

FULL SPEC TELETEXT DESIGN
Plugs In To The Aerial Socket!
POLYPHONIC KEYBOARD
40 CMOS CLOCKS!
LIFE ON OTHER WORLDS
SOIL MOISTURE INDICATOR



CHROMATHEQUE 5000

5 CHANNEL LIGHTING EFFECTS SYSTEM

All kits also available as separate packs (e.g. PCB P.C.B. component sets hardware sets etc.)
Prices in FREE CATALDGUE

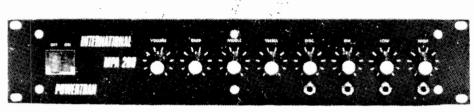


COMPLETE KIT ONLY £49.50 + VAT!

This versatile system featured as a constructional article in ELECTRONICS TODAY INTERNATIONAL has 5 frequency channels with individual level controls on each channel. Control of the lights is comprehensive to say the least. You can run the unit as a straightforward sound-to-light or have it strobe all the lights at a speed dependent upon music level or front panel control or use the internal digital circuitry which produces some superb random and sequencing effects. Each channel handles up to 500W and as the kit is a single board design wiring is minimal and construction very straightforward

Kit includes fully finished metalwork, fibreglass PCB, controls, wire, etc. — Complete right down to the last nut and bolt!

MPA 200 100 WATT (rms into 8 Ω) MIXER/AMPLIFIER



COMPLETE KIT ONLY £49.90 + VAT!

Featured as a constructional article in ETI, the MPA 200 is an exceptionally low priced — but professionally finished — general purpose rugged high power amplifier. It features adaptable input mixer which accepts a wider range of sources, such as disc, microphone, guitar etc. There are wide range tone controls and a master volume control. Mechanically the MPA 200 is input mixer which accepts a wider range of sources such as disc, microphone guitar e simplicity itself with minimal wiring needed, making construction very straightforward

The kit includes fully finished metalwork fibre glass PCBs, controls, wire etc. — complete down to the last nut and bolt

Parts to build power amp module (mc. PCB Custom designed toroidal transformer with res caps s/c etc) £10.60 + VAT.

mounting clamp £10.50 + VAT.

Parts for power supply only (caps, rects., fuses, F. holders) £3.40 + VAT

TRANSCENDENT 2000 SINGLE BOARD SYNTHESIZER

LIVE PERFORMANCE SYNTHESIZER DESIGNED BY CONSULTANT TIM ORR (FORMERLY SYNTHESIZER DESIGNER FOR EMS LIMITED) AND FEATURED AS A CONSTRUCTIONAL ARTICLE IN ELECTRONICS TODAY INTERNATIONAL.

The TRANSCENDENT 2000 is a 3 octave instrument transposable 2 octaves up or down giving an effective 7 octave range. There is portamento pitch bending a VCO with shape and pitch modulation, a VCF with both low and high pass outputs and a separate dynamic sweep control a noise generator and an ADSR envelope shaper. There is also a slow oscillator, a new pitch detector. ADSR repeat, sample and hold, and special circuitry with precision components to ensure tuning stability amongst its many features.

The kit includes fully finished metalwork fully assembled solid teak cabinet filter sweep pidal professional quality components (all resistors either 12% metal oxide or 1) x metal trimly and it really is complete — right down to the last not and bold and last piece of wrier 1 here is even a 13A plug in the kit — you need buy abbolidely no more parts before plugging in and making great music? Virtually all the components are on the one professional quality bibrigals x PCB printed with component locations. All the controls mount directly on the main board all connections to the board are made with connector plugs and contructions is so simple it can be built easily in a few evenings, by aimust anyone capable of neat soldering? When finished you will pussess a synthesizer cumprable in performance and quality with ready built units willing for between \$500 and \$700!

COMPLETE KIT ONLY £172.00 + VAT!

Comprehensive handbook supplied with all complete kits! This fully describes construction and tells you how to set up your synthesizer with nothing more elaborate than a

NWFRTRAN



Cabinet size 24.6" x 15.7" x 4.8" (rear) 3.4" (front)

ORDERING INFORMATION **AND MORE KITS ON PAGE 8**





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Gear down your movements.

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Wet or dry ETI gives you it straight. 67

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State of charge flashed for your convenience.

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Quality audio modules and accessories for

S450

STEREO FM TUNER Fitted with phase lock-loop



FREQUENCY RANGE	88-108 Mhz
SENSITIVITY	3 0 µV
BANDWIDTH	250 kHz
SPURIOUS REJECTION	50 dB
SELECTIVITY ± 400 kHz	55 dB
AUDIO OUTPUT (22 5 kHz devia	ation) 100 mV
STEREO SEPARATION	30 dB
SUPPLY REQUIREMENTS	20 to 30V (90mA max)
AERIAL IMPEDANCE	75 ohms
DIMENSIONS	240mm · 110mm · 32mm

The 450 Tuner provides instant programme selection at the touch of a button ensuring accurate tuning of 4 pre-selected stations, any of which may be altered as often as you choose, simply by changing the settings of the pre-sel controls. Features include FET input stage Vari-Cap diode tuning Switched AFC LED Stere diocator.

Stereo 30 COMPLETE AUDIO CHASSIS £21.57

OUTPUT POWER	7 Watts RMS	
LOAD IMPEDANCE	8 ohnis	
TOTAL HARMONIC DISTORTION	Less than 5% (Typically 3%)	
FREQUENCY RESPONSE	50 Hz to 20 kHz ± 3dBs	
TONE CONTROL RANGE	± 12 dBs at 100Hz and 10kHz	
SENSITIVITY	190 mV for full output	
INPUT IMPEDANCE	1 M ohrys	
TRANSFORMER REQUIREMENTS	S 22 V.A.C. rated at 1A	
DIMENSIONS (Less controls and papel)	200mm - 130mm - 33mm	

The Stereo 30 comprises a complete stereo pre-amplifier, power amplifiers and power supply. This, with only the addition of a transformer or overwind will produce a high quality audio unit suitable for use with a wide range of inputs i.e. high quality ceramic pick-up, stereo tuner, stereo tape deck etc. Simple to install, capable of producing really first class results this unit is supplied with full instructions, black front panel, knobs, main switch, luse, and fuse holder and universal mounting brackets.

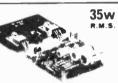
AL60 AUDIO AMPLIFIER MODULE 25 Watts RMS



OUTDUIT DOWED	25 Watts RMS
OUTPUT POWER	
SUPPLY	30-50 ♥
LOAD IMPEDANCE	8-16 ohms
TOTAL HARMONIC DISTORTION	Less than 1% (Typically 06%)
FREQUENCY RESPONSE	20 Hz to 30 kHz - 2 dBs
SENSITIVITY	280 mV for full output
MAX. HEAT SINK TEMPERATURE	90°C
DIMENSIONS	103mm - 64mm - 15mm

This high quality audio amplifier module is for use in audio equipment and stereo amplifiers and provides output powers up to 25 RMS with distortion levels below 0.1%

AL80 AUDIO AMPLIFIER MODULE £7.92*



OUTPUT POWER	35 Watts RMS
SUPPLY	40-60 V
LOAD IMPEDANCE	8-16 ohms
TOTAL HARMONIC DISTORTION	Less than 1% (Typically 06%)
FREQUENCY RESPONSE	20 Hz to 30 kHz · 2 dBs
SENSITIVITY	280 mV for full output
MAX. HEAT SINK TEMPERATURE	90°C
DIMENSIONS	103mm - 64mm - 15mm

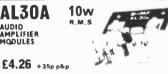
The AL80 is similar in design to the AL60 above and is of the same high quality but provides output powers up to 35W with distortion levels below 0.1%



OUTPUT POWER	125 Watts RMS continuous
OPERATING VOLTAGE	50-80 V
LOADS	4-16 ohms
FREQUENCY RESPONSE	25 Hz 20 kHz measured at 100 Watts
SENSITIVITY FOR 100 WATTS O/P AT 1 kHz	450 mV
INPUT IMPEDANCE	33 K ohms
TOTAL HARMONIC DISTORTION 50 WATTS into 4 ohms 50 WATTS into 8 ohms	0 1% 0 06%

£19.24* +66p p&p This unit, designated AL250, is a power amplifier providing an output of up to 125W RMS, into a 4 ohm load

AL30A AUDIO AMPLIFIER MODULES



Л	MAXIMUM SUPPLY VOLTAGE	30 V
П	POWER OUTPUT for 2% THD	10 Walts RMS
1	TOTAL HARMONIC DISTORTION	Less than 25%
ı	LOAD IMPEDANCE	8-16 ohms
1	INPUT IMPEDANCE	100 K ohms
1	FREQUENCY RESPONSE	50 Hz-25 kHz ± 3 dBs
ı	SENSITIVITY	75 mV for full output
1	DIMENSIONS	74mm - 63mm - 28mm

These low cost 10 watt modules offer the utmost in reliability and performance, whilst being compact in size

SPM80 STABILISED POWER SUPPLY £4.95 35p p&p



NPUT A.C. VOLTAGE	33-40V
OUTPUT D.C. VOLTAGE	33 V nominal
OUTPUT CURRENT	t0 mA-1 5 amps
OVERLOAD CURRENT	1 7 amps approx.
DIMENSIONS	105mm - 63mm - 30mm

Designed to power two AL60s at 15 Watts per channel simultaneously. Circuit Techniques include full short circuit protection.

PA100 STEREO PRE-AMPLIFIER

i di	The Contract of the Contract o	
C 1 Q N 5		

FREQUENCY RESPONSE	20 Hz to 20 kHz · 1 dB
TOTAL HARMONIC DISTORTION	Less than 1% (Typically 07%)
SENSITIVITY 1. TAPE INPUTS 2. RADIO TUNER 3. MAGNETIC P U.	100 mV/100 K ohms } For an 100 mV/100 K ohms } output 3.5 mV/50 K ohms] 250 mV
EQUALISATION	Within ± 1 dB from 20 Hz to 20 kHz
BASS CONTROL RANGE	± 15 dBs at 75 Hz
TREBLE CONTROL RANGE	+ 10-20 dBs at 15 kHz
SIGNAL/NOISE RATIO	Better than 65 dBs (All inputs)
INPUT OVERLOAD	Better than 26 dBs (All inputs)
SUPPLY	20 to 40 V
DIMENSIONS	300 - 90 - 33mm (less controls)

A top quality stereo pre-amplifier and tone control unit, the PA100 provides a comprehensive solution to the front end requirements of stereo amplifiers or audio units. The six push button selector switch gives a choice of inputs together with two filters for high and low frequencies.

STEREO MAGNETIC CARTRIDGE PRE-AMPLIFIER



£3.35

SENSITIVITY	3 5 mV for 100 mV output
EQUALISATION	Within ± 1 dB from 20 Hz to 20 kHz
INPUT IMPEDANCE	50 K ohms
SUPPLY	18 to 30 V-re earth
DIMENSIONS	110 · 50 · 25mm (inc DIN socket)

PA12 STEREO PRE-AMPLIFIER



£8.75

The PA12 Stereo Pre-Amplifier chassis is designed and recommended for use with the AL 20/30 Audio Amplifier Modules, the PS12 power supply and the T538 Transformer Features include on/off volume Balance, Bass and Treble controls. Complete with Japo pulse.

	and fredie Controls. Complete will	in tape output
	FREQUENCY RESPONSE	20 Hz-20 kHz (-3dB)
	BASS CONTROL	± 12 dB at 60 Hz
	TREBLE CONTROL	± 14 dB at 10 kHz
	INPUT IMPEDANCE	1 Meg. ohm
	INPUT SENSITIVITY	300 mV
	CROSSTALK	60 dB
	SIGNAL/NOISE RATIO	65 dB
	OVERLOAD FACTOR	± 20 dB
	TAPE OUTPUT IMPEDANCE	25 K ohms
Ī	DIMENSIONS	152mm + 84mm × 25mm

PS12 POWER SUPPLY MODULE

Power supply for AL20A-30A, PA12, S450 etc. Transformer T538.

Input A.C. Voltage 15, 20V Output D.C. Voltage 22–30 approx. (Dependent upon

Output Current 800mA

maximum.
Dimensions 60 - 43 - 26mm



5 WATTs -

£2.13

BP124 SIREN ALARM MODULE

American Police screamer powered from any 12 volt supply into 4 or 8 ohm speaker Ideal for car burglar alarm, freezer break-down, and other security purposes.



35p p&p. MA60 HI-FI AMPLIFIER KIT

Build you own top quality amplifier, save yourself pounds. The MA60 kit comprises the following Bl-kits modules, 2 · At60 amps, 1 · PA100 pre-amp, 1 · SPM80 slab power supply, 1 · BMT80 transf. giving 15 walts RMS per channel STREO. All modules covered by the BI-PAK satisfaction or money back guarantee. Details of the above modules are in this ad. Price £36.00 + 62p p&p.

TC60 KIT

A beautifully designed genuine TEAK WOOD veneered cabinet to put the professional touches to your home built amplifier. Full set of parts incl. Front & Back Panels, Knobs, Chassis, Fuses, Sockets, Noen, etc. Ideal for the MA60. Size. 425mm. 290mm.

Price £22,44 + 86p p&p.

TRANSFORMERS

T538 For use with S.450 AL30A MPA30 Order No. 2036 T2050 For use with Stereo 30 Order No. 2050 BMT80 For use with AL60 SPM80 Order No. 2034 BMT250 For use with AL250 Order No. 2035 2040. For use with AL60 Order No. 2035 2040. For use with AL60 Order No. 2035 Control No. 2040 For use with AL60 Order No. 2041 For use with AL80 AL120 and AL250 Order No. 2041 Price: £3.60 + 55p p&p Price: £3.66 + 55p p&p Price: £6.08 + 86p p&p Price: £5.85 + 80p p&p Price: £7.65 + 86p p&p

CASES

TEAK 30, 32 \times 23 \times 8cm, designed mainly for use with our stereo 3Ô Audio System but has proved very helpful to home constructors. Fitted with solid uncut front and back of n 139 £8.69 + p8p 70p. TEAK 80, 42 \times 29 \times 9cm, for use with AL50 / MK60 Audio Kit. Useful for the home constructor requiring an amplifier sleeve — has no front or back panel, o/n 140 £7.87 + p&p 85p.

Professionals and Enthusiasts from BI-PAK

AL120 AMPLIFIER

(With integral heat sink and short circuiprotection)





OUTPUT POWER SLIPPLY

70 Watis LOAD IMPEDANCE 8-16 ohms 05% Max. (Typically 02%) TOTAL HARMONIC DISTORTION FREQUENCY RESPONSE ± 1dB 25Hz-20kHz SENSITIVITY 500mV MAX HEAT SINK TEMP 45 dea. C DIMENSIONS 192 x 89 x 49 mm

Introduced to fulfill the demand for a fully protected power amp, capable of driving high quality speaker systems at up to 50w with distortion levels below 05% ideal for domestic use. Discos. P.A. systems, electronic organs etc. The generously rated components ensure continuous operation at high output levels.

STABILISED POWER SUPPLIES SPM120/45 SMP120/55 SMP120/65

£6.52

OFFEIES	. A
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1	F

PM120/45 40-48v PM120/55 50-U5v PM 120/65 60.654 OUTPUT CURRENT 2.54 RIPPLE 1A 100mV

SPM120 is a fixed voltage stabiliser available with an output voltage of either 45v, 55v, or 65v. Designed primarily for use in audit applications, the stabiliser which provides output currents up to 2.5A operates direct from a mains transformer requiring only the addition of 2.Electrolytic capacitors to complete the s/c protection.

GE100 Mk2. 10 CHANNEL MONOGRAPHIC **EQUALISER** £22.50

Control Range 110dB Dynamic Bange Maximum Output - 15dB Frequency Response 30Hz-20KHz (+1dB) 15 0 15v Power Supply 3v R.M.S Voltage Handling Input

Only 155mm x 65mm x 50mm including the 10 x 10K 1 in slider potentiometers and knobs which are mounted on a board positioned above the circuitry. In the frequency raige of 31Hz to 20kHz you can cut and boost + 12dB with the 10 siders each of which has its frequency marked on the circuit board. The GE100 has numerous uses including mixers. P.A. systems and discos. It will also greatly improve the sound reproduction of your existing audio equipment. Power Supply for GE100, ord SG30 f 3.80.

VPS30 REGULATED VARIABLE STABILISED POWER SUPPLY £8.20



Voltage Regulation 2-30v Regulated Current 0-2A Incorporating short circuit protection

This NEW versatile Regulated Variable Stabilised Power Supply with short circuit protection and current limiting is a must for a rins new versatile neglicated variable statistical supply with a current limiting range of 0.2A. With this moduling electronics enthusiasts. It incorporates adjustable voltage from 2v.30v with a current limiting range of 0.2A. With this moduling there is no need to build a separate power supply for each of your projects, with the simple addition of a transformer to 0.2033 or 10 to 10 to

PA200



£18.61

FREQUENCY RESPONSE 20Hz to 20kHz × 1dB Less than 1% (Typically 70%) TOTAL HARMONIC DISTORTION 100mV 100 K ohms For an output 3 5mV 50 K ohms 500mV SENSITIVITY -1 TAPE INPUTS 2 RADIO TUNER 3. MAGNETIC P.U 3 5mV 50 K ohms Within - 1dB from FOUALISATION 20Hz to 20kHz BASS CONTROL BANGE - 15dBs at 75Hz = 10-20dBs at 15kHz TREBLE CONTROL BANGE SIGNAL NOISE RATIO Better than b5dBs (All inputs) Better than 2dBs (All inputs) NPUT OVERLOAD SUPPLY 35 to 706v DIMENSIONS

The PA200 is basically our popular PA100. Modifications have been made to make it compatible with the higher output AL120 and AL250 amplifiers.

HEADPHONES

HEADPHONES

A top quality headphone with cushoned earpads and headband. Separate balance/volume controls. Stereo or Mono switch. Impedance 8 ohms. Frequency. 30-18.000Hz. or/n.884.69.78.p&p.70p.

A brilliant compromise between price and performance. Superb stereo reproduction for the newcomer to Hi-FI. Impedance 8 ohms. Frequency. 30-15.000Hz. or/n.885. £4.95.p&p.50p.

HI-FI ACCESSORIES

Parallel Tracking GROOV KLEEN

The very lates in automatic record cleaning. Designed to suit all modern single play docks. Simple to fit, it is extremely efficient. Complete with two types of base and three height extensions. o/n 8101. £3.97 p&p 35p.

extensions. o/n 8101. £3.97 p&p 35p.

Casenter Tape Editing Kit

Enables cassette tapes to be edited and joined easily, quickly
and accurately Kit comprises. Tape Splicer ¼" (3.2mm). 2

Precision Tape Cutters. Tape Piercer. 9 Self-adhesive Labels.
Reel of Splicing Tape. 3 Winders and removers and
instructions, all in a handy wallet. o/n 811. £2.59 p&p 35p.

GROOV-STAT.

GROOV-STAT
The BIB Groov-Stat static reducer neutralises the static charge on records and other plastic surfaces. o/n 8103. £5.89 p&p 35p.
Cassette Head Cleaner
Essential for cleaning of tape heads, capstans and rollers. Pack contains Tape Head Applicator and tape head poisher tools. Plus bottle of special formula cleaning flurd and full instructions. o/n 832. £0.72 p&p 35p.

METERS

Ministure Balance & Tuning Meter
Miniature Moving-coil meter for stereo balance indicator,
tuning indicator for FM or similar application. Pointer at
centre indicates zero or null position. Robust construction.
Sensitivity: 100–0–100MA. Dimensions 23 x 22 x 26mm
o/n 1318. £2.11 p&p 35p.

Balance and Tuning Meter Clear view adgewise mater. Centre zero application. Sensitivity: 100—0—100UA. Dimensions: 45 x 22 x 34mm. o/n 1319. £2.16 p&p 35p.



Miniature Level Meter
Moving coil, for accurate level indication for tape recorders,
amplifiers, etc. Neat design, rugged construction will
withstand five times rated value. Sensitivity: FSD. 200UA
0dB 130UA. Dimensions. 23 x 22 x 26mm. o/n 1320.
£3.02 p&p 35p.



Vu Meter
Calibrated —20 to +3 and 0-100%, making it suitable for

use as a recording level meter or as a power output indicator.

Sensitivity: 130uA. Dimensions 40 x 29vm. o/n 1321.
£2.16 p&p 35p.



AC-DC enables a large range of battery powered powered radios, recorders, calculators to be run off the mains. (220-240v AC). Switchable for 6 3x-68-9y-12v. Current rating 300MA Polarity reversing switch. Universal plug incorporated. 6/n 137 £4.05 p&p 35p.

DC-OC for use in all cars, boats, etc, with pos, or neg, earth for a regulated output of 6, 7.5v or 9 voits DC at 300MA. For radios, recorders etc. o/n 138. £3.15 p&p 35p.

CROSSOVER NETWORKS

2-WAY channels for high and low frequencies to correct speakers — high to tweeters, low to wooters. Complete with instructions. Frequency: 3,000Hz o/n 1904. E1.24 p&p. 354.
2-WAY for 8 ohms speakers up to 30 watts. Frequency: 3KHz o/n 1905. E1.85 a&p. 359.

2-WAY for 8 ohms speakers up to 30 watts. Frequency: 3KHz **o/n 1905.** £1.85 p&p 35p.
3-WAY for 8 ohms speakers up to 30 watts. Frequency?: 800Hz and 4 5KHz o/n 1906. £3.32 p&p 35p.

MICROPHONES

DYNAMIC CASSETTE

For equipment requiring a high quality microphone. Sturdy, solid moulded body in black with neat chrome surround. Pick-up pattern is omnidirectional. On/off switch. 1 metre of tough lead with floating 2.5 and 3.5mm plugs. Matching moulded strut. Impedance 200 ohms. Sensitivity: 90dB. Frequency. 90-10,000Hz. Size: 20mm dla. x 120mm o/n 1326. £1.80. p&p 35p.

DYNAMIC MICROPHONE

DYNAMIC MICROPHONE
Superior quality portable cassette recorder mike with built-in remote control switch and lead, fitted with 5-ps a 240° DIN plug (remote switch) and 3-pin DIN plug (microphone). Provides a direct replacement for those supplied with recorders. With detachable stand. Omnidirectional. Impedance. 200 ohm. Freq. response. 100 to 10,00Hz. Sensitivity: 7988 at 1,000Hz. 4/n 1327.

RE-317: DYNAMIC MICROPHONE

RE-317: DYNAMIC MICROPHONE
Highly sensitive, high-grade desk or hand mike suitable for use with many popular casset decks. Incorporates on/off switch and 1 metre lead with moulded standard jack plug. Complete with desk stand. Omnidirectional Impedance: 5,000 ohms. Freq. response: 100 at 12,000Hz. Sensitivity: (—7dB at 1,000Hz). o/n 1336. £4.48 p&p 35p.

OMNIDIRECTIONAL CARDIOID

OMNIDIRECTIONAL CARDIOID
Powered by a 1½ vb attery located within the aluminium body. Satin silver finish with front disc protection to the diaphragm housing On / Off switch. Also with Busy type windshied! "U" bracket and stem and extremely supple cable. Consumption: 0.2mA from 1½ v battery providing approx. 8-10,000 hours continuous life. Impedance 600 ohms. sensitivity; 70d8. Frequency; 30-16:000Hz. Size: 23mm dia + 267mm. o/n 1329.£14.40 p&p.35p.

UNIDIRECTIONAL CARDIOID
Dual imp. 600 and 50,000 ohms. Response 50 to 14,000Hz. Sensitivity
54dB at 50K/ohms. Size: 1½" dia x 6½" long. Weight approx. 190gm. o/n
1328. £12.32 p&p 35p.

STANDS
GOOSENECK CHROME FLEXIBLE HOLDERS
Length 320mm o/n 1333. £2.70 p&p 35p.
Length 515mm o/n 1334. £3.83 p&p 35p.
FLOOR STAND Heavy shrome. Stow away feet with rubber ends for maximum stability. Draws to a height of 5' maximum on 1335 + £10.89 p&p

85p.

BOOM ARM for use with the above stand. Heavy chromed metal, it gives 30" reach from the stand. o/n 1337 £10.35 p&p 70p.

WINDSHIELD COVERS
/n 1331 Medium per pair £1.35 p&p 35p o/n 1332 Large per pair £2.03

AUDIO LEADS

	AUDIO LEADS	
107 113	3.5mm Jack plug to 3.5mm lack plug. Length 1.5m	€0.68° €0.84°
115	to pins 3&5. Length 1.5m	£0.95
	to pins 1&4. Length 1.5m	£0.96*
116	lead. Fitted plug & ski.	£1.24"
11	7 AC mains connecting lead for cassette recorders & radios, 2 metres	£0.76
118		£1.18°
111	9 2+2 pin DIN plugs to stereo jack socket with attenua-	
120	tion network for stereo headphones. Length 0.2m Car stereo connector. Variable geometry plug to fit most car cassette, 8 track cartridge & combination units. Supplied	£1.01°
12	with inline fused power lead and instructions	£0.68*
12	4 3 pin DIN plug to 3 pin DIN plug. Length 1.5m	£1.62° £0.84°
12		£0.84'
12	7 5 pin DIN plug to 4 Phono Plugs	
12		£1.46° £0.90°
13	image. Length 1.5m	£1.18° £0.76°
13	5 pin OIN plug to 3 pin DIN plug 1&4	
13	and 3&5. Length 1.5m 2. 2 pin DIN plug to 2 pin DIN socket. Length 1.0m	£0.93°
13	3 5 pin DIN plug to 2 phono plugs	
13		€0.84
13		£0.76°
13	Connected pins 3&5. Length 23cm	£0.76°
	Black Length 6m	£1.97
17	8 AC mains lead for calculators etc. All prices inc. VAT	£0.54



Components Shop: 18 Baldock Street, Ware, Herts.



(A DIVISION OF GOTHIC ELECTRONIC COMPONENTS LTD)

PO Box 290 8 Hampton Street

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CAPACITORS Electrolytic Axi	al Lea	ds	Order Code	
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μF V d.c.	16	25	40	63
1.0				В
1.5				8
22				8
3.3				8
4 7				8
6.8			8	9
10		7		9
15	7		8	10
22		7		12
33	7		8	
47		7	10	12
68	8			
100		8	12	
150	8	9		29
220	12		24	34
330			28	37
470	19	21	30	44 50
680		28	36 55	50
1000	23	28	55	
1500 2200	32	36		
2200	39			

Electroly			Order Code	
High Rippl	e, IEC Gra	de 1, Low E.S.R.	Cap HR + µF 4	Volts
Supplied co	implete w	th Vertical Fixing Cli	p	
2200 µF	16V	Ripole 1A @ 85°C	1.4A @ 50°C	166
4700 µF	. 16V	2.6A	3.6A	184
10000 µF	16V	5.8A	8.1A	222
22000 µF	16V	9.8A	13.7A	346
2200 µF	25V	1.3A	1.8A	175
4700 µF	25V	4.6A	6.4A	201
10000 µF	25V	A0.8	11.2A	264
22000 µF	25V	12.BA	17.9A	438
1000 µF	40 V	0 9A	1.2A	168
2200 µF	40 V	2.4A	3.3A	188
4700 µF	40V	5.6A	7.8A	231
10000 µF	40V	9.2A	12.8A	367
1000 μF	70 V	1.8A	2 5A	190
2200 µF	70 V	4.0A	5.6A	235
4700 µF	70 V	7.5A	10.5A	376
1000 µF	100V	4.0A	5.6A	222
2200 µF	100V	7.8A	10.9A	346
	-			-
Electroly	tic Radia	Leads	Order Code	

	424	632	630	629	ρF	424	632	630	629	n F	424	632	630	629
					100	16	6			10	25			6
2					120	16	8			12	26"			
5					150	16	. 8			15	26			
B		. 5			180	16	6			18	27			
2		5			220	16	6			22	28			В
7		5			270	18	8			27	38			
3		5			330	18	8			33	41			
9		5			390	18		5		39	43			
7		5			470	18		5						
5		5			560	16		5						
3		5			680	16		5						
2		5			820	16		5						
		5			1000	16		5	5					
		5			1200	16		5						
		5			1500	18		6						
		5			1800	18		G						
		5			2200	18		6	8					
		5			2700	18		6						
		5			3300	18		6						
		5			3900	18		6						
		5			4700	23		7	6					
		6			5600									
		6			6800									
- 1		6			8200	23								

Tantalum Bead			Ca		rder C		
μF 0.1 0.15 0.22 0.33 0.47 0.68	3.15	6.3	10	16	25	35 9 9 9 9 9	
2.2 . 3.3 4.7 6.8		9		9 10 11	11 14 15,	11 14 15 -6	
10 15 22 33 47	11	10 11 14 15 16	11 14 16 20	14 15 16 20	16	20	
68	16	20					

10% to +5i					Cap	034 +	μF + \	oits	- 1	
μF V d.c.	6.3	10	16	25	35	40	50	63		
.68 1.0 1.5								6 6 6	1	
2.2 3.3 4.7						6		6 7	+	_
6.8			6	6		7	7	8 8		
15 22 33		6	7	8		8	10			
47 68		7	8	10	10					
100 150 220	10	8 10	10							
Trimmers			Ord	ler Co	de	_		-		

μF	352	360	PHE280	μF 1	352	360	PHE280
.001		5	6	1 1	6	8	9
.0015		5	6	.15	7	9	
.0022	5	6	7	22	8	10	
0033	5	6	7	.33	10		
0047	5	6	7	47	12		
.0068	5	6	7	.68	15		
.01	5	6	7	1.0	19		
.015	5	7	8	1.5	27		
.022	5	7	8	2.2	32		
.033	5	7	8				
.047	5	7	8				
.068	6	8	9				

D.I.L. Sockets

Heatsinks

P.C.B. Components

Suit 20mm x 5mm Lises. F.C.B. Mounting, Open Type Chassis Mounting, Open Type Panel Mounting, Screwdriver Stot Fanel Mounting, Finger Release

20mm x 5mm Glass.

Dalo Pen, Blue Ink, Slow Drying

8 Pin Low Profile Socket Tin 14 Pin Low Profile Socket Tin 16 Pin Low Profile Socket Tin 24 Pin Low Profile Socket Gold 28 Pin Low Profile Socket Gold 40 Pin Low Profile Socket Gold

Individual Type for 1 x T05 50°C/W
Individual Type for 1 x T066 10.5°C/W
Individual Type for 1 x T03 7.2°C/W
Individual Type for 1 x T03 7.2°C/W
Individual Type for 1 x T0126 17°C/W
Individual Type for 1 x T0220 17°C/W

CASES

Small Desk Console — Boss Industrial Mouldings Small Desk Console — Buss ...
Slope Front Console, Reessed Top
ABS Base, C W Brass Bushes, In Orange
Thim Aluminium Top Panel Finished Grey
Order Code



250V D.C Wkg. Film Dielectric, Miniature

VERO ELECTRONICS PROD

25" -5" -1" pilch Verobasord

3.75" -5 " 1" pilch Verobasord

5.75" -5 VERO 21069J VERO 21072D VERO 21078C VERO 21078C VERO 21078C VERO 21087E VERO 21015F VERO 21015F VERO 210178 VERO 21322C VERO 21322C VERO 213341D VERO 21341D VERO 21341D VERO 21341D VERO 21341D VERO 21341D VERO 21341D

Order Code

Cap 802 3 Cap 802 6 Cap 802 12 Cap 802 18

500V D.C. Wkg. C004 EA Tubular Type

Plastic Boxes — Boss Industrial Mouldings
Mouldert Box and Close Fitting Flanged Ltd
ABS Box C W Brass Bushes, and Ltd In Orange
Order Code

L112 W62 O31 87 L150 W80 D50 115 L190 W110 D60 195 Case BIM2003 OR Case BIM2005 OR Case BIM2006 OR



Small Desk Consoles — Boss Industrial Mouldings

Slope Front Console, Recessed Top ABS Base, C/W Brass Bushes, In Grange Imm Aluminium Top Panel Finished Grey Ventilation Slots In Base

Order Corle W105 D143 H32 (56) W170 D143 H32 (56) W170 D214 H32 (82)

VERO ELECTRONICS PRODUCTS



Plastic Boxes with Metal Lids — Boss Industrial Mouldings

Order Code
 L85 W56 D29
 97
 Case BIM4003 OR

 L111 W71 D42
 130
 Case BIM4004 OR

 L161 W96 D53
 182
 Case BIM4005 OR



W102 O140 H28 (51) 15 slope W165 D211 H33 (76) 15 slope W254 O287 H33 (76) 15 slope W356 D287 H33 (76) 15 slope W102 D140 H28 (76) 30 slope W105 D183 H28 (102) 30 slope W254 D259 H28 (102) 30 slope W356 D259 H28 (102) 30

Eurocard Size Desk Console - Boss Industrial Mouldings Slope Front Console ABS Case, C/W Brass Bushes, In Orange 1mm Aluminium Top Panet, Finished Grey W169 D127 H45 (70) 375 Case BIM8006 OR

Fuse 20 A/S Fuse 20 · Rating Lampholders, Panel Mounting Similar In Style to Fuse/H 20P Low Voltage Type Suits LES and M/F Bulbs Bulbs, Low Voltage, L.E.S. Bulb LES

Diecast Boxes - Boss Industrial Mouldings Diecast Box and Flanged Lid Aluminium Box and Lid in Natural Finish

Order Code Case BIM5003 NA Case BIM5005 NA Case BIM5006 NA

RESISTORS				
Carbon Film, Flxed				Order Code
0.25W E24 Values IRO-10M, 0.5W, E12 Values IRO-4M7,		90p/100 (Mult 10/Value) 1.25p/100 (Mult 10/Value)	£7,90/1000 (Mult 100/Value) £10,10/1000 (Mult 100/Value)	Res RD% Res RD%
Metal Film, Fixed	*			. 40106
0.5W, E24 Values, SRI IM, 29 2.5W E12 Values 10R-27K, 5		3.80/100 (Mult 10/Value) 7.90/100 (Mult 10/Value)	£32.40/1000 (Mult 100/Value)	Res MR30 Res PR52 + Value
Metal Glaze, Fixed				- Auge
0.5W, E24 Values, IM-33M. 5	% Tol. 10 ea.	5.40/100 [Mult 10/Value]		Res VR37

Skeleton Presets, Miniature		Order Code
0.1W, E3 Values, 100R-IM, Lin. Vertical Mounting 0.1W, E3 Values, 100R-IM, Lin. Horizontal Mounting	7	Min Preset V Min Preset H
Skeleton Presets, Standard		v side
0.3W, E3 Values, 100R-4M7, Lin. Vertical Mounting 0.3W, E3 Values, 100R-4M7, Lin. Horizontal Mounting	10 10	Std Preset V Std Preset H
Potentiometer, Rotary		
0.5W, E3 Values, 1K-2M2 Lin. 0.25W, E3 Values, 4K7-2M2 Log.	3 4 34	Pat Lin Pot Lou • Value

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DIGITAL INTEGRATED CIRCUITS			
4000 Buffered C-MOS - High Speed 5 15V 'B' Series, Up to 20MHz HEF4000 14 HEF4046 100 HEF4511 HEF4001 14 HEF4047 87 HEF4515 HEF4001 14 HEF4049 28 HEF4516 HEF4006 95 HEF4050 28 HEF4517 HEF4007 14 HEF4051 59 HEF4517 HEF4008 80 HEF4051 77 HEF4519 HEF4013 12 HEF4051 77 HEF4519 HEF4013 12 HEF4056 387 HEF4519 HEF4013 12 HEF4056 1387 HEF4519 HEF4013 12 HEF4056 14 HEF4518 HEF4016 50 HEF4058 14 HEF4518 HEF4017 55 HEF4070 14 HEF4581 HEF4018 60 HEF4058 14 HEF4581 HEF4019 46 HEF4071 14 HEF4531 HEF4019 46 HEF4070 16 HEF45451 HEF4010 17 HEF4070 16 HEF4551 HEF4017 18 HEF4070 16 HEF4551 HEF4018 11 HEF4070 16 HEF4551 HEF4019 46 HEF4070 16 HEF4551 HEF4010 14 HEF4081 16 HEF4560 HEF4010 14 HEF4081 16 HEF46081 17 HEF46081 18 HEF	7400 T.T.L. 250 N7400N 9 N7444N 83 N74122N 269 N7401N 11 N7445N 65 N74123N 2740 T. N7405N 11 N7445N 65 N74123N 2740 N7405N 11 N7445N 65 N74123N 2740 N7405N 12 N7465N 14 N74125N 2740 N7405N 12 N7454N 14 N74125N 2740 N7405N 12 N7454N 13 N74147N 2740 N7405N 13 N7454N 13 N74147N 2740 N7405N 13 N7454N 13 N74147N 2740 N7406N 13 N7454N 13 N74147N 2741 N7405N 14 N7475N 2741 N7415N N7475N 15 N7415N 2741 N7415N N7475N 17 N7475N 2851 N7414N 18 N7475N 28 N7415N 286 N7413N 23 N7475N 28 N7415N 287 N7414N 26 N7455N 28 N7415N 287 N7414N 26 N7456N 28 N7415N 288 N7414N 26 N7456N 28 N7415N 297 N7417N 23 N746N 28 N7415N 297 N7417N 23 N746N 28 N7415N 298 N7417N 23 N746N 28 N7415N 299 N7420N 17 N746N 28 N7415N 290 N7420N 17 N746N 28 N7415N 291 N7420N 17 N746N 28 N7415N 292 N7420N 292 N746N 293 N7416N 293 N7425N 292 N746N 293 N7416N 294 N7420N 11 N746N 23 N7416N 295 N7420N 292 N746N 293 N7416N 296 N7420N 293 N746N 293 N7416N 297 N7420N 293 N746N 293 N7416N 298 N7420N 293 N746N 293 N7416N 299 N7420N 203 N746N 203 N7416N 203 N7425N 293 N746N 293 N7416N 204 N7420N 204 N7416N 204 N7416N 205 N7420N 205 N746N 205 N7416N 207 N7420N 207 N746N 207 N746N 208 N7417N 207 N746N 207 N746N 208 N7417N 207 N746N 207 N746N 208 N7417N 207 N746N 207 N746N 209 N7420N 207 N746N 207 N746N 200 N7410N 207 N7416N 207 N7416N 200 N7420N 207 N746N 207 N7416N 200 N7420N 207 N746N 207 N746N	39	80 N74L\$490N 130 110 N74L\$670N 170 160 160 160 160 160
LINEAR INTEGRATED CIRCUITS	0PTO ELECTRONICS Order Code	65 N74LS22N 24 N74LS136N 37 N74LS251N	90 1
CA3011 92 NE592K 162 CA3018 75 RC4136 130 CA3020 191 T8A120S 79 CA3028A 86 TCA580 346 CA3048 245 TCA740 450 CA3048 245 TCA740 450 CA3089E 253 T0A1028 338 CA3089E 253 T0A1028 338 CA31306 89 TOA1028 338 CA31306 10 T0A1028 338 CA31308 10 T0A2640 202 LM318N 20 T0A2640 202 LM318N 20 T0A2640 140 LM318N 216 T0A2640 140 LM318N 216 T0A267 46 LM339N 71 UA709CN 40 LM318N 110 UA710CN 41 LM381AN 180 UA711CN 65 LM318N 180 UA711CN 65	DPTO ELECTRONICS	SWITCHES	Order Code 58
UA741CN 18 UA747CN 50 UA748CN 35	Pt. Red 230 XAN6620 C. Anode L.H. Decimal Pt. Green 230 XAN6520	SEMICONDUCTORS	
\(\)\(\)\(\)\(\)\(\)\(\)\(\)\(\)\(\)\(\	C Cahode L.M.	Diodes 1/10 1/1	61 OA202 9 15 34 19 Microwave 10 7 BAW95D 1091 7 CL8960 2592 9 CXY11C 1280
NE571N 459 UA78L15CS 32	FCDB20 150 FCDB20	Transistors	24 8 5 ×88 18
Rectifier Bridges	0-12V	20,1183	24 85X88 18 24 MPF102 32 25 MPF102 32 26 15 26 26 27 27 27 27 28 27 27 28 28 27 27 27 28 28 27 27 27 28 29 29 29 29 29 29 29 29 29 29 29 29 29 2

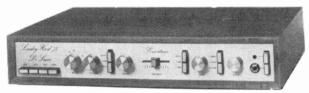
PSI 4002 STUDIO MODEL



cabinet size 17,2" x 17,2" x 6,7

COMPLETE KIT ONLY £196.90 + VAT

READ THE REVIEW IN SOUND INTERNATIONAL DEC. '78







T20 + 20 20W STEREO AMPLIFIER £33.10 + VAT

This kit, based upon a design published in Practical Wireless, uses a single printed circuit board and offers at very low cost, ease of construction and all the normal facilities found on quality amplifiers. A 30 watt version of this kit (T30 \pm 30) is also available for £38.40 \pm VAT.

