
Calibration	By calibrated potentio-
•	meter scaled 0-1 and
	0–3.
Trigger pulse	
delay	$0.02-0.3 \mu \text{sec} \text{ and } 0.3-2$
	sec.
Number of samples	25, 50, 100 or 200
	approx.
P.r.f. limits	Approx. 50 c/s-10 kc/s.
The L362 is dis	tributed in the U.K. by

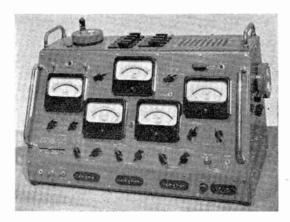
Research & Control Instruments Ltd., 207 King's Cross Road, London, W.C.1.

Valve Analyser and Bridge

The Metrix valve analyser type U-61B is designed for the accurate and detailed analysis of static characteristics of receiving and low-power transmitting valves. In addition, it can be used to obtain neon-tube regulation curves and thyratron control characteristics. Positive-grid characteristics may also be obtained.

Five meters indicate simultaneously: heater voltage, anode voltage, screen voltage, grid voltage and anode or screen current. Four separate stabilized voltage sources provide the necessary electrode voltages, all of which are variable and available for external use by means of sockets on the front panel. A series of adaptors each carrying one or two valve bases is supplied, these adaptors fit into nine jacks on the valve panel and are available fitted with any valve base. Between the voltage and pin selectors and the adaptor jacks, there are sockets and jumpers which





Electronic & Radio Engineer, September 1959

allow circuit elements to be interposed in the electrode circuits.

The instrument is fitted with a system of overload cut-outs which protect the d.c. sources of h.t. and the milliammeters in the event of an overload caused by faulty setting-up or a defective valve.

The valve bridge type 661 is designed for the measurement of the dynamic characteristics of valves; amplification factor, internal resistance and slope.

It is almost identical in appearance to the analyser U-61B, and the two instruments can be connected together by means of a cable provided to form a completely self-contained assembly for the measurement of all static and dynamic characteristics. With this arrangement, the d.c. supplies from the U-61B are used to obtain the accurate static operating conditions when taking dynamic measurements on the bridge.

Possible measurements include: amplification factor ranging from 0.01 to 1,000, internal resistance from 100Ω to $10 M\Omega$ and slope from 0.001 to 100 mA/V. The minimum accuracy is 5% for the resistance range and 2.5% for other characteristics.

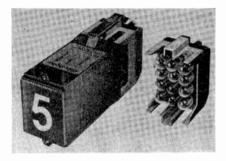
Manufactured by Compagnie Générale de Métrologie, France, these intruments are distributed in the U.K. by

Metrix Instruments Ltd.,

54 Victoria Road, Surbiton, Surrey.

Projection Type Indicator

Known as the Aldis Digilite Type Al00, this new unit provides display facilities for



figures 0 to 9 plus two decimal points, one left, one right.

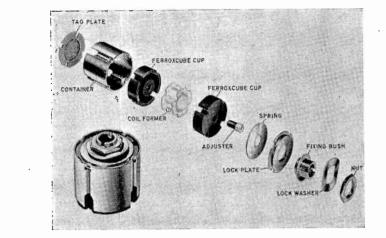
It comprises 12 lamps in a quick-release lamp housing and an optical lens system for projecting illuminated figures on to the front-viewing screen. Flush panel mounting gives an angle of view of 75° off axis in all directions. The height of the figures is $1\cdot 2$ in.

R. B. Pullin & Co. Ltd., Phoenix Works, Great West Road, Brentford, Middx.

Adjustable Ferrite Pot-Core Assemblies

Mullard has introduced a new range of adjustable ferrite pot-core assemblies known as 'Vinkors'.

They are made from a new grade of Ferroxcube material and incorporate an adjustable magnetic shunt which can vary



the inductance of an assembled coil $\pm 7\%$ with an accuracy of better than 2%.

The present range of 'Vinkors' comprises five types for use at frequencies up to 200 kc/s, with outside core diameters of 18, 21, 25, 30 and 35 mm respectively. Each size of core is available with an effective permeability of 160, 100 or 63.

Mullard Ltd.,

Torrington Place, London, W.C.1.

Spectrum Analysers

. 1.00

The new Polytechnic Series 860 spectrum analysers have been designed for precise spectrum measurements—evaluation of high v.s.w.r., leakage and loss; and analysis of radar, radio relay and other signals. Four



models are available, each with an accuracy of $\pm 0.8\%$ or ± 1 Mc/s, to cover the frequency ranges 2,400 to 3,400 Mc/s, 3,000 to 3,700 Mc/s, 5,100 to 5,900 Mc/s and 8,500 to 9,600 Mc/s.

The Polytechnic analyser is essentially a sensitive, continuously-scanning microwave receiver which resolves the spectrum of an r.f. signal and presents it on a 5-in. c.r.t. screen. A complete analyser consists of one or more r.f. heads, with an indicator unit which contains a narrow-band i.f. amplifier, video amplifier, sweep circuits, cathode-ray tube, metering circuits and power supplies.

The radio-frequency range is determined by the r.f. head, each of which contains a calibrated input attenuator with 100-dB range, a swept microwave local oscillator, a calibrated frequency meter and a crystal mixer. The local oscillator is swept in synchronism with the horizontal trace of the c.r.t. so that the spectrum amplitude is displayed as a function of frequency; the sweep speed is variable from 5 to 30 c/s. The sensitivity of each r.f. head is better than -80 dBm and the maximum resolution between two adjacent signals is 40 kc/s.

These instruments are manufactured by Polytechnic Research & Development Co., Inc., U.S.A. and are distributed in the U.K. through

Leland Instruments Ltd.,

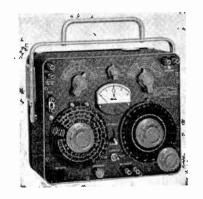
Abbey House, Victoria Street, London, S.W.1.

Impedance Bridge

Claude Lyons Ltd., U.K. distributors for General Radio Company, U.S.A., have announced the introduction of a new impedance bridge type 1650-A.

It is a general-purpose instrument designed for R, C, L and Q or D measurements. The bridge is complete with built-in transistorized 1-kc/s oscillator and selective detector and it incorporates the 'Orthonull' mechanism, which is a device to speed bridge-balance convergence when high-loss components are measured. The basic 'Orthonull' mechanism is a friction clutch that drives exponential variable-resistance arms making the normally electrically-interdependent RCL and QD adjustments independent by non-reciprocally ganging them.

When used with an external d.c. supply, the resistance range will measure a.c. and d.c. resistance values from $0.001 \ \Omega$ to $10 \ M\Omega$ with an accuracy of $\pm 1\% \pm$ $0.001 \ \Omega$. The capacitance range covers 1 pF to 1,000 μ F ($\pm 1\% \pm 1$ pF) and the inductance range 1 μ H to 1,000^t₁H ($\pm 1\%$



 \pm 1µH). The Q and D ranges measure a maximum of 1,000 and 50 respectively.

The carrying handle and protective face-plate cover combine to provide an adjustable-angle prop-stand for the bridge. Distributed in U.K. by

Claude Lyons Ltd., Valley Works,

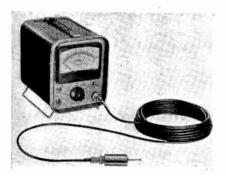
4-10 Ware Road, Hoddesdon, Herts.

Capacitance-Sensing Tachometer

Designed for the measurement of speed of rotating objects, this instrument can also be used for such applications as proximity measurement, timing and control of automatic processes and synchonization of fast-moving machinery.

Known as type CTM-1, it utilizes a capacitance probe which can be supplied with detachable end-pieces of various shapes, lengths and diameters.

In operation, the end-piece of the probe



is mounted near to, but not in contact with, any irregularity on the rotating part moving at the speed to be measured. The irregularity may be an indentation or a projection but must not be less than $\frac{1}{16}$ in. diameter \times $\frac{1}{16}$ in. deep. Each time the irregularity passes the end-piece of the probe, a capacitance change is produced. This develops a voltage pulse which is fed via a cable to the counting instrument, which may be as much as several hundred yards away from the **probe.**

Details from the makers' specification include:

Range	••	0 to 200,000 r.p.m. (6 ranges)
Accuracy		better than 2%.
Drift	••	less than 1% in any hour.
Stability	••	better than $\pm 0.5\%$ for \pm

10 V mains fluctuation. Power supply 200/250 V, 50 c/s.

Grunther Instruments Ltd.,

14 Oriental Street, London, E.14.

Time Calibrator Unit

A new version of their time calibrator unit has been announced by Cawkell Research & Electronics Ltd.

Known as type CU3A, it provides eight basic time-interval pulses which range from $0.5 \,\mu$ sec to 1 msec. Selection of the output is made by press-button switches and arrangements are made so that one, or any combination of the eight time intervals is available, in positive- or negative-going form, at one of the common output sockets.



The eight basic time interval pulses are also available from individual sockets mounted on the front panel of the instrument.

The markers are calibrated against an internal 2-Mc/s crystal-controlled oscillator and may be free-running or keyed from an external source.

Details from	the makers' data includes :
Accuracy	$\pm 0.05\%$ (when set agains
	internal crystal)
Amplitude	\pm 50 V
Pulse width	0.5 and $1 \mu sec$
Rise time	0·1 μsec.
Output loading	100 pF max.
Internal gate	-
amplitude	- 50 V peak max.
Synchronizing	-
signal	l V peak min.
Cawkell Research	& Electronics Ltd.,
Scotts Road, South	hall, Middx.

Solder Pins

Two new ranges of solder pins have been introduced by Harwin Engineers Ltd. to meet the 0.052-in. hole recommended in B.S.S. 3081/1959 and Defence Guide 5007. They are available for rivet or force-fit



assembly for either single- or double-ended connections.

The pins are turned from solid brass and are flow-tinned. Harwin Engineers Ltd.,

Rodney Road, Portsmouth, Hants.

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'L'-Band Signal Generator

Winston Electronics has recently announced a new generator which provides a source of c.w. or pulse-amplitude-



modulated power over the frequency range 800-2,100 Mc/s.

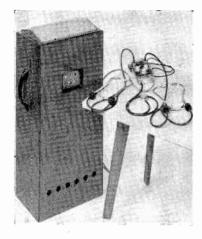
Known as type 957, it utilizes a single continuously - variable control which is directly calibrated to an accuracy of $\pm 1\%$. Frequency drift is less than 0.2% during the 'warm-up' period, after which it is approximately 0.003%/°C. The output power can be varied over the range 0 to -100 dB(relative to 1mW), by a directly-calibrated control. The output is taken via an 'N'-type connector which has an output impedance of 50 Ω at a v.s.w.r. not worse than 0.5. Modulation may be provided by: external pulses, the internal pulse generator or the internal generator synchronized by an external pulse or sine-wave generator at a rate of 40 to 4,000 c/s.

Other facilities include three calibrated controls for pulse width, pulse delay, pulse rate and two outputs for synchronization, one undelayed and the other delayed. *Winston Electronics Ltd.*, *Govett Avenue, Shepperton, Middx.*

Electronic Stethoscope

The Soniscope is an electronic stethoscope giving high gain in the audio range. It incorporates treble - and bass-frequency attenuators for the selection of required groups of frequencies in the sonic range.

The stethoscope consists of a miniature battery-operated valve amplifier, crystal



contact microphone and two sets of conventional earpieces. A special extension speaker is also available for use with the Soniscope. Faraday Electronic Instruments Ltd.,

65 Fairview Road, London, S.W.16.

Abstracts and References

COMPILED BY THE RADIO RESEARCH ORGANIZATION OF THE DEPARTMENT OF SCIENTIFIC AND INDUSTRIAL RESEARCH AND PUBLISHED BY ARRANGEMENT WITH THAT DEPARTMENT

The abstracts are classified in accordance with the Universal Decimal Classification. They are arranged within broad subject sections in the order of the U.D.C. numbers, except that notices of book reviews are placed at the ends of the sections. U.D.C. numbers marked with a dagger (†) must be regarded as provisional. The abbreviations of journal titles conform generally with the style of the World List of Scientific Periodicals. An Author and Subject Index to the abstracts is published annually; it includes a selected list of journals abstracted, the abbreviations of their titles and their publishers' addresses. Copies of articles or journals referred to are not available from Electronic & Radio Engineer. Application must be made to the individual publishers concerned.

					Page			Page
					A			A
Acoustics and Audio Frequencies		•••	••	•••	137	Measurements and Test Gear		148
Aerials and Transmission Lines	••			••	138	Other Applications of Radio and Electronics	• •	149
Automatic Computers	••	••	••	•••	139	Propagation of Waves	••	149
Circuits and Circuit Elements	••	••	••		139	Reception	••	150
General Physics	••	••	••	••	141	Stations and Communication Systems	••	15 0
Geophysical and Extraterrestrial	Pheno	mena			142	Subsidiary Apparatus	••	150
Location and Aids to Navigation	••	••	••		145	Television and Phototelegraphy	••	151
Materials and Subsidiary Techni	ques	••	••		145	Transmission		152
Mathematics	••	••	••	•••	148	Valves and Thermionics		152
Mis	cellane	ous	••	•••		 A 154		



534.001.5(51) 2808 Acoustics in China.—Ma Da-Yu. (Akust. Zh., Oct./Dec. 1958, Vol. 4, No. 4, pp. 373–375.) Outline of the development of research in China since 1949, in the fields of ultrasonics, architectural acoustics, electroacoustics, speech, musical acoustics and hearing.

534.213.4 2809 Attenuation of Plane Sound Waves of Finite Amplitude in Gases.—B. F. Podoshevnikov & B. D. Tartakovskii. (*Akust. Zh.*, Oct./Dec. 1958, Vol. 4, No. 4, pp. 369–371.) Investigation of the dependence of attenuation on sound intensity. A graph shows the distribution of sound pressure in a resonant aluminium tube at a frequency of 13 kc/s.

534.22-8-14 2810 The Propagation of Sound in Seawater.—A. V. J. Martin. (Ann. Géophys., Oct.—Dec. 1957, Vol. 13, No. 4, pp. 307– 309.) A brief description of laboratory experiments using an ultrasonic pulse technique to determine the velocity of sound in pure and salt water. See 1 of January.

534.22-8-14 2811 The Velocity of Ultrasound in Water near the Freezing Point.—N. F. Otpushchennikov. (Akust. Zh., Oct./Dec. 1958,

Electronic & Radio Engineer, September 1959

Vol. 4, No. 4, pp. 367-369.) Brief description of measurements made in distilled water at a frequency of 0.7 Mc/s in the temperature range + 20° to 0°C. Results indicate a velocity minimum at 0.7° C and a maximum adiabatic compression at + 2°C.

534.232-8-14: 537.228.2 2812 Electrostrictive Generation of Ultrasonics in Liquids.—E. Gerdes. (Naturwissenschaften, June 1958, Vol. 45, No. 12, pp. 280–281.) Preliminary report on measurements to determine the magnitude of electrode deformation due to Coulomb attraction. See e.g. 310 of 1956 (Goetz).

534.26 2813 Diffraction of Sound Waves in Converging Beams.—B. D. Tartakovskii. (Akust. Zh., Oct./Dec. 1958, Vol. 4, No. 4, pp. 355–360.) Approximate formulae are derived for the sound field near the focal point of a converging beam, characterized by a nonuniform amplitude distribution over the wave front and spherical aberration.

534.522.1

Measurements of Finite Amplitude Distortion of Progressive Ultrasonic Waves at Moderate Intensities.—K. L. Zankel & E. A. Hiedemann. (*Naturwis*senschaften, July 1958, Vol. 45, No. 14, pp. 329–330. In English.) Low-amplitude waves were investigated by measurements in water at 2 and 4 Mc/s, and in carbon tetrachloride at 2 and 3 Mc/s over a range of pressures and at various distances from the transducer.

2814

534.614-8

Measurement of Ultrasonic Wave Velocities and Elastic Moduli for Small Solid Specimens at High Temperatures. --H. J. McSkimin. (J. acoust. Soc. Amer., March 1959, Vol. 31, No. 3, pp. 287–295.) Data for fused silica and single-crystal Ge are listed for temperatures up to 300°C in illustration of the measurement methods described.

534.614-8-14 **Modification of Ultrasonic Inter ferometer Design.**—A. A. Isaev, I. G. Mikhaĭlov & A. S. Khimunin. (*Akust. Zh.*, Oct./Dec. 1958, Vol. 4, No. 4, pp. 363–364.) Note on the design of an improved quartz oscillator for use in interferometric measurements of sound velocity in liquids.

534.75 2817 Unpleasantness of Distorted Sounds : a Criterion derived from the Distortion Spectrum.—E. R. Wigan. (*Nature, Lond.*, 9th May, 1959, Vol. 183, No. 4671, p. 1320.) An objective criterion of 'unpleasantness' has been computed. Methods for checking it's validity are briefly discussed.

534.76:534.85 2818 Moving-Magnetic Stereo.—H. Horowitz. (Audio, May 1959, Vol. 43, No. 5, pp. 19-21..47.) A description of a pickup in which the stylus lever is attached to a magnet pivoted between the pole faces of two pairs of pickup coils. Characteristics are discussed.

534.78 : 621.39 **2819**

Intelligibility Evaluation of Voice Communications.-H. Schwarzlander.

(Electronics, 29th May 1959, Vol. 32, No. 22, pp. 88-91.) The integral of a difference voltage due to the pure speech signal and that passed through the system under test is used as a measure of intelligibility.

534.781:621.374.33

An Electronic Speech Sampler for Studying the Effect of Sample Duration on Articulation.—R. Fatchchand & R. Ahmed. (J. Instn Telecommun. Engrs, India, March 1959, Vol. 5, No. 2, pp. 86–88.) The start of any word is signalled by a pulse which itself operates the subsequent electronic delay and gate.

534.845

Panel Absorbents for Low-Frequency Sound Absorption.—N. K. D. Choudhury & M. V. S. S. K. Rao. (J. Instn Telecommun. Engrs, India, March 1959, Vol. 5, No. 2, pp. 103–108.) Resonant plywood panels show effective absorption in the range 75–300 c/s.

534.861:534.84

The Acoustic Design of Talks Studios and Listening Rooms.—C. L. S. Gilford. (Proc. Instn elect. Engrs, Part B, May 1959, Vol. 106, No. 27, pp. 245–256. Discussion, pp. 256–258.)

621.395.623.7.001.4 2823 The Impedance and Phase Angle of Loudspeaker Loads.—R. E. Cooke. (Muirhead Technique, April 1959, Vol. 13, No. 2, pp. 11–16.) A description of the basic measurement circuit and a discussion of the impedance and phase-angle characteristics obtained for moving-coil and e.s. loudspeaker systems.

621.395.623.8

Column Loudspeakers for Public-Address Systems.—M. L. Gayford. (*Electronics*, 12th June 1959, Vol. 32, No. 24, pp. 64–65.) The principles of design are briefly described, with particular reference to polar response.

621.395.625.3

A Regulator of Speed and Pitch for Sound Recordings.—A. M. Springer. (*Elektronische Rundschau*, Aug. 1958, Vol. 12, No. 8, pp. 275–276.) An adaptor unit for magnetic-tape recorders is described. This has a rotating assembly of four magnetic heads to provide independent changes of speed and pitch in recordings.

> AERIALS AND TRANSMISSION LINES

621.372.8

The Design and Testing of Integrally Constructed Waveguide Assemblies.— G. Craven & V. H. Knight. (*Proc. Instn elect. Engrs*, Part B, Vol. 106, No. 27, pp. 321–334.) A microwave-link repeater is described as an example of an assembly. Testing facilities include a plug-in reflectometer and a frequency-sweep reflection display.

621.372.8: 537.226

Dielectric Image Lines.—S. P. Schlesinger & D. D. King. (Trans. Inst. Radio Engrs, July 1958, Vol. MTT-6, No. 3, pp. 291–299. Abstract, Proc. Inst. Radio Engrs, Oct. 1958, Vol. 46, No. 10, p. 1777.)

621.372.821

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Measurement of the Properties of a Strip Line and its Transition Junction. —F. Norman. (*Proc. Instn Radio Engrs, Aust.*, Dec. 1958, Vol. 19, No. 12, pp. 788–795.) Measurements made in the range 8–11 cm λ indicate that a single modified TEM mode could be excited efficiently by means of a simple transition junction.

621.372.823

The Waveguide for Low-Loss Transmission.—K. Noda, A. Konose, T. Fujii & K. Miyauchi. (*Rep. elect. Commun. Lab.*, *Japan*, Oct. 1958, Vol. 6, No. 10, pp. 394– 400.) A report of measurements of attenuation in straight circular waveguides, and in serpentine and uniform bends propagating the H_{01} mode in circular and elliptic waveguides.

621.372.826

Launching Efficiency of Wires and Slots for a Dielectric Rod Waveguide.— R. H. DuHamel & J. W. Duncan. (*Trans. Inst. Radio Engrs*, July 1958, Vol. MTT-6, No. 3, pp. 277–284. Abstract, *Proc. Inst. Radio Engrs*, Oct. 1958, Vol. 46, No. 10, p. 1777.)

621.372.832.43 **Centre-Excited TE**°₁₀-**TE**°₀₁ **Mode Transducer.**—B. Oguchi &K. Yamaguchi. (*Ref. elect. Commun. Lab., Japan*, Oct. 1958, Vol. 6, No. 10, pp. 389–393.) Experimental data are given on the design and performance of a new type of mode transducer for use in the 24-kMc/s band.

621.372.832.8 2832 X Circulator.—S. Yoshida. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, p. 1150.) A new four-port waveguide circulator; experimental results are given.

621.372.837.2 2833 A New Form of High-Power Microwave Duplexer.—P. D. Lomer & R. M. O'Brien. (*Trans. Inst. Radio Engrs*, July 1958, Vol. MTT-6, No. 3, pp. 264–267. Abstract, *Proc. Inst. Radio Engrs*, Oct. 1958, Vol. 46, No. 10, p. 1776.)

621.372.837.3: 621.318.134 2834 A Fast Ferrite Switch for Use at 70 kMc/s.—E. H. Turner. (Trans. Inst. Radio Engrs, July 1958, Vol. MTT-6, No. 3, pp. 300–303. Abstract, Proc. Inst. Radio Engrs, Oct. 1958, Vol. 46, No. 10, p. 1777.)

621.372.837.3: 621.396.65 2835 A Faraday-Rotation Switch for the TH System.—J. A. Weiss. (Bell Lab. Rec., April 1959, Vol. 37, No. 4, pp. 139–143.) Description of a rapid-acting microwave switch based on the Faraday effect, designed for switching stand-by oscillators into service.

621.372.852.22

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A Perturbation Method for Circular Waveguides containing Ferrites.— P. J. B. Clarricoats. (Proc. Instn elect. Engrs, Part B, May 1959, Vol. 106, No. 27, pp. 335-340.) The propagation coefficient of a guide containing a longitudinally magnetized ferrite is derived. Good agreement is obtained with experimental data.

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621.372.852.22

A Phenomenological Theory of the Reggia-Spencer Phase Shifter.—J. A. Weiss. (*Proc. Inst. Radio Engrs*, June 1959, Vol. 47, No. 6, pp. 1130–1137.) Explains the essential properties of the device by means of a simplified model. See 387 of 1958 (Reggia & Spencer).

621.372.852.22 2838 Theory of the Mode Spectra of

Cylindrical Waveguides containing Gyromagnetic Media.—R. A. Waldron. (J. Brit. Instn Radio Engrs, June 1959, Vol. 19, No. 6, pp. 347–356.) The cut-off equations are derived and solved for the dielectric-centred case and the normal modes are studied. The relations between this case and that of the ferrite-centred case studied previously (341 of February) are pointed out.

621.372.852.323: 621.318.134 **Theoretical Analysis of the Operation of the Field-Displacement Ferrite Isola tor.**—K. J. Button. (*Trans. Inst. Radio Engrs*, July 1958, Vol. MTT-6, No. 3, pp. 303–308. Abstract, *Proc. Inst. Radio Engrs*, Oct. 1958, Vol. 46, No. 10, p. 1777.)

621.396.67.095 **2840** Four-Dimensional Electromagnetic Radiators.—H. E. Shanks & R. W. Bickmore. (*Canad. J. Phys.*, March 1959, Vol. 37, No. 3, pp. 263–275.) The effect of modulating one or more parameters of an aerial or aerial array, such as aperture dimensions, frequency or phase distribution, is discussed, and applications to multipattern operation, simultaneous scanning and sidelobe suppression are considered.

621.396.67.095:537.311.5 2841 Determination of a Current Distribution over a Cone Surface which will Produce a Prescribed Radiation Pattern. —H. Unz. (Trans. Inst. Radio Engrs, April 1958, Vol. AP-6, No. 2, pp. 182–186. Abstract, Proc. Inst. Radio Engrs, July 1958, Vol. 46, No. 7, p. 1439.)

621.396.674.31

The Effects of the Physical Parameters on the Bandwidth of a Folded Dipole.—J. F. German & F. E. Brooks, Jr. (*Trans. Inst. Radio Engrs*, April 1958, Vol. AP-6, No. 2, pp. 186–190. Abstract, *Proc. Inst. Radio Engrs*, July 1958, Vol. 46, No. 7, p. 1439.)

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621.396.674.33 The Characteristic Impedance of Two Infinite Cones of Arbitrary Cross-Section.—R. L. Carrel. (Trans. Inst. Radio Engrs, April 1958, Vol. AP-6, No. 2, pp. 197–201. Abstract, Proc. Inst. Radio Engrs, July 1958, Vol. 46, No. 7, p. 1439.)

621.396.677: 523.164: 621.318.57 2844 A Compact Antenna Switch for Scintillation Measurements.—W. D. Ryan. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, p. 1159.) This switch introduces a phase shift of 90° successively into the lines from each of two aerials.

621.396.677.029.63

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The Performance of Directive Aerials in Complex U.H.F. Fields.—J. A. Saxton & B. N. Harden. (*Proc. Instn elect. Engrs*, Part B, May 1959, Vol. 106, No. 27, pp. 315–317.) Apparent gains of directive aerials, relative to a half-wave dipole, were measured at 580 and 904 Mc/s on a number of urban and rural sites. The median gains were similar to the calculated plane-wave gains, but the apparent gain was low, owing to the complexity of the field, on a significant number of sites.

621.396.677.3: 523.164.32 2846 A New High-Resolution Interferometer for Solar Studies.—Kundu. (See 2936.)

621.396.677.3 : 621.396.965 **2847 A Note on the Effective Aperture of Electrically Scanned Arrays.**—R. W. Bickmore. (*Trans. Inst. Radio Engrs*, April 1958, Vol. AP-6, No. 2, pp. 194–196. Abstract, *Proc. Inst. Radio Engrs*, July 1958, Vol. 46, No. 7, p. 1439.)

621.396.677.32 2848 The Radiation Characteristics of a Zig-Zag Antenna.—D.L. Sengupta. (*Trans. Inst. Radio Engrs*, April 1958, Vol. AP-6, No. 2, pp. 191–194. Abstract, *Proc. Inst. Radio Engrs*, July 1958, Vol. 46, No. 7, p. 1439.)

621.396.677.71 **Design Data for Small Annular Slot Antennas.**—W. A. Curming & M. Cormier. (*Trans. Inst. Radio Engrs*, April 1958, Vol. AP-6, No. 2, pp. 210–211. Abstract, *Proc. Inst. Radio Engrs*, July 1958, Vol. 46, No. 7, p. 1439.)

621.396.677.75 2850 Hemi-isotropic Radiators for the S or X Band.—E. G. A. Goodall. (Proc. Instn elect. Engrs, Part B, May 1959, Vol. 106, No. 27, pp. 318–320.) "An aerial having approximate hemi-isotropic properties has been constructed on the principle that a dielectric rod will act as a guiding medium for electromagnetic energy. Using this principle, a broad-band, shaped dielectric element has been developed, which, when placed at the aperture of an openended circular waveguide, radiates with hemi-isotropic cover over a 20% frequency band."

621.396.677.81: 621.397.7 2851 The Passive TV Relay and its Practical Possibilities.—R. Aschen. (*TSF et TV*, Nov. 1957, Vol. 33, No. 349, pp. 329–330.) Field strength and aerial gain calculations for typical passive relay systems comprising a coupled receiving and transmitting aerial are given. See also 2852 below.

Electronic & Radio Engineer, September 1959

621.396.677.83

Passive Relay by Microwave Mirror. --R. Aschen. (*TSF et TV*, Jan. 1958, Vol. 33, No. 351, pp. 5-7.) Formulae are given for calculating the mirror area and reflection losses for a typical relay circuit based on a received field strength of 2 mV/m at a frequency of 200 Mc/s.

621.396.677.83

A Log-Periodic Reflector Feed.—D. E. Isbell. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1152–1153.) An aerial of the log-periodic reflector type has been constructed which has been used over the range 105–430 Mc/s. Its effective aperture is fairly constant below 325 Mc/s.

621.396.677.85 **2854** Microwave Stepped-Index Luneberg Lenses.—G. D. M. Peeler & H. P. Coleman. (*Trans. Inst. Radio Engrs*, April 1958, Vol. AP-6, No. 2, pp. 202–297. Abstract, *Proc. Inst. Radio Engrs*, July 1958, Vol. 46, No. 7, p. 1439.)

AUTOMATIC COMPUTERS

681.142

The Design of a Standard Block for a Digital Computing System.—R. J. Miles. (*Mullard tech. Commun.*, April 1959, Vol. 4, No. 38, pp. 222–248.) Logical theory, design considerations and practical circuit of a block based on alloy-junction transistors operating at frequencies up to 1 Mc/s.

681.142 2856 Binary Multiplication in Digital Computers.—A. Green. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1159–1160.) Shows how many steps can be eliminated from the usual process of multiplication by computer.

681.142 2857 Computation of Sin N, Cos N and $m\sqrt{N}$ using an Electronic Computer. -E. G. Kogbetliantz. (*IBM J. Res. Developm.*, April 1959, Vol. 3, No. 2, pp. 147-152.)

681,142

Rotating-Disk Function Generator for Analogue Computers.—M. E. Young, W. M. Alexander & H. D. Schwetman. (*Rev. sci. Instrum.*, May 1959, Vol. 30, No. 5, pp. 318–322.) A variable-radius revolving lamina modulates the light incident upon the cathode of a photomultiplier tube to produce a required voltage/time function.

681.142:518.4 **2859 A Design for an Automatic Graph Plotter.**—M. P. Atkinson, W. T. Bane & D. L. A. Barber. (*Proc. Instn elect. Engrs*, Part B, May 1959, Vol. 106, No. 27, pp. 299–306.) Transistors and printed circuits are used in equipment based on digital techniques. Points may be plotted at a rate of three per second, with an accuracy within 0.01 in.

681.142 : 621.318.042

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Magnetic-Core Matrices for Logical Functions.—A. L. Freedman. (*Electronic* Engng, June 1959, Vol. 31, No. 376, pp. 358–361.) Some applications of cores having a square hysteresis loop.

681.142:621.318.57 **2861 The Design of Biased-Diode Function Generators.**—C. C. Ritchie & R. W. Young. (*Electronic Engng*, June 1959, Vol. 31, No. 376, pp. 347–351.) Relations between the number and spacing of diode

sections to give minimum error are derived.



621.3.049.7

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Recent Advances in Potted and Printed Circuits.—H. G. Manfield (J. Brit. Instn Radio Engrs, May 1959, Vol. 19, No. 5, pp. 289–302.) "The various potting resins are described in relation to the variation of properties with different proportions of hardener and the effects on the parameters of the potted components. The causes of failure of potted circuits are discussed. Design problems in the use of printed circuits are examined with particular reference to questions of conductor thickness and spacing. A method of sealing printed circuits by a thin polysulphide rubber layer which is sprayed or brushed on is described."

621.3.049.7 : 621.385.1

Thermionic Integrated-Micromodules.—J. E. Beggs, W. Grattidge, P. J. Molenda, A. P. Haase & A. F. Dickerson. (*Electronics*, 15th May 1959, Vol. 32, No. 20, pp. 80..83.) The construction and application of microminiature heaterless valves, resistors and capacitors using titanium and ceramic materials are described.

621.318.57 : 537.227 **2864**

The Transpolarizer: an Electrostatically Controlled Circuit Impedance with Stored Setting.—C. F. Pulvari. (*Proc. Inst. Radio Engrs*, June 1959, Vol. 47, No. 6, pp. 1117–1123.) The device operates by the controlled transfer of polarization through two or more ferroelectric dielectric sections in series.

621.318.57 : 621-52 **2865**

An Electronic Timer with Voltage Control of Setting.—R. Gladstone. (*Electronic Engng*, June 1959, Vol. 31, No. 376, pp. 362–363.) A new grid-controlled 'bootstrap' circuit with common-cathode trigger provides accurately controlled time delays up to about 100 seconds.

621.318.57 : 621.314.63 **2866**

Microwave Switching by Crystal Diodes.—M. R. Millet. (Trans. Inst. Radio Engrs, July 1958, Vol. MTT-6, No. 3, pp. 284–290. Abstract, Proc. Inst. Radio Engrs, Oct. 1958, Vol. 46, No. 10, p. 1777.)

621.319.4 : 621.3.049.75

Tantalum Printed Capacitors.— R. W. Berry & D. J. Sloan. (*Proc. Inst. Radio Engrs*, June 1959, Vol. 47, No. 6, pp. 1070–1075.) Description of the structural features and characteristics of capacitors using sputtered Ta films as the base for the anodized oxide film, with evaporated metal counter-electrodes.

621.319.45:669.718.5

The Surface Enlargement of Aluminium for Electrolytic Capacitors. —P. Werner. (*Nachr Tech.*, June 1958, Vol. 8, No. 6, pp. 269–277.) Various chemical and electrochemical methods are described and compared, and details are given of a method of measuring the increase in surface area achieved.

621.372.5

General Solution of the Symmetric Iterative Analysis of Asymmetric Passive Linear Quadripoles.—S. Mayr. (Arch. Elektrotech., 8th Dec. 1958, Vol. 44, No. 2, pp. 120–129.) The asymmetric quadripole is divided into two symmetric quadripole sections which can be treated by iterative matrix methods.

621.372.57: 621.3.087.4: 551.594.6 2870 Investigation of an Apparatus for Recording Atmospherics.—R. Benoit & J. Kernevez. (Ann. Geophys., Oct./Dec. 1957, Vol. 13, No. 4, pp. 321–324.) An analysis of an integrating circuit with a long time-constant and its response to a series of pulses.

621.372.6

A Topological Nonreciprocal Network Element.—A. W. Keen. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1148–1150.) The element is a threeterminal device which may be used with physical elements (immittances) to model the more complex nonreciprocal devices.

621.372.6 **2872** Traditors, a New Class of Nonenergic Nonlinear Network Elements. --S. Duinker. (*Philips Res. Rep.*, Feb. 1959, Vol. 14, No. 1, pp. 29-51.) From an analysis based on the Lagrangian dynamical equations a class of nonlinear multiport elements is defined, which are characterized by the property of neither dissipating nor storing but only transferring energy.

621.372.632 : 621.314.63

Transmitting Frequency Converter in which Gold- or Silver-Bonded Diode is Used.—Kita, Sanpei & Okajima. (See 3145.)

621.372.632.029.6 2874 One Aspect of Minimum-Noise-Figure Microwave Mixer Design.— S. M. Bergmann. (*Trans. Inst. Radio Engrs*, July 1958, Vol. MTT-6, No. 3, pp. 324– 326. Abstract, *Proc. Inst. Radio Engrs*, Oct. 1958, Vol. 46, No. 10, p. 1777.)

621.373 : 537.312.62 **2875** A Cryogenic Oscillator.—G. B. Rosenberger. (*IBM J. Res. Developm.*, April 1959, Vol. 3, No. 2, pp. 189–190.) A relaxation process based on the transition between the superconducting and conducting phases of a Pb film is described. Oscillations at frequencies around 100 kc/s have been obtained.

621.373.42.029.422

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A Sine-Wave Generator with Periods of Hours.—G. Klein & J. M. den Hertog. (*Electronic Engng*, June 1959, Vol. 31, No. 376, pp. 320–325.) An 'inverse function generator' based on the difference amplifier [see e.g. 362 of 1956 (Klein)] is examined and examples of its use are considered, (a) in a logarithmic voltmeter, and (b) for sine-triangle waveform transformation. Triangle-sine transformation can be achieved by negative feed-back; a v.l.f. triangular waveform obtained from a CRcircuit and relay is thus converted to an accurate sine wave without transients.

621.373.43 : 621.314.7 : 621.385.1 **2877**

Tube-Transistor Hybrids Provide Design Economy.—G. A. Dunn & N. C. Hekimian. (*Electronics*, 5th June 1959, Vol. 32, No. 23, pp. 68–70.) A bistable cathode follower and four-stage ring counter are described. The transistors appear in the cathode circuits of the valves.

621.373.52

Physical Principles of Avalanche-Transistor Pulse Circuits .- D. J. Hamilton, J. F. Gibbons & W. Shockley. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1102–1108.) "A model for the transistor is defined in terms of charge variables and the physical parameters of the device. The transient performance of the model is calculated by focusing attention on the minority-carrier charge stored in the base region and the influence of base-width modulation upon this stored charge. In the charge formulation of the problem, the physical details of the avalanche multiplication process need not be considered; multiplication is accounted for by the boundary conditions which it imposes upon the stored charge. Good agreement has been obtained between calculated and experimentally observed data for a simple avalanche-transistor relaxation oscillator."

621.374.3: 621.387.4 **2879 Time to Pulse-Height Converter.**— J. V. Kane. (*Rev. sci. Instrum.*, May 1959, Vol. 30, No. 5, pp. 374–375.) A circuit is

Vol. 30, No. 5, pp. 374–375.) A circuit is described for deriving pulses the amplitudes of which decrease linearly with time.

621.374.3: 621.387.4 **2880** Linear Gate of 20-mµs Duration.— E. L. Garwin. (*Rev. sci. Instrum.*, May 1959, Vol. 30, No. 5, pp. 373–374.) Diodes with a 6 mµs recovery time are used in a coincidence circuit.

621.374.5 : 538.652

A Torsional Magnetostrictive Delay Line.—A. Rothbart. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1153–1154.) An application of the Wiedemann effect, using toroidal coil transducers.

621.375.018.75 : 537.311.33

Pulse Amplification using Impact Ionization in Germanium.—M. C. Steele, L. Pensak & R. D. Gold. (*Proc. Inst. Radio Engrs*, June 1959, Vol. 47, No. 6, pp. 1109–1117.) Some aspects of the phenomena of impact ionization in an impurity-doped semiconductor at $4 \cdot 2$ °K are described. Control of the breakdown process is used to obtain pulse amplification in the millimicrosecond range, using two- and threeterminal devices.

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621.375.2.029.3

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Reducing Distortion in Class-B Amplifiers.—B. Sklar. (*Electronics*, 22nd May 1959, Vol. 32, No. 21, pp. 54–56.) Linearization is accomplished by a nonlinear compensation network containing diodes. The calculations for an a.f. amplifier with 2.6% distortion are described.

621.375.232.4 2884 Grounded-Grid Power Amplifier Design.—J. L. Dautremont, Jr. (*Electronic Equipm. Engng*, Dec. 1958, Vol. 6, No. 12, pp. 33–36.) A graphical design procedure is described, using a disk-seal valve Type

 2C39-A as an example.

 621.375.4.029.3
 2885

 Single-Ended Amplifiers for Class-B

 Operation.—H. C. Lin & B. H. White.

 (Electronics, 29th May 1959, Vol. 32, No. 22,

(Electronics, 29th May 1959, Vol. 32, No. 22, pp. 86–87.) A transistorized 10-W high-fidelity push-pull amplifier is described in detail.

621.375.4.029.3

Designing High-Quality A.F. Transistor Amplifiers.—R. Minton. (*Elec*tronics, 12th June 1959, Vol. 32, No. 24, pp. 60–61.) A seven-stage 25-W amplifier is described.

621.375.4.029.3 2887 One-Transistor 'Push-Pull'.--J. A.

Worcester. (*Electronics*, 12th June 1959, Vol. 32, No. 24, p. 74.) An a.f. output stage in which the biasing condition is controlled by the rectified output.

621.375.9: 538.569.4 **2888 Molecular Oscillators and Amplifiers.**—N. G. Basov & A. M. Prokhorov. (*Priroda, Mosk.*, July 1958, No. 7, pp. 24–32.) The principle and operation of molecularbeam oscillators and amplifiers are described with reference to the ammonia-beam maser. Molecular amplifiers based on paramagnetic crystals give a wider pass-band and a higher output power than the molecularbeam type. The frequency stability achieved is within one part in 10⁹.

621.375.9: 538.569.4 **2889 Zero-Field Masers.**—G. S. Bogle & H. F. Symmons. (*Aust. J. Phys.*, March 1959, Vol. 12, No. 1, pp. 1–20.) "Solid state three-level masers operating with zero magnetic field are shown to be feasible and to have advantages over magnetic field masers in many applications. The requirements of the working substance are discussed and it is found that compounds of Cr²⁺, Fe³⁺, Ni²⁺, and Gd³⁺ should be suitable. Diagrams and tables of maser properties of selected compounds are given; on the basis of present knowledge a number of amplifying frequencies between 120 and 75 000 Mc/s should be available. The range of suitable compounds which has been studied is very small, and should be extended."

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2891

Role of Double-Quantum Transitions in Masers.—S. Yatsiv. (*Phys. Rev.*, 15th March 1959, Vol. 113, No. 6, pp. 1538–1544.) Conditions are found in which the operation of a three-level maser is governed by the double-quantum process and does nor require a true 'pumping' stage. Such a case, although realizable in practice, may be of doubtful technical applicability.

621.375.9 : 538.569.4

Travelling-Wave Solid-State Masers. —A. E. Siegman, P. N. Butcher, J. C. Cromack & W. S. C. Chang. (Proc. Instn elect. Engrs, Part B, 1958, Vol. 105, Supplement No. 11, pp. 711–712. Discussion.)

621.375.9: 538.569.4: 523.164 2892 A Maser Amplifier for Radio Astronomy at X Band.-J. A. Giordmaine, L. E. Alsop, C. H. Mayer & C. H. Townes. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1062-1069.) "The design and operating characteristics of a maser radiometer for use in radio astronomy at 3-cm wavelength are discussed. The operating system which is described has a bandwidth of 5.5 Mc/s and an input noise temperature, including background radiation into the antenna, of about 85° K. An r.m.s. fluctuation level of about 0.04° K is attained using an averaging time of 5 seconds. A discussion of the factors determining the sensitivity of such devices is presented."

621.375.9: 538.569.4: 538.222 2894 Theory of Three-Level Paramagnetic Masers.—P. N. Butcher. (Proc. Instn elect. Engrs, Part B, 1958, Vol. 105, Supple-

ment No. 11, pp. 684–711.) Part 1—Quantum Theory (pp. 684–690).

Part 2-Amplification and Oscillation (pp. 691-698).

Part 3—Output Noise Power Spectrum (pp. 699–704).

Part 4—Noise Figure (pp. 705–709). Discussion (pp. 709–711).

Discussion (pp. 703–711):

621.375.9 : 550.389.2 : 629.19

Parametric Amplifier Receives Space Signals.—(*Electronics*, 5th June 1959, Vol. 32, No. 23, pp. 80–81.) Signal amplification was in L band and pump frequency in X band giving a noise factor of 1 dB and bandwidth 100 kc/s. Using a 32-dB paraboloid (diameter 18 feet) the fraction of a watt radiated by Pioneer IV was received at 410 000 miles.

621.375.9:621.3.011.23

Microwave Parametric Amplifiers and Convertors.—G. Wade & H. Heffner. (Proc. Instn elect. Engrs, Part B, 1958, Vol. 105, Supplement No. 11, pp. 677–679.) The inherent gain, noise and bandwidth characteristics of basic circuits are discussed and a brief description is given of a laddernetwork converter in which the output frequency is higher than the pumping frequency.

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621.375.9:621.3.011.23

Circuit Conditions for Parametric Amplification.—J. E. Pallett. (J. Electronics Control, March 1959, Vol. 6, No. 3, pp. 261–262.) Correction of an error in Valdes' paper (75 of January).

621.376.23

Simplified Product Detector Design. —J. L. Ekstrom. (QST, May 1959, Vol. 43, No. 5, p. 43.) A circuit is described for a pentagrid converter which may be self-excited or separately excited and which has an inter-modulation balance adjustment to reduce rectification effects.

621.376.4 **2899 The Modulator as a Phase Detector.** —W. Frazer & R. E. Schemel. (*Electronic Engng*, June 1959, Vol. 31, No. 376, pp. 345–346.) A note on the error due to a finite switching voltage applied to a shunt modulator.

GENERAL PHYSICS

535.13

Solution of Maxwell's Equations in Terms of a Spinor Notation: the Direct and Inverse Problem.—H. E. Moses. (*Phys. Rev.*, 15th March 1959, Vol. 113, No. 6, pp. 1670–1679.) The use of spinor notation enables the solution to be obtained in more compact form than does vector notation.

537.226

2895

The Quantum Mechanical Theory of the Dielectric Orientation Polarization of Gases: Part 1—The Static Orientation Polarization of a Dipole Gas consisting of Symmetric Spin Molecules.—W. Maier & H. K. Wimmel. (Z. Phys., 5th Dec. 1958, Vol. 153, No. 3, pp. 297-313.)

537.311.1: 621.396.822
2902
Noise Theory for Hot Electrons.—
P. J. Price. (IBM, J. Res. Developm.,
April 1959, Vol. 3, No. 2, pp. 191–193.)
Nyquist's theorem is extended to the case in which the distribution of electrons is disturbed by a steady electric field.

 537.311.4
 2903

 Transient Behaviour of the Ohmic
 Contact....M. A. Lampert & A. Rose.

 (Phys. Rev., 1st March 1959, Vol. 113, No.
 5, pp. 1236–1239.)

ohmic injecting contacts is analysed for transient currents at a fixed voltage. These occur when the free-carrier density in the solid is changed by some exciting agent as in photoconductivity or bombardmentinduced conductivity.

537.311.5: 538.566 2904 The Calculation of the Field in a Homogeneous Conductor with a Wavy Interface.—J. R. Wait. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1155–1156.) Analysis showing that the perturbation of an e.m. field in the conductor due to the ripples is proportional to their amplitude.

537.311.5: 621.3.015.3 2905 Penetration of Transient Electromagnetic Fields into a Conductor.—A. Grumet. (*J. appl. Phys.*, May 1959, Vol. 30, No. 5, pp. 682–686.) Theory for a uniform electric field abruptly applied to a plane boundary.

537.322.1 2906 On the Theory of the Peltier Heat Pump.—E. S. Rittner. (*J. appl. Phys.*, May 1959, Vol. 30, No. 5, pp. 702–707.) The figure of merit for a single-stage pump is optimized in the region of partial Fermi degeneracy.

537.527: 537.56 2907 The Space - Charge Field - Emission Hypothesis applied to Hayashi Data on Discharges through Gases.—H. Ritow. (J. Electronics Control, March 1959, Vol. 6, No. 3, pp. 236–245.)

537.533 2908 Concerning the Nature of the Aberrations in Electron Sheet Beams.— W. E. Waters. (J. opt. Soc. Amer., March 1959, Vol. 49, No. 3, pp. 304–307.) A power-series expansion is used to derive expressions for the aberrations up to the third order in electron sheet beams subject to purely electrostatic focusing. Four purely geometric aberrations and four aberrations due to chromatic effects are found.

537.542 2909 New Hollow-Cathole Glow Discharge.—A. D. White. (*J. appl. Phys.*, May 1959, Vol. 30, No. 5, pp. 711–719.) Current densities of 0.5 A/cm² can be obtained with a cathode consisting of a refractory metal with a spherical cavity. In neon, stable characteristics at a few milliamperes are obtained.

537.56 : 538.56 2910 New Experimental Results for Plasma Electron Oscillations.—D. W. Mahaffey. (J. Electronics Control, March 1959, Vol. 6, No. 3, pp. 193–203.) Study of oscillations in low-pressure mercury vapour discharges with plane oxide-coated cathodes.

537.56: 538.56 **A Lagrangian Formulation of the Boltzmann-Vlasov Equation for Plasmas.**—F. E. Low. (*Proc. roy. Soc. A*, 11th Nov. 1958, Vol. 248, No. 1253, pp. 282–287.) A variational principle is found which leads to a new formulation of the problem of small oscillations about equilibrium.

537.581

Wave-Mechanical Correction of the Richardson-Dushman Emission Formula.—F. Ollendorff. (Arch. Elektrotech., 12th Feb. 1959, Vol. 44, No. 3, pp. 177–188.) An attempt is made to overcome the discrepancies between the spin-corrected theory of thermionic electron emission and empirical results.

538.1

Bose-Einstein Lattice Gases equivalent to the Heisenberg Model of Ferro-, Antiferro- and Ferri-Magnetism. —T. Morita. (Progr. theor. Phys., Nov. 1958, Vol. 20, No. 5, pp. 614-624.) A Hamiltonian is presented that has the form of a finite series of Bose operators and is equivalent to the Heisenberg model. See also *ibid.*, pp. 728-736.

538.3 : 535.13 Formation of Discontinuities in Classical Nonlinear Electrodynamics. --M. Lutzky & J. S. Toll. (*Phys. Rev.*, 15th March 1959, Vol. 113, No. 6, pp. 1649-1652.)

538.566

Polarization and Angle Dependence of the Reflection Factor of Absorbers for Centimetre Electromagnetic Waves. --K. Walther. (Z. angew. Phys., June 1958, Vol. 10, No. 6, pp. 285–295.) The dependence of the reflection factor on the angle of incidence and plane of polarization of e.m. waves is investigated for various types of absorbers and results are confirmed experimentally.

538,566

Transients in Conducting Media.— P. I. Richards. (Trans. Inst. Radio Engrs, April 1958, Vol. AP-6, No. 2, pp. 178–182. Abstract, Proc. Inst. Radio Engrs, July 1958, Vol. 46, No. 7, p. 1439.)

538.566 : 535.42] + 534.26 **2917 The Effect of Incident Wave Fluctua tions on the Mean Intensity Distribu tion near the Focal Point of a Lens.**--M. N. Krom & L. A. Chernov. (Akust. Zh., Oct./Dec. 1958, Vol. 4, No. 4, pp. 341–347.) An extension of Chernov's analysis (3772 of 1958) to the case of fluctuations of arbitrary amplitude.

538.566 : 535.42 **2918 The Kirchhoff-Young Theory of the Diffraction of Electromagnetic Waves.** --O. Laporte & J. Meixner. (*Z. Phys.*, 14th Nov. 1958, Vol. 153, No. 2, pp. 129-148.) A transformation is discussed which facilitates the evaluation of Kirchhoff's double integrals.

538.566: 535.43] + 534.26 **On Propagation of Waves in Slightly Rough Ducts.**—J. C. Samuels. (*J. acoust. Soc. Amer.*, March 1959, Vol. 31, No. 3, pp. 319–325.) Mathematical treatment of acoustic and e.m. wave propagation assuming that the heights of the roughness peaks are small compared to the average separation of the duct walls.

538.566.2

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The Propagation of a Variable Electromagnetic Field in a Stratified Anisotropic Medium.—A. N. Tikhonov. (*Dokl. Ak. Nauk S.S.S.R.*, 11th June 1959, Vol. 126, No. 5, pp. 967–970.) Computation of the field on the surface of an anisotropic conducting medium due to a dipole lying in the surface. See also 3036 of 1956 (Tikhonov & Shakhsuvarov).

538.566.2:548 **2921 On the Propagation of Electromagnetic Waves in a Medium with Appreciable Spatial Dispersion.**—V. M. Agranovich & A. A. Rukhadze. (*Zh. eksp. teor. Fiz.*, Oct. 1958, Vol. 35, No. 4(10), pp. 982– 984.) Brief description of a method more detailed then that of Ginzburg (1169 of April), in which expansions are obtained for 'direct' and 'inverse' dispersion. It is shown that in cubic crystals inclusion of the spatial dispersion leads to a weak anisotropy of the index of refraction.

538.569.4 2922 A General Theory of Magnetic Double Resonance.—K. Tomita. (Progr.theor.Phys., Nov. 1958, Vol. 20, No. 5, pp. 743–773.) The theory describes a system consisting of two interacting different species of spin, one being saturated by a strong resonant radiation field and the other being detected by a weak field. See also 95 of January.

538.569.4 2923 Multiple-Quantum Transitions in Nuclear Magnetic Resonance.—S. Yatsiv. (*Phys. Rev.*, 15th March 1959, Vol. 113, No. 6, pp. 1522–1537.)

538.569.4 2924 The Application of Magnetic Resonance to Solid-State Electronics.—D. J. E. Ingram. (J. Brit. Instin Radio Engrs, June 1959, Vol. 19, No. 6, pp. 357–367.) A description of the basic principles and techniques and an outline of some recent applications.

538.569.4 2925 Excitation of Spin Waves in an Antiferromagnet by a Uniform R.F. Field. —R. Orbach & P. Pincus. (*Phys. Rev.*, 1st March 1959, Vol. 113, No. 5, pp. 1213–1215.) It is possible to excite spin waves in an antiferromagnet by a uniform r.f. field provided that spins on the surface of the specimen experience anisotropy interactions different from those acting on spins in the interior.

538.569.4 2926 Exchange Effects in Ferromagnetic Resonance.—M. A. Gintsburg. (Zh. eksp. teor. Fiz., Oct. 1958, Vol. 35, No. 4(10), pp. 1047–1049.) A single dispersion law for transverse e.m. waves and for spin waves is derived which takes account of both relativistic and exchange interactions.

538.569.4: 538.222 Paramagnetic Electron-Resonance Induction.—E. Lutze & D. Bösnecker. (*Naturwissenschaften*, July 1958, Vol. 45, No. 14, p. 332.) Preliminary note on investigations of induced emission at paramagnetic resonance. $CuSO_4 \cdot 5H_2O$ was used at room temperature and a wavelength of $3 \cdot 33$ cm.

538.569.4:621.318.132 **Ferrimagnetic Resonance Modes in Spheres.**—P. C. Fletcher & R. O. Bell. (*J. appl. Phys.*, May 1959, Vol. 30, No. 5, pp. 687–698.) The magnetostatic solutions of ferrimagnetic resonance in ferrite spheres are briefly derived. Some experimental results are compared with the theory.

	538.569.4 : 621.375.9	2929
	Role of Double-Q	antum Transitions
•	in MasersYatsiv.	(See 2890.)

538.652

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Form Effect in Linear Magnetostriction.—H. E. Stauss. (J. appl. Phys., May 1959, Vol. 30, No. 5, pp. 698–701.)

539.2 Electron Interaction in Solids. Characteristic Energy Loss Spectrum.—P. Nozières & D. Pines. (*Phys. Rev.*, 1st March 1959, Vol. 113, No. 5, pp. 1254–1267.) The characteristic energy loss spectrum is analysed with the aid of the dielectric formulation of the many-body problem.

GEOPHYSICAL AND EXTRATERRESTRIAL PHENOMENA

523.164 : 621.396.677.8

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Improved Measurements of the Positions of 17 Intense Radio Stars.—B. Elsmore. (Mon. Not. R. astr. Soc., 1958, Vol. 118, No. 6, pp. 603–608.) Observations have been made at $1.9 \text{ m} \lambda$, using the Cambridge radio telescope as a crossed-axis interferometer. See also 103 of January (Edge et al.).

523.164.32 The Extension of Solar Radio Spectroscopy to Decametre Wavelengths... K. V. Sheridan, G. H. Trent & J. P. Wild. (Observatory, April 1959, Vol. 79, No. 909, pp. 51-53.) Preliminary report on spectrographic investigations in the frequency range 24-40 Mc/s.

2934 523.164.32 On Short Periodic Variations in Solar Noise Storms on 200 Mc/s.—Ø. Hauge. (Astrophys. norveg., Jan. 1958, Vol. 6, No. 5, pp. 43-54.) 19 days of enhanced solar radiation on 200 Mc/s in June, July and August 1955 are investigated by an autocorrelation method in a search for short periodic variations with repetition times between 7.5 and 90 min. Results indicate that some noise storms are characterized by periodic variations with repetition times differing from day to day, while other noise storms exhibit no periodic variations. It is possible that a specific noise storm area retains its characteristics of short periodic variations in radio emission for a solar rotation or longer.

523.164.32

2935

On the Fine Structure of Solar Bursts in the 200-Mc/s Range and their Drift in Frequency.—Ø. Elgarøy. (Astrophys. norveg., Jan. 1958, Vol. 6, No. 6, pp. 55-74.) High-speed records have been obtained simultaneously on 199 Mc/s and 200.5 Mc/s with a twin-channel receiver at the Harestua Solar Observatory during the period February-September 1957. An analysis of the records shows that 48 % of the bursts occur first on the lower frequency, 34 % first on the higher frequency and 18% simultaneously. The results are discussed and the receiving equipment is described.

523.164.32 : 621.396.677.3 2936 A New High-Resolution Interferometer for Solar Studies .- M. R. Kundu. (J. Instn Telecommun. Engrs, India., March 1959, Vol. 5, No. 2, pp. 77-85.) The device is essentially a two-element interferometer with the two aerials aligned equatorially which permits use far from the median plane and gives a resolving power of the order of 1'. See 2733 of 1957 (Alon et al.).

523.164.4

2937

A High-Resolution Survey of the Andromeda Nebula at 408 Mc/s.-M. I. Large, D. S. Mathewson & C. G. T. Haslam. (Nature, Lond., 2nd May 1959, Vol. 183, No. 4670, pp. 1250-1251.) A report of observations made with the Jodrell Bank radio telescope.

523,164.4

2938 A High-Resolution Survey of the Coma Cluster of Galaxies at 408 Mc/s. -M. I. Large, D. S. Mathewson & C. G. T. Haslam. (Nature, Lond., 13th June 1959, Vol. 183, No. 4676, pp. 1663-1664.)

523.164.4: 621.396.11: 523.755 2939 The Scattering of Radio Waves in the Solar Corona.—A. Hewish. (Mon. Not. R. astr. Soc., 1958, Vol. 118, No. 6, pp. 534-546.) An account is given of measurements carried out each June during the period 1952-1958 of the radio emission from the Crab nebula at wavelengths of 7.9, 3.7 and 1.9 m. Results indicate a pronounced sunspot-cycle variation in certain regions of the corona, a scatter anisotropy, and the presence of refraction effects in addition to scattering. See also 2286 of 1955.

523.5:621.396.11 2940 Theory of the Radio-Echo Meteor Height Distribution in a Non-isothermal Atmosphere.—A. A. Weiss. (Aust. J. Phys., March 1959, Vol. 12, No. 1, pp. 54-64.) The height distribution of echoing points of shower and sporadic meteors belonging to a homogeneous velocity group is calculated for a model atmosphere whose scale height is a linear function of height. Experimental cut-off and the theoretical approximations involved limit the accuracy with which actual scale height and density may be found from observed meteor trails.

523.5:621.396.11 2941 Elevation, Height, and Electron **Density of Echoing Points of Meteor** Trails.—A. A. Weiss. (Aust. J. Phys., March 1959, Vol. 12, No. 1, pp. 65-76.)

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These parameters may be evaluated by the continuous operation of c.w. equipment on 27 Mc/s. At least 60 % of all echoes are found to be distorted. The electron density distributions are in qualitative agreement with known meteor mass distributions and trail shapes.

523.745 : 523.165

Solar Activity and Transient Decreases in Cosmic-Ray Intensity .--D. Venkatesan. (J. geophys. Res., May 1959, Vol. 64, No. 5, pp. 505-520.)

523.755

A New Theory of the Solar Corona. P. J. Kellogg & E. P. Ney. (Nature, Lond., 9th May 1959, Vol. 183, No. 4671, pp. 1297-1301.) It is proposed that the solar corona consists of trapped charged particles moving in the magnetic fields of the sun. Experimental data are discussed in terms of this model.

550.385

Disturbances of the Earth's Magnetic Field considered as Relaxation Variations.—P. Herrinck. (Ann. Géophys., July-Sept. 1957, Vol. 13, No. 3, pp. 211–221.) Records of the horizontal magnetic component at Elisabethville and elsewhere show relaxation processes analogous to postdisturbances of magnetic storms and subject to the 27-day recurrence tendency.

550.385 2945 Possible Causes of Geomagnetic Fluctuations having a 6-sec Period.-H. J. Duffus, J. A. Shand & C. Wright. (Nature, Lond., 23rd May 1959, Vol. 183, No. 4673, pp. 1479-1480.) Comment on 1532 of May (Daniels). Short- and longperiod oscillations, sometimes preceding but more often accompanying a main train of magnetic activity are described. They are considered to be associated and of electromagnetic origin.

550.385.37

Geographical Variations in Geomagnetic Micropulsations. - H. J. Duffus, J. A. Shand, C. S. Wright, P. W. Nasmyth & J. A. Jacobs. (J. geophys. Res., May 1959, Vol. 64, No. 5, pp. 581-583.) Significant differences consistently occur in simultaneous data obtained at stations 25 miles apart.

550.385.37: 551.594.5 2947 On a Possible Auroral Origin of Certain Geomagnetic Pulsations.-J. Coulomb. (Ann. Géophys., April-June 1957, Vol. 13, No. 2, pp. 91-102.)

550.385.4 : 523.745 2948 The Relation between the Sudden **Disappearance of Filaments and Mag**netic Storms .- M. Dizer. (Ann. Géophys., Oct.-Dec. 1957, Vol. 13, No. 4, p. 325.) An analysis of records shows a correlation between the sudden disappearance of filaments close to the sun's central meridian and magnetic disturbances.

550.386: 523.755 2949 Green Coronal Line Intensity and Geomagnetism.—C. Warwick. (J. geophys. Res., May 1959, Vol. 64, No. 5, pp. 527531.) Statistical analysis indicates a minimum in geomagnetic activity following the central meridian passage of regions of high green-line intensity.

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550.389.2 : 629.19

Laws of Motion of an Earth Satellite. -Yu. A. Pobedonostsev. (Priroda, Mosk., Jan. 1958, No. 1, pp. 19-25.) The principles of multistage rocket flight are considered and formulae for rocket velocity are derived. Tables give the satellite velocity and duration of flight for heights up to 6000 km.

550.389.2 : 629.19

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A Discussion on Observations of the **Russian Artificial Earth Satellites and** their Analysis.-(Proc. roy. Soc. A, 28th Oct. 1958, Vol. 248, No. 1252, pp. 1-87.) The text is given of fifteen papers discussed at a meeting in London, 29th November 1957. These include results obtained using radio telescopes and interferometers, Doppler recorders and direction-finding and field-strength measuring equipment. Applications are made to the computation of orbit parameters. See also 1720 of 1958 for a similar discussion.

550.389.2:629.19

Observations on the U.S.S.R. Earth Satellites and the Study of Radio-Wave Propagation .- W. C. Bain & E. D. R. Shearman. (Proc. Instn elect. Engrs, Part B, May 1959, Vol. 106, No. 27, pp. 259-263.) Measurements of bearing, angle of elevation and Doppler frequency shift were made at 20 and 40 Mc/s. The observed phenomena could be explained in terms of existing knowledge of ionospheric propagation. The derivation of orbital parameters from the observations is discussed.

550.389.2:629.19

A Type of Variation of the Signal Strength from 1958 82 (Sputnik 3).---L. Liszka. (*Nature, Lond.*, 16th May 1959, Vol. 183, No. 4672, pp. 1383–1384.) Fluctuations of signal strength relative to the satellite position in orbit indicate that the satellite produces heavily ionized tracks of very long lifetime. Observations have been made to test this hypothesis and results are given.

550.389.2 : 629.19 2954 Diurnal Lapse of Signals from Sputnik III.—G. H. Munro. (*Nature, Lond.*, 30th May 1959, Vol. 183, No. 4674, p. 1549.) A brief note, dated 28th April 1959, states that systematic observations have established that pulse modulation is present only when the satellite 19588 2 is in sunlight. On very close transits the c.w. signal can be detected with sufficient strength to record the Doppler shift.

550.389.2 : 629.19 2955 Density of the Atmosphere at Heights between 200 km and 400 km from Analysis of Artificial-Satellite Orbits.-D. G. King-Hele. (Nature, Lond., 2nd May 1959, Vol. 183, No. 4670, pp. 1224-1227.)

550.389.2 : 629.19 2956 Fluctuations in the Brightness of the Second Artificial Earth Satellite.---V. P.

Electronic & Radio Engineer, September 1959

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Tsesevich. (Priroda, Mosk., April 1958, No. 4, pp. 78-79.) These brightness fluctuations are explained by the rotation of the satellite on its axis, its maximum brightness corresponding to its greatest cross-section as seen by the observer. A graph shows these brightness variations as recorded by the Odessa Observatory.

550.389.2 : 629.19

The Antipodal Reception of Sputnik III.-E. Woyk (Chvojková). (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, p. 1144.) The mechanism of the propagation of waves around the earth within the ionospheric layers is discussed and the best conditions for antipodal reception are deduced. It is concluded that at Stanford, Calif., the best conditions for frequent reception occur from the south-east during summer afternoons. This is in agreement with observations.

550.389.2 : 629.19

Satellite-Measured Radiation.-G. W. Stuart. (Phys. Rev. Lett., 15th May 1959, Vol. 2, No. 10, pp. 417-418.) The relevance of atomic change-exchange processes to the nature of the radiation belt is noted.

550.389.2 : 629.19

Some Results of Investigations on Cosmic Rays using Artificial Earth Satellites .- L. V. Kurnosova. (Priroda, Mosk., June 1958, No. 6, pp. 85-86.) The intensity variations of cosmic rays as recorded during the flight of the second sputnik are shown. There were no appreciable corresponding variations at ground level.

550.389.2 : 629.19 2960 Corpuscular Radiation and the Acceleration of Artificial Satellites.-L. G. Jacchia. (Nature, Lond., 13th June 1959, Vol. 183, No. 4676, pp. 1662-1663.) C servations of satellites 1958 β 2 and δ 1 have been re-examined and more accurate values of acceleration have been calculated at twice the original resolution (see 2564 of August). Correlation with 10.7-cm solar radiation is higher for $\beta 2$ than $\delta 1$, probably due to greater observational accuracy. An increased acceleration of $\delta 1$ at the time of two major geomagnetic disturbances following flares indicates the effect of corpuscular radiation on atmospheric density at the 200-km level.

550.389.2 : 629.19 : 551.510.535 2961 On the Existence of a Strong Magneto-ionic Effect Topside of the F Maximum of the Kennelly-Heaviside Layer.—P. R. Arendt. (J. appl. Phys., May 1959, Vol. 30, No. 5, pp. 793-795.) Observations of the Faraday effect in 108-Mc/s signals from artificial satellites showed noticeable magneto-ionic effects at altitudes up to 2 000 km.

550.389.2:629.19:621.375.9 2962 Parametric Amplifier Receives Space Signals.—(See 2895.)

550.389.2: 629.19: 621.396.11 2963 Radio Reflections from Satellite-Produced Ionization.-C. R. Roberts, P. H. Kirchner & D. W. Bray. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1156-1157.) Observations have been made on frequencies of 5, 10, 15 and 20 Mc/s and two very different effects obtained on both 10 and 15 Mc/s are described.

550.389.2 : 629.19 : 621.398

Cosmic-Ray Instrumentation in the First U.S. Earth Satellite.-G. H. Ludwig. (Rev. sci. Instrum., April 1959, Vol. 30, No. 4, pp. 223-229.) The instrumentation was designed for conservation of electrical power and for stable and reliable operation over a wide range of temperatures.

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Some Results of Investigations of the Upper Atmosphere.---V. V. Mikhnevich. (Priroda, Mosk., May 1958, No. 5, pp. 71-72.) Vertical rocket investigations carried out in U.S.S.R. between 1949 and 1958 showed that, contrary to established opinion, above the E-layer there is only a very shallow minimum in electron density. The electron density increases up to 250-300 km with a maximum at 300 km and then slowly decreases so that at 470 km the density is 10⁶ electrons/cm³.

551.510.535

2966 A Theoretical Study of the Dynamical Structure of the Ionosphere.-T. Shimazaki. (J. Radio Res. Labs, Japan, March 1959, Vol. 6, No. 24, pp. 109-241.) A comprehensive survey of the modifications to Chapman theory which are necessary to explain the actual behaviour of the Both the large F2-layer ionosphere. anomalies and the smaller ones for the E and F1 layers are discussed. Over 100 references.

551.510.535

Conditions in the Outer Ionosphere. -Ya. L. Al'pert. (Priroda, Mosk., June 1958, No. 6, pp. 86-87.) It is found that the electron concentration in the outer ionosphere decreases with the height considerably less rapidly than it increases at lower levels. The values obtained show that at 2 000-3 000 km the concentrations of electrons and neutral particles are of the order of 103-103 and 1 per cm3 respectively.

551.510.535 2968 Investigation of the Equatorial Electrojet by Rocket Magnetometer. -L. J. Cahill, Jr. (J. geophys. Res., May 1959, Vol. 64, No. 5, pp. 489-503.) Two layers of electrical current were detected, one existing near an altitude of 100 km and the other about 20-25 km higher.

551.510.535

Geophysical Effects of High-Altitude Nuclear Explosions .- T. Obayashi, S. C. Coroniti & E. T. Pierce. (Nature, Lond., 23rd May 1959, Vol. 183, No. 4673, pp. 1476-1478.) A report of observations made at Hiraiso Observatory on 1st and 12th August 1958. Fade-outs on frequencies between 10 and 20 Mc/s and an enhancement of atmospheric noise at 28 Kc/s have been recorded. These effects are attributed to an increase in D-layer ionization extending over much greater distances than had previously been envisaged.

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551.510.535

Sporadic E-Region Ionization, 'Spread F', and the Twinkling of Radio Stars .- D. F. Martyn. (Nature, Lond., 16th May 1959, Vol. 183, No. 4672, pp. 1382-1383.) Kinematic instability in the ionization gradient of a medium drifting across a magnetic field is considered to be responsible for the three phenomena.

551.510.535 2971

The Effect of Sudden Ionospheric Disturbances (S.I.D.'s) on 2.28 Mc/s Pulse Reflections from the Lower Ionosphere.-F. F. Gardner. (Aust. J. Phys., March 1959, Vol. 12, No. 1, pp. 42-53.) During a typical large S.I.D., associated with a class 2 or class 3 flare, the increase in ionization might vary from 20/1 at 65 km through 3/1 at 90 km to unity at 110 km. The amplitude recovery of the E-layer echo lagged about 4 min behind the recovery of the lower echoes around 85 km. At all heights below 85 km, echo recovery occurred simultaneously.

551.510.535 : 621.396.11 2972

Rocket Measurements of Absorption in the Lower Ionosphere.-H. Mende, K. Rawer & E. Vassy. (Ann. Géophys., July-Sept. 1957, Vol. 13, No. 3, pp. 231-233.) Results are given of measurements of the field strength of one long-wave and two medium-wave transmitters. The D-layer minimum height is about 70 km and medium-wave observations indicate maximum absorption at 80 km, the attenuation being 1.2 dB/km for normal incidence.

551.510.535 : 621.396.11 : 523.164 2973 **Refraction of Extraterrestrial Radio** Waves in the Ionosphere.--M. M. Komesaroff & C. A. Shain. (Nature, Lond., 6th June 1959, Vol. 183, No. 4675, pp. 1584-1585.) Expressions are derived for estimating ionospheric refraction at low frequencies. Horizontal gradients of electron density are considered. Positions of a discrete source obtained from observation at 19.7 Mc/s after applying corrections for refraction are within a few minutes of arc of the observed position at 85.5 Mc/s.

2974 551.594 Simultaneous Occurrence of Sub-

visual Aurorae and Radio Noise Bursts on 4.6 kc/s.-R. A. Duncan & G. R. Ellis. (Nature, Lond., 6th June 1959, Vol. 183, No. 4675, pp. 1618-1619.) Records show that there is a correlation between aurorae and noise bursts but anomalies exist which cannot be explained satisfactorily.

551.594.5

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2975 Auroral Isochasms.-B. Hultqvist. (Nature, Lond., 23rd May 1959, Vol. 183, No. 4673, pp. 1478-1479.) Observed isochasms and projections of circles in the equational plane along the geomagnetic lines of force are compared.

551.594.6: 621.3.087.4: 621.372.57 2976 Investigation of an Apparatus for Recording Atmospherics. - Benoit & Kernevez. (See 2870.)

551.594.6: 621.396.11.029.45/.51 2977 : 551.510.535

An Experimental Proof of the Mode Theory of V.L.F. Ionospheric Propagation .-- Obayashi, Fujii & Kidokoro. (See 3094.)

LOCATION AND AIDS TO NAVIGATION

621.396.93

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Radio Aids to Navigation.— (Engineer-ing, Lond., 5th Sept. 1958, Vol. 186, No. 4826, pp. 313-323.) Three papers presented at the British Association meeting in Glasgow, September 1958.

(a) Position Finding by Radio.-R. L. Smith-Rose (pp. 313-315).

(b) Marine Radio Navigational Aids .--B. G. Pressey (pp. 316-318).

(c) Radio Aids and Aeronautical Navigation .--- C. Williams (pp. 318-323).

621.396.96

Doppler Radar Navigation .--- F. B. Berger. (Electronics, 8th May 1959, Vol. 32, No. 19, pp. 62-63.) A table of characteristics of existing airborne systems.

621.396.96:621.314.63 2980 Using Silicon Diodes in Radar Modulators.—Gray. (See 3110.)

621.396.963 : 621.374.32

2981 **Digital-Counter Techniques increase** Doppler Uses .- B. E. Keiser. (Electronics, 22nd May 1959, Vol. 32, No. 21, pp. 46-50.) The frequency of an oscillator is adjusted automatically to the Doppler frequency of the returned signal and is measured using a circuit which counts 100 pulses per 360° cycle.

621.396.969.3

'Ring Angels' over South-East England.-E. Eastwood, J. D. Bell & N. R. Phelp. (Nature, Lond., 20th June 1959, Vol. 183, No. 4677, pp. 1759–1760.) The unexplained phenomena described have been observed on high-power L-band radar equipment during the sunrise period at heights up to 2 000 ft. The rings expand as ripples at a velocity of 25-55 m.p.h., the maximum diameter recorded being 30 miles.

621.396.969.33

'Escort'-a Marine Radar with Unusual Features .-- (Beama J., May 1959, Vol. 66, No. 2, pp. 57-59.) Four types of p.p.i. display can be selected and provision is made for automatic resetting of the ship's own position on the display and for automatic alignment correction.

621.396.969.34 + 621.396.9342984 Anti-aircraft Radiolocation Techniques.-K. Trofimov. (Radio, Mosk., Feb. 1958, No. 2, pp. 27-31.) A description of radar techniques for the location of enemy aircraft and their destruction by guided missiles.

MATERIALS AND SUBSIDIARY TECHNIQUES

533.5 : 621.385.032.22

2985 Measurements of Gas Evolution or Sorption of Anode Materials under Simulated Life Conditions.-C. H. Rehkopf. (Sylvania Technologist, Oct. 1958, Vol. 11, No. 4, pp. 114-116.) A brief description of techniques and results of measurements.

2986 533.58 Electrical Absorption of Gases in the High-Vacuum Pressure Range.-G. Strotzer. (Z. angew. Phys., May 1958, Vol. 10, No. 5, pp. 207-216.) Various hypotheses for the 'clean-up' effect in low-pressure gases are investigated.

535.215 : 538.6 : 546.682.86

Indium Antimonide Photoelectro-magnetic Infrared Detector.—P. W. Kruse. (J. appl. Phys., May 1959, Vol. 30, No. 5, pp. 770-778.) The theory of operation, construction, and performance data are presented.

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2988 535.215:539.2 Photoconductor Performance, Space-Charge Currents, and the Steady-State Fermi Level.—A. Rose & M. A. Lampert. (Phys. Rev., 1st March 1959, Vol. 113, No. 5. pp. 1227-1235.) "The performance of a photoconductor is analysed, via the concept of the steady-state Fermi level, and shown to be limited by the injection of space charge. Using the gain-bandwidth product G/τ_0 as a measure of performance, it is found that $G|\tau_0 = M|\tau_r$ where τ_r is the dielectric relaxation time under operating conditions, and $M = \mathfrak{N}_A/\mathfrak{N}_T$, with $e\mathfrak{N}_A$ the total charge on the anode and $e \mathfrak{N}_T$ the total volume charge, free plus trapped, effectively in thermal contact with the free charge."

2989 535.215: 546.472.21 Anomalous Photovoltaic Effect in ZnS Single Crystals. — A. Lempicki. (Phys. Rev., 1st March 1959, Vol. 113, No. 5, pp. 1204-1209.) Photovoltages larger than the band gap have been observed in both cubic and hexagonal crystals with stacking faults but not in hexagonal crystals free of such faults.

535.215 : 546.482.21 2990 Lattice Scattering Mobility of Electrons in Cadmium Sulphide .--- H. Miyazawa, H. Maeda & H. Tomishima. (J. phys. Soc. Japan, Jan. 1959, Vol. 14, No. 1, pp. 41-47.) The temperature variation of the lattice scattering mobility is found to be given by the expression $\mu_L =$ A {exp (Θ/T) - 1} with A = 92.5 ± 15 cm²/V.sec and Θ = 370 ± 30 °K. The The Conwell-Weisskopf formula is used to correct for impurity scattering.

535.215: 546.482.21

Polarization of **Photoconductivity** Excitation Bands in CdS Single Crystals. -R. L. Kelly & W. J. Fredericks. (Phys.

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Rev. Lett., 1st May 1959, Vol. 2, No. 9, pp. 389-390.) The wavelength of incident light exciting maximum photoconductivity was measured as a function of its angle of polarization with respect to crystal orientation. Results are interpreted with an energylevel model.

535.215 : 546.482.21 : 538.63

Relaxation-Time Anisotropy in Cadmium Sulphide Studied with Electrical Resistivity and Magnetoresistance Effect.—T. Mazumi. (J. phys. Soc. Japan, Jan. 1959, Vol. 14, No. 1, pp. 47-56.) Experimental results indicate unusual anisotropic temperature dependence of the galvanomagnetic effects in hexagonal CdS single crystals.

2993 535.215 : 546.482.21 : 539.23 Electric Breakdown of Vapour-Deposited CdS Films .--- K. W. Böer, U. Kümmel & W. Misselwitz. (Naturwissenschaften, July 1958, Vol. 45, No. 14, p. 331.) Breakdown field-strength is plotted as a function of film thickness for both polarities of the applied voltage.

535.215: 546.817.221: 539.23 2994 Effect of Thickness of Thin Films of Lead Sulphide on the Spectral Response of Photoconductivity.--H. E. Spencer. (*Phys. Rev.*, 15th March 1959, Vol. 113, No. 6, pp. 1417-1420.)

535.215:548.73 2995 Crystal Structure of Scdium-Potassium Antimonide (Na₂KSb).-J. J. Scheer & P. Zalm. (Philips Res. Rep., April 1959, Vol. 14, No. 2, pp. 143-150.) The structure of Na₂KSb, a photoemissive material, has been determined by X-ray analysis. It closely resembles that of Cs₃Sb.

535.37 2996 Two-Stage Optical Excitation in Sulphide Phosphors.-R. E. Halsted, E. F. Apple & J. S. Prener. (Phys. Rev. Lett., 15th May 1959, Vol. 2, No. 10, pp. 420-421.) Optical evidence shows that the same impurities give rise to electron transitions involving energy levels near or in the valence band as well as the conduction band.

535.37:061.3 2007 Transactions of the 5th Conference on Luminescence (Crystal Phosphors). -(Izv. Ak. Nauk S.S.S.R., Ser. fiz., April & May 1957, Vol. 21, Nos. 4 & 5, pp. 475-784.) The text is given of 98 papers presented at the conference held in Tartu, Estonia, 25th-30th June 1956. For a list of titles in English, see Translated Contents Lists of Russian Periodicals, Feb. & May 1958, Nos. 107 & 110, pp. 43-45 & 47-50.

535.37 : 539.2 2008 Energy-Level Positions of Silver Luminescent Centres in Sulphides .---C. C. Klick. (Phys. Rev. Lett., 15th May 1959, Vol. 2, No. 10, pp. 418-420.)

2999 535.37:546.472.21 Excitation Spectra and Temperature Dependence of the Luminescence of ZnS Single Crystals .--- A. Halperin & H. Arbell. (Phys. Rev., 1st March 1959, Vol. 113, No. 5, pp. 1216–1221.) "The luminescence of ZnS: C1 and ZnS: Cu: Cl crystals was measured for the temperature region $80-500^{\circ}$ K and for different wavelengths of exciting light. The behaviour of the luminescence versus temperature curves differed from similar curves for powders reported in literature."

535.376

A.C.-D.C. Electroluminescence.—W. A. Thornton. (*Phys. Rev.*, 1st March 1959, Vol. 113, No. 5, pp. 1187–1191.) The addition of a direct voltage to an alternating voltage exciting visible electroluminescence in certain ZnS powders increases the emission by as much as 250 times under conditions where the d.c. luminescence alone is about equal to the initial a.c. luminescence.

535.376

Rise and Decay of Intensity of Luminescence of Short - Persistence Phosphors.—R. Feinberg. (*Nature, Lond.*, 30th May 1959, Vol. 183, No. 4674, pp. 1546–1547.) Results of measurements made on three c.r. tube phosphors are discussed in relation to theory.

535.376: 537.533.2 Investigations of Exo-electron Emission and Luminescence of Inorganic Crystals.—G. Gourgé. (Z. Phys., 14th Nov. 1958, Vol. 153, No. 2, pp. 186–206.) The investigations discussed were carried out to determine the relation between exo-electron emission and luminescence; measurements were made at temperatures down to -165° C.

535.376: 546.281.26 **3003 Electroluminescence of Silicon Car bide.**—D. Rücker. (Z. angew. Phys., June 1958, Vol. 10, No. 6, pp. 254–263.) The external and internal light emission observed on d.c.-excited SiC junctions [see e.g. 3890 of 1957 (Patrick)], is investigated on blue and green single crystals, and an interpretation of the various effects is given.

535.376: 546.482.21 **3004 On the Mechanism for Carrier Excitation in CdS.**—D. D. Snyder & C. E. Bleil. (*J. appl. Phys.*, May 1959, Vol. 30, No. 5, pp. 736–739.) The production and absorption of X-rays in the experimental crystals have been calculated and some confirmatory data presented.

535.376 : 546.561-31 **Electroluminescence in Cuprous Ox ide.**—R. Frerichs & R. Handy. (*Phys. Rev.*, 1st March 1959, Vol. 113, No. 5, pp. 1191–1198.) The electroluminescent properties of Cu₂O are not directly analogous to those of a semiconductor such as Ge or an insulating phosphor such as ZnS. A detail study has been made of current creep effects occurring in Cu₂O plate rectifiers with d.c. excitation.

537.226/.228.1

Studies on (Ba-Pb) (Ti-Zr)O₃ System. —T. Ikeda. (J. phys. Soc. Japan.) Feb. 1959, Vol. 14, No. 2, pp. 168–174.)

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537.226/.227 : 546.431.824-31

Polarization Reversal in Barium Titanate.—(Bell Lab. Rec., April 1959, Vol. 37, No. 4, p. 144.) A note on the polarization reversal in single crystals which occurs by extensive sideways motion of domain walls. See 155 of January (Miller).

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537.227 : 547.476.3

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Ferroelectric Hysteresis and After-Effect Phenomena in Rochelle Salt.— H. E. Müser. (Z. angew. Phys., June 1958, Vol. 10, No. 6, pp. 249–254.) Investigation of the constriction of ferroelectric hysteresis loops observed in Rochelle salt. For a similar anomaly in $BaTiO_3$ see e.g. 2757 of 1958 (Hegenbarth).

537.228.1 : 549.514.51

 β -Quartz as High-Temperature Piezoelectric Material.—D. L. White. (J. acoust. Soc. Amer., March 1959, Vol. 31, No. 3, pp. 311–314.) Lengthwise extensional, face shear and thickness shear modes can be excited piezoelectrically by suitable rotation of the crystal plate.

537.311.33

On a Simple Model for Impurity-Band Conduction.—K. Helmers. (*Philips Res. Rep.*, Feb. 1959, Vol. 14, No. 1, pp. 1-10.) A study of the influence of impuritycentre distribution on the resistance of the sample using a stochastic resistance network.

537.311.33 3011 Some Optical Characteristics of Semiconductors.—O. Simpson. (*Research*, *Lond.*, April 1959, Vol. 12, No. 4, pp. 127–132.) A number of optical phenomena are described and related to the electronic structure of semiconductors.

537.311.33

Space Charge in Semiconductors resulting from Low-Level Injection.— M. Green. (J. appl. Phys., May 1959, Vol. 30, No. 5, pp. 744–747.) A solution of the continuity equations is obtained for the space-charge distribution by assuming that (a) deviations from neutrality are small, and (b) the space-charge fields give rise to pure diffusion and pure 'drift-wave' terms with time-dependent coefficients.

537.311.33

Role of Single Phonon Emission in Low-Field Breakdown of Semiconductors at Low Temperatures.—M. A. Lampert, F. Herman & M. C. Steele. (*Phys. Rev. Lett.*, 1st May 1959, Vol. 2, No. 9, pp. 394–397.) Observations of low-field breakdown are correlated with the known energy-band structure and phonon spectra of Ge and Si. A simple, necessary condition for breakdown is suggested.

537.311.33: 535.34-15

Effect of Pressure on the Infrared Absorption of Semiconductors.—L. J. Neuringer. (*Phys. Rev.*, 15th March 1959, Vol. 113, No. 6, pp. 1495–1503.) Measurements were made on Ge, Si, and Te in the pressure range 1–2 000 atm. The pressure coefficients were used to calculate the thermal dilation term in the equation for the change of the energy gap with temperature and hence the magnitude of the electron-lattice interaction.

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537.311.33 : 537.32

On the Theory of the Thermoelectricity in Two-Band Semiconductors.—E. Haga. (*J. phys. Soc. Japan.*, Jan. 1959, Vol. 14, No. 1, pp. 35–38.) A theory is developed taking account of the temperature dependence of the energy gap. The Thomson relations are shown to be satisfied.

537.311.33 : 537.533

Field Emission from Semiconductors.—G. Busch & T. Fischer. (Brown Boveri Rev., Nov./Dec. 1958, Vol. 45, Nos. 11/12, pp. 532–539.) Theoretical and experimental work on field emission is reviewed. Results are discussed of an investigation carried out on SiC point electrodes, which confirm the exponential relation between current and field which is characteristic of field emission.

537.311.33: 538.214

The Effect of Concentration on the Magnetic Susceptibility of Trapped Electrons and Holes in Semiconductors.—F. T. Hedgcock. (Canad. J. Phys., March 1959, Vol. 37, No. 3, pp. 381–383.) A model proposed to explain the anomalous magnetic susceptibility of certain impurity semiconductors at low temperatures [see 2800 of 1957 and 3513 of 1958 (Sonder & Stevens)] is found to be attractive qualitatively but quite inadequate quantitatively.

537.311.33: 538.614 **3018 The Faraday Effect in Anisotropic Semiconductors.**—I. G. Austin. (*J. Electronics Control*, March 1959, Vol. 6, No. 3, pp. 271–274.) "The theory of the Faraday effect in semiconductors is extended to uniaxial crystals with spheriodal energy surfaces, using the classical Drude-Zener theory. Expressions applicable at infrared frequencies are given and used to discuss preliminary measurements on Bi₂Te₂."

537.311.33: [546.28 + 546.289 3019 Semiconductor Surface Phenomena. —A. Many. (Sylvania Technologist, Oct. 1958, Vol. 11, No. 4, pp. 117-124.) 'Slow' and 'fast' surface states have been established for Ge and Si; their characteristics are summarized and discussed.

537.311.33: [546.28 + 546.289 3020 Metallurgy of Semiconductors, in Particular Germanium and Silicon... A. J. Goss. (*Marconi Rev.*, 1st Quarter 1959, Vol. 22, No. 132, pp. 3-17.) 54 references.

537.311.33 : 546.28 **3021**

The Effects of Seed Rotation on Silicon Crystals.—A. J. Goss & R. E. Adlington. (*Marconi Rev.*, 1st Quarter 1959, Vol. 22, No. 132, pp. 18–36.) Single crystals pulled in an argon atmosphere at rotation rates up to 200 r.p.m. have been examined. The effect of rotation on crystal pulling, the growth interface, dislocations, etching, resistivity, 9μ absorption data and heat treatment of the crystal are given. Results are discussed in relation to a mechanical model of stirring in the melt.

537.311.33 : 546.281.26

Some Surface Properties of Silicon Carbide Crystals.—J. A. Dillon, Jr, R. E. Schlier & H. E. Farnsworth. (*J. appl. Phys.*, May 1959, Vol. 30, No. 5, pp. 675–679.) Both work-function and electron-diffraction studies indicated that SiC surfaces obtained by ion bombardment and annealing were nonstoichiometric.

537.311.33 : 546.289

High-Electric-Field Effects in Germanium p-n Junction.—J. Yamaguchi & Y. Hamakawa. (J. phys. Soc. Japan., Jan. 1959, Vol. 14, No. 1, pp. 15–21.) Increase of ambient temperature caused the critical voltage for avalanche breakdown to increase and the voltage for the onset of negative resistance to decrease. The barrier temperature was independent of the ambient temperature.

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Barrier Temperature at Turnover in Germanium *p-n* Junction.—J. Yamaguchi & Y. Hamakawa. (*J. phys. Soc. Japan.*, Feb. 1959, Vol. 14, No. 2, pp. 232-233.)

537.311.33: 546.289

Injection and Extraction of Minority Carriers at the Surface of a Germanium Electrode as a Result of Electrochemical Processes.—Yu. V. Pleskov. (Dokl. Ak. Nauk S.S.S.R., 1st May 1959, Vol. 126, No. 1, pp. 111–114.)

537.311.33: 546.289 **Sb Distribution in Quenched Ge-Sb Alloys.**—G. Pröpstl & G. Zielasek. (Z. *angew. Phys.*, May 1958, Vol. 10, No. 5, pp. 201–204.) The distribution of Sb in alloys prepared for doping Ge single crystals is investigated using a radioactive isotope. A considerable degree of inhomogeneity is observed in spite of rapid quenching. This difficulty can be overcome by zone melting.

537.311.33 : 546.289 : 535.215 **3027 The Photoconduction of Germanium after Bombardment with Fast Elec trons.**—F. Stöckmann, E. E. Klontz, J. MacKay, H. Y. Fan & K. Lark-Horovitz. (Z. Phys., 5th Dec. 1958, Vol. 153, No. 3, pp. 331–337.) The spectral distribution of photoconduction was measured on differently doped specimens of single-crystal Ge after bombardment with 4 · 5-MeV electrons.

537.311.33: 546.289: 548.4 3028 The Generation of Dislocations by Thermal Stresses.—P. Penning. (*Philips tech. Rev.*, 22nd Aug. 1958, Vol. 19, No. 12, pp. 357–364.) A study is made of etch-pit distribution over the cross-section of a Ge rod to assess the influence of the cooling rate on its internal perfection. The theoretical dislocation distribution is calculated assuming that stresses are only partially relieved by plastic flow. Results are in good agreement with observations. See also 2459 of 1958.

537.311.33: 546.289: 548.5 3029 The Pulling of Germanium Single Crystals from 'Floating Crucibles'.— J. Goorissen & F. Karstensen. (Z. Metallkde,

Jan. 1959, Vol. 50, No. 1, pp. 46-50.) The floating-crucible technique is described and its theoretical yield is compared with that of the Czochralski and zone-refining methods.

537.311.33 : 546.623.86

The Formation of Barrier Layers in Aluminium Antimonide by the Alloying Method.—H. J. Henkel. (Z. Metallkde, Jan. 1959, Vol. 50, No. 1, pp. 51–53.) A *p*-*n* function is produced by alloying *n*-type AlSb with Zn-doped aluminium foil.

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537.311.33 : 546.681.241

The Changes in the Crystal Structure of Gallium Telluride (Ga₂Te₃) Doped with Copper.—G. Harbeke & G. Lautz. (*Naturwissenschaften*, June 1958, Vol. 45, No. 12, pp. 283–284.)

537.311.33 : 546.682.19

Effect of Heat Treatment upon the Electrical Properties of Indium Arsenide.—J. R. Dixon & D. P. Enright. (J. appl. Phys., May 1959, Vol. 30, No. 5, pp. 753–759.) Large reversible variations in carrier concentration, Hall Mobility, and carrier lifetime have been produced in InAs by heat treatment. The observed phenomena are consistent with a model involving the segregation and dispersion of donor impurities to and from dislocations.

537.311.33: 546.682.86 **3033 Properties of the Semiconductor InSb.**—M. Rodot. (*J. Phys. Radium*, Feb. 1958, Vol. 19, No. 2, pp. 140–150.) Properties are reviewed with special reference to the value of the effective mass of the electrons and the scattering mechanism. The theory of thermoelectric and thermomagnetic effects is given and experimental results are presented. See 2469 of 1958.

537.311.33: 546.824-31

Infrared Absorption of Reduced Rutile TiO₂ Single Crystals.—D. C. Cronemeyer. (*Phys. Rev.*, 1st March 1959, Vol. 113, No. 5, pp. 1222–1226.)

538:061.3

Transactions of the 3rd Conference on the Physics of Magnetic Phenomena. --(*Izv. Ak. Nauk S.S.S.R., Ser. fiz.*, June, Aug. & Sept. 1957, Vol. 61, Nos. 6, 8 & 9, pp. 787-904, 1038-1212 & 1215-1336.) The text is given of 74 papers presented at the conference held in Moscow, 23rd-31st May 1956. For a list of titles in English, see *Translated Contents Lists of Russian Periodicals*, May & June 1958, Nos. 110 & 111, pp. 50-51 & 32-34.

538.22 : 538.569.4

Indirect Coupling of Nuclear Spins in Antiferromagnet with Particular Reference to MnF₂ at Very Low Temperatures.—T. Nakamura. (*Progr. theor. Phys.*, Oct. 1958, Vol. 20, No. 4, pp. 542–552.) The line width (\approx 14 oersteds) of the F¹⁹ nuclear magnetic resonance in MnF₂ at $1 \cdot 4^{\circ}$ K observed by Jaccarino & Shulman (527 of 1958) is shown to come mainly from indirect coupling of nuclear spins through hyperfine interaction with spin waves. The line width of the Mn⁵⁵ resonance is about 600 oersteds.

538.22: 538.569.4: 621.375.9 **3037 Two-Level Maser Materials.**—R. H. Hoskins. (*J. appl. Phys.*, May 1959, Vol. 30, No. 5, p. 797.) Comment on some advantages of paramagnetic ions in ionic crystals as materials for two-level solid-state masers.

538.221 **3038 Distribution of Magnetic Domains between the Two Phases in a Single- Crystal Flat Disk of Iron.**—K. F. Niessen. (*Philips Res. Rep.*, April 1959, Vol. 14, No. 2, pp. 101–110.)

 538.221:539.23
 3039

 Magnetic Properties of Very Thin
 Films of Nickel.—G. Goureaux & A.

 Colombani.
 (C. R. Acad. Sci., Paris, 26th

 Jan. 1959, Vol. 248, No. 4, pp. 543–546.)
 (C. R. Acad. Sci., Paris, 26th)

538.221: 539.234: 538.63 Determination of the Distribution of Orientation of the Magnetization Vectors in Nickel and Iron Vapour-Deposited Films using the Magnetoresistance Effect.—W. Hellenthal. (Z. Phys., 5th Dec. 1958, Vol. 153, No. 3, pp. 359–371.)

3041 538.221:621.318.134 Temperature Dependence of the Paramagnetic Susceptibility of Nickel-Zinc Ferrites .--- V. I. Chechernikov & Yu. D. Volkov. (Zh. eksp. teor. Fiz., Oct. 1958, Vol. 35, No. 4, (10), pp. 875-879.) The reciprocal of molar susceptibility for a range of Ni-Zn ferrites is plotted as a function of temperature in the range 300°-1500° K. Near the ferromagnetic Curie point the dependence of specific magnetization σ on magnetic field strength H is expressed in the form $H = a\sigma + b\sigma^3$, where the coefficients a and b depend on temperature and pressure.

538.221: 621.318.134: 538.569.4 **3042 Magnetic Resonance Studies in the Reaction of Nickel Cobalt Ferrite.** S. L. Blum & M. H. Sirvetz. (*J. appl. Phys.*, May 1959, Vol. 30, No. 5, p. 795.) Use is made of the analysis of ferromagneticresonance line shapes to obtain indications of the course of the reaction as a function of the reaction conditions.

 538.221:621.318.134:538.569.4.029.64 3043
 Microwave Resonance in Gadolinium-Iron Garnet Crystals.—W. V. Smith, J.
 Overneyer & B. A. Calhoun. (IBM J. Res.
 Dertreyer A. 11 1050 Mich. 20 Proc.

Developm., April 1959, Vol. 3, No. 2, pp. 153-162.) Ferrimagnetic resonance at 9479 and 23 725 Mc/s is described in terms of a two-sublattice model.

538.221: 621.318.134: 621.318.57 3044 Reciprocity Relationships for Gyrotropic Media.—R. F. Harrington & A. T. Villeneuve. (*Trans. Inst. Radio Engrs*, July 1958, Vol. MTT-6, No. 3, pp. 308–310. Abstract, *Proc. Inst. Radio Engrs*, Oct. 1958, Vol. 46, No. 10, p. 1777.)

538.221: 621.318.134: 621.375.9 **3045** Power-Flow Relations in Lossless Nonlinear Media.—H. A. Haus. (*Trans.* Inst. Radio Engrs, July 1958, Vol. MTT-6,

No. 3, pp. 317-324. Abstract, Proc. Inst. Radio Engrs, Oct. 1958, Vol. 46, No. 10, p. 1777.)

621.315.3 (083.7) 3046 Wire in the Electronic Industry. (Electronic Ind., Dec. 1958, Vol. 17, No. 12, pp. 89..97.) U.S. specifications, wire codes and general information are tabulated.

621.793: 621.3.049.75 3047 **Electroless Copper Plating in Printed** Circuitry.—E. B. Saubestre. (Sylvania Technologist, Jan. 1959, Vol. 12, No. 1, pp. 6-11.) The deposition of copper films on plastic printed-circuit boards by chemical reduction is discussed, and a procedure for producing 'plated-through' holes is described.

An extension of the plating process for

unclad laminates is noted.



512:621.318.57:681.142 3048 Classification and Minimization of Switching Functions: Part 1.-N. C. de Troye. (Philips Res. Rep., April 1959, Vol. 14, No. 2, pp. 151-193.) An attempt to find from a given Boolean function either the minimal sum of products or the minimal product of sums.

516.7:621.3

Geometric-Analytic Theory of Transition in Electrical Engineering.-E. F. Bolinder. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1124–1129.)

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517.942.9 : 517.949.8

Numerical Solution of Laplace's Equation, given Cauchy Conditions.-I. Sugai. (IBM J. Res. Developm., April 1959, Vol. 3, No. 2, pp. 187-188.) An expression giving the order of magnitude of the propagated errors is obtained for numerical analysis by methods of finite differences. For the practical aspect in the design of electron guns with curved electron trajectories see Proc. Inst. Radio Engrs, Jan. 1959, Vol. 47, No. 1, pp. 87-88.

MEASUREMENTS AND TEST GEAR

621.3.011.4 (083.74)

The Cylindrical Cross-Capacitor as a Calculable Standard.--A. M. Thompson. (Proc. Instn elect. Engrs, Part B, May 1959, Vol. 106, No. 27, pp. 307-310.) The capacitor consists of a hollow conducting cylinder divided into four insulated sections by gaps parallel to the axis. A practical form described consists of four parallel bars of circular cross-section. The capacitance can be computed with precision.

621.3.018.41 (083.74)

A Portable Frequency Standard .---L. F. Koerner. (Bell Lab. Rec., May 1959, Vol. 37, No. 5, pp. 173-176.) Description of a unit, the size of a miniature camera, which operates at about 15 Mc/s with an accuracy within 1 part in 10⁶.

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621.3.018.41 (083.74)

Construction of a Mobile Caesium Frequency Standard.-A. H. W. Beck & J. Lytollis. (Proc. Instn elect. Engrs, Part B, 1958, Vol. 105, Supplement No. 11, pp. 712-715. Discussion.) Practical details of the construction of a sealed-off version are given.

621.3.018.41 (083.74) : 538.569.4 3054 Construction and Application of a Frequency Standard for Microwave Spectrometers .- H. G. Fitzky. (Z. angew. Phys., July 1958, Vol. 10, No. 7, pp. 297-303.) A 10-Mc/s crystal oscillator and frequency multiplication to 1080 Mc/s are used in the equipment described for measurements of frequency up to 25 kMc/s with an accuracy better than 1 part in 107.

3055 621.317.3:621.396.822 Measurement of Equivalent Noise Resistance of a Noise-Thermometer Amplifier.-H. Pursey & E. C. Pyatt. (J. sci. Instrum., June 1959, Vol. 36, No. 6, pp. 260-264.) Amplifier noise is compared with that of a wire-wound resistance at a standard temperature, using a vibrating switch to connect the sources alternately to a single channel. An accuracy within 1% is obtained.

621.317.4 : 538.569.4 3056 Measurement of Magnetic Flux Density by Paramagnetic Resonance .---C. P. Allen & M. Sherry. (J. Electronics Control, March 1959, Vol. 6, No. 3, pp. 264-270.) The method is based on measurement of the frequency of paramagnetic resonance in an organic compound. It uses a simple coaxial-line probe unit and enables flux densities in the range of a few hundreds up to some thousands of gauss to be measured to an absolute accuracy of ± 0.06 %.

621.317.4: 621.3.042.1: 621.397.62 3057 Magnetic Measurements on Ferrite U-Cores for Horizontal-Deflection Output Transformers.-R. Fälker & E. E. Hücking. (Elektronische Rundschau, Aug. 1958, Vol. 12, No. 8, pp. 270-274.) Methods of measurement are reviewed and a specially designed core tester is described.

621.317.42 : 550.385

The Influence of the Self-Inductance of Magnetic-Core Windings used for the Recording of Rapid Variations of the Earth's Magnetic Field.-G. Grenet. (Ann. Géophys., July-Sept. 1957, Vol. 13, No. 3, pp. 249-251.)

621.317.61:621.385.1 3059

A Method for the Accurate Measurement of Mutual Conductance of Thermionic Valves .--- M. R. Child & D. J. Sargent. (Proc. Instn elect. Engrs, Part B, May 1959, Vol. 106, No. 27, pp. 311-314.) Absolute errors are estimated to be less than $0\!\cdot\!25$ %, and comparative error less than 0.1%. Adaptations for measurement of anode conductance and screen-grid amplification factor are described.

621.317.7:621.314.7 3060

A Transistor Characteristic Curve Tracer.—J. F. Young. (Electronic Engng, June 1959, Vol. 31, No. 376, pp. 330–336.) "A Dekatron is used to develop a stepped voltage controlling the base current of the transistor under test. At each step a half sinusoidal voltage is applied to the transistor and the resulting collector current is plotted against voltage on an external oscilloscope. A series resistor provides the current signal and limits the transistor dissipation. The unit can also be used to plot the characteristics of normal or of Zener diodes."

621.317.733: 621.375.2.024 3061

Use of a Direct-Current Amplifier and Recorder to Balance a Mueller Resistance Bridge.-G. T. Armstrong, P. K. Wong & L. A. Krieger. (Rev. sci. Instrum., May 1959, Vol. 30, No. 5, pp. 339-343.) Methods of reducing system noise to give improved sensitivity.

621.317.733.011.4 : 621.372.54 3062 The Balanced Unsymmetrical Parallel-T Network as a Three-Terminal Frequency-Dependent Bridge for the Measurement of Capacitance and Dissipation Factor.-K. Posel. (Trans. S. Afr. Inst. elect. Engrs, Aug. 1958, Vol. 49, Part 8, pp. 287-298.) The theory of operation of the bridge and its design are detailed. See also 2656 of 1958.

621.317.733.029.62

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Coaxial Displacement Dielectric Cell for Liquids Usable to 250 Mc/s.-S. E. Lovell & R. H. Cole. (Rev. sci. Instrum., May 1959, Vol. 30, No. 5, pp. 361-362.) Construction details of a bridge element useful in the determination of capacitance, dielectric loss, or conductivity.

621.317.74 : 534.2-8 : 621.373.52 3064 Zero-Crossing Technique syncs Wave-Train Outputs.-J. A. Wereb, Jr. (Electronics, 8th May 1959, Vol. 32, No. 19, pp. 64-65.) A technique for producing a sinusoidal wave-train starting from the zerocrossing point of another sine wave. The generator is used in testing ultrasonic equipment.

621.317.75.087.6

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Homodyne Detector for Reproduction of Periodic Waveforms .--- C. Lagercrantz. (J. sci. Instrum., June 1959, Vol. 36, No. 6, pp. 257-259.) An a.f. signal is scanned using 20-µs gating impulses whose phase is shifted slowly and linearly. The gated output is recorded on a pen recorder. The circuit and performance tests are described.

621.317.763.029.64 : 621.372.413 3066 The Design of Broad-Band Circular Wavemeters .- P. Andrews. (Brit. Commun. Electronics, May 1959, Vol. 6, No. 5, pp. 354-357.) The design is considered mainly with cylindrical cavities in the TE₁₁ mode. Mode suppression and the temperature coefficient of wavemeters are treated.

OTHER APPLICATIONS OF RADIO AND ELECTRONICS

531.721:621.397.9	3067
The Video Differential Pla	
M. Tobin. (Rev. sci. Instrum.,	May 1959,
Vol. 30, No. 5, pp. 323-327.)	Description
of an instrument for measuring	variations in
the projected area of a remot	e object by
means of a television camera	system or
flying-spot scanner.	
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538.566.029.6 : 541.126 3068 **Observations of Detonation in Solid** Explosives by Microwave Interferometry.-G. F. Cawsey, J. L. Farrands & S. Thomas (Proc. roy. Soc. A, 9th Dec. 1958, Vol. 248, No. 1255, pp. 499-521.) Confined detonation processes have been studied by a method noted earlier [1833 of 1956 (Farrands & Cawsey)], using apparatus developed from that described by Froome (3532 of 1952).

3069 550.340:621.3.087.6 An Electronic Seismic Transducer for Visual Recording.—P. Gouin. (Ann. Geophys., July-Sept. 1957, Vol. 13, No. 3, pp. 234-241. In English.) A detailed description of the capacitance-type transducer, amplifier and recorder.

3070 551.508.71:621.372.413 Recording Microwave Hygrometer. J. Sargent. (Rev. sci. Instrum., May 1959, Vol. 30, No. 5, pp. 348-355.) A description is given of a microwave refractometer designed at the National Bureau of Standards for measurement of low water-vapour pressures in a moving air stream.

3071 621.384.6:621.319.3 Electrostatic-Transformer-Type Particle Accelerator using Ceramic BaTiO₃ -Ferrostac.-T. Shibata, A. Toi & T. Suita. (J. Phys. Soc. Japan, Feb. 1959, Vol. 14, No. 2, p. 227.) A note on the construction of a 150-kV accelerator in which the h.v. generator has rotating ferroelectric disks which carry electric charges.

621.384.8: 621.318.381	3072
· 621 316 7 078 3	

Current and Field Stabilization of the 9-kW Electromagnet of the A.E.I. Magnetic Spectrograph.-R. Bailey & E. C. Fellows. (J. Brit. Instn Radio Engrs, May 1959, Vol. 19, No. 5, pp. 309-321.) Signals obtained from nuclear resonance are used to control the strength of a magnetic field to within ± 0.01 %.

3073 621.385.833 Numerical Computation of Electrostatic Immersion Objectives.—E. Hahn. (Optik, Stuttgart, Aug. 1958, Vol. 15, No. 8, pp. 500-515.)

3074 621.385.833 Space-Charge Aberration and Resolving Power in Electron Microscopes. W. E. Meyer. (Optik, Stuttgart, July 1958, Vol. 15, No. 7, pp. 398-406.)

Space-charge effects may limit the resolving power more than spherical aberration. Methods of reducing the influence of space charge are indicated.

621.385.833 3075 Stigmatic Image in Rotationally Asymmetric Electron Lenses.—F. Lenz. (Optik, Stuttgart, July 1958, Vol. 15, No. 7, pp. 393-397.)

621.385.833 : 535.317.3 3076 Compensation of the Chromatic Dependence of Magnification in the Electrostatic Electron Microscope .-W. Weitsch. (Optik, Stuttgart, Aug. 1958, Vol. 15, No. 8, pp. 492-499.)

3077 621.385.833: 621.3.032.21 Some Electron-Optical Properties of Point Cathodes.-S. Maruse & Y. Sakaki. (Optik, Stuttgart, Aug. 1958, Vol. 15, No. 8, pp. 485-491.) Experimental results show that electron emission of the point cathode is mainly determined by the Schottky effect. The use of the point cathode as a cold cathode in electron microscopes is discussed. See also 245 of 1957 (Sakaki & Möllenstedt).

