# HOWARD W. SAM HANDBOOK OF 

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& \text { ELECTRONIC } \\
& \text { TABLES } \\
& \text { FORMULA }
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AN INVALUABLE REFERENCE FOR TECHNICIANS, ENGINEERS, STUDENTS, EXPERIMENTERS, AND EVERYONE IN ELECTRONICS

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## HANDBOOK OF

## ELECTRONIC TABLES

## \& FORMULAS

Howard W. Sams Handbook of Electronic Tables and Formulas has been planned, compiled and published by Howard W. Sams \& Co., Inc., the world's largest publisher of electronic data. Through the unique and diversified nature of the work it performs, the Sams Engineering Staff has long been close to the "pulse of the industry." As a result of this unparalleled position, this reference book has been designed as a real time-saver and working tool for engineers, technicians, students and serious hobbyists.

Checked and re-checked for accuracy and completeness, the Howard W. Sams Handbook of Electronic Tables and Formulas represents the handiest compilation of its type on the market. As such, it will serve well as a complete reference library by itself.

# HOWARD W. SAMS <br> HANDBOOK OF <br> ELECTRONIC TABLES <br> \& FORMULAS 

## Completely Revised,

 Updated, and Expanded
## A MUST FOR ANYONE

CONNECTED WITH ELECTRONICS
Fast access to needed facts and figures is an absolute necessity to those engaged in work or study of a technical nature. The wide acceptance of the first edition of Howard W. Sams Handbook of Electronic Tables and Formulas is evidence of its success as a handy, one-source reference. This second edition has been expanded by nearly $50 \%$-and includes much of the material suggested by purchasers of the first volume. Now, more than ever, it is truly a one-stop reference.

A unique feature of this book is the 6 -page fullcolor foldout chart, which shows the latest FCC allocations for the entire frequency spectrum. This easy-touse chart shows, at a glance, which services operate within given frequency bands, and what frequencies are allocated for specific services.

## Includes Seven Major Sections

## ELECTRONIC FORMULAS AND LAWS

Formulas for voltage, current, power, resistance, capacitance, inductance, coupling coefficients, Q-factors, resonance, admittance, susceptance, conductance, energy units, reactance, impedance, power factors, time constants, transformer characteristics, voltage regulation, $D C$ meters, frequency, transmission line characteristics, modulation, decibels, and others.

## CONSTANTS AND STANDÁRDS

Dielectric constants, conversion factors, metric prefixes, standard frequencies, time signals, frequency and power tolerances of stations, commercial operator license requirements, amateur operator license requirements, amateur bands, types of emission, TV channel frequencies, TV signal standaras, audio- and radio-frequency standards, and others.

## SYMBOLS AND CODES

Q-signals, " 10 " signals, international code, Greek alphabet, electronic symbols and abbreviations, semiconductor abbreviations, color codes for transformers, resistors, and capacitors, and schematic symbols.

## SERVICE AND INSTALLATION DATA

Coaxial cables, test pattern interpretation, classes of vacuum-tube operation, miniature and gas-filled lamp data, relay rewinding data, speaker connections, machine screw and drill sizes, resistance of metal and alloys, wire table, and others.

## DESIGN DATA

Vacuum-tube and transistor formulas, three-phase power calculations, coil windings, filter and attenuator formulas.

## MATHEMATICAL TABLES AND FORMULAS

Mathematical constants and symbols, decimal equivalent of fractions, powers of 10 , slide rule, algebraic operations, geometric formulas, trigonometric functions, binary numbers, Boolean algebra, and common logarithms.

## MISCELLANEOUS DATA

Temperature conversion, power consumption of appliances, characteristics of the elements, measures and weights, metric equivalents, winds, hydraulic equations, and others.

## Hownsidann <br> HANDBOOK OF

# ELECTRONIC TABLES \& formulas 

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## PREFACE

In the Preface to the first edition of this book, published in November, 1959, we asked for recommendations of additional items to consider for inclusion in a future edition. Many suggestions were received and considered; most of them are incorporated in this volume. Hence, this book contains the information which users of the first editionengineers, technicians, students, experimenters, and hobby-ists-have told us they would like to have in a comprehensive one-stop edition.

The basic formulas and laws, so important in all branches of electronics, are given in Part One. Also included are nomographs to speed up the solution of problems involving Ohm's law, power, parallel resistance, and reactance.

Useful, but hard to remember constants, and standards which have been established by the government or industry, are included in Part Two. The comprehensive Table of Conversion Factors is especially helpful in electronic computations.

Part Three contains symbols and codes which have been adopted over the years. The latest semiconductor information is included, to keep you abreast of this rapidly expanding field.

Items of particular interest to electronics service technicians are included in Part Four. Data most often used in circuit design work are given in Part Five. The filter and attenuator configurations and formulas are particularly useful to service technicians and design engineers.

