

## CHROMATHEQUE 5000

 5 CHANNEL LIGHTING EFFECTS SYSTEMAll kits also avalable as separate packs !e g All kits also avalable as separate packs ie 9 Prices in FREE CATALDGUE


## COMPLETE KIT

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This versatile system featured as a constructional article in ELECTRONICS TODAY INTERNATIONAL has 5 frequency channels with individual level controls on each channel Control of the lights is comprehensive to say the least You can run the untr as a straightforward sound-to-light or hiave it strobe all the lights at a speed dependent upon music level or front panel control or use the internal digital circuitry which produces some superb randoni and sequencing effects Each channel handles up to 500 W and as the kit is a single bodrd design wiring is minimal and consituction very straightforward
Kit includes fully finished metalwork fibreglass PCB contols wire etc - Complete right down to the last nut and bolt

MPA 200100 WATT (rms into $8 \Omega$ ) MIXER / AMPLIFIER


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Featured as a construct onal article in ETi the MPA 200 is an exceptionally low priced - but professionally finished - general purpose rugged high power amplifier 'it features adaptabie mput mixer which accepts a wider range of souices such as disc, microphone gutiar eir There are wide range tone controls and a master volume control Mechanically he MPA 200 simplicity itself with minimal wiring needed making construction very straightorward

The kit includes fully finished metalwork fibre glass PCBs controls wire etc - complete down to the last nut and bolt
Parts to buld power amp module (mc. PCB Custom designed toroidal transformer with Parts for power supply only res caps $s / c$ etc) $\mathbf{£ 1 0 . 6 0}+$ VAT. mountıng clamp $\mathbf{£ 1 0 . 5 0}+$ VAT. (caps, rects., fuses. F. holders) $£ \mathbf{3 . 4 0}+V A T$

## TRANSCENDENT 2000 SINGLE BOARD SYNTHESIZER

LIVE PERFORMANCE SYNTHESIZER DESIGNED BY CONSULTANT TIM ORR (FORMERLY SYNTHESIZER DESIGNER FOR EMS LIMITED) AND FEATURED AS A CONSTRUCTIONAL ARTICLE IN ELECTRONICS TODAY INTERNATIONAL.
The TRANSCENDENT 2000 is a 3 octave instrument transposable 2 octaves up or down giving on effective 7 octave range There is portamento pitch bending a VCO with shape and pith modulation, a VCF with both low and high pass outputs and a separate dynamic sweep control a noise generator and an ADSR envelope shaper There is also a slow oscillator a new pitch detector $A D S R$ repeat, sample and hold and special circuitry with precision components to ensure tuning stability amongst its many feature
The knt int ludes tully finished metal work fully assembled sillid teak cabinet fillier
sweep pedal protessionial quality components fall resistors either $2 \%$ metal oxide or \%ep netal trmotessiond ald quality components iall resistors enther $2 \%$, metal oxide or more parts hetore pluqging mand making grear music' Vou need bux alibsolutily ro
 mode with connestor plugs and contruc hion is so simple it an be bult easily in a ted


COMPLETE KIT ONLY
$£ 172.00$ + VAT!

Comprehensive handbook suppled with all complete kitst This fully describes construction and tells you how to set up you synthesizer with nothing more elaborate than a mulu meter and a par of ears!


ORDERING INFORMATION AND MORE KITS ON PAGE 8


Plant pampers p. 67


## FEATURES

NEWS DIGEST<br>AUDIO MAGNETIC AMPLIFIERS PARIS IN SPRINGTIME 40 CMOS CIRCUITS AUDIOPHILE

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## TELETEXT <br> POLYPHONIC KEYBOARD MOTOR SPEED CONTROLLER SOIL MOISTURE INDICATOR <br> TUNER AMP 2 <br> BATTERY INDICATOR

20 A quick newsflash on your telly
36 Multi-note organs to you
47 Gear down your movements.
67 Wet or dry ETI gives you it straight
79 The final part of System 8000.
92 State of charge flashed for your convenience.

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T20 + 20 20W STEREO AMPLIFIER £ 33.10 + VAT
This kit, based upon a design published in Practical Wireless. uses a single printed circuit board and offers at very low cost. ease of construction and all the normal facilities found on

## POWERTRAN SFMT TUNER $£ 35.90$ + VAT

This is a simple low cost design which can be constructed easily without special alignment equipment but which still gives a first-class output suitable for feeding any of our very popular amplifiers or any other high quality audio equipment. A phase-locked-loop is used for stereo selection (adjustable by controls on the front panel). This unit matches well with the T20 +20 and $\mathrm{T} 30+30$ amplifiers

## WWII TUNER £47.70 + VAT

This cost reduced model of our highly successful Wireless World FM Tuner kit was designed to complement the T20 +20 and T30 +30 amplifiers and the cabinet size, front panel format and electrical characteristics make this tuner compatible with either. Facilities included are pre-aligned front-end module, switchable afc, adjustable switchable muting. LED funing indication and both continuous and push-button channel selection (adjustabie the front panel)

FOR ELECTRONIC KITS OF DISTINCTION $200+200$ watt AMPIIIIER

As featured in Electronics Today International 400W rms continuous - 800W peak! $0.03 \%$ THD at FULL power!

## PLUS all the following features too!

* Each channel totally independent with its own stabilised power supply driven by custom designed TOROIDAL ransformers!
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* Professional quality components, sturdy $19^{\prime \prime}$ rack mounting chassis complete with sleeve and feet for free gtanding work too.
- Easy to build - plenty of working space with ready access to all components, minimal wiring extensive instruction suitable for both experience constructors and newcomers to electronics.
* Value for money - quality and performance comparable with ready-built amplifiers costing over E6001


## DE LUXE EASY TO BUILD LINSLEY HOOD 75W STEREO AMPLIFIER £99.30 + VAT

This easy to build version of our world-wide acclaimed 75 W amplifier kit based upon circuit boards interconnected with gold plated contacts resulting in minimal wiring and construction features include monitoring whilst distortion is less than $0.01 \%$.

## WIRELESS WORLD FM TUNER $£ 70.20$ + VAT

A pre-aligned front-end module makes this Wireless World published desige very simple to Anstruct and adiust without special instruments. Features include an excellent a.m. rejection, push-button station selection as well as infinitely variaole tuning and a phase locked loop stereo decoder incorporating active filters for "birdy" suppression.

LINSLEY-HOOD CASSETTE DECK £79.60 + VAT
This design, published in Wireless World, although straightforward and relatively low cost provides a very high standard of performance. There are separate record and replay amplifiers mechanism is the Goldring-Lenco CRV with electronic speed control.


COMPLETE KITS: Our complete kits really are complete. All of the projects shown on this page-are supplied with fully finished metalwork, ready assembled high quality teak veneer cabinet. cables, nuts, boits, etc, and full instructions - in fact everything!

All of the kits shown on this page are available as separate packs (except the Powertran SFMT Tuner) for those customers who wish to spread their purchase or perhaps make their own cabinets or metalwork. Prices are given in our FREE CATALOGUE

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# news digest. 

## CARRY-PACKS FROM JVC

A new range of equipment from JVC brings their VHS domestic video system into the portable market.
Leading the range is the HR4 100 colour portable video vassette recorder, with a price tage of $£ 799.92$ including VAT' it is fully compatible with all VHS recorders and weighs only 9.3 kg , complete with cassette, battery pack and RF converter.
The new GC4 100 colour video camera is a self-contained unit with the camera control unit built into the camera head. Two-tube design uses a new colour strife filter to improve colour reproduction, with an aperture correction circuit to give excellent resolution. Recording is possible with illumination as low as 100 lux. Retail price will be $£ 934.20$ p.
JVC have also launched the TV41 tuner/timer, which, when connected to the HR4100,
provides all the usual record/ playback facilities of a decktype recorder, the HR 3330, is a development of the previous successful model, but also includes extra refinements such as eight day timer, remotecontrol pause switch and audio dubbing facilities.

For further information on this new video range, contact JVC (UK) Ltd., Eldonwall Trading Estate, Staples Corner, 6-8 Priestley Way, London NW2 7AF.
to give



## OPTO FETS

A new trio of opto-coupled FETs, available from JermynMogul Distribution, feature a minimum isolation resistance of 100 gigohms between input and output.

These new GE opto-couplers consist of a gallium arsenide infra-red emitting diode coupled to a symmetrical bilateral silicon photo detector. The detector is electrically isolated from the input and performs like an ideal isolated FET designed for distortion - free control of low level AC and DC analogue signals. They do this by varying in resistance from between 100
ohms to 300 megohms, the change in resistance being controlled by the amount of current flowing through the infra-red emitting diode.
Applications include isolated variable attenuators, 70 db automatic gain control, remote band switching, sample and hold circuits, optically isolated multiflexers and reed relay replacement. The H11F family come in the popular six pin DIL package.
For products and application sheets contact Jermyn-Mogul Distribution of Vestry Estate, Sevenoaks, Kent.
"HELLO, HELLO-ABOUT THIS NEW
GARDENING COMPUTER ...."


MADEN

## news digest.......



## BARGAIN

BOXES

A new service from OK Machine \& Tool can save up to $65 \%$ on the cost of cases for some commercially produced items.

If you need more than 1000 units, OK can incorporate you special requirements into their latest range of Pac Tec moulded enclosures, available in over 25 sizes.

As an example of the success of their new cost-cutting service, OK have been able to produce 2,500 alarm unit housings for $£ 3.92$ each, compared to $£ 5.52$ for sheet metal units. Taking the total assembly time into total assembly time into
account, the saving rose to $65 \%$. account, the saving rose to $65 \%$.
Customised
front and rear panels can be supplied.
For further information, contact OK Machine \& Tool (UK) Ltd, 48a The Avenue, Southampton, Hants SO1 2SY'.

## LOW KEY

A new range of enclosures designed for housing a variety of keyboards has recently been introduced by Boss Industrial Mouldings.

Bimconsoles are all-aluminium cases with a textured black base which contrasts with either the semi-gloss sand or charcoal grey top panels.

The top panels slope at about 20 to provide a relaxed keyboard operating position. Vibration is reduced to a minimum by the use of a gasket assembly between top and bottom panels.

Bimconsoles are available in three sizes and are suitable for both prototype and OEM type applications. Further details

from Boss Industrial Mouldings Ltd, Higgs Industrial Estate, 2 Herne Hill Road, London SE24 0AU.

## ELECTRONIC TACHO

Orbit Controls are now producing a four decade electronic tachometer for measuring speed, rate, flowrate and frequency.
The 74A 430 has a four decade, solid state, digital readout and a pre-wired timebase, controlled by a high precision 1 MHz crystal oscillator.
Flexibility of construction allows pre-wiring to any interval from 1 mS to 10 S . The unit features high noise immunity and freedom from false triggering counts.
The frequency range extends from 0.5 Hz to 10 kHz with an input sensitivity of 100 mV (adjustable). Input, positive puise or sinewave, is fully protected to 240 V rms. Power may be from $100-110 \mathrm{~V}$ or 210 $260 \mathrm{~V} 50 / 60 \mathrm{~Hz}$, or from 12 V DC.

Further details from Orbit Controls Ltd, Lansdown Industrial Estate, Gloucester Road, Cheltenham, Gloucestershire GL51 8PL

## TEST CLIPPY

New IC test clips from Lektrokit offer a simple means of accessing any IC pin or lead.
The new aid clips over the IC bringing its individual pin connections out to a set of contacts at the opposite end of the clip. There are test clips available to match 8,14 and 16 pin DIL packages.
The gold-plated, phospho bronze spring contacts have been designed to achieve a wiping/cleaning action, making for high reliability.
The TC-14 which, as its name suggests, clips over a 14 pin DIP, costs $£ 2.95$. Further details from Lektrokit Ltd., Sutton Industrial Park, London Road, Earley, Reading, Berkshire RG6 1AZ,



## COOLING OFF

Got any hot-spots in your cabinets? You can get the air circulating round your equipment with the Vero Electronics Fan Tray (AB 087).
Two versions (1U and 2U) are available for either 115 V or $230 \mathrm{~V}(50 / 60 \mathrm{~Hz})$ input. Each is supplied with four 119 mm square axial fans, but
additional fans can be fitted as required.
The 2 U version has a polyurethane foam filter covering the air intake. If your living room or office isn't a smokeless zone, never fear, the filter is cleanable. Both versions operate at low noise levels.
If you need cooling off, contact Vero Electronics Ltd, Industrial Estate, Chandler's Ford, Hampshire SO5 3ZR.

## Measure Resistance to $0.01 \Omega$ At a Price that has no resistance at all

## Newelenco sprecision Digital Multimeter M1200B USA

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- $31 / 2$ digits $0.56^{\prime \prime}$ high LED for easy reading
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- High input impedance 10 Megohm
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- Mains (with adaptors not supplied) or battery operation-built-in charging circuitry for NiCads
- Overrange indication
- Hi Low power ohms, Lo for resistors in circuit, Hi for diodes

|  | SPECIFICATIONS: |
| :---: | :---: |
| DC Volts | Range $200 \mathrm{mV}, 2 \mathrm{~V}, 20 \mathrm{~V}, 200 \mathrm{~V}, 1000 \mathrm{~V}$ |
|  | Accuracy $1 \% \pm 1$ digit, Resolution .1 mV |
|  | Overload protection 1,000 volts max |
| AC Volts |  Accuracy $1.5 \% \pm 2$ digits, Resolution .1 mV |
|  | Overload protection 1000 V max, 200 mV scale 600 V |
| DC Current | Range $2 \mathrm{~mA}, 20 \mathrm{~mA}, 200 \mathrm{~mA}$, 2 amp . |
|  | Accuracy 1\% $\pm 1$ digit, Resolution 1 Microamp |
|  | Overload protection -- 2 amp fuse and diodes |
| AC Current | Range $2 \mathrm{~mA}, 20 \mathrm{~mA}, 200 \mathrm{~mA}, 2 \mathrm{mp}$ |
|  | Accuracy 1.5\% $\pm 2$ digits, Resolution 1 Microamp |
|  | Overload protection - 2 amp fuse and diodes |
| Resistance | Range 20, 200, 2K, 200K, 2 Meg .20 Meg . |
|  | Accuracy $1 \% \pm 1$ digit, Resolution .01 ohms |
| Environmental | Temp coefficient $0^{\circ}$ to $30^{\circ} \mathrm{C} \pm .025 \%{ }^{\circ} \mathrm{C}$ |
|  | Operating Temp $0^{\circ}$ to $50^{\circ} \mathrm{C}$ Storage - $20^{\circ}$ to $60^{\circ} \mathrm{C}$ |
| General | Mains adaptor: 6-9 Volts @ 200mA (not supplied) |
|  | 4 C size batteries (not supplied) |
|  | Size $81 / 4 \times 5 \frac{1}{4} \times 21 / 4$ Weight $21 / 2 \mathrm{lbs}$. |

At $£ 55, \mathrm{M} 1200 \mathrm{~B}$ is the best buy among DMM's currently available. Its 0.01 ohms resolution allows you to detect shorted windings in coils, transformers or motors. It is also useful in checking low contact resistance in switches, relays or connectors. Poor solder connections can also be spotted. The low power ohms function permits accurate measurements of in circuit resistance without forward biasing semiconductor junctions.
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HY5 Preamplifier. Input, magnetic pickup 3 mV , ceramic 30 mV . Output: Mains 500 mV HY30 Amplifier Kit is Watts into 80 extremely easy to construct. Output 15 W RMS. Distortion $0.1 \%$ at 15 W Freq. $10 \mathrm{~Hz}-16 \mathrm{KHz}$. Supply $\pm 18 \mathrm{~V}$

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HY200 Hi-Fi/ Disco Amplifier Module - 120 Watts 80 . Input sens. 500 mV 120W RMS Freq. $10 \mathrm{HZ}-45 \mathrm{KHz}$. Power Supply $\pm 45 \mathrm{~V}$. Size $114 \times 100 \times 85 \mathrm{~mm}$ Freq. 10HZ-45KHz. Powar Supply = Price: £27.99* HY400 (Big Daddy) Amplifier Module - 240 Watts $4 \Omega$. Ideal for High Power Disco
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| CRYSTALS* |  |
| 100 KHz 385 |  |
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| 1 MHI 323 <br> 1.0008 M 305 |  |
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| $3.2768 \mathrm{M} \quad 323$ |  |
| 4.032 MHz | $\mathrm{Hz}^{323}$ |
| 4.433619 M 135 |  |
| $5.09 \mathrm{MHz} \quad 365$ |  |
| 8.08333 M 276 |  |
| $\begin{array}{ll}10.0 \mathrm{MHz} & 323 \\ 10.7 \mathrm{MHz} & 323\end{array}$ |  |
|  |  |
| $18.432 \mathrm{M} \quad 323$ |  |
| 20 OMHz | 323 |
| $27.648 \mathrm{M} \quad 323$ |  |
| 48.0 MHz | 323 |

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## LATEST CASIO MINIS

Casio have managed to reduce their successful LC-78G calculator in three ways.
First of all - price. The RRP of the LC-78G is down by $£ 3.00$ to £16.95.
Second is the new Casio LC-7 which has the same display and functions except that the fully independent memory is replaced by a simple automatic accumulating memory and a square root function. The LC-78S has a RRP of only $£ 13.95$.

Thirdly, thickness has been cut down from four to two millimetres. Casio's new Mini Card LC-79 remains credit card size, but in upright format. It keeps eight digits capacity and LCD, four functions and independent memory plus perfect
percent and function indicator. Also featured is a responsive, 'feather touch' keyboard, so light that it can be operated inside its protective wallet. A battery-conserving circuit automatically switches off nine minutes after the last key depression. The Casio LC-79 will retail at $£ 19.95$ (or less, if you're lucky).

If you prefer something a bit beefier, try the LC-841, another new one from Casio. With the same technical features as Mini Cards (including independent memory), the LC-841 is 62 x 110 mm , but still only 3.9 mm thick, with digits 6 mm high, and will retail at about $£ 15.95$.

For enquiries, get in touch with Casio Electronics Co Ltd, 28 Scrutton Street, London EC2A 4TY.


MILITARY FLASHER

Need a tough twinkler? Oxley are now producing a solid state indicator lamp, type PS/LH/8, in a military style rugged mounting.
The mounting incorporates the latest high brightness, high reliability LEDs. The lamp is fitted with a sealed glass lens and black shroud to optimise the visual effect and afford emitter protection.

Standard colours are available, red, yellow and green, and light output is calibrated to photometric standards to ensure consistent performance. The aluminium alloy body is compatible with standard chassis and provides electromagnetic shielding for military applications. Further details from Oxley Developments Co Ltd, Ulverston, Cumbria LA12 9Qg.




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## CHESS COMPUTERS



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This 6502 based microcomputer comes with a full 8 K Microsoft basic in ROM. Full keyboard. 4 K static user RAM (on board expandable to 8 K ). Kansas City standard interface for use with an ordinary cassette recorder. Machine code monitor and I/O utilities in ROM. Direct Video access with 1 K dedicated RAM (besides 4 K user RAM) and full graphics set.

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2: Coffee stains (instant).
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4: Rough calculations for your new combined egg timer/laser cannon project.

5: ETI makes a fair soldering iron stand.
6: The dog insisted on carrying your copy to you along with your slippers.

## WHAT A BIND!

Half our orders for binders are repeats: we think that says a lot for their quality. At $£ 3.00$ all inc. you get a great deal of peace of mind too!

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## GENTLEMEN The PET OISK has landed...



The U.K. designed and manufactured Novapac disk system for Commodore's PET*, first seen at Compec '78, is (after extensive industrial evaluation), now available to the domestic user. Its unique saddle configuration continues the integrated design concept of your PET, with no trailing wires or bulky desktop modules.

- Novapac may be used with any available RAM plane.

Data transfer takes place at 15,000 char/sec - effectively 1000 times faster than cassettel

- Storage capacity is $125 \mathrm{~K} /$ bytes (unformatted) on 40 tracks per diskette side
- Dual index sensors permit dual side recording for $250 \mathrm{~K} / \mathrm{bytes}$ per diskette
- Easy operation full width doors prevent media damage.

System expandable to $1 / 2 \mathrm{M} /$ byte on-line storage ( 4 drives)

- Dual head and 2D versions provide $2 \mathrm{M} /$ bytes on-line.
- Industry Standard IBM 3740 recording format for industry
wide media compatibility only offered by NOVAPAK
- Dedicated Intel 8048 microprocessor and 1771 FDC minimise

PET software overhead.

- Local hardware and software support available

The sophisticated Disk Operating System is disk resident, which allows for future DOS enhancements without hardware alterations. PDOS supports multiple file handling, dynamically allocating disk space to each as and when necessary. Any file may occupy from 1 to 600 sectors as required, at up to 16 noncontiguous locations on the disk, PDOS may be used alone, or within a BASIC program, and offers user-specified password security for any file. Multiple access-modes simplify BASIC program construction

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# Hobby 

Electronics

BUMPER SHORT CIRCUIT ISSUE


Look out this month for more than your usual share of our very popular. Short Circuit feature. Plenty of circuit designs for you to develop and experiment with.

## SHARK



Not a game for the nervous. An LED-based game for two players which involved two swimmers in a race for survival in a sharkinfested sea. Which of these two castaways will reach the safety of the island? The unfortunate one is swallowed by the hungry shark, accompanied by a shrill scream. All good family fun!

## LINEAR SCALE OHMMETER



If you ever look at a multimeter on the ohms range you'll notice that most of the numbers are all squashed up one end; this makes accurate readings difficult. The HE Ohmmeter overcomes this difficulty with a linear scale. The range of resistance covered is from 1 k to 1 M ohms in four ranges, a useful addition to any workshop's range of test equipment.

## CASSETTE DECKS

 AND TAPES

Next to the TV and Transistor radio, the Cassette tape recorder is probably the most common piece of domestic electronic equipment. Next month Gordon King takes a close look at what has made the Compact Cassette so popular and one or two of its advantages and drawbacks, warts and all.

## RESISTORS



Following the success of our feature on Capacitors (according to our reader questionnaire) we're doing a follow up on the ins-and-outs of Resistors. Like Capacitors it's not going to be a formula-strewn study but a rather slanted look into their construction and use. So if you've never heard of Thick Film resistors and Metal Oxide, now's your chance.

