MARCH 1979



STAGE LIGHTING CONTROLLER

Cellular Logic * Analogue To Digital

Visual Hi-Fi * Magnetic Amplifiers

NEWS....PROJECTS....MICROPROCESSORS....AUDIO...

CHROMATHEQUE 5000

5 CHANNEL LIGHTING EFFECTS SYSTEM

All kits also available as separate packs (e.g P C.B., component sets, hardware sets, etc.) Prices in FREE CATALOGUE



COMPLETE KIT **ONLY** £49.50 + VAT!

This versatile system featured as a constructional article in ELECTRONICS TODAY INTERNATIONAL has 5 frequency channels with individual level controls on each channel. Control of the lights is comprehensive to say the least. You can run the unit as a straightforward sound-to-light or have it strobe all the lights at a speed dependent upon music level or front panel control or use the internal digital circuitry which produces some superb random and sequencing effects. Each channel handles up to 500W and as the kit is a single board design wiring is minimal and construction very straightforward

Kit includes fully finished metalwork, fibreglass PCB, controls, wire, etc. - Complete right down to the last nut and bolt!

LAST MONTH'S FRONT COVER FEATURE!

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Parts to build power amp module only. (PCB, res, caps, s/cs) Custom designed toroidal transformer with mounting clamp Parts for power supply only (caps, rects, fuses, F. holders)

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Kit includes fully finished metalwork, fibreglass PCB, controls, wire, etc. Complete right down to the last nut and bolt!

TRANSCENDENT 2000 SINGLE BOARD SYNTHESIZER

LIVE PERFORMANCE SYNTHESIZER DESIGNED BY CONSULTANT TIM ORR (FORMERLY SYNTHESIZER DESIGNER FOR EMS LIMITED) AND FEATURED AS A

CONSTRUCTIONAL ARTICLE IN ELECTRONICS TODAY INTERNATIONAL.

The TRANSCENDENT 2000 is a 3 octave instrument transposable 2 octaves up or down giving an effective 7 octave range. There is portamento, pitch bending, a VCO with shape and pitch modulation, a VCF with both low and high pass outputs and a separate dynamic sweep control, a noise generator and an ADSR envelope shaper. There is also a slow oscillator, a new pitch detector, ADSR repeat, sample and hold, and special circuitry with precision components to ensure tuning stability amongst its many features.

The kit includes fully finished metaliwork fully assembled solid teak cabinet, filter sweep pedal, professional quality components (all resistors either 2% metal oxide or 12% metal firml) and it really is complete — right down to the last nut and bolt and last piece of wrier 1 here is even a 13A plug in the kit — you need buy absolutely no more parts before plugging in and making great music! Virtually all the components are on the one professional quality fibreglass PCB printed with component locations. All the controls mount directly on the main board, all connections to the board are made with connector plugs and contrictions is so simple it can be built easily in a few evenings by almost anyone capable of neat soldering! When finished you will possess a synthesizer comparable in performance and quality with ready built units selling for between £500 and £700!

COMPLETE KIT ONLY £172.00 + VAT!

Comprehensive handbook supplied with all complete kits! This fully describes construction and tells you how to set up your synthesizer with nothing more elaborate than a multi-meter and a pair of ears!



Cabinet size 24.6" x 15.7" x 4.8" (rear) 3.4" (front)

ORDERING INFORMATION AND MORE KITS ON PAGE 6

ectronics to



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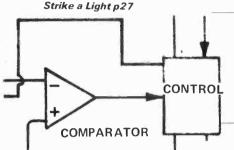
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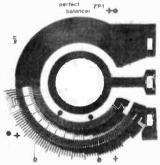
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7405	E0.09	7437	£0.20	7480	£0.40	74121	€0.22	74176	€0.55
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7407	£0.22	7440	£0.10	7482	€0.65	74123	£0.38	74180	€0.80
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Negative No. MVR7905 No. MVR7912 No. MVR7915 No. MVR7918 No. MVR7924	μΑ7905 μΑ7912 μΑ7915 μΑ7918 μΑ7924	TO220 TO220 TO220 TO220 TO220	75p 75p 75p 75p 75p
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		like OA70/81	40p
lo.	16132	100 200mA Sil. diodes like	
		OA200	40p
lo.	16133	150 75mA Sil. Fast switching	
		diodes like IN4148	40p
lo.	16134	50 750mA Sil. top hat Rects.	40p
lo.	16135	20.3 amp Sil. stud Rect.	40p

20 3 amp Sil. stud Rect. 40p 50 400mw Zeners 0.0.7 case 30 NPN Plastic trans. like BC107/8 40p* 30 PNP Plastic trans. like BC177/8 40p* No. 16138

No. 16139 25 NPN trans. like 2N697/ 2N1711 T039 4 No. 16140 25 PNP trans. like 2N2905 T039 No. 16141 30 NPN trans. like 2N706 TO18 No. 16143 30 NPN Plastic trans. like 2N3906

No. 16144 30 PNP Plastic trans. like 2N3905 40p*
30 PNP Germ. trans. like 0C71 40p
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2N3055 80p

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40 MIXED VALUES 1 watt & 2 watt al

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	VC	E	VCB		HFE		
NKT30	1 40	60	30-	00	35p	per	pair
NKT30	2 40	60	50-	100	35 p	per	pair
NKT30	3 20	30	30-	100	25p	per	pair
NKT30	4 20	3.0	E 0	150	25-		:-

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UT46 TIS43

FFT's

2N3819 15p

S99

2N545B 2 AMP. BRIDGE RECTIFIERS

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No. S45	50V (KBS 005)	
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Mixed Pak 2 — 5 Amp. 50-600v. All coded. 4 for £1.00*

	SIMILAR IN 4000 SERIES	
No. S41	25 Like IN4001 (1A 50V)	60
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SPECIAL OFFER! **COMPONENT PAKS**

Order No	Quantity	
16168	5 pieces Assorted Ferrite rods	40p
16169	2 pieces Tuning gangs MW/LW	40p
16170	50 metres Single strand wire	
	assorted wire	40p
16171 16172	10 Reed switches	40p
16172	3 Micro switches	40p
10170	20 Assorted electrolytics	
16177	Trans types 1 pack Assorted Hardware	40p
10177	nuts/bolts, etc	40-
16179	20 Assorted tag strips and panels	40p 40p
16180	15 Assorted control knobs	40p
16184	15 Assorted Fuses 100mA 5 amp	40p
16188	601/2W resistors mixed values	40p
16187	30 metres stranded wire	чор
	assorted colours	40p
STUD	120 ¼ wait resistors Pre-formed	
_	1978 Prod. Our mix	60p*
S101	120 1/2 watt resistors Pre-formed	
S102	1978 Prod. Mixed values	60p
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S103	Range 100 ohms-10 meg	£2.00°
5103	220 ½ watt resistors	
\$104	Range 100 ohms 10 meg 60 Low ohms 1/8 watt resistors	£2.00°
3104	10 100 ohms	
S105	40 Low ohms ½ watt resistors	60p
0.00	10-00hms	60p°
S106	25 Mixed wirewound resistors	60b.
S107	20 Tantalum bead caps	оор
	0 22-100mF Our mix	£1.00°
S108	High-quality electrolytics 10mF-50	0mF
	voltage range 15 50V	
	Our mix 40 for	£1.00°
16204	C280 Pak Contains 50 metal	
	foil caps	£1.00°

POTENTIOMETERS

Slider 40mm TRAVEL

01144	70111111 1 1 1 I	V	
Order N	ow		
16191	6 x 470 Ohm	LIN Single	40p*
S24	6 x 1 K	LIN Single	40p*
S25	6 x 5 K	LIN Single	40p
16193	6 x 22 K	LIN Single	40p
16195	6 x 47 K	LOG Single	40p*
16194	6 x 47 K	LIN Single	40p*
S27	6 x 100 K	LIN Single	40p*
S28	6 x 100 K	LOG Single	40p*
S29	6 x 500 K	LOG Single	40p*
		-	

Slider 60mm TRAVEL

\$30	6 x 2 5 K	LOG Single	4op*
S32	6 x 50 K	LIN Single	40p
S34	4 x 5 K	LOG Dual	40p*
S36	4 x 100 K	LOG Dual	40p
S37	4 x 1 3 MEG	LOG Dual	40p*
S94	6 x 220 K	LIN Single	40p*
S95	6 x 100 K	LOG Single	40p*
S96	6 x 500 K	LIN Single	40p'

S38 Mixed slider pots—various values and sizes, our mix only £1.00° S39 6 x Chrome slider knots 40p°

WIREWOUND

S90 Wirewound Pots Linear 1 Watt rapng Mixed—useful values 5 for

CARBON TYPES

S91 Car Radio type Dual Switched Pot 100 K Lin switched 2 5 K Lin

each 60p*

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S92 4 x 100 K Lin	€1.00
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16173 15 Rotary Pot Assorted	40p
16186 25 Pre-sets Assorted Values	40p
16 186 25 Pre-sets Assorted Values	40p

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No \$55	20 mixed values 400mW Zener diodes 3-10V
No S56	mixed values 400mW Zener diodes 11 33V
No \$57	10 mixed values 1W Zener diodes 3 10V
No \$58	10 mixed values 1W Zener

SILICON POWER TRANS, N.P.N.

S97	BD371 2 Amp 1 2w 60Vceo Hfe 40-400 Case TO92
598	with heat lab — 5 for 2N5293 R C A 36w 4 Amps 75Vceo Hfe 30-120 — 5 for

Crystal Ear Pieces S126 Less plug £0.20

Plugs for al	ove	
No 16106	2.5 plastic	£0.09
No 1697	3 5 plastic	£0.11

Mono Crystal Cartridge

Super Save Pak S124 6×741P S125 5×555

S127 GP91/1SC Special Offer £1 00 Nickel Cadnium Rechargeable Batteries,

1.25v		
S128	3500D Cell size = U2	£2.50
S129	900C Cell size = 1/2 U 1 1	£0.90
	Complete kit of parts to	
bui	d nickel cadnium charger	£3.50
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\$138 Suiplus/End of Manufacturers Line/Pre-amp with Bass, Treble Volume Control & circuit diagram supplied **ONCE ONLY OFFER, £1.25.**

	20 Assorted Slider Knobs — Chrome	£1.00
\$13 \$133 \$133 \$134 \$136	2 2×24v Relays, plastic case 3 1 Switch bank, 5-way incl silver knob 4 2× Magnets suitable for reed switches	£0.70 £0.60 £0.75 £0.10

5130	15 veroboard pak, 2 pcs oosq ins approx
	€1.10
16199	1 Veroboard pak, 30sq ins approx £0.50
16200	15 Veroboard pak 30sq ins approx £0.50

5" wire culters 5" long wire plier	£1.55 £1.45

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STA35 35 watts per channel amplifier kit CONSISTS 2×AL80 — 1×PA100 — 1×SPM120 — 1×2041 transformer — 1 reservoir capacitor — 2×coupling capacitors £48.45 inc. V.A.T.+£1.16 p&p.

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TRANSISTORS

DIODES									
Туре	Price	Туре	Price	Туре	Price	Туре	Price	Type	Price
AA119	5р	BAX16/		BYZ16	30p	OA85	7p	IS44	3р
AAZ13	4p	OA202	5p	BYZ17	28p	OA 90	6р		
BA 100	6р		•	BYZ18	28p	OA 91	7p	IN5400	10p
BA 115	5p	BY 100	15p	BYZ19	28p	OA95	7p	IN5401	11p
BA 144	5p	BY127	'10p	OA47	5p			IN5402	12p
BA148	10p	BYZ10	32p	OA70	5p	IN34	5р	IN5404	13p
BA173	10p	BYZ11	32p	OA79	7p	IN60	6р	IN5406	16p
BAX13/	-	BYZ12	32p	OA81	7p	IN914	4р	IN5407	17p
OA 200	5p	BYZ13	30p		•	IN 148	4р	IN5408	19p

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TBA800	*£0.75	uA709	£0.20	748P	£0.28
TBA810	'£0.85	uA711	£0.25	uA748	£0.28
TBA820	*£0.65	uA703	£0.20	72558	£0.45
LM380	'£0.80	741P	£0.18	MC1310P	£1.25
LM381	'£1.25	72741	£0.20	76115	£1.25
72709	£0.20	uA741C	£0.20	NE555	£0.22
		72747	€0.55	SL414A	£1.80

ZN 414 RADIO CHIP 75' OPTOELECTRONICS

40n

DIS	PLAY	s ·		
			LED Display	£0.70
			LED Display	£1.50
No.	1512	727	Dual LED Display	£1.55

LEC)'s		
No	S120	125 Bright Red	£0.09
No	S121	2 Bright Red	£0.09
No	1502	125 Green	£0.12
No	1505	2 Green	£0.12
No	1503	125 Yellow	£0.12
No	1506	2 Yellow	£0.12
No	S82. CI	lear 2 Huminating	Red
			£0.10

	1506 2 S82. Clea	minating	Red	£0.		
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P.O. RELAYS S85 - 2 Off Post Office relays

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Order Code

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Electrol	ITORS ytic Axi +50% To	al Lea	ds	Order Code Cap 015 + µF	+ V d.c.
μF	V d.c.	16	25	40	63
1.0					8
1.5					В
2,2					8
3.3					8
4.7					В
6.8				8	9
10			7		9
15		7		8	10
22			7		12
33		7		8	
47			7	10	12
68		8			
100			8	12	
150		8	9		29
220		12		24	34
330				28	37
470			21	30	50
680		19	28	36	50
1000		23	28	55	
15 0 0 2200		32	36		

		_		_		_
Tantalum Bead					rder C	
20% Tol.			Ca	ip PR +	µF + 1	Volts
μF V d.c.	3.15	6.3	10	16	25	35
0.1						9
0.15						9
0.22						9
0.33						q
0.47						9
0.68						9
1						9
1.5						10
2.2				9		11
3.3				9	11	14
4.7			l	10	14	15
6.8		9		11	15	.6
10		10	11	14	16	20
15		11	14	15	20	
22	11	14		16		
33		15	16	20		
47		16	20			
68	16	20				

Electroly	tic Can T	ype	Order Code	
High Rior	le. IEC Gra	de 1, Low E.S.R.	Cap HR + µF	+ Volts
Supplied (complète w	ith Vertical Fixing Cti	p	
2200 µF	16∨	Ripple 1A @ 85°C		166
4700 µF	16V	2.6A	3.6A	184
10000 µF	16V	5.8A	8.1A	222
22000 µF	16 V	9.8A	13.7A	346
2200 µF		1.3A	1.8A	175
4700 µF	25V	4.6A	6.4A	201
10000 µF	25V	8.0A	11.2A	264
22000 µF		12.8A	17.9A	438
1000 µF	40 V	0.9A	1.2A	168
2200 µF	40 V	2.4A	3.3A	188
4700 µF	40V	5.6A	7 8 A	231
10000 µF	40V	9,2A	12.8A	367
1000 µF		1.8A	2.5A	190
2200 µF	70 V	4.0A	5 6 A	235
4700 µF	70V	7.5A	10.5A	376
1000 uF		4.0A	5 6A	222
2200 µF		7.8A	10.9A	346

Electrolytic		al Le	ads			ler Co 034 +		/glts
µF ,V d.c.	6.3	10	16	25	35	40	50	63
47								6
68								6
1.0								6
1.5								6
2.2								6
3.3						6		7
6.8				6			7	8
10			6			7		8
15	į		6	7			8	10
22		6	7			8	10	
33			7	8	1.2	10		
47		7	8		10			
68			В	10				
100		8	10					
150 220	10	10						
220	10							1

	47 68 100 150 220	10	7 8 10	8 8 10	10	10	
Ī	Trimmers 250V D.C. Wk-	g. FII	m Dieli		er Co		
	1.4 - 4.1pF 2 8pF 2 - 20pF		19 19 21	Ca Ca	808 q 808 q 808 q	B C	3.

Ceram	ic Pla	te, Rad	ial, Me	d K, +10	pF -8.2p % Tol, 10 0% to +8	00 V D	C. Wk	g					Ci + V	
pF	424	632	630	629	pF	424	632	630	629	nF.	424	632	630	629
1				i i	100	16	6			10	25			6
1.2					120	16	8			12	26			
1.5					150	16	8			15	26			
1.8		5			180	16	6			18	27			
2.2		5			220	16	ô			22	28			8
2.7		5			270	18	8			27	38			
3.3		5			330	18	8			33	41			
3.9		5			390	18		5		39	43			
4.7		5			470	18		5						
5.6		5			560	16		5		1				
6.8		5			680	16		5						
8.2		5			820	16		5						
10		5			1000	16			5					
12		5			1200	16		5						
15		5			1500	18		6						
18		5			1800	18		6						
22		5			2200	18		6	6					
27		5			2700	18		6						
33		5			3300	18		6		1				
39		5			3900	18		6						
47		5			4700	23		7	6					
56		6			5600	23								
68		6			6800									
82		6			8200	23				1				

	Dipped		20% T	ads of, 250V Tol, >100V					
-				Tol, >100\					
	uF	352	360	PHE 280	1	μF	352	360	PHE28
	.001		5	6	-1	1	6	8	9
	.0015		5	6	-	15	7	9	
- 4	0022	5	6	7		.22	8	10	
	.0033	5	6	7		.33	10		
	.0047	5	6	7		.47	12		
	0068	5	6	7	- 1	68	15		

CASES

Small Desk Console - Boss Industrial Mouldings Slope Front Console, Recessed Top ABS Base, C'W Brass'Bushes, In Orange 1mm Aluminium Top Panel Finished Grey





		Order Cod
L112 W62 D31	87	Case BIM2003 C
L150 W80 D50	115	Case BIM2005 C
L190 W110 D60	195	Case BIM2006 C

Instrument Case - Boss Industrial Mouldings Covers Manufactured from 14SWG Aluminium Chassis Manufactured from 18SWG Mild Steel Covers Finished Orange Chassis Finished Matt Black

W250 D167.5 H 68.5 (Chassis 153mm Deep) 1480 Case BIM3000 OF



Order Code

Plastic Boxes with Metal Lids - Boss Industrial Mouldings

Diecast Boxes — Boss Industrial Mouldings Diecast Box and Flanged Lid Aluminium Box and Lid in Natural Flnish

Case BIM5003 NA Case BIM5005 NA Case BIM5006 NA

0.5W, E24 Values, 1M-33M, 5% Tol. 10 ea. 5.40/100 (Mult 10/Value)

Professional Components for the Amateur

500V D.C. Wkg. C004 EA Tubular Type

Small Desk Consoles - Boss Industrial Mouldings Slope Front Console, Recessed Top ABS Base, C/W Brass Bushes, In Orange 1mm Aluminium Top Panel Finished Grey Ventilation Slots In Base

Order Code 206 Case BIM6005 OR 271 Case BIM6006 OR 375 Case BIM6007 OR W170 D143 H32 (56) W170 D214 H32 (82)

All Metal Desk Consoles — Boss Industrial Mouldings Slope Front Console, Recessed Top Two Piece All Aluminium Construction Ventilation Slots In Rear and Base Choice of 15° or 30° Stoping Front Off White Top Panel, Blue Base

Order Code

Eurocard Size Desk Console + Boss Industrial Mouldings

W169 D127 H45 (70)

Res VR37 + Value



ı	HARDWARE		Order Code
	D.I.L. Sockets		
	8 Pin Low Profile Socket Tin 14 Pin Low Profile Socket Tin 16 Pin Low Profile Socket Tin 24 Pin Low Profile Socket Gold 28 Pin Low Profile Socket Gold 40 Pin Low Profile Socket Gold	11 13 14 66 78 127	DIL SKT 8 DIL SKT 14 DIL SKT 16 DIL SKT 24 DIL SKT 28 DIL SKT 40
ı	Heatsinks		
	Individual Type for 1 × T05 50°C/W Individual Type for 1 × T056 10.5°C/W Individual Type for 1 × T056 10.5°C/W Individual Type for 1 × T0126 17°C/W Individual Type for 1 × T0126 17°C/W	10 26 24 23 23	Sink 5F Sink TV2 Sink TV3 Sink TV4 Sink TV5
1	P.C.B. Components		
١	Dato Pen, Blue Ink, Slow Drying Single Sided P.C.B. Pins (040" Diam, 100 pcs Double Sided P.C.B. Pins (040" Diam, 100 pcs	92 55/Pack 55/Pack	Pen 33PC SS Pin 040 DS Pin 040
ı	Fuseholders		
ı	Suit 20mm × 5mm fuses.		i i
	P.C.B. Mounting, Open Type Chassis Mounting, Open Type Panel Mounting, Screwdriver Slot Panel Mounting, Finger Release	8 17 77 56	Fuse/H20B Fuse/H20C Fuse/H20PT Fuse/H20P
ı	Fuses		
ı	20mm x 5mm Glass.		
l	Quick Blow, Range 100mA-5A Slow Blow, Range 250mA-5A	8 22	Fuse 20 A/S Fuse 20
1			Rating
1	Lampholders, Panel Mounting		
ı	Similar in Style to Fuse/H 20P Low Voltage Type Suits LES and M/F Bulbs.		
	Low Voltage, Red, Amber or Green Internal Neon 200/240V Red or Amber	75 95	Lamp LV Lamp N
1			· Cotour
1	Bulbs, Low Voltage, L.E.S.		
	6V, 0.36W; 5.5V, 1W; 14V, 0.75W.	22	Bulb LES + Voltage

				THE REAL PROPERTY AND ADDRESS OF THE PARTY O	
RESISTORS Carbon Film, Fixed				Order Code	Skeleton Presets, Miniature 0.1W, E3 Values, 100R-IM, Lin. Vertical Mour
0.25W, E24 Values IRO-10M, 5% Tol.	1:5 ea.	90p/100 (Mult 10/Value)	£7.90/1000 (Mult 100/Value)	Res RD%	0.1W, E3 Values, 100R-IM, Lin. Horizontal Me
0.5W, E12 Values IRO-4M7, 10% Tol.	2 ea.	1.25p/100 (Mult 10/Value)	£10.10/1000 [Mult 100/Value]	Res RD%	Skeleton Presets, Standard
Metal Film, Fixed					0.3W, E3 Values, 100R-4M7, Lin. Vertical Mo-
0.5W, E24 Values, SRI-IM, 2% Tol.	6 ea	3.80/100 (Mult 10/Value)	E32.40/1000 (Mult 100/Value)	Res MR30 Res PR52	0.3W, E3 Values, 100R-4M7, Lin. Horizontal I
2.5W, E12 Values 10R-27K, 5% Tol.	13 ea.	7.90/100 (Mult 10/Value)		+ Value	Potentiometer, Rotary
Metal Glaze, Fixed					0,5W, E3 Values, 1K-2M2 Lin.
0 EW E24 Values 1M-33M 5% Tol	10 ea	5.40/100 (Mult 10/Value)		Res VR37	0.25W, E3 Values, 4K7-2M2 Log.

Order Code

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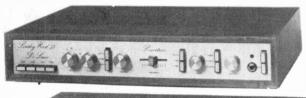
CA3011 92 NE592K 162 Light Emitting Diodes, Individual Miniature Toggle — Honeywell CA3018 75 RC4136 130 .125" (3mm) Red 14 CQY54 SPDT 2A/250V A.C., 5A/28V D.C. 58 SW8 CA3020 191 TBA1205 79 Green 17 CQY95 SPDT C/OH 67 SW8	104 104 107
HFF4000 14 HFF4073 87 HFF4015 89 NF4015 9	104 104 107
NEFADO 14	104 104 107
HEF400B 80 HF54052 72 HEF4519 55 N,7405N 12 NJ745N 13 NJ7413N 46 NJ7427N 160 NJ741539N 24 NJ741518N 80 NJ74152N 16 HF54011 14 HEF4053 72 HEF4521 188 N,7405N 27 NJ745N 13 NJ7414N 150 NJ74154N 150 NJ74154N 54 NJ74154N 17 NJ7415N 12 NJ7415N 12 NJ7415N 150 NJ7415N 12 NJ7415N 150 NJ7415N 12 NJ7415N 150 NJ7415N 12 NJ7415N 150 NJ7415N 12 NJ7415N 12 NJ7415N 150 NJ7415N 12 NJ7415N 150 NJ7415N 170	N 40 40 13
HEFA013 32 HEFA068 14 HEFA528 99 N7A08N 13 N7A58N 13 N7A56N 150 N7ALSSIN 22 N7ALSIGNN 120 N7ALSSIN 78 N7ALSSIN 178 N7AS6N 150 N7ALSSIN 22 N7AS6N 150 N7ALSSIN 178 N7ALSSIN 178 N7AS6N 150 N7ALSSIN 178 N7AS6N 150 N7ALSSIN 178 N7ALSSIN 178 N7AS6N 150 N7ALSSIN 178 N7ALSSIN 178 N7ALSSIN 178 N7ALSSIN 178 N7AS6N 150 N7ALSSIN 178 N7ALSSIN 17	IN 100 IN 100 IN 170 IN 170 IN 105 IN 150 IN 150 IN 150 IN 150 IN 170 IN 170 IN 170 IN 170 IN 180 IN 130 IN 150 IN
HEF4017 55 HEF4018 14 HEF4633 155 N7412N 17 N742N 23 N74158N 58 N74158N 58 N74158N 100 N74158N 58 N74158N 100 N741	N 108 N 108 N 108 N 108 N 150
REFAURD N. REFA	N 108 N 150 N 150 N 160 N 160 N 160 N 170 N 170 N 170
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PSI 4002 STUDIO MODEL



cabinet size 17.2" x 17.2" x 6.7'

COMPLETE KIT ONLY £196.90 + VAT **READ THE REVIEW** IN SOUND INTERNATIONAL DEC. '78







T20 + 20 20W STEREO AMPLIFIER £33.10 + VAT

This kit, based upon a design published in Practical Wireless, uses a single printed circuit board and offers at very low cost, ease of construction and all the normal facilities found on quality amplifiers. A 30 watt version of this kit (T30 \pm 30) is also available for £38.40 \pm VAT.

POWERTRAN SFMT TUNER £35.90 + VAT

This is a simple low cost design which can be constructed easily without special alignment This is a simple low cost design which can be constructed easily without special alignment equipment but which still gives a first-class output suitable for feeding any of our very popular amplifiers or any other high quality audio equipment. A phase-locked-loop is used for stereo decoding and controls include switchable afc, switchable muting and push-button channel selection (adjustable by controls on the front panel) This unit matches well with the T20 + 20 and T30 + 30 amplifiers

WWII TUNER £47.70 + VAT

This cost reduced model of our highly successful Wireless World FM Tuner kit was designed to complement the T20 + 20 and T30 + 30 amplifiers and the cabinet size, front panel format and electrical characteristics make this tuner compatible with either. Facilities included are pre-aligned front-end module, switchable afc, adjustable switchable muting, ED tuning indication and both continuous and push-button channel selection (adjustable by controls on the front panel).

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- * Professional quality components, sturdy 19 rack mounting chassis complete with sleeve and feet for free standing work too
- Easy to build plenty of working space with ready access to all components, minimal wiring, extensive instruction suitable for both experience constructors and newcomers to electronics.
- Value for money quality and performance comparable with ready-built amplifiers costing over £600!

DE LUXE EASY TO BUILD LINSLEY HOOD 75W STEREO AMPLIFIER £99.30 + VAT

This easy to build version of our world-wide acclaimed 75W amplifier kit based upon circuit boards interconnected with gold plated contacts resulting in minimal wiring and construction delightfully straightforward. The design was published in Hi-Fi News and Record Review and features include rumble filter, variable scratch filter versatile tone controls and tape monitoring whilst distortion is less than 0.01%

WIRELESS WORLD FM TUNER £70.20 + VAT

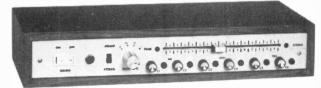
A pre-aligned front-end module makes this Wireless World published design very simple to construct and adjust without special instruments. Features include an excellent a military push-button station selection as well as infinitely variable tuning and a phase locked loop stereo decoder incorporating active filters for "birdy" suppression

LINSLEY-HOOD CASSETTE DECK £79.60 + VAT

This design, published in Wireless World, although straightforward and relatively low cost provides a very high standard of performance. There are separate record and replay amplifiers and switchable equalisation together with a choice of bias levels are also provided. The mechanism is the Goldring-Lenco CRV with electronic speed control.







