

TRANSCENDENT 2000 SINGLE BOARD SYNTHESIZER

LIVE PERFORMANCE SYNTHESIZER DESIGNED BY CONSULTANT TIM ORR (FORMERLY SYNTHESIZER DESIGNER FOR EMS LIMITED) AND FEATURED AS A CONSTRUCTIONAL ARTICLE IN ELECTRONICS TODAY INTERNATIONAL.

The TRANSCENDENT 2000 is a 3 octave instrument transposable 2 octaves up or down giving an affective 7 octave range. There is portamento: pitch bending: a VCO with shape and pitch modulation: a VCF with both low and high pass outputs and a separate dynamic sweep control, a noise generator and an ADSR envelope shaper. There is also a slow oscillator, a new pitch detector. ADSR repeat, sample and hold, and special circuitry with precision components to ensure tuning stability amongst its many features.

The TRANSCENDENT 2000 is a 3 octave instrument transposable 2 octaves up modulation a VCF with both low and high pass outputs and a separate dynamic detector ADSR repeat sample and hold and special circuitry with precision cor. The kit includes fully finished metalwork fully assembled solid teak cabinet. If liter sweep pedal professional quality components (all resistors either 2% metal oxide or ½½ metal trim¹) and it really is complete — right down to the last nut and bolt and last piece of wirel. There is even a 13A plug in the kit — you need buy absolutely no more parts before plugging in and making great music! Virtually all the components are on the one professional quality fibreglass PCB printed with component locations. All the controls mount directly on the main board all connections to the board are made with connector plugs and construction is so simple it can be built easily in a few evenings by almost anyone capable of neat soldering! When finished you will possess a synthesizer comparable in performance and quality with ready-built units selling for between £500 and £700!

COMPLETE KIT ONLY £168.50 + VAT!

Comprehensive handbook supplied with all complete kits! This fully describes construction and tells you how to set up your synthesizer with nothing more elaborate than a multi-meter and a pair of early.





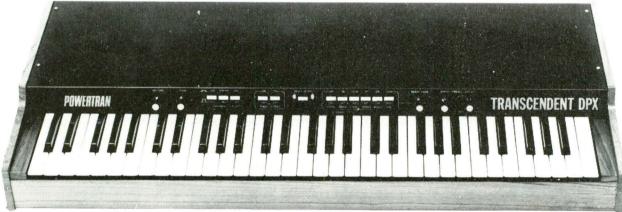
Cabinet size 24.6" x 15.7" x 4.8" (rear) 3.4" (front)

INCREASED CAPACITY AT OUR BIG NEW FACTORY MEANS MANY PRICES DOWN! ALL OTHERS FROZEN!

TRANSCENDENT DPX

DIGITALLY CONTROLLED, TOUCH SENSITIVE, POLYPHONIC, MULTI-VOICE SYNTHESIZER

The Transcendent DPX is a really versatile new 5 octave keyboard instrument. There are two audio outputs which can be used simultaneously. On the first there is a beautiful harpsichord or reed sound — fully polyphonic i.e. you can play chords with as many notes as you like. On the second output there is a wide range of different voices. Still fully polyphonic. It can be a straightforward piano or a honky tonk piano or even a mixture of the two! Alternatively you can play strings over the whole range of the keyboard or brass over the whole range of the keyboard or should you prefer — strings on the top of the keyboard and brass at the lower end (the keyboard is electronically split after the first two octaves) or vice versa or even a combination of strings and brass sounds simultaneously. And on all voices you can switch in circuitry to make the keyboard touch sensitive! The harder you press down a key fiel louder it sounds — just like an acoustic piano. The digitally controlled multiplexed system makes practical touch sensitivity with the complex dynamics law necessary for a high degree of realism. There is a master volume and tone control, a separate control for the brass sounds and also a vibrato circuit with variable depth control together with a variable delay control so that the vibrato comes in only after waiting a short time after the note is struck for even more realistic string, sounds.



Cabinet size 36.3" x 15.0" x 5.0" (rear) 3.3" (front)

COMPLETE KIT ONLY £299.00 + VAT!

To add interest to the sounds and make them more natural there is a chorus ensemble unit which is a complex phasing system using CCD (charge coupled device) analogue delay lines. The overall effect of this is similar to that of several acoustic instruments playing the same piece of music. The ensemble circuitry can be switched in with either strong or mild effects.

As the system is based on digital circuitry digital data can be easily taken to and from a computer (for storing and playing back accompaniments without pitch or key change computer composing etc. etc.) and an interface socket (25 way D type) is provided for this purpose

Although the DPX is an advanced design using a very large amount of circuitry, much of it very sophisticated, the kit is mechanically extremely simple with excellent access to all the circuit boards which interconnect with multiway connectors, just four of which are removed to separate the keyboard circuitry and the panel circuitry from the main circuitry in the cabinet

The kit includes fully finished metalwork, solid teak cabinet professional quality components (all resistors 2 % metal oxide) nuts bolts etc. even a 13A plug — you need buy absolutely no more parts before plugging in and making great music! When finished you will possess an instrument comparable in performance and quality with ready-built units selling for over £1 200

POWERTRAN

ORDERING INFORMATION AND MORE KITS ON PAGE 8

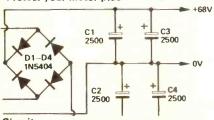
All kits also available as separate packs (e.g. P.C.B. component sets hardware sets. etc.)
Prices in FREE CATALOGUE

INTERNATIONAL APRIL 1980 Vol 9. No 4



A complete budget system p.44









FEATURES

DIGEST **ANALOGUE SWITCHES** DESIGNERS NOTEBOOK **AUDIOPHILE**

CIRCUIT SUPPLEMENT MICROFILE

RAVEN ON TOMORROW'S OFFICE

- 9 And now the good news
- 18 Taming analogue signals
- 34 Touching technology
- 44 Sounds peculiar
- 55 16 pages of goodies
- 82 New machines on view
- 92 Chinese style
- 96 Crystal balls at the ready
- TECH TIPS 103 More of your ideas

PROJECTS

RADIO CONTROL FAIL—SAFE BATTERY CHARGER CAR SECURITY DEVICE

300W AMPLIFIER MODULESS M More power to your elbow

28 A DIY guardian angel

39 Automatic charging 50 Alarming possibilities

TOUCH DIMMER 87 The dimmer with a difference

INFORMATION

ETI MAY

17 It certainly will

MARKETPLACE

37 Your bargain basement

SPECIALS

54 A few extra this month

ETI PRINTS

81 Rub down a PCB

CT MAY

95 The Hobby future

ETI 1999 101 A very SPÉCIAL special

BOOK SERVICE 109 Technical tomes

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ELECTRONICS & TIME CENTRES

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6 digit, 11 functions, Hours, mins., secs., day, date, day of week, 1/100th, 1/10th, secs., 10X secs., mins. Split and lap modes. Back-light, auto calendar. Only 8mm thick. Stainless steel bracelet Also available

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М9

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mode, Alarm test, Chronograph, lap time, stop watch 1/10

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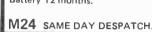
M22 SAME DAY DESPATCH.



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81CS - 36B
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M25 SAME DAY DESPATCH.



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CASIO F-8C 3 year battery life

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Accuracy 15 secs: per month.

Battery life approx. 3 years.



Price only M36 SAME DAY DESPATCH. £10.95

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Price only SAME DAY DESPATCH. £79.95 M10 including POST & PACKING SEIKO DIGI-ANA **CHRONOGRAPH**

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POLYESTER CAPACITORS: Axial lead type. 400v: Inf. In5. 2n2. 3n3. 4n7. 6n8. 10n. 15n 9p; 18n 150n. 220n 24p; 330n. 470n 41p; 680n 48p; 1µF 64p; 160v: 10n6. 12n 39n. 100n. 150n. 220n 11p. 330n. 47	2μ2 82p.		AF115 AF116 AF117 AF118 AF139	60 E 50 E 76 E	CY40 CY42 CY70 CY71 CY72	48 14 14 16 158	MD8001 MJ491 MJ2955 MJE340 MJE370	179 175 105 54 58	TIS43 TIS44 TIS45 TIS46 TIS88	30 45 45 45 45 35	2N3053 19 2N3054 55 2N3055 48 2N3108 32 2N3442 140
1000V: 10n, 15n 20p; 22n 22p; 47n 26p; 100n 38p; 47 POLYESTER RADIAL LEAD CAPACITORS: 250V: 10n, 15n, 22n, 27n 5p; 33n, 47n, 68n, 100n 7p; 150n 1	On 53p; 1 µ F 175p. Op; 22On,	ULTRASONIC TRANSDUCERS	AF178 AF186 AF239 ASZ21	75 B 50 B 42 B	0124 D131 D132 D133	115 42 42 50	MJE371 MJE520 MJE521 MJE2955	54 65 74 90	TIS 90 TIS 91 ZTX 107 ZTX 108	20 24 11 11	EN3663 14 2N3702 10 2N3704 10 2N3705 10
330n 13p: 470n 17p: 680n 19p; 1 µ 22p; 1 µ 5 30p; 2 µ 2 ELECTRONIC CAPACITORS: (Values are in µF) 500v: 1 1.5, 2 2, 3.3, 4.7, 6.8, 8p; 47, 32, 11p; 63, 100, 27p;	0 40p; 47 68p; 250V: 10 50V: 50, 100, 220, 25p	470 32n: 1000 60n:	BC107 BC1078 BC108 BC108B	10 B	D135 D136 D137 D138	30 30 30 35	MJE3055 MPF102 MPF103 MPF104	70 66 36 36	ZTX109 ZTX300 ZTX301 ZTX302	11 13 16 20	2N3706 10 2N3707 10 2N3708 11 2N3709 11
40V: 22, 33, 8p; 100, 12p; 2200, 3300, 85p; 4700, 98 25V: 10, 22, 47, 80, 100 8p; 160, 220, 250, 15p; 470 2t 3300, 77p; 4700 85p; 16V: 10, 47, 7p; 100, 125, 8p; 2 36p; 10V: 100, 7p; 640, 12p; 1000, 16p.	ip; 640, 35 p; 1000, 33 p; 20, 330, 14 p; 470, 20 p;	1500, 40p ; 2200, 45p ; 1000, 1500, 30p ; 2200	BC10BC BC109 BC109B BC109C	12 E	D139 D140 D144 D145	30 30 198 175	MPF105 MPF106 MPSA05 MPSA06	36 40 15 16	ZTX303 ZTX304 ZTX314 ZTX326	25 17 24 45	2N3710 10 2N3711 10 2N3771 179 2N3772 195
TAG-END TYPE: 450V: 100 pF 180p; 70V: 4700. 16: 150p; 3300 135p; 2200 99p; 40V: 15,000 389p; 470 4700 110p; 25V: 15000 195p; 6400 120p; 4700 100p	0 130p;4 000 92p; 3300; 3300 80p ; 2200 60p .	98p; 2500 90p; 30V:	BC114 BC115 BC117	20 E 20 E	D205 D245 D378	110 50 70	MPSA12 MPSA55 MPSA56 MPSU02	22 22 22 22 58	ZTX341 ZTX500 ZTX501 ZTX502	28 15 15 17	2N3773 288 2N3819 20 2N3820 45
35V: 0.1μF, 0-22, 0-33, 0-47, 0-68, 17ack, 0.25W 1-0, 2.2μF, 3-3, 4-7, 6-8, 25V: 1-5, 10, 68ΩΩ, 1KΩ & 68ΩΩ, 1KΩ & 68ΩΩ	ETERS: Rotary, Carbon, Log & 0.5W Lin. 470Ω, 2KΩ (Linear only) Single	2102-2 225 2111 195 2112-2 250	BC119 BC140 BC142 BC143	26 B	D434 D517 D695A D696A	32 70 85 85	MPSU05 MPSU06 MPSU52	50 50 65	ZTX503 ZTX504 ZTX531	15 25 25	2N3823 70 2N3866 90 2N3903 20 2N3904 18
16V: 15, 22. 25p. 47, 100 50p. 220 5KΩ·2MΩ Sin 70p.	gle Gang Log & Lin. 27p gle Gang 0 / P Switch 65p able Gang Log & Lin 78p	2114 396 2708 675	BC147 BC1478 bc148 BC148B	9 B 10 B	F115 F154 F158 F167	26 29 30 25	MPSU55 MPSU56 OC26 OC28	55 60 170 120	40311 40313 40315	25 60 125 55	2N3905 18 2N3906 17 2N4037 52 2N4058 17
MYLAR FILM CAPACITORS 100V: 0-001, 0-002, 0-005, 0-01μF 6p 0-015, 0-02, 0-04, 0-05, 0-056μF 7p 5ΚΩ-500ΚΩ s		4047 750 6502 995 81LS95 125	BC149 BC149€ BC153 BC154	9 B 10 B 20 8	F173 F177 F178 F179	24 25 30 38	0C35 0C36 0C41 0C42	125 130 125 48	40316 40326 40327 40347	85 52 62 80	2N4061 17 2N4062 17 2N4859 65
	uated Bezels 30p	81LS97 135 AY-3-1015 550 AY-5-1013 399	BC157 BC158 BC159	10 B 10 B 11 B	F180 F194 F195	38 11 12	OC43 OC44 OC45	55 55 30	40348 40368 40361 40362	105 43 45 42	2N5172 25 2N5179 60 2N5191 70
0.047 μ F 5p; 0.1 μ F, 0.2 μ F 7p & Horizontal	MΩ Miniature Vert'cal 7p -3-3MΩ horiz, larger 10p -4-7MΩ Vert. 10p	AY-5-2376 920 MC1488 85 MC1489 90 MC14411 695	BC160 BC167A BC168C BC169C	11 B 10 B 10 B	F196 F197 F198 F199	12 12 16 29	0C70 0C71 0C72 0C74	35 28 35 50	40468 40408 40411	60 95 280	2N5305 40 2N5457 32 2N5458 32 2N5459 32
82, 85, 100, 120, 150, 220 11p each 250, 270, 300, 330, 360, 390, 470, 600, 800, 820 16p each Miniature High	- Erie make 5% Carbon Stability, Low noise	MC14412 1080 MK4027-2 470 MK4027-4 350 MK4116-4 1025	BC170 BC172 BC177 BC178	11 B	F200 F224A F244B F256A	40 24 60 50	0C75 0C76 0C77 0C81	45 36 76 35	40594 40595 40603 40673	98 90 67 25	2N5485 35 2N5777 45 2N6027 40 2N6109 50
1000, 1200, 1800, 2000 26p each RANG POLYSTYRENE CAPACITORS: 10pF to 1nF 8p; 1.5nF to 47nF 10p 1/2 2.20.4 1/2	M E24 2p 1p M E12 2p 1p	MK4118-4 2099 RO-3-2513 650 SFF96364E 1050 SFC71301 820	BC179 BC182 BC183 BC184	15 8 10 B 10 B	2568 257 258 259	45 30 28 28	OC82 OC83 OC84 OC140	50 48 45 110	2N697 2N698 2N699 2N706A	40 40 30 19	2SD234 50 3N128 112 3N140 112
	10Ω-1MΩ 6p 4p 1M E24 8p 6p plies to Resistors of each	TMS2716 (3v) 1700 TMS4035 250 TMS4039 250	BC182L BC183L BC184L	10 B 10 B	451 336 594	20 35 30	OC170 OC171 OC200 TIP29	85 45 48 31	2N708 2N918 2N1131 2N1132	33 33 22 24	
COMPRESSION TRIMMERS 3.40pF; 10-80pF; 25-190pF 100-500pF 45p		TMS4045 1083 TMS6011 355 Z80 CPU 2.5M 990 Z80 CPU 4M 1099	BC187 BC212 BC212L BC213	9 B 9 B	595 R39 R40	20 25 25 24	TIP29B TIP29C TIP30	56 60 32	2N1303 2N1304 2N1305	50 50 35	
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Oilectric 0.2 365pF with slow motion Drive 8A102 395p 500pF 225p 0.0 208/176 325p AA215	15 RECTIFIERS (plastic case) p	702 75 709 14 pin 38	CM7216C 195 CM7217A 79 CM7555 8 .D130 45	0 NE570 9 NE571	170 375 420	(TEXAS 7400 7401	7493	78 65 57	74191 95 74192 98 74193 98 74194 98	S287 S288 S470 S472	325 125 60 210 126 60 325 132 95 1150 136 55
4511/DAF 125p motion drive 395p BY126 C804-5pF: 10: 15 6:1/36:1 650p 25 50pF 250p CRO33	12 1A/100V 22 12 1A/200V 25 157 1A/400V 29	710 67 1 723 14 pin 38 1 733 99	F356 9 M10 32 M301AP 2 M308T 7	SAD102 SG3402 SN7600	1350 295 3N 170	7402 7403 7404 7405	14 7497 14 74100 14 74104	119 62	74195 98 74196 93 74197 80	74L	825 138 85 139 85
Drum 54mm 40p 100.150pF 335p 0A9 0-1-365pF 275p L 3x310pF 695p 0A47 00 2 365pF 325p 00-3x25pF 490p 0A70	12 2A/50V 35 12 2A/100V 44 15 2A/200V 46	741105 35 747C 14 pln 70 748C 8 pin 36	M311 8 M318S 19 M324A 4 M339 7	5 SN76011 5 SN76011 5 SN76021	IND 130 148 170	7406 7407 7408	38 74107 38 74109 17 74110	54 54 68	74198 150 74221 132 74246 204 74247 204	00 01 02	11 148 173 11 151 96 13 153 76
TF CHOKES	15 2A/400V 53 14 2A/600V 65 7 4A/100V 72 7 4A/400V 79	810 159 AY-1-0212 580 AY-1-1313A 660,	M348 9 M349 12 M379 37	5 SN76111 5 SN76111	N 195 N 215 110	7409 7410 7411 7412	17 74111 15 74116 20 74118 17 74119	83 149	74248 240 74249 204 74251 125 74265 63	03 04 05 08	13 155 96 14 156 96 23 157 76 22 158 95
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2½ x 5" 55p 50p 31p IN916 3¾ x 3¾" 55p 50p — IN4001/ 3¾ x 5" 62p 67p 43p IN4003	5 VM18 DIL 50	AY-3-8500 390 L AY-3-8910 850 L AY-5-1224A 260 L	M387 15 M1458 44 M3900 66 M3909N 7	TAA960		7420 7421 7422 7423	16 74125 29 74126 24 74128 27 74132	57 74 73	74284 385 74285 395 74290 125 74293 125	13 14 15 20	38 164 114 75 165 75 30 166 226 20 170 288
3½ x 17" 218p 180p 120p 4½ x 17" 280p — 183p IN4006/ Pkt of 36pins 20p Spot face cutter 105p IN5404	7 7 ZENERS 4 Range: 2V7 to	AY-5-1315 560 L AY-5-1317A 630 L AY-5-2376 980	M3911 12: M3914 24: M13600 13: 4252AA 62:	TAD100 TBA1209	353 159 70 220	7425 7426 7427 7428	27 74136 36 74141 27 74142 35 74143	56 209 314	74298 185 74365 128 74366 118 74367 124	21 26 27 28	22 173 105 48 174 106 28 175 110 48 181 398
Pin insertion tool 140p VQ Boards 129p 0IP Boards 290p. Veroblock 324p VERO WIRING PEN 13A / 100V Plus Sociol 325p 3A / 100V 24 / 100F	20 Range, 3V3 to 33V, 1,3W	AY-5-3500 510 AY-5-3507 415 AY-5-3600 1090 M	#253AA 79 #C663 27 #C1204 00 #C1301 7	TBA5500 TBA641- BX or BX	330 112	7430 7432 7433 7437	17 74144 25 74145 40 74147 30 74148	65 175 109	74368 124 74390 184 74393 184 74490 198	30 32 33 37	22 183 298 27 190 140 39 191 140 39 193 130
Plus Spool 325p Spare spool (wire) 80p Combs 7p each	V30	AY-5-8100 735 CA3011 110 CA3012 150	AC1303 88 AC1304P 264 AC1310P 179 AC1312PQ 199	TBA800 TBA810 TBA820	90 95 70 260	7438 7440 7441	33 74150 17 74151 74 74153 68 74154	64 64 96	75150 120 75450 84 75451 70 75452 70	38 40 42 47	39 194 166 28 195 136 98 196 100 63 197 140
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Fibre Single- Double- SRBP MVAM1 Glass sided sided 9.5"×8.5" 6" x 6" 75p 90p 80p BA102 6" x 12" 130p 175p 8B104		CA3028A 80 A A CA3035 235 CA3036 115	AC3340P 120 AC3360P 120 AC3401 5	TDA1008 TDA1022 TDA1024	575 105	7447 7448 7450	82 74160 56 74161 17 74162	82 92 92 92	74L	55 63 73	30 243 232 150 244 155 46 245 270
DIL PLUGS 14 pin 35p; 16 pin 40p; 24 pin 85p; 40 pin 375p	40 5A600V 43 8A300V 48 8A500V 58	CA3045 365 CA3046 71 CA3048 214	AC3403 13! AEM 780 20! AFC6040 9: AK50253 656	TLO61CP TLO62CP TLO64CN	54 125 159	7451 7453 7454 7460	17 74163 17 74164 17 74165 17 74166	105 105 140 200	74L00 65 L30 70 L47 599 L75 298	74 75 76 78	41 247 190 48 248 190 40 249 190 40 251 134
Soldercon pins 100 50p; 500 200p. 3A2000 DIL SOCKETS EDGE 3A4000	12A100V 42 12A300V 59 12A500V 92	CA3080E 65 CA3081 190 CA3085 95	4K50362 656 4K50398 638 4M5303 638 4M5307 1278	TL072CP TL074CN TL081CP	45 90 140 42	7470 7472 7473 7474	28 74167 25 74170 32 74172 27 74173	185 625 120 87	£85 525 £121 150 £123 495	83 85 86 90	115 253 142 118 257 110 43 258 110 38 259 160
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16pin 13p 46p 2x15 way — 99p 12A400\\ 18pin 16p 52p 2x18 way 115p 120p 12A800\\ 20pin 22p 65p 2x22 way 130p 135p 16A100\\ 22pin 25p 70p 2x25 way 149p 160p 16A400\\	115 TIC45 25 240 2N4444 140	CA3140 48 N CA3160 95 N ICL7106 795 N	E544 189 E555 20 E556 59 E560 329	UAA 180 ZN414 ZN424E	150 80 130	7482 7483 7484 7485	69 74178 72 74179 95 74180 106 74181	53 153 85	\$132 350 \$138 250 \$158 524 \$188 210	96 107 109	116 279 66 44 283 192 55 290 128 55 293 128
24pin 36p 78p 2x30 way 170p 16A5000 28pin 39p 85p 2x36 way 194p 25A5000 36pin - 1055p 2x40 way 210 25A8000 25A	/ 120 / 235 / 295 DIAC	ICL8038CC 335 ICM7205 1150 ICM7215 1050 N	E561 39! E562B 410 E564 42! E565A 120	ZN 1034E ZN 1040E	200 685	7486 7486 7489 7490 7491	31 74182 210 74184 33 74185 75 74188	88 135 135	\$188 210 \$189 158 \$194 195 \$195 795 \$241 195	113 114 122	50 295 185 50 295 185 50 298 168 70 324 240 70 325 290
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	4 pole on / off	54p	PUSH BUT	
	SUB-MIN TOO SP changeover SPST on/off SPST biased		Spring to a SPST on/o SPDT c/ove DPDT 6 Tag	ff 60p
	DPDT 6 tags	70p	MINI. Nor	Locking
	DPDT centre of		Push to Ma	
	DPDT Biased	115p	Push Break	25p
			Push to c/c	over 85p
*	Adjustable St modate up to Mains Switch	op Shafti 6 Wafers DPST to		80p 40p
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CRYSTAL	s	
100KHz	323	
455KHz	383	
1 MHz	323	
1.008M	395	
1.28MHz	392	
1.6MHz	323	
1.8MHz	323	
1 8432MHz	362	
2.4576MHz	362	
3.2768M	323	
3.57954M	195	
4.000MHz	290	
4 032Mhz	323	
4 433619M	135	
5.0MHz	355	
5.185M	323	
6.5536M	200	
7.680M	323	
8 86723M	323	
9 375M	323	١
10.0MHz	323	
10.7MHz	323	
12MHz	392	
14.3181MHz		
18MHz	323,	
18.432M	323	
20.0MHz	323	
27.648M	323	
48.0MHz	323	
100.00MHz	323	

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DM900

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6-0-6V; 9-0-9V; 12-0-12V 10DmA 95;	D
3VA: 0.6V 0.6V (PCB mouning) 150	p
8VA: 6V5A 6V5A; 9V4A 9V4A; 12V3A	à
12V3A; 15V25A 15V25A 215	p
12V: 4.5V-1.3A 4.5V-1.3A; 6V-1.2A 6V-1.2A	
12V5A 12V5A; 15V4A 15V:4A; 20V3A	۹
20V3A 235p (20p p&p	1
24VA: 6V-1.5A 6C-1.5A; 9V-1.3A 9V-1.3A	í
12V-1A 12V-1A; 15V-8A 15V-8A; 20V-6A	À
20V6A 320p (45p p&p)	١.
50VA: 6V-4A 6V-4A; 9V-2.5A 9V-2.5A; 12V-2A	Ĺ
12V-2A; 15V-1.5A 15V-1.5A; 20V-1.2A 20V	ļ,
1.2A; 25V-1A 25V-1A, 30V8A 30V8A	
365n (50n n&n)	ı

1.2h, 259-1A 259-1A, 509-5A 509-6A
365p (50p p&p).
100VA: 12V-4A 12V-4A; 15V-3A 15V-3A;
20V-2 5A 20V-2.5A: 30V-1.5A 30V-1.5A:
40V-1 25A 40V-1 25A; 50V-1A 50V-1A 695p
(60p p&p). (N.B. p&p charge to be added above
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12x5x3" 215 12x8x3" 265	0-50V AC 0-300V AC
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VOLTAGE REGULATORS TO3 7805 7812 7815 7818 + ve 145p 145p 145p 145p

4513 4514

	1A 5V 12V 15V 18V 24V	7805 7805 7812 7815 7818 7824	65p 65p 65p		7905 7912 7915 7918	75p 75p 75p 75p
I	100m	A T	noż pla	stic Casıno		
ı	5V	78L0	5 30p	ı `	79L05	65p
ı	6V	78L6				_
ı	8/	78L8				www
ı	12V	78L1	2 30p	•	79L12	65p
ı	15V	78L1	5 30 p	1	79L15	65p
ı	LM 30	ЮН	170p	LM327		270p
ı	LM30)5H	140p	LM723		38p
ı	LM30	9K	135o	TAA550)	50p
١	LM31		350p	TBA625	в	95p
١	LM32	23K	550p	TDA141	12	150p
١	LM32		240p	.78HO5		595n

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i5p	
-	TIL 78 Detector
www	LS400
5Бр	OCP71
15p	ORP12
	ORP61
/0p	2N5777
18p	2143777
Op	ISOLATO
)5p	IL74
οp	TH.111/2
95p	Th. 114
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H205 Detector \$	06	7 Segment Disp	aysic
	8	TIL307	675
	0	TIL312 .3" CA	105
		TIL313 .3" CC	105
400 25		TIL321 .5" CA	115
P71 12	0	TIL322 .5" CC	115
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5777 4	15	DL747.6" CA	180
		FND357 Red	120
ISOLATORS		3" Groon CA	150
4 4	18	6" Green CA	215
.111/2 8	15	. U GIEBII CA	213
.114 9	15		
.117 11	0	LCD 31/2 Digit	875
		LCD 4 Digit	975

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326	294	4010	38	4048	58	4099	14
327	286	4011	28	4049	48	4160	10
347	148	4012	18	4050	48	4161	10
348	186	4013	42	4051	72	4162	10
352	228	4014	80	4052	73	4163	10
353	228	4015	82	4053	72	4174	11
365	65	4016	45	4054	110	4175	9
366	65	4017	79	4055	128	4194	10
367	85	4018	87	4056	135	4408	72
368	66	4019	38	4057	1650	4409	72
373	180	4020	99	4059	480	4410	72
374	180	4021.	105	4060	115	4411	95
375	160	4022	95	4061	1200	4412F	125
377	212	4023	22	4062	995	4412V	105
378	184	4024	66	4063	110	4415F	25
379	215	4025	19	4066	58	4415V	50
384	86	4026	180	4067	380	4419	28
390	230	4027	45	4068	22	4422	54
393	230	4028	81	4069	20	4433	99
395	218	4029	99	4070	32	4435	82
396	215	4030	58	4071	21	4440	127
398	276	4031	205	4072	21	4450	29
399	230	4032	100	4073	21	4451	29
445	150	4033	145	4075	23	4452	
447	144	4034	216	4076	85	4490F	69
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668	182	4036	335	4078	21	4501	- 1
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	OS*	4040	105	4086	52	4507	5
4000	13	4041	80	4089	150	4508	29
4001	18	4042	75	4093	78	4510	9
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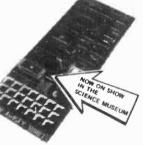


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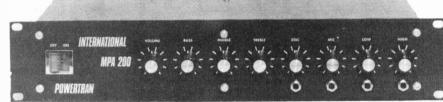
This versatile system featured as a constructional article in ELECTRONICS TODAY INTERNATIONAL has 5 frequency channels with individual level controls on each channel. Control of the time versative system reducted as a constructional article in ELECTRUNICS TODAY INTERNATIONAL has 5 frequency channels with individual level controls on each channel. Control of the lights is comprehensive to say the least. You can run the unit as a straightforward sound-to-light or have it strobe all the lights at a speed dependent upon music level or front panel control or use the internal digital circuitry which produces some superb random and sequencing effects. Each channel handles up to 500W and as the kit is a single board design wiring is minimal and construction very straightforward.

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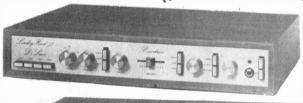
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Featured as a constructional article in ETI, the MPA 200 is an exceptionally low priced — but professionally finished — general purpose high power amplifier. It features adaptable input mixer which accepts a wider range of sources such as microphone guitar, etc. There are wide range tone controls and a master volume control. Mechanically the MPA 2000 is simplicity itself with minimal writing needed making construction very straightforward. The kit includes fully finished metalwork, fibgeglass PCBs, controls, wire etc. — complete down to the last nut and bolt.







T20+20 20W STEREO AMPLIFIER £33.10+VAT

This kit, based upon a design published in Practical Wireless, uses a single printed circuit board and offers at very low cost, ease of construction and all the normal facilities found on quality amplifiers. A 30 watt version of this kit (T30 + 30) is also available for £38.40 + VAT.

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This easy to build version of our world-wide acclaimed 75W amplifier kit based upon circuit boards interconnected with gold plated contacts resulting in minimal wiring and construction delightfully straightforward. The design was published in H-Fi News and Record Review and features include rumble filter, variable scratch filter, versatile tone controls and tape monitoring whilst distortion is less than 0.01%

WIRELESS WORLD FM TUNER £70.20 + VAT

A pre-aligned front-end module makes this Wireless World published design very simple to construct and adjust without special instruments. Features include an excellent a m. rejection push-button station selection as well as infinitely variable tuning and a phase locked loop stereo decoder, incorporating active filters for "birdy" suppression.

LINSLEY-HOOD CASSETTE DECK £79.60+VAT

This design, published in Wireless World, although straightforward and relatively low cost provides a very high standard of performance. There are separate record and replay amplifiers and switchable equalisation together with a choice of bias levels are also provided. The mechanism is the Goldring-Lenco CRV with electronic speed control.



DIGEST

Nevada News

From January 5th to 8th a large contingent of electronic retailers, wholesalers, agents and distributors once again descended upon Las Vegas, Nevada for the Winter Consumer Electronic Show - to date the World's largest showpiece reflecting current and future trends in audio, video, computer games, telephones, personal communications/computers and allied electronic products. This menagerie was staged at three venues: the Las Vegas Convention Centre, the Hilton Hotel and the Jockey Club.

The emphasis from the Japanese contingets was centred on remote control, including ultra sonic, infra red, and voice control! That's right, I said voice control. 1980 could be the year in which voice activated electronic products finally live up to their vast potential.

Industrial uses for voice activation are already in effect while consumer products have yet to hit the market. For example, in America United Parcels Service has a voice activated parcel sorting system. Other industrial uses involve warehousing and distribution inventory and quality control as well as aids to the handicapped such as voice activated wheel-chairs.

One company, Heuristics Inc. of Sunnyvale, California, has sold between five and ten thousand speech recognition units for use with personal computers. However, all existing equipment requires close talking or a hand held microphone, making it only slightly more advanced than many remote control units.

A television set that can be operated by human voice and confirms command is one of the latest developments announced by Toshiba. They also have a hi-fi system which responds to fifteen words. At a recent lapanese electronic show, Sharp showed a device able to recognise three voices, twenty-two words each. Such products are speaker trained, meaning each system can recognise onlyone or two voices. This form of recognition will be prevalent for some time since speaker independent systems, capable of responding to a pre-trained vocabulary spoken by anyone, pose extreme difficult technical and pricing problems. An existing speaker independent system with thirty words vocabulary sells for \$50,000. So, it seems in the very near future, your hi-fi system will truly respond to 'HIS MASTER'S VOICE'.

Last year's magic phrase in video cassette recording waslonger playing time. This year's magic phrase appears to be special effects as supplies of both VHS and Beta systems used this Winter's C.E.S. to unveil a new generation of feature laden home decks and portables with such special effects as visual slow motion, freeze frame, single frame advance and fast forward at up to fifteen times normal speed.

Now the VHS camp has also jumped into the visual scan frame. Although JVC was the first VHS supplier with visual scan model, RCA, Quasar, Magnavox and MGA have unveiled new models with special effects visual scan features. RCA coupled its mid-December video disc announcement with the introduction of new 2, 4 and 6 hour decks with visual freeze frame, variable slow motion, single frame advance and double speed playback. All functions can be operated by remote unit and the suggested list price for the new deck is \$1,395. Hitachi also introduced their model VT5800A. This is a new 2, 4 or 6 hour deck with ten key programming for up to seven days plus a new lightweight camera which will sell in the US for less than \$800. Whilst the VHS and Beta camps slug it out on the video cassette recorder market, Toshiba has added a dramatic new element to the fight, marketing plans for the first consumer LVR systems. Toshiba is introducing two units, the L10A (stan-



dard) and the L10S with electronic programmable tuner and full mode remote control. If Toshiba realises its plans, the units will be the first and only LVR's in the domestic market. BASF has shown a competitive prototype in Germany, but has taken no further initiative so far.

Matsushita has the Visc system - Visc 2. It's the closest design to normal a record with the information in the grooves of the disc. All the above systems are totally incompatible. 1,800 rpm is common to most of the systems. This number is derived from the fact that there are sixty seconds in a minute and thirty seconds per frame in US video, so one revolu-

tion of the disc gives you one video frame.

So it appears on the surface that the consumer is faced with another non-standard consumer orientated video product.

As television, audio and games manufacturers add more microprocessor controlled units to their product lines, it seems manufacturers can count on expecting continued chip shortages throughout 1980. When allocating chips, the semiconductor industries look more favourably on such financially established industries as computers, television and audio, according to sources within the consumer electronics industry. There has been a demand for chips building up in the television industry for some

It appears that both the audio and video categories will get the chips that they want for 1980. Supplies of microprocessor audio components which sell far fewer units than the \$500,000,000 electronic games industry report no difficulties in obtaining chips. Almost every product in the future will incorporate microprocessors hence companies like Atari, who have planned on introducing eight new products, have to limit themselves because of the shortage of chips.

There just are not enough chips to go around. The games industry has had a very steep growth. In the last two years, a ten fold increase in demand which is still growing at the same rate, but if the current trend in games diminishes, semiconductor manufacturers will be in embarrassing positions should they increase their chip manufacturing facilities. Gerald Chevin

Hot 'n' Fast

This powerful little package can deliver up to 75 watts in only five seconds at the touch of its fingertip control lever. The miniature iron uses the unique Scope

carbon heater and is powered from the Scope 3V3 transformer.

The Mini-Super-Speed Iron costs £12.50 plus VAT, the 3V3 Safety Transformer £7.50 plus VAT, and the element/tip spares

pack £2.50 plus VAT. All Scope products, which are manufactured in Australia, are available exclusively in the UK through Toolrange Ltd, Upton Road, Reading RG3 2IA.

Metal Locator (March)

The Metal Locator project from the March issue has already caused quite a stir at Altek Instruments' office in darkest Surrey. Now, do you want the good news or the good news. Well, the good news is that Altek have been inundated with orders to such an extent that they have been able to reduce their prices. The complete kit is now £79.70. The search head alone is £13.55. And now the good news. Both prices include VAT and postage - no extras

The Shadow VLF Metal Locator is available in kit form from Altek Instruments, 1 Green Lane, Walton-on-Thames, Surrey KT12 5HD.