Mathematical tables, formulas, and other information are presented in Part Six. Binary numbers and an introduction to Boolean algebra-the tools of the computer field-are also included in this section. Many items of a miscellaneous nature are included in Part Seven.

No effort has been spared to make this revised handbook of maximum value to anyone, in any branch of electronics. Once again your comments, criticisms, and recommendations for additional data you would like to see included in a future edition, will be welcomed.


January, 1962

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## Electronics Formulas and Laws

## 1. OHM'S LAW FOR DIRECT CURRENT

All substances offer some obstruction to the flow of current. Ohm's law states that the current which flows is directly proportional to the applied voltage and inversely proportional to the resistance. Thus:

$$
\begin{aligned}
\mathrm{I} & =\frac{\mathrm{E}}{\mathrm{R}} \\
\mathrm{E} & =\mathrm{IR} \\
\mathrm{R} & =\frac{\mathrm{E}}{\mathrm{I}}
\end{aligned}
$$

where,


Fig. 1

I is the current in amperes, $E$ is the voltage in volts, $R$ is the resistance in ohms.

## 2. DC POWER

The power P expended in load resistance R when current I flows under a voltage pressure E can be determined by the formulas:

$$
\begin{aligned}
& \mathrm{P}=\mathrm{EI} \\
& \mathrm{P}=\mathrm{I}^{2} \mathrm{R} \\
& \mathrm{P}=\frac{\mathrm{E}^{2}}{\mathrm{R}}
\end{aligned}
$$

where,
$P$ is the power expressed in watts,
E is the voltage in volts,
I is the current in amperes,
$R$ is the resistance in ohms.

## Ohm's Law Nomograph



Fig. 2

## 3. OHM'S LAW NOMOGRAPH

The nomograph on the preceding page is a convenient way of solving most Ohm's law and DC power problems. If two values are known, the two unknown values can be determined by placing a straightedge across the two known values and reading the unknown values at the points where the straightedge crosses the appropriate scales. The figures in bold face (on the right side of all scales) cover one range of given values, and the figures in light face (on the left side) cover another range. For a given problem, all values must be read in either the bold- or light-face figures.

Example-What is the value of a resistor if a 10 -volt drop is measured across it and a current of 500 milliamperes ( .5 ampere) is flowing through it? What is the power dissipated by the resistor?
$A N S W E R$ : The value of the resistor is 20 ohms . The power dissipated in the resistor is 5 watts.

## 4. KIRCHHOFF'S LAWS

Kirchhoff's voltage law states: "The sum of the voltage drops around a DC series circuit equals the source or applied voltage. In other words, disregarding losses due to the wire resistance:

$$
\mathrm{E}_{\mathrm{T}}=\mathrm{E}_{1}+\mathrm{E}_{2}+\mathrm{E}_{3}
$$

where,

Fig. 3

$\mathrm{E}_{\mathrm{T}}$ is the source voltage,
$\mathrm{E}_{1}, \mathrm{E}_{2}$, and $\mathrm{E}_{3}$ are the voltage drops across the individual resistors.

Kirchhoff's current law states: "The current flowing toward a point in a circuit must equal the current flowing
away from that point." Hence, if a circuit is broken up into several parallel paths, the sum of the currents through the individual paths must equal the current flowing to the point where the circuit branches, or:

$$
\mathrm{I}_{\mathrm{T}}=\mathrm{I}_{1}+\mathrm{I}_{2}+\mathrm{I}_{3}
$$



Fig. 4
where,
$\mathrm{I}_{\mathrm{T}}$ is the total current flowing through the circuit, $I_{1}, I_{2}$, and $I_{3}$ are the currents flowing through the individual branches.
In a series-parallel circuit, the relationships are as follows :

$$
\begin{aligned}
\mathrm{E}_{\mathrm{T}} & =\mathrm{E}_{1}+\mathrm{E}_{2}+\mathrm{E}_{3} \\
\mathrm{I}_{\mathrm{T}} & =\mathrm{I}_{1}+\mathrm{I}_{2} \\
\mathrm{I}_{\mathrm{T}} & =\mathrm{I}_{3}
\end{aligned}
$$



Fig. 5

## 5. RESISTANCE

The following formulas can be used for calculating the total resistance in a circuit.

Resistors in series (Fig. 6) :


Fig. 6

Resistors in parallel (Fig. 7) :

$$
\mathrm{R}_{\mathrm{T}}=\frac{1}{\frac{1}{\mathrm{R}_{1}}+\frac{1}{\mathrm{R}_{2}}+\frac{1}{\mathrm{R}_{3}}+\ldots}
$$



Fig. 7

Two resistors in parallel (Fig. 8) :

$$
\mathrm{R}_{\mathrm{T}}=\frac{\mathrm{R}_{1} \times \mathrm{R}_{2}}{\mathrm{R}_{1}+\mathrm{R}_{2}}
$$



Fig. 8
where,
$R_{T}$ is the total resistance of the circuit, $R_{1}, R_{2}$, and $R_{3}$ are the values of the individual resistors.