POWERTRAN SFMT TUNER £35.90 + VAT

This is a simple low cost design which can be constructed easily without special alignment equipment but which still gives a first-class output suitable for feeding any of our very popular amplifiers or any other high quality audio equipment. A phase-locked-loop is used for stereo decoding and controls include switchable afc, switchable muting and push-button channel selection (adjustable by controls on the front panel). This unit matches well with the T20 + 20 and T30 + 30 amplifiers

WWII TUNER £47.70 + VAT

This cost reduced model of our highly successful Wireless World FM Tuner kit was designed to complement the T20 + 20 and T30 + 30 amplifiers and the cabinet size, front panel format and electrical characteristics make this tuner compatible with either. Facilities included are pre-aligned front-end module, switchable act, adjustable switchable muting. LED tuning indication and both continuous and push-bytton channel selection (adjustable by controls on the feets receil). the front panel)

FOR ELECTRONIC KITS OF DISTINCTION

200 + 200 watt Amplifi

As featured in Electronics Today International 400W rms continuous - 800W peak! 0.03% THD at FULL power! PLUS all the following features too!

- ★ Each channel totally independent with its own stabilised power supply driven by custom designed
- ★ Inherent reliability monster heat sinks for cool running at the hottest venues electronic open and short circuit protection!
- Ultra low feedback (an incredible low 14dB overall!), super high slewing rate (20V/µs). 200W rms continuous to 4 ohm from EACH channel, input sensitivity 0.775V (0dB).
- * Professional quality components, sturdy 19" rack mounting chassis complete with sleeve and feet for free standing work too
- Easy to build plenty of working space with ready access to all components, minimal wiring, extensive instruction suitable for both experience constructors and newcomers to electronics.
- * Value for money quality and performance comparable with ready-built amplifiers costing over

DE LUXE EASY TO BUILD LINSLEY HOOD 75W STEREO AMPLIFIER £99.30 + VAT

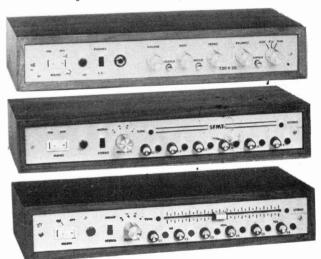
This easy to build version of our world-wide acclaimed 75W amplifier kit based upon circuit boards interconnected with gold plated contacts resulting in minimal wiring and construction delightfully straightforward. The design was published in Hi-Fi News and Record Review and features include rumble filter, variable scratch filter, versatile tone controls and tape monitoring whilst distortion is less than 0.01%.

WIRELESS WORLD FM TUNER £70.20 + VAT

A pre-aligned front-end module makes this Wireless World published design very simple to construct and adjust without special instruments. Features include an excellent a.m. rejection, push-button station selection as well as infinitely variable tuning and a phase locked loop stereo decoder incorporating active filters for "birdy" suppression.

LINSLEY-HOOD CASSETTE DECK £79.60 + VAT

This design, published in Wireless World, although straightforward and relatively low cost provides a very high standard of performance. There are separate record and replay amplifiers and switchable equalisation together with a choice of bias levels are also provided. The mechanism is the Goldring-Lenco CRV with electronic speed control.



COMPLETE KITS: Our complete kits really are complete. All of the projects shown on this page-are supplied with fully finished metalwork, ready assembled high quality teak veneer cabinet, cables, nuts, bolts, etc., and full instructions — in fact everything!

All of the kits shown on this page are available as separate packs (except the Powertran SFMT Tuner) for those customers who wish to spread their purchase or perhaps make their own cabinets or metalwork. Prices are given in our FREE CATALOGUE

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\$2.50 (VAT inclusive) per kit.

SALES COUNTER: If you prefer to collect your kit from the factory, call at Sales Counter (at rear of factory). Open 9 a.m.-4.30 p.m. Monday-Thursday

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WERTRAN ELECTRON

PORTWAY INDUSTRIAL ESTATE ANDOVER, HANTS SP10 3NM

ANDOVER (STD 0264) 64455

news digest.

CARRY-PACKS FROM JVC

A new range of equipment from JVC brings their VHS domestic video system into the portable market.

Leading the range is the HR4100 colour portable video vassette recorder, with a price tage of £799.92 including VAT' it is fully compatible with all VHS recorders and weighs only 9.3 kg, complete with cassette, battery pack and RF converter.

The new GC4100 colour video camera is a self-contained unit with the camera control unit built into the camera head. Two-tube design uses a new colour strife filter to improve colour reproduction, with an aperture correction circuit to give excellent resolution. Recording is possible with illumination as low as 100 lux. Retail price will be £934.20p.

JVC have also launched the TV41 tuner/timer, which, when connected to the HR4100,

provides all the usual record/ playback facilities of a decktype recorder, the HR 3330, is a development of the previous successful model, but also includes extra refinements such as eight day timer, remotecontrol pause switch and audio dubbing facilities.

For further information on this new video range, contact JVC (UK) Ltd., Eldonwall Trading Estate, Staples Corner, 6-8 Priestley Way, London NW2 7AF. to give







OPTO FETS

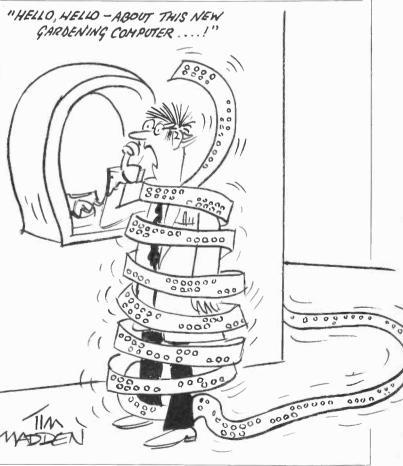
A new trio of opto-coupled FETs, available from Jermyn-Mogul Distribution, feature a minimum isolation resistance of 100 gigohms between input and output.

These new GE opto-couplers consist of a gallium arsenide infra-red emitting diode coupled to a symmetrical bilateral silicon photo detector. The detector is electrically isolated from the input and performs like an ideal isolated FET designed for distortion - free control of low level AC and DC analogue signals. They do this by varying in resistance from between 100

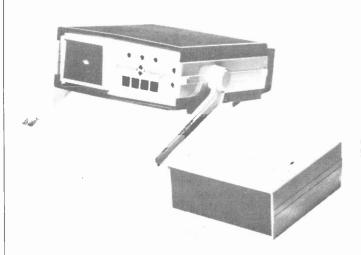
ohms to 300 megohms, the change in resistance being controlled by the amount of current flowing through the infra-red emitting diode.

Applications include isolated variable attenuators, 70 db automatic gain control, remote band switching, sample and hold circuits, optically isolated multiflexers and reed relay replacement. The H11F family come in the popular six pin DIL

For products and application sheets contact Jermyn-Mogul Distribution of Vestry Estate, Sevenoaks, Kent.



news digest.....



BARGAIN BOXES

A new service from OK Machine & Tool can save up to 65% on the cost of cases for some commercially produced items. If you need more than 1000 units, OK can incorporate your

If you need more than 1000 units, OK can incorporate your special requirements into their latest range of Pac Tec moulded enclosures, available in over 25 sizes.

As an example of the success of their new cost-cutting service, OK have been able to produce 2,500 alarm unit housings for £3.92 each, compared to £5.52 for sheet metal units. Taking the total assembly time into account, the saving rose to 65%. Customised front and rear panels can be supplied.

For further information, contact OK Machine & Tool (UK) Ltd, 48a The Avenue, Southampton, Hants SO1 2SY.

LOW KEY

A new range of enclosures designed for housing a variety of keyboards has recently been introduced by Boss Industrial Mouldings.

Bimconsoles are all-aluminium cases with a textured black base which contrasts with either the semi-gloss sand or charcoal grey top panels.

The top panels slope at about 20 to provide a relaxed keyboard operating position. Vibration is reduced to a minimum by the use of a gasket assembly between top and bottom panels.

Bimconsoles are available in three sizes and are suitable for both prototype and OEM type applications. Further details



from Boss Industrial Mouldings Ltd, Higgs Industrial Estate, 2 Herne Hill Road, London SE24 0AU.

ELECTRONIC TACHO

Orbit Controls are now producing a four decade electronic tachometer for measuring speed, rate, flowrate and frequency.

The 74A 430 has a four decade, solid state, digital readout and a pre-wired timebase, controlled by a high precision 1MHz crystal oscillator.

Flexibility of construction allows pre-wiring to any interval from 1mS to 10S. The unit features high noise immunity and freedom from false triggering counts.

The frequency range extends from 0.5Hz to 10kHz with an input sensitivity of 100mV (adjustable). Input, positive pulse or sinewave, is fully protected to 240V rms. Power may be from 100 - 110V or 210 - 260V 50/60Hz, or from 12V DC.

Further details from Orbit Controls Ltd, Lansdown Industrial Estate, Gloucester Road, Cheltenham, Gloucestershire GL51 8PL

TEST CLIPPY

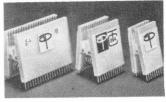
New IC test clips from Lektrokit offer a simple means of accessing any IC pin or lead.

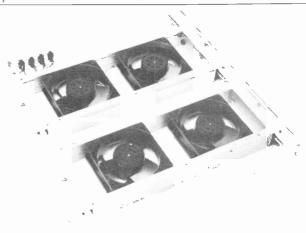
The new aid clips over the IC bringing its individual pin connections out to a set of contacts at the opposite end of the clip. There are test clips available to match 8, 14 and 16 pin DIL packages.

pin DIL packages.

The gold-plated, phosphor bronze spring contacts have been designed to achieve a wiping/cleaning action, making

The TC-14 which, as its name suggests, clips over a 14 pin DIP, costs £2.95. Further details from Lektrokit Ltd., Sutton Industrial Park, London Road, Earley, Reading, Berkshire RG6 1AZ,





COOLING OFF

Got any hot-spots in your cabinets? You can get the air circulating round your equipment with the Vero Electronics Fan Tray (AB 087).

Two versions (1U and 2U)

Two versions (1U and 2U) are available for either 115V or 230V (50/60 Hz) input. Each is supplied with four 119mm square axial fans, but

additional fans can be fitted as required.

The 2U version has a polyurethane foam filter covering the air intake. If your living room or office isn't a smokeless zone, never fear, the filter is cleanable. Both versions operate at low noise levels

at low noise levels.

If you need cooling off, contact Vero Electronics Ltd, Industrial Estate, Chandler's Ford, Hampshire SO5 3ZR.

Measure Resistance to 0.01 \(\Omega \) At a Price that has no resistance at all

New ELENCO PRECISION Digital Multimeter M1200B

NLY £55 (+£3 p&p+VAT£4.64 =£62.64)

*FULLY GUARANTEED FOR 2 YEARS

*METAL CASE

*EX STOCK DELIVERY (Subject to availability)



THE ULTIMATE IN PERFORMANCE - MEASURES RESISTANCE TO 0.01 OHMS, VOLTAGE TO 100 MICROVOLTS, CURRENT TO 1 MICROAMPS AT LOWEST EVER PRICE!

FEATURES

- 3½ digits 0.56" high LED for easy reading
- $100 \mu V$, $1 \mu A$, 0.01Ω resolution
- High input impedance 10 Megohm
- High accuracy achieved with precision resistors, not unstable trimpots
- Input overload protected to 1000V (except 200mV scale to 600V)
- Auto zeroing, autopolarity
- Mains (with adaptors not supplied) or battery operation-built-in charging circuitry for NiCads
- Overrange indication
- Hi Low power ohms, Lo for resistors in circuit, Hi for diodes

	A ACTO CALADORICA
	SPECIFICATIONS:
DC Volts	Range 200mV, 2V, 20V, 200V, 1000V
	Accuracy 1% ± 1 digit, Resolution .1mV
	Overload protection 1,000 volts max
AC Volts	Range 200mV, 2V, 20V, 200V, 1000V (Response 45Hz to 5KHz)
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Accuracy 1.5% ± 2 digits, Resolution .1mV
	Overload protection 1000V max, 200mV scale 600V
DC Current	Range 2mA, 20mA, 200mA, 2amp.
	Accuracy 1% ± 1 digit, Resolution 1 Microamp
	Overload protection 2 amp fuse and diodes
AC Current	Range 2mA, 20mA, 200mA, 2 amp
	Accuracy 1.5% ± 2 digits, Resolution 1 Microamp
	Overload protection - 2 amp fuse and diodes
Resistance	Range 20, 200, 2K, 200K, 2 Meg. 20 Meg.
	Accuracy 1% ± 1 digit, Resolution .01 ohms
Environmental	Temp coefficient 0° to 30° C ± .025%° C
_	Operating Temp 0° to 50° C Storage - 20° to 60° C
General	Mains adaptor: 6 - 9 Volts @ 200mA (not supplied)
	4C size batteries (not supplied)
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33/35 CARDIFF ROAD, WATFORD, HERTS, ENGLAND	AC125* 20 BC170 18 BF179* 30 MPSU02 58 TIS46 45 2N2220A* 26 AC126* 20 BC171 11 BF180* 35 MPSU05 50 TIS47 50 2N2221A* 23
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POLYESTER CAPACITORS: Axial lead type. (Values are in µF). 400V: 0-001, 0-0015, 0-0022, 0-0033, 0-0047, 0-0068, 0-01, 0-015, \$p; 0-018 10p; 0-022,	ACY44* 39 BC214L 10 BF394 27 OC70* 28 ZTX326 40 2N3108 32 AD149 70 BC307B 14 BF594 40 OC71* 28 ZTX341 20 2N3442* 140 AD161* 42 BC308 13 BF595 38 OC72* 45 ZTX540 15 ZN3563 20
0-033, 11p; 0-047, 0-068 14p; 0-1, 17p; 0-15, 0-22, 24p; 0-33, 0-47 42p; 0-68 48p. 160V: 0-039, 0-15, 0-22 11p; 0-33, 0-47 19p; 0-68, 1-0 22p; 1-5 29p; 2-2 32p. 4-7 48p.	AD161* 42 BC327 15 BFR39 25 OC75* 45 ZTX500 15 ZN3563 20 AF106 50 BC328 15 BFR40 25 OC75* 45 ZTX502 19 ZN3615* 289
DUBILIER: 1000V: 0-01, 0-015 20p; 0-022 22p; 0-047 26p; 0-1 36p; 0-47 46p. POLYESTER RADIAL LEAD (Values in μF). 250V: FEED THROUGH	AF114* 40 BC338 12 BFR41 28 OC76* 36 ZTX503 15 2N3663* 26 AF115* 40 BC441* 36 BFR79 28 OC77* 76 ZTX504 26 2N3702 11
0-01, 0-015, 0-022, 0-027 5p; 0-033, 0-047, 0-068, 0-1-7p; 0-15 11p; 0-22, 0-33 CAPACITORS 13p; 0-47 17p; 0-68 19p; 1-0 22p; 1-5 30p; 2-2 34p. 1000pF/350V 8p.	AF116* 40 BC461* 36 BFR80 28 OC79* 76 ZTX531 25 2N3703 11 AF117* 40 BC477* 25 BFR81 28 OCB1D* 50 ZTX550 25 2N3704 11
ELECTROLYTIC CAPACITORS: Axial lead type (Values are in µF). 500V: 10 40p; 47 68p; 250V: 100 65p: 63V: 0.47, 1.0, 1.5, 2.2, 3.3, 4.7, 6.8, 8, 10, 15, 22, 8p; 47, 32, 11p; 63, 100, 27p; 50V; 50, 100	AF121+ 48 BC548 12 BFX29+ 28 OC83+ 48 40251+ 97 2N3706 11
7p; 330, 470, 32p; 1000, 50p; 40V; 22, 33, 8p; 100, 12p; 2200, 3300, 68p; 4700, 85p; 35V; 10, 33, 7p; 330, 470, 32p; 1000, 50p; 25V; 10, 22, 47, 6p; 80, 100, 160, 8p; 220, 250, 13p; 470, 640, 25p;	AF125* 35 BC557 15 BFX84* 28 OC122* 75 40313* 125 2N3708 11 AF126* 50 BC558 20 BFX85* 28 OC123* 75 40315* 56 2N3709 11
14p; 470, 16p; 1000, 1500, 20p; 2200, 34p; 10V: 100, 6p; 640, 12p; 1000, 14p; 100, 12b, 8p; 220, 330, 14p; 470, 16p; 1000, 14p, 170, 170, 170, 170, 170, 170, 170, 170	AF127# 35 BC559 20 BFX86# 28 OC139# 110 40316# 85 2N3710 16 AF139# 35 BCY30# 57 BFX87# 28 OC140# 110 40317# 52 2N3711 12
15,000 299p. 25V; 4700 68p; 2000 48p; 40V: 2000 + 2000 95p.	AF178* 70 BCY34* 75 BFX88* 28 OC141* 110 40319* 71 2N3771* 275 AF180* 70 BCY39* 80 BFY18* 50 OC170* 85 40320* 56 2N3772* 195
TANTALUM BEAD CAPACITORS POTENTIOMETERS (AB or EGEN) 35V: 0.1 µF, 0-22, 0-33, 0-47, 0-68, Carbon Track, WW Log & 1/2 W Linear ELECTRONICS *	AF239# 42 BCY42# 48 BFY51# 20 OC200# 85 40324# 85 2N3819 22
1-0, 2.2μF, 3-3, 4-7, 6-8-25V: 1-5, 10. values 500Ω 1ΚΩ & 2ΚΩ (lin, only) single. LEDs with Clips gang 27pi TIL209 Red 13p	ASY26* 40 BCY58* 90 BFY53* 28 0C204* 85 40327* 62 2N3823* 95 ASY27* 45 BCY59* 90 BFY53* 28 0C204* 85 40327* 62 2N3823* 95
10V: 15, 22 28p. 47, 100, 220 40p. 1 KG-2MG single gang 27p TIL211 Gri 17p 10V: 15, 22, 33, 20p; 100 35p. 5KG-2MG single gang D/P switch 65p TIL212 Yellow 18p 5KG-2MG dual gang stereo 78p· . 2" Red 14p	ASY76 # 95 BCY70 # 16 BFY64 # 40 TIP29 43 40348 # 106 2N3866 # 90 ASY76 # 95 BCY71 # 20 BFY71 # 20 TIP29A 44 40360 # 43 2N3903 20
MYLAR FILM CAPACITORS SLIDER POTENTIOMETERS Yellow 18p	ASZ21 60 BCY72* 20 BRY39* 39 TIP29B 56 40361* 45 2N3904 18 BC107* 9 BCY78* 25 BSX20* 18 TIP29C 60* 40362* 48 2N3905 18
1000: 0-001, 0-002, 0-005, 0-01μF	BC1078+ 10 BCZ11 145 BSX26+ 75 TIP30 47 40406+ 65 2N3906 17 BC1088+ 9 BD115+ 65 BSX29+ 45 TIP30A 50 40407+ 52 2N4037+ 52 BC1088+ 10 BD121+ 78 BSX78+ 55 TIP30B 64 40408+ 70 2N4041+ 80
10 10 10 10 10 10 10 10	BC108C# 12 BD123* 98 BSY95A* 18 TIP30C 65 40411* 295 2N4058* 17 BC109* 9 BD124* 115 BU105* 140 TIP31* 50 40412* 65 2N4061 17
Renges: 0-5pF to 10,000ρF 3p 0-015μF, 0-022μF, 0-033μF 4p PRESET POTENTIOMETERS 0RP11 85p 0R12 63p 0R12 63p	BC1098* 12 BD131* 45 BU205 190 TIP31A* 52 40467* 95 2N4062 17 BC109C* 12 BD132* 45 BU208 228 TIP31B* 58 40594* 90 2N4064* 120
0.147 b 4p; 0.1 \(\psi \) 5p 0.1\(\psi \) 5p 0	8C113 20 BD133* 43 E421 150 TP31C* 66 40595* 98 2N4069 45 8C114 20 BD135* 36 E113* 95 TP32* 56 40603* 66 2N4236 145
6-8, 10, 12, 18, 22, 33, 47, 50, 68, 75, 82, 85, 100, 120, 150, 220 peach TIL307 TIL307 TIL307 TIL312 .3" CA 105p	3C115 20 8D136* 40 55567 65 TIP32A* 58 40636* 125 2N4286 20- 3C116 20 8D137* 40 MD8001* 158 TIP32A* 70 40673* 68 2N4289 20 3C117 20 8D138* 50 ME1120 25 TIP32C* 75 2N997* 25 2N4859 66
250, 270, 300, 330, 360, 390, 470, 600, 800, 820 16p each Miniature High Stability, Low noise TIL313, 3" CC 105p TIL321, 5" CC 115p	3C118 20 8D139* 40 ME4102 10 TIP33* 80 2N698* 44 2N4922* 55 3C119* 28 8D140* 36 ME6002 10 TIP33A* 85 2N699* 54 2N5135 42
POLYSTYRENE CAPACITORS: 100 200 4 7M 524 150 100 100 100 100 100 100 100 100 100	3C134 20 BD142* 59 MJ400* 90 TIP33B* 100 2N706A* 19 2N5136 42 3C135 20 BD144* 196 MJ491* 160 TIP33C* 106 2N707* 39 2N5138 20
10pF to 1nF 8p; 1.5nF to 47nF 10p	C137 20 BD181* 125 MJE340* 54 TIP34A* 85 2N914* 32 2N5179* 60 3C140* 35 BD205* 110 MJE370* 58 TIP34B* 110 2N916* 27 2N5180* 60
2.5-6pF, 3-10pF; 10-40pF 22p 2%Metal Film 10Ω-1MΩ 6p 4p 3"Green. CA 180p 5-25pF; 5-45pF; 60oF; 88oF 30p 1960.5W 51Ω-1M E24 10p 8p 6"Green. CA 225p	C142* 30 BD378* 65 MJE371* 60 TIP34C* 110 2N918* 40 2N5191* 70 8C143* 30 BD434 42 MJE520* 65 TIP35* 179 2N920* 61 2N5305* 40
COMPRESSION TRIMMERS 100+ price applies to Resistors of each LCD 3½ Digit 875p LCD 4 Digit 975p LCD 4 Digit	16.147 8 80517* 65 MJE521* 74 T1P35A 185 2N930* 18 2N5457 32 16.1478 10 80695A* 65 MJE2955* 99 T1P35B* 195 2N1131* 22 2N5458 32 16.148 8 806996A* 65 MJE2955* 70 T1P35G* 220 2N1132* 22 2N5459 32
100-500pF 45p; 1250pF 65p THERMISTORS: VA1034, 1039, 1174 48p	xc148 8 BD6996A* 65 MUE3055* 70 TP35C* 220 2N1132* 22 2N5459 32 10 BDY11 220 MPF102 66 TP36* 210 2N1303* 50 2N5485 35 10 BDY17* 196 MPF103 35 TP36A* 220 2N1304* 90 2N5777* 45
TGS 812 & 813 415p; Socket 25p 1098, 1100 20p each. TIL111/2 85p TIL1114 95p	C149 8 8DY60* 110 MPF104 36 TIP366* 230 2N1305* 28 2N6027 40 C149C 10 BDY61* 165 MPF105 36 TIP36C* 255 2N1306* 36 2N6109 50
Dielectric 0 2 365pF with slow	IC153 27 BF115* 34 MPF106 40 TIP41A* 63 2N1307* 50 2SD234* 50 IC154 27 BF154* 25 MPF107 50 TIP41B* 73 2N1308* 46 3N128* 112
100/300pF 140p motion Drive 325p AA119 18 RECTIFIERS Evaluation - 165p 00 208/176 285p AAZ15 15 (plastic case) p Kith	C157 10 BF158* 29 MPS3904 40 TIP42A* 64 2N1613* 23 3N140* 112 U158 11 BF160 30 MPSA05 25 TIP42B* 82 2N1670* 150 C159 11 BF161 60 MPSA06 25 TIP2955* 65 2N1671B* 215 Meliched
4511/DAF 115p* motion drive 325p. BY126 12 14/100/ 20 (ED 2635p	25 111 2500 11
Dial Drive 4183	C160± 42 BF167 30 MPSA12 42 TIP3055± 60 2N2160± 350 Pmi C167A 11 BF173± 25 MPSA55 25 TIS43 34 2N2217± 43 20pm
Dial Drive 4183 C804-5pF: 10: 15: 8Y127 12 1A/200V 22 LINEAR Cs 1CM7 Drum 54mm 30p* 100, 150pf 235p 0A9 75 1A/200V 29 LINEAR Cs 1CM7 702 75 CM7	C167A 11 BF173* 25 MPSA55 25 TIS43 34 202277* 43 20p = 1074 7482 69 74175 87 42 98 175 110 1774* 790 NE5654* 120 - 7482 69 74175 87 42 98 175 110 1774* 790 NE5654* 120 - 7482 69 74175 87 47 63 181 398
Dial Drive 4183 C804-5pt 10:15 87127 12 1A/200V 22 189 127 16 16 17.36:1 650pt 25 50pf 175pt 10:15 601/36:1 6400 25 50pf 175pt 10:15 601/36:1 6400 25 60pf 10:15 60pf	C167A 11 B173* 25 MPSA55 25 TIS43 34 202217* 43 20p m C167A 1050 NE5664* 425 TIL 74 7482 69 74175 87 42 98 175 110 C17A* 790 NE566* 160 TEXAS 120 1483 72 74176 75 47 63 181 398 C167A* 790 NE566* 160 TEXAS 120 132 298 120 132 298 C167A* 790 NE567* 170 7400 11 7485 106 74180 85 49 120 190 140 C167A* 790 NE567* 170 7400 11 7485 106 74180 85 49 120 190 140 C167A* 790 7400 7485
Dial Drive 4183	C167A 11 B173* 25 MPSA55 25 T1543 34 202277* 43 20p m 2174* 7482 69 74175 87 42 98 175 110 2174* 7483 72 74176 75 47 63 181 398 74175 75 75 75 75 75 75 75
Dial Drive 4183	C167A 11 BF173* 25 MPSA55 25 T1543 34 202217* 43 20p m
Dial Drive 4183	
Dial Drive 4183	C167A 11 BF173* 25 MPSA55 25 T1543 34 202277* 43 20p m
Dial Drive 4183	C167A 11 BF173* 25 MPSA55 25 T1543 34 202277* 43 20p m
Dial Drive 4183	C167A 11 BF173* 25 MPSA55 25 T1543 34 202277* 43 20p m
Dial Drive 4183	C167A 18 B173
Dial Drive 4183	C167A 18 B173
Dial Drive 4183	C167A 11 BF173
Dial Drive 4183	
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Dial Drive 4183	C167A 11 BF173
Dial Drive 4183	C167A 11 BF173
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	2	-						
JAC	K PLUG	5		SOCKETS	TOGGLE: 2A. 2			
2.5mm 13p 1: 3.5mm 15p 1: MONO 25p 1		Plastic body 10p 10p 14p 17p	open metal 8p 8p 13p 15p	moulded with break contacts 20p 24p	in line couplers 11p 12p 17p 22p	SPST DPST DPDT 4 pole on / off SUB-MIN TOG SP changeover		
		P	LUGS	SOCKETS	in Line	SPST on / off SPST biased		
			10p 15p	7p 10p	20p 20p	DPDT 6 tags DPDT centre of DPDT Biased		
			14p	14p	14p	ROTARY: M.		
		10p		Sp single Sp double 15p 4-way	12p 20p	Adjustable Stomodate up to Mains Switch Break Before		
				12p 10p 6p	=	2p/6 way. 3p Spacegrand Spacegrand Spacegran		
			8p 15p 15p	8p 20p 15p		1 pole/2 to pole/2 to 4 v ROTARY: M		
DM9	00	TI 6-	1ANSF0	RMERS+ (Ma	ns Prim. 2 100mA	20-240V) 95p		

OGGLE: 2A, 250V. SPST 28p OPST 34p OPDT 38p	1A DPDT c/over 15 1/2A DPDT 13 4 pole 2-way 24
OPDT 38p Ipole on / off 54p	PUSH BUTTON
BUS-MIN TOGGLE SP changeover 59p SPST on/off 54p SPST biased 55p DPDT centre off 79p DPDT Biased 115p	Spring loaded SPST on / off 60 SPDT c / over 55 DPDT 6 Tag 85 MINIATURE Non Locking Push to Make 15 Push Break 25
ROTARY: Make your	own multiway Switch.

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Spacewand Screen 5p
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18p 15p ROTARY
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D44000	TRANSFORMERS& (Mains Prim. 220-240	M ALUM.	PANEL
DM900 3½ DIGIT LCD Multimeter with Capacitance Meter (ETI Aug. 78) Complete Kit £54.50 * only (p&p 80p)	S.O. B.V. 9.O. 9V. 12.O-12V 100mA BWA: 6V. 5A. 6V. 5A; 9V. 4A, 9V. 4A, 12V 12V. 3A; 15V. 25A 15V. 25A 12V. 4.5V. 13A; 4.5V. 13A; 6V.1.2A 6V.1 12V. 5A 12V. 5A; 15V. 4A 15V. 4A; 20V 20V. 3A 220° 20V. 3A 12V. 15V. 15A; 9V. 15A; 9V. 13A 9V.1 12V.1A; 15V. 8A; 15V. 8A; 20V 20V. 6A 20V. 6A; 9V. 15A; 9V. 25A; 9V. 25A; 20V 20V. 6A; 9V. 4A; 9V. 4A; 9V. 25A; 9V. 25A; 20V 20V. 6A; 9V. 4A; 9V. 4A; 9V. 25A;	95p/ .3A BOXES ★ WITH LID' p .1.2A, √.3A p&p) 4x4x119'' 68 .3A: 4x25x11'' 88 .4x51x11'' 88 .4x51x11'' 88 .4x51x2'' 84 .4x51x2'' 92	METERS* FSD 60x46x 35mm 0.50μA 0.100μA 0.500μA 0.1mA 0.5mA 0.10mA
CRYSTALS★ 100KHz 385 455KHz 385 1.0008M 306 3.2768M 323 4.032MHz 323 4.433619M 135	12V-2A, 15V-1, 5A, 15V-1, 5A, 20V-1, 2A 1, 2A, 25V-1A, 25V-1A, 30V-8A, 30V-8A 350p (50p 100VA: 12V-4A, 12V-4A; 15V-3A, 15V 20V-2, 5A, 20V-2, 5A, 30V-1, 5A, 30V-1 40V-1, 25A, 40V-1, 25A; 50V-1A, 50V-1A (60p p&p), (M. B, p&p charge to be added in our normal postal charge.)	7x5x2½" 129 8x6x3" 168 10x7x3" 199 10x4½x3" 162 12x5x3" 190 12x8x3" 260	0-50mA 0-100mA 0-500mA 0-1A 0-2A 0-25V 0-50V AC
5.0MHz 355 8.08333M 276 10.0MHz 323 10.7MHz 323 18.432M 323 20.0MHz 323 27.648M 323 48.0MHz 323	VOLTAGE REGULATORS ★ 1A TO3 + ve -ve 5V 7805 145p 7905 220p 12V 7812 145p 7912 220p 15V 7815 145p 7912 220p 18V 7818 145p - 18V 7818 145p 1A T022D Plastic Casing 5V 7805 80p 7905 90p	2102-2 170 , 2107B 490 2111 175	"S" "VU" 475p each 41/4x31/4x11/2" 0-50 μ A 0-500 μ A 0-500 μ A
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ULTRASONIC TRANS- DUCERS	LM305H 140p LM723 4.3 LM309K 135p MVR5 180 LM317K 350p MVR12 180 LM323K 625p TAA550 50	74S287 325 TM 74S470 325 TM 74S475 825 TM	AS6011 320 AS9900 3500 AS9980 1989 80 1199

5p for list		15V		30p	79L M327	-	00	74L75 74S188	165	TMS4042 TMS4045	240
ULTRASC TRANS- DUCERS 450p* pe		LM30! LM30! LM31 LM32: LM32 LM32	5H 140p 9K 135p 7K 350p 3K 625p 5N 240p	, N	M723 AVR5 AVR12 AA550 BA625B DA1412	18 18 5	Op Op Op	74\$262 74\$287 74\$470 74\$475 81L\$95 81L\$96	876 325 325 825 99 99	TMS6011 TMS9900 TMS9980 Z80	325 3500
393 230 395 218 396 215 398 276 399 230 445 150 447 144 490 180 668 182 669 182 670 248 CMOS★	4018 4019 4020 4021 4022 4023 4024 4025 4026 4027 4028 4029	87 48 98 91 88 20 66 19 180 45 81	4046 4047 4048 4049 4050 4051 4052 4053 4054 4055 4057 4059 4060	128 87 58 48 48 72 72 72 110 128 1950 480 115	4085 4086 4089 4093 4094 4096 4097 4098 4099 4160 4161 4162 4163	74 73 150 85 190 105 372 110 145 109 109	445 445 449 449 450 450 450 450 450 450 451	1 295 2 0F 695 0V 525 1 19 2 120 3 69 6 51 17 55 8 298 0 99	MODU Corwert using the TV-CRT SF.F963 characte Cursor managel erasing computi	rs text ref managemen ment on so Compatible ng system	a VDU by npson-CSF er chip ne by 64 freshment, nt. Cursor treen, Line
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news

LATEST CASIO MINIS

Casio have managed to reduce their successful LC-78G calculator in three ways.

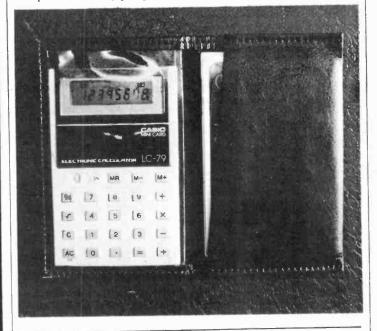
First of all - price. The RRP of the LC-78G is down by £3.00 to £16.95.

Second is the new Casio LC-7 which has the same display and functions except that the fully independent memory is replaced by a simple automatic accumulating memory and a square root function. The LC-78S has a RRP of only £13.95.

Thirdly, thickness has been cut down from four to two millimetres. Casio's new Mini Card LC-79 remains credit card size, but in upright format. It keeps eight digits capacity and LCD, four functions and independent memory plus perfect percent and function indicator. Also featured is a responsive, 'feather touch' keyboard, so light that it can be operated inside its protective wallet. A battery-conserving circuit automatically switches off nine minutes after the last key depression. The Casio LC-79 will retail at £19.95 (or less, if you're lucky).