## HOBBY CHIT CHAT

Ray Marston our Project Editor / Designer starts a new monthly series looking at our fast-moving hobby from the technical point of view. These articles are designed to take a look into the worlds largest growth industry, what's new and how it will affect us in our daily lives as well as a more specific look at our own side of the fence in HE .

## KIT REVIEW



One for the motorist this month, we have built up an Electronic Ignition system from Sparkrite (X4); read all about it next month. .

## LINEAR ICs

If you've been wondering what's going to happen now Into Electronics has finished, don't worry, Ian Sinclair has begun his follow-up series Linear ICs. Month by month the articles will introduce most aspects of IC use, construction and theory. With the background knowiedge gained from Into Electronics your understanding of new technology should increase dramatically.

POINTS CONTROLLER


Another project for model railway buffs. This unit gives full control over an unlimited number of electro-mechanical points using a pushbutton control. This makes an ideal companion to our HE Model Train Controller featured in the April issue.

## BABY ALARM

A really simple project to keep one ear on the kids whilst you're building your latest HE project.

## The July issue will be on sale June 8th

# TELETEXT SYSTEM 



## A complete ultrasonic controlled Teletext design employing the newly released Mullard chip set. Design by GMT Electronics for ETI. Facilities include double size characters and video superimpose.

THIS PROJECT is designed to allow the home constructor to produce himself a full spec Teletext unit at around half the cost of comparable commercial units. The design requires no hard wiring into the set, as it contains its own modulator and works into the aerial socket. Definition usually suffers utilising this method, but here great attention has been paid to overcoming this problem.
As with all decent designs remote control is ultrasonic, and gives both full and half page displays. The keyboard arrives already fitted to the PCB, and only needs the decoder chip and transducer soldering in to produce a complete unit.
A complete kit is available from GMT electronics, which includes plated-through hole PCBs, full metalwork and the hand controller. See Buylines for final details.

## Construct-a-Text

Despite the complexity of this project construction is amazingly straightforward, all that is required is to assemble the four boards CAREFULLY following the overlays, and fit these into the chassis. Interwiring between the PCBs is dealt with by following the list given here, and referring to the wire nos. shown on the overlays. Don't be tempted to change this, best results - indeed any results - will only be obtained by strict adherence!
Once you're satisfied that all is as it should be, fit the ICs into their sockets and move on to the setting up.


## Set up!

1) Disconnect encoder video $O / P$ from the modulator board.
2) Disconnect blanking and picture on (PO) outputs from main board.
3) Connect UHF O/P to set, and UHF aerial to converter.
4) Select spare channel on $T / V$ set
5) Tune $T / V$ for blank screen (ie. no noise).
6) Switch off.
7) Link P.O. input of UHF and mixer board to 12 V .
8) Switch on.
9) Tune RV 201 (front panel to obtain best picture on BBC1
10) Re-adjust set for best colour picture, modulator RV 401 may need adjustment.
11) Repeat 7 and 8 as required
12) Switch off
13) Reconnect steps 1 and 2 remove link step 6
14) Switch on.
15) Set RV 100 to midpoint.
16) Connect pin 1 C103(VIP) to 12 V
17) Connect pin 7 via 5 M 6 to 12 V .
18) With transmitter switch to mix mode.
19) Adjust CV101 until characters lock with picture
20) Switch off.
21) Remove steps 14 and 15
22) Switch on.
23) Adjust L101 to obtain page header and time clock stepping (note this setting is sharply defined). L101 should not need adjustment (ignore any colour flicker).
24) Switch off
25) Link pin 10 1C103 to 12 V rail.
26) Switch on. Note CV102 and L101 interactive repeat 20 and 24 as necessary.
27) Adjust CV102 for best display (approx $1 / 4$ closed).
28) Switch off
29) Remove step 22.
30) Switch on.
31) Switch to text mode.
32) Adjust CV301 for best colour.
33) Other channels can now be tuned (hit reset followed by channel No $1=\mathrm{BBC} 1: 2=1 \mathrm{TV}$; $3=B B C 2$ ).


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## INSTANT ELECTION <br> RESULTS. . . . . . 274

Above and below, two typical screen displays from the ITV, Oracle service. Now do you see what you're missing out on?


## HOW IT WORKS

## Ultrasonic Receiver And Transmitter

In the transmitter the keyboaid, commands are encoded by the SAA 5000 which switches the HEF 4069 transmitter IC in the correct code sequence.
This pulse coded 40 Hz transsmission is received by the TDB 1033 which provides 90 dB of gain in AGC system and a carrier filter. The output is fed to the decoder section.

## The Decoder

This design is based on the Mullard L.S.I. design and uses four main IC's and a memory section of seven 2102's.
The signal from the TDB 1033 is fed to the SAA 5010 receiver decoder and checked for error content and then produces various outputs.

1. Analogue Controls - Not used in this design.
2. Station Selector Drive Output Used via an HEF 4011 inverter to step an HEF 4017 station selector.
3. Message Received Output - Used to drive an LED and audible indicator.
4. Control Signals for the SAA 5040 TAC.

## SAA 5030 VIP Video Input Processor

The data retrieval section of IC, slices the incoming data signal by means of an automatic adaptive data slicer circuit. This circuit sets the threshold level for slicing at half the data amplitude, regardless of the amplitude of the incoming signal, and provides some compensation for distortion such as cochannel interference; the performance of the system under noisy conditions is thus improved. A clock signal is generate from the sliced data by using an external 6 M 9375 Hz tuned circuit, and this signal is used to clock the data into the TAC integrated circuit.
A 6 MHz display system clock is also included in the VIP, the output of which is divided in the TIC to produce a clock pulse every 64us. This signal is passed back to the VIP where it is compared with the incoming line sync signals. By this means, the timing system of the teletext display is phase-locked with the incoming television picture signal.
A 'signal quality' detector circuit is also included. When a signal with a high noise content is being received, or in the
absence of an incoming signal, the signal quality detector cuts off the teletext data to the TAC and allows the display system to free-run. Thus the detector prevents the data stored in the memory from being corrupted by noise. This facility, combined with the local display clock, allows a stable display even in the absence of an incoming television signal. Both are essential for after-hours display.
The IC also contains an adaptive sync separator which extracts the sync signals from the incoming video signal and also provides a sync output signal for the timebases of the television receiver. When a full page of text is displayed, the sync output signal is derived from the SAA 5020 TIC.

## SAA 5040 TAC Teletext Data

## Acquisition And Control

The principal function of the data acquisition section of the TAC integrated circuit is to process the teletext data so that it can be written into the memory. The control section processes the information from the remote control

system, and uses this information to operate the various display functions of the teletext decoder system such as selection of television, teletext, or viewdata modes; page hold, time display, or timed page select.
The datā acquisition section, divides the data from the VIP into its component parts. The Hamming-coded address words are checked, and words having a single wrong bit are corrected. Address words having two wrongs bits are rejected. The row address of the incoming data line (one of twenty-four) is fed by this section to the 5-bit row address bus, and the character date is fed through the data to the memory as a sequence of forty 7 -bit parallel words.
A signal denoted as WOK (Write O.K.) indicates to the memory when valid data is to be written in, and a WACK (Write Address Clock) signal causes the address counters 74LS 161 to step on after each character.

The IC also contains circuits for the implementation of the control bits for the page header.

## SAA 5020 TIC Timing Chain

The divider stages in the TIC integrated circuit sub-divide the 6 MHz clock signal from the VIP down to 25 Hz , the television frame rate, and generate all the timing signals for the teletext display. During the display period, a 1 MHz clock signal RACK (Read Address Clock) takes over from WACK to step the character addresses. The address counters 74LS161 are cleared at the end of every line and reset to the first position. After every ten lines during the display, the TIC steps the row address on by one to access the next row of characters in the memory.

In addition to providing all the timing signals for the display, the IC also generates a complete composite sync signal. This signal can be used to drive the timebases of the television receiver without the need for the transmitted sync signal. (This form of operation is also termed 'after-hours' operation.)

## Memory Blcok

The memory block consists of seven $1 \mathrm{k} \times 1$ static RAMs.

## SAA 5050 TROM Teletext

## Read-Only Memory

The read-only memory of the TROM converts the 7 -bit character data from the memory into a dot matrix pattern. This matrix is in a 7 -by- 5 dot form for each character. It also contains a 'character rounding' facility which effectively increases this matrix to 14 -by- 10 dots, giving improved definition to the displayed characters.

Additional circuits enable various control functions to be performed. These functions are determined by control characters received from the memory. Examples of these control functions are the selection of graphics or alphanumerics, 'flashing' words, or newsflashes and subtitles displayed in boxes within television pictures.

A 'concealed display' function is also provided which can be operated by the user.


## BUYLINES

The designers of this project GMT - have a complete kit of parts available. This includes all metalwork, PCBs and hardware. A manual is also included. Cost is $£ 155$ plus VAT (total $£ 178$ inc p\&p).

As an alternative the teletext decoder board and control system is available separately at $£ 125$ for those who wish to wire into their own television.

PCBs and chip sets are available separately also - but are PoA.

See advert on page 6 for address.


Fig. 2. Relay switching circuit (board four).


Fig. 3. Hand controller circuitry. Note that no overlay is shown for this, as no constructional work is needed using the kit. IC 1 is a SAA5000 for those wishing to go it alone.



Above: a unit complete except for mounting of the ultrasonic receiver


Next month we conclude the project with component overlays, parts lists and some erudite hints upon getting the best results from this superlative design.

Fig. 5. (Above, left): tuning circuit.
Fig. 6. (Below): Power supply circuitry to produce the three rails needed.


# MAGNETIC FIELD AUDIO AMPLIIIERS 


#### Abstract

Carver Corporation's Model M400 amplifier using the unique 'magnetic cavity' was released in the US a few short months ago. Employing FETs throughout, except for bipolar silicon output transistors, Carver Corp. claims that the M400 has a slew rate around $\mathbf{8 0}$ volts per microsecond, hum and noise over 100 dB down, $\mathbf{0 . 0 5 \%}$ distortion and a frequency response from $1 \mathbf{H z}$ to 250 kHz - all for an expected retail of US\$300!


IT REALLY DOĖS EXIST. ETI first reported Bob Carver's Magnetic Field Audio amplifier in our Australian issue saying . . . "we hear from normally authoritative sources that Bob Carver founder of Phase Linear - has developed a totally new concept in audio amplifiers which $\qquad$ stores energy in a magnetic field rather than in power supply capacitors . . . his new device generates no heat, weighs a mere five kilos•for vast numbers of watts and lasts for ever".

It seemed a bit hard to take seriously - even though we were totally aware of Bob's previous efforts such as the range of Phase Linear super-amps and the Autocorrelator noise reducer.

But it seems as if this revolutionary concept in audio amplifiers is for real patent protection has been arranged and preliminary details have been released.

Bob's basic concept is to store energy in a magnetic field rather than very large value electrolytic capacitors - eliminating at the same time the need for a bulky expensive power transformer.

Our circuit drawing shows the essential features. The heart of the circuit is
the magnetic cavity ( $M C$ ). This is basically similar to the AM detector transformer used in conventional AM radios but constructed on a grand scale. A further and significant difference is that the transformer is arranged such that an output occurs as the primary field collapses rather than builds up.

The secondary winding of the magnetic cavity is centre-tapped and the resultant full-wave output is rectified by a pair of high current diodes - the output waveform is thus a conjugate pair of time-varying audio voltages. Further circuitry, described later in this article, provides a feedback loop to remove commutation noise and reduce distortion.

- The primary of the magnetic cavity is energised by an amplitude-modulated current (corresponding to the audio signal voltage). The current signal is produced from the audio input, via the optical isolator and modulation and control logic, to the scanning SCR, the ramp SCR, a pair of scanning and commutating diodes, and L1, L2 and C1.

This current signal energises the
primary of the magnetic cavity. The time taken for this is called the 'ramp period'. The primary energy is then reflected in the secondary windings (and thence to the speaker) during the subsequent 'scan period'.

As our graph shows, the ramp and scan periods are made up of four separate timing intervals. During the period $t_{0}-t_{2}$ an incoming audio signal has caused a magnetic field to 'ramp' up in the primary of the magnetic cavity. At $t_{2}$ the field has reached its peak and is beginning to collapse. This collapsing field generates an associated decaying current $i_{1}$ and this decaying current falls to zero when the energy in the primary field falls also to zero (point $t_{3}$ ). During the time period $t_{2}-t_{3}$, the control logic provides a positive signal on the gate of the scanning SCR, however this SCR will not again conduct until sufficient voltage is applied between its anode and cathode.

Throughout the scanning period, energy is of course being transferred from the primary of the magnetic cavity to the secondary - and thence to the speaker load.


Fig. 1. This schematic shows the major operating components.

At time $t_{3}$ the direction of current is reversed - current being no longer maintainable by cavity inductance and the scanning diode is reverse biased - this causes the scanning SCR to be forward biased and current flows as shown in our sketch.

Summarising then, energy stored in the magnetic cavity is caused to shuttle around the circuit of L1, L2, C1 and the speaker load depending on instructions from the control logic.

## Noise and distortion

Components Q1 - Q3 form a feedback loop which reduces the inherently poor bandwidth, noise and distortion to very acceptable levels. Theoretically the circuit has some quite strong objections - at low frequencies Q1 and Q 2 will act much as switches except that the feedback correction voltage developed by Q3 will adequately cancel aberrations but at higher frequencies, i.e. $10 \mathrm{kHz}-$ 20 kHz the modulator circuit is unable to follow accurately the audio input


Fig. 2. During the ramping period energy builds up in the primary of the 'magnetic cavity'. Throughout the scanning period energy is transferred from the primary to the secondary of the magnetic cavity and thence to the speaker load via Q1 and Q2.
signal. Hence the filtered output from the magnetic cavity is a dc level with a superimposed ac signal and Q1 and Q2 thus operate much as any other conventional amplifier.

Nevertheless as less power is generally required at high audio frequencies than at mid frequency and low frequency, amplifier efficiency is very high if fed with music signals. This situation does not of course apply if the amplifier is fed with a high frequency steady tone.

Bob Carver's radical amplifier will be rated in accordance with FTC rules - the specification is expected to include power output: 200 watts-perchannel into eight ohms from 20 Hz to 20 kHz . Total harmonic distortion is expected to be less than $0.08 \%$ across this range.

Signal noise ratio is expected to be 100 dBA below rated maximum output. All-up weight is an incredible 5.5 kg .

As far as we are aware the magnetic field amplifier exists at present solely as a prototype unit but we understand that Bob Carver has very real plans for putting the unit in to production at a presently projected price of US $\$ 300$ or so.

It's a fascinating concept, one that will cause amplifier designers and manufacturers world-wide to furiously rethink their design philosophies. It may even herald the coming of a new hifi technology.

ETI


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# POIYPHONIC KEYBOARD CONTROLIER 

## Tired of playing one note at a time on a boring old monophonic synthesizer? In this design Tim Orr describes how you can build a four octave polyphonic keyboard controller incorporating first note priority.



THE MUSIC synthesizer is probably the most powerful musical instrument of today, and it will most probably form the basis of the next generation of keyboard instruments However, the synthesizer suffers from one major drawback due to its unique structure. The disadvantage is that it is a monophonic instrument as opposed to traditional keyboard instruments, such as organs and piano's which are polyphonic, or multi-voiced. A brief resumé of synthesizer structure should clarify the reasons behind this.

To start with, the synthesizer is composed of a set of modules or independent circuit packages whose parameters in most cases are voltage controllable. For instance, a voltage controlled oscillator (VCO) has an output frequency (pitch) which is dependant on the magnitude of the input control voltage. These modules can be split up into three distinct
groups. Firstly there are Sources, such as:

1. Noise
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Secondly there are Modifiers which form by far the largest 'group:

1. Voltage controlled filters (VCF's)
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Thirdly there are control voltage sources:

1. Sample and holds
2. Sequencers
3. Transient generators
4. Trigger delays
5. Keyboard controllers

## Getting Your Priorities Right

First note priority was adopted for this design, i.e. first note pressed to channel 1 , second to channel 2 , and so on. If more notes are pressed then the system can cope with, these are locked out. The reason for this, as opposed to last note priority, is that first note priority stops the note jumping that can occur when, momentarily, more notes are pressed than the system caters for.

## Binary Notation

When the code (note code) driving the decoder energises a contact which is closed, the output of the OR gate goes high, showing a unique code on the input representing the particular note being pressed. This code, the note code, is arranged such that the lowest note is binary zero, the next note up binary one, the next
two and so on up to N .
The scanning can also be achieved using a multiplexer.

The size of keyboard decided on was a 4 octave one having 49 notes. Hence this makes the value of N49 and therefore the size of the note code will be 6 bits ( 64 possibilities). In fact this is useful in that a 6 bit code will be just big enough to scan a 5 octave keyboard (61 notes) if required. In the case of this design it will simply be a mattter of adding 12 extra diodes since the decoder already had a total of 64 outputs. Incidentally, the scanner will have another output not yet mentioned. This is called 63rd note, the 63rd output on the decoder) which simply provides a pulse to the decision logic to say that a scan has been completed. The multiplexer method would require decoding of the note code to do this. The scanner simply gives each note a binary code, but how can this be extracted as a set of control voltages with associated gate signals?

## Pumping Caps

The note code is changed to an analogue voltage using a D-A ,converter, the output of which is switched onto the correct analogue channel and held using a set of sample and holds. The gate signals are dealt with in a similar way using CR circuits. The counter for the note code causes the scanner to increment from the lowest note upwards. If three notes are depressed the scanner reaches the lowest note first and causes the output of the D-A to be stored by channel 1 sample and hold, and channel 1 gate capacitor to be pumped up. On moving on the channel counter is incremented, prepairing the output channels for channel 2 data. When the scanner reaches the second note up the process occurs again only using channel 2 and again for channel 3 , with the third note. When the scan has been completed the channel counter is reset and made ready for the next scan.

## Dying Charge

If on the next scan the notes are still depressed, the gate capacitor will again be pumped up maintaining the gate output high. When a note is released the time constant is such that the gate capacitor's charge dies away in about one and a half scan


The largest of the four PCB's, carrying the logic circuitry.
times, thus removing the gate signal. By experiment it was found that the scan time needs to be about 4 mS . Even when a key is pressed and released very quickly, it will have been scanned about ten times or more. The NAND gate should be mentioned because it allows two adjacent notes to be played. This is because if two notes right next to each other are depressed, the output of the scanner remains high for the duration of both notes and so only one note would be detected. By NANDing the scanner output with the clock the output is broken up allowing adjacent notes to be detected.

## Note Jumping

Although this circuit will work, it is far from satisfactory. When notes other than the top note are released, the channels on which the remaining notes appear, above the released note, all jump down one place. This makes the instrument very difficult to play as it must be remembered to release the keys from the upper one downwards, to get a chord that dies away nicely without the note jumping effect.

## Special Decision

This means that the simple logic must be replaced by some special decision logic, incorporating a memory of notes already activated in previous scans.

The scheme here is that note codes are gathered into the memory as the scanner sweeps up the keyboard. When the $63^{\text {rd }}$ note is reached, the
entire memory is dumped onto the output channels by sequencing the peripheral address lines. It is also necessary to reset all of the gate data bits in preparation for the next scan. This means that while a particular key remains pressed, the gate for that channel will be refreshed on every scan. When the key is released, the gate for that channel will go low when data is again output.

## Logical Channels

The effect of the decision logic from the musicians point of view, is that upon playing a chord, say C, E and G the first one depressed normally comes out on channel 1 , the second on channel 2 and the third on channel 3 (the difference in time between depresssions need only be milliseconds). There is, however, an exception to this when a note is depressed that is already stored in memory. For instance, if the three note chord described above were depressed such that $C$ was first $E$ second and G third, then it would be expected that $C$ would come out on channel 1, E on channel 2 and $G$ on channel 3. But if a previous chord had been played using the same $C$ which had emerged on channel 2 then the decision logic would cause it to remain on channel 2 and so the E would be placed onto channel 1 and G onto channel 3.

## Key Question

Construction of this project will depend almost entirely upon the keyboard it is built around. If you


Fig. 1. Circuit diagram of the scanner. The four 74154 's are used as a one out of 64 line decoder.
address counter reaches 2 the comparator output goes high acknowledging that the note is already entered. This causes the gate bit to be refreshed (since it is reset during data block) along with the data being re-entered into the note memory, (re-entering the data in the note memory is not necessary but occurs due to circuit architecture) after which the decision flip flop IC15 is again reset and the scanner restarted.
All the time a note remains depressed the decision logic will refresh the gate bit associated with the channel in which the note has been placed. At the end of a scan the gate bits are reset immediately after they have been placed on the output channels meaning that if the note is not still depressed on the next scan the gate signal on the output channel will go low in the next data block period.
During a scan the data valid signal is high, it only toggles in data block. Simply enabling the gate RAM during the decision cycle loads it with a ' 1 ', since data valid is the input. Note that loading these Ram's with a ' 1 ' results in the output going to a ' O ' as they invert. This is the reason for the invertors on the outputs of the note RAM's, which are also tri-state for the computer interface.
The clock for the system is an NE555 timer wired in the astable mode.
The Output Channels
There are two_outputs per channel which
are multiplexed out by the data block period. These are the gate outputs and the control voltage outputs. The gates are obtained from the CD4099 addressable latch (note that these outputs may need buffering depending on the impedance they are driving as the CD4099 is CMOS). The address lines of the latch are attached to the memory address counter and the input is connected to the gate data line (IC10 pin 2 ). The enable input of the latch is connected to the data strobe line so that as the data is output from the memory the correct gate state ( 1 or 0 ) is stored on the relevant channel.