621.385.833: 621.3.032.213.6 3078 Oxide-Cored Cathode.-K. Ando, O. Kamigaito, Y. Kamiya, S. Takahashi & R. Uyeda .- (J. Phys. Soc. Japan, Feb. 1959, Vol. 14, No. 2, pp. 180-185.) Description of a cathode for electron microscopy consisting of a drawn platinum wire filled with oxide powder. The method of preparation and performance tests are described.

3079 621,387.494 Improved Design for Halogen-Quenched End-Window Geiger Counters. -K. van Duuren & J. Hermsen. (Rev. sci. Instrum., May 1959, Vol. 30, No. 5, pp. 367-368.)

621.387.464

Modern Development of Scintillation Counters .- W. Hanle & H. Schneider. (Z. angew. Phys., May 1958, Vol. 10, No. 5, pp. 228-248.) Detailed review of design, construction and applications. 242 references.

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621.387.464 : 621.383.27

The Resolving Power of Scintillation Multipliers and the Influence on it of Various Parameters .- P. Görlich, A. Krohs, H. J. Pohl, R. Reichel & L. Schmidt. (Z. angew. Phys., July 1958, Vol. 10, No. 7, pp. 303-309.) Results of measurements on a photomultiplier for scintillation counting are discussed.

621.397.9:522.2 3082 Using TV Techniques in Astronomy. -J. Borgman. (Electronics, 8th May 1959. Vol. 32, No. 19, pp. 66-68.) A variable star is detected by a differential photographic method which eliminates constant features. Television techniques are used to display the difference signals.

621.397.9:522.2 3083 Television Techniques in Astronomy. -N. F. Kuprevich. (Priroda, Mosk., March 1958, No. 3, pp. 50-54.) Two systems are

described based on : (a) a two-stage electronoptical converter consisting of a photocathode emitting electrons which form an image on a 35-mm luminous screen with a possible increase of brightness up to 100-130 times; (b) the use of an orthicon-type 625line television screen on which an image is obtained with magnification up to 6.5 times.

621.398

Radio Telemetry: Part 1-Systems. -A. J. Shimmins. (Proc. Instn Radio Engrs, Aust., Dec. 1958, Vol. 19, No. 12, pp. 775-787.) Factors which determine system performance are analysed, taking as an example the R.A.E. subminiature f.m./a.m. system.

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3085 621.398: 616.831-073.97 A Miniature Electroencephalograph Telemeter System.—D. C. Gold & W. J. Perkins. (Electronic Engng, June 1959, Vol. 31, No. 376, pp. 337-339.) Transmits the electrical activity of the brain of an unrestrained cat on a 6.8-Mc/s a.m. carrier.

681.61 : 621.319 High-Speed Read-Out for Data Pro-

cessing.-R. E. West. (Electronics, 29th May 1959, Vol. 32, No. 22, pp. 83-85.) Description of an e.s. teletypewriter which can print more than 3000 words/min. Input pulses to the print heads charge the surface of paper to which powdered ink adheres.

PROPAGATION OF WAVES

3087 621.396.11:550.389.2:629.19 Radio Reflections from Satellite-Produced Ionization .- Roberts, Kirchner & Bray. (See 2963.)

3088 621.396.11:551.510.52 The Role of Turbulent Mixing in Scatter Propagation.-R. Belgiano, Jr. (Trans. Inst. Radio Engrs, April 1958, Vol. AP-6, No. 2, pp. 161–168. Abstract, Proc. Inst. Radio Engrs, July 1958, Vol. 46, No. 7, p. 1438.)

3089 621.396.11:551.510.52 The Influence of Moisture in the Ground, Temperature and Terrain on Ground Wave Propagation in the V.H.F. Band.-B. Josephson & Å. Blomquist. (Trans. Inst. Radio Engrs, April 1958, Vol. AP-6, No. 2, pp. 169-172. Abstract, Proc. Inst. Radio Engrs, July 1958, Vol. 46, No. 7, p. 1439.)

3090 621.396.11:551.510.52 Distance Dependence, Fading Char-acteristics and Pulse Distortion of 3000-Mc/s Transhorizon Signals.--B. Josephson & G. Carlson. (Trans Inst. Radio Engrs, April 1958, Vol. AP-6, No. 2, pp. 173-175. Abstract, Proc. Inst. Radio Engrs, July 1958, Vol. 46, No. 7, p. 1439.)

621.396.11:551.510.52 3091 Some Microwave Propagation Experiences from a 'Just-Below-Horizon' Path.

Electronic & Radio Engineer, September 1959

A149

-B. Josephson & F. Eklund. (Trans. Inst. Radio Engrs, April 1958, Vol. AP-6, No. 2, pp. 176-178. Abstract, Proc. Inst. Radio Engrs, July 1958, Vol. 46, No. 7, p. 1439.)

621.396.11:551.510.52

The Diffraction of Electromagnetic Waves by the Earth's Curvature-a Theory of Tropospheric Propagation Near and Beyond the Radio Horizon.-O. Tukizi. (Rep. elect. Commun. Lab., Japan, Nov. 1958, Vol. 6, No. 11, pp. 421-425.) Classical diffraction theory is modified to account for the slow rate of decrease of fieldstrength well beyond the horizon. A saddlepoint method is used to take into account the contribution of all the terms of the residue series.

621.396.11: 551.510.535: 523.164 3093 **Refraction of Extraterrestrial Radio** Waves in the Ionosphere.--Komesaroff & Shain. (See 2973.)

621.396.11.029.45/.51 : 551.510.535 3094 : 551.594.6

An Experimental Proof of the Mode Theory of V.L.F. Ionospheric Propagation.—T. Obayashi, S. Fujii & T Kidokoro. (J. Geomag. Geoelect., 1959, Vol. 10, No. 2, pp. 47-55.) V.l.f. atmospherics are received on a receiver which continuously sweeps over the frequency band 5-70 kc/s. The output is displayed on an intensity-modulated c.r. tube which is photographed on continuously moving film. There is an intensity maximum near 10 kc/s and selective absorption bands which vary with time of day and may be associated with the cut-off frequencies of the earthionosphere waveguide. The effects of solar flares are also discussed.

621.396.11.029.63

A Contribution to the Knowledge of Propagation Conditions at 1.3 Gc/s based on Measurements over a Transmission Path within Optical Range.-U. Kühn. (Tech. Mitt. BRF, Berlin, Oct. 1957, Vol. 1, No. 1, pp. 4-10.) Statistical analysis of field-strength recordings taken in one year over an 82-km path, and comparison with meteorological data for the same period.

621.396.11.029.63

Measurements of 1250-Mc/s Scatter Propagation as Function of Meteorology .-- D. L. Ringwalt, W. S. Ament & F. C. MacDonald. (Trans. Inst. Radio Engrs, April 1958, Vol. AP-6, No. 2, pp. 208-209.) Short detailed report and discussion of the results of measurements made over a 262mile over-water path between Florida and the Bahamas in December 1956. Ground and airborne field-strength measurements, refractometer soundings, radiosonde data and visual observations were recorded.

621.396.11.029.63

Apparent Correlation between Tropopause Height and Long-Distance Transmission Loss at 490 Mc/s.-D. R. Hay. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1144-1145.) For a 640-mile path in June-July 1957 signals were low and steady when the tropopause was low, but were higher and fluctuated more when the tropopause was high.

621.396.812

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Prolonged Signal Fade-Out on a Short Microwave Path .-- D. R. Hay & G. E. Poaps. (Canad. J. Phys., March 1959, Vol. 37, No. 3, pp. 313-321.) During a period of one year, the incidence of signal fade-out has been observed in 2-kMc/s transmissions over a 21-mile path near Ottawa. Fade-out durations varied from a few minutes to several hours, with the most frequent occurrence in the summer and during the night. An analysis of the refractivity of the air at the middle of the radio path indicates that fade-out is associated with a shallow horizontal transition zone in vapour pressure at a level near the aerial heights.

RECEPTION

621.376 3099 Correlation Devices Detect Weak Signals.-H. R. Raemer & A. B. Reich. (Electronics, 22nd May 1959, Vol. 32, No. 21, pp. 58-60.) Operating principles of autocorrelators, cross-correlators, and radiometers are described.

621.396.621:621.314.7 3100 How to Design Reflexed Transistor Receivers.—J. Waring. (Electronics, 8th May 1959, Vol. 32, No. 19, pp. 70-72.) Methods for obtaining i.f. and a.f. gain in the same stage without motorboating.

621.396.66 : 621.396.828 3101 Negative-Supply Outboard Codan. R. L. Ives. (Audio, May 1959, Vol. 43. No. 5, pp. 22-23. . 73.) Details are given of a circuit which silences the a.f. stages of a receiver when the carrier amplitude falls below a predetermined level. The circuit does not alter the characteristics of the receiver to which it is connected.

621.396.812.3: 621.396.666

3102 Linear Diversity Combining Techniques .--- D. G. Brennan. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1075-1102.) An analysis and results of measurements of the relative performance are given for three types of diversity combining techniques: (a) selection diversity, (b) maximalratio diversity, and (c) equal-gain diversity systems. The effects of various departures from the ideal conditions are considered and the relative merits of predetection and postdetection combining and of long-term distributions are discussed.

STATIONS AND COMMUNICATION SYSTEMS

621.391

On Asymmetric Information Channels .--- R. B. Banerji. (J. Brit. Instn Radio

3103

Engrs, May 1959, Vol. 19, No. 5, pp. 305-308.) A study of channel capacity in terms of the probability of possible errors, and application to p.c.m. with amplitude keying.

621.396.3 : 621.391

Some Operational Considerations Affecting the Use of Automatic Error Correcting Equipment on H.F. Telegraph Networks .--- E. G. Copper. (Point to Point Telecommun., Feb. 1959, Vol. 3, No. 2, pp. 21-34.) A discussion of some of the problems associated with the radio errorcorrecting multiplex (REM) system.

621.396.5:534.76 3105

Compatible Stereo Radio using A.M/ F.M. Multiplex .-- H. E. Sweeney. (Electronics, 8th May 1959, Vol. 32, No. 19, pp. 56-58.) Transmission of two channels by amplitude and frequency modulation of the same carrier. A circuit is given for the addition of a f.m. channel to an a.m. receiver.

621.396.65

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3106

The TJ Radio System .--- S. D. Hathaway & H. H. Haas. (Bell Lab. Rec., April 1959 Vol. 37, No. 4, pp. 129-133.) Description of a 6-channel 11-kMc/s relay system using dual frequency-diversity transmission, giving details of arrangement of subcarriers in the spectrum and examples of use for telephony, television and data transmission.

621.396.65 : 621.396.41 3107 F.M. Multiplexing for Studio-Transmitter Links. D. Harkins. (Electronics, 22nd May 1959, Vol. 32, No. 21, pp. 44-45.) Three program signals modulate subcarriers at 26, 65 and 175 kc/s, which are combined to modulate a 946 Mc/s carrier for transmission to the transmitter site 16 miles away.



621.3.087.45: 621.395.625.3 3108

A Multiple-Channel D.C. Recording System.-H. D. Scott. (Electronic Engng, June 1959, Vol. 31, No. 376, pp. 340-344.) Describes an a.m. system with tape-noise cancellation enabling up to twelve 0-10-c/s channels to be recorded on a conventional single-track recorder together with speech and timing signals.

3109

The Thermal Behaviour of Semiconductor Rectifiers .--- O. Jakits. (Brown Boveri Rev., Nov./Dec. 1958, Vol. 45, Nos. 11/12, pp. 540-544.) Measurements are described which were made on heavycurrent Ge diodes to determine the thermal inertia. The effect of cooling on the overload characteristic is discussed.

621.314.63 : 546.289

621.314.63:621.396.96 3110 Using Silicon Diodes in Radar Modulators.-M. G. Gray. (Electronics, 12th June 1959, Vol. 32, No. 24, pp. 70-72.) A peak power of 250 kW is developed using

Si diodes for charging the artificial line and for clipping reverse voltage swings. The diodes dissipate instantaneous powers up to 300 kW.

621.314.634

Selenium Rectifiers with Artificial Layers of Selenides of Cadmium, Tin, Bismuth and Lead.--Y. Moriguchi. (J. Phys. Soc. Japan, Feb. 1959, Vol. 14, No. 2, pp. 152-167.) The action of various selenides as barrier layers has been investigated by measurement of the rectifier d.c. and a.c. characteristics. CdSe and SnSe layers play an important role in rectification but the selenides of Bi and Pb seem to be unsuitable. In general, the layer material should have a resistivity $< 10^4 \Omega$ cm.

621.314.64 3112 Current/Time Relationship in the Forward Direction of Electrolytic Rectifiers.—W. C. van Geel & C. A. Pistorius. (*Philips Res. Rep.*, April 1959, Vol. 14, No. 2, pp. 123–131.) Qualitative explanation of the effects observed on applying alternating rectangular and sinusoidal voltages.

621.316.721.078 : 621.375.2.024 3113 Use of Operational Amplifiers in Precision Current Regulators.—K. Eklund. (*Rev. sci. Instrum.*, May 1959, Vol. 30, No. 5, pp. 328–331.) Low-drift high-gain d.c. amplifiers in a control loop can reduce steady-state error.

TELEVISION AND PHOTOTELEGRAPHY

621.397.24

Carrier Transmission for Closed-Circuit Television.—L. G. Schimpf. (*Electronics*, 12th June 1959, Vol. 32, No. 24, pp. 66–68.) A simple and inexpensive coaxial-cable transmission system, using transistors in the terminal and repeater circuits is described. D.c. supplies to the repeaters are applied via the signal cable.

621.397.611.2 3115 Measurement of the Transmission Characteristics of Television-Camera Preamplifiers.—W. Eckardt. (*Tech. Mitt. BRF*, Berlin, Dec. 1957, Vol. 1, No. 2, pp. 27–32.)

621.397.62 3116 Two Realizations of the New Synchrophase.—L. Chrétien & R. Aschen. (*TSF et TV*, March-May 1957, Vol. 33, Nos. 341-343, pp. 71-76, 152-157 & 167-168.) A rejector circuit and a variable videofrequency gain control compensate for phase distortion by altering the shape of the videofrequency response curve. Detailed descriptions are given of a medium-range and a long-range television receiver, with a note on the adjustment of the phase-correction circuit.

621.397.62

Television I.F. Amplifiers with Linear Phase Response.—A. N. Thiele. (Proc. Instn Radio Engrs, Aust., Nov. 1958, Vol. 19, No. 11, pp. 652–668.) This type of response is discussed in relation to ease of tuning and alignment and to phase equalization at the transmitter.

621.397.62 : 535.623

3111

Automatic Controls for Colour Television.—Z. Wiencek. (*Electronics*, 15th May 1959, Vol. 32, No. 20, pp. 58–59.) A method of control of the phase (hue) and amplitude (chroma) of the colour signal using a low-frequency diode gate.

3118

621.397.62: 535.623: 535.88 3119 The Projection of Colour-Television Pictures.—T. Poorter & F. W. de Vrijer. (*Philips tech. Rev.*, 22nd Aug. 1958, Vol. 19, No. 12, pp. 338–355.) Three projectiontype c.r. tubes are used respectively with red, green and blue fluorescing phosphors. Each is mounted in a Schmidt optical system the superposition of the three images being effected either by dichroic mirrors [1701 of May (van Alphen)] or by mounting the three tubes side by side. Projectors using these systems are described.

621.397.621.2 3120 Noise-Immune Synchronizing Circuits for Television Timebase Circuits. —D. J. Howlett & L. Buduls. (Proc. Instn Radio Engrs, Aust., Nov. 1958, Vol. 19, No. 11, pp. 680–689.) Noise limiting and a.g.c. circuits are discussed and details are given of an improved form of the heptode sync separator described by Marks (252 of 1953).

621.397.621.2 3121 Some Aspects of Synchronization in Television Receivers.—J. van der Goot. (*Proc. Instn Radio Engrs, Aust.*, Nov. 1958, Vol. 19, No. 11, pp. 690–706.) A discussion of scanning oscillators and a.f.c. systems.

621.397.621.2

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The Synchronization Separator—an Unexpected Observation.—J. Goldthorp. (*Proc. Instn Radio Engrs, Aust.*, Nov. 1958, Vol. 19, No. 11, pp. 706–707.) A note describing the improved performance obtained using a remote-cut-off pentode as composite sync separator in place of a valve with sharp cut-off.

621.397.621.2

Improvements in Television Receivers: Part 5-Stabilization of Line and Frame Output Circuits.—B. G. Dammers, A. G. W. Uitjens, A. Boekhorst & H. Heyligers. (*Electronic Applic.*, Nov. 1958, Vol. 18, No. 4, pp. 129–142.) Detailed descriptions are given of circuits suitable for a 110° c.r. tube. Line output stages with flyback ratios of 16, 18 or 21 % have been stabilized by voltage-dependent resistors (see Part 4: 989 of March). The frame output stage derives its charging voltage from the stabilized boost voltage. A protective circuit to limit beam current is described.

621.397.621.2 3124 Improvements in Television Receivers : Part 6—Design Considerations for Stabilized Line Output Circuits.—B. G. Dammers, A. Boekhorst & D. Hoogmoed. (Electronic Applic., Nov. 1958, Vol. 18, No. 4, pp. 143–157.) Essential formulae and graphs are given for a quantitative investigation of circuits in which the line output valve operates above the knee of the I_a/V_a characteristic. For practical circuits see 3123 above.

621.397.621.2: 535.623: 621.385.832 3125 Errors of Magnetic Deflection: Part 2.—J. Haantjes & G. J. Lubben. (Philips Res. Rep., Feb. 1959, Vol. 14, No. 1, pp. 65–97.) Approximate formulae for the design of deflection coils have been developed from a theoretical study [Part 1: 2990 of 1957]. Convergence errors in the shadowmask tube and in an experimental tube with three guns vertically in line are discussed.

621.397.621.2 : 621.373.444.1 3126 . : 621.314.7

For the latter tube a deflection coil can be

designed which makes dynamic convergence

unnecessary.

Transistor Line Deflection Circuits for Television.—P. B. Helsdon. (Marconi Rev., 1st Quarter 1959, Vol. 22, No. 132, pp. 38–70.) The shunt diode circuit and the retrace-driven circuit due to Guggi (2382 of 1957) are analysed and their limitations discussed. A flyback-driven circuit is described with automatic phase control, and reverse base current drive to the shunt diode circuit. The output is sufficient for scanning a 70° picture tube.

621.397.621.2 : 621.385.832 3127 A New Approach to Short Picture-

Tube Design.—G. A. Burdick. (Sylvania Technologist, Jan. 1959, Vol. 12, No. 1, pp. 2–5.) A brief description of the construction and principle of operation of the tripotential focus (TPF) gun which can be focused by varying the potential to any one of the three elements.

621.397.621.2: 621.385.832.032.269.1 3128 A New Electron Gun for Picture Display with Low Drive Signals.—K. Schlesinger. (J. Telev. Soc., Jan.–March 1959, Vol. 9, No. 1, pp. 15–25.) High control sensitivity required for transistor drive is achieved by a new electron-optical approach. Beam focusing and modulation are effected in a cylindrical cavity by two separate e.s. fields: one of circular symmetry for focusing, and one of transverse-plane geometry for modulation.

621.397.7

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ABN Television Transmitter.—F. M. Shepherd. (Proc. Instn Radio Engrs, Aust., Nov. 1958, Vol. 19, No. 11, pp. 609–614.) A brief description of main and standby equipment at Gore Hill.

621.397.7 **3130**

The ATN Television Centre.—M. H. Stevenson. (*Proc. Instn Radio Engrs, Aust.*, Nov. 1958, Vol. 19, No. 11, pp. 614–621.) A general description of the Centre which is near Sydney. Factors which influenced its design and the provisions made for expansion are discussed.

621.397.7 : 535.623

Holding Video Level while Switching Studios.—J. O. Schroeder. (Electronics,

Electronic & Radio Engineer, September 1959

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29th May 1959, Vol. 32, No. 22, pp. 96–98.) An automatic circuit designed to compensate for wide variations in colour or monochrome input signal levels and to maintain a constant output level.

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621.397.7 : 621.396.65

Equalization of Aural and Visual Delay.—I. Kerney & W. D. Mischler. (*Bell Lab. Rec.*, May 1959, Vol. 37, No. 5, pp. 182–186.) The delay of audio signals relayed by coaxial cable relative to video signals relayed by microwave link is reduced by bypassing demodulating equipment at coaxial relay points.

621.397.7: 621.396.677.81 3133 The Passive TV Relay and its Practical Possibilities.—Aschen. (See 2851.)

621.397.8 3134 Echo Phenomena in Television Images.—J. Polonsky, L. Amster & G. Melchior. (J. Telev. Soc., Jan.–March 1959, Vol. 9, No. 1, pp. 2–14.) English version of 283 of 1957.

621.397.8

Results of Investigations on the Recognizability of Small Details on a Television Screen.—F. Below, W. Kroebel & H. Springer. (Z. angew. Phys., June 1958, Vol. 10, No. 6, pp. 277–285.) An objective method of measuring detail recognition is described based on the use of Landoltring test pictures (see 3321 of 1957). The effects of bandwidth limitation and contrast are investigated.

621.397.8

The Perceptibility of Image Details in Television Images.—W. Kroebel, F. Arp & H. Baurmeister. (Z. angew. Phys., July 1958, Vol. 10, No. 7, pp. 320–327.) The test described in 3136 below is applied to television images. Results are closely related to those obtained with optically projected images.

621.397.8

Phase-Shift Considerations in Television Broadcasting and Reception.— M. W. Davies. (*Proc. Instn Radio Engrs, Aust.*, Nov. 1958, Vol. 19, No. 11, pp. 642–651.) A general description of phase distortion and of the effects this distortion can have on the received signal of a vestigial-sideband system. Methods available for compensation are discussed; see e.g. 3117 above.

621.397.8:535.7

The Visual Properties of the Human Eye as a Contribution to the Problem of Assessing the Quality of Projection and Television Images.—W. Kroebel, F. Arp & H. Baurmeister. (Z. angew. Phys., July 1958, Vol. 10, No. 7, pp. 309–317.) A test is described for the quantitative assessment of the perception of small objects by the eye and a mathematical expression is derived relating perception to contrast and object size. For the underlying statistical considerations see *ibid.*, pp. 317–320 (Arp).

621.397.8 : 621.396.822

Effects of Noise in Television Transmission.—T. Kilvington. (J. Telev. Soc., Jan.-March 1959, Vol. 9, No. 1, pp. 26-31.) The nature of random noise and its effect on sound and vision reception are reviewed. The subjective effects on the picture of both random and periodic noise are described and methods of minimizing them are considered.

621.397.8 : 621.396.822

Theoretical and Experimental Characteristics of Random Noise in Television.—R. Fatehchand. (J. Brit. Instn Radio Engrs, June 1959, Vol. 19, No. 6, pp. 335–344.) The characteristics of noise distributed uniformly over the frequency band and that concentrated at the high frequency end of the pass-band are compared. The effects of a nonlinear transfer characteristic on noise alone and on noise plus signal are studied and the relation between these effects and noise visibility on a picture tube is examined.



621.396.61 : 629.19

Minimum Transmitter System Weight for Space Communications.— R. S. Davies & C. S. Weaver. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, pp. 1151–1152.) A method is given for calculating optimum transmitter weight and aerial size.

621.396.71 **3142** New Radio Transmitters at Ongar.— (*Engineer, Lond.*, 27th Feb. 1959, Vol. 207, No. 5379, p. 339.) Operational data are given on the seven new radiotelegraphy transmitters of the British Post Office.

VALVES AND THERMIONICS

621.314.63 **3143** The D.C. and A.C. Characteristics of Point-Contact Diodes.—H. Beneking. (Z. angew. Phys., May 1958, Vol. 10, No. 5, pp. 216–225.) A p-n diode of spherical symmetry [see e.g. 2411 of July (Hofmeister & Groschwitz)] is investigated by analogy with calculations for the plane configuration (1398 of April). An interpretation of the injection mechanism of point contacts is obtained. Good agreement between measured and theoretical diode characteristics is found.

621.314.63 : 621.318.57 **3144 Millimicrosecond Switching Diodes.** --J. Halpern & R. H. Rediker. (*Electronics*, 5th June 1959, Vol. 32, No. 23, pp. 66–67.) Describes briefly the construction of Ge-In-Sb diffusion diodes for switching speeds of 2–3 $m\mu$ s (see 2909 of 1958). A method of measuring the reverse recovery time is outlined.

621.314.63:621.372.632

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Transmitting Frequency Converter in which Gold- or Silver-Bonded Diode is Used.—S. Kita, H. Sanpei & T. Okajima. (*Rep. elect. Commun. Lab., Japan*, Nov. 1958, Vol. 6, No. 11, pp. 415–420.) More than 8 dB conversion gain with output frequency 4130 Mc/s has been obtained using nonlinear-capacitance Ge diodes [see *Proc. Inst. Radio Engrs*, June 1958, Vol. 46, No. 6, p. 1307 (Kita)].

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621.314.63 + 621.314.7]-71 (083.57) 3146

Taking the Heat off Semiconductor Devices.—W. Luft. (*Electronics*, 12th June 1959, Vol. 32, No. 24, pp. 53–56.) Charts and nomograms are given for the design of cooling fins.

621.314.7 + 621.314.63 **3147 Transistors and Associated Semiconductor Devices.**—R. G. Hibberd. (*Proc. Instn elect. Engrs*, Part B, May 1959, Vol. 106, No. 27, pp. 264–278.) Progress in the manufacture and application of these devices is reviewed. Characteristics of many available types are tabulated.

621.314.7 **3148** Diffusion Capacitance in Transistors. —K. Böke, J. B. M. Spaapen & N. B. Speyer. (*Philips Res. Rep.*, April 1959, Vol. 14, No. 2, pp. 111–122.) Calculations taking into account the influence of the second junction are in agreement with the results of capacitance measurements at different temperatures, voltages and frequencies.

621.314.7 **3149** A Particular Problem of Temperature Distribution concerning the Theory of Junction Transistors.—A. Pignedoli. (*R.C. Accad. naz. Lincei*, Nov. 1957, Vol. 23, No. 5, pp. 257–262.) The temperature distribution as a function of position and time is analysed for a cylinder of circular or elliptical cross-section; the solution is applicable to the investigation of temperature distribution in a transistor whose junction temperature is raised.

621.314.7:546.28:621.317.3 3150 The Measurement of the Temperature Dependence of the Mobility and Effective Lifetime of Minority Carriers in the Base Region of Silicon Transistors. —D. M. Evans. (J. Electronics Control, March 1959, Vol. 6, No. 3, pp. 204-208.) The mobility of holes in the base of a fusionalloy p-n-p transistor was found to vary with the absolute temperature T as $T^{-2\cdot 1}$; the corresponding result for electrons in the base of a grown-junction n-p-n transistor was $T^{-2\cdot 5}$. Results for the effective lifetime of minority carriers in the base are also given.

621.314.7 : 621.317.7		3151
A Transistor	Characteristic	Curve
TracerYoung.	(See 3060.)	

621.314.7:621.385.4 **3152 Theory and Use of Field-Effect Tetrodes.**—H. A. Stone, Jr. (*Electronics*, 15th May 1959, Vol. 32, No. 20, pp. 66–68.) Characteristics and circuit applications of the device are discussed and a description is given of a technique by which laboratory

Electronic & Radio Engineer, September 1959

models have been constructed.

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Transmission-Line Analogue of a Drift Transistor .-- J. te Winkel. (Philips Res. Rep., Feb. 1959, Vol. 14, No. 1, pp. 52-64.) A method is described based on a constant drift field, for deriving base transport parameters and the small-signal equivalent circuit without solving the differential equations explicitly.

621.314.7.012.8

Three-Dimensional Electric-Circuit Model of the High-Frequency Phenomena in a Junction Transistor.-G. Brouwer. (Philips Res. Rep., April 1959, Vol. 14, No. 2, pp. 132–142.) The linearized problem, corresponding to small-signal operation of a transistor, is solved with the aid of a model.

621.383.27

New Photoelectron Multipliers.-N.S. Khlebnikov. (Izv. Ak. Nauk S.S.S.R., Ser. fiz., Jan. 1958, Vol. 22, No. 1, pp. 70-77.) Five types of photomultiplier are briefly described. Typical field distributions and electron paths are illustrated and operating characteristics are tabulated.

621.383.27

Manufacture of Photoelectron Multipliers and Their Basic Parameters .---A. E. Melamid. (Izv. Ak. Nauk S.S.S.R., Ser. fiz., Jan. 1958, Vol. 22, No. 1, pp. 78-82.)

621.383.42

3157 The Open-Circuit Electromotive Force of a Selenium Photocell at Low Temperatures.—G. Blet. (J. Phys. Radium, Feb. 1958, Vol. 19, No. 2, pp. 166-169.) Assumptions concerning the internal mechanism of photocells are checked and a general expression, independent of photocell size, is given.

621.383.5

Photovoltaic Effect in Se Photocells having Artificial Intermediate Layers

of CdSe, CdTe, ZnSe and ZnTe.-H. Tubota & H. Suzuki. (J. phys. Soc. Japan., Jan. 1959, Vol. 14, No. 1, pp. 38-40.)

621.385.029.6

International Convention on Microwave Valves .-- (Proc. Instn elect. Engrs, Part B, 1958, Vol. 105. Supplement No. 11, pp. 609-812.) The text is given of the following papers which were included among those read at the I.E.E. Convention held in London 19th-23rd May 1958. Others are abstracted separately. For titles of papers included in Supplement No. 10 see 2788 and 2800 of August. Technology:

(a) A new Ceramic Waveguide Window for Use on X-Band Valves .- W. F. Gibbons & A. V. Whale (pp. 609-613).

(b) Photo-etching Molybdenum Foil.— H. A. C. Hogg (pp. 614–616).

(c) High-Power Windows at Microwave Frequencies .- J. V. Lebacqz, J. Jasberg, H. J. Shaw and S. Sonkin (pp. 617-622).

(d) Study of the Lives of Dispenser-Type Barium-Tungsten Cathodes .- T. Hashimoto (p. 622).

(e) Application of Discharge Machining to Millimetre-Wave Magnetrons .- M. Nishimaki & T. Asaba (p. 623).

Space-Charge Waves:

(f) Large-Signal Linear-Beam Tube Theory.-C. C. Wang (pp. 624-632).

(g) A Variation Principle for Small-Amplitude Disturbances of Electron Beams. --P. A. Sturrock (pp. 632-634).

(h) Space-Charge Waves on Annular Beams in Drift Tubes .- A. H. W. Beck & P. E. Deering (pp. 635-641).

(i) Magnetic Oscillations in Electron Beams.-R. H. C. Newton (pp. 642-644).

(j) Microwave Amplification using an Unstable Electron Beam in Crossed Electric and Magnetic Fields .- D. J. Harris (pp. 645-648).

Semiconductors and New Methods of Generation :

(k) Parametric Amplification of Space-Charge Waves .- A. Ashkin, T. J. Bridges, W. H. Lousell & C. F. Quate (pp. 649-651). See 1025 of March.

(1) Some Proposals for Generating High-Frequency Electromagnetic Waves using the Doppler Effect.-R. B. R. Shersby-Harvie (pp. 652-655).

(m) Fast-Wave Interactions with an Electron Film at Cyclotron Resonance .---A. Karp (pp. 656-661).

(n) Junction Diodes in Microwave Circuits.—A. Uhlir (p. 661).

(o) Theory of the Microwave Crystal Mixer.--C. Baron (pp. 662-664).

(p) Microwave Amplification by means of Intrinsic Negative Resistances .- E. Rostas & F. Hülster (pp. 665-673).

Resonators and Slow-Wave Structures :

(q) Dielectric Loading for U.H.F. Valves. -G. B. Walker (pp. 717-718).

(r) A Structure, using Resonant Coupling Elements, suitable for a High-Power Travelling-Wave Tube .--- A. F. Pearce (pp. 719-726).

(s) Results on Delay Lines for High-Power Travelling-Wave Tubes .--- P. Palluel & J. Arnaud (pp. 727-729).

(t) Theoretical Investigation of some Closed Delay Structures for High-Power Travelling-Wave Tubes .- F. Sellberg (pp. 730-735).

Discussion (pp. 735-736).

(u) A New Type of Slow-Wave Structure for Millimetre Wavelengths .- E. A. Ash (pp. 737-745).

(v) Multiple Ladder Circuits for Millimetre-Wavelength Tubes .- R. M. White, C. K. Birdsall & R. W. Grow (p. 746). Discussion (p. 746).

(w) Dispersion Curves for a Helix in a Glass Tube .- D. T. Swift-Hook (pp. 747-755).

(x) Some Aspects of the Design of a Helical Coupler for a Travelling-Wave Tube Operating in the 2-Gc/s Band .----P. A. Lindsay & K. D. Collins (pp. 756-761).

(y) Modified Transmission-Line Couplers for Helices.-E. A. Ash & J. D. Pattenden (pp. 762-768).

(z) The Coupling of Three Coaxial Helices.-B. Minakovic (pp. 769-778). Discussion (pp. 778-779).

(aa) Characteristics of Interdigital Circuits and their Use for Amplifiers .-- J. Hirano (pp. 780–785).

Noise :

(bb) Calculations concerning the Noisiness of a Drifting Stream of Electrons.-J. R. Pierce (pp. 786-789).

(cc) Progress in Low-Noise Microwave Tube Design.—W. R. Beam (pp. 790-795).

(dd) Frequency Noise in Travelling-Wave Tubes.-R. Liebscher & R. Müller (pp. 796-799).

(ee) Noise in Backward-Wave Oscillators. -N. W. W. Smith (pp. 800-804).

(ff) Oxide Cathodes for Low-Noise Travelling-Wave Tubes .- E. Windsor (pp. 805-809).

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621.385.029.6

Kinetic Theory of Space-Charge: Part 2-Electron Collisional Damping in the Magnetron (and Diode).-L. Gold. (J. Electronics Control, March 1959, Vol. 6, No. 3, pp. 209-235.) A detailed analysis of the part played by scattering in determining the field and charge distribution in a planar diode or magnetron. Various combinations of magnetic field, scattering frequency and transit time are considered. Part 1: 3696 of 1957.

621.385.029.6

curve.

A.C. Operation of Continuous-Wave Magnetrons.-W. Schmidt. (Electronic Applic., Nov. 1958, Vol. 18, No. 4, pp. 158-162.) English version of 4013 of 1958.

621.385.029.6 3162 **Current Limitation of A.C.-Operated** Continuous-Wave Magnetrons by means of Inductance .- E. G. Dorgelo. (Electronic Applic., Nov. 1958, Vol. 18, No. 4, pp. 163-170.) Adjustment of the angle of flow, combined with high efficiency, can be achieved using a supply unit of low resistance incorporating an inductance of suitable value

in the form of stray inductance or a choke.

3163 621.385.029.6 A Proposed Ferrite-Tuned Magnetron. -A. Singh & R. A. Rao. (J. Instn Telecommun. Engrs, India, March 1959, Vol. 5, No. 2, pp. 72-76.) The frequency of an inverted interdigital magnetron can be controlled by varying a biasing magnetic field applied to a ferrite cylinder placed near the shorted end of a coaxial line which is coupled to the interdigital resonator. A tuning range of 5-10 % may be expected as

621.385.029.6 : 621.372.8 3164 Backward-Wave Oscillations in an Unloaded Waveguide.-R. H. Pantell. (Proc. Inst. Radio Engrs, June 1959, Vol. 47, No. 6, p. 1146.) Using a system in which electrons travel in a helical beam in ordinary S-band waveguide, oscillations have been observed in the range $2 \cdot 5 - 4 \text{ kMc/s}$ at a power level of 0.4 W.

shown by a theoretically evaluated tuning

621.385.029.6:621.396.822 3165 An Experimental Study of Interception Noise in Electron Streams at Microwave Frequencies.--B. A. McIntosh. (Canad. J. Phys., March 1959, Vol. 37, No. 3, pp. 285–299.) The frequency used was 3 kMc/s. An electron beam was produced in a demountable vacuum system by a parallel-flow Pierce gun in a confining

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magnetic field. A series of circular apertures and mesh grids on a plate capable of being moved within the vacuum chamber intercepted various fractions of the beam current. The excess noise caused by interception was measured at the anode of the electron gun and at various points in a drift region. Interception noise caused by mesh grids was much greater than that caused by circular apertures.

621.385.032.213.13:538.632 **3166 Hall Effect in Oxide Cathodes.**—T. Yabumoto. (*J. phys. Soc. Japan*, Feb. 1959, Vol. 14, No. 2, pp. 134–139.) The apparent electron mobility in the range 700° K– $1 200^{\circ}$ K was about 10^{3} – 10^{4} cm²/V.sec which is very high as compared with the values obtained for single crystals. The pore conduction hypothesis is discussed.

621.385.1:621.3.049.7

Thermionic Integrated-Micromodules.—Beggs, Grattidge, Molenda, Haase & Dickerson. (See 2863.)

621.385.1 : 621.314.7 : 621.373.43 **3168 Tube-Transistor Hybrids Provide Design Economy.**—Dunn & Hekimian. (See 2877.)

621.385.1:621.317.61

A Method for the Accurate Measurement of Mutual Conductance of Thermionic Valves.—Child & Sargent. (See 3059.) The Mu of Ordinary Receiving Tubes.—G. D. O'Neill. (Sylvania Technologist, Oct. 1958, Vol. 11, No. 4, pp. 125–132.) A distinction is made between the electronic mu and the electrostatic mu. A new formula is given for mu in terms of electrode dimensions; it is simple to evaluate and more accurate than others which are available.

621.385.832 : 621.397.62

Design of a Flat Rectangular C. R. Tube.—W. R. Aitken. (*Electronic Equipm. Engng*, Dec. 1958, Vol. 6, No. 12, pp. 24–28.) A qualitative description with a note on operating experience. See 977 of 1958 for detailed analysis.

621.385.832 : 621.397.621.2 : 535.623 3172 Errors of Magnetic Deflection : Part 2.—Haantjes & Lubben. (See 3125.)

621.385.832.032.36

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Energy Losses of Cathode Rays at Binder Films of the Phosphor Screens of Cathode-Ray Tubes.—G. Gergely & I. Hangos. (Z. angew. Phys., May 1958, Vol. 10, No. 5, pp. 225–228.) Measurements of light emission were made on a number of phosphor screens with colloidal binder films of differing composition and thickness, to determine the dependence of losses on electron energy and film characteristics.

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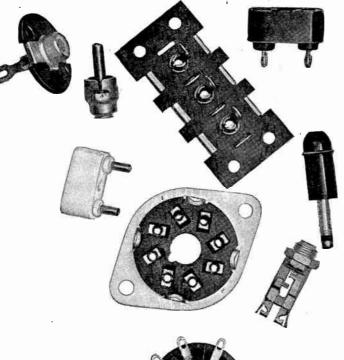
The Effect of Trigger Pulse Polarity on the Anode Breakdown Time of the Cold-Cathode-Arc Conduction Tetrode. —R. Feinberg. (*J. Electronics Control*, March 1959, Vol. 6, No. 3, pp. 246–257.) The breakdown time is found to depend on the trigger pulse duration if this pulse is positive, but not if it is negative. The explanation of this result is discussed.

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621.3.029.6 3175 Report of Advances in Microwave Theory and Techniques-1957.--R. E. Beam. (Trans. Inst. Radio Engrs, July 1958, Vol. MTT-6, No. 3, pp. 251-263.) 320 references.

621.37/.39(81) 3176 Electronics and Communications in Brazil.—J. I. Caicoya. (Brit. Commun. Electronics, May 1959, Vol. 6, No. 5, pp. 364–370.) Gives details of manufacturing and research organizations.





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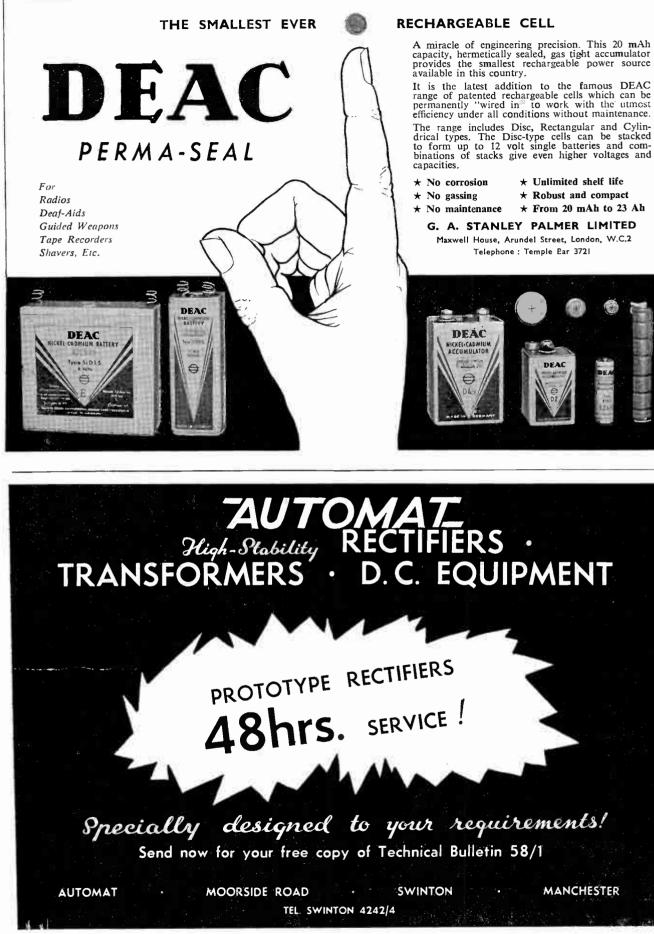
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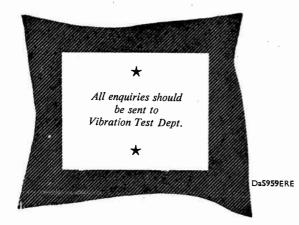
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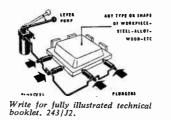
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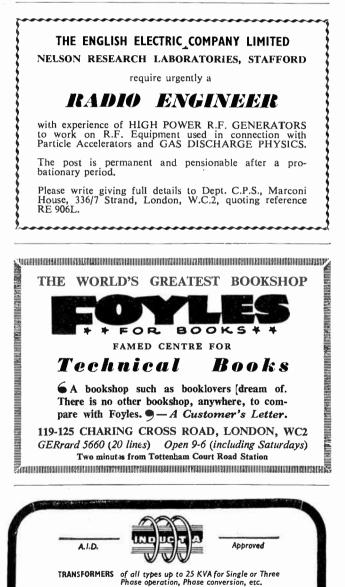
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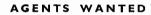
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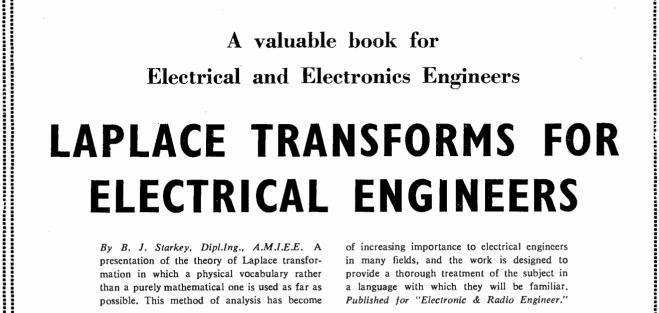
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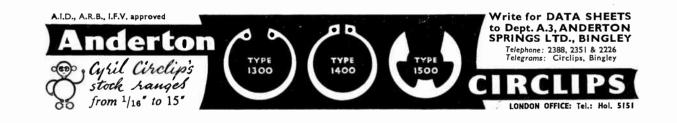
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Index to Advertisers

PAGE	PAGE	PAGE
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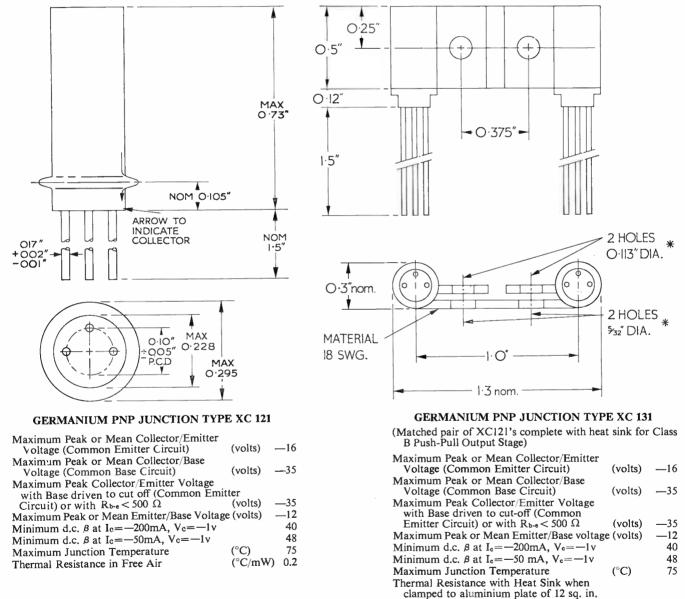
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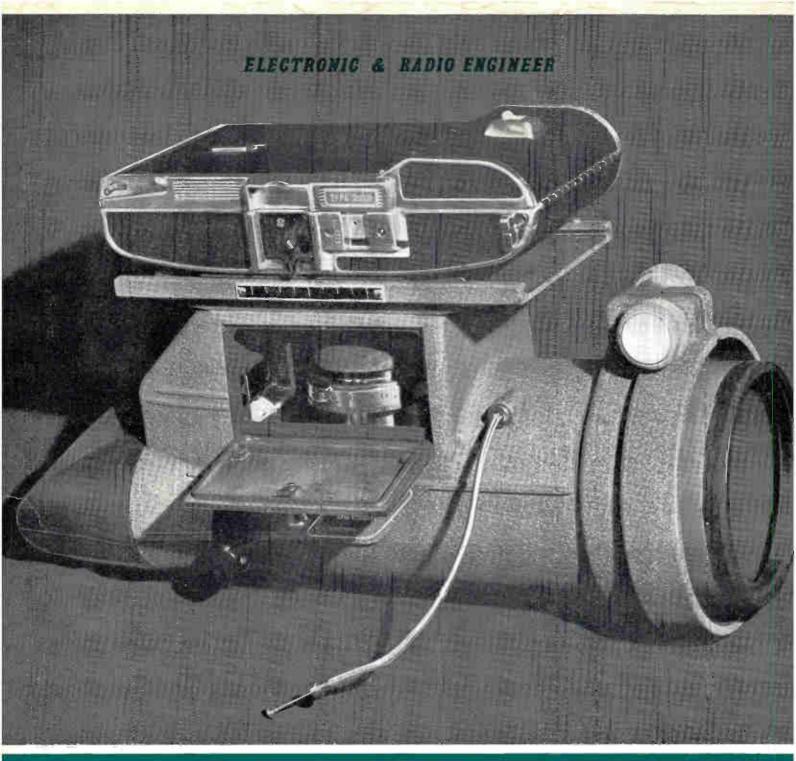
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Index

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INDEX TO ABSTRACTS AND REFERENCES

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a.c.	alternating current
d.c.	direct current
h.v.	high voltage
l.v.	low voltage
a.f.	audio frequency
i.f.	intermediate frequency
r.f.	radio frequency, including :
v.l.f.	very low frequency, <30 kc/s
1.f.	low frequency, 30–300 kc/s
m.f.	medium frequency, 300–3000 kc/s
h.f.	high frequency, 3–30 Mc/s
v.h.f.	very high frequency, 30-300 Mc/s
u.h.f.	ultra high frequency, >300 Mc/s
a.m.	amplitude modulation
f.m.	frequency modulation
p.m.	pulse modulation, including:—
p.a.m.	pulse amplitude modulation
p.c.m.	pulse code modulation
p.f.m.	pulse frequency modulation
p.ph.m.	pulse phase modulation
p.p.m.	pulse position modulation
p.w.m.	pulse width modulation
ph.m.	phase modulation
v.m.	velocity modulation
c.w.	continuous wave
i.c.w. J	modulated c.w.
m.c.w. J	
s.w.*	short wave
u.s.w.*	ultra short wave
λ	wavelength
c.r.	cathode ray
c.r.o.	cathode-ray oscilloscope
d.f.	direction finding
e.m.	electromagnetic, but
e.m.f.	electromotive force
e.s.	electrostatic
a.f.c.	automatic frequency control automatic gain control
a.g.c.	
a.ph.c.	automatic phase control automatic volume control
a.v.c.	maximum usable frequency
m.u.f.	plan position indicator
p.p.i. s.s.b.	single sideband
d.s.b.	double sideband
-	standing-wave ratio
s.w.r. v.f.o.	variable-frequency oscillator
R/T	radiotelephony
W/T	wireless telegraphy
TV	television
. •	

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CONTENTS Abbreviations I.1 Author Index I.2 Subject Index I.35

List of Journals I.51

Errata I.51

Book Review B Note of Correction Discussion D

A name followed by 'and' is that of the first author of a jointly written paper, while the word 'with' indicates that the name indexed is that of the second author

Author Index

Symbols

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AUTHOR INDEX

- Aaron, M. R., with J. A. Narud, transistor blocking oscillator, 2504
 Abbott, W. N., displacements of radiant point during auroral disturbance, 138; seasonal illumination of circumpolar earth satellite, 793
 Abdullaev, G. B., and A. A. Bashshaliev, thermal conductivity of Se, 1606
 Abe, H., paramagnetic resonance in copper propionate monohydrate, 98
 Abel, J. L., with A. G. Chynoweth, polarization reversal in triglycine sulphate, 3742
 Abkevich, I. I., distribution of slow traps on surface of Ge and Si, 3768
 Abraham, M., M. A. H. McCousland and F. N. H. Robinson, dynamic nuclear polarization, 3412
 Abrikosov, A. A., L. P. Gorkov and I. M. Khalatnikov, superconductor in high-frequency field, 2195
 Abrikosov, N. Kh., with L. D. Dudkin, alloying of

- 2195
 Abrikosov, N. Kh., with L. D. Dudkin, alloying of semiconductor compound CoSb₃, 2667
 Acheson, M. A., interaction reliability, 1038
 Adams, E., with others, sendust flake, 894
 Adams, I., with others, electroluminescence of AlN, 4082

- 4082
 Adams, J. A., miss-distance indicator, 2601
 Adcock, F., radio direction finding in three dimensions, 3314
 Addington, R. E., with A. J. Goss, effects of seed rotation on Si crystals, 3021
 Adirovich, E. I., and K. V. Temko, transition frequency and phase characteristics of transitor, 634 Adirovich, E. I., and K. V. Temko, transition frequency and phase characteristics of transistor, 634.
 Yu. S. Ryabinkin and K. V. Temko, field potential and charge carriers in fused-in junctions, 3787
 Adlam, J. H., and J. E. Allen, structure of collision-free hydromagnetic waves, 1162
 Adler, R., and G. Hrbek, low-noise electron-beam parametric amplifer, 321
 with G. Wade, method for pumping fast space-charge wave, 1412
 Agarwal, P. D., eddy current losses in Fe, 4130
 der Agohian, R., detection of non-ionizing shock waves, 3447
 and L. Lijschitz, propagation of non-ionizing shock waves, 4016
 Agostinelli, C., spherical vortices in magneto-hydrodynamics, 92
 Agranovich, V. M., and A. A. Rukhadze, propagation of e.m. waves in medium with spatial dispersion, 2921
 V. E. Pafomov and A. A. Rukhadze, Cherenkov radiation in medium with spatial dispersion, 3648
 Agranovskaya, A. I., with others, nonferroelectric phase transitions in solid solutions, 1912; effect of polarization on Pb_NiNb_Og-Pb_3MgNb_Og. 2631; new ferroelectric, 2632
 Agrawal, D. B., with M. S. Sodha, low-field mobility of carriers in nondegenerate semiconductors, 164
 Agusta, B., sorting components by measuring waveforms, 1645
 Ahačić, A., reactance transformation of low-pass ladder networks, 2152
 Ahlstrom, E., W. G. Matthei and W. W. Gärtner, surface-barrier photodiodes as photocapacitors, 3885
 Ahmed, R., with R. Fatehchand, electronic speech same 2820

- 3885
 Ahmed, R., with R. Fatehchand, electronic speech sampler, 2820
 Aiken, W. R., fat rectangular c.r. tube, 3171
 Ainsworth, J., with F. H. Harris, single-line-scan television, 2033
 Aitchison, C. S., frequency synchronization of reflex klystron, 3524 y
 Aitchison, G. J., and K. Weekes, ionospheric informa-tion from observations of satellite 1957 a2, 326
- Altenson (G. 9., and A. Preses, complete Information from observations of satellite 1957 a2, 3296
 J. H. Thomson and K. Weekes, ionospheric information from observations of satellite 1957 a2, 3297
 Aitchison, R. E., breakdown voltage of Ge transistors, 3519
 with C. T. Murray, high-stability valve heater supply, 1697
 Aitken, D. K., long-transit-time multipactoring at u.h.f., 3524c
 Altya, S. V. C., average power of impulsive atmospheric noise, 1354
 Akimoto, S., T. Katsura and M. Yoshida, magnetic properties of Tife₂O₂-Fe₂O₄ system, 542
 Akita, K., with others, temperature fluctuations accompanying solar eclipse, 2559
 Akulov, N. S., and A. V. Cheremushkina, Hall effect at Curie point, 2680
 Albanese, V. J., and W. P. Peyser, analysis of a broad-band coaxial hybrid ring, 3552
 Albrecht, H. J., instrument effects in ionosphere data, 807, great-circle propagation between Australia and Europe, 2777
 Alcock, B. J., 4-pole analysis for transistors, 48
 Aldrich, R. W., and N. Holonyak, Jr, Si-controlled rectifiers from oxide-masked diffused structures, 2418
 Aleksandrov, V. T., with S. V. Suechnikov, phototion 3296

- 2418
 Aleksandrov, V. T., with S. V. Suchnikov, photo-electric properties of CdSe and CdTe, 468
 Alekseeva, V. G., and chers, influerce of group III and V elements on recombination in Ge, 1614
 Alers, G. A., J. R. Neighbours and H. Sato, depend-ence of sound attenuation on magnetization direction in Ni, 4125
 Alexander, W. M., with others, rotating-disk function generator, 2858
 Alimov, Yu. I., with G. V. Skrotskil, ferromagnetic resonance in circularly polarized e.m. field, 3646

- I.2

- Allan, A. H., and J. E. Drummond, Doppler measurements on Soviet satellites, 443
 Allan, D. W., reversals of earth's magnetic field, 436
 Allanson, J. T., network synthesis, 1113; synthesis of LC networks, 2147; network characteristics, 2167
- of LC networks, 2147; network characteristics, 2496 Allcock, G. MCK., electron density distribution in outer ionosphere, 3307 and M. G. Morgan, solar activity with whistler dispersion, 144 Allen, C. P., and M. Sherry, measurement of
- dispersion, 144 Allen, C. P., and M. Sherry, measurement of magnetic flux density, 3056

- magnetic flux density, 3056
 Allen, E. J., frequency-shift telegraph receiver, 1675
 Allen, J. E., with J. H. Adlam, structure of collision-free hydromagnetic waves, 1162
 Allen. J. W., delay time in plastic flow of InSb, 3387
 and F. A. Cunnell, diffusion of Zn in GaAs, 1259
 Allen, P. J., and R. D. Tomphins, instantaneous microwave polarimeter, 3432
 Allerton, G. L., microwave directional couplers, 3936
 Allogier, P. S., magnetoresizance in PS, PbSe and

- Allerton, G. L., microwave directional couplers, 3936
 Allerton, G. L., microwave directional couplers, 3936
 Allerton, R. S., magnetoresistance in PbS, PbSe and PbTe, 1267
 and W. W. Scanlon, mobility in PbS, PbSe and PbTe, 181
 Allin, P. E. V., tuning of coupled-cavity reflex klystrons, 3524 cc
 Allred, W. P., with others, preparation and characteristics of single-crystal InP, 4114
 Allsopp, H. L., and D. F. Gibbs, electromechanical properties of BaTIO, 3333
 Almer, F. H. R., and P. G. Van Zanten, transistor pyrometer, 3424
 Al'pert, Ya. L., ionosphere and artificial satellites, 1873; conditions in outer ionosphere, 2967; investigation of ionosphere by earth satellite, 3295
- 3295
 and others, electron concentration of ionosphere from observations of first earth satellite, 3298
 van Alphen, P. M., interference of light in thin films, 1701
 Alsop, L. E., with others, maser amplifier for radio
- astronomy, 2892 Ament, W. S., airborne radiometeorological research, 2726

- 2726
 with others, measurements of 1250-Mc/s scatter propagation, 3096
 Amer, S., nonlinear theory of plasma oscillations, 88
 Ames, L. A., and T. F. Rogers, 220-Mc/s reception at 700-1000 miles, 1351
 E. J. Martin and T. F. Rogers, persistent v.h.f. field strengths beyond radio horizon, 2737
 Amster, L., with others, echo in television images, 3134
 Amgueya A. A. calculations for picton two piccos
- Anan'eva, A. A., calculations for piston-type piezo-
- Anan'eva, A. A., calculations for piston-type piezo-electric radiator, 1045
 Anastassiades, M., and L. Carapiperis, influence of meteorological factors on u.h.f. propagation, 1333 m
 C. Caroumbalos and C. Bouloheris, optimum radiation from sawtooth aerial, 3578
 Anderson, D. A., CdS and CdSe photistors, 1011
 Anderson, D. G., luminescence and luminescent materials, 1595
 Anderson, J. C., surface impedance, 1306
 and B. Donovan, internal ferromagnetic resonance in Ni, 2684
 and T. Winer, temperature-stabilized phototranistor relay circuit, 1109
 Anderson, J. C., aufation associated with solar radio noise storm, 429
 Anderson, L. J., with L. G. Trolese, foreground terrain effects, 3457
 Anderson, M. E., magnetic head reads tape at zero speed, 2020
 Anderson, O., and others, hydromagnetic capacitor, 1843

- Anderson, O., and others, hydromagnetic capacitor, 1843
 Anderson, P. W., spectral diffusion, phonons and paramagnetic relaxation, 3652
 Anderson, S. R., and R. B. Flint, C. A. A. Doppler omnirange, 2610
 Anderson, W. P., and N. A. Godel, latching counters, 58
 Ando, K., and others, oxide-cored cathode, 3078
 Andrés, P., with others, influence of high-energy electron bombardment on Ge, 3773
 Andresen, M. G., propagition of fundamental modes in curved waveguides, 3929
 de Andrés, M. P., with W. Jellinghaus, crystal anisotropy and magnetostriction with Hall effect, 3803
 Andresen, P., O. Sette and S. Tiberio, characteristic parameters of barrier layer in metal/ semiconductor junction diodes, 2415
 Andrew, P., electroforming of waveguide components, 1436; broad-band circular wavemeters, 3066
 Andrich, W., with K. Küpfmüller, speech trans-
- 3066 Andrich, W., with K. Küpfmüller, speech trans-mission with quantization, 3855 Angel, Y., and G. A. Boutry, parametric amplifiers and cancellation of ferromagnetic hysteresis, 3244

- 3244
 Angell, B. C., and others, propagation measurements at 3480 Mc/s, 2000 r
 Angstadt, R. T., with P. Rüetschi, self-discharge reactions in batteries, 2403
 Angulo, C. M., and W. S. C. Chang, excitation of dielectric rod by cylindrical waveguide, 3558
 Anisimova, Yu. V., with R. G. Mirimanov, circular waveguide partially filled with ferrite, 2116

World Radio History

- Anson, W. J., with others, water cooling of low-power klystrons, 312
 Antes, L. L., progress in CdS, 829
 Aol, S., and others, magnetrons for min A, 4248
 Aono, Y., and K. Kawakami, cosmic rays observed by satellite 1958 a, 448
 Aoyagi, K., with others, ferromagnetic domain structure in Co-Ni crystal, 192
 Apker, L., with others, two-stage optical excitation in phosphors, 2966
 Apple, E. F., with others, two-stage optical excitation in phosphors, 2996
 Applebaum, M., and E. Midgley, f.m. receiver using transistors, 4188
 Appleton, E. V., E region of ionosphere, 1554
 Arai, M., with others, effect of solar eclipse on geomagnetic field, 2562
 Arams, F. R., low-field ruby maser, 3624
 and G. Krayer, low-loss L-band circulator, 1769
 and S. Okwit, tunable L-band ruby maser, 2523
 Arbell, H., with A. M. Thompson, comparator for 100. Kc/s frequency standards, 1299
 Yon Ardenne, M., and H. B. Sprung, ingestible intestinal transmitter, 1327, 3834
 Arendt, P. R., magneto-ionic effect above F layer, 2961; measurements on Doppler shift of satellite emissions, 3697
 Arlies, R., Ta capacitors, 2137
 Arima, Y., with T. Yonezawa, F. layer, semidiumal lunar variations of, 196, variations in electron density of, 4055
 with others, electron and ion density distributions in Fergion, 2579
 Armstrong, G. T., P. K. Wong and L. A. Krieger, use of d.c. amplifier and recorder to balance resistance bridge, 3061
 Armstrong, R. L., electrical recovery of gas after pulse discharge, 2531; eddy-current heating, 2716
 Armstrong, R. L., Warnecke, increase of bandwidth

pulse discharge, 2531; eddy-current heating, 2716
Armstrong, R. L., with M. S. Rao, radio reflections along meteor train, 2226
Armaud, J., and R. Warnecke, increase of bandwidth in O-type traveling-wave valves, 317
with P. Palluel, results on delay lines for travelling-wave tubes, 3159 s
with others, characteristics of carmatron tube, 2188 r
Arnold, J. S., and J. G. Martner, resonances of BaTiO, cylinders, 2446
Arnoldy, R., with others, auroral phenomena during storm, 3309
Aroyan, G. F., spatial filtering, 4165
Arp, F., with others, ninority carriers in dislocated Ge, 1618
Arthur, J. B., and J. Henry, laws of magnetism and static electricity, 1514
Asaba, T., with M. Nishimaki, discharge machining for mm-wave magnetrons, 3159 e
Asanabe, S., electrical properties of SnSe, 3389

Asanabe, S., electrical properties of SnSe, 3389 — and A. Okazaki, Hall coefficients of SnSe and GeSe, 2669 Asch, G., magnetic resonance of polycrystalline Co, 3802

Gese, 2609
Gese, 2609
Asch, G., magnetic resonance of polycrystalline Co, 3802
Aschen, R., passive television relay, 2851; passive relay by microwave mirror, 2852
with L. Chrétien, compatible system for colour television, 1700; synchrophase, 3116
Ash, E. A., magnitude of locking signal for backwardwave oscillators, 2788 b; slow-wave structure for mn h, 3159 u
and J. D. Pattenden, modified transmission-line couplers for helices, 3159 y
Ashby, D. E. T. F., wave matrices applied to periodically loaded travelling-wave tube, 1020
and R. B. Dyott, measuring modulation noise of c.w. klystron amplifer, 3524 k
Ashkin, A., parametric amplification of space-charge waves, 3159 k
Aspinwall, J. F. H., 'third' method, 970
Assaly, R. N., dielectric sphere as microwave lens, 714
d'Asst, L., with F. Perrier, rapid testing of direct-voltage stabilizers, 608
Atala, B. S., method of calculating reverberation-chamber coefficients, 3921
Atala, M. M., E. Tamenbaum and E. J. Scheibner, stabilization of Si surfaces by thermally grown oxides, 2650
Athwavle, V. N., with M. W. Chiplonkar, recording of atmospherics in 1.f. region, 813
Atiya, F. S., band-pass amplifier, 2512
Atkinson, M. P., W. T. Bane and D. L. A. Barber, automatic graph plotter, 2859

Electronic & Radio Engineer

- Atlas, D., meteorological 'angel' echoes, 2603
 Atwood, J. B., and others, 468-Mc/s tropospheric scatter propagation, 245
 Audoin, C., with R. P. Musson-Genon, electronic hysteresis and secondary emission in reflex klystrons, 3524 gg
 Auer, P. L., and H. Hurwitz, Jr, space-charge neutralization in diodes, 2432
 H. Hurwitz, Jr, and S. Tamor, theory of cathode sheath in discharge, 82
 Augustyniak, W. M., with W. L. Brown, defect formation in electron irradiation of n-type Ge, 4110
 with others, annealing of radiation defects in

- 4110
 with others, annealing of radiation defects in semiconductors, 4089 o
 Aukerman, L. W., radiation-produced energy levels in semiconductors, 4089 m
 Ault, C. F., digital-to-analogue conversion for storage-tube deflection, 2135
 Austin, I. G., optical properties of Bi₂Te₃, 533; Faraday effect in anisotropic semiconductors, 3018
- Fara 3018

- Austary careet in anisotropic semiconductors, 3018
 Austin, N. A., and S. C. Fullz, 22-MeV electron linear accelerator, 2719
 Autler, S. H., maser amplifier system, 388
 Avak'yants, G. M., theory of transfer phenomena on semiconductor surface, 2280
 Avignon, Y., and M. Pick, relation between type-IV emissions and other solar activity, 3283
 Avins, J., T. Brady and F. Smith, synchronous and exalted-carrier detection, 1378
 Awender, H., crystal-resonator techniques, 2142

 and A. Ludioff, crystal-controlled transistor oscillators, 1129
 Ayakawa, T., with others, life tests of microphone
- oscillators, 1129 Ayakawa, T., with others, life tests of microphone carbon, 1758 Ayres, W. P., broad-band λ/4 plates, 1081; mm-wave generation utilizing ferrites, 3983 Azbel', M. Ya., quantum theory of conductivity, 762; h.f. surface impedance, quantum oscilla-tions of, 763, quantum theory of, 1221
- Baba, K., with others, magnetrons for mm-λ, 4248
 Babcock, H. W., with others, magnetic field associated with solar flare, 4043
 Babcock, W. E., tube effects cause circuit troubles,

- associated with solar late, 4043
 associated with later 3688

- measurement of time dilation in earth satellite, 3688
 Baer, W., with others, conduction of heat from anodes, 4252
 Baghdady, E. J., and G. J. Rubissow, dynamic trap for weak i.m. signals, 1350
 Bagl, R. R., with H. R. Johnson, electron beam technique for measuring circuit velocity, 3524 o
 Bahr, O. F., with E. Zeiller, quantitative electron microscopy, 3444
 Bailley, D. K., abnormal ionization in ionosphere and cosmic-ray enhancements, 1562; effect of echo on h.f. communication circuits, 3471
 Bailley, G. C., with others, effect of neutron irradiation on Curie temperature of ferrites, 898
 Bailley, R., and E. C. Fellows, stabilization of 9-kW electromagnet, 3072
 with others, 308
 Bailley, V. A., possible effects of gyro-waves in ionosphere, 3308
 Bailley, L. L., and R. J. Spellmire, radiation fields from slots in circular cylinders, 1093
 Bail, L. L., R. Shaerman, observations on

- Bain, W. C., angular distribution of energy received by ionospheric scatter, 2000 h
 and E. D. R. Shearman, observations on U.S.S.R. earth satellites, 2952
 Baines, J. E., with D. H. Roberts, photoconductivity in PDSe films, 830
 Baker, B. W., with others, dual-cavity microwave discriminator, 1487
 Baker, D., machine for lapping semiconductor materials, 1943
 Baker, J. M., W. Hayes and D. A. Jones, para-magnetic resonance of impurities in CaF₄, 3411 with others, r.f. spectra of hydrogen deuteride, 1852
 Baker, W. P., high-speed-sweep single-stroke
- Baker, W. P., high-speed-sweep single-stroke oscilloscope, 1317 Baker, W. R., with others, hydromagnetic capacitor,
- 1843
- Bakhru, K., with others, triple splitting of F echoes, 1885 Balashek, S., with H. Dudley, automatic recognition
- Balasnek, S., with H. Dudley, automatic recognition of phonetic patterns in speech, 1061
 Baldinger, E., transistor applications in pulse circuits, 3228
 H. Bilger and M. A. Nicolet, influence and creation of lattice defects in junction transistors, 2771
- 2771
 Baldwin, J. E., with J. R. Shakeshaft, radio emission from 'supergalaxy', 3660
 Balkanski, M., and R. D. Waldron, internal photo-effect and exciton diffusion in CdS and ZnS, 824
- Balluffi, R. W., with F. L. Vook, irradiated Ge, length and resistivity changes in, 2306, structure of, 2308

- Balser, M., scattering by turbulent inhomogeneities, 1335
 W. B. Smith and E. Warren, reciprocity of ionospheric transmission, 1667
 Banbury, P. C., with J. D. Nizon, changes in excess-carrier concentrations, 1228
 Bancle-Grillot, M., and others, luorescent emission lines and luminous absorption lines in CdS, 2618
 with others, influence of magnetic field on fluorescence of pure CdS, 2622
 Bane, W. T., with others, automatic graph plotter, 2859
 Bancell, R. B., asymmetric information channels

- Banerji, R. B., asymmetric information channels, 3103
- 3103
 Banks, E., with A. H. Mones, cation substitutions in BaFe₁₂O₁₉, 540; [ferrimagnetism in system Na₄O-ZnO-Fe₂O₃, 904
 Bannerman, R. C., J. A. Lucken and D. J. Wootton, design of gridless low-voltage reflex klystron, 3524 dd
- others, experimental annular reflex klystron, with oin 3524 bb

- 3524 bb Banno, N., with others, effect of solar eclipse on geomagnetic field, 2562 Bappu, M. K. Vaina. See Vaina Bappu, M. K. Baranova, Z. N., and K. A. Velizhanina, acoustic properties of sound-absorbing material, 686 Baranskil, P. I., volume Peltier effect in Ge, 3776 and V. E. Lashkarev, bulk thermo-e.n.f. in Ge, 524

- and v. E. Lassharev, but the information of the second state of the secon
- 1981
 Barkhatov, A. N., acoustic field in medium with homogeneous surface layer, 666
 and I. I. Shmelev, attenuation of sound beam traversing layer of discontinuity, 669
 Bar-Lev, A., negatively biased multivibrator, 55
 Barlow, D. A., rigidity of loudspeaker diaphragms, 334
 Barlow, H. D. K.
- Barlow, D. A., rigidity of loudspeaker diaphragms, 334
 Barlow, H. E. M., power radiated by circulating surface wave, 2098; propagation around bends in waveguides, 2106
 with L. M. Stephenson, power measurement at 4 Gc/s by Hall effect, 1312
 Barnes, R. C. M., and J. H. Stephen, operating experience with transistor digital computer, 2132
 Barnette, W. E., with H. Kihn, microminiature decoder for selective communication, 2018
 Barron, C., theory of microwave crystal mixer, 3159 o
 Barrar, R. B., and C. H. Wilcox, Fresnel approximation, 1442
 Barrington, A. E., and J. R. Rees, 3-cm Q-meter, 562
 Barron, D. W., and K. G. Budden, numerical solution of equations governing reflection of long waves from ionosphere, 3455
 Barry, A. L., and J. M. Fornwalt, underwater missile tracking instrumentation, 2597
 Barryis, A. P., tropospheric radio wave propagation, 234
 Barsukov, Yu. K., blocking junction process in planar Ge diodes. 1708: circuit transistorized pulse amplifier, 2518

- Janky, J. N., and D. M. Leakey, transistorized pulse amplifer, 2518
 Barsis, A. P., tropospheric radio wave propagation, 234
 Barsukov, Yu. K., blocking junction process in planar Ge diodes, 1708; circuit representation of semiconductor diode, 2035
 Bartels, J., cause of air resistance changes in satellite orbits, 1186
 Barth, B. P., with others, electrical properties of epoxy resins, 911
 Barthel, F., investigations of nonlinear Helmholtz resonators, 1424
 Bartnch, R. H., and M. C. Pease, space-chargelimited crossed-field gun, 3894
 Bartacta, A., with H. Gobrecht, semiconductor properties of SnS, 886; elastic properties of hexagonal CdS, 2278; piezoelectric and elastic behaviour of CdS, 3746
 Baruch, P., with others, influence of high-energy electron bombardment on Ge, 3773
 Barzilai, G., and G. Gerosa, modes in guides filled with magnetized ferrite, 1770
 Bashkirov, Sh. Sh., with K. A. Valiev, stimulated r.f. paramagnetic amplifiers, 2181
 Bassey, F. G., with Achers, auroral ionosphere studies using earth satellites, 4052
 Bassy, F. G., with A. K. Mare, statistical theory of propagation over ideally conducting plane, 3840
 Battdorf, R. L., and F. M. Smits, diffusion of impurities into evaporating Si, 1925
 Bate, R. T., R. K. Willardson and A. C. Beer, transverse magnetoresistance and Hall effect in n-type InSb, 4119
 Bateman, R. H., J. McSkimin and J. M. Whelan, elastic moduli of GaAs, 3360
 Bates, L. F., and D. J. Sansom, magnetothermal effects in Fa and SiFe, 4129
 Bath, H. M., and M. Cutler, measurement of surface recombination velocity in Si by steady-state photoconductance, 1246
 Battaglia, A., G. Boudouris and A. Goszini, refractive index of humid air, 1333 n

World Radio History

- with F. W. Heineken, absorption and refraction of NH, at 6 mm A, 2213
 Batterman, B. W., X-ray integrated intensity of Ge, 3376, effect of chemical impurities on, 177
 Baty, A. J. B., with others, electronic clock coder for coded radio beacons, 4669
 Bauer, H. J., temperature dependence of resistance of Ni alloys and thin films, 3805
 Bauer, S. J., with F. B. Daniels, Faraday fading of satellite signals, 450
 Bauer, K. J., may the others, thermoelectric materials, InAs and InSb, 3384, In(As, P), 3759
 Baumgrdner, J., magnetic recording of pulse-amplitude data, 1989
 Baur, K., evaluation improvement with 2-channel c.r.d.f., 2258; investigation of polarization properties at 4 Gc/s, 3564
 Bauwens, J. C., digital-analogue converter, 3206
 Bayer, J., with F. B. Bulthgen, pulse generation controlled by heart phases, 4169
 Bayer, M., J. L. Delcroix and J. F. Denisse, wave interaction ings, 1333 a
 Bayh, W., emission microscopy with secondary electrons, 1330
 Bazzard, G. H., with C. M. Minnis, indices of solar activity, 3281
 Beach, E. H., and others, electronic subsystem development problems in naval ordnance, 2803
 Beach, R. E., advances in microwave theory and techniques, 3175
 Beam, R. E., advances in microwave theory and techniques, 3175
 Beam, R. E., advances in microwave theory and techniques, 3175
 Beam, M. R., noise-wave excitation of microwave beam amplifier, 1023; low-noise microwave signal spectra on ocean roughness, 242
 Beard, C. I., and I. Kaiz, dependence of microwave signal spectra on ocean roughness, 242
 Beard, C. J., and I. Kaiz, dependence of microwave signal spectra on ocean roughness, 242
 Beard, D. B., microwave emission from hightermetric with a conselement of the changes on transistor, 631
 Beard, D. B., microwave emission from hight

Beardow, T., waveguide manufacturing techniques, 700

700
 Beattie, A. R., and P. T. Landsberg, Auger effect in semiconductors, 3341
 Beatty, R. W., with G. E. Schafer, measuring directivity of directional couplers, 3821
 — with others, water cooling of low-power klystrons, 312

312
Beauchamp, K. G., and A. J. Tyrrell, image converter equipment for observation of discharges, 3522
Beaver, W. L., experimental high-perveance klystron amplifier, 3524 b
Beck, A. H. W., high-current-density emitters, 3693
and P. E. Deering, space-charge waves on annular beams, 3159 h; 3-cavity L-band pulsed klystron amplifier, 3524 e
and J. Lytollis, mobile Cs frequency standard, 3053
Beck, G. E. and T. G. There sinters. Deering

klystron amplifier, 3524 e
and J. Lytolkis, mobile Cs frequency standard, 3053
Beck, G. E., and T. G. Thorne, airborne Doppler navigation equipment, 2259 e
Becker, F. K., compatible stereophonic sound system, 3474
Becker, G., properties of high-quality oscillator crystals, 1127; pulse-beat method for frequency and phase measurements, 1643; theory of inductive 3-terminal circuit, 1804
Becker, J. J., domain boundary configurations during magnetization reversals, 2319
Becker, R. C., with P. D. Coleman, rectangular and circular mm waveguides, 2463; mm-wave generation, 3982
with others, slow-wave structures for power generation at mm and sub-mm λ, 1743
Becker, W., routine determination of vertical distributions of electron density, 1333 b
Beckmann, P., reflection of u.h.f. waves in troposphere, 1333 o
Beddendo, G., and D. Sette, photoconductivity and lifetime of charge carriers, 3342
Bedford, L. H., magnetic tape recording, 3923
Bedinger, J. F., with others, wind determinations in upper atmosphere, 3302
Beer, H. B., and G. V. Planer, preparing ferrites, 1959
Beer, Y. H., voltage-transfer circuits, 2443
Beegis, J. E., and others, thermionic integrated micromodues, 2863
Bedjartile in anisotropic medium, 3635
Belejarstoile, M. L., M. Beun and J. te Winkel, junction transistor as network element, 1719, 2781, 3518
Beiser, A., external magnetic field of earth, 435
Beitel, F. P., Jr, and E. M. Pugh, Hall effects of Fe-Co alloys, 1953

2781, 3518
Beiser, A., external magnetic field of earth, 435
Beitel, F. P., Jr, and E. M. Pugh, Hall effects of Fe-Co alloys, 1953
Belger, E., measurement of program level, 3187
and F. von Rautenfeld, interference protection ratios for sound broadcasting, 3464
Belgiano, R., Jr, turbulent mixing in scatter propagation, 3088

I.3

with 312

Beljers, H. G., amplitude modulation of cm waves by ferroxcube, 1151
Béll, B., meteorological research in Hungary, 452
Bell, D. A., demodulation and detection, 959
and T. C. Duggan, relative speeds of telegraphic codes, 593
Bell, J. D., with others, ring angels over south-east England. 2982

- and T. C. Duggan, relative speeds of telegraphic codes, 593
 Bell, J. D., with others, ring angels over south-east England, 2982
 Bell, J. S., and K. Brewster, matrices in transistor circuit analysis, 1141
 Bell, M. D., and W. J. Leivo, rectification and photo-effects in semiconducting diamond, 504
 Bell, R. O., with P. C. Fletcher, ferrimagnetic resonance modes in spheres, 2928
 with others, magnetostatic modes of ferrimagnetic spheres, 3813
 Bell, W. E., A. Bloom and R. Williams, microwave frequency standard, 4150
 Bellchambers, W. H., and W. R. Piggott, ionospheric measurements at Halley Bay, 1881
 Belowbeck, E., propagation characteristics of slowwave structures, 650
 Belowsov, V. V., and B. I. Silkin, international scientific collaboration, 3674
 Below, F., simple test pattern for monochrome television 3502
 W. Kroebel and H. Springer, detail recognition on television systems, 2750
 Bemski, G., recombination properties of Au in Si, 862; paramagnetic resonance in electronirradiated Si, 4089 g
 and J. D. Studkers, Au in Si, 2290
 Bendeell, S. L., and K. Sadashige, image retention in image orthicon, 615
 Bender, P. L., with T. L. Skillman, measurement of carth's magnetic field, 112
 Bender, P. L., with T. L. Skillman, incastrent of share-teristics of p-n junctions, 1398; characteristics of p-n junc

2366
Bennett, A. I., electrical phenomena on liquid Ge surfaces, 2656
Bennett, F. D., with G. D. Kahl, coherence requirements for interferometry, 398
Bennett, R. R., and others, circuits for space probes, 3286
W. M. ender series strength forms with

- Bennett, R. R., and others, circuits for space probes, 3286
 Bennett, W. H., solar proton stream forms with laboratory model, 1864
 Bennett, W. R., statistics of regenerative digital transmission, 957
 Bennington, T. W., ionosphere review 1958, 1199; sporadic E and F. Jo. Morien, measurement of surface recombination velocity on 51, 859
 Benoit, H., and J. Hennequin, measurement of geomagnetic field by maser, 3823
 P. Griveit and H. Oltavi, maser-type selfoscillator, 2521; weak-field maser, 2548
 Benoit, R., and J. Kernevez, circuit for recording atmospherics, 2870
 Benoit à la Guillaume, C., with others, light due to recombination of impurities in Ge, 3369
 Benson, F. A., and P. M. Chalmers, effects of argon content in glow-discharge tubes, 2442
 and M. S. Seaman, surface structure of saturated-diode filaments, 1418
 Benson, K. E., with others, constitution of AgSbSe, AgSbTe, AgBiTe, AgBiTe, system, 1270; improvement in floating-zone technique, 2337
 Beretzé, R., transfer function of oscillating system, 3979
 Berezin, Yu. V., with others, large inhomogeneities in F, laver, 2581

- Bertaut, F., magnetostatic energy of α-Fe₄O₈, 893
 Bertaut, F., magnetostatic energy of α-Fe₄O₈, 893
 A. Deschamps and R. Pauthenet, substitution of Al, Ga and Cr in BaO.6Fe₂O₃, 541
 Berteaud, A. J., with R. Vautier, Y-Fe garnet with substituted Cr, g-factor of, 2328, width of absorption curve of, 2329; direct measurement of width of resonance curves, 3814
 von Bertele, H., electron emission from thin Hg films, 1157

- Berz, F., field effect at high frequency, 2640
 Besprozvannaya, A. S., with V. M. Driatski, ionospheric conditions in the circumpolar region, 3717
 Bessey, W. H., with others, electromechanical behaviour of BaTiO, 3334
 Béthoux, P., signal discrimination in Gaussian noise, 1357; discrimination between signals in telecommunication, 2008
 Betzenhammer, B., Al-telegraphy reception disturbed by fading, 1352
 Beun, M., with others, junction transistor as network element, 1719, 2781, 3518
 Bevc, V., J. L. Palmer and C. Süsskind, design of transition region of beam valves, 1017
 Beynon, W. J. G., and G. M. Brown, geomagnetic distortion of region E, 2246
 and G. L. Goodwin, horizontal drifts and temperature in E region, 804
 Bhart, J. N., and P. Dhar Bhowmik, study of noon F, ionization, 2584
 Bhonsle, R. V., and K. R. Ramanathan, cosmic radio noise on 25 Mc/s, 3699 f
 Bhowmik, P. Dhar. See Dhar Bhowmik, P. Bialecke, E. P., and A. A. Dougal, electron-ion recombination coefficient in nitrogen, 125
 Blancon, G., with B. Percni, tropospheric-scatter multichannel telephone links, 1361
 Biard, J. R., with W. T. Matzen, differential amplifier features d.c. stability, 1496
 Bibby, R. J., with others, lightweight airbore navigation system, 2599
 Bibl, K., A. Paul and K. Rawer, variation of ionospheric absorption, 3716
 Bichara, M. R. E., one-triode multivibrator with no filament current, 3988
 Bickelhaupt, M. H., with others, tropospheric scatter system using angle diversity, 2751

- Bickart, T. A., amplitude slicer for signal analysis, 1976
 Bickelhaupt, M. H., with others, tropospheric scatter system using angle diversity, 2751
 Bickerton, R. J., anplification of magnetic field by high-current discharge, 401
 Bickmore, R. W., effective aperture of scanned arrays, 2847
 with H. E. Shanks, four-dimensional e.m. radiators, 2840
 Biermann, L., and R. Lüst, radiation and particle precipitation from solar flares, 1530
 Bilger, H., with others, influence and creation of lattice defects in junction transistors, 2771
 Billing, A. R., step detection, 590; sampling of signals, 1356; multiplex vocoder, 2394
 Billings, J. A., with T. G. Thorne, Doppler navigation systems, 2608
 Bimont, J., band-pass ladder filter half-sections, 3223
 Binder, R. C., with D. A. Gibrech, portable instru-

- 3223
 Binder, R. C., with D. A. Gilbrech, portable instrument for locating noise sources, 2091
 Biondi, M. A., and others, evidence for energy gap in superconductors, 393
 with others, neasurement of attachment of slow electrons in oxygen, 2533
 Biorci, G., and D. Pescetti, behaviour of ferromagnetic materials, 197
 A: Ferro and C. Montalenti, instability of Bloch walls in ferromagnetic material, 535
 Bir, G. L., influence of surface recombination on

- walls in ferromagnetic material, 535
 Bir, G. L., influence of surface recombination on photoconductivity of semiconductors, 2643
 with G. E. Pikus, influence of deformation on properties of *p*-type Ge and Si, 2649
 Birdsall, C. K., travelling-wave tubes using paralleled electron streams, 2788 i
 and A. J. Lichtenberg, travelling-wave focusing for plasma containment, 4022
 with C. C. Johnson, M-J crossed-field travelling-wave tube, 2788 dd
 with others, multiple ladder circuits for mm-wave

- tor plasma containment, 4022
 with C. C. Johnson, M.J crossed-field travelling-wave tube, 2788 dd
 with others, multiple ladder circuits for mm-wave tubes, 3159 v
 Birdsall, T. G., with W. P. Tanner, Jr, definitions of d' and n, 3854
 Birk, M., with M. Simhi, sensitive single-channel pulse-height analyser, 59
 Birman, J. L., theory of piezoelectric effect in zincohende structure, 846; polarization of fluorescence in CdS and ZnS, 2268
 Birrell, A., Olifantsfontein and Derdepoort radio stations, 2015
 Bishop, B. E., with K. L. Berns, high-speed multi-plexing with closed-ring counters, 3218
 Bishop, F. W., highly biased gun on electron microscope, 3443
 Bisson, D. K., and R. F. Dyer, bi-controlled rectifier, 4227
 Bittner, G., wave propagation in plasma cable, 2104
 Bjorkstam, J. L., and E. A. Uehling, magnetic resonance and relaxation in KD_PO, 3743
 Black, J., S. M. Ku and H. T. Minden, seni-conducting properties of HgTe, 4112
 Black, W. N., combined broadcast transmitters, 623
 Blackband, W. T., and others, deduction of electron content from Faraday fading, 2572
 Blackburne, N. F., bridges for semiconductor measurements, 1648
 Blackman, M., and F. Grünbaum, magnetic leakage field in Co, 202
 and N. D. Lisgarten, magnetic models for interpreting domain effects on electron beam, 3407
 Blakemore, J. S., inpurity conduction in In-doped
- Blakemore, J. S., impurity conduction in In-doped
- Blakemore, J. S., impurity conduction in In-doped Ge, 3368
 with K. C. Nomura, decay of excess carriers in semiconductors, 1915
 Blanc, D., and others, ionization chambers as sources of current, 4152
 Blank, K., with A. Hersping, after-effect in ceramic dielectrics, 3328

World Radio History

- Blaser, J. P., and J. Bonanomi, comparison of NH, maser with Cs frequency standard, 915
 and J. De Prins, comparison of astronomical time measurements with atomic frequency standards, 914
 Blatt, F., with others, Zeenan-type magneto-optical studies of interband transitions, 2283
 Blattner, D. J., and F. Sterzer, backward-wave oscillator tubes for 29-74-kMc/s range, 1740; voltage-tunable mm-wave oscillators, 3529
 and F. E. Vaccaro, electrostatically focused travelling-wave tube, 1414
 Bleaney, B., materials for Bloembergen-type masers, 3242
 Bleil, C. E., with D. D. Snyder, mechanism for carrie excitation in CdS, 3004
 Blet, G., open-circuit e.m.f. of Se photocells, 3157
 with D. Vidal, influence of annealing time on thermoelectric power of Se, 2648
 Plevis, B. C., u.h.f. auroral radar observations, 1573
 Blitzer, L., earth oblateness in terms of satellite orbital periods, 2234
 Blodgett, F. W., properties of C., Fs, 3415
 Bloom, M., with A diters, tross-relaxation in spin systems, 3270
 Blomquist, A., with others, microwave frequency standard, 4150
 Bloom, A., with others, microwave frequency standard, 4150
 Blount, E. I., energy levels in irradiated Ge, 2664, 4109; ultrasonic structure and properties of ferrites, 4133
 and M. H. Siruetz, magnetic resonance studies in reaction of Ni-Co ferrite, 3042
 Blumenson, L. E., with others, generalized Rayleigh processes, 210

in reaction of Ni-Co ferrite, 3042
 Blumenson, L. E., with others, generalized Rayleigh processes, 210
 Blüthgen, F., and J. Bayer, pulse generation controlled by heart phases, 4169
 Blyakhman, E. A., and L. A. Chernov, pulsation frequency of field at focus of lens, 4031
 Bock, R., and others, fixed-frequency cyclotron with one dee. 1985

Bockernuehl, R. R., transistor rectifier gives d.c.,

3481
 Bödeker, H., German standards converter technique, 4213

nique, 4213
Bodó, Z., with others, tin.e-dependent spectra of ZnS:Cu, Pb, 4080
Boekhorst, A., with others, stabilization, of line output circuits, 989, 3124, 3871, of line and fran e output circuits, 3123
Boella, M., television study centre, 2761
Boensel, D. W., switching circuits for missile count-downs, 3598
de Boer, E., acoustic interaction in loudspeaker enclosures, 2456
de Boer, F., and W. F. Nienhuis, low-voltage oscilloscope tubes, 2713
Böer, K. W., and H. Guijahr, spectral distribution of photoconductivity in CdS, 1904
and U. Kümmel, electrostatic charging of CdS, 3731

and U. Kümmel, electrostate **3731** H. J. Hänsch and U. Kümmel, rendering visible conductivity inhomogeneities of semiconductors, **3757** *U. Kümmel and W. Misselwitz*, breakdown of

3757
U. Kümmel and W. Misselwitz, breakdown of CdS films, 2993
S. Oberländer and J. Voigt, evaluation of con-ductivity glow curves, 3321
Bogler, B. P., delay distortion correction by time-reversal techniques, 981
Bogle, G. S., and H. F. Symmons, paramagnetic resonance of Fe³⁺ in sapphire, 1949; zero-field masers, 2889
Bogner, G., and E. Mollwo, preparation of ZnO, 878
Bogmolov, V. N., and V. A. Myasnikov, equipment for Hall-effect measurements in semiconductors, 503

for Hall-effect measurements in semiconductors, 503
Bohlmann, H., and A. Rettig, installation for outside sound broadcasts, 4204
Bohn, E. V., current distribution of cylindrical antennas, 1085
Boiko, I. V., theory of field effect, 2639
Boischoft, A., and J. W. Warwick, radio emission following flare, 3276
Boisthott, A., and P. Misme, guided propagation in the Mediterranean, 940
Bok, J., and R. Veilex, semiconductivity experiments on hot electrons in InSb, 3781
with Y. Simon, photoconductivity of ZnTe, 3726
Böke, K., J. B. M. Spaapen and N. B. Speyer, diffusion capacitance in transistors, 3148
Bokov, V. A., piezoelectric properties of polycrystalline solid solutions, 845; temperature dependence of total polarization, coercive force and hysteresis losses, 3745
Boley, F. I., scattering of microwave radiation by plasma column, 769
Bolglano, R., Jr, convective transfer in turbulent mixing, 11661; wavelength dependence in transhorizon propagation, 1666
Bolinder, E. F., Minkowski model of Lorentz space, 1799; geometric analytic theory of transition, 3049; non-Euclidean geometry in quadripole theory, 3606
Bolle, A. P., cable circuits for television trans-

3049; non-Euclidean geometry in quadripole theory, 3606
Bolle, A. P., cable circuits for television transmission, 273
Bolle, G., operation of ionic loudspeakers, 1759; mixing colour subcarrier of variable frequency with black and white picture, 2032
Bolt, F. D., four simultaneous transmissions from one aerial, 1443

Electronic & Radio Engineer

one dee. 1985

- Boltaks, B. I., and B. T. Plachenov, self-diffusion in Se, 1605
 Boltax, A., behaviour of semiconductor and magnetic materials under radiation, 2646
 Bömmel, H. E., and K. Dransfield, hypersonic waves, attenua ion in quartz, 2636, excitation by ferromagnetic resonance, 3817
 Bonage, W. F., v.h.f. communication in port and harbour control, 3480
 Bonanomi, J., and others, improvements in NH₃ maser, 758 g
 with J. P. Blaser, comparison of NH₃ maser with Cs frequency standard, 915
 Bonch-Bruevich, V. L., interaction of electrons with phonons and impurities, 1859; theory of field effect, 3749; recombination centres and trapping levels, 3764
 Bond, M. E., with B. G. Higdon, thyratron stabilized d.c. supplies, 4208
 Bond, W. L., with R. A. Legan, density change in

- d.t. supplies, 4206
 Bond, W. L., with R. A. Legan, density change in Si on melting, 2292
 Bonljoly, P., with I. Eyraud, differential bridge for impedance measurements, 3429
 Bonner, R. E., L. H. Kosowsky and P. F. Ordung, functional characteristic of node determinant,
- 548 Bonnerot, J., investigation of planar electron guns,
- 2708
- Z/108
 Booher, C., increased cooling for power transistors, 636
 Boone, E. M., M. Uenohara and D. T. Davis, Barkhausen-Kurz oscillator at cm λ, 1486

- Boone, E. M., M. Uenohara and D. T. Davis, Barkhausen-Kurz oscillator at cm λ, 1486
 and others, processing Ni-matrix cathodes, 4250
 van Boort, H. J. J., M. Klerk and A. A. Kruithof, interference from fluorescent lamps, 3463
 Boot, H. A. H., H. Foster and S. A. Self, design of high-power S-band magnetron, 2788 d
 Boott, A. D., physical realization of digital com-puter, 26
 Bopo, F., and E. Werner, theory of spin waves, 2214
 Borck, A., power density meter, 3831
 Bordovskill, G. A., with others, investigation of solar radiation using earth satellites, 3293
 Borel, J. P., and P. Gornaz, Overhauser effect in gas in presence of paramagnetic material, 2546
 Borgman, J., TV techniques in astronomy, 3082
 Borner, M., flexural vibrations in mechanical filters, 2154
 Eordovskil, P. A., application of harmonic vibrations of electrons for u.h.f., 1725
 Boronsy, A. D., electronic ratio calculator, 1102
 Bosanquet, C. H., scale height of upper atmosphere, 1184; change of inclination of satellite orbit, 1552

- 1542; change of inclination of saterite orbit, 1543;
 Bosse, K. K., effect of magnetic field on point-contact transistors, 630
 Bösnecker, D., with E. Lutze, paramagnetic electron-resonance induction, 2927
 Bossard, B. B., superregenerative reactance amplifier, 3243
 Botka, A. T., with others, organized electrification and precipitation in thunderstorms, 2253
 Böttger, O., power limits of thermoelectric effects in semiconductors, 1231
 Bouchard, J., study of ionospheric propagation, 1333 c
 Bouchar, G., carcinotrons for short and long
- 1333 c Boucher, G., carcinotrons for short and long wavelengths, 3524 q Boucherle, A., and J. Mey, pulse-height analyser,
- Boudarenko, P. N., with others, lifetime of injected current carriers in Sb-doped Ge, 1932

- current carriers in Sb-doped Ge, 1932
 Boudouris, G., with others, refractive index of humid air, 1333 n
 Boulx, M., application of distributions to equations of Maxwell and Helmholtz, 405
 Boundoeris, C., with others, optimum radiation from sawtooth aerial, 3578
 Bournas, M. A., with R. Plomp, hearing threshold and duration for tone pulses, 3009
 Bourassin, L., multichannel sound transmission from single transmitter, 983
 Boutry, G. A., with Y. Angel, parametric amplifiers and cancellation of ferromagnetic hysteresis, 3244
 Bouwkamp, C. J., method of calculating capaci-

- and cancellation of ferromagnetic hysteresis, 3244
 Bouwkamp, C. J., method of calculating capacitance, 2193
 Bouzitat, J., with J. A. Ville, finite-duration signals with maximum filtered energy, 2390
 Bowden, F. P., J. B. P. Williamson and J. A. Greenwood, electrical conduction in solids, 485
 Bowers, K. D., with J. P. Gordon, microwave spin echoes from donor electrons in Si, 860
 Bowers, R., J. E. Bauerle and A. J. Cornish, In(As, P) as thermoelectric material, 3759
 and others, InAs and InSb as thermoelectric materials, 3844
 Bowhill, S. A., Faraday-rotation rate of satellite radio signal, 796
 Bowie, R. M., electroluminescent television display, 566

- Bowler, R. M., electroiuminescent television display, 566
 Bowlden, H. J., with R. F. Wallis, impurity photo-ionization spectrum of semiconductors in magnetic fields, 1232
 Bowley, A. E., R. Delves and H. J. Goldsmid, magnetothermal resistance and magnetothermo-electric effects in Bi₃Te₃, 182
 Bowman, D. R., instability in radio receivers, 250
 Bowtell, J. N., electroluminescence and applica-tions, 151
 Boyd, D. R., and Y. T. Sikvonen, growing CdS single crystals, 1905
 with others, properties of green and red-green luminescing CdS, 2621
 Boyd, M. R., with G. M. Roe, parametric energy conversion in distributed systems, 3240

Electronic & Radio Engineer

- Boyd, R. L. F., and N. D. Twiddy, electron energy distributions in plasmas, 3260
 Boyle, W. S., and K. F. Rodgers, oscillations in infrared transmission of Bi, 2620
 with others, splitting of As donor ground state in Ge, 1615
 Bozorth, R. M., weak ferromagnetism in rare-earth orthoferrites, 905

- orthoferrites, 905 Braae, R., accuracy of ohmmeter, 1649 Bracewell, R. N., and O. K. Garriot, rotation of earth satellites, 795 Brachet, C., with others, irradiation of photo-conductive single crystals of CdS, 2617 Bradley, E. M., and M. Prutton, magnetization reversal by rotation and wall motion in NiFe films, 1955 Bradley, R. C., secondary positive ion emission from metals, 1508 Bradshaw, C. G., 1-Mc/s transistor decade counter, 1131
- 1131
- Bradshaw, J. A., space-charge-limited current in planar-diode magnetron, 1018 Brady, D. J., with others, transistor phase-locked oscillators, 2162
- OSCHIATORS, 2162
 Brady, M. M., frequency stability of coherent radar oscillators, 2607; oscillator design using voltage variable capacitors, 3986
 Brady, T., with others, synchronous and exalted-carrier detection, 1378
 Braginskil, S. I., transport phenomena in plasma, 400

- 400
 Brand, F. A., W. G. Matthei and T. Saad, 'reactatron' microwave amplifier, 1150
 with others, microwave techniques in lifetime measurement, 3774
 Braner, H., with J. L. Easterday, derating requirements for carbon composition resistors, 2491
 Brannian, W., transistorized 3-phase power supplies, 3482
 Braslau N., with G. O. Brink, atomic-beam magnet-stabilization system, 4170
 Bratenahl, A., with others, hydromagnetic capacitor, 1843

- stabilization system, 4170
 Bratenahl, A., with others, hydromagnetic capacitor, 1843
 Brattha, W. J., deformation processes in armco iron, 4124
 Bratt, J. B., band-pass filter, 3977
 Braucks, F. W., remote-focus cathode, 936
 Braudes, S. Va., with others, phase fluctuations of 10-cm waves over sea, 2738
 Brauer, F., and D. Kammer, mobile-radio system, 262
 von Braun, W., the 'explorers', 1546
 Bray, D. W., with others, radio reflections from satellite-produced ionization, 2963
 Breazeale, M. A., and E. A. Hiedemann, investigation of progressive ultrasonic waves by light refraction, 1050
 B. D. Cook and E. A. Hiedemann, determination of ultrasonic waveform by light refraction, 3538
 Brebrick, R. F., interdiffusion in ionic semiconductors, 3343
 Bremmer, H., propagation through curved stratification reduced stration
- Bremmer, H., propagation through curved strati-fied medium, 4178

- Bremmer, H., propagation through curved stratified medium, 4178
 Brennet, J., with J. P. Chevillot, semiconductivity of MnO₈, 3783
 Brennan, D. G., linear diversity combining techniques, 3102
 Brewer, G. R., characteristics of magnetically focused electron beam, 3888
 with T. Van Duzer, space-charge simulation in electrolytic tank, 2356
 Brewer, R., American electronics reliability symposium, 2805
 Brewester, K., with J. S. Bell, matrices in transistor circuit analysis, 1141
 Brice, J., with H. C. Wright, indium mono-telluride, Brice, N. M., variations in F-region characteristics

- Brice, N. M., variations in F-region characteristics, 2241

Brice, N. M., Variations in F-region characteristics, 2241
Brice, P. J., amplitude of v.h.f. signals reflected from E₁ layer, 2000 k
Brick, D. B., and J. Galejs, radar interference, 465
Bridges, T. J., with others, parametric amplification of space-charge waves, 3159 k
Briggs, G. R., with others, transfluxor-controlled electroluminescence display panel, 568
Brill, A., H. A. Klasens and T. J. Westerhof, cathodothermoluminescence, 2624
Brill, P. H., and R. F. Schwarz, radiative recombination in Ge, 869
Brink, G. O., and N. Braslau, atomic-beam magnetstabilization system, 4170
Brinkrann, C., printed circuits, 1788
Britsyn, K. I., with V. S. Vavilov, quantum yield of photoionization in Si, 863

- of photoionization in S1, 665 Britt, C. O., with others, phantom radar targets at mm λ , 3315 Britton, G. A. C. R., with C. W. Sowton, radio interference, 954 Brockelsby, C. F., ultrasonic mercury delay lines, 361
- 361

- 361
 Brockhouse, B. N., lattice vibrations in Si and Ge, 2286
 and P. K. Ivengar, normal modes of Ge by neutron spectrometry, 173
 Broderick, D., D. Harthe and M. Willrodt, precision generator for radar range calibration, 2352
 Brodie, I., R. O. Jenkins and W. G. Trodden, evaporation of Ba from impregnated cathodes, 2792
 Broderic M. E. Department of the first filled
- Brodwin, M. E., propagation in ferrite-filled microstrip, 2109
 Brömer, H. H., and V. Stille, electron recombination in afterglowing active nitrogen, 1510
 Broneer, C. S., with B. D. Solomon, constant-S equalizers, 3226
 Bronzi, G., tests on Kahn's theory of anti-fading reception, 952; asymmetrical modulation, 3465
 Brooks, F. E., J.r., with J. P. German, bandwidth of folded dipole, 2842

World Radio History

- Brooks, W. O., stepping-up frequency with counter circuits, 3614
 Brophy, J. J., influence of surfaces on 1/f noise in Ge, 172; Scebeck effect fluctuations in Ge, 178
 Broser, I., and R. Broser-Warminsky, energy transfer in CdS, 827
 Broser, Department, Provide L. Baroer, Science, Sci
- Broser, I., and R. Broser-Warminsky, energy transfer in CdS, 827
 Broser-Warminsky, R., with I. Broser, energy transfer in CdS, 827
 Broudy, R. M., with J. D. Venables, photo-anodization of InSb, 3782
 Broussaud, G., aerials for long-range radio links, 1333 r
 with others, superdirectivity of aerial, 3572
 Brouwer, G., model for h.f. phenomena in junction transistor, 3154
 Brower, W. S., with P. H. Fang, temperature dependence of breakdown field of BaTiO₄, 2627
 Brown, A. aerials for lelevision broadcasting, 3571
 Brown, A. V., transient phenomena in microwave tubes, 2788 n
 Brown, D. A. H., behaviour of square-loop magnetic cores, 3217
 Brown, J., and K. P. Sharma, launching of radial cylindrical surface waves by circumferential slot, 2110
 with A. Carne, reflections from rod-type artificial dielectric, 2123

Brown, S., and K. P. Sharma, launching of radial cylindrical surface waves by circumferential slot, 2110
with A. Carne, reflections from rod-type artificial dielectric, 2123
with J. S. Seeley, dispersive artificial dielectries in beam-scanning prism, 2124
Brown, J. N., automatic sweep-frequency iono-sphere recorder, 1564
Brown, R. K., and others, lightweight airborne navigation system, 2599
Brown, R. R., laitude variation of 27-day cosmicray intensity decreases, 1862
Brown, R. C., with J. L. Hirshfield, measuring probability of electron collision in gas, 768
with R. G. Meyerand, Jr, high-current ion source, 1986
Brown, W. L., and W. M. Augustyniak, defect formation in electron irradiation of n-type Ge, 4110
W. M. Augustyniak and T. R. Waite, annealing of radiation defects in semiconductors, 4089 o
Browne, G. D., a.f.c. in band-11 f.m. receivers, 951
Browne, S. S. F., common-channel common-programme operation of helds on plasma ions, 1160

Broyles, A. A., calculation of fields on plasma ions, 1160

Broyles, A. A., calculation of fields on plasma ions, 1160
Bruaux, A., radiation diagram of linear aerials, 3567
Brueckner, K. A., and K. Sawada, magnetic susceptibility of electron gas, 759
Bruijning, H. G., and A. Rademakers, pulse transformer with pre-magnetization, 1469
Brumbaugh, J. M., E. D. Goodale and R. D. Kell, colour TV recording on black and white lenticular film, 1371
Bruynseels, J. P., and R. Gonze, coaxial reflectometer for metre waves, 3431
Bryant, R. J., R. B. Coulson and J. K. Fowler, low-noise travelling-wave tubes, 2063
Bryant, M. O., beam and coupling parameters for broad-band klystrons, 3524 f
J. F. Gittins and F. Wray, c.w. power travelling-wave tube, 2787
Bryant, N. H., with others, antenna-beam distortion in transhorizon propagation, 1347
Bryant, P. R., topological investigation of network determinants, 2157
Bryndahl, O., and E. Ingelstam, diffraction patterns in microscopes and microwave fields, 2206
Brysk, H., measurement of scattering matrix with intervaning horespace.

