AMAY 1979 INTERNATIONAL MAY 1979

50p

Six Channel
Fully Proportional
RADIO
CONTROL
SYSTEM

HEADPHONE AMPLIFIER

HOW IT WORKS -RADIO STAR

CHESS



... NEWS.... PROJECTS.... MICROPROCESSORS... AUDIO...

CHROMATHEQUE 5000

5 CHANNEL LIGHTING EFFECTS SYSTEM

All kits also available as some tell tacks (e.g. P.C.B. component sets in div ire sets etc.) Prices in FREE CATALOGUE



COMPLETE KIT ONLE £49.50 + VAT!

in ELECTRONICS To Y i ERNATIONAL has 5 free only channels with individual level controls on dy the least Yor and equinitias a straightfor viril sound-to-light on an extractional straightfor virilights at a cuttry which produce some superbirandors and sequenting effects. Each controls with a cuttry which produce some superbirandors and sequenting effects. Each controls with a cuttry which produce some superbirandors and sequenting effects. Each controls with a cuttry which produce some superbirandors and sequenting effects. Each controls with a cuttry which produce some superbirandors and sequenting effects. This versatile system featured as a construit each channel. Control of the lights is com, speed dependent upon music level or front p channel handles up to 500W and as the kit is a le board design wirin.

Kit includes fully finished metalliple fibreglass PCB, controls, w

MPA 2 10 100 VA T (Is into (2)) MIXED AMPLIFIER



COMPLETE KIT CHILY

uction ticle in Electronics To lay emational the MFA 330 is a nex in mixer lich takes a wide and of inputs such as distribution to the extreme with minimal win... making construct on any straightform. Introls and a master volume control. Mechanically the shed general purpose rugged high power amplifier design simplication

fully fin and metalwork fiber gl. PCB is controls wire in — Complete gold down to the restrict and both use wer amp module res, caps, s/col £10.60 + VAT commer with insunting class £10.50 ± VAT

Parts for power supply only (caps, rects , fuses, F holders) £3:40 + VAT

TRANSCENDENT 2000 SINGLE BOARD SYNTHESIZER

LIVE SERFORMANCE SYNTHERZER DESIGNED BY CONSCIANT TIM ORR (FORMERLY SYNTHESIZER DESIGNER FOR EMS LIMITED) AND FEATURED AS A

JCTIONAL ARTICE NELECTRON 3 TODAY INTERNATIONAL.

ANSCENDENT 200 3 3 octave instrument transposable 2 octaves up or down giving an effective 7 octave range. There is portamento, pitch bending, a VCO with shape and pitch lation, a VCF with 6 you and high pass outputs and a separate dynamic sweep control a noise generator and an ADSR envelope shaper. There is also a slow oscillator, a ne - pitch after a pitch and special circuitry with precision components to ensure tuning stability amongst its many features.

The kit includes fully finished metalwork fully assembled solid teak cabinet filter sweep pedal professional quality components fall resistors either 2% metal oxide or a metal trimi) and it really is complete. — right down to the last nut and bult and last piece of write. There is even a 13A plug in the kit. — you need buy absolutely no more parts before plugging in and making great music. Virtually all the components are on the non-professional quality biperglass PCB printed with component for atoms. All the controls mount directly on the main board, all connections to the board are made with connector plugs and contrictions vis os simple in can be built easily in a few evenings by almost anyone rapable of neat soldering! When finished you will possess a synthesizer comparable in performance and quality with ready built units selling for between 1500 and 1700?

COMPLETE KIT ONLY £172.00 + VAT!

Comprehensive handbook supplied with all complete kirs! This fully describes construction and tells you how to set up your synthesizer with nothing more elaborate than a

PNWFRTRAN

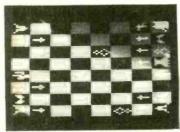


Cabinet size 24.6" x 15.7" x 4.8" (rear) 3.4" (front)

ORDERING INFORMATION AND MORE KITS ON PAGE 8



ETI goes to war! The model tank shown on our cover is a Tamiya 1/16th Leopard A4, kindly supplied by Richard Konstam Ltd who import the kits. See page 62 for marching orders.



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Get ahead p.77

ronics to

FEATURES

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Editor

Art Director

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Project Engineer

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Editorial Assistants

Production Editor

Technical Illustrators

Project Development

EDITORIAL AND ADVERTISEMENT OFFICE

Ron Harris, B.Sc

INTERNATIONAL EDITIONS

AUSTRALIA Collyn Rivers

Publisher Les Bell **Acting Editor**

HOLLAND Anton Kriegsman

Editor-in-Chief

CANADA Steve Braidwood

Editor Graham Wideman **Assistant Editor**

GERMANY Udo Wittig

Editor





25-27 Oxford Street, London W1R 1RF. Telephone 01-434 1781/2. Telex 8811896

Rick Maybury, Ian Graham, Henry Budgett Diego M. Rincon Pete Howells Paul Edwards, Tony Strakas Ray Marston John Fitzgerald Steve Ramsahadeo Margaret Hewitt Alan Carlton (Manager), Kim Hamlin

Halina Di-Lallo, Bren Goodwin, Tim Salmon Christopher Surgenor (Manager),

David Sinfield, Joy Cheshire, Sandy Neville Halvor Moorshead Advertising

Editorial Director

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SEMICONDUCTORS POTS & IRONS

SOCKETS

1611	8 pin DIL	€0.11
1612	14 pin DIL	€0.12
1613	16 pin DIL	£0.13
1614	24 pin DIL	£0.25
1615	28 pin DIL	€0.30
1616	TO18 Transistor	£0.12
1617	TU3 Transistor	€0.35
16117	TO5 Transistor	60.12

VOLTAGE REGULATORS

Positive	
MVR7805 v.a. 7805 TO220	£0.70
MVR7812 v.a. 7812 TO220	£0.70
MVR7815 v.a. 7815 TO220	£0.70
MVR7818 v.a. 7818 TO220	€0.70
MVR7824 v.a. 7824 T0220	€0.70
Negative	
MVR7905 v.a. 7905 TO 220	€0.80
MVR7912 v.a. 7912 TO220	€0.80
MVR7915 v.a. 7915 TO220	€0.80
MVR7918 v.a. 7918 TO220	€0.80
MVR7924 v.a. 7924 TO220	€0.80
72723 14 pin DN	€0.45
LM 309K TO 3	€1.50

ZENER DIODES

400mm (Bzy88) DO7 Glass encaps wwww (tzy88) DO7 Glass encapsulated range of voltages available 1,3 2,2 2v, 2,7v, 3,3v, 3,9v, 4,3v, 4,7v, 5,1v, 5,6v, 6,2v, 6,8v, 7,5v, 8,2v, 9,1v, 10v, 11v, 12v, 13v, 15v, 16v, 18v, 20v, 22v, 24v, 27v, 30v, 33v, 39v.

No. Z4 8p ee.

No. Z& Bp en.

1w-1.Ew Plastic and metal encapsulated ranges of voltages available.

1.3v. 2.2v. 2.7v. 3.3v. 3.9v. 4.3v.
4.7v. 8.1v. 5.6v. 6.2v. 6.Bv. 7.5v.
8.2v. 8.1v. 10v. 11v. 12v. 13v. 15v.
18v. 18v. 20v. 22v. 24v. 27v. 30v.
33v. 48v. 47v. 51v. 68v, 72v. 75v.
82v. 81v. 10ov.
No. Z13 15p ea.

No. Z13 15p ea.

10w Metal stud type S010 case.
Range of voltages available. 1.3v.
2.2v. 2.7v. 3.3v. 3.9v. 4.3v. 4.7v.
5.1v. 5.6v. 6.2v. 6.8v. 7.5v. 8.2v.
9.1v. 10v. 11v. 12v. 13v. 15v. 16v.
18v. 20v. 22v. 24v. 27v. 30v. 33v.
43v. 47v. 51v. 68v. 72v. 75v. 82v.
91v. 100v.
No. Z10 35p ea.

SILICON RECTIFIERS

	200mA IS920 50v IS921 100v IS922 150v IS923 200v IS924 300v	£0.05 £0.07 £0.08 £0.09 £0.10
-	1 Amp IN4001 50v IN4002 100v IN4002 200v IN4004 400v IN4005 600v IN4006 800v IN4007 1000v	£0.04 ½ £0.05 £0.06 £0.07 £0.08 £0.09 £0.10
	1.5 Arrep ISO15 50v ISO20 100v ISO21 200v ISO23 400v ISO25 600v ISO27 800v ISO29 10000v ISO31 1200v	£0.09 £0.10 £0.11 £0.13 £0.14 £0.18 £0.20 £0.25
	3 Amp IN5400 50v IN5401 100v IN5402 200v IN5404 400v IN5406 600v IN5407 800v IN5408 1000v	£0.14 £0.15 £0.16 £0.17 £0.21 £0.25 £0.30
	10 Amp IS10/50 50v IS10/100 100v IS10/200 200v IS10/400 400v IS10/600 600v IS10/100 1000v IS10/1200 1200v	£0.19 £0.21 £0.23 £0.35 £0.42 £0.61 £0.60 £0.69
	30 Amp 1S30/160 50v 1S30/100 100v 1S30/100 200v 1S30/400 400v 1S30/600 600v 1S30/800 800v 1S30/1000 1000v 1S30/1200 1200v	£0.68 £0.69 £0.93 £1.25 £1.76 £1.84 £2.31 £2.88
	60 Amp 1570/50 50v 1570/100 100v 1570/100 100v 1570/200 200v 1570/400 400v 1570/600 600v 1570/600 800v 1570/1000 1000v 1570/1000 1000v 1570/1000 68 300v BYX38/300 68 300v BYX38/300 Rev 6A 300v BYX38/600 Rev 6A 600v BYX38/600 Rev 6A 600v	£0.75 £0.84 £1.20 £1.75 £2.25 £2.50 £3.00 £0.45 £0.60 £0.45 £0.60

POTENTIOMETERS

CARBON POTS (Linear Track)
Single gang with wire end terminations, 6mm×50mm plastic shaft 10mm bushes supplied with shake proof washer & nut. Tolerance ± 20% of resistance.

1831 1k ohms £0.26* 1836 47k ohms £0.26* 1832 2k2ohms £0.26* 1837 100kohms £0.26* 1833 4K70hms £0.26* 1838 220kohms £0.26* 1834 10k ohms £0.26* 1839 470kohms £0.26* 1835 22kohms £0.26* 1840 1 Meg £0.26* 1841 2M2 £0.26*

CARBON POTS (Log Treck)
1842 4K7ohms £0.26* 1846 100kohms £0.26*
1843 10kohms £0.26* 1847 220kohms £0.26*
1844 22kohms £0.26* 1849 1 Meg £0.26*
1850 2M2 £0.26*

DUAL CARBON POTS (Lin Track)
These high quality dual gang pots are fitted with
wire end terminations and 6mm x50mm plastic
shaft 10mm, bush and supplied with shake proof
washer & nut track tolerance ± 20% but matched
to within 2db of each other. VC3
1851 4V7 £ 0.88° 1855 100kohms £0.88°
1852 10kohms £0.86° 1855 20kohms £0.88°
1853 22kohms £0.88° 1857 470kohms £0.88°
1854 100kohms £0.88° 1858 1Meg £0.88°

 DUAL CARBON POTS (Log Law)

 1860 4k7ohms £0.86* 1864 100kohms £0.86*

 1861 10kohms £0.86* 1865 220kohms £0.86*

 1862 22kohms £0.86* 1866 470kohms £0.86*

 1863 47kohms £0.86* 1867 Meg £0.86*

SINGLE GANG SWITCHED (Lin Law)
These potentiometers are fitted with double pole

SINGLE GANG SWITCHED (Lin Law)
These potentiometers are fitted with double pole on-off switches. The switch is incorporated within the rotary action of the pot. Specification of pot is as VC1.
Switch rating 1.5 amps at 250v AC.
1870 4470hms £0.65* 1874 100kohms £0.65*
1871 10kohms £0.65* 1875 220kohms £0.65*
1872 22kohms £0.65* 1876 470kohms £0.65*
1873 47kohms £0.65* 1877 1Meg.
£0.65*1873 47kohms £0.65* 1877 1Meg.

1878 2M2 60 65°

SWITCHED POT (Log Track)
Specification as VC2 but track having (log) law.
1879 4k7ohms £0.65' 1833 100kohms £0.65'
1880 10kohms £0.65' 1884 220kohms £0.65'
1881 22kohms £0.65' 1885 470kohms £0.65'
1882 47kohms £0.65' 1886 1 Meg
1887 2M2 £0.65'

DUAL GANG LOG-ANTI-LOG POT toop track specification as dual gang pots VC3, but tracks mounted to log-anti-log action 100kohms £0.75°

SPECIAL VOLUME CONTROLS

A miniature 16mm type replacement volume control incorporating single pole on-off switch. Resistance value 5kohms. Tolerance ±20% 1/8watt_rating. 1890 £0.54* VC8

MINIATURE ROTARY VOL

Skohms log law with on/off switch, 20mm growed spindle. Tag connections 17mm dia. Supplied with fixing nut. Used mainly for replacement. ment. 1890 £0.54* VC9

WIRE WOUND POTS

A range of wire wound single gang pots with linear tracks of 1 watt rating, fitted with 10mm bush and supplied with shakeproof washer and nut. V.C.

1891 10ohms £0.80*1895 220ohms £0.80*
1892 22ohms £0.80*895 470ohms £0.80*
1893 47ohms £0.80*897 1897 1kohms £0.80*
1894 20ohms £0.80*898 2k2ohms £0.80*
1894 20ohms £0.80*898 2k2ohms £0.80*

PRE-SET POTS
HORIZONTAL MOUNTING
Miniature type for transistor circuits. The wiper of
the preset is provided with a slot for screw driver
adjustment. The targe of the preset will fit printed
wiring boards with a pitch of 2.54mm. All tracks
are linear law.
VC7

VC7 1801 100chms £0.09* 1808 22kchms £0.09* 1802 220chms £0.09* 1809 47kchms £0.09* 1803 470chms £0.09* 1810 100kchms £0.09* 1804 1kchms £0.09* 1811 220kchms £0.09* 1805 2k2chms £0.09* 1812 470kchms £0.09* 1806 4k7

PRE-SET POTS
VERTICAL MOUNTING
Miniature type for transistor circuits. Wiper
adjustment is made by a screw driver slot.
Designed to fit 2.54mm pitch board. All tracks are
kneer law.

Designed to the second of the

ANTEX IRONS

perfect insulation break-down voltage of 1500 volts AC and a leakage current of only 3-5uA and another shaft of stainless steel to ensure strength.

O/No. 1935. Replacement element for 1931 iron.
O/No. 1932. Iron coated bit 1/8" for 1931 iron.
O/No. 1933. Iron coated bit 3/18" for 1931 iron.
O/No. 1933. Iron coated bit 3/18" for 1931 iron.
O/No. 1934. Iron coated bit 3/32" for 1931 iron.
O/No. 1938. Iron coated bit 3/32" for 1931 iron.
So.50
O/No. 1938. Iron coated bit 3/32" for 1931 iron.
So.50
O/No. 1953. SKI soldering kit—this kit contains 15 watt soldering iron fitted with a 3/16" bit plus two spare bits, a reel of solder, heat-sink and a booklet "How to Solder." in presentation display box.

Doked flow a sough. In presentation snaper E.5.55 O/No. 1939. ST3 soldering iron stand. State made from high grade bakelite material chromium plated strong steel spring, suitable for all models includes accommodation for six spare bits and two spoinges which serve to keep the soldering iron bits clean.

PRINTED CIRCUIT TRANSFERS

0000000 00000000 0000000

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8000000000000

Draw your own boards with the new BI-PAK etch-resistant transfers. Lay the symbols on the board, rub over with a sent pencil. The transfer will adhere to the board. Then complete the circuit with your BI-PAK etch-resist pen. Each pack contains 11 sheets of transfers 1 of each as shown above.

Iffustration — approx. ½ size,

O/No. TR400 @£1.50 p&p £0 10

BRIDGE RECTIFIERS

SILICON 1 amp		
Туре	Order No.	Price
50V RMS	BR1/50	€0.2
100V RMS	BR1/100	€0.2
200V RMS	BR1/200	€0.2
400V RMS	BR1/400	€0.3
SILICON 2 amp		
50V RMS	BR2/50	€0.4
100V RMS	BR2/100	€0.4
200V RMS	BR2/200	£0.5
400V RMS	BR2/400	€0.5
1000V RMS	BR2/1000	€0.6

OPTOELECTRONICS

NEW INCREASED RANGE — ALL 1ST QUALITY LED'S (diffused)

O/No. Type	Size	Colour	Price
1501 ARL209(TIL209)	.3mm (.125)	RED	€0.10
1502 MIL3232(TIL211)	.3mm (.125)	GREEN	£0.15
1503 MIL3331(OPL212A)	.3mm (.125)	YELLOW	£0.15
1504 ARL4850(FLV117)	.5mm (.2)	RED	£0.10
1505 MIL5251(TIL222)	.5mm (.2)	GREEN	£0.15
1506 MIL5351(MV5353)	.5mm (.2)	YELLOW	£0.15
1509 FLV111	.5mm (, 2)	CLEAR	£0.11
		(ill., Red)	
CHARGINE ALL T			

SUPER 'Hi-Brite' Typ 1521 MIL32 1522 MIL52 1514 ORP12 Light do 1520 OCP71 Photo to	.3mm (.125) .5mm (.2) spendent resistor	RED RED	£0.10 £0.10 £0.55 £0.35
LED CLIPS 1508/125 pack of 5 1508/2 pack of 5	125 clips 2 clips		€0.15 €0.18

DISPLAY	8:			
DL303	7 segment D.P. left (.30" height)	Common Anode		
RED	Single Digit	O/No. 1523	£0.70	
DL707	7 segment D.P. left (.03" height)	Common Anode		
RED	Single Digit	O/No. 1510	€0.95	
DL527	7 segment D.P. left (,50" height)	Common Anode		
RED	Two-Digit Reflector	O/No. 1524	€1.70	
DL727	7 segment D.P. right (.510" height)	Common Anode		
RED	Two-Digit Light Pipe	O/No. 1521	€2.20	
DL747	7 segmen tD.P. left (.630" height)	Common Anode		
RED	Single-Digit Light Pipe	O/No. 1511	£1.70	
	ALL @ 8% VAT			

OPTO-ISOLATORS
Isolation Breakdown — Voltage 1500 — continuous fwd current 100mA

CIL74 Single-Channel 6 pin DIP standard type — optically coupled pair with Infra-red LED Emitter and NPN Silicon Photo Transistor.

O/No. 1497 £0.50 ### O/No. 1497 E0.5u

CILD74 Multi-Channel 8 pin DIP Two Isolated Channels.

O/No. 1498 £1.00

CILQ74 Multi-Channel 16 pin DIP Four Isolated Channels.

O/No. 1499 £2.20

ALL @ 8% VAT

2nd GRADE LEDs

A pair of 10 standard sizes and colours which fail to perform to their very rigid specification, but which are ideal for amateurs who do not require the full spec.

O No. 1507 £1.50

THYRISTORS

100ma	TO 18 Case	7 amp
/olts No.	Price	Volts No
10 THY600 / 10	€0.15	50 TH
20 THY600/20	€0.16	100 TH
30 THY600/30	€0.20	200 TH
50 THY600/50	€0.22	400 TH
00 THY600/100	€0.25	600 TH
200 THY600/200	€0.38	800 TH
100 THY 600 / 400	£0.44	
		10 amp

1 amp	TO 5 Case
Volts No.	Price
50 THY1A/50	€0.28
100 THY1A/100	€0.28
200 THY1A/200	€0,32
400 THY1A/400	€0.38
600 THY1A/600	€0.48
800 THY1A/800	€0.68

3 am	ID .	TO 68 Case
Volts	No.	Price
50	THY3A / 50	£0.28
100	THY3A/100	€0.30
200	THY3A / 200	€0.33
400	THY3A/400	€0.42
600	THY3A/600	£0.50
800	THY3A/800	€0.65

5 amp	TO 66 Case
Volts No.	Price
50 THY5A/50	€0.36
100 THY5A/100	€0.45
200 THY5A/200	€0.50
400 THY5A/400	€0.57
600 THY5A/600	€0.69
800 THY5A/800	€0.81

_		
5 am	. т	0 220 Case
Volts		Price
400	THY5A/400P	€0.67
800	THY5A/600P	60.69
800	THY5A/800P	€0.81

/ armp	10 40 088
Volts No.	Price
50 THY7A/50	£0.48
100 THY7A/100	£0.51
200 THY7A/200	€057
400 THY7A/400	€0.62
600 THY7A/600	€0.78
800 THY7A/800	£0.92

10 m	mp	TO 48 Case
Volts	No.	Price
50	THY10A/50	£0.51
100	THY10A/100	€0.57
200	THY10A/200	€0.62
400	THY10A/400	£0.71
600	THY10A/600	£0.99
800	THY10A/800	£1.22
		TO 10 0

16 amp	TO 48 Case
Volts No.	Price
50 THY16A/50	€0.64
100 THY16A/100	80.58
200 THY16A/200	€0.62
400 THY16A/400	£0.77
600 THY16A/600	0.90
800 THY16A/800	£1.39
30 amp	TO 94 Case
Volts No.	Price
50 THY30A/50	£1,18
100 THY30A/100	£1.43
200 THY30A/200	£1.63
400 THY30A / 400	€1.79

400 THY30A/400	£1.79
600 THY30A/600	€3.50
	- Darley
No.	Price
BT101/500R	€0.80
BT102/500R	£0.80
BT106	£1.25
BT107	£0.93
BT108	£0.98
2N322B	£0.70
2N3535	£0.77
BTX30/50L	€0.33
BTX30/400L	€0.46
C106/4	£0.60

CABLES

DESCRIPTION	O/No.	Price/ Metre
Microphone Cable	3126	€0.10
Twin Microphone	3127	€0.20
Twin Steree Screened Cable	3128	£0.15
Multicore Standard 4-Core Screened	3129	€0.30
4-Core Individually Screened	3130	€0.22
Heavy Microphone Cable	3131	·£0.18
Light-Core mains	3132	£0,10
Twin Oval Mains	3133	60.03
Speaker Cable	3134	£0.07
Low Loss Co-axial Cable	3135	£0.22
15-Way Multi-Coloured Ribbon Cable	3136	€0.40

SEMICONDUCTORS

	T	RANSI	STO	RS			
Type AC107 60.22 AC113 60.20 AC117 60.30 AC117 60.30 AC117 60.30 AC117 60.30 AC117 60.30 AC117 60.30 AC122 60.18 AC122 60.18 AC125 60.18 AC126 60.18 AC128 60.16 AC128 60.16 AC128 60.16 AC128 60.16 AC128 60.20 AC134 60.20 AC134 60.20 AC134 60.20 AC135 60.20 AC136 60.20 AC137 60.20 AC141 60.20 AC161 60.35 AC11 60.35 AC1	Type 8C125 8C125 8C126 8C127 8C126 8C132 8C132 8C138 8C139 8C140 8C139 8C140 8C139 8C141 8C139 8C141 8C139 8C142 8C142 8C143 8C142 8C143 8C142 8C144 8C147 8C178 8C167 8C160 8C161 8C160 8C161 8C160 8C161 8C160 8C161 8C160 8C161 8C160 8C161 8C160 8C160 8C161 8C160 8C160 8C161 8C160 8C160 8C160 8C161 8C160 8C160 8C160 8C170 8C180 8C170 8C1	Type Price BO185 €0. 68 BO186 €0. 68 BO187 €0. 78 BO189 €0. 78 BO199 €0. 78 BO199 €0. 78 BO199 €0. 90 BO199 €0. 90 BO199 €0. 90 BO200 €0. 80 BO201 £0. 80 BO202 £0. 80 BO203 £0. 80 BD204 £0. 80 BD205 £1. 70 BD206 £0. 80 BD207 £1. 70 BD208 £1. 70 BD209 £1. 70 BD208 £1. 70 BD209 £1. 70 BD207 £1. 70 BD208 £1. 70 BD209 £1. 70 BD237 £0. 56 BD237 £0. 56	Type	Type	£0.10' £0.10' £0.10' £0.12' £0.12' £0.16' £0.16' £0.16' £0.16' £0.16' £0.12'	Type 2 N 3053 2 N 3054 2 N 3055 2 N 3055 2 N 3056 2 N 3391 2 N 3056 2 N 3391 2 N 3393 2 N 3395 2 N 3295 2 N 329	Price 60.18 60.40 60.27
ACY35 60.36 ACY40 60.50 ACY44 60.35 ACY44 60.35 ACY44 60.35 ACY44 60.35 ACY44 60.35 ACY46 60.35 ACY46 60.35 AD140 60.60 AD161 60.35 AD161 162 ACY66 60.35 AD161 162 ACY66 60.35 AD161 162 ACY66 60.35 ACY66 60.35	BC214	BF163	OC25	1.00 2N717 1.00 2N718 0.80 2N718 0.80 2N718A 0.90 2N726 0.90 2N726 0.90 2N727 0.20 2N734 0.20 2N743 0.20 2N914 0.24 2N918 0.26 2N130 0.27 0.28 2N130 0.29 2N130 0.29 2N130 0.20 2N130 0.20 2N130 0.21 2N130 0.22 2N130 0.24 2N130 0.35 2N180 0.35 2N180 0.35 2N180 0.35 2N180	60.30 60.25 60.50 60.29 60.20 60.20 60.15 60.30 60.20 60.18 60.18 60.18 60.18 60.18 60.25 60.30 60.20	2N 4293 2N 4921 2N 4923 2N 5135 2N 5136 2N 5136 2N 5136 2N 5136 2N 5294 2N 5294 2N 5257 2N 5251 2N 6027 2N 5251 2N 6027 2N 5251 2N 6027 2N 5251 2N 525	60.18 60.65 60.65 60.10' 60.10' 60.10' 60.10' 60.14' 60.36 60.32 6
AL103 €1.18 ASY26 €0.38	BCY31 £0.55 BCY32 £0.60	BF258 £0.25 BF259 £0.35 BF262 £0.60*	OC204	0.90 2N2193 1.15 2N2194	60.38 60.22 60.22 60.22 60.20 60.18 60.14 60.25 60.25 60.25 60.25 60.25 60.25 60.25 60.25 60.25 60.25 60.25 60.25 60.25 60.25 60.26 60.20	2S325 2S326	£0.71 £0.71

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Туре	Price	Туре	Price	Туре	Price	Type	Price	Type	Price
7400	£0.09	7427	£0.24	7472	£0.20	74105	86.03	74163	€0.62
74D1	€0.11	7428	£0.26	7473	€0.25	74107	€0.24	74164	€0.68
7402	€0.11	7430	€0.11	7474	£0.25	74110	€0.36	74165	\$0.68
7403	€0.11	7432	£0.22	7475	€0.29	74111	£0.58	74166	€0.78
7404	€0.11	7433	£0.30	7476	€0.25	74118	€0.80	74174	£0.65
7405	€0.11	7437	£0.21	7480	£0.44	74119	€1.18	74175	£0.62
7406	€0.22	7438	£0.21	7481	£0.85	74121	£0.24	74176	£0.58
7407	€0.22	7440	£0.12	7482	€0.68	74122	£0.39	74177	£0.58
7408	€0.13	7441	€0.50	7483	£0.58	74123	£0.40	74180	£1,50
7409	€0.13	7442	£0,40	7484	£0.88	74136	£0.52	74181	£0.58
7410	€0.11	7443	€0.70	7485	€0.68	74141	€0.55	74182	€0.70
7411	€0.17	7444	€0.70	7486	€0.22	74145	€0.55	74184	£0.70
7412	£0.15	7445	£0.65	7489	£1.70	74150	€0.68	74190	£0.68
7413	€0.24	7446	60.60	7490	€0.32	74151	€0.48	74191	£0.62
7414	€0.50	7447	€0.48	7491	€0.64	74153	£0.48	74192	£0.60
7416	£0.23	7448	€0.56	7492	€0.35	74154	€0.82	74193	€0.58
7417	€0.23	7450	€0.11	7493	€0.30	74155	£0.50	74194	€0.62
7420	€0.11	7451	€0.11	7494	€0.75	74156	£0.50	74195	£0.60
7421	£0.20	7453	€0.11	7495	€0.50	74157	£0.50	74196	£1.05
7421	£0.20	7454	€0.11	7496	€0.50	74160	€0.58	74197	£1.05
7423	£0.10	7460	€0.11	74100	€0.85	74161	€0.62	74198	£1.85
	€0.19	7470	£0.25	74104	€0.39	74162	€0.62	74199	€1.85
7425 7426	£0.19	7470	LU. LU	, , , , , ,					

CMOS ICs

Type Price CD400 £0.14 CD4001 £0.15 CD4002 £0.16 CD4006 £0.82 CD4007 £0.17 CD4008 £0.92 CD4009 £0.45 CD4011 £0.15 CD4012 £0.16	Type Price CD4015 £0.76 CD4015 £0.76 CD4016 £0.42 CD4017 £0.75 CD4019 £0.42 CD4020 £0.90 CD4021 £0.82 CD4022 £0.82 CD4023 £0.15 CD4024 £0.65	Type Price C04026 £1.20 C04026 £1.20 C04027 £0.50 CD4028 £0.68 CD4029 £0.85 CD4030 £0.45 £1.00 CD4035 £1.00 CD4035 £1.00 CD4037 £0.85 CD4040 £0.86 CD4041 £0.76	Type Price CD4043 60.88 CD4044 £0.82 CD4045 £1.40 CD4047 £0.87 CD4049 £0.42 CD4050 £0.42 CD4050 £0.42 CD4055 £1.00 CD4056 £1.35	Type Price CD4070 £0.17 CD4071 £0.17 CD4072 £0.17 CD4081 £0.17 CD4081 £0.17 CD4082 £0.18 CD4510 £0.99 CD4511 £0.95 CD4516 £1.00 CD4518 £1.00 CD4520 £1.00
CD4012 £0.16	CD4024 £0,65	CD4041 £0.76	CD4056 £1.35	CD4520 £1.00
CD4013 £0.42	CD4025 £0.15	CD4042 £0.72	CD4069 £0.17	CD4014 £0.80

LINEAR ICs

Type Price CA3011 £0.80 CA3014 £1.35 CA3018 £0.85 CA3028 £1.70 CA3028 £1.40 CA3036 £1.40 CA3036 £1.40 CA3042 £1.50 CA3042 £1.50 CA3043 £1.85 CA3045 £1.85 CA3045 £1.85 CA3045 £1.85 CA308 £2.85 CA3143 £1.50 CA3081 £2.00 CA3081 £1.50 CA3081 £2.00 CA3081 £0.70 CA3081 £	Type LM301 c0.29* LM304 c1.60* LM308 c1.00* LM309 c1.50* LM320-12V c1.50* LM320-12V c1.50* LM320-24V c1.50* LM380 c0.85* LM3800 c0.85* LM3102 c0	Type Price MC1312E1.90 MC1352E1.20 MC1352E1.20 MC1352E1.20 MC1459 E2.95 MC1495E0.90 ME565 E2.86 ME555 E0.24 ME556 E0.80 ME566 E1.50 ME566 E1.50 ME567 E1.70 UA702C E0.45 UA702	Type Price 72710 £0.30* 10.31* 10.32* 72711 £0.32* 72711 £0.32* 72711 £0.32* 72741 £0.24* 72741 £0.24* 72741 £0.32* 72748 £0.35* 72748 £0.35* 72748 £0.35* SN76013N £1.75* SN76023 £1.75* SN7611D £1.50*

	Price	Туре	Price
10 (60.30	SN 761	15
	E0.32*		£1.90°
	E0.32"	SN 766	60
	£0.45		£0.75
	€0.45	SL4144	£1.95"
	E0.24'	TAA550	B£0.35
	E0.24*	TAA62	1A
	E0.20		£2.00°
	E0.60°	TAA62	1B
	60.60		£2.50°
	€0.35	TAA66	£1.50
	£0.35		£1.30
	£0.35*	T8A540	£2.10
76012		TBARO	€0.80
	£1.75	TBAB10	
76023		12.10.1	€0.75
	£1.75	TBA810	£0.98
			€0.70°
76110		TBA920	
	£1.50'		€2.50
		TCA27	
		TOMET	£2.00°
			EE.00

DIODES

Type AA119 AA120 AA129 AAY30 AAZ13 BA100 BA102 BA148 - BA154 BA155 BA173 BB104	Price £0.08 £0.08 £0.09 £0.15 £0.10 £0.32 £0.15 £0.12 £0.14 £0.18 £0.15	BAX13 BAX16 BY100 BY101 BY105 BY114 BY124 BY126 BY127 BY128 BY130 BY133	Price £0.07 £0.08 £0.22 £0.22 £0.22 £0.22 £0.22 £0.15 £0.16 £0.17 £0.17	Type BY164 BY176 BY206 BY210 BY211 BY212 BY213 BY216 BY217 BY218 BY218 BY219 OA5	Price £0.51 £0.75 £0.30 £0.45 £0.45 £0.40 £0.41 £0.36 £0.36 £0.36	Type OA10 OA47 OA70 OA79 OA81 OA85 OA90 OA91 OA95 OA182 OA200 OA202	Price £0.35 £0.08 £0.08 £0.10 £0.10 £0.10 £0.10 £0.10 £0.10 £0.10 £0.10	Type SD10 SD19 IN34 IN34A IN914 IN916 IN4148 IS44 IS920	Price £0.06 £0.06 £0.07 £0.07 £0.06 £0.06 £0.06 £0.06
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TRIACS

		11/1/	465		
2 amp Volts 100 200 400	TO5 Case No. TR12a/10D TR12a/2D0 TR12a/400	Price £0.31 £0.51 £0.71	200 TR	TO48 Ca No. 110a / 100 100a / 200 100a / 400	Price £0.77 £0.92
6 Amp Volts 100 200	T066 Cme No. TR16a/100 TR16a/200	Price £0.51 £0.61	Volts	0220 P No. 00a/400 DIACS	Price P £1.12
400	TR16a/400	£0.77	BR1D0 €0.2	:0 D	32 €0.20

ORDERING Do not forget to state order number and your name and address.

V.A.T. Add $12\frac{1}{2}\%$ to prices marked *. 8% to those unmarked. Items marked † are zero rated.

P & P: 35p unless otherwise stated. GIRO account No. 388 7006.



DEPT. ET15, P.O. BOX 6, WARE, HERTS.

SHOP AT 18 BALDOCK ST., WARE, HERTS. OPEN 9 to 5.30 MON.-SAT.