If you prefer something a bit beefier, try the LC-841, another new one from Casio. With the same technical features as Mini Cards (including independent memory), the LC-841 is 62 x 110mm, but still only 3.9mm thick, with digits 6mm high, and will retail at about £15.95.

For enquiries, get in touch with Casio Electronics Co Ltd, 28 Scrutton Street, London EC2A 4TY



MILITARY FLASHER

Need a tough twinkler? Oxley are now producing a solid state indicator lamp, type PS/LH/8, in a military style rugged mounting.

The mounting incorporates the latest high brightness, high reliability LEDs. The lamp is fitted with a sealed glass lens and black shroud to optimise the visual effect and afford emitter protection.

Standard colours are available, red, yellow and green, and light output is calibrated to photometric standards to ensure consistent performance. The aluminium alloy body is compatible with standard chassis and provides electromagnetic shielding for military applications. Further details from Oxley Developments Co Ltd Ulverston, Cumbria LA12 9Qg.

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T.V. GAMES

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This TV Game can be compared to an audio cassette deck and is programmed to play a multilude of different games in COLOUR, using programmed to play a multitude of different games in volucion, same variesc plug in carbridges. At loog last a 17 yame is available which will knop pace with improving technology by allowing you to extend your Harary at games with the perchase of additional carbridges as new yames are developed. Each carbridge contains up to ten different action games and the first carbridge containing ton sports games is included free with the console. Other carbridges are currently table to enable you to play such games as Grand Prix Motor mg. Super Wipeout and Stunt Rider, Further cartridges are to be send later this year, including Tank Bettle, Hunt The Sub, and Target. The console cames compilete with two removable joystick player controls to enable you to move in all four directions top/down/right/left) and built into those joystick controls are built carve and target fire buttons. Other is abres include several difficulty option switches, automatic on across digital scering and colour coding on scenes, into and balks. Lifelike sounds transmitted through the TV's

simulating the actual game being played. ctured by Waddingtons Videomas naster and guaran-



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CHESS COMPUTERS



THE WADDINGTONS VIDEOMASTER STAR CHESS - £59.50 inc. VAT PLAY CHESS AGAINST YOUR PARTNER

PLAY CHESS AGAINST YOUR PARTNER using your own TV to display the board and pieces Star Chess is a new absorbing TV games for two players, which will infarest and excite all ages. The unit gives into the aerial socket of your TV set and displays the board and pieces in full colour (or black and white) on your TV screen, 8 ased on the moves of chess. It adds even more excitement and infarest to the game, For those who have never played. Star Chess is a novel introduction to the classic game of chess. For the experienced chess player, there is a whole new dimensions of unpradictability and chance added in the strategy of the game. Not only can pieces be taken in conventional chess type moves; but each piece can also exchange rocket fire with its opponents. The unit comes camplets with a linear law mains adaptor, full instructions and twelve model in garantee.

CHESS CHAMPION 6 - £89.50 inc. VAT

CHESS CHAMPION 6 - £89.50 inc. VAT PLAY CHESS AGAINST THE COMPUTER -6 LEVELS

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World chess champion AMATOLY KARPOV says:

"This chess computer is a new and interesting partner with remarkable game variations."

This chess computer is a new and interesting partner with remarkable game variations.

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Challenger 10 but unit has only 7 fevels of play.] Price includes unit with
wood grained housing, and Stainton design chess pieces. Computer plays
black or white and against itself and comes complate with a mains adaptor
and 12 months, ourrantee.

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BORIS - 4

(Chess Challenger 10 ittustrated above)





BORIS - £178.50 inc. VAT
Borts is an advanced chess computer that's programmed
for all classic chess moves. He will play Black or White,
even himself. He'll even leach you how to play chess and even himself. He'll even teach you how to play chess and suggests the moves for you when you're unsure of what lot do next. Boris can talk to his opponent through his alphanumeric display and will litash different messages during each game to keep you on your toes. Boris will not allow allegal moves, and will allow you to enter problems or set up your own board positions. Boris comes in hand crafted, solid welenut case with chess pieces and board. Comes complete with a mains adaptor and 12 months our analyse.

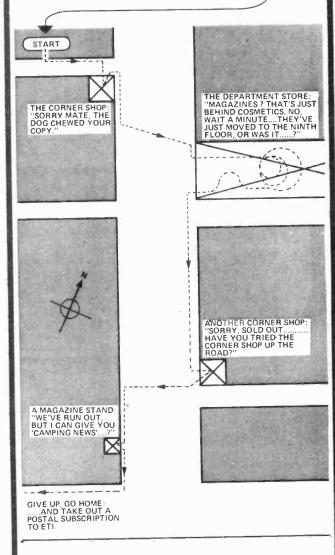
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Apple II



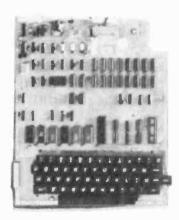
Apple II was the original with full colour high resolution microcomputer Basic, and it is still the best. With a very wide range of expansion available, including disk drive, interface cards, voice recognition card, light pen and many others.

Apple II has been well tried and approved by the public (over 200,000 sold) because of its thoroughly professional design and high quality engineering. You cannot get better value for money. Please send us a large s.a.e. for further details.

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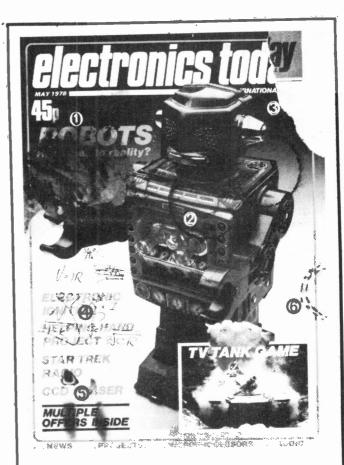
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- 1: The bit of chocolate you thought you'd leave for later.
- 2: Coffee stains (instant).
- 3: A useful-sized bit of stiff paper to stop the window from rattling.
- 4: Rough calculations for your new combined egg timer/laser cannon project.
- 5: ETI makes a fair soldering iron stand.
- 6: The dog insisted on carrying your copy to you along with your slippers.

WHAT A BIND!

Half our orders for binders are repeats: we think that says a lot for their quality. At £3.00 all inc. you get a great deal of peace of mind too!

ETI Binders 25-27 Oxford Street, London W1R 1RF.

GENTLEMEN the PET DISK has landed...



The U.K. designed and manufactured Novapac disk system for Commodore's PET*, first seen at Compec '78, is (after extensive industrial evaluation), now available to the domestic user. Its unique saddle configuration continues the integrated design concept of your PET, with no trailing wires or bulky desktop modules.

- Novapac may be used with any available RAM plane.
- Data transfer takes place at 15,000 char/sec effectively 1000 times faster than cassette!
- Storage capacity is 125 K/bytes (unformatted) on 40 tracks per diskette side
- Dual index sensors permit dual side recording for 250 K/bytes per diskette
- Easy operation full width doors prevent media damage.
- System expandable to ½ M/byte on-line storage (4 drives). Dual head and 2D versions provide 2 M/bytes on-line.
- Industry Standard IBM 3740 recording format for industry-wide media compatibility only offered by NOVAPAK
- Dedicated Intel 8048 microprocessor and 1771 FDC minimise
- PET software overhead
- Local hardware and software support available.

The sophisticated Disk Operating System is disk resident, which allows for future DOS enhancements without hardware alter-PDOS supports multiple file handling, dynamically allocating disk space to each as and when necessary. Any file may occupy from 1 to 600 sectors as required, at up to 16 non-contiguous locations on the disk, PDOS may be used alone, or within a BASIC program, and offers user-specified password security for any file. Multiple access-modes simplify BASIC program construction.

Novapac dual-disk system complete with PDOS and BASIC demonstration programs on disc £950 + VAT. Available from the manufacturer or selected dealers.

Terms; 50% with order, balance on delivery Full cash with order is subject to 5% discount VAT-FREE Export arranged (Must be shipped by us)

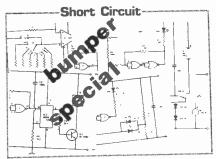
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Hobby Electronics

BUMPER SHORT CIRCUIT ISSUE



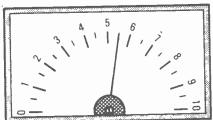
Look out this month for more than your usual share of our very popular. Short Circuit feature. Plenty of circuit designs for you to develop and experiment with.

SHARK



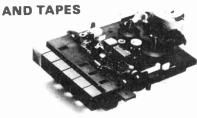
Not a game for the nervous. An LED-based game for two players which involved two swimmers in a race for survival in a shark-infested sea. Which of these two castaways will reach the safety of the island? The unfortunate one is swallowed by the hungry shark, accompanied by a shrill scream. All good family fun!

LINEAR SCALE OHMMETER



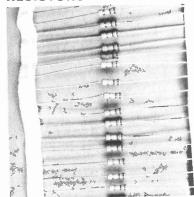
If you ever look at a multimeter on the ohms range you'll notice that most of the numbers are all squashed up one end; this makes accurate readings difficult. The HE Ohmmeter overcomes this difficulty with a linear scale. The range of resistance covered is from 1 k to 1 M ohms in four ranges, a useful addition to any workshop's range of test equipment.

CASSETTE DECKS



Next to the TV and Transistor radio, the Cassette tape recorder is probably the most common piece of domestic electronic equipment. Next month Gordon King takes a close look at what has made the Compact Cassette so popular and one or two of its advantages and drawbacks, warts and all.

RESISTORS



Following the success of our feature on Capacitors (according to our reader questionnaire) we're doing a follow up on the ins-and-outs of Resistors. Like Capacitors it's *not* going to be a formula-strewn study but a rather slanted look into their construction and use. So if you've never heard of Thick Film resistors and Metal Oxide, now's your chance.

HOBBY CHIT CHAT

Ray Marston our Project Editor / Designer starts a new monthly series looking at our fast-moving hobby from the technical point of view. These articles are designed to take a look into the worlds largest growth industry, what's new and how it will affect us in our daily lives as well as a more specific look at our own side of the fence in HE.

KIT REVIEW



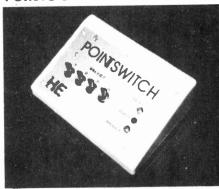
Month

One for the motorist this month, we have built up an Electronic Ignition system from Sparkrite (X4); read all about it next month.

LINEAR ICs

If you've been wondering what's going to happen now Into Electronics has finished, don't worry. Ian Sinclair has begun his follow-up series Linear ICs. Month by month the articles will introduce most aspects of IC use, construction and theory. With the background knowledge gained from Into Electronics your understanding of new technology should increase dramatically.

POINTS CONTROLLER



Another project for model railway buffs. This unit gives full control over an unlimited number of electro-mechanical points using a pushbutton control. This makes an ideal companion to our HE Model Train Controller featured in the April issue.

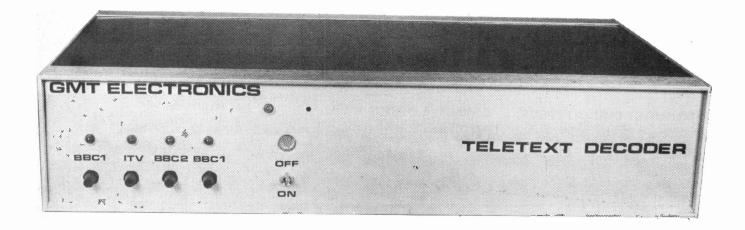
BABY ALARM

A really simple project to keep one ear on the kids whilst you're building your latest HE project.

The July issue will be on sale June 8th

The items mentioned here are those planned but circumstances may affect the actual contents

TELETEXT SYSTEM



A complete ultrasonic controlled Teletext design employing the newly released Mullard chip set. Design by GMT Electronics for ETI. Facilities include double size characters and video superimpose.

THIS PROJECT is designed to allow the home constructor to produce himself a full spec Teletext unit at around half the cost of comparable commercial units. The design requires no hard wiring into the set, as it contains its own modulator and works into the aerial socket. Definition usually suffers utilising this method, but here great attention has been paid to overcoming this problem.

As with all decent designs remote control is ultrasonic, and gives both full and half page displays. The keyboard arrives already fitted to the PCB, and only needs the decoder chip and transducer soldering in to produce a complete unit.

A complete kit is available from GMT electronics, which includes plated—through hole PCBs, full metalwork and the hand controller. See Buylines for final details.

Construct-a-Text

Despite the complexity of this project construction is amazingly straightforward, all that is required is to assemble the four boards CAREFULLY following the overlays, and fit these into the chassis. Interwiring between the PCBs is dealt with by following the list given here, and referring to the wire nos. shown on the overlays. Don't be tempted to change this, best results — indeed any results — will only be obtained by strict adherence!

Once you're satisfied that all is as it should be, fit the ICs into their sockets and move on to the setting up.

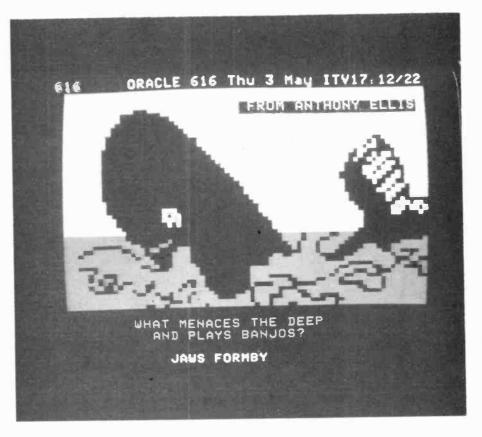
	— FACILITIES————
	Keyboard Commands
RESET	The screen is cleared and the
	converter is ready for channel
	change (timed page is cancelled).
STATUS	Television station identification
	appears top left of screen.
HOLD	Displayed page is held.
TOP	Large (2x) top half of display.
ВОТТОМ	Large (2x) bottom half of display.
MIX PAGE	Cancels both above displays
	channel video and teletex
TIMED PAGE	together.
TIMED PAGE	On: — The selected time for the
	page selected can be inserted and
*	is displayed in the top right of screen (4 Digits).
	Off: — Above cancelled.
REVEAL	Displays hidden characters.
TEXT	Calls up teletext. Page 100
	selected automatically (currently
	for BBC 2 Ceefax key in 200).
CANCEL	Cancels text.
DATA	Used for external data (not used
	in current design).
TV ON	Not used in current design.
	Last two facilities available for
	further expansions.

Set up!

- Disconnect encoder video O/P from the modulator board.
- 2) Disconnect blanking and picture on (PO) outputs from main board.
- 3) Connect UHF O/P to set, and UHF aerial to converter.
- 4) Select spare channel on T/V set.
- 5) Tune T/V for blank screen (ie. no noise).
- 6) Switch off.
- 7) Link P.O. input of UHF and mixer board to 12V.
- 8) Switch on
- 9) Tune RV 201 (front panel to obtain best picture on BBC1.
- Re-adjust set for best colour picture, modulator RV 401 may need adjustment.
- 11) Repeat 7 and 8 as required.
- 12) Switch off.
- 13) Reconnect steps 1 and 2 remove link step 6.
- 14) Switch on.
- 15) Set RV 100 to midpoint.
- 16) Connect pin 1 1C103(VIP) to 12V.
- 17) Connect pin 7 via 5M6 to 12V.
- 18) With transmitter switch to mix mode.
- 19) Adjust CV101 until characters lock with picture.
- 20) Switch off.
- 21) Remove steps 14 and 15.
- 22) Switch on.
- 23) Adjust L101 to obtain page header and time clock stepping (note this setting is sharply defined). L101 should not need adjustment (ignore any colour flicker).
- 24) Switch off
- 25) Link pin 10 1C103 to 12V rail,
- 26) Switch on. Note CV102 and L101 interactive repeat 20 and 24 as necessary.
- 24 as necessary.27) Adjust CV102 for best display (approx ¼ closed).
- 28) Switch off.
- 29) Remove step 22.
- 30) Switch on.
- 31) Switch to text mode.
- 32) Adjust CV301 for best colour.
- 33) Other channels can now be tuned (hit reset followed by channel No 1=BBC1; 2=ITV; 3=BBC2).



Above and below, two typical screen displays from the ITV, Oracle service. Now do you see what you're missing out on?



HOW IT WORKS

Ultrasonic Receiver And Transmitter

In the transmitter the keyboard, commands are encoded by the SAA 5000 which switches the HEF 4069 transmitter IC in the correct code sequence.

This pulse coded 40Hz transmission is received by the TDB 1033 which provides 90dB of gain in AGC system and a carrier filter. The output is fed to the decoder section.

The Decoder

This design is based on the Mullard L.S.I. design and uses four main IC's and a memory section of seven 2102's.

The signal from the TDB 1033 is fed to

the SAA 5010 receiver decoder and checked for error content and then produces various outputs.

Analogue Controls - Not used in

this design.

2. Station Selector Drive Output -Used via an HEF 4011 inverter to step an HEF 4017 station selector.

Message Received Output — Used to drive an LED and audible indicator.

Control Signals for the SAA 5040

SAA 5030 VIP Video Input Pro-

The data retrieval section of IC, slices the incoming data signal by means of an automatic adaptive data slicer circuit. This circuit sets the threshold level for slicing at half the data amplitude, regardless of the amplitude of the incoming signal, and provides some compensation for distortion such as cochannel interference; the performance of the system under noisy conditions is thus improved. A clock signal is generate from the sliced data by using an external 6M9375Hz tuned circuit. and this signal is used to clock the data into the TAC integrated circuit.

A 6MHz display system clock is also included in the VIP, the output of which is divided in the TIC to produce a clock pulse every 64us. This signal is passed back to the VIP where it is compared with the incoming line sync signals. By this means, the timing system of the teletext display is phase-locked with the

incoming television picture signal.

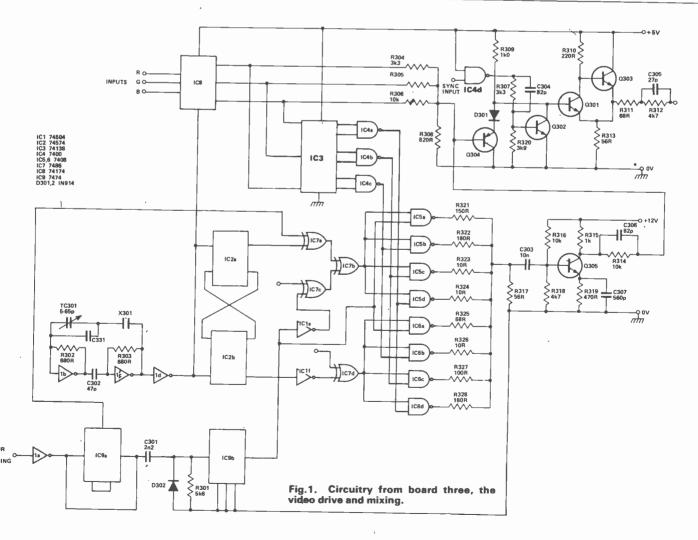
A 'signal quality' detector circuit is also included. When a signal with a high noise content is being received, or in the

absence of an incoming signal, the signal quality detector cuts off the teletext data to the TAC and allows the display system to free-run. Thus the detector prevents the data stored in the memory from being corrupted by noise. This facility, combined with the local display clock, allows a stable display even in the absence of an incoming television signal. Both are essential for after-hours display.

The IC also contains an adaptive sync separator which extracts the sync signals from the incoming video signal and also provides a sync output signal for the timebases of the television receiver. When a full page of text is displayed, the sync output signal is derived from the SAA 5020 TIC.

SAA 5040 TAC Teletext Data Acquisition And Control

The principal function of the data acquisition section of the TAC integrated circuit is to process the teletext data so that it can be written into the memory. The control section processes the information from the remote control



system, and uses this information to operate the various display functions of the teletext decoder system such as selection of television, teletext, or viewdata modes; page hold, time display, or timed page select.

The data acquisition section, divides the data from the VIP into its component parts. The Hamming-coded address words are checked, and words having a single wrong bit are corrected. Address words having two wrongs bits are rejected. The row address of the incoming data line (one of twenty-four) is fed by this section to the 5-bit row address bus, and the character date is fed through the data to the memory as a sequence of forty 7-bit parallel words.

A signal denoted as WOK (Write O.K.) indicates to the memory when valid data is to be written in, and a WACK (Write Address Clock) signal causes the address counters 74LS161 to step on after each character.

The IC also contains circuits for the implementation of the control bits for the page header.

SAA 5020 TIC Timing Chain
The divider stages in the TIC integrated circuit sub-divide the 6MHz clock signal from the VIP down to 25Hz, the television frame rate, and generate all the timing signals for the teletext display. During the display period, a 1MHz clock signal RACK (Read Address Clock) takes over from WACK to step the character addresses. The address counters 74LS161 are cleared at the end of every line and reset to the first position. After every ten lines during the display, the TIC steps the row address on by one to access the next row of characters in the memory.

In addition to providing all the timing signals for the display, the IC also generates a complete composite sync signal. This signal can be used to drive the timebases of the television receiver without the need for the transmitted sync signal. (This form of operation is also termed 'after-hours' operation.)

Memory Blcok

The memory block consists of seven 1k x 1 static RAMs.

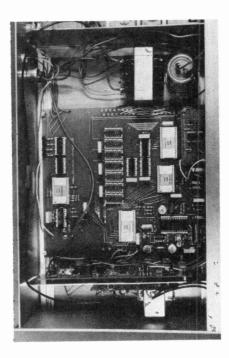
SAA 5050 TROM Teletext Read-Only Memory

The read-only memory of the TROM converts the 7-bit character data from the memory into a dot matrix pattern. This matrix is in a 7-by-5 dot form for each character. It also contains a 'character rounding' facility which effectively increases this matrix to 14-by-10 dots, giving improved definition to the displayed characters.

Additional circuits enable various control functions to be performed. These functions are determined by control characters received from the memory. Examples of these control functions are the selection of graphics or alphanumerics, 'flashing' words, or newsflashes and subtitles displayed in

boxes within television pictures.

A 'concealed display' function is also provided which can be operated by the user.



BUYLINES

The designers of this project -GMT — have a complete kit of parts available. This includes all metalwork, PCBs and hardware. A manual is also included. Cost is £155 plus VAT (total £178 inc p&p).

As an alternative the teletext decoder board and control system is available separately at £125 for those who wish to wire into their own television.

PCBs and chip sets are available separately also — but are PoA.

See advert on page 6 for address.

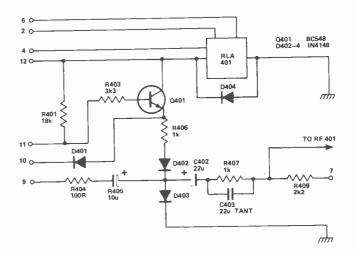


Fig. 2. Relay switching circuit (board four).

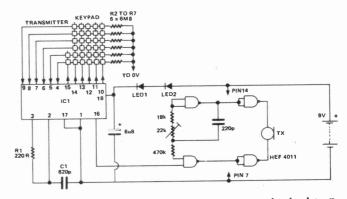
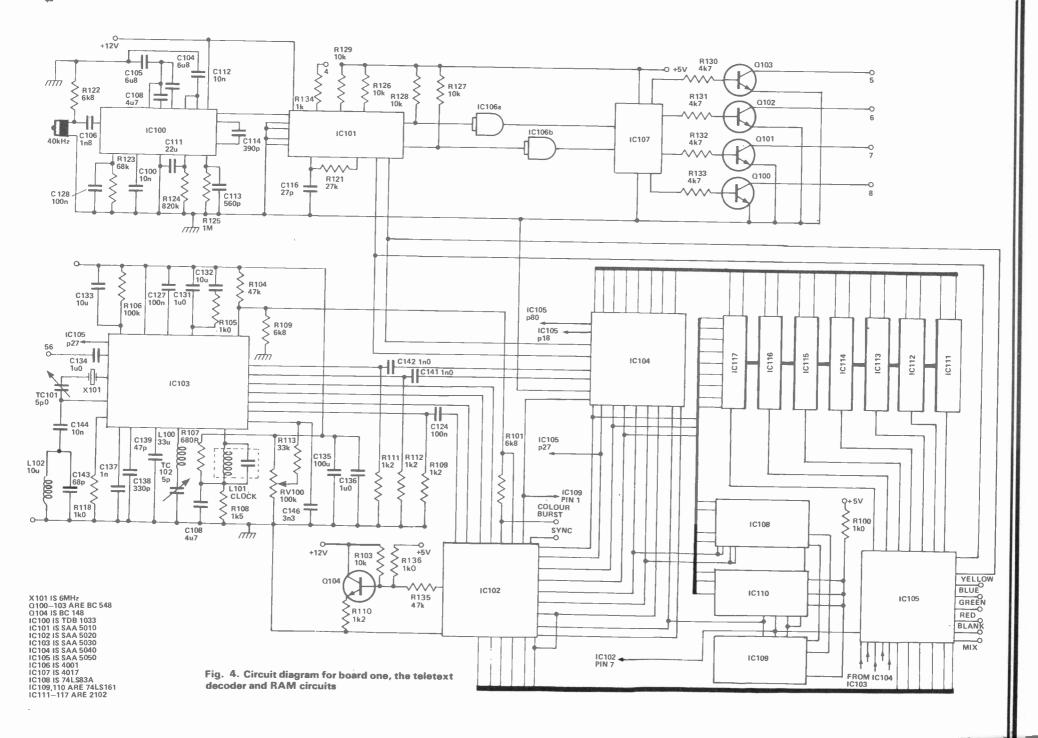
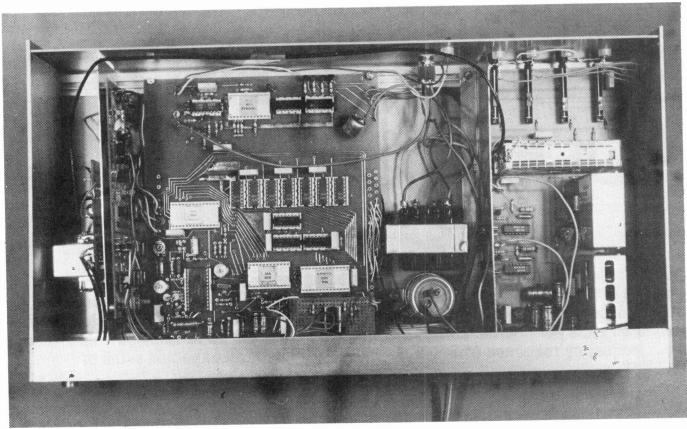


Fig. 3. Hand controller circuitry. Note that no overlay is shown for this, as no constructional work is needed using the kit. IC1 is a SAA5000 for those wishing to go it alone.





Above: a unit complete except for mounting of the ultrasonic receiver

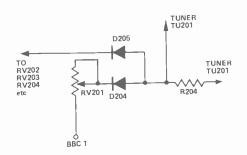


Fig. 5. (Above, left): tuning circuit.

Fig. 6. (Below): Power supply circuitry to produce the three rails needed.

Next month we conclude the project with component overlays, parts lists and some erudite hints upon getting the best results from this superlative design.

-O 12V NOTE: ₹ R209 00000000000000000 1C203 240V AC C215 470p ≤ R212 5k1 R208 1k5 TR1 240-24V C 207

EΠ

MAGNETIC FIELD AUDIO AMPLIFIERS

Carver Corporation's Model M400 amplifier using the unique 'magnetic cavity' was released in the US a few short months ago. Employing FETs throughout, except for bipolar silicon output transistors, Carver Corp. claims that the M400 has a slew rate around 80 volts per microsecond, hum and noise over 100 dB down, 0.05% distortion and a frequency response from 1 Hz to 250 kHz — all for an expected retail of US\$300!

IT REALLY DOES EXIST. ETI first reported Bob Carver's Magnetic Field Audio amplifier in our Australian issue saying . . "we hear from normally authoritative sources that Bob Carver — founder of Phase Linear — has developed a totally new concept in audio amplifiers which . . . stores energy in a magnetic field rather than in power supply capacitors . . . his new device generates no heat, weighs a mere five kilos for vast numbers of watts and lasts for ever".

It seemed a bit hard to take seriously — even though we were totally award of Bob's previous efforts such as the range of Phase Linear super-amps and the Autocorrelator noise reducer.

But it seems as if this revolutionary concept in audio amplifiers is for real – patent protection has been arranged and preliminary details have been released.

Bob's basic concept is to store energy in a magnetic field rather than very large value electrolytic capacitors — eliminating at the same time the need for a bulky expensive power transformer.

Our circuit drawing shows the essential features. The heart of the circuit is

the magnetic cavity (MC). This is basically similar to the AM detector transformer used in conventional AM radios but constructed on a grand scale. A further and significant difference is that the transformer is arranged such that an output occurs as the primary field collapses rather than builds up.

The secondary winding of the magnetic cavity is centre-tapped and the resultant full-wave output is rectified by a pair of high current diodes — the output waveform is thus a conjugate pair of time-varying audio voltages. Further circuitry, described later in this article, provides a feedback loop to remove commutation noise and reduce distortion.

. The primary of the magnetic cavity is energised by an amplitude-modulated current (corresponding to the audio signal voltage). The current signal is produced from the audio input, via the optical isolator and modulation and control logic, to the scanning SCR, the ramp SCR, a pair of scanning and commutating diodes, and L1, L2 and C1.

This current signal energises the

primary of the magnetic cavity. The time taken for this is called the 'ramp period'. The primary energy is then reflected in the secondary windings (and thence to the speaker) during the subsequent 'scan period'.

As our graph shows, the ramp and scan periods are made up of four separate timing intervals. During the period $t_0 - t_2$ an incoming audio signal has caused a magnetic field to 'ramp' up in the primary of the magnetic cavity. At to the field has reached its peak and is beginning to collapse. This collapsing field generates an associated decaying current i₁ and this decaying current falls to zero when the energy in the primary field falls also to zero (point t3). During the time period t_2 - t_3 , the control logic provides a positive signal on the gate of the scanning SCR, however this SCR will not again conduct until sufficient voltage is applied between its anode and cathode.

Throughout the scanning period, energy is of course being transferred from the primary of the magnetic cavity to the secondary — and thence to the speaker load.

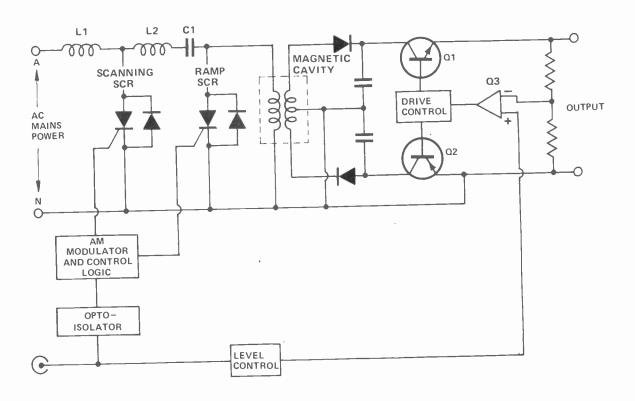


Fig. 1. This schematic shows the major operating components.

At time t₃ the direction of current is reversed — current being no longer maintainable by cavity inductance — and the scanning diode is reverse biased — this causes the scanning SCR to be forward biased and current flows as shown in our sketch.

Summarising then, energy stored in the magnetic cavity is caused to shuttle around the circuit of L1, L2, C1 and the speaker load depending on instructions from the control logic.

Noise and distortion

Components Q1 — Q3 form a feedback loop which reduces the inherently poor bandwidth, noise and distortion to very acceptable levels. Theoretically the circuit has some quite strong objections — at low frequencies Q1 and Q2 will act much as switches except that the feedback correction voltage developed by Q3 will adequately cancel aberrations — but at higher frequencies, i.e. 10 kHz — 20 kHz the modulator circuit is unable to follow accurately the audio input

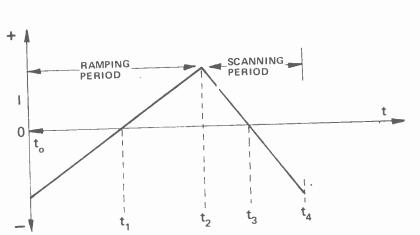


Fig. 2. During the ramping period energy builds up in the primary of the 'magnetic cavity'. Throughout the scanning period energy is transferred from the primary to the secondary of the magnetic cavity and thence to the speaker load via $\Omega1$ and $\Omega2$.

signal. Hence the filtered output from the magnetic cavity is a dc level with a superimposed ac signal and Q1 and Q2 thus operate much as any other conventional amplifier.

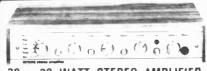
Nevertheless as less power is generally required at high audio frequencies than at mid frequency and low frequency, amplifier efficiency is very high if fed with music signals. This situation does not of course apply if the amplifier is fed with a high frequency steady tone.

Bob Carver's radical amplifier will be rated in accordance with FTC rules — the specification is expected to include power output: 200 watts-perchannel into eight ohms from 20 Hz to 20 kHz. Total harmonic distortion is expected to be less than 0.08% across this range.

Signal noise ratio is expected to be 100 dBA below rated maximum output. All-up weight is an incredible 5.5 kg.

As far as we are aware the magnetic field amplifier exists at present solely as a prototype unit but we understand that Bob Carver has very real plans for putting the unit in to production at a presently projected price of US \$300 or so.

It's a fascinating concept, one that will cause amplifier designers and manufacturers world-wide to furiously rethink their design philosophies. It may even herald the coming of a new hifi technology.



20 x 20 WATT STEREO AMPLIFIER

VisCount IV unit in teak simulate cabinet. Silvet finish totary controls and pushbuttosis with marching fascra, red minis indicator and stereo jack socket functions switch for mic magnetic and crystal pickups, tape funer and auxiliary. Rear panel features two mains outlets DIN speaker and nous tockets plus fuse 20.20 waits RMS 40x40 waits peak For use with 8 to 15 ohm speakers.

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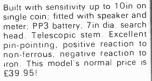
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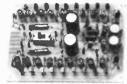
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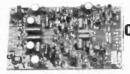
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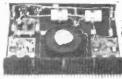
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004	Metal Locator Mk II Ultrasonic Tx/Rx 5 Watt Stereo Amp (mod Metronome Shutter Time	Feb 78 Feb 78 lified) Jan 77 Feb 78 Feb 78	011	Watchdog (2 PCBs) Stars & Dots PSU Noise Generator General Preamp		017	Complex Sound Gen Tele Bell Extender Power Bulge	Oct 78
005	Op-Amp Supply Frequency Shifter LCD Panelmeter Light Dimmer (3 times)	Mar 78		Flash Trigger Compander Active Crossover (2 PCBs)	Project Book Six	018	RF Power Meter Proximity Switch Audio Oscillator (2)	Oct 78 Oct 78 Nov 78
006	CMOS Switched Preamp From Experimenters	Electronics	012	Disco Lightshow Stereo Simulator Digital Thermometer	Project Book Six	019	Car Alarm (2) Wine Temp (2) Curve Tracer	Dec 78 Dec 78 Dec 78
007	P.S.U. 555 Boards (twice Star Trek Radio CD Ignition	May 78 May 78	013	Amplifier Module Amplifier PSU Equaliser Equaliser PSU	Book Six	020	Digital Tacho Module Digital Dial	Jan 79 Jan 79 Jan 79
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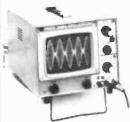
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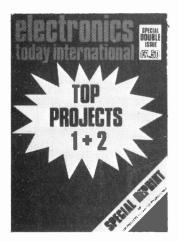
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from ETI

POLYPHONIC KEYBOARD CONTROLLER

Tired of playing one note at a time on a boring old monophonic synthesizer? In this design Tim Orr describes how you can build a four octave polyphonic keyboard controller incorporating first note priority.



THE MUSIC synthesizer is probably the most powerful musical instrument of today, and it will most probably form the basis of the next generation of keyboard instruments. However, the synthesizer suffers from one major drawback due to its unique structure. The disadvantage is that it is a monophonic instrument as opposed to traditional keyboard instruments, such as organs and piano's which are polyphonic, or multi-voiced. A brief resumé of synthesizer structure should clarify the reasons behind this.

To start with, the synthesizer is composed of a set of modules or independent circuit packages whose parameters in most cases are voltage controllable. For instance, a voltage controlled oscillator (VCO) has an output frequency (pitch) which is dependent on the magnitude of the input control voltage. These modules can be split up into three distinct

groups. Firstly there are Sources, such as:

- 1. Noise
- 2. Voltage controlled oscillators

Secondly there are Modifiers which form by far the largest group:

- Voltage controlled filters (VCF's)
- 2. Voltage controlled amplifiers (VCA's)
- 3. Ring modulators
- Filter banks or graphic equalisers
- 5. Phase shifters
- 6. Reverbration

Thirdly there are control voltage sources:

- 1. Sample and holds
- 2. Sequencers
- 3. Transient generators
- 4. Trigger delays
- Keyboard controllers

Getting Your Priorities Right

First note priority was adopted for this design, i.e. first note pressed to channel 1, second to channel 2, and so on. If more notes are pressed then the system can cope with, these are locked out. The reason for this, as opposed to last note priority, is that first note priority stops the note jumping that can occur when, momentarily, more notes are pressed than the system caters for.

Binary Notation

When the code (note code) driving the decoder energises a contact which is closed, the output of the OR gate goes high, showing a unique code on the input representing the particular note being pressed. This code, the note code, is arranged such that the lowest note is binary zero, the next note up binary one, the next

two and so on up to N.
The scanning can also be achieved using a multiplexer.