Brysk, H., measurement of scattering matrix with intervening ionosphere, 1345; scattering by low-density meteor trails, 1665
 and others, radar cross-section of finite cones,

4073
Buchanan, D. N. E., with G. K. Wertheim, electron-bombardment damage in oxygen-free Si, 4089 k
Buchanan, R. W., and B. Kautz, dynamic testing of computer blocks, 3591
Buchar, E., motion of nodal line of 1957 β, 118
Buck, T. M., and F. S. McKim, chemical and atmospheric effects on surface properties of Si, 4097

atmospheric effects on surface properties of Si, 4097
Buckelew, J. W., and E. D. Knob, through-connections for printed wiring, 38
Bücks, K. E., with others, application of radio alti-meters to aircraft approach, 2259 o
de Buda, R. G., characteristic impedance of strip transmission line, 3555
Budden, K. G., with D. W. Barron, numerical solution of equations governing reflection of long waves from ionosphere, 3455
Buduls, L., with D. J. Howlett, noise-immune synchronizing circuits, 3120
Bugnolo, D. S., correlation function and power spectra of radio links, 4203
de Budn, J., representation of general lossy quadri-pole, 1477
Buick, R. I., A. Reddish and I. J. Zucker, frequency pushing in crossed-field oscillators, 2788 q
Bukstein, E., how ring counters work, 2507
Bulgakov, R. M., and V. P. Shestopalov, propagation in retarding systems with helix and dielectric, 3869
Bullough, R., R. C. Neuman and J. Waksfield,

Bullough, R., R. C. Newman and J. Wakefield, diffusion across semiconductor/vapour interface,

and others, precipitation on a dislocation, 2289 Bunting, E. N., with others, infrared studies on SiO₂ and GeO₂, 205

I.5

anu 4073

165

Burbank, R. D., with others, magnetic annealing in perminwar, 3797
Burdick, G. A., short picture-tube design, 3127
Bureau, J. L., sudden commencements at Tamanrasset, 1183
Burfoot, J. C., model for switching of BaTiO₂ crystals, 2635
and R. V. Peacock growth of formelectric

- crystals, 2635
 and R. V. Peacock, growth of ferroelectric hysteresis loops, 3329
 Burger, J. F., with J. P. A. Lochner, subjective masking of delayed echoes, 5; intelligibility of reinforced speech, 3912
 Burgess, B., with others, deduction of electron content from Faraday fading, 2572
 Burgess, R. E., polarization fluctuations in ferro-electric crystal, 842; avalanche breakdown in Si, 4095
- Burgess, R. E., polarization fluctuations in ferroelectric crystal, 842; avalanche breakdown in Si, 4095
 Burkard, O., radio reflexions from moon and solar corna, 2583; ionosphere model, 3705
 Burke, B. F., with K. L. Franklin, observations of planet jupiter, 1522
 Burke, P. F. C., 4-Gc/s travelling-wave tube for microwave radio links, 2788 o
 Burke, R. H. W., pyrolytic carbon resistors, 2490; total-excursion resistor, 3216
 Burnham, J., dielectric films in Al and Ta capacitors, 725
 Burrus, C. A., mus pulse generator, 2500
 Burrus, C. A., mus pulse generator, 2500
 Burrus, C. A., mus pulse generator, 2500
 Burrus, C. G., satellite tracking, 122
 Buryak, E. M., with others, anomalously high Hall effect in CrTe, 2681
 Busch, G., and T. Fischer, field emission from semiconductors, 3016
 and R. Kern, magnetic properties of AgSe, 758 a
 and R. Kern, magnetic properties of AmBV compounds, 2645
 F. Hullinger and R. Jaggi, field parameters of galvano- and thermo-magnetic effects in ferromagnets, 786 c
 R. Kern and B. Lüthi, magnetic resistance variation of InSD, 758 b
 Busch, R., E. Harmischmacher and K. Rawer, ionospheric observations during solar eclipse of 30th June 1954, 131
 Busbore, K. R., with W. L. Teeter, microwave power divider and multiplexer, 1078
 Butcher, C. H., with others, new method for fine-wite others, '50 I. R. E. Show, 2801
 Bushore, K. R., with W. L. Teeter, microwave power divider and multiplexer, 1078
 Butcher, P. N., theory of three-level paramagnetic masers, 2894
 with others, travelling-wave solid-state masers, 2891
 Butcher, F., transistor audio amplifier, 67; regenerative-modulator frequency divider using transistor invertors and rectifier-

- wun others, travelling-wave solid-state masers, 2891
 Butler, F., transistor audio amplifier, 67; regenerative-modulator frequency divider using transistors, 1133; transistor invertors and rectifier-filter units, 3483
 Butler, K. H., and F. Koury, sylvatron electroluminescent display, 224
 Butler, T. W., Jr, ferroelectrics tune circuits, 1472
 Butler, T. W., Jr, ferroelectric stune circuits, 1472
 Butler, P. C., and G. T. Thompson, effect of flanges on radiation patterns, 3582
 Butterweck, H. J., with E. Schuon, linearization of f.m. characteristic of reflex klystron, 1739
 Button, K. J., analysis of field-displacement isolator, 2839
 and others, Zeeman effect of excitons in Ge, 2299
 with others, exciton- and magneto-absorption of

- 2299 states, bettinn electron and magneto-absorption of transitions in Ge, 3364
 Buxton, A. J., and M. O. Felix, reduction of threshold by frequency compression, 2000 q
 Byatt, D. W. G., with J. F. Hatch, direction finder with automatic read-out, 2600
 Bye, W., effects of temperature on junction transistors, 299
 Byers, H. G., and M. Katchky, slotted waveguide array for radar, 711

- Byers, H. G., and M. Katchky, slotted waveguide array for radar, 711
 Cabessa, R., pulse techniques in radio communication networks, 2014 b
 Cade, C. M., maser microwave oscillator, 1500
 with H. R. Whifeld, analysis of collision-course prediction, 2259 r
 Cahill, L. J., Jr, investigation of equatorial electroiet, 2968
 Cahil, W. F., with others, satellite orbits from radio tracking data, 2568
 Cahn, J. H., irradiation damage in Ge and Si, 4089 r
 Caiong, J. I., optical approach in microwave measurements, 563; electronics and communications in Brazil, 3176
 Cairns, R. B., and G. C. McCullagh, discharge modes using thermionic cathodes, 2441
 Cakenberghe, J., with J. M. Gilles, photoconductivity and crystal size in evaporated CdS, 828
 with G. Offergeld, stoichiometry of Bi, Te, 3785.
 Caldwell, J. W., and T. C. G. Wagner, boosting power-transistor efficiency, 978
 Callaby, D. R., with the M. Lee, measurement of velocity of propagation of domain boundary in perminvar, 194
 Callaway, J., and M. L. Glasser, Fourier coefficients of crystal potentials, 785
 Callanger, M. V., loudspeaker enclosure calculations, 1763
 Callager, M. V., loudspeaker enclosure calculations, 1763

- Construction of horn-type aerials with parabolic reflectors, 1777
 Cameron, D. B., with R. N. Lane, current integra-tion with solion liquid diodes, 2023

I.6

- Carmeron, W. A., coaxial-cable performance, 3925
 Campbell, J. O., with Y. J. Liu, collision detection without range data, 3722
 Campbell, L. L., properties of frequency-staiblizing circuit, 738
 Campbell, R. D., radar interference to microwave communication services, 1353
 Campbell, W. H., and B. Nobel, micropulsation measurements, 4045
 Cane, P. E., and W. E. Taylor, cooling high-power valves by vaporization, 654
 Cantz, R., diode circuit for a.v.c. in transistor receivers, 2742
 Cap, S. T., and N. P. White, guidance systems in space flight, 3839
 Capelli, M. P. G., A. E. Outten and K. E. Bücks, application of radio altimeters to aircraft approach, 2259 o
 Cappian, P. J., with others, analysis of emissive phase of pulsed maser, 756
 Capps, R. H., behaviour of intense relativistic electron beams, 4017
 Cappuccini, F., passive repeaters, 1778
 Capricoli, L., attenuation in circular waveguides, 3194
 Caracciolo, A., and L. Guerri, final computer model of Pisa C.S.C.E. 3966

- 3194
 Caracciolo, A., and L. Guerri, final computer model of Pisa C.S.C.E., 3966
 Carapiperia, L., with M. Anastassiades, influence of meteorological factors on u.h.f. propagation, 1232 area
- meteorological lactors and 1333 m Carassa, F., reactance-valve frequency modulator, 2034 I. and R. W. Pittman, thermoelectric

- 1333 m
 Carasso, F., reactance-valve frequency modulator, 2034
 Carasso, J. I., and R. W. Pittman, thermoelectric observations on grey Se, 1272
 Card, W. H., 4-transistor inverter drives induction motor, 1983
 Carden, H. T., with A. D. Cawdery, application of magnetic amplifiers, 2516
 Cardona, M., and W. Pawi, quadratic photoelectromagnetic effect in Ge, 1253
 Carder, Y. M., inductive control in computer circuits, 3967
 Carlor, F. de, with others, circular waveguides for long-distance transmission, 2107
 Carlin, H. J., with others, claratic photoelectromet of microwave power, 2358
 Carres, A., with B. Josephson, fading and distortion of 3-kMC/s transhorizon signals, 3090
 Carne, A., and J. Brown, reflections from rod-type artificial dielectric, 2123
 Caroumbalos, C., with others, optimum radiation from sawtooth aerial, 3578
 Carrest, N., P. F. Checcacci and L. Roncki, determination of satellite orbit, 441, 1188
 Carrest, N., P. F. Checcacci, radio observations, on anificial stelletor of anomalous magnetic moment on electron spin, 99
 Carret, R. L., characteristic impedance of two infinite cones, 2843
 Carrel, R. L., characteristic impedance of two infinite cones, 2843
 Carrel, R. E. Bushor and S. Weber, '59 I.R.E. Show, 2801
 Carster, R., with V. J. Hammond, visualization of uservation for anomalous for a compared theory in finite cones in fields in the earth, 3668
 Carter, R., with V. J. Hammond, visualization of uservation for a compared count of defaure of a compared cone in formation of anomalous for a compared cone of the compared count of the compared compared compared comp

- Carstoiu, J., induced e.m. fields in the earth, 3668
- Carter, R., with V. J. Hammond, visualization of ultrasonic beam in fused quartz, 674 Carter, R. E., effect of O₂ pressure on Mg ferrite, 1287

- 1287
 Caruso, F., with others, current amplification of junction transistors, 631
 de Carvalho Fernandes, A. A. See Fernandes, A. A. de C.
 Casci, C., and V. Giavotto, indirect method of determining high-atmosphere density, 3686
 Cashen, J. F., with A. Harel, unified representation of transistor transient response, 2050
 Cashman, R. J., film-type infrared photoconductors, 4076 4076

- 4076
 Caspary, R., lifetime measurements on CdS using Kerr cell, 3322
 Cassedy, E. S., Jr, surface-wave parametric amplifier, 3625
 Casseiman, C. J., D. P. Heritage and M. L. Tibbals, v.I.f. propagation measurements for Radux-Omega system, 2736
 Casseite, J., with N. Segard, theoretical investigation of ultrasonic field, 1423
 with others, crystal probe for measurement of ultrasonic power, 1752
 Cassidy, M., flight testing of radio facilities, 460
 Castelliz, L., with W. W. H. Clarke, ferromagnetic

- Cassidy, M., flight testing of radio facilities, 400
 Castelliz, L., with W. W. H. Clarke, ferromagnetic after-effect in mumetal, 3320
 Castro, P. S., and J. S. Needle, beam-defocusing microwave detector, 1413
 Cawdery, A. D., and H. T. Carden, application of magnetic amplifiers, 2516
 Cawsey, G. F., J. L. Farrands and S. Thomas, observations of detonation by interferometer, 3068
 Carde J. and charge on functions in Ge 3485
- Černý, L., and others, p-n junctions in Ge, 3485

- Cerný, L., and others, p-n junctions in Ge, 3485
 Chako, N., asymptotic development in diffraction theory, 1850
 Chakkraborti, N. B., wide-band discrimination, 2526
 Chalikyan, G. A., with G. M. Garibyan, radiation from charged particle, 3634
 Chalmers, J. A., atmospheric electricity, (B)1201
 Chalmers, P. M., with F. A. Benson, effects of argon content in glow-discharge tubes, 2442
 Champion, F. C., and S. B. Wright, diamond con-duction counters with small electrode separa-tions. 1990
- Champion, J. A., grid emitting properties of Ti, 1030
 Champion, K. S., microplasma fluctuations in Si, 3770

World Radio History

- Champness, C. H., transverse magnetoresistance in p-type InSb, 1265
 Chandler, H. G., electron-tube evaluation for missile applications, 2431
 Chaney, J. G., simple solution to problem of cylindrical antenna, 23
 Chang, K. K. N., harmonic generation with non-linear reactances, 61; 4-terminal parametric amplifier, 1148; low-noise tunnel-diode amplifier, 3246; analysis of parametric amplifier, 4005
 Chang, W. S. C., with C. M. Angulo, excitation of dielectric rod by cylindrical waveguide, 3558

 with others, travelling-wave solid-state masers, 2891
- 2891 Chanin, L. M., A. V. Phelps and M. A. Biondi, measurement of attachment of slow electrons in
- Chapman, S., thermal diffusion in ionized gases, 89; earth and its environment, 1540
 and K. Davies, daytime constancy of absorption of radio waves in lower ionosphere, 809 of racio waves in lower ionosphere, 809 Charakhech'yan, A. N., and T. N. Charakhech'yan, measurement of cosmic-ray intensity in strato-sphere, 3277 Charakhech'yan, T. N., with A. N. Charakhech'yan, measurement of cosmic-ray intensity in strato-cribere 3277

Charnley, W. J., approach and landing aids, 2259 l; blind landing, 3723
 Charru, A., shape of paramagnetic-resonance signals, 1170
 Chase, K. H., and J. L. Pierzga, reducing radar interference, 3316

interference, 3318
Chasmar, R. P., and E. Cohen, electrical multiplier utilizing Hall effect, 349
Chatterjee, R. with others, dielectric aerials, 2118
Chatterjee, S. D., and S. K. Sen, induced con-ductivity at surface of contact, 1271
Chatterjee, S. M., with others, dielectric aerials, 2118
Chavasse, P. J. A. H., and R. Lehmann, loudspeaker measurements, 1761
Checcacci, P. F., and C. Carreri, radio observations, on artificial satellites, 1192, of Sputnik III, 2569
and V. Russo, microwave configuration lens

and V. Russo, microwave configuration lens tests, 1450 with others, determination of satellite orbit, 441, 1199

Chechernikov, V. I., and Yu. D. Volkov, temperature dependence of paramagnetic susceptibility of Ni-Zn ferrites, 3041
Chen, C. W., magnetic properties of Si-Fe, 193
Chen, T. C., and O. B. Stram, digital memory system, 2129
Chengta E. B. industry

2129
Chenette, E. R., influence of inductive source on transistor noise, 2047
Cheng, D. K., simulation of Fraunhofer radiation patterns, 1096
Cheremushkina, A. V., with N. S. Akulov, Hall effect at Curie point, 2660
Cherepanov, A. M., growing of BaTiO₂ single crystals, 1599
Chernosky, E. J., and M. P. Hagan, Zurich support

Cheropanov, A. M., growing of BaTiO₂ single crystals, 1599
Chernosky, E. J., and M. P. Hagan, Zurich sunspot number and variations, 1529
Chernosky, E. J., correlation of field fluctuations, 663
with E. A. Blyakhman, pulsation frequency of field at focus of lens, 4031
with M. N. Krom, effect of fluctuations on intensity distribution near focus of lens, 2917
Chernov, Z. S., interaction of e.m. waves and electron beams with centrifugal e.s. focusing, 2788 cc
Chevillot, J. P., and J. Brenet, semiconductivity of MnO₂, 3783
Chiesa, A., effect of mechanical vibrations on response of microphones, 690
Child, M. R., and V. N. Athavale, recording of atmospherics in 1.f. region, 813
and others, nature and origin of atmospherics, 3699 a
Chirlkov, B. V., passage of nonlinear oscillator through resonance, 2499
with V. I. Volosk, compensation of space charge in electron beam, 1836

through resonance, 2499
with V. I. Volosk, compensation of space charge in electron beam, 1836
Chisholm, D. A., with others, reflex klyston as negative-resistance-type amplifier, 1741
Chisholm, J. H., and others, measurements of band-width of waves propagated beyond horizon, 3459
Chivers, H. J. A., and H. W. Wells, new ionospheric phenomenon, 2582
Cholorow, M., and others, current distribution in modulated electron beams, 644; high-power pulsed klystrons, 1410
Cholet, P., with others, bigh-sensitivity infrared detectors, 1012
Choudnury, N. K. D., and M. V. S. S. K. Rao, panel absorbents for low-frequency sound, 2821
Chown, J. B., W. E. Scharfman and T. Morita, voltage breakdown characteristics of microwave antennas, 3581
Choyke, W. J., with L. Patrick, SiC p-n junctions, electron emission from breakdown regions in, 1610, impurity bands of electroluminescence in, 1910
Chrétien, L., and R. Aschen, compatible system for colour television. 1200: synchronbase, 3116

Chrétlen, L., and R. Aschen, compatible system for colour television, 1700; synchrophase, 3116
 Christ, K., O. Laaff and K. Schmid, radio-link installations for telephony and television, 1687
 Chu, K., and J. R. Singer, thin-film magnetization analysis, 3394
 Chudakov, A. E., with others, mechanism of terrestrial corpuscular radiations, 2216; investi-gation of cosmic radiation, 3663, by cosmic rockets, 2231

Chudesenko, E. F., with others, electron concentration of ionosphere from observations of first earth satellite, 3298
 Chynoweth, A. G., radiation damage effect in triglycine sulphate, 2273; effect of space-charge fields on BaTiO₂, 2274

Electronic & Radio Engineer

1188

- and J. L. Abel, polarization reversal in triglycine sulphate, 3742 Ciuciura, A., X radiation from television receivers, 4219
- 4219 Clapp, F. D., with A. Yariv, determination of cavity parameters, 4154 Clark, C., checking jitter in moving-target radar, 3725
- Clark, J. L., with W. A. Prowse, u.h.f. gas breakdown, 395

- parameters, s134
 Glark, C., checking jitter in moving-target radar, 3725
 Clarke, J. L., with W. A. Prowse, u.h.f. gas breakdown, 395
 Clarke, E. L., auto self-excited transducers, 1791
 Clarke, G. M., power limitations in helix travelling-wave tubes and application of fluid cooling, 2788 j
 and R. D. Rooks, microwave reflectometer display system, (D)2703
 Clarke, R. L., diffusion of Cu in CdS, 3732
 Clarke, W. W. H., with L. Castellis, ferromagnetic after-effect in mumetal, 2320
 Clarricoats, P. J. B., perturbation method for circular waveguide, 2836
 Claudel, C., with others, properties of mixed Gd-Er and Gd-Y garnet, 1633
 Clavier, P. A. parametric and pseudo-parametric amplifiers, 4247
 Clayton, C. G., B. C. Haywood and J. F. Fowler, conductivity induced by radiation in CdS and polyethylene, 2672
 Clegg, J. E., and J. W. Crompton, low-power c.w. Doppler navigation equipment, 2259 f
 and J. W., with J. H. Crawford, Jr, bombardment damage and energy levels in semiconductors, 4091
 with others, radiation-induced recombination centres in Ge, 868
 Clogston, A. M., with others, low-temperature linewidth maximum in Y-Fe garnet, 3812
 Cloud, W. H., crystal structure and ferrimagnetism in NiMnO, and CoMnO, 199
 Coates, R. V., and H. F. Kay, dielectric properties of metaniobate and metatalate ceramics, 3326
 Cobbold, R. S. C., charge storage in junction transistor, 2773
 Cohen, A. M., with J. D. Pearson, 20-kW pulsed travelling-wave tube, 2788 l
 Cocquerez, F., with thers, roystal probe for measurement of ultrasonic power, 1752
 Coet, e., with R. P. Chasmar, electrical multiplier utilizing Hall effect, 349
 Cochran, W., lattice vibrations in Ge, 3367
 Cohen, A. M., with J. A. Lesk, Ge diffused minicrystals and use in transistors, 637
 Cohen, K. H., nuclear magnetic resonance in impure InSb, 1262
 and W. H., cry

- 107 CiVil aviation, 2259 β
 Cole, C. F., Jr., characteristics of e.m. wave reflected from moving object, 410
 Cole, H., and E. Kineke, lattice vibrational spectra of Si and Ge, 857
 Cole, K. D., low-energy corpuscular radiation, 2551
 Cole, R. H., with S. E. Lovell, coaxial displacement dielectric cell, 3063
 Cole, W. A., magnetic matrix stores, 2482
 Coleman, H. P., with G. D. M. Peeler, stepped-index Luneberg lenses, 2854
 Coleman, P. D., and R. C. Becker, rectangular and circular mm waveguides, 2463; mm-wave generation, 3982
 with others, slow-wave structures for power generation at mm and sub-mm λ, 1743
 Coleman, P. J., Jr., with others, ionizing radiation at 3 500-36 000 km, 3691
 Colin, J. E., interchange of infinite-attenuation elements, 2150; filter technique in France, 2153; generalization of Zobel-type ladder filters, 3224
 Colin, L., with S. Weisbrod, refraction of v.h.f. signals, 3698
 Collin, R. E., properties of slotted dielectric inter-faces, 3584

- Colling K. E., properties of slotted dielectric inter-faces, 3584 Collings, E. W., filament noise source for 3 kMc/s, 2344
- Collins, C., and P. A. Forsyth, bistatic radio investiga-
- Collins, C., and P. A. Forsyth, bistatic radio investigation of auroral ionization, 2001
 with G. C. Reid, abnormal v.h.f. absorption, 2380
 Collins, D. J., and J. E. Smith, regulated power supplies, 2401
 Collins, K. D., with P. A. Lindsay, design of helical coupler for 2-Gc/s band, 3159 x
 Collins, R. J., edge emission in CdS, 4089 c
 Colombani, A., and G. Goureaux, conductivity of thin Ni films, 3395
 P. Huet and C. Vautier, measurement of very slight variations of resistance, 555
 C. Vautier and P. Huet, properties of Sb films, 2693

- 2693
- 2693
 with G. Goureaux, magnetic properties of very thin films of nickel, 3039
 with others, Hall effect in Ni films, 1279
 Como, R. J., with A. Y. Rumfelt, rapid insertion device for coaxial attenuators, 3927
 Comte, G., and others, circular waveguides for long-distance transmission, 2107
 Conda, A. M., with J. R. Wait, pattern of antenna on curved lossy surface, 3195
- Electronic & Radio Engineer

- Conwell, E. M., lattice mobility of carriers in Ge, 4101
- Cook, A. H., determination of the earth's gravita-

- Cook, A. H., determination of the earth's gravitational potential, 4048
 Cook, B. D., with others, determination of ultrasonic waveform by light refraction, 3538
 Cook, G. H., vidicon camera lenses, 1375; modern optics in relation to television, 3498
 Cooke, G. H., vidicon camera lenses, 1375; modern optics in relation to television, 3498
 Cooke, M. S., with others, diffraction of e.m. waves by ridge, 241
 Cooke, R. E., impedance and phase angle of loudspeaker loads, 2823
 Cooley, C. C., Jr, wide-band sweep generator, 558
 Cooleg, A. W., with H. N. Price, development of ceramic hydrogen thyratrons, 3535
 Coon, R. M., with others, radio system performance in noise, 963 Coon, R. M., with in noise, 963

- in noise, 963
 Cooper, B. K., electronics in railway industry, 2717
 Cooper, B. R., magnetic anisotropy constant of Y-Fe garnet, 901
 Cooper, R. B., Jr, sporadic-E skip on 200 Mc/s?, 574
 Cooper, V. J., differential phase distortion in colour television transmitters, 614
 Cooperran, M., magnetic demodulators for colour TV, 1379
 Coopern, P. J., with A. L. Barry, transistors reach for higher frequencies, 1399
 with P. A. Iles, delineation of p-n junctions in Si, 514
 Coopert, E. G., use of automatic error correction

- with P. A. Iles, delineation of p-n junctions in Si, 514
 Copper, E. G., use of automatic error correcting equipment, 3104
 Coppola, P. P., with others, dispenser cathodes, 2791
 Corazza, G. C., and G. Zoldan, physical realizability of microwave junction, 2139
 Corbett, J. W., with others, spin resonance in electron-irradiated Si, 4089 h
 Corenzwit, E., with others, magnetic moments of Fe and Co with rare-earth metal additions, 2321
 Corliss, E. L. R., uniform transient error, 216
 Corneter, M., with V. A. Cumming, design data for annular slots, 2849
 Cornaer, P., with J. P. Borel, Overhauser effect in gas in presence of paramagnetic material, 2546
 Cornetet, W. H., Jr., with others, processing Nimatrix cathodes, 4250
 Cornlish, A. J., with others, thermoelectric materials, InAs and InSb as, 3384, In(As.P) as, 3759
 Coronitt, S. C., and R. Penndorf, foFz over polar regions, 1882
 with R. Penndorf, polar E., 1561
 with others, geophysical effects of high-altitude nuclear explosions, 2969
 Costas, J. P., notes on space communications, 3860
 Coste, J. P., with others, readiation, 3278
 Cotte, M., propagation in medium with dielectric losses, 2208
 Cotterill, M. J., and J. W. Halina, bridge negative feedback amplifiers in carrier telebonv, 974
- Cotter, M., Disposance in the second s

- signals, 2186
 Cottony, H. V., and A. C. Wilson, gains of cornerreflector antennas, 3205
 and others, U.R.S.I. report on antennas and waveguides, 3565
 Coughlin, B. J., G. L. Davis and R. L. Kingsnorth, orientation control for Ge wafers, 1935
 Coulomb, J., possible auroral origin of certain geomagnetic pulses, 2947
 Coulson, R. B., with others, low-noise travelling-wave tubes, 2063
 Coupland, M. J., diffusion of P into Si 2651
- Coupland, M. J., diffusion of P into Si, 2651

- tubes, 2063
 Coupland, M. J., diffusion of P into Si, 2651
 Coutrez, R., principles and present results of radio astronomy, 3273
 Cowen, J. A., W. R. Schafer and R. D. Spence, polarization of Al nuclei in ruby, 3792
 Cowie, A., comparison of telemetry systems, 4172
 Cox, B. C., triode-connected pentode with stabilized anode current, 750
 Cox, J. T., and G. Hass, antireflection coatings for Ge and Si in infrared, 864
 Crabbe, H. J. F., electronics and the phonetician, 2450
 Cragg, T., with others, magnetic field associated with solar flare, 4043
 Cratke, D. J., and P. M. Griffiths, domain configurations on ferrites, 1283
 Crane, H. D., logic system using magnetic elements, 1104
 Craven, G., and V. H. Knight, integrally constructed waveguide assemblies, 2826
 Crawford, A. B., D. C. Hogg and W. H. Kummer, tropospheric propagation beyond horizon, 4185
 Crawford, J. H., Jr, and J. W. Cleland, bombardment damaze and energy levels in semiconductors, 4091
 with others, radiation-induced recombination centres in Ge 868

- conductors, 4001
 with others, radiation-induced recombination centres in Ge, 868
 Cressey, J., with others, tracking weather with satellites, 2715
 Cretella, M. C., and H. C. Gatos, reaction of Ge with HNO₃, 2310
 Cripps, L. G., transistor h.f. parameter f₁, 4236
 Croit, W. F., with others, capabilities of coaxial cable, 2457
 Croitedale, A. C. Antrophysical and A. C. Antrophysical antrophysical antrophysical antroph

- Croisdale, A. C., teleprinting over long-distance radio links, 960
 Cromack, J. C., with others, travelling-wave solid-state masers, 2891
 Crompton, J. W., with J. E. Clegg, low-power c.w. Doppler navigation equipment, 2259 f
 Cronner, E. A., with E. W. Lehtonen, a.c.-controlled magnetic amplifiers, 382
 Cronergyer, D. C., photoconductive response of Ge layers, 867; infrared absorption of reduced rutile, 3034
 Crosby, M. G., compatible system of stereo transmission, 1363

World Radio History

Crowley, T. H., with U. F. Gianola, 'Laddic', 1463
 Crysdale, J. H., and others, diffraction of e.m. waves by ridge, 241
 Cuccia, C. L., voltage control of magnetron fre-quency, 3528

- Cutcha, C. J., Voltage Control of Inagaterion frequency, 3528
 Culbertson, A. F., with M. H. Kebby, 6-kMc/s system for toll telephone service, 2393
 Cullen, A. L., and I. M. Stephenson, experimental investigation of velocity-modulated electron beams, 3524 g
 B. Rogal and S. Okamura, torque-operated wattmeters for 3 cm λ, 2359
 Cullington, A. L., artificial aurora, 1569
 Cummack, C. H., 'Chapman behaviour' in lower ionosphere, 3301
 and G. A. M. King, disturbance in F region, following nuclear explosion, 3712
 Cummerow, R. L., thermally induced glide in Ge, 3363

- 3363 Cumming, W. A., ratiation account 2714 — and M. Cormier, design data for annular slots, 2849 Cumliffe, A., and R. N. Gould, high-Q echo boxes, 740 Cunnell, F. A., with J. W. Allen, diffusion of Zn in GaAs, 1259 Curle, C., and Y. Descamps, compensation for further that an orde current, 1369 Cumming, W. A., radiation measurements at r.f.,

Gans, 1599 Curle, C., and Y. Descamps, compensation for fluctuations in anode current, 1369 Curnow, H. J., design of multicavity klystrons, 3324 h

3524 h with others, coaxial-line diode, 3524 m Currie, C. H., carcinotron harmonics boost receiver range, 2006 Currie, M. R., and D. C. Forster, noise-reduction mechanism in electron beams, 1727; minimum noise generation in backward-wave amplifiers, 1734

noise generation in backward-wave amplifiers, 1734
Currin, C. G., guide for Si dielectrics, 2694
Curtis, H. E., echoes cause f.m. intermodulation, 2396
Curtis, O. L., Jr, radiation effects on recombination in Ge, 4107
— J. W. Cleand and J. H. Crawford, Jr, radiation-induced recombination centres in Ge, 868
Cushner, S. H., optical-microwave system considerations, 40101
Cuttler, M., with H. M. Bath, measurement of surface recombination velocity in Si by steady-state photoconductance, 1246
Cutler, P. H., and D. Williams, scatter-signal analyser, 2000 b
Cutolo, M., self-demodulation of waves in ionosphere,

Cutolo, M., self-demodulation of waves in ionosphere, 1333 d Czaja, W., application of thermodynamics of irreversible processes to semiconductors, 2638

Daams, H., wilk others, Canadian caesium-beam standard of frequency, 2701
Daddario, A. S., transistor blocking-oscillator circuits, 56
Dahlberg, R., theory of thermoelectric cooling, 3449
Dain, J., u.h.f. power amplifiers, 380
Daisenberger, G., with K. H. Fischer, amplification of wide frequency bands, 1490
Dammers, B. G., A. Bockhorst and D. Hoogmoed, stabilization of line output circuits, 3124
A. G. W. Uitjens and W. Ebbinge, transistor circuits, temperature-stable, 71, based on half-supply-voltage principle, 755
A. G. W. Uitjens and H. Heytigers, protection device for stabilized line output circuits, 3123
Danforth, J. L., design of 10-MeV particle accelerator, 934
Danforth, W. E., polarization studies with ThO₁, 3335
Daniel, A. F., with D. Linden, power sources for

3335
Daniel, A. F., with D. Linden, power sources for space age, 2399
Daniel, P. J., and others, control of luminescence by charge extraction, 473
Daniels, F. H., causes of geomagnetic fluctuations, 1532
and S. I. Bener, Production of the statement o

Daniels, F. B., causes of geomagnetic fluctuations, 1532
and S. J. Bauer, Faraday fading of satellite signals, 450
Daniels, H. L., and D. K. Sampson, magnetic drum provides analogue time delay, 1655
Daniels, J. M., with H. Wesemeyer, influence of saturation of paramagnetic resonance absorption on Faraday effect, 2547
Danielson, G. C., with S. Sawada, electrical conduction in WO, 2668
Danielson, W. E., low noise in solid-state parametric amplifiers, 1503
H. L. McDowell and E. D. Reed, helix travelling-wave amplifier, 2788 a
Danilin, B. S., and others, pressure and density measurements in high atmosphere by earth satellites, 3694
Danko, S. F., W. L. Dozey and J. P. McNaul, micromodule approach to miniaturization, 2485
Darmony, M., and B. Dreyfus-Alain, solid-state diffusion applied to semiconductor devices, 184
with B. Dreyfus-Alain, Si transistors by alternate doping, 301
Das, J., coder and decoder for teleprinter signals, 1685
Das, J. N., semiconducting properties of pyrolusite, 1266

1685
Das, J. N., semiconducting properties of pyrolusite, 1266
with P. V. Khandekar, I/V characteristics of n-p contacts on galena, 3874
Dash, W. C., growth of Si crystals free from dislocations, 3354
Datta, S., electron production rate in F₂ region, 800
Dautremont, J. L., Jr, grounded-grid poweramplifier design, 2884
Dauvillier, A., structure and mechanism of sunspots, 3665

I.7

- Davern, W., with P. Dubont, calculation of statistical absorption coefficient, 3920
 David, E. E., Jr., artificial auditory recognition in telephony, 331
 N. Guttman and W. A. van Bergeijk, mechanism of binaural fusion, 1055
 Davidse, J., adaptation of N.T.S.C. system to European standard, 4212
 Davidson, M., H. Joseph and N. Zucker, markerless pulse trains for communication, 956
 Davidson, R., ferrite-cored capacitors, 726
 Davies, D. E. N., radar-systems with electronic sector scanning, 818
 Davies, D. H., and K. F. Sander, electron trajectories in gun of M-type carcinotron, 318
 Davies, D. G., and A. C. B. Lovell, observations of the Russian moon rocket Lunik II, 4051
 and others, radar observations of 1957 B, 3290

- and clustral moor observations of 1957 *β*, 3290
 Davies, K., with S. Chapman, daytime constancy of absorption of radio waves in lower ionosphere, 809
- 809
 Davies, L. W., and D. K. Milne, metallic contacts to Ge and Si, 491
 Davies, M. W., phase-shift consideration in television, 3137
 Davies, R. S., and C. S. Weaver, minimum trans-

- Davies, M. W., phase-shift consideration in television, 3137
 Davies, R. S., and C. S. Weaver, minimum transmitter weight for space communications, 3141
 Davis, C. F., Jr, M. W. P. Strandberg and R. L. Khyl, electron spin-lattice relaxation times, 417
 Davis, C. M., Jr, with S. F. Ferebe, effect of divalent-ion substitutions on Ni ferrite, 1292
 Davis, D. T., with others, Barkhausen-Kurz oscillator at cm Å 1486
 Davis, G. L., with others, Barkhausen-Kurz oscillator at cm Å 1486
 Davis, G. L., with others, orientation control for Ge wafers, 1935
 Davis, G. L., with others, orientation control for Ge wafers, 1935
 Davis, G. L., with L. W. Schmidt, solar-cell power supply, 4206
 Davis, F. M., Jr, E. K. Smith and C. D. Ellyett, sporadic E at v.h.f. in U.S.A., 2587
 Davis, W. D., lifetimes and cross-sections in Au-doped Si, 3769
 Davydov, B. E., with others, producing polymers with semiconductor properties, 4121
 Dawson, J. M., nonlirear electron oscillations in cold plasma, 2535
 Day, J. W. B., with others, fuffaction of e.m. waves by ride, 241
 Da-Yü, Ma. See Ma Da-Yu.
 Dearborn, E. F., with J. W. Niclson, growth of single crystals of magnetic garnets, 1289
 Deb, S., and A. N. Daw, lifetime and diffusion constant of injected carriers, 2043
 Deeker, R. P., design of rhombic antenna, 3956
 Deeley, E. M., quadratic interpolation in tapped-potentiometer function generators, 2133
 Deering, P. E., with J. H. W. Beck, space-charge waves on annular bears, 3159 h; 3-cavity L-band pulsed klystron amplifier, 3524
 Deganou, U., with J. Barducci, research on probe microphones, 1429
 Deelors, S. et al. P. Scowit, 3-level solid-state travelling-wave maser, 2177
 With others, spin refrigeration and naser action at 1500 Mic/s, 3654
 De Hoop, A. T., with J. P. Schouten, reflection of

- Scout, 3-level solid-state travelling-wave maser, 2177
 with others, spin refrigeration and maser action at 1 500 Mc/s, 3654
 De Hoop, A. T., with J. P. Schouten, reflection of plane e.m. wave, 1333 v
 De Jager, C., solar radio bursts, 1333 g
 Dekhtyar, M. V., antiferromagnetic orientation in NiFe, 537
 Dekleva, J., and K. W. Robinson, shunt impedance measurement, 3421
 De Lange, O. E., timing of regenerative repeaters, 967
 and M. Pustelnyk, timing of regenerative repeaters, 968
 Delcroix, J. L., with others, wave interaction in gas, 1333 a
 De Loach, C. B., and W. M. Sharbless X-band

- Delcroix, J. L., with others, wave interaction in gas, 1333 a
 De Loach, C. B., and W. M. Sharpless, X-band parametric amplifier, 4006
 Delves, L. M., with H. A. Whale, relations between bearing and amplitude of fading radio wave, 947
 Delves, R., with others, magnetothermal resistance and magnetothermoelectric effects in Bi₁Te₂, 182
 Delves, R. T., transport coefficients for polar semiconductors, 2642
 Denney, R. C., with others, 21-in glass colour picture tube, 280
 Denes, P., mechanical speech recognizer, 2451
 Denisse, J. F., with M. R. Kumau, solar radiation at dm A as index for ionospheric studies, 787
 with others, wave interaction in gas, 1333 a
 Dennard, R. H., ferroresonant series circuit containing square-loop reactor, 2141
 De Prins, J., with J. P. Blassr, comparison of astronomical time measurements with atomic frequency standards, 914
- requency standards, 914 with others, improvements in NH, maser, 758 g ick, L., with C. J. Frosch, diffusion control in Si, 4096 Derick
- Derick, L., with C. J. Prosch, diffusion control in Si, 4096
 Dermit, G., with C. A. Stahl, Ge photo-tetrode, 308
 Deryagin, B. V., with V. P. Smitga, role of surface properties of semiconductors in adhesion, 495
 DeSautels, A. N., stable d.c. transistor servo preamplifier, 2176
 Descamps, Y., effect of thermal delay with grid compensation, 3864
 with C. Curie, compensation for fluctuations in anode current, 1369
 Deschamps, A., with others, substitution of Al, Ga and Cr in BaO.6Fe₂O₃, 541
 Desloge, E. A., S. W. Mathysse and H. Margenau, conductivity of plasmas to microwaves, 1842

I.8

- Dessler, A. J., hydromagnetic waves, above ionosphere, 110, ionospheric heating by, 2585; effect of magnetic anomaly on particle radiation, 3662; upper-atmosphere density variations due to hydromagnetic heating, 4057
 Dessoulavy, R., feedback in transistor amplifiers, 3239
- 3239
- Destriau, G., 'memory' effect in enhancement of luminescence, 1213 Detert, K., with G. W. Wiener, cube-oriented magnetic

- luminescence, 1213
 Detert, K., with G. W. Wiener, cube-oriented magnetic sheet, 896
 Deutsch, J., ferrites and their microwave applications, 4140
 Deutscher, K., interference photocathodes of increased yield, 2053
 De Vaux, L. H., with others, infrared detectors, 4239
 Devratl, G. V., with others, optics and photography in flying-spot store, 2363
 DeVyatkova, N. D., electronic devices for extremely high frequencies, 641
 Devyatkova, E. D., and I. A. Smirnov, thermoconductivity of Ge, 1620
 De Waard, R., and E. M. Wormser, thermal detectors, 4010 g
 De Witt, R. N., with others, auroral ionosphere studies using earth satellites, 4052
 Dhar Bhowmik, P., with J. N. Bhar, study of noon F₃ ionization, 2584
 Dickerson, A. F., with others, thermionic integrated micromodules, 2863
 Dicknson, W. A., and W. D. Schuster, picture tubes with 110° defection. micromodules, 2863
 Dickinson, W. A., and W. D. Schuster, picture tubes with 110° deflection, 284
 Diemer, G., G. J. van Gurp and W. Hoogenstraaten, exciton diffusion in CdS crystals, 2265
 and A. J. Van der Houven van Oordt, nature of blue edge emission in CdS, 2269
 H. A. Klasens and P. Zalm, electroluminescence and image intensification, 1597
 Dieminger, W., pulse propagation experiments.

- and image intensification, 1597
 Dieminger, W., pulse propagation experiments, 1333 e
 H. G. Möller and C. Rose, long-distance single-F-hop transmission, 943; sweep-frequency oblique-incidence pulse transmissions, 2378
 Dierk, E. A., with others, temperature dependence of electron emission of B if lims, 2619
 Diessel, T. J., with others, primary pyroelectricity in BaTiO₃ ceramics, 156
 Diestel, H. G., and W. Mike, reciprocity method for vibration measurements, 3178

- vibration measurements, aluge, reciprocity method for vibration measurements, 3178
 Dieter, F. A., with others, analysis of emissive phase of pulsed maser, 756
 Dillenburger, W., standards converter using vidicon camera, 2405; limiters in television equipment, 3491
 Dillon, J. A., Jr, R. E. Schlier and H. E. Farnsworth, surface properties of SiC crystals, 3022
 Dillon, J. F., Jr, observation of domains in ferrimagnetic garnets by transmitted light, 200; ferrimagnetic modes in Y-Fe garnet, 907; magnetostatic modes in ferrimagnetic spheres, 908
 and H. E. Farl. Is domain minimum sphere.
- and H. E. Earl, Jr, domain-wall motion and resonance in Mn ferrite, 1958

- and H. E. Edd, Jr, comain-wall motion and resonance in Mn ferrite, 1958
 and J. W. Nielsen, effect of impurities on resonance in Y-Fe garnet, 3811
 Dion, A., nooresonant slotted arrays, 3202
 Diserens, N. J., with K. H. Kreuchen, development of high-power klystrons, 3524 i
 Ditchfield, C. R., and P. A. Forrester, maser action in 60°K region, 1143
 Ditl, A., amplitude and frequency of modulated carrier wave, 2007; power transmission at high efficiency, 3944
 Dix, C. H., and R. G. Robertshaw, pulsed travelling-wave tubes in 10-Gc/s region, 2788 m
 Dix, J. R., and D. P. Envight, effect of heat treatment on InAs, 3032
 with F. Stern, narrowing energy gap in semiconductors by compensation, 1917
 Dixon, N. E., phase relations in stagger-tuned klystron amplifier, 3524 d
 Dizer, M., sudden disappearance of filaments and

- Dixon, N. E., phase relations in stagger-tuned klystron amplifier, 3524 d
 Dizer, M., sudden disappearance of filaments and magnetic storms, 2948
 Diugatch, I., optimizing antenna switches, 3568; miniature resonators for u.h.f., 3604
 Dnestrovskii, Yu. N., variation of natural frequencies of membranes, 1039
 Doak, P. E., fluctuations of sound pressure when receiver posi ion is varied, 3915
 Dobesch, H., characteristics of all-pass filters for delay equalization. 737
 F. Weide and H. Sulanke, equalization in television transmission by cable, 3488
 Dobryo, W. I., with otlers, primary pyroelectricity in BaTiO₂ ceramics, 156
 Dobryakova, F. F., with otlers, electron concentration of ionosphere from observations of first earth satellite, 3298
 Doctor, N. J., with otlers, D.O.F.L. microelectronics program, 2484
 Doehler, O., A. Dubois and D. Maillart, M-type pulsed amplifier, 2788 k
 B. Epstein and J. Arnaud, characteristics of carmatron tube, 2788 r
 with others, lectron velocities and pass band in travelling-wave amplifiers, 316
 Doehring, A., with others, fixed-frequency cyclotron with one dee, 1985
 Dohory, L. H., and G. Neal, 215-mile radiolink, 4202
 Dolginov, S. Sh., with N. V. Pushkov, investigation of earth's magnetic field using earth satellite, 3693
 Dolphin, L., with others, radar investigations of auroral echoes, 4065
- Dolphin, L., with others, radar investigations of auroral echoes, 4065

World Radio History

Domb, C., fluctuation phenomena and stochastic

- Domb, C., fluctuation phenomena and stochastic processes, 4007
 Dörme, P., with J. Lüscher, transistor simulator, 4156
 Dorme, R. B., inexpensive sound for television receivers, 2027; amplifier design reduces plate dissipation, 2514
 Doniach, S., lattice screening in polar semiconductors, 3344
 Donovan, B., with J. C. Anderson, internal ferromagnetic resonance in Ni, 2684
 Dooley, J. C., Melbourne-Toolangi magnetic observatory, 1531
 Dorbrotin, N. A., investigation of cosmic rays by earth satellites, 3690
 Dorremus, L. W., charge release of ceramic ferroelectrics, 2630
 Dorgelo, E. G., output and load resistance of triodes for r.f. heating, 2072; oscillator triodes in h.f. generators with variable load, 2795; current limitation of c.w. magnetrons, 3162
 and J. C. van Warmerdam, intermittent use of valves in r.f. heating generators, 2071
 Dortort, I. K., current-balancing reactors for semiconductor rectifiers, 606
 Dosse, D., theory of wide-band distributed amplifiers, 747
 Douce, J. L., and J. C. West, magnetic-drum store for

Dosse, D., theory of wide-band distributed amplifiers, 747
Douce, J. L., and J. C. West, magnetic-drum store for analogue computing, 348
Doucette, E. I., with others, semiconductor current limiter, 1368
Dougal, A. A., with E. P. Bialecke, electron-ion recombination coefficient in nitrogen, 125
Dougharty, W., broad-band coupled circuits, 3995
Dougharty, W., broad-band coupled circuits, 3995
Dougharty, G., semiconductor surface potential from field-induced changes, 851; effects of carrier injection on recombination velocity, 1916
and R. C. Duncan, Jr, space-charge regions in semiconductor surfaces, 848
Dowden, R. L., and G. T. Goldstone, 'whistler mode' echoes, 2731
Doxey, W. L., with others, micro-module approach to miniaturization, 2485
Doyle, R. J., R. A. Meyer and R. P. Pedowitz, automatic failure recovery in data processing system, 1453
Doyle, J. R., galvanomagnetic effects in p-type

Doyle, W. T., selective photoelectric effect, 4075
Drabble, J. R., galvanomagnetic effects in p-type Bi, Teg., 183; effect of strain on thermoelectric properties of many-valley semiconductor, 854
and C. H. L. Goodman, chemical bonding in Bi, Teg., 531
and R. D. Groves, strain-induced changes in Seebeck coefficient of n-type Ge, 3374
Drachev, L. A., with others, large inhomogeneities in Fg layer, 2581
Dracott, E. D., with others, high-power 400-Mc/s klystron, 3524 j
Dransfield, K., with H. E. Bömmel, attenuation of hypersonic waves by ferromagnetic resonance, 3817
Drechsel, D., test equipment for ferrites, 4155

asi7
Drechsel, D., test equipment for ferrites, 4155
Drechsel, W., with J. Kranz, observation of Weiss domains in polycrystalline material, 1281
Dreher, J. J., with J. Kranz, observation of Meiss domains in polycrystalline material, 1281
Dreher, J. J., with H. Kallmann, excitation of luminescent materials by ionizing radiation, 3325
Drewes, G. W. J., with others, h.f. susceptibilities of paramagnetic alums, 2332
Dreyfus-Alain, B., and M. Darmony, Si transistors by alternate doping, 301
with M. Darmony, solid-state diffusion applied to semiconductor devices, 184
Driatski, V. M., and A. S. Besproxannaya, ionospheric conditions in the circumpolar region, 3717
Drickamer, H. G., with T. E. Slykhouse, effect of

Driatski, V. M., and A. S. Besprozvannaya, ionospheric conditions in the circumpolar region, 3717
 Drickamer, H. G., with T. E. Slykhouse, effect of pressure on absorption edge of Ge and Si, 1243
 Drougard, M. E., with others, electromechanical behaviour of BaTiO, 3334
 Drozdov, N. G., with others, investigations on Li-Zn ferrites, 1957
 Drummond, J. E., microwave propagation in hot magneto-plasmas, 1841
 with A. H. Allan, Doppler measurements on Soviet satellites, 443
 Dryden, J. S., measurement of dielectric properties of liquids in H_a resonator, 922
 and R. J. Mcakins, impregnants for paper capacitors, 1474
 Dubols, R., Ge power transistors, 302
 Dubont, P., and W. Davern, calculation of statistical absorption coefficient, 3920
 Duclaux, F., and R. Will, lunar-diurnal variation of geomagnetic field, 2228
 Dudding, R. W., and D. J. Finnett, application of organic films to phosphor screens, 2438
 Dudkey, H., phonetic pattern recognition vocoder for narrow-band speech transmission, 1057
 and S. Balashek, automatic recognition of phonetic patterns in speech, 1061
 Dudley, M. J., J. A. Shand and C. Wright, causes of geomagnetic fluctuations with 6-sec period, 2945
 and others, geographical variations in geomagnetic macrow-band speech transmission geomagnetic marrow-band speech transmission, 1057
 and S. Balashek, automatic recognition of phonetic patterns in speech, 1061
 Dudley, M. J., A. Shand and C. Wright, causes of geomagnetic fluctuations with 6-sec period, 2945
 and others, geographical variations in geomagnetic micropulsations, 2946
 Duggan, T. C., with D. A. Bell, relative speeds of telegraphic codes, 593
 Duthamel, R. H., and J. W. Duncan, launching efficiency of wires and slots, 2830
 with J. W. Dumean, radiation from dielectric rod wavegui

Electronic & Radio Engineer

Duivenstijn, A. J., 30 years' s.w. broadcasting in Netherlands, 265
 Dulberger, L. H., pulse amplifier with nonlinear feedback, 386; improved RC oscillator, 1808
 Dummer, G. W. A., future electronic components, 254

feedback, 386; improved RC oscillator, 1808
Dummer, G. W. A., future electronic components, 354
Dumont, A., and H. d'Hoop, measurement of pulsed powers at m A, 3829
Duncan, J. W., and R. H. DuHamel, radiation from dielectric rod waveguides, 1095
with R. H. DuHamel, launching efficiency of wires and slots, 2830
Duncan, R. A., dG. R. Ellis, subvisual aurorae and radio noise bursts, 2974
Duncan, R. A., computations of electron density distributions in ionosphere, 126
Duncan, R. A., outh G. C. Dousmanis, space-charge regions in semiconductor surfaces, 648
with others, evidence for carriers with negative mass, 875
Dunham, B., and others, multipurpose bias device of logical elements, 1461
Dunn, D. A., wide-band microwave tubes, 642; travelling-wave amplifiers and backward-wave oscillators for v.h.f., 1024
with others, 20-40-kMc/s backward-wave oscillator, 1742
Dunn, G. A., and N. C. Hekimian, tube-transistor hybrids, 2877
Dunn, J. H., and D. D. Howard, effects of a.g.c. on accuracy of monopulse radar, 1894
D. D. Howard and A. M. King, scintillation noise in radar tracking systems, 2609
Duansurir, R., theory of circular magnetrons with rotating space charge, 2788 g
Durandeau, P., B. Fagot and C. Fert, spherical aberation in magnetic lenses, 3838

reduction in feedback integrators, 369
Durandeau, P., B. Fagot and C. Fert, spherical aberration in magnetic lenses, 3838
B. Fagot and M. Laudet, measurement of induction in magnetic electron lenses, 2704
Dutka, J., error-correcting techniques, 1358
Dutton, D., anisotropy of edge luminescence in CdS, 474; fundamental absorption edge in CdS, 1208
with A. Smith, behaviour of PbS photocells in ultraviolet, 1407
Dutton, J., and E. Jones, electrical discharges, 2196
van Duuren, K., and J. Hermsen, halogen-quenched end-window Geiger counters, 3079
A. J. M. Jaspers and J. Hermsch, G-M counters, 3446
Dwight, K., with N. Menyuk, low-temperature

Dwight, K., with N. Menyuk, low-temperature transition in Ni-Fe ferrite, 902

D'yakonova, T. S., with A. I. Likhter, dependence of Hall effect on pressure in n-type Ge, 2663
 Dye, N. E., and others, vacuum-diode microwave detection, 2794
 Dyer, R. F., with D. K. Bisson, Si-controlled rectifier, 4227

4227
4227
4227
4227
4229
4230
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modulation noise of c.w. hyston and 3524 k Dyson, J. D., capacitance of two infinite cones, 3820; equiangular spiral antenna, 3949

Equivalgurar spiral antenna, 3949
Earl, H. E., Jr, with J. F. Dillon, Jr, domain-wall motion and resonance in Mn ferrite, 1958
Early, J. M., structure-determined gain-band product of junction triode, 997
Earp, C. W., and D. L. Cooper-Jones, evolution of commutated-aerial d.f. systems, 2259 k
Easter, B., G. H. Maddock and R. G. Medhurst, dependence of combine tiversity gain on signal-level distribution, 4191
Easterday, J. L., and H. Braner, derating requirements for carbon composition resistors, 2491
Eastman, P. C., with M. S. Sodha, nondegenerate semiconductors, Hall mobility in, 856, mobility of electrons in, 1225, drift and Hall mobility in, 3340
Easton, R. L., and M. J. Votaw. Vanguard I. 1868

Easton, R. L., and M. J. Votaw, Vanguard I, 1868

Source State St

- 4194

4194 Echizenya, Y., with others, F₂-layer multiple reflections, 1342 Eckardt, W., measurements on television-camera preamplifiers, 3115 Eckart, G., rotation of polarization of electric waves, 2451

- 3451
 3451
 Eckels, A., with others, earth's gravitational potential from satellite orbit, 1867; Vanguard measurements of earth's figure, 2236
 Ecker, G., and J. Fassbender, conduction mechanism of CdS sandwich photocells, 1406
 Eckhardt, H. E., and A. G. Robeer, 100-kW s.w. broadcast transmitter, 293
 Edels, H., with Y. Ettinger, time-controlled unit-function constant-voltage generator, 4205
 Eden, E., designing optimum transmitter networks, 3501
 Edens, A. H., sealing window and constant.

Edens, A. H., sealing window and cone of television picture tubes, 1035

Electronic & Radio Engineer

Edge, D. O., P. A. G. Scheuer and J. R. Shakeshaft, spatial distribution of radio sources at 159 Mc/s, 103

103
Edmond, J. T., behaviour of impurities in III-V compounds, 2641
Edmonds, D. T., and R. G. Petersen, effective exchange constant in Y-Fe garnet, 3401
Edsman, S., new electron tubes for wide-band amplifiers, 1032
Edwards, C., influence of output time-constant of cathode follower, 751
Edwards, K. A., O. Golubjatnikov and D. J. Brady, transistor phase-locked oscillators, 2162
Edwards, L. C., with D. A. Hedlund, polarization

transistor phase-locked oscillators, 2162
Edwards, L. C., with D. A. Hedlund, polarization fading over oblique-incidence path, 1668
Edwards, S. F., classical plasma, equilibrium properties of, 86, charge density of, 87; evaluation of conductivity in metals, 1507
Efimov, E. A., and I. G. Erusalimchik, Ge electrode with p-n junction, 527
Efremov, A. I., with S. L. Mandel'shtam, ultraviolet solar radiation, 3664
Egan, R. D., with others, 3-frequency back-scatter sounder, 1565
Egorov, V. A., dynamic problems of flight to moon, 3675

Egorov, V. A., dynamic problems of flight to moon, 3675
Ehlers, H., and H. Thies, synchronizing transmitter frequencies, 4224
Ehrenreich, H., transport of electrons in intrinsic InSb, 4117
with others, observation of phonons during tunnelling in junction diodes, 4226
Eichenbaum, A. L., and R. W. Peter, exponential gun, 2064
Eichhoff, G., emission spectra and absorption edge of S in CdS, 1216
Eichholz, J. J., C. F. Nelson and G. T. Weiss, extended-range distributed-amplifier design, 1492
Eichin, V. A., with A. P. Vyatkin, origin of fluctuation of crystal triode parameters, 628
Eichin, W., and G. Landauer, gain and stability of travelling-wave valve, 1411
Eidman, V. Ya., with V. L. Ginzburg, Cherenkov radiation from dipoles, 3647
Eisenhauer, G. M., with others, lattice vibrations in Ge by neutron scattering, 2304
Eklund, F., with J. Josephson, microwave propagation experiences, 3091
Eklund, K., operational amplifiers in current regulators, 3113
Ekstrom, J. L., sinplified product detector design, 2896

Ekstrom, J. L., simplified product detector design,

2898

2598
 Elders, D., construction concept for linear delay lines, 697
 Eldredge, K. R., F. J. Kamphoefner and P. H. Wendt, automatic input equipment for data processing, 3586
 Eldridge, D., digital technique for computer use, 2127

Eldridge, D., digital technique for computer use, 2127
Elford, W. G., with others, c.w. technique for measurement of meteor velocities, 105
Elgaroy, O., fine structure of solar bursts in 200-Mc/s range, 2935
Ellias, P., computation in presence of noise, 345
Eliezer, C. J., consistency condition for electron wave functions, 2537
Elliott, R. J., T. P. McLean and G. G. Macfarlane, effect of magnetic field on absorption edge in semiconductors, 501
Elliott, R. S., pulse waveform degradation in waveguide, 1071
— and K. C. Kelly, serrated waveguide, 1074
— with others, U.R.S.I. report on antennas and waveguides, 3565
Ellis, G. R., trapping of cosmic radio waves beneath

waveguides, 3565
 Fillis, G. R., trapping of cosmic radio waves beneath ionosphere, 788
 with R. Duncan, sub-visual aurorae and radio noise bursts, 2974
 Ellis, S. G., growth of GaAs crystals from melt, 3382

Ellis, S. G., growth of GaAs crystals from melt, 3382
Ellyett, C., and H. Leighton, solar-cycle influence on lower ionosphere and v.h.f. scatter, 130
Ellyett, C. D., with others, sporadic E at v.h.f. in U.S.A., 2587
Elsmore, B., positions of 17 intense radio stars, 2932
Emeleus, K. G., and D. W. Mahaffey, transit-time relation for plasma electron oscillations, 1840
Endler, H., A. D. Berk and W. L. Whirry, relaxation phenomena in diode parametric amplifiers, 3626
Enev, T. M., with D. E. Okhotsimskif, variational problems of satellite launching, 3680
with others, determination of lifetime of artificial earth satellite, 3681
Enemark, D., transistors improve telemeter trans-

earth satellite, 3681 Enemark, D., transistors improve telemeter trans-mitter, 2373 Engbert, W., manufacture and characteristics of junction transistors, 4229 Enge, H. A., ion focusing properties of quadrupole lens pair, 2721 Engelmann, R. H., wide-band amplifier design data, 1401

1491
 Engen, G. F., amplitude stabilization of microwave signal source, 2353
 Enkel, F., automatic monitoring of broadcast channels, 1397
 Enoch, J. M., and G. A. Fry, model retinal receptor, 1325

1325
Enright, D. P., with J. R. Dixon, effect of heat treatment on InAs, 3032
Enslein, K., Si junction diodes as voltage-reference devices, 2039
Enz, U., relation between disaccommodation and magnetic properties of Mn ferrite, 2327
Epprecht, G. W., low-reflection discontinuities in diameter of coaxial lines, 1073; circle diagram for transformations in transmission-line technique, 2460; compensated support disks for coaxial lines, 3926

World Radio History

Epstein, M., with others, magnetostrictive delay line for video signals, 1134 **Epsztein**, B., large-signal behaviour in M-type valves, 2788 ee

Epsztein, B., large-signal behaviour in M-type valves, 2788 ee
with others, electron velocities and pass band in travelling-wave amplifiers, 316; characteristics of carmatron tube, 2788 r
Ernest, J., radiation from fine slot, 21, 22; conical radiation from travelling-wave slot, 3580
Erusalimchik, I. G., with E. A. Efimov, Ge electrode with p-n junction, 527
Esaki, L., with T. Yajima, excess noise in narrow Ge p-n junctions, 1257
Eshelby, J. D., elastic model of lattice defects, 1173
Eshleman, V. R., with L. A. Manning, meteors in ionosphere, 1526; Booker's theory of meteoric reflection, 1527
Esan, O. A., with V. L. Zyazev, influence of shortrange order on type of conductivity, 3750
Essen, L., E. G. Hope and J. V. L. Parry, circuits in N.P.L. Cs standard, 2340
and others, comparison of Cs frequency standards, 212
Ettinger, Y., and H. Edels, time-controlled unit

and others, comparison of CS frequency standards, 212
 Ettinger, Y., and H. Edels, time-controlled unit-function constant-voltage generator, 4205
 Evans, D. M., dependence of moinority-carrier life-time on majority-carrier density, 849; temper-ature dependence of mobility and lifetime in Si transistors, 3150
 Evans, H. W., with S. D. Hathaway, radio attenuation at 11 kMc/s, 1673, 2381
 Evans, J. V., with others, radar observations of 1957 β, 3290
 Evseev, V. M., operational amplifier without stabilized power supply, 1494
 Ewing, R. D., with R. D. Spence, antiferromagnetism in Cu₃(Co₃)₄(OH)₂, 1947
 Eyraud, I., and P. Bonijoly, differential bridge for impedance measurements, 3429
 Eyraud, J. P., with others, instrumenting Explorer I, 1547

Fagot, B., with others, magnetic lenses, measurement of induction in, 2704, spherical aberration in, 3838

3838
Fahring, R. H., with W. E. Medcalf, growth of CdS crystals, 4077
Fain, V. M., with V. L. Ginzburg, quantum effects in interactions in resonators, 1844
Fakidov, I. G., and E. A. Zavadskii, oscillation of resistance of n-type Ge in pulsed inagnetic fields, 872

helds, 872
helds, 872
Fälker, R., and E. E. Hicking, magnetic measurements on ferrite U-cores, 3057
Fan, H. Y., and A. K. Ramdas, infrared absorption and photoconductivity in irradiated Si, 4089 b
with P. Fisher, absorption effects of group III impurities in Ge, 3366
with R. A. Laff, magnetoresistance in n-type Ge, 870

870
 with others, photoconduction of Ge after bombardment, 3027
 Fan Shou-syan'. See Shou-syan' Fan.
 Fang, P. H., conductivity of plasmas to microwaves, 2020
 and W. S. Brower, temperature dependence of breakdown field of BaTiO₃, 2627
 Fant, G., acoustic studies of speech, 1058
 Darbeing B. L. with S. P. Boucheinge macupaget

Fant, G., acoustic studies of speech, 1058
Farber, R. J., with S. P. Ronsheimer, measurement of colour television receiver performance, 986
Farmer, J. C., long-range radio navigation aids, 2259 b
Farnell, G. W., axial phase anomaly for microwave lenses, 713
Farnsworth, H. E., with H. H. Madden, high-vacuum studies of surface recombination velocity for Ge, 1248
with others, surface properties of SiC crystals, 3022
Farrads, J. L., with others, observations of detona-

3022 Farrands, J. L., with others, observations of detona-tion by interferometer, 3068 Farris, H. W., alternative detection of co-channel f.m. signals, 581 Fassbender, J., with G. Ecker, conduction mechanism of CdS sandwich photocells, 1406

of Cas sandwich photocens, 1400
 Fatebchand, R., characteristics of random noise in television, 3140
 and R. Ahmed, electronic speech sampler, 2820
 Favre, M., cross-field carcinotrons under pulse operation, 2788 s

Tavre, R., cross-field carcinotrons under pulse operation, 2788 s
 Feaster, G. R., thermionic diodes as energy converters, 324
 Federici, M., sound echo reflected from sphere under pulse conditions, 1046
 Fedorov, E. K., investigation of upper atmosphere by rockets and satellites, 439
 Federici, M., sound echo reflected from sphere under pulse conditions, 1046
 Fedorov, G. V., with others, Hall-effect in pure Ni at He temperatures, 2322; change of sign of Hall constant in alloys, 2675
 Feher, G., nuclear polarization via 'hot' conduction electrons, 4011; electron-spin-resonance experiments on donors in Si, 4098
 D. K. Wilson and E. A. Gere, electron-spin-resonance experiments on Genors in Si, 4097
 D. K. Wilson and E. A. Gere, electron-spin-resonance experiments on spherics, 1579; geophysical effects of nuclear explosions, 4056
 Feibelman, W. A., 27-kc/s anomaly in sudden enhancement of atmospherics, 1579; geophysical effects of symmetrical multivibrator, 1806
 Feinberg, E. L., propagation of radiowaves along inhomogeneous surface, 3841
 Feinberg, R., effect of temperature on persistence of c.r. tube screens, 2440; luminescence of shortpersistence phosphors, 3001; effect of trigger pulse polarity in cold-cathode tetrode, 3174
 Feldman, L., f.m. tuner adaptor for multiplexed stereo, 1679

Feldmann, W. L., with G. L. Pearson, powder-pattern techniques, for delineating domain imanu, pattern technik structures, 4085 M. O., wit

structures, 4085
Felix, M. O., with A. J. Buzton, reduction of threshold by frequency compression, 2000 q
Fellows, E. C., with R. Builey, stabilization of 9-kW electromagnet, 3072
Felsen, L. B., radiation from ring sources, 3965

- Fen, G. I., valence semiconductors-Ge and Si. 3351 Fennick, B., phase-selective gate rejects quadrature, 719
- 719
 Fenton, A. G., and others, decreases in cosmic-ray intensity during period October 1956-January 1958, 4037
 Fer, F., cyclotrons with star-shaped field, 2370
 Ferebee, S. F., and C. M. Davis, Jr, effect of divalent-ion substitutions on Ni ferrite, 1292
 Ferguson, K. H., with others, generation of stable carrier frequencies, 3987

- Ferguson, K. H., with others, generation of stable carrier frequencies, 3987
 Fernandes, A. A. de C., design of rhombic antenna arrays, 3576
 Ferro, A., with others, instability of Bloch walls in ferromagnetic material, 535
 Fert, C., and F. Pradal, energy spectrum of electron beam passing through thin film, 3255
 with others, spherical aberration in magnetic lenses, 3838
 Fewer, D. R., transistor nonlinearity, 1817
 Fiala, W. T., acoustic-front damping, 2455
 with J. K. Hilliard, generating high-intensity sound with loudspeakers, 692
 Fiedler, H., influence of penetration factor fluctuations on triode Type 2C40, 2437
 Fiedler, H. C., with others, cube-oriented magnetic sheet, 896
 Fiedly, J., tropospheric scatter propagation and equipment, 3452
 Field, A. G., predicting reliability of complex equipment, 2806
 Field, C. C., trap improves TV picture, 988
 File, S. L., 3-band aerial combining network, 733

- Field, G. C., trap improves TV picture, 988
 Fife, S. L., 3-band aerial combining network, 733
 Finn, G., and R. Parsons, Si and rectifier design, 604
 Finnett, D. J., with R. W. Dudding, application of organic films to phosphor screens, 2438
 Finney, J. W., with others, I.G.Y. observations of F-layer scatter in Far East, 2733
 Finzi, L. A., and J. J. Suozzi, feedback in magnetic amplifiers, 2172, 3998
- Finst, L. A., and J. J. Subzz, leedback in magnetic amplifiers, 2172, 3998
 Firsov, Yu. A., magnetic susceptibility in Te-type semiconductors, 1607; cyclotron resonance in semiconductors, 2647
 Fischacher, R. E., reliability in electronic instru-mentation, 2076
 Fischell, R. E., with others, radiation effects in magnetic materials, 196
 Fischer, F. A., equivalent circuits for transient vibrations of transducers, 3904
 Fischer, K., multicoupler and antenna amplifier for v.h.f., 749
 Fischer, K. H., and G. Daisenberger, amplification of wide frequency bands, 1490
 Fischer, T., with G. Busch, field emission from semiconductors, 3016
 Fischern, M., transistorized horizontal deflection, 3870

- 3870 3870
 Fischmann-Arbel, A., sampling comparator, 919
 Fisher, F., and I. P. Valkó, new mechanism for generation of flicker noise, 1028
 Fisher, M. E., and M. F. Sykes, Ising model of ferromagnetism, 3263
 Fisher, P., and H. Y. Fan, absorption effects of group III impurities in Ge, 3366

- group III impurities in Ge, 3366
 Fistul', V. I., with R. N. Rubinshtein, determination of surface conductivity of semiconducting crystals, 2671
 Fitch, E., and R. Ruddlesden, aerial height for ionospheric scatter links, 2000 c
 Fitzgerald, E. R., mechanical resonance dispersion in quartz at a.t., 1219
 Fitzky, H. G., frequency standard for microwave spectrometers, 3054
 Fitx, H., portable television cameras for outside broadcasts, 2026

- Fleischer, H., radio observations of earth satellites, 3289

- r isscner, H., radio observations of earth satellites, 3289
 Fleischer, I., communication theory for infinite alphabets, 958
 Fleishman, B. S., optimum detector for weak signals in noise, 2004
 Fletcher, P.C., and R. O. Bell, ferrimagnetic resonance modes in spheres, 2928
 I. H. Solt, Jr, and R. Bell, magnetostatic modes of ferrimagnetic spheres, 3813
 Flinn, M., with others, high-power 400-Mc/s klystron, 3524 j
 Flint, R. B. with S. R. Anderson, C.A.A. Doppler omnirange, 2610
 Flippen, R. B., with J. H. Wasilik, piezoelectric effect in InSb, 180
 Florine, J., practical applications of semiconductors, 3233
 Flubacher, P., A. J. Leadbetter and J. A. Morrison.

- 3233
 Flubacher, P., A. J. Leadbetter and J. A. Morrison, heat capacity of pure Si and Ge, 3353
 Flügge, S., Handbuch der Physik, Vol. 16, (B)3657
 Flunkert, H., with H. E. Müser, upper Curie temperature and domain structure in Rochelle salt, 1218
- salt, 1218
 Flynn, J. B., saturation currents in Ge and Si electrodes, 4093
 Foldes, P., travelling-wave cylindrical antenna design, 3569
 and L. Solymar, lens-aerial design, 1100
 Follingstad, H. G., linear characterization of transistors, 2048
 Fomenko, L. A., magnetic spectra of ferrites, 3398
 Foner, S., L. R. Momo and A. Mayer, multilevel pulsed-field maser, 3623
 Foot, J. B. L., with others, propagation measurements at 3480 Mc/s, 2000 r

- Forbes, G. R., Jr, with others, tracking earth satellites, 123
 Forbush, S. E., cosmic-ray intensity variations during solar cycles, 1523
 Forgue, S. V., with G. A. Morton, infrared pickup tube, 4242
 Forman, J. M., and G. P. Kirkpatrick, screen persistence of colour picture tubes, 4218
 Formwalt, J. M., with D. T. Barry, underwater missile tracking instrumentation, 2597
 Forrester, M. P., analysis of mas pulse transmission, 362

- 362
 Forrester, A. T., with others, evidence for energy gap in superconductors, 393
 Forrester, P. A., with C. R. Ditchfield, maser action in 60°K region, 1143
 Forster, D. C., with M. R. Currie, noise-reduction mechanism in electron beams, 1727; minimum noise generation in backward-wave amplifiers, 1734
 Forster J. H. and M. S. Valaria, offer the sufficient of the
- Forster, J. H., and N. S. Veloric, effect of surface
- Forster, J. H., and N. S. Veloric, effect of surface potential on junction characteristics, 3390
 Forsyth, P. A., forward-scattered signal from overdense meteor trail, 576
 with C. Collins, bistatic radio investigation of auroral ionization, 2001
 Fort, E., with others, ionization chambers as sources of current, 4152
 Forte, S. S., synthesis of 2-terminal-pair networks, 2146; design of band-pass filters in waveguides, 3339
 Fortini, M. M., and J. Vilms, solid-state generator

- Forte, S. S., synthesis of 2-terminal-part fletworks, 2146; design of band-pass filters in waveguides, 3339
 Fortinil, M. M., and J. Vilms, solid-state generator for microwave power, 3991
 Fortunatova, N. N., with others, Ge with Fe impurity, recombination of current carriers in, 1933, effect of annealing on carrier lifetime in, 1934
 Foster, H., with others, design of high-power S-band magnetron, 2788 d
 Foster, J. S., microwave antenna with sawtooth scan, 2121
 Foster, K., impedance and phase velocity of triplate line, 701
 Foulds, K. W. H., and P. M. J. C. da S. Sampaio, electric-field distributions in waveguide containing dielectric slab, 3940
 Fowler, J. F., with others, low-noise travelling-wave tubes, 2063
 Fowler, P. H., and C. J. Waddington, artificial aurora, 1888
 Fowler, T. C. R. S., 6-channel high-frequency telemetry system, 4173
 Fraioli, A. V., solid-state electrolytic capacitors, 111
 Frank, L. A., with J. A. Van Allen, radiation around the earth, 2553; radiation measurements

- Fraioli, A. V., solid-state electrolytic capacitors, 1111
 Frank, L. A., with J. A. Van Allen, radiation around the earth, 2553; radiation measurements with Fioneer 1V, 4041
 Frankl, D. R., electroluminescence of ZnS crystals with cathode barriers, 835
 Franklin, C. A., with others, lightweight airborne navigation system, 2599
 Franklin, K. L., and B. F. Burke, observations of planet Jupiter, 1522
 Franklin, P. J., with others, voltage-sensitive switch, 39
 Franz, G. R., development of DEW line, 1592
 Franz, G. R., development of DEW line, 1592
 Franz, G. R., development of DEW line, 1592
 Franz, S. J., with others, waveguides for use in cryostats, 1767
 Frazer, W., and R. E. Schemel, modulator as phase detector, 2899
 Fredericks, W. J., with R. L. Kelly, polarization of excitation bands in CdS, 2991
 Freedman, A. L., magnetic-core matrices for logical functions, 2860
 Freetney, F. E., with others, ceramic X-band cavity resonators, 363

- logical functions, 2860
 Freethey, F. E., with others, ceramic X-band cavity resonators, 363
 Frei, A. H., and M. J. O. Strutt, analogue-computer measurements on diodes and transistors, 3508
 Freier, P. S., E. P. Ney and C. J. Waddington, cosmic-ray α particles during solar maximum, 3279
- cosm 3279 ith others, protons from sun 12th May 1959,
- with others, protons from sun 12th May 1959, 4040
 Freitag, W., and H. J. Martin, electronic ultrasonic image converter, 2084
 Fréon, A., J. Berry and J. P. Coste, recurrent variations in the intensity of primary cosmic
- variations in the intensity of primary cosinic radiation, 3278
 Frerichs, R., and R. Handy, electroluminescence in Cu₂O, 3005
 Fric, C., magnetic-field stabilizer with feedback, 1365
 Fricker, S. J., and others, u.h.f. signals reflected from moon, 1525
- moon, 1525 Fridrikhov, S. A., with others, secondary emission from Ni, 3789 Fried, L., forced-convection cooled electronic equipment, 1750 Friedel, J., electron structure of metals, 418 Friedheim, H. O., hybrid transformers, 1468 Friedman, H., rocket observations of ionosphere, 1559
- 1559

- 1559
 Friedman, I. B., constant-voltage regulators, 607
 Friedrich, J., with H. Schirmer, electrical conductivity of plasma, 1161
 Friedinghaus, R., with others, generation of very short ultrasonic pulses, 2078
 Frisch, E., two-valve oscillators in π-network form 3985
- form 3985 Frisch, H. L., with others, formation of donor states in heat-treated Si, 1926 Frischmann, P. G., with others, cube-oriented magnetic sheet, 896 Fritzsche, H., resistivity and Hall coefficient of Sb-doped Ge, 526

World Radio History

and K. Lark-Horovitz, effect of minority impurities in p-type Ge, 2658
 Froese, C., calculation of velocity of sound in sea-water, 3903
 Fröling, H. E., short aerial systems, 3946
 Froome, K. D., velocity of e.m. waves, 2190
 Frosch, C. J., and L. Derick, diffusion control in Si, 4096
 with others, infrared properties of SiC film, 2298
 Fröschle, E., etching method for manufacture of thin base layers of n-type Ge, 2665
 Frumkin, A. L., with others, investigations on Li-Zn ferrites, 1957
 Fry, D. B., theory of mechanical speech recognition, 2452
 Fry, G.A., with J. M. Enoch. model retinal recentor

Fry, G. A., with J. M. Enoch, model retinal receptor, 1325

Fry, G. A., with J. M. Enoch, model retinal receptor, 1325
Fryer, T. B., frequency analyser with two reference signals, 2712
Frubini, E. G., and E. A. Guillemin, minimuminsertion-loss filters, 1117
Fujli, S., with others, proof of mode theory of v.l.f. ionospheric propagation, 3094
Fujli, T., and A. Saburi, analysis of electron beam by mechanical scanner, 3524 l
with others, waveguide for low-loss transmission, 2829
Fujlisaki, H., with others, preparation of ZnS single crystals, 2625
Fujisakai, H., with others, associated with radar echoes, 2604
Fukushima, Y., with others, measurements of field

echoes, 2604
Fukushima, Y., with others, measurements of field patterns for comb-type slow-wave structure, 3524 n
Fuller, C. S., and J. M. Whelan, behaviour of Cu in GaAs, 882
with K. Wolfstirn, comparison of radio-copper and hole concentrations in Ge, 1250
Fulop, W., cut-off characteristics of magnetrons, 2057

and hole concentrations in co., and solutions of the solution of the

Fumeron-Rodot, H., and M. Rodot, properties of HgTe, 3779
Funakawa, K., with others, measurement of attenua-tion by rain, 4187
Funk, H., with J. Goldmann, film-recording of television transmissions in Germany, 2024
Furduev, V. V., interference and coherence of acoustic signals, 3910
Furth, H. P., with others, hydromagnetic capacitor, 1843
Fürth, R., and E. Morris, charge penetration into conductor, 3251
Furukawa, A., with others, m'crowave power

conductor, 3251 Furukawa, A., with others, m'crowave power standard, 3433

standard, 3433
 Furutsu, K., antenna circuit theory based on variational method, 1090; wave propagation over irregular terrain, 2723; e.m. radiation from vertical dipole, 3950
 Fuse, S., Y. Takahashi and A. Furukawa, microwave

power standard, 3433 Futtermenger, W., with H. J. Schmitt, multistage resonance absorbers for cm waves, 1846

Futtermenger, w., with H. J. Schmitt, multistage resonance absorbers for cm waves, 1846
Gabler, H., and M. Wächtler, component determination in d.f. for coherent waves, 816
Gabor, D., and others, c.r. tube for monochrome and colour television, 619
Gallit, T. A., with others, large inhomogeneities in F, layer, 2881
Galaiko, V. P., and L. E. Pargamanik, correlation function for particles carrying like charges, 1829
Galaiko, V. P., and L. B. Brick, radar interference, 465
Galaiko, V. P., and L. B. Brick, radar interference, 465
Galaiko, V. P., and L. B. Brick, radar interference, 465
Galaiko, V. P., and I. B. Brick, radar interference, 465
Galaiker, L. E., servo system for flying-spot store, 2364
Galler, R. M., v.1.f. emissions generated in earth's exosphere, 1575
— and R. A. Helliwell, origin of v.1.f. emissions, 4066
Gal'perin, F. M., interatomic distances in ferromagnetics, 891
Gampathy, C. V., and others, temperature-sensitive ceramic reactance element, 45
Gander, M. C., and P. L. Mothersole, frame multivitoria ond oldoe separator, 3409; multi-triode flywheel synchronizing circuit, 3500
Gandy, H. W., cathodoluminescence of SrO, (Be-Sr)O and MgO, 150
Ganzhorn, K., square hysteresis loop of ferrites, 2326

Gardner, F. F., effect of S.I.D's on pulse reflections, 2971

2971
Garfield, W. L., TACAN, 2259 i
Garfunkel, M. P., with others, evidence for energy gap in superconductors, 393
Garibyan, G. M., and G. A. Chalikyan, radiation from charged particle, 3634
Garner, K. C., linear multitapped potentiometers, 2159

2159
 Garner, W. R., discriminability criterion for loudness scale, 1062
 Garriott, O. K., whistler propagation in regions of low electron density, 1578
 with R. N. Bracewell, rotation of earth satellites, 795

795 Garrison, G. R., with others, sound absorption at 50 to 500 kc/s, 2082 Garstens, M. A., calculating resonance conditions in maser, 3622

Electronic & Radio Engineer

- Gärtner, R., cathode-follower circuits, 3235
 Gärtner, W. W., and others, current amplification of junction transistor, 631
 with others, surface-barrier photodiodes as photocapacitors, 3885
 Garton, J. H., with others, lightweight airborne navigation system, 2599
 Garver, R. V., E. G. Spencer and M. A. Harper, and the tangent techniques

- crowave semiconductor switching techniques, 3507
- Garwin, E. L., 20-mµs linear gate, 2880 Garwin, R. L., A. M. Patlach and H. A. Reich, transistorized crystal-controlled marginal oscil-
- Garwin, R. L., A. M. Pallach and H. A. Reich, transistorized crystal-controlled marginal oscillator, 1805
 Gaskins, F. J., with R. C. Kennedy, electronic composites in television, 612
 Gassner, J. A., 60-kW r.f. power amplifier, 290
 Gasson, D. B., with E. Billik, preparation of single-crystal Si by pulling technique, 168
 Gates, D. M., N.B.S. radio and ionospheric observations during 1.G.Y., 4046
 Gates, H. W., and A. G. Gatfield, scan converter for radar relay, 2605
 Gatlin, B., with H. W. Gates, scan converter for radar relay, 2605
 Gatlin, B., with M. C. Cretella, reaction of Ge with HNO, 2310
 Gauthé, B., electron characteristic energy losses in intermetallic compounds, 4092
 Gautiler, P., and C. Lalour, field of series of magnetic lenses, 3445 *and M. Laudet*, calculation of fields, 4023
 Gavin, M. R., W. Fulop and L. J. Herbst, electrode spacing in disc-seal triodes, 2788 u
 Gay, M. J., measurements of transistor parameters, 3430
 Gayford, M. L., column loudspeakers for publicadoff.

- 3430
 Gayford, M. L., column loudspeakers for public-address systems, 2824
 Gazaryan, Yu. L., waveguide sound propagation in stratified medium, 665; sound field generated by point source, 1040
 Gazzard, A. D., lunar tides in Eze at Brisbane, 132
 Gea Sacasa, R., ionospheric propagation, 1339; mobile maritime service, 3859
 Geballe, T. H., radiation effects in semiconductors, 4089 c

- Geballe, T. H., radiation effects in semiconductors, 4089 e
 with others, phonon-drag thermomagnetic effects in n-type Ge, 2662
 Gedalin, E. V., with G. A. Begiashvili, motion of charged particle in anisotropic medium, 3635
 van Geel, W. C., and C. A. Pistorius, current/time relations of electrolytic rectifiers, 3112
 Gelderikh, M. A., with others, producing polymers with semiconductor properties, 4121
 Gelst, D., and E. Preuss, etching and polishing of Gesurfaces, 1252
 Gekker, I. R., energy distribution of electrons in transit-type klystron, 2424
 van Gelder, G., and E. Scholten, radar echo box, 1590
 Geller, S., and E. Scholten, radar echo box, 1590
 Geller, S., and E. Scholten, radar semicon-ducting compounds: AgSbSe₂, AgSbTe₃, AgBiSe₄, 3gBiSe₄, 1269
 with others, multiple quantum transitions in paramagnetic resonance, 1856
 Gemmel, F., definition of lossy quadripoles by voltage node displacements, 1114; analysis of lossy symmetrical quadripoles, 1801
 Genco, J. I., with others, preparation and charactering of singlacrustal Inp. 4114

- lossy symmetrical quadripoles, 1801
 Genco, J. I., with others, preparation and characteristics of single-crystal InP, 4114
 Genna, W. N., with others, microwave model for study of s.w. aerials, 709
 Genoud, R. H., infrared search-system range performance, 4070
 Gentry, F. E., current surge failure in semiconductor rectifiers, 1367
 Genzel, L., and R. Weber, theory of interference modulation, 2191; spectroscopy in far infrared, 2192

- modu 2192
- George, R. G., magnetic viscosity displayed on hysteresis-loop traces, 2325 Gerard, V. B., propagation of world-wide sudden commencements, 3285

- commencements, 3285
 with others, magnetic effects of two high-altitude explosions, 3671
 Gerber, E. A., and L. F. Koerner, measurements of parameters of piezoelectric vibrators, 211
 Gerdes, E., generation of ultrasonics in liquids, 2812
 Care P. A. and C. Fabre duration of ultrasonics in liquids, 2812
- 2812
 Gere, E. A., with G. Feher, electron spin resonance experiments or donors in Si, 4099
 with others, electron-spin-resonance experiments on Ge, 3775
 Gereth, R., and H. A. Müser, test equipment for photosensitive semiconductors, 4078
 Gergely, G., cathodoluminescence efficiency of 25 (1998)
- photosensitive semiconductors, 4078
 Geréely, G., cathodoluminescence efficiency of ZnS-type phosphors, 472
 and I. Hangos, energy losses at binder films in c.r. tubes, 3173
 Gerhard, F. H., with W. Hochwald, amplifier with transistor chopper, 2519
 Gerlach, L., with others, grain growth in Ni ferrites, 544

- German, L., with others, grain growth in Ni ferrites, 544
 German, J. P., and F. E. Brooks, Jr, bandwidth of folded dipole, 2842
 Gerosa, G., with C. Barzilai, modes in guides filled with magnetized ferrite, 1770
 Gerritsen, H. J., W. Ruppel and A. Rose, photoproperties of ZnO, 826
 and others, structure and relaxation times of Cr⁴⁺ in TiO, 2333
 with others, approach to intrinsic ZnO, 877
 Gershtein, E.Z., T. S. Stautskaya and L. S. Skilbans, thermoelectric properties of PbTe, 1941
 Gerson, N. C., very-long-distance ionospheric propagation, 942
 Gerstenberg, D., magnetic investigations on Pd mixed crystals, 3790

- Getmantsev, G. G., V. L. Ginzburg and I. S. Shklovskil, radio-astronomy investigation by earth satellites, 3292
 Geusic, J. E., M. Peter and E. O. Schulz-DuBois, paramagnetic resonance spectrum of Cr³⁺ in emerald, 1628
- emerator, 1020 and chers, spin refrigeration and maser action at 1 500 Mc/s, 3654 Geyger, W. A., frequency control of magnetic nultivibrators, 3612
- Ghandbi, S. K., photoelectronic circuit applications, 1108
- 1108
 Gheorghiu, O. C., with T. V. Ionescu, coupling of oscillator and tube of ionized gas, 1156
 Ghose, A., and others, lattice vibrations in Ge by neutron scattering, 2304
 Ghose, R. N., field intensities from linear radiating source, 17
 Ghosh, B. B., and S. N. Mitra, measurement of atmospheric noise, 2743
 Glacoletto, L. J., junction capacitance using graded-impurity semiconductors, 852; avalanche-controlled semiconductor amplifier, 3620
 Gianola, U. F., and T. H. Crowley, 'Laddic', 1463

- controlled semiconductor amplifier, 3620
 Gianola, U. F., and T. H. Crowley, 'Laddic', 1463
 Glavotto, V., with C. Cassi, indirect method of determining high-atmosphere density, 3686
 Gibbons, D. F., and C. A. Renton, velocity of sound in Sn, 4122
 Gibbons, J. F., Hall effect in high electric fields, 1235
 with W. Shockley, current build-up in semi-conductor devices, 889; transient build-up in avalanche transistors, 2416
 with others, avalanche-transistor pulse circuits, 2878
 Gibbons, J. J. J. and A. H. Warmich, D. region of

- 2878
 Gibbons, J. J., and A. H. Waynick, D region of ionosphere, 1553
 Gibbons, W. F., and A. V. Whale, ceranic waveguide window for X-band values, 3159 a
 Gibbs, D. F., with H. L. Alsopp, electromechanical properties of BaTiO, 3333
 Gibson, A. F., and E. G. S. Paige, transport properties in dislocated Ge, 1619
 with others, minority carriers in dislocated Ge, 1618
- 1618
- With Objects, Initionity Carliers in dislocated Co., 1618
 Gleless, J. P. M., 4-kMc/s amplifier with disk-seal triode, 2798
 Glelessen, J., with K. H. v. Klützing, influence of pressure on magnetizability of Au₄Mn, 1273
 Glese, C. F., ion source for mass spectrometers, 2720
 Gilbert, E. G., with M. S. Uberoi, measurement of cross-spectral density of random functions, 2349
 Glibert, E. N., and E. F. Moore, variable-length binary encodings, 3467
 Gilberch, D. A., and R. C. Binder, portable instrument for locating noise sources, 2091
 Gilford, C. L. S., acoustic design of talks studios, 2822
 Gill, A., transistor switch design. 723; evaluating

- 2622
 Gill, A., transistor switch design, 723; evaluating logarithmic diodes, 2038
 Gill, P. J., with others, magnetic effects of two high-altitude explosions, 3671
 Gilland, J. R., transistor circuitry for radiation counting, 3231
 Gilles, J. M., and J. van Cakenberghe, photoconductivity and crystal size in evaporated CdS, 828
- 828 Gillette, P. R., and K. Oshima, pulser design for

- Gillette, P. R., and K. Oshima, pulser design for magnetron operation, 648
 K. Oshima and R. M. Rowe, measurement of pulse-front response of transformers, 357
 Gintsburg, M. A., surface waves on boundary of gyrotropic medium, 1076; exchange effects in ferromagnetic resonance, 2926
 Ginzburg, V. L., e.m. waves in isotropic and crystalline media, 1169; nonlinear interaction of waves propagating in plasma, 3847; use of earth satellites for verification of theory of relativity, 3684
 and V. Ya. Eldman, Cherenkov radiation from dipoles, 3647
 and V. M. Fain, quantum effects in interactions in resonators, 1844
 with others, radio-astronomy investigation by earth satellites, 3292

- m resonators, 1649
 with others, radio-astronomy investigation by earth satellites, 3292
 Ginzton, E. L., microwave Q measurements, 3819
 with others, high-power pulsed klystrons, 1410
 Glordmaine, J. A., and others, maser amplifier for radio astronomy, 2892
 Glorgenzult, B. C. dera puffs as cause of type III flare-puffs as cause of type III
- Giovanelli, R. G., f
- Glovanelli, R. G., hare-pulls as cause of type III radio bursts, 431
 and J. A. Roberts, observations of solar dis-turbances causing type II radio bursts, 432
 Gippius, A. A., with others, reflection coefficients of Ge and Si, 3765
 Giralt, G., measurement of peak value of h.v. pulse, 920
 Giralt, G., bareldown of paper canacitors
- Girant, G., measurement of peak value of mit-pulse, 920
 Girling, D. S., d.c. breakdown of paper capacitors, 1473
 Giron, V. S., and R. Pauthenel, variation of magneti-
- zation of uniaxial substances, 3806 Gittins, J. F., with others, c.w. power travelling-wave tube, 2787
- wave tube, 2107 Gladhorn, U., with H. Lindner, automatic recorder for c.r. oscillography, 1978 Gladstone, R., electronic timer with voltage control, 2865 Glarum, S. H., microwave dielectric measurements,
- 921
- 921
 Glass, D. G., with A. Kavadas, polarization of radar echoes from aurora, 4064
 Glass, M. S., leakage flux around t.w.t. focusing magnet, 315
 Glasser, M. L., with J. Callaway, Fourier coefficients of crystal potentials, 782
 Gleghorn, G. J., with others, circuits for space probes, 3286
 Glicksman, M., and M. C. Steele, plasma pinch effects in InSb 3388
 and K. Weiser, electron mobility in InP, 4115
 with others, electron mobilities in GaAs, 529

- Glicksman, R., with C. K. Morehouse, dry cells with C-nitroso compounds, 2402; Mg-BiO dry cells 3865
- with c-introso compounds, 2402, Mg-Dio dry cells, 3865
 Glinchuk, K. D., E. G. Miselyuk and N. N. Fortunatova, Ge with Fe impurity, recombination of current carriers in, 1933, effect of annealing on carrier lifetime in, 1934
 Glotov, V. P., reverberation tank for study of sound absorption, 1043
 Gnaedinger, R. J., Jr, precision evaporation and alloying, 307
 Gobeli, G. W., α-particle irradiation of Ge at 4.2°F, 1254
 with others, thermal and radiation annealing of Ge, 2305
 Gobiet, G., Weissfloch transformation theorem, 4153
 Goblock, T. J., Jr, with others, radar echoes from Venus, 2556
 Gobrecht, H., and A. Bartschat, semiconductor

- Cobrecht, H., and A. Bartschat, semiconductor properties of SnS, 886; elastic properties of hexagonal CdS, 2278; piezoelectric and elastic behaviour of CdS, 3746 behaviour of CdS, 3746
 and others, cathode-electroluminescence pheno-inena in ZnS phosphors, 834
 Godard, B. E., with others, electrical properties of epoxy resins, 911
 Godel, N. A., with W. P. Anderson, latching counters, 58

epoxy resins, 911
Godel, N. A., with W. P. Anderson, latching counters, 58
Godfrey, A. I., statistical methods in receiver manufacture, 1676
Godziński, Z., ground-wave propagation over inhomogeneous earth, 2375
Goering, H. L., with others, preparation and properties, of MgTe, 1258, of single-crystal InP, 4114
Goetz, W. E., and N. J. Woodland, data reduction of spot diagram information, 1105
Goff, K. W., with others, instrumentation for study of sound propagation, 2081
Gofman, I. I., and others, e.s. electron emission of seniconductors, 1922
Golay, M. J. E., binary decoding, 2747
Gold, D. C., and W. J. Perkins, electroencephalograph telemeter system, 3085
Gold, L., sputnik for geodetic information, 1156; 1/W behaviour in plasma, 1509; kinetic theory of space charge, 3160; hot-electron behaviour in G. 8, 3777
Gold, R. D., and J. W. Schwartz, drive factor and gamma of conventional kinescope guns, 1417
with others, pulse amplification using impact ionization in Ge, 2882
Gold, T., origin of radiation near earth, 2552
Goldben, R. M., and others, power-line aerial, 1672; v.li, c.w. transmitter for ionospheric investi-

3738 Golden, R. M., and others, power-line aerial, 1672; v.l.f. c.w. transmitter for ionospheric investi-gation, 3873 with others, antenna to eliminate groundwave interference in ionospheric sounding, 710

interference in ionospheric sounding, 710
 Goldey, J. M., two terminal p-n-p-n switches, 3883
 Golding, J. F., c.r.o. survey, 1977
 and L. G. White, linear amplifier for decimicrosecond pulses, 3993
 Goldmann, J., and H. Funk, film-recording of television transmissions in Germany, 2024
 Goldsmidt, H. J., C. C. Jenns and D. A. Wright, thermoelectric power of semiconducting diamond, 1924
 with others, magnetothermal resistance and magnetothermoelectric effects in Bi₂Te, 182
 Goldsmith, P., and J. V. Jelley, optical transition radiation, 4018
 Goldstein, B., and L. Pensak, high-voltage photovoltaic effect, 1907
 Goldstein, L., nonreciprocal e.m. wave propagation,

Goldstein, L., nonreciprocal e.m. wave propagation, 2541

2541 Goldstone, G. T., with R. L. Dowden, 'whistler mode' echoes, 2731 Goldthorp, J., synchronization separator, 3122 Göllnitz, H., with others, conduction of heat from anodes, 4252

Göllnitz, H., wih others, conduction of heat from anodes, 4252
 Golubjatnikov, O., with others, transistor phase-locked oscillators, 2162
 Goncharov, K. V., theory of piezoelectric trans-ducers, 672; frequency-sensitivity characteristics of transducers, 3906
 Gonzalez, R. E., with 1. A. Lesk, selective etching of junction transistors, 1402
 Gonze, R. E., with 1. P. Bruymseels, coaxial reflecto-meter for metre waves, 3431
 Goodale, E. D., with others, colour TV recording on black and white lenticular film, 1371
 Goodall, E. G. A., hemi-isotropic radiators, 2850
 and J. A. C. Jackson, transmission of e.m. waves through wire gratings, 3964
 Goodenough, J. G., cooling techniques for infrared detectors, 4010 h
 Goodman, A. M., photoconductivity as function of optical absorption, 1828
 Goodman, C. H. L., semiconducting properties in inorganic compounds, 847
 with J. R. Drabble, chemical bonding in Bi₂Te₃, 531
 Goodwin, F. E., and H. R. Senf, volumetric scanning

www.f. A. Drawee, chemical bonding in Bi₂1e₃, 531
 Goodwin, F. E., and H. R. Senf, volumetric scanning of radar with ferrite phase shifters, 1896
 Goodwin, G. L., with W. J. G. Beynon, horizontal drifts and temperature in E region, 804
 Goodyear, R. S., solving thermistor problems, 40
 Goorissen, J., and F. Karstensen, pulling of Ge crystals, 3029
 van der Goot, J., synchronization of television receivers, 3121
 Gorbach, V. I., with others, phase fluctuations of 10-cm waves over sea, 2738
 Gordon, D. I., R. S. Sery and R. E. Fischell, radiation effects in magnetic materials, 196

- Gordon, J. P., and K. D. Bowers, microwave spin echoes from donor electrons in Si, 860
 Gordon, W. E., Scattering by free electrons and space exploration by radar, 451
 Gordon-Smith, A. C., and J. A. Lane, gas-discharge noise sources at cm λ, 658
 Gordyakova, G. N., G. V. Kokosh and S. S. Sinani, thermoelectric properties of Bi₁Te₂-Bi₁Se₉, 3758
 Gore, D. C., with A. D. Williams, low-noise triode for use up to 1 kMc/s, 1419
 with others, new method for fine-wire grids, 2788 y
 Gorelik, A. G., and V. V. Kostarev, radioechoes from invisible objects in troposphere, 2240
 Gor'kov, L. P., with athers, superconductor in high-frequency field, 2195
 Görlich, P., A. Krohs and W. Lang, photoresistors, photodiodes and phototransistors, 3520
 and others, image converters for quantity production, 1404; resolving power of scintillation multipliers, 3081
 Gorshkov, M. M., with others, reflection coefficients of ge and Si, 3765
 Gorter, C. J., with others, h.f. susceptibilities of paramagnetic alums, 2332; absorption in paramagnetic alums, 2325 Mc/s, 2674
 Gosar, P., propagation through medium with cubic paralogical science of the and unit of the science of the scien

- Gosar, P., propagation through medium with cubic periodic structure, 93; p-n junctions, lateral photovoltaic effect in, 2614, photomagneto-mechanical forces on, 3357
 Gosnet, A., O. Parodi and C. Benoit à la Guillaume, light due to recombination of impurities in Ge, 3369
- 3369
 Goss, A. J., metallurgy of semiconductors, 3020

 and R. E. Addington, effects of seed rotation on Si crystals, 3021
 Gossard, A. C., and A. M. Portis, nuclear resonance in ferromagnet, 4126
 Gossett, R. E., with others, manufacture of wave-guide parts, 3553
 Gossick, B. R., disordered regions in semiconductors, 4089 i
 with L. Suttle D.