COMPLETE KITS: Our complete kits really are complete. All of the projects shown on this page-are supplied with fully finished metalwork, ready assembled high quality teak veneer cabinet, cables, nuts, bolts, etc., and full instructions — in fact everything!

All of the kits shown on this page are available as separate packs (except the Powertran SFMT Tuner) for those customers who wish to spread their purchase or perhaps make their own cabinets or metalwork. Prices are given in our FREE CATALOGUE.

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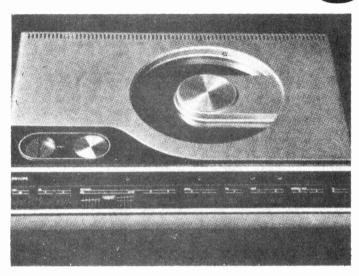
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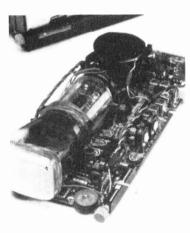
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news digest.....



VIDEO DISC REVISITED

It looks like the video disc is rearing its domestic head again. Philips have introduced a 60 minutes per side system, release and price for UK market have yet to be announced, but be prepared for yet another compatability war as other manufacturers join the fray.



SINCLAIR ANNOUNCE UK MICROVISION

A 'UK only standard' version of the top selling Microvision has been developed by Sinclair Radionics. Outwardly it has the same dimensions as the International version, but fewer controls. Good news for bank managers too, it costs less than half the previous version at less than £100. Further details from Sinclair Radionics, London Road, St Ives, Huntingdon, Cambs. PE17 4HJ.

STRIKE A BLOW

We are reliably informed that due to the industrial action within the transport industry, copies of ETI have not reached some areas for last month's (February) issue. We apologise to our readers for this and hop you'll bear with us through the trouble.

Owing to the continuing — as we go to press — troubles, this issue too may be delayed. In some cases this may well be severe. If you read this later than you would normally have done so — thank you for sticking it out, and we promise normal service will be resumed as soon as possible.

Ron Harris Editor

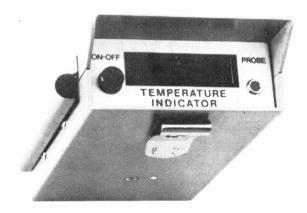
HAND-HELD GAMES



After the inroads made into the leisure market by TV video games, a new generation of hand-held calculator-style games seem to be making their way across the Atlantic. The 'AMAZE-A-TRON' (groan) is a micro-based game specifically aimed at the 5 years and up age range. It is basically a maze game

with a claimed one million variations. Also in the pipeline are 'ZAP' a missile game, 'DIGITS' a code game, and 'LIL GENIUS', a teaching type calculator. Prices will range from £9-£18 and will be marketed by Spectrum Electronic Games, 113-115 Gloucester Road, London SW7 4TE.

HOT STUFF



Details of a new pocket-sized thermometer, 'computerised' no less, have just arrived. Designated the ITS there are four models in the range, two cover the range 0-110°C and the other two from -35°C to 149°C. The LED display can handle Fahrenheit as well as Centigrade. More

than 25 interchangeable probes are available for various applications, and its rugged high impact aluminium case is ideal for field use. Contact British Rototherm Co Ltd for further details at Kenfig Industrial Estate, Margam, Port Talbot, West Glam. SA13 2PW (South Wales).

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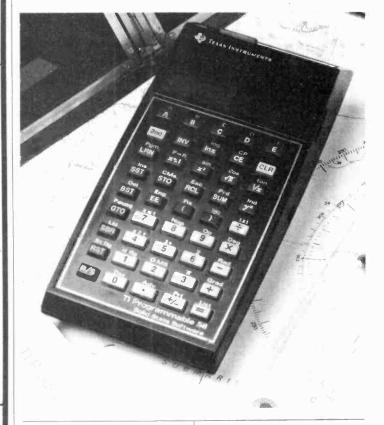
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51	management, Cursor manage-	
55	ment on screen, Line erasing	
298	Compatible with any computing	
99	system.	
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98	SF F96364E £11.75*	
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99	(Send 30p stamps for full tech-	Ľ
165	nical data)	g
85		۲

news digest

LOST AND FOUND AT SEA DEPARTMENT

An interesting variation on the programmable calculator has sailed into our offices, Texas Instruments have introduced a TI58, complete with brass handled, mahogany case and adaptor/charger. Software in-

a 30 cludes programme navigational package. It will tell you just about everything from where you are, to how fast you'll be going somewhere else. Want to know more, then contact: Texas Instruments Limited, European Consumer Division, Manton Lane, Bedford MK41



ELECTRONIC SUMMER SCHOOL

The Department of Electrical Engineering Science at the University of Essex will be holding its annual electronics summer school for teachers during the week 9th-13th July, 1979. This year, as well as courses in linear circuit design and digital circuit design, a third course in electronic systems is also available which is closely related to the A.E.B. electronics systems Alevel. Further information on the Summer School may be obtained from The Department of Electrical Engineering Science, University of Essex, Wivenhoe Park, Colchester CO4 3SQ.

ORIENTAL TELETEXT

Sony are to launch a Teletext equipped receiver with infra red remote control. This is the first eastern set in a virtually all-European market. Costing about £800, it is likely to give the home TV industry some added headaches. The sets are to be built at the Bridgend factory.

CATALOGUE CORNER

This month's releases include the 1979 Marshalls catalogue, usual comprehensive assortment of components and hardware. Interesting to see they deal in KIM and PET, all in all not bad for value for your 40p.

77Ls by TEXAS 7400 13p 7401 14p 7402 14p 7403 14p 7404 17p 74S04 90p	74190 74191 74192 74193	700p 100p 100p 100p 100p 100p 95p	74LS390 160p 74LS393 160p 4000 SERIES 4000 15p	93 SERIES 9301 9302 9308 9310 9311 9312	160p 175p 316p 275p 275p 160p	2 ½ × 3 ¼ 41 2 ½ × 5 49 3 ¾ × 3 ¾ 49 3 ¾ × 5 56 2 ½ × 1 7 152	9 33p 9 45p 9 45p 9 60p 9 121p	TRANSISTORS AC126 25p AC127/8 20p AC176 25p AC287 8 25p AF116/7 30p AD149 70p	BFW10 90p 8FY50 22p BFY51/2 22p BFY56 33p BFY90 90p BLY83 700p 8RY39 45p	TIP2955 78p TIP3055 70p TIS43 34p TIS93 30p ZTX108 12p ZTX300 13p ZTX500 15p	2N3905/6 20p 2N4036 65p 2N4058/9 12p 2N4060 12p 2N4061/2	010DES '8Y127 12p 'OA47 9p 'OA81 15p 'OA85 15p 'OA90 9p 'OA91 9p	*ZENERS 2 7V-33V 400mW 9 1W 15
7405 18p, 7406 32p, 7407 32p, 7408 19p, 7409 19p, 7410 15p, 7411 24p, 7412 20p, 7413 30p, 7416 27p, 7420 17p, 7420 17p, 7421 40p, 7422 22p, 7423 30p, 7425 30p, 7425 40p	74199 74200 74221 74251 74259 74265 74278 74278 74283 74284 74284 74285 74290 74293 74294	95p 80p 150p 150p 150p 250p 90p 250p 90p 290p 140p 140p 150p 400p 150p 150p	4001 17p 4006 95p 4008 95p 4008 95p 4008 90p 4009 40p 4010 17p 4011 17p 4011 17p 4011 18p 4013 50p 4014 84p 4015 84p 4016 45p 4016 45p 4017 80p 4018 80p 4019 4019 4019 4019 4019 4021 100p	9314 9316 9321 9322 9334 9368 9370 9374 LINEAR ICs 'AV1-0212 'AV1-1313 'AV1-1320 'AV1-5050 'AV5-1317 'AV5-1317 'CA3019	225p 4 225p 5 150p 9 225p 6 200p 1 200p 1	P4 x 17 252 Pkt of 35 pins Spot face cutter Pin insertion tool VERO WIRING PI Plus Spool Spare spool (wire)	30p 85p 99p	AD161/2 45p 8C107 8 11p 8C109 11p 8C109 11p 8C117 20p 8C147/8 9p 8C149 10p 8C157/8 10p 8C157/8 10p 8C157/8 17p 8C172 12p 8C177 8 17p 8C172 12p 8C177 8 17p 8C182/3 10p 8C182/3 10p 8C182/3 10p 8C182/3 11p 8C1817 30p 8C212/3 11p 8C212/3 11p 8C212/3 11p	BSX19-2020/p BU104 225p BU105 190p BU109 225p BU109 225p BU208 200p BU208 200p BU406 145p MJ481 120p MJ2501 225p MJ2955 100p MJ3001 225p MJ2955 100p MJ3001 225p MJ2955 100p MJ3005 70p MJ2505 25p MJ2955 45p	'2TX502 18p 2TX503 30p 2N457A 250p 2N696 35p 2N699 25p 2N699 25p 2N706A 20p 2N706A 20p 2N918 45p 2N708A 20p 2N918 25p 2N930 18p 2N1131 2 20p 2N1131 25p 2N2102 60p 2N2103 300p 2N2219A 22p 2N2219A 22p 2N22219A 22p	18p 2N4123 4 22p 2N4125 6 2N4289 22p 2N4289 20p 2N4401 3 27p 2N4401 3 2N5089 27p 2N5087 27p 2N5179 90p 2N5179 90p 2N5191 83p 2N5194 90p 2N5245 40p 2N5245 40p	**OA95** OA90** OA200** OA200*	TRIACS PLASTIC 3A 400V 60) 3A 500V 66, 6A 400V 70, 6A 500V 88, 8A 400V 75, 8A 500V 95, 12A 400V 100, 16A 500V 130, T2800D 130,
7427 34p 7428 36p 7430 30p 7432 30p 7433 40p 7437 35p 7438 17p 7440 17p 7441 70p	74365 74366 74367 74368 74390 74393	200p 150p 150p 120p 150p 200p 200p 225p	4022 100p 4023 22p 4024 50p 4025 20p 4026 130p 4027 50p 4028 84p 4029 100p 4030 55p	*CA3046 *CA3048 CA3080E CA3086 *CA3089E *CA3090AQ CA3130E CA3140E CA3160E	70p 225p 72p 48p 225p 375p 100p 70p 100p	NE565 NE566 NE567 NE571 'SAD1024A SFF96364 'SN 76003N 'SN 76013N 'SN 76018	130p 155p 175p 425p £15 1150p 175p 140p 140p	BC477/8 30p BC516/7 50p BC5478 16p BC549C 16p BC549C 18p BC5578 16p BC5578 16p BC559C 18p BC770 18p BCY70 18p	**MPF103 4** **MPF105 40p** MPSA06 30p** MPSA06 32p** MPSU06 63p** MPSU06 63p** MPSU06 78p** 0C28 130p** 0C35 130p**	2N2369A 16p 2N2484 30p 2N2646 50p 2N2904/5 2N2906A 24p 2N2907A 30p 2N2926 9p 2N3053 22p 2N3053 65p	2N5401 50p 2N5457 8 40p 2N5459 40p 2N5460 40p 2N5465 44p 2N6027 48p 2N6247 190p 2N6254 130p 2N6254 130p 2N6290 65p	HEAT SINKS For TO 220 Voltage Regs and Transistors 22p For TO 5 12p	THYRISTORS 1A 50V 40 1A 400V 85 1A 600V 70 3A 400V 90 8A 600V 140
744/2A	74LS SERI 74LS00 74LS02 74LS04 74LS05 74LS08 74LS10 74LS11 74LS13 74LS14 74LS20 74LS21 74LS21	14p 14p 16p 25p 22p 20p 40p 45p 90p 20p 40p 28p	4031 200p 4033 180p 4034 200p 4035 110p 4040 100p 4041 80p 4042 80p 4044 90p 4046 110p 4047 100p 4048 55p 4049 32p 4050 49p 4051 80p	CA3161E CA3162E FX209 ICL7106 ICL8038 LF356P LF358P LM301A LM311 LM318 LM324 LM324 LM339 LM348 LM377 LM377 LM377 LM380 LM380	120p 420p 750p 850p 340p 95p 75p 30p 120b 200p 75p 95p 175p 95p 175p	'SN 76013ND 'SN 76023N 'SN 76023N 'SN 76023N 'SN 76023N 'SN 76477 'SN 76477 'SP 8515 'TAA621 'TBA641811 'TBA651 'TBA800 'TBA810 'TDA1004 'TDA1008	120p 140p 120p 110p 175p 250p 275p 225p 200p 90p 100p 90p 175p 300p 320p	BC131/2 50p BC135/6 54p BC139 56p BC140 60p BC140 60p BC242 70p BF200 32p BF200 32p BF258 70p BF258 70p BF257/8 32p BF259 36p BFR39 30p BFR41 30p BFR41 30p	R20088 200p TIP29A 40p TIP29C 55p TIP30C 60p TIP31C 62p TIP31C 62p TIP31C 62p TIP32A 68p TIP33A 68p TIP33A 68p TIP33A 61p TIP33A 61p TIP33A 61p TIP34A 61p TIP34A 61p TIP34A 62p TIP33C 62p TIP35C 72p TIP	2N3055 48p 2N3442 140p 2N3553 240p 2N3565 30p 2N3663 44 2N3702/3 12p 2N3704 5 12p 2N3706 7 14p 2N3708 7 2N3708 7 2N3708 7 2N3708 7 2N3708 7 300p	2N6292 65p. 3N128 120p. 3N144 100p. 3N201 110p. 40290 250p. 40360 40p. 40361/2 45p. 40408 70p. 40409 65p. 40411 300p. 40595 97p.	8RIDGE RECTIFIERS 11A 50V 21p 11A 100V 22p 11A 400V 30p 11A 600V 35p 22A 100V 35p 22A 100V 35p 32A 200V 60p 33A 200V 60p 44A 100V 95p 44A 400V 100p	12A 400V 160 16A 100V 160 16A 400V 180 16A 600V 220 8T106 110 C1060 45 MCR101 36 2N3525 130 2N4444 140 2N5060 34
7475 36p 7476 35p 7480 50p 7481 100p 7482 84p 7483A 90p 7484 100p 7485 110p	74LS27 74LS30 74LS32 74LS42 74LS47 74LS55 74LS72 74LS73	38p 22p 27p 95p 90p 30p 00p 50p	4053 80p 4054 150p 4055 125p 4056 135p 4059 600p 4060 115p 4063 120p 4066 55p	LM389N LM709 LM710 LM725 LM733 LM741 LM747 LM748	140p 36p 50p 350p 100p 20p 70p 35p	TDA1022 TDA2020 TL084 TL170 ULN2003 XR2206 XR2207 XR2211	600p 320p 130p 50p 100p 350p 400p 600p	BFR80 30p BFR81 30p BFX29 30p BFX30 34p BFX84/5 30p BFX86 7 30p BFX88 30p	TIP35C 290p TIP36A 270p TIP36C 340p TIP41A 65p TIP41C 78p TIP42A 70p TIP42C 82p	'2N3819 25p '2N3820 50p 2N3823 70p 2N3866 90p '2N3903/4 18p	40673 75p 40841 90p 40871/2 90p	6A 50V 90p 6A 100V 100p 6A 400V 120p 10A 400V 200p 25A 400V 400p	**COUDSPEAKER 2½ 64R 70; 2½ 8R 70; 2 8R 75; 1½ 8R 75;
7486 34p 7489 210p 7490A 33p 7491 80p 7492A 48p 7492A 48p 7495A 70p 7495A 70p 7497 180p	74LS74 74LS75 74LS83 74LS85 74LS86 74LS90 74LS92 74LS93 74LS107	40p 45p 90p 100p 40p 60p 72p 60p 45p 100p 75n	4067 450p 4068 22p 4069 20p 4070 30p 4071 22p 4072 22p 4073 22p 4075 22p 4076 107p 4081 22p 4082 22p	LM3900 LM3911 LM4136 "MC1310P MC1458 MC1495L 'MC1496 'MC3340P 'MC3360P 'MFC4000B	70p 130p 120p 150p 55p 350p 100p 120p 120p 120p	XR2216 XR2240 'ZN414 ZN424E ZN425E ZN1034E 95H90 IIC90	675p 400p 90p 135p 400p 200p 800p £14	MEMORIES 2102-2 2102-1-4 2107-8 2111-1 2112-2 2114 5101 6810 ROM/PROMe	120p 140p 500p 225p 300p 700p 510p 350p	UART AY-3-1015P AY-5-1013P TMS6011NC CHARACTEF GENERATOF 3257ADC MCM6576 RO-3-2513U RO-3-2513U	995p 750p C 600p 550p		
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74147 180p 74148 150p 74510 100p 74151A 70p 74153 70p	74LS190 74LS191	320p 100p 100p 140p	40085 200 p 40097 90 p 14411 £11 14412V £11 14433 £11	OPTO-ELECT 2N5777 ORP12 ORP61	RONICS 45p 90p 90p	OCP71 ORP60 TIL78	130p 90p 70p	8 pin 11p 14 pin 12p 16 pin 13p	18 pin 21 20 pin 21 22 pin 30	51p 24-pm 3 81p 28-pm 4	WIRE \ 8 pin 12p 14 pin 16 pin	40p 20 pm 7	55p 24 pin 86 70p 28 pin 100 75p 40 pin 120
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74170 240p 74172 720p 74173 120p 74174 93p	74LS258 74LS259 74LS266 74LS273	250p 160p 50p 130p 140p	75451 72p 75491/2 96p 8726 250p 8728 300p 8795 160p	747 Gr FND357	225p 225p 120p VERS 93	TIL321/2 TIL330 7750/60 368/9370 200 ₁	130p 140p 200p	Data Books on LINEARS, MEM SISTORS ETC. A	ORIES, TRAN-	Trouble-s	hooting ser	vices availabl rchased from	e for kits or us
74175 85p 74176 90p 74177 90p 74178 160p 74180 93p 74181 200p 74182 90p 74184A 150p 74185 150p	74LS298 74LS324 74LS365 74LS367	249p 200p 160p 160p 160p 180p 180p	8T97 160p 81LS95 120p 81LS96 140p 81LS97 140p 81LS98 140p 9601 100p 9602 220p 9603 60p	6-0-6 9-0-9 12-0-12 0-12 0-12	100i 75i 100i 500	mA 92p mA 95p)mA 280p+ arge to all items ma		. 2A 0 1A 1A bove our normal p&p	270p+ 350p+ 340p+ 265p+ charge)	SFF	PCB £6.00 96364 £11 of "Practic	now on at ou + VAT + P8 1.50 + VAT - cal Electronic t 75p + S.A.	P• ' + P&P :s'' articles
*RESISTORS Senes 1/4W 10R-1M ½w 10R-10M *MINIATURE 100R-1M *CARBON TR. 1/4 LOG or LIN Single Single with DP Dual	1 1p 80p / 10 1 5p 120p / PRESETS H ACK POTER	00 (one 100 (o Horz /V	ne value) ert 1 IETERS 5K-2M 2 5K-2M 5	\$0L IROI Modi CX 1 X25 CCN	DERING NS el C 15W 7W	360p 360p 360p 360p (With 10r) Conn	16 pin Dit oard 4 5 tracks fo ector Plug ector Soci loard for	14 5 x 6 15 270p 1x 14 pin or 1Cs) x 6 15 340p r 31 way connec-	implement a and a minim weighing e replacemen power-supp	onverter with BCI a 2-chip 3-digit re num of external p equipment, med t for analog par	D-to-seven segreadout system (arts Ideally sur dical diagnosti nel meters ten	READOUT SYS' ment decoder driv that features simp ted for wide range tic equipment, w inperature measu utomotive accesso	er can be used to dicity of operation of uses including relding controls ring instruments
			at 8% exceptere 12½9	6		ip p&p & VA	T at a	ppropriate ra	17 B	urniey Road	, London N		
Please sen	d SAE f	or lis	st	CALLE	RS WE	LCOME		Mon -Fri 9 30-5 30 Saturday 10 30-4 30) 	nutes Dollis I 01-452 150		tion) (ample s	treet parking iex: 92280

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T03 HEAT SINKS!!! Two types of heat sink. Ex-equipment, but condition as new Most still contain a power transistor (condition unknown). 'Christmas tree type, 92×66×35mm 20p each. Rectangular type 130×63×32mm 30p each. Please add 25p per heat sink post and packing.

PACK M1. Contains two brand new multifunction calculator keyboards. Excellent

key action Only £1.00.

key action Only £1.00.

PACK T2. A high contrast 3½ digit Liquid Crystal wristwatch display with data Don't miss out — only £1.00.

PACK T4. At a new low price, what a bargain A 0 8" common cathode, 3½ digit. 12-hour clock display Now offered at only £3.95.

PACK S1. 25 miniature glass 1N3470 germanium diodes (600mA 35v) All brand new (at just 2p each how can you go wrong?) 25 diodes for 50p.

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PACK \$3. 10 x 1N4151 high-speed switching diodes. Same as 1N4148, but has higher P.I.V. 10 for 35p.

PACK P1. With this MM5330 digital voltmeter I C. we include the data sheet and circuit diagram to build a high accuracy digital multimeter. Only £3.95.

PACK E2. Calculator style L C. D. 8 digit with right-hand decimal points. Digit height 0.33". With data only £2.95.

PACK E3. The same as Pack E2, but has 0.5" high digits. £4.25.

EVER THOUGHT of using 7 segment gas discharge displays as an alternative to LED's or LCD's? Gives a nice bright orange display and are comparatively very low in price. Requires. 180v. d.c. supply (easily achieved in mains-operated projects). All have right-hand decimal points and are supplied with data.

PACK E4. 0.3" high 1½ digit display. Now only 50p.

PACK E5. A. 0.3" high dual digit display. Now only 50p.

PACK E7. A. 0.25" high 12 digit display with free socket. £1.50.

PACK DM1. Want to buy 115 quality switching diodes for 50p? These 14 pin chips each contain 23 matrixed diodes. 5 chips for 50p.

PACK M4 CALCULATORS!!! This pack contains a production line reject calculator Either repair them (not much wrong with some of them) or strip them for spares. Lots of accessible goodies inside, approximately 25 transistors, 2 chips display case and detachable keyboard. Such is bargain, you can't go wrong. Only £2.50.

PACK MU1 (untested — so no guarantees). 2 × Upper half of hand held calculator case with integral keyboard. Ex-equipment, but believed to be 0. K. A gift at only 50p the pair.

the pair PACK DL1 (untested — so no guarantees). A bumper pack of 30 mixed I C $_{\rm S}$. You test them and save £££'s. Could include anything linear or digital. A snip at only

E1.UU.

PACK E1 (80% guaranteed good) Contains 5 seven segment LED displays Digit height 0.127" with right-hand decimal Common cathode Still only £1.00. Your satisfaction is guaranteed or return the complete pack for replacement or a return

For free catalogue send stamped addressed envelope Postage and packing please add 25p (overseas orders add 60p)

CODESPEED, P.O. Box 23, 34 Seafield Road, Copnor, Portsmouth, Hants,



news



This is apparently same sort of aircraft navigation aid, but secret sources indicate it is in fact the British Home Stores Lampshade farm.

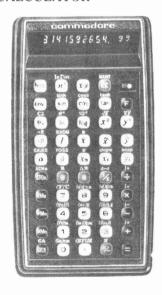
LCD POCKET TV

Matsushita have developed a pocket TV with better resolution than any previous LCD type. 57,600 elements are arranged in a 240x240 matrix which measures 2.4 inches (presumably diagonally). But even though CMOS circuits are used the TV consumes 1.5 W

BBC TV TRANSMITTER OPENS AT LOCH NESS

We couldn't resist this one, the transmitter is sited at Wester Erchlite, opposite Urquhart Bay. We hear the installation is O.K. so far, but they have had a few teething troubles with programmes like 'All Creatures Great and Small,' something to do with frequency loch.

LANDLUBBER'S **CALCULATOR**



For those of us who are landbased, and taking O/A or degree level studies, Commodore have introduced an updated version of their successful 419OR, designated the SR919OR. It has nine memories with over 100 scientific functions at only £30. It has all the usual features, 10 + 2LED display, rechargeable batteries and a l year guarantee. Your local calc, shop should be able to show you it in action.

NEW CASES FROM VERO

New Eurocard-sized cardframes have just been announced by Vero. The frames, called the KM6, are available from Vero Electronics Ltd, Industrial Estate, Chandlers End, Eastleigh, Hampshire SO5 3ZR.

STEVENSOR

Electronic Components

METAL FILM RESISTORS

A range of high precision, very high stability, low noise resistors. Rated at ¼W. 1% tolerance.

Available from 51 ohms to 330K in E24 series. Any mix

each 100+ 1000+ ¼W 1% 4p 3.5p 3.2p

Special development pack consisting of 10 of every value from 51 ohms to 330K (a total of 930 resistors) . . . £23.75

BRIDGE RECTIFIERS

Type	PIV	1		Туре	9	PIV	1	
W005	50	1A	22p	2KB	B10	100	2A	39p
W01	100	1 A	25p	2KB	B20	200	2A	45p
W02	200	1 A	30p	2KB	B40	400	2A	50p
W04	400	1 A	35p	BY2	25	200	4.2A	100p

REGULATORS

78L05	30p	79L05	70p	LM309K	110p
78L12	30p	79L12	70p	LM317	220p
78L15	30p	79L15	70p	LM323K	530p
7805	60p	7905	80p	LM723	35p
7812	60p	7912	8 0p		
7815	60n	7915	8∩n		

Subminiature toggle. Rated at 3A 250V.

SPDT 65p SPDT centre off 70p DPDT 75p DPDT centre off 90p

Standard toggle

DPDT ,48p 34p

Wavechange switches.

1P12W, 2P6W, 3P4W or 4P3W all 37p each.

Miniature switches (non-locking)

Push to make 15p Push to break



Plastic cased Thyristers. Texas

	4 A	8A	12A
100V	36p	45p	62p
200V	42p	53p	68p
400V	51p	66p	86p

Plastic cased Triacs. Texas

All rated at 400V

4A	70p	12A	90p	20 A	185p
8A	80p	16A	95p	25A	215p

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TRANSISTORS

				214007	120
				3N1302	38b
AC127	17p.	BCY71	1.4p	2N2905	22p
AC128	16p	BCY72	14p	2N 2907	22p
AC176	18p.	BD131	35p	2N3053	18p
AD161	38p	BD132	35p	2N3055	50թ
AD162	38p	BD135	38p	2N3442	135p
BC107	8p	BD139	35p	2N3702	8p
BC108	8p	BD140	35p	2N3704	8p
BC109	8p	BF244B	36p	2N3705	9p
BC147	7p	BFY50	15p	2N3706	9р
BC148	7p	BFY51	15p	2N3707	9р
BC149	8p	BFY52	15p	2N3708	8p
BC158	9p	MJ2955	98p	2N3819	22p
BC177	14p	MPSA06	20p	2N3904	8p
BC178	14p	MPSA56	20p	2N3905	8p
BC179	14p	TIP29C	60p	2N3906	8p
BC182	10p	TIP30C	70p	2N4058	12p
BC182L	10p	TIP31C	65p	2N5457	32p
BC184	10p	TIP32C	80p	2N5458	30p
BC184L	10p	ZTX107	14p	2N5459	32p
BC212	10p	ZTX108	14p	2N5777	50p
BC212L	10p		DIA	DDES	
BC214	10p	41.04.4			_
BC214	10p	1N914	4p	1N4148	3р
BC477	19p	1N4001	4p	1N5401	13p
BC478	19p	1N4002	4p	1N5402	15p
BC479	19p	1N4004	5p	1N5404	16p
BC548	10p	1N4006	6р	1N5406	18p
BCY70	14p	BZY88 se	ries 2\	/7 to 33 V 8p	each.