The equivalent value of resistors in parallel can be solved with the nomograph given in Fig. 9. Place a straightedge across the points on scale $R_{1}$ and $R_{2}$ where the known value resistors fall. The point at which the straightedge crosses the $R_{T}$ scale will show the total resistance of the two resistors in parallel. If three resistors are in parallel, first find the equivalent resistance of two of the resistors, then consider this value as being in parallel with the remaining resistor.

If the total resistance needed is known, the straightedge can be placed at this value on the $R_{T}$ scale and rotated to find the various combinations of values on the $R_{1}$ and $R_{2}$ scales which will produce the needed value.

Scales $R_{1 Y}$ and $R_{T Y}$ are used with the $R_{1}$ scale when the values of the known resistors differ greatly. The range of the nomograph can be increased by multiplying the values of all scales by $10,100,1,000$, or more, as required.


Fig. 9

Example 1-What is the total resistance of a 50 -ohm and a 75 -ohm resistor in parallel.

ANSWER: 30 ohms.
Example 2-What is the total resistance of a 1,500 -ohm and a 14,000 ohm resistor in parallel?

ANSWER: 1,355 ohms. (Use $\mathrm{R}_{1}$ and $\mathrm{R}_{1 \mathrm{y}}$ scales; read answer on $\mathrm{R}_{\mathrm{T}}$ scale.)

Example 3-What is the total resistance of a 75 -ohm, an 85 -ohm, and a 120 -ohm resistor in parallel?

ANSWER: 30 ohms. (First, consider the 75 -ohm and 85 -ohm resistors, which will give 40 ohms; then consider this 40 ohms and the 120 -ohm resistor, which will give 30 ohms.)

## 6. CAPACITANCE

## (A) Total Capacitance

The following formulas can be used for calculating the total capacitance in a circuit.

Capacitors in parallel (Fig. 10) :
$\mathrm{C}_{\mathrm{T}}=\mathrm{C}_{1}+\mathrm{C}_{2}+\mathrm{C}_{3}+\ldots$.


Fig. 10

Capacitors in series (Fig. 11) :

$$
\mathrm{C}_{\mathrm{T}}=\frac{1}{\frac{1}{\mathrm{C}_{1}}+\frac{1}{\mathrm{C}_{2}}+\frac{1}{\mathrm{C}_{3}}+\ldots}
$$



Fig. 11

Two capacitors in series (Fig. 12) :

$$
\mathrm{C}_{\mathrm{T}}=\frac{\mathrm{C}_{1} \times \mathrm{C}_{2}}{\mathrm{C}_{1}+\mathrm{C}_{2}}
$$



Fig. 12
where,
$\mathrm{C}_{\mathrm{T}}$ is the total capacitance in a circuit,
$\mathrm{C}_{1}, \mathrm{C}_{2}$, and $\mathrm{C}_{3}$ are the values of the individual capacitors.
The parallel-resistance nomograph in § ${ }_{5}$ can also be used to determine the total capacitance of capacitors in series.

The capacitance of a parallel-plate capacitor is determined by :
$0.0555 f_{6}$

$$
\mathrm{C}=0.2235 \frac{\mathrm{KA}}{\mathrm{~d}}(\mathrm{~N}-1)
$$

where,
C is the capacitance in micromicrofarads, K is the dielectric constant,*
A is the area of one plate in square inches, d is the thickness of the dielectric in inches, N is the number of plates.
(B) Charge Stored

The charge stored in a capacitor is determined by :

$$
\mathrm{Q}=\mathrm{CE}
$$

where,
Q is the charge, in coulombs,
C is the capacitance in farads,
E is the voltage impressed across the capacitor.
(C) Energy Stored

The energy stored in a capacitor can be determined by :

$$
\mathrm{W}=\frac{\mathrm{CE}^{2}}{2}
$$

where,
W is the energy in joules (watt-seconds),
C is the capacitance in farads,
E is the applied voltage in volts.

[^0]
## (D) Voltage Across Series Capacitors

When an AC voltage is applied across a group of capacitors connected in series (Fig. 13), the voltage drop across the combination is, of course, equal to the applied voltage. The drop across each individual capacitor is inversely proportional to its capacitance. The drop across any capacitor in a group of series capacitors is calculated by the formula:

$$
\mathrm{E}_{\mathrm{C}}=\frac{\mathrm{E}_{\mathrm{A}} \times \mathrm{C}_{\mathrm{r}}}{\mathrm{C}}
$$



Fig. 13
where,
$\mathrm{E}_{\mathrm{C}}$ is the voltage across the individual capacitor in the series ( $\mathrm{C}_{1}, \mathrm{C}_{2}$, or $\mathrm{C}_{3}$ ),
$\mathrm{E}_{\mathrm{A}}$ is the applied voltage,
$\mathrm{C}_{\mathrm{T}}$ is the total capacitance of the series combination,
C is the capacitance of the individual capacitor under consideration.