(A DIVISION OF GOTHIC ELECTRONIC COMPONENTS LTD)

PO Box 290 8 Hampton Street

MAIL **TELEPHONE: ORDER** Birmingham B19 3JR **021-233-2400** ONLY

ALL PRICES IN PENCE EACH UNLESS OTHERWISE STATED

CAPACIT					
Electrolytic		ds	Order Code		
-10% to +509	% Tol		Cap 015 + µF	+ V d.c.	
μF ' V c	l.c. 16	25	40	63	
1.0	1			8	
1.5				8	
2.2				8	
3.3				8	
4,7				8	
6.8			8	9	
10		7		9	
15	7		8	10	
22		7	1	12	
33	7		8		
47		7	10	12	
68	8				
100		8	12	1	
150	8	9		29	
220	12		24	34	
330			28	37	
470		21	30	44	
680	19	28	36	50	
1000	23	28	55		
1500	32	36	1		
2200	39				

1000 1500 2200		23 32 39	28 36		55		50	
Tantalum	Bead			Ca	O ip PR +	rder C		
µF 0.1 0.15 0.22 0.33 0.47 0.68 1 1.5 2.2	√ d.c.	3.15	6.3	10	16	25	35 9 9 9 0 9 9 9	
3.3					9	11	14	
6.8 10			9 10	11	11	15	.6 20	

16 20

Electrolyt	ic Can 7	уре	Order Code	
High Ripple	e. IEC Gr	ade 1, Low E.S.R.	Cap HR + µF	+ Volts
		ith Vertical Fixing Cli	p	
2200 µF	16 V	Ripple 1A @ 85°C	1.4A @ 50°C	166
4700 µF	16V	2.6A	3.6A	184
10000 uF	16 V	5.8A	8.1A	222
22000 µF	16 V	9.8A	13.7A	346
2200 µF	25 V	1.3A	1.8A	175
4700 µF	25V	4.6A	6.4A	201
10000 µF	25V	A0.8	11.2A	264
22000 µF	25V	12.8A	17.9A	438
1000 µF	40 V	0.9A	1.2A	168
2200 µF	40V	2,4A	3,3A	188
4700 µF	40V	5.6A	7.8A	231
10000 #F	40V	9.2A	12.8A	367
1000 µF	70V	1.8A	2.5A	190
2200 µF	70V	4.0A	5.6A	235
4700 µF	70 V	7.5A	10.5A	376
1000 µF	100V	4.0A	5 6A	222
2200 µF	100V	7.8A	10.9A	346
			-	

Electrolyt				Order Code Cap 034 + µF + Volts				
μF V d.c	6.3	10	16	25	35	40	50	63
.47	1							6
.68								6
1.0								6
1.5								6
2.2	1						ĺ	- 6
3.3	1							6
4.7	i					6		7
6.8				6			7	8
10			6			7		8
15			6	7			8	10
22		6	7			8	10	
33			7	6		10		
47	1.	7	8		10			
68	1		8	10				
100		8	10					
150	1	10						
220	10							

Order Code

250V D.C. Wkg. Film Dielectric, Miniature

Mini	ature	Low \	/alue										Order	Code	
Polystyrene, Axial, ±1% Tol., ≥ 63V D.C. Wkg										Ca	D 424				
Ceramic Plate, Radial, Low K, 1.8pF -8.2pF : 25pF Tol, 10-330pF : 2% Tol, 100V D.C. Wkg											p 632				
Ceramic Plate, Radial, Med K, ±10% Tol, 100V D.C. Wkg											ip 630				
Ceramic Plate, Radial, High K, -20% to +80% Tol, 63V D.C. Wkg											p 629				
and the state of t											+ V:				
pF	424	632	630	629	pF	424.	632	630	629	nF	424	632		629	
1					100	16	6			10	25			6	
1.2					120	16	8			12	26				
1.5	1 1				150	16	8			15	26				
1.8		5			180	16	.6			18	27				
2.2		5			220	16	ô			22	28			8	
2.7		5			270	18	8			27	38				
3.3		5			330	18	8			33	41				
3.9		5			390	18		5		39	43				
4.7		5			470	18		5							
5.6		5			560	16		5							
6.8		5			680	16		5							
8:2		5			820	16		5							
10		5			1000	16		5	5						
12	1	5			1200	16		5							
15		5			1500	18		6							
18		5			1800	18		6							
22		5			2200	18		6	6	1					
27		5			2700	18		6							
33		5			3300	18		6							
39		5			3900	18		6							
47		5			4700	23		7	6						
56		6			5600	23									
68		6	1		6800	23									
82		6			8200	23									

2 6			8200	23				
	Polyester Radial Leads Olpped Type, ±20% Tol.; Moulded Type, ±10% Tol. Moulded Type, ±10% Tol;							
	μĒ	352	360	PH				
	.001		5	6				
	.0015		5	6				
	.0022	5	6	7 7 7				
	.0033	5	6	7				
	.0047	- 5	6	7				
Order Code	.0068	5	6	7				
Tubular Type	.01	5	-6	7				
L LUDUIAL LYDE	A1E		- 2	-				

500V D.C. Wkgs C004 EA Tubular

.8 - 3.8pF .8 - 6.8pF 1 - 13pF 1.7 - 19.7

VERO ELECTRONICS PRODUCTS

25" x 5". 1" pitch Veroboard 3.75" x 5". 1" pitch Veroboard 3.75" x 5". 1" pitch Veroboard (5) 3.75" x 5". 1" pitch Veroboard (5) 3.75" x 2.5" 1" pitch Pilain Board 5.87" x 2.5" 1" pitch Pilain Board 5.87" x 2.5" 1" pitch V. 20 IIP Board Pint Insection Tool for, 0.40 type pin DS Pins, 0.40 (1.00) SS Pins, 0.40 (1.00) SS Pins, 0.40 (1.00)

SS Pins, 040 (100)
6mm Board Standoff (100)
15mm Board Standoff (100)
15mm Board Standoff (100)
19mm Board Standoff (100)
Verowire Kit (1-pen, 2-wire, 25-comb)
Verowire Kombs (100)
Verowire Wire (4)
Filip Top Box, Smell, Black
Filip Top Box, Large, 8lack

Tol. > 250V D.	C. Wkg. Ca	280/35	2 Style								
% Tal, ≥100V D C. Wkg. 10.2mm Pitch Centres											
6 Tol; ≥100V D.C. Wkg. 7.6mm Pitch Centres											
PHE280	μF	352	360	PHE28							
6	.1	6	В	9							
6	,15	7	9								

	Cap 352	
	Cap 360	
	Cap PHE280	
	+ Value	
)		

Order Code

DIL SKT 8 DIL SKT 14 DIL SKT 16 DIL SKT 24 OIL SKT 28 DIL SKT 40

Order Code

CASES

Small Desk Console - Boss Industrial Mouldings Slope Front Console, Recessed Top ABS Base, C/W Brass Bushes, In Orange 1mm Aluminium Top Panel Finished Grey

		Order Cod
W161, D96, H39 (57)	186	Case BIM1005 O
W215, D130, H47 (73)	268	Case BIM1006 O



Plastic Boxes - Boss Industrial Mouldings Moulded Box and Close Fitting Flanged Lid ABS Box, C/W Brass Bushes, and Lid In Drange

		Order Code
L112 W62 D31	87	Case BIM2003 OR
L150 WB0 D50	115	Case BIM2005 OR
L190 W110 D60	195	Case BIM2006 OR





Small Desk Consoles — Boss Industrial Mouldings
Slope Front Console, Recessed Top
ABS Base, C/W Brass Bushes, In Orange
1mm Aluminium Top Panel Finished Grey
Ventilation Slots In Base

Slope Front Console, Recessed Top Two Piece All Aluminium Construction Ventilation Slots In Rear and Base Choice of 15° or 30° Sloping Front Off White Top Panel, Blue Base

Order Code Case BIM6005 OR Case BIM6006 OR Case BIM6007 OR W170 D143 H32 (56) W170 D214 H32 [82] All Metal Desk Consoles — Boss Industrial Mouldings

W250 i	0167.5	H 68.5	(Chassis	153mm	Deepl	1480	Case	B1M3000 C)R

Plastic Boxes with Metal Lids - Boss Industrial Moulding Recessed Top Box
ABS Base, C/W Brass Bushes, In Orange

Imm Aluminium	Top Panel	Finished Gr	eV.
			Order Code
L85 W56 D29		97	Case BIM4003 OR
L111 W71 D42		130	Case BIM4004 OR
L161 W96 D53		182	Case BIM4005 OR



Diecast Box and Flanged Lid Aluminium Box and Lid In Natural Flinish L113 W63 D31 L152 W82 D50 L192 W113 D61



Eurocard Size Desk Console - Boss Industrial Mouldings Slope Front Console ABS Case, C/W Brass Bushes, In Orang Imm Aluminium Top Panel, Finished Order Code W169 O127 H45 (70) 375 Case BIM8006 DR

VERO 21069J VERO 21072D VERO 21076C VERO 21078E VERO 21084E VERO 21013A VERO 21015F VERO 21087G	HA D.I. 8 P 14 P 16 P 24 P 28 P 40 P
VERO 210178 VERO 21321K VERO 21322G VERO 21323D VERO 21334D VERO 21334D VERO 21339F VERO 21340G VERO 21317D VERO 21317D	Hea Indi Indi Indi Indi
3	P.C Date Fus
-	P.C.I Chas Pane Pane

HARDWARE

D.I.L. Sockets

Heatsinks

8 Pin Low Profile Socket Tin 14 Pin Low Profile Socket Tin 16 Pin Low Profile Socket Tin 24 Pin Low Profile Socket Gold 28 Pin Low Profile Socket Gold 40 Pin Low Profile Socket Gold

Individual Type for 1 x T05 50°C/N Individual Type for 1 x T056 10.5°C/W Individual Type for 1 x T03 7.2°C/N Individual Type for 1 x T0126 11°C/N Individual Type for 1 x T0220 17°C/W	10 26 24 23 23	Sink 5F Sink TV2 SInk TV3 SInk TV4 Sink TV5
P.C.B. Components		
Dato Pen, Blue ink, Slow Drying	92	Pen 33PC
Fuseholders		
Suit 20mm x 5mm fuses.		
P.C.B. Mounting, Open Type Chassis Mounting, Open Type Panel Mounting, Screwdriver Slot Fanel Mounting, Finger Release	8 17 77 96	Fuse/H20B Fuse/H20C Fuse/H20PT Fuse/H20P
ffuses		
20mm x 5mm Glass.		
Cuick Blow, Range 100mA-5A Slow Blow, Range 250mA-5A	8 22	Fuse 20 A/S Fuse 20
Lampholders, Panel Mounting		+ Rating
Similar In Style to Fuse/H 20P Low Voltage Type Suits LES and M/F Bulbs.		
Low Voltage, Red, Amber or Green Internal Neon 200/240V Red or Amber	75 95	Lamp LV Lamp N
		+ Colour
Bulbs, Low Voltage, L.E.S.		
6V, 0.36W: 6.5V, 1W: 14V, 0.75W.	22	Bulb LES
		+ \range

RESISTORS				Order Code	1	Skeleton Presets, Miniature		Order Cod
Carbon Film, Fixed				Order Code		0.1W, E3 Values, 100R-IM, Lin, Vertical Mounting	7	Min Preset \
0.25W, E24 Values IRO-10M, 5% Tol. 0.5W, E12 Values IRD-4M7, 10% Tol.	1.5 ea. 2 ea.	90p/100 (Mult 10/Value) 1.25p/100 (Mult 10/Value)	£7.90/1000 (Mult 100/Value) £10.10/1000 (Mult 100/Value)	Res RD% Res RD%		0.1W, E3 Values, 100R-IM, Lin. Horizontal Mounting	7	Min Preset i
M . 153 . 51 . 4				+ Value		Skeleton Presets, Standard		
Metal Film, Fixed						0.3W, E3 Values, 100R-4M7, Lln. Vertical Mounting	10	Std Preset V
0.5W, E24 Values, SRI-IM, 2% Tol. 2.5W, E12 Values 10R-27K, 5% Tol.	6 ea. 13 ea.	3.80/100 (Mult 10/Value) 7.90/100 (Mult 10/Value)	£32.40/1000 (Mult 100/Value)	Res MR30 Res PR52		0.3W, E3 Values, 100R-4M7, Lin. Horizontal Mounting	10	Stri Preset H + Value
				+ Vàlue		Potentiometer, Rotary		
Metal Glaze, Fixed					,	0.5W, E3 Values, 1K-2M2 Lln.	34	Pot Lin
0.5W, E24 Values, IM-33M, 5% Tol.	10 ea.	5.40/100 (Mult 10/Value)		Res VR37 + Value		0.25W, E3 Values, 4K7-2M2 Log	34	Pot Log + Value

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THE R. P. LEWIS CO., LANSING, MICH.	1		-							A. 100 To			A	
	NTEGRATED O d C-MOS — High S													
515V 'B' Serie	es, Up to 20MHz			7400 T.T.L.	9 N7444N	83 N74122N	39 N7419		N74LS2BN	32 16	N74LS138N N74LS139N	85	N74LS253N N74LS257N	105 104
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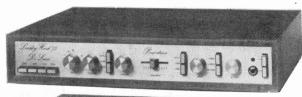
PSI 4002 STUDIO MODEL



cabinet size 17.2" × 17.2" × 6.7"

COMPLETE KIT ONLY £196.90 + VAT

READ THE REVIEW IN SOUND INTERNATIONAL DEC. '78







T20 + 20 20W STEREO AMPLIFIER £33.10 + VAT

This kit, based upon a design published in Practical Wireless, uses a single printed circuit board and offers at very low cost, ease of construction and all the normal facilities found on quality amplifiers. A 30 watt version of this kit (T30 \pm 30) is also available for £38.40 \pm VAT.

POWERTRAN SFMT TUNER £35.90 + VAT

This is a simple low cost design which can be constructed easily without special alignment equipment but which still gives a first-class output suitable for feeding any of our very popular amplifiers or any other high quality audio equipment. A phase-locked-loop is used for stereo decoding and controls include switchable afc, switchable muting and push-button channel selection (adjustable by controls on the front panel). This unit matches well with the T20 + 20 and T30 + 30 amplifiers.

WWII TUNER £47.70 + VAT

This cost reduced model of our highly successful Wireless World FM Tuner kit was designed to complement the T20 + 20 and T30 + 30 amplifiers and the cabinet size, front panel format and electrical characteristics make this tuner compatible with either. Facilities included are pre-aligned front-end module, switchable afc. adjustable switchable muting. LED tuning indication and both continuous and push-button channel selection (adjustable by controls on the front appli).

FOR ELECTRONIC KITS OF DISTINCTION

As featured in Electronics Today International 400W rms continuous — 800W peak! 0.03% THD at FULL power! PLUS all the following features too!

- * Each channel totally independent with its own stabilised power supply driven by custom designed TOROIDAL transformers!
- Inherent reliability monster heat sinks for cool running at the hottest venues electronic open and short circuit protection!
- ★ Ultra low feedback (an incredible low 14dB overall!), super high slewing rate (20V/μs), 200W rms continuous to 4 ohm from EACH channel, input sensitivity 0.775V (0dB).
- * Professional quality components, sturdy 19 rack mounting chassis complete with sleeve and feet for free standing work too.
- Easy to build plenty of working space with ready access to all components, minimal wiring, extensive instruction suitable for both experience constructors and newcomers to electronics.
- Value for money quality and performance comparable with ready-built amplifiers costing over $\pounds 600!$

DE LUXE EASY TO BUILD LINSLEY HOOD 75W STEREO AMPLIFIER £99.30 + VAT

This easy to build version of our world-wide acclaimed 75W amplifier kit based upon circuit boards interconnected with gold plated contacts resulting in minimal wiring and construction delightfully straightforward. The design was published in Hi-Fi News and Record Review and features include rumble filter, variable scratch filter, versatile tone controls and tape monitoring whilst distortion is less than 0.01%.

WIRELESS WORLD FM TUNER £70.20 + VAT

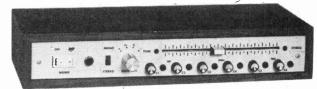
A pre-aligned front-end module makes this Wireless World published design very simple to construct and adjust without special instruments. Features include an excellent a.m. rejection. push-button station selection as well as infinitely variable tuning and a phase locked loop stereo decoder incorporating active filters for "birdy" suppression.

LINSLEY-HOOD CASSETTE DECK £79.60 + VAT

This design, published in Wireless World, although straightforward and relatively low cost provides a very high standard of performance. There are separate record and replay amplifiers and switchable equalisation together with a choice of bias levels are also provided. The mechanism is the Goldring-Lenco CRV with electronic speed control.







COMPLETE KITS: Our complete kits really are complete. All of the projects shown on this page-are supplied with fully finished metalwork, ready assembled high quality teak veneer cabinet, cables, nuts, bolts, etc., and full instructions -; in fact everything!

All of the kits shown on this page are available as separate packs (except the Powertran SFMT Tuner) for those customers who wish to spread their purchase or perhaps make their own cabinets or metalwork. Prices are given in our FREE CATALOGUE.

PRICE STABILITY. Order with confidence. Irrespective of any price changes. We will honour all prices in this advertisement until June 30th, 1979, if the May, 1979 issue is mentioned with your order. Errors and VAT rate changes excluded.

EXPORT ORDERS: No VAT. Postage charged at actual cost plus 50p handling

and documentation.

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SECURICOR DELIVERY: For this optional service (U.K. mainland only) add

£2,50 (VAT inclusive) per kit. **SALES COUNTER:** If you prefer to collect your kit from the factory, call at Sales Counter (at rear of factory). Open 9 a.m.-4.30 p.m. Monday-Thursday.

OUR CATALOGUE IS FREE! WRITE OR PHONE NOW!

VERTRAN ELECTRO

PORTWAY INDUSTRIAL ESTATE ANDOVER, HANTS SP10 3NM

ANDOVER (STD 0264) 64455

news digest.



BYTE SIZED CHUNKS

Some new expansion kits for the three most popular MPU systems have been announced by Ithaca Audio Ltd. Each pack contains eight 16K Rams, packed in anti-static foam and are all 100% guaranteed. The kits are intended for the TRS 80, Apple 11, and Exidy Sorcerer. UK price and availability are yet to be announced but for those who can't wait you could contact Ithaca Audio at:- Box 91, New York, 14850.



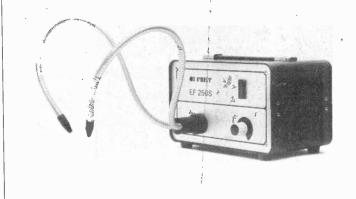
FRED'S BIG BILLS

Another Electricity Board first, 'Fred' is an electronic spokesman and will give advice on how to save energy by using more economical appliances. Using only 5KW, it is hoped to supply every home that has a 'white meter' with their own 'Ered'.

PUTTING OUT THE FEELERS

Pointing the way with their new 'cold' light-source boxes Optronic Fort Ltd are introducing a new design incorporating fibre-optic techniques. The Flexible or semi-rigid light guides can be obtained in a choice of thicknesses, and up to 1800 mm long. Because the light is 'cold' it would be ideal for illuminating areas sensitive to heat, particularly microscopic

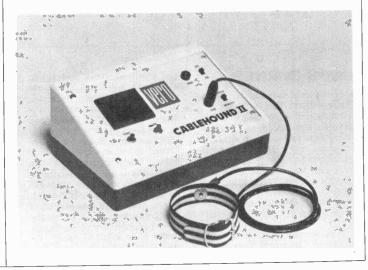
work. The light sources are available in a variety of ratings, from 50 to 250 Watts. The boxes will work on an AC supply of 110-240V (selectable) 50/60 Hz. The Tungsten-Halogen lamps are fully adjustable for brightness and are cooled by fan to prevent over-heating. Prices for the light sources start at around £145, call Optronic Fort Ltd at Cambridge Science Parl, Cambridge CB44BH for more information.



TROUBLE LOOMING?...

Anyone who has ever had to build up, or fault find a wiring loom will realise how useful the Vero Cablehound promises to be. It works by connecting one end of the loom to the unit and a wrist strap from the Cablehound to the operator. Particular wires can be identified simply by touching each wire in turn. Another feature is the

inclusion of a digital readout to further identify individual wires. Two or more Cable-Hounds can be connected together to increase the loom identification size from 100 to 10 000 separate wires (or more if further units are added). Vero Systems Ltd will be only too pleased to supply any more details, contact them at 362 Spring Road, Sholing, Southampton, Hampshire.



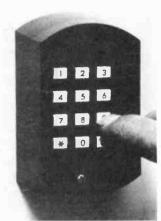
....news digest.....



GATES ON YOUR DOORS

Two interesting devices to grace your front door have been announced by Optimisation Ltd (45 South Street, Bishops Stortford, Herts). The first is the 'Door Guard', a calculator sized, fifteen digit keyboard. A caller is required to enter a three digit number whereupon a chime will sound. Should an incorrect number be pressed a piercing 96 dB siren will start, enough to deter even the most determined intruder. There are 2730 user pre-settable combinations, so the chances of a 'lucky guess' are almost negligable.

Another useful feature is the possibility of using the Door Guard for signalling departures, a good idea if there are children about. The device should be on sale by the time



you read this, asking price — £14.95, installation should take only minutes and is powered by a 9V alkaline battery, with average use it will last for over one year.

LCD MULTIMETER

It's a fair bet that 1979 will see the digital multimeter make it's long awaited debut into the amateur market. It's true that one or two examples have appeared in the low price bracket, but have rarely been as good as an analogue meter of the same price. Data Precision hope to change all that with the introduction of their model 935. It features a 31/2 digit LCD display with a claimed 0.1% basic accuracy. The unit has 29 ranges what the selectable by manufacturers call 'ergonomically designed' pushbutton switches. The device is fully protected over current and voltage and short duration high viltage transients. A standard 9V alkaline battery (PP9) should give over 200 hours of useful life, battery and over current fuses are accessible through a removable hatch, a replacement fuse is also located under the hatch.

Optional extras include high voltage, current and temperature probes, the case is claimed to be virtually unbreakable and it's small size puts it into the truely 'pocket size' class. Price is around the £99 plus VAT mark and includes leads, battery and instruction manual. If you're interested Franell International Instruments Ltd at Dandbeck Way, Wetherby, West Yorkshire, should be able to help.

The se rejoic COMP sugges lock, combin small

COMP-U-LOCK
The second piece of equipment rejoices under the name of COMP-U-LOCK. As it's name

rejoices under the name of COMP-U-LOCK. As it's name suggests this is a digital door lock, requiring a four digit combination to be entered on a small waterproof key-pad strategically placed on your front door. Included in the kit is an electric door latch, a transformer for mains operation and a battery pack for back-up in the case of a power cut. We just hope that potential users do not forget their combinations, (numbers we hasten to add) because there are over 10 000 possible sequences to try if you are locked out.

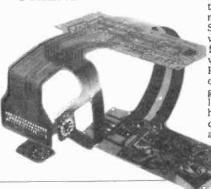
BOOK CORNER

A couple of new books from Babani have just arrived, the first is called Practical Electronic Calculations and Formulae. Just crammed with all those obscure and elusive equations you'll probably only need once, but can never find (it's got plenty of the more mundane ones too). Definitely one for the workshop bookshelf. Order number is: BP 53 and it costs £2.25.

The second new publication is 'Your Electronic Calculator

and your Money', the book, although well written (both books are written by F. A. Wilson) is just a trifle outdated, especially in these days of pre-packaged software for MPU systems. But for the confirmed calculator addict, particularly one who can't afford an MPU this book is a veritable mine of information. It shows in detail calculations for mortgages, profit and loss etc, all of which can be carried out on the most rudimentary of machines. Order code is BP 54 and it will retail for £1.35.

YOUR FLEXIBLE FRIEND



Flexible printed circuit boards have been around for some years now, so what's new? Well the one shown is the first to meet stringent new British Standard specifications. Welwyn the resistor people are the first British company to meet with BS 9765 approval. Flexible PCBs offer several advantages over conventional SRBP or glass fibre boards, they are lighter, smaller and allow better heat dissipation and are particularly suitable for wiring loom applications.

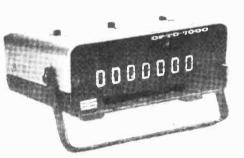
FREQUENCY COUNTING BREAKTHROUGHS

ADVANCING THE-STATE-OF-THE-ART IN FREQUENCY COUNTERS - INTRODUCING NEW LSI TECHNOLOGY COUNTERS AT AFFORDABLE PRICES.

MODEL OPTO 7000 7 Digits AC/DC/Portable MINIATURE 10 Hz to 600 MHz COUNTER + 1 ppm TCXO ONLY £99.00 + £3 p&p + 8% VAT

The go anywhere portable counter that gives you more range, visibility, accuracy and versatility than any comparable unit at anywhere near its low, low price.

- De-luxe black and gold anodized aluminium case combination handle/tilt-up bail
- Built-in pre-scaler and preamps standard
- Automatic Decimal placement
- No direct-connect required for RF pick-up
- Built-in amplifiers in both direct and pre-scale input circuits
- Signal inputs diode/overload protected
- DC power plug and chord included
- Built-in Ni-Cad rechargeable battery pack & charger (optional) £16.00
- Rear panel switch (S4) for 1 Hz resolution (optional) #5.00



Ex Stock Delivery Subject to availability

SPECIFICATIONS

10 Hz to 60 MHz (65 MHz Typical) 10 MHz to 600 MHz Guaranteed

(10 MHz to 700 MHz Typical)

Input Impedance:

1 megohm shunted by 20 pf (60 MHz input) 50 ohm (600 MHz input)

Input Protection:

1 megohm/60 MHz input - 100V up to 10 MHz 50V up to 60 MHz

50 ohm/600 MHz input - 2V max.

100 millisecond (1/10 second)

(Switch Selectable)

1 second

Resolution

1 Hz (10 Hz to 6 MHz) with switch (S4) Option 10 Hz [10 Hz to 60 MHz]

100 Hz (10 MHz to 600 MHz)

Sensitivity

<10 mV to 60 MHz 25 mV to 150 MHz 50 mV 450 MHz typ (<75 mV Guaranteed)

Quartz Crystal, 5.24288 MHz, TCXO, first

Time Base

order linear compensation

*1 count. Temperature stability and aging 08PPM/CO (± 1 PPM 200 to 400C, Typ.)

Temp. Stability: Aging:

< 2 PPM/year

Display

7, .4" Red LED Digits

Decimal Point: Connectors

Auto Placement

BNC type

Power Requirement: 1.5 Watts 7.5 - 15V AC/DC < 250 ma

*4 - AA Ni-Cad, Constant Current Charger

Weight

1.3/4"H v 4.1/4"W x 5.1/4"D

14 oz (17 oz. with batteries & charger) 'Optional - not included with basic

Also available from retailers AUDIO ELECTRONICS

301 Edgeware Road, London, W2 and Z & I AERO SERVICES 85 Tottenham Ct. Road, London, W.1

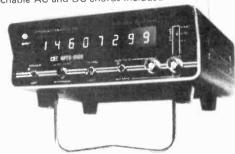
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Maclin-Zand Electronics Ltd., 38 Mount Pleasant, London WC1X OAP Tel: 01-837 1165 or Hemel Hempstead 832 966 MODEL OPTO 8000.1A Mains/DC/Portable 8 Digits 10 Hz to 600 MHz FREQ. COUNTER 1-1 ppm TCXO ONLY £240.00 £5 p&p+ 8% VAT

The OPTO 8000 1A is a no compromise professional quality counter. Thanks to new CMOS LSI technology, size, power and cost have shrunk while performance improved. The OPTO 8000 1A combines this new technology with careful circuit design and unique packaging for a state-of-the-art counter that sets the pace.

- Selectable step attenuation X1, X10, X100
- 50 ohm and 1 Megohm inputs diode protected against overload
- Amplifier circuits for Super Sensitivity
- Front panel features "Lead Zero Blanking Control" and LED gate period indicator.
- Built-in Ni-Cad rechargeable battery pack & charger (optional)
- Detachable AC and DC chords included



SPECIFICATIONS

Frequency Range

10 Hz to 600 MHz in two over-lapping ranges.

1 Megohm input - 10 Hz to 60 MHz 50 Ohm input - 20 MHz to 600 MHz

Gate Times: (Switch Selectable)

100 milliseconds (1/10 second) 1 second

Resolution Display

1 Hz to 60 MHz. 10 Hz to 600 MHz

8 LED digits with floating decimal point. Flashing LED gate period indicator

TIME BASE

5 242880 MHz

Frequency

Aging:

TCXO (Temperature Compensated Crystal

less than .1 ppm from 17° to 40° C less than 1.0 ppm from 0° to 60° C

less than 1.0 ppm first year. (less than 1.0 ppm

first three years typical) less than 0.5 ppm per year thereafter

less than 0.5 Hz at 25° C

External adjustment

range

Impedance

Connectors

Dimensions:

1 Megohm shunted by 20pF, DC coupled (10 Hz to 60 MHz) 50 Ohm, AC coupled (20 MHz to 600 MHz)

BNC type 2 - 10 MV RMS below 150 MHz

Typical Sensitivity: 10 - 50 MV RMS below 600 MHz

1 Meg input - 100 V peak to peak up to 10 MHz Max Input Signal 50 V peak to peak up to 60 MHz 50 Ohm input - 2 V peak to peak max.

220-250V AC nominal, 50 Hz, 2 Watts

8 to 16 VDC, 300 MA or internal batteries

3-1/4" H x 7-1/4" W x 6-3/4" D Approximately 2.5 pounds

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33/35 CARDIFF ROAD, WATFORD, HERTS, ENGLAND	AC117* 35 BC169C 44 BF178* 25 MPSA70 34 TIS45 45 2N2219A* 22 AC125* 20 BC170 18 BF178* 36 MPSA70 34 TIS45 45 2N2219A* 22
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Nearest Underground/BR Station: Watford High Street. Den Monday to Saturday. Ample Free Car Parking space available.	ACY39± 78 BC214 9 BF259* 30 OC44± 31 ZTX311 17 2N3053± 20 ACY31± 78 BC214K 9 BF259* 30 OC45± 28 ZTX314 24 2N3054± 85
POLYESTER CAPACITORS: Axial lead type, (Values are in µF). 400V: 0-001, 0-0015, 0-0022, 0-0033, 0-0047, 0-0068, 0-01, 0-015, Bp ; 0-018 10p ; 0-022,	ACY44# 39 BC214L 10 BF394 27 OC70# 28 ZTX326 40 2N3108 32 AD149 70 BC307B 14 BF594 40 OC71# 28 ZTX341 201 2N3442 440 OC71# 2
0.033, 11p; 0.047, 0.068 14p; 0.1, 17p; 0.15, 0.22, 24p; 0.33, 0.47 42p; 0.68 48p. 160V: 0.039, 0.15, 0.22 11p; 0.33, 0.47 19p; 0.68, 1.0 22p; 1.5 28p; 2.2 32p. 4-7 48p.	AD161 ± 42 BC308 13 BF595 38 OC72 ± 42 ZTX500 15 2N3563 20 AD162 ± 42 BC327 15 BFR39 25 OC74 ± 55 ZTX501 14 2N3614 288
POLYESTER RADIAL LEAD (Values in u.F.). 250V:	AF114# 30 BC338 12 BFR41 28 OC76# 38 ZTX503 15 2N3663# 26
13p; 0-47 17p; 0-68 9p; 1-0 22p; 1-5 30p; 2-2 34p.	AF116# 30 BC461# 36 BFR80 28 OC79# 76 ZTX531 25 2N3703 111 AF117# 30 BC477# 25 BFR81 28 OC81D# 76 ZTX550 25 2N3703 111
ELECTROLYTIC CAPACITORS: Axial lead type (Values are in μF). 500V: 10 40p; 47 68p; 250V: 100 68p; 63V: 0.47, 1.0, 6.5, 2.2, 3.3, 4.7, 6.8, 8. 10, 15, 22, 6p; 47, 32, 11p; 63, 100, 27p; 50V; 50, 100, 270; 260; 470, 32, 110; 63, 100, 27p; 50V; 50, 100, 27p; 50V; 50V; 50V; 50V; 50V; 50V; 50V; 50V	AF121# 48 BC548 12 BFX29# 28 OC83# 48 40251# 97 2N3706 11
7p: 330, 470, 32p: 1000, 80p: 284/-10, 22, 47, ep. 90, 100, 12p; 2200, 3300, 68p; 4700, 65p; 36V: 10, 33,	AF125# 35 BC557 13 BFX84# 26 OC122# 48 40313# 125 2N3708 11
14p; 470, 16p; 1000, 1500, 20p; 2200, 34p; 10V; 100, 6p; 640, 12p; 100, 125, 8p; 220, 330, TAG-END TYPE; 70V; 2000, 89a; 4700, 135p; 80V; 10, 000, 245a; 480, 2500, 67a, 2000, 47a, 47a, 47a, 47a, 47a, 47a, 47a, 47a	AF127# 35 BC559 20 BFX86# 28 OC139# 110 40316# 85 283710 18 AF139# 36 BCY30# 57 BFX87# 28 OC140# 110 40316# 82 283711 12
TANTALINA BEAD CARGOTTO	AF180± 70 BCY39± 80 BFX88± 28 OC141± 110 40319± 71 2N3771± 276. AF180± 70 BCY39± 80 BFY18± 50 OC170± 40 40320± 56 2N3772± 185
38V: 0.1 μF, 0.22, 0.33, 0.47, 0.68. Carbon Track, 1/4W Log & 1/2W Linear ELECTRONICS ±	AF239# 42 BCY42# 48 BFY51# 20 OC200# 48 40324# 80 2N3773# 288 AFZ11 128 BCY43# 75 BFY52# 20 OC200# 48 40324# 82 2N3819 22
20V: 1-5, 16V: 10 μF 13p each. 9 TIL 203 Red 13p TIL 203 Red 13p TIL 203 Red 13p KΩ-2MΩ single gang 27p TIL 211 Grn 17p	ASY26# 40 BCY58# 90 BFY53# 28 OC204# 85 40327# 62 2N3823# 95 ASY27# 45 BCY59# 90 BFY55# 45 SJE5039# 95 40347# 80 2N3824# 70
6V: 47, 68, 100 30p; 3V: 100 20p. 5KΩ-2MΩ single gang D/P switch 65p 7Rp-1212 Yellow 18p 5KΩ-2MΩ dual gang stereo 78p 2" Red 14p	ASY50# 95 BCY71# 15 BFY64# 40 TIP29 43 40348# 105 2N3866# 90 ASY76# 95 BCY71# 20 BFY71# 20 TIP29A 44 40360# 43 2N3903 20
100V: 0.001, 0.002, 0.005, 0.01 µF 6p 0.25W log and linear values 60mm Spare Clips 2p	BC107# 9 BCY78# 20 BSX20# 18 TIP29C 60 40362# 48 2N3905 18 BC107B# 10 BCZ11 145 BSX26# 75 TIP30 47 40406# 48 2N3905 17
0.1 μF, 0-2 Sp. 60V: 0.47 μF 12p 10KΩ-500KΩ single gang 10KΩ-500KΩ dual gang 80p 0CP71 120p	BC108# 9 BD115# 62 BSX29# 43 TP30A 50 40407# 50 2N4037# 52 BC1088# 12 BD121# 78 BSX78# 55 TIP30B 64 40408# 70 2N4041# 80
CERAMIC CAPACITORS SQV Self Stick Graduated Bezeis 22p ORP61 85p ORP61 0.000 OR912 6.3p O.015 0.022 0.023 0.033 PRESE POTENTION STREET 2.000 2.000 2.000 0	BC109# 9 BD124# 115 BU105# 140 TIP31# 50 40412# 65 2N4058# 17 BC109# 9 BN131# 45 BU105# 140 TIP31# 50 40412# 65 2N4061 17
0.047 μF 4p; 0.1 μF 6p 0.1 W 50Ω — 5MΩ Miniature Vertical 7 Segment 0 isplays	BC109C# 12 BD132# 45 BU208 228 TIP318# 56 40594# 90 2N4064# 120 BC113 20 BD133# 43 E421 96 TIP31C# 66 40595# 98 2N4069 48
SILVER MICA (Values in pF) 3-3, 4-7, 0-25W 100Ω—3-3MΩ horiz. larger 10p TIL312.3" CA 105p 6-8, 10, 12, 18, 22, 33, 47, 50, 68, 75. 0-25W 200Ω—4-7MΩ Var.	BC114 19 8D135 38 E113 95 TIP32 55 40603 65 2N4236 145 BC115 19 BD136 37 E5567 66 TIP32A 58 40636 125 2N4286 20
250, 270, 300, 330, 360, 390, RESISTORS — Erie make 5% Carbon TIL322.5"CC 115p	BC1.17 20 BD138# 50 ME1120 25 TIP32C# 75 2N697# 25 2N4859 65 BC118 19 BD139# 40 ME4102 10 TIP33# 80 2N698# 44 2N6934
1000, 1200, 1800, 2000 20p each DL707 .3" CA 99p	BC119# 28 BD140# 36 ME6002 40 TIP33A# 85 2N699# 54 2N5135 42 BC134 19 BD142# 59 MJ400# 90 TIP33B# 100 2N706A# 19 2N5136 42
10pF to 1nF 8p; 1.5nF to 47nF 10p	30.135 20 BD144\times 198 MJ491\times 160 TIP33C\times 105 2N707\times 50 2N5138 20 BD145\times 198 MJ2955\times 99 TIP34\times 85 2N708\times 19 2N5172 24
2.5-6pF; 3-10pF; 10-40pF 22p 2%Metal Film 100-11M0 6p 4p IL 32 Infra-Red 58p 15-25pF; 5-45pF; 60-5; 69	3C140± 28 BD205± 110 MJE370± 55 TIP34B± 110 2N916± 27 2N5180± 60 BD378± 65 MJE371± 60 TIP34C± 110 2N918± 4012N5191± 70
COMPRESSION TRIMMERS 100 + price applies to Resistors of each type not mixed values. OPTO	3C143 ± 25 BU534 42 MJE520± 65 TIP35± 179 2N920± 51 2N5305± 40 BD517± 65 MJE521± 74 TIP35A 185 2N930± 18 2N5457 32
100-500pF 45p; 1250pF 65p THERMISTORS: VA1034 1039 IL74 48p	0C148 7 BD696A± 65 MJE3055± 70 TIP35C± 220 2N1132± 22 2N5458 32 3C148B 10 BDY11 220 MPF102 86 TIP36± 210 2N1303± 50 2N5459 32
1GS 812 & 813 415p; Socket 25p 1098, 1100 20p each. TH.114 95p	10 8DY17* 195 MPF103 36 TIP36A* 220 2N1304* 50 2N5777* 46 3C149 8 BDY60* 110 MPF104 36 TIP36B* 230 2N1305* 28 2N6027 40
Dielectric 0 2 365pF with slow DIODES *BRIDGE INTERSIL	10 051014 100 MPF105 38 TIP36C* 255 2N1306* 36 2N6109 50 10153 27 8F154* 38 MPF106 50 TIP41A* 63 2N1307* 50 2SD234* 50
1007300pF 140p motion Drive 325p AA119 18 RECTIFIERS Evaluation 165p 00 208/176 285p AAZ15 15 (plastic case) p	C157 10 BF158* 29 MPS3904 40 TIP42A* 64 2N1613* 23 3N140* 112 C158 11 BF160 30 MPSA05 26 TIP42B* 82 2N1670* 180
4511/DAF 115p* motion drive 325p 8Y126 12 1A/100V 22 LED 2633p LED 2183a	C159 11 8F161 60 MPSA06 25 TIP2955 63 2N16718± 215 Mauchaid C1604 42 8F167 30 MPSA12 42 TIP2955 63 2N2160± 380 Pair C167A 11 8F173 ± 25 MPSA15 25 TISA3 24 29237 3 20 200 20 20 20 20 20 20 20 20 20 20 20
6:1/36:1 650p* 25:50pF 175p* CR033* 148 148 129 14/400V 25 14/400V 25 15/25 100, 150pF 215p* 0A9 75 14/200V 25 17/20 15/25 100, 150pF 215p* 0A9 75 15/25 100 16/200V 25 15/25 100	* 452 NE566* 160 T 74 7482 69 74175 87 142 98 175 110
00 2 365pF 275p 00-3x25pF 430p 0A47 12 2A/50V 35 709C 8 pin 35 LM3C 0A70 12 2A/100V 44 710+ 67 LM3C	H* 170 NE570* 375 (TEXAS) 7484 95 74177 78 48 120 183 298
DENCO COILS RDT2 92p OA79 15 2A/200V 46 723±14 pin 45 UM30	T 110 RAM2102-2* 150 7401 13 7486 31 74181 166 51 24 191 140 * 120 RC4136D 120 7402 14 7480 31 74181 166 51 24 191 140
Range 1-5 B,Y,R,W RFC 7 (19mH) 96p OA90 7 4A/100V 72 7747ch 14 pin 70 LM31	HR 206 SAU 10/24A* 1450 7403 14 7490 33 74184 135 55 30 193 130 195 SG3402* 295 7404 14 7491 75 74185 135 63 150 194 186
1-5 Green 92p 1FT 18/1.6 99p 0A95 8 4A/400V 79 753 8 pin 150 UM32 1-5 Green 92p 1FT 18/465 105p 0A200 9 4A/600V 105 810 159 UM33	* 125 SN76013 140 7406 38 7493 32 74190 95 74 41 196 100 * 70 SN76018* 148 7407 38 7494 78 74192 98 75 48 197 140
86p IN914 4 6A/100V 73 AY-1-1313A 660 LM34	* 90 SN/5023 140 /408 17 7495 65 74193 98 76 40 221 96
RF CHOKES N4001/2±5 6A/400V 85 AY-1-5050 180 LM38 AY-1-5051 145 LM38 AY-1-5051	90 SN76131* 110 7411 20 74100 119 74196 93 85 118 242 232 N 145 SN76227N 115 7412 17 74104 82 74197 90 93 85 1242 232
1 µH. 4.7 10. 22. 33. 47. 100. 200. 470 750, 1mH. 25. 5. 10 35p each 1N4006/7**7 NHBDIL 40 AY-38721/6 195 AY-38500* 390 NH4188 4 AY-51224A*260 IM3804 AY-51224A*260 IM3904/5**6	122 SN76477* 226 7413 30 74105 62 74198 150 90 38 245 270 8* 50 SN76660* 90 7414 51 74107 29 74279 119 91 104 247 190
VEROBOARD ± 0.1 0.15 0.15 S44 20 ZENERS AY-5-1230 ± 450 LM39 AY-5-1315 AY-5-13	9N# 70 TAA621AX1 228 7417 30 74110 54 74365 128 93 89 249 190
(copper clad) (plain) 2½ x 3¾" 46p 39p 24p 3A/400N 20 2½ x 5" 55p 50p 31p 3A/400N 20 8 peach 4X-53500 510 M252	A± 750 TAA700 363 7421 29 74116 198 74367 115 96 116 253 142 A± 795 TAD100 159 7422 24 74118 83 74368 124 107 44 257 110
3½ x 3¾" 55p 50p — 3A/1000M 30 33V 13W AY-5-4007D 650 MC13 3½ x 5″ 62p 67p 43p 64/600 30 33V 13W	275 18A1205 70 7423 27 74120 118 74393 184 109 55 258 110 3 88 78A5400 220 7425 27 74121 25 75150 120 112 55 259 180
3½ x 17" 16%p 135p 92p NOISE CA3012# 150 MC13	0P 149 TBA641-A12 7427 27 74123 48 75491 00 114 50 266 52 2PQ 195 BX or BX11 250 7428 35 74125 38 75492 00 122 70 273
Pit of 35 pins Spot face cutter Section Column Col	8* 85 TBA651 180 7430 17 74126 57 74LS* 123 70 275 280 9* 90 TBA800 90 7432 25 74128 74 74LS* 124 180 279 66
Pin insertion tool 120p MVAM2 135 0.6A200V 30 CA3028A± 80 MC14 MVAM115 0.8A100V 30 CA3035 240 MC14	331 1250 188810 95 7433 40 74132 73 00 13 125 60 283 192 5* 350 TBA820 70 7437 30 74141 56 01 13 126 60 290 128
Plus Spool 325p BA102 25 1A100V 42 CA3043 190 MC33	OP* 120 TBA990Q 395 7440 17 74143 314 03 14 136 55 295 185 OP 120 TCA270Q 220 7441 74 74144 314 04 14 138 85 298 168
Spare spool (Wire) 80p ★ Combs 7p each BB104 40 1A600V 70 CA3045 140 MC24	1 52 TDA1004* 290 7442 68 74145 65 05 23 139 85 324 240 3* 135 TDA1008* 310 7443 115 74147 175 08 22 145 108 325 290
11b bag Anhydrous 65p + 35p P& P TRIACS★ 8A300V 48 CA3075 175 MFC6 RA500V 58 CA3080E★ 70 MK50	40* 97 TDA2020 320 7445 94 74150 99 10 20 148 173 327 286 53* 650 TL061CP* 76 7446 94 74151 64 11 22 151 96 347 148
75p 3A400V 50 12A300V 59 CA3081 190 MK50	62# 650 TL062CP# 125 7447 82 74153 64 12 23 153 76 348 186 98* 635 TL064CN* 199 7448 56 74154 96 13 38 155 96 352 228
Fibre Single Double SRBP 8A400V 64 12A800V 120 CA3090AQ 398 MM52	73* 835 1LU71CP* 60 7450 17 74155 53 14 75 156 96 353 228 7451 7451 74156 80 15 30 157 76 365 65
Glass sided sided 7.5"x7.5" 12A100V 60 BT116 150 CA3130\(\preced{h}\) 85 NE516 6" x 6" 75p 90p 60p 12A400V 70 C106D 38 CA3140\(\preced{h}\) 70 NE543	80 TLO81CP# 62 7454 17 74160 82 21 22 160 128 367 65 210 TLO82CP# 96 7460 17 74161 92 26 48 161 98 368 66
12A800V TIC44 22 F944DC 60 NE544 DIL SOCKET8*Low Profile (TEXAS) 15A100V 789 TIC45 25 ICL7106* 795 NE555	* 185 TL083CP* 105 7470 28 74163 92 27 28 162 138 373 180 * 22 TL084CN* 130 7472 25 74164 105 28 48 163 102 374 180
20p; 20 pin 27p; 22 pin 30p; 24 pin 30p; 24 pin 30p; 25 pin 16A400V 105 2N5064 36 (CL8038CC* 336 NE566 16A500V 120 (CM7205* 1150 NE561	30 UAA170 198 7474 37 74166 105 3D 22 164 116 375 160 32 32 UAA180 198 7474 27 74166 140 32 27 165 75 377 212
25A500V 235 SOLDERCON PINS* 25A800V 295 DIAC* ICM7215* 1060 NE564	3* 410 ZN424E* 130 7476 38 74172 625 37 39 170 288 379 215 425 ZN425E* 415 7480 48 74173 120 38 39 173 105 384 88
100 pins 50p 500 pins 200p 40669 99 ST2 20 ICM7555* 89 NE565	A* 120 ZN1D34E* 200 7481 86 74174 87 40 28 174 108 390 230

