

... NEWS.... PROJECTS... MICROPROCESSORS... AUDIO...

TRANSCENDENT 2000 SINGLE BOARD SYNTHESIZER

LIVE PERFORMANCE SYNTHESIZER DESIGNED BY CONSULTANT TIM ORR (FORMERLY SYNTHESIZER DESIGNER FOR EMS LIMITED) AND FEATURED AS A CONSTRUCTIONAL ARTICLE IN ELECTRONICS TODAY INTERNATIONAL. The TRANSCENDENT 2000 is a 3 octave instrument transposable 2 octaves up or down giving an effective 7 octave range. There is portamento, pitch bending, a VCO with shape and pitch modulation. a VCF with both low and high pass outputs and a separate dynamic sweep control, a noise generator and an ADSR envelope shaper. There is also a slow oscillator, a new pitch detector, ADSR repeat, sample and hold, and special circuitry with precision components to ensure tuning stability amongst its many features

The kit includes fully finished metalwork, fully assembled solid teak cabinet, filter sweep pedal, professional quality components (all resistors either 2% metal oxide or ½% metal film!) and it really is complete — right down to the last nut and bolt and last piece of wire! There is even a 13A plug in the kit — you need buy absolutely no more parts before plugging in and making great music! Virtually all the components are on the one professional quality fibre glass PCB printed with component locations. All the controls mount directly on the main board, all connections to the board are made with connector plugs and construction is os impleit can be built easily in a few evenings by almost anyone capable of neat soldering! When finished you will posses a synthesizer comparable in performance and quality with ready built units selling for between £500 and £700!



Comprehensive handbook supplied with all complete kits! This fully describes construction and tells you how to set up your synthesizer with nothing more elaborate than a multi-meter and a pair of ears¹



Cabinet size 24.6" x 15.7" x 4.8" (rear) 3.4" (front)

THIS MONTH'S FRONT COVER FEATURE!



COMPLETE KIT

ONLY

£49.50 + VAT!

PSI 4002 STUDIO MODEL



cabinet size 17.2" × 17.2" × 6.7"

COMPLETE KIT ONLY £196.90 + VAT

The kits shown on this page are also available as separate packs (e.g. P C component sets, hardware sets etc). Prices are given in our FREE CATALOGUE

PRICE STABILITY: Order with confidence irrespective of any price changes we will honour all prices in this advertisement until January 31st, 1979 if ETI December 1978 issue is mentioned with your order Errors and VAT rate changes

EXPORT ORDERS: No VAT Postage charged at actual cost plus 50p handling

and documentation U.K. ORDERS. Subject to 12%% surcharge for VAT' (i.e. add % to the price). No charge is made for carriage for at current rate if changed SECURICOR DELIVERY: For this optional service (U.K. mainland only) add E2 50 (VAT inclusive) per kit SALES COUNTER: If you prefer to collect your kit from the factory call at Sales Counter (at rear of factory). Open 9 a.m. -4.30 p.m. Monday-Thursday

200 + 200 watt Amplifier

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- * Each channel totally independent with its own stabilised power supply driven by custom designed TOROIDAL transformers¹
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- for free standing work too * Easy to build - plenty of working space with ready access to all components, minimal wiring
 - extensive instruction suitable for both experience constructors and newcomers to electronics
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OUR CATALOGUE IS FREE! WRITE OR PHONE NOW! POWERTRAN ELECTRONICS

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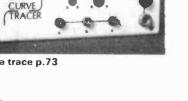


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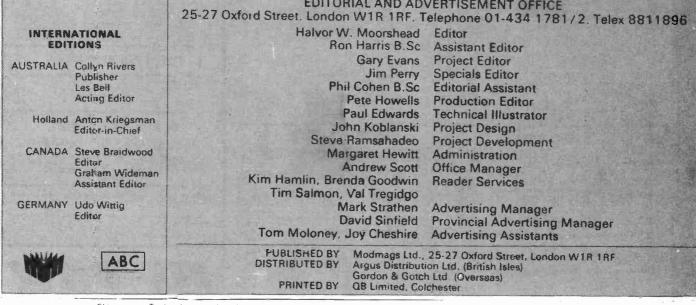
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and Logic Symbols 60p† BP29 Major Solid State Audio Hi-Fi Construction	Miniatrue SPOT toggle, 2 amp. 250V a.c. 1959 £0.65*	Vettages available by use of tags
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ELECTRONICS TODAY INTERNATIONAL - DECEMBER/1978

AUDIO KITS OF DISTINCTION FROM



cabinet size 18.3" × 12.7" × 3.1".

WIRELESS WORLD FM TUNER £70.20 + VAT

A pre-aligned front-end module makes this Wireless World published design very simple to construct and adjust without special instruments. Features include an excellent a.m. rejection, push-button station selection as well as infinitely variable tuning and a phase locked loop stereo decoder incorporating active filters for "birdy" suppression.

DE LUXE EASY TO BUILD LINSLEY-HOOD 75W AMPLIFIER £99.30 + VAT

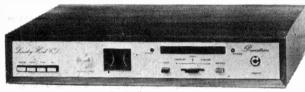
This easy to build version of our world-wide acclaimed 75W amplifier kit based upon circuit boards interconnected with gold plated contacts resulting in minimal wiring and construction delightfully straightforward. The design was published in Hi-Fi News and Record Review and features include rumble filter, variable scratch filter, versatile tone controls and tape monitoring whilst distortion is less than 0.01%.



cabinat size 18.3" × 12.7" × 3.1".

LINSLEY-HOOD CASSETTE DECK £79.60 + VAT

This design, published in Wireless World, although straightforward and relatively low cost provides a very high standard of performance. There are separate record and replay amplifiers and switchable equalisation together with a choice of bias levels are also provided. The mechanism is the Goldning-Lenco CRV with electronic speed control.



cabinet size 18.3" × 12.7" × 3.1".

T20 + 20 AMPLIFIER £33.10 + VAT

This kit, based upon a design published in Practical Wireless, uses a single printed circuit board and offers at very low cost, ease of construction and all the normal facilities found on quality amplifiers. A 30 watt version of this kit (T30 + 30) is also available for $\pounds 38.40 + VAT$.



14

cabinet size 15.5" × 6.7" × 2.8".

WWII TUNER £47.70 + VAT

This cost reduced model of our highly successful Wireless World FM Tuner kit was designed to complement the T20 + 20 and T30 + 30 amplifiers and the cabinet size, front panel format and electrical characteristics make this tuner compatible with either. Facilities included are pre-aligned front-end module, switchable afc, adjustable switchable muting. LED tuning indication and both continuous and push-butten channel selection (adjustable by controls on the freet or and). the front panel)

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cabinet size 15.5" x 6.7" x 2.8".

POWERTRAN SFMT TUNER £35.90 + VAT

This is a simple low cost design which can be constructed easily without special alignment equipment but which still gives a first-class output suitable for feeding any of our very popular amplifiers or any other high quality audio equipment. A phase-locked-loop is used for stereo decoding and controls include switchable afc, switchable muting and push-button channel selection (adjustable by controls on the front panel). This unit matches well with the T20 + 20 and T30 + 30 amplifiers.



cabinet size 15.5" × 6.7" × 2.8".

COMPLETE KITS: Our complete kits really are complete. All of the projects shown on this page are supplied with fully finished metalwork, ready assembled high quality teak veneer cabinet, cables, nuts, bolts, etc., and full instructions — in fact everything!

à

All of the kits shown on this page are available as separate packs (except the Powertran SFMT Tuner) for those customers who wish to spread their purchase or perhaps make their own cabinets or metalwork. Prices are given in our FREE CATALOGUE.

PRICE STABILITY: Order with confidencel irrespective of any price changes. We will honour all prices in this advertisement until January 31st, 1979. If ETI December, 1978 issue is mentioned with your order. Errors and VAT rate

EXPORT ORDERS: No VAT. Postage charged at actual cost plus 50p handling

and documentation. U.K. ORDERS: Subject to 12½% surcharge for VAT (i.e. add ½ to the price). No charge is made for carrier, for at current rate if changed. SECURICOR DELIVERY. For this optional service (U.K. mainland only) add

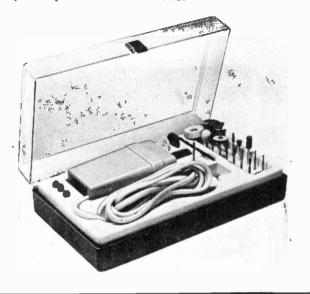
SECONTON DELIVERT, for this option a stress (of the manufacture), E2.50 (VAT inclusive) per kit. SALES COUNTER: If you prefer to collect your kit from the factory, Call at Sales Counter (at rear of factory). Open 9 a.m.-4.30 p.m. Monday-Thursday.

OUR CATALOGUE IS FREE! WRITE OR PHONE NOW! POWERTRAN ELECTRONICS ANDOVER PORTWAY INDUSTRIAL ESTATE (0264) 64455 ANDOVER HANTS SP10 3NM

news digest

Be boring better!

Thi is known as a Bimdrill (Don't blame us — it's their name). It costs £19.50 + VAT and comes complete as you see it here. It is mains powered, runs at 7500 RPM, and looks very useful indeed. Any more questions to: Boss Mouldings Ltd, Higgs Industrial Estate, 2 Herene Hill Road, London SE24 0AU

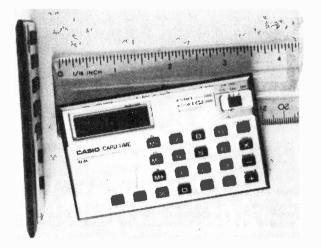


Catch these

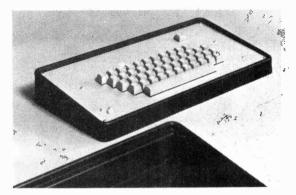
Two more companies sent us in catalogues this, month. The first was ACE who do a 36 page affair for 30p. The range they stock is pretty good as are the prices. A nice touch is the new range of new kits fot the beginner. Worth having.

The other was Stevenson. This catalogue is produced superbly and as it's free it's worth a look just to see how these things should be done. IC's are a strong point here, and a range of books is also included. Some very useful data is given in the back of the booklet which should also be on your bookshelves.

Addresses for these people appear on their ads elsewhere in this issue. Catalogues are things you should collect if you're serious about the hobby, as there is always something you'll want from somewhere at sometime or other!



ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978



Key feature

New from Vero of box frame is the new keyboard enclosure. Supplied as a kit it comes complete as a one piece ABS enclosure, anodised aluminium cover plate with self adhesive feet and all fixings. It will house a standard keyboard or individual keys as required — ideal for small desk-top terminals. Vero Electronics Ltd, Industrial Estate, Chandlers Ford, Eastleigh, Hampshire



Just the thing for Casanova?

Timetrac is a new little helper for people with busy lives and lousy memories. It contains a calendar preprogrammed, and can sound alarms

Time to calculate?

'Credit card' calculators do have advantages. Here's another one that can tell you how long you took to spend a fortune. Called the ST 24, it is a four-function plus % and stopwatch calculator. Maximum time to be when required. Two stopwatch facilities are also incuded.

Power is normally from AC adaptor, but battery power is provided as standby.

Optimisation Ltd, 45 South Street, Bishop's Stortford, Hertfordshire.

watched — 23hrs 59mins 59secs. Lap timing, second place timing normal stop/ start and 1/10th sec indication are all possible.

The calculator can be used while the timers (with possible repeat option) or stopwatch is being used. The most you'll pay for it is £24.95 anywhere. Available now.



KEY:

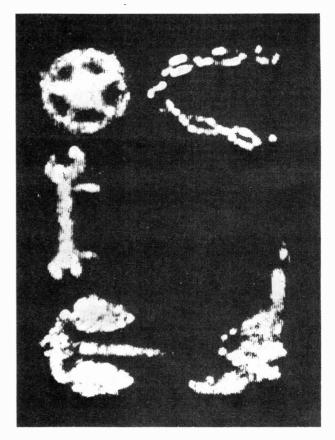
- 1: The bit of chocolate you thought you'd leave for later.
- 2: Coffee stains (instant).
- 3: A useful-sized bit of stiff paper to stop the window from rattling.
- 4: Rough calculations for your new combined egg timer/laser cannon project.
- 5: ETI makes a fair soldering iron stand.
- 6: The dog insisted on carrying your copy to you along with your slippers.

WHAT A BIND!

Half our orders for binders are repeats: we think that says a lot for their quality. At £3.00 all inc. you get a great deal of peace of mind too!

ETI Binders 25-27 Oxford Street, London W1R 1RF.

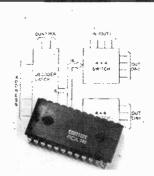
news



The image of it

The picture shows images achieved in lousy conditions by EMIs new wonder underwater TV system. The system has just won the IR100 award in America for its solving of the problems associated with the quartz and frequency troubles earlier systems experienced.

The whole thing is comparitively simple, and uses 201 lines per frame, 12½ frames per second. A range of several meters is possible even in atrocious conditions.



Cross point

Now available from Jermyn are 2 new Crosspoint Switches complete with control memory which are ideally suited where numerous analogue or data lines have to be switched.

These CD22101 and CD22102 devices consist of 4x4x2 arrays of crosspoint transmission gates, 4 to 16 line decoders and 16 latch circuits, with any one of the 16 crosspoint pairs being selected by applying the appropriate four-line address and any number of crosspoints being ON simultaneously.

Bandwidth is 10 MHz and low ON resistance is typically 750hms @ 12 Volts V_{DD} . Other significant features include closely matched switched characteristics, high linearity and standard CMOS noise immunity. Mogul Electronics Ltd, 272 High Street, Epping, Essex CM16 4DA.

ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978

digest



Less than (h)armless?

This mechanical arm is controlled by a microcomputer and has been designed to enable even the most severely paralysed patients to fend for themselves. The electronic super-arm of the future was amongst new developments shown for the first time at a two-day 'Aids to Independence' exhibition organised by North Surrey, Community Health Council at Ashford Hospital, Middlesex.

Although the arm is only in its prototype form, Dr. Jackson Todd of Queen Mary College, London (pictured above), demonstrated that it could be programmed to carry out separate or a series of quite delicate movements. A patient only able to move his head could con-

SCUNDS

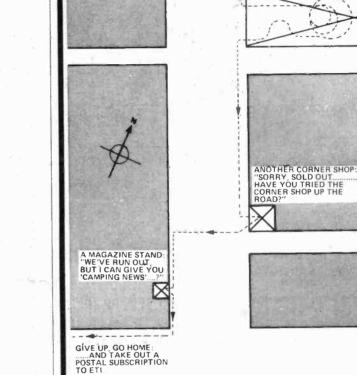
VINTACE

raiting for 1.

trol it using a stick held in his mouth to activate control buttons.

The so-called bionic arms that are now becoming available depend on the patient having some muscle movement. But this microprocessor controlled version can be programmed to carry out any type of function independently of the patient. The project has been underway at Queen Mary College for about a year and the control system, believed to be the first of its kind in the world, is complete. The next step is to produce a properly engineered prototype arm and integrate it with the input devices and the microprocessor control unit.

For further information contact: Tom West, Director of Public Relations, Surrey Area Health Authority.



It can be a nuisance can't it, going from newsagent to newsagent? "Sorry squire, don't have it — next one should be out soon."

NON-SUBSCRIBERS

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START HERE

START

THE CORNER SHOP: "SORRY MATE, THE DOG CHEWED YOUR COPY."

Although ETI is monthly, it's very rare to find it available after the first week. If it is available, the newsagent's going to be sure to cut his order for the next issue — but we're glad to say it doesn't happen very often.

Do yourself, your newsagent and us a favour. Place a regular order for ETI; your newsagent will almost certainly be delighted. If not, you can take out a postal subscription so there's nothing for you to remember — we'll do it for you.

For a subscription, send us £7.00 (£8.00 overseas) and tell us which issue you want to start with. Please make your payment (in sterling please for overseas readers) to ETI Subscriptions and keep it separate from any other services you want at the same time.

ETI Subscription Service Electronics Today International 25-27 Oxford Street, London W1R 1RF

It's not all old hat A new magazine is to be

launched soon — January

- specifically for enthusiasts of vintage sound equipment. It will be bimonthly and on subscription only. Among the areas covered will be wireless equipment, gramophones and cylinders, valves pre-war pioneering exploits and tales of the companies involved.

It will begin life as a 32 page job and sample Nols can be obtained for 65p all inc. Subs rates will be £5.80.

U.K. Sounds Vintage, 28 Chestwood Close, Billericay, Essex.

ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978

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POLYESTER RADIAL LEAD (Values in vF) 2509'. 0-01.0-015.0-022.0-027.5p:0-033.0-047.0-068.0-17p;0-15.11p;0-22.0-33 13p;0-47.15p;0-68.18p;1-0.24p;1-5.27p;2-2.31p. 1000pf/3509 8p	AF115+ Z5 BC345 12 Dirag 20 C77* 76 ZTX503 15 2v3663* 24 AF115+ Z5 BC441* 30 BFR41 25 C77* 76 ZTX504 25 2v3702 10 AF115+ Z5 BC461* 30 BFR41 28 C079* 76 ZTX504 25 2v3702 10 AF117+ Z5 BC461* 30 BFR41 28 C081D* 28 ZTX531 25 2v3703 11 AF117+ Z5 BC477 Z5 BFR79 28 C081D* 26 ZTX503 15 2v3703 11
ELECTROLYTIC CAPACITORS: Axial lead type (Values are in µ F). 63v: 0.47. 1.0, 1.5, 2.2, 2.5, 3.3, 4.7, 68, 8, 10, 15, 22, 8p; 47, 32, 50, 11p; 63, 100, 27p; 50V; 50 100, 220, 25p; 470, 50p; 1000, 2200, 68p; 40v; 22, 33, 7p; 100, 11p; 330, 62p; 4700, 64p; 35V; 10, 33, 7p; 330, 470, 32p; 1000, 49p; 25V; 10, 22, 47, 6p; 80, 100, 160, 8p; 220, 250, 13p; 470, 640, 25p; 1000, 27p; 1500, 30p; 2200, 34p; 3300, 58p; 4700 64p; 15V: 10, 1500, 20p; 2200, 34p; 10V; 4, 100, 66p; 640, 10p; 1000, 14p; 3000, 1500, 20p; 2200, 34p; 10V; 4, 100, 66; 640, 10p; 1000, 14p; 40V; 4000, 70p; 2500, 65p; 25V; 4700, 48p; 04V; 15,000 450p, 35V; 2000, 10P; 40V; 4000, 70p; 2500	AF121* 45 B6C547 11 DPROV 26 OCB3* 40 40.250* 85 2N3705 11 AF121* 48 B6C548 11 BFR81 28 OCB3* 44 40.257* 97 2N3705 10 AF124* 45 B6C548 13 BFR81 28 OCB3* 44 40.257* 97 2N3705 10 AF124* 55 B6C547 13 BFR29* 26 OC122* 48 40.311* 50 2N3707 10 AF125* 35 B6C557 13 BFX29* 26 OC122* 48 40.313* 152 2N3707 10 AF127* 35 B6C59 20 BFX84* 24 OC13* 48 40.315* 55 2N3709 10 AF139* 35 BC530* 57 BFX85* 24 OC140* 85 40.316* 85 2N3710 16 AF139* 70 <t< td=""></t<>
TANTALUM BEAD CAPACITORS 35V: 0.1µF, 0.22, 0.33, 0.47, 0.68, 1.0, 2.2µF, 33, 47, 648, 25V: 1.5, 10 POTENTIOMETERS (AB or EGEN) Carbon Track, WW Log & YW Loneer values 500(1 NG & 2XQ (fin. orly) Single gang 20V; 1.5, 16V: 10µF 13p each, 10V: 22µF, 33, 47, 6V: 47, 68, 100 OPTO SKQ-2MQ single gang 5KQ-2MQ single gang OPTO 27p 7p DILECTRONICS + LED splus Clip 7p DILECTRONICS LED splus Clip 7p 10V: 22µF, 33, 47, 6V: 47, 68, 100 5KQ-2MQ single gang 5KQ-2MQ single gang 7p 71L212 Yellow 27p 11L212 Yellow 27p 11L212 Yellow 27p 15p	AF180* 50 BCY40* 78 DFA80* 2* 0 C2200+ 48 40323* 60 2va319 22 AF239* 42 BCY42* 48 BY13* 50 OC200* 45 40323* 60 2va319 22 AF211 128 BCY43* 75 BFY50* 20 OC201* 75 40326* 52 2va3823 * 65 ASY26* 40 BCY59* 22 BFY51* 20 OC204* 85 40326* 52 2va3823 * 65 ASY50* 95 BCY59* 22 BFY53* 20 OC204* 85 40327* 62 2va3824 * 70 ASY50* 95 BCY70* 15 BFY53* 28 S1E5039* 95 40347* 80 2va3864* 90 ASY50* 95 CY70* 17 BFY55* 28 TIP29 43 40348* 43 20300* 18 SY70*
SLIDER POTENTIONETERS Amber Amber Green 1000: 0.001, 0.002, 0.005, 0.01µ F 50 5100F 5000F 190 190 0.1 µ F, 0.15, 0.2 9p, 50V: 0.47µ F 100 5000 (0.1000) 1000 (0.1000)	BC107# BC/72# 10 BC/72# 17 10 10 10 BC/72# 10 <th10< th=""> 10 <th10< th=""> <th10< td="" th<=""></th10<></th10<></th10<>
Range: 0.5pF to 10.000pF 3p PRESET POTENTIOMETERS 2N577 45p 0.015 µF, 0-022 µF, 0-033 µF 4p 0.11 µF 6p 0.11 µF 5p 11 µF 6p 11 µF 7 11 µF	BC103C+ 12 BD131+ 38 BU205 190 1731A+ 40 4045/* 99 2740564 120 BC113 17 BD132+ 38 BU208 228 TP318+ 40 40554* 80 274055 45 BC114 19 BD133+ 34 BU208 228 17931C+ 65 40495+ 90 274236 145 BC115 19 BD133+ 43 E421 96 TP31C+ 65 40495+ 90 274236 145 BC115 19 BD132+ 24 E5567 65 17452+ 45 40603+ 58 274286 220
6.8.10, 12, 18, 22, 33, 47, 50, 68, 75, 82, 85, 100, 120, 150, 220, 99, each 250, 300, 330, 360, 390, 600, 820, 100, 120, 150, 120, 120, 120, 120, 120, 120, 120, 12	BC116 19 BD136* 37 MO8001* 158 IP32A* 49 40536* 129 244269 20 BC117 15 BD137* 36 KE1120 25 IP32B* 70 40673* 68 24859 65 BC118 19 BD138* 36 KE4102 10 TP32C* 70 246974* 21 24922* 55 BC119 25 RD139* 36 KE4102 10 TP32C* 70 246974* 21 24922* 55
1000.1800.2000.2200 200 each POLYSTYRENE CAPACITORS: 1005 Find 25 Find 25 Find 26 Fi	BC134 19 BO140+ 50 M_4O0+ 90 TP33A+ 80 2N699+ 39 2N5136 42 BC135 20 BO142+ 59 M_491+ 190 TP33A+ 80 2N/506A+ 19 2N5138 20 BC135 20 BO142+ 59 M_491+ 190 TP33C+ 105 2N/07+ 19 2N5138 20 BC136 18 B0142+ 198 M_12955+ 99 TP33C+ 105 2N/07+ 19 2N5179+ 60 BC136 18 B0144+ 198 M_129,055+ 99 TP33C+ 105 2N/07+ 19 2N5179+ 60
Opp to thir sp. 1.5in to 4 min to 7 1/W 2.2Q.4 7M E12 2p 1.5p 180p CERAMIC TRIMMER CAPACITORS 1/W 2.2Q.10M E12 2p 1.5p 4p 2.7pF; 4.15pF; 6.25pF; 8.30pF 20p 1/M E12 1/D 4p 1/200 1.000 1/M 6p 4p 1/200 1/	BC140+ 28 BD1B1+ 85 MJE370+ 55 TP34A+ 85 2N914+ 32 2N5191+ 65 BC142+ 25 BD205+ 110 MJE371+ 60 TP34A+ 110 2N915+ 27 2N5191+ 65 BC143+ 25 BD205+ 110 MJE321+ 61 TP34C+ 110 2N915+ 30 2N5205+ 24 BC143+ 25 BD205+ 24 DJ2520+ 110 MJE520+ 110 2N915+ 30 2N5205+ 24
MINIATURE TYPE TRIMMERS 2.5.6pF, 3.10pF: 10-40pF 2.5.25pF; 5-45pF; 60pF; 88pF; 30p 2.5.25pF; 5-45pF; 60pF; 88pF; 30p	BC147 7 B0434 42 MJE951# 05 TP35A 225 2N930+ 18 2N5458 32 BC1478 7 BD695A* 75 MJE955*70 TP35B* 240 2N131* 22 2N5459 32 BC148 7 BD695A* 75 MJE3055*70 TP35B* 240 2N131* 22 2N5485 32
COMPRESSION TRIMMERS THERMISTORS: VA1034 1035 1111/2 105 3-40pf: 10-80pf: 25p 1040 1055 1056 1057 TIL114 110p 100-500pf: 450 1098 1100 20p each TIL117 164p	BC148C 10 BDY11 220 MPF103 36 TP365 260 2N1303+ 501 2N5777 40 BC149 8 BDY17 195 MPF104 36 TP368+ 265 2N1303+ 501 2N6027 40 BC149 0 BDY17* 195 MPF104 36 TP368+ 200 2N1305+ 50 2N6027 40 BC149C 0 BDY60* 110 MPF105 36 TP368+ 300 2N1305+ 35 2N6129 45 BC149C 0 BDY60* 110 MPF105 36 TP368+ 300 2N1305+ 35 2N2134+ 50
JACKSONS VARIABLE CAPACITORS Dielectric 0 2 355pF with slow 100/300pF 140p moton Drive 325p P RECTIFIERS 2008 25p	BC153 14 B0Y01# 165 MPF107 50 TIP41A# 63 2N1307# 50 3N128# 85 BC154 14 BF115# 22 MPF107 50 TIP41A# 63 2N1307# 50 3N128# 85 DC157 10 DF154 25 MPF3904 40 TIP41B# 73 2N1308# 46 3N140# 85
StoppF 165p 00 208/176 285p AA119 15 (plastic case) FX 30008 2 5p 6 1 Ball Drive	BC160 * 27 BF161 60 MPSA12 42 TIP2955 * 63 2N1671B* 195 Pair BC167A 11 BF167 25 MPSA55 24 TIP3055 * 60 2N2160 * 105 10p extra
Dial Drive 4183 C804-50 F 10 15 BY100 24 [A/200V 25] 61/36 1 550 p ± 25 50 p ± 175 p ± BY126 14 [A/200V 25] Drum 54mm 30 p ± 100, 150 p ± 215 p ± BY127 14 [A/400V 34] 70.2 75 LM 0.1-365 p ± 245 p ± 13 °3 10 m ± 35 LM	300H 170 NE565A* 120 TTL 74★ 7482 69 74175 87 76 40 221 96 301AP* 30 NE566* 160 (TEXAS) 7483 72 74176 75 78 40 240 236 304* 240 NE567V* 170 (TEXAS) 7484 95 74177 78 83 115 241 232
O0 2 365pF 275p O0 3.25pF 430p OA47 12 ZA/100V 44 709C 114 pin 49 LM DENCO COLLS RD72 92p 0A70 12 2A/200V 46 709C 105 35 LM BEF 5 choices 91p 0A79 12 2A/200V 46 723 ± 14 pin 45 LM	3011 + 10 RAM102.2 + 170 740 13 748 16 7418 165 86 43 243 232 318 + 205 RC41360 120 7402 14 7489 210 74182 90 90 90 60 259 160 319 + 205 RC4131 + 200 7402 14 7489 210 74182 90 90 90 60 259 160
DF VALVE LYPE RFC 7 (19mH) 956 D481 15 224/500V 65 14*14 pin 22 LM Range 1-5 B, YR. B5p 1713/14/15/16/ DA95 12 44/100V 75 741*14 pin 22 LM 6-7 B, YR 75p 17 85p 1049 6 4A/200V 75 747*14 pin 70 LM	324A 79 SASS60 240 7404 14 7491 75 74185 135 92 89 266 52 339# 80 SAS570 240 7405 18 7492 38 74188 75 93 89 273 244 348# 95 SG3402# 295 7405 38 74190 115 95 116 275 250
I-5 Green 92p 1FT 18/465 105p 0.495 8 4A/600V 105 1.59 I.M T1 1-5 B.Y.R.W 93p TOC1 86p 0A200 9 4A/800V 102 101 159 I.M B9A Valve Holder MW5FR 82p 104 8 6A/100V 73 AY-10212 580 I.M	372 125 SN72710+ 43 7408 17 7495 55 74193 105 107 442 283 192 379 375 SN72730+ 125 7409 17 7496 57 74193 105 107 442 283 192 379+ 375 SN72733+ 125 7409 17 7496 57 74194 105 109 55 290 128 380 95 SN75450+ 84 7401 15 7497 189 74195 51 112 55 293 128 380 95 SN75450+ 84 7401 15 7497 189 74195 51 112 55 293 128
RF CHOKES IN915 5 6A/400V 85 AY-1-320 305 LM 1yH 4.7 10 22 33.47 100 200 470 114003* 6 AY-1-5050 180 LM 19H 4.7 10 22 33.47 100 200 470 114003* 6 AY-1-5051 145 LM 19H 4.7 10 22 33.47 100 200 470 114003* 6 AY-1-5051 145 LM 19H 2.5 5 10 35p each 114006/7.7* 7 AY-3-10721/6 195 LM 10H 10H06/7.7* 7 10H06/7.7* 7 10F 56 AY-3-10721/6 195 LM	Join 145 SN /54548# 46 7412 17 74104 62 74197 85 114 50 298 168 381AN 248 SN 76030N 175 7412 17 74104 62 74197 85 114 50 298 168 381AN 248 SN 76030N 175 74120 62 74197 85 114 50 298 168 381AN 245 SN 76013 140 7413 30 74105 62 74198 150 122 70 324 240 1458 + 50 SN 76018 + 148 74107 29 74 LS 70 325 290 3900 + 60 SN 76023 140 7416 74197 54 74LS ★ 124 180 326 294
VEROBOARD * 0 1 0.15 0.15 (copper clad) (plain) (copper clad) (copper clad) (c	Byoline TO SN76033N 175 7417 30 7410 54 00 18 129 60 347 148 39114 125 SN76115N 215 7420 16 74111 68 01 18 129 60 347 148 39114 125 SN76131+ 110 7421 29 74116 198 02 20 132 95 348 186 252AA# 750 SN76131+ 110 7421 29 74116 198 02 20 132 95 348 186 253AA# 750 SN76127N 116 7421 24 74118 83 03 20 136 55 352 228
2½ x 5 49p 45p 28p 3A/600V* 27 Range 3V 3V A F:1224A*260 M 3½ x 3½ 49p 45p _	2663 275 SN76477* 225 /423 27 /4120 115 04 20 138 85 335 65 5/724* 175 SN76810* 150 7425 27 74121 25 05 23 139 85 365 65 C1303 88 TAA550 50 7426 36 74122 26 08 22 145 108 366 65 C1303 88 TAA550 50 7426 36 74122 46 08 22 145 108 366 65 C1304P 260 TAA621AX1 228 7427 27 74123 48 09 22 147 170 367 65 C1304P 260 TAA621AX1 278 74123 48 09 22 147 170 367 65
3½ x 17 195p 163p 107p AY-5-3807* 4500* 510 4½ x 17 252p 165p 30p NOISE SCRs* AY-5-3807* 415 MA 9kt of 35 pins 30p 30p Spot face cutter 85p ZSJ 160 Thyristors AY-5-3807* 550 415 MA AY-5-3807* 550 AY-5-3807* 550 AY-5-3807* 550 AY-5-3807* 550 AY-5-3807* 550 AY-5-8100* 731 MA AY-5-8100* 735 MA AY-5-810* 735 MA AY-5-810* AY-5-810* AY-5-810* AY-5-810* AY-5-810* AY-5-810* AY-5-810* AY-5-810* AY-5-810* AY-5-810* <td>C1312PQ 195 IAABOLA 193 7430 17 74126 57 11 22 151 96 373 120 C1488 85 TAA700 353 7432 25 7128 74 12 23 153 76 375 160 C1489 ± 90 TAA960 300 7432 40 74132 73 13 38 155 96 377 212 C14499 ± 90 TAA960 300 7433 40 74132 73 13 38 155 96 377 212 C144391 273 737 74141 56 14 76 156 96 378 184</td>	C1312PQ 195 IAABOLA 193 7430 17 74126 57 11 22 151 96 373 120 C1488 85 TAA700 353 7432 25 7128 74 12 23 153 76 375 160 C1489 ± 90 TAA960 300 7432 40 74132 73 13 38 155 96 377 212 C14499 ± 90 TAA960 300 7433 40 74132 73 13 38 155 96 377 212 C144391 273 737 74141 56 14 76 156 96 378 184
Pin insertion tool 99p 14500 38 CA3014* 137 MM VERO WIRING PEN* VARICAPS 14000/ 47 CA3014* 137 MM Plus Spool 325p MVAM2: 135 14400V 52 CA3020 170 MM	1495# 385 IBA1205 70 7438 33 74142 269 15 30 157 76 379 215 11495# 385 IBA5400 210 7440 17 74143 314 20 157 76 379 215 12456L 92 TBA5400 220 7440 17 74143 314 20 158 96 245 270 12170CG 79 TBA500 320 7441 74 74144 314 21 22 160 128 247 190 21340P# 150 TBA641A12 7442 68 74145 65 26 48 161 98 248 190 21340P# 150 TBA641A12 7442 68 74145 65 26 48 161 98 248 190
Spare spool (wire) sup # Collids / p actor 105 3450V 38 C A30280 + 80 MI FERRIC CHLORIDE★ Ba102 25 34100V 43 CA3035 240 MI Ibb ag Anhydrous 65 p + 30p p. & p. BB104 40 3A200V 60 CA3035 110 MI Ibb ag Anhydrous 65 p + 30p p. & p. BB105 40 3A200V 60 CA3043 110 MI	C3360P 120 BX or BX11 250 /44.4 115 /41.4 175 27 28 162 138 251 132 23401 70 TBA651 180 7444 112 74148 109 28 48 163 118 251 134 EM780 205 TBA800 90 7445 94 74150 99 30 22 164 114 253 142 EV40008 85 TBA8105 99 7445 94 74151 64 32 27 165 257 110
DALO ETCH RESIST PEN★ + spare tip BB106 40 34600V 120 CA3046 71 MI 75p TRIACS★ 73400V 120 CA3048 200 MI	FC6040+ 97 TBA820 70 7447 82 74153 64 33 39 166 226 258 146 K502534. 650 TBA8202 260 7448 56 71154 96 37 39 160 288 384 86 K502534. 650 TCA270SQ 260 7448 553 38 39 170 286 86 K50352+ 650 TCA270SQ 240 7450 77 74155 53 38 39 173 105 386 86 K50352+ 650 TCA270SQ 240 7450 7455 38 39 173 105 386 86
COPPER CLAD BOARDS★ 3A200V 49 BA400V 150 CA3080± 70 MI Fibre Single- Double- SRBP 3A400V 55 BT06 150 CA3081± 190 MI Glass sided 50 56 CA3081± 210 MI 6 = 6 75 900 600 6A400V 70 C106D 55 CA3090AQ 210 MI	AU2112+ 10 IDA(1022* 395 7453 17 74159 210 42 28 17 110 393 230 M57160* 620 TL071* 60 7454 17 74169 24 7 90 181 398 395 218 1515 80 TL081/0* 240 17 74160 24 84 120 183 298 395 215 515 80 TL081/0* 240 17 74160 24 81 200 183 395 215
6 x.12 130p 175p 8A200V 60 11C45 45 CA3123E 200 N DIL SOCKETS + Low Profile (TEXAS) 8A400V 75 2N4444 140 CA3130# 85 N	5543 210 TL082CP * 96 7470 28 74163 92 49 120 190 140 399 230 5544 155 TL084CP * 130 7472 25 74164 105 51 24 191 140 399 230 5555 * 29 UAA170 198 7473 32 74165 105 54 28 192 130 445 150 5556 µ = 0 UAA170 198 7473 32 74165 105 54 28 192 130 445 150 5556 µ = 0 UAA170 198 7474 27 74165 155 193 130 447 144
20p; 20 pn 70p; 22 pn 30p; 24 pn 30p; 15,400v 185 16,400v 185 28 pin 42p; 40 pn 55p, 60 pin 245p. 16,4400v 185 16,400v 185 SOLDERC* IPINS* 16,4500v 210 ST2 25	5550B# 50 ZN414 90 7474 27 7400 161 55 30 130 </td
100 pins 56, 1000 pins 400p 40669 95 L0130+ 452 NE	