Note: $\mathrm{C}_{\mathrm{T}}$ and C may be in any unit of measurement as long as the unit selected is the same for both.

## 7. INDUCTANCE

The following formulas can be used for calculating the total inductance in a circuit.

Inductors in series (with no mutual inductance) (Fig. 14) :


Fig. 14

Inductors in parallel (with no mutual inductance) (Fig. 15) :


Fig. 15

Two inductors in parallel (with no mutual inductance) (Fig. 16):

$$
\mathrm{L}_{\mathrm{T}}=\frac{\mathrm{L}_{1} \times \mathrm{L}_{2}}{\mathrm{~L}_{1}+\mathrm{L}_{2}}
$$

where,


Fig. 16
$\mathrm{L}_{\mathrm{T}}$ is the total inductance of the circuit,
$L_{1}, L_{2}$, and $L_{3}$ are the inductances of the individual inductors (coils).
The parallel-resistance nomograph in §can also be used to determine the total inductance of inductors in parallel.

## (A) Mutual Inductance

The mutual inductance of two coils with fields interacting can be determined by :

$$
\mathrm{M}=\frac{\mathrm{L}_{\mathrm{A}}-\mathrm{L}_{\mathrm{B}}}{4}
$$

where,
M is the mutual inductance expressed in the same unit as $\mathrm{L}_{\mathrm{A}}$ and $\mathrm{L}_{\mathrm{B}}$,
$L_{A}$ is the total inductance of coils $L_{1}$ and $L_{2}$ with fields aiding,
$L_{B}$ is the total inductance of coils $L_{1}$ and $L_{2}$ with fields opposing.

## (B) Coupled Inductance

The coupled inductance can be determined by the following formulas.

In parallel, with fields aiding:

$$
L_{T}=\frac{1}{\frac{1}{L_{1}+M}+\frac{1}{L_{2}+M}}
$$

In parallel, with fields opposing:

$$
L_{T}=\frac{1}{\frac{1}{L_{1}-M}+\frac{1}{L_{2}-M}}
$$

In series, with fields aiding:

$$
\mathrm{L}_{\mathrm{T}}=\mathrm{L}_{1}+\mathrm{L}_{2}+2 \mathrm{M}
$$

In series, with fields opposing:

$$
\mathrm{L}_{\mathrm{T}}=\mathrm{L}_{1}+\mathrm{L}_{2}-2 \mathrm{M}
$$

where,
$\mathrm{L}_{\mathrm{T}}$ is the total inductance,
$\mathrm{L}_{1}$ and $\mathrm{L}_{2}$ are the inductances of the individual coils, M is the mutual inductance.

## (C) Coupling Coefficient

When two coils are inductively coupled to give transformer action, the coupling coefficient is determined by:

$$
\mathrm{K}=\frac{\mathrm{M}}{\sqrt{\mathrm{~L}_{1} \mathrm{~L}_{2}}}
$$

where,
K is the coupling coefficient, M is the mutual inductance, $\mathrm{L}_{1}$ and $\mathrm{L}_{2}$ are the inductances of the two coils.

## (D) Energy Stored

The energy stored in an inductor can be determined by:

$$
\mathrm{W}=\frac{\mathrm{LI}^{2}}{2}
$$

where,
W is the energy in joules (watt-seconds),
L is the inductance in henries,
I is the current in amperes.

## 8. Q FACTOR

The ratio of reactance to resistance is known as the $Q$ factor. It can be determined by the following formulas.

For a coil wherein R and L are in series :

$$
\mathrm{Q}=\frac{\omega \mathrm{L}}{\mathrm{R}}
$$

For a capacitor wherein R and C are in series:

$$
\mathrm{Q}=\frac{1}{\omega \mathrm{RC}}
$$

For a capacitor wherein R and C are in parallel:

$$
\mathrm{Q}=\omega \mathrm{RC}
$$

where,
$Q$ is a ratio expressing the factor of merit,
$\omega$ equals $2 \pi f$,
L is the inductance in henries,
R is the resistance in ohms,
C is the capacitance in farads.

## 9. RESONANCE

The resonant frequency, or the frequency at which the reactances of the circuit add up to zero ( $\mathrm{X}_{\mathrm{L}}=\mathrm{X}_{\mathrm{C}}$ ), is determined by the formula:

$$
\mathrm{f}_{\mathrm{R}}=\frac{1}{2 \pi \sqrt{\mathrm{LC}}}
$$

where,
$f_{R}$ is the resonant frequency in cycles per second,
L is the inductance in henries,
C is the capacitance in farads.
The resonant frequency of various combinations of inductance and capacitance can also be obtained from the reactance charts in §14. Simply lay a straightedge across the values of inductance and capacitance, and read the resonant frequency from the frequency scale of the chart.

## 10. ADMITTANCE

The measure of the ease with which alternating current flows in a circuit is the admittance of the circuit.