The data sample pulses are for loading the sample and holds on the analogue channels. They are derived from the 1 of 8 decoder and the clock. To interface bet ween the TTL logic and the analogue switches comparators are used so that the analogue signals can be between -3 volts and +12 volts. All the comparator outputs are disabled when the clock is high by using the two resistors R65 and R53 to feed the reference input to the comparators, the clock signal being attached to R65. The binary codes representing the notes are converted into analogue voltages using the D-A convertor IC14.
As the memory address counter is incremented in data block the data in the note memory is converted into an analogue voltage and passed onto the correct analo gue channel by the comparator and analo-
gue switch. The D-A convertor has a cur rent output such that when the resistor R82 is added to convert it into a voltage, the output goes more negative with increasing binary codes. The op-amp IC29 (pins 12, 13 and 14) corrects this by inverting the out put of the D-A. It also allows the scaling or volts per octave of the keyboard to be adjusted, by varying the resistor in the feedback loop. Another function that the op-amp allows is the summing of voltages that have to appear on all the output channels at once.
There are three sources of voltage that are summed at this point, the tune voltage the vibrato voltage, and the pitch bender voltage. The tune voltage is derived from a potentiometer which draws its current from the voltage reference circuit. The vibrato voltage is generated by a standard triangle wave generator comprising a regenerative comparator IC29 pins 8,9 and 10 and an integrator IC29 pins 5, 6 and 7. The output is coupled to the summing amplifier via a pair of back to back electrolytics to remove any DC offset and a pair of resistors that allow their centre point to be connected to earth via an externa vibrato depth potentiometer.

Offsets around the circuit are trimmed out using the trimmer RV1 which obtains its reference from the diode D1. Since the offsets are predominantly in one direction due to Q 2 the offset control only works in the negative voltage direction.

employ the ARAK kit, no problems should arise at all. The PCBs are designed to fit their keys and comprehensive instructions are included with the kit.

We have not attempted to go into any detail with any other unit, simply because there is such a great diversity available on the market.

## Setting Up

Once the components are all mounted on their boards, each section has to be set up. Let's start with the

## PSU

Before the mains is connected to the PSU it should be thoroughly checked for shorts. The three low voltage fuses FS202, FS203 and FS204 should then be removed and the mains turned on. Now check the voltages across the smoothing capacitors C201, C202 and C203 which should be around $+8 \mathrm{~V},+17 \mathrm{~V}$ and -17 V respectively. If this is the case the +12 V regulator can be tested by replacing FS203. If this works the +5 V regulator can be tested by replacing FS202. As the +5 V regulator is supplied from the +12 V supply via R201 they must be tested in this order. Finally the -12 V and -3 V supplies can be tested by inserting FS204. It should be noted that the fuse holders may need bending to give correct contact to the fuses as they are very simple pressed steel pieces for PC mounting

## The Logic Board

Check the logic board thoroughly for shorts on supplies. It is also wise to
'buzz out' every connection on the board to test for continuity which may well save a lot of fault finding time, but note that it will not guarantee correct operation as it does not test for shorts.

When these preliminary tests have been carried out and the power supply unit is functioning correctly. power can be applied to the logic board. Firstly only apply the +5 V supply until the TTL is known to be working correctly.

## And a Log

Once the logic is working the analogue section can be tested. This time some setting up can also be done:

First check the positive reference is sitting at about 6 V 2 above earth. This level can be increased using the trimmer RV7 if a higher reference is required for any reason.

If the touch circuit is not to be used R63 should be removed as it will probably cause the output of IC29 pin 14 to saturate against one of the supplies as the output of the touch circuit is indeterminate.

R19 sets the maximum glide rate. The smaller it is the longer the maximum glide rate will be However, it is unwise to make it any smaller as the maximum range is set by the $\mathrm{V}_{\mathrm{EE}}$ on SAT of the switching transistor, this only creating an offset when it is turned on and not when it is turned off. It may be necessary to increase the value of R19 although problems will probably occur on one channel only and will most likely be remedied by replacing the switching transistor for one with a lower $\mathrm{V}_{\mathrm{CE}}$




Fig. 4. (below) Component overlay of power supply board.
Fig. 5 (above) One of the two keyboard PCBs, designed to fit Araks keys.



| CAPACITORS <br> C1-3, C8, C9, <br> C11, C12, C14, C15 |  | IC9-11, IC13 | 74LS93 |
| :---: | :---: | :---: | :---: |
|  |  | 1 Cl 2 | 74LS123 |
|  |  | IC14 | MC1408L-8 |
| C17, C18, C24 | 10 n polyester | IC15-18, |  |
| C4 | 22p | IC31, IC32 | 74 LSOO |
| C5, C6 | 100p | IC19, IC20 | $74 \mathrm{LSO4}$ |
| C7, C10, C13, C16, |  | IC21 | $\begin{aligned} & \text { 74LS366 } \\ & \text { (or 74LS368) } \end{aligned}$ |
| C19, C25, C26 | 100n polyester |  |  |
| C20, C21 | 33u | IC22, IC23 | $74 \mathrm{LS10}$ |
| C22, C23, C29 | 1 uO 35 V electrolytic | IC24 | CD4066 |
| C27, C28 | 330p | IC25 | LM339 |
| SEMICONDUCTORS | BCY72 | IC26, IC27, IC28, IC30 | TL084 |
| Q2-6, Q8 | BC107 | IC29 | LM4741 |
| 07 | 2N5163 | D1, D3-7 | 1 N914 |
| IC1 | NE555 | D8 | LED |
| IC2 | CD4099 | Miscellane |  |
| IC3, IC4 | 74LS85 | MISCELLANE |  |
| IC5-7 | 7489 | 37 way 'D' st | jack (3 off), SPDT |
| IC8 | 74LS155 | switch (4 off). | tre off. |



ELECTRONICS TODAY INTERNATIONAL - JULY 1979



#### Abstract

As a London-based magazine, we tend to concentrate our interest on exhibitions and electronics shows in the London area. Lest we become too parochial in our outlook, we decided to see what our fellow Europeans have to offer. We sent our roving reporter, Ian Graham, to Paris to see how the other half live.


I PROBABLY RECEIVE a couple of hundred Press releases every day. Most, concerning orders for electronic equipment won by companies or appointments to the top management of larger corporations or annual accounts, end up in the waste paper bin. Our reports on the cream of the rest appear monthly in our news pages. Occasionally I am invited to attend Press receptions. Again, few are interesting enough to prise us out of our armchairs. However, I did sit up and take notice when I was invited to attend an electronic components exhibition 'sur le continent'. The occasion was the Salon International des Composants Electroniques 79, held in Paris from the 2nd to 7th of April. Well, I thought about it, for several seconds at least, and decided that I had indeed been neglecting our European brothers.
On a sunny April morning I made my way from Charles de


The tops of stands stretch into the distance, in the biggest of the three exhibition halls.


Row upon row of stands full of goodies - paradise for the exhibition addict.

Gaulle airport to the exhibition site at the Parc des Expositions in the Place de La Porte de Versailles. My first impression as 1 emerged from the Metro station was of the unexpected size of the exhibition, which stretched over a staggering 63,000 square metres, split up into four sections. It would have taken several days to see everything on display, certainly more than the single day I had allowed myself.
Although it was essentially a trade show, the atmosphere inside was more akin to that of our own Ideal Home Exhibition. However, great expectations of an entertaining exhibition were not borne out by my admittedly swift tour of the stands.


A fun way of counting trains with photocounters. This stand attracted a great deal of interest from people who had probably never seen a photocounter before. This simple display illustrated the principle of the unit admirably for the layman.

## Dry Stuff?

Unfortunately, few exhibitors showed any imagination in the presentation of their wares. Sound to light units and TV games naturally lend themselves to entertaining stands, but what about more mundane electronic components? General Instrument Microelectronics (a British firm, I'm happy to say) managed to make microprocessors a crowd puller (I wouldn't have thought it possible) by using one to control a noise generator. Pretty dry stuff, you might say. However, the generator was producing car engine, gear change, skid and crash noises for a model racetrack. Visitors could control the cars with conventional pistol grips. Well, perhaps a model race track has little to do with microprocessors and vice


A closer look at the electronic 'train' spotter above. One colour of wagon, in this case blue, can be counted, ignoring the train and all the other wagons.
versa, but it did attract interested visitors. Isn't that what it's all about?

## Eyecatching Pyramids

Another firm displayed photocounters by using them to count wagons on a pyramid of model railway layouts. Talking about pyramids, yet another firm (American) presented a striking display, a pyramid of multimeters. They might uncharitably be called gimmicks, but they were eyecatching. Too many exhibitors relied on a glass case full of components accompanied by row upon row of standard black and white exhibition photos, none of which deserved or got a second look. Still, there were plenty of product demonstrations to keep me busy, as I made my way through the maze of stands. There were also lectures. How do you fancy soaking up 'Monolithic Memories' at half nine in the morning? No, neither did I.


Keithley's pyramid of multimeters. We strongly suggest that you don't try this with your Avo. 8's, or if you do, don't blame us if there are disastrous consequences.

## Light Entertainment to Heavy Machinery

Although I found plenty to criticise at the Paris show, it put some of our own electronics shows to shame. Whatever you are interested in, from hi-fi to heavy machinery, there's plenty of it at the Salon, with some 1300 firms exhibiting. Hi-fi enthusiasts could spend a day or two wandering round the stands devoted to the love of their life. That goes equally well for every field of interest represented and there wasn't much that was not represented.

## See You Next Year

My brief visit to the show was very enjoyable. There was plenty of food and drink to be had from seemingly numerous bars. The French exhibition staff were so good to me that I'm thinking of doing it again next year. If you feel like joining me, the Salon International des Composants Electroniques 80 will be held from March 27 to the 2nd of April. If you feel like nipping across the pond to pay your visit on Sunday, March 30th, don't......they're closed. ETI


# MOTOR SPEED CONTROULER 

## A sophisticated unit that allows control of model electric motor speed and direction via a single radio control channel. The unit can supply peak currents up to 10 amps .

THIS DEVICE lets you use a single channel of your radio control system to control both the speed and direction of an electric model motor. The unit has been designed specifically to control the drive motor of our 1/16th scale Tamiya Leopard tank but can in fact be used to control any 4 V 5 to 8 V DC electric motor that draws peak current below 10 amps . The unit is ideal for use in model boats and large-scale land vehicles, and costs only a fraction of the price of equivalent commercial units.

The unit derives it's control signals from one of the output channels of a radio control decoder. It accepts standard positive or negative decoder pulses, which have widths variable over the 1 mS to 2 mS range, and is designed to work with systems having fixed frame (or frame repeat) periods of approximately 20 mS . The Strato $4+2$ system, published in the May and June editions of ETI, can be used with the controller.

The controller circuit incorporates only two pre-set pots. One of these is a 'set null point' control, and can be used to set the motor speed to zero in any desired position of the transmitter joystick control. The other pre-set is used to set the maximum speed of the motor.

The two pre-sets can be used to give a variety of operating modes. If they are adjusted so that the null point occurs at the centre of the joy stick travel, the motor will have identical maximum speeds in forward and reverse. If the null is set to occur towards the 'low' end of the joy stick travel, the motor will have a high maximum forward speed and a low maximum reverse speed.


## Construction And Use

The unit is assembled on two PCB's. Board 1 holds all the logic, timing components, and the two pre-set pots, and board 2 holds the power driver transistors and the relay. Construction of board 1 should present few problems: note, however, that no provision is made on the PCB for decoupling capacitor C8, since we hooked this component into the wiring harness on our prototype unit.

Note when constructing board 2 that power transistor Q4 can either be mounted directly on the board in low- to medium-power applications, or can be mounted externally on a suitable heat sink (such as a vehicle chassis, etc) in high power applications. The relay used on this board is a 6 volt two pole changeover type with a coil resistance of 70R (see Buylines).


When construction is complete the two boards can be mounted in the model, preferably as far away from interference-generating motors and servos as possible. Board 1 is powered from the radio control decoder supply lines. The signals from the selected output channel of the decoder are fed to either the positive pulses or negative pulses input leads of board 1, depending on the pulse polarity of the particular decoder that is used.

Board 2 is powered from the motor supply leads. Note that the OV line of the motor supply must be made common with the OV line of the decoder. Also note that one lead must be connected between R6 on board 2 and pin 4 of IC1 on board 1, and another lead must be connected between R12 on board 2 and Q1 collector on board 1


The input pulses from one channel of the decoder, which have widths that are variable between 1 mS and 2 mS , are fed to either pin 1 or IC 2 a (negative input pulses) or to pins 12 and 13 of ICla (positive input pulses), and appear in positive-going form at the output of IC2a. This positive-going pulse is fed directly to pin 12 ot 1 C 2 b , and is fed in inverted form to pin 5 of IC2c: the inverted pulse is also used to trigger reference-pulse generator IC3 via Cl. This reference pulse has a nominal width of 1.5 mS , which equals the mid-band width of the input pulses from the decoder.

The positive-going reference pulse is fed directly to pin 6 of IC2c, where it is compared with the negative-going version of the input pulse on pin 5 . The action of IC2c is such that its output is normally high, but switches low for a period equal to the difference between the reference and input pulse widths only when the input pulse duration is less than that of the 1.5 mS reference pulse. This negative-going output pulse, which has a width that is variable between zero and a nominal 0.5 mS , is used to rapidly discharge C4 via D1 and thus cause the output of ICId to switch high and drive relay RLA on via Q1 and R6. This relay, which dictates the direction (forward or reverse) of the motor that is being controlled, is thus off when the input

## HOW IT WORKS

pulses are greater than 1.5 mS (nominal), and on when the input pulses are less than 1.5 mS .

The 1.5 mS reference pulse of IC3 is inverted by IClc and fed to pin 13 of IC2b, where it is compared with the positive-going version of the input pulse from the decoder. The action of IC2b is such that it's output is normally high, but switches low for a period equal to the difference between the reference and input pulse widths only when the input pulse duration is greater than that of the 1.5 mS reference pulse. This negative-going pulse, which also has a width that is variable between zero and a nominal 0.5 mS , is fed to pin 9 of IC 2 d .

Thus, a negative-going pulse appears on pin 9 of IC2d if the decoder pulse is greater than 1.5 mS , or on pin 8 of IC 2 d if the decoder pulse is less than 1.5 mS . Consequently, IC2d generates a positive-going output pulse that has a width that varies from zero on a 1.5 mS decoder input pulse to 0.5 mS on a 1 mS or 2 mS input pulse.

This pulse is fed, via D2, to a pulse-expander circuit designed around IC4, which expands the pulse width by a factor of about 40 . The resulting expanded pulse is passed on to the external motor via transistors Q2 to Q4 and the contacts of the relay, and is used to give pulse-width or variable
mark/space-ratio control of the motor speed. Diode D4 is used to damp motor back-EMF, and lamp LP1 is used to minimise the effects of
interference-generating current surges.
In practice, RV1 is used to adjust the width of the reference pulse (nominally 1.5 mS ) so that the motor speed is zero when the transmitter joy-stick control is in its central or null position, and RV2 is used to adjust the expansion factor of the pulse expander circuit and thus pre-set the maximum speed of the motor when the transmitter control is in its 'maximum' position.

## BUYLINES

The relay is the only component that calls for comment here. It is a 6 Volt 2-pole changeover type with a coil resistance of 70R, and is available from Greenweld, 443 Millbrook Road, Southampton, SO1 OHX. The price is $£ 3.30$, including postage and the usual extras.


And this is how the boards should look once you've built them up. Check very carefully before switching on.


## What A Turn On

When installation is complete, turn on all power switches, check that the unit functions correctly, and then adjust pre-set pots RV1 and RV2 for the required operation. To set RV1, move the transmitter joy stick to the required 'null' position, and then adjust RV1 for zero motor speed: under this condition the relay should be on the verge of switching between the on and off states. Next, move the transmitter joy stick fully forward, and adjust RV2 for the desired maximum motor speed. The setting up procedure is then complete.

Finally, note that the operation of the motor speed controller can be adversely affected by electrical interference from motors, etc. All motors in the model must therefore be adequately suppressed. A 100 n disc ceramic connected directly across the motor terminals works pretty well in most cases. ETI


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| Lm701C | 2.99 | LM7812KC | 1.56 | CA3041 | 1.65 |
| Lm702C | 81 | [1.7815kC | 1.56 | CA3042 | 1.65 |
| Lm7031m | 1.15 | 1m7824KC | 1.56 | Ca3043 | 2.20 |
| [m709CH | . 70 | Lm78L05cz | . 30 | C43045 | 1.55 |
| Lm709.8 | . 50 | 1m7812cz | . 30 | CA3046 |  |
| IM709-14 | . 49 | 1m78L15cz | . 30 | CA3047 | 2.20 |
| Lm710C\% | . 67 | Lm7BL24Cz | 30 | ca3047 | 3.70 |
| Lmp10.14 | 48 | mC667P | 2.75 | CA3048 | 2.45 |
| (m711CM | 48 | mC671p | 1.75 | CA3049 | 1.98 |
| tm716 | 1.00 | MC672P | 1.75 | CA3050 | 2.66 |
| 1 1m73C\% | 62 | MC724P | 2.10 | CA3051 | 1.83 |
| LM723C-14 | 45 | MC789P | 1.80 | CA3052 | 1.78 |
| Lm741CH | 50 | MC 790p | 3.10 | C13053 | 77 |
| Lm741C.8 | 30 | MC798p | 2.20 | Ca3054 | 1.10 |
| Lm741C.14 | 60 | MC799p | 2.20 | Са3059 | 2.10 |
| Lm747CM | . 78 | mC832P | . 70 | ca3060 | 2.50 |
| LM748-8 | 50 | mC833P | . 70 | C13062 | 3.75 |
| Lm748-14 | . 50 | MCB36p | B2 | CA3064 | 1.1 |
| LM 900 | 50 | MC837P | . 2 | CA3065 | 1.10 |
| LM911 | . 50 | MC83ap | 2.35 | CA3068 | 3.80 |
| Lm921 | 50 | MCB40p | 1.65 | CA3070 | 1.90 |
| Lm923 | . 50 | MC844P | . 70 | CA3071 | 1.90 |
| LM1303M | 1.15 | mC346P | . 70 | CA3072 | 1.90 |
| Lm13094 | 1.52 | mC348p | 1.10 | CA3075 |  |
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# 40 CMOS CLOCKS 

## There are many ways of using the CD4001 and CD4011 CMOS ICs to make bistable, astable and monostable multivibrator circuits. Ray Marston presents the definitive work on the subject, with 40 practical circuits.

THE AMATEUR AND PROFESSIONAL circuit designer often finds himself in the situation where he needs to use a minimum-cost CD4001 or CD4011 CMOS pulse or clock generator circuit, or where he needs to use a few spare CMOS NAND or NOR gates from an existing circuit to make up a multivibrator that will meet his specific design needs. In either case, the designer will find a concise guide to practical NAND- and NOR-gate CMOS multivibrator circuits of inestimable value.

This article is just such a guide. It presents some forty different ways of using the low-cost CD4001 and CD4011 quad 2-input gate CMOS integrated circuits in bistable, astable and monostable multivibrator applications. All of the circuits shown can be operated over the full five volts to fifteen volts supply range when used with ' $B$ ' series CMOS.


Fig. 1. Outline and pin connections of the CD4001.

## THE CD4001 and CD4011 ICs

Figures 1 and 2 show the outlines and pin connections of the CD4001 and CD4011 integrated circuits. These two ICs are quad 2 -input gates. The CD4001 provides NOR gate functions and the CD4011 provides NAND gate functions. Fig. 1 shows the truth table of each of the four NOR gates of the CD4001. Note that the output is high if both inputs are low, but goes low if either or both inputs go high. Fig. 2 shows the truth table of each of the four NAND gates of the CD4011. The output is normally high and goes low only if both inputs are high.



Fig. 2. Outline and pin connections of the CD4011.

The CD4001 and CD4011 are very inexpensive ICs. They typically retail at about 16 pence each in one-off quantities (allowing for some variation between suppliers), which works out at about 4 pence per gate. They can be used in a wide variety of very useful two-gate multivibrator applications and are thus highly costeffective devices.

## Bistable Multivibrator Circuits

The CD4001 and CD4011 can both be used in two-gate R-S (Reset-Set) bistable multivibrator circuits, but have quite different input triggering requirements. Fig. 3 shows the practical circuit and waveforms of a pulsetriggered NOR version of the bistable. The circuit has two outputs, a normal output from IC 1a and an inverted output from IC1b. When a positive-going trigger pulse which switches between roughly zero and full supply is applied to the IC1b input, the normal output sets high and locks in this state irrespective of any further signals at the input of 'IC1b. The output can only be reset low again by applying a positive-going pulse to the input of IC1a, at which point the output goes low and is then immune to any subsequent trigger pulses at the input of IC1a.


Fig. 3. Practical circuit of a pulse-triggered NOR bistable.
Note that the input terminals of IC1a and IC 1 b are tied to ground (the zero-volts line) via R1 and R2: these resistors can have any convenient values in the range 10 k to 10 M . If inputs to IC 1 a and IC1b are directcoupled from preceding logic networks, however, R1 and R2 can be omitted from the circuit.

## Manual NOR Gate

Fig. 4 shows a manually-triggered version of the Fig. 3 NOR gate circuit. This type of circuit is often referred to as a 'noiseless' switch, since its output is unaffected by the contact bounce, etc., of its two control switches.


Fig. 4. Manually triggered NOR bistable.

## NAND Bistable

Fig. 5 shows the CD411 NAND gate version of the bistable circuit. This circuit is almost identical with that of Fig. 3, except for the positioning of R1 and R2. Note, however, that the NOR gate circuit needs positive-going trigger pulses, while the NAND circuit needs negativegoing pulses, and that the set pulse is applied to IC 1 b in the NOR circuit, but to IC 1 a in the NAND circuit.


Fig. 5. A CD4011 NAND bistable, pulse triggered.

## Manual NAND Bistable



Fig. 6. Manually triggered NAND bistable.
Fig. 6 shows the manually-triggered version of the NAND-type bistable. Note here that although R1 and R2 are shown as having values of 10 k , they can in fact have any resistance values from a few thousand ohms up to about 10 M , depending on the precise details of the specific application. This versatility leads to the development of the touch-triggered NAND bistable circuit of Fig. 7, in which R1 and R2 have values of 10M, and the circuit can be triggered by placing any resistance that is significantly less than 10 M (such as finger resistance) across the touch contacts. R3 and R4 are used in this circuit to protect the inputs of the two gates.


Fig. 7. Touch-triggered NAND bistable.