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12p 10p 6p

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	SPST	28p:
1	DPDT	38p
1	4 pole on / off	54p
_	SP changeover	59p
	SPST on/off SPST biased	54p 85p
7	DPDT 6 tags DPDT centre off	70p 79p

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12V-5A 15V-5A: 15V-4A 15V-4A 20V-3A
20V. 3A
20V. 3A
20V. 3A
20V. 15A 6V-1.5A 6V-1.5A: 9V-1.3A 20V-1.3A:
12V-1A: 12V-1A: 15V-8A 15V-78A: 20V-6A
60VA: 6V-4A 6V-4A: 9V-2.5A 9V-2.5A: 12V-2A
12V-2A: 15V-1.5A 15V-1.5A: 20V-1.2A 20V-1.2A: 25V-1A 25V-1A: 30V-8A 30V-8A
10V-2A: 12V-4A 12V-4B 15V-3A (50 pA)
100VA: 12V-4A 12V-4B 15V-3A 50V-1A
20V-1.5A 20V-1.5A: 50V-1A 50V-1A 50V-1A
60V-1.25A 20V-2.5A: 30V-1.5A 50V-1A
60V-1.25A 20V-2.5A: 30V-1.5A 50V-1A
60V-1.25A 20V-2.5A: 30V-1.5A 50V-1A
60V-1.25A 20V-2.5A: 30V-1.5A 50V-1A
60V-1.25A 40V-1.25A: 50V-1A 50V-1A
60V-1.25A 40V-1.25A: 50V-1A 50V-1A
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I55KHz	385
MHz	323
.0008M	395
3.2768M	323
1.032MHz	323
4.433619M	135
5.OMHz	356
8.08333M	275
IO.OMHz	323
10.7MHz	323
18 432M	323

00KHz 05KHz MHz 0008M 2768M 032MHz 433619M	385 385 323 395 323 323 135	350r 100VA: 12V-4A 12V-4A; 15V-37 20V-2 5A 20V-2 5A; 30V-1.5A 40V-1.25A 40V-1.25A; 50V-1A 50' (60p p&p), (N.B. p&p charge to be all our normal postal charge.)
0MHz 08333M	356 275	VOLTAGE REGULATORS *
O.OM Hz	323	1A TO3 + ve — ve 5V 7805 145p 7905
0.7MHz 8.432M	323	5V 7805 145p 7905 12V 7812 145p 7912
D.OMHz	323	15V 7815 145p
7.648M	323	18V 7818 145p 1A TO220 Plastic Casing
B.OMHz	323	TA TUZZU Plastic Casing

20.0MHz 27.648M 48.0MHz	323 323 323
ETI Projet Parts ave for: Eliminate Ambush, tar Effec Unit. SAE plus 5p for lis	cliable Click or Gui- t Send
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27.648M 48.0MHz	323 323
ETI Proje Parts ava for: Eliminate Ambush, tar Effec Unit. SAE plus 5p for lis	ilable Click or Gui- t Send
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450p★ per pair

.OMHz 323	1A T	
Il Projects: erts available r: Click	12V 7 15V 7 18V 7 24V 7	71
iminator mbush, Gui- r Effect nit. Send AE plus p for list.	12V	71
JLTRASONIC FRANS- DUCERS	LM309 LM309 LM317 LM323	1

3 1	157	7815	149p	
3 3	18V	7818	145p	
3	1A	TO220	Plastic	: Casing
-	5V	7805	80p	7905
- 1	12V	7812	80p	7912
	15V	7815	80p	7915
	18V	7818	85p	7918
k	24V	7824	85p	7924
	100m	A TO9	2 Plastic	Casing
i- i	5V	78L05	30p	79L05
	6V	78L62	30p	
d	87	78L82	30p	
-	12V	78L12	30p	79L12
	15V	78L15	30p	79L15
	- LM 30	YOH 17		LM327
_	LM30		LO _{ID}	LM723
2	LM30		5o	MVR5
	LM3		50p	MVR12
	LM3	1/K 3%	yup .	

, ,05, 006		
OmA TO92 Plast	ic Casing	
V 78L05 30p	79L05	65p
V 78L62 30p		_
78L82 30p		_
V 78L12 30p	79L12	65p
V 78L15 30p	79L15	65p
1300H 170p	LM327	270p
4305H 140p	LM723	43p
4309K 135p	MVR5	180p
//317K 350p	MVR12	180p
	TAA550	50p
	TBA625B	95p
4325N 240p	TDA1412	150p
4326N 240p	TUAT412	тэор

ŀ	1A	TO220	Plastic (ic Casing			25		
l	5V	7805	80p	7905		}p		16	
	12V	7812	80u	7912)p		80	
		7815	80p	7915 7918	90	Op		108	
1	18V	7818	85p	7918	3 90	Dip		16	
ŀ	24V	7824	85p	7924	1 90	Op		64	
١	100mA	TO 92	Plastic (Casing		- 1		127	
i	5V	78L05	30p	79L05	6 :	5p		47	
ı		78L62	30p			- 1	74	S188	
١	87	78L82	30p			- 1	74	S262	
١	12V	78L12	30p	79L12	2 6	50 l	7.4	S287	
I	15V	78L15	30p	79L1		5p	74	15470	
Ì				M327	27		74	15475	
d	FW 300		TP	M723		3p	81	LS95	
1	LM30		P	IVR5		0p	81	LS96	
i	LM 30		T	IVR12		00	81	LS97	
ı	LM31		AA550		00	99	900		
ı	LM32		Ψ	BA625B		5p		MS601	11
	LM32		~ -	DA1412		Op	Z8	30	
	LM32	6N 240)p	UAT412	13	ор		-	_
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	91	4049	48	4093	85	449	OF	695	ď
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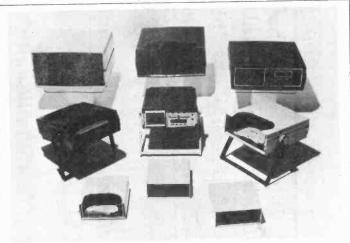
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_		4031	205	4063	110	4174	110	4512	98	ı
4000	15	4032	100	4066	58	4175	99	4513	206	ł
4001		4033	145	4067	380	4194	108	4514	265	ł
4002	17	4034	196	4068	22	4408	720	4515	299	ı
4006	105	4035	111	4069	20	4409	720	4516	125	ł
4007	18	4D36	325	4070	32	4410	720	4517	382	ı
4008	87	4037	100	4071	21	4412F	1650	4518	102	ı
4009	50	4038	108	4072	21	4412V	1380	4519	55	ı
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4011	16	4040	105	4075	23	44 15V	795	4521	188	
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4016	44	4044	145	4082	21	4440	1275	4530	85	١
4017	89	4045	145	1 -002						į

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CASE FOR TREATMENT

Some good looking new boxes from the OK Machine & Tool (UK) Ltd., there are over 25 sizes available with numerous variations to accommodate printers, terminals, clocks etc. Moulded from tough ABS plastic they are all dust and splashproof. All the cases come in a choice of 3 colours, black, blue, or beige. The range is called 'Pac Tec' and is denoted the C series. OK will be delighted to help you. They live at 48a The Avenue, Southampton, Hants, SOI 2SY.

KEY BAUD?

A new Keyboard Terminal module has just come to our attention, it features all the currently favoured features and will interface with any RS232 computer (SYM-1 etc) up to 9600 Baud. The terminal boasts 128 graphic characters on a 40 character by 24 line format, each character having an 8x8 dot matrix. At £218 it's got to be the bargain of the month as the postage is free. Rostra Electronics can help with any queries - they can be found at: 275-281 aking Street, Hammersmith, London W6.



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7401 14p 7402 14p -7403 14p	74191 90 9 74192 90 9 74193 90 9	FULL 74L8 SERIES	9301 160p 9302 175p 9308 316p 9310 275p	2½ x 3% 41p 33p 2½ x 5 49p 45p 3% x 3% 49p 45p	AC127/8 20p AC176 25p AC287/8 25p	BFX84/5 30p 8FX86/7 30p 8FX88 30p	TIP41C 78p TIP42A 70p TIP42C 82p	*2N3903/4 18p *2N3905/6	DIODES *BY127 12p *0A47 Sp	*ZENERS 2.7V-33V 400mW \$p
7404 14p 74S04 90p 7405 18p	74194 100p 74195 95p 74196 95p 74197 80p	4000 SERIES 4000 150	9311 275 p 9312 160 p 9314 165 p	3% x 5 56p 50p 2½ x 17 152p 121p 3% x 17 195p 163p	AF116/7 30p AD149 70p AD161/2 45p 8C107/8 11p	BFW10 90p BFY50 22p BFY51/2 22p BFY56 33p	TIP2955 78p TIP3055 70p TIS43 34p TIS93 30p	20p 2N4036 65p 2N4058/9	*0A81 15p *0A85 15p *0A90 9p	1W 15p
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7410 15p 7411 24p 7412 20p	74221 150 p 74251 140 p 74259 250 p	4007 18p 4008 80p 4009 40p	9334 225 p 9368 200 p 9370 200 p	VERO WIRING PEN Plus Spool 325p	BC147/8 9p 8C149 10p BC157/8 10p	BSX19/2020p BU104 225p '8U105 190p	*ZTX502 18p *2N4123 *ZTX504 30p	*2N4123/4 *2N4125/6	*1N914 4p *1N916 7p *1N4148 4p	3A 400V 60p 3A 500V 65p 6A 400V 70p
7413 30p 7414 50p 7416 27p	74265 90 p 74278 290 p 74279 110 p	4010 50p 4011 17p 4012 18p 4013 50p	9374 200 p	Spare spool (wire) 80p Combs 7p each	BC159 11p BC169C 12p BC172 12p	*8U108 250p BU109 225p *8U205 200p	2N696 35p 2N697 25p 2N698 45p	22p 2N4289 20p 2N4401/3	1N4001/2 5p 1N4003/4 6p 1N4005 5p	6A 500V 88p 8A 400V 75p 8A 500V 95p 12A 400V 85p
7417 27p 7420 17p 7421 40p	74283 190 p 74284 400 p 74285 400 p	4014	'AY1-0212 600 'AY1-1313 668	p. NE531 110p	BC177/8 17p BC179 18p BC182L 10p	*8U208 200p *BU406 145p MJ481 175p MJ491 200p	2N706A 20p 2N708A 20p 2N918 45p	27p 2N4427 90p 2N4871 60p	1N4006/7 7p 1N5401/3 14p 1N5404/7 19p	12A 400V 85p 12A 500V 105p 16A 400V 110p 16A 500V 130p
7422 22p 7423 34p 7425 30p	74290 150p 74293 150p 74294 200p 74298 200p	4017 80p 4018 80p 4019 45p	'AY1-1320 320 'AY1-5050 200 'AY5-1315 600 'AY5-1317A 636	P NE543K 225p P NE565 25p	'BC182/3 10p 'BC183L 10p '8C184L 11p BC187 30p	MJ491 200p MJ2501 225p MJ2955 100p MJ3001 225p	2N930 18p 2N1131/2 20p 2N1613 25p	*2N5087 27p *2N5089 27p *2N5172 27p	*1S920 9p	T2800D 130p
7426 40p 7427 34p 7428 36p 7430 17p	74365 120p 74366 120p 74367 120p	4020 100p 4021 110p 4022 100p	*CA3019 80 *CA3046 70 *CA3048 225	P NE561B 425p P NE5628 425p	BC212L 11p BC212 3 11p BC213L 11p	MJE340 65p MJE2955 100p	2N1711 25p 2N2102 60p 2N2160 300p	2N5179 90p 2N5191 83p 2N5194 90p 2N5245 40p	HEAT SINKS For TO220 Volt-	
7432 30p 7433 40p 7437 35p	74368 120 p 74390 200 p 74393 180 p	4023 22p 4024 50p 4025 20p 4026 130p	CA3080E 72 CA3086 48 CA3089E 225 CA3090AQ 375	NE567 178p NE571 425p	BC214 12p 8C461 36p BC477/8 30p	MJE3055 70p 'MPF102 45p 'MPF103/4 40p	2N2219A 22p 2N2222A 20p 2N2369A 10p	*2N5296 55p *2N5401 50p *2N5457/8	age Regs. and Transistors 22p For TO5 12p	THYRISTORS 1A 50V 40p 1A 400V 65p 1A 600V 70p
7438 35p 744D 17p 7441 70p 7442A 60p	74490 225p	4027 50p 4028 84p 4029 100p	CA3130E 100 CA3140E 70 CA3160E 100	SFF96364 1150p SN76003N 175p	BC516.7 50p BC5478 16p BC548C 16p BC549C 18p	*MPF105 40p MPSA06 30p *MPSA12 50p	2N2484 30p 2N2646 50p 2N2904/5 25p	*2N5459 40p *2N5460 40p 2N5485 44p		3A 400V 90p 8A 600V 140p 12A 400V 160p
7443 112p 7444 112p 7445 100p	74LS00 13p 74LS02 14p 74LS04 14p	4030 55p 4031 200p 4033 180p 4034 200p	CA3161E 150 CA3162E 450 FX209 750	P "SN76018 140p P "SN76013ND 120p P "SN76023N 140p	BC557B 18p BC558B 18p BC559C 18p	MPSA56 32p MPSU06 63p MPSU56 78p	2N2906A 24p 2N2907A 30p 2N2926 9p	"2N6027 48p 2N6247 190p 2N6254 130p	BRIDGE RECTIFIERS	16A 100V 180p 16A 400V 180p 16A 600V 220p
7445A 93p 7447A 80p 7448 80p	74LS05 25p 74LS08 22p 74LS10 20p 74LS11 40p	4035 110p 4040 100p 4041 80p	ICL7106 850 ICL8038 340 LF356P 96 LF358P 75	SN76131 110p SN76033N 175p	BCY70 18p BCY71/2 22p BC131/2 50p BD135/6 54p	OC28 130p OC35 130p 'R2008B 200p 'R2010B 200p	2N3053 22p 2N3054 65p 2N3055 48p 2N3442 140p	2N6290 65p 2N6292 65p 3N128 120p	"1A 50V 21p "1A 100V 22p "1A 400V 30p	8T106 110p C106D 45p 'MCR101 36p 2N3525 130p
7450 17p 7451 17p 7453 17p 7454 17p	74LS13 36p 74LS14 70p 74LS20 20p	4042 80 p 4043 90 p 4044 90 p	LM301A 30 LM311 120 LM318 200	P 'SP8515 750p P 'TAA621 275p	BD139 56p BD140 60p BD242 70p	*TIP29A 40p *TIP29C 55p *TIP30A 48p	2N3553 240p '2N3565 30p '2N3643/4	3N140 100p 3N141 110p 3N201 110p 40290 260p	11A 600V 35p 12A 50V 30p 12A 100V 35p	2N4444 140p '2N5060 34p '2N5064 40p
7460 17p 7470 36p 7472 30p	74LS21 40p 74LS22 28p 74LS27 38p	4046 110p 4047 100p 4048 85p 4049 40p	LM324 70 LM339 75 LM348 95	P TBA651 200p TBA800 90p TBA810 100p	BDY56 200p BF200 32p BF244B 35p	*TIP30C 60p *TIP31A 58p TIP31C 62p	*2N3702/3 12p	40360 40p 40361/2 45p 40364 120p	"2A 400V 45p "3A 200V 60p "3A 600V 72p "4A 100V 95p	
7473 34p 7474 30p 7475 38p	74LS30 22p 74LS32 27p 74LS42 95p 74LS47 90p	4060 48p 4051 80p 4052 80p	"LM377 175; LM380 75; "LM381AN 160; "LM389N 140;	TCA940 175p	*BF2568 70p 8F257/8 32p 8F259 36p *BFR39 30p	TIP32A 68p TIP32C 82p TIP33A 90p TIP33C 114p	*2N3704/5 12p *2N3706/7 14p	40408 70p 40409 65p 40410 65p 40411 300p	*4A 400V 100p 6A 50V 90p 6A 100V 100p	'LOUDSPEAKERS 2%" 64R 70p
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7483A 70p 7484 100p 7485 90p	74LS74 40p 74LS75 45p 74LS83 90p 74LS85 100p	4056 135p 4059 800p 4060 115p 4063 120p	LM733 100 LM741 20 LM747 70 LM748 35	P TL084 130 P TL170 50 P ULN2003 100 P	BFR80 30p BFR81 30p	TIP35C 290p TIP36A 270p	'2N3819 25p '2N3820 50p	40841 90 p 40871/2 90 p		
7486 30p 7489 210p 7490A 30p 7491 80p	74LS86 40p 74LS90 60p 74LS92 72p	4066 55p 4067 450p 4068 22p	LM748 35; LM3302 80; LM3900 70; LM3911 130;	XR2207 400p XR2211 800p	2102-2L 21078 2111-2	120p 500p 225p	UART AY-3-1015P AY-5-1013P IM6402	500p 400p 500p		NIATURE TCHES 51p
7492A 46p 7493A 30p 7494 84p	74LS93 60p 74LS96 75p 74LS107 45p	4069 20p 4070 30p 4071 22p 4072 22p	LM4136 120 MC1310P 150 MC1458 55	xR2240 400p 72N414 80p 72N424E 135p	2112-2 2114 4027	300p 700p 370p	TMS6011NC CHARACTE GENERATO	400p	SPDT DPDT DPDT (centre o	53p 55p
7495A 70p 7496 65p 7497 180p 74100 130p	74LS112 100p 75LS123 65p 74LS124 180p 74LS125 80p	4073 22p 4075 22p 4076 107p	MC1495L 380 'MC1496 100 'MC3340P 120 'MC3360P 120	ZN 1034E 200p 95H90 800p	4116 5101 6810	1100p 510p 350p	3257ADC MCM6576 RO-3-2513U	995p 800p	Push to make (Red, Green, Ye Push to break	
74104 65p 74105 65p 74107 34p	74LS132 95p 74LS133 60p 74LS136 55p	4081 22p 4082 22p 4093 80p 4094 175p	VOLTAGE	REGULATORS	ROM/PROI 4S188 74S287 74S387	Ms 225p 350p 350p	RO-3-2513L SN74S262A OTHER	C 650p	(Black only) CRY 100KHz 1MHz	25p BTAL\$ 300p 370p
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by film?

The various liveds of play can be changed at any time during the game and you can use the everyide key to make metigle minus of beard changes without the computer responding. The computer will only make responses which skey intervalsant class raise. Casting, we passed and premoting a pawa are all included as part of the computer's programme. It is possible to enter any given whose from mappines or extensively established met own house positions and write the computer class also add as subtract places during the pame or re-enter the board socilians to part years of their of so straining of the computer class of the part of th

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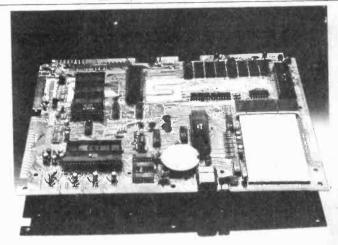
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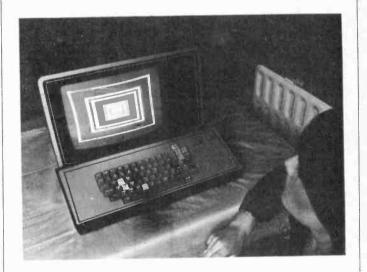
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SYM-1

AN ideal companion to the keyboard terminal (see key Baud) is the new SYM-1. MPU system. Intended clearly for the development market it should appeal to both engineers and hobbyists. The board is complete and ready to go, needing only the addition of a 5 V DC supply. The unit has 4K onboard software and 1k of static RAM. Full access is available to important busses and ports. The SYM uses the popular 6502 MPU already a firm favourite with TV games manufacturers, price is £175, post free. See Rastra Electronics for details.



UNCLE SAMS LATEST

Good to see the American built Compucolor II' is at last available in the UK. For £1,390 you get a very comprehensive system indeed. The integral VDU (8 colour) and Mini-Floppy Disk drive support the on-board 8K RAM which works in Basic. Abacus Computers Ltd will be importing the machines and examples can be seen at the Byte Shop and Trans Am of Chapel Street, London.

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M12

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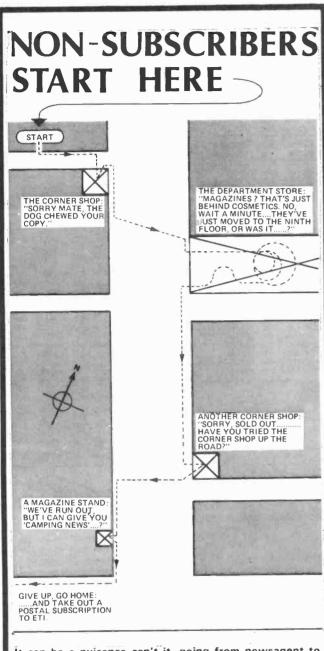


M13

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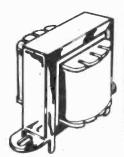
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SURFACE ACOUSTIC WAVES

Surface ustic Wave Filters (SAWFs) are a comparatively recent newcomer to the scene. They promise to revolutionise entire sections of colour TV. Richard Maybury and Peter Haywood* take a look into the workings of

RODYNE RECEIVER has been with us for now (although opinions vary as to its t time the basic concept has altered very dvent of semiconductors came Varicaping with it the demise of the mechanical t). As ICs began to appear another bulky perhet shrank dramatically — the audio however, seems to have resisted any ne good old IF, indeed many a radio nirties and forties would still recognise a stage, possibly even feel quite at home

on the operation of the IF would not is point, as most of you will realise the

superhet works by mixing the incoming RF (from the aerial through a series of RF amplifiers) with an internally generated oscillator (the 'local' oscillator usually runs at a higher frequency to that of the incoming RF, around 465 or 470 kHz in the case of an AM receiver and 10.7 MHz for FM). The oscillator 'tracks' with the RF when the tuner dial is altered the local oscillators frequency will change accordingly. The result of mixing these two frequencies is to produce a product, sum and difference output. The IF stage will reject all but the difference output, hence it is really nothing more than a highly accurate 'notch' filter, tuned in the case of AM to 465 (or 470) kHz.



conductors Ltd)

Early Days

Development work on SAWFs first began in the late sixties — the theory, however, was known as early as 1940. The SAWF is perhaps unusual in that it uses no silicon in it's construction, instead it relies on a substance called Lithium Niobate, which has very predictable piezoelectric properties. Simply explained that means it has the ability to convert electrical energy into mechanical energy and vice-versa. An electrical signal applied to the interleved Aluminium fingers (see Fig. 1.) of the input transducer sends an 'acoustic' wave across the surface of the filter and is converted back into electrical energy by a similar transducer at the other end of the device. Because the signal is acoustic it will travel slower than an equivalent electrical signal, so there is a significant delay between the input and output transducers.

A Notch In Time

Regarding the IF just as a filter can be somewhat misleading, because the accuracy and stability of an IF stage is of a very high order, and up to now could only have been achieved with a series of highly accurate LC networks. The main drawback apart from sheer physical bulk has always been the setting up needed for a conventional IF strip, often involving up to six or more separate tuning operations on sophisticated pieces of test equipment, (wobbulators or sweep-generators). With all these constraints it's not surprising that a search (mostly fruitless) has been going on for many years to find a suitable alternative; the most likely candidate looks like being the Surface Acoustic Wave Filter or SAWF for short.

Pioneering Plessey

Most of the early development work was carried out by Plessey Semiconductors Ltd at their Caswell plant about a decade ago, and in fact within three months of the research department being set up they had a working prototype. This early success led to the department being given a brief to produce a viable TV IF filter, demonstrating what had previously been possible only theoretically.

Early efforts to market SAWFs met with a slow response. This was not so much because of technical performance but because a comparison of costs showed little, if any, cost advantage of the SAWF version at that time over the conventional coil-type of IF most UK TV companies were committed to. Many TV manufacturers had invested a lot of money in coil-winding equipment and were naturally reluctant to scrap such expensive machinery.

The breakthrough came when Spain and Italy started colour TV transmissions. Because the IF is one of the most difficult areas of a TV set to design and build. (Colour TV demands a particularly high standard of IF design), the Spanish and Italian TV setmakers were saved from a difficult design problem by the use of SAWFs and sales of Plessey filters rocketed to around 70 000 a month. This naturally led to a rapid reduction in prices and gave Plessey confidence to invest further capital in setting up a high volume SAWF production plant capable of producing 10 million devices per annum.

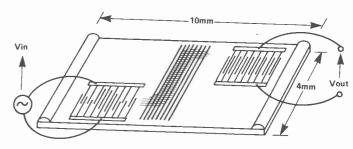


Fig. 1

Typical SAWF construction, the ridges at the two ends of the substrate act as acoustic absorbers for unwanted signals. The central electrodes serve to guide the acoustic wave from the input transducer to the output transducer.

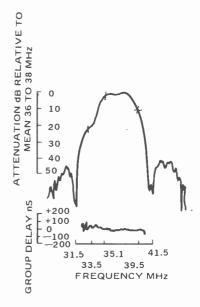


Fig. 2.

Typical response curve for a TV IF filter (Plessey), note the almost 'square' response, this kind of accuracy is nearly impossible to duplicate by conventional means.

Filtering Through

Technical refinement, and acceptance by the TV setmakers, enabled Plessey to penetrate some of the traditionally difficult markets. In the UK all but one of the TV manufacturers will be in full production with SAWFs by the end of 1979.

Although most of the initial arguments against the use of SAWF's were on economic grounds. The advantages found by users when in production are very wide ranging.

Perhaps the most commonly cited advantages are the consistently good performance, the simplicity from a production viewpoint due to the lack of adjustments and the small number of components on the IF board. Other advantages are the flexibility to change from UK standard sets to any other standard by changing the SAW filter and a few other components, and the improved reliability since the SAW filter is a robust passive component.

Construction

Basically a Surface Acoustic Wave Filter consists of Two transducers (see Fig. 1) on a piezo-electric substrate. An

applied to the input transducer electrical & causes an a vave (proportional to V in) to be propagated bis. ry along the surface of the substrate. The transducer sanerates a wave symmetrically across it's surface producing an unwanted output to the left of it's body, this is absorbed by a raised wedge to prevent any spurious reflections crossing the 'chip'. The wave to the right of the transducer is re-directed by the central coupling grid to the output transducer where it is reconverted into an electrical signal (V out). The time taken for the wave to cross the device is typically 1.6 microseconds. The input transducer generates a further unwanted signal called a Bulk Wave this, not being a surface component passes under the central coupler and misses the output transducer.

Material

The substrate material commonly used for SAWF devices is Lithium Niobate (LiNbo3) which has a very high piezo-electric coupling factor, this results in filters with a low insertion loss. Being relatively cheap and having a low temperature co-efficient make it a practical choice, although much research is being carried out at the moment into alternative materials.

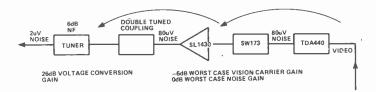


Fig. 3.

Block diagram showing diagram of SAWF within receiver design, noise levels are shown. The SL1430 is a purpose-designed SAWF pre-amplifier (Plessey) for use in TV IF filtering.

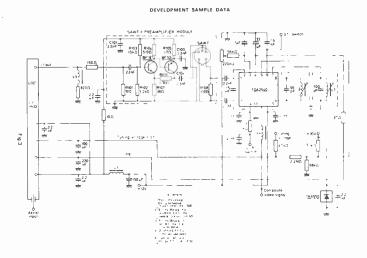
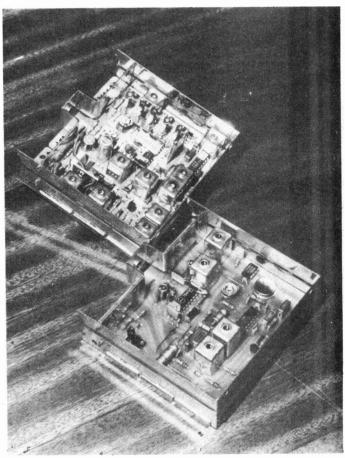


Fig. 4.

Complete Tuner/IF circuit using a Mullard SAWF, the component count is around a quarter that of a conventional IF (Diagram courtesy Mullard Ltd).



Pre-assembled Plessey IF/Tuner units. With the introduction of SAWFs these modules can be made substantially smaller than current IF and Tuner modules.

Transducers

The Transducers consist of interdigital grids or fingers of electrodes formed from Aluminium. Each grid is around 200 Angstroms thick and 10 micro Meters wide.

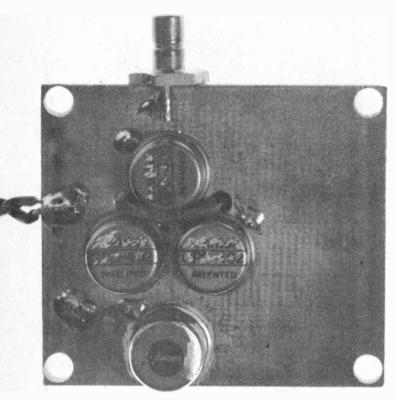
Practical Considerations

In practice several other features are incorporated into SAWF design, the use of an acoustic absorber on the back face of the substrate is used to isolate the transducers from any mechanical interference (it also serves to mount the substrate on to the package or encapsulation). The edges of the substrate are 'cut' at an angle to steer any reflections away from the input and output transducers. Double thickness electrodes are also used to further reduce spurious reflections.

Bandwidth

The 'geometry' of the transducers dictates the effective frequency response (fo) and bandwidth of the device. By 'tailoring the shape and sizes of the electrodes a variety of

FEATURE: Surface Acoustic Waves



Simplified Plessey IF filter, it would be difficult to reduce component count further.

devices can be produced to suit different applications, or in the case of TV filtering, for different systems (ie PAL, -SECAM, NTSC etc). If the electrodes are evenly spaced with a gap of λ o between electrodes of the same polarity the frequency response of the filter would be sin x/x where the centre frequency is given by:

(velocity of wave propagation)

fo =

The bandwidth (Δf) is given by:

 $\Delta f/fo = 2/N$

Where N is the number of electrode pairs. Such a device would possess a linear phase response.

The central coupling grids consist of uniform strips of isolated electrodes, which effectively re-direct the surface wave to the output transducer.

The Future?

So far, SAW filters have been competing against conventional IF filters and are now recognised as being economic and technically advantageous. Already techniques are emerging from the development laboratory which will give even better response and cheaper filters. Parallel sound filters, which have separate outputs for sound and video signals are now in development. These will make possible TV sets with Hi-Fi quality sound. Professional SAW filters are now also being produced and these filters are very stable and can have response shapes which are almost impossible to produce any other way. For instance the CATV filter from Plessey in virtually square. It has an 8 MHz bandwidth which is flat ± 0.2dB and then falls off almost vertically to sidelobes which are lower than 55 dB down. The filters have also made new types of pulse compression/expansion radar possible.

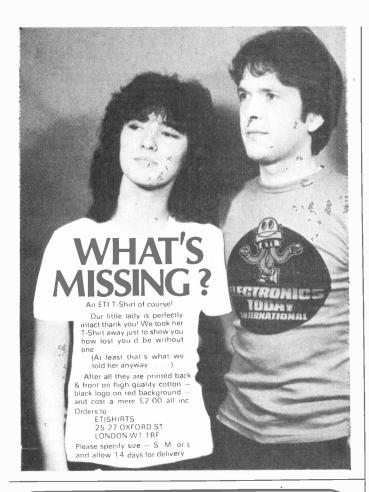
Our thanks to Peter Haywood of Plessey Semiconductors Ltd for his help in preparing this article and to Mullard Ltd for additional information.



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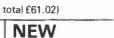
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SO WHAT, YOU MAY ASK, is the advantage of an electronic dice over its conventional and inexpensive plastic (solid state?) counterpart? The answer is that, apart from looking better (and being a better conversation piece), the electronic die or dice is very fast: it can be 'thrown'' and read in a fraction of a second, compared to the several seconds needed for the mechanical item. That enables the rate of play of a game to be speeded up, and consequently makes most games more fun to play. The electric die-dice is a particular boon to the war-games enthusiast.

Our dice has a few unusual features. It has only two panel-mounted controls. One of these is a two-way switch that lets. you select either a single die or a double die (dice) display: the displays are naturally presented in the conventional die format. The other control is a push-button that gives the roll-and-throw action. When the button is pressed the die are rolled and the display is blanked out. The die are thrown and displayed on release of the pushbutton. Once thrown, the die are displayed for about seven seconds, and then black out automatically. When using the device, you can roll-and-throw as fast as you like: you don't have to wait for an autoblanking phase between actions. The unit consumes negligible current when in the standby mode, so no on-off switch is required.