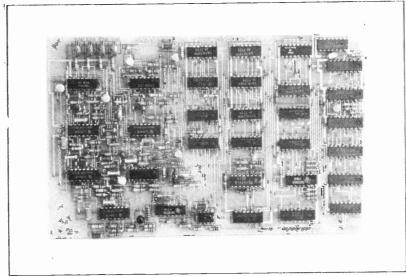
The size of keyboard decided on was a 4 octave one having 49 notes. Hence this makes the value of N 49 and therefore the size of the note code will be 6 bits (64 possibilities). In fact this is useful in that a 6 bit code will be just big enough to scan a 5 octave keyboard (61 notes) if required. In the case of this design it will simply be a mattter of adding 12 extra diodes since the decoder already had a total of 64 outputs. Incidentally, the scanner will have another output not yet mentioned. This is called 63rd note, (the 63rd output on the decoder) which simply provides a pulse to the decision logic to say that a scan has been completed. The multiplexer method would require decoding of the note code to do this. The scanner simply gives each note a binary code, but how can this be extracted as a set of control voltages with associated gate signals?

Pumping Caps

The note code is changed to an analogue voltage using a D-A converter, the output of which is switched onto the correct analogue channel and held using a set of sample and holds. The gate signals are dealt with in a similar way using CR circuits. The counter for the note code causes the scanner to increment from the lowest note upwards. If three notes are depressed the scanner reaches the lowest note first and causes the output of the D-A to be stored by channel 1 sample and hold, and channel 1 gate capacitor to be pumped up. On moving on the channel counter is incremented, prepairing the output channels for channel 2 data. When the scanner reaches the second note up the process occurs again only using channel 2 and again for channel 3, with the third note. When the scan has been completed the channel counter is reset and made ready for the next scan.

Dying Charge

If on the next scan the notes are still depressed, the gate capacitor will again be pumped up maintaining the gate output high. When a note is released the time constant is such that the gate capacitor's charge dies away in about one and a half scan



The largest of the four PCB's, carrying the logic circuitry.

times, thus removing the gate signal. By experiment it was found that the scan time needs to be about 4 mS. Even when a key is pressed and released very quickly, it will have been scanned about ten times or more. The NAND gate should be mentioned because it allows two adjacent notes to be played. This is because if two notes right next to each other are depressed, the output of the scanner remains high for the duration of both notes and so only one note would be detected. By NANDing the scanner output with the clock the output is broken up allowing adjacent notes to be detected.

Note Jumping

Although this circuit will work, it is far from satisfactory. When notes other than the top note are released, the channels on which the remaining notes appear, above the released note, all jump down one place. This makes the instrument very difficult to play as it must be remembered to release the keys from the upper one downwards, to get a chord that dies away nicely without the note jumping effect.

Special Decision

This means that the simple logic must be replaced by some special decision logic, incorporating a memory of notes already activated in previous scans.

The scheme here is that note codes are gathered into the memory as the scanner sweeps up the keyboard. When the 63rd note is reached, the

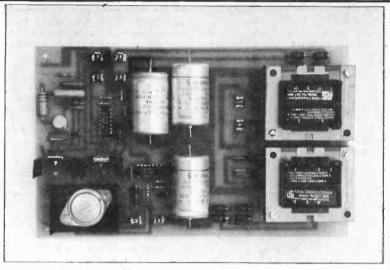
entire memory is dumped onto the output channels by sequencing the peripheral address lines. It is also necessary to reset all of the gate data bits in preparation for the next scan. This means that while a particular key remains pressed, the gate for that channel will be refreshed on every scan. When the key is released, the gate for that channel will go low when data is again output.

Logical Channels

The effect of the decision logic from the musicians point of view, is that upon playing a chord, say C, E and G the first one depressed normally comes out on channel 1, the second on channel 2 and the third on channel 3 (the difference in time between depresssions need only be milliseconds). There is, however, an exception to this when a note is depressed that is already stored in memory. For instance, if the three note chord described above were depressed such that C was first E second and G third, then it would be expected that C would come out on channel 1, E on channel 2 and G on channel 3. But if a previous chord had been played using the same C which had emerged on channel 2 then the decision logic would cause it to remain on channel 2 and so the E would be placed onto channel 1 and G onto channel 3.

Key Question

Construction of this project will depend almost entirely upon the keyboard it is built around. If you



Power for the keyboard controller comes from this twin transformer board.

D100 17 LOWEST NOTE 22 IC101 11 OTHER DIODES & CONTACTS 20 19 18 0V KEYBOARD CONTACTS D116 C102 22 20 DIODES & CONTACTS 19 NOTE: IC100 IS 74LS04 IC101,2,3&4 ARE 74154 D100-148 ARE 1N914 Onv KEYBOARD CONTACT BUS BAR +5V Ď132 13 23 22 IC103 11 OTHER DIODES & CONTACTS 20 19 D147 O OV +5V HIGHEST NOTE (ON 4 OCTAVE KEYBOARD) D148 22 IC104 21 20 19 O nv 63rd NOTE SCAN

Fig. 1. Circuit diagram of the scanner. The four 74154's are used as a one out of 64 line decoder.

HOW IT WORKS

The Scanner: The IC's used for the scanner itself are 74154, which are one out of 16 line decoders. They are arranged such that one output goes low with the rest remaining high, dependent on the four bit code on the input. These IC's also have a pair of enable inputs both of which must be low. These allow four 74152's to be used as a one out of 64 line decoder, simply by the inclusion of the two inverters on inputs 16 and 32. The 63rd note output is obtained from the 63rd output of the decoder, and the scanner output is taken from the keyboard contact bus bar, having been ORed using the diodes.

Logic: The reaction of the circuit to a new note that has not been picked up by the scanner before is as follows: the note code counter increments the scanner by one note on alternate falling edges of the clock, until it reaches this particular note. The output of the scanner goes high registering that the contact is closed. This triggers the monostable IC12 pin 2 causing its Q output to go low long enough to set the decision cycle flip flop IC15 input pin 9 The output of this flip flop pin 11, then inhibits further pulses from clocking the note coder by taking pin 1 of IC15 low. At the same time it initiates the first decision cycle by allowing the counters IC9 (address counter) and IC13 (decision counter) to run by taking their clear inputs high. When the output of the decision counter is zero the memory address counter is clocked round, so that the logic can check if the note is already in the memory.

The memory address counter is incremented on the low going edge of the K pulse, which is simply the clock divided by two. Since the decision counter is only 2 bits it was convenient to derive K using the spare single stage counter in the 7493. Note that K is only active during the decision cycles and data block since the counter is cleared down when the scanner is scan-

ning.

When the address counter reaches the number set on the Phonics switch, it is reset, and the decision counter incremented by one via the NAND gates IC18. This starts the second decision cycle where the logic is looking for a spare location to insert the new note. It has been assumed that channel 1 is in use and that the first available channel is channel 2. The circuit stops the data being entered in channel 1 by observing the state of the gate data output from the gate RAM pin 5. If this output is a logical 'O' the channel is in use and must not be corrupted, and so the address counter is incremented so that the next channel can be tested.

In the case of this example the decision logic succeeds in entering its data in channel 2, but if the decision counter is incremented a second time before an empty channel is found, simply because all channels are in use, the decision cycle is ended and the scan continued. This third condition of the decision counter is decoded by the NAND gate IC16 and the invertor IC19, and reset is achieved via the three input NAND gate IC22 and invertor IC20, which reset the decision cycle flip flop restarting the note code counter and clearing down the memory address and decision counters.

The second and subsequent times that the scanner is stopped by the note that was loaded in channel 2, the decision logic will only get as far as its first test 'Is the note already in the RAM', so when the memory

PROJECT: Keyboard Controller

address counter reaches 2 the comparator output goes high acknowledging that the note is already entered. This causes the gate bit to be refreshed (since it is reset during data block) along with the data being re-entered into the note memory, (re-entering the data in the note memory is not necessary but occurs due to circuit architecture) after which the decision flip flop IC15 is again reset and the scanner restarted.

All the time a note remains depressed the decision logic will refresh the gate bit associated with the channel in which the note has been placed. At the end of a scan the gate bits are reset immediately after they have been placed on the output channels meaning that if the note is not still depressed on the next scan the gate signal on the output channel will go low in the next data block period.

During a scan the data valid signal is high, it only toggles in data block. Simply enabling the gate RAM during the decision cycle loads it with a '1', since data valid is the input. Note that loading these Ram's with a '1' results in the output going to a '0' as they invert. This is the reason for the invertors on the outputs of the note RAM's, which are also tri-state for the computer interface.

The clock for the system is an NE555 timer wired in the astable mode.

The Output Channels

There are two outputs per channel which

are multiplexed out by the data block period. These are the gate outputs and the control voltage outputs. The gates are obtained from the CD4099 addressable latch (note that these outputs may need buffering depending on the impedance they are driving as the CD4099 is CMOS). The address lines of the latch are attached to the memory address counter and the input is connected to the gate data line (IC10 pin 2). The enable input of the latch is connected to the data strobe line so that as the data is output from the memory the correct gate state (1 or 0) is stored on the relevant channel.

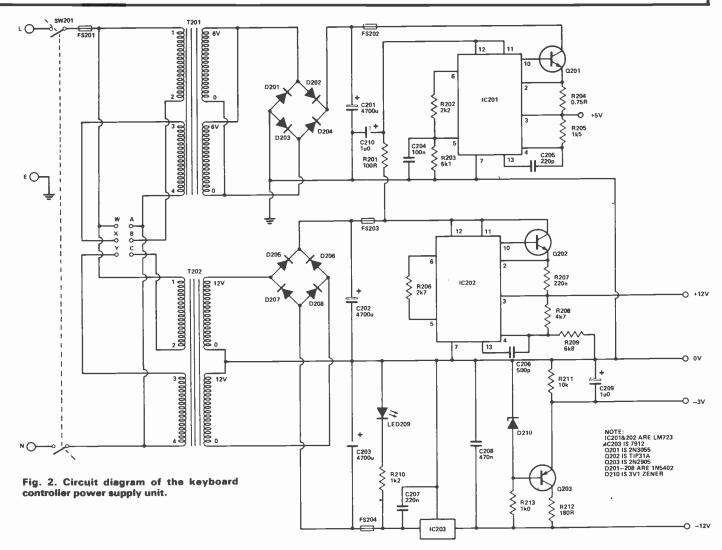
The data sample pulses are for loading the sample and holds on the analogue channels. They are derived from the 1 of 8 decoder and the clock. To interface between the TTL logic and the analogue switches comparators are used so that the analogue signals can be between —3 volts and +12 volts. All the comparator outputs are disabled when the clock is high by using the two resistors R65 and R53 to feed the reference input to the comparators, the clock signal being attached to R65. The binary codes representing the notes are converted into analogue voltages using the D-A convertor IC14.

As the memory address counter is incremented in data block the data in the note memory is converted into an analogue voltage and passed onto the correct analogue channel by the comparator and analogue channel analogue c

gue switch. The D-A convertor has a current output such that when the resistor R82 is added to convert it into a voltage, the output goes more negative with increasing binary codes. The op-amp IC29 (pins 12, 13 and 14) corrects this by inverting the output of the D-A. It also allows the scaling or volts per octave of the keyboard to be adjusted, by varying the resistor in the feedback loop. Another function that the op-amp allows is the summing of voltages that have to appear on all the output channels at once.

There are three sources of voltage that are summed at this point, the tune voltage, the vibrato voltage, and the pttch bender voltage. The tune voltage is derived from a potentiometer which draws its current from the voltage reference circuit. The vibrato voltage is generated by a standard triangle wave generator comprising a regenerative comparator IC29 pins 8, 9 and 10 and an integrator IC29 pins 5, 6 and 7. The output is coupled to the summing amplifier via a pair of back to back electrolytics to remove any DC offset and a pair of resistors that allow their centre point to be connected to earth via an external vibrato depth potentiometer.

Offsets around the circuit are trimmed out using the trimmer RV1 which obtains its reference from the diode D1. Since the offsets are predominantly in one direction due to Q2 the offset control only works in the negative voltage direction.



employ the ARAK kit, no problems should arise at all. The PCBs are designed to fit their keys and comprehensive instructions are included with the kit.

We have not attempted to go into any detail with any other unit, simply because there is such a great diversity available on the market.

Setting Up

Once the components are all mounted on their boards, each section has to be set up. Let's start with the

Before the mains is connected to the PSU it should be thoroughly checked for shorts. The three low voltage fuses FS202, FS203 and FS204 should then be removed and the mains turned on. Now check the voltages across the smoothing capacitors C201, C202 and C203 which should be around +8V, +17V and -17V respectively. If this is the case the +12V regulator can be tested by replacing FS203. If this works the +5V regulator can be tested by replacing FS202. As the +5V regulator is supplied from the +12V supply via R201 they must be tested in this order. Finally the -12V and -3V supplies can be tested by inserting FS204. It should be noted that the fuse holders may need bending to give correct contact to the fuses as they are very simple pressed steel pieces for PC mounting.

The Logic Board

Check the logic board thoroughly for shorts on supplies. It is also wise to 'buzz out' every connection on the board to test for continuity which may well save a lot of fault finding time, but note that it will not quarantee correct operation as it does not test for shorts.

When these preliminary tests have been carried out and the power supply unit is functioning correctly power can be applied to the logic board. Firstly only apply the +5V supply until the TTL is known to be working correctly.

And a Log

Once the logic is working the analogue section can be tested. This time some setting up can also be done:

First check the positive reference is sitting at about 6V2 above earth. This level can be increased using the trimmer RV7 if a higher reference is required for any reason.

If the touch circuit is not to be used R63 should be removed as it will probably cause the output of IC29 pin 14 to saturate against one of the supplies as the output of the touch circuit is indeterminate.

R19 sets the maximum glide rate. The smaller it is the longer the maximum glide rate will be. However, it is unwise to make it any smaller as the maximum range is set by the V on SAT of the switching transistor, this only creating an offset when it is turned on and not when it is turned off. It may be necessary to increase the value of R19 although problems will probably occur on one channel only and will most likely be remedied by replacing the switching transistor for one with a lower V CE SAT.

1k

2N3055

BOARD 2 R201 100R R202 2k2 R203 5k1 R204, R207 0R75 1W R208 4k7 R209 6k8 R210 R211 10k R212 180R 1W

CAPACITORS C201-203

R213

4700u 25V electrolytic C204 100n polyesti re C205 220p C206 C207 500p 220n polyester C208 470n polyester C209, C210 1u0 35v electrolytic

SEMICONDUCTORS Q201

Q202	TIP31A
Q203	2N2905
IC201, IC202	LM 723
IC203	7912
D201-208	1N5402
D209	LED
D210	3V1 Zener

MISCELLANEOUS

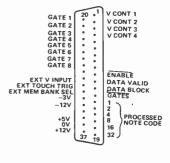
RS 207-683 TX202 RS 207-699 1A, 1A5, A (2 off) fuses and holders. DPST rocker switch.

BOARDS 3 AND 4

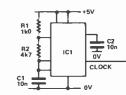
SEMICONDUCTORS

IC100 74LS04 IC101-104 74154 D100-148

2 off of these components are required, as board 4 is identical to board 3



CANNON 'D' TYPE CONNECTIONS



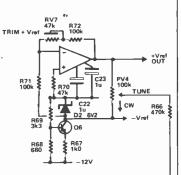
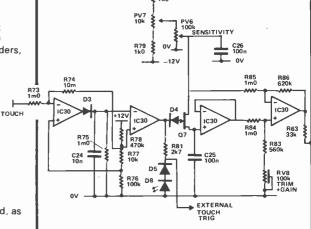
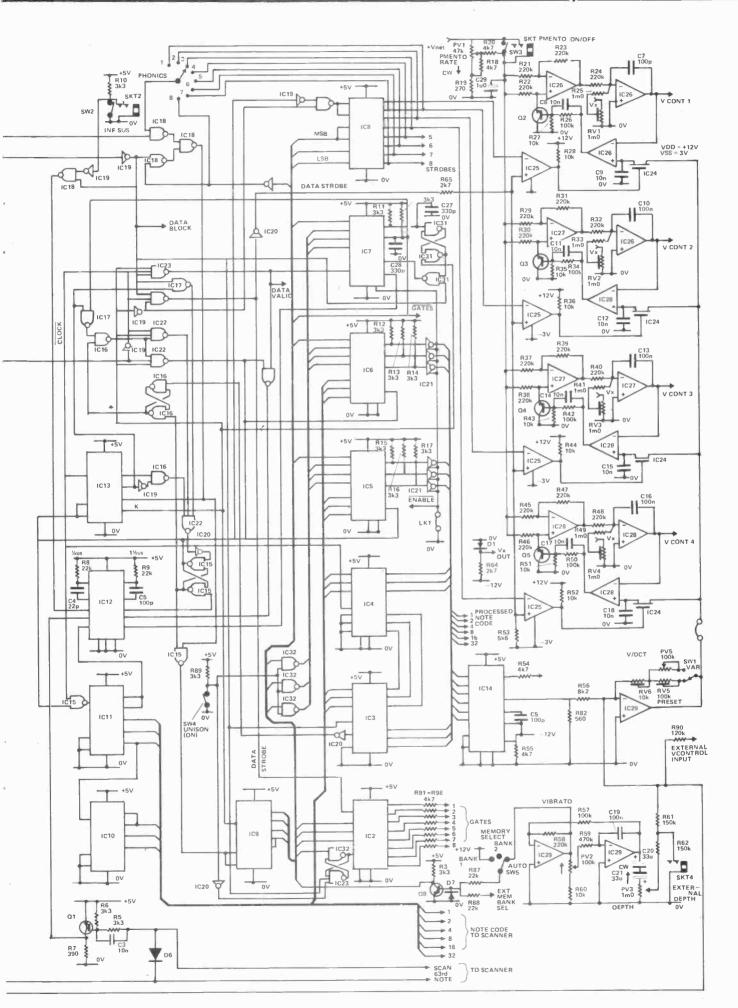


Fig. 3. Circuit diagram of the logic board.





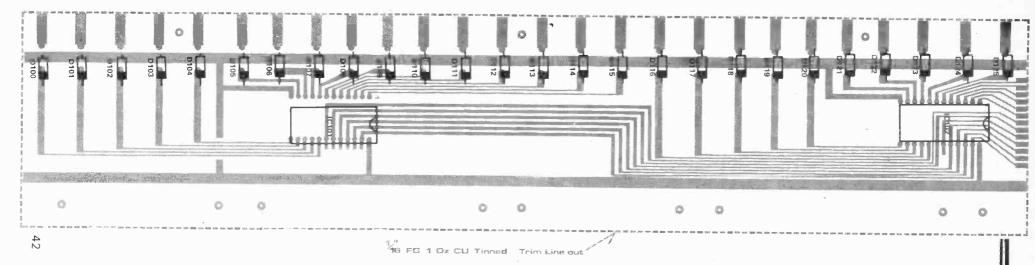
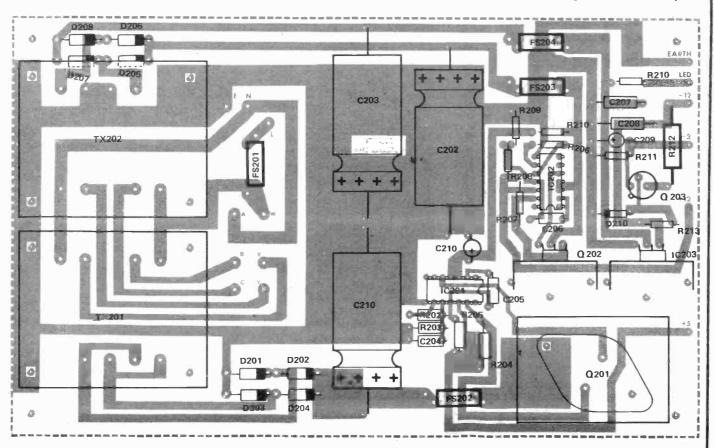


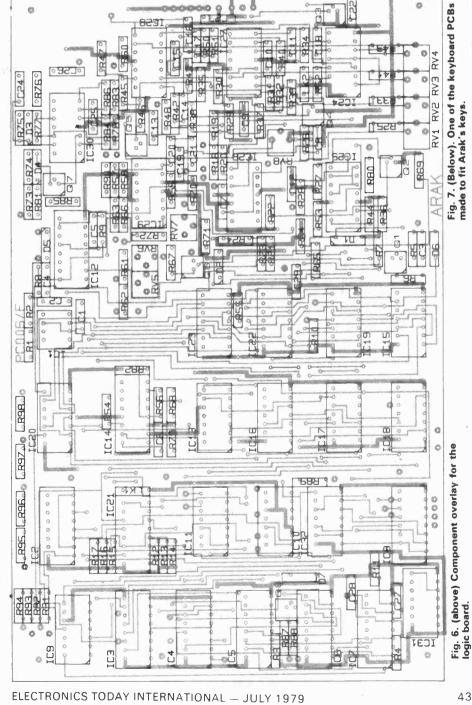
Fig. 4. (below) Component overlay of power supply board.
Fig. 5 (above) One of the two keyboard PCBs, designed to fit Araks keys.

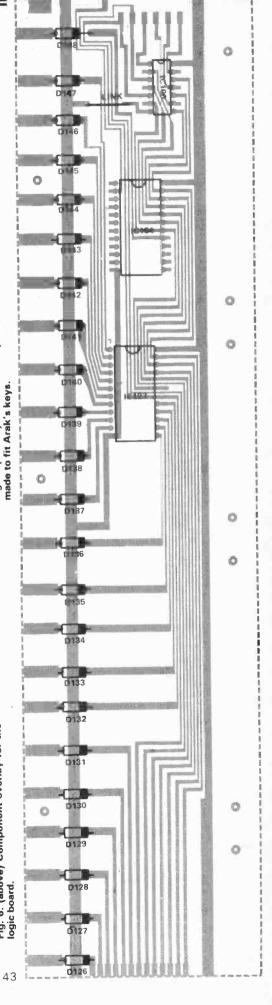


R8, R9, R87, R88 R19 R21-R24, R29-R32, R37-R40, R45-R48, R58 R25, R33, R41, R49, R73, R75, R84, R85, R26, R34, R42, R50, R57, R71, R72, R75, R57, R71, R72, R75, R57, R28, R35, R36, R43, R44, R51, R52, R60, R64, R77 R53, R66, R78 RESISTORS R1, R67, R79, R80 R2, R18, R20, R54, R55, R91-R98 R3-R6, R10-R17, R69, F R89 4k7 3k3 390R 22k 270k 220k 1 M O POTENTIOMETERS
PV1
PV2, PV4, PV5, PV6
PV3
PV7
RV1-4
RV5, RV8
RV6
RV7 R61, R62 R63 R65, R81 R70 R74 R82 R82 R83 R86 R90 **PARTS** 150k 33k 2k7 680R 47k 10M 560R 560K 620k 120k

ELECTRONICS TODAY INTERNATIONAL — JULY 1979

CAPACITORS		IC9-11, IC13	74LS93
C1-3, C8, C9,		ICI2	74LS123
C11, C12, C14, C15		IC14	MC1408L-8
C17, C18, C24	10n polyester	IC15-18.	
C4	22p	IC31, IC32	74LS00
C5. C6	100p	IC19, IC20	74LS04
C7, C10, C13, C16,		IC21	74LS366
C19, C25, C26	100n polyester		(or 74LS368)
C20, C21	33u ´ ´	IC22, IC23	74LS10
C22, C23, C29	1u0 35V electrolytic	IC24	CD4066
C27, C28	330p	IC25	LM339
SEMICONDUCTORS	•	IC26, IC27,	
Q1	BCY72	IC28, IC30	TL084
Q2-6, Q8	BC172 BC107	IC29	LM4741
Ω7	2N5163	D1, D3-7	1N914
IC1	NE555	D2	6V2 Zener
IC2	CD4099	D8	LED
IC3, IC4	74LS85	MISCELLANEOUS	S
IC5, 1C4	7489	37 way 'D' skt. s	tereo jack (3 off), SPDT
IC8	74LS155	switch (4 off), SPI	







PARIS

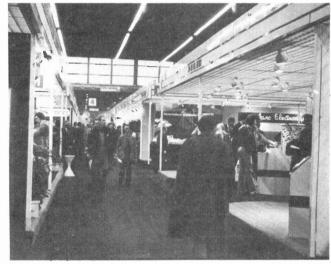


IN SPRINGTIME

As a London-based magazine, we tend to concentrate our interest on exhibitions and electronics shows in the London area. Lest we become too parochial in our outlook, we decided to see what our fellow Europeans have to offer. We sent our roving reporter, lan Graham, to Paris to see how the other half live.

I PROBABLY RECEIVE a couple of hundred Press releases every day. Most, concerning orders for electronic equipment won by companies or appointments to the top management of larger corporations or annual accounts, end up in the waste paper bin. Our reports on the cream of the rest appear monthly in our news pages. Occasionally I am invited to attend Press receptions. Again, few are interesting enough to prise us out of our armchairs. However, I did sit up and take notice when I was invited to attend an electronic components exhibition 'sur le continent'. The occasion was the Salon International des Composants Electroniques 79, held in Paris from the 2nd to 7th of April. Well, I thought about it, for several seconds at least, and decided that I had indeed been neglecting our European brothers.

On a sunny April morning I made my way from Charles de



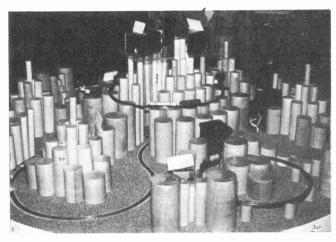
Row upon row of stands full of goodies — paradise for the exhibition addict.



The tops of stands stretch into the distance, in the biggest of the three exhibition halls.

Gaulle airport to the exhibition site at the Parc des Expositions in the Place de La Porte de Versailles. My first impression as I emerged from the Metro station was of the unexpected size of the exhibition, which stretched over a staggering 63,000 square metres, split up into four sections. It would have taken several days to see everything on display, certainly more than the single day I had allowed myself.

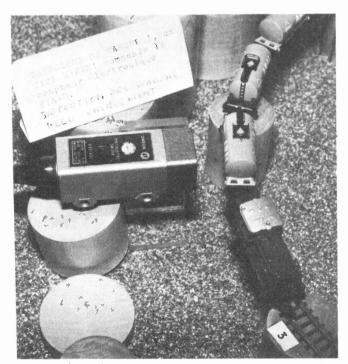
Although it was essentially a trade show, the atmosphere inside was more akin to that of our own Ideal Home Exhibition. However, great expectations of an entertaining exhibition were not borne out by my admittedly swift tour of the stands.



A fun way of counting trains with photocounters. This stand attracted a great deal of interest from people who had probably never seen a photocounter before. This simple display illustrated the principle of the unit admirably for the layman.

Dry Stuff?

Unfortunately, few exhibitors showed any imagination in the presentation of their wares. Sound to light units and TV games naturally lend themselves to entertaining stands, but what about more mundane electronic components? General Instrument Microelectronics (a British firm, I'm happy to say) managed to make microprocessors a crowd puller (I wouldn't have thought it possible) by using one to control a noise generator. Pretty dry stuff, you might say. However, the generator was producing car engine, gear change, skid and crash noises for a model racetrack. Visitors could control the cars with conventional pistol grips. Well, perhaps a model race track has little to do with microprocessors and vice

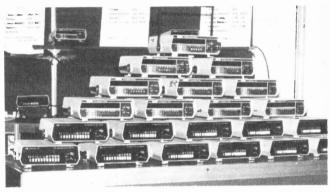


A closer look at the electronic 'train' spotter above. One colour of wagon, in this case blue, can be counted, ignoring the train and all the other wagons.

versa, but it did attract interested visitors. Isn't that what it's all about?

Eyecatching Pyramids

Another firm displayed photocounters by using them to count wagons on a pyramid of model railway layouts. Talking about pyramids, yet another firm (American) presented a striking display, a pyramid of multimeters. They might uncharitably be called gimmicks, but they were eyecatching. Too many exhibitors relied on a glass case full of components accompanied by row upon row of standard black and white exhibition photos, none of which deserved or got a second look. Still, there were plenty of product demonstrations to keep me busy, as I made my way through the maze of stands. There were also lectures. How do you fancy soaking up 'Monolithic Memories' at half nine in the morning? No, neither did I.



Keithley's pyramid of multimeters. We strongly suggest that you don't try this with your Avo. 8's, or if you do, don't blame us if there are disastrous consequences.

Light Entertainment to Heavy Machinery

Although I found plenty to criticise at the Paris show, it put some of our own electronics shows to shame. Whatever you are interested in, from hi-fi to heavy machinery, there's plenty of it at the Salon, with some 1300 firms exhibiting. Hi-fi enthusiasts could spend a day or two wandering round the stands devoted to the love of their life. That goes equally well for every field of interest represented and there wasn't much that was not represented.

See You Next Year

My brief visit to the show was very enjoyable. There was plenty of food and drink to be had from seemingly numerous bars. The French exhibition staff were so good to me that I'm thinking of doing it again next year. If you feel like joining me, the Salon International des Composants Electroniques 80 will be held from March 27 to the 2nd of April. If you feel like nipping across the pond to pay your visit on Sunday, March 30th, don't.....they're closed.

CALCULATORS

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#TEXAS T158 (New Key prog 480 steps or 60 mem)

#TEXAS PC1008 (New updated Printing Unit for T158 /T159)

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#TEXAS T157 (Key Prog 8 mem. 150 Keystrokes / 50 Prog Steps)
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#EXAS T130 (New — same spec. as T130 but 3 mail

TEXAS T133 (New — same spec. as T130, but 3 mem) £25.00 £13.95 #TEXAS T145 (New updated version of the Texas T140) £13.95 #TEXAS 42MBA (10 Dig Fin / Stat Prog 12 mem 32 keystrokes)

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TEXAS T125 LCD (Sci/Stats)

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Rine" 12 huction Chronograph until you have
wore it ... until you have enjoyed the
compliments it penarales.
The "Silm-line" Chronograph gives
centinous saay to reae LOD display of hours
minutes. seconds, AM/PM, All the bush of
button you have date — month date — day of
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MOTOR SPEED CONTROLLER

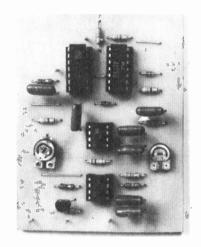
A sophisticated unit that allows control of model electric motor speed and direction via a single radio control channel. The unit can supply peak currents up to 10 amps.

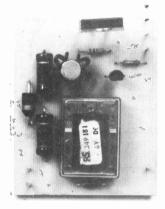
THIS DEVICE lets you use a single channel of your radio control system to control both the speed and direction of an electric model motor. The unit has been designed specifically to control the drive motor of our 1/16th scale Tamiya Leopard tank, but can in fact be used to control any 4V5 to 8V DC electric motor that draws peak current below 10 amps. The unit is ideal for use in model boats and large-scale land vehicles, and costs only a fraction of the price of equivalent commercial units.

The unit derives it's control signals from one of the output channels of a radio control decoder. It accepts standard positive or negative decoder pulses, which have widths variable over the 1 mS to 2 mS range, and is designed to work with systems having fixed frame (or frame repeat) periods of approximately 20 mS. The Strato 4+2 system, published in the May and June editions of ETI, can be used with the controller.

The controller circuit incorporates only two pre-set pots. One of these is a 'set null point' control, and can be used to set the motor speed to zero in any desired position of the transmitter joystick control. The other pre-set is used to set the maximum speed of the motor.

The two pre-sets can be used to give a variety of operating modes. If they are adjusted so that the null point occurs at the centre of the joy stick travel, the motor will have identical maximum speeds in forward and reverse. If the null is set to occur towards the 'low' end of the joy stick travel, the motor will have a high maximum forward speed and a low maximum reverse speed.





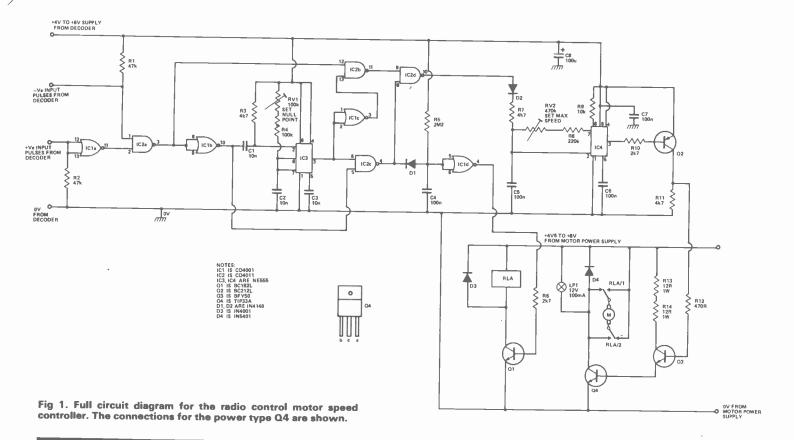
Construction And Use

The unit is assembled on two PCB's. Board 1 holds all the logic, timing components, and the two pre-set pots, and board 2 holds the power driver transistors and the relay. Construction of board 1 should present few problems: note, however, that no provision is made on the PCB for decoupling capacitor C8, since we hooked this component into the wiring harness on our prototype unit.

Note when constructing board 2 that power transistor Q4 can either be mounted directly on the board in low- to medium-power applications, or can be mounted externally on a suitable heat sink (such as a vehicle chassis, etc) in high power applications. The relay used on this board is a 6 volt two pole changeover type with a coil resistance of 70R (see Buylines).

When construction is complete, the two boards can be mounted in the model, preferably as far away from interference-generating motors and servos as possible. Board 1 is powered from the radio control decoder supply lines. The signals from the selected output channel of the decoder are fed to either the positive pulses or negative pulses input leads of board 1, depending on the pulse polarity of the particular decoder that is used.

Board 2 is powered from the motor supply leads. Note that the OV line of the motor supply must be made common with the OV line of the decoder. Also note that one lead must be connected between R6 on board 2 and pin 4 of IC1 on board 1, and another lead must be connected between R12 on board 2 and Q1 collector on board 1.



HOW IT WORKS

The input pulses from one channel of the decoder, which have widths that are variable between ImS and 2mS, are fed to either pin 1 or IC2a (negative input pulses) or to pins 12 and 13 of IC1a (positive input pulses), and appear in positive-going form at the output of IC2a. This positive-going pulse is fed directly to pin 12 ot IC2b, and is fed in inverted form to pin 5 of IC2c: the inverted pulse is also used to trigger reference-pulse generator IC3 via C1. This reference pulse has a nominal width of 1.5mS, which equals the mid-band width of the input pulses from the decoder.

The positive-going reference pulse is fed directly to pin 6 of IC2c, where it is compared with the negative-going version of the input pulse on pin 5. The action of IC2c is such that its output is normally high, but switches low for a period equal to the difference between the reference and input pulse widths only when the input pulse duration is less than that of the 1.5mS reference pulse. This negative-going output pulse, which has a width that is variable between zero and a nominal 0.5mS, is used to rapidly discharge C4 via D1 and thus cause the output of IC1d to switch high and drive relay RLA on via Q1 and R6. This relay, which dictates the direction (forward or reverse) of the motor that is being controlled, is thus off when the input

pulses are greater than 1.5mS (nominal), and on when the input pulses are less than 1.5mS.

The 1.5mS reference pulse of IC3 is inverted by IC1c and fed to pin 13 of IC2b, where it is compared with the positive-going version of the input pulse from the decoder. The action of IC2b is such that it's output is normally high, but switches low for a period equal to the difference between the reference and input pulse widths only when the input pulse duration is greater than that of the 1.5mS reference pulse. This negative-going pulse, which also has a width that is variable between zero and a nominal 0.5mS, is fed to pin 9 of IC2d.

Thus, a negative-going pulse appears on pin 9 of IC2d if the decoder pulse is greater than 1.5mS, or on pin 8 of IC2d if the decoder pulse is less than 1.5mS. Consequently, IC2d generates a positive-going output pulse that has a width that varies from zero on a 1.5mS decoder input pulse to 0.5mS on a 1mS or 2mS input pulse.

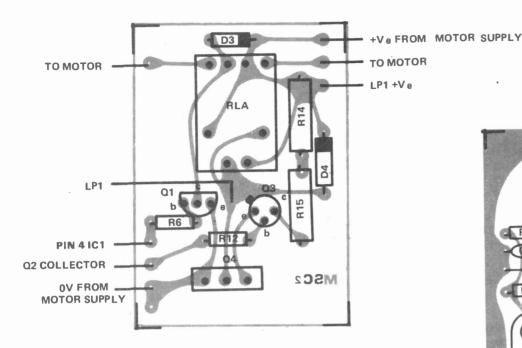
This pulse is fed, via D2, to a pulse-expander circuit designed around IC4, which expands the pulse width by a factor of about 40. The resulting expanded pulse is passed on to the external motor via transistors Q2 to Q4 and the contacts of the relay, and is used to give pulse-width or variable

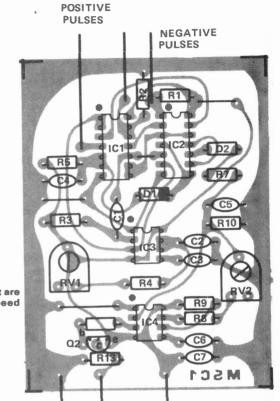
mark/space-ratio control of the motor speed. Diode D4 is used to damp motor back-EMF, and lamp LP1 is used to minimise the effects of

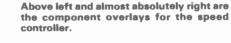
interference-generating current surges. In practice, RV1 is used to adjust the width of the reference pulse (nominally 1.5mS) so that the motor speed is zero when the transmitter joy-stick control is in its central or null position, and RV2 is used to adjust the expansion factor of the pulse expander circuit and thus pre-set the maximum speed of the motor when the transmitter control is in its 'maximum' position.

