## elertronims today December 1979 <br> Intefrational

## 50

## SFET Applications

## Chess Machines

Coral MC 81

## TRANSCENDENT 2000 SINGLE BOARD SYNTHESIZER

LIVE PERFORMANCE SYNTHESIZER DESIGNED BY CONSULTANT TIM ORR (FORMERLY SYNTHESIZER DESIGNER FOR EMS LIMITED) AND FEATURED AS A CONSTRUCTIONAL ARTICLE IN ELECTRONICS TODAY INTERNATIONAL
The TRANSCENDENT 2000 is a 3 octave instrument transposable 2 octaves up or down giving an aftective 7 octave range There is portamento pitch bending avCO with shape and pitch modulation. a VCF with both low and high pass outputs and a separate dynamic sweep control a noise generator and an ADSR envelope shaper There is also a slow oscillator a new pitch The kit includes fully finished metalwork fully assembled solid teak cabinet filter sweep pedal professional quality components (all resistors ether $2 \%$ metal oxide or $1 / 2 \%$ metal irml) and it really is complete - right down to the last nut and bolt and last piece of wire There is even a 13 A plug in the k 1 t - you need buy absolutely no more parts before plugging in and making great musicl Virtually all the components are on the one protessional quality fibreglass PCB printed with component locations All the controls mount directly on the main board. all connections to the board are made with connector plugs and construction is so simple it can be built easily in a few evenings by almost anyone capable of neat soldering! When finished you wil possess a synthesizer comparable in pertormance and quality with ready-buit units selling for between $£ 500$ and $£ 700^{\prime}$

COMPLETE KIT ONLY $£ 172.00$ + VAT!

Comprehensive handbook supplied with all complete kits! Th ully describes construction and tells you how to set up you parr of ears


AS FEATURED IN AUGUST-NOVEMBER'79 Another superb design by synthesizer expert Tim Orr!
TRANSCENDENT DPX

DIGITALLY CONTROLLED, TOUCH SENSITIVE, POLYPHONIC, MULTI-VOICE SYNTHESIZER ( reed sound - fully polyphonic e you can play chords with as many notes as you like On the second output there is a wide range of different voices still fully polyphonic lit can be a straightforward piano or a honky tonk prano or even a mixture of the two Atternatively you can play strings over the whole range of the keyboard or brass over the whole range of the keyboard or sounds - just like an acoustic paro The doly There is a master volume and pone control a separa control for the comes in only after waiting a short time after the note is struck for even more realistic string sounds


Cabinet size $36.3^{\prime \prime} \times 15.0^{\prime \prime} \times 5.0^{\prime \prime}$ (rear) $3.3^{\prime \prime}$ ( (ront)
COMPLETE KIT ONLY £365.00 + VAT!
, 0 To add interest to the sounds and make them more natural there is a chorus ensemble unit which is a complex phasing system using CcD (charge coupled device) analogue delay
overall effect of this is similar to that of several acoustic instruments playing the same piece of music The ensemble circuitry can be switched in with either strong or mild effects As the system is based on digital circuitry digital data can be easily taken to and trom a computer (for storing and playing back accompaniments with or without piten or key change, computer composing etc etc) and an interface sockel ( 25 way $D$ type) is provided for this purpose
Abthough the DPX is an advanced design using a very large amount of circuitry much of it very sophisticated the kit is mechanically extremely simple with excellent access to all the circuit boards which interconnect with multiway connectors fust four of which are removed to separate the keyboard circuitry and the panel circuitry from the main circuitry in the cabinet

The kit includes fully finished metalwork solid teak cabinet professional quality components \{all resistors $2 \%$ metal oxide\} nuts bolts etc even a 13 A plug - you need buy absolutelyno more parts before plugging in and making great music' When tinished you will possess an instrument comparable in performance and quality with ready-built units selling for over £' 200 '

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LONG PERIOD TIMER
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THE BEAST Pt 2
TOUCH SWITCH
FLASH TRIGGER
LOGIC PROBE
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35 Don't be a drip
46 Sound device
55. Wait a minute . . . or an hour . . .

67 Have a row
76 Ear to the air
86 Remotely interesting
93 Do it by feel
97 Out with the bulbs
101 Bit useful

## INFORMATION

| ETI NEXT TIME | $\mathbf{3 1}$ | Advance warning |
| ---: | :--- | :--- |
| MARKETPLACE | $\mathbf{4 4}$ | A new watch offer |
| SPECIALS | $\mathbf{5 1}$ | One offs from ETI |
| SUBSCRIPTIONS | $\mathbf{8 0}$ | Why do it any other way? |
| BOOK SERVICE | $\mathbf{8 5}$ | Fine print |
| HE FOR THEE | $\mathbf{7 2}$ | Don't be left out |



[^1][^2]EHFTXSEMICONDUCTORS TRANSISTORS







 74 SERIES TTL ICs

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| LINEAR ICs |  |  |  |  |  |


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|  | Intesrated Circuirs |  |  |
|  | Electronics |  |  |
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| 221 | Hi－Fi |  | c1．15 |
| 222 | 20 Solid State Proi for Car |  | ¢1．95 |
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| 228 | Electricity | 1 | E1．15 |
| 229 | Beginners Guide to Electronics |  | 25 |
| 230 | Beginners Guide to Television |  | ¢2．25 |
| 231 | Beginners Guide to Transistors |  | ¢2．25 |
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| 233 | Beginners Guide to Radio |  | （e2．75 |
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| 9 | 50 Photoelectric C Circuit |  | $\underline{11.80}$ |
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## SWITCHES



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DL 7037 segment D．P．let（ $30^{\prime \prime}$ nerght）Common Anode
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RED Single Digit Lrght Pipe ofno． 1511 E1．73 OPTO－ISOLATORS
Cil74 Sind 1500 －continuous twd current 100 ma with infra－red LED Emitter and NPN Silicon Photo Transistor $\begin{gathered}\text { o／no．} 1497 \text { £0．61 }\end{gathered}$ CILD74 Multi－Channel 8 pin DIP Two Isolated Channels CLO74 Multi－Channel 16 pin DIP Four Isolated Channels $\begin{gathered}0 / \mathrm{no} \\ \text { o／no．} 1499 \\ £ 2.69\end{gathered}$

MEL 11 （TILSI）NPN LIGHT DETECTOR
Silcoon Photo Darlington Amplifier－VCBO 30 v VECO 10 v Ic 100 mA

## NUTS AND BOLTS

| cheese head．Supplied in multiples of 50 ． |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Type | No． | Price | Type | No． | Price |
| Iin OBA | 839 | E1．38 | 1／3in 4BA | 846 | ¢0． 37 |
| 1／2in 08A | 840 | c0．86 | 1／4in 4BA | 847 | c0． 29 |
| 1 in 2BA | 842 | E0．75 | lin 6BA | 848 | ¢0．46 |
| $1 /$ in 2BA | 843 | ¢0．52 | $1 / 2 \mathrm{in} 68 \mathrm{~A}$ | 849 | ¢0．24 |
| $1 / \mathrm{in} 2 \mathrm{BA}$ | 844 | E0．60 | $1 / 4$ in 68A | 850 | c0． 28 |
| 1 in 48A | 845 | c0．51 |  |  |  |
| BA NUTS－packs of cadmium plated full nuts in multiples of 50 |  |  |  |  |  |
| Typp | No． | Price | Type | No． | Price |
| OBA | 855 | c0．${ }^{\text {3 }}$ | 48 A | 857 | ¢0． 35 |
| 284 | 856 | C0．55 | 6BA | 858 | c0． 28 |
| BA WASHERS－Hat cadmium plated plain stamped washers supplied in multiples of 50 ． |  |  |  |  |  |
|  |  |  |  |  |  |
| Type | No． | Price | Typa | No． | Price |
| OBA | 859 | ¢0．16 | 4 BA | 861 | ¢0．14 |
| 284 | 860 | c0． 14 | 6BA | 862 | ¢0． 14 |
| SOLDER TAGS－Hot tinned supplied in multiples of 50 |  |  |  |  |  |
| Type | No． | Price | Type | No． | Price |
| OBA | 851 | ¢0．46 | 4 BA | 853 | 60.25 |
| 2BA | 852 | ¢0．32 | 6BA | 854 | ¢0．25 |

## AUDIO LEADS

|  |  | Pric． |
| :---: | :---: | :---: |
| $107$ | FM indoar Ribbon Aerial | ${ }_{\text {c }}^{60.69}$ |
| 1 | 5 pin Oin plug to 3.5 mm Jack connectied to pins |  |
|  |  |  |
|  | 184 Length 15 m | ¢0．98 |
| 116 | Car aerial extension Sc |  |
|  | Firted plug and soct |  |
|  | and radios 2 metres | ¢0．78 |
| 118 | 5 pin Din phono plug |  |
|  | socket | ¢1． |
| 119 | $2+2$ pin attenuation network for stereo headphones |  |
| 120 | Length 0.2 m |  |
| 120 | til most car cassetes．8－track cartridge and |  |
|  | combitation uni s supplien |  |
| 123 | 6.6 m Conted Gutar Lead Mono Jack plug to Mono |  |
|  | Jack plug Bla |  |
|  | 3 pin Din plug to 3 pin din plug Length！ 5 m |  |
| 125 | 5 pin Din plug to 5 pin din pi |  |
|  | 5 pin Din plug to Tinned ope |  |
| 127 | 5 Pin Din plug to 4 Phore |  |
|  | All colour coded Length 15 m |  |
|  | andin piug to 5 pin Oin socker Length 15 m |  |
|  | 5 pin Din pug to 5 pin din plug mirror image． |  |
|  | Lengin 1.5 m |  |
| 130 |  |  |
|  | 5 pin Oin plug to 3 min OIN plug i \＆ 4 an |  |
|  | Len |  |
| 13 | DiN piug io 2 din DiN sockel Length 10 m | E1．13 |
|  | 5 prin Oin piug to 2 Pho |  |
|  | Comnecteo pins 3 \＆ 5 ．Length 15 m | 60.86 |


| AUDIO LEADS |  |  |  |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & 134 \\ & 135 \\ & 136 \\ & 178 \end{aligned}$ |  |  | $\varepsilon 0.78$ $\substack{62.01 \\ 60.52}$ |
| TRANSFORMERS |  |  |  |
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| $\begin{aligned} & \text { No } \\ & \text { No24 } \\ & 2025 \end{aligned}$ | Thers <br> TMP0．0．6V 0.6 V MT1 $50-0+22 \mathrm{O} 0.1$ |  | $\begin{aligned} & \text { fitice } \\ & \text { E1.84 } \end{aligned}$ |
| $\begin{aligned} & \text { NAMP } \\ & \text { No } 2026 \\ & \text { 2026 } \\ & \text { 2026 } \\ & 2026 \\ & 202030 \end{aligned}$ |  |  |  |

STANDARD MAINS Primary 240 V Mutti－tapped secondary mains transformers available in $1 / 2 \mathrm{amp}$ ． 1 amp
and 2 amp current rating．Secondary taps are $0-19-25-33-40-50 \mathrm{~V}$



$2035 \quad 240 \mathrm{~V}$ Primaiyo－55V＠
2A Secondary
2042240 V Priman 0 SPECIAL OFFEA
each welt from the secondary winding any voltage up to 20 V ＠ 2 A is
each volt from the secondary winding any voltage up to $20 V @$
sasily obtainable．Ideal for the experimenter
$E 1.50 \quad$ P．\＆P． 86 p

## CASES AND BOXES




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adequate heatsinks, protected sealed circuitry,
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The HY5 pre-amp is compatible with all I.L.P. amplifiers and P.S.U.'s. It is contained within a single pack 50 x $40 \times 15 \mathrm{~mm}$. and provides multifunction equalisation for Magnetic/ Ceramic/Tuner/Mic and Aux (Tape) inputs, all with high overload margins. Active tone control circuits; 500 mV out. Distortion at $1 \mathrm{KHz}-0.01 \%$. Special strips are provided for connecting external pots and switching systems as required. Two HY5's connect easily in stereo. With easy to follow instructions.
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I.L.P. Power Supply Units are designed specifically for use with our power amplifers and are in two basic forms - one with circuit panel mounted on conventionally styled transformer the other with toroidal transformer half weight and height of conventional laminated types

| Model | Output <br> Power <br> R.M.S. | Dis- <br> tortion <br> Typical <br> at 1KHz | Minimum <br> Signal/ <br> Noise <br> Ratio | Power <br> Supply <br> Voltage | Size <br> in mm | Weight <br> in gms | Price + <br> V.A.T. |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| HY30 | 15 W <br> into 8 $\Omega$ | $0.02 \%$ | 80 dB | $-20-0-+20$ | $105 \times 50 \times 25$ | 155 | $£ 6.34$ <br> $+95 p$ |
| HY50 | 30 W <br> into 8 $\Omega$ | $0.02 \%$ | 90 dB | $-25-0-+25$ | $105 \times 50 \times 25$ | 155 | $£ 7.24$ <br> $+£ 1.09$ |
| HY120 | 60 W <br> into 8 $\Omega$ | $0.01 \%$ | 100 dB | $-35-0-+35$ | $114 \times 50 \times 85$ | 575 | $£ 15.20$ <br> $+£ 2.28$ |
| HY200 | 120 W <br> into 8 $\Omega$ | $0.01 \%$ | 100 dB | $-45-0-+45$ | $114 \times 50 \times 85$ | 575 | $£ 18.44$ <br> $+£ 2.77$ |
| HY400 | 240 W <br> into $4 \Omega$ | $0.01 \%$ | 100 dB | $-45-0-+45$ | $114 \times 100 \times 85$ | 1.15 Kg | $£ 27.68$ <br> $+£ 4.15$ |

Load impedance - all models 4-16 $\Omega$
Input sensitivity - all models 500 mV
Input impedance-all models $100 \mathrm{~K} \Omega$
Frequency response - all models $10 \mathrm{~Hz}-45 \mathrm{KHz}-3 \mathrm{~dB}$

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PSU $30+15 \mathrm{~V}$ at 10 ma to drive up to five HY5 pre-amps $£ 4.50+68$ p VAT
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## CHROMATHEQUE 5000

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5 CHANNEL LIGHTING <br> \section*{\title{
5 CHANNEL LIGHTING EFFECTS SYSTEM EFFECTS SYSTEM <br> <br> <br> COMPLETE KIT
}} <br> <br> <br> COMPLETE KIT
}}

ONLY<br>$£ 49.50$ + VAT!

Panel size $19.0^{\prime \prime} \times 3.5^{\prime \prime}$. Depth 7.3"
This versatile system featured as a constructional article in ELECTRONICS TODAY INTERNATIONAL has 5 frequency channels with individual level controls on each channel. Control of the lights is comprehensive to say the least You can run the unit as a straightorward sound-to-light or have it strobe all the lights at a speed dependent upon music level or front panel control or use the internal digital circuiry which produces some superb random and sequencing effects. Each channel handles up to 500 W and as the kit is a single board design wiring is minimal and construction very straightforward.

Kit includes fully finished metalwork, fibreglass $P C B$ controls wire eic - Comolete right down to the last nut and bolt

## MPA 200100 WATT (rms into $8 \Omega$ ) MIXER / AMPLIFIER

COMPLETE KIT ONLY $£ 49.90$ + VAT!

MATCHES THE CHROMATHEQUE 5000 PERFECTLY!


Featured as a constructional artucle in ETI the MPA 200 is an exce. mixer which accepis a wider range of sources such as microphone, guitar, etc. There are wide range tone inpu mixer which accepis a wider range of sources such as microphone. Guitar, etc There are wide range tone controls and a master volume control Mechanically the MPA 2000 is simplicity The kit includes fully finished metalwork, fibreglass PCBs. controls, wire. etc



T20 + 20 20W STEREO AMPLIFIER £33.10 + VAT This kit, based upon a design published in Practical Wireless. uses a single printed carcuir
board and offers at very low cost, ease of construction and all the normal facihties found on board and offers at very low cost, ease of construction and all the normal facilites found on quality amplitiers. A 30 watt version of this kit ( $T 30+30$ ) is also avallable for $\mathbf{£ 3 8 . 4 0 + V A T}$.
matching tuners - see our free catalogue

This easy to build version of our world-wide acclaimed 75 W amplifier kit based upon circuit boards interconnected with gold plated contacts resulting in minimal wiring and construction delightfully straightforward. The design was published in H-Fi News and Record Review and features include rumble filter, variable scratch filter, versatile tone controls and tape
monitoring whilst distortion is less than $0.01 \%$.

## WIRELESS WORLD FM TUNER £70.20 + VAT

A pre-aligned front-end module makes this Wireless World published design very simple to construct and adjust without special instruments. Features include an excellent a.m. rejection push-butron station selection as well as infinitely variable tuning and a phase locked loop stereo decoder, incorporating active filters for "birdy" suppression.

## LINSLEY-HOOD CASSETTE DECK £79.60+VAT

This design, published in Wireless World, although straightforward and relatively low cost provides a very high standard of performance. There are separate record and replay amplifiers and switchable equalisation together with a choice of bias levels are also provided. The


COMPLETEKITS: Our complete kits really are complete All of the projects shown on this page are supplied with fully finished metalwork, ready assembled high quality teak veneer cabinet (last 4 kits on this page), or protessional quality rack mounting cabinet (first 2 kits on this page), cables, nuts, bolts, etc.. and full instructions - in fact everything!
All of the kits shown on this page are available as separate packs for those customers who wish to spread their purchase or perhaps make their own cabinets or metalwork. Prices are given in our
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## Silence Is

## Golden

It's also ball-shaped. (I'm not going to be rude, honest). The Golden Ball is a new, automatic sound level controller for discos and dance halls. Made by Ardente of Windsor, wellknown for their work in noise control, this unit is designed to help club owners avoid complaints, keep neighbours happy and reduce health risks to audiences.

A sensitive directional mike detects harmful noise levels, a golden, ball-shaped light switches on when the sound is too loud and a control box shuts off amplifier power if the warning is ignored.
The mechanically accepted
figure at which sound becomes a danger to health is 90 dB , so the system automatically cuts out noise in excess of this figure. Below that, users can set their own particular comfortable maximum noise level

So what happens when the maximum is exceeded? Well, the ball lights up to warn everyone that the limit has been reached. Five seconds then elapses in which the sound level can be reduced voluntarily. If this isn't done, there's an embarrassing five seconds of silence until the system resets itself.

Full details of the Golden Ball are available from the AntiNoise Pollution Division Ardent Ltd, Thames Avenue Windsor, Berkshire.

## Air-Porters

If you've had to lug cases miles around an airport, from terminal to bus station or car park, you're well aware of the need for transport within an airport complex. Gatwick are going in for a luxury system - unman ned vehicles.

However, these won't be the sort of unmanned buses that sit stationary by the kerbside defying all timetables and raising the blood pressure. Built by Westinghouse (couldn't a British firm do it?) the system will comprise two fully automatic buses, each operating on its own track connecting the main terminal to the new satellite building

Each bus will carry 80 passengers, mainly standing although some seats will be provided for the elderly, infirm or panic-stricken. Doors will open and shut automatically and pre-recorded message will advise passengers to mind the doors and hold tight. No passenger should have to wait more than 90 seconds for a lift.

Although it's an American system, $45 \%$ of the work will be done by UK industry. Work has already begun on the new satellite project, which is due for completion in 1982.

## Sitting Comfy?

How do you rate the ride comfort of your daily commuter train? Perhaps the number of coffee spills per mile or the number of times you're woken from pleasant slumbers.

Well, the ride comfort on the new Advanced Passenger Train should be improved, thanks to the Jacobmeter. This interesting little instrument (named after the BR engineer who developed the concept) measures vertical and horizontal accelerations separately and displays calculated root mean square values according to criteria in ride comfort curves derived from the ISO and motion sickness data. The integration period can be set to either 10 or 60 seconds.
The Jacobmeter is currently being used in commissioning trials on the prototype Advanced Passenger Train. It may later be used as a tool for general use throughout British Rail. So, fellow commuters, it looks like chuff-chuff comfort may be a bit better by the time we take out a mortgage on our next season ticket.

The Jacobmeter is made to a BR design by Kemo Ltd, 9-12 Goodwood Parade, Elmers End, Beckenham, Kent BR3 3QZ.