Admittance of a series circuit is given by :

$$
Y=\frac{1}{\sqrt{R^{2}+X^{2}}}
$$

Admittance is also expressed as the reciprocal of impedance; thus:

$$
\mathrm{Y}=\frac{1}{\mathrm{Z}}
$$

where,
Y is the admittance in mhos,
R is the resistance in ohms,
X is the reactance in ohms,
$Z$ is the impedance in ohms.

## 11. SUSCEPTANCE

The susceptance of a series circuit is given by :

$$
\mathrm{B}=\frac{\mathrm{X}}{\mathrm{R}^{2}+\mathrm{X}^{2}}
$$

When the resistance is zero, susceptance becomes the reciprocal of reactance; thus:

$$
\mathrm{B}=\frac{1}{\mathrm{X}}
$$

where,
B is the susceptance in mhos,
X is the reactance in ohms,
$R$ is the resistance in ohms.

## 12. CONDUCTANCE

Conductance is the measure of the ability of a component to conduct electricity. Conductance for DC circuits is expressed as the reciprocal of resistance; therefore:

$$
\mathrm{G}=\frac{1}{\mathrm{R}}
$$

where,
G is the conductance in mhos,
$R$ is the resistance in ohms.

Ohm's law formulas when conductance is considered are:

$$
\begin{aligned}
\mathrm{I} & =\mathrm{EG}=\stackrel{\mathrm{E}}{\mathrm{k}} \\
\mathrm{G} & =\frac{\mathrm{I}}{\mathrm{E}} \\
\mathrm{E} & =\frac{\mathrm{I}}{\mathrm{G}}
\end{aligned}
$$

where,
I is the current in amperes,
E is the voltage in volts,
G is the conductance in mhos, $R$ is the resistance in ohms.

## 13. ENERGY UNITS

Energy is the capacity or ability to do work. The joule is a unit of energy. One joule is the amount of energy required to maintain a current of one ampere for one second through a resistance of one ohm. It is equivalent to a watt-second. The watt-hour is the practical unit of energy; 3600 wattseconds equals one watt-hour. The number of watt-hours is calculated:

$$
\text { Watt-hours }=P \times T
$$

where,
$P$ is the power in watts,
T is the time in hours the power is dissipated.
See § 6 for the energy stored in a capacitor, and § 7 for the energy stored in an inductor.

## 14. REACTANCE

The opposition to the flow of alternating current by the inductance or capacitance of a component or circuit is called the reactance.

## (A) Capacitive Reactance

The reactance of a capacitor may be calculated by the formula:

$$
\mathrm{X}_{\mathrm{C}}=\frac{1}{2 \pi \mathrm{fC}}
$$

where,
$\mathrm{X}_{\mathrm{C}}$ is the reactance in ohms, $f$ is the frequency in cycles per second, C is the capacitance in farads.

## (B) Inductive Reactance

The reactance of an inductor may be calculated by the formula:

$$
\mathrm{X}_{\mathrm{L}}=2 \pi \mathrm{fL}
$$

where,
$\mathrm{X}_{\mathrm{L}}$ is the reactance in ohms, f is the frequency in cycles per second, L is the inductance in henries.

## (C) Reactance Charts

Charts for determining unknown values of reactance, inductance, capacitance, and frequency are given on the following pages. The chart in Fig. 17A covers 1 to 1,000 cycles, Fig. 17B covers 1 to 1,000 kilocycles, and Fig. 17C covers 1 to 1,000 megacycles.

To find the amount of reactance of a capacitor at a given frequency, lay the straightedge across the capacitor value and the frequency. Then read the reactance from the reactance scale. By extending the line, the value of an inductance which will give the same reactance can be obtained.

Since $\mathrm{X}_{\mathrm{C}}=\mathrm{X}_{\mathrm{L}}$ at resonance, by laying the straightedge across the capacitance and inductance values, the resonant frequency of the combination can be determined.

Example-If the frequency is 10 cycles per second and the capacitance is 50 mfd , what is the reactance of the capacitor? What value of inductance will give this same reactance?

ANSWER: The reactance is 310 ohms. The inductance needed to produce this same reactance is 5 henries. Thus, it follows that a $50-\mathrm{mfd}$ capacitor and a 5 -henry choke are resonant at 10 cps . [Place the straightedge, on the proper chart (Fig. 17A), across 10 cps and 50 mfd . Read the values indicated on the reactance and inductance scales.]

## 15. IMPEDANCE

The basic formulas for calculating the total impedance are as follows.

For parallel circuits:

$$
\mathrm{Z}=\frac{1}{\sqrt{\mathrm{G}^{2}+\mathrm{B}^{2}}}
$$

Reactance Chart - 1 cps to 1 kc


Fig. 17A

Reactance Chart - 1 kc to 1 mc


Fig. 17B

Reactance Chart - 1 mc to $1,000 \mathrm{mc}$


Fig. 17C

For series circuits:

$$
\mathrm{Z}=\sqrt{\mathrm{R}^{2}+\mathrm{X}^{2}}
$$

where,
Z is the total impedance,
G is the total conductance or the reciprocal of the total parallel resistance,
$B$ is the total susceptance,
R is the total resistance,
X is the total reactance.
The following formulas can be used to find the impedance of the various combinations of inductance, capacitance, and resistance.