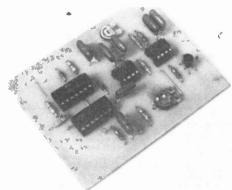
BUYLINES

The relay is the only component that calls for comment here. It is a 6 Volt 2-pole changeover type with a coil resistance of 70R, and is available from Greenweld, 443 Millbrook Road, Southampton, SO1 OHX. The price is £3.30, including postage and the usual extras.









And this is how the boards should look once you've built them up. Check very carefully before switching on.

PARTS	LIST		
RESISTORS (all ¼w	, 5%)	SEMICONDUCTORS IC1	4001
R1, 2 R3, 7, 11	47k 4k7	IC2 IC3, 4	4011 555
R4 R5	100k 2M2 2k7	Q1 Q2	BC182L BC212L
R6, 10 R8 R9	220k 10k	Q3 Q4	BFY50 TIP33A
R12 R13, 14	470R 12R 1W	D1, 2 D3	IN4148 4001
CAPACITORS C1, 2, 3	1 On polyester	D4	IN5401
C4, 5, 6, 7 C8	100n polyester 100u 25V electrolytic	Relay = 6V, 2-pole resistance 70R.	changeover type. Coil

What A Turn On

R12

nν

When installation is complete, turn on all power switches, check that the unit functions correctly, and then adjust pre-set pots RV1 and RV2 for the required operation. To set RV1, move the transmitter joy stick to the required 'null' position, and then adjust RV1 for zero motor speed: under this condition the relay should be on the verge of switching between the on and off states. Next, move the transmitter joy stick fully forward, and adjust RV2 for the desired maximum motor speed. The setting up procedure is then complete.

FROM DECODER

Finally, note that the operation of the motor speed controller can be adversely affected by electrical interference from motors, etc. All motors in the model must therefore be adequately suppressed. A 100n disc ceramic connected directly across the motor terminals works pretty well in most cases.

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Nov. 76 Jul. 77	'General Purpose Preamp	609	1.00	4.85	BEG
Jul. 77	GSR Monitor	612	1.10	19.75	BEGHL
Apr. 77	*Burgiar Alarm	613	1.10	10.85	BEGH
Feb. 77	*Bench Amplifier *Compander	615	1.15	13.20 27.35	BEGHL BEGHL
Nov. 77 Mar. 77	*50 watt High Power Amp	618	2.55	9.75	BE
Mar. 77	100 watt High Power Amp	619	2.10	12.80	BE
Mar. 77	'High Power Amp P.S.U.	620	1.65	8.70	BEJ
Mar, 77 Oct. 77	*Digital Thermometer	621	1.70	21.85	8FGHL
Feb. 77	'LED Dice	624	.90	7.10	BEGHL
	*Active Crossover (2 pcbs)	625	3.30	15.30	BFGHL
	'Marker Generator	626	1.20	8.40	BEGHL
Nov. 77	Skeet	627 628	2.55 1.10	21.90 6.25	BEGHL BEGJ
1/2	*Flash Trigger *Disco Light Show	629	4.25	25.95	BFGJ
	*Pink Noise Generator	630	1.05	4.30	BEL
Nov. 76	541 Train Controller	T001	1.35	18.85	BEHL
Jan. 77	444 5 watt Stereo (2 pcbs)	T002	3.10	26.95	BEGK
Feb. 77	448 Disco Mixer	T003	2.35	19.40	BEJ
Dec. 77 Jan. 78	Clock B.	T004	3.30	16.75	BE
Jan. 78	House Alarm A. House Alarm B.	T005 T006	3.20 1.50	30.50	BEHM
Feb. 78	Metal Locator Mk. II	T007	1.60	5.50 22.60	BEHL
March 78	Frequency Shift P.S.I.I	T008	1.10	5.95	BE
Walcii 70	Frequency Shift P.S.U. Frequency Shifter	T009	2.50	24.95	BEL
	L.C.D. Meter	T010	1.60	27.95	BEG
1	Light Dimmer	TO 1 1	.90	8.60	BEH
Apr. 78	Gas Monitor	T012	1.40	15.95	BEHL
May 78	Star Trek Radio	T013	1.55	9.80	BFH
	Stars & Dots	T014	3.00	T.B.A.	BEHL
June 78	Spectrum Analyser (2 pcbs)	T015 T016	13.90 1.45	76.95 17.20	CEHM 8EHL
	Wein Oscillator Torch Finder	T018	.75	2.40	BE
	Temperature Meter	T019	1.60	27.70	BEG
Aug. 78	Etiwet Plant Waterer	T020	1.30	6.10	BEH
Sept. 78	Cross Hatch Generator	T021	2.10	14.95	BEGHL
100	Stac Timer	T022	3.00	27.45	BEJL
	Wheel of Fortune	T023	1.55	9.80	BEHL
Oct. 78	Complex Sound Generator R.F. Power Meter	T024 T025	3.95 1.60	25.75 15.30	BEH BEHL
	Power Bulge	T026	.85	3.65	BEHL
	Telephone Bell Extender	1027	1.25	11.40	BEHL
Oct. 78	Proximity Switch	T028	2.30	15.35	BEGH
Feb. 78	Ultra Sonic Receiver	T029	1.00	10.75	BEH
Feb. 78	Ultra Sonic Transmitter	T030	.90	5.65	BEH
Nov. 78	Cuts Cassette Interface Audio Oscillator (2 pcbs)	T031 T032	2.70 4.60	14.95 39.95	BEHL BEHL
Dec. 78	Car Alarm (2 pcbs)	T032	2.50	6.95	BEJ
UBC. 76	Wine Temperature Meter	T034	1.30	- 0.55	_
	Curve Tracer	T035	1.20	10.95	BEHL
f f	Eprom Programmer	T036	2.65	23.35	BEH
	Eprom Programmer P.S.U.	T037	1.70	6.25	BE
Jan. 78	Car Tachometer	T038 T039	2.50 2.55	12.20 21.55	BF BE
	Digital Module A & B (2 pcbs) Digital Dial (Excl.=T039)	T040	1.40	8.90	BE
	Log Converter	T040	3.60	26.75	BE
Feb. 79	Tape Slide Synchroniser	T042	2.30	20.95	BEHL
1007 10	Tape Noise Limiter	T043	.80	3.70	BEHL
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Mar. 79	Headlight Delay	TO 45	.75	6.75	BEHL
	Logic Trigger	TO 46	2.70	18.95	ВЕН
- may 1.5	Stage Dimmer Control Module	TO 47	2.95	47.95	TBA BEH
	Stage Dimmer Module 10 amp Stage Dimmer Module 20 amp	TO48 TO49	6.30	28.30 27.05	BFJ
	Audio Power Meter	TO50	3.45	72.45	BEH
Api. 79	Click Eliminator	TO51	4-55	49.95	BEHL
	Wind speed indicator	TO52	3.40	27.40	BEH
	Guitar effect unit	TO53	1.20	11.69	BEGHL
May 79	Double Die	TO54	1.65	14.95	BEHM
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June 79	Tuner Amp Main's speaker	TO58 TO59	TBA .90	5.45	BEGHL
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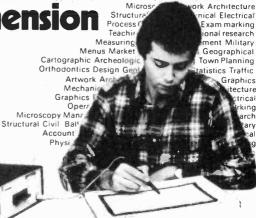
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1	LM386N		LM3914N	2.79	CA3034
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1	LM388N	1.10	LM78L05CH	.85	CA3036
1		1.00	LM78L12CH		CA3038
1	LM389N	1.00	LM78L15CH		CA3038A
1	LM392N	.87	LM78L24CH		CA3039
1	LM7018	2.99	LM7805KC	1.56	CA3840
1	LM701C	2.99	LM7812KC	1.56	CA3041
ı	LM702C LM703LN	.81	LM7815KC	1.56	CA3042
1		1.15	LM7824KC		CA3043
1	LM 709CH LM 709-8	.70	LM78L05CZ	.30	CA3045
	LM709-8 LM709-14	.50	LM78L12CZ	.30	CA3046
1		.49	LM78L15CZ	.30	CA3047
J	LM710CH LM710-14	.67	LM78L24CZ	.30	CA3047A
1	LM711CN	. 4 B	MC667P	2.75	CA3048
ł		.48	MC671P	1.75	CA3049
ı	LM716 LM723CH	1.00	MC672P	1.75	CA3050
ı		.62	M C 7 2 4 P	2.10	CA3051
ı	LM723C-14	.45	MC789P	1.80	CA3052
ı	LM741CH	.50	M C 7 9 D P	3.10	CA3053
1	LM741C-8	.30	MC798P	2.20	CA3054
l	LM741C-14	.60	MC799P	2.20	CA3059
ı	LM747CH	.78	MC832P	.70	CA3060
ı	LM748-8	.50	MC833P	.70	CA3062
1	LM748-14	.50	MC836P	. B 2	CA3064
ı	LM900	.50	M C 8 3 7 P	.82	CA3065
ı	LM911	.50	M C 8 3 8 P	2.35	CA3068
1	LM921	.50	MC840P	1.65	CA3070
1	LM923	.50	MC844P	.70	CA3071
1	FW1303N	1.15	MC846P	.70	CA3072
	LMI3D4N	1.52	MCB48P	1.10	CA3075
ı		1.52	M C 8 4 9 P	.70	CA3076
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4

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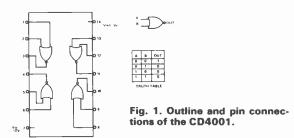
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40 CMOS CLOCKS

There are many ways of using the CD4001 and CD4011 CMOS ICs to make bistable, astable and monostable multivibrator circuits. Ray Marston presents the definitive work on the subject, with 40 practical circuits.

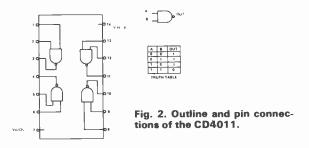
THE AMATEUR AND PROFESSIONAL circuit designer often finds himself in the situation where he needs to use a minimum-cost CD4001 or CD4011 CMOS pulse or clock generator circuit, or where he needs to use a few spare CMOS NAND or NOR gates from an existing circuit to make up a multivibrator that will meet his specific design needs. In either case, the designer will find a concise guide to practical NAND- and NOR-gate CMOS multivibrator circuits of inestimable value.

This article is just such a guide. It presents some forty different ways of using the low-cost CD4001 and CD4011 quad 2-input gate CMOS integrated circuits in bistable, astable and monostable multivibrator applications. All of the circuits shown can be operated over the full five volts to fifteen volts supply range when used with 'B' series CMOS.



THE CD4001 and CD4011 ICs

Figures 1 and 2 show the outlines and pin connections of the CD4001 and CD4011 integrated circuits. These two ICs are quad 2-input gates. The CD4001 provides NOR gate functions and the CD4011 provides NAND gate functions. Fig. 1 shows the truth table of each of the four NOR gates of the CD4001. Note that the output is high if both inputs are low, but goes low if either or both inputs go high. Fig. 2 shows the truth table of each of the four NAND gates of the CD4011. The output is normally high and goes low only if both inputs are high.



The CD4001 and CD4011 are very inexpensive ICs. They typically retail at about 16 pence each in one-off quantities (allowing for some variation between suppliers), which works out at about 4 pence per gate. They can be used in a wide variety of very useful two-gate multivibrator applications and are thus highly cost-effective devices.

Bistable Multivibrator Circuits

The CD4001 and CD4011 can both be used in two-gate R-S (Reset-Set) bistable multivibrator circuits, but have quite different input triggering requirements. Fig. 3 shows the practical circuit and waveforms of a pulse-triggered NOR version of the bistable. The circuit has two outputs, a normal output from IC1a and an inverted output from IC1b. When a positive-going trigger pulse which switches between roughly zero and full supply is applied to the IC1b input, the normal output sets high and locks in this state irrespective of any further signals at the input of 'IC1b. The output can only be reset low again by applying a positive-going pulse to the input of IC1a, at which point the output goes low and is then immune to any subsequent trigger pulses at the input of IC1a.

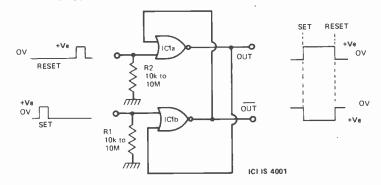


Fig. 3. Practical circuit of a pulse-triggered NOR bistable.

Note that the input terminals of IC1a and IC1b are tied to ground (the zero-volts line) via R1 and R2: these resistors can have any convenient values in the range 10k to 10M. If inputs to IC1a and IC1b are direct-coupled from preceding logic networks, however, R1 and R2 can be omitted from the circuit.

Manual NOR Gate

Fig. 4 shows a manually-triggered version of the Fig. 3 NOR gate circuit. This type of circuit is often referred to as a 'noiseless' switch, since its output is unaffected by the contact bounce, etc., of its two control switches.

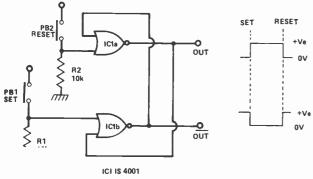


Fig. 4. Manually triggered NOR bistable.

NAND Bistable

Fig. 5 shows the CD411 NAND gate version of the bistable circuit. This circuit is almost identical with that of Fig. 3, except for the positioning of R1 and R2. Note, however, that the NOR gate circuit needs positive-going trigger pulses, while the NAND circuit needs negative-going pulses, and that the set pulse is applied to IC1b in the NOR circuit, but to IC1a in the NAND circuit.

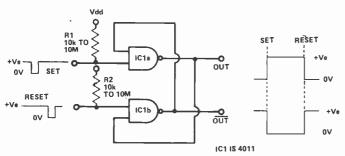


Fig. 5. A CD4011 NAND bistable, pulse triggered.

Manual NAND Bistable

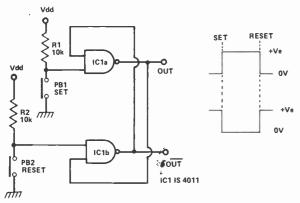


Fig. 6. Manually triggered NAND bistable.

Fig. 6 shows the manually-triggered version of the NAND-type bistable. Note here that although R1 and R2 are shown as having values of 10k, they can in fact have any resistance values from a few thousand ohms up to about 10M, depending on the precise details of the specific application. This versatility leads to the development of the touch-triggered NAND bistable circuit of Fig. 7, in which R1 and R2 have values of 10M, and the circuit can be triggered by placing any resistance that is significantly less than 10M (such as finger resistance) across the touch contacts. R3 and R4 are used in this circuit to protect the inputs of the two gates.

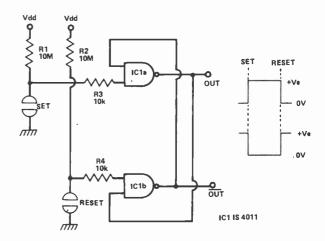
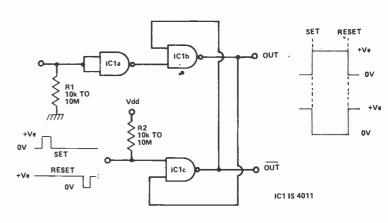


Fig. 7. Touch-triggered NAND bistable.

The bistable circuits that we have looked at so far all use same-polarity (either both positive or both negative) trigger signals. In some applications, however, it is necessary or convenient to use opposite-polarity signals to trigger the bistable, and this type of action can be obtained by placing an inverter stage in series with one or other of the normal bistable input terminals. Figs. 8 and 9 show two alternative circuits of this type.



Using opposite-polarity signals to trigger a 4011 bistable, Fig. 8 (above), and a 4001 bistable, Fig. 9 (below).

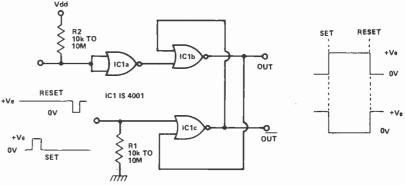


Fig. 10 shows alternative ways of connecting a 2-input NAND or NOR gate so that it acts as a simple pulse inverter stage. These circuits are useful in a multitude of applications.

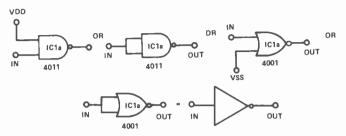


Fig. 10. Using a 2-input NAND or NOR gate as an inverter.

Basic 2-Gate Astable Circuits

The CD4001 and CD4011 can both be used in a variety of basic 2-gate astable multivibrator circuits. In these circuits the gates are connected as simple inverters, so the two types of IC give identical performances.

CMOS Astable

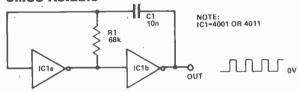


Fig. 11. Circuit of the basic 2-gate CMOS astable.

The most basic and useful 2-gate CMOS astable circuit is shown in Fig. 11. This circuit generates a decent square wave output, has excellent thermal stability and operates at about 1 kHz with the comfort values shown. The frequency is inversely proportional to the C-R time constant, so the frequency can be raised by lowering the values of either C1 or R1. In practice, C1 must be a non-polarized capacitor, and can have any value from a few tens of picofarads to a few microfarads. R1 can have any value from about 4k7 to 10M. For variable frequency operation, wire a fixed and a variable resistor in series in the R1 position.

The output of the Fig. 11 astable circuit switches (when lightly loaded) almost fully between the zero and positive supply voltage levels, but the junction of R1 and C1 is prevented from swinging below zero or above the positive rail levels by the built-in clamping diodes at the input of IC1a. This characteristic causes the operating frequency of the circuit to be somewhat dependent on supply rail voltages. As a rough rule of thumb, the frequency falls by about 0.08% for each 1% rise in supply voltage. Typically, if the frequency of this astable is normalised with a 10 volt supply, the frequency will fall by 4% at 15 volts, or rise by 8% at 5 volts.

Also, the operating frequency of the Fig. 11 circuit depends somewhat on the transfer voltage value of the individual gate that is used and can be expected to vary by as much as 10% between individual ICs. The output symmetry of the waveform is also dependent on the transfer voltage value of the IC and, in most cases, the circuit will give a non-symmetrical output. In the vast majority of 'hobby' and other non-precision applications, these deficiencies of the basic astable circuit are of little practical consequence.

Some can be minimised by using the 'compensated' astable circuit of Fig. 12, in which resistor R2 is wired in series with the input of IC1a. This resistor can have any value between two and ten times that of R1, and its main purpose is to allow the R1-C1 junction to swing freely below the zero and above the positive supply rail voltages during the switching action and thus reduce the dependance of the circuit operating frequency on the supply voltage. Typically, when R2 is given a value ten times greater than R1, the frequency varies by only about 0.5% when the supply voltage is varied between 5 and 15 volts.

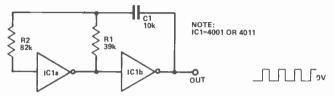


Fig. 12. A compensated astable circuit.

The basic and compensated astable circuits of figs. 11 and 12 can be built with a good number of detail variations. Some of these are shown in Figs. 13 to 18. In the basic astable circuit, for example, C1 alternately charges and discharges via R1. Figs. 13 to 15 show how the basic circuit can be modified to give alternate C1 charge and discharge paths.

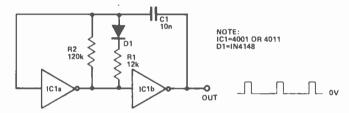


Fig. 13. Modifying the circuit to give C1 alternate charge and discharge paths and produce a non-symmetrical output waveform

Fig. 13 shows one way of modifying the stable so that it gives a non-symmetrical output waveform. Here, C1 charges in one direction via R1 and R2 in parallel, to give a high output, but discharges in the reverse direction via R2 only, to give a low output.

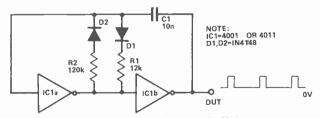


Fig. 14. Controlling the astable's on and off time.

On/Off Control

Fig. 14 shows how the circuit can be further modified by also wiring a diode in series with R2, so that the ON time of the output is controlled only by R1, and the OFF time is controlled only by R2. These two circuits can be made to give variable outputs by replacing either or both of their timing resistors with a fixed and a variable resistor in series.

Variable Symmetry

Fig. 15 shows how the astable can be modified to give a variable symmetry or M/S-ratio output, while maintaining a near-constant frequency. C1 in this circuit charges on one direction via D1-R2 and one half of RV1, and in the other direction via D2-R1 and the other half of RV1. The M/S-ratio can be varied over the range 1:10 to 10:1 via RV1.

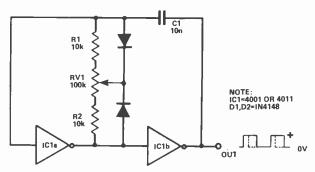
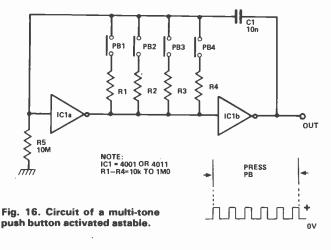


Fig. 15. Controlling the mark/space ratio.

Fig. 16 shows the circuit of a multi-tone push-button activated astable. Normally, when all push-button switches are open, R5 holds the input of IC1a (and thus the output of IC1b) low. Resistors R1 to R4 all have values that are low relative to R5, so the circuit acts as a normal astable when any one of the push-button switches is closed. This circuit can be used in multi-tone musical instruments and gadgets, etc. and has the major advantage that it draws negligible current when in the standby mode. There is no limit to the number of push-button switches that can be used with the circuit.



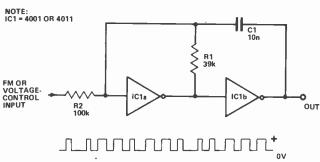


Fig. 17. Frequency modulation of an astable.

Frequency Modulation

Fig. 17 shows how the astable can be subjected to frequency modulation or voltage control of frequency by simply feeding the FM or voltage-control signal to the input of IC1a via a resistance that is much larger than R1 and Fig. 18 shows how the circuit can be further modified to act as a special-effect voltage-controlled oscillator that shuts off when the input voltage falls below a pre-set value.

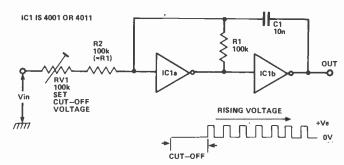


Fig. 18. Using an astable as a voltage-controlled oscillator with an output cut-off.

Gated 2-Gate Astable Circuits

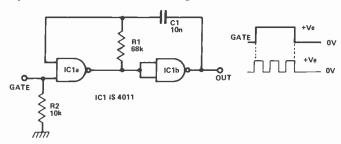


Fig. 19. A NAND astable with a normally-low output, gated by a high input signal.

All of the astable circuits of Figs. 11 to 15 can be modified for gated operation, so that they can be turned on and off via an external signal, by simply using a 2-input NAND or NOR gate in place of the inverter in the IC1a position and applying the input control signal to one of the gate input terminals. The CD4001 and CD4011 ICs can both be used in this type of application, but give quite different types of gate control and output operation. Figs. 19 and 20 show the two basic versions of the gated astable circuit.

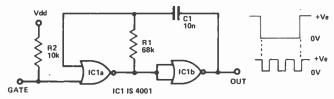


Fig. 20. A NOR astable with a normally-high output, gated by a low input signal.

Note that the Fig. 19 NAND astable circuit has a normally-low output and is gated by a high input signal, while the fig. 20 NOR astable has a normally-high output and is gated by a low input signal. Also note that, although R2 is shown in the diagram as having a value of 10k, R2 can in fact have any value in the range 10k to 10M and can be omitted altogether if the gate signal is applied from a preceeding logic state.

Note in the Fig. 19 and 20 circuits that the output signal terminates immediately the input gate signal is removed. Consequently, any noise present at the gate terminals of these circuits also appears at their outputs.

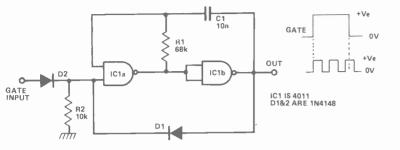
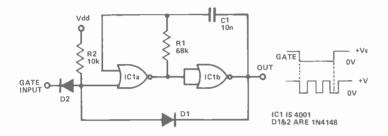


Fig. 21 (above) and Fig. 22 (below) overcome the problem of noise appearing at the gate terminals.



Figs. 21 and 22 show how the circuits can be modified to overcome this defect. Here, the gate signal of IC1a is derived from both the outside world and from the output of IC1b via diode OR gate D1-D2-R2. As soon as the circuit is gated from the outside world via D2 the output of IC1b reinforces the gating via D1 for the duration of one half astable cycle, thus eliminating any effects of a noisy outside world signal. The outputs of the circuits are complete numbers of half cycles. Note that R2 is an essential part of these circuits.

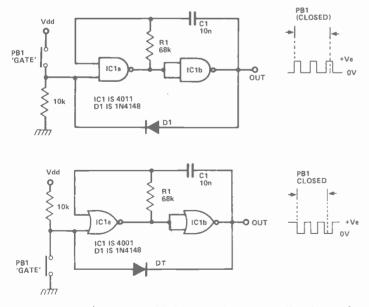


Fig. 23 (top) and Fig. 24 (above) show manually-triggered astables with noise-elimination networks.

Figs. 23 and 24 show manually-triggered versions of the Fig. 21 and 22 circuits. These circuits are of particular value when they are used as low speed clock generators, operating at about 5 Hz: when PB1 is briefly stabbed, the generate a single clean clock pulse: when PB1 is held down, they generate five clean clock pulses per second.

Clock Generator Circuits

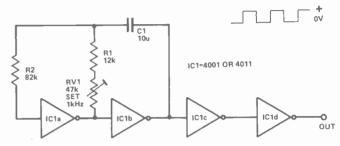


Fig. 25. Speeding up the rise and fall times of the astable output to produce clean clock signals.

The 2-gate astable circuit is generally not suitable for direct use as a clock generator with fast-acting counting and dividing circuits. Such circuits require the use of clean clock signals, with fast rise and/or fall times. The problem is that 2-gate astables designed around 'A' series or non-buffered CMOS produce clock outputs with rather slow rise and fall times, whereas 2-gate astables designed around buffered-output 'B' series CMOS produce outputs with good rise and fall times, but tend to produce 'dirty' clocking if there is the slightest trace of noice on their power supply lines.

Fortunately, these problems can easily be overcome by wiring a couple of inverter-connected gate stages in series with the output of the astable circuit, as shown in the example of Fig. 25. These inverter stages speed up the rise and fall times of the astable output waveform and also produce effective level shifting between the output of the astable and the clock input terminal of any external device, thereby reducing or eliminating the effects of noise on the clock circuit.

The Ring-of-Three Astable Circuit

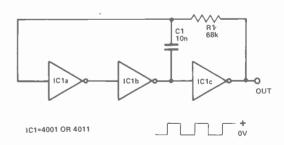


Fig. 26. The 'ring of three' astable circuit produced a very clean output waveform.

An alternative way of making a clock generator is to use the 'ring-of-three' astable circuit of Fig. 26. This circuit is similar to the basic circuit of Fig. 11, except that the positions of R1 and C1 are transposed, and the inverting input stage (IC1a) of the Fig. 11 circuit is effectively replaced by an ultra-high-gain non-inverting stage (comprising IC1a and IC1b in series) in the Fig. 26.

circuit. Because of the very high gain of its composite input stage, the Fig. 26 'ring-of-three' circuit produces a very clean output waveform, with excellent rise and fall times, and is directly suitable for use as a clock generator.

The 'ring-of-three' astable circuit can be subjected to all of the basic design variations shown for the 2-gate astable. For example, C1 alternatively charges and discharges via R1 in the same way as in the Fig. 11 circuit, so the circuit can be subjected to all of the variations shown in Figs. 13 to 15. It can be designed in either basic or 'compensated' versions, etc.

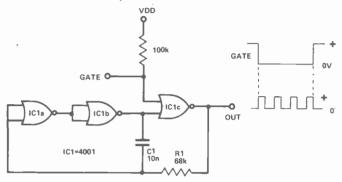


Fig. 27. A gated NOR 'ring of three' circuit with a normally low output, gated by a low input.

The 'ring-of-three' circuit offers interesting possibilities when it is used in the gated mode, because it can be gated on and off via either its IC1b or IC1c. stages. Figures 27 to 30 show four variations on this theme.

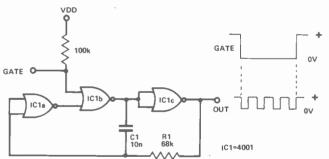


Fig. 28. A gated NOR 'ring of three' circuit with a normally high output, gated by a low input.

Figs. 27 and 28 show alternative versions of the gated NOR-type 'ring-of-three' circuit. Both circuits need a 'low' signal to gate the astable on. Note that the output of the circuit is normally-low if the gate signal is applied to IC1c, or is normally-high if the gate signal is applied to IC1b.

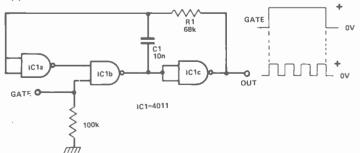


Fig. 29. A gated NAND 'ring of three' circuit with a normally low output, gated by a high input.

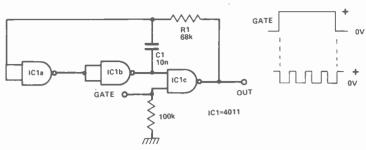


Fig. 30. A gated NAND 'ring of three' circuit with a normally high output, gated by a high input.

Similar variations are found in the NAND version of the gated 'ring-of-three' circuit, as shown in Figs. 29 and 30. These circuit need a 'high' signal to gate them on, and have a normally-low output if the gate signal is fed to IC1b, or a normally-high output if the gate signal is fed to IC1c.

Monostable Multivibrator Circuits

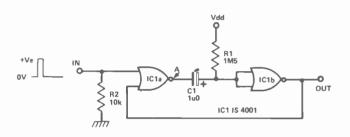
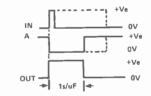


Fig. 31. A 2-gate NOR monostable multivibrator.

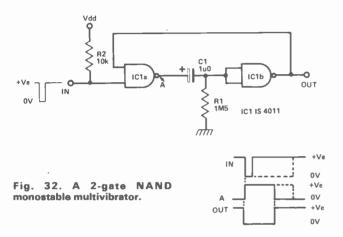


The CD4001 and CD4011 can both be used to make an exceptionally useful type of 2-gate monostable multivibrator or pulse generator circuit. The two basic versions of this circuit are shown in Figs. 31 and 32. In these circuits the duration of the output pulse is determined by the values of R1 and C1, and approximate one second per microfarad of C1 value when R1 has a value of 1M5. In practice, C1 can have any value from roughly 100 p to a few thousand u, and R1 can have any value from about 4k7 to 10M.

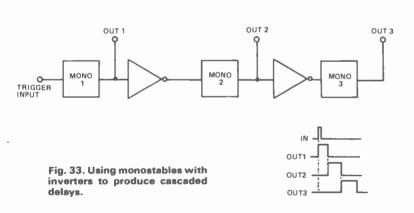
One outstanding feature of these circuits is that the input trigger pulse or signal can be direct coupled and has no appreciable effect on the length of the circuit's output pulse: the trigger pulse can be shorter or longer than the output pulse. The NOR version of the circuit has a normally-low output, and is triggered by a positive-going input pulse, while the NAND version of the circuit has a normally-high output and is triggered by a negative-going input pulse.

A signal feature of these circuits is that the pulse signal appearing at point "A" has a length that is equal to that of either the output pulse or the input trigger pulse, depending on which is the greater of the two. This feature is of value when making pulse-length comparators and over-speed alarms, etc.

The Fig. 31 and 32 circuits have only two significant defects. One of these is that the pulse length depends somewhat on the transfer voltage value of the individual IC that is used in the circuit. The other is that the pulse length also depends somewhat on the supply voltage value that is used with the circuit, just as the operating frequency of the basic 2-gate CMOS astable varies slightly with the supply voltage value. These defects are of little consequence in most practical applications, however.



If a number of the Fig. 31 and 32 circuits are to be interconnected to give cascaded delays (as in a delayed-pulse generator, for example), an inverter stage must be interposed between the outputs and inputs of successive monostables, to give correct-polarity trigger signals. Figure 33 shows the basic system.



Alarm Call Sound Generator Circuits

A single CD4001 or CD4011 IC and one or more transistors can readily be used to make a variety of types of very useful alarm call sound generator circuits. Figs. 34 to 41 show some practical circuits of this type. In all cases, the circuits can be powered from any supply in the range 5V to 15V and can be used with any speaker in the range 3R to 100R. Output powers range from tens to hundreds of milliwatts, depending on speaker impedances and supply rail voltages used, but can readily be boosted to tens of watts by using additional transistor power-boosting stages.

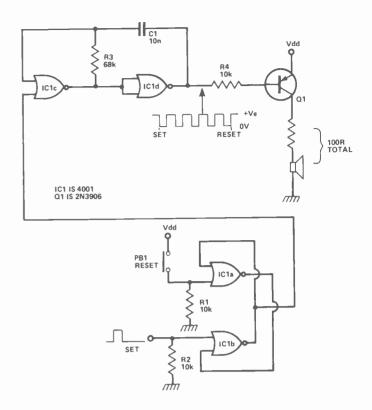


Fig. 34. Circuit of a NOR latching monotone alarm call generator.

Figs. 34 and 35 show two versions of a latching monotone alarm call generator. IC1a and IC1b are wired is applied to the circuit the IC1a-IC1b bistable self-latches and switches on the IC1c-IC1d-1kHz astable tone generator. The circuit can be reset to the OFF state by momentarily closing PB1.

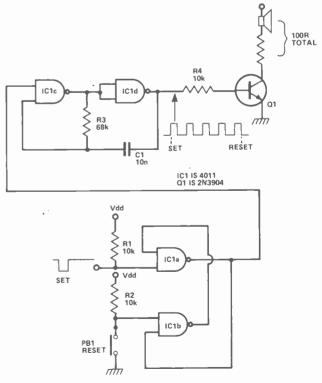


Fig. 35. Circuit of a NAND latching monotone alarm call generator.

FEATURE: 40 CMOS CLOCKS

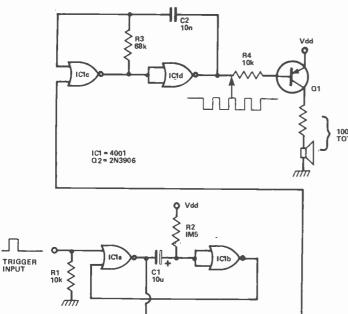


Fig. 36. A NOR alarm call generator with auto turn-off.

Figs. 36 and 37 show versions of an auto-turn-off monotone alarn call generator. IC1a and IC1b are wired as a monostable multivibrator, which turns on the IC1c-IC1d astable for about 10 seconds each time that it is triggered.

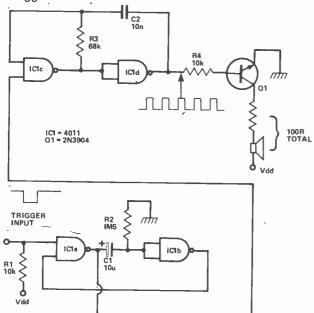


Fig. 37. A NAND alarm call generator with auto turn-off.

The Fig. 38 and 39 circuits generate a pulsed-tone signal, in which a 1 kHz astable (IC1c and IC1d) is gated on and off by a 6 Hz astable (IC1a and IC1b) when a suitable control signal is applied to the input terminal of IC1a.

Finally, Fig. 40 shows a warble-tone generator, which switches through a 2-tone cycle once per second when a suitable control signal is applied to the inputs of IC1a and IC1c, and which generates a sound similar to a British police car siren. The depth of frequency variation of the circuit is determined by R3, which can have any value in the approximate range 120k to 1MO.

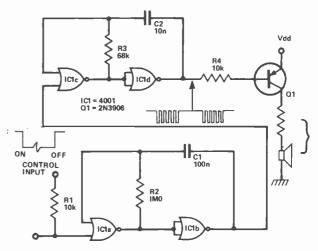


Fig. 38. Generating a pulsed-tone signal with 6Hz and 1kHz NOR astables.

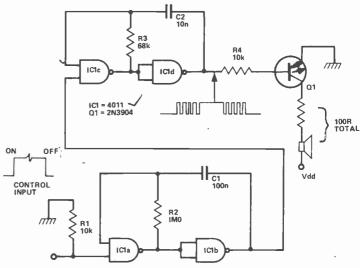


Fig. 39. Generating a pulsed-tone signal with 6Hz and 1kHz NAND astables.

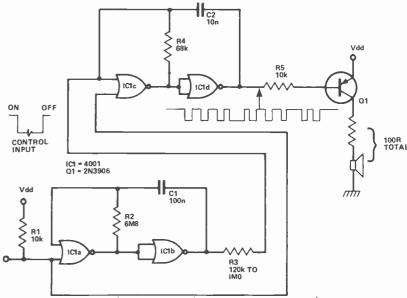


Fig. 40. A warble-tone generator — sounds like a police car siren.

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ELECTRONICS TIME CENTRES

M13

audiophile...

Hi-fi 79 at the Cunard Hotel attracted Ron Harris this month, as did a new record cleaner. Also a good chance to show how witty you are and win a free subscription.

A TALE OF MANY speakers is what the 1979 Spring hi-fi show turned into. Wandering the halls of the Cunard in search of the sonic grail you get buffeted from side to side by the alternate blasts of sound emanating from the demo rooms. After about two hours of solid listening I start to get ear fatigue and thingd son't seem the same somehow.

In consequence things get done in bursts of two hours at a time punctuated with clincking of refreshments. On the first pass this year it became apparent that it was to be the Year of the Cone.

MA24U

Monitor Audio first. The MA2 is a 'domestic reference' design and stands some 850mm high. (About 33in in English height). It will handle around 100W of programme power, and produces a very nice sound indeed. At about £300 the pair they are going to give the competition a tough time.