The ETI die-dice is designed around readily-available CMOS IC's. It is the most economically die-dice circuit that we've seen so far. It uses only five IC's and eight discrete components, apart from the 14 LED's and 8 limiting resistors associated with the actual display.

Construction

Not much to say here. All the electronics, except the LEDs, are mounted on a single PCB, so construction should present no problems. On our prototype we

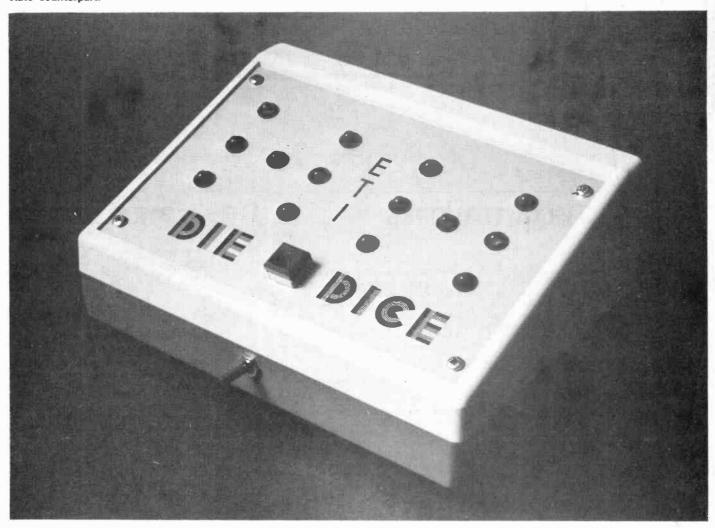
gamble: DOUBLE DIE

used red LEDs for the left-hand die display, and orange for the right. Not a good idea: the orange LEDs aren't contrasty enough, and are difficult to read. Our advice is use red LEDs for both displays.

Our prototype unit is housed in a sloping-front Verocase. The PCB is held in place by Sellotape sticky fixers. That's a good idea: it saves drilling holes in the case and the PCB.

Fig. 1. The random element in Double Die is comparable to the mechanical version. The table on the right was compiled from extensive practical tests and as you can see it produces identical results to it's 'solid state' counterpart.

26% O COMPANY	
COMBINATION	ODDS
any double number	1 in 6
a specified double	1 in 36
total of 2 or 12	1 in 36
total of 3 or 11	1 in 18
total of 4 or 10	1 in 12
total of 5 or 9	1 in 9
total of 6 or 8	1 in 7.2
seven	1 in 6
any two numbers	1 in 18



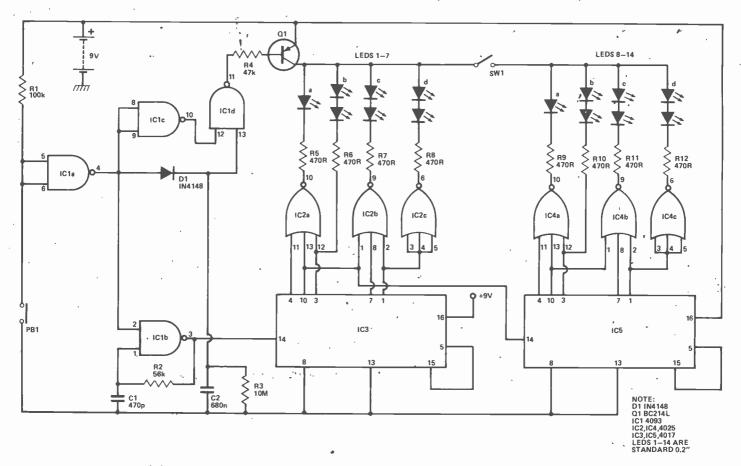


Fig. 2. The complete circuit diagram of Double Dice, as you can see the component count is significantly lower than any previously published design. ICs 3 and £ are 4017s arranged as divide by six, counter-dividers.

HOW IT WORKS

The circuit may be divided into three sections; the clock-control and two identical counter-decoder stages. IC1 handles the control fuction and generates the clock pulses to drive the 4017 counters IC3 and IC5. The output from these in then decoded to provide a conventional die display by IC2 and IC4.

When PB1 is depressed the output of IC1a goes high. This signal, inverted by IC1c, disables IC1d as long as the switch is closed and Q1 remains off so no LEDs are lit. During this time, C2 is charged to about 9 volts through D1 and the clock oscillator IC1b is enabled.

Clock pulses are input to IC3, a 4017 configured as a divide by 6 counter-decoder. This is achieved by connecting decoded output '6' to the rest input. As the outputs are numbered from zero, output '6'

goes high on the seventh clock cycle resetting the counter and providing six decoded outputs which go high sequentially. The rest pulse generated is too short to reliably clock the second counter IC5 so one of the decoded outputs from IC3 is used.

clock the second counter IC5 so one of the decoded outputs from IC3 is used.

When PB1 opens, IC3 and IC5 which have been cycling continuously will stop at a random position as clock oscillator IC1b is disabled. The output of IC1 a will go low again and this signal inverted by IC1c enables one input IC1d. The other input of IC1d will be at a high level as C2 is still charged and so its output will go low turning on Q1 and the LEDs until the charge on C2 leaks away through R3 after about six seconds when the LEDs will extinguish. One or both displays will be illuminated depending on the position of SW1. If you wish to replace PB1 by a touch contact, R1 may be increased to 4M7.

PARTS LIST

RESISTORS (5% all ¼-watt) R1 R2 R3 R4 R5, 6, 7, 8, 9, 10, 11, 12,	100k 56k 10M 47k :: 470R
CAPACITORS C1 C2	470p 680n
SEMICONDUCTORS D1 Q1 IC1 IC2, IC4 IC3, IC5 LEDs 1-7 red 8-14 yellow, standard	IN4148 BC214L 4093 4025 4017 0.2"
MISCELLANEOUS PB1 push-button SPST SW1 SPST P.C.B. Vero-case to suit.	

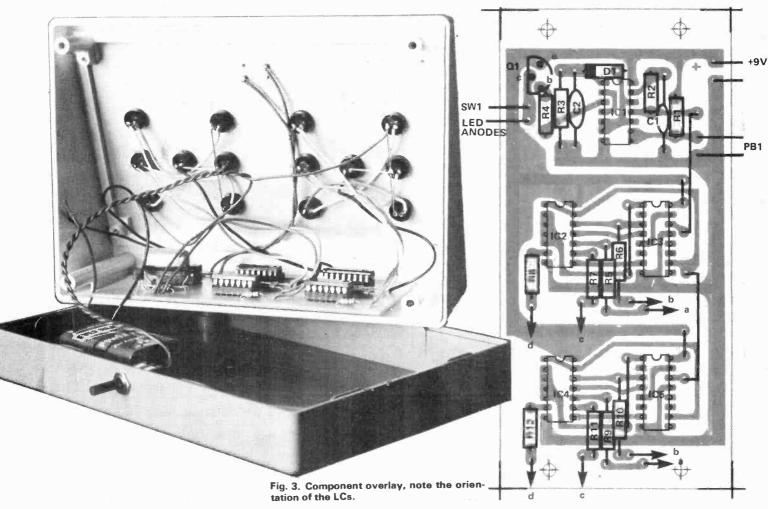
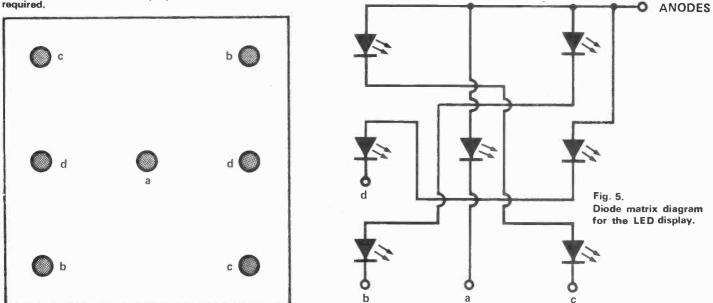


Fig. 4. Layout for the LED display, two are required.



BUYLINES

There should be no problem in obtaining any of the components used in this project. The !Cs are common types available from most electronics hobby shops.

international

The PW Sandbanks Metal Locator: a kit based on this recently published design for this uniquely effective type of metal locator is available for only £35.00 + 8% VAT. The kit closely resembles the appearance as published, except that a close fitting injection molded housing replaces the vacuum molded electronics box \cdot to improve the environmental suitability of the construction. Carriage for complete kits £1.

The New Catalogue - "Tecknowledgey Part 2"

Part 2 of the catalogue: by the time this advert reaches the press, part 2 should be on sale. Sorry it's late, but it contains so many new and interesting things that we felt we had to hold up production to include them. Part three by the autumn and already there are many new items to go in! Part one 45p, part 2 50p. (inc PP etc).

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TBA120	limiting amp+detector	0.75	Yellow	0.18	0.15	0.20
TBA120S	high gain	1.00	Orange	0.22	0.29	0.24
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7415		24	7485	104	99	74151	64	84	74253		105	NE555	30p
7416	30		7486		40	74153		54	74257		108	NE556	78p
7417	30	1 '	7489	205		74154	96		74258		153	NE558	≱ 80p
7420	16	24	7490	33	90	74155		110	74259		420	ICM721	
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7422	24	24	7492	38	78	74157		55 60	74261		353	ICL7106	
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HOW IT WORKS AM & FM RADIO

Gordon King manages to dispell a few rumours about a very widely misunderstood subject, Radio. Such diverse subjects as Varicap Tuning and Stereo FM are clearly explained.

OF THE TWO sound broadcasting systems the AM (amplitude modulation) system is capable of far greater range of reception than the FM (frequency modulation) system. This has nothing to do with the type of the modulation but is related to the carrier frequencies involved. FM sound radio uses a part of the VHF (very high frequency) spectrum called Band II and covering approximately 88 to 108 MHz, though all of this is not yet, used in the UK specifically for entertainment radio.

AM radio broadcasting occupies the long, medium and short wavebands which range respectively from about 50 kHz (6,000 metres) to 600 kHz (500 metres), 600 kHz to 1.5 MHz (200 metres), and 1.5 MHz to 300 MHz (1 metre). Conversion from frequency to wavelength merely involves dividing the propagation velocity (virtually 300 metres per microsecond) by the frequency, or from wavelength to frequency by dividing the velocity by the wavelength.

With increasing carrier frequency the waves tend more closely to follow the laws of light, and at VHF they emanate from the top of the transmitting aerial in rather the same way as light is radiated from the top of a lighthouse. They are less affected by obstructions, though, and are more prone to diffraction and refraction than light which to some extent allows them to pass round obstacles and penetrate walls, etc, but this accommodation is diminished at even higher frequencies. The reception distance of VHF waves, therefore, is limited to a little in advance of the 'line of sight' distance between the transmitting and receiving aerials, the extra being provided by atmospheric refraction and diffraction round the curved Earth.

On Reflection

However, VHF waves are less reflected back to Earth by the ionosphere, and most wave energy skyward-bound penetrates the ionosphere and vanishes into space — which is just as well for space communications! At the lower AM broadcast frequencies the ionosphere acts more like a 'mirror' to the signals, which not only prevents them getting into space but it also reflects them back to Earth over ranges far in advance of the 'line of sight' distance. World-wide reception is thus possible by the waves undergoing a number of 'hops' between ionosphere and Earth.

At certain frequencies ionospheric reflection is enhanced as night falls which means that signals well outside the basic reception range appear and are likely to cause interference with the signals from wanted local

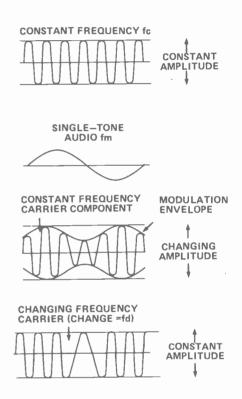
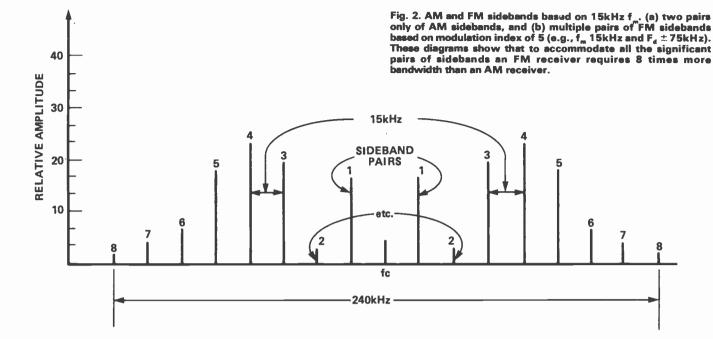


Fig. 1. Impressions of modulation (not to scale). (a) carrier wave, (b) single-tone modulation signal, (c) AM waveform, and (d) FM waveform.

stations. To some extent this is avoided by an international agreement of wavelength spacing; but because there are so many medium-frequency stations to take account of the spacings cannot be very wide, so to reduce the effect of interference the bandwidth of AM receivers is restricted, as this attenuates or deletes the higher-order sidebands the quality of the reception is impaired. This is not necessary at FM because the stations can be adequately separated in Band II without the fear of distant stations producing signals which could interfere with those of the wanted signals. Moreover, FM has a far better immunity than AM so far as this sort of interference is concerned.

The FM system, therefore, is capable of far better audio quality than the AM system as it is currently exploited. It also carries an additional channel of information for stereo reproduction and is thus a 'hi-fi' broadcasting system as will be explained.



Sidebands

Audio information at AM is carried by the carrier wave being caused to change in *amplitude* in sympathy with the sound. The stronger the sound, the greater the amplitude change; and the higher the audio frequency the faster the rate of amplitude change.

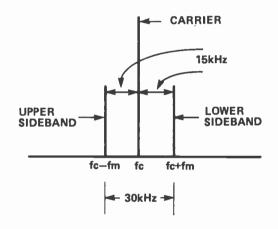
At FM it is the *frequency* of the carrier that is altered in sympathy with the sound. The stronger the sound, the greater the frequency change; and the higher the audio frequency the faster the rate of frequency change.

It is always instructive to look at a carrier wave modulated by a single-tone audio signal, as in Fig. 1, where at (a) we have the carrier, at (b) the modulation tone, at (c) the resulting AM signal and at (d) the resulting FM signal (not drawn to scale, of course!).

100% AM occurs when the carrier amplitude dissolves to zero at the troughs of the modulation envelope. If the modulation level is increased beyond this point very severe distortion sets in owing to the carrier holding at zero for a period of time. With FM sound broadcasting 100% modulation is said to occur when the change in carrier frequency is ± 75 kHz on audio signal peaks. This is called the deviation frequency (f_d). It is noteworthy that with 625-line TV sound, which is also FM, f_d is ± 50 kHz for 100% modulation. With stereo the total f_d includes both the mono and stereo information, the latter occupying approximately 10% of f_d, so that approximately ± 67.5 kHz is available for the mono part.

Modulation

When a carrier wave (f_c) is modulated sideband signals corresponding to every component frequency of the modulation signal (f_m) result. With AM and a pure singletone f_m upper and lower sidebands at f_c — f_m and f_c + f_m occur, as shown at (a) in Fig. 2. With FM the resulting sideband structure per pure single-tone of f_m is far more complicated, as shown at (b). At 100% AM each of the sidebands is 50% greater in amplitude than that of the



unmodulated carrier; but with FM f_d as well as f_m determine both the amplitude and number of the sidebands. Ratio f_d/f_m is the *modulation index* which has a value of five at full deviation by the top audio frequency (15 kHz).

Fig. 2 (b) shows that FM yields a sideband structure which spreads out either side of the carrier over a far greater spectrum than AM, and for the least distortion all sideband pairs above 1% amplitude must be accommodated by the receiver. The multiple sidebands result from the change from sinusoidal form of the carrier as its frequency is changed by f_m, and Bessel functions are used to determine the sideband amplitudes and frequencies for any modulation index. It is not proposed to become involved in the deep mathematics of this, but it can be so proved that for top quality mono the bandwidth requirement is about 240 kHz, and a little greater than this for the best stereo.

Assuming a top modulation frequency of 15 kHz at AM, the total bandwidth requirement is a mere 30 kHz, some 8 times less than for FM. Sadly, 30 kHz spacing between stations just cannot be accommodated in the highly congested medium-frequency scene, and to avoid

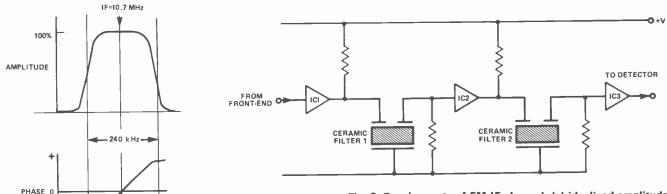


Fig. 3. Requirements of FM IF channel. (a) idealised amplitude response over 240kHz passband having sharply falling side skirts, (b) phase linearity within the passband, and (c) the type of circuit from which these requirements are closely approximated.

adjacent station interference the receiver bandwidth needs to be curtailed to 7 or 8 kHz at best with a consequent attenuation of the upper audio frequencies.

The Capture Effect

With FM channel spacing is 200 kHz (there is much more elbow room at VHF), and local station groups use far greater spacings between transmitters (2.2 MHz) so there is very little danger of interference. Moreover, FM exhibits what is called the *capture effect* which itself avoids interference provided the wanted signal is a little stronger than the unwanted one, even when the two stations have the same frequency! This results from the insensitivity of an FM receiver to amplitude variations of the carrier. When two signals interact one tends to amplitude modulate the other, which means that on AM the wanted signal needs to be very much stronger than the interfering one to give the same interference immunity as FM.

Receiver Requirements

From Fig. 2 it is dramatically apparent that an FM receiver requires much more bandwidth than an AM counterpart to do full justice to the high quality audio signal. The bandwidth needs to be reasonably phase-linear to ensure the least distortion at high modulation index and for the best stereo performance (channel separation, distortion, etc). Latter-day creations employ phase-linear quartz, ceramic and surface-wave acoustical filters to achieve these requirements, as distinct from the earlier LC transformer couplings, as shown in Fig. 3.

To help maintain a high S/N (signal-to-noise) ratio the VHF front-end must employ low noise-figure transistors, especially for the RF (radio-frequency) amplifier, and have a good coupling match to the VHF aerial. Most of the

selectivity and response tailoring is undertaken in the IF (intermediate-frequency) channel at the standard IF of 10.7 MHz. Even so, a reasonable degree of front-end selectivity is desirable to restrict the amplitude of off-tune VHF signals arriving at the mixer from the aerial. A multiplicity of fairly strong signals here can generate intermodulation products of the 3rd-order variety and hence produce spuriae which might detract from the quality of the wanted signal. RFIM (radio-frequency intermodulation) immunity is achieved by using two or more variable-tuned circuits between the aerial and mixer and VHF transistors of good linearity (e.g., bipolars running at fairly high emitter current or FETs).

One important aspect of 3rd-order RFIM lies in the production of an interfering signal of $f_2+f_4-f_3$ where f_2 , f_3 and f_4 correspond to Radios 2, 3 and 4. This interfering signal lies in the f_3 transmission and is perturbed by the modulation of any of the three transmissions. In bad cases of this interference (stemming from a receiver with a poor RFIM performance) the only solution lies in attenuating

the aerial signal.

Most front-ends use an RF amplifier followed by the mixer which may generate its own local oscillator signal (f_o) or call for a separate oscillator stage. Whatever the arrangement, the mixer receives f_c and f_o and thus delivers $f_o \pm f_c$. The vast majority of FM front-ends use an f_o equal to $f_c + IF$, the IF thus corresponding to $f_o - f_c$, and it is this signal only which is accepted by the IF channel, as shown in Fig. 4.

Thus, if the aerial signal is, say, Radio 2 from Wrotham at 89.1 MHz, the local oscillator will be 10.7 MHz above this at 99.8 MHz, so that 99.8-89.1 equals the 10.7 MHz IF. Both additive and multiplicative mixing are used, the former generally when the mixer has just one input port,

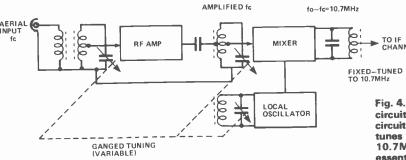


Fig. 4. FM front-end with RF amplifier using two variable-tuned circuits between aerial and mixer. The RF and mixer input circuits are tuned in step while the ganged oscillator tuning tunes over Band II so that the oscillator frequency is always 10.7MHz above the carrier frequency. Accurate tracking is essential to avoid a decrease in sensitivity over the tuning range. Some receivers have double bandpass tuning between the RF amplifier and mixing for further improvement in front-end selectivity.

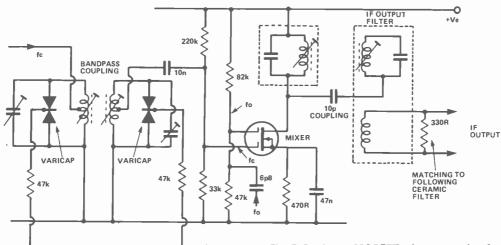


Fig. 5. Dual-gate MOSFET mixer accepting f_c on one gate and f_c on the other gate. The circuit also shows varicap tuning and a capacitively-coupled IF output filter.

and the latter when there are two inputs, such as with a dual-gate FET as shown in Fig. 5. This sort of FET (MOS) may also be used for the RF amplifier, with one gate accepting f_{c} and the other an AGC (automatic gain control) bias \emph{via} an amplifier as shown in Fig. 6.

Varicap Tuning

Some contemporary receivers, especially of European origin, use varicaps (e.g., capacitor diodes) instead of a mechanical tuning gang. The bandpass section in front of the mixer in Fig. 5 is tuned in this way. The varicaps are diode pairs arranged to neutralise non-linearity which, when biased for reverse conduction, exhibit capacitance of value which decreases as the reverse bias is increased. For continuously variable tuning, therefore, it is necessary merely to bias the diodes together from a potentiometer which is mechanically coupled to the tuning system. To eliminate capacitance change and hence tuning drift the tuning voltage is derived from a stablizer or regulator. The scheme also lends itself to press-button station selection.

Also in Fig. 5 the IF signal is filtered out by a capacitively coupled circuit. The 330 ohm resistor

matches the output to the following ceramic filter in the IF channel, as do the input and output filter resistors in Fig. 3. Unless this matching is correct the filters fail to provide the proper symmetry, selectivity and skirt sharpness.

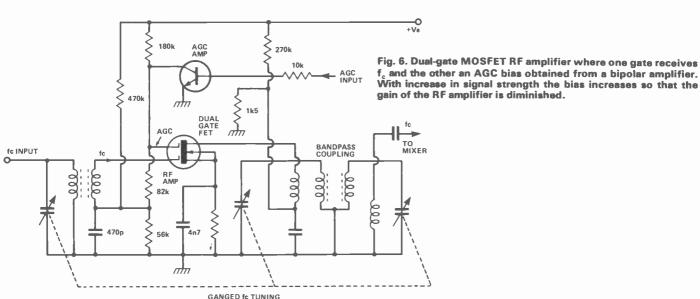
Bandpass coupling at the output of the RF amplifier is also used in Fig. 6, but the tuning here is by a ganged mechanical capacitor.

Oscillator Stage

To avoid oscillator 'pulling' on strong carriers state-of-art FM receivers use a local oscillator followed by a 'buffer' stage, as shown in Fig. 7. Less elaborate models either use a separate oscillator coupled direct to the mixer or a self-oscillating mixer.

AM Front-Ends

Exactly the same principles apply to AM, but because f_c is that much lower the design of the front-end section is less critical. The IF is generally around 455 kHz and, as with FM, f_o is often the IF above f_c ; but some models place f_o the IF below f_c , though this may reverse on some wavebands.



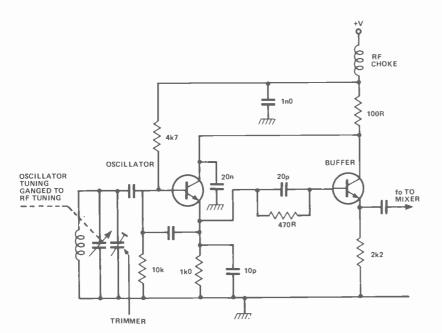


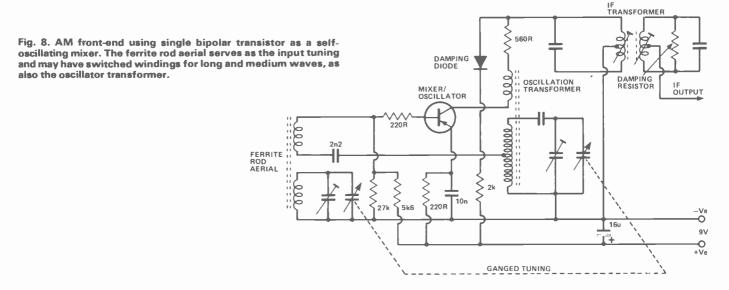
Fig. 7. FM local oscillator followed by buffer stage for feeding the mixer.

The majority of AM transistor portables employ a ferrite rod aerial which also serves as the input tuning. Only the more elaborate models boast an RF amplifier, and a self-oscillating mixer is commonly adopted, as shown in Fig. 8. Receivers with poor front-end selectivity are relatively prone to spurious responses at frequencies removed from the tuned frequency. A typical one is the 'image' or 'second channel' response where the IF is produced from an input two times the IF above the tuned frequency when the oscillator is running at the IF above the signal frequency. For example, if the receiver is tuned to, say, 1,000 kHz the oscillator will be running at 1,455 kHz, so an incoming signal at 1,910 kHz (two times the IF above the tuned frequency) will heterodyne with the oscillator signal to yield the IF in terms of 1,910-1,455. When the front-end selectivity is sharp a signal two times the IF away from the tuned frequency would be well attenuated and not so likely to cause interference. Another is called the half-IF or 'repeat spot' response which falls half the IF away from the tuned frequency owing to

the 2nd-harmonic of the oscillator heterodyning with the 2nd-harmonic of the off-tune signal from the RF stage and producing the IF again.

IF Channels

IF channels nowadays use ICs for the gain and resonant filters of the type already mentioned for the selectivity. FM IF channels employ amplitude limiting ICs or ICs deliberately arranged to limit above a certain signal amplitude. Although FM detectors are essentially insensitive to amplitude variations of the IF-converted carrier, especially ratio detectors, additional limiting is desirable in the IF channel further to enhance the AM rejection ratio and to help with the capture effect. A top-flight modern FM receiver will fail to rise in audio output level once the input cartier at the aerial has reached the 2 to 3 microvolt level, the effect then being a progressive improvement in S/N ratio with increasing level of aerial input, as shown by the curves in Fig. 9. Less exacting models will require an input of 100 microvolts or more before full limiting occurs. The



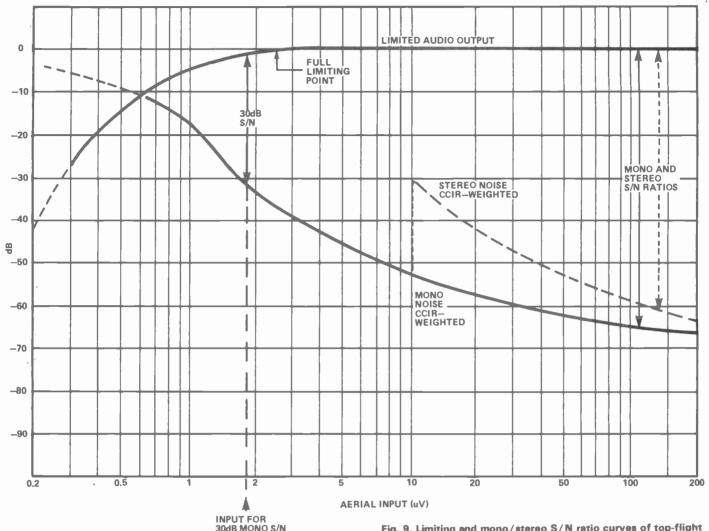


Fig. 9. Limiting and mono/stereo S/N ratio curves of top-flight hi-fi FM receiver.

action of the stereo decoder impairs the S/N ratio at the lower signal levels, catching up with though never reaching the mono ratio at higher inputs. There is always an ultimate S/N ratio impairment of about 2 dB on stereo with respect to mono owing to approximately 10% of the available deviation being used for the stereo information and the greater noise power bandwidth of the receiver in stereo mode.

The FM IF channel also provides the AGC bias for the front-end (when used), AFC control voltage (automatic frequency correction potential derived from the FM detector or separate discriminator for application to the oscillator varicap to hold the carrier at the centre of the IF passband), signal strength and tuning metering, and inter-station muting (where the audio output is disabled until the input reaches a predetermined level as a means of cutting the noise when tuning between FM stations).

The most complex of FM IF channels may employ a cascade of ICs (three or four) feeding into a bipolar transistor which in turn drives the FM detector. Additional ICs and bipolar transistors may be used for front-end AGC, AFC, muting and metering. The simplest adopts a complex IC, such as the CA3089E, which provides IF amplification, limiting, FM detection and audio preamplification for driving the stereo decoder, as shown in Fig. 10. The device contains no fewer than 80 transister

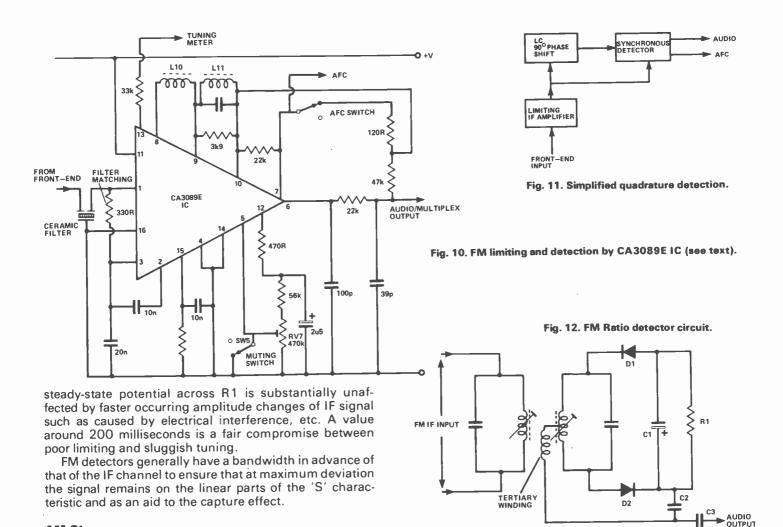
integrations, and includes sections for delayed front-end AGC, AFC, signal strength meter drive, tuning indication and interstation muting. In the circuit the muting is operated by S5 and the threshold level set by RV7. S4 switches the AFC on and off, while coils L10 and L11 are concerned with the FM detection.

Quadrature FM Detector

The coils, in fact, are a part of a quadrature detector circuit, which is fast finding favour in FM receivers, facilitated by ICs, without which would demand a complex of discrete components. The arrangement is based on a 90-deg. phase shift and synchronous detector, as shown in Fig. 11. FM IF signal is amplified and heavily limited, and the resulting 'clipped' signal is passed to one input of the detector direct and to a second input via the phase shift, which is merely an LC circuit such as L10/11 in Fig. 10. The detector is essentially a 'multiplier' which combines the two inputs vectorially. Owing to the relative phase shift and the deviating FM signal the output consists of varying width rectangular pulses, and from these the audio signal is obtained by low-pass filtering.

Ratio Detector

This is another very popular FM detector whose circuit is given in Fig. 12. When the primary and secondary of the



AM Stages

The IF channel is far simplier in AM than FM receivers. Gain is given by a couple of bipolars or an IC and selectivity is introduced either by two tuned transformers or a ceramic filter (sometimes both). AM IF is around 455 kHz which, with the restricted bandwidth, makes it easier than FM to achieve the required gain with fewer devices.

Detection is invariably accomplished by a simple diode circuit as shown in Fig. 13. From the signal point of view this rectifies the AM waveform so that the average value varies in sympathy with the modulation. Subsequent filtering deletes the IF component. The rectified DC value of the carrier is commonly used as an AGC potential automatically to control the gain of the IF amplifier. At the front-end a damping diode may be used to reduce the mixer output on very strong aerial signals. Such a diode is shown in Fig. 8. This conducts and thus damps the IF output when the signal level rises above the value established by the biasing. Fig. 13 shows alternative biasing for this diode.

The tapped primary of the IF transformer ensures that the tuned circuit is not excessively damped by the output resistance of the transistor. This technique is also used in other sections as will be observed from the circuits.

FM Pre- and De-Emphasis

The S/N ratio of the FM system is further enhanced by the application of treble boost to the modulation signal at the transmitter (pre-emphasis) and compensating treble cut (de-emphasis) at the receiver. These are based on a

time-constant which is 50 microseconds UK and 75 microseconds America. It thus refers to the 'turnover' frequency (that frequency where the boost or cut occurs) and is equal to $1/2\pi T$, where the frequency is in Hz and the time-constant (T) in seconds, which works out to about 3,184 Hz at 50 microseconds. The ultimate rate of boost or cut approximates 6 dB per octave (e.g., single-pole filter). FM produces a triangular noise output because the output from the detector is proportional to $f_{\rm d}$. Because $f_{\rm d}$ max is \pm 75 kHz and $f_{\rm m}$ max 15 kHz the noise content is significantly reduced and is reduced by a further 4 dB or so by the pre- and de-emphasis.

The de-emphasis consists of a simple RC time-constant at the detector output in the case of mono and at the decoder output in the case of stereo. It is not possible to apply de-emphasis at the detector when this is followed by a stereo decoder since the effect would be seriously to attenuate the complex stereo multiplex signal. The net result of the \pm 75 kHz f_d and the pre- de-emphasis is a weighted S/N ratio of 75 dB or more mono and just over 70 dB stereo, depending on the noise figure and quality of design of the receiver.

Stereo Encoding

After separate pre-emphasis of the left (L) and right (R) audio channels at the transmitter the signals are fed to a combined adder and subtractor (matrix) which yields L+R mono information and L-R stereo information. The mono signal is passed to the transmitter in the usual way

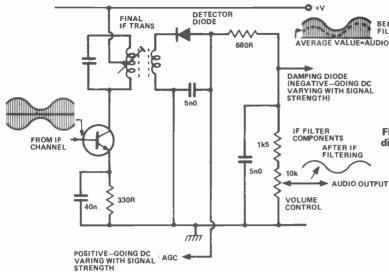


Fig. 13. AM detector circuit with feeds for AGC and damping diode (also see Fig. 8).

tuned transformer are resonated to the undeviated carrier the two diodes conduct equally and since the diodes are connected in series a potential is developed across R1 which charges C1.

When the input deviates either side of its nominal frequency the balanced phasing condition is destroyed and the diodes fail to conduct equally. This results in current flowing out of the circuit through the 'phasing' or tertiary winding, and because this external current is geared to the deviation the audio signal develops across C2, which is fed out through C3.

An advantage of the ratio detector compared with the Foster-Seeley detector or discriminator (which also uses two diodes but connected back-to-back and is without the tertiary winding) is that it yields amplitude limiting. Provided time-constant R1/C1 is large enough the (allowing receivers not equipped with a stereo decoder to work on the signal without undue loss, which is an aspect of system compatibility), while the stereo signal is separately processed and subsequently 'added' to the mono signal for transmission. It is applied to an amplitude modulator whose carrier frequency is 38 kHz but which is suppressed so that only the lower and upper sidebands of the stereo information remain (in practice the residual 38 kHz subcarrier accounts for no more than 1% of the maximum deviation — e.g., less than ±750 Hz). The stereo information sidebands along with the mono information are then applied to the normal VHF modulator of the transmitter

For the detection of suppressed carrier AM the carrier needs to be regenerated at the receiver (in the stereo decoder), and to facilitate this a 19 kHz pilot tone using up approximately 9% of the maximum deviation (e.g., about ±6.75 kHz) is also applied to the VHF modulator. The total modulation signal thus applied to the VHF carrier has the spectrum shown in Fig. 14. The L+R mono signal occupies the normal audio range from about 30 Hz to 15 kHz, next comes the 19 kHz pilot tone and then the lower and upper stereo sidebands between which is the suppressed 38 kHz sub-carrier. At no time can the total deviation of all these signals exceed ±75 kHz (e,g, 100% modulation). In Fig. 14 the total modulation consists of 45% L+R mono, 22.5% L-R stereo in each sideband (45% in all), 9% pilot tone and 1% residual subcarrier, adding up to 100%. This condition would obtain with an

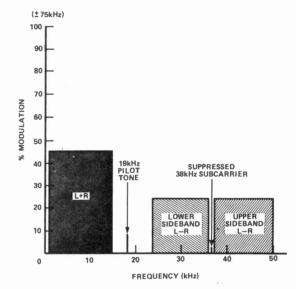


Fig. 14. Spectrum of multiplex signal at FM detector output on stereo signal when one channel only is modulated. See text for other modulation levels.

input only to one channel (e.g., L or R 1 unit and R or L zero). With both inputs receiving the same intensity of 'in phase' signal (e.g., stage-centre mono condition), the stereo information would be virtually zero so that a full 90% modulation capacity would be available for the L+R mono information (the remaining 10% being used by the pilot tone and residual subcarrier). With both inputs equal but in phase opposition (a very rare happening) all the information would be in the L-R stereo channel. Under normal music conditions, of course, the mono and stereo information is continuously changing, but the balance of 100% maximum is always maintained.

Stereo Decoding

The encoding system just described is based on the Zenith-GE developments which is universally adopted. Various schemes for decoding the signals back to the L and R channels for reproduction have been devised, the earlier ones using discrete components with valves and later transistors, and the latest ones using ICs specially developed for encoding. It is clearly outside the scope of this article to venture back into history, but a phase lock loop (PLL) IC decoder circuit used in many receivers is given in Fig. 15.