TTI	s by TEXAS	74259	250p	4019	45p	93 SERIES	VEROBOARDS 0.1 0.15	TRANSISTORS	BF259	36p	TIP30A 48p	2N3054 65 p	40361/2 45p	10A. 400V 200p
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742 742	2 22p	74LS11 74LS13 74LS14	40p 40p 72p	4042 4043 4044	90p 90p	AY5-1224A 240p AY5-1315 800p	NE561B 425 p NE562B 425 p NE565 130 p	BC187 30p BC212/3 11p	BU205 BU208	200p. 200p	TIP147 160p TIP2955 78p TIP4055 70p	2N4061/2 18p 2N4123/4 27p 2N4125/6 27p	1N914 4p 1N916 7p	128000 130p
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743 743 743	2 30p	74LS30 74LS32 74LS42	20p 27p 70p	4050 4051 4052	49p 80p 80p	CA3086 48p CA3089E 225p	SAD1024A 1250p SFF96364 1100p SN76003N 1750	BC461 36p BC477/8 30p	MJ295 MJ300	5 90p	ZTX500 15p ZTX502 18p ZTX504 30p	2N5089 27p 2N5172 27p 2N5179 90p	1N5401/3 14p 1N5404/7 19p	3A 400V 90p 8A 600V 140p
743 743	7 35p	74LS47 74LS51	90p 24p	4053 4054	80p 150p	CA3090AQ 375p CA3130E 90p CA3140E 50p	SN76013N 140p SN76013NO 120p	BC516 /7 50p BC547B 16p BC548C 9p		55 100p	2N457A 250p 2N696 35p	2N5191 83p 2N5194 90p	HEAT SINKS	12A 400V 160p 16A 100V 160p 16A 400V 180p
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744 744	5 100p	74LS83 74LS85	110p 100p	4066 4067	55p 450p	FX209 750p ICL7106 850p	TBA641B11 225p TBA651 200p	BD131/2 50p 80135/6 54p	MPS65	6 30p	2N930 18p 2N1131/2 20p	2N5460 60p 2N5485 44p	BRIDGE RECTIFIERS	TIC44 35p 2N3525 120p 2N4444 140p
744 744	7A 50p 8 80 p	74LS86 74LS90 74LS92	40p 40p 70p	4068 4069 4070	27p 27p 30p	ICL8038 340p ICM7555 80p	TBA800 90p TBA810 100p	B0139 56p B0140 60p	MPSA1 MPSA1 MPSA2	3 50p	2N1613 25p 2N1711 25p 2N2102 70p	2N5875 250p 2N6027 48p 2N6107 65p	1A 50V 19p 1A 100V 20p 1A 400V 25p	2N5060 34p 2N5064 40p
745 745 745	1 17p	74LS93 74LS96	60p	4071 4072	25p 25p	LF356P 95p LM10C 425p LM301A 30p	TBA820 90p TCA940 175p TDA1004 300p	BD189 60p BD232 95p BD233 75p	MPSA4	2 50p 3 50p	2N2160 350p 2N2219A 30p	2N6247 190p 2N6254 130p	1A 600V 30p 2A 50V 30p	
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747 747 747	2 30p	74LS112 74LS113 74LS114	90p	4076 4081 4082	107p 27p 27p	LM319 225p LM324 50p LM339 75p	TDA1022 600p TOA1024 120p TDA10348 250p	BD242 70p BDX538 160p BDY56 200p	MPSU(7 90p 15 90p	2N2484 30p 2N2646 45p 2N2904/5 25p	2SC1172 150p 3N128 120p 3N140 100p	3A 200V 60p 3A 600V 72p 4A 100V 95p	SPEAKERS Size 2½" 64R 70p
747	4 30p	74LS122 74LS123	80p 70p	4086 4089	72p 138p	LM348 95p LM377 175p	TDA1170 250p TOA2002V 325p	BF200 32p BF244B 35p	MPSU6	130p	2N2906A 24p 2N2907A 30p	3N141 110p 3N201 110p	4A 400V 100p 6A 50V 80p	2½" 8R 70 p 2" 8R 90 p
747	6 35p 10 50p	74LS124 74LS125 74LS126		4093 4094 4095	80p 250p 95p	LM380 75 p LM381AN 180 p	TDA2020 320p TL071 50p TL072 95p	BF256B 70p BF257/8 32p	OC35 TIP29A TIP29C		2N2926 9p 2N3053 30p	3N204 100p 40290 250p 40360 40p	6A 100V 100p 6A 400V 120p	1½" 8R 80p
748 748 748	2 84p	74LS132 74LS133	95p 30p	4096 4097	95p 340p	LM709 36p LM710 50p LM725 250p	TL074 150p TL081 45p	MEMORIES 2102-2L	120p	UART	0150 500		IL SOCKETS BY TEXA	s
748 748	14 100p 15 110p	74LS136 74LS138 74LS139	55p 75p 75p	4098 4099 40100	120p 200p 220p	LM733 100p LM741 18p	Ti082 95p TL084 130p	21078	500p 225p	AY-3-1 AY-5-1 IM640	013P 400p	8 pin 10p 14 pin 11p		pin 30p pin 38p
748 748 749	9 175 p	74LS145 74LS147	120p 220p	40101 40102	132p 180p	LM747 70p LM748 35p LM2917 250p	TL170 50p UAA170 200p UDN6118 320p	2112-2 2114	300p 525p	TMS60	011NC 400p	16 pin 12p		pin 48p
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749 749	65p 7 180 p	74LS156 74LS157	90p 60p	40108 40109 40110	470p 100p 300p	LM4136 120p MC1310P 150p	XR2216 675p XR2240 400p	745201	350p 325p 325p		2513 L.C. 650p 3262AN 900 p	SUBMINIATURE SWITCHES	ANTEX SOLE	- 4
741 741 741	04 65p	74LS 158 74LS 160 74LS 161	90p 130p 100p	40114 4411	250p 1100p	MC1458 48p MC1495L 350p MC1496 100p	ZN414 90p ZN419C 225p ZN424E 135p	ROM/PROMs 71301	700p	KEYB	DER		60p C-15W CX-17W CON 15W	400p 415p
741 741	07 34p 09 55p	74LS162 74LS163	140p 100p	4502 4503 4507	120p 70p 55p	MC3340P 120p MC3360P 120p	ZN425E 400p ZN1034E 200p	74S287	225p 350p 350p	AY-5-2	376 900 p	DPDT (centre off) 8	70p X25	415p 415p
741 741 741	11 70p	74LS164 74LS165 74LS166	120p 160p 180p	4508 4510	290p 99p	WK50398 750p VOLTAGE REGULATO	'95H90 800 p	74S470 74S471	650p 650p	(prim 220			Sp C/CX/CCN	46p 50p
741 741	18 130p 19 210p	74LS173 74LS174	110p	4511 4512	150p 80p	Fixed Plastic TO-220 1A +ve	Ve		650p 750p 400p	6-0-6 9-0-9 0-120	100mA 88p 75mA 92p 12500mA 280p	SLIDE DPDT 1	SPARE ELEM C/CX/X25	180p
741 741 741	21 28p	74LS175 74LS181 74LS190	110p 320p 100p	4514 4515 4516	265p 300p 110p	5V 7805 80p 12V 7812 60p 15V 7815 80p	7905 70p 7912 70p 7915 70 p	93436 93446	650p 650p	0-25V (5) 9-0-9 1A	√A) 250p 270p*	WAFER	ADCOLA IRO	200p NS 550p
741 741	23 48p 25 55p	74LS191 74LS192	100p 100p	4518 4520	100p 100p	18V 7818 60p 24V 7824 60p	7918 70p 7924 70p	CPUs	900p	12V 2A 0-12-15 20-24-30	350p*	3P/4W 4 4P/3W 4	15p K2000	550p
741 741 741	28 75 p	74LS193 74LS195 74LS196		4521 4526 4527	250p 108p 150p	100mA TO-92 5V 78L05 30p	79L05 70 p	2650A 2	200p 2000p 1000p	15-0-15			DIP Breadboard	
741 741	35 50 p	74LS197 74LS221	120p 140p	4528 4538	120p 120p	12V 78L12 30p 15V 78L15 30p	79L12 70p 79L15 70p	6800 6802 1	900p 250p	mal p&p	charge).	CRYSTALS 100KHz 30 1MHz 37	16 × 16 pin 0	L ICs) DIP
741 741	42 200p	74LS240 74LS241 74LS242	175p	4543 4553 4556	180p 450p 72p	OTHER REGULATORS LM309K 135p LM317T 200o	TBA625B 120p 78HGKC 675p	8080A	550p 550p 400p	RESISTO		1.008MHz 37 3.2768MHz 35	for 31 way con	
741 741 741	47 190p	74LS243 74LS244	170p 195p	4560 4569	250p 250p	LM323K 550p LM723 37p	78H05KC 625 p 78MGT2C 135 p 78P05 900 p	1NS8060 1 Z80 1	100p 100p	Stab 5% I Carbon Fil		4MHz 35	(No track cuttin	g)
	50 100p 51A 70p	74LS245 74LS247 74LS248	140p	4572 4583 4584	40р 90р 90р	OPTO-ELECTRONICS 2N5777 45p	ORP60 90 ₀	EPROMS	1250	1/4W 10R one valu	e	10.7MHz 35 18MHz 30	31 way Plug	110p
741 741 741	54 100p	74LS249 74LS251	140p 140p	4724 40097	250p 90p	OCP71 130p · · ORP12 90p	ORP61 90p TIL78 70p	2516 2	500p 100p 800p	½W 10R one valu			31 way Socket S-100 Busboar	110p £12
741 741	56 90 p 57 70 p	74LS253 74LS257	140p 120p	14412	1100p 1100p 1100p	0PTO-ISOLATORS ILD74, 130p MCT26 100p	THL111 90p TIL112 90p	2716 2 SUPPORT	2100p	Miniature Hor/Vert	Presets 100R-1M 12p	EDGEBOAR 2 x 10 way	D CONNECTORS 0.19	6" PITCH 135p
741 741 741	60 100p	74LS258 74LS259 74LS266	160p 160p 100p	14500 14599	700p 290p	MCS2400 190p LEDS	TIL116 .90p	3245 6532 1	400р 100р	Carbon Tr	ack Pots .og or Lin	2 x 15 way 2 x 18 way	100p 2 x 25 way 120p	160p
741 741	62 100p 63 100p	74LS273 74LS279 74LS298	195p 90p 249p	CD22100 CD22101 CD22102	350p 700p	0 125" TIL32 75 p	0.2 TIL220 Red 16p	6820 6821	500p 500p	Single Single w	th Switch 60p	COUNTERS 74C925	475p TTL &	ECL
741 741 741	65 130p	74LS324 74LS348	200p	INTERFAC		TIL209 Red 13p TIL211 Gr 20p TIL212 Ye 25p	TIL222 Gr 18p TIL228 Red 22p MV5491 TS 120p	8205	500p 320p 225p	SLIDER P	OTS 60mm Track OK, 50K, 100K	74C928 ICM7216B	600p MC402	24 325p 4 325p
741 741	67 200 p 70 240 p	74LS365 74LS367	100p 100p	DM8123 DP8304	175p 550p	TIL216 Red 18p DISPLAYS	Clips 3p	B216	225p 400p	LDG 10K	60p 60p	ICM7217A ZN1040E	850p 10116 700p 10231	70p 350p
741 741 741	73 120p	74LS368 74LS373 74LS374	100p 180p 195p	0S8835 0S8836 MC1488	250p 150p 100p	3015F 200 p DL704 140 p	NSB588 f 570p TIL311 600p TIL312/3 110p	8228 8251	525p 700p	SPE	CIAL OFF	ERS (subi	ect to stock	(2
741 741	75 85p 76 90p	74LS378 74LS390	200p 160p	MC1489 25S10	100p 350p	DL707 Red 140p 707 Gr 140p DL747 Red 225p	TIL321/2 130p TIL330 140p	8255	1200p 550p 1100p	555	1	£18/100	7805	£5/10
741 741 741	78 160p	74LS393 74LS445 74LS668	140p	75107 75150 75154	160p 175p	747 Gr 225p FND357 120p	7750 60 200p DRIVERS	Z80P10	400р 650р	741 2114	L-3	£4.50	7812 7905	£5/10 £6/10
741 741 741	81 160p	74LS669 74LS670	100p	75182 75322	175p 230p 300p	FND500 120p FND507 120p MAN3640 175p	9638 200 p 9370 200 p UON6118 320 p	Z80CTC	800p 650p 100p		(plus 5V only)	£21.00	7912	£6/10
741 741	84A 150p 85 150p	4000 SE	18p	753 2 4 75325	375p 375p	MAN4640 200 p	UDN6184 320p	MC14412 1	100p	l	(200 ns)		P&P + VAT Extra	
741 741 741	88 325p	4001 4002 4006	25p 25p 95p	75361 75363 75365	300p 400p 350p	EXP350 3 6" x 2.1" (Up to 3 x 14 pin ICs)	£3.15 BOARDS	Bus Strips/Binding F		(R	6 KEY KEYPAD leed Switches) HF Modulators		PUTER KITS PRY MAPPED VOU INTI	
741 741	91 90 p 92 90 p	4007 4008	18p 80p	75451 75491/2	72p 96p	EXP650 3 6" x 2.4" (Up to 1 x 40 pin IC) EXP300 6" x 2.1"	£3.60 on sturdy base PB6 6 x	plate. 4 DtL tCs	£	9. 20 LC	ed Switches (12VA) GIC PROBE	£0.25 SERIAL £18.00 ELF II N	L I / P VOU INTERFACE MICROCOMPUTER KIT	£45.00 £56.00 £79.95
741 741 741	94 90 p	4009 4010 4011	40p 50p 25p	8T26 8T28 8T95	250p 300p 200p	EXP300 6" x 2.1" (Uto 6 x 14 pin ICs) EXP600 6" x 2.4"	£5.75 PB100 10 x 1 PB102 12 x 1 £6.30 PB103 24 x 1	4 DIL ICs	€22	1.80 M 2.95 St	ULTIMETERS UPERTESTER 680R	£33.00 GIANT	WIRED AND TESTED MONITOR BOARD KIT I	€99.95 OR FIF II €35.00
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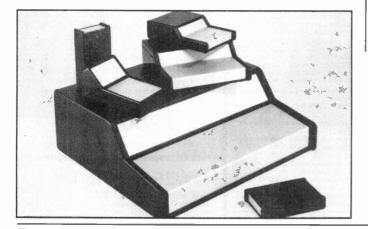
The page to be read is placed over the scanning unit which then converts the written text to digital signals for the computer. The computer then converts them into

sound with the speech synthe-

Syntax analysis is also incorporated to ensure that the right stress is placed on the correct word in a sentence

The optical system can accommodate a wide range of type faces, but must be programmed to

If the machine is a success it offers enormous benefits to the blind. It is curently being tested by the Royal National Institute for the



Building Block

New from National Semiconductor, the LM13600 is a programmable dual operation transconductance amplifier designed to be used as a fundamental building block in current controlled amplifiers, filters and oscillators. It can also be used in multiplexers, timers and even sample and hold circuits. In some cases it could be used to replace mechanical potentiometers. It is well suited for use in electronic organs and music synthesisers, because it can modulate waveshapes with ease.

The 16 pin LM13600 is programmable over six decades,

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The recently announced Dolby HX Headroom Extension System for noise reduction uses the LM13600 for dynamic control of recording bias.

The remarkable LM13600 is made by National Semiconductor (UK) Ltd., 301 Harpur Centre, Horne Lane, Bedford.

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NEWS:Digest

Fireside Viewing

Once upon a time there was a Mr Slaymaker whose factory in Esher was almost completely destroyed in a fire. While tiptoeing through the ashes, Mr Slaymaker found his telly - hanging chain broken from the intense heat, case badly distorted, front panel non-existent and full of water from the firemen's hoses. After a few months Mr Slaymaker unwelded the controls and plugged it in. Using a hacksaw for an aerial, he obtained a near perfect picture. There's a moral there somewhere. If you're intending to burn your house down round your ears during crossroads I should get hold of a IVC Videosphere colour telly pretty quickly.



Shell Kit

ot vourself a circuit diagram Gfor a metal locator? Construction of the PCB's no problem, but if the tantalising treasure-tracing tit-bit doesn't come as a complete kit, where do you get your hardware from. At worst, you can end up using plant pot saucers to house the search coil and broom handle (complete with splinters) for the shaft.

Fear not - Sonasonics comes to the rescue. They can now supply a metal locator shell in kit form from £17.25 including VAT and carriage. The kit includes a search coil case, shaft, handle and a case for the electronics. The case can be supplied drilled or undrilled, if requested.

Further details from Sonasonics Electronics, 11 Park Road, Ashford, Kent TN24 8LU.

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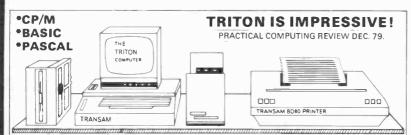
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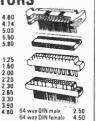
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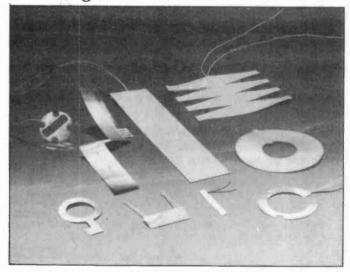
MCC Preamp (Jan)

We've had enquiries about the power supply for the Moving Coil Cartridge for use with the Audiophile System 4000 project. You don't have to build a separate supply. The MCC Preamp will run happily from the

15-0-15 volts System 4000 preamp supply (see ETI Oct 79).

If you're just building the MCC Preamp and not the complete system, then have a look at ETI October 1979 for details of the 15-0-15 supply.

Foiled Again



arel Components have announced a new range of thermofoil heaters designed and made by Minco Products, the pioneers of etched foil heater technology.

The flexible, chemically etched foil heater elements are laminated between thin insulating layers to provide a uniform or profiled heating pattern. Applica-

tions? Temperatures of everything from inertial guidance systems to batteries, baths and ovens can all be controlled.

For a complete temperature control system, foil or wirewound sensors can be integrated with the heater element for more accurate temperature control. For further details contact Carel Components Ltd, 40-44 The Broadway, Wimbledon SW19.

World-beater

Hitachi's new HA12017 is claimed to be the world's lowest noise audio preamp IC. The Hitachi silicon surface process ensures that the exceptionally low noise characteristic is reliably repeatable in mass production.

So you want to see some figures. Under standard pick-up conditions, a S/N ratio of 82.6 dB is achieved, with an equivalent

input noise of just 0.185 uV. Moreover, the IC has less than 0.002% THD over the audio band (20 Hz to 20 kHz) at an output level of 10 V rms (under RIAA conditions). The SIL package provides maximum isolation between stages.

If you're just dying to design a preamp round the HA12017 you can get hold of one for £1.57 from Ambit International, 200 North Service Road, Brentwood, Essex CM14 4SG.

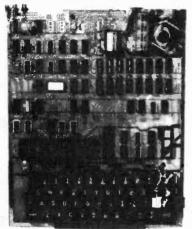


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Dynamic RAMS	-	Interface		CA3046	0.65	1 1 1 1 1 1 1 1 1	PLU: perbo	S		LS series		74LS125		74LS279	0.57
	£	8205	3.00	CA3053	0.72	Su	perbo:	ard II	THE NAME OF	74LS00		74LS126	0.36	74LS283	1.09
4027	3.01	8212	2.00	CA3075	2.00					74LS01	0.12	74LS132	0.60	74LS289	4.50
4050 (200ns)	2.50	8216	2.08	CA3078S	1.90	only	£188	+VAT	A	74LS02	0.14	74LS133	0.39	74LS290	0.91
4050 (350ns)	2.35	8224	2.77	CA3080	0.67	LM3065N	1.50	SN 76660N	0.75	74LS03	0.14	74LS136	0.36	74LS293	0.91
4060 (300ns)	2.39	8228	4.13	CA3080E	0.67	LM3900N		SN76666N	0.75	74LS04	0.16	74LS138	0.58	74LS295	1.30
4116	6.74	8251	5.00	CA3081	1.30	LM3905N		TAA263	2.20	74LS05		74LS139	0.58	74LS298	1.16
4110	6.74		6.93		1.30				0.50	74LS08		74LS145	0.97	74LS348	1.39
Static RAMS		8253		CA3082		LM3909N		TAA320A		74LS09		74LS151	0.81	74LS352	1.04
2102A	1.16	8255	5.08	CA3086	0.45	LM3911N		TBA120S			0.18	74LS153	0.52	74LS353	0.92
				CA3089	1.75	M252 B1 AA		TBA 231		74LS10		74LS154	1.30	74LS362	4.21
2102A-2	1.16	Baud Rate		CA3090Q	3.95	M 253 B1 AA		TBA5200		74LS11		74LS154	0.72		0.47
2111A-1	1.70	Generators		CA3097E	1.85	MC1310P		TBA530Q	1.50	74LS12	0.18			74LS365	
2112A-2	1.83	MC14411	5.87	CA3123E	1.70	MC1312P		TBA540Q	1.50	74LS13	0.37	74LS156		74LS366	0.47
21L02	1.16	MM5307	9.38	CA3130E	0.85	MC1314P		TBA550Q	1.50	74LS14		74LS157	0.57	74LS367	0.47
2114	5.17			CA3140E	0.36	MC1315P		TBA560Q	3.75	74LS15		74LS158	0.57	74LS368	0.47
4035 (1000ns)	1.07	UARTS		CA3160E	1.00	MC1327P	0.95	TBA651	1.80	74LS20		74LS160	1.09	74LS373	0.78
4045 (250ns)	6.15	AY-5-1013	3.65	CA3600E	3.69	MC1330P		TBA 750Q	2.64	74LS21		74LS161	0.69	74LS386	0.36
5257 (TMS4	044)	MM5303	5.04	ICL7038A	3.57	MC1350P		TBA800	0.83	74LS22		74LS162	1.16	74LS393	0.84
	6.93	TMS6011NC	4.30	ICL8038BC	8.82	MC1351P	1.20	TBA810S	1.10	74LS26	0.18	74LS163	0.69	74LS668	1.17
6810	3.03			ICL8038CC	3.40	MC1352P	1.35	TBA810AS	0.80	74LS27		74LS164	1.06	74LS670	1.71
		2700	The Party	ITT7120	1.90	MC1375P		TBA820	0.70	74LS28	0.18	74LS165	0.72		
ROMS		2708		LF351N	0.40	MC1445L		TBA920Q	1.75	74LS30	0.18	74LS166	1.65	A STATE OF THE PARTY.	J-100
2513 (U.C.)	6.25	only		LF356N	0.80	MC1456CG		TBA990Q	1.50	74LS32	0.26	74LS168	1.71	8 x 411	I G
2513 (L.C.)	6.25			LM301AH	0.36	MC1458CP1		TCA270Q	1.00	74LS33	0.26	74LS169	1.71		
MM5230	4.62	£6.25		LM301AN	0.25	MC1495L		TCA730	3.97	74LS37		74LS170	1.72	only	
1411410230	4.02	+VAT		LM307H	0.66	MC1496P		TCA 740	3.97	74LS38	0.23	74LS173	0.81	£49.50	
CPU				LM307N	0.43	MC3302P		TCA940		74LS40		74LS174	0.97		ALC: N
6800	6.01	Integrated Circ	iee	LM308N	0.95	MC3340P		TDA1054	1.20	74LS42		74LS175	0.97	+ VÁT	
8080	5.08	703 (8 pin)	0.95	LM308	0.55	MEM 780		TDA1327	0.95	74LS47		74LS181	2.77		
	26.05	709 (8 pin)	0.35	LM318N	1.95	NE531N		TDA1352	1.35	74LS48		74LS188	0.44		
Z80	9.00	709 (8 pin) 709 (14 pin)	0.38	LM319H	2.25	NE540L		TDA2020	3.20	74LS49		74LS189	2.08		
6502	9.50	709 (T099)	0.45		3.87	NESSEN		TL072CP	0.95	74LS51		74LS190	0.86		
				LM322N					1.50	74LS54		74LS191	0.86	21L02	
E-PROMS		710 (8 pin)	0.36		0.50	NE556N		TL074CN		74LS55		74LS192	1.04		
1702AQ	5.16	710 (14 pin)	0.38	LM339N	0.50	NE560N		TLO81CP	0.45			74LS193	1.04	8 for	
2708	6.26	710 (T099)	0.45	LM348N	0.90	NE561N		TL082CP	0.95	74LS73		74LS193	0.86		
	24.00	711 (14 pin)	0.40	LM370N	2.90	NE562N		TL083CP	1.05	74LS74	0.27		0.86	£8.50	
2710	14.00	711 (T099)	0.87	LM371H	2.05	NE565N		TL084CN		74LS75		74LS195		70.70	
T.V. Controller		739 (14 pin)	1.80	LM373N	2.90	NE566N		UAA 170		74LS76	0.27	74LS196	0.97		
		741 (8 pin)	0.18	LM374N	2.90	NE567N		UAA180	1.98	74LS78		74LS197	0.97	10 400	THE R. P. LEWIS CO., LANSING
37790304	14.59	741 (14 pin)	0.35	LM377N	1.75	SAA 1024		ZN404	0.80	74LS83		74LS221	0.92	16 for	
		741 (T099)	0.42	LM 378N	2.05	SAA1025		ZN414	0.80	74LS85	0.81	74LS240	2.08	CHAE	
Buffers		747 (14 pin)	0.70	LM379S	3.75	SL414A		ZN417E	1.90	74LS86		74LS241	2.08	£14.50	100
74365	0.52	748 (8 pin)	0.33	LM380N8	0.85	SL440		ZN423T	1.05	74LS90	0.57	74LS242	2.08		
74366	0.52	748 (14 pin)	0.45	LM380N	0.75	SD6000V	2.98	ZN 424E	1.15	74LS91		74LS243	2.08		
74367	0.52	748 (T099)	0.48	LM381N	1.45	SN75491N	0.75	ZN424P	0.80	74LS92		74LS245	2.50	32 for	
74368	0.52	753 (8 pin)	1.50	LM381AN	2.50	SN75492N	0.85	ZN 425E	3.75	74LS93		74LS247	1.09		
81LS95	0.86	AY-10212	5.80	LM382N	1.20	SN76001N		ZN458A	1.35	74LS95		74LS248	1:09	£26.50	
81LS96	0.70	AY-1-5050	1.90	LM386N	0.78	SN76003N		ZN459CP	2.73	74LS96	1.16	74LS249	1.09	220.0	18.8
81LS97	0.86	AY-1-5051	1.45	LM387N	0.95	SN76008K		ZN1034E	1.90	74LS107		74LS251	0.96		
81LS98	0.70	AY-16721/6	1.95		0.95	SN76013N		ZN1040E	6.85	74LS109		74LS253	0.92	64 for	
8T26	1.90	AY-3-8500	5.00		2.25	SN76013ND		ZN1066E	5.85	74LS112		74LS257	0.92	04 10	1000
8T28	1.90	AY-5-1224	2.40		1.00	SN76018K		ZNA116E		74LS113		74LS258	0.92	£49.5	n
8T95	1.57	AY-5-3507	4.15	LM1808N	1.95	SN76023ND		ZNA 134J	26.95	74LS114		74LS259	1.39	249.0	U
8T96	1.57	AY-5-4007	1.10	LM1812N	5.40	SN 76033N	2.00	214/1/1/34/3	23.33	74LS122		74LS261	4.50	All excluding	VAT
8T97	1.57	CA3036		LM 1820N	1.00	SN 76532N	1.55			74LS122		74LS266	0.37		
8T98	1.57									74LS124		74LS273	1.70		
0130	1.37	CA3045F	1.40.	I LM 1830N	1.98	SN76544N	1.25			17760124	1.33		1.70) TDAD5	

ETI MAY 1980

THE BLACK HOLE

We proudly present the latest offering from Tim Orr, the prolific producer of music machines — the Black Hole Chorus Machine. It's capable of processing the output of both natural instruments and synthesisers. In addition to the chorus effect you can also choose genuine vibrato. That's not all — you can select a 'double' chorus option. The speed of both effects can be controlled manually. If you're not into knobtwiddling or you don't have a free hand or two, the Black Hole can be controlled by footswitch. Keep up with what's happening in music machines and much, much more in the next audio special issue of ETI.

KIT SURVEY

Across the length and breadth of this sceptred isle, there are companies producing kits of everything from power supplies and pin ball games to amplifiers and ignition systems. Want to buy a kit? How do you know who the supplier is, where he is, how reliable his product is and how much it costs? You could search through a dozen or so electronics magazines and spend a small fortune on postage to collect a library of catalogues.

Why don't you do it the easy way? Let ETI's fingers do the walking for you. Next month we get it all together - kits, suppliers, prices, quality - in an easy to compare format.

IMAGE CO-ORDINATOR

How to throw your voice without straining your vitals — build the ETI Image Co-ordinator. The clever co-ordinator takes your single vocal (or guitar, etc.) input and splits it in two. What can you do with two half voices? You can recreate a single sound image and make it move around, suggesting a few interesting stage and studio effects. The Image Co-ordinator uses two of the 1537A VCA chips introduced by Keith Brindley in March.

LED VU

Banish the bearings from your VU meters. Change over to a stylish LED display. Our LED VU meter is based on the LM3915, a chip which gives you VU or peak programme (PPM) options with bar or dot display. Look in next month to see the VU from ETI.

SERVO TESTER

Last month's Radio Control Fail—Safe stops your plane or boat disappearing into the sunset if you lose control of a channel, for whatever reason. When you get your plane or boat back onto dry land, a thorough systems check is number one on the list of things to do. A servo fails to operate. Is it the servo or the receiver? You can eliminate the servo by using our servo tester—an unusual and useful little piece of test gear.

SYNTHESISER

The Project 80 Modular Synthesiser returns with designs for the four filters most widely used in music synthesis - low pass, high pass, band pass and phase shift. They are four pole filters with one volt per octave control of their cut-off, or centre, frequency. Voltage control of signal regeneration is also included.

ETI APRIL 1980

ANALOGUE SWITCHING

Tim Orr, ETI's man of a thousand and one circuits, presents another of his astounding features. This time his subject is analogue signals. How to switch and with what.

There are many electronic functions that need to be able to turn off and on analogue signals just as they would be by conventional mechanical switches. The relay used to perform that task but it has almost entirely been superceded by electronic analogue switches. The relay is still in use but it is now generally used to handle heavy voltages and currents. A small version of the relay, the reed relay (Fig. 1), still has many advantages that have not yet been

overcome by electronic technology, these being very low contact resistance, virtually zero noise generation and distortion and almost total isolation between the control and switching section.

These features make the reed relay an ideal switch for high quality audio signal routing. The device drawbacks are, that it is physically large, heavy, expensive, consumes considerable power, is susceptible to vibrations and generates interference.

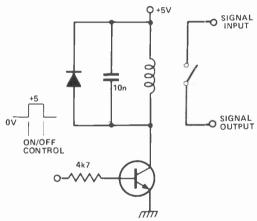
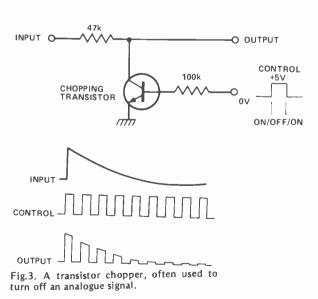
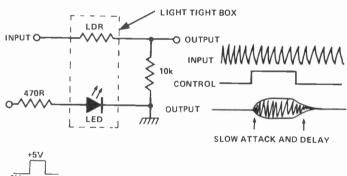


Fig.1. A typical reed relay.





OFF/ON/OFF

Fig. 2. A light dependent resistor can be used to make an analogue

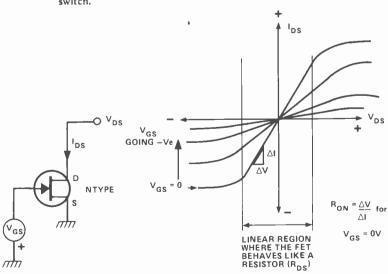


Fig.4. N-type JFET characteristics.

Dependable Resistor

A simple electronic analogue switch can be made from a light dependent resistor (Fig. 2). When light from the LED shines onto the LDR, the resistance drops from a few meghoms to a few hundred ohms. The device generates very little distortion and noise and is thus suitable for routing audio signals.

The response time of the LDR is very slow, sometimes taking 100 mS to switch, it is both relatively expensive and large and it consumes a large LED current. The transistor chopper, (Fig. 3), is often used as a simple device to turn OFF an analogue signal. This is done by turning ON the transistor and driving it hard into saturation, which in turn shorts the signal to ground. The transistor chopper is often used in organ and electronic piano circuits to produce audio tones by chopping the envelope waveforms with squarewaves generated by a tone divider network. It is not easy to use the bipolar transistor as a floating switch, as most applications require but the JFET lends itself readily to this purpose. The characteristics of a JFET (Fig. 4) show that in the region where the curves pass through the origin the device is behaving very much like a voltage control-

When V_{GS} is O V, the curve passing through the origin is at its steepest, the FET having at this point its lowest Drain Source resistance (R_{DS}), known as R_{ON}. This is typically a few hundred ohms.

However, as V_{GS} is increased negatively for an N type FET, the slope resistance increases until the pinch off voltage is exceeded. The FET is then 'PINCHED OFF' and the effective RDS is typically a few hundred meghoms. The JFET can be used as a variable resistance device changing from a few hundred ohms to a few hundred meghoms in times much shorter than a micro-second. This, combined with smallness of size, low cost, low power consumption, a very high impedance at its control input and the ability of the drain and source to float, makes the JFET an ideal analogue switch.

The series switch (Fig. 5) passes the signal with very little attenuation when the FET is on and stops the signal when the FET is off. There is a small stray capacitance (a few picofarads), between the drain and source and this causes high frequency breakthrough when the switch is off.

The shunt mode shorts the signal to ground when the FET is turned on (switch off). The attenuation in this mode is R/R_{ON} which requires large values of R to get a large attenuation. To get the advantages of both types of arrangement, a series/shunt switch can be constructed using two FETs (Fig. 6).

When a FET switch is rapidly turned on there is often a click generated, partly as capacitive breakthrough from the gate and partly as an abrupt amplitude modulation of the analogue signal. This can be greatly reduced by band limiting the gate voltage (C2. R3) and by removing any DC component from the analogue signal

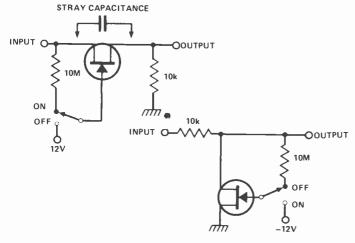
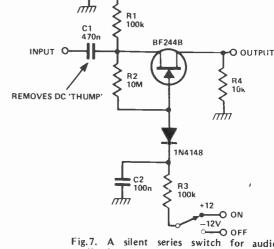
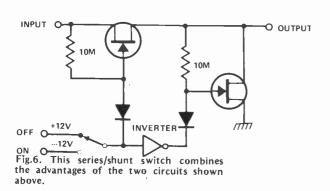


Fig.5. The series switch (top) passes the signal when the FET is on and stops it when the FET is off. The shunt switch (above) shorts the signal to ground when the FET is turned on.



applications.



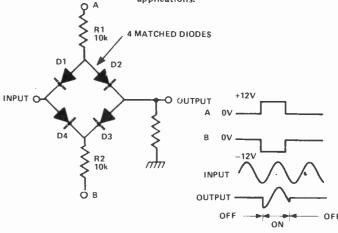
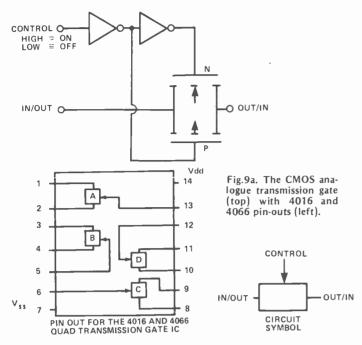
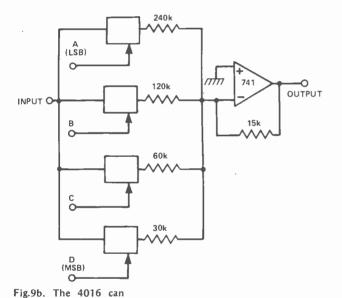


Fig.8. The diode ring switch can operate at very fast speeds.



* THE INPUT VOLTAGE MUST NOT EXCEED THE POWER SUPPLY VOLTAGE LEVELS OF THE 4016



be used to construct a 4-bit multiplying DAC.

Ring An Ode

The diode ring switch (Fig. 8) is very simple in concept and can be operated at very fast speeds. When A and B are both at O V no signal can pass through the ring switch because there is always a reverse biased diode in the route. When A is +ve and B -ve (both with same amplitude), then the 4 diodes are all conducting. Any voltage at the input of this bridge will cause the same voltage to appear at the output.

Switch In Packs

It is now possible to buy a wide variety of integrated circuits that perform analogue switch functions. There are perhaps over a hundred different types available, many of which are IFET configurations. These are usually rather expensive and I shall only discuss the more common (and relatively inexpensive) CMOS devices. The CMOS analogue transmission gate (Fig. 9) is a bidirectional switch element, having a relatively low on resistance of a few hundred ohms and a high off resistance.

The input and output terminals can float anywhere in between the power supply rails and the control input has a high input impedance. A high (logic 1) connected to the control input turns the switch on. To avoid distortion problems, the supply voltage should be kept as high as possible (10 to 15 V) and the load on the output above 10k. There are two commonly available analogue gate IC's, the 4016 and the 4066. These are both quad devices with the same pin-out, the 4066 has the lower RON resistance, typically about 100R.

Gain Code

The 4016 is a very versatile electronic building block. It can be used to construct a simple multiplying DAC (Fig. 9). The gain of the amplifier is linearly proportional to the size of the 4 bit digital code and can be programmed to give any one of sixteen gains. A low pass filter (Fig. 10) can have its break frequency programmed by switching in timing capacitors. When all the gates are OFF, the timing capacitors are 1n. The low pass filter can then be tuned by the dual gang pot over the range 1.5 kHz to 15 kHz. When gates B and D are on, the timing capacitor is 11n and so the frequency range is 150 Hz to 1.5 kHz. Also, when A and C are on, the timing capacitor is 101n and so the filter range is 15 Hz to 150 Hz. It is possible to build guite elaborate filter structures, fourth or even sixth order designs and to make them programmable with analogue switches.

The analogue switch can be used to modify the parameters of an integrator (Fig. 11). The integrator slew rate can be programmed by a combination of RA,B,C and the output may be reset to zero using gate D, which shorts out the timing capacitor.

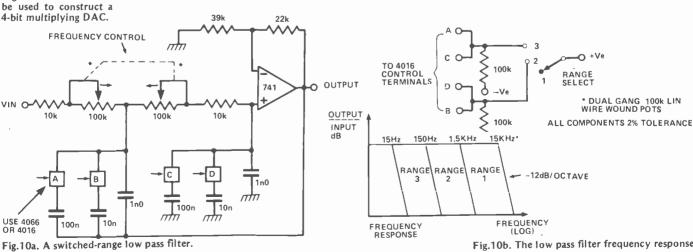
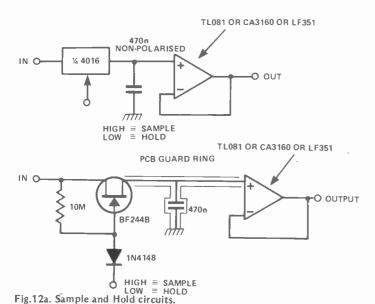


Fig. 10b. The low pass filter frequency response.