A SELECTION ONLY! DETAILS IN CATALOGUE.

ZTX300

709	25p	LM324	50p	NE556 60 ₁	0
741	22p	LM339	50p	NE565 120	0
747	50p	LM380	75p	NE567 170	О
748	30p	LM382	120p	SN76003 200	0
CA3046	55p	LM1830	150p	SN76013 140	0
CA3080	70p	LM3900	50p	SN76023 140)
CA3130	90p	LM3909	60p	SN76033 200)
CA3140	70p	MC1496	60p	TBA800 70)
LM301AN	28p	MC1458	35p	TDA1022 650r)
LM318N	125p	NE555	25p	ZN414 75r)

OPTO

LEDs	0.125in.	0.2in.	
Red Green Yellow Clips	TIL209 TIL211 TIL213 3p	TIL220 TIL221 TIL223	9p 1,3p 13p

DISPLAYS

DL704	0.3 in CC	130p
DL707	0.3 in CA	130p
FND500	0.5 in CC	100p



Carbon film resistors. High stability, low noise 5%

	L 12 30110.	s. 4.70mms to	TOWN. Ally IIIIX.
	each	100+	1000+
0.25W 0.5W	1p 1.5p	0.9p 1.2p	0.8p 1p

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HERE ARE JUST A FEW OF THE CAPACITORS STOCKED

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0.1, 0.15, 0.22, 0.33, 0.47, 0.68,1 & 2.2uF @ 35V	9р
4.7, 6.8, 10uF @ 25V	13p
22 @ 16V, 47 @ 6V, 100 @ 3V	16p

MYLAR FILM

0.001, 0.01, 0.022, 0.033, 0.047

RADIAL LEAD ELECTROLYTIC

63 V	0.47	1.0	2.2	4.7	10	50
			22	33	47	7p
	100					13p
			220			20p
25 V	10	22	33	47		5p
	100					8p
		220				10p
				470		15p
	1000					23p 5p
10V		220				5p
				470		9p
	1000					13p
		2200				13p 23p

-		LS95	65p
74L	5	LS123	56p
The last	1	LS125	40p
		LS126	40p
LS00	16p	LS132	60p
LS01	16p	LS136	36p
LS02	16p	LS138	54p
LS03	16p	LS139	50p
LS04	16p	LS151	50p
LS08	16p	LS153	50p
LS10	16p	LS155	80p
LS13	30p	LS156	80p
LS14	70p	LS157	45p
LS20	16p	LS164	90p
LS30	16p	LS174	60p
LS32	24p	LS175	60p
LS37	26p	LS190	80p
LS40	22p	LS192	70p
LS42	53p	LS193	70p
LS47 LS48	70p	LS196	80p
LS48 LS54	48p 16p	LS251	60p
LS54	29p	LS257 LS258	55p
LS73	29p	LS258	55p 40p
LS75	44p	LS283	60p
LS76	35p	LS290	55p
LS78	35p	LS365	45p
LS83	60p	LS366	45p
LS85	70p	LS367	45p
LS86	33p	LS368	45p

45p 45p

LS386

LS670

35p

1.590

LS93

ı	THE R.	134	7494	52p
ı		-	7495	52p
			7496	50p
	7400	12p	74121	25p
	7401	12p	74122	33p
	7402	12p	74 1 23	40p
	7404	12p	74125	35p
	7408	14p	74126	35p
	7410	12p	74132	50p
	7413	25p	74141	56p
	7414	48p	74148	90p
	7420	12p	74150	70p
	7427	24p	74151	50p
	7430	12p	74156	52p
	7442	43p	74157	52p
	7447	55p	74164	70p
	7448	58p	74165	70p
	7454	14p	74170	125p
	7473	25p	74174	68p
	7474	25p	74177	58p
	7475	32p	74190	72p
	7476	28p	74191	72p
	7485	70p	74192	64p
	7489	145p	74193	64p
	7490	32p	74196	55p
	7492	35p	74197	55n

FULL DETAILS IN CATALOGUE 4029 60p

		4040	68p
4001	15p	4042	54p
4002	15p	4046	100p
4007	15p	4049	28p
4011	15p	4050	28p
4013	35p	4066	40p
4015	60p	4068	20p
4016	35p	4069	16p
4017	55p	4071	16p
4018	65p	4075	16p
4023	15p	4093	48p
4024	45p	4510	70p
4026	95p	4511	70p
4027	35p	4518	70p
402B	52p	4520	65p



Low profile by Texas

8 pin	10p	24 pin	24p
14 pin	12p	28 pin	28p
16 pin	13p	40 pin	40p
Soldercon	,	100: 50p	400

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DELIVERY

FROM STOCK



news digest

FIBRE OPTIC LIGHT **PEN**

A:

Light pens have never figured very greatly in the amateur market, but this device from Optronic Fort Ltd hopes to change that, particularly with the tremendous interest in mini-computers. It is TTL compatible and uses a pinphotodiode, weighs only 35 grammes and can be yours for only £175. Call them at Cambridge Science Park, Milton Road, Cambridge CB4 5BH.

VIDEO DISC 2

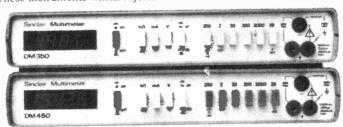
Further to the Philips video disc launch, news has just arrived about the RCA 'Selecta Vision' video disc system, pioneered in the USA. The RCA system uses a grooved disc, with diamond stylus. The disc rotates at 450 rpm, and has one hour's playing time per side. Again only drawback is you can't record your own material, but just think, you will be able to buy your own copy of Star Wars or even Emmanuel, if your that way inclined, and you can see the good bits over and over again, Cor.

BREADBOARD '79

What! already. Well this year there are two dates to put into your Letts Electronic diaries. The Midlands show will be at Bingley Hall, Birmingham, on May 23rd-26th, and the London show is at the Royal Horticultural Hall, Westminster, December 4th-8th. Figures show over 10 000 people attended the first show, and that's a fantastic response for the first ever home electronics exhibition, indeed the Birmingham show is due entirely to response from contributors and visitors, we'll see you there.

SINCLAIR AGAIN

Two new laboratory quality multimeters are promised for 1979. As usual you can expect the Sinclair innovations in cost and features. These instruments which rejoice under the titles of DM450 (41/2 digit 5 function) and DM350 (31/2 digit, 34! ranges). They both have good technical specifications and accessories. See the Microvision article for Sinclair's address.





Following the tragic death of John Miller Kirkpatrik a memorial fund has been established for the benefit of his family. Those wishing to make a donation should send this to: John Miller Kirkpatrik John Miller Kirkpatrik Memorial, Lloyds Bank Ltd, 39 Threadneedle Street, London

EXPORT

ENGUIRIES

INVITED

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LONDON W2 1ED

404 EDGWARE ROAD,

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You're also wasting money if you're building circuits and you scrap them just because you've no further use for them.

In both cases you're wasting time too.

Breadboards are fully re-usable and avoid these losses - you only need to hard wire your circuit to keep the final design.

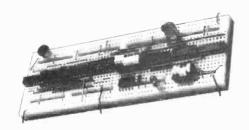
LEKTROKIT offer you a full range of breadboards, any of which allows you to build a circuit or try out mods in a fraction of the time. And with no soldering or de-soldering.

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So you save money. And you save time.

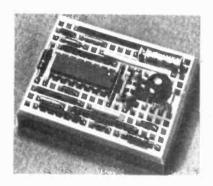
Further, LEKTROKIT breadboarding is expandable to match whatever configuration you

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Lektrokit Super Strip SS2 Only £11.05 inc. p & p and VAT

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(All prices	include p & p a	nd VAT)		

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Switches on to preset brightness Can be switched and dimmed from many locations using TDE/K kit making 2-way **PRICE TDK £8.99



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DIGITAL TO ANALOGUE TECHNIQUES

Digital to Analogue conversion (DAC) is a fast growing section of electronics. Tim Orr explains some of the more practical applications.

ELECTRONICS HAS CHANGED enormously in the past ten years, having swung away from valves, germanium transistors, even from descrete devices themselves. The trend is towards more and more complex integrated circuits, complete systems in a chip, large scale integration (LSI). Also the trend has swung heavily towards digitally based systems rather than analogue ones, partly because the IC manufacturers can get a greater success rate from making digital devices and partly because there are very many applications which can only be contemplated with a digital device. Such examples as pocket calculators and microprocessors spring immediately to mind. However there are several areas where analogue techniques present the only realistic solution (at this moment in time), such as tone controls in an audio amplifier. In fact, good cases can be made out for both analogue and digital systems and there are many examples where both are needed. In these it will be necessary to change from the analogue to the digital world or vice versa and to do this, some sort of conversion process has to be practised.

Digital to Analogue Conversion.

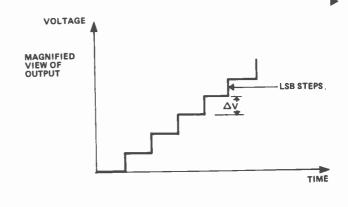
The job of a digital to analogue converter (DAC) is to convert a binary code (a digital data word) into an analogue voltage. The data word is a digital representation of that analogue voltage. Thus if we presented the DAC with a digital word that was linearly increasing in magnitude, the output would be a linearly increasing analogue voltage. This digital word would be the output of a binary counter driven by a constant clock frequency. The analogue output is a linear ramp, or rather a linear staircase where the step size is controlled by the 'size' of the DAC. If the DAC is an 8 bit device, ie it can accept data words 8 bits wide, then it can generate a possible 28

descrete output level. Now 28 is 256, so therefore an 8 bit DAC could generate a staircase with 256 steps in it. The resolution of the DAC is thus 1 part in 256, or rather a change of one LSB (least significant bit) in the data word will make the output voltage change by 1/256th of the full scale output.

To get really fine resolution then a high performance DAC is needed. DAC prices seem to be almost linearly proportional to their resolution. I have got several DAC's amongst my collection of bits. There is an 8 bit DAC costing about £4, a 12 bit DAC costing about £35 and a 16 bit DAC costing just over £200. It is now possible to buy a monolithic (a single I C) DAC with a bit size of 6, 8, 10 and 12, but above this the devices are usually modular.

Size And Resolve

Fig 2 shows the relationship between DAC size and resolution. Notice that a 16 bit DAC with a 10 V full scale output is made up of a staggering 65,536 descrete



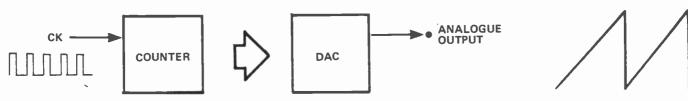


Fig 1. Converting binary code to analogue voltage.

	T .	1	
WORDLENGTH n	RESOLUTION 1 PART IN 2n	MAXIMUM THEORETICAL DYNAMIC RANGE	BIT SIZE ASSUMING FULL SCALE = 10V
1 2 3 4 5 5 6 7 7 8 8 9 10 11 12 13	2 4 8 16 32 64 128 256 512 1024 2048 4096 8192	6dB 12dB 18dB 24dB 30dB 36dB 42dB 48dB 54dB 60dB 66dB 72dB 78dB	5.0V 2.5V 1.25V 0.625V 0.312V 0.156V 78.1mV 39.1mV 19.5mV 9.7mV 4.8mV 2.4mV 1.2mV
14 15 16	16384 32768 65536	90dB 96dB	610uV 305uV 152uV

Fig 2. Relationship between size and resolution.

levels each $152~\mu V$ in size. (There is also available an 18 bit device, costing a small fortune. The larger the bit size of the DAC, the larger is the dynamic range (best signal to noise ratio) of its output. This increases by 6~dB per bit. Thus a 10~bit DAC can give a best range of 60~dB.

The human anatomy has developed over the last few million years to respond to its environment. This has resulted in the following performance figures. The sensitivity of the eye to colour is not that good. Colour television transmission doesn't give much of its bandwidth to the colour part of the signal. Have a look at a TV and see how well defined the colour is; it is usually just "sort of smeared around" the subject. Thus it is possible to get quite good digital video using only 4 bits for the colour. The eye sensitivity to resolution is somewhat better, but even so an 8 bit oscilloscope memory will look fairly continuous, giving little indication that it is made up of descrete steps.

Ear Lead

However the ear can still outperform present day technology. Using a 16 bit high quality audio system a trained ear can still detect the difference between the digitally processed sound and the original. Thus, when using DAC's in professional audio equipment great care has to be taken to eliminate all types of abberations in the system. These digital abberations don't just worsen

the signal to noise ratio (as an analogue system might), but they produce discordant harmonic distortion, sidebands like those obtained from ring modulation and other little funnies.

Figure 3 shows a DAC system in operation. The output of the DAC is meant to produce nice clean square wave steps, but the leading edges of these steps always have small spikes (glitches), caused by the switching times associated with the DAC's internal workings. These glitches are not regular in nature and so filtering cannot eliminate them. The glitches give the sound a "dirty" quality, or, if the system is an oscilloscope display it produces fuzzy pictures.

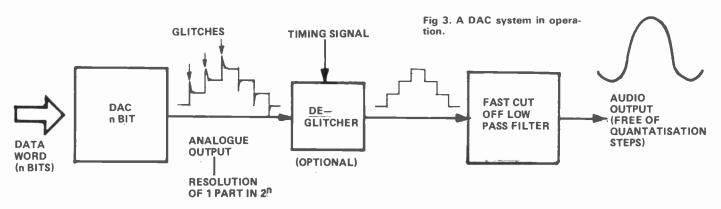
The glitches can be removed with a little module called a DEGLITCHER, fig 4. This is a logic controlled sample and hold which holds during the glitch period, but otherwise tracks the signal from the DAC. Thus the glitches are ignored. The output from the deglitcher then passes through a low pass filter and this removes the "stepped" quality of the signal and produces a smooth analogue output. The cut off frequency of this filter is very important and is related to the data rate of the DAC, The rule of thumb is that the filter cut off frequency should always be less than half of the data rate frequency.

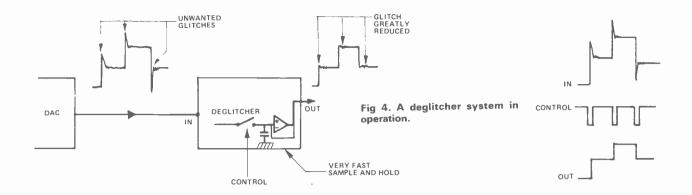
Buying And Building

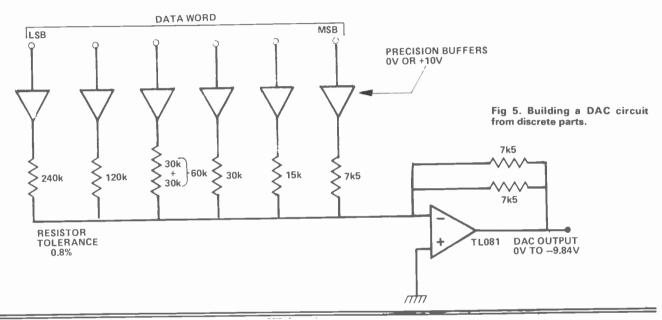
DAC's can be bought fairly cheaply as complete IC's or they can be constructed out of generally available parts, fig 5. This circuit uses precision buffers (a CD4041 will do), E24 resistors and a FET op amp. The buffers are run from a + 10 V supply and their purpose is to provide high (+10 V) and low (0 V) output with low source resistance. They are driven by a 6 bit data word, the MSB (most significant bit) thus drives the 7k5 resistor, the LSB (least significant bit) the 240k resistor. So, when the MSB changes, the output of the op amp will move by a large amount (5 V), but when the LSB changes the output will only change a little (0V156). Going from the MSB down to the LSB, each bit has only half the effect of its predecessor. This is obtained by doubling the resistor values (7k5, 15k, 30k, 60k, 120k, 240k).

A 6 bit DAC can produce 2^6 descrete output levels. Now 2^6 is 64 and so the overall resistor tolerance should be \pm 1 part in 2 x 64, which comes out at \pm 0.8%. This type of DAC is known as a resistance ladder DAC, but in its presented form it is rather limited. For instance, a 10 bit device would require a resistor range of 1024 to 1

and a tolerance of 0.05%.







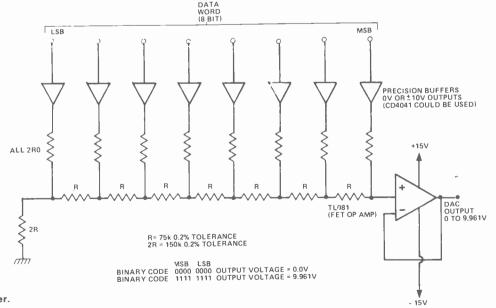


Fig 6. An R-2R ladder.

Multiple Choice

The DAC shown in Fig 6 overcomes the problem of multiplicity of resistor values; only two are needed. The resistor tolerance

still applies. Also the ratio between the resistor value and the buffer ON/OFF resistance is important. The 2R resistors connected to the buffers should ideally be 2R — (the buffer output resistance).

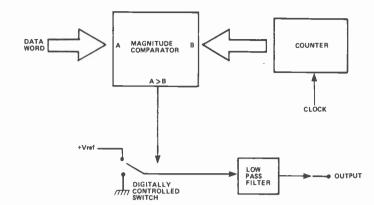
Counting On This

A "counting" type ADC is composed of a fast comparator, a gate, a counter and a DAC. This is why ADC's always cost more than DAC's, the ADC uses a DAC to do the conversion. Assuming that the analog input is positive, and the DAC produces a positive output, the conversion operation is as follows:

1) The signal "start conversion" is generated. This resets the counter to all zero's, the DAC output goes to zero, the comparator output goes high and so the clock is allowed to enter the counter. Thus the count proceeds and the DAC generates a positive going staircase.

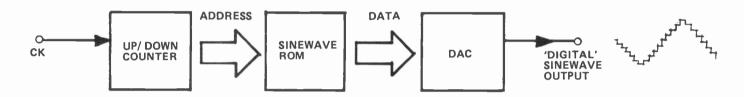
2) When the DAC output exceeds the level of the analog input the comparator output goes low, the counter stops. This is the end of the conversion, and the data that is held on the counters output is the data output. It would then be transferred to some latches, and held there until the next conversion is finished.

This data word describes as precisely as is possible the magnitude of the analogue input. Although simple to operate, this method has a major disadvantage, it is slow. Imagine that the ADC is a 10 bit device and the clock frequency is 500KHz,



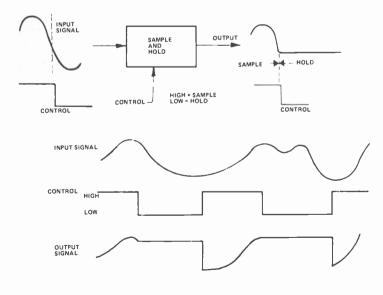
then the longest conversion time will be 1024 counts at $2\mu\,\text{Sec}$ per count which is 2.048mSec, this means that the conversion rate will be less than 500 per second.

Memory Planning



The data that drives DAC's can come from several sources. It could be generated by computation or read from a programmed memory as shown. In this example a ROM (read only memory), has been programmed with the data necessary to produce a

sinewave. An updown counter provides the address for the ROM and the data is converted into an analog output by the DAC. The clock frequency divided by the size of the counter determines the sinewave frequency.

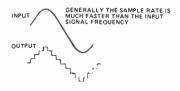


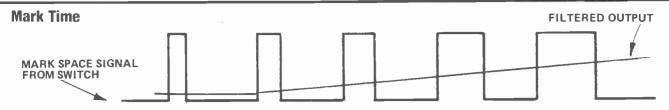
Data Lining

Another method of generating data is to convert analogue information into digital words. The signal must first be passed through a low pass filter, the cut off frequency of which must be less than half of the conversion frequency. The signal is then "held" in a sample and hold unit so that the ADC can do its conversion on a static signal. Control logic sends commands to the ADC giving it various instructions. The sequence of events is:

- 1) Tell sample and hold to HOLD.
- 2) Tell ADC to start conversion (SC).
- 3) Conversion finished, generate end of conversion signal (EOC).
- 4) Tell sample and hold to SAMPLE.

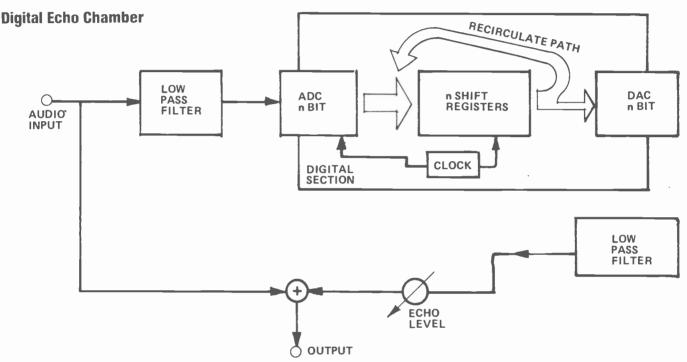
The process then repeats itself. The sample and hold mechanism is shown below. Generally, in one period and the input signal several ADC conversions will be done. The data generated is then stored, processed or transmitted.





Yet another type of DAC, a mark space modulation DAC is shown above. The data word is presented to one side of a magnitude comparator, the output from a fast running counter to the other. When the counter is greater than the data word the A>B output goes low. The output is a mark space waveform the ratio of which is linearly proportional to the magnitude of the

data word. The mark space signal operates a precision switch, the output of which is lowpass filtered, providing a smoothed DC output. This type of DAC requires a fast running counter, but gives a relatively low bandwidth output signal. It is a gots solution for a system where lots of slow moving outputs are required, because the counter can be common to all the DAC's.



There are several professional echo chambers that are all digital. The audio input is converted into a digital word and then put into a parallel set of shift registers. A 10 bit system would use 10 sets of registers. The clock that starts the ADC conversion also shifts the data along the shift registers. The data coming out of the shift registers is then converted back into an analogue voltage by the DAC. It is then filtered and mixed with the original signal.

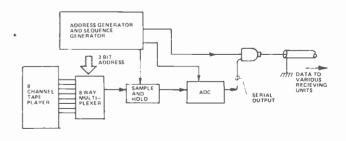
The echo can be made to repeat indefinitely by using the digital recirculate path around the shift registers. The amount of

digital storage required is rather large. Let us assume that we want a good quality echo. This would be a 10kHz bandwidth, 60 dB dynamic range which implies a clockrate of about 25kHz and a 10 bit system. Thus to store 1 second of sound (to give one second delay), we would need 10 × 25,000 bits of memory, 0.25 Mbits!

The usual solution to this dilemma is to get longer delays at the expense of bandwidth. Thus a 1 second delay would be 1kHz bandwidth, a 0.1 second delay would be 10 kHz bandwidth. This would only require 25K of memory.

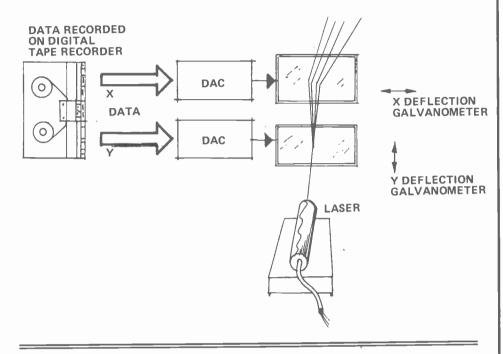
Multiplexed Sound System

Next time you are on an aircraft with a multichannel music system, it is quite possible that the sound you are hearing via your stethoscope is digitally generated. The sounds are usually stored on a multichannel tape player and each channel is connected to a multiplexer. This is a digitally controlled rotary switch and it is continually scanning all the audio channels. The output of the multiplexer is then fed to the ADC. Thus each channel is converted to a digital code. This digital code is then transmitted in serial mode and mixed with a sync pulse. The transmitted information is a series of serial data words, each representing a small piece of the eight music channels, plus some synchronisation data which passes down a two wire system to each receiving unit. This saves wire weight, there is less crosstalk and low pickup due to the high noise immunity of digital systems.



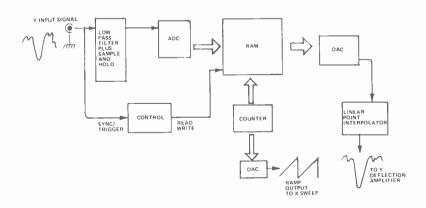
Laser Light Show.

One of the recent laser light shows in London used a digital tape recorder to store the data for the show. Two outputs were produced which were converted into control voltages by DAC's. These voltages were then used to manipulate the X and Y Co-ordinates of the laser. Thus it was possible to draw pictures and cartoon characters with a moving laser beam.



Digital Memory for an Oscilloscope.

There are several products on the market that enable an ordinary oscilloscope to store waveform information. This is particularly useful if you are trying to capture non-repeating events. The system is very similar to the digital echo unit, there is an ADC, a memory and a DAC. Also there is a trigger circuit so that one shot events can be captured and a ramp generator to produce the Xsweep. The output of the DAC is rather interesting, because it is not low pass filtered, but it uses a linear point interpolation device. Basically, what this does is to join up the dots, so that a waveform that is represented by only a few points, can be made to look like the original signal. The visual results of interpolation are very good indeed.



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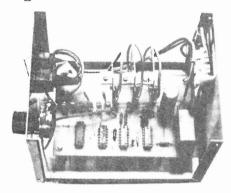
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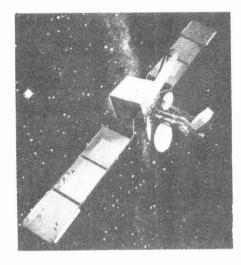


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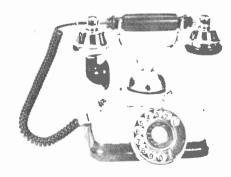
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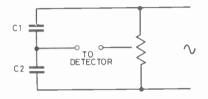
Speak to someone on the phone outside Europe and the chances are that your voice will spring out into space for thousands of miles on the way. The commercial ends of the space programme are described

Telephones



Do you know how the 'phone, one of the most widespread pieces of electronics, works? Lots of exciting things are happening on this front; we pull back the curtain and take a peep next month.

Crossing your Bridges



The Wheatstone Bridge is one of the commonest circuit configurations in electronics. Next month K. T. Wilson examines the theory of this and describes the variations that we now use.

Experimenters Power Supply

Second in our series of test gear projects is a 0-20V, 1A bench power supply, stabilised of course as well as short circuit protected.

Workshop Test Gear

The HE project team have prepared a feature giving their views about what you need in the way of test gear in your workshop. It's a thoroughly practical approach and continually bears in mind the limitations of finance.

How TV Signals are Propogated



Put up an aerial in most areas of Britain and you'll have no trouble in getting a good signal but that's only because the broadcast engineers have taken into account a multitude of factors. We take a look at this subject in the March increase.

The March issue will be on sale February 9th

The items mentioned here are those planned for the next issue but circumstances may affect the actual content.

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Feature and Specification ★ Hour/minute display

- Hour/minute display Large LED display with p.m. and alarm on indicator 24 Hours alarm with on-off control Display flashing for power loss indication Repeatable 9-minute snooze

- Display bright / dim modes control

Size 5.15 x 3.93 x 2 36 (131mm x 100mm) Weight: 1 43 lbs (0 65 kg)

Guaranteed same day despatch

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- Calculater with %, √ & memory.
- Hrs, mins, secs, day, month, day of week
- * Alarm

 * Stop-watch with 1/10 secs to 10 hours + lap
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- Batteries last 1 year continuous operation
 Dimensions %" x 2%" x 4%" in.
 Complete with leatherette wallet.

LIST PRICE £24.95 METAC SPECIAL EXCLUSIVE PRICE

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Cannot be found cheaper anywhere else

SEIKO

UPERIOR WATCHES

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SOLAR

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5 function LCD



CHRONOGRAPH List price £85 **METAC PRICE £68**

THE METAC

DIGITAL CLOCK

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Silent Synchronous Accuracy - Fully electronic
Pulsating coles - Push-butten setting
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Easy-to-follow instructions - Size 10.5 x 5.7 x 8 cm
Ready drilled PCB to accept components

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15:28

COMPLETE KIT *

SEIKO

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Snooze + backlight. Batteries last 1 year

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approx Include Excellent value

Includes batteries and travel pouch.