Multiplex signal (of Fig. 14 spectral form) is fed to pin 1 input *via* Q1. Inside the IC the PLL is formed by a 76 kHz voltage controlled oscillator (VCO), two divided-by-two stages yielding first 38 kHz and then 19 kHz, a 19 kHz

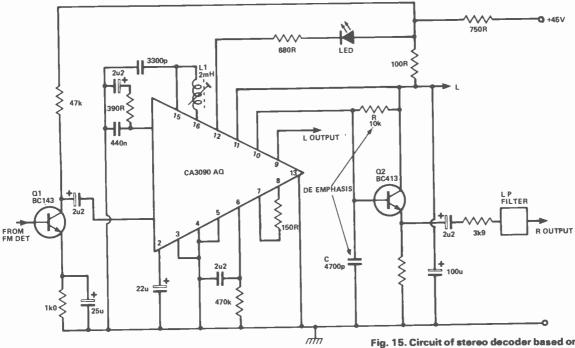


Fig. 15. Circuit of stereo decoder based on the CA3090AQ IC. L1 is PLL tuning and RC the de-emphasis. One channel only is shown; the other channel is similar.

phase comparator, low-pass filter and DC amplifier whose output is fed back to the VCO for control, as shown in Fig. 16.

The multiplex signal is first buffered and then fed to the phase comparator where the pilot tone component is compared with the loop-derived 19 kHz signal. The loop is thus locked and the 38 kHz signal from the first divider constitutes the reclaimed subcarrier which, along with the multiplex direct, is applied to the decoder section. This can be regarded as an 'inverse' of the encode matrix which, after AM demodulation, yields the L audio from (L+R)+L-R) and the R audio from (L+R)-(L-R). Each output is subjected to de-emphasis before being applied to the L and R audio amplifiers for driving the loud-speakers.

The IC is also equipped with automatic stereo switching so that on a non-stereo signal the two outputs deliver mono signal, and a stereo indicator switch which lights a small bulb or light emitting diode (LED) when stereo information (pilot tone) is detected. The circuit connections involved are shown in Fig. 15. The VCO locking is achieved by L1 which is a 2 millihenry inductor. Audio from each channel is 'buffered' by Q2 (same for the other channel though not shown) and passed through a low-pass filter for attenuating residual pilot tone and subchannel spuriae before arriving at the audio stages of the receiver. Some of the very recent ICs incorporate a pilot tone cancelling circuit so avoiding the need for low-pass filtering and maintaining an excellent response to 15 kHz or more.

Of course, all stereo receivers have two separate audio channels for the Land R signals. Hi-fi receivers employ the latest technology in this area, some models yielding 60W per channel or more at remarkably low distortion. Less exacting receivers have relatively simple audio stages based on push-pull transistor pairs or hybrid power ICs.

There is no doubt that latter-day hi-fi receivers operating from off-air stereo signals (particularly when these correspond to 'live' transmissions) are capable of extremely high audio quality, on par with the best of most other programme sources.

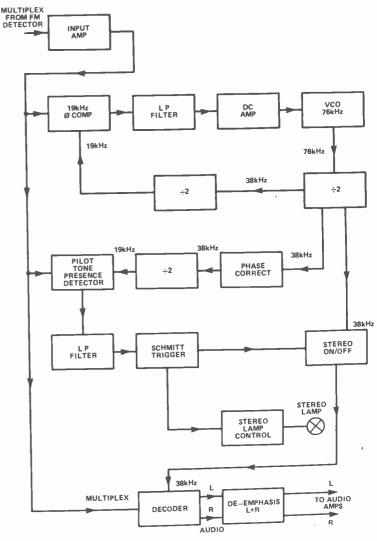


Fig. 16. Block diagram of PLL stereo decoder IC.

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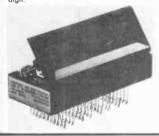
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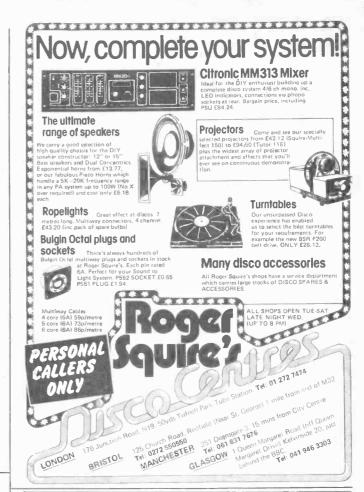
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		BD235	49	*#2008#	170	*WC1330P	75	90	ters 150
AC176/187	18	8D695A/6A	65	*9 20 1 GB	178	*90C1357P	120	A17 10xBCY70 110	A35 50X 74 series with
AD161 :	35	BF115	18	*TIP29/30	39	*80 7666CW	68	A18 3x8D115 110	proformed plas, in-
		*BF167	23	TIP31A	39	"TAA621AXI	195	A19 2x8D695A or 6A	cledies 7400, 7410,
AL113 12	20	0F173	20	TIP 32A	46	*TBA641 B11	210	110	7430 & 7453 220
A\$Y66 I	82	BF178	25	TIP41A	61	"TBA800	80	A20 3x8F180, 1 or 5	
AU110 17	75	BF 180	28	TIP42A	62			70	
AU113 21	10	BF181/4/5	28	"ZTX212	16			*A21 SxBF196 55	ANTEX IRON
BC107/8/9	8	*BF194/5	9	*ZTX302	12	BARGAM PAKS		A22 4xBF324 80	15W 240v with 3/32"
*BC11778 1	15	*BF197	10	1014001/2	5	PAK No.		*A23 4x BFR86 75	telt 360
	14	*BF198	16	HH4804/5	б	A1 5x741 8 pin		A24 5x8FY 50 or 52	
*8C147/8/9	8	9F200	28	11/4005/7	7			75	*ZENERS 400mW
		BF257/8/9	26	211796	12		75	A25 5xB\$X 19 pr 20	TYPE
	9		26	29930		A4 SxAC128	75	65	2.7. 3. 3.6. 4.7. 6.2. 8.2.
		*BF336	32		20	A5 3xAD161 or 16	2 90	*A26 IQxBY127 80	10. 18. 20. 24 mr 27
		*BF337	28	2103054	46	*A6 25x8AX13	70	A27 3±C1060 120	mits 8
		0F 458		2N3055	48	*A7 5x80105A or 8		"A28 25x15 44 or 941	79188
			18		- 8	*A8 5x8C117	80	70	
			16	*7103704/5		*A9 10xBC132	90	A29 5x211930 80	
		°BT106		2103773	250	"A 10 10x8C147, 8	or 9	*A30 10x2103702 3. 4	
		*80205	150	*2114443	80		70	er 5 66	
		*8U206	166			*A12 10x8C182, 3		A31 10x1 megabm	
		*BU206A	175				70	preset 0.25W 60	
	10		-44	LIMEAR LC.'s		*A13 10x8C2048 c	crop-	A32 50x Mixed w/w	
		NUE340	43	741 B-pin	19	ped leads	50	resisters, 2.5W, 5W.	
		MJE520		555 8-pin		*A14 10xBC212, 31	or 4	10W, etc. 150	
		0C28	88		35		70	A33 50X 2.5W w/w	
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AMBUSH! PART 2

At last the second and final part of our very own space game Ambush. Red blood sweat and tears have gone into the production of the game and we beleive it's all been worthwhile. Virtually guaranteed to provide hours of excitement, not one of those games you easily tire of. So switch it on and prepare to do battle with the forces of evil.

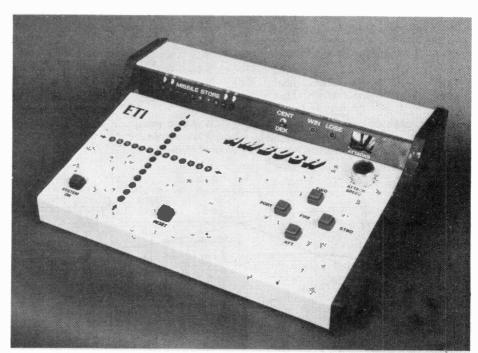
THE MAJOR part of the Ambush circuitry, other than the LED displays, is wired up on a set of three PCB's. Considerable care should be taken over the construction, due to the difficulty that will occur in trouble-shooting the circuitry if it does not work correctly first time. Take special care to ensure that all diodes are fitted in the correct polarity, and that all IC's are correctly located.

On our prototype unit we mounted all IC's in holders. We used Wafercon connectors on each board. rather than solder pins, to facilitate the interwiring. Take great care over the interwiring.

When it comes to fitting the LED's for the Main Display and for the Missile Store indicators, take the precaution of testing each LED individually to confirm its polarity and functioning before finally wiring it in place. Note that silicon diodes D22 to D25 are mounted directly on

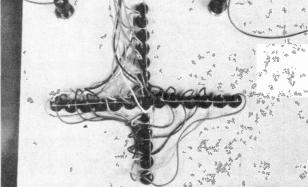
the Main Display matrix.

Our own Ambush game is mounted in an attractive but rather expensive case that we obtained from Boss Industries. The same company produces an 'economy' range of similarly shaped sloping front cabinets. We have powered our unit from a set of eight HP2 batteries, fitted in two 4-section holders. Our Attack counter is mounted on a 20mm x 60mm 0.1 inch matrix Vero board that is epoxy-glued into position on the front panel of the case.



The finished AMBUSH prototype, it really does look good in its case. The staff of ETI have had great fun over the past few weeks playing with the game. A case similar (or the same) to ours is highly recommended and would look good almost anywhere.





case.

SCENARIO

Like all good wargames 'Ambush' has a scenario to go with it. This is it. The scout cruiser Eatyeigh is on a vital war mission to the planet Tora. An enemy fleet (Yappanies) is detected closing in on it by long range hyper radar. A message is flashed ahead to the cruiser's captain. The communications officer, white-faced, takes it to the control room wherein the crew are gathered to hear the news. . . .

The Captain read the message he had been handed. A worried frown briefly creased his brow. He looked up again and spoke, "Men, I have just received a message from Command Headquarters. Our intelligence units report that the Yappanies know of our mission. They are determined to stop us at any cost, and will probably attack us with a suicide fleet somewhere in space sector seventeen. We will reach that sector in just over three hours. All units will maintain Battle stations until further notice. Message ends." The screen flickered, and went blank.

Joe Reader sat back thoughtfully in his chair. He glanced at his three fellow gunners. He spoke reassuringly to they. "Don't worry, mates. The Yappanies haven't got a chance against us. We've got masses of Phanton missiles on board, enough to fight off an entire suicide fleet each. All you've got to do is sit there and wait for the little devils to appear on your sector screens, then press your Phanton FIRE buttons and blast 'em to hell.' His three companions laughed. One of them made a

Three hours later Joe Reader was sitting in the data viewing room, adjacent to the Fire .Control centre, reading up on Yappanie battle techniques. A terrible explosion suddenly blasted through the ship. He was thrown to the floor by the blast. The ships starboard engine had ripped itself apart and hurled great chunks of white hot metal through the hull. The ships self-repair system immediately set to work, sealing the damaged hull. Joe raised himself from the floor, forced open a connecting door, and staggered into the Fire Control centre. A

ghastly sight met his eyes.

The control centre was a shambles. His three companions were clearly dead. Blood was spattered on the walls and across the floor. Three of the four Phanton missile magazines had disappeared, blasted into space before the hull had resealed itself. Joe's mind raced. The ship was about to enter space sector seventeen. The Yappanie attack was about to start. Joe would have to fight off the attack alone. Feverishly, he started to patch all four quadrant fire control switches into his own control console. A damage control report could be heard echoing through the ship. All external attack sensors were damaged. Attack warnings would be minimal.

A few moments later the battle attack sirens screamed through the ship. Joe knew that the Yappanies would attack with either a full Century of one-man Kamanzi suicide craft, or a Dekuron of ten heavily armoured Sutzma battle cruisers. Ten fire units of Phanton missiles were needed to destroy a single Sutzma cruiser, whereas a single unit would destroy a Kamanzi. Joe checked the ammunition register, and made a quick calculation. He had just enough ammunition, in the form of Phanton missiles, to destroy either type of attack, so long as he fought off the attacks with fire bursts of no more than one hundred milliseconds each.

Joe knew how the attacks would be delivered. The Yappanies always attacked one at a time, at random intervals and from random directions, until they had either won the battle, or had been totally destroyed. He switched on the attack indicator unit. A cross formation appeared on the screen in front of him, each arm of the cross indicating a possible quadrant of attack. At the centre of the cross a red indicator gleamed, representing the starship Eatyigh. He switched on the attack simulation computer, to check the extent of the sensor damage. The ships sensor system projected a continuous beam that reflected back from the hull of any attacking vessel, and was modulated by the vessel's hull vibrations in the process. The reflected beams were then demodulated to give a visual output of range and an audible output of engine noises

The computer showed that the Forward sensor was inoperative on sound, and gave only 250 milliseconds of range warning at normal battle speed. Port and Starboard sensors were operating at half strength on sound, and gave 300 milliseconds of range warning. The Aft sensor was fully operational on sound, and gave 350 milliseconds of range

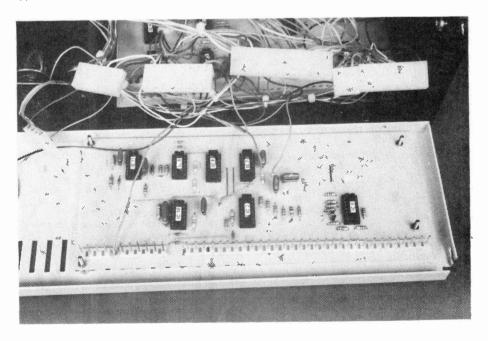
The Commander's voice boomed through the ship again. "All units at Red Alert. A Yappanie century of Kamanzi suicide craft has been detected, closing at high speed. Out."

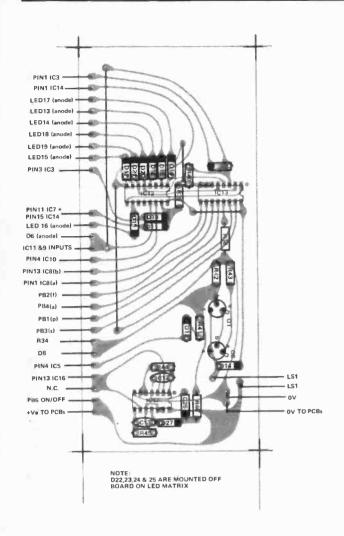
Joe threw the attack mode switch to the CENT position, and the fire control computer automatically adjusted the Phanton missiles into packets suitable for fighting a Kamanzi attack. Almost instantly, the first Kamanzi craft appeared as a rapidly moving spot of light at

the bottom of the attack indicator screen, and the staccato sound of the crafts engine burst from the audio simulator. Joe stabbed his finger at the AFT fire button, heard the screech of a Phanton missle pack leaving its silo, and instantly saw the Kamanzi craft obliterated from his screen. Without hesitation, another attack started in the starboard quadrant, and was rapidly stopped by another pack of missiles. A pause of five seconds, then another attack from the aft quadrant.

The attacks continued relentlessly. Sixty attacks were clocked up on the attack counter within the first five minutes. Joe glanced at the ammunition state indicator. Nearly seventy per cent of his ammo was used up. If he was to survive, he must reduce the fire time on each attack. He glanced back at the screen and saw an attack rushing in silently on the forward quadrant. He groped frantically for the Forward fire button, and hit three buttons at once. Three packets of Phantons screamed from the silo. The attacking craft disappeared from the screen. The ammo store indicator lurched downwards. An attack from the stern. Fire! A three-second pause. A port attack. Fire! Instantly, another attack in the same quadrant. Fire again. The attacks continued.

Part way through the seventh minute Joe noticed that the attack register recorded ninety-five, and that the ammo register was only a notch above the EMPTY state. He wondered if he could ward off the final five attacks. The crew of Eatyigh were depending entirely on him. "It's up to you now, Reader, he thought. Another attack came rushing in on the starboard quarter.





D10 (anode) PIN2 IC10 PIN10 IC7 PB3 (S) PB4 (A) PB2 (F) PB1 (P) D12 (cathode) PIN11 IC6 C4 +12V PIN1 IC10 SW2b COMMON PINS 5,6 1C9 SW2b (OEK) 7 SEGMENT DISPLAY (f) SW2b (CENT) 7 SEGMENT DISPLAY (d) 200 (c) (f) PIN2 IC12 ov . 7 SEGMENT DISPLAY (c) PCB B

PCB, C. The display drive and sound output sections.

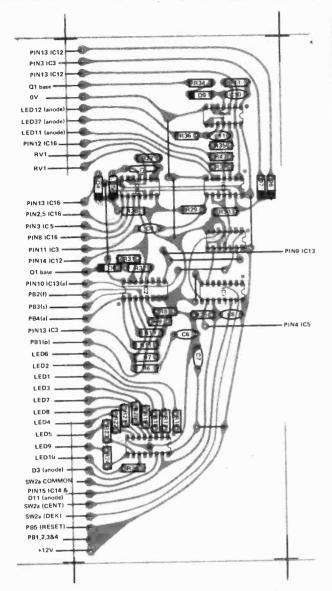
PCB, B. Most of the display functions are carried out on this panel.

	PAI	RT	S LIST	
AL SECTION OF THE SECTION OF	6M8	1000	SEMICONDUCTOR	
R2	390k	2.90	IC1	4016
R3, 8, 9, 10, 11, 31, 40, 48	22k		IC2, 13	4052
R4	10M		IC3, 9, 10	4001
R5, 26, 28, 29, 30, 39	47k		IC4, 6, 12	4017
R6, 16-25, 36, 37, 47	1k		IC5, 17, 11	4011
R7, 12, 13, 14, 15	100k	Sike	IC7	4040
R27	330k		IC8, 16	4026
R32	6k8		IC14, 15	4013
R33	680k		NOTE. All CMOS devices	aro A Sories
R34, 41, 42, 46	10k			
R35	2M2		Q1	BC109
R38	270R		02	BFY50
R43	33R		D14	1N4001
R44, 45	1,M5		All other diodes are	1N4148
R49-62	470R		LED 1-37 are standard 0	
			LED 7 segment disple cathode 0.3in	ays are commo
POTENTIOMETER				
RV1	1MO		MISCELLANEOUS	
			LS1 2in 40R	
			5 off SPST push buttons	
CAPACITORS			1 off SPST latching push 1 off DPDT min, toggle	Dutton
	100n		8 off HP11	Ed Sell Was
C1, 5, 6, 7, 8, 11, 14, 15	100n		2 off 4 section battery ho	Idore
C2, 3, 4, 10, 12, 13	150n		case to suit	idera
C9	1301		case to suit	

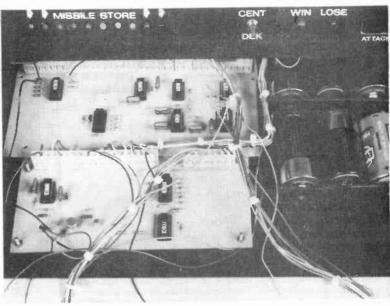
BUYLINES

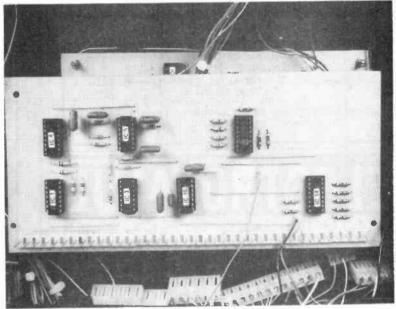
The case we used for the Ambush project is available from Boss Industries. Since panel layout is not critical, inventive ETI readers may be able to come up with their own hardware designs. All the ICs are common types, available from most component mail order firms.

If you think you are likely to spend every waking hour zapping the starfleet, it's worthwhile investing in a mains adaptor, available from your local Tranny shop.

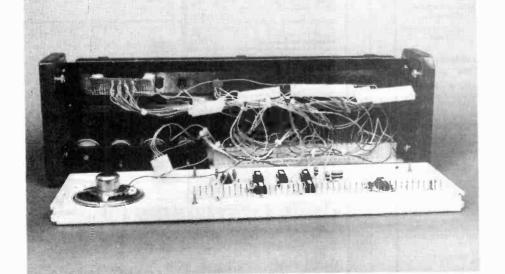


PCB, A. This panel holds the ammo register, random multiplex cock generater and most of the amplex switching functions.





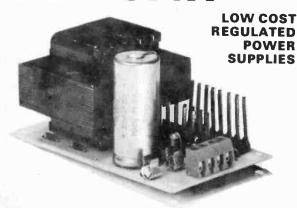
Above. Internal view of ambush with top panel removed. The PCBs are mounted within the case on stand-off pillars.



Centre. PCB, B showing the interconnecting plugs removed, the use of plugs or PCB connecting pins makes troubleshooting (we hope you don't have to) simple.

Left. Inside Ambush from the rear, the apeaker can be clearly seen, note also the battery pack on the base panel.

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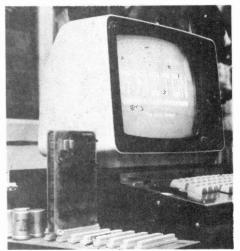
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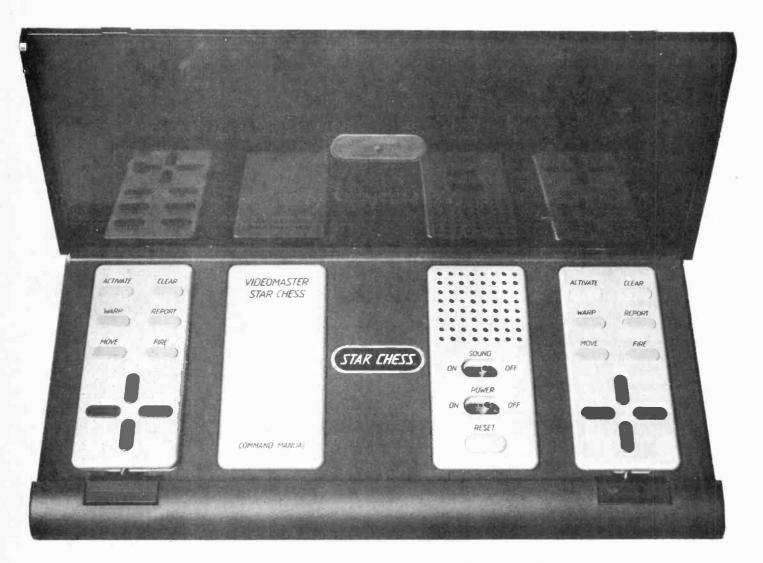
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STAR CHESS

MOST OF YOU probably think that people who work on electronic magazines spend their days burrowing through mounds of exotic electronic equipment sent into us by eager manufacturers. Well to an extent that's true, we do get to see a fair amount of new stuff but how enthusiastic can you get over a 20 amp power supply or yet another revolutionary device that indicates 'heads or tails' at the flip of a switch?

Perhaps we're being a little unfair, the odd calculator or TV game does catch our jaded eyes but is usually followed by "Oh yeah and how many games does this one play?" It's true that we see more TV games than most people, so it's got to be good to get any kind of reaction, and such a game crept unceremoniously into the ETI offices last week. It had all the odds stacked against it from the beginning, for one thing it only had a one game repertoire, not a very good start for something costing almost sixty quid. It almost didn't get switched

on! Perhaps it would have been better if it hadn't because ETI came to a virtual standstill for nearly three days.

Button boxes

Called STARCHESS it boasts a fine pedigree, coming as it does from Videomaster (now owned by Waddingtons). The game is housed in a fairly un-imposing black/grey box, looking like so many other TV games. The remote control boxes seemed to have more than their fair share of buttons but we're so used to a plethora of 'reset' and 'serve' knobs we didn't think much of it. Duly connected up to the power and TV set, it was switched on. Our ears were immediately assaulted by a shrill warbling sound punctuated by what can only be described as a noise like someone treading on a cat's tail—coming from the built-in speaker. A touch of the re-set



Chess games seem to be a growth area in the electronic games market, so find a mate and switch on the TV — Rick Maybury tells what to expect then

and clear buttons soon cured that.

A quick fiddle with the TV's tuner brought in a sharp well defined chess board (in full colour) with some rather unconventional looking pieces lined up on the back ranks. A lengthy study of the instruction manual (more of that later) is highly recommended before any play commences.

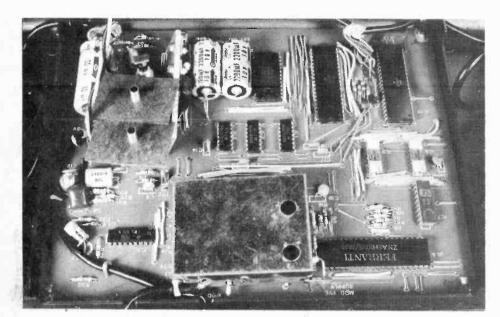
At this point it must be said that you've got to be able to play chess but that hurdle over you can forget any ideas you may have about playing ordinary chess with this machine, that's about as likely as the editor of ETI becoming the next Prime Minister. After a game or two it soon becomes abundantly clear that what this game has that others seem to lack is the need to think, rather than a question of who can twiddle their knobs fastest?

A typical game is both noisy and exciting, the manufacturers have seen fit to include as many variables as possible but without making it cumbersome. We take

our hats off to the software engineers who wrote the game.

A lovely mover

Each piece is moved by shifting a cursor with a set of four positional buttons arranged in a cross, when the cursor is over the piece to be moved the 'move' button is pressed, then the cursor is placed on the square to be occupied and the 'activate' button pushed. Every action is accompanied by a virtual symphony of 'squarks, warbles' and other equally strange noises, adding tremendously to the fun of the game. All of the pieces except the 'pawns' move exactly as ordinary chess. The main feature of the game, however, is the ability of each piece to 'fire' missiles in the direction it would normally move, so instead of taking an opponent's man you can take a pot-shot at it, although you're not guaranteed a



(1

Starchess, naked to the world. It has a surprising amount of parts for a 'dedicated' game, many of the ICs are unknown to us. The modulator deserves a mention: it produces one of the most stable and clear pictures of any TV game we've come across.

(2)

The preliminary stages of a game, the pieces may look rather unusual, particularly the 'queen' which looks a little like the 'Starship Enterprise.'

(3)

It's a bit confusing showing a game in black and white, there is an explosion on the screen (square C4). In fact the explosion is in red and accompanied by some very 'Star Wars' like sound effects.

hit, in fact you take a chance of hitting one of your own men if they are too close.

Each direct hit will destroy one of your enemy's 'shields' which can number from two (pawns) to seven for the King and Queen, and the amount of ammunition each man has is similarly limited. The pieces, however can replenish their ammunition by returning to the 'starbase' which is the squares occupied by the king and queen. When an opponent's shields have all been destroyed a further hit will produce a satisfying 'double explosion' (in red) and obliterate the piece completely.

Warped ideas

The second major feature is the ability to 'warp' any of your pieces from the board, the only danger in doing this is that the piece will return after a random period (from a few seconds to several minutes) and will reappear anywhere on the board, even on top of one of your own men (or your opponent's). The piece coming out of 'warp' makes a banshee like wail and slowly materialises (just like the transporter on the Starship Enterprise), but this is an extremely useful feature lending itself to risky but worthwhile tactics.

Yet another feature is the 'report' facility which apparently gives a readout of shield and weapon status but we found we rarely used it as it counted as one move.

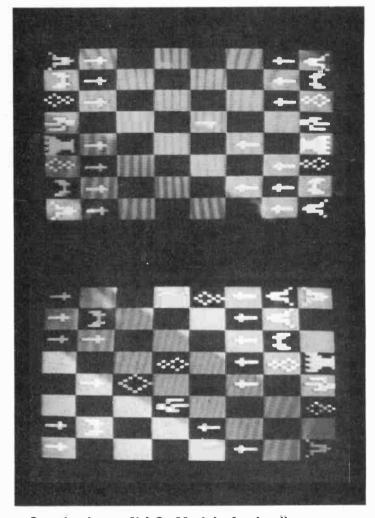
All of the pieces are given alternative names which is just as well, because none of them look even remotely like ordinary chessmen, the rook for instance is a starcruiser. The final objective of the game is to destroy your opponent's King, although it can't be taken on its Starbase, it can still be fired upon.

We did find we had one or two small niggles with the machine, it would have been a good idea for it to play ordinary chess, especially when most of the hardware is already there, and the power supply could have been located inside the case.

Taken overall, however it's without doubt the best 'dedicated' game we've ever come across and recommend it highly. By the way ETI Starchess team confidently challenges all comers to a shootout!

Any takers?





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		-	211 0	CH	-	سينا	unu			V					PIECE	A PERSON	Extension of the	
100	N	LS	7476	N	LS		N	LS					Static RAM's 2102A (350ns)	1+	17-63	.88*	LM326N LM345K	1
01	.13"	.19'	7478	.30*	.291	74170 74173	1.85° 1.41°	1.65	4000	.16	4077	.21	2102A (350hs)	1.05		1.08*	L129/30/31	
02	.15*	.19	7482	.73*	.28	74174	1.01	1.05	4001	.16	4081	.21'	2111A-1 (500ns)	2.46		2.05	L125/30/31	
03	.15	.19	7483	.73	.75	74175	.81*	1.05	4006	.92*	4085	.92	2112A-2 (250ns)	2.14		1.78	I.C's	
04	.16	.211	7485	1.181	.88	74176	1.01	-	4007	.18*	4086	.92"	21L02 (350ns)	1.07		.86*	CA3080	
05	.16	.21'	7486	.25	.29'	74177	1.01*	1 - 1	4008	.92	4093	.81	MM5257 (TMS4044)	8.10		6.75*	CA3130E	
06	.26	-	7489	2.60	-	74180	1.01		4009	.54	4099	1.81	2114 (450ns)	8.10		6.75	CA3140E	
07	.26*	-	7490	.34*	.62*	74181	2.21	2.99	4010	.54"	4502	.92*	.6810	3.50	2.97	2.52'	LM301AN	
80	.17°	.191	7491	.73*	1.05"	74182	.81*		4011	.18"		2.46	Dynamic RAM	-	8251	5.97	LM324N	
09	.17"	.19'	7492	46°	.75	74184	1.81		4012	.181		1.07	4116	12.75	8253	8.10*	LM348N	
10	.151	119"	7493	.34*	.65	74185	1.62		4013	.48	4511	.95"	CPU's		8255	5.51	LM380N	
11 12	.18	.19	7495	.54*	.88	74188 74189	2.97		4014	.92"		2.70	8080	5.95*	Regulators		LM381N	1
13	.27	40	7496 74107	.67*	1.85	74109	3.17° 1.21°	2.25	4015 4016	.92	4515		6800	8.99°	78L series		LM382N	1
14	.71*	.79	74107	.27	.35	74191	1,21	.75	4017	.81*		1.07	9900	42.50°	+(POS) 100mA		LM3900N	
15		.19	74112	,444	.35	74192	1.21	1.85	4018	.92	4517	.95	E-Prom's UV		5v, 6v, 8v, 12v &	15v	LM3909N	
16	.25*		74113	- 3	.35	74193	1.211	1.85	4019	.56	4521	2.54	1702AQ 2708Q	5.75*	All 30p° each		SN76001N	1
17	.34"	_ [74114		.35*	74194	1.211	-	4020	.92*		1.89	TriState Buffers	7.87	78M series		SN76003N SN76013N	
20	.16"	.191	74121	.27	-	74195	1.01	1.05	4021	.92*	4526	1.89	81LS95	.75	+(PQS) 500mA		SN76023N	
21	-	.191	74122	.50	.75*	74196	1.18*	1.05	4022	.92"	4528	.92"	81LS96	.75*	5v, 6v, 8v, 12v, 1	5v. 20v & 24v	TBAB10AS	
22		.19"	74123	.60	.781	74197	1.18*	1.05°	4023	.181	4534	7.12"	81LS97	.75	All 60p' each		TCA940	
23	.25*	- 1	74124	_	1.25	74198	1.81*	- 1	4024	.65"		3.74"	81LS98	.75	79M series		ZN414	
25	.25'	- 1	74125	.51*	.39*	74199	1.81*		4025	.181		1.62	74365	.75*	—(NEG) 500mA	F DO 0 04	ZN424E	
26	.25*	.19"	74126	.51*	.391	74221	_	.99*	4026	1.84	4553		74366	.75*	5v. 6v. 8v. 12v. 1	5v, 20v & 24v	ZN425E	
27 28	:391	.19*	74132	.78*	.65*	74240		2.25	4027	.51		1.51	74367	,75°	All 85p* each 78 series		ZN459CT	3
28 30	.38	.21'	74133	_	.19	74241 74242	-	2.25	4028	7·0°	4583		74368	.75°	+(POS) 1A		ZN1034E	
32	.16"	.191	74136 74138	_	.39*	74242		2.25	4029 4030	1.18	4585	1.07	Buffers		5v. 8v. 12v. 15v.	18v & 24v	ZN1040E	
33	.25	.28	74138	= =	4.55*	74247	_	.95*	4030	1.08	I.C.		8T26P	1.65	All 85p' each	101 (124)	ZNA116E	
37	.25°	.25	74141	.76*	.55	74248	_	.95	4034	1.89	SOCI		8T28P	1.65*	79 series			
38	.25'	.25	74145	.75	1.05	74249		.95	4035	1.06	DIL (T		*8T95P 8T96P	1.490	-(NEG) 1A		The Items shows	n in this adve
40	.17'	.19*	74147	1.59	1.03	74251		.83'	4040	.92"	8pin		8T97P	1.49*	5v, 8v, 12v, 15v.	18v & 24v	just a small sele	ection taken
41	.70*	_	74149	1.38	_	74253	_	.99	4042	.70	14pln	.12"	8T98P	1.49	All £1.00° each		our new 78 / 79	Catalogue :
43	.50*	.55*	74150	1:08"	- 1	74257	_	.99*	4043	.81°	16pin	.13*		1.70	4 700 (011)	40*	is now availa	
45	.60°	- 1	74151	.67*	.88*	74258	-	.99*	4046	1.061	18pin 20pin	.18"	Interface 8212	2 241	uA723 (DIL) L200	1.99*	everything from	
46	.60*	- 1	74153	.67°	.48"	74259	_	1.50*	4049	.43°	22pin	.24*	8216	2.21	LM304H	2.40	latest in Micro-	
17	.60°	.87'	74154	1.31*	1.35	74266		.35*	4050	.43	24pin	.26'	8224	3.59	LM323K	6.25	delay order you	
18	.16"	.87	74155	.67	.78	74273	_	2.25*	4051	.81*	28pin	.30°	8228	5.51	LM325N	2.60*	price is only	4Up (inc
19	.16"	.87*	74156	.67*	.781	74279 74283	_	.48*	4052 4053	.81°	40pin	.44*		3.31	2020.1		wouchers)	
51	.16'	.19	74157 74158	.67*	.55'	74283	_	.99*	4053	1.29	Wire		OPTO					
53	.16"		74160	1.21	.52	74290	-	.83	4054	1.46	8pin	.23	.125 1+	10+	50+ 100+	0.0		
54	.16	.19	74160	1.21	.65	74395		1.05	4059	5.18	14pin	.34*	TIL209 Red X .15"	.101	.10" .09"	2"	1+ 10+	50+ 1
55		19.	74162	1.21	1.85	74298	_	1.25	4060	1.24	16pin	.37*	TIL212 Yel X ,20°	.18"	.16' .14'	TIL220 TIL224 Yel X	.16' .125'	.125' .195'
60	.16"		74163	1.21	.65	7,4365	_	.51'	4066	.48	18pin	.43*	TIL216 Red X .20*	.18"	.16' .14'	TIL228 Red X	.23 .21	.195
70	.27	- 1	74164	1.08	1.15	74366	-	.51'	4068	21	20pin	.55°	TIL232 Gre X .20*	.18"	.16' , .14'	TIL234 Gre X		.195
72	.23'	- 1	74165	-	.78	74367		.511	4069	.211	24pin	.60°	X = High Brightness		who the same	TILLED Y GIE X	market and the last	
73	.28	.29"	74166	1.02*	-	74368	_	.51°	4070	.21"	28pin	.65°	DL747	UA741	NESS	5	TIL209	TIL220
74	.28*	.29*	74168	_	1.85	74386	-	.391	4071	.21	36pin	.95"	4 for £6,00*	5 for £1.				8 for £1.0
5	.44	.43	74169	-	1.85	74670	10.00	1.851	4072	.211	40pin	1.05	4 101 E8.00	3 107 2 4	3U T 4 10f E 1	.00 10	for £1.00*	9 TUT 2 1 U



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RADIO CONTROL SYSTEM PART 1: TRANSMITTER

THERE WERE SEVERAL criteria we considered important in any radio control system before this project came up, and these have been perhaps the main reason for ETI keeping out of this field thus far.

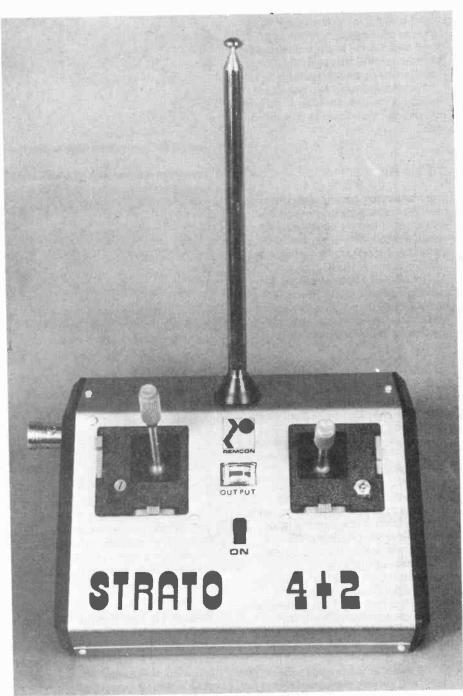
However Rencoms design, presented here, satisfys our requirements perfectly and fulfills a few we hadn't thought of. Firstly it is easily constructed and easy to set up — too many systems are marred by their requirements for expensive test gear in the alignment procedures. All that is needed here is a simple voltmeter.

Secondly the transmitter produces a 'clean' output which does not interfere with adjacent channels to any degree worth mentioning. This is an essential requirement since the receiver can handle 10kHz channel spacing, and interference would render this unusable. In any case this is now a legal requirement in many countries.

The charger for both transmitters and receiver can be built into the transmitter case itself, which any enthusiast will recognise as a decided convenience a five pin socket fitted to the case allows access to the charger circuit for this facility, and the same socket holds the transmitter crystal (normally encased within a DIN plug). This means channels can be changed quickly — or the set disabled — simply by removing the plug.

Tune In

The Strato system can be built as either a four or six channel unit, and is suitable for any kind of model from airplane to boat. Choice of servo will be made according to the vehicle to be controlled.