FEATURE: Analogue Switching



Hold On To It

Sample and Hold circuits also employ analogue switches. During the sample period, the storage capacitor is connected to the input voltage via the switch which is turned on. When the switch is turned off (Hold period) the voltage on the capacitor has got three possible discharge routes.

1. As leakage across the printed circuit board. This can be greatly reduced by provision of a guard-ring that surrounds the capacitor with a potential exactly the same as that on the capacitor. Surface leakage which is a function of potential difference is thus reduced by removing the potential difference.

2. The switch can discharge the capacitor with leakage currents. These are generally very small and insignificant.

3. The input bias current of the op-amp can discharge the capacitor, but if a FET op amp is used this effect can be insignificant. If all three discharge routes are small, then a long hold period can be expected.

More and Mode

The 4051 is an 8 way multiplexer (Fig. 13). This device has a 3 bit binary code input which it decodes internally to turn on one of the eight analogue switches. The 4051 is effectively an 8 way single pole, code selected switch. There is also an inhibit input; a logic 1 at this pin turns off all the switches.

There are some problems to be encountered when using this

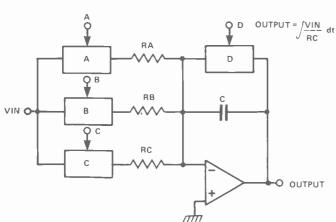
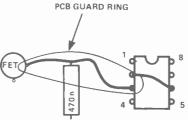


Fig.11. A programmable integrator with reset to zero.



IN/OUT

Fig.12b. A guard ring surrounding the capacitor can reduce leakage across the PCB.

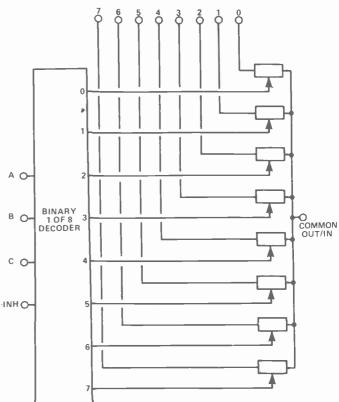


Fig. 13. A 4051 analogue 8-way multiplexer/demultiplexer.

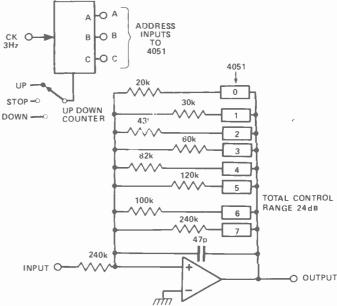


Fig. 14. An audio volume control with 3 dB steps.

device. The internal decoding exhibits some race conditions when the input address changes which may cause switches to momenta-

rily overlap in their ON states.

If the 4051 is used as demultiplexer with sample and hold outputs, then the data on each output capacitor gets spread around to other outputs during the overlap periods. This 'make before break' effect can cause serious problems to occur. (There are JFET 'break before make' multiplexers but these tend to be rather expensive).

Louder Yet

A programmable volume control can be constructed with a 4051 and an up down counter (Fig. 14). The state of the count at any point in time determines which resistor is in the feedback loop of the op amp. The resistors are arranged such that there is a 3dB change in gain for each LSB change in the address code. By making the counter count up the gain will increase and vice versa. It is necessary to stop the counter at 000 and 111 otherwise the gain will roll round giving an abrupt change in level.

It is possible to construct an 8 bit analogue Random Access

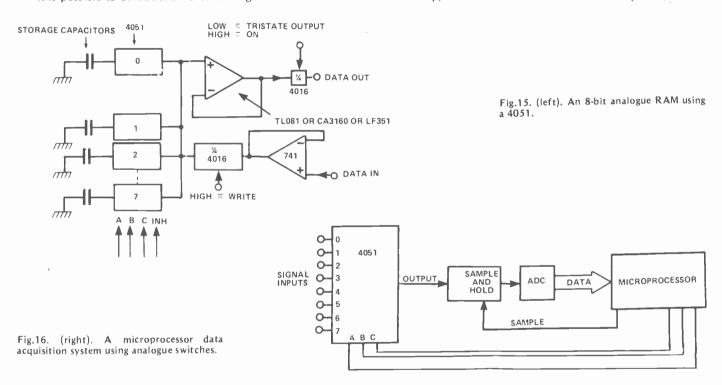
Memory using a 4051 (Fig. 15). Analogue information is written into memory by first selecting the address and then enabling the 'write' switch. The capacitor at this address is charged up to the voltage level of the data in signal. Reading is performed continuously using a FET op amp so as not to discharge the storage capacitors.

This gives the RAM a tristate output capability, which when used with the INH input allows several RAMs to be built into a larger memory system. Improved performance may be obtained by using 'break before make' multiplexers. An analogue RAM can be used for producing short time delays and perhaps some rudimentary pitch shifting.

MPUs Get Theirs

Analogue switches are used in microprocessor data acquisition systems (Fig. 16). An input multiplexer, addressed by the microprocessor selects which channel to look at. A sample and hold then freezes the selected input signal so that the ADC can perform a conversion on it. National Semiconductors make a single chip that performs most of this data acquisition.

The chip, the ADC0817 has a 16 channel multiplexer, an ADC



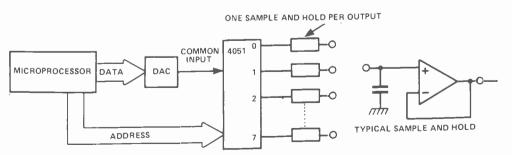


Fig. 17 (left). Analogue switches can also be used in a microprocessor data distribution system.

and output latch, but you have to provide your own sample and hold. Analogue switches are also used in microprocessor data distribution systems (Fig. 17). Data generated by the microprocessor is converted into an analogue voltage by the DAC and is then multiplexed into sample and hold circuits. This is a common technique for systems that require a large number of analogue parameters such as microprocessor controlled music and speech synthesisers.

Plexing Info

In most telecommunication systems, a major cost is that of the wire that links transmitter to receiver. If several channels of information can be transmitted down one wire then the cost of the overall system may be considerably reduced. (Fig. 18).

Eight audio channels, band limited to 10 kHz in this example, are fed into an 8 way analogue multiplexer. Each channel is sampled every 50 nS for a duration of 6.25 nS. The eight audio signals can thus be fed down one wire pair as a sequential series of pulses that represent the instant values of the signals in the eight channels. The process is known as Pulse Multitude Modula-

tion (PAM). Sync pulses are mixed with this signal so that the channels may be decoded at the receiver end.

Decoding is performed by stripping off the sync signal and using it to address the demultiplexer. The required channel can then be selected by monitoring the respective demultiplexer output with a sample and hold followed by a 10 kHz lowpass filter. It is important that the sampling frequency is at least twice the audio bandwidth so that aliasing effects can be avoided.

Mixing It In

Monitoring the signal levels in an audio mixer can cause problems, due to the large number that have to be observed. There are now several devices that use a conventional oscilloscope or TV to display all the information on one screen (Fig. 19). Each audio channel is processed by a peak detecting envelope follower. This generates a signal that describes the peak signal amplitude in that channel and it is known as a PPM (peak programme) response. These PPM signals are then multiplexed and passed through a single log compressor to give a display of level in dBs versus channel number on an XY screen.

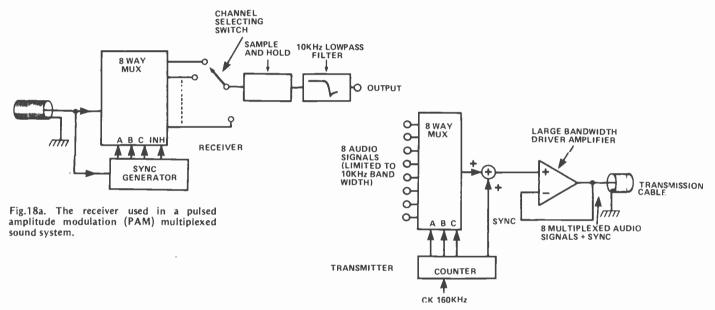


Fig. 18b. The multiplexed sound system transmitter

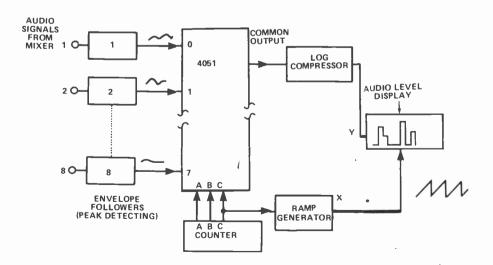


Fig. 19. (left). The levels of any number of mixer channels can be displayed on one screen with this multiplexed system.

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160 IF PRINT DIJJECT THEN GO TO
24 LET PRIJJECT
25 LET RITJECT
26 LET RITJECT
27 LET KEJ-1
37 IF KK; THEN GO TO 16

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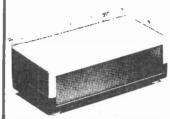
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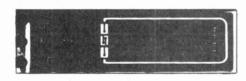
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RADIO CONTROL GUARDIAN

A superb project for the radio control enthusiast. This unique unit automatically sets as many as four servos or other control units to pre-set 'safe' positions in the event of control-signal loss. The unit has four channels, each with fully independent fail-safe control.

adio control fail-safe units are intended to be connected between the radio control receiver/decoder and the system's servounits. Under normal operating conditions the decoded command signals pass straight through the fail-safe unit, enabling the servos to operate in the normal manner. If, however, the command signals are lost (because of a system failure or by the receiver going out of range), the fail-safe unit automatically feeds internally-generated pre-set command signals to the servos and causes them to move to pre-set 'safe' positions.

In a boat or a plane the fail-safe unit may, for example, cut the speed and put the craft into a gentle turn in the event of control failure, thus ensuring that the craft does not simply disappear into the wild blue yonder. In reality, only the most important of the system's servos need to be subjected to fail-safe control, so a four-channel fail-safe unit is more that adequate for all practical applications.

Fail-safe units are already available commercially but all of them suffer from a number of defects. The Chromatronics PP1M-4CH is one example. This 4-channel unit measures only 41mm x 62mm x 23mm and is highly recommended for use in craft with limited space and/or limited weight carrying capacity. Specific defects of the PP1M-4CH, however, are that it gives failsafe operation only in the event of TOTAL signal failure on all four channels and gives no fail-safe operation if any one of the decoder output channels locks high. Also, all the servos are pulsed simultaneously (rather that sequentially) in the fail-safe mode, thus generating high (and possibly harmful) transient currents in the system.

The ETI fail-safe unit described here has been designed specifically as a 'De-Luxe' unit that it gives a virtually fool-proof performance. It is probably the most advanced fail-safe device ever published. It has four FULLY INDEPENDENT channels, each giving fail-safe operation if its own

decoder input signal is lost or latches high. The servos are pulsed sequentially (rather that simultaneously) in the fail-safe mode, ensuring that excessive transient currents are not generated in the system. Also, the fail-safe frame width is adjustable, enabling the unit to be used with electronic motor-speed control units as well as with all types of servo.

The performance sophistication of the ETI fail-safe unit necessitates the use of a total of six ICs in the design. The unit is in fact built up on two PCBs which, when stacked, give overall dimensions of about 52mm x 90mm x 25mm (uncased), making it roughly twice the size of the Chromatronics PP1M-4CH. The unit is thus suitable for use only in craft with a fairly substantial amount of free space. The unit can be used with any 3 to 9 volt positive-pulse radio control receiver producing nominal pulse widths of 1 to 2 milliseconds (the 'standard' range) and can control virtually all types of 3-wire servo.

Construction & Use

This is not a project for the beginner. Construction calls for a good deal of care. The first point to note is that one of the PCBs is double sided, so unless you are really good at making your own PCBs you'll have to wait until ready-made boards become available from one of our advertisers. Assuming that PCBs are available, double-check all their tracks to make sure there are no breaks or shorts, particularly on the double-sided unit,

Start construction with the double-sided PCB. Use miniature components throughout. Note that the three ICs are CMOS types (normal 555s must NOT be used in the IC5-IC6 positions) and should be mounted in suitable sockets. If you have a 'scope you can give the completed PCB a functional check by connecting it to a 6 volt battery supply and checking that pulses with 1:3 mark/space ratios are available at outputs R4-R8-R12-R16 and a variable 4-

pulse train is available at the R17 output.

Construction of the double-sided PCB calls for extra care. Veropins or similar must be pushed through the board in various places (see overlay photos) and used to connect the upper and lower tracks by soldering to both sides of the PCB. Use miniature components throughout the rest of the assembly procedure, taking care to observe the polarities of all devices. The three CMOS ICs can be mounted in suitable sockets. When assembly is complete decide on suitable casing arrangement (we favour the idea of stacking the boards in a home-made box) and then set about interconnecting the two PCBs. Seven interconnection leads are required and their positioning requires particular care, with constant reference to both the circuit diagram and the overlay. There are two power supply interconnections and five interconnections to resistors 4-8-12-16 and 17.

When construction is complete, set RV5 to mid position and give the circuit a quick functional check by connecting a servo and suitable supply to channel 1 (A) output and check that the servo position can be varied via RV1. If all is well, recheck the servo functioning on channels 2 (B), 3 (C) and 4 (D), using RV2, 3 and 4 respectively to give control.

The procedure for fitting the completed unit into an installation is quite simple. The unit connects between the receiver/ decoder outputs and the servo inputs. When installation is complete switch the receiver on and the transmitter off and adjust the fail-safe unit's pre-sets to set the servos to the desired fail-safe positions. Finally, switch on the transmitter and confirm that the system responds to normal remote control and reverts to fail-safe when control is removed.

BUYLINES.

All components used in the R/C Fail-Safe unit should be readily available from major stockists.

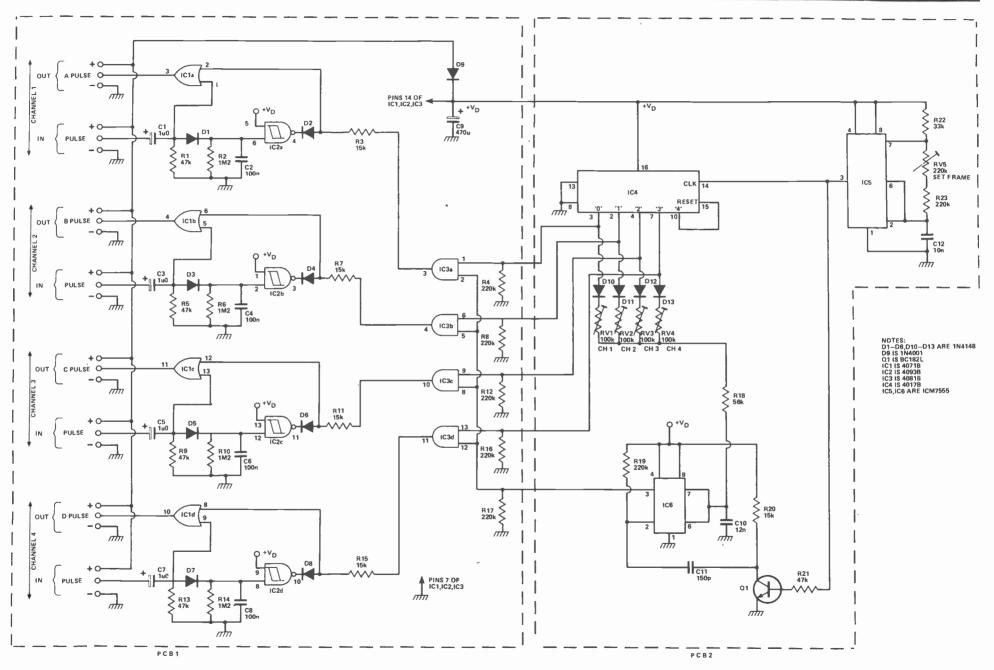


Fig.1. Circuit diagram. Dotted lines show which components are mounted on each PCB.PCB A left, PCB B right.

In a conventional multi-channel 'proportional' radio control system a variable-width (1-2 mS) pulse is passed to each servo via the transmitter-receiver-decoder 'link' roughly once every 20 mS (the 'frame' time.) The pulse width of each channel is variable at the transmitter (via joy-stick, etc) and determines the position of the servo. At 1 mS the servo may, for example, be full left, at 1.5 mS 'neutral' and at 2 mS full right. If the servo command signals are lost (due to system malfunctioning or because the receiver goes out of range) the servos simply lock into their existing positions, causing the craft to either crash or sail off into the wild blue yonder. Fail-safe units are designed to prevent such mishaps and automatically set the servos to pre-set 'safe' positions in the event of signal failure.

Our fail-safe unit incorporates a fourchannel sequential pulse generator (IC3-4-5-6 and Q1) and four independent 'automatic data selection' networks, each built around one quarter of IC1—IC2. These data selectors feed command signals to their respective servos directly from the receiver decoder if the radio control system is functioning correctly or from the internal pulse generator if a system defect (loss of command signal) occurs. Each channel takes about 60 mS to switch from the 'normal' to the 'fail-safe' mode.

The internal pulse generator functions as follows. IC5 is a low voltage astable which feeds clock pulses to a divide-by-four counter with four decoded outputs designed around IC4. The action of these two ICs is such that the four outputs of IC4 switch high (one at a time) sequentially with a repeat or 'frame' time that is variable between 12 mS and 24 mS via RV5. The IC5 clock signals also trigger monostable multi IC6 via Q1 and the timing periods of the mono are controlled sequentially by

the RV1 — RV4 pulse-width presets as the system clocks through each frame. The circuit thus sequentially generates a series of four independently adjustable pulses. Each of these pulses is steered to its own independent output channel via the IC3 circuitry. Thus, each of the four IC3 output signals consists of an independently pre-settable pulse.

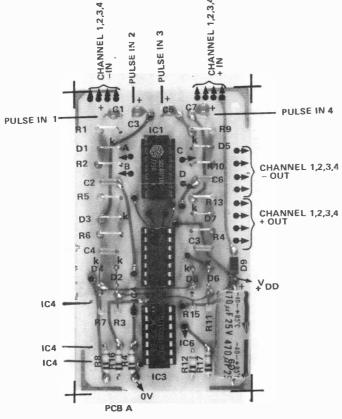
The 'automatic data selection' circuitry consists of four identical and independent networks. Let's take the example of the channel 1 network. The circuit consists of an input signal detector (C1-R1-D1-R2-C2), a pulse selector (IC2a-D2-R3) and a servo driver (IC1a). If decoded input pulses are available they are passed through blocking capacitor C1 and fed to one input of servo driver IC1a. Simultaneously, the input signals charge C2 via D1 and the resulting DC drives the output of IC2a low, thereby removing the internally generated fail-safe

pulses from the IC1a input. Thus, only the input pulses are presented to IC1a input and are fed directly through to the servo.

If the input command signals are lost, the bias voltage is no longer generated at the input of IC2a, so its output goes high and enables the internally generated fail-safe pulses to be fed to the input of IC1a and thence on to the servo. Blocking capacitor. C1 ensures that the unit will switch to the fail-safe mode even if a decoder output locks into the 'high' position."

Note that the fall-safe channels of this system are fully independent, so if a control signal is lost on (say) only a single channel, that channel will go to fail-safe but the remaining channels will retain normal operation. Also note that, as is normal practice, the unit is powered from the receiver/servo battery via the decoder/servo harness connections. The supply is, however, decoupled via D9—C9.

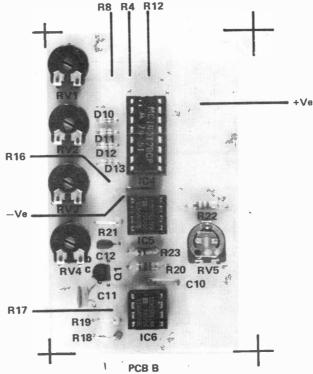
DADTC LICT



= Pin through

= lead out

Fig.2. PCB A component overlay (left). PCB B component overlay (right).



	/ 11(10 110 1 110 1
RESISTORS R1,5,9,13, 21 R2,6,10,14 R3,7,11,15, 20 R4,8,12,16, 17,19,23 R18 R22	47k 1M2 15k 220k 56k 33k
POTENTION RV1-4 RV5	METERS 100k 220k
C2,4,6,8 C9 C10	RS 1u0 35V tantalum 100n ceramic 470u 25V electrolytic 12n polycarbonate 150p ceramic 10n ceramic
SEMICOND	UCTORS (all CMOS ICs are 'B'
IC1 IC2 IC3 IC4 IC5,6 Q1 D1-8, 10-13	4071 4093 4081 4017 ICM7555 BC182L 1N4148 1N4001

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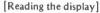
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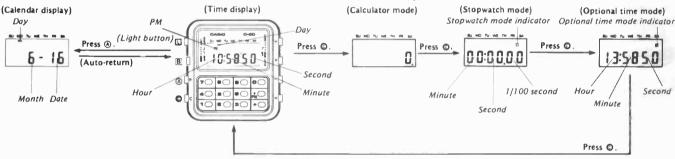
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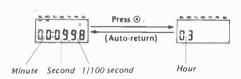
® RESET BUTTON ii 00:09,98 (A) @ LAP BUTTON START/STOP 000 BUTTON

(Working range)

The stopwatch display is limited to 23 hours 59 minutes 59 seconds 99.

[Stopwatch operation]

Thereafter it can be reset and started again. The hour digits can be shown by pressing the A button.



A function command sign

[Calculator operation]

Appears when a number is set as a constant.

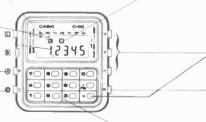
Indicates that the last 2 digits can be shown.

8-digit entry (7-digit for negatives) can be made.

of the display becomes 7 or 8 digits. Clears entry for correction.

Shows the last 2 digits when the content

Releases overflow or error check.
Overflow is indicated by an "E" sign and stops the calculation.
Overflow occurs when the integer part of an answer, whether intermediate or final, exceeds 8 digits (7 digits for negatives).



Perform the four basic calculations. An incorrect function command is corrected by pressing the correct button.

Obtains answer

Enter numerals For decimal places, use the ① key in its logical sequence.

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DESIGNER'S NOTEBOOK

In this month's 'Notebook' project editor Ray Marston takes a peek at the fascinating world of 'touch switch' technology.

f you ever get involved in the design of electronic equipment, there is a fair chance that you will eventually come accross a circuit that requires the use of a 'press-to-do-something' switch. You'll then have to decide whether to use an electro-mechanical push-button switch or a solid-state 'touch' switch to do the job.

The main disadvantages of the push-button switch are that it is unreliable, tends to be a bit expensive and is available only in those designs that manufacturers care to produce. These switches are also 'noisy' in that they generate contact-bounce spikes that can play

havoc with fast digital circuitry.

This last mentioned problem can be overcome by using the 'debouncer' circuit of Fig 1. Here, one quarter of a 4093B CMOS quad 2-input NAND Schmitt is used as a simple Schmitt trigger. When PB1 is closed, C1 charges rapidly to full supply volts and the Schmitt output switches high: When PB1 is released C1 discharges slowly via R1 until eventually the Schmitt output switches low again. The circuit is thus unaffected by switch contact bounce and produces a clean on/off signal at the Schmitt output.

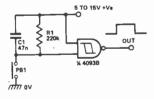


Fig.1. Push-button debouncer circuit.

Fig. 2 shows a useful way of obtaining a toggle (alternate on off) action from a simple push-button switch. The switch signal is debounced by R1-C1 and is then used to clock one half of the 4027B dual JK flip-flop, which divides the clock signal by two. Thus, the 4027B output goes high on one press, low on the next, high on the next and so on. Two of these toggle switches can be built from each 4027B IC.

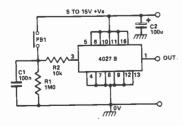


Fig. 2. Push-button toggle switch.

Touch Switch Circuits

The main advantages of solid-state switches are that they are reliable (they have no troublesome mechanical parts), can be less expensive than their electro-mechanical counterparts and can readily be produced in almost any shape or form that the designer or home constructor wishes.

Touch switch circuits come in three basic types (ignoring 'freak' circuits such as thermo-switches, etc). The crudest and least attractive of these are the 'resistive' types, which use the 'touched' or 'untouched' resistance change that occurs between two adjacent

touch contacts to give activation.

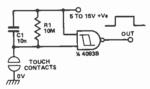


Fig.3. Resistive touch switch.

Fig. 3 shows a typical resistive touch switch circuit. Normally, with the contacts untouched, R1 holds the Schmitt input high and its output is low. When a finger is used to bridge the two contacts the resulting skin resistance (less than 3MO) pulls the Schmitt input low and drives its output high. C1 is used to 'debounce' the circuit. Fig. 4 shows how the circuit can be modified to give 'toggle' action.

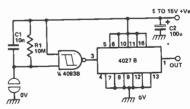


Fig.4. Resistive touch toggle switch.

A very serious disadvantage of the resistive touch switch is that it can be disabled by moisture or contamination bridging the contacts. Also, it may be disabled by persons with damp fingers or may be immune to operations by persons with very dry skins.

A great improvement in reliability is given by a second type of 'hum detecting' touch switch. This type of circuit relies for its operation on the fact that the human body acts as a kind of antenna

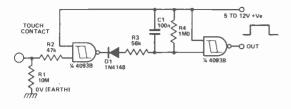


Fig.5. Hum-detecting touch switch.

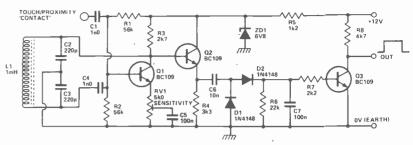


Fig.8. Damped oscillator touch/proximity switch.

that is coupled to the mains and carries a high-impedance mains signal. Fig. 5 shows an example of this type of circuit. When the input contact is touched the hum pick-up signal is fed to the input of the first Schmitt stage via limiting resistor R2 and produces a full-amplitude square wave at the Schmitt output. This square wave is converted to DC and debounced by the D1-R3-R4-C1 network and drives the final output of the second Schmitt high. The Schmitt output goes low again some 60 mS after the input touch is removed. Fig. 6 shows how the above circuit can be modified to give toggle operation: D2 and C2 prevent unwanted feedback from the 4027B to the Schmitt.

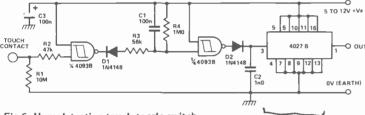


Fig.6. Hum-detecting touch toggle switch.

Capacitive Touch/Proximity Switches

The third and most important class of switch are those that work on the capacitive loading principle. In most simple cases, these circuits rely on the fact that the human body acts as a small capacitor that is earthed at one end. The actual value of capacitance depends on physique and on environmental conditions, but is reckoned to have a value of 150 - 300 p under normal domestic/industrial conditions.

Fig. 7 shows a number of basic ways of using the body capacitance effect. In Fig. 7a it causes loading of an HF oscillator, in Fig. 7b it causes capacitive potential-division and in Fig. 7c it causes filter-

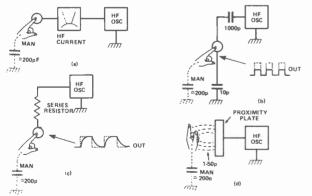


Fig. 7. Body capacitance effects on a touch contact. (a) Causes oscillator loading, (b) capacitive potential divider action or (c) degradation of oscillator waveform (harmonic filtering). (d) If contact is of sufficient area, loading and other effects can be obtained without physical contact, by capacitive or proximity coupling.

ing of oscillator harmonics. Of particular interest is Fig. 7d, which shows that these effects can be obtained without physical contact, by capacitive or 'proximity' coupling.

Fig. 8 shows the practical circuit of a touch/proximity switch that works on the oscillator damping principle. The oscillator is a Colpitts, working at about 300 kHz. RV1 is carefully adjusted so that oscillation is barely sustained when the contact is untouched. Under this condition the rectified output of the oscillator drives Q3 to saturation and holds the circuit's output low. When the contact is touched the resulting capacitive loading kills the oscillator, causing Q3 to turn off and switch the output high. The output has relatively slow rise and fall times, but can be speeded up with a Schmitt circuit if required.

The zero volts line of the Fig. 8 circuit should (ideally) be of out grounded. The touch contact must be made from a conductive material, but can be any shape or size that is desired: in most cases the 'contact' face can be covered with an insulating material without detracting from the circuit's performance. Pin-head sized contacts will require actual-contact operation, but 'contacts' with surface area of a square metre or so can be proximity-operated at ranges up to 20 - 40 cms.

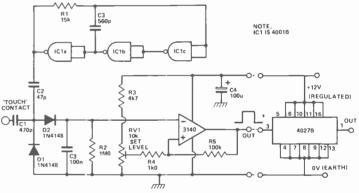


Fig.9. Capacitive-divider touch switch (left) with modification for toggle operation (right).

Finally, Fig. 9 shows the circuit of a touch switch that works on the capacitive-divider principle. Here, IC1 is wired as a ring-of-three oscillator working at a frequency of a few hundred kHz. The oscillator output is fed to a capacitive potential divider formed by C2 and the stray capacitance around D1 and the touch contact. The resulting potential divider output signal is rectified by D1-D2-C3-R2 and fed to the 3140 regenerative voltage comparator, which is adjusted (via RV1) so that its output is just switched to the low state when the input contact is untouched. When the contact is touched, the resulting capacitive loading increases the effective capacitance of the lower half of the potential divider, thereby reducing the divider's output voltage and causing the 3140 output to switch high. Fig. 9b shows an add-on section that can be used to convert the circuit to toggle operation

As in the case of the Fig. 8 circuit, the zero volt line of Fig. 9 should be grounded. The touch contacts can again be any desired shape or size.



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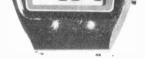


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AUTOMATIC BATTERY CHARGER

A 12 volt battery charger project that automatically switches to a 'trickle charge' mode when the battery reaches full charge. The circuit can be built as a stand-alone project or can be used to up-date an existing charger.



onventional car battery chargers are simple and inexpensive devices which continuously charge the battery (at a rate of a few amps) for the duration of the switch-on period. The owner has to occasionally check the state of the battery with a hydrometer and switch the charger off when the battery reaches the 'fully charged' state. If the owner does not switch the charger off the battery will overcharge and its electrolytic solution may eventually be lost through evaporation or the cell plates may buckle and destroy the battery.

Our ETI battery charger overcomes the deficiencies outlined above. It incorporates an electronic charge-state sensing and feedback control network which causes the battery to charge at maximum rate until full-charge is attained, at which point the charger automatically switches to 'trickle charge' mode which maintains the battery in the fully charged state indefinitely. A red LED illuminates when the battery is fully charged.

Our charger is designed to charge 12 volt batteries only. The unit can either be built as a self-contained 'stand-alone' project, complete with transformer and case,

etc, or alternatively the electronics can simply be added to an existing charger unit, to update a conventional design. We have included the circuit of a typical 'conventional' charger, for comparison purposes.

Construction & Use

Construction of the unit should present few problems. If you decide to build the complete 'stand alone' project, assemble the PCB components exactly as shown in our overlay, noting that the two LEDs are mounted off-board. If you decide not to fit the optional meter (a difficult-to-get component, which MAY be available from some car accessory shops) short the two M1 connections together using heavy gauge wire.

If you decide to simply use the automatic charger circuit to update an existing battery charger, omit BR1 from the PCB and take the outputs of your existing charger rectifier directly to the appropriate '+' and '-' points on the PCB track. Whichever version of the unit you decide to use, be sure to use a reasonably heavy gauge of wire for the main interconnections.

When construction is complete, turn RV1 slider fully to the 'ground' position and give the unit a functional check as follows.

1 Check that, with no battery connected, both LEDs illuminate.

2 Connect a car battery into place on the charger. Check that LED No. 2 turns off and that a charge current (typically 2 to 4 amps) flows to the battery.

3 Rotate RV1 and check that LED No.2 can be turned on and the charge current cut off via the pot.

4 Return RV1 slider to the 'ground' position and charge the battery up using the normal 'hydrometer' technique. When the battery reaches full charge, carefully adjust RV1 so that LED No. 2 just starts to turn on and the charge current falls to a 'trickle' level of a few hundred milliamps.

If RV1 is correctly set, you'll find that on subsequent charges LED 2 will first start to flicker as the 'full charge' level is attained. The LED will subsequently turn on at reduced brightness or will alternatively cut on and off as the 'fully charged' state is maintained. RV1 should require no further adjustment throughout the life of the charger.

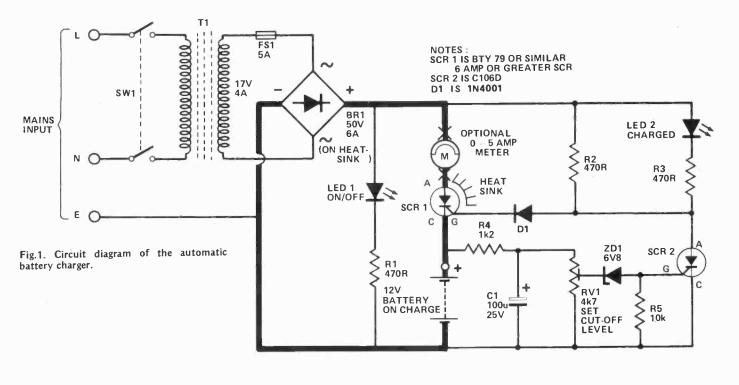
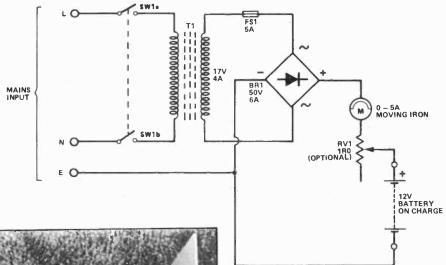
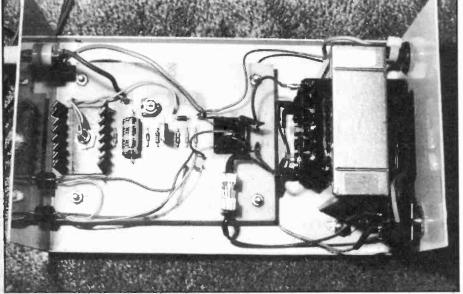


Fig. 2. (right). For comparison we have included the circuit diagram of a conventional charger.



(Below). The PCB and transformer installed in a suitable case. Note the heatsink on SCR1.



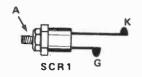


Fig.3. Connections to SCR1, the BTY79.

HOW IT WORKS

In a conventional battery charger (see diagram) the unsmoothed full-wave rectified output of a 17 volt transformer is fed to the battery via a moving-iron 0-5A monitor meter. The battery is charged by a 'pulsed' current at a rate determined by the differential voltage between the battery and the charger and by the total series resistance of the circuit (the effective resistance of the transformer, rectifier, meter and battery). A 'flat' battery has a low terminal voltage and typically draws an initial charging current of about 4 amps, falling to about 2 amps as the terminal voltage rises to the full charge value. The total series resistance of the circuit is usually sufficient to limit the charge current to a safe value: 'De Luxe' battery charger sometimes have a low-value rheostat in the series network, enabling the charge rate to be varied over a limited range. You'll notice from the above descrip-

tion that the battery terminal voltage rises as the battery charges up and can thus be used to give an indication of the state of charge of the battery. This fact is put to practical use in our automatic battery charger, which operates as follows.

Silicon controlled rectifier SCR1 is

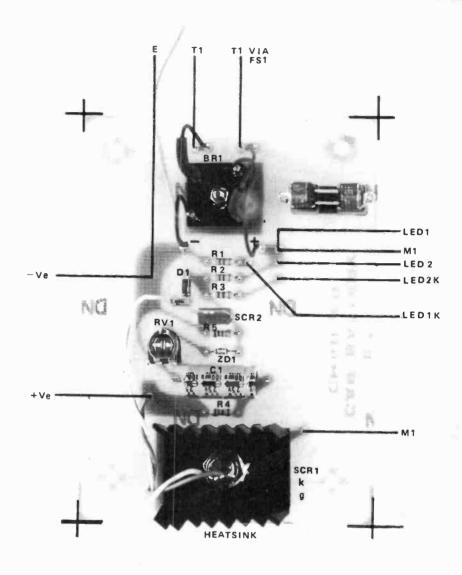
wired in series with the battery circuit and can be gated on via the R2-R3-LED 2 network: this network can be disabled by gating on SCR2. The battery terminal voltage is monitored by the R4-C1-RV1-ZD1 network and turns SCR2 on when the terminal voltage exceeds a value pre-set by

When a 'flat' battery is first put on charge its terminal voltage is low. Under this condition SCR2 is cut off and SCR1 is gated on in each half cycle via the R2-R3-LED 2 network. SCR1 acts as a simple rectifier under this condition and the battery charges at maximum rate: the forward volt drop of SCR1 is only a few hundred millivolts and is insufficient to turn

As the battery charges up its terminal voltage rises. If the terminal voltage rises above the trip level pre-set by RV1, SCR2 is gated on via ZD1. Under this condition SCR2 removes the gate drive from SCR1, which turns off and no longer passes a charge current to the battery: LED 2 is turned on via SCR2 and R3, indicating that the battery is fully charged.

In practice, the terminal voltage of the battery depends on both the battery state and the magnitude of the charging current and decreases when the charging current is removed. Consequently, the circuit does not abruptly stop providing a charging current when the battery reaches full charge, but goes into a progressive skip-cycling mode, which progressively reduces the mean charging current to a low 'trickle' value. This action automatically maintains the battery in a fully charged (but not overcharged) state.

The correct setting of pre-set pot RV1 is established Initially by charging the battery up in the conventional (hydrometer, etc) manner until it reaches the fully charged state. RV1 is then carefully set so that the charger goes into a skip-cycling or trickle-charge mode under this condition. The RV1 setting is then valid for all sub-sequent 'automatic' recharging actions. Current monitor meter M1 is an entirely optional component in this circuit.