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LADIES LCD

thick. 5 function; hours. mins, secs, day, date. + back light and auto cal. Elegant metal bracelet in silver or gold. State pre-ference.

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Mains operated Soft glow green display MW / FM & LW radio Alarm with 9 min. snooze feature

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GENUINE

SOLAR CHRONOGRAPH

Daly 25 x 20 mm and 6 mm

£9.95



.

10:08

ALARM LCD

CALCULATOR WATCH

List price £165

METAC PRICE £127

ONLY £19.65

6 digit 7 functions + penetrating alarm. Hours Mins Secs Day Date Alpha Day Year. Back light + 200 vear calendar.

THOUSANDS SOLD

11 FUNCTION

SLIM CHRONO

6 digit 11 functions

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O PERSON

10:08".

16 4 2 50 5 13 1 43 55 63 - 0 5 6 8 10 25 73 0 4 5 8 0 5 15 6 15 86 80

Hours, mins, secs.

Day date day of week * 1/100, 1/10, secs, 10 x secs, mins.
* Split and lap modes.

Back light, auto calendar Daly 8 mm thick. This same watch is being sold for £22,00 in newspaper and magazine special offer

Metac Price

£12.65

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WATCHES

Full spec. calculator

+ 6 function watch.

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- Automatic brightness control
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Constant LCD display of constant CCD display of hours and minutes. plus optional seconds or date display, plus day of the week and am/pm indication

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- Perpetual calendar; day, date, month and year.
- ●24-hour alarm with on/ off indication.
- 1/10 second chrono-graph measuring net, lap and first and second place times.

£27.95 Dual time zone facility Night light.



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HEADLIGHT DELAY

Use your car headlights to give post-parking illumination with this simple unit.

THIS SIMPLE LITTLE UNIT lets you use your car head or spot lights to illuminate your pathway for a pre-set period of about 50 seconds after you have parked the vehicle. At the end of this period the unit turns the lights off automatically

The unit thus enables you to avoid walking into dustbins or tripping over junk that may be obstructing your private driveway, and helps you avoid stepping into various nasty bits that may be laying on the public sidewalk. The unit is easy to install in the vehicle.

Construction and Use

Construction of the unit should present no problems at all. The relay can be any 12V type with a coil resistance of 120ohms or greater, and with two or more sets of N.O. contacts that are rated at 3 amps or greater.

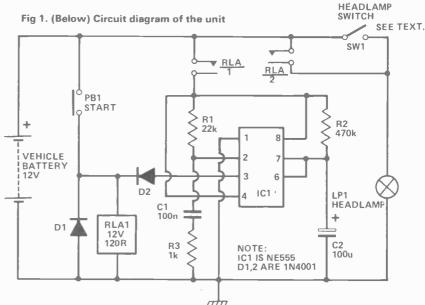
When it comes to installing the unit, note that two methods of correction to the vehicle are possible. On some vehicles the headlight switch is connected directly to he battery so that the headlights operate even when the ignition is turned off (see Fig 2a). In this case take connection 4 of the 5-day terminal block directly to the live side of headlamp switch SW1, and connection 5 to the headlamp side of SW1.

The alternative connection is shown in Fig 2b. Here, the headlight switch is wired in series with the vehicles ignition switch, so that the headlights only operate when the ignition is turned on. If your vehicle uses this type of connection, take connection 4 of the 5-way terminal block to the live side of the ignition switch, and take connection 5 to the headlamp side of SW1.

BUYLINES

With the small number of components involved, it would be surprising if there were any problems in obtaining them.





HOW IT WORKS

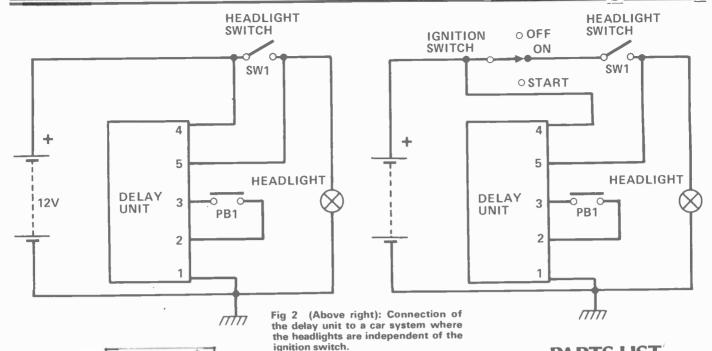
The unit is designed around a type-555 timer i.e., with a relay output. The relay has two sets of normally-open contacts. Normally, START switch PB1 and the relay contacts are open, so zero power is fed to the timer circuit and (assuming that HEADLIGHT switch SW1 is open) the headlights are off. Circuit Action is initiated by briefly closing push-button switch PB1.

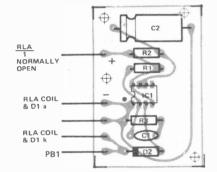
When PB1 is momentarily closed power is fed directly to the relay coil, and the relay turns on. As the relay turns on contacts RLA/2 close and apply power to the headlights and contacts RLA/1 close and apply power to the timer circuit, but pin 2 of the IC is briefly tied to ground via C1 and R3 at this moment, so a negative trigger

pulse is immediately fed to pin 2 of the IC and a timing cycle is initiated. Consequently, pin 3 of the IC switches high at the moment that the relay contacts close, and tbus locks the relay on irrespective of the subsequent state of switch PB1.

The 555 is wired as a one-shot timer or monostable with a timing period of about 50 seconds (determined by R2 and C2). Thus, the relay and headlights are held on for the duration of this 50 second timing period. At the end of the timing period pin 3 of the IC switches to the low state, so the relay turns off and contacts RLA/1 and RLA/2 open, removing power from the timing circuit and the headlights. The operating sequence is then complete.

PROJECT: Headlight Delay





CONNECTIONS 2 5 1 3 0 0 \oslash 0 0 0 \oslash SW1 **HEADLAMP** PB₁ SIDE

PB1

SW1

0V

CHASSIS

(Above Left): Connection to all other systems!

Fig 3. (Left): Component overlay for the delay unit

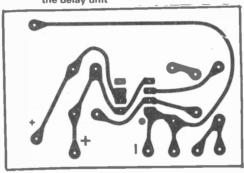


Fig 4. (Left): Wiring of the delay unit to a 5 terminal connection block

Fig 5. (Above): Full size foil pattern of the headlight delay PCB.

Fig 6. (Below right): The relay and DI wiring.



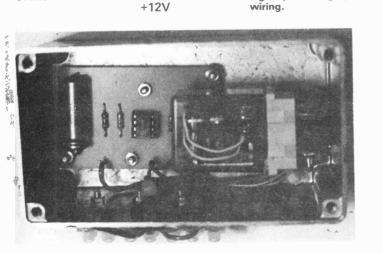
RESISTORS 22k 470k R1, R2, R3, 1k

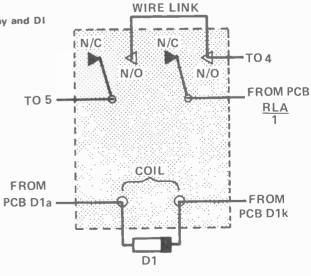
CAPACITORS C1 C2, 100n polyester 100u elect.

SEMICONDUCTORS IC1 NE555 IC1 D1, 2 IN4001

MISCELLANEOUS Relay rated at 3A 2 pole c/o Coil 7120 SPST push button 5 way terminal. Block rated at 5A Die-cast case

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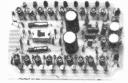
	TELERIE, SONNET ONS SEB				-
7400 SERIES 74LS00 SERIES	7400 SERIES . 74LS00 SERJE	7400 SERIES 74LS00 SERIES	CM05		
1+ 25+ 100+ 1+ 25+ 100+ 7400 .08 .075 .07 .155 .14 .13 7401 .11 .105 .10 .155 .14 .13 7402 .11 .105 .10 .155 .14 .13 7403 .11 .105 .10 .155 .14 .13	1+ 25+ 100+ 1+ 25+ 10 7490 .30 .28 .26 .42 .38 .3 7491 .60 .55 .52 7492 .33 .30 .28 7493 .28 .25 .23 .43 .40 .3	74167 2.20 2.05 1.95 74168 1.60 1.40 1.25 74169 1.60 1.40 1.25	1+ 25+190+ 4000 .13 .11 .10 4001 .13 .12 .11 4002 .13 .12 .11 4006 .70 .62 .58	1+ 25+ 100+ 1+ 25+ 100+ 4072 14 13 12 4554 90 78 68 4073 14 13 12 4555 75 62 36 4075 14 13 12 4555 75 62 26 26 4076 8.2 78 75 4557 37 280 280 240 4076 8.2 78 75 4557 370 280 280 240 4076 8.2 78 75 4557 370 280 280 240 4076 8.2 78 75 4557 370 280 280 240 4076 8.2 78 75 4557 370 280 280 240 4076 8.2 78 75 4557 370 280 280 240 4076 8.2 78 75 4557 370 280 280 240 4076 8.2 78 75 4557 370 280 280 240 4076 8.2 78 78 78 78 78 78 78 78 78 78 78 78 78	LIMEARS GA3045-14 .30 CA3046-14 .40 LM380N-14 .68 LM381N-14 .90
7404 .11 .105 .10 .16 .15 .135 7405 .12 .115 .11 .16 .15 .135 7406 .22 .21 .20 7407 .22 .21 .20	7494 .50 .45 .42 7495 .50 .45 .42 .64 .58 .5 7496 .48 .42 .38 7497 1.80 1.70 1.65	74172 3.80 3.55 3.40 74173 .90 .84 .80 .85 .80 .76 74174 .64 .60 .56 .58 .52 .49 74175 .58 .54 .51 .58 .52 .49	4007 .13 .12 .11 4008 .58 .52 .48 4009 .32 .29 .27 4010 .36 .32 .30	4077 38 35 32 4558 90 80 72 4078 14 13 12 4559 3.00 2.50 2.20 4081 14 13 12 4560 1.45 1.20 1.05 4082 14 13 12 4561 62 55 .50	LM710N-14 .26 LM711N-14 .26 MC1310P-14 1,30 NE555-8 .23
7408 .13 .125 .12 .155 .14 .13 7409 .13 .125 .12 .16 .15 .135 7410 .11 .105 .10 .155 .14 .13 7411 .17 .16 .15 .16 .15 .135 7412 .14 .135 .13 .16 .15 .135	74105 .37 .34 .32 74107 .22 .20 .18 .32 .28 .2 74109 .28 .26 .24 .32 .28 .2	74180 .80 .70 .62	4011 .13 .12 .11 4012 .13 .12 .11 4013 .30 .25 .22 4014 .68 .62 .56 4015 .60 .55 .52	4085 .58 .54 .52 4562 4.20 3.60 3.25 4086 .59 .54 .52 4566 .98 .86 .80 4089 1.29 1.08 1.00 4568 1.70 1.50 1.38 4083 .45 .40 .38 4569 1.37 1.5 1.05 4084 1.38 1.25 1.15 4580 4.20 3.65 3.40	ME556-14 .50 ME25018-14 1.25 SN75110M .40 SN75003M 1.65 SN76013M 1.25
7413 23 21 20 28 26 24 7414 46 43 40 65 57 50 7415 7416 22 20 18 15 135 7417 .22 20 18	74113 .28 .26 .24 .32 .28 .2 74114 .32 .28 .2	5 74185A1.00 .90 .86 5 74186 7.20 6.90 6.70	4016 .32 .28 .26 4017 .50 .46 .44 4018 .55 .50 .47 4019 .40 .35 .32 4020 .68 .64 .60	4095 .85 .80 .77 4581 1.98 1.67 1.40 4096 .85 .80 .77 4582 .82 .74 .68 4097 3.00 .280 2.67 4583 .70 .60 .52 4099 .90 .84 .78 4584 .30 .7 .25 4099 .10 .95 .88 4585 .82 .78 .70	\$N76023N 1,25 \$N76033N 1.65 TAA550B .30 TAA661B 1.00 TBA120S .58
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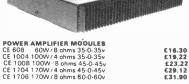
Suitable for nearly all moving-coil cartridges. Sensitivity 70/170uV switchable on the pic b. This module brings signals from the now popular low output moving-coil cartridges up to 3 5mV (typical signal required by most pre-amp disc inputs). Can be powered from a 9V battery or from our REG 1 regulator board.

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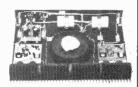


TOROIDAL POWER SUPPLIES CPS 1 for 2 x CE 608 or 1 x CE 1004 CPS2 for 2 x CE 1004 or 2 / 4 x CE 608 CPS3 for 2 x CE 1008 or 1 x CE 1704 CPS4 for 1 x CE 1008

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CELLULAR LOGIC MAGE PROCESSING

At University College, London, there is a research group working on a method of image processing which could prove to be the link between the human eye and the TV camera. Computing Today's Phil Cohen talked to Dr. Michael Duff about Cellular Logic Image Processing.

CELLULAR LOGIC IMAGE PROCESSING was first proposed in 1958 by S. Ungar in the States. It was suggested that the cells of the human eye do a lot of the processing *before* what we see is fed up the optic nerve to the brain.

What exactly do we mean by image processing?

Generally, it means processes like perimeter-finding — producing the outline of an object, or skeletonising — finding a set of lines which are unbroken and follow the object's shape.

This sort of process can be used in such diverse applications as fingerprinting, character recognition (OCR) or even intruder detection (spotting movement on a TV picture) but perhaps the two most useful areas will be biomedical scanning — chromosome counting or looking for abnormalities on X-ray plates — and production line quality control.

Parallel Processing

The model of the human eye previous to 1958 was of a simple camera — the point-by-point information was fed to the brain, which did all the clever processing.

However, it was pointed out that for processes such as edge-finding it was much more efficient to use a

parallel processing system.

The essential difference between serial and parallel processing schemes is that in a serial scheme the data is processed bit by bit in a central unit (CPU) and the intermediate results are stored in memory, In parallel processing the data is fed in as an array and the processing takes place all at the same time — there is one processor for each data element. The intermediate results are passed from processor to processor as the calculations continue.

In the human eye, then, the question is: could a number of cells just behind the light-detecting ones be the parallel processors, responding to commands from the brain to find the edges of objects, or detect movement? Certainly it is known that the edges of the field of vision are extraordinarily good at spotting movement — could this be because the structure of the eye is different there?

The Processors

Going back to the CLIP machine, in this sort of application the type of processor we are talking about is in no way as complex as a modern MPU. The sort of data it receives are single-bit inputs from the image sensor

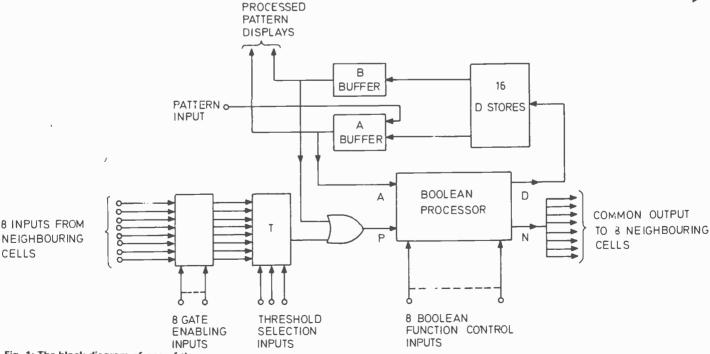


Fig. 1: The block diagram of one of the processors.

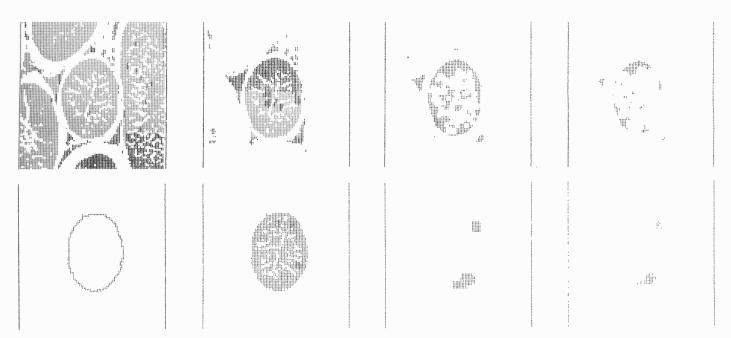


Fig. 2: Stages in the processing of a microscope picture of part of a rat's anatomy.

associated with it and one bit each from the eight nearest processors' outputs.

Why eight? Well, this provides an optimum "connectivity" - too few and the processing becomes slow, too many and the cost of connecting the processors together becomes enormous.

The sort of operation the processor would have to perform would be to give an output if any of its neighbours gave an output and the image bit fed to it was a "0"

The program example (in PET BASIC) given shows the usefulness of this sort of process. Of course, we cannot perform parallel processing directly in BASIC the program has to scan the image bit by bit, simulating the action of each processor in turn.

The important thing about using this sort of scheme for image processing is that the outputs of the units will change in "waves", travelling at speeds dependant on the propogation delay of the devices involved. This means that, by having four "edge registers" which are not connected to the image input, we can do things like finding the outer edge of an object by starting a signal from the edge registers and programming the processors to stop propogating it at the edge of the object. The program example carries out this sort of process.

Structure

In the CLIP machine, the processors each have the structure shown in Fig 1. Each is connected to its eight neighbours and its output fans out to the same neighbours. There is also a "pattern input" for connection to the picture signal (which is derived from a TV camera and multiplexed to provide each processor with a 1-bit signal from one point of the camera's image).

The gate enabling threshold selection and function control inputs are from a programming bus common to all processors.

The gate enabling inputs allow instructions like "If the output from the processor to the left is '1' . . . "The threshold selection inputs allow "If more than three inputs are '1' . . .

Combining the two allows very comprehensive processing of the inputs — "If any two of the processors to the left give and output . . ." for example.

There are also various buffers for more complex

instruction types.

The boolean processor itself can be programmed via the function controls to "look" like any combination of memory-less logic gates.

Implementation

The processors come in custom-built ICs, each chip containing eight units. The CLIP 4 machine contains an array of 96 x 96 processors.

CLIP 4 is the product of ten years of research at University College. It's a commercially viable product it fits into one 7-foot instrumentation rack, including power supplies and controller. The cost? In the region of £30-40 thousand.

The processors themselves are based on NMOS technology and the control circuitry (the part that acts as a "conductor" - in the musical sense - directing all of the processors) is implemented in hardware — an MPU would be too slow!

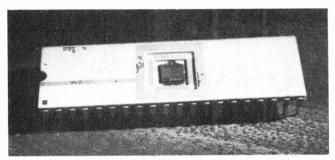
The input signal is from a TV camera (only part of the picture is used — 96 lines x 96 points). This is encoded either as a black and white picture with no grey or as a grey-scale image. CLIP can handle grey-scale pictures, performing processes such as smoothing.

The output from the system would be to a video monitor or, in some applications, just a few bits of data to another peripheral, such as a warning indicator in the case of intruder detection.

Software

The software for the system consists of a series of inputs for the function-definition bus of the processors and a loop structure which is linked to the processor outputs.

Looking at Fig. 2, the machine is trying to find the outline of the largest isolated mass of black in the input pattern.



One of the chips in the CLIP - each contains eight processors.

The original input is shown in the top left. The first instruction propagates white from the edge registers through all connected black. This leaves the pattern second from the left on the top line. The program then 'erodes' the image by removing all black dots not surrounded by black and then removing their neighbour black dots as well

It repeats this erosion until one more step would cause all black to vanish completely. This leaves the image as it is at the end of the top line.

The program then surrounds each black by eight blacks. It does this twice. It then recalls from the original input pattern the part which is "connected" to the current pattern. The last step finds its outline.

Naturally, this sort of software cannot be written in a conventional language - the group have developed what is effectively an assembler for the system and all the groups working on image processing worldwide are due to meet this spring to discuss a suitable high-level language.

Applications

One very interesting application mentioned earlier is production line control. CLIP can tell the difference between an object which has been correctly punched out of metal and one with the wrong surface area or the wrong number of holes, etc.

The amazing thing is that it can do this fifty times a second! In fact, the machine can perform 1500 parallel processes per TV frame period.

The machine could be fitted to the "reject" solenoid on a production line so that badly produced pieces could be pushed off the line.

Another area in which the machine could be useful is in microscopic counting. There are systems available already which will count the number of items in a picture, or even the number between certain size limits, but the inherent flexibility of CLIP make it invaluable for complex tasks such as red blood cell deformity checking and other applications where previously a human operator was the only alternative.

One slightly more frightening possibility is the use of such a system in facial recognition - enabling authorities to keep track of every individual automatically.

When the system was first proposed about ten years ago, the device which was envisaged was a pair of super-binoculars, with photo-diodes at one end and LEDs at the other, modifying images so that only moving objects, or even more selectively, only enemy tanks would be seen! This is some way from the present state of the art but in a few years . . . who knows?

We would like to thank Dr Michael Duff and University College in general for their help.

CLIP SIMULATION PROGRAM

The following program simulates the action of the CLIP machine by pretending to be each processor in turn in a 10 x 10 array. It's very slow to run (several minutes) and this shows the advantage which a parallel processing system has over a serial one.

10 S = 10

S is the dimension of the 2-dimensional square processor array. 20 DIM A(S, S), B(S, S)

A is the image input to the system. B represents the processor outputs. Load the image into the system:

30 FOR I = 2 TO S - 140 FOR J = 2 TO S - 1

50 READ A(S, S)

60 NEXT J 70 NEXT I

The outer layer of processors represent the edge register, in which we can initialise processing 'ripples' (see text).

80 DATA 0,0,0,0,0,0,0,0

90 DATA 0,1,1,1,1,1,0 100 DATA 0,1,0,0,1,0,0,0

110 DATA 0,1,1,0,1,1,0,0 120 DATA 0,1,1,0,1,1,1,0

130 DATA 0,1,1,1,1,0,0 140 DATA 0,0,0,0,0,0,0,0 150 DATA 0,0,0,0,0,0,0,0

Now for the 'seed' which will propogate during processing. Note that it's in the edge register:

1010 B(S, S) = 1

Now print the results so far:

1014 GOSUB 2000

1015 F = 0

F is set to 1 if any changes are made.

1020 FOR I = 2 TO S - 11030 FOR J = 2 TO S - 1 ... For each processor 1040 FOR K = -1 TO 1 1050 FOR L = -1 TO 1

... For each of the eight 'connected' processors

1055 IF L = 0 AND K = 0 THEN 1090

. . . Except the one we're simulating

1060 IF B(I+K, J+L) <> 1 OR A(I, J) <> 0 THEN 1090

skips the next bit unless the image is zero at this point and one of the neighbours outputs is one.

1070 IF B(I,J) = 0 THEN F = 1

B(I,J) is going to be set to 1. F is set to 1 if this represents a change.

1080 B(I,J) = 1

1090 NEXT L:NEXT K:NEXT J:NEXT I

1130 IF F = 1 THEN 1014

1140 STOP

repeats the process until the output is stable (ie there were no changes during this pass).

The following subroutine prints the results:

2000 REM PRINT

2010 PRINT"": REM CLEAR SCREEN CHARACTER 2020 FOR I = 1 TO S

2030 FOR J = 1 TO S

2040 IF A(I,J) = 1 THEN PRINT "A";:GOTO 2060 2050 PRINT"":

2060 NEXT J

2070 PRINT 2080 FOR J = 1 TO S

2090 IF B(I,J) = 1 THEN PRINT "B";:GOTO 2110

2100 PRINT

2110 NEXT J

2120 PRINT

2120 NEXT I

2140 RETURN

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7406	40p	7432	27p	7492	52p	74161	99p	74193	€1.38
7408	18p	7440	18p	7493	39p	74164	£1,12	74195	£1.03
7410	16p	7442	73p	7496	97p	74165	£1.12	74196	£1.00
7411	22p	7447	75p	74107	35p	74166	€1.60	74221	£1.75
7412	24p	7473	35p	74121	29p	74170	£2.48	74H00	35p
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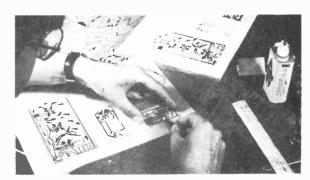
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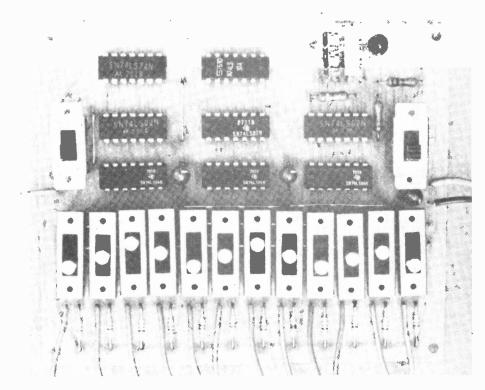
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LOGIC TRIGGER

No need to be in the dark any more, see your pulses, doing their stuff before your very eyes.

WHEN USING AN oscilloscope to examine or fault find digital circuitry, it is often desirable to see what happens just before a pulse or edge occurs. An example of this is when measuring the propagation delay in a ripple counter. Here it is easy to trigger on the last output but the edge of the counter input which initiated the change in the output may have occurred over 100 ns earlier. Even with the delay line built into modern oscilloscopes the edge is too early to see.

Triggering on the input waveform allows this edge to be seen but if the output pulse occurs only once every thousand or so pulses it will not be seen. With this unit, the output of all the stages in the divider can be examined and a pulse can be generated anywhere in the cycle. By selecting a pulse very close to, but before, the edge in question and using it to trigger the oscilloscope (use ext trigger) both the clock waveform and output waveform can be see n.



SPECIFICATION

Modes Asynchronous or synchronous

No. of inputs 12 address, 1 clock

Pulse extension mono 10 ms

Pulse indication LED

Minimum pulse detectable <40 ns
Propagation delay <45 ns

Trigger (synchronous) positive or negative edge of clock input

Set up time (synchronous)
address to clock
<40 ns

logical "1" when input agrees with switch

Output logical "1" when input agrees with switch setting and/or clock (synchronous only)

Power requriement +5V @ 50 mA

With the advent of microprocessors it has become increasingly difficult to fault find as things happen (e.g. the CE input to a memory may go low) only when a particular address is given. As the address bus is always in motion it is almost impossible to trigger the scope on any one address. Again with this unit the address bus is interrogated along with the necessary write or read lines, and its output can be used to trigger the oscilloscope only when the correct sequencer is received.

Construction

We mounted all the components on the board including the switches. The only difficult (fiddly) bit is the writing of the three position slide switches which have to be preassembled before fitting to the pcb. The wiring is shown in fig. 3.

To aid this we have provided 12 holes in the pcb the size of the toggle of the switches; if the

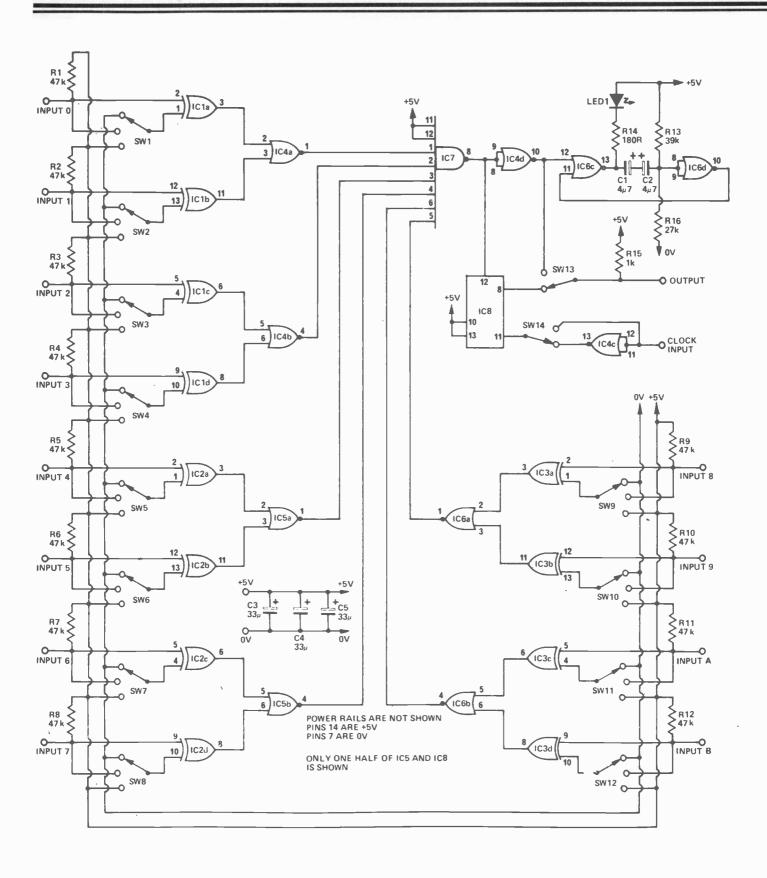


Fig 1. Full circuit diagram of the logic

unit.