- Gossick, B. R., disordered regions in semiconductors, 4089 i
 with L. Stubbe, Dember potential measurements in Ge, 3359
 Goswami, S. N., effect of magnetic field on electrodeless discharge, 83
 Goto, E., parametron, 3588
 Goubau, G., and C. E. Sharp, model surface-wave transmission line, 10
 Gough, M. W., analysis of field-strength records 564; diurnal influences in tropospheric propagation, 1337
 Gouin, P., electronic seismic transducer, 3069
 Gould, R. N., with A. Cunliffe, high-Q echo boxes, 740
 Gould, R. W., characteristics of travelling-wave

- Gould, R. N., with A. Cumuiffe, high-Q echo boxes, 740
 Gould, R. W., characteristics of travelling-wave tubes with periodic circuits, 1732; travelling-wave couplers for longitudinal beam-type amplifiers, 2067
 and A. V. Trivelpiece, electromechanical modes in plasma waveguides, 2800 f
 Goulding, F. S., nucleonic instrumentation—transistorization, 3446
 Gourcaeux, M., thin absorbent films, 3268; optimum absorption thickness of thin film, 3651
 Goureaux, G., and A. Colombani, magnetic properties of very thin films of nickel, 3039
 P. Huet and A. Colombani, Hall effect in Ni films, 3395
 Gourgé, G., exo-electron emission and luminescence

- hims, 3395
 Gourgé, G., exc-electron emission and luminescence of inorganic crystals, 3002
 Gouskov, L., and N. Nifontoff, chemical action and oxidation of oriented Ge surfaces, 3370
 Goutte, R., with R. Bernard, image of surface obtained with negative ions, 567
 Gove, H. E., 10-MeV particle accelerator at Chalk River, 935
 Gorzini A. with chere, refractive index of humid

- Gove, H. E., 10-MeV particle accelerator at Chalk River, 935
 Gozzini, A., with others, refractive index of humid air, 1333 n
 Graf, C. R., concentric-feed Yagi, 344
 Grahnert, W., frequency spectrum of power-law double tones, 3908
 Gramatke, B., R. Netzband and E. Paulsen, r.f. protection ratios for v.h.f. fm., 1348
 Gränicher, H., K. Hübner and K. A. Müller, hyperfine splitting in paramagnetic resonance of Pr³⁺ in ceramic LaAlO₂, 758 f
 with A. Steinemann, dielectric properties of ice crystals, 1600
 Grant, D. S., R. O. Jones and T. Scott, power transistors, 2769
 Grant, J. A., scatter equipment for Canadian use,
- Grant, J. A., scatter equipment for Canadian use, 975

- Grant, J. A., scatter equipment for Canadian use, 975
 Grant, J. P., 'Plymouth effect', 577
 Granville, J. W., with others, minority carriers in dislocated Ge, 1618
 Grattidge, W., with others, thermionic integrated microinodules, 2863
 Grave, G., and W. Heimann, thermocouples and bolometers for radiation measurements, 1652
 Gravel, C. L., with A. D. Kurtz, diffusion of Ga in Si, 513
 Gray, D. A., with others, high-power 400-Mc/s klystron, 3524 j
 Gray, M. G., Si diodes as radar modulators, 3110
 Graydon, A., application of pulse-forming networks, 742
 Greefkes, J. A., with F. de Jager, 'Frena' speech

- WORS, 742
 WORS, 742
 WORS, 742
 Greefkes, J. A., with F. de Jager, 'Frena' speech transmission system, 2753
 Green, A., binary multiplication in digital com-puters, 2856
 Green, D. A., transistor equivalent circuit, 1718
 Green, D. M., detection of multiple-component signals, 3540
 Green, H. H. with others, manufacture of wave
- Green, H. H. H., with others, manufacture of wave-
- Green, H. H. H., *with others*, manufacture of wave-guide parts, 3553
 Green, J. H., Jr, and R. L. San Soucie, error-correcting encoder and decoder, 257

- Green, J. J., with E. Schlömann, decline of ferro-magnetic resonance absorption with increasing power level, 4139

- magnetic resonance absorption with increasing power level, 4139
 Green, M., space charge in semiconductors, 3012
 Green, P. E., Jr, with others, radar echoes from Venus, 2556
 Greenburg, J., effect of magnetic field on thermionic emission from Mo, 1945
 Greene, R. F., with D. R. Muss, reverse breakdown in In-Ge alloy junctions, 534
 Greenhow, J. S., and E. L. Neufeld, turbulence measurements in upper atmosphere, 4058
 Greenspan, M., and R. M. Wilmotte, distributed transducer, 673
 Greenwood, J. A., with others, electrical conduction in solids, 485
 Greent, G., self-inductance of magnetic-core

- in Solids, 345 Grenet, G., self-inductance of magnetic-core windings, 3058 Grenoble, H. E., with others, cube-oriented magnetic sheet, 896 Gretener, E., eidophor system, 620
- Grier, M. B., behaviour of single-stage thermo-electric microrefrigerator, 4010 i; infrared colour translation, 4010 o
 Grierson, J. K., with L. R. O. Storey, time-symmetric filters, 365

- Grier, M. B., behaviour of single-stage thermolelectric microrefrigerator, 4010 *i*; infrared colour translation, 4010 o
 Grierson, J. K., with L. R. O. Storey, time-symmetric filters, 365
 Griesinger, W., E. Popp and E. Schulz, distribution of lightning currents in earthing system of radio mast, 1451
 Griffiths, H. V., long-distance v.h.f. reception, 2003
 Griffiths, J. W. R., signal/noise ratio in p.c.m. systems, 2009
 Griffiths, J. W. R., signal/noise ratio in p.c.m. systems, 2009
 Griffiths, P. M., with D. J. Craik, domain configurations on ferrites, 1283
 Grigorov, N. L., with others, mechanism of terrestrial corpuscular radiation, 2216
 Grillot, E., with others, fluorescent emission lines and luminous absorption lines in CdS, 2618; influence of magnetic field on fluorescence of pure CdS, 2622
 Grimm, F., car radio design, 252
 Grimsdale, R. L., and others, automatic recognition of patterns, 2372
 Grinberg, A. A., calculation of transients in transistors, 2774
 Grinberg, G. A., new method for solution. of diffraction problem, 1851
 and Yu. V. Pimenov, diffraction of e.m. waves at flat screens, 1515
 Grinberg, K. L., and D. ter Haar, ferroelectric behaviour of KH, PO, 3331
 Grindzug, K. I., and M. Kh. Zelikman, measurement of ion concentration along satellite orbit, 3696
 Grinker, P., with Aubers, maser-type self-oscillator, 2521; weak-field maser, 2548
 Groce, J. C., with P. J. Kelso, encoder measures random-event time intervals, 2339
 Groendijk, H., microwave triodes, 2478 z; noise diode for u.h.f. 3533
 de Groot, D. G., with P. Winkel, impedance of dielectric layers, 2271
 Creschwitz, E., with E. Hofmeister, influence of point contact of Ge diodes, 2411
 Grosskopf, H., importance of video receiver in black-level transmission, 1377
 Grosskopf, H., importance of video receiver in black-level transmission, 1377
 Gro

- 3689, Dory, and Markey in Appet attain-induced changes in Seebeck coefficient of n-type Ge, 3374
 Grow, R. W., and others, 20-40-kMc/s backward-wave oscillator, 1742
 with C. M. Lin, broadband microwave coaxial connector, 3551
 with others, multiple ladder circuits for mm-wave tubes, 3159 v
 Grubbs, W. J., Hall-effect circulator, 2113; Hall-effect devices, 2692
 Grumet, A., transient e.m. fields in conductor, 2905
 Grünbaum, E., with M. Blackman, magnetic

- Grümer, A., transient e.m. helds in conductor, 2905
 Grünbaum, E., with M. Blackman, magnetic leakage field in Co, 202
 Grunewald, H., and W. Neumann, conductivity of lead oxide, 3784
 Gubanov, A. L, change of semiconductor properties with fusion, 1918
 Gubkin A. N., phonomenological shapes of electrotic
- Gubkin, A. N., phenomenological theory of electrets, 1602

- and G. I. Skanavi, stability of inorganic poly-crystalline electrets, 1603
 Gudmandsen, F., and B. F. Larsen, microwave propagation measurements in Denmark, 579
 Guerri, L., with A. Caracciolo, final computer model of Pisa C.S.C.E., 3966
 Guertler, R. J. F., characteristic impedance of balanced two-wire line, 3928
 Gugen, D., change of spontaneous magnetization with hydrostatic pressure, 892
 Guggenbühl, W., and W. Wunderlin, equivalent circuit of h.f. transistors, 2423
 Guillemin, E. A., with E. G. Fubini, minimum-insertion-loss filters, 1117
 Guminescence phenomena in ZNS phosphors, 834
 Gumowski, I., effect of reaction on gain of non-linear amplifiers, 2167
 Günther, K. G., vapour-deposited films of III-V compounds, 3349, 3761
 Guptill, E. W., with athers, coefficient of therma expansion of BaTiO, 2629
 Gurevich, A. V., temperature of electrons in plasma in variable fold 2532
- Gurevich, A. V., temperature of electrons in plasma in variable field, 2532
 Guro, G. M., stationary electronic processes in semiconductors, 2637

semiconductors, 2637 van Gurp, G. J., with others, exciton diffusion in CdS crystals, 2265 Gusev, V. D., and ethers, large inhomogeneities in F₁ layer, 2581 Gutin, S. S., with others, electron-hole transition in

Gutin, S. S., with others, electron-noie transition in point-contact rectifiers, 185
 Gutjahr, H., with K. W. Böer, spectral distribution of photoconductivity in CdS, 1904
 Gutman, A., asymptotic integration of wave equation, 2461

equation, 2461 Gutsche, E., measurement of elastic constants of CdS, 3728; displacement of absorption edge of CdS, 3729 Guttman, N., with others, mechanism of binaural fusion, 1055 Gyorgy, E. M., modified rotational model of flux reversal, 900 - with F. B. Humphrey, flux reversal in soft

 Analities, J., and G. J. Lubben, errors of magnetic deflection, 3125
 ter Haar, D., with J. Grindlay, ferroelectric behaviour of KH₂PO₄, 3331
 Haar, H., multitrack and stereo heads, 3550
 Håård, B., f.m. broad-band microwave systems, 2014 d
 Haas G. A. and F. M. M. Start, Start and Start an Haantjes, J., and G. J. Lubben, errors of magnetic

Haas, G. A., and F. H. Harris, X-Y pulse measuring

Harris, C. A., and F. H. Harris, X.-Y pulse measuring system, 4160
 and J. T. Jensen, Jr, preconversion of oxide cathodes, 3891
 Haas, H. H., with S. D. Hathaway, TJ radio system, 3106

cathodes, 3891
Haas, H. H., with S. D. Hathaway, TJ radio system, 3106
Haase, A. P., with others, thermionic integrated micromodules, 2863
Haber, J. F., with others, sendust flake, 894
Haberecht, R. R., with others, preparation and properties of AlSb, 2311
Hadders, H., P. R. Locher and C. J. Gorter, absorption in paramagnetic salts at 1 325 Mc/s, 2674
Hadley, C. P., W. G. Rudy and A. J. Sloackert, moulded Ni cathode, 2069
Haering, R. R., Zeenan splitting of donor states in Ge, 525; electrons and holes in perturbed lattices, 2528
Hagan, M. P., with E. J. Chernosky, Zurich sunspot number and variations, 1529
Hagelparger, D. W., recurrent codes, 3468
with others, improvement in floating-zone technique, 2337
Hagger, C. K., network design of microcircuits, 3972
Hagger, E., J. Mulfew and E. Warren, spiral occurrence of E., 3304
Hahn, D., and F. W. Seemann, significance of boundary layers and polarization fields for electroluminescence, 833
Hahn, E., computation of e.s. immersion objectives, 3073
Hahn, H., and M. Sauzade, transistor stabilized supply at 5-9 V 800 mA, 601

3073 Hahn, H., and M. Sauzade, transistor stabilized supply at 5-9 V 800 mA, 601 Haines, J. H., and G. R. Tingley, vitascan flying-spot colour scanner, 279 Hakura, Y., power spectrum of solar radio outburst, 1178

1178
and Y. Takenoshita, s.w. transmission disturbance of 11th Feb. 1958, 573
with others, world wide distribution of fmin and Dellinger effect, 2588
Halina, J. W., with M. J. Cotterill, bridge negative-feedback amplifiers in carrier telephony, 974
Hall, C. J., dual-standard television receivers, 4217
Hall, G. G., electronic structure of diamond, Si and Ge, 1238
Hall, J. E., with others, radar observations of 1957 β, 3290

3290

Hall, J. E., With Others, lader Observations of 1607, p., 3290
Hall, R. C., crystal anisotropy and magnetostriction of ferromagnetic alloys, 3393
Hall, R. N., with others, observation of phonons during tunnelling in junction diodes, 4226
Hall, T. C., with M. F. Millea, surface mobility in Ge and Si, 505
Halperin, A., and H. Arbell, excitation spectra and luminescence of ZnS, 2999
Halpern, J., and R. H. Rediker, mµs switching diodes, 3144
Halsey, R. J., and A. R. A. Rendall, prospects for transatlantic television by cable, 4211
Halstead, M. B., with others, activation of ZnS and (Zn,Cd)S phosphors, 3736

Electronic & Radio Engineer

ferromagnetics, 3405

Humphrey, flux reversal in soft

- Halsted, R. E., electrophotoluminescent amplification, 831
 E. F. Apple and J. S. Prener, two-stage optical excitation in phosphors, 2996
 Hamakawa, Y., with J. Yamaguchi, Ge p-n junction, high-electric-field effects in, 3023; barrier temperature at turnover in, 3024
 Hamberger, S. M., wide-band multi-way electronic switch, 2800 e

- switch, 2800 e Hambley, N., low-frequency phasemeter, 1319 Hame, T. G., and E. M. Kennaugh, transmissions from 1958 82, 2570 Hamilton, D. J., J. F. Gibbons and W. Shockley, avalanche-transistor pulse circuits, 2878 Hammerslag, J., circuit design using Si capacitors, 3974
- 3974
 Hammond, V. J., and R. Carter, visualization of ultrasonic beam in fused quartz, 674
 Hamrick, J. J., measuring and evaluating noise, 6
 Handler, P., with G. Heiland, influence of atomic hydrogen on conductivity of Ge, 2301
 Handy, R., with R. Frerichs, electroluminescence in Cu₂O, 3005
 Hanel, B., and others tracking meether with the second second
- Cu₂O, 3005 Hanel, R., and others, tracking weather with satellites, 2715 with others, current amplification of junction transistor, 631
- Hangos, I., with G. Gergely, energy losses at binder films in c.r. tubes, 3173
 Hanle, W., and H. Schneider, scintillation counters, 2000 Hanle, V 3080

- 3050
 Hannam, H. J., and A. van der Ziel, noise in oxide cathodes, 1027
 Hannon, J. R., attenuation of coaxial cables above 3 kMc/s, 337
 Hänsch, H. J., with others, rendering visible conductors, 3757
 Hangel, P. C. VOR comparison computer complex c
- Hansel, P. G., VOR-compatible Doppler onini-range, 1897
- range, 1897
 Hansen, R. C., with R. W. Hougardy, scanning surface-wave antennas, 3201
 Hansen, R. T., recurrent geomagnetic storms and solar prominences, 1865
 with C. S. Warwick, geomagnetic activity following large solar flares, 3284
 Hanssen, K. J., asymmetric unipotential electron lenses, 937
 Happ, W. W., with T. R. Nisbet, Jacobians, 2775
 with others, estimate of transistor life in satellites, 2780

- ada, R. H., and A. J. Strauss, preparation of InAs, 1624 Har

- 2780
 Harada, R. H., and A. J. Strauss, preparation of InAs, 1624
 Harang, L., and J. Tröim, angle of arrival of auroral echoes, 2254
 Harbeke, G., and G. Lautz, crystal structure of Ga, Te, doped with Cu, 3031
 Hardcastle, C., 3-valve preamplifier, 63
 Harden, B. N., with J. A. Saxton, performance of directive aerials at u.b.t., 2845
 Hardin, C. D., and J. Salerno, miniature X-band radar, 1584
 Hare, E. W., evaluation of Dectra, 463
 Hare, A. and J. F. Cashen, unified representation of transistor transient response, 2050
 Hargreaves, J. K., radio observations of lunar surface, 1863
 Harkins, D., f.m. multiplexing for studio-transmitter links, 3107
 Harkless, E. T., network for combining radio systems, 3954
 Harnan, T. C., M. J. Logan and H. L. Goering, preparation and properties of MgTe, 1228
 and others, preparation and characteristics of single-crystal InP, 4114
 Harnik, F., A. Many and N. B. Grover, phase-shift method of carrier lifetime measurements, 515
 Harnik, Taker, A. Many and N. B. Grover, base-shift method of 'similar fades', 801
 with others, inoospheric observations during solar eclipse of 30th June 1954, 131
 Harper, M. C., nonvacuum devices control klystrons, 1737
 Harper, M. A., with others, microwave semiconductor systemic approximation and properties of strains of strains (3597)

- Harp, M 1737
- 1737
 Harper, M. A., with others, microwave semi-conductor switching techniques, 3597
 Harrick, N. J., properties of semiconductor surface, 2281; measuring particle drift mobilities in semicorductors, 2313
 Harrington, R. D., and A. L. Rasmussen, perme-ability spectra of V-Fe garnet, 1291
 Harrington, P. E. scattering by large conducting

- Harrington, R. F., scattering by large conducting bodies, 4029
 and A. T. Villeneuve, reciprocity relations of gyrotropic media, 3044
 Harris, B., and K. C. Morgan, binary symmetric decision feedback systems, 591
- decision feedback systems, 591
 and others, binary communication feedback systems, 2387
 Harris, D. J., microwave amplification using urstable electron beam, 3159 j
 Harris, F. H., and J. Ainsworth, single-line-scan television, 2033
 with G. A. Haas, X-Y pulse measuring system, 4160
- 4160
- Harris, I., R. Jastrow and W. F. Cakill, satellite orbits from radio tracking data, 2568 Harris, L. A., toroidal electron guns for hollow beams, 3527

- beams, 3527
 Harrison, D. E., and F. A. Hummel, system ZnO.CdO.B₂O₃, 3735
 Harrison, D. P., and C. D. Watkins, radio echoes from aurora australis and aurora borealis, 140
 Harrison, S. E., with others, structure and relaxation times of Cr³⁺ in TiO₂, 2333
 Harrowell, R. V., characteristic impedances of elliptic waveguide, 702

Electronic & Radio Engineer

- Hartke, D., with others, precision generator for radar range calibration, 2352
 Hartmann, G., braking action in magnetic-tape recorders, 694
 Hartz, T. R., auroral radiation at 500 Mc/s, 139
 Harvey, A. F., r.f. aspects of electro-nuclear accelerators, 1328; optical techniques at microwave frequencies, 2099; parallel-plate microwave transmission systems, 2108
 Hashimoto, T., life of dispenser-type cathodes, 3159 d
- 3159 4
- Hashimoto, U., with K. Komatsubara, annealing of radiation-induced 1/f noise in Ge p-n junction, 298
- Mashimoto, U., with K. Komatswoara, annealing of radiation-induced 1/f noise in Ge p-n junction, 298
 Haslam, C. G. T., with others, high-resolution survey, of Andromeda nebula, 2937, of Coma Cluster, 2938
 Hass, G., with J. T. Cox, antireflection coatings for Ge and Si in infrared, 864
 Haszko, S. E., with others, line width in Y-Fe garnet, 2330
 Hatch, J. F., and D. W. G. Byatt, direction finder with automatic read-out, 2600
 Hathaway, S. D., and H. W. Evans, radio attenuation at 11 kMc/s, 1673, 2381
 and H. H. Haas, T.J radio system, 3106
 Hatsopoulos, G. N., with others, diode thermoelectron engine, (D)2435
 Hatta, Y., telemetering using principle of gasfield stepping tube, 2374
 Hattiangadi, M. S., with others, nature and origin of atmospherics, 3699 a
 Hatton, W. L., with others, engineering of 1.f. communication systems, 2750
 Hauder, A., radio choes observed on sea swell at Casablanca, 2724
 Haude, G., sorretjon of aperture error in e.s. lenses, 4171
 Hauge, G., with others, system design of flying-spot store, 2362

- with others, system design of flying-spot Haugk, G., with store, 2362
- Haun, R. D., Jr, and T. A. Osial, gain measurements on pulsed ferromagnetic microwave amplifier, 2184

- store, 2362
 Haun, R. D., Jr., and T. A. Osial, gain measurements on pulsed ferromagnetic microwave amplifier, 2184
 Hauptschein, A., with others, binary communication feedback systems, 2387
 Hauri, E. R., limits of transistor characteristics, 629; transistor amplifier, with negative feed-back, 1142, for acoustic measurements, 1499
 Haus, H. A., power-flow relations in lossless non-linear media, 3045
 Hauser, W., theory of anisotropic obstacles in waveguides, 706; guided e.m. waves in aniso-tropic materials, 707
 Hawkens, H. W., method of generating rotating radiation diagram, 2120
 Hawkins, G. S., search for magnetic effects from meteors, 106
 Hawkins, P. O., active microwave duplexing systems, 2800 c
 H. J. Curnow and R. Redstone, coaxial-line diode, 3524 m
 Hay, D. R., tropopause height and transmission loss at 400 Mc/s, 3097
 and G. E. Poaps, prolonged fade-out on short microwave path, 3098
 Hayasaka, T., and M. Suzuki, errors of electro-acoustic standards, 3186
 Hayes, M., with others, paramagnetic resonance of inpurities in CaF, 3411
 Haynes, H. E., and D. T. Hoger, stop-go scanning saves spectrum space, 277
 Haywood, B. C., with others, conductivity induced by radiation in CdS and polyethylene, 2672
 Head, H. T., measurement of television field strength, 288
 Head, J. W., with C. G. Mayo, wide-range RC oscillator, 54
 Heasell, E. L., N. R. Howard and E. W. Timmins, apparatus for measuring electrical resistivity of Si, 214
 Heathrote, V. A., and others, travelling-wave multiple-beam klystron, 3524 z
 Heathcote, V. A., and others, travelling-wave multiple-beam klystron, 3524 z
 Heathrote, J. R., and K. R. Johne, electron-ray tracing in electric and magnetic fields, 3534 i
 Hechtel, J. R., and K. R. Johne, electron-ray tracing in electric and magnetic fields, 3524 z

- 4137
 and H. Reiner, storage properties of square-loop ferrites, 3397
 with J. Rupprecht, dielectric properties of oriented Ba ferrite, 3807
 k. L., multiple-track magnetic sound recording, 3190
- Heck. video output stage with wound
- Hecker, K., video output stage with v resistor, 2347 Heckl, M., sound insulation of cylinders, 3547
- and K. Seifert, influence of self resonances of measurement chambers on sound insulation measurements, 2090
 Hedgcock, F. T., magnetic susceptibility of semi-conductors, 3017
 Hedges, C. P., digital recorder holds data after shock, 2365

- shock, 2365
 Hedlund, D. A., and L. C. Edwards, polarization fading over oblique-incidence path, 1668
 Heeger, A. J., T. R. Nisbet and W. W. Happ, estimate of transistor life in satellites, 2780
 Heffner, H., solid-state microwave amplifiers, 4004
 and G. Wade, characteristics of variable-parameter amplifiers, 77

World Radio History

- with J. E. Sterrett, periodic magnetic focusing structures, 1021
 with G. Wade, gain, bandwith and noise in cavity-type parametric amplifier, 2066; microwave parametric amplifiers and convertors, 2896
 with others, parametric amplifiers as superregenerative detectors, 3245
 Heidenreich, R. D., E. A. Nesbitt and K. D. Burbank, magnetic annealing in perminvar, 3797
 with E. A. Nesbitt, magnetic annealing in perminvar, 3798
 Heider, E., with E. O. Willoughby, omnidirectional paraboloid aerial, 1447
 Heidenter, R., and K. Vogt, diversity reception by aerial selection method, 2741
 Heiland, G., field effect and photoconductivity in ZnO, 880
 and P. Handler, influence of atomic hydrogen on conductivity of Ge, 2301
 Heimann, W., with G. Grave, thermocouples and bolometers for radiation measurements, 1652
 Heimke, G., anomaly in characteristics of Ba ferrite 2685

- conductivity of Ge, 2301
 Heimann, W., with G. Grave, thermocouples and bolometers for radiation measurements, 1652
 Heimke, G., anomaly in characteristics of Ba ferrite, 2685
 Hein, H., input-admittance curves of 2-stage band filters, 734
 Heine, K., measurement of short afterglows of electronically excited luminophores, 2350
 Heine, K., measurement of short afterglows of metals and alloys, 910
 Heineken, F. W., and A. Battaglia, absorption and refraction of NH₃ at 6 mm Å, 2213
 Heine, W., H. Göllmitz and W. Baer, conduction of heat from anodes, 4252
 Heisler, L. H., giant travelling ionospheric disturbances at night, 2580
 with G. H. Murro, recording signals from earth satellites, 2573
 Hell, H. J., error probability of binary coded messages, 2389; reliability of binary transmissions, 2746
 Heller, G. S., with L. C. Kravitz, resonance isolator at 70 kMc/s, 1439
 Helliwell, R. A., properties of lightning inpulses which produce whistlers, 142
 and M. G. Morgan, atmospheric whistlers, 1576
 with R. M. Gallet, origin of v.l.f. emissions, 4066
 Hellwerth, G. A., constant-anplitude randomfunction generator, 373
 Helmer, J. C., small-signal analysis of molecularbeam masers, 1501
 and M. W. Muller, noise figure of maser amplifier, 2343
 Helmer, J. C., small-signal analysis of molecularbeam masers, 1501
 and M. W. Muller, noise figure of maser amplifier, 2343

Helmers, K., simple model for impurity-band conduction, 3010 Helsdon, P. B., transistor line deflection circuits, 3126

Hendee, C. F., and W. B. Brown, stroboscopic operation of photomultiplier tubes, 1722
Henderson, K. W., elliptic-function filter design, 367
Henderson, K. W., elliptic-function filter design, 367
Henderson, S. T., P. W. Rawby and M. B. Halstead, activation of ZnS and (Zn,Cd)S phosphors, 3736
Hendricks, C. D., Jr, G. W. Swenson, Jr, and R. A. Schorn, radio reflections from satellite-produced ion columns, 121
Hendry, A., noise temperature ratio in Ge diodes, 627
— with L. K. Anderson, Ge mixer crystals at low temperatures, 3876
Hendsch, H. K., semiconducting SiC, 3771

Henisch, H. K., semiconducting SiC, 3771 Henkel, H. J., formation of barrier layers in AlSb, 3030

3030
Henkels, H. W., and G. Strull, very-high-power transistors, 1001
Hennequin, J., with H. Benoit, measurement of geomagnetic field by maser, 3823
Henniger, H., temperature coefficient of initial permeability of dust core materials, 1282
Henry, J., with H. Arzeliżs, laws of magnetism and static electricity, 1514
Henry M. temperature reached by the junction

Henry, R. M., temperature reached by p-n junction, 295; point-contact Ge and Si diodes, 296; Si transistors, 300
Henry, W. E., magnetization and structure of Ba terrate III, 899
Hensel, J. C., and M. Peter, Stark effect for cyclotron resonance, 3346
Hepburn, F., interpretation of smooth-type atmospheric waveforms, 3312
Hepper, H., delay equipment for unattended operation, 3924
Heppert, J. P., with others, results obtained with rocket-borne ion spectrometers, 3703
Herbert, J. M., ferroelectric crystals and ceramics, 153

153

Herbert, J. M., ierroelectric crystals and ceramics, 153
Herbst, L. J., with others, electrode spacing in disc-seal triodes, 2788 u
Herczog, A., R. R. Haberecht and A. E. Middleton, preparation and properties of AlSb, 2311
Hergenhahm, G., orbit of satellite 1085 & 23 3685
Hérinckx, C., and A. Monfils, determination of thermal parameters of semiconducting thermoelements, 3348
Heritage, D. P., with others, v.l.f. propagation measurements for Radux-Omega system, 2736
Herman, F., with others, single phonon emission in breakdown of semiconductors, 3013
Hermann, J., with K. van Duwren, halogen-quenched end-window Geiger counter, 3079
with others, G-M counters, 3446

- Herndon, R. C., with T. Sekiguchi, thermal conductivity of electron gas, 766
 Hernqvist, K. G., M. Kanefsky and F. H. Norman, thermionic energy converter, 325
 Herrinck, P., disturbances of geomagnetic field, 2944; prediction of sunspot numbers, 3282
 Herring, C., T. H. Geballe and J. E. Kunsler, phonon-drag thermomagnetic effects in n-type Ge, 2662
 Herrinst, D. R., polyhedral satellite for measurement of orbit data, 794
 with others, flying-spot store, system design of, 2362, optics and photography in, 2363
 Herrmann, J., with others, improvements in NH₃ maser, 758 g
 Hersee, G., and J. R. T. Royle, B.B.C. transparencies for testing camera channels, 984
 Hersping, A., and K. Blank, after-effect in ceramic dielectrics, 3328
 den Hertog, J. M., with G. Klein, sine-wave generator. 2876

- dielectrics, 3328 den Hertog, J. M., with G. Klein, sine-wave generator, 2876 Herz, A. J., and others, radiation observations with satellite 1958 8, 4042 Herzenberg, A., geomagnetic dynamos, 108 Herzog, A. W., computer for simulation of aircraft, 2477

- Hess, H. A., recording Sputnik II on 40 002 kc/s, 3291

- Mess, M. A., Fecording Sputhik II on 40 002 kc/s, 3291
 Hessler, J., Jr, with others, vacuum-diode microwave detection, 2794
 Hessler, V. P., and E. M. Wescott, correlation between earth-current and geomagnetic disturbance, 4044
 Hewish, A., scattering of radio waves in solar corona, 2939
 Hey, J. S., and T. B. A. Scnior, e.m. scattering by thin plates, 772
 J. T. Pinson and P. G. Smith, radio observations of hypersonic shock waves, 1658
 Heydenrych, J. C. R., design of transductors for maximum power transfer, 381
 Heyligers, H., with others, protection device for stabilized line timebase circuit, 262; stabilization, of line output circuits, 989, 3871, of line and frame output circuits, 3123
 Heymann, O., application of Laplace transforma-

- frame output circuits, 3123
 Heymann, O., application of Laplace transformation, 2695
 Hiatt, R. E., with others, radar cross-section of finite cones, 4073
 Hibbard, W. R., with others, cube-oriented magnetic sheet, 896
 Hibberd, F. H., with J. A. Thomas, satellite Doppler measurements and ionosphere, 1874
 Hibberd, R. G., transistors and semiconductor devices, 3147
 Hiedemann, E. A., with M. A. Breazeale, investigation of progressive ultrasonic waves by light refraction, 1050
 with R. B. Miller, intensity distribution of light diffracted by ultrasonic waves, 1051
- with K. B. Mailer, intensity distribution of light diffracted by ultrasonic waves, **1051** with K. L. Zankel, amplitude distortion of ultrasonic waves, **2814** with others, determination of ultrasonic wave-form by light refraction, **3538**

- form by light refraction, 3538
 Hierholzer, F. J., Jr, linear power amplifiers using dynistors or trinistors, 2174
 Higdon, B. G., and M. F. Bond, thyratron-stabilized d.c. supplies, 4208
 Higley, J. B., with others, precision guarded resistance measuring facility, 561
 Hilbrand, J., and W. R. Beam, semiconductor diodes in parametric subharmonic oscillators, 3981 3981
- 3961 in particular, 'thyristor' switching transistor, 1005
 With C. W. Mueller, 'thyristor' switching transistor, 1005
 Hill, E. R., emission at 3.5 in from local supergalaxy, 2223
 O. B. Slee and B. Y. Mills, pencil-beam survey of galactic plane at 3.5 in, 2220
 with others, radio sources between declinations +10° and -20°, 423
 Hill, J. E., and K. M. van Vliet, carrier-density fluctuations in Ge, 1617
 Hill, J. presision thermoeloctric waturates 1220

- Hill, J. E., and K. M. van Vliet, carrier-density fluctuations in Ge, 1617
 Hill, J. J., precision thermoelectric wattneter, 1320
 Hill, L. O., with L. K. Wanlass, digital-analogue conversion with cryotrons, 1103
 Hill, N. E., application of Onsager's theory to dielectric dispersion, 392.
 Hilliard, J. K., and IV. T. Fiala, generating high-intensity sound with loudspeakers, 692
 Hillsum, C., multiplication by semiconductors, 350; effects of Cu in InAs, 2666; properties of p-type InSb, 4118
 and A. C. Rose-Innes, new method of measuring susceptibility, 1313
 Hines, C. O., motions in ionosphere, 1556
 and L. R. O. Storey, time constants in geomagnetic storm effect, 1535
 Hirabayashi, H., deterioration of microphone carbon powder, 3189
 and others, life tests of microphone carbon, 1758
 Hirai, M., Y. Fujii and H. Saito, diffraction at w.h.f. and u.h.f. by ridges, 243
 with others, long-distance u.s.w. propagation, 244
 Hirao, K., durnal variation of fading at v.h.f., 256

- Hirao, K., diurnal variation of fading at v.h.f., 256
 K. Akita and I. Shiro, temperature fluctuations accompanying solar eclipse, 2559
 Hird, E. V., use of radio carrier in telephone system, 1362
- 1362
 Hirshfield, J. L., and S. C. Brown, measuring probability of electron collision in gas, 768
 Hitchcock, R. J., future difficulties facing long-distance h.f. communications, 261
 Hoare, F. E., with biters, pulse techniques, 2449
 Hochman, R. H., with G. C. Kuczynski, light-induced plasticity in Ge, 1938

- Hochwald, W., and F. H. Gerhard, amplifier with transistor chopper, 2519
 Hodara, H., h.f. integrator design, 1479
 Hoell, P. C., d.c. amplifier with whole-loop feedback, 1137
 Hofer, R., influence of unsymmetric r.f. stages on signal bands with a.m., 3992
 Hoffman, D., and E. Schulzman, analysis of noise-signal amplitudes, 3826
 Hoffman, L. A., with others, circuits for space probes, 3286

- 3286
- 3286
 Hoffman, R., with others, auroral phenomena during storm, 3309
 Hoffman, R. W., with T. G. Knorr, geometric magnetic anisotropy in Fe films, 2683
 Hoffman, T. R., feedback design for transistor amplifiers, 3619
 Hoffman, W. C., optimum apertures of aerials, 1333 s
 Hoffman A. mode of operation of a two photo

- Hoffmann, A., mode of operation of n-p-n photo-transistors, 4233
 Hoffmann, F., with U. Schley, noise in radiation thermocouples, 1653
- Hoffmann, R., interconnection of television cable links, 992
 Hoffmann, W., broadcasting equipment at Karlsruhe studio, 2016
 Hofmeister, E., and E. Groschwitz, influence of point contact of Ge diodes, 2411

- and the second meter, 416
- meter, 416
 Hojo, H., with others, world-wide distribution of fm. and Dellinger effect, 2588
 Holcomb, D. F., magnetic resonance line shapes at onset of saturation, 1948
 Holden, J. T., with others, Ti getter pump, 1204
 Holford, K., and L. M. Newall, video amplifiers using transistors, 385
 Holland, J. D., with L. J. Heaton-Armstrong, h.f. receiver RX.5C, 3462
 Holland, L., getter-ion pumps 1899

- Holland, L., getter-ion pumps, 1899 L. Laurenson and J. T. Holden, Ti getter pump, 1204

- Holander, L. E., Jr., piezoresistivity in TiO₂, 887
 Hollander, L. E., Jr., piezoresistivity in TiO₂, 887
 Holleufer, W. O., construction of miriature magretic microphones, 1431
 Hollis, J. L., frequency shifts improve pulse communications, 3470
 Holloway, J. H., with others, comparison of Cs frequency standards, 212
 Holmes, J. C., with others, results obtained with rocket-borne ion spectrometers, 3703
 Holonyak, N., Jr, and others, observation of phonons during tunnelling in junction diodes, 4226
 with R. W. Aldrich, Si-controlled rectifiers from oxide-masked diffused structures, 2418
 Holstein, T., ultrasonic absorption in metals, 2444

- with K. W. Alarten, Si-controlled rectifiers from oxide-inasked diffused structures, 2418
 Holstein, T., ultrasonic absorption in metals, 2444
 Holt, E. H., with S. Takeda, microwave propagation nethod of studying decaying gas plasmas, 4021
 Holter, M. R., and W. L. Wolfe, optical-mechanical scanning techniques, 4010 k
 Holtzman, J., reducing errors caused by powersupply variations, 3615
 Hong, K., carbonization of thoria cathodes, 3530
 Honig, H., and E. Stupp, electron spin-lattice relaxation in P-doped Si, 512
 Honnell, P.M., with R. E. Horn, matrix programming of analogue computers, 347
 Hoogenstraaten, W., electron traps in ZnS phosphors, 1596
 with others, exciton diffusion in CdS crystals, 2265
 Hoogended, D., microphonic effects in electron tubes, 3896
 A. Boekhorst and H. Heyligers, stabilization of
- 3896 A. Boekhorst and H. Heyligers, stabilization of line output circuits, 3871 with others, stabilization of line output circuits, 3124

- with others, stabilization of line output circuits, 3124
 d'Hoop, H., with A. Dumont, measurement of pulsed powers at m A. 3829
 Hoover, C. W., Jr, G. Haugk and D. R. Herriott, system design of flying-spot store, 2362
 Hoover, M. V., advances in very-high-power gridcontrolled tubes, 2788 v
 Hope, E. G., with others, circuits in N.P.L. Cs standard, 2340
 Hope, J., with others, horizontal drift measurements near equator, 1557
 Hopengarten, A., with others, colour purity adjustment for 'apple' c.r. tube, 1386
 Hopf, H., delay equalization for residual-sideband television, 3490
 Hopper, E., modulation-demodulation system for data transmission, 1664
 Hopper, W. C., with others, waveguides for use in cryostats, 1767
 Horn, H., Saite, thermodynamics of harmonic oscillator, 81
 Hormuth, W., statistics of fading-dependent noise, 3858
 Horn, F. H., melted-layer crystal growth, 1251

- Hormuth, W., Statistics of Jaune Repeated and the statistics of Jaune Repeated and Statistics of Jaune Repaired and Statistics of Jaune Repeated and Statist

Horner, F., atmospheric radio noise and lightning, 814
Hornig, A. W., R. C. Rempel and H. E. Weaver, electron paramagnetic resonance in BaTiO₃, 476
Horowitz, H., moving-magnetic stereo, 2818
Horowitz, R., and H. E. LaGow, auroral-zone atmospheric-structure measurements, 1560
van der Horst, H. L., and P. H. C. van Vlodrop, induction-heating generator using hydrogen thyratrons, 3439
Horton, B. M., noise-modulated distance measuring system, 2611
Horton, C. W., and A. E. Sobey, Jr, near fields of acoustic sources, 3537
Hoshino, S., and others, (NH₄)₂ SO₄ and (NH₄)₄BEF₄ transitions, 836
with others, ferroelectricity in Li(N₂H₄) SO₄, 840; (NH₄)HSO₄ ferroelectric with low coercive field, 841
Hoskins, R. F., signal flow graphs, 3602

- (NH₄)HSO₄ ferroelectric with low coercive field, 841
 Hoskins, R. F., signal flow graphs, 3602
 Hoskins, R. H., two-level maser materials, 3037; spin-level inversion and spin-temperature mix-ing in ruby, 4123
 Hougardy, R. W., and R. C. Hansen, scanning surface-wave antennas, 3201
 Houseley, P. J., rotating-loop reflectometer for waveguide, 2117
 Houston, J. M., efficiency of thermionic energy converter, 3437
 Howard, D. D., with J. H. Dunn, effects of a.g.c. on accuracy of monopulse radar, 1894
 with others, scintillation noise in radar tracking systems, 2609
 Howard, J. N., transmission of atmosphere in infrared, 4010 b
 Howard, R., T. Cragg and H. W. Babcock, magnetic field associated with solar fare, 4043
 Howard, B., hal-cycle resonant delay circuit, 2501
 Howlett, D. J., and L. Buduls, noise-immune syn-obsensing and the synchronic synchronic synchronic synchronic metal syn-ophysic synchronic 3437

Howlett, D. J., and L. Buduls, noise-immune syn-chronizing circuits, 3120

Hozumi, H., with others, measurements of field patterns for comb-type slow-wave structure,

Hozumi, H., with others, measurements of field patterns for comb-type slow-wave structure, 3524 n
Hrbek, G., with R. Adler, low-noise electron-beam parametric amplifier, 321
Hrlanca, J., with B. Rothenstein, mobility of Bloch walls, 3794; influence of temperature on distribution of ferromagnetic domains, 3795
Hrostowski, H. J., and R. H. Kaiser, infrared spectra of heat-treatment centres in Si, 167; absorption spectrum of As-doped Si, 1244
Hsu, C. S., simple subharmonics, 4146
Hsu, W. K., reversible dekatron counter, 1812
Hu, Yueh-Ying. See Yueh-Ying Hu.
Hubbard, R. M., shunt-coupled magnetic-amplifier circuits, 3997
Hubbard, W. M., E. Adams and J. F. Haben, sendust flake, 894
Hubbart, K., with others, hyperfine splitting in paramagnetic resonance of Pr³⁺ in ceramic LaAlO₃, 758 f
Hücking, E. E., with R. Falker, magnetic measure-

⁷⁵⁵ J.
 ⁷⁵⁶ J.
 ⁷⁵⁶ Hücking, E. E., with R. Falker, magnetic measurements on ferrite U-cores, 3057
 ⁷⁵⁷ Hudson, A. C., and E. J. Stevens, data on ferrite core materials, 897

Indits on letrice Orotes, Solarian Mudson, A. C., and E. J. Stevens, data on ferrite core materials, 897
Huet, P., with others, incasurement of very slight variations of resistance, 555; Hall effect in Ni films, 1279; properties of Sb films, 2693
Huey, R. M., noise in communications and servo systems, 1682
Hugen, W., transistor oscillators in carrier-frequency techniques, 1811
Hugeney, E. H., A. Seljak and A. Towle, frequency stepper for propagation tests, 1485
Hughes, D. J., with Others, lattice vibrations by neutron scattering, in Si, 2291, in Ce, 2304
Hughes, R. C., with others, lattice vibrations by neutron scattering, in Si, 2291, in Ce, 2304
Hughes, N. A., melsing with ferrite isolators, 11
Hughes, W. A., designing with ferrite isolators, 11
Hughes, W. A., designing with ferrite isolators, 11
Hughey, etc., ordical method for determining carrier lifetimes, 1230
Huldt, L., optical method for determining carrier lifetimes, 1230
Huldt, L., optical method for determining carrier lifetimes, 1230
Huldinger, F., with others, field parameters of galvano- and thermo-magnetic effects in ferromagnets, 758 c
Hulst, G. D., communication technique for multi-

Hullinger, F., with others, field parameters of galvano- and thermo-magnetic effects in ferromagnets, 758 c
Hulst, G. D., communication technique for multipath channels, (D)596
van de Hulst, H. C., light scattering by small particles, 1519
Hülster, F., with E. Rostas, microwave amplification by intrinsic negative resistances, 3159 p
Hultqvist, B., auroral isochasus, 2975, (D)4062
and J. Ortner, ionization below 50 km after strong solar flares, 2576
Humby, A. M., equatorial sunset effect, 3461
Humphrey, F. B., and E. M. Gyorgy, flux reversal in soft ferromagnetics, 3405
Humphrey, F. B., and E. M. Gyorgy, flux reversal in Get, 3377
Hurd, I. D., A. W. Simpson and R. H. Tredgold, anomalous polarization in ferroelectrics, 1911
Hurd, R. A., magnetic fields of ferrite ellipsoid, 403; scattering from small anisotropic ellipsoid, 413

Electronic & Radio Engineer

- Hurley, R. B., designing transistor circuits, 43, 3613
 Hurney, P., with R. Wasserman, tones find data in high-speed tape systems, 932
 Hurwitz, H., Jr, with P. L. Auer, space-charge neutralization in diodes, 2432
 with others, theory of cathode sheath in discharge, 82
 Husa, V., with others, p-n junctions in Ge, 3485
 Husimi, K., ultra-low velocity component of spontaneous polarization in BaTiO₃, 160; polarizability in BaTiO₃, 3744
 and K. Kataoka, pulse-width dependence of switching velocity in BaTiO₃, 2275
 Huster, E., and E. Ziegler, spreading of discharge in counter tubes, 1332
- Huzimura, R., and T. Sidei, effects of impurities and temperature on electroluminescence speetra, 152
- Hyde, F. J., drift transistors, internal current gain of, 999, current gain of, 3880, h.f. power gain of, 3881; current gain of alloy-junction transistor, 387
- 3878
 with R. W. Smith, transistor current gain, 3426
 Hyde, N. G., telemetering information from satellites, 124
 Hynek, J. A., with F. L. Whipple, I.G.Y. optical satellite tracking program, 2566
 Hyvärinen, L., Fourier analysis, 1298

- Iglitsyn, M. I., Yu. A. Kontsevol and A. I. Sidorov, pon-equilibrium charge carriers, distribution of in base region of p-n junction, 1919, lifetime of in Ge, 1929
 Igo, T., E. Yamaka and M. Yatani, band structure
- in base region of p-n junction, 1919, lifetime of in Ge, 1929
 Igo, T., E. Yamaka and M. Yatani, band structure of InSb, 1940
 Igras, E., with others, domain structure of ferroelectrics, 158
 Ikeda, T., internal friction of BaTiO₂ ceramics, 475; studies on (Ba-Pb) (Ti-Zr) O₃, 3006
 Iles, P. A., and P. J. Coppen, delineation of p-n junctions in Si, 514
 Imamutdinov, F. S., N. N. Meprimerov and L. Ya. Shekma, magnetic double refraction of microwaves, 776
 Imyanitov, I. M., measurements of e.s. fields in upper atmosphere, 3713
 Inage, N., with others, parametric amplifier using Ge doide, 1149
 Indiresan, P. V., negative resistance for d.c. computers, 3605
 Ingalts, R. P., with others, u.h.f. signals reflected from moon, 1525
 Ingelstam, E., with others and microwave fields, 2206
 Ingraham, R., theory of the cosmic-ray equator,

- Ingraham, R., theory of the cosmic-ray equator, 3661
- 3661 Ingram, D. J. E., applications of microwave physics, 779; application of magnetic resonance to solid-state electronics, 2924

- Intrator, A. M., reduction of magnetic resonance to solid-state electronics, 2924
 Intrator, A. M., reduction of interference from television receivers, 955
 Ioffe, A. F., semiconductor thermoelements and thermoelectric cooling, (B)207; present and future of semiconductors, 489; development of theory of semiconductors, 490
 Ionescu, G., u.s.w. propagation in towns, 3850
 Ionescu, T. V., and O. C. Gheorghiru, coupling of oscillator and tube of ionized gas, 1156
 Iordanisbvili, E. K., and L. G. Tkalich, semiconductor thermostat for self-oscillators, 609
 Irie, H., with others, microwave propagation over sea beyond line of sight, 2734
 Irland, E. A., data signalling system, 259
 Isaev, A. A., I. G. Mikhailov and A. S. Khimumin, ultrasonic interferometer design, 2816
 Isbell, D. E., log-periodic reflector feed, 2853
 Isenberg, C. R., with others, solubilities of Sn in Si and Ge, 4094
 Ishida, T., with others, Fa-layer multiple reflections, 1342
 Isted, G. A., round-the-world echoes, 1343; meteor activity and scatter signal recordings, 2600 f; Marcori and communication beyond horizon, 2000 c; analysis of Gibraltar-U.K. iono-spheric scatter signal recordings, 2600 f; Marcori and communication beyond horizon, 2000 l
- Marcori and communication beyond horizon, 2000 l
 Istomin, V. G., with B. A. Mirtov, investigation of ionic composition of atmosphere, 3702
 Isupov, V. A., with others, nonferroelectric phase transitions in solid solutions, 1912; new ferroelectric, 2632
 van Iterson, P. W. L., television transmitters, 3493; video correction equipment, 3495
 Ives, R. L., negative-supply outhoard Codan, 3101
 Iwasaki, H., thermoelastic loss in quartz vibrators, 206

- 206
- Iyengar, P. K., with B. N. Brockhouse, no modes of Ge by neutron spectrometry, 173
 Izbak, I. A., influence of unilateral compressio permittivity of BaTiO₃ ceramics, 481 normal
- Jacchia, L. G., atmospheric effects in orbital acceleration of artificial satellites, 2564; corpuscular radiation and acceleration of artificial satellites, 2960
 Jackson, J. A. C., with E. G. A. Goodall, transmission of e.m. waves through wire gratings, 3964
 Jackson, L. E. with L. C. Sadder incorporate

- 3964
 Jackson, J. E., with J. C. Seddon, ionosphere electron densities, 3714
 Jackson, W. H., with others, semiconductor current limiter, 1368
 Jacobs, H., with others, microwave techniques in lifetime measurement, 3774
 Jacobs, I. S., and R. W. Schmitt, low-temperature behaviour of dilute alloys Mn-Cu and Co-Cu, 2673 beha⁻ 2673

- Jacobs, J. A., with others, geographical variations in geomagnetic micropulsations, 2946
 Jacobse, P. G., micro-module design progress, 2486
 Jacobsen, E. H., piczoelectric production of micro-wave phonons, 2277
 N. S. Shiren and E. B. Tucker, effects of 9.2-kMc/s ultrasonics on resonances in quartz, 3816
- 3816

- N. S. Shiren and E. B. Tucker, effects of 9.2-kMc/s ultrasonics on resonances in quartz, 3816
 Jacobson, M. J., correlation with similar uniform collinear arrays, 1066
 Jacobson, R. L., with R. K. Mueller, grain-boundary photovoltaic cell, 1723
 Jaeschke, F., N.T.S.C. colour modulator for C.C.I.R. standard, 2762
 Jaffe, H., piezoelectric ceramics, 4086
 de Jager, F., and J. A. Greefkes, 'Frena' speech transmission system, 2753
 Jaggi, R., with others, field parameters of galvano-and thermo-magnetic effects in ferromagnets, 758 c
 Jagy, J. P., design of resonant notch filters, 368
 Jakits, O., thermal behaviour of semiconductor rectifiers, 3109
 James, A. V., with others, calorimeters for measure-ment of microwave power, 2358
 James, B. H. L., and M. T. Slockford, microwave frequency standard, 1300
 James, J. C., with M. L. Meeks, frequencies for meteor-burst communication, 597
 James, M., microwave network spans Canade, 973
 James, M., with others, fixed-frequency cyclotron with one dee, 1985
 Janes, H. B., with M. C. Thompson, Jr, phase stability over low-level tropospheric path, 4176
 Jansen, L., molecular theory of dielectric constant, 761
 Jansen, J. H., reciprocity in acoustical systems, 332
 Jansen, J. H., reciprocity in acoustical systems, 332

- Jansen, L., molecular theory of dielectric constant, 761
 Janssen, J. H., reciprocity in acoustical systems, 332
 Jansson, L. E., with J. F. Berry, transistor 20-kc/s oscillator, 745
 Jarrett, H. S., and R. K. Waring, ferrimagnetic resonance in NiMO_a, 543
 Jasberg, J., with others, high-power pulsed klystrons, 1410; high-power windows at microwave frequencies, 3159 c
 Jastrow, R., with others, G-M counters, 3446
 Jastrow, R., with others, satellite orbits from radio tracking data, 2568
 Jaumann, J., and E. Neckenbürger, dielectric behaviour of Sc, 2285
 Jauquet, C., excitation of surface wave on dielectric cylinder, 1438
 Javan, A., production of negative temperature in discharges, 3656
 Jelley, J. V., with P. Goldsmith, optical transition radiation, 4018
 Jellinghaus, W., and M. P. de Andrés, crystal anisotropy and magnetostriction with Hall effect, 3803
 Jenkins, R. O., theory of ballast tubes or barretters, 270

- 270

- Jenkins, R. O., theory of ballast tubes or barretters, 270
 with others, evaporation of Ba from impregnated cathodes, 2792
 Jennings, D. A., and W. H. Tanttila, frequency modulator for marginal oscillator, 1826
 Jennison, R. C., interferometer for measurement of brightness distributions, 1177; detection of coherent harmonics in solar outbursts, 4035
 Jenns, C. C., with others, thermoelectric power of semiconducting diamond, 1924
 Jerens, R., single sideband, present and future, 263
 Joglekar, P. J., power distribution diagrams for dipole arrays, 2470
 Johler, J. R., and L. C. Walters, mean absolute value and standard deviation of phase, 3416; propagation of ground-wave pulse, 3842
 John, H. F., properties of Ge single crystals grown from molten metals, 4102
 Johne, K. R., with J. R. Hechtel, electron-ray tracing in electric and magnetic fields, 3524 t
 Johns, B. R., receiver for Australian d.m.e. beacon, 145

- In electric and magnetic news, sort.
 Johnson, B. R., receiver for Australian d.m.e. beacon, 145
 Johnson, C. G., and C. K. Birdsall, M.J crossed-tield travelling-wave tube, 2788 dd
 Johnson, C. Y., and others, results obtained with rocket-borne ion spectrometers, 3703
 Johnson, E. C., with H. Vantine, Jr, transceivers compute distance, 146
 Johnson, F. A., lattice absorption bands in Si, 1608 and J. M. Lock, vibrational spectrum and specific heat of Ge, 517
 Johnson, F. M., and A. H. Nethercot, Jr, antiferromagnetic resonance in MnF₂, 3791
 Johnson, F. M., feature of galactic radio emission
- Johnson, H. M., feature of galactic radio emission, 4034

- Johnson, H. R., *and R. R. Bagi*, electron beam technique for measuring circuit velocity, 3524 o
 Johnson, M. A., tropospheric scatter propagation theory and application to experiment, 2000 v
 wilh F. A. Kitchen, turbulent scattering in propagation at m h, 575
 Johnson, M. D., and D. A. G. Tait, filter attenuation characteristics, 731
 Johnson, S. D., and J. R. Singer, current regulator using transitors, 979
 with J. R. Singer, transistorized nuclear-resonance magnetic-field probe, 1810

- Johnson, W. C., with others, path combinations in whistler echoes, 1577
 Johnston, T. W., perturbations in electron beams from shielded and immersed guns, (D)2429; nonlaminar electron beams in high magnetic fold 2574 c.

- Johnston, T. W., perturbations in electron beams from shielded and immersed guns, (D)2429; nonlaminar electron beams in high magnetic fields, 3524 s
 Jones, C. I., with R. C. Lyman, electroluminescent panels for automatic displays, 3434
 Jones, C. I., with R. C. Lyman, electroluminescent panels for automatic displays, 3434
 Jones, E. I., with R. C. Lyman, electroluminescent purities in CaF., 3411
 Jones, E. E., inductance of eccentric tubular conducting system, 3191
 Jones, E. E., inductance of eccentric tubular conducting system, 3191
 Jones, E. M. T., and J. K. Shimizu, wide-band strip-line balun, 3931
 with J. K. Shimizu, coupled-transmission-line directional couplers, 3556
 Jones, R. C., R. Matheware and J. H. Sanders, radiosonde measurement of electric field and polar conductivity, 1195
 Jones, R. C., radar of echoes from atmospheric inhomogeneities, 819
 Jones, R. F., radar echoes from atmospheric inhomogeneities, 819
 Jones, R. C., with others, power transistors, 2769
 Jones, R. C., with others, power transistors, 2769
 Jones, R. C., with others, U.R.S.I. report on antennas and waveguides, 3565
 Josephson, B., and A. Blomquist, ground-wave v.h.f. propagation, 3069
 and G. Carlson, fading and distortion of 3-kMc/s transhorizon signals, 3090
 and F. Ekkund, microwave propagation experiences, 3091

Jouguet, M., propagation in discontinuous periodic structures, 2103; effects of amplitude and phase distortion on signal carried by h.f. wave, 3473

3473
Jovanovic, D. T., multivibrator circuit using junction transistors, 2503
Jowett, J. K. S., measurement and prediction of v.h.f. tropospheric field strengths, 2000 n
Joy, W. R. R., long-range propagation at 10 cm λ, 2000 t; 3·2 cm λ propagation beyond horizon, 2000 u

2000 ú
 with others, influence of ocean duct on scatter propagation beyond horizon, 578
 Julesz, B., coding television signals, 3489
 Jungfer, H., properties of Mathieu and related functions, 2509
 Junius, W., automatic evaluation of sound reflections, 3545
 Junod, P., with G. Busch clostical evaluation

renections, 3545 Junod, P., with G. Busch, electrical properties of Ag₂Sc, 758 a Jurgen, R. K., solid-state panels for display or storage, 1654

Kaganov, M. I., and V. M. Tsukernik, theory of kinetic processes in ferromagnetic dielectrics, 1285
Kahl, G. D., and F. D. Bennell, coherence require-ments for interferometry, 398
Kahn, L. R., compatible s.s.b. modulation system, 1277

ments for interferometry, 398
Kahn, L. R., compatible s.s.b. modulation system, 971
Kahng, D., with others, processing Ni matrix cathodes, 4250
Kaiser, R. H., with H. J. Hrostowski, infrared spectra of heat-treatment centres in Si, 167; absorption spectrum of As-doped Si, 1244
Kaiser, W., H. L. Frisch and H. Reiss, formation of donor states in heat-treatted Si, 1926
Kakita, K., with K. Morita, fading in microwave relays, 3475
Kalashnikov, S. G., E. Yu. L'vona and V. V. Ostroborodova, properties of Ge doped with Zn, 1613
with others, influence of group III and V elements on recombination in Ge, 1614
Kallistratova, M. A., scattering in turbulent atmosphere, 2083
Kalimann, H. K., model atmosphere based ou rocket and satellite data, 3300
Kalman, P. G., with others, c.r. tube for monochrome and colour television, 619
Kalman, P. G., with others, c.r. tube for monochrome and colour television, 619
Kalman, J. K., Bailey and H. Daans, Canadian caesium-beam standard of frequency, 2701
C. F. Pattenson and M. M. Thomson, Canadian standard of frequency, 2700
Kamigaito, O., with others, oxide-cored cathode, 3078
Kamiryo, K., and others, measurements of serial drum nemory, 346

and others, measurements of field or comb-type slow-wave structure,

I.15

3078 Kamiryo, K., an patterns for

patterns 3524 n

Kamiya, Y., with others, oxide-cored cathode, 3078 Kammer, D., with F. Brauer, mobile radio system, 262

- Kammer, D., with F. Brauer, mobile radio system, 262
 Kamphoefner, F. J., with others, automatic input equipment for data processing, 3586
 Kanai, Y., electrical conductivity, in p-type InSb, 179, in n-type InSb, 530
 Kanaya, S., and K. Ueno, h.f. propagation related to annular eclipse, 2730
 Kane, J. A., arctic measurements of collision frequencies in D region, 1886
 Kane, J. V., time to pulse-height converter, 2879
 Kanefsky, M., with others, magnetostrictive delay line for video signals, 1134
 Kaner, E. A., and F. G. Bass, statistical theory of propagation over ideally conducting plane, 3840
 Kanner, M., error reduction in loaded potentiometers, 3969
 Kanzaki, S., with others, to uble-vane torque-operated wattmeter for 7 kMc/s, 223
 Kaplan, D. E., and M. E. Browne, electron free

- Kaplan, D. E., and M. E. Browne, electron free precession in paramagnetic free radicals, 3408
 Kaplan, S. H., error correction in colour television tubes, 990
 Kaplunova, E. I., and K. B. Tolpygo, temperature dependence of Hall coefficient in semiconductors, 1621
- 1621
- Kaposi, A. A., transistor blocking oscillator for digital systems, 3970
 Kaposi, J. F., magnetic cores as switching elements, 2492

- Kaposi, J. F., magnetic cores as switching elements, 2492
 Kapur, K. N., and J. W. McGrath, r.f. unit for n.m.r. spectrometer, 2544
 Kapustinskil, A. F., effective radius of electron in crystal lattices, 1858
 Karal, F. C., Jr, and S. N. Karp, diffraction of skew plane e.m. wave by absorbing wedge, 3266
 Karavainikov, V. N., amplitude and phase fluctuations in spherical wave, 662
 Karbowiak, A. E., guided wave propagation in sub-mm region, 13
 Karekar, R. N., with others, nature and origin of atmospherics, 3699 a
 Kargin, V. A., with others, producing polymers with semiconductor properties, 4121
 Karnovskii, M. I., with N. F. Vollerner, concentration coefficient of directional acoustic systems, 3905
 Karo, D., impedance measurement circuit, 554
 Karp, A., fast-wave interactions with electron film,

- Karp, A., fast-wave interactions with electron film, 3159 m
 Karp, S. N., with F. C. Karal, Jr, diffraction of skew plane e.m. wave by absorbing wedge, 3266
 Karpova, I. V., with others, influence of group III and V elements on recombination in Ge, 1614

- and V elements on recombination in Ge, 1614
 Karstensen, F., with J. Goorissen, pulling of Ge crystals, 3029
 Kartaschoff, P., with others, improvements in NH₄ maser, 758 g
 Kashcheev, B. L., with E. G. Proshkin, inhomogeneous structure of F region, 2244
 Kashprovskil, V., radio wave propagation and soil conductivity, 434
 Kasuya, I., variations of E₂ layer in Japan, 127
 Y. Hakura and H. Hojo, world-wide distribution of *fmtn* and Dellinger effect, 2588
 Kasuya, T., theory of impurity conduction, 1223; general theory of transport, 4014
 and S. Koide, theory of impurity conduction, 1224
- and K. Yamada, electrical and thermal con-ductivity of monovalent metals, 4015
 Katano, S., with others, F₂-layer multiple reflections, 1342

- 1342
 1342
 Kataoka, K., with K. Husimi, pulse-width dependence of switching velocity in BaTiog, 2275
 Katchky, M., with H. G. Byers, slotted waveguide array for radar, 711
 Kato, J., with others, measurement of attenuation by rain, 4187
 Kato, S., prevailing wind in ionosphere and S_q variations, 453
 with others, ionospheric scattering, under influences of ion production and recombination, 4059, in electrodynamically controlled turbulence, 4060
 Kato, Y., and T. Watanabe, geomagnetic storm in

- hilluences of ion production and recombination, 4059, in electrodynamically controlled turbulence, 4060
 Kato, Y., and T. Watanabe, geomagnetic storm in relation to geomagnetic pulsation, 1537
 Katsenelenbaum, B. Z., critical cross-sections in irregular waveguides, 699
 Katsura, T., with others, magnetic properties of TiFe₂O₄-Fe₂O₄ system, 542
 Katz, H., trends of construction in development of valves, 2793
 Katz, I., with C. I. Beard, dependence of microwave signal spectra on ocean roughness, 242
 Kaufman, A. B., solders for nuclear and space environments, 4144
 Kaufman, A., B., solders for nuclear and space environments, 4144
 Kaufman, M. M., with others, end-fired memory, 36
 Kaus, P., negative effective mass in negative resistance, 3632
 Kautz, B., with R. W. Buchanan, dynamic testing of computer blocks, 3591
 Kavadas, A., and D. G. Glass, polarization of radar echoes from aurora, 4064
 with G. F. Lyon, radar echoes from aurora, 2255
 Kawai, N., acoustic field of vibrating source, 1044
 Kawatami, K., with Y. Anon, cosmic rays observed by satellite 1958 a, 448
 Kay, H. F., spherically symmetric lenses, 3583; scattering of surface wave, 3844
 Kay, H. F., with R. V. Coades, dielectric properties of meanicolate and metatantalate ceramics, 3326
 Kay, H. F., with R. V. Coades, dielectric properties of meanicolate and metatantalate ceramics, 3326
 Kay, H. F., with R. V. Coades, dielectric properties of meanicolate and metatantalate ceramics, 3326
 Kay, H. F., with R. V. Coades, dielectric properties of metanicolate and metatantalate ceramics, 3326
 Kay, I., measurement of virtual height, 3715

- Kay, L., comparison of echo ranging systems, 1893
 Kay, R. H., C. G. Phillips and R. H. Teal, versatile stimulator, 229
 Kaye, J., with others, diodc thermo-electron engine, (D)2435

- (D)2435
 Kazan, B., feedback light-amplifier panel for picture storage, 1408
 Keast, D. N., with F. M. Wiener, propagation of sound over ground, 3900
 with others, instrumentation for study of sound propagation, 2081
 Keays, S. K., with others, distress beacon for crash position indicator, 1891
 Keby, M. H., and A. F. Culbertson, 6.kMc/s system for toll telephone service, 2393
 Keeling, H., air trials of Decca, 462
 Keen, A. W., topological nonreciprocal network element, 2871
 Keebsom, P. H., and G. Seidel, specific heat of Ge and Si, 2287
 Keibs, L., and W. Tismer, measuring acoustic

- and Si, 2287 Keibs, L., and W. Tismer, measuring acoustic impedance of air spaces, 3180 Keidel, L., acoustic design of studio in Karlsruhe, 1756 Keiser, B. E., digital counter techniques for radar, 2981

- Keiser, B. E., digital-counter techniques for radar, 2961
 Keldysh, L. V., influence of lattice vibrations on production of electron-hole pairs, 850
 Kell, R. D., with others, colour TV recording on black and white lenticular film, 1371
 Kelleher, K. S., and J. P. Shelton, limitations of satellite antennas using spherical arrays, 1091
 Keller, J. B., with B. R. Levy, propagation of e.m. pulses around earth, 1662; diffraction by smooth object, 3265
 with B. D. Seckler, theory of diffraction, geometric, 2538, asymptotic, 2539
 Keller, P. R., and L. K. Wheeler, automatic error correction, 966
 Keller, S. P., and G. D. Pettil, phosphor with fluorescence larger than energy gap, 2623
 Kellerer, J., magnetic coupling in disk-seal triodes, 2788 w
 Kellog, P. J., possible explanation of Van Allen radiation at high altitudes, 2217
 and E. P. Ney, new theory of solar corona, 2943
 E. P. Ney and J. R. Winckler, geophysical effects associated with high-altitude explosions, 2575
 Kelly, G. E., Jr, ferrosonant circuit, 2140
 Kelly, G. E., Jr, ferrosonant circuit, 2140
- 2575
 Kelly, G. E., Jr, ferroresonant circuit, 2140
 Kelly, K. C., with R. S. Elliott, serrated waveguide, 1074
 Kelly, M., with others, radio control of ventricular contraction, 929
- Kelly, M., with others, radio control of ventricular contraction, 929
 Kelly, R. L., and W. J. Fredericks, polarization of excitation bands in CdS, 2991
 Kelso, R. J., and J. C. Grace, encoder measures random-event time intervals, 2339
 Kemhadjian, H., transistor amplifiers for d.c. signals, 1498; temperature-control system for transistors, 1693
 Kemp, J., with others, radiation damping effects in 2-level maser, 1818
 Kendall, J. T., Si transistors, 1007
 and J. S. Walker, h.f. tetrode transistors, 3516
 Kendall, M. G., and A. Stuart, The Advanced Theory of Statistics, Vol. 1, (B)1639
 Kennody, E. M., with T. G. Hame, transmissions from 1958 82, 2570
 Kennedy R. C., and F. J. Gaskins, electronic composites in television, 612
 Kent, G. S., short bursts of amplitude of 50-Mc/s wave received over 480 km, 2000 filler, 3688
 Kern, R. L., with others, measurement of time dilation in earth satellite, 3688
 Kern, R. L., with R. Benoit, circuit for recording atmospherics, 2870

- Inso, 786 o
 Inso, 786 o
- 1450

- Ketchledge, R. W., logic for digital servo system, 1459
 Kettel, E., with others, mechanical filters for communications technique, 2155
 Key, F. A., and W. G. P. Lamb, analogue computer for prediction of acoustic propagation, 3207
 Keyes, R. W., effects of electron-electron scattering in semiconductors, 492; mobility and effective mass in semiconductors, 2279
 Keys, J. E., and R. J. Primich, nose-on radar crosssections, 3320
 Keyston, J. R. G., J. D. Macpherson and E. W. Guptill, coefficient of thermal expansion of BaTiO₂, 2629
 Khaikkin, S., radio astronomy, 420; determination of velocity of artificial satellite, 442
 Khaikkin, S., radio astronomy, 420; determination propagation in inhomogeneous media, 1041
 Khalthin, L. A., with att. M. Khaltovich, sound propagation in inhomogeneous media, 1041
 Khan, K. M. I., with others, amplitude/frequency response display using ratio method, 219
 Khankar, P. V., and J. N. Das, 1/V characteristics of n-p contacts on galena, 3874
 Kharybin, A. E., analysis of errors in determination of mean value, 1638
 Khaskind, M. D., diffraction and radiation of acoustic waves in liquids and gases, 664

World Radio History

- Khastgir, S. R., with others, triple splitting of F echoes, 1885
 Khe-Yui-Lyan, with A. V. Sandulova, diffusion and solubility of Ta in Ge, 4104
 Khimunin, A. S., with others, ultrasonic interfero-meter design, 2816
 Khlebnikov, N. S., new photoelectron multipliers, 3155
- 479
- 479
 Khutsishvili, G. R., Overhauser effect in paramagnetic salts and semiconductors, 3653
 Khyl, R. L., with others, electron spin-lattice relaxation times, 417; maser amplifier with large bandwidth, 1144
 Kibler, L. U., directional-bridge parametric amplifier, 2183 2183
- 2183
 Kidokoro, T., with others, proof of mode theory of v.l.f. ionospheric propagation, 3094
 Kiel, A., and others, propagation in crossed-field periodic structure, 1731
 v. Kienlin, A., nagnetic materials with perminvar effect, 1284, 2324
 v. Kienlin, L. Lucz de Körel propagation for the periodic structure of the struc

v. Kienlin, U., and A. Kürzl, waveguide termination with film-type resistors, 1082 Kihara, T., irreversible processes in highly ionized gas, 4020

With nim-type resistors, 1062
Kihara, T., irreversible processes in highly ionized gas, 4020
Kihn, H., and W. E. Barnette, microminiature decoder for selective communication, 2018
Kikoin, I. K., E. M. Buryak and Yu. A. Muromkin, anomalously high Hall effect in CrTe, 2681
Kikuchi, C., and others, ruby as maser material, 3793
Kilburn, T., with others, automatic recognition of patterns, 2372
Kilmgton, T., effects of noise in television, 3139
Kimpara, A., ionospheric disturbances by atomic explosion, 3711
Kinartwala, B. K., synthesis of active RC networks, 3978
Kineke, E., with H. Cole, lattice vibrational spectra of Si and Ge, 857
King, A. M., with others, scintillation noise in radar tracking systems, 2609
King, G. A. M., with C. H. Cummack, disturbance in

King, D. D., with S. P. Schlesinger, dielectric image lines, 2827
King, G. A. M., with C. H. Cummack, disturbance in F region following nuclear explosion, 3712
King, G. A. M., with C. H. Cummack, disturbance in F region following nuclear explosion, 3712
King, H. E., directivity of broadside array of isotropic radiators, 3955
King, J. C., anelasticity of quartz at low temperatures, 2334
King, P. G. R., 5%-bandwidth 2.5-MW S-band klystron, 3524 a
King, R. R., experimental Clogston-2 transmission line, 2102
King, R. W. P., with T. T. Wu, driving point and input admittance of linear antennas, 1440
King, F. W. P., with T. T. Wu, driving point and input admittance of linear antennas, 1440
King, Hele, D. G., progress of Sputnik 3, 1545; effect of earth's oblateness on satellite orbit, 2235; density of the atmosphere from analysis of satellite orbits, 2955
and R. H. Merson, new value for earth's flattening, 2567
and R. H. Merson, use of artificial satellite to generate the satellite, 2232
wilk R. H. Merson, use of artificial satellites to explore earth's gravitational field, 792
wilk R. H. Merson, use of artificial satellites to explore earth's gravitational field, 792
wilk R. H. Merson, we of artificial satellites to explore earth's gravitational field, 792
wilk R. H. Merson, we of artificial satellites to explore earth's gravitational field, 792
wilk R. H. Merson, vilk others, orientation control for Ge wafers, 1935

orbits to equator, 2235 Kingsnorth, R. L., with others, orientation control for Ge wafers, 1935 Kingston, R. H., u.h.f. solid-state maser, 4002 — with others, radar echoes from Venus, 2556 Kinnear, J. A. C., automatic swept-frequency impedance meter, 220 Kino, G. S., with P. T. Kirstein, solution to equations of space-charge flow, 764 Kinzer, G. D., with B. B. Phillips, electrification of droplets in cumuliform clouds, 456 Kirby, R. S., service area for television broadcasting, 287 Kirchner, P. H., with others, radio reflections from

Kirby, R. S., service area for television broadcasting, 287
287
Kirchner, P. H., with others, radio reflections from satellite-produced ionization, 2963
Kirenskil, L. V., and V. V. Veter, measurement of boundary layer width between domains, 2676
Kirkpatrick, G. P., with J. M. Forman, screen persistence of colour picture tubes, 4218
Kirschstein, P., and H. Krieger, phase and group delay, 698, (D)3193
Kirstein, P. T., electrodes required to produce given electron gun, (D)653; equations of space-charge flow, 3886
mad G. S. Kino, solution to equations of space-charge flow, 764
Kirsubin, V. P., influence of dielectric on phase constants of helix, 2100
Kiselev, M. L., and V. I. Tseplyaev, oblique shock waves in plasma, 1163
Kita, S., H. Sampei and T. Okajima, transmitting frequency converter, 3145
with others, parametric amplifier using Ge diode, 1149
Kitchen, F. A., and M. A. Johnson, turbulent screening in programmer at marking and the space of the space of

1149
Kitchen, F. A., and M. A. Johnson, turbulent scattering in propagation at m., 575
and G. Millington, Gibraltar-U.K. ionospheric scatter measurements, 2000 a
W. R. R. Joy and E. G. Richards, influence of ocean duct on scatter propagation beyond horizon, 578
E. G. Richards and I. J. Richmond, m-λ propagation in transhorizon region, 2000 p

Electronic & Radio Engineer

- Kitchen, G. F., with others, atmospheric discontinuity layer effects on propagation, 2000 o
 Kitchen, H. D., simplified mains transformer design, 356; cathode compensation, 1814
 Kittaka, S., static charge on high polymer, 4013
 Kittel, C., energy absorption by charge carriers of negative effective mass, 3747; anomalous magnetic crystaline anisotropy peaks in ferromagnetic crystals, 4138
 Kiyanovskii, M. P., with others, large inhomogeneities in F₂ layer, 2581
 Klages, G., with H. Buseck, rectangular waveguide with attenuating foil, 1772
 Klasens, H. A., intensity dependence of photoconduction and luminescence, 1207
 with others, electroluminescence and image intensification, 1597; cathodothermoluminescence, 2624
 Klasky, P. S., with others, capabilities of coaxial

- Klasky, P. S., with others, capabilities of coaxial cable, 2457
 Kleiger, L. B., improving relay reliability, 610
 Klein, C. A., radiation-induced energy levels in Si,
- Klein, C. 4089 j Klein, G., and J. M. den Hertog, sine-wave generator,
- 2876
- Klein, J. M., with D. E. Thomas, automatic trans-istor a measuring set, 3427 Klein, M. W., image converters and image inten-sifiers, 2783

- M. M. W., image converters and image intensifiers, 2783
 with R. S. Wiseman, photoemissive image-forming systems, 4238
 Klein, W., transformer as 2-terminal network, 1467
 and H. Neutjscher, travelling-wave tubes for 4- and 6-Gc/s bands, 2788 b
 Kleiner, W. H., and L. M. Roth, deformation potential in Ge, 2655
 with others, Zeeman effect of excitons in Ge, 2299
 Kleinman, D. A., with others, infrared properties, of SiC, 2297, of SiC film, 2298; anisotropic mobilities in deformed Ge, 3362
 Klemp, H. J., with M. Redlich, electromechanical transducer for stereophonic recording, 2096
 de Klerk, J., ultrasonic wave propagation in Ni, 1951
 Klerk, M., with others, interference from fluorescent lanps, 3463
 Kletsky, E. J., design criteria for magnetic modulators, 2165

- lamps, 3463 Kletsky, E. J., design criteria for magnetic modul-ators, 2165 Kley, W., with others, lattice vibrations in Si by neutron scattering, 2291 Klick, C. C., Ag luminescent centres in sulphides, 2006

- neutron scattering, 2291
 Klick, C. C., Ag luminescent centres in sulphides, 2998
 Klinger, M. I., magnetic susceptibility of semiconductors with impurity zone, 499
 and G. A. Makaryckeva, theory of semiconductors with excited impurity band, 3752
 and Yu. I. Zozulya, theory of semiconductors with excited impurity cone, 1604
 Klipsch, P. W., stereophonic sound with two tracks, three channels, 1064
 Klitzing, K. H., and J. Gielessen, influence of pressure on magnetizability of Au₂Mn, 1273
 Klivans, L. S., d.c. amplifiers for control systems, 748
 Klontz, E. E., with J. W. Mackay, annealing studies in Ge, 4089 p
 with others, thermal and radiation annealing of Ge, 2305; photoconduction of Ge after bombardment, 3027
 Klopfenstein, R. W., corner-reflector antennas, 1099
 von Klüber, H., intensities, polarization and electron densities of solar corona, 1182
 Kluwmpp, R. G., with others, evaluation of modulated air. Gwith others, 691
 Knappe, W., radiation field of delta aerial, 3199
 Knapter, W., with R. C. Knachtli, electron cooling by heat exchange, 397
 Knecht, R. W., lunar influence on E_a at Huancayo, 3305
 Knechtli, R. C., effect of electron lenses on beam noise, 1726

- Knechtli, R. C., effect of electron lenses on beam
- Schtli, R. C., effect of electron lenses on beam noise, 1726 and W. Knauer, electron cooling by heat exchange, 397 and R. D. Weglein, low-noise parametric amplifier, 2185
- ampliner, 2185
 Kneller, E., temperature dependence of spontaneous magnetization in ferromagnetic particles, 2678
 Knight, A. J., with others, vacuum-diode microwave detection, 2794
 Knight, K. V., range equation for active devices, 4010 f
 Knight, P., horizontal radiation patterns of dipole arrays 343

- 4010 f
 Knight, P., horizontal radiation patterns of dipole arrays, 343
 Knight, V. H., with G. Craven, integrally constructed waveguide assemblies, 2826
 Knob, E. D., with J. W. Buckelew, through-connections for printed wiring, 38
 Knopf, W., radio interference in u.s.w. range, 2386
 Knovles, C. H., 'mesa' transistor, 635
 Knowles, R. B., with others, electronic subsystem development problems in naval ordnance, 2803
 Knongole, 3948
 Ko, H. C., amplitude scintillation of extraterrestrial radio waves, 427
 Koch, B., radio waves from detonations, 3650
 Koch, B., radio waves from detonations, 3650
 Koch, B., radio waves from detonations, 3650
 Koch, W., high-resolution emission microscope, 1987
 Kociński, J., influence of demagnetizing field on domain structure, 2677
 Kock, B., Sommerfeld ground wave, 1334
 Kockis, R. D., variational principles in h.f. scattering, 412

- Kodis, R. D., variational principles in h.f. scattering, 412
- Electronic & Radio Engineer

- Koenig, S. H., interelectron collisions and 'temperature' of hot electrons, 3345
 Koepke, G., measurement of dielectric constant of ferrites, 4158
 Koerner, L. F., portable frequency standard, 3052

 with E. A. Gerber, measurements of parameters of piezoelectric vibrators, 211

 Koester, L., with others, fixed-frequency cyclotron with one dee, 1985
 Kogbetliantz, E. G., sin N, cos N and N^{1/m} using electronic computer, 2857
 Kogelnik, K., energy relations in electron beams, 4245
- 4245
- 4245
 Köhler, J., subjective assessment of shared-channel interference, 3479
 with H. Niese, influence of peak content on sensation of loudness, 1754
 Kohn, G., generation of steep pulse edges in non-linear amplifiers, 1488
 Kolde, S., with T. Kasuya, theory of impurity conduction, 1224
 Kokaku, T., with others, F₂-layer multiple reflections, 1342
 Kokin, A. A., with G. V. Skrotskii, system of mag-

- Kokin, A. A., with G. V. Skrotskil, system of mag-netic moments in weak variable magnetic field, 3644

- 3644 Kokosh, G. V., with others, thermoelectric properties of Bi₁Te₃-Bi₂Se₃, 3758 Kokurin, Yu, L., with V. V. Vitkevich, irregularities in ionospheric refraction, 2251 Kolachevskii, N. N., measurement of noise from cyclic remagnetization, 3796 Kollanyi, M., gas-discharge tubes as noise sources, 559
- Kollányi, M., gas-discharge tubes as noise sources, 559
 Kolomenskii. A. A., and Fan Shou-syan', cyclic motion of charged particles in electric field, 3835
 Kolomiets, B. T., with T. N. Vengel', vitreous semiconductors, 1920
 Komar, A. P., N. V. Volkenshtein and G. V. Fedorov, change of sign of Hall constant in alloys, 2675
 Komatsubara, K., noise at Ge fused junction, 1255; change of surface recombination velocity of Ge by gamma rays, 3372
 and U. Hashimoto, annealing of radiation-induced 11/ noise in Ge p-n junction, 298
 Komesaroff, M., polarization measurements of solar radio bursts, 101
 and C. A. Shain, refraction of extraterrestral radio waves, 2973
 Kompancets, A. S., radio emission from atomic explosion, 3649
 Komdratlev, B. V., with J. R. Pierce, transoceanic communication by means of satellites, 2012
 with others, reflex klystron as negative-resistance-type amplifier, 1741
 Kondo, G., with others, 223
 Kondratlev, B. V., with V. P. Shestopalov, space resonance in helix waveguide, 2464
 Köno, H., ferromagnetic phase in Mn.Al system, 2679
 Konsee, A., with others, distribution of nonequilibrium charge carriers in base region of p-n

- Konose, A., with others, waveguide for low-loss transmission, 2829
 Konose, A., with others, distribution of non-equilibrium charge carriers in base region of p-n junction, 1919; lifetime of non-equilibrium charge carriers in Ge, 1929
 Kool, C. F., R. W. Moss and D. C. Stinson, oriented ferrites with cubic anisotropy, 3399
 Kopp, H. J., and W. Petsold, linearization of multipliers at high anode currents, 2054
 Koppelmann, J., R. Frielinghaus and F. J. Meyer, generation of very short ultrasonic pulses, 2078
 Kornfield, N. R., with others, end-fired memory. 36
 Kornfield, N. R., with others, chromium corundum paramagnetic amplifier, 1145
 Korpel, A., with A. J. Seyler, voltage-controlled low-rass filter, 1119
 Kosthere, V. V., with others, functional characteristics of node determinant, 548
 Kossowsky, L. H., with others, functional characteristics of node determinant, 548
 Kostarev, V. V., with A. G. Goreik, radio echoes from invisible objects in troposphere, 2240
 Kosterev, V. M. and H. Statz, Zeeman splittings of paramagnetic ions, 2549

- baramagnetic ions, 2349
 Kostyshyn, B., and D. D. Roshon, Jr, magnetic field probe, 1973
 Kotadia, K. M., meteors and E, ionization, 3699 g
 Koury, F., with K. H. Builler, sylvatron electro-luminescent display, 224
 Kovalenko, E. S., gyrotropic elliptical waveguide, 3933

- 3916
 Kozak, W. S., capacitor storage in analogue memory, 32
 Kozlovskii, V. Kh., stability of ferroelectric crystals,
- 483 Kraft, L. G., Jr, with others, radar echoes from Venus, 2556
- Krajewski, I., transistor circuits for 1-Mc/s computer, 3229
 Kramer, A. G., and P. M. Platzman, microwave manometer, 565
 Kramer, A. S., c.r. storage tubes for direct viewing, 1744

- 1744 Kranz, J., and W. Drechsel, observation of Weiss domains in polycrystalline material, 1281 Krasil'nikov, V. A., acoustics conference, 661 Krasovskiki (Krasovsky), V. I., investigation of upper atmosphere with Sputnik III, 1550, 1872

- Yu. M. Kushnir and G. A. Bordovskil, investiga-tion of solar radiation using earth satellites,
- 3293
 and others, discovery of 10-keV electrons in upper atmosphere, 3294
 Kraus, C. R., experiments in television over telephone cable, 274; city-wide personal signalling, 3477
- Kraus, J. D., Ohio State University radio telescope, 3962

- Kraus, J. D., Ohio State University radio telescope, 3962
 Kravitz, L. C., and G. S. Heller, resonance isolator at 70 kMc/s, 1439
 Krayer, G., with F. R. Arams, low-loss L-band circulator, 1769
 Krentself, B. A., with others, producing polymers with semiconductor properties, 4121
 Krentself, B. A., waith others, producing polymers with semiconductor properties, 4121
 Kreutself, B. A., with others, producing polymers delay, 698, (D)3193
 Krieger, H., with F. Kischstein, phase and group delay, 698, (D)3193
 Krieger, H., with others, use of d.c. amplifier and recorder to balance resistance bridge, 3061
 Krinitz, A., magnetic circuits for pulse radar, 3316
 Krishnamurthi, M., G. S. Sastry and T. S. Rao, abnormal ionospheric behaviour at 10 m Å, 808; emission from sun at 30 Mc/s, 3699 o
 Krishnan, R., with others, temperature-sensitive ceramic reactance element, 45
 Krishnan, S., diode phase detectors, 1152; cathodefolower for d.c. reference level, 2164
 Kroebel, W., assessing quality of television images and projection systems, 1393; assessment of picture quality, 4222
 F. Arp and H. Baurmeister, perceptibility of image details in television, 3136; visual properties of human eye, 3138
 with others, detail recognition on television singer and projections in Solids, 1175
 Krobns, A., with others, image converters for quantity production, 1404; resolving power of scintillation multipliers, 3081; photoresistors, photodia design of scintilly distribution near focus of lens, 4027

Krom, M. N., held fluctuations near focus of lens, 4027
and L. A. Chernov, effect of fluctuations on intensity distribution near focus of lens, 2917
Krömer, H., negative-mass amplifier, 1824
Krug, W., and J. Schusta, electronic production of lines of equal density, 4167
Krugman, L. M., nomographs for narrow-band transistor amplifiers, 1497
Kruithof, A. A., with others, interference from fluorescent lamps, 3463
Kruser, P. W., InAs infrared detector, 2987
Kruserneyer, H. J., surface potential, nuobility and conductivity of ZnO, 3778
Krzyczkowski, R., planning telecommunications systems, 1355
Ksendzov, Ya. M., with others, relaxation polariza-

systems, 1355
Ksendzov, Ya. M., with others, relaxation polarization and losses in nonferroelectric dielectrics, 480
Ku, S. M., with others, semiconducting properties of HgTe, 4112
Kuck, R. G., expansion of Pacific coast nicrowave network, 2398
Kuczynski, G. C., and R. H. Hochman, light-induced plasticity in Ge, 1938
Kuebler, W., with C. F. Pulvari, polarization reversal ir BaTiO₃, 159
Kuh, W., characteristics of reverberation plates, 1755

Kühn, U., v.h.f. field-strength measurements near Berlin, 2740; propagation conditions at 1.3 Gc/s, 3095; propagation over nonuniform terrain, 3456

Kuhrt, F., with H. J. Lippmann, influence of geometry on Hall effect and magnetoresistance effect, 1234

Kukarkin, B. V., launching of cosmic rockets, 3677
 Kulcsar, F., electroinechanical properties of Pb(Zr,Ti)O₃ ceramics, 3739
 Kümmel, U., and K. W. Böer, electrostatic charging of CdS, 3731

of semiconductors, 3757
 Kummer, M., ideal plane reflector, 1097
 Kummer, W. H., with others, tropospheric propagation beyond horizon, 4185
 Kundu, M. R., investigations of persistent solar sources at cm A, 424; dimensions of sources of solar bursts, 425; time relations of metre-wave and 3-cm wave bursts, 2555; high-resolution interferometer, 2936
 and J. F. Denisse, solar radiation at dm λ as index for ionospheric studies, 787
 Kundu, P., phase-angle measurement, 1970
 Kundu, P., with others, hydromagnetic capacitor, 1843

1843
Kunze, C., inertia effects in vidicon-type tubes, 985; Sb₅S, films, optical properties, 1209, photo-electric properties, 1210
Kunzler, J. E., with others, phonon-drag thermo-magnetic effects in n-type Ge, 2662
Küpfmüller, K., and W. Andrich, speech trans-mission with quantization, 3855
Kuprevich, N. F., television techniques in astronomy, 3083
Kurbatov, L. V., with G. V. Skrotskii, anisotropy of width of ferromagnetic resonance absorption lines, 2210
Kurnosova, L. V., investigations on cosmic rays by earth satellites, 2959

I.17

with others, breakdown of CdS films, 2993; rendering visible conductivity inhomogeneities of semiconductors, 3757

1755

1843

with G. A. Skuridin, scientific investigations by earth satellite, 440
 Kurokawa, K., expansions of e.m. fields in cavities, 2143

2143
Kurokawa, S., T. Takahashi and M. Arai, mutually coupled CR-type directional coupler, 9
with others, double-vane torque-operated wattmeter for 7 kMc/s, 223
Kurov, G. A., and Z. G. Pinsker, thin layers of variable composition in In-Sb system, 3780
Kuroyangi, N., flux-controlling-type adder, 3210
Kurth, C., band filters with bandwidth control, 735
Kurtz, A. D., and C. L. Gravel, diffusion of Ga in Si, 513

- 513
- 513

 with others, avalanche breakdown in n-p Ge diffused junctions, 3378

 Kurtze, G., and B. G. Watters, wall design for high transmission loss, 3917
 Kürzl, A., with U. v. Kienlin, waveguide termination with film-type resistors, 1082
 Kushnir, Yu. M., with others, investigation of solar radiation using earth satellites, 3293
 Kustanovich, I. M., with others, producing polymers with semiconductor properties, 4121
 Kurtruff, H., characteristics of reverberation curves, 3546

- 3546 Kwestroo, W., with G. H. Jonker, ternary systems with BaO-TiO₂, 838
 Kyle, R. F., super-gain aerial beam, 3952

- Laaff, O., with others, radio link installations for telephony and television, 1687
 Lacoste, R., criterion for surface conduction on insulating solids, 3252
 with others, ionization chambers as sources of current, 4152
 Lacrolx, R., effect of cubic field on Gd³⁺ ion, 758 e; theory of paramagnetic resonance of Eu and Gd, 1630
- 1630
- Lacy, R. E., gain across mountainous obstacles, 1333 t; U.S. Army communications, 2744
 Ladany, I., d.c. characteristics of junction diode, 2410
- 2410
 with A. Levitas, semiconductor-semiconductor 'point-contact' diode, 2037
 Lafargue, M., and R. Milleamps, c.m. properties of glacier ice, 1994
 Laff, R. A., and H. Y. Fan, magnetoresistance in n-type Ge, 870
 Lafleur, C., transfer properties of a linear system, 3220

- n-type Ge, 870
 Lafleur, C., transfer properties of a linear system, 3220
 Lagasse, J., with others, ionization chambers as sources of current, 4152
 Lagercrantz, C., homodyne detector for periodic waveforms, 3065
 Lagerstrom, R. P., with others, 20-40-kMc/s backward-wave oscillator, 1742
 LaGow, H. E., with R. Horowitz, auroral-zone atmospheric-structure measurements, 1560
 Laine, E. L., dividing wide frequency bands, 2506
 Lamb, J., M. Redwood and Z. Shteinshleifer, absorption of compressional waves in solids, 3536
 Lamb, W. G. P., with F. A. Key, analogue computer for prediction of acoustic propagation, 3207
 Lamber, J., with others, irradiation of photocouctive single crystals of CdS, 2617
 Lamming, J. S., h.f. Ge transistors, 1000
 Lamopert, M. A., and A. Rose, transient behaviour of onine contact, 2903
 F. Herman and M. C. Steele, single phonon emission in breakdown of seniconductors, 3013
 with A. Rose, gain-bandwidth product for photoconductors, 1900; photoconductor performance and Fermi level, 2988
 Landmark, B., with T. Hagfors, simultaneous variation of anylitude and phase of Gaussian noise, 583; direction of arrival of long-duration meteor echoes, 1993
 Landsberg, P. T., with A. R. Beattie, Auger effect in semiconductors 3341

- b33; direction of arrival of long-duration meteor echoes, 1993
 Landsberg, P. T., with A. R. Beattie, Auger effect in semiconductors, 3341
 Landsman, A. P., with others, Si solar batteries for earth satellites, 3862
 Lane, J. A., resistive-film calorimeters for microwave prover uncouragenet, 4162
- earth satellites, 3862
 Lane, J. A., resistive-film calorimeters for microwave power measurement, 4162
 with A. C. Gordon-Smith, gas-discharge noise sources at cm A, 658
 Lane, R. N., and D. B. Cameron, current integration with solion liquid diodes, 2023
 Lang, bein, D., solution of Bloch's integral equation for metal electrons, 1914
 Lange, F. H., coding law of information theory, 4195
 Langer, D., with others, cathodo-electroluminescence phenomena in ZnS phosphors, 834
 Langford, R. C., versatile van istor, 42
 Langmuir, R. V., with others, opower-line aerial, 1672; v.1.f. c.w. transmitter for ionospheric investigation, 3873
 Lapin, A. D., scattering of sound waves in irregular waveguides, 1042
 Laponsky, A. B., with N. R. Whetten, secondary emission from MgO thin fins, 3216
 Laporte, O., and J. Meisner, Kirchhoff-Young theory of diffraction, 2918
 Laporte, M. L., D. S. Mathewson and C. G. T. Haslam,

- 649
- 649
 Large, M. I., D. S. Mathewson and C. G. T. Haslam, high-resolution survey, of Andron.eda nebula, 2937, of Coma Cluster, 2938
 Larish, E., and J. Shekhiman, production of two temperatures in ionized gas, 2536

- Lark-Horovitz, K., with H. Fritzsche, effect of minority impurities in p-type Ge, 2658
 with others, photoconduction of Ge after bombard-ment, 3027

- ment, 3027 Larmore, L., range equation for passive infrared devices, 4010 e Larrabee, R. D., drift velocity saturation in p-type Ge, 3361 Larsen, B. F., with P. Gudmandsen, microwave propagation measurements in Denmark, 579 Lashkarev, V. E., and others, lifetime of injected current carriers in Sb-doped Ge, 1932 with P. I. Baranskii, bulk thermo-e.m.f. in Ge, 524
- with P. I. Baranskii, bulk thermo-e.m.f. in Ge, 524
 with V. A. Zhidkov, diffusion and electric state of thermal acceptors in Ge, 520
 Lasser, M. E., P. Cholet and E. C. Wurst, Jr, highsensitivity infrared detectors, 1012
 with others, control of luminescence by charge extraction, 473
 Latham, R., and others, high-power 400-Mc/s klystron, 3524 j
 Latour, C., with P. Gautier, field of series of magnetic lenses, 3445
 LaTourrette, J. T., with others, r.f. spectra of

- lenses, 3445
 LaTourrette, J. T., with others, r.f. spectra of hydrogen deuteride, 1852
 Laudet, M., with P. Gawlier, calculation of fields, 4023
 with others, measurement of induction in magnetic electron lenses, 2704
 Laurenson, L., with others, Ti getter pump, 1204
 Laurent, T., physical relations in ladder-type filters, 1116
- 1116 Lauter, E., and K. Sprenger, detecting solar flare effects in ionosphere, 1181 Lautz, G., with G. Harbeke, crystal structure of Ga₂Te₃ doped with Cu, 3031 Laverick, E., calibration of microwave attenuators, 1123
- and f. Welsh, automatic standing-wave indicator, 2711
- Lavine, J. M., apparatus for measuring Hall coefficient, 918; ordinary Hall effect in Fe₃O₄, 3403

- Lavine, J. M., apparatus for measuring Hall coefficient, 918; ordinary Hall effect in Fe₂O₄, 3403
 Lawley, A., processing materials with electron bounbardment, 4168
 Lawrie, J. A., V. B. Gerard and P. J. Gill, magnetic effects of two high-altitude explosions, 3671
 Lawson, G. J., with others, deduction of electron content from Faraday fading, 2572
 Lawson, J. D., perveance and Bennett pinch relation in electron beams, 84; e.m. wave problems, 4025
 Lax, B., with others, Zeeman effect of excitons in Ge, 2299; exciton- and magneto-absorption of transitions in Ge, 3364; optical magneto-absorption effects in semiconductors, 3365
 Lax, M., with R. Rosenberg, free-carrier absorption in n-type Ge, 1249
 Lead, N., quartz servo oscillator, 371
 Leadabrand, R. L., and A. M. Peterson, radio echoes from auroral ionization, 1670
 and I. Yabroff, geometry of auroral communications of auroral echoes, 4065
 Leady, D. G., C. Y. Lee and G. H. Mealy, verifications of auroral echoes, 4065
 Leady, D. M., with J. N. Barry, transistorized pulse amplifier, 2518
 Leary, F., microwave health hazards, 2075
 Lebacqz, J. V., and others, high-power windows at mcreating otential torpuscular radiation, 2216
 Lebolond, A. F., electron trajectories in guns for M-type tubes, 3524 jj
 Lecar, M., J. Sorenson and A. Eckels, earth's gravitational potential torp called of the system by diperimential confliction of waveguide and pipe, 3932
 Lecargw, R. C., with T. Sorenson and A. Eckels, earth's gravitational potential form satellite orbit, 1867
 Lechleider, J. W., mode conversion at junction of waveguide and pipe, 3932
 Lecargen, R. C., with T. S. Spencer, magnetoacoustic resonance in Y-Fe garnet, 201
 with others, low-temperature line-width maximum in Y-Fe garnet, 201
 with others, verification of logic system by digital computer, 2134
 Leedig. C., h. transistor, 2768

- with others, verification of logic system by digital computer, 2134
 Lee, E. W., and D. R. Callaby, measurement of velocity of propagation of domain boundary in perminvar, 194
 Lees, C. H., digital computers in Britain, 1779
 Lefevre, H. W., and J. T. Russell, vernier chronotron, 1965, 2338

- Deley G. H. W., and J. T. Russell, vernier chronotron, 1965, 2338
 Lefevre, H. W., and J. T. Russell, vernier chronotron, 1965, 2338
 Lefkowitz, I., and T. Mitsui, effect of irradiation on coercive field of BaTiO₂, 1913
 Lego, P. E., and T. W. Sze, obtaining transient response using digital computer, 2130
 Legrand, J. P., forecasting solar activity by study of cosmic radiation, 1179
 Lehmann, R., absolute calibration of standard microphones, 1430
 with P. J. A. H. Chavasse, loudspeaker measurements, 1761
 Lehmann, W., electroluminescence of ZnS phosphors as equilibrium process, 832; particle size and efficiency of electroluminescent ZnS, 2266
 Lehtonen, E. W., and E. A. Cronauer, a.c.-controlled magnetic amplifiers, 382
 Leighton, H., with C. Ellyett, solar-cycle influence on lower ionosphere and v.h.f. scatter, 130
 Leighton, L. G., and A. Makulec, improvements in lamps for television studios, 286
 Leinbach, H., and G. C. Reid, upper-atmosphere ionization by particles from solar flare, 1521
 with C. G. Little, riometer, 1566
 Leivo, W. J., with M. D. Bell, rectification and photoeffects in semiconducting diamond, 504

World Radio History

- Lekhtinen, G. N., M. A. Rzaev and L. S. Stil'bans, temperature dependence of work function of semiconductors, 494
 Lempicki, A., polarization of fluorescence in ZnS and CdS, 2267; anomalous photovoltaic effect in ZnS, 2989
 Leng, L., medium-wave aerials for simultaneous transmission, 16
- transmission, 16
 Lennartz, H., magnetic-tape recorder for ultrasonic frequencies, 2085
 Lenz, F., distribution of stream of particles with multiple scattering, 1837; stigmatic image in asymmetric electron lenses, 3075
 Lenz, K. L., transmission lines for low-reflection absorption, 1765
- Lenz, K. L., transmission lines for low-reflection absorption, 1765
 and O. Zinke, absorption of e.m. waves in absorbers and li-es, 1068
 Leonard, R. S., v.h.f. radar for auroral research, 1574
 Lépéchinsky, D., magneto-ionic theory and its results, 572
 and C. Davoust, effects of nuclear explosions on ionospheric soundings, 3710
 Lépichinsky, D., magneto-ionic theory and its results, 572
 and C. Davoust, effects of nuclear explosions on ionospheric soundings, 3710
 Lépicnux, M., discrimination between chromospheric eruptions, 1180
 Leroux, J. P., and P. Thureau, photoluminescence of ZnS-Cu, 1908
 Lesk, I. A., and R. E. Coffman, Ge diffused mini-crystals and use in transistors, 637
 and R. E. Gonzalez, selective etching of junction transistors, 1402
 weith others, observation of phonons during tunnelling in junction diodes, 4226
 Levesque, P., L. Gerlach and J. E. Zneimer, grain growth in Ni ferrites, 544
 Levi, L., correction of slant range distortion in high-altitude radars, 821; high-fidelity video record-ing, 931
 Levin, E., R. B. Muchmore and A. D. Wheelon, aperture-to-medium coupling on line-of-sight paths, 4183
 Levin, I., photovoltaic pile, 231
 Levinstein, H., impurity photoconductivity in Ge, 4106

Levinstein, H., impurity photoconductivity in Ge,

4106
Levitas, A., and I. Ladaw, semiconductor-semiconductor 'point-contact' diode, 2037
Levy, B. R., and J. B. Keller, propagation of e.m. pulses around earth, 1662; diffraction by smooth object, 3265
Levy, R., hybrid junctions, 3560
Lewin, L., theory of evlindrical antennas, 3945
Lewis, B., ferroelectric ceramics, 1217
Lewis, D. J., mode couplers and nultimode measurement techniques, 3935
Lewis, R. R., with others, structure and relaxation

Lewis, H. R., with others, structure and relaxation times of Cr³⁺ in TiO₁, 2333 Libin, I. Sh., multivibrator with negative feedback, 1, 1997 Licht, J., with others, tracking weather with satellites, 2715

2715
 Lichtenberg, A. J., with C. K. Birdsall, travelling-wave focusing for plasma containment, 4022
 Li-Chzhi-Tszyan', induced conductivity of CdS and CdSe films bombarded by slow electrons, 2616

and Cose nins boinbarded by slow electrons, 2616
Lidlard, A. B., with M. J. S. Slephen, Faraday effect in semiconductors, 4088
Lieb, A., electron-beam voltage indicator tube, 2073
Liebscher, R., and R. Miller, frequency noise in travelling-wave tubes, 3159 dd
Lifschitz, L., with R. der Agobian, propagation of non-ionizing shock waves, 4016
Lignon, J., with others, centipede aerial, 1333 u
Likhter, A. I., and T. S. D'vakonova, dependence of Hall effect on pressure in n-type Ge, 2663
Lin, C. M., and R. W. Grow, broadband microwave coaxial connector, 3551
Linden, D., and A. F. Daniel, power sources for space age, 2399
Linden, D. A., sampling theorem's, 3417
Lindmayer, J., and R. Zuleeg, determining trans-

age, 2399
Lindmayer, J., and R. Zuleeg, determining transistor bigh-frequency limits, 4232
with R. Zuleeg, sweep equipment displays transistor β, 928
Lindmayer, J., and U. Gladhorn, automatic recorder for c.r. oscillography, 1978
Lindmer, P., and U. Gladhorn, automatic recorder d.c. amplifiers, 65
Lindsay, J. E., and H. J. Woll, design of transistor d.c. amplifiers, 65
Lindsay, P. A., and K. D. Collins, design of helical coupler for 2-Gc/s band, 3159 x
with others, travelling-wave multiple-beau klystron, 3524 x
van Lint, V. A. J., and H. Roth, electron irradiation of Ge and Te, 4089 1
Lippin, D. M., transfer function of linear filter. 3607
Lippincott, E. R., and Al. B. Negnevitskit, theory of half-wave magnetic amplifier, 1495
Lippincott, E. R., and J. B. Negnevitskit, theory of solar dees, 205
Lippmann, H. J., and F. Kuhrl, influence of geometry on Hall effect and magnetoresistance effect, 1234
Lisgarten, N. D., with M. Blackman, magnetic models for interpreting domain effects on electron beam, 3407
Liszka, L., variation of signal strength from 1958 62, 2953
Litovchenko, V. G., with others, lifetime of injected current carriers in Sb-doped Ge, 1932

2953
Litovchenko, V. G., with others, lifetime of injected current carriers in Sb-doped Ge, 1932
Little, A. G., with others, parametric amplifiers as superregenerative detectors, 3245
Little, C. G., and H. Leinbach, riometer, 1566
Little, R. P., H. M. Ruppel and S. T. Smith, beam noise in crossed electric and magnetic fields, 313

Electronic & Radio Engineer

4106

Little, V. I., 1.f. measurement of dielectric constant of conducting liquids, 215
Liu, S. H., with R. H. Mattson, switching v.h.f. with Si diodes, 3486
Liu, Y. J., and J. O. Campbell, collision detection without range data, 3722
Lo, A. W., with others, transfluxor-controlled electro-luminescent display panels, 568
Löb, E., dielectric properties of quartz sands, 2272
Lobanov, A. M., with G. P. Mikhaldov, dielectric losses and permittivity of polymers, 3818
Lobanov, I. V., suppression of unwanted sideband, 589

Lobanov, I. V., suppression of unwanted sideband, 589
Locher, P. R., with others, absorption in paramagnetic salts at 1 325 Mc/s, 2674
Löcherer, K. H., noise of space-charge diodes, 2436
Lochner, J. P. A., and J. F. Burger, subjective masking of delayed echoes, 5; intelligibility of reinforced speech, 3912
Lock, J. M., with F. A. Johnson, vibrational spectrum and specific heat of Ge, 517
Lockwood, J. A., with L. C. Towle, cosmic-ray increases associated with solar flares, 2557
Loeb, J., binary channels in cascade, 2388; physical interpretation of Shannon's ambiguity, 3853
Loebner, E. E., and E. W. Poor, Jr, bimolecular transitions in GAP, 3737
Loferski, J. J., and P. Rappaport, effect of radiation on Si solar-energy converters, 1366; electron-bombardment-induced recombination centres in Loce, 4108

bombardment-induced recombination centres in Ge, 4108 Logachev, E. G., passage of random noise signals through detector, 2005 Logachev, Yu. I., with others, cosmic rays and terrestrial corpuscular radiation by cosmic rocket, 2231; investigation of cosmic radiation, 3663 3663

rocket, 2231; investigation of cosmic radiation, 3663
Logan, M. J., with others, preparation and properties of MgTe, 1258
Logan, R. A., and W. L. Bond, density change in Sion melting, 2292
G. L. Pearson and D. A. Kleinman, anisotropic mobilities in deformed Ge, 3362
Loh, S. C., electric potential and capacity of tore, 4012; toroidal functions, 4145
and J. Y. Wong, radiation field of elliptic loop, 20
with J. Y. Wong, radiation resistance of elliptic loop, 1776; radiation field of elliptic helical antenna, 3577
Lomax, R. J., effect of inclination of focusing electrodes on electron-beam formation, 2060
Lombardo, P. P., and E. W. Sard, low-frequency travelling-wave reactance amplifier, 2524
Lomer, P. D., passive protection cells, 2800 d
and R. M. O'Brien, microwave pulsed attenuator, 2800 b; high-power microwave duplexer, 2833
Long, D., C. D. Motchenbacher and J. Myers, impurity

- Lormer, F. D., passive protection cens, 2800 a
 and R. M. O'Brien, microwave pulsed attenuator, 2800 b; high-power microwave duplexer, 2833
 Long, D., C. D. Motchenbacher and J. Myers, impurity compensation and magnetoresistance in Si, 2293
 with others, effect of pressure on Hall-coefficient reversal in Te, 1237
 Long, R. R., and G. H. Munro, radio signals from first earth satellite, 444
 Long, W. G., and R. R. Weeks, quadruple-diversity tropospheric scatter systems, 972
 Looney, C. H., Jr, with others, tracking orbits of man-made moons, 1190
 Loriers, J., with G. Villers, properties of mixed Dy-Y, Dy-Gd and Dy-Fr garnets, 2331
 with others, magnetic properties of Er garnet, 1290; properties of mixed Gd-Er and Gd-Y garnet, 1633
 Lothian, B. W., A. C. Robinson and W. Sucksmith, properties of dilute ferromagnetic alloys, 1631
 Lotkin, M., smoothing of data, 208
 Louisell, W. H., parametric amplifier and frequency converter, 2065
 with others, parametric amplifier and frequency converter, 2065
 with others, parametric amplification of space-charge waves, 3159 k
 Lovell, A. C. B., with J. G. Davies, observations of the Russian moon rocket Lunik II, 4051
 Lovell, S. E., and R. H. Cole, coaxial displacement dielectric cell, 3063
 Low, W., and D. Shaltied, electron paramagnetic resonance in BaTiO, 477; paramagneticresonance spectrum of Gd in TLGO, 909
 with M. Weger, parametric-resonance spectrum of Gd in TLGO, 909
 with M. Weger, parametric-resonance spectrum of Gd in TLGO, 901
 with M. Weger, paramagnetic-resonance spectrum of Gd in TLGO, 911
 Low, W., and D. Shaltied, electron paramagnetic resonance in BaTiO, 477; paramagnetic-resonance spectrum of Gd in TLGO, 909
 with M. Weger, paramagnetic-resonance spectrum of Gd in TLGO, 901
 with M. Weg

1745
 Lucardie, J. A. van der Vorm. See van der Vorm Lucardie, J. A.
 Lucas, A. R., relativistic flow of electrons in straight lines, 396
 Lucas, L. matching wavespide directional and better

Jucas, I., matching waveguide directional couplers, 1083
Lucas, I., matching waveguide directional couplers, 1083
Lucas, W. J., with others, propagation measurements at 3 480 Mc/s, 2000 r
Lucasson-Lemasson, A., L-spectrum of Ge, 3772
Lucke, W. H., magnetic amplifier commutating and pulse-width encoding circuit, 2188
Lucken, J. A., with others, experimental annular reflex klystron, 3524 bd
Lüdicke, E., synchronization characteristics of television receivers, 1388
Ludioff, A., with H. Awender, crystal-controlled transistor oscillators, 1129
Ludwig, G. H., cosmic-ray instrumentation in earth satellite, 2964

Electronic & Radio Engineer

with others, radio observations with satellite 1958, 2238
 Ludwig, G. W., and H. H. Woodbury, electron spin resonance in Ni-doped Ge, 2661
 Lueg, H., W. Schallehn and H. Toedter, Telefunken traffic radar, 1898
 Luft, W., cooling of semiconductor devices, 3146
 Lundh, Y., dgital techniques for small computations, 1452

1452

1452
 Lunze, K., stabilization of transistor circuits at variable temperature, 2051
 Lüscher, J., and P. Döme, transistor simulator, 4156
 Lüst, R., with L. Biermann, radiation and particle precipitation from solar flares, 1530
 Lüthi, B., magnetoresistance of metals in high fields, 3337

with others, magnetic resistance variation of InSb, 758 b

whit others, magnetic resistance variation of InSb. 758 b
 Luttinger, J. M., Hall effect in ferromagnetics, 1277
 Lutze, E., and D. Bösnecker, paramagnetic electron-tinuities in nonlinear electrodynamics, 2914
 L'vova, E. Yu., with others, properties of Ge doped with Zn, 1613
 Lyamshev, L. M., sound scattering by thin rod, 676
 Lyman, R. C., and C. I. Jones, electroluminescent panels for automatic displays, 3434
 Lynch, R. D., measuring load characteristics of Si cells, 3484
 Lyon, G. F., and A. Kavadas, radar echoes from aurora, 2255
 Lyons, J. F., Jr, analysing multipath delay, 4192

Lyons, J. F., Jr, analysing multipath delay, 4192
 Lysanov, Yu. P., sound scattering on inhomogeneous surfaces, 675; theory of wave-scattering on periodic surfaces, 775
 Lytollis, J., with A. H. W. Beck, mobile Cs frequency standard, 3053

Ma Da-Yu (Maa, D. Y.), normal modes of vibration in rectangular room, 684; acoustics in China, 2808

Macarlo, R. C. V., avalanche transistors, 2772 MacArthur, J. W., origin of v.l.f. radio emissions, 3311

MacArnutr, J. W., origin of V.I.I. radio emissions, 3311
Macdiarmid, I. F., waveform distortion in television links, 4209
MacDonald, A. D., h.f. breakdown in air at high altitudes, 1834
MacDonald, C., narrow-band image transmission system, 276
MacDonald, F. C., thermoelectricity at very low temperatures, 2529
MacDonald, F. C., with others, measurements of 1 250-Mc/s scatter propagation, 3096
Macdonald, N. J., with others, geomagnetic disturbances and changes in atmospheric circulation at 300 mb, 2229
Mackek, O., television monitoring installations, 2763, 3869

Mackey S., television monitoring installations, 2763, 3869
 Macfarlane, G. G., and others, fine structure in absorption-edge spectrum of Si, 509
 with others, effect of magnetic field on absorption edge in semiconductors, 501
 Mack, G., measurement of lattice constant of Ge, 1936; X-ray investigations on Ge-In p-n alloy junctions, 1937
 MacKay, J. W., and E. E. Klontz, annealing studies in Ge, 4089 p
 E. E. Klontz and G. W. Gobeli, thermal and radiation annealing of Ge, 2305
 with others, photoconduction of Ge after bombardment, 3027

ment, 3027
 MacKellar, A. C., with others, electronic clock coder for coded radio beacons, 4069
 MacKimmie, G. B., quadruplexer for simultaneous transmission of television stations, 2119
 with others, 468-Mc/s tropospheric scatter propagation, 245
 Mackimon, L., with others, pulse techniques, 2449
 Mackworth, J. F., and N. H. Mackworth, eye fixations recorded by television eye-marker, 930
 Mackworth, N. H., with J. F. Mackworth, eye fixations recorded by television eye-marker, 930

Maclean, D. J. H., design curves for simple filters,

MacLeod, G. A., with others, Doppler satellite measurements, 1191
 MacLeod, G. A., with others, Doppler satellite measurements, 1191
 Macmillan, R. S., W. V. T. Rusch and R. M. Golden, antenna to eliminate groundwave interference in ionospheric sounding, 710
 with others, power-line aerial, 1672; v.l.f. c.w. transmitter for ionospheric investigation, 3873
 Macpherson, J. D., with others, coefficient of thermal expansion of BaTiO₂, 2629
 Madden, H. H., and H. E. Farnsworth, high-vacuum studies of surface recombination velocity for Ge, 1248
 Maddever, R. S., with others, radiosonde measure-

Maddever, R. S., with others, radiosonde measure-ment of electric field and polar conductivity,

Maddever, K. S., Euk obsers, alsosofic metasate-ment of electric field and polar conductivity, 1195
 Maddock, C. H., with others, dependence of combiner diversity gain on signal-level distribution, 4191
 Madsen, E. R., application of velocity microphones to stereophonic recording, 7
 Maeda, H., geomagnetic disturbances due to nuclear explosions, 3670
 with others, lattice scattering mobility in CdS, 2990

2990

2990
 Maeda, K., electroluminescence of insulated particles, 1215
 Maeda, K. I., and T. Sato, F region during magnetic storms, 1563
 S. Kato and T. Tsuda, ionospheric scattering, under influences of ion production and recombination, 4059, in electrodynamically controlled turbulence, 4060

World Radio History

Machlum, B., diurnal variation of f₀F₁ near auroral zone during magnetic disturbances, 803
Maguire, T., microwave systems using low-noise devices, 3971
Mahaffy, D. W., plasma electron oscillations, 2910
with K. G. Emeleus, transit-time relation for plasma electron oscillations, 1840
Mahar, T. M., with R. MoFee, effect of surface reflections on rain cancellation of radars, 4072
Mailer, W., and H. K. Winmel, quantum theory of dielectric polarization of gases, 2901
Maier-Leibnitz, H., with others, fixed-frequency cyclotron with one dee, 1985
Maillart, D., with others, M-type pulsed amplifier, 2788
Mainberger, W. A., frequency standard using Cs,

Mainberger, W. A., frequency standard using Cs,

550

with others, comparison of Cs frequency stan-dards, 212
 Mainstone, J. S., W. G. Elford and A. A. Weiss, c.w. technique for measurement of meteor velocities,

 105
 Majumder, D. D., track switching system for magnetic-drum memory, 718
 Makarycheva, G. A., with M. I. Klinger, theory of semiconductors with excited impurity band, 3752
 Makhov, G., with others, ruby as maser material, 3793

transistors, 306
Malovetskaya, V. M., with others, Si solar batteries for earth satellites, 3862
Malurkar, S. L., geomagnetic work at Alibag, 3699 c; solar control of unusual geophysical events, 3699 n.
Malyuzhinets, G. D., scattering of sound in sea, 3902
Mambo, M., with others, reception of radio waves from Russian earth satellite 1, 120
Mandel L. impace much solar in carde intensifiers.

Mandel, L., image fluctuations in cascade intensifiers,

3521

805

Mandel', L., image intertuations in cascade intensities, 3531
Mandel'shtam, S. L., and A. I. Efremov, ultraviolet solar radiation, 3664
Mandrell, W. L., with C. A. Master, variable-frequency instrument calibration source, 1696
Mannekov, A. A., with others, chromium corundum paramagnetic amplifier, 1145
Manfield, H. G., advances in potted and printed circuits, 2862
Mangiaracina, R. S., with E. Stern, ferrite high-power effects in waveguides, 3937
Mann, P. A., with others, conductance of dipoles, 1089
Manning, L. A., oblique echoes from over-dense meteor trails, 2225
and V. R. Eshleman, meteors in ionosphere, 1526; Booker's theory of meteoric reflection, 1527
Manoglan, H. A., challenge of space, 2807

1520; Booker's theory of interestic federical, 1520;
 Manoogian, H. A., challenge of space, 2807
 Manring, E., and others, wind determinations in upper atmosphere, 3302
 Mansfield, R., and W. Williams, electrical pro-perties of Bi₃Te₃, 532
 Mansford, H. L., K. M. I. Khan and D. T. A. Margets, amplitude/frequency response display using ratio method, 219
 Many, A., semiconductor surface phenomena, 3019
 with others, phase-shift method of carrier lifetime measurements, 515
 Marais, A., effect of Co on magnetic dispersion of Ni-Zn ferrites, 3808
 and T. Merceron, disaccommodation of permeters

and T. Mercron, disaccommodation of perme-ability of Ni-Zn ferrites, 4136
 with R. Vautier, switching time of square-loop ferrite, 3404
 Marasigan, V., bifurcations in F region at Baguio, 802; height gradient of electron loss in F region, 805

802; height gladient of electron tossin F legion, 803;
804; March, F. C., solderless grounding for braided shields, 336
Marchal, M., and M. T. Marchal, ingestible radio capsule, 1326
Marchal, M. T., with M. Marchal, ingestible radio capsule, 1326
Marchat, H., with R. W. Williams, resistance potentiometers as function generators, 35
Marcuse, S. M., with J. T. Walmark, semiconductor devices for microminiaturization, 3213
Marcuse, D., attenuation of TE₀₁ wave in curved helix waveguide, 704
Margenau, H., with others, conductivity of plasmas to microwaves, 1842
Margetts, D. T. A., with others, amplitude/frequency response display using ratio method, 219
Mariani, F., world-wide distribution of F₂-layer

Margerts, D. 1. A., win others, amplitude/inequency response display using ratio method, 219
Mariot, E., and Pham Mau Quan, e.m. tensor in presence of induction, 407
Mariot, L., and Pham Mau Quan, e.m. tensor in presence of induction, 407
Mariot, J., and Mam Mau Quan, e.m. tensor in transmission, 962; direct measurement of transmission frequency of aircraft, 3423
Mark, M., and M. Slephenson, air-cooled chassis for electronic equipment, 353
Markow, E. W., servo phase control shapes antenna pattern. 1092
Martin, A. V. J., ultrasonic velocity in liquids under pressure, 1; sound distribution at Brussels exhibition, 1691; propagation of sound in sea water, 2810
Martin, E. J., with others, persistent v.h.f. field strengths beyond radio horizon, 2737
Martin, E. J., Jr, calibrated source of mµs pulses, 2706

- Martin, H. J., with W. Freitag, electronic ultrasonic image converter, 2084
 Martin, J. R., G. W. Warnick and R. N. Vandeland, reniote-control carrier systems in two-way closed-circuit television, 285
 Martin, R. J., with J. E. Rowe, electron-trajectory calculator and Poisson cell, 3524 kk
 Martin, W. A., inverter for 20 kc/s using power transistors, 2021
 Martineau, M., photoconductivity of irradiated CdS, 1594

- transistors, 2021
 Martineau, M., photoconductivity of irradiated CdS, 1594
 with others, irradiation of photoconductive single crystals of CdS, 2617
 Martner, J. G., with J. S. Arnold, resonances of BaTiO₂ cylinders, 2446
 Marton, L., Advances in Electronics and Electron Physics, Vol. 9, (B)327
 Martyn, D. F., F region of ionosphere, 1555; sporadic-E, spread-F and twinkling of radio stars, 2970
 Maruse, S., and Y. Sakaki, electron-optical properties of point cathodes, 3077
 Maslov, A. A., analogue multiplier-divider using thyrites, 1458
 Maslov, V. P., characteristic functions of equation Δu + k^{tu} = 0, 2696
 Mason, D. R., and J. C. Sarace, contacts to p-type Si, 2296
- Si, 2296
- Mason, R. G., and M. J. Vitousek, geomagnetic phenomena associated with nuclear explosions, phc. 3672
- 3672
 Mason, W. C., with others, u.h.f. signals reflected from moou, 1525
 Massey, H. S. W., molecular vibration and rotation
- Massey, R. S. W., molecular vibration and rotation by electron impact, 3259
 Master, C. A., and W. L. Mandrell, variable-frequency instrument calibration source, 1696
 Mataré, H. F., dislocation planes in semiconductors, 3338
- with others, conductivity of grain boundaries in Ge bicrystals, 2657; grain-boundary amplifier, 3241
- Mathams, R. F., voltage-operated logarithmic
- Mathams, R. F., voltage-operated logarithmic amplifier, 3996
 Mather, R., and J. Sharpe, tuning cavitics for reflex klystrons, 3525
 Mathewson, D. S., with others, high-resolution survey, of Andronneda nebula, 2937, of Coma Cluster, 2938
 Mathews L. and F. L. Rabb. obmic Allacture Si
- Cluster, 2938 Matlow, S. L., and E. L. Ralph, ohmic Al/n-type Si contact, 3356 Matossi, F., quenching of photoconductivity and electron lifetime, 2263 Matsumaru, K., reflection of tapered waveguides, 1768

- electron lifetime, 2263
 Matsumaru, K., reflection of tapered waveguides, 1768
 Matsumaru, T., H. Fujisaki and Y. Tanabe, preparation of ZnS single crystals, 2625
 Matsushita, S., study of morphology of ionospheric storms, 2248; upper atmosphere in auroral zone, 3704; geomagnetic and ionospheric phenomena associated with nuclear explosions, 3709
 Matsuzwa, K., microphones for airborne ultrasonics, 2448, microphones for airborne ultrasonics, 2448
 Matthei, W. G., with others, 'reactatron' microwave amplifier, 1150; surface-barrier photodiodes as photocapacitors, 3885
 Matthews, D. J., with H. Sutcliffe, transistor junction temperature, 1974
 Matthigs, B. T., with H. Sutcliffe, transistor productors, 3633
 Matthysse, S. W., with others, conductivity of plasmas to microwaves, 1842
 Mattingley, R. L., B. McCabe and M. J. Traube, split reflector for inicrowave antennus, 712
 Mattson, R. H., and S. H. Liu, switching v.h.f. with Si diodes, 3486
 Mattura, Y., Ge-Si alloy junctions, 3379
 Matura, N., and T. Nagata, turbulence in upper atmosphere, 2577
 Matveev, A. N., capture mechanism and limiting current in betatrons, 2718
 Mattner, R., pin triode in television bands IV and V, 2796
 Mautner, R. S., with R. E. Murphy, transistorized i.f. strip design, 70

- 2796
 Mautner, R. S., with R. E. Murphy, transistorized i.f.-strip design, 70
 Maxwell, E., with J. H. Phillips, broad-band amplifier for radar and scatter, 64
 Maxwell, E. L., with others, radio system performance in noise, 963; 1.f. propagation paths in arctic areas, 4182
 May J. pulse amplitude discriminator. 2505
- ance in holse, 795, 11. propagation pairs in arctic areas, 4182
 May, J., pulse amplitude discriminator, 2505
 Mayaud, P. N., scientific reports of French polar expeditions S IV 2, 111
 Mayer, A., with others, multilevel pulsed-field maser, 3623
 Mayer, C. H., with others, maser amplifier for radio astronomy, 2892
 Mayer, F., Faraday effect and birefringence in ferrites, 1632
 Mayer, H. J. G., infrared absorption by conduction electrons in Ge, 871
 Mayer, L., magnetic writing with electron beam, 539; electron mirror microscopy of stray fields, 3800

- 3800
- 3800
 Mayer, N., colour television experiments, 1372
 Mayer, W., industrial television installations, 1394
 Mayeur, J. P., impedance of capacitors, 2136; probable life of paper capacitors, 3219
 Mayo, B. J., effect of reactive loads on reflex klystrons, 3524 ff
 Mayo, C. G., and J. W. Head, wide-range RC oscillator, 54
 and H. Page, a.m. transmitter class-C output stage, 624
 Mayr, S., iterative analysis of asymmetric quadripoles, 2869
 Mazumi, T., relaxation-time anisotropy in CdS, 2992

- McCabe, B., with others, split reflector for micro-

- McCabe, B., with others, split reflector for microwave antennas, 712
 McClure, J. W., analysis of multicarrier galvanomagnetic data for graphite, 1241
 McCollom, K. A., nucleonic instrumentation-discriminators, 3446
 McCousland, M. A. H., with others, dynamic nuclear polarization, 3412
 McCracken, K. G., and N. R. Parsons, unusual cosmic-ray intensity fluctuations, 1860
 with others, decreases in cosmic-ray intensity during period October 1956 January 1958, 4037
 McCullagh, G. C., with R. B. Caime disclosure

- With others, decreases in cosmic-ray intensity during period October 1956 January 1958, 4037
 McCullagh, G. C., with R. B. Cairns, discharge modes using thermionic cathodes, 2441
 McDonnell, D., and R. W. Perkins, interpolation and prediction of signals plus noise, 2391
 McDowell, H. L., with others, helix travelling-wave amplifier, 2788 a
 McElhinny, M. W., E-layer measurements during solar eclipse, 3306
 McFadden, M. H., with R. J. A. Paul, measurement of phase and amplitude at I.f., 1651
 McGrae, R., and T. M. Maher, effect of surface reflections on rain cancellation of radars, 4072
 McGraire, W. S., radio links for control of aeronautical equipment, 1689
 McIlwain, C., with P. Rothwell, satellite observations of solar tosmic rays, 3692
 McIlwain, C. E., with others, radio observations with satellite 1958, 2238; ionizing radiation at 3500-36 000 km, 3691
 McIntosh, B. A., interception noise in electron streams, 3165
 McIntyre, J. W., with C. C. Willhite, analowne computer for evaluating radar performance, 1465
 McKenna, M. F., low-loss structures in waveguides, 340
 McKernow, C. A., with others, engineering of 1.f.