PARTS LIST

RESISTORS R1,2,3 470R

POTENTIOMETERS:

4k7 preset

CAPACITORS :

100u 25V electrolytic

10k

SEMICONDUCTORS:

BTY 79 C106D SCR1

SCR2 1N4001 ZD1 6 V8 400 mW

LED1,2 TIL220 200V @ 6A BR1

MISCELLANEOUS: Charger transformer CT4, 5A fuse, dPdT Toggle, instrument case, H 95, W 125, D 220mm.

Fig.3. Component overlay. Short the meter connections together with heavy gauge wire, if you decide not to fit the meter.

ETI

BUYLINES

All components used in the Battery Charger are available from major stockists. The Charger transformer can be obtained from Electro Value.

Greenbank

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development system is almost essential. however in the past to understand more than one several separate development systems have had to be purchased. The reason that separate systems, one for each processor, have been necessary is due to the fact that individual microprofessors have their own individual seatures in one case to secremently a separate read strobe and write strobe is required, in another a load /write, line is used in combination with a combined strobe called valid memory aseparate read strobe and write strobe is required, in another a load /write, line is used in combination with a combined strobe called valid memory address and phi-2. With some processors, this more processor, this makes it more difficult to graft some other unrelated microprocessor onto the same bus at a later date. A Universal Micro System provides a basic bus structure on which any one microprocessor can be connected. The system uses a CPU (Central Processor Unit) card which is separate from the rest of the system, and this allows the same memory and interfaces to be retained when a different MPU is, used. The basic system bus consists of data and address bus stongent with read and write strobes. By locating the data input (Keyboard) and output (VDU) in the memory space then such chips as the 8080/280 family, which normally use unjut /output ports, can now be used without any fundamental change to the bus fand as a bonus, users of these MPU is have all the ports entirely like the formal ports and the same man of the port of the larger power PSU A power supply, which normally use unjut /output ports, can now be used without any fundamental change to the sus fand as a bonus, users of these MPU is have all the ports entirely like for their own purposes).

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а	4019	480	4059	£4.80	40107	68p			4509	£1.84
-1		99p	4060	£1.15	40108	£5.36	4506	51 p	4560	
	40 20		4061	£15.67	40109	£1.02	4507	55p	4561	65p
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AUDIOPHILE

Ron Harris goes gardening with some rogue speaker boxes and shifts his sights to budget hi-fi.

round the middle of this month I got lost. Nothing unusual in that, you may say, some of the best people get lost from time to time. This was in the country though, surrounded by all these woolly pre-packed lamb chops and things. Healthy things too, like fresh air, grass and circular brown patches of earth that heave up and drown your shoes when you step in them...

Being of sound mind and thirst, the first thing I do when lost is head for a pub. One of Britain's real strong points that is, regardless of where you are or who you are, you're never more than half-anhour from a pint of bitter and a barmaid.

Sure enough after about ten minutes of 40 MPH down these 'roads' a suitably shaped building loomed in the headlights. All would be well now, with a pint inside us and some worldly words of wisdom from the friendly landlord we'd soon be heading back into civilisation.

Oh veah?

This pub turned out to be the one Hammer films line up werewolves outside for howling practise. Weird it was, surrounded by a massive car park which was totally devoid of cars. Just the wind and us.

Once inside I suppose it wasn't that bad, empty but not bad. The only customer was the 'local character', otherwise known as the tramp, a little lumpy old man whose party trick turned out to be saying 'Hello Sailor' in ten languages. Probably explains the lumps. Stranger yet was the manner in which music issued forth into the bar. Had they been playing church organ or choir stuff I'd had been across those fields faster than the Russians in Afghanistan.

No speakers you see. A nice plain ordinary music centre, being played by a nice plain ordinary barmaid and nice plain ordinary music, but no speakers. We searched the place, - plenty of pretty beams and dead animals around the walls, but no speakers. Upon enquiring at the bar I was informed by a suspicious look, a grunt and a wave which took in half the known Universe, that they were 'over there'

Not wishing to look too ridiculous, I looked around again. Slowly it dawned that the only things in approximate position to be producing sound were two massive cylinders covered in greengrocers grass! From zero feet away it became clear that was indeed the source of the treble-less thudding which prevaded the building.

Green Green Grass of Ohm

Oh my God! A closer look into these apparitions acquired overwhelming importance. 'In the name of Audiophile, I command thee - revelest unto me thine drive units.....' sort of thing.

Anyway, while our illustrious Art Director distracted the barmaid - a brilliant tactical maneouvre involving a pint glass, the tramp and two felt tip pens - I managed to peel back the turf a little. Inside resided three KEF B200s and a T27, no crossover, and no padding. The tweeter pointed up out of the top of the cylinder while the mid-ranges units attempted to push the rest of the sound straight through the grass, failing miserably.

A great deal of work had obviously gone into the construction

of these enclosures and no doubt someone somewhere thought that grass finish attractive. The end result was nothing short of an horrific treble free thudding which occasionally coincided with the music.

As I've no idea where the pub is, short of saying it's somewhere north of London but south of Colchester, at least I ain't gotta go back and be thudded at.

If there's a moral to this tale at all it must be to avoid homebrew speakers, even in pubs.

Budget Time

Three hundred pounds is not a lot by today's standards. Right now it buys you 1/20z of gold, or maybe the rear bumper of a new car. Once upon a time (of inflation) it would have bought you a very nice little hi-fi too, although to-day around five hundred is more like an average starting price.

However, the arrival at ETI of a JVC amplifier, the AS5, with a retailing price of around £85 and a nice sound indeed provoked some debate as to how possible it is to assemble a complete (record playing) system of good quality for that £300.....

That then, is the starting point for the system described here. All in all, at present prices, the outfit totals between £293 and £327 depending on the state of your discounts.

Giving names to it all produces a list which looks a little like:-

TURNTABLE: JVC QLA5R - quartz lock, auto return. Wow/flutter 0.04% DIN. s/n 75dB DIN.

CARTRIDGE: CORAL 555E - elliptical stylus. Compliance = 15/20 cu. FR. 20-20 k = 2 dB. output 4 mV (5 cm/sec)

AMPLIFIER: IVC AS5 - 30W rms at 0.06% thd across 20-20 kHz phono:- 2mV/47k, overload 150mV, s/n 70dB.

SPEAKERS: VIDEOTONE GB2 - 5OW (RMS) power holding, two unit ported design.

OK, so I know that there is nothing British in there and that the Goldring G900E and any one of several British loudspeaker manufacturers have good reason to feel left out, but then most of those products have been reviewed to death elsewhere and the components employed here all have a great deal to offer in their own right.

So no Union Jacks in the post, eh? (I've got one anyway!) Photographs of Felicity Kendal are of course perfectly acceptable...

Around a Roundtable

The turntable, JVC, QLA5R, is fairly new and retails at the £100 mark. For that you acquire an auto-return quartz-lock machine with a good (but flimsy) construction and the possibility of varying the speed, should you so desire, by $\pm 6\%$. Quaintly entitled a pitch control, this facility is even endowed with some nice little lights to show how far away from the correct speed you are.

All these speed change facilities have one thing in common they are totally and utterly useless. Better to have spent the pounds on a more solid plinth. A turntable that goes around at 29 or 37 RPM is wrong, whether by design or not.



can see the finish is to a very high standard and good adjustment is provided on the pickup arm. Noise level from the deck was around the -45 dB mark under test and no meaningful comment could be made about the quartz-lock speed control - except that is is accurate! Experiments seemed to suggest that this deck is a good partner for low compliance moving coil cartridges.

The arm is of a good standard with high quality bearings and a nice range of adjustments - unusual on an automatic in this league. The turntable switches on as you move the arm from the rest, and is turned off once the arm returns, its duty done.

The strobe markings around the rim are machined into the platter itself and, having sharp edges, are the best reason you'll find for not touching the deck until it has stopped! (I've got the scars to prove it, too).

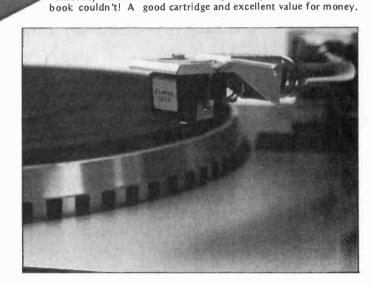
At first I was less than happy with the deck - the lift/lower behaved like a Kamakaze pilot for a start - and I thought the plinth too light. However, once you have adjusted the arm height for a good clearance, totally ignoring the misleading instruction manual, the lower control performs more sensibly. The deck is certainly more prone to acoustic feedback than I might like, but a good solid mounting shelf (no coffee tables entertained) should prevent any trouble there.

Getting the Point

My cartridge is from the same stable as the amazing MC81 (which remains my nomination for God's gift to hi-fi) and all sarcastic cries of 'surprise' 'surprise' will be studiously ignored. The Coral 555E is a moving magnet design or more restrained ambition and hence more general appeal. At its price of somewhere beneath £20 it faces numerous competitors of varying ability, so there is no lack of units to compare it against!

Physically the 555 is guite a deep unit with a medium/low compliance rating, and a weight of six grammes. Output is high-ish at around 5mV at 5cm/sec, and so an amplifier with a healthy overload is called for, lest it clips away at the peaks other beers can't

Once the arm height had been suitably adjusted the Coral proved a good match for the QLA5R and gave a satisfyingly musical reproduction in the test system. Substituting the deck into our reference system could only be called unfair I suppose, but still it's a cruel world anyway so what the hell...



depth necessitated raising the arm pillar an appreciable

amount, which the deck could cope with, but the instruction

The deck itself is a competent offering, very good mechanically and producing a good sound quality at its price. Compared against a high quality reference the sound is shown to be a little boomy, probably due to its constructional failings. A slight edge is imparted to the higher regions too.

However, being unfair has the advantage that once you start you may as well carry on, so I took the 555E out of the QLA5R and the reference MC81 was parted from its carressing SME 111 and the two interchanged. The JVC handled the moving coil unit very well indeed and the results were very, very impressive.

The 555 in its turn was shown to be a high class unit by absolute standards, lacking only that subtle handling of complex signals which comes only with a high pile of poundnotes. Tracking is competent, if not outstanding, and the sound balance is a well restrained mixture on the right side of bright - if you'll pardon the rhyme.



Centre Point?

And so to that from where we came. JVC's A-S5 began this and is indeed a worthy offering. As you can see from the photo it has a simple appearance (if I was polite I could call it restrained) but it is in full possession of all necessary controls. The tone controls are of the 'click' variety and worked well in use producing no deterioration in the quality of sound for a moderate amount of tonal correction.

Although 30W is not a great deal of power by today's standards, the JVC performed well in most situations. A large room with large speakers is not the universe in which this star shines brightest, nor is it intended to do so. When used sensibly the A-S5 has a clean sound with good smooth treble extension and a firm bass response. With speakers of the ABR type i.e. Celestion 15's etc. a certain lack of control was noted, which vanished with infinite baffle or ported speakers such as the Videotone GB2s married to it here.

There is nothing in the specification to explain this oddity. The

Right: a naked GB2. The port is visible below the bass unit in the photograph. The bass unit itself seems small for the enclosure size at first but gives a good account of itself. The only criticism I had of the speakers was that they were more directional than most enclosures with a dome HF unit. Perhaps that (relatively) wide baffle had something to do with it. Overall though the GB2 is a fine little speaker which will take a bit of power and return a healthy bass punch.



damping factor holds up well at all frequencies - which is the first place one searches in a case like this. Anyway, a minor condition, a trifle in fact. Choose your speakers well and enjoy the best amplifier sound available under £100. All comes included! Congrats JVC.

Point of Speech

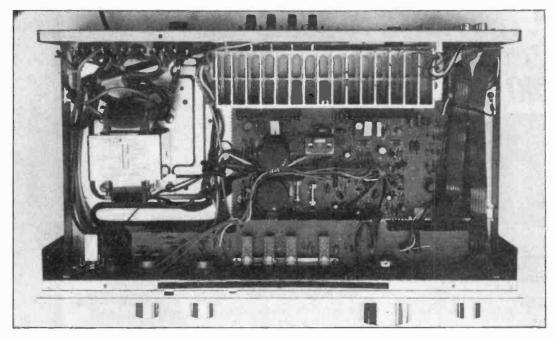
Hands up all those who have not heard of the Minimax. No takers?... One?... Who? Never heard of him either.

Oh very well..... they were the greatest thing since ears a few years back, sweeping all before their cones - including the reviewers. Singlehandedly they... etc... etc... That's right, a past rave machine. Correctly so, at the time. Videotone established themselves in the UK with the Minimax's and have consolidated since.

The GB2 is a well made little two unit enclosure of ported intent and a hefty bass punch for its size. It matches the A-S5 very well and for its £100 asking price returns a good deal of perfor-

A metal tape. Anyone who has tried to buy one of these elusive plastic cases will no doubt appreciate the sight. Machines to play the metallic illusions DO exist however and next month I'll be revealing the ferric truth about the Sony TCK 55 II — a £200 example of the iron art.

The cassette? Oh, well that is because Sony are shipping them in quantity which means that TDK no longer have it all their own way.



Left and Far Left: the machine which is to blame for this months Audiophile, AS5 from IVC. As you can see from the internal shot the amp is very well made with sensible heatsinking. I hasten to add that the tone control settings shown were put on by our photographer and NOT by me. He even managed to press the loudness button in - before I decapitated him for sacrilege. I tried hard to find something wrong with this amp and was sorely disappointed! Highly highly recommended.

mance. The overall sound is smooth, with a slightly recessed midrange and may be a little lacking in that presence so beloved of hard-rock enthusiasts. Nonetheless, the compromise is a good one at this price level and one which will tune many a phono cartridge. A good match here for the Coral 555E, lending a balanced and well extended sound to the system overall.

So there you have it. A £300 system of fine pedigree and

performance. It will not fill the Albert Hall with 100 dB of suicide watts, nor will it rattle the neighbour's china from his mantlepiece.

It will provide a good accurate rendition of vinyl information presented to it in the average living room, however, and that is all you could ask in a system - is it not?

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CAR SECURITY DEVICE

Bring your ETI Car Alarm up to date with this add-on alarm control module from Compu-Tech Systems. This module's muscle is guaranteed to double your alarm's scare coefficient.

any readers who have built and installed the Compu-Tech Systems car alarm (featured in ETI, December 1978) have expressed an interest in two additions to the alarm system, which increase its effectiveness at night and in noisy or high theft risk areas. This unit is also recommended if your horn is prone to faults or if it is located in an easily accessible place. If it's easy for you to get at, it's equally easy for a thief to get at.

The first requirement of the design is a method of sounding the horn, flashing the vehicle's lights and breaklights simultaneously when the alarm is activated. Whilst maintaining complete isolation between these circuits while the car is in normal use. The second design requirement is a method of driving a continuous supply of 12 volts for a sifen from the pulsating DC alarm signal without recourse to a large capacitor and the resulting slow run down of the siren when the alarm is switched off.

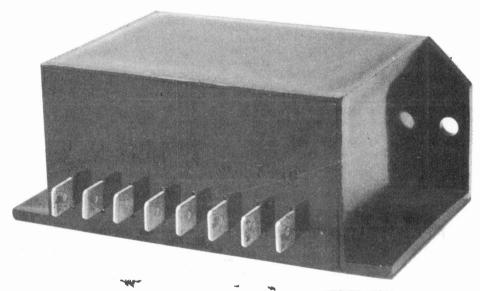
The project outlined has combined these two requirements into a compact weather resistant housing suitable for mounting in the engine compartment.

Add-on Power

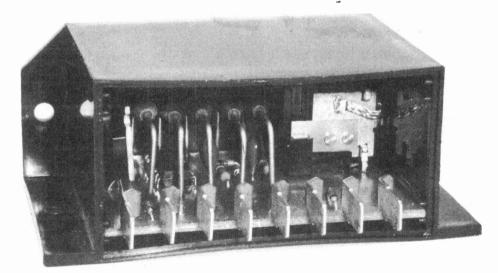
The current rating of the Alarm Control Module is 15 A, which is adequate for the demands of vehicle horn circuits ranging from seven to twelve amps. In order to meet the increased current demands of the vehicle lighting circuits, which range from six to ten amps, an additional fused circuit, independent of the Main Alarm Control Module, must be provided and independently switched by the alarm signal.

Construction

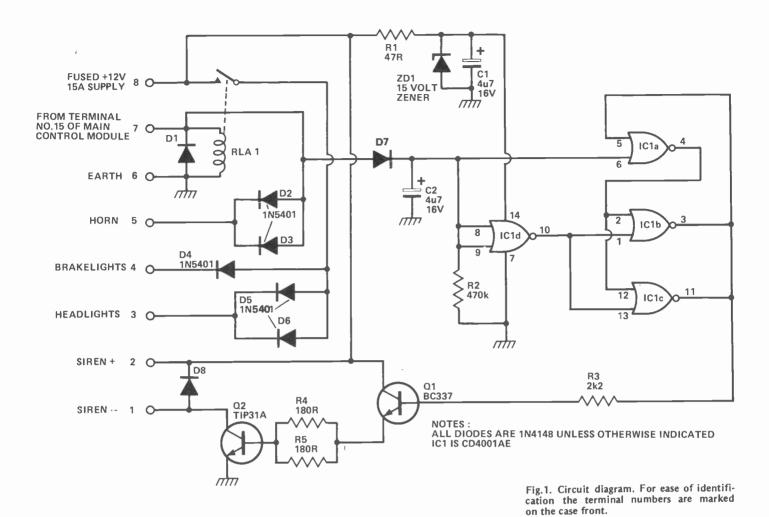
Construction is straight-forward with the Compu-Tech kit Of course, this little project must be used in conjunction with the ETI Car Alarm (Dec. 1978). Photocopies of this article are available from ETI for 50 pence.



Compu-Tech's add-on alarm control module comes complete with weather resistant housing to give trouble-free service from its hiding place.



Undo the snap-on front of the plastic housing and there's the compact PCB nestling inside.



HOW IT WORKS

The 1 Hertz pulsating alarm signal from the Main Alarm Control Module is connected to the Flasher Module via terminal (7). The horn output is derived directly from this signal at terminal (5) via blocking diodes D2 and D3. The signal from the alarm control module also energises RLA1. D1 absorbs the spikes created by the collapsing magnetic field of RLA1 which occurs during the pause in the alarm signal. Whenever RLA1 energises the second DC supply provided at terminal (8) is switched to the brakelight circuit at terminal (4) via blocking diode D4 and to the headlight circuit at terminal (3) via blocking diodes D5 and D6. Blocking diodes D2—6 ensure that the horn, headlight and brakelight circuits remain isolated when in normal use.

The DC supply provided at terminal (8) supplies the siren directly via terminal (2) and also supplies the internal logic circuitry via R1. ZD1 limits the DC supply to 15 volts which protects the IC from spikes that may be present on the incoming supply. C1 filters out any noise that may interfere with the operation of IC1. IC1 is connected as set-reset flip-flop. This arrangement provides a quick snap action to switch the siren on

and off thereby avoiding prolonged rundown of the siren. The alarm signal, when present at terminal (7), is coupled to IC1 via D7. The alarm signal will charge C2 to 12 volts which is sensed as a logic '1' by IC1 locking it to a stable state with a logic '1' at the output of IC1b/IC1c. IC1b is parallel with IC1c for increased output current drive capability. The logic '1' present at the output of IC1b/IC1c drives a modified darlington pair consisting of R3, Q1, R4, R5 and Q2 into conduction which provides an earth return path for the siren at terminal (1) This particular darlington configuration exhibits a very low saturation voltage across Q2 when it is conducting which minimises the power losses that would occur with a conventional darlington saturated switch. D8 absorbs the spikes created by the commutator in the siren. The time constant of C2 and R2 is approximately two seconds which is twice the period of the alarm signal from the control module. Therefore, the pulsating alarm signal will be seen as a continuous logic '1' as long as the alarm signal continues. Once the alarm signal is reset C2 will discharge to a logic '0' which will reset the set-reset flip-flop to its quiescent state with a logic '0' at the output of IC1b/IC1c silencing the siren.

BUYLINES

Compu-Tech Systems, Laundry Loke Industrial Estate, North Walsham, Norfolk will supply a complete kit of parts for this project including wire, connectors and hardware for £11.95; Siren £7.75 extra. (PCB only: £1.00).

A prerequisite for proper operation of

A prerequisite for proper operation of this project is the installation of the Vehicle Alarm Project in the December 1978 issue of ETI. A complete kit of parts for this project which also includes wire, connectors, hardware and switches is still available for £14.75. (PCB's only: £1.00 each).

Both projects and Siren for £29.95. (Prices are all inclusive; UK only).

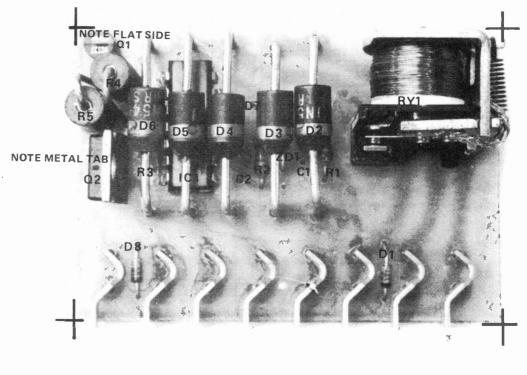


Fig. 2. Component overlay. Make sure you connect all the diodes the right way round.

*	3		*			*	*
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)

PARTS LIST.

RESISTO R1 R2 R3 R4,5	[†] 47R 470k 2k2 180R	IC1 Q1 Q2 D1,7,8	ONDUCTORS CD4001AE BC337 TIP31A 1N4148	MISCE 12V re Compu nents 1 compa
CAPACIT	ORS	D2-6	1N5401	case. V
C1,2	4u7 16V tantalum	ZD1	15V 400 mW zener	sure it'

MISCELLANEOUS
12V relay, 120R with s.p. n/o contacts.
Compu-Tech Systems' kit of components for this project includes a smart, compact snap-front, weather resistant case. When using an alternative, make sure it's weather-proof.

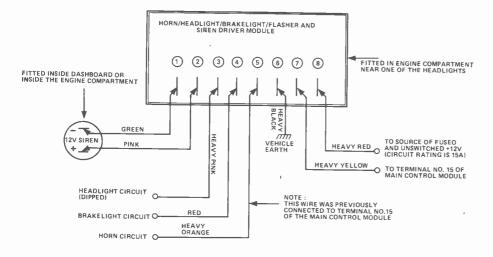


Fig.3. This is how you connect the box of tricks to your wheels. You shouldn't encounter any problems here.

ETI

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Minimum & Sub Ministure				
	Milli-	Ref.	Price	
	amps	No.	£	P&P
Volts				
3-0-3	200	238	2.45	.65
0.6, 0.6	1A 1A	212	2.85	.70
9-0-9	100	13	2.15	.65
0.9, 0.9	330 330	235	2.00	.65
0-8-9, 0-8-9	500 500	207	2.60	.70
0-8-9, 0-8-9	1A 1A	208	3.70	.70
0-15, 0-15	200 200	236	2.00	.65
0-20, 0-20	300 300	214	2.60	.85
20-12-0-12-20	700(DC)	221	3.35	.85
0-15-20, 0-15-20	1A 1A	206	4.45	1.00
0-15-27, 0-15-27	500 500	203	3.90	.85
0-15-27, 0-15-27	1A 1A	204	5.95	1.00
12 AND/OR 24	VOLT			- 1

12	AND/OR	24 VOLT
Pri:	220-240	Volts

rn. 220	7-240 VOII:	5		
	Amps		Price	
12v	24V	Ref.	£	P&P
0.5	0.25	111	2.15	.70
1.0	0.5	213 -	2.60	.85
2	1	71	3.10	.85
4	2	18	3.90	.85
6	3	70	5.45	.90
8	4	108	7.30	1.15
10	5	72	8.10	1.15
12	6	116	8.70	1.15
16	8	1.7	10.70	1.25
20	10	115	13.70	1.45
30	15	187	16.70	1.45
60	30	226	33.20	1.75

30 VOLT (Prí: 220-240V) Sec: 0-12-15-20-24-30V

Amps	Ref. No.	Price £	P&P
0.5	112	2.70	.85
1.0	79	3.45	.85
2.0	3	5.45	1.00
3.0	20	6.15	1.15
4.0	21	6.45	1.15
5.0	51	9.45	1.15
6.0	117	10.95	1.15
8.0	88	14.20	1.45
10.0	89	16.45	1.45

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	T (Pri: 220 9-25-33-4	
Sec: U-1	9-25-33-4 Ref.	Price
Amps	No.	3
0.5	102	3.45
1.0	103	4.45
2.0	104	7 4 5

.85 1.00 1.15 104 8.45 1.15 10.70 14.95 20.05 1.25 4.0 106 6.0 8.0 10.0 107 1.65 23.95 119 2.15

60 VOLT (Pri: 220-240) Sec: 0-24-30-40-48-60

	Ref.	Price	
Amps	No.	£	P&P
0.5	124	3.70	.85
1.0	126	5.45	1.00
2.0	127	7.40	1.15
3.0	125	10.95	1.25
4.0	123	12.20	1.45
5.0	40	14.00	1.55
6.0	120	17.45	1.55

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V M	rigi.	11,00	
(Watts)	No.	£	P&P
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75	64	3.95	.85
150	4	5.45	1.00
Input/O	utput Ta	ped	
0-115-21	0-220-2	40V	
300	53	9.05	1.15
500	67	10.70	1 45

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Pri: 120/240V			20/240V
ÝΑ	Ref.	Price	
(VVatts)	No.	£	P&P
60	149	6.45	1.00
100	150	7.45	1.25
200	151	10.95	1.25
250	152	13.15	1.45
350	153	16.15	1.55
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ETI CIRCUIT COOKBOOK

The province and the second



Project Editor Ray Marston digs into his treasure chest of 'Tried and Tested' circuits and pulls out over fifty of the best for his special ETI feature.

Power Amp Circuits

wide range of special-purpose single and dual ICs are available for use as audio power amplifiers giving maximum outputs from a few hundred milliwatts to a respectable 'several watts'. The specific IC chosen for a given application depends mainly on the constraints of the available power supply voltage and on the required output power level or levels.

In cases where supply voltages are restricted to the 6 to 12 volt range and power levels less than a few watts are needed, the National Semiconductor LM388 range of ICs can be used.

The LM388 uses a high-impedance gain-programmable ground-referenced differential input stage that is automatically biased to a quiescent half-supply value, for maximum non-clipped output swing. In the interest of power efficiency, the output stage has no short-circuit protection network.

The output stage of the LM388 is designed for use with a bootstrapped external bias network. The LM390 is a similar IC but has an improved output stage which enables 1 watt to be fed to a 4RO speaker load from a 6 volt supply. The LM386 is also similar to the LM388, but has a simplified output stage incorporating a built-in bias network. Finally, the LM389 circuit is identical to the LM386 but additionally an array of three fully accessible NPN transistors are built into the IC package.

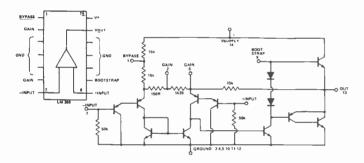


Fig.1.1. The outline and equivalent circuit of the LM388 1.5 watt device, specifically designed for low voltage applications. The IC has a built-in 'frame', which acts as a heatsink and is connected to six of the IC pins. Power dissipation can be enhanced by soldering these pins to a large area of copper track on a PCB, which thus serves as an additional heatsink.

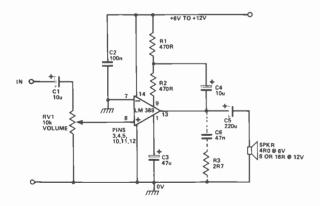


Fig.1.2. One way of using the LM388 as a 1-watt non-inverting power amplifier with grounded speaker. The voltage gain is internally set at 20. R1-R2 are the output stage bias resistors, bootstrapped by C4. C3 improves supply ripple rejection and C2 provides high frequency decoupling. The dotted C6-R3 components (also shown in all other practical circuits in this section) form a Zobel network that is intended to damp parasitic oscillations from low-impedance loads and should ONLY be used if instability problems are experienced.

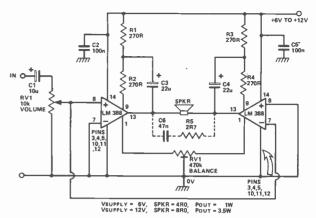


Fig.1.3. Maximum available output power can be increased by bridge connection of a pair of LM388s, so that the power losses are shared between the two. RV1 is used to set the quiescent speaker current to zero.

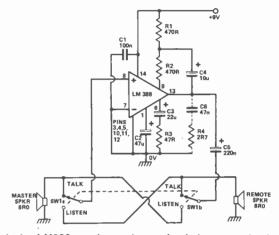


Fig.1.4. An LM388 can be used as a simple intercom circuit. The IC voltage gain is set at 300 by the C3-R3 decoupling network.

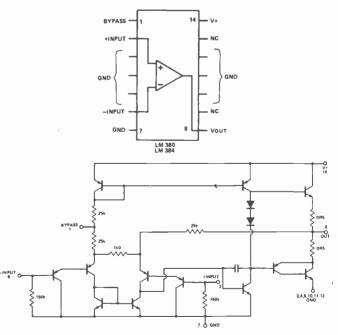


Fig.1.5. In cases where supply voltages are not restricted to the 6 to 12 volts range and output powers of only a few watts are required, the popular LM380 2-watt or its identical, but uprated LM384 5-watt 'brother' can be used. These ICs have full output short-circuit protection and use the same type of heatsink 'frame' as the LM388.

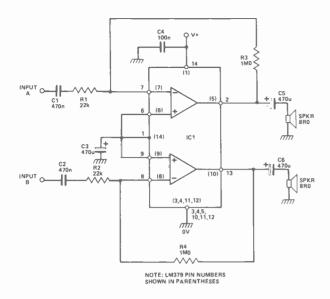


Fig.1.6. A simple inverting stereo amplifier using the LM377, LM378 or LM379 dual amplifier IC.

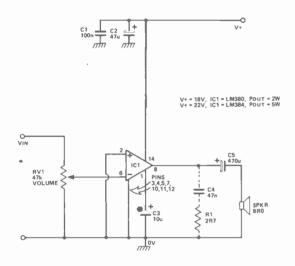


Fig. 1.7. A 2 watt or 5 watt amplifier with simple volume control and ripple rejection.

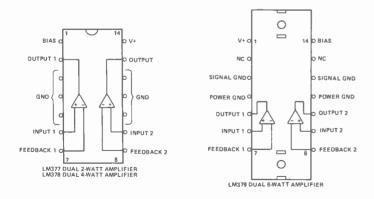


Fig.1.8. The outlines and pin notations of the LM377, LM378 and LM379.

V+	LM377	LM378	LM379		TPUT POWER
	1			8R0	16R
12V	†			1.6W	1W
16V	TO 2.5W	1 .		2.2W	1.5W
18V	T TO 2.5W	SW		3W	1.8W
20∨	LIMIT PER C	T TO SW	BW INEL	3.8W	2.4W
	1 2 2	LIMIT PER CE	HAN H	4.6W	2.8W
22∨		2 =	LIMIT TO GW PER CHANNEL	5.4W	3,6W
24V	<i>\\\\\\\\</i>		2=	6W	4.2W
26V	<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>	<i>\\\\\\\</i>		7W	5W
28V	<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>	<i>\\\\\\\</i>		-	5.5W ⁴
30W	<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>	X////////			

Fig. 1.9. The approximate performance characteristics of the three ICs. All three ICs have similar internal circuits with ground-referenced differential input stages and fully protected output stages.

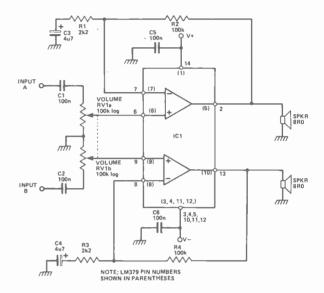


Fig.1.10. A non-inverting stereo amplifier using a split supply.

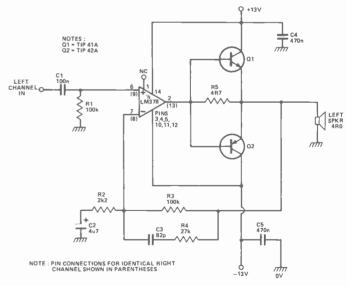


Fig.1.11. One channel of a 12 watts per channel stereo amplifier using a split supply. The circuit produces negligible output DC offset, so the quiescent output current is near zero.

Audio Preamp Circuits

udio preamplifier ICs are specifically designed to give very low noise figures, excellent supply 'ripple' rejection, low distortion and wide bandwidth. They give small-signal performances that are superior to those obtainable with conventional op-amps.

IC pre-amps usually come in the 'dual' form, with two identical but independent (apart from the supply connections) circuits in one package. National Semiconductors produce a range of five popular low-noise dual pre-amplifier ICs, the LM381 and LM381A, the LM382, the LM387 and the LM387A. The 'A' suffix devices are premium versions of their type, with superior low-noise figures.

All five ICs use the same basic amplifier circuit and essentially differ only in minor details and in their pin-outs. All amplifiers accept differential or single ended inputs, use internal compensation, use internal power supply decoupler - regulator circuitry and can provide large output voltage swings and wide power bandwidths. The LM381 and LM381A have provisions for externally optimising noise figures and for adding external compensation for narrow-band applications. The LM382 has a built-in resistor matrix that enables the user to select a variety of closed loop gain options and frequency response characteristics. The LM387 and LM387A are 8-pin 'utility' versions of the LM381/LM381A.

In most of the practical circuits that follow, only one amplifier of the IC is shown in use. Equivalent IC pin numbers forthe remaining amplifier are shown in parantheses.

The LM382, with its built-in resistor matrix, enables many amplifier designs to be achieved with a minimal number of external components.

The small physical size of the 8-pin LM387 and LM387A IC makes it attractive for use in many low-noise pre-amplifier applications.

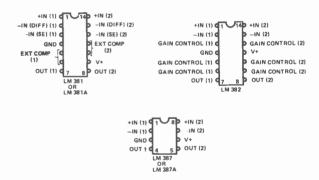


Fig.2.1. Outlines and pin notations of the LM381, LM381A, LM382, LM387 and LM387A.

	LN 381	LM 381A	LM 382	LM 387	LM 387A
VSUPPLY	9V - 40V	9V - 40V	9V ~ 40V	9V - 30V	9V - 40V
IQUIESCENT (TYP)	10 mA				
POWER BANDWIDTH (20V pk-pk)	75 kHz				
SUPPLY REJECTION RATIO AT 1 kHz (TYP)	120 dB	120 dB	120 dB	110 dB	110 dB
EQUIVALENT TYP	0.5	0.5	0.8	0.8	0.65
FIGURE MAX	1.0	0.7	1.2	1.2	0.9

Fig. 2.2. Typical performance of the five low-noise dual preamplifier ICs.

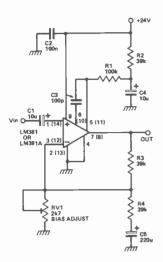


Fig. 2.3. A low-noise X1000 amplifier circuit. Bias is determined by R3-RV1 and gain by R3-R4. R1-R2 set the amplifier to optimum minimum noise conditions.

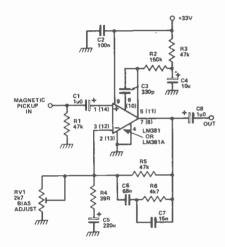


Fig. 2.4. The circuit shown in Fig. 2.3 can be modified for use as an ultra low-noise phono preamp, with RIAA equalisation given by the R5-R6-C6-C7 network. The circuit gives 42 dB gain at 1 kHz.

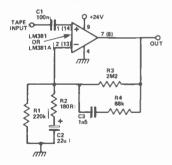


Fig.2.5. A simplified version can be used as a low-noise tape playback amplifier, with NAB equalisation.

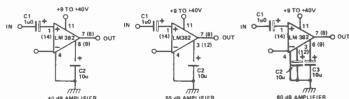


Fig. 2.6. Alternative methods of connecting the LM382 to make fixed gain non-inverting amplifiers.

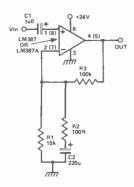


Fig. 2.7. Fixed gain (X1000) non-inverting preamplifier. The gain is determined by the ratio of R2 and R3. Alternative values of gain can be obtained by changing the value of R2. The circuit is biased by R1-R3.

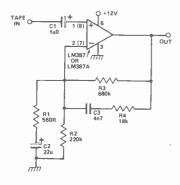


Fig.2.8. 12 V NAB tape playback preamp.

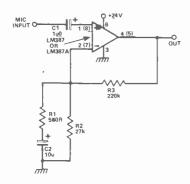


Fig. 2.9. Low-noise microphone preamp with a gain of 52 dB. The circuit is intended for use with low to medium impedance microphones.

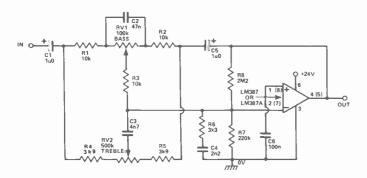


Fig. 2.10. A high performance active tone control.

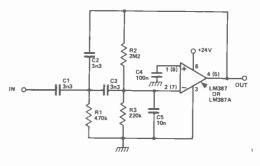


Fig. 2.11. 50 Hz rumble filter with 12 dB/octave roll-off.

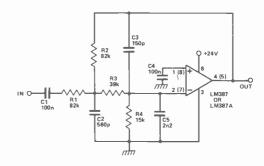


Fig.2.12. 10 kHz scratch filter with 12 dB/octave roll-off.

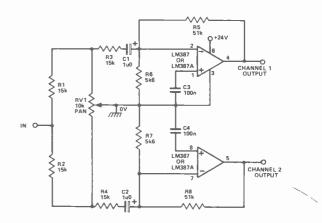


Fig.2.13. This two channel panning circuit enables a mono input to be swept or 'panned' between two channels in any desired ratio determined by RV1. It can be used to make a sound source appear to originate from any point between two widely spaced speakers.

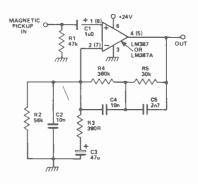


Fig. 2.14. RIAA equalised, single supply rail, pre-amplifier for magnetic pickup cartridges. Input impedance 47k, determined by R1.