## Romane Electronics

## LOW POWER SCHOTTKY TTL EX STOCK

We are holding substantial stocks of the Devices listed below. All orders, large and small, will be dealt with in strict rotation. Please add $15 \%$ V.A.T. to all orders plus 30p for P\&P. Export orders no VAT but postage at cost air/surface. Prompt delivery on all orders.

| Device | Price | 74LS38 | 39p | 74LS 132 | 70p | 74LS 197 | 120 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 74LS00 | 13 p | 74LS40 | 23p | 74LS 136 | 45p | 74LS221 | 110p |
| 74LS01 | 14p | 741547 | $80 p$ | 74LS 138 | 75p | 74LS244 | 250p |
| .74LSO2 | 13 p | 74LS48 | 130 p | 74LS 139 | 80p | 74LS245 | 260p |
| 74LS03 | 14p | 74LS49 | 130p | 74LS 151 | 65p | 74LS247 | 150p |
| 74LS04 | $15 p$ | 74LS73 | 40p | 74LS153 | 65p | 74LS 248 | 150p |
| 74LS05 | 25p | 74LS 74 | 40p | 74LS 155 | $96 p$ | 74LS249 | 90p |
| 74LS08 | 30p | 74LS75 | 38p | 74LS 156 | $96 p$ | 74LS251 | 100p |
| 74LS09 | 30p | 74LS 76 | 38p | 74LS 157 | 65p | 74LS 273 | 200p |
| 74LS 10 | 16p | 74LS 78 | 43p | 74LS 158 | 83 p | 74LS279 | 85p |
| 74LS 11 | 23p | 74LS83 | 120p | 74LS 160 | 118p | 74LS 283 | 92p |
| 74LS 12 | 25p | 74LS85 | 120p | 74LS 161 | 100p | 74LS290 | 92p |
| 74LS 13 | 36p | 74LS86 | 40p | 74LS 162 | 130p | 74LS293 | 100p |
| 74LS 14 | 75p | 74LS90 | 50p | 74LS 163 | 130p | 74LS298 | 100p |
| 74LS 15 | 25p | 74LS93 | 90p | 74LS 164 | 100p | 74LS352 | 170p |
| 74LS20 | $17 p$ | 74LS95 | 110p | 74LS 173 | 90p | 74LS353 | 170p |
| 74LS21 | 24p | 74LS107 | 40p | 74LS174 | $90 p$ | 74LS365 | 95p |
| 74LS22 | 25p | 74LS 109 | 50p | 74LS 175 | 92p | 74LS366 | 95p |
| 74LS26 | 35p | 74LS112 | 50p | 74LS 190 | 120p | 74LS367 | 95p |
| 74 LS 27 | 25p | 74LS 113 | 50p | 74LS 191 | 120p | 74LS368 | 95p |
| 74LS28 | 40p | 74LS 114 | 50p | 74LS 192 | 120 p | 74LS374 | 160p |
| 74LS30 | 19p | 74LS 123 | 80p | 74LS 193 | $110 p$ | 74LS386 | 50p |
| 741532 | 27p | 74LS 125 | 40p | 74LS 195 | 110 p | 74LS670 | 200p |
| 74LS37 | 32p | 74LS 126 | 40p | 74LS196 | 100p |  | 200p |

 I.C. TEST CLIPS $10 \%$ Discount for $25+$ clips, $15 \%$ Discount for $100+$ $8 \mathrm{Pin} \mathbf{£ 4 . 5 0} 14 \mathrm{Pin} \mathbf{£ 2 . 7 3} 16 \mathrm{Pin} \mathbf{£ 2 . 8 8} 18 \mathrm{Pin} \mathbf{£ 6 . 0 6}$ 20 Pin $£ 7.0022$ Pin $\mathbf{£ 7 . 4 3} 24$ Pin $£ 8.4128$ Pin $£ 9.24$ 36 Pin $£ 12.0940$ Pin $£ 12.73$
SUPERSTRIP BREADBOARDS 840 solderless plug-in tie points. Accom modates up to nine 14 Pin DIPs. Price £ 10.07 with $10 \%$ Discount for $10+$ supersirips and 15\% Discount for 25 +
POWERACE PROTOTYPING LABS Two Superstrip Breadboards plus power supplies
POWERACE $1015-15 \mathrm{VDC}$ supply @ 600mA plus $0-15 \mathrm{~V}$ meter. Price £68.55.
POWERACE $102+5$ VDC supply @ 1 A plus 3 logic indicators and pulse detector, 2 logic switches, 4 data switches, clock generator and one-shot Price $£ 92.75$
POWERACE 103 + 5VDC supply@ 750 mA plus + 15VDC @ 250 mA and $-15 \mathrm{VDC} @ 250 \mathrm{~mA}$. Also meter (15-0-15V). 2 logic indicators, 2 logic switches and 2 data switches. Price £99.80

## VERO PRODUCTS

Vero Wiring Pen
$2 \times$ Spare Spools
Spot Face Cutters
Veroblock Bread boards

| 276p | $2.5^{\prime \prime} \times 5^{\prime \prime}$ | 62p |
| :---: | :---: | :---: |
| 276p 95p | $2.5{ }^{\prime \prime} \times 3^{\prime} 75^{\prime \prime}$ | 53p |
| 93p | $2.5^{\prime \prime} \times 17^{\prime \prime}$ | $186 p$ |
| 325p | $3.75{ }^{\prime \prime} \times 5^{\prime \prime}$ | 69p |

## MEMORIES

2114 500p
TMS 2516 KK EPROM. Single 5V Supply $£ 27.00$
76477 Sound generator drip $210 p$
LIGHTEMITTING DIODES

|  | $0.122^{\prime \prime}$ | Price |  | $0.2^{\prime \prime}$ | Price |
| :--- | :--- | ---: | :--- | :---: | ---: |
| RED | TIL209 | $\mathbf{1 3 p}$ | RED | TIL220 | $\mathbf{1 5 p}$ |
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All orders, large and small, will be dealt with IN STRICT ROTATION. Please add $15 \%$ V.A.T. to all orders plus 30p for P\&P (£1 P\&P for Poweraces). Export orders no V.A.T. but postage at cost air / surface. Prompt delivery on all orders. A full range of Breadboards, I.C. test clips, ribbon cable assembles available (mostly ex-stock). Please seno large S.A. E, for catalogue and price lists.


## SOS (Save

## Our Servos)

Radio-control fans remember that sinking feeling in your stomach as you watched your R/C model fall out of the sky, unable to do anything about it. Bet it was a shock, especially if your model was a yacht.
Chromatronics have just announced the introduction of an electronic fail-safe for radio modellers to minimise the danger of a model going out of control in the event of interference or loss of signal. Interference from what? Who said Citizen's Band (or is it Banned)?

The system will cope with co-channel interference from another R/C transmitter or CB (I promise I won't mention it again), total or partial transmitter or receiver failure and the model moving out of range. If your model tips the scales at 5 kg or more, a fail-safe device is obligatory under CAA regulations.

Unlike earlier simple devices, the PPIM-4CH works by two level threshold detection on all four receiver outputs. So, all primary control functions can be protected from severe
glitches from whatever source The unit is used to set up to four control servos in preset safe positions during a catastrophe. So, if the world should end, your Sopwith or Starfighter will still be zooming around the blue yonder until it runs out of four star, thanks to Chromatronics.

The unit works with any three wire positive pulse servo and has individual preset controls for each servo and variable fault detection thresholds. Cutin time is only 0.1 seconds. The PP1M-4CH is connected between the receiver and servos and works with either AM or FM systems on the 27 MHz UHF band or any other operational frequencies. It is small $(62 \times 42 \times 23 \mathrm{~mm})$ and lightweight, packed in a robust plastic capsule. It comes with four input leads and four output leads already fitted, but you have to fit the appropriate plugs and sockets for your equipment.
For only $£ 14.95$ (including VAT), this electronic fail-safe device sounds like remarkably good value, considering the cost of replacing a crashed model. The PPIM-4CH is available from Chromatronics, Coachworks House, River Way, Harlow, Essex.

## New <br> Neosid

Neosid, a name well known in professional and consumer electronics, has recently established a new outlet for the amateur constructor and small user.

The new Small Order Catalo-
gue covers a broad cross sec tion of the company's products - ferrite beads, screw cores, rods, $E, I$ and $U$ cores and coil assemblies, plastic formers and trimming tools.

Send a stamped, addressed envelope for the Small Orders Catalogue to Neosid Small Orders, PO Box 86, Welwyn Garden City, Herts AL7 IAS.


## Please add 30p p\&p \& VAT

Government, Colleges, etc. Orders accepted


## ILP MODULES 15-240 WATTS

We are now stockists for these world famous fully guaranteed (2 years guarantee on all e ane now stockists for these world famous

HY5 Preamp. 500 mV RMS ¢4.75; HY120 Power Amp 60W RMS/8
 HY50 Amplifier 25 W RMS/8Q E7.25;


POWER SUPPLIES
PSU36 - Drives $2 \times$ HY30s $\ldots \mathrm{E} 6.38$ PSU50 - Drives $2 \times \mathrm{HY} 50 \mathrm{~s}$ … $£ 8.18$ PSU70 - Drives $2 \times \mathrm{H} 120 \mathrm{~s} \ldots \mathrm{E}$.... $£ 13.70$ PSU90 one HY200 PSU $1802 \times$ HY200 or one HY400

OHIO SUPERBOARD II
Only £188.00
Yes, we are now selling this popular single board
microcomputer at the giveaway price of E18B..OO Oue microcomputer at the giveaway price of $£ 1818.00$ Due
to the recent devevuation of US Doltar against $\&$ Sterting.
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should Mrs. Thatcher $\&$ Co. decide to devalue the Pound. Supertoaard II is suppliied fully assembled and tested to British TV specitication. Atso included at no extra cost 4 manuals and a Casselte with programmes,
Requires $+5 V$ at $3 A$ and a video Monitor or $T V$ with $R F$ Convertor to be up and running. (Oata sheet supplied We can also supply the RF Convertor and Power Supply in Kit form or ready built). 8K Microsofi BASIC in ROM 4 K Static RAM - on
BOARD expandable to 8 KK . Full 53 Key Keyboard with Upper/Lower Case \& User programmability and a tot more. See it for yourself. Continuous demonstration on
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Specially designed antractive fibreglass case NDU Unit

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| can be mounted on ti) |  |
| Power Supply Kit with RF Modulator | $\mathbf{£ 2 6 . 0 0}$ |
| Extra 4 K of RAM | $\mathbf{£ 3 . 7 5}$ |
|  | $\mathbf{\$ 3 8 . 5 0}$ | Extra 4 K of RAM


| SWITCHEE | SLIDE 250V: <br> 14 DPDT 14p |  |
| :---: | :---: | :---: |
|  |  |  |
| SPST 28p | 1A DPDT /over | 150 |
| DPST 34p | $1 / 24$ DPDT | 13p |
| DPDT 38p | 4 pote 2-way | 240 |
| 4 pole on/off 54p | PUSH EUTTON Spring loeded |  |
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| SUP-MIN TOGGLE |  |  |
| SP changeover 5 | SPDT $/$ /over | 65p |
| SPST on/otf 54p | DPDT 6 Tag | 85p |
| SPST biased ${ }^{85 p}$ | miniature |  |
| DPDT 6 lags 70p | Non Locking |  |
| DPDT dentre off 79p | Push to Make | $15 p$ |
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6-0.6V 9.0 .9 V 12-0.12V


## ETI Projects: Parts available

 for: Click EliminatorAmbuash; Gui-
tar Effect Unit: Audio Display; DMile Amp. phile Amp, System. Train Sonstem. Tr Sentroller $5 p$ for list. ズ


## Core

Blimey
Walmore Electronics have in troduced a new range of trans former cores for switched mode power supplies. The range includes itoroidal cores and three sizes of $E$ core.

The cores are made from iron powder, the advantage over ferrite being that high saturation flux density is maintained to unit operating temperatures Because of this, inductors can also often be reduced in size. The use of a distributed gap enables a reduction to be made in the external flux leakage. Other core materials need large lumped air gaps to maintain incremental inductance at high DC bias levels.

Also from Walmore are three new ranges of power Darlington transistors in TO-92 miniature plastic packages. The devices are Unitrode types U2TA506/508/510 and feature a current gain of 500 at a collector current of 3A and a saturation voltage of only 1 V 5 at 3 V . They are planar NPN devices, each consisting of a two transistor circuit on a single monolithic clip which also includes an integral bias resistor and protective diode. Each type is specified according to its maximum collector-emitter voltage -60 V for the $506,80 \mathrm{~V}$ for the 508 and 120 V for the 510 . These new Darlingtons are ideally suited to pulse power applications in power supplies, printers, solid state relays, etc.

The new ranges of cores and power Darlingtons are available from Walmore Electronics, 11-15 Betterton Street, Drury Lane, London WC2H 9BS.

## Oops OOPS Microwave Oven Leakage Detector

This has proved to be a very popular project. We've had a lot of inquiries about the diode used. If you're having trouble finding one, you can get it from Brian J. Reed, 161 St. John's Hill, Battersea, London SW11 1TQ. Mr Reed's catalogue is 75p + a large stamped (27p) addressed envelope. If you just want one diode, send $30 p+a$ 10 p s.a.e.

## Motor Speed Controller

Let's see if we can get it right this time. The unmarked resistor above Q 2 on the overlay on page 49 should be marked R11. Now, if we take the overlay labelling on page 49 as correct, let's alter the circuit diagram to agree with it. The first column shows the published resistor labelling and the second column shows the corrected version

$$
\begin{array}{ll}
\text { R10 } & \text { R11 } \\
\text { R11 } & \text { R13 } \\
\text { R13 } & \text { R14 } \\
\text { R14 } & \text { R15 }
\end{array}
$$

Also, a resistor has been omit ted from the circuit diagram R10, a 2 M 2 resistor, should be shown between pin 2 of IC4 and the OV line ie in parallel with C5. These changes in resistor labelling also apply to the parts list.

## Typical Reader Competition

We're interested to know what our readers think of us. We don't usually hear what readers think of themselves, though. This is what Mr. O'Donohoe figures a typical ETI reader looks like. Wot - no suspenders and stockings? You've shattered my illusions, Mr. O'Donohoe. But you've started something. Let's see what the rest of you think (or hope) the typical ETI reader looks like. If we get any photos that are printable, there could be a few free $T$ shirts in the post.

# Tecknowledgey for sale. <br> DIY Hi-Fi will never seem the same again. Ambit's Mark Ill tuner system is electrically and visually superior to all others Some options available, but the illustrated version with reference series modules $£ 149.00+£ 22.35$ VAT With Hyperfi Series module <br>  <br> lesign of all parts <br> Ime/frequency display State of the art performance with lachities for updat ystems. <br> Deviation level calibrator All ustal tuner features 

| Digital Dorchester All Band Broadcast Tuner: LW/MW/SW/SW/SW/FM stereo |  |
| :---: | :---: |
| A multiband superhet tuner, constructed using a single IC for RF/IF processing - but with all features you would expect of designs of far greater complexity. The FM section uses a three section (air gang) tuned FET tunerhead, with ceramic IF filters and |  |
|  |  |
| AM employs a double balanced mixer input stage, with mechanical IF filters . plus a BFO and MOSFET product detector for CW/SSB reception. Styled in matehing unit 10 |  |
| Mark III FM only tuner, employing the same degree of care in mechanical design to enable easy construction. MW/LW reception via a ferrite rod antenna. |  |
|  |  |
| mplete with digital frequency readout/clock-timer hardwa |  |
| Complete with MA1023 clock/timer module with dial scale |  |
|  |  |
|  |  |


| LW/MW F/I LCD Digital Freguency Display - July PW feattire |  |
| :---: | :---: |
| Update your old radio, or build this into a new design. |  |
| Or use it as a servicing aid - this low power unit with |  |
| LCD display reads direct frequency in $\mathrm{k} / \mathrm{H}_{2} / \mathrm{MHz}$, or |  |
| with usual AM/FM IF offsets for received frequency. |  |
| Low power LCD means no RFI - 15.20 mA at 9v even |  |
| with the divide by 100 prescalar. FM resolution is |  |
| $100 \mathrm{kHz}, ~ A M ~ 1 \mathrm{kHz}$. Sensitivities better than 10 m |  | $100 \mathrm{kHz}, \mathrm{AM} 1 \mathrm{kHz}$. Sensitivities better than 10 mV Ambit stocks and distributes a wide range of frequency counter $\angle S /$ for all types of OFM MSL 2318 dive MSL 2318 divide by ten or hundred prescalar IC. The DFMI combined counter for AM, FM professional case structure. Please deduct

Maintaining our professional approach to
home constructor kits, we offer the pulse home constructor kits, we offer the pulse induction 'Sandbanks'. Now with inject-
ion molded casing for greatly improved enviromental sealing. $£ 37.00+£ 5.55$ vat VHF MONITOR RX WITH PLESSEY IC but using standard (fundx9) crystals, and transformers. Coil sets from our standard transformers. Coll sets from our standard Complete module kit $£ 31.25+£ 4.68$ vat

| MICROMARKET |  |  | OSTS overilow: |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6800P | 650p | 8212 | 230p | 2102 | 170p |
| 6820P | 600 p | 8216 | 195p | 2112 | 340 p |
| 6850P | 275p | 8224 | 350p | 2513 | 754 p |
| 6810 | 400p | 8228 | 478p | 4027 | 578p |
| 6852 | 365p | 8251 | 625p | 2114 | 1000p |
| 8080 | 630p | 8255 | 540p | +15\% | VAT |

## RADIO and AUDIO MODULES : Consistently the most advanced

5801 Oual gate stage varicap tuning, all with oscillator autput $\begin{array}{lll}5803 & \text { Dual gate MOSFET RF stages, bipolar mixer } & £ 17.45+2.61 \mathrm{VAT} \\ 5804\end{array}$ 5 and utira wide range tuning system
EF5402 4 stage varicap tuner with TDA 1062 and LO
FOR $30-200 \mathrm{MHz}$
$\frac{\text { FOR FM IFs at } 10.7 \mathrm{MHz}}{7030} \frac{\mathrm{MHz}}{\operatorname{single} 6 \mathrm{pos}}$
single 6 pole linear phase fiter JF with HA1137f10 $95+1$ CaVAI 7130 two 6 pole linear phase filtar IF with CA3189£ $£ 16.25+2.44$ VAT EECODERS for MPX (STEREO)
$\frac{\text { LARSHOLT FM TUNE RSETS }}{7252} \frac{\text { MOSFET front en }}{\text { MOS }}$
7252 MOSFET front end combined with CA3089 IF $£ 26.50+3.97 \mathrm{VAT}$
7252 JFET front end, combined with IF and decoder $£ 26.50+3.97 \mathrm{VAT}$ EM/AM tuning synthesiser, see details elsewhere in th is advertisement

| COMPONENTS FOR RADIO/COMMUNICATIONS/AUDIO/TV etc. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| As usual, Ambit brings you the latest and best, a small selection of which is shown in this advertisement. The Ambit catalogues contain information on most of the devices mentioned here - and an order for the new part three will ensure you stay up with latest developments. Data photocopying service described in pricelist info. |  |  |  |  |  |  |  |  |  |
| RADIO ICs for FM va |  |  | SL1600 series |  |  | Audio preamps val |  |  |  |
| CA3089E | 1.94 | 29 | SL1610 | 1.60 | 24 | LM381N | 1.81 |  |  |
| CA3189E | 2.45 | 37 | SL1611 | 1.60 | 24 | LM382N | 1.65 | 25 |  |
| A1137W | 2.20 | 33 | SL1612 | 1.60 | 24 | KB4436 | 2.5 | 38 |  |
| HA11225 | 2.20 | 33 | SL1613 | 1.89 | 28 | KB4438 | 2.22 | 33 |  |
| SN76660N | 0.75 | 11 | SL1620 | 2.17 | 33 | TDA 1028 | 3.50 | 53 |  |
| RADIO ICs | or AM | FM | SL1621 | 2.17 | 33 | TDA1029 | 3.50 | 53 |  |
| TOA1090 | 3.35 | 50 | SL1623 | 2.44 | 37 | TDA1074 | 3.7 | 56 |  |
| TDA1083 | 1.95 | 29 | SL 624 | 3.28 | 49 | Audio power |  |  |  |
| TDA1220 | 1.40 | 21 | SL1625 | 2.17 | 33 | TBA820M | 0.75 | 11 |  |
| IF AMPLIF | RS |  | SL1626 | 2.44 | 37 | teas 10 A | 1.09 | 16 |  |
| KB4406 | 0.50 | 07 | SL1630 | 1.62 | 24 | LM380N | 1.00 | 15 |  |
| MC1350 | 1.20 | 18 | SL1640 | 1.89 | 28 | ULN2283 | 1.00 | 15 |  |
| see comms ic | also |  | SL1641 | 1.89 | 28 | TDA2002 | 1.95 | 29 |  |
| COMNIUN | Atio |  | SL6640 |  | 41 | HA1370 | 2.99 |  |  |
| KB4412 | 2.55 | 38 |  |  | 48 | FETs. MOSFETs, bipolars. |  |  |  |
| KB4413 | 2.75 | 41 |  |  |  |  |  |  |  |  |
| SD6000 | 3.75 | 56 |  |  |  | and variou |  |  |  |

## assurance that all devices are very best first quality commercial types. Sources LPSN TIL is presently in great demand, so please check by phone before ordering.

ML:Standard RND LP Sthotthy

|  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Current news: A PCB for the Mullard DC tone and volume control system is now available $£ 3+0.45$ VAT. HMOS PA modules for $60-100 \mathrm{~W}$ - kit $£ 14+£ 2.10 \mathrm{VAT}$, heatsink $£ 4.10+0.61$
 Terms. AT, which is usually shown as a separate amount. Overseas customers welcome. please allow forder. Minimum credit invoice for account customers $£ 10.00$. Please follow instructions on Catalogues: Ambit. Part 145 p. Part 2500 90p pair. TOKO Euro shortform 20p. Micrometals toroid cores 40 p. All inc. PP etc. Full data service described in pricelist supplements. Hours/phone: We are open from 9 mm .7 pm for phone calls. Caliers from 10 am to 7 pm . Administrative enquines 9 am to 4.30 pm please (not Saturdays). Saturday service 10 am to 6 m

| CMOS SALE | THE MOST VERSATILE LIOUID CRYSTAL DISPLAY |
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| Compare our make, quality and prices. All |  |
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| CD4015BE RCA | LCD106 $6.45 \quad 5.50 \quad 5.25$ |
| $\begin{array}{ll}\text { CD40278E } & \text { RCA } \\ \text { CD4028BE } & \text { RCA }\end{array}$ |  |
| CD40538E $\quad$ RCA 60 p |  |
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| DSPLAY LEBS AT LOWES PRICES | "LO BAT" indicator. Ideal for DMMs, DPMs, |
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| NOW THE CHIPS ARE DOWN | Just look at the features. Ultra low power con- |
| Due to butk purchase, we are able to offer unbeatable prices on INTERSIL chips. Compare our prices and see how much you save | sumption, high contrast ratio-wide <br> viewing |
|  ${ }^{1-24}$ $25+$ $100+$ <br> ICL7106CPL $6.50^{2}$ 6.25 5.95 <br> ICL7107CPL 6.25 5.95 5.75 | angle-rapid response- proven sealing |
| ICL8038CCPD | techniques-superior |
| 7216A | MTBF-reflective |
| $18.75 \quad 17.75$ | aluminium foil. Over |
| $\begin{array}{lll}16.75 & 14.75 & 12.25\end{array}$ | 300,000 alread |
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| Now you can operate $\{20$ Volts. American equipment from 240 Voltsl Only $£ 9.95$ complete with British type plug. | $\begin{array}{lll}86800 & 7.00 & 2114 \text { low p } \\ \text { Z.80 } & \mathbf{8 . 5 0} & 300 \text { NS }\end{array}$ |
|  |  |
|  | Z-80A 10.50 |
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|  |  |
| New from National LM3914. Drives 10LED directly for making bar graphs, audio |  |
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spec. units as sold by some of our com pentors. These are factory prime, firs STOCKII 8) EACH 100077 6p EACH 1,000077 Texas Instruments
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Happy

## Families

The latest offspring of RCA Solid State is a new family of dual variable operation amplifiers. The CA3280G Series combines two operational transconductance amplifiers in a single package.