Publication of the system will be in two parts, transmitters first. Next month there will be full details of the receiver unit along with some hints on installing the radio control. There will also be a follow up article later designed to give some ideas of what can be achieved with a system of this versatility.

We chose an armoured vehicle as the example upon which to base our articles, as this is more general in principle than most and allows easier illustration. The model we used was the excellent Tamiya 1 / 16th Leopard kit. This gives a splendid model of the W. German tank with Tamiyas usual superb moulding detail and a drive system designed for radio control through an ingenious twin clutch system.

It is an expensive kit, but in our opinion is well worth it, and includes everything right down to the servo rods.

A Case For It

The transmitter case is designed for four channels to be controlled by joystick and two by either pot or simple switch. The latter could be useful for aircraft undercarriage and the like.

The angled aerial produces a radiation pattern that reduces the risk of an aircraft (in particular) getting itself into an area of low strength and thus passing beyond operator control.

The meter on the front panel is a form of field strength meter and is used initally for setting the only tuning control in the TX circuitry, and thereafter indicates RF output as a check upon performance.

Construction

Building the Tx should pose no problems to the average constructor, but when fitting the joystick and case, follow the photographs carefully otherwise it could cause unnecessary problems.

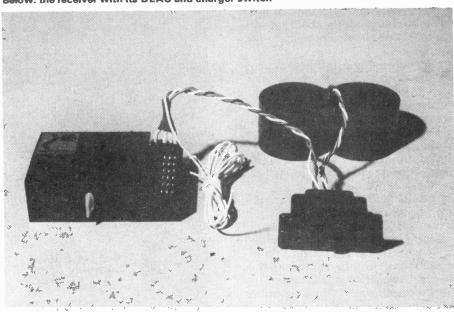
Assemble the PCB first, and check carefully the polarity of semiconductors etc. Fit the aerial and other sockets initially, then the passives and leave the transistors until last. Note the inductors are labelled

The small PCB fits aback the meter and carries the components for the FSM.



Above: the Tamiya tank upon which the system is based

Below: the receiver with its DEAC and charger switch



Solder the output wires to the board at this stage as fitting the control pots later will be tricky else. Follow the installation drawings carefully and there should be no trouble. Check everything carefully though.

Power To The Aerial

Once the board is complete and the sticks wired fit the rechargeable cells, screw in the aerial (telescoped) and plug in your crystal. Switch on.

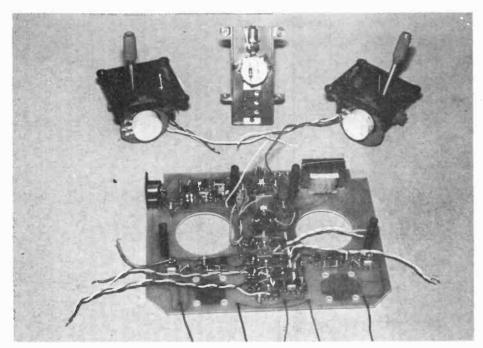
The meter should show a reading.

Rotate CI using a small insulated screwdriver or better yet a plastic control trimmer the reading will rise and fall as CI is rotated.

Extend the aerial fully and rotate CI to get a maximum meter reading. It helps during this operation to keep a finger on the —ve of the cells to provide an earth load.

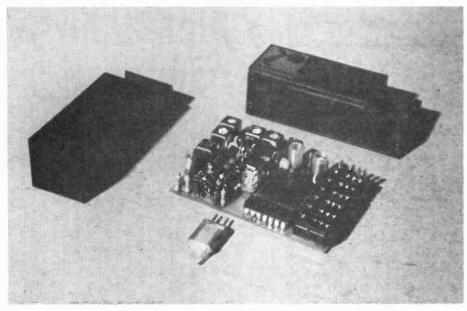
The reading should be about 80-90% of FSD so move the FSM aerial around slightly to obtain this.

The transmitter is now tuned. Presets PRI-6 are used to set the centres of servo operation and do not interfere with RF output at all.



Above: a denuded transmitter unit. The joysticks mount above the board.

Below: the receiver removed from its case. Note the crystal.



Fit the completed assembly to the case, lining up the aerial bush with the plastic grommet on the case top. For those not fitting the internal charger, cover the holes in the back of the case with some tape or card.

Charge

Remember that the cells used will take 14 hours to charge from flat, and the bulb will light quite brightly at first and then dim as charging progresses. To charge the Tx batteries alone fit the DIN plug with R32 across pins 1 and 2 and plug in the mains lead to the rear socket.

That same DIN socket is utilised many ways. Pins 4 and 5 are the connections for the Tx crystal. Pins 1 (+ve) and pin 2 (—ve) allow charging of both the Tx and Rx cells together. Pins 2 and 3 if strapped together can switch on the Tx so that when removed 'locks off' the unit. Makes unauthorised use a little difficult! Pins 2 (+ve) and pin 5 (—ve) connect an external charger to the Tx cells. 50mA maximum please.

Crystal Clear

By changing crystal you change channel, and the colour can be used

BUYLINES

With a project of this type the metalwork is more important than for our usual endeavours. For the transmitter in particular, with the joysticks and aerial to be mounted, we cannot imagine anybody enjoying filing away for hours. In consequence we strongly recommend use of the hardware packs offered by the designers, Remcon. Our photographs and text employ these.

Ambit are marketing the components for this project, so between the two a complete kit is to be had. We estimate that, including four servos, the project will cost about £130 in total, which is approximately £60 less than a commercial set-up of approximately equal performance would cost.

The model we intend to base our installation on is the Tamiya Leopard A4 in 1/16th scale, which is designed for radio control. The kit is superb in all respects, both as a model and as a vehicle for radio control, and cannot be recommended highly enough. Beatties chain of stores stock the kit and it will cost around £90 including the gearbox/clutch/motor assembly for direction control.

Component details: From Remcon.

Manual for system (worthwhile step-bystep constructional details) £2.75

£1.00 refundable against purchase of packs over £25

Transmitter hardware pack (everything except components and batteries):

4 channel £39.95 6 channel £45.00

All components available separately. SAE to Remcon for details.

Receiver hardware pack complete (six channels) £18.50

All components available separately.

From Ambit —

Transmitter components £10.95
Two PCB DIN plugs and charging resistors £1.60

Matched crystals (2) and DIN plug

Five-pin plug DIN (options) £0.75
Receiver components (complete) £8.95

All components available separately. Rechargeable batteries also available. SAE for details.

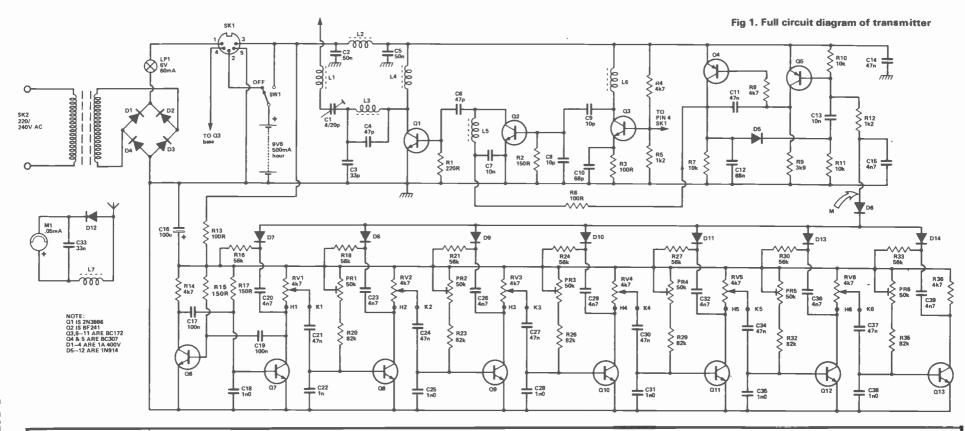
Any servo will operate with the Strato system. Next month we will give wiring details for the different types.

Addresses:

Ambit International, 2 Gresham Road, Brentwood, Essex.

Remcon Electronics, 1 Church Road, Bexleyheath, Kent.

Add 12%% VAT to all prices except manual.



HOW IT WORKS

This has been designed to meet the stringent requirements of continental post offices in respect of harmonic radiation and sidebands and has adequate power output to ensure out-of-sight range for model aircraft.

Referring to the transmitter circuit Q6, 7 R14-17, RV1, C16-19 comprise a conventional astable mutivibrator of unity M/S ratio, and period approximately 20mS. This is the system clock. If we look for a moment at Q8-!1 it will be seen that these initially have their collectors close to the - ve rail potential due to their base bias. Now when the collector of Q7 goes to logic 0, the step change in voltage at the slider of channel 1 control potentiometer RV1, is passed via C21 to the base of Q8, cutting off its collector current. The collector of Q8 therefore goes to logic 1. The base potential of Q8 slowly rises on a time constant C21 (R19+R20) until the base/emitter diode

again becomes forward biassed At this point the collector goes to logic 0 once again. When this happens, the -ve going stage voltage at the channel 2 control. potentiometer RV2 cuts off Q9, followed by the same pattern of events as detailed for Q8. This sequence is followed by Q10 and Q11. Potentiometers RV1-4 are the operator controls, and R19, 22, 25, 28 permitsetting of the pulse width with the channel controls centred. These adjustments are carried out to set the mid-travel position of the servos.

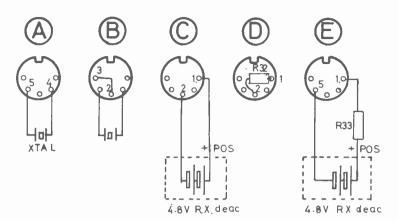
The encoding process is completed by the C,R and diode network at the collectors of Q7-11. Taking as an example, C26, C21, D9, capacitor C26 is normally charged to a potential approximately that on C16, When Q9 is cut-off by the pulse from Q8, C26 discharges on a time constant C26 (R21+RV3), which is much less than the

lms minimum duration of channel data. When O9 is again turned on, D9 and D6 are forward biassed by the current through R12 turns on Q5 which is part of the monostable which modulates the buffer stage Q2. Before triggering, Q5 to cut-off, and Q4 therefore turned on by base bise current through R9. R6. When triggered by an encoder pulse via D6, Q5 conducts turns off Q4, which reverse biasses D5. C13 then charges through R11, maintaining Q5 in its turned on state for a period determined by C13, R11. Since this occurs when Q7-11 collector go to logic 0 then five absolutely identical pulses will be generated by Q4 and Q5 in every 20 mS frame of data.

The RF section is one of elegant simplicity, having only one adjustment, C1, Q3 is the crystal oscillator using 27 MHz 3rd overtone crystal base to -ve rail 27 MHz output is coupled to the base of buffer/

modulator stage Q12 via C9. As we mentioned in the description of the encoder, Q4 is normally conducting, which means that collector voltage is applied to Q2 via R6 and L5. The amplified RF from Q2 collector passes to the power amplifier O1 via C6. Impedance matching from Q1 collector to the power amplifier Q1 via C6. Impedance matching from Q1 collector to the aerial is effected by pre-coupler C3, L3 C4, and base loading by the adjustable network L1, C1. A simple RF meter circuit is included, comprising the meter, C33, L7, D12, it is used to peak the aerial matching adjustments during initial setting up. Thereafter it constantly indicates the carrier strength.

Before leaving the transmitter it is perhaps worth mentioning C2, L2, C5, C11, C14, C15, C18, C22, C25, C28, C31. They are all there to prevent R.F. from reaching unauthorised, and sensitive parts of the circuit!



and the second s

The field strength meter, with PCB ready for bending at the meter tabs.

Fig 2. All the possible DIN plug configurations. See text for uses.

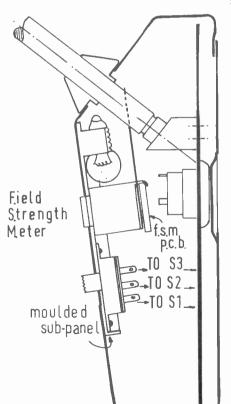
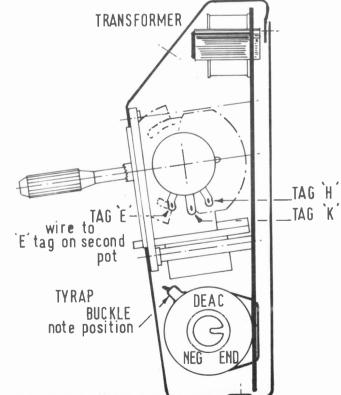
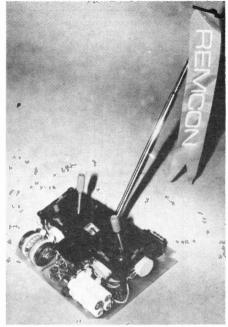
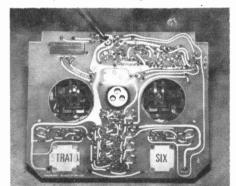


Fig 3. Section through transmitter case. Should help with assembly.

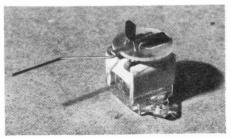




The complete Tx excluding case.



Copper side of PCB. Note earth bush.



The field strength meter with pCB bent over for fixing.

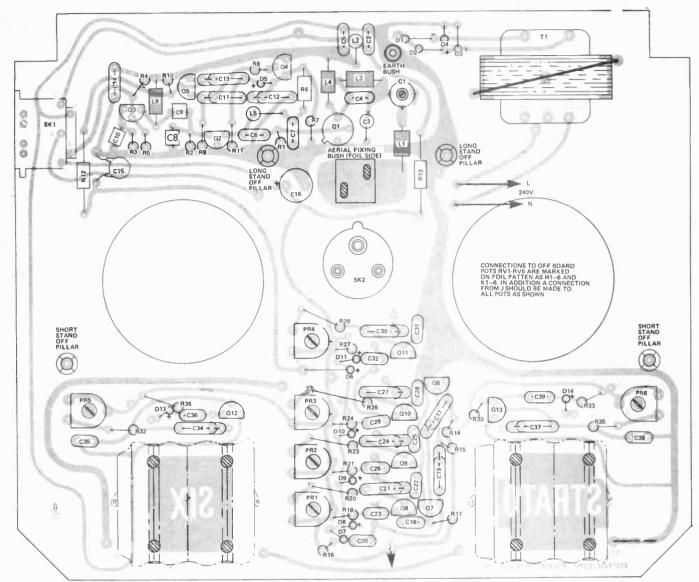


Fig 4. the main component overlay for the transmitter. Note that PR1-6 are 50k in value.

RESISTORS (all 1/4)/ R1 R2,15,17 R3,6,13	220R 150R 100R	PARTS	LIST	INDUCTORS L1,2 L3 L4	4u7 220n 22u
R4,8,14,36	4k7			L5	680n
R5,12	1k2	C3	33p polystyrene	L6	1u5
R7,10,11	10k	C4,6	47p polystyrene	L7	10u
R9	3k9	C7	10n polyester 5%		
R18,21,24,27,30,		C8,9	10p polystyrene	SEMICONDUCTO	RS
33,16	56k	C10	68p polystyrene	01	2N3866
R20,23,26,29,32,	82k	C11,14	47n ceramic	02	BF241
35	02K	C12	68n polyester 5%	Q3. 6-11	BC172
Note that R19,22,25,28,31,34 are annotated as PRI-6 to correspond to channel number		C13 C15,20,23,26,29, 32,36,39 C16	10n ceramic 4n7 ceramic 100u electrolytic 25V	Q4,5 D1-D4 D5-D12	BC307 ITT 2002 or equi- valent 1N914
POTENTIOMETER	S 4k7	C17,19 C18,22,25,28,31,	100n polyester 5%	MISCELLANEOUS	S (for charger version)
RV1-RV6 CAPACITORS	41.7	35,38 C21,24,27,30,34,	1n0 ceramic	secondary trans	60mA bulb, 20V 1A former, meter 200uA
C1	4-20p trimmer	37	47n ceramic		l skt, metalwork (see
C2,5	50n polystyrene	C33	33n ceramic	Buylines), aerial -	– 1.4m long.

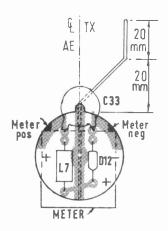
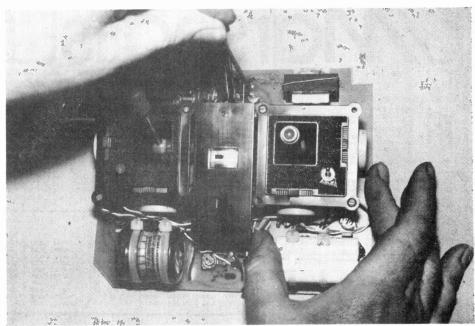
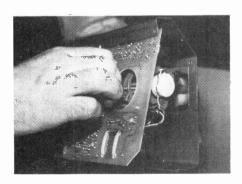


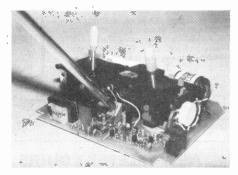
Fig 5. (Above) the overlay for the meter PCB. This mounts stop the meter itself



Tuning involves one adjustment only one note thumb on battery earth.

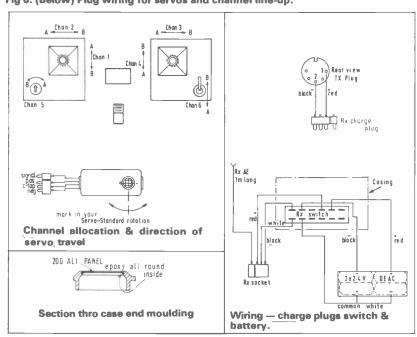


The top of the PCB slips under the flange at the top of the case.



The Rf end of the PCB.

Fig 6. (Below) Plug wiring for servos and channel line-up.



to identify operation easily. The standard system of coding is:—

Tx 26.995 27.045 27.095 27.145	26.54 26.59 26.64 26.69	Colour Brown Red Orange Yellow
27.145	26.69	Yellow
27.195	26.74	Green
27.255	26.80	Blue

Conclusion

SE1 8UA.

So that's about it for the transmitter, except to remind you that to run a radio control system you NEED A LICENCE. This costs £2.80 for five years and obtained from:—

The Home Office
Radio Regulatory Dept
Waterloo Bridge House
London

Next month we will be giving full details of the receiver and installation of the system into a model. In the meanwhile for the fleet of soldering iron, or just plain impatient, Remcons manual contains full constructional details of the complete system and will be available shortly.

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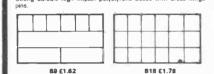
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LM340T-15	0.88			4.60
		LM 1800N 1.94	CA3006	
LM340T-24	0.88	LM1801N 2.25	CA3007	4,15
LM341P-5	0.56	LM1808N 2.10	CA3008	2.55
LM341P 12				
	0.56	LM1812N 6.20	CA3012	1.65
LM341P-15	0.56	LM1820N 1.16	CA3013	1.85
LM341P-24	0.56	LM1828N 1.90	CA3014	2.20
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	6.97	LM1830N 1.90	CA3018	0.75
LM348N	0.95	LM 1845N 1.50	CA3018A	1.10
LM350K	6.50	LM1848N 1.98	CA3020	2.20
LM358N	0.60		CA3020A	2.50
LM360N	3.00	LM 1889N 2.50	CA3021	2.40
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		MC671P 1.75		
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LM741C-14	0.60		CA3062	3.75
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· LM911	0.50	MC840P 1.65	CA3070	1.90
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LM 1304N	1.52	MC849P 0.70	CA3076	2.12
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ı	74C04N	0.24	74C74N	0.56	74C150N	4.14	CD4002	0.18	CD4015	0.75
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ı	74C20N	0.24	74C86N	0.64	74C160N	1.11	CD4009	0.58	CD4019B	0.52
ı	74C30N	0.24	74C89N	4.39	74C161N	1.11	CD4010	0.58	CD40208	1.15
ı	74C32N	0.24	74C90N	0.85	74C162N	1.11	CD40118	0.20	CD4021	1.05
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2N3416 .21	2N3583 1.25	2N3708 .12	2N4914 1.65	2N5088 .30		2N5356	.23	2N5640 .46	2N6180 1.05		1.25	BFX13	.33
2N3417 .25	2N3584 1.35	2N3709 .12	2N4915 2.40	2N5089 .30		2N5358 1	1.75	2N5654 .55	2N6181 .88		1.28	BFX19	.49
2N3420	2N3605 .18	2N3710 .12	2N4916 .22	2N5126 .44		2N5365	.24	2N5655 .55	2N6253 1.00		1.35	BFX29	.34
12.50	2N3606 .18	2N3711 .12	2N4917 .27	2N5127 _22	2N5223 .16	2N5400	.33	2N5656 .65	2N6254 1.45		.66	BFX30	.34
2N3439 .85	2N3607 .18	2N3712 1.35	2N4918 .65	2N5128 .22	2N5224 .16	2N5401	44	2N5657 .75	2N6288 .50		.66	BFX34	.66
2N3440 .75	2N3632	2N3713 1.50	2N4919 .70	2N5120 .22	2N5225 .16	2N5415 1	1.05	2N5661	2N6289 .50	BD222	.66	BFX37	.49,
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2N3445 6.50	2N3639 .33	2N3724 .65	2N4923 .75	2N5137 .22	2N5232A 23	2N5449	20	2N6027 .64	AF240 1.25	BD233	.45	BFX86	.30
2N3443	2N3640 .25	2N3725 .60	2N4924 1.15	2N5138 .22	2N5239 2.25	2N5450	.16	2N6036 1.39	AF279 88	BD234	.46	BFX87	.35
10.00	2N3641 .25	2N3732 2.00	2N4926 1.70	2N5139 .22	2N5245 .37	2N5451	.16	2N6039 1.17	AF 280 .95	BD235	.46	BFX88	.30
2N3447	2N3642 .22	2N3734 .75	2N4927 1.70	2N5140 22		2N5457	.35	2N6099 .62	AFY42 1.68	BD538	.77	BFX89	1.37
10.50	2N3643 .38	2N3735 7.00	2N4928 2.20	2N5142 .22	2N5247 44	2N5458	.36	2N6107 .45	AU110 1.70		.60	BFY10	1.10
2N3448	2N3644 .40	2N4871L .51	2N4944 30	2N5143 .22	2N5248 44	2N5459	32	2N6108 .55	AU113 1.70		.60	BFY18	1.10
12.00	2N3645 .38	2N4888 .54	2N4945 .30	2N5172 .24	2N5249 .38	2N5460	.65	2N6109 .55	BC409 .27	BD581	1.10	BFY19	1.10
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10.00	2N3663 .29	2N4898 1.55	2N4966 .28	2N5183 1.20	2N5294 44	2N5484	.37	2N6122 44	BC415 .16		.65	BFY41	.88
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SN75H40N	0.55	74LS83AN	0.90	74LS194N	0.70
SN74H51N	0.55	74LS85N	0.95	74LS195N	0.70
SN74H53N	0.56	74LS86N	0.44	74LS196N	0.80
SN74H54N	0.55	74LS90N	0.64	74LS197N	0.80
SN74H55N	0.55	74LS91N	1.20	74LS221N	
SN74H50N	0.55	74LS91N			0.80
SN74H62N	0.55		0.70	74LS240N	1.50
		74LS93N	0.64	74LS241N	1.50
SN74L00N	0.55	74LS95AN	0.90	74LS242N	1.25
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SN74L85N	2.62	74LS113N	0.42	74LS248N	1.09
SN74L93N	2.30	74LS114N	0.42	74LS249N	1.09
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74LS01N	0.26	74LS123N	0.83	74LS253N	1.00
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74LS05N	0.29	74LS132N	0.85	74LS261N	3.25
74LS08N	0.26	74LS136N	0.42	74LS266N	0.44
74LS09N	0.26	74LS138N	0.65	74LS273N	1.30
74LS10N	0.26	74LS139N	0.65	74LS275N	3.20
74LS11N	0.26	74LS145N	1.30	74LS279N	0.58
74LS12N	0.26	74LS147N	1.65	74LS280N	1.65
74LS13N	0.58	74LS148N	1.35	74LS283N	1.20
74LS14N	0.75	74LS151N	0.58	74LS289N	3.74
74LS15N	0.26	74LS153N	0.58	74LS290N	1.00
74LS20N	0.26	74LS154N	1.45	74LS293N	1.00
74LS21N	0.26	74LS155N	0.80	74LS295N	1.35
74LS22N	0.26	74LS156N	0.80	74LS298N	1.35
74LS26N	0.32	74LS157N	0.60	74LS299N	2.95
74LS27N	0.26	74LS158N	0.65	74LS323N	3.50
74LS28N	0.29	74LS160N	0.80	74LS324N	1.65
74LS30N	0.26	74LS161N	0.85	74LS325N	2.40
74LS32N	0.27	74LS162N	0.80	74LS326N	2.70
74LS33N	0.29	74LS163N	0.85	74LS327N	2.55
74LS37N	0.32	74LS164N	1.10	74LS348N	1.10
74LS38N	0.32	74LS165N	1.15	74LS352N	1.07
74LS40N	0.26	74LS166N	1.65	74LS353N	1.07
74LS42N	0.80	74LS168N	1,45	74LS365N	0.55
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74LS55N	0.26	74LS181N	2.75	74LS375N	0.66

KNOBS for 1/4" spindles (see catalogue for full range)



Black plastic with mach, metal insert 25mm dia 50.25 As M1 but 33mm dia with pointer 60.31 Black plastic with machined metal insert and sket 35mm dia 60.37 Black plastic with machined metal insert and sket 35mm dia 60.37 Black plastic with machined metal insert and sket 35mm dia 60.38 Black plastic with machined metal insert and sket 30mm dia 60.38 Black plastic body with metal inlay 21mm diameter 60.18 Heavy metal metal black instruction diameter 24mm diameter 60.52 As above but 28mm dia 60.52 As above but 28mm dia 60.52 M4

M6

M8 As above but 28mm dia tune.
M15 Black plastic pointer knob with white
marker, QD 18 mm (skirt) pointer
31mm long £0.15
M16 Highly polished metal
pointer, diameter 22mm £0.20











CECTONICS TOTAL International

What to look for in the June in ue: On sale May 4th

HI-FI RECEIVER



A fifty watt stereo amplifier and a high quality tuner would make two excellent projects in themselves. With specifications such as these boast, we could be sure that the units would soon become widely accepted as the very best in DIY hi-fi. However we've gone one better to combine the two units to produce a receiver of outstanding merit. If you're about to buy, build or borrow a high-class hi-fi — stop it at once until you've read next months ETI.

ECM

ECM (Electronic Counter Measures). Without extensive capability in this field a modern fighter aircraft stands about as much chance against its opponents as would a bi-plane. Radar homing missiles can be jammed, locating radar foiled and laser targeting pick out a plane for ground-to-air attack in a fraction of a second. On the ground too, anti-tank missiles, remotely guided, can "take out" highly sophisticated (and expensive) tanks before they get time to retaliate. The principle behind the machinery are fascinating and their implications chilling. Read about them next month in our comprehensive article.

ANYBODY THERE?

That intelligent life exists elsewhere in the Universe is a mathematical certainty. Whether or not it rides around in flying saucers we cannot afford to ignore the fact that it is there — somewhere. Steps are being taken to communicate with other worlds by some of this planet's largest observatories, and they may surprise you. Don't blame us if after close reading of this, you encounter more than lights in the sky!

READERS' DESIGNS

Next month's is a remote controlled light dimmer which uses an ingenious voltage control circuit and ultrasonic transmission technique. Can be adapted to give remote level control of just about anything.



data sheet

TDA 1008

MULLARD

Introduction

The TDA1008 integrated circuit provides frequency-dividing and gating functions for tone signal generation in electronic organs and other electronic musical instruments. An increasing variety of electronic organs has become available in recent years, their popularity having been enhanced by the rapid expansion of the home entertainments market. To provide effects such as sustain, percussion, and fifth coupling, the organ designer has usually needed to add special electronic circuits to the basic organ design, increasing overall cost. However, in a system based on TDA1008 ICs, these and many other effects can be easily provided without significantly adding to circuit complexity. The reduction in component count and number of key contacts compared with conventional systems results in a significant saving in cost, greater reliability, and easier servicing. With simplified circuits and fewer components, organ designs using TDA1008 ICs are also ideal for the home constructor.

The main features of the TDA1008 are

given below.

The IC is a monolithic bipolar device using I²L logic, and therefore requires no special

handling techniques.

Only a single set of contacts is required for each key, because the TDA1008 provides five octave-related output signals when each of five key inputs is activated. Thus, in a typical system, only one busbar is required for each manual.

An outstanding feature of the TDA1008 is that the tone-output signals are symmetrical about a fixed DC level, and so no DC jump occurs in the outputs when the keys are operated. Thus 'plopping and scratching' sounds are eliminated from the audio output without the need for the usual additional suppression components.

The amplitudes of the five output signals from the IC are proportional to the DC voltage applied to each key input, and because the nominal impedance of these inputs is high, sustain and percussion effects can be added by using simple RC networks in conjunction with the key circuits.

The rate of attack and decay can be adjusted simply by varying a DC voltage applied to a 'sustain control' pin on the IC.

Description of TDA1008

The circuit of the TDA1008 IC with basic peripheral components is shown in Fig. 1. The IC comprises eight divide-by-two circuits and a matrix of gate circuits.

As shown in Fig. 1, the TDA1008 can be driven directly from a top-octave synthesiser, because only one input signal applied to pin 15 is required to produce nine octave-related notes within the IC. The minimum impedance at pin 15 is 28 k ohm.

Up to five keys can be connected to pins 8 to 12. When a DC voltage is applied to one of these inputs, five of the nine octave-related

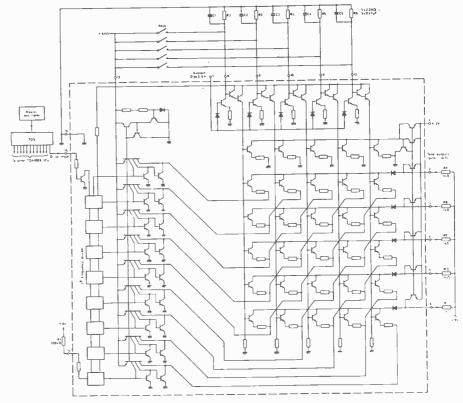


Fig. 1. TDA1008 and basic peripheral circuit.

notes are routed by the matrix circuit to the five tone outputs, as shown in the truth table. Although the maximum input frequency of the TDA1008 is 100 kHz, as can be seen from the truth table the frequency chosen would normally be within the audio range to give the full range of audible tones. If more than one key input is activated, then the signal from each tone output will comprise the sum of all the tones for the activated inputs.

The signal amplitude at each tone output (pins 2 to 6) is proportional to the DC voltage applied to each key input. Sustain and percussion effects can, therefore, be obtained by connecting simple RC networks to the key inputs. Some practical networks are described later. The networks shown in Fig. 1 (resistors R2 to R6 and capacitors C1 to C5) provide a simple sustain effect. The impedance of the key inputs, and hence the rate of discharge of C_1 to C_5 , is determined by the DC voltage applied to pin 7 of the IC. With pin 7 at 0 V, the impedance of each key input is greater than 8 M ohms. When this voltage is increased towards 2.5 V DC, the impedance of each input falls accordingly. Thus the decay of the output waveforms at pins 2 to 6 can be adjusted continuously by simply varying the sustain control voltage at pin 7 The impedance of the tone outputs is determined mainly by the values of the load resis tors R_7 to R_{11} (1 k ohms in the circuit shown).

The ungated output from the last divider stage is provided at pin 14. This output is used when the IC is tested during manufacture, but it can also be used by the organ manufacturer for a quick operational check of each TDA1008. (An output signal from pin 14 when an input signal is applied to pin 15 indicates that all the divider stages are operating correctly.) During normal operation, pin 14 should be connected through a resistor to the +6 V supply so that a current of 20 µA is drawn. In a practical circuit, this can be achieved by connecting a 330 k ohms resistor (R₁ in Fig. 4) between pins 14 and 13.

It is possible to derive a low-frequency output signal for a pedal board from pin 14. Provided that the current drain of 20 μ A is maintained, a transistor can be used to amplify the low-frequency signal from this pin.

Practical Circuits for Organs Using TDA1008 ICs

The number of TDA1008 ICs required for a particular system depends on the number of octaves required by the organ designer. Normally, a minimum of twelve of these ICs

would be required for subdivision of the twelve top-octave notes. For example, a master oscillator, a top-octave synthesiser IC, and twelve TDA1008 ICs would be required for a five-octave single-manual organ. All the ICs, together with the peripheral components, can be mounted on a single compact printed-wiring board.

A brief description of a variety of practical circuits for use with TDA1008 ICs is given below. The five-octave organ has been chosen as a practical example of a system using these circuits.

onounts.

Master oscillator

The Hartley oscillator is a popular choice for electronic organs because of its inherent high stability. The sinewave output signal from this oscillator must be shaped by a Schmitt trigger to provide a squarewave with the correct slew rate for driving the TOS, as shown in Fig. 2. For TOS circuits that require two input signals of opposite phase, these can be provided as shown.

However, because the TDA1008 IC requires a stabilised supply, use can be made of this supply to simplify the oscillator circuit greatly, as shown in Fig. 3. Only four NAND gates contained in a single HEF4011P IC, three resistors (one variable), and a capacitor, are required to produce an output signal of the correct shape for the TOS. One of the gates can be used as shown to provide an output signal of opposite phase.

Switching and envelope-shaping circuits

The TDA1008 IC can be connected as shown in Fig. 4, and will provide five octave-related tones at pins 2 to 6 by operation of a single key contact connected to each key input (pins 8 to 12). The signal obtained from each output, relative to the three supply voltages, is shown in Fig. 5. The amplitude of this signal is dependent on the voltage applied to the key inputs. If any of the output pins remain unused, these pins should be connected to the +9 V supply to avoid intermodulation between the output signals.

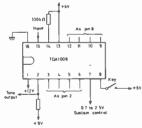


Fig. 4. Simplified connection diagram for TDA1008.

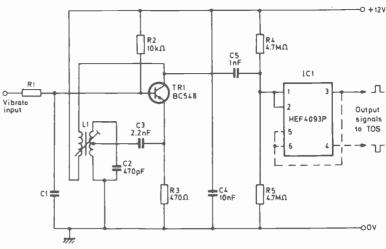


Fig. 2. Hartley oscillator and Wave- Shaping circuit.

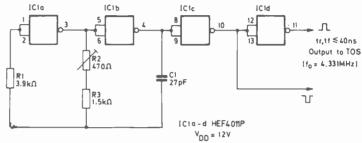


Fig. 3. Master oscillator using NAND gates.

Sustain

The sustain effect, the continuation of a note or notes for a predetermined period after a key has been released, can be easily obtained in an organ system using TDA1008 ICs.

To apply sustain to the five tone-output signals simultaneously, it is only necessary to connect a capacitor between each key input of the TDA1008 and earth, as shown in Fig. 6. With pin 7 either open-circuit or at a low DC voltage, the impedance of each key input is high (\$8M ohms). This impedance, com-

bined with capacitor C_1 , provides a time-constant which gives the maximum sustain period (about 4s with the value shown for C_1). Resistor R_2 is included to reduce this maximum period to a practical value, determined mainly by the time-constant of R_2 and C_1 . The time-constant is given by:

 $t=C_1R_2$, where t is in seconds.

For more details of the device contact Mullard Ltd, at: Mullard House, Torrington Place, London WC1E 7HD.

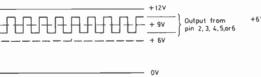


Fig. 5. Output signal from pin 2, 3, 4, 5 or 6.

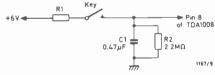


Fig. 6. Sustain circuit.

Tono outnut nin	Key input pin								
Tone output pin	8	9	10	11	12				
2	f _{in}	f _{in} /2	f _{in} /4	f _{in} /8	f _{in} /16				
3	f _{in} /2	f _{in} /4	f _{in} /8	f _{in} /16	$f_{in}/32$				
4	f _{in} /4	f _{in} /8	f _{in} /16	$f_{in}/32$	f _{in} /64				
5	f _{in} /8	f _{in} /16	$f_{in}/32$	f _{in} /64	$f_{in}/128$				
6	f _{in} /16	$f_{in}/32$	f _{in} /64	f _{in} /128	f _{in} /256				

TDA1008 Truth Table.

microfile

Microfile this month has been taken over by Henry Budget, (editorial assistant of Computing Today) during Gary Evans absence.

A slight case of sunstroke

COMMODORE, THOSE WONDERFUL people who gave you a PET, have just taken a great step forward in the true American tradition. Rather than going to the moon they have headed for the Sun. A new solar powered industrial complex has been built in Silicon Valley at Santa Clara and they are moving in. The building was constructed with the help of the United States ERDA and is the first to get a 'solar grant.' The design was chosen out of 80 applications from 35 states.

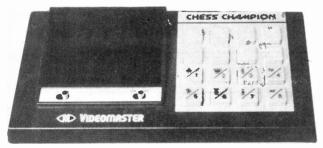
In the 60 000 sq ft Commodore will house their headquarters, the LED and LCD production line, Pet and KIM assembly and warehousing space. The boffins reckon that 90% of all heating requirements will be met by the 6000 sq ft of roof mounted solar panels and a further 3000 sq ft of passive collectors. By using this little lot as a giant heatsink the building will be kept cool in summer and warm in winter . . .





Two views of the new Commodore plant in Silicon Valley. The picture on the right shows some of the roof-top solar panels used for heating.

Also from Commodore I have just heard the current UK sales figures for the PET. They are selling at 200 a week, with about 10% going to the hobby end of the market — that's about 13000 quid a week. (Who said hobbyists were poor?) Commodore reckon that they are holding up well against the competition as well . . .



The Videomaster Chess Champion, the level of play can be altered to suit your prowess, but be prepared for some slow games on the high levels.

We had a new chess player through the office last week micro based of course, and it nearly bored one of our staff to death. He decided to play it on level 5 and the machine took nearly six hours to make four moves. The device is the new Chess Champion from Videomaster and can cater for up to six levels so we may never see our colleague again if he tries that one . . .