ELECTRONICS TODAY INTERNATIONAL — DECEMBER 1978

WATFORD ELECTRONICS



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Introducing DM900 - The DIGITAL MULTIMETER with "Hidden Capacity" - It measures Capacitance too!

(as published in E.T.I. August 1978) Away with analogue meters for with some of these you may often as not use a crystal ball to make circuit measurements instead gaze into our crystal — not a ball but the 3½ 0.5 LIQUID CRYSTAL DISPLAY — on our amazingly accurate DMM incorporating incorporating.

5 AC & DC Voltage ranges; 6 resistance ranges 5 AC & DC Current ranges; 4 Capacitance ranges The prototype accuracy is better than 1% This is a unique design using the latest MOS ICs and due to the minimal current drain, is powered by only one PP3 battery. There is also a battery check facility. The DM900 is an attractive hand-held, light weight device, built into a high impact case with carrying handle and has been ingeniously designed to simplify assembly. Never before have all these features been offered to the electronics enthusiast in a single unit. unit

JACK PI	LUGS			SOCKET	10n on at	T	SWITCH	IES*	1	SLIDE	
Screen	ed Pla	ISTIC	open	moulded	in line	-1	TOGGLE	2A. 2	50V 28p		DT c/over 15p
2 5mm	120	ody 8p	metal 8p	with break	coupler 11p		DPST DPDT		34p 38p	1/2 A DP 4 pole	2 way 24p
3.5mm 1	15p	10p 15p	8p 13p	contacts 20p	12p 18p		4 pole on		54p	Spring	BUTTON
		18p	15p	24p	22p	_	SUB-MI SP chang	teover	59p	SPST o SPDT c	/over 65p
DIN		-	JGS	SOCKETS	and the second second		SPST on SPST bia	sed	54p 85p	DPDT 6	TURE
2 PIN Loudsp 3, 4, 5 Audio			1p 3p	7p 8p	18p 20p		DPDT 6 1 DPDT ce	ntre of	70p 79p	Push to	Make 15p
CO-AXIAL	(TV)	1.	4p	14p	14p		BOTAL		115p	Push B	reak 25p
PHONO			9p	5p single	15p	-	Adjusta	ble Sto	op Shaltu 6 Wafers	ng Asse	mbly. Accom- 69p
assorted cold Metal screen		13	2p	8p double 10p 3-way			Mains S	Switch	DPST to	fit	34p pole/12 way.
BANANA 4	4 m m	1	lp Dp	12p 10p	-		2p/6w	ау Зр	/4 way	4p/3 w	ay. 6p/2 way 47p
1	mm		7p	7p	-	_	Spacer ROTAF	and So	reen djustabk	e Stop)	5p
WANDER 3 DC Type	3 mm		Bp 5p	8p 20p			1 pole.	/2 to		2p/2	to 6 way. 3
AC 2-pin Am	-		5p	15p	1		ROTAR	Y Ma	ains 2501	AC. 4	Amp 45p
VOLTAGE REGULAT		TRA	NSFO	RMERS* (N	Aains Prim	220	-240V)		ALUN		PANEL
	*********			mA; 9-8-9V			95	PII	BOXE		METERS*
103 Can Typ 1A +ve 5V, 15V, 18V	140	12V-	3A: 15	A 6V5A: 5V25A 15	/25A		195	o 3	×2×1	45	FSD 60x46x
MVR5 or 12 1A ve 5V,		12V-	5A 12	1 3A 4.5V- 2V- 5A; 15V	4A 15V	- 4A;	201.24	A	x4x1½"	68	35mm 0-50µ A
Plastic (TO92	220	24V	A: 6V-	0p (20p p& 1.5A 6V-1 2V-1A: 15V	.5A: 9V-1	3A	9V-1.3A	. 4	x4x 1 ½ x2 ¼ x 1 ½	5" 60	0-100µ A 0-500µ A
+ve 0.1A 5\ 8V, 12V, 15\	30 J	20V-	6A 29	0n (45n n&	n)			4	x2½x2'' x4x2''	64 82	0-1mA 0-5mA
+ve 1A (TO) 5V, 12V,	220)	120	2A, 1	4A 6V-4A; 9 5V-1.5A 15 1A 25V-1A;	V-1.5A; 2	0V-1	2A 20	7. E	x4×2'' /x5x2½''	88	0-10mA 0-50mA
18V. 24V	85	(50p	p&p).	2V-4A 12				8	8×6×3'' 0×7×3''	148	0-100mA 0-500mA
-ve 0.5A 5 8V: 12V. 15	V.6V. V 86	20V 40V-	2.5A 1.25A	20V-2.5A 40V-1.25A	30V-1.5 50V-1A	A 3	0V-1.5A		0x4¼x3 2x5x3″ 2x8x3″	142 165 210	0-1A 0-2A 0-25V
⊶ve1A 5V.	12V 110		p&p).	charge to be	added abo	ove o	ur norma	-			0-50V AC 0-300V AC
—ve 0.1A (T 5V. 12V, 15\	092)		l charg			,		S	PEAK	ERS	S" VU"
LM309K LM320-12	135						. 1	_ 8 2	Ω 0.3W	р 65	475p each
LM320-15 LM323K	165 598	K1	Biac	to fit ¼ sha k Pointer typ	He .		9p	2	.5 3" 0 Ω 2.5"	58 65	4% x3% x1%
LM304H LM317H	240 100	K14 K2	Siim	e Pointer typ Silvered Alu	iminium		11p 12p	6	4 Ω 2.5" 0.5W	65	0-5DµA 0-100µA
LM317K LM325N	350 240	K3 K4	Blac	n Black Ribb k Serrated N	letal top wi		120	7	Ω 3W	190	0-500µ A 595p each
LM326N LM723	240 45		a As K	itor 35mm d 4 but 25mm k Fluted, me	i diam.		22p 20p	6	⁷⁷ x 4''	160	sop outin
EARPHON Magnetic	ES		brated	0.9. 37mm 5 but with p	diam.		28p 28p	HE			
2.5mm	18p	K7	Biac	k Knurled, berated 0-9 3	tapered, m	etal		TO	NKS★ 32 8p		TI PROJECTS
3.5mm Crystal	18p 33p	K7: K8	a Asa	bove but poi k or Silvered	nter on skir		26p 10p	TO: TO	5 9p	Ge	nerator dio Oscillator
ULTRASO	NIC	K1	2 Alun	ninised plast 22mm diam	ic with line		16p	TO	220 24p	ET1 Par	Light Show
TRANS- DUCERS		K1	9 Soli	d Aluminium ndicator, skir	Amplifier	Knob		то то	3 24p 66 24p	ava	ailable. Send E for List.
£3.95* pe		1								1	
CMOS★ 4000 15	4030 4031	58 205	406 406	3 110	4174 1	109	4511 4512	150 98		Chip	
4001 17 4002 17	4032 4033	100 145	406 406	7 380	4175	99 108	4513 4514	206			Or TV V into a VDU by
4006 105 4007 18	4034 4035	196 111	406	9 20	4409	720	4515 4516	299 125		he new	Thompson-CSF
4008 87 4009 50	4036 4037	325 100	407 407	21	4412F 1	720 6 50	4517 4518	382 102	SF.F96	6364	16 line by 64 it refreshment,
4010 50 4011 18	4038 4039	108 320	407 407	3 21	4415F	380 795	4519 4520	55 108	Cursor	manag	ement, Cursor
4012 18- 4013 42	4040 4041	105 80	407	6 85	4419	795 280	4521 4522	188 199	erasing	Comp ting syst	atible with any
4014 86 4015 89	4042	75 94	407	8 21	4433 1	545 099	4527 4528	152 99 165	SF.F96	6364E	£11.75*
4016 45 4017 89	4044	88 145	408	2 21	4440 1	825 275	4529 4530	85		013UA	
4018 89 4019 48	4046	128 87	408	6 73	4454	295 295				102 RA	£8.20*
4020 99 4021 91	4048 4049	58 48	409	3 85	4490F	695			SN754	63 RAN 50	£1.20*
4022 88 4023 20	4050 4051	48	409	6 105	4501	525			SN754 SN754	152	70p* 70p*
4024 66 4025 19	4052 4053	72	409	8 110	4502 4503 4506	120 69				odulato	
4026 180 4027 45	4054 4055 4057	110 128 2570	409	0 109	4507	51 55 298	1		(Send	ete Mod 30 p s cal data)	ule £136.50* tamps. for full
4028 81											

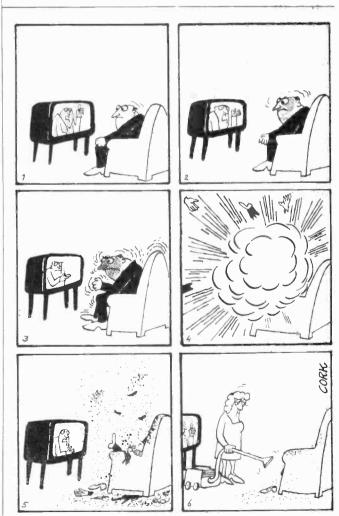
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Each sheet measures 180mm X 240mm and comes packed flat in a stiff cardboard envelope for protection. There should be enough for dozens of projects here - and the longer you wait the worse they'll look!

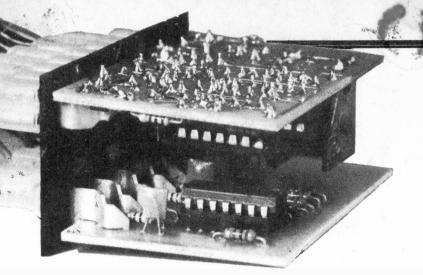
Send £1.75 (includes VAT and postage) for the twosheet set to: **Panel Markings** ETI Magazine, 25-27 Oxford Street, London W1R 1RF.



ELECTRONICS TODAY INTERNATIONAL -- DECEMBER 1978







A straightforward, low cost design, with a number of sophisticated features, that should protect your car from unwelcome attention.

DADTC LICT

CAR ALARM

THERE IS ONLY ONE way to ensure that you never have a car stolen and that is not to be stupid enough to buy one in the first place. However accepting the fact that many of us will feel the need to own a car how do we ensure that it remains ours amongst the ever increasing crime levels in this country. Well you could do worse than to fit the alarm system described here. Not only does this system protect the car itself, monitoring all doors and disabling the ignition when set, but also offers protection to the car's accessories.

The alarm provides an entry and exit delay before the horn is sounded, this means that there is no need to fit an external lock switch to the car. When leaving, the concealed alarm switch is activated whereupon the owner has 30 seconds before the alarm is set. On entry a 15 second delay is provided.

When triggered the system will sound the horn intermittantly for two minutes before resetting. However, if the initial cause of the alarm is still present, the alarm will retrigger.

The alarm provides for both active high and active low inputs allowing all types of sensor to be employed.

An additional accessory protection module provides an independent monitor of the car's accessories.

Construction is quite straightforward. The use of Incar connectors will allow the unit to be readily fitted and removed from any **BUYLINES**

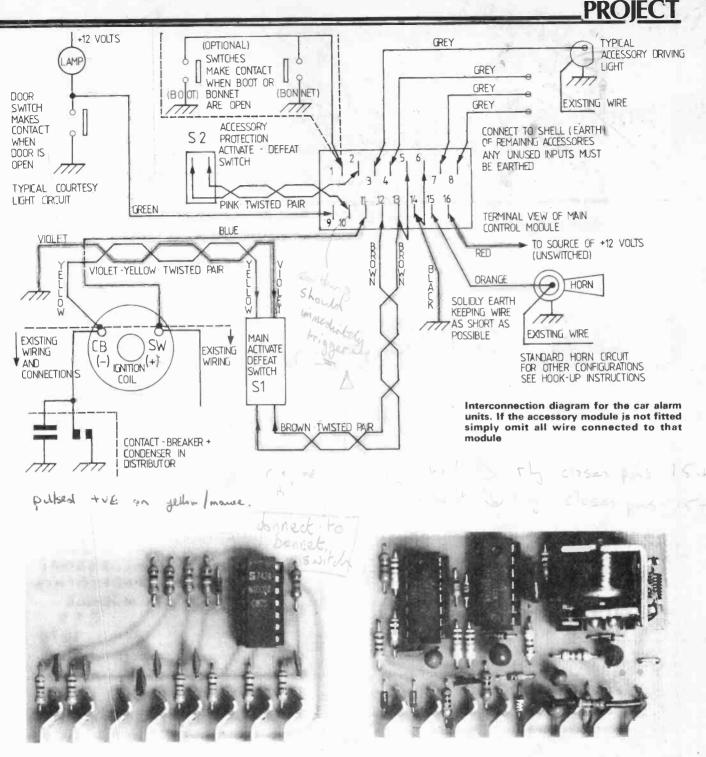
Compu-Tech Systems of 7 Sandhole Lane, Lt Plumstead, Norwich, NR13 5HZ will supply a complete kit of parts for this project.

car. These connectors should be fitted first. The rest of the components can then be fitted as shown in the appropriate overlay. Note that any polarity sensitive device is mounted in the correct position. The main board's jumper should be fitted when construction is complete. If your car's horn has one wire coming from it fit jumper A, if it has two wires with one going to earth also fit jumper A. If the horn has two wires neither going to earth, fit jumper B.

With construction complete the PCBs can be glued into the housing chosen for the alarm.

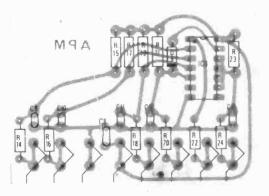
Installation of the alarm in the car must be left up to the constructor. The overall interconnection diagram is shown and it should be clear how to proceed in general. The detailed installation will however vary widely from car to car.

		S LIS 1
	RESISTORS R1,9 - R2 - R3 - R4,5,7,8,10 - R6,11 - R12 - R13	1 k0 100R 1 M0 10M0 4 k7 4 7 R 4 M7
e 3 s	CAPACITORS C1,2 C3 C4,6,7 C5	10n ceramic 16u 16 V tantalum 4u7 16 V tantalum 47n polyester
	SEMICONDUCTOR IC1,2 Q1 D1-7 ZBL.」から	S 4001 BC337 1N4148 15 V 400mW
	SWITCH SW1	DPDT
	RELAY RLa	12 V 85R with 15A contacts
S	MISCELLANEOUS PCB as pattern, cor cable, etc.	inectors, case to suit,
t th D	RESISTORS R14,16,18,20 R15,17,19,21 R22,24 R23	10k 100k 100R 1k0
	CAPACITORS C8-13	10n ceramic
r	SEMICONDUCTOR IC3 D9	S 4002 1N4148
1	SWITCH SW2	SPST
/	MISCELLANEOUS PCB as pattern, con	nectors, cable, etc.

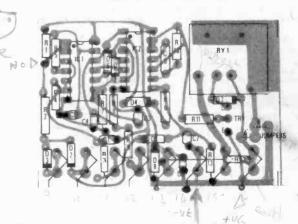


Overlay for the accessory protection board.

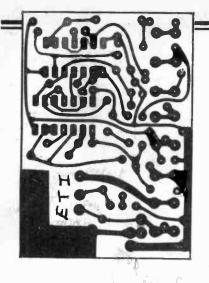
Overlay for main control board.

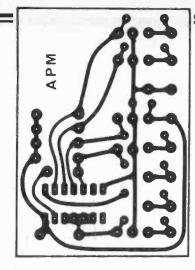


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To the far left is the foil pattern for the main control unit while left is the accessory module's PCB layout.

pulsual tugor mad "

In the quiesent state with the alarm defeated via S1 the following logic levels are present at the outputs of the gates indicated. ICla-0, IClb-1, IClc-0 ICld-0, IC2a-1, IC2b-0, IC2c-0, IC2d-1, transistor Q1 is cut-off, and RY1 is de-energized. R12, ZD1 and C6 form an overvoltage and electrical noise suppression circuit that protects the power supply rail of the circuit from spikes and battery overvoltage. The input of ICla is held at logic 1 by pull-up resistor R1. R2 protects the input of ICla from noise spikes.

If an earth appears at the inputs taken to D2 and D3 the logic 1 normally present at the input of IC1a changes to logic 0 which is inverted to a logic 1 by IC1a and connected to pin 5 of IC1b. D2 and D3 isolate the two inputs from each other. The input at D2 has a special function which is explained at the end of the text. Pin 6 of IC1b is held at Logic 0 by pull-down resist R4. R3 and C1 form a noise suppression circuit for this input. If this input goes to + 12 volts a logic 1 will be present at pin 6 of IC1b. Thus under normal conditions both inputs of IC1b are at logic 0 and in any alarm condition the input (s) will be at logic 1. Any logic 1 at the input of IC1b will force it's output to logic 0. R5 and C2 form another noise suppression circuit to increase the noise immunity and prevent any noise spikes from reaching pin 13 of IC1c.

from reaching pin 13 of ICIc. Whenever SI is in the DEFEAT position a logic 1 is present at pin 12 of IC1c and pin 1 of IC2b. This logic 1 is buffered by R9 (spike protection). With a logic 1 at pin 12 of IC1c the output of this gate will remain logic 0 and ignore the input at pin 13. The vehicles ignition system works normally with SI in the DEFEAT position. By placing SI in the ACTIVATE position an earth is placed across the contact breaker and the vehicles ignition system will be disabled. Also when SI is in the ACTIVATE position the logic 1 is removed from R9 and C4 will begin to discharge thru R8, D6 prevents C4 from discharging into IC1d.

In approximately 30 seconds C4 will have discharged to the threshold of IC2b pin 1 and IC1c pin 12 and a logic 0 will now be present at these points. The logic 0 present at pin 12 of IC1c will enable it and any alarm condition sensed by the inputs will be reflected by a logic 4 being present at the output of IC1c which is passed to IC2a pin 5. The 30 second delay after S1 changes states to the ACTIVATE position and IC1c being enabled is the EXIT delay.

ICsa and IC2b form a set reset flip-flop with the normal state as a logic 1 at pin 4 of

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IC2a. It is set by a logic 1 at pin 5 of IC2a (alarm condition) and is reset by a logic 1 at pin 1 of IC2b (defeated or timed reset/ validate condition). Once the flip-flop changes states it can only be changed back again by applying a logic 1 to the opposing input. Thus even a momentary logic 1 at pin 5 of IC2a would latch the flip-flop into the alarm status and initiate the alarm sequence. A momentary logic 1 would be generated by opening one of the vehicles doors and then closing it. When the flip-flop senses a logic 1 at pin 5 of IC2a it will change state and lock with a logic 0 at pin 4 of IC2a.

HOW

IT WORKS

When the logic 0 appears at pin 4 two things happen: First C7 will begin to discharge through R13, D4 prevents C7 from discharging into IC2a. In approximatly 15 seconds C7 will have discharged to the threshold of IC2c and a logic 0 will be present. With a logic 0 at pin 8 of IC2c the 1 Hertz astable multivibrator formed by IC2c, IC2d, R10 and C5 is enabled. Pin 10 of IC2c will alternate between logic and Logic 1 at a 1 Hertz rate driving Q1 in and out of conduction RY1 energizes and de-energizes, closing and opening the contacts. These contacts are wired thru jumper "A" or "B" providing a pulsating + 12V or pulsating earth which is connected to the horn circuit sounding the horn and raising the alarm. The 15 second delay between the flip-flop changing states (alarm detected) and the horn beginning to sound is the ENTRY delay.

The second thing that happen when the flip-flop changes states is that C3 will begin to discharge thru R7, D5 prevents C3 from discharging into IC2a. In approximately 2 minutes C3 will have discharged to the threshold potential of IC1d and a logic 0 will be present. IC1d inverts this to a logic 1 and presents it via D6 to pin 1 of IC2b reseting the flip-flop and to pin 12 of IC1c inhibiting the alarm condition (if present) from reaching IC2a. When the flip-flop resets a regenerative action takes place and beings to recharge C3 and C7. When C3 has charged past the threshold of IC1d a logic 0 will be present at it's output and IC1c will be enable in a few seconds as the small charge placed on C4 prior to the regenerative action will have discharged thru R8. If the alarm is no longer present C3 and C7 will completely charge and the alarm will reset and wait for another intrusion. If the alarm condition is still present the flip-flop will again latch and the small charges that developed on C3 and C7 will discharge thru R7 and R13 respectively

in a few seconds. Thus every two minutes the alarm will reset itself for approximately 3 seconds and then start over again. This cycle is the RESET/VALIDATE cycle

This cycle is the RESET/VALIDATE cycle and is provided to prevent the battery from being completely dicharged by a momentary intrusion. The input T(OD)2 is a special function input and is for use with the accessory protection module. When this input goes to earth C7 is immediately discharged via D1 and the alarm will begin to sound, R6 prevents IC2a from being destroyed by the pull-down action. This earth is sensed by IC1a and will latch the alarm (providing the exit delay cycle is complete). This input is verified by the RESET/ VALIDATE cycle in the manner described above. The main ACTIVATE/DEFEAT switch S1 does not affect this input making it completely independent of the main system.