The two amps are independent, differential input types and the output is a current proportional to the differential input voltage and the transconductance, which is programmable via a separate input terminal.

All characteristics of the two amplifiers are matched to within $5 \%$. Peak output current can be as high as 650 uA at a bias current of 500 uA and operating bandwidth is 9 MHz at a bias current of 1 mA

Applications include voltagecontrolled amplifiers, voltage controlled filters, voltage controlled oscillators, function generators, etc. The devices are supplied in 16 lead DIL plastic packages and are available with operating temperature ranges of -55 to $+125^{\circ} \mathrm{C}(\mathrm{CA} 3280 \mathrm{AG})$ and 0 to $+70^{\circ} \mathrm{C}$ (CA3280) from RCA Solid State - Europe Sunbury on Thames, Middlesex TW16 7HW


## Display <br> Giants

New from Fairchild are a range of large area liquid crystal displays, suitable for clock and digital panel meter purposes

There are two versions - $31 / 2$ digit (FLB 3513) and 4 digit (FLB 4013), both featuring 0.5 inch digits. The inclusion of a colon allows the displays to be
used in timekeeping applica tions. Decimal point and polarity signs are included for digital panel meter use.

Power requirements? - 5 V typical with a maximum drive current requirement, at 3 V with all segments on, of 5 uA .

You can find out more about these LCDs from Fairchild Camera \& Instrument (UK) Ltd, 230 High Street, Potters Bar, Herts EN6 5BU

# Quartz Melody Multi－Alarm Chrono For 1980 Try this 34 Function <br> \section*{Count－down Timer} <br>  

Can be used for a host of applica tions from boiling an egg to warning you your parking meter is expired． The timer is presettable to 23 hours 59 mins .00 secs in 1 min ．steps and counts down in 1 sec ．steps．It operates quite independently of the other counters and the watch can be in any other mode whilst it is being used．
At the preset time the musical tone will sound for 1 minute

## Alarm

8.50

The alarm can be set at 1 minute intervals to any time within the 24 hour period．
A clear．firm musical tone sounds for 1 minute at the appointed time．An automatic roll－over to the normal time is a feature after the alarm has been read．A clear indicator displays whether the alarm is set or not．

## Time Zone <br> © <br> 2.0818

The time zone enables you to tell the time in two places at once．It can be useful on holiday or business trips．Just programme the second time zone and it will be per－ manently recorded for your easy reference．

## Chronograph <br> 

This watch incorporates a sophisticated and very accurate stop／start counter which has many appli－ cations in sporting events and timing for recordings
etc．
Mode 1：Is the normal stop－watch mode．Stop－ Mode 1：
Mode 2：The lap timer enables first and second past the post times to be recorded．The display is frozen but the counter continues to count．
Mode 3：Longer timing intervals，such as journey times，can be recorded whilst the watch is reading its normal time，or the count－down is being used The counter counts to 1 hour in $1 / 100 \mathrm{sec}$ ．steps in all its modes


A very impressive new watch at a superbly low price from Metac．This super slim watch is only 7 mm thick（that＇s thinner than most mechanical tick－tocks），but its micro－ processor heart packs 34 different features．

In addition to those listed on the left the watch can display the day of the week in French or German or English（just select the one that suits you）．－－

It has fast and slow setting rates for the counter and the alarm as well as the normal time setting．

There are 7 display indicators， 6 digits and a back light for night viewing．The 5 working modes are independent of each other，and the watch can be operated in all 5 modes at once．

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# FUNCTION GENERATOR 

## A wide range ( $1 \mathrm{~Hz}-100 \mathrm{kHz}$ ) sine/triangle and

 square wave generator with built-in analogue frequency meter.
## A really nice piece of test gear from ETI.



The main characteristic of a function generator is that it produces a basic fixed-amplitude waveform other than a sine wave, from which a fixed-amplitude sine wave is then synthesised. The main advantage of this technique is that the resulting output waveforms of the generator are immune to amplitude 'bounce' when they are swept through their frequency ranges, thus enabling amplifier or filter gain/ frequency tests, etc. to be carried out very rapidly. The only disadvantage of the technique is that the resulting sine wave has an inherently higher degree of distortion than is obtainable from good 'Wien bridge' and similar 'tuned' oscillator circuits.

The ETI function generator produces three output waveforms (sine, triangle and square) and covers the frequency range 1 Hz to 100 kHz in five decade ranges. The sine wave output typically produces a THD (total
harmonic distortion) value of only $0.5 \%$, has a maximum amplitude of 2 volts rms, and is ideal for general purpose testing. The triangle output has a typical linearity of $1 \%$, a maximum peak-to-peak amplitude of 5 V 6 and is ideal for cross-over distortion testing of class-AB amplifiers, etc. The square wave output is positive-going, has a maximum peak amplitude of 8 volts, has typical rise and fall times of less than 200 nS and is ideal for testing digital circuits. All ouput waveforms of the generator are DC coupled, with the sine and triangle waveforms swinging symmetrically about the zero volts line.

Our function generator incorporates a number of additional, very attractive features. It has a built-in analogue frequency meter, for ease of calibration. It has two output terminals, each with its own attenuator network. A sine or triangle waveform is available from one output and a

## PARTS LIST

| RESISTORS All $11 / 4 \mathrm{~W}, 5 \%$ |  |
| :---: | :---: |
| R1,2,14 10 | 10k |
| 73,17 1 | 1k0 |
| R4,5,10 | 2k2 |
| R6,7,9 22 | 22k |
| 78 | 470 R |
| R11,18 100 | 100R |
| R12,13,15, 4 | 47R |
| 16 |  |
| R19 1 | 11R |
| POTENTIOMETERS |  |
| 2V1,2 | 47 k cermet multiturn $\left(3 / 4^{\prime \prime}\right)$ |
| 2V3 | 22 k cermet multiturn $\left(3 / 4^{\prime \prime}\right)$ |
| 7 V 41 | 470 cermet multiturn ( $3 / 4^{\prime \prime}$ ) |
| 2V5 | 4 k 7 cermet multiturn $\left(3 / 4^{\prime \prime}\right)$ |
| 2V6 | -00k lin dual gang |
| 9V7-10 | -0k |
| RV11 | : OOk cermet multi- |
|  | turn (3/4") |
| RV12,13 | 7k0 lin |
| CAPACITORS |  |
| C1,2 | 100 u 25 V electrolytic |
| c3,9 | 150 p polystyrene |
| C4,13 | 10 n polyester |
| C5,10,14,11 | 100 n polyester |
| C6,15 | 140 polycarbonate |
| c7, 8 | 10 u 25 V electrolytic |
| C12 | in0 polystyrene |
| SEMICONDUCTORS |  |
| C1 | XR2206CP |
| C2 | NE555 |
| 01,3 | BC182L |
| 02,4 | BC212L |
| D1-3 | 1 N4148 |
| ZD1 | BZY885V6 |
| MISCELLANEOUS |  |
| SW1 | DPDT (PCB type) |
|  | toggle. |
| SW/2 | 4 pole 5 way wafer switch assembly and 2 |
|  | PCB wafers (2 pole 6 way) |
| SW3 | DPDT toggle |
| SW4 | 1 pole 3 way rotary |
|  | switch |
| 2 BNC connectors, 2 PP7 batteries, case to suit, PCB. |  |

square wave is available from the other. The square wave output is available at all times, is synchionous with the sine/triangle waveform and can thus be used to provide synchronisation signals to an oscilloscope timebase during sine wave testing, etc. The unit is battery powered, for maximum user convenience.

A fine unusual feature is that the frequency ranges are alternately contra-connected, so that to increase frequency you turn the 'fine' control clockwise on one range, anticlockwise on the next range and clockwise on the next range, etc. This facility enables the frequency to be swept through several decades very rapidly when testing the frequency response of amplifiers and filters, etc. As we said in the introduction, this is a really nice piece of test gear.

## Construction

Most of the circuit is built up on a single large PCB. Various points should be noted before starting construction. First, note that 4 -pole 5 way range switch SW1 is mounted directly on the PCB and in fact is a 6 -way PCB type (see Buylines) with one of the 'ways' unused. The next point to note is that the $\mathrm{C} 6(1 \mathrm{uO})$ and C 7 (10u) main timing capacitors are non-electrolytic types. We obtained ours from Electrovalue.


## SPECIFICATION

Frequency range
Output waveforms:
Sine: distortion (typical)
Triangle: linearity (typical)
Square: rise/fall times (typical) Waveform stability (typical)

Maximum output levels (with 9-0-9 V supply).

Supply
Total current consumption

1 Hz to 100 kHz in 5 decade ranges.
$0.5 \%$ at 1 kHz .
$1 \%$ at 1 kHz .
less than 200 nS .
$.002 \%$ per ${ }^{\circ} \mathrm{C}$.
$.01 \% / \mathrm{V}$ supply sensitivity.
Sine $=2 \mathrm{~V}$ rms.
Triangle $=5 \mathrm{~V} 6 \mathrm{pk}-\mathrm{pk}$.
Square $=8 \mathrm{~V}$ peak.
Two 9 V batteries.
30 mA typical.


At this stage access to a distortion meter is desirable, so that RV3 and RV4 can be trimmed for minimum distortion. With care, a thd figure of $0.5 \%$ can be obtained. In the absence of a distortion meter, the simple twin-T 1 kHz filter of Fig. 2 can be used in conjunction with the oscilloscope or with a milivoltmeter to set the generator for minimum distortion at 1 kHz . The procedure is to apply the sine wave output of the generator to the input of the filter at about 1 volt rms at approximately 1 kHz and take the output of the filter to the input of the 'scope or millivoltmeter. Next, adjust the generator frequency and R4 of the filter to give minimum output indication and, finally, adjust RV3 and RV4 of the generator to reduce the output indication of the filter to the minimum possible value. At final balance, the output of the filter corresponds to approximately $0.1 \%$ thd per $m V$ rms of indicated reading, ie if the indicator shows a reading of 5 mV rms , the thd of the generator approximates $0.5 \%$. Now retrim OFFSET control RV5.. The sine wave calibration procedure is then complete.
(3). Set the unit to TRIANGLE mode. Monitor the waveform on the 'scope and adjust RV2 for a pk-pk amplitude of 5 V 6 .
(4). Check that the unit is functional on all ranges, in all waveform modes.
(5). Switch the unit to its top frequency range, set the output frequency to 100 kHz and adjust RV7 for full scale deflection. If necessary, slightly reduce the value of C3 so that 100 kHz can be obtained.
(6). Repeat the frequency calibration procedure on all ranges, using the
appropriate pre-set (RV8 to RV11), noting that a very 'Jerky' reading will be obtained on the lowest ( 1 Hz to 10 Hz ) range. The calibration procedure is then complete, and the unit is ready for use.
A final point to note is that we used 10-turn cermets for all pre-sets on our prototype unit. A slight touch of luxury, this. You can get away with ordinary presets, if you prefer, but in this case you'll have to make slight modifications to the PCB.

Actual construction on the PCB is fairly straightforward, but take extra care to observe the polarities of all electrolytics and all semiconductor devices. When construction is complete, fit the board into a suitable case and complete the interwiring to the remaining switches, -pots and to the moving coil meter. The unit is then ready for testing and calibration.

## CALIBRATION

Calibration of the unit is fairly tricky and requires access to an oscilloscope and some kind of frequency reference (you can use the 'scope timebase as a reference if it is known to be reasonably accurate). The calibration procedure is as follows:
(1). Set the unit to the SINE mode. Set' the attenuator controls for maximum output. Set the frequency controls for approximately 1 kHz on the $1-10 \mathrm{kHz}$ range. Set all pre-set pots at mid value. Switch the unit on, and use a scope to check that some kind of waveform is available (the waveform may be pretty awful at this stage). Check that the frequency is variable via RV6.
(2). Reset RV6 for a 1 kHz output and adjust RV1 for a pk-pk amplitude of about 5V6. Adjust RV4 for a 'passable' sine wave, and then readjust RV1 for 5V6. Now alternately adjust RV4 for MINIMUM DISTOR-


Rear view of the front panel controls.
HOW IT WORKS
There is not an enormous amount we can say here, since most of the work of the say here, since most of the work of the a special function generator chip that produces a square wave output from pin 11 and a sine or triangle wave from pin 2. The purity of the sine wave can be trimmed via RV3 and RV4 and the maximum amplitude can be preset via RV1. The maximum triangle amplitude can be preset wia RV2 and both waveforms can be offset via RV5. The sine/triangle waveforms are made available to the outside world via buffer amplifier Q3-Q4 and the associated attenuator network. The square wave is made available, in positive-going RV12.

The operating frequency of the gen-
TION and RV3 for best SYMMETRY, occasionally readjusting RV1 for 5V6 pk-pk until a good sine wave is produced. Adjust RV5 for zero offset (so that the output waveform swings symmetrically about the zero volts level) and retrim RV3 and RV4 for a good sine wave.
erator is variable via timing capacitors C3 to C7 and via resistor network R2-RV6. The frequency is monitored on a simple analogue frequency meter that is designed
around 555 timer IC2, which is triggered via the square wave output of the Q1-Q2 buffer amplifier.

The entire circuit is powered from two 9 voli batteries, and the circuit consumes a typical total current of about 30 mA .


Fig. 2 This simple twin-T filter can be used to set the generator for minimum distortion


Fig 3 Range switch wafer pin-out.

## BUYLINES

The 10 u (C7) capacitor can be purchased from Electrovalue Ltd. All other components used in *the function generator should be readily available from major mail vorder companies that advertise in this issue.






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# VFET APPLICATIONS 

## Is the VMOS power FET a really important device, or a mere flash-in-the-pan? In the next few pages Project Editor Ray Marston appraises the device.

MAGINE a power transistor that has virtually infinite input impedance, 'beta', and power gain which has a bandwidth extending from $D C$ to 600 MHz and which can switch 1 A on or off in a mere four nanoseconds. Imagine also that this device is immune to secondary breakdown and has a negative temperature coefficient that minimises thermal runaway problems and enables devices to be directly parallelled for increased power handling capability.

The above 'miracle' device already exists, and is readly avaibale at fairly low cost. It is known as a VMOS Power FET. VMOS Power FETs were first introduced by Siliconix. in 1976. At that time they were hailed as "the most revolutionary semiconductor in decades - likely to eliminate bipolars within five years". Now, three years on, VMOS still hasn't made a great impact on the industrial or consumer market.

## What Is It?

The term 'VMOS power FET' stands for 'Vertical structured Metal-Oxide Silicon power Field-Effect Transistor'. Conventioal MOSFETs use the form of construction shown in Figure 1, in which current flows Horizontally from source to drain through the channel, which is induced on the top surface of the silicon substrate. This form of structure results in low current densities, poor heat dissipation capabilities, very limited power handling capacity and relatively large chip capacitance.


Fig 1. Cross Section of a conventional FET.

VMOS power FETs, on the other hand, use the form of structure shown in Figure 2, in which current flows vertically from source to drain. This structure results in high current densities, low saturation resistance, excellent heat dissipation and power handling capabilities, low chip capacitance and excellent wide band performance.

VMOS power FET technology has been pioneered by Siliconix, who currently produce a variety of such devices


Fig 2. Cross Section of a VMOS power FET.
with maximum continuous drain current ratings ranging from a modest 500 mA up to a hefty 12 A 5 , and with maximum drain-to-source voltage ratings ranging from 35 to 90 V . All the products in their present VMOS range are n-channel enhancement-mode devices, in which the source-to-drain path is normally closed but can be opened by applying a positive gate voltage. The gate has a near-infinite input impedance.

A major defect of the existing VMOS technology is that it is not readily compatible with the production of $p$-channel devices. This factor greatly reduces the devices' attractions in audio power amplifier applications, where calss-AB output stages are currently in vogue.

A more detailed account of VMOS construction and operation theory is given in the July' 78 edition of ETI.

## Characteristics

Figure 3 shows typical output and saturation characteristics of the type VN67AF VMOS power FET. Note the following points:

1 The device passes negligible drain current until the gate voltage reaches a threshold value of approximately 1 volt The drain current then increases non-linearly as the gate is varied up to approximately 4 volts, at which point the drain current has a value of about 400 mA . The device, in fact, has square law transfer characteritics below 400 mA .

2 The device has a highly linear transfer characteristic above $400 \mathrm{~mA}(4 \mathrm{~V}$ on the gate) and thus offers great potential as a low-distortion class-A power amplifier.

3 The drain current is controlled almost entirely by the gate voltage and is almost independent of the drain voltage so long as the device is not saturated. A point not shown in the diagram is that, for a given value of gate voltage, the


Fig 3. Output and saturation characteristics of the VN67AF VMOS power FET.
drain current has a negative temperature coefficient of about $0.7 \%$ per ${ }^{\circ} \mathrm{C}$ so that the drain current decreases as temperature rises. This characteristic gives a fair degree of protection against thermal runaway.

4 When the device is saturated (switched fully on) the drain-to-source path acts as an almost pure resistance with a value controlled by the gate voltage. The resistance value is typically $2 R O$ when 10 volts are on the gate, and $10 R$ when 2 volts are on the gate. The off resistance of the device is in the order of megohms. These characteristics make the device highly suitable for use as a low-distortion high-speed analogue power switch.

Figure 4 shows the circuit symbol and the case outline of the VN67AF, which incorporates a 15 V input-protection


Fig 4. Symbol and outline of the VN67AF.
Zener and Fig. 5 summarises the static and dynamic characteristics of the device. Points to note here are that the input (gate-to-source) signal must not be allowed to exceed the 15 V Zenerating of the device and that the device has a typical dynamic input capacitanceof only 50 p : this capacitance dictates the dynamic input impedance of the device. The static input impedace is of the order of a million megohms.

## Digital Circuits

VMOS is delightfully easy to use in digital switching and amplifier applications. Figure 6 shows the basic connections. The load is wired between the drain and the positive supply rail and the digital input signal is fed directly to the gate. Switch-off occurs when the input goes below the gate threshold value (typically 1 V 2 ). The drain on current is determined by the peak amplitutde of the gate signal, as shown in Figure 3, unless saturation occurs. In most digital applications the on current should be chosen to ensure saturation.


Fig 5. Summary of the static and dynamic characteristics of the VN67AF.

The static input impedance of VMOS is virtually infinite, so zero drive power is required to maintain the VN67AF in the on or off state. Drive power is, however, required to switch the device from one state to the other. This power is absorbed in charging or discharging the 50 p input capacitance of the VN67AF

Fig 6. Basic VMOS digital switch or amplifier.


The rise and fall times of the output of the circuit are determined by the source impedance of the input signal, the input capacitance and forward transconductance of the VMOS device and the value of $R_{L}$. If $R_{L}$ is large compared to $R_{S}$ the VN67AF gives rise and fall times of roughly 0.11 nS per ohm of $R_{S}$ resistance. Thus, a $100 R$ source impedance gives an 11 nS rise or fall time.

If $R_{L}$ is not large compared to $R_{S}$ these times may be considerably changed. A point to note when driving the -VN67Af is that it's input Zener forward and reverse ratings must never be exceeded. Also, because of the very high frequency response of VMOS, the device is prone to unwanted oscillations if circuitry is improerly designed. Gate leads should be kept short, or be protected with a ferrite bead or small resistor in series with the gate.

VMOS can be interfaced directly with the output of CMOS, as shown in Figure 7. Rise and fall times of about 60 nS can be expected, due to the limited output currents available from a single CMOS gate. Rise and fall times can be reduced by driving the VMOS from a number of CMOS gates in parallel, as shown in Figure 8, or by using a special high-current driver.

VMOS can be interfaced with TTL jeither standard or LS type) by using a pull-up resistor on the TTL output, as shown in Figure 9. The 5 volt TTL output of this circuit is


Fig 7. Method of interfacing VMOS with CMOS!


Fig 8. VMOS switching times can be reduced by driving with a number of gates in parallel. Typical $R_{T}=25 \mathbf{n S}$.
sufficient to drive 600 mA through a single VN67AF Higher currents can be obtained either by wiring a levet shifter between the TTL output and the VN67AF input, or by wiring a number of VN67AFs in parallel as shown in Figure 10.

## Analogue Circuits

VMOS power FETs can be used with relative ease in either the common source or common drain (voltage follower) modes. The voltage gain in the common source mode is equal to the product of RL and the devices gm or forward transductance. In the case of the VN67AF, the device gives a voltage gain of 0.25 per ohm of $R_{L}$ value, i.e., a gain of 4.0 with $16 R$ load, or a gain of 25 with a 100 R load. The voltage gain in the common drain mode is slightly less than unity.