Wharfedale have extended their 'E' series upwards into an E90 design which is twice the size of the E70 nearly and more than twice as imposing. We've got no photographs of the beast simply because Wharfedale hadn't got any and haven't kept their promise to send us any since! So there. Its still a nice speaker anyway.

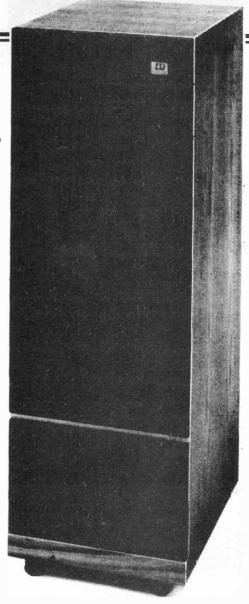
KEFs contribution to the herd was a small one. Tiny in fact. I'd go so far as to say it was so small I almost missed it. The Reference 101 is a bookshelf speaker that just might fit into a bookshelf. This was the real surprise of the show, however, as upon first encounter the almost universal reaction was to hunt the 105s that were not hiding behind the curtains.

The sound was open and spacious with good imaging and a convincing bass response. Very nice one Kef.

Celestions Follies

The Celestion stand was dominated by two huge double boxes which, when energised, did a quick 'room empty' job. The efficiency is somewhat high you see, and the amplifier somewhat powerful.

I think they're designed for PA and studio usage but they are finished in wood veneer and more than likely quite a few dozen will end up in living rooms. Big living rooms I hope. At their price and size they come up against things like the JBLs and for sound quality I personally prefer the P1s (that's what they're called by the way). Well worth the listen if you're in that market.



Above: the Monitor Audio MA2 loudspeaker. A highly recommended domestic design.

Below: the Celestion PI. It sounds as imposing as it looks.





Below: KEF's 101 reference model. If your living room (or preference) favours small enclosures then don't miss 'em out.



Below: Celestions new Dittons. In the centre is the new 662, which is their new version of our reference-the faithful ole 66. It remains to be compared whether it is *that* much better!



Below: No this wasn't at the show but it's worth the look anyway. A new record cleaner called a TANTRACK. Two arms are provided to cope with any turntable height, and the finish is a very posh steel and chrome. Available from Dorking Systems Ltd, 23 South Street, Dorking, Surrey. Price £6.25 plus VAT.



Left: JVCs KDA8 computerised cassette deck. It fixes up its own own bias and equalisation levels, and can cope with metal tape.

Right: Goldring headphones! Superex classic CL1s, a good smooth sound at a decent price. No, I'm not gonna tell you how much, find out yourselves!

Head Man

New for heads from Goldring is the Suprex headphone range. Amongst the four models they decided to import the Classic C1 — the middle of the group caught my attention most. They possess a nice smoothness to them that could be lived with. And they're comfortable. Koss take note please. Speaking as someone stuck with the habitual earache engendered by ESP10s the Suprex could be very attractive if for no other reason than that.

On Your Metal

Scotch and JVC between them made an exhibition of the new metal tape formulations and the JVC KDA8 machine to use them. The KDA8 is quite a story in itself really. It sets up for each type offered to it by recording a test tone and optimising bias, sensitivity and equalisation automatically — it even rewinds to the beginning again and all in 25secs. The demonstration was most impressive — as they usually are — and we hope to do more with the machine in the near future.

Before anyone asks I could find no possible reason to include the beautiful Felicity Kendal in this months Audiophile. She was not at the exhibition nor has she anything to do with any of the products featured here. That being the case I have no reason to mention the lovely lady and therefore I shall refrain.

This here picture advertises Marantz. But we couldn't find the Marantz stand!! Now with a picture like this, there just HAS to be a brilliant, witty, superb caption. But we can't find THAT either, so its open to you lot. The best wins a years subscription. Closing date June 30th. Mark envelopes 'Audiophile Caption.'



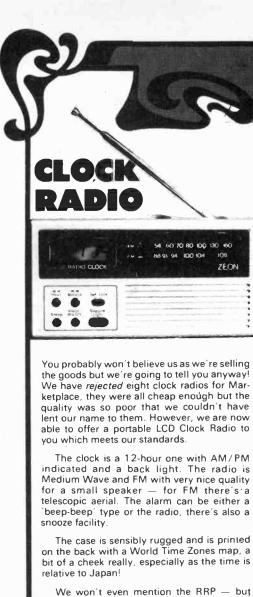
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The clock is a 12-hour one with AM/PM indicated and a back light. The radio is Medium Wave and FM with very nice quality for a small speaker — for FM there's a telescopic aerial. The alarm can be either a

on the back with a World Time Zones map, a bit of a cheek really, especially as the time is

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RKET PLACE

LCD CHRONO



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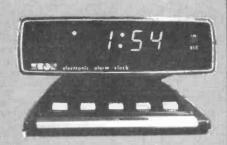
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20FE09	9+9	1A each	3.25	70p	50FE30	36+30	0.75A each	3.25	70p
50FE09	9+9	2.5A each	3.98	85p	60FE30 '	30+30	1A each	3.98	85p
60FE09	9+9	3A each	1.58	50p	80FE30	30+39	1.2A-each	4.72	1.00
06FE12	12+12	B.25A each	1.90	50p	Multi Ten B	nego. Voltage		,	
08FE12	12+12	0.3A each		60p	Austinble 2	45680	10, 12, 15, 18.		- 1
12FE12	12+12	0.5A each	2.10	70a	VASIISBIG 2	19819	CR 15.0-15 0-1	2-15	
20FE 12	12+12	0.8A each	2.74	70p	-		On To.o to	3.55	7Up
50FE12	12+12	2A each	3.25	85p	30FE30	24+30	14	4.78	85e
60FE12	12+12	2.5A each	3.98	1.00	60FE36	24+30	2A	5.95	1.00
80FE12	12 + 12	3A each	4.72		80FE36	24+30	3A		1,15
06FE15	15+15	0.2A each	1.58	50p	100FE40	24+30	4A	7.10	1.14
08FE15	15+15	0.25A each	1.90	50p	Contro Ton	Secondary		-	
12FE15	15+15	0.4A each	2.10	60p	FE06	6-8-6	1A each	2.10	60p
20FE15	15+15	0.6A each	2.74	70p	£009	9-6-9	1A each	2.74	700
50FE15	15+15	1.6A each	3.25	70p		12-0-12	1A each	2.86	70g
60FE15	15+15	2A each	3.98	85p	FE12	15-0-12	1A sach	3.25	700
80FE15		3A each	4.72	1.00	FE15	20-0-20	1A sack	3.25	70p
06FE20	20+20	0.15A each	1.58	50p	FE20		1A each	3.98	1.00
08FE20	20+20	0.2A each	1.90	50p	60FE52	26-0-26	1A each	3.98	1.00
12FE20	20+20	0.25A each	2.10	60p	60FE28	28-0-29	1A each	3.98	1.00
20FE20	20+20	0.5A each	2.74	70p	80FE80	30-8-30	2A each	5.15	
50FE20	20+20	1.2A each	3.25	70p	100FE26	26-0-26	2A each	5.15	1.15
60FE20	20+20	1.5A each	3.98	85p	100FE30	30-0-30	ZA Back	5.15	1.15
80FE 20	20+20	2A each	4.72	1.00	100FE36 -	36-0-36	ZA BOCH	5.10	1.15
	Char	ger Transformur				Audio Cross	Over Cells	-	-
48FE12	0-6-12	- 4A	3.25	70p 1	FE01	[0,1mH		0.26	28p
66FE12	0-6-12	5A	4.00	85p	FE03	0.3mH	1	0.26	20p
79FE12	8-6-12	6A	5.10	1.00	FE05	9.5mH		0.30	20p
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7/8	2R-22k	14p	10 ½ p
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1-99

.0010082 µ	4p	3р
.011 µ	5p	3.6p
.15	7p	4.8p
.22 µ	9p	6.2p
.33μ	10p	7.4p
.47μ	14p	10.6p
250V polyeste	r	
Value	1-99	100+
.01068	4p	2.8p
.122	5p	3.8p
.33	8p	5.6p
.47	12p	7.3p
.68	15p	9.6p
1.0	20p	13.4p
1.5	26p	18p
2.2	32p	22p
3.3	39p	26p
4.7	49p	32p
6.8	63p	39p

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ELECTROLYTICS
25V: 0.47 1 2.2, 3.3, 4.7, 10, 15, 22, 23, 47μ 7p; 100μ 8p; 150μ 10p; 220μ 12p; 330μ 15p; 470μ 19p; 1000μ 26p; 1500μ 31p; 2200μ; 38p; 3300μ 51p; 470μ 60p; 10000μ can 87p; 40V: 47 1μ 7p; 2.2, 4.7, 10, 15, 22μ 8p; 47μ 9p; 100μ 11p; 150μ 13p; 220μ 15p; 330μ 20p; 470μ 24p; 1000μ 34p; 1500μ 45p; 220μ 60p; 470μ 72p, 63V; 1, 22μ 8p; 47μ 9p; 10μ 10p; 22μ 11p; 47μ 12p; 100μ 13p; 220μ 18p; 470μ 26p; 1000μ 51p; 220μ 18p; 470μ 26p; 1000μ 51p; 220μ 78p; 470μ 26p; 1000μ 51p; 2200μ 78p; 470μ 26p; 1000μ 25p; 1000μ 51p; 2200μ 78p; 470μ 26p; 100μ 26p; 1

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ı				
ı	Value	volts	1-99	100+
Į	0.1-1 μ	35	12p	7р
ł	1.5 µ	35	12p	7 ½ p
1	2.2μ	35	12p	8р
ı	3.3μ	35	12p	8 ½ p
i	4.7μ	35	14p	9 ½ p
Į	6.8 _µ	35	14p	10 ½ p
١	10.0 µ	35	14p	11 ½ p
ı	15μ	20	14p	11 ½ p
1	22μ	16	14p	11½p
ı	33μ	10	14p	11 ½ p
ı	47μ	6	14p	11½ p
ı	68 µ	3	14p	11 ½ p
Į	100 µ	3	14p	11½p

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76013N	130p	85p
76023N	130p	85p
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Noise. K114—15 XK 6116 (BF 241) N.P.N. 200MHz. K115—18 SP 1218 (2N 3702)

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Amp. K118-16 ME 4101 N.P.N. 60V. Low Noise.

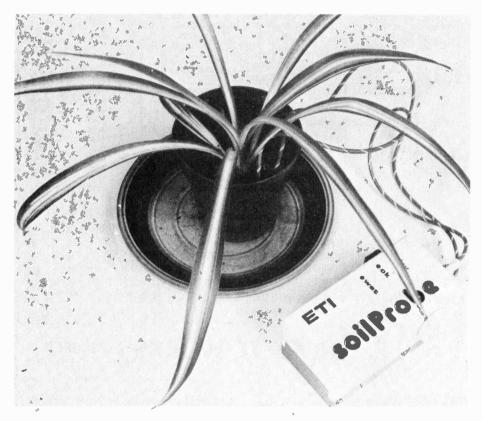
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SOIL PROBE

Check out the roots scene with this ETI soil probe and have happier, healthier plants.



THIS COMPACT UNIT enables you to accurately check the moisture content of your plants' soil in one simple operation. Its range and sensitivity may be adjusted to complement the most fastidious horticulture and horticulturist. The unit works by measuring the resistance of the water in the soil between two probes and comparing it with a previously selected internal resistance adjustable between 1k and 250k.

A Better Buzz

A small 9 volt battery powers the circuit which is built around a few cheap CMOS chips and a low power quad op-amp. To avoid undesirable electrolytic effects at the probes, the resistance bridge is AC

energised. We don't known if the plants like this but we have had no complaints. The probes may be made of any conducting material or just tinned copper

What it is that is on the inside. ETIs Soilprobe exposed. Note that there is not much room in here — not even enough to swing dahlia. So be ye careful of placing and wiring up. A PP3 is the only power source that will fit the box specified so if you want more amps (not needed) be it

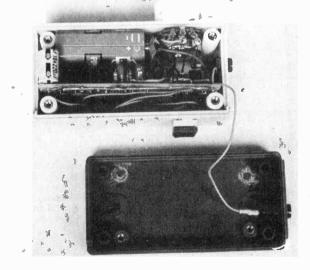
in your own case.

wires placed in the soil a few inches apart and a couple of inches deep. The circuit will tolerate wire leads up to a few feet in length and no special screening is required. A three level comparator whose pass range is internally preset indicates whether the soil is too wet, dry or OK and the required resistance is set by adjustment of a case-mounted potentiometer.

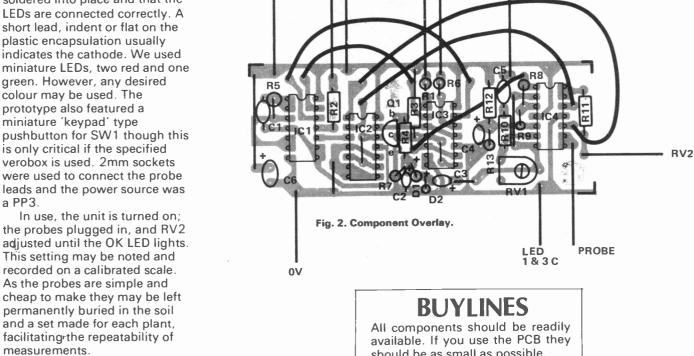
Construction and Use

If you want to use the case shown in the accompanying photographs, be prepared for some precision work as some of the internal pillars need to be removed and the components and PCB are a very snug fit.

Construction is straightforward provided care is taken and attention paid to the polarity and orientation of the diodes and capacitors. Wire links should be inserted first, note that some of these are mounted under the integrated circuit sockets, followed by the sockets themselves, resistors, capacitors, transistor and diodes. The ICs should be inserted last after the off-board components have been



connected. Also ensure that the flying leads have all been soldered into place and that the



OK' LED 2

SW1

LED 1 (WET)

LED₃

(DRY)

should be as small as possible.

RV2 AND PROBE

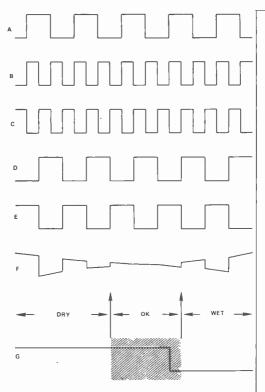


Fig. 1. Waveforms associated with the ETI Soil Moisture indicator, resulting in an LED display of whether the soil is wet, OK or dry.

HOW IT WORKS

The circuit consists of an AC energised bridge whose two active arms are formed by R11 plus RV2 and the soil resistance between the probes. Its operation may be best understood by reference to the circuit diagram and Fig.1. ICla and IClb are configured as an astable oscillator whose squarewave output (Fig. 1b) clocks IC2a. This signal, inverted by IC1c (Fig.1c), clocks IC2b.

The antiphase Q and Q outputs of IC2b are buffered by IC4a and IC4b whose outpits (Fig. 1d and 1e) drive the resistance bridge formed by R11 plus RV2 and the soil resistance between the probes. R11 protects the amplifier outputs against inad-

vertent short circuits.

'The output of IC2a (Fig. 1a) is a squarewave of the same frequency, phase shifted by 90 degrees. This means that the edges of the waveform are coincident with the centre of the squarewave from IC2b (Fig 1d and 1e) and facilitates phase detection by IC3a and IC3b. When the soil resistance measured between the probes is equal to the resistance of R11 plus RV2, the signals from IC4a and IC4b will cancel out. However, when an imbalance occurs, there will be an error signal whose phase will depend on whether the soil has a greater or lesser resistance than the other arm of the bridge. The amplitude of the error signal will also diminish as the bridge approaches balance (Fig. 1f).

This signal is coupled via C5, R10 to amplifier IC4c and squared up to provide CMOS input levels by schmitt trigger IC4d, where it is input to IC3a and IC3b and clocked in by the signal from IC2a. The outputs of IC3a and IC3b will follow the phase of the input; reflecting the state of imbalance of the bridge, and either LED 1 or LED 3 will be lit (Fig. 1g).

The amplified signal from IC4c is also fed

via C3, D1 and D2 to C2 which will acquire a charge proportional to the level of the input. This drives Q1 which controls the direct, clear, and set inputs of IC3a and IC3b respectively. When the input signal is insufficient to turn on Q1, these inputs are driven to their active high state by R3.

This causes both LED 1 and LED 3 to extinguish and the condition (shown shaded in Fig. 1g) is detected by nand gate ICld whose output goes low causing LED 2 to light. The sensitivity of the circuit to this condition is preset by adjustment of RV1 which controls the gain of IC4c. The required soil resistance is set by RV2. The circuit is powered from a 9V battery decoupled by C6. A mid voltage point is provided by R12 and R13 decoupled by C4.

PARTS LIST

RESISTORS

POTENTIOMETERS

RV1 470k preset RV2 250k lin

CAPACITORS

C1 1n C2 4u7 C3 10u C4 22u C5 220u

SEMICONDUCTORS

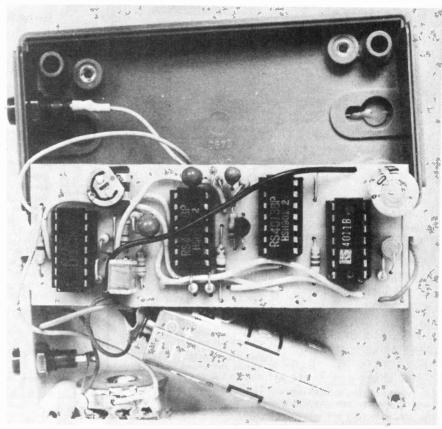
IC1 4011B IC2, 3 4013B IC4 LM324 Q1 BC10B D1, 2 IN4148 LED 1, 2, 3 0.125"

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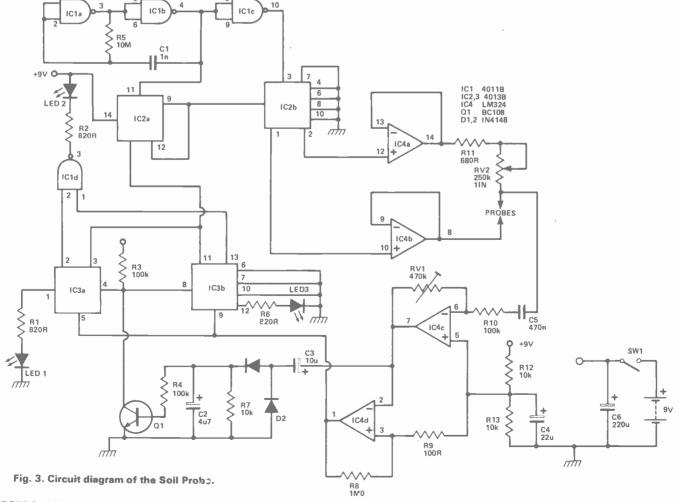
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An internal view of the Soil Moisture Indicator, showing the position of the four ICs.



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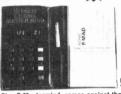
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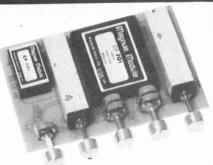
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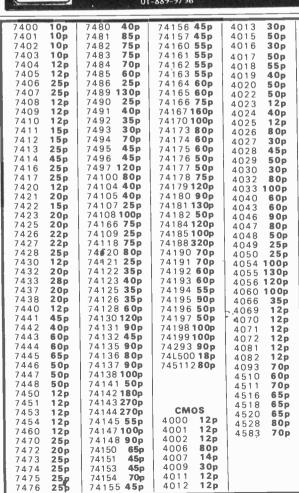


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CA3065 200p	LM555 25p	SN76013N 150p	TCA4500A 380p
CA3076 250p	LM565 130p	SN76013ND 130p	-TDA1004 300p
CA3080 75p	LM709C 40p	SN76023N 150p	TDA1008 300p
CA3084 250p	LM710T05 60p	SN76023ND 150p	TDA1022 575p
CA3085 85p	LM710DIL 65p	SN76033N 180p	TDA1024 150p
CA3086 60p	LM723T05 40p	SN76131N 125p	TDA1034 250p
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CA3089 160p	LM733 120p	SN76228N 180p	TDA2020 320p
CA3090AQ 360p	LM739 150p	SN7666ON 75p	TL081 50 p
CA3123E 130p	LM741 20 p	TAA300 150p	TL082 100p
CA3130 100p	LM747 75 p	TAA350 270p	TL083 130p
CA3140 60p	LM 748 40p	TAA550 35p	TL084 130p
CA3161E 150p	LM1303N 100p	TAA570 250p	UAA170 220p
CA3162E 400p	LM1458 100p	TAA661B 150p	XR320 250 p
CA3189E 270p	LM3080 75p	TAA700 350p	XR2003 150p
FX209 800p	LM3900 55p	TAA790 350p	XR2206 450p
LD130 460p	LM3909N 65p	TAD100 150p	XR2207 450p
LF356 80p	MC1310P 140p	TAD110 130p	XR2208 600p
LF357 80p	MC1312P 150p	TTD120A 60p	XR2216 675p
LM211H 250 p	MC1314P 190 p	TBA120S 70p	XR2264 450p XR2265 450p
LM300T05 170p	MC1315P 230p	TBA120T 90p	
LM301AN 30p	MK50398 650 p	TBA480Q 200p	XR2567 250p XR4136 150p
LM301T05 45p	MM5314 380p	TBA520Q 200p	
LM304 200p	MM5316 480p	TBA530Q 200p	XR4151 350p XR4202 150p
LM307N 65p	NE 529K 150p	TBA540 200p	XR4202 150p
LM308T05 100p	NE555 25p	TBA550Q 250p	XR4212 150p XR4739 150p
LM308DIL 100p	NE556 90p	TBA560C 250p	ZN414 100p
LM309K 140p	NE562B 400p	TBA641A12 250p TBA700 180p	ZN1034E 200p
LM310T05 150p	NE566 150p	TBA700 180p	95H90 800p
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LM339 60p	SAS570 160p	TBA810 100p	l

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EECTONICS today international

What to look for in the August Issue: On sale July 6th

STRING THING

To call this project an electronic piano would be an injustice. To call it a string ensemble likewise fails to explain all the mysteries and beauties awaiting the builder once this beast is activated. Yes it can be a piano. Yes it can play string sounds.

The designer (Tim Orr who also can be blamed or praised for the Transcendent 2000) wanted to call it a "Digital Multi-

Voice String Synthesising Keyboard Instrument". But we wouldn't let him. We couldn't think of a better title ourselves, but we still wouldn't let him. It's the way we are.

Being fitted with a CCD choraliser allows our String Thing to sound like several of 'em at once. Why not tune in and be amazed next month?



BENCH AMPLIFIER

One for the workshop or table top. How many times have you been half-way through a project and needed to test something, somehow, somewhen. And that of course is exactly when it occurs to you that there is nothing around suitable.

A bench amp is worth its weight in soldering ten times over, and if you DON'T build this you will regret it.

MICROSENSE

MPUs are definitely for you. Oh yes they are, don't give me that old line about them being all covered in mystery and incomprehension. MPUs are nice friendly little chips, and next month we've got the definitive article to prove it. Based on a book by John Miller Kirkpatrick it takes you through the subject from scratch in a thorough but light-hearted manner.

LED AUDIO DISPLAY

A really lovely little design to amaze, astound and hypnotise the entire universe. This project takes the input from your hi-fi or TV or budgie and turns it into a dazzling and bemusing shifting pattern of light upon a LED matrix.

Build it any size you like it'll add a bit of visual spice to the hi-fi rack — or simply keep mother-in-law quiet while you nip off down the local.

ZENER DIODES (400mW)		OPTO/	LINEARS	1	7443	18p	74165	36p	4048	50p	BC147	8 p	BF115	35p	TIP33	60 p
2.7V to 33V	8p	DISPLAY	710CN	30p	7444	60p	74166	75p	4049	25p	BC149	8 p	BF167	25p	TIP34A	40p
	2	2N5777 50p	741-8	22 p	7445	64p	74173	80p	4050	25 p	BC157	8p	BF173	20p	TIP35A TIP36A	230 ₁
		OCP71 70p	747C-14	45p	7446	50p	74174	60p	4066	35p	BC158 BC159	8p	8F17B BF179	27p 25p	TIP41A	60
(ERO BOAROS (0.1" Copper)	51p	ORP12 70p	748C-8	30p	7447 7448	50p	74175	36p	4069 4070	12p	BC159	8p	BF180	8p	TIP42A	60
?.5" × 5" 1.75" × 5"	60p	0L704 100p 0L707 100p	CA3011 CA3018	80p	7450	10p	74176 74177	50p	4070	12p	BC170	8p	BF181	16 p	T1P2955	65
1.13 × 3	oop.	.125" 8 .2"	CA3028A	85p	7451	12p	74180	20p	4072	12p	BC171	8p	BF182	20p	T1P3055	55
SECIETORS (I/H)		LEDs		120p	7453	12p	74181	66p	4073	16p	BC172	8p	BF183	20 p	ZTX108	12
RESISTORS (¼ watt) O ohms to 1 Mohm	1p	Red 9p	CA3046	75p	7454	10p	74182	25p	4081	14p	8C173	6р	BF184	20 p	ZTX109	12
O onais to 1 month		Green 13p		110p	7460	14p	74190	36p	4082	14p	BC182	8 p	BF185	20p	ZTX300 ZTX500	14 16
ancorro (Harianatal)		Yellow 13p	CA3080	70p	7470 7472	16p 20p	74191	70p	4086	60p	BC183 BC184	8p 9p	BF194 BF196	8p	2N706	10
PRESETS (Morizontal) 00 ohm to 1 Mohm	5p	.125" Clip 3p	CA3140E LM301AN	51p	7473	12p	74192	25 p	4510 4511	60p 70p	BC186	19p	BF197	8 p	2N1131	15
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			LM380N	61p	7475	25p	74195	50p	4518	65p	8C207	8 p	BF200	33p	2 N 1 3 0 2	38
POTENTIDMETERS (carbon)	220			120p	7476	25p	74196	50p	4520	65p	BC212	10p	BF224	18p	2N1304	50
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Koum to I would to A mitte smite!	Job	DIDDES	NE556	60p	7485	60p	74198	100p	TRANCIC	rone	BC214	10p	BF258	28p	2N1306 2N1308	38 50
		8Y127 10p 0A47 8p	T8A641-B11	200n	7486 7490	10p 25p	74199	90p	TRANSIS	17p	8C237 8C238	15p 15p	8F259 8FR39	15p 18p	2N1613	18
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		0A202 9p	IDADIO	Поор	7493	15p	4001	12p	128/176		BC328	16p	BFRBO	22p	2N2217	24
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01, .015, .022, .033, .047, .068, .1 uF	5p	1N916 5p	7400	10p	7495	25p	4006	68p	AC141	24p	8C547	11p	BFX30	32p	2N2369	10
.15, .22, .33 uF	6p 12p	1N4001 4p	7401	10p	7496	25p	4007 4008	14p	AC142 AC151	18p 22p	BC548	11p	BFX85	20p	2N2484 2N2905	18 22
.4768 uf 1 uf	15p	1 N 4 0 0 2 4 p 1 N 4 0 0 3 5 p	7402	10p	7497 74100	120p 40p	4008	25p	AC153	22p	BC549 BC557	11p 11p	8FX86 BFX87	27p 20p	2N2906	10
2.2 uF	20p	1N4004 6p	7404	120	74105	40p	4010	35p	AC176	16 p	8CY30	60p	BFY50	15p	2N2907	12
		1N4005 7p	7405	12p	74107	10p	4011	12p	AC187	23p	8CY34	66p	8FY51	15p	2N2926	10
		1N4006 8p	7406	12p	74109	30p	4012	12p	AC188	20 p	BCY59	16p	BFY53	17p	2N3053	15
ELECTROLYTIC CAP 25V		1N4007 9p	7407	24p	74110	46p	4013	30p	A0149	65 p	8CY70	14p	BSX19	20 p	2N3054	50
1 uF to 47 uF 68 uF, 100 uF	6p 7p	1N5400 13p	740B	12p	74118	75p	4014	60p	A0161	35p	8CY71	14p	-BSX20	18p	2 N 3 0 5 5	50
150 uF	7р 8р	1N5401 14p	7409 7410	12p	74121	20p	4015 4016	50p	A0162 AF114	35p 23p	B0115	30p	8 U 2 0 5 B U 2 0 8	130p 150p	2N3702 2N3703	8
220 uF	9p	1N5402 15p 1N5404 20p	7411	12p	74122 74123	20p 40p	4017	50p	AF118	30p	80121 80123	70p 60p	0025	76p	2N3704	8
330 uF	11p	180404 20p	7412	15p	74125	35p	4018	55p	AF125	22p	80124	77 p	0028	70p	2N3706	8
\$70 uF	14p		7413	25p	74126	35 p	4019	40p	AF126	22p	80131	35p	0035	70p	2N3707	8
000-uF	22p		7414	45p	74132	45p	4020	50p	AF127	22p	B0132	35 p	0071	16p	2N3710	8
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		VOLTAGE	7417	24 p	74142	180p	4022	50p	AF186 AF239	54 p 40 p	B0136	30p	DC84	42p	2N3772	100
		REGULATORS 320H-05 40p	7420 7421	12p 20p	74145 74150	30p	4023 4024	12 p 45 p	ASY53	33p	B0137 80138	30 p	TIP29 TIP30	40p 35p	2N3773 2N3866	54
		320H-24 40p	7422	15p	74151	45p	4025	12 p	ASY54	33p	80139	30p	TIP31	45p	2N3904	8
OIL SOCKETS BRIDGE		7805 60p	7427	10p	74153	45p	4027	30 p	ASY55	33p	80140	36 p	TIP32	45p	2N4061	12
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4 pin 12p 1A/50 V	22p	7815 60p	7430	12p	74155	45p	4029	50p	8C108	8p						
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2A/400V	48p	7924 80p	7442	40p	74164	60p	4047	80p	BC143	12p	62 NA	YLOR	ROAD,	, LOND	ON, N2	O OF
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IBM 3740 COMPATIBLE DISC SYSTEM

The twin drives and controller are housed in a metal saddle maintaining an integrated configuration, one of the major features of the PET. Connection is via the PET memory expansion port and the system comes complete with a PROM which boots the disc resident P-DOS into RAM. Control of the disc system via PET BASIC USR instruction with simple commands from either the keyboard or under program control.

COMPLETE SYSTEM £1,900

Other accessories: Saddle conversion package £180, S100 Buff expansion £96, Voice recognition £176, Voice response £182, Robot control £236, Quum Printer £1,400.

The following disc system commands are available: LOAD, SAVE, CREATE, DELETE and CATALOGUE.

The file management system provides for up to 8 files to be opened concurrently. Files can be opened in READ, WRITE, UPDATE and APPEND mode. The user

APPEND mode. The user may write his own disc system modules to expand the facilities of the disc resident system.

£950.00 excluding VAT







LIFE OUT THERE?

Is there anybody there? Does anyone care? Yes to both. Read on . . .

ABOUT 20 YEARS AGO scientists, realised that their equipment might be able to detect suitably powerful radio emissions from intelligent beings on planets in other solar systems which may be many light years away from us. Attempts to detect Extra-Terrestrial Intelligence (appropriately abbreviated to ETI!) have already been made in the USA, Canada and the USSR without success, but much more work with larger aerials is required to provide workers in this field with a reasonable chance of success.

Apart from the Search for Extra-Terrestrial Intelligence (SETI), drawings and radio signals have been sent into space outside the solar system in the hope that they will eventually be detected and understood by intelligent beings many light years distant. Unfortunately the chances of two way communications with such beings are very remote, since the nearest star is a few light years away and most planetary systems are at much greater distances. Thus anyone sending a message from the earth to anywhere but one of the very nearest of the stars would be dead by the time any reply could be returned to the earth.

Attempts have also been made to detect signs of life within the solar system. In particular, the Viking spacecraft which landed on Mars conducted prolonged tests

to try to detect life or the chemicals associated with life. Although no organic molecules that could be the past or present constituents of living things were found and the results were generally rather discouraging, they were certainly not conclusively negative as regards the possibility of life on Mars.

Communication Techniques

It seems likely that there are three possible ways in which we may be able to communicate with intelligent beings from outside the solar system. The first way involves a direct meeting of space vehicles or a landing by them on the earth. Unless the other beings have a longevity which far exceeds that of man, the journey time would make this method quite impossible. Many people do not fully appreciate how much vaster are the distances involved in interstellar space than those within the solar system. Light takes about 8 minutes to reach us from the sun, but about 180 000 years to cross our galaxy and some thousands of millions of years to reach us from the farthest known objects.

As we require something which will convey information quickly, the obvious thing to use is electro-magnetic

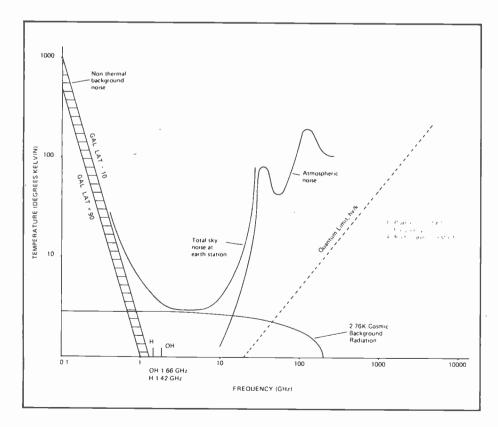


Fig. 1. Some of the most important factors which determine the choice of listening frequency. As signals from other stars would be very weak, it is important to choose a frequency where the natural background noise is relatively small. Most SETI work has been done in the relatively low total noise region of 0.5 to 10 GHz, christened the 'Water Hole', since it contains frequencies strongly associated with water. The favourite frequency is 1.42 GHz, emitted when the electron in a hydrogen atom flips over, reversing its direction of spin.

The noise contributions shown are — the 2.76 K cosmic background radiation (remnants of the big bang), atmospheric noise (as water and oxygen absorb and reradiate energy), quantum noise associated with the arrival of each photon in the atmosphere and synchrotron radiation emitted by particles spiralling round galactic magnetic fields (the level varies with galactic latitude. The extreme lines shown are for galactic latitudes of 10° and 90°).

signals which travel at the speed. ht. We can only send signals by this technique and no material objects, but generally it is far more sensible to send information on how to construct an object rather than to send the object itself over such vast distances. Should one use light, infra-red, radio waves or some other form of electromagnetic radiation? Radio-waves are to be preferred, since the energy required per transmitted photon is relatively low.

The third possible communicating technique involves the acceleration of sub-atomic particles to velocities very near to the speed of light, but as far as is known this technique has not yet been tried. If particles which can travel faster than light (known as 'tachyons') are ever discovered, one can only wonder whether they could be used in an extra-terrestrial communications system if they can be produced relatively easily; however, at the moment such a suggestion is nothing more than pure speculation.

It has been suggested that we should avoid transmitting any signals into space which would inform possibly hostile intelligent beings of our location. It is generally felt, however, that we can take comfort from the fact that any intelligent beings would be more interested in sharing information with us and co-operating with us as far as possible rather than in attacking us as in science fiction stories. In any event, it seems likely that it would take them so long to arrive here that our civilization would be in a very different state by the time they could reach us.

Basic Problems

Let us first consider the basic problems associated with receiving radio signals from outside the solar system, since any of our attempts to send messages are not likely to bring any result for an enormously long time. Any radio signals reaching the earth from outside the solar system are likely to be extremely weak owing to huge distances involved and it therefore follows that SETI projects require the use of the largest radio telescopes in the world.

One is left with decisions to make on the direction in which one should point the telescope, the frequency or frequencies which one should attempt to receive, the bandwidth one should use and perhaps even the time at which one should attempt to receive any transmissions. In the work on SETI which has been performed up to the present time, the telescopes have usually been pointed towards some star in our galaxy which is not excessively distant and which astronomers feel may possibly have a satellite system on which life could have evolved in some form or other.

In general astronomers have concentrated their searches in the regions of stars of the same or similar spectral classes as the sun. It has been felt that if a star has a luminosity much greater than that of the sun, then the lifetime of any planetary system associated with that star is probably too short to have enabled life to have developed to the point where intelligent civilizations have evolved. Stars of luminosity much smaller than that of the sun seem to have rather violent coronal activity which would probably result in any associated planetary system being rather inhospitable to most imaginable forms of life. Other stars have departed from the main sequence as a result of a super-nova or nova explosion and SETI workers have tended to disregard these

because it seems doubtful whether any living species could survive the catastrophe event of such an explosion in the star.

Signal Types

What types of signal should we expect to receive from other planetary systems and how could we recognise such signals as originating from intelligent life? The SETI workers are basically searching for coherent signals, possibly modulated. For example, our own radio transmissions have a coherent carrier wave, although the modulation present inevitably involves a finite bandwidth. The presence of this type of signal would almost certainly indicate it is not of natural origin and hence would imply the existence of intelligent life elsewhere in the universe.

There are three basic types of signal from other planetary systems which we may be able to detect. The first type of signal is leakage of a signal into space in just the same way that our own radio and television signals leak away to a greater or lesser extent through our ionosphere. Indeed, a spherical wave of radio signals of a fairly wide range of frequencies has been travelling away from the earth over a period of rather over 50 years. In the case of more highly developed societies, it seems probable that they have been transmitting such signals for a far longer period (although one hopes they have not been stupid enough to destroy themselves by nuclear war).

A second type of signal we may possibly be able to receive is some form of inter-stellar or even inter-galactic communications between highly developed communities. Such reception would be by chance and it must be assumed that highly developed communities would employ very high gain antennae which are unlikely to be pointing towards our solar system. Thus the chances of intercepting such messages cannot be regarded as being very high.