For a single resistance (Fig. 18) :

$$
\begin{aligned}
& \mathrm{Z}=\mathrm{R} \\
& \theta=0^{\circ}
\end{aligned}
$$



Fig. 18

For resistances in series (Fig. 19) :

$$
\begin{aligned}
\mathrm{Z} & =\mathrm{R}_{1}+\mathrm{R}_{2}+\mathrm{R}_{3}+\cdots \\
\theta & =0^{\circ}
\end{aligned}
$$



Fig. 19

For a single inductance (Fig. 20) :

$$
\begin{aligned}
\mathrm{Z} & =\mathrm{X}_{\mathrm{L}} \\
\theta & =90^{\circ}
\end{aligned}
$$

$\qquad$
L Fig. 20

For inductances in series (with no mutual inductance) (Fig. 21) :
$\begin{aligned} \mathrm{Z} & =\mathrm{X}_{\mathrm{L}_{1}}+\mathrm{X}_{\mathrm{L}_{2}}+\mathrm{X}_{\mathrm{L}_{3}}+\ldots \\ \theta & =90^{\circ}\end{aligned}$


Fig. 21
For a single capacitance (Fig. 22) :

$$
\begin{aligned}
\mathrm{Z} & =\mathrm{X}_{\mathrm{C}} \\
\theta & =90^{\circ}
\end{aligned}
$$



Fig. 22

For capacitances in series (Fig. 23) :

$$
\begin{aligned}
\mathrm{Z} & =\mathrm{X}_{\mathrm{C}_{1}}+\mathrm{X}_{\mathrm{C}_{2}}+\mathrm{X}_{\mathrm{C}_{3}}+\ldots \\
\theta & =90^{\circ}
\end{aligned}
$$



Fig. 23

For resistance and inductance in series (Fig. 24) :

$$
\begin{aligned}
& \mathrm{Z}=\sqrt{\mathrm{R}^{2}+\mathrm{X}_{\mathrm{L}}{ }^{2}} \\
& \theta=\arctan \frac{\mathrm{X}_{\mathrm{L}}}{\mathrm{R}}
\end{aligned}
$$



Fig. 24

For resistance and capacitance in series (Fig. 25) :

$$
\begin{aligned}
& \mathrm{Z}=\sqrt{\mathrm{R}^{2}+\mathrm{X}_{\mathrm{C}}{ }^{2}} \\
& \theta=\arctan \frac{\mathrm{X}_{\mathrm{C}}}{\mathrm{R}}
\end{aligned}
$$



Fig. 25

For inductance and capacitance in series (Fig. 26) :
When $\mathrm{X}_{\mathrm{L}}$ is larger than $\mathbf{X}_{\mathbf{C}}$

$$
\mathrm{Z}=\mathrm{X}_{\mathrm{L}}-\mathrm{X}_{\mathrm{C}}
$$

When $\mathrm{X}_{\mathrm{C}}$ is larger than $\mathrm{X}_{\mathrm{L}}$


Fig. 26

$$
\begin{aligned}
\mathrm{Z} & =\mathrm{X}_{\mathrm{C}}-\mathrm{X}_{\mathrm{L}} \\
\theta & =0^{\circ} \text { when } \mathrm{X}_{\mathrm{L}}=\mathrm{X}_{\mathrm{C}}
\end{aligned}
$$

For resistance, inductance, and capacitance in series (Fig. 27) :

$$
\begin{aligned}
& \mathrm{Z}=\sqrt{\mathrm{R}^{2}+\left(\mathrm{X}_{\mathrm{L}}-\mathrm{X}_{\mathrm{C}}\right)^{2}} \\
& \theta=\arctan \frac{\mathrm{X}_{\mathrm{L}}-\mathrm{X}_{\mathrm{C}}}{\mathrm{R}}
\end{aligned}
$$



Fig. 27

For resistances in parallel (Fig. 28) :

$$
\begin{aligned}
& \mathrm{Z}=\frac{1}{\frac{1}{\mathrm{R}_{1}}+\frac{1}{\mathrm{R}_{2}}+\frac{1}{\mathrm{R}_{3}}+\ldots} \\
& \theta=0^{\circ}
\end{aligned}
$$



Fig. 28

For inductances in parallel (with no mutual inductance) (Fig. 29) :

$$
\begin{aligned}
& \mathrm{Z}=\frac{1}{\frac{1}{\mathrm{X}_{\mathrm{L}_{1}}}+\frac{1}{\mathrm{X}_{\mathrm{L}_{2}}}+\frac{1}{\mathrm{X}_{\mathrm{L}_{3}}}+\ldots} \\
& \theta=90^{\circ}
\end{aligned}
$$