Accessory Protection Module -- Theory of Operation

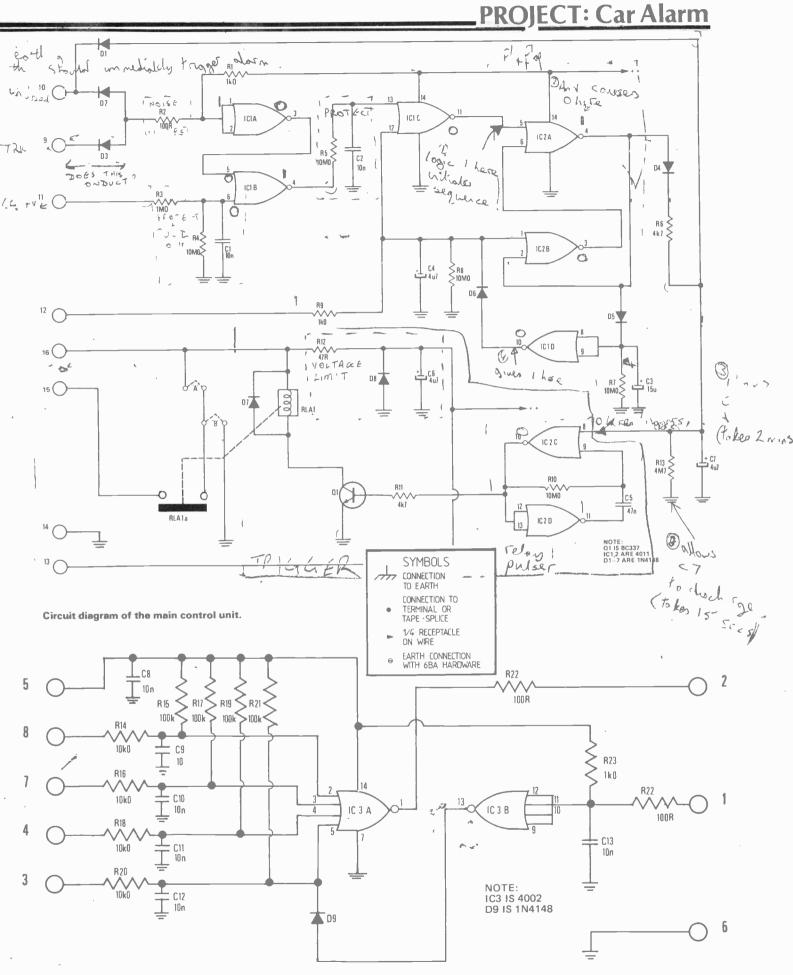
In the quiesent state IC3a output is logic 1 and the output of IC3b is logic 0. Under normal conditions, i.e. no alarms sensed, all inputs to IC3a will logic 0 (sunk to earth via R14, R16, R18, R20 and the sense wires). The input to IC3b will be open or at +12 volts, R23 being the pull-up resistor for an open circuit, R23-C13 are noise suppression components. C8 by-passes any noise present on the supply rail to earth. If any of the sense wires open R15, R17, R19, or R21 will pull the respective input to logic 1. C9 thru C12 in conjunction with R14, L16, R19, R20, for conjunction with R14, R16, R18, R20 form a noise suppression circuit for these inputs. Any logic 1 present at IC3a inputs will result in a logic 0 at the output which is connected via buffer resistor R22 to the unit's output. This is connected through ACTIVATE/ DEFEAT switch S2 to the main control unit. S2 has been provided to make the accessory protection system independent of the main system and will normally be activated continuously.

An earth at the active low I/P will force the output of IC3b to logic 1. This logic 1 is coupled via D9 to IC3a forcing pin 5 to logic 1 regardless of the status of the sense wire this will result in a logic 0 at the output of IC3a as explained above. D9 is provided to that IC3b can only force pin 5 of IC3a to logic 1, it cannot force it to Logic 0.

Any time a logic $\overline{0}$ is present at terminal () and S2 is in the activate position the alarm will sound immediately as explained in the description of the main control unit.

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New this month from Intersil, <u>the ICM 7216.</u> This is probably the most significant new IC for frequency counter/timer applications ever devised, It drives a full 8 digit display (LED)	Apart from the MC3357, mentioned alongside, Ambit has the first easy-to-use low noise, low cost UHF dual gate MOSFET - the BF960 from Siemens. With a gain of 18dB, and
and operates on inputs of up to 10MHz minimum. The single 28 pin DIL also has:- *Leading zero blanking *Frequency ratio *Period *Unit counter *Time Interval *overrange The IC cost is £19.82, and the 10MHz HC18U Xtail £2.50 (for timebase functions). The	a noise figure of only 2,8dB at 800MHz, you will see what we mean. At 200 MHz, the gain is 23dB, and NF only 1.6dB. Combine these figures with the famous ease of use of a
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4028 72p 4097 372p 4666 159b 78MGT2C %amp adjustable volts 175p 4029 100p 4098 110p 4568 281p 79MGT2C %amp adjustable volts 175p 4030 58p 4099 122p 4569 303p 79MGT2C %amp adjustable volts 175p	HA1137W/K 4420 as 3089 + deviation mute 2.20 BLR3152 Mono 4k7 impedance 100p CA3189E update with deviation mute 2.75 BLR3157 Mono 4k7/3k0 imp 100p
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HOW IT WOR RFC LEVISION

Ever wondered just how your TV actually works — all those cunningly interconnected and interrelated bits of high-voltage circuitry? Gordon King takes a good long look in this, the first of a series of How It Works articles based around consumer electronics products.

THIS FIRST ARTICLE in the 'How It Works' series looks at monochrome television based on a recent mains/ battery chassis from Thorn Consumer. Electronics. In addition to prodiding an insight into modern television technology the article is also styled to give a fair impression of how the picture is developed on the screen of the picture tube. The basic principles are common to all receivers except that for the reception of colour there are circuit additions for the decoding of the colour information (and a tricolour tube for display!)

Sound and vision signals are modulated on to two carrier waves, the former using frequency-modulation (FM) and the latter amplitude-modulation (AM). On the prevailing UK 625-line system the signals are transmitted in Bands IV and V which are located in the UHF spectrum. Each channel occupies a width of 8MHz with the sound carrier being 6MHz above the vision carrier. For example, Channel 21 has sound and vision frequencies of 477.25 and 471.25 MHz respectively,

while the frequencies for Channel 68 are 853.25 and 847.25 MHz.

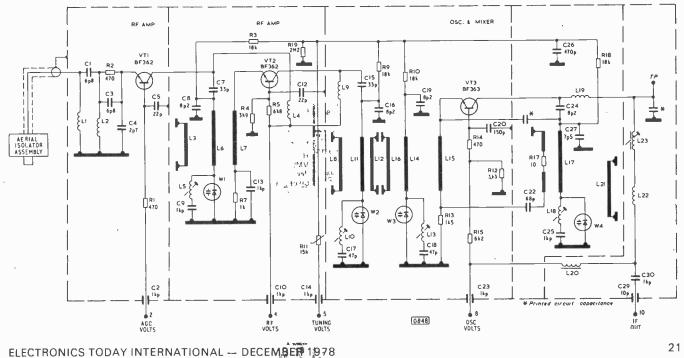
Vision modulation is negative-going (see Fig. 3) and is transmitted in 5.5MHz upper sideband and 1.25MHz lower sideband. Peak FM deviation is 50kHz (as distinct from 75kHz on FM sound radio) based on 50uS preemphasis. Ratio of peak vision to peak sound power is 5.1. Further information on the signal is given later.

Tuner-Front-End

The start of any television receiver is the 'front-end' or tuner (Fig. 1), whose job it is to select the required channel and to convert the sound and vision carriers to lower frequency ones for subsequent intermediatefrequency (IF) amplification and response tailoring. In Fig. 1 the aerial signals are coupled to an aperiodic RF amplifier, VT1, through an 'isolator' for preventing spurious mains voltages in the receiver from reaching

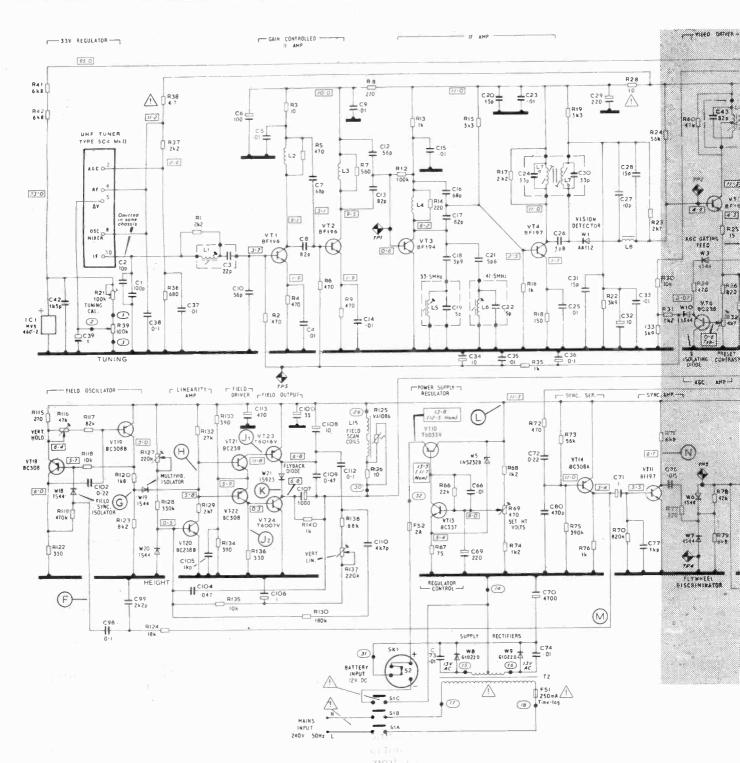
Fig 1. Circuit diagram of UHF varicap tuner, which uses two RF amplifiers and a mixer stage. Resonant lines tuned by capacitor-

diodes select the required channel and provide the necessary front-end selectivity.



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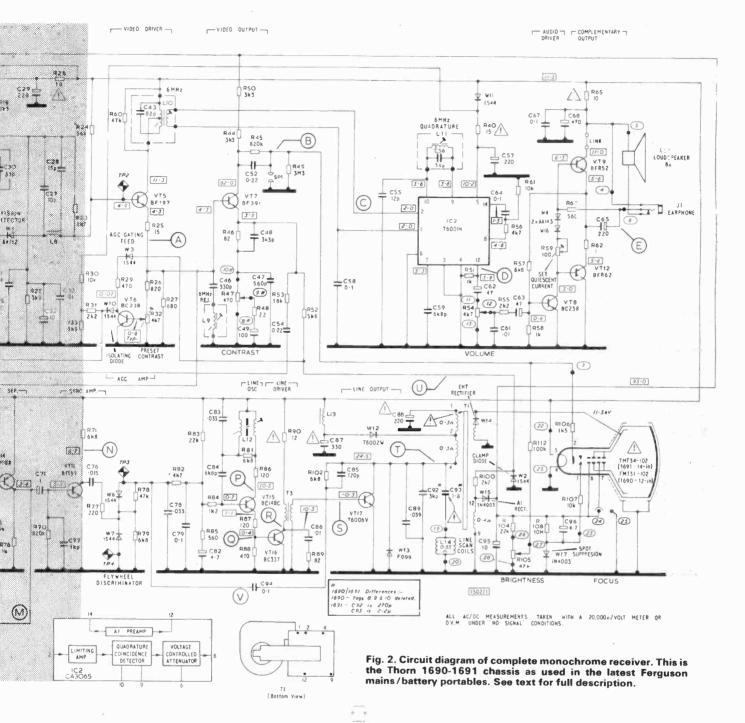
the aerial at lethal power! The transistor is in commonbase mode so that the input is applied to the lowimpedance emitter. Further input matching is provided by the emitter components and the base is biased either from a constant potential or from an AGC potential (see later).

VT2 is a tuned RF amplifier, also in common-base mode, but the tuning is by resonant lines rather than coils. Any transmission line whose length is adjusted to correspond to a tuned frequency is the equivalent of a tuned LC circuit. An open-circuit line is resonant at 1/2, 3/2, 5/2, etc. wavelength. Excluding velocity factor,

the physical length of a line for, say, Channel 33 would be around 280mm. Happily, it is possible to reduce the physical length while retaining the required electrical length by cutting off the ends of the line and replacing them with capacitance, which reduces the physical length to about 50mm. Moreover, tuning the channels then becomes a question of varying the capacitance at one end.

Looking at line L6 in Fig. 1 shows that the bottom connects to varicap W1 and the top to C8 and VT1 collector capacitance. A varicap is essentially a junction diode. As the reverse bias is increased so the depletion

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region widens, and as this constitutes the dielectric between the n and p regions. The effect is tantamount to the two plates of a capacitor being moved away from each other, with a consequent reduction in capacitance. The four varicaps in Fig. 1 are biased by a positive potential being applied to the 'tuning volts' input. The potential is obtained form a stabilised (by IC1) supply in the main chassis (Fig. 2) via tuning potentiometer R39. Thus as this control is tuned so the resonance frequency of the lines alter in step and tune over the UHF channels.

The second RF amplifier stage VT2 starts to give selectivity. Emitter coupling is via low impedance aperiodic line L7. Further selectivity is provided by the bandpass coupling between VT2 collector and VT3 emitter formed by lines L11, L12, L16 and L14, tuned

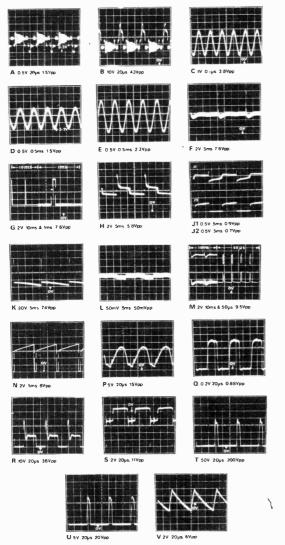
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by varicaps W2 and W3. Common-base VT3 uses collector/emitter feedback for the local oscillator tuned by line L17 and varicap W4. Line L15 couples the RF signal to the oscillator/mixer stage. The circuits are trimmed by L5, L10, L13 and L18 (so they all tune in step), while the closed lines L3, L8 and L21 also assist with the tuning and matching.

The oscillator is arranged to operate at the IF frequency above the input frequency, and additive mixing yields the IF output, which is resonated by L23 and associated components. The IF signal is coupled to the IF input of Fig. 2 via C30. The high degree of selectivity minimises spurious responses such as image, IF, repeat spot, etc., while also providing a good 3rd-order intermodulation rejection ratio. This is further

Oscillograms

These were taken from a typical receiver at the points indicated by corresponding letters in the circuit diagram. The voltage and time figures refer to the sensitivity per division of the graticule. The receiver was set up for normal reception (test card with tone on sound) and the oscillograms were taken via a \pm 10 probe having an input capacitance of 12pF in parallel with 10 M\Omega. The mixed mode timebase facility was used for G and M.



aided by the nature of the transistor and design of the first stage VT1.

The circuit also reveals various signal coupling, decoupling and isolating components, which are essential for the stable performance of this important part of the receiver. The tuner is built into a fully screened box with feed-through capacitors for the inputs and outputs.

IF Channel

Sound and vision signals of the selected channel undergo amplification with bandpass and selectivity tailoring in the IF channel comprising VT1/2/3/4. Tuner signal is applied to VT1 base from the tuned coupling L1/C3, and the amplified and bandpass defined output is yielded by transformer L7a/b. Gain is controlled automatically (AGC) to suit the level of the input signal by a bias fed to the bases of VT1 and VT2. The four stages are each in common-emitter mode, and impedance matching at the couplings is achieved essentially by capacitor divide-down.

The bandpass characteristic is provided in the main by L1/C1/C3/C10/R1 at the input and by L7a/b at the output. Additional selectivity is provided by collector inductors L2/L3/L4, while sound and adjacent channel sound rejections are introduced at 33.5MHz by L5/ C18/C19MHz and at 41.5MHz by L6/C21/C22.

With the 625 line system (system 'I' is used in the UK) the sound carrier is 6MHz *above* the vision carrier, but because the local oscillator of the tuner is working at the IF above the signal frequencies, the IF appears at 33.5MHz for sound, which is 6MHz *below* the 39.5MHz vision IF. The sound and vision signals are handled simultaneously by the IF channel, which is possible because frequency modulation (FM) is used for the sound signal. Vision bandwidth of the 'I' system is 5.5MHz upper sideband, accommodated by the IF bandwidth, and overall channel width 8MHz.

Vision Detector

Sound and vision signals from L7b are coupled to vision detector W1, which yields a changing amplitude output corresponding to the picture information (Fig. 3) and also an output at 6MHz resulting from intermodulation of the sound and vision signals by the diode non-linearity, the difference frequency of the two signals being 6MHz. The intercarrier sound signal (as it is called) retains the FM of the sound signal because this is one of the components from which it is derived.

If the ratio of the levels of the sound and vision signals is incorrect a buzz occurs on sound — called intercarrier buzz. Hence the reason for the 33.5MHz trap, which sets the sound signal level below that of the vision carrier while helping to establish one side of the bandpass. The 41.5MHz trap avoids the sound signal from the next channel causing interference while helping to establish the other side of the bandpass. The vision carrier is set 6dB down the response to equalise for the single side band signal.

Video Channel

Picture and intercarrier signals from W1 are directly coupled to the base of the video driver VT5 via low-pass filter L8/C27/C28, which removes residual IF signal. VT5 collector is loaded into transformer L10 which tunes the 6MHz intercarrier signal and couples it to the sound section for FM demodulation and subsequent pre and power amplification for driving the loudspeaker.

VT5 also serves as an emitter-follower for the video signal with network R26/R27/R32 as the load. The signal across this is directly coupled to the base of the video output transistor VT7, which feeds negative-going picture signal to the cathode of the picture tube from its collector. A series rejector L9/C46 tuned to 6MHz is also active at VT7 base to prevent intercarrier signal from getting into the video output stage, where it would cause picture interference. The level of video signal reaching the tube is adjustable by R47, the contrast control, which is a kind of current feed-back control working by the progressive shunting effect across R47 emitter resistor by R48. C49 is a DC isolator. Video-frequency compensation is also provided by capacitors in the feedback loop.

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Automatic Gain Control (AGC)

VT5 base is biased from a resistive divider complex (R24/R33/R22/etc.) from the supply rail. It is also partly biased from rectified IF signal at W1 anode, and since direct-coupling is used an increase in IF signal level results in a reduction in positive bias at VT5 base and hence a fall in potential across VT5 emitter load.

The voltage across R32 (the preset contrast control part of the load) is fed to the base of the AGC amplifier VT6 at a level established by the setting of the control. Because VT6 collector is energised via W3 from positive-going 5Vpp pulses derived from a winding on the line output transformer (bottom right-hand corner of Fig. 2, next to the picture tube), the transistor conducts only during the line sync pulses when there is no picture content which the AGC circuit might otherwise falsely read. The degree of conduction and hence the level of the collector potential are determined by the DC level of the line sync pulses at VT6 base. This is called line-gated AGC.

Thus with increase in input signal level (such as when tuning to a stronger channel) VT6 is turned down and the positive potential at its collector rises. This is reflected via forward conducting W10 to the bases of VT1 and VT2 by way of R2/R6 and the filter consisting of C34/C35/C36/R35, which removes line pulses. The small-signal transistors VT1 and VT2 are the type designed for forward AGC; that is, increased gain reduction resulting from positive-going AGC potential.

The preset contract control R32 sets the operating range of the AGC. With a test card signal of average strength the control is adjusted for 1.5Vpp picture *plus* sync signal at VT5 base.

Some sets include delayed AGC for the tuner RF amplifier which comes into effect after the gain has been reduced initially on a strong signal by the IF AGC; but for the monochrome portable this is barely necessary as maximum front-end gain is generally necessary for most of the time for the best signal-to-noise ratio when a simple set-top aerial is utilised. It will be seen that the tuner 'block' in Fig. 2 has an AGC input which, in this model, is terminated to a supply potential-divider.

Field Timebase

The electron beam needs to be deflected both vertically and horizontally to build up the raster upon which the picture appears. The vertical deflection is handled by the field timebase which deflects the beam from the top to the bottom (scanning stroke) and then very swiftly back to the top again (retrace) at 50 Hz repetition rate.

This is achieved by a 50Hz sawtooth current passing through the field scan coils (L15) on the tube neck. The oscillatory requirements are provided by the field oscillator VT18/19, which is an RC multivibrator. The retrace is initiated by the arrival of a field sync pulse at VT18 base (see later), while the repetition rate is determined by the vertical hold control R116 with R117/118 and C102.

Consider the circuit during the scanning stroke when a rising voltage (ramp) occurs at the base of high-gain amplifier VT20 owing to C104 charging through R127/128. This turns on VT20, VT22 and VT24, and turns of VT21 and VT23. At the conclusion of the stroke VT24 is fully 'bottomed', at which time a positive-going

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pulse from VT19 collector 'hits' the bases of VT21 and VT22 via the multivibrator isolating diode W19. The pulse is initiated from the field sync action. The retrace is thus triggered by VT21 and VT23 turning on, and VT22 and VT24 turning off.

During the retrace, VT24 collector voltage rises at a rate established by the L/R ratio of the scan coils, and when the supply line voltage is exceeded W21 goes into reverse conduction and VT23 is isolated. The rate of rise is then defined by C109. After a peak, the retrace voltage falls until W21 goes into forward conduction again. This allows the remainder of the retrace energy to be fed back into the supply line, after which the scanning stroke recommences.

The resulting rise in current through the field scan coils during the scanning stroke produces a magnetic field such that the electron beam is drawn downwards. To avoid vertical non-linearity fo the display the *rate of change of current* must be linear. Owing to resistive losses in the scan coils and circuit non-linearities, a slight correction to the current waveform is required, and this is achieved by a parabola waveform produced by R138/R137/C106 being added to the ramp via the linearity amplifier VT20. The degree of correction is adjustable by the vertical linearity control R137.

When the retrace is initiated the rapid reversal of scan coil current deflects the beam swiftly upwards to start a new downward scan, and during the retrace diode W20 goes hard into forward conduction so that the base of VT20 is clamped to earth.

Line Timebase

Horizontal deflection of the beam is achieved by the line timebase driving a sawtooth current wave through the line scan coils (L14) during the scanning stroke, Deflection is from left to right, and at the end of the scanning stroke a swift reversal of current deflects the beam back to its starting point again. During the retrace a considerable amount of energy stored in the inductive elements of the line output stage is released to provide the extra high tension (EHT) for the final anode and the high voltage for the first anode (A1) of the picture tube. Boosted voltage is also used to energise the line output transistor VT17 once the line oscillator has started.

Line repetition rate of the 625 line system is 15625Hz. Thus the horizontal rate is significantly greater than the vertical rate. We have seen that in the UK the vertical rate is 50Hz. This means, then, that a raster of $312\frac{1}{2}$ lines is produced (15 625/50). For a complete picture there are two vertical scans, each producing a raster of $312\frac{1}{2}$ lines, so that the complete picture is made up of 615 lines and produced every twenty-fifth of a second (in actual fact not all the lines are used for the picture as some occur during the field sync period when the electron beam is cut off).

A complete full-line-picture is achieved because the scanning lines of one field *interlace* in the spaces between the lines of the partnering field. To obtain 625 lines without interlacing the line frequency would need to be increased to 31 250Hz. This in turn would call for a greater rate of change in beam intensity and hence spot brightness to trace out the fine detail over each line, and because a greater rate of change of signal amplitude involves a greater bandwidth, more radio space would be needed to accommodate the picture detail of each

channel. With the 5.5MHz vision bandwidth of the 'l' system good definition is obtained at the 15 625Hz 'line rate.

Interlacing *could* be avoided without using up extra radio space by reducing the field rate to 25Hz, but then the picture would suffer bad flicker (subjectively apparent up to about 45Hz). Interlacing thus solves the problems of bandwidth and flicker without unduly detracting from the displayed information.

Returning to the circuit in Fig. 2, the line frequency is established by a blocking oscillator incorporating VT15 Forward base bias through R83 turns the transistor on so that the current through the collector winding of L12 rises. The reversed phase of the other winding puts a negative-going pulse on the base which cuts the transistor off. The on/off cycles are timed by L12/C83/ C84 with the oscillator in the free-running mode, the frequency being set by L12 core. The oscillator is synchronised to the line pulses of the signal (as will be explained later).

VT16 amplifies and shapes the pulses from VT15 emitter and transformer T3 couples them to the base of output transistor VT17. The pulses switch this transistor on during the scan so that current flows through the upper left-hand windings of the line output transformer (LOT) T1 and scan coils L14. Because the coils are essentially inductive the current rises as a fairly linear ramp. However, because the effective length of the beam changes with scanning stroke owing to the wide scanning-angle and flat screen of a contemporary tube, 'S-correction' is required. This is achieved by C93 which reduces the rate of scan at the start and end of a line with respect to the centre. Further linearity correction and width adjustment are provided by a closed-loop sleeve set under the scan coils. The field produced by the current induced into this counteracts the non-linearity of the field produced by the scan coils themselves

VT17 switches off at the end of a scan and the swiftly collapsing current through the scan coils and LOT windings returns the beam to its starting point and yields a high voltage pulse owing to the sudden release of the inductively-stored energy. The repetitive pulses are increased in voltage by the overwind at the top right-hand side of T1, rectified by W14 and smoothed by a capacitance formed by the inner and outer conductive layers on the tube flare, the inner connected to the final anode. The result is a potential of 11.5kV for the final anode. After rectification by W15, pulses from the lower right-hand winding charge C95 to yield a 95V line for the tube first and third anodes, video output VT7 (to provide about 50V video swing for the tube) and varicap tuning.

Oscillatory energy is rectified by the booster diode W12 conducting during the retrace to charge C87/C88. This not only damps the unwanted energy which would otherwise cause vertical lines at the left of the picture, but the potential developed from it is used to energise VT17 collector, and contribute to the line scan, thereby improving the efficiency of the line output stage. The stage also adopts 3rd harmonic tuning of the pulses. This tends to flatten the tops of the pulses, which leads to improved EHT regulation. The tuning capacitor is C89 in parallel with a low-inductance disc capacitor C92 providing flashover protection.

Sync Stages

Video signal at VT5 emitter is coupled to the base of the sync separator transistor VT14 through R72/C72. On the 625 line system the picture signal is negative-going (modulation level falling with increasing brightness), and at the end of each line a line sync pulse occurs whose tip reaches 100% amplitude, as shown in Fig. 3 a.

Composite video (picture plus sync) from VT5 emitter is fed to the base of VT14 (sync separator) which is biased to conduct only during the sync pulses so that they resolve free from picture signal at the collector. For line sync, coupling is to VT11 (sync amplifier/inverter), whose output drives 'flywheel' discriminator W6/W7 etc. The discriminator is also fed positive-going line pulses from the LOT via C94 which, after RC integration,

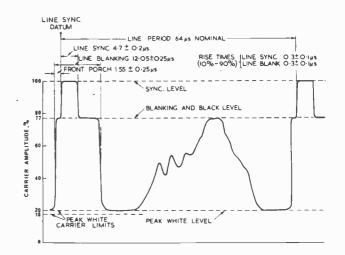
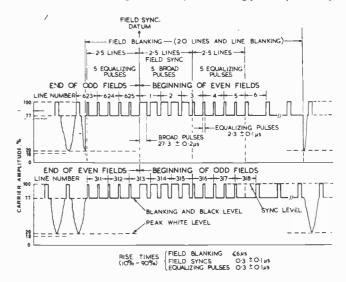


Fig. 3. BBC 625-line television signals. (a) One line of signal showing sync pulses. These keep the line scan in step with that at the transmitter, while the picture signal causes the deflected scanning spot on the face of the picture tube to change in brightness at a rate determined by the detail of the transmitted picture and by an amount governed by the brightness of the transmitted scene at any instant. (b) Pulses transmitted during the synchronising period at the end of one field scan and the start of the next (upper end of odd fields and beginning of even ones, and lower end of even fields and beginning of odd ones). The pulses provide correct interlacing while keeping the line timebase in sync during the field synchronising period (see text).



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form a ramp whose phase is compared with that of the line sync pulses. Phase error results in a potential at the top of R78 which, after being filtered by C78/C79/R82 to remove pulse residual, is applied to the line oscillator. As this is a VCO, frequency correction and hence line synchronisation are achieved.

^A^{*} From the end of one field scan to the start of the next one, five narrow equalising pulses are followed by five broad field sync pulses and then by another five equalising pulses. The width and spacing of the pulses keep the line synchronised during the field sync period, while the equalising pulses ensure equal blanking on both even and odd fields, and also identify the two fields for accurate interlacing by cutting off the picture half way through a line at the end of odd fields and starting it after a line is half over at the beginning of even fields, as shown in Fig. 3 (b).

It is worth noticing that test signals and certain teletext data are transmitted on blank lines — the latter at a bit rate of 7 megabits per second. The 1.55 and 5.8us front and back porches to the line sync pulses provide time for the line retrace, and it is the 5.8us porch which carries colour burst signal.

The positive-going field sync pulses at VT14 collector are integrated by C99/R124 and applied to VT18 base through W18. The integration builds up a composite pulse for triggering the field retrace and attenuates line pulses.

Tube Biasing and Video Feed

During normal working the tube grid is held at chassis potential by W17. When the set is switched off W17 is reverse-biased and the charge held by C96 drives the grid negative, thereby suppressing the beam, while the supply voltages collapse.

Beaming current cut-off is set by R105 (brightness control) which merely adjusts the tube cathode potential. Video signal from VT7 collector is also applied to the cathode, and as the signal is negative-going the beam current increases with increasing picture brightness. Beam cut-off or black-level is set by the brightness control so that the sync pulses drive the tube below black.

Sound Channel

Intercartier signal from L10 is fed to IC2 which incorporates a 6MHz limiting amplifier; quadrature coincidence detector tuned by L11; voltage-controlled attenuator operated by the volume control R54 and an audio preamplifier for driving the class B push-pull output transistors VT9/VT12 via driver VT8. The bases of the output transistors are driven together from VT8 collector, which is possible because VT9 is NPN and VT12 PNP (a complementary pair). Quiescent current is set by R59 at 8mA. Negative feedback is from the emitters of the output pair via R57 to VT8 base. Since the mains supply is isolated by transformer T2 it is possible to use a headphone set or earphone connected to jack J1.