PARTS LIST

RESISTORS R1-R12 R13 R14 R15 R16	all ½W, 5% 47k 39k 180R 1k 27k
CAPACITORS C1,2 C3-C5	4µ7 25Velectro 33µ 16V tantalum
SEMICONDUCTORS IC1-IC3 IC4-IC6 IC7 IC8	74LS86 74LS02 74LS30 74LS74
LED1	Red LED
MISCELLANEOUS PC board ETI 141 Twelve 3 position slide Two 2 position slide Front panel Box to suit	

Fig 2 (right): Foil pattern shown full size.

HOW IT WORKS

The twelve inputs are compared to the levels set on the slide switches SW1-SW12 by the exclusive OR gates IC1-IC3. These ICs have a high output only if the two inputs differ. If they are the same, either both low or both high, the output will be low. If the two inputs are joined together, as when the switches are in the don't care position, the output will always be low.

The outputs from the exclusive OR gates are combined in pairs by the NOR gates IC4-IC6. If the 12 input signals match the preset selection, the output of all 6 NOR gates will be high. If any one is not in agreement with the selection one or more of the NOR gates will have a low output.

These NOR gate outputs are combined by IC7 which is an eight input NAND gate. The output of this gate will low only if all 12 inputs match. The output of this IC is inverted by IC4/d to provide the asynchronous output.

This output also triggers the monostable formed by IC6/c and IC6/d. This gives a 10 ms long pulse of light the LED indicationg a pulse was received. If it is a steady state signal the LED will stay on.

The output of the NAND gate, IC7, also joins the data input of IC8 (D type flip flop). This IC is toggled on the positive edge of the clock waveform transferring the data to the output. This is the synchronous output. To allow for either positive or negative synchronization an inverter is used on the clock input and either polarity can be selected by SW13.

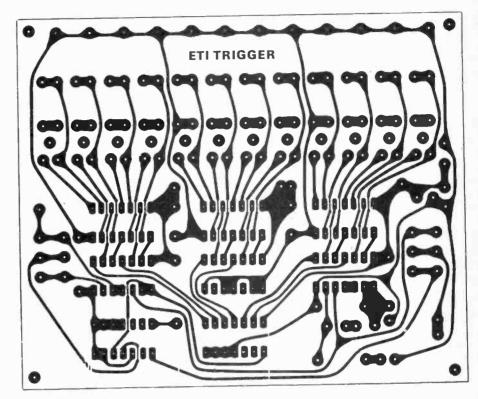
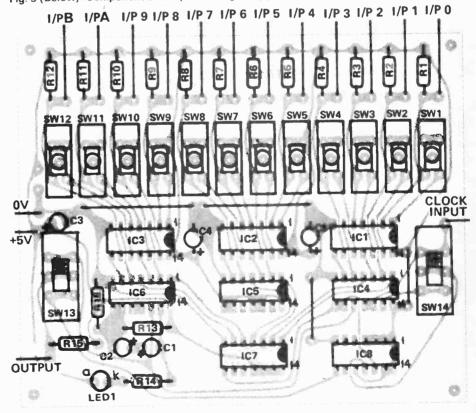


Fig. 3 (Below). Component overlay of the logic trigger



switches are initially placed upside down in these holes the board will act as a template to provide the correct spacing. We have also used two wires of the switch to provide mechanical support. While only a single pole switch is needed the

only ones readily available are two pole.

The switches can now be mated to the PC board with the two longitudinal wires being terminated in the holes provided at the end of the switch bank.

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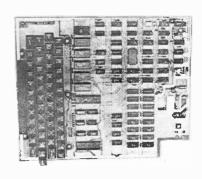


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Commands	LIST	NEW	NULL	RUN	
Statements CLEAR GOTO NEXT	DATA GOSUB ONGOTO	DEF IFGOTO ONGOSUB	DIM IFTHEN POKE	END INPUT PRINT	FOR LET READ
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WHO NEEDS ELECTRONICS?

K. T. Wilson explores the all too frequently ignored and misunderstood field of Magnetic Amplifiers.

THINK OF AMPLIFICATION, and you automatically think of transistors. Perhaps if you're a bit longer in the tooth you remember valves. Have you ever thought of large amounts of power gain being obtained without using either transistors or valves? It's power gain we're talking about, too, not just voltage gain. A transformer will give voltage gain, up to 100 times, but at the expense of current, so that the power out is never quite as much as the power in. There's no power gain there, but a device called the magnetic amplifier, which looks very like a transformer, can give very large values of power gain, can control AC power into a load very smoothly, and is used in the sort of applications where thyristors would be a natural choice for many.

The magnetic amplifier has been used in industrial control for decades, yet has never really caused any stir of interest anywhere else. Perhaps it's because it's always a ready-made item, but then so is an IC amplifier, and everyone seems to make use of those. Perhaps it's just because so very few people outside the ranks of professional engineers know just what a magnetic amplifier is. Let's remedy that!

Induced Knowledge

To start with, we need a pretty clear idea of what happens inside an inductor. A simple inductor has a winding which consists of insulated wire wound round a core of a soft magnetic material. Soft doesn't mean that you can spread it on your bread, but that the material magnetises easily, and demagnetises just as easily. Take a piece of this material, hold a magnet near it, and it's magnetised. Take a magnet away and it's demagnetised. This material we use for the cores of inductors, transformers, electric motors, relays etc.

An inductor makes use of this 'soft' magnetism. The winding has an alternating current flowing in it. This alternating current (changing smoothly from a peak in one direction to a peak in the opposite direction and back) causes the core of the inductor to magnetise. The magnetism isn't steady like a bar magnet, but alternating, which is the point of using soft magnetic material. a graph of the magnetism (called flux density) of the core plotted against time would, ideally, have exactly the same shape as that of the waveform of the AC applied.

So far so good — it's an alternating magnet. But we've known for about $150\ \text{years}$ (or someone has) that

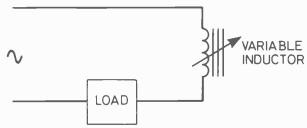


Fig. 1. Control of a load using a variable inductor, this configuration has very little power lost as heat, unlike a resistive controller.

wherever there's an alternating magnetic field, any piece of wire or other metal will have an alternating voltage induced.

Stick a piece of wire near your alternating magnet and you'll find an alternating voltage across the ends of the wire. The voltage is small if you use just a few centimetres of straight wire, but if you wrap several metres or wire round the core, so that all the magnetism of the core is at the centre of the coil of wire, then you find quite a respectable amount of AC. Recognise it?, a transformer.

Laying Down the Laws

The laws of Electricity are very consistent, though, Any coil of wire around a core that has an alternating magnetic field will have an AC voltage induced. That means that if we have only one coil, and we send AC through to generate the magnetism, it will also have an AC voltage induced in it. This voltage which the text books call a "back EMF", opposes the current which causes the magnetism which causes the voltage.

Result?

It's a darn sight more difficult to pass AC through an inductor than it is to pass DC!.

When we use an inductor in a DC circuit, then apart from some effects at the moments of switch-on and switch-off the thing behaves like a resistance, good old Ohm's Law and all the rest, and a fairly low value of resistance at that.

Now you might think that it should pass the same amount of current for AC as for DC, but it doesn't.

Imagine that the resistance is 2R, so that 10 V DC passes 5 A. Apply 10 V AC and the current's nothing like 5 A. It's not because Ohm's law stops working, it's because of the induced voltage. We're trying to push AC

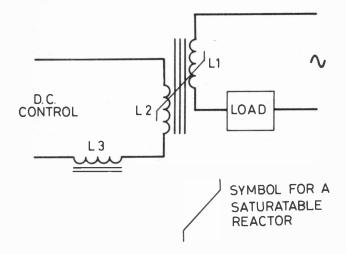


Fig. 2. Simple magnetic amplifier circuit, showing DC control winding.

through with one voltage, and the induced voltage is opposing our efforts. It's only the difference between the two voltages that has any effect at all.

Impedance Impediment

Suppose for example, that with 10 V AC applied, the induced voltage is 9V9. This makes the difference equal to 0V1, and the current is

$$\frac{0.1}{2} = 0.05 \text{ A}$$
, (by Ohm's Law)

Now these are calculations we seldom bother to make. Instead we measure a quantity called the self-inductance, L, of the coil and use this quantity and the resistance value to calculate impedance, which is the ratio

for the coil. In our example, 10 V causes 0.05 A to flow, making the impedence 10/.05 = 200 R, not a particularly large impedance, but much greater than the resistance of 2 R.

The useful thing about an impedance is that there's practically no loss of power in it. Pass a current through a 200 R resistor, and you lose energy in the form of heat the amount of heat lost per second is $200 \times (\text{current})^2$ joules for a 200 R resistor. The same current through the inductor in our example doesn't look anything like this — only its resistance loses heat, and that's only $2 \times (\text{current})^2$ joules, because the resistance is only $2 \times (\text{current})^2$.

We can therefore use an inductor to control the flow of AC in a circuit (see Fig. 1) with none of the power loss that a resistor would cause. Now if we could just have a variable inductor, we could be very neatly control the flow of current in that circuit. Of course, we could use an inductor with tapped turns and slide contacts, built like a potentiometer, and we make use of just such a device, the familiar Variac. It's possible though, to control the inductance of a winding with no mechanical movement at all, and what makes it possible is the effect called saturation.

Control-A-Coil!

When we send a current, AC or DC, through a coil of wire which is wound round a magnetic core, we can't pass as much current as we like and expect the magnetism to keep pace. At some stage in the game the core saturates, which means that it's as magnetised as it's ever going to be, no matter how much current is used. Now when a core is saturated like this, a change of current doesn't cause a change in the magnetism, so there's no more induced voltage. In other words, the inductance is no more and the impedance is practically zero.

Let the AC flow to it's load through an inductor whose core we can cause to saturate. How? By passing DC through another winding, by making the core of material which saturates easily, and the making the core continuous with no air gap.

That's our recipe for a magnetic amplifier.

Amps For Amps

Figure 2 shows a simple magnetic amplifier circuit. The inductor L1 has a large inductance when the core is not saturated, because of that, its impedance is very large, enough to make the current in the circuit very small. Now let DC flow through the second winding L2, and the core saturates.

If we can keep the core saturated for the whole of the AC cycle, then the inductance of L1 is almost zero, and the full amount of AC current flows through the load.

We don't of course, have to switch between saturation and no-saturation. We can adjust the control current so that the core saturates only on half of the AC cycle, or in peaks so that the average current through the lead is controlled.

Self Satisfied

Even such a simple magnetic amplifier has a lot of advantages, such as low power dissipation and high power gain, but better results are possible by using what is called a self-saturating design. Self-saturation is a form of positive feedback, using some of the signal current to assist the DC control current. Fig 3 shows a half-wave self-saturating circuit. The rectifier D1 ensures that only one direction of current flows through the coil L1 and the rated load current will cause the core to be close to saturation. The DC control current in winding L2 need only be quite small to cause the core to saturate on peaks, so that less power is needed to control the load current, and power gain is much higher.

Only half cycles are passing into the load, however, so that a full wave version is more desirable.

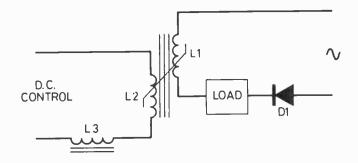


Fig. 3. Half-wave control using self-saturation.

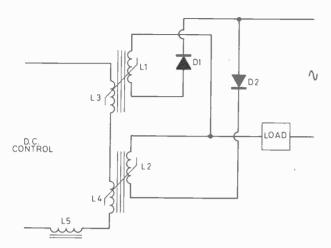


Fig. 4. Full-wave amplification with self saturation, by positive feedback.

A full-wave self-saturating magnetic amplifier is shown in Fig 4. Two sets of windings are used, each handling half of the wave, with rectifiers ensuring that the AC wave is split into its two halves.

In all these circuits, an additional inductor is used in the DC control line to prevent AC appearing in the control circuit because of transformer action.

Going Straight

DC amplification? Simple enough, just rectify the output of the magnetic amplifier — the self-saturating full wave type already has two rectifiers included in the circuit and only two more are needed. More sensitivity? Add another winding to pass DC bias current, and the sensitivity increases because the bias can be set so that the core is very close to saturation.

Nothing could be that perfect, there has to be a snag somewhere, and response time is it for magnetic amplifiers. Being slow beasts a sudden change of control signal may not cause much change in the output current until several cycles of AC have passed through. Nevertheless for stabilising AC supplies, for control of large AC loads and for high power gains magnetic amplifiers are not so easily displaced by electronics. There's not much to go wrong, they can be built to order, and they can be repaired.

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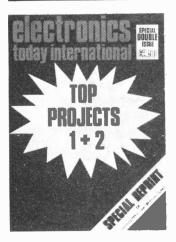
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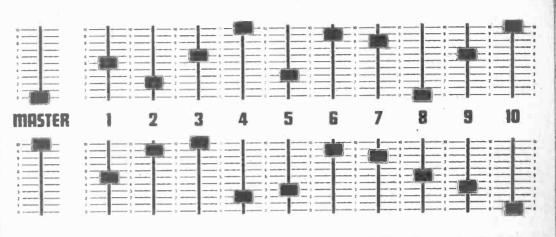
The first types of dimmer used, of which there are still some examples in older theatres, was a variable resistance type which used either a variable or switched power resistor in series with the load. With small loads a wire wound resistor or a carbon pile was used while larger loads used a tank of saline solution with a central

electrode which was raised or lowered in the liquid, effect vely changing the resistance. This type of dimming, while reasonably effective, dissipated a lot of power which made life uncomfortably hot for the operator, since to minimise mechanical linkages the dimmers themselves were often in the control room.

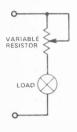


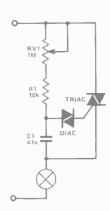
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Electronics

With the advent of electronics, life was a little bit easier. The use of phase controlled dimming using thyratrons and later SCRs and Triacs reduced the heat dissipation dramatically (if you'll excuse the pun) and also allows the control to be physically separate from the dimmer. Besides being easier for the operator performances were greatly enhanced by the much better control available.

Today the use of phase control is almost universal as it is simple, reliable and cheap. Another method in use today is by magnetics; this type has the advantage of generating no RFI but unfortunately is

expensive.

The problem of RFI is common to all phase control circuits, but can usually be reduced to acceptable levels by the use of a choke and several capacitors. For RFI the choke need not be very large, but one other effect of phase control is the audible rattling of the lamp filament (especially with the larger globes) which is due to the sudden application of power, and the magnetic field so produced, each half cycle. This can be cured by reducing the rate of the rise of current by using a larger choke.

Type Casting

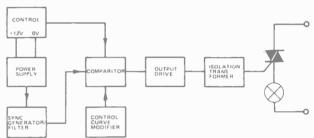
We have given some schematic diagrams of types of dimmers which have been used previously. Fig. 1 is the oldest type comprising simply a variable resistor in series with the load. The second (Fig. 2), probably the most common type in use today (mainly in homes) is very simple but lacks the versatility needed for theatrical work.

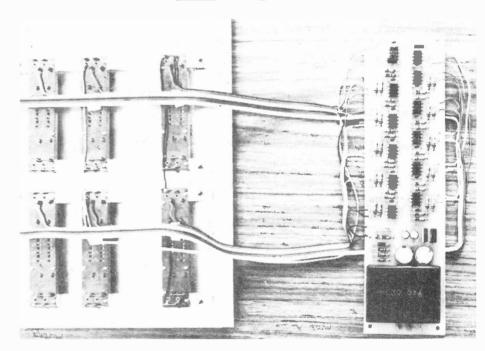
The third type (Fig. 3) is in common use and while still very simple does have many good features. These include having the

Fig 1. (Far left). The earliest type of dimmer employing just a variable resistor controlling the load.

Fig 2. (Left). Common! The most usual kind of light dimmer in use today.

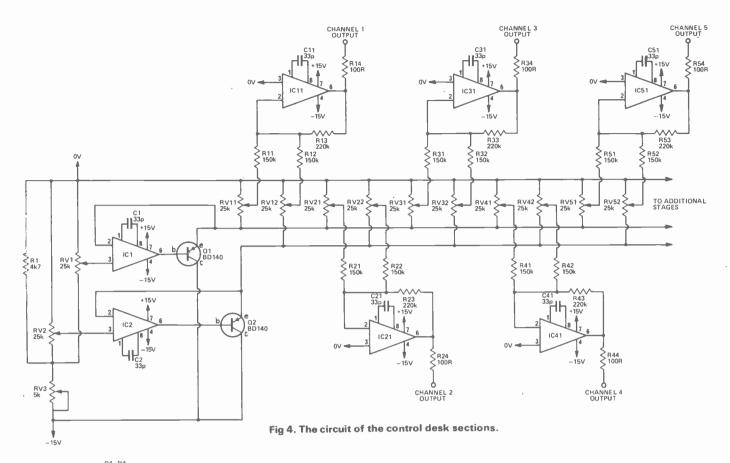
Fig 3. (Right). A more refined realisation of the art, which at least has the control isolated!





control potentiometer isolated from the mains voltage and also a modified control curve to give a better input-output voltage relationship. Synchronization is referred to the zero crossing of the mains voltage, making the unit more suitable for driving inductive (fluorescent) loads; this also eliminates hysteresis which occurs with the simple dimmers.

The dimmer to be described here is more complex than most but a great deal of effort has been taken to ensure that all problems have been solved. A low pass filter, with phase



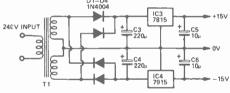


Fig 5. Power supply circuit

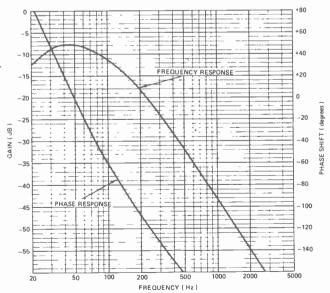
HOW IT WORKS ~ CONTROLLER

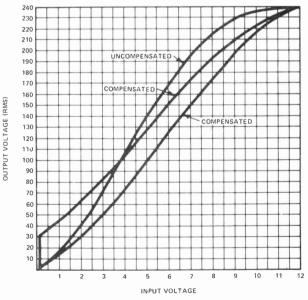
There are two controls for each dimmer along with two master controls. The master controls vary the voltage on the individual level control potentiometers from 0 V (no light) to -8 volts (full light). Normally one master will be at maximum and the second at zero. The outputs of the two controls for each dimmer are added by an operational amplifier, referred to 0 V. As one set of potentiometers has 0 V on both of its ends it

can be varied without changing the output allowing it to be set for the next scene. By varying the master controls together, but in opposite directions, the complete lighting set up can be smoothly varied from one scene to the next.

As we need +12V out to drive the dimmers the supply voltage of the control desk is ± 15 volts.

Fig 6. (Below). Showing the phase v frequency responses effect of compensation upon response





PARTS LIST

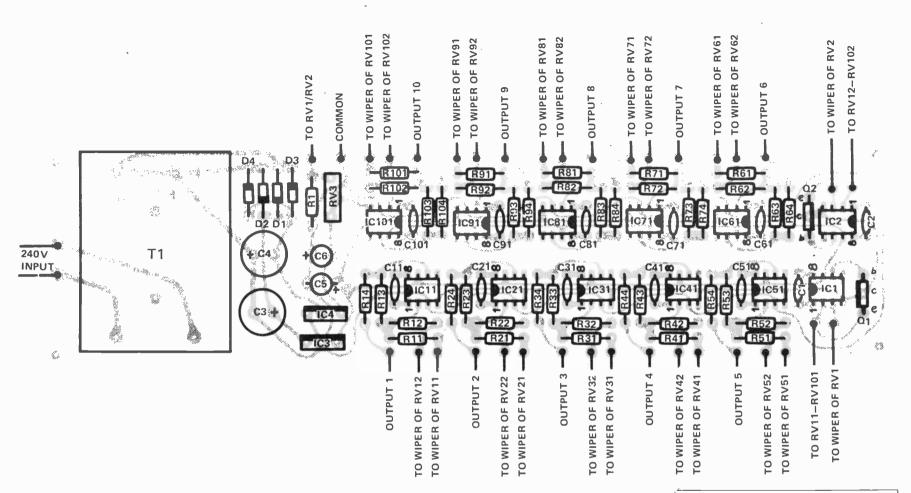
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Fig 7. (Right): Component Overlay for the Controller Module.

BUYLINES

Apart from the pulse transformer T1—for details of which see Table One—none of the components in this (admittedly huge) project should tax your local supplier overmuch. If you send us an SAE we will send you the foil patterns for the PCBs used here, as they were simply too big to print full size.

Any 400V ten or twenty amp triac will probably serve if you can't find the specified type easily.



correction, is used to ensure accurate synchronization. The control curve is also modified to give a subjectively more linear response and it has the ability to drive a fluorescent load without requiring a ballast resistor. Both the maximum and minimum light levels are adjustable without interaction giving reliable and predictable output. This is especially necessary if a dimmer fails for some reason and is replaced by a spare unit.

The Protection racket

The protection of SCRs and Triacs, especially Triacs, is usually difficult as they tend to fuse faster than the fuse purportedly protecting them. The use of a cheap Triac which requires an expensive fuse to protect it is false economy. We have used a large rugged Triac (40 A device for the 20 A dimmer) which allows economical fuses to be used, especially for the 10 A version.

On the control side we will be describing a panel with two sets of long sliders per dimmer with two master controls which allow the next scene to be set up then faded in when required. A digital memory which can 'prerecord' scenes and recall them on demand may be published later.

Dimmer Module — Construction

Assemble the boards with the aid of the overlay. The heatsink should be drilled and tapped for the triac to allow easy replacement if ever necessary. Note that the mounting of the fuse is different for the 10 and 20 A dimmers.

The choke is bolted onto the PCB using the long clamping bolts, preferably using rubber gremmets in the holes in the board (they may have to be drilled out to do this). The leads from the choke should be bent such that they go into the holes provided without going near the mounting bolts which are at earth potential. The leads can now be soldered (both sides on the 20 A unit).

The pulse transformer can now be added according to Table 1 Be careful when winding this transformer not to damage the insulation on the wire as there is 240 V between windings. We also recommend some epoxy between the transformer and the board.

The printed circuit boards for the two versions of the dimmer board are identical in layout and differ only in that the connector end of the 20 A board is double sided to present a greater area of contact with the connectors.

Controller-Construction?

The component numbering system used on the controller drawings is designed to indicate which channel a particular component is part of. The printed circuit board drawing for the dimmer board is too large to publish in the magazine at full size; however, the pattern is available from our offices for the cost of an SAE — a large SAE!

If the diffmer modules are not required to be connected through sockets, the total cost can be reduced by connecting directly to the modules and mounting them in a box. In the 20 A unit the heavy wires should be bolted on to the appropriate pads to ensure contact to both sides of the board.

One more modification to the control desk is the addition of a black-out switch which allows all lights to be blacked out without moving the master control. This is simply done by switching the supply voltage on the master potentiometers from the 8 V supply as set by RV3 to OV. RV3 should be adjusted such that with one master at maximum, the second at minimum and one

individual control at maximum that its output voltage should be +10 volts.

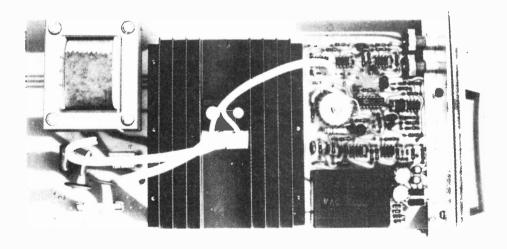
Setting up

With the dimmer module the trim potentiometer has to be adjusted so that the output pulse from IC7 occurs at the very end of each half cycle. This is easiest set using an oscilloscope although an approximate setting can be made without one.

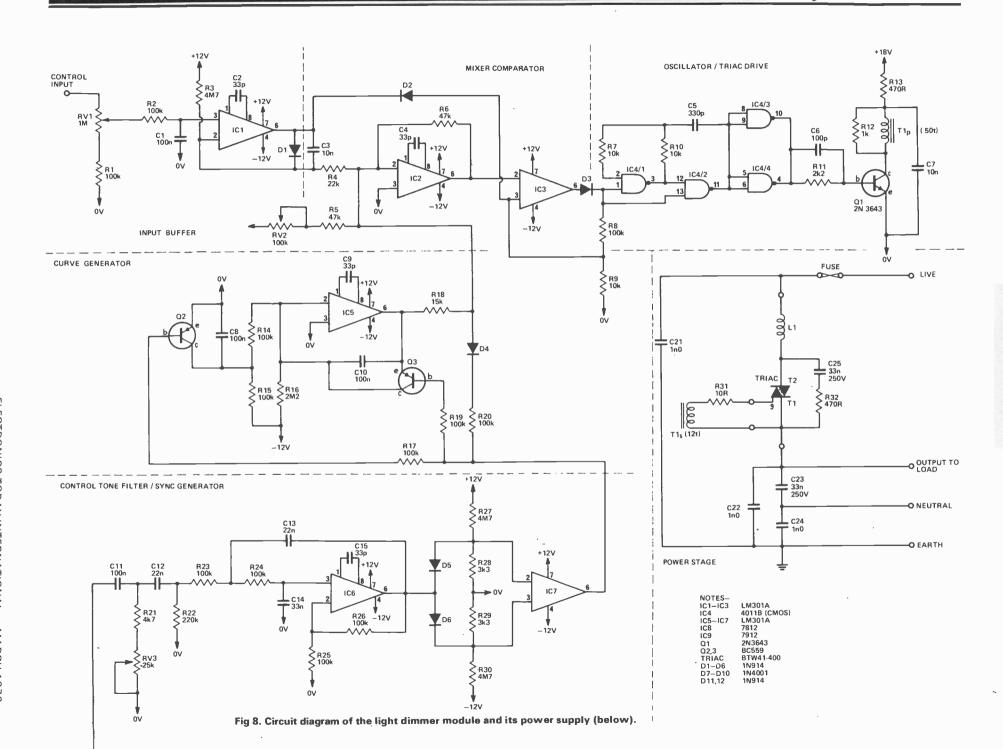
If the dimmer is connected up to a reasonably heavy load and adjusted for about 1/3 level it will probably be found that with RV3 at one end the light level is not stable and tends to flash. This is caused by the sync pulse occurring after the end of the half cycle and the trigger pulses from the previous half cycle triggering the next. The trim potentiometer RV3 should be turned back about ½ turn from the position at which this effect stops.

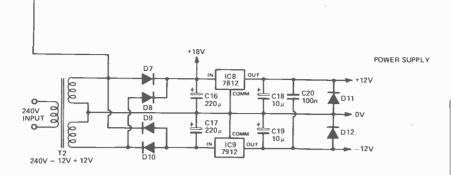
Max and Min

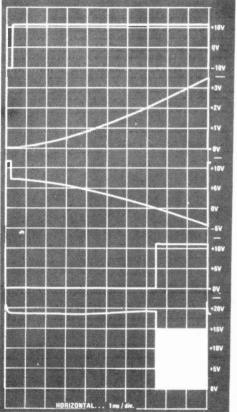
When adjusting the maximum and minimum levels the minimum should be adjusted first. Note that the control potentiometer must be slightly up off zero to get any light and minimum should be adjusted at this point. The maximum should be adjusted with both the master and individual control at maximum and set to the point where the light level is just starting to drop.