- 340 McKerrow, C. A., with others, engineering of 1.f. communication systems, 2750 McKim, F. S., with T. M. Buck, chemical and atmospheric effects on surface properties of Si, 4097
- McLaughlin, S. W., with others, 20-40-kMc/s backward-wave oscillator, 1742
 McLean, T. P., with others, effect of magnetic field on absorption edge in semiconductors, 501; fine structure in absorption-edge spectrum of Si, 509 500
- McLeish, C. W., and R. S. Roger, h.f. direction-finding errors caused by vertical reradiators, 1203 McLeod, M. G., with cthers, circuits for space probes, 3286
- 3286
 McMahon, R. E., transistorized core nemory. 1783
 McNamara, F., noise problem in coincident-current core memory, 1787
 McNaney, J. T., clectron gun operates high-speed printer, 34
 McNaughton, R., and B. Mitchell, rectifier nets with multiple outputs, 29
 McNaught, J. P., with others, micro-module approach to miniaturization, 2485

- McNaul, J. F., with Others, micro-module approach to minaturization, 2485
 McNeill, W., preparation of cadmium niobate, 2276
 McNicol, A. S., tr. switch, 44
 McSkimin, H. J., ultrasonic measurements on solids at high temperature, 2815
 with others, elastic moduli of GaAs, 3380
 McSpadden, W. R., and E. Eberhard, designing transistor oscillators, 746
 McWhorter, A. L., and R. H. Rediker, cryosar, 3211
 Meadows, E. B., with others, results obtained with rocket-borne ion spectrometers, 3703
 Meadows, R. W., reflections from neteor trails and E₄ on N-S path at v.h.f., 2000 i
 Meadis, S. K., design of pulsed distributed amplifiers, 2166
 Meakins, R. J., with J. S. Dryden, impregnants for paper capacitors, 1474
 Mealy, G. H., with others, verification of logic system by digital computer, 2134
 Medcalf, W. E., and R. H. Fahring, growth of CdS crystals, 4077
 Medhurst, R. G., echo distortion in f.m., 3472
- crystals, 4077
 Medhurst, R. G., echo distortion in f.m., 3472
 with others, dependence of combiner diversity gain on signal-level distribution, 4191
 Medici, I., transmission quality in f.m. radiotelephony, 2014 e; expression for a signal at output of limiter, 4189
 Medicus, G., energy spectrum of plasma electrons, 765
- 765

- Medicus, G., energy spectrum of plasma electrons, 765
 Medina, M. A., with E. N. Skomal, nuclium-power microwave limiter, 2468
 Medved, D. B., electronic scan ferrite-aperture Luneberg-lens system, 2473
 Meeks, M. L., and J. C. James, frequencies for meteor-burst communication, 597
 Meewezen, W. D., permeability tuning, 1678
 Megla, G., planning radio links, 1364; metallic reflectors for location purposes, 1582; origin of multipath propagation of microwaves, 4186
 Melboom, S., with A. Szöke, radiation damping, 2543
 Meier, D. A., mus magnetic gating and storage element, 1462
 Meihardt, J., low-frequency small-signal transistor amplifiers, 399
 Meinke, H., properties of lossy inhomogeneous lines,

- Meinke, H., properties of lossy inhomogeneous lines, 3192
- and A. Rihaczek, bandwidth compression of radar displays, 3724
 Meissinger, H. F., simulation of infrared systems, 4071 4071
- 40/1 Meixner, J., with O. Laporte, Kirchhoff-Young theory of diffraction, 2918 Melamed, N. T., energy transfer in phosphors,
- 4081
 Melamid, A. E., manufacture of photoelectron multipliers, 3156

Melchior, G., with others, echo in television images, 3134

- Melchior, G., with others, echo in televisiou images, 3134
 Melchor, J. L., and P. H. Vartanian, temperature effects in microwave ferrite devices, 3938
 Melcherčik, J., with H. Rabenhorst, dielectric properties of BaTiO₃, 1601
 Mellichamp, J. W., with others, electroluminescence of AIN, 4082
 Mel'nik, I. G., with others, electron-hole transition in point-contact rectifiers, 185
 Mel'nik, V. G., I. G. Mel'nik and S. S. Gutin, electron-hole transition in point-contact rectifiers, 185
 Mel'nik, O. W., deplistor semiconductor switching device, 2420
 Men'A. V., S. Ya. Braude and V. I. Gorbach, phase fluctuations of 10-cm waves over sea, 2738
 Mende, H., K. Rawer and E. Vassy, rocket measurements of absorption in lower ionosphere, 2972 meas 2972
- measurements of absorption in lower ionosphere, 2972
 Menyuk, N., and K. Dwight, low-temperature transition in Ni-Fe ferrice, 902
 Merceron, T., with A. Marais, disaccommodation of permeability of Ni-Zn ferrites, 4136
 Mercler, J. M., development of semiconductor devices, 294
 Mercurio, J. F., 1-Mc/s oscillator, 1484
 Merkulov, V. V., e.m. wave propagation in media with random heterogeneities, 414
 Merson, R. H., and D. G. King-Hele, use of artificial satellites to explore earth's gravitational field, 792
 D. G. King-Hele and R. N. A. Plimmer, changes in inclination of satellite orbits to equator, 2235
 with D. G. King-Hele, new value for earth's flattening, 2567
 Merten, L., lattice oscillations in crystals with zinc

Merten, L., lattice oscillations in crystals with zinc blende structure, 3413
 Messenger, G. C., deterioration of transistor life, 1715

1715
 Meszaros, G. W., transistor voltage regulators, 980
 Meth, M., television sound detector uses drift transistor, 2028
 Metzon, G. H., conductivity of oxide cathodes, 2428
 Metz, A., deflection of waves by movement of propagating media, 3248
 Metze, O., automatic tuning of transmitter aerials, 3197

3197
 Metzger, P. H., with E. P. Warekois, X-ray method for A¹¹¹E^V compounds, 3786
 Mevel, J., study of interaction between adjacent spheres, 1333 p.
 Mey, J., with A. Boucherie, pulse-height analyser, 377
 Meyer, F. J., with others, generation of very short ultrasonic pulses, 2078

Meyer, N. I., variation of transistor small-signal parameters, 995 Meyer, R. A., with others, automatic failure recovery in data processing system, 1453 Meyer, W. E., space-charge aberration in electron microscopes, 3074

Meyer-Brötz, G., junction-transistor applications, 4228

4228
Meyerand, R. G., Jr, and S. C. Brown, high-current ion source, 1986
Meyerhofer, D., transition to ferroelectric state in BaTiO₈, 843
Meynieux, R., method of Liouville applied to Weber's equation, 912; y functions applied to Weber's equation, 913

Meynteux, R., method of Liouville applied to Weber's equation, 913
Middleton, A. E., with others, preparation and properties of Alsb, 2311
Middleton, D., with others, multipurpose bias device of logical elements, 1461
Midgley, E., with M. Applebaum, f.nl. receiver using transistors, 4188
Miesch, R. A., with others, vacuum-diode microwave detection, 2794
Mikazan, P. S., diffraction of e.m. waves at open end of helix waveguide, 3958
Mikhail, H., with Y. L. Yousef, electrodynamic magnetic field gradiometer, 218
Mikhailov, G. P., and A. M. Lobanov, dielectric losses and permittivity of polymers, 3818
Mikhailov, I. G., ultrasonic absorption in viscous liquids, 671
and V. A. Shutilov, diffraction of light by ultrasonic waves, 678
with others, urasonicinterferometer design, 2816
Mikhnevich, V. V., upper atmosphere, investigation in high atmosphere by earth satellites, 3694
Miles, R. J., standard block for digital computing system, 2855
Millard, G. H., triple v.h.f. reflectometer, 923; nonlinearity in cracked-calbon resistors, 1106
Millea, M. F., and T. C. Hall, surface mobility in Ge and Si, 505
Millear, M. F., with M. Lafargue, e.m. properties of glacier ice, 1994
Miller, I. C., and C. W. Sharek, designing ultrasonic

Miller, I. C., and C. W. Sharek, designing ultrasonic

Miller, I. C., and C. W. Sharek, designing ultrasonic delay lines; 28
Miller, J. D., temporary threshold shift and masking, 681
Miller, K. S., R. I. Bernstein and L. E. Blumenson, generalized Rayleigh processes, 210
Miller, N. B., reflections from gradual-transition absorbers, 3548
Miller, R. B., and E. A. Hiedemann, intensity distribution of light diffracted by ultrasonic waves, 1051
Miller, R. C., motion of 180° domain walls in BaTiO₂, 155

Electronic & Radio Engineer

- and A. Savage, observations of antiparallel domains in BaTiO₂, 2634; hysteresis loops and pyroelectric effect in BaTiO₂, 3332
 Miller, R. E., with others, antenna-beam distortion in transhorizon propagation, 1347
 Miller, R. H., coincidence circuits using transistors and diodes, 3230
 Miller, M. R., microwave switching by crystal diodes, 2866
 Millington, G., propagation at great heights in the atmosphere, 1336; I.E.E. radio and telecommunications section: chairman's address, 1421
 with F. A. Kitcher, Gibraltar-U.K. ionospheric scatter measurements, 2000 a
 Millen, B. Y., O. B. Slee and E. R. Hill, radio sources between declinations + 10° and -20°, 423
 with others, pencil-bean survey of galactic plane at 3.5 m, 2220
 Millon, D. K., with L. W. Davies, netallic contacts to Ge and Si, 491
 Milosevic, L. J., and R. Vauley, travelling-wave resonators, 2144
 Milwright, A. L. P., harbour approach aids, 2259 n; developments in marine radar, 2259 g
 Minakowic, B., coupling of three coaxial helices, 3159 z
 Minden, H. T., intermetallic semiconductors, 163

- 3159 z
 Minden, H. T., intermetallic semiconductors, 163
 with others, semiconducting properties of HgTe, 4112
- 4112
 Minn, S., and H. Damany, influence of Se on conductivity of gold film, 488
 Minnhagen, L., an l. L. Stigmark, excitation of ionic spectra by 100-kW h.f. pulses, 376
 Minnis, C. M., accuracy of ionospheric forecasts, 1333 h; ionospheric changes at Singapore during solar eclipse, 1883
 and G. H. Bazzard, indices of solar activity, 3281
 Minorsky, N., parametric excitation, 1963
 Minow, D. E., timed-signal generator with flexible output, 1966
 Winton, B. bigh-quality, a f. transistor amplifier

- output, 1966
 Minton, R., high-quality a.f. transistor amplifier, 2886
 Mints, M. Ya., theory of magnetron, with single-anode, 646, with split-anode, 647
 with L. E. Pargamanik, diffusion theory of magnetron, 645
 Mirimanov, R. G., and Yu. V. Anisimova, circular waveguide partially filled with ferrite, 2116
 Mirkotan, S. F., with others, large inhomogeneities in F₄ layer, 2581
 Mirtov, B. A., rocket investigation of atmosphere, 3700

- Mirtov, B. A., rocket investigation of atmosphere, 3700
 and V. G. Istomin, investigation of ionic composition of atmosphere, 3702
 Misawa, T., theory of p-n junction device using avalanche multiplication, 988
 Mischler, W. D., with I. Kenney, equalization of aural and visual delay, 3132
 Miselyuk, E. G., with others, Ge with Fe impurity, recombination of current carriers in, 1933, effect of annealing on carrier lifetime in, 1934
 Mishima, M., with others, helix-type travelling-wave amplifier, 1415

- of annealing on carrier lifetime in, 1934
 Mishima, M., with others, helix-type travelling-wave amplifer, 1415
 Mishin, L. N., incressing stability of sound amplification systems, 693
 Misme, P., influence of frontal discontinuities, 1333 q
 with L. Boithias, guided propagation in the Mediterranean, 940
 Misra, R. P., planar reference diode, 4253
 and W. H. Moll, servo system for processing oxide-coated cathodes, 651
 Misselwitz, W., with others, breakdown of CdS films, 2993
 Missen, J. I., rating of semiconductor rectifiers under dynamic conditions, 2341
 Misni, T., with K. Takashima, measurement of input impedance of u.h.f. triodes, 2788 aa
 Mitchell, B., with A. R. McNaughton, rectifier nets with multiple outputs, 29
 Mitchell, J., with others, lightweight airborne navigation system, 25:91
 Mitra, A. P., Indian program for I.G.Y., 3299; ionosphere disturbances at low latitudes, 3699 e: time and height variations in daytime ionosphere, 3708
 and others, radio patrol of solar flares, 3699 p
 with M. N. Rao, effect of vertical drifts on nocturnal ionization of lower ionosphere, 1878
 Mitra, S. N., with B. B. Ghosh, measurement of atmospheric noise, 2743
 Mitsui, T., drolectric effect in Rochelle salt, 484
 with I. Lefkowitz, effect of irradiation on coercive field of BaTiO, 1913
 Miyauchi, K., with others, 4.kMc/s-band v.s.w.r. scanner, 1975
 Miyauchi, K., with others, 4.kMc/s-band v.s.w.r. scanner, 1975
 Miyauchi, K., with others, 4.kMc/s-band v.s.w.r. scanner, 1975
 Miyauchi, K., with others, waveguide for low-loss transmission, 2829
 Mizano, H., conduction mechanism of oxide cathode, 1026
 Moats, R. R., output windows for microwave power tubes, 643

- 1026 Moats, R. R., output windows for microwave power tubes, 643 Moerder, C., transistor equivalent circuits, 1009 Möhring, F., power reflex klystron TK7, 1730; electron oscillations in vacuum tubes, 4251 Molenda, P. J., with others, thermionic integrated micromodules, 2863
- Electronic & Radio Engineer

- Moles. A., voice characteristics. 4: iteration method and V. Ussachevsky, use of acoustic spectro-
- graph, **1425** Moll, A., properties of thin single-crystal films of Ba-Sr titanate, 4083

- Ba-Sr titanate, 4083
 Moll, W. H., with R. P. Misra, servo system for processing oxide-coated cathodes, 651
 Möller, H. G., with others, long-distance single-F-hop transmission, 943; sweep-freouency oblique-incidence pulse transmissions, 2378
 Mollwo, E., with G. Bogner, preparation of ZnO, 878
 Mollwo, L., electron temperature and noise in h.f. torch discharges, 3253
 with J. Smejkal, measurement of u.h.f. quadripole, 1968

- torch discharges, 3253
 with J. Smejkal, measurement of u.h.f. quadripole, 1968
 Molmud, P., Langevin equation and conductivity of plasmas, 3261
 Molo, F., impedance converters, 1480
 Momo, L. R., with others, multilevel pulsed-field maser, 3623
 Mones, A. H., and E. Banks, cation substitutions in BaFe₁O₁, 540; ferrimagnetism in system Na₁O-ZnO-Fe₂O₂, 904
 Monfils, A., with C. Hérinckz, determination of thermal parameters of semiconducting thermoelements, 3348
 Monk, J., 3:8-mm-wavelength pulsed magnetron.
- Monk, A. J., 3 8-mm-wavelength pulsed magnetron, 2788 h
- Monod-Herzen, G., and Nguyen Chung-Tu, luminescent complexes of Cdl₂ and Pbl₂, 149 Montalbetti, R., H₂ emissions in aurorae and air-
- glow, 3310 Montalenti, G., with others, instability of Bloch walls in ferromagnetic material, 535 Monteath, G. D., reciprocity in r.f. measurements,
- Montgomery, G. F., diode reactance modulator, 2187
- Monti-Guarnieri, G., transappennine radio link,
- Monti-Guarnieri, G., transappendiate
 2014 a
 Moody, N. F., with others, lightweight airborne navigation system, 2599
 Mook, C. P., meteorological study of whistlers, 3719
 Moon, P., and D. E. Spencer, solution of integral equations, 209
 Moorcroft, G. J., precision approach radar, 2259 m
 Moorcroft, G. J., precision approach radar, section of the sect
- Moorer, G. J., precision approach radar, 2439 m
 Moore, A. R., with J. O. Kessler, magnetic susceptibility of carriers in Ge, 2300
 Moore, C. B., with others, organized electrification and precipitation in thunderstorms, 2253; wind determinations in upper atmosphere, 3302
 Moore, E. F., with E. N. Gilbert, variable-length binary encodings, 3467
- Moore, E. J., galvanomagnetic, thermomagnetic and thermoelectric effects, 161
 Moore, G. E., dissociation of SrO by electron impact, 3892
 Moore, R. C., A. Hopengarten and P. G. Wolfe,
- re, R. C., A. Hopengarten and P. G. Wolfe, colour purity adjustment for 'apple' c.r. tube, 1386

- Mosser, E., and W. B. Pearson, structure and properties of group VB to VIIB elements, 1226
 Morcan, M. J., with T. Gray, Decca Doppler, 820
 Morcom, W. J., linear-amplifier transmitters, 291
 Morehead, F. F., Jr, electron traps and electro-luminescence brightness, 1214
 Morehouse, C. K., and R. Glicksman, dry cells with C-nitroso compounds, 2402; Mg-BiO dry cells, 3865 3865
- Morgan, K. C., with B. Harris, binary symmetric decision feedback systems, 591
- with others, binary communication feedback systems, 2387 gan, M. G., correlation of whistlers and with

- systems, 2387
 Morgan, M. G., correlation of whistlers and lightning flashes, 458 *H. W. Curtis and W. C. Johnson*, path combina-tions in whistler echoes, 1577 *with G. McK. Alleock*, solar activity and whistler dispersion, 144 *with R. A. Helliwell*, atmospheric whistlers, 1576
 Morgan, S. P., solution of Luneberg lens problem, 24
 Morgenthaler, F. R., velocity modulation of e.m. waves, 2207; radiation from ferri-magnetically compled electrons in transient magnetic fields, 4026 magneticativ complea electrons in transient magnetic fields, 4026Mori, T., with others, Fg-layer multiple reflections, 1342
- 1342 Moriarty, T. H., resonant-ring diplexing in forward scatter, 3196 Moriguchi, Y., Se rectifiers with artificial layers,
- Moriguchi, Y., Se rectifiers with artificial layers, 3111
 Morin, F. J., oxides showing metal/insulator transition, 3756
 Morita, K., and K. Kakita, fading in microwave relays, 3475
 Morita, T., Bose-Einstein lattice gases equivalent to Heisenberg model, 2913
 with others, voltage breakdown characteristics of microwave antennas, 3581
 Morleigh, S., ferroelectric storage devices, 717; sensing system for punched cards, 1455
 Morozov, A. I., with others, influence of group III and V elements on recombination in Ge, 1614
 Morozov, Yu. A., with others, secondary emission

- and V elements on recombination in Ge, 1614
 Morozov, Yu. A., with others, secondary emission from Ni, 3789
 Morrell, A. M., with others, 21-in glass colour picture tube, 280
 Morris, A. L., microwave ferrite modulators, 1825
 Morris, D. P., R. R. Preston and I. Williams, search for new Heusler alloys, 1950
 Morris, D. W., and C. J. Hughes, phase characteristics of radio signals, 2384
 E. W. Thurlow and W. N. Genna, microwave model for study of s.w. aerials, 709
 Morris, R. J., R. L. Khyl and M. W. P. Strandberg, maser amplifier with large bandwidth, 1144
 with A. E. Siegman, 'staircase' maser, 2522

- Morrison, J. A., with others, heat capacity of pure Si and Ge, 3353
 Morrison, S. R., slow capture of holes and electrous by surface states, 3352
 Morten, F. D., with A. H. Benny, measurement of surface recombination velocity on Si, 859
 Mortimer, G., Bi as a donor-type impurity in Ge, 4105
- 4105

- Mortimer, G., Bi as a donor-type impurity in Ge, 4105
 Morton, G. A., infrared photoemission, 4010 d
 and S. V. Forgue, infrared pickup tube, 4242
 Morton, J. Y., artificial ear for insert earphones, 3
 Moses, H. E., solution of Maxwell's equations, 2900
 Moss, T. S., and A. K. Walton, effective electron mass in GaAs, 4113
 with A. K. Walton, magneto-photoelectric theory for three carriers, 1923; photoelectromagnetic effect in Ge, 2660; free-carrier Faraday effect in *n*-type Ge, 3375
 Motherbacher, C. D., with others, impurity compensation and magnetoresistance in Si, 2293
 Mothersole, P. L., video amplifier using PCL 84, 379
- 379
- Motifiers of e. 1. E., viteo amplifier using 102 of, 379
 with M. C. Ganler, frame multivibrator and diode separator, 3499; multi-triode flywheel synchronizing circuit, 3500
 Motzke, K., influence of magnetic annealing on perminvar rings, 3396
 Mourier, G., surface waves in electron beams, 2786
 Mowery, V. O., surface conductivity changes and space charge in Ge and Si, 858
 with M. Nesenbergs, logic synthesis of digital comparators, 1456
 Mozumder, A., evaluating aerial performance, 1087
 Mozumder, A., evaluating aerial performance, 1087

Mozumder, A., energy states of one-dimensional crystal, 1174

crystal, 1174
Muchmore, R. B., with others, aperture-to-medium coupling on line-of-sight paths, 4183
Mueller, C. W., and J. Hilibrand, 'thyristor' switching transistor, 1005
Mueller, R. K., grain boundaries, transient response of, 3788, capacitance and barrier heizht in, 3339 — and R. L. Jacobson, grain-boundary photovoltaic cell, 1723
Mühe, W., with H. G. Diestel, reciprocity method for vibration measurements, 3178
Mühlorf, E., tornary switching algebra. 1636:

Mühldorf, E., ternary switching algebra, 1636; circuits for ternary switching variables, 1789
 Mulders, C. E., nonlinear properties of carbon resistors, 41
 Muldrew, D., with others, spiral occurrence of E_s, 3304

Müller, E. W., with R. D. Young, energy distribution of field-emitted electrons, 2198
 Müller, K. A., electron paramagnetic resonance of Mn IV in SrTiO₃, 2633

Mn IV in STIO₃, 2633
 with others, hyperfine splitting in paramagnetic resonance of Pt³⁺ in ceramic LaAlO₃, 758 f
 Müller, K. E., radiation characteristics of open waveguides, 3959
 Muller, M. W., with J. C. Helmer, noise figure of maser amplifier, 2343
 Müller, R., with R. Liebscher, frequency noise in travelling-wave tubes, 3159 dd

uaveining: wave (noise, 5157 az)
 Mullett, L. B., with others, miniature nuclear generator, 2757
 Mumford, H., television transmission over long-distance cable links, 4210
 with E. J. Osborne, Laguerre-function equalizer, 1881

von Münch, W., transistor with thyratron char-acteristics, 1006; theory of switching transistor, 1401

2777
Mungall, A. G., dielectric properties of low-loss materials at mm λ, 2348
Munro, G. H., diurnal lapse of signals from Sputnik III, 2954
and L. H. Heisler, recording signals from earth satellites, 2573
with R. R. Long, radio signals from first earth satellite, 444
Murach, N. N., high-purity metals and semiconductors, 486
Murakami, T., and R. W. Somenfeldt, detection of

conductors, 486 B. Purify inclusion and configuration of asymmetric-sideband signals in presence of noise, 248
 Murakami, T., and R. W. Sommenfeldt, detection of asymmetric-sideband signals in presence of noise, 248
 Murphy, A., with J. R. Wait, influence of ridge on 1.6 ground wave, 233
 Murphy, B. T., method of focusing electron beams. 3524 men
 Murphy, E. B., electroforming of electronic components, 4143
 Murphy, R. E., and R. S. Mauther, transistorized

n-p Ge diffused junctions, 3378 Murphy, R. E., and R. S. Mautner, transistorized i.f.-strip design, 70 Murphy, S. R., G. R. Garrison and D. S. Potter, sound absorption at 50 to 500 kc/s, 2082 Murray, A. M., with C. Strachan, spin-orbit coupling and extraordinary Hall effect, 1952 Murray, C. A., error in determination of ΔT , 4147

Murray, C. T., and R. E. Aitchison, high-stability valve heater supply, 1697 Murray, R. P., transistor RC amplifiers, 1816

Murray, R. P., transistor RC amplifiers, 1816
Murrmann, H., with C. Schwink, field superposition for electron-optical shadow method, 3441
Murty, D. S., with B. R. Rao, c.w. method for study of drifts, 3699 vit
Murty, Y. V. R., with others, effect of magnetic activity on F₄ drifts, 2586
Murzin, V. S., with others, mechanism of terrestrial corpuscular radiation, 2216
Musai, H. M., with G. I. Cohn, transient response of phosphors, 1211

1.21

and H. Salow, storing and switching transistor, 2777

1481

Müser, H. A., with R. Gereth, test equipment for photosensitive semiconductors, 4078
Müser, H. E., ferroelectric hysteresis in Rochelle salt, 3008
and H. Flunkert, upper Curie temperature and domain structure in Rochelle salt, 1218
Muss, D. R., and R. F. Greene, reverse breakdown in In-Ge alloy junctions, 534
Musson-Genon, R. P., and C. Audoin, electronic hysteresis and secondary emission in reflex klystrons, 3524 gg
Myasnikov, V. A., with V. N. Bogomolov, equipment for Hall-effect measurements in semiconductors, 503

ment for Hall-Effect measurements in semi-conductors, 503
 Myers, A., L. Mackinnon and F. E. Hoare, pulse techniques, 2449
 Myers, J., with others, effect of pressure on Hall-coefficient reversal in Te, 1237; impurity com-pensation and magnetoresistance in Si, 2293

Nag, B. R., ultraharmonic and subharmonic resonance, 3611; study of oscillator by differential analyser, 3980
 Nagaraja, N. S., Fourier analysis by electronic analogue computer, 33
 Nagata, T., with N. Matuwa, turbulence in upper atmosphere, 2577
 Nail C. D. failing of dielectrice, 2336

- atmosphere, 2577
 Nail, C. D., failing of dielectrics, 2336
 Nair, K. K., with M. N. Srikamaswamy, matrix analysis of valve circuits, 2497
 Nakagawa, E., with others, effect of solar eclipse on geomagnetic field, 2561
 Nakajima, S., with others, magnetrons for mm-λ, 4248

on geomagnetic field, 2561
Nakajima, S., with others, magnetrons for mm-λ, 4248
Nakamura, T., indirect coupling of nuclear spins in antiferromagnet, 3036
Nakata, Y., auroral echoes in ionogram, 457
Nall, J. R., with others, D.O.F.L. microelectronics program, 2484
Nalos, E. J., hybrid-type travelling-wave tube for pulsed amplification, 1733
Nalot, J., and R. Visocekas, anomalous behaviour in M-type carcinotron, 2788 t
Naresky, J. J., numerical approach to electronic reliability, 2804
Narud, J. A., and M. R. Aaron, transistor blocking oscillator, 2504
Nasmyth, P. W., with others, geographical variations in geomagnetic micropulsations, 2946
Nasugle, A. B., with others, measurement and interpretation of photodetector parameters, 4240
Naugol, A. B., with others, measurement and interpretation of photodetector parameters, 4240
Naugol, M. W. H. Campbell, micropulsation measurements, 4045
Needle, J. S., with P. S. Castro, beam-defocusing microwave detector, 1413
Nedel, L., effect of coupling between grains of ferromagnetic material, 203; coupling between elementary ferromagnetic domains, 546; random creep and thermal fluctuation fields, 4024
Negnevitskil, I. B., with R. A. A. Lipman, theory of half-wave magnetic amplifier, 1495
Neher, H. V., change of cosmic rays in space, 4036
Neighbours, J. R., with others, field effect and surface recombination in Ge, 12928

- in Ni, 4125
 Neizvestnyl, I. G., with others, field effect and surface recombination in Ge, 1928
 Nelkowski, H., with others, cathodo-electro-luminescence phenomena in ZnS phosphors, 834
 Nelson, C. E., with W. L. Whirry, microwave cavity filters, 2467
 Nelson, C. F., with others, extended-range dis-tributed amplifier design, 1492
 Nelson, H., surface-immune transistor structure, 4230
 Neprimerov, N. N., with others, magnetic double

42.50 Neprimerov, N. N., with others, magnetic double refraction of microwaves, 776 Nergaard, L. S., nonlinear-capacitance amplifiers, 1820

- with others, magnetic annealing in perminvar, 3797
 Nesenbergs, M., and V. O. Mowery, logic synthesis of digital comparators, 1456
 Nethercor, A. H., Jr, with F. M. Johnson, antiferromagnetic resonance in MnF₄, 3791
 Netzband, R., with others, r.f. protection ratios for v.h.f. f.m., 1348
 Neu, H., extension of Townsend's formula, 2200
 Neuffeld, E. L., with J. S. Greenhow, turbulence measurements in upper atmosphere, 4058
 with others, radar observations, of 1957B, 3290
 Neuffscher, H., with W. Klein, travelling-wave tubes for 4 and 6-Gc/s bands, 2788 b
 Neugebauer, H. E. J., with others, effect of mountains with smooth crests on wave propagation, 3458
 Neumauser, R. G., sensitivity of television camera tubes, 4215
 Neumann, L., transistorized generator for pulse circuit design, 2161
 Neuringer, L. J., effect of pressure on infrared absorption, 3014
 Newall, L. M., with K. Holford, video amplifiers using transistors, 385

- Newby, J. R., with others, travelling-wave multiple-beam klystron, 3524 z
 Newell, A. F., design of logical circuits, 351; use of transistors in inductive circuits, 722
 Newhouse, V. L., N. R. Kornfield and M. M. Kawfman, end-fired memory, 36
 Newman, R., optical properties of n-type InP, 883
 Newman, R. C., with others, diffusion across semi-conductor/vapour interface, 165; precipitation on a dislocation, 2289
 Newton, C. E., and G. M. C. Stone, I.G.Y. v.h.f. programme, 115
 Newton, R. H. C., magnetic oscillations in electron beams, 3159 i
 Newton, R. R., motion of satellite around unsym-metrical central body, 1541
 Ney, E. P., J. R. Winckler and P. S. Freier, protons from sun 12th May 1959, 4040
 with P. J. Kellogg, new theory of solar corona, 2943
 with others, geophysical effects associated with

- 2943
 with others, geophysical effects associated with high-altitude explosions, 2575; cosnic-ray a particles during solar maximum, 3279
 Nguyen Chung-Tu, with G. Monod-Herzen, luminescent complexes of CdI₃ ard Pbl₂, 149
 Nguyen Van Dang, creep of asymmetric hysteresis cycles, 204, 547, 1294
 N'guyen, Van Dong. See Van Dong, N.
 Nichols, B., auroral ionization and magnetic disturbances, 1570
 Nichols, J. W., A. C. MacKellar and A. J. B. Baty, electronic clock coder for coded radio beacons, 4069
- 4069

- 4069
 Nicholson, S. B., and O. R. Wulf, diurnal variation of geomagnetic fluctuations, 1533
 Nicolet, M., constitution of upper atmosphere, 1551; atomic nitrogen in thermosphere, 3699 d
 Nicolet, M. A., equivalent circuit of junction transistors, 2770

- Nicolet, M. A., equivalent circuit of junction transistors, 2770
 with others, influence and creation of lattice defects in junction transistors, 2771
 Nielsen, C. E., and A. M. Sessler, space-charge effects in particle accelerators, 1984
 Nielson, J. W., and E. F. Dearborn, growth of single crystals of magnetic garnets, 1289
 with J. F. Dillon, Jr, effect of impurities on resonance in Y-Fe garnet, 3811
 Nienhuis, W. F., with F. de Boer, low-voltage oscilloscope tubes, 2713
 Niese, H., testing 'echo parameter' criterion, 685; loudness of rhythmic sounds, 1426; proposal for loudness meter, 1427; sensation of loudness of rhythmic sounds, 1426; proposal for loudness meter, 1427; sensation of loudness, or power klystrons, 312
 Niesen, E., R. W. Beatly and W. J. Anson, water cooling of low-power klystrons, 312
 Niessen, K. F., non-magnetic ions in antiferromagnetic, 189; distribution of magnetic domains between two phases in Fe, 3038
 Nifontoff, N., with L. Gowskov, chemical action and oxidation of oriented Ge surfaces, 3370
 with M. Teboul, flicker effect in photovoltaic diodes, 639
 Nightingale, A., sensitivity of 1.f. amplifiers for electromyography, 230
 Niklas, W. F., averator costiloscope tube with travelling-wave deflection, 927

- tubes, 1704
 and J. Wimpffen, oscilloscope tube with travelling-wave deflection, 927
 with W. O. Reed, shutter image converter tube for multiple-frame photography, 2369
 Nikol'skii, V. V., phase shifts of gyrotropic inhomogeneities in waveguide, 2115
 Ninomiya, Y., N. Miyamcio and A. Yanagi, 4-kMc/s-band v.s.w.r. scanner, 1975
 with others, estimate of transistor life in satellites, 2776

- 1011h 2780
- 2780
 Nishikori, K., A. Takahira and H. Irie, microwave propagation over sea beyond line of sight, 2734
 Nishimaki, M., and T. Asaba, discharge machining for min-wave magnetrons, 3159 e
 Nishizaki, R., with others, F₂-layer multiple reflections, 1342
 Niwa, S., with others, long-distance u.s.w. propagation, 244

tion, 244
Nixon, J. D., and P. C. Banbury, changes in excess-carrier concentrations, 1228
Noda, K., and others, waveguide for low-loss trans-mission, 2829
Noggle, T. S., and J. O. Stiegler, electron-microscope studies on etching of irradiated Ge, 4089 q
Noland, J. A., and L. D. Cohen, BWO uses ridge-loaded ladder circuit, 2790
Nomura, K. C., and J. S. Blakemore, decay of excess carriers in semiconductors, 1915
Nomura, S., with others. thermal conductivity of

- Nomura, S., with others, thermal conductivity of BaTiO₃ ceramics, 2628 Nomura, Y., and others, F₂-layer multiple reflections, 1342
- Nonweller, T., effect of solar flares on satellite 1957 β , 449 Norman, F., line and properties of strip junction, 2828

- 2828
 Norman, F. H., with others, thermionic energy converter, 325
 Norquist, R. G., testing high-speed computer circuits, 3585
 North, J. H., with others, multipurpose bias device of logical elements, 1461
 Northwood, T. D., and E. J. Stevens, acoustical design of Alberta Jubilee Auditoria, 688
 Norton, K. A., system loss in radiowave propagation, 4174
- Norton, K. A., system loss in radiowave propagation, 4174
 Norton, L. E., spontaneous microwave emission by pulsed resonance excitation, 1165
 Nottingham, W. B., diode as heat-to-electrical-power transducer, 2434
 G. N. Halsopoulos and J. Kaye, diode thermo-electron engine, (D)2435

World Radio History

- Novikova, Z. I., with L. I. Rabkin, design of coils with ferrite cores for a.f., 1790
 Novototskil-Vlasov, Yu. F., with others, field effect and surface recombination in Ge, 1928
 Nowell, J. C., with others, measurement of time dilation in earth satellite, 3688
 Nowicki, J. R., 4-W 500-kc/s transistor transmitter, 3504
 Nozières, P., and D. Pines, dielectric formulation of many-body problem, 1830; electron interaction in solids, 2931
 Nupp, W. D., critical analysis of communication systems derived from amplitude modulation, 2752

- syst. 2752

Nusbaum, A., J. Myers and D. Long, effect of pressure on Hall-coefficient reversal in Te, 1237 Nye D. D., Jr, low-pass *RC* filter, 51

- Obayashi, T., anomalous changes in ionosphere related to magnetic storm, 134; F, layer deduced from 'frequency spectrum' of Q figures, 135; v.l.f. spectra of atmospherics, 3313; geonag-netic pulsations and earth's outer atmosphere, 3673 Itom requericy spectrum of Q figures, 135;
 v.I.f. spectra of atmospherics, 313; geonagnetic pulsations and earth's outer atmosphere, 3673
 S. C. Coroniti and E. T. Pierce, geophysical effects of high-altitude nuclear explosions, 2969
 S. Fujii and T. Kidokoro, proof of mode theory of v.I.f. ionospheric propagation, 3094
 Oberheitinger, F., diffraction by wedges and corners, 1167
 Oberländer, S., with others, evaluation of conductivity glow curves, 3321
 Oberländer, S., with others, evaluation of conductivity glow curves, 3321
 Oberländer, S., with others, evaluation of conductivity glow curves, 3321
 Oberländer, R. J., energy spectrum of particles bombarding earth, 419
 O'Brien, R. M., with P. D. Lomer, microwave pulsed attenuator, 2800 b; high-power microwave duplexer, 2833
 Oetrell, J. H., and T. M. Scott, measurement of transistor characteristics in 3-250-Mc/s range, 1304
 Oetrl, G., secondary emission of Se, 3762
 Offregeld, G., and J. van Cakenberghe, stoichiometry of Bil'Te₂, 3785
 Ogawa, T., frequency variations in s.w. propagation, 916
 Oglubile, R., M. W. and Chers, radiation observations with satellite 1958 8, 4042
 Oguchil, B., and K. Yamaguchi, centre-excited mode transducer, 2831

and others, parametric amplifier using Ge diode,

1149

devic 2182

and others, parametric amplifier using Ge diode, 1149
 Oguchi, T., with others, measurement of attenuation by rain, 4187
 O'Hara, F. J., and H. Scharfman, ferrite serrodyne for microwave frequency translation, 3942
 Ohnsorge, H., with others, mechanical filters for communications technique, 2155
 Okada, J., recombination centres in Ge, 516
 Okajima, T., with others, parametric amplifier using Ge diode, 1149; transmitting frequency con-verter, 3145
 Okamoto, S., and K. Takeuchi, dielectric loss of oxidized high-density polyethylene, 3414
 Okamura, S., and others, double-vane torque-operated wattmeter for 7 kMc/s, 223; measure-ment of attenuation by rain, 4187
 with others, torque-operated wattmeters for 3 cm λ, 2359
 Okaya, Y., with others, (NH₄)₂SO₄ and (NH₄)₂BeF₄ transitions, 836; ferroelectricity in Li(N₂H₄)₃SO₄. 840; (NH₄)HSO₄ ferroelectric with low coercive field, 841
 Okazaki, A., crystal structure of GeSe, 876

840: (NH, HSO, ferroelcctric with low coercive field, 841
Okazaki, A., crystal structure of GeSe, 876
with S. Asanabe, Hall coefficients of SnSe and GeSe, 2669
O'Keefe, J. A., A. Eckels and R. K. Squires, Vanguard measurements of earth's figure, 2236
Okhotsimskil, D. E., and T. M. Eneeu, variational problems of satellite launching, 3680
T. M. Eneeu and G. P. Taratynova, determination of lifetime of artificial earth satellite, 3681
Otsman, A. K., interference in television channel of coaxial cable, 611
Okwit, S., with F. R. Arams, tunable L-band ruby maser, 2523
Olimer, A. A., and W. Rotman, periodic structures in trough waveguide, 3934
with W. Rotman, asymmetrical trough-waveguide antennas, 3960
Oliver, B. M., gamma-derived capacitor, 3973
Oliendorff, F., wave-mechanics correction of emission formula, 2912
Olson, F. A., C. P. Wang and G. Wade, parametric devices tested for phase-distortionless limiting, 2182
Olson, H. F., and J. Preston, e.s. uniangular micro-

Olson, H. F., and J. Preston, e.s. uniangular microphone, 1432
O'Meara, T. R., single-crystal wide-band filters, 1120; characteristics of four-crystal lattice filter, 1121
and R. L. Sydnor, balun transformer for v.h.f. and u.h.f., 338
OmelYyanovskaya, N. M., with others, lifetime of injected current carriers in Sb-doped Ge, 1932
O'Neill, G. D., mu of receiving tubes, 3170
O'Neill, G. D., nu of receiving tubes, 3170
O'Neill, J. J., and J. J. Dreher, word masking by prolonged vowel sounds, 680
Onoe, M., M. Hirai and S. Niwa, long-distance u.s.w. propagation, 244
Oranovskii, V. E., electroluminescence, 1909
Orbach, R., and P. Pincus, excitation of spin waves in antiferromagnet, 2925
Ordung, P. F., with others, functional characteristics of node determinant, 548

Electronic & Radio Engineer

Olson, H. F., and J. Preston, e.s. uniangular micro-

Ortloff, M., radio-telephone suppression equipment, 4193 Ortner, J., with B. Hultqvist, ionization below 50 km

- Ortner, J., with B. Hultqvist, ionization below 50 km after strong solar flares, 2576
 Orton, J. W., with J. H. E. Griffiths, weak lines in paramagnetic resonance spectrum of impure MgO, 3410
 Osborne, E. J., and H. Mumford, Laguerrefunction equalizer, 1481
 Osborne, W. E., receiver for space vehicles, 4197
 Oshima, H., with others, effect of solar eclipse on geomagnetic field, 2562
 Oshima, K., with P. R. Gillette, pulser design for magnetron operation, 648
 with others, Mcasurement of pulse front response of transformers, 357
 Oslal, T. A., with R. D. Haum, Jr, gain measurements on pulsed ferromagnetic microwave amplifier, 2184
 Oskam, H. J., microwave investigation of dis-
- 2184
 Oskam, H. J., microwave investigation of disintegrating plasmas, 2203
 Osterberg, H., propagation of e.n. wave in inhomogeneous media, 771
 Ostroborodova, V. V., with others, properties of Ge doped with Zn, 1613
 Oswald, H., and H. Straubel, photoelectric amplifier, 1405
- 1405
- 1405
 Oswald, J., branched filters, 2151
 Otley, K. O., P. J. Shoemaker and P. J. Franklin, voltage-sensitive switch, 39
 Otpushchennikov, N. F., velocity of ultrasound in water 2811
- Orpusachennikov, N. F., velocity of ultrasound in water, 2811
 Ottavi, H., with others, maser-type self-oscillator, 2521; weak-field maser, 2548
 Outten, A. E., with others, application of radio altimeters to aircraft approach, 2259 o
 Ovcharov, V. T., theory of formation of electron beams, 2059
- Overney er, J., with others, microwave resonance in Gd-Fe garnet crystals, 3043 Overton, B. R., transistors in television receivers, 987
- Oxenius, J., Hall generators in analogue multipliers, 2131
- 2131
 Packard, K. S., optimum dimensions for strip transmission line, 1072; cut-off wavelength of trough waveguide, 3554
 Packard, R. H., and M. G. Schorr, power supply for video circuits, 602
 Paetzold, H. K., and H. Zschörner, radio observations at 20 Mc/s of first Russian earth satellites, 2237; density of outer atmosphere from satellite observations. 3695
 Pafomov, V. E., with others, Cherenkov radiation in medium with spatial dispersion, 3648
 Page, C. H., harmonic generation with ideal rectifiers, 60
 Page, E. G. S., electron temperature in electric fields applied to Ge, 518
 with A. F. Gibson, transport properties in dislocated Ge, 1619
 with others, minority carriers in dislocated Ge, 1619

- with others, minority carriers in dislocated Ge, 1618
- with others, minority carriers in dislocated Ge, 1618
 Fajak, Z., and J. Stankowski, polarization changes during aging of BaTiO₂-type ferroelectrics, 844
 Palevsky, H., and others, lattice vibrations in Si by neutron scattering, 2291
 with others, lattice vibrations in Ge by neutron scattering, 2304
 Pallett, J. E., parametric amplification, (C)2897
 Palluel, P., and J. Arnaud, results on delay lines for travelling-wave tubes, 3159 s
 Palma, M. U., with M. B. Palma-Vitorelli, microwave spectrometer, 96
 Palmer, J. L., with others, design of transition region of beam valves, 1017
 Palmer, W. F., peak flyback voltage in horizontal deflection circuits, 4220
 and C. Schiess, transistorized vertical deflection systems, 1381
 Palmisano, R. R., and A. Sherman, waveguide coils make compact delay lines, 339
 Palmiter, R. B., digital system positions shaft over phone line, 1656
 Pankel, R. H., power relation for nonlinear resistive elements, 729; backward-wave oscillations in

- phone line, 1656
 Pankove, J. I., radiative surface effect in Ge, 523
 Pantell, R. H., power relation for nonlinear resistive elements, 729; backward-wave oscillations in unloaded waveguide, 3164 *P. D. Coleman and R. C. Becker*, slow-wave structures for power generation at min and submm λ, 1743
 Paolini, E., response of loudspeaker near principal resonance, 1433
 Papenhuijzen, P. J., transmitting triode for frequencies up to 900 Mc/s, 2797
 Papoulis, A., strongly nonlinear oscillations, 80
 Pape, with others, vacuum-diode microwave detection, 2794
 Pargamanik, L. E., and M. Ya. Mints, diffusion theory of magnetron, 645
 with V. P. Galatko, correlation for particles carrying like charges, 1829
 Paris, J. M., with others, circular waveguides for long-distance transmission, 2107
 Parker, A. B., new form of X-band pre-t.r. cell, 2800 a

- 2800 a
 Parker, E. N., inadequacy of ring-current theory for main phase of geomagnetic storm, 1536; auroral phenomena, 1568
 Parker, M. J., with others, electronic subsystem development problems in naval ordnance, 2803
 Parker, R., resistivity of compounds with ordered spin arrangements, 1220
 and M. S. Smith, dispersion phenomena in inhomogeneous dielectrics, 837
 Parker B. L. permagnet magnets in audio devices
- Parker, R. J., permanent magnets in audio devices, 1760
- Electronic & Radio Engineer

- Parkyn, D. G., atmospheric tides and earth satellite observations, 2565
 Parmenter, R. H., acoustoelectric effect, 2189
 Parcodi, O., with others, light due to recombination of impurities in Ge, 3369
 Parravano, G., with others, magnetic properties of (Ni,Li)O, 3799
 Parry, C. A., over-horizon links in telecommunication networks, 600; C.C.I.T.T. recommendations for multichannel relays, 4199
 Parry, J. V. L., with others, comparison of Cs frequency standards, 212; circuits in N.P.L. Cs standard, 2340
 Parsons, N. R., with K. G. McCracken, unusual cosmic-ray intensity fluctuations, 1860
 Parsons, R., and G. Finn, Si and rectifier design, 604
 Parthasrathy R., and R. N. De Witt, auroralionosphere studies using earth satellites, 4052
 with G. Swarup, solar brightness distribution at 60 cm, 430
 Parthasrathy, S., acoustics research at N.P.L. of India 3177

- 60 cm, 430
 Parthasarathy, S., acoustics research at N.P.L. of India, 3177
 and C. B. Tipnis, diffraction of light by ultra-sonic waves, 1049, 1751
 Parzen, P., with others, propagation in crossed-field periodic structure, 1731
 Paschke, F., dispersion of interdigital delay lines, 1022; generation of second harmonic in v.m. electron beam, 1409; propagation of perturba-tions along magnetically focused electron beams, 4246
- 2440
 Patlach, A. M., with others, transistorized crystal-controlled marginal oscillator, 1805
 Patrick, L., and W. J. Choyke, SiC p-n junctions, electron emission from breakdown regions in, 1610, impurity bands and electroluminescence in 1910
- 1610, impurity bands and electroluminescence in, 1910
 Pattenden, J. D., with E. A. Ash, modified trans-mission-line couplers for helices, 3159 y
 Pattenson, C. F., with others, Canadian standard of frequency, 2700
 Paul, A., with others, variation of ionospheric absorption, 3716
 Paul, D. I., scattering in beyond-horizon trans-mission, 1663
 Paul, R. J., onset of oscillations in transistor oscillators, 1809
 Paul, B. J. A., and M. H. McEadden, measurement

- Paul, R. J. A., and M. H. McFadden, measurement of phase and amplitude at 1.f., 1651
 Paul, W., and D. M. Warschauer, optical properties of semiconductors under hydrostatic pressure, 506

- and the series of the series of

- Ge, 3362
 Pearson, J. D., and H. S. Cockroft, 20-kW pulsed travelling-wave tube, 2788 l
 Pearson, W. B., with E. Mooser, structure ard properties of group VB to VIIB elements, 1226
 Peart, R. F., T. B. Rymer and D. H. Tomlin, Ge junction cells for photoelectric control circuits, 309
 Pease M. C. Structure T. Structure
- Pease, M. C., with R. H. Bartram, space-charge-limited crossed-field gun, 3894
 Pease, R. L., propagation of surface waves over ferrite slab, 1435

- ferrite slab, 1435
 Pech, H., ground resistivity measurements, 3420
 Pechhold, W., excitation problems in acoustic resonators, 3907
 Pedowitz, R. P., with others, automatic failure recovery in data processing system, 1453
 Peeler, G. D. M., and H. P. Coleman, stepped-index Luneberg lenses, 2854
 Pekar, S. I., e.m. waves in crystal with excitons, 409
 Pelah, I., with others, lattice vibrations in Ge by neutron scattering, 2304
 Peless, Y., response of cascaded double-tuned circuits, 1815
 Penfold, A. S., linear amplifier for the state of the state of
- circuits, 1815
 Penfold, A. S., linear amplifier for negative pulses, 62
 Pengelly, P., with F. Rosner, transistors and cores in counting circuits, 2479
 Penhall, B. W. G., and J. D. Thomson, signalling for single-channel and mobile radio-telephone systems, 4200
 Penndorf, R., and S. C. Coroniti, polar E₄, 1561
 with S. C. Coroniti, f₀F₂ over polar regions, 1882
 Penning, P., generation of dislocations by thermal stresses, 3028
 Pensak, L., with B. Goldstein, high-voltage photovoltaic effect, 1907
 with others, pulse amplification using impact

- with others, pulse amplification using impact ionization in Ge, 2882

World Radio History

- Pentecost, J. L., and P. E. Ritt, lightweight ceramic materials, 839
 Pentz, M. J., with others, source-modulated micro-wave cavity spectrometer, 416
 Pepinsky, R., and K. Vedam, room-temperature ferroelectric, 4084
 and others, ferroelectricity in Li(N₂H₆) SO₄, 840; (NH₄)HSO₄ ferroelectric with low coercive field, 841
- with others, (NH4)2 SO4 and (NH4)2BeF4 transi-
- with others, (NH₄)₂ SO₄ and (NH₄)₂BeF₄ transitions, 836
 Perakis, N., J. Wucher and G. Parravano, magnetic properties of (Ni,Li)O, 3799
 Perdijk, H. J. R., with J. J. B. Fransen, Ba getter films, 2613
 Perell, J., stabilization by Zener diodes, 271
 Perking, A. F., with others, transistorized compandor, 2395
 Perking, A. F., with others, transistorized compandor, 2395

- Perkins, J., Stabilization by Zeiler uloues, 271
 Perkins, A. F., with others, transistorized compandor, 2395
 Perkins, J. C., Jr, D. A. Perreault and A. F. Perkins, transistorized compandor, 2395
 Perkins, R. W., with D. McDonnell, interpolation and prediction of signals plus noise, 2391
 Perkins, W. H., with others, night-time reception of major solar burst, 2554
 Perkins, W. J., with D. C. Gold, electroencephalograph telemeter system, 3085
 Perist, T. A., T. J. Diesel and W. J. Dobrov, primary pyroelectricity in BaTiO, ceramics, 156
 Pernett, J. M., with others, measurement and interpretation of photodetector parameters, 4240
 Peroni, B., and G. Bianconi, tropospheric-scatter multichannel telephone links, 1361
 Perreaut, D. A., with others, transistorized compandor, 2395
 Perrier, F., and L. d'Ast, rapid testing of direct-voltage stabilizers, 608
 Perry, V. G., maintenance of television studio equipment, 622
 Persham, P. S., with others, cross-relaxation in spin systems, 3270
 Pescetti, D., with G. Biorci, behaviour of ferromagnetic materials, 197
 Peter, M., mm-wave paramagnetic resonance spectrum of MgWO, 2691

Pescetti, D., with G. Biorci, behaviour of ferromagnetic materials, 197
Peter, M., mm-wave paramagnetic resonance spectrum of MgWO, 2691
and M. W. P. Strandberg, efficiency of frequency measurements with atomic clock, 1311
with J. C. Hensel, Stark effect for cyclotron resonance, 3346
with others, paramagnetic-resonance spectrum of Cr³⁺ in emerald, 1628
Peter, R. W., with A. L. Eichenbaum, exponential gun, 2064
Peters, J. M., elements of electronic circuits, 1795, 2138, 2494, 3221, 3600
Peters, M., therey of helical aerials, 3570
Petersen, R. G., with D. T. Edmonds, effective exchange constant in Y-Fe garnet, 3401
Peterson, A. M., R. D. Egan and D. S. Pratt, 3-frequency back-scatter sounder, 1665
with R. L. Leadabrand, radio echoes from auroral ionization, 1670

auroral ionization, 1670
 with others, radar investigations of auroral echoes, 4065
 Peterson, D. W., vertical polarization to solve 'ghosting' problems, 289; tests of u.h.f. television broadcasting aerials, 1088
 Peterson, G. E., W. S. Wang and E. Sivertsen, segmentation techniques in speech synthesis, 1059
 with W. S. Wang apprention for groups

1059
 with W. S. Wang, segment inventory for speech synthesis, 1060
 Peterson, L., and J. R. Winckler, y-ray burst from solar flare, 104
 R. L. Howard and J. E. Winckler, balloon gear monitors cosmic radiation, 437
 with others, auroral phenomena during storm, 3309

3309
 Petritz, R. L., fundamentals of infrared detectors, 4010 c
 with G. R. Pruett, detectivity and preamplifier considerations for InSb photovoltaic detectors, 4241

considerations for inso photovoltale detectors, 4241
Pettengill, G. H., with others, radar echoes from Venus, 2556
Pettit, G. D., with S. P. Keller, phosphor with fluorescence larger than energy gap, 2623
Pettit, H. B., with others, wind determinations in upper atmosphere, 3302
Petukhov, V. A., possible mechanism of nonstable solar processes, 3666
Petzold, W., with H. J. Kopp, linearization of multipliers at high anode currents, 2054
Peyser, W. P., with V. J. Albanese, analysis of a broad-band coaxial hybrid ring, 3552
Pfann, W. G., K. E. Benson and D. W. Hagelbarger, improvenent in floating-zone technique, 2337
Pfund, E. T., Jr, and others, capabilities of coaxial cable, 2457
Pham Mau Quan. See Quan, Pham Mau.

Pfund, E. T., Jr, and others, capabilities of coaxial cable, 2457
Pham Mau Quan. See Quan, Pham Mau.
Phelp, N. R., with others, ring angels over south-east England, 2982
Phelps, A. V., with others, measurement of attachment of slow electrons in oxygen, 2533
Philipp, H., with others, exciton-induced photoemission from BaO, 2264
Philippo, H. R., and E. A. Taft, optical constants of Ge, 2659
Philipps, B. B., and G. D. Kinzer, electrification of droplets in cumuliform clouds, 456
Phillips, J. C., energy-band interpolation based on pseudopotential, 1236; vibration spectra of diamod-type lattices, 2284
Phillips, J. H., and E. Maxwell, broad-band amplifier for radar and scatter, 64
Piazza, R., surface absorption of sound in ducts, 683
Pick, M., with Y. Avignon, relation between type-IV emissions and other solar activity, 3283

I.23

auroral ionization. 1670

- Pick-Gutmann, M., and J. L. Steinberg, 16-aerial array at 9 300 Mc/s, 3659
 Pickett, J. M., and I. Pollack, speech intelligibility at high noise levels, 3543
 Pickin, J. R., and D. H. Trevena, new development of monotron oscillator, 3524 aa
 Picus, G. S., with others, Zeenan-type magneto-optical studies of interband transitions, 2283
 Piddington, J. H., interplanetary magnetic field and its control of cosmic-ray variations, 783; growth of waves in moving ion streams, 3267
 Piefke, G., propagation in diaphragm-type and corrugated waveguide, 1075; theory of helical line of ferrite wire thickness, 2459
 Piening, J., phase and amplitude fluctuations in subcarrier transmission in colour television, 993
 Piepers, H., with J. J. M. Warringa, open rectangular waveguides in r.f. oscillators, 3984
 Pierce, E. T., with others, geophysical effects of high-altitude nuclear explosions, 2969
 Pierce, J. R., noisness of drifting electron stream, 3159 bb

- antitude indicer explosions, 2995
 Pierce, J. R., noisiness of drifting electron stream, 3159 bb
 and R. Kompfner, transoceanic communication by means of satellites, 2012
 with W. Rigrod, space-charge-wave excitation in Brillouin beams, 1735
 Piercy, B., dielectric properties of polycrystalline stannates and cerates, 2626
 Pierzga, J. L., with K. H. Chase, reducing radar interference, 3118
 Piggott, W. R., obtaining accurate virtual heights from ionogram, 2249
 with W. H. Bellchambers, ionospheric measurements at Halley Bay, 1881
 Piglone, L., voltage- and current-controlled negative resistance 2-poles, 1476
 Pignedolf, A., temperature distribution in junction transistors, 3149
 Pikus, G. E., and G. L. Bir, influence of deformation on properties of p-type Ge and Si, 2649
 and O. V. Sorokin, measuring magnetic field intensity, 1972
 with others, determination of surface recombination velocity, 500
 Pilkngton, W., with others, instrumenting Explorer 1, 1547
 Pilze, F., with R. Theile, television transmission of non-transparent still pictures, 1374
 Pimenov, Yu. V., with Of A. Grinberg, diffraction of c.m. waves at flat screens, 1515
 Pinckney, C. B., calibration of precision voltagedividers, 4157
 Pinckney, C. B., calibration of spin waves in antiferromagnet, 2925.

- Pinckney, C. B., calibration of precision voltage-dividers, 4157
 Pincus, P., with R. Orbach, excitation of spin waves in antiferromagnet, 2925
 Pines, D., with P. Nozičres, dielectric formulation of many-body problem, 1830; electron interaction in solids, 2931
 Pinsker, Z. G., with G. A. Kurov, thin layers of variable composition in In-Sb system, 3780
 Pinson, J. T., with others, radio observations of hypersonic shock waves, 1658
 Pippin, J. E., and C. L. Hogan, resonance measure-ments on Ni-Co ferrites and Ni-ferrite-alumin-ates, 2689
 with others, ferrimagnetic resonance in poly-crystalline rare-earth garnets, 2690
 Pio, E., operating characteristic of magnetic amplifier, 3617
 With E. Bernard, operation of magnetic amplifiers, 3237

- 3237
- with E. Bernard, operation of magnetic amplifiers, 3237
 Pires de Carvalho, A., band structure of Te, 3763
 Pistorius, C. A., with W. C. van Geel, current/time relations of electrolytic rectifiers, 3112
 Pitt, G. F., B. P. Barth and B. E. Godard, electrical properties of epoxy resins, 911
 Pitteway, M. L. V., reflexion from stratified ionosphere, 2250
 Pittman, R. W., with J. I. Carasso, thermoelectric observations on grey Se, 1272
 Piwkowski, T., Bi-Te photovoltaic p-n 'sandwich' layer, 2055; semiconductive properties of Bi-Te solid solutions, 4120
 Plachenov, B. T., with B. I. Boltaks, self-diffusion in Se, 1605
 Planer, G. V., with H. B. Beer, preparing ferrites, 1959
 Plass, G. N., selective radiators, 4010

- Planter, G. v., whit it. D. Davis, preprinting the second secon

- Plush, R. W., with A. D. Watt, worldwide standard-frequency broadcasting system, 4201
 with others, radio system performance in noise, 422

- Prosent, R. W., Bink M., Unitary, Worldwide Standards frequency broadcasting system, 4201
 with athers, radio system performance in noise, 963
 Poaps, G. E., with D. R. Hay, prolonged fade-out on short microwave path, 3098
 Pobedonostsev, Yu. A., laws of motion of earth satellite, 2950
 Pocock, W. E., Al Anishes for use in electronics, 1962
 Podoshevnikov, B. F., and B. D. Tartakovski, attenuation of plane sound waves, 2809
 Pohl, H. G., measurement limit of photocell compensators, 2354
 with others, image converters for quantity production, 1404; resolving power of scintillation multipliers, 3081
 Pohrte, T. W., with others, geomagnetic disturbances and changes in atmospheric circulation at 300 mb, 2229
 Poincelot, P., edge condition in diffraction problems, 774; diffraction of e.m. wave by conducting half-plane, 1168; criterion of uniqueness for solutions of Maxwell's equations, 3628

I.24

- Pokrovskii, V., F. Ulinich and S. Savvinykh, nonlocal reflection in waveguides of variable cross-section, 1766
 Polak, L. S., with others, producing polymers with semiconductor properties, 4121
 Polimerou, L. G., spectrum analysis of random noise generators, 1309
 Pollack, I., with J. M. Pickett, speech intelligibility at high noise levels, 3543
 Pollack, J. R., catapult end-speed recorder, 924
 Polonsky, J., L. Amster and G. Melchior, echo in television images, 3134
 Poloskov, S. M., and T. N. Nazarova, investigation of interplanetary matter, 3718
 Polovin, P. V., and N. L. Tsintsatze, longitudinal vibrations of electron-ion beams, 1835
 Poloyanskaya, V. A., field of pulse radiator under water, 3901
 Ponthus, A., with others, circular waveguides for long-distance transmission, 2107
 Poor, E. W., Jr., with F. E. Loebner, bimolecular transitions in GaP, 3737
 Poorter, T., and F. W. de Vrijer, projection of colour-television pictures, 3119
 Popkin-Clurman, J. R., video testing techniques for monochrome and colour, 613
 Popoy, S. N., with others, effect of polarization on Pb₂Ninb₂O₂-PhyMpNb₂O₂, 2631
 Porpea, A., with *Stress*, distribution of lightning currents in earthing system of radio mast, 1451
 Porter, G., applications for Zener diodes, 1711
 Porter, G., applications for Zener diodes, 1711
 Portis, A. M., and D. Teaney, microwave Faraday rotation, 770
 with A. C. Gossard, nuclear resonance in ferromagnet, 4126
 Poschenrieder, W., electromechanical wave filters, 3225
 Pöschl, K., and W. Veith, focal length of diaphragm for clectron beaus, 1416

- Poschenrieder, W., electromechanical wave filters, 3225
 Pöschl, K., and W. Veith, focal length of diaphragm for electron beams, 1416
 Posel, K., balanced unsymmetrical parallel-T network as 3-terminal bridge, 3062
 Posthurmus, K., merits of telegraph codes and methods of detection, 2010
 Pottel, R., absorption of cm waves in artificially anisotropic media, 1847
 Potter, N. S., with others, sound absorption at 50 to 500 kc/s, 2082
 Potter, N. L., electrical analogue for heat flow problems in semiconductors, 4087
 Potter, R. F., J. M. Pernett and A. B. Naugle, measurement and interpretation of photo-detector parameters, 4240
 Powell, C., Decca navigator system, 2259 c
 Prache, P. M., ferromagnetic granular structures, 2318

- measurent and mergeneration of photo-detector parameters, 4240
 Powell, C., Decca navigator system, 2259 c
 Prache, P. M., ferromagnetic granular structures, 2318
 Pradal, F., and R. Saporte, energy spectrum of reflected electron beam, 399
 and R. Simon, energy spectrum of secondary electrons, 1838
 with C. Fert, energy spectrum of electron beam passing through thin film, 3255
 Pratt, D. S., with others, 3-frequency back-scatter sounder, 1565
 Prene, J. S., with others, two-stage optical excitation in phosphors, 2996
 Pressey, B. G., marine radio navigational aids, 2978 b; signals from satellite 1958 8 2, 4049
 with H. G. Hopkins, current d.1. practice, 2259 j
 Pressey, B. G., with others, search for new Heusler alloys, 1950
 Preuss, E., with D. Geist, etching and polishing of Ge surfaces, 1252
 Price, H. N., and A. W. Coolidge, development of ceramic hydrogen thyratrons, 3535
 Price, P. J., noise theory for hot electrons, 2902
 Price, R. and others, radar echoes from Venus, 2556
 Primeth, R. L., transmission and reflection properties of strip grating, 94
 with J. E. Keys, nose-out radar cross sections, 3320
 Prince, M. B., and M. Wolf, Si photovoltaic devices, 640

- 3320
 3320
 Prince, M. B., and M. Wolf, Si photovoltaic devices, 640
 Prins, B. H. G., and J. M. G. Seppen, Rotterdam Harbour radar system, 1589
 Proctor, E. K., and M. H. Rees, scanning lens design for minimum phase error, 1101
 Prokhorov, A. M., molecular amplifier for sub-mm waves, 1146
 with N. G. Basov, molecular oscillators and amplifier, 1146
 with others, chromium corundum parameter auplifier. 1145
- with others, chromium corundum paramagnetic amplifier, 1145
 Prokhvatilov, V. G., with others, relaxation polariza-
- Prokhvatilov, V. G., with others, relaxation polarization and losses in nonferroelectric dielectrics, 480
 Pröpstl, G., and G. Zielasek, Sb distribution in Ge-Sb alloys, 3026
 Proshkin, E. G., and B. L. Kashcheev, inhomogeneous structure of F region, 2244
 Provost, F., Si junction diodes, 297
 Prowse, W. A., and J. L. Clark, u.h.f. gas breakdown, 395
 Prudhon, M., gyrators and nonreciprocal systems, 2145
 Pruett, G. R., and R. L. Petritz, detectivity and pre-

- Pruett, G. R., and R. L. Petritz, detectivity and pre-
- amplifier considerations for InSb photovoltaic detectors, 4241
 Prugh, T. A., J. R. Nall and N. J. Doctor, D.O.F.L. microelectronics program, 2484
 Prussin, S., and A. Stevenson, infrared strain-optic coefficient of Si, 2295

World Radio History

Prutton, M., ferroelectrics and computer storage, 1781

- with E. M. Bradley, magnetization reversal by rotation and wall motion in NiFe films, 1955 , R. H., with others, cube-oriented magnetic sheet, 896 Ргу,
- Pry, R. H., with others, cube-oriented magnetic sheet, 896
 Przedpelski, A. B., reversing ferrite temperature coefficients, 2686
 Pshenichnikov, A. M., static transmitting device for pulse-frequency telemetry, 1659
 Psutka, M. E., with others, diffraction of e.m. waves by ridge, 241
 Pucillo, G. L., determination of h f. sky-wave absorption, 1341
 Pugh, E. M., with F. P. Beitel, Jr, Hall effects of Fe-Co alloys, 1953
 Pugh, E. W., and F. M. Ryan, susceptibility of Cu-Ni and Ag-Pd alloys, 190
 Pula, T. J., transfer efficiency in fast-response magnetic amplifiers, 2171
 G. E. Lynn and J. F. Ringelman, transfer efficiency of magnetic amplifiers, 3238
 Pullman, J. O., microwave antenna saves space, 3961
 Pulvari, C. F., transpolarizer, 2864

Pulvari, C. F., transpolarizer, 2864 — and W. Kuebler, polarization reversal in BaTiO₈, 159

159
Pursey, H., and F. C. Pyatt, measurement of equivalent noise resistance, 3055
Purton, R. F., common base versus common emitter, 1139
Purvis, M. B., G. V. Deverall and D. R. Herriott, optics and photography in flying-spot store, 2363
Pushkov, N. V., and S. Sh. Dolginov, investigation of earth's magnetic field using earth satellite, 3693

3693
Pustelnyk, M., with O. E. De Lange, timing of regenerative repeaters, 968
Putley, E. H., concentration of impurity carriers in Si, 510; conduction in p-type InSb, 1260; oscillatory transverse magnetoresistance effect in InSb, 1264; conduction in n-type InSb, 1625
with W. H. Mitchell, cryostat for semiconductor, 1967

Putman, J. L., with others, miniature nuclear generator, 2757

generator, 2017
Pütter, P. S., and F. Sauter, statistics of plasma, 1159
Pyatnitskii, A. I., energy distribution of electrons from Sb-Cs cathodes, 2070
Pyatt, E. C., with H. Pursey, measurement of equivalent noise resistance, 3055
Pye, T. R., transistor power converters, 1470, 4207

Quan, Pham Mau, singular e.m. induction, 406

 with L. Mariot, e.m. tensor in presence of induction, 407
 Quartington, J. E., with others, fine structure in absorption-edge spectrum of Si, 509
 Quarta, P., propagation tests at 1 kMc/s, 2002
 Quarta, C. F., R. Komp/ner and J. A. Chisholm, reflex klystron as negative-resistance-type amplifier, 1741
 with others, parametric amplification of space-charge waves, 3159 k

charge waves, 3159 k Quenby, J. J., and W. R. Webber, cosmic-ray cut-off rigi3i ies, 3280 de Quervain, A., h.f. transmission on h.v.lines, 2748 Quiter, W. A. E., radio relay systems and C.C.I.F., 264 Quinn, W. E., and others, r.f. spectra of hydrogen deuteride, 1852 Quirk, J. B., u.h.f. tuner using r.f. amplifier, 1383

Rabenhorst, H., and J. Melicherčik, dielectric properties of BaTiO₃, 1601
Rabkin, L. I., and Z. I. Novikova, design of coils with ferrite cores for a.f., 1790
Radelt, H., lamination-type structure of CdS crystals, 3727

crystals, 3727 Rademakers, A., with H. G. Bruijning, pulse transformer with pre-magnetization, 1469 Radford, H. E., and V. W. Hughes, microwave Zeeman spectrum of atomic oxygen, 4032 Radstake, G., Netherlands broadcasting centre at Lopik-Radio, 266 Raemer, H. R., and A. B. Reich, correlation devices detect weak signals, 3099 Ragavan, D. G., slit resonators as sound absorbers, 687 Rainville, L. P. with others

Rainville, L. P., with others, measurements of bandwidth of waves propagated beyond horizon, 3459

Namivine, E. Y., with obsers, inclusive leaves in the solutions of horizon, 3459
Raisbeck, G., nonuniformities in laminated transmission lines, 2101
Raizer, M. D., and I. S. Shpigel', microwave investigation of plasma, 3262
Raja Rao, K. S., seat of L currents causing geomagnetic tides, 2247
and K. R. Sivaraman, lunar geomagnetic tides at Kodaikanal, 1534
Rajchman, J. A., magnetics for computers, 1782
G. R. Briggs and A. W. Lo, transfluxor-controlled electroluminescent display panels, 568
Raju, T. A., with others, nature and origin of atmospherics, 3699 a
Ralph, E. L., with S. L. Matlow, ohmic Al/n-type Si contact, 3336
Ramanurti, T. V., with others, temperaturesensitive ceramic reactance element, 45
Ramanathan, K. R., with R. Rao, diurnal variation of absorption on 5.65 Mc/s, 3699 j
Ramanathan, K. R., with H. Y. Fan, infrared absorption and photoconductivity in irradiated Si, 4089 b
Ramsa, A. P., H. Jacobs and F. A. Brand, microwave techniques in lifetime measurement, 3774
Ramsey, N. F., with others, r.f. spectra of hydrogen deuteride, 1852
Ranby, P. W., with others, activation of ZnS and (Zn,Cd)S phosphors, 3736

Electronic & Radio Engineer

1967

Randolph, L. W., with others, instrumenting Explorer I satellite, 1547
 Rangan, C. S., with others, temperature-sensitive ceramic reactance element, 45
 Ranzi, I., back-scatter ionospheric sounding experi-ments, 1197
 and A. Porreca, skip-distance determination by back-scatter sounding, 1340

- ments, 1197
 and A. Porreca, skip-distance determination by back-scatter sounding, 1340
 Rao, B. R., and D. S. Murly, c.w. method for study of drifts, 36991
 and K. V. V. Ramana, diurnal variation of absorption on 5-65 Mc/S, 3699 j
 and E. B. Rao, horizontal drifts in F₁ and F₂ regions at Waltair, 2242; effect of enhanced solar activity on F₄ drifts, 3699 k
 R. Chatterjee and S. K. Chatterjee, dielectric activity on F₄ drifts, 2586
 with others, magneto-ionic fading in pulsed radio waves, 944
 Rao, B. V. T., and M. K. Rao, horizontal drifts in F₁ and F₂ regions at Waltair, 2242; effect of enhanced solar activity on F₄ drifts, 3699 k
 wath others, effect of magnetic absorption over Delhi, 810
 Rao, E. B., with B. R. Rao, horizontal drifts in F₁ and F₂ regions at Waltair, 2242; effect of enhanced solar activity on F₄ drifts, 3699 k
 with others, effect of magnetic activity on F₂ drifts, 2586
 Rao, M. N., and A. P. Mita, effect of vertical drifts on nover Delhi, 810
 Rao, M. N., and A. P. Mita, effect of vertical drifts on nocturnal ionization of lower ionosphere, 1878
 with others, hourly median field strength of 1940/mc/s signal. 255

- Auo, M. I., and A. P. Mira, enect of Vertical drifts on nocturnal ionization of lower ionosphere, 1878
 with others, hourly median field strength of 1940-Mc/s signal, 255
 Rao, M. S., irregularities in E region, 4054
 and R. L. Armstrong, radio reflections along a meteor train, 2226
 with others magneto-ionic fading in pulsed radio waves, 944
 Rao, M. V. S. S. K., with N. K. D. Choudhury, panel absorbents for low-frequency sound, 2821
 Rao, N. N., with Y. V. Somayajulu, galactic radiation at 30 Mc/s, 3699 i
 Rao, P. R., analysis of circuit transients using Laplacian transformation, 728
 Rao, P. V. S., character display system for digital computer output, 3968
 Rao, R. A., with A. Singh, ferrite-tuned magnetron, 3163
 Rao, T. S., with others, abnormal ionospheric

- 3163
 Rao, T. S., with others, abnormal ionospheric behaviour at 10 mJ, 808
 with others, emission from sun at 30 Mc/s, 3699 o
 Rapaport, H., ferrite frequency separator, 2466
 Rappaport, P., with J. J. Loferski, effect of radiation on Si solar-energy converters, 1366; electronbombardment-induced recombination centres in Ge, 4108
 Rapaport, W., witch distribution in German
- Ge, 4108
 Rappaport, W., pitch distribution in German language, 2068
 Rasmussen, A. L., with R. D. Harrington, permeability spectra of Y-Fe garnet, 1291
 Rassadin, B., single-sideband modulation, 587
 Rastogi, R. G., geomagnetic influence of F₁ and F₂ regions, 2245; diurnal development of equatorial F₁, 3707
 Ratcliffe, J. A., information by radio from satellites, 1869
 Rath. H. L., properties of Signation.

- regions, 2245; diurnal development of equatorial F, 3707
 Ratcliffe, J. A., information by radio from satellites, 1869
 Rath, H. L., properties of Si rectifiers for communications, 2022
 Rausch, R. H., and T. T. True, reference generator for colour TV receivers, 1324
 von Rautenfeld, F., evaluation of field-strength measurements, 3419
 with E. Belger, interference protection ratios for sound broadcasting, 3464
 Ravi Varma, A. R., and H. D. Krishna Prasad, effect of restricted frequency characteristics on intelligibility of speech, 2755
 Rawer, K., The Ionosphere, (B)1200; problems in ionospheric forcesating, 1333 i
 and K. Sucky, 'fourth reflection condition' of e.m. waves in plasma, 1164; equivalent theorems of wave absorption in plasma, 1669; dispersion formula of Lorentz plasma, 3641
 with E. Harnischmacher, drift observations evaluated by method of 'similar fades', 801
 with others, ionospheric observations during solar celipse of 30th June 1954, 131; rocket measurements of absorption in lower ionosphere, 2972; variation of ionospheric absorption, 3716
 Raymer, G. H., calibration of inductors, 2346
 redith others, ine spectra of absorption edge of CdS, 471; fluorescent emission lines and luminous absorption lines in CdS, 2618
 Reber, G., radio interferometry at 3 km above Pacific Ocean, 2219; suppressed-sidelobe anterna, 3575
 Reddish, A., with others, frequency pushing in crossed-field oscillators, 2786 g
 Reddy, C. A., B. R. Rao and M. S. Rao, magnetoionic fading in pulsed radio waves, 944
 with others, comparison of CS frequency standards, 212
 Rediker, R. H., with J. Halpern, mus switching diodes, 3144
 with A. L. McWhorter, cryosar, 3211
 Rediker, R. H., with others, coatal-line diode, 3524 m
 with others, coatal-line diode, 3524 m
 with othe

- with others, grain-boundary amplifier, 3241 Reed, E. D., with others, helix travelling-wave amplifier, 2788 a

Electronic & Radio Engineer

- Reed, J., multiple-branch waveguide coupler, 3559
 Reed, W. O., and W. F. Niklas, shutter image converter tube for multiple-frame photography, 2240 2369
- Reed, W. O., and W. F. Nsklas, shutter image converter tube for multiple-frame photography, 2369
 Rees, J. R., with A. E. Barrington, 3-cm Q-meter, 562
 Rees, M. H., and G. C. Reid, aurora, radiation belt and solar wind, 4063
 with E. K. Proctor, scanning lens design for minimum phase error, 1101
 Reeves, R. J. D., recording and collocation of waveforms, 1650, 3357
 Rehkopf, C. H., gas evolution or sorption of anode materials, 2985
 Reich, A. B., with H. R. Raemer, correlation devices detect weak signals, 3099
 Reich, H. A., with others, transistorized crystal-controlled marginal oscillator, 1805
 Reichel, R., audibility of nonlinear distortion, 3185
 Reid, G. C., electric-field theory of aurorae, 1887
 and C. Collins, abormal v.h.f. absorption, 2380
 with R. Parthasarathy, signal-strength recordings of satellite 1958 02; 1193
 with M. H. Rees, aurora, radiation belt and solar wind, 4063
 Reimer, L., investigations of thermal transformation of cathode-sputtered Ni films, 895; Hall-effect measurements in Ni films, 1280
 Reinse, H., with C. Heck, storage properties of square-loop ferrites, 3397
 Reiss, H., diffusion-controlled reactions in solids, 4089 d
 with others, formation of donor states in heattraeted Si, 1926

- 4089 a with others, formation of donor states in heat-treated Si, 1926 Reitan, D. K., capacitance of parallel-plate capaci-tors, 1794 Reker, H., line transformer with tuned h.v. winding,
- 1387

- Reger, H., the transformer with tunch h.v. whitning, 1387
 Remeika, J. P., with others, domain behaviour in transparent magnetic oxides, 1956
 Rempel, R. C., and H. E. Weaver, microwave reflection bridge, 1982
 with others, electron paramagnetic resonance in BaTiO, 476
 Rendall, A. R. A., with R. J. Halsey, prospects for transatlantic television by cable, 4211
 Rennie, J. C., wide-band microwave mixer and i.f. preamplifier, 949
 Renton, G. A., with D. F. Gibbons, velocity of sound in Sn, 4122
 Repnev, A. I., with others, pressure ard density measurements in high atmosphere by earth satellites, 3694
 Reshetow, W. D., radiation errors of radiosondes, 226

- 226
 Rettig, A., with H. Bohlmann, installation for outside sound broadcasts, 4204
 Reynolds, D. K., J. Lignon and P. A. Szente, centipede aerial, 1333 at Reynolds, S. I., surface charges on insulators, 2527
 Rhoderick, E. H., nuclear magnetic resonance in InSb 1261; superconducting computer elements, 3209
 Riblet, H. J. high-0 unsuggide filter design of the second second

- a209
 Riblet, H. J., high-Q waveguide filter design theory, 3561
 Rice, L. P., radio transmission into buildings, 1688
 Rich, E., Jr, with others, tracking weather with satellites, 2715
 Richards, E. G., estimation of transmission loss in transhorizon-region, 2000 w
 with others, influence of ocean duct on scatter propagation beyond horizon, 578; m-A propagation in transhorizon region, 2000 b
 Richards, J. C. S., low-capacitance input circuit, 752; apparatus for measuring dielectric constants and losses, 1305
 Richards, P. I., transients in conducting media, 2916
- 2916
- 2916
 Richmond, I. J., with others, m-A propagation in transhorizon region, 2000 p
 Richter, H. L., Jr, and others, instrumenting Explorer I, 1547
 Ricke, F. F., L. H. DeVaux and A. J. Tuzzolino, infrared detectors, 4239
 Rider, D. K., foil-clad lanninates in printed circuitry, 355
 Rider, G. C., propagation measurements at 858 Mc/s, 1346; tropospheric scatter propagation measurements and aerial siting tests, 2000 s
 Ridler, P. F., transistor tape preamplifier, 387
 Ridley, B. K., lifetime measurement by photoconductive decay, 1921
 Rieck, H., aperiodic barretter probe for power measurements, 1322; low-noise h.f. preamplifier, 3236

- 3236
 Riesz, R. P., with G. L. Pearson, switching diodes from plastically deformed Ge, 2412
 Riety, P., equipment for the absolute calibration of microphones, 2093
 Rietz, W., mcasurement and recording of phase characteristics for wide-band transmission, 1310
 Riggs, L. P., with B. R. Bean, synoptic variation of radio reflective index, 4177
 Rigcod, W. W., space-charge-wave harmonics and noise propagation in rotating electron beams, 1736
 and I. R. Pierce, space-charge-wave excitation

- 1736 J. R. Pierce, space-charge-wave excitation in Brillouin beams, 1735
 Rigterink, M. D., ceramic electrical insulating materials, 4142
 Rihaczek, A., with H. Meinke, bandwidth compres-sion of radar displays, 3724
 Rikitake, T., and others, effect of solar eclipse on geomagnetic field, 2561
 Ringelman, J. F., with others, transfer efficiency of magnetic amplifiers, 3238

World Radio History

Ringwalt, D. L., W. S. Ament and F. C. MacDonald, measurements of 1250-Mc/s scatter propagation, 3096

- Anig Wait, D. U., V. Shahr and C. Mc/s scatter propagation, 3096
 Rishbeth, H., radio emission from Vela-Puppis region, 2221
 Riste, T., K. Blinowski and J. Janik, spin-fluctuation scattering of neutrons in magnetite, 4127
 Ritchie, C. C., and R. W. Young. design of biased-diode function generators, 2861
 Ritow, H., wire-cylinder discharges in air, 394; space-charge field-emission hypothesis, 2907
 Ritt, P. E., with J. L. Pentecost, lightweight ceramic materials, 839
 Rittner, E. S., theory of Pcltier heat pump, 2906
 Rittner, E. S., theory of Pcltier heat pump, 2906
 Rittner, B. Galin, rectangular-guide ferrite phase shifters, 1771
 Roach, F. E., night airglow, 1567
 Robbins, A., with J. O. Thomas, electron distribution in ionosphere over Slough, 806
 Robbercht, G. G., and J. L. Verhaeghe, measurements of permeability tensor for 'ferroxcube' at 24 kMc/s, 1293
 Robeer, A. G., with H. E. Eckhardt, 100-kW s.w. broadcast transmitter, 293
 Robeer, A. G., with H. E. Schhardt, 100-kW s.w. broadcast transmitter, 293
 Robeer, N. G., gravitational torque on satellite vehicle, 117; air drag effect on satellite orbit, 119
 Roberts, C. R., P. H. Kirchner and D. W. Bray,

119
Roberts, C. R., P. H. Kirchner and D. W. Bray, radio reflections from satellite-produced ionization, 2963
Roberts, D. H., photoconductivity in PbSe, 470
and J. E. Baines, photoconductivity in PbSe films, 830
and B. L. H. Wilson, effects of O₂ on resistivity in Si, 2294

Si, 2294
Roberts, G. A., with T. W. Buller, Jr, ferroelectric capacitors, 3247; voltage-variable capacitor guide, 3599
Roberts, J. A., echoes in solar corona from new type of radio burst, 102
with R. G. Giovanelli, observations of solar disturbances causing type II radio bursts, 432
with R. Q. Twiss, e.m. radiation from electrons in ionized medium, 408
Roberts, N. W., stability of evaporated films, 1295
Roberts, V., with others, fine structure in absorption-edge spectrum of Si, 509

edge spectrum of Si, 509 Robertshaw, R. G., with C. H. Dix, pulsed travel-ling-wave tubes in 10-Gc/s region, 2788 m Robillard, P. E., with others, diffraction of c.m. waves by ridge, 241 Robillard, T. R., and R. W. Westberg, transistors for electronic switching, 2778 Robin, L., harmonic distortion in f.m., 1504 Robin-Kandare, S., and B. Vodar, reflecting power of bulk Si and Ge, 3766 Robin, D. A. uscentibility and resistivity of

of bulk Si and Ge, 3766
 Robins, D. A., susceptibility and resistivity of transition-metal silicides, 1274
 Robinson, A. C., with others, properties of dilute ferromagnetic alloys, 1631
 Robinson, D. Z., methods of background description, 4010 m

4010 m
 Robinson, F. N. H., current and velocity fluctuations at potential minimum, 320
 with chers, dynamic nuclear polarization, 3412
 Robinson, K. W., with J. Dekleva, shunt impedance measurement, 3421

Roch, J., electronic paramagnetic-resonance spectro-meters, 3269, sensitivities of, 1172
 Roche, J. F., with others, measurements of bandwidth of waves propagated beyond horizon, 3459
 Rockstuhl, F., crystal-controlled 3-terminal valve oscillators, 1483

oscillators, 1483 Roddam, T., return loss, 12; bifilar-T circuit, 1122 Rodgers, K. F., with W. S. Boyle, oscillations in infrared transmission of Bi, 2620 with others, splitting of As donor ground state in Ge, 1615 Rodie, V. N. Schwarz, Schwarz, 167

with H. Fumeron-Rodot, properties of HgTe, 3779

3779
Rodrigue, G. P., and others, ferrimagnetic resonance in polycrystalline rare-earth garnets, 2690
Rodriguez, S., cyclotron resonance in metals, 1855
Roe, G. M., and M. R. Boyd, parametric energy conversion in distributed systems, 3240
Roessler, E., propagation of e.m. waves, radio location and radio astronomy, 1581
Rogal, B., with others, torque-operated wattmeters for 3 cin λ, 2359
Roder, R. S., with C. W. McLeish, h.f. direction-

Roger, R. S., with C. W. McLeish, h.f. direction-finding errors caused by vertical reradiators,

finding errors caused by vertical reradiators, 1203
Rogers, T. F., with L. A. Ames, 220-Mc/s reception at 700-1000 miles, 1351
with others, persistent v.h.f. field strengths beyond radio horizon, 2737
Rohan, P., radio telemetry, 3448
Rollett, J. M., characteristic frequencies of junction transistors, 996
Ronchi, L., with others, trajectory of earth satellites, 441; determination of satellite orbit, 1188
Ronzheimer, S. P., and R. J. Farber, measurement of colour television receiver performance, 986
Rookes, R. D., with G. M. Clarke, microwave reflectometer display system, (D)2703
Root, H. G., with others, maxurements of bandwidth of waves propagated beyond horizon, 3459
Rose, A., and M. A. Lampert, gain-bandwidth product for performance and Fermi level, 2988
with E. O. Johnson, analysis of anplifier devices, 2041

I.25

Rodin

1203

2041

in, V. N., electron analyser of contact circuits, 1460

- with M. A. Lampert, transient behaviour of ohmic contact, 2903

- onnic contact, 2903
 with others, photo-properties of ZnO, 826; approach to intrinsic ZnO, 877
 Rose, A. S., metaulographic aspects of alloy junctions, 187
 Rose, C., with others, long-distance single-F-hop transmission, 943
 Rose, D. C., with others, decreases in cosmic-ray intensity during period October 1956 to January 1958, 4037
- Rose, F. W. G., impact ionization in Si *p*-*n* junctions, 1927
- Rose, F. W. G., Impact ionization in Si p-n junctions, 1927
 Rose, G., with others, sweep frequency oblique-incidence pulse transmissions, 2378
 Rose, M. E., electrostatic interaction of charge distributions, 760
 Rose-Innes, A. C., observation by cyclotron resonance of effect of strain on Ge and Si, 507
 with C. Hilsum, new method of measuring susceptibility, 1313
 Rosen, A., and others, ionizing radiation at 3 500-36 000 km, 3691
 Rosenberger, G. B., cryogenic oscillator, 2875
 Rosenon, D. D., Jr, with B. Kostyshyn, magnetic field probe, 1973
 Rosei, F. D., effect of crystal growth variables on

- field probe, 1973
 Rosie, F. D., effect of crystal growth variables on Generative for the second second
- 3365
 with W. H. Kleiner, deformation potential in Ge, 2655
 with others, Zeeman effect of excitons in Ge, 2299; exciton- and magneto-absorption of transitions in Ge, 3364
 Roth, W. C., with J. G. White, polarity of GaAs, 3381
 Roth, W. L., multispin axis structures for anti-ferromagnets, 188
 Rothbart, A., torsional magnetostrictive delay line, 2881
 Rotherstein B. and J. Heingra mobility of Bloch

- Rothenstein, B., and J. Hrianca, mobility of Bloch walls, 3794; influence of temperature on distri-bution of ferromagnetic domains, 3795
 Rothwell, P., cosmic rays in earth's magnetic field, 1524
- 1524

- ISOU Market A. A. Cosine rays in earth's magnetic field, 1524
 and C. McIlwain, satellite observations of solar cosmic rays, 3692
 Rotman, W., wide-angle scanning with microwave pillboxes, 1448
 and A. A. Oliner, asymmetrical trough-wave-guide antennas, 3960
 with A. A. Oliner, periodic structures in trough waveguide, 3934
 Rowden, R. A., L. F. Tagholm and J. W. Stark, tropospheric wave propagation measurements by B.B.C., 2000 m
 Rowe, J. E., theory of crestatron, 2427

- Rowe, J. E., theory of crestatron, 2427
 and R. J. Martin, electron-trajectory calculator and Poisson cell, 3524 kk
 Rowe, R. M., with chers, measurement of pulse front response of transformers, 357
 Rowland, R., printed circuits applied to microwave links, 2488
 Rowley, G. C., digital differential analysers, 1780
 Rowson, B., angular diameter measurements of radio sources at 10.7 cm Å, 3658
 Roy, B., properties of strongly connected graph, 1964
 Royle, J. R. T., with G. Hersze, B.B.C. transparencies for testing camera channels, 984
 Rozis-Saulgeot, A. M., highly ionized regions of intestellar matter, 3272
 Rozner, F., television waveform generator using
- Rozner, F., television waveform generator using transistors, 1373

- transistors, 1373
 and P. Pengelly, transistors and cores in counting circuits, 2479
 Rubbia, C., and G. Torelli, differential discrimination for fast pulses, 3990
 Ruben, S., Zo/Hg-dioxysulphate dry cell, 3866
 Rubinshtein, R. N., and V. I. Fistul', determination of surface couductivity of semiconducting crystals, 2671
 Rubissow, G. J., with F. I. Baghdady, dynamic transition
- crystals, 2671
 Rubissow, G. J., with E. J. Baghdady, dynamic trap for weak f.m. signals, 1350
 Ruby, S. L., F. D. Schupp and E. D. Wolley, effect of fast neutrons on n-type Ge, 866
 Rücker, D., electroluminescence of SiC, 3003
 Rudd, J. B., correlation between stagger-tuned and synchronously-tuned coupled circuits, 364; double-tuned transformers, 3595
 Ruddlesden, R., with E. Fitch, aerial height for ionospheric scatter links, 2000 c
 Rudin, M., R. E. Shafer and B. W. Baker, dual-cavity microwave discriminator, 1487
 Rudy, W. G., with achers, moulded Ni cathode 2069

- cavity microwave discriminator, 1487
 Rudy, W. G., with others, moulded Ni cathode, 2069
 Rüetschi, P., and R. T. Angstadt, self-discharge reactions in batteries, 2403
 Ruggles, P. C., design and performance of high-density electron guns, 3524 u
 Rukhadze, A. A., with V. M. Agranovich, propagation of e.m. waves in medium with spatial dispersion, 2921

- with others, Cherenkov radiation in medium with spatial dispersion, 3648
 Rumfelt, A. Y., and R. J. Como, rapid insertion device for coaxial attenuators, 3927
 Rumsey, V. H., with others, U.R.S.I. report on antennas and waveguides, 3565

- Runyan, W. R., growth of large Si and Ge crystals, 3767

- Runyan, W. R., growth of large Si and Ge crystals, 3767
 Rupp, H., network of broadcast and television transmitters in Württemberg, 1692
 Ruppel, H. M., with others, beam noise in crossed electric and magnetic fields, 313
 Ruppel, W., field effect in insulating ZnO powder, 1903
 H. J. Gerritsen and A. Rose, approach to intrinsic ZnO, 877
 with others, photo-properties of ZnO, 826
 Rupprecht, H., concentration and mobility of electrons in ZnO, 879; Hall coefficient of doped InAs, 3385
 Rupprecht, J., and C. Heck, dielectric properties of oriented Ba ferrite, 3807
 Rusch, W. V. T., with others, antenna to eliminate groundwave interference in ionospheric sounding, 710; power-line aerial, 1672; v.l.f. c.w. transmitter for ionospheric investigation, 3873
 Ruske, W., magnetic properties of electrolytic Ni films, 3804
 Russel, J. T., with P. F. Checcacci, microwave configuration lens tests, 1450
 Ruthroff, C. L., broad-band transformers, 3593
 Rutz, R., end F. Singer, properties of experi-

- Ruthberg, S., double-sweep method for analysis of cavity characteristics, 926
 Ruthroff, C. L., broad-band transformers, 3593
 Rutz, R. F., and D. F. Singer, properties of experimental 1-kMc/s transistors, 3510
 Rvachev, A. L., time-lag of photoeffect and conductivity of Cu₂O, 3734
 Ryabinkin, Yu. S., modern transistors, 3509
 with others, field potential and charge carriers in fused-in junctions, 3787
 Ryan, F. M., with E. W. Pugh, susceptibility of Cu-Ni and Ag-Pd alloys, 190
 Ryan, W. D., antenna switch for scintillation measurements, 2844
 Ryboner, J., and E. Ungstrup, influence of auroral zone on communications, 1333 j
 Ryder, F. L., Lagrange equations in electrical networks, 360
 Ryer, W. H., with W. E. Sheehan, circuits for transistor receivers, 1349
 Ryperson, J. L., with others, tropospheric scatter system using angle diversity, 2751
 Rylme, T. B., with adrers, Ge junction cells for photoelectric control circuits, 309
 Ryter, C., 10-kMc/s paramagnetic resonance in Eu and Gd, 1629
 Rzanov, M. A., with others, temperature dependence of work function of semiconductors, 494
 Rhanov, A. V., Yu. F. Novototskit-Vlasov and I. G. Neizerstnyl, field effect and surface recombination in Ge, 1928

- tion in Ge, 1928
 Saad, T., with others, 'reactatron' microwave amplifier, 1150
 Sabbatini, A., response of amplifier operating on interrupted cycle, 1138
 Saburi, A., with T. Fujii, analysis of electron beam by mechanical scanner, 3524 l
 Sacerdote, C. B., detecting sound fields, 2447
 Sacerdoti, G., and R. Toschi, potential of e.s. field and trajectories of charged particles, 1505
 Sachdev, D. K., study of atmospheric radio noise at Delhi, 1580
 Sack, E. A., ELF electroluminescent display, 225
 Sadashige, K., with S. L. Bendell, image retention in image orthicon, 615
 Sagar, A., piezoresistance in GaAs, 1939
 Saito, H., with others, diffraction at v.h.f. and u.h.f. by ridges, 243
 Saito, Y., and S. Yamanaka, residual polarization of BaTiO₂ ceramics, 3327
 Sakaki, Y., with S. Maruse, electron-optical properties of point cathodes, 3077
 Salccanu, C., and M. Zägünszu, correction to velocity of sound by resonance method, 328; influence of thickness of walls of resonance tube, 1422
 Salerno, J., with C. D. Hardin, miniature X-band

- 1422
 Salerno, J., with C. D. Hardin, miniature X-band radar, 1584
 Salkovitz, E. I., G. C. Bailev and A. I. Schindler, effect of neutron irradiation on Curie temperature of ferrites, 898
 Salow, H., with W. v. Münch, storing and switching transistor, 2777
 Sampaio, P. M. J. C. da S., with K. W. H. Foulds, electric field distributions in waveguide containing dielectric slab, 3940
 Sampath, S., with others, electronic and ionic devices with thermionic cathodes, 3551; cylindrical, elliptical and prismatic forms of electronic tubes, 3895
 Sampson, D. K., with H. L. Daniels, magnetic drum provides analogue time delay, 1655
 Sarnson, C. A., effect of atomic tests on radio noise, 4067
 Samuels, J., O., propagation of waves in rough

- Samuels, J. O., propagation of waves in rough ducts, 2919
 Sander, A., wide-band radiator with adjustable matching in range 30-70 cm λ, 2361
 Sander, K. F., with M. R. Barber, electron optics of e.s. electron guns, 3524 r
 with D. H. Davies, electron trajectories in gun of M-type carcinotron, 318
 Sanders, J. H., optical maser design, 3655
 with others, radiosonde measurement of electric field and polar conductivity, 1195
 Sandors, C. A., *et al. Structure of the structure of t*

- Sandulova, A. V., and Khe-Yui-Lyan, diffusion and solubility of Ta in Ge, 4104
 Sanghi, I., electrolytic etching of Ta, 359
 Sanpei, H., with L. F. Bates, magnetothermal effects in Fe and SiFe, 4129
 San Soucie, R. L., with J. H. Green, Jr, error-correcting encoder and decoder, 257
 Saporte, R., with D. R. Mason, contacts to p-type Si, 2296
 Sarada, K. A., cösmic-noise absorption associated with solar event, 789
 with others, radio patrol of solar flares, 3699 p
 Sarada, K. A., cösmic-noise absorption associated with solar event, 789
 with others, radio patrol of solar flares, 3699 p
 Sarf, D. J., with M. R. Chidi, accurate measurement of mutual conductance, 3059
 Sargent, J., recording microwave hygrometer, 3070
 Sarrma, N. V. G., with others, radio patrol of solar flares, 3699 p
 Sassier, M., Si power rectifiers, 268
 Sastry, G. S., with others, radio patrol of solar flares, 3699 p
 Sato, H., with others, dependence of sound attenuation on magnetization direction in Ni, 4125
 Sato, K., and M. Kyasu, effect of room shape on sound field, 3916
 Satterthwaite, C. B., with others, evidence for energy gap in superconductors, 393
 Satyanarayana, R., K. Bakhru and S. R. Khastgir, triple splitting of Fedoes, 1885
 with P. Venkateswariu, flading of radio waves, 585
 Saubestre, E. B. H., electroless copper plaing in printed circuitry, 3047
 Sauzade, M., transistor stabilized supply to feed electromagnet, 2758
 with H. Hahn, transistor stabilized supply to feed electromagnet, 2758
 with H. Hahn, transistor stabilized supply to feed electromagnet, 2758
 Savingth, S., with others, nolocal reflection in waveguides of variable cross-section, 1766
 Sawade, K., Mit A. A. Brucekner, magnetic succeptibility of electroid gas, 759
 Savingth, S., with others, fuller, observations of antiparialel domains in BaTiO, 263

Schallehn, W., with others, Telefunken traffic radar, 1898
Schanda, J., with others, time-dependent spectra of ZnS: Cu, Pb, 4080
Scharfman, H., with *F. J. O'Hara*, ferrite serrodyne for microwave frequency translation, 3942
Scharfman, W. E., with others, voltage breakdown characteristics of microwave antennas, 3581
Schawlow, A. L., and C. H. Townes, infrared and optical masers, 1857
Scheer, J. J., and P. Zalm, crystal structure of Na₄KSb, 2995
van der Scheer, J. W. A., portable instrument for i.f. measurements on f.m. radio links, 222
Scheibner, E. J., with others, stabilization of Si surfaces by thermally grown oxides, 2650
Schemel, R. E., with W. Frazer, modulator as phase detector, 2899
Schenck, E., accuracy obtainable with transistor in p.a.m. and p.w.m., 1827
Schenkerman, S., designing transistor d.c./a.c. converters, 267
Scheiss, C., with W. F. Jost, evaluation of quadripole and inaterial measurements using chart, 2702
Schiess, C., with W. F. Palmer, transistorized vertical deflection systems, 1381
Schiffman, B. M., microwave 90° phase shifters, 2114
Schliffzzi, T. E., radar data transmission, 1586

Schimman, B. M., microwave 90° phase shirters, 2114
Schillzzi, T. E., radar data transmission, 1586
Schiller, M. I., television station list, 2030
Schilling, G. F., and T. E. Sterne, densities and temperatures of upper atmosphere from satellite observations, 1871
Schimpf, L. G., carrier transmission for closed-circuit television, 3114
Schindler, A. I., with others, effect of neutron irradiation on Curie temperature of ferrites, 898
Schirmer, H., and J. Friedrich, electrical conductivity of plasma, 1161
Schlabach, T. D., and E. E. Wright, test patterns for printed-circuit materials, 2487
Schleimann-Jensen, A., generation of submillimetre waves by avalanching semiconductor, 3875
Schlesier, H., significance of 90° phase shift in modulation systems, 4196

Electronic & Radio Engineer

- Schlesinger, K., new electron gun for picture display, 3128
 Schlesinger, S. P., and D. D. King, dielectric image lines, 2827
 Schley, U., and F. Hoffmann, noise in radiation thermocouples, 1653
 Schlichting, K., investigations on harmonic frequency dividers, 1132
 Schlier, R. E., with others, surface properties of SiC crystals, 3022
 Schlömann, E., ferromagnetic resonance in polycrystalline ferrites, 777, 906
 and J. J. Green, decline of ferromagnetic resonance absorption with increasing power level, 4139
 Schmeltzer, R. A., stabilization of transistor gain, 4231
- 4231 Schmelzer, C., with others, fixed-frequency cyclotron
- Schmelzer, C., with others, fixed-irequency cyclotron with one dee, 1985
 Schmerling, E. R., and C. A. Ventrice, rapid reduction of k'f records to N-h profiles, 3303
 Schmid, H., function generator for sines or cosines, 1457
- 1457
 Schmid, K., with others, radio link installations for telephony and television, 1687
 Schmidt, G., plasmas in external magnetic fields, 3642
- 3642
 Schmidt, L., with others, resolving power of scintillation multipliers, 3081
 Schmidt, L. W., and J. I. Davis, solar-cell power supply, 4206
 Schmidt, W., c.w. magnetron, 4244, a.c. operation of, 3161

- of, 3i61 Schmidt-Rohr, U., with others, fixed-frequency cyclotron with one dee, 1985 Schmidt-Tiedemann, K. J., amplifier for investi-gation of electron avalanches, 1136 Schmitt, H. J., back-scattering measurements, 3843 and W. Futtermenger, multistage resonance absorbers for cm waves, 1846 Schmitt, R. W., with I. S. Jacobs, low-temperature behaviour of dilute alloys Mn-Cu and Co-Cu, 2673 Schmouker, J., with others, irradiation of photo-

- 2673
 Schmouker, J., with others, irradiation of photo-conductive single crystals of CdS, 2617
 Schmucker, G., Telefunken s.w., cr.d.f., 2257
 Schneider, B., and M. J. O. Strutt, shot noise in Si p-n junction diodes and transistors, 2413
 Schneider, H., representation of a.c. characteristics of earthed-base transistor, 2042
 with W. Hanle, scintillation counters, 3080
 Schneider, J., stimulated emission of radiation by electrons in magnetic field, 3264
 Schoen, S., transistors provide computer clock

- with W. Hanle, scintillation counters, 3080
 Schneider, J., stimulated emission of radiation by electrons in magnetic field, 3264
 Schoen, S., transistors provide computer clock signals, 1784
 Scholeld, H. H., H. H. H. Green and R. E. Gossett, manufacture of waveguide parts, 3353
 Scholtend, R. H., H. H. H. Green and R. E. Gossett, manufacture of waveguide parts, 3553
 Scholt, K., with others, correlation measurements in s.w. range, 953
 Schorn, R. A., with others, radio reflections from satellite-produced ion columns, 121
 Schorr, M. G., and R. H. Packard, power supply for video circuits, 602
 Schorder, F. K., progress in construction of loud-speakers, 1762
 Schröder, F. K., progress in construction of loud-speakers, 1762
 Schröder, W., pulse-width filter for television receivers, 1802
 Schroeder, C. A., C. H. Looney, Jr, and H. E. Carpenter, Jr, tracking orbits of man-made moons, 1190
 Schroeder, J. O., holding video level, 3131
 Schroeder, M. R., stereophonic effect obtained from single audio signal, 1056; measurement of diffusivity in reverberation chambers, 3919
 Schulz, E., with others, distribution of lightning currents in earthing system of radio mast, 1451
 Schulz, J., characteristics of cathode-coupled limiter, 1813
 Schulz, J., characteristics of cathode-coupled limiting wave transmission lines, 1627
 G. J. Wheeler and M. H. Sirvetz, high-power L-band resonance isolator, 3563
 with H. E. D. Scovil, 3-level masers as heat engines, 2212
 with others, paramagnetic-resonance spectrum of Cr³⁴ in emerald, 1628; 3-level solid-state travelling-wave maser, 2177; spin refrigeration and maser action at 1 500 Mc/s, 3654
 Schumann, R., u.s.w. propagation along rough layers, 2379
 Schuon, E., long-slot directional couplers, 2112; approximation of modul

- Schuommann, R., u.s.w. propagation along rough layers, 2379
 Schuon, E., long-slot directional couplers, 2112; approximation of modulus and argument of transmission factor, 3976
 and H. J. Butterweck, linearization of f.m. characteristic of reflex klystron, 1739
 Schupp, F. D., with others, effect of fast neutrons on n-type Ge, 866
 Schuster, W. D., with W. Krug, electronic production of lines of equal density, 4167
 Schuster, W. D., with W. A. Dickinson, picture tubes with 110° deflection, 284
 Schutzman, E., with D. Hoffman, analysis of noise-signal amplitudes, 3826
 Schwartz, E., television techniques, 1699; sound and television broadcasting, 2749
 Schwartz, J. W., high-transconductance electron gun for kinescopes, 322; annular-geometry electron gun, 652
 with R. D. Gold, drive factor and gamma of conventional kinescope guns, 1417

- Electronic & Radio Engineer

- Schwartz, L. S., with others, binary communication feedback systems, 2387
 Schwarz, R. F., with P. H. Brill, radiative recombin-ation in Ge, 869

- Schwarz, R. F., with P. H. Brill, radiative recombination in Ge, 869
 with others, control of luminescence by charge extraction, 473
 Schwarzlander, H., intelligibility evaluation of voice communications, 2819
 Schweinler, H. C., thermal neutron capture in Si and Ge, 4089 a
 Schweizerhof, S., ferrites for magnetostriction oscillators, 1954
 Schweitek, H., absorption index of ionosphere, 2732
 Schwetnek, H., absorption index of ionosphere, 2732
 Schweitek, H., absorption index of ionosphere, 2732
 Schwettek, G., expiration index of ionosphere, 2732
 Schwettek, G., and H. Murmann, field superposition for electron-optical shadow method, 3441
 Schwuttke, G. H., crystal orientation of Ge and Si, 166
 Scofield, B. T., etching Ge to precise limits, 4103
 Scott, H. D., multichannel d.c. recording system, 3108
 Scott, T., with others, power transistors, 2769

- Scott, H. D., multichannel d.c. recording system, 3108
 Scott, T., with others, power transistors, 2769
 Scott, T. M., with J. H. O'Connell, measurement of transistor characteristics in 3-250 Mc/s range, 1304
 Scott, W. T., with others, Doppler satellite measurements, 1191
 Scott, M. H. E. D., and E. O. Schulz-DuBois, 3-level masers as heat engines, 2212
 with others, level solid-state travelling-wave maser, 2177; spin refrigeration and maser action at 1500 Mc/s, 3654
 Scrivens, A. K., pulse-modulated beam current in klystron operation, 1016
 Seaman, M. S., with F. A. Benson, surface structure of saturated-diode filaments, 1418
 Searis, A. W., with others, generation of stable carrier frequencies, 3987
 Sears, J., time delays in ultrasonic delay lines, 2698
 Seavey, M. H., J. F. and F. C. Tannemudal, direct observation of spin-wave resonance, 191
 Seckler, B. D., and J. E. Jackson, ionosphere electron densities, 3714
 Seedgr. G., with others, theory of multiple lines, 2458

- densities, 3714
 Seed, T. J., v.h.f. observations on aurora australis, 141
 Seeger, G., with others, theory of multiple lines, 2458
 Seeger, K., delayed electron emission and photo-effect of Fe atter electron bombardment, 874; microwave-induced carrier multipleiation in Ge, 2302; drift mobility in Ge, 3371
 Seeley, J. S., quarter-wave matching of dispersive materials, 2125
 and J. Brown, dispersive artificial dielectrics in beam-scanning prism, 2124
 Seemann, F. W., with D. Hahn, significance of boundary layers and polarization fields for electroluminescence, 833
 Segalin, V. G., simplified analysis of transients in linear circuits, 2148
 Ségard, N., and J. Cassette, theoretical investigation of ultrasonic field, 1423
 J. Cassette and F. Cccquerez, crystal probe for measurement of ultrasonic power, 1752
 Seidel, G., with M. Heckl, influence of self resonances of measurement chambers on sound insulation measurements, 2090
 Sekiguchi, T., and R. C. Herndon, thermal conductivity of electron gas, 766
 Sells, S., with others, design of high-power S-band magnetron, 2788 d
 Sellberg, F., theoretical investigation of closed relay structures, 3159 t
 Selzer, E., field of permeable alloy cylinder, 90
 Sermenov, A., and V. Versunov, phase compensation methods of shaping s.b. signal, 588

- Semennikov, Yu. B., electronic-acoustic converter, 679
 Semenov, A., and V. Versunov, phase compensation methods of shaping s.s.b. signal, 588
 Sen, A. K., rhombic antenna with cylindrical helices, 19
 Sen, S. K., with S. D. Chatteriee, induced conductivity at surface of contact, 1271
 Senf, H. R., with F. E. Goodwin, volumetric scanning of radar with ferrite phase shifters, 1896
 Sengupta, D. L., radiation characteristics of zig-zag antenna, 2848
 Senior, T. B. A., currents on strip aerials, 1086; diffraction by imperfectly conducting wedge, 4028
 with J. S. Hey, e.m. scattering by thin plates, 772
 Senitzky, I. R., behaviour of 2-level solid-state maser, 73
 Senn, J. C., testing diodes for r.f. noise, 3507
 Seppen, J. M. G., and J. Verstraten, 8-mm radar, 1591
 with B. H. G. Prins, Rotterdam harbour radar

- Seppen, J. M. G., and J. Verstraten, 8-mm radar, 1891
 with B. H. G. Prins, Rotterdam harbour radar system, 1589
 Sergeeva, V. M., with others, new semiconducting compounds, 3755
 Sery, R. S., with others, radiation effects in magnetic materials, 196
 Sessler, A. M., with C. E. Nielsen, space-charge effects in particle accelerators, 1984
 Sethuraman, R., rates of fading of reflected pulses at 2-6 and 4 Mc/s, 3609 h
 Sette, D., with G. Bedendo, photoconductivity and lifetin e of charge carriers, 3342
 with others, characteristic parameters of barrier layer in metal/semiconductor junction diodes, 2415

Setty, P. S. V., r.f. oscillations in 'silent' discharges, 1155

- 1155
 Severin, H., acoustic and e.m. boundary-value problems, 4008
 Seyler, A. J., and A. Korpel, voltage-controlled low-pass filter, 1119

 and C. R. Wilhelm, video transmission test set, 4159
- and C. K. Wilhelm, video transmission test set, 4159
 Shabanskii, V. P., non-equilibrium processes in impurity semiconductors, 2282
 Shafer, R. E., with others, dual-cavity microwave discriminator, 1487
 Shafer, Yu. G., with others, investigation of cosmic radiation, 3663
 Shafronov, V. D., propagation of e.m. field in medium with spatial dispersion, 1166
 Shain, C. A., radio emission from Centaurus-A and Fornax-A, 2222
 with M. M. Komesaroff, refraction of extra-terrestrial radio waves, 2973
 Shakeshaft, J. R., and J. E. Baldwin, radio emission from 'supergalaxy', 3660
 with others, spatial distribution of radio sources at 159 Mc/s, 103
 Shal'nikov, G. I., electron-beam high-voltage volt-meter, 560
 Shaltiel, D., with W. Low, electron paramagnetic resonance in BaTiO₃, 477; paramagnetic resonance spectrum of Gd in ThO₂, 909
 Shand, J. A., with others, causes of geomagnetic fluctuations with 6 here nericed 2945; reographical

resonance spectrum of Gd in ThO₂, 909
Shand, J. A., with others, causes of geomagnetic fluctuations with 6-sec period, 2945; geographical variations in geomagnetic micropulsations, 2946
Shanks, H. E., and R. W. Bickmore, four-dimensional e.m. radiators, 2840
Shannon, C. E., channels with side information at transmitter, 592; probability of error for optimal codes in Gaussian channel, 2745
Shapiro, B. S., with others, electron concentration of ionosphere from observations of first earth satellite, 3298

Shapiro, B. S., with others, electron concentration of ionosphere from observations of first earth satellite, 3298
Shapiro, H. S., and D. L. Slotnick, mathematical theory of error-correcting codes, 1683
Shapiro, S., with others, cross-relaxation in spin systems, 3270
Shapley, A. H., coordination of I.G.Y. observations, 1539

1539
Sharek, C. W., with I. C. Miller, designing ultrasonic delay lines, 28
Sharma, K. P., excitation of radiation by surface waves, 2097; reactance of loss-free surface, 3557
with J. Brown, launching of radial cylindrical surface waves by circumferential slot, 2110
Sharp, C. E., with G. Goubau, model surface-wave transmission line, 10
Sharpe, J., with R. Mather, tuning cavities for reflex klystrons, 3525
Sharpe, J. S., photomultipliers for scintillation counting, 3446
Sharpe, R. G., and D. R. Gamlen, radio communication in Ghana, 961
Sharpless, W. M., GaAs point-contact rectifiers, 1710
with C. B. De Loach, X-band parametric

tions in Ghana, 961
Sharpless, W. M., GaAs point-contact rectifiers, 1710
with C. B. De Loach, X-band parametric amplifier, 4006
Shaw, A. W., A. E. Siegman and D. A. Watkins, reduction of electron-beam noise, 1728
Shaw, H. J., with others, current distribution in modulated electron beams, 644; high-power pulsed klystrons, 1410; high-power windows at microwave frequencies, 3159 c
Shaw, R. F., amplifiers for digital data systems, 27
Shcheglov, P. V., with I. S. Shklowskii, optical observations of earth satellites, 3288
Shchekin, V., solar battery, 603
Shchelovanov, L. N., transients in phase-correcting systems for p.c.m., 599
Shea, R. F., Transistor Circuit Engineering, 757
Sheeham, W. E., and W. H. Ryer, circuits for transitor receivers, 1349
Shekhtman, I., with C. Larish, production of two temperatures in ionized gas, 2536
Shekun, I. Ya., with others, magnetic doubler refraction of microwaves, 776
Shehen, J. P., with K. S. Kelleher, limitations of satellite antennas using spherical arrays, 1091
Shepherdson, M., and R. Walters, stroboscopie method for frequency response neasurements, 2079

method for frequency response measurements, 2079
Sheridan, K. V., radio sources in Centaurus, Fornax and Puppis, 422
G. H. Trent and J. P. Wild, extension of solar radio spectroscopy, 2933
Sherman, A., with R. R. Palmisano, waveguide coils make compact delay lines, 339
Sherman, G., measurement of average value of magnetic field, 3824
Sherry, M., with C. P. Allen, measurement of measurement of average value of magnetic field, 3824
Sherry, N. P. R., trochotron, 1724
Shersby-Harvie, R. B. R., generating high-frequency waves using Doppler effect, 31591
Shervood, R. C., J. P. Remeika and H. J. Williams, domain behaviour in transparent magnetic oxides, 1956
Shestopalov, V. P., and B. V. Kondratiev, space resonance in helix waveguide, 2464
with B. M. Bulgakov, propagation in retarding systems with helix and dielectric, 3899
Sheval, W. L., Jr, rotational switching in ferrites, 1634

Shevál, W. L., Jr, rotatioual surveysion of f₀F₁, 129;
 Shibata, H., world-wide distribution of f₀F₁, 129;
 'minimum loss operation time' for s.w. communication, 226, 1359
 with others, reception of radio waves from Russian earth satellite I, 120; life tests of microphone 1758

- Shibata, T., A. Toi and T. Suila, e.s.-transformer-type particle accelerator, 3071
 Shibata, Y., with others, measurements of field patterns for comb-type slow-wave structure,
- patterns for comb-type slow-wave structure, 3524 n Shibuya, Y., with others, circuits for space probes, 3286
- Shields, J., breakdown in Si p-n junctions, 2652
 Shimazaki, T., dynamical structure of ionosphere, 2966
- 2966
 Shimizu, J. K., and E. M. T. Jones, coupled-transmission-line directional couplers, 3556
 with E. M. T. Jones, wide-band strip-line balun, 3931

- with E. M. T. Jones, wide-band strip-line balun, 3931
 Shimmins, A. J., radio telen etry, 3084
 Shimoda, K., beam-type maser, 389
 Shimn, D. H., aerial requirements for ionospheric scatter communication, 2000 g; health hazards from radio transmissions, 2074
 Shipley, D. G., with others, 468-Mc/s tropospheric scatter propagation, 245
 Shipley, W. S., with others, instrumenting Explorer I satellite, 1547
 Shipman, J. S., with others, multiple Fourier analysis in rectifier problems, 2382
 Shiren, N. S., and E. B. Tucker, spin-phonon interaction in ruby, 2317
 with others, effects of 9.2-kMc/s ultrasonics on resonances in quartz, 3816
 Shirk, W. H., Jr, with others, temperature fluctuations accompanying solar eclipse, 2559
 Shiroo, I., with others, then Pratice BaTiO₃ ceramics, 479
 Shkarofsky, I. P., H. E. J. Neugebauer and M. P.