Fig 9. VMOS can be driven from the output of TTL if a pull-up resistor (R1) is used.


Fig 10. Boosting the output of Fig 9 by driving three VN67AF in paraliel.

Fig. 11 shows three alternative basic ways of biasing the VMOS power FET for common source operation. In most practical applications, the device will be biased into the linear mode, with the drain at a quiescent value of approximately $V_{\text {supply }} / 2$, so that maximal signal swings can be accommodated between the cut-off and saturation clipping levels.

In Fig 11a the gate is biased at a supposedly fixed level by potential divider R1-R2. The input impedance of the circuit is (at low frequencies) equal to the parallel values of R1 and R2. Defects of this simple biasing arrangement are that the voltage biasing level varies with the supply voltage, and the drain current biasing level depends on the characteristics of the individual VN67AF that is used in the circuit. An advantage of the circuit is that the quiescent drain voltage can be biased below that of the gate.

The alternative circuits of Figs. 11 b and 11 c can be used in cases where the quiescent drain voltage is greater than that of the gate. In Fig 11b, potential divider R1-R2 is fed from the drain of the VN67AF, and DC negative feedback makes the quiescent drain current substantially independent of variations in supply voltage and device characteristics. AC negative feedback also occurs, and reduces the effective input impedance to a value approximating the parallel values of R1 and R2 divided by the voltage gain ( $g m \times R$ ) of the circuit.

Figure 11 c is a simple modification of the Fig 11 b circuit, and results in increased input impedance. R3 is wired


Fig 11. Methods of bias for common source VMOS operation.

between the gate of the VN67AF and the junction of R1-R2. R3 does not effect the biasing of the circuit, but if its value is large relative to that of $R 1$ and $R 2$ it raises the input relative to that of R1 and R2 it raises the input impedance to a value approximating that of R3. If the source impedance of the input signal is low relative to R3, the $A C$ negative feedback effects of the circuit are virtually eliminated and the input impedance is further increased. If. in the Fig 11c circuit, the drain is likely to swing below the desired gate bias level under active conditions, a capacitor can be wired across R2 to preserve stable biasing conditions.

Fig. 2 shows methods of biasing VMOS power FETs for common drain operation. In Fig. 12 a the circuit is biased by a simple potential divider (R1-R2), and the source takes up a value a few volts below that of the gate. Because of the inherently high level of negative feedback of this configuration, the resulting bias (quiescent) source/drain current of the circuit is substantially independent of the characteristics of the individual VN67AF that is used. The input impedance of this circuit is equal to the parallel values of $R 1$ and R2.

Figures 12 b and 12 c show how the input impedance of the basic Fig 12a circuit can be increased. In Fig 12b, R3 is given a value that is large relative to R1 and R2, thereby raising the input impedance to a value approximating that of R3 without effecting the biasing of the circuit. In Fig 12c the value of R3, and thus the input impedance, is effectively increased by a factor of $1 /(1-A v)$ via bootstrap capacitor C2. Thus, if $R 3$ is 10 M and $A v$ is 0.95 , the input impedance is raised to 20 M . If $R 3$ is 1 MO and $A v$ is 0.99 , the input impedance is raised to 100 M . C2 must have the


Fig 12. Bias for common drain VMOS operation methods.
impedance that is low relative to R1 and R2 over the required bandwidth of the amplifier.

## Practical Circuits

The best way to get to know VMOS power FETs is to experiment with them in a few practical circuits. With this in mi..ıa, Figs. 13 and 22 show a few simple designs that you can play with. All of these circuits are based on the VN67AF, which typically costs less than a pound in one-off quantities.


Fig 13. Touch switch.


Fig 14. Water switch.

Figs, 13 and 14 couldn't be simpler. When the contacts/probes are open, zero volts are on the gate of the VN67AF and the device passes zero current. When a resistance (zero to tens of megohms) is placed across the contact/probes (by contrast with skin resistance, water, etc), a substantial gate voltage is developed by potential dividier action and the VN67AF passes a high drain current.


Fig 16. DC lamp dimmer.

Fig 15. Delay turn off switch.

In the Fig. 15 circuit, C1 charges rapidly via R1 when S1 is closed and discharges slowly via R2 when S1 is open Thus, the load activates as soon as S 1 is closed, but does not deactivate until some tens of seconds after S1 is released.

Figs. 16 to 18 are lamp control circuits. In Fig. 16 the drain current and lamp brightness is controlled via RV1. In

Fig 17. Soft-start analogue lamp switch.


Fig. 17 the lamp turns on slowly when the switch is closed as C1 charges up via R3, and turns off slowly when the switch is opened as C1 discharges via R3.

The Fig. 18 circuit is a highly efficient 'digital' lamp dimmer. The two 4011 gates are connected as an astable


Fig 18. Digital DC lamp dimmer.
multivibrator that has a mark/space ratio that is variable from 10:1 to $1: 10$ via RV1, and has it's output fed to the gate of the VN67AF, thereby enabling the 'mean' lamp


Fig 19. Warble-tone alarm (2 tone output).
brightness to be varied from virtually full-off to full-on.
Fig. 19 is an inexpensive but very impressive alarm-cell generator circuit that produces a police-like 'dee-dah' sound. The alarm can be turned on by closing PB1 or by feeding a 'high' voltage to the R1-R2 junction. The circuit is used with an 8RO speaker, and generates roughly 6 watts of output power.


Fig 20. Super simple class-A amplifier.
The Fig. 20 class-A power amplifier gives an incredibly impressive performance, but is very inefficient. The VN67AF must be mounted on a decent heat sink. Since the amplifier is used in the class-A mode, it produces a valve sound output. Because of the excellent linearity of the VN67AF, the apparent distortion of the amplifier is remarkably low. When used with 8 RO resistive load, the amplifier has a bandwidth that extends up to 10 MHz .

## The Appraisal

VMOS is undoubtedly a remarkable technology with many great advantages over conventional bipolar technology. Latest reports indicate that at least five major semiconductor companies other than Siliconix are now actively researching into or actually manufacturing VMOS power FETs, so that technology is clearly not just a 'flash in the pan'. Each of these companies is apparently developing it's own particular version of the technology and preliminary reports indicate that the Siliconix technology is still way ahead of the competition in most areas (switching speeds, device linearity, high voltage rating, etc.).

Siliconix are expected to announce a 400 volt 8 amp device, which can switch 8 amps in less than 100 nanoseconds, within the next few months. They already have a 65 volt 8 amp 100 watt device on the stocks that can give a 10 dB gain at 175 MHz .

The simple circuit of Fig. 21 makes an excellent radio control or CW transmitter output stage. The L1-C2 and L2-C3 values must be chosen to suit the required operating


Fig 21. 60 mW R /C or CW transmitter L1-C2 is tank circuit, C3-L2 is the artenna circuit.

Finally, Fig. 22 shows the basic circuit of a . 20-watt class-D audio power amplifer using a pair of VN67AF's. We hope to publish a practical version of this circuit in ETI in the near future, so keep your eyes open.


Fig 22. Besic circuit of a 20W clas-D switched-mode audio power amplifier. An ideal application for VMOS.

The only criticism that we've been able to make against the Siliconix VMOS power FET technology concerns the present total lack of p-channel devices. Our spies tell us, however, that Siliconix are already working on that problem, and will have it beaten within a year. If that is so, we reckon that the 1976 prediction that "VMOS may eliminate bipolars within five years" could still come true.

In the meantime, we at ETI are already 'sold' on VMOS, and plan to use a good deal of it in the coming year. We reckon that once you've started using it, you'll like it as much as we do.

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# Liven up your Ludo with the ETI Dinkydie. Throw away that Block of wood with dots on and bring your board games into the twentieth century. 



Fed up with shaking rattling and rolling that boring set of wooden dice? Need something to brighten up that game of which the kids have grown tired?

We've spent some time designing this little project - an example of just how difficult it can sometimes be to get something 'just right': As few components as possible, all the desirable features, no obscure parts and nice low price for the constructor.

Operation couldn't be simpler: To 'throw' the dice, touch two fingers across one set of screw heads seen either side of the front panel in the picture here. Your 'throw' then appears in a dice pattern on the LEDs behind the perspex.

To throw again, touch the pair of screw heads once more.

If you leave the dice 'un-thrown' for a few seconds, the display fades and the circuit switches itself off, drawing only a miniscule current in its quiescent
state.
Mount all the components on the. board, placing the LEDs last. These should be spaced off the board by about 3 mm so to ensure that they are the highest components. If the bolts are level no spacers are needed as they can be tightened just enough to hold the LEDs hard against the perspex. If you wish, a piece of block cardboard may be cut to cover the other components to obscure the board.

Once the board is assembled the battery clip and battery may be connected and the device tested. Once bolted in the nuts on the underside of the board should be quickly soldered to the pads to ensure good contact. To complete the assembly the bottom of the case can be screwed in, and the battery jammed in place with a small piece of foam rubber or styrofoam. (Use the bit ${ }^{4}$ the CMOS IC's came in perhaps). Finally, if you fear for the coffee table top, four adhesive rubber feet on the bottom would be a good idea?

ET

## BUYLINES

All the components used in the Dinkydie should be readily available from your favourite mail order supplier.

PARTS LIST

,-:


An LED sandwich - make sure the LED's are the highest components on the PCB.


Fig.2. Component overlay.
Fig. 3. Details of the hardware.

## HOW IT WORKS

This device' simulates a single dice 'die" * electronically by illuminating LEDs in a đie face pattermafter you have held

- your fingers on two sensor contacts for a period to 'throw' the dice. The
? device operates by counting pulses
* from a free running astable multivibrator, hence the number finallydisplayed is defined by the duration of the touch.

As the quiescent current is well below luA, no power switch is used.

Initially, Q1 and Q2 are biased off. The astable multivibration, formed by ICla and b , is disabled and the display driver Q6 is also off. When the sensor
contacts are touched, a small leakage current flows into the base of Q1/Q2 which form a Darlington pair, and the collectors go high.
This has two effects. Firstly, the astable multivibrator made up of two nand gates (IC1a and b) is enabled and clocks the counter, IC2, at about 1 kHz . Secondly, C2 is discharged via D1, in preparation for initiating the display delay period. The duration of the touch defines the number which results, but the clock is sufficiently fast to prevent any form of cheating.

When the touch contacts are released the clock stops and the inputs
of 1 Cld are pulled low. The gate is connected as an inverter, and the output thus sources current to Q7 which enables the display by pulling the LED cathodes low. The contents of counter IC2 are thus displayed in die-face format by the LEDs, When C2 recharges to above the threshold of IC1d via Q5 the display fades. Quiescent current is well below luA, so no power switch is required. The "all ones" state (i.e. 1111) is detected by the carry output and causes 1001 to be loaded by "the parallel load input, IC1c does the required logic inversion for the parallel load function.


# RAIN ALARM 

## Don't get wet feet, don your wellies and come and see the Rain in Spain fall

 Mainly on the ETI Rain Alarm. - By George, we've got it!Have you ever been tied up with other jobs, such as polishing the furniture, doing the washing up, etc while your washing is out drying on the line? Then, just as you are finishing your present chore you look out of the window and see that the heavens have opened on your nearly dry washing. Well, this happens virtually every Monday (being washing day) to the ETI Project Team and we were just about getting fed up with it . . .
.so we had a conference!
It became apparent, after we had looked in the piggybank and found we didn't have enough for a second-hand tumble dryer, that we should do something constructive (for a change). We decided that even we couldn't design a machine to stop it raining on Mondays (though officially we won't admit it) so the alternative was the ETI Rain Alarm, which, at the vaguest hint of rain, will ring out loud and clear so that the pots and pans can be dropped while we run outside and fetch in the washing from the line.


## HOW IT WORKS



Fig. 1. Circuit diagram.

The heart of the rain alarm lies around the thyristor SCR 1 which switches the bell or buzzer on. Normally, in D.C. mode a thyristor is switched on by a small gate current. It will not switch off however, until the voltage applied across the whole device reduces to near zero, at which point it will remain off until the voltage at the gate increases enough to switch it on again.

When used with a make and break device such as a bell or buzzer the applied voltage momentarily decreases to zero at whatever frequency the bell or buzzer is operating at. This will in turn, switch off the SCR. This gives us a non-latching D.C. switch, operated by applying a small D.C. voltage to its gate.

Ql provides switching action in that as the resistance across the probes decreases from infinity to a comparitively low value (ie. as rain falls on them) then the voltage across R3 increases from near zero to above the threshold voltage necessary to switch SCRI on.

## PARTS LIST



Fig. 2. Component overlay.

Of course detecting rain to keep your washing dry needn't be its only function. Anywhere a device to detect the presence of water is required, then the Rain Alarm will do it. It takes only minimal current when in standby mode so can quite happily be left on for long periods without significantly battery wastage.

## Construction

As the whole rain alarm only contains
seven components, including the on/ off switch, it fits very neatly onto a small PCB only about 1 inch by $1 \frac{1}{2}$ inches (or 25 mm by 40 mm if you have already been metricated by the vet). In fact, the $41 / 2$ volt bell battery is by far the biggest item in the project.

The construction of the circuit on our PC layout will present no difficulties - just take care that the semiconductors are inserted cor-

## BUYLINES

All parts should be easily obtainables from your local stockists. However: any of the mail order firms advertising in ETI should be able to help. if you are stuck.
rectly. Use a printed circuit mounting switch for SW1 if you can obtain one - it makes a neater job, but if not, any SPST switch will do.

The probes in our prototype were constructed from a small piece of commercially available stripboard, the two leads soldered to alternate copperstrips, providing an interleaving of the copper. Any small drop of water landing on the copper side of the stripboard will automatically bridge at least two of the strips, therefore operating the alarm.

And, now that you have finished the ETI Rain Alarm, you can go - in the words of the immortal and legendary Gene Kelly (Ray's hero) Ringing in the Rain.

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# AUDIOPHILE 

# Having spent a month coiled up with a lump of Coral (well each to his own) Ron Harris presents a review of the new MC81 pick up. 

IThas been a month of musical evenings. The television has remained off, the soldering iron cold, the wargames unplayed and the books unopened. Meanwhile the power amp glows red in the night and my neighbours have taken to wearing ear defenders and shaking their fists at my approach.

Ah, the fools, they know not the delights they scorn. .
You see. I have been playing a lot of records this month, all due to this MC81 device I mentioned when last you read Audiophile. They should put a warning on the side of the box - "This cartridge can seriously damage your social life."

At first glance it is a most unimpressive blob of black plastic, but that in itself brought to mind something someone once told me about not covering judges with books - or something like that anyway.

## Book Covers

Being of the moving coil strain, the Coral MC81 needs a head amp, or pre-pre-amp as some people with stutters persist in calling them, to increase the voltage level to around 3 mV in order that a normal RIAA input can process the signal.

The unit designed to work with the MC81 in this manner is the H300, which possesses a few unusual points itself. There are head amps on the market which will work with the majority of cartridges, but none are totally satisfactory with all. The best of these is possibly the Sony HA55, (which is mains powered). The H 300 has a variable input impedance facility which suggests that it too is aimed this way and it will be interesting to see if it gains acceptance on the end of cantilevers other than the MC81. I confess I did not audition it any other way myself, but I will get around to that. . . .

Back to the cartridge. It weighs a puny 5 g , but is surprisingly large for this weight as you can see from the photos. Set up in the SME III the Coral tracked most material happily at 1.8 g , and took everything (just!) at 2.0 g . The damping option on the SME should be exercised, although the fluid may need thinning for best results.

One good point about the cartirdge body itself is that the top is sensibly large and flat - allowing for a large contact area with the headshell and thus good mechanical coupling between the two. At least it would do if the SME headshell was long enough!


## Coiled Up

Initially I had the MC81 operating through a HA55, while the H300 was getting over its birth pains and into this cruel world. In this configuration the cartridge worked well, but I was less than happy with the lowest bass registers. The mid-range, however, came as a revelation. It was crystal clear and sharp and 'opened out' relative to the other cartridges I was comparing with it (Coral's own 777EX and the Entré 1). Treble quality was all I'd hoped for, being both accurate and extended without either emphasising surface noise or wielding that steel edge with which some moving coils cut through the music. I was impressed!

I was further beguiled once I had the MC81 and H300 operating together, a combination which went a long way to taking the ground from under my objections to the bass. It was never that the unit lacked bass at all, but that I had a feeling that the level was down upon what I would have expected.


Fig. 1. Frequency response of the MC81. If you can't see it that's because it's so straight it's hidden behind the graph paper. What happened to all those nice dips and peaks reviewers could have such fun commenting on?

Bass quality was immaculate. Each instrument, bass guitar, drum, double bass or whatever was clearly and precisely identified and distinguishable. If you think that's easy, try it with your own cartridge - now - can you absolutely distinguish the different notes from a bass guitar for instance? Is the bass drum in full possession of it's transients?

As regards this aspect the Coral has the best bass I've heard and I'm not prepared to trade that quality back in for a bit more quantity of a less than equal pedigree.

## Timely Decision

Running through an evening of the best recorded LPs I had soon convinced me that any initial unease I had experienced was groundless. Direct comparison between the $\vee 15 \mathrm{IV}$, the Entre an FR1 and the MC 91 led to others being employed in ever shorter bursts and, before the day was through, left alone.

In each comparison there were differences. The FR1 had a 'sweeter' mid-range but not the incredible detail. The Shure had for more bass signal present but not the attack and the Entré just didn't measure up at all - with either or any head amp.

In fact it was probably the V15 IV's slight bass emphasis that had led me up the garden path in the first place.

## Talking Of Heads

Consider the H 300 for a moment. The input of this device has variable gain and variable capacitance facility. Loading can be switched from 5000p to 20000p in steps of 5 n . Gain can be switched up from $23-30 \mathrm{~dB}$.

Both these are controlled by DIL switch banks on the front of the PCB, but can only be accessed by removing the front panel entirely. That same panel contains the power switch and 'charge' light.

The H300 takes its electrons from a Ni-Cad source, and when switched off the batteries go on trickle charge. It takes (say Videotone) twelve hours to deplete the storage - I didn't fancy staying awake long enough to get an accurate figure - and forty eight hours to replace the power once used up. The charge light (LED) comes on when the box is switched off, a changeover relay diverts the input from a separate mains adaptor to the charger. This same relay operates as a switch-on delay system to prevent a 'thump' which is potentially dangerous to amp, ears and cones.

Unfortunately this relay doesn't seem to work on switch off and I got a loud 'whoop' if I did things in the wrong order! It could all lead to a flat cell and no music tonight, Josephine.

All in all, even weighing the advantages of reduced hum and lower source resistance (hence less RF interference etc), I think 1 prefer a plain mains supply with the extra costs that infers.

Still the H300 system works, and works well. The head amp sounds very fine indeed, and on audition proved indistinguishable from the Sony HA55 at a fraction of that unit's cost.

Full marks for circuit design and final performance Videotone but the grumble on supply you'll have to live with - it's an odd solution albeit one that works.

## System Round- Up

Taken together the MC81/H300 system is an impressive and exciting new pickup system. The cartridge is well-nigh excellent and does not entail a second mortage on the


Above: the H300 sat sitting between the MC81 in SMEdressing and an ACl it fed. Small is it not?
mortage to afford it, like some Oriental Offerings I could name (It costs about $£ 90$ in the shops).

The H300 sounds very healthy indeed; but has that quirky PSU arrangement. This should give no trouble but does not make life as "thought-free" as it could. (Cost circa £60).

I would heartily recommend anyone interested in a new cartridge to head for an MC81 with open ear, and try and get a good listen.

If Felicity Kendal was interested, I'm sure I could find SOMEONE willing to extend the hospitality of his hi-fi for an evening or two (thousand!).

## A Gold Ring To It?

The point on the right has a point to it. A very strange shaped point-but a point nonetheless, a Van den Hul point in fact. After many months of trial and tribulation Goldring have fitted said sharp bit to a cantilever for their new G900IGC pick-up cartridge.

To all things under heaven there is a season, eh?
Welcome to the pickup season. After the Coral cometh the IGC and Io, music was bountiful upon the ears of Man and he heard that it was good.
The new G900 is claimed to exhibit greatly reduced distortion when compared to either a conventional ellipital point or the Shibata variation upon the theme. This is claimed to be due to the straight line of contact between stylus and groove and the smaller minor radius of the Van den Hul design.

The finish and presentation of the cartridge is superb, but up to now I haven't had a chance to listen to my sample at all. So once again its next month folks . .


Above: the point of Goldring's new G900IGC is easily seen.


## Tuning In JVC

Interesting looking new tuner from JVC, the TX5, features their award winning Phase Tracking Loop detector stage. Naturally PTL is claimed to improve everything from AM objection to sliced bread - and judging by the details I've seen could be Wonderloaf are in for a hard time.

The TX5 also has two patented ideas incorporated - a 'quieting slope' control which acts as a sort of signal sensitive noise reducer, and a new tuning system. The price is around $£ 250$.

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| LM308T05 | 100p | NE555 | 25p | TBA540 | 220p | XR4151 | 350p |
| LM308DIL | 100p | NE556 | 70p | TBA5500 | 250p | XR4202 | 150p |
| LM309K | 140p | NE562B | 420p | TBA560C | 240p | XR4212 | 150p |
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| LM311T05 | 150p | NE567 | 170p | TBA 700 | 200p | ZN414 | 95p |
| LM317K | 350p | SAD 1024 | 1400p | TBA7200 | 240p | ZN1034E | 200p |
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# HUM 

## FILTER

## Got a hum problem that's making your hi-fi distinctly lo-fi?

Our natty notch filter cuts the moronic mains monotone down to size.