Shown above is a completed dimmer module







output (IC4), transformer drive

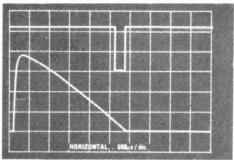


Fig 10. Relationship between the end of half cycle and the sync pulse.

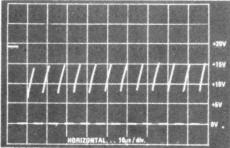


Fig 9. Waveforms shown are: Fig 11. An expanded view of the Sync pulse (output IC7), curve drive waveform showing Q1 generator (output IC5), mixer collector voltage. output (output IC2), oscillator

HOW IT WORKS ~DIMMER MODULE

be broken into seven sections.

1. Power supply

This is a simple full wave rectifier which gives about ± 18 V after being filtered by C16 and C17. Using 3 terminal regulators this is reduced to ± 12 volts which is needed for the circuitry.

2. Control tone filter and sync generator

As the name implies this removes the control tones that the supply authority superimposes on the mains voltage. These are normally about 1050 Hz and can cause problems by upsetting synchronization of dimmers. The filter is a low pass type comprising IC6 and associated components. As filters always alter the phase relationship this is corrected using phase shift networks, C11/R21 and C12/R22. Potentiometer RV3 is used to ensure the phase shift is zero (at 50 Hz) with normal component variations. If the output of IC6 is between +0.6 volts and -0.6 volts. neither D5 nor D6 will be forward biased sufficiently to change the input voltages to IC7 so its output will be -10 volts. As the output voltage of IC6 is a 'clean' 50 Hz sine wave of about 6 volts amplitude this will only occur at a small region about the zero crossing point. At all other times the output of IC7 will be + 10 volts. The result is a negative pulse, about 250 us wide at the zero crossing point of the 50 Hz.

3. Curve generator

This produces the output shown in Fig. 6. When the sync pulse occurs, transistors O2 and O3 discharge capacitors C8 and C10. R16 charging C10. However, while initially the voltage across R14 is zero and therefore does not affect the charging of C10, as C8 begins to charge due to R15 its effect becomes more and more dramatic. A curve is necessary as it gives a better input/output 7. Power stage voltage relationship but the curve must be This is simply a triac with a choke in series to reproduceable hence the circuit used.

4. Input buffer

This serves two purposes; firstly, it allows a prevent RF1.

To help explain the operation the circuit can megohm input impedance and secondly it detects when the input voltage falls below 0.1 volt and turns the dimmer output completely off. This allows the minimum light control to be turned up to give a better control range, ie with the filaments just glowing, yet have them off if the control voltage is reduced to

If the voltage is above 0.1 volt, the diode D1 will lift the voltage on pins of IC1 to equal that of the input on pin 3. However if the voltage falls below this level, the voltage on pin 2 will remain at about 0.1 volt due to R3 and the output of IC1 will go to about -10 volts.

5. Mixer-comparator

IC2 mixes the input voltage, the output of the curve generator the sync pulse and the minimum adjustment potentiometers. This gives the waveform shown in Fig. 2 with the input voltage and the minimum adjustment only moving the curve up and down without altering the shape. When the output of 1C2 falls below zero volts the output of IC3 goes from -10 V to +10 volt with D3 and R8/9 providing about I volt of positive feedback. The voltage has to rise to above IV to force the output back to -10 volts. The diode is necessary to ensure that the voltage at the input of the oscillator IC4 remains within the supply voltage of the IC (+12 V, 0 V).

6. Oscillator/triac drive

A CMOS oscillator 1C4 is used to drive O1 which supplies the energy for the pulse transformer T1. The oscillator will only operate when the control inputs (pins 1 and Immediately on release of the sync pulse the 13) are +10 V. The frequency is controlled by output of IC5 begins to ramp up slowly due to C5 and is set at about 150 kHz. Resistor R13 provides current limiting for the pulse transformer while R12 prevents the reverse voltage damaging Q1 if the load on the secondary load (the triac) becomes disconnected.

prevent both RFI and 'filament rattle' and a fuse to protect against short circuits. Capacitors are also used as bypasses to help

(Q1).

T2 Fig 12. Component Overlay for the dimmer module board. Both the 10A and 20A versions are identical in layout, but the 20A is double sided to aid dissapation. TRIAC LIVE +12V CONTROL INPUT NEUTRAL

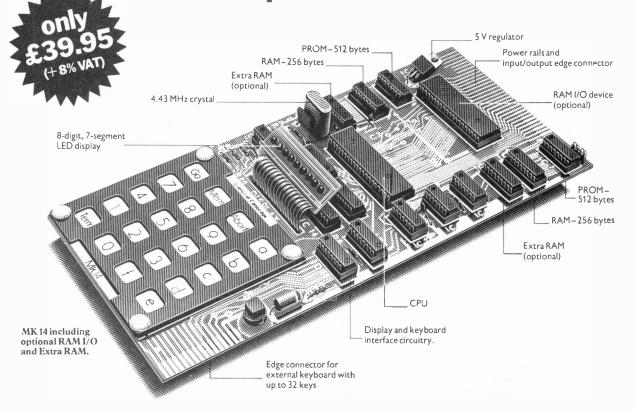
PARTS LIST

	· · · · · · · · · · · · · · · · · · ·
RESISTORS all ¼W 5%	
R1,2,8,14,15, 17,19,20,23-26, R3,27,30 R4 R5,6 R7,9,10 R11 R12 R13 R16 R18 R21 R22 R28,29 R31 R32	100k 4M7 22k 47k 10k 2k2 1k 470R IW 2M2 15k 4k7 220k 3k3 10R 47R 1W
POTENTIOMETERS	
RV1 RV2 RV3	1 M linear 100k linear 25k trimmer
CAPACITORS	
C1,8,10,11,20 C2,4,9,15 C3,7 C5 C6 C12,13 C14 C16,17 C18,19 C21,22,24 C23,25	100n polyester 33p ceramic 10n polyester 330p ceramic 100p ceramic 22n polyester 33n polyester 220u 25V 10u 25V 1n polyester 33n 250V AC
SEMICONDUCTORS 1C1-3,5,6,7 1C4 1C8 1C9 Q1 Q2,3 TRIAC D1-D6,11,12 D7-D10	LM 301A 4011B 7812 7912 2N3643 BC 559 BTW41/400 1N 914 1N 4001
MISCELLANEOUS	
TI see text, T2 24V, 5VA, hand fuse 10A or 20A to suit	neatsink and choke it, fuse holders.

TABLE ONE

The pulse transformer T1 is the most difficult component in the project to find or produce. Tandy market a 4:1 device and this must be first choice. If this, and all other, commercial units prove elusive — try winding it yourself onto an ferrite ring of about 2in outside diameter, using 50 turns and 12 turns for the windings to obtain the required ratio. Some experimentation may be needed here in order to get the triac to fire properly, and we do not recommend you try this unless you have wound coils previously.

From Science of Cambridge: the new MK 14. Simplest, most advanced, most flexible microcomputer-in kit form.



The MK 14 is a complete microcomputer with a keyboard, a display, 8 x 512-byte preprogrammed PROMs, and a 256-byte RAM

programmable through the keyboard. As such the MK 14 can handle dozens of user-written programs through the hexadecimal keyboard

Yet in kit form, the MK 14 costs only £39.95 (+£3.20 VAT, and p&p)

More memory - and peripherals!

Optional extras include:

- 1. Extra RAM 256 bytes.
 2. 16-line RAM I/O device (allowed for on the PCB giving further 128 bytes of RAM.
- 3. Low-cost cassette interface module which means you can use ordinary tape cassettes/ recorder for storage of data and programs.
- 4. Revised monitor, to get the most from the cassette interface module. It consists of 2 replacement PROMs, pre-programmed with sub-routines for the interface, offset calculations and single step, and singleoperation data entry.
- 5. PROM programmer and blank PROMs to set up your own pre-programmed dedicated
 - All are available now to owners of MK 14.

A valuable tool—and a training aid

As a computer, it handles operations of all types - from complex games to digital alarm clock functioning, from basic maths to a pulse delay chain. Programs are in the Manual, together with instructions for creating your own genuinely valuable programs. And, of course, it's a superb education and training aidproviding an ideal introduction to computer technology.

SPECIFICATIONS

 Hexadecimal keyboard ● 8-digit, 7-segment LED display • 8 x 512 PROM, containing monitor program and interface instructions ●256 bytes of RAM ● 4 MHz crystal ● 5 V regulator • Single 8 V power supply • Space available for extra 256-byte RAM and 16 port I/O • Edge connector access to all data lines and I/O ports

Free Manual

Every MK 14 kit includes a Manual which deals with procedures from soldering techniques to interfacing with complex external equipment. It includes 20 sample programs including math routines (square root, etc), digital alarm clock, single-step, music box, mastermind and moon landing games, self-replication, general purpose sequencing, etc.

Designed for fast, easy assembly

The MK 14 can be assembled by anyone with a fine-tip soldering iron and a few hours' spare time, using the illustrated step-by-step instructions provided.

How to get your MK 14

Getting your MK 14 kit is easy. Just fill in the coupon below, and post it to us today, with a cheque or PO made payable to Science of Cambridge. And, of course, it comes to you with a comprehensive guarantee. If for any reason, you're not completely satisfied with your MK 14, return it to us within 14 days for a full cash

Science of Cambridge Ltd, 6 Kings Parade, Cambridge, Cambs., CB2 ISN. Telephone: Cambridge (0223) 311488

To: Science of Cambridge Ltd, 6 Kings Parad Please send me the following, plus details of oth MK 14 Standard Microcomputer Kit # £43.5 Extra RAM # £3.88 (inc p&p.) RAM I/Odevice # £8.42 (inc p&p.)	er peripherals:
I enclose cheque/money order/PO for L	(indicate total amount.)
NameAddress(please print	Science of Cambridge

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	-			CHC			N	LS					Static RAM's	1+	17-6			2.
400	.13°	LS .19'	7476	.30°	LS .29'	74170	1.85	1.65	4000	.15*	4077	.211	2102A (350ns)	1.05	.95		LM345K L129/30/31	8.
101	.13	.19	7478	.30	.29'	74173	1.41	.88	4001	.16"	4081	.21'	2102A-2 (650ns)	1.29	1.15 2.19		L129/30/31	
02	.15	.19	7482	.731	-	74174	1.01	1.05"	4002	.16"	4082	.21'	2111A-1 (500ns)	2.46	1.90		I.C's	
03	.15'	.19"	7483		.75	74175	.81"	1.05"	4006	.92"	4085	.92	2112A-2 (250ns) 21L02 (350ns)	2.14 1.07	.96		CA3080	
04	.16	.211	7485	1.18'	.88	74176	1.01	- 1	4007	.18	4086	.92"	MM5257 (TMS4044)	8.10			CA3080 CA3130E	3
05	.16'	.211	7486	.25	.29"	74177	1.01	- 1	4008	.92*	4093	.81'	21 14 (450ns)	8.10	2.12	6.75	CA3140E	
06	.26"	- 1	7489	2.60'	·	74180 74181	1.01° 2.21°	2.99	4009 4010	.54	4099 4502	1.81	6810	3.50		2.52	LM301AN	
07	.26*	-	7490	.34'	.62	74182	.81	2.99	4011	.18		2.46	Dynamic RAM		8251	5.97		
08 09	.17	.19'	7491 7492	.73 .46	1.05°	74184	1.81	= 1	4012	.18		1.07	4116	12.75	8253	8.10	LM348N	
10	.15	.19	7492	.34	.65'	74185	1.62	1	4013	.48	4511	.95*	CPU's		8255	5.51	LM380N	
11	.25	.19'	7495	.54*	.88	74188	2.97	- 1	4014	.92"	4514	2.70	8080	5.95*	Regulators		LM381N	1.
12		.19	7496	.67	1.85	74189	3.17	2.25	4015	.92	4515	2.70"	6800	8.99"	78L series		LM382N	1.
13	.27	.40	74107	.27	.35	74190	1.211	.75	4016	.43'		1.07	9900	42.50	+(POS) 100mA		LM3900N	
14	.711	.79	74109	.44"	.351	74191	1.211	.75	4017	.81		4.10	E-Prom's UV		5v. 6v. 8v. 12v		LM3909N SN76001N	1.
15	- 1	.19"	74112	-	.351	74192	1.21'	1.85	4018	.92	4518	.95	1702AQ	5.75	All 30p' each		SN76003N	2.
16	.25	- 1	74113	_	.35'	74193	1.21	1.85	4019	.56	4521 4522	2.54° 1.89°	2708Q	7.87	78M series		SN76013N	1.
17	.34"	Ξ.,	74114		.35*	74194 74195	1.211	1.05	4020	.92		1.89	TriState Buffers 81LS95	.75	+ (POS) 500m/		SN76023N	1.
20	.16'	.19"	74121	.27'	75.	74196	1.18	1.05	4022	.92	4528	.92	81LS96	.75		. 1,5v. 20v & 24v	TBAB 10AS	
21 22	_	.19'	74122	.50	.75°	74197	1.18	1.05	4023	.18'		7.12	811597	.75'	All 60p' each		TCA940	1.
22	.25*	.19	74123	.60	1.25	74198	1.81	- 1	4024	.65	4536	3.74	81LS98	.75'	79M series —(NEG) 500m/		ZN 4 1 4	
25	.25	= 1	74125	.51'	.39	74199	1.81*	-	4025	.18"	4543		74365	.75		. 15v. 20v & 24v	, ZN424E	1.
26	.25	.191	74126	.511	.391	74221	-	.991	4026	1.84	4553		74366	.75	All 85p' each		ZIN425E	3
27	.39*	.19"	741.32	.78	.65'	74240		.25	4027	.51		1.51	74367	.75	78 series		ZN459CT ZN1034E	3.
28	.38	.21	74133	_	.19'	74241	400	2.25	4028	.70	4583		74368	.75'	+(POS) 1A		ZN 1034E ZN 1040E	8
30	.16"	.19'	74136	_	.39'	74242	_	2.25	4029	1.18	4585	1.07	Buffers	1.65	5v. 8v. 12v. 15	iv. 18v & 24v	ZNA116E	6
32	.25	.25	74138	_	.55*	74243 74247	=	.95	4030	1.08	1.C.		8T26P 8T28P	1.65	All 85p' each		LIVATIVE	-
33		.28*	74139	70:	.55	74248		.95	4034	1.89	SOC		8T95P	1.49	79 series		The items show	i m abio maluo.
37 38	.25*	.25	74141	.76°	1.05	74249		.95	4035	1.06	DIL		8T96P	1.49	—(NEG) 1A	10. P. 24.	iust a small se	
40	.17'	.19	74147	1.59	1.03	74251	_	.83	4040	.92"	8pin 14pin	.10	8T97P	1.49*	5v, 8v, 12v, 15 All £1.00* each		our new 78 / 7	
41	.70		74149	1.38	_	74253	_	.99	4042	.70	16pln	.131	8T98P	1.49	MILET.OU GALII		is now avail	
43	.50	.55'	74150	1.08	- 1	74257	_	.99*	4043	.81	18pin	.18'	Interface		uA723 (OIL)	.40	everything fro	m Resistors to
45	.60*	= 1	74151	.67*	.88	74258	_	.99	4046	1.06	20pin	.20	8212	2.21	L200	1.99	. Idiesi III Iviici	o-processors. [
46	.60	- 1	74153	.67	.48	74259	_	1.50	4049 4050	.43	22pin	.24"	8216	2.35	LM304H	2.40		our copy today
47	.60	.87	74154	1,31	1.35	74266 74273	-	2.25	4050	.81	24pin	.26	8224	3.59	LM323K	6.25 2.60	price is one	y 40p (inc
48	.16	.87'	74155	.67	.78	74273	_	.48	4052	.81	28pin	.30	8228	5.51'	LM325N	2.00	vouchers)	
49	.16'	.87	74156 74157	.67°	.78°	74283	_	.99	4053	.81*	40pin	.44	OPTO					
50 51	.16	.19	74157	.67	.52	74290	_	.83'	4054	1.29"		Wrap	125 1+	10+	50+ 100+			
53	.16'	.19	74160	1.21	.99	74293	-	.83	4056	1.46	8pin	.23'	TIL 209 Red X .15"	.10"	.10" .09"	2"	1+ 10+	50+ 10
54	.10	.19"	74161	1.21'	.65	74395	_	1.05	4059	5.18"	14pin	.34	TIL212 Yel X .20"	.18"	.16' .14'	TIL220	.16' .12!	5' .125' .195'
55		.19*	74162	1.21	1.85	74298	_	1.25	4060	1.24	1 6pin	.37'	TIL216 Red X .20	.18'	.16' .14'	TIL224 Yel X		
60	.16'	_	74163	1.21	.65	74365		.51	4066 4068	.48	18pin 20pin	.55*	TIL232 Gre X .20"	.18"	.16' .14'	TIL228 Red X		
70	.27'	-	74164	1.08	1.15	74366 74367	_	.51	4068	.21	24pin	.60	X = High Brightness			11L234 GIB A	-	Section 1
72	.23'	=	74165		.78	74368	_	.51"	4070	.21	28pin	.65"	DL747	U.4741	Sel Section	E 555	TIL209	TIL220
73	.28	.29	74166	1.02	1.85	74386		.39	4071	.21	36pin	.95		UA741			0 for £1.00*	8 for £1.0
74	.28	.29	74168 74169	_	1.85	74670	_	1.85	4072	.21	40pin	1.05	4 for £6.00*	5 for £1.	JU 4 101	21.00	U TOT LT.UU	

				hed the same	2	-					THE STATE OF					
N SUG				TTV	?	TI	4-81	AT	17	1	1/4	nn	11	PRIC	FC	
ME R				8FX30	32p	2N3054	44p	7451	12p	74177	50p	4070	-12p	INDAOL LAND	1917 anb 1910	80p
TRANSIST AC126 AC127	17p 16p	8C213 8C214 8C237	10p 10p 12p	8FX85 8FX86	20p 27p	2N3055 2N3702	44 p 8 p	7453 7454	12p 12p	74180 74181	80p 130p	4071 4072	12p 12p	1N5402 15p 1N5404 20p	7915 80p 7924	80p
AC128 Matched	14p	8C238 8C301	14p 30p	8FX87 8FY5D	20p	2N3703 2N3704 2N3706	8 p 8 p 8 p	7460 7470 7472	14p 24p 24p	74182 74190 74191	50p 70p 70p	4073 4081 4082	16p 14p 14p	BRIDGE RECTIFIERS	ZENER DIDDES 400mW 2.7V to 33V	8p
128/176 AC141 AC142	35p 24p 18p	8C303 8C328 8C338	30p 13p 13p	8FY51 8FY53 8SX19	12p 17p 20p	2N3707 2N3710	8p 8p	7473 7474	25 p 25 p	74192 74193	60p 60p	4086 4510	59p 60p	1A/50V 22p 1A/100V 24p	1	
AC151 AC152	22p 22p	8C547 8C548	11p	85 X 2 D 8 U 2 O 5	18p 130p	2N3711 2N3772	8p 172p	7475 7476 7480	25p 25p 40p	74194 74195 74196	55p 50p 50p	4511 4516 4518	70p 64p 65p	1A/200V 27p 1A/400V 30p 2A/50V 34p	VERO BOARDS .1" copper 2.5" × 5" 3.75" × 5"	51p 60p
AC153 AC176 AC187	25p 16p 23p	8C549 8C557 8CY30	11p 11p 60p	8U208 0C25 0C28	150p 76p 87p	2N3773 2N3866 2N3904	275p 54p 8p	7485 7486	60p	74197 74198	50p	4520 4528	65p 55p	2A/100V 36p 2A/200V 38p	CERAMIC CAP 50V	501
AC188 A0149	20p 65p	8CY34 8CY59	66p 24p	0C35 0C71	76p 16p	2N4D61 2N4D62	12p 12p	7490 7491	25p 40p	74199	100p	LINEARS 710CN	40p	2A/400V 40p OPTO/	22pF to 50.000pF	3р
A0161 A0162	35p 35p	BCY70 BCY71	14p 14p	0 C 7 2 0 C 8 4 T I P 2 9	26 p 42 p 37 p	TTL 7400	10p	7492 7493 7494	35p 30p 51p	CMOS 4000 4001	12p	741-8 747C-14	22 p 50 p	DISPLAY 2N5777 50p	POLYESTER CAP 250V .01, .0150220330470681 ul	F 5p
AF114 AF118 AF125	23p 30p 25p	80115 80121 80123	30p 70p 60p	TIP30 TIP31	35p 45p	7401 7402	10p 10p	7495 7496	45 p 45 p	4002 4006	12p 68p	748C-8 CA3D11	30p 80p	0CP71 70p 0RP12 70p 0L704 100p	.15, .22, .33 uF .47, .68 uF	6p 12p
AF126 AF127	25p 25p	80124 80131	77p 35p	TIP32 TIP33 TIP34	45 p 58 p 64 p	7403 7404 7405	10p 12p 12p	7497 74100 74105	120p 80p 40p	4007 4008 4009	14p 64p 30p	CA3018 CA3028A CA3035	80p 85p 140p	OL 707 100p .125" & .2" LEOs	1 uF 2.2 uF	15p 25p
AF 139 AF 186 AF 239	32p 54p 40p	80132 80135 80136	35p 30p 30p	TIP35A TIP36A	168p 165p	7406 7407	24p 24p	74107 74109	25p 30p	4010 4011	35p 12p	CA3036 CA3046	120p 75p	Red 9p Green 13p Yellow 13p	ELECTROLYTIC CAP 25V	
ASY53 ASY54	33p 33p	B0137 B0138	30p 30p 30p	T1P41A T1P42A T1P2955	54p 60p 65p	7408 7409 7410	12p 12p 12p	74110 74118 74121	46p 75p 25p	4012 4013 4014	12p 30p 60p	CA3054 CA3080 CA3140E	110p 70p 51p	Clip 3p	1 uF to 47 uF 68 uF, 100 uF 150 uF	6р 7р 8р
ASY55 BC107 BC108	33p 7p 7p	80139 80140 8F115	30p 25p	TIP3055 ZTX108	55p 12p	7411 7412	15p 15p	74122	33p 40p	4015 4016	50p 30p	LM301AN LM308N	28p 64p	B pin 10p 14 pin 12p	220 uF 338 uF	9p 11p
8C109 8C113	7 p 12 p	8F167 BF173	25p 20p	ZTX 109 ZTX 300 ZTX 500	12p 14p 16p	7413 7414 7416	25 p 45 p 24 p	74125 74126 74132	35p 35p 45p	4017 4018 4019	50p 55p 40p	LM380N LM381N NE555	61p 120p 25p	16 pin 13p 22 pin 22p	470 uF 1000 uF	14p 22p
BC117 8C119 8C140	15p 25p 27p	8F178 8F179 BF180	25 p 25 p 20 p	2N706 2N1131	10p 20p	7417 7420	24 p 12 p	74141 74142	50p 180p	4020 4021	50p 60p	NE556 T8A641	60p 143p	24 pin 24p 28 pin 28p 40 pin 40p	RESISTORS 10 chms to 1 Mohm	1p
8C142 8C143	20p 24p	8F181 8F182	20p 20p	2N1132 2N1302 2N1304	20p 20p 20p	7421 7422 7427	20p 15p 22p	74145 74150 74151	55p 65p 45p	4022 4023 4024	50p 12p 45p	T8A800 T8A810	70p 100p	40 pin 40p		14
BC147 BC149 BC157	7p 7p 7p	8F183 8F184 8F185	20p 20p 20p	2N1304 2N1305 2N1306	20p 20p 27p	7428 7430	25p 12p	74153 74154	45p 70p	4025 4027	12p 30p	BY127	16p	REGULATORS 7805 60p	POTENTIOMETERS 1 Kohm to 2 Mohms log/linear 5 Kohm to 1 Mohm log with swilch	22p 50p
8C158 8C159	7p 7p	8F194 8F196	7 p 7 p	2N1308 2N1613	33p 18p 20p	7432 7433 7437	20p 24p 20p	74155 74156 74157	45p 45p 45p	4028 4029 4030	45p 50p 30p	0A47 0A91 0A200	10p 15p 6p	7812 60p 7815 60p 7818 60p		
8C168 8C170 8C171	7p 7p 7p	8F197 8F198 8F200	7p 7p 33p	2N1711 2N1893 2N2217	25p 24p	7438 7440	20p 12p	74160 74161	55p 55p	4035 4041	60 p 57 p	DA2D2 1N4148	9p 4p	7824 60p 7905 80p	PRESETS horizontal 100 ohm to 1 Mohm	5р
BC172 BC173	7 p 7 p	8F224 8F257	16p 16p	2N2219 2N2369 2N2483	21p 15p 26p	7441 7442 7443	46p 40p 60p	74162 74163 74164	55p 55p 60p	4042 4043 4044	54p 54p 50p	1N916 1N4001 1N4002	5 p 4 p 4 p	7 to 12 to	Please add 25p for p&p.	Sold S
BC182 8C183 8C184	9 p 9 p 9 p	8F258 8F259 8FR39	28p 28p 18p	2N2484 2N2905	18p 19p	7444 7445	60p 64p	74165 74166	60p 75p	4047 4048	80 p 50 p	1N4003 1N4004	5 p 6 p	DEI	TA TECH & CO	
BC186 BC187	19p 19p	BFR40 BFR79	18p 18p	2N2906 2N2907 2N2926	19p 20p 10p	7446 7447 7448	50p 50p 50p	74173 74174 74175	80p 60p 60p	4049 4050 4066	25p 25p 35p	1N4005 1N4006 1N4007	7 p 8 p 9 p		R ROAD, LONDON, N2	
8C207 BC212	10p 10p	BFRBO BFX29	27p 20p	2N3053	15p	7450	12p	74176	50p	4069	12p	1N5400	13p		DNATIONAL MARCI	

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What to look for in the April issue: On sale March 2nd

Amp Survey

Build-it-yourself hi-fi continues to flourish, and new designs appear almost daily. Power amplifiers are a favourite in the field, and their numbers, by now, are legion.

Unfortunately there is no way for the home constructor to 'listen in' to a module before he builds it, and thus he is left to fall back on the spec. sheets. Fine if you like it, rotten if you don't.

Next month we're surveying the field, giving full details of all the models we can find, and putting the market leaders against top quality commercial equipment to find out how they sound.

MAINS SEEKER

So you are about to drill the living room wall to hang up those shelves you promised the wife 7 years ago. Black & Decker in hand you advance to the plaster. Wait a minute there a mains socket right beneath.

Doubt sets in — to drill or not to drill — that is the question. Which way do the wires run? Will you black out the entire Universe if you try it? How can you find those wires?

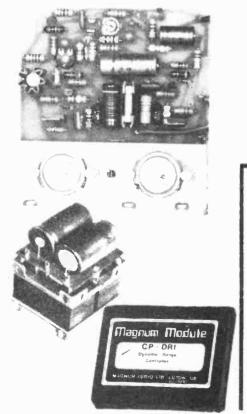
Simple really — just read ETI next month when we have a neat little project to show you exactly where the mains wires lie!

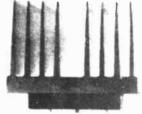
OCTAVE SHIFTER

A superb little circuit to add that instant 'jump' to guitar playing. Operated by a footswitch the effect has a unique sound all its own — not to be missed — no strings attached to this one.

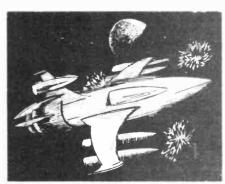


Well ten of them anyway The 3080 is a much under-rated device, and next month's IETs circuit man Tim Orr hopes to put that right with ten ways to use device, all comprehensively explained to help you design the other 3070 circuits vourself.