- electric properties of polarized BaTiO, ceramics, 479
 Shkarofsky, I. P., H. E. J. Neugebauer and M. P. Bachynski, effect of mountains with smooth crests on wave propagation, 3458
 Shklovskii, I. S., and P. V. Shcheglov, optical observations of earth satellites, 3288
 with others, radio-astronomy investigation by earth satellites, 3292; discovery of 10-keV electrons in upper atmosphere, 3294
 Shmatov, V. T., with G. V. Skrotskii, thermodynamic theory of resonance and relaxation dynamic theory of resonance and relaxation phenomena in ferromagnetics, 538
 Shmelev, I. I., with A. N. Barkhalov, attenuation of sound beam traversing layer of discontinuity, 669
 Shnurer, F., aperture-coupled filters, 1112
 Shockley, W., and J. Gibbons, current build-up in semiconductor devices, 889; transient build-up in avalanche transistors, 2416
 with others, avalanche-transistor pulse circuits,

- with others, avalanche-transistor pulse circuits, 2878
- Shodin, L. F., with others, tracking earth satellites, 123
- 123
 Shoemaker, R. F., with others, voltage-sensitive switch, 39
 Sholokhova, E. D., with others, nonferroelectric phase transitions in solid solutions, 1912
 Short, G. W., transistorized absorption wavemeter, 1979

- Short, G. W., transistorized absorption wavemeter, 1979
 Shorter, D. E. L., high-quality monitoring loud-speakers, 333
 Shotov, A. P., with B. M. Vul, edge breakdown of p-n junction in Ge, 1616
 Shou-syan' Fan, with A. A. Kolomenskii, cyclic motion of charged particles in electric field, 3835
 Shpigel', I. S., with M. D. Raizer, microwave investigation of plasma, 3262
 Shteinshleifer, Z., with others, absorption of com-pressional waves in solids, 3536
 Shtepa, N. I., graphical-analytical plotting of particle trajectories, 1832, 3630
 Shtrum, E. L., with others, new semiconducting compounds, 3755
 Shul'man, A. R., and others, secondary emission from Ni, 3789
 Shulman, R. G., Co⁵⁹ nuclear magnetic resonance in paramagnetic salts, 3409

- in paramagnetic salts, 3409 Shul'man, S. G., with Yu. I. Ukhanov, influence of intense electric field on Ge-diode transparency, 1921
- 1931

- Shuppe, G. N., with others, e.s. electron emission of semiconductors, 1922
 Shuppe, G. N., with others, e.s. electron emission of semiconductors, 1922
 Shutllov, V. A., with 1. G. Mikhallov, diffraction of light by ultrasonic waves, 678
 Shvidkovskii, E. G., with others, pressure and density measurements in high atmosphere by earth satellites, 3694
 Sidel, T., with R. Husimura, effects of impurities and temperature on electroluminescence spectra, 152
 Sideris, G., production machinery for electronics industry, 1037; insulation for electronic equipment, 1296; magnet-wire insulation, 1635; powdered magnets, 1961
 Sidorov, A. I., with others, distribution of non-equilibrium charge carriers in base region of p-n junction, 1919; lifetime of non-equilibrium charge controlled swept-frequency RC oscillator, 1125
 Siegel, K. M., with others, U.R.S.I. report on antennas and waveguides, 3565; radar cross-section of finite cones, 4073
 Siegman, A. E., phase-distortionless limiting by parametric method, 1819
 and others, travelling-wave solid-state masers, 2891
 with others, reduction of electron-beam noise, 1728

- with others, reduction of electron-beam noise, 1728
- 1728
 Siekanowicz, W. W., and F. E. Vaccaro, periodic e.s. focusing of electron beams, 2061
 Sihvonen, Y. T., with D. R. Bcyd, growing CdS single crystals, 1905
 D. R. Boyd and C. D. Woelke, properties of green and red-green luminescing CdS, 2621
 Silberstein, R., pulse-propagation experiment on 20.1 Mc/s, 240

- I.28

- Silkin, B. I., with V. V. Belousov, international scientific collaboration, 3674
 Silver, P., with others, radar echoes from Venus, 2556
 Silverman, R. A., scattering of plane waves by dielectric noise, 415; fading of scattered radio waves, 3450
 Silverman, S. J., and J. B. Singleton, preserving lifetime in diffused Si, 2288
 Silverstein, A. N., quartz crystal testing, 1642
- Silverstein, A. N., quartz crystal testing, 1642 Silverster, D. D., measuring techniques for back-ward-wave oscillators, 3524 p
- ward-wave oscillators, 3524 p
 Sim, A. C., surface recombination velocity and photoconductive decays, 498
 Simhi, M., and M. Birk, sensitive single-channel pulse-height analyser, 59
 Simmons, B. D., saturable-transformer switches, 1471
 Simmons, C. D., with C. C. T.

- Mindons, B. D., saturable-transformer switches, 1471
 Simmons, C. D., with C. G. Thornton, high-current mode of transistor operation, 1004
 Simmon, S. R. O., lattice parameter changes in deuteron-irradiated Ge, 2307
 Simon, G., damping of h.f. elastic waves in ferromagnetic crystals, 1278
 Simon, J. C., G. Broussaud and E. Spitz, superdirectivity of aerial, 3572
 Simon, J. M., network analysis of transducers, 352
 Simon, P., geomagnetic activity and eruptions, 113
 Simon, R., with F. Pradal, energy spectrum of secondary electrons, 1838
 Simon, Y., and J. Bok, photoconductivity of ZnTe, 3726
 Simonyi, K., accelerator with 800-kV cascade

- 3726
 Simonyi, K., accelerator with 800-kV cascade generator, 1657
 Simpson, A. W., with others, anomalous polarization in ferroelectrics, 1911
 Simpson, O., optical characteristics of semiconductors, 3011

- Simpson, Co., Optical characteristics of semi-conductors, 3011
 Sims, C. C., underwater sound transducers, 2445
 Sinani, S. S., with others, thermoelectric properties of Bi.Tc₃-Bi₂Se₃, 3758
 Sinel'nikov, M. S., electron emission from Mo after electron bombardment, 3258
 Singer, D. F., with R. F. Ruiz, properties of experi-mental 1-kMc/s transistors, 3510
 Singer, J. R., with R. Chu, thin-film magnetization analysis, 3394
 and S. D. Johnson, transistorized nuclear-resonance magnetic-field probe, 1810
 with S. D. Johnson, current regulator using transistors, 979
 with others, radiation damping effects in 2-level maser, 1818
 Singer, S. F., cause of minimum in earth's radiation belt, 4038
 Singh, A., and R. A. Rao, ferrite-tuned magnetron,

- Singer, S. F., cause of minimum in earth's radiation belt, 4038
 Singh, A., and R. A. Rao, ferrite-tuned magnetron, 3163
 Singh, C., noise spectra of probe in hot-cathode discharge, 4019
 Singh, C., noise spectra of probe in hot-cathode discharge, 4019
 Singh, S., with others, hourly median field strength of 1940-Mc/s signal, 255
 Singleton, J. B., with S. J. Silverman, preserving lifetime in diffused Si 2288
 Sinno, K., hit nates of radio proparation disturbance warnings, 116: solar flare as source of geomagnetic storm, 433; characteristics of solar outbursts, 2558
 Sirs, J. A., correcting for response time delays of measuring equipment, 551; galvanother feedback systems, 2707
 Sirvetz, M. H., with S. L. Blum, magnetic resonance studies in reaction of Ni-Co ferrite, 3042
 with others, high-power L-band resonance isolator, 3563
 Siukola, M. S., travelling-wave television transmitting antenna, 1094
 Sivaraman, K. R., with K. S. Raja Rao, lunar geomagnetic tides at Kodaikanal, 1534

- mitting antenna, 1094
 Sivaraman, K. R., with K. S. Raja Rao, lunar geomagnetic tides at Kodaikanal, 1534
 Sivertsen, E., with others, segmentation techniques in speech synthesis, 1059
 Skanavi, G. I., and others, relaxation polarization and losses in nonferroelectric dielectrics, 480
 with A. N. Gubkin, stability of inorganic polycrystalline electrets, 1603
 Skilliman, T. L., and P. L. Bender, measurement of earth's magnetic field, 112
 Skinner, N. J., J. Hope and R. W. Wright, horizontal drift measurements near enuator, 1557
 with R. W. Wright, lunar tides in E. layer, 1880
 Sklar, B., reducing distortion in class-B amplifiers, 2883
 Skomal, E. N., and M. A. Medina, medium-power

- Sklar, B., reducing distortion in class-B amplifiers, 2883
 Skornal, E. N., and M. A. Medina, medium-power microwave limiter, 2468
 Skrotskil, G. V., and Yu. I. Alimov, ferromagnetic resonance in circularly polarized e.m. field, 3646
 and A. A. Kokin, system of magnetic moments in weak variable magnetic field, 3644
 and L. V. Kurbatov, anisotropy of width of ferromagnetic resonance absorption lines, 2210
 and V. T. Shmatov, thermodynamic theory of resonance and relaxation phenomena in ferromagnetics, 538
 Skuridin, G. A., and L. V. Kurnescva, scientific investigations by earth satellite, 440
 Skwirzynski, J. K., and J. C. Thackrav, transmission of em. waves through wire gratings, 3963
 Sladek, R. J., magnetically induced impurity banding in n-InSb, 1263
 Slanavi, G. I., with A. N. Gubkin, stability of inorganic polycrystalline electrets, 1603
 Slee, O. B., with others, radio sources between declinations +10° and -20°, 423; pencil-beam survey of galactic plane at 3.5 m, 2220
 Sletten, C. J., G. R. Forbes, Jr, and L. F. Shodin, tracking earth satellites, 123
 Sliedregt, M. van, waveguide filter theory, 53
 Slinkman, R. W., tube developments for guidedmissia explications, 310
 Sloan, D. J., with R. W. Berry, Ta printed capacitors, 2867

- Sloan, D 2867

- Slotnick, D. L., with H. S. Shapiro, mathematical theory of error-correcting codes, 1683
 Slykhouse, T. E., and H. G. Drickamer, effect of pressure on absorption edge of Ge and Si, 1243
 Smakula, A., and J. Kalnajs, O₂ impurity in Si single crystals, 511
 Smale, J. A., field-strength recordings and performance of v.s.w. radio links, 2014 f
 Smejkal, J., and L. Mollwo, measurement of u.h.f. quadripole, 1968
 Smetana, C., first- and second-order gradient receivers, 1757; gradient receiver for intercommunication, 2094
 Smilga, V. P., and B. V. Deryagin, role of surface properties of semiconductors in adhesion, 495
 Smirnov, B. G., with others, c.s. electron emission of semiconductors, 1922
 Smirnov, L. S., measurement of short lifetimes of charge carriers in Ge, 1930
 Smith, A., and D. Dutton, behaviour of PbS photocells in ultraviolet, 1407
 Smith, A. G., T. D. Carr and W. H. Perkins, night-tive properties of semiconductor of the properties of the properties of the properties of the properties of properties of semiconductor, 1922

Smith, R. W., properties of deep traps, 1901
 and F. J. Hyde, transistor current gain, 3426
 Smith, S. T., with others, beam noise in crossed electric and magnetic fields, 313
 Smith, W. B., with others, reciprocity of ionospheric transmission, 1667; radar echoes from Venus, 2556

Smith, W. V., J. Overmeyer and B. A. Calhoun, microwave resonance in Gd-Fe garnet crystals, 3043

with others, multiple quantum transitions in

microwave resonance in Gd-Fe garnet crystals, 3043
with others, multiple quantum transitions in paramagnetic resonance, 1856
Smith-Rose, R. L., electron-density profiles in ionosphere, 438; international radio organizations, 1036; position finding by radio, 2978 a
Smits, F. M., with R. L. Batkorf, diffusion of impurities into evaporating Si, 1925
smolenskii, G. A., A. I. Agranovskaya and S. N. Popov, effect of polatization on Pb₂NiNb₂O₂-Pb₂MgNb₂O., 2631
V. A. Isupov and A. I. Agranovskaya, new ferroelectric, 2632
and others, nonferroelectric phase transitions in solid solutions, 1912
Smyth, H. R., with others, distress beacon for crash position indicator, 1891
Snitko, O. V., influence of adsorption on photoconductivity of Cu₂O, 3733
Snow, W. B., impedance-matched or optimum, 37
Snyder, C. W., upper boundary of Van Allen radiation belts, 4039
Soyder, D. D., and C. E. Bleil, mechanism for carrier excitation in CdS, 3004
Snyder, R. H., video time-delay systems, 3867
Sobey, A. B., thernistor compensation of resistance and conductance, 721; thermistors for linear temperature readings, 2469
Sodha, M. S., and D. B. Agrawal, low-field mobility of carriers in nondegenerate semiconductors, 164
and Y. P. Varshni, fully ionized gas, transport phenomena in, 3753, transport properties of, 3754
Solomon, A. H., and F. Sterzer, mag microwave ferrite modulator, 1107
Solomon, B. D., and C. S. Broneer, constant-S equalizers, 3226
Solomon, J., relaxation in magnetic resonance, 2542
Solmon, A. H., and F. Sterzer, mag microwave ferrite modulator, 1107
Solomon, B. D., and C. S. Broneer, constant-S equalizers, 3226
Solomon, J., relaxation in magnetic resonance, 2542
Solmon, J., vith others, magnetostatic modes of ferrimagnetic spheres, 3813
Solymar, L., stepped transmission-line transformers, 3594
with

3594
with P. Foldes, lens-aerial design, 1100
Somayajulu, Y. V., and N. N. Rao, galactic radiation at 30 Mc/s, 3699 i
Somerville, M. J., with E. M. Dunstan, l.f. noise reduction in feedback integrators, 369
Sommers, H. S., Jr, tunnel diodes as h.f. devices, 3565

3505
 Sonder, E., properties of reactor-irradiated Si, 4100
 Sondheimer, E. H., with J. E. Hebborn, diamagnetisn of conduction electrons in metals, 2194
 Sonett, C. P., with others, ionizing radiation at 3 500-36 000 km, 3691

Electronic & Radio Engineer

3505

- Sonkin, S., with others, high-power windows at microwave frequencies, 3159 c
 Sonnenfeldt, R. W., with T. Murakami, detection of asymmetric-sideband signals in presence of noise, 248

- asymmetric-sideband signals in presence of noise, 248
 Sorensen, H. O., with cthers, magnetostrictive delay line for video signals, 1134
 Sorenson, J., with others, earth's gravitational potential from satellite orbit, 1867
 Sorokin, O. V., with G. E. Pikus, measuring magnetic field intensity, 1972
 with others, detern ination of surface recombination velocity, 500
 Sorokin, P. P., 1. L. Gelles and W. V. Smith, multiple quantum transitions in paramagnetic resonance, 1856
 Sosin, B. M., with V. O. Stokes, wide-band amplification at h.f., 3203
 Soule, D. E., magnetic-field dependence of Hell 27.

- 3200
 Soule, D. E., magnetic-field dependence of Hall effect and magnetoresistance in graphite, 1239; analysis of galvanomagnetic oscillations in graphite, 1240
 Sowton, C. W., and G. A. C. R. Britton, radio inter-ference, 954
 Spaapen, J. B. M., with others, diffusion capacitance in transistors, 3148
 Sparkes, J. J., measurement of transistorequivalent-circuit narameters 1646

- circuit parameters, 1646 Spear, W. E., surface effects in electron-irradiated Ge, 873

- Spear, W. E., surface effects in electron-irradiated Ge, 873
 Spears, R. A., thermally compensated crystal oscillators, 370
 Spector, J. O., with T. Tamir, swept-frequency klystron operation, 3524 hh
 Spelght, C. S., Miller sweep circuit, 743
 Spelnrire, R. J., with L. L. Bailin, radiation fields from slots in circular cylinders, 1093
 Spence, R. D., and R. D. Ewing, antiferromagnetism in Cu₃(CO₃)₃(OH)₃, 1947
 Spencer, D. E., with P. Moon, solution of integral equations, 209
 Spencer, E. G., and R. C. LeCraw, magnetoacoustic resonance in Y-1^e garnet, 201
 R. C. LeCraw and A. M. Clegston, low-temperature line-width maximum in Y-Fe garnet, 3812
 with others, poincowave semiconductor switching
- 3812
 with others, microwave semiconductor switching techniques, 3597
 Spencer, H. E., spectral response of PbS thin films, 2994; photoconductance and time constant in PbS films, 3323
- Spenke, E., induction behaviour of *p-n* rectifiers, 2036
- 2036
 Spetner, L. M., model for forward scattering off rough surface, 1518
 Speyer, N. B., with others, diffusion capacitance in transistors, 3148
 Spicer, W. E., studies of alkali-antimony compounds, 825; influence of defect levels on photoemission, 1206
 Spiegel, E. F., applications of industrial television,
 Calify and W. L. Tailing therebold elevation

- 1206
 Spiegel, E. F., applications of industrial television, 1395
 Spieth, W., and W. J. Trittipoe, threshold elevation produced by noises, 682; noise exposure and temporary threshold shifts, 1053
 Spinrad, R., core-saturation blocking oscillator control, 3989
 Spirin, G. S., with others, e.s. electron emission of semiconductors, 1922
 Spitzer, C. F., lunistors, 3884
 Spitzer, W. G., and J. M. Whelan, infrared absorption and effective mass in n-type GaAs, 3383
 D. A. Kleinman and C. J. Frosch, infrared properties of SiC film, 2298
 D. Kleinman and D. Walsh, infrared properties of SiC film, 2298
 D. J. Kleinman and D. Walsh, infrared properties of SiC film, 2298
 Spitzer, C. F., Igras and I. S. Zheludev, domain structure of feroelectrics, 158
 Sponer, D. J., checking crystal oscillators, 372
 Spracklen, J. G., W. Stroh and G. C. Wood, noisegated ag.c. and sync system, 1382
 Sprenger, K., ionospheric drift measurements in long-wave range, 1198
 springer, A. M., regulator of speed and pitch for recordings, 2825
 Springer, H., with others, detail recognition on television screen, 3135
 Sproule, D. O., with P. Smith, experiments on the acousto-electric effect, 4009
 Sprung, H. B., with M. von Ardenne, ingestible intestinal transmitter, 1327, 3834
 Squires, R. K., with others, Vanguard measurements of earth's figure, 2236
 Srkantaswamy, M. N., and K. K. Nair, matrix analysis of valve circuits, 2497
 Srlvastava, G. P., with S. Swarup, directivity pattern of 3-cm parabolic reflector, 2474
 Stibalein, H. G., with others, theory of multiple lines, 2458
 Stacey, F. D., fluctuating-field ferromagnet at low temperatures, 536; thermal activation of ferromagnet at low temperators. 275
- 2458
 Stacey, F. D., fluctuating-field ferromagnet at low temperatures, 536; thermal activation of ferromagnetic domains, 1275
 Stadler, H. L., ferroelectric switching time of BaTiO, crystals, 478
 Stafeev, V. I., current multiplication in nonideal p-n junction, 1626
 Staflin, T., with L. Huldt, infrared absorption of photogenerated carriers in Ge, 176; valenceband structure of Si, 508
 Stagg, J. M., and B. Hultqvist, auroral isochasnus, (D)4062

- Stagg, J. M (D)4062

- Stahl, F. A., and G. Dermit, Ge photo-tetrode, 308
 Stampfl, R., with others, current amplification of junction transistor, 631; tracking weather with satellites, 2715
 Stankowski, J., with Z. Pajak, polarization changes during aging of BaTiO₃-type ferroelectrics, 844
 Staras, H., antenna-to-medium coupling loss, 235

 and A. D. Wheelow, theoretical research on tropospheric scatter propagation, 3846

 Stark, R., coupling between vibrations of AT-cut crystal plates, 3975
 Starkey, B. J., and others, atmospheric discontinuity layer effects on propagation, 2000 ø
 Statz, H., with G. F. Koster, Zeeman splittings of paramagnetic ions, 2549
 Stavitskaya, T. S., with others, thermoelectric properties of PbTe, 1941
 Stearker, A., nicrowhony in electron tubes, 1013
 Steele, M. C., electrical breakdown in n-InP, 4116
 and F. D. Rosi, thermal conductivity and thermoelectric power of Ge-Si alloys, 528
 L. Pensak and R. D. Gold, pulse amplification using impact ionization in Ge, 2882
 with dikers, single phonon emission in breakdown with others, single phonon emission in breakdown

- 3388
- with others, single phonon emission in breakdown of semiconductors, 3013
 Stein, F., N. G. Einspruch and R. Truell, temperature
- dependence of fractional velocity changes in Si, 3355

- dependence of fractional velocity changes in Si, 3335
 Steinberg, J. L., with M. Pick-Gutmann, 16-aerial array at 9 300 Mc/s, 3659
 Steinberg, J. L., with M. Pick-Gutmann, 16-aerial array at 9 300 Mc/s, 3659
 Steinberch, K., automatic character recognition, 1991; automatic speech recognition, 3913
 Steinermann, A., and H. Gräwicher, dielectric properties of ice crystals, 1600
 Steiner, F., and H. Stittgen, reduction of bearing errors in long-base-line systems, 3720
 Steinert, L. A., geometrical anisotropy of magnetic materials in waveguides, 3809
 Stepanov, K. N., kinetic theory of magnetohydrodynamic waves, 767; damping of e.m. waves in plasma, 2201; low-frequency oscillations of plasma, 3639
 Stephen, J. H., with R. C. M. Barnes, operating experience with transistor digital computer, 2132
 Stephenson, I. M., with A. L. Cullen, experimental investigation of velocity-modulated electron beams, 3524 g
 Stephenson, M., with M. Mark, air-cooled chassis for electronic equipment, 353
 Stepherson, W. L., transistor d.c. converter circuit, 1698

- Stephenson, W. L., transistor d.c. converter circuit, 1698

- 1698 (m) E., transfer E.: Control endowing 1698
 Stern, E., and R. S. Mangiaracina, ferrite high-power effects in waveguides, 3937
 Stern, F., and J. R. Dixon, narrowing energy gap in semiconductors by compensation, 1917
 Sternberg, R. L., J. S. Shipman and S. R. Zohn, multiple Fourier analysis in rectifier problems, 2382
 Sterne, T. E., motion of satellite around unsymmetrical central body, 1866
 with G. F. Schilling, densities and temperatures of upper atmosphere from satellite observations, 1871
 Sternett, J. E., and H. Heffner, periodic magnetic

- 1871
 Sterrett, J. E., and H. Heffner, periodic magnetic focusing structures. 1021
 Sterzer, F., pulse amplifier with sub-mµs rise time, 1135; random-number generator, 2476; narametric oscillators for digital computing, 3590
 with D. J. Blattner, backward-wave oscillator tubes for 29-74-kMc/s range, 1740; voltage-tunable inni-wave oscillators, 3529
 with A. H. Solomon, mus microwave ferrite

- tunable inn-wave oscillators, 3529
 with A. H. Solomon, inμs microwave ferrite modulator. 1107
 Stevens, E. E., with others, frequency prediction techniques for high latitudes, 2729
 Stevens, E. J., with A. C. Hudson, data on ferrite core materials, 897
 with T. D. Northwood, acoustical design of Alberta Jubilee Auditoria, 688
 Stevens, K. W. H., wave-inechanical damped harmonic oscillator, 739; inicrowave physics, 1171
- 1171
 Stevenson, A., with S. Prussin, infrared strain-optic coefficient of Si, 2295
 Stevenson, M. H., ATN television centre, 3130
 Stevenson, M. J., with D. C. Mattis, theory of negative-mass cyclotron resonance, 3760
 Stewart, J. L., and E. C. Westerfield, active sonar detection, 2596
 Stickler, D. C., e.n. diffraction by dielectric strips, 1516

- Isile Construction of the second se

- stratton, A. W., with C. W. Tolbert, absorption of num waves over extended ranges, 246
 with athers, phantom radar targets at nm A, 3315
 Stram, O. B., with T. C. Chen, digital memory system, 2129
 Strandberg, M. W. P., with M. Peter, efficiency of frequecy measurements with atomic clock, 1311
 with others, electron spin-lattice relaxation times, 417; maser amplifier with large bandwidth, 1144
 Stratton, R., hot-electron effect in n-type Ge, 175
 Straube, G. F., voltage-variable capacitor, 46
 Strattend, P. R., transistor thermal equivalent circuit, 1720
 Strickla, V. I., with others, lifetime of injected current caricers in Sb-doped Ge, 1932
 Strocht, G., radio-link equipment for 60-120 channels, 2013
 Strotor, G. E., aspects of short-range rho-theta systems, 2259 h
 Strotzer, G., electrical absorption of gases, 2986
 Struther, J. D., with G. Bemski, An in Si, 2290
 Strutter, J. D., with G. Bemski, An in Si, 2290
 Strutter, J. D., with G. Bemski, An in Si, 2290
 Strutter, G. A, and B. Gossich, Dember-pote

Stittgen, H., with F. Steiner, reduction of bearing errors in long-base-line system, 3720
Stockford, M. T., with B. H. L. James, microwave frequency standard, 1300
Stöckmann, F., and others, photoconduction of Ge after bombardment, 3027
Stoddart, H. F., nucleonics instrumentation-scalers, 3446

- Stoeckert, A. J., with others, moulded Ni cathode,
- 2060
- 2009
 Stoffregen, W., l.f. radio reflections during intense aurora, 812
 Stokes, V. O., and B. M. Sosin, wide-band amplifi-cation at h.f., 3234
- cation at h.f., 3234
 Stoiz, H., depolarization in small conducting bodies, 3631
 and H. W. Streitwolf, secondary electron emission of metals, 3257
 Stone, G. M. C., I.G.Y. progress report, 114
 with C. E. Newton, I.G.Y. v.h.f. programme, 115
 Stone, H. A., Jr, field-effect tetrodes, 3152
 with others, semiconductor current limiter, 1368
 Stone, M. L., with others, u.h.f. signals reflected from moon, 1525
 Stone, K. E., microwave multiplexing circuits, 2465
 Storey, L. R. O., and J. K. Grierson, time-symmetric filters, 365
 with C. O. Hines, time constants in geomagnetic storm effect, 1535
 Stoyko, A., apparent velocity of s.w., 1333 k
 and N. Stoyko, random variation in speed of rotation of earth, 1301
 Stoyko, N., with A. Stoyko, random variation in speed of rotation of earth, 1301
 Stracca, G. B., i.f. circuits with 3 coupled resonators, 1803
 Strachan, C., and A., M. Murray, spin-orbit Stolz, H., depolarization in small conducting bodies,

1803
Strachan, C., and A. M. Murray, spin-orbit coupling and extraordinary Hall effect, 1952
Strack, W., systems engineering of personal radio signalling systems, 3478
Strafford, F. R. W., second band-III program, 1775; band-III aerial problem, 2122
Straiton, A. W., with C. W. Tolbert, absorption of mm waves over extended ranges, 246
with chters, phantom radar targets at nm A, 3315
Stram, O. B., with T. C. Chen, digital memory system, 2129
Strandberd M. W. P. with M. Peter, efficiency of

Sucksmith, W., with others, ferromagnetic alloys, properties of, 1631, magnetization of, 3392 Sugai, I., numerical solution of Laplace's equation, 3050

Suhl, H., and B. T. Matthias, impurity scattering in superconductors, 3633
 Suhrmann, R., contrast filters for television sets, 2765

- Suhl, H., and B. T. Matthias, impurity scattering in superconductors, 3633
 Suhrmann, R., contrast filters for television sets, 2765
 G. Wedler and E. A. Dierk, temperature dependence of electron emission of Biflins, 2619
 Suita, T., with others, e.s.-transformer-type particle accelerator, 3071
 Sulanke, H., with others, equalization in television transmission by cable, 3468
 Sumni, M., excitation of oscillations in plasma layer, 1513; theory of excited plasma waves, 2534
 Sumner, F. H., with others, automatic recognition of patterns, 2172, 3998
 Surplice, N. A., reversible poisoning of oxide-coated cathodes, 4249
 Süsskind, C., with others, design of transition region of beam valves, 1017
 Sutcliffe, H., digital voltmeter, 2355
 and D. J. Matthews, transistor junction temperature, 1974
 Sutverkrop, B., with others, capabilities of coaxial cable, 2457
 Suzuki, M., with T. Hayosaka, errors of electroacoustic standards, 3186
 Svechnikov, S. V., photoconductive properties of CASe, 469; parameters of ASS barrier-layer photocells, 638; conductivity of CASe under X-ray excitation, 1906
 and V. T. Aleksandrov, photoelectric properties of CASe, 469; parameters, discovery of 10-keV electrons in upper atmosphere, 3294
 Svirskii, M. S., with S. V. Vonsovskii, absence of superconductivity in ferromagnetics, 195
 Swanckamp, F. W., with others, line width in Y-Fe garnet, 2330
 Swarue, G., and R. Parthasarathy, solar brightness distribution at 60 cm, 430
 Swarue, S. J., J., W., Michers, discovery of 10-keV electrons in upper atmosphere, 3294
 Svirskii, M. S., With S. V. Vonsovskii, absence of superconductivity in ferromagnetics, 195
 Swancean, F. W., with others, line width in Y-Fe garnet, 2330
 Swarue, S., and G. P. Sriuastava, directivity pattern of 3-cm parabolis

- 2511
 Swift, J., wide-band thermistor mounts, 564
 Swift, J. W., application of analogue calculation to flight simulators, 1466
 Swift-Hook, D. T., dispersion curves for helix, 3159 m

- Swift-Hock, D. T., dispersion curves for helix, 3159 w
 Sydnor, R. L., with T. R. O'Meara, balun transformer for v.b.f. and u.h.f., 338
 Sykes, M. F., with M. E. Fisher, Ising model of ferromagnetism, 3263
 Sylvan, T. P., bistable circuits using unijunction transistors, 744; transistor d.c.-a.c. beta tester, 1647; 2-terminal solid-state switches, 2040; solid-state thyratrons, 2046
 Symmons, H. F., with G. S. Bogle, paramagnetic resonance of Fe⁺⁺ in sapphire, 1949; zero-field masers, 2889
 Sze, T. W., with P. E. Lego, obtaining transient resonase using digital computer, 2130
 Szente, P. A., with others, centipede aerial, 1333 u
 Szöke, A., and S. Meiboom, radiation damping, 2543
 Szulkin, P., reflection of e.u. waves in ionosphere, 2728

- Szulkin, P., reflection of e.m. waves in ionosphere, 2728
 Szulkin, P., reflection of e.m. waves in ionosphere, 2728
 Tabuchi, S., with others, radio observation of satellite 1957a, 446
 Taft, E. A., H. Philipp and L. Apker, excitoninduced photoemission from BaO, 2264

 with H. R. Philipp, optical constants of Ge, 2659
 Tagholm, L. F., with others, tropospheric wave propagation measurements by B.B.C., 2000 m
 Taguchi, Y., with others, radio observation of satellite 1957a, 446
 Tait, D. A. G., with M. D. Johnson, filter attenuation characteristics, 731
 Takahashi, H., with others, electron and ion density distributions in F region, 2579
 Takahashi, Y., with others, nutually coupled C.Y. pedirectional coupler, 9
 Takahashi, Y., with others, nuturally coupled C.Y. with others, nuturally coupled C.Y. pedirectional coupler, 9
 Takahashi, Y., with others, nutrowave propagation over sea beyond line of sight, 2734
 Takahashi, Y., with others, nutrowave propagation nethod of studying decaying gas plasmas, 4021
 Takenoshita, Y., with Y. Hakura, s.w. transmison disturbance of 114 Feb. 1985, 573
 Takeuchi, K., with S. Okamoto, dielectric loss of oxidized high-density polyethylene, 3443
 Taus, G. G., with P. S. Zyryanov, acoustic electrical phenomena in degenerate plasma, 3638
 Tamir, T., and J. O. Spector, swept frequency, Mystron operation, 3524 Ar.
 Tamaoka, I., with others, effect of solar eclipse on crystals, 2625
 Tanguch, S., with others, ferromagnetic domainstructure in Co-Ni crystal, 192

- Tannenbaum, E., with others, stabilization of Si surfaces by thermally grown oxides, 2650
 Tannenwald, P. E., with M. H. Scavey, Jr, direct observation of spin-wave resonance, 191
 Tanner, W. P., Jr, what is masking?, 3541
 and T. G. Birdsall, definitions of d' and n, 3854
 Tantilla, W. H., with D. A. Jennings, frequency modulator for marginal oscillator, 1826
 Tantry, B. A. P., and R. S. Sriusstava, polarization of atmospherics by successive reflections, 143; waveforms of atmospherics, 459, with superimposed pulses, 815
 Tanzman, H. D., high-accuracy time-interval measurements, 3418
 G. A. MacLeod and W. T. Scott, Doppler satellite measurements, 1191
 Tao, K., radio scattering in terms of ionosphere turbulence, 236

- Tao, K., radio scattering in terms of ionosphere turbulence, 236
 Taratynova, G. P., motion of artificial satellite, 3682
 with others, determination of lifetime of artificial earth satellite, 3681
 Tartagila, A. A., with F. A. Trumbore, resistivities and hole mobilities in Ge, 519
 Tartakovskii, B. D., ultrasonic interference filters, 677; diffraction of sound waves in converging beams, 2813
 with B. F. Podosheumikov, attenuation of plane sound waves, 2809
 Tartu, Y., measurement of transistor cut-off frequency, 2705
 Tastenoy, R., development of s.w. telegraphy systems, 1686
 Tattersall, R. L. O., frequency meter for 3975-4275 Mc/s, 4161
 Taylor, D. F., alloy junctions in semiconducting devices, 888
 Taylor, R. J., thermal structures in lower atmosphere, 136
 Taylor, S., with others, processing Ni-matrix cathodes, 4250
 Taylor, W. E., with P. E. Cane, cooling high-power valves by vaporization, 654
 Taylor, W. E., with P. E. Cane, in the sate of the sate of

- valves by vaporization, 654
 Taylor, W. K., pattern recognition by automatic analogue apparatus, 2371
 Tchoubar, C., with A. Oberlin, shadow-casting carbon films for electron microscopy, 938
 Teal, R. H., with others, versatile stimulator, 229
 Teaney, D., with A. M. Portis, microwave Faraday rotation, 770
 Teboul, M., and N. Nilonteff, flicker effect in photovoltaic diodes, 639
 Teeter, W. L., and K. R. Bushore, microwave power divider and multiplexer, 1078
 Tetlord, M., tropospheric scatter system evaluation, 595

- 595
 Temko, K. V., with E. I. Adirovich, transition frequency and phase characteristics of tran-sistor, 634
 with others, field potential and charge carriers in fused-in junctions, 3787
 Teodorescu, I., investigation of r.f. properties of ferrites, 3815
 Terhune, R. W., with others, ruby as maser material, 3793

- 3793
 Terpugov, N. V., resolving power of automatic frequency analysers, 1969
 Tertlan, L., with J. J. Trillat, electron-microscope images without photographic emulsion, 1331
 Teunissen, H. A., television transmitter design, 3492
 Thackeray, D. P. C., constant-current/constant-voltage stabilizer, 605; selecting matched components. 659
- components, 659
- Thackray, J. C., with J. K. Skwirzynski, trans-mission of e.m. waves through wire gratings, 3963

- mission of e.m. waves through wire gratings, 3963
 Thain, R. S., with others, engineering of l.f. communication systems, 2750
 Tharma, P., public-address amplifiers using transistors, 68
 with J. F. Pamking, 4.5-W sliding-bias amplifier using OC16, 384
 Thayer, G. D., with B. R. Bean, models of atmospheric radio refractive index, 2725
 Thelle, R., operation of image orthicon, 3497
 and F. Pilz, television transmission of nontransparent still pictures, 1374
 Theis, M. E., divital storage on punched tape, 1785
 Theissing, H. H., F. A. Dieter and P. J. Caplan, analysis of emissive phase of pulsed maser, 756
 Theile, A. N., television i.f. amplifiers with linear phase response, 3117
 Thiele, A. P., magnetostrictive filters, 52
 Theile, A. P., magnetostrictive filters, 52
 Thiele, A. P., tegin of Sidwestfunk studio building, 3183

- Iniele, R., design of Südwestfunk studio building, 3183
 Thies, H., with H. Ehlers, synchronizing trans-mitter frequencies, 4224
 Thomas, D. E., and J. M. Klein, automatic transistor a measuring set, 3427
 with others, surface barrier height changes on transistors, 633
 Thomas, D. G., diffusion and precipitation of In in ZnO, 4111
 Thomas, J. A., and F. H. Hibberd, satellite Doppler measurements and ionosphere, 1874
 and E. K. Smith, survey of knowledge of E., 1879
 Thomas, J. B., with T. R. Williams, current noise and nonlinearity in carbon films, 3596
 Thomas, J. O., distribution of electrons in ionosphere, 1552
 and A. Robbins, electron distribution in ionosphere over Slough, 806

World Radio History

- Thomas, L., measurements of horizontal movements in region F, 2243
 Thomas, L. G., Tacan system, 461
 Thomas, S., with others, observations of detonation by interferometer, 3068
 Thompson, A. M., cylindrical cross-capacitor as standard, 3051
 and R. W. Archer, comparator for 100-kc/s frequency standards, 1299
 Thompson, B. J., intensity distribution near focus of diffracted waves, 3256
 Thompson, F. C., factors affecting life of magnetrons, 2788 f
 Thompson, G. T., with P. C. Butson, effect of flanges on radiation patterns, 3582
 with others, propagation measurements at 3 480 Mcfs, 2000 r
 Thompson, M. C., Jr., and H. B. Janes, phase stability over low-level tropospheric path, 4176
 and M. J. Vetter, microwave refractometer for aircraft, 1321
 and D. M. Waters, studying ionospheric structure using earth satellites, 799
 F. E. Freethey and D. M. Waters, ceranic X-band cavity resonators, 363
 Thompson, P. M., with others, lightweight airborne navigation system, 2599
 Thompson, P. M., application of phase-measuring techniques, 1895

Thompson, W. J., application of phase-measuring techniques, 1895
 Thomson, J. D., r.f. powers and noise levels in multichannel R/T systems, 598
 with B. W. G. Penhall, signalling for single-channel and mobile radio-telephone systems, 4200

Thomson, J. H., rotation of first Russian satellite, 1187 with others, radar observations of 1957β , 3290; ionospheric information from observations of

ionospheric information from observations of satellite 1957 a2, 3297
 Thomson, M. M., with others, Canadian standard of frequency, 2700
 Thorne, T. G., and J. A. Billings, Doppler navigation systems, 2608
 with G. E. Beck, airborne Doppler navigation equipment, 2259 e
 with J. E. Clegg, Doppler navigation, 2259 d
 Thornton, C. G., and C. D. Simmons, high-current mode of transistor operation, 1004
 Thornton, W. A., electroluminescent thin films,

Thornton, C. G., and C. D. Stmmors, high-current mode of transistor operation, 1004
Thornton, W. A., electroluminescent thin films, 1598; a.c.-d.c. electroluminescence, 3000
Thun, R., electron-diffraction apparatus for continuous recording, 3442
Thureau, P., with J. P. Leroux, photoluminescence of ZnS-Cu, 1908
Thurlow, E. W., with others, microwave model for study of s.w. aerials, 709
Tibbals, M. L., with others, vi.f. propagation measurements for Radux-Omega system, 2736
Tiberio, S., with others, characteristic parameters of barrier layer in metal/semiconductor junction diodes, 2415
Tiberio, U., echo filtering in radar, 2602
Tichy, J., equivalent circuit of oscillating piezo-electric rods, 1475
Tiemann, J. J., with others, observation of phonons during tunnelling in junction diodes, 4226
Tien, P. K., parametric amplification and frequency mixing in propagation of variable e.m., field medium, 2920

Tikhonov, A. N., propagation of variable e.m. field in stratified medium, 2920
 Tillman, J. R., transistors in line communications, 594

Tilman, J. R., transistors in line communications, 594
Timmins, E.W., with others, apparatus for measuring electrical resistivity of Si, 214
Tingley, G. R., with J. H. Haines, Vitascan flyingspot colour scanner, 279
Tipnis, C. B., with S. Parthasarathy, diffraction of light by ultrasonic waves, 1049, 1751
Tischer, F. J., resonant properties of nonreciprocal ring circuits, 2462
Tismer, W., with L. Keibs, measuring acoustic impedance of air spaces, 3180
Titheridge, J. E., variations in direction of arrival of h. f. waves, 941; ray paths in ionosphere, 2377
Tkalich, L. G., with E. K. Iordanishvili, semiconductor thermostat for self-oscillators, 609
Fobiack, P. L., Zener dodes stabilize heater voltages, 2759
Tobin, M., video differential planimeter, 3067
Toedter, H., with others, Telefunken traffic radar, 1898
Tol, A., with others, e.s.-transformer-type particle

1898
Toi, A., with others, es.-transformer-type particle accelerator, 3071
Tokunaga, K., with G. S. Verma, antiferromagnetism of CuF₂, 2H₂O, 1946
Tolansky, S., and A. F. B. Wood, interferometric studies on oscillating quartz crystals, 2335
Tolbert, C. W., and A. W. Straiton, absorption of min waves over extended ranges, 246
A. W. Straiton and C. O. Britt, phantom radar targets at mm A, 3315
Toil, J. S., with M. Lutzky, formation of discontinuities in nonlinear electrodynamics, 2914
Tolprigo, K. B., emission capacity of p-n junction, 496
with E. I. Kaplunova, temperature dependence

496
 with E. I. Kaplunova, temperature dependence of Hall coefficient in semiconductors, 1621
 Toman, K., geometrical properties for ionospheric propagation, 3848

propagation, 3848
Tomishima, H., with others, lattice scattering mobility in CdS, 2990
Tomita, K., theory of magnetic resonance saturation, 95; theory of magnetic double resonance, 2922
Tomlin, D. H., with others, Ge junction cells for photoelectric control circuits, 309
Tompkins, R. D., with P. J. Allen, instantaneous microwave polarimeter, 3432

Electronic & Radio Engineer

4200

- Topchiev, A. V., and others, producing polymers with semiconductor properties, 4121
 Torelli, G., with C. Rubbia, differential discrimination for fast pulses, 3990
 Toschi, R., with G. Sacerdot, potential of e.s. field and trajectories of charged particles, 1505
 Towle, A., with others, frequency stepper for propagation tests, 1485
 Towle, L. C., and J. A. Lockwood, cosmic-ray increases associated with solar flares, 2557
 Townes, C. H., with A. I. Schawlow, infrared and optical masers, 1857
 with others, maser amplifier for radio astronomy, 2892
 Townend, J. W., Jr, rocket and satellite

- 2892
 Townsend, J. W., Jr, rocket and satellite symposium, 1870
 Toyoda, H., with others, life tests of microphone carbon, 1758
 Traube, M. J., with others, split reflector for microwave antennas, 712
 Tredgold, R. H., with others, anomalous polarization in ferroelectrics, 1911
 Treharne, R. F., analogous transistor system design, 1796
 Trange S. N. electron guns for construct back
- Treneva, S. N., electron guns for cone-type beams, 2430 Trent, G. H., with others, extension of solar radio

- 2430
 Trent, G. H., with others, extension of solar radio spectroscopy, 2933
 Trevena, D. H., space-charge waves, 2058

 with J. R. Pickin, new development of monotron oscillator, 3524 aa

 Triebwasser, S., ferroelectric transition in triglycine sulphate, 157; ferroelectric transitions of KNbO₂-KT20, 3330
 Trigubenko, V. A., with others, relaxation polarization and losses in nonferroelectric dielectrics, 480
 Trillato, J. J., and L. Tertien, electron-microscope images without photographic emulsion, 1331
 Trinkus, J. W., pulse-forming networks, 375
 Trittipoe, W. J., residual effects of low noise levels on temporary threshold shift, 1054
 with W. Spieth, threshold elevation produced by noises, 682; noise exposure and temporary threshold shift, 1053
 Trivelpiece, A. V., with R. W. Gould, electron
- threshold shitts, 1095 Trivelpiece, A. V., with R. W. Gould, electro-mechanical modes in plasma waveguides, 2800 f Trodden, W. G., with others, evaporation of Ba from impregnated cathodes, 2792 Trofimov, K., anti-aircraft radiolocation techniques, 2004

- Trofimov, K., anti-aircraft radiolocation techniques, 2984
 Tröim, J., with L. Harang, angle of arrival of auroral echoes, 2254
 Troitskii, V. N., fading in u.s.w. radio links, 586
 Trolese, L. G., and L. J. Anderson, foreground terrain effects, 3457
 Troost, A., S.w. cathode-ray direction finders, 2256
 Troude, J., elimination of noise and interference on radar, 3319
 de Troye, N. C., classification and minimization of switching functions, 3048
 with H. J. Heijn, fast method of reading magnetic-core memories, 3587
 Truel, R., with others, temperature dependence of for colour TV receivers, 1324
 Truell, R., with others, temperature dependence of fractional velocity changes in Si, 3355
 Trumbore, F. A., and A. A. Tartaglia, resistivities and hole mobilities in Ge, 519
 C. R. Isenberg and E. M. Porbansky, solubilities of Sn in Si and Ge, 4094
 Trzeba, E., null-point band filters, 736
 Tsarev, B. M., development of thermionic cathodes, 2068
 Tseitlin, M. Z., frequency dividers using transistors, 371

- Tseitlin, M. Z., frequency dividers using transistors, 378

- 378
 Tseplyaev, V. I., with M. I. Kiselev, oblique shock waves in plasma, 1163
 Tsesevich, V. P., brightness fluctuations of second earth satellite, 2956
 Tsintsatize, N. L., with P. V. Polovin, longitudinal vibrations of electron-ion beams, 1835
 Tsuda, T., with others, ionospheric scattering, under influences of ion production and recombination, 4059, in electrodynamically controlled turbulence, 4060
 Tsukernik, V. M., with M. I. Kaganov, theory of kinetic processes in ferromagnetic dielectrics, 1285
- 1285

- Tsukernik, V. M., with M. I. Kaganov, theory of kinetic processes in ferromagnetic dielectrics, 1285
 Tubota, H., and H. Suzuki, Se photocells with artificial intermediate layers, 3158
 Tucker, D. G., signal/noise performance, of electroacoustic strip arrays, 2, of super-directive arrays, 329
 with V. G. Welsby, multiplicative receiving arrays, 3953
 Tucker, E. B., with N. S. Shiren, spin-phonon interaction in ruby, 2317
 with others, effects of 9.2-kMc/s ultrasonics on resonances in quartz, 3816
 Tukizi, O., diffraction of e.m. waves by earth's curvature, 3092
 Tulchin, H., u.h.f. transistor data, 2044
 Tunis, C. J., with others, lattice vibrations in Si by neutron scattering, 2291
 Tunkelo, E., with others, lattice vibrations in Si by neutron scattering, 2291
 Turner, H., galactic radio emission, 1176
 Turf, J., with others, multipactor effect, 3836
 Turner, D. R., electropolishing Si in HF solutions, 1245
 Turner, R. J., and P. Herman, transistor design for picture i.f. stages, 1385
 Turner, R. W., submarine antenna systems, 2469
 Turner, W. R., with others, amospheric disconinuity layer effects on propagation, 2000 o
 Tutovan, V., magnetic permeability in circular and longitudinal fields, 3645

- Electronic & Radio Engineer

- Tuttle, W. N., Zobel filters for Tchebycheff inser-tion loss, 1118
 Tuzzolino, A. J., piezoresistance constants of InAs,

- tion loss, 1118
 Tuzzolino, A. J., piezoresistance constants of InAs, 884
 with others, infrared detectors, 4239
 Tvanenko, I. P., with others, mechanism of terrestrial corpuscular radiation, 2216
 Tveten, L. H., with others, 1.G.Y. observations of F-layer scatter in Far East, 2733
 Tweet, A. G., vacancy clusters in dislocation-free Ge, 522; precipitation in semiconductors, 4089 n and W. W. Tyler, enhanced Cu concentration in Ge containing Ni, 521
 Twersky, V., calculation of, reflection coefficients, 1333 w
 Twiddy, N. D., with R. L. F. Boyd, electron energy distributions in plasmas, 3260
 Twisleton, J. R. G., transformation of admittance through matching section, 2111
 Twiss, R. Q., radiation transfer and possibility of negative absorption in radio astronomy, 2218; growth of electron space-charge and radio waves in moving ion streams, 4030
 Tychinskil, V. P., conductance of space-charge cloud in magnetron, 2425
 Tyler, W. W., with A. G. Tweet, enhanced Cu concentration in Ge containing Ni, 521
 Tyrrell, A. J., with K. G. Beauchamp, image converter equipment for observation of discharges, 3522
 Uberoi, M. S., and E. G. Cibbert, measurement of

- Uberol, M. S., and E. G. Gilbert, measurement of cross-spectral density of random functions, 2349 Uda, H., with others, measurement of attenuation by rain, 4187

- Uberol, M. S., and E. G. Gibert, measurement of cross-spectral density of random functions, 2349
 Uda, H., with others, measurement of attenuation by rain, 4187
 Uda, S., with others, hourly median field strength of 1940-Mc/s signal, 255
 Uebele, G. S., ferrite microwave limiters, 3943
 Uehling, E. A., with J. L. Bjorkstam, magnetic resonance and relaxation in KD₂PO, 3743
 Ueno, K., with S. Kanaya, h. I., propagation related to annular eclipse, 2730
 Uenohara, M., with others, Barkhausen-Kurz oscillator at cm A, 1486
 Uhlir, A., junction diodes in microwave circuits, 3189 n
 Uitgens, A. G. W., with others, temperature-stable transistor circuit, 71; protection device for stabilized line timebase circuit, 282; transistor circuits based on half-supply-voltage principle, 755; stabilization, of line output circuit, 989, of line and frame output circuits, 3123
 Ukhanov, Yu. I., frequency characteristic of Ge infrared diode modulator, 1721
 Umor, S. G. Shu'man, influence of intense electric field on Ge-diode transparency, 1931
 Ulinch, F., with others, nonlocal reflection in wave-guides of variable cross-section, 1766
 Unger, S. H., computer oriented toward spatial problems, 30
 Ungstrup, E., with J. Rybner, influence of auroral zone on communications, 1333 j
 Unterberger, R. R., microwave spectrometer tests electror resonance, 2211
 Unwin, R. S., geometry of auroral ionization, 137; movement of auroral echoes, 2593
 Unz, H., current distribution over cone surface, 2841
 Urakowitz, H., using cascading charts, 2513
 Usber, T., Jr, performance of class-B audio amplifiers with random noise signals, 2168
 Ussachevsky, V., with A. Moles, use of acoustic spectrograph, 1425
 Uyeda, R., with others, neception of radio waves from Russian earth satellite 1, 120
 Uyeda, R., with others, ffect of solar eclipse on geosmagnetic field, 2561

- Vaccaro, F. E., with D. J. Blattner, electrostatically focused travelling-wave tube, 1414
 with W. W. Siekanowicz, periodic e.s. focusing of electron beams, 2061
 Vaina Bappu, M. K., optical tracking of satellites, 3699 g.
- Vaina Bappu, M. K., optical tracking of satellites, 3699 q
 Vainshtein, L. A., electron waves in periodic structures, 1738; group velocity of damped waves, 1848; electron waves in retarding systems, 2062; nonlinear theory of travelling-wave valve, 2426
 Vakulov, P. V., with others, cosmic rays and terrestrial corpuscular radiation by cosmic rocket, 2331
 Valdes, L. B., circuit conditions for parametric amplification, 75; microwave mixer diode of improved conversion efficiency, 2414
 Valeev, Kh. S., N. G. Drozdov and A. L. Frumkin, investigations on Li-Zn ferrites, 1957
 Valiev, K. A., and Sh. Sh. Bashkirov, stimulated r.f. paramagnetic amplifiers, 2181
 Valko, I. P., theory of cardioid microphone, 2092
 with F. Fisher, new mechanism for generation of ficker noise, 1028
 Vallese, L. M., properties of hook transistors, 753;

- Vallese, L. M., properties of hook transistors, 753; transistor bias design, 1140
 Van Allen, J. A., Scientific Uses of Earth Satellites, (B)2595
 and L. A. Frank, radiation around the earth, 2553; radiation measurements with Pioneer IV, 4041 4041

- C. E. McIlwain and G. H. Ludwig, radio observa-
- C. E. McLindam and G. H. Luding, radio observations with satellite 19556, 2238
 Van Bueren, H. G., plastic creep of Ge single crystals, 2654
 Van Cakenberghe, J., with J. M. Gilles, photoconductivity and crystal size in evaporated CdS, 828

- J. L. Verhaeghe and J. Turf, multipactor effect, 3836 3836
 Vantine, H., Jr, and E. C. Johnson, transceivers compute distance, 146
 Van Uitert, L. G., F. W. Swanekamp and S. E. Hassko, line width in Y-Fe garnet, 2330
 Van Valkenburg, A., with others, infrared studies on Sio₂ and Geo, 205
 Van Vliet, K. M. See van Vliet, K. M.
 Van Zanten, P. G., with F. H. R. Almer, transistor pyrometer, 3424
 Varnerin, L. J., transistor base transit analysis, 2417

varierin, L. J., transistor base transit analysis, 2417
Varshni, Y. P., with M. S. Sodha, fully ionized gas, transport phenomena in, 402, electron mobility in, 36643; nondegenerate semiconductors, transport phenomena in, 3753, transport properties of, 3754
Vartanian, P. H., with J. L. Melchor, temperature effects in microwave ferrite devices, 3938
Vassy, E., propagation and radio navigation systems, 1333 i
with others, rocket measurements of absorption in lower ionosphere, 2972
Vatter, M. J., with M. C. Thompson, Jr, microwave refractometer for aircraft, 1321
Vaughan, W. C., power in angle-modulated wave, 3851
Vautey, R., with L. J. Milosevic, travelling-wave

Vautgrain, W. C., power in angle-modulated wave, 3851
Vautey, R., with L. J. Milosevic, travelling-wave resonators, 2144
Vautier, C., with others, measurement of very slight variations of resistance, 555; properties of Sb films, 2693
Vautier, R., and A. J. Bertand, Y.-Fe garnet with substituted Cr, g-factor of, 2328, width of absorption curve of, 2329; direct measurement of width of resonance curves, 3814
and A. Marais, switching time of square-loop ferrite, 3404
Vavilov, V. S., and K. I. Britsyn, quantum yield of photoionization in Si, 863
A. A. Gippins and M. M. Gorshkov, reflection coefficients of Ge and Si, 3765
and others, Si solar batteries for earth satellites,

and others, Si solar batteries for earth satellites, 3862 3862 Veazie, C. E., transistorized radar sweep circuits, 3317

3317
 Vedam, K., with R. Pepinsky, room-temperature ferroelectric, 4084
 with others, (NH₄)₂SO₄ and (NH₄)₂BeF₄ transitions, 836; ferroelectricity in Li(N₂H₆)SO₄, 840; (NH₄)HSO₄ ferroelectric with low coercive field, 841

stiins, 836; ferroelectricity in Li(N;H₂)SO, 840; (NH₄)HSO₄ ferroelectricity in Li(N;H₂)SO, 840; (NH₄)HSO₄ ferroelectric with low coercive field, 841
 Veillex, R., with J. Bok, semiconductivity experi-ments on hot electrons in InSb, 3781
 Veith, F. S., TV canera tubes, 616
 Veith, W., calculation of electron-beam contours, 3524 w
 with K. Pöschl, focal length of diaphragm for electron beams, 1416
 Veksler, V. I., and L. M. Kowrizhnykh, cyclic acceleration of particles in h.f. fields, 3440
 Velizhanima, K. A., with Z. N. Baramova, acoustic properties of sound-absorbing material, 686
 Veloric, H. S., with J. H. Forster, effect of surface potential on junction characteristics, 3390
 Venables, J. D., and R. M. Broudy, photoanodiza-tion of InSb, 3782
 Venema, A., and others, dispenser cathodes, 2791
 Vengel', T. N., and B. T. Kolomiets, vitreous semi-conductors, 1920
 Venkatesan, D., solar activity and cosmic-ray intensity, 2942
 Venkateswarlu, P., and R. Satyanarayana, fading of radio waves, 585
 Venkrie, C. A., with Z. R. Schwerking, rapid reduction of k'f records to N-h profiles, 3303
 Vengopalan, M., potential variation of Joshi effect, 2530
 Verfane, R., orientational superstructure from deformation of K-f Records to N-h profiles, 3303
 Vengene, R., orientational superstructure from deformation of K-f Neuros for 'ferroxcube' at 24 kMc/s, 1293
 with others, multipactor effect, 3836
 Vermeulen, R., stereo-reverberation, 1065
 Verneulen, R., stereo-reverberation, 1065
 Verstelle, J. C., G. W. J. Drews and C. J. Corter, h.f., susceptibilities of paramagnetic alums, 2321

Verstelle, J. C., G. W. J. Drewes and C. J. Gorter, h.f., susceptibilities of paramagnetic alums,

I.31

2332

- Verstraten, J., frequency stability of r.f. heating generators, 933
 with J. M. G. Seppen, 8-mm radar, 1591
 Verzeno, M., R. C. Webb, Jr, and M. Kelly, radio control of ventricular contraction, 929
 Verzunov, V., with A. Szemenov, phase compensation methods of shaping s.s.b. signal, 588
 Veter, V. V., with L. V. Kirnskii, measurement of boundary layer width between domains, 2676
 Victorov, I. A., Rayleigh-type waves on cylindrical surfaces, 670
 Vidal, D., and G. Blet, influence of annealing time on thermoelectric power of Se, 2648
 Vierhout, R. R., models for transmission lines, 1067
 Vikramsingh, R., and others, hourly median field strength of 1940-Mc/s signal, 255
 Vila, P., with K. Sucky, magnetic field in F, layer at Dakar, 133
 Vilbig, F., long-distance telecommunications by mears of satellites, 964
 Villard, O. G., Jr, with K. C. Yeh, new type of fading on path crossing equator, 945
 Viller, J. A., application of information theory to amplitude compression, 3466
 amd J. Bouxiat, finite-duration signals with maximum filtered energy, 2390
 Villers, G., and J. Loriers, properties of mixed D. Y. Dy-Gd and Dy-Fr garnets, 2331
 J. Loriers and R. Pauthenet, magnetic properties of mixed G-Fr and Gd-Y garnet, 1633
 J. Loriers and R. Pauthenet, magnetic properties of Er garnet, 1290
 Villers, P., diffraction of ultrasonic waves by arrays of rods, 1048
 Vilms, J. J., with M. M. Fortini, solid-state generator for microwave power, 3991
 Vink, J., with M. B. A. Kröger, concentrations of imperfections in solids, 1175
 Vinogradova, M. B., with others, large inhomogeneities in F, layer, 2581
 Vint, J. P., satellite orbits, effect of drag on, 3287, theory of, 3687
 Vishenevsky, A. I., grades of vacuum in electronic tubes, 3895
 Visocekas, R., with J. Malot, anomalous behaviour in M-type carcinotron, 27884
 Visosek, M. J., wi

- 3672
 Vlaardingerbroek, M. T., active admittances of triote at 4 Gc/s, 2788 x
 van Vliet, K. M., and A. van der Ziel, noise generated by diffusion mechanisms, 2422
 with J. E. Hill, carrier-density fluctuation in Ge, 1617
 van Vlodrop, P. H. C., with H. L. van der Horst, induction-heating generator using hydrogen thyratrons, 3439
- Vocolides, J., with others, conductance of dipoles, 1089

- Inyratrons, 3439
 Voolides, J., with others, conductance of dipoles, 1089
 Vodar, B., with S. Robin-Kandare, reflecting power of bulk Si and Ge, 3766
 Voge, J., travelling-wave tubes, 1019
 Vogelman, J. H., high-power microwave filters, 3562
 J. L. Ryerson and M. H. Bickelhaupt, tropospheric scatter system using angle diversity, 2751
 Vogt, K., with R. Heidester, diversity reception by aerial selection method, 2741
 with others, correlation measurements in s.w. range, 953
 Volgt, F., dispersion in transverse susceptibility of Li ferrite, 1288
 Volgt, J., with others, evaluation of conductivity glow curves, 3321
 Voligt, S., measurement of capacitance of junction transistors, 3425
 Vokees, J. C., with others, high-power 400-Mc/s klystron, 3524 j
 Volkenshtein, N. V., G. V. Fedorov and S. V. Vomosvski, Hall effect in pure Ni at He temperatures, 2322
 with others, change of sign of Hall constant in alloys, 2675
 Volkov, Yu. D., with V. I. Chechernikov, temperature dependence of paramagnetic susceptibility of Ni-Zn ferrites, 3041
 Vollerner, N. F., and M. I. Karnovskii, concentration coefficient of directional acoustic systems, 3905
 Volsok, V. I., and B. V. Chirikov, compensation of
- tion **3905**

- tion coefficient of directional acoustic systems, 3905
 Volosok, V. I., and B. V. Chirikov, compensation of space charge in electron beam, 1836
 Volz, H., frequency-diversity method, 2385
 Vonbun, F. O., method for tuning maser cavity, 74
 Vonnegut, B., C. B. Moore and A. T. Boka, organized electrification and precipitation in thunderstorms, 2253
 Vonsovskli, S. V., and M. S. Svirskif, absence of superconductivity in ferromagnetics, 195
 with others, Hall effect in pure Ni at He temperatures, 2332
 Vook, F. L., and R. W. Balluffi, deuteron-irradiated Ge, length and resistivity changes in, 2306, structure of, 2308
 Vore, M. P., of random-noise transformers, 3214
 van der Vorm Lucardie, J. A., automatic supervision of f.m. transmitters, 3924
 Vose, A. W., and F. V. Wilson, airborne weather radar, 147
 Voss, W. G., 2-hole directional coupler, 705

- I.32

- Votaw, M. J., with R. L. Easton, Vanguard I, 1868
 de Vrijer, F. W., with T. Poorter, projection of colour-television pictures, 3119
 Vul, B. M., and A. P. Shotou, edge breakdown of p-n junction in Ge, 1616
 Vyatkin, A. P., and V. A. Elchin, origin of fluctuation of crystal triode parameters, 628
 Vysokovskii, D. M., geometric characteristics of scattering of radio waves in troposphere, 571; nultiple dispersion in u.s.w. scatter propagation, 1995

- Wachtel, A., ZnS-Sn, Li phosphors, 1212
 Wächtler, M., with H. Gabler, component determination in d.f. for coherent waves, 816
 Waddington, G. J., with P. H. Fowler, artificial aurora, 1888
 with others, cosmic-ray α particles during solar maximum, 3279
 Wade, C. M. radio emission of hydrogen pabulas
- Wade, C. M., radio emission of hydrogen nebulae, 421

- with others, cosmic-ray a particles during solar maximum, 3279
 Wade, C. M., radio emission of hydrogen nebulae, 421
 wade, G., and R. Adler, method for pumping fast space-charge wave, 1412
 and H. Heffner, gain, bandwidth and noise in cavity-type parametric amplifiers and convertors, 2896
 with H. Heffner, characteristics of variable-parameter amplifiers, and the state of the state

- 2838

- 2838
 Waldron, R. D., with M. Balkanski, internal photo-effect and exciton diffusion in CdS and ZnS, 824
 Walk, K., with H. Zemanck, Tchebycheff approximations for Gauer filters, 2498
 Walker, D. F., inprovement in detecting power of iron-cored search coils, 2351
 Walker, D. M. C., with D. G. King-Hele, last minutes of satellite 1957 β, 447; irregularity in atmospheric drag effects, 797; predicting orbits of near earth satellites, 2232; irregularities in density of upper atmosphere, 2571
 Walker, G. B., dielectric loading for u.h.f. valves, 3159 q

- in density of upper atmosphere, 2571
 Walker, G. B., dielectric loading for u.h.f. valves, 3159 g
 Walker, J. S., with J. T. Kendall, h.f. tetrode transistors, 3516
 Walker, R. M., with others, spin resonance in electron-irradiated Si, 4089 h
 Wallis, G., surface states on Ge, 171
 with S. Wang, recombination centres on ionbombarded Ge surfaces, 2303
 Wallis, R. F., and H. J. Bowlden, impurity photoionization spectrum of semiconductors in magnetic fields, 1232
 with others, Zeeman-type magneto-optical studies of interband transitions, 2283
 Wallmark, J. T., and S. M. Marcus, semiconductor devices for microminiaturization, 3213
 Walsh, D., improving microwave tube efficiency, 387
 With others, infrared properties of SiC, 2297

- 3887
 with others, infrared properties of SiC, 2297
 Walter, J. L., and others, cube-oriented magnetic sheet, 896
 Walters, L. C., with J. R. Johler, mean absolute value and standard deviation of phase, 3416; propagation of ground-wave pulse, 3842
 Walters, R., with M. Shepherdson, stroboscopic method for frequency response measurements, 2079
- 2079
 Walther, K., reflection factor of absorbers for cm waves, 2915
 Walton, A. K., and T. S. Moss, magneto-photo-electric theory for three carriers, 1923; photo-electromagnetic effect in Ge, 2660; free-carrier Faraday effect in n-type Ge, 3375
 with T. S. Moss, effective electron mass in GaAs, 4113

- 4113
 Walton, J., pickup for low record wear, 1764
 Wang, C. C., large-signal linear-beam tube theory, 3159 /
 Wang, C. P., with others, parametric devices tested for phase-distortionless limiting, 2182

- Wang, S., and G. Wallis, recombination centres on ion-bombarded Ge surfaces, 2303
 Wang, W. S., and G. E. Peterson, segment inventory for speech synthesis, 1060
 with others, segmentation techniques in speech synthesis, 1059
 Wangsness, R. K., ferrimagnetic-resonance parameters, 91, 2545
 Wanlass, L. K., and L. O. Hill, digital-analogue conversion with cryotrons, 1103
 Ward, A. L., effect of space charge in cold-cathode gas discharges, 1833
 Warekols, E. P., and P. H. Metsger, X-ray method for A¹¹¹B^v compounds, 3786
 Waring, R. K., with H. S. Jarrett, ferrimagnetic resonance in NiMnO, 543
 Warmeckam, J. C., with E. G. Dorgelo, intermittent use of valves in r.f. heating generators, 2071
 Warnecke, M., with H., Huber, Ti pump, 1205
- Warnecke, M., with H. Huber, Ti pump, 1205 Warnecke, R., O. Doehler and B. Epstlein, electron veloci ies and pass band in travelling-wave amplifiers, 316
- amplifiers, 316
 with J. Arnaud, increase of bandwidth in O-type travelling-wave valves, 317
 Warner, R. M., Jr, and others, semiconductor current limiter, 1368
 Warnick, G. W., with others, remote-control carrier systems in two-way closed-circuit television, 285
 Warren, E., with others, reciprocity of ionospheric transmission, 1667; spiral occurrence of E., 3304
 Warren, E. S., with others, frequency prediction techniques for high latitudes, 2729
 Warring, J. J. M., and H. Brieters, onen rectangular

Warringa, J. J. M., and H. Piepers, open rectangular waveguides in r.f. oscillators, 3984
 Warschauer, D. M., with W. Paul, optical properties of semiconductors under hydrostatic pressure, 506

506
Warwick, C., green coronal line intensity and geomagnetism, 2949
Warwick, C. S., and R. T. Hansen, geomagnetic activity following large solar flares, 3284
Warwick, J. W., interaction of solar plasma and geomagnetic field, 2550

3276

with 1728

963

1729

with A. Boischot, radio ecuission following flare, 3276
 Wasilik, J. H., and R. B. Flippen, piezoelectric effect in InSb, 180
 Wasserman, R., and P. Hurnev, tones find data in high-speed tape systems, 932
 Wasson, H. M., with G. E. Theriault, transistor performance characteristics at v.h.f., 1115
 with H. B. Yin, r.f. amplifier for v.h.f. television receivers, 1384
 Watanabe, T., with Y. Kato, geomagnetic storm in relation to geomagnetic pulsation, 1537
 Waterman, A. T., Jr, transhorizon propagation, scattering relationships in, 570, rapid beamswingling in, 3198
 N. H. Bryant and R. E. Miller, antenna-beam distortion in transhorizon propagation, 1347
 Waters, D. M., with M. C. Thompson, Jr, studying ionospheric structure using earth satellites, 799
 with others, ceramic X-band cavity resonators, 363
 Waters, W. E., azimuthal electron flow in spherical

Waters, W. E., azimuthal electron flow in spherical diode, 2433; aberrations in electron sheet beams, 2908

Watkins, C. D., with D. P. Harrison, radio echoes from aurora australis and aurora borealis, 140
 Watkins, D. A., helitron oscillator, 319
 — with others, reduction of electron-beam noise,

1728
 Watkins, G. D., J. W. Corbett and R. M. Walker, spiir resonance in electron-irradiated Si, 4089 h
 Watkins, T. B., 1/f noise in Ge devices, 1256
 with others, surface-barrier height changes on transistors, 633
 Watt, A. D., and R. W. Plush, worldwide standard-frequency broadcasting eyeton, 2001

Figure V broadcasting system, 4201
 E. L. Maxwell and E. H. Whelan, 1.f. propagation paths in arctic areas, 4182
 and others, radio system performance in noise,

and others, radio system performance in noise, 963
 Watters, B. G., with G. Kurtze, wall design for high transmission loss, 3917
 Watts, J. M., interpretation of night-time l.f. ionograms, 1558
 with others, I.G.Y. observations of F-layer scatter in Far East, 2733
 Way Dong Woo, tape recording system for data processing, 1464
 Waymick, A. H., with J. J. Gibbons, D region of ionosphere, 1553
 Weaver, C. S., with R. S. Davics, mininum transmitter weight for space communications, 3141
 Weaver, H. E., with R. C. Rempel, microwave reflection bridge, 1982
 with others, electron paranagnetic resonance in BaTiO₃, 476
 Weaver, L. E., measurement of random noise in television, 2345; impairment of television pictures, 2408
 Webb, R. C., Jr, with others, radio control of ventricular contraction, 929
 Webber, S. E., ballistic analysis of 2-cavity klystron.

Webber, S. E., ballistic analysis of 2-cavity klystron.

Webber, W. R., with J. J. Quenby, cosmic-ray cut-of rigidi!ies, 3280 Weber, L. A., f.m. digital subset for data trans mission, 2392
 Weber, R., with L. Genzel, theory of interference modulation, 2191; spectroscopy in far infrared, 1963

Weber, K., with L. Genzi, theory of Interference modulation, 2191; spectroscopy in far infrared, 2192
Weber, S., mavar: low-noise nicrowave amplifier, 79; transistor for cryogenic temperatures, 1712 ---- with others, '59 I.R.E. Show, 2801
Webley, R. S., thin magnetic films, 2682
Webster, H. C., spread-F echoes at night at Brisbane, 454

Electronic & Radio Engineer

with A. Boischot, radio e:uission following flare,

- Webster, H. F., performance of thermionic energy converter, 3438 Webster, J. C., R. G. Klumpp and A. L. Witchey, evaluation of modulated-air-flow loudspeaker, 1, 3922
- 3922
 Wedler, G., with others, temperature dependence of electron emission of Bi films, 2619
 Wedlock, B. D., stability of transistor amplifiers, 4000

- 4000
 Weekes, K., with G. J. Aitchison, ionospheric information from observations of satellite 1957 α2, 3296
 with others, ionospheric information from observations of satellite 1957 α2, 3297
 Weeks, R. R., with W. G. Long, quadruple-diversity tropospheric scatter systems, 972
 van Weel, A., analysis of diode detector for asymmetric-sideband signals, 249; detector stages for symmetrical or asymmetrical sidebands, 580
 Weeder, M., and W. Low, paramagnetic-resonance
- bands, 580
 Weger, M., and W. Low, paramagnetic-resonance spectrum of Gd in LaCl₃.7H₁O, 780
 Weglein, R. D., with R. C. Knechtli, low-noise parametric amplifier, 2185
 Weibel, E. S., confinement of plasma by r.f. fields, 1511; orbits of charged particles in c.m. field, 3250

- 3250
 Weibel, G. E., masers and quantum-mechanical devices, 72
 Weide, F., with others, equalization in television transmission by cable, 3488
 Weihe, W. K., classification and analysis of imageforming systems, 4237
 Weihberg, L., tables for optimum ladder networks, 49
- 49
 Weingärtner, A., a.f. equipment in Südwestfunk studios, 3188
 Weinreich, G., T. M. Sanders, Jr, and H. G. White, acoustoelectric effect in n-type Ge, 3373
 and others, splitting of As donor ground state in Ge, 1615
 C. A. U. Matari, and B. Utad amin.
- arms otners, splitting of As donor ground state in Ge, 1615
 Weinreich, O. A., H. Mataré and B. Reed, grain-boundary amplifier, 3241
 with others, conductivity of grain boundaries in Ge bicrystals, 2657
 Weir, C. E., with others, infrared studies on SiO₂ and GeO₂, 205
 Weisberg, L. R., J. R. Woolston and M. Glicksman, electron mobilities in GaAs, 529
 Weisbrod, S., and L. Colin, refraction of v.h.f. signals, 3698
 Weiser, K., distribution coefficients of impurities in Ge and Si, 1242
 with M. Glicksman, electron mobility in InP, 4115
 Weisman, L., telemetry demodulator. 1992

- 4115 Weisman, L., telemetry demodulator, 1992 Weiss, A. A., meteor trails, electron density in, 2224, electron density of echoing points in, 2941; radio detection of weak meteor showers, 2227; theory of radio-echo meteor height distribution, 2940
- with others, c.w. technique for measurement of

- 2940
 with others, c.w. technique for meisurement of meteor velocities, 105
 Weiss, G. T., with thers, notended-range distributed-amplifier design, 1492
 Weiss, H., with H. Welker, semiconductor compounds of homopolar character, 1227
 Weiss, J. A., Faraday-rotation switch for TH system, 2835; theory of Reggia-Spencer phase shifter, 2837
 Weiss, M. T., microwave and l.f. oscillations due to resonance instabilities in ferrites, 198
 Weiszburg, J., J. Schanda and Z. Boló, time-dependent spectra of ZnS: Cu, Pb, 4080
 Weitsch, W., compensation of chromatic dependence in electron microscope, 3076
 Weils, C. P., prolate spheroidal antenna, 1445
 Wells, C. P., noist espheroidal antenna, 1445
 Wells, R. P., timing-signal transmission at Canaveral, 2722
 Weils, R. W., colour television, display system for, 621, Faraday cell in, 1705
 Weilsy, V. G., improving aerial directivity, 3574
 and D. G. Tucker, multiplicative receiving arrays, 3953
 Welsh, J., production testing equipment for micro-

- ana D. G. Iucker, multiplicative receiving arrays, 3953
 Welsh, J., production testing equipment for inicrowave components and systems, 221
 with E. Laverick, automatic standing-wave indicator, 2711
 Weltzien, J. W., with others, multipurpose bias device of logical elements, 1461
 Wendt, P. H., with others, automatic input equipment for data processing, 3586
 Wentworth, J. W., technical standards for colour television, 278
 Werreb, J. A., Jr, zero-crossing technique for wave-train outputs, 3064
 Werner, P., surface enlargement of Al for electrolytic capacitors, 2868
 Werrick, J. H., S. Geller and K. E. Benson, con-

- 2454
 Wernick, J. H., S. Geller and K. E. Benson, constitution of AgSbSe₂-AgSbTe₂-AgBiSe₂-AgBiTe₂ system, 1270
 with S. Geller, ternary semiconducting
- h S. Geller, ternary semiconducting com-unds: AgSbSe₂, AgSbTe₂, AgBiS₂, AgBiSe₃,
- i269
 with others, magnetic moments of Fe and Co with rare-earth metal additions, 2321
 Wertheim, G. K., neutron-bombardment damage in Si, 861; recombination properties of bombardment defects in semiconductors, 4090
 and D. N. E. Buchanan, electron-bombardment damage in oxygen-free Si, 4089 k
 Wescott, E. M., with V. P. Hessler, correlation between earth-current and geomagnetic disturbance, 4044

- Electronic & Radio Engineer

- Wesemeyer, H., and J. M. Daniels, influence of Westineyer, n., and J. M. Danks, Inducte of saturation of paramagnetic resonance absorption on Faraday effect, 2547
 Wessel, G. K., u.h.f. ruby maser, 2178
 West, J. C., with J. L. Douce, magnetic-drum store for analogue computing, 348
 West, R. E., high-speed read-out for data processing, 3066

- 3086
- 3086
 Westberg, R. G., ionizing-potential space waves in glow-to-arc transitions, 3254
 Westberg, R. W., with T. R. Robillard, transistors for electronic switching, 2778
 Westerfield, E. C., with J. L. Stewart, active sonar detection, 2596
 Westerhof, T. J., with others, cathodothermo-luminescence, 2624
 Westoby, P. J., ring counter, 2506
 Weston, D. E., guided propagation in slowly varying medium, 2204
 Weston, M. A., breakdown of Si power rectifiers, 3863
 Weston, V. H., with others, radar cross-section of

- 3863 Weston, V. H., with others, radar cross-section of finite cones, 4073 Wexler, G., with others, high-power 400-Mc/s klystron, 3524 j Weyss, N., class-C operation of transmitter valves, 1033

- 1033
 Whale, A. V., with W. F. Gibbons, ceramic wave-guide window for X-band valves, 3159 a
 Whale, H. A., effects of ionospheric irregularities on bearings of s.w. signals, 1998
 and L. M. Delues, relations between bearing and amplitude of fading radio wave, 947
 Wheatley, G. H., with J. M. Whelan, preparation and properties of GaAs, 881
 Wheaton, R. N., techniques of transistor production, 2049
- 2049
- Wheeldon, A. J., tropospheric scatter tests, 260 Wheeler, G. J., with others, high-power L-band resonance isolator, 3563 Wheeler, H. A., radiansphere around small antenna, 3566
- 3566
 Wheeler, L. K., with P. R. Keller, automatic error correction, 966
 Wheeler, M. S., beam steering by scattering from ferrites, 2472
 Wheeler, R. G., multiplet structure of excitons in CdS, 3324
 A. D. sectors of provide structure of background by the structure of t

- Wheeler, R. G., multiplet structure of excitons in CdS, 3324
 Wheeler, R. G., multiplet structure of excitons in CdS, 3324
 Wheelon, A. D., spectrum of passive scalar mixed by turbulence, 1660
 with H. Slaras, theoretical research on tropospheric scatter propagation, 3846
 with H. Slaras, theoretical research on line-of-sight paths, 4183
 Whelan, E. H., with cthers, I.f. propagation paths in arctic areas, 4182
 Whelan, J. M., and C. H. Wheatley, preparation and properties of GaAs, 881
 with G. S. Fuller, behaviour of Cu in GaAs, 882
 with W. G. Spitzer, infrared absorption and effective mass in n-type GaAs, 3383
 Whetten, N. R., and A. B. Laponsky, secondary en ision from MgO thin films, 2316
 Whitry, W. L., and C. E. Nelson, microwave cavity filters, 2467
 white, A. D., gas-diode switch, 724; hollow-cathode glow discharge, 2909
 White, B. H., with H. C. Lin, single-ended amplifiers for class-B operation, 2885
 White, B. H., with H. G. Lin, single-ended amplifiers for class-B operation, 2885
 White, B. L., C., frequency modulator for broadcast transmitters, 3872
 White, B. G. K., and S. B. Woods, resistivity of Bi and Sb at low temperatures, 1222
 White, C. K., and W. C. Roth, polarity of GaAs, 3381
 White, N. P., with S. T. Cap, guidance systems in space fight, 3899
 White, R. L., line widths and g-factors in ferrites, 3402
 White, R. M., C. K. Birdsall and R. W. Grow, multiple ladder circuits for min-wave tubes,

- White, R. M., C. K. Birdsall and R. W. Grow, multiple ladder circuits for mm-wave tubes, 3159 v
- Whitehead, C. C., 'variable- μ ' magnetic amplifier, 2170
- Whiteway, F. E., pre-pulse techniques in high-speed oscillography, 3827
 Whitfield, G. D., theory of electron-phonon inter-actions, 2215

- actions, 2215
 Whitfield, H. R., and C. M. Cade, analysis of collision-course prediction, 2259 "
 Whitham, K., relation between secular change and non-dipole fields, 790
 Wickersham, A. F., Jr, anomalous dispersion in artificial dielectrics, 482; Stokes' equations and refractivity of thin films, 1154
 Wickizer, G. S., with others, 468-Mc/s tropospheric scatter propagation, 245
 Widdowson, A. E., D. C. Gore and C. H. Butcher, new method for fine-wire grids, 2788 y
 Wieder, H. H., ferroelectric properties of colemanite, 3741
- 3741
- 3/41
 Wiekhorst, F., absorption of e.m. waves by lossy resonant slots, 2205
 Wiencek, Z., automatic controls for colour television, 3118
 Wiener, F. M., and D. N. Keast, propagation of sound over ground, 3900

- K. W. Goff and D. N. Keast, instrumentation for study of sound propagation, 2081 Wiener, G. W., and K. Detert, cube-oriented inagnetic
- Wiener, G. W., and K. Detert, cube-oriented inagnetic sheet, 896 van Wieringen, J. S., paranagnetic resonance, 778 Wiessner, W., with G. Zickner, influence of leads on capacitors, 1316
- an, E. R., unpleasantness of distorted sound, 2817 Wigan
- Wigan, E. R., unpleasantness of distorted sound, 2817
 Wigington, R. L., new concept in computing, 2126
 Wijn, H. P. J., with A. L. Stuijts, crystal-oriented ferroxplana, 2687
 Wilcox, C. H., with R. B. Barrar, Fresnel approximation, 1442
 Wild, J. P., with others, extension of solar radio spectroscopy, 2933
 Wilhelm, C. R., with A. J. Seyler, video transmission test set, 4159
 Wilkinson, E. J., slot-antenna array for missiles and aircraft, 1774
 Wilkinson, J. H., and D. W. Davies, automatic computing engine at N.P.L., 2128
 Will, R., with F. Duclaux, lunar-diurnal variation of geomagnetic field, 2228
 Willardson, R. K., transport properties in Si and GaAs, 4089 f
 with others, transverse magnetoresistance and Hall effect in n-type InSD, 4119
 Willhims, A. D., and D. C. Gore, low-noise triode for

1465
 Williams, A. D., and D. C. Gore, low-noise triode for use up to 1 kMc/s, 1419
 Williams, C., review of radio aids to navigation, 2259 a; radio aids and aeronautical navigation.

2978 /

2259 a; radio aids and aeronautical navigation, 2978 c
Williams, D., structure of h.f. ionospheric scatter signals, 2000 d
with P. H. Cutler, scatter-signal analyscr, 2000 b
Williams, H. J., with others, domain behaviour in transparent magnetic oxides, 1956
Williams, R., with others, search for new Heusler alloys, 1950
Williams, R. Quith others, microwave frequency standard, 4150
Williams, R. C., with others, evidence for carriers with negative mass, 875
Williams, R. W., and H. Marchant, resistance potentiometers as function generators, 35
Williams, T. R., and J. B. Thomas, current noise and nonlinearity in carbon films, 3596
Williams, W., adiabatic and isothermal effects in Bi₁Te₃, 2670
Williams, W. E., step discontinuities in waveguides, 14

Williams, W. E., step discontinuities in waveguides, 14
Williamson, D. T. N., e.s. loudspeakers, 8
Williamson, J. B. P., with others, electrical conduction in solids, 485
Williamson, L. A., cooling airborne electronic equipment, 1420
Willis, D. W., data storage and processing on magnetic tape, 1786
Willis, B., with others, precipitation on a dislocation, 2289
Willimore, A. P., new method of tracking earth satellites, 1189
Willoughby, E. O., and E. Heider, omnidirectional paraboloid aerial, 1447
Willrodt, M., with others, precision generator for radar range calibration, 2352
Wilmotte, R. M., with M. Greenspan, distributed transducer, 673
Wilson, A. C., with the V. Collony, gains of corner-reflector antennas, 3205
Wilson, B. L. H., with D. H. Roberts, effects of O₈ on resistivity in Si, 2294
Wilson, F. V., with other s, electron-spin-resonance experiments on Ge, 3775
Wilson, F. V., with A. W. Vose, airborne weather radar, 147

experiments on Ge, 3775
Wilson, E. F., divider vernier to synchronizc pulses, 3232
Wilson, F. V., with A. W. Vose, airborne weather radar, 147
Wilson, J. M., large-scale preparation of Gc, 2653
Wilson, V. C., conversion of heat to electricity by thermionic emission, 3436
Wilson, W. P., group delay and group velocity, 1798
Wiltse, J. C., characteristics of dielectric image lines at mm λ, 3930
Wimmel, H. K., with W. Maier, quantum theory of dielectric polarization of gases, 2901
Wimmelfen, J., with W. F. Niklas, oscilloscope tube with travelling-wave deflection, 927
Winckel, F., acoustic criteria for concert halls, 1063
Winckel, F., and others, balloon gear monitors cosmic radiation, 437
Winckeler, J. R., and others, auroral phenomena during storm, 3309
with L. Peterson, yray burst from solar flare, 104
with others, geophysical effects associated with high-altitude explosions, 2575; protons from sun 12th May 1959, 4040
Windsor, E., oxide cathodes for travelling-wave tubes, 3159 ff
Winet, J., T., with J. C. Anderson, temperature-stabilized photo-transistor relay circuit, 1109
te Winkel, J., drift transistor relay circuit, 1109
te Winkel, J., 2781, 3518
with others, junction transistor as network we element, 1719, 2781, 3518

line analogue of, 3153
with others, junction transistor as network element, 1719, 2781, 3518
Winkel, P., and D. G. de Groot, impedance of dielectric layers, 2271
Winkler, G. M. R., with others, comparison of Cs frequency standards, 212
Winslow, D. K., with others, current distribution in modulated electron beams, 644

- Wintenberger, M., measurement of Hall effect i anisotropic media, 213
 Winwood, J. M., magnetic forces and relativistic speeds in stationary electron beams, 85
 Wisch, W., instrument for measurement of Q-factor, 2709

- Wisch, W., Instrument for measurement of Q-factor, 2709
 Wiseman, R. S., and M. W. Klein, photoemissive image-forming systems, 4238
 Wisotzky, W., constant-frequency oscillators without stabilized supplies, 1482
 Witchey, A. L., with others, evaluation of modulated-air-flow loudspeaker, 3922
 Wittey, E. L., c.r. tube adds third dimension, 1747
 Wittke, H., image distortion by RC quadripoles of c.r.o., 1318
 Wittke, J. P., with others, structure and relaxation times of Cr³⁺ in TiO₂, 2333
 Woelke, C. D., with others, properties of green and red-green luminescing CdS, 2621
 Wolf, M., with M. B. Prince, Si photovoltaic devices, 640

- 640 Wolf, W. P., with others, ferrimagnetic resonance in

- 640
 Wolf, W. P., with others, ferrimagnetic resonance in polycrystalline rare-earth garnets, 2690
 Wolfe, J. L., satellite tracking by h.f. d.f., 798
 Wolfe, P. G., with others, colour purity adjustment for 'apple' c.r. tube, 1386
 Wolfe, W. L., with M. R. Holter, optical-mechanical scanning techniques, 4010 k
 Wolff, G. A., I. Adams and J. W. Mellichamp, electroluminescence of AlN, 4082
 Wolff, P. A., plasma resonance in solids, 781
 Wolfft, P. A., plasma resonance in solids, 781
 Wolfft, P. A., plasma resonance in solids, 781
 Wolfft, P. A., plasma resonance in solids, 781
 Wolfstein, K. and C. S. Fuller, comparison of radiocopper and hole concentrations in Ge, 1250
 Wolk, B., breakdown of cathode coatings, 1029
 Wolk, B., Dreakdown of cathode coatings, 1029
 Wolk, B., Dreakdown of the coatings, 1029
 Wolk, E. D., with others, effect of fast neutrons on efficiency of travelling-wave tubes, 314
 Woller, E. D., with others, effect of fast neutrons on n-type Ge, 866
 Woller, L., theorem on force-free magnetic fields, 784
 Wong, J. Y., scattering of plane e.m. wave, 2540
 and S. C. Lok radiation resistance of elliptic

- Wong, J. Y., information for force free magnetic fields, 784
 Wong, J. Y., scattering of plane e.m. wave, 2540
 and S. C. Lok, radiation resistance of elliptic loop, 1776; radiation field of elliptic helical antenna, 3577
 with S. C. Lok, radiation field of elliptic loop, 20
 Wong, P. K., with others, use of d.c. amplifier and recorder to balance resistance bridge, 3061
 Woo, Way Dong. See Way Dong Woo.
 Wood, A. F. B., with S. Tolansky, interferometric studies on oscillating quartz crystals, 2335
 Wood, C. C., with others, noise-gated a.g.c. and sync system, 1382
 Wood, P. W., transistorized f.m. oscillator, 1489
 Woodbridge, D. D., N. I. Macdonald and T. W.

- Wood, P. W., transistorized f.m. oscillator, 1489
 Woodbridge, D. D., N. J. Macdonald and T. W. Politie, geomagnetic disturbances and changes in atmospheric circulation at 300 mb, 2229
 Woodbury, H. H., with G. W. Ludwig, electron spin resonance in Ni-doped Ge, 2661, or condition of spot diagram information, 1105
 Woods, J., photochemical effects and effect of O, on CdS, 1593
 Woodward, O. M., Jr, circularly polarized corner-reflector antenna, 1098
 Woodyard, O. C., with others, U.R.S.I. report on antennas and waveguides, 3565
 Woolson, J. R., with others, electron mobilities in

- Wooltey, R. v. d. R., Royal Greenwich Observatory, 2550
 Woolston, J. R., with others, electron mobilities in GaAs, 529
 Wootton, D. J., J. A. Lucken and R. C. Bannerman, experimental annular reflex klystron, 3524 bb
 with others, design of gridless low-voltage reflex klystron, 3524 dd
 Worcester, J. A., one-transistor push-pull, 2887
 Worrster, E. M., with R. De Waard, thermal detectors, 4010 g
 Worst, E. C., Jr, with others, high-sensitivity infrared detectors, 1012
 Woschni, E. C., permissible circuit impedance of i.f. filters for f.m., 732; distortion factor in v.h.f. f.m. receivers, 4190
 Woyk (Chvojková), E., signals from earth satellites.