Relay-Switching Circuits

Relay-switching circuits are popular and useful projects and are always in demand by ETI readers. The relay may, depending on the individual circuit configuration, be made to switch on in response to increases or decreases in light or temperature levels, or by voltages or by currents going above or below pre-set values. Alternatively, the relay may be made to turn on or off in response to some time-delay factor, or may merely be made to respond to the presence or absence of a voltage, as in the case of some car anti-theft and immobilisation circuits. A wide variety of such circuits are shown in the following section.

These are circuits that activate if a parameter falls outside of two pre-set limits.

Figs. 3.10 to 3.12 show time-delay switching circuits. Figs. 3.10 and 3.11 operate in the simple 'C-R timing' mode and call for no explanation.

To complete this section, Fig. 3.13 to 3.15 show a selection of car immobiliser and anti-theft alarm circuits. The Fig. 3.13 circuit turns on and immobilises the ignition automatically when the ignition switch is first closed: the ignition can be re-enabled by briefly opening PB1.

The Figs. 3.14 and 3.15 anti-theft alarm/immobiliser circuits are designed for use in cars with negative ground electrical systems. Before trying to fit either of these systems, however, check that your vehicle is fitted with door switches that connect the dome (courtesy) light to chassis, as shown, when they are activated.

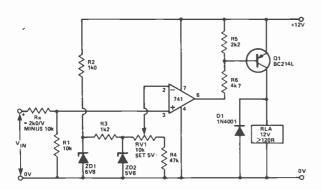


Fig.3.1. A precision DC under-voltage relay switch. The op-amp is wired as a voltage comparator, with a reference voltage applied to pin 2 and the test voltage applied to pin 3: the relay turns on when the pin 3 voltage exceeds that of pin 2. The circuit can be made to trip at any voltage in excess of 5 volts by suitable choice of Rx value.

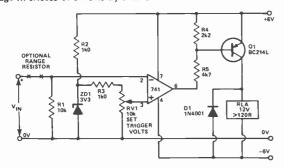


Fig. 3.2. An over-voltage switch that can be used to trip at any pre-set voltage in excess of about 10 mV. The input voltage can be connected directly to pin 2 if trip values in the range 10 mV to 3 volts are required. For voltages in excess of 3 volts, a suitable range resistor must be connected in the position shown, to keep the pin 2 voltage drive to a suitable level. The circuit can be converted to an under-voltage switch by transposing the pin 2 and pin 3 connections of the op-amp. The circuit can be used as an AC voltage switch by first rectifying the AC input signal.

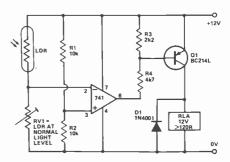


Fig.3.3. A precision light-sensitive switch that activates when the sensed quantities go above or below pre-set values. The LDR can be any cadmium-sulphide unit that has a resistance in the range 500R to 20k at the required trip level.

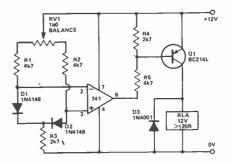


Fig.3.4. A differential temperature switch circuit using ordinary silicon diodes as temperature-sensing elements and responding to differentials of a fraction of a degree. RV1 can be used to apply an effective offset of several degrees to the two diodes. To adjust the circuit, apply the required differential temperature to the diodes and then adjust RV1 so that the relay just turns on. The circuit responds to the relative temperatures, rather than the absolute temperatures, of the two diodes.

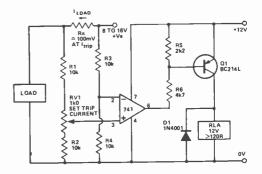


Fig. 3.5. A DC current-sensing switch, in which the current is applied from an 8 to 16 volt supply. The Rx value is chosen so that it generates roughly 100 mV at the required trip current.

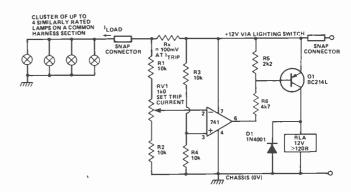


Fig. 3.6. shows how the above circuit can be made to act as a car lampfailure switch which turns on if any of the monitored lamps burn out. Rx is wired in series with the wiring harness feed to a selected 'cluster' of up to four similarly rated lamps.

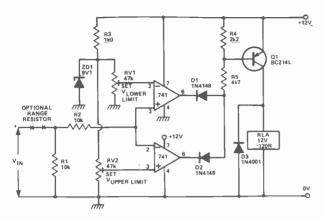


Fig. 3.7. A voltage-window switch. In practice the basic lower window limit of this circuit is roughly 3 volts and the upper limit is 9 volts. The window range can be extended by fitting a suitable range resistor in the position shown.

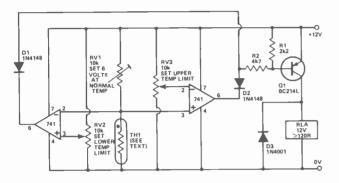


Fig. 3.8. is basically a resistance-sensing window switch, except that the 'resistor' takes the form of an ntc thermistor and the circuit thus responds to temperature. TH1 must have a resistance in the range 500R ot 9k0 at the desired 'mean' temperature. RV1 is used to set half-supply volts on the RV1-TH1 junction at the 'mean' temperature.

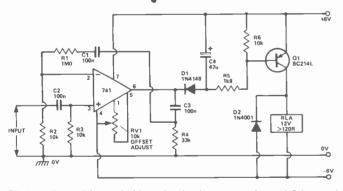


Fig.3.9. A sensitive switching circuit that responds to AC inputs in excess of about 5 mV rms. It responds to all signals in the 50 Hz to 3 kHz 'voice' range. RV1 is adjusted so that the relay is just off with zero input.

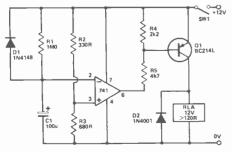


Fig.3.10. A 100 second delayed-turn-on relay switch.

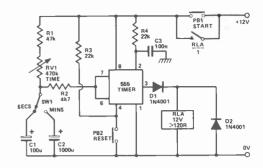


Fig.3.11. A two range 6-60 second and 1-10 minuted auto-turn-off relay timer circuit.

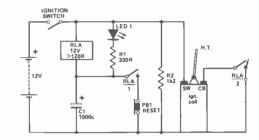


Fig.3.12. An automatic immobiliser circuit for cars fitted with negative ground electrical systems.

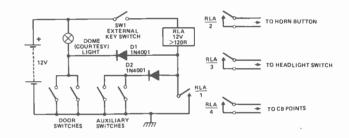


Fig. 3.13. An anti-theft alarm/immobiliser for cars, which operates horn and lights until switched off or until the battery runs flat.

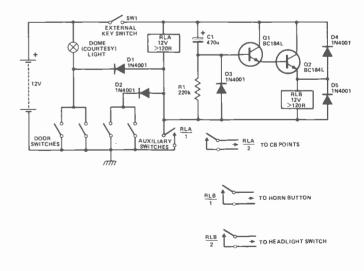


Fig.3.14. An improved car alarm/immobiliser, which disables the ignition indefinitely but turns the horn and lights off automatically after four minutes.

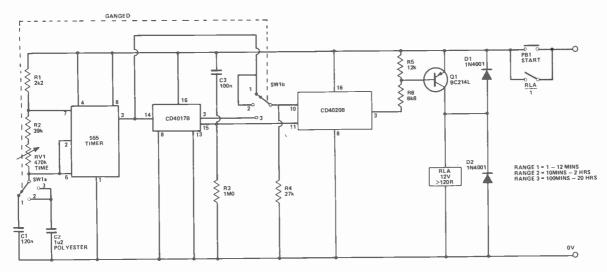


Fig. 3.15. A wide-range auto-turn-off timer covering 1 minute to 20 hours in three ranges. As soon as power is applied to the circuit the 555 starts to oscillate happily and feeds clock pulses to the 4017. The 4017 and 4020 give a combined count rate of 81920 before the output of the 4020 goes high and turns Q1 on.

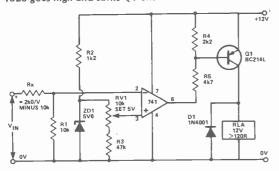


Fig. 3.16. Precision DC over-voltage relay switch, covering 5V upwards.

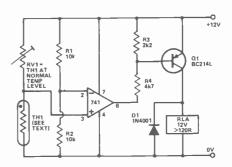


Fig.3.17. Precision over-temperature, or 'FIRE' switch. This circuit can be converted to a 'frost' or under-temperature switch by transposing RV1 and TH1.

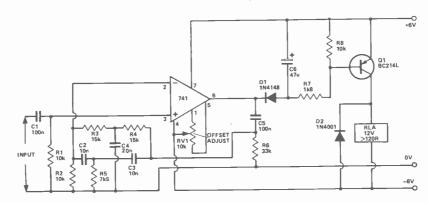


Fig.3.18. A sensitive (1 kHz) tone activated relay switch, which has a typical sensitivity of 5 mV RMS at the input.

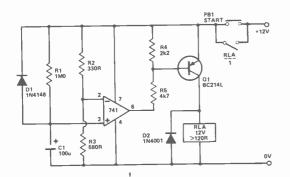


Fig.3.19. A delayed turn-off relay switch. With component values of R1 and C1 as shown, the time delay is determined at 100 seconds.

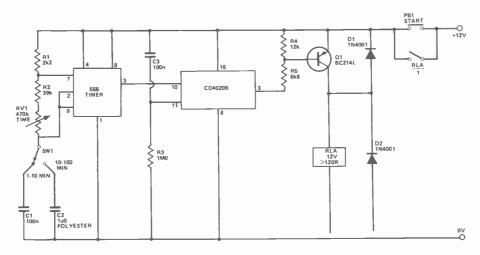


Fig.3.20. A two-range 1-10 minute and 10-100 minute auto turnoff relay timer circuit. Different ranges can be obtained by varying the values of capacitors C1 and C2.

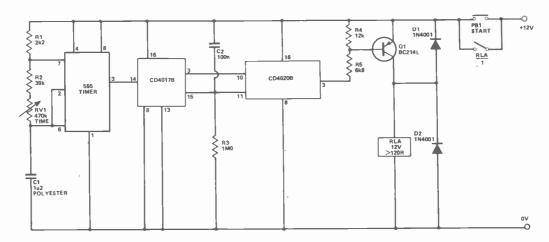


Fig.3.21. An extra-long period timer, which could be used as a long process cycle controller. The period obtainable from this circuit is between 100 minutes and 20 hours. Auto turn-off operation has been selected.

Waveform Generators

aveform generator circuits are widely used both as pieces of test gear and as simple 'noise making' gadgets. Types of waveform generated range from accurate sine, square and pulse waveforms to 'mushy' white and pink noise forms.

If you need a variable sine wave generator for audio or ultrasonic testing purposes, you are faced with a number of circuit choices, depending on which parameter you consider to be most important. If low cost is important and a distortion factor of up to 0.5% is acceptable, the lamp-regulated Wien-bridge oscillator (Fig. 4.1) is a good choice.

If low distortion is your most important parameter, the thermistor-regulated Wien-bridge oscillator in Fig. 4.2 is a good choice. This circuit typically produces about .05% distortion at 1 kHz and shows how range switching can be incorporated.

If minimal bounce is your most important parameter and a distortion factor of 0.5% is acceptable, the circuit of Fig. 4.8 is an ideal choice. The circuit uses a special function generator IC (available from several ETI advertisers) and a single frequency-control pot and spans its frequency range with absolutely zero bounce.

If you ever need to generate a fixed or variable HF or RF signal you'll have the option of using either a Hartley (Fig. 4.4) or a Colpitts (Fig. 4.5) oscillator. The Hartley oscillator uses a tapped coil and is easily tuned over a wide range.

If you are a dedicated 'radio' listener you'll need a BFO circuit to enable you to listen to CW transmissions. Fig. 4.6 shows a practical BFO unit. An alternative BFO circuit is shown in Fig. 4.7.

Square wave forms are very easy to produce. The circuit in Fig. 4.8 can be used to generate a variable-frequency variable-mark/ space ratio waveform. Two excellent CMOS square wave generator circuits are shown in Fig. 4.9. Both circuits produce clean output waveforms and can accept a very wide range of C - R timing components.

Pulse generator circuits can be readily built from standard 555 timer chips or from CMOS ICs, but in these cases have typical rise and fall times of a hunderd nanoseconds or so. Where brief rise and fall times are important (as in standard test gear circuits), TTL ICs offer a good solution to the pulse-generator problem. The 74121N monostable multivibrator IC (in either standard or LS form), for

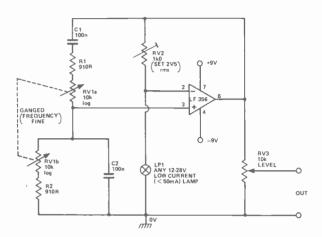
example, produces pulse rise and fall times of only a few nano-

Fig. 4.10 shows how a 74121 can be used as an add-on pulse generator, triggered by an external clock signal. Fig. 4.11 shows how two of these circuits can be cascaded to make an add-on delayed pulse generator in which both the delay and the width can be varied from 100 nS to 100 mS.

White and pink noise sources are widely used for testing amplifiers and for generating special sound effects. White noise

produces a +3 dB rise in amplitude per octave of frequency change (equal energy per constant bandwidth). Pink noise has a flat amplitude response per octave change in frequency (equal energy per octave). White noise is best produced by a pseudo-random sequence generator, such as the MM5837 shown in Fig. 4.12: unfortunately, this IC is rather difficult to find. The MM5837 is housed in an 8-pin package.

White noise can be converted to pink via a simple filter network, as shown in Fig. 4.13.



1k0 OUTPUT (LEVEL) XR -2 206 R2

Fig.4.1. A low-cost 150 Hz - 1k5 Hz lamp-regulated Wien-bridge oscillator, producing a sine wave with a typical distortion factor of less than 0.5%. The frequency range of the circuit can be changed by using different C1–C2 values. Reducing the values by a factor of ten (to 10n) raises the frequency range by a decade (to 1k5 Hz – 15 kHz). The specified op amp will give useful operation up to about 150 kHz. LP1 can be any 12-28 V low current (less than 50 mA) lamp and the circuit is set up initially by simply adjusting RV2 to give a nominal maximum sine wave output of about 2V5 RMS.

Fig.4.3. The high quality function generator IC produces 'bounceless' sine waves with typical distortion factors of 0.5%. Initial setting up is a matter of twiddling with the RV2-RV3-RV4 controls to obtain a minimal distortion output signal with a maximum RMS value of about 2 V. Once you've initially set up the circuit, you can forget these pots forever. The frequency range is controlled by RV1 and C1.

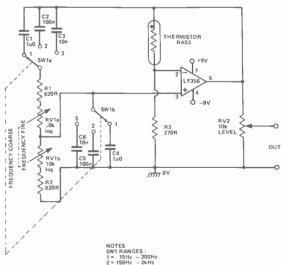


Fig.4.2. This low-distortion (0.05% typical) Wien-bridge oscillator

Fig.4.4. In the Hartley oscillator the frequency = $1/2\pi \sqrt{L_1 C_1}$ must be a tapped inductor.

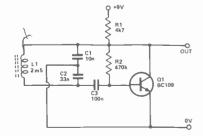


Fig.4.5. In this 37 kHz Colpitts oscillator the frequency = $1/2\pi\sqrt{L_1C_x}$, where Cx is the equivalent series capacitance of C1 and C2. L1 is untapped. It is effectively an 'autotransformer' tapped by the C1-C2

Fig. 4.2. 'This low-distortion (0.05% typical) Wien-bridge oscillator spans 15 Hz to 20 kHz in three decade ranges (with the component values shown). The only defect of this low-distortion type of circuit is that it suffers from 'amplitude bounce' as the frequency is varied from one value to another, which is a bit of a pain if you are testing the frequency response of an amplifier. The degree of 'bounce' depends on the quality of the pot used in the RV1 position.

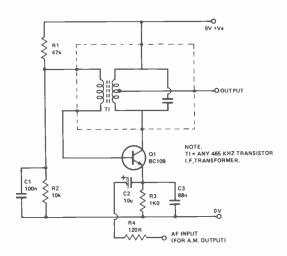


Fig.4.6. A 465 kHz BFO with amplitude modulation facility. T1 can be any standard IF transformer. The output can be modulated via an AF signal.

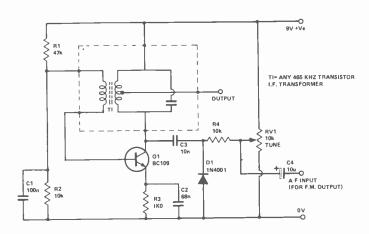


Fig. 4.7. A 465 kHz BFO with 'varicap' tuning and FM facility. D1 is used as a varicap diode and the oscillator is tuned via RV1. The oscillator can be frequency modulated via an AF source.

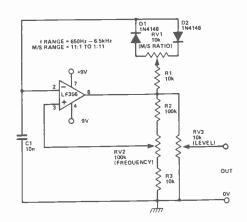


Fig.4.8. A variable-frequency, variable M/S ratio 'square wave' generator. The mark/space ratio is controlled by RV1, the frequency by RV2 and the output level by RV3.

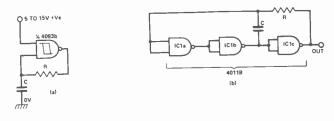


Fig.4.9. Two excellent CMOS square wave generators are the Schmitt oscillator (a) and the ring-of-three oscillator (b). Both circuits produce clean otuputs. 'R' values can be varied from a few kilohms to many megohms. 'C' values can vary from a few dozen picofarads to many microfarads.

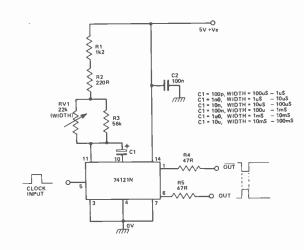


Fig.4.10. An add-on pulse generator covering the range 100 nS to 100 mS, using a 74121 triggered by an external clock signal. The circuit produces fixed amplitude inverted and non-inverted outputs, each protected against short-circuit damage by a 47 R series resistor. By suitable choice of the value of C1 the triggered pulse width can be varied from 100 nS to 100 mS.

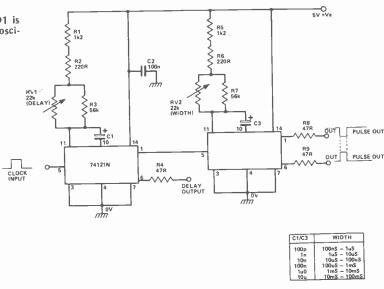


Fig.4.11. An add-on delayed pulse generator covering delay and width ranges of 100 nS to 100 mS.

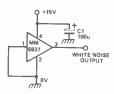


Fig. 4.12. The National Semiconductor's MM5837 is an MOS/MSI pseudo-random sequence generator, designed to produce a broad-band white noise signal for audio applications. It is housed in an eight pin package.

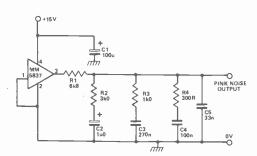


Fig.4.13. Pink noise generator.

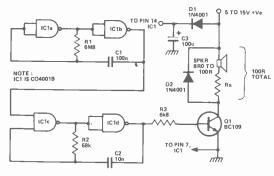


Fig.4.14. This pulsed-tone alarm call generator produces a typical output of a few hundred milliwatts.

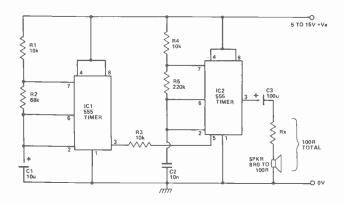


Fig.4.15. This warble-tone generator simulates a British police car 'Dee-Dah' siren.

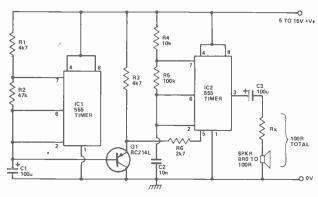


Fig.4.16. This wailing alarm simulates an American police siren.

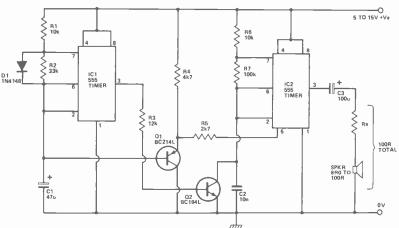


Fig. 4.17. This 'Red Alert' generator simulates the 'Star Trek' alarm signal.

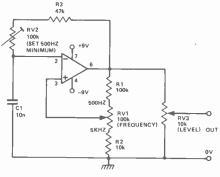


Fig.4.18. An op-amp relaxation oscillator producing a good quality 500 Hz to 5 kHz square wave.

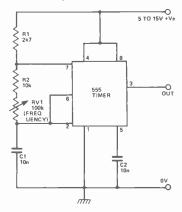
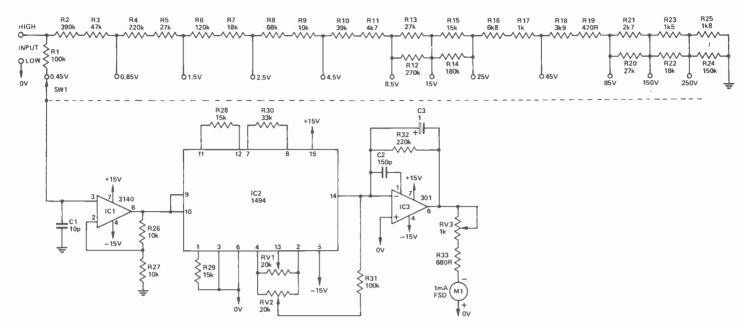


Fig.4.19. A variable-frequency, variable mark-space ratio square-wave generator which takes longer to say than it does to build!

Test Meter Circuits



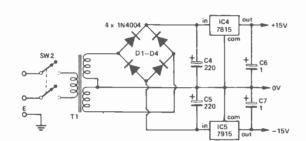


Fig.5.1. A true RMS voltmeter. The input voltage is divided by the input network such that the input IC1 is 0.47 volts (DC or RMS) for full scale deflection. IC1 provides buffering and a gain of two.

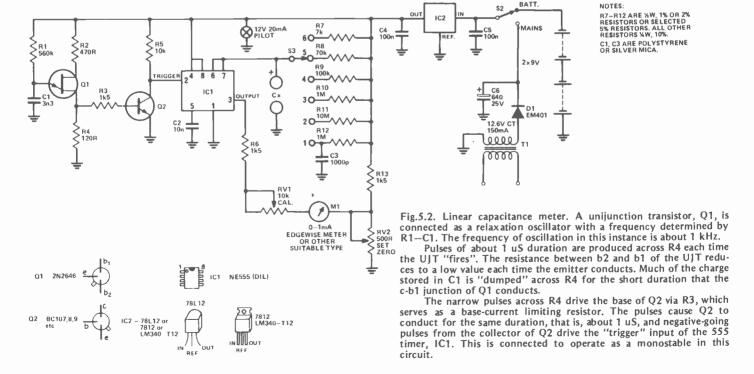
Squaring of the output of IC1 is done by IC2 (1494), a four

quadrant multiplier, which gives a current output proportional to the produce of the voltages at its two inputs (pin 9 and 10). As we are feeding the same signal into both inputs the result is the square function.

The output of this IC is a current which is converted to a voltage by IC3 which also provides the averaging network (C3, R32). Its output drives the meter whose scale is a square root function.

Adjustments are provided for the input offset of IC2 (RV1) output offset (RV2) and overall calibration (RV3).

As the power requirement of all the ICs is ± 15 V we use a mains supply and three-terminal regulators. Current drain is about 15 mA on both supplies.



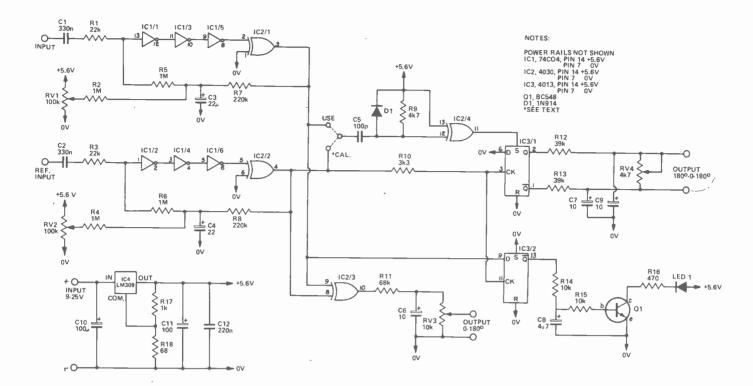
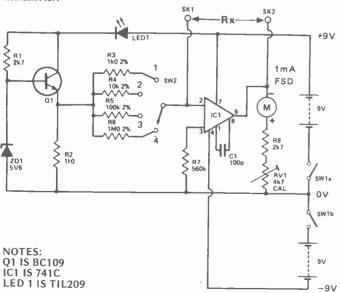


Fig.5.3. Phase meter circuit. The two inputs are first squared. For example the reference input is amplified by gates IC1/2, IC1/4 and IC1/6 and then applied to IC2/2, one of the spare EX.OR gates whose other input is grounded. This conveniently behaves as a Schmitt trigger type of bistable circuit. The average of the output of this gate is formed by R8 and C4, and this is inserted via R6 as the DC level at gate IC1/2.

This produces two important consequences. Firstly it forces the output of IC2/2 to a symmetrical 180° on/180° off condition which is kept stable by almost complete DC feedback. And secondly, because we now have a true squaring circuit rather than a zero-crossing detector, all errors due to even-order harmonic distortion are cancelled. R4 and RV2 are used to adjust for input offset and set the exact 180° condition.

IC gates IC1/1, IC1/3, IC1/5 and IC2/1 process the signal from the other channel in an identical manner, and the two squared outputs are fed to gate IC2/3 which is the gate that forms the EX.OR of them. Its output is filtered by R11 and C6 and a voltage proportional to the phase difference of the inputs may be taken from across C6. RV3 is used to set this to a convenient value — for instance it may be set to 180 mV for a 180° phase difference and read it on a digital multimeter.



In order to detect which of the inputs is leading the other, the two voltages from the squaring circuits are also fed to the D type flipflop IC3/2. One voltage is used for the clock input and the other as a data input. This type of flip-flop is really a data latch, and whatever voltage is present at the D input at the moment when the clock voltage changes from low to high is held until the next clock pulse. Thus if the D input stays low until after the clock input goes high, the output Q will always remain low showing that the D input lags the clock input. The complementary output Q will be high and this is used to turn on the transistor and LED indicating this lag condition. Since any noise arriving at the clock input can cause spurious resetting of the flip-flop, it is preferable to use a clean voltage to drive it. This is why this channel has been designated the reference. Noise on the other channel is almost completely ignored.

These then are the basic EX.OR functional parts of the phase-

These then are the basic EX.OR functional parts of the phasemeter, and his would leave one flip-flop unused. In fact it turns out that there are two functions that these gates can usefully perform. First, for setting up the input squaring circuits: if the flip-flop is slaved to the squaring circuit, the exact 180° condition can be set when the complementary outputs Q and Q have equal average values. Secondly these gates can be arranged to turn the flip-flop on and off to give a conventional phase meter circuit output. While this does not give as accurate a reading, it does give one which is of opposite polarity for leading and lagging voltages and which can therefore be recorded graphically and unambiguously on an instrument such as a chart recorder. This is therefore designated the recorder output.

Fig. 5.4. (Left). Linear ohm-meter circuit. The circuit is divided into two parts: a reference voltage generator and a readout unit that indicates the value of the resistor under test. The reference voltage generator section of the circuit comprises zener diode ZD1, transistor Q1, and resistors R1 and R2. The action of these components is such that a stable reference of about 5 V is developed across R2. This reference voltage is fed to the op-amp resistance-indicating circuit via range resistors R3 to R6.

The op-amp is wired as an inverting DC amplifier, with the 1 mA meter and R8-RV1 forming a voltmeter across its output, and with the op-amp gain determined by the relative values of ranging resistors R3 to R6 and by the negative feedback resistor Rx. RV1 is adjusted so that the meter reads full scale when Rx has the same value as the selected range resistor. Under this condition the op-amp circuit has a voltage gain of precisely unity. Since the values of the reference voltage and the ranging resistors are fixed, the reading of the meter is directly proportional to the value of Rx, and the circuit thus functions as a linear-scale ohm-meter and has a full scale value equal to the value of the selected range resistor.

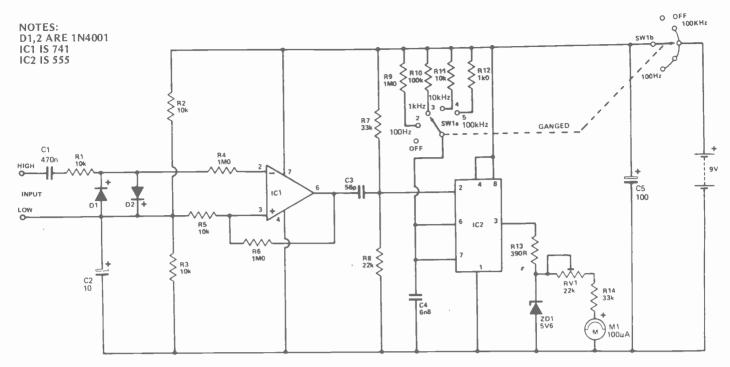


Fig. 5.5. Linear frequency meter. The circuit consists of an op-amp operated as a Schmitt trigger to amplify and square the input signal, followed by a 555 timer wired as a monostable, giving a short output pulse of fixed width for each cycle of input signal. This pulse drives a moving-coil meter, the reading being an average of the pulse amplitude, which is proportional to the pulse frequency. As the pulse frequency is directly related to the input frequency, the meter reading is directly proportional to the input frequency.

The input signal is coupled into IC1 via C1, which provides DC blocking. Protection from overload caused by high amplitude input signals is provided by a diode clipper consisting of D1, D2 and R1. The diodes are connected in an inverse-parallel arrangement so that both positive and negative peaks, above the diode forward conduction voltage, are clipped.

The output of IC1 is a train of square waves at the same frequency as the input. The output of IC1 is differentiated to provide short trigger pulses for the 555 timer, IC2. The differentiating network consists of C3, R7 and R8. This network is arranged to provide a trigger pulse that is always shorter than the output pulse of the 555. Capacitor C3 is selected to give the shortest possible pulse to the 555 consistent with reliable triggering.

The output of the 555 monostable will be a pulse of fixed width, determined by the range resistors, R9 to R12, and capacitor C4. The ranges are arranged to give a 75% output duty cycle at frequencies of 100 Hz, 1 kHz, 10 kHz and 100 kHz on the input.

The output pulse from the 555 is clipped at 5V6 by a zener diode, ZD1, to avoid inaccuracies caused by falling battery voltage (as the battery ages). The meter responds to the average value of the clipped pulses. As the frequency increases, the duty cycle (on/of ratio) of the pulse train increases, increasing the average voltage and thus the meter current in direct proportion. Thus the reading on the meter will be linearly related to frequency.

Fig. 5.6. (Right). Sequential Logic Tester. Anyone testing a sequential logic circuit requires input pulses free of contact bounce. This unit does this, providing two switched, jitter-free outputs and a 'slow' variable speed clock. The complements of these signals are also provided.

The components shown give the clock a frequency range of 1-200 Hz. The clock's buffered output will drive up to two TTL inputs.

The 100R resistors on all outputs provide some measure of accidental short circuit protection.

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COMPONENTS

IN4148 0. Pp. IN4002 2. Pp. IN4004 3.4p. bc109b 6.5p. 723 14 dil 33p. NE555 8 dil 24p. 741 8 dil 18p. bc183. bc213. bc547. bc548 4.9p. bc182. bc184. bc212. bc214. bc548 5.5p. tp31c. ip32c. 36p. tp41c 46p. bd13 27p. plastic equiv bcy72 4.8p. fuses 20mm x 5mm cartridge 1.5. .25. .5. 1, 2, 3, 5Amp quickbiow 1, anti-surge 3.6p. resistors 5% kW E12 10R to 10M 1p. 0.8p for 50 + of one value. Polyester capacitors 5 50 v.5 1 for 15 for

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S-DECS AND T-DECS S-Dec £3.79. T-Dec £4.59. u-DecA £4.69. u-DecB £7.16. 16 dii adaptor £2.31.

Please add 35p for F DELTA TECH & I	CU	LM308N 60p LM318N 200p LM324N 75p	4066 4069 4070/1	50p 18p 18p	7491 45 p 7492 30 p 7493 35 p	AC153 AC176 AC187/8	30p 23p 23p	BF185 8F194/5 8F196/7	25p 12p 12p	ZTX304 ZTX311 ZTX341	27p 19p 22p
	Company of the last of the las	LM339N 60p LM348N 90p	4072/3	18p	7494 50 p 7495 40 p	AD149 AD161/2	70p 40p	8F2248 8F2448	14p 35p	ZTX500 / 1 ZTX502	16p 21p
62 NAYLOR ROAD, LONDON,		LM377N 175p	4086	80p	7496 50p	AF114	30p	8F258	34p	ZTX503	17p
Mail Order only		LM380N 90p		100p	7497 200p	AF124	45p	BF259	40p	ZTX504	28p
THE RESERVE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER, THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.		LM381N 140p		100p	74100 70p 74105 43p	AF125 AF126/7	35p 37p	8FR39 8FR40	32p 20p	2N696 2N697	35p 25p
RESISTORS (1/4 W) 10 ohms to 10 Mohms 1.5p	2A/2001 TOP .	LM382N 130p LM1310N 150p		100p	74103 20p	AF139	40p	8FR79	32p	2N698	35p
PRESETS (.15W Horizontal)		LM3900N 55p		100p	74109 40 p	AF239	47p	8FR80	20p	2N706	14p
100 ohms to 2 Mohms 8p		LM3909N 70p		100p	74110 40 p	8C107/8	10p	BFX29	25p	2N914	20p
POTENTIOMETERS (1/4 W)	REGULATORS	MC1496P 85p	A	1	74118 90 p	BC109	10p	BFX84	25p	2N918	35p
Linear & Log Scale	7805 70 p	NE531 150p	TTL		74121 26 p 74122 30 p	8C117	25p	8FX87/8	25p	2N1131	20p
4.7 Kohms to 2.2 Mohms 30p	7012/3 70P .	NE555 25p	7400/1	13p	74122 30 p 74123 45 p	8C142/3 BC147/8	30p	8FY50 8FY51/2	22p 22p	2N1132 2N1302	13p 35p
VEROBOARDS (0.1" Coppet) 2.5" x 5" 55n	/010/24 //OP	NE556 60p NE566 140p	7402/3	13p	74125/6 37p	BC147/8 BC149	10p	8FY53	10p	2N1302 2N1303	40p
2.5" x 5" 55p 3.75" x 5" 65p	/905 30p ,	T8A641B 200p	7404/3	20p	74132 48p	8C157/8	12p	8RY39	60p	2N1304	50p
ZENER DIODES (400mW)		TBA800 75p	7408/9	13p	74141 50 p	8C159	12p	BSX19	12p	2N1305	13p
2.7V to 33V 8p		TBA810S 110p	7410	13p	74145 55 p	8C167	14p	8SX20	22p	2N1306	30p
CERAMIC CAP (50V)		ZN414 100p	7411	18p	74150 78 p	8C169C	13p	8U205	150p	2N1308	22p
33pF to 47nF 3p	8Y127 10p	ZN1034 200p	7412	15p	74151 48 p 74153 43 p	BC171 8C173	10p	8U208 MJ2955	210p	2N1613 2N1711	25p 13p
POLYSTYRENE CAP (50V)		CMOS	7413 7414	27p 31p	74153 43 p	8C177/8	8p	MJE340	70p	2N1893	25p
10pF to 1,000pF POLYESTER CAP (100V)	0.00	4000 18p	7416/7	25p	74155 46 p	8C179	20p	MJE2955	110p	2N2222A	25p
1nF to 68nF 6p	OA200 6p / 4	4001/2 18p	7420	14p	74156 40p	BC182/3	12p	MJE3055	85p	2N2217	18p
100nF, 150nF 7p	OA202 9p 4	4006 70p	7421/2	17p	74157 43 p	BC184	12p	MPF102/3	40p	2N2219	23p
220nF, 330nF 8p		4007 18p	7427	20p	74160 64 p	BC186	30p	MPF104/5		2N2369	17p
470nF: 9p 680nF: 10p		4008 84p	7428	25p	74161 55 p	BC207/9	13p	MPF106	50p	2N24B4	30p
1uF: 14p 2.2uF: 20p		4009 40p	7430	14p	74162/3 64p 74164 78p	BC212/3 BC214	12p	MPSA06 MPSA56	26p	2N2646 2N2904	55p 23p
3.3uF: 22p 4.7uF: 24p ELECTROLYTIC CAP (uF/V)		4010 42p 4011/2 18p	7432 7433	18p	74164 70p	BC214L	12p . 14p	MPSU06	61p	2N2904 2N2905	23p
1/25 to 47/25 6p	4 4	4011/2 18p 4013 40p	7437/8	15p	74166 85 p	BC238	18p	OC28	92p	2N2906	- 20p
68/50, 100/35 8p	1N5400 1 3p 4	4014 85p	7440	10p	74173/4 70 p	BC261B	25p	OC35	92p	2N2907	20p
150/25, 200/12 9p		4015 75 p	7441	56p	74175 60p	BC301/3	32p	OC72	20p	2N2926G	11p
220/25, 250/12 10p		4016 44p	7442	51p	74176 64 p	BC32B	17p	TIP29	40p	2N3053	20p
470/25, 500/30 13p		4017 55p	7443	70p	74177 60p 74180 50p	BC338 BC461	17p	TIP29B TIP30	48p	2N3054 2N3055	50p
1000/10: 14p 1000/25: 22p 1500/25: 26p 2200/6: 20p		4018 80 p 4019 45 p	7444 7445	80p 75p	74180 50p	BC461 BC477	40p	TIP30	40p	2N3055 2N3442	50p
1500/25: 26p 2200/6: 20p		4019 45p 4020 95p	7446	65p	74182 45 p	BC477	27p	TIP31	40p	2N3702 TO	
OPTO/DISPLAY 16 pin 14p		4021/2 85p	7447	55p	74190 75p	BC547/8	14p	TIP32	40p	2N3711	11p
2N5777 55p 18 pin 18p	709-T05 40p 4	4023 18p	7448	62p	74191 70 p	BC549	14p	TIP33	60p	2N3772	150p
OCP71 65p 22 pin 22p		4024 58p	7450	10p	74192 50p	BC557/B	15p	TIP33C	80p	2N3773	250p
ORP12 60p 24 pin 24p		4025 18p	7451/3	13p	74193 64p 74194 70p	BC559	15p	TIP34A	90p	2N3819	22p
DL704 110p 28 pin 28p DL707 110p 40 pin 40p		4027 45p 4028 70p	7454 7460	10p	74194 70 p 74195 57 p	8CY70 8CY71/2	18p	TIP35B TIP368	240p 280p	2N3820 2N3823	40p 70p
0.125" & 0.2" 40 pin 40p		4028 70p 4029 82p	7470	20p	74196 100p	8D115	58p	TIP41A	60p	2N3866	90p
LEDs:		4030 60p	7472	21p	74197 80p	BD121/3	75p	TIP42A	60p	2N3903/4	10p
Red 10p BRIDGE		4035 107p	7473	28p	74198 135 p	8D124	81p	TIP2955	70p	2N3905/6	10p
Green 14p RECTIFIERS		4041 75p	7474	24p	74199 90 p	BD131 TO		TIP3055	55p	2N4037	45p
Yellow 14p 1A/50V 22p		4042 70p	7475	34p	TRANSISTORS	8D140	42p	ZTX107/8	13p	2N4058/9	14p
.125" Clip 3p 1A/100V 27p .2" Clip 4p 1A/200V 32p		4043/4 88p 4047 92p	7476	30p 25p	AC126/7 23p	BF178 8F180	32p 30p	ZTX109 ZTX300	13p	2N4060/1 2N5457/8	14p 40p
2" Clip 4p 1A/200V 32p 1A/400V 34p		4047 92p 4048 55p	7485	80p	AC128 23p	8F181	8p	ZTX300	18p	2N5459	35p
8 pin 11p 2A/50V 40p		4049 35p	7486	25p	AC128/176	8F183	34p	ZTX302	20p	2N6027	40p
14 pin 13p 2A/100V 42p		4050 44p	7490	36p	Mt. pr. 42p	8F184	25p	ZTX303	24p		
SEND FOR TRADE	ORDERS			700 5	DGWARE ROAD			120 V	ENTICL	H TOWN RO	AD

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You in the sold the

TRANSOUCERSVI MEASUREMENOL MEAO CONTROL

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Quality audio modules and accessories for

\$450

STEREO FM TUNER Fitted with phase lock-loop





FREQUENCY RANGE	88-108 Mhz
SENSITIVITY	3 0 µV
BANDWIDTH	250 kHz
SPURIOUS REJECTION	50 dB
SELECTIVITY ± 400 kHz	55 dB
AUDIO OUTPUT (22:5 kHz devi	ation) 100 mV
STEREO SEPARATION	30 dB
SUPPLY REQUIREMENTS	20 to 30V-(90mA max)
AERIAL IMPEDANCE	75 ohms
DIMENSIONS	. 240mm - 110mm - 32mm

The 450 Tuner provides instant programme selection at the touch of a button ensuring accurate tuning of 4 pre-selected stations, any of which may be altered as often as you choose, simply by changing the settings of the pre-set controls. Features include FET input stage. Vari-Cap diode tuning. Switched AFC LED Stere Indicator.