AMBUSH



Your starship crashes through the void — running between the lines of enemy dreadnoughts to deliver medical supplies to the seiged plant of Tora. In order to preserve energy your ship has no weapons, only its shields and its speed.

Missiles can appear from any direction, and to destroy them you must actuate your shields at the precise moment of impact, thereby conserving power and allowing the engines to keep you moving at Warp Factor 20.

Can you make it through the Ambush and make Capt. Kirk look a cissy?

microfile.

ALTHOUGH out of the first flush of youth I still consider myself to be young at heart so the young computing funfair seemed just the thing for me. Organised by the British Computer Society (BCS) the fair filled the Bloomsbury Centre Hotel early in January with the younger members of the ever growing group of people with an interest in computers.

Following on from the 'Living with Computers' conference, again organised by the BCS and held in the Institute of Education near the Bloomsbury Centre, the event provided a fitting climax to a very stimulating few days

The funfair included exhibits ranging from minicomputers, computers being used for choreography in ballet, computer controlled games, DIY computer kits, a micro-computer controlled railway and many stands showing how the computer is in use in our everday life. Among this last group of exhibits were the Abbey National Building Society (they got the computing habit, they have) and the police, showing that big brother was alive and well at the funfair.

The NASCOM stand was a great attraction for many people, demonstrating as it did the latest add ons to that popular DIY computer kit, the NASCOM 1. The buffer board, mother board and expansion RAM cards allowed the NASCOM's on display to run the 2K BASIC interpreter NASCOM are now producing. The BASIC includes all the facilities common to basics of this size, interger arithmetic, 26 variables (Designated A-Z), single dimension array plus assorted commands, operators and functions. In addition a machine code call greatly extends the power of the interpreter. NASCOM's super tiny BASIC makes use of this machine code call to provide amongst other commands, an edit function which allows the insertion/deletion of individual characters within a line, a renumber command and a facility for string inputs - something sadly lacking in the basic BASICS.

Undoubtedly though the exhibits that caused the greatest interest amongst the younger generation that made up the majority of the visitors to the fair were the rows of amusement machines. Everything from cowboys at the OK coral to star wars in space quadrant 0040. 7689. Microprocessors have revolutionised the arcade industry, both in bringing arcade type games into the home and in dramatically increasing the sophistication and supposedly, entertainment value of the machines in the public domain. Certainly the young audience were impressed.

Altergo ran a painting competition in conjunction with the funfair and Saturday saw the prize giving ceremony. The subject for the painting was "My Friendly Computer." The first prize was an Altergon robot, a beast that walks, talks, moves and flashes its eyes. Talking of beasts brings us onto beauty and Joanna Lumley — of the new Avengers — who presented the prize to the winner of the competition — 12 year old Fiona Mackay.

As well as the exhibition stands a concurrent series of lectures was presented in a hall adjacent to the main event. The lectures concentrated on introducing people to the various aspects of computing and the careers potential offered by the computing industry. These were well attended in spite of the attractions of the afforementioned amusement machines.

All in all a successful gathering that introduced the fascinating and diverse world of the computer to people who will form the systems engineers, computer operators, engineers etc. of tomorrow.



Any excuse to get a robot onto the pages of ETI is eagerly taken up. The fact that there are a couple of ladies in frame is incidental. The robot was first prize in the painting competition organised by Altergo. Fiona Mackay won the robot which was presented by Joanna Lumley.

Following on from my item last month concerning low cost keyboard designs Mr Charles Lacey has written to me with details of a project along these lines that is at the prototype stage. Designed as a touch keyboard with fifty keys including space bar, 2 shift keys, a delete key and two spare controls the system is more elegant than my attempt. Looking back at the circuit I proposed it does seem a bit clumsy.

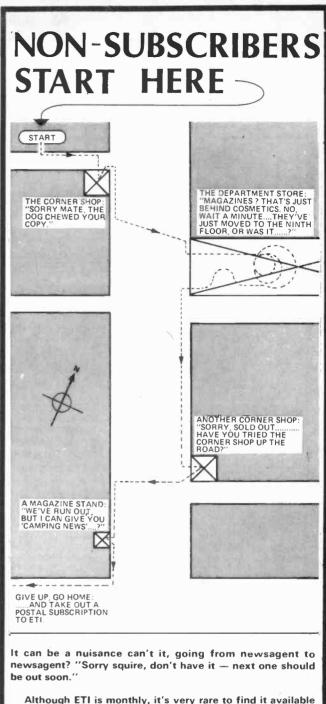
With luck Mr Lacey should have a very nice project in a couple of months time. We'll keep in touch.

By the way if anybody else has had ideas along these lines please let me know.

Finally may I add my own tribute to John Miller-Kirkpatrick who died last December. I'd known John just on two years and it was the System 68 project that brought us together. John handled the design and construction of the system while I dealt with the production from the magazine's end. System 68 had many teething problems but it was the first such project tackled in this country, way ahead of its time, and John remained enthusiastic throughout the problems and put in vast amounts of time to get things sorted out.

The last time I saw John was at the Breadboard exhibition. He took a keen interest in all of the stands and no doubt had a few ideas of his own for things to tackle in the future.





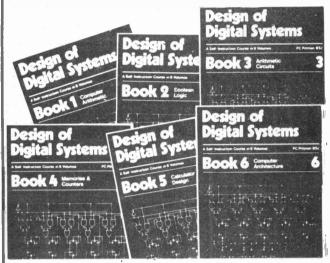
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Book 4 Flip flops; shift registers; asynchronous and synchronous counters; ring, Johnson and exclusive-OR feedback counters; random access memories (RAMs) and read only memories (ROMs).

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AUDIO POWER METER

An accurate way to determine whats watt in your hi-fi system, with our true reading power meter

POWER IS PROBABLY the least understood and most misrepresented quantity in the electric measurement system. This is especially so in the area of audio amplifier and speaker specifications when terms like peak, peak to peak, music and RMS are related to power.

Power is simply the rate at which energy is being used. It is expressed in watts and the value may vary from femtowatts (10-12 W), as in the input power of a FET, to thousands of megawatts in the power generation field. The term thousand megawatts is generally used in preference to the more correct term, gigawatts.

Power can be calculated simply by multiplying voltage and current:

P = E1

In a DC circuit where both voltage

and current remain constant no problem arises. However in an AC or a DC circuit where the voltage is not constant with time, this formula only holds for instantaneous power as the power varies with time. Power as we usually use the term is the time average of this. If the load is resistive, i.e. contains no inductance or capacitance, and we can measure the RMS value of the voltage, we can still use this simple formula. However measuring the RMS voltage is not easy as most voltmeters measure the peak or average rectified voltage with a suitable scaling factor built in to give a correct result when measuring a sine wave signal.

Reactive Reaction

If the load is reactive the current and voltage will no longer be in phase,

i.e. the peaks do not occur at the same point in time. The difference can be expressed either by the phase angle in degrees or by the cosine of this angle (known as the power factor). The current waveform can either be ahead of the voltage (leading) or behind it (lagging). Capacitive circuits give rise to a leading power factor while inductive circuits lag.

If working with a sine wave, and if the power factor is known, the formula for power can be expressed as:

P=EI cos Ø
where Ø is the phase angle. In a DC
circuit cos Ø is unity so the formula
holds for this case as well. An
example is a 40 W fluorescent light
which takes 430 mA from the 240 V
mains. At first sight, this implies a



power consumption of over 100 W, until it is realised that its power factor is about 0.45 lagging. The formula above, using $\cos \alpha = 0.45$, thus gives a power consumption of only 46.4 W. (The additional 6 odd watts is dissipated in the ballast.) The product of voltage and current is known as the VA rating and is used when calculating the currents in a circuit. If a capacitor is connected across a sine wave AC circuit the current taken can be calculated by dividing the voltage by the reactance of the capaitor. While this circuit draws current, it has a power factor of very near zero (90° phase lead) and therefore takes no power! By adding the correct amount of capacitance to an inductive circuit (i.e. the fluorescent light) the power factor can be altered, reducing the current drawn (but not the power).

Confused yet?

Ample Reason

Getting back to audio amplifiers and their ratings, the problem lies in the complex nature of the music waveform and how to specify the amplifier's rating. As the waveform is far from a constant sine wave with the peak power being anything up to 20 times the average, numerous methods such as peak power, peak to peak power, music power, etc. evolved. However, for a long time there was no set standard, and one amplifier advertised with a 50 W (music) rating was in fact a 5 W stereo amplifier. The situation got so out of hand that the US Government brought down legislation on how amplifiers were to be tested. This is with a continuous sine wave signal with level set so that the distortion is at a specified level and power calculated from the RMS output voltage: hence the term RMS power. Note however that the term RMS refers to the method of measurement, i.e. the use of RMS voltage, and it is not the RMS value of the power waveform. It is, in fact, the average of the power waveform.

Speakers are just as confusing. They are normally specified not in terms of the power they can dissipate, but the maximum power of amplifier they are suitable for. This is due to the fact that music is never (well, rarely) a continuous sine wave and the average power in the speaker may be only 10% of the RMS rating of the amplifier, even with the amplifier clipping.

To measure the power actually being delivered to the speaker under music conditions, a wattmeter must be used.

Design Features

To multiply current and voltage together we had the choice of analogue or digital techniques. Unfortunately while digital is the 'in' thing, offering versatility and accuracy, it is not fast enough to calculate the instantaneous power on high frequencies. We therefore chose the analogue method.

Looking around the ICs, the only ones with reasonable price and availability were the MC1494, 1495 and 1496. The 1496 (or 796) is the cheapest and most readily available, but has the disadvantage of not being able to multiply DC signals or AC signals with a DC offset. The 1494 and 1495 are about the same price, and of the two, the 1494 was more linear and easier to use.

We chose not to use any input buffer on the voltage input but had to pay the penalty of having a lower input impedance than normal with voltmeters.

Using the Power Meter

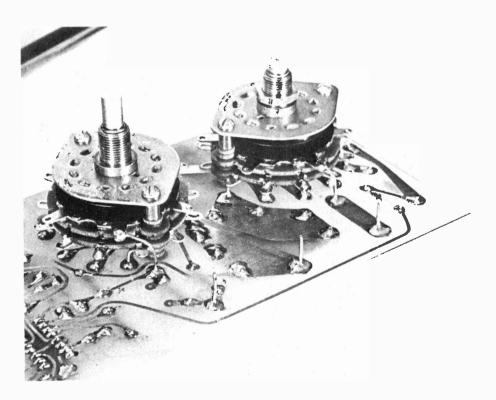
To use the meter we must measure both voltage and current. There must be a common point for these measurements. The current connection can be in either of two ways as shown in the drawings below. One measures the power out of the supply and the second the power into the load. The difference? The current shunt in the wattmeter drops one volt when working at the full range value and this may or may not affect the reading. At 10 A this accounts for 10 W which, if the power being measured is only 100 W, is a 10% error — although if the measured power is 2400 W the error is only 0.4%.

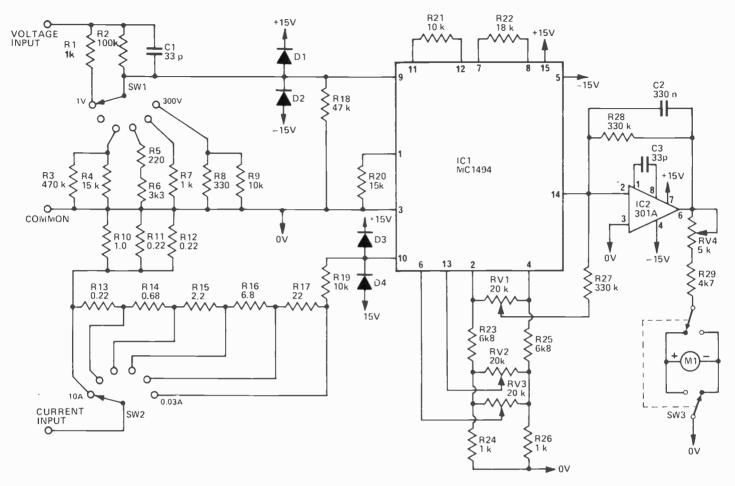
The range of the meter is the product of the individual ranges, i.e. on 30V and 1 A the fsd is 30 W, while 30 V and 3 A gives 100 W FSD. To help give a reading reasonably high on the scale, the voltage range can be overvoltaged by a factor of 2. Due to power dissipation problems this should not be attempted on the current ranges. The peak voltage or current can be as high as three times the range value.

Construction

We mounted all the components associated with the meter and the switches on a single pc board and if the same or similar case is to be used this is recommended.

Except for the meter and the switches the components are mounted on the 'normal' side of the pc board. These should be mounted >





HOW IT WORKS

Power is the product of current and voltage. This holds irrespective of the nature of the load, provided you are talking about instantaneous power. By multiplying current and voltage together and then taking the average of these instantaneous values we find the true power. Again this works irrespective of the load.

In this circuit the multiplying is done by IC1 (MC1494), the output of which is a current proportional to the product of the inputs. For more detailed notes on this IC, see the separate section. The current output of this IC is converted to a voltage by IC2 with C2 providing the averaging. The meter is then simply wired across the output of this IC with a meter reversing switch provided. This reversing switch is needed not to measure negative power, but to correct for reversed readings due to differing external connections.

The power supply is a full wave bridge with a centre tap giving about $\mp 20V$ DC which is then regulated to the ∓ 15 V required by IC1.

Adjustments for zeroing the voltage and current inputs are provided by RV2 and RV3 while RV1 compensates for offsets in the output. These are supplied by a stable ∓ 4 V reference in IC1. Range switching is done by SW1 and SW2. Protection against overvoltaging the IC is provided by D1 — D4.

Fig. 1. The circuit diagram of the audio power meter.

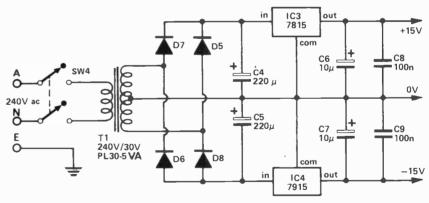
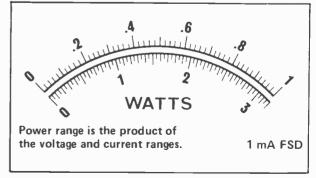


Fig. 2. Power Supply Circuit.

Right: meter scale designed for a 1mA FSD meter. These scales may need to be altered for differing meter units.



0 SW2 MOUNTED ON FRONT OF PCB **CURRENT** INPUT 0 COMMON SW1 MOUNTED ON FRONT OF PCB 0 VOLTAGE INPUT IC3 240V INPUT FROM SW4 \exists

Fig. 3. Overlay for the Power Meter.

PARTS LIST

	THE LI	
Resistors	all 5% ½W unless stated	
R1, 7, 24, R2 R3 R4, 20 R5 R6 R8 R9, 19, 2' R10 R11-13 R14 R15 R16 R17 R18 R22 R23, 25 R27, 28 R29	100k 470k 15k 220R 3k3 330R	V V
POTENTIO	METERS	
RV1-3 RV4	20k trimi 5k trimi	
CAPACITO	DRS	
C1 C2 C3 C4, 5 C6, 7 C8, 9	330n po 33p cera 220u 35	mic V electrolytic ' electrolytic
SEMICON	DUCTORS	
IC 1 IC 2 IC 3 IC 4	MC1494 301A 7815 7915	1
D1-D4 D5-D8	1N914 1N4004	
MISCELLA	ANEOUS	
Radiospar SW3, 4 tv Transform Meter 1 m Three bind Instrumen	vo pole toggle switc er 15-0-15, 5VA A FSD ding posts It case 255 x 100 x d and clamp s	hes

BUYLINES

Most of the parts for this project are readily available. Two things which may cause trouble are the switch assemblies and the quadrant multiplier itself.

The switch is an RS unit and as such can be obtained from any of their stockists. As for the IC, Tamtronik — who advertise on page 32 of this issue — can supply this and by the time you read this they will be able to sell you all the rest as well!

first with the only critical part of the assembly in the area of the range switches. Here the high powered resistors should be spaced at least 5mm from the PCB as they run hot at maximum current. Also the leads of all the reistors in this area should be cut off close to the pc board after soldering. This is to give adequate clearance to the rotary switches. We used two self tapping screws into the plastic of the transformer case to help fix it onto the board. We have made

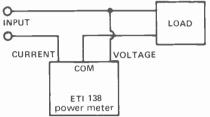


Fig. 4. This connection measures the power into the load,

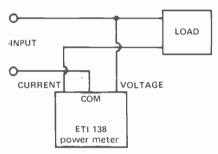


Fig. 5. This connection measures the power out of the supply.

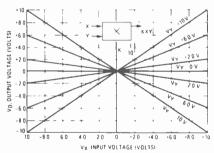


Fig. 6. Transfer characteristics of the IC.

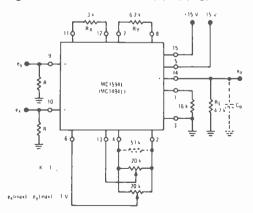


Fig. 7. Typical connections for a wide band multiplier or balanced modulator.

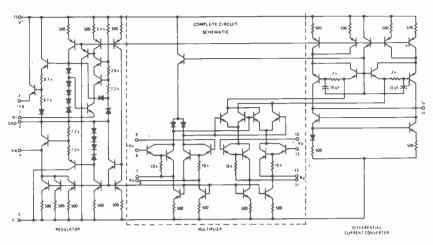


Fig. 8. The internal circuit diagram of the IC.

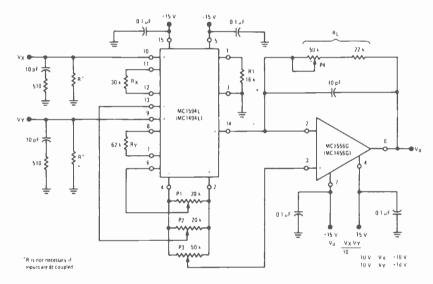


Fig. 9. Typical connection of a low frequency multiplier. For a squaring circuit simply parallel the two inputs. In this case pin 6 can be connected to 0V and P1 deleted.

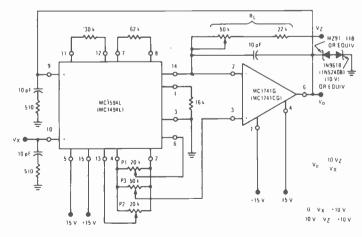
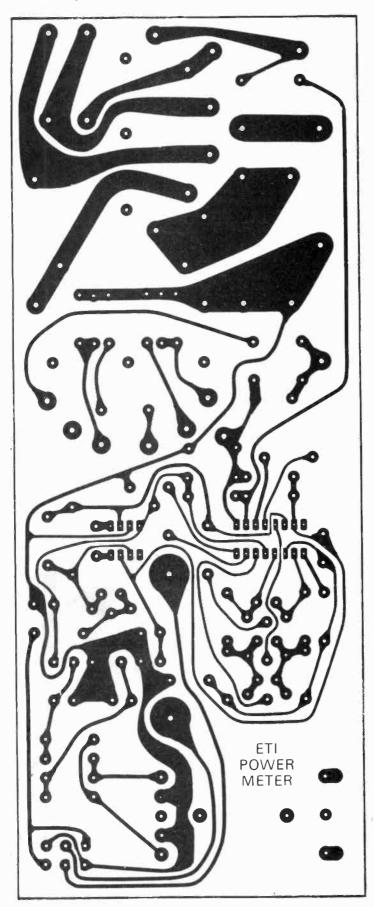


Fig. 10. Typical connection of a divide circuit. For the square root joins pin 9 and 10. Like the squaring circuits pin-6 can be connected to OV and P1 deleted.

Full size foil pattern for the power meter.



allowance for either the cermet (VTP) or the normal carbon trim pontentiometer.

Calibration

Four adjustments are required, which are performed as follows:

Select the 1 V and 0.03 A ranges and switch on. If the meter reads in reverse, toggle SW3. Don't worry about the reading unless it is off scale. If it is, adjust RV1 to bring it back towards zero. Now apply a voltage of about 1V DC to the voltage input and note the meter deflection. Adjust RV2* until there is no deflection when this voltage is applied. Now apply the voltage to the current input (it will take about 30 mA) and adjust RV3 until there is no deflection. Recheck the voltage input and readjust if necessary.

Now with no voltage applied adjust RV1 to give zero output. Apply exactly 1 V to both current and voltage inputs and adjust RV4 to make the meter read FSD.

This is all the calibration that should be necessary.

About the 1494

The 1494 is a variable transconductance multiplier with a bidirectional current source output. What this means is that it looks at the voltage on the two points and gives an output current potential to the product of the two. Typical applications include: multiply, divide, square, square root, phase detection, frequency doubling, balanced modulation/demodulation and electronic gain control. An internal circuit diagram is given for those interested.

Values and Limitations

1 For best temperature coefficient R1 (pin 1 to OV) should be 16k (we used 15k as it is easier to obtain). This sets the value of all the current sources inside the IC (I1 = 8 / R1) 2 The value of Rx (pin 11 to pin 12)

should be $\ge 3x$ peak input voltage(X) expressed in k ohms.

3 The value of Ry (pin 7 to pin 8) should be ≥ 6x peak input voltage(Y) expressed in k ohms.

4 Choose the scaling factory required ie Vout = K.Vx.Vy.

5 Load resistance (pin 14 to 0V) can be calculated by

RL=(K.Rx.Ry.)(1)/2

6 If RL is connected between pin 14 and 0V without an inverting amp, the frequency response is limited by the output capacitance of 10pF.

7 For best temperature coefficient the load between pins 2 and 4 should be 8.6k.

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audiophile VISUALLY HI~FI? SONY'S TAE88 PREAMP



BY NOW I expect most of you have already heard of the TA-E88 pre-amp, the Sony flagship design. Costing a mere £699 it has been designed to match the TA-N88 VFET power amp, and uses FETS in the later stages of its circuitry. Overall the finish of the unit is probably up to a £700 standard. All sockets are gold plated, and a gold ended twin phono lead is supplied as standard. The controls are very nice to operate, and the volume and balance controls are very special indeed. Stepped attenuators are employed, but the operation is so smooth as to make you doubt it.

As you can see from the internal shot below, the signal path lies entirely along the PCB. There are no leads from the board carrying signal potentials, all switches and sockets are mounted in place, and extended to the front panel where need be.

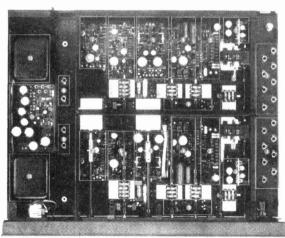
Shifting Load

There is even provision for switching about the resistance and capacitance associated with the magnetic phono inputs. Gold plated switches of course. Adjustment is variable between 10k-100pf and 100k-500pf. A useful provision this.

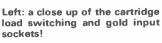
Completely separate channels — and PSUs — keep the right insensitive to the meanderings of the left and with the moving coil inputs especially this can be no bad thing.

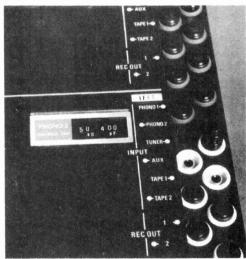
The head amp incorporated is a version of Sony marketed HA55, one of the best mains powered units on the market, and has two possible input)impedances.

All this and no tone controls. It should be interesting to go through the circuit section by section, so I suppose the place to begin is the beginning.



Right: an internal shot of the TAE88. The two channel construction can be clearly seen.



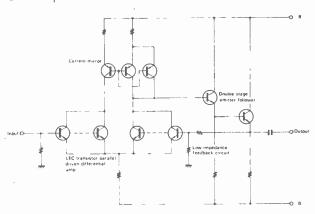


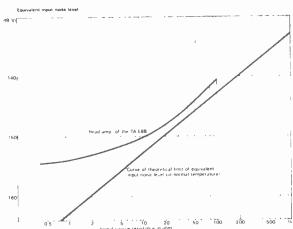
Head Start

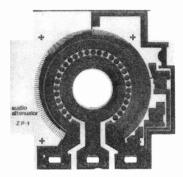
As shown below, the moving coil amp consists of a differential pair with current minor driving an emitter

follower output stage.

The differential circuit consists of cascade connected transistors to get the noise and gain figures required, and 44dB of negative feedback is applied to lower distortion as usual. Low impedance feedback paths like this are fine for some applications, but need careful design indeed to avoid becoming more of a hindrance than a help.







Above: moving coil input circuit and performance graph.

Left: the PCB from the balance control. Each 'step' is connected to a precision resistor!

Magnetic Charm

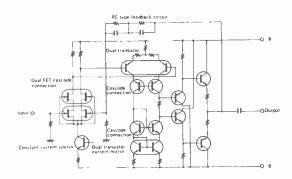
For more normal pickups the TA88 employs dual FET inputs (in cascode mode) and more conventional RC feedback equalisation circitry. The FETs used were developed specially for the amplifier, when your 'Sony' of course you can get these things done.

The second stage is a differential amplifier also, to further stabilise and give the overall circuit greater immunity from current source drift. Dual transistors are

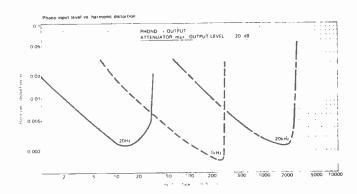
used in both the second differential amplifier and in the constant current stages of the circuit.

The output is once more an emitter follower following an emitter follower, and the components used are the expensive metal film resistors and polypropylene capacitors. Still when you've got £700 to spend — why not eh?

Equalisation is unusually accurate at 0.2%.

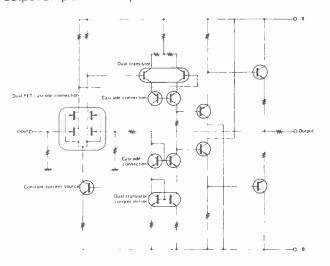


Magnetic cartridge input board.

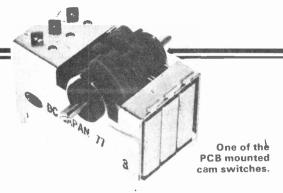


Standing At The Buffers

Buffer stages are liberally employed in the TAE88, between source inputs (non phono) and selector, and then either side of the volume control. Sony call the output amp a 'flat' amplifier for no reason I can fathom.

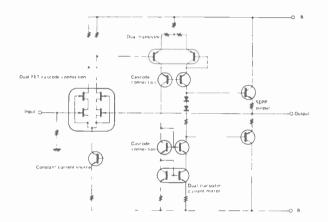


Buffer amplifier circuitry.



You can see the circuit for the buffer circuit opposite. Once again dual FET inputs, and if you thought that there is a very strong similarity between this and the phono amps, I don't think you'll get many arguments from me.

The 'flat' amplifier (below) differs in as much as it is designed to work into the load presented by cable and power amp. To do this without loss of frequency res-



Output buffer circuit.

ponse, a design closely akin to a power amplifier configuration has been adopted.

Output impedance is about 100 ohms, so that fairly long interconnection runs can be tolerated, and up to 15 V can be safely output at around .001% THD.

Lugged Around

After reading through all the imposing technical info supplied with the unit I was almost afraid to wire up the box into my merely mortal system. I suppose I suspected some form of electron snobbery whereby the TAE88 would refuse to 'talk' to any power amp of less than immaculate pedigree.

In practice however it was a case of 'noblesse oblige' and the Sony worked impeccably with the rest of the universe.' Several power amplifiers were tried, including the Lecson AP3II and a Crimson set up.

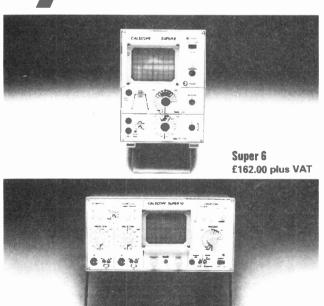
At first the TAE88 sounds very impressive with a particularly good bass end. The treble is a little thin, but nothing to comment adversely on. After a while though I came to suspect that maybe the unit wasn't as good as I thought at first, and perhaps adds a certain metallic quality to the sound.