The magnetic field around the transformer in the power amplifier can couple to the preamp or tape deck. Also, the location of nearby 240 V mains wiring can cause problems that can be very difficult to overcome. In theory, if the equipment and leads have been properly shielded and earthed this problem shouldn't exist. In practice it's a very different story.

This project aims at overcoming some of the problems of mains induced hum by using a notch filter at the hum frequency of 50 Hz . At this frequency any signal present will be attenuated. At frequencies either side of the notch the response should return to the unattenuated input level.

The ' O ', or Quality Factor, of a tuned circuit - which the RC network in this circuit forms, determines, the bandwidth, or narrowness, of the amplitude response of the circuit (see the diagram). As this circuit forms a notch filter, the Q of the circuit determines the narrowness of the notch.

With a high-Q notch the frequency response of the circuit will dip suddenly around the notch frequency. Frequencies a little either side of the notch centre frequency will be little affected. If the O is low, frequencies some way either side of the notch frequency will be attenuated. The actual attenuation at the notch frequency is greater with a high $-O$ circuit than with a low- $Q$ circuit.

High -0 circuits have the disadvantage that slight changes in component values, due to temperature changes etc, will affect the centre frequency. Tuning of the circuit to frequency is also quite critical. Lower-Q circuits do not suffer


so much from this disadvantage.
The design Q chosen for this project was a compromise between the constraints of critical tuning and drift effect and good attenuation at the notch with little affect on nearby frequencies. Peak attenuation at the notch centre frequency of 50 Hz is around 80 dB while attenuation of only 3 dB is obtained at 40 Hz and 58 Hz . There is some audible effect on the bass response of a system, but this is minimal.

## Construction

Mount the resistors and capacitors on the board first. Be sure the orientation of the tantalum capacitors is correct. These are polarized and can only be installed one way round. Next, install the preset pot. Finally, solder the transistor in place.

The circuit is run from a single nine volt battery. The current consumption of the prototype was 200 uA so the battery life should be good for several months. If it is found that battery life is not long enough a power switch could be fitted.

The filter can be used almost anywhere in the amplification chain since its overload margin is very high (typically 8 V p-p). It should obviously be placed after the point where the hum is being picked up. If the hum is in the turntable and the magnetic phono input of the amplifier since the input impedance is 47 k shunted by 10 pF , which should suit most magnetic cartridges.

Once the filter is in place, the presets are adjusted so that the hum is brought to a minimum by adjusting each channel independantly.

## HOW IT WORKS

The circuit consists of a "Twin-T" notch filter formed by capacitors C3, C4 and C5 and resistors R3, R4, R8 and preset PR1.

The operation of the Twin-T requires that $C_{3}=C_{4}=C_{5}$
and $R_{3}+P R 1 \stackrel{2}{=} R_{4}=2 R_{8}$
These conditions must be met with reasonable accuracy if a good, deep notch is to be obtained. The preset corrects to a certain extent for errors due to component
mis-match and assumes that the notch can be adjusted to the exact frequency of the hum to be rejected.

The frequency of the notch is then given by
$\mathrm{f}=1$

$$
2 \pi R_{4} C_{4}
$$

The transistor is operating as an emitter follower, giving zero voltage gain, but providing feedback into the notch to increase the $Q$ to acceptable limits.


The finished PCB fitted to the front panel, with the battery on flying leads.


Fig.2. Component overlay.

## PARTS LIST

| Resistors all $11 / 4 \mathrm{~W}, 5 \%$ |  |  |
| :--- | :--- | :---: |
| R1,R101 | 68 k |  |
| R2,R102 | 27 k |  |
| R3,R103,8, |  |  |
| 108 | 22 k |  |
| R4,R104 | 47 k |  |
| R5,R6,R105, |  |  |
| R106 | 470 k |  |
| R7,R107 | 33 k |  |
| Capacitors |  |  |
| C1,C101 | 10 pf ceramic |  |
| C2,C102,6, |  |  |
| 106 | 1 l tantalum |  |
| C3,C4,C103, |  |  |
| C104 | 68 n polyester |  |
| C5,C105 | 150 n polyester |  |

Potentiometers
RV1,RV101 50 k min preset
Semiconductors
Q1,Q101 BC549, BC109
Miscellaneous
ETI 451 PCB, box to suit, 4 panel mounting.

Components for 100 Hz operation
$\begin{array}{ll}\text { R4,R104 } & 22 \mathrm{k} \\ \text { R8,R108 } & 10 \mathrm{k}\end{array}$
Replace R3 with wire link.

## BUYLINES

You shouldn't have any difficulty in getting hold of any of the components for this project. We haven't bothered to box our prototype. You can use anything from a plain aluminium box to a classy "wooden case whatever takes your fancy.

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This month Dave Raven, of Metac Electronics, has a bash at crystal gazing into the future of computers and delves into chip reliability.

Predicting the future in electronics is a regular feature of TV and the press with "Tomorrows World" and newspaper features on technology. People not involved in science probably have difficulty believing the forecasts since they are quite often so far outside what we already understand.

Home computers and Robotics are two areas which receive quite a lot of attention since they are predicted to be areas which will have major effects on the ways in which we work and live. At a recent symposium held in France by a computer manufacturer, experts assembled to discuss the future. It was predicted that there will be at least four major computer revolutions during the 1980s. The component processors revolution forecast for 1979/80 begins with the basic building blocks for computers and communication systems, large scale integration and very large scale integration of devices, hardware, intelligent machine products, people appliances, digital automation products, communications ICs and intelligent data communication satellite systems. All this resulting in components becoming the end product.

Phase two will begin 1981/83 with the Component Computer revolution. This will provide intelligent data management systems and communications subsystem components with the machine / computers becoming just components. Carrying on in 1983/85 we should have the component memory age. This kicks off with the basic building block for information systems, distributed memory, a system component revolutionising com-
munications, information appliances, a data base computer and knowledge based systems. This results in memory becoming components and offices becoming portable machines. Phase four brings the component systems revolution forecast for 1985/88. The component systems will further revolutionise our institutions leading to the end of the main frame computer and allow factories to become machines. The era will be the "system on a wafer technology", communications will substitute for travel and buildings and an information society will emerge. Computers become components and factories become machines. Computer evolution is increasing tenfold every decade and chip technology at $100 x$ / decade while innovation is going at 1000 x / decade.

## Robots for Robots

People amplifier appliances, the knowledge based system and robots. In the 1990s we can expect intelligent robots, androids and world linked robots. Also, would you believe worker/slave robots for robots. If you find a credibility gap emerging between yourself and the prophets of the future it may be of interest to read this extract from The Times of January 28th 1926 - "Members of the Royal Institution and other visitors to a laboratory in an upper room in Frith Street, Soho, on Tuesday, saw a demonstration of apparatus invented by Mr J. L. Baird. For the purpose of the demonstration the head of a ventriloquist's doll was

manipulated as the image to be transmitted through the human face was also reproduced, first on a receiver in the same room as the transmitter and then on a portable receiver in another room. The visitors were shown recognisable reception of the movement of the dummy head and a person speaking. The image transmitted was faint and often blurred, but substantiated a claim that through the 'televisor' as Mr Baird has named his apparatus, it is possible to transmit and reproduce instantly the details of movement and such things as the play of expression on the face.

The Cathode Ray tube was of course still only a suggestion made back in 1907 by Cambell Swinton in England and Boris Rosing in Russia. So far, though, this suggestion had produced no satisfactory system of television.

## Global Games

Electronic home entertainment equipment is largely imported into the UK from Japan and Hong Kong. Some items are made in Taiwan and South Korea. However, these two countries have stronger links with America. Several European firms have set up manufacturing in special export zones in India which have very attractive tax benefits. Both Philips and Rank Radio are in India, also many other companies have goods manufactured in the Far East with their own brand name on. Hong Kong is particularly strong in exporting to England due mainly to our colonial ties. Goods from Hong Kong have been much maligned over the years for low quality probably due to the cheap plastic toy image they are best known for. Early electronic products were of varying quality but since this new technology was not completely debugged it was not only Hong Kong that had problems (reference UK made TV games, calculators and electronic watches).

The high failure rate of electronic goods at the onset of production is nearly always caused by the chip. The low yields of TV game, calculator and watch chips is well documented but as usual the problems are eventually solved and the yield dramatically improves. Now with calculators, TV games and many watch chips the producer just cranks the handle and out they come by the bucketful.

## Nipon Word Box

Having referred to the possibility of an electronic dictionary last month it is not surprising that one has now appeared, such is the speed of development in electronics. Made in Japan this time by Sharp it will be going on sale next month.

It features 48 kilobytes of read-only meory together with logic and display control circuits. The liquid crystal display is in dot-matrix and this enables it to run for about 1,000 hours on three silver-oxide batteries.

The dictionary is for Japanese-English, EnglishJapanese and is intended primarily for Japanese people learning English. It has a central processing unit, two display-control chips and four 12-kilobyte ROMs encoded with a total of 2,500 English words, 300 English compounds and 5,000 Japanese words. Conjugations of English verbs are provided and the dictionary form can be called up from another tense at the push of a button. One further novel feature is a test key for checking the spelling of an English word with a reply of "good" or "wrong". It can also process incorrect or incomplete information. If a user tries to translate "speake" the display will respond with "speak?

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# INTERVAL TIMER 

## The ultimate in analogue - scale precision timers. This inexpensive wide-

 ranged relay-output unit spans 1 minute to 20 hours in three switchselected ranges and has a long term calibration accuracy better than $1 \%$.Electronic timer units have numerous home, hobby and engineering applications. They can be designed to have either analogue or digital "Time set" indicators or scales, on which the required timing period is initially set. Their relaycontact outputs can be used to control lamps, heaters, battery chargers, photographic enlargers etc.

Analogue-scale timer circuits have the advantage of low cost. Most previously published circuits of this type, however, have had very restricted maximum timing ranges (fifteen minutes or less) and have suffered from very poor long-term accuracy ( $20 \%$, or worse), due to the use of electrolytic timing capacitors and high-value timing resistors. Digitalscale timer circuits, on the other hand, have the advantage of high accuracy, but the disadvantage of relatively high cost.

Our new wide-range timer gives you the best of both worlds. It is an analogue-scale device that uses digital frequency division techniques to give a very wide timing range ( 1 minute to 20 hours), but uses a basic clock generator with non-electrolytic timing capacitors and consequently has a high degree of intrinsic longterm accuracy (better than $1 \%$ ). The timer is inexpensive, having a typical component cost (excluding the relay) of three or four pounds. The unit consumes zero current when it is in the 'standby' mode and thus does not need a separate on / off switch.

## CONSTRUCTION

All of the components of this unit (including the switches and the pot but excluding the relay) are assembTed on a single PCB and construction should present few problems. The three ICs should be mounted in suitable holders. The two switches are


PCB-mounting types (see components list). Note that we have made up the 1 2 value of C2 by wiring two capacitors in paraliel.

Take special care to relate the circuit diagram to the PCB overlay when connecting the relay and the power supply to the unit. The PCB is provded with five external connection points (one is rather sneakily hidden to the left of push-button PB1 on the overlay). Two of these connections go to the relay coil, one goes to supply zero, one goes to one of the relay contacts, and the remaining connection goes to the other relay contact and also to the supply positive. If the relay fails to latch on when you first give the unit a functional check, suspect an incorrect connection to the relay.

When construction is complete,
check that the unit is fully functional by momentarily closing PB1 and checking that the relay locks on for the timing period. You can then, if you wish, mount the unit in a suitable box and calibrate the RV1 scale against a clock on the two lowest timing ranges. The calibration of the top (100min-20 hours) timing range will be a factor of precisely ten above the middle ( $10 \mathrm{~min}-2$ hours; timing range.

## BUYLINES

There should be no problems in obtaining any of the components used in the timer.

All ICs are common types available from most components shops.


Fig. 1. Circuit diagram.


Fig. 2. Component overlay.

## PARTS LIST

RESISTORS All $1 / 4 W$, 5\%


Relay to suit.
Foil pattern.
NOTE: The value of C3, shown on the circuit diagram and component overlay, is 220 n .

HOW IT WORKS

In this circuit IC1 is a 555 timer, connected in the astable mode, and is used as a clock generator for the IC2 and IC3 frequency divider circuitry. IC2 is a 4017 decade divider. IC3: is a 4020 14-stage binary counter and in this particular application effectively divides the clock frequency by a factor of 8192 .

Power is applied to the circuit by momentarily closing PB1, at which moment the two counters are set to zero via C3 and the relay is driven on via Q1. As the relay turns on $\mathrm{it}^{2}$ 's contacts change over and maintain the power supply connections to the unit when PB1 is subsequently released. The IC1 astable starts to generate clock pulses as soon as power is applied.

On range 1 ( $1-12$ mins) the astable period is determined by C1 and R2RV1. The clock signal is divided down by IC3, which changes state on the arrival of the 8192nd pulse and turns the relay off and breaks the supply connections to the circuit. A similar action takes place on range 2 ( 10 mins - 2 hours), except that the clock frequency is determined by C 2 and R2-RV1.

On range 3 ( 100 mins to 20 hours) the clock frequency is again determined by C2 and R2-RV1, but in this case the frequency is divided by both IC2 and IC3, so that the relay turns off and breaks the supply connections on the arrival of the 81920th clock pulse.

The spare (RLA/2) set of RLA changeover contacts can be used to control external circuitry.


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ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1979

# BUY n๑лcom-2 NOW AND GETA FREE 16K RAMBOARD 

The lack of availability of the MK4118 RAMs has seriously delayed the launch of the Nascom 2, so we have decided to relaunch the product with an offer few will be able to refuse. The Nascom 2 will be supplied without the optional user 4118 s. Instead, we will supply a 16 K dynamic RAM board and the interconnect for the NASBUS absolutely FREE. This board allows further expansion to 32 K . Also, when the 4118 s become available, customers taking advantage of this offer can have the 8 K for just $£ 80$ (plus VAT).

Meanwhile, the empty sockets on the Nascom 2 can be filled with 2708 EPROMs allowing dedicated usage, now with 1.6 , or 32 K of extra RAM. All the other features of the Nascom 2 are available and these include :

## MICROPROCESSOR

Z80A 8 bit CPU which will run at 4 MHz but is selectable between $2 / 4 \mathrm{MHz}$.

## HARDWARE

$12^{\prime \prime} \times 8^{\prime \prime}$ PCB through hole plated, masked and screen printed. All bus lines are fully buffered on-board. PSU: r-12v, $5 v,-12 v,-5 v$.

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- 2K Monitor-NASSYS 1 (2K ROM) - 1 K Workspace/User RAM - 1 K Video RAM - 8 K Microsoft BASIC (MK 36000 ROM)


## INTERFACES

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# CHESS MACHINES SURVEY 

# With the Christmas of the chess computer rapidly approaching, lan Graham has been mating his way through the electronic playmates. 

Well, not much mating actually. I did manage to mate with a couple of the computerised com'panions on their lowest level.
As my chess isn't up to comparing the programs these machines use, I decided to play them off against one another. On their lowest level, the games were evenly matched. There were lots of stalemates. The Voice Chess Challenger managed to win all but one of its games. So, once, and once only, I heard the Voice Chess Challenger announce 'I lose'.

Perhaps more differences would have shown up at higher levels of play. However (and it's a big however), if all the games were playing at a ten minute
response time and if one assumes $\mathbf{2 5}$ moves each for black and white in each game, the E T.I chess computer league would have taken over three weeks of button-pushing, 24 hours a day, to play. No thank you.

Whether you're looking for a portable or desk top game, one complete with board or complete without one, or even a game that talks to you, there's one in our survey.

At the end of the survey you'll find a table bringing together the chess games, their suppliers, prices and their most important features. Prices are changing so often that, if you're thinking of buying a system, give a few of the suppliers a ring to confirm the latest prices.

## BORIS

Boris is probably the most infuriating of the computer opponents. It comments on your game. After considering your next move at length and finally plucking up enough courage to actually move the piece, you sit back with a smug grin on your face. Then the machine responds with 'RUBBISH', flashing on its display. It's enough to shake anyone's confidence in his game.

One welcome feature on both Boris and the Boris Diplomat is an easy way of checking where the pieces are on the board. There's nothing worse than manoeuvring into position to take the computer's Queen to find that it wasn't where you thought it was anyway. All the playmates will allow you to check the state of the board. Usually they assign a numerical value to each piece. The display shows the position of each square and the value of the piece on it. The two Boris's go one better. They display the square location and a stylised outline of the piece on it. The outlines are difficult to decipher at first, but soon become familiar.

A card board (a cardboard what? - No, a chess board made from card) is supplied with Boris, but I think it's totally unnecessary. If you can afford the $£ 165$ or so for Boris you're likely to have enough pennies left over for a decent board, if you haven't got one already.

Unlike the other games, which have a series of levels of play to choose from, Boris has a built-in 100 hour timer. The longer a response time you set on the timer, the longer Boris has to think about his/it's next move and the higher the level at which it plays.

Boris can be set to play either white or black. If you don't
like the situation you've played yourself into, you can change sides and make Boris take over your pieces.

You don't have to start every game from the beginning. Any problem or advanced stage of play can be set up on the board and entered rank by rank into Boris's memory. If Boris's response to one of your moves is rather disturbing, you can go back to where you were and try a different move.

As you can see, Boris comes in an attractive walnut case, with a compartment for the pieces and mains adaptor. $\quad$


## BORIS DIPLOMAT

My first impressions of the Boris Diplomat were less than favourable. I found that the flickering LED display was set at an awkward viewing angle. The keyboard, although large and clearly laid out, was unsatisfactory in use. It was absolutely rigid and, in the absence of sound effects, I had to glance at the display after each key pressing to ensure that the move had, in fact, been successfully entered. The chess board itself is even smaller than the keyboard and the pieces almost microscopic.

Having got all that off my chest, let me now say that I think Boris Diplomat is the perfect travelling chess computer. It's completely self-contained. You could quite happily sit on the BA shuttle to Glasgow or the 8.20 from Staines to Waterloo (the sardine special) with Boris Diplomat on your knee flashing it's gems at you.

The Diplomat shares the features of its big brother Boris. It doesn't have a series of levels. Instead it has an internal timer which can be set to give a response time of up to 100

hours. The longer you give the Diplomat to think, the higher the level of its play.

## COMMODORE CHESSMATE



Commodore's Chessmate is another newcomer to the market. This computerised mate didn't stir any great feelings either for or against it, on the whole. Although it employs the same control method as Chess Champion (separate keys/touch pads for the letter and number of each square location) I didn't find it at all awkward to use. On pressing each touch pad, a trill of tones signals
successful pressing. Another trill accompanies the appearance of Chessmate's response on the display.

My orily criticism is that there is no on/off switch for the sound effects. They do become a little irritating after a couple of games. The control panel is well laid out and more colourful than most.

There are eight levels of play and internal black and white 60 minute timers. Unlike all the other systems, which automatically reset to level one at the beginning of each new game, Chessmate resets to level 4 - its average level.

Chessmate copes quite happily with castling and en passant but it trusts you to observe the correct rules of castling. It will also check where the pieces are on the board, assigning a numerical value to each piece for identification. An illegal move is answered by a pair of flashing question marks on the display.

The computer companion's memory stores 32 familiar chess openings - from the Bishop's game to the NimzoIndian defence. It chooses one of these at random and tries to follow it for 16 moves, after which it has to think for itself.

## CHESS MATE

Not to be confused with Commodore's Chessmate, this Chess Mate isn't on the market yet. It's a battery (rechargeable)/mains game complete with fold out board. It will play at ten levels with average response times of from eight seconds to a day and a half. As with all the other games in our survey you can set up any problem on the board, so you don't have to start every game at the beginning.

The prototype I saw had one minor disadvantage. The board folds away very neatly to make a compact portable game. No, that's not the disadvantage. Unlike the Boris Diplomat which is self-contained with its set of on-board pieces, this game has no provision for carrying pieces. So, you have to carry around a little bag of pieces separately. However, there may be enough space in the folding board

to accommodate them when the game finally appears on the market.

## CHESS CHAMPION



You have to supply your own board when you play against the Champion. The good news is that the Champ's price has come down recently. ('Wonder if it's anything to do with the competition from the new Commodore Chessmate?) It has six levels of play - from an instant
response beginners level to the marathon 2-day computing time level (for correspondence chess).

As chess computers go, the Champion is a simple animal. It will only play black. Special moves need special treatment. The execution of the en passant move is a little puzzling. To take the Champion's black pawn en passant, you enter your white pawn's diagonal move. Now, you have to remove the black pawn from the board as seen by C.C., so you have to enter what appears to be an illegal sideways move to erase the C.C.'s pawn from it's memory. Castling? The Champ castles at the first opportunity.

You may have noticed that Chess Champion has more keys than most of it's brethren. Whereas one key usually serves for both the letter and number of a square's location eg C3, Chess Champion has a separate key for each. In my humble opinion, as a fully paid up member of the buttonpusher's union, the Champ would be a much more attractive proposition if it incorporated dual-function buttons or touch pads, perhaps with a button-press sound effect.

## CHESS CHALLENGERS

This latest addition to the Chess Challenger range is a bit special. It talks to you. It not only repeats every move, it tells you which piece it's moving and, if it's taking something, which piece it's taking. If you're stuck for a move, the Voice C.C. will even whisper a few suggestions in your shell-like. If you're a bit slow off the mark, the machine will remind you that you really ought to get a move on. It's no slow-coach itself, with response times of about half those of its predecessors.

There are nine levels of play plus an H level. If you select $H$, the chatty Challenger goes on thinking about it's next move until you tell it to stop. Checking the position of pieces on the board is simplicity itself. Each time you press the PV key, the computer-generated voice tells you which piece is on each square and whose piece it is. Positions are also shown on the display. Like Chess Challenger 10, the Voice C.C. comes with magnetic pieces. However, the usual Challenger touch keypad for a pushbutton pad with a click action.