Fig. 29

For capacitances in parallel (Fig. 30) :


For resistance and inductance in parallel (Fig. 31) :

$$
\begin{aligned}
& \mathrm{Z}=\frac{\mathrm{RX}}{\mathrm{~L}} \\
& \sqrt{\mathrm{R}^{2}+\mathrm{X}_{\mathrm{L}}{ }^{2}} \\
& \theta=\arctan \frac{\mathrm{R}}{\mathrm{X}_{\mathrm{L}}}
\end{aligned}
$$



Fig. 31

For capacitance and resistance in parallel (Fig. 32) :

$$
\begin{aligned}
& \mathrm{Z}=\frac{\mathrm{RX}}{\mathrm{X}_{\mathrm{C}}} \\
& \sqrt{\mathrm{R}^{2}+\mathrm{X}_{\mathrm{C}}{ }^{2}} \\
& \theta=\arctan \frac{\mathrm{R}}{\mathrm{X}_{\mathrm{C}}}
\end{aligned}
$$



Fig. 32

For capacitance and inductance in parallel (Fig. 33) :
When $X_{L}$ is larger than $X_{C}$ :
$\mathrm{Z}=\frac{\mathrm{X}_{\mathrm{L}}, \mathrm{X}_{\mathrm{C}}}{\mathrm{X}_{\mathrm{L}}-\mathrm{X}_{\mathrm{C}}}$
When $\mathrm{X}_{\mathrm{C}}$ is larger than $\mathrm{X}_{\mathrm{L}}$ :
$\mathrm{Z}=\frac{\mathrm{X}_{\mathrm{C}} \mathrm{X}_{\mathrm{L}}}{\mathrm{X}_{\mathrm{C}}-\mathrm{X}_{\mathrm{L}}}$


Fig. 33

$$
\theta=0^{\circ} \text { when } \mathrm{X}_{\mathrm{L}}=\mathrm{X}_{\mathrm{C}}
$$

For inductance, capacitance, and resistance in parallel (Fig. 34) :

$$
\begin{aligned}
& \mathrm{Z}=\frac{\mathrm{RX}_{\mathrm{L}} \mathrm{X}_{\mathrm{C}}}{{\sqrt{\mathrm{X}_{\mathrm{L}}{ }^{2} \mathrm{X}_{\mathrm{C}}^{2}+\mathrm{R}^{2}\left(\mathrm{X}_{\mathrm{L}}-\mathrm{X}_{\mathrm{C}}\right)^{2}}}^{2}} \begin{aligned}
& \\
& \theta \arctan \frac{\mathrm{R}\left(\mathrm{X}_{\mathrm{L}}-\mathrm{X}_{\mathrm{C}}\right)}{\mathrm{X}_{\mathrm{L}} \mathrm{X}_{\mathrm{C}}}
\end{aligned}
\end{aligned}
$$



Fig. 34

For inductance and series resistance in parallel with resistance (Fig. 35) :

$$
\begin{aligned}
& \mathrm{Z}=\mathrm{R}_{2} \sqrt{\frac{\mathrm{R}_{1}{ }^{2}+\mathrm{X}_{\mathrm{L}}{ }^{2}}{\left(\mathrm{R}_{1}+\mathrm{R}_{2}\right)^{2}+\mathrm{X}_{\mathrm{L}}{ }^{2}}} \\
& \theta=\arctan \frac{\mathrm{X}_{\mathrm{L}} \mathrm{R}_{2}}{\mathrm{R}_{1}{ }^{2}+\mathrm{X}_{\mathrm{r}}{ }^{2}+\mathrm{R}_{1} \mathrm{R}_{2}}
\end{aligned}
$$



Fig. 35

For inductance and series resistance in parallel with capacitance (Fig. 36) :


For capacitance and series resistance in parallel with inductance and series resistance (Fig. 37) :

$$
\mathrm{Z}=\sqrt{\frac{\left(\mathrm{R}_{1}{ }^{2}+\mathrm{X}_{\mathrm{L}}{ }^{2}\right)\left(\mathrm{R}_{2}{ }^{2}+\mathrm{X}_{\mathrm{c}}{ }^{2}\right)}{\left(\mathrm{R}_{1}+\mathrm{R}_{2}\right)^{2}+\left(\mathrm{X}_{\mathrm{L}}-\mathrm{X}_{\mathrm{C}}\right)^{2}}}
$$