Stereo 30 COMPLETE AUDIO CHASSIS £24.25

7 Watts RMS
8 ohms
Less than 5% (Typically 3%)
50 Hz to 20 kHz ± 3dBs
± 12 dBs at 100Hz and 10kHz
190 mV for full output
1 M ohms
22 V.A.C. rated at 1.A
200mm - 130mm - 33mm

The Stereo 30 comprises a complete stereo pre-amplifier, power amplifiers and power supply. This, with only the addition of a transformer or overwind will produce a high quality audio unit suitable for use with a wide range of imputs i.e. high quality ceramic pick-up, stereo tuner, stereo tape deck etc. Simple to install, capable of producing really first class results, this unit is supplied with full instructions, black front panel, knobs, main switch, fuse, and fuse holder and universal mounting brackets.

AL60

+ 66p p&p

AUDIO AMPLIFIER MODULE 25 Watts RMS

£6.81 + 35p p&p

25w

OUTPUT POWER	25 Watts RMS
SUPPLY	30-50 V
LOAD IMPEDANCE	8-16 ohms
TOTAL HARMONIC DISTORTION	Less than 1% (Typically 06%)
FREQUENCY RESPONSE	20 Hz to 30 kHz - 2 dBs
SENSITIVITY	280 mV for full output
MAX. HEAT SINK TEMPERATURE	90°C
DIMENSIONS	103mm - 64mm × 15mm

This high quality sudio amplifier module is lor use in audio equipment and stereo amplifiers and provides outpul powers up to 25 RMS with distortion levels below 0.1%

AL80

AUDIO "AMPLIFIER MODULE

£10.67



-		
	OUTPUT POWER	35 Watts RMS
	SUPPLY	40-60 V
- 1	LDAD IMPEDANCE	8-16 ohms
	TOTAL HARMONIC DISTORTION	Less than 1% (Typically 06%)
-1	FREQUENCY RESPONSE	20 Hz to 30 kHz - 2 dBs
	SENSITIVITY	280 mV for full output
	MAX. HEAT SINK TEMPERATURE	90°C
	DIMENSIONS	103mm - 64mm - 15mm

The AL80 is similar in design to the AL60 above and is of the same high quality but provides output powers up to 35W with distortion levels below 0.1%

AL250 125W R.M.S. POWER AMPLIFIER

OUTPUT POWER	125 Watts RMS continuous
OPERATING VOLTAGE	50-80 V
LOAOS	4-16 ohms
FREQUENCY RESPONSE	25 Hz 20 kHz measured at 100 Watts
SENSITIVITY FOR 100 WATTS O/P AT 1 kHz	450 mV
INPUT IMPEDANCE	33 K ohms
TOTAL HARMONIC DISTORTION 50 WATTS into 4 ohms 50 WATTS into 8 ohms	0·1% 0·06%

+ 76p p&p This unit, designated AL250, is a power amplifier providing an output of up to 125W RMS, into a 4 ohm load

AL30A AUDIO AMPLIFIER

£25.91





MAXIMUM SUPPLY VOLTAGE	30 V
POWER OUTPUT for 2% THD	10 Watts RMS
TOTAL HARMONIC DISTORTION	Less than 25%
LOAD IMPEDANCE	8-16 ohms
INPUT IMPEDANCE	100 K ohms
FREQUENCY RESPONSE	50 Hz-25 kHz ± 3 dBs
SENSITIVITY	75 mV for full output
DIMENSIONS	74mm - 63mm - 28mm

These low cost 10 watt modules offer the utmost in reliability and performance, whilst being compact in size

SPM80

£5.57 + 350 P40



INPUT A.C. VDLTAGE	33-40V
OUTPUT D.C. VOLTAGE	33 V nominal
OUTPUT CURRENT	10 mA-1 5 amps
OVERLOAD CURRENT	1 7 amps approx.
DIMENSIONS	105mm - 63mm - 30mm

Within ± 1 dB from 20 Hz to 20 kHz

± 15 dBs at 75 Hz + 10-20 dBs at 15 kHz Better than 65 dBs (All inputs)

Better than 26 dBs (All inputs)

Designed to power two AL60s at 15 Walts per channel simultaneously. Circuit Techniques include full short circuit protection.

EQUALISATION

INPUT OVERLOAD

BASS CONTROL RANGE TREBLE CONTROL RANGE SIGNAL/NOISE RATIO

PA100

IPLIFIER	12 CV	CE	S.
	4		
30			

£20.30	
. 46n n&n	

	SUPPLY	20 to 40 V
	DIMENSIONS	300 - 90 - 33mm (less controls)
pre-amplifier and tone control eo amplifiers or audio units. The and low frequencies.	I unit, the PA100 provides a ne six push button selector sw	comprehensive solution to the front end litch gives a choice of inputs together with

A top quality stereo requirements of stere two fillers for high a

MPA30

MAGNETIC CARTRIDGE PRE-AMPLIFIER



£3.76

Enjoy the quality of a magnetic cartridge with your existing ceramic equipment using the MPA 30 which is a high quality preamplifier enabling magnetic cartridges to be used where facilities exist for the use of ceramic cartridges only.

SENSITIVITY	3 5 mV for 100 mV output
EQUALISATION	Within ± 1 dB from 20 Hz to 20 kHz
INPUT IMPEDANCE	50 K ohms
SUPPLY	t8 to 30 V-re earth
DIMENSIONS	110 · 50 · 25mm (inc DIN socket)

PA12



£9.63

+ 350 p&p

PRE-AMPLIFIER
The PA12 Stereo PreAmplifier chassis is designed and recommended for use with the AL 20/30 Audio Amplifier Modules, the PS12 power supply and the T538 Transformer, Features include on/off volume, Balance, Bass and Treble controls. Complete with tape output.

FREQUEN	CY RESPONSE	20 Hz-20 kHz (-3dB)		
BASS CONTROL		± 12 dB at 60 Hz		
TREBLE C	CONTROL	± 14 dB at 10 kHz		
INPUT IM	PEDANCE	1 Meg. ohm		
INPUT SE	NSITIVITY	300 mV		
CRDSST.	ALK	-60 dB		
SIGNAL/	NOISE RATIO	65 dB		
OVERLO	AD FACTOR	± 20 dB	•	
TAPE OU	TPUT IMPEDANCE	25 K ohms		
DIMENSI	DNS	152mm + 84mm + 25mm		

PS12 POWER SUPPLY MODULE

Power supply for AL20A-30A, PA 12, S450 etc. Transformer T538,

Input A.C. Voltage 15-20V Output D.C. Voltage 22-30V approx. (Dependent upon input.) Output Current 800mA

maximum. Dimensions 60 x-43 x 26mm

LORLIA

£1.90

+ 35p p&p

BP124 SIREN ALARM MODULE

American Police screamer powered from any 12 volt supply into 4 or 8 ohm, speaker. Ideal for car burglar alarm, freezer break-down. other security purposes

ONLY £4.43

+ 35p p&p.

5 WATTs -

STA15 STEREO AMPLIFIER KIT

Build you own top quality amplifier, save yourself pounds. The STA15 kit comprises the following Bi-kits modules, 2x AL60 amps, 1 > PA100 pre-amp, 1 - SPM80 stab. power supply, 1 - BMT30 transf. giving 15 watts RMS per channel STEREO. All modules covered by the BI-PAK satisfaction or money back guarantee. Details of the above modules are in this ad. Price £44.68 + 62p p&p.

STA15 ACCESSORY KIT

A beautifully designed genuine TEAK WOOD veneered cabinel to put the professional touches to your home built amplifler. Full set of parts incl. Front & Back Panels, Knobs, Chassis, Fuses, Sockets, Noen, etc. Ideal for the MA60. Size. 425mm · 290mm ·

95mm. Price £21-94 + 86p p&p. Order No. 2240.

TRANSFORMERS

T538 For use with S.450 AL30A MPA30 Order No. 2036 Price: £3-88 + 55p p&p. T2050 For use with Stereo 30 Order No. 2036 Price: £3-74 + 55p p&p. BMT50 For use with AL60 SPM80 Order No. 2034 Price: £6-21 + £1,00 p&p. BMT250 For use with AL250 Order No. 2035 Price: £7-30 + £1-10 p&p. Order No. 2041.

Price: £7:30 + 11:10 ps

2040. For use with AL60

Order No. 2040

Price: £6:98 + 80p p&p.

2041. For use with AL80, AL120 and AL250

Order No. 2041.

Price: £7:82 + 86p p&p.

CASES

TEAK 30, $32 \times 23 \times 8$ cm, designed mainly for use with our stereo 30 Audio System but has proved very helpful to home constructors. Fitted with solid uncut front and back, o/n 139, £6-27, p&p 70p.

TEAK 60, 42 \times 29 \times 9cm, for use with AL60/MK60 Audio Kit. Useful for the home constructor requiring an amplifier sleeve — has no front or back panel. o/n 140. £8-63. p&p 85p.

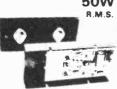
Professionals and Enthusiasts from BI-PAK

AL120

AMPLIFIER (With integra heat sink and

£17.38

+ P. & P. 35o



OUTPUT POWER	50 Watts R.M.S.
SUPPLY	70 Watts
LOAD IMPEDANCE	8-16 ohms
TOTAL HARMONIC DISTORTION	05% Max. (Typically 02%)
FREQUENCY RESPONSE 1 1dB	25Hz-20kHz
SENSITIVITY	500mV
MAX HEAT SINK TEMP	45 deg. C
DIMENSIONS	192 x 89 x 49 mm

Introduced to fulfill the demand for a fully protected power amp,, capable of driving high quality speaker systems at up to 50w with distortion levels below 05%. Ideal for domestic use. Discos, P.A. systems, electronic organs etc. The generously rated components ensure continuous-operation at high output levels.

SPM120 STABILISED POWER SUPPLIES

SPW120/45 SMP120/55 SMP120/65 £7.34 + P. & P. 35o



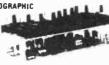
AC INPUTS		
SPM 120/45	40-48v	
SPM 120/55	50 USV	
SPM120/65	60-65v	
OUTPUT CURRENT	2.5A	
RIPPLE	1A 100mV	
	2A 150mV	

SPM 120 is a fixed voltage stabiliser available with an or $9061 \frac{u/o}{3}$ e of either 45v, 55v, or 65v. Designed primarily for use in audio applications, the stabiliser which provides output currents up to 2.5A, operates direct from a mains transformer requiring only the addition of 2 Electrolytic capacitors to complete the s/c protection.

GE100 Mk2.

10 CHANNEL MONOGRAPHIC EQUALISER

£26.45 + P. & P. 35p



Control Range	±12d8
Dynamic Range	110dB
Maximum Output	+ 15dB
Frequency Response	30Hz-20KHz (±1dB)
Power Supply	15 O 15v.
Voltage Handling Input	3v R M.S.
T H.D.	-05%

Only 155mm x 65mm x 50mm including the 10 x 10K. Tin slider potentiometers and knobs which are mounted on a board positioned above the circuitry. In the frequency range of 31Hz to 20KHz you can cut and boost ±12d8 with the 10 sliders, each of which has its frequency marked on the circuit board. The GE100 has numerous uses including mixers, P.A. systems and discos. It will also greatly improve the sound reproduction of your existing audio equipment. Power Supply for GE100, o/d SG30 f 3.80

VPS30 STABILISED POWER SUPPLY





v
4

This NEW versatile Regulated Variable Stabilised Power Supply with short circuit protection and current limiting, is a must for all electronics enthusiasts. It incorporates adjustable voltage from 2v-30v, with a current limiting range of 0-2A. With this module there is no need to build a separate power supply for each of your projects, with the simple addition of a transformer (ord 2033) 0, Ima (ord 1310 or 1305), plus a suitable shunt, a vollmeter (ord 1311 or 1306), a 470ohm pot (ord 1896) a 447 pot (ord.) 899), it can be used again and again as a self-contained bench, power supply, eliminating the use of batteries and thus saving

PA200

PRE-AMPLIFIER



£20.98

	FREQUENCY F		20Hz to 20kHz × 1dB					
- 1	TOTAL HARM	ONIC DISTORTION	Less than 1% (Typically -70%)					
	SENSITIVITY INPUTS	1 TAPE 2. RADIO TUNER 3. MAGNETIC P.U.	100mV/100 K ahms 100mV/100 K ahms 3-5mV/50 K ahms					
	EQUALISATIO	N	Within + 1dB from 20Hz to 20kHz					
- 1	BASS CONTRO	DL RANGE	+ 15d8s at 75Hz					
- 1	TREBLE CONT	ROL RANGE	+ 10 20dBs at 15kHz					
-	SIGNAL NOISI	RATIO	Better than 65dBs (All inputs)					
-1	INPUT OVERLO	DAD	Better than 26dBs (All inputs)					
- 1	SUPPLY		35 to 70V					
- 1	DIMENSIONS		300 × 90 × 33mm (less controls)					

The PA200 is basically our popular PA100. Modifications have been made to make it compatible with the higher output AL120 and

HEADPHONES

A top quality headphone with cushioned earpads and headband. Separate balance/volume controls. Stereo and the switch impedance. 8 ohms. Frequency. 30-

A brilliant compromise between price and performance. Superb stereo reproduction for the newcomer to Ni-Fi. Impedance 8 ohms. Frequency 30-15,000Hz. e/n 885. £8-06. p&p 50p.

BIB HI-FI ACCESSORIES

Parallel Tracking GROOV KLESU
The very latest in automatic record cleaning. Designed to suit all modern single play decks. Simple to fit, if is extremely efficient. Complete with two types of base and three height extensions. o/n 8101. £4-23 p&p.35p.

p&p 35p.

Cassette Tape Editing Kit
Enables cassette tapes to be edited and joined easily quickly and accurately. Kit comprises Tape Spincer (32 mml 2 Precision Tape Cutters Tape Piercer 9 Self adhesive Labels Reel of Spincing Tape 3 Winders and removers and instructions all in a handy wallet, orn 811. £2.76, p&p 35p.

GROOV-STAT
The fills Groov Stat static reducer neutralises static charge on records and other plastic surfa o/n 8103 £6-27. p&p 35p.

Cassette Head Cleaner
Essential for cleaning of tape heads, capstans and rollers. Pack contains Tape Head Applicator and tape head polisher tools. Plus bottle of special formula. cleaning fluid and full instructions. o/n 832, £0-74, p&p 35p.

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Miniature Balance & Tuning Meter
Miniature moving-coil meter for stereo balance
indicator tuning indicator for FM or similar
application Pointer at centre indicates zero or null
position Robust construction. Sensifivity
100.0.100M. Dimensions 23 x 22 x 26mm
o/n 1318. £2-24. p&p.35p.



Balance and Tuning Meter Clear view edgewise meter. Centre zero application. Sensitivity. 100. 0. 100UA Dimensions. 45 x. 22 x. 34mm. o/n 1319. £2-30, p&p.35p.

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Miniature Level Meter
Moving coil for accurate level indication for tape
recorders ampliliers etc. Neat design rugged construction will withstand five times rated value
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135

178

Vu Mieter Calibrated 20 to -3 and 0 100 % making it suit able for use as a recording level meter or as a power output indicator. Sensitivity 130uA Dimensions: 40 x 29mm. e/n 1321, £2-30, p8p35p.



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DYNAMIC CASSETTE
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moulded body in black with neat chrome surround. Pick-up pattern is
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120mm.e/n 1326.£1.84. p&p 35p.

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Superior quality portable cassette recorder mike with built-in remote control switch and lead fitted with 5-pin 240° DIN plug fremote switch and 3-pin DIN plug fmicrophonel. Provides a direct replacement for those supplied with recorders. With detachable stand. Omnidirectional Impedance. 200 ohms. Freq. response: 100 to 10,000Hz. Sensitivity; 79dB at 1,000Hz. e/n 1327. £3-05.

pap sap.

RE – 317: DYNAMIC MICROPHONE
Highly sensitive high-grade desk or hand mike suitable for use with
many popular cassette decks. Incorporates On/Off switch and 1 metre
lead with moulded standard jack plug. Complete with desk stand.
Omnidirectional Impedance: 5,000 ohms. Freq. response: 100 at
12,000Hz. Sensitivity: (-7dB at 1,000Hz). g/n 1336. £5-25.

OMNIDIRECTIONAL CARDIOID

OMNIDIRECTIONAL CARDIOID
Powered by a 11y battery located within the aluminium body. Satin silver finish with front disk protection to the diaphragm housing On/Off switch Also with Busby type windshield. U bracket and stem and extremely supple cable. Consumption 0.2mA from 11y battery providing approx. 8-10,000 hours continuous life. Impedance: 600 ohms. Sensitivity. 70d8. Frequency. 30-16,000Mz. Size. 23mm dia + 267mm. o/n 1329. £14-72. p&p 35p.

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Dual imp. 600 and 50.000 ohms Response 50 to 14.000Hz.

Sensitivity 54dB at 50K.ohms. Size 1; dia x 6; long Weight approx. 190gm. o/n 1328. £12-58. p&p 35p.

STANDS

GOOSENECK CHROME FLEXIBLE HOLDERS Length 320mm. a/n 1333. £2.99. p&p 35p. Length 515mm. a/n 1334. £4.03. p&p 35p.

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113	3.5mm Jack plug to 3.5mm jack plug. Length 1.5m.	€0.86
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115	to pins 38/5. Length 1.5m	20.98
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116	to pins 18.4. Length 1.5m. Car aerial extension. Screened insulated	86.03
	lead. Fitted plug & skt	£1-44
117	AC mains connecting lead for cassette	F 1 - 44
	recorders & radios 2 metres	€0.78
118	5 pin DIN phono plug to stereo	
	headphone jack socket	£1-21
119	2 + 2 pin DIN plugs to stereo jack socket	
	with attenuation network for stereo	
120	headphones Length 0.2m Car stereo connector Variable geometry	£1-04
120	plug to fit most car cassette 8 track	
	cartridge & combination units Supplied	
	with inline fused power lead and instructions.	€0.69
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	to Mono Jack Plug BLACK	£1.73
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125	5 pin DIN plug to 5 pin DIN plug Length 1.5m	£0-86
127	5 pin DIN plug to Tinned open end. Length 1 5m	€0.86
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128	5 pin DIN plug to 5 pin DIN socket. Length 1.5m	£0.92
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	image Length 1.5m	£1-21
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131	5 pin DIN plug to 3 pin DIN plug 184	
	and 3&5 Length 1 5m	€0-95
132	2 pin DIN plug to 2 pin DIN socket Length 10m	£1-13
133	5 pin DIN plug to 2 phono plugs.	
134	Connected pins 3&5 Length 1 5m 5 pin DIN plug to 2 phono sockets	€0-86
	Connected and 28 E. Landth 22	en 70

5 pin DIN plug to 2 phono sockets
Connected pins 38.5 Length 23cm
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300 WATT AMP MODULE

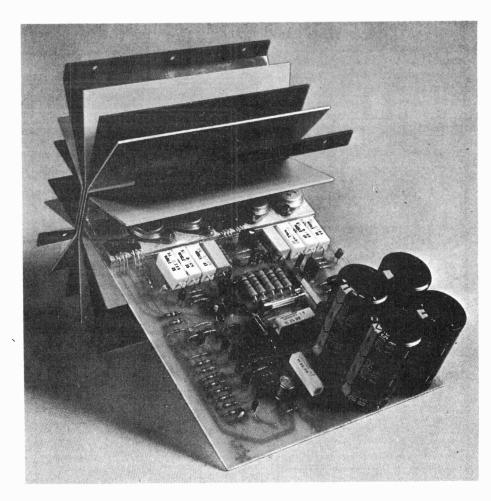
For many applications there's no substitute for sheer power - low efficiency speakers, outdoor sound systems, or maybe you like the full flavour of the dynamic range of a high power amp. Whatever your requirement - this 'super power' module should fit the bill.

i-fi amplifiers are becoming more and more powerful, and with good reason. Modern recordings, especially direct-cut discs, have a useful dynamic range approaching 40 dB between the quieter musical passages and the peaks of the crescendos. If the quieter passages are played at at a power output of 100 mW, which is not untypical in a domestic environment, to faithfully reproduce the full recorder dynamic range of a good record without clipping the peaks would require an amplifier capable of delivering 1000 watts! This, coupled with the current trend amongst some manufacturers to build speakers having quite low efficiency, plus the number of people who like their music loud (and undistorted) makes the case for high power amplifiers very strong indeed.

Over the past six or seven years we've had many requests for a high power amplifier. It would have been possible to design a unit using a large number of readily available power transistors in the output - in fact, one design used a total of 24 devices in the output stage! Difficulties for the home constructor in this approach are obvious, regardless of expense.

For various reasons a bridge amplifier was ruled out when the design of this amplifier was considered. Hence a plentiful source of suitable output transistors was

There are really not too many transistors available that meet the requirements. Firstly, adequate safe operating area (SOAR) is of prime importance. Next, and probably of equal importance, is availability. Let's have a look at the SOAR problem first. Some high power transistors don't compare too well with the ubiquitous 2N3055 (and its complement, the MJ2955) when operated as an amplifier. Take a look at the set of curves plotted on the accompanying diagram. This compares the safe operating area curves of a number of power transistors. Operation of any power device



must be confined to the area inside the device's curve at worst case. If the current/ voltage operating point is allowed to fall outside the area of the SOAR curve during any part of the operating cycle for the device, it will be destroyed - with amazing rapidity. Now, the 2N3773 and MJ802 transistors have been around for some time and at first glance would seem good choices for a high power amp, but note that their SOAR characteristics are not much better than the 2N3055. In fact, at 40 V (Vcc) the MJ802 is actually worse. In contrast, the MJ15003 is quite a long way outside the curve for the 2N3055 and therefore has a much higher power rating when used in an amplifier. Hence the MJ15003 and its complement - the MJ15004, were chosen as the output devices for this design.

Another problem that arises with a design such as this is protection for the output devices. Amplifiers using transistors such as the 2N3055 can easily be protected with a fuse. In high power amplifiers where supply rails of 60 - 70 volts are necessary. the energy available (from the filter capacitors) will easily destroy the transistor and the fuse - in that order. The answer is to use electronic current limiting in the output. This adds complexity, but is cheap insurance against accidental (or deliberate!) abuse. The curve showing the limiting effect on the SOAR characteristics of the MJ15003 for the protection network used in this amplifier is shown on the diagram with the other SOAR curves.

Output Cost

The main cost of the amplifier is in the output stage, transformer and heatsink. We therefore decided to go to a slightly more complex input stage to improve the performance. This type of amplifier usually uses a Class A driver which introduces second harmonic distortion. By using a complementary-differential input circuit we have been able to eliminate the Class A driver and therefore kept the second harmonic distortion very low indeed. The distortion curve shows the distortion is well under 0.1% until almost full power output. The 'bump' in the curve around the watt is the point where the output stage changes from Class A (peak output being less than the bias current) to Class AB operation.

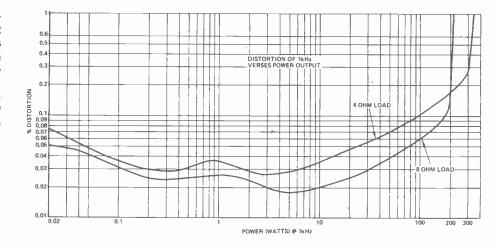
The complete amplifier, including the power supply components and the output transistors, is assembled on a single PCB. An aluminium bracket holds the output transistors conducting heat from the output stage to the heatsink. Only three sets of external connections are made to the PCB: input, output and power supply AC input from the transformer.

Construction

Start the construction by making the aluminium bracket. We used two length of 3 mm angle. This bracket is 3 mm thick and two must be placed back to back to make the required 6 mm thickness for adequate thermal conduction to the heatsink assembly. If you elect to use a Philips 6 5D6CB heatsink (see the box on 'Heatsinks'), a single 6 mm thick angle extrusion can be used, fixed to the flat side of this heatsink.

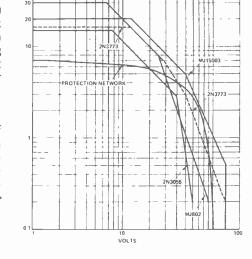
Heatsinks

There are several alternatives you can choose from for heatsinking the amplifier output stage. The heatsink shown was made from sheet aluminium and has a thermal rating of 0.55 C/watt. This is the rating we recommend for any heatsink if the amplifier is to drive a four ohm load, particular-



ly for pop group use. If it is driving an eight ohm load in typical domestic use, half the fins may be left out (every second one) resulting in a thermal rating for this heatsink arrangement of 0.75 C/watt. Use 1.6 mm thick aluminium sheet - certainly nothing thinner. A heatsink with about 1 C/watt rating and substantial fan cooling is another alternative.

Remember that dissipation in the heatsink will be about 200 watts at full power output. That means a temperature rise of 110 C above ambient if the amplifier is run continuously. Poached eggs anyone? Temperature rise with music or intermittent use is considerably less, of course, as average power dissipated is much lower.



Above and right: operating characteristic of the 300W module circuit.

SPECIFICATION

PENGr output 8 ohm load	200 watts RMS	4 ohm load	1 V for 300 W output
4 ohm load	310 watts RMS	Total harmonic	€
Frequency response 20 Hz to 20 kHz	±0.5 dB	distortion	see graph ·
Hum and noise re 200 W into 8 ohm	-105 dB	Damping factor 20 Hz to 3 kHz 5 kHz	65 55
Input sensitivity 8 ohm load	1 V for 200 W output	10 kHz 20 kHz	45 35 _

BUYLINES.

Most of the components used in the 300 W power amplifier module are standard and readily available. The output transistors (types MJ15003 and MJ15004) are available from Macro Marketing Ltd. If you don't feel up to making the heatsink shown, Maplin can supply a suitable heatsink — type 60DN (order code YB26D).

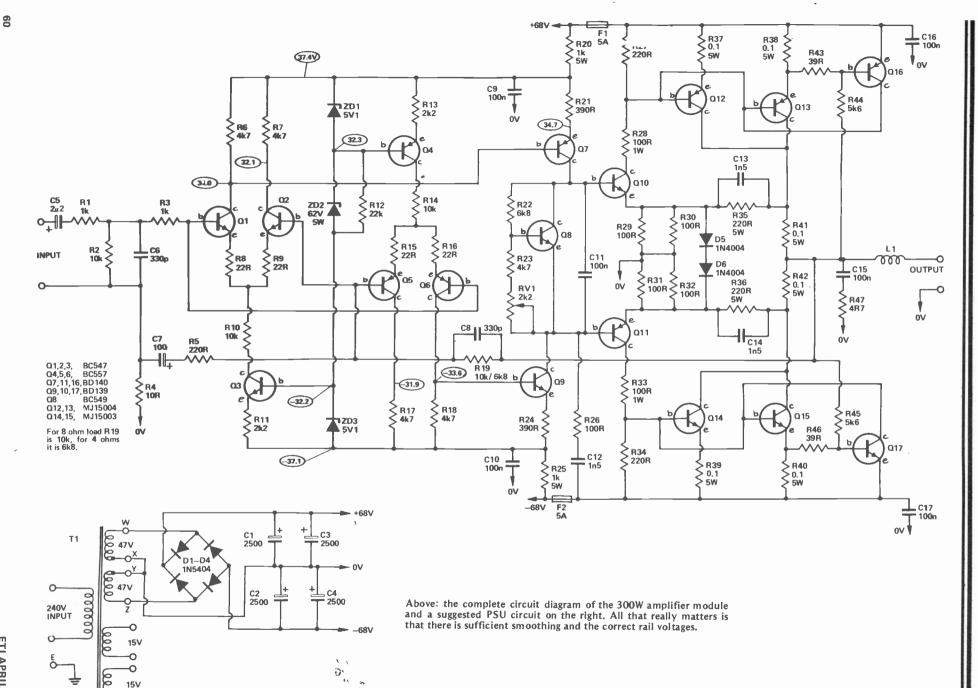
The power supply transformer and capacitors may prove a little more elusive. If you are unable to find the 2500u 80 V types, you can use 100 V capacitors mounted off the board. The transformer specified is a high power type, which you may have

to have wound to order. Several firms advertise a transformer winding service in the classified sections of electronics publications. Shop around for the best price. Trent Transformers will supply the transformer for £16.95 plus postage.

Macro Marketing Ltd.,

396 Bath Road, Slough, Berkshire. Tel: 06286 4422.

Trent Transformers Ltd., 26 Derby Road, Long Eaton, Nottingham. Tel: 06076 66716.



ETI APRIL 1980

The amplifier can be divided into three The output stage, Q10 - Q15, has a gain separate parts. These are: the input stage - of about five, set by R39 and R29 plus R30 which consists of Q1 - Q9, a high gain, low Diodes D5 and D6 prevent reverse biasing of power driver; the output or power stage - Q10 and Q11 (otherwise the output would which only has a voltage gain of four but be limited.) enormous power gain; and the power

The input stage is a complementary, both current and voltage in the output trandifferential network, each 'side' with its own current source. Each transistor in this limit is exceeded. stage is run at a collector current of about 0.7 mA. Emitter resistors are employed to with a centre-tap on the transformer giving stabilize the gain and improve linearity. The the 0 V rail, providing ±68 volts. A total of output of Q1 - Q6 drives Q7 and Q9. The latter are virtually two constant-current sources run at about 7 mA collector current. a reduced supply rail, derived from ZD1-

With an input signal these 'current' sources are modulated out of phase - the collector current of one decreases while the other increases. This configuration provides quite an amount of gain.

In between the bases of these two tran-limit. sistors is Q8, the thermal sensing-bias transistor. The voltage across Q8 may be windings of 15 V AC each. These are not adjusted by RV1, thus setting the quiescent used here but are suitable for powering a bias current for the output stage.

Protection of the output transistors is provided by Q16 and Q17 which monitor sistors and bypass the base current if the

The power supply is a full-wave rectifier, 5000u is used across each supply rail for filtering. The amplifier input stage works on ZD3 via R20 and R25.

Frequency stabilisation is provided by capacitors C8, 13, 14 and the RC networks R26/C12 plus R47/C15. Frequency response of the amplifier is set by C5 and C7 lower limit), C8 sets the upper frequency

The transformer has two additional preamplifier.

PCB Assembly

The components may be assembled on the PCB starting with the smaller resistors and capacitors. Carefully follow the overlay drawing. When you come to the OR1 5 W resistors note that they should be mounted about 2 - 3 mm off the board to allow a free air flow around them. Next mount the power supply electrolytics. Note that the recommended types have three pins projecting from the base. This is to provide mechanical rigidity. All three pins are soldered to the board and the capacitors can only be inserted one way round. The inductor L1 is made by winding a layer of 26 swg enamelled wire (or the nearest equivalent gauge) along the body of a 1 W resistor. The number of turns is not critical, just wind enough wire on the resistor to cover the body with one layer. The value of this resistor may be anything over 100 ohms. Two 5 A fuses are mounted on the PCB, held in place with fuse clips.

Next come the semiconductors. Leave Q7, 8, 9, 10 and Q11 plus the output stage devices Q12, 13, 14 and Q15 until last. Be careful with the orientation of the diodes.

heatsink fins. Don't skimp on these lest the output pair set light to themselves and pass on to that great heatsink in the sky.

Right: metalwork details for the

Now you can assemble the heatsink Smear both sides of each washer with heat- brackets until the end faces are flush. bracket to the PCB plus Q7 to Q15 sink compound. Place the bracket pieces Check that all holes line up and then tighton the board - component side - and secure en the nuts and bolts. First smear heatsink compound on the Q7, Q9, Q10 and Q11 with nuts and bolts. two mating surfaces of the bracket assemb- Only tighten the nuts finger tight at this 14 and Q15 may now be assembled to the ly. Note that insulating washers are used on stage. Now, take the whole board and bracket and PCB. all the transistors, Q7 to Q15, mounted on place the bracket ends against a flat surface the bracket assembly (except Q8 of course). - such as the flat heatsink fin - and juggle the

65 95

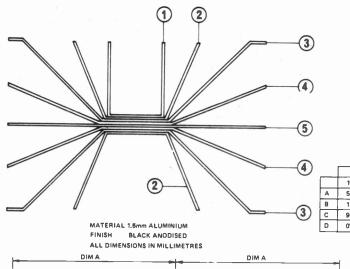
17 19

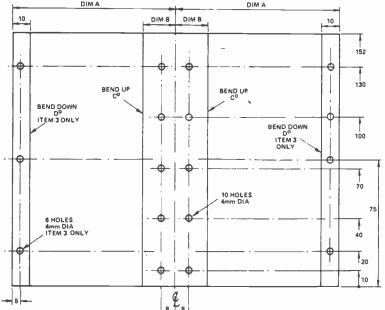
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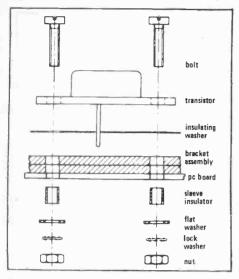
67.5° 45° 22.5° 0°

The TO3 power transistors Q12, 13,

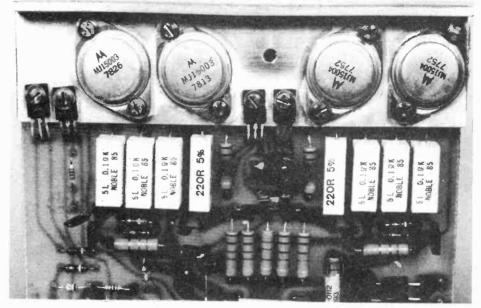
Don't solder any leads yet. Allow time for the heatsink compound ▼



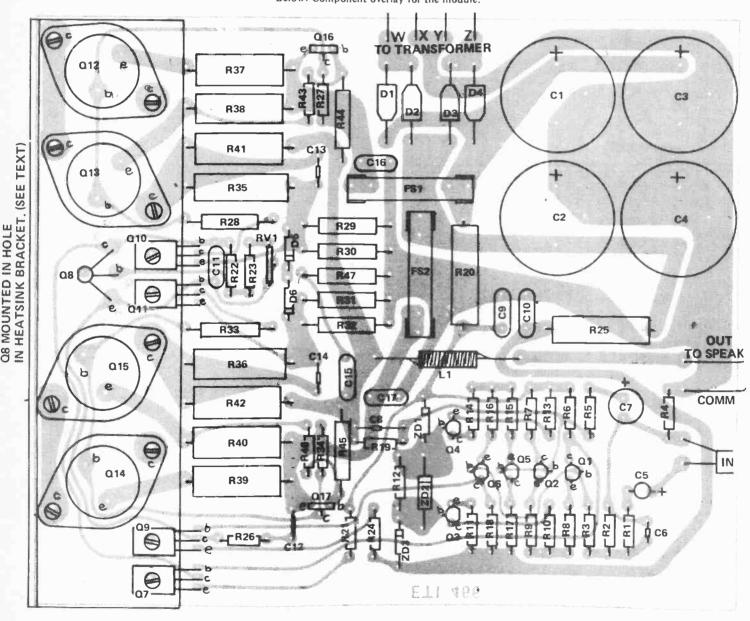




Exploded view of how the TO3 output transistors are assembled to the angle brackets.