The bistable circuits that we have looked at so far all use same-polarity (either both positive or both negative) trigger signals. In some applications, however, it is necessary or convenient to use opposite-polarity signals to trigger the bistable, and this type of action can be obtained by placing an inverter stage in series with one or other of the normal bistable input terminals. Figs. 8 and 9 show two alternative circuits of this type.


Using opposite-polarity signals to trigger a 4011 bistable, Fig. 8 (above), and a 4001 bistable, Fig. 9 (below).


Fig. 10 shows alternative ways of connecting a 2 -input NAND or NOR gate so that it acts as a simple pulse inverter stage. These circuits are useful in a multitude of applications.


Fig. 10. Using a 2-input NAND or NOR gate as an inverter.

## Basic 2-Gate Astable Circuits

The CD4001 and CD4011 can both be used in a variety of basic 2-gate astable multivibrator circuits. In these circuits the gates are connected as simple inverters, so the two types of IC give identical performances.

## CMOS Astable



Fig. 11. Circuit of the basic 2-gate CMOS astable.
The most basic and useful 2-gate CMOS astable circuit is shown in Fig. 11. This circuit generates a decent square wave output, has excellent thermal stability and operates at about 1 kHz with the comfort values shown. The frequency is inversely proportional to the C-R time constant, so the frequency can be raised by lowering the values of either C1 or R1. In practice, C1 must be a non-polarized capacitor, and can have any value from a few tens of picofarads to a few microfarads. R1 can have any value from about 4 k 7 to 10 M . For variable frequency operation, wire a fixed and a variable resistor in series in the R1 position.

The output of the Fig. 11 astable circuit switches - (when lightly loaded) almost fully between the zero and positive supply voltage levels, but the junction of R1 and C1 is prevented from swinging below zero or above the positive rail levels by the built-in clamping diodes at the input of IC1a. This characteristic causes the operating frequency of the circuit to be somewhat dependent on supply rail voltages. As a rough rule of thumb, the frequency falls by about $0.08 \%$ for each $1 \%$ rise in supply voltage. Typically, if the frequency of this astable is normalised with a 10 volt supply, the frequency will fall by $4 \%$ at 15 volts, or rise by $8 \%$ at 5 volts.

Also, the operating frequency of the Fig. 11 circuit depends somewhat on the transfer voltage value of the individual gate that is used and can be expected to vary by as much as $10 \%$ between individual ICs. The output symmetry of the waveform is also dependent on the transfer voltage value of the IC and, in most cases, the circuit will give a non-symmetrical output. In the vast majority of 'hobby' and other non-precision applications, these deficiencies of the basic astable circuit are of little practical consequence.

Some can be minimised by using the 'compensated' astable circuit of Fig. 12, in which resistor R2 is wired in series with the input of IC 1a. This resistor can have any value between two and ten times that of R1, and its main purpose is to allow the R1-C1 junction to swing freely below the zero and above the positive supply rail voltages during the switching action and thus reduce the dependance of the circuit operating frequency on the supply voltage. Typically, when R2 is given a value ten times greater than R1, the frequency varies by only about $0.5 \%$ when the supply voltage is varied between 5 and 15 volts.


Fig. 12. A compensated astable circuit.
The basic and compensated astable circuits of figs. 11 and 12 can be built with a good number of detail variations. Some of these are shown in Figs. 13 to 18. In the basic astable circuit, for example, C1 alternately charges and discharges via R1. Figs. 13 to 15 show how the basic circuit can be modified to give alternate C1 charge and discharge paths.


Fig. 13. Modifying the circuit to give C1 alternate charge and discharge paths and produce a non-symmetrical output waveform.

Fig. 13 shows one way of modifying the stable so that it gives a non-symmetrical output waveform. Here, C1 charges in one direction via R1 and R2 in parallel, to give a high output, but discharges in the reverse direction via R2 only, to give a low output.


Fig. 14. Controlling the astable's on and off time.

## On/Off Control

Fig. 14 shows how the circuit can be further modified by also wiring a diode in series with R2, so that the ON time of the output is controlled only by R1, and the OFF time is controlled only by R2. These two circuits can be made to give variable outputs by replacing either or both of their timing resistors with a fixed and a variable resistor in series.

## Variable Symmetry

Fig. 15 shows how the astable can be modified to give a variable symmetry or M/S-ratio output, while maintaining a near-constant frequency. C 1 in this circuit charges on one direction via D1-R2 and one half of RV 1 , and in the other direction via D2-R1 and the other half of RV1. The M/S-ratio can be varied over the range 1:10 to $10: 1$ via RV1.


Fig. 15. Controlling the mark/space ratio.
Fig. 16 shows the circuit of a multi-tone push-button activated astable. Normally, when all push-button switches are open, R5 holds the input of IC 1a (and thus the output of IC1b) low. Resistors R1 to R4 all have values that are low relative to R 5 , so the circuit acts as a normal astable when any one of the push-button switches is closed. This circuit can be used in multi-tone musical instruments and gadgets, etc. and has the major advantage that it draws negligible current when in the standby mode. There is no limit to the number of push-button switches that can be used with the circuit.


NOTE:


Fig. 17. Frequency modulation of an astable.

## Frequency Modulation

Fig. 17 shows how the astable can be subjected to frequency modulation or voltage control of frequency by simply feeding the FM or voltage-control signal to the input of IC1 a via a resistance that is much larger than R1 and Fig. 18 shows how the circuit can be further modified to act as a special-effect voltage-controlled oscillator that shuts off when the input voltage falls below a pre-set value.


Fig. 18. Using an astable as a voltage-controlled oscillator with an output cut-off.

Gated 2-Gate Astable Circuits


Fig. 19. A NAND astable with a normally-low output, gated by a high input signal.

All of the astable circuits of Figs. 11 to 15 can be modified for gated operation, so that they can be turned on and off via an external signal, by simply using a 2-input NAND or NOR gate in place of the inverter in the IC1a position and applying the input control signal to one of the gate input terminals. The CD4001 and CD4011 ICs can both be used in this type of application, but give quite different types of gate control and output operation. Figs. 19 and 20 show the two basic. versions of the gated astaile circuit.


Fig. 20. A NOR astable with a normally-high output, gated by a low input signal.

Note that the Fig. 19 NAND astable circuit has a. normally-low output and is gated by a high input signal, while the fig. 20 NOR astable has a normally-high output and is gated by a low input signal. Also note that, although $R 2$ is shown in the diagram as having a value of $10 \mathrm{k}, \mathrm{R} 2$ can in fact have any value in the range 10 k to 10 M and can be omitted altogether if the gate signal is applied from a preceeding logic state.

Note in the Fig. 19 and 20 circuits that the output signal terminates immediately the input gate signal is removed. Consequently, any noise present at the gate terminals of these circuits also appears at their outputs.


Fig. 21 (above) and Fig. 22 (below) overcome the problem of noise appearing at the gate terminals.


Figs. 21 and 22 show how the circuits can be modified to overcome this defect. Here, the gate signal of IC1a is derived from both the outside world and from the output of IC1b via diode OR gate D1-D2-R2. As soon as the circuit is gated from the outside world via D 2 the output of IC1b reinforces the gating via D1 for the duration of one half astable cycle, thus eliminating any effects of a noisy outside world signal. The outputs of the circuits are complete numbers of half cycles. Note that R2 is an essential part of these circuits.


Fig. 23 (top) and Fig. 24 (above) show manually-triggered astables with noise-elimination networks.

Figs. 23 and 24 show manually-triggered versions of the Fig. 21 and 22 circuits. These circuits are of particular value when they are used as low speed clock generators, operating at about 5 Hz : when PB1 is briefly stabbed, the generate a single clean clock pulse: when PB1 is held down, they generate five clean clock pulses per second.

Clock Generator Circuits


Fig. 25. Speeding up the rise and fall times of the astable output to produce clean clock signals.

The 2-gate astable circuit is generally not suitable for direct use as a clock generator with fast-acting counting and dividing circuits. Such circuits require the use of clean clock signals, with fast rise and / or fall times. The problem is that 2 -gate astables designed around ' $A$ ' series or non-buffered CMOS produce clock outputs with rather slow rise and fall times, whereas 2-gate astables designed around buffered-output 'B' series CMOS produce outputs with good rise and fall times, but tend to produce 'dirty' clocking if there is the slightest trace of noice on their power supply lines

Fortunately, these problems can easily be overcome by wiring a couple of inverter-connected gate stages in series with the output of the astable circuit, as shown in the example of Fig. 25. These inverter stages speed up the rise and fall times of the astable output waveform and also produce effective level shifting between the output of the astable and the clock input terminal of any external device, thereby reducing or eliminating the effects of noise on the clock circuit.

## The Ring-of-Three Astable Circuit



Fig. 26. The 'ring of three' astable circuit produced a very clean output waveform.

An alternative way of making a clock generator is to use the 'ring-of-three' astable circuit of Fig. 26. This circuit is similar to the basic circuit of Fig. 11, except that the positions of R1 and C1 are transposed, and the inverting input stage (IC1a) of the Fig. 11 circuit is effectively replaced by an ultra-high-gain non-inverting stage (comprising IC1a and IC1b in series) in the Fig. 26:
circuit. Because of the very high gain of its composite input stage, the Fig. 26 'ring-of-three' circuit produces a very clean output waveform, with excellent rise and fall times, and is directly suitable for use as a clock generator.

The 'ring-of-three' astable circuit can be subjected to all of the basic design variations shown for the 2-gate astable. For example, C1 alternatively charges and discharges via R1 in the same way as in the Fig. 11 circuit, so the circuit can be subjected to all of the variations shown in Figs. 13 to 15 . It can be designed in either basic or 'compensated' versions, etc.


Fig. 27. A gated NOR 'ring of three' circuit with a normally low output, gated by a low input.

The 'ring-of-three' circuit offers interesting possibilities when it is used in the gated mode, because it can be gated on and off via either its IC1b or IC1c. stages. Figures 27 to 30 show four variations on this theme.


Fig. 28. A gated NOR 'ring of three' circuit with a normally high output, gated by a low input.

Figs. 27 and 28 show alternative versions of the gated NOR-type 'ring-of-three' circuit. Both circuits need a 'low' signal to gate the astable on. Note that the output of the circuit is normally-low if the gate signal is applied to IC1c, or is normally-high if the gate signal is applied to IC1b.


Fig. 29. A gated NAND 'ring of three' circuit with a normally low output, gated by a high input.


Fig. 30. A gated NAND 'ring of three' circuit with a normally high output, gated by a high input.

Similar variations are found in the NAND version of the gated 'ring-of-three' circuit, as shown in Figs. 29 and 30. These circuit need a 'high' signal to gate them on, and have a normally-low output if the gate signal is fed to IC 1 b , or a normally-high output if the gate signal is fed to IC 1 c .

Monostable Multivibrator Circuits


Fig. 31. A 2-gate NOR monostable multivibrator.


The CD4001 and CD4011 can both be used to make an exceptionally useful type of 2 -gate monostable multivibrator or pulse generator circuit. The two basic versions of this circuit are shown in Figs. 31 and 32. In these circuits the duration of the output pulse is determined by the values of R1 and C1, and approximate one second per microfarad of C1 value when R1 has a value of 1 M 5 . In practice, C 1 can have any value from roughly $100 p$ to a few thousand $u$, and R1 can have any value from about 4 k 7 to 10 M .

One outstanding feature of these circuits is that the input trigger pulse or signal can be direct coupled and has no appreciable effect on the length of the circuit's output pulse: the trigger pulse can be shorter or longer than the output pulse. The NOR version of the circuit has a normally-low output, and is triggered by a positivegoing input pulse, while the NAND version of the circuit has a normally-high output and is triggered by a negative-going input pulse.

A signal feature of these circuits is that the pulse signal appearing at point " $A$ " has a length that is equal to that of either the output pulse or the input trigger pulse, depending on which is the greater of the two. This feature is of value when making pulse-length comparators and over-speed alarms, etc.

The Fig. 31 and 32 circuits have only two significant defects. One of these is that the pulse length depends somewhat on the transfer voltage value of the individual IC that is used in the circuit. The other is that the pulse length also depends somewhat on the supply voltage value that is used with the circuit, just as the operating frequency of the basic 2-gate CMOS astable varies slightly with the supply voltage value. These defects are of little consequence in most practical applications, however.


If a number of the Fig. 31 and 32 circuits are to be interconnected to give cascaded delays (as in a delayed-pulse generator, for example), an inverter stage must be interposed between the outputs and inputs of successive monostables, to give correct-polarity trigger signals. Figure 33 shows the basic system.


## Alarm Call Sound Generator Circuits

A single CD4001 or CD4011 IC and one or more transistors can readily be used to make a variety of types of very useful alarm call sound generator circuits. Figs. 34 to 41 show some practical circuits of this type. In all cases, the circuits can be powered from any supply in the range 5 V to 15 V and can be used with any speaker in the range 3 R to 100 R . Output powers range from tens to hundreds of milliwatts, depending on speaker impedances and supply rail voltages used, but can readily be boosted to tens of watts by using additional transistor power-boosting stages.


Fig. 34. Circuit of a NOR latching monotone alarm call generator.
Figs. 34 and 35 show two versions of a latching monotone alarm call generator. IC 1 a and IC 1 b are wired is applied to the circuit the IC1a-IC1b bistable selflatches and switches on the $1 \mathrm{C} 1 \mathrm{c}-\mathrm{IC} 1 \mathrm{~d}-1 \mathrm{kHz}$ astable tone generator. The circuit can be reset to the OFF state by momentarily closing PB1.


Fig. 35. Circuit of a NAND latching monotone alarm call generator.


Fig. 38. Generating a pulsed-tone signal with 6 Hz and 1 kHz NOR astables.


Fig. 39. Generating a pulsed-tone signal with 6 Hz and 1 kHz NAND astables.


Fig. 37. A NAND alarm call generator with auto turn-off.
The Fig. 38 and 39 circuits generate a pulsed-tone signal, in which a 1 kHz astable (IC1c and IC1d) is gated on and off by a 6 Hz astable (IC1a and IC1b) when a suitable control signal is applied to the input terminal of IC1a.

Finally, Fig. 40 shows a warble-tone generator, which switches through a 2-tone cycle once per second when a suitable control signal is applied to the inputs of IC1a and IC1c, and which generates a sound similar to a British police car siren. The depth of frequency variation of the circuit is determined by R3, which can have any value in the ăpproximate range 120 k to 1 MO . ETI


Fig. 40. A warble-tone generator - sounds like a police car siren.


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## Hi-fi 79 at the Cunard Hotel attracted Ron Harris this month, as did a new record cleaner. Also a good chance to show how witty you are and win a free subscription.

A TALE OF MANY speakers is what the 1979 Spring hi-fi show turned into. Wandering the halls of the Cunard in search of the sonic grail you get buffeted from side to side by the alternate blasts of sound emanating from the demo rooms. After about two hours of solid listening 1 start to get ear fatigue and thingd son't seem the same somehow.

In consequence things get done in bursts of two hours at a time punctuated with clincking of refreshments. On the first pasś this year it became apparent that it was to be the Year of the Cone.

## MA24U

Monitor Audio first. The MA2 is a 'domestic reference design and stands some 850 mm high. (About 33 in in English height). It will handle around 100 W of programme power, and produces a very nice sound indeed. At about $£ 300$ the pair they are going to give the competition a tough time.

Wharfedale have extended their ' $E$ ' series upwards into an E90 design which is twice the size of the E70 nearly and more than twice as imposing. We've got no photographs of the beast simply because Wharfedale hadn't got any and haven't kept their promise to send us any since! So there. Its still a nice speaker anyway.

KEFs contribution to the herd was a small one. Tiny in fact. I'd go so far as to say it was so small I almost missed it. The Reference 101 is a bookshelf speaker that just might fit into a bookshelf. This was the real surprise of the show, however, as upon first encounter the almost universal reaction was to hunt the 105s that were not hiding behind the curtains.

The sound was open and spacious with good imaging and a convincing bass response. Very nice one Kef.

## Celestions Follies

The Celestion stand was dominated by two huge double boxes which, when energised, did a quick 'room empty' job. The efficiency is somewhat high you see, and the amplifier somewhat powerful.

I think they're designed for PA and studio usage but they are finished in wood veneer and more than likely quite a few dozen will end up in living rooms. Big living rooms I hope. At their price and size they come up against things like the JBLs and for sound quality I personally prefer the P1s (that's what they're called by the way). Well worth the listen if you're in that market.

Above: the Monitor Audio MA2 loudspeaker. A highly recommended domestic design.

Below: the Celestion P I. It sounds as imposing as it looks.


Left: JVCs KDA8 computerised cassette deck. It fixes up its own own bias and equalisation levels, and can cope with metal tape.

Right: Goldring headphones! Superex classic CLis, a good smooth sound at a decent price. No, I'm not gonna tell you how much, find out yourselves!
Head Man
New for heads from Goldring is the Suprex headphone range. Amongst the four models they decided to import the Classic C1 - the middle of the group caught my attention most. They possess a nice smoothness to them that could be lived with. And they're comfortable. Koss take note please. Speaking as someone stuck with the habitual earache engendered by ESP 10s the Suprex could be very attractive if for no other reason than that.

On Your Metal
Scotch and JVC between them made an exhibition of the new metal tape formulations and the JVC KDA8 machine to use them. The KDA8 is quite a story in itself really. It sets up for each type offered to it by recording a test tone and optimising bias, sensitivity and equalisation automatically - it even rewinds to the beginning again and all in 25 secs. The demonstration was most impressive - as they usually are - and we hope to do more with the machine in the near future.

Before anyone asks I could find no possible reason to include the beautiful Felicity Kendal in this months Audiophile. She was not at the exhibition nor has she anything to do with any of the products featured here. That being the case I have no reason to mention the lovely lady and therefore I shall refrain.

This here picture advertises Marantz. But we couldn't find the Marantz stand!! Now with a picture like this, there just HAS to be a brilliant, witty, superb caption. But we can't find THAT either, 80 its open to you lot. The best wins a years subscription. Closing date June 30th. Mark envelopes 'Audiophile Caption.'

Below: No this mesn's at the show but it's worth the look anyway. A now record cleaner called a TANTRACK. Two arms are provided to cope with any turntable height, and the finish is a very posh steel and chicme. Availablie from Dorking Systems Ltd, 23 South Streat, Dorking, Surrey. Price £6.25 plus VAT.


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This new addition to our unbeatable selection of bargains is no ordinary LCD watch. It's a slim, multi-function, dual time chronograph alarm watch, no less.

This model will show hours, minutes, seconds, date, day of the week, stop watch, split time, alarm and alternate dual time zone - not all at once, of course. There is also a night light.

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An example of this watch can be seen and examined at our Oxford Street offices.

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| 06FE12 | $12+12$ | 0.254 atch | 1.58 | 50p | 80 FE30 | $30+3$ | l.24act | 4.72 |  |
| 08FE12 | $12+12$ | 0.34 sach | 1.50 | ${ }^{50 p}$ | WhariTom | 9. Voliaen |  |  |  |
| 12 FE 12 | $12+12$ | 0.51 asch | 2.10 | 60p | Avainte 3 | . 5. 6, 8, | 12, 15. |  |  |
| 20 FE 12 | $12+12$ | 0.84 eseh | 2.74 | 70 p |  | $124-12$ | A $15.0-15$ |  |  |
| 50 FE 12 | $12+12$ | $2{ }^{2}$ esch | 3.25 | 70 p | 30 FE 30 | $24+30$ | 14 | 3.55 |  |
| 60 FE12 | $12+12$ | 2.54 asch | 3.98 | ${ }^{85 p}$ | 60FE36 | $24+30$ | 2 A | 4.76 | 85 |
| 80 FE12 | $12+12$ | 3. asch | 4.72 | 1.00 | 80FE36 | $24+30$ | 3 A | 5.95 | 1.15 |
| 06 FE15 | $15+15$ | 0.2h mach | 1.50 | 50 p | 100 Ft 40 | $24+30$ | 40 | 7.10 |  |
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| 12 CE 15 | $15+15$ $15+15$ | 0.44 вach | 2.10 | $60 p$ $70 p$ | FEOC | 686 | 1 A asch | 210 | 60p |
| 20 FE 15 50 FE 15 | $15+15$ $15+15$ | 0.68 bach | 2.74 3.25 | 70p | Fte9 | 969 | 14 esel | 2.74 | 70p |
| S0FE15 60FE15 | $15+15$ $15+15$ | 23 arch | 3.25 3.98 | 85p | FE12 | 120-12 | 14 each | 2.00 | 70 p |
| 80 FE 15 | $15+15$ | 34 日ach | 4.72 | 1.00 | FE15 | 15-0.15 | 1 A mach | 3.25 | $70 p$ |
| 06FE20 | $20+20$ | 0.15 esch | 1.58 | 50p | FE20 | $20-0-20$ | 14 each | 3.25 | 70 p |
| 08FE20 | $20+20$ | 0.24 mech | 1.90 | 50p | 60\%E52 | 26-0.26 | 14 each | 3.98 | 1.00 |
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| 20FE20 | $20+20$ | 0.54 mech | 2.74 | 70p | 60FE0 | 30-0.30 | 1 A asch | 3.88 | 1.00 |
| 50FE20 | $20+20$ | 1.24 erch | 3.25 | 70 p | 1005 F 26 | 26-0-26 | 24 math | 5.15 | 1.15 |
| 60FE20 | $20+20$ | 1.54 日ach | 3.98 | $85 p$ | 100FE30 | $300-30$ | 24 nach | 5.15 | 1.15 |
| 80FE20 | $20+20$ | 24 asch | 4.72 | 1.00 | Ifare36 | 36-0.36 | 2A anct | 5.15 | 1.15 |
|  |  | Yranstormer |  |  | Als cero | - | or Colt |  |  |
| 48 FE 12 66 FE 12 76 FE 12 | $\begin{aligned} & 0-5-12 \\ & 0-6-12 \\ & 0-6-12 \end{aligned}$ | $\begin{aligned} & 4 A \\ & 5 A \\ & 6 A \end{aligned}$ | 3.25 4.00 5.10 | $70 p$ <br> $85 p$ <br> 1.00 | FE01 FE03 FE05 | $\begin{aligned} & 0.1 \text { wiw } \\ & 0.3 \text { winh } \\ & 0.5 m H \end{aligned}$ |  | $\begin{aligned} & 0.26 \\ & 0.26 \\ & 0.30 \end{aligned}$ | $\begin{aligned} & 20 p \\ & 20 p \\ & 20 p \end{aligned}$ |
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Carbon Film
$1 / 2$ watt 1 to 10

| 1/2 watt 47 to 4M7 | E12 values | $\begin{aligned} & \text { en. } 2 p \\ & \text { en } \end{aligned}$ |
| :---: | :---: | :---: |
| $3 / 4$ watt 47 to 10 | E24 values | en. 2p |
| 1 watt 4.710 M | E12 values | ea. 5p |
| Metal Oxide - |  |  |
| $1 / 2$ watt Electrosil TR510 to 1 M$2 \%$ E24 values |  |  |
|  |  |  |
| Metal Fitm |  |  |
| 0.4 watt Mullard MR25 |  |  |
| 5.1 to 300K | 2\%E24 | ea. 5p |
| Wirewound |  |  |
| 1 watt 022 to 39 | E12 values | ea. 15p |
| 2.5 watt 1 to 1 K | E12 values (vitreous) | อ.. 26p |
| 3 watt 1 to 10K | E 12 values | อ.. 16p |
| 7 watt to 10K | E12 values | ea. 16p | 7 watt to 10 K THERMISTORS

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# SOIl PROBE 

Check out the roots scene with this ETI soil probe and have happier, healthier plants.