For all the Micro-men (and women) in Readerland, the Voice Challenger uses 96 K of ROM for program and operational stages, 32 K bits of ROM for voice generation and 8 K bits of RAM for scratch pad and intermediate storage. The heart of the clever bits is a 280-A, 8-bit CPU. The unit is preprogrammed with 48 standard opening moves which it will select either randomly or under your command.

This is by far the most expensive chess computer on sale now, but it does have the most powerful program yet to appear on the market. If you're a serious club player, and a wealthy one at that, the Voice Chess Challenger is the most competent opponent (non-human, that is) you can face today.

I hoped this Challenger would make full use of it's voice and show a little character by blowing a raspberry when it won, but it just said 'check and mate', like a well programmed American dalek.


Chess Challenger 10 is a ten level opponent in an attractive package with an integral board and magnetic pieces. The calculator-style touch pad has a positive click action and sound effects. The manufacturers - Fidelity Electronics of Miami - have included a sound off switch. Whilst sound effects are useful to indicate successful key pressing, they can get rather monotonous and irritating after a while. The challenger 10 has one big advantage over its star successor, the voice box - it's around $£ 80$ cheaper - but its chess program is not as powerful or as fast.

Chess Challenger 7 was the first of the Challenger series to retail at under $£ 100$ and the last to appear before the Challenger acquired the power of speech.

It incorporates all the features of its predecessors plus a few extras. It will play against you (naturally), but it will also play against itself (if you're into spectator chess). You can change sides in mid-game and see how the Challenger gets out of the mess you got into. Not surprisingly, it looks very like its predecessor, the Challenger 10.

## ATARI CHESS CARTRIDGE

If you're buying a programmable TV games centre, or if Santa. Claus is bringing you one, you've probably got you eyes on the Atari Video Computer Systems. It's an expensive way of playing chess - over $£ 200$, including $£ 45$ just for the chess cartridge.

I thought it would be unfair to test the chess cartridge only. To give the system a fair and complete trial I decided to try out all the games cartridges I could get my hands on. There were air-sea battles, space wars, golf, basketball, breakout and many more cartridges. About a month later I thought I was sufficiently familiar with the system to try the chess cartridge. My eyes resumed their by now customary square shape as the board appeared on the screen.

My first criticism is that the board could be much larger. It sits in the middle of the screen with a large unused border round it. The pieces are controlled by a joystick with a push button. When the cursor is moved onto a piece, the piece is 'picked up' by pushing the button, then moved with the joystick and finally 'released' by pushing the button again. This sort of control method always seems at first to be a bit of a long-winded business, but soon becomes second nature. You have to decide for yourself whether it will interfere with your game.

There are eight levels of play. I assumed that level one was the simplest and level eight the most difficult. Silly me

Level eight is the simplest followed by levels one to seven.
The Atari Videocomputer system and chess cartridge are available from Videotime Products, who can supply the full range of games cartridges. The cartridges are mostly $£ 14.95$ each. The exceptions are chess at $£ 45$ and backgammon at $£ 34.50$.


|  | SUPPLIERS AND PRICES |  |  |  |  | GAME FEATURES |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | K | AJD | NIC | CGL | V | POWER | LEVELS | TNTEGRAL BOARD | CONTROLS | SOUND |
| BORIS | 169.95 | . 187.50 | - | - | - | M | T | NO | PB | No |
| BORIS DIPLOMAT | 94.50 | 94.77 | - | - | - | M/B | T | YES | TP | NO |
| CHESS CHALLENGER 7 | 98.50 | 99.65 | 99.95 | 99.95 | - | M | 7 | YES | TP | No |
| CHESS CHALLENGER 10 | 155.25 | 159.50 | 169.95 | 169.95 | - | M | 10 | YES | TP | NO |
| VOICE CHESS CHALLENGER | 229.95 | 245.00 | 249.95 | 249.95 | - | M | 10 | YES | PB | YES/S |
| CHESS CHAMPION | - | 54.50 | 54.95 | - | - | M | 6 | NO | PB | NO |
| COMMODORE CHESSMATE | 59.95 | - | 59.95 | - | - | M | 8 | No | TP | YES |
| CHESS MATE | 95.00 | - | - | - | - | M/B | 10 | YES | PB | YES/S |
| ATARI CHESS CARTRIDGE | 45.00 | - | - | - | 45.00 | M | 8 | YES | JB | YES |

Power:
M - mains
B - battery
Levels:
T- internal timer

Sound:
YES/S - sound effect may be switched off.
Controls: PB - push button
TP - touch pads
JP - joystick and push button

NIC - N.I.C. Models
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AJD - AJD Direct Supplies Ltd
102 Bellegrove Road
Welling
Kent DA16 3QD
Tel: 01-303 9145

V - Videotime Products
56 Queens Road
Basingstoke
Hants RG12 1REA
Tel: (0256) 56417
(0256) 26620

CGL - Computer Games Ltd
Spectrum House 48 Cambridge Road Barking
Essex
Tell: 01-591 5654
The list of suppliers is by no means exhaustive. Many of the High Street hi-fi stores will have a chess machine or two in the window. Prices vary a lot, so it's worth shopping around, especially with Christmas coming up and some prices coming down. STOP PRESS - Latest prices from Mountaindene: Commodore Chessmate - $£ 58.00$, Boris - £155.25, Boris Diplomat - $£ 90.00$, Challenger 10 $£ 155.25$, Challenger 7 - £88.00, Voice Challenger $£ 230.00$

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W'hite, noise can be simply described as a signal containing a full spectrum of quite randomly generated frequencies or tones, all with randomly determined amplitudes, but which have equal mean power when averaged over a reasonable unit of time. The basic sound of white noise resembles that of hissing steam, but this sound can be greatly modified, to give a variety of special sound effects (such as wind, waves, surf, jet roar, etc), by passing it through low-pass or narrow-band filters.

Most of the white noise generator circuits that have been published in the electronics press in recent years have been analogue designs. They have taken the relatively low-level white noise outputs of selected 'leaky' Zener diodes or of special (and expensive) 'noise' diodes and then amplified these signals to a level suitable for general use. A major problem with these circuits has been that they

have given highly unpredictable end results, with circuits of identical designs giving outputs that range from non-existent to excellent.

Our new ETI design is a digital unit, and does not suffer from the deficiencies of the earlier analogue circuits. Its output is produced via a clock generator and a pseudo- or apparently-random shift register. The
output has all of the basic characteristics of a conventional white noise signal, but in reality has a preprogrammed pattern that is faithfully reproduced in all units that are built from the design. The amplitude of the output signal is inherently large, and required no further amplification before being fed to external filter networks.



Fig. 2. Practical circuit of the noise generator.

## Construction

The circuit uses only two IC's, one transistor, and half a dozen passive components, so construction is simplicity itself. As the ICs are CMOS devices, they should be handied with due care, and preferably should be mounted on the PCB via suitable
sockets or via Soldercon pins. When construction is complete, check the performance by connecting a crystal earpiece or microphone across the output terminals, and switch on. If all is well, the unit will produce a hissing noise like escaping steam.

ET

## BUYLINES

No problems here. All components are standard parts, available from most mail-order suppliers advertising in this issue.

## HOW IT WORKS

The theoretical circuit of the generator is shown in Figure 1, and a more practical representation is shown in Fig 2.1 C 2 is an 18 -stage $(5+4+5+4)$ static shift register. in which the logic (0 or 1) information of the Data terminal is fed forward one step on the arrival of each new pulse from the Cla-IC1b 30 kHz clock generator. IClc and IC ld are Exclusive-OR gates, and are used in conjuriction whith inverter. cominected Ol to feed various outputs of IC2 back to the Data terminal in such a way that the data feeds through the register in an APPARFNTI Y random or iumbled fashion.

In reality, a complex sequence of 0's and I's flows throught the register. repeating once every few seconds and producing an apparently random fumble of fundamental frequencies. Since these fundamental frequencles are produced digitally, however, they each produce a vast number of harmonics which, when subsequently (externally) filtered, produce a signal that appears to vary randomly in boft frequency and aplitude. and thus to have all the basic character. istics of white noise.

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| R2 | 10k |  |  |
| R3 | 2k2 |  |  |
| R4 | 27k | SEMICONDUCTORS |  |
|  |  | IC1 | 4070B |
| POTENTIOMETER |  | 1 C 2 | 4006B |
| RV1 | 10 k | 01 | BC182L |



Fig. 3. Component overlay.


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# Henry Budgett's comments last month spurred some of you to take up pen and phone. This month micro-man brings news from the North and gives the Beeb a plug. 

My little plea for help over the problems involved in modem style connection of home computers has borne some fruit. A very helpful gentleman, who just happens to work for the PO, wrote in with a few comments. Apparently the Post Office regard acoustic modems as attachments in much the same way as answering machines and there are a considerable number of specifications to be met. Such items are the maximum sound level of -13 dBm and the maximum sound pressure at the transmitter of 0.5 Newtons per square metre. Type approval for these kinds of devices should be obtained and I gather that ad-lib experimentation may be frowned on, so take care!

It should also be noted that hard wiring of a computer to the PO lines is definitely not on. I didn't suggest it last month, but just in case it has crossed your mind ... . forget it.

One other comment that was thrown in from another PO person was that there is a rather critical frequency around 2200 Hz . A tone of this frequency will cause the exchange to close down your call, slightly embarrasing. You have a bandwidth of 300 to 3500 Hz to play with so steer clear of this area. Full technical details of the specifications are contained in Technical Guide No 11, which should be obtainable from the telephone section of the Post Office.

And finally on this subject, I understand that Greenbanks cassette interface for their SCMP system has provision for an op-amp to be connected for direct tape head drive. It should prove possible to use this to drive a loudspeaker for our purposes. The board is currently being re-designed so contact them soon for details. Many thanks to Mike for his helpful comments on the Post Office's position.

## Standard Letters

A vast epistle squeezed its way into my mailbag this week after my diatribe on standards last month. One problem there was a lot in it about misspeling and general missuse of Her Britannic Majesty's English but not a sausage (courtesy of That's Life) on computer jargon. Have you no shame, or perhaps you were all stunned into silence? Please will someone say something, hopefully polite, as the article was supposed to inspire general comment.

## Plea For Clubs

Not a single word from anyone this month. Are you all too busy to write to Microfile with your news? Many thanks to
those who have filled in the little form and sent it back. If any club hasn't had one please let us know as we are trying to produce a second Club Directory for CT and we go to press in four weeks. After all, if the Beeb think it's good enough to use what have you got to lose, poetic stuff.

## BBC Speaks Out

A superb pair of programmes were boradcast this month on Radio 4. Cailed "Machines with Mouths" and "Machines with Ears" they dealt with speech synthesis and recognition systems and techniques which are currently being used. Having worked in this area for a number of years I found them to be excellently produced and most enjoyable. A definite pat on the back for the Science Department. What was even more impressive was that it was done on radio. One would expect this mind of subject to be tackled on a programme such as Horizon. It was also amusing to hear many voices from the past (such as my old boss) expounding their views on the subject. A repeat soon one hopes, how about it?

## News From The North

Microdigital have released the first of a series of Nasbus based general purpose interface boards. This one has sixteen relays and is addressable to any two consecutive ports on the Nascom. Power requirements are a modest 250 mA on both the +12 and +5 volt rails and the unit is supplied as a kit complete with sockets for all IC's along with a manual and sample software. Price is around the £50 mark.

The ACFA single board computer that we had a slight mix-up over a month or so back is currently being reengineered for the new 6809 CPU and some more $1 / 0$. The problems caused by the NTSC (Nasty Television System for Computers) have now been overcome and a demo model will shortly be going round the shows. Look out for it, it may suit your needs.

The Liverpool software gazette has just been launched priced at 50p per issue or £6 per year for twelve copies. It is packed with software and reviews, including a look at Pascal on the Apple. One of the most interesting items is the complete listing of the M5 language, which has now gone public, for the Nascom. For more details on the language see our review in CT May. The magazine is not intended for the beginner as it assumes a reasonable knowledge of computers. Details on all these products can be obtained from Microdigital at 25 Brunswick Street, Liverpool 2.

ET

Have we got an issue for you next month? Yes of course we have, just cast your tired eyes over this little lot. (Tired eyes can be avoided by refraining from reading lesser electronic magazines)

## SCALEXTRIC SPECIAL

Yes folks, HE's done it again. Just in time for Christmas. The HE workshop staff have been really getting their noses to the grindstones and have tirelessly, without any regard for personal health. been playing with their Scalextric set. Whilst they were doing so one of them had a bright idea, 'how about doing some projects on this lads?' He was quickly silenced and play reçommenced. A little while later, after this momentous statement sunk in, they thought about it and actually all agreed, it was a good idea. So now we proudly present the last word in electronic Lap Counters. Precision Hand Controllers and other amazing things to grace your layout. Miss it at your peril


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## UNIJUNCTION TRANSISTOR

Our brainy chief designer Ray Marston takes time off from his train controller to look at those oft maligned, collectorless transistors that are known to all and sundry as Unijunctions. So pay attention because we might be coming round your house to ask you questions about them.

## TV-THE CONTINUING STORY

This month Rick Maybury looks at the other end of the TV system, the box that sits in the corner of your living room. Find out just what happens when the on off switch is twiddled, the educated electron strikes again.

## PROJECT FAULT FINDING

Gasp . . your project didn't work, if it wasn't our fault (is it ever?) then it must be your fault. Keith Brindley, who has had to deal with one or two faulty projects in his time discusses the heart wrenching subject of dead projects.

HEBOT GROWS UP


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# AIRCRAFT BAND CONVERTER 

Listen in to the world's airlines with the ETI Biggles detector and

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Domestic aircraft communications, both private and commercial, generally involve a pilot talking from his plane to a traffic controller at an airfield as well as talking to other pilots. Signals from aircraft can be heard over quite long distances as they are flying quite high and thus the horizon, from the aircraft, can be up to several hundred miles away.

There are 360 channels allocated in the aircraft band, each assigned a specific use or for use in a particular area. Amplitude modulated (AM) transmission is used which simplifies the requirements for a receiver to listen on this band.

## The Convertor

Why a converter - why not a complete receiver? Firstly, a shortwave listener will already have a receiver. A converter to 'change down' the aircraft band frequencies to a suitable band between

3 MHz and 30 MHz is a simple, and inexpensive, solution. For those wishing to monitor some portion of the aircraft band the output of the converter could be connected to an ordinary multi-band transistor portable to provide quite adequate results. Alternatively, a fixed frequency IF (intermediate frequency) strip with detector and audio stages could be constructed.

The converter is crystal locked that is, a quartz crystal oscillator is mixed with the signals from the antenna, the signals then appearing at a lower frequency at the converter output. The frequency of the crystal used will determine the frequency band of the converter output.

For a number of reasons, we chose the output (or IF) frequency to be around 10 MHz . Inexpensive crystals are available for the aircraft band to give an IF output from the converter of 10.7 MHz - a standard IF frequency. The
same crystals can be employed if you wish to use a tunable shortwave receiver following the converter. There is a minor inconvenience though - the tunable receiver's dial has no simple relationship to the input frequency. The advantage is that inexpensive crystals cost around half that of a crystal made to order to provide a direct frequency relationship.

As the converter has quite a deal of gain, resulting in very good sensitivity, an RF Gain control has been provided. Very strong signals on a channel near to the one being monitored may cause interference. Judicious use of the RF gain control will reduce or remove the interference while enabling you to still hear the desired signal. Then again, a very strong signal on the channel you are monitoring may overload your receiver, resulting in very distorted reception. Reducing the RF gain will remove the problem.

Fig. 1 Circuit diagram.


## Construction

The printed circuit board has been specially designed for this application and no other construction technique should be employed unless you are very experienced in circuit construction at these frequencies.

It is best to commence construction by mounting the coil formers. They may be glued on the board over the pilot holes or the board drilled to the appropriate diameter for the base of the formers and then gluing the formers in place. Use the shield cans to locate and/ or hold the formers on the board. It is wise to insert the slugs in the formers after gluing to avoid accidentally gluing them to the formers. The best type of glue to use is one of the 'instant' bond glues such as "Superglue". Many glues available will not bond to substrate materials - particularly fibreglass material.

The next step is to wind the coils. They may be wound in situ if you wish, alternatively they may be wound on a suitable diameter former (such as a 5 mm or $3 / 16^{\prime \prime}$ drill shank) and then slipped over the formers on the board.

Take careful note of winding direction and the start and finish connections. Refer to the component overlay when soldering the coil leads in place. Do not mount the shield cans until all the minor components have been soldered in place.

When mounting the minor components take particular care with orientation of the transistors, FETs and the

## HOW IT WORKS

The circuit is quite straightforward, comprising an RF stage (Q1), a mixer (Q2) and an overtone crystal oscillator-multiplier *Q3). Dual-gate MOSFETs are used in the RF and mixer stages as they have good gain, low noise figure and good freedom from crossmodulation and overload problems.

Signals from the antenna are first amplified by Q1 and passed to gate-1 of the mixer Q2. The oscillator, Q3, is set to a sprecise frequency by the crystal. The finjection frequency to gate-2 of the mixer is derived from the collector of Q3, being two or three times the crystal frequency. The signal frequency are mixed in Q2, their difference is selected by the tuned circuit in the drain - this is the desired output frequency.

A low-Q tuned circuit, L1-C1, is used between the antenna input and gate-1 of Q1. The antenna input impedance is mismatched to the impedance of the gate to: optimise noise figure. The drain of Q1 is coupled to gate-1 of the mixer, Q2, via a double-tuned, bandpass coupling circuit consisting of L2, C6, Cc, C7 and L3. A combination " of inductive coupling and
zener diode. All components should be mounted right down on the board to minimise lead length. Stakes or pins should be used for the connections to the antenna input, IF output and dc connections.

There is provision on the pc board to mount a crystal socket for a 'style-D' crystal. These have a 12 mm pin spacing and stand about $20 \cdot \mathrm{~mm}$ high. Alternatively, if the smaller size crystals are used, having a pin spacing of 5 mm or pigtail connections, then they may be soldered in place under the board. Take
common-capacity coupling is used to achieve a wide bandwidth.

Gate-2 of Q1 requires a bias of +6 V for full stage gain. A link between gate-2 decoupling (R1,C2,C3) and the junction of R2-R3 allows for the connection of a gain control potentiometer.

The mixer has above IV5 of bias applied to gate-2. The conversion frequency is injected at this gate and a small amount of forward bias improves the mixer conversion gain. The output, or IF, is coupled via L4 which is resonant at 10 MHz with C10. This is a low-Q tuned circuit for the broad bandwidth necessary if the tunable IF receiver is used.

The crystal oscillator stage, Q3, is designed to cope with either third or fifth overtone crystals and may double or triple the crystal frequency in the collector. Tuned circuit L5-C15 selects the appro-s priate harmonic. Energy is coupled from L5 to L 6 which is resonated to the required fres. quency with C17. These two tuned circuits filter the injection frequency. This prevents any spurious mixing occurring in Q2.

Coil L7 is used to 'trim' the crystal.
care when doing this. Do it quickly and use the minimum amount of heat to avoid damaging the crystal.

If desired, the crystal may be mounted separate from the board. Keep lead length between the crystal and the board connections as short as practicable in this case.

The shield cans for the coil assemblies should be mounted last. It may be a wise idea to check that the converter is working before soldering the shield pins to the pc board.

The completed converter may be


Fig. 2 Component overlay.


The PCB fitted to its front panel, showing connections to the gain control, RV1.
mounted, we used a small box measuring $159 \times 96 \times 50 \mathrm{~mm}$ overall. They are available from a number of component suppliers. The board was mounted on the aluminium panel using two spacers. Antenna and IF output sockets, along with the RF gain pot, were also mounted on the panel and power leads taken through a hole in the side of the box. Small lengths of coax cable were used to connect the input and output sockets to to the board connection.

## Control

The particular method of alignment will depend on how you will be using the converter. To commence the alignment you will need to have on hand the appropriate aligning tool. You will need a plastic screwdriver-tip alignment tool
to suit the Neosid ferrite cores. They are readily available from many suppliers.

You will need a power supply delivering between 12 and 15 volts; the converter will draw between 30 and 50 milliamps. A receiver with a S-meter is a decided advantage when aligning the converter. You will need a signal generator, with AM modulation, covering the range of $118-126 \mathrm{MHz}$.

If you are using a tunable receiver for the IF, then the following procedure should be followed:

Connect the converter to the receiver. Use a short length of coax cable. If the converter is working you will notice an increase in the noise level on a sensitive receiver when power is applied. You can check that the crystal oscillator is working by removing the crystal tem-

## PARTS LIST

| Resistors all | , $5 \%$ * |
| :---: | :---: |
| R1,4 | 150R |
| R2,3 | 100k |
| R5 | 1 M |
| R6 | 56 k |
| R7 | 560R |
| R8 | 680R |
| R9 | 10k |
| R10 | 4 k 7 |
| R11 | 470 R |
| R12 | 270R |
| Potentiomet | ter |
| RV1 | 100k |
| Capacitors |  |
| Cc | 22 p ceramic |
| C1,15,17 | $76 p 8$ ceramic |
| C2-C5 | In ceramic |
| C6-C8 | 6 p 8 ceramic |
| C10,12 | 100 p ceramic |
| C11,18 | 10 n ceramic |
| C13 | 68p ceramic |
| C14 | 47p ceramic |
| C16 | In ceramic |
| C18 | 10 n ceramic |

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Q1,2 MFE131, 40673,40841
Q3 2N3563, 2N3564, 2N5770
ZD1 BZY88/C8V2 or /C6V8 or /C5V6 or /C5V1
Miscellaneous
$7 \times 722 / 1$ Neosid coil formers
$3 \times 7100$ Neosid screening cans
$2 \times 7300$ Neosid screening cans
$7 \times$ Neosid ferrite slugs, $4 \times 5 \times$
10/F29 coil wire
crystal - see text
box (see text), 2 coax sockets,
$2 \times 20 \mathrm{~mm}, 6$ BA spacers, nuts, bolts, etc.
*Resistor values may be plus or minus one standard value either side of those quoted without ill effect. Capacitor values should not be altered.
porarily - a decrease in the noise from the receiver will be noticed.