The machine actually plays a very good game of chess and the response time is a good indication of the amount of thought that the program is putting in to each move. For the average player Level 1 or 2 will provide a reasonable game, Level 6 is strictly for the budding Grand Master.

Teletext comes home at last

On the subject of micro's — the faithful old 6800 is about to appear in a new home machine, with an added plus. The Liverpool based firm of Technalogics is producing a system that includes full Teletext decoding, allowing you to store information off-line and also to use the full graphics capabilities when running your own programs. The unit is configured for easy expansion and they hope to gain PO approval to connect to Prestel in the not too distant future. The cost of all this is only about £450 for a basic system and I hope to go and see one in the next couple of weeks. A full report will be published in Computing Today if I can get my hands on one

Is it, will it . . .?

BUZZ! Down the grapevine came some news of the long awaited Texas micro. Allegedly it will be a 16 bit machine running PASCAL as the main language and a possible date of arrival is June. The last time I spoke to anyone from Texas the reply was 'No Comment' so we will just have to wait and see . . .

Club round-up

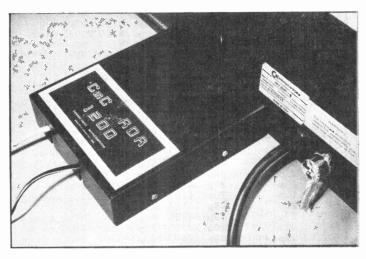
We have been getting news from around the country about computing clubs. A couple of recently formed ones have asked me to give a quick plug. This is a service we delight in performing so please keep the information coming in.

The Bristol Computing Club now meets regularly on the third Wednesday of each month and further information may be obtained from the Chairman, Mr L. Wallace, 6 Kilbernie Road, Bridge Farm Estate, Bristol BS14 OHY. Another new club is the Hull and District TRS 80 Users club. They will be meeting on the second Tuesday of each month and you can write for further information to the Chairman, Mr F. Brown, 421 Endike Lane, Hull, Yorkshire HU6 8AG.

Many thanks to the East London Branch of the ACC for the notice about their third meeting. They meet at the Harrow Green Library in Cathall Road, Leytonstone on the third Tuesday of each month between 7 and 10pm. Your contact here is Jim Turner at 63 Millais Road, London E11. Please note that when you write to these or any other club we may have mentioned in the past it will greatly help them if you enclose an SAE.

Connect your pet to better things

I've just received an interface adapter for the PET that should provide a solution to the problem of getting printout. The device is a CMC ADA 1200, such a lovely name, and has been announced by Petsoft in conjunction with their CMC Word Processor. It arrives in a small case that plugs directly onto the IEEE-488 bus port and will drive any RS232 device such as a printer. The unit comes complete with an encapsulated power supply and can be preset to any Baud rate from 110 to 9600 which makes it suitable for any printer around. The parity and stop bits are settable on a DIL switch to your own needs. The output port can be called direct from BASIC to give program listings or result output from calculations etc. The main use however is that it is directly accessed from the word processor package and will give you the basis of a small office package to handle letters and documents. The cost of the Word Processor program is £25 and the interface adaptor is going to set you back about £90 . . .



Another odd-on for PET, this time an interface adapter for a printer.

The BBC and ETI show.

We've had more than our fair share of dealings with the Beeb this month. First the bad bit, we wish to categorically state that the so-called spelling error shown on 'Thats Life,' was deliberate. Honest. Did you see that recent episode of 'Blakes Seven', our old friend Tolinka, the chess displaying MPU based devices was used for a

game of speed-chess. The BBC recently got in touch with us with a view to using yet another of our past projects Twonky, the musical MPU as the basis for some theme music for a new childrens series. Alack and alas the programme was hit by industrial action, so Twonkys golden moment will have to wait.

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NEOTORS 1-5 to vic Model Molors, 20p. Sub. Min. "Big lock." Motors, 115vm: 3rpm 30p. 12vm: 5 pole model motors 35p. 8 trust 12vic motors El 25, Cazantte motors vic ux napid. 65p. Ceracial guarent motors, 115vm: 4rpm 95p. Smiths cleck mater, syncb. 240vm: 1rev. per hower. 95s.	SERBICOREDICTORIS. All full spec. devices. 741 8 pis DIL 6 for E1.00. No 555 Timers Z5p. T34800 andio RC's 50p. 7415 [wide band- wiren 35p. LISSO BID, 24M4 radio RC 75p. Rallard Offers 30p. T1355 Ayaha nemorical dispiry E2.50. Minister's LDRS (same spec. es PPR1 2) 30p.	TOSHIBA LEGS, 0.2" green 13p, 0.2" green filst tep 14p, 0.2" Green filst tep 14p, 0.2" Green filst tep 14p, 0.2" Clear 17p.	MMULTIMETERS big price reductions on peckal size meters. Model KRTIDO 1,000 shams per vell, mirro scale, range salector switch. 1,000 v AC/DC, TOUK-res. 150ms DC current E4.55. Model KRTIGH same spec. as McKRTIGO but range salectice is vis pred by KRTIGO but range salectice is vis pred	TRANSFORMERS. All 240 vsc primary [pastage per transfermer is shown in brackets after price. Millat/Mark RAME: 6-40 v 100ms. 9-9 v 75ms. 12-012 50ms at 75 peach [159], 12-0-12 10ms 59; 1159, 1-0-6, 0-0 v 200ms £1.10 [20], 0-4.5 9 v 200ms these have an ethical pracket 159; 1159, 12 v 500ms 359; 1229, 12 v 500ms 159, 159, 150 v 15	TRIAC XEMOM PULSE TRAMS- FORMERS. If (PPD style) 30p. Inplus I anh. min. pcb movesting 60p.	
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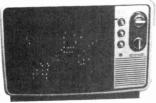
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7400	10p	7460	12n	74137	90p	74195	50p	4055	130p	CA 3140	60p	LM 3909 N		TBA 480 Q	200p
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7402	10p	7472		74141	50p	74197	50p	4060	100p	LF 357	80p	MC 1312 F	150p	TBA 530 Q	200p
7403	10p	7473	25p	74142		74198	100p	4066	35p	LM 211 H	250p	MC 1314 F	190p	TBA 540	200p
7403	12p	7474				74199	100p	4069	12p	LM 300 TR5		MC 1315 F	230p	TBA 550 Q	250p
7404				74143				4070	12p	LM 301 AN		MK 50398		TBA 560 C	250p
7405	12p	7475	25p	74144		74293	90p	4071	12p	LM 304		MM 5314	380p	TBA 641 A12	2 250p
	25p	7476	25p	74145	55p	74L500		4071	12p	LM 307N	65p	MM 5316	480p	TBA 700	180p
7407	25p	7480	40p	74147		74511		4072		LM 308 TO5		NE 529 K	150p	TBA 720 Q	225p
7408	12p	7481	85p	74148	90p	CM			12p	LM 308 DIL		NE 555	25p	TBA 750 Q	200p
7409	12p	7482	75p	74150	65p	4000	12p	4082	12p	LM 309 K	100p	NE 556	90p	TBA 800	80p
7410	12p	7483		74151	45p	4001	12p	4093	70p	LM 310 TO5	150p	NE 562 B	400p	TBA 810	100p
7411	15p	7484	70p	74153	45p	4002	12p	4510	60p	LM 311 TO5		SAD 1024	1500p	TBA 820	100p
7412	15p	7485	60p	74154	70p	4006	80p	4511	70p	LM 317 K	325p	SL 917 B	650p	TBA 920 Q	280p
7413	25p	7486	25p	74155	45p	4007	14p	4516	65p	LM 324	70p	SN 76003		TCA 270 Q	220p
7414	45p	7489	130p	74156	45p	4009	30p	4518	65p	LM 339	60p	SN 76013		TCA 270 S	220p
7416	25p	7490	25p	74157	45p	4011	12p	4520	65p	LM 348 N	90p	SN 76013		TCA 760	300p
7417	25p	7491	40p	74160	55p	4012	12p	4528	80p	LM 346 N	60p	SN 76023		TCA 4500 A	450p
7420	12p	7492	35p	74161	55p	4013	30p	4583	70p	₁ LM 381 N				TDA 1008	350p
7421	20p	7493	30p	74162	55p	4015	50p		VEAR	LM 382	90p	SN 76023		TDA 1034	450p
7422	15p	7494	70p	74163	55p	4016	30p	AY3 85	00 450	PLM 391	90p			TDA 2002	300p
7423	20p	7495	45p	74164	60p	4017	50p	CA 303	9 70	LIVI 39 I	180p			TDA 2002	300p
7425	20p	7496	45p	74165	60p	4018	55p	CA 304	6 60	LIVI 555	25p			TL 084	120p
7426	22p	7497	120p	74166	75p	4019	40p	CA 306	0 225	LIVI 709 C	40p	SN 76660	N 75p	XR 320	250p
7427	22p	74100	80p	74167	160p	4020	50p	CA 306	5 200	LM 710 TO5		TAA 300		XR 2206	450p
7428	25p	74104	40p	74170	100p	4022		CA 307		LIVI / TO DIL	65p	TAA 350	190p	XR 2207	450p
7430	12p	74105	40p	74173	80p	4023	12p	CA 308	0 75	TILM /23 105	40p	TAA 550	35p	XR 2208	
7432	20p	74107	25p	74174	60p	4024	40p	CA 308	4 · 250	LIVI /23 DIL	40p		220p		600p
7433	28p	74108	100p	74175	60p	4025		CA 308		IN LIVI / 33	120p	1		XR 2216	650p
7437	20p	74166	75p	74176	50p	4026	á08	CA 308	6 60	LIVI /41	20p		350p	XR 2567	250p
7438	20p	74109	25p	74177		4027		CA 308		_ LM /48		TAA 790	350p	XR 4136	150p
7440	12p	74118	75p	74178		4028				FINI 1202 IA	100p		150p	XR 4202	150p
7441	45p	74120	80p	74179		4029	- 8-	10, 1000	0AQ 360	LIVI 1458		TAD 110	130p	XR 4212	150p
7442	40p	74121	25p	74180		4030			3 E, 130	_ LIVI 3000		TBA 120 S	6 0 p	XR 4739	150p
7443	60p	74122	35p	74181		4032	80p	CA 312			55p	TBA 120	⊺ 85p	ZN 414	1,00p
7444	60p	74123	40p	74182		4033	100p	DA 313		- 21	T /Tax	10060-5	1 50	First gra	de LEDa
7445	65p	74125	35p	74184		1 .	60p			8 Diodes by IT				125	
7446	50p	74126	35p		100p	1	60p	Sta		102 1024×1				10p_each.	100 for
7447	50p				320p	1 - 1 - 1	90p	l		12 256×4 bit 4				£ 7.50, 1. nair £60.	,000 for
7448	50p	74130		74190			80p	Murat	ta Ultraso	nic Transducers	4UKHZ	, £Z.UU eac	in; £3.50 p	idii too.	
7450	12p	74131	90p	74191			50p			All prices inch	ud post ar	10 VAI			
7451	12p	74132		74192			25p			T	DO	WFI			
7453	12p	74135		74193			25p		206 CT 04	ULS ROAD, HIGH	BILBYCO		ON N 1 751	01.226 1489	
7454		1		74194		4054	100p		300 ST. PA			redit cards acce		. 01-220 1403	
/454	12p	74136	80p	1/4194	+ aab	14054	TUUP	1			1000000 0				

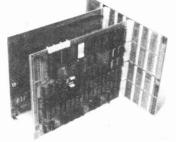
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Suitable mains power supply parts: consisting of mains transformer, bridge rectifier, smoothing capaci-tor and set of rotary stereo cen-

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HEADPHONE AMPLIFIER

Here's a project for the true hi-fi enthusiast, or for the guy who simply likes to 'listen in silence'.

A HEADPHONE AMPLIFIER is a gadget for the true hi-fi stereo enthusiast. It is a low-distortion wide-band low-power amplifier, without built-in tone controls. It lets its owner hear signals virtually 'as recorded', with none of the usual problems from 'processing' distortion, or from room acoustics. Equally important, it lets its owner listen to recordings at full orchestral levels without upsetting the neighbours or causing the pet budgie to shed its feathers.

The ETI headphone amplifier has a couple of special features. It has a low-noise RIAA-equalised preamplifier built into each channel, so it can accept input signals directly from a phono pick-up. It can switch-select either phono, tape, or tuner inputs, and can drive up to four sets of 8 ohm headsets simultaneously at total power levels up to a few hundred milliwatts. The unit can thus be used for both individual and group listening.

Each 'phone output channel of the amplifier has a source impedance of 10 ohms. This impedance provides each 'phone with good damping and transient response, and at the same time makes each output immune to short-circuit damage. The available power at each output is sufficient to drive the ear drums of a 'phone user to the threshold of pain when using a decent 8 ohm headset; you can't ask more than that.

Construction

All of the units electronics components, including the mains transformer, are mounted on a single PCB. The layout is quite compact, so extra care needs to be taken over the construction, particularly with regard

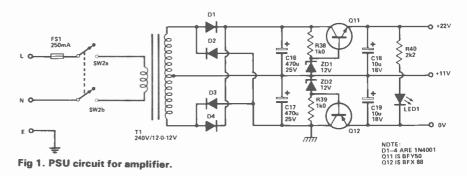


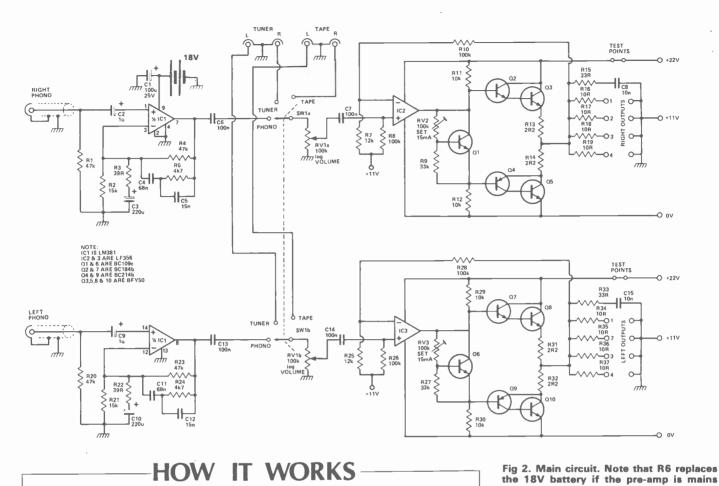
to the polarities of semiconductor devices and electrolytic capacitors.

We fitted our prototype unit in a fairly tight-fitting Verobox, and used a 6-way DIN connector for the inputs, rather than the six individual connectors shown in the circuit diagram. Note that screened lead must be used to connect the two phono inputs to the input of the preamplifiers.

When construction is complete, set RV2 and RV3 to minimum

resistance, insert a DC current meter in series with the test point of the Right channel, and switch the unit on. Check that the unit is functional, and then adjust RV2 so that the meter reads a quiescent current of 15 mA. Repeat the procedure for the Left channel, using RV3 to set the 15 mA quiescent current, and remembering to fit links across the test points after the meter is removed. The unit is then complete and ready for use. Good listening.





HOW IT WORKS

The ETI Headphone Amplifier uses two identical amplifier channels, each comprising an RIAA-equalised preamplifier, an input-selection switch and a volume control, and a main amplifier stage. The design uses two mains-derived stabilised power lines, which are fed to each of the two channels.

Each pre amplifier stage is designed around one half of an LM381 low-noise dual preamplifier IC. In the Right channel, R1 matches the preamp input impedance to that of a standard magnetic pick-up, R2 and R4 set the quiescent output of the pre amplifier at approximately half-supply voltage, and R3 to R5 and C3 to C5 serve as the RIAA equalisation network. The preamplifier stage has a voltage gain of about 41 dB at 1 kHz, and gives an output of about 600 mV from a 5 mV input at this frequency.

Input signals to the main amplifier stage are derived from either the preamplifier output or the tape or tuner inputs via switch SW1 and volume control RV1. The amplifiers are standard class-AB types,

with voltage gains of about ten. In the Right channel, the voltage gain is determined by R7 and R10. The quiescent current of the output transistor stages (Q3 and Q5) are controlled by 'amplified diode' transistor Q1, and are adjustable via RV2. Outputs are fed to each channel of each headset via a 10 ohm limiting resistor: R15 and C8 act as a Zobel network across the output, and enhance circuit stability.

Note that the op-amp used in each main amplifier stage is an LF356 high slew-rate type, which enables the amplifier to give a good high-frequency performance. Also note that the input and outputs of the amplifier are referenced to the 11 volt 'half supply' power line, and not to the zero volts grounded line.

The two power supply lines are derived from the mains via 12 V - 0 - 12 V step-down transformer T1. Each output is controlled by a series-pass transistor and zener diode regulator network. The nominal output voltages of the lines are 11 V and 22 V. The zero-volts line is grounded.



PARTS LIST-

RESISTORS	
R1,4,20,23	47k
R2,21	15k
R3,22	39R
R5,24	4k7
R6	390R
R7,25	12k
R8,10,26,28	100k
R9,27	33k
R11,12,29,30	10k
R13,14,31,32	2R2
R15,33	33R
R16,17,18,19,34,35,36,37	10R
R38,39	1k
R40	2k2

POTENTIOMETER

PUTENTION	ALILA
RV1	dual 100k
RV2,3	100k sub-min
	preset

CAPACITORS

C1	100µ, 25V
C2,9	1μ



BUYLINES

The only component that may be difficult to find is the LF356 FET on-amp

Marshall's can supply this IC.

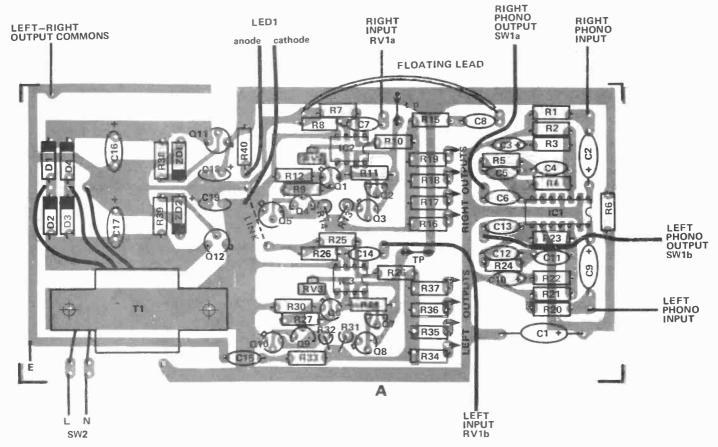


Fig 3. Component Overlay for the headphone amplifier with R6 in place to mains power the pre-amp. A lower noise figure can be obtained by battery powering the pre-amp. Connect the battery as shown in the circuit, and break the track at point A, Remove R6 from overlay.

 $\begin{array}{cccc} C3,10 & 220\,\mu \\ C4,11 & 68n \\ C5,12 & 15n \\ C6,7,13,14 & 100n \\ C8,15 & 10n \\ C16,17 & 470\,\mu,\,25V \\ C18,19 & 10\,\mu,\,18V \\ \end{array}$

SEMICONDUCTORS IC1 LM381

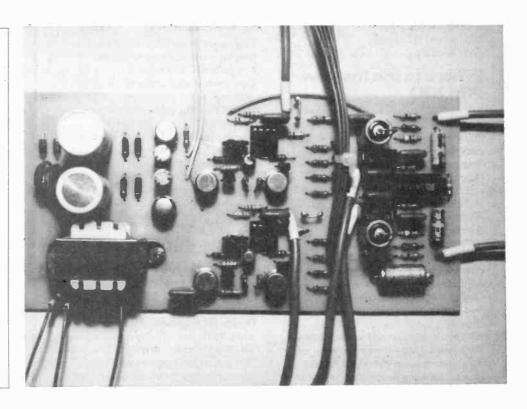
IC2,3 LF356 BC109C Q1,6 BC184B BC214B 02.7 04.9 Q3,5,8,10,11 BFY50 BFX88 Q12 D1,2,3,4 IN4001 ZD1,2 12V zener standard 0.2" LED1

MISCELLANEOUS

SW1 2-pole 3-way SW2 DPDT

T1 12-0-12V, 100mA

Fuseholder and 250mA fuse connectors and case to suit.



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Digital testing: check computer clock frequencies, divider ratios and other digital circuitry.

RF circuit checks: test local oscillators, BFOs, test IF and detector performance. Video equipment: check syncronised circuits, scanning frequencies, video bandwidths, etc.

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Frequency range: 20 Hz.to 200 MHz Display resolution: up to 8 digits Lowest frequency resolution: 0.1 Hz Gate time: decade adjustable from 0.01 secs to 10 secs

Sampling rate: varies with gate time up to 5 per second

Display format: 8 LEDs, direct reading in kHz.

Attenuator: -20 db

Input impedance: 1M in parallel with 50 pF Timebase accuracy: 0.3 ppm/°C,

10 ppm/ year

Dimensions: 6.2 in x 3 in x 1.25 in

Weight: 6 oz

Power requirement: 9V DC or AC adaptor

Sockets: standard 4 mm for resilient plugs Standard accessories: test leads and prods, carrying wallet, owner's instruction

Optional equipment: AC adaptor for 240 V 50 Hz power; deluxe padded carrying case; connector kit comprising BNC, co-ax, DIN and phono adaptors, plus telescopic aerial for off-air transmitter measurements

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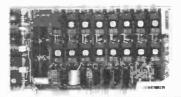
16K OR 32K EPROM

4K EPROM wmc/in.

This board is designed to operate with any speed or power 1702A. Addressable in 4K byte increments and can be configured to occupy either 2K or 4K segments. It can be populated one memory chip at a time. Bare

board \$30, board with parts \$200, assembled \$230. Part No. EPM-1

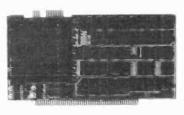
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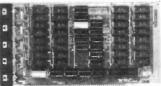
8080A CPU (With Eight Level Victor Interrupt Capability) wmc

Uses the 8080A and the 8224 clock chip. The crystal frequency used is 18 MHz and the vector interrupt chip is the 8214. The board will function normally without the interrupt circuitry. When the interrupt circuitry is built up, the board will respond to eight levels of interrupts. Designed to be a plug-in replacement for the IMSAI CPU board and will work in other computers with the appropriate modifications made to the ribbon cable connector pin out from the front panel. The board will work in systems without a front panel if the system has a PROM board that simulates the functions of the panel. Bare board \$30, with parts \$185, assembled \$220. Part No. CPU-1



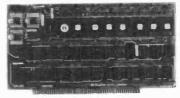
16K STATIC RAM

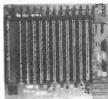
Operates with any speed or power 2114. All put and output lines are fully buffered. Addressable in 4K byte increments. If the system has a front panel, the board will allow itself to be protected. If there is no front panel, the board will not allow itself to be protected. The board has Bank Address capability, Phantom Disable, MWRITE, and selectable wait states. Bare board \$30, board with parts \$665. Part No. MEM2



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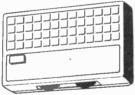
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STANDING WAVES

A standing wave has nothing to do with goodbyes on railway stations, but they could just be responsible for the poor quality of 'Crossroads'.

YOU KEEP COMING across that phrase, don't you, and it seems a bit daft. Waves wave, after all, they don't stand about. Or do they? Depends how you look at it and what you're looking at.

Pick a wave, any wave, radiating off an aerial into space. When this happens, the wave is radiating out from the aerial in all directions. The wave is an electromagnetic wave but since we only usually detect the electric part we can forget about the magnetic part for the moment. Let's just remind ourselves of what a wave like this is and does.

Equating With The Problem

A radiated wave of this type is a travelling wave. If we intercept it with an aerial attached to a sensitive oscilloscope what we would see on the screen (Fig. 1) would be the familiar sine wave trace, so that we could measure the time between peaks of the wave. This time between peaks is called the period or periodic time (T) of the wave, and is the quantity we measure by making use of the calibrated time base of the oscilloscope. This time period is related to the frequency of the wave: f = 1/T with T in uS frequency f is in MHz. For example: if the period is 0.4 uS, then the frequency is 1/0.4 = 2.5 MHz.

The wave is travelling, though, so that places a distance apart will get a different phase of wave. In the drawing, of Fig. 2, A will receive a peak of the wave earlier than B, simply because A is nearer the transmitter. The distance between two places which receive peaks which are just 360° out of phase is the distance we call the wavelength.

In the time of one complete cycle, the wavelength is the distance that a wavepeak travels, so that the speed of the wave is simply frequency wavelength. For an electromagnetic wave (radio wave) in space, the speed is a constant 300 million metres per second $(3 \times 10^8 \text{m/S})$, so that this is the quantity equal to frequency \times wavelength. For a 1 MHz wave, the wavelength is $3 \times 10^8 / 1 \times 10^6 = 300 \text{m}$.

For a 1000 MHz wave, though, the wavelength is just $3\times10^8/10^9=0.3$ m — hence the alternative title of 300 mm wave. This frequency × wavelength business applies also to sound waves, incidentally, except that sound waves crawl along a lot slower, about 330 m/S. A 1 kHz sound

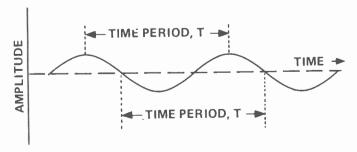


Fig. 1. Time period. This can be measured between neighbouring peaks or from one zero-crossing to the next-but-one, as shown.

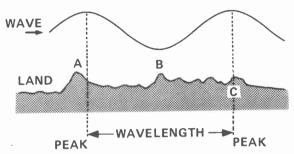


Fig. 2. Wavelength. Imagine the wavepeaks moving from left to right. At the instant shown, a peak is at point A, and a trough at point B, but the previous peak has reached point C. The distance between points A and C is one wavelength of this wave.

has a wavelength of 330/1000 metres, which is only 330 mm, almost the same as a 1000 MHz radio wave.

If we're in the business of beaming waves into space or testing loudspeakers in open fields, this is as much as we need to know about waves, but we find nearly always that there's some reflections around. Now the effect of a wave reflection meeting a wave is the same as the effect of two waves meeting each other — if the wave and the reflection are in phase, then the result is a large amplitude wave, if they are out of phase the result is a reduced wave. We can expect to find some variations in wave amplitude, then, if a wave meets its own reflection.

Reflecting On The Problem

The easiest example to sort out is when a wave meets a reflection of the same size travelling in the opposite direction. Now the mathematicians can do this without drawings, simply by fiddling with equations, and those of us who play with programmable calculators can sort it out that way - the fortunate owners of computers can watch the whole thing - play it out in slow motion. We have to do it the hard way - using imagination with the help of a few drawings. Fig. 3a shows a forward moving wave meeting a reflection — it's a diagram frozen at an instant in time because what is plotted is wave amplitude against distance. Fig. 3b shows the same picture an instant later, both waves have moved an identical distance in their opposite directions. A few more stills from this exclusive movie, and we begin to see glimmerings of something interesting. The combination of the forward wave and its reflection travelling in the opposite direction has produced a new wave pattern. At some points along this pattern, there is always complete cancellation — the forward wave and the reflected wave are always in antiphase so that there is no signal at this place — ever. At other places there are varying amounts of signal right up to a whopping great peak whose amplitude is about twice as much as either of the travelling waves. This pattern is what we call a standing wave (Fig. 4) there is still a wave present, because a graph of voltage

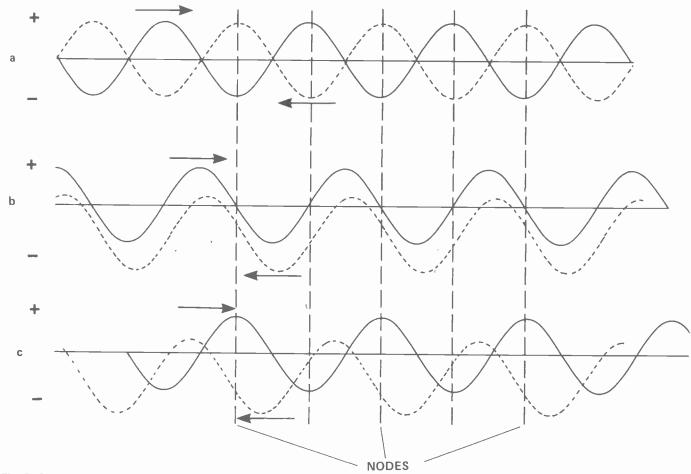


Fig. 3. Setting up standing waves. The solid line (a) represents a wave moving from left to right, the dotted line represents its reflection moving in the opposite direction. At (b), each wave has moved about $\frac{1}{4}$ cycle, and at (c) $\frac{1}{2}$ cycle along in its own direction. The positions where the waves cancel (because they are equal and opposite, or both zero) remain fixed though. These positions are called nodes.

plotted against time shows a wave, but there's no movement of phase. In any standing (or stationary) wave like this there will be nodes — places where there's no wave signal, at all — which are half a wavelength apart and antinodes — where there's a maximum wave signal — which are also half a wavelength apart but out of phase with the nodes.

The Effect On You

What's in it for us? Quite a lot, whether you dabble with high frequency signals or with loudspeaker cabinets. Standing waves have a lot of influence whenever a wave can be reflected. For example, there are places where UHF TV reception is terrible. Shifting the aerial slightly, though, makes the world of difference. Why? Because we're sitting in the middle of a standing wave pattern, that's why. Place your aerial at a node and you can forget about Kojak. Shift it by just half a wavelength, and yours is the strongest signal around. At 500 MHz, half a wavelength is just 300mm — not very far to shift.

How To Find Them

Standing waves can exist on a wire as well. One of the old classic methods of measuring the wavelength of a high-frequency radio oscillator is called Lecher Lines. The Lecher lines are two parallel metal bars of thick wires which are connected to the oscillator output. A shorting bar is fitted

with a detector, which might be a neon lamp (for high voltage signals) a small lamp-bulb (for low voltage signals) or a diode/meter circuit. Sliding the bar along the lines (Fig. 5) results in the detector indicating points of no signal, the nodes; and points of maximum signal, the antinodes. The distance between two neighbouring nodes, or two neighbouring antinodes, can be measured — this distance is half a wavelength.

The wavelength of a sound wave can be measured in the same way. One classic method of measuring the wavelength of a sound along a pipe was to sprinkle powder on the pipe. When the sound wave set up standing waves, the powder would gather into piles at the nodes of the standing waves, and spray away from the antinodes, so that the half-wave distance between nodes could be measured. It's equally easy to measure the wavelength of standing waves in a room by moving a microphone attached to an AC voltmeter and noting the position of nodes — once again the distance between two neighbouring nodes is equal to half a wavelength.

Leaving Loose Ends

If a length of coaxial cables connected to a circuit is left either open circuit or short circuit, standing waves can be set up in it, with a node at the short circuit or an antinode at the open circuit end. If the length of the cable is just right, that's fine. If it's not, then signals will reflect to and from along the cable, arriving at the circuit and with a time delay equal to the time taken to travel along the cable and back. Because of this effect, we seldom cut cables to a length which will permit standing waves — instead we terminate each end of the cable in a resistance value which will

prevent reflections — this value of resistance has to be equal to a quantity called the characteristic impedance of the cable (calculated from the inductance and capacitance per metre of cable). With an open or shorted cable, on your telly, you can expect to see 'ghost' images — several edges to each object.

Advantages And Disadvantages

We do, however, encourage standing waves in aerials. TV and FM aerials are cut to a total of half a wavelength so that a standing wave is set up on them. This allows us to do two things which would not otherwise be possible. One is to extract the maximum energy from the signal — the aerial responds like a tuned circuit to the correct wavelength; the other is to match the aerial to its cable. At one end of a half wave aerial we have an antinode — maximum wave amplitude. At this point we have maximum voltage, but no current. At the centre of the aerial there is a node — zero voltage but maximum current. We can select a point along the aerial to connect the cable so that the ratio of voltage to current is just right — 75 ohms for most coaxial cables, and

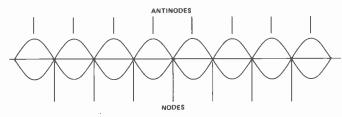


Fig. 4. Representing a standing wave. The standing wave has the same wavelength as the moving waves which cause it, but the nodes and antinodes are at fixed points, quarter of a wavelength apart from one another.

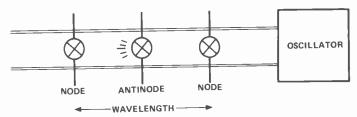


Fig. 5. Using Lecher lines. A high-frequency oscillator attached to parallel wires can display standing waves, using a small light bulb to detect the positions of nodes and antinodes.

in this position there will be the maximum transfer of signal from the aerial to the cable.

At the tuner, standing waves create another sort of problem — the problem of how to earth conductors. Earth one point of a conductor and there will be a node at that point — but there will also be an antinode (maximum signal) just ¼ wavelength away. The result is that earthing, a conductor may have just the opposite of the effect you expect unless you earth at just the right place. Move any of the conductors in a tuner, and you disturb the standing wave pattern — even a dent in the metal case of a UHF tuner can make a difference.

It's not always such a happy story. The greatest difficulties with standing waves arise when we try to design a loudspeaker cabinet. Each solid surface and cracks or gaps will behave as a short circuit or an open circuit respectively. A loudspeaker cabinet will be a mess of standing waves, therefore, unless we do something to absorb them. The room we use for listening will also have standing waves at some frequencies (depending on its dimensions) and in some directions — this is particularly noticeable in an empty room stripped of all its furniture. All in all, standing waves are all around us — we have to live with them!

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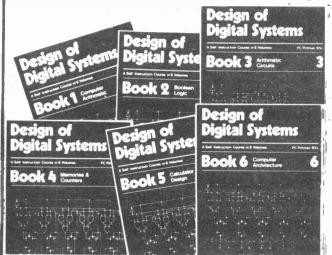
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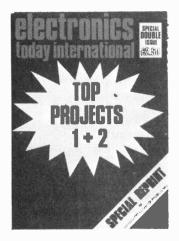
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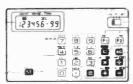
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CAR IMMOBILISER

Here's a low-cost project that gives your car good protection against joy riders and a drunken driver.

THE ETI AUTOMATIC
Immobiliser is an inexpensive but
highly original car protection device.
It has been designed to prevent a car
being driven away by the 'joy rider'
type of thief, or by a drunken
owner-driver. Major features of the
design are lack of circuit complexity.

design are lack of circuit complexity, low building costs, and simple installation of the unit in any vehicle.

The circuit is designed to immobilise a vehicle's ignition system, by shorting out its contact-breaker points via a pair of relay contacts, as soon as the ignition is turned on. The owner then has five seconds to turn the immobiliser off by sequentially operating a set of four push buttons. If the four buttons are not correctly operated within the five second period, the ignition system remains immobilised and the

vehicle's engine cannot be started. The automatic immobiliser timing sequence restarts each time the ignition is turned on.

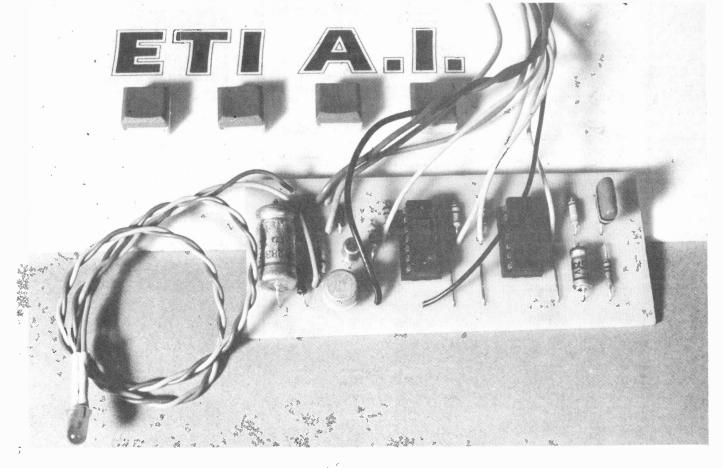
There are four basic concepts behind the ETI Automatic Immobiliser system. The first of these is that, since the immobiliser activates automatically as soon as the vehicle's ignition is turned on, the vehicle is given a good degree of protection against the drive-away car thief, even if the owner leaves the car doors open and leaves the ignition key in its lock.

The second concept is that a thief entering the vehicle will have no idea of the purpose of the four push-button switches associated with the immobiliser, so these switches can be quite openly displayed on the vehicle's instrument panel, together

with a LED that tells its legitimate owner the immobiliser circuit state.

Thirdly, because only five seconds are available to de-activate the immobiliser via the four sequentially-operated switches after first turning the ignition on, the system gives a good deal of protection against the fumble-fingered drunken owner-driver.

The final concept is that, because of the three factors already outlined above, the final circuit does not need to be super-sophisticated or to have an unbreakable 'key' sequence network in order to be highly effective in its functioning. Simplicity and effectiveness are thus the key features in the design of this ETI Automatic Immobiliser unit.



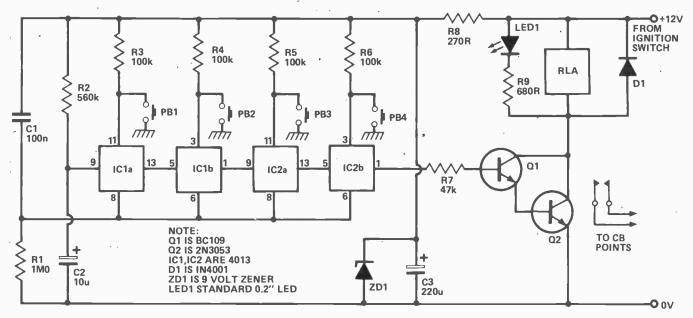


Fig. 1. Circuit diagram for immobiliser.

Construction

There should be no problems here. The relay can be any 12-volt type with a coil resistance greater than 100 ohms, and with one or more sets of normally-open contacts. The PCB and relay can be fitted in a metal box, or can be simply mounted on an aluminium plate that is screwed to the rear of the vehicle's instrument panel.

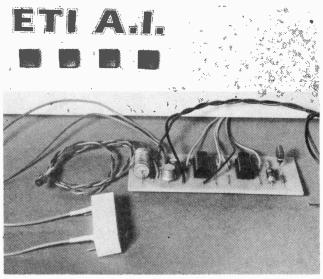
The unit's 12-volt rails must be connected to the vehicle's supply via the ignition switch. The normally-open relay contacts should be connected across the vehicle's contact breaker points. The LED and the four push-buttons can be mounted on the vehicle's instrument panel, either directly or via a screw-on panel.