THIS COMPACT UNIT enables you to accurately check the moisture content of your plants' soil in one simple operation. Its range and sensitivity may be adjusted to complement the most fastidious horticulture and horticulturist. The unit works by measuring the resistance of the water in the soil between two probes and comparing it with a previously selected internal resistance adjustable between 1 k and 250k.

## A Better Buzz

A small 9 volt battery powers the circuit which is built around a few cheap CMOS chips and a low power quad op-amp. To avoid undesirable electrolytic effects at the probes, the resistance bridge is AC
energised. We don't known if the plants like this but we have had no complaints. The probes may be made of any conducting material or just tinned copper
wires placed in the soil a few inches apart and a couple of inches deep. The circuit will tolerate wire leads up to a few feet in length and no special screening is required. A three level comparator whose pass range is internally preset indicates whether the soil is too wet, dry or OK and the required resistance is set by adjustment of a case-mounted potentiometer.

## Construction and Use

If you want to use the case shown in the accompanying photographs, be prepared for some precision work as some of the internal pillars need to be removed and the components and PCB are a very snug fit.

Construction is straightforward provided care is taken and attention paid to the polarity and orientation of the diodes and capacitors. Wire links should be inserted first, note that some of these are mounted under the integrated circuit sockets, followed by the sockets themselves, resistors, capacitors, transistor and diodes. The ICs should be inserted last after the off-board components have been

connected. Also ensure that the flying leads have all been soldered into place and that the LEDs are connected correctly. A short lead, indent or flat on the plastic encapsulation usually indicates the cathode. We used miniature LEDs, two red and one green. However, any desired colour may be used. The prototype also featured a miniature 'keypad' type pushbutton for SW1 though this is only critical if the specified verobox is used. 2 mm sockets were used to connect the probe leads and the power source was a PP3.

In use, the unit is turned on; the probes plugged in, and RV2 adjusted until the OK LED lights. This setting may be noted and recorded on a calibrated scale. As the probes are simple and cheap to make they may be left permanently buried in the soil and a set made for each plant. facilitatingrthe repeatability of measurements


## BUYLINES

All components should be readily available. If you use the PCB they should be as small as possible.


The circuit consists of an AC energised bridge whose two active arms are formed by R11 plus RV2 and the soil resistance between the probes. Its operation may be best understood by reference to the circuit diagram and Fig.1. ICla and IC1b are configured as an astable oscillator whose squarewave output (Fig. lb) clocks IC2a. This signal, inverted by IClc (Fig.1c), clocks IC2b.

The antiphase $Q$ and $\bar{Q}$ outputs of $\operatorname{IC} 2 b$ are buffered by IC4a and IC4b whose outpits (Fig. 1d and 1e) drive the resistance bridge formed by R11 plus RV2 and the soil resistance between the probes. Rll protects the amplifier outputs against inadvertent short circuits.
*The output of IC2a (Fig. 1a) is a squarewave of the same frequency, phase shifted by 90 degrees. This means that the edges of the waveform are coincident with the centre of the squarewave from IC2b (Fig 1d and le) and facilitates phase detection by IC3a and IC3b. When the soil resistance measured between the probes is equal to the resistance of R11 plus RV2, the signalls from IC4a and IC4b will cancel out. However, when an imbalance occurs, there will be an error signal whose phase will depend on whether the soil has a greater or lesser resistance than the other arm of the
bridge. The amplitude of the error signal will also diminish as the bridge approaches balance (Fig. 1f).

This signal is coupled via C5, R10 to amplifier IC4c and squared up to provide CMOS input levels by schmitt trigger IC4d, where it is input to IC3a and IC3b and clocked in by the signal from IC2a. The outputs of IC3a and IC3b will follow the phase of the input; reflecting the state of imbalance of the bridge, and either LED 1 or LED 3 will be lit (Fig. 1g).

The amplified signal from IC4c is also fed via C3, D1 and D2 to C2 which will acquire a charge proportional to the level of the input. This drives Q1 which controls the direct, clear, and set inputs of IC 3a and IC3b respectively. When the input signal is insufficient to turn on Q1, these inputs are driven to their active high state by R3.

This causes both LED 1 and LED 3 to extinguish and the condition (shown shaded in Fig. 1g) is detected by nand gate ICId whose output goes low causing LED 2 to light. The sensitivity of the circuit to this condition is preset by adjustment of RVI which controls the gain of IC4c. The required soil resistance is set by RV2. The circuit is powered from a 9 V battery decoupled by C6. A mid voltage point is provided by R12 and R13 decoupled by C4.

Fig. 1. Waveforms associated with the ETI Soil Moisture indicator, resulting in an LED display of whetper the soil is wet, OK or dry.

HOW IT WORKS

| PARTS LST |  |
| :---: | :---: |
| RESISTORS |  |
| R1, 2, 6 | 820R |
| R3, 4, 10 | 100k |
| R5 | 10M |
| R7, 12, 13 | 10k |
| R8 | 1 M |
| R9 | 100R |
| R11 | 68R |
| POTENTIOMETERS |  |
| RV1 | 470k preset |
| RV2 | $250 k \mathrm{lin}$ |
| CAPACITORS |  |
| C1 | 1n |
| C2 | $4{ }^{4}$ |
| C3 | 10u |
| C4 | 22u |
| C5 | 220u |
| SEMICONDUCTORS |  |
| IC1 | 4011 B |
| IC2, 3 | 4013B |
| IC4 | LM324 |
| Q1 | BC108 |
| D1, 2 | IN4148 |
| LED 1, 2, 3 | $0.125^{\prime \prime}$ |
| MISCELLANEOUS |  |
| PCB |  |
| SW1 | SPST |
| VERO BOX |  |



An internal view of the Soil Moisture Indicator, showing the position of the four ICs.


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## STEREO FUNCTION MODULE CP-FG 1

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CP-FG1 - £13.25 inc. (U.K.). £15.25 incl. (Export).
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## 

## What to look for In the August Issue: On sale July 6ih

## STRING THING

To call this project an electronic piano would be an injustice. To call it a string ensemble likewise fails to explain all the mysteries and beauties awaiting the builder once this beast is activated. Yes it can be a piano. Yes it can play string sounds.

The designer (Tim Orr who also can be blamed or praised for the Transcendent 2000) wanted to call it a "Digital Multi-

Voice String Synthesising Keyboard Instrument'. But we wouldn't let him. We couldn't think of a better title ourselves, but we still wouldn't let him. It's the way we are.

Being fitted with a CCD choraliser allows our String Thing to sound like several of 'em at once. Why not tune in and be amazed next month?


## BENCH AMPLIFIER

One for the workshop or table top. How many times have you been half-way through a project and needed to test something, somehow, somewhen. And that of course is exactly when it occurs to you that there is nothing around suitable.
A bench amp is worth its weight in soldering ten times over, and if you DON'T build this you will regret it.

## MICROSENSE

MPUs are definitely for you. Oh yes they are, don't give me that old line about them being all covered in mystery and incomprehension. MPUs are nice friendly little chips, and next month we've got the definitive article to prove it. Based on a book by John Miller Kirkpatrick it takes you through the subject from scratch in a thorough but light-hearted manner.

## LED AUDIO DISPLAY

A really lovely little design to amaze, astound and hypnotise the entire universe. This project takes the input from your hi-fi or TV or budgie and turns it into a dazzling and bemusing shifting pattern of light upon a LED matrix.

Build it any size you like it'll add a bit of visual spice to the hi-fi rack - or simply keep mother-in-law quiet while you nip off down the local.

| ZENER DIODES ( 400 mW )2.7V 1033 V |  |  | 8 p | OPTO/ oisplar | LIMEARS |  |  | $\begin{aligned} & 18 p \\ & 60 p \end{aligned}$ | $\begin{aligned} & 74165 \\ & 74166 \end{aligned}$ | $\begin{aligned} & 36 p \\ & 75 p \end{aligned}$ | $\begin{aligned} & 4048 \\ & 4049 \end{aligned}$ | $\begin{aligned} & 50 p \\ & 25 p \end{aligned}$ | $\begin{aligned} & \text { BC147 } \\ & \text { BC149 } \end{aligned}$ | 8p | $\begin{aligned} & 8 f 115 \\ & 8 F 167 \end{aligned}$ | $\begin{aligned} & 35 p \\ & 25 p \end{aligned}$ | 51P33 TIP34A | $\begin{aligned} & 60 \mathrm{p} \\ & 40 \mathrm{p} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 710CM |  | 30p | 7444 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 2 5 5777 50p | 741.8 | 22 p | 7445 | 64 p | 74173 | 80 p | 4050 | 25p | BC157 | 8 | Bf 173 | 20p | TIP354 | 230 p |
|  |  |  |  | OCP7.1 70p | 7476-14 | $45 p$ | 7446 | 50p | 74174 | 60p | 4066 | 35 p | BC158 | 8 p | 8 F 178 | 27p | TIP36A | 290p |
| VERO BOAROS (0.1" Copper) |  |  |  | ORP12 70p | $748 \mathrm{C}-8$ | 30 p | 7447 | 50p | 74175 | 36 p | 4069 | 12p | 8C159 | 8 p | Bf 179 | 25p | TIP4IA | 60 p |
| $2.5^{\prime \prime} \times$ |  |  |  | $51 p$ | 02704 100p | CA3011 | 80 p | 7448 | 50p | 74176 | 50 p | 4070 | 12p | BC168 | 8 p | BF180 | 8 p | T1P42A | 60 p |
| $3.75{ }^{\prime \prime} \times 5^{\prime \prime}$ |  |  | 60p | 01707 100p | CA3018 | 80 p | 7450 | 10p | 74177 | 50 p | 4071 | 12p | 8 C 170 | 8 p | BF181 | $16 p$ | T1P2955 | 65 p |
|  |  |  | . $125^{\circ \prime \prime}$ \% $2^{\prime \prime}$ | CA3028A | 85 | 1451 | 12 p | 74180 | 20 p | 4012 | 12p | BC171 | 8 p | BF182 | 20 p | TIP3055 | 55p |  |
|  |  |  |  | LED: | CA3036 | 120p | 7453 | 12p | 74181 | $66 p$ | 4073 | 16 p | 8C172 | 8 p | Bf 183 | $20 p$ | $27 \times 108$ | 12p |
|  |  |  |  | Red ${ }^{\text {dp }}$ | CA3046 | 75 p | 7454 | $10 p$ | 74182 | 25p | 4081 | 14p | $8 \mathrm{C173}$ | 6 p | 8F184 | 20p | $27 \times 109$ | 12p |
| RESISTORS (1/4 watt) <br> 10 ohms to 1 Mahm |  |  |  | 1p | Green 13p | ca3054 | 110 p | 7460 | 14 p | 74190 | $36 p$ | 4082 | 14 p | 8C182 | 8 p | 8F185 | 20 p | $21 \times 300$ | 14 p |
|  |  |  | Yellow 13p |  | СА3080 | 70p | 1470 | 16p | 74191 | 70p | 4086 | 60 p | BC183 | 8 p | BF194 | 8 p | 210500 | $16 p$ |
| PRESETS [Horizontal] |  |  |  | 125"c11p 3p | CA3140E | 51 p | 7472 | $20 p$ | 74192 | $25 p$ | 4510 | 60 p | BC184 | 9 p | BF196 | 8 p | 2N706 | 10 p |
| 100 ohm to 1 Mobm |  |  | 5p | $2^{\prime \prime} \quad \text { Clip }$ | Lm301an | 28p | 7473 | $12 p$ | 74193 | 60 p | 4511 | 70 p | BC186 | 19p | BF197 | 8 p | 2N1131 | 15p |
|  |  |  | Lm308H |  | 64 p | 7474 | 12p | 74194 | 55 p | 4516 | 64 p | BC187 | 19p | BF 198 | 8 p | 2N1132 | 24p |  |
|  |  |  |  |  | Lm380M | 61 p | 1475 | 25p | 74195 | 50 p | 4518 | $65 p$ | 8C207 | 8 p | BF200 | 33p | 2W1302 | 38 p |
| POTENTIDMETEAS (carbon) <br> I Konta to 2 Mohess log.linear |  |  |  | $\begin{aligned} & 22 p \\ & 50 p \end{aligned}$ |  | LM381\% | 120p | 7476 | 25p | 74196 | 50 p | 4520 | 65 p | BC212 | 10p | BF224 | 18 p | 2 W 1304 | 50 p |
|  |  |  |  |  | ME555 | 25 p . | 1480 | 20p | 74197 | 32p | 4528 | 80 p | BC213 | 10 p | BF257 | 14p | 2W1305 | 40 p 380 p |
| 5 Kohm to 1 Mohm $\log$ with switch |  |  | DIODES |  | HE556 | 60 p | 1485 | 60 p | 74198 | 100 p |  | ap | 8 C 214 | 10 p | BF258 | 28 p | 2 W 1306 | $38 \mathrm{p}$ |
|  |  |  |  | BY127 10p | T84641-811 |  | 7486 | 10 p | 74199 | 90p | TRANSI |  | 8 C 237 | 15p | 8 8259 | 15p | 2 W 1308 | 50p |
| CERAMIC CAP (5OV) |  |  |  | 0447 8p |  | 200p | 7490 | 25p |  |  | ${ }_{\text {AC }} 126$ | 17p | ${ }^{8} \mathrm{C} 238$ | 15p | 8 FR39 | 18 p | 2 N 1613 | 18p |
| 22pF to 50,000.pf |  |  | 3p | $0 \mathrm{A91}$ 8p | T84800 | 70p | 7491 | 25p | CMOS |  | ${ }_{\text {ACl }} 127$ | 17p | 8 8301 | 25p | BFR40 | 18p | 2 N 1711 | 20p |
|  |  |  | 0 A 200 6p | tbabio | 100p | 7492 | 15p | 4000 | 12p | ${ }_{\text {AC }} 128$ | 17p | 8 C 303 | $25 p$ | BFR79 | 18p | 2 W 1893 | 25p |  |
|  |  |  | 0 A 202 9p |  |  | 7493 | 15 p | 4001 | 12p | 128/176 |  | BC328 | 16p | BFRBO | 22p | 2 L 2217 | 24 p |  |
| POLYEStER CAP [250y |  |  |  | IM4148 4p | ITL |  | 7494 | 25p | 4002 | 12p | \#P | 35p | BC338 | $16 p$ | BFx 29 | 20p | $2 \mathrm{2N219}$ | $21 p$ |
| .01, .015, .022, 033, .047, .068, . 1 uf |  |  |  | 5p | 1 N 916 5p | 7400 | 10p | 7495 | 25p | 4006 | $68 p$ | AC141 | 24p | 8 C 547 | $11 p$ | BF×30 | 32p | 2N2369 | 10p |
|  |  |  | 6p | 1144001 4p | 7401 | 10p | 7496 | 25p | 4007 | 14p | ${ }^{\text {AC }} 142$ | 18 p | BC548 | $11 p$ | BF×85 | 20p | 2 N 2484 | 18 p |
|  |  |  |  | 12p | 1\%4002 4 P | 7402 | 10 p | 7497 | 120p | 4008 | 64 p | AC151 | 2p | BC549 | 11p | $8 \mathrm{~F} \times 86$ | 27p | 2N2905 | 22 p |
| $\begin{aligned} & 1 \quad \mathrm{uF} \\ & 2.2 \mathrm{uF} \end{aligned}$ |  |  | 15p | IN4003 5p | 7403 | 10p | 74100 | 40p | 4009 | 25p | ${ }^{\text {AC153 }}$ | 22p | BC557 | 11p | BF $\times 87$ | 20 p | 2 N 2906 | 10 p |
|  |  |  | 20p | 1 144004 6p | 7404 | 12p | 74105 | 40p | 4010 | $35 p$ | AC176 | 16 p | $8 \mathrm{Cr30}$ | 60p | BFY50 | 15p | 2 N 2907 | 12p |
| $2.2 \mathrm{uF}$ |  |  |  | 114005 7p | 7405 | 12p | 74107 | 10p | 4011 | 12p | ${ }_{\text {AC }} 187$ | 23 p | 8 CY 34 | 66p | $8 \mathrm{FY51}$ | 15p | 2 N 2926 | 10 p |
| ELECTRDLYTIC CAP $25 \%$ |  |  |  | IM4006 8p | 7406 | 12p | 74109 | 30p | 4012 | 12p | AC188 | 20p | BCY59 | 16 p | BFY53 | 17p | 2 W 3053 | 15p |
|  |  |  |  | 1 144007 9p | 7407 | 24 p | 74110 | 46 p | 4013 | 30p | A0149 | 65p | 8 CY 70 | 14 p | BSX19 | 20p | 2 W 3054 | 50 p |
| 68 uF, 100 uF |  |  |  | 6p | 1 115400 13p | 7408 | 12p | 74118 | 75p | 4014 | 60 p | 40161 | 35p | 8 Cr 71 | isp | BSx20 | 18p | $2 H 3055$ | 50p |
|  |  |  | 68 uF, 100 uF 150 uF |  |  |  | 1155401 14p | 7409 | 12p | 74121 | 20p | 4015 | 50p | 00162 | 35 p | 80115 | 30 p | 8 U 205 | 130p | 2 W 3702 | 8 p |
|  |  |  |  |  |  |  | 1\%5402 15p | 7410 | 12p | 74122 | 20p | 4016 | 30 p | AF114 | 23p | 80121 | 70p | Bu208 | 150p | 2 W 3703 | 8 p |
| 220 uF |  |  |  | 1月5404 20p | 7411 | 15p | 74123 | 40p | 4017 | 50p | AF\|18 | 30p | 80123 | 60p | OC25 | 76p | 2 F 3704 | 8 p |
| 330 uF 11 |  |  |  |  | 7412 | 15p | 74125 | 35p | 4018 | $55 p$ | AFi25 | 22p | 80124 | 77p | OC28 | 70p | 2N3706 | 8 p |
| $\begin{aligned} & 470 \mathrm{uF} \\ & 1000 \text { uF } \end{aligned}$ |  |  | $14 p$ |  | 7413 | 25p | 74126 | 35p | 4019 | 40p | AF126 | 22p | 80131 | 35p | 0 C 35 | 70p | 2H3707 | 8 p |
|  |  |  | 22p |  | 7414 | 45p | 74132 | 45p | 4020 | 50p | AF127 | 22p | 80132 | 35p | 0C71 | 16p | $2 \text { 24 } 3710$ | 8 p |
|  |  |  |  | 7416 | 24p | 74141 | 35p | 4021 | 60p | AFI39 | 32p | 80135 | 30p | 0C72 | 32p | 2N3711 | ${ }^{8} \mathrm{p}$ |  |
|  |  |  | voltage <br> REGULATORS | 7417 | 24 p | 74142 | 180 p | 4022 | 50 p | AF186 | 54 p | 80136 | 30 p | 0 C 84 | 42p | 2N3772 | 100p |  |
|  |  |  | 7420 | 12p | 74145 | 30p | 4023 | 12p | AF239 | 40p | 80137 | 30p | TIP 29 | 40p | 243713 | $280 p$ |  |  |
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|  |  |  |  | 320H-24 40p | 7422 | 15p | 74151 | 45p | 4025 | 12p | ASY54 | 33p | 80139 | 30 p | TIP31 | 45p | 2 N 3904 | 8p |
| DIL SOCNETS ${ }^{\text {a }}$ ( BRIUGE |  |  |  | 7805 60p | 7427 | 10p | 74153 | 45p | 4021 | 30p | ASY55 | 33 p | 80140 | 30 p | T1P32 | 45p | 2N4061 | 12p |
| 8 pin | 10p | hectifier |  | 7812 60p | 7428 | 25p | 74154 | 25p | 4028 | 45p | BC107 | 8 p |  |  |  |  |  |  |
| 14 pin | 12p | 1A/50Y | 22p | 7815 60p | 7430 | 12p | 74155 | 45p | 4029 | 50 p | $8 \mathrm{8C108}$ | 8 p |  |  |  |  |  |  |
| 16 pill | 13p | 14/100V | 24p | 7818 60p | 7432 | 10 p | 74156 | 25p | 4030 | 30 p | 8 8C109 | ${ }^{8 p}$ |  |  |  |  |  |  |
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## IBM 3740 COMPATIBLE DISC SYSTEM

The twin drives and controller are housed in a metal saddle maintaining an integrated configuration, one of the major features of the PET. Connection is via the PET memory expansion port and the system comes complete with a PROM which boots the disc resident P-DOS into RAM. Control of the disc system via PET BASIC USR instruction with simple commands from either the keyboard or under program control.

## COMPLETE SYSTEM $£ 1,900$

Other accessories: Saddle conversion package $£ 180$, S100 Buff expansion £96, Voice recognition £176, Voice response $£ 182$, Robot control $£ 236$; Quum Printer £1,400.