The third type of signal we may hope to receive is an intentional one directed at our solar system by a society in a distant stellar system in order to notify us of their presence. It is also possible that such a society may send signals out isotropically (that is, all directions at equal intensities), but unless they have transmitters of extremely high power, such signals would be so weak at the earth that it is doubtful if we could detect them.

It is difficult to make an estimate of the optimum bandwidth one should select for SETI work. Narrow bandwidth receivers (possibly with a bandwidth of a few Hz) enable very weak signals to be detected, since the narrower the bandwidth of the channel used, the less the external noise which can penetrate into that channel. (Someone once said: "The wider you open the window, the more the amount of dirt that flies in," and this certainly applies to radio bandwidths). Unfortunately if one has a very narrow bandwidth channel, it takes a very long time to examine an appreciable range of frequencies. Modern plans are to use both narrow and wide band search techniques together with spectrum analysers for the simultaneous examination of numerous frequencies by computer techniques.

The Drake Equation

Before spending millions of dollars on SETI programmes, one would like to have some approximate

estimate of the number of civilizations which are likely to possess the technology to be able to communicate with us. Such an estimate can be obtained by the use of the Drake equation. Professor Frank Drake is one of the leading SETI workers and is now Director of the National Astronomy and lonosphere Centre of Cornell University. His equation reads:

$N = R^* f_p n_e f_l f_i f_c L$

where

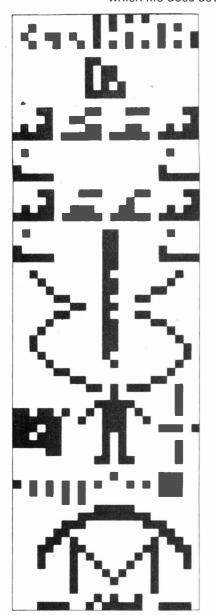
- is the number of existing civilizations possessing the interest and capability for inter-stellar communications
- R* is the mean rate of star formation averaged over the lifetime of a galaxy
- f_p is the fraction of stars with planetary systems
- n_e is the mean number of planets in each system with an environment favourable for the origin of life
- f, is the fraction of suitable planets on which life does develop

- fi is the fraction of life bearing planets on which intelligence together with manipulative abilities appears
- f_c is the fraction of the planets evolving advanced technical civilization
- L is the lifetime of the technical civilization (perhaps very difficult to estimate!)

The estimate obtained from the use of this equation will obviously vary widely according to the estimated values employed. However, most estimates now place the value of N around one million, these being distributed amongst approximately 500 million stars in our galaxy.

SETI History

Perhaps the first important paper on SETI work appears in *Nature* in 1959 under the title "Searching for Interstellar Communications" by Philip Morrison and Guiseppe Cocconi. It is interesting to note that they suggested the use of the 1.420 MHz hydrogen



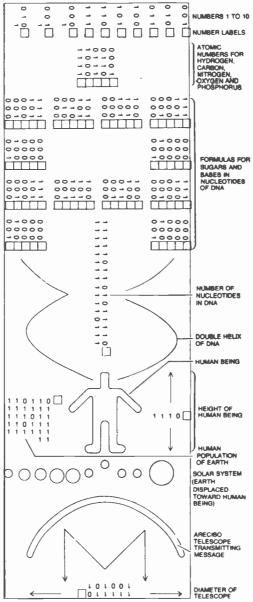


Fig. 2. On November 16th, 1974, the Arecibo telescope was used to transmit a message at 2380 MHz towards the Great Cluster in Hercules, Messier 13, some 25,000 light years away.

The message, 1679 bits long, can be decoded by breaking it into 73 consecutive groups of 23 characters and arranging these groups in sequence under one another as shown. The first piece of information consists of the first ten digits in binary form — the numbering system to be used. It continues with the atomic numbers of five common elements found in living things. Information on sugars and DNA follows, with a sketch of a human being and the solar system, ending with information about the Arecibo telescope.

Encoding information in various types of message poses some interesting problems in order that decoding can be carried out as easily as possible by intelligent remote beings.

frequency, since it is a unique standard frequency which must be known to every observer in the universe.

Eight separate major efforts have been made by US, Canadian and Russian radio astronomers since 1960 to detect extra-terrestrial signals from intelligent beings. Although each search has concentrated on one or more specific frequencies in the range from 600 MHz to 22.2 GHz, the receivers used were those designed mainly for normal radio astronomical work which involves the detection of incoherent naturally produced radiation rather than the coherent radiation the SETI workers were seeking.

Although no confirmed sources of signals from intelligent beings outside the solar system have yet been detected, it has been estimated that the number of stars which have been examined is about 0.1% of the number which would have to be investigated if there is to be a reasonable statistical chance of detecting extraterrestrial intelligent signals.

Project Ozma

The first SETI work was led by Frank Drake using the 1420 MHz hydrogen frequency. It was named "Project Ozma" after the ruler of Oz — a far away place populated by exotic beings. Drake employed a bandwidth of 100 Hz and aimed his receiver at the two stars Tau Ceti and Epsilon Eridani which are both some 11 light years away from the earth. The observing time was some 150 hours using a 26 m (85 feet) diameter steerable antenna in 1960.

Project Ozma II is a much more extensive one which has also been carried out at the National Radio Astronomy Observatory, Green Bank, West Virginia. In this work some of the largest and most sophisticated radio telescopes in the world have been used; they include the 92 m (300 feet) diameter partially steerable antenna completed in 1962 at a cost of about 1 million dollars (500 000 pounds) and the 43 m (140 feet) diameter

equatorially mounted, fully steerable antenna which was completed in 1965 at a cost of some 14 million dollars (£7 million).

Project Ozma II was commenced in late 1972 under the leadership of Benjamin M. Zuckerman of the University of Maryland and Patrick Palmer, of the University of Chicago, the intention being to run the project for about two years. However, the Observatory made more time available and the project continued until December 1976 with an examination of about 700 stars at distances of up to some 65 light years. The prime targets were main sequence stars of the F5 to K5 class. The observations were carried out at 1420 MHz, each of 384 separate receivers being tuned to a slightly different frequency near to the 1420 MHz hydrogen line. A total bandwidth of 3 kHz was used.

At the end of the Project Ozma II work, about 12 stars showed some unexplained phenomena which were probably due to terrestrial radio interference, but which could have been due to faint signals from intelligent beings. These stars will doubtless be examined very carefully at some later date.

Arecibo

Some SETI work has been carried out using the largest telescope in the world at the Arecibo Observatory in Puerto Rico which has a diameter of 305 m (500 feet) in the air. The reflector panels consist of 38,778 individual panels each a little over 1 m by 2 m in size; each pane, must be positioned with an accuracy of better than 1 mm.

In 1967 a British post-graduate student noticed a mysterious regular pulsing signal from space and there was much speculation as to whether this was a signal from intelligent life beaming a message to earth. The Arecibo antenna was used to show that this signal was coming from the first pulsar to be discovered and that it was in the Crab Nebula.



The Goldstone 26 m Deep Space Network Antenna may be used in an all sky search. (Photo by courtesy of Jet Propulsion Laboratory)

Two of the best known SETI workers, Prof. Frank Drake and Prof. Carl Sagan, have used the Arecibo antenna to examine the radiation from whole galaxies for signs of signals from intelligent life. Although the use of this technique has enabled them to examine many millions of suitable types of stars simultaneously, it would require a signal of very great intensity to enable frequencies of 1420 MHz, 1654 MHz and 2380 MHz, but the time allocated to this work is relatively small.

Canadian Work

Dr. Bridle and Dr. Feldman commenced work at Canada's nationally owned Algonquin Radio Observatory in Algonquin Park, Ontario in 1974. They are using a 46 m (150 feet) diameter telescope to examine many of the nearest sun-like stars, but the frequency employed is 22.2 GHz — the emission frequency of the water molecule — which is much higher than that used by other workers.

Project Cyclops

One of the most ambitious SETI projects yet proposed is known as Project Cyclops. This is intended to be suitable for not merely detecting high power signals (such as those from our own Arecibo antenna), but also to allow eavesdropping on much lower intensity signals which other civilizations use for their own communications (like our radio and television transmitters). In order to be able to receive such signals from stellar systems at distances of a few hundred light years from the earth, enormous antenna systems are required.

It seems unlikely that it would be a practical possibility to construct a single reflecting dish of adequate size and therefore it has been suggested that the Cyclops project could employ an enormous array of radio telescopes, each of which may be about 100 m in diameter. For example, as many as 1500 such 100 m dishes could be spread out in lines over an area of perhaps 65 km² and connected together electrically to

provide the same performance as a single dish of enormous dimensions.

Project Cyclops was initiated as a study by the NASA Ames Research Centre and Stanford University in 1971 under the leadership of Dr. John Billingham and Dr. Bernard Oliver. There have been vast improvements since then in solid state memories, microprocessors, wideband maser low-noise amplifiers, etc.

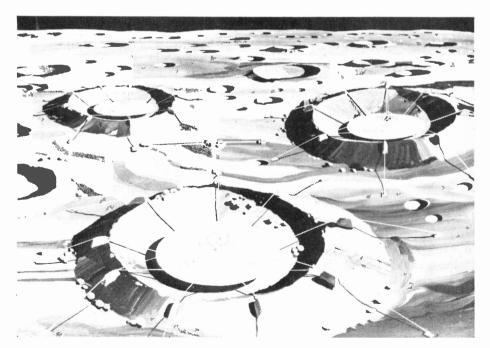
Conclusion

The Search for Extra-Terrestrial Intelligence has not yet been successful, but this is not particularly surprising in view of the small number of star systems which have been examined with high sensitivity equipment. Some people (including many of those who control scientific finance) may feel that the SETI project is rather frivolous and perhaps even a silly one. However, there are many scientists very strongly committed to work in this field — a point which can be demonstrated by the fact that a new journal, *Cosmic Search* devoted entirely to SETI work will be published from January 1979 under the editorship of Dr. Robert S. Dixon who is well-known for his SETI work at the Ohio State University Radio Observatory.

Dr. Frank Drake at times feels somewhat cynical about the cuts in the SETI budgets. Indeed, he has commented that the search for extra-terrestrial intelligence begins with the search for intelligence here on earth! He feels that at the present time there is a very well qualified group of people who are keen to carry out an extensive SETI project and, if no funds are forthcoming for a year or more, it is likely that many of these people will move to other work. If you were paying taxes in a country considering becoming involved in an extensive SETI project, how would you feel about paying an extra amount (far less in total than that to place a man on the moon) in order that the project could proceed? SETI work will doubtless continue, but more funds are required if it is to proceed at a rate which is likely to bring success within the lifetime of most people who are living today.

An artists impression of a complex Cyclops array on the far side of the moon containing 216 large (200 m diam.) reflecting radio telscopes with a control building in the middle of the array. The lunar base is in the middle distance towards the left-hand side and is quite small.

(Photo by courtesy of NASA Ames Research Centre).



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TUNER~AMPLIFIER

PART TWO: This month we conclude the System 8000 project with the setting up procedure and a description of the digital frequency readout.

THE SETTING UP and alignment must be approached in a systematic fashion.

Procedure

- a) Power Supply
- b) Power Amp L & R
- c) Auxilliary
- d) Tone Controls
- e) Filter Controls
- f) Tape
- g) Magnetic pre-amplifier
- h) FM sections
- I) AM
- J) Frequency read out module

Before commencing alignment it is necessary to check that:

- All wiring has been checked and components are correctly positioned and orientated
- ii) That there are no solder bridges
- iii) A good multimeter is also required

Power Supply

Remove all fuses except for the mains fuse. Switch on, you should

hear the relay click over. Measure from earth to positive and negative on the smoothing capacitors. The voltage should read approximately plus or minus 50V. Check that regulator reads about 30V. Switch off.

Power Amp

Check each power amp in turn, ensure that speakers are switched out. Using a meter, do a resistance check from the case of each power transistor to chassis to ensure that there is no short. Find two high wattage resistors (56R-300R will do) and place in fuse holders of amp being checked.

Switch on volume control (minimum). If there appears to be no problems feel cases of power transistors — should be cool. Switch on speaker. Power transistors may be slightly warm. Now 'Buzz' input pins of the amplifier with your finger. If okay switch off, remove the resistor fuses, insert two amp fuses. Switch on, if everything is okay one can now set RV1.

If you have access to a low distortion audio generator put this on the input and a distortion meter across the speaker sockets using a dummy load. Feed in 100mV sine wave and set for minimum distortion. Without this test equipment set RV1 to mid travel. Repeat for other channel.

Tone and Filters

Insert either an audio generator, or any music source such as a tape-recorder, into the Aux. socket. Select Aux. on switchbank, slowly increase volume, and listen to sound, check that the tone controls are working. To check the high and low filters turn the bass control on full and this will emphasise the rumble filter, likewise the treble control will emphasis the scratch filter.

Tape

If the above is working, check that pressing tape 1 and tape 2 disconnects the Aux. Transfer the tape recorder/audio generator to take 1 and 2 in turn and ensure that



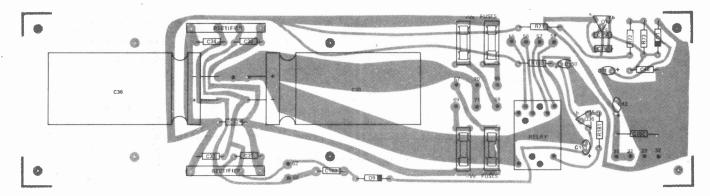


Fig. 1. Component overlay for the power supply board.

pressing the respective switch brings them into circuit. The pre-set resistors are adjusted to match the levels of your own tape recorders otherwise they can be turned full on.

Magnetic

Using a record player with a magnetic cartridge check that everything sounds okay. Excessive hum indicates an earthing fault.

FM

Before aligning this section it may be an advantage to set the frequency counter straight away. However, this is not essential. The tuner head is pre-aligned and will not need adjustment. Tune through the band with an aerial connected — ensure that mute and AFC are off. You should hear a continuous hiss, with stations heard between 88 MHz and 95 MHz. If this is so, tune to an area above 95 MHz without stations and adjust using a non-inductive tool L4 until centre zero needle is centred. This should correspond with

maximum hiss level. L3 can only be adjusted ideally if an FM signal generator is used. Generate 100 MHz, attach a distortion meter to pin 6 of the CA3189E, there is a test pin for this, tune for maximum signal strength and adjust L3 for minimum distortion. Re-adjust L4 for centre zero. Adjust L1 for maximum signal level. RV11 is the muting adjustment, and can be set all the way from no mute to absolute quiet between stations - however, do not overset, as the mute may not lift quickly enough when tuning a station.

Move next to the stereo decoder, KB 4437 — either:—tune to a stereo broadcast, set RV6 to the middle of the range that brings the stereo light on, set VC5 and RV7 for mid-way; or:—using a stereo generator, adjust VC5 and RV6 for maximum, set separation at 1 kHz. Observing the 19 kHz component of the multiple signal on a oscilloscope, set RV7 for minimum 19 kHz. This completes the

Amplitude Modulation

The frequency counter can help considerably, and an AM generator is an asset.

MW Tune to minimum volts on varicap line, feed in a 470 kHz signal, peak until there is no improvement, Tune L9 for a 550 kHz station. Move to maximum varicap volts, set CV1 for a 1620 kHz signal. Tune up and down the band checking that 550-1620 kHz is covered without any shifting in noise level. Tune to 600 kHz. Peak L5 and L3 for maximum. Tune to 1400 kHz. Peak CV2 and CV4 for maximum. Repeat until there can be no improvement. RV8 is set to give a satisfactory signal level reading on the meter.

LW Switch to LW. Set CV3 so that minimum varicap volts 175KHz. Tune to 200 kHz (Radio 4) peak L6 and L8 for maximum. If no generator

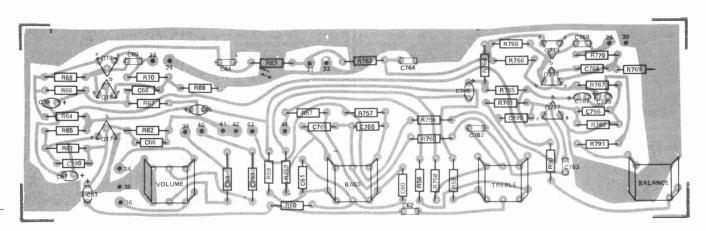


Fig. 2. Component overlay for the tone control board.

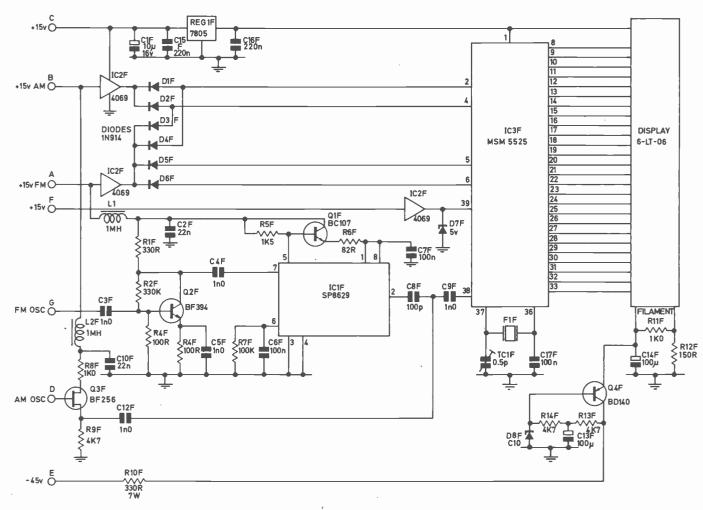


Fig. 3. Circuit diagram of the digital frequency meter.

HOW IT WORKS

A digital frequency readout is both cost effective and an accurate method of displaying the frequency of a radio station. GEM has been developed to interface directly with the tuner sections of the SYSTEM 8000, and most existing AM/FM receivers.

The principle of operation is simple, and is a progression from the many digital clock ICs. Basically, the oscillator of the radio being 'read' is fed (via buffer stages) into the 5525, and converted to digital pulses. These are counted by the IC, for a period determined by the external crystal, and the count is fed to the display.

Allowance is made for the IF offset of the radio — $470\,\mathrm{kHz}$ and $10\,\mathrm{k7Hz}$. This offset is externally programmed by the diodes DID6.

In this application, the source for switching from AM to FM is obtained from the switch bank of the System 8000, and uses the positive power line. This is converted from

a 'Hi' to a 'Lo' signal by IC2, a HEX invertor. The beauty is that the buffer stages for the AM/FM oscillators are also switched off when not in use, and thus cannot cause interference.

Because the display would be running when the tuner is not being used. A section of the hex invertor takes an additional 15V input (F) and uses this to reset the counter and thus give a fixed reading. D7 ensures that this signal cannot accidentally exceed 5V. The unit must be earthed directly to the central earthing point of the system 8000, otherwise noise may be fed back into the system.

The unit may be used independently of course and requires ±12V at least, for operation. If using a supply of lower than ±20V, omit R10. Maximum supply is ±35V. Other IF offsets may also be programmed in. It uses a fluorescent display for a good readibility and gives AM/FM and MHz/kHz indication.

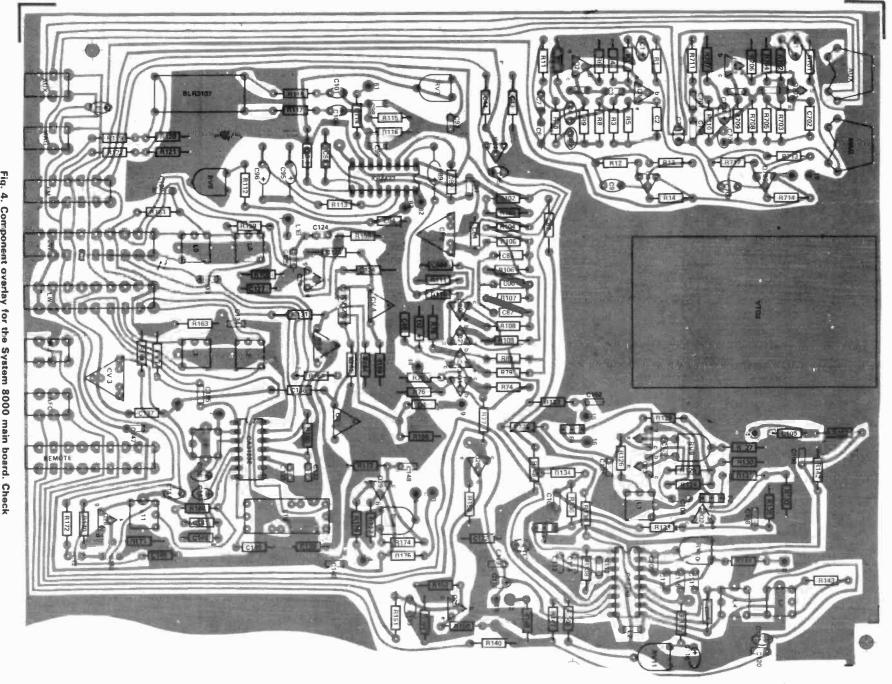
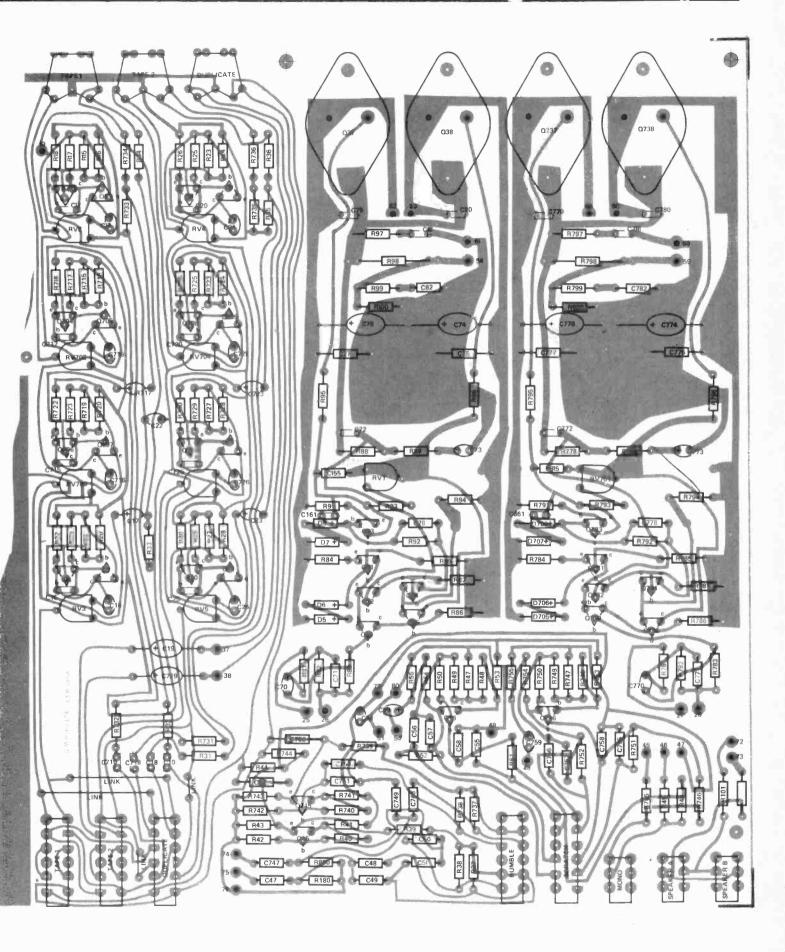


Fig. 4. Component overlay for the System 8000 main board. Check this board very barefully before you switch on, particularly capacitor and diode polarity and transistor connections.



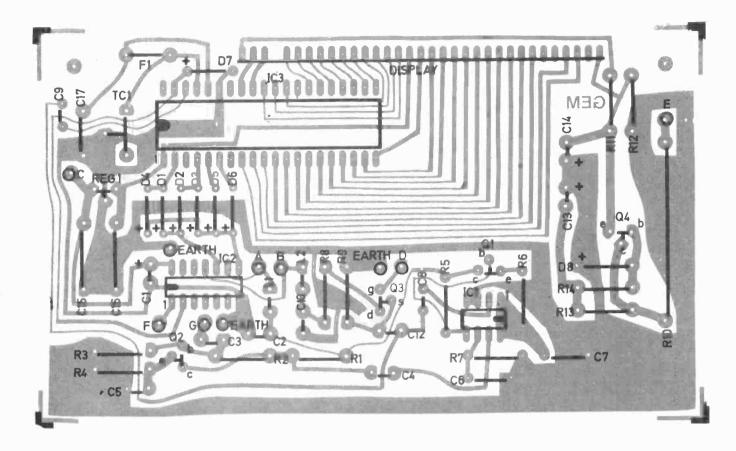
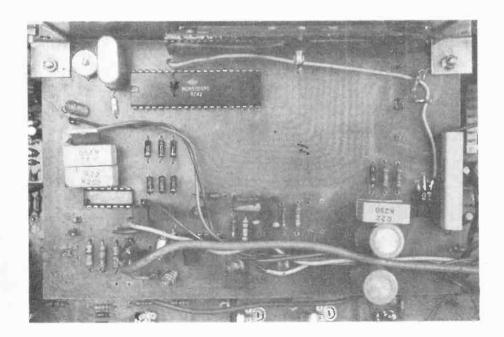


Fig. 5. Component overlay for the digital frequency meter board.

(Below) The digital frequency meter display and driver board.



is available, the digital frequency counter can be peaked. L11, L10, can be set for maximum output (be careful — small adjustment only).

Readout

The frequency counter should need no adjustment, however, if another frequency counter is available, the crystal input should be tuned to precisely 6553k6Hz with TC1.

NB: It has been found in practice that two laminated transformers give excellent regulation and a low hum field, also low voltage taps are available to power the centre zero and signal meter. The metal case will take both torroidal and conventional transformers.

PARTS LIST

```
RESISTORS (all 1/2W 5%)
R1, 10
               330R
R2
               330k
R3
                1 M
R4
               100R
R5
               1k5
R6
               82R
R7
                100k
R8, 11
R9, 13, 14
               4k7
R12
               150R
CAPACITORS
               10u 16V electrolytic
C1, 14
C2, 10
               22n polyester
C3, 4, 5, 9, 12
C6, 7
               1n polvester
               100n polvester
C8
               100p ceramic
C13
               100n 45V electrolytic
C14, 15
               220n nolvester
C17
               220 ceramic
SEMICONDUCTORS
               BC107
02
               BF394
Q3
               BF256
Q4
               BD140
IC1
               5525
IC2
               4069
IC3
               SP8629
D1-6
               1N914
D7
               5V 400mW zener
D8
               10V 400mW zener
Reg.
INDUCTORS
L1 2
               1mH
MISCELLANEOUS
TC1-0-50p, F1-6553k6 H7 X71, 6LT06
display, PCB
```

```
30/ to pin (28)
31/ to pin (31)
32/
33/ to pin (33)
34/ to pin (37)
35/ Earth
36/ to 38 pin
37/
    to pin (34)
38/ to pin (36)
39/
    to pin (45)
40/ to pin (46)
41/
    to pin (47)
42/ Earth pin 49 and 51
43/ pin 48
44/
     pin 50
45/
    pin 39
46/
    pin 40
47/
    pin 41
    pin 43
Earth pin 42
48/
49/
50/
    pin 44
51/
     Earth pin 42
52/
     to 56V winding of Transformer
53/
54/
    Connect
55/
56/
     to speaker switch L
57/ to speaker switch R
58/
59/
60/ pin 70
    pin 71
61/
     +45V fuse 66
62/
63/
     -45V fuse 67
64/ +45V fuse 68
    -45V fuse 69
65/
66/ to 62
67/ to 63
68/ to 64
69/ to 65
70/ to 60
71/ to 61
/2/ }
73/ }
      -to L and R of Head-Phones
74/ —L
75/ —R to FM switch
76/ Farth
77/ on FM switch, to mono switch
```

```
78/ +15V
79/ on mono switch, to stereo. LED anode
80/ Earth
81/ to stereo LED
82
82
83/ mono options, disconnected
```

All other earth connections to tabs of power board—including centre-tap of transformer.

CORRECTIONS FOR DIGITAL FREQUENCY DISPLAY pin 7—(FM tuner lead) to pin 100 pin (6) —to pin 101

Uni-Electric have sent us the following list of corrections to the parts list and circuit diagrams published last month.

C105 in 100n.

Circuit diagram shows a short from output of 7815 to earth. Omit indicated line.

Switch marked 'rumble' is tape switching. 'Mono' switch, left channel shown connected to earth, via a 470k resistor. This should be connected to Mono switch via a 1k resistor.

C67 and C150 are 10 uf capacitors.

C136 is 470p. C137 is 330p. 10n capacitor omitted from pin 7 to CFU050D. C147 is 10n. R171 is 10k.

R120 are R121 are 47k. Base of Q20 is shown shorted to earth — should be a 47p capacitor here.

R10 is shown connected to the base of Q2, and Q2 connected to earth. This is wrong, R10 goes to earth and not to Q2, R3 is 47R, not 47k.

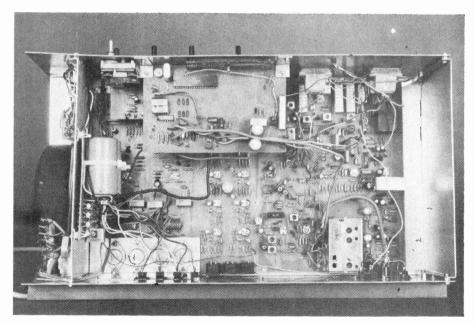
Mast head preamp uses 2 not 5 Mosfets. AM coverage is 2 band not 5 band. Sensitivity is $1.0\ uV$ not $10\ V$.

In Buylines, the complete kit with metalwork is £165. Uni-Electric will align the RF sections and check finished mother boards for £15.00.

Pin Wiring for PCBs

29/ to pin (27)

```
AM Aerial
 2/
      —Link
 3/
 4/
    To +Ve of signal level
 5/ To -Ve of signal level and pin (8)
 6/ Output to D.F.D.
 7/
     Test Point
 8/ To pin (5)
 9/ of Varicap pot
10/ +12V end of Varicap pot
11/
     +1V end of Varicap pot
12/
13/ }—Link
14/ to (3) on Tunerhead
15/ to (6) on Tunerhead
16/ to (8) on Tunerhead
17/ to pin (19), and pin 20 (on Power
Board)
18/ to pin 22 (on power board)
19/ to pin (17)
20/ to pin (19)
21/ to pin ((31) (on Tone Board)
22/ to pin (18)
23/ to pin (25)
24/ to pin (26)
25/ to pin (23)
26/ to pin (24)
27/ to pin (29)
28/ to pin (30)
```



An internal view of the complete unit, ready for the setting up procedure. The digital frequency meter board is top centre.

STEVENSON Electronic Components

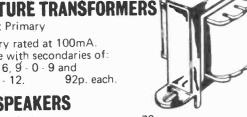
REGULATORS

78L05 30p	7805	60p	79L05 70p	7912 80	р
78L12 30p	7.812	60p	79L12 70p	7915 80	þ
78L15 30p	7815	60p	7905 80p	LM723 35	p

HARDWARE **MINIATURE TRANSFORMERS**

240 Volt Primary

Secondary rated at 100mA. Available with secondaries of: 6 - 0 - 6, 9 - 0 - 9 and 12 - 0 - 12.



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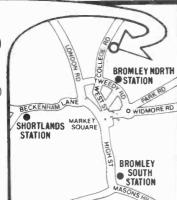
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709	28p	LM380	75p	SN 76013	140
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747	40p	LM1830	150p	SN76033	200
748	30p	LM3900	50p	SN76477	220
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	socket	socket
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ı	LS04	13p	LS86	30p	LS193	60p
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	7442	38p	74123	38p	74193	50p
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0		4024	40p	4068	18p
4001	12p	4026	90p	4069	12p
4002	12p	4027	30p	4071	12p
4007	12p	4028	48p	4081	13p
4011	12p	4029	50p	4093	45p
4013	28p	4040	60p	4510	65p
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DESIGNER'S NOTEBOOK

A monthly look at the notebook of ETI's chief design engineer, project editor Ray Marston.

AUNTI IRIS (the one with the big eyes) says that the ETI gremlins loved last month's ''Notebook.'' They gobbled up the original figure 1 (a method of precision gating a 555 astable) and left a copy of Fig 4 (a 555 pulse expander) in it's place. To set the record straight, this month's Fig 1 shows what last month's Fig 1 should have looked like. I hope aunti Sible approves.

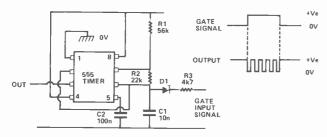


Fig. 1. Here it is in all its glory, the missing link, Fig 1 from last month — a precision gated astable.

Who Loves Yer, Baby?

Regular readers of ETI will have noticed that the design team has a particular love of the CD4017 IC. This modestly priced (about 80 pence in 1 off quantities) little device glories in the title of a "decade counter/divider with ten decoded outputs." It's the "ten decoded outputs" bit of the title that makes us really like the device, because those outputs can be used to do a lot of useful things.

The ten decoded outputs of the B-series 4017 can be used to directly drive a bank of LED's to make pretty displays, or to switch tone generators to create pretty tunes. Alternatively, outputs can be coupled back to the devices control terminals to make the IC count to, or divide by, 'n' (any number from 2 to 9) and then either stop or recycle. Numbers of 4017 IC's can readily be cascaded to give either multi-decade division, or to make counters with any desired number of decoded outputs. Let's take a closer look at the device.

4017 Basics

Figure 2 shows the outline and pin designations, the functional diagram, and the basic timing diagram of the CD4017, which incorporates a 5-stage Johnson counter. The device has clock, reset, and clock inhibit input terminals

The counters are advanced one count at each positive transition of the clock signal when the clock inhibit and reset terminals are low. Nine of the ten decoded outputs are low, with the remaining output high, at any given time. The outputs go high sequentially, in phase with the clock signal, with the selected output remaining high for one full clock cycle. An additional carry out signal completes one cycle for every ten clock input cycles, and can be used to ripple-clock additional 4017's in multidecade counting applications.

The 4017 counting cycle can be inhibited by setting

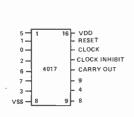
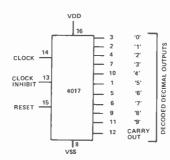


Fig. 2a. Outline and pin designations of the CD4017



CLOCK IS INHIBITED BY A HIGH SIGNAL ON PIN 13 COUNTER IS RESET BY A HIGH SIGNAL ON PIN 15 COUNTER ADVANCES ON POSITIVE TRANSITION OF CLOCK SIGNAL.

Fig. 2b. Functional diagram and data for the CD4017.

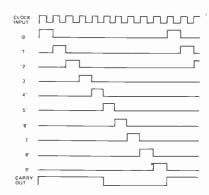


Fig. 2c. Waveform timing diagram of the CD4017, with its RESET and CLOCK INHIBIT terminals grounded.

the clock inhibit terminal high. A high signal on the reset terminal clears the counter to zero and sets the 'O' output terminal high.

4017 Applications

Figures 3 to 7 show a few ways of employing the decoded outputs of a single B-series 4017.

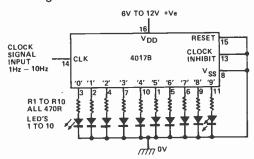


Figure 3: the circuit of a 10-stage sequential LED flasher or cheser, in which one LED is on and the other nine are off at any given time, and the on LED moves one step up the line each time a clock pulse arrives. An alternative action, in which nine LED's are on and one is off at any given time, can be obtained by reversing the polarity of all LED's and taking their common point to the positive supply line.

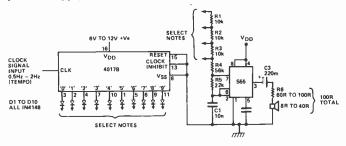


Figure 4: the circuit of a 10-stage 4-note musical sequencer, that can be used to generate simple tunes or melodies. The number of available notes can be increased by adding more resistors to the R1-R2 component chain.

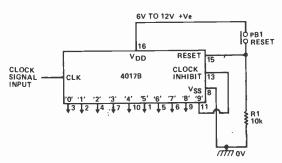


Figure 5: how to connect the 4017 so that it stops operating after completing a pre-determined counting sequence. Here, the counter is set to stop when it's clock inhibit terminal is driven high by the '9' output. The count sequence can be restarted by pressing reset button PB1.

Note in the figure six and seven circuits the counter can be made to divide by any number simply by taking the 'free' terminal of the circuit's multi-vibrator to the Nth output terminal of the counter.

Greater than 10

There are times when ten stages of counting/decoding aren't enough for a particular task. Examples that spring to mind are complex remote control coders and decoders

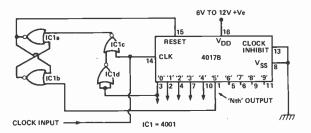


Figure 6: one way of connecting a 4017 as a divide-by-N (2 < N < 9) counter with N decoded outputs. This circuit is set to divide by 5. The circuit operation here is such that the Nth output of the counter momentarily goes high on the positive transition of the Nth clock pulse, and immediately causes the IC1a-IC1b flip-flop to change state and apply a reset command to pin 15 of the 4017, which in turn causes it's 'O' output to go high and feed a low signal to one terminal of NOR gate IC1c. When the negative transition of the Nth clock pulse arrives, it places a low signal on the remaining terminal of the IC1c NOR gate, which therefore feeds a high signal to IC1a and causes the flip-flop to again change state and remove the reset command from pin 15 of the 4017. The 4017 is then free to count again.