Below: Component overlay for the module.



PARTS LIST

RESISTORS	All ½W, 5% unless noted	R44,45	5k6 1W	Q7 :	BD140
R1,3		R47	4R7 1W	Q8	BC549 =
	10k			Q9,10	BD139
	100	POTENTION	METERS	Q11	BD140
	220R		2k2 trim	Q12,13	M115004
R5,27,34	220K		202 01111	Q14,15	M115003
R6,7,17,18,		CAPACITO	**	Q16	BD140 or BC640
	4k7 **			017	BD139 or BC639
			250uu 80 V electrolytic	D1-D4	1N5404
		*CS *			1N4004
R12	22k	C6 C7	330p ceramic 👙 🗀 🏅	D5,6	
R19	10k (6k8 for 4 ohm loads)		100u 25 V electrolytic	ZD1	5V1 300 mW
R20,25	1k0 5W	C8 .	330p ceramic	ZD2	62 V 5W
	390R	C9-11	100n polyester 😿 🛼	ZD3	5V1 300 mW
	6k8	C12-14	1n5 polyester		
	100R	C15-17	100n polyester		
	100R 1W			MISCELLA	NEOUS
	220R 5W	SEMICOND	UCTORS	Heatsink	see text, PCB, Transform
		Q1-Q3	BC547		- 300W), 4 fuse clips, 2 x 5
	39R	Q4-Q6	BC557	fuses.	

to spread under compression and finally tighten all nuts. Last of all insert Q8. Smear the inside of the hole it sits in with heatsink compound to ensure good thermal contact.

Now you can solder all transistor leads.

Check the component placement against the overlay now, just to ensure all is in order. If you wish, you can test the amplifier up to the driver stages for correct operation before assembling the the unit to the heatsink. Remove the fuses before applying AC input from the transformer. Refer to the 'powering up' procedure. If there are any problems, look for errors in component placement or orientation - particularly with diodes. If all is well, assemble the module to the heatsink and you're ready for the big test.

Powering Up

The set of output transistors are expensive to replace. Therefore, we recommend you follow this test procedure in the interest of conserving supplies of same.

The power supply AC input should be connected to the transformer (see the overlay) but no power applied. You'll need a multimeter of at least 20k ohms/V sensitivity.

- 1. Remove the two fuses.
- 2. Solder a small link across C11.
- 3. Solder a wire between this link and the ouput pad.
- 4. With no load connected and no input signal, switch the power on.
- Check the supply rail voltages. These should be about 68 volts each (plus and minus).
- Check the voltages on the cathode of ZD1 (should be about +37 V) and the anode of ZD3 (should be about -37V) with respect to 0 V.
- 7. If these two voltages differ with respect to each other by a volt or so, check other voltages around the input stage

- to determine the reason.
- Check the DC voltage on the output (with respect to 0 V). It should be within 20 mV of zero.
- Inject a sinewave signal into the input at a level of about 20 mV (RSM). Don't use a higher input level. Output should be 1 V RMS.
- Switch off the main power and allow the filter capacitors to discharge. Remove the input signal.
- 11. Solder a 10 ohm ½W resistor across each fuse holder. Rotate the trimpot RV1 so that it is set at maximum resistance. Remove the short across C11 and the link from there to the output pad.
- 12. Switch on...... if the 10 ohm resistors immediately vaporise you either have a short or some fault in the output stage!
- 13. If all is well, check the DC output voltage. It should be near zero.

ALL OTHERS 4mm DIA

- 14. Measure the voltage drop across one of the 10 ohm resistors placed across the fuse holders and adjust RV1 to give a reading of 1.0 V.
- 15. Switch off, allow the filter capacitors to discharge and remove the two 10 ohm resistors. Replace the fuses.
- Connect suitably rated loudspeakers, warn the neighbours, connect a signal source to the input (turn down the volume), switch on the power and put the amp through its paces.

At this stage we'll leave the applications of this module up to you. No doubt you have plenty in mind already.

We are preparing a follow-up article for a later issue in which we may cover such things as pre-amps, bridge operation, design parameters and variations etc.

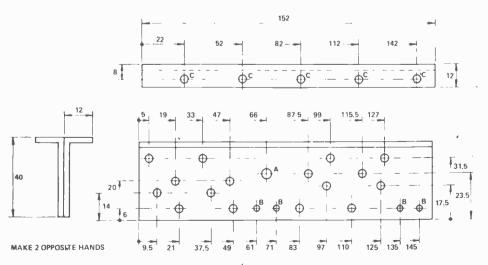
Below: heatsink bracket metalwork details.

Keep reading.

ETI

HOLES MARKED A 4.5mm DIA
HOLES MARKED B 3mm DIA
HOLES MARKED C TAP 4BA OR 4mm DIA

MATERIAL 40 x 12 x3 ALUMINIUM ANGLE EXTRUSION







The new MK III EM tuner sitting under the Dorchester multiband AM/FM tuner

Revisions to the Mark III include a centre zero tuning indicator meter and silent switching



Choosing the products to advertise each month can be quite a task at AMRIT since we tend to introduce at least one new line per week. So it is nearly impossible to say all we would like in this space other than to bring you as far up to date as possible with current events. The major medium for finding out about what we have to offer is our unique catalogue system, and we ask that you invest in a copy of parts 1,2 & 3 since many questions we are asked can be readily answered by reference to these.

Each part costs 60p, or £1.60 for all three current editions.

We are also launching a new and greatly elongated version of our PRICE LIST, which now includes a large number of quantity listings, and many items not previously listed. The new style price list is a quick reference short form to our general catalogues - available FOC with a large (A4) SAE please.

As a result of the soaring price of oil - and the subsequent huge increases in the cost of wax for Mr Tom Jackson's famous moustache, the Post Office have increased their charges (Feb. 4th). Accordingly, our standard cover charge has been increased to 35p per order (CWO)

. 1

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Ambit has the biggest range of digital frequency readout systems for various applications in Broadcast and Communications. Prices range from £18,50 for a complete AM/FM broadcast frequency display (kit of DFM2). Most are detailed in the latest catalogue.

TUNING SYNTHESIZERS are also heavily featured, and we offer our first complete system covering MW/LW/SW2 and FM based on Hitachi parts. The unit is retrofittable to voltage tuned radio systems - and will shortly be incorporated in a complete tuner project. Cost for the synthesiser will be circa £40 A versatile communications system based on the new Mullard 2 IC system is nearing completion, together with 16 station CMOS memory and optical shaft encoder system with fast tune facility. Synthesiser circa £70, memory £50.

Latest semiconductor news:

CM OS, TTL and LPSN TTL are in stock (ask for our OSTS price leaflet). Some of the very popular types are still "difficult" but we have things like 4011s, 4017s at the time of writing.

ADJIO Its -- interesting developments here, we now have the Hitachi HA11225 and the HA12412 ultra high specification members of the CA3089E family. The PLESSEY SL1600 range now includes the SL6600 high performance PLL NBFM IF and detector.

CA3089E	2.11	HA1197	1.61	SD6000	4.31	SL1610	1.84	SL1626	2.80
CA3189E	2.53	CA3123E	1.61	TDA4420	2.59	SL1611	1.84	SL1630	1.86
HA1137W	1.95	TDA1072	3.09	MC1330P	1.38	SL1612	1.84	SL1640	2.17
HA11225		TBA651	2.53	MC1350P	1.38	SL1613	2.17	SL1641	2.17
HA12412		TDA1090	3.51	KB4412	2.24	SL1620	2.50	SL6600	4.31
KB4420		TDA1220	1.61	KB4413	2.24	SL1623	2.80	SL6640	3.16
TBA120S		TDA1083	2.24		2.53	SL1624	3.77	SL6690	3.68
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BC413-5	0.115 2SD666A	0.345 2SA1085E	0.391 2SK 168	0.402 BF274 0.207
BD414-6	0.126 2SB646A	0.345 2SK 133	6.32 3SK 51	0.62 BFT95 1.138
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MODULE NEWS

We are at last able to quote for quantities of our modules, following a program of standardization and revision to speed manufacture and test. The following types are the results of the standardization program

UM1181	5 varicap MOSEET input VHF band 2 tunerhead	£12.00 inc
911225 A	High Performance FM IF system, with switched BW	£23.95 inc
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91072 A	DC tuned and single pole switched MW LW tuner	£14.43 inc
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All are supplied housed in screened metal cases 97x56x24mm, with all connections along a single edge, suitable for verticle or horizontal mounting.

Previously advertized units are still available although there may have been some price changes in the latest edition of the Price List (Date Feb.80). A separate leaflet covering the new range of modules is available from April 80, with an A4 SAE please

NEW LINE: ALPS switches and rotary potentiometers. With a general catalogue that's over 3 inches thick, we cannot begin to offer a comprehensive list of what we can offer but we are already stocking the keyboard switches, keyswitches, pushbutton switches etc. In particular, the pushbutton switches really put all others in the shade (scholdow?) when it comes to quality and price. A special new shortform is being prepared (and may be ready when you read this). All the potentiometers and switches you could ever need from a single source. Keypad switches cost as little as 15p ea (1 off), with a range of two part caps for easy ledgending. You must see the shortform catalogue (30p) and our new pricelist for full details of this huge range of components







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COMPUTER CAPABILITIES

COMPUTER CAPABILITIES

Ambit has been keeping a low profile on the subject of the MPU and its applications. Interestingly enough, the first project we offer with MPU content does rather more in the way of processing than simply playing a daft game, or looking like an enormous calculator. Our MPU facility and expertise is now for hire on a fully commercial basis. Z80, 6800, 6809, 2650 etc.

Keyboard switch SCK41505 typ 6m ops 23p each (1-24)



NEW LINE: DC/DC+AC converters for fluorescent displays. TOKO CPS series 12v IN, -20 and 3v AC out at 65mA. Thick film design £2.34 ea Qty. prices OA



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GENERAL INFORMATION

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026	Motor Speed Controller (2 Boards For Controller) Battery Indicator	July 79	033	LED Audio Display (2 boards) (topside pattern) Bench Amp NICD Charger	Aug 79	036D.	Power Switch Selector (double sided)	Nov 79
027	CCD Phaser	Danings		Cable Tester	Nov 79	037A	Encoder (double sided)	Dec 79
027	Rev. Monitor	Project Book Seven	034	Reaction Tester Speech Compressor	1400 / 9	037B	Decoder (top.side)	Dec 79
028	Race Track, Spirit Level	Project		Preamp Power Supply Rectifier & De-Thump Board		037C	Decoder (bottom side)	Dec 79
	Egg Timer, Bongos Bench Supply, Oscillator	Book Seven		Power Amp (2) (price £1.60)		038A	Long Period Timer	Dec 79
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MICROFILE

We've seen hide nor hair of Henry Budgett, since he took delivery of two new machines. He's finally returned to the land of the living with his reports on the new HP85 and Microtan systems and more besides.

wo months may only be eight weeks to you but to someone in here it has been a very packed time. Certainly in terms of the home and personal computer market it has been a very fast moving time indeed. Owing to a wide variety of reasons last month's offering never reached your waiting eyes so some of the news may be a little less than fresh - it is slightly less than boring, though.

This is really a preview offering. I shall be dealing with at least two of these machines again, probably devoting a whole month to each. The first two are now well known, but I have been fortunate enough to have one of a very limited quantity of the top system for review and......

The Dream Machine

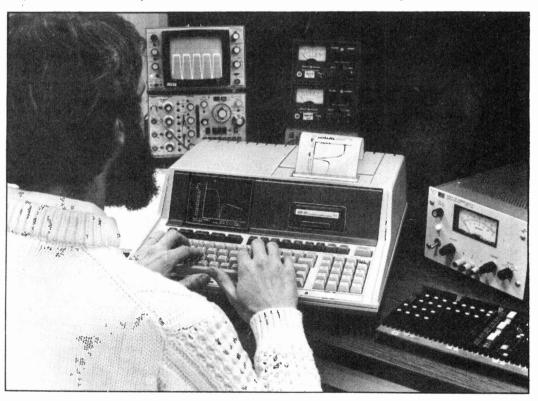
The reason most people give when asked why they chose a PET is that it is a complete unit; VDU, keyboard and mass storage all in one small unit. Whilst this new system from Hewlett Packard has all the previously mentioned parts and a thermal printer as well it resembles a PET in about the same way as a racing car resembles an MG; they are of the same genus but the HP is so far advanced that it outstrips almost anything in the personal computer market. This is a personal computer and not a home machine. Why the difference? Well, with some few notable exceptions, the home computers

Hewlett Packard's new HP85 (right) is a powerful machine in a compact package and at a reasonable price. The Atari 800 (far right), one of two new Video Computer Systems on their way. currently available are overgrown programmable video games, notthat that in any way detracts from their worth. This has been designed for research laboratories, education and other serious users who will be able to benefit from the superb range of facilities that are offered

Basically, the HP85, for that is its name, consists of a single box, slightly larger than an Apple, with a 5" VDU, tape cartridge, thermal printer/plotter and full ASCII, numeric and function keyboards. Inside is a complete custom designed system. For example, the CPU card consists of the custom built CPU, four ROMs holding 32K of BASIC/operating system, eight RAMs (16 K of dynamic) controlled by yet another custom built chip, the keyboard controller (again custom) and finally the bus driver chip which is, quite naturally, custom built. Grand total is sixteen chips! The VDU has a totally independent memory of four screens-full that can be scrolled or copied direct to the printer at any time or under program control.

The graphics capability is excellent with an available by points. Program access is simple, you can manipulate scales and put labels on graphs and diagrams. To make life a little easier for the user the built in plotter turns diagrams on their edge for printing, this allows continuous strip charts to be produced.

Finally on the hardware side we have the tape system. This is mechanically the same as that used on the HP minis but unfortunately the format has been slightly changed. The method used is



similar in many ways to a soft sectored floppy disc; you have a directory which is searched for your required program, this is then located and loaded. The speed of this operation is considerably faster than that of the conventional cassette.

Super Software

The HP has tucked away inside its diminutive frame the best version of BASIC that I have come across on a micro. It meets, and often exceeds, all the latest ANSI standards for this, much abused, language. I strongly suspect that anyone who had been brought up solely on a Microsoft type implementation would get severe brain damage! In fact this BASIC has everything you could wish for, and it's logical too. For example, you get renumbering, full error checking programmable user keys, full debugging, single stepping, optional screen (DISP) or printer (PRINT) displays, or both... the list goes on and on.

One of the most common complaints about home produced software is that it isn't 'bombproof'. Well I've written more than a few on the HP and you can protect them very easily, even to the point of securing your files on the tape so that no-one can list or edit them.

A possible moot point is that, to quote any of my rivals in the game, 'HP do not even say what processor the 85 uses'. As you may have guessed I'm talking about machine code, and as mentioned earlier the HP has a custom chip. Not only did someone not read their press release carefully they also didn't listen when it was stated that an assembler will be available soon! Anyway you don't really need machine code as in the main this machine will be used as an instrumentation controller, or as a system to analyse results produced by other systems.

In Brief

There you have it, unfortunately in brief form because of a lack of white space to fill, but the HP 85 has arrived, bringing with it a whole new generation of professional computers that are cheap enough to be dished out to each member of a research team. I said 'cheap enough', it does cost £2000 but this price is artificially high-



they can't make enough to go round - and it is quite possible that it will fall to around £1200. If that happens it could well clean up the micro market overnight. After all, people are generally prepared to pay for quality! (My thanks are due to the team at HP who let me keep the system until they lost all hope of ever seeing it again!)

Video Strikes Back

Ingersoll, the watch people who expanded into electronics recently, are to distribute the Atari 400 and 800 Video Computer Systems in this country. Information is scarce at the moment, but it appears that the top model, the 800, will be equipped with 8K RAM - expandable to 48K - and 8K ROM - expandable to 40K. CPU is the trusty old 6502 and the system will handle four floppies and has a full feature ASCII keyboard with programming being done in Atari Basic. Prices will range from £400 to £750 approximately and features such as full colour and sound are standard. For more details watch this space.

The Odd One

Whilst making one of my occasional tours around London's Computer shops I came across a familiar sight. There, sitting on a service bench, was what appeared to be a 32K, large keyboard PET. However, on closer peeking it turned out to be something rather different. It had a full terminal style keyboard. Some of the keys had been moved to more sensible places (such as the cursor controls) and there were no graphics legends on the keys. What was it? Simple really, it's the PET Business Machine. Owing to the fact that some of the RAM had expired I couldn't see it going but apparently the lower case, that you normally have to POKE out, is available and you have to POKE the graphics if you want them. A very sensible idea really, but this machine had an American transformer so I decided to track down some details. Commodore say that they are not yet available in this country but they are planned to arrive in the near future, a few months but that's their estimate.

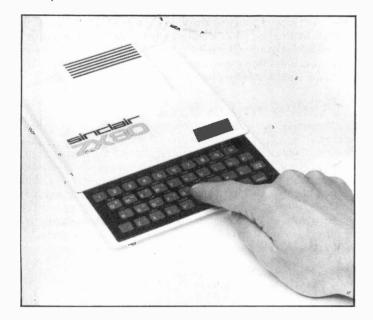
If you are planning to set up a business system with a PET in the driving seat I reckon this would be much better and easier to use than having graphics floating about. If anyone out there has one or knows more about it please drop me a line and give me your impressions.

Tone Deaf

Regular readers may remember that I wrote a piece on modems not so long ago. Well, Microfile bears fruit occasionally, we are going to publish a design in the march issue of Computing Today, but just for those of you who want to go your own way here is the standard frequency set for data transmissions.

US Stand	lard		CCITT Standard			
	Mark	1270 Hz		Mark	980 Hz	
Originate			Chan. 1			
	Space	1070 Hz		Space	1180 Hz	
	Mark	2225 Hz		Mark	1650 Hz	
Answer			Chan. 2			
	Space	2025 Hz		Space	1850 Hz	

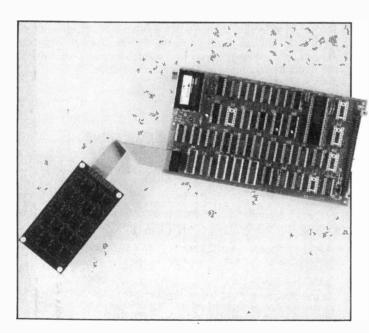
CTs modem project is being produced in PCB form by ZOT Engineering Ltd of Bogpark Road, Musselburgh, Lothian. Naturally it uses the above frequencies and runs at 600 Baud.



And Now For The News

So much for last month's delayed offerings, here is the news. As most of you will probably be aware Britain's enterpreneur extraordinaire, Clive Sinclar, launched his new micro onto the british public in a blaze of TV and Press publicity. Called the ZX80 (well it uses a Z80 so why not) it s about the smallest home computer with built in BASIC yet, you could even call it hand-held. I have not yet received a sample for review but when it comes in I'll take a close look. Here, however, are a few observations from the launch and subsequent perusal of the handbook.

Based on the Z80A, running at 3.25 MHz to save timebase dividers, it has a sealed, touch sensitive keyboard which offers single key programming of *most* BASIC functions. I say most because this is really only a Tiny BASIC but it has been squashed even further by use of a look-up table system where each command word



Sinclair's ZX80 - a Tiny BASIC machine in every sense.

is reduced to a single digit number. It is very restricted, as you would expect, on data processing functions like string handling and because of the design the CPU has to produce all the functions of the system, hence the blurring of the screen when a program line is entered. Each line is syntax checked on entry at the bottom of the screen before it is allowed to move up and join the others at the top, an unusual feature on small systems.

Overall the new Sinclair has very interesting possibilities, and at £99.95, inclusive of VAT but not power supply, it does represent one of the cheapest entry points to high level programming.

With no facility for machine code, and not much mention was made, so one presumes, that the MK 14 will continue to support this area of the Sinclair market. In my humble opinion this machine will be excellent for education on the mass scale but once people have had a taste they may well find that they cannot expand enough to meet even moderate needs. Still, as the executive toy for 1980 its success is assured.

Further design restrictions have meant that you can only add an extra 16K of RAM onto the unbuffered bus. These expansions are in 3K blocks for which you pay £12 for the board and a further £16 per K of RAM. Talk was made of adding new ROM sets, masking the board, new extras like languages, disks, etc but as the CPU is already rather overworked I somewhat doubt the practicality of these ideas.

Orange Blossom

From the stable that brought forth the Tangerine VDU system about a year ago now comes a new micro system called the Microtan. This is an excellent kit, also available ready built, that sells for a mere £69. It offers an excellent start in 6502 based systems. I have built one up in the last week, it worked first time, and I would seriously suggest that if you feel unsure about soldering on double-sided, plated-thru boards you buy the ready-built system. It is not a beginners' kit; I spent over an hour and a half soldering and I'm no novice, but what you get at the end is really worth all the trouble.

The monitor is one of the best 1K versions I've come across in quite a while and the concept is excellent. Basically at this stage you need a five volt power supply, the Microtan and a hex keypad to start on the machine code. However, if you want a full ASCII you can plug it in place of the hex pad - the monitor actually works out which type you are using. Many people will make comparisons with the Acorn. Both are low cost 6502-based kits, but the Microtan gives you a VDU, rock steady I'm glad to say, right from the start with optional graphics and lower case rather than a sub-calculator type LED display.

Expansion is by a way of second board called Tanex, cunning names these, which gives you an extra 7K RAM, 6K ROM, 8K Microsoft BASIC, cassette I/O and enough general purpose parallel and serial I/O to get most of you frothing at the mouth. And; believe it or not, both cards are on PCBs not much bigger than a Eurocard. Further expansion is by way of a 40K, yes that's forty, RAM board and a disk board which will offer up to four units. Not only is the cost extremely reasonable but the design hasn't been skimped. In the days of Britain-Knocking dare one even say that Microtan will probably knock the (expletive deleted) out of the lower end of the market and possibly make at least one other UK firm look to its laurels in haste? I will be presenting a complete Microfile on this gem at a later date so keep your ears on.

Microtan - an excellent introduction to 6502 based systems.

CM	05	4020 4022 4023 4024	100p 100p 20p 50p	4060 4066 4068 4069	120p 50p 20p 20p
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4007	20p	4028	85p	4072	20p
4009	40p	4029	85p	4081	20p
4011	20p	4040	110p	4093	50p
4012	20p	4041	85p	4510	80p
4013	35p	4042	80p	4511	90p
4015	80p	4043	95p	4518	90 p
4016	30p	4046	110p	4520	80p
4017	65p	4049	45p	4527	90p
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7408	12p	7490	25p	74164	55p
7410	10p	7492	30p	74165	55p
7413	22p	7493	25p	74174	55p
7414	39p	7496	45p	74177	50p
7420	12p	74121	25p	74190	50p
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BC548

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BD132 BD139

BD140

BFY50 BFY51 BFY52

MJ2955 MPSA06 MPSA56

TIP29C

TIP30C TIP31C

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ZTX107

ZTX108 ZTX300

ZTX500

2N3053 2N3054

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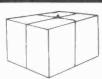
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his unsusual lamp dimmer project does away with the usual on/off/dim control knob and replaces it with a single touch-sensing pad or switch. The touch pad is coupled to a sophisticated IC which processes touch-duration information and then controls the brilliance of the lamp (via a track) in accordance with that

nformation.

If the pad is simply touched for a brief period (60 to 400 mS) the lamp merely changes state, ie, from OFF to ON, or vice versa, depending on its previous state. A longer touch (greater than 400 mS) causes the lamp brilliance to cycle slowly from dim to bright or vice versa for the duration of the touch, taking about seven seconds to span the full brilliance range: when the touch is removed the prevailing brilliance level is 'remembered' and maintained indefinitely. At switch-off (a brief touch) the chosen brightness level is stored: this brightness level is set again at switch-on

(another brief touch). In the case of dimming, control starts from the stored value.

Remote Control

The dimmer unit can be controlled locally either by the touch pad already mentioned or via a simple press-to-close switch. Additionally, however, the unit is provided with a pair of 'extension' pins which enable the unit to also be fully controlled by any number of remotely positioned switches or touch-pad modules. All control points work in the 'OR' mode.

The touch dimmer circuit uses the 'hum pick-up' principle of touch detection and is specifically designed to operate with 'modern' house wiring in which the lamp is connected to the Neutral side of the mains and the on/off switch (or dimmer) is connected to the Live side. The basic dimmer circuit can, however, also be used in 'old' house wiring systems, in which the lamp is

The ETI Touch
Dimmer is designed
to fit into a standard
plaster-depth lighting
switch box. The
triangular touch plate
from Maplin gives the
project a professional
finish.



connected to the Live side of the mains and the switch is connected to the Neutral, but in this case the unit' must be activated via push-button (rather than 'touch') contacts. In either case, the circuit can be used to control up to 300 watts of lamp power.

Construction & Use

Our prototype unit is designed to fit into a standard plaster-depth lighting switch box. Before starting construction, check the project's suitability to your existing wiring by making an accurate cardboard cut out of the PCB and checking that it will fit comfortably into an existing lighting switch box. If all is well you can proceed with the construction.

Construction calls for a certain amount of care. Note that the capacitors are miniature types (see Buylines). Components L1-C1 and R10 are RF interference suppression components. L1 consists of approximately 50 turns of 0.5 mm enamel copper wire, wound on the body of C1

When construction of the PCB is complete, connect the unit to the mains via a suitable lamp in accordance with the circuit diagram and the overlay and give the unit a functional check via the touch pad lead. Check that the unit dims and turns on and off as already described. Also check that it does not cause excessive interference on your radio set: if excessive interference is experienced, try reducing the value of R10 to 47R.

When you are satisfied that it is operating correctly you can fit the PCB and the touch pad (see Buylines) to a standard blanking plate (available from your local electrical shop) as shown in the photos. The plate is provided with a central 'knock-out' hole. Open the hole, push the touch pad through the plate hole and the central hole on the PCB and bolt the two units firmly together. Now connect the touch pad to the PCB touch pin via a solder tag and nut. Finally, check that the holes on either side of the PCB line up with the securing holes of the blanking plate.

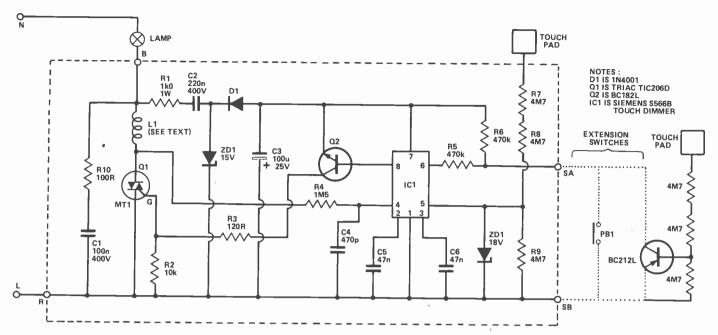


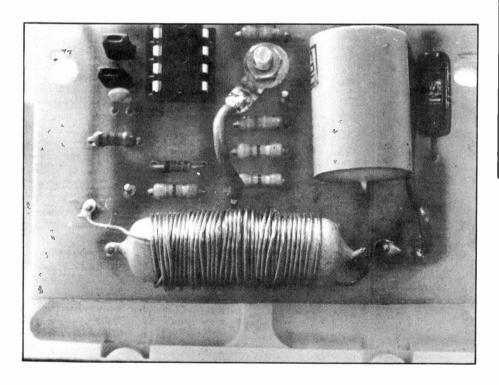
Fig.1. Circuit diagram of the dimmer.

When you finally fit the completed unit into its switch box take care to ensure that no short circuits occur. You can cover vulnerable components such as L1 with insulation tape if you wish. When fitting the unit, note that the box's earthing lug should, in most instances, be at the C1-C2 corner of the PCB.

If you decide to fit extension switches to the unit note that the connecting leads

carry live mains and normal safety precautions must be taken.

NOTE: The S566B IC used in this project is a special-purpose touch dimmer device manufactured by Siemens and must not be confused with the similarly numbered NE566N voltage controlled oscillator IC.



PARTS LIST. RESISTORS R1 R2 R3 R4 1k0 1W 10k 120R 1M5 R5,6 R7,8,9 470k R10 100R CAPACITORS 150n 400 V polyester 220n 400 V polyester (see C1 C2 Buylines) 100u 25 V electrolytic **C**3 470p ceramic C4 C5,6 47n (see Buylines) **SEMICONDUCTORS** IC1 S566B Touch Dimmer Q1 Q2 ZD1 ZD2 TIC 206D BC182L BZY88 15V BZY88 18V 1N4001 MISCELLANEOUS MK blanking plate, touch pad, 2-way terminal block (2A rated), Coil - 50 turns of 0.5 mm enamelled copper wire on C1. 10

L1 is wound on C1 - 50 turns of 0.5 mm enamelled copper wire. As an additional safeguard, a turn of insulating tape keeps it out of harms way in the box.

HOW IT WORKS

Most of the 'intelligent' action of the circuit is carried out in special-purpose P-MOS integrated circuit IC1. This IC receives instructions via a touch pad or touch switch. It processes the input touch-duration information and then does or does not send appropriate gate drive pulses to lamp-switching triac Q1 via pin 8 and current-booster transistor Q2.

If the IC decides that the lamp should be switched on it sends one 30 uS, 100 mA gate pulse to the triac in each mains half cycle (every 10 mS), at some phase-delayed time after the start (zero-crossing point) of each half cycle. The magnitude of the phase-delay determines the brilliance of the lamp: if the triac is triggered shortly after the start of each half cycle (short delay) the lamp burns brightly: if it is triggered near the end of each half cycle (long delay) the lamp burns dimly. The maximum and minmum phase delays are limited to 150° and 30° respectively, enabling the lamp power

to be varied from roughly 3% to 97% of maximum via the triac,

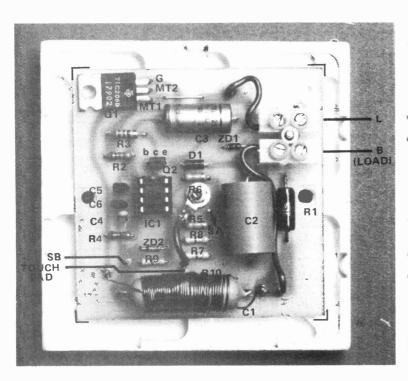
Although IC1 and Q2 generate relatively high peak drive power (1.2 watts), their MEAN power dissipation is very low (about 12 mW). This power is derived from the mains via R1-C1-ZD1-D1 and C3 and is delivered to IC1 and Q2 as a smooth 14 volts DC from 'reservoir' capacitor C3. This method of operation is only made possible by the fact that the triac is not gated on until at least 30° after the start of each half cycle, thereby enabling C3 to attain and maintain a virtually full 14 volt charge throughout each half cycle. The IC logic operations are synchronised to the zero-crossing points of the mains signal via the R4-C4 network.

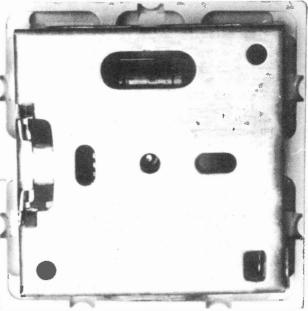
'Touch' information can be fed to either pin 5 or pin 6 of IC1. The pin 5 input is

intended for genuine 'touch contact' use and works on the high-impedance humpickup principle. The touch pad is effectively connected to the mains live terminal via high-value resistors R7 and R8, which limit the touch pad currents to safe and minimal levels. ZD2 limits the pin 5 'hum' signal amplitudes to safe values.

The pin 6 input is intended for use with push-button touch switches or with any number of parallel-connected 'extension' switches. The extension switches can either be normal push-button switches or 'touch switch modules', each comprising one transistor and three 4M7 resistors connected as shown.

The dimmer can be used with lamp loads up to 300 watts. L1 and C1 and the associated resistor are RFI-suppression components.





BUYLINES

Due to miniaturisation certain components have been selected for their physical size. These are C5, C6 and C4 and are Siemens type B37448, which are available from Electrovalue. C2 has also been carefully chosen. This capacitor is an ERO type MKC 1864 and can be obtained from Watford Electronics. The following companies stock the S566B touch dimmer—Electrovalue, Watford Electronics and TK Electronics. An anodised touch plate which can be purchased from Maplin Electronics gives an attractive appearance to the completed project.

All the other components should not prove difficult to obtain from major stockists advertising in this issue.

Fig. 2. (above left). This is how you fit a quart into a pint lighting box. Q1 is mounted flat on the board to save space. Note the orientation of C3.

The PCB fits neatly into its box (above). If you have any bits sticking out, you've done it wrong!

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RAVEN ON...

Jet-setter Dave Raven of Metac Electronics reports on his latest trip (purely business, of course) to Hong Kong, complete with holiday snaps

he first indication that Hong Kong is overcrowded came as the aircraft made its final approach to the runway. Washing billowed from the network of multi-storey buildings which appeared almost close enough to reach out and touch. Kai Tak Airport is situated on the side of Kowloon Peninsula with its runway projecting out towards Victoria Harbour. The giant Jumbo hurtles itself down between the skyscrapers and races out towards the end of the runway, which of course is surrounded by water. Reminding myself that the pilot must have done this many times before and that it would be extremely unlucky for this particular aeroplane to overshoot, I nestled down into my seat and thought about how many times the stewards had demonstrated putting on and inflating the life jackets. The sweet placid smile of the Singapore Air hostess hadn't cannged throughout the landing, which I had monitored continuously knowing that tell-tale signs of trouble would first appear there.

Street Life

If Hong Kong can survive the effect of its massive over population then the future growth of their electronics industry looks set to follow the same pattern as Japan. If the Government could somehow restrict any poor quality products leaving the country as happens in Japan by subjecting all exports to independent quality checks, then the effect of this would up-lift their whole product image.

Hong Kong is split into two main parts - Hong Kong Island, which is the original British Colony, and Kowloon, which is on the mainland tip of China. Kowloon is the controversial part of Hong Kong and also the adjoining New Territories which are on lease to Britain until 1999. The site of so much construction and land reclamation must infer that no one is particularly worried about the likely outcome of events when our lease does run out. A new multi million pound underground railway system has just been opened. Motorway sections, bridges, flyovers and a road tunnel under the harbour increase your confidence that the British expect to be here for some time yet. On occasions I found it necessary to remind myself that this was, in fact, still a British colony, since the life style was certainly different from any other I have seen. How much a part of Britain the Chinese felt, I just could not gauge. I did, however, notice when walking around the Chinese districts of Mong Kok that most of the corner street players, strange fortune tellers with caged birds and story tellers had a lot more common with say Pekin than with Manchester.

While U Wait

The other area in which we differ is our capacity for work. Never before have I been so amazed at the speed in which things can happen. All readers must have heard tales of the Hong Kong tailor-made suits. Well, I can confirm they are true. In just three days which included Saturday and Sunday my colleague and I had a suit made to measure and three shirts each. This included a fitting of course which all took place in our hotel rooms. This story will of

course inflame the wrath of clothing manufacturers in this country who will try to make me feel guilty by pointing out the rate at which companies that manufacture suits are going out of business. While feeling genuine sympathy I cannot help feeling that it takes a little more than sweated labour to be as efficient as the Hong Kong Chinese. Wage rates are generally regarded as good and working conditions are not dissimilar to those I have seen in many British factories. A visit to the East End of London will demonstrate this point, particularly the little clothes manufacturers off Middlesex Street (Petticoat Lane). My admiration for the tenacity of the Chinese in building up such a prosperous country in an area about the size of Leicester is tremendous. The contribution which has been made by our own Government deserves praise too when one considers that the whole country is administered by British Civil Servants.

Visiting the industrial area of Hong Kong is an experience in itself. This must be a unique environment of multi-storey blocks of factories containing more people than 1 think 1 have ever seen. Walking through the little street markets during the lunch hour (they do have one), I can only describe it as similar to trying to traverse the crowds at Wembley Stadium on Cup Final Day. As part of my brief was to discover the source of the Digital Watch it was with much trepidation that I entered the factory blocks. Travelling up in a lift with about three times as many people as I would think was safe, I hesitantly made my entrance. Where were the rows of children assembling my watches? No sign of malnutrition or overseers lashing the workers to produce more.

Swiss Watches - Chinese Style

I am afraid to report to the sceptics of Hong Kong products that I was only confronted by modern UK style offices with splendid clean modern production lines, manned by rows of pretty healthy looking girls who were carefully assembling the products. Rows of computerised automatic bonding machines were churning out watch modules and automatic computer testing was being carried out on a million pound computer system. The design engineers, quality assurance managers and factory managers were all highly competent people whose only crime against the workers of Britain is a high level of job satisfaction and a level of productivity that we can only hope to aspire to. One of the companies visited has a complete in-house design capability so forget the stories that all the products are ripped-off from American or British designs. This same firm is building a new factory to give them their own wafer fabrication plant which reduces their reliance on American chip manufacturers. Stainless Steel, mineral glass watches, water proofed to three hundred atmospheres are soon to be typical specifications coming out of Hong Kong. Some of these companies are now approved to Swiss Watch Industry standards and to prove it some well known names are being assembled here. Hand held games are to be very important products this year, probably as big as the early TV Game. Models to watch out for are the LCD varieties with little stick-figure football players that dart about on the display. These nay not be ready this year in the UK but this has to be the start of a flat screen, LCD hand held television.

Rural Smells

No visit to Hong Kong can be made complete without visiting the New Territories, and this rural part of Hong Kong must be very similar to Main Land China (only 22 miles from Hong Kong). We travelled to the China border on a train full of young Chinese youths off on a Sunday outing. The journey took about two hours due to delays caused by trains coming from the opposite direction loaded with ducks, cattle, pigs, sheep and also armed guards at the rear. In the station these trains were halted along side our own train and with the windows down the smell managed to ruffle our normal calm British decorum. The houses in the rural areas are still very small by our standards. I was amazed to see how every available patch of ground was beautifully cultivated and tangerines were being grown in pots for part of the New Year celebration. The China border is not too impressive, but then how could it be, with just open fields and a twisting road leading off into the distance. With binoculars you could just make out the guards at the border and I was amazed to see a few people wandering across carrying shopping bags. I later learned that they live on the border and are free to cross into Hong Kong but clearly prefer to go back to China. I must confess that I had an urgent desire while standing there, to walk off down the road and discover if there really are nearly one billion people living over those hills all capable of being as industrious as the 5.5 million on the side I was on.