The following disc system commands are available LOAD, SAVE, CREATE, DELETE and CATALOGUE

The file management system provides for up to 8 files to be opened concurrently. Files can be opened in READ, WRITE, UPDATE and
APPEND mode. The user may write his own disc system modules to expand the facilities of the disc resident system


# LIFE OUT THERE? 

Is there anybody there? Does anyone care? Yes to both. Read on . . .

ABOUT 20 YEARS AGO scientists, realised that their equipment might be able to detect suitably powerful radio emissions from intelligent beings on planets in other solar systems which may be many light years away from us. Attempts to detect Extra-Terrestrial Intelligence (appropriately abbreviated to ETI!) have already been made in the USA, Canada and the USSR without success, but much more work with larger aerials is required to provide workers in this field with a reasonable chance of success.

Apart from the Search for Extra-Terrestrial Intelligence (SETI), drawings and radio signals have been sent into space outside the solar system in the hope that they will eventually be detected and understood by intelligent beings many light years distant. Unfortunately the chances of two way communications with such beings are very remote, since the nearest star is a few light years away and most planetary systems are at much greater distances. Thus anyone sending a message from the earth to anywhere but one of the very nearest of the stars would be dead by the time any reply could be returned to the earth.

Attempts have also been made to detect signs of life within the solar system. In particular, the Viking spacecraft which landed on Mars conducted prolonged tests
to try to detect life or the chemicals associated with life. Although no organic molecules that could be the past or present constituents of living things were found and the results were generally rather discouraging, they were certainly not conclusively negative as regards the possibility of life on Mars.

## Communication Techniques

It seems likely that there are three possible ways in which we may be able to communicate with intelligent beings from outside the solar system. The first way involves a direct meeting of space vehicles or a landing by them on the earth. Unless the other beings have a longevity which far exceeds that of man, the journey time would make this method quite impossible. Many people do not fully appreciate how much vaster are the distances involved in interstellar space than those within the solar system. Light takes about 8 minutes to reach us from the sun, but about 180000 years to cross our galaxy and some thousands of millions of years to reach us from the farthest known objects.

As we require something which will convey information quickly, the obvious thing to use is electro-magnetic


Fig. 1. Some of the most important factors which determine the choice of listening frequency. As signals from other stars would be very weak, it is important to choose a frequency where the natural background noise is relatively small. Most SETI work has been done in the relatively low total noise region of 0.5 to 10 GHz , christened the 'Water Hole', since it contains frequencies strongly associated with water. The favourite frequency is 1.42 GHz, emitted when the electron in a hydrogen atom flips over, reversing its direction of spin.

The noise contributions shown are - the 2.76 K cosmic background radiation (remnants of the big bang), atmospheric noise (as water and oxygen absorb and reradiate energy), quantum noise associated with the arrival of each photon in the atmosphere and synchrotron radiation emitted by particles spiralling round galactic magnetic fields (the level varies with galactic latitude. The extreme lines shown are for galactic latitudes of $10^{\circ}$ and $90^{\circ}$ ).
signals which travel at the speed . ht. We can only send signals by this technique and $n_{c}$ material objects, but generally it is far more sensible to send information on how to construct an object rather than to send the object itself over such vast distances. Should one use light, infra-red, radio waves or some other form of electromagnetic radiation? Radio-waves are to be preferred, since the energy required per transmitted photon is relatively low.

The third possible communicating technique involves the acceleration of sub-atomic particles to velocities very near to the speed of light, but as far as is known this technique has not yet been tried. If particles which can travel faster than light (known as 'tachyons') are ever discovered, one can only wonder whether they could be used in an extra-terrestrial communications system if they can be produced relatively easily; however, at the moment such a suggestion is nothing more than pure speculation.

It has been suggested that we should avoid transmitting any signals into space which would inform possibly hostile intelligent beings of our location. It is generally. felt, however, that we can take comfort from the fact that any intelligent beings would be more interested in sharing information with us and co-operating with us as far as possible rather than in attacking us as in science fiction stories. In any event, it seems likely that it would take them so long to arrive here that our civilization would be in a very different state by the time they could reach us.

## Basic Problems

Let us first consider the basic problems associated with receiving radio signals from outside the solar system, since any of our attempts to send messages are not likely to bring any result for an enormously long time. Any radio signals reaching the earth from outside the solar system are likely to be extremely weak owing to huge distances involved and it therefore follows that SETI projects require the use of the largest radio telescopes in the world.

One is left with decisions to make on the direction in which one should point the telescope, the frequency or frequencies which one should attempt to receive, the bandwidth one should use and perhaps even the time at which one should attempt to receive any transmissions. In the work on SETI which has been performed up to the present time, the telescopes have usually been pointed towards some star in our galaxy which is not excessively distant and which astronomers feel may possibly have a satellite system on which life could have evolved in some form or other.

In general astronomers have concentrated their searches in the regions of stars of the same or similar spectral classes as the sun. It has been felt that if a star has a luminosity much greater than that of the sun, then the lifetime of any planetary system associated with that star is probably too short to have enabled life to have developed to the point where intelligent civilizations have evolved. Stars of luminosity much smaller than that of the sun seem to have rather violent coronal activity which would probably result in any associated planetary system being rather inhospitable to most imaginable forms of life. Other stars have departed from the main sequence as a result of a super-nova or nova explosion and SETI workers have tended to disregard these
because it seems doubtful whether any living species could survive the catastrophe event of such an explosion in the star.

## Signal Types

What types of signal should we expect to receive from other planetary systems and how could we recognise such signals as originating from intelligent life? The SETI workers are basically searching for coherent signals, possibly modulated. For example, our own radio transmissions have a coherent carrier wave, although the modulation present inevitably involves a finite bandwidth. The presence of this type of signal would almost. certainly indicate it is not of natural origin and hence would imply the existence of intelligent life elsewhere in the universe.

There are three basic types of signal from other planetary systems which we may be able to detect. The first type of signal is leakage of a șignal into space in just the same way that our own radio and television signals leak away to a greater or lesser extent through our ionosphere. Indeed, a spherical wave of radio signals of a fairly wide range of frequencies has been travelling away from the earth over a period of rather over 50 years. In the case of more highly developed societies, it seems probable that they have been transmitting such signals for a far longer period (although one hopes they have not been stupid enough to destroy themselves by nuclear war).

A second type of signal we may possibly be able to receive is some form of inter-stellar or even inter-galactic communications between highly developed communities. Such reception would be by chance and it must be assumed that highly developed communities would employ very high gain antennae which are unlikely to be pointing towards our solar system. Thus the chances of intercepting such messages cannot be regarded as being very high.

The third type of signal we may hope to receive is an intentional one directed at our solar system by a society in a distant stellar system in order to notify us of their presence. It is also possible that such a society may send signals out isotropically (that is, all directions at equal intensities), but unless they have transmitters of extremely high power, such signals would be so weak at the earth that it is doubtful if we could detect them.

It is difficult to make an estimate of the optimum bandwidth one should select for SETI work. Narrow bandwidth receivers (possibly with a bandwidth of a few Hz ) enable very weak signals to be detected, since the narrower the bandwidth of the chănnel used, the less the external noise which can penetrate into that channel. (Someone once said: '"The wider you open the window, the more the amount of dirt that flies in," and this certainly applies to radio bandwidths). Unfortunately if one has a very narrow bandwidth channel, it takes a very long time to examine an appreciable range of frequencies. Modern plans are to use both narrow and wide band search techniques together with spectrum analysers for the simultaneous examination of numerous frequencies by computer techniques.

## The Drake Equation

Before spending millions of dollars on SETI programmes, one would like to have some approximate
estimate of the number of civilizations which are likely to possess the technology to be able to communicate with us. Such an estimate can be obtained by the use of the Drake equation. Professor Frank Drake is one of the leading SETI workers and is now Director of the National Astronomy and Ionosphere Centre of Cornell University. His equation reads:

$$
N=R^{*} f_{p} n_{e} f_{1} f_{i} f_{c} L
$$

where $N$ is the number of existing civilizations possessing the interest and capability for inter-stellar communications
$R^{*}$ is the mean rate of star formation averaged over the lifetime of a galaxy
$f_{p} \quad$ is the fraction of stars with planetary systems
$n_{e} \quad$ is the mean number of planets in each system with an environment favourable for the origin of life
$f_{1} \quad$ is the fraction of suitable planets on which life does develop
$\mathrm{fi} \quad$ is the fraction of life bearing planets on which intelligence together with manipulative abilities appears
$f_{c} \quad$ is the fraction of the planets evolving advanced technical civilzation
$L \quad$ is the lifetime of the technical civilization (perhaps very difficult to estimate!)

The estimate obtained from the use of this equation will obviously vary widely according to the estimated values employed. However, most estimates now place the value of $N$ around one million, these being distributed amongst approximately 500 million stars in our galaxy.

## SETI History

Perhaps the first important paper on SETI work appears in Nature in 1959 under the title "Searching for Interstellar Communications" by Philip Morrison and Guiseppe Cocconi. It is interesting to note that they suggested the use of the 1.420 MHz hydrogen


Fig. 2. On November 16 th, 1974 , the Arecibo telescope was used to transmit a message at 2380 MHz towards the Great Cluster in Hercules, Messier 13, some 25,000 light years away.

The message, 1679 bits long, can be decoded by breaking it into 73 consecutive groups of 23 characters and arranging these groups in sequence under one another as shown. The first piece of information consists of the first ten digits in binary form - the numbering system to be used. It continues with the atomic numbers of five common elements found in living things. Information on sugars and DNA follows, with a sketch of a human being and the solar system, ending with information about the Arecibo telescope.

Encoding information in various types of message poses some interesting problems in order that decoding can be carried out as easily as possible by intelligent remote beings.
frequency, since it is a unique standard frequency which must be known to every observer in the universe.

Eight separate major efforts have been made by US, Canadian and Russian radio astronomers since 1960 to detect extra-terrestrial signals from intelligent beings. Although each search has concentrated on one or more specific frequencies in the range from 600 MHz to 22.2 GHz , the receivers used were those designed mainly for normal radio astronomical work which involves the detection of incoherent naturally produced radiation rather than the coherent radiation the SETI workers were seeking.

Although no confirmed sources of signals from intelligent beings outside the solar system have yet been detected, it has been estimated that the number of stars which have been examined is about $0.1 \%$ of the number which would have to be investigated if there is to be a reasonable statistical chance of detecting extraterrestrial intelligent signals.

## Project Ozma

The first SETI work was led by Frank Drake using the 1420 MHz hydrogen frequency. It was named "Project Ozma' after the ruler of Oz - a far away place populated by exotic beings. Drake employed a bandwidth of 100 Hz and aimed his receiver at the two stars Tau Ceti and Epsilon Eridani which are both some 11 light years away from the earth. The observing time was some 150 hours using a 26 m ( 85 feet) diameter steerable antenna in 1960.

Project Ozma II is a much more extensive one which has also been carried out at the National Radio Astronomy Observatory, Green Bank, West Virginia. In this work some of the largest and most sophisticated radio telescopes in the world have been used; they include the 92 m (300 feet) diameter partially steerable antenna completed in 1962 at a cost of about 1 million dollars ( 500000 pounds) and the 43 m ( 140 feet) diameter
equatorially mounted, fully steerable antenna which was completed in 1965 at a cost of some 14 million dollars ( $£ 7$ million).

Project Ozma II was commenced in late 1972 under the leadership of Benjamin M. Zuckerman of the University of Maryland and Patrick Palmer, of the University of Chicago, the intention being to run the project for about two years. However, the Observatory made more time available and the project continued until December 1976 with an examination of about 700 stars at distances of up to some 65 light years. The prime targets were main sequence stars of the F5 to K5 class. The observations were carried out at 1420 MHz , each of 384 separate receivers being tuned to a slightly different frequency near to the 1420 MHz hydrogen line. A total bandwidth of 3 kHz was used.

At the end of the Project Ozma II work, about 12 stars showed some unexplained phenomena which were probably due to terrestrial radio interference, but which could have been due to faint signals from intelligent beings. These stars will doubtless be examined very carefully at some later date.

## Arecibo

Some SETI work has been carried out using the largest telescope in the world at the Arecibo Observatory in Puerto Rico which has a diameter of 305 m ( 500 feet) in the air. The reflector panels consist of 38,778 individual panels each a little over 1 m by 2 m in size; each pane, must be positioned with an accuracy of better than 1 mm .

In 1967 a British post-graduate student noticed a mysterious regular pulsing signal from space and there was much speculation as to whether this was a signal from intelligent life beaming a message to earth. The Arecibo antenna was used to show that this signal was coming from the first pulsar to be discovered and that it was in the Crab Nebula.


The Goldstone 26 m Deep Space Network Antenna may be used in an all sky search. (Photo by courtesy of Jet Propulsion Laboratory)

Two of the best known SETI workers, Prof. Frank Drake and Prof. Carl Sagan, have used the Arecibo antenna to examine the radiation from whole galaxies for signs of signals from intelligent life. Although the use of this technique has enabled them to examine many millions of suitable types of stars simultaneously, it would require a signal of very great intensity to enable frequencies of $1420 \mathrm{MHz}, 1654 \mathrm{MHz}$ and 2380 MHz , but the time allocated to this work is relatively small.

## Canadian Work

Dr. Bridle and Dr. Feldman commenced work at Canada's nationally owned Algonquin Radio Observatory in Algonquin Park, Ontario in 1974. They are using a 46 m ( 150 feet) diameter telescope to examine many of the nearest sun-like stars, but the frequency employed is 22.2 GHz - the emission frequency of the water molecule - which is much higher than that used by other workers.

## Project Cyclops

One of the most ambitious SETI projects yet proposed is known as Project Cyclops. This is intended to be suitable for not merely detecting high power signals (such as those from our own Arecibo antenna), but also to allow eavesdropping on much lower intensity signals which other civilizations use for their own communications (like our radio and television transmitters). In order to be able to receive such signals from stellar systems at distances of a few hundred light years from the earth, enormous antenna systems are required.

It seems unlikely that it would be a practical possibility to construct a single reflecting dish of adequate size and therefore it has been suggested that the Cyclops project could employ an enormous array of radio telescopes, each of which may be about 100 m in diameter. For example, as many as 1500 such 100 m dishes could be spread out in lines over an area of perhaps $65 \mathrm{~km}^{2}$ and connected together electrically to.
provide the same performance as a single dish of enormous dimensions.

Project Cyclops was initiated as a study by the NASA Ames Research Centre and Stanford University in 1971 under the leadership of Dr. John Billingham and Dr. Bernard Oliver. There have been vast improvements since then in solid state memories, microprocessors, wideband maser low-noise amplifiers, etc.

## Conclusion

The Search for Extra-Terrestrial Intelligence has not yet been successful, but this is not particularly surprising in view of the small number of star systems which have been examined with high sensitivity equipment. Some people (including many of those who control scientific finance) may feel that the SETI project is rather frivolous and perhaps even a silly one. However, there are many scientists very strongly committed to work in this field a point which can be demonstrated by the fact that a new journal, Cosmic Search devoted entirely to SETI work will be published from January 1979 under the editorship of Dr. Robert S. Dixon who is well-known for his SETI work at the Ohio State University Radio Observatory.

Dr. Frank Drake at times feels somewhat cynical about the cuts in the SETI budgets. Indeed, he has commented that the search for extra-terrestrial intelligence begins with the search for intelligence here on earth! He feels that at the present time there is a very well qualified group of people who are keen to carry out an extensive SETI project and, if no funds are forthcoming for a year or more, it is likely that many of thesêe peöple will move to other work. If you were paying taxes in a country considering becoming involved in an extensive SETI project, how would you feel about paying an extra amount (far less in total than that to place a man on the moon) in order that the project could proceed? SETI work will doubtless continue, but more funds are required if it is to proceed at a rate which is likely to bring success within the lifetime of most people who are living today.

ET

An artists impression of a complex Cyclops array on the far side of the moon containing 216 large ( 200 m diam.) reflecting radio telscopes with a control building in the middle of the array. The lunar base is in the middle distance towards the left-hand side and is quite small.
(Photo by courtesy of NASA Ames Research Centre).


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# TUNER~AMPLIFIER 

## PART TWO: This month we conclude the System 8000 project with the setting up procedure and a description of the digital frequency readout.

THE SETTING UP and alignment must be approached in a systematic fashion.

## Procedure

a) Power Supply
b) Power Amp L \& R
c) Auxilliary
d) Tone Controls
e) Filter Controls
f) Tape
g) Magnetic pre-amplifier
h) FM sections
I) AM
J) Frequency read out module

Before commencing alignment it is necessary to check that:
i) All wiring has been checked and components are correctly positioned and orientated
ii) That there are no solder bridges
iii) A good multimeter is also required

## Power Supply

Remove all fuses except for the mains fuse. Switch on, you should
hear the relay click over. Measure from earth to positive and negative on the smoothing capacitors. The voltage should read approximately plus or minus 50 V . Check that regulator reads about 30 V . Switch off.

## Power Amp

Check each power amp in turn, ensure that speakers are switched out. Using a meter, do a resistance check from the case of each power transistor to chassis to ensure that there is no short. Find two high wattage resistors (56R-300R will do) and place in fuse holders of amp being checked.

Switch on volume control (minimum). If there appears to be no problems feel cases of power transistors - should be cool. Switch on speaker. Power transistors may be slightly warm. Now 'Buzz' input pins of the amplifier with your finger. If okay switch off, remove the resistor fuses, insert two amp fuses. Switch on, if everything is okay one can now set RV1.

If you have access to a low distortion audio generator put this on the input and a distortion meter across the speaker sockets using a dummy load. Feed in 100 mV sine wave and set for minimum distortion. Without this test equipment set RV1 to mid travel. Repeat for other channel.

## Tone and Filters

Insert either an audio generator, or any music source such as a tape-recorder, into the Aux. socket. Select Aux. on switchbank, slowly increase volume, and listen to sound, check that the tone controls are working. To check the high and low filters turn the bass control on full and this will emphasise the rumble filter, likewise the treble control will emphasis the scratch filter.

## Tape

If the above is working, check that pressing tape 1 and tape 2 disconnects the Aux. Transfer the tape recorder/audio generator to take 1 and 2 in turn and ensure that



Fig. 1. Component overlay for the power supply board.
pressing the respective switch brings them into circuit. The pre-set resistors are adjusted to match the levels of your own tape recorders otherwise they can be turned full on.

## Magnetic

Using a record player with a magnetic cartridge check that everything sounds okay. Excessive hum indicates an earthing fault.

## FM

Before aligning this section it may be an advantage to set the frequency counter straight away. However, this is not essential. The tuner head is pre-aligned and will not need adjustment. Tune through the band with an aerial connected - ensure that mute and AFC are off. You should hear a continuous hiss, with stations heard between 88 MHz and 95 MHz . If this is so, tune to an area above 95 MHz without stations and adjust using a non-inductive tool L4 until centre zero needle is centred. This should correspond with
maximum hiss level. L3 can only be adjusted ideally if an FM signal generator is used. Generate 100 MHz , attach a distortion meter to pin 6 of the CA3189E, there is a test pin for this, tune for maximum signal strength and adjust L3 for minimum distortion. Re-adjust L4 for centre zero. Adjust L1 for maximum signal level. RV11 is the muting adjustment, and can be set all the way from no mute to absolute quiet between stations - however, do not overset, as the mute may not lift quickly enough when tuning a station.

Move next to the stereo decoder, KB 4437 - either:-tune to a stereo broadcast, set RV6 to the middle of the range that brings the stereo light on, set VC5 and RV7 for mid-way: or:-using a stereo generator, adjust VC5 and RV6 for maximum, set separation at 1 kHz . Observing the 19 kHz component of the multiple signal on a oscilloscope, set RV7 for minimum 19 kHz . This completes the FM

## Amplitude Modulation

The frequency counter can help considerably, and an AM generator is an asset.

MW Tune to minimum volts on varicap line, feed in a 470 kHz signal, peak until there is no improvement, Tune L9 for a 550 kHz station. Move to maximum varicap volts, set CV1 for a 1620 kHz signal. Tune up and down the band checking that $550-1620 \mathrm{kHz}$ is covered without any shifting in noise level. Tune to 600 kHz . Peak L5 and L z for maximum. Tune to 1400 kHz . Peak CV2 and CV4 for maximum. Repeat until there can be no improvement. RV8 is set to give a satisfactory signal level reading on the meter.

LW Switch to LW. Set CV3 so that minimum varicap volts 175 KHz . Tune to 200 kHz (Radio 4) peak L6 and L8 for maximum. If no generator


Fig. 2. Componenf overlay for the tone control board.


Fig. 3. Circuit diagram of the digital frequency meter.

## HOW IT WORKS

A digital frequency readout is both cost effective and an accurate method of displaying the frequency of a radio station. GEM has been developed to interface directly with the tuner sections of the SYSTEM 8000 , and most existing AM/FM receivers.

The principle of operation is simple, and is a progression from the many digital clock ICs. Basically, the oscillator of the radio being 'read' is fed (via buffer stages) into the 5525 , and converted to digital pulses. These are counted by the IC, for a period determined by the external crystal, and the count is fed to the display.

Allowance is made for the IF offset of the radio -470 kHz and 10 k 7 Hz . This offset is externally programmed by the diodes DID6.
In this application, the source for switching from AM to FM is obtained from the switch bank of the System 8000, and uses the positive power line. This is converted from
a 'Hi' to a 'Lo' signal by IC2, a HEX invertor. The beauty is that the buffer stages for the AM/FM oscillators are also switched off when not in use, and thus cannot cause interference.

Because the display would be running when the tuner is not being used. A section of the hex invertor takes an additional 15 V input ( F ) and uses this to reset the counter and thus give a fixed reading. D7 ensures that this signal cannot accidentally exceed 5 V . The unit must be earthed directly to the central earthing point of the system 8000 , otherwise noise may be fed back into the system.

The unit may be used independently of course and requires $\pm 12 \mathrm{~V}$ at least, for operation. If using a supply of lower than $\pm 20 \mathrm{~V}$, omit R10. Maximum supply is $\pm 35 \mathrm{~V}$. Other IF offsets may also be programmed in. It uses a fluorescent display for a good readibility and gives AM/FM and $\mathrm{MHz} / \mathrm{kHz}$ indication.