Using the unit is a treat of the first order, and it inspires confidence better than Mr Callaghan ever did. Reservations must inevitably include that optimistic price level, and the less than perfect (just!) sound quality — which is as close to excellent as any other (but no closer!), but is more expensive approximation.

A lovely machine nontheless and if Sony can pull down the price (exit gold?) one which would have received a wholehearted recommendation.

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OUTPUTS Tape 100mV: Main output 500mV R M S

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Five connections — No external components

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INPUT SENSITIVITY 500mV
OUTPUT POWER 120W RMS into 812 LOAD IMPEDANCE 4-1612 DISTORTION 0.05% at 100W at

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SIZE 114 x 100 x 85mm

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The HY400 is LLP is "Big Daddy" of the range producing 240W into 4 Ω ! It has been designed for high nower discolor public address applications. If the amplifier is to be used at continuous high power levels a cooling fan is recommended. The amplifier includes all the qualities of the rest of the family to

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FEATURES: Thermal shutdown — Very low distortion — Load line protection — No external

components

APPLICATIONS: Public address -- Disco -- Power slave -- Industrial

OUTPUT POWER 240W RMS into 40 LOAD IMPEDANCE 4-160 DISTORTION 0.1% at 240W at

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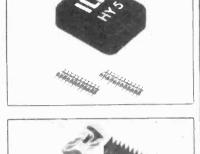
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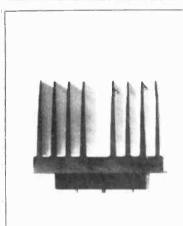
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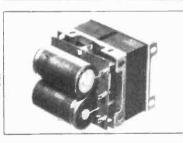
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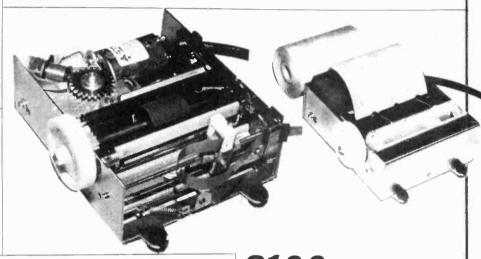
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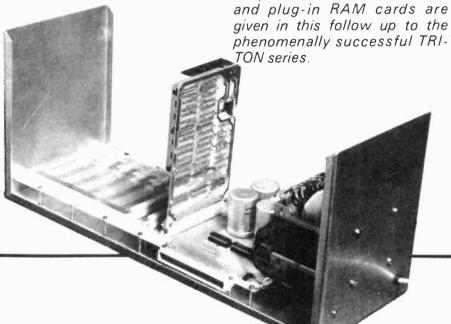
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bussing two PCBs together 35p/pair p/p 20p.

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ELMAC 4" SCOPE

ELECTRICAL DATA
VERTICAL AXIS (7) Deflection Sensitivity — 100m V./division
Bandwidth (between 3 dB points) — DC — 5MHz, Input Attenuation
— (calibrated) — 9 step 0 1, 0 2, 0 5, 1 2, 5, 10, 20, 50 / div
Input Impedia — 1 Meg/40 pf in shunt. Input Voltage — Max —

SÖÖV P.P.

HORIZONTAL AXIS(X) Deflection Sensitivity — 0:400 mV /
division. Bandwidth (between 3 dB points — 1 Hz.350 KHz. Gain Control — Continuous when time bases in EXT position. Input Impedance — 1 Meg. Input Voltage — Max — 600 V.P.

TIME BASE. Sweep Range (calibrated) — 100 msec / div. to 1 ¼ sec/div. in 5 steps. FINE Control — Variable between steps — includes time-base calibration position. Blanking — Internal — on

includes time-base calibration positive to negative.

SYNCHRONISATION Selection — Internal, external, Synchronisation Level — Continues from positive to negative.

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CRT DATA — 4in, — flat lace, single beam — Maximum high voltage — 1 StV — Fitted with 8x10 divisions blue filter gralicule PHYSICAL DATA Dimensions — 15cm(h)x20 5cm(w)x28cm(d).

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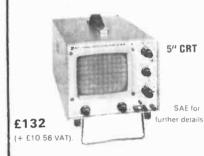
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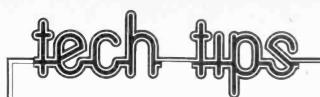
C100B £151 20, T157 £28.30, T151-3 £28.40 158 £64.80, T159 POA Little Prof. £10.80.

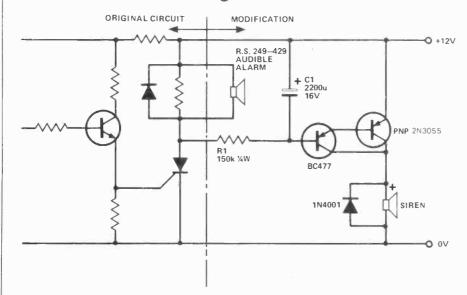
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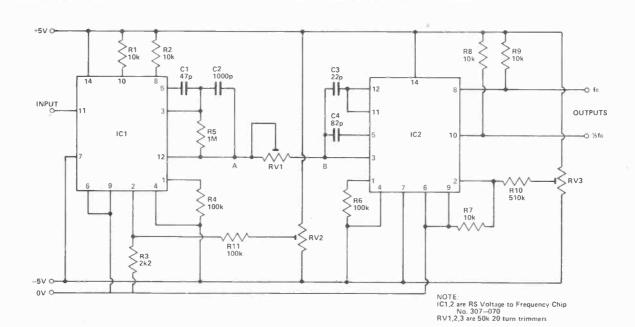




Less Alarming

J. Master.

The April, 1977 ETI Burglar Alarm works well enough but I thought you may be interested in this modification which enables a low power audible alarm to sound 40 seconds before the main alarm. The main advantage is that the alarm can be set when one is retiring to bed at night and if the alarm is inadvertently triggered at least there is enough time to turn the unit off before the main alarm sounds. This also applies when people come home with the alarm set, no front door by-pass switch is required and accidental setting off of the alarm is avoided. The delay time can be varied by altering RI and CI.



Keyboard Guitar

A. Parker

The purpose of this project is to convert the waveform from a guitar or other instrument into pure square or pulse waveforms of the same frequency. The circuit is basically a frequency to voltage converter feeding a linear VCO.

The construction is straightforward provided the usual care is taken with the Cmos chips. For RV1, 2 and 3 we suggest 20 turn presets

as these will be needed for fine tuning of the circuit later. Also as an aid in testing we suggest that VR1 should NOT be soldiered in until after initial testing has been completed.

The tuning of the circuit is best done using a Meter, PSU, Signal Generator and frequency meter if possible. First set the sig gen to some suitable frequency (ie 100 Hz) and using the meter between point A and earth adjust RV2 to give a voltage according go the formula

 $V = F_{in} \times 10^{-3}$

(for 100 Hz V = 100 --V

Now using an ACCURATE PSU set point B to +1 V and using VR3 adjust the output to 1 kHz then set to +10 V and adjust to 10 kHz. Now solder RV1 and adjust until

 $F_{in} = F$ out

(NB This is a gross over simplification and patience is vital. Remember the price of the Chips before you throw them out of the window).

. Tech-Tips is an ideas forum and is not aimed at the beginner. We regret we cannot answer queries on these items.

queries on these items.

ETI is prepared to consider circuits or ideas submitted by readers for this page. All items used will be paid for. Drawings should be as clear as possible and the text should preferably be typed. Circuits must not be subject to copyright. Items for consideration should be sent to ETJ TECH-TIPS, Electronics Today International, 25-27 Oxford St., London W1R 1RF.

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K009 Extended mylar pack. Contains all values from 1000pF to 0.47 μF. Total 290-capacitors to £11.25
K005 Polystyrene capacitors, 10 each value

values from 1000pF to 0.47μF. Total 290-capacitors to £11.25 K005 Polystyrene capacitors, 10 each value from 10pF to 10.000pF, £12 Series 5% 160V Total 370 for £12.30 K006 Tantalum bead capacitors. 10 each of the following: 0.1.0.15, 0.22.0.33, 0.47, 0.68, 1, 2.2, 3.3, 4.7, 6.8, all 35V; 10/25, 15/16 22/16 33/10 47/6 100/3. Total 170 tants for £14.20 K007 Electrolytic capacitors 25V working, small physical size. 10 each of these popular values: 1, 2.2, 4.7, 10, 22, 47, 100μF. Total 70 for £3.50 K008 Extended range, as above, also including 220, 470 and 1000μF. Total 100 for £5.90 K021 Miniature carbon film 5% resistors. CR25 or similar. 10 of each value from 10R to 11M, £12 series.

£6.00 K022 Extended range, total 850 resistors from 1R to 10M £8.30 K041 Zener diodes, 400mW 5% BZY88, etc. 10 of each value from 27V to 36V, E24 series Total 280 for £15.30 K042 As above but 5 of each value £8.70 £6.00

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CBM Shoot

I. Holdstock

Shown here is the Shooting Program that I have devised for use on the Commodore PR-100 Programmable Calculator.

The idea is to try to shoot at targets that appear at random ranges. To do this the operator has to guess the correction that is necessary to score a Bullseye. To make things more difficult it is assumed that there is a strong wind blowing from the left, and the correction has to accommodate for this as well. The program works out where the shot would have hit the target and gives a score accordingly out of 5. Points are deducted for complete misses. The number of shots actually fired is stored, together with the total score. To use the program you enter the keystrokes and go to 00. Then 1000 is entered in memory 6. Then take the Sin of any integer less than 100 and run the number obtained. A random range will be displayed. Using the chart below the program listing, the operator has to guess the corrections necessary to score a bullseye and enter them at the correct stages into the program. A score will be displayed after the last correction. To re-use the program, simply press run after the score has been displayed, and a new range will be shown. Before the second correction is entered, O will be displayed. If the present range has been forgotten, it is simply obtained by pressing MR 1. (See instructions at the end of the program listing).

STEP NO 00 01 02 03 04 05 06 07 08 09 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 4 35	KEYSTROKE M 0 1 F M+ 7 MR 0 ++ pi = y* 5 = F Frac M 0 X MR 6 = M 1 STOP MR 0 inv tan = F int SKIP GO TO 3	CHECK CODE 51 91 81 21 84 61 52 91 84 45 95 34 45 95 34 72 95 21 51 51 51 81 31 24 95 31 21 52 73 51 81 81 81 81 81 81 81 81 81 81 81 81 81	A) GO TO O B) 1000 in C) Any 2 dii D) RUN — E) Enter elei F) 0 will be G) Enter wir H) Score wi I) RUN — a J) Enter elei K) 0 will be L) Enter win M) Score wi	memory 6 git number, then S the range is display vation guess-RUN displayed ndage guess — RU Il be displayed new range is display vation guess — RU	IN it ved N ayed N
36	8	62	USEFUL H	INTS	
37 38 39 40 41 42 43 44 45 46 47 48 49 50	M 2 C/CE STOP — (MR 1 X 2 tan = F	94 51 82 25 13 — 64 52 81 74 82 24 95 21	SCORE IS IN M BULLSEYE II INNER IS 4 MAGPIE IS 3 OUTER IS 2	s 5	

Versatile CMOS Test bed

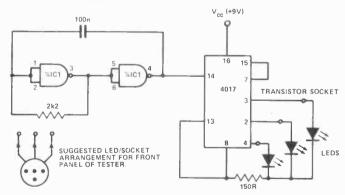
J. Anderson

It is a cheap and easily constructed transistor tester utilising inexpensive and readily available CMOS ICs.

It not only carries out the normal GO/NO-GO test but will differentiate between PNP & NPN type as well as identifying their base leads.

Use of the tester is simple and is as follows:

- 1) GO/NO-GO:—If the transistor is "a dud", either all the LEDs will come on or they will all go out.
- 2) PNP/NPN differentiation:—a PNP only one of the LEDs will come on.
- b) NPN one of the LEDs will go out.
- 3) base lead identification: -the

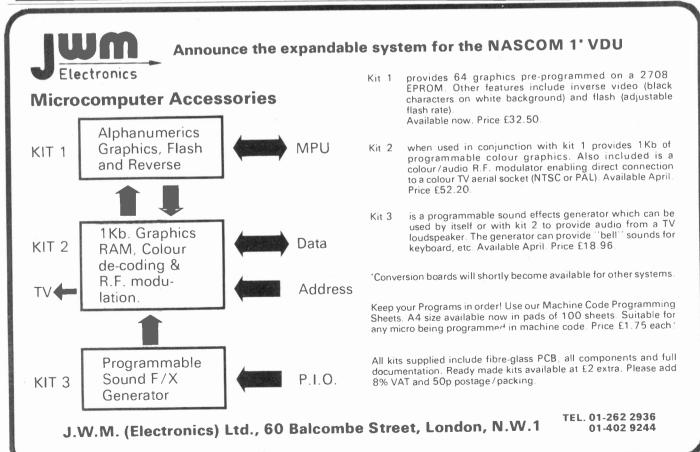


base lead is identified by the "odd LED out". (ie the one LED that is on with the other two out or the one that is out with the other two on).

The unit will also test diodes by the use of only two of the sockets of

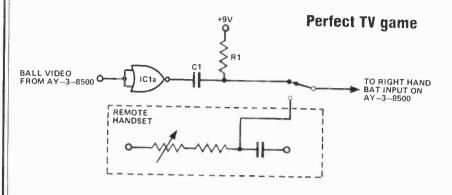
the transistor socket in this case the anobe of the diode is identified by the LED associated with its lead going out. The device also tests and identifies the gates of JUGFETs, SCRs & TRIACS.

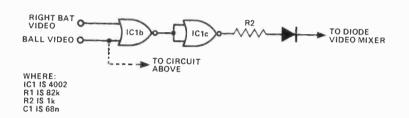
_																
7400	10p	7460	120	74137	90p	74195	50p	4055	130p	CA	3140		LM 3909 N		TBA 480 Q	200p
7400	10p	7470		74137	- -	74196	50p	4056	120p	LF	356		MC 1310 F		TBA 520 Q	200p
7401	10p	7472		74141		74197	50p	4060	100p	LF	357		MC 1312 F		TBA 530 Q	200p
7402	10p	7473		74141			100p	4066	35p	LN	И 211 H		MC 1314 F		TBA 540	200p
7403	12p	7474	25p	74142			100p	4069	12p	LN	vi 300 TR5	170p	MC 1315 F		TBA 550 Q	250p
7404						74293	90p	4070	12p	L	vi 301 AN	30p	MK 50398		TBA 560 C	250p
7405	12p	7475 7476	25p	74144		74L500		4071	12p	L	vi 304	200p	MM 5314	380p	TBA 641 A12	
	25p	7470	25p	74145	55p	745112		4072	12p	L	VI 307N	65p	MM 5316	480p	TBA 700	180p
7407 7408	25p	7480	40p	74147		CM(* 1	4081	12p	L	M 308 TO5	100p	NE 529 K	150p	TBA 720 Q	225p
	12p	7482	85p	74148	90p	4000	12p	4082	12p	L	M 308 DIL	100p	NE 555	25p	TBA 750 Q	200p
7409	12p		75p		65p	4000	12p	4093	70p	l Li	M 309 K	100p	NE 556	90p	TBA 800	80p
7410	12p	7483	75p		45p	1	12p	4510	60p	L	M 310 TO5	150p	NE 562 B	400p	TBA 810	100p
7411	15p	7484	70p	74153	45p	4002 4006		4511	70p	LI	M 311 TO5	150p	SAD 1024	1500p	TBA 820	100p
7412	15p	7485	60p	74154	70p		80p	4516	65p		M 317 K	325p	SL 917 B	650p	TBA 920 Q	280p
7413	25p	7486	25p	74155	45p	4007	14p	4518	65p		M 324	70p		N 150p	TCA 270 Q	220p
7414	45p	7489	130p	74156	45p			4520	65p		м 339	60p	SN 76013	N 110p	TCA 270 S	220p
7416	25p	7490	25p	74157	45p	4011	12p	4528	469 a08		M 348 N	90p	SN 76013	ND 125p	TCA 760	300p
7417	25p	7491	40p	74160	55p	4012	12p		70p		M 380	60p	SN 76023	N 110p	TCA 4500 A	450p
7420	12p	7492	35p		55p	4013	30p	4583			M 381 N	90p	1	ND 125p	TDA 1008	350p
7421	20p	7493	30p		55p	4015	50p		NEAR	- II	M 382	90p		N 150p	TDA 1034	450p
7422	15p	7494	70p			4016		AY3 85		Up	M 391	180p	SN 76271	V 160p	TDA 2002	300p
7423	20p	7495	45p	74164	60p	4017		CA 303		Op	M 555	25p			TDA 2020	300p
7425	20p	7496	45p	74165		4018		CA 304		Up	M 709 C	40p	l		TL 084	120p
7426	22p	7497	120p	74166	- 4-	4019		CA 306		5p T	M 710 TO5			100p	XR 320	250p
7427	22p	74100	80p	74167		4020		CA 306		0p -	M 710 DIL	65p		190p	XR 2206	450p
7428	25p	74104				4022		CA 307		υp	M 723 TO			35p	XR 2207	450p
7430	12p	74105		74173		4023		CA 308		5p	M 723 DIL		TAA 570	220p	XR 2208	600p
7432	20p	74107	25p	74174		4024		CA 308		oup	M 733		TAA 6618		XR 2216	650p
7433	28p	74108		74175				CA 308		Sop 🔓	M 741		TAA 700	350p	XR 2567	250p
7437	20p	74166	- 0-	74176	4-	4026		CA 308		oup	M 748		TAA 790	350p		150p
7438	20p	74109		74177		4027		CA 308		Op	M 1303 N		TAD 100	150p		150p
7440	12p	74118				4028		CA 308		iOp	M 1458		TAD 110	130p		150p
7441	45p	74120		74179	120p				90AQ 36	i0p	LM 3080		TBA 120			150p
7442	40p	74121	25p	74180				CA 31:		Effica II	LM 3900		TBA 120		ZN 414	100p
7443	60p	74122			130p			CA 313	30 10	gue		-		•	i .	
7444	60p	74123					100p		IN 4	4148	Diodes by	TT/Tex	as, 100 for	£1.50	First gra	
7445	65p	74125	8-		120p		60p		Static Rar	m 21	02 1024×	1 bit 45	O nano sec,	£1.00 ead	ch 125 or (10p each	
7446	50r				100p		60p			2112	2 256×4 bi	t 450 na	ano sec, £2.	.50	£7.50.1	
7447	50p	74128					90p		rata Ultra	asoni	c Transduce	ers 40kh	tz, £2.00 ea	acn; £.3.5 0	pair £60.	
7448	50p					4040	80p	1			All prices in	clude post	and VAT			
7450	12p						50p				-	DO	VA/ET			
7451	12p					1	25p	1				TU	VVEL			
7453	12p						25p		306 ST. P	PAULS	ROAD, HIGH	BURY CO	RNER, LOND	ON, N.1. TEL	01-226 1489	
7454	12p	74136	80p	7419	4 55p	4054	100p	1			Barcla	// Access c	redit cards acce	:DIEG		
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The circuit shown allows a player to play tennis or squash against a perfect opponent, which is useful if one wishes to practise and cannot find another player.

The circuit 'plays' tennis or squash simply following the ball up and down the screen, thus it is always in the right place in order to hit the ball.

B. Harvey

Although the circuit appears simple, (it only uses one gate from one IC!) the way it works is quite complex, suffice to say that it relies upon the way the AY-3-8500 games chip determines bat position from the setting of the hand controls.

The only modifications to the TV game are: (i) One lead connected to the ball video output of the games chip.

(ii) A switch wired in, selecting either a manual or an automatic player on the right hand bat.

(iii) This may not be necessary in home built games that use CMOS video mixers, but may have to be used in commercial units that sometimes use diode mixing circuits. The modification is shown and uses gates from the same IC. This will give a brighter bat and ball which is useful when playing squash.

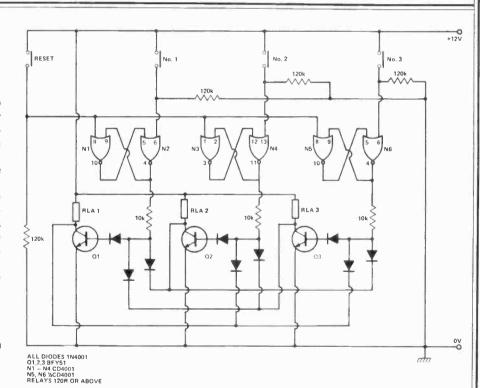
Sequence Switch

B. Willis.

The circuit right was designed to enable three relays to be individually switched by their appropriate buttons but such that only one relay can be energised at any one time. When any one relay has been energised the corresponding collector falls to near zero volts, which is connected to the base of the remaining two transistors; now if another relay is attempted to be energised the base of it's transistor will remain bottomed and keep the relay off. The rest button must be pressed before another relay can be energised. DI ensures that each transistor is kept off until the voltage applied to the base exceeds 0.6 V

The flip-flops and push buttons can of course be replaced with standard switches if momentary action is not required.

The circuit was used to control three radio transmitters where it was important that two should not be



switched on at the same time. The circuit lends itself to further applications; for example, switching various

inputs into an amplifier where it can replace the self-cancelling selector buttons.

The PW Sandbanks Metal Locator: a kit based on this recently published design for this uniquely effective type of metal locator is available for only £35.00 + 8% VAT The kit closely resembles the appearance as published, except that a close fitting injection molded housing replaces the vacuum molded electronics box to improve the environmental suitability of the construction. Carriage for complete kits £1.

The New Catalogue - "Tecknowledgey Part 2"

Part 2 of the catalogue: 1 ecknowledgey Part 2 of the catalogue: by the time this advert reaches the press, part 2 should be on sale. Sorry it's late, but it contains so many new and interesting things that we felt we had to hold up production to include them. Part three by the autumn and already there are many new items to go in! Part one 45p, part 2 50p. (inc PP etc).

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TDA1083 One chip AM/FM rx 1.95 BF: TDA1090 One chip HiFi am/fm 3.35 TDA1220 One chip am/fm rx 1.75 HA1197W HiFi AM tuner IC 1.40 406	961 822 823 673 J49/2sK13	200MH FM RF FM mi: Famou: 3 120v	z/2.0dB nf amp xer s MDSFET		0.80° 0.43° 0.51°			
TDA1090 One chip HiFi am/fm 3.35 TDA1220 One chip am/fm rx 1.75 HA1197W HiFi AM tuner IC 1.40	822 823 673 J49/2sK 13	FM RF FM mi: Famou: 3 120v	amp xer s MDSFET		0.43° 0.51°			
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	J49/2sK13	3 120			0,55°			
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The Dorchester has been described in PW Dec., Jan. and Feb. issues - but for those of you who may have missed it - it is an All Band broadcast tuner, covering LW/MW/SW and FM stereo in 6 switched ranges. Construction is very straightforward, with all the switching being PCB mounted - and the revolutionary TDA1090 IC used for AM/FM.

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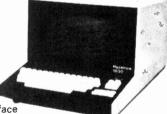


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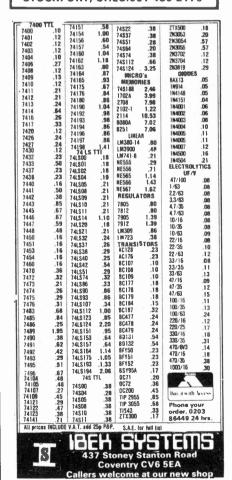
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The kit is complete, all that is required is a power supply a domestic T.V. and a domestic cassette recorder

POWER SUPPLIES

There are two power supplies available, a 3 amp supply which will power the basic kit and some expansion and an 8 amp supply with toroidal transformer which will power a very large system. Both supplies can be mounted in the vero frame.

3 amp P.S.U.	£26.46
8 amp P.S.U. kit	£04.0U

Nascom I is expanded by connection to a buffer board which creates a 77 way bus structure "NASBUS" into which expansion boards plug directly. The bus structure is carried along a motherboard which allows future boards to be added and to keep your computer neat the Nascom I, power supply, buffer board, mother board and expansion boards can all be mounted in a vero frame.

Buffer £27.00	
	,
Mother C40 00	
Mother £10.26)
Mini Motherboard£3.13	6
Vero CO4 OC	
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way Nasbus has the following advantages:

Uses standard Veroboard as a motherboard and Standard 0.1 single sided edge con-nectors for expansion cards. These components are readily and cheaply available.

2. The bus structure leaves 8 spare data lines and 4 spare address lines for future use of 16 bit processors

The power lines are regulated, on board regulators are therefore not needed which obviates the necessity for fan assisted

All prices include VAT and Carriage All cards use lower power, low noise shottky buffering which means the bus is quiet and does not need sophistications like active

termination or interleaved ground planes. Expansion boards are standard 8" x 8" DIP boards which are economic and give a

The memory expansion board can carry 16 dynamic RAM chips, these can be either 4K bit or 16K bit chips and the board is offered with8,16 or 32K bytes of RAM. The 16K board can be expanded to 32K by plugging in 8 more 4116

The memory expansion board also has room for 4 2708 UVEPROMS each of IK bytes and a lot of pre-programmed systems software is available

14 111 111400 00011010	
8K RAM board kit	£91.80
16K RAM	0454 00
16K RAM board kit	£151.20
32K RAM	0046.00
32K RAM board kit	£210.UU
Set	075 60
Set 8 x 4116	t /3.0U
Additional 2708	44 04
2708	1 1.34

INPUT/OUTPUT

For people wanting to use more peripherals than the standard kit allows for, Nascom are producing an I/O board which can carry a counter timer chip and a number of PIO's and UARTS. This will be available in March.

I/O board	
стс	£8.64
UART	£5.94
PIO	£8.64

To allow high level language programming Nascom have produced a 2K Tiny basic and a 3K Super Tiny Basic in 2 or 3 2708 EPROMS respectively. Also available is an 8K Microsoft precision floating point basic in 8 2708's which will be available in April on a single 64K bit ROM to fit the EPROM board.

Phone in your Access/Barclaycard Number on 051-236-0707 or complete this order form PLEASE SEND ME:

Tiny	£27 nn
Basic	£27.00
Super Tiny	027 00
Basic	£37.80
(8 x 2708)	£108.00
8K Basic	042.20
(ROM)	£43.20

EPROM BOARD

Available in March this board will carry 8 x 2708 UVEPROMS and the 64K bit ROM containing basic. The board can also be used for burning in 2708 LIVEDROMS

PROM	042.20
EPROM BOARD	£43.ZU

GRAPHIC BOARD

Allows high resolution graphics on your Nascom I. Contains 4K of RAM.

Graphics	0400	CO
Graphics board	 Ł IUZ.	טס.

MONITOR

Nascom have written a new monitor, T4 the most powerful yet available for this machine it contains many desirable features not found on any other monitor. T4 comes in 2 x 2708 to plug into the main Nascom I board.

Nasbug T4	£27 00
T4	£21.00

FIRMWARE

A powerful editor assembler zeap 15 available to run under Nasbug in 3 x 2708 or on tape. ICL Dataskill have produced a letter Editor available in 2 x 2708

Zeap (tape)	633 40
(tape)	L32.40
Zeap	049 60
Zeap (Eprom)	£40.00
Letter	275 60
Letter Editor	L/3.00

THE FUTURE

In the near future a mini-floppy disk system will be available with either single or double drive. These will probably offer in excess of ½ a megabyte and 1 megabyte respectively at prices that will allow even the hobbyist to have a large data base. To take full advantage of the business and scientific uses opened up by disks Nascom intend to release several high level languages. Looking further forwards Nascom is a developing product, and the fact that many thousands are now in use will ensure that the latest in computer technology will be available at a competitive price

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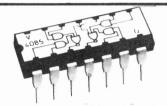
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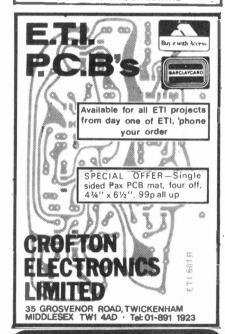
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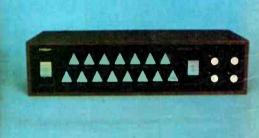
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