- Wray, C. Horolková), E., signals from earth satellites, 1549; antipodal reception of Sputnik III, 2957
 Wray, D., frequency compensation for stepped wave-guide transforming sections, 1077
 Wray, F., with others, c.w. power travelling-wave type 2787
- Wray, F., with tube, 2787 Wright, C., te
- Wright, C., temperature stabilization of transistor circuits, 2052
- Wright, C. S., with others, causes of geomagnetic fluctuations with 6-sec period, 2945; geographical variations in geomagnetic micropulsations, 2946
 Wright, D. A., thermoelectric properties of semiconductors, 3347
 with others, thermoelectric power of semiconducting diamond, 1924
 Wright, E. E., with T. D. Schlabach, test patterns for printed-circuit materials, 2487
 Wright, G. T., space-charge-limited currents in insulating materials, 1622
 Wright, R. W., and J. C. Brice, indium monotelluride, 2312
 Wright, R. W., and N. J. Skinner, lunar tides in E. layer, 1850
 with others, horizontal drift measurements near equator, 1557
 Wright, S. B., with F. C. Champion, diamond

- wright, S. B., with F. C. Champion, diamond conduction counters with small electrode separations, 1990
 Wu, T. T., and R. W. P. King, driving point and input admittance of linear antennas, 1440

- Wucher, J., with others, magnetic properties of (Ni,Li)O, 3799
 Wulf, O. R., with S. B. Nicholson, diurnal variation of geomagnetic fluctuations, 1533
 Wunderlin, W., with W. Cuggenbühl, equivalent circuit of h.f. transistors, 2423
 Wunsch, G., practical design of 2-phase networks, 2158; general network theorem, 2495
 Wyatt, S. P., so ar effects on motion of Vanguard, 4050
 Wyeth, F. H., I. B. Hieley and W. H. Swith Is
- Wyeth, F. H., J. B. Higley and W. H. Shirk, Jr, precisiou guarded resistance measuring facility, 561
- Wynne, C. G., lens designing by digital computer, 2483
- Yabroff, I., with R. L. Leadabrand, geometry of auroral communications, 1671
 Yabumoto, T., Hall effect in oxide cathodes, 3166

- auroral communications, 1671
 Yabumoto, T., Hall effect in oxide cathodes, 3166
 Yadavalli, S. V., broad-band operation of multicavity klystrons, 1015
 Yaffee, P., with others, electronic subsystem development problems in naval ordnance, 2803
 Yajima, T., and L. Esaki, excess noise in narrow Ge p-n junctions, 1257
 Yakobson, M. A., with others, line spectra of absorption edge of CdS, 471
 Yamada, K., with T. Kasuya, electrical and thermal conductivity of monovalent metals, 4015
 Yamaguchi, J., and Y. Hamakawa, Ge p-n junction, high-electric-field effects in, 3023, barrier temperature at turnover in, 3024
 Yamaguchi, S., measurement of residual magnetism of thin film, 1314; magnetic analysis with electron beams, 2199; magnetic perturbation of cathode rays, 3636; magnetic and crystallographic analysis by electron of InSb, 1940
 Yamamoto, M., S. Taniguchi and K. Aoyagi, formarento, M., S. Taniguchi and K. Aoyagi, formarento, and structure of InSb, 1940
- Yamanak, E., with others, ballo stitucture of Hiso, 1940 Yamanoto, M., S. Taniguchi and K. Aoyagi, ferromagnetic domain structure in Co-Ni crystal, 192 Yamanaka, S., with Y. Saito, residual polarization of BaTiO₃ ceramics, 3327 Vanodi A. with view of the band have a structure of BaTiO₃ ceramics, 3327

- of BaTiO₃ ceramics, 3327
 Yanagi, A., with others, 4-kMc/s-band v.s.w.r. scanner, 1975
 Yanaoka, I., with others, helix-type travelling-wave amplifier, 1415
 Yankov, V. V., behaviour of conducting gaseous sphere ir quasi-stationary e.m. fie d, 3640
 Yariv, A., coupling coefficients in 'coupled-mode' theory, 1014
 and F. D. Clapp, determination of cavity parameters, 4154
 J. R. Singer and J. Kemp, radiation damping effects in 2-level maser, 1818
 Yasuda, S., with M. Kenmoku, package-type travelling-wave amplifier, 2788 p
 Yatani, M., with others, band structure of InSb, 1940
 Yates, B., conductivity and Hall coefficient of

- Yatani, M., with others, band structure of InSb, 1940
 Yates, B., conductivity and Hall coefficient of Bi, Te, 1942
 Yatsiv, S., double-quantum transitions in masers, 2890; multiple-quantum transitions in magnetic resonance, 2923
 Yatsunskii, I. M., effect of geophysical factors on satellite motion, 3683
 Yavich, L. R., wave matrices of quadripole, 2149
 Yae B. and others, avalance herededown is a 4

- satellite motion, 3683
 Yavich, L. R., wave matrices of quadripole, 2149
 Yee, R., and others, avalanche breakdown in n-p Ge diffused junctions, 3378
 Yeh, K. C., and O. G. Villard, Jr, new type of fading on path crossing equator, 945
 Yeh, L. P., tropospheric-scatter system design, 1360; loop control of scatter power to offset fading, 1694; communications in space, 3469
 Yerg, D. G., analysis of drifts of signal pattern, 1884
 Yin, H. B., and H. M. Wasson, r.f. amplifier for v.h.f. television receivers, 1384
 Yonezawa, T., influence of electron-ion diffusion on formation of F₂ layer, 128
 and Y. Arima, F₄ layer, semidiurnal lunar variations of, 1196, variations in electron density of, 4055
 H. Takahashi and Y. Arima, electron and ion density distributions in F region, 2579
 Yoshida, I., S. Nomura and S. Sawada, thermal conductivity of BaTiO₃ ceranics, 2628
 Young, J. F., alternatives to Wien bridge, 1124; simple v.l.f. oscillator, 2160; transistor character-istic curve tracer, 3060
 Young, J. W., pagemaster receiver and modulation enument. 3476

- Young, J. W., pagenaster receiver and modulation equipment, 3476
 Young, L., predicting accurate radar ranges, 2606
 Young, M. E., W. M. Alexander and H. D. Schwetman, rotating-disk function generator, 2858

- 2588
 Young, R. D., energy distribution of field-emitted electrons, 2197
 and E. W. Müller, energy distribution of field-emitted electrons, 2198
 Young, R. W., with C. C. Ritchie, design of biased-diode function generators, 2861
 Young, S. G., h.f. exponential-line transformers 1070
- Younger, J. J., and others, parametric amplifiers as, superregenerative detectors, 3245
 Yousef, Y. L., and H. Mikhail, electrodynamic magnetic field gradiometer, 218
 Yu, Y. P., coincident slicer measures phase directly, 217
- Yueh-Ying Hu, back-scattering cross-section of cylindrical antenna, 1444
 Yukutake, T., with others, effect of solar eclipse on geomagnetic field, 2561

- Zågånescu, M., with C. Sålceanu, correction to velocity of sound by resonance method, 328; influence of thickness of walls of resonance tube, 1422
 Zakharchenya, B. P., with E. F. Gross, Zeeman effect and exciton structure in Cu₂O, 1623
 with others, influence of magnetic field on fluorescence of pure CdS, 2622
 Zakirova, I. R., with others, secondary emission from Ni, 3789

- from N1, 3789
 Zalm, P., with J. J. Scheer, crystal structure of Na, KSb, 2995
 with others, electroluminescence and image intensification, 1597
 Zankel, K. L., and E. A. Hiedemann, amplitude distortion of ultrasonic waves, 2814
 Zavadskil, E. A., with I. G. Fakidov, oscillation of resistance of n-type Ge in pulsed magnetic fields, 872
- Zawels, J., wide-band bridge for transistor parameters, 1003
 Zeitler, E., and G. F. Bahr, quantitive electron microscopy, 3444
- Zelikman, M. Kh., with K. I. Gringauz, measure-ment of ion concentration along satellite orbit, 3696
- Zemanek, H. solution of equations in switching algebra, 1297 and K. Walk, Tchebycheff approximations for Cauer filters, 2498

Can P. Puke, 1 Clebychen approximations for Cauer filters, 2498
 Zernel, J. N., surface transport theory, 1233
 Zerbst, G., with others, image converters for quantity production, 1404
 Zheleznyakov, V. V., radio emission of sun and planets, 3275
 Zheleztsov, N. A., and M. I. Feigin, operating conditions of symmetrical multivibrator, 1806
 Zheludev, I. S., with others, domain structure of ferroelectrics, 158
 Zhidkov, V. A., and V. E. Lashkarev, diffusion and electric state of thermal acceptors in Ge, 520
 Zhirnov, V. A., theory of domain walls in ferro-electrics, 3740
 Zhuze, V. P., G. E. Pikus and O. V. Sorokin, deter-mination of surface recombination velocity, 500
 V. M. Sergeeva and E. L. Shtrum, new semi-conducting compounds, 3755
 Zickner, G., and W. Wiessner, influence of leads on

Zickner, G., and W. Wiessner, influence of leads on capacitors, 1316 Ziegler, E., with E. Huster, spreading of discharge in counter tubes, 1332 Ziehm, G., true-phase capacitive goniometers, 4068 with K. Baur, ferromagnetic transmitter aerial for distress at sea, 4223

van der Ziel, A., with H. J. Hannam, noise in oxide cathodes, 1027 with K. M. van Vliet, noise generated by diffusion mechanisms, 2422

Zielasek, G., growth phenomena in Ge crystals, 3358; semiconductor component for electronic circuits, 4225
 with G. Pröpstl, Sb distribution in Ge-Sb alloys,

With G. Fropsa, So assessment of Fermi 3026
 Ziman, J. M., galvanomagnetic properties of Fermi surfaces, 3271

Zimmermann, A., thermal expansion coefficient of ferrites, 4128
Zinke, O., with K. L. Lenz, absorption of e.m. waves in absorbers and lines, 1068

Zito, G., measurement of phase difference on power transmission lines, 1971

Zito, G., measurement of phase difference on power transmission lines, 1971
Zitter, R. N., role of traps in photoelectromagnetic and photoconductive effects, 1229
Zlotykamin, C., high-density electron gun, 3524 x
Zmuda, A. J., analysing values of scalar magnetic intensity, 109
Zneimer, J. E., with others, grain growth in Ni ferrites, 544
Zohan, S. R., with others, multiple Fourier analysis in rectifier problems, 2382
Zoldan, G., with C. C. Corazza, physical realizability of microwave junction, 2139
Zozulya, Yu. I., with M. I. Klinger, theory of semiconductors with excited impurity zone, 1604
Zschörner, H., with H. K. Paetsola, radio observations at 20 Mc/s of first Russian earth satellites, 2237; density of outer atmosphere from satellite observations, 3695
Zucker, I. J., with thers, frequency pushing in consultance of the scillator 2788 a

Zucker, I. J., with others, frequency pushing in crossed-field oscillators, 2788 g crossed-field oscillators, 2788 q Zucker, N., with others, markerless pulse trains for communications, 956 Zuhrt, H., addition of distortion voltages in long-

Zuhrt, H., addition of distortion voltages in long-distance a.m. systems, 3856
 Zuleeg, R., effective collector capacitance in transistors, 632
 and J. Lindmayer, sweep equipment displays transistor *b*, 928
 with J. Lindmayer, determining transistor high-frequency limits, 4232
 Zverev, A., and H. Blinchikoff, network transformations for wave filter design, 3222
 Zverev, G. M., and others, chronium corundum paramagnetic amplifier, 1145
 Zwerdling, S., and others, exciton- and magneto-absorption of transitions in Ge, 3364
 with others, optical magneto-absorption effects in semiconductors, 3365
 Zwicker, E., psychological and systematic bases of loudness, 3344
 Zwobada, R., 220-kW Q-band magneton, 2788 e

loudness, 3544
 Zwobada, R., 220-kW Q-band magnetron, 2788 e
 Zyazev, V. L., and O. A. Esin, influence of short-range order on type of conductivity, 3750
 Zyryanov, P. S., and G. G. Takuts, acoustic-electrical phenomena in degenerate plasma, 3638

Electronic & Radio Engineer

SUBJECT INDEX

- Absorption, (See also Resonance; Wave Propagation) acoustic, calculation of statistical coefficient from coustic, calculation of statistical coefficient from impedance-tube measurements, 3920 of fibrous materials, coefficients for, 3549 of hollow cylinders, 3547 in lined ducts, 683
 low-frequency, slit-resonators for, 687 reciprocity violation in, 332 resonant plywood panels for, 2821 in reverberant field, calculation of coefficient from impedance value, 3921
 in sea, reverberation tank for measurements, 1043
 of sound-insulation materials, 686 in transition layer between homogeneous media, 669 in transition layer between homogeneous media, 669 waveform distortion effects in, 668 of e.m. waves, by resonant slots, 2205 structures for, 1068 microwave, in artificially anisotropic media, 1847 by grid of lossy dipoles, 1846 in NH, at 6 mm Å, 2213 polarization and angle dependence of reflection of absorbers, 2915 Zeeman spectrum of atomic oxygen, 4032 ultrasonic, in metals, 3336 collision-drag effect, 2444 in quartz, at 1-4 kMc/s, 2636 in seawater, at 50-500 kc/s, 2082 in solids, at 100-1000 Mc/s, 3536 in viscous liquids, 671 ccoustices, (See also Absorption; Diffraction; 669 in viscous liquids, 671 Acoustics, (See also Absorption; Diffraction; Sound; Ultrasonics) architectural, automatic evaluation of sound reflections, 3545 design of Albcra auditoria, 688 design of talks studios, 2822 distribution of normal modes in rooms. 684 'echo parameter' criterion in, testing of, 685 effect of room shape on sound field, 3916 features of auditoria and concert halls, 1063 iteration wethod applied to speech and music, 1428 reverberation-curve characteristics, 3546 as passive relay system, using Hertzian inirror, 2852 for television, 2851 pillbox-type, with wide-angle scanning, 1448 with plane reflector, radiation patterns as function of spacing, 1097 prolate-spheroid, current distribution and im-pedance of, 1445 'radiansphere' around, 3566 radiation fields of, Fresnel approximation for, Sommerfeld expansion in, 1442 for radio-astronomy, high-resolution 2-element interferometer, 2936 'optimum' design, 2471 16-element array for 9300 Mc/s, 3659 using 360-ft parabola and plane reflector, 3962 receiving, influence of top-end capacitance on inductive coupling of, 2383 long-wire, delta-type, 3199 reflector-type, attenuation in radio links of, 1778 corner, with arbitrary dipole orientation and apex angle, 1099 circularly polarized, 1098 gain of, 3205 log-periodic, for 105-430 Mc/s, 2853 parabolic, with feed displaced from focus, 2474 rhombic, with cylindrical helices as arms, 19 design methods, 3956 scanning system, using ferrite-loaded aperture, 2472, 2473 short, bandwidth and efficiency of, 3946 slot, annular, design data, 2849 in filled and unfilled waveguide, radiation from, 21, 22 in parallel-plate transmission line, 3203 voltage breakdown characteristics, 3581 slotted-cylinder, for four simultaneous trans-1428 reverberation-curve characteristics, 3546 sound pressure fluctuations when receiver position is varied, 3915 studio design for exclusion of traffic noise in Karlsruhe, 1756 wall design for high transmission loss, 3917 artificial ear for insert earphones, 3 diffusion measurements, in reverberation chambers, 3919 using rotating microphone, 3918 insulation me surements, influence of resonances on, 2090 measurement of impedance of closed air spaces, 3180 3180 research in China, 2808 reverberation plates with electrodynamic excit-ation, 1755 spectrograms of experimental inusic, 1425 stereo-reverberation effect in, loudspeaker system for, 1065 Acousto-electric effect, experiments on Cu and al 4009 Acousto-electric effect, experiments on Cu and Al, 4009 in metals and semiconductors, 2189 Aerials, (See also Lenses, microwave) aircraft, automatic switching circuit for, 3568 aperture- and horn-type, effect of flanges on radiation patterns of, 3582 aperture-type, using helix waveguide, optimum dimensions for, 3958 using open waveguide, radiation characteristics of, 3959 using trough waveguide, 3960 arrays, broadside, directivity of, 3955 dipole, directivity factors, method of plotting, 2470 horizontal radiation patterns around support mast, 343 directivity control by servo system, 1092 directivity control by servo system, 1092 directivity improvement for pulsed signals, 3574 directivity improvement for pulsed signals, 3574 multiplicative, for reception, 3953 rhombic, design of, 3576 with rotating radiation field, 2120 scanned electrically, effective aperture of, 2847 sidelobe suppression for m., 3575 slot, for missiles and aircraft, 1774 slotted, nonresonant, 3202 strip, signal/noise performance, 2 superdirective, signal/noise performance, 329 slotted, 3572 beam-swinging, for transhorizon propagation measurements, 3198 cone-type, surface current distribution for required radiation pattern, 2841 cylindrical, back-scattering cross-section of, 1444 current distribution and input impedance of, 1085 first-order solution by generalized circuit, 23 1085 first-order solution by generalized circuit, 23 theory of, 3945 dielectric, control of radiation from, 1095 verification of theory using perspex rod, 2118 wax models for design of, 3204 diplexers, resonant-ring, for forward-scatter systems, 3196 dipole, circuit theory based on variational method, 1090 conductance of 1099

 - - conductance of, 1089 conical, characteristic-impedance calculations, 2843
 - electric and magnetic field of, 17

- Aerials, dipole, folded, bandwidth of, 2842 radiation over surface of given impedance, 3950 transient ground wave radiated from, 239 Yagi concentric feed for, 344
 directive, aperture field distribution for high-gain bean, 3952
 u.h.f., performance in complex fields, 2845 for earth satellites, spherical-array problems, 1091 efficiency calculations, 3944
 ferromagnetic, for sea-rescue transmitter, 4223 helical, elliptic, radiation field of, 3577 theory of, 3570
 hemi-isotropic, using dielectric element in wave-guide aperture, 2850
 horn-type, beam-width reduction by plexiglass plates, 3961
 with parabolic reflectors, for radio links, 1777
 linear, asymmetrically fed, radiation diagram of, 3567
 driving point and input admittance of, 1440

- Article and a second sec
- Fresnel zone of, 1096 radiation from ring-source excited cone, 3965 sawtooth, 3578 scanning, Foster-type, 2121 split reflector for reducing mismatch, 712 with wire-grid reflector, transmission-loss data, 3963, 3964 modulation of parameters for multipattern operation, etc. 2840

- modulation of parameters for multipattern operation, etc., 2840 monopole, top-loaded, earth currents near, 3947, 3948 parabelat
- paraboloid, omnidirectional, vertically polarized, 1447
- as passive relay system, using Hertzian mirror, 2852 for television, 2851

- In parallet-plate transmission line, 5203 voltage breakdown characteristics, 3581 slotted-cylinder, for four simultaneous trans-missions, 1443 radiation patterns of, 1093 slotted-waveguide, for marine radar, 711 on smooth curved surface, radiation pattern of, 3195

- on smooth čurved surface, radiation pattern of, 3195 spiral, equiangular, 3949 strip-type, current distribution with normally incident plane wave, 1086 for submarines, design of, 2469 surface-wave, corrugated and dielectric-clad, for beacon applications, 1449 scanning-type, using corrugated conductor, 3201 s.w., for ionospheric sounding, 710 microwave model for studying directivity characteristics, 709 switches, phase-shift type, for radio-astronomy interferometer, 2844 television, receiving, adaptation problems, 1775 frame-type, 3200 wide-band, for band 111, 2122 transmitting, quadruplexer for, 2119 slotted-cylinder, for v.h.f., 1094 Süddeutscher Rundfunk, 1773 u.h.f., post-installation tests of, 1088 in U.K., 3571 transmitting, automatic tuning systems, 3197 performance data for, 1087 for simultaneous transmission of broadcast programs, 16 travelling-wave, design method for, 3569 for determination of end-fire echo area of long thin bodizs, 1446 U.R.S.I. report on, 3565 v.h.f. 3-band combining network for, 733
- U.R.S.I. report on, 3565 v.h.f., 3-band combining network for, 733

World Radio History

- Aerials, v.l.f., using power transmission line, 1672 zig-zag, radiation characteristics of, 2848 Alloys, Mn-Cu and Co-Cu, dilute, low-temperature electrical and magnetic properties of, 2673 of transition metals, electron structure of, 418
- Amplification, parametric, circuit conditions for, 75, (C)2897 and frequency mixing in propagating circuits, 76 of space-charge waves, 1025 wide-band, at h.f. using artificial transmission lines, 3234 technique for 1400 or space-cnarge waves, 1025 wide-band, at h.f. using artificial transmission lines, 3234 techniques for, 1490 a.f., using auxiliary ultrasonic signal, 2514 class-B, distortion reduction in, 2883 performance with random noise signals, 2168 ultralinear, using cathode followers in place of tapped transformer, 1493 3-valve, 63 band-pass, design formulae for, 2512 cathode-follower, design data, 3235 maximum amplitude as function of output time-constant, 751 class-C, response of, 1138 d.c., compensation for changes in heater supply voltage, 750 for control systems, 748 using magnetic inodulators, 2165 for measurements, zero adjustment of, 2342 with transistor chopper, 2519 with whole-loop feedback, 1137 d.c. and chopper-type, using transistors, 1498 differential, for reducing effects of power-supply variations, 3615 distributed, using straight-wire transmission line, 1492 v.h.f., for coupling receivers to actial, 749 wide-band, for short pulses. 747

 - v.h.f., for coupling receivers to acrial, 749 wide-band, for short pulses, 747 for 200-Mc/s pulses, 2166

 - for 200-Mc/s pulses, 2166 feedback, matrix analysis of equivalent quadripoles, 2497 h.f., low-noise, using disk-seal triode, 3236 input circuits for, low-capacitance, 752 linear, for negative pulses, 62 logarithmic, voltage-operated, 3996 wide-band, 50 c/s-100 kc/s, 2169 lumistor, using coupled electroluminescent cell and photocell, 3884 magnetic, a.e.-controlled, 382 analysis of, 3237 applications of, 2516 with combined magnetic and electrical feedback, 3998

 - anaiysis of, 3237 applications of, 2516 with combined magnetic and electrical feedback, 3998 design for maxinum power, 381 with dynistor and trinistor semiconductor switching devices, 2174 fast-response, transfer efficiency of, 3238 feedback in, 2172 hali-wave, theory of, 1495 operating characteristic of, graphical determin-ation of, 3617 for servo systems, 2173 shunt-coupled, using gate voltage as output, 3997 'variable-µ', 2170 volt-second transfer efficiency in, 2171 maser, Bleembergen-type, materials for, 3242 dual system with lossless power-dividing net-work, 388 based on hyperfine levels of Cu ions, 2181 for infrared and optical wavelengths, 1857 method for tuning cavity, 74 molecular-beam, sub-mm:A, 1146 multiple-level, pulsed-field, 3623 NH₄-beam, as frequency standard, 389 noise-figure measurement, 2343 paramagnetic, theory of, 2894 3-kMc/s, using Al₄O₃.Cr₂O₃ crystal, 1145 principles of, 1500 pulsed, analysis of emission conditions, 756 ruby, 2178 L-band, tunable, 2523 low-field, 3624 wide-band, tunable, 1144 3-level, 1143, calculation of resonance cou-ditions in, 3622 ruby as material for, 3793 small-signal analysis of, 1501 solid-state, travelling-wave, 2891, 3-level, 2177 2-level, behaviour of, 73, materials for, 3037 3-level, 1502 300-500-Mc/s, 4002 'staircase' type, proposal for, 2522 weak-field, for nuclear-magnetic-resonance investigations, 2548 self-oscillator, 2521 X-band, for radio astronomy, 2892 zero-field, 2899 2-level, radiation damping effects in, 1818 3-level, double-quantum process for, 2890 as heat engine, 2212 maser and quantum-mechanical devices, theory of, 72 microwave, using negative-conductance 'tunnel' diode, 3246 negative-mass, using semiconductors, principles

microwave, using negative-conductance 'tunnel' diode, 3246

negative-mass, using semiconductors, principles of, 1824 solid-state, 4004 molecular-beam and paramagnetic-crystal types, 2888

I.35

nonlinear, effect of reaction on gain of, 2167

- Amplifiers, operational, without stabilized supply, 1494
- parametric, 2896
 cancellation of ferromagnetic hysteresis by orthogonal polarization, 3244
 cavity-type, with variable coupling, 2185
 electron-beam, 321
 cavity-type, 2066
 design of travelling-wave couplers for, 2067
 pumping of fast space-charge wave for, 1412
 with transverse modulation, 4247
 3-frequency, analysis for, 2065
 ferromagnetic, pulsed, gain measurements on, 2184
- ferromagnetic, pulsed, gain measurements on, 2184 using grain boundary in Ge, 3241 as limiter without phase distortion, 1819 'mavar' operation, 79 nonlinear-capacitance, 1820 performance of, 77 for reception of space signals, 2895 using Si-diode, for 900-Mc/s scatter link, 390 solid-state, low-noise, 1503 superregenerative, 3243 as superregenerative detectors, 3245 surface-wave, ferroelectric, 3625 travelling-wave, analysis of, 3240 4·5-Mc/s, 2524 using variable-reactance diodes, with directional bridge system, 2183 as phase-distortionless limiter, 2182 relaxation phenomena in, 3626 X-band, using GaAs diodes, 4006 4-terminal, using Ge diodes, 1148, analysis of, 4000-Mc/s, 'reactatron', using junction diodes, 1150

- 1150
 4-kMc/s, using Ge diodes, 1149
 power, grounded.grid, using disk-seal valve, design data for, 2884
 pulse, based on impact ionization in Ge, 2882 with sub-mµs rise time, 1135
 0-1-µs, using auxiliary boost circuit, 3993
 r.f., unsymmetric, sideband currents with a.m. in, 3992
 60-kW, 6-27-Mc/s, 290
 semiconductor, avalanche-controlled, theory of, 3620
 transistor, a.f., 67
- 3620 transistor, a.f., 67 for acoustic measurements, 1499 preamplifier for magnetic-tape playback, 387 push-pull, single-ended, 2885, 2885 *RC*-coupled, design of, 1816 4.5-W, sliding-bias, 384 25-W, 2886
- bias-network design using thermal parameters, 1140 Dias-network design using thermal parameters, 1140
 class-A, common-emitter, nonlinearity of, 1817
 common-base and common-emitter, gain stability and frequency response of, 1139
 d.c., design considerations for, 65
 differential circuit for reducing drift in, 1496 for servo system, 2176
 feedback, design of, 3239, equations for, 3619
 i.f., emitter-current-controlled, 2517
 l.f. design procedure, 3999
 low-noise input stages for, 4001
 low-noise input stages for, 4001
 low-noise input stages for, 4001
 low-noise input stages for, 4091
 negative-resistance, for Q-multiplication, 3618
 pulse, 2518
 with nonlinear feedback, 386
 stability of, 4000

- pulse, 2518
 with nonlinear feedback, 386
 stability of, 4000
 tetrode, for 30-Mc/s i.f. stages, 70
 thermal stabilization using half-supply-voltage principle, 71, 755
 video-frequency, design of, 385
 stagger-tuned, 754
 with 80-V output, 69
 2-stage, high-gain circuit, 66
 15-W, for public-address system, 68
 tuned-transformer-coupled, design charts for, 2513
 u.h.f., power-type, using travelling-wave valves, 380
 video-frequency, with cathode compensation, 1814, 2515
 wide-band, design data for, 1491
 for investigation of electron avalanches, 1136
 400-450-Mc/s, for radar and scatter, 64
 Analysers, amplitude, with variable-width output pulse, 1976
 frequency, uside-range, using 2 reference signals, 2712
 pulse-height, using beam-deflection valve, 3990
 multichannel. using distributed circuits, 377 2712 pulse-height, using beam-deflection valve, 3990 multichannel, using distributed circuits, 377 single-channel, 59 10-Mc/s, 2505 spectrum, for testing quartz crystals for spurious response, 1642 time-interval, encoder for, 2339 vernier chronotron, 2338 for nuclear particles, 1965 waveform, for frequency characteristics of filters, 1969

- 1969 for sorting of circuit components, 1645 for spectrum of random-noise generator, 1309 uniform transient error in power-level measure-
- Antiferromagnetic materials, Curie-point phen-omena in, 3391 nonmagnetic on in, 189 rock-salt-type, multispin axis structures in, 188

- Antiferromagnetism, in Cu₃(CO₃)₂(OH)₂, 1947 of Cu₇Fe.2H₂O, 1946
 Astrophysics, highly ionized regions in interstellar medium, 3272
 interplanetary magnetic field and effect on cosmic-ray variations, 783
 theorem on force-free magnetic fields, 784

- Atmosphere, (See also Ionosphere; Troposphere) electrical properties of, radiosonde measurements of, 1195 lower, thermal structure of, 136

- upper, in auroral zone, **3704** composition of, **1551** density variations due to hydromagnetic heat-ing, **4057** geophysical effects of high-altitude explosions, 2575

 - investigation of ionization by rockets and satellites, 3702 night airglow in, phenomenological description of, 1567
 - pressure measurements at 50-100 km, 3701 rocket-borne ion-spectrometer measurements, 3703

Breakdown, of air at high altitudes, for frequency range 100 Mc/s-35 kMc/s, 1834
of air and other gases at 9.6 Mc/s, 395
in solid dielectrics, electron bombardment as cause of, 2336
Bridges, a.c., for measurement of p-n junction characteristics, 1648
capacitance, balanced unsymmetrical parallel-T network as, 3062
coaxial displacement dielectric cell for liquids, 3063
double-T, for dielectric constant of ferrites, 4158
microwave, with ferrite isolator for paramagnetic resonance detection, 1982
Mueller, use of d.c. amplifier and recorder for balancing, 3061
Wheatstone, screned, for precision measurement of resistance, 561
Broadcasting, a.m., interference protection ratios for, 3464
measurement of program level, 3187
shared-channel, subjective tests of interference in, 3479
sound and television, progress review, 2749
stereophonic, systems for, 2397
studios, Karlsruhe, equipment of, 2016
Sudwestfunk, design of, 3182, 3183
equipment of, 3188
s.w., in Netherlands, 30-year survey, 265
Netherlands World Centre at Lopik-Radio, 266

Cables, coaxial, eccentric, inductance of, 3191 response calculations for transient waveform in, 3925

Cables, coaxial, eccentric, inductance of, 3191
response calculations for transient waveform in,
3925
solderless technique for splicing and earthing,
336
solid-dielectric, attenuation above 3 kMc/s, 337
supporting-disk data, 3926
test results under extreme conditions, 2457
theory, construction and testing, 335
Capacitance, bridge measurements of, errors due
to leads in, 1316
measurement for two infinite cones, 3820
standards, laboratory determination of absolute
unit, 2699
Capacitors, Al and Ta, dielectric films in, 725
ceramic, temperature-sensitive, using CeO, 45
electrolytic, Al, methods of increasing electrode
surface area, 2868
solid-state, advances in, 1111
Ta, increase of capacitance by etching, 359
solid-electrolyte, 2137
ferrite-cored, 726
ferroelectric, for f.m. of v.f.o., 3247
as tuning elements, 1472
hydromagnetic, 1843
impedance of, as function of frequency, 2136
paper, d.c. breakdown of, 1473
impregnants for, comparison of wool wax and
petroleum jelly, 1474
probable life of, 3219
parallel-plate, subarea method for calculating
capacitance of, 1794
printed, Ta, 2867
pulse-loaded, dielectric losses in, 2493
standard, cylindrical, sectioned, 3051
variable, giving linear frequency variation, 3973
voltage-variable, selection guide, 3599
Si-junction, 46, 3974

voltage in form of long-tailed puise, 1317
amplitude/frequency display using ratio method, 219
camera for automatic recording from, 1978
for character writing, using combination of 1.f. waveforms, 467
image distortion by RC networks in, 1318
for phase characteristics of transmission systems in range 0.1-10 Mc/s, 1310
pre-pulse techniques for extending range of, 3827
pulse system for high-accuracy V/I characteristics, 4160
sample method for displaying mus pulses, 3828
survey of types available in U.K., 1977
with travelling-wave deflection system and large field of view, 927
Cathode-ray tubes, (See also under Television)
automatic electrical welding of, 2799
energy losses at binder films of phosphor screens in, 3173
low-voltage, development of, 2713
inagnetic-deflection, errors in and coil design for, 3125
'peritron', with moving screen for 3-dimensional display, 1747
phosphors for low-scanning-speed displays, 4254
screens for, aluminized, surface phenomena associated with organic barrier film in, 2438
effect of temperature on persistence of, 2440
storage-type, for direct viewing, survey of, 1744
half-tone, survey of, 1745
iatron, 1746
thin, rectangular, 3171

iatron, 1746 thin, rectangular, 3171 for 'writing' directly on current-sensitive paper, 1748

1748
Cathodes, (See also Electron emission; Photocathodes) activated, Ni-base, research on, 2069 breakdown of coatings on, 1029 carbonization techniques for high-power magnetrons, 3530
Cs-Sb, energy distribution of electrons from, 2070 development of, 2068 discharge modes with, 2441 dispenser-type, pressed and impregnated, 2791 for high current densities, 3893 impregnated with Ba-Ca aluminate, evaporation of Ba from, 2792
Ni-matrix, processing technique for, 4250 oxide, conduction mechanism of, 1026 conductivity in magnetic field, 2428 Hall effect in, 3166

Electronic & Radio Engineer

- rocket investigations of composition of, 3700 temperature distribution in, 1876 temperature of regions of nightglow, 1877 turbulence ineasurements at 80–100 km, 4058 turoutence measurements at 80-100 km, 4058 wind determination using artificially generated Na cloud, 3302 100-800 km, model based on rocket and satellite data, 3300 Atmospheric electricity, charge distribution in clouds, 456
- thunderstorms, electrification and precipitation in, 2253
- Atmospherics, average power of impulsive noise, 1354
- effect of atomic explosions on 4067

- effect of atomic explosions on, 4067 1.f., simultaneous recordings on 4 frequencies, 813 noise measurements at h.f. in India, 2743 polatization by successive reflections from iono-sphere, 143 recording of, integrating circuit for, 2870 related to lightning discharges, 814 with superimposed pulses, recording of waveforms of, 815 v.f.f., enissions from exosphere, 1575, 3311 propagation-mode measurements, 3094 spectra of, 3313 theory of travelling-wave amplification for, 4066 waveforms of, classification and interpretation of, 459, 3312 'whistler-node' echoes remote from conjugate
- 459, 3312 'whistler-mode' echoes remote from conjugate point, 2731 whistlers, 1576 correlation with lightning flashes, 458 cyclonic disturbances as cause of, 3719 dispersion and solar activity, 144 path combinations for observed echo groups, 1577 propagation in regions of low electron density

- propagation in regions of low electron density, 1578
- 1578 27-kc/s, sudden enhancement of, solar-fiare anomaly in, 1579 at 27 and 100 kc/s, observations at Delhi, 1580 Attenuators, coavial, alignment aid, 3927 microwave, calibration by absolute bridge method, 1123
- 1123 Aurora, and airgiow, photoelectric measurements of H₂ emissions in, 3310 artificial, due to nuclear explosion, 1569, 1868 australis, radar echoes at 69 Mc/s, 141 australis and borealis, comparison of radar echoes from, 140 displacement of radiant point during disturbance, 138 disturbances contening of arti-

- from, 140 displacement of radiant point during disturbance, 138 disturbances, scattering of radio waves during, 2001 drift effects related to radiation belt and solar wind, 4063 electric-field theory of, 1887 equal-frequency lines (isochasms), theoretical and observed, 2975, (D)4062 formation of, 1568 intense, 1.1. reflections from 75-90 km during, 812 ionization and magnetic disturbances, 1570 at low latitudes, spectroscopic observations, 2592 phenomena during storm, 3309 radar echoes from, horizontal motion observed at Saskatoon, 2255 movement related to magnetic-disturbance current system, 2593 polarization of, 4064 u.b.f. observations of, 1573 at 400 Mc/s, 139 radio reflections from, angle-of-arrival measure-ments at Kjeller, 2254 geometry of, 1671 on ionograms obtained in minauroral region, 457 at low latitudes, 1670 subvisual, and simultaneous occurrence of noise bursts on 4-6 kc/s, 2974 v.h.f. radar for research on, 1574 Barretters, (See also Power supplies) dry, using C-nitroso compounds, 2402 internal resistance, pulse measurement of, 2760 lead-acid, self-discharge reactions in, 2403 Book notices and reviews, The Advanced Theory of Statistics, Vol. 1: Distribution Theory, 1639 Advances in Electronics and Electron Physics, Vol. 9, 327

1639 Advances in Electronics and Electron Physics, Vol. 9, 327 Atmospheric Electricity, 1201 Handbuch der Physik, Vol. 16, 3657 The Ionosphere, 1200 Light Scattering by Small Particles, 1519 Radio Research, 1957, 2077 Russian-English Electronics and Physics Glossary, 660 Scientific Uses of Earth Satellites, 2595 Semiconductor Thermoelements and Thermo-electric Cooling, 207 Transistor Circuit Engineering, 757

Cathodes, oxide, noise in, 1027 preconversion technique for, 3891 processing of, servo system for, 651 reversible poisoning of, 4249 SrO, dissociation by electron impact, 3892 oxide-cored, for electron microscopy, 3078 point-type, for electron microscopes, 3077 Cells, (See also Batteries; Photocells) dry, Mg-BiO, 3865 Zn/Hg-dioxysulphate type, 3866 Circuits, (See also Networks) amplitude-comparison, 3600 cathode-follower, for d.c. reference level, 2164 clamping or d.c. restoration, 2138 construction using thin-film components, 354 counter, coincidence, using transistors and diodes, 3230 decade, 1-Mc/s, using transistors, 1131 dekatron, for addition and subtraction, 1110, 1812 multiphase-output, from d.c. to 500 kc/s, 58 ring.ture 2564 2267 1812
nultiphase-output, from d.c. to 500 kc/s, 58
ring-type 2506, 2507
transistor, 3231
coupled, double-tuned, response of, 1815
stagger-tuned and synchronously tuned, correlation between, 364
wide-band, design data for, 3995
differentiating, 1795
diode and triode, with short time-constant, 3221
ferroresonant, 2140
with square-loop reactor, 2141
gating, neon-bulb, for digital computers, 358
phase-selective, rejecting quadrature component, 719
integrating, compensation for waveform distortion gating, neon-bulb, for digital computers, 358
phase-selective, rejecting quadrature component,
719
integrating, compensation for waveform distortion
due to valve capacitances, 1479
feedback, 1.f. noise reduction in, 369
long-time-constant, pulse response of, 2870
limiter, 2494
cathode-coupled, characteristics of, 1813
microcircuits with distributed resistance and
capacitance, 3972
microminiaturization, micromodule system, 2485,
2486
program at D.O.F.L., 2484
microwave, using low-noise devices, 3971
theory and techniques of, 3175
miniaturization of, using integrated semiconconductor devices, 3213
modular, integrated micromodules, 2863
potted and printed, 2862
printed, electroless copper plating for, 3047
foil-clad laminates for, 355
manufacture and assembly of, 1788
for microwave links, 2487
through-connections for, 38
pulse, using cold-cathode valves, 374
time/height converter, 2879
avalanche-type, 2878
20-ms linear gate, 2880
pulse-forming, for radar, 375, 742
regenerative, using 'hybrid' valve-transistor
arrangements, 2877
seouential, using transistors, 3613
switching, coincidence-diode, for radar displays,
1792
using crystal diodes, 2866
using electroluminescent cells and photocon-1792 using crystal diodes, 2866 using electroluminescent cells and photocon-ductors, 1108 ferroelectric, 'transpolarizer' with stored setting, 2864 2864 using gas-filled diode, 724 using magnetic cores, 2492 performance of, 3217 phototransistor, temperature-stabilized, 1109 representation by binary-decision programs, 3215 representation by binary-decision programs, 3215 ring-type, for high-speed multiplexing, 3218 using saturable transformers, 1471 using semiconductors, current build-up in, 889 microwave, 3597 ternary, 1789 transistor, 43 delayed switch-off effect in, 722 for missile count-down, 3598 parameters of various types, 723 with voltage-controlled delay, 2865 transistor, nodal construction method for, 1796 trigger, bistable, using unijunction transistors, 744 increased sensitivity using crystal diode in feedback loop, 57 with series valve connection, 2163 Colls, ferrite-cored, for a.f., 1790 inductance, calibration at power and audio frequencies, 2346 Colour, vision, characteristics and two-coordinate system for, 3629 Communication circuits, h.f., effect of echo on operation of, 3471 maritire, signal strength measurements at Caliz, 3859 'minimum-loss operation time' for, 258, 1359 'minimum-loss operation time' for, 258, 1359 U.K.-Commonwealth, performance index for, 'min. U.K.-Co. 261 261
Communication systems, (See also Photo-telegraphy; Radiolinks)
a.m., long-distance, addition of distortion voltages in, 3856
binary-code, decision feedback systems, 591
decoding techniques in, 27447
error probability in, 2389
feedback, 2387
keying systems, error probability in, 2746
in Brazil, 3176
in buildings, field-strength measurements at v.h.f., 1688
compandor for speech transmission, 2395

Communication systems, for data transmission over telephone lines, 1684 f.m. digital subset for, 2392 using earth satellites, 964, 2012 'Frena' and 'Frenac', nonlinear system for trans-missions at high noise levels, 2753 in Chana, 961

- missions at high house levels, 2000 in Ghana, 961 l.f., design of, 2750 line, transistor applications in, 594 meteor-burst-type, choice of frequencies for, 597 JANET, 4198
- microwave, network for Pacific coast, 2398 tropospheric-scatter, using angle diversity, 2751 mobile, with 920 channels between 30 and 76 Mc/s, 262

- 262 multichannel, using angular modulation, r.f. powers and noise levels in, 598 carrier telephony on power lines, 2748 f.m., measurement of derree of intermodulation due to mismatch, 2396 frequency-diversity, two-tone, 2011 11-kK/c/s, TJ, 3106 p.c.m., digital, regenerative statistics of, 957 timing of regenerative statistics of, 967, 968, 969 for telephone service, 6 kK/che, 2392 11-KMUCK, 1.J. 3100
 p.c.m., digital, regenerative statistics of, 957
 timing of regenerative repeaters for, 967, 968, 969
 for telephone service, 6-kMc/s, 2393
 multichannel relays, C.C.I.T.T. recommendations and white noise, 4199
 multiplex, f.m., Canadian TD-2 transcontinental microwave network, 973
 echo distortion in, 3472
 for studio-transmitter links, 3107
 h.f. error-correcting system for REM, 3104
 receiver and modulation equipment, 3476
 selective, at Allentown-Bethlehem, P.a., 3477
 f.m., microminiature decoder for, 2018
 performance in presence of thermal and atmospheric noise, 963
 planing of, evaluation method for comparison of radio and cable systems in, 1355
 pulse, frequency-shift method for, 3470
 'Rake', for multipath channels, using correlation technique, (D)596
 R/T, carrier-frequency-shift signalling for, 4200
 intelligibility of speech with restricted frequency characteristics, 2755
 multichannel, high-frequency bridging, branching and interconnecting of, 1362
 SAGE data signalling method, 259
 in space, infrared receiver for space vehicles, 4197
 minimum transmitter weight for, 3141
 problems of, 3469
 telemetry system analysis, 3860
 s.b. and d.s.b., suopressed-carrier, for aeronautical services, 2752
 s.b. and d.s.b., suopressed-carrier, for aeronautical services, 2752
 s.b. and independent-sideband, for ground/air communication, 263
 stereophonic, compatible, using a.m./f.m. multipox, 3105
 using f.m. multiplex, 1363
 using structure, system for, 966
 1.f. and v.l.f., frequenccy-shift keying for, 965
 p.c.m., phase correcting systems for, 593
 error-correcting 'autoplex' system for, 966

- n. and then, herefully sint systems for, 599
 teleprinting, coder and decoder for, 1685
 over long-distance radio links, 960
 telephony, carrier-current, bridge negative-feedback amplifiers for, 974
 tropospheric-scatter, description of Canadian equipment, 975
 design of, 1360
 evaluation of, 595
 multichannel, t.m., system parameters for, 1361
 quadruple-diversity method, 972
 tests, Start Point-Chelmsford, 260
 in U.S. army, 2744
 v.h.f., for port and harbour control, 3480
 vocoder, time-division, 2394
 waveguide transmission with h.f. carrier, pulse distortion in, 3473
 Communication theory, application to amplitude compression, 3466
 capacity of asymmetric information channels, 3103
 channels with side information at transmitter, 592
 coding systems, binary, burst-correcting, 3468
 variable-length, 3467
 binary and Gaussian, merits and methods of detection of, 2010
 definitions of and n in signal detection, 3854
 demodulation and detection processes in, 959
 discrimination of signals in noise, 1357, 2008
 error-correcting codes, with constant bit-rate of transmission, efficiency of, 1358
 mathematical theory of, 1683
 using regenerative shift-register sequences, 257
 error probability for optimum codes in Gaussian channel, 2745
 for infinite alphabets. 958
 physical interpretation of Shannon's ambiguity, 3853
 sampling of signals without d.c. components, 1356
 speech transmission, threshold levels for quantization, 3852
 Components, (See also Circuits, printed; Electronic equipment)
 electroforming technique for complex shapes, 4143
 microwave, production testing equipment for, 221
 selection f

World Radio History

- Computers, analogue d.c., negative-resistance circuit for, 3605
 differential analyser, Fourier analysis by, 33
 for evaluating radar performance, 1465
 function generators, biased-diode, design of, 2861
 rotating-disk type, 2858
 for sines or cosines, 1457
 tapped-potentiometer, 35, quadratic interpolation by, 2133
 using loaded potentiometers, error reduction technique, 3969
 matrix programming of, 347
 multiplier, using Hall effect in semiconductors, 349, 350, 2131
 multiplier-divider, using thyrite resistors, 1458
 for prediction of sound propagation, 3207
 ratio calculator, 1102
 resistance-network, design principle for, 2480
 use of, 2481
 for simulation of aircraft performance, 1466, 2477
 storage systems for, magnetic-drum, 348
 analyser for relay-circuit contacts, 1460
 control system softies, 1105
 digital, ACE, 2128
 ADDAM II differential analyser, 1780
 adders, controlled by magnetic cores, 3210
 applications, for lens designing, 2483
 for automatic graph plotting, 2859
 binary multiplication in, 2856
 capacitive sensing system for punched cards or continuous foil, 1455
 charter display system for output of, 3968
 counting circuits for, using transistors and magnetic cores, 2479
 C.S.C.E. Pisa, using parametric cells, 3966
 data-processing, automatic failure recovery system, 2153
 automatic magnetic 'reading' equipment for, 3586
 information handling in, 1454
 magnetic-tape recording system for, 1464
 tape amplifiers for, 27

 - 3586 information handling in, 1454 magnetic-tape recording system for, 1464 tape amplifiers for, 27 efficiency of logical elements as multipurpose bias devices, 1461 electromechanical input-output equipment, 26 high-speed, using ferrite cores and transistors, 2127

 - 2127 test generator for, 3585 with inductive control of switching, 3967 'laddic' ferrite device for switching in logic circuitry, 1463 logic synthesis of high-speed comparators, 1456 logic systems, using magnetic elements, 1104 based on signal phase in nonlinear reactances, 2126

 - using transistors and square-loop ferrite cores, 351

 - magnetic-core matrices for logical functions, 2860 magnetic materials for storage and switching, 1782 Instant Internals for storage and switching, 1782 operation of, 25 parametric subharmonic oscillators for, 3590 'parametron' reactance element for, 3588 pulse generator using transistor blocking oscillator with saturable transformer, 3970 rectifier networks for, 29 sequence transducers, network analysis of, 352 for simple algebraic functions, 1452 sin N, cosN and N^{1/m} computations by, 2857 for spatial problems, operating on information in planar form, 30 standard block design using transistors, 2855 storage systems, ferrite-core, using transistors, 1783 ferrite plates for end-fired type. 36

 - 1783 ferrite plates for end-fired type, 36 ferroelectric, 717, 1781 magnetic, core, using core-threading technique, 3587, noise problem in, 1787 magnetic-disk, 2129 magnetic-drum, control apparatus, 346, track switching system for, 718 magnetic-film and ferrite-core characteristics, 3212

switching system for, 718 magnetic-film and ferrite-core characteristics, 3212 matrix-type, using ferrites, 2482 punched-tape, 1785 storage and processing of data using magnetic tape, 1786 switching circuits using transistors for, 1784 switching elements for, cryosar', 3211 superconducting, 3209 tabulated reference to 27 models, 1779 test generator for, variable-frequency, 3591 transistor, operating experience with, 2132 1.Mc/s, transistor circuits for, 3229 digital/analogue conversion, using bistable multi-vibrator, 3206 using cryotrons, 1103 for storage-tube deflection, 2135 printing of pulse-code data using shaped-beam c.r. tube, 34 random-number generator using subharmonic oscillators, 2476 conduction, in solids, theory of, 485 surface, of insulating solids, criterion for, 3252 theory of electron transport in magnetic fields, 4014 in ThO, crystals, polarization effects in, 3335 induced by radiation in CdS and polyethylene, 2672 of metals, evaluation of, 1507 of monovalent metals, 4015 Conductors, charge penetration in, 3251

Conductors, charge penetration in, 3251

Conductors, penetration of transient e.m. field in,

- 2905 solution of Bloch's equation for electrons in, 1914 with wavy interface, e.m. field distribution in, 2904 Conferences and conventions, acoustics, Moscow, June 1957, 661 British Association Meeting, Glasgow, Sept. 1958, 1171, 1202

- British Association Meeting, Glasgow, Sept. 1958, 1171, 1202
 3 papers on radio navigation aids, 2978
 cosmical gas dynamics, Cambridge, Mass., June 1957, 1861
 cosmical gas dynamics, Cambridge, Mass., June 1957, 100
 electrical discharges, Physical Society, Swansea, Sept. 1958, 2196
 electronic standards and measurements, Boulder, Aug. 1958, 1303
 electronics reliability symposium, Philadelphia, Jan. 1959, 2605
 fluctuation phenomena and stochastic processes, Physical Society, London, March 1959, 4007
 I.E.E. Radio and Telecommunications Section, Chairman's address, 1421
 I.G.Y. Special Committee, 5th Assembly, Moscow, Aug. 1958, 3674
 information processing, Paris, June 1959, 3208
 I.R.E. National Convention, New York, 1959, 2801
 long-distance transmission by waveguide, I.E.E., London, Jan. 1959, 1437
 luminescence, Estonia, June 1956, 2997
 microwave valves, I.E.E., London, May 1958, 2788, 2800, 3159, 3524
 physics of magnetic phenomena, Moscow, May 1956, 3035

- 2788, 2800, 3159, 3524 physics of magnetic phenomena, Moscow, May 1956, 3035 propagation of radio waves, Paris, Sept. 1956, 1333 radiation effects in semiconductors, Tennessee, May 1959, 4089 radio aids to aeronautical and marine navigation, I.E.E., London, March, 1958, 2259 radio links, Rome, June 1957, 2014 rockets and satellites, Moscow, July/Aug. 1958, 1870 semiconducting SiC Boston, April 1950, 3771

- 1870 settines, indeevit, jury/rdg. 1936, semiconducting SiC, Boston, April 1959, 3771 solid-state memory and switching devices, London, Sept. 1958, 2478 solid-state physics, Brussels, 1958, 497 space vehicles, satellites and missiles, Buffalo, N.Y., June 1958, 2239 stereophony, I.E.E., London, March 1959, 2086 Swiss Physical Society meeting, Neuchatel, Sept. 1957, 758 transistors, I.E.E., London, May 1959, 3511
 Onnectors, coaxial hybrid-ring analysis of 3552
- Connectors, coaxial, hybrid-ring, analysis of, 3552 as microwave filter, 3551
- Connectors, coaxial, nyorid-ring, analysis or, 3552 as microwave filter, 3551
 Control systems, (See also Electronic applications; Frequency control; Servomechanisms)
 digital, for positioning shafts, using telephone-line carrier system, 1656
 feedback, test equipment for, 1651
 review of techniques for, 3861
 Converters, (See also Frequency, converters)
 d.c., high-power, using transistors, 1470
 d.c./a.c., using transistors, 3483
 design data, 267
 for driving induction motor, 1983
 for 3-phase 115-V output, 3482
 using 4 transistors in bridge circuit, 1698
 20-kc/s, using power transistors, 2021
 d.c./d.c., using transistors, 4207
 parametric, microwave, 2896
 Cooling, air, chassis design for, 353
 forced-convection, prediction of temperatures in, 1750
 liquid, for airborne equipment, 1420

- forced-convection, prediction of temperatures in, 1750
 liquid, for airborne equipment, 1420
 of semiconductor devices, nomograms for, 3146
 Cores, (See also Coils)
 ferrite, for television receivers, test methods, 3057
 powder, Fe, properties of, 2323
 Cosmic radiation, (See also Radio astronomy)
 balloon equipment for monitoring, 437
 corpuscular, low-energy, at high latitudes, 2551
 cosmic-rocket data on, 2231
 cut-off rigidity and geomagnetic field, 3280
 effect of magnetic anomalies on belt of trapped particles, 3662
 energy spectrum of, 419
 flux and energy spectrum of α particles during solar maximum, 3279
 increases in, interplanetary magnetic-field model for explanation of, 783
 related to solar flares, 2557
 intensity of, cause of inaccuracies in prediction of, 1524
 decreases in, 27-day, latitude variation of, 1862

- mtensity of, cause of inaccuracies in prediction of, 1524 decreases in, 27-day, latitude variation of, 1862 1956-1958, 4037 fluctuations, at southern stations, 1860 measurements in stratosphere, 3277 variations, review of, 4036 at solar maximum, 3278 during two solar cycles, 1523 in interplanetary space, rocket and satellite investigations of, 3718 investigations of, arth satellite, 3663 measurements of, at distances up to 107 400 km from earth, 2553 with Pioneer IV, 4041 nature of sources, 3274 observations, before intense solar activity, 1179 of 1958 6 over Australia, 4042 proton, during solar flare 12th May 1959, 4040 r.f., absorption associated with solar event, 789, 1521
- 1521 trapping beneath ionosphere of, 788 terrestrial corpuscular radiation due to, 2216 theory of cosmic-ray equator, 3661 Van Allen belt, cause of minimum between zones, 4038 origin of, 2217, 2552 upper boundary of, 4039 Cosmic rays. See Cosmic radiation.

Direction finders, c.r.o.-type, s.w., Telefunken, 2257
 2-channel, integration method for improving bearing evaluation in, 2258
 h.f., with averaging system and automatic read-out, 2600

out, 2600 interferometers for tracking airborne vehicles, 1583 long-base-line, error reduction in, 3720 v.h.f., automatic, using rotating Adcock aerial, 817 true-phase capacitive goniometers for, 4068 Direction finding, coherent-wave, component determination using 2-channel c.r. d.f., 816 h.f., errors caused by nearby vertical reradiators, 1203

1203 3-dimensional, using spaced aerials, 3314 Discharge tubes. See Valves, gas-filed. Discharges, (See also Breakdown; Plasma) cold-cathode, space-charge effects in, 1833 effect of coupling oscillator coil to discharge tube, 1156

1156 - electrodeless, in air at reduced pressure, effect of magnetic field on, 83 glow-to-arc transitions, ionizing-potential space waves in, 3254 glow-type, hollow-cathode, 2909 h.f., torch-type, electron temperature and noise in, 3253

Hg-vapour, noise spectra measurements in, 4019 Joshi effect, potential variation in, 2530 low-density, theory of cathode sheath in, 82 propagation of non-ionizing shock waves in, 4016 pulse, gas recovery after, method of studying, 2531 'silent', r.f. oscillations in light and darkness in,

1155
 space-charge field-emission hypothesis applied to, 2907
 thermal noise in, 1158
 wire-cylinder, in air, in relation to space-charge field-emission hypothesis, 394
 Discriminators, frequency, linear, wide-band, using transmission lines, 2526
 microwave, for stabilizing klystron oscillators, 1487
 Distortion, of am and fm simple, 2007

Distortion, of a.m. and f.m. signals, 2007 harmonic, in f.m. system, 1504 of signal on b.f. carrier in circular waveguide, 3473

Earth, conductivity, mapping by radio technique in U.S.S.R., 434 measurement of, 3420
Earth satellites, applications, for transoceanic communication system, 2012 for verification of theory of relativity, 3684 atmospheric density determination, lifetime data for, 3686 from orbital data, 3689, 3695 irregularities in, 2571 at 200-400 km, 2955 atmospheric pressure and density measurements by, 1871, 3694 instrumentation for, 439 cosmic-radiation investigations by, 3690 analysis of, 2958 Instrumentation for, 3663
Doppler measurements on, 1191, 3697 velocity determination from, 442
electron energy levels at 470-1880 km recorded by, 3294

velocity determination from, 442 electron energy levels at 470-1880 km recorded by, 3294 errors in tracking, due to refraction at ionospheric heights, 3698 Explorer series, firing system, instrumentation and tracking of, 1546 flight principles and velocity data, 2950 geodetic information from, 1185 geomagnetic field measurements by, 3693 gravitational torque on, 117 ion-concentration measurements by, 3696 ionization trails, radio reflections from, 121, 2963 ionosphere investigation by, 1873, 3295 launching problems, 3680 lifetime determination and orbit perturbations, 3681 optical observation, over polar regions, 793 tracking program for I.G.Y., 2566 in U.S.S.R., 3288 orbital acceleration of, atmospheric effects in, 2564 orbital data, calculations, 3662 and geophysical factors, 3683 value for earth's flattening obtained from, 2567 orbits of, air-drag effect on, 3287 allowing for earth's oblateness, 1184 described by difference equations, 119 irregularity in, 797, 1543, atmospheric tides as cause of, 2565 cause of air resistance changes in, 1186 coordinate system for, 3687 determination from tracking data, computer program for, 2568 Doppler method for determination of, 1188 effect of earth's oblateness on, 2233, 2234 prediction of, 2232 around unsymmetric central body, 1541, (D)1866 polyhedral, for accurate orbital data, 794 radar scattering from, effect of Faraday rotation

around unsymmetric central body, 1541, (D)1866 polyhedral, for accurate orbital data, 794 radar scattering from, effect of Faraday rotation on, 1345 radio-astronomy investigations by, 3292 radio observations of, comparison of methods of studying ionospheric structure by, 799 derivation of ionosphere data from, 1548 ionospheric effects on, 1549 in Italy, 1192 signals from, Faraday fading of, deduction of ionospheric electron content front, 2572, correction for, 450 .Faraday rotation of, 796 magneto-ionic effects up to 2 000 km in. 2961 recording of, 2573 solar corpuscular radiation investigated by, 3293 time-dilation measurement method, 3688 tracking, methods for, 122, 4047 'minitrack' system for, 1190 photoelectric optical method for, 1189

Electronic & Radio Engineer

- Counters, (See also Circuits, counter) diamond, with small electrode spacings, 1990 G-M, end-window, improved design of, 3079 for nucleonics, 3446
 radiation, with magnetic recording of pulse-amplitude data, 1989
 self-quenching mechanism of spreading discharge in, 1332
 scintillation, photomultiplier-type, resolving power of, 3081
 review of, 322, 3080
 Couplers, (See also Waveguides) directional, CR-type, nutually coupled, 9 measurement of directivity of, 3821
 Crystals, (See also Molecular systems; Piezoelectric materials; Quartz; Resonators) growth of, floating-zone technique for, 2337
 SiOs, and GeOs, infrared studies on polymorphs of, 205
 with zinc blende structure, calculation of lattice oscillations in, 3413
 Delay lines, (See also Computers, storage systems) magnetostrictive, for pulsed video signals, 1134 torsional, 2881 quartz, for radar systems, 2511
 ultrasonic, design of, 28 Hg, characteristics of, 361 measurement method for, 2698
 Detection, of asymmetric-sideband signals in noise, 248
 of co-channel f.m. signals, by correlation method, 581
- of co-channel f.m. signals, by correlation method, 581
- 581 microwave, tests on coaxial diodes for, 2794 power-law, with 3 input signals, multiple Fourier analysis for, 2382 of pulsed signals in noise, optimum filter functions, 247

- of pulsed signals in noise, optimum filter functions, 247
 response of nonlinear devices to band-limited h.f. signals and noise, 1674
 step system for multiplex systems, 590
 Detectors, correlation devices for weak signals, 3099
 correlation function of output noise with biasing and limiting effects, 2005
 diode, analysis for asymmetric-sideband signals, 249
 optimum, with log I₀ characteristic, for weak signals in noise, 2004
 phase, diode, push-pull, theory and design curves for, 1152
 product-type, using pentagrid converter, 2898
 for symmetric or asymmetric-sideband signals, 580
 Dielectric constant, contribution of exciton to, 1831
 of conducting liquids, 1.f. measurements, 215
 method using coaxial cable, 921
 method based on Weissfloch transformation theorem, 4153
 static, molecular theory of, 761
 Dielectric properties, of glacier ice, 1994

- theorem, 4153
 static, molecular theory of, 761
 Dielectric properties, of glacier ice, 1994
 of ice crystals, 1600
 of low-loss materials, free-space min-\u03b3 technique for measuring, 2348
 measurement bridge for 10 c/s-50 kc/s, 1305
 measurement technique for liquids, using H_{e1} resonator, 922
 Onsager's theory of, 392
 polarization of gases, quantum theory for, 2901
 of polycrystalline stannates and cerates, 2626
 Dielectrics, (See also Insulating Materials)
 artificial, anomalous dispersion in, 482
 dispersive, for beam scanning, 2124
 \u03b4/4 matching of, 2125
 formed by array of thin films, 1154
 rod-type, reflections from, 2123
 BaTiO,, breakdcwn field of, temperature depend-ence of, 2627
 ceramic, effect of compression on permittivity, 481
 thermal conductivity of, 2628
 low-temperature properties at 9-1 kMc/s, 1601
 thermal expansion coefficient of, 2629
 Ba(Ti,Sn)Oa, and Ba(Ti,Zr)Oa, ternary systems, 838
 ceramic, after-effect in, 3328
 light-weight, 839
 gaseous, C₄F₆, properties of, 3415
 inhomogeneous electrical dispersion phenomena in, 837
 (NH₄)₈ SO₄ and (NH₄), BeF₄, transitions in, 836

- inhomogeneous electrical dispersion phenomena in, 837
 (NH₄)₂ SO₄ and (NH₄)₂ BeF₄, transitions in, 836 nonferroelectric, relaxation polarization and losses in, 480
 solid, impedance of layers of, 2271
 Diffraction, acoustic, of converging beams, 2813
 of acoustic and e.m. waves, asymptotic solution of problems in, 1850
 effect of fluctuations on intensity distribution near focus of lens, 2917
 by smooth object, geometrical theory for, 3265
 by wedges or corners, for plane, cylindrical or spherical wave, 1167
 of e.m. waves, by circular hole in plane screen, comparison with optical microscope, 2206
 by dielectric strips, 1516
 at ideally conducting medge, 4028
 Kirchoff-Young theory of, 2918
 by perfectly conducting solid, 774
 polarized, by wide slit and complementary strip, .
 411
 skew-plane, by absorbing wedge. 3266

411
 skew-plane, by absorbing wedge, 3266
 by slit, approximation for, 1851
 by slit and rectangular apertures, intensity distribution near focus 3256
 in inhomogeneous media, asymptotic theory of, 2539

2539 geometric theory of, 2538 of light, by ultrasonic waves, intensity distribution for, 1051 at oblique incidence, 1049 of ultrasonic waves, by arrays of rods, 1048 Direction finders, c.r.o.-type, s.w., comparison of, 2256

- Earth satellites, tracking, 108-Mc/s interferometer system for, 123 trajectory determination, ground equipment for, 441

- Sarth satellites, tracking, 108-Mc/s interferometer system for, 123 trajectory determination, ground equipment for, 441 U.S. and U.S.S.R., tabulated data on, 3679 telemetry data for, 124 U.S.S.R., observations related to ionospheric propagation, 2952 tracking by Doppler measurements, 443 weather observations prelated to ionospheric propagation, 2952 tracking by Doppler measurements, 443 weather observation by, 2360 instrumentation for picture transmission in, 2715 1957 a (Sputnik 1), determination of orbit and regions of reception, 120 Doppler measurements at Johannesburg, 445 electron density determinations in outer iono-sphere by, 3298 ionospheric information from, 3296, 3297 ionospheric information from, 3291 Royal Society discussion, 2951 tracking of, using h.f. d.f., 798 1957 β (Sputnik 11), brightness fluctuations of, 2956 change of inclination of orbit of, 1542 cosmic-ray intensity variations recorded by, 2959 field-strength recordings at 40 Mc/s in West Germany, 3291 gravitational-field investigations by, 792, 4048 instrumentation of, 440 last minutes of, 447 orbit of, changes in inclination to equator, 2235 motion of nodal line in, 118 radar observations of, 3290 solar-flare effect on period of, 449 1958 β (Vanguard I), instrumentation, orbital data and applications of, 3668 orbit of, determination of coefficient J of gravitational potential from, 1867 variations related to gravitational field, 2236 solar effects on motion of, 4050 1958 β (Vanguard I), instrumentation, 2957 auroral ionosphere investigation using, 4052 diurnal lapse of signals from, 295

- ratio observations of, 2009 signal-strength recordings, in Alaska, 1193 in Ohio, 2570 upper-atmosphere investigation by, 1872 1958 ¢ (Explorer IV), cosmic radiation increases detected by, 3692 observations of radiation belt by, 2238
- Electrets, CaTiO_s, anomalous stability of, 1603 phenomenological theory of, 1602
- Electroacoustics, standards, calibration and errors of, 3186 Electrodynamics, classical, as distribution theory,

- Electrodynamics, classical, as distribution theory, 404 nonlinear, formation of discontinuities in, 2914 Electroluminescence, (See also Phosphors) in Cu₂O, and current creep effects in rectifiers, 3005 display panels, for automatic displays, 3434 for character generation and storage, 1654 transfluxor-controlled, 568 display systems, ELF, 225 'sylvatron', 224 in GaP and InP, bimolecular transitions at rectifying junctions, 3737 of insulated particles, 1215 mechanism of, 1597 'memory' effect in enhancement of, 1213 modulation of photoluminescent emission by alternating field, 831 processes and application to picture tubes, 1909 screens for television display, problems of, 566 in SiC, 3003 in SiC *n*-n junctions, 1910 Electrolyte tank, anisotropic field plotting in, 3825
- Electrolyte tank, anisotropic field plotting in, 3825 servo system for automatic tracing of equipotential curves, 3428 space-charge simulation by current injection, 2356, 2709
- 2708
- 2708 Electromagnetic field, in stratified medium, excited by dipole in surface, 2920 Electromagnetic theory, electron wave functions, consistency condition for, 2537 e.m. waves in crystal with exciton absorption, 409 helical coordinate system for, 773 of induction, 407 Maxwell's equations, in general relativity theory, 1514 solution in terms of spinor notation, 2000

- Maxwell's equations, in general relativity theory, 1514
 solution in terms of spinor notation, 2900
 uniqueness criterion for solutions of, 3628
 Maxwell's and Helmholtz's equations, application of distribution theory to, 405
 of 'singular' induction, 406
 Electron beams, axially symmetric, with uniform velocity profile, 3526
 distribution of particles with multiple scattering, 1837
 effect of inclination of focusing electrodes on formation of, 2060
 homogeneous, plasma heat-exchange technique for producing, 397
 influence of angle of diffusion on energy spectrum in thin films, 3255
 magnetic analysis based on Lorentz effect in, 2199

- Électron beams, magnetically focused, anomalous noise in, 2789
 characteristics of, 3888
 periodic permanent-magnet structures for, 1021
 parallel-flow, periodic e.s. focusing of, 2061
 partially neutralized, perveance and Bennett pinch relativistic, intense, behaviour of, 4017
 rotating, space-charge-wave harmonics and noise in, 1736
 sheet-type, aberrations in, 2908
 space-charge in, compensation of, 1836
 space-charge flow in, solution of equations for, 764
 splitting effect on penetrating magnet, 3636
 stationary, magnetic forces and relativistic speeds in, 85
 theory of formation and trajectory in magnetic field, 2059
 Electron emission, (See also Cathodes; Photoelectric emission)
 field-type, total-energy distribution for, 2197 measurement of, 2198
 from Hg films in discharge tube, 1157
 from Mo, after electron bombardment, 3258
 secondary, due to ion beam, energy spectrum analysis, 1838
 of metals, theory of, 3257
 from Ng() films, 2316
 from Ni, 3789
 thermionic, from Mo, effect of magnetic field on, 1945
 wave-mechanics correction of Richardson-Dushnan equation, 2912

Electronic applications, 'tellurometer', for measurement of distance, 1980
video differential planimeter, 3067
Electronic equipment, in Brazil, 3176
in naval ordnance, design problems, 2803
production and assembly techniques for, 1037
reliability of, calculations on, 2806
design factors for, 2076
'interaction' in, 1038
numerical approach for, 2804
Soviet, review of, 3899
transistorized, data on, 3592
Electrons, collision probability in gas, microwave measurement method, 768
relativistic flow in straight lines with no external magnetic field, 396
slow excitation of nolecular vibration and rotation by, 3259
spin kinematics in uniform field, 99
Electrostatics, generation of static charge on high polymers, 4013
interaction of two charge distributions, 760
potential and capacitance of torus, 4012
potential distribution usar p-n junction, 1506
simple method of calculating capacitance, 2193
surface charges on insulators, 2527
Equalizers, constant-S, 3226
Laguerre-function, using passive elements, 1481
Ether, deflection of light waves by movement of, 3248
Exhibitions, Audio Fair, London, April 1959, 2095
electronic computers, London, 1953, 715
German Radio, London, Sept. 1959, 3897, 4255
Physical Society, London, April 1959, 2802
S.B.A.C., Farnborough, Sept. 1959, 4256

Faraday effect. See Magnetic effects.
Ferrimagnetic materials. See Ferrites.
F'errites, with anomalous magnetization loops, hysteresis losses of, 3400
Ba, anomalous characteristics of samples con-taining CaO.SiO, 2685
dielectric properties of, anisotropy in, 3807
magnetization curve analysis, 3806
substitution of cations in, 540, 541
BaO.GF.Qo, magnetization and structure of, 899
containing Co.perminvar effect in, 1284, 2324
semiconducting properties of, 4135
dielectric-constant measurement bridge for, 4158
Dy-Y, Dy-Gd and Dy-Er mixed garnets, properties of, 2331
e.m. fields in ellipsoidal samples, 1286
Er garnet, Al- and Cr- substituted, interpretation of properties of, 1290
Fe₂O₄ and (NiO)_{e-36}Fe₂O₃, Hall-effect measurements on, 3403
'ferroxcube', permeability tensor of, at 24 kMc/s, 1293

1293 'ferroxplana', crystal-oriented, 2687 flux reversal in, modified rotational model for, 900 frequency characteristics of, 3398 garnets, domain observation by transmitted light, 200

200 growth of single crystals of, 1289 Gd-Er and Gd-Y mixed garnets, properties of, 1633 Gd-Fe garnet, microwave resonance in, two-sublattice model for, 3043 as gyrotropic media, reciprocity relations for, 3044 hysteresis loop evaluation by computer, 2326 kinetic processes in, phenomenological theory of, 1285

1285 Li, susceptibility of, transverse, dispersion in range 10-10 000 Mc/s, 1288 Li-Zn, magnetic properties of, 1957 for magnetostriction oscillators in filter circuits, 1954

1954 measurements by resonance-cavity methods on, formulae for, 545 Mg, effect of Mn and firing conditions on, 903 effect of oxygen pressure on, 1287 solubility of MgO in, 2688 Mg-Mn, magnetic viscosity in hysteresis loop tracings, 2325 microstructure and properties of, 4133 microwave Faraday effect and birefringence in, 1632 Mg, domain-wall motion and recommending 1000

Mn, domain-wall motion and resonance in, 1958 magnetic properties and disaccommodation of, 2327 $Na_3O\cdot SnO-Fe_3O_3$, 904 neutron irradiation effects on Curie temperature of,

898 Ni, effect of divalent-ion substitutions on magneto mechanical properties of, 1292 grain growth in, 544 Ni-Co, magnetic resonance studies during reaction, 3042

NHCO, Marketter resonance studies during reaction, 3042
and Ni ferrite-aluminates, resonance measurements on, 2689
Ni-Fe, magnetic anisotropy in, low temperature transition of, 902
NiMnO₃, resonance in, 543
NiMnO₃, and CoMnO₃, crystal structure of, 199
Ni-Zn, effect of Co on magnetic dispersion, 3808
hysteresis reduction by transverse field, 3244
paramagnetic susceptibility of, temperature dependence of, 3041
permeability variation with time in, 4136
oriented, with cubic anisotropy, 3399
permeability and loss data for cores, 897
polycrystalline, resonance in, spin-wave analysis of, 777
powergain relations for 3- and 4-frequency

777 power-gain relations for 3- and 4-frequency excitation, 3045 preparation of, by continuous electrolytic co-precipitation, 1959 properties and applications of, 4134 rare-earth garnets, resonance in, 2690 rare-earth orthoferrites, weak ferromagnetism in, 905

I.39

Electronic applications, 'tellurometer', for measure-

- 1945 wave-nechanics correction of Richardson-Dushnan equation, 2912 Electron gas, dielectric formulation of many-body problem for, 1830 high-deusity, magnetic susceptibility of, 759 Electron guns, for kinescope, annular, 652 high-transconductance, 322 electrode requirements for prescribed field dis-tribution, 323 magnetically shielded and investor

- magnetically shielded, election-beam dynamics of, 1031
 magnetically shielded and immersed, perturbations in beams from, (D)2429
 Pierce-type, design theory for, (D)653
 'ramp'-type, space-charge-limited crossed-field, theory of, 3894
 for solid and hollow cone-type beams, 2430
 toroidal, for dense hollow beams, 3527
 Electron lenses, asymmetric, stigmatic image in, 3075
 unipotential design of, 937
 e.s., correction of aperture error by space charge, 4171
 ion-focusing properties of quadrupole pair, 2721
 - ion-focusing properties of quadrupole pair, 2721 magnetic, induction along axis of, measurement of, 2704
- weakly convergent, spherical aberration in, 3838

- 2704
 weakly convergent, spherical aberration in, 3838
 Electron microscopes, cathodes for, oxide-cored, 3078
 point-type, 3077
 remote-focus, 936
 emission-type, using secondary electrons, 1330
 using ultraviolet radiation, 1987
 e.s. charging of photosensitive material in, 1988
 chromatic variation of magnification in, compensation of, 3076
 field of series of cylindrical magnetic lenses, 3445
 with highly biased electron gun, 3443
 image contrast analysis, 3444
 space-charge aberration and resolving power of, 3074
 Electron microscopy, image in, e.s. method for obtaining, 1331
 obtained by negative-ion bombardment, 567
 review of developments since 1957, 3832
 shadow casting, use of carbon films in, 938
 Electron optics, diffractograph for continuous recording, 3442
 energy spectrum of electron beam reflected by unetallic object, 399
 e.s. inmersion objectives, computation methods, 3073
 shadow technique, field superposition for increasing sensitivity, 3441
 Electronic applications, automatic character recognition systems, 1991

- shadow technique, field superposition for increasing sensitivity, 3441
 Electronic applications, automatic character recognition systems, 1991
 automatic pattern recognition, by analogue apparatus, 2371
 using flying-spot scanner, 2372
 catapult end-speed recorder, 924
 electron-bombardment processing of materials, 4168
 e.s. teletypewriter for data processing, 3086
 hygrometer, microwave-refractometer, recording-type, 3070
 in inertial guidance system for space flight, 3839
 manometer, microwave, for pressures >0.1 mm Hg, 565
 in medicine, control of ventricular contraction in experimental heart block, 929
 ingestible radio capsule, 1326, 1327, 3834
 microwave routiator for heat therapy, 2361
 pulse generator for electrocardiograph, 4169
 sensitivity of v.l.f. amplifiers for electromyography, 230
 variable-pulse stimulator, 229
 microwave model of human eye, 1325
 mµs light source using Si p-n junction containing P, 3435
 observation of confined detonation processes using microwave interferometer

 - P, 3435 observation of confined detonation processes using microwave interferometer, 3068 photoelectric apparatus with mechanical scanning for photometry, 4167 plasma engine, 3833
 - radar meter for vehicle speed measurement, 1898, 1981
 - radar technique, for detection of shock waves, 3447 for shock-wave velocity determination, 1658 in railway industry, 2717 seismic transducer for visual recording, 3069

Ferrites, resonance in, magnetostatic modes of, 3813 properties and microwave applications of, 4140 theory of, 906 resonance line widths, and g-factors in, 3402 measurements in cross-guide coupler, 3810 resonance in spheres, magnetostatic modes in, 908 reversal of temperature coefficient by d.c. field, 2686

- reversal of temperature coefficient by do. field, 2686
 reversal of temperature coefficient by do. field, 2686
 single-crystal, domain configurations on, 1283
 square-loop, rings, test equipment for, 4155
 storage properties of, test methods for, 3397
 switching-time investigation using asymmetrical pulses, 3404
 storage-type, magnetic reversal in, 4137
 susceptibility of ellipsoid in uniform field, 3809
 switching in, rotational, mechanisms of, 1634
 thermal expansion coefficient of, 4128
 Til'e_0.7Fe_0.2, system, properties of, 542
 transparent, domain observations in, 1956
 Y-Fe garnet, effective exchange constant in, 3401
 magnetica anisotropy constant of, 901
 magnetic of rare-earth impurities on, 3811
 resonance in, 4138
 resonance line widths, 2330
 at liquid-He temperatures, 907
 maximum at low temperature, 3812
 with substituted Cr, absorption curve, variation in width of, 2329
 g-factor of, 2328
 Y and Gd garnet, resonance absorption with increasing power level, 4139

- increasing power level, **4139** Ferroelectric materials, (See also Piezoelectric materials) anomalous polarization in, **1911** (Ba,Sr)TiO₃, thin films, vapour-deposited in electric field, **4083** Ba(Ti,Sn)O₃ and Ba(Ti,Zr)O₃, polarization varia-tion with temperature, **3745** BaTiO₃, ceramics, anomalous residual polarization in, **3327** polarized properties of, **479** primary pyroelectric effect on, **156** crystals, triangular, growth of, **1599** domian structure observed by electron micro-scope, **156**

 - crystals, triangular, growth of, 1599 domian structure observed by electron micro-scope, 158 domains in, antiparallel, during polarization reversal, 2634 effect of space-charge fields on, 2274 electron paramagnetic resonance in, 476, 477 hysteresis loops and pyroelectric effect in, 3332 irradiation effects on coercive field of, 1913 motion of 180° domain walls in, 155 polarizability increase during switching, 3744 polarization changes during aging of, 844 polarization changes during aging of, 844 polarization changes during aging of, 844 polarization tof, 160 switching current in, domain model for, 2635 switching urent in, domain model for, 2635 switching urent in, pulse-width dependence of, 2275 transition to ferroelectric state in, 843

 - 2275 transition to ferroelectric state in, 843 CaSr(Ti,Zr)O₃ and Na(Nb,Ta)O₃ solid solutions, nonferroelectric phase transitions in, 1912 Cd₃Nb₃O₃, preparation of, by anodic spark reaction, 2276
- nonferroelectric phase transitions in, 1912
 Cd_xNb_yO_y, preparation of, by anodic spark reaction, 2276
 ceramics, charge release for different temperature and stress conditions, 2630
 energy loss processes in, 1217
 ceramics and crystals, review of, 153
 colemanite, properties of, 3741
 domain structures of, powder-pattern techniques for delineating, 4085
 domain wall theory for, 3740
 hysteresis loops of, growth of, 3329
 KD_yPO_y, magnetic resonance spectrum and relaxation in, 3743
 KH,PO_y, properties of, 3331
 KNbO_y-KTaO_y system, transitions in, 3330
 LHs₁(SeC₃), crystallography, dielectric and thermal measurements on, 4084
 Li(N_xH₃) SO_y, 841
 PbNi and PbMg niobates, temperature dependence of permittivity and loss angle, 2631
 PbN₅CND₀, and Pb₅CTAO_y, temperature dependence of permittivity and loss angle, 2632
 properties and selection of, 154
 Rochelle salt, Curie temperature and domain structure of, 1218
 hysteresis and after-effects in, 3008
 local-field theory of clamped crystal, 484
 SrTiO_y, electron paramagnetic resonance of Mn ions in, 2633
 stability of, 483
 thermal fluctuations of electric polarization in, 842
 triglycine sulphate, polarization reversal by sideways expansion of domains, 3742
 radiation damage in, 2273
 second-order transition in, 157

- second-order transition in, 157
 Ferromagnetic materials, (See also Ferrites; Magnetic properties)
 α-Fe₂O₃, magnetostatic energy and magnetic anisotropy of, 893
 alloys, Co- and Fe-rich, magnetization of, 3392
 Co-Gd, magnetic moments of, 2321
 Co-Ni, domain-structure changes after quenching, 192
 - Co-NI, domain-structure changes are equencing, 192 CrTe, Hall effect in, 2681 crystal anisotropy and magnetostriction of, 3393 dilute, experimental investigation of, 1631 Fe-Al, Hall effect at Curie point in, 2680 Fe-Co, Hall effects in, 1953

- Ferromagnetic materials, alloys, Fe-Si, temperature dependence of magnetic properties, 193
 Fe-Si-Al, sendust flake, for l.f. applications, 894
 Heusler-type, Ag and Au, 1950
 Mn-Al, metallographical investigation of, 2679
 Mn-Bi, films, magnetic writing on, 539
 Ni-Cu and Ni-Cr, temperature dependence of resistance of, 3805
 Ni-Fe, films, magnetization reversal by rotation and wall motion in, 1955
 orientational superlattices arising from mechanical deformation, 1276
 Ni₃Mn, change of sign of Hall constant in, 2675
 permalloy, direct observation of spin-wave resonances in thin film, 191
 perminvar, influence of magnetic annealing on, 3396
 magnetic annealing in, 3797, 3798

Films, thin, Au, effect of Se film on conductivity of, 488 Au and Cu, resistance variation and noise in, 3350

Au and Cu, resistance variation and noise in, 3350
magnetoresistance measurement circuit, 555
microwave refractivity of, 1154
oxide, on Al, impedance, rectification and electroluminescence of, 4141
Sb, resistivity and magnetoresistance measurements on, 2693
Filters, (See also Networks; Waveguides)
active, band-pass, 16-175-c/s, multirange, 3977
using transistors and twin-T networks, 2156
all-pass, for delay equalization in television transmission, 737
attenuation characteristics, formulae for, 731
band, normalized admittance curves and mismatch circles for, 734
null-point, 736
2-stage, with feedback amplification for bandwidth control, 735
branched, 2151
constant-k, stagger-tuned, for servo systems, 368
crystal, lattice-type, symmetrical transfer characteristics (1121)
wide-band, design of, 1120
development of technique in France since 1947, 2153
elliptic-function, design curves for, 367
i.f., Dermissible circuit immedances for fm 732

2153 elliptic-function, design curves for, 367 i.f., permissible circuit impedances for f.m., 732 triple-tuned, operational and design data for, 1803

image-parameter, Tchebycheff approximations for, 2498

Indee parameter, Tchevychen approximations for, 2498
 ladder, band-pass, half-sections formulae for, 3223
 coupling coefficients for maximally flat amplitude response, 1478
 interchange of infinite-attenuation elements in, 2150
 LC, design curves for, 366
 low-pass/band-pass transformation of, 2152
 mismatch conditions for improving characteristics of, 1116
 optimum, design tables for, 49
 Zobel-type, simplified design method for, 3224
 linear, transfer-function relation for, 3607
 low-pass, RC, with optimum response, design data, 51

Zobel-type, simplified design method for, 3224
 linear, transfer-function relation for, 3607
 low-pass, RC, with optimum response, design data, 51
 response to finite-duration signals, 2390
 voltage-controlled, continuously variable, 1119
 magnetostrictive, narrow-band, 52
 mechanical, for communication equipment, 2155
 ffexural vibrations in, 2154
 theory and technique of, 3225
 microwave, cavity-type, aperture-coupled, 1112
 for minimum insertion loss, 1117
 pulse-width, for television receivers, 1802
 rejector, bifilar-1, analysis of, 1122
 Tchebycheff-type, symmetrical, estimation of dissipative effects in, 50
 synthesis of, 3608
 time-symmetric, for gliding-tone analysis, 365
 wave, design of, network transformations for, 3222
 Zobel-type, for Tchebycheff insertion loss, 1118
 Frequency, control, automatic, using junction diode, for f.m. receivers, 951
 converters, ferrite 'serrodyne' for X band, 3942
 u.h.f., using nonlinear-capacitance diode, 3145
 dividers, harmonic-type, investigations on, 1132
 for pulse synchronization, 3232
 regenerative-modulator-type, process related to Mathieu functions, 2509
 using transistors, 378, 1133
 wide-band, 2508
 measurement equipment for transmissions from aircraft in flight, 3423
 of response of electromechanical devices, 2079
 meter, microwave, H_{a1},-mode, 4161
 multiplication, using counter circuits, 3614
 stabilization, using double mixing circuit, 738
 standards, Canadian, 2700
 using Cs beam, 2701
 Cs, 'atomichron', 550, comparison of, 212, drift in, 4148
 comparison with NH₃-beam maser, 915
 correction for earth's ellipticity, 4147</l

Galvanormagnetic effects. See Magnetic effects.
 Galvanormeters. See Meters, galvanometer.
 Gases, ionized, (See also Plasma)

 auroral afterglow of nitrogen, 1510
 dependence of electron inobility on magnetic field, 3643
 electron and ion temperature difference in magnetic field, 2536
 introversible processes in, 4020
 in strong fields, as hydromagnetic capacitor, 1843
 thermal diffusion in, 89
 transport phenomena in, considering electron-electron scattering, 402
 oxygen, attachment of slow electrons in, 2533
 Generators, (See also Oscillators; Signal generators)

oxygen, attachment of slow electrons in, 2533 Generators, (See also Oscillators; Signal generators) frequency-sweep, using voltage-variable p-n-junction capacitor, 3986 wide-band, with 100 kc/s-300 Mc/s sweeps, 558 harmonic, efficiency with ideal rectifiers, 60 microwave, using capacitive-mode crystal diode, 3991

Electronic & Radio Engineer

- magnetic annealing in, 3797, 3798
- magnetic annealing in, 3797, 3798
 measurement of domain-boundary propagation velocity by Kerr effect, 194
 Co, fiims, resistivity of, 162
 resistivity and thermoelectric power of, 487
 leakage-field determination using divergent electron beam, 202
 nuclear resonance in, 4126
 polycrystalline, magnetic resonance of, 3802
 creep of asymmetric hysteresis cycles in, 204
 cube-oriented sheet, 896
 Curie-point phenomena in, 3391
 cyclic remagnetization of, noise measurements on, 3796
 domain boundary configuration during magnetiza-

- cyclic remagnetization of, noise measurements on, 3796
 domain boundary configuration during magnetiza-tion reversals in, 2319
 domains in, observation by magneto-optical Kerr rotation, 1281
 thermal activation of, 1275
 width of boundary layer between, 2676
 elastic-wave damping in, high-frequency, 1278
 electron diffraction method of analysis of, 3801
 electron diffraction method of analysis of, 3801
 electron diffraction investigation of deforma-tion in, 4124
 domain structure, influence of demagnetizing field on, 2677
 eddy-current losses in, 4130
 films, evaporated, chemisorption of O₂ in, 1295
 magnetic anisotropy in, 2683
 influence of carbon inclusions on mobility of Bloch walls, 3794
 Fe and Ni films, magnetization vectors determined from magnetoresistance effect, 3040
 Fe and SiFe, magnetothermal effects in, 4129

- Fe and SiFe, magnetothermal effects in, **4129** films, energy relations for magnetization analysis, **3394**
- films, energy relations for magnetization analysis, 3394
 monitoring hysteresis loop during and after deposition, 2662
 Hall effect in, measurements on, effect of crystal anisotropy and magnetostriction in, 3803 theory of, 1277
 hysteresis in, calculation of, 197
 hysteresis cycles in, creep of, 547
 intratomic distances in, 891
 irradiation effects on, 2646
 magnetize, spin-fluctuation scattering of neutrons in, 4127
 magnetization of, change with hydrostatic pres-sure, 892
 model for interpreting domain effects on electron beam, 3407
 mu-metal, 'after-effect' in, 2320
 Ni, domain distribution in, influence of tempera-ture on, 3795
 Hall effect at low temperatures in 2322

- mu-metal, 'after-effect' in, 2320
 Ni, domain distribution in, influence of temperature on, 3795
 Hall effect at low temperatures in, 2322
 resonance in, 2684
 ultrasonic velocity and attenuation changes with magnetization direction, 4125
 ultrasonic wave propagation in, 1951
 Ni, films, cathode-sputtered, thermai transformation of, 895
 electrolytically produced, properties of, 3804
 Hall effect in, 1279, 1280
 magnetic properties of, 3039
 magnetic properties of, 3039
 magnetics in paramagnetic alloy, variation of spontaneous magnetization with temperature, 2678
 powder-core, temperature coefficient of initial permesbility of, 1282
 reading effects in paramagnetic on phenomena in, thermodynamic theory of, 538
 soft, flux reversal mechanism in, 3405
 spin-orbit coupling and extraordinary Hall effect in, 1952
 structure of, instability of Bloch walls due to interstitial atoms, 535
 superconductivity conditions for, 195

Ferromagnetism, coupling of elementary domains effect of coupling between grains on hysteresis, 203

203 excluded-volume problem and Ising model of, 3263 fluctuating-field theory and low-temperature ordering, 536 granular structures in, analysis of, 2318 Heisenberg model for, equivalence of Bose-Einstein lattice gases to, 2913 Field strength, (See also Reception; Wave propaga-tion, e.m.) measurements, recording and evaluation of, 3419

Flims, thin, absorption of e.m. wave by, optimum thickness for, 3268 absorption/field-strength curves for, determina-tion of width of, 3814

- Generators, harmonic, using nonlinear reactances, 61 pulse, mµs, calibrated, using coaxial line, 2706 using half-cycle delay principle, 2501 using vibrating-read Hg switch, 2500 using nonlinear amplifiers to shorten rise time, 1488 for radar range calibration, 2352 using transistors, 2161

 - using transistors, 2161 variable, using pulse transformer and transistor, 1128
- 1128
 80-μs, 100-kW, for spectroscopy, 376
 pulse and square-wave, commercial, 2710
 random-function, with constant peak-to-peak amplitude, 373
 sine-wave, 1.f., commercial, 552
 Geomagnetic storms, activity following large solar flares, 3284
 correlation with sudden disappearance of solar filaments, 2948
 recurrent, 1917-1944, related to solar prominences, 1865
 in relation to geomagnetic bulsation. 1537

- recurrent, 1917-1944, related to solar prominences, 1865
 in relation to geomagnetic pulsation, 1537
 ring-current theory of, inadequacy of, 1536
 sudden commencements, observations at Taman-rasset, 1183
 propagation of, 3285
 time constants for, 1535
 Geomagnetism, activity, in polar regions, from report of French expeditions, S 1V 2, 111
 related to green coronal-line intensity, 2949
 relation with solar flares, 113
 dynamo theory of, 108
 far-field discrepancies in cosmic-ray and surface data, 435
 field disturbances, correlation with earth currents, 4044

 - 4044 due to nuclear explosions, 3669, 3670, 3671, 3672, 3709
 - s709 related to atmospheric circulation at 300 mb, 2229

 - as relaxation variations, 2944 due to solar plasma, 2560 field fluctuations, irregular, diurnal variations of, 1533

 - field fluctuations, irregular, diurnal variations of, 1533 in 0.1-30-c/s range, 1532 with 6-sec period, causes of, 2945 field geometry at ionospheric heights, 3849 field intensity, scalar, method for analysis, 109 solar-eclipse effect on, 2561, 2562 field measurement, using weak-field maser, 3823 field micropulsations, in Alaska and California, 4045

 - 4045 geographic variations, 2946 field pulsations, auroral origin of, 2947 related to oscillations, 636 field variations, e.m. fields induced by, 3668 lunar tides at Kodaikanal, 1534 lunar-diurnal, at Tamanrasset, 2228 secular, relation to non-dipole fields, 790 hydromagnetic waves above ionosphere, 110 measurement with Rb vapour magnetometer, 112

- Hall effect, (See also under Semiconductors) devices based on, 2692 generators, semiconducting thin films for, 3349 measurement apparatus, a.c., for ferromagnetic and semiconductor materials, 918
 Hearing, binaural fusion in, mechanism of, 1055 definitions of d' and η in signal detection, 3854 detection of signals in noise, 3540 as function of frequency ensemble, 1052, 3539 masking in, definition and index for, 3541 stereophonic effect obtained with single signal, 1056 threshold, and duration of tone pulses, 3909 threshold shift, due to noise, 682, 1053, 1054 relation with masking, 681
 Heating, eddy-current system using gas-filled triodes, 2716
 induction, generator using hydrogen thyratrons, 3439
 r.f., frequency stability of generators for, 933
- r.f., frequency stability of generators for, 933 Hysteresis. See Magnetic properties.

- Image converters, electron-acoustic, using piezo-electric plate scanned by electron beam, 679, 2084
 for military and scientific use, 2783
 pulsed, for observation of luminous discharges, 3522
 for quantity production, and definition of gain characteristic, 1404
 shutter-type, for multiple-frame photography, 2369
 Image intensifiers, cascade, fluctuations in, 3521
 with optical feedback, for picture storage, 1408
 solid-state, application of electroluminescence in, 1597
 Impedance, matched or optimum, assessment of. 37
- 1597
 Impedance, matched or optimum, assessment of, 37 measurements, by differential bridge, between 10 kc/s and 10 Mc/s, 3429
 in waveguide, automatic frequency-sweep c.r.o. method, 220
 100 c/s-50 Mc/s, 3-branch phase-opposition circuit for, 554
 shunt, of resonant cavity, measurement method, 3421

- shuft, of resonant cavity, measurement method, 3421
 surface, measurement technique for v.h.f., using disk-terminated coaxial line, 1306
 quantum theory of, 1221
 Indouctors. See Coils.
 Information theory. See Communication theory.
 Information theory. See Communication theory.
 Infarred, (See also Photocells) physics and technology, 4010
 Insulating materials, (See also Dielectric pro-perties; Ferroelectric materials)
 ceramic, structure and properties of, 4142
 for magnet wires, 1635
 plastics, epoxy resins, properties of, 911
 polyethylene, oxidized, dielectric loss of, 3414.
 polymers, dielectric losses and permittivity at cm \lambda, 3818
- Electronic & Radio Engineer

- Insulating materials, silicone, tabulated data on, 2694
- 2694 tape- and film-type, for electronic equipment, 1296 Interference, (See also Noise; Reception) froin fluorescent lamps, 3463 froin industrial, scientific and medical apparatus and radiating receivers, 954 from radar, in microwave communication services, 1353 in shared changel broadcasting subjective tests
- in shared-channel broadcasting, subjective tests, 3479
- supression equipment for lifts and screened rooms, 4193 from television receivers, reduction of, 955 u.s.w., measurement equipment for, 2386

- u.s.w., measurement equipment for, 2386
 Interferometry, double-beam, coherence requirements for, 398
 International Geophysical Year, coordination of observational program for, 1539
 Indian program, 3299
 Indian work during, texts of papers covering, 3699
 N.B.S. radio and ionospheric observations during, 4046
 organization and data-collection arrangements for, 1538
 - 1538

 - 1538 program of atmospheric research, 1540 R.S.G.B. progress report, 114 for v.h.f. program, 115 S.W.I. and disturbance warnings, improvement of, 116 World Data Centre for rockets and satellites, 1194
- Inverters. See Converters, d.c./a.c. Ionization, in homogeneous field, extension of Townsend's approximation formula, 2200

Jonosphere, F., layer, critical frequency, derived from quality figures of WWV transmissions, 135 variation near auroral zone during magnetic disturbances, 803 world-wide distribution, 129
 drifts in, effect of magnetic activity on, 2586 electron production rate in, 800 equatorial, diurnal development of, 3707 horizontal movements in, vertical-incidence recordings of, 2243 influence of electron-ion diffusion on formation of, 128 ionization, relation of magnetic dip to, 2584 lunar variations of, semidiurnal, 1196 magnetic field calculations at Dakar, 133 model for, 3705 observations at Halley Bay, 1881 polar, critical frequency, diurnal and annual variations of, 1882 structure and movement of large inhomogenetics in, 2581 world-wide electron density distribution, anomalies in, 3706 geomagnetic tides in, origin of L, currents causing, 2247 heating by hydromagnetic waves, 2585 height, changes deduced from v.l.f. phase velocity measurements, 2735 virtual, measurement of, 3715 k/ records, coefficients for N(k) profiles from, 3303 inhomogenetites, irregularities of refraction due to, 2251 ionograms, accurate virtual height from, method of obtaining, 2249
 lower, abnormal ionization associated with cosmicray enhancements, 1562 'Chapman behaviour' in, 3301 nocturnal ionization of, effect of vertical drifts on, 1878 solar-cycle influence on, 130 magnetic-side and instrument effects in, 807 motions in, interpretation of observational data on, 1556 outer, electron density distribution from whistler data, 3307 electron density and neutral particles in, 2967 reflection coefficient at v.l.f. from measurements of atmospheries, 2589 refraction of extraterrestrial waves by, 2973 research in Hungary 1964–1966, 452 review for 1968, 1199 rocket observations of, 1559 self-demodulation and self-distortion of radio waves in, 2252 solar-cellipse effects on, observations at Freiburg, 131 observations at Singapore, Dec. 1955, 1883 solar-flare effects on, observations at Freiburg, 131 observations of,

structure of, dynamic model for, 2966 temperature and electron-density determinations by vertical-incidence scatter measurements, 4061

4061 turbulence in, 2577 winds in, and S_q variations, 453 Ions, emission, secondary, from metal surfaces, 1508 pressure generation by ion-drag, 3637 sources, high-current, 1986

Lenses, (See also Aerials; Electron lenses) microwave, axial phase anomaly in, 713 'conflection'-type, tests on, 1450 design of, 1100 dielectric sphere as, 714 Luneberg-type, general solution for refractive index of, 24 properties of slotted dielectric interface for, 3584 scanning, design for minimum phase error, 1101 spherically symmetric, design method for, 3583 stepped-index, 2854
 Lightning. See Atmospherics.
 Limiters. See Circuits, limiter.
 Loudspeakers, (See also Acoustics; Sound; Trans-ducers) acoustic testing of, 1761
 with bass-reflex cabinet, acoustic interactions in, 2456
 analogue network for performance calculations,

analogue network for performance calculations, 1763

column-type, for public-address systems, 2824 design methods for improved performance, 1762 diaphragms, rigidity of 'sandwich' construction, 334

e.s., development and constant-charge operation of,

8
 generating high-intensity noise for component testing, 692
 impedance and phase measurements on, 2823
 ionic, design and performance of, 1759
 with modulated air flow, for high-intensity sound, 3922

3922 monitoring, performance criteria and design of, 333 permanent magnets for, 1760 response of, théoretical study near principal resonance, 1433 Luminescence, (See also Electroluminescence; Phosphors) control by charge extraction, 473

I.41

- Townsend's approximation formula, 2200 Ionosphere, (See also Atmosphere; Earth satellites; Wave propagation, e.m.) abnormal effects on cosmic noise at 10 m A, 808 absorption in, interpretation of variations in, 3716 'riometer' cosmic-noise equipment for measure-ment of, 1566 at 5 Mc/s over Delhi, 810 in arctic, measurements from drifting observatory, 3717
- in auroral zone, rocket measurements 100-210 km, 1560
- 1560
 D region, absorption in, explanation of daytime constancy of, 809 rocket measurements of, 2972 arctic, electron-collision frequencies in, 1886 fmin and sudden disturbances of, 2588 low-frequency sounding and reaction-rate investigation of, 1553
 disturbances in, effects on communication circuits, 573 sudden, effect on 2.28-Mc/s pulse reflections, 2971 travelling, night-time, 2580

- sudden, effect on 2-28-Mc/s pulse reflections, 2971
 travelling, night-time, 2580
 driftin, evaluation by method of 'similar fades', 801
 measurements at 1.f., 1198
 E region, effect of ion production and recombination on wave scattering in, 4059
 geomagnetic distortion of, 2246
 lower, horizontal drifts and temperature in, 804
 measurements during solar eclipse, 3306
 size of irregularities in, 4054
 structure and variations of, 1554
 turbulence due to e.m. forces and wave scattering in, 4060
 E and F regions, drift observations at Ibadan, 1557
 E, layer, long-term variations in Japan, 127
 lunar influence at Huancayo, 3305
 lunar influence at Giosconde data, 1561
 spiral, occurrence of, 3304
 spread-F and radio-star scintillation, causes of, 2970
 survey of data. 1879

- 2970
 survey of data, 1879
 v.h.f. observations in U.S., 2587
 v.h.f. observations in U.S., 2587
 tand F₂ layers, comparison of data on, 2578
 E₂₁ layer, lunar tides observed at Brisbane, 132
 effects of nuclear explosions on, 3709, 3712, 4056
 radio observations of, 2969
 in recordings of atmospherics and solar r.f. bursts, 3711
 in vertical-incidence absorption measurements, 3710
 effects on radio reflections from moon and solar

- in vertical-incidence absorption measurements, 3710
 effects on radio reflections from moon and solar corona, revised formula for, 2583
 effects related to cosmic noise level variations around 80 Mc/s, 2582
 effects of strong gyro-waves in, 3308
 electron density of, computations of, 126
 daytime decay variations with height, 3708
 investigations by rocket in U.S.S.R., 2965
 measurements using rocket-to-ground c.w. transmission, 3714
 profiles, during I.G.Y., 791
 preparation from ionograms for I.G.Y., 438
 electron distribution in, derivation of N(h) profiles for, 1552
 over Slough, 806
 electron energy levels recorded at 470-1880 km.