Fig. 5. Component overlay for the digital frequency meter board.
(Below) The digital frequency meter display and driver board.

is available, the digital frequency counter can be peaked. L11, L10, can be set for maximum output (be careful - small adjustment only)

## Readout

The frequency counter should need no adjustment, however, if another frequency counter is available, the crystal input should be tuned to precisely 6553 k 6 Hz with TC 1.

NB: It has been found in practice that two laminated transformers give excellent regulation and a low hum field, also low voltage taps are available to power the centre zero and signal meter. The metah case will take both torroidal and conventional transformers.

PARTS LIST

| RESISTORS (all $1 / 2 \mathrm{~W}$ 5\%) |  |
| :---: | :---: |
| R1, 10 | 330R |
| R2 | 330 k |
| R3 | 1 M |
| R4 | 100R |
| R5 | 1k5 |
| R6 | 82R |
| R7 | 100k |
| R8, 11 | 1k |
| R9, 13, 14 | 4k7 |
| R12 | 150R |
| CAPACITORS |  |
| C1, 14 | 10 u 16 V electrolytic |
| C2, 10 | 22 n polyester |
| C3, 4, 5, 9, 12 | 1 n polyester |
| C6, 7 | 100 n polyester |
| C8 | 100p ceramic |
| C13 | 100 n 45 V electrolytic |
| C14, 15 | 220 n polyester |
| C17 | 22p ceramic |
| SEMICONDUCTORS |  |
| Q1 | BC107 |
| Q2 | BF394 |
| Q3 | BF256 |
| Q4 | BD 140 |
| IC1 | 5525 |
| IC2 | 4069 |
| IC3 | SP8629 |
| D1-6 | 1 N914 |
| D7 | 5 V 400 mW zener |
| D8 | 10 V 400 mW zener |
| Reg. | 7805 |
| INDUCTORS |  |
| L1 2 | 1 mH |
| MISCELLANEOUS |  |
| TC 1-0-50p, F1-6553k6 H7 X71, 6LT06 display, PCB |  |

$30 /$ to pin (28)
31 / to pin (31)
$\left.\begin{array}{l}32 / \\ 33 /\end{array}\right\}$ to pin (33)
34/ to pin (37)
35/ Earth
$36 /$ to 38 pin
37/ to pin (34)
$38 /$ to $\operatorname{pin}$ (36)
$39 /$ to pin (45)
40/ to pin (46)
41 / to pin (47)
42/ Earth pin 49 and 51
$43 /$ pin 48
44/ pin 50
45/ pin 39
46/pin 40
47/pin 41
$48 /$ pin 43
49/ Earth pin 42
50/ pin 44
51/ Earth pin 42
$\left.\begin{array}{l}52 / \\ 53 /\end{array}\right\}$ to 56 V winding of Transformer
54/ $\}$
55/ $\}^{C}$
56/ to speaker switch L.
57/ to speaker switch R
$58 /\}$
59/
60 / pin 70
61/ pin 71
62/ +45V fuse 66
63 / -45V fuse 67
64/ +45V fuse 68
65/ -45V fuse 69
$66 /$ to 62
67 / to 63
68/ to 64
69/ to 65
$70 /$ to 60
71 / to 61
$\left.\begin{array}{l}72 / \\ 73 /\end{array}\right\}$-to L and R of Head-Phones
74/ -L
75/ -R to FM switch
76/ Earth
$77 /$ on FM switch, to mono switch

78/ +15V
79/ on mono switch, to stereo. LED anode
80/ Earth
81/ to stereo LED
82 8/ \}mono options, disconnected
All other earth connections to tabs of power board-including centre-tap of transformer.

## CORRECTIONS FOR DIGITAL <br> FREQUENCY DISPLAY <br> pin 7-(FM tuner lead) to pin 100 <br> pin (6) -to pin 101

Uni-Electric have sent us the following list of corrections to the parts list and circuit diagrams published last month.

C105 in 100n.
Circuit diagram shows a short from output of 7815 to earth. Omit indicated line.
Switch marked 'rumble" is tape switching. 'Mono' switch, left channel shown connected to earth, via a 470 k resistor. This should be connected to Mono switch via a 1 k resistor.
C67 and C1 50 are 10 uf cápacitors.
C 136 is 470 p. C 137 is 330 p. 10 n capacitor omitted from pin 7 to CFUO50D. C147 is 10 n . R171 is 10 k .
R120 are R121 are $47 k$. Base of Q20 is shown shorted to earth - should be a 47p capacitor here.
R10 is shown connected to the base of Q2. and Q 2 connected to earth. This is wrong. R10 goes to earth and not to 22, R3 is 47R. not 47 k .
Mast head preamp uses 2 not 5 Mosfets. AM coverage is 2 band not 5 band.
Sensitivity is 1.0 uV not 10 V .
In Buylines, the complete kit with metalwork is $£ 165$. Uni-Electric will align the RF sections and check finished mother boards for $£ 15.00$.

Pin Wiring for PCBs



An internal view of the complete unit, ready for the setting up procedure. The digital frequency meter board is top centre.

# STEVENEON Electronic Components <br> REGULATORS <br> <div class="inline-tabular"><table id="tabular" data-type="subtable">
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<td style="text-align: left; border-right: none !important; border-bottom: none !important; border-top: none !important; width: auto; vertical-align: middle; ">$30 p$</td>
<td style="text-align: left; border-right: none !important; border-bottom: none !important; border-top: none !important; width: auto; vertical-align: middle; ">7805</td>
<td style="text-align: left; border-right: none !important; border-bottom: none !important; border-top: none !important; width: auto; vertical-align: middle; ">$60 p$</td>
<td style="text-align: left; border-right: none !important; border-bottom: none !important; border-top: none !important; width: auto; vertical-align: middle; ">$79 L 05$</td>
<td style="text-align: left; border-right: none !important; border-bottom: none !important; border-top: none !important; width: auto; vertical-align: middle; ">$70 p$</td>
<td style="text-align: left; border-right: none !important; border-bottom: none !important; border-top: none !important; width: auto; vertical-align: middle; ">7912</td>
<td style="text-align: left; border-bottom: none !important; border-top: none !important; width: auto; vertical-align: middle; ">$80 p$</td>
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<td style="text-align: left; border-right: none !important; border-bottom: none !important; border-top: none !important; width: auto; vertical-align: middle; ">$30 p$</td>
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</tbody>
</table>
<table-markdown style="display: none">| $78 L 05$ | $30 p$ | 7805 | $60 p$ | $79 L 05$ | $70 p$ | 7912 | $80 p$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $78 L 12$ | $30 p$ | 7812 | $60 p$ | $79 L 12$ | $70 p$ | 7915 | $80 p$ |</table-markdown></div> <br> $78 L 15$ 30p 7815 60p 7905 80p LM72335p <br> <br> HARDWARE <br> <br> HARDWARE MINIATURE TRANSFORMERS <br> <br> 240 Volt Primary <br> <br> 240 Volt Primary <br> Secondary rated at 100 mA . <br> Available with secondaries of <br> 6-0-6,9.0-9 and <br> 12-0-12. <br> 92p. each <br> <br> LOUDSPEAKERS <br> <br> LOUDSPEAKERS <br> 56 mm dia. 8 ohms 64 mm dia. 8 ohms 64 mm dia. 64 ohms <br> 70 mm dia. 8 ohms <br> 70 mm dia. 80 ohms <br> <br> TERMINALS <br> <br> TERMINALS <br> Rated at 10A. Accepts 4 mm plug, black <br>  

TRANSISTORS


| 7415 |  | LS73 | 25p | LS156 | 60p |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LS74 | 25p | LS157 | 48p |
|  |  | LS75 | 30p | LS164 | 65p |
| LSOO | 13p | LS76 | 25p | LS174 | 48p |
| LSO1 | 13p | LS78 | 35p | LS175 | 48p |
| LSO2 | 13p | LS83 | 35p | LS190 | 62p |
| LSO3 | 13p | LS85 | 700 | LS192 | 60p |
| LSO4 | 13p | LS86 | $30 p$ | LS193 | 600 |
| LS08 | 15p | - LS90 | $36 p$ | LS196 | 60p |
| LS10 | 13p | LS93 | 38p | LS251 | 50p |
| LS13 | 28p | LS95 | 450 | LS257 | 50p |
| LS14 | 45p | LS123 | $70 p$ | LS258 | 50p |
| LS20 | 13p | LS125 | 38p | LS266 | 300 |
| LS30 | 13p | LS126 | $38 p$ | LS283 | $60 p$ |
| LS32 | 16p | LS 132 | 60p | LS290 | 60p |
| LS37 | 24p | LS136 | $28 p$ | LS365 | 40p |
| LS40 | 17p | LS138 | 50p | LS366 | 400 |
| LS42 | 400 | LS139 | $50 p$ | LS367 | 40p |
| LS47 | 900 | LS151 | 50p | LS368 | 40p |
| LS48 | 70p | LSi53 | 50 p | LS386 | 35p |
| LS54 | 150 | LS155 | 550 | LS670 | 40p |
| $T \mathrm{~L}$ |  | 7454 | 12p | 74132 | 450 |
|  |  | 7473 | $20 p$ | 74141 | 55p |
|  |  | 7474 | 22p | 74148 | 90p |
|  |  | 7475 | 250 | 74150 | 55p |
| 7400 | 10p | 7476 | 20p | 74151 | 40p |
| 7401 | 10 p | 7485 | 550 | 74156 | 40p |
| 7402 | 100 | 7489 | 1350 | 74157 | 40p |
| 7404 | 12p | 7490 | 25p | 74164 | 55p |
| 7408 | 12p | 7492 | 30p | 74165 | 550 |
| 7410 | 10p | 7493 | 250 | 74170 | 100p |
| 7413 | 22p | 7494 | 450 | 74174 | 50p |
| 7414 | 39p | 7495 | 350 | 74177 | 50p |
| 7420 | 10 p | 7496 | 45p | 74190 | 50p |
| 7427 | 20p | 74121 | 25p | 74191 | 500 |
| 7430 | 100 | 74122 | $38 p$ | 74192 | 500 |
| 7442 | 38p | 74123 | 38p | 74193 | 500 |
| 7447 | 45p | 74125 | 350 | 74196 | 500 |
| 7448 | 50p | 74126 | 35p | 74197 | 50p |
| CMOS |  | 4018 | 55p | 4050 | 25p |
|  |  | 4023 | 12p | 4066 | 35p |
|  |  | 4024 | 400 | 4068 | 18p |
| 4001 | 12p | 4026 | 900 | 4069 | 12p |
| 4002 | 12p | 4027 | 300 | 4071 | 12p |
| 4007 | 12p | 4028 | 48p | 4081 | 13p |
| 4011 | 12p | 4029 | 500 | 4093 | 45p |
| 4013 | $28 p$ | 4040 | 600 | 4510 | 650 |
| 4015 | 50p | 4042 | 500 | 4511 | 65p |
| 4016 | 30p | 4046 | 90p | 4518 | 65p |
| 4017 | 48p | 4049 | 25p | 4520 | 600 |
| FULL DETAILS IN CATALOGUE! |  |  |  |  |  |

## SKTS

## Low profile



8 pin $8 p \quad 16$ pin 11p 23 pin 22p 14 pin $10 p \quad 24$ pin $18 p$ 40 pin $32 p$ Soldercon pins: 100:50p. 1000:370p

## OPTO

LED's 0.125 in . 0.2 in each $100+$ Red TiL209 TIL220 9p 8p $\begin{array}{lllll}\text { Green } & \text { TIL211 } & \text { TIL221 } & 13 p & 12 p \\ \text { Yellow } & \text { TIL213 } & \text { TIL223 } & 13 p & 12 p\end{array}$ $\begin{array}{lllll}\text { Yellow } & \text { TIL213 } & \text { TIL223 } & \text { 13p } & \text { 12p } \\ \text { Clips } & 3 p & 3 p & & \end{array}$ Clips 3p
DISPLAYS
DL704 $\quad 0.3$ in CC $\quad 1300 \quad 1200$ $\begin{array}{llll}\text { FND500 } & 0.5 \text { in CC } & 1000 & 800\end{array}$

## RESISTORS

Carbon film 'resist ors. High stability low noise 5\%.
E12 series. 4.7 ohms to 10 M . Any mix: $\begin{array}{llll} & \text { each } & 100+ & 1000 \\ 0.25 W & 1 p & 0.9 p & 0.8 p \\ 0.5 W & 1.5 p & 12 p & 1 p\end{array}$ Soecial development packs consisting of 10 of each value from 4.7 ohms to Meg
ohm ( 650 res) $0.5 \mathrm{~W} £ 7.50$. $0.25 \mathrm{~W} £ 5.70$. METAL FILM RESISTORS
Very high stability, low noise rated at $1 / 4 W$ 1\%. Available from 510 hms to 330 k E24 series. Any mix.

| each | $100+$ | $1000+$ |
| :--- | :--- | :--- | :--- |
| $4 p$ | $3.5 p$ | $3.2 p$ |

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## SWITCHES

Subminiature toggle. Rated at 3 A 250 V . SPDT 70p SPDT centre off 75p DPDT 80p DPDT centre off 95p

## CAPACITORS

TANTALUM BEAD
$0.1 .0 .15,0.22,0.33,0.47,0.68$
182.2 uF @ 35 V

22 @16V, 47@6V.100@3V
MYLAR FILM
$0.001,0.01,0.022,0.033,0.047$
POLYESTER
$0.01,0.015,0.022,0.033,0.047,0.06$ 合, $0.1 .5 p$ $0.15,0.22$
0.33 .0 .47
$14 p$
CERAMIC
Plate type 50 V . Available in E 12 series from 22 pF to 1000 pF and E 6 series from 1500 pF to RADIAL LEAD ELECTROLYTIC
$\begin{array}{llllll}63 V & 0.47 & 1.0 & 2.2 & 4.7 & 10\end{array}$ $\qquad$ $5 p$

## NEMSMD

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# DESIGNER'S NOTEBOOK 

## A monthly look at the notebook of ETI's chief design engineer, project editor Ray Marston.

AUNTI IRIS (the one with the big eyes) says that the ETI gremlins loved last month's "Notebook." They gobbled up the original figure 1 (a method of precision gating a 555 astable) and left a copy of Fig 4 (a 555 pulse expander) in it's place. To set the record straight, this month's Fig 1 shows what last month's Fig 1 should have looked like. I hope aunti Sible approves.


Fig. 1. Here it is in all its glory, the missing link, Fig 1 from last month - a precision gated astable.

## Who Loves Yer, Baby?

Regular readers of ETI will have noticed that the design team has a particular love of the CD4017 IC. This modestly priced (about 80 pence in 1 off quantities) little device glories in the title of a "decade counter/divider with ten decoded outputs." It's the "ten decoded outputs" bit of the title that makes us really like the device, because those outputs can be used to do a lot of useful things.

The ten decoded outputs of the B-series 4017 can be used to directly drive a bank of LED's to make pretty displays, or to switch tone generators to create pretty tunes. Alternatively, outputs can be coupled back to the devices control terminals to make the IC count to, or divide by, ' $n$ ' (any number from 2 to 9 ) and then either stop or recycle. Numbers of 4017 IC's can readily be cascaded to give either multi-decade division, or to make counters with any desired number of decoded outputs. Let's take a closer look at the device.

## 4017 Basics

Figure 2 shows the outline and pin designations, the functional diagram, and the basic timing diagram of the CD4017, which incorporates a 5 -stage Johnson counter. The device has clock, reset, and clock inhibit input terminals.

The counters are advanced one count at each positive transition of the clock signal when the clock inhibit and reset terminals are low. Nine of the ten decoded outputs are low, with the remaining output high, at any given time. The outputs go high sequentially, in phase with the clock signal, with the selected output remaining high for one full clock cycle. An additional carry out signal completes one cycle for every ten clock input cycles, and can be used to ripple-clock additional 4017's in multidecade counting applications.

The 4017 counting cycle can be inhibited by setting


Fig. 2a. Outline and pin designations of the CD4017
the clock inhibit terminal high. A high signal on the reset terminal clears the counter to zero and sets the ' $O$ ' output terminal high

## 4017 Applications

Figures 3 to 7 show a few ways of employing the decoded outputs of a single B-series 4017 .


Figure 3: the circuit of a 10 -stage sequential LED flasher or cheser, in which one LED is on and the other nine are off at any given time, and the on LED moves one step up the line each time a clock pulse arrives. An alternative action, in which nine LED's are on and one is off at any given time, can be obtained by reversing the polarity of all LED's and taking their common point to the positive supply line.


Figure 4: the circuit of a 10-stage 4-note musical sequencer, that can be used to generate simple tunes or melodies. The number of available notes can be increased by adding more resistors to the R1-R2 component chain.


Figure 5: how to connect the 4017 so that' it stops operating after completing a pre-determined counting sequence. Here, the counter is set to stop when it's clock inhibit terminal is driven high by the ' 9 ' output. The count sequence can be restarted by pressing reset button PB1.
Note in the figure six and seven circuits the counter can be made to divide by any number simply by taking the "free" terminal of the circuit's multi-vibrator to the Nth output terminal of the counter.

## Greater than 10

There are times when ten stages of counting/decoding aren't enough for a particular task. Examples that spring to mind are complex remote control coders and decoders


Figure 6: one way of connecting a 4017 as a divide-by-N $(2<N$ $<9$ ) counter with $\mathbf{N}$ decoded outputs. This circuit is set to divide by 5. The circuit operation here is such that the Nth output of the counter momentarily goes high on the positive transition of the Nth clock pulse, and immediately causes the IC1a-IC1b flip-flop to change state and apply a reset command to pin 15 of the 4017. which in turn causes it's ' $O$ ' output to go high and feed a low signal to one terminal of NOR gate IC1c. When the negative transition of the Nth clock pulse arrives, it places a low signal on the remaining terminal of the IC1c NOR gate, which therefore feeds a high signal to IC1 a and causes the flip-flop to again change state and remove the reset command from pin 15 of the $\mathbf{4 0 1 7}$. The 4017 is then free to count again.


Figure 7: an alternative way of obtaining divide-by-N operation. Here, the Nth output (the 5 th in this diagram) momentarily goes high on the arrival of the positive transition of the Nth clock pulse and causes the IC1a-IC1b monostable to generate a 15 US pulse that immediatley resets the counter to the ' $O$ ' or empty state, reedy for the arrival of the positive transition of the next clock pulso.
that may require as many as nineteen sequential stages, simple music or tone sequencers that may require more than twenty stages, and LED-driving electronic games such as roulette which may require up to thirty-eight sequential stages. In such cases it is a fairly simple matter to interconnect a number of 4017 IC's to obtain any required total of decoded output stages.
Note in the Fig 9 circuit that the 1 counter gives nine useful outputs, and that all succeeding stages give eight useful outputs. The basic circuit can be expanded to incorporate any number of 4017 stages by simply adding slightly modified IC2-IC4a-IC4b stages between IC1 and the final two stages of the system.

## Rabbiting on

You may be wondering why l've chosen this precise moment of history to rabbit on about applications of the 4017. The fact is, I'm presently playing with some rather unușual 4017-based multi-channel remote control systems for possible future projects, and all the stuff that I've crammed into this month's Notebook is spin-off from that development work. I'll tell you more about these next month.

In the meantime, if you want to play with the 4017 circuits that l've already described, you may find the Fig 11 clock generator circuit useful. It uses only one quarter of a CD4093 Schmitt, but generates beautifully clean and interference-free clock pulses.

You can fiddle with the R1 and C1 values to get any


Figure 8 how to interconnect a pair of 4017's to make a 10- to 17 -stage counter/decoder. The circuit is shown set for divide-by-17 operation.

The clock input signal is parallel-fed to IC1 and IC2. When, however, the count is below 9, the '9' output of IC1 is Iow and causes the clock inhibit terminal of IC2 to be set high via IC3c, so IC2 is not influenced by the clock signals. As soon as the 9th clock pulse arrives the ' 9 ' output of IC1 goes high and inhibits IC1 from further clocking action, and simultaneously drives the clock inhibit terminal of IC2 low via IC2c and enables IC2 to respond to subsequent clock signals.

Eventually, on the arrival of the 17 th clock pulse, the ' 9 ' output of IC2 goes momentarily high and triggera the IC3a-IC3b 15 us monostable, which in turn resets both counters to the empty or ' $O$ ' states. The counting sequence then repeats.

Note that the ' 9 ' output of IC1 and the ' 0 ' and ' 9 ' outputs of IC2 are "'lost" in the counting action, so the circuit provides a maximum of 17 usable counter/decoder stages. The circuit can be made to count by any number in the range 10 to 17 by connecting the "'free" input terminal of IC2a to the appropriate output terminal of IC2.
clock' frequency that you want. C1 can have any value from 100 p to 10 u , and R 1 can have any value from 10 k to 10 M . Values of 10 n and 100 k give a clock frequency of about 1 kHz .

## Smarter than the average bear

Does your cranium tend to inflate ever-so-slightly each time that you develop a particularly clever little circuit? If
so, imagine how Robert J. Widlar must feel. He's the guy who, virtually single handed, designed the original 709 op-amp. And the 710, the 711, the LM 101, the 108, the 109, and the 111 . On top of that, he either owns or shares patents on the band gap reference and the super beta transistor.

Old smarty boots has done it again, and designed an opamp called the LM10. The LM 10 is reckoned to represent one of the most important developments in IC op-amp technology in recent years. Amongst other things it can operate over the supply voltage range 1 V 1 to 40 V , drawing only 270 uA of current in all cases. Its output can swing within 15 mV of the supply terminals, or will deliver 20 mA of output current with 400 mV saturation.

We plan to give full details of the LM 10, complete with extensive applications information, in the near-future. Meantime, it really does seem that Robert J. Widlar is a lot smarter than your average bear.


Fig. 11. This simple circuit makes an excellent clock generator for driving 4017 circuits.