For those not familiar with the quadrature FM detector the following brief description may help. After passing through the limiting amplifier chain, the intercarrier signal is changed to squarewave and the signal fed two ways. one way to a synchronous detector and

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the other way to a 90-degree phase shift circuit and thence to the synchronous detector. The synchronous or coincidence detector combines the two inputs vectorially so that the output consists of the vector sum which, relative to the fixed 90-degree phase shift, changes with the FM deviation. The result is a variable width squarewave (pulse width modulation) which, after integration, yields the audio signal.

Power Supplies

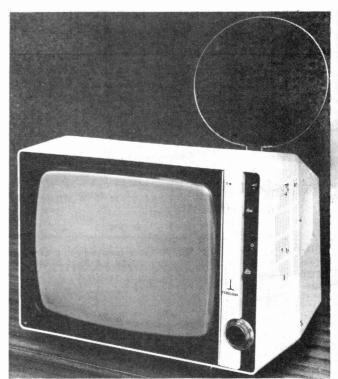
The receiver can be operated from a 12V car battery or the mains supply. On mains, isolation is provided by transformer T2 and full-wave rectification by W8/W9, with C70 the reservoir. The supply is fed to the emitter of series regulator VT10. VT13 is the error amplifier which compares a ratio of the collector output voltage with a reference potential provided by zener W5. Starting current is provided by R66 and the base potentiometer R69 sets the output voltage for the correct value of EHT voltage. Stabilisation is effective over a mains input of 220-264V. The high V_{be} rating of VT10 provides automatic protection against reversed battery polarity.

Final Points

Finally, one or two minor points: SP1 at VT7 collector is a spark gap which liberates energy in the event of a flashover inside the tube, directing current away from VT7 collector. The tube is a quick-heat type whose heater is energised from the 11.3V line and one which is happy with a relatively low focus electrode voltage.

Acknowledgement

I would like to thank Thorn Consumer Electronics and Mr. R. V. Arnaboldi and Mr. D. A. Pike of this Company for permission to use the circuit of the 1690-1691 chassis in this article.



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ELECTRONICS TODAY INTERNATIONAL

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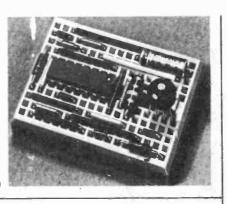
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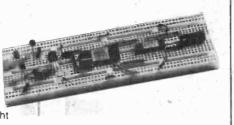
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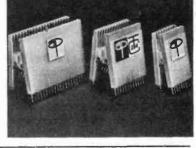
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WINE TEMPERATURE METER

Ensure your wine is at the correct temperature with this little idea from our project team

WINE, WOMEN AND SNOG - no not another misprint but ETI's updated version of that phrase that so aptly describes that which a young man's fancy turns to in spring, or any other time of year for that matter. We at ETI can't do much about the provision of the above items but this project will at least ensure that when you get your hands on one of them it will be in perfect condition. Before going any further let's make it clear that its the wine we're talking about in this connection.

In use the wine temperature meter's sensor is clipped to the plonk of your choice and the condition of the booze, with regard to temperature, read off from the three LEDs on the meter's front panel. To set up the instrument consult our table showing the range of temperatures considered acceptable



Above, the complete unit while below the sensor, a bicycle clip painted black with the sensor epoxied to it.

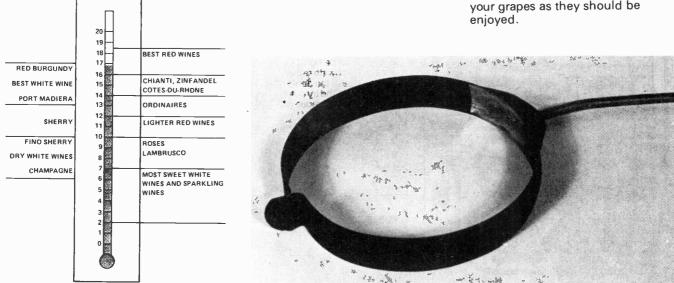
for the various types of wines. Turn RV2 fully anticlockwise and bring the sensor to a temperature that is in the middle of the desired range. Adjust RV1 until the centre LED just lights

Next lower the temperature of the sensor until it is at the lower temperature limit. Adjust RV2 until the lower LED is just extinguished.

Construction of the project is quite straightforward. Assemble all the components according to the overlay shown. Space is at a premium if the case chosen for our prototype is used so keep everything tidy.

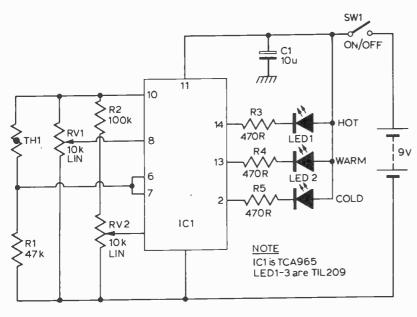
Our sensor was made from a bicycle clip. The thermistor was epoxied to the clip - we smeared a small amount of silicon grease on the clip before mounting the sensor this provides a good thermal contact. We coated the sensor in a laver of black paint when it was complete leaving the area under the sensor as bare metal.

Insert the battery and start getting your grapes as they should be



ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978

PROJECT



Circuit diagram of the wine temperature meter.

-HOW IT WORKS

The project is based on the TCA965 window discriminator IC. This device can be used in a number of different modes, the one selected for this application allows the potentiometers RV1 and RV2 to set up a "window height" and "window width" respectively.

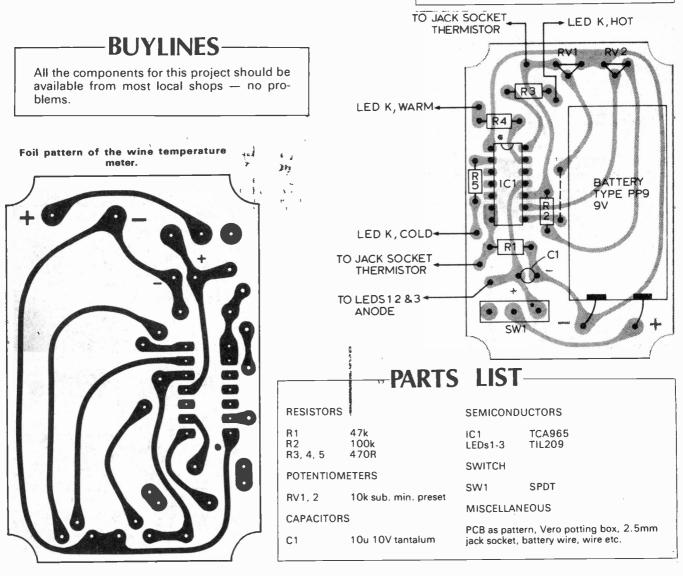
R1 and thermistor TH1 for a potential divider connected across the supply lines. The value of R1 is chosen such that at ambient temperature the voltage at the junction of these two components will be approximately half supply.

As the temperature of the sensor changes so the voltage will change and it is the temperature dependent voltage that is input to ICI.

RV1 will set the point which corresponds to the centre voltage of a windoe the width of which is set by RV2. The switching points of the IC feature a Schmitt characteristic with low hysteresis.

The outputs of IC1 indicate whether the input voltage is within the window or outside by virtue of being either too high or too low.

The outputs of IC1 are all open collectors capable of providing up to 50mA. In our circuit however they are only required to drive a LED via a current limiting resistor.



~ELECTRONICS TODAY INTERNATIONAL — DECEMBER 1978



ELECTRONICS TODAY INTERNATIONAL -- DECEMBER 1978

Video games have only been around for a short period of time. The original units were developed by the Magnavox Corporation in America, with these early units you could play any game – as long as it was Tennis! Besides being reasonably boring, they were built from dozens of seperate logic devices and cost a small fortune.

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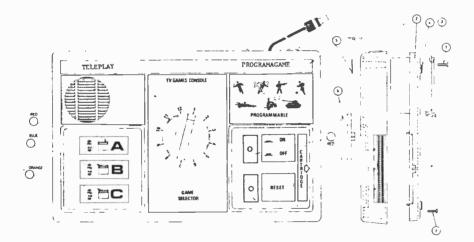
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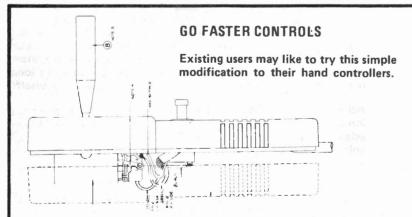
The first major breakthrough, in cost and versatility, came from General Instruments — with their introduction of the AY-8500 game chip. The now famous (and obsolete) AY-8500, allowed you to play upto six games and also produced sound effects. Since the days of the AY-8500 General Instruments have

Since the days of the AY-8500 General Instruments have produced several other dedicated devices, allowing you to race a motorbike, command a tank and even drive a Formula One racing car (to name just a few). By continually introducing new and exciting products General Instruments have become the major T.V. game device manufacturer in the World.

Every time a new game is launched the electronic magazines publish a D.I.Y. version, but you always need a new case and U.H.F. modulator. By the time you have paid for all the bits & pieces, the £10 chip has turned into a £30 project — and probably used up a lot of time.

Teleplay have developed the Programagame as the answer to the D.I.Y. enthusiasts need – for an inexpensive, easy to construct, up-to-the-moment, professional looking, full colour T.V. game system.

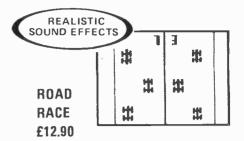




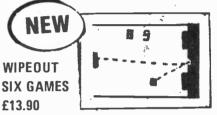
Remove the 220k resistor and 470p capacitor from each controller. Then set both joysticks to the bottom right position. Set the PRO/AM switch to give small bats, then adjust the cartridge preset until both bats are just on the bottom boundary.

This modification gives a much better feel to the controllers. You can also give the plastic sleeves a sharp tap, with a blunt instrument (the wrong end of your screwdriver), to make them fit closer to the case - this also improves the feel of the controllers.

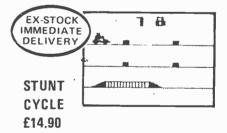
If you want to use the Road Race after making the modification, you will need to fit the two 470p capacitors inside the cartridge. They go between pins 10 & Earth and 14 & Earth.



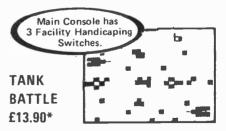
Road race has two different games inside it. The first is a two player version, with a switchable handicap on the left-hand track. The second game is you against the machine, see if you can score 15 laps without crashing! Uses the normal Joystick.



The latest game from General brought to you by Instruments. Teleplay first! Based on the popular arcade game Breakout, the cartridge has 6 games built into it. On each of the games there are 3 variables - bat size, ball size and ball speed. The is an AY-3-8606. device type The games are single and double Wipeout, single and double Breakout, two player Wipeout with barrier, and solo Wipeout (not the same as single).

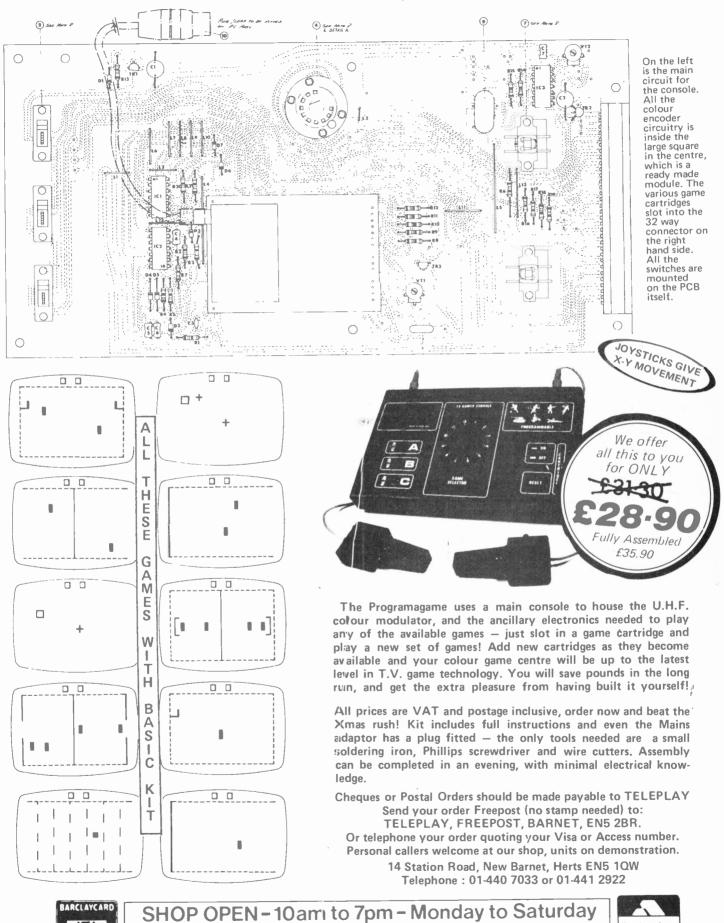


You too can be a dare-devil Stunt Rider with the AY-3-8765 and special hand controls. With 4 different games, this cartridge is bound to give hours of pleasure over Christmas and the New Year.



Complete with special hand controls but without the Tank chip. Due to extreme supply difficulties we are unable to provide any Tank chips at present. If you have one of these AY-3-8710 in your workshop why not take advantage of this £6 off offer.

COLOUR PROGRAMAGAME



CLOSE TO NEW BAR NET BR STATION - MOORGATE LINE

ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978

MESA

We welcome Access



A profile of how electronics is applied to a hobby which is essentially scale modelling. By Peter J. Thorne.

"PLAYING WITH TRAINS" is probably how most readers would describe Model Railroading, the latter being the much preferred expression. Of course, there's a heck of a lot more who do just "play with trains". Names such as Hornby Dublo or Triang bring back memories of bygone youth to many an adult.

However, the hobby is not just one of running a train around a circle of track under the Christmas tree; the mature model railroader invests a great deal of effort into scale realism of operating models, structures, scenery and track. And if you tie that need for realism into the extensive growth of electronics as a hobby in the last ten years or so, you'll see why the expert on precision scale operation is keenly interested in how electronics can help this hobby.

Or, to look at it another way, there are so many variables possible in controlling several trains on a model railroad—as indeed there is in a real one—that it's not surprising that several companies have used model railroads at trade shows to demonstrate microprocessor versatility. A recent example was discussed in Byte magazine for July 1977.

Apart from computer control, which is really outside the scope of this short article, there are several uses for both digital and analog electronics in the model train empire. Let's discuss them in stages—control, signalling, lighting and sound.

Control

Most model locomotives use 3, 5 or 6 pole DC permanent magnet motors. A few use brushless, ironless rotor motors and a very few AC motors. Power is picked up directly from the two rails, and reversal of track polarity reverses the locomotive direction except in the case of the AC motors, where an extra "kick" of AC triggers a reversing contact in the locomotive.

The Christmas train set power pack is nothing but a full wave rectifier delivering pulsating unfiltered DC to the track via a 100ohm variable resistor as speed control. This gives very poor control at low speeds for the simple reason that stall current on a permag motor is much higher than its low speed current. Consequently there's a tendency for jackrabbit starts. Now the dyedin-the wool hobbyists wants precise control of low speeds because nearly all layouts have miniature freight yards. box-cars and cabooses have couplers operated by magnet remote control so the operator can make up and break down his trains. The more or less ideal speed control-or one approach there to anyway-looks like the circuit of Fig. 1. A simpler version shows on the lead photo. This type of control has several features; the variable DC output has a pulse ripple added at lower speeds to vibrate the motor armature and reduce motor cogging and "stiction", secondly it has a low source

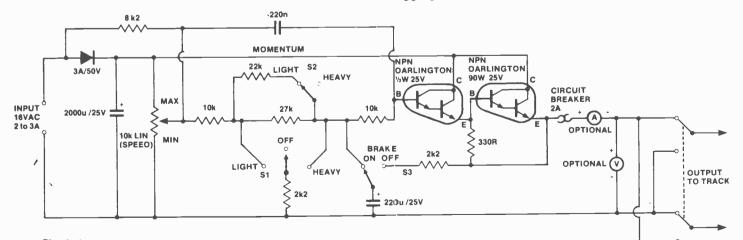
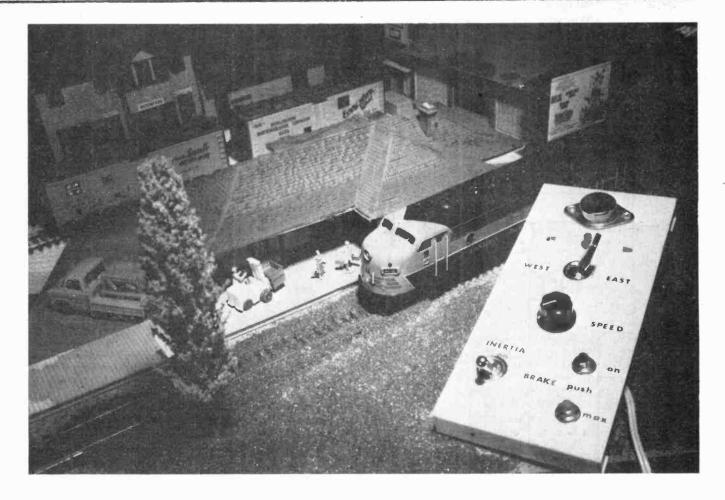


Fig. 1. An electronic speed control for model trains.

FEATURE



impedance for the motor, thirdly a delayed action can be switched in and out so that the controlled inertia of a heavy train can be simulated together with brake levers; and lastly it's short-circuitproof by virtue of heavy duty transistors and an overload trip. The last is indeed essential because short-circuits abound on the model railroad!

Though the circuit I've shown uses two darlington transisotrs, commercial versions are available, particularly from the USA, using op amps, SCR control or pulse width modulation. Even the renowned Heathkit has introduced a version. The most important feature is probably that superimposed pulse, for if it's too small in amplitude or too high in frequency, it is not effective; but if it goes too far in the opposite direction, the resulting buzz or rattle from the motor becomes objectionable. Anyway, you electronic fans with a dusty train set in your attic, dig it out, build a momentum-pulse-throttle and you just might pick-up an extra hobby!

In terms of current rating, the power pack shown should be capable of about 2A5 at 12V. This is adequate for any HO scale models, which scale 1.87, even with double heading locomotives. As you'd anticipate, the current requirements decrease with scale size—the second most popular scale is 1:160 (n for Nine mm, which is the track width) scale. Going up asize to 0 scale (1.48) many motors will need the full 2A5. By the way, in case you home computer builders are thinking "why waste money on electronics for toys" some of these "toy" locomotives retail for over £500 apiece and lately have been appreciating in value at well over 20%.

Signals

A natural for digital IC application is signaling. Model signals in two (red and green) or three aspect (red, yellow, green) with operating miniature 12V 60mA lamps are available. Until recently, relays were widely used by modellers to operate these lamps in controlled sequence and often automatically disconnected a section of track ahead of a red signal for automatic train control. The relays used were typically low resistance coils in series with the power supply to the track. When the locomotive entered a particular track section, the relay contacts closed. All model railroads use track sections from 2 to 20 feet long insulated from each other and switchable to alternate power packs. This facilitates the operation of multiple trains.

Complete model railroads still exist using these series relays for automatic control and signalling; but they're a maintenance nightmare for their intermittently proud owners. Up to date techniques use TTL gates driving red, yellow and green LED's for signals.

Relay driver ICs can be added to drive the small 12 V signal lamps if preferred and also to operate good solid 12 V relays for automatic stops and starts.

The interface between train and TTL is a little more tricky; you've noticed, of course, that the track has only two rails which are required to conduct power (in either direction) to the locomotive. The requirement to detect locomotive presence led a few years back to a widely used detector circuit known as a ''Twin-T''.

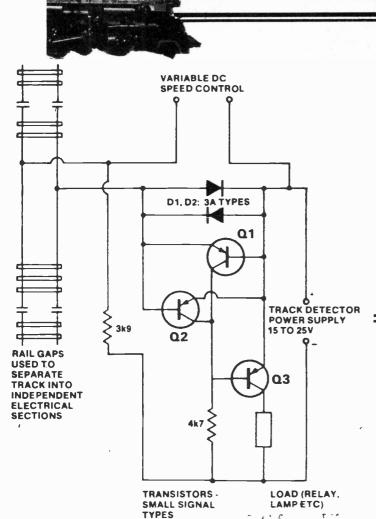


Fig. 2. Widely used "Twin T" track detector circuit, Q3's load de-energises whenever a resistance appears across track in the section being detected, regardless of whether power is connected to that track section. Consequently presence of any train or item of rolling stock can be sensed remotely.

The simple circuit is shown in **Fig**: 2. The circuit detects resistance between the rails as high as 50k, but is insensitive to the connection of the power supply in the circuit, so it will respond only to the presence of a locomotive motor or any rolling stock with a 10k to 47k resistor wired between its wheels. Other less subtle interfaces are magnetic reed switches between the track, triggered by disc magnets under rolling stock—ideal for JK flip-flop operations, or opto-electronics, where ambient light can be interrupted by the movement of rolling stock to trigger or detrigger a light activated SCR, for example.

With a light activated system, the light source and the opto detector must be angled to the track to avoid gaps between moving rolling stock causing light modulation.

All three track detection systems are, of course, suitable input interface for microprocessor control of signals . . . and track voltage, polarity, etc.

Turnout Control

Turnouts, (switches, or points) control train routing. Remote control of these, on the models as on the prototype has nearly always been electric. The usual method is the use of a solenoid motor (Fig. 5). A soft iron armature can be moved into either of two high flux

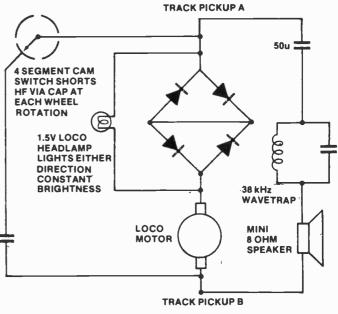


Fig. 3. These components, mounted in locomotive tender reproduces audio signals superimposed on DC motor voltage., Cam switch signals synchronization of "chuff" sound to trackside audio generator.

copper wound coils, depending on which is energised using 16 Volt AC or DC. The armature is linked mechanically to the movable track section to control the train's alternate paths. These coils of necessity are about 2 to 4 ohms resistance and hence can draw a 4 A: if left connected to the supply for more than a second or so, the 50 W of heat show—rapidly. So recently the electronically minded modeller adopted capacitor discharge.

Typically a 220 u capacitor charged to 25 V stores enough energy to operate a couple of the low resistance coils and as you can see from the circuit, there's no fire hazard if the power is left on. Also a small transformer can be used. Also shown is a method of discharging the capacitor into the coil via an SCR, which permits the controlling push button to carry only the low SCR gate current, instead of a contact-blowing multiampere current.

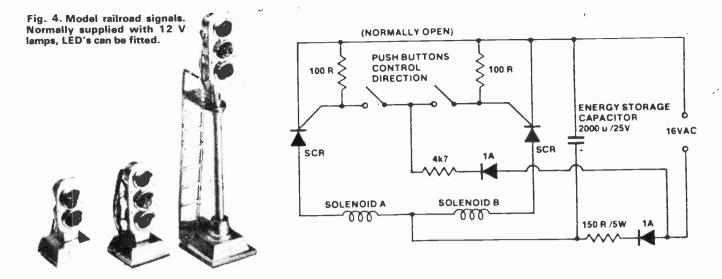
, Again, this basic control circuit is adaptable to TTL control.

Sound

Now you hi-fi fans know it's impossible to reproduce the sound of a gigantic steam locomotive without a 100 W amp and a 4 cubic foot bass reflex enclosure. Except those model railroad nuts don't believe you! Quite expensive, at about US \$350, is a Pacific Fast Mail sound unit that transmits sound and motor power through just those two rails. The sound is synchronized to the piston position, that is for a two cylinder steam engine there are four "chuffs" per driver wheel revolution. Plus bell sound and the required wailing steam chime can also be sent from the trackside to be nicely reproduced in a miniature speaker located in the locomotive tender.

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FEATURE : Trains



The PFM unit synchonizes the "chuff" sounds by transmitting a 2 V 38 kHz (approx). signal superimposed on the DC motor voltage going to the track. The DC voltage source (a transistorized circit, which is a simplified version of the circuit shown in Fig. 1) has a low resistance choke in series with its output: this prevents the 38 kHz and the audio tones from disappearing into the speed circuitry. When the 38 kHz reaches the locomotive, it is intermittently shorted out in a capacitor (see Fig. 3). The capacitor is grounded four times per drive wheel revolution via a phospor-bronze contact, which rubs on the inside of a drive wheel equipped with insulated quarter sections. As the 38 kHz signal shorts out, a relay operates in the track-side unit, sending out transistorized hiss to the locomotive-borne speaker. Being highly inductive, the locomotive motor bypasses neither the 38 kHz nor hiss-nor bell nor steam chime sounds, all of which are solid-state generated in the PFM box with full operator control. And even though the speaker is less than 2 inches in diameter, the sound is very effective.

Another electronic gimmick in the PFM system is the bridge rectifier of Fig. ³. There's a constant voltage drop of 1V4 across the bridge, since it's in series with the motor—regardless of the motor/voltage polarity. Connect a miniature 1V5 headlamp across the bridge and presto—constant brightness, regardless of motor speed.

A California based firm — Modeltronics, produces sound systems that are completely contained in the model — also synchronized for "chuff". The supply voltage for the noise generator and miniature amplifier is derived from the track voltage much as the PFM "constant lighting section". Of course, the Modeltronics system does not offer bell or chime — yet.

LED Hazard Flashers

Pop a 3mm red or yellow LED into the cabin roof of a model diesel, drive it from an internal LM3909 flasher integrated circuit, oscillating at 0.3 Hz, powered up from 0V5-3V, and you've duplicated real life on the "Atcheson Topeka and the Santa Fe".

Grade crossing flashers in model form are available ready made, with miniature 12 V lamps, just like signals. To flash, take on 555 IC timer, put one pair of lamps from IC output to + rail, another pair from output to-rail, apply 12 V, time at 20/minute and grade flashers are in business.

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Fig. 5. Capacitor discharge system enables solenoids to be thrown with small average energy. System also prevents solenoid burnup if accidentally left powered-up. SCR switch control enables small current push buttons to switch heavy current. The SCR's automatically switch off when capacitor stored charge zeroes.

Lighting

Whole passenger trains can be lit up using a supersonic generator at around 25-40 kHz. This can be fairly easily constructed using a 10 W audio power amplifier with the conventional negative feedback rephased to positive. Connected in parallel with the train motor power, with a blocking choke between the two, constant lighting can give a superb visual effect with artificial twilight on a layout. Switch off the generator — and the lights go out. Each train group of lights uses a 220n capacitor in series to block the otherwise additive lighting power from the DC motor voltage.

Radio Control and Carrier Control

As a purely personal observation, I feel the next and imminent step in electronics with model railroads is radio control. At least one experimental, but practical circuit has already been published. Taken to the ultimate, needed are very low current motors powered by rechargeable NiCd batteries together with the radio receiver, variable speed and direction controls, and sound generator circuit plus amplifier. Of necessity'the concept requires extreme miniaturization because for HO scale (the most widely used size), the space available for everything is hardly more than 5 or 6 cubic inches. The entire receiver and motor drive circuit can easily be derived from model aircraft RC designs, particularly if the new Signetics NE544 motor/servo driver chip is employed. On-board sound - for example a diesel horn sound, can use a 556 IC in the self-oscillating mode generating two tones, each around 250 Hz, amplified by an LM380 audio chip.

Individual function control is practical using 555 tone generators in the transmitter with phase lock loop decoders in the receiver. The advantage of this type of control is that the modeller has become free of the power-to-the-rails restriction.

In summary, I hope this overview shows how another hobby can adapt techniques of electronics in order to add to the fun. Maybe I've tempted you to pop round to your nearest Model Railroad emporium.

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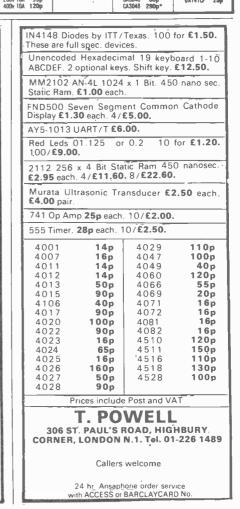


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SOUND-TO-LIGHT

Designed by Richard Bekker of Powertran, especially for ETI, this superb light show can act as strobe, linear five channel sound-to-light or random switching unit and can be digitally controlled!

OVER THE YEARS several lighting control units have appeared, some performing switching and others performing modulation of the light output according to the musical input. The Chromatheque combines both of these functions in a most original way. It is capable of controlling five banks of lamps -- of up to 500 watts each in either analogue or digital mode. By being a five channel controller not only is the sound to light modulation made more exciting than three or four channel systems by virtue of the extra colours, but linear and random sequencing between the channels gives a tantalizing effect which could not occur with a smaller number of channels.

Singled Out

Being conceived as a single board design wiring is minimal and construction very simple. All components are cheap, readily available items but a complete kit is being made available by Powertran of Andover, including metalwork.

Modes

In the analogue mode the audio signal first passes through an amplifier stage with automatic gain control. This ensures that sound to light modulation occurs smoothly even when the overall sound level changes. After this the signal is split into active filter bands the outputs of which are used to phase control triacs which determine the current in the lamps.

By doing this channel 1 (red) responds to the lowest frequencies varying the light in time with the bass notes in the music. Channel 5 (blue) responds to the highest frequencies. The other 3 channels handle the intermediate frequency bands. separate light level control is provided for each channel to allow for intensity adjustment to personal taste to suit different types of music.