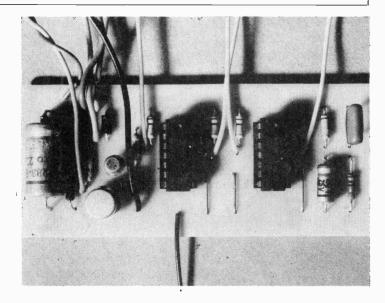
HOW IT WORKS

The circuit is designed around the 4013 D type flip-flop. It derives its power from the car battery via R8 with stabilization provided by ZD1, C3. The chip features direct set and clear inputs and complementary outputs. Data at the D input is transferred to the outputs on the positive going edge of the clock. The clear inputs are not used in this design and are tied to ground, the set inputs are connected together to the junction of R1, C1. This ensures that on switchon the flip-flops will start up in the same state and a high level, logic 1, will be present at the output of IC2b. This voltage is fed to the base of Q1 via R7 and will cause the relay to turn on, disabling the car. Q1 and Q2 are connected as a super-alpha pair which effectively produces a super high gain transistor whose gain equals that of Q1 multiplied by Q2. D1 protects the transis-

tors against the back EMF of the relay. System status is indicated by LED1.

To re-enable the system and start the car a logic 'O' must be present at the output of IC2b. This is produced by passing it down the line from the input of IC1a by depressing PB1, 2, 3 and 4 in turn. A novel feature is introduced here. At switch-on C2 is discharged and IC1a will see a low level logic 'O' at its input. This must be transferred to the output by depressing PB1 before the voltage rises above the transition level of the D input as C2 charges via R2. If PB1 is not depressed until about five seconds after switch-on then the junction of R2, C2 will present a logic '1' disabling the system until power is removed and re-applied. To make the system really difficult to beat, resistor, capacitor networks could be inserted between stages.





PARTS LIST RESISTORS all 1/4 watt 5% 1MO 'R2 560k R3, R4, R5, R6 100k R7 47k 270R R8 R9 680R CÁPACITORS 100n C2 10u 16V electrolytic C3 220u 16V electrolytic SEMICONDUCTORS Q1 BC109 2N3053 IC1, IC2 IN4001 ZD1 BZY88 C9V1 400mW 9 volt zener MISCELLANEOUS ' PB1_PB2_PB3_ push to make pushbutton switches

12v relay (see text)

PR4

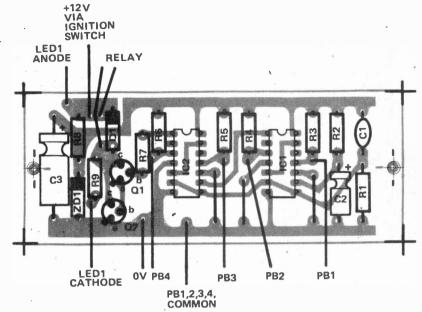


Fig. 2. Component overlay.

RUYI INFS

No problems whatsoever with any of the parts for the Car Immobiliser, Maplin and Watford should be able to supply all the parts. The case is

very much up to the individual, a strong watertight case however is essential to prevent any 'false alarms' due to ingress of water.

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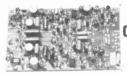
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audiophile.

Not strictly news this month. Views. Readers views. Most of the letters to Audiophile are 'upgrading' enquiries. Most but not all — some of the more interesting appear below, presided over by Ron Harris.

THIS MONTH IT'S over to you. With all the letters that have come in to Audiophile since it began I thought it was about time some of them saw the light of print. The selection is taken over about three months, and I hasten to add that all have been answered prior to this public pondering.

As you can see we get quite a varied mailbag to put it mildly, but still not enough of you are writing (to ETI in general) for our liking. Let's have more feedback please. Mind you the two gentlemen who wrote in to ask who this Felicity Kendal is anyway have not been answered. After the

sedatives had calmed my outrage, and the expletives died from the air, it was somehow still not possible for me to compose a reply within Home Office rules.

Time has passed, however, and has healed the wounds in passing. (And wounded the heels I hope.). So gentlemen, let me state the obvious in as calm a manner as possible. Felicity Kendal is quite simply the most beautiful woman in the universe. Write it out 1000 times before one more copy of ETI reaches your unworthy hand.

Anyway onto more sonic matters

BAD START?

Dear Sir,

I own a hi-fi system comprising a Garrard SP25 Mk.5, Goldring G800, and 'home brew' amp and speakers. The loudspeakers are comprised of twin-coned Fane bass units and a pair of EMI drivers for mid and top.

I should like to upgrade this system, and wonder what would be the first thing you'd do?

J. WATERS FAVERSHAM

Sell It.

STEAM VALVE

Dear Sir,

Some time you (ETI) published a series of articles on the subject of valve sound in amplifiers. A friend recently brought these to my notice and it surprised me that an otherwise modern magazine like what ETI is known for should be backing this old-fashioned nostalgic rubbish. Do you really believe that valves sound better than transistors? Of course they can't! Why did we ever change if they do?

I suggest you set yourselves a

listening test and then have the courage to publish the results!

W. WITHERS, M.Eng.
PERTH

Hold it a minute mush.
Somewhere amid the prejudices I think you express the opinion that ETI is pro-valve. If this is indeed the message, then it is mistaken. To condemn a whole technology in such sweeping terms, be it valve or transistor, is akin to running down football because the All Blacks beat Liverpool at hockey. (Think about it.)

My own opinion is that the best of the solid state designs give a more accurate representation of the signal than do the top vacuum tube units. Beyond that yer pays yer money and takes yer choice

BARK DISTORTION

Dear Sir,

I am writing to tell you (and your readers if you should choose to print this) and the great fun we used to have in the 'Old Days' of hi-fi. My very first gramophone used to use wooden needles, pine I think, which wore out very quickly, but gave (to me) amazing tone. Somehow nowadays it never sounds as good as I remember it

being then. Are there any of your "more mature" readers who'd care to correspond with this old'un about the early days? Anyone remember shellac?

F. NEWTON MANCHESTER

I can't resist this:— the pitch in pine sounded fine eh? In apology for that, if any readers care to write to Mr Newton via Audiophile, I will pass on the epistles.

EAT YOUR HEART OUT

Dear Sir,

ETI hi-fi reviews!?! How come? Not a bad idea but stop ignoring the budget end of the business. We also play records who stand and drool (at SME's) you know.

Also let's see yer credentials Mr Harris — wots yer reference system? Reveal all and get rid of these evil thoughts telling me it's a wind-up job from Woolies! Keep up the reviews but more radio? It still exists you know.

D. ALEXANDER LONDON

You keep your hands off my credentials, they've never hurt anyone and are certainly not to be revealed within the pages of ETI. I didn't get where I am today going

around revealing me credentials.

As for reference system that consists of: Technics SL150 Mk.2, SME 3009 Mk.3, Goldring G900SE Mk.2, Shure V15 Mk.4, Lecson AC1 and AP3 Mk.2, Pioneer TX9500 Mk.2, Celestion Ditton 66 loudspeakers and Sony EL7 Elcaset (for as long as they let me hang onto it!) Occasional use is also made of Ultimo 20 and Coral 777EX moving coil cartridges. The Technics is fitted with a GA Audio glass turntable mat, and for headphones I use Koss Pro 4AAs or ESP10s as the occasion demands. My budgie has a green beak and my plants all died last week.

Revealing enough?

QUADRUPLE QUERY

Dear Sir.

Please could you explain some terms I keep reading in hi-fi magazines (including yours) and that no one has ever explained? These are 1) Selectivity 2) Modulus 3) Dynamic Range 4) Musicality.

Also I wish to upgrade my Quad 33/303 set up for more power and would welcome suggestions. Thank you.

H. COHEN STOKE

Easy ones first. A new amplifier to replace a Quad. Since you give very little information as to speakers, cartridge, room size etc etc I'm gonna have to assume that all you seek is a more powerful version of the same thing! In which case why not try the Quad 405 as a starting point? If this fails to appeal, and funds allow, cast an ear over units by Lecson, Meridian and maybe the Sony VFET designs.

Now to the definitions you requested. Quite a mixed bag this little lot. Ah well here goes:—
1) Selectivity (of tuners):—the ability of the machine to discriminate against signals on adjacent channels (± 200kHz) to the one you're trying to tune to. Good selectivity is a must with sensitive tuners.

2) Modulus:—Presumably you spotted this lying next to the word impedance. Otherwise it must have been a maths book. In literal terms modulus means "size

of", ignoring positive and negative aspects. Phase differences can make impedance (resistance to passing a signal) difficult to express simply. Non-mathematically it is best just to regard modulus as meaning 'magnitude of' but remember there is more to it!

Mathematicians please don't write in -z=x+iy=r ($\cos\theta+i\sin\theta$) mod $z=/z/=r=\sqrt{x^2+y^2}$ OK?

3) Dynamic Range:—the difference, in dB, between the softest and loudest sounds reproducible by the hi-fi under discussion. For example a cassette with 20dB of tape noise, and on which compression sets in at 70dB, has a dynamic range of 50dB.

4) Musicality:—oh what a lovely word! Whichever anomic intellect invented it has my congratulations. The really nice thing about it is that NO-ONE knows what it means! Currently it is employed (I think) to express the amount of 'information retrieval' a system is capable of. Earlier in its history it was simply a word reviewers used to mean 'nice' with exactly the same amount of precision as the word implies. Next week it could be describing how satisfying a crunch is generated in the destruction of a piece of toast. **Musical Mothers Pride?**

EH?

Dear Sir,

I strongly feel that transient intermodulation distortion and slew rate limiting together with uneven harmonic distribution are the total reason for the so-called 'transistor sound' in modem amplifiers. Do you agree?

M. DAWES SWANSEA

My answer lies entirely within the negative quadrant of the sphere of communication.

ALL AT SEA

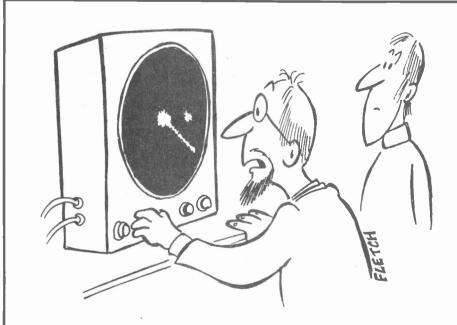
Dear Sir,

As a regular subscriber to ETI, I am writing to express my protest at ETI's hi-fi content. If I wanted to read about hi-fi I would buy hi-fi magazines, God knows there are enough of them.

What ETI should be doing is more articles explaining how circuits work, so that your readers can design them themselves. And how about more circuits for us boating enthusiasts?

S. McGREGOR LONDON

How did you get on this page?



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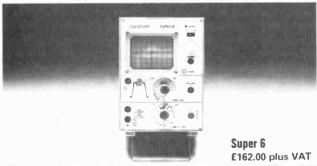
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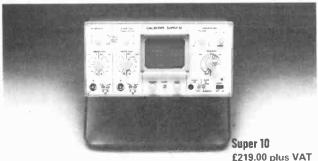
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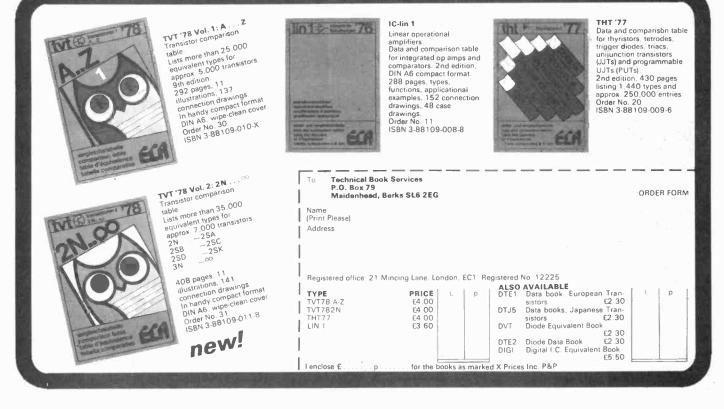
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Sep 77	'Graphic Equaliser	601	1 75	20 28	BFGH
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Oct. 77	Watchdog	604	90	18 80	BEGHL
Oct 77	Watchdog P S U	605	75	6 1 4	BEH
Aug. 77	'Sweep Oscillator	606	2 90	36 41	BFGHL
Sep. 77	'Stereo Simulator	607	70	5 77	BEGHL
Dec 77	'Freezer Alarm	608	65	7 0 7	* BFHL
Nov 76	'General Purpose Preamp	609	70	3.83	BEG
Jul 77	'GSR Monitor	612	80	16 55	BEGHL
Apr 77	'Burglar Alarm	613	70	9.00	BEGH
Feb 77	Bench Amptilier	615	80	11 10	BEGHL
Nov 77	Compander	617	1 75	23.30	BEGHL
Mar 77	'50 watt High Power Amp	618	1 45	7 9 1	BE
Mar 77 Mar 77	100 watt High Power Amp	619	1 45 -	10 61	B€
Oct 77	'High Power Amp P S U 'Digital Thermometer	620	1 20	14 75	BEJ
Feb 77	'LED Dice	621	1 40	18 70	BFGHL BEGHL
reb //		624 625	2 40	5 83 12 70	8FGHL
	'Active Crossover (2 pcbs) 'Marker Generator	626	90	6 97	BEGHL
Nov 77	Skeet	627	1 75	18 37	BEGHL
	Flash Trigger	628	75	5.07	BEGJ
	'Disco Light Show	629	3 30	21 94	BFGJ
	Pink Noise Generator	630	70	3 3 5	BEL
Nov 76	541 Train Controller	T001	80	15 86	BEHL
Jan 77	444 5 watt Stereo (2 pcbs)	T002	2 15	26 47	BEGK.
Feb 77	448 Disco Mixer	1003	1 75	16 36	BEJ
Dec 77	Clock B.	T004	2 30	13.61	BE
Jan 78	House Alarm A	T005	2 20	25 68	BEHM
3017 70	House Alarm B	1005	95	3 99	BE
Feb 78	Metal Locator Mk III	1007	1 05	19 10	BEHL
March 78	Frequency Shift P S U	T008	75	4 89	BE
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	L C D Meter	T010	1 10	25 72	BEG
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	560 ABC VDU (Set 3)	5 60	Jul	081 Tachometer	60
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0	710 2m Power Amp	1 50		Alarm Alarm	60
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		60	Lug	Bongas	7.5
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	(Set 2)	3 15	Sep	Loud Hailer	70
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	(Set 2)	2 20	Oct	Spirit Level	95
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	446 Audio Limiter	1 35	HUV	Rev Monitor	1 10
			Elect	CMOS Switched Pre Amp	1 :0
1977			LIECI	Set 2)	3 80
Jan	570 Reaction Tester	1 60	To-	132 Experimenters P 5	1 00
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	(Set 4)	4 30	Mar	Line Follower	70
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	(Set 2)	1 40		Helping Hand (Set 2)	2 20
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	63D Hex Display	70	Jan	Digital Module A	1 10
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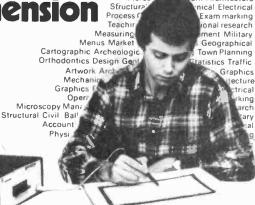
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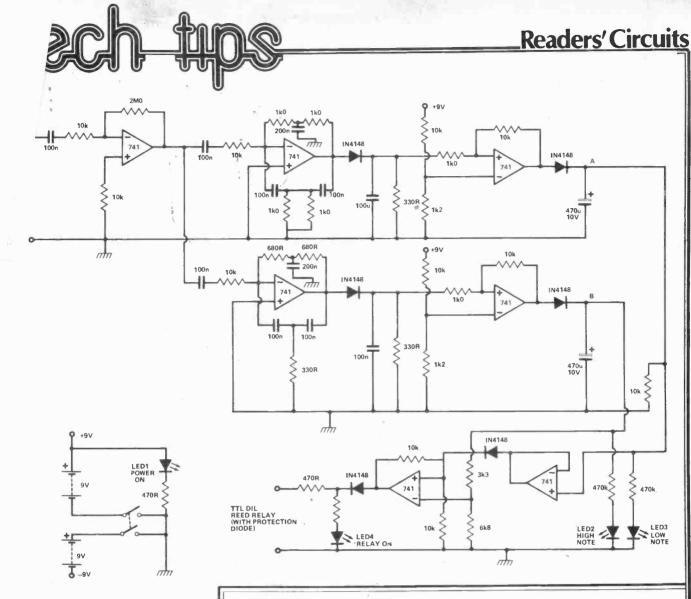
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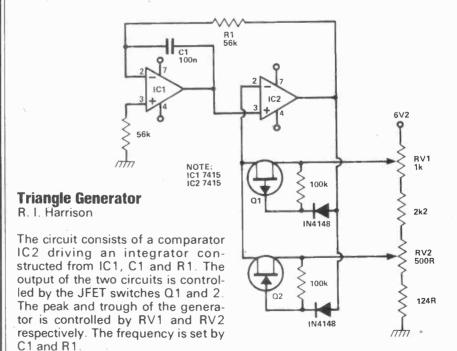


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R. C. W. Gate

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Value		100 /
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.01-,1μ	5р	3.6p
.15	7p	4.8p
.22 µ	9p	6.2p
.33 μ	10p	7.4p
47μ	14p	10.6p
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Value	1-99	100 (
		100+
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.122	5p	3.8p
.33	8р	5.6p
.47	12p	7.3p
.68	15p	9.6p
1.0	20p	13.4p
1.5	26p	18p
2.2	32p	22p
3.3	39p	26p
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25V: 0.47 1 2.2, 3.3, 4.7, 10, 15, 22, 23, 47μ 7p; 100μ 8p; 150μ 10p; 220μ 12p; 330μ 15p; 470μ 19p; 1000μ 26p; 1500μ 31p; 2200μ; 38p; 3300μ 51p; 470μ 60p; 10000μ can 87p; 40V: 47 1μ 7p; 2.2, 4.7, 10, 15, 22μ 8p; 47μ 9p; 100μ 11p; 150μ 13p; 220μ 15p; 330μ 20p; 470μ 24p; 1000μ 34p; 1500μ 45p; 220μ 60p; 470μ 72p, 63V: 1, 2.2μ 8p; 47μ 9p; 10μ 10p; 22μ 11p; 47μ 12p; 100μ 13p; 220μ 18p; 470μ 26p; 1000μ 13p; 220μ 18p; 470μ 26p; 1000μ 51p; 220μ 18p; 470μ 26p; 1000μ 51p; 220μ 78p; 4700μ can 220p. can **220p.** 100+ of any one type, less 25%

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6.8 _µ	35	14p	10 ½ p
10.0 µ	35	14p	11½ p
15μ	20	14p	11 ½ p
22 µ	16	14p	11 ½ p
33 µ	10	14p	11½ p
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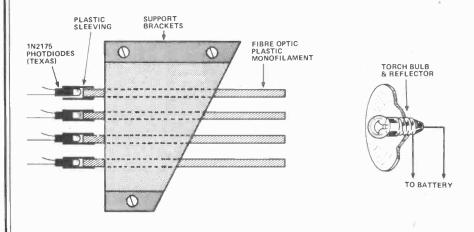
The performance of this unit may be greatly improved by this simple modification. The original circuit assumes that a high level music signal will mask background noise. In reality a high level bass signal will

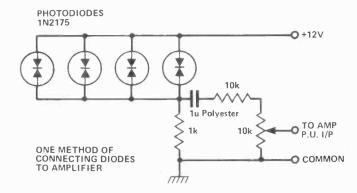
trigger the filter, giving an audible 'whoosh' of noise. This can be alleviated by adding a simple high pass filter to the control circuit. The filter removes signals below 5 kHz, resulting in a cleaner, less breathy, sound. It should be noted that the input impedance of this circuit is only about 3 k and it may be advisable to precede this circuit with an emitter follower.

Upgrading Valve Tuners

R. N. Soar

Older valve tuners often use an ECC85 type valve as the RF amplifier-mixer amplifier. The performance of these tuners can be permanently upgraded by using a solid state replacement such as a Fetron. A typical example is the TS12AT7, a plug in replacement for the ECC81/12AT7 range of valves but the performance is almost the same as the ECC85, only the heater connections are different and this does not apply to solid state. The advantages of replacement are that gain never falls off, thermal drift does not occur and performance is generally better. The only disadvantage is that the Fetrons cost several pounds but can be obtained from East Cornwall Components Ltd.





Fibre Optic Bass Guitar

J. Smith.

This item is in effect a simple musical instrument. It consists of a number of short lengths of plastic monofilament fibre optic material arranged in such a way that when a fibre is touched then released it vibrates at its own natural resonant frequency (like a ruler twanged on the edge of a desk). When in a light beam supplied from a torch battery the vibrating end sends sine wave impulsed along the fibre, at the fixed end there is a photodiode which with suitable circuitry feeds a signal to a normal audio amplifier. The sound produced is similar to that obtained using a tea chest, piece of string and Broom handle, remember those days? Thickness of the fibres and length are not critical and it is best to experiment to obtain the sound that pleases the constructor. The fibres need be no longer than about 60m/m. Remember the shorter they are the higher the note produced.

			LINEAR	
t	T.1	T.IL.	LM709 .20	TRANSIS-
2000		-	LM741 .17	TORS
	.10	74125 .32	LM380 .55	BC107 .08
	.10	74126 .32	LM3900	BC177 .12
	.10	74132 .45	.45	BC182 .09
	.10	74141 .50	NE555 .22	BC212 .09
	.13	74150 .65	NE556 .55	BC547 .09
	.22	74151 .45	NE565 .80	BC548 .09
	.24	74153 .45	NE566 1.15	BC549 .09
	.12	74154 .70	NE567 1.20	BC557 .09
	.12	74156 . 45	142307 1.20	BC558 .09
	.12	74157 . 45	VOLTAGE	BC559 .09
	.15	74161 .55	REGULA-	2N3055
	.15	74163 .55	TORS	.40
	.25	74164 .55	LM340T5	2N3819
	.45	74165 .60	.55	.18
	.12	74166 .75	LM340T12	2N3904
	.20	74175 .60	.35	.08
	.20	74176 .50	LM340T15	2N3906
	.12	74180 .75	.55	.08
	.20	74181 1.25	LM340T18	
	20	74182 .50	.55	
	.20	74190 .70	LM340T24	8
	.12	74191 .70	.55	1
	.60	74192 .55		DIODES
	.38	74193 .60	BRIDGES	1N4001
	.60	74194 .55	(1A)	.04
	.60	74195 .55	W01 100V	1N4148
	.60	74196 .55	.25	.03
	.50	74197 .55	WO4 400V	1N5401
7447	.50			
		74198 1.00	.35	.11
7448	.50	74 198 1.00	.35	
7448 7450	.50 .14	74 198 1.00	.35	
7448 7450 7451	.50 .14 .14	74198 1.00	MICROSETS	
7448 7450 7451 7453	.50 .14 .14 .14	210	MICROSETS	-
7448 7450 7451 7453 7454	.50 .14 .14 .14 .14		MICROSETS	1.00
7448 7450 7451 7453 7454 7460	.50 .14 .14 .14 .14	210	MICROSETS	1.00
7448 7450 7451 7453 7454 7460 7470	.50 .14 .14 .14 .14 .14	210	MICROSETS 22L 14	1.00
7448 7450 7451 7453 7454 7460 7470 7472	.50 .14 .14 .14 .14 .14 .25	210 21° 25°	MICROSETS 22L 14	1.00 8.90 5.25
7448 7450 7451 7453 7454 7460 7470 7472 7473	.50 .14 .14 .14 .14 .14 .25 .21	210 21° 25°	MICROSETS 021 14 13 08	1.00 8.90 5.25
7448 7450 7451 7453 7454 7460 7470 7472 7473 7474	.50 .14 .14 .14 .14 .14 .25 .21 .21	2-10 2-11 2-5 2-70	MICROSETS 021 14 13 08 MICROS etc	1.00 8.90 5.25 7.10
7448 7450 7451 7453 7454 7460 7470 7472 7473 7474 7475	.50 .14 .14 .14 .14 .14 .25 .21 .21 .21	2:10 2:1 2:5 2:70	MICROSETS 02L 4 13 08 MICROS etc 2 450ns	1.00 8.90 5.25 7.10
7448 7450 7451 7453 7454 7460 7470 7472 7473 7473 7474 7475 7476	.50 .14 .14 .14 .14 .14 .25 .21 .21 .25 .25	210 211 25 270 210 808	MICROSETS 02L 14 13 08 MICROS etc 12 450ns 0A	1.00 6.90 5.25 7.10
7448 7450 7451 7453 7454 7460 7470 7472 7473 7474 7475 7476 7480	.50 .14 .14 .14 .14 .14 .25 .21 .21 .21 .25 .25 .40	2:10 2:1: 2:5 2:70 2:10 8:08 8:21	MICROSETS 02L 4 3 08 MICROS etc 2 450ns 0A 2	1.00 8.90 5.25 7.10
7448 7450 7451 7453 7454 7460 7470 7472 7473 7474 7475 7476 7480 7483	.50 .14 .14 .14 .14 .25 .21 .21 .25 .25 .40 .75	210 21° 25° 270 210 808 821 821	MICROSETS 02L 4 13 08 MICROS etc 2 450ns 0A 2	1.00 8.90 5.25 7.10 .95 4.95 1.90
7448 7450 7451 7453 7454 7460 7470 7472 7473 7474 7476 7480 7483 7485	.50 .14 .14 .14 .14 .25 .21 .21 .25 .25 .40 .75 .60	210 211 255 270 210 808 821 821 822	MICROSETS 121. 4 4 13 308 MICROS onc 2 450ns 10A 2 4 4 4	1.00 8.90 8.25 7.10 .95 4.95 1.90 4.90 2.50
7448 7450 7451 7453 7454 7460 7470 7472 7473 7474 7475 7476 7480 7483 7486	.50 .14 .14 .14 .14 .25 .21 .21 .25 .25 .40 .75 .60	210 211 25 270 210 806 821 821 822 822	MICROSETS 121 4 3 3 8 MICROS entr 12 450ns 10A 2 4 4 4 8	1.00 8.90 5.25 7.10 .95 4.95 1.90 4.90 2.50 3.90
7448 7450 7451 7453 7454 7460 7470 7472 7473 7474 7475 7476 7480 7483 7485 7489	.50 .14 .14 .14 .14 .25 .21 .21 .25 .25 .40 .75 .60 .25	21(21) 25 270 210 808 821 821 822 822 822	MICROSETS 121 4 13 18 MICROS etc. 2 450ns 10 24 4 4 4 11	1.00 8.90 6.25 7.10 .95 4.95 1.90 4.90 2.50 3.90 6.50
7448 7450 7451 7453 7454 7460 7470 7472 7473 7474 7475 7476 7480 7483 7485 7489	.50 .14 .14 .14 .14 .25 .21 .21 .25 .25 .40 .75 .60 .25	21(1 21) 25) 270 210 808 821 821 822 825 825	MICROSETS 2L 4 3 3 38 MICROS entre 2 2 4 50 ns 0.0 4 4 4 4 5 5 5	1.00 8.90 6.25 7.10 .95 4.95 1.90 4.90 3.90 8.50 8.50 8.50
7448 7450 7451 7453 7454 7460 7470 7470 7472 7473 7474 7475 7476 7480 7483 7486 7489 7490	.50 .14 .14 .14 .14 .14 .25 .21 .21 .25 .25 .40 .25 .25 .40 .25 .25 .40	21(21; 25; 27(210 808 82; 82; 82; 82; 82, 82, 82, 84,	MICROSETS 21 4 3 8 MICROS etc. 2 450ns 02 4 4 4 8 8 15 5 1013	1.00 8.90 8.25 7.10 .95 4.95 1.90 2.50 3.90 8.50 7.00
7448 7450 7451 7453 7453 7454 7470 7472 7473 7474 7476 7483 7485 7486 7489 7490 7491	.50 .14 .14 .14 .14 .14 .25 .21 .21 .25 .40 .25 .25 .40 .25 .25 .40 .25 .25 .40 .25 .25 .40 .25 .25 .40 .25 .25 .25 .25 .25 .25 .25 .25 .25 .25	21(21; 25; 27(210 808 82; 82; 82; 82; 82, 82, 82, 84,	MICROSETS 22L 4 33 8 MICROS ento 22 450ns 00A 2 4 4 4 4 8 8 15 5 5-1013	1.00 8.90 6.25 7.10 .95 4.95 1.90 4.90 3.90 8.50 8.50 8.50
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5MHz. Input Attenuator — (calibrated) — 9 step 0.1,
0.2, 0.5, 1, 2, 5, 10, 20, 50/div. Input impedance — 1
Meq /40 pf in shunt Input Voltage — Max — 600V P.P.
HORIZONTAL AXIS(X). Deflection Sensitivity —
0,400mV/division. Bandwidth (between 3 dB points —
1Hz-350KHz. Gain Control — Continuous when time
bases in EXT position. Input Impedance — 1 Meg. Input
Voltage — Max — 500V P.P.
TIME BASE. Sweep Range (calibrated) — 100msec/div
to 1µ sec/div in 5 steps. FINE Control — Variable
between steps — includes time-base calibration position. Blanking — Internal — on all ranges.
SYNCHRONISATION. Selection — Internal external.
Synchronisation Level — Continues from positive to
negative.

negative. SUPPLY, Input voltage — 115/200V AC± 10% at 50/60Hz Power Dissipation — 18W. CRT DATA — 4in. — flat face, single beam. — Maximum high voltage — 1.5kV. — Fitted with 8x10

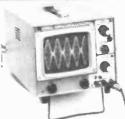
Maximum nigh voltage — 1,5kV. — Fitted with 6x1 U division blue filter graticule.

PHYSICAL DATA Dimensions — 15cm(h)x20.

5cm(w)x28cm(d) Weight — 4.3Kg(approx.) Stand — 2 position filta and inclined Case — Steel, epoxy enamely led. Front panel — Aluminium enamelled epoxy printing (As recommended by ETI)

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Sweep rate continuously adjust-

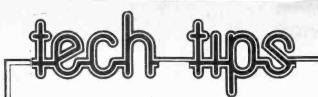
Internal or external AM/FM
400 Hz and 1000 Hz internal modula-

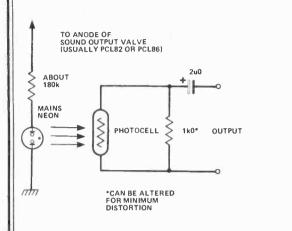
n 0-100% tinuously adjustable

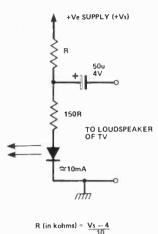
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Television Optoisolator

A. P. Hiley

The problem of how to connect a tape recorder, or amplifier, to a television set is not an easy one to solve, because most televisions, having no mains transformer, have the chassis connected directly to the mains. The easiest, and simplest solution is to incorporate some form of optoisolation between the television and the external equipment. This particular design is simple, has a very low noise level, and introduces negligible distortion.

The LED or neon is brightness modulated by the output of the television sound channel. The light is picked up by a small, cheap silicon photocell, placed a fraction of an inch away. A small current is produced, proportional to light intensity, which produces a PD across the load resistor, which is a replica of the original signal.

Telephone Amplifier

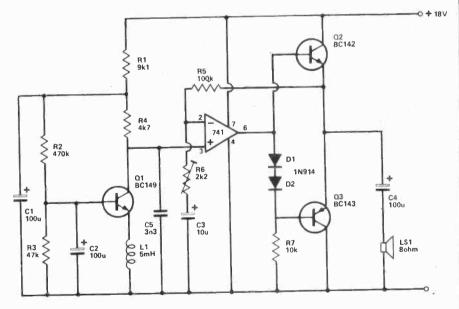
J. P. Macaulay

One of the most frustrating things in life must be to wait in line whilst one's wife converses (nags?) on the phone, What makes the matter worse is that only one side of the conversation is heard. The circuit here will at least enable you to hear what's going on at the other end of the line.

The signals are picked up by the coil L1, a 5 mH RF choke taped to the side of the set. Q1 operates in the common base mode with the output signal appearing across the collector resistor, R4. The output stage consists of two complementary transistors fed from the output of IC1 and included in it's feedback loop.

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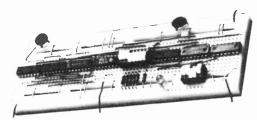
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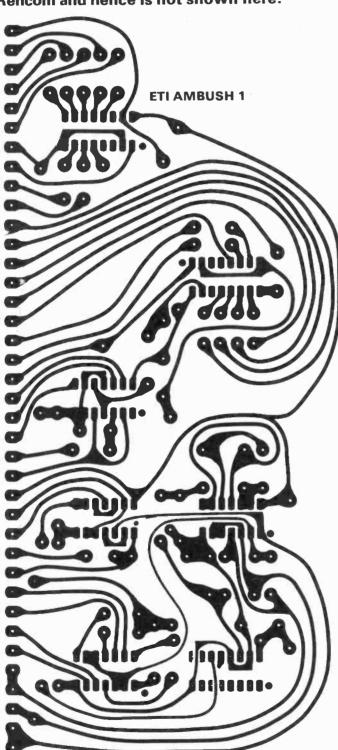
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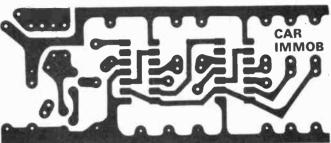
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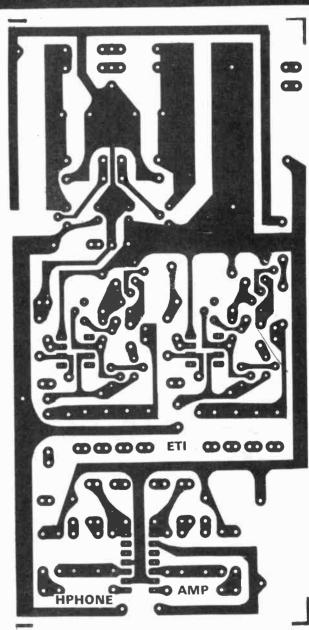
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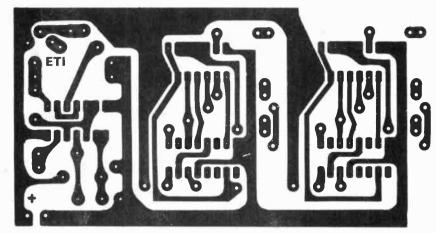
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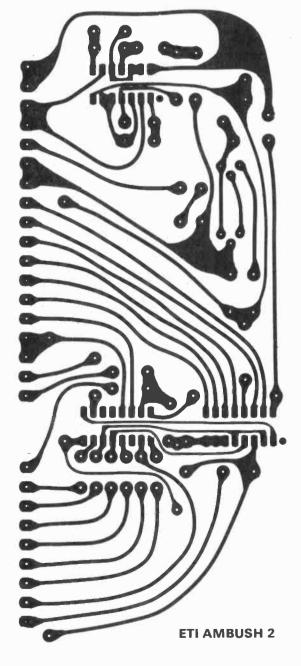
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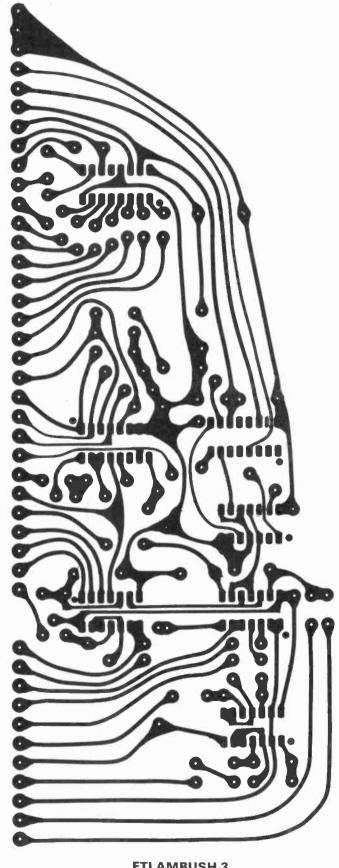












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SPECIFICATIONS:
OUTPUT POWER 15W R.M.S. into 8Q. DISTORTION 0.1% at 15W.
INPUT SENSITIVITY 500mV. FREQUENCY RESPONSE 10Hz-16kHz — 3dB.
SUPPLY VOLTAGE ± 18V.

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HY30

15 Watts into 8Ω

25 Watts into 8Ω

HY120

60 Watts into 8Ω

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SPECIFICATIONS: INPLIT SENSITIVITY 500mV

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FEATURES: Thermal shutdown — Very low distortion — Load line protection — Integral Heatsink —

120 Watts into 80 APPLICATIONS: Hi-Fi — Disco. — Monitor — Power Slave — Industrial — Public address

SPECIFICATIONS:

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OUTPUT POWER 120W RMS into 8\(\text{N}\). LOAD IMPEDANCE 4-16\(\text{Q}\). DISTORTION 0.05% at 100W at

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HY400

240 Watts into 4Ω

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FEATURES: Thermal shutdown — Very low distortion — Load line protection — No external.

APPLICATIONS: Public address - Disco - Power slave - Industrial

SPECIFICATIONS:
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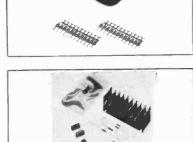
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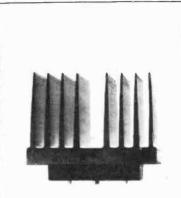
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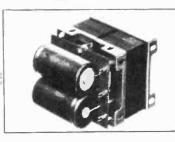
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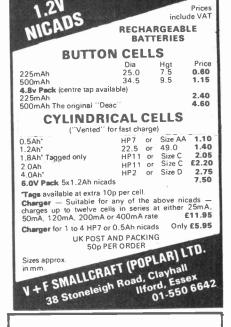
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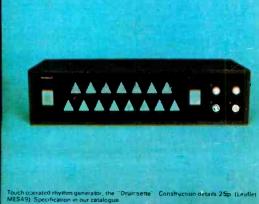












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