1. Set the receiver frequency to the middle of the tuning range of the converter's output. The converter RF gain should be at maximum all through the alignment procedure.
2. Tune the slug in L4 to obtain a peak in the receiver noise level.
3. Set all the other coil slugs flush with the tops of the coil formers.
4. Using the signal generator, with a fairly high output level, peak L4 again for best signal strength.
5. Set the generator to a frequency near 119 MHz and tune the receiver until you pick up the signal. Now adjust the slugs in L2 and L6 for best signal strength. Decrease the output of the signal generator so that these
adjustments are made on a fairly weak signal.
6. Set the generator to a frequency near 125 MHz , or the highest frequency in which you are interested, and tune the receiver until you pick up the signal. Adjust the slugs in L1 and L5 for best signal strength. Keep the generator output at a low level for best results.
7. Now set the generator to a frequency half way between these two frequencies. Tune the receiver to pick up the signal and adjust the slug in L3 for best signal. Check the adjustment of L4.
8. Return to 119 MHz and peak the slug in L2 again.
9. Repeat the procedure, 'touching up' each slug.
If the converter is to be used on one channel, or a couple of channels less than 1 MHz apart, then all the coils need only be adjusted for best signal strength on one channel.

Overall sensitivity of the converterreceiver system is very good, signals as low as 0.2 uV being clearly audible. The gain control range is about 20 dB .

## CHOOSING A CRYSTAL

The frequency injected at gate 2 of the mixer FET, Q2, may be above or below the signal frequency by an amount equal to the IF frequency. For a turnable receiver used as an IF, the injection frequency should be lower than the lowest signal frequency by 10 MHz . Thus, as you tune the receiver upwards in frequency from 10 MHz , you will tune signals above the lowest aircraft band frequency ( 118 MHz ). In this way there will be a simple relationship between the signal frequency and the receiver's dial. If 10 MHz equals $118 \mathrm{MHz}, 10.5 \mathrm{MHz}$ will equal 118.5 MHz , and so on. For this situation the injection frequency will be $118-10=108$ MHz . As the crystal oscillator output (collector of Q3) is twice the crystal frequency, the crystal frequency should be half of $108 \mathrm{MHz}=54 \mathrm{MHz}$.

If you use a tunable receiver than a fifth overtone crystal at 54.000 MHz should be ordered. Tolerance and adjustment range also have to be specified. A value of 20 parts per million (ppm) for tolerance and adjustment range is satisfactory. Firms such as Bright Star Crystals or Hy-Q should be able to supply a crystal to order.

Alternatively, a crystal at one-third the injection frequency may be used. Taking the 108 MHz injection frequency, as just illustrated a 36 MHz crystal may be used.

To determine the crystal frequency required for any case, use the following formula:

Crystal $=$ lowest signal frequency - IF
2 or 3
Inexpensive crystals intended for use in 'scanning' receivers are available from Dick Smith's. These provide an injection frequency above a particular aircraft channel frequency for the standard IF frequency of 10.7 MHz . For example, for the 125.8 MHz channel, the injection frequency is 136.5 MHz . These crystals have the channel frequency marked on them, not the crystal frequency.

SETTING THE CRYSTAL FREQUENCY If you require accurate frequency readout then the crystal frequency will need "trimming'. Coil L7 is provided for this purpose. For best results a digital frequency meter capable of measuring to 150 MHz is necessary.

Lightly couple the DFM to L5 or L6 via a small value capacitor and see if you get a sensible reading. You may need to connect it directly across gate-2 of the mixer, Q2.

Adjust L7 until you obtain the correct injection frequency according to the crystal chosen.

## BUYLINES

Components for this profject are available from Catronics Ltd, Communications House, 20 Wallington Square, Wallington, Surrey SM6 8RG.

## Coil Data

-Wind L2, L3, L4, L5, L6 and L7 clockwise up the former. L1 is wound anticlockwise up the former. The start of each coil is the 'cold' or 'earthy' end. All slugs are F29 type ferrite.
L1 5 turns, 22 B \& S tinned copper wire spaced over 10 mm , tap at 2 turns from cold end.
L2, L3 6 $1 / 2$ turns, 22 B \& S enamelled L4 wire, spaced over 8 mm . L4 25 turns closewound with enamelled wire, any gauge between 25 and 30 B \& S, 5 turn link at top of former.
L5, L6 5½ turns, 22 B \& S enamelled wire, closewound.
L7 "10turns, 22 B \& Senamelled wire, closewound, for crystals in the range 30 MHz to 50 MHz .

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# DESIGNER'S NOTEBOOK 

## Project Editor Ray Marston passes around a few design problems with LEDs and chews a CMOS 555!

TI he path of the electronics design engineer is fraught with nasty booby traps in the form of seemingly simple little circuits which fail, in practice, to work in the anticipated manner. Take, for instance, one of the problems that faced the ETI projects team when the 'AMBUSH' game was being designed last year (see the April ' 79 issue).

## Ambushed by LEDs

This particular booby trap centred on the LED 'attack' display that was used in the 'ambush' game. In essence, the display comprised four unequal-length lines of LEDs. All LEDs were driven from the outputs of a single 4017, but the lines were selected one at a time by a multiplexer, so that only one LED was on at any given moment. A greatly simplified diagram of the original (defective) version of this display is shown in Fig. 1. Although this diagram shows only three columns of LEDs, with a maximum of three LEDs in any one column, it does illustrate the basic 'trap' perfectly well.


Fig. 1. A simplified view of the original Ambush LED lines.

In this diagram, the ' $x$ ' lines are driven by the outputs of the 4017, so that one line is high (at +12 V ) at any given moment and the other two lines are at zero volts. The ' $y$ ' lines are driven by a multiplexer or multi-way single-pole switch, which pulls one line to zero but leaves the other two lines open-circuit at any given moment of time.

Figure 2 shows the results that were (rather naively) expected from the circuit under two specific operating conditions and compares them with the results that were actually obtained. In Fig. $2 \mathrm{a},+12 \mathrm{~V}$ was fed to the xl line

| $x 1$ | $x 2$ | $x 3$ |
| ---: | :---: | :---: |
| $+12 V$ | $0 V$ | $0 V$ |
| $y 1$ | $y 2$ | $y^{3}$ |
| $0 V$ | $0 / c$ | $0 / c$ |


| $x 1$ | $x 2$ | $x 3$ |
| :---: | :---: | :---: |
| $0 V$ | $o V$ | $+12 V$ |
| $y 1$ | $y 2$ | $y 3$ |
| $0 V$ | $0 / c$ | $0 / c$ |


(a)

(b)

Fig. 2. Given the operating conditions, shown (top), these are the results which were expected (middle) and actually obtained (bottom).
and the yl line was coupled to zero volts. As expected, LED 6 illuminated.

In Fig. 2b, +12 V was fed to the $\times 3$ line and the $y 1$ line was coupled to zero volts. It was expected that no LEDs would illuminate. In practice, LEDs 3 and 6 illuminated. Equally confusing results were found to occur in certain other combinations of switching position.

If you read last month's 'Notebook,' which dealt with LED pitfalls, you'll have already figured out the cause of the 'ambush' problem(!) If not, Fig. 3. illustrates the cause of the trouble quite well. The problem arises because of the low reverse breakdown voltages ( 5 V in this case) of the LEDs. In this particular instance, forward current was flowing through LEDs 3 and 6 via reverse-biased LED 1 , which had gone into the Zener mode.

The solution to this particular design problem is shown in Fig. 4. Here, ordinary diodes are used in place of all absent LEDs in the matrix, so that a ready conducting path exists in all switching positions, and no LEDs therefore become reverse biased. When this circuit is applied to the


Fig. 3 (left) Low reverse breakdown voltages cause the problem here. Fig. 4 (right). Replacing absent LEDs with ordinary diodes is the solution here.

Fig. 2b situation, D3 conducts and all LEDs remain off.
As we pointed out last month, LEDs can be tricky little brutes.

We ran into a rather intriguing little problem when building the hand-held remote-control unit for 'The Beast' that is featured in this month's issue of ETI. The problem was that the unit's up/down counter was giving erratic operation. We knew that the fault was one of construction, rather than design, so laboriously went through all the normal troubleshooting procedures and finally isolated the fault (by intuition, rather than anything else) to the area of the 4093B dual-oscillator circuit shown in Fig. 5.


Fig. 5. A broken track caused problems in this 4093B dual oscillator, but proved difficult to find.

As you can see from the circuit, the fault was actually caused by a broken track connection to the IC's positive supply terminal. In practice, however, this simple fault was the devil's own job to find, for the following reasons:

First, the PCB was double-sided, which made it difficult to trace some of the tracks on visual inspection. Next, normal test-meter checks showed that a near-enough 12 V supply did in fact appear on positive supply terminal 14 of the IC. Finally, oscilloscope inspection of the output terminals of the IC showed that the two oscillator waveforms of the circuit (see Fig. 5.) were indeed present, further strengthening the belief that the positive supply connection was OK. Suspicion was caused, however, by the fact that the waveform from output 1, which should have been a clean square wave, showed signs of being amplitude modulated by waveform 2. The fault was eventually located visually.

Figure 7 illustrates how the circuit managed to work and produce a 'supply voltage' on it's pin-14 $\mathrm{V}_{\mathrm{DD}}$ terminal, in spite of the broken supply rail track connection. The diagram shows the internal gate protection network that is fitted to each one of the input terminals of the 4093B. On gates IC1c and IC1d one of these inputs is taken directly to the positive supply rail, enabling supply current to flow to the $V_{D D}$ terminal via RA and D1, and thus power the oscillator circuits!

So how's that for an unusual 'beasty' story?

## CMOS 555-- 7555

If you've ever played with the ubiquitous 555 timer chip (and who hasn't?), you'll know that it has a few inherently unpleasant characteristics, as well as a whole stack of good ones. It does not, for example, like supply voltages that are significantly below 5 V , and it typically draws a hefty 10 mA of quiescent current when operating from a 15 V supply. Worst of all, it draws a massive 400 mA 'spike' of current from the supplies as it transitions from one state to another, and this spike tends to play havoc with any digital circuitry that is powered from the same supply lines.

Fig. 6. (Below). A rationalised comparative summary of the bipolar and CMOS 5555.

PARAMETER
TEST CONDITION
SUPPLY VOLTAGE RANGE
CPERATING TEMP. RANGE
SUFPLY CURRENT, TYP.
OUTPUT CURRENT, MAX
POWER DISSIPATION, MAX
TRANSITION 'SP!KE'
CURRENT, TYPICAL
TIMING ERROR, MONOSTABLE
INITIAL ACCURACY, TYP.
THERMAL DRIFT, TYP
DRIFT WITH Vcc, TYP
THRESHOLD CURRENT
TRIGGER CURRENT
RESET CURRENT
OUTPUT RISE TIME, TYP OUTPUT FALL TIME, TYP PROPAGATION DELAY OF TRIGGER PULSE, TYP MINIMUM PULSE WIDTH REQUIRED FOR TRIGGERING

| TEST CONDITION | BIPOLAR 555 |
| :---: | :---: |
|  | $\begin{gathered} 4.5 \text { to } 16 \\ 0 \text { to }+70 \end{gathered}$ |
| $V c c=15 \mathrm{~V}, \mathrm{RL}=\infty$ | $\begin{gathered} 10 \\ 200 \end{gathered}$ |
|  | 600 |
| $\mathrm{Vcc}=15 \mathrm{~V}$ | 400 |
| $\mathrm{R}=2 \mathrm{k} 0$ to 100 k | 1 |
| $C=100 \mathrm{n}$ |  |
| $\mathrm{Vcc}=15 \mathrm{~V}$ | 50 |
|  | 0.1 |
|  | 100 |
|  | 0.5 |
|  | 0.1 |
| $R L=10 \mathrm{M}, \mathrm{CL}=7 \mathrm{pF}$ | 100 |
| $R L=10 \mathrm{M}, \mathrm{CL}=7 \mathrm{pF}$ | 100 |
| $\checkmark$ trig MINIMUM LEVEL <br> $=O V, T E M P=25^{\circ} \mathrm{C}$ | 100 |
| $V$ trig MIN LEVEL $=O V$ <br> $V C c=15 \mathrm{~V}$ TEMP $=25^{\circ} \mathrm{C}$ | 20 |


| BIPOLAR 555 | CMOS 555 | UNITS |
| :---: | :---: | :---: |
| 4.5 to 16 | 2.0 to 18 |  |
| 0 to +70 | -20 to +70 | ${ }^{\circ} \mathrm{C}$ |
| 10 | 0.1 | mA |
| 200 | 100 | mA |
| 600 | 200 | mW |
| 400 | 10 | mA |
| 1 | 2 | $\%$ |
| 50 | 50 | $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ |
| 0.1 | 1.0 | $\% / \mathrm{nA}$ |
| 100 | $.01-5$ | nA |
| 0.5 | $10^{-5}$ | mA |
| 0.1 | $2 \times 10^{-8}$ | nS |
| 100 | 40 | nS |
| 100 | 40 | nS |
| 100 | 310 | nS |
| 20 | 90 |  |

You'll be pleased, therefore, to hear that Intersil have recently introduced a CMOS version of the 555 timer, known as the ICM 7555, which does not suffer from the basic defects of the bipolar version. Specifically, it can operate over the supply voltage range 2 VO to 18 V , typically draws only 100 uA quiescent from a 15 V supply, and draws a trivial 10 mA 'spike' of current when transitioning. Additionally, the required threshold, reset, and trigger currents of the CMOS device are several orders of magnitude down on the bipolar version, enabling timing resistors (for example) to be given values of hundreds of megohms.

## Twice As Nice?

On the debit side, this new CMOS chip costs twice as much as the bipolar version, has worse initial-timingaccuracy and drift-with-voltage characteristics, has poorer output current drive and power dissipation capability, and


Fig. 7 (left) the internal gate protection network of the 4093B. Fig. 8 (right) The internal circuitry of the familiar bipolar 5555.


Fig. 9. The internal circuitry of the CMOS 555.
has worse propogation delay and pulse-triggering characteristics. A 'rationalised' comparative summary of the characteristics of the two devices is shown in Figure 6.

Figures 8 and 9 show the simplified internal circuits of the two devices. Note particularly the great differences in the relative values of the voltage divider chains that are used in the different versions of the IC.

The CMOS and bipolar versions of the IC are housed in identical packages. The CMOS chip can be used as a plug-in replacement in existing 555 bipolar circuits. The reverse is not necessarily the case, since the CMOS version can use timing and other resistance values that are several orders of magnitude greater than is possible with the bipolar version.

If you want to play with the ICM 7555, you can buy it from Watford Electronics, whose advert appears elsewhere in this issue.

ETI

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This month you can sink into your armchair and
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command of your remote controller.

## Encoder/Transmitter

The major part of the encoder (Fig 2) circuit is wired up on a double-sided PCB, with the LED Readout circuitry implemented on an additional singlesided board. The display board is identical fapart from component numbering) to that used in the Train and Points-Controller units, and construction should present no problems.

The most important point to notice on the double-sided PCB is that wirewrap IC sockets are used in the construction, to enable solder connections to be made to tracks on either or both sides of the PCB where necessary. All pin-throughs and other components that pass through tracks in both sides of the PCB should, naturally, be soldered to both tracks. Bearing these points in mind, construction should present few problems if the overlay is followed with due care

When construction of the two boards is complete, you can temporarily interconnect the two circuits and
give them a functional check, in conjunction with the 'How It Works' section. The 16-LED display should be fully variable via Points Selector switch SW4. If you have a 'scope, you can check that the output waveform conforms to Fig 1 by triggering the scope via pin 9 of IC5

When the boards have been given a functional check, fit the into a suitable box and couple them up to their controls and indicator LEDs. If you are
using a 2 -wire control system, you wilo have to fit a couple of 6 volt cells into the controller to provide a 12 V supply. In the 3 -wire system, the 12 V supply is derived from the decoder/ data distributor unit via the third wire. You an if you wish, fit the controller with an ON/OFF switch wired in series with the positive supply line.

On our prototype unit we used a 2-pole 4-way DIL switch in the SW1 'System Select' position, the switch is


Fig. 1. The 15 -bit 'simultaneous' code used by the remote control system.


The points controller (above) can control up to sixteen sets of points or relays. It can activate several times per second. The set of points chosen is shown on the row of LEDs on the front panel. Think about your own particular points control needs before you start to build this unit. The data distribution unit is shown on page 91.
epoxied to the front panel. Our controller unit connects to the decoder/ data-distributor
unit
via approximately 3.5 metres of 3 -core coiled cable and a 3-pin DIN plug and socket.

The main power supply unit (below) has electronic overload on its output and can power up to four sets of track systems simultaneously.



The train controller (above) gives exceptionally fine speed control, from crawt to supersonic (well nearly). There's also a built-in track cleaner to keep things running smoothly.

## REMOTE CONTROL ENCODER


 The completed PCB is shown below.

## HOW IT WORKS

The circuit of the remote-control encoder is shown in Figure 8. Here, IC4 and C5, together with IC2c and IC2d and IC3a, are wired together as a 17 -stage decade counter with 17 decoded outputs, and are clocked at a 500 Hz rate via [Cl. vibrator that produces a narrow pulse on the arrival of each clock pulse, and it's outputs are ORed with the outputs of the counter via D14-D15-D16 and R6, to form a serial chain of negative-going output pulses from R32.
Bits 10 to 13 of the code (derived via IC6) originate as the 4 -bit outputs of up/down counter IC9, which functions in the same way as the 'Points Select' counter of the F 6 Power-Switch Selec decoded and fed to a 6 LED display on the hand-held transmitter/encoder unit to give the operator a visual indication of the numer of the point that has been selected.
The optional remote-control system uses a serial 15 -bit 'simultaneous' code, as shown in Figure 7. The code comprises the fifteen bits, each separated by 2 mS
plus a 3 mS reset or synchronisation pulse, all frame. A narrow code bit represents a ' 0 ' or OFF logic state, and a wide code bit represents 'l' or ON logic state.
The first two bits of the code are used to select the desired (one of four) track system. Bits 3 to 8 are used to control the train on that track. The remaining seven bits are used to select and activate the (up to 16 ) points on that track system.
When the remote control system was being developed, we considered the possibility of using an ultra-sonic, infra red, or radio 'link' between the transmitter/encoder and the receiver/ sound technical and/or ergonomic grounds. We finally settled on the use of a 2. or 3-wire flexible link, that can be simply plugged into any ore of a number of jack sockets scattered around the of jack sockets scattered around the
layout at (typically) 4 metre intervals. The layout at (typically) 4 metre intervals. The
two control systems are identical, except that the 2-wire transmitter/encoder uses it's own 12 volt battery supply, while the 3 -wire unit derives its 12 volt supply from the receiver/decoder unit

## PARTS LIST

| Resistors all 1/4W 5\% |  | C3 | In0 polyester |  |
| :---: | :---: | :---: | :---: | :---: |
| R1,7,8 | 12k | C5 |  | petrolytic |
| R2 | 150k | C8 | 1 l 01 | ctrolytic |
| R3 | 33k | C9 | 10 u | ectrolytic |
| R4 | 47k |  |  |  |
| R5,15 | 22k | SEMICON | TORS |  |
| R6 | 10k | 1 Cl |  | 555 |
| R9 | 1 k 5 | 1C2,7 |  | 4001 |
| R10 | 27k | IC3 |  | 4011 |
| R11 | 5k6 | IC4,5 |  | 4017 |
| R12,16-20 | 100k | IC6 |  | 4081 |
| R13 | 220k | IC8 |  | 4093 |
| R14 | 56k | IC9 |  | 4029 |
| R21-36 | 470R | IC10 |  | 4514 |
| R37 | 560 R | D1-19 |  | 1N4148 |
|  |  | LED1-16 |  | TIL 209 |
| CAPACITORS |  | MISCELL | US |  |
| C1,7 | 100 n polyester | SW1 doubl | 4 way | y switch |
| C2,4,6 | 10n polyester | SW2-4 sin | le cha | er switch |

## REMOTE CONTROL DECODER



PARTS LIST

| Resistors all $1 / 4 \mathrm{~W} 5 \%$ |  |
| :---: | :---: |
| R1 | 1 kO |
| R2,7 | 100k |
| R3 | 180k |
| R4 | 68 k |
| R5 | 27k |
| R6 | 2k7 |
| R8-22 | 1 M 0 |
| R23 | 56 k |
| CAPACITORS |  |
| C1,2 | 10 n polyester |
| C3 | 1 n 0 polyester |
| C4, 6, 7-22 | 100n polyester |
| C5 | 10 u 15 V electrolytic |
| SEMICONDUCTORS |  |
| IC1,5,6,7,8 | 4011B |
| IC2 | 4001 |
| IC3,4 | 4017B |
| IC9, 10, 11, 12 | 4093B |
| D1-15 | 1N4148 |
| ZD1 | $12 \mathrm{~V}, 400 \mathrm{~mW}$ zener |

## Remote Control

 DecoderThe complete decoder (Fig. 4) circuit is built on one double-sided PCB. This board uses conventional IC holders and construction should present few problems if the overlay is followed with care.