Fingers and Digits

In the digital mode TTL integrated circuits are used to

selectively switch either all the lamps in strobe fashion or alternatively one lamp at a time either sequentially or randomly. The speed at which the switching is carried out is controlled either manually with a potentiometer on the front panel or automatically. In this case the switching rate increases with the level of the audio signal. This is particularly effective in the sequential or random switch positions — a crescendo sets the lights racing whilst they freeze when the music stops.

On music with a heavy beat the lights will step round one position on each beat.

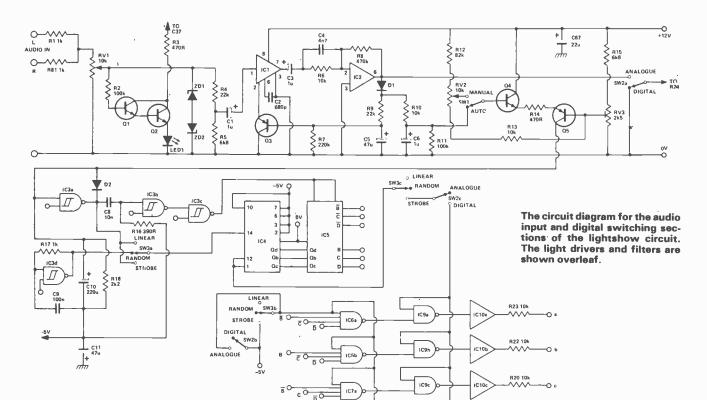
Because of the light level controls, the lamps can be turned just partially on to suit the mood of the occasion.

Construction

Start by assembling the board. This is entirely straightforward — just follow the overlay. All the potentiometers mount directly on the board though the switches are hardwired.



PRO



IC7b

IC8a

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HOW IT WORKS

Input section:

Audio is applied across RV1. Q1,2 drive a LED which indicates when excess signal is being taken off RVI. ZDI.2 clip the signal in cases of gross overload. ICI is a variable attenua-tor, the output of which is amplified by IC2. This feeds a 'diode' pump' setting up a vol-tage on C5 which rises as the output in creases. This youtage is used to control Q2 creases. This voltage is used to control Q3 which in turn controls the attenuation of ICI.

Digital section: IC3 is a block of 4 Schmidt triggers two of which are used to form oscillators. C9,R17 determine the speed of the fast oscillator and fast clock pulses are produced at pin 8. The slow oscillator rate is determined by the rate at which C10 is charged via Q5, the current through which is either varied by RV2 or else the signal on C6, depending on the position of S1. D2 is a germanium type for the benefit of SI. D2 is a germanium type for the benefit of its low turn-on voltage. In the linear sequen-cing or strobe mode the low speed clock is applied to IC4 which is a ± 2 , ± 5 counter, the outputs of which are applied to decoding ICs 6,7,8 via 4 bit latch IC5. The outputs of IC6,7,8 are taken via gates in IC9 and half of IC8 to inverters in IC10 to provide negative turn voltages to the triac driver stages. In the linear mode only one of the inverter outputs a bc de is negative at any instant whilst in a,b,c,d,e is negative at any instant whilst in the strobe mode all the outputs are at OV. In the random mode the fast clock is applied to the counter, the output of which is sampled at a low rate by means of the slow clock being applied to IC5. C8 and two trigger sections of IC3 convert the slow clock into narrow pulses suitable for this sampling. As the two clocks are independent the sampling will be at a totally random point of the count by IC4 thereby making the lamp selection truly random.

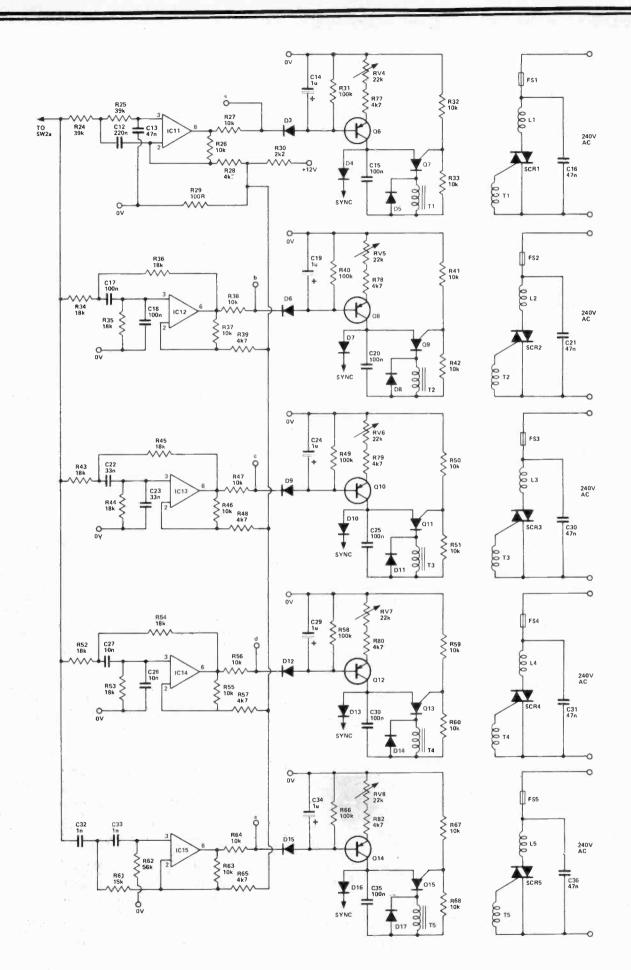


IC9d

1081

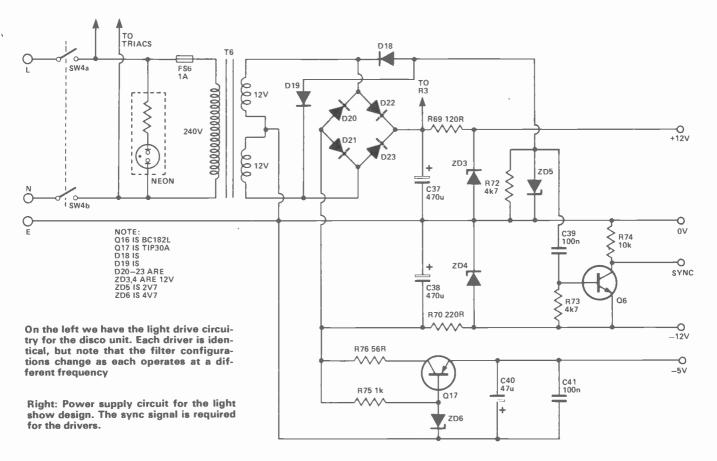
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PROJECT: Lightshow



IT WORKS HOW

Filter section:

The output of IC2 is taken to 5 active filters based round IC11-15. IC11 is the low pass suddenly conducts discharging C15 through filter, IC15 the high pass and IC12-14 bandpass. The cut-off and centre frequencies are 40 Hz, 120 Hz, 400 Hz, 1200 Hz, 4 KHz. R29,30 of the 50 Hz mains cycle a sync. pulse is are used to bias the filters to give a small generated which discharges C15 via D4. For a negative offset voltage at the outputs which given charging, current C15 will always are applied to the triac driving stages. This reach 6 V at the same point in the mains means that the series diodes are biased on cycle. We therefore have phase control and control of the lamp can start even when the signal level is very low thereby improving the smoothness of the modulation. Triac drivers:

All 5 stages are identical so only the low IC11 charges C4 via R27,D3. The voltage

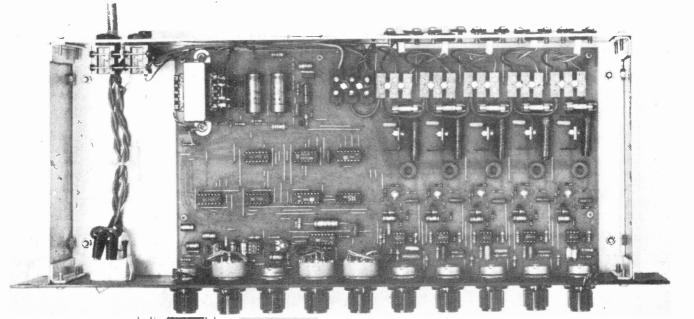
across C4 causes Q6 to conduct and charge C15. When this reaches about 6 volts PUT Q7 transformer T1 generating a pulse to turn on the triac SCR1. At the zero voltage point which is dependent on Q6 current which in turn is dependent on the audio signal level and the setting of RV4. Phase control is used in preference to burst control because of its superiority in producing smooth flicker free frequency one will be considered. Signal from modulation of the lamps. Filtering of the switching surges is performed most effec-

tively by C16,L1 and the RF interference generated is substantially less than that from a domestic light dimmer. Syncing:

To generate the 100 Hz sync pulses the 12 V AC output of T6 is full wave rectified by D18, 19 and without smoothing is applied to ZD5 across which is produced a spikey waveform. This is then applied via C39 to Q16 which is sufficiently turned on by the spikes to sink the charge on C15.C20 etc.

Power supply:

Highly stable voltages are unnecessary and the 12 V lines for the op. amps are taken off simple zener regulators whilst the TTL-5 V line is regulated by a single series transistor 017



PARTS LIST-

		CENICONDUCTORS	
RESISTORS 1/4W 5% exce	ptwhere stated	SEMICONDUCTORS Q1, 2, 4 16 Q3, 5, 6, 8, 10, 12, 14	BC182L BC212L
R1, 17, 71, 74, 81	1k	Q7, 9, 11, 13, 15	BRY39
R2, 11, 31, 40, 49, 58, 66	100k	Q17	TIP30A RA Trian
R3, 14	470R	SCR1-5 IC1	8A Triac MC3340p
R4, 9 R5, 15	22k 6k8	IC2, 11-15	741
R6, 10, 13, 19-23, 26, 27,	10k	IC3	74132
32, 33, 37, 38, 41, 42, 46	TOR	IC4	7490
47, 50, 51, 55, 56, 59, 60,		IC5	7475
63, 64, 67, 68, 73	_	IC6-8	7420
R7	220k	109	7400 7405
R8	470k	IC10 D1, 3-19	IN4148 or IN4151
R12 R16	82k 390R	D2	0A95
R18, 30	2k2	D20-23	IN4002
R24, 25	39k	ZD1, 2, 6	4V7 zener
R28, 39, 48, 57, 65, 72,	4k7	ZD3, 4	12V zener
76-80		ZD5	2V7 zener
R29	100R		
R34-36, 43-45, 52-54 R61	18k 15k	SWITCHES	
R62	56k	SW1-3	4p 3w adjustable stop
R69	120R 1/2W		rotary
R70	220R 1/2W	SW4	illuminated mains switch
R75 .	56R 1W		' DPDT 10 Amp
	1		
POTENTIOMETERS	1	TRANSFORMERS	
RV1	10k log 11 11	T1-5	FX3008 with 10 turns 35g
RV2	10k lin PCB mounting	Т6	for both windings 240V to 15V-0-15V at
RV3 RV4-8	2k5 preset → 22k lin '' ''	10	200mA
1040	228 111		
CAPACITORS		INDUCTORS	
C1, 3, 6, 14, 19, 24, 29, 34	1 1u 63V electrolytic	L1-5	FX1089 with 40 turns 25g
C2	680p polystyrene or ceramic		
C4	4n7 polystyrene	FUSES	
C5, 11, 40	47u 10V electrolytic	F1-5	2A fast
C7	22u 25V electrolytic	F6	1A anti surge
C8, 27, 28	10n polycarbonate		
C9, 15, 17, 18, 20, 25, 30, 35, 39, 41	100n polycarbonate		
C10	220u 4V electrolytic	MISCELLANEOUS	
C12	220n polycarbonate	Two ¼" mono jack sockets 13A mains cable, cable cl	s, 5 cooling clips, amost ive 3 ter-
C13	47n polycarbonate	minal FA connector blocks	3 terminal 10A
C16, 21, 26, 31, 36	47n 400V polycarbonate 33n polycarbonate	connector block, fibre glass	ready drilled PCB,
C22, 23 C32, 33	1n polystyrene	metalwork to suit ten kn	obs, grommets,
C37, 38	470u 25V electrolytic	spacers, nuts, bolts etc.	

Use 3" lengths of coloured wire for these. The switches supplied in Powertrain kits are of the adjustable stop variety. The tag on the stop plate goes in the hole stamped 2 for two way switches and the hole stamped 3 for the 3 way switch.

Mains transformer T6 is bolted onto the board and the 15 V windings connected to the Plug in the unit between your board by means of short wire links from the tags down to the holes directly beneath them.

Pulse transformer T1-5 you wind yourself. Wrap round the ferrite rings 10 turns of 35g wire for both the primary and secondary. It doesn't matter which you call the start or the finish of the windings as the circuit operates with them either way round. The wire supplied in the kits is self fluxing polyurethene covered and can be soldered directly to the board.

Wind coils L1-5 with about 35 turns of 25g wire. A smear of glue on the windings will help them stay in place before

fitting and reduce buzzing when in use. The triacs are kept cool by means of a finned tab bolted to each of them. The outputs to the lamps are taken from the board via connector blocks screwed to the board and linked to it with short lengths of 18g wire.

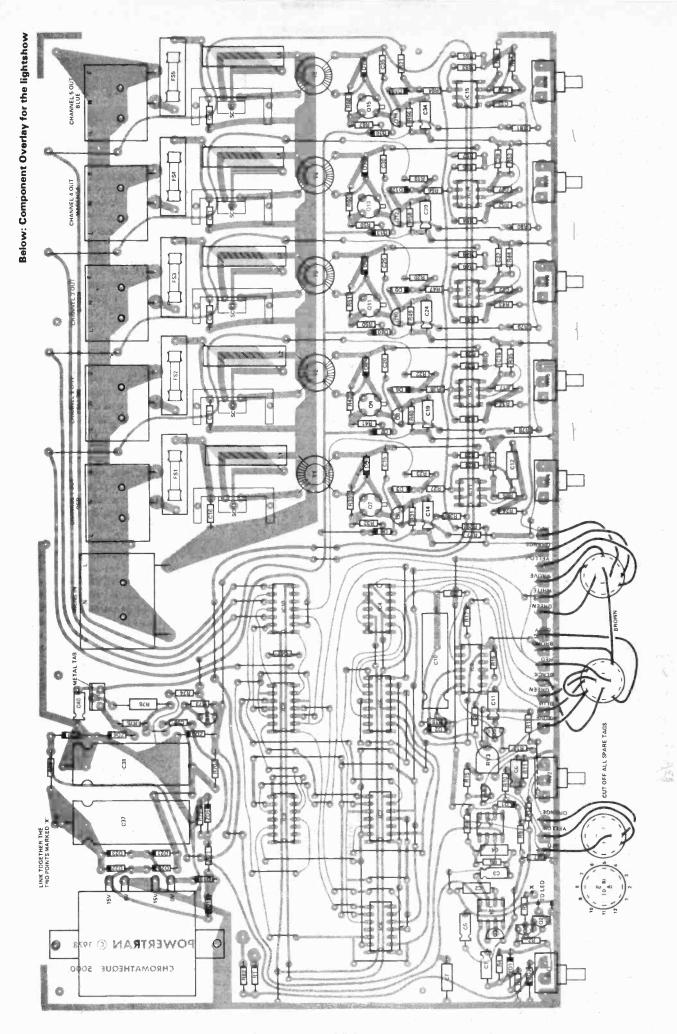
Testing and Setting Up

amplifier and speakers, wire in the lamps securing the cables with the clamps on the rear panel, turn all controls anticlockwise, switch on and set auto level to where the LED only comes on occasionally. Switch SW2 to A and turn up the level controls and watch the lamps operate smoothly in time with the different frequency bands in the music. Switch SW2 to D, SW3 to S, SW1 to A, adjust the level controls for the lamps to be equally turned on by the strobing and set the one and only pre-set (RV3) for a strobe rate as fast as the lamps will follow.

ET

BUYLINES

A complete kit of parts including metalwork is to be made available by Powertran Electronics. Address from the inside front cover. The PCB will be available only from them as it is their design. All components are available separately.



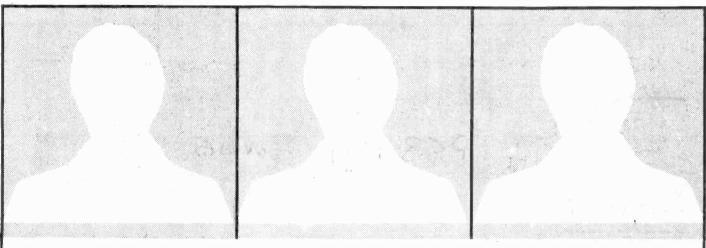
ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978

RAT



Last month we advertised for someone to fill the position of Editorial Assistant, and we are still receiving applications for that. However our expansion plans now mean we need three additional recruits!

ETI NEEDS YOU!



IF YOU have a genuine interest in electronics and project building and an above-average ability to express yourself in writing, you could be the person we're looking for. We are being serious.

We are looking for someone to join the editorial team and reckon that an enthusiastic reader is likely to be the type to join us. Not an uncritical reader - we want to continue to improve. The work will entail dealing with articles and news - licking them into shape - and making them better than anyone else's articles and news. The applicant will work on both ETI and our new sister publication Hobby Electronics. Readers employed in journalism at the moment will be considered but we are not primarily looking for someone with magazine experience.

We are flexible about age and experience but imagine that the person who gets the job will be between 21 and 28.

Salary will depend upon age and experience but will be in the range £3,700 to £4,100, possibly more for someone with exceptional qualifications.

Experience has told us that people who read ads like this think a) that it doesn't apply to them b) that their own knowledge is far too limited or c) that ads of this type are only put in because we have to fill half a page. None of these is true. Editorial Assistant (Home Computing):— in order to complement and add to our existing staff skills we are looking for someone with a real knowledge of this everexpanding field. Everyone here at ETI is fascinated by the field — PET nearly stopped the magazine dead — but we feel we need a person who has a broad overal knowledge of- the systems around today and the principles behind them, in order to assist with the magazine generally and our 'Computing Today' supplement in particular.

Salary in the range £3,700-£4,100. Age flexible.

Project Engineer:— the person who fills this position will be able to design and build up projects to the standard of finish ETI readers are used to seeing in their magazine. This calls for someone with a good knowledge of circuit design, and with the patience to carry the design through to a finished state. Existing staff are available to assist in all aspects of design work. The easiest part of the job will be writing up the project once it is completed. None of the present ETI staff were journalists previous to joining, and no-one has found the writing a difficult task.

One again we have no preconceived notions of age required, and salary will be negotiable upwards from £4,000.

Apply in writing to: Halvor Moorshead, Editor, Electronics Today International, 25-27 Oxford Street, London W1R 1RF.

Applications should reach us as soon as possible with C.V. Prospective applicants may telephone the Editor for further details but this must be followed by written application.

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INDEX 78

INTRODUCTION

IT WAS APRIL last year when we last provided an index of our own efforts. That one went right back to our first issue in April 1972. This month's brings us once more up to date. In future these listings will appear each December issue (there's long-term planning!).

Producing a definitive index is not simply a matter of reading from the contents pages and rearranging to nice neat alphabetical order. There will be some items which can be classified in several ways, and which are usually entered more than once as a result. All articles here are included just once for simplicity.

All articles, except Tech-Tips and the news features, are included in the index. Projects are simply listed consecutively, whilst the features are divided into categories for ease of reference.

Computing Today is a separate entity from ETI, and articles appearing within it are not eligible for inclusion in our index.

Projects

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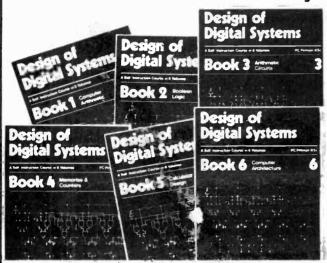
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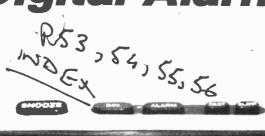
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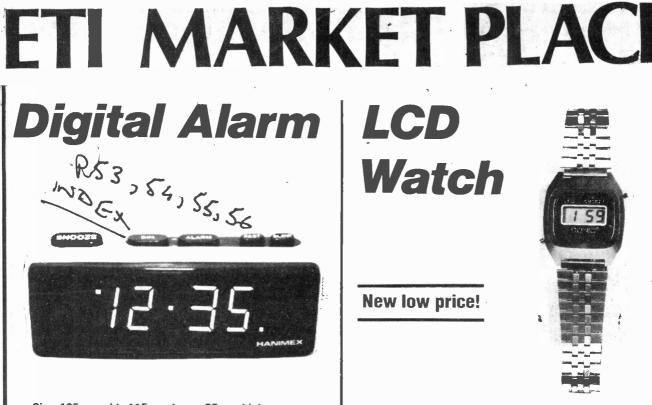
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What to look for in the January issue: On sale Dec 1st

ELIMINATOR

Fed up with low quality records? Had a hard day and dropped your favourite LP? Kiddies used Bach for target practice?

We can help — do not despair. Next month we present a design to remove the clicks and scratches from records. The system works in a novel manner, and the system can be built at a fraction of the cost of commercial units.



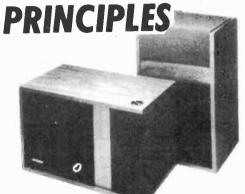
DIGITAL TACHO

Compact, easy to build, 10 rev resolution, fast response due to PLL technique and a range to 9999 rpm. With all that going for it how can you afford to miss it? Suitable for standard, CDI, and transistor assisted ignition systems.

LOG/EXP CONVERTER

This design can be set up for either log or exponential convertion, and incorporates a neat heater for temperature stability. Has an eight octave range.

Articles mentioned here are in an advanced state of preparation but circumstances may affect the final contents.



LOUDSPEAKERS

An article to explain what goes on behind the grilles on those large wooden boxes dominating the living room. All the major types will be covered, moving coil electrostatic piezoelectric etc, as well as explanations of the different methods of 'loading' the units to do their job better.

computing today no 3

NEWBEAR'S BEARGAGS are an economical way of adding extra power to any small system. Next month we take a look at a typical bag — the petitevid VDU II kit.

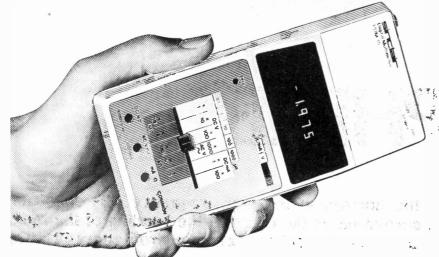


BASIC II

Tandy's level two BASIC upgrade for TRS-80 machines is now available in this country — what extra power does this conversion provide?

COMPUTERS IN BUSINESS. A look at how one small businessman uses a microcomputer at work.

The Sinclair PDM35. A personal <u>digital</u> multimeter for only £29.95



Now everyone can afford to own a digital multimeter

A digital multimeter used to mean an expensive, bulky piece of equipment.

The Sinclair PDM35 changes that. It's got all the functions and features you want in a digital multimeter, yet they're neatly packaged in a rugged but light 'pocket-size case, ready to go anywhere.

The Sinclair PDM35 gives you all the benefits of an ordinary digital multimeter – quick clear readings, high accuracy and resolution, high input impedence. Yet at £29.95 (+8% VAT), it costs less than you'd expect to pay for an analogue meter!

The Sinclair PDM35 is tailormade for anyone who needs to make rapid measurements. Development engineers, field service engineers, lab technicians, computer specialists, radio and electronic hobbyists will find it ideal.

With its rugged construction and battery operation, the PDM35 is perfectly suited for hand work in the field; while its angled display and optional AC power facility make it just as useful on the bench.

What you get with a PDM35

 $3\frac{1}{2}$ digit resolution. Sharp, bright, easily read LED display, reading to ± 1.999 . Automatic polarity selection. Resolution of 1 mV and 0.1 nA (0.0001 µ Å).

Direct reading of semiconductor forward voltages at 5 different currents. Resistance measured up to 20 Mm. 1% of reading accuracy. Operation from replaceable battery or AC adaptor. Industry standard 10 M(1) input

impedance. Compare it with an analogue meter!

The PDM 35's 1% of reading compares with 3% of full scale for a comparable analogue meter. That makes it around 5 times more accurate on average.

The PDM35 will resolve 1 mV against around 10 mV for a comparable analogue meter – and resolution on current is over 1000 times greater.

The PDM35's DC input impedance of 10 M Ω is 50 times higher than a 20 k Ω /volt analogue meter on the 10 V range.

The PDM35 gives precise digital readings. So there's no need to interpret ambiguous scales, no parallax errors. There's no need to reverse leads for negative readings. There's no delicate meter movement to damage. And you can resolve current as low as 0.1 nA and measure transistor and diode junctions over 5 decades of current. THOSE Technical specification (+8%)

DC Volts (4 ranges) Range: 1 mV to 1000 V. Accuracy of reading $1.0\% \pm 1$ count. Note: 10 M α input impedance. AC Volts (40 Hz-5 kHz) Range: 1 V to 500 V. Accuracy of reading: $1.0\% \pm 2$ counts.

DC Current (6 ranges) ³Range: 1 nA to 200 mA. Accuracy of reading: 1.0% ± 1 count. Note: Max. resolution 0.1 nA.

Resistance (5 ranges)

Range: 1(1 to 20 M(1). Accuracy of reading: $1.5\% \pm 1$ count. Also provides 5 junction-test ranges. **Dimensions:** 6 in x 3 in x 1½ in. **Weight:** 6½ 07. **Power supply:** 9 V battery or

Sinclair AC adaptor. Sockets: Standard 4 mm for resilient plugs.

Options: AČ adaptor for 240 V 50 Hz power. De-luxe padded carrying wallet. 30 kV probe.

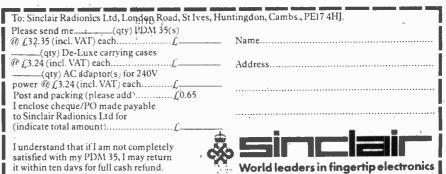
The Sinclair credentials

Sinclair have pioneered a whole range of electronic world-firsts – from programmable pocket calculators to miniature TVs. The PDM35 embodies six years' experience in digital multimeter design, in which time Sinclair have become one of the world's largest producers.

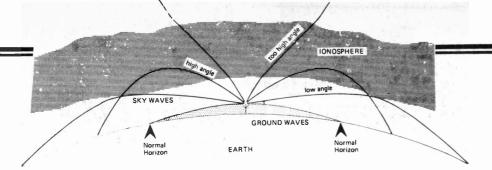
Tried, tested, ready to go!

The Sinclair PDM35 comes to you fully built, tested, calibrated and guaranteed. It comes complete with leads and test prods, operating instructions and a carrying wallet. And getting one couldn't be easier. Just fill in the coupon, enclose a cheque/ PO for the correct amount (usual 10-day money-back undertaking, of course), and send it to us.

Sinclair Radionics Ltd, London Road, St Ives, Huntingdon, Cambs., PE17 4HJ, England. Regd No: 699483.



FEATURE



IONOSPHERE

Radio communications beyond the horizon in the high frequency (HF) spectrum between 3 MHz and 30 MHz are carried on as the result of the bending of the radio waves in the ionosphere, that region of our atmosphere extending from about 60 km to about 1000 km above the earth.

THE IONOSPHERE CAN bend radio waves so that they return to earth from hundreds of kilometres to many thousands of kilometres distant.

Without the existence of the ionosphere, long distance radio communications, shortwave broadcasting, amateur radio 'DX' etc. would not be possible — and one G. Marconi would probably have died an unknown pauper!

The ionosphere enables shortwave radio stations such as Radio Peking, The Voice of America etc to broadcast programmes across the world. It enables radiotelephone communications to ships at sea and contact with international aircraft.

The Solar Prime Mover

The sun, which dominates almost every phase of our lives, influences all HF radio communications beyond the horizon. The sun generates the ionosphere; solar activity has a considerable influence on this area of our atmosphere and thus affects propogation of HF radio waves.

lonisation of the upper atmosphere is brought about largely by unitraviolet radiation from the sun, along with solar X-ray radiation. This solar radiation strips electrons from the atoms of the rarified atmospheric gases existing in our upper atmosphere.

The result is not a single, thick region of 'band' ionisation, as you may suppose. The ionosphere separates into several readily defined regions having varying densities, located in layers at different heights.

Each layer has a relatively dense region, called the *peak* of the layer, the ionisation tapering off above and below this region. The peak is not necessarily located in the centre of the layer, nor does the ionisation always disapper completely between layers.

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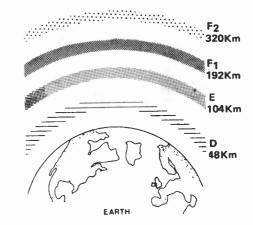
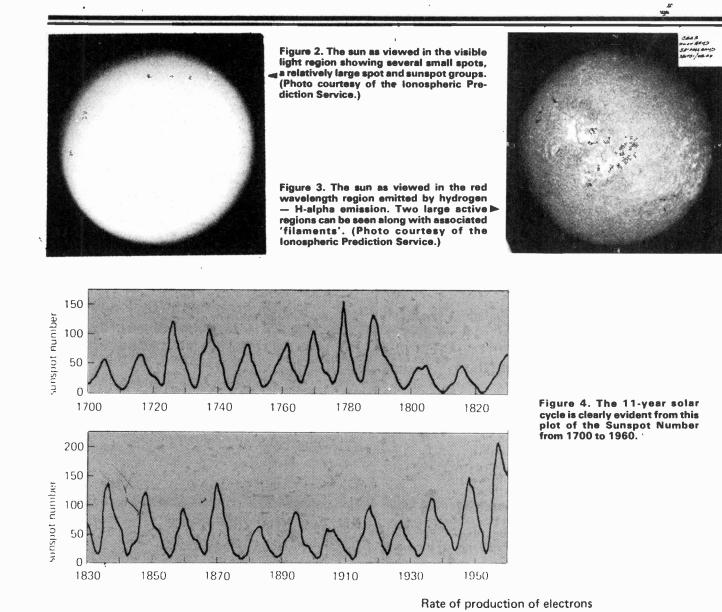


Figure 1. The ionosphere divides into readily defined regions which have been designated as illustrated here. The amount of ionisation in each layer varies diurnally (i.e.: throughout the day), seasonally (through the year) and through the 11-year sunspot cycle. Disturbances on the sun have a variety of effects on the ionosphere and thus on radio communications.