Figure 9 shows the connections for making an 18- to 25-stage counter/decoder from three 4017 's. In this case IC3 is inhibited via IC4b and the low output '9' of IC2. and IC2 is inhibited via IC4a and the low output ' 9 ' of IC1, up to the 9 th clock pulse. IC1 is inhibited via it's high '9' output, and IC3 is inhibited via IC4b and the low output '9' of IC2, between the 10 th and 17 th clock pulses.


Fig. 10. A 26-to 33-stsge counter/decoder set for divide-by-33 operation. This circuit can be expanded to give a ny number of decoded output stages by interposing additional IC2-IC52-IC5b stages between IC2 and IC3. Each additional 4017 B stage makes an extra eight decoded outputs available.

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# BATTERY INDICATOR 

## you've just offered a friend a lift? The conversation goes a little flat when you're both riding the bus to work, 20 minutes late. Jonathan Scott found a solution...



THE OLD, RELIABLE lead-acid battery may be way ahead of what ever is in second place for vehicle electrical systems, but they do need a 'weather eye' kept on them. Particularly if they're out of warranty. The same applies to 'reconditioned' batteries, so often found in secondhand vehicles of some age.

That's the problem with cars running out of petrol and running out of battery produces the same heartrending result. Immobility.

Most vehicles have a petrol gauge. Few have an equivalent for the battery. Many 'older' cars included a 'charging current' meter. This told you something about the car's generatorregulator and required some inter-
pretation to figure out whether the battery was in good health.

Probably the best way to oheck on the state of your battery is to use a hydrometer. However, hydrometers have a number of drawbacks. Being made of glass,'they're fragile and can't be used while a car is in motion. The small amount of battery acid that remains on them presents a storage problem - the drips and fumes attack most metals and materials. They're okay for the corner garage but justifying their cost, for the occasional use they get in home workshops, is not always possible.

Another method of testing battery condition is by checking the voltage 'on load'. A lead-acid vehicle battery in a reasonable state of charge will have a
terminal voltage under normal working load somewhere between 11.6 and 14.2 volts. When a battery shows a terminal voltage below 11.6 volts its capacity is markedly decreased and it will discharge fairly quickly. Like as not, it won't turn the starter motor for very long! On the other hand, if the voltage on load is above 14.5 volts then the battery is definitely fully charged! However, if it remains that way for any length of time while the car is on the road, the vehicle's alternator-regulator system is faulty and the battery may be damaged by overcharging.

Reading the battery voltage can be done in a number of ways. You could use a digital panel meter, set up as a voltmeter. Their drawback is that they cost nearly ten times as much as a hydrometer! The next best method is to use an 'expanded-scale voltmeter'. Reading the voltage range between 11 and 15 volts on a meter face calibrated $0-16$ volts is a squint-and-peer exercise. On a $0-30$ volts scale, as used on many modern multimeters, it's worse. A meter which reads between 11 volts at the low end of the scale and 16 volts at the high end is ideal. Hence, the term 'expandedscale'.

However, you don't want to be peering at a meter on the dash board when you're driving through traffic. The range of voltage over which your battery is healthy is some two volts. An indicator which simply requires the



The circuit diagram and component overlay (below). During construction, make sure all of the diodes and LEDs are the right way round.

## TO BATTERY + Ve



## HOW IT WORKS

4
This circuit depends for its operation upon the different voltage drops across different colour LEDs.

At 20 mA the voltage drops across red, yellow and green LEDs are typically $1.7,3.0$ and 2.3 volts respectively. When the vehicle battery voltage is too low to cause either ZD1/ZD2 or ZD3 to conduct, Q1 and Q2 are held off by R3 and R5. Under these conditions the yellow LED is forward biased and conducts via Dl producing a potential of about 3.7 volts at point A (see circuit diagram). When the supply rises above about 11.6 volts ZD3 conducts, biasing Q2 on. By virtue of its lower voltage requirements the green LED conducts, reducing the voltage at point $A$ to approximately 2.6 volts. This is not enough to bias D1/LED3 on, so the yellow LED goes off. The green LED 'steals' the bias from the yellow LED. When the supply rises above about 14.2 volts, Q1 is biased on and the red LED 'steals' the bias from the green. The potential at point A falls to two volts and only the red LED conducts.

R1 limits the current through the LEDs. R2 and R4 limit the base currents into Q1 and Q2.

## PARTS LIST

| Resistors all $1 / a W, 5 \%$ |  |
| :---: | :---: |
| R1 | 470 R |
| R2 | 100 R |
| R3, R5 | 10 k |
| R4 | 680 R |

Semiconductors

| D1 | 1 N914 |
| :---: | :---: |
| ZD1, ZD2 | 6V8 400 mW zener |
| ZD3 | 11 V 400 mW zener |
| Q1. 02 | BC547,8,9 or |
|  | BC107,8,9 or |
|  | common silicon |
|  | NPN type |
| Miscellaneous |  |
|  |  |
| Aluminium ang | bracket for under- |
| dash mounting |  |

Aluminium angle bracket for underdash mounting.

## BUYLINES

Nothing to worry about here really, but make sure the LEDs are the correct colours, otherwise the voltage drops will not be correct!
occasional glance, and needs no 'interpretation', is what is really needed.

With this project, that's exactly what we've done.

## Go, caution, stop

We have devised a simple circuit that indicates as follows:
Yellow: battery 'low'
Green: battery okay
Red: battery overcharging
When the battery voltage is below 11.6 volts, a yellow indicator lights. This indicates the battery is most likely undercharged or a heavy load (such as high power driving lights) is drawing excess current. When it is between 11.7 and about 14.2 volts the green indicator lights, letting you know all is sweet. If the red indicator lights, as it will if the voltage rises above 14.2 volts, maybe the vehicle's voltage regulator needs adjusting or there is some other problem.

## The circuit

The circuit is ingeniously simple, having barely a handful of parts. Reliability should be excellent.

We actually started out with a somewhat complex circuit. It used only two indicators and required you to 'interpret' what was happening. In trying to convert that to a yellow-green-red style of indication it sort of grew like topsy. This circuit had four transistors, a dozen resistors etc and didn't look at all attractive as a simple project that the average hobbyist or even handyman could build one Saturday afternoon and get going immediately. A rival circuit was devised by another staff member using a common IC. This sparked a controversy as to which was the better! Certainly, both did the job required . . but maybe there was a simpler method.

It was discovered that different coloured light emitting diodes (LEDs), which we had decided to use for the indicators in the project, had different voltage drops when run at the same current. Seizing on this idea, the original circuit (four transistors, a dozen resistors . . .) was modified to exploit this characteristic and the simple circuit you see here was the result.

## Construction

Construction is straightforward. If you haven't soldered electronic components before - and this project was designed for the motorist/handyman as well as electronics enthusiasts - then we suggest you practice on something before tackling this project. Soldering is one of those things like swimming or riding a bicycle, or sex - it's okay once
you've done it once or twice but you don't practice out on the street!

We recommend you use the printed circuit board designed for this project. The actual layout of the components themselves is not critical but a printed circuit board reduces the possibility of errors.

It is best to mount and solder the resistors first. Follow this by soldering in the diodes D1 and the zener diodes ZD1, ZD2 and ZD3. Carefully follow the accompanying component overlay making sure the diodes are all inserted the correct way around. Next, mount the transistors, again referring to the overlay, checking to see they are inserted correctly before soldering.

Finally, mount the light emitting diodes. These too may only be inserted one way. Check with the component overlay and connection diagrams. Make sure they are in the correct sequence. On the component overlay, LED 1 is the red LED, located at the left. The yellow LED is on the right, marked with a ' 2 '. The green LED, marked ' 3 ' is between them.

The circuit could be tested at this
stage if you have a variable power supply, or access to one. Simply vary the voltage across the range between 11 and 16 volts and note whether the LEDs light up in the correct sequence and close to the voltages indicated.

## Mounting

As vehicles vary so much in dash panel layout, we can only make general suggestions.

Clearly, the indicator should be mounted such that the three LEDs are not in direct sunlight. A low part of the dash, but make sure it's readily visible from your normal driving position, will pretty well ensure the display may be easily read during the daytime. Alternatively, if you have an 'overhung' dash, or a portion which overhangs (usually where the instruments are mounted anyway), then a suitable position will generally suggest itself.

Exact mechanical details will have to be determined according to your particular situation. Two holes are provided in the board for mounting bolts. Alternatively, the whole assembly
may be mounted from the LEDs. Three LED holders inserted through part of the dash panel, or an escutcheon plate mounted on the dash, will hold the LEDs quite securely. Providing the leads on the LEDs are fairly short, the board will place little strain on them and the assembly should be mechanically secure.

## Connection

The indicator may be installed in vehicles having positive or negative earth electrical systems.

The component overlay shows the connection for a negative earth vehicle. The 'battery +ve' lead goes to the ignition switch - the indicator only operates when the vehicle is being used - the battery negative lead should be taken to a good 'earth' point on the vehicle frame.

For a positive earth vehicle, the lead marked 'battery - ve' goes to the ignition switch connection, while the 'battery +ve' lead goes to the vehicle frame.

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# microfile 

## Henry Budgett wandered across the States in the name of Microfile. This is his report, and other small world shattering items that happened to crop up while he was away.

## Pets in Business

THE LONG AWAITED PET add-on's have arrived at last, honest! Launched at a Cafe Royal press conference was a new PET based business system with a price tag of $£ 2,500$ excluding software. Utilizing the new, largekeyboard 32 K machine with Commodores own dual disk drive and tractor-fed printer it forms the cheapest small business system yet available. The software is being written by a new division of ACT, Petsoft's parent company, called PETACT and will cost between £225 for a single package to about $£ 800$ for a complete suite of programs. It will be available in either disk or cassette format and is the first business software for a micro to be written by a professional software house. The software price also includes a day's training for an employee.

We rather thought that the printer was never going to arrive as it was trapped at Heathrow in customs but it surfaced during the Champagne and Orange cocktails and appeared to be of high quality. The second reason for the Press reception was to announce the forming of an 'endorsement" scheme for non-Commodore produced PET add-on's, the PETACT software being the first product to be launched under the scheme.

Deliveries of the new style PET's have started and should be available in most areas now, the disks and printers will start to appear in mid-May at some of the 100 dealers and will hopefully be generally available within a couple of months. Chuck Peddle the father of the PET and KIM was at the reception and gave a strong indication that new and exciting things were on the way in connection with both machines, memory expansion being one possibility.

On a final note the sales of the UK machine were around 3000 during 1978 and this figure had been reached by the end of April of this year, the market is still growing.

## NASCOM With Added Plus

After the phenomenal success of the NASCOM I ( 150,000 sales worldwide) the company have announced a new single board machine called NASCOM II.

Although it is physically the same size as the ' 1 ' and uses the same bus structure it is not intended as a simple upgrade but rather as a new starting point in the home computing market. Based on the Z80A it offers a $75 \%$ increase in processing speed along with an 8 K Microsoft BASIC in ROM. Several new features are included on the machine, a new 2 K monitor with many improvements over the T4, A CUTS cassette interface, 8 K of user RAM and a new extended keyboard. The interfaces supplied include an on-board UART for the RS232 or the cassette interface, capable of running at 300 or 1200 Baud, and an uncommitted P10 for two 8 bit ports. The video is run from a 1 KA RAM with a 2 K character generator, an optional socket is supplied for another 2 K graphics ROM which is software selectable.


Above and below: the new bits for PET.


## Below: the new more powerful NASCOM.



Both the new monitor and the BASIC can be used with the ' $I$ ' and all the peripherals for the ' $I$ ' can be used with the 'II' making it the basis of a very nice OEM system. The circuit board is of the usual superb quality and the kit will be available from June at $£ 295$ ex VAT. We hope to get our hands on one to review soon and this will be published in CT as close to the release date as possible

## Clubbing Together

A couple of new clubs have sent us details of themselves this month. The first is the Sorcerer Programme Exchange Club, SPEC, which has been formed to promote the Exidy Sorcerer. Rather than having an actual club they are aiming to become an information exchange on useful. hints and programs for the machine and would be most grateful for anyone who has some to send them in. The people to contact are Mr G. F. Counsell and Mr M. P Hannaby at 65 Trafalgar Road, Birkdale, Southport, Merseyside.

The second club is the South Yorkshire Personal Computing Group, SYPCG, who are appealing to people in the area interested in do-it-yourselr computing. They hope to meet on the second Wednesday of each month with a variety of topics under discussion. Membership is $£ 3$ for 1979 and the meetings will be held at 7.00 pm in the University of Sheffield. For further information you should contact the Secretary, Mr Tony Rycroft, at 88 Spinneyfield, Moorgate, Rotherham, S. Yorkshire.

## Showing It Off USA Style

I spent a pleasant weekend in Orlando, Florida, last month at a micro-show. It really was a micro-show, dealing with the machines and also being very small. However this was really an advantage as it allowed free and personal access to the exhibitors rather than the situation which arises at some of the UK exhibitions. The variety of machines was impressive, ranging from an IAM 65 to an LSI 11, but there were no PET's, KIM's or Superboards which was rather surprising. The only new machine there was an $\mathrm{Z80}$ based S100 system called Informer which also used an SC / MP for keyboard and video control. Supplied either with or without an integral floppy it looked impressive but is unlikely to appear on this side of the Atlantic.

The show also featured a siminar programme, again on a very informal and personal level which resulted in a most entertaining question and answer forum. The whole show was most professionally run and I only wish that some of the UK shows coutd adopt a similar attitude and become smaller and more personal instead of bigger and unhelpful.
The biggest business system at the show, an LSI II with dual floppies being used for stock control.



The familiar Apple II with a speech recognition board installed. It worked remarkably well and 'echoed' back your word


New TRS 80 printer. Will it reach us, we wonder.
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Mine Sweeper

## E. A. Johnson

The object of the game is to locate and destroy a moving minesweeper. The ship moves along a set course, but, to avoid destruction it can deviate slightly from the course and alter its speed.

## Playing the game

The game is started by entering a number (in the range 0 to 1 ) into register $E$, to set the initial position of the minesweeper through a random number generator. A shot is made by entering the xy co-ordinates (into the $A$ and $B$ registers respectively) of the square where the ship is believed to be. The calculator determines the position of the ship and displays the distance by which the shot missed. If the shot is within five units of the ship, damage occurs which slows the ship down in proportion to the nearness of the shot. When the ship is destroyed the display flashes.
After the ship has been destroyed, the number of shots used can be displayed by pressing ' C ', and a new game can be started by pressing ' D '.

## Method of calculation

The initial value of $\Theta$, which determines the ship's position is determined using the calculator's random number package. The ship's co-ordinates are then calculated by the following equations:

$$
x=(50+45 \cos 3 \Theta)+\text { RNUMX }
$$

$$
y=(50+45 \sin 2 \Theta)+\text { RNUMY }
$$

where RNUMX and RNUMY are random numbers (in the range of -3 to +3 ) to give the ship its avoiding action.
The distance of the shot from the ship is calculated using pythagoras and displayed in integer mode.

The next value of $\Theta$ is then given by

$$
\Theta=\Theta+\Theta \text { INCR }
$$

where ©INCR is originally set to 5 , the calculator then determines the new co-ordinates of the ship.
When the distance of the shot from the ship is less than five units, the value of OINCR is reduced to slow the ship down. The new value is given by ©INCR $=$ OINCR - $(5 \div$ distance $)$.
The above procedure continues until OINCR $\leqslant 0$ when the ship is destroyed.
A new game, if required, is started by automatically generating a new random initial value of $\Theta$.

MINESWEEPER PROGRAM FOR TI 58 \& 59


| Example Game |  |  |  |
| :---: | :---: | :---: | :---: |
| Comment | Enter |  | Display |
| Enter a number between 0 \& 1 | 0.258 | E | 0 |
| Enter guess for x co-ordinate | 50 | A | 0 |
| Enter guess for y co-ordinate | 11 | B | 65 (Distance) |
| $\times$ co-ordinate | 84 | A | 0 |
| y co-ordinate | 70 | B | 62 |
| x | 40 | A | 0 |
| y | 85 | B | 7 |
| x | 43 | A | 0 |
| y | 87 | B | 3 |
| $x$ | 51 | A | 0 |
| y | 89 | B | 3 |
| x | 54 | A | 0 |
| y | 90 | A | 9.999999999 |
|  |  |  | ( Flashing ) |
| To display number of shots |  | C | 6 |
| To start a new game |  | D | 0 |
| $\times$ co-ordinate | 50 | A | 0 |
| y co-ordinate | 11 | B | 42 |

ETC.

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Lunar Landing
Sarah J. Owen.
This program was devised for use on the Commodore PR. 100 calculator, but is easily adapted for use on any other programmable ones. Imagine you are the Astronaut controlling the final descent of a lunar module, at regular intervals the speed of descent is displayed, the period of burn of the retro-rocket has to be calculated, after allowing for the reducing weight of the fuel on board. . . . . . . . Five speed corrections are allowed, after which the final impact velocity is displayed. If an error is made and all fuel is used, there is just time to transmit an urgent S.O.S. message before destruction on the lunar surface. . . . . . . Due to the lack of program space, the method of selecting the initial random speed is unusual, but ranges between 20 and $100 \mathrm{~m} . \mathrm{p} . \mathrm{h}$.

Recommended periods for
Retro-rocket firing

| SPEED | BURN |  |
| :---: | :---: | :---: |
|  |  |  |
| 5 | 1.6 |  |
| 7 | 1.9 | 200 |
| 10 | 2.3 | 220 |
| 15 | 2.7 | 250 |
| 20 | 3.0 | 270 |
| 30 | 3.4 | 300 |
| 40 | 3.7 | 330 |
| 50 | 3.9 | 365 |
| 60 | 4.1 | 400 |
| 70 | 4.2 | 450 |
| 80 | 4.4 | 500 |
| 90 | 4.5 | 550 |
| 100 | 4.6 | 600 |
| 110 | 4.7 | 660 |
| 120 | 4.8 | 730 |
| 130 | 4.9 | 800 |
| 150 | 5.0 | 900 |
| 160 | 5.1 | 1000 |

PROGRAM

| LOC | CODE | KEY | fuel allow 1 period for weight of fuel remaining (approx) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 00 | 21 | F | 36 | 85 | - |
| 01 | 63 | S | 37 | 52 | MR |
| 02 | 21 | F | 38 | 81 | 1 |
| 03 | 51 | FRAC | 39 | 85 | - |
| 04 | 74 | X | 40 | 52 | MR |
| 05 | 81 | 1 | 41 | 91 | 0 |
| 06 | 91 | 0 | 42 | 74 | X |
| 07 | 95 | $=$ | 43 | 95 | $=$ |
| 08 | 51 | M | 44 | 35 | $x$ |
| 09 | 91 | 0 | 45 | 51 | M |
| 10 | 53 | $X_{n}$ | 46 | 91 | - |
| 11 | 82 | 2 | 47 | 52 | MR |
| 12 | 91 | 0 | 48 | 81 | 1 |
| 13 | 51 | M | 49 | 94 | +/- |
| 14 | 81 | 1 | 50 | 15 | SKIP |
| 15 | 71 | 4 | 51 | 14 | GOTO |
| 16 | 51 | M | 52 | 73 | 6 |
| 17 | 82 | 2 | 53 | 63 | 9 |
| 18 | 52 | MR | 54 | 52 | MR |
| 19 | 91 | 0 | 55 | 82 | 2 |
| 20 | 74 | $\times$ | 56 | 85 | - |
| 21 | 62 | 8 | 57 | 81 | 1 |
| 22 | 84 | + | 58 | 95 | $=$ |
| 23 | 52 | MR | 59 | 15 | SKIP |
| 24 | 81 | 1 | 60 | 14 | GOTO |
| 25 | 95 | $=$ | 61 | 81 | 1 |
| 26 | 51 | M | 62 | 73 | 6 |
| 27 | 91 | 0 | 63 | 52 | MR |
| 28 | 21 | F | 64 | 91 | 0 |
| 29 | 52 | INT | 65 | 13 | R/S |
| 30 | 13 | R/S | 66 | 14 | GOTO |
| 31 | 21 | F | 67 | 91 | 0 |
| 32 | 85 | M- | 68 | 91 | 0 |
| 33 | 81 | 1 | 69 | 72 | 5 |
| 34 | 21 | F | 70 | 91 |  |
| 35 | 32 | $e^{x}$ | 71 | 72 | 5 |


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To play:
Player $A$ enters a 5 figure number and then presses GSB 1.

Player B enters his guess and presses $R / S$. After several seconds calculation the display shows a number such as 1.2 which means 1 digit in the right place and 2 more correct figures but in the wrong position.

Player B then enters another guess and presses $R / S$, etc. until he achieves a score 5.0.

For cheats (!) or if the number set has been forgotten, it is held in STO . 5 .

The use made of the calculators stores is shown below.
If the number set was $A B C D E$, and the guess is FGHIJ, then:

| STO | 0 | Used |
| :--- | :--- | :--- |
| 1 | J |  |
| 2 | I |  |
| 3 | H |  |
| 4 | G |  |
| 5 | F |  |
| 6 | Used |  |
| 7 | Used |  |
| 8 | Used |  |
| 9 | Used |  |
| .0 | E |  |
| .1 | D |  |
| .2 | C |  |
| .3 | B |  |
| .4 | A |  |
| .5 | ABCDE |  |


| STEP | INSTRUCTION |
| :---: | :---: |
| 01 | gLBL1 <br> fFIX1 <br> STO. 5 <br> 1 <br> 4 <br> CHS <br> GSBO <br> gLBL9 <br> 0 |
| 10 |  |
| 20 | $\begin{aligned} & \text { RCLi } \\ & 9 \\ & \text { STO }+0 \\ & x \gtrless y \\ & \text { RCLi } \\ & - \\ & \text { gx }=0 ? \\ & \text { GSB3 } \\ & 8 \\ & \text { STO- } 0 \end{aligned}$ |
| 30 | RCLO 6 $\mathrm{fx}=\mathrm{y}$ ? GTO4 GTO5 gLBL3 STO+7 RTN gLBLO |
| 40 | $\begin{aligned} & \text { STO } 0 \\ & x \gtrless y \\ & \text { EEX } \\ & 4 \\ & \div \end{aligned}$ |
| 45 | $\begin{aligned} & \mathrm{gLBL} 2 \\ & \text { fINT } \end{aligned}$ |



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