- for, 1552
 over Slough, 806
 electron energy levels recorded at 470-1880 km, 3294
 electron-ion recombination measurements on nitrogen, 125
 equatorial, electric-current measurements by rocket magnetometer in, 2968
 e.s. field measurements by rocket or satellite, 3713
 F region, bifurcations in, at Baguio, 1952-1957, 802 drifts in, horizontal, at Waltair, 2242
 electron and ion density distributions in, 2579
 height gradient of electron loss in, 805 *Kf* records at Macquarie Island, 2241
 inhomogeneous structure of, 2244
 magnetic-storm effects on, 1563
 physical conditions and effects of, 1555
 solar-activity effects on, 2245
 spread-echo observations at Brisbane, 454
 triple-splitting measurements at low latitudes, 1885

Luminescence, and exo-electron emission of inor-ganic crystals, 3002

- ganic crystals, 3002 Magnetic effects, (See also Hall effect) Faraday rotation, design of bimodal cavity for experiments on, 770 galvanomagnetic properties of Fermi surfaces, 3271 magnetoresistance of metals in high fields, 3337 magnetoresistance, 784 of ferrite ellipsoid, 403 flux function and induction calculations, 4023 improvement in detecting power of search coils for measuring, 2351 interplanetary, and cosmic-ray variations, 783 measurement, electrodynamic gradiometer using microvibration technique, 218 by nuclear-resonance technique, 1644, 3824 using semiconductor, 1972 probe, Bi, miniature, based on Hall effect, 1973 uniform, effect of permeable alloy cylinder in, 90 Magnetic properties, hysteresis, creep character-istics, influence of temperature on, 1294 from succeptibility measurements, 4024 of (Ni,Li)O, 3799 perneability of iron wire under action of circular alternating field and d.c. longitudinal field, 3645 of perovskite-type mixed crystals LaSrCoO₉, 890 reinanence, measurement in thin films, 1314

- 3043
 of perovskite-type mixed crystals LaSrCoO₃, 890
 renanence, measurement in thin films, 1314
 susceptibility, of Cu-Ni and Ag-Pd alloys at low temperatures, 190
 measurement, by analogue of Wheatstone bridge, 1313
 and desire terms is 2000

- 1313

 on Pd mixed crystals, 3790
 of transition-metal silicides, 1274

 Magnetization, of Au₄Mn, influence of pressure on, 1273
 theory of, system of magnetic moments in, 3644
 Magnetobydrodynamics, spherical vortices in, 92
 Magnetometers, influence of self-inductance of core winding in, 3058
 Magnetoresistance. See Magnetic effects.
 Magnets, permanent, stability of, factors influencing, 1960
 powder, properties of, 1961

- 1960
 powder, properties of, 1961
 Mathematics, characteristic functions of ∠u + k²u
 = 0, asymptotic nature of, 2696
 elliptic integrals, numerical evaluation method, 549
 flow-diagram analyses, 1964
 forced-oscillator equation, simple-subharmonic solutions for, 4146
 Fourier analysis, template method for evaluation, 1298
 repueralized Rayleigh processes 210

- Fourier analysis, template method for evaluation, 1298 generalized Rayleigh processes, 210 generatized Rayleigh processes, 210 generatic-analytical theory of transition, 3049 integral equations, approximate solutions of, 209 Lagrange equation, meterical networks, 360 Laplace expansion, modification for Cauchy conditions, 3050 Laplace expansion, modification for network analysis, 548 Laplace transformation, for summation of weakly convergent series, 2695 Mathieu and related functions, regenerative modulation process as analogue for, 2509 parametric solutions of nonlinear differential equations, 1963 statistics, analysis of errors in determination of mean value, 1638 switching algebra, solution of equations in, 1297 ternary, 1636 switching functions, classification and minimiza-tion of, 3048 toroidal functions, theory and numerical tables,

- toroidal functions, theory and numerical tables, 4145
- tion of, 3048
 toroidal functions, theory and numerical tables, 4145
 vectors, probability distribution of phase with Rayleigh-distributed component, 3416
 Weber's equation, approximation method of solving, 913
 Liouville method applied to, 912
 Z transforms, derivation and applications, 1637
 Measurements, (See also individual subjects)
 calibration centre at Boulder, Colorado, 1302
 of characteristics of u.h.f. quadripoles, 1968
 of cross-spectral density of random functions, 2349
 microwave, interferometer and grating-spectrometer techniques for, 563
 of polarization, with instantaneous display, 3432
 of phase and amplitude, 0.01 (s)-10 kc/s, for testing control systems, 1651
 of phase and amplitude, 0.01 (s)-10 kc/s, for testing control systems, 1651
 of phase and amplitude, 0.12 (s)-10 kc/s, for testing control systems, 1651
 of phase and sime delay, video transmission test set, 4159
 response-time delays in equipment, correction formulae for, 551
 r.f. reciprocity in, 917
 of r.f. radiation, survey of techniques, 2714
 slotted-line, logarithnic chart for evaluation of, 2702
 of valve temperatures, using phototransistor pyrometer, 3424
 Metals, (See also Alloys; Conduction; Ferromagnetic materials)
 Al, surface finishes for, 1962
 alkali and noble, band structures of, 910
 Bi, infrared transmission of, de Haas-van Alphentype oscillations in, 2620
 diamagnetism of conduction electrons in, 2194
 electron structure of, 418
 high-purity, 486
 isotropic, galvanomagnetic, thermomagnetic and thermoelectric effects in, 161
 surface impedance of, h.f., quantum theory of, 1221
 ultrasonic absorption in, collision-drag effect for, 2444

Navigation aids, d.m.e. system, using common-fre-quency transceivers, 146 infrared, search-system range performance, 4070 simulation techniques for system evaluation, 4071

4071
marine, electronic clock coder for radio beacons, 4069
v.l.f., radux-omega system, phase stability measurements for, 2736
Networks, (See also Circuits; Filters) active, RC, synthesis of, 3978 combining, 3-band, 733
linear, transfer properties based on growth of spectral energy, 3220
matching, 'immittance' chart design method for transistor measurements, 1115
multipole, analysis of multitapped potentiometers

matching, 'immittance' chart design method for transitor measurements, 1115
multipole, analysis of multitapped potentiometers with loaded output, 2159
RLC, topological analysis for, 2157
'traditor', nouenergic nonlinear elements in, 2872
2-phase, design of, 2158
quadripole, analysis based on determinant technicue, 48
CR divider, response of, 47
general theorem for synthesis of, 2495
group delay and group velocity related to transfer function, 1798
using gyrators, as nonreciprocal systems, 2145
for impedance conversion, 1480
LC, synthesis of, 2147
linear, asymmetric, iterative analysis for, 2869
passivity condition for, 1800
transient analysis with f.m. input, 2148
lossy, geometric representation of, 1477
microwave, matrix analysis for, 2149
voltage-mode displacement for definition of, 1114
Minkowski model of Lorentz space in analysis of,

Minkowski model of Lorentz space in analysis of, 1799 non-Euclidean geometry in, 3606 symmetrical, analysis by voltage-node displace-ment method, 1801

synthesis of, using symmetrical lattice structure,

synthesis of, using symmetrical lattice structure, 2146
transfer-function approximation by polynomial, 3976
transformation theorem for, 2496
twin-T, response time of, 730
u.h.f., 3-point measuring method for, 1968
RC, asymmetrical, synthesis of, 1113
transients in, analysis using Laplace transformation, 728
2-terminal, negative-resistance, 1476
reactance theorem for, 1797
3-terminal, nonreciprocal element for topological analysis, 2871
Noise, (See also Atmospherics; Solar radiation; Sound)
in communication and servo systems, 1682
contact, theory of, 2422
current, in film-type resistors and semiconductor diodes, 3506
extension of Nyquist's theory to field-excited 'hot' electrons, 2902
Gaussian, limited, spectrum of, 1681
sinultaneous variation of amplitude and phase, 583
measurements on noisc-thermometer amplifier, 2055

measurements on noisc-thermometer amplifier, 3055

3055
 standom, measurement of, in presence of television signal, 2345
 sources, diode for u.h.f., 3533
 discharge-tube, for 1 700-2 300-Mc/s band, 559
 standard, filament-type for 3 kMc/s, 2344
 statistical analysis using digital technique, 3826

Observatories, Melbourne-Toolangi, 1531 Royal Greenwich, 2550
 Oscillations, microwave, 30-3 000-kMc/s, methods of generating, 1845 strongly nonlinear, analysis for, 80
 Oscillators, Barkhausen-Kurz, cm-A, 1486 blocking, with transformer-core saturation for control of pulse duration, 3989 using transistors, analysis and design of, 2504 waveform control methods, 56
 constant-frequency, controlled by thermistor bridge, 1482
 cryogenic, based on relaxation process in Pb film, 2875

2875
crystal-controlled, for equally spaced frequencies in given band, 741
Hartley-type, theory of, 1804
'marginal', using transistors, for nuclear mag-netic resonance observations, 1805
with servo control, 371
testing of, 372
thermally compensated, using thermistor, 370
3-terminal, design of, 1483
1-Mc/s, using transistors, 1484
with cubic nonlinearity, ultraharmonic and sub-harmonic resonance in, 3611
f.m., using transistors, 1489
harmonic, damped, wave-mechanics treatment of, 739
thermodynamics of, 81

namonic, damped, wave-internatics treatment of, 739 thermodynamics of, 81 microwave, based on ferrimagnetically coupled electrons in transient fields, 4026 mm· λ , using ferrites, 3983 review of techniques, 3982 multivibrator, analysis of, phase-space method for, 1806 low-impedance, using transistors, 2503 magnetically coupled, frequency control of, 3612 with negative feedback, 1807 negatively biased, 55 using series diode for increased sensitivity, 2502 using single triode with no filament current, 3988 nonlinear, analysis of, 2499 parametric, subharmonic, for digital computing, 3590

Electronic & Radio Engineer

4071

2146

- Metals, ultrasonic attenuation by electrons in, 3336
 Meteors, magnetic effects from, absence of, 106
 radio-echo height distribution, theory of, 2940
 radio search method for weak showers, 2227
 reflection of radio waves from, Booker's theory for, 1527
 trails, drift of reflection point along, 2226
 echoing points, height and electron density from c.w. measurements at 27 Mc/s, 2941
 electron density in, approximations for, 2224
 over-dense, oblique echoes from, 2225
 reflection of radio waves from, research applications of, 1526
 velocity of, c.w. technique for measurement, improvement to, 105
 Meters, galvanometer, feedback systems for, 2707
 mirror-type, improved performance using photoelectric, for 1–100 c/s, 1319
 voltmeter, digital, 2335
 high-voltage, using electron beam, 560
 wattmeter, double-vane torque-operated for 7 kMc/s, 223
 thermoelectric, for 50 c/s-30 kc/s, 1320
 torque-operated, for 3 cm A, 2359
 Microphones, (See also Transducers)
 carbon, powder for, deterioration of, 3189
 preparation of, 1758
 cardioid, theory of, 2092
 concentration coefficient and directivity factor in surrounding noise, 691
 condenser-type, for airborne ultrasonic applications, 2448
 differential-type, characteristics of, 1757
 dynamic, acoustic-front damping in, 2455

- tions, 2448 differential-type, characteristics of, 1757 dynamic, acoustic-front damping in, 2455 effect of mechanical vibrations on, 690 c.s., uniangular, 1432 gradient-type, for intercommunication systems, 2094
- 2094 magnetic, ministure, construction of, 1431 probe-type, design for, 1429 standard, calibration of, absolute methods for, 1430, 2093 Missiles, guided, miss-distance indicator based on space-coupled oscillatory system, 2601 Mixers, microwave, design for minimum noise figure, 2874

- Mixers, microwave, design for minimum noise figure, 2874
 Modulation, amplitude, microwave, by ferroxcube, 1151
 amplitude and frequency, transient response of networks and transmission lines for, 2186
 asymmetrical, distortion calculations, 3465
 frequency, negative-feedback method for broadcasting transmitter, 3872
 phase, mathematical treatment of power in, 3851
 phase-shift circuits for s.s.b. and quadrature, 4196
 pulse, accuracy obtainable with transistors, 1827
 markerless systems for communications, 956
 pulse-code, with amplitude keying, channel capacity, 3103
 signal/noise ratio in, 2009
 pulse-sideband, multiphase, suppression of unwated sideband in, 589
 phase compensation method for, 588
 system for, 587
 Modulators, ferite, microwave, 1825
 frequency, diode reactance-type, 2187
 using ferroelectric capacitor, 3247
 for imarginal' oscillator, 1826
 portable unit for television link, 2034
 pulse-code, magnetic-amplifier circuit for, 2188
 shunt-type, as phase detector, error in, 2899
 Molecular systems, effective radius of lectron in, 1858
 electron-phonon interactions in, and impurities in
- - 1858 elastic model of lattice defects, 1173 electron-phonon interactions in, and impurities in metals, 1859 theory of, 2215 energy-loss spectrum of electron interaction in solids, 2931

 - energy potentials in crystals, Fourier coefficients of, 782
- energy states of one-dimensional crystal, 1174 imperfections in solids, relations between, 1175 negative-mass charge carriers in, energy absorption
- by, 3747 nuclear polarization by means of 'hot' electrons, 4011

- 4011 plasma resonance in solids, theory of, 781 spin-wave theory for, validity of equations in, 2214. Zeeman splitting of paramagnetic ions in, 2549 Moon, radio echoes at 412.85 Mc/s, rapid fading rate of, 1525 radio observations of surface of, 1863
- Navigation aids, (See also Direction finders; Radar)
- airborne, Doppler systems, characteristics of, 2979 review of performance of military equipment, 2608
- self-contained, with automatic computer system, 2599
- 2599 for aircraft, automatic blind-landing system, B.L.E.U., 464, 1892, 3723 collision detection without range data, 3722 for distress beacon, operating on 243 Mc/s, 1891 Doppler omnirange system, 2610 VOR, design considerations, 1897 'Vorac', rotating aerial array for, 2120 flight testing of, 460 radio equipment for B.O.A.C.'s Comet, 1890 TACAN, general description of, 461 beacons, metallic reflectors for, 1582 Decca, Doppler sensor, description of, 820 Mk. 10 receiver, air trials of, 462 Dectra, interim report on field trials of, 463 d.m.e. system, Australian, 206-Mc/s receiver for, 145

- Oscillators, parametric, semiconductor-diode, 3981 RC, frequency-sweep, voltage-controlled, 1125 incremental frequency control of, 1126 wide-range, 54 4 c/s-850 kc/s, using bridged-T circuit, 1808 for stable carrier frequencies of 8 800-4 200 Mc/s, 3987 stepped-frequency, for propagation tests, 1485 sub-mm A, using avalanche effect in semiconductor, 3875

 - 3875 (standard)
 3876 (standard)
 3875 (standard)
 3876 (standa

 - using Zen 2160 Zener-diode limiter and harmonic filter,
 - Wien bridge, modified, for improved characteristics, 1124
 - 1124
 2-valve, with feedback via *m*-network, 3985
 500-Mc/s, using open rectangular waveguide, 3984
- Particle accelerators, betatron, electron capture and limiting current in, 2718
 cyclic, controlled by h.f. field, 3440
 cyclotron, fixed-frequency, with one dee, 1985
 microtron, maximum energy and intensity in, 3837

- 3837
 with star-shaped field, 2370
 linear, electron, anomalous attenuation in, 1329
 multipactor effect in, 3836
 22-MeV, 2719
 r.f. aspects of design of, 1328
 space-charge effects in, longitudinal, 1984
 tandem Van de Graaff, at Chalk River, 935
 10-MeV, design of, 934
 150-kV generator using rotating ferroelectric disks (ferrostac), 3071
 with 800-kV cascade generator, Budapest model, 1657
 Particles, charged, correlation function for, 1829
- 1657
 Particles, charged, correlation function for, 1829
 cyclic motion in electric field, 3835
 in e.m. field, stable orbits of, 3250
 energy losses in gyrotropic medium, 3635
 e.s. field and trajectories of, 1505
 longitudinal vibrations of electron-ion beams, 1835
 in generation field, trajectory platting methods
 - - in magnetic fields, trajectory plotting methods, 1832

- in magnetic fields, trajectory plotting methods, 1832
 moving through dielectric, radiation from, 3634
 trajectory plotting, graphical-analytic method for, 3630
 Phase, measurement, using coincident slicer, 217
 using heptode mixer, 1970
 and locking of frequency changer, pulse-beat method for, 1643
 for power supply systems, 1971
 splitter, concertina-type, performance analysis, 3616
 Phosphors, AIN, electroluminescence of, 4082
 cathodothermoluminescence of, 2624
 CdI, and PbI, luminescence of, 2624
 CdI, bue edge emission in, mechanism of, 2269
 carrier excitation due to electron bombardment in, 3004
 edge luminescence anisotopy in, 474
 emission spectra and absorption edge of S in, 1216
 energy transfer mechanism in, 827

 - 1216
 energy transfer mechanism in, 827
 excitation by ionizing radiation, 3325
 with/green and red-green luminescence, 2621
 influence of magnetic field on blue fluorescence or luminous absorption of, 2622
 multiplet structure of excitons in, 3324
 pure fluorescent emission lines and luminous absorption lines at 4.2°K, 2618
 CdS and ZnS, polarization of fluorescence in, 2267, 2268

 - 2267, 2268 electrolun inescence characteristics and applica-tions of, 151 luminophore, measurement of short afterglows of, 2350 review of, 1595 SrO, (Ba,Sr)O and MgO, cathodoluminescence of, 150

 - SrS-Pr, with 2623 with fluorescence larger than energy gap,

 - 2623 sulphide, Ag luminescence centres in, energy levels of, 2998 two-stage optical excitation of, 2996 transient response of, 1211 ZnO.CdO.B₁O₃ system, phase relations and fluor-escence, 3735 ZnS, cathodo-electroluminescence phenomena in, 834 othodoluminescence efficiency of 472
 - cathodoluminescence efficiency of, 472
 - electroluminescence in, with a.c.-d.c. excitation, 3000
 - a) 3000
 effects of impurities and temperature on, 152
 based on equilibrium conditions, 832
 particle size and efficiency of, 2266
 under pulse excitation, 833
 significance of particle size in, 3738
 of single crystals with cathode barriers, 835
 electron traps in, 1596
 excitation spectra and temperature dependence of luminescence of, 2999
 films, preparation from electroluminescent powder, 1598
 preparation of single crystals by gas reaction and sublimation methods, 2625
 short-persistence, luminescence of, 3001
 ZnS and ZnCdS, activation by Au and other elements, 3736

 - Electronic & Radio Engineer

- Phosphors, ZnS-Cu, chromatic effects in photolumin-escence of, 1908
 electroluminescence brightness and brightness waveform of, 1214
 ZnS-Cu,In, energy transfer in, 4081
 ZnS-Cu,PB, electroluminescent, time-dependent spectra of, 4080
 ZnS-Sn,Li, excitation and emission spectra of, 1212

Photoconductive materials, ZnO, with ohmic and blocking contacts, photocurrent measurements, 826
powder, field-effect measurements on, 1903
ZnS, anomalous photovoltaic effect in, 2989
ZnTe, conductivity at high field strengths, 3726
Photoconductivity, as function of optical absorption, 1828
quenching of, model for, 2263
Photoelectric effect, photovoltaic, in CdTe films, 1907
Photocetric consistent. (See also Electron emission)

Photoelectric enect, photovoltaic, in Cd1e hims, 1907
 Photoelectric emission, (See also Electron emission) influence of defect levels on, 1206
 Photoemissive materials, alkali-antimony com-pounds, 825
 alkali metals, peak-emission wavelengths, 4075
 BaO, exciton-induced, 2264
 Bi films, temperature dependence of spectral emission, 2619
 Na₃KSb, crystal structure of, 2995
 Phototelegraphy, delay distortion correction by time-reversal techniques for, 981
 narrow-band system using flying-spot scanner and photomultiplier, 276
 'stop-go' scanning system for reducing bandwidth, 277
 Physics, optical and optical-electronic devices,

stop-go scanning system for reducing balawidth, 277
Physics, optical and optical-electronic devices, development of, 391
Pickups, crystal, with low effective mass, 1764 moving-magnet type, 2818
Piezoelectric materials, (See also Quartz) (Ba-Pb)(Ti-Zr)O, system, properties of, 3006 (Ba,Sr)TiO, Ba(Ti,Sn)O₈ and Ba(Ti,Zr)O₈, properties of, 845
BaTiO₉, ceramic, internal friction in, 475 electromechanical properties of, 3333, 3334
CdS, hexagonal, elastic properties of, 2278 influence of activator and irradiation on, 3746 ceramic, properties of, 4086
Pb(ZrTiO₉, with substituted Ca and Sr, increased dielectric constant of, 3739
ZnS-type, theory of, 846
Plasma, a.c. conductivity and Langevin equation

ZnS-type, theory of, **546 Plasma**, a.c. conductivity and Langevin equation for, **3261** charge density of, **87** conductivity of, **1161** confinement by r.f. fields, **1511** in electric and magnetic fields, transport pheno-mena in, **400** electron energy distributions in, **3260** electron oscillations, in Hg-vapour discharge with oxide cathode, **2910** transit-time relation for, **1840** electrin temperature in variable electric field, **2532** e.m. waves in, 'fourth reflection condition' for, **1164** energy spectrum of electrons in, **765**

1104 energy spectrum of electrons in, 765 equilibrium properties of, 86 gaseous, thermal conductivity of electron gas in, 766 high temperature

⁵⁰⁵COUS, Internal conductivity of electron gas in, 766
 ⁷⁶⁶high-temperature, microwave emission from, 1512
 ⁵⁰⁶ion for planar diode, 1509
 ⁷⁰⁷Lorentz-type, dispersion formula for, derivation of, 3641
 ⁵⁰⁶magnetic field, 3642
 ⁵⁰⁸damping of e.m. waves, 2201
 ⁵⁰⁹low.frequency oscillations, 3639
 ⁵⁰⁹oscillations, 'hydromagnetic' wave structure of, 1162
 ⁵⁰⁷magnetohydrodynamic waves in, kinetic theory of, 767

767 microwave conductivity of, 1842, 2202 along magnetic field, 1841 microwave investigation, 3262, 4021 of afterglow in, 2203 microwave scattering by, 769 oblique shock waves in, 1163 oscillations in, electron-beam excitation of, 1513, 2534

2534 Lagrangian formulation for, 2911 nonlinear, 2535 oscillations and waves in, nonlinear theory of, 88 stability in quasistationary e.m. field, 3640 statistics of, 1159 travelling-wave focusing for containment of, 4022 ultrasonic absorption by, 3638 Potentiometers, calibration of, 4157 Power measurement of (See also Bolometers:

Potentiometers, calibration of, 4157 Power, measurement of, (See also Bolometers; Meters, wattmeter) density-meter design for high-intensity micro-wave fields, 3831 based on Hall effect in semiconductor, 556 microwave, detector characteristics, 3830 resistive-film calorimeters for, 4162 standard, bolometer-type instrument for, 3433 wide-band calorimeters for, 2358 using wide-band thermistor mounts, 564 at 4 kMc/s, by Hall effect in semiconductor, 1312 at 30-1500 Mc/s. aperiodic barretter probe for

1312 at 30-1500 Mc/s, aperiodic barretter probe for 1322 pulse measurement at m λ , 3829 standards, microwave, international comparison of, 4163

standards, incidenter, incidenter of particular of the second s

I.43

- Photocathodes, interference-type, with increased yield and variable response, 2053
- Photocells, AgS, barrier-layer, determination of parameters, 638 amplifier, using divided crystal in bridge circuit, 1405
- Bi-Te, photovoltaic 'sandwich' *p-n* barrier type, 2055

- 2055 CdS, noise power and time constants of, 1010 classification and analysis of image-forming systems, 4237 classification of photoconductive materials for, 3520 compensating, for mirror-galvanometer measure-ments, 2354
- systems, 4237 classification of photoconductive materials for, 3520 compensating, for mirror-galvanometer measure-ments, 2354 electron-multiplier, characteristics of different types, 3155 linearization of response for light-intensity measurements, 2054 manufacture of, 3156 for scintillation counting, 3081 for stroboscopic analysis of low-intensity light flashes, 1722 Ge, junction-type, for control circuits, 309 *p-n-p* tetrode-type, response of, 308 for infrared detection, 1012 with beam-scanning read-out, 4242 InSb, preamplifier design, 4241 based on intrinsic absorption, 4239 performance measurements, 4240 pbotoelectromagnetic InSb detector, 2987 infrared modulator, Ge diode, 1721 for light sensing, based on transient response of grain boundaries, 3788 operating with electroluminescent cells as 'lumistor' amplifier, 3884 PbS, ultraviolet response of, 1407 photoemissive, properties of image-forming sys-tems, 4238 photovoltaic, Ge, grain-boundary-type, 1723 *p-n* junction, flicker effect in, 639 multi-electrode, analogous to retina, 231 Si, *p-n* junction, 640 sandwich-type, CdS, conduction mechanism of, 1406 Se, with artificial intermediate layers, 3158 influence of microstructure on characteristics of, 2056 open-circuit e.m.f. at low temperature, 3157 surface-barrier diode, as photocapacitor, 3885 transistor, equivalent-circuit analysis of, 4233 Photoconductive materials, (See also Semicon-ductors)

- Photoconductive materials, (See also Semicon-
- ductors) ductors) GG, absorption and reflection spectrum of, **1208** anisotropy in galvanomagnetic effects, **2992** conductivity glow curves of, **3321** crystal growth, at high pressure and temperature, **4077**
- crystal growth, at high pressure and temperature, 4077
 by vaporization method, 1905
 diffusion of Cu in, 3732
 displacement of absorption edge by pressure, 3729
 effect of deformation on spectrum of, 3730
 effects of porton irradiation on, 2617
 elastic constants of, 3728
 e.s. charging in strong fields, 3731
 evaporated layers, effect of heating, 828
 exciton diffusion in, 2265
 irradiation effects on, 1594
 laminar structure of, 3727
 lattice scattering mobility of electrons in, 2990
 lifetime measurements using Kerr cell, 3322
 photochemical effects and effects of 0, on, 1593
 polarization and wavelength of incident light for maximum conductivity. 2991
 review of development of, 829
 space-charge-limited currents in, 1622
 spectral distribution of, 1904
 spectral structure near absorption edge, 471
 thin films, breakdown field-strengths, 2993
 CdS and CdSe, films, bombarded by slow electrons, 2616
 photistors, characteristics of, 1011
 powders response and tran distributions in 1902
- phofistors, characteristics of, **1011** powders, response and trap distributions in, **1902**
- CdS and ZnS, internal photoeffect and exciton diffusion in, 824 CdSe, conductivity anomalies in, 469 conductivity increase under X-ray excitation,

1906 CdSe and CdTe, properties of, 468 Cu_8O , influence of adsorption on conductivity of, 3733

3733 time-lag of photoeffect in, 3734 film-type, infrared, properties of, 4076 gain-bandwidth product for, 1900 evaluation from current measurements, 1901 PbS, films, effect of thickness on spectral response, 2994

PbSe, films, chemically deposited, 830 investigations on films and filaments of, 470 performance analysis based on Fermi level, 2988 photoconduction and luminescence of, intensity dependence of, 1207 p-n junction, lateral photoeffect in, theoretical study of, 2614
Sb₄S₆, films, optical properties of, 1209 photoelectric properties of, 1210 semiconductor, test equipment for, 4078

relation,

optical properties, 4079 oxidized, measurements on, 2615 photoconductivity/time-constant 3323

Power supplies, thermoelectron engine, diode configuration for, 2434, (D)2435
 transistor, rectifier giving d.c. of either polarity, 3481
 for video circuits, 602
 transistor-stabilized, for an electromagnet, 2758
 5-9-V 800-mA, 601
 for valve heaters, high-stability, using tuned amplifier and thermistor bridge, 1697
 variable-frequency, stabilized, for instrument calibration, 1696
 Public-address systems, acoustic feedback system for increased stability, 693
 at Brussels Exhibition, 1691
 Pulses, (See also Amplifiers; Circuits; Generators)

- at brussets Exhibition, 1691 Pulses, (See also Amplifiers; Circuits; Generators) distribution system using dekatrons, 1130 mus, analysis of transmission through uniform systems, 362 synchronization, using divider vernier, 3232

Q-factor, measurement method for inductances, 2709 2709 microwave measurements of, 3819 Quartz, (See also Resonators, crystal) anelasticity at low temperatures, 2334 β-type, for high temperatures, 3009 mechanical resonance dispersion at a.f., 1219 production of microwave phonons in, 2277 sands, dielectric properties in range 3 cm-800 m, 2272 visualization of ultrasonic heam in 674

- visualization of ultrasonic beam in, 674

- Radar, airborne, for weather observations, 147 altimeters, Marconi Type S 244, 2612 miniature, X-band, 1584 anti-aircraft techniques, 2984 beam-scanning system, use of f.m., and artificial dielectric for, 2124 cavity resonator for artificial echoes, unwanted modes in, 740 cross-sections, of circular cones, 3320 of finite cones, 4073 delay lines, quartz, 2511 for detection of shock waves, 3447 determination of velocity of shock wave by, 1658 DEW-line warning system, 1592 digital counter techniques for, 2981 displays, bandwidth compression for transmission over telephone channel, 3724 distance-measurement systems, noise-modulated, 2611

 - Doppler systems, frequency stability criteria, 2607 echo box, remotely controlled, 1590 echoes, from atmospheric inhomogeneities, 819 filtering of, 2602

- mesosystems associated with, 2604 due to meteorological effects, 2603 ranging systems, p.m. and f.m., comparison of, 1893
- effect of surface reflections on rain echo cancel-lation, 4072 high-altitude, correction of slant-range distortion,

- high-altitude, correction of slant-range distortion, 821
 interference, inutual, reduction of, 3318
 suppression methods, 465
 marine, 'Escort', 2983
 3-D system for Rotterdam Harbour, 1589
 3-D system for remote presentation, 976
 modulators, Si diodes as, 3110
 moving-target system, monitor for automatic indication of jitter, 3725
 noise in, elin ination using storage system, 3319
 noise-based, improvement in range determination by, 148
 phantom targets at mm \, 3315
 phase-measurement techniques for angle and distance measurements, 1895
 pulse, effects of a.g. on accuracy of, 1894
 magnetic circuits for, 3316
 range calibration in, precision pulse generator for, 2352
 receivers, dynamic compression for, 1588
 remote presentation of data, by radio link, 1586
 review of developments in, 1561
 ring angels over south-gast England, 2982
 scan-converter storage tube for phone-line relay, 2605
 scanning systems, using electronic sector scanning, % volumetric', by ferrite phase shifters, 1896
 simulators, marine, 466

- *volumetric', by ferrite phase shifters, 1896
 simulators, marine, 466
 sweep circuit, low-power, using transistors, 3317
 tracking systems, scintillation noise effects, 2669
 traffic, Doppler system for vehicle-speed measurement, 1981
 Telefunken, 1898
 v.h.f. low-power, for auroral research, 1574
 8-mm high-definition equipment, description of, 1591
 adiation (See also Aeriale)

- 8-mm high-definition equipment, description of, 1591
 Radiation, (See also Aerials) detectors, noise in, 4166 properties and efficiency of, 4164 spatial filtering technique for, 4165 e.m., from atomic explosion, 3649 Cherenkov, from dipole, 3647 in medium with spatial dispersion, 3648 fi un detonations, 3650 of electrons in ionized medium in uniform magnetic field, 408 health hazards from, 2074, 2075 microwave, coherent, from pulse-excited NH_s molecules, 1165 stimulated emission by electrons in magnetic field, 3264 transition-type, from protons entering metal surfaces, 4018
 infrared, measurement of, thermocouples and bolometers for, 1652

- Radio astronomy, (See also Cosmic radiation; Solar radiation)

Recording, (See also Sound recording) digital, using ferrite-core storage system, 2365 film, video, using ultrasonic light modulation, 931 magnetic-tape, braking action in, 694 method for extraction of selected data, 932 multichannel, 0-10-c/s, on single-track system, 3108 for per proceeding of h f sizes la 2020

for pen recording of h.f. signals, 2020 for sampling discriminators in data reduction, 2366

2366 storage system and equipment for evaluating field-strength records, 3419 for television, 'Ampex' system, 1702 transistor amplifier for playback in, 2175 for ultrasonic frequencies, 2085 pen, circuit for converting to rectilinear output, 165

1695

peti, chicui for converting to rectilinear output, 1695
Rectifiers, (See also Semiconductors; Valves, crystal)
controlled, principles and applications of, 2421
Cu/Cu₂O and Au/Ge junctions, methods of deter-mining parameters of, 2415
electrolytic, current/time relation for, 3112
Ge, heavy-current, thermal effects in, 3109
p-n junctions for, 3485
Ge and Si, for industrial use, 269
p-n junctions, temperature limits for, 295
Se, with artificial selenide layers, 3111
semiconductor, forward-current-surge failure in, 1367

testing and establishing rating under dynamic conditions, 2341
 Si, breakdown with h.v. high-frequency supply, 3863

3663
 construction of alloy-junction type, 268
 construction of alloy-junction type, 268
 controlled, switching characteristics and rating of, 4227
 2-impurity diffusion process for, 2418
 with current rating 1A, 2022
 measurement of load characteristics of, 3484
 p-n junction, design of, 604
 as radar modulators, 3110
 Reflectometers, for bands I and II, 923
 coaxial, m-A, 3431
 microwave, display system for, (D) 2703
 with reflection-coefficient/frequency display, for 7.5-11 kMc/s, 1308
 rotating-loop, for waveguide, 2117
 Refractometers, microwave, for aircraft use, 1321
 recording-type, N.B.S., 3070
 Regulators, (See also Control systems; Stabilizers)

recording-type, N.B.S., 3070 Regulators, (See also Control systems; Stabilizers) constant-current/constant-voltage, 605 curreut, using high-gain d.c. amplifier in control loop, 3113 using transistors, for electromagnets, 979 current-balancing reactors for semiconductor rectifiers, 606 current-lim.ting, semiconductor, 1368 for electromagnet, using integrating circuit and feedback, 1365 thermostat, semiconductor, for oscillators, 609 valve, with grid compensation, delay network for, 3864 voltage, design of, 607

3864 voltage, design of, 607 using transistors, 980 Relay systems. See Radiolinks; Television. Relays, ball-contact type, 3487 reliability improvement of, 610 Resistance, contact, between K and Al, influence of electric stress on, 1271 measurement, using ion chamber as current source, 4152 on seniconductors at low temperature, cryostat

4152 on seniconductors at low temperature, cryostat for, 1967 of slight variations, in thin films, 555 negative, variable, for d.c. conputer, 3605 of obmic injecting contact, transient properties of, 2003

2903 Resistivity, of Bi and Sb, electrical and thermal, at low temperatures, 1222 of compounds with ordered spin arrangements, 1220 of transition-metal silicides, 1274

of transition-metal silicides, 1274 Resistors, carbon, derating methods for, 2491 film-type, noise and nonlinearity in, 3596 nonlinear characteristics of, measurement of, 41 pyrolytic, performance of, 2490 cracked-carbon, nonlinearity measurements on, 1106 design for guaranteed tolerance range, 3216 nonlinear, positive and negative, power relation-ships for, 729 varistors, construction, specification and per-formance, 42 wire, measurement of inductance of, 2347

Iormance, 42
 wire, ineasurement of inductance of, 2347
 Resonance, absorption, paramagnetic, influence of saturation on Faraday effect, 2547
 antiferromagnetic, in MnFa, 3791
 indirect coupling of nuclear spins in, 3036
 cross-relaxation in spin systems, 3270
 cyclotron, in metals, theory of, 1855
 electron-spin, in quartz, effect of 9·2 kMc/s ultrasonics on, 3816
 excitation of atomic levels in discharges for maser action, 3656
 excitation of spin waves in antiferromagnet by r.f. field, 2925
 ferrimagnetic, effective parameters in, 91, 2545
 in spines, magnetostatic solutions for, 2928
 ferromagnetic, absorption line width in, theory of, 2210
 in circularly polarized e.m. field, 3646

in circularly polarized e.m. field, 3646 exchange effects in, 2926 in Ni film on quartz, ultrasonic excitation by, 3817 magnetic, applications and techniques in solid-state electronics, 2924

Electronic & Radio Engineer

2903

- Radio astronomy, (See also Cosmic radiation; Solar radiation)
 interferometer, array at Nançay for solar r.f. radiation at 9 300 Mc/s, 3659
 high-resolution, for solar studies, 2936
 phase-sensitive, for measurement of brightness distributions, 1177
 interferometry using sea surface, 2219
 Jodrell Bank observations, of Andronueda nebula at 408 Mc/s, 2937
 of Coma Cluster at 408 Mc/s, 2938
 principles and results of, 3273
 radia choses from Venus, 2556
 radiation transfer and negative absorption in, 2218
 review of developments in, 1581
 r.f. emission, galactic, intensity distribution, 1176, (D)4034
 pencil-beam survey at 3.5 m λ, 2220
 mechanism in hydrogen nebulae, 421
 following solar flare, 3276
 from sun and planets, 3275
 from sun and planets, 3275
 from surces, catalogue for declinations + 10° to -20°, 423
 in Vela-Puppis region, 2221
 r.f. sources, catalogue for declinations + 10° to -20°, 423
 in Centaurus, Fornax and Puppis, 422
 Centaurus-A and Fornax-A, at 19.7 Mc/s, 2222
 Cygnus and Cassiopeia, angular diameter measurements at 10.7 cm λ, 3658
 improved measurements of position with Cambridge radio telescope, 2932
 on Jupiter, observations of, 1522
 scintillation measurements, 427
 survey at 159 Mc/s, 103
 Russian developments in, 420
 scattering of radio waves from Crab nebula by solar corona, 2939
 telescopes, Ohio State University, 3962
 Radio Hinks, for control of aircraft communication equipment, 1689
 correlation function and power spectra of signals, 4203
 fun., portable instrument for measurement of i.f. level in, 222

- 4203
 f.m., portable instrument for measurement of i.f. levelin, 222
 microwave, fading in, 3475 for radar networks, 976
 multichannel, scatter, in telecommunication networks, 600
 telephony, and C.C.I.F. recommendations for cable systems, 264
 for 60-120 channels, Italian equipment for, 2013
 planning of, 1364
 statistics of fading-dependent noise power in. 3858
 for telephony and television in 2- and 4-kMc/s bands, 1687
 u.h.f., multichannel, Oslo-Karlstad, 2756
 215-mile, 4202
 cadiosondes, radiation errors of, 226

- Radiosondes, radiation errors of, 226 Radiotelegraphy. See Communication systems. Radiotelephony. See Communication systems. Radomes, rigid, design of, 2475

- Radomes, rigid, design of, 2475
 Receivers, (See also Television) broadcast, analysis of repairs, 253 car, design of, 252 codan unit for a.f. suppression, 3101
 f.m., a.f.c. system using junction diode, 951
 converter unit for reception of multiplex-type stereophonic transmission. 1679
 using diffused-base mesa transistors, 4188
 tuner, using transistors, 251
 v.h.f. distortion due to incomplete limiting in, 4190
 'sonobuoy', modification for broadcast recen-
- 4190
 'sonobuov', modification for broadcast reception, 254, 582
 frequency-sweep, using low-pass video amplifier in place of if. stage, 1677
 h.f., dual space-diversity. Type-RX.5C, 3462
 input circuit design, 2383
 instability in, 250
 manufacture of, statistical methods in, 1676
 microwave, wide-band mixer and i.f. preamplifier for, 949
 transistor, a.v.c. circuit using diode for, 2742
 portable, design data summary, 1349
 reflex-type, design of, 3100
 30 Mc/s-75 kMc/s, using carcinotron local oscillator, 2006
 eception, (See also Television; Wave propagation,

lator, 2006 Reception, (See also Television; Wave propagation, e.m.) analysis of field-strength records for radio-link assessment, 584 correlation function and power spectra of signals in random dielectric noise, 4203 diversity, by aerial selection method, 2741 dependence of gain on signal-level distribution, 4191 frequency simplified method of 2785

4191 frequency, simplified method of, 2385 frequency, simplified method of, 2385 sector of the system using, 1675 linear combining techniques for, 3102 s.w., correlation measurements in, 953 double-diversity, tests on methods for, 952 fading effects, on A1-telegraphy signals, 1352 at m.f., 585 in u.s.w. radio links, 586 at v.h.f., diurnal variation of, 256 f.m., high-Q trap for capture of weaker signal, 1350 signal at output of limiter under noise con-ditions, 4189 v.h.f., r.f. protection ratios for, 1348 multipath pulse delay, automatic recorder for, 4192 phase-measurement system using spaced aerials, 2384 selectivity and stability in multiplex systems, 1686

2384 selectivity and stability in multiplex systems, 1686 u.b.f., diurnal variation of field strength in India and meteorological data, 255 v.h.f., distributed amplifiers, for common-aerial system, 749 220 Mc/s, over 700-1 000 miles, 1351

- Resonance, magnetic, double, theory of, 2922

 in Li and CaF₁, saturation line shapes, 1948
 nuclear, of Co⁴⁹ ions in paramagnetic salts, 3409
 free-precession observation technique for, 1853
 multiple-quantum transitions in, 2923
 radiation damping in, 2543
 spectrometer for, r.f. unit for, 2544
 weak-field maser for investigation of, 2548
 relaxation in, theory of, 95
 maser devices for infrared and optical wavelengths,
 1857
 microwave, applications of, 1171
- precession', 2542 saturation in, theory of, 95 maser devices for infrared and optical wavelengths, 1857 microwave, applications of, 1171 spin refrigeration and maser action at 1 500 Mc/s, 3654 nuclear polarization due to saturation of resonance of impurities, 3412 paramagnetic, absorption and dispersion in salts at 1 325 Mc/s, 2674 of Al nuclei in ruby, 3792 asymmetry of curve for organic radicals, 1170 in copper propionate monohydrate, 98 in Cr and Fe alums at low temperature, 2332 of Cr ions in TiO, 2333 electron free precession in, 3408 electron spin-lattice relaxation time measure-ments in, 417 in Eu and Gd, theory of, 1630 at 10 kMc/s, 1629 of Fe³⁺ in saphire, 1949 of impure MgO, 3410 of impure MgO, 3410 of impure MgO, 3411 induced emission in CuSO, 5H,O, 2927 in ionic crystals for solid state masers, 3037 microwave spectrometer technique for, 2211 multiple quantum transitions in, 1856 in nonmetals, stationary nuclear polarization by saturation, 3653 Overhauser effect in propane in diphenyl picryl hydrazyl, 2546 quantum-mechanics theory of, 778 relaxation phenomena at low temperatures, 3652 in ruby, for maser applications, 3793 sensitivity of spectrometer equipment for, 1172 spectrum of Cr ions, in emerald, 1628 in ruby, 1627 spectrum of C di In LaCl₂.7H₂O, 780 spin-level inversion and mixing in ruby, 4123 spin-level inversion and mixing in subr, 4123 spin-level inversion and mixing in subr, 4123 spin-level inversion and mixing in subr, 4123 spin-level inversion and mixing in ruby, 4123 spin-level inversion and mixing in rubr, 4123 spin-level inversion and mixing in rubr, 4124 cavity, bimodal, design for Faraday rotation coefficient of, 1424 cavity, bimodal, design for Faraday rotation experiments, 770 electron interaction with h.f. fields in, quantum effects in, 1644 expansions of e.m. fields in, 2143 measurement of parameters of, 4154 time-dependent characteristics of, microwave double-sweep method for analysis of, 926 unwanted modes in, suppression of, 740 X-band, ceramic, fobrication of, 363 cav

 - 3975 manufacture and performance of, 2142 piezoelectric, BaTiO₃, disks, vibration distributions on surface of, 2446 for generation of very short ultrasonic pulse, 2078

- for generation of very short ultrasonic pulse, 2078 quartz, high-quality, construction of, 1127 multiple-beam interferometer studies of, 2335 test equipment for detecting spurious response in, 1642 thermoelastic loss in, 206 rods, equivalent circuit for, 1475 standard measurements of parameters, theory for, 211 travelling-wave, 2144 Scattering, (See also Diffraction; Sound; Wave propagation, e.m.) of acoustic and e.m. waves, by random refractive-index fluctuations, 415 over sea or uneven ground, 775 of e.m. waves, by anisotropic ellipsoid, 413 end-fire echo area of long thin bodies, 1446 by large conducting bodies, 4029 microwave, by positive column of Hg discharge, 769

- microwave, by positive column of Hg discharge, 769
 by obstacles, variation principles for, 412
 plane, by cylindrical dielectric tube, 2540
 scalar, by periodic medium, 93
 from rough surface, statistical model for, 1518
 by thin conducting plates, 772
 by thin dielectric rings, 1517
 by turbulent inhomogeneities, 1335
 of ultrasonic wave, by periodic surface, 1047
 Semiconductors, (See also Photocells; Photocon-ductive materials; Transistors; Valves, crystal)
 absorption edge in, effect of magnetic field on, 501
 AlSb, formation of p-n junction in, 3030
 preparation and properties of, 2311
 Bi-Te, adiabatic and isothermal effects in, 2670
 conductivity and Hall coefficient of, 1942
 galvanomagnetic effects in, 183
 magnetothermoelectric effects in, 182
 model for chemical bonding in, 531

Semiconductors, Bi₁Te₃, optical properties of, 533 properties of, 532 stoichiometry of, 3785
Bi₂Te₃·Bi₂Se₃, thermoelectric properties of, 3758 bombardment damage effects in, 4091 bombardment defects in, recombination properties of, 4090
breakdown of, low-field, single phonon emission in, 3013
carrier-lifetime measurement, optical method for, 1230
phase-shift method for. 515

.ets 14

`

Semiconductors, Ge, doped with Fe, charge-carrier lifetime in, 1933, effect of annealing on, 1934 with Ga and As, changes of carrier concentration with introduction of Cu, 1250 with group III inpurities, optical and magneto-optical absorption effects of, 3366 heavily, resistivity and hole mobilities in, 519 with In, impurity conduction in, 3368 influence of group III and V elements on recombination velocity in, 1614 with Ni, electron-spin resonance in, 2661, enhanced Cu concentration in, 521 with Sb, charge-carrier lifetime in, 1932, resistivity and Hall coefficient of, 526 with Zn, properties of, 1613 drift mobility in, microwave field dependence of, 3371

A statut of the second statut of the seco

..., relays ou surface recombination velocity of, 3372
 on recombination in, 4107
 junctions, alloy, In, reverse breakdown in, 534, Si, formation of, 3379
 barrier temperature at turnover, 3024
 diffused, avalanche breakdown in, 3378
 edge breakdown, 1616
 high-electric-field effects, 3023
 infrared transparency with pulsed field, 1931
 narrow, excess noise in, 1255
 1/f noise in, theory for, 1256
 L-absorption spectrum of, 3772
 lattice constant in, precision measurement of, 1936

1936
lattice constant fit, precision measurement of, 1936
lattice vibrations in, theory of, 3367
by neutron scattering, 2304
lifetime of non-equilibrium charge carriers in, 1929
liquid surfaces, electrical phenomena on, 2656
magnetic susceptibility of photogenerated carriers in, 2300
microwave absorption techniques for measurement of lifetime, 3774
negative-mass carriers revealed by cyclotron-resonance experiments, 875
noise spectrum in near intrinsic crystals, at high field strengths, 1617
normal-mode determination by neutron spectrometry, 173
*-type, acoustoelectric effect in, 3373

metry, 173 metry, 174 metry,

3374
 optical constants of, 2659
 orientation control for wafers of, 1935
 Peltier effect in, 3776
 photoconductive response of films prepared from GeI₂, 867
 photoconductivity after electron bombardment, 3027
 photoelectromagnetic effect in, influence of fast bols or 2660

photoelectromagnetic effect in, influence of fast holes on, 2660 quadratic, 1253 plastic creep of single crystals, 2654 plasticity in, light induced, 1938 preparation of, large-scale, 2653 p-type, drift velocity measurements in, ohmic, noninjecting contact for, 3361 effect of minority impuri: ies on conduction in, 2658

radiation due to recombination of impurities in, 3369

3369 radiation-induced recombination centres in, 868 radiative recombination in, 869 reaction with HNO₃, 2310 recombination centres in, 516 Seebeck-effect fluctuations in, 178 short lifetir es of charge carriers in, 1930 splitting of As donor ground state in, 1615 surface influence on 1/f noise in, 172 surface recombination velocity in, high-vacuum studies of, 1248

I.45

3374

¥ .

X

- 1230
 phase-shift method for. 515
 charce carriers, in perturbed lattices, 2528
 A^{III}BV, behaviour of impurities in, 2641
 K-edge structures of elements of, 853
 magnetic properties of, 2645
 surface differentiation by X-ray method, 3786
 Ag, ternary, with NaCl-type structure, 1269, solid solutions of, 1270
 energy losses in, 4092
 Hall effect in, and applications of, 855
 of homopolar character, 1227
 intermetallic, preparation, properties and applications, photoelectric

- cations of, 163
 vitreous, photoelectric and thermoelectric properties of, 1920
 compounds and elements of Groups VB-VIIB, properties of, 1226
 conductivity at high frequencies, depolarization effects in, 3631
 contacts on, adhesive forces developed in, 495
 CoSb₂, thermoelectric properties, effect of alloyed impurities on, 2667
 CuFeS₂, CuFeTe₂, AgFeS₂ and AgFeTe₂, 3755
 CuFeS₂, diamagnetic Zeeman effect and exciton structure in, 1623
 current build-up during switching in, 889
 current density calculation using drift velocity, 3751

- 3751
 cyclotron resonance in, 2647
 development and future application of, 489
 diamond, rectification and photo-effects in, 504
 Si and Ge, electronic structure of, 1238
 thermoelectric power of, 1924
 diamond-type, vibration spectra and specific heats of, 2284
 diffusion across vapour interface, 165
 dislocation planes in, 3338
 doped, compensation technique for narrowing energy gap, 1917
 electron-electron scattering in, 492
 electron-electron scattering in, 492
 electron-ble pairs in, effect of lattice vibrations on, 850
 energy-band interpolation based on pseudo-potentials, 1236
 equilibrium charge density in bipolar diffusion in, 2637

- equilibrium charge density in bipolar diffusion in, 2637 excess carriers in, decay of, 1915 time-dependent chances in presence of surface recombination, 1228 with excited impurity band, theory of, 3752 Faraday effect in, 4088 FeSe, preparation and measurement results, 885 field effect at high frequency in, 2640 field-effect theory, 2639, 3749 field-effect theory, 2639, 3749 field-effect theory, 2639, 3749 diffusion and electrical behaviour of Cu in, 882 diffusion of Zn in, at 1 000°C, 1259 effective electron mass determined by infrared Faraday effect, 4113 elastic moduli of single crystals, 3380 electron mobilities in, 529 m-type, infrared absorption and electron effective mass in, 3383 piezoresistance of, 1939 single crystals, polarity of, 3381 galvanomagnetic, thermomagnetic and thermo-clectric effects in, surface transport theory for, 1233

- galvanomagnetic effects in, surface transport theory for, 1233 Ga₃Te₃, doped with Cu, crystal structure changes, 3031

3031 Ge, Bi as donor in, 4105 bicrystals, grain-boundary conduction in, 2657 carrier mobility in, effects of temperature and field on, 4101 carrier multiplication in, microwave-induced, 2302

2302 contact-potential measurements on cleaned surfaces, 3360 crystal pulling from floating crucible, 3029 crystal, with dislocation array, minority carriets in, 1618, transport properties in, 1619 dislocation-free, vacancy clusters in, 522 dislocations in, 1247, produced by thermal shock, 865, produced by thermal stresses, 3028 growth effects on properties of 170

shock, 865, produced by thermal stresses, 3028 growth effects on properties of, 170 growth phenomena, 3358 melted-layer growth of, 1251 X-ray integrated intensities for, effect of impurities on, 177, 3376 X-ray measurement of microstrains in, 3377 X-ray transmission anomalies, 2309 deformation potential from optical absorption lines, 2655 Dember potential measurements in, 3359 diffusion of B in, 1612 diffusion of Cu in, theory of, 1611 diffusion of Cu in, theory of, 1611 diffusion of thermal acceptors in, 520 doped, with Au cr Zn, photoconductivity response. 4106 crystal growth from molten metals, 4102

- Semiconductors, surface states on, 171 surfaces, effects of chemical action and oxidation, 3370
 etching and polishing, 1252 etching to precise limits, 4103 influence of H⁺ on conductivity of, 2301 recombination centres after ion bombard-ment, 2303
 thermal conductivity of, 1620
 thermally induced glide of dislocations in, 3363
 thermo-e.m.f. measurements on, 524
 thermonagnetic effects and phonon drag in, 2662
 transitions in, exciton- and magneto-absorption of, 3364
 theory of optical magneto-absorption for, 3365
 vibrational spectrum and specific heat of, 517
 Zeeman splitting of donor states in, 525
 Ge and Si, band structure during strain, observa-tion by cyclotron resonance, 507
 contacts on, metal, preparation of, 491
 crystals, large, growth by Teal-Little method, 3767
 orientation by optical technique, 166
 distribution coefficients of impurities in, calcula-tion of, 1242
 as electrodes in electrolyte, saturation-current investigation, 4093
 heat capacity and vibrational frequency spectra of, 3353
 infrared antireflection coatings for, 864
 lattice vibrational spectra of, 857

 - of, 3353 infrared antireflection coatings for, 864 lattice vibrational spectra of, 857 lattice vibrations in, 2286 metallurgy of, 3020

 - negative-mass cyclotron resonance effects in, 3760
 - optical absorption edge of, effect of pressure on, 1243 p-type, effect of deformation on properties of, 2649

 - p-type, effect of deformation on properties of, 2649
 recombination centres and trapping levels in, distinction between, 3764
 reflection coefficients of, 3765, 3766
 slow capture of holes and electrons by surface states, 3352
 solubility of Sn in, 4094
 specific heat at low temperatures, 2287
 surface distribution of slow traps in, 3768
 surface tables on, 3019
 theory and properties of, 3351
 Ge-In junctions, X-ray investigations of, 1937
 generation-recombination noise in, 493
 Ge-Sb alloys, distribution of 528
 grain boundarics, capacitance and barrier height in, 3339
 graphite, galvanomagnetic data for, analysis of

 - in, 3339 graphite, galvanomagnetic data for, analysis of, 1241
- in, 3339 graphite, galvanomagnetic data for, analysis of, 1241 galvanomagnetic oscillations in, 1240 Hall effect and magnetoresistance of, field dependence of, 1239 Hall effect and magnetoresistance effect, influence of geometry on, 1234 heat flow in, RC-network analogue for, 4087 HgTe, Hall coefficient and resistivity of, 4112 thermonagnetic properties of, 3779 high-purity, 486 impurity-band conduction in, simple model for, 3010 theory of, 1223, 1224 impurity paramagnetism at low temperatures, 2644 impurity photo-ionization spectrum in magnetic field, theory of, 1232 In monotelluride, properties of, 2312 InAs, doped, with Cu, 2666 with p-type material, anomalous temperature characteristic of Hall coefficient of, 3385 effect of heat treatment on, 3032 n-type, piezoresistance constants of, 884 preparation of, 1624 InAs, and InSb, as thermoelectric materials, 3384 vapour-deposited films, preparation and pro-perties of, 3761 InAs, 1,-2Pz, thermoelectric properties of, 3759 infrared absorption of, effect of pressure on, 3014 inhomogeneities made visible by micrography, 3757 inorganic compounds, prediction of semiconducting properties in, 847 InP, breakdown in low field, 4116 electron mobility in, 4115 n-type, optical properties of, 4114 InSb, band structure of, 1940 distribution coefficients and carrier mobilities in, 3386 intrinsic, electron transport in, 4117 n-type, conduction in, 1625

- 3386 intrinsic, electron transport in, 4117 *n*-type, conduction in, 1625 conductivity in strong field, 530 magnetically induced impurity banding in, 1263

- 1263 mp interest and Hall effect in, 4119 oscillatory transverse magnetoresistance effect in, 1264 nuclear magnetic resonance in, 1261, 1262 oscillator based on field effect in, 3781 photoanodization of, 3782 piezoelectric effect in, 1800 plasma pinch effects in, 3388 plastic flow of, delay time in, 3387 properties of, 3033 \$p-type, conduction in, 1260

- Semiconductors, InSb, *p*-type, conductivity in strong field, **179**
- field, 179 photoelectric properties and lifetimes, 'in 4118 transverse magnetoresistance at liquid-nitrogen temperature, 1265 thin layers of variable composition, 3780 irradiation effects on, 2646 junctions, capacitance with graded impurity density, 852 effect of surface potential variations on character-istics, 3390 metallographic aspects of, 187 non-ideal, increase of minority-carrier current by, 1626

- p-n, charge-carrier distribution in base region, 1919
- 1919
 injection efficiency of, 496
 p-n and p-i, analysis of field distribution and carrier concentration in, 3787
 preparation of, theory for, 888
 lapping machine for thin slices of, 1943
 lifetime measurement by photoconductive decay, 1921

- 1921 magnetic susceptibility of trapped electrons and holes in, 3017 magnetoresistance and photoelectric effects due to electrons and slow and fast holes in, 1923 MgTe, preparation and properties of, 1258 minority-carrier lifetime, dependence on majority-carrier density, 849 MoQ, influence of foreign ions on semiconductivity of, 3783

Semiconductors, Si microplasma fluctuations in, 3770,
microwave spin echoes from donors in, 860
neutron-bombardment damage in, comparison with electron-bombardment effects, 861
*type, ohmic Al contact on, 3356
photoionization quantum yield, 863
p-type, bonding materials for, 2296
recombination properties of Au in, 862
resistivity of, effects of 0, on, 2294
surface properties of, effects of treatment and atmosphere on, 4097
surface recombination velocity, measurement of, 859, by steady-state photoconductance, 1246
surface stabilization by thermally grown oxides, 2650
valence-band structure of, 508
SiC, films, cubic, infrared properties of, 2298
infrared properties of 2297
junctions, electron emission from breakdown regions in, 1610
report of conference on, 3771
surface properties of crystals, 3022
SnS, synthetic crystals, properties of, 886
SnSe, electrical properties of, 3389
space-charge distribution due to low-level injection, 3012
Stark effect for study of valence bands, 3346
surface recombination velocity, determination from photoconductive decay, correction formulae for, 498
determined by change of resistance in magnetic field, 500
effects of carrier injection on, 1916
surfaces, properties of, 3763
magnetic susceptibility in, 1607
thermoelectric prosenties of, 3347
effect of strain of, 490
thermoelectric effects in, power limits of, 1231
thermoelectric effects of, 3347
effect of strain on, 854
thermoelectric effects of, 3347
effect of strain on, 854
thermoelectric properties of, 3347
effect of strain on, 854
thermoele

Ti and V oxides, conductivity measurements on, 3756 TiO₂, infrared absorption of, 3034 piezoresistivity in, 887 transitions in, interband, Zeeman-type, magneto-optical studies of, 2283 two-band, theory of thermoelectricity in, 3015 variation of properties with fusion, 1918 V₂O₂, binary nixtures, conductivity mechanism, 3750 W₂C, field-emission characteristic of, 1922 WO₃, conduction in, 2668 work function of, temperature dependence of, 494 ZnO, conductivity of powder form, 877 diffusion and precipitation of In in, 4111 doped, conductivity and Hall effect in, 879 field effect and photoconductivity in, 880 preparation of single crystals with defined impurity content, 878 surface potential, field-effect mobility and conductivity of, 3778 Servomechanisms, (See also Control Systems) digital, using c.r. tube beam in photographic storage system, 1459 for temperature control of transistors, 1693 for u.h.f. scatter-link transmitter, 1694

for u.h.f. scatter-link transmitter, 1694 Signal generators, (See also Generators; Oscil-lators)

lators) microwave, amplitude stabilization of, 2353 timed-pulse, portable, 1966 Signals, finite-duration, maximum efficiency for transmission through low-pass filter, 2390 flow graphs, 3601, 3602 interpolation and prediction of, optimum filter for, 2391

2391
Solar activity, causing transient decreases in cosmic-ray intensity, 2942
eruptions, possible mechanism for nonstable processes, 3666
flares, as cause of geomagnetic storm of 11th Feb. 1958, 433
and intense long-duration ionization below 50 km, 2576
magnetic field associated with, 4043
radiation and particle precipitation from, 1530
associated with r.f. noise at 200 Mc/s, 1180
25th-27th Sept. 1957, observations at 4:3 mm λ, 786
indices based on ionospheric and r.f. noise data,

indices based on ionospheric and r.f. noise data, 3281

Solar eclipses, temperature fluctuations during, 2559

2559
Solar radiation, (See also Radio astronomy) nonthermal, gyro theory of, 408 outbursts causing geomagnetic storms, 2558 proton streams, laboratory model using 'Störmertron' tube, 1864
r.f., brightness distribution at 60 cm λ, 430 bursts of, anomalous night-time reception of, 2554 m-λ and 3-cm-λ, time relations of, 2555 power spectrum and relation to s.w. fades and

power spectrum and relation to s.w. fades and geomagnetic storms, 1178 type-II, observations of solar disturbances causing, 432

Electronic & Radio Engineer

- and e., induce of ioreign ions on semiconductivity of, 3783
 mobility and effective mass in, correlation of, 2279
 negative effective mass related to negative resistance, 3632
 nondegenerate, electron mobility in, 1225
 Hall mobility in, 856
 low-field carrier mobility in, 164
 "type, impure, drift and Hall mobility of electrons in, 3340
 thermal effects in, 1604
 transient response of grain boundaries in, light sensor based on, 3788
 transport phenomena in, integration method for, 3754

- 3754
 in magnetic field, 3753
 optical characteristics of, 3011
 optical properties under hydrostatic pressure, 506
 PbO, conductivity measurements with impurity additions, 3784
 PbS, PbSe and PbTe, magnetoresistance in, 1267
 mobility of electrons and holes in, 181
 PbTe, thermoelectric properties of, 1941
 photoconductivity of, influence of surface recombination on, 2643
 photoconductivity and lifetime measurements, 3342

- 5342 photoelectromagnetic and photoconductive effects in, 1229 piezoresistance of, electric-field dependence of, 3345

- piezoresistance of, electric-field dependence of, 3345
 polar, binary, interdiffusion in, 3343
 lattice screening in, 3344
 theoretical transport coefficients for, 2642
 polymeric, acrylnitryl, 4121
 pyrolusite, properties of, 1266
 research at N.B.S., 3748
 Sb₁Te₂ and Sb₂Te₂, Hermoelectric effects in, 1266
 Se, dielectric behaviour at dm \lambda. 2285
 diffusion of impurities in, 1605
 polycrystalline, influence of annealing time on thermoelectric power, 2648
 secondary-emission measurements as function of doping, 3762
 thermal conductivity of, effect of Br additions on, 1606
 Si, absorption bands in, 1608
 absorption-edge spectrum of, 509
 avalanche breakdown in, statistical theory of, 4095
 compressional waves at 10-170 Mc/s in, tempera-

4095 compressional waves at 10-170 Mc/sin, tempera-ture dependence of velocity of, 3355 crystal growth, effects of seed rotation on, 3021 free from dislocations, 3354 by pulling technique, furnace for, 168 density change on melting, 2292 diffusion of Ga in, 513 diffusion of Ga in, 513 diffusion of Pin, 2651 doped, with Al, precipitation on dislocation in, 2289 with As, absorption spectrum of 1244

doped. with Al, precipitation on dislocation in, 2289
with As, absorption spectrum of, 1244
with As, absorption spectrum of, 1244
with Au, measurement of lifetimes and capture cross-sections, 3769
with P, electron spin-lattice relaxation in, 512
electron-spin-resonance experiments on donors in, 4098, 4099
electropolishing in HF solutions, 1245
formation of donor states in, mechanism of, 1926
heat-treated, change of characteristics due to introduction of Au, 2290
impurities in, O, 511
impurity-carrier concentration in, variation with temperature, 510
impurity compensation and magnetoresistance in, 2293
infrared spectra of heat-treatment centres in, 167
infrared strain-optic coefficient for, 2295
irradiated by neutrons, magnetic and electrical properties of, 4100
junctions, breakdown in, 2652, effect of heat treatment on, 1609 *p*-m, delineation of, 514, impact ionization in, 1927, photomagnetomechanical effect in, 3357
lattice vibrations by neutron scattering, 2291
lifetime preservation by getter action. 2288

lattice vibrations by neutron scattering, 2291 lifetime preservation by getter action, 2288 measurement of resistivity using 4-point probe method, 214

- Solar radiation, r.f., bursts of type-III, flare-puffs as cause of, 431 type-IV, and relation with storm centres, 3283 3-cm- λ , dimensions of sources of, 425 dm- λ , as index for ionospheric studies, 787 echoes in solar corona, 102 ionizing radiation associated with noise storm, 429

 - 429 polarization measurements of, 101 spectroscopy at 24-40 Mc/s, 2933 at 3 and 27 cm λ , during y-ray burst from solar flare, 104 at 3.2 cm λ , distribution and brightness of sources, 424 at 200 Mc/s, fine structure and drift in frequency, 2035
 - 2935
 - during noise storms, short-period variations in, 2934
- 2934 ultraviolet, investigation of, 3664 Solders, for nuclear and space environments, 4144 Sound, (See also Absorption; Acoustics; Diffrac-tion; Transducers; Ultrasonics) attenuation in gases, 2809 audibility of nonlinear distortion, 3185 build-up of oscillations in enclosed spaces, 3184 constant-pressure source, using microphone and feedback system, 2447 distorted, criterion for, 2817 field of vibrating source on ribbon plate, 1044 frequency spectrum of power-law double tones, 3908 interference and coherence of reiterated signals.
- frequency spectrum of power-law double tones, 3908 interference and coherence of reiterated signals, 3910 'lateral-wave' field of point source, 1040 loudness, evaluation, 3544 influence of peak content in noise, 1754 meter, 1427 scale, discrimination criterion, 1062 sensation for rhythmic sounds, 1426 tests with periodic sounds, 3911 noise, from data processing machines, measure-ment and evaluation of, 6 impact, instrument for measuring peak intensity of, 2089 measurement methods, 2453 spectra evaluation, 3914 pitch fluctuations, measurement of, 3179 propagation of, amplitude and phase fluctuations of spherical wave in, 662 amplitude fluctuations in turbulent medium, 667 correlation of field with amplitude and phase fluctuations in, 663 diffraction and radiation in liquids and gases, 664 over ground, experimental study of, 3900, in-strumentation for 2081

 - 664
 over ground, experimental study of, 3900, instrumentation for, 2081
 in inhomogeneous media, 'effective' parameters for, 1041
 in medium with negative velocity gradient and homogeneous surface layer, 666
 in sea-water, velocity calculations, 3903
 underwater, analysis for different pulse shapes, 3901

in sea-water, velocity calculations, 3903
 underwater, analysis for different pulse shapes, 3901
 waveguide mode in stratified medium, 665
 propagation of Rayleigh-type waves on cylindrical surfaces, 670
 radiators, concentration coefficient of focusing systems, 3905
 distance determination from near-field measurements, 3537
 superdirective arrays, signal/noise performance, 329
 reflected from sphere under pulse conditions, 1046
 reflections from gradual-transition absorbers, 3548
 scattering, on inhomogeneous surfaces, 675
 by thin rod, 676
 in irregular waveguides, 1042
 at layer of discontinuity in sea, 3902
 in turbulent atmosphere, 2083
 stereophonic, compatible system based on 'precedence effect', 3474
 velocity of, in liquids, influence of wall thickness of resonance tube, 1422
 viscosity correction, 328
 in pure and salt water, using ultrasonic pulse technique, 2810
 Sound ranging, active sonar detection, theory of, 2596
 direction finder for location of noise sources, 2091
 multiple-receiver correlation system, 1066
 underwater missile tracking instrumentation, 2597
 Sound recording, disk, standardization of, 2454
 magnetic, for delaying reproduced sound, 3500
 speed and pitch regulator for, 2825
 theory of, 3923
 stereophonic, cutting head for single-groove disk, 2096
 velocity-type microphones in, 7
 stereophonic reproduction system for, two-track, there of wanget 1064

- stetepinion, curring nata to ungo growther intro 2096
 velocity-type microphones in, 7
 sterophonic reproduction system for, two-track, three-channel, 1064
 Space research, communication, navigation and guidance systems in, 2807
 cosmic rockets, instrumentation of Pioneer vehicle and tracking stations, 3286
 interferometer for tracking, 1544
 launching problems, 3677
 Lunik I, 2230, 2563, 3678
 cosmic-ray data from, 2231
 progress of, 3676
 Lunik II, observations at Jodrell Bank, 4051
 Pioneer I, cosmic radiation measurements by,
 x
- - Lun... Pioneer 1 3691
- 3691 Pioneer IV, signal reception using parametric amplifier, 2895 dynamic problems of flight to moon, 3675 radar technique based on back-scatter from free electrons, 451 Spectrographs, magnetic, current and field stabili-zation of 9-kW electromagnet for, 3072
- Electronic & Radio Engineer

- Spectrographs, mass, magnet stabilization by atomic-beam resonance, **4170** Spectrometers, mass, ion source for, strong-focusing, **2720** microwave, high-Q Stark absorption cell for, **2209** for paramagnetic-resonance measurements, **1172** influence of modulation amplitude on line shape, **3269** source-modulated criteria for **416**

Telemetry, transmission system, using magnetic-modulator/multivibrator circuit, 1659
u.h.f., 6-channel, 4173
Television, (See also Aerials; Interference) applications, in astronomy, 3082, 3083 for determining rocket orientation, using single-line-scan vidicon, 2003
for recording eye fixations on changing visual scenes, 930
camera tubes, image-orthicon, image retention in, 615
operation of, 3497

scenes, 930 camera tubes, image-orthicon, image retention in, 615 operation of, 3497 quantum efficiency of detection, 4216 recent developments in, 616 sensitivity of, 4215 vidicon-type, inertia effects, 985 lenses for, 1375, 1376 target materials in, 1703 cameras, measurements on preamplifiers for, 3115 portable, for outside broadcasts, 2026 . single-lens reflex, 3496 zoon lenses for closed-circuit systems, 1370 cameras and film scanners, video amplifier using transistors, 4214 centre, ATN, Sydney, 1330 colour, automatic hue and chroma controls for, 3118 camera tubes, vidicon, for industrial service, 2025 'chroma-key' technique for simulating optical effects, 612 compatible 819-line system for, 1370 film, lenticular system for, 1371 flying-spot scanning system, 279 magnetic demodulators for, 1379 N.T.S.C. system, adaptation to European 625-line standard, 4212 modulator for C.C.R. standard, 2762 phase and amplitude fluctuations in subcarrier transmission, 993 picture quality in, 2404 and perception of colour detail in N.T.S.C. system, 1391 picture tubes, afterglow in, 2407 deflection coil design for, 3125 mask-type, error correction in, 990 screen-persistence test equipment, 4218 21-in, Type-21CYP22, glass, 280 projection systems, 3119 display with controlled filters, 621, 2029 picture tube using Faraday cell, 1705 receivers, 'apple' system, colour-purity adjust-ment techniques, 1386 performance measurement, 986 signal-distortion in envelope-type second detectors, 1392 standards, F.C.C., 278 test equipment, for investigating interference of subcarrier with monochrome reproduction, 2032 for N.T.S.C. system, 1372 signal generator for, 1324 transmitters, correction of phase distortion in, 614 use of dichroic mirrors in, 1701 echo phenomena in, methods of eliminating, 3134 industrial. equibment for 1394. 1304

signal generator for, 1324 transmitters, correction of phase distortion in, 614 use of dichroic mirrors in, 1701 echo phenomena in, methods of eliminating, 3134 industrial, equipment for, 1394, 1395 interference reduction in co-channel systems by precise carrier frequency control, 4221 links, cable, interconnection at carrier-frequency stage, 992 long-distance, 4210 for switching and control centres, 275 transatlantic, 4211 using trunk coaxial cable, fluctuation Inter-ference in, 611 delay equalization method, 3132 waveform distortion testing, 4209 networks, European, survey of, 1707 Eurovision, German standards converter equip-ment, 4213 optimum design for bands IV and V, 3501 in Württemberg, 1692 picture quality, assessment of, 4222 test pattern for, 1393 comparison method for measurement of random fluctuations in, 2031 detail perception test, 3135, 3136, 3138 impairment by noise, tests on, 2408 use of bifilar-T trap for improving, 988 picture tubes, contrast filters for, tests with, 2765 current characteristic of, 1704 electroluminescent, problems of, 566 flat-type, for monochrome and colour, 619 guns for, drive factor and gamma of, 1417 kinescope, high-transconductance electron gun for, 322 measurement of resolution characteristics, 1390

urement of resolution characteristics,

1390 with luminous surround, subjective tests on, 2764 new electron gun with transistor drive, 3128 sealing of, 1035 short, using TPF gun, 3127 thin, rectangular, 3171 1109-deflection, development problems, 284 projection, eidophor system, 620 random-noise measurement in presence of signal, 2345 receivers deflection circuits using transistors

receivers, deflection circuits, using transistors, peak flyback voltage in, **4220** dual-standard, for French and C.C.I.R. systems,

effects of valve faults in, 311 frame multivibrator and diode separator circuit, 3499

3499 i.f. amplifiers with linear phase response, 3117 line-deflection transformer, magnetic measure-ments on ferrite U-cores for, 3057 with tuned h.v. winding, 1387 line and frame output stabilization, 3123, 3124 line output circuit stabilization, 3871

I.47

measure 1390

- Interventer of the absolution cell for, 2409
 for paramagnetic-resonance measurements, 1172
 influence of modulation amplitude on line shape, 3269
 source-modulated, criteria for, 416
 X-band, for paramagnetic-resonance observations, 1854
 for X and K bands, 96
 Spectroscopy, infrared, theory of interference modulation for, 2191
 application of, 2192
 Speech, acoustic studies of, instruments and methods for, 1058
 analysis and synthesis of, 2450
 characteristics, theoretical analysis of, 4
 compandor, for transmission circuits, 2395
 intelligibility of, evaluation of, 2819
 at high noiselevels, prediction of, 3543
 subjective masking of delayed echoes, 5
 masking by prolonged vowel sounds, 680
 pitch distribution in German language, 2083
 recognition systems, automatic, 3913
 mechanical, 2451
 system for telephony, 331
 theory of, 2452
 phonetic-pattern vocoder, 1057
 for voice dialling, 1061
 reinforcement systems, factors affecting intelligibility of, 1753
 vocoder transmission system for, 2394
 Stabilizers, of anode-current fluctuations due to heater-current changes, 1369
 thyrater, 2719
 standard-frequency transmissions, JJY, frequency variation of received signal, 916
 MSF, correction with reference to Ephemeris time, 1640
 poweria of received signal, 916
- 1640 power requirements and optimum frequency for world-wide system, 4201 Standards, on navigation aids, 59 I.R.E. 12.S1, 3721 on recording and reproducing, calibration of mechanically-recorded lateral frequency records, 58 I.R.E. 10.S1, 689 on terminology, of audio techniques, 58 I.R.E. 3.S1, 727 for magnetic amplifiert of S.T.
- 727 for magnetic amplifiers, A.I.E.E. Committee report, 383 of static magnetic storage, 59 I.R.E. 8.S1, 2019 on waveguides and waveguide component measure-ments, 59 I.R.E. 2.S1, 2105 Standing-wave indicators, automatic, for 3-cm band, 2711 for production testing of microwave components, 221 for 4.Mole band using onc. 1975

- for 4-kMc/s band, using c.r.o., 1975
 Stations, (See also Broadcasting; Television; Transmitters)
 Olifantsfontein and Derdepoort, South Africa, 2015
 WWI, for v.h.f. research, 977
 Storage systems, (See also under Computers) magnetic-drum, 1655
 flying-spot, beam-positioning servo system for, 2364
 destruction of 2362
- design factors of, 2362
- 4304
 design factors of, 2362
 optics and photography in, 2363
 Sun, (See also Solar activity: Solar radiation)
 brightness of disk, comparison of results obtained during 1944 and 1954 eclipses, 785
 corona, intensity, polarization and electron density of, 1182
 investigations using r.f. emission from Crab Nebula, 426
 new theory of, 2943
 Sunspots, numbers, mean values and data for 1700-1967, 1529
 for 1944-1959, 107
 for 1949-1968, 3282
 structure and mechanism of, 3665
 Superconductors, energy gap in, evidence for, 393
 in h.f. field, impedance of, 2195
 impurity scattering in, 3633
 Sn, change in sound velocity from normal state, 4122
 Sn and In, frequency variation of resistance of,

- 4122 Sn and In, frequency variation of resistance of, 2314 Switches, (See also Circuits, switching) coaxial, using Si diodes, for v.b.f. aircraft aerials, 3486

3486
 microwave, using ferrite ring inside helix, 1107
 t.r., electronic, 44
 voltage-sensitive, using dielectric breakdown of oxide film, 39
 Switching, functions, classification and minimization of, 3048
 solution of equations for, 1297
 systems, ternary, algebra for, 1636

Telecontrol systems, h.f. characteristics, in terms of parameter f₁, 4236 timing-signal transmission at Canaveral test range, 2722

Telemetry, balloon-borne units using transistors, 2373

2373 miniature system for electroencephalograph, 3085 p.p.m., demodulator system for, 1992 for rotational displacements, 2374 systems, comparison, 4172 performance analysis, 3084 techniques for guided missiles, 3448

- Television, receivers, line output circuit stabilization, using voltage-dependent resistance, 989
 line timebase circuit, stabilized, protection devices for, 282
 manufacture, statistical methods in, 16
 multitriode flywheel synchronizing circuit, 3500
 noise-gated a.g.c. and sync system for, 1382
 pin triode for bands IV and V, 2796
 r.f. amplifier, constant-impedance, 1384
 scanning oscillators and synchronization, 3121
 sound-channel, 'delta' f.m. system with a.m. compression, 2027
 detector using drift transistor, 2028
 synchronization, characteristics in presence of noise, 1388
 noise-limiting circuits and a.g.c. for, 3120
 separator using remote-cut-off pentode, 3122
 synchronous and exalted-carrier detection in, 1376 Transductors, (See also Amplifiers, magnetic) auto self-excited, analysis of, 1791 Transformers, balun, for v.h.f. and u.h.f., 338 double-tuned, general analysis of, 3595 equivalent 2-terminal networks for, 1467 bybrid, design and applications of, 1468 mains, lamination data and design procedure, 356 pulse, with premagnetization of core, 1469 pulse-front response of, measurement of para-meters of, 357 for random-noise voltages, 3214 transmission-line, stepped, design of, 3594 twisted-pair, wide-band, 3593 with zero phase shift, design of, 720 Transistors, (See also Photocells; Semiconductors; Valves, crystal) with ∞ 1, current multiplication in, 1626 alloy-junction, base resistance for, 1714 Ge, dependence of current gain on emitter current and frequency, 3878 with symmetrical characteristics, 2419 alloy-junction and grown-junction types, Si, comparison of, 300 analogue-computer determination of design data, 3508 analysis of quadripole networks containing, 48 applications in the band' synchrophase, for phase-distortion correction, 3116 synchrophase, for phase-distortion correction, 3116 transistor circuits, 987 for i.f. stages, 1385 for line deflection, 3126 for vertical-deflection system, 1381 for 90° deflection, 3870 u.b.f. tuner using r.f. amplifier, 1383 video output stage with wire resistor, 2347 X radiation from, 4219 for 625-line C.C.I.R. standard, 617. reception, effects of random noise, 3139, 3140 field-strength measurements and propagation curves, 288 measurement of service area, 287 vertical-polarization tests at u.h.f., 289 recording, film, methods and equipment in Germany, 2024 magnetic-tape, 'Ampex' system, 1702 systems for international program exchange, 3867 relay systems, passive, aerial calculations for, 2851 analysis of quadripole network unit of types, Si, comparison of, 300
 analogue-computer determination of design data, 3508
 analysis of quadripole networks containing, 48
 applications, in 'hybrid' regenerative valve circuits, 2877
 for i.f. amplifer, 305
 in line communication systems, 594
 review of, 4228
 in television receivers, 987
 avalanche-type, 2772
 theory of, 186, 998
 transient build-up in, 2416
 characteristics, a.c., representation of, 2042
 curve tracer, 3060
 frequency and phase, for common-emitter operation, 634
 pased on insertion of, 631
 diffused-base, evaporation alloying technique for, 307
 manufacture of, 4229
 unesa, in f.m. receiver, 4188
 for range 10-20000 Mc/s, 635
 diffusion capacitance in, 3148
 drift-type, current gain to 105 Mc/s, 3880
 diffused-base, for 1-kMc/s, properties of, 3510
 equivalent circuits for, 3672
 h.f. power gain of, 3681
 internal current gain of, 999
 transmission-line analogue of, 3153
 effective collector capacitance in, 632
 emitter efficiency of, 2043
 equivalent circuits for, 3679
 current anneling of, 3519
 equivalent circuits for, 3672
 grain-boundary, for low-temperature, 3882
 diffusion and thigh temperature operation, 1722
 grown-junction, n-p-n, Si, construction of, 301
 h.f., equivalent -circuit analysis and characteristics of of 4239 relay systems, passive, aerial calculations for, 2851 research work at Turin study centre, 2761 review of developments, 1699 standards converter, using vidicon, 2405 stations, in N. America, list of, 2030 studio equipment, improved design of tungsten filament lamps, 286 unaintenance of, 622 systems, cable, equalization in, 3488 closed-circuit, coaxial-cable, using transistors, 3114 3114 for industrial applications, 272 two-way, remote-control carrier system for, 285 In industrial applications, 272 two-way, remote-control carrier system for, 285 coding method based on 'edge' detection, 3489 optical performance criteria, 3498 vestigial-sideband, phase distortion in, 3137 for 50-kc/s bandwidth, 982 test equipment, B.B.C. transparencies for testing cannera channels, 984 waveform generator using transistors, 1373 test patterns, for monochrome installations, 3502 testing techniques for monochrome and colour transmission, 613 transmission, 513 transmission, 513 delay equalization in, filters for, 787 delay equalization in, filters for, 737 limiter circuit stor, 273 correction equipment, 3495 delay equalization in, filters for, 737 limiter circuit technique, 3491 in conitoring installations, 3669 in Germany, 2763 residual-sideband, delay equalization, 3490 of still pictures, using flying-spot scanning system, 1374 over telephone lines, experiments using 250-kc/s bandwidth, 274 video level control during studio switching, 3131 transmitters, automatic frequency translation for improving local reception, 991 band-1, ABN, Gore Hill, Australia, 3129 design of, 3492 Isle of Wight I.T.A. Station, and associated radio links, 1706 vestigial-sideband filters and diplexers, 3494 5- and 10-kW, 3493 Chermistors, circuits using, design for, 40 for compensation of resistance and conductance, and extraction at high temperature, 3882
 diffused ninicrystals for, 637
 grain-boundary, for low-temperature operation, 1712
 grown-junction, n-p-n, Si, construction of, 301
 h.f., equivalent-circuit analysis and characteristics of, 2423, 2768
 Ge, design theory and production of, 1000
 Ge and Si, 3509
 production techniques for, 2049
 progress in development of, 1399
 h.f. phenomena in, model for, 3154
 high-current mode of operation of, 1004
 hook, properties of, in switching and amplifying eircuits, 753
 interchangeability chart for 500 types, 3517
 lattice defects in, influence and creation of, 2771
 life expectation of, in earth satellites, 2780 mechanisms affecting, 1715
 limiting-frequency determination up to 1 kMc/s, 4232
 measurements, of a cut-off frequency, 2705
 apparatus and techniques, 3430
 of current gain, 3426
 automatic equipment for, 3427
 d.c.-a.c. beta tester, 1647
 of equivalent-circuit parameters, 1646
 simulator for, 4156
 sweep generator for c.r.o. display of β/Ie characteristic, 928
 of temperature-dependent base leakage current, 1974
 of v.h.f. characteristics, design of matching networks for, 1115
 wide-band bridge for, 1002
 as network element at 1.f., 1719, 3518
 noise figure of, influence of inductive source on, 2047
 parameter conversion, using Jacobians, 2775
 point-contact, effect of magnetic field on, 630
 power-type, cooling system for, 636
 Ge, with Al electrodes, 1001
 applications and performance limits, 302
 for horizontal-deflection stage, 306
 increasing efficiency of, 978
 techniques for improving, 2769
 selective etch Thermistors, circuits using, design for, 40 for compensation of resistance and conductance, 721 for deriving linear temperature-control voltage, 2489 for u.h.f. power measurements, design of mounts for, 564 Thermocouples, radiation, noise in, 1653 Thermoclectric effects, (See also Semiconductors) in Bi, Sb, Te and Bi-Te, effect of oxide impurities on, 2315 in grey Se, 1272 Peltier heat pump, theory of, 2906 for refrigeration, theory of, 3449 at very low temperatures, 2529

- at very low temperatures, 3529 Time, (See also Clocks) interval measurement, by vernier technique, 3418 standards, atomic and astronomical, variation in speed of earth's rotation in terms of Cs resonance, 1301 Timebases, linear, using Miller integrator and Puckle flyback circuits, 743
- Puckle flyback circuits, 743 Transducers, differential-transformer, 557 electroacoustic, calibration for operation under increased pressure, 330 distributed-type, 673 equivalent circuits for transient vibrations, 3904 frequency-sensitivity characteristics by spectral analysis of thermal noise, 3906 signal/noise performance of strip arrays, 2 for underwater use, 2445 electrochemical, 'solion', current integration with, 2023

 - 2023

- Transducers, electromechanical, stroboscopic method for frequency response of, 2079 piezoelectric, piston-type, operating in water, 1045 theory of, 672 Transductors, (See also Amplifiers, magnetic) auto self-excited, analysis of, 1791

Transistors, Si, temperature dependence of . mobility and lifetime in, 3150 small-signal parameters for, variation of, 995 stabilization, calculations for, 2051 of gain over wide temperature range, 4231 using negative-temperature-coefficient resistors, 2052 surface-broging height absence in the state

- stabilization, calculations for, 2051

 of gain over wide temperature range, 4231
 using negative-temperature-coefficient resistors, 2052

 surface-barrier height changes in, method of studying, 633
 surface-effect immunity in, structure giving, 4230
 structure-determined gain-band product of, 997
 switching parameters, 723
 switching type, 'deplistor', 2420
 Si, p-n-p-n, 3883
 for telephone service, 2778
 theory of, 1401
 with thyratron characteristics, and related devices, 1606
 'thyristor', high-speed, 1005
 with tungsten point in collector, 2777
 3-terminal, 2046
 temperature distribution in, 3149
 termology and notation, revision of, 1008
 tetrode-type, characteristics, applications and construction of, 3152
 field-effect, 2779
 h.f., grown-junction, Si, theory, characteristics and applications of, 3516
 thermal equivalent circuit for, 1720
 thermal equivalent circuit for, 1720
 thermal stability criteria, 1713
 transient response of, calculations for, 2050
 transit-time analysis of, stored-charge method for, 2417
 unfied representation for, 2050
 transiston lines, (See also Cables; Waveguides)
 coil-loaded, phase and group delay in, 698, (D)3193
 delay, interdigital, dispersion in, 1022
 lumped-parameter, linear, construction technique for, 697
 surface-wave propagation conditions along, 696
 with distributed conductance, for e.m. wave absorption, 1068
 equivalent circuit for exponential, for impedance matching, 1070
 helios, circe diagram for, 2460
 measurements, logarithmic chart for evaluation of, 2702
 mutiple, theory of, 2458
 pulse, mus, propagation constants of, 362
 return loss of, 12
 surface-wave, cylindrical, power radiated from, 2098
 excitation of radiation by discont

Surface wave, cylinarical, power radiated non, 2098
 excitation of radiation by discontinuity on, 2097
 Goubau-type, tests on, 10
 impedance measurement method, 1069
 surface-wave-propagation theory for stratified medium, 939
 2-wire, balanced, screened, characteristic impedance of, 3928
 Transmitter-receivers, for outside broadcasts, f.m., 80-W, 4204
 Transmitters, (See also Television)
 a.m., class-C output stage for, 624
 broadcast, automatic monitoring system for, 1397
 combined operation of, using bridged-T network, 623

combined operation of, using bridged-T network, 623
common-channel operation of, synchronization techniques for, 4224
uni.f., eonmon-channel common-program operation of, 1690
network in Württemberg, 1692
s.w., 100-kW, Type-SO2 204/00, 293
f.m., renote control and change-over equipment for, 292
h.f., 60-kW r.f. power amplifier for, 290
linear-amplifier, for independent-sideband operation, 291
sea-resoue, 2-Mc/s, with ferromagnetic aerial, 4223
s.s.b. and i.s.b., rating of, 3503
telegraphy, Post Office, at Ongar, 3142
v.I.f., c.w., for inonspheric investigation, using power-line aerial, 3873
W/T, below 50 Mc/s, I.R.E. Technical Committee report on test methods, 1396
500-kc/s, 4-W, using transistors, with automatic keying, 3504
roposphere, (See also Atmosphere; Wave programmer em)

Troposphere, (See also Atmosphere; Wave propagation, e.m.) climatology of radio ducts, 4053 radio echoes from invisible objects in, 2240 refractive index of, models for, 2725

Tuners, permeability, 1678 Tuning indicators, electron-beam, Type-EM84, for voltage indication, 2073

Ultrasonics, (See also Absorption; Scattering; Transducers)
 applications, to high-fidelity video recording on film, 931
 diffraction of light by, 678, 1751
 distortion of small-amplitude waves in liquids, 2814
 field due to piston-type resonator in liquids, 1423
 generators, electrostrictive, electrode deformation in liquids, 2812
 interference filters, variable-frequency, 677
 interference to field, quartz probe for, 1752
 measurement of field, quartz probe for, 1752
 measurement of velocity, pulse technique for
 metals with low attenuation, 2449

Electronic & Radio Engineer

- Ultrasonics, measurement of velocity and elastic moduli at high temperature, 2815
 research at N.P.L. of India, 3177
 velocity, in liquids under pressure, pulse measurement of, 1
 in water near freezing point, 2811
 waveform determination by light refraction, 1050, 3538
 wave true underschilding technicute for emission

 - wave-train synchronizing technique for equipment testing, 3064
- Vacuum technique, 'clean-up' effect, hypotheses for, 2986
 getter-ion pumps, theory and design data for, 1899 Ti, 1204, 1205
 getters, Ba film, 2613 Ti, 4074

- grades of vacuum in electron and ion tubes, 2262 measurements of gas evolution or sorption of anode materials, 2985
- measurements of gas evolution or sorption of anode materials, 2985
 Valves, (See also Cathode-ray tubes; Electron beams; Rectifiers; Transistors) amplifier, general analysis for transistor, triode and beam-deflection types, 2041 for wide-band operation, data for, 1032 construction of, trends in, 2793 cooling techniques, 4252 'vapotron', 654 crystal, and associated equipment, data on, 3592 diffusion techniques, for, 184 production techniques, development of, 294 review and characteristics of, 3147 crystal-diode, analogue-computer determination of design data, 3508 avalanche effect for generation of sub-mm waves, 3875 circuit representation and pulse method of voltage division for, 2035 d.c. characteristics of, 2410 Ge, annealing of radiation-induced 1/f noise in, 298

 - 298 manufacture of, 1709 as mixers, noise at low temperatures, 3876 new types and applications of, 994 noise temperature ratio variation with temperature, 627 Russian GD-Ts type, blocking junction process in, 1708 time-lag in, 2767 Ge and Si, tests for r.f. noise in, 3507 Ge-In-Sb, diffusion-type, for mµs switching, 3144 hole storage in, 'turn-on' and 'turn-off' times for, 626
 - nozo inductive behaviour under high ioads, 2036 influence of adjacent connections on character-istics of, 1398 logarithmic characteristic of, test method for, 2038

 - 2038
 microwave, mixer-type, with improved conversion efficiency, 2414
 recent developments, 3877
 nonlinear-capacitance, for frequency conversion, 3145
 PbS, *I/V* characteristics of *n-p* contacts on galena, 3874 *p-n-p-m*, as 2-terminal switches, or the potential optical o
 - point-contact, d.c. and a.c. characteristics of,
 - 3143 effect of geometrical factors on characteristic of, 2411

 - or, 2411 electron-hole transition in, 185 GaAs, for u.h.f. applications, 1710 Ge, current noise of, 3506 Ge and Si, characteristics and manufacture of, 296
 - semiconductor-semiconductor 'point contact',

 - semiconductor-semiconductor 'point contact', 2037
 shot noise in, 2413
 Si, construction and properties of, 297
 as voltage-reference devices, 2039
 switching-type, from plastically deformed Ge, 2412
 tunnel-type, for h.f. applications, 3505
 phonon processes in, 4226
 'variode', for gating and control circuits, 4225
 V/I characteristics of, 625
 Zener-type, list of inaufacturers and applications of, 1711
 diode, coaxial-type, for microwave detection, 2794
 as noise generator for u.h.f., 3533
 planar, reference-type, for test purposes, 4253
 saturated, surface structure of filaments in, 1418
 space-charge neutralization by ions in, 2432
 as thermionic energy converters, 324, 325, 2434, (D)2435
 diode and triode, space-charge, shot noise in, 2436
 double-triode, Type-PCC88, characteristics and application forcascodecircuit, 655
 electron-beam, amplifier, noise due to cathode in, 1023
 using beam of flat elliptical cross-section, 3887

 - 1023 using beam of flat elliptical cross-section, 3887 crossed-field, noise in, 313 current and velocity fluctuations at potential minimum, 320 defocusing system for microwave detection, 1413 design of transition region for, 1017 energy relations in, 4245 equations of space-charge flow, 3886 focal length of diaphragm for, 1416 'helitron' oscillator, 319 interception noise in, 3165 magnetically focused, current distribution in, 644

 - magnetic 644

 - 644 noise in, effect of electron lenses on, 1726 mechanism of reduction of, 1727 reduction by low-potential drift region, 1728 for parametric amplification, 1025 by pumping of fast space-charge wave, 1412 parametric-amplifier, 321
- Electronic & Radio Engineer

Valves, electron-beam, parametric-amplifier, cavity-type, 2066 design of couplers for, 2067 with transverse modulation, 4247 as parametric amplifier and frequency converter, 2065

× ...

* + _ . .

Valves, travelling-wave. slow-wave structures for mm and sub-mm λ , 1743 survey of, 1019 theory of electron waves in periodic structures for, 1738 theory of electron waves in retarding systems of, 2062 x b f camplifer and oscillator 1024

2062 v.h.f., amplifier and oscillator, 1024 triode, disk-seal, transmitting-type, for frequencies up to 900 Mc/s, 2797 Type-2040, influence of penetration factor fluctuations on conductance of, 2437 for 4.-kMc/s amplifier, 2798 pin-type, Type-PC86, for bands IV and V, 2796 for r.f. heating, class-C operation of, 1033 intermittent use of, 2071 as oscillator with.variable load, 2795 output power as function of load resistance, 2072 Type-26251, for low-noise operation up to

2072 Type-A2521, for low-noise operation up to 1 kMc/s, 1419 u.h.f., thinble, Type-7077 and 'Nuvistor', 3534 v.h.f. and u.h.f., 20 years' development of, 641 Vibrations, measurement of, reciprocity method for,

of membranes and resonators, variation of natural frequency with load, 1039 Voltage, peak, measurement for h.v. pulses, 920

Wave propagation, acoustic and e.m., analogous effects in, 3249

 analogy of boundary-value problems in, 4008
 fluctuation distribution near focus of lens, 4027
 guided, in slowly varying medium, 2204
 in rough ducts, 2919

 Wave propagation, e.m., (See also Diffraction; Reception; Scattering; Television; Transmission lines; Waveguides; Waves)
 in air-earth-ionosphere cavity, 1338
 angle-of-arrival measurements in, crossed-loop method for, 1664
 attenuation and velocity of transients and triangular pulses in conducting media, 2916
 back-scatter measurements by space-separation

angular pulses in conducting media, 2716 back-scatter ineasurements by space-separation method, 3843 echoes observed on sea swell at Casablanca ionospheric sounding station, 2724 fading in, relations between bearing and amplitude, 947

ionospheric sounding station, 2724
 fading in, relations between bearing and amplitude, 947
 ground-wave, comparison of Millington's method and equivalent-numerical-distance method with theory of, 2375
 of pulse from damped current source, 3842
 transient, over spherical earth, 239
 group velocity of damped vaves, 1848
 in inhomogeneous media, 771
 ionospheric, absorption, index from analysis of field-strength recordings, 2732
 of sky wave, graphical determination of, 1341
 validity of theorems for, 1669
 analysis of signal-pattern drift in, 1884
 during annular eclipse, 2730
 between Australia and Europe, analysis of observation in relation to predictions, 2727
 back-scatter sounding for skip-distance determination, 1340
 disturbance warnings, inprovement of, 116
 during disturbance 11th Feb. 1958, 573
 F-layer scatter observations in Far East, 2733
 Fr-layer multiple reflections, focusing effects as cause of, 1342
 forecasts for, comparison of, 1339
 prediction techniques for high latitudes, 2729
 frequency variation of JJY transmissions, 916
 geometrical properties applied to, 3848
 importance of F₁ layer in oblique-incidence transmissions, 2378
 I.f., analysis for, 4179
 mode expansion for, 4178
 numerical solutions of equations for, 3455
 over long distances, possible explanation for, 942
 pulse experiment at 20-1 Mc/s, 240
 via single F hop, 943
 magneto-ionic fading in vertical-incidence pulsed transmissions, 944
 magneto-ionic fading in vertical-incidence pulsed transmissions, 945
 nonlinear interaction effects in, 3847
 considering plasma layer bounded by dielectric, 1996
 polarization fading over o

polarization fading over oblique-incidence path, 1668 ray path calculations for, 2377 reciprocity tests, 1667 reflection conditions for vertical sounding, 2728 reflection in stratified medium with weak irregularities, 2250 refraction irregularities at 4 m λ , 2251 round-the-world echoes, 1343 by scatter, amplitude and phase characteristics related to Gaussian noise, 583 during auroral disturbance, 2001 due to electrodynamically controlled turbu-lence in, 4060 due to equatorial sunset effect, 3461 importance of metor activity in, 1344 under influence of ion production, 4059 scattering cross-section for turbulent fluctu-ations, 236 self-demodulation and self-distortion in, 2252 signal bearing variations due to irregularities and aurora, 1998 test between Ascension Island and Slough, 2376 u.h.f., during annular eclipse, 2739 between U.K. and Japan, 3453 variations in direction of arrival, 941 v.h.f., refraction effects in satellite tracking, 3698

v.h.f., refraction effects in satellite tracking, 3698

I.49

3178

- retarding system with helix in dielectric, analysis of, 3889
- space-charge-wave excitation for Brillouin flow, 1735
- 1735 space-charge waves in, 2058 surface-wave electron velocities in magnetic field, 2786 v.m., generation of second harmonic in, 1409 sctron oscillations due to transit-time effects in, 4251 schemenic in effect of esthede percenty on 1028
- electron
- 4251
 flicker noise in, effect of cathode porosity on, 1028
 gas-filled, cold-cathode, tetrode, effect of trigger pulse polarity on anode breakdown time, 3174

 - 3174
 triodes for switching, 2443
 as noise source, for cm λ, measurements on, 658
 u.b.f., helix-coupled, 559
 stabilizer, neon-argon-type, effect of argon content on, 2442
 'Störmertron', for simulating solar proton streams, 1864
 thyratron ceramic for high-nower radar, 3535
- thyratron, ceranic, for high-power radar, 3535 grid emission in, properties of Ti for preventing, 1030
- for guided missiles, development of, 310 klystron, energy distribution of electrons in, 2424 frequency control by magnetic amplifiers and transistors, 1737 high-power, pulsed, design of, 1410 low-power, water cooling system for, 312 multicavity, effect of beam coupling coefficient on wide-band operation of, 1015 multigap, 2785 pulse-modulated beam current for mixer operation, 1016 reflex, linearization of f.m. characteristic of, 1739 Type-TK7, 1730 wide-range tuning cavities for, 3525 as 11-kMc/s negative-resistance-type amplifier, 1741 resonant-cavity design theory 3890

- 1741
 resonant-cavity design theory, 3890
 2-cavity, ballistic analysis of, 1729
 magnetron, a.c.-operated, advantages of, 3161
 current limitation by inductance, 3162
 cut-off characteristics of, 2057
 c.w., 2·5-kW, Type-7091, 4244
 diffusion theory of, 645
 ferrite-tuned, 3163
 mm-λ, development of, 4248
 planar-diode, space-charge-limited current in, 1018

 - 1018
 - pulser design for, 648 reflex-type, with voltage control of frequency, 3528
- 3528 single-anode, diffusion theory for, 646 space-charge theory, considering electron scat-tering, 3160 electronic conductance in, 2425 split-anode, diffusion theory for, 647 manufacturing techniques, 3523 measurement method for mutual conductance, 3059 microminiature, heaterless, for modular circuit construction, 2863 microphony in, analysis of, 1013 effects of, 3896 microwave, output window. design of broadband

- construction, 2863 microphony in, analysis of, 1013 effects of, 3896 microwave, output window, design of broadband matching for, 643 review of construction techniques, 4243 survey of, 2784 wide-band, new developments in, 642 receiving-type, circuit effects of faults in, 311 formula for mu of, 3170 with rectangular envelopes, theoretical comparison with cylindrical forms, 3531 shape, comparative study of different forms, 3895 subminiature, vibration tests for guided-missile applications, 2431 switching, trochotron, 1724 transit-time, strophotron-type, for u.h.f., 1725 travelling wave, amplifier, C- and L-band, design and characteristics of, 2063 backward-wave, using helical electron beam in unloaded waveguide, 3164 minimum-noise conditions in, 1734 as mm-A voltage-tuned oscillator, 3529 M-type carcinotron, electron trajectories in gun of, 318 oscillator, 20-40 kMc/s, 1742, 29-74 kMc/s, 1740 with ridge-loaded ladder circuit, 2790 'coupled-mede' theory of, coupling coefficients in, 1014 coupled-resonator slow-wave structures for, 650 crestatron, 2427 with crossed-field periodic structure, field theory for, 1731 dispersion of interdigital delay line in, 1022 efficiency of, effect of collector potential on, 314 electrostatically focused, 1414 experimental electron gun for, 2064 gain and stability of, effect of attenuator surface on, 1411 helix.type, for 48 kMc/s, 1415 hybrid-type, for pulsed amplification, 1733 leakage flux around focusing magnet for, analysis of, 315 nonlinear theory of, 2426 O-type, effect of double beams in, 317 O-type and M-type, spread of electron velocities

of, 315 nonlinear theory of, 2426 O-type, effect of double beams in, 317 O-type and M-type, spread of electron velocities and bandwidth of, 316 with periodic circuits, characteristics of, 1732 periodically loaded, wave matrix treatment of oscillations in, 1020

- Wave propagation, e.m. ionospheric, v.h.f. scatter, solar-cycle influence on, 130
 v.l.f., mode theory confirmation from spectra of atmospherics, 3094, 3313
 phase stability deduced from waveguide mode theory, 2735
 using power-line aerial, 1672
 17-kc/s, 'whistler-mode' echoes remote from conjugate point, 2731
 over irregular terrain, 2723
 in isotropic and crystalline media with spatial dispersion, 1169
 l.f., in arctic areas, 4182
 in glaciers, 1994
 influence of ridge on, 233
 in medium with random inhomogeneities, effect of receiver focusing system on field fluctuations, 4031
 in medium with spatial dispersion, 2921

 - in medium with spatial dispersion, 2921

 - nonreciprocal, in ionized gas, 2541 in plasma in magnetic field, with spatial dispersion, 1166
- in plasma in magnetic field, with spatial dispersion, 1166
 pulse, around earth, 1662
 in medium with dielectric losses, 2208
 and radiation problems, physical description and analogies for, 4025
 reflected wave from moving object, characteristics of, 410
 reflection, from auroral ionization, 1670
 geometry of, 1671
 from satellite-produced ionization, 2963
 by scatter, aerial-to-medium coupling loss, 235
 from low-density meteor trails, 1665
 from meteor trails, direction of arrival of long-duration echoes, 1993
 from random inhomogeneities, 414
 role of turbulent mixing in, 3088
 scattering, by free electrons in and above atno-sphere, 451
 of surface wave by reactance discontinuity, 3844
 by turbulence, theory of, 1660, 1661

- of surface wave by reactance discontinuity, 3844 by turbulence, theory of, 1660, 1661 scattering matrix for echoes through intervening ionosphere, 1345 statistical theory for medium with random fluctuations over conducting plane, 3840 surface-type, Sommerfeld treatment of, 1334 over stratified ground, 939 system loss, 4174 theory for inhomogeneous path, 3841 transmission loss due to aerial environment, 1999 tropospheric, airborne research work on, 2726 climatology of ground-based ducts, 4053 diffraction by earth's curvature in, 3092 diffraction by mountain ridges, 243 diurnal influences for path near Persian Gulf, 1337 fading due to scattering by dielectric turbulence,

- fading due to scattering by dielectric turbulence, 3450

- rading due to scattering by dielectric turbulence, 3450
 at great heights, theory for nonstandard atmosphere, 1336
 mechanism for different scattering surfaces in atmosphere, 2379
 polarization rotation in, 3451
 refractive-index, models for, 2725
 synoptic variation, 4177
 by scatter, Australian tests, 3452
 calculation of multiple dispersion in, 1995
 geometric characteristics, 571
 theoretical research in U.S., 3846
 transhorizon, 1663, field-strength relations for, 570
 tests in U.S.A., 234
 h.f., aperture-to-medium coupling on line-of-

I.50

- tests in 0.5.A, 234 u.h.f., aperture-to-medium coupling on line-of-sight paths, 4183 through array of parallel metallic plates, 94 attenuation by rain at 8-6 mm λ, 4187 attenuation and rainfall data for 11-kMc/s relay, 1673, 2381
- attenuation and rainfall data for 11-kMc/s relay, 1673, 2381 diffraction by mountains, 3458 effect of cloud layers on field strength, 4186 foreground terrain effects in, 3457 in Italy over 196-km path, 2002 long-distance, path loss over 864 km, 244 over Mediterranean at 10 cm λ , 940 mm- λ , absorption over extended ranges, 246 optical techniques for, 2099 phase stability measurements, 4176 over rough terrain and sea surfaces, 4184 by scatter, over English Channel, 578 measurements at 250 Mc/s related to metarological data, 3096 transhorizon, wavelength-dependence in, 1666 at 468 Mc/s over 289-mile path, 245

- Wave propagation, over sea, in Denmark, 579 over sea surface, 242 phase fluctuations in, 2738 transhorizon, aerial-beam distortion in, 1347 bandwidth measurements, 3459 distance dependence, fading and distortionor, 3090 3090
 - 3090
 rapid-beam-swinging measurements, 3198
 over sea path, 2734
 over 171-mile land path, 4185
 490-Mc/s, transmission loss related to tropopause height, 3097
 13-kMc/s, analysis of field-strength recordings, 3095

 - 3095 2-KMC/s, prolonged fade-out on short path, 3098 2 300-MC/s, disturbances on 'just-below-horizon' path, 3091 velocity measurements, 2190 velocity modulation in dielectric medium, 2207
- velocity modulation in dielectric medium, 2207
 v.h.f., abnormal absorption of cosmic noise at 30 Mc/s, 2380
 back-scatter from sea in anomalous television reception, 577
 field-strength measurements, near Berlin, 2740
 e.m., v.h.f., field-strength measurements, over nonuniform terrain in East Germany, 3456
 influence of moisture, temperature and terrain on, 3089
 long-distance, due to E, and F layers and troposphere, 2003
 role of turbulent scattering in, 575
 long-range reception of television signals, 574
 by scatter from overdense meteor trail, 576
 in towns, 3850
 transhorizon, field-strength measurements of, 2737
- 2737 v.l.f., long-distance, waveguide-mode analysis of, 948
- phase stability measurements for radux-omega system, 2736
- Waveform, recording, using homodyne detector, 3065
- by stroboscopic methods, 1650, 2357 sampling comparator, 919

- Samping cultor, 919
 Waveguides, (See also Transmission Lines) assemblies, integrally constructed, design and testing of, 2826
 attenuators, ferrite-type, medium-power, 2468
 bends in, propagation around, 2106
 circular, with absorbing walls, attenuation of, 3194
 containing ferrite rod, propagation constants, 341 341

 - 341 containing gyromagnetic media, mode spectra, 2838 effect of diaphragms and corrugations in, 1075 ferrite-loaded, as delay device, 2116 perturbation method for propagation co-efficient, 2836 loaded with paramagnetic salt, rotation of plane of polarization in, 776 for long-distance transmission, 2107
- circular and elliptic, attenuation measurements, 2829

- 2829 circular and elliptic, attenuation measurements, 2829 circulators, ferrite, low-loss, L-band, 1769 1-kW, X-band, 1079 using semiconductor Hall effect, 15 3-port, using Hall effect, 2113 4-port, 2832 coaxial, low-reflection junctions for, 1073 coiled, as delay-line, 339 couplers, directional, comparison of, 3936 end sections for matching, 1083 long-slot, 2112 measurement of directivity of, 3821 wide-band, interference-type, 705 and multimode measurement techniques, 3935 multiple-branch, 3559 hybrid ring as, 2465 variable-ratio power divider and multiplexer, 1078

- 1078 curved, fundamental modes in, 3929 dielectric, image-type, 2827 characteristics at mm λ , 3930 dielectric-loaded, field distribution in, 3940 propagation of orthogonal dominant modes in, 1081

World Radio History

- 1081 elliptic, characteristic impedances of, 702 ferrite-loaded, analysis for, 3933 ferrite-loaded, high-power effects in, 3937 as microwave limiters, 3943 phase-shift calculations for, 2115 for phase shifting, 1771 propagation in, 707, 1770 thermal effects in, 3938 filters, band-pass, design of, 3939 cavity-type, ferrite-loaded, 2467 ferrite-type, 2466

- Waveguides, high power, **3562** high-Q, design theory, **3561** multistage, formulae for, **53** theory of wire-grid transmission loss for, **3963** helix-type, curved, attenuation of TE₀₁ wave in, **704**
 - influence of dielectric on phase constants for, 2100
 - in magnetic-dielectric medium, resonance in, 2464
 - mode conversion at junction with copper pipe, 3932
- theory and application of, 703 irregular, critical cross-sections in, 699 irregularities in, reflection and scattering from, 1766

- Hregular, critical cross-sections in, 699
 irregularities in, reflection and scattering from, 1766
 isolators, ferrite, design for magnetron, 11
 field-displacement, analysis for, 2839
 resonance-type, high-power, L-band, 3563
 for 70 kMc/s, 1439
 junctions, hybrid, 3560
 matrix representation of, 2139
 stepped, frequency compensation technique, 1077
 transformation of admittance using variable
 reactance and phase shifter, 2111
 loaded, with attenuating foil, 1772
 evaluation of equivalent-circuit parameters by
 field measurement, 340
 for low-temperature cryostats, 1767
 manufacture of components for, electroforming
 process for, 1436
 frozen-mercury process for, 3553
 techniques for, 700
 for mm waves, 2463
 mode transducer, centre-excited, 2831
 obstacles in, anisotropic, theory of, 706
 phase-shifter, ferrite-type, 'serrodyne' modulator
 for frequency translation, 3942
 for 200-800 Mc/s, 3941
 phenomenological theory for, 2837
 00° wide-band, 2114
 'plasma cable', with brass outer conductor and
 external magnetic field, 2104
 polarization measurements at 4 kMc/s, equipment
 for, 3564
 propagation in, theory for discontinuous periodic
 structures applied to, 2103
 propagation at sub-inm \u00e0, 2117

propagation at sub-inm A in, analysis of, 13 pulse waveform distortion due to dispersion in, 1071 reflectometer for, rotating-loop, 2117 ring circuits, nonreciprocal, resonance properties of, 2462 scattering in, characteristic functions of wave equation for, 2696 serrated, 1074

Schletet, 1074 stotted, surface-wave launching efficiency of, 2110 step discontinuities in, 14 strip and parallel-plate types, characteristics and manufacture of, 2108 strip-type, characteristic-impedance calculation, 3555

Infanture of, 2106
stip-type, characteristic-impedance calculation, 3555
with coaxial feed, properties of, 2828
directional couplers, 3556
ferrite-filled, propagation in, 2109
high-Q triplate-type, impedance and phase velocity of, 701
optimum dimensions for, 1072
as wide-band balun, 3931
surface-type, dielectric, excitation of, 3558
dielectric-rod, launching efficiency of wires and slots for, 2830
with constant external magnetic field, 1435
reactance calculation for, 357
switches, Faraday-rotation, for TH system, 2835
fast, for 70 kMC/s, 2834
high-power duplexer, 2833
switches and branching networks, comparison of different types, 1080
tapered, reflections in, 1768
terminations, with film-type resistors, 1082
trough-type, cut-off wavelength of, 3554
wave equation for, asymptotic integration of, 2461
Vavemeters, (See also Frequency, meters)

Wavemeters, (See also Frequency, meters) absorption-type, 1-100-Mc/s, using transistors, 1979

1979 microwave, cavity-type, cylindrical, 3066 Waves, (See also Diffraction; Sound; Ultrasonics) growing, kinematics of, 1849 space-charge and e.m., growth in moving ion streams, 3267, 4030

Electronic & Radio Engineer

Wire, U.S. specifications and codes for, 3046

ERRATA

IN ABSTRACTS AND REFERENCES 1959

Abstract No.	
515	Change U.D.C. number to 537.311.33 : 535.215
1052 1529	For 'F. A. Vaniar' read 'F. A. Veniar' In line 5, for 'auroral' read 'annual'
1824	In line 7, for 'frequency band' read 'energy band'
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2113	In line 4, for 'three-part' read 'three-port'
2159	In line 7, for 'joints' read 'points'
2278	In title, for 'Electric' read 'Elastic'
2408	In line 7, for '605-line' read '625-line'
2669	For 'S. Asanabo' read 'S. Asanabe'
2720	Change U.D.C. number to 621.384.8 537.54
2831	In title, for 'TE° ₁₀ -TE° ₀₁ ' read 'TE° ₁₀ -TE° ₀₁ ' (N') and (N')(m')
2857	In title, for 'm //v' read 'lv'
2958	In line 4, for 'change-exchange' read 'charge-exchange'
3030	In line 5, for 'function' read 'junction'
3136	In line 5, for '3136' read '3138'
3171	For 'W. R. Aitken' read 'W. R. Aiken'
3256	Change U.D.C. number to 538.566 : 535.42
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3836	For 'J. L. Veshaeghe' read 'J. L. Verhaeghe'

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The practice of allocating individual abstract numbers to corrections has been largely discontinued; a list of published corrections noted during 1959 is given below. The journal in which the correction appeared was in each case the same as that in which the original paper was published.

Abstract No.	
3235 of 1955	Jan. 1959, Vol. 14, No. 1, pp. 115–116
1405 of 1957	July 1957, Vol. AP-5, No. 3, p. 313
2959 of 1957	Dec. 1958, Vol. 5, No. 6, pp. 510-513
84 of 1958	Jan. 1959, Vol. 6, No. 1, p. 80
295 of 1958	Sept. 1959, Vol. 36, No. 9, p. 352
971 of 1958	Sept. 1958, Vol. 29, No. 9, p. 1383
1228 of 1958	Dec. 1959, Vol. 47, No. 12, p. 2105
1858 of 1958	April 1958, Vol. 3, No. 30, p. 312
1892 of 1958	April 1958, Vol. 3, No. 30, p. 312
3028 of 1958	Sept. 1958, Vol. 29, No. 9, p. 1383
3271 of 1958	Dec. 1959, Vol. 47, No. 12, p. 2084
3472 of 1958	Dec. 1958, Vol. 18, No. 12, p. 714
3544 of 1958	15th Dec. 1958, Vol. 112, No. 6,
	p. 2139
3890 of 1958	15th Sept. 1959, Vol. 115, No. 6,
	p. 1778
3902 of 1958	15th March 1959, Vol. 113, No. 6,
	p. 1697
3962 of 1958	Dec. 1958, Vol. 46, No. 12, p. 1913
173 of 1959	15th March 1959, Vol. 113, No. 6,
	p. 1696
239 of 1959	July 1957, Vol. AP-5, No. 3, p. 313

337 of 1959 Dec. 1957, Vol. CP-4, No. 4, pp.

	135-137
379 of 1959	Feb. 1959, Vol. 4, No. 37, p. 220
385 of 1959	May 1959, Vol. 4, No. 39, p. 272
501 of 1959	1st June 1959, Vol. 73, No. 474, p. 976
635 of 1959	Oct. 1958, Vol. 17, No. 10, p. 117
745 of 1959	Feb. 1959, Vol. 4, No. 37, p. 220
855 of 1959	March 1959, Vol. 36, No. 3, p. 95 March 1959, Vol. 9, Nos. 3/4, p. 340
890 of 1959	March 1959, Vol. 9, Nos. 3/4, p. 340
1233 of 1959	15th June 1959, Vol. 114, No. 6,
	p. 1652
1368 of 1959	Sept. 1959, Vol. 47, No. 9, pp. 1653-
1000 (1050	1654
1372 of 1959	June 1958, Vol. 2, No. 3, p. 144
1493 of 1959	Dec. 1958, Vol. 17, No. 12, p. 36
1498 of 1959	Feb. 1959, Vol. 4, No. 37, p. 220
1559 of 1959	April 1959, Vol. 47, No. 4, p. 567
1615 of 1959	1st Sept. 1959, Vol. 3, No. 5, p. 244
1693 of 1959	Feb. 1959, Vol. 4, No. 37, p. 220
1795 of 1959	May 1959, Vol. 65, No. 5, p. 232
1952 of 1959	1st June 1959, Vol. 73, No. 474, p. 976
2024 of 1959	Oct. 1958, Vol. 2, No. 5, p. 252
2202 of 1959	15th June 1959, Vol. 114, No. 6,
0400 -61050	p. 1652
2408 of 1959	Aug. 1959, Vol. 36, No. 8, p. 314 July 1959, Vol. 47, No. 7, p. 1252
2410 of 1959	July 1959, Vol. 31, No. 377, p. 427
2503 of 1959	
2750 of 1959 2841 of 1959	Aug. 1959, Vol. 47, No. 8, p. 1324 Jan. 1959, Vcl. AP-7, No. 1, p. 104
3076 of 1959	Jan. 1959, Vol. 16, No. 1, p. 56
3076 of 1959	Jan. 1959, Vol. 16, No. 1, p. 50
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3081 of 1959	Dec. 1996, Vol. 10, No. 12, p. 570
3419 of 1959	Oct. 1958, Vol. 2, No. 5, p. 252 Nov. 1959, Vol. 47, No. 11, p. 1840
3588 of 1959	July 1959, Vol. AP-7, No. 3, p. 251
3965 of 1959	July 1999, Vol. AP-7, No. 5, p. 201

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- Acta Polytechnica Scandinavica, Publishing Office, Box 5073, Stockholm 5, Sweden. (Acta polyt. scand.) Acustica, S. Hirzel Verlag, Stuttgart-N, Germany. (Acustica)
- (Acustica) Advances in Physics, Taylor & Francis Ltd, Red Lion Court, Fleet Street, London, E.C.4, England. (Advances Phys.) Akusticheskil Zhurnal, Moskva, B-64, Podsosenskil per., 21, U.S.S.R. (Akust. Zh.) Akustische Beihefte, as for Acustica. (Akust. Reikefte)
- Beihefte Alta Frequenza, Associazione Elettrotecnica Itali-ana, Milano (202), Via S. Paolo 10, Italy. (Alta Frequenza)
- Frequenza) Annalen der Physik, J. A. Barth, Leipzig C1, Salomonstrasse 18B, East Germany. (Ann. Phys.,
- Salomonstrasse 100, 2007
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 Annales de Géophysique, Service des Publications du C.N.R.S., 13 Quai Anatole France, Paris 7^e, France. (Ann. Géophys.)
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 Applied Scientific Research, Martinus Nijhoff, The Hague, Netherlands. (Appl. sci. Res.)
 Archiv der elektrischen Übertragung, S. Hırzel Verlag, Stuttgart, Germany. (Arch. elekt. Übertragung)
 Archiv für Elektrotechnik, Springer Verlag, Berlin-Wilmersdorf, Heidelberger Platz 3, Germany. (Arch. Elektrotech.)
 Archiv für technisches Messen, R. Oldenbourg KG, München 8, Rosenheimer Str. 145, Germany. (Arch. elekt. Messen)
 Arkiv för Fysik, published for Royal Swedish Academy of Sciences by Almqvist & Wilse'l, Stockholm, Sweden. (Ark. Fys.)
 A.T.E. Journal, Automatic Telephone & Electric Co. Ltd, Strowger Works, Liverpool 7, England, (A.T.E. J.)

Electronic & Radio Engineer

- Audio, Radio Magazines, Inc., P.O. Box 629, Mineola, N.Y., U.S.A. (Audio)
 Australian Journal of Physics, Commonwealth Scientific and Industrial Research Organization, 314 Albert Street, East Melbourne C.2, Victoria, Australia. (Aust. J. Phys.)
 Avtomatika i Telemekhanika, Moskva, I-53, Kalanchevskaya ul., 15a, U.S.S.R. (Automatika i Telemekhanika)
 A.W.A. Technical Review, Amalgamated Wireless (Australasia) Ltd, Sydney, Australia. (A.W.A. tech. Rev.) tech. Rev.)
- tech. Rev.)
 B.B.C. Engineering Division Monographs, British Broadcasting Corporation, 35 Marylebone High Street, London, W.1, England. (B.B.C. Engng Div. Monographs)
 Beama Journal, British Electrical and Allied Manufacturers' Association, 36 Kingsway, London, W.C.2, England. (Beama J.)
 Bell Laboratories Record, 463 West Street, New York 14, N.Y., U.S.A. (Bell Lab. Rec.)
 Bell System Technical Journal, American Telephone and Telegraph Company, 195 Broadway, New York 7, N.Y., U.S.A. (Bell Syst. tech. J.)
 British Communications & Electronics, Hey-wood & Co. Ltd. Drury House, Russell Street, Drury Lane, London, W.C.2, England. (Brit. Commun. Electronics)
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 Bulletin de l'Association Suisse des Électriciens, Seefeldstrasse 301, Zürich 8, Switzerland. (Bull. schweiz elektrolech. Ver.)
- schwerz elektrolech. Ver.) Bulletin of the Technical University Istanbul, Istanbul Teknik Universitesi, Gümüssuyu, Istan-bul, Turkey. (Bull. tech. Univ. Istanbul)
- Câbles & Transmission, Sotelec, 16 rue de la Baume, Paris 8°, France. (Câbles & Transm.) Cabiers de Physique, 165 rue de Sèvres, Paris 15°, France. (Cah. Phys.)

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 Electrical Engineering, American Institute of Electrical Engineers, 33 West 39th Street, New York 18, N.Y., U.S.A. (Elect. Engng, N.Y.)
 Electrical Journal, Bouverie House, 154 Fleet Street, London, E.C.4, England. (Elect. J.)
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 Electronic Applications, N. V. Phili's' Gloeilam-penfabricken, Technical and Scientific Literature Department, Eindhoven, Netherlands. (Electronic Applic.)
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Printed in Great Britain for the Publishers, Iliffe & Sons, Ltd., Dorset House, Stamford Street, London, S.E.I, by Gibbs & Bamforth, Ltd., St. Albans, Distributed in U.S.A. by Eastern News Company, 306 West 11th Street, New York, 14.

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