When construction is complete connect the board to an 18 volt power supply, connect the input signal from the encoder/transmitter, and give the circuit a full functional check in con



# TOUCH SWITCH 

# A unique relay-output bistable touch switch that works on the capacitive loading principle. It uses a single touch contact, and is unaffected by moisture and dirt. 

Most touch switch circuits published in recent years use a pair of metal contacts as sensors. When human skin resistance bridges these contacts, a readilydetectable indication of the touch action is given. A major problem with this type of circuit is that, since it is simply a resistance-sensing system, it can easily be disabled by any conductive medium, such as dirt or moisture, that bridges the contacts.

The ETI touch switch does not suffer from this problem. It is activated via the capacitive loading that occurs when a person touches or is 'coupled' to a single sensor contact. This contact can take any one of a large variety of forms. It can be a piece of metal the size of a pin head, or a piece of wire with a length variable from a fraction of a centimetre to several metres, or a large plain or highly decorated metal plate or printed circuit board. In the latter two cases, the plate or board can even be covered in an insulating material, such as plastic or varnish, since it is not necessary to actually touch the metal of the sensor to cause circuit operation, but merely to be capacitively coupled to it.

Our touch switch has a relay output andmgives bistable operation. If you 'touch' the sensor contact once, the relay turns on and latches into that state until the next time you touch the sensor, at which point the relay turns off. You can use the relay contacts to control house lights, etc, in which case you get alternate touch-ON, touch-OFF, touch-ON, etc, operation.

## Construction And Use

All electronic componénts are mounted on a single PCB, leaving only the battery and relay output con-

nections and a single lead to the touch pad to be soldered, so you should have no trouble in construction. Use IC sockets and double check that all semiconductors are inserted correctly before initial switch on. When construction is complete, connect a suitable touch pad (a length of wire, or a metal plate, etc) in place, connect up the relay and apply power to the circuit.

Initial setting up of the circuit is quite simple, but is necessary whenever a different touch pad is connected to the unit. Turn the present pot fully anti-clockwise and then, with the touch pad untouched, adjust the pot clockwise until LED 1 just comes on and the relay is heard to operate. Note the setting of the pot. Now touch the sensor pad firmly, and turn the pot slowly anti-clockwise until the LED just goes out. Note the new setting of the pot. Release the touch pad and adjust the pot to half way between the two settings. You should now find that the LED and relay activate whenever you touch the sensor and that the LED turns off again (but the relay does
not) when the sensor is released. This setting up procedure gives an optimum sensitivity/stability performance.

## Scope For Proximity

There is plenty of scope for experimenting with this circuit. If a touch pad with a large surface area (a metal plate or an area of foil) is used and the circuit is set for maximum sensitivity, it will act as a proximity switch. The proximity range can be maximised by taking the negative supply line of the circuit to earth via the mains ground line.

You'll notice from the circuit diagram that only one half of dual J-K flip-flop IC3 is used. Consequently, if you want to make two touch switches and are capable of doing a little of your own design work, you can make the second switch by simply duplicating the C2, rectifier, and IC2 circuitry, using the spare half of IC3, and feeding the new C2 from the output of the existing IC1 oscillator circuit.


Fig. 1 Circuit diagram.

## HOW IT WORKS

IC1 forms an astable multivibrator clocking at a frequency in the region of 100 kHz . Capacitor Cl forms a capacitive voltage divider effect with stray capacitance of the touch pad, which, after rectification via D1 and 2, charges capacitor C2. This voltage varies according to the capacitance of the touch pad, which in turn varies as it is touched. The voltage across C2 is, therefore, dependent on whether the touch pad is touched or not.

IC2 forms a comparator, using only a small amount of positive feedback, which compares the voltage across C 2 with that from the wiper of level preset RV1. As the voltages cross, upon touching the pad, the output of IC2 goes high and LED 1 lights. Preset RVI can be adjusted to suit any form of touch pad.

The output of IC2 is fed to the clock input of IC3, a dual JK type flip-flop. This device output changes state ie on/off or off/on, with every pulse input and consequently turns the relay on and off via transistor switch Q2.

Transistor Q1 forms a series pass regulator with R5 and ZD1 to maintain a stable voltage for the main part of the circuit, so that the delicate balance is not upset with variations in applied voltage.


## BUYLINES

There should be no problems in obtaining any components for this project.

## PARTS LIST

RESISTORS All $1 / 4 W, 5 \%$
RESISTORS All, /4W, 5\%
R1
R2
R3
R4
R5

POTENTIOMETER
RV1 10 k min horiz preset
CAPACITORS

| C1 | 560p polystyrene |
| :--- | :--- |
| C2 | 47 p polystyrene |
| C3 | 100 n polyester |
| C4 | 100 u 16 V electrolytic |


| SEMICONDUCTORS |  |
| :--- | :--- |
| IC1 | 4011 |
| IC2 | 741 |
| IC3 | 4027 |
| Q1,2 | BC182L |
| D1,2 | 1N4148 |
| D3 | 1N4001 |
| ZD1 | 12 volt 400 mW |
| LED 1 | TIL 220 or similar |

MISCELLANEOUS
12 V relay 120 R coil or greater


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# FLASH TRIGGER 

# Fascinating freeze frame photos from frenetic action with our phenomenal flash trigger. 

IF raindrops keep falling on your head, now is the time to build ETI's fabulous flash trigger and catch them bouncing back. See astounding shapes as everyday objects perform a dynamic ballet (Usually too fast for the unaided eye to see).

Of course, you will need a camera and a flash gun. However, even the cheapest electronic flash guns usually have a flash duration of one thousandth of a second or less - fast enough to catch drops of liquid performing their complex aerobatics or freeze a shattering light bulb. If you want to stop a humming bird in flight or investigate instant insects then you will probably have to look elsewhere for your equipment. The attraction of this unit is that it needs no fancy ancillary equipment; you don't need an SLR, just a simple camera whose shutter can be locked open and something to photograph. With a powerful flash gun, even a pinhole camera will do!



SCR1. Check polarity with a voltmeter but carefully as there may be several hundred volts present.

In use, the unit is switched on and adjusted until it triggers reliably from the chosen sensor. Set up your
camera according to the guide table supplied with the flash. Remember that the apertures given relate to the flash-to-subject distance. Place your camera for the best picture (open the shutter) and enjoy instant exposure!

## Construction

The unit is assembled on one PCB with flying leads connecting the controls. Power is supplied by a PP3 battery or any nine volt DC source.

There are no links to make on the board and none of the components are sensitive to static electricity or otherwise delicate making this an attractive project for assembly by a beginner or student.

A socket is recommended for IC1. These chips do not often fail but it can be infuriating to have to desolder one of you suspect it. In any case, a socket removes any chance of damage from excessive heat. The only point to watch is the orientation of the semiconductors. Use the ones specified; they're cheap and readily available. Make sure you connect the flash gun the right way round across



Fig. 1. Circuit diagram for the Flash Trigger project.

## HOW IT WORKS

IC1 is a 555 timer connected in the monostable mode. The timing period is determined by RV2, R4, C4 and is adjustable between 11 mS and 231 mS with the values shown. The trigger input of the chip is held just above its firing potential of one third supply voltage by adjustment of RVI which acts as a sensitivity control. A negative-going signal is coupled to the input by capacitor C2. Note that the values of $R 1,2,3, R V 1$ provide a medium input impedance and screened cable may be required when the sensor must be separated from the unit.

When ICI is 'fired', its output (pin 3) goes high for the monostable period. With SWI switched to 'direct', this positive going pulse will fire the SCR and discharge the flash enabling the unit to be used as a slave flash. There will be a tinite delay owing to rise time of phototransistor response, propagation delay within IC1 and rise time of its output. However, this will be measurable in microseconds and should be negligible.

When used in the 'delay' mode, the output pulse is inverted by Q1 causing the flash to fire on the trailing edge of the monostable pulse. To avoid repeated use of the tlash when setting up the unit, indicator LED 1 is provided. Each negative excursion of Q1 collector causes (5 to charge via R7, D1 effectively stretching the monostable pulse and providing a clearly visible tlash. An optional alarm; for example a solid-state-buzzer, can be connected into the circuit providing audible indication of triggering. C1 provides overall decoupling. Supply current is about 10 mA .

Below: what to do with it once you've built it. Taken with an ETI
Flash Trigger.


## PARTS LIST

RESISTORS All $1 / 4 W, 5 \%$
R1,2,3 150k
R4,5 100k
R6,8 10k
R7,9 470R
POTENTIOMETERS
RV1 50 k lin
RV2 2 M lin
CAPACITORS
C1 $\quad 1000$ electrolytic
C2,6 10n polyester
C3,4 100n polyester
C5 4 u 7 tantalum
SEMICONDUCTORS

| IC1 | 555 |
| :--- | :--- |
| Q1 | BC107 |
| Q2 | BC477 |
| SCR1 | C106D |
| D1,2 | 1N4148 |
| LED 1 | any LED |

MISCELLANEOUS
SW1 SPDT SW2 SPST PCB
flash-gun-connector, phototransistor, crystal mic. 9V battery


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Photo transistor is TIL. 78


Fig. 2. Wiring details for different triggers.


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C-Copy
E-Execute
G-Generate
H-Operate as hall duplex.
terminal.
J-Intelligent copy
J-Executeat FFA
K—set
L-losd fromird options
M-Memory modily

N-return io nopmal
O-Output to $p .10$.
O-Output to P.I.O.
R-Reary tape
S-Single step
T -Tabulate memory
U -activale user I/O drivers
V -Verlly tape
W-Write tape
X -sef erternal device
M-Memory madily
Z-execute at FFD

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-pole c/o with 2 second delay. Change R \& C for different timing. 50p
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    40V input Sec 12V 100MA Size 60 < 40 < 42mm 50p ench. P&
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    50%. P&,P 75%.
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    50%. P&,P 75%.
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| :---: | :---: | :---: | :---: | :---: |
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In its most basic form this should provide an indication of the logic level at any point in a circuit without overloading the section being tested. Other desirable features are the ability to follow high frequency pulse trains (preferably over 1 MHz ) and to detect isolated, narrow pulses less than 1 uS in width. Finally, the instrument should be compatible with both TTL and CMOS ICs and be able to operate from a wide range of supply voltages (say five to 15 volts).

Commercial logic probes that satisfy all these requirements are available, but they invariably cost over $£ 30$. The probe design described here offers comparable performance for less than $£ 4$.
combined with an excuse to enjoy a good cigar - a cigar tube is used for the case!

Indication is by means of three LEDs. Two red LEDs indicate either a HIGH or a LOW condition on the point under test, a green LED is used to indicate that a pulse train is occurring.

The circuit uses a single CMOS IC and a handful of resistors and capacitors. The components are mounted on a small board and housed in a tubular case such as an aluminium cigar tube or a length of plastic conduit. The power is supplied from the actual circuit under test and the performance characteristics of the prototype are described in the specification listed here.

## Construction

A printed circuit board is recommended for this project to provide consistent performance characteristics.

Before attempting to mount the components on the printed circuit


The logic probe in a cigar tube, showing the Hi, Lo and Pulse indication LEDs.
board check to see that it fits easily into the case. The board must be a loose enough fit to allow it to be moved up and down within the case over a range of at least 5 mm . (Refer to the diagram).

Mount the wire links, the resistors and the capacitors on the board, keeping all components as close to the board as possible. Note that C3 is mounted on the underside of the board. Next, install the three LEDs. The height of the LEDs above the board must be such that the assembly will slide into the case with the board pushed down against the bottom of the case (see diagram). For a 20 mm diameter case this height should be about 12 mm . If the LEDs are not high enough, then it will not be possible to push the assembled board up into a position where the LEDs project through the holes in the case.

Next, add the power leads (without clips or E-Z hooks at this stage) and the 10 cm wire to the probe tip. Last of all solder IC1 into position, observing all
the usual precautions - shorted pins, heat sink, earthed soldering iron, pins 8 and 16 soldered first.

Drill the 3 mm holes for the LEDs at 10 mm intervals, starting 75 mm from the front of the case. The hole for the supply leads is drilled in the back of the case and fitted with a small rubber grommet (or plastic LED housing) to prevent the case rubbing through the insulation on the leads.

Before mounting the assembled board in the case check the circuit for dry joints, solder bridges, incorrectly mounted components, etc. Then test the device as follows. Connect to a five volt supply and observe the three LEDs. None should light with the probe tip isolated. If the LOW LED (LED 2) comes on or flashes, then R2 is too small and must be replaced by a slightly larger resistor (say 820 k ). Touching the probe tip with the fingers may cause LED 2 to light, but this should go off when the tip is isolated. Touching the probe tip to either supply rail should

Fig.2. Component overlay.

$$
\begin{aligned}
& \text { Rs Bl/ gell } \\
& \bullet 1 \text { TOPROBE } O \text { O O O } \\
& -1 / \mu \mathrm{F} \\
& \text { TIP } \\
& \text { Fig.2. Component overlay. }
\end{aligned}
$$

$\square$
$\square$
$\square$

$$
\begin{aligned}
& \text { and R3 ensure that the outputs of both } \\
& \text { IC1 and IClf remain high when the input } \\
& \text { is 'floating'. C1 is connected across R2 as a } \\
& \text { 'speed-up capacitor' to maintain a sharp }
\end{aligned}
$$

$$
\begin{aligned}
& \text { is 'tloating'. C1 is connected across R2 as a } \\
& \text { 'speed-up capacitor' to maintain a sharp } \\
& \text { pulse shape into IC1e and so improve the } \\
& \text { ability to follow high frequency pulse } \\
& \text { trains (over 1MHz). }
\end{aligned}
$$

$$
\begin{aligned}
& \text { ability to follow high frequency pulse } \\
& \text { trains (over } 1 \mathrm{MHz} \text { ). } \\
& \text { The two inverters } \mathrm{ICla} \text { and } \mathrm{b} \text { form a }
\end{aligned}
$$

$$
\begin{aligned}
& \text { Three of th six invertei/buffer in IC1 are } \\
& \text { used in the high/low detection circuit. IC 1c } \\
& \text { Is eonnected to the probe tip via R9. When } \\
& \text { the input goes HIGH (logic 1), ICIc output }
\end{aligned}
$$

$$
\begin{aligned}
& \text { LIST } \\
& \text { LED 1,2 } 3 \\
& \text { LED 3 } \\
& \text { DI } \\
& \text { Miscellaneous } \\
& \text { PCB; red an } \\
& \text { alligator clip } \\
& \text { cigar,case ( } \\
& \text { minimum d } \\
& \text { 140mm lon } \\
& \text { * Resistors R2 } \\
& \text { be altered } \\
& 470 \mathrm{k} \text { to } 820 \\
& \text { characterjsti }
\end{aligned}
$$





light the appropriate LED, with the PULSE LED flashing when the tip first touches the positive rail. If the LOW LED does not light when the probe is connefted to $0 V$, then R2 is too large. Change R2 to 560 k and repeat the sequence above.

Now try a 15 volt supply. Again, all LEDs should be extinguished when the probe tip is isolated. The HIGH LED (LED 1) may glow very faintly. If this glow is too strong, reduce the value of R3 to say 470k. However, if R3 has to be altered it will be necessary to recheck the circuit at 5 V to see that the low voltage performance is still satisfactory. At 15 volts repeat the process of touch. ing the probe tip to the two supply rails. The results should be the same as in the case of the 5 volt supply, but the LEDs will be considerably brighter. EIn

Fig.3. The PCB slides into the cigar tube and rests on a piece of wood or plastic.


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## 555 Micro Input Reset

P. Davidson

When dealing with a microprocessor system, there are several features which place requirements on the duration of their input leg reset. These
signals are usually negative (in the author's experience) and so, with the use of a 555, these requirements can be filled reliably (as opposed to the normal flip-flop debounce circuit) The circuit saves on logic used to invert the normal 555 monostable action.

## LED Audio Power Indicators

M. P. Downes

The circuit diagram shows the input circuitry from the loudspeaker terminals. For simplicity only two of the monostable and LED driver cuits are shown. Six of these circuits can be constructred using three 4001 s and one 4049 CMOS ICs. The circuit is based on the fact that CMOS has an input threshold of approximately half the supply voltage (actually $0.45-0.55$ supply volts). IC1a and IC1b are dual input NOR gates connected in a monostable configuration with timing components R1 and C1. When the input to IC1a exceeds the threshold voltage, the monostable's output goes high for a period determined by R1 and C1 (with values shown approximately 200 mS ). This output is inverted and buffered to drive a LED for this period. The input to trigger the monostable comes from the speaker terminals where it is full wave rectified and לppears across RV1. R3 is a safety resistor in case of bridge failure. IN4005 diodes have the desired voltage and frequency characteristics for the bridge. R2 is to limit the current flowing into IC1a's internal protection diodes under large signal conditions and the value of RV1 depends on the desired input triggering voltage.

The lowest input voltage that can trigger the monostable is limited by the voltage drop across the bridge (OV8) and the threshold voltage of ICia (approximately $2 \vee 5$ ). The


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thireshold limit is largely overcome by using RV2 to bias point $A$ to just below the threshold voltage. In practice, the circuit operates on an input frequency of from less than 5 Hz to more than 50 kHz sinewave and at an input voltage of from approximately 1 V4 RMS ( 0.25 W into 8R) to more than $90 \vee$ RMS ( 1 kW into 8R). A single positive or negative 4 uS wide pulse will also operate the circuit.

The +5 V supply must be stabilised to ensure stable threshold levels and the usual decoupling of ICs and supply is advisable. If two units are
required for stereo use, two completely separate +5 V power supplies are essential to prevent partial shorting out of the input bridge, due to a possible common loudspeaker terminal in the amplifier. Greater input sensitivity can be achieved by using 0A91 diodes in the input bridge, but with slight loss in high trequency response and a lower maximum input voltage. If there is a variation in the threshold voltage of individual ICs then the lower threshold ICs should be used in the most sensitive positions of the circuit, i.e. 0.25 W .

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## Autowah Without Tears

S. N. Goodwin

The main disadvantage of a simple wah-wah circuit is that it requires a manual trigger for the effect, usually provided by a foot-pedal, which needs solid (and often expensive) mechanical construction and also prevents the guitarist from moving freely about the stage. After a couple of hand-made pedal systems collapsed in use, the standard wah-wah circuit was modified as follows: A light dependent resistor was mounted on the soundboard of the guitar about 2 cms from the highest string, pointing out about 1 cm from the front of the instrument. The shadow of the player's hand moving across the guitar triggers the effect - the more light

shining on the LDR, the higher the frequency-range boosted by the circuit.

It is tolerant of quite a wide range of light levels and if the range is found to be incorrect this can be rectified in two ways. Lenses or filters can be put across the LDR, or resistors can be connected in series/parallel with it.

Fluorescent lights could give problems with mains hum, but, under normal incandescent lighting, none were experienced. The wire to the LDR should ideally be screened, but over short distances this is not vital. Avoid bending its leads close to the body, as they can be snapped off very easily.

## A Simple Sequencer

P. Hill

A simple sequencer can be constructed using shift registers.

A logic 1 is shifted down the shift registers (IC4, 5) outputs, otherwise at logic 0, at each clock pulse. This places a voltage across the variable
resisters RV1 - 16 in turn. A preset DC voltage is thus available at the output, after being buffered by R1 . 16 and IC6 for each clock pulse. A sequence of control voltages can be set up and used to drive a voltage controlled oxillator.

The sequencer is reset by S 1 . The switch is debounced by IC -ia and


IC lb. Resetting zeros all shift register outputs and results in a logic 1 appears at the input of IC4.

When a clock is applied a positive going edge at pin 8 of IC4 and 5 corresponds to a negative-going edge at pin 1 of IC2, due to inverters IC Ic and IC id. The first positive

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## One Chip Preamplifier

## J. P. Macaulay

The circuit shown utilises the four Norton op amps contained within an LM3900 to produce a high quality stereo preamp, catering for magnetic cartridges.

IC1 is used in the inverting mode. Signals from the cartridge are fed via the blocking capacitor and R1 to the inverting input. R1 defines the input impedance and provides the right damping for the cartridge.

R5 and R6 define the midband gain of the stage whilst the network R3, R4, C2 and C3 provide the required RIAA equalisation. From here the equalised signal is fed to a standard Baxendall tone control net-
work built around IC2. This required little comment although it should be noted that individual volume controls are employed four each channel. This not only reduces crosstalk between channels but also works out cheaper in that only two single gang potentiometers are used.

Performance is good with overall distortion below $0.1 \%$ and a $\mathrm{S} / \mathrm{N}$ ratio of -67 db unweighted, ref 500 mV out.

## 2 Chip Electronic Dice

## P. Adams

This electronic dice produces a true dice display using only two IC's - a 74132 and a 7495. The 7495 is a 4-bit parallel-access shift register. It can either operate as a shift-register or be parallel (broadside) loaded at inputs A-D. Control over these two functions is by a mode control unput. When the mode is high data is loaded into Qa - Od from inputs A - D on the next negative-going clock edge. When the mode is low. data is shifted on Oa - Od on the next negativegoing clock edge.

By connecting the mode control to Oa so that the register alternates between load and shift and making the input word a function of the existing output word, with some simple logic, the register can be made to execute a count that will drive LEDs in a dice display. Note LEDs are lit when outputs are low. IC1a is connected as a conventional Schmitt oscillator providing clock pulses to the register. SW1 stops the oscillator and halts the count. On switch-on the register may start on an invalid count, but in a couple of clock cycles it will. produce a valid count and then remain in that sequence.


## PCB FOIL PATTERNS

We didn't have room in this issue to pack in all the foil patterns. Never fear, if you're anxious to get started on your PCBs, send us a large sae and they'll be on their way to you. If you can bear to wait until next month's issue, we'll find a little space somewhere for them. Rest assured, they will all appear on Etiprints.



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