Spotting Good Propagation

The sun's UV radiation output varies over an approximately 11-year cycle, greatly influencing the behaviour of the ionosphere. For many years this cyclic behaviour of the sun has been monitored by means of sunspots - dark areas which appear on the face of the sun, and over the last two decades, by measurement of the solar flux (RF noise radiation) at 2800 MHz (10.7 cm wavelength).

Sunspots are enormous areas on the sun's surface which are cooler, and thus do not appear as bright as the surrounding area, Hence they look like 'spots' on the face of the sun. Their size can range from several hundred kilometres across to greater than 100,000 km. By comparison, the earth's diameter is only 13,000 km.



gas concentration rate of production of electrons strength of ionising radiation

Fig. 5. How a layer of electrons is produced when ionising radiation comes from above the atmosphere. The gas concentration increases with decreasing height while the radiation strength decreases. Peak production of electrons occurs at the height where the curves cross.

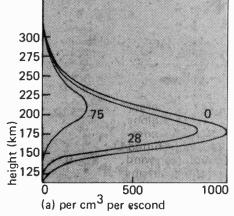
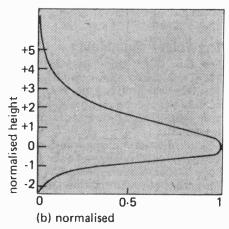
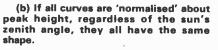


Fig 6. (a) Theoretical 'Chapman' layers showing how electron production is affected by the angle of the sun's rays best when sun is overhead (o° zenith angle).





Records of systematic sunspot observations date back some 300 years. However, reasonably reliable data is only available since about 1850.

The sun is monitored continuously from a number of observatories around the world. Sunspot observations are statistically smoothed to provide a continuous record — this is termed the Zurich Sunspot Number, which is a statistical 'fudge factor' on which ionospheric propagation predictions are based. More of this later.

On the Spot

Sunspot Number does not mean 'numbers of sunspots'. It is a statistical term which allows comparison with past figures and provides an index of sunspot activity.

The sunspot number has a cyclical variation with a mean period of 11 years. Periods between sunspot peaks have been as short as nine years and as long as 13 years. The sunspot number between the peaks and minimums of the cycles also vary greatly. The sunspot cycles have been 'numbered', for the conveneince of reference, back for 200 years. Ccyle 18 peaked in 1947, cycle 19—the biggest on record — peaked in 1957 with a sunspot number in excess of 200. Cycle 20 peaked in 1969 reaching a sunspot number of about 120, which is about average intensity.

If you thought the DX wasn't anything spectacular in 1969-70, you should have been around in 1907 when the sunspot number barely reached 60 during the peak!

Sunspot cycle minimums don't always reach zero levels. Some minimums however have shown little or no activity for many months.

The sunspot cycle, while having an 11-year mean period as observed between peaks, has been identified in recent years as actually being a roughly 22-year period based on the magnetic field variations of the sun. Alternate sunspot cycles show a pole reversal in the solar magnetic field.

Solar Disturbances

On occasions, the surface of the sun is disturbed by sudden 'storms'. These disturbances are not normally visible but are readily detected when the sun is viewed at a particular red light wavelength, known as H-alpha, emitted by hydrogen.

These very intense, localised outbursts increase very rapidly to a peak taking a minute or less, and then the intensity of the H-alpha emission decreases to its normal value in about half an hour or so.

This phenomenon is called a *solar flare*, usually occuring near, or associated with, a sunspot.

Solar flares generate enormous amounts of energy, and increased solar X-ray radiation from these regions cause disturbances to the ionosphere and to communications. Electrons and protons are also emitted from solar flares, and these travel through solar wind towards the earth. The particles are emitted in a stream and are much more numerous tha move at greater velocities than those particles contained in the normal solar wind.

Upon reaching the region near the earth these particles have a considerable influence on the earth's ionosphere and magnetic field, producing sudden and dramatic changes as well as precipitating other events such as aurorae — which will be described in more detail later.

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Apart from flares, disturbances not associated with sunspots also cause disturbances to the ionosphere and the earth's magnetic field. *Hot Spots* — which are of longer duration than flares, are emitting regions on the sun's surface that expel streams of particles which affect the ionosphere. These, and other areas on the sun's surface which emit persistent streams of particles, have longer durations than flares but the effects of the particles emitted is less severe.

Formation of the lonosphere

As mentioned previously, the ionosphere is produced principally by ultraviolet radiation from the sun. The amount of ionisation produced is almost wholly dependent on the strength of the UV radiation and its wavelength. Different wavelengths of the radiation ionise different gases.

The process of ionisation absorbs energy from the UV wave, and as the radiation proceeds down through the atmosphere, it is almost completely absorbed in this way.

This process of creation of ions and free electrons in the ionosphere is offset by recombination which is continually taking place between the two to form neutral atoms once again.

In the lower atmosphere, the molecular density is so great that recombination occurs almost immediately after ionisation, the rate of recombination is very rapid. However, in the upper atmosphere, where the number of molecules is very much smaller, the chances of a free electron meeting up with an ion is very much less. Hence, recombination occurs at a much slower rate.

These two opposing mechanisms result in regions in the upper atmosphere where a large amount of ionisation is present, the amount being determined by the balancing forces between the rate of ion production and the recombination rate.

The gases of the upper atmosphere which the solar UV radiation meets first are very rarified, hence little ionisation results and little of the radiation energy is lost. As the radiation penetrates further, the molecular density of the gases increases and hence the ionisation increases.

Height Maximum

More and more energy is extracted from the ionising radiation as it penetrates further and at some stage the amount of ionisation which the radiation can produce begins to decrease. There is thus a certain height at which ionisation is maximised. The region around this height is known as an ionisation layer.

This is how the ionosphere comes to derive its name. It is the region of the upper atmosphere where appreciable ionisation can take place.

The lower limit of the ionosphere is about 50 km and it extends to beyond 1000 km.

' Sydney Chapman, a British scientist, investigated the production of ionisation in the early 1930s and showed that the rate of production of ionisation would vary with height as shown in figure 6. The corresponding layers of electrons have been called Chapman layers.

The height of the 'peak' is determined by the concentration at particular heights of the atmospheric gas and by the ability of the gas to absorb the solar radiation. The less easily absorbed wavelengths of the radiation penetrate lower in the atmosphere before forming a layer of electrons. The *height* of the layer does *not*

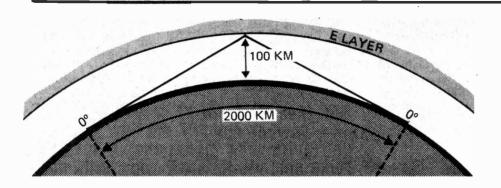
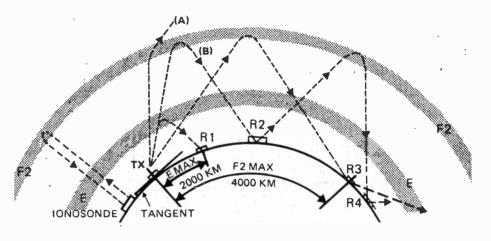


Fig. 7. Geometry of E-layer propagation. As the layer height is about 100 km, low angle radiation from a transmitter will reach distances of about 2000 km maximum.

Fig. 8. The transmitter (TX) radiating RF at several different angles illustrates how signals are propagated by the various layers. A wave radiated at a high angle will be deviated by one or both of the layers, but unless the layer is dense enough, will pass through (A). A ray at a lower angle (B) will skip a relatively short distance and may do so several times (R2-R4 etc). A low angle ray from TX will skip a maximum of 4000 km from the F2 layer (TX to R3) and subsequently further. The ionosonde measures the heights and critical penetration frequencies of the layers vertically.



depend on the strength of the ionising radiation.

The production rate of electrons at the peak of the layer depends on the strength of the ioning radiation and on its direction of arrival. When the radiation is vertically incident on the layer, ionisation is maximum, less when it arrives at an angle.

When curves representing the production rate of electrons of all possible shapes are 'normalised' with respect to the layer peak, they all look the same.

The Three Regions

There are three main regions of the ionosphere. They are designated by the symbols 'D,' 'E,' and 'F.' The F-layer actually divides into two layers, F_1 and F_2 , which I will go into shortly.

The structure of the ionosphere varies widely over the earth's surface as the strength of the sun's radiation will obviously vary with geographical latitude.

The D-layer

This is a region of low ionisation density which does not show the well-defined 'peak' of maximum ionisation density associated with the other layers.

The D-layer only appears during daylight hours and extends rather diffusely from about 50 km to about 90 km. The density of electrons in the D region is generally insufficient to cause appreciable bending of radio waves but they do suffer considerable attenuation in passing through this region.

Solar X-ray radiation with wavelengths less than about 20 Angstroms contributes to some of the ionisation in the D-layer. This radiation can ionise all the gases present at these heights in the atmosphere, but this alone does not account for the level of free electrons found in this region.

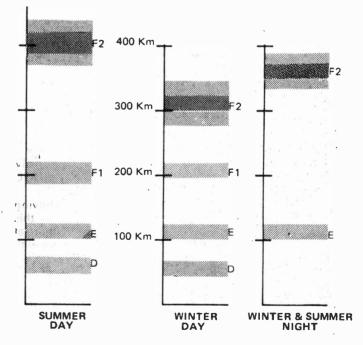


Fig 9. Illustrating the diurnal and seasonal variations in the various layers.

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Nitric oxide (NO) is formed at heights between 60 and 90 km by a photochemical process that diffuses atomic nitrogen down from the E-layer above 100 km. This nitric oxide is ionised by UV radiation from the sun having a wavelength of 1216 Angstroms — the Lyman-Alpha wavelength.

Hydrogen in the sun radiates very strongly at this wavelength which coincides almost exactly with a 'spectral window' in the atmosphere which allows this radiation to penetrate to very low levels in the atmosphere with little attenuation.

Because it penetrates down to where the nitric oxide is produced there is an abundant supply of electrons which contribute to the general ionisation of the D-layer at a height of around 75 km. Solar X-ray and Lyman-Alpha radiation contribute in roughly equal proportions to the ionisation of the D region. However, the strength of the X-rays varies by a large factor both daily and through the solar cycle as well as with solar disturbances. There is no appreciable change in the strength of the Lyman-Alpha radiation.

Up the X-rays

Increased X-ray radiation associated with solar flares can increase the ionisation of the D layer thus causing increased absorption of radio waves travelling through the D region. These solar disturbances can be the cause of a complete 'radio blackout' at times.

As cosmic rays are deviated by the earth's magnetic field ionisation of the lower D region is greater near the magnetic poles than it is near the equator.

Since the D-layer absorbs radio waves it affects the propagation of radio signals. During the day signals below about 5 MHz are almost completely absorbed. Only signals radiated at a very high angle, and above a critical frequency where all signals are absorbed, manage to pass through the layer, being subsequently reflected by the E-layer.

Communication during daylight hours on the lowest frequencies of the HF spectrum from 3 MHz to about 5 MHz or so is thus limited to short distances, not much beyond ground-wave coverage.

Low angle radiation on these frequencies during the day travels a long way through the D-region and is thus absorbed.

The D-layer of course affects higher frequencies but its attentuation affect lessens as the frequency is increased.

The E-layer

This occurs during daylight hours, the maximum density or peak of the layer lying between about 100 and 150 km. It remains weakly ionised at night.

E-layer ionisation is produced jointly by X-rays having wavelengths less than about 100 Angstroms — this ionising oxygen and nitrogen in the upper atmosphere at heights close to 100 km — as well as UV radiation with wavelengths near 100 Angstroms which ionise oxygen.

The atmosphere in the E-region is still dense enough for recombination to take place fairly rapidly. As a consequence, the E-layer can only maintain its signal reflecting ability when it is continuously in sunlight.

lonisation is generally the best around noon, disappearing rapidly some time after local sunset. (The sun sets on the ionosphere at a height of 100 km about half an hour after local sunset.)

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The F-layer

The F-layer is that region of the ionosphere above about 150 km extending up to 800 km and beyond.

During daylight hours, two distinct layers appear in the F-region of the ionosphere — the lower is known as the F_1 layer, the upper as the F_2 layer.

The F_1 layer generally occurs around a height of 200 km and does not vary greatly in height. Its ionisation density is lower in winter than in summer.

As one would expect, the F_2 layer, being the uppermost has the considerable variations in density and height

There is only one layer during the night in the F-region which is likewise dependant on atmospheric temperature. The height and density of the nighttime F-layer is also very variable owing to a number of factors.

The principal ionising agent of the F-layer is the extreme ultra-violet region (EUV). Solar UV with wavelength between about 200 and 800 Angstroms does most of the work in this respect. Radiation at these wavelengths ionises molecular nitrogen and atomic oxygen at heights between about 150 and 180 km.

The resulting electronic distribution with height does not always show a peak at this level — when there is a peak it is usually that of the F1 layer.

The shape of the F_2 layer electron distribution, and thus the height of the peak, is largely determined by the variation with height of the loss process and by diffusion of the electronics to other regions. Ions and electronics diffuse above the peak of the layer, the production and loss of electronics (by recombination, etc) below the peak determine both the position of the peak and the shape of the layer. The peak then occurs at a height where the effects of diffusion and loss of electrons reaches an equilibrium.

The F-layer will provide communications out to a range of 4000 km on a single 'hop,' multi-hop propogation being used for distances greater than this.

The F_1 layer will provide communications up to about 9 or 10 MHz during the day. The F_2 layer will support propagation beyond 30 MHz under favourable conditions, even higher in frequency and for longer durations at lower frequencies, during a sunspot maximum.

The maximum usable frequency of the F-layer varies seasonally, being greater during summer than during winter.

Summary So Far

The *daytime* ionosphere consists of an absorbing region - the D-region - with three reflecting ionised layers above that - the E, F₁ and F₂ layers.

The night-time ionosphere consists almost entirely of the F-layer.

It should be noted that the allocation of the letters of these layers above that — the E, $F_{1-52 \text{ and } F_2}$ layers.

The night-time ionosphere consists almost entirely of the F-layer.

It should be noted that the allocation of the letters of these layers was made by Sir Edward Appleton. It was he who did most of the early investigative work on the ionosphere. The F-layer, which he discovered, is also known as the "Appleton Layer." The E-layer was originally named the "Kennelly-Heaviside Layer" (or just the Heaviside Layer) after the two gentlemen who discovered its existence.

ЕП

The HY5 is a mono hybrid amplifier ideally suited for all applications. All common input functions: (mag Cartridge, tuner, etc.), are catered for internally, the desired function is achieved either by a multi-way switch or direct connection to the appropriate pins. The internal volume and tone circuits merely require connecting to external potentiometers (not included). The HY5 is compatible with all L.P. power amplifiers and power supplies. To ease construction and mounting a P.C. connector is supplied with each pre-amplifier in single pack -- Multi-function equalization -- Low noise -- Low distortion -- High overload -- two simply combined for stereo. APPLICATIONS: HI-FI--- Mixers -- Disco -- Guitar and Organ -- Public address SPECIFICATIONS:

-240 Watts!

SPECIFICATIONS:

SPECIFICATIONS: INPUTS Magnetic Pick-up.3mV Ceramic Pick-up 30mV: Tuner 100mV: Microphone 10mV: Auxiliary 3-100mV, input impedance 47k) at 1kHz. OUTPUTS Tape 100mV; Main output 500mV R.M.S. ACTIVE TONE CONTRÔLS Treble ± 12dB at 10kHz, Bass ± at 100Hz. DISTORTION 0.1% at 1kHz, Signal/Noise Ratio 68dB. OVERICAD, 38dB on Magnetic Pick-uo: SUPPLY VOLTAGE ± 16.50V Price 56.27 + 78p VAT. P&P free. HY5 mounting board B1 48p + 6p VAT P&P free

SPECIFICATIONS: OUTPUT POWER 15W R.M.S. into 8(). DISTORTION 0.1% at 15W. INPUT SENSITIVITY 500mV. FREQUENCY RESPONSE 10Hz-16kHz -- 3dB SUPPLY VOLTAGE ± 18V.

The HY30 is an exciting New kit from (L.P., it features a virtually indestructible I.C. with short circuit and thermal protection. The kit consists of I.C., heatsink, P.C. board, 4 resistors, 6 capacitors, mounting kit, together with easy to follow construction and operating instructions. This amplifier is ideally suited to the beginner in audio who wishes to use the most up-to-date technology available **FEATURES**: Complete kit – Low Distortion – Short, Open and Thermal Protection – Easy to Build. **APPLICATIONS**: Updating audio equipment – Guitar practice amplifier – Test amplifier – Audio oscillator.

The HY50 leads UL.P°s total integration approach to power amplifier design. The amplifier features an integral heatsink together with the simplicity of no external components. During the past three years the amplifier has been refined to the extent that it must be one of the most reliable and robust High Fidelity modules in the World.

Fidelity modules in the World. FATURES: Low Distortion – Integral Heatsink – Only five connections – 7 Amp output transistors – No external components APPLICATIONS: Medium Power Hi-Fi systems – Low power disco – Guitar amplifier SPECIFICATIONS: INPUT SENSITIVITY 500mV OUTPUT POWER 25W RMS in 8() LOAD IMPEDANCE 4-16() DISTORTION 0.04% at 25W at

15 Watts into $8\Omega_{\star}$

oscillator

1kHz

Price £6.27 + 78p VAT. P&P free

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HY5

Preamplifier

HY30

HY50

25 Watts into 8Ω

HY120

60 Watts into 8Ω

HY200

120 Watts into 8Ω

HY400

240 Watts into 4Ω

Price £8.18 + £1.02 VAT. P&P free. The HY120 is the baby of LLP is new high power (ange, designed to meet the most exacting requirements including load line and thermal protection, this amplifier sets a new standard in modular design FEATURES: Very low distortion -- Integral Heatsink -- Load line protection -- Thermal protection --Five connections -- No external components. APPLICATIONS: Hi-F -- High quality disco -- Public address -- Monitor amplifier -- Guitar and organ. SPECIFICATIONS: INPUT SENSITIVITY 500mV OUTPUT POWER 60W RMS into 812 LOAD IMPEDANCE 4-1612 DISTORTION 0.04% at 60W at SIGNAL/NOISE RATIO 90dB. FREQUENCY RESPONSE 10Hz-45kHz ---3dB. SUPPLY VOLTAGE ±35V Size 114 x 50 x 85mm

SIGNAL/NOISE RATIO 75dB. FREQUENCY RESPONSE 10Hz-45kHz \sim 3dB SUPPLY VOLTAGE \pm 25V. SIZE 105.50.25mm

Price £19.01 + £1.52 VAT. P&P free.

The HY200, now improved to give an output of 120 Watts, has been designed to stand the most rugged conditions, such as disco or group while still retaining true Hi-Fi performance. FEATURES: Thermal shytdown — Very low distortion — Loadiline protection — Integral Healsink —

APPLICATIONS: HEFT - Disco - Monitor - Power Slave - Industrial - Public address. SPECIFICATIONS: HEFT - Disco - Monitor - Power Slave - Industrial - Public address. SPECIFICATIONS: INPUT SENSITIVITY 500mV. OUTPUT POWER 120W RMS into 8(2) LOAD IMPEDANCE 4-16(2) DISTORTION 0.05% at 100W at

1kHz SIGNAL/NOISE RATIO 96dB. FREQUENCY RESPONSE 10Hz-45kHz - 3dB SUPPLY VOLTAGE +45V

SIZE 114 x 100 x 85mm. Price £27.99 + £2.24 VAT. P&P free.

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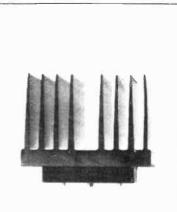


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Sweet sixteen stereo amp., waa.waa, audio level meter, expander/compressor, car theft alarm, headlight reminder, dual-tracking power supply, audio millivolt-meter, temperature meter, intruder alarm, touch switch, push-button dimmer, exposure meter, photo timer, electronic dice, high-power beacon, electronic one-armed

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Moorshead Editor, Hobby Electronics.



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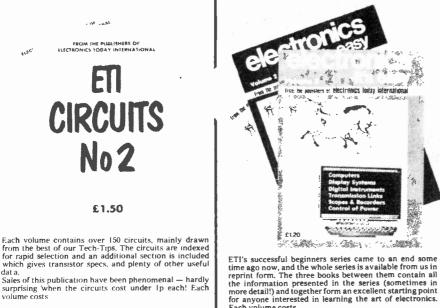
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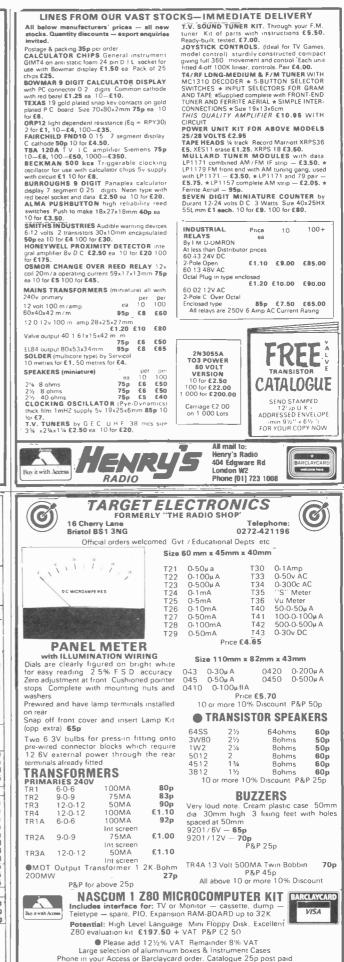
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12FE12 20FE12	12+12 12+12 12+12	0.5A each 0.8A each	2.00	60p 70p	Available 3.	4, 5, 6, 8, 9,	10, 12, 15, 18,	2-15	
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08FE15	15+15	0.25A each	1.80	50p 60p	Centre Tan	Secondary			
12FE15 20FE15 50FE15 80FE15 06FE20 08FE20 12FE20 20FE20 50FE20 50FE20 80FE20	$\begin{array}{c} 15+15\\ 15+15\\ 15+15\\ 15+15\\ 20+20\\ 20+20\\ 20+20\\ 20+20\\ 20+20\\ 20+20\\ 20+20\\ 20+20\\ 20+20\\ 20+20\end{array}$	0.44 each 0.6A each 1.6A each 2A each 0.15A each 0.2A each 0.25A each 0.25A each 1.2A each 1.5A each 1.5A each 2.5A each	2.00 2.60 3.10 3.60 4.50 1.50 1.80 2.00 2.60 3.10 3.60 4.50	50p 70p 85p 1.00 50p 60p 70p 70p 85p 1.00	FED6 FED9 FE12 FE15 FE20 60FE52 60FE28 60FE28 100FE30 100FE30 100FE30	6.0.6 9-0.9 12-0-12 15-0-15 20-0-20 26-0-26 28-0-29 30-0-30 26-0-26 30-0-30 36-0-36	1A each 1A each 1A each 1A each 1A each 1A each 1A each 1A each 2A each 2A each 2A each	2.00 2.60 2.60 3.10 3.60 3.60 3.60 3.60 5.15 5.15 5.15	60p 70p 70p 70p 1.00 1.00 1.15 1.15 1.15
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CALLAN Sheet LH0063/LH0063C DAMN FAST BUFFER

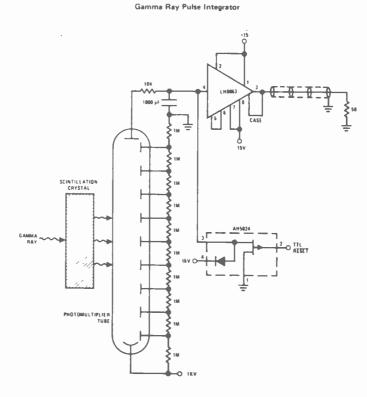
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TYPICAL APPLICATIONS

The LH0063/LH0063C is a high speed, FET input, voltage follower/ buffer designed to provide high current drive at frequencies from DC to over 100MHz. It will source or sink 250 mA into 50 ohm loads (500 mA peak) at slew rates of up to 6000V/ us. In addition, it exhibits excellent phase linearity up to 20 MHz.

It is intended to fulfil a wide range of buffer applications such as high speed line drivers, video impedance transformation and high impedance input buffers for high speed A to Ds and comparators.

It can also be used as a diddle yoke driver for high resolution CRT displays*.

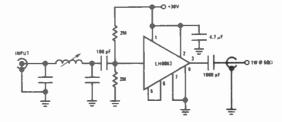


FEATURES

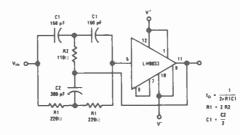
—Damn fast	6000V/us
-Wide power bandy	width
DC	to 100 MHz
-High output drive	
+ or — 10 V with	50 ohm load
-Low phase non-lin	earity
-	2 degrees
—Fast rise times	2 ns
—High current gain	120dB
-High input impeda	nce
_	10 000 M

These devices are constructed using specially selected junction FETs and active laser trimming to achieve guaranteed performance specification. The LH0063 is specified for operation from -55 to +125 C, while the LH0063C is specified from -25 to +85 C. Both are available in a 5W 8-pin TO-3 package.

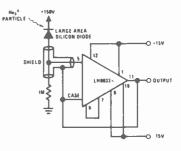
*NOTE. In VDUs where the basis of operation is for the beam to be pointed at the start of the character and then 'diddled' by means of a separate set of coils in order to form the shape of the character on the screen, the beam being switched on and off as required. **1W CW Final Amplifier**



4.5 MHz Notch Filter



Nuclear Particle Detector



LH0063/LH0063C DAMN FAST BUFFER

DC ELECTRICAL CHARACTERISTICS

LH0063/LH0063C (Note 1)

PARAMETER	CONDITIONS		LH0063 LH0063C					
		MIN	TYP	MAX	MIN	TYP	MAX	
Output Offset Voltage	$\begin{array}{l} {\sf R}_{\sf S} \leq 100 \; {\sf k} \Omega, \; {\sf T}_{\sf C} = 25^\circ {\sf C} \\ {\sf R}_{\sf S} \leq 100 \; {\sf k} \Omega \end{array}$		10	25 100		10	50 100	mV mV
Average Temperature Coefficient of Output Offset Voltage	$R_{s} \leq 100 \ k\Omega$		300			300		µV/°C
Input Bias Current	T _c = 25°C		.1	.2 10		.1	.2 5	nA nA
Voltage Gain	$eq:VIN_sigma_si$.96	.98	1	.96	.98	1	V/V
Voltage Gain	$\label{eq:VIN_sigma_l} \begin{split} V_{\rm IN} &= \pm 10 V, R_{S} \leq 100 \; k \Omega, \\ R_{L} &= 50 \Omega, T_{C} = 25^{\circ} C \end{split}$.94	.96	.98	92	.96	.98	V/V
Input Resistance		10 ¹⁰	+ 1011		1010	10''		Ω
Input Capacitance	Case Shorted to Output		8			8		pF
Output Impedance	$V_{OUT} = \pm 10V, R_s = 100 k\Omega$		1	4	1	1	4	Ω
Output Current Swing	V_{1N} = ±10V, $R_S \le 100 \ k\Omega$.2	.25		.2	.25		Amps
Output Voltage Swing	R _L = 50Ω	±10	±13		±10	±13	}	v
Output Voltage Swing	V _s = ±5V, R _L = 50Ω, T _C = 25°C	5	7		5	7		Vpp
Supply Current	₹ _C = 25°C, R _L = ∞, V _S = ±15V		60	75		60	80	mA
Supply Current	V _s = ±5V		50			50		mA
Power Consumption	₹ _C = 25°C, R _L = ∞, V _S = ±15V		1.80	2.25		1.80	2.40	w
Power Consumption	V _s = ±5V		500			500		mW

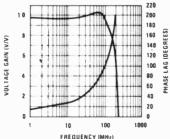
NOTE 1: Unless otherwise specified, these specifications apply for +15V applied to pins 1 and 2, -15V applied to pins 7 and 8, and pin 5 shorted to pin 6. Unless otherwise noted, specifications apply over a temperature range of -55 C to 125 C for the LH0063 and -25 C to 85 C for the LH0063C. Typical values shown are for 25 C.