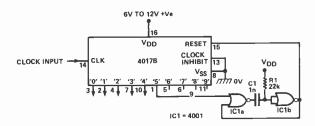


Figure 7: an alternative way of obtaining divide-by-N operation. Here, the Nth output (the 5th in this diagram) momentarily goes high on the arrival of the positive transition of the Nth clock pulse and causes the IC1a-IC1b monostable to generate a 15 uS pulse that immediately resets the counter to the 'O' or empty state, ready for the arrival of the positive transition of the next clock pulse.

that may require as many as nineteen sequential stages, simple music or tone sequencers that may require more than twenty stages, and LED-driving electronic games such as roulette which may require up to thirty-eight sequential stages. In such cases it is a fairly simple matter to interconnect a number of 4017 IC's to obtain any required total of decoded output stages.

Note in the Fig 9 circuit that the 1 counter gives nine useful outputs, and that all succeeding stages give eight useful outputs. The basic circuit can be expanded to incorporate any number of 4017 stages by simply adding slightly modified IC2-IC4a-IC4b stages between IC1 and the final two stages of the system.

Rabbiting on

You may be wondering why I've chosen this precise moment of history to rabbit on about applications of the 4017. The fact is, I'm presently playing with some rather unusual 4017-based multi-channel remote control systems for possible future projects, and all the stuff that I've crammed into this month's Notebook is spin-off from that development work. I'll tell you more about these next month.

In the meantime, if you want to play with the 4017 circuits that I've already described, you may find the Fig 11 clock generator circuit useful. It uses only one quarter of a CD4093 Schmitt, but generates beautifully clean and interference-free clock pulses.

You can fiddle with the R1 and C1 values to get any

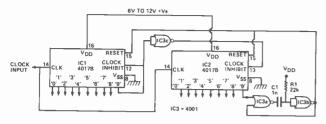


Figure 8 how to interconnect a pair of 4017's to make a 10- to 17-stage counter/decoder. The circuit is shown set for divideby-17 operation.

The clock input signal is parallel-fed to IC1 and IC2. When, however, the count is below 9, the '9' output of IC1 is low and causes the clock inhibit terminal of IC2 to be set high via IC3c, so IC2 is not influenced by the clock signals. As soon as the 9th clock pulse arrives the '9' output of IC1 goes high and inhibits IC1 from further clocking action, and simultaneously drives the clock inhibit terminal of IC2 low via IC2c and enables IC2 to respond to subsequent clock signals.

Eventually, on the arrival of the 17th clock pulse, the '9' output of IC2 goes momentarily high and triggers the IC3a-IC3b 15 uS monostable, which in turn resets both counters to the empty or 'O' states. The counting sequence then repeats.

Note that the '9' output of IC1 and the '0' and '9' outputs of IC2 are "lost" in the counting action, so the circuit provides a maximum of 17 usable counter/decoder stages. The circuit can be made to count by any number in the range 10 to 17 by connecting the "free" input terminal of IC2a to the appropriate output terminal of IC2.

clock frequency that you want. C1 can have any value from 100p to 10u, and R1 can have any value from 10k to 10M. Values of 10n and 100k give a clock frequency of about 1 kHz.

Smarter than the average bear

Does your cranium tend to inflate ever-so-slightly each time that you develop a particularly clever little circuit? If so, imagine how Robert J. Widlar must feel. He's the guy who, virtually single handed, designed the original 709 op-amp. And the 710, the 711, the LM101, the 108, the 109, and the 111. On top of that, he either owns or shares patents on the band gap reference and the super beta transistor.

Old smarty boots has done it again, and designed an opamp called the LM10. The LM10 is reckoned to represent one of the most important developments in IC op-amp technology in recent years. Amongst other things it can operate over the supply voltage range 1V1 to 40V. drawing only 270 uA of current in all cases. Its output can swing within 15 mV of the supply terminals, or will deliver 20 mA of output current with 400 mV saturation.

We plan to give full details of the LM10, complete with extensive applications information, in the near-future. Meantime, it really does seem that Robert J. Widlar is a lot smarter than your average bear. FIL

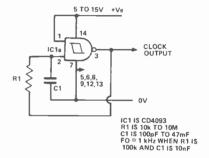


Fig. 11. This simple circuit makes an excellent clock generator for driving 4017 circuits.

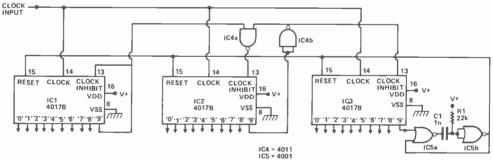


Figure 9 shows the connections for making an 18- to 25-stage counter/decoder from three 4017's. In this case IC3 is inhibited via IC4b and the low output '9' of IC2, and IC2 is inhibited via IC4a and the low output '9' of IC1, up to the 9th clock pulse. IC1 is inhibited via it's high '9' output, and IC3 is inhibited via IC4b and the low output '9' of IC2, between the 10th and 17th clock pulses.

Finally, IC1 is inhibited via it's high '9' output, and IC2 is inhibited via the high '9' outputs of IC1 and IC2 via IC4c between the 18th and 25th clock pulses, and the entire circuit is reset to the 'O' stage via the IC5a and IC5b monostable on the 25th-plus-one clock pulse.

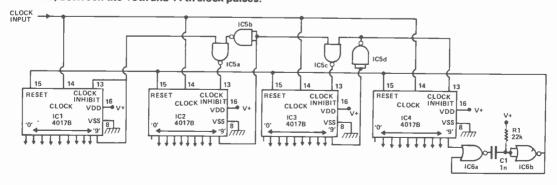
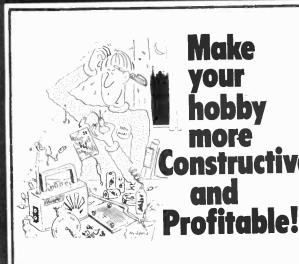


Fig. 10. A 26- to 33-stage counter/decoder set for divide-by-33 operation. This circuit can be expanded to give a ny number of decoded output stages by interposing additional IC2-IC52-IC5b stages between IC2 and IC3. Each additional 4017B stage makes an extra eight decoded outputs available.



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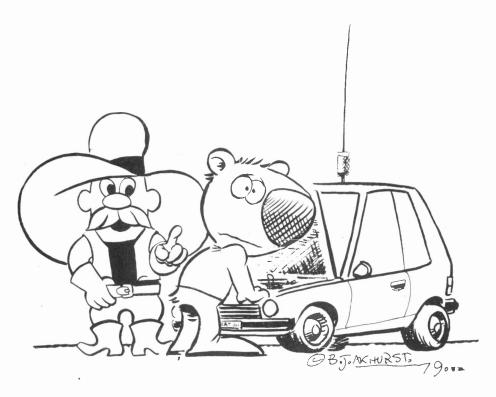
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BATTERY INDICATOR

Ever been caught by a battery that went flat at an embarrassing moment — like when you've just offered a friend a lift? The conversation goes a little flat when you're both riding the bus to work, 20 minutes late. Jonathan Scott found a solution . . .



THE OLD, RELIABLE lead-acid battery may be way ahead of what ever is in second place for vehicle electrical systems, but they do need a 'weather eye' kept on them. Particularly if they're out of warranty. The same applies to 'reconditioned' batteries, so often found in secondhand vehicles of some age.

That's the problem with cars — running out of petrol and running out of battery produces the same heart-rending result. Immobility.

Most vehicles have a petrol gauge. Few have an equivalent for the battery. Many 'older' cars included a 'charging current' meter. This told you something about the car's generator-regulator and required some inter-

pretation to figure out whether the battery was in good health.

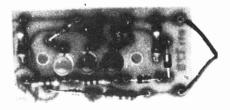
Probably the best way to check on the state of your battery is to use a hydrometer. However, hydrometers have a number of drawbacks. Being made of glass, they're fragile and can't be used while a car is in motion. The small amount of battery acid that remains on them presents a storage problem — the drips and fumes attack most metals and materials. They're okay for the corner garage but justifying their cost, for the occasional use they get in home workshops, is not always possible.

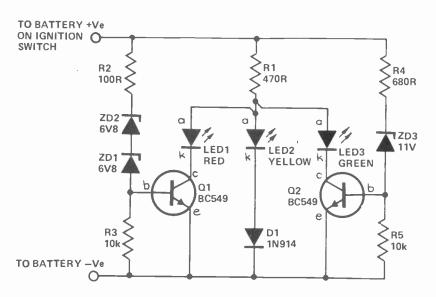
Another method of testing battery condition is by checking the voltage 'on load'. A lead-acid vehicle battery in a reasonable state of charge will have a

terminal voltage under normal working load somewhere between 11.6 and 14.2 volts. When a battery shows a terminal voltage below 11.6 volts its capacity is markedly decreased and it will discharge fairly quickly. Like as not, it won't turn the starter motor for very long! On the other hand, if the voltage on load is above 14.5 volts then the battery is definitely fully charged! However, if it remains that way for any length of time while the car is on the road, the vehicle's alternator-regulator system is faulty and the battery may be damaged by overcharging.

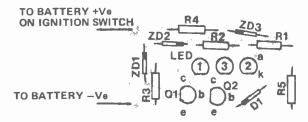
Reading the battery voltage can be done in a number of ways. You could use a digital panel meter, set up as a voltmeter. Their drawback is that they cost nearly ten times as much as a hydrometer! The next best method is to use an 'expanded-scale voltmeter'. Reading the voltage range between 11 and 15 volts on a meter face calibrated 0-16 volts is a squint-and-peer exercise. On a 0-30 volts scale, as used on many modern multimeters, it's worse. A meter which reads between 11 volts at the low end of the scale and 16 volts at the high end is ideal. Hence, the term 'expandedscale'.

However, you don't want to be peering at a meter on the dash board when you're driving through traffic. The range of voltage over which your battery is healthy is some two volts. An indicator which simply requires the





The circuit diagram and component overlay (below). During construction, make sure all of the diodes and LEDs are the right way round.



HOW IT WORKS

This circuit depends for its operation upon the different voltage drops across different colour LEDs.

At 20 mA the voltage drops across red, yellow and green LEDs are typically 1.7, 3.0 and 2.3 volts respectively. When the vehicle battery voltage is too low to cause either ZD1/ZD2 or ZD3 to conduct, Q1 and Q2 are held off by R3 and R5. Under these conditions the vellow LED is forward biased and conducts via D1 producing a potential of about 3.7 volts at point A (see circuit diagram). When the supply rises above about 11.6 volts ZD3 conducts, biasing Q2 on. By virtue of its lower voltage requirements the green LED conducts, reducing the voltage at point A to approximately 2.6 volts. This is not enough to bias D1/LED3 on, so the yellow LED goes off. The green LED 'steals' the bias from the yellow LED. When the supply rises above about 14.2 volts, Q1 is biased on and the red LED 'steals' the bias from the green. The potential at point A falls to two volts and only the red LED conducts.

R1 limits the current through the LEDs. R2 and R4 limit the base currents into Q1 and Q2.

PARTS LIST

Resistors all ¼W, 5% R1 470R R2 100R

R2 100R R3, R5 10k R4 680R

Semiconductors

D1 1N914 ZD1, ZD2 6V8 400 mW zener ZD3 11V 400 mW zener Q1, Q2 BC547,8,9 or BC107, 8, 9 or common silicon NPN type

Miscellaneous

Aluminium angle bracket for underdash mounting.

BUYLINES

Nothing to worry about here really, but make sure the LEDs are the correct colours, otherwise the voltage drops will not be correct!

occasional glance, and needs no 'interpretation', is what is really needed.

With this project, that's exactly what we've done.

Go, caution, stop

We have devised a simple circuit that indicates as follows:

Yellow: battery 'low' Green: battery okay

Red: battery overcharging

When the battery voltage is below 11.6 volts, a yellow indicator lights. This indicates the battery is most likely undercharged or a heavy load (such as high power driving lights) is drawing excess current. When it is between 11.7 and about 14.2 volts the green indicator lights, letting you know all is sweet. If the red indicator lights, as it will if the voltage rises above 14.2 volts, maybe the vehicle's voltage regulator needs adjusting or there is some other problem.

The circuit

The circuit is ingeniously simple, having barely a handful of parts. Reliability should be excellent.

We actually started out with a somewhat complex circuit. It used only two indicators and required you to 'interpret' what was happening. In trying to convert that to a yellow-green-red style of indication it sort of grew like topsy. This circuit had four transistors, a dozen resistors etc and didn't look at all attractive as a simple project that the average hobbyist or even handyman could build one Saturday afternoon and get going immediately. A rival circuit was devised by another staff member using a common IC. This sparked a controversy as to which was the better! Certainly, both did the job required . . but maybe there was a simpler method.

It was discovered that different coloured light emitting diodes (LEDs), which we had decided to use for the indicators in the project, had different voltage drops when run at the same current. Seizing on this idea, the original circuit (four transistors, a dozen resistors...) was modified to exploit this characteristic and the simple circuit you see here was the result.

Construction

Construction is straightforward. If you haven't soldered electronic components before — and this project was designed for the motorist/handýman as well as electronics enthusiasts — then we suggest you practice on something before tackling this project. Soldering is one of those things like swimming or riding a bicycle, or sex — it's okay once

you've done it once or twice but you don't practice out on the street!

We recommend you use the printed circuit board designed for this project. The actual layout of the components themselves is not critical but a printed circuit board reduces the possibility of errors.

It is best to mount and solder the resistors first. Follow this by soldering in the diodes D1 and the zener diodes ZD1, ZD2 and ZD3. Carefully follow the accompanying component overlay making sure the diodes are all inserted the correct way around. Next, mount the transistors, again referring to the overlay, checking to see they are inserted correctly before soldering.

Finally, mount the light emitting diodes. These too may only be inserted one way. Check with the component overlay and connection diagrams. Make sure they are in the correct sequence. On the component overlay, LED 1 is the red LED, located at the left. The yellow LED is on the right, marked with a '2'. The green LED, marked '3' is between them.

The circuit could be tested at this

stage if you have a variable power supply, or access to one. Simply vary the voltage across the range between 11 and 16 volts and note whether the LEDs light up in the correct sequence and close to the voltages indicated.

Mounting

As vehicles vary so much in dash panel layout, we can only make general suggestions.

Clearly, the indicator should be mounted such that the three LEDs are not in direct sunlight. A low part of the dash, but make sure it's readily visible from your normal driving position, will pretty well ensure the display may be easily read during the daytime. Alternatively, if you have an 'overhung' dash, or a portion which overhangs (usually where the instruments are mounted anyway), then a suitable position will generally suggest itself

Exact mechanical details will have to be determined according to your particular situation. Two holes are provided in the board for mounting bolts. Alternatively, the whole assembly may be mounted from the LEDs. Three LED holders inserted through part of the dash panel, or an escutcheon plate mounted on the dash, will hold the LEDs quite securely. Providing the leads on the LEDs are fairly short, the board will place little strain on them and the assembly should be mechanically secure.

Connection

The indicator may be installed in vehicles having positive or negative earth electrical systems.

The component overlay shows the connection for a negative earth vehicle. The 'battery +ve' lead goes to the ignition switch - the indicator only operates when the vehicle is being used - the battery negative lead should be taken to a good 'earth' point on the vehicle frame.

For a positive earth vehicle, the lead marked 'battery -ve' goes to the ignition switch connection, while the 'battery +ve' lead goes to the vehicle frame.

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Pets In Business

THE LONG AWAITED PET add-on's have arrived at last, honest! Launched at a Cafe Royal press conference was a new PET based business system with a price tag of £2,500 excluding software. Utilizing the new, large-keyboard 32K machine with Commodores own dual disk drive and tractor-fed printer it forms the cheapest small business system yet available. The software is being written by a new division of ACT, Petsoft's parent company, called PETACT and will cost between £225 for a single package to about £800 for a complete suite of programs. It will be available in either disk or cassette format and is the first business software for a micro to be written by a professional software house. The software price also includes a day's training for an employee.

We rather thought that the printer was never going to arrive as it was trapped at Heathrow in customs but it surfaced during the Champagne and Orange cocktails and appeared to be of high quality. The second reason for the Press reception was to announce the forming of an 'endorsement' scheme for non-Commodore produced PET add-on's, the PETACT software being the first product to be launched under the scheme.

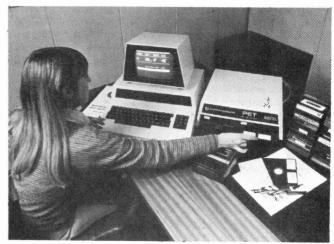
Deliveries of the new style PET's have started and should be available in most areas now, the disks and printers will start to appear in mid-May at some of the 100 dealers and will hopefully be generally available within a couple of months. Chuck Peddle the father of the PET and KIM was at the reception and gave a strong indication that new and exciting things were on the way in connection with both machines, memory expansion being one possibility.

On a final note the sales of the UK machine were around 3000 during 1978 and this figure had been reached by the end of April of this year, the market is still growing.

NASCOM With Added Plus

After the phenomenal success of the NASCOM I (150,000 sales worldwide) the company have announced a new single board machine called NASCOM II.

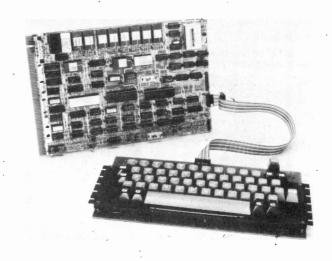
Although it is physically the same size as the 'I' and uses the same bus structure it is not intended as a simple upgrade but rather as a new starting point in the home computing market. Based on the Z80A it offers a 75% increase in processing speed along with an 8K Microsoft BASIC in ROM. Several new features are included on the machine, a new 2K monitor with many improvements over the T4, A CUTS cassette interface, 8K of user RAM and a new extended keyboard. The interfaces supplied include an on-board UART for the RS232 or the cassette interface, capable of running at 300 or 1200 Baud, and an uncommitted P10 for two 8 bit ports. The video is run from a 1KA RAM with a 2K character generator, an optional socket is supplied for another 2K graphics ROM which is software selectable.



Above and below: the new bits for PET.



Below: the new more powerful NASCOM.



Both the new monitor and the BASIC can be used with the 'I' and all the peripherals for the 'I' can be used with the 'II' making it the basis of a very nice OEM system. The circuit board is of the usual superb quality and the kit will be available from June at £295 ex VAT. We hope to get our hands on one to review soon and this will be published in CT as close to the release date as possible.

Clubbing Together

A couple of new clubs have sent us details of themselves this month. The first is the Sorcerer Programme Exchange Club, SPEC, which has been formed to promote the Exidy Sorcerer. Rather than having an actual club they are aiming to become an information exchange on useful, hints and programs for the machine and would be most grateful for anyone who has some to send them in. The people to contact are Mr G. F. Counsell and Mr M. P. Hannaby at 65 Trafalgar Road, Birkdale, Southport, Merseyside.

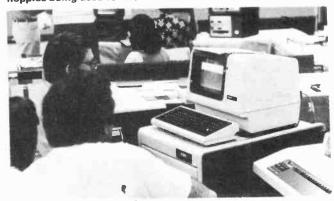
The second club is the South Yorkshire Personal Computing Group, SYPCG, who are appealing to people in the area interested in do-it-yourselr computing. They hope to meet on the second Wednesday of each month with a variety of topics under discussion. Membership is £3 for 1979 and the meetings will be held at 7.00pm in the University of Sheffield. For further information you should contact the Secretary, Mr Tony Rycroft, at 88 Spinneyfield, Moorgate, Rotherham, S. Yorkshire.

Showing It Off USA Style

I spent a pleasant weekend in Orlando, Florida, last month at a micro-show. It really was a micro-show, dealing with the machines and also being very small. However this was really an advantage as it allowed free and personal access to the exhibitors rather than the situation which arises at some of the UK exhibitions. The variety of machines was impressive, ranging from an IAM65 to an LSI 11, but there were no PET's, KIM's or Superboards which was rather surprising. The only new machine there was an Z80 based S100 system called Informer which also used an SC/MP for keyboard and video control. Supplied either with or without an integral floppy it looked impressive but is unlikely to appear on this side of the Atlantic.

The show also featured a siminar programme, again on a very informal and personal level which resulted in a most entertaining question and answer forum. The whole show was most professionally run and I only wish that some of the UK shows could adopt a similar attitude and become smaller and more personal instead of bigger and unhelpful.

The biggest business system at the show, an LSI II with dual floppies being used for stock control.





The familiar Apple II with a speech recognition board installed. It worked remarkably well and 'echoed' back your word through a synthesizer.



New TRS 80 printer. Will it reach us, we wonder.

A Texas system with dual floppies and integral thermal printer as well as a Centronics 702 on-line. It played a mean game of Star Trek!



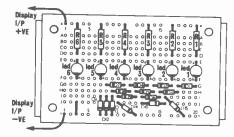
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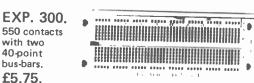
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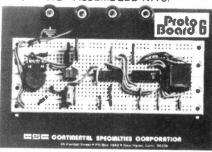
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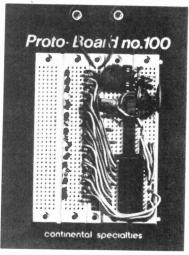
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PROGRESSIVE RADIO

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lists.

tech-tips

Calculator Special

Mine Sweeper

E. A. Johnson

The object of the game is to locate and destroy a moving minesweeper. The ship moves along a set course, but, to avoid destruction it can deviate slightly from the course and alter its speed.

Playing the game

The game is started by entering a number (in the range 0 to 1) into register E, to set the initial position of the minesweeper through a random number generator. A shot is made by entering the xy co-ordinates (into the A and B registers respectively) of the square where the ship is believed to be. The calculator determines the position of the ship and displays the distance by which the shot missed. If the shot is within five units of the ship, damage occurs which slows the ship down in proportion to the nearness of the shot. When the ship is destroyed the display flashes.

After the ship has been destroyed, the number of shots used can be displayed by pressing 'C', and a new game can be started by pressing 'D'.

Method of calculation

The initial value of Θ , which determines the ship's position is determined using the calculator's random number package. The ship's co-ordinates are then calculated by the following equations:

 $x = (50 + 45 \cos 3\Theta) + RNUMX$

 $y = (50 + 45 \sin 2\Theta) + RNUMY$ where RNUMX and RNUMY are random numbers (in the range of -3 to +3) to give the ship its avoiding action.

The distance of the shot from the ship is calculated using pythagoras and displayed in integer mode.

The next value of Θ is then given by $\Theta = \Theta + \Theta INCR$

where Θ INCR is originally set to 5, the calculator then determines the new co-ordinates of the ship.

When the distance of the shot from the ship is less than five units, the value of Θ INCR is reduced to slow the ship down. The new value is given by Θ INCR = Θ INCR - (5 \div distance).

The above procedure continues until Θ INCR \leq 0 when the ship is destroyed.

A new game, if required, is started by automatically generating a new random initial value of Θ .

MINESWEEPER	PROGRAM	FOR	T1 58	& 59
MINIMEDIAFEREN	FILOGITAIN	1 011	11 30	000

LOC	CODE	KEY		03	3		00	0
000	43 01 44 00 43 02	RCL 1 SUM 0 RCL 2	040	58 00 36 15 71 88 65	Fix 0 Pgm 15 SBR D.MS X	080	65 02 54 38 71 33 85	x 2) som SBR X +
010	91 76 33 65 04 05 85 05 00 85 36 15	R/S Lbl X x 4 5 + 5 0 + Pgm 51 SBR	050	03 06 00 95 42 00 25 91 76 11 69 23	X 3 6 0 = STO 0 CLR R/S Lbl A Op 23	090	05 32 95 34 42 02 77 00 00 55 32 95	5 x
020	88 65	D.MS	060	75 53 53	(100	35 22 44	1/x INV SUM
	06 75 03 95 33 92 76 15	X 6 3 = X INV SBR Lbl E STO		43 00 65 03 54 39 71 33 32	RCL 0 x 3) cos SBR X x t	110	01 29 43 01 77 00 00 25 35 22	1 CP RCL 1 x>t 0 00 CLR 1/x INV
030	09 76 14 05 42 01 00 42	9 Lbl D 5 STO 01 0 STO	070	00 91 76 12 75 53 53 43	O R/S LЫ B - ((RCL	110	58 91 76 13 25 43 03 91	Fix R/S Lbl C CLR RCL 3 R/S

Example Game

Example	Game	
Comment	Enter	Display
Enter a number between 0 & 1	0.258 E	0
Enter guess for x co-ordinate Enter guess for y co-ordinate x co-ordinate y co-ordinate x y x y	50 A 11 B 84 A 70 B 40 A 85 B 43 A 87 B 51 A	0 65 (Distance) 0 62 0 7 0 3
y x y	89 B 54 A 90 A	3 0 9.9999999 99 (Flashing)
To display number of shots To start a new game x co-ordinate y co-ordinate ETC.	C D 50 A 11 B	6 0 0 42

Tech-Tips is an ideas forum and is not aimed at the beginner. We regret we cannot answer

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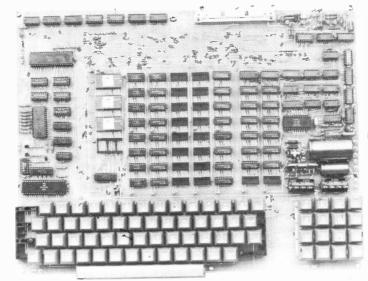
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ANDOVER (0264)64455



.Calculator Special

Lunar Landing

Sarah J. Owen.

This program was devised for use on the Commodore PR.100 calculator, but is easily adapted for use on any other programmable ones. Imagine you are the Astronaut controlling the final descent of a lunar module, at regular intervals the speed of descent is displayed, the period of burn of the retro-rocket has to be calculated, after allowing for the reducing weight of the fuel on board. Five speed corrections are allowed, after which the final impact velocity is displayed. If an error is made and all fuel is used, there is just time to transmit an urgent S.O.S. message before destruction on the lunar surface. Due to the lack of program space, the method of selecting the initial random speed is unusual, but ranges between 20 and 100 m.p.h.

Recommended periods for Retro-rocket firing

SPEED	BURN		
5 7 10 15 20 30 40 50 60 70 80 90 100 110 120 130 150 160	1.6 1.9 2.3 2.7 3.0 3.4 3.7 3.9 4.1 4.2 4.4 4.5 4.6 4.7 4.8 4.9 5.0 5.1	180 200 220 250 270 300 330 365 400 450 500 550 600 660 730 800 900 1000	5.2 5.3 5.4 5.5 5.6 5.7 5.8 5.9 6.1 6.2 6.3 6.4 6.5 6.6 6.7 6.8 6.9

11						
	PROGRAM			Memory 1 Memory 0	Seconds ofAccurate desc	fuel left ent speed
Result of impact speed:—	LOC	CODE	KEY	N.B. Adjust	burn period for m.p.h. for each	weight of
nesurt of impact speed:—	00	0.4	_	36		
	00 01	21	F	37	85	
0 - 5 m.p.h. PERFECT LANDING	02	63 21	S	38	52 81	MR
6 10 mmh SUCHT DAMAGE	03		F	39		1
6 - 10 m.p.h. SLIGHT DAMAGE, LIFT OFF DELAYED.	03	51	FRAC	40	85	_
11 - 15 m.p.h. STRUCTURAL DAMAGE		74 81	X	41	52 91	MR
LIFT-OFF DOUBTFUL	06	91	1	42	74	0
16 - 25 m.p.h. SEVERE DAMAGE &	07	95	0	43	95	X
INJURY - USE	08	95 51	= 1	44	35	=
SUICIDE PILL.	09	91	M	45	51	X
ABOVE	10	53	0	46	91	M 0
25 m.p.h. MODULE & ALL	11	82	Xn 2	47	52	MR
LIFE DESTROYED	12	91	0	48	81	1
	13	51	M	49	94	+/_
	14	81	1	50	15	SKIP
	15	71	4.	51	14	GOTO
	16	51	M	52	73	6
	17	82	2	53	63	9
SET UP:-	18	52	MR	54	52	MR
	19	91	0	55	82	2
F-CA-F-FP-8-GOTO-00	20	74	X	56	85	_
Mode switch to load — enter program —	21	62	8	57	81	1
mode switch to run - goto - 00 enter	22	84	+	58	95	=
any two or more numbers (date etc.)	23	52	MR	59	15	SKIP
Each followed by Xn key. Press R/S	24	81	1	60	14	GOTO
speed of descent displayed.	25	95	=	61	81	1
Allow for weight of fuel remaining,	26	51	M	62	73	6
enter period (in seconds) of rocket burn	27	91	0	63	52	MR
to reduce speed, press R/S – new rate	28	21	F	64	91	0
of descent displayed, correct as before.	29	52	INT	65	13	R/S
After five speed corrections, impact	30	13	R/S	66	14	GOTO
speed will be displayed. If fuel in	31	21	F	67	91	0
excess of 20 seconds is used, module	32	85	M-	68	91	0
transmits an urgent message before	33	81	1	69	72	5
destructing.	34	21	F	70	91	0
Press R/S to re — start.	35	32	e ^X	71	72	5

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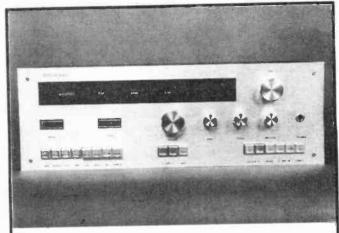
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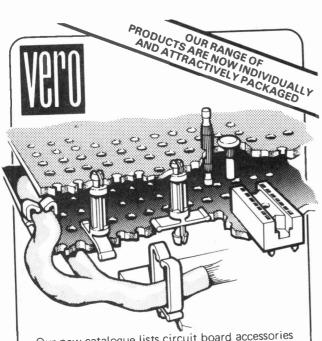
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wrong position. To play: Player A enters a 5 figure number and then presses GSB 1.	10	STO7 STO8 R R/S (Enter guess) 5		gLBL 4 1 4 STO 9
Player B enters his guess and presses R/S. After several seconds calculation the display shows a number such as 1.2 which means 1 digit in the right place and 2 more correct figures but in the wrong position.		CHS GSBO 1 STOO gLBL5	60	gLBL6 RCL 9 STO 0 RCL i STO 6 5
Player B then enters another guess and presses R/S, etc. until he achieves a score 5.0. For cheats (!) or if the number set has been forgotten, it is held in STO .5.	20	RCLi 9 STO+0 x≷y RCLi	70	STO 0 gLBL 7 RCL i RCL 6
		gx = 0? GSB3 8 STO-0		g x = 0? GSB 0 gDSZ GTO 7
The use made of the calculators stores is shown below. If the number set was ABCDE, and the guess is FGHIJ, then:	30	RCL0 6 fx = y? GTO4		STO-9 RCL 9 9 f x ≠ y?
STO 0 Used 1 J 2 I 3 H 4 G 5 F 6 Used		GTO5 gLBL3 1 STO+7 RTN gLBL0	80	GTO 6 RCL 7 STO-8 1 0 STO÷8 x ≷ y
7 Used 8 Used 9 Used .0 E .1 D .2 C	40	STO 0 x ≷ y EEX 4 ÷	90	RCL ['] 8 + GTO 9 gLBL 0
.2 B .3 B .4 A .5 ABCDE	45	gLBL2 fINT	90	gLBL 0 1 STO+8 RTN
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MM7 C7200EM 20,000 opv



0 to 6, 30, 120, 300, 600, 1200 0 to 6, 30, 120, 600, 1200 3000, 6000

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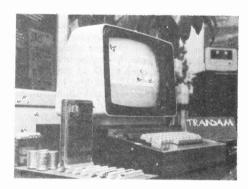
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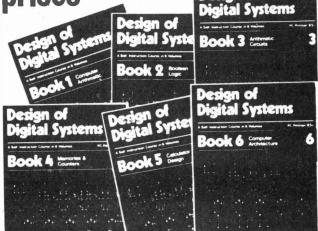
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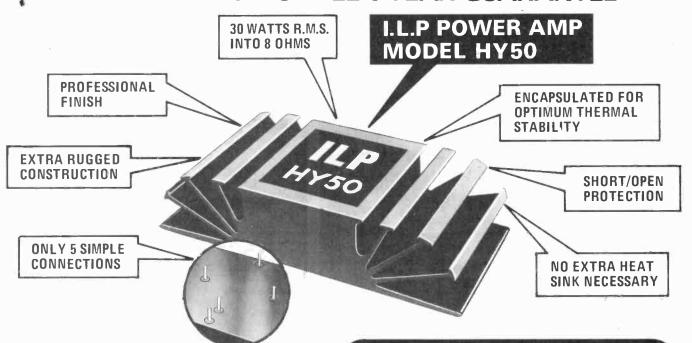
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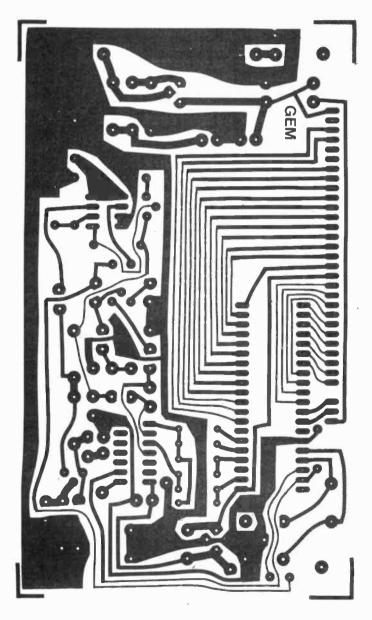
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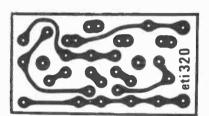
GATHERED HERE are all the PCBs for this month's projects.

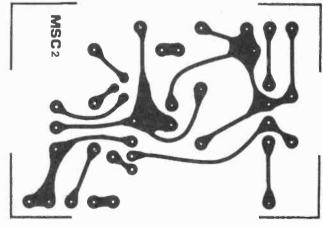
All are shown foil side up, and full size. Companies wishing to produce these for sale as ready made PCBs should note that where the board carries a copyright symbol, the designer retains that copyright to himself, so his company,

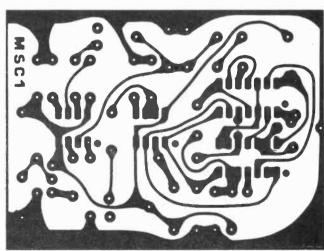
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These pages form the basis of our ETIPRINT sheets, which are etch resistant transfers of the foil patterns, designed to simplify one-off PCB production.









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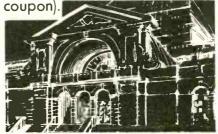
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Various other DFM systems described in our catalogue part 2 - including a one chip solution to providing digital display of FRG7 kHz dial, combined with clock/timers etc

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Inotec 1-A fully DC tuned and switched LW/MW/FM stereo tuner to interface with synthesiser control etc. A first! Details OA

COMPONENTS for Radio and Audio ICs, HMOS etc.

The list is too long to attempt here, but AMBIT specializes in all types of semiconductor for radio reception, including devices operating from DC to 5GHz. New low cost SBL1 diode ring mixers (equiv case MD108 etc) -first with HMOS fets, now with a PCB for DC amplifier, and offset sense and protection relay for speakers. See catalogue and updates for most info, pse ou cannot find in catalogues.

		L 101	111101	mation on an	A runnir	Jγι
ļ	Radio ICs	cost 4	- vat	Stereo ICs	cost 4	- va
	CA3089E	1.94	24	MC1310P	1.50	19
	CA3189E	2.45	30	uA758	2.20	27
	HA1137W	2.20	27	CA3090A	2.75	34
	SN76660	0.75	9	HA1196	3.95	49
	TDA1090	3.35	42	HA11223	4.35	54
	TDA1083	1.95	24	KB4437	4.35	54
	TDA1220	1.40	17	KB2224	2.75	34
	SL6640	2.75	34	Preamp ICs	/switc	hes
	MC3357	3.12	39	TDA1028	3.50	44
	HA1197W	1.40	17	TDA1029	3.50	44
	MC1496	1.25	16	TDA1074	4.14	52
	LM373/4	3.75	49	KB4438	2.22	28

AF power ICs cost + vat LM380N 1.00 12 TBA810AS 1.09 14 TDA2002 TBA820M 0.75 9 from the general list: LEDs:all colours and low prices 2SJ48/2SK134 HMOS 9.90 +£0.80 vat (Pair) Signal fets/transistors and TOKO COILS & FILTERS!

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7402	14	20	7463		124	74132	73	78	74190	115	92	74378	130
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Current news: Work continues apace on our HMOS PA kit, and by the time this is published - we expect to be about to launch the product in a style that matches the Mark III system. The unit uses separate transformers and power supplies, and includes a DC offset sensing circuit combined with slow switch-on using a relay. We introduce the HyperFi FM IF with this The unit uses separate transformers and power supplies, and includes a DC offset sensing circuit combined with slow switch-on using a relay. We introduce the HyperFi FM IF with this advert - and a separate leaflet is available on request with an SAE. All new pricelist revision also available with an SAE. The Mullard DC controlled tone/volume and switch ICs with a more than HiFi' specification are in stock at last - together with reams of data (over 50 pages now). Also, RC enthusiasts will be interested to learn that we are supplying parts for various kits now CWO please. Account facilities for commercial customers OA. Postage 25p per order. Minimum credit invoice for account customers £10,00. Please follow instructions on VAT, which is usually shown as a separate amount. Overseas customers welcome uplease allow for postage etc according to desired shipping method. Access facilities for credit purchases.

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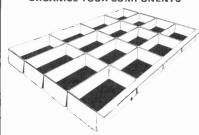
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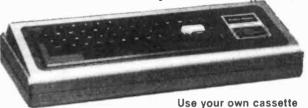
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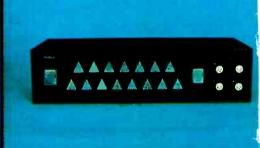
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