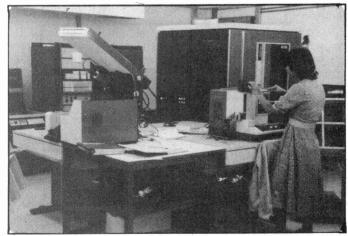
Arab Solar Energy

While in Britain we rapidly use our scant supplies of oil, energy conscious Arabs in the Middle East are investing millions of pounds in conserving their own. The future of solar energy looks very promising according to a report published by the political editor of Middle East Magazine. The arab world receives solar energy equivalent to an average of 275 watts per square meter. With a land area of over 11.5 million square kilometers and assuming that only one percent of this could be utilised for solar energy collection, a total of over 30 billion megawatts is potentially available. This could be converted to usable electricity at an efficiency of at least 10 per cent producing over 3 million MW or the equivalent of 3000 large power stations, generating 1000 MW each.

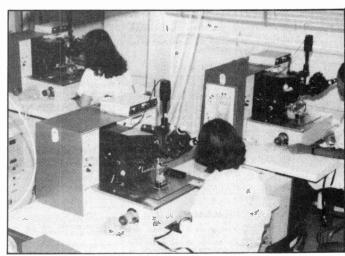
SOLERAS

Large scale solar projects are under way and include a 1.5 million dollar solar-powered heating complex for a massive air force school that is being built at Tabuk. It involves 4370 sq. m. of solar collectors and is being built by an American firm on subcontract. By far the biggest project undertaken to date is the SOLERAS programme with the USA. On the American side the Department of Energy has set up an agency, the Solar Energy Reasearch Institute (SERI), run by the Mid West Research Institute in Colorado.

Most effort so far has gone into building a 350 kW solar power station near Riyadh using photovoltaic cells to supply electricity to

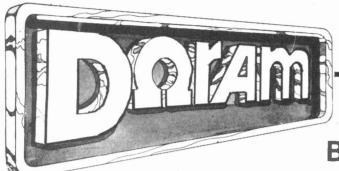


This computer is used at Elcap Electronics in Hong Kong for automatic testing of watch chips.



Automatic wire bonding of watch modules at Elcap.

two villages. Plans are also under way to build a desalinating plant and contracts will shortly be awarded for this work. By introducing greenhouses into agriculture, Jordan has increased its production of cucumbers and tomatoes fivefold, especially in the winter. Perhaps the most spectacular innovation has been the construction of a solar powered emergency roadside telephone system. most major roads now have such phones and the director of the Jordan Telecommunication Corps is investigating the possibility of introducing solar powered television sets to remote areas (he obviously hasn't heard about Sinclair's Microvision).



BACK IN BUSINESS

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PUSH SWITCHES (15×6mm), red tep. push io make 15p each, pash oo broak version black vinyl 17p eack. SLIDE SWITCHES all GPOT $15\times 6\times 12mm$ $13p. 16\times f1\times 6mm$ $13p. 22\times f3\times 6mm$ $13p. 22\times f3\times 6$ contro off 14p. Multipolo alidor double actus [12 tags] $29\times 9\times 11mm$ 25p.

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Whilst the stock exchanges of reality are curious and wonderful establishments this game is based on proper theories and a full and detailed explanation of the processes needed is given. So, if you don't own a T159 do not despair you will be able to use the information to implement the game on virtually any programmable system.

So if you want to be among the market leaders next month invest your sixty pence in our May issue, it could be the best investment you'll ever make.

Does your car or motorcycle seem to want more DRIVEN TO DESPAIR? money than you bargained for? The author of our Home Finance program presents a second offering which will cater for your automotive expenses.

The program runs on the family PET but is easily adaptable to any BASIC using system with the PETs facilities. Access is available to a number of accounts for details of repair and servicing costs and reminders are given about the life expectancy of wearable items such as tyres.

If you depend on your car and can't account for the money you spend, load up and discover where its all going to. Rumour has it that Panther De Ville owners with that optional PET may be buying all copies so get to the newsagents early.

TRITON REVISITED ETIs own computer system is over a year old now, and changes have been made since its conception that make it rather more than a single board computer.

> In our continuing series of owners reports on popular machines John Hiscott takes his system through the stages of development and lays his observations open to the public eye.

No, that's not the art of making connections, but a TERMINOLOGY glossary of the "hundred most used terms" in home and hobby computing. Many of our enquiries start out with, 'I can't tell the difference between RAM and ROM' so we decided to reveal all.

As an aid to simulating conversation this pull out extra should not be missed, you might even learn the elusive art of confusion!

TOMORROWS OFFICE?

Take a step into the future at the Design Centre. Ian Graham reports on time travel in the Haymarket.

f you find yourself within visiting distance of London's Haymarket between now and March 8th, it's worth popping into the Design Centre. They've collected together a handful of exhibits to show what the office of tommorrow might be like and they've called it 'Tomorrow's Office Today'.

The typewriter has been the office workhorse since granny was knee-high to an abacus, but two boxes of tricks on display may well see it off the the scrap heap - the Supertyper word processor and the Microwriter.

Box No. 1

The Supertyper FD85 word processor takes much of the repetition out of typing. When I visited the show, a demonstration of the FD85 had attracted a small crowd of exhibitionists (or do I mean exhibition goers?). Corrections or major alterations to typewritten text usually means retyping. Not so with the word processor. The letter that needs an alteration can be displayed on a screen above the keyboard. Then, at a touch of a button or two, words or letters can be added or deleted, columns can be shifted, lines ruled, paragraphs moved and so on ad miraculum. When the boss is happy with his words of wisdom, the processor can print out as many copies of them as he wants in his favourite type face.

If you have to send out a few dozen standard letters, the processor can print them out, adding a different name and address to each.

Box No. 2

If you're working away from the office and you want to make a few notes you could reach for the nearest scrap of paper or use one of those pocket cassette recorders. The scrap of paper stands a good chance of getting lost and the cassette recording has to be transcribed on your return to the office. How about giving a Microwriter a try?

Five Finger Excercise

The Microwriter is about the size of a large pocket calculator, but it only has six keys (five plus control). These can be used in various combinations to enter letters (upper and lower case), numerals, punctuation and all the other normal keyboard symbols. The text is displayed as you write it on a twelve character LED display, moving from right to left. There is also an optional TV display for sixteen line read-out and editing.

The control functions let the operator read or jump forwards or backwards and allow instant editing - the deletion or insertion of letters, words or even complete paragraphs.

Microwriter's memory can hold 8,000 characters (about 1500 words) in RAM and further storage is possible by means of microcassette.

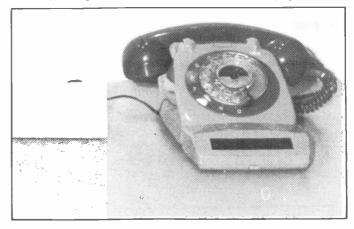
The contents of the memory can be printed out when you finally get round to calling in at the office or it can be transferred to micro-cassette for playback later.

When the Microwriter is plugged into its automatic, high speed printer, your notes are transferred on to paper at up to ten times the speed of your best secretary. Each printer can handle between ten and fifteen Microwriters.

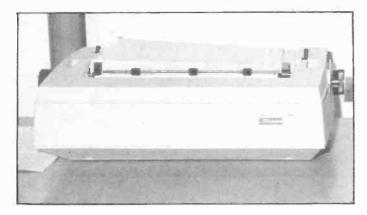
Now meet SUE, designed by Tom Stout and on show for the first time. Sue is an automatic draughtsman. The hardware includes a display screen, a plotter and a disc memory system. The drawing and the typewritten additions from the keyboard are shown on the display. When the drawing is satisfactory SUE can transfer the display on to paper. If your paper copy of the drawing is lost or damaged or needs further alterations, don't worry - the original is still stored on the disc memory.

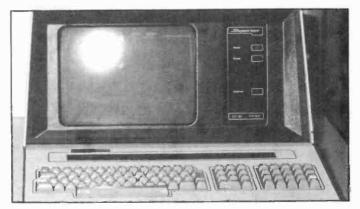
When you hear that spine-chilling word - time - and have to toddle back to the office, the Logatel phone aid shows you who's been trying to call you.





80 ETI APRIL 1980





The several-secretary-power Supertyper word processor system takes the repetition out of office paperwork.

Phone Bugs

Minster Automation would love to come and bug your phones. It's worthwhile, though. Their Tiger Cub telephone management and accounting system records the length, cost and distance of outgoing calls and the number of incoming calls that go unanswered. What good is that? Well, Tiger Cub can identify under-used extensions which you could do without. All the recorded information can be printed out if necessary.

Call Again

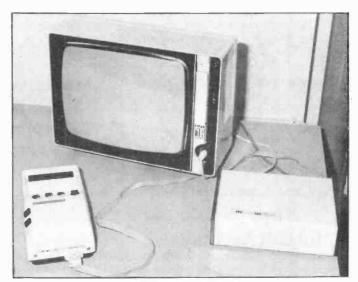
When you ring an extension on your internal phone system for the sixth time and no-one answers, the atmosphere can start to go a bit blue. Why waste all that time and effort dialling and hanging on the end of a deserted extension? Instead of regularly ringing back, why not just ring once and let the phone do the rest? If your system is fitted with the Logatel aid, you can ring once, wait for the tone that begins when the phone is left unanswered and then dial your own number. When the phantom phoner finally returns to his office, Logatel can display the numbers he has to ring back - yours among them. Logatel is manufactured by Feedback Ltd of Crowborough.

First Class Chips

The silicon chip has even got into the post room. Although your accounts department and your company records may be computerised à la space age technology, is your post room staffed by little old men in frock coats using a steam franking machine under one of Edison's original light bulbs? Mailtronic's postal weighing device is aimed at you. You put your letter or package on top and touch the finger sensitive keys for postal zone, class of post, registered post, etc and the chip in Mailtronic uses all the information to compute the correct postage. When there's an increase in postage, all is not lost. You just change the chip.

Push-button postal charges from Mailtronic.

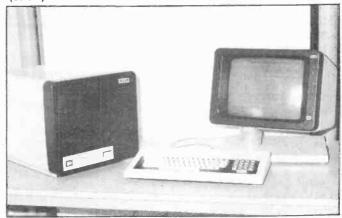




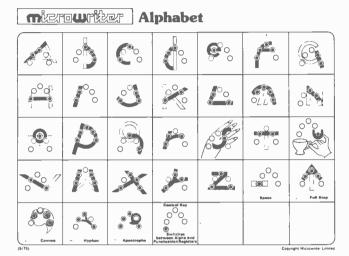
16 lines at a time from Microwriter (above) can be displayed on TV.



Put a Tiger Cub on your phones (above) or Euro C your accounts (below).



Once you've mastered Microwriter's keyboard (right) you can happily tap in up to about 1500 words, without a tape recorder or reams of paper. Like everything else, mastering the keyboard alphabet (shown below) is just a matter of practice.





Instant Accounts

EuroC is a British-made desk-top microcomputer system designed to handle a company's entire accountancy procedures at low cost. It is capable of being operated by staff without any computing or accounting knowledge. Produced by Eurocalc Ltd of London, with hardware form Plessey, the system can store up to 12,000 transactions per month for 1,000 clients, so it is particularly suitable for small to medium sized companies. Each daily purchase or sale is entered via the keyboard on one of eight standard 'input' forms displayed on the screen. As each form is completed, the computer automatically updates the firm's records. Every month a set of management accounts can be printed out. Necessary reports can be printed out at any stage.

Paper Mill

If you have several thousand sheets of paper and you need to assemble sets of notes from them, it could take your Girl Friday

hours to get all the sheets in the right order. The Watkiss all-purpose collator could do it for you and much quicker (it doesn't have to stop to powder its nose). It can handle a wide variety of material at the rate of 45,000 sheets per hour.

The Film Business

When you keep some of your records on microfiche, reading them can be a bit of a strain on the eyes. Take the load off your lenses with the Alpha microfiche reader from CAPS Microfilm of London. It will magnify the sheet of film to an easily readable size. The reader has a special grid index plate with a moveable pointer to select a particular page in seconds.

Seeing Is Believing

Many of these exhibits are demonstrated from time to time. You can try some of them out yourself. If you want to know when your favourite box of tricks is going to be demonstrated, give the Design Centre supervisor a ring on 01-839 8000 ext 309.

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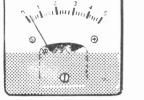
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ME7 T27 T27 O - 50 MA ME8 T28 O - 100 MA ME9 T29 O - 500 MA ME10 T30 O - 1 AMP ME10A T31 O - 2 AMP ME10B T32 O - 25 Volts ME11 T33 O - 50v AC ME12 T34 O - 300v AC STAN ME14 T36 STAN ME15 T40 ME15 T40 ME15 T40 ME16 T41 T42 S00 - 0 - 500 UA ME17 T42 S00 - 0 - 500 UA ME17 T43 O - 30v DC	£3.75 each + VAT 15% P&P 35p 10 Plus 10% discount

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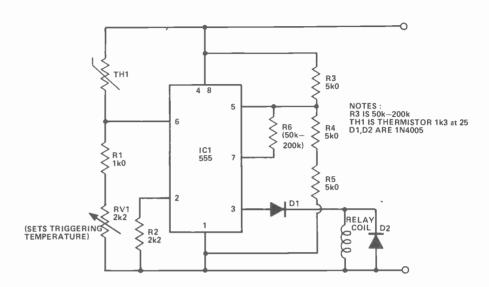
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TECH TIPS

Boat Heater Thermostat B. Kongstad

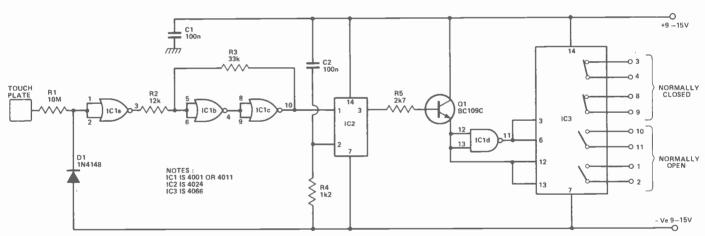
When thethermistor R1senses it is time to start the heater it is essential that the relay pulls distinctly even if temperature falls slowly. The heater must be on till temperature has risen by at least 2 C, otherwise it has to start and stop too often. The desired Schmitt action is achieved in the following way. When temperature falls the resistance of the thermistor increases and the comparator at pin 6 triggers the flip-flop. Then pin 3 goes high and pulls the relay. At the same time pin 7 goes low. Resistor R6 shunts the lower part of the 5-5-5 k voltage divider and this helps the comparator to give a definite trigger for the flip-flop.

If the thermistor is replaced by an LDR the trigger action will take place when it is



sufficiently dark. By this means a riding light can be lit at dusk when at anchor and the light turns off at dawn. But don't use

50 Hz incandescent or fluorescent light when setting the sensitivity. Your eye will not sense the flickering but the LDR does.



One Contact Touch Switch G.N. Durant

The switch is operated by stray mains hum, connected to the touch plate when briefly touched. The hum is coupled to the input of IC1a (used as an inverter) via R1 (a low pass filter). The output of IC1a is not sufficient to operate the final stage, so it goes through a

Schmitt trigger (IC1b,c). Once the trigger output starts to change, R3 provides the trigger for a rapid change.

IC2 is a seven stage ripple counter. Q1 is driven from the output of the seventh stage via R5 (current limiter resistor). C2 and R4 reset IC2 at switch-on so the outputs are all low and the switching transistor is off. When the touch-plate is touched, IC2 will receive a 50 Hz signal. At pin 3, the logic state changes every 64 pulses, switch-

ing Q1 on and off. The plate is touched until the desired state is obtained and then

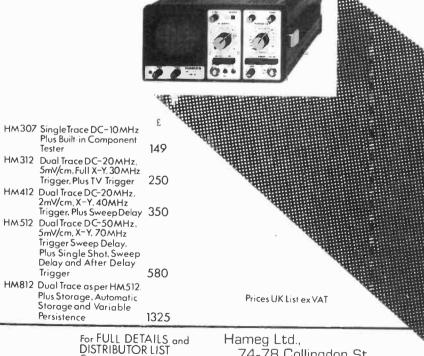
Q1 sends a pulse through to IC3, a solid state CMOS switch. This can be fed via an inverter if desired. The switch must not be used at more than its supply voltage - up to 15 V. The 'off' switch resistance is about 10^{13} ohms and the 'on' resistance is about 80 ohms at 15 V V_{DD} (at 9 V V_{DD} it is 120 ohms99

Tech-Tips is an ideas forum and is not aimed at the beginner. We regret we cannot answer queries on these items.

ETI is prepared to consider circuits or ideas submitted by readers for this page. All items used will be paid for. Drawings should be as clear as possible and the text should preferably be typed. Circuits must not be subject to copyright. Items for consideration should be sent to ETI TECH-TIPS, Electronics Today International, 145 Charing Cross Road, London WC2H 0EE.

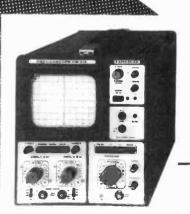
	9 9		•						U U					U			
TRANSIS	15p	8F179 8F183 8F200 8F336	25p 25p 29p 33p	OPTO Leds		T	RIACS	with loternal tringer disc.	74LS124 74LS132 74LS139	115p 89p 79p		504	BRIDGE	S 200	w	400¥	6004
AC187K AC188K ACY17 AD149 AF127 ASZ17 AU113	30p 30p 90p 55p 35p 120p 150p	BFX30 BFX86 BFX88 BFY50 BFY51 BFY64 BFY90	32p 26p 22p 13p 13p 28p 56p	.125 Orange 1 .125 Yellow 1	8A 600V 10A 400		54j 60g 66g 66g 72g 72g	1 16p 15p 15p 19p 19p 15p 15p	74LS151 74LS155 74LS156 74LS157 74LS165 74LS168 74LS174	89p 91p 89p 69p 69p 139p	2A 4A 6A	45p 52p 60p	52p 60p 68p	60 ₁ 68 ₁ 75 ₁	p	75p 82p 90p	100p 105p 112p
BA154 BA156 BC107 BC108 BC108A BC108C	9p 9p 7p 7p 7p 7p	B\$X19 B\$Y95A BU204 BU206 OC29	80p 16p 149p 150p 89p	Displays	15A 6001 15A 6001	1	84p 108p 126p	120p	7486 7491 7492 7493 7494	25p 63p 35p 28p 63p	DIL	SOCKETS	CMOS		4070 4071		19p 19p
BC136 BC140 BC141 BC142 BC143	15p 28p 30p 25p 28p	0C43 2N696 2N930 2N1132 2N1304 2N1613	50p 15p 20p 19p 40p 12p	704 110 727 160 741 166 747 166 750 166	p	TTL	7480	38p 25p 23p 2*p 44p	7495 74100 74107 74121 74122 74123	63p 110p 30p 25p 36p	8 pia 14 pia 16 pin 20 pia 24 pis	10p 12p 13p 25p 30p	4000 4001 4002 4006 4007	14p 14p 14p 79p 14p	4072 4073 4075 4076 4077 4081		19p 19p 19p 75p 35p 19p
BC147 BC147B BC149 BC149C BC159 BC150	6p 6p 7p 7p 9p 35p	201711 202217 202219A 202221 202221	15p 20p 20p 18p 15p	REGULATORS	7402 7403 7404 7405 7406	9 10 14 30	7482 74LS00 74LS01 74LS02 74LS02 74LS03	6mp 1 p 1 p 12p 12p	74145 74154 74157 74161 74175	44p 72p 80p 60p 85p 63p		MORIES	4006 4009 4010 4011 4012 4014	79p 36p 36p 19p 16p 75p	4082 4482 4484 4412 4445		19p 36p 110p 86p 174p
BC167A BC178 BC179 BC182 BC182L	10p 12p 12p 8p 9p	2N2369 2N2894A 2N2904 2N904A 2N2905 2N2906	14p 20p 15p 15p 15p 15p	7805 57 7812 57 7815 57 7818 57 7824 57 LM34075 74	7408 7409 7410 7410	30 17 17 12 17; 25	74LS10 74LS11 74LS20 74LS30	12p 15p 2tsp 18p 18p 24p	74180 74181 74191 74192 74193 74194	84p 151p 80p 80p 80p 80u	21L02 2114 4027 4116	109p 400p 275p 750p	4015 4016 4017 4018 4019	79p 42p 79p 79p 45p	4446 4502 4511 4512 4514		148p 99p 132p 89p 2290
BC183 BC183L BC184L BC186 BC212	9p 9p 9p 20p 9p	2N2926Y 2N29260 2N2926R 2N3442 2N3702	10p 10p 10p 102p 8p	LM340T8 74 LM340T15 74 LM340T16 74 7905 140 7912 140	7414 7416 7417 7420 7427	45 25 25 14 28	74LS51 74LS55 74LS55 74LS74 74LS75	2 mp 2 mp 2 mp 3 mp 4 mp	74LS175 74LS190 74LS192 74LS194 74LS195	99p 110p 115p 115p	2708 2716	PROMS 750p 3200p	4020 4021 4022 4023 4024	89p 89p 79p 19p 49p	4515 4516 4520 4522 4526 4531		229p 109p 99p 129p 125p 125p
8C212L 8C2138 8C327 8C328 8C337 8C338	9p 9p 13p 13p 16p 11p	2N3704 2N3705 2N3708 2N3709K 2N3866	8p 8p 8p 8p 35p	7915 140 7918 140 7924 140 LM32075 149 LM32078 149	7432 7438 7442 7447	14 22 26 48 50	74LS85 74LS90 74LS93 74LS93	35p 95p 35p 75p 45a	74LS196 74LS197 74LS257 74LS260 74LS273	95p 125p 99p 99p 199p	Mk 3880	PU'S	4025 4026 4027 4028 4029 4030	17p 159p 39p 79p 89p 49p	4555 4556 4581 4582 4584		92p 69p 269p 115p 59p
BC440 BC547 BC548 BC550 BC558	32p 9p 9p 14p	293906 294058 294427 DIODES	10p 12p 60p	MEMOF	7451	EPR		CPL	74L\$367 74L\$378	59p 159p	Mk 3881 Mk 3882 PT(750p 750p	4034 4035 4042 4043 4044	169p 99p 69p 86p 86p	4585		99p
BCY33 BCY34 BCY39 BCY58 BCY70	99p 99p 299p 16p 12p	AA119 W4001 W4002 W4003 W4005	10p 4p 4p 5p 5p	OAKFIELD CO	IN PRNER	TERFACE SYCAM	COMP ORE RO	ONENTS DAD, AME	LIMIT RSHA	ED, M, BUCK	s HP6	6SU	4046 4049 4050 4051 4052	119p 45p 45p 69p 69p		35p P8	LP
8CY71 8CY72	12p 12p	M4148 IS44	5p 3p	Wri	e,telep	PHUNE:(hone or c	JZ4Ų3 2 ali. Acce	2307. TE ess or Baro	LEX:8 :laycar	37788 d accepted			4063 4066 4069	69p 55p 17p	a	dditior	nal

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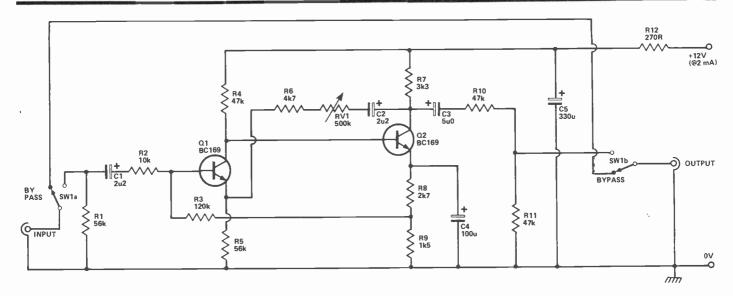
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Transcendent 2000 Preamp

R.N. Johnson

If this preamp is connected between the External VCF Audio Input socket and some musical instrument such as a guitar, then the output from the synthesiser will consist of the guitar sound modified by the synthe-

siser's VCF, mixed with the normal output of the synthesiser. The preamp is necessary because the VCF requires about 1 V to work, but most guitars produce only 10-20 mV. The voltage gain needed is about 36 dB. Most other musical instruments should also work as long as they have a pick-up which produces about 10 mV or more (even a microphone works and produces some pretty weird noises). The level controls of the synthesiser and the preamp can

be used to determine the mixture of synth/guitar in the output.

The circuit itself is suitable for low or high impedance microphones/guitars and RV1 varies the gain from about 10-36 dB. The power supply of the synthesiser can be used and the preamp will easily fit inside the cabinet of the synthesiser (near socket SK6 but away from the mains leads). The switch is provided to bypass the preamp if necessary.

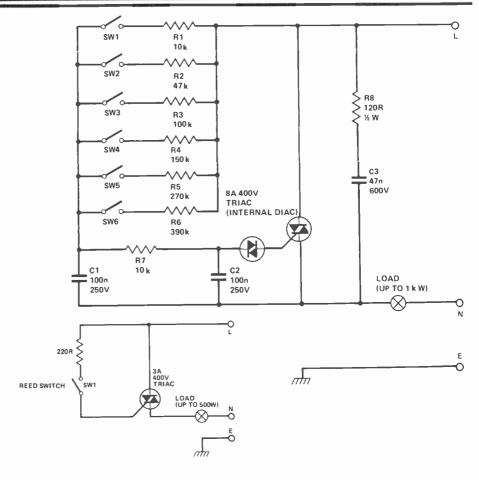
Magnetic Light Dimmer T. Hopkins

A partial solution to the problem of leaving lighting on unnecessarily is to have a resettable timer in place of a switch. However, The choice of delay is difficult, particularly when the room may be used continuously.

Ideally, it should be impossible to leave the room without turning out the light. One solution, shown in Fig. 1 is to build the circuit into a wall box and carry a small magnet on a keyring. When the magnet is placed over the reed switch, the lights are turned on and, if the circuit is mounted on a steel front panel, the magnet will stay in place for as ling as is required.

The magnetic dimmer shown in Fig. 2 allows a choice of six different light levels depending on which reed switch is operated. The resistor values shown were chosen to suit the available triac. Other triacs may require changes to some of these values.

The reed switches used measured approximately 1.125" and were mounted on a piece of tinplate with epoxy resin (Fig. 3). The front was then covered with a thin layer of plastic. A magnet of y_2 " diameter was used to operate the dimmer.



STEREO THNER AMPLIFIER CHASSIS

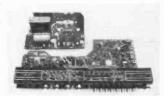
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Stereo Beacon Indicator LED or bulb. Size Tuner $-2\frac{3}{4}$ " $\times 15$ " $\times 7\frac{1}{2}$ " approx. Power amp. 2" $\times 7\frac{1}{2}$ " $\times 4\frac{1}{2}$ " approx.

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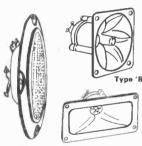
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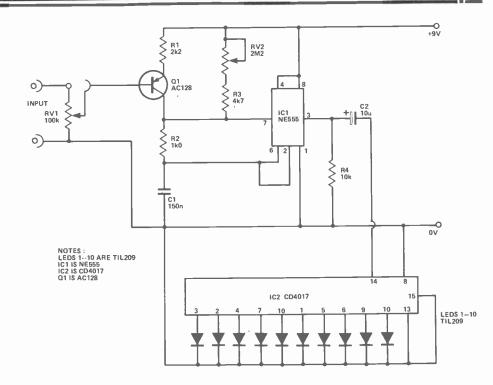
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Audio Display C.S. Histed

his circuit is a novel LED display, which when plugged into your hi-fi will send a dot of light zooming around a ring of LEDs at different speeds, depending on the music. The input signal from your hi-fi is fed into a voltage controlled oscillator (IC1), which then sends its variable length pulses to the clock input of a 4017.

This causes each LED in turn to be briefly lit and, because the clock input changes, the time taken for the dot of light to move along the LEDs varies in time with the music. The best visual output is achieved if the LEDs are arranged in a circle of about 1½" to 2" in diameter.

The input voltage can be adjusted by the 100k preset and the normal speed of the leds can be adjusted as desired using the 2M2 preset. The 4017 is able to drive the LEDs directly and no current limiting resistors are needed.



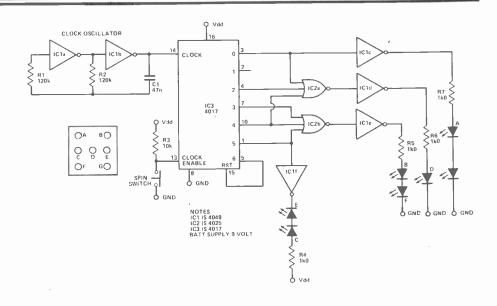
LOC	CODE	KEY	15 16	61 1 32 3	SBR 1 STO 3	32 33	71 00	RST 0
00	34 6	SUM 6	17	33 1	RCL 1	34	81	R/S
01	. 33 6	RCL 6	18	22	x t	35	71	RST
02	35	Yx	19	33 2	RCL 2	36	86 0	2nd LBL 0
03	30	2nd	20	76	2nd x t	37	55	X
04	85	=	21	22	x t	38	01	I
05	-35	INV Yx	22	33 3	RCL 3	39	00	0
06	05	5	23	76	2nd x t	40	85	=
07	85	=	24	51.5	GTO 5	41	32 5	STO 5
08	-49	INV 2nd INT	25	333 7	RCL 7	42	49	2nd INT
09	36	2nd PAUSE	26	39 4	2nd PRD 4	43	-61	INV SBR
10	34 6	SUM 6	27	516	GTO 6	44	86 1	2nd LBL 1
11	61 0	SBR 0	28	86 5	2nd LBL 5	45	35 5	RCL 5
12	32 1	STO 1	29	39 4	2nd PRD 4	46	-49	INV 2nd INT
13	61 1	SBR 1	30	86 6	2nd LBL 6	47	61 0	SBR 0
14	32 2	STO 2	31	56	2nd DSZ	48	-61	INV SBR

Electronic Travelling Dice

M.G. Argent

The heart of the unit is the 4017 divide by n counter, IC3. The outputs in turn give a logic 1 level (+9 V) with each clock pulse. To divide by six as required by a dice, the seventh count (output six, confusingly) is connected to the reset (RST) input. This resets all outputs to logic 0 and the count starts all over again ad infinitum.

So long as the clock enable input is connected via the 10k resistor to $V_{\rm DD}$, the count carries on as normal. If it is connected to 0 V the counter stops and remains in the state it was in at that time. This is achieved by a normally-open push switch which acts as the SPIN switch. When the switch is operated it stops the counter.



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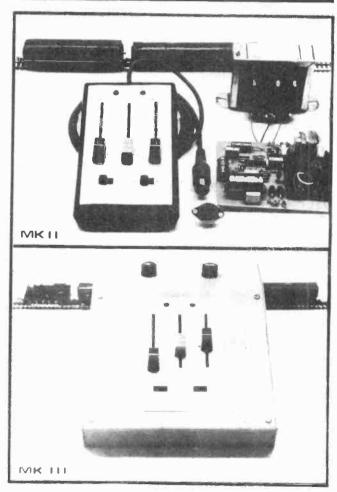
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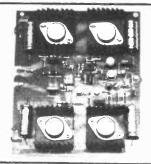
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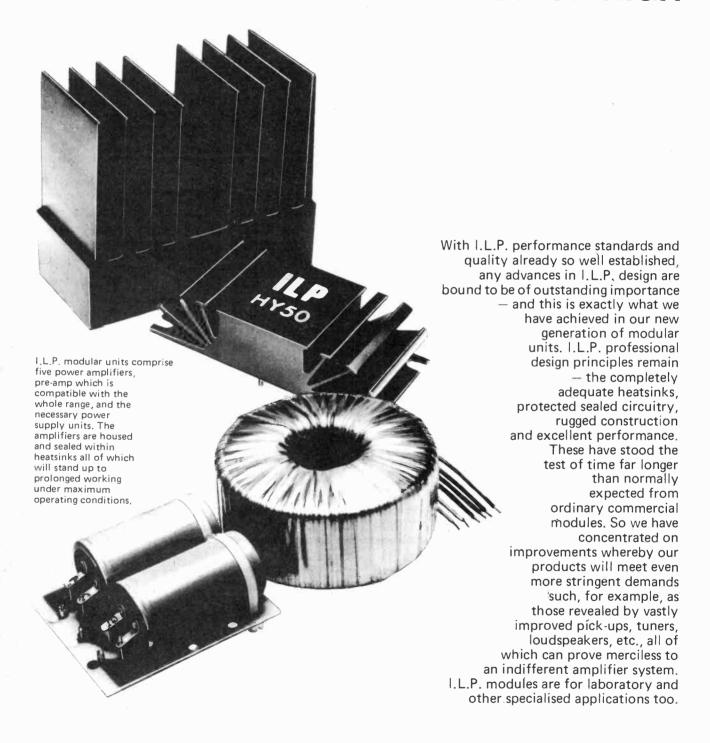
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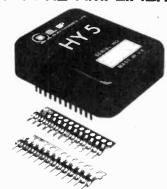
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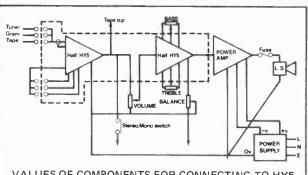
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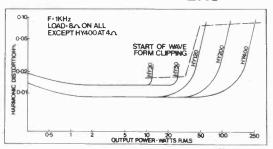
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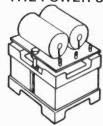
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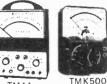
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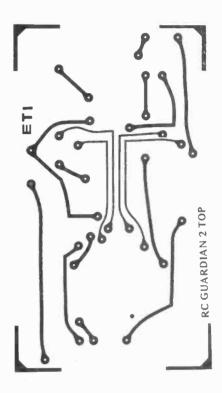
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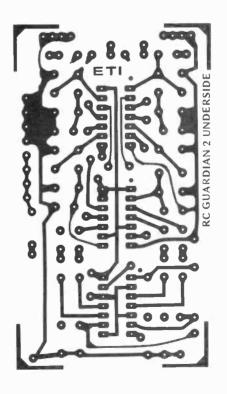
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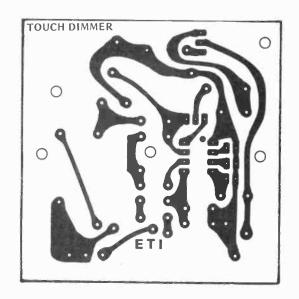
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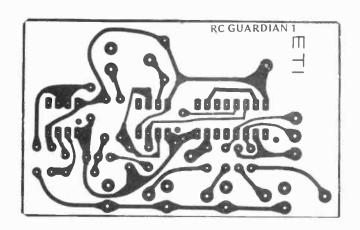
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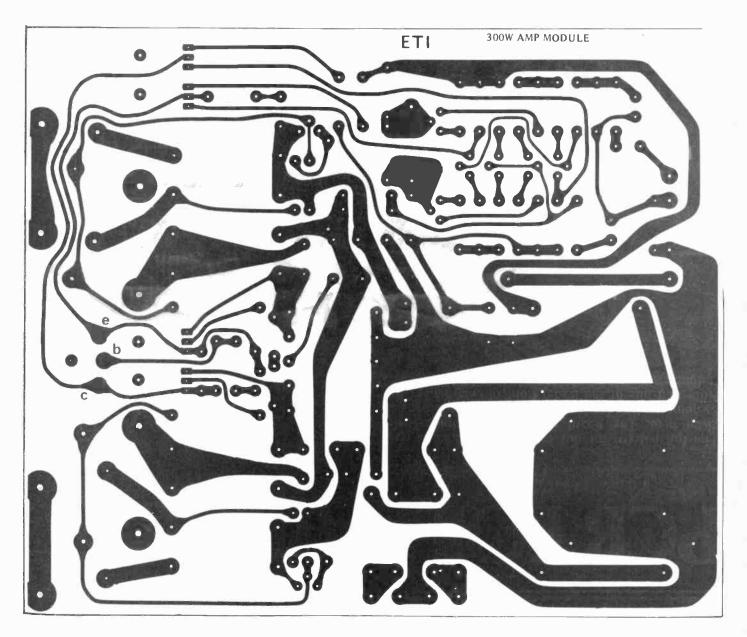












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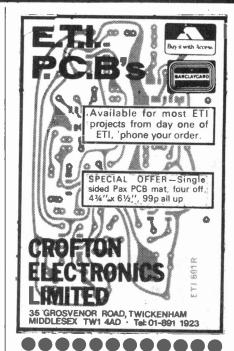
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ADVERT INDEX

Akhter Instruments	8
Altek Instruments	27
Ambit International	64
Audio Electronics	98
Baringlock Ltd	92
Bavdis	53
Bi-Pak Semiconductors 56 &	57
B.K. Electronics	90
Calculator Sales & Service	99
	49
Catronics	27
Chiltmead	
Chromasonics	
	53
Codespeed	99
Commodore	28
Comp Comp Comp 106 & 1	07
Crofton Electronics	90
Crimson Elektrik	99
C.S.C	47
Delta Tech & Co Facing	55
Digisound	90
Display Electronics	12
Doram Electronics	78
E.D.A	53
Electrovalue	74
GMT Electronics 94 & 9	95
Greenbank	42
Greenweid	26
Hameg Ltd	88
Happy Memories	74
Henrys Radio	92
I.L.P. Electronics 96 & 9	97

Interface Components 88
Kode Services
Kode Services
L. & B. Electronics 92
Maplin 108
Menorcrest 86
Metac 4 & 5
Metac
Midland Trading
Mighty Micro 7
Monolith
Mountaindene
E.R. Nicholls
NIC Models
Polar Enterprises
Powertran Computers 102
Powertran Electronics 2 & 8
Progressive Radio 78
J. W. Rimmer
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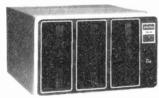
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