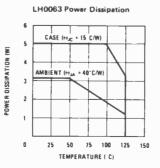
AC ELECTRICAL CHARACTERISTICS LH0063/LH0063C: (Tc=25 C, Vs= \pm 15V, Rs=50 Ω ,

 $R_L = 50\Omega$)

	CONDITIONS	LIMITS						
PARAMETER		LH0063			LH0063C			UNITS
		MIN	TYP	MAX	MIN	TYP	MAX	
Slew Rate	R _L = 1 kΩ, V _{IN} ≈ ±10 V	1	6000			6000		V/µs
Slew Rate	$R_{L} = 50\Omega, V_{1N} = \pm 10V$ $T_{C} = 25^{\circ}C$	2000	4000		2000	4000	1	V/µs
Bandwidth	V _{IN} = 1 Vrms		200			200		MHz
Phase Non-Linearity	8W = 1 to 20 MHz		2			2		degrees
Rise Time	$\Delta V_{IN} = 5V$		1.6			1.9		ns
Propagation Delay	۵۷. × ۱۰۷ V		19			2.1		ns
Harmonic Distortion			<0.1		çs ·	<0.1		*
1				1	िषणाः स्टे ब्रह्म			
		′ q ∉ ⊽ či q01 √ r LH0063 DC Safe Operating						rating

LH0063 Frequency Response

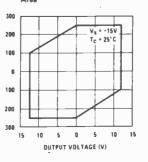


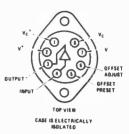


LH0063 DC Safe Operating Area

(mA)

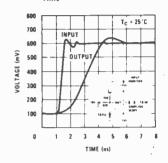
OUTPUT CURRENT



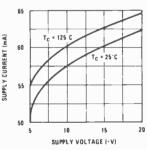


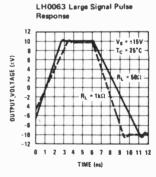
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LH0063 Small Signal Rise Time

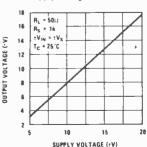








LH0063 Output Voltage vs Supply Voltage



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7432 26p	7438	30p	7442	50p
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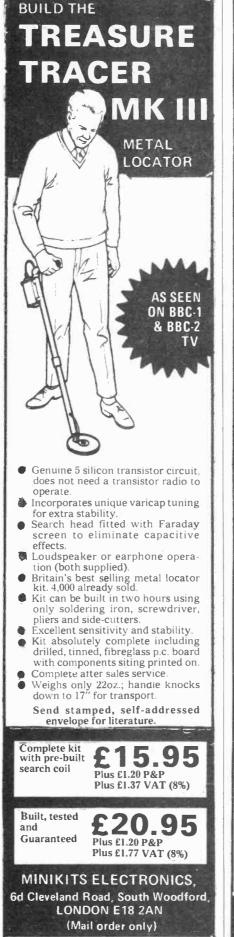
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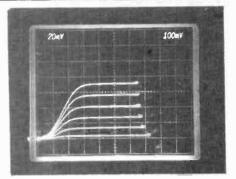
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PROJECT

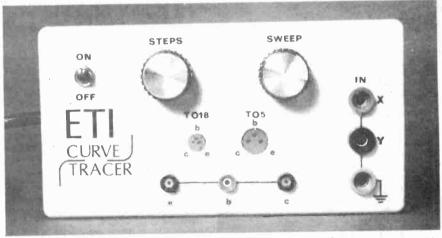
CURVE TRACER



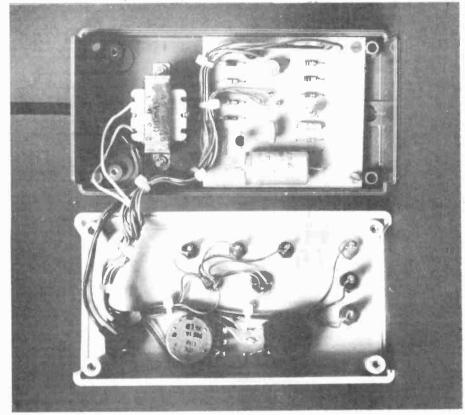
Display the dynamic characteristics of a variety of semi conductor devices with out curve tracer. Design by J. H. Adams.

THE CURVES INVOLVED in this design are not unfortunately those of the Bardots and Welchs of this world but curves that, to some, are just as interesting. The design will allow the dynamic voltage-current characteristics of diodes and transistors to be displayed on the screen of a DC 'scope capable of taking an external X input.

The performance of the unit will not be up to that of a commercial machine but considering such commercial designs are priced in the thousand pound range while our design could be built for around five pounds, we're not doing too badly.



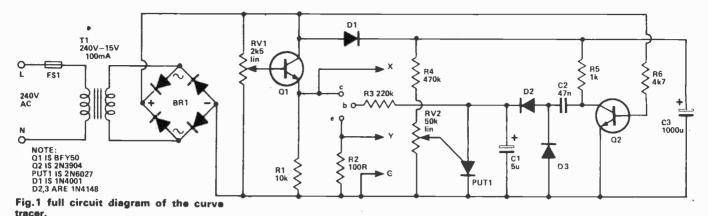
View of the internal layout of the prototype version



Construction of the curve tracer is straightforward. Mount all the components on the PCB according to the overlay. The interal layout of our prototype is shown in the photographs. The unit is mains powered and a battery supply is not suitable for this circuit.

Initially try the curve tracer with a high gain nrn transistor, a BC108 will be ideal. Connect it to one of the tracer's sockets and connect the unit to the 'scope. Set the Y gain on the 'scope at maximum and set up the maximum required level of collector voltage by adjusting RV1. RV2 will control the number of steps displayed on the screen. The X sensitivity of the 'scope should be 1V per division.

The performance of the unit is degraded by the slight drop in the DC potential on C1 during the 10mS sweep and the slight effect of the 100R sampling resistor, in that its volt drop is included in the observed collector potential. However as stated above the unit will give a good indication of the dynamic performance of a wide range of semiconductor devices (as the photograph shows) at a price that is a fraction of similar commercial equipment.



HOW IT WORKS

The principles of the full circuit can perhaps be best explained by consideration of a simpler form of the circuit. Figs. 2 and 3 show circuits for investigating the dynamic characteristics of a diode and transistor (at fixed base current) respectively.

The 'diode circuit' will, unless an inverter is available, produce a trace that will appearupside down.

Operation of this circuit is quite straight forward. RVI allows the peak value of the AC supply to be adjusted. This is then applied to the device under test via a current limiting resistor as well as to the X input of the 'scope. The current flow in the device at any time is proportional to the voltage developed across a low value sampling resistor in the current path. This voltage is fed to the Y input of the scope.

The simple transistor tester functions in much the same way. RV1 allows the base current to be adjusted within the range 10aA to 100aA.

The characteristics of an N-Channel FET (2N3819) may also be examined with this basic building block. The output characteristics are displayed for a gate voltage selected by RV1. Transfer characteristics (gate voltage vs. Drain Current) may be shown by transferring lead X to the gate terminal and mining the 1000μ F capacitor to the 15V supply (observing the change in polarity).

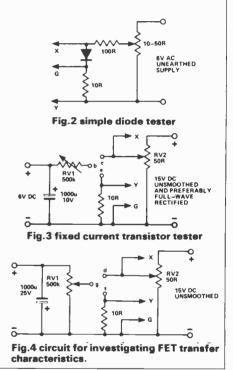
Moving now to the full circuit of Fig I that allows a far more informative display providing, as it does, simultaneous displays of the characteristic curves for several equally spaced values of base current.

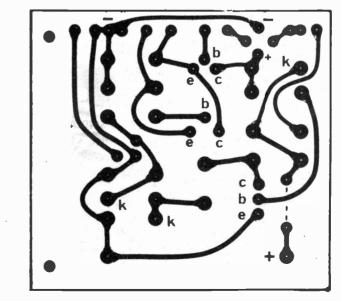
The circuit operates as follows. Every 10 ms the collector supply swings up and back over a half cycle of the full-wave rectified supply. At the end of each half cycle, there is a short period during which the supply potential is below about 0.6 V, and during this time, Q3 turns off, sending a pulse from its collector into the charge store C1 C2 D3 D2. Each pulse increases the potential in C1 by approximately 0.2 V. This would go on until the potential on Cl was 20 V were it not for Q2, the little known and much mis-described programmable unijunction transistor, PUT. This device is the semiconductor version of a neon lamp, insulating up to a certain p.d. and conductiong heavily at potentials above this breakdown value, but with the added advantage in that, through a third terminal, this breakdown potential is programmable over quite a wide range. Varying this control potential through the setting of VR2 sets the number of steps that will occur before the potential on Cl is great enough to make Q2 fire, reducing the capacitor's potential to approximately 0.6 V and so re-starting the sweep sequence.

The tracer can hardly be expected to match all the performance of a commercial curve tracer, the prices of which range into thousands of pounds. There are errors, due to the slight droop in d.c. potential on C1, and hence in base current, during the 10ms sweep, and due to the slight effect of the 100R sampling resistor, in that its volt drop is included in the observed collector potential, but as can be seen, these are quite insignificant as regards the final display. The only problem which may arise is the appearance of Radio 4 on the current axis (seen as a thickening of the trace). This is easily cured by placing a 10n disc capacitor across the actual Y-inputs of the oscilloscope.

A suitable transistor for the device under test is any reasonably high gain npn transistor, e.g. BC108. VR1 controls the maximum collector voltage, whilst VR2 sets the number of sweeps displayed. With the values given, the difference in base current between one step and the next is approximately given by:

 $\frac{1}{5R}$ μ A, where R is in megohms.



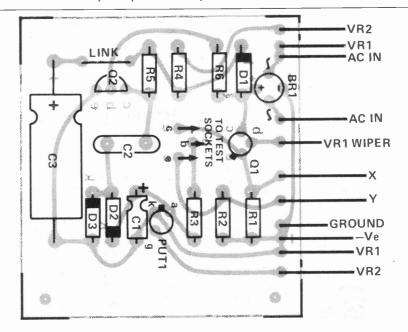


PARTS LIST-

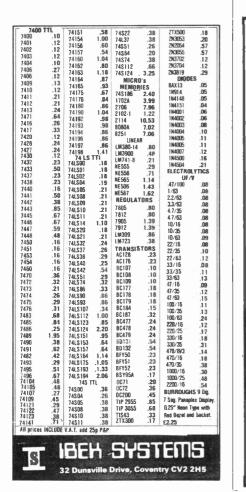
RESISTORS R1 R2 R3 R4 R5 R6	10k 100R 220k 470k 1k0 4k7
CAPACITORS C1 C2 C3	5u0 25 V electrolytic 47n polyester 1 000 25 V elec- trolytic
SEMICONDUCTORS Q1 Q2 PUT1 D1 D2,3 BR1	S BFY50 2N3904 2N6027 1N4001 1N4148 0.9A 400V
POTENTIOMETERS RV1 RV2	2k5 1in 50k 1in
MISCELLANEOUS PCB as pattern, ca knobs, cable, etc.	ase to suit, sockets,

available - the only component likely mail order outlets.

The components used in this project to cause problems is the PUT, but this should in the main, be generally should be available from the larger



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ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978

microfile.....

Gary Evans has been out and about this month, taking in a Personal Computer show and visiting a TV studio amongst other things.

THE NUMBER OF shows/seminars concerning themselves with many aspects of Microprocessors and personal computers has, like the hardware itself, shown a dramatic increase over the past few years. Unfortunately not all these events live up to their initial promise and some are not worth the cost of travelling to the venue, let alone the extortinate prices charged for admission to some of these gatherings. The PCW show towards the end of September was a refreshing change.

When it comes to exhibitions, about the only thing to do is to get as many people with products likely to be of interest to visitors to set up a stall. If you can arrange to have some new products launched, a competition and some interesting activity going on in the sidelines — all well and good. PCW did just this and it worked.

I'd have liked to have gone to all three days of the show in order to attend the various seminars held — as it was, last month's ETI was printed at the same time as the show and I was only able to get to the exhibition on the Saturday morning. I suspect the seminars were up to the general high standard of the rest of the event however.

The fact that the exhibition was crowded when I was there, it took me all my time trying to get from one stall to another amongst the multitude of people who see their role in life as standing in the middle of gangways, is not a criticism, more a testament to the show's success.

I look forward to more shows along these lines in the future.

Anita Harris – Pet?

A couple of months ago I went to the recording of a TV show pilot where one of the stars of the show, along with Anita Harris and Roger Elliott, was a Pet Computer.

I'll say more about the show but may I just digress for a couple of lines to tell one of the few after dinner stories' I know — this desire having been brought on by the mention of the word pilot above.

If you do certain jobs, being a pilot or trendy journalist are amongst them, when at parties that informationsis dragged out of you the same string of inevitable questions tions pour out — different questions for different jobs — ^M but the same questions for the same jobs — if you know what I mean. Very boring. Well, my story concerns a pilot who, being fed up with the situation, in response to the next such interrogation replied ''I travel in aluminium tubing'' — that a least provened no questions. That's the story then — not very exciting but it's the way I tell 'em

Back to the PET and the TV show however and to why the PET was there. One of the computer's co-stars may have given some of you a clue. Roger Elliott is the TV Times astrologer and — slight groan — the PET was put to the task of flashing Anita's details (astrological) over it's screen. They say that an actor should never go on stage with animals or small children, for fear of being upstaged. To this list, although for a different reason, should be added small computers. The reason is they very rarely behave for any length of time as Roger Elliott found out when the PET started promising that it was "Time for a song" when Anita obviously was ready for no such thing.

The program was made by HTV who's main claim to fame, or is it eternal damnation, in my book to date is that they produce Mr and Mrs. While not in that league — the pilot was much better — I did not enjoy the show that much but the production team seemed to think it was OK so maybe you'll see it on your screens at some time in the future.

I can't resist just one more tilt at Mr and Mrs — it appears that four of these dreadful things are reeled off in the same day — not all in front of the same audience, who could stand the strain?, especially when you consider that the people who have parted with their hard earned time to watch this entertainment are in the main, old age pensioners, who should really be taking things easier at their age.

I mustn't be too unkind to Mr and Mrs though, after all there is Nicholas Parsons.

Pet Problems

When Julian Allason of PETSOFT phoned this month to ask if I had any problems I was just about to mention the fact that my car had just fallen to bits, and that my dog had a limp amongst other things when he explained that he was merely reading from the screen of PET which was running a new program called Eliza. Eliza simulates a consulation with a psychiatrist and my encounter with the machine went something like this.

- PET What is your problem?
- ME Emotional insecurity
- PET Do you have any psychiatric problems?
- ME Yes
- PET Are you sure?
- ME Yes
- PET: Do not repeat yourself.
- ME_Oh God!
- PET What does that suggest to you?
- ME I'm not sure
- PET. Did you come to be because you're not sure?
- ME Yes
- PET. I see
- ME Where do we go from here?
- PET. Why do you ask?
- ME Because I'm not sure
- PET How long have you been not sure?
- ME Five years
- PET. I see

Well, follow that — Petsoft have probably the widest range of PET software in this country with 70 titles in their current catalogue and aims for 100'in the next. A recipricol arrangement with Personal Software Inc, whereby Petsoft material will be distributed in the United States and Canada and the best of Personal Software's material sold over here means even more to choose from.—If you have a PET, Petsoft are worth knowing.

PETSOFT, P.O. BOX 9, NEWBURY, BERKSHIRE, RG13 1PB.

Put A Chrysler Sidelight In Your Life

I've been exposing myself this month, but before you get the wrong idea — although I suspect most of you already have, I mean to say that I've been out and about talking to computer clubs.

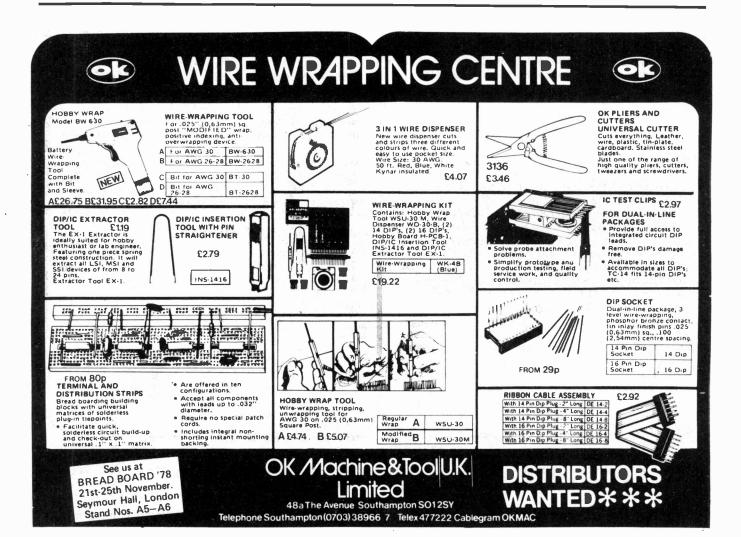
The meetings ranged in size from the 400 or so at the first meeting of the North London Computer Club,

through a 100 or so at Sussex University to the twenty or so at the Thames Valley group of the ACC's meeting. I enjoyed myself at each event, and picked up some very good ideas from the very high calibre of people that numbered among the audience at each event. Among the handy things I learn't at Sussex was that the exact sequence of operations required to turn the sidelights of a Chrysler Sunbeam on this could not be discovered by your humble reporter, a number of undergraduates and a lecturer in mathematics, but had to be resolved by a call to the car hire firm.

All the clubs would welcome new members — The North London Computing Club is held at the North London Polytechnic, Holloway, LONDON N7 8DB. Tel. Stephanie Bromley — 01-607 8663 (Office), 01-359 2282 (Home), or Mike O'Reilly, — 01-607 2789 ext 2100.

The Thames Valley ACC group meets on the first Thursday of every month at the Griffin (A pub-good move ACC) 10 Church Road, Caversham, Reading, Berkshire.

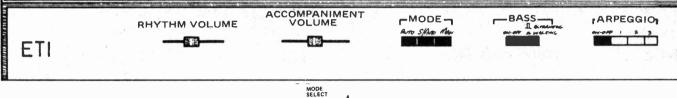
For the Sussex University Group — who will welcome outsiders to their meeting with open arms and hands, for the money you know — Contact. Pete Guile, University of Sussex, Falmer, BRIGHTON, Sussex.





ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978

AUTOCHORD PART TWO



THIS MONTH WE complete the description of the auto chord instrument. Last month's article covered the circuit descriptions of the various blocks that make up the unit and of the operation of the complete design.

This month we complete the project by describing the construction of the instrument.

Construction

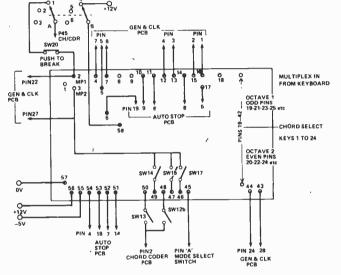
The components should be mounted on the PCBs according to the overlays shown. Pay particular attention to the diodes, capacitors and other polarity sensitive devices.

The project involves a great deal of interwiring between the various boards and switches of the design.

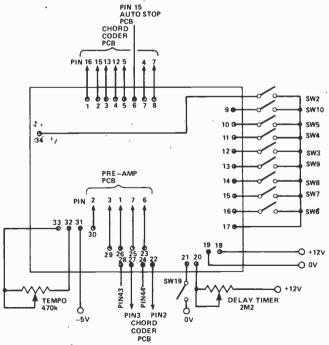
The interconnections are shown in the accompanying diagrams and great care should be taken to ensure that no errors are made at this stage — they will prove difficult to trace at this stage.

We give no details of the housing of the project as this will depend entirely upon the instrument in which the auto chord is to be installed.

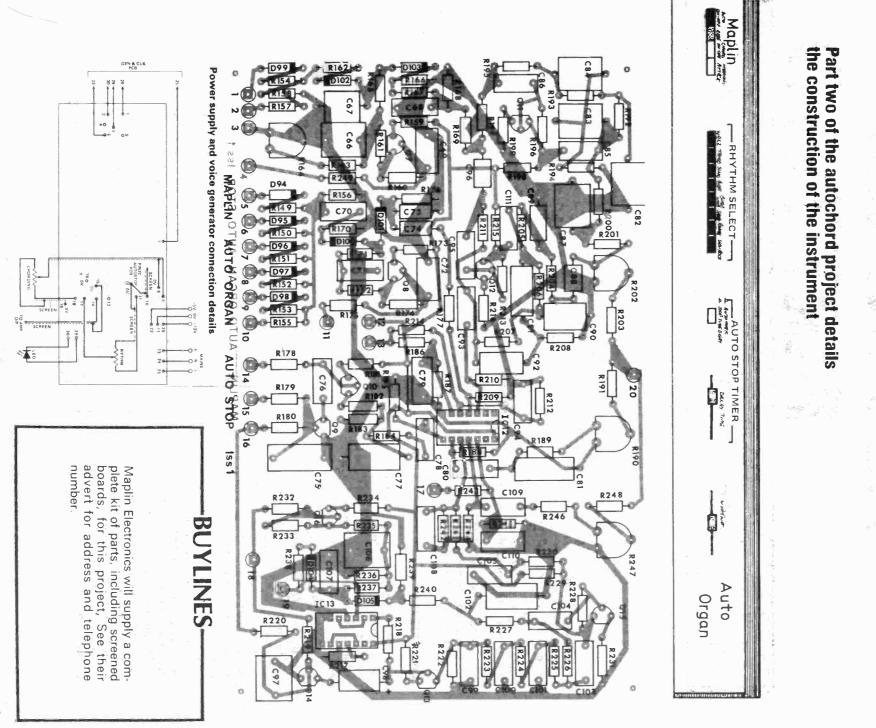
The finished unit can be added to most organs, being easiest to fit to a unit that uses DC keying. In use the project should add an extra dimension to even the most limited of musicians efforts.



Above and below interconnection details for the generator and coder boards

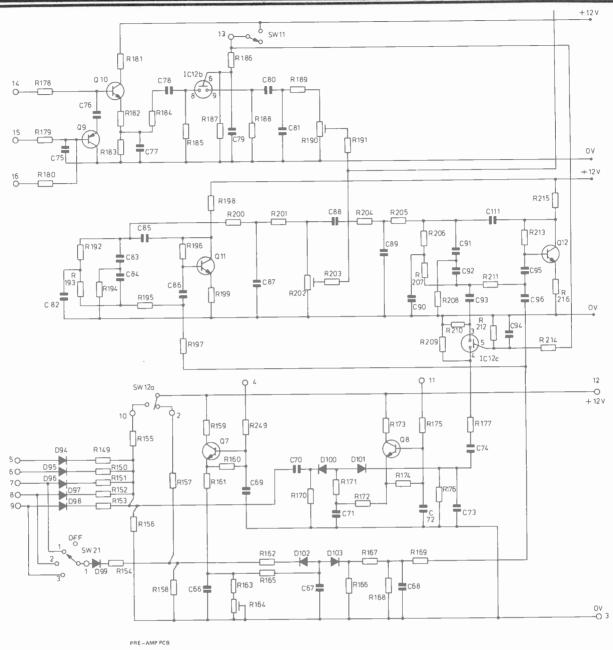


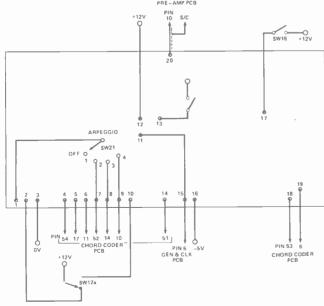




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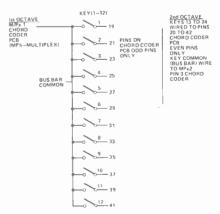
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KEYING ARRANGEMENTS

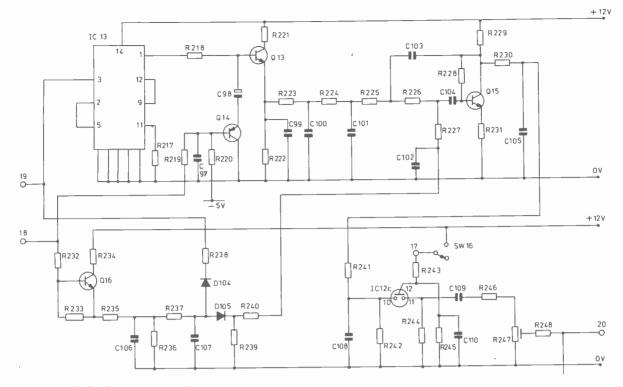
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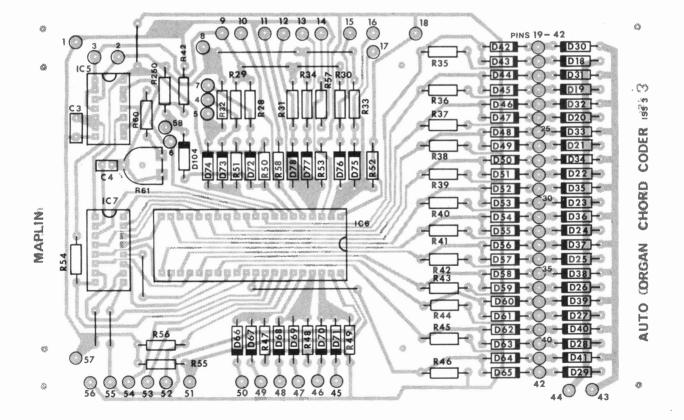
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<u>PROJECT</u>

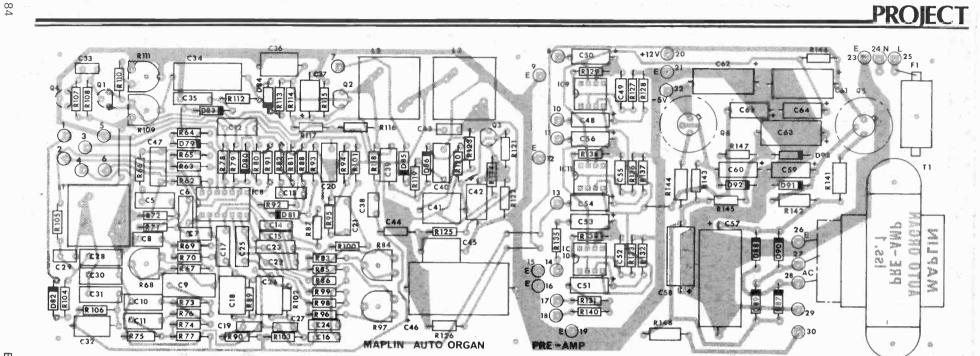


Above, and to the left, circuit diagram of the auto stop module

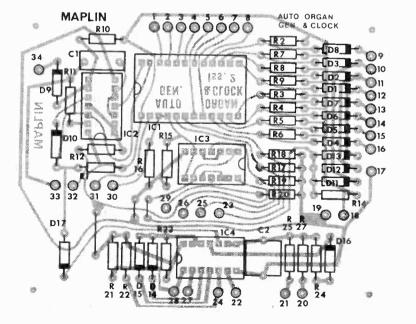


The overlay for the chord coder is shown below take care that all the diodes are inserted in the right position.

83



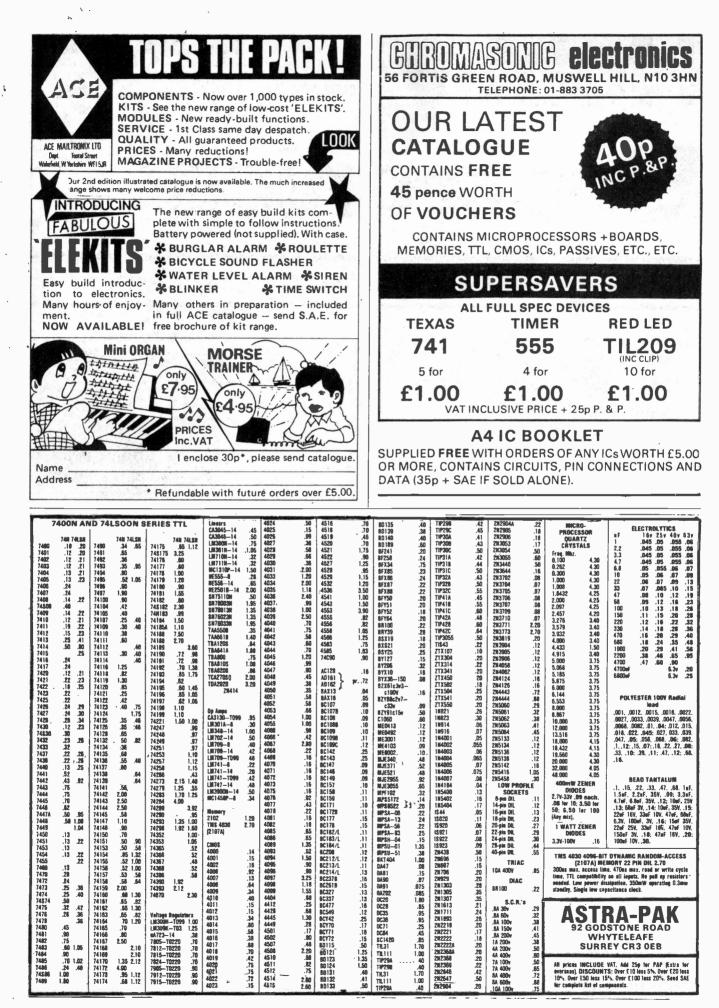
Above the power supply and pre-amp board of the auto organ. The interconnections between this and the rest of the boards are shown in the accompaning drawings.



Left is the overlay for the generator and clock section of the auto organ.

ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978





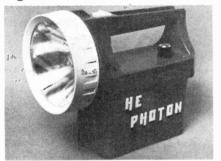
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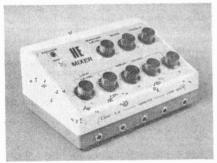
The December issue will be on sale on November 10th

Light Beam Phone



True wire-less communication for which you don't need a licence! Our project next month which we are calling the 'HE Photon Phone' uses two standard torches which we've converted — all the electronics fit into it beautifully. In our tests we've been able to make our units work over a distance of 50 feet; even if you don't want to build it, you'll be fascinated by the techniques there's even a remote control facility included.

Audio Mixer Project



A really neat project designed by a professional audio engineer — that's a quick summary of our mixer, choose your own number of inputs (we've opted for three high level and two low level ones). There's a bass and treble control and of course a master level control. Building it should be simplicity itself as everything, including the level controls is on a single printed circuit board. Power is supplied by two PP3 batteries; inputs and outputs are via standard jack sockets.

Bias

No — not political, tape. Why do you need a high frequency signal added to a tape recording — you never hear it so why is it necessary? Next month we tell you.

DIY PCB's



The neatest way to build a project is on a PCB — few would deny that, yet PCB's are frightening to those who haven't tackled them before. Next month we will be launching Hobbiprints — a really easy way to make the PCB's which we show in HE and we'll show you how to use them.

Calculators



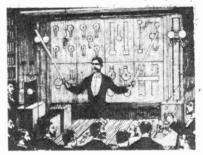
The world of calculators has gone the way of HiFi — the facilities offered often cause confusion. We take a look at the current terminology of the calculator market enabling you to find out if the facilities offered are really the ones you want.

Electronic Dice



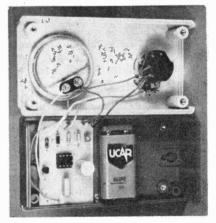
Press the button and one of six LED's comes on at random. From the photograph you can see this is really a straightforward project. The light stays on automatically — there isn't even an on-off switch!

The Tesla Controversy



Nikola Tesla was without doubt a genius — he even has a unit of measurement named afterhim — but even 35 years after his death there are those who believe that much of his work has been suppressed.

Metronome



Using just a single 555 IC, this project can be built on either a PCB or Veroboard — we give you details for both. The beat rate can be varied from 30 to 120 beats a minute.

SPECIAL OFFER

Next month you'll be able to get a top quality soldering iron, either 240V or 12V, through our offer in HE. Today's regular price is £4.00 but next month you can get this for:

audiophile

Ron Harris takes to the high seas this month — well the Thames anyway — to discover a remarkable new drive unit from Strathearn. Back on dry land news of a linear motor tone arm

IT WAS ENOUGH to make Nelson spin in his grave. One of Her Majesty's ships, battle-worn from the fire of enemy guns, put to use as an area to hold a press reception! And for something as totally unmaritime as loudspeakers!

Mind you, HMS Belfast can only be considered appropriate, for it was Strathearn Audio (based in Belfast and government owned) who sent me the music echoing through the wardrooms.

The occasion was the launching — for once no pun intended — of their new speaker system, the 21000. This is a 'four box' affair with the base units cast loose from the rest. Frequencies up to 500Hz are handled by the 8 bass drivers reflex mounted in the enclosures. Above 500Hz everything is produced by the real star of the system, Strathearn's new driver, the SLC2.

Film Star?

The principle on which these speakers operate is very similar to that of the Wharfedale Isodynamic headphones. In the SLC2 an aluminium conductor, about a metre long, is bonded onto a polyester film which is stretched inside a moulded frame about 130mm x 600mm. Rows of magnets flank the diaphragm creating a high uniform field in the vicinity. When the signal current passes through the conductor it is driven by the force generated due to its being in a magnetic field.

Thus the polyester film is the speakers 'cone' if you like. Since this will radiate from both front and back (dipole radiation) the unit has damping pads fitted to absorb the anti-phase rear radiation. Mass of the driver is very low, so very little overhang to worry about. As the area is effectively all driven, it should not 'break up' at all on any input signal.

The only drawback is the very low impedance of the aluminium strip itself, about OR5 in fact. In order to make this usable Strathearn have transformer coupled — which at least makes the unit adaptable to any required input impedance.

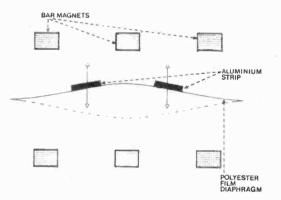
To claim, however, that this produces a purely resistive load is at best extremely optimistic, at worst

Sound Track

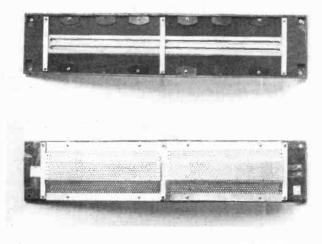
I'm going to reserve judgement on the 21000 system as a whole until I've had an opportunity to listen under more favourable conditions than HMS Belfast at 100 F with 49 other people crowding me lugholes! It was clear though that the SLC2 is a remarkable unit, and is perhaps worthy of better. We shall see.

The system sells for £375 RRP, and is expected to have appeared in the shops by the time you can get down there.





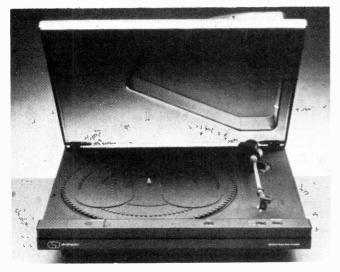
The 21000 from all angles. At the top we have the full system. Below that the diagram shows the operating principle of the SLC1. The polyester diaphram acts as the speaker cone. Below this caption two internal views of the unit. The radiating areas can be seen in the top diagram, and the lower rear view illustrates the damping material to control rear radiation.



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Decked Out

At the same demo Strathearn were using their SM2000 turntable as the sound source. It was a good advert. They had a line of Sonus, Supex, ADC, Shure and Ortofon cartridges all neatly installed in spare carry arms, and all of which tracked very well when asked to. Several people — me included — were surprised at the ease with which the SM2000 handled these devices and



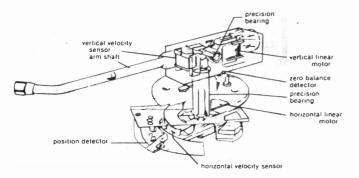
how well the sound each is capable of was preserved. Indeed on this evidence the SM2000 is a very capable unit indeed — a comparison with some better established machines (including schhh — you know what) might be very interesting indeed. How about it, Strathern?

Details of both from Strathearn Audio Ltd, Kennedy Way Industrial Estate, Kennedy Way, Belfast.

Arms Against The British?

There can be only two basic ways of doing a job simple and complicated. Both can take vast amounts of thoughts to realise (who said simple meant obvious?) and are capable of excellent results. Witness belt and direct drive turntables as represented by the Linn and the Technics SP10.

Sony have applied the latter approach to pickup arm design with the result that they end up with two linear motors, two velocity sensors, two position sensors, a deal of electronics and potentiometers to set tracking weight!

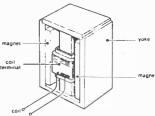


Exploded view of the Sony motorised pickup arm. Tracking weight is applied by a potentiometer mounted remotely on the plinth.

ELECTRONICS TODAY INTERNATIONAL — DECEMBER 1978

In fact the velocity sensors are simply two more linear motors used as generators. Servos drive the motors which take the arm across the record in he proper manner. In the vertical direction too all control of the arm movement is down to a linear motor. Arm resonance is suppressed, by varying the current to the coils — from somewhere around 25dB in an undamped system to about 3dB in the Sony system using their XL55 cartridge.

Right: A close up of the linear motors used in the arm design. These double as position sensors by using the same device as a generator, i.e. allowing them to be moved by the arm and measuring the current generated in the coils.



Advantage Complications

Gains from this method are claimed to be insensitivity to external vibration, improved tracking and better definition and imaginery. Bias of course can be forgotten, as the motor controls movement across the vinyl canyons, and tracking weight can be changed while the stylus is in action.

All this sounds well-nigh perfect does it not? On paper the design looks marvellous (so did the Titanic — cynic) but we shall have to wait until they market it in this country to find out *how* good it is. Meanwhile eat your heart out SME!

From Service to Taste

A little congratulation and a whoopee cushion to finish on. Firstly many thanks to Celestion for some fast excellent service this month. Some nameless person from the pit (no not me — *another* one!) blew a bass unit in one of our Ditton 66's. One phone-call later I was on me way to pick up a replacement from Ipswich. And that four years after buying the speakers — and it was our fault. Nice to be able to commend a big hi-fi firm for service for a change.

Now Audiophile enquiry service is normally dealing with people with impeccable taste. However it appears there is one exception. So that this person does not have derision heaped upon his unworthy shoulders and be cast from the company of his peers let us refer to him as Mr Smith.

This person wrote in — nothing wrong there you may say — he even dated his letter. Again nothing amiss about that. Trouble was he 'dayed' and timed it too. I quote with shaking head and furrowed brow . . .

"So at 8.05 pm on Thursday evening I am turning off some corny comedy on the television set to write enquiring about ..."

There we have it. The heronious crime is in the open. Thursday eh? 8.05 eh? Corny comedy eh? The only comedy on TV at that time is the 'Good Life' — which any human male with a micro-gram of taste and appreciation of the opposite gender should be watching avidly for the glorious presence of Felicity Kendal!

Oh Mr Smith may your hi-fi forgive you - I cannot!

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IT'S FREEL

T'S FREEI Jur monthly Advance Advertising Bargains List gives details of bargains vriving or just arrived -- often bargains which sell out before our idvertisement can appear. -- It's an interesting list and it's free -- just end S.A.E. Below are a few of the bargains still available from previous

lists. Pot Cores. We have now received our delivery of Ferrox pot cores. Thes are ex unused equipment. They contain the bobbins but of course thes have to be wound and you would have to unwind. Three pairs available diameter Thickness Price

FX 2243 4.5 cm FX 2242 3.5 cm FX 2240 2.5 cm	3.0 cm 2.3 cm 1.6 cm	81 70 60	per Pair	
Quantity discounts apply.				

Component Panel Ref. 3055. Taken from unused P.S.U.s. these contain 4×2N 3055 power transistors with mica insulators all on heat sink and 4 variable pots, preset type with spindle locks. Real bargain at .08 each

C1.08 each and bord picture type time pyterine to be to be added to a set of the set

6 Digit Counter - Resettable, coil voltage 48 DC or 115V AC, current

6 Digit Counter — Resettable, coil voltage 48 DC or 115V AC, current 100 mA acors, ance 62 10 10 Digit Swifch Pad. Made, we believe, for GPO pushbutton telephones, each button operates 2 pole switch which returns when depressed, panel size 2%, x3%, x1%, pushbuttons with clear plastic protected digits 0-9, price 21.6. Mains Blower, Real bargain blower made by Smiths, the motor is let into the turbulator so these can be stacked sideways to give variable air outlet using the minimum of space. Overall size of the blower is 7 dia x2% and the air outlet 1% x2%. Price only £2.50 Dial Indicator used in tool making and precision measuring, the famous John Bull shows differences of 01 mm. A beautifully made precision instrument, price in most tool shops would be £12-£15. We have a fair quantity, price £10.75.

MOLLARIE OF 18 Strend system. Rated one of the finest performers in the states list likey would make a wonderful gift to allos diary one in asyst assessmble modelful form and compiled with a pair of Piessey speakers bits should stall at sheat 330 - with diven to a special bulk buy and as an incestive for y buy like mosth we offer the system compiles at only EIS including AT and pestage. High Voltage Mains transformer. Normal mains primary secondary by our meas equipment is 8Kv approx, at 5mA. We are offering these at a bargain price of £4.50 measuring

A Special Bulk Purchase enables us to offer this keyboard at a lowest ever price. 49 Coded keys encoded Into a direct TTL compatible 7 bit output. Features such as delayed strobe. 5 volt D.C. single rail operation and rollover protection make this an absolute must for the MPU constructor! Supplied complete with connection diagram and edge connector. at a secondhand ''no time to test'' price of only £18.63, post £1.50.

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Readers' Circuits



'Cold-start' For CD Units

T. Lyons

L

Many cars are fitted with cold-start coils, which operate at full current only on starting, then are fed via a ballast resistor. This resistor is normally discarded when CD ignition is fitted, and the coil is run at 'full power' all the time. It's a simple matter to arrange for the cold-start circuit to operate a relay inside the CD unit which switches in a second capacitor C2 across the main one, thus increasing the energy of the spark when the engine is starting. After starting, C2 is no longer in circuit and the main capacitor C1 alone supplied current to the coil, thus alleviating any charging problems with attendant loss of power at high revs.

RLA is any 12 volt relay, and C2 can have the same value as the existing capacitor C1, usually 470n or 1u0.

Now that the novelty of TV games has worn thin and most of the units are gathering dust in the corner reserved for other five-minute wonders, here's a chance to add new spice to leisure time. The circuit is an oscillator clocking at about one cycle per 4 seconds. This switches the ball angle ''randomly'' making the game unpredictable and difficult. Also this prevents

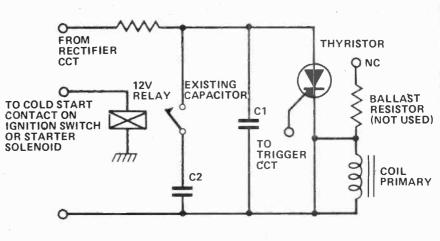
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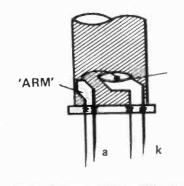
IC = CD4001A

2M2

2u2

S. Rice





TV Game Resurrection

LED Spotting

A. Kenny

Since the leadout on LED's varies according to the manufacturers preference, leadout diagrams are not always worthy of the trust placed in them. In some cases a reverse connection will destroy the device being used.

A simple way to avoid this is to use the following technique:

If the LED is held up to the light, the structure can be clearly seen. There is a "cup" and an "arm" carrying a fine wire to the LED itself, which is in the "basin" of the cup (see drawing).

The lead with the cup is the cathode, and the other is the anode (of course).

FIXED

ΠΠ

CHANGE BALL ANGLE

the ball from getting stuck and bouncing back and forth from the bats and boundaries. Do not use B suffix CMOS except for Schmidt trigger and gates.

Tech-Tips is an ideas forum and is not aimed at the beginned. We regret we cannot answer queries on these items. ETI is prepared to consider circuits or ideas submitted by readers for this page. All items used will be paid for. Drawings should be as clear as possible and the text should preferably be typed. Circuits must not be subject to copyright, Items for consideration should be sent to ETJ TECH-TIPS, Electronics Today International, 25-27 Oxford St,, London W1R 1RF.

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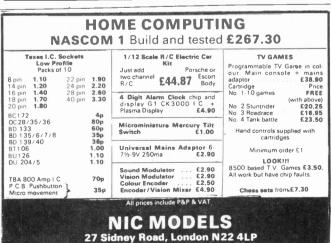
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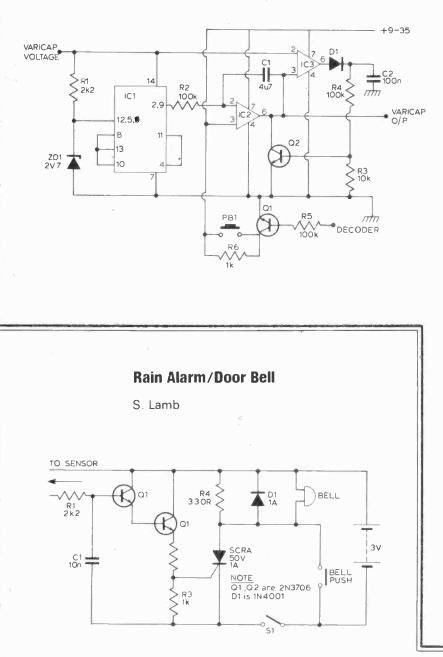


ELECTRONICS TODAY INTERNATIONAL - DECEMBER 1978

Readers' Circuits

Automatic Stereo Tuner





The circuit shown will automatically tune an FM tuner to stereo broadcasts only. On switch on the indicater pin of the stereo decoder is at OV. In consequence Q1 is biased off and pins 6 and 3 of IC1 are at the positive varicab supply voltage. As this IC, a 4007, is wired as a transmission gate this voltage holds the gate on. The impedance across the a gate is in the region of 300 ohms. IC2, a 741, is used as an integrater, the input voltage from across ZD1 is connected through the gate. The output of this IC therefore is a positive going ramp which is fed to the varicap tuning diodes.

On reception of a stereo broadcast the voltage at the decoder indicater pin goes positive driving Q1 into saturation and closing the transmission gate.

Since the closed position of the gate places an impedance of the order of 10° ohms in series with the inggrater the output is "frozen" keeping the station in tune. This state of affairs continues until PB1 is pressed, whereupon the integrater will once again start to ramp positively in search of another station

A second 741, IC3, is used as a comparator. The varicap voltage is sampled by the inverting input whilst the tuning voltage feeds the non-inverting input. As soon as the tuning voltage reaches the same leve as the varicap voltage the comparator's output swings positive forward biasing Q2 and discharging C1. The circuit will now go through the entire sequence again.

The varicap voltage must not exceed 15V unless the transmission gate is operated from a stabilised supply of less than 15V output. The supply line to the op amps should be several volts greater than this.

With S1 open the circuit function as a bell. R4 provides the holding for the made from 3 square inches of copper on the sensor will turn on Q1, Q2 and

doorbell. With S1 closed, rain falling thyristor while D1 prevents any damage to the thyristor from back the thyristor will trigger activating the EMF in the bell coil. The sensor is

clad board with a razor cut down the centre. C1 prevents any mains pickup in the sensor leads.

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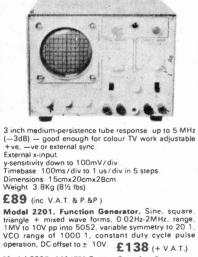


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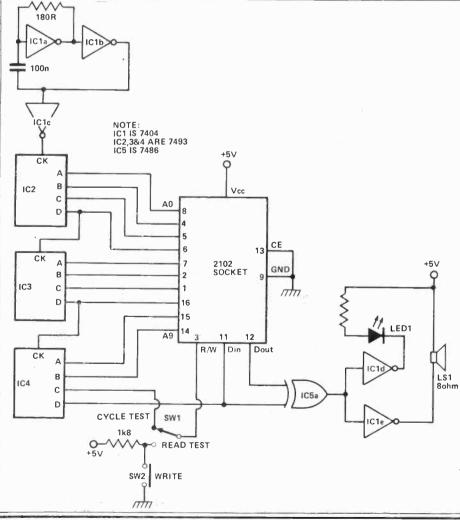
Readers' Circuits

Unijunction Pulse Stretcher Door Bell Extender

D. Wedlake

The circuit presented is a practical monostable timer which was designed to extend the ringing time of a door bell. It can be useful in cases when the bell push button might not be engaged long enough to attract attention, though it could be used in many other applications.

When the push button is closed the thyristor will switch on delivering power to the unijunction transistor timing circuit and energising the relay, the contacts of which are used to control the bell circuit. At the same time, capacitor C2 quickly charges to the load voltage potential via R3. After a time interval given approximately by 0.8 C1 R1 (about 6 seconds in this case) the unijunction switching it off. With these values the transistor will fire and the correspon- relay will become energised for at ding output pulse which is coupled to least 6 seconds.



O 12 V PUSH BUTTON 1 k CIO3YY 560 R 220 R RI 680 k C2 ĺυ R2 RLA 2N2646 TO BELL IN400I 81 CIRCUIT IN400I **R.S.COMPONENTS** CL R2 348-908 47 R R3 Ik 10 u nnv the cathode of the thyristor via C2 will

put the thyristor in reverse bias

2102 Memory Tester

S. Sunderland

This circuit provides for the testing of 1024 Bit X1 memories, such as the 2102 series, in two modes. Mode-1 cycles the memory continuously through write and read, alternately writing zeros and ones then reading to ensure the write was successful. Mode-2 allows the write of a signal onto the memory, then continuously reads it to ensure the data is stable.

In both modes, the output from the memory is compared with what should be there, and if there is a difference, an LED flashes, accompanied by a click from the speaker. In mode-2, on power on, a continuous noise will be heard from the speaker, on pressing the 'WRITE' button this should vanish, similarly, a brief pulse of noise will be heard in mode-1 before the write is completed. The oscillator frequency is about 20 kHz with components shown.

In mode-2, when the supply voltage drops below 4.5V memory is not stable for more than a fraction of a second, although this does not show up using mode-1.

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							# marro										
TRANSIST	085	8C328	15p	80208	160p	2N4061	12p	7490	32 p	74194	92p	4501	19p	C:ODES		ZENER DIDDES 400mW	
AC126	18p	BC338	15p	0C25	76p	2N4062	20p	7491	65p	74195	85p	4507	59p	BY127	18p	2.7V to 33V	10p
AC127	170	80547	11p	0C28	1080	2N4123	23p	7492	45p	74196	92p	4510	110p	DA47	10p	2.11 10 001	
AC128	16p	BC548	10p	0C35	108p			7493	34p	74197	92p	4516	110p	0A81	15p		
AC141	24p	80549	11p	0C71	19p			7494	80p	74198	150p	4518	75p	0A200	6p	VERO BOAROS 0,1" copper	
AC142	24p	BC557	14p	0C72	34p			7495	55p	74199	150p	4519	60p	0A202	9p	2.5" x 5"	57p
AC151	42p	8CY30	67p	0C84	46p	TTL		7496	62p			4520	110p	1N914	4p	3.75" x 5"	67p
AC152	53p	BCY34	74p	TIP29	400	7400	12p	7497	240p	CMOS		4528	107p	1N916	5p		
AC152	58p	8CY59	24p	TIP30	40p	7401	120	74100	95p	4000	15p	4578	27p	1N4001	4p	CERAMIC CAP 50V	
AC176	180	BCY70	140	TIP31	50p	7402	12p	74104	50p	4001	15p	4583	83p	1N4002	4p	22pF 10 47000pF	2p
AC187	23p	BCY71	14p	TIP32	55p	7403	12p	74105	40p	4002	16p	4585	105p	1N4003	6p	cchi le di opohi	-
AC188	23p	80115	52p	TIP33	75p	7404	130	74107	28p	4006	110p		•	1 N4004	7p		
AD1 49	65p	80121	79p	TIP34	980	7405	130	74109	45p	4007	16p	VOLTAGE		114005	10p	POLYESTER CAP 250V	_
AD161	380	80123	79p	TIP35A	253p	7406	290	74110	46p	4008	94p	REGULATO	RS	1N4006	10p	.01, .015, .022, .033, .047, .068, .1 uF	
A0162	38p	80124	970	TIP36A	389p	7497	29p	74116	160p	4009	46p	7805	82p	1N4007	11p	.152233	7p
AF1 14	30p	80131	35p	TIP41A	59p	7408	14p	74118	82p	4010	50p	7812	82p	1N5400	16p	.4768 uF	13p
AF118	30p	80132	35p	TIP42A	59p	7409	14p	74120	125p	4011	15p	7815	82p	1N5401	16p	luF	17p
AF125	27p	B0135	38p	T1P2955	126p	7410	120	74121	26p	4012	16p	7818	82p	1N5402	18p	2.2 uF	28p
AF126	270	B0136	36p	TIP3055	64p	7411	19p	74122	55p	4013	35p	7824	82p	1N5403	20p	6.8 uF	48p
AF127	270	B0137	380	ZTX108	14p	7412	21p	74123	40p	4014	108p	7905	98p		· ·		
AF139	36p	80138	38p	ZTX109	14p	7413	25p	74125	45p	4015	80p	7912	98p			ELECTROLYTIC CAP 25V	
AF186	54p	80139	35p	ZTX300	16p	7414	54p	74126	46p	4016	45p	7915	98p			LuF to 47 uF	7p
AF239	40p	80140	35p	ZTX500	16p	7416	27p	74132	70p	4017	65p	7918	98p			68uF, 100uF	8p
ASY53	810	8F115	25p	2N706	13p	7417	27p	74136	79p	4018	90p	7924	98p	BRIDGE		1 50uF	9p
ASY54	810	BF167	29p	211131	23p	7420	12p	74141	56p	4019	65 p			RECTIFIERS	,	220uF	10p
ASY55	69p	BF173	27p	211132	23p	7421	28p	74142	202p	4020	95p	THYRISTO		1A/50V	22p	330uF	12p
BC107	8p	8F178	34p	2N1302	38p	7422	18p	74145	65p	4021	98p	1A/50V	28p	1A/100V	24p	470uF	15p
BC108	80	BF179	37p	2N1304	54p	7427	25p	74147	135p	4022	85p	1A/100V	30p	1A/200V	27p		
BC109	80	BF180	37p	2N1305	25p	7428	34p	74148	120p	4023	15p	1A/200V	38p	1A/400V	30p	RESISTORS 0.25W	
8C113	170	8F181	37p	2N1306	39p	7430	12p	74150	70p			1A/400V	40p	2A/50V	34p		1p
BC117	20p	8F182	37p	2N1308	40p	7432	24p	74151	50p	CMOS		3A/100V	36p	2A/100V	36p	4.7 ohms to 1 Mohm	14
8C119	29p	BF183	37p	2N1613	22p	7433	32p	74153	60p	4024	68p	3A/200V	38p	2A/200V	38p		
BC140	340	BF184	28p	2N1711	21p	7437	24p	74154	106p	4025	15p	3A/400V	51p	2A/400V	40p	POTENTIOMETERS (carbon)	
8C142	27p	8F185	30p	2N1893	44p	7438	24p	74155	63p	4027	35p			2017 4001	Top	1 Kehm to 2 Mohms log/linear	26p
BC143	27p	BF194	13p	2N2217	27p	7440	13p	741 56	63p	4028	70p	LINEARS				5 Kohm to 1 Mohm log switched	600
80147	7p	BF196	13p	2N2219	21p	7441	52p	74157	63p	4029	90p	710CN	41p			o tonin to a monini tog antionau	
BC149	8p	8F197	16p	2N2369	16p	7442	45p	74160	80p	4030	50p	741 OIL8	22p				
BC157	9p	BF198	16p	2N2483	26p	7443	90p	74161	80p	4035	130p	747C 01L14	70p	OPTO/DISF	PLAYS	PRESETS 0.1W horizontal	_
BC158	9p	8F200	36p	2N2484	22p	7444	90p	74162	80p	4041	87p	748C 01L8	35p	2N5777	50p	, 100 ohm to 1 Mohm	6p
80159	9p	BF224	16p	2N2905	22p	7445	70p	74163	80p	4042	75p	CA3011	BOp	0CP71	70p		
BC168	Bp	BF257	37p	2N2906	22p	7446	70p	74164 74165	70p	4043	85p	CA3018	80p	ORP12	700	TRANSFORMERS 240V primary	
BC170	9p	BF258	40p	21/2907	22p	7447	55p		90p	4044	96p	CA302BA	85p	01704	90p	6-0-6V 100mA	95p
BC171	9p	8F259	44p	2 N29269	10p	7448	58p	74166	100p 270p	4047	95p	CA3035	140p	01707	90p	0-6VX2 1AX2	360p
BC172	9p	BFR39	30p	2N2926R	8p	7450	14p	14167 74173	270p 120	4048	63p 40p	CA3036	120p	LEO 3/5mm		9-0-9V 100mA	250p
BC173	9p	BFR40	30p	2N3053	18p	7451	14p	74173	90p	4049	40p 45p	CA3046	75p	Red	10p	9-0-9V 1A	290p
BC182	10p	BFR79	30p	2N3054	50 p	7452	13p	74174	90p 70p	4050	45p 40p	CA3054	110p	Yellow	17p	9-0-9V 2A	400p
80183	10p	BFR80	30p	2N3055	50p	7453	19p	74175	70p 90p	4068	40p 20p	CA3080	70p	Green	17p	0-12V 2A	370p
BC184	10p	BFX29	25p	2N3702	8p	7454 7460	14p	74170	90p 90p	4066	20p 16p	CA3140E	74p	Clip	3p	0-15VX2 200mAX2	2400
8C186	23p	BFX30	38p	2N3703	8p	7400	28p	74178	120p	4009	16p	LM301AN LM308N	30p 54p			e terre seemine	- / •P
BC187	26p	BFX85	29p	2N3704	8p		20-p 24-p	74178	85p	4070	16p	LM308M	54p 76p				
BC207	13p	BFX86	31p	2N3706	9p	7472	24p 25p	74180	195p	4071	20p	LM381N	105p	Add	25p f	or p&p. All items new and full sp	ec
BC212	10p	8FX87	20p	2N3707	9p	7473	25p 25p	74182	75p	4072	20p 20p	NE555	25p				
BC213	10p	8FY50	15p	2N3710	8p		∠əp 48p	74184	243p	4073	20p 65p	NE556	25p 65p			A TROLLO O	0
8C214	10p	BFY51	15p	2N3711	8p	7475	28p	74190	720	4078	16p	TBA641	240p			A TECH & C	U.
8C237	14p	BFY53	28p	2N3772	177p	7480	20p 46p	74191	100p	4076	19p	TBA800	70p		6. U	A ILUII & U	
8C238	14p	BSX19	25p	2N3773	230p	7485	40p 90p	74192	100p	4082	23p	TBA810	113p			DOAD LONDON N20	
BC301	30 p	8SX20	21p	2N3866	61p	7486	26p	.74193	110p	4082	23p 24p	10/010	11.04	5Z NAY	LOK	ROAD, LONDON, N20	NUM
8C303	30p	80205	140p	2N3904	<u>8p</u>	1400	eah	14190	1100	4000	r.4h		_				
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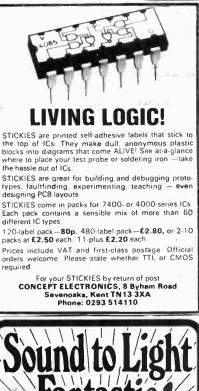
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