Fig. 37
$\theta=\arctan \frac{\mathrm{X}_{\mathrm{L}}\left(\mathrm{R}_{2}{ }^{2}+\mathrm{X}_{\mathrm{C}}{ }^{2}\right)-\mathrm{X}_{\mathrm{C}}\left(\mathrm{R}_{1}{ }^{2}+\mathrm{X}_{\mathrm{L}}{ }^{2}\right)}{\mathrm{R}_{1}\left(\mathrm{R}_{2}{ }^{2}+\mathrm{X}_{\mathrm{C}}{ }^{2}\right)+\mathrm{R}_{2}\left(\mathrm{R}_{1}{ }^{2}+\mathrm{X}_{\mathrm{L}}{ }^{2}\right)}$
where,
Z is the impedance in ohms,
R is the resistance in ohms,
L is the inductance in henries,
$\mathrm{X}_{\mathrm{L}}$ is the inductive reactance in ohms,
$\mathrm{X}_{\mathrm{C}}$ is the capacitive reactance in ohms,
$\theta$ is the phase angle in degrees by which the current leads the voltage in a capacitive circuit or lags the voltage in an inductive circuit. $0^{\circ}$ indicates an in-phase condition.

## 16. OHM'S LAW FOR ALTERNATING CURRENT

The fundamental Ohm's law formulas for alternating current are given by :

$$
\begin{aligned}
\mathrm{E} & =\mathrm{IZ} \\
\mathrm{I} & =\frac{\mathrm{E}}{\mathrm{Z}} \\
\mathrm{Z} & =\frac{\mathrm{E}}{\mathrm{I}}
\end{aligned}
$$



Fig. 38
where,
E is the voltage in volts,
$I$ is the current in amperes,
Z is the impedance in ohms.
The power expended in an AC circuit is calculated by the formula:

$$
\mathrm{P}=\mathrm{EI} \cos \theta
$$

where,
$P$ is the power in watts,
E is the voltage in volts,
I is the current in amperes,
$\theta$ is the phase angle in degrees.
The phase angle is the difference in degrees by which the current leads or lags the voltage in a reactive circuit. In a series circuit, the phase angle is determined by the formula:

$$
\theta=\arctan \frac{X}{\mathrm{R}}
$$

where,
X is the inductive or capacitive reactance in ohms, $R$ is the nonreactive resistance in ohms.

Therefore:
For a purely resistive circuit:

$$
\begin{aligned}
\theta & =0^{\circ} \\
\cos \theta & =1 \\
\mathrm{P} & =\mathrm{EI}
\end{aligned}
$$

For a resonant circuit:

$$
\begin{aligned}
\theta & =0^{\circ} \\
\cos \theta & =1 \\
\mathrm{P} & =\mathrm{EI}
\end{aligned}
$$

For a purely reactive circuit:

$$
\begin{aligned}
\theta & =90^{\circ} \\
\cos \theta & =0 \\
\mathrm{P} & =0
\end{aligned}
$$

## 17. AVERAGE, RMS, PEAK, AND PEAK-TO-PEAK VOLTAGE AND CURRENT

The following table can be used to convert sinusoidal voltage (or current) values from one method of measurement to another. To use the table, first find the given type of reading in the left-hand column, then find the desired type of reading across the top of the table. To convert the given value to the desired value, multiply the given value by the factor listed under the desired value.

Example-What factor must peak voltage be multiplied by to obtain rms voltage?

ANSWER: .707.

Table I. Average, Rms, Peak, and Peak-to-Peak Values

| Given <br> Value | Multiplying Factor To Get |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Average | Rms | Peak | Peak-to-Peak |
| Average | - | 1.11 | 1.57 | 3.14 |
| Rms | 0.9 | - | 1.414 | 2.828 |
| Peak | 0.637 | 0.707 | - | 2.0 |
| Peak-to-Peak | 0.32 | 0.3535 | 0.5 | - |

## 18. POWER FACTOR

Power factor is the ratio of true power to apparent power in an alternating circuit. Thus:

$$
\begin{aligned}
\mathrm{pf} & =\frac{\mathrm{P}_{\mathrm{T}}}{\mathrm{P}_{\mathrm{A}}}=\frac{\mathrm{EI} \cos \theta}{\mathrm{EI}} \\
& =\cos \theta
\end{aligned}
$$



Fig. 39
where,
pf is the power factor,
$\mathrm{P}_{\mathrm{T}}$ is the true power in watts,
$P_{A}$ is the apparent power in volt-amperes,
EI $\cos \theta$ is the true power in watts,
EI is the apparent power in volt-amperes.

Therefore:
For a purely resistive circuit:

$$
\begin{aligned}
\theta & =0^{\circ} \\
\mathrm{pf} & =1
\end{aligned}
$$

For a resonant circuit:

$$
\begin{aligned}
\theta & =0^{\circ} \\
\mathrm{pf} & =1
\end{aligned}
$$

For a purely reactive circuit:

$$
\begin{aligned}
\theta & =90^{\circ} \\
\mathrm{pf} & =0
\end{aligned}
$$

## 19. TIME CONSTANTS

A certain amount of time is required, after a DC voltage has been applied to an R-C or R-L circuit, before the capacitor can charge or the current can build up to a portion of the full value. This time is called the time constant of the circuit. However, the time constant is not the time required for the voltage or current to reach the full value; instead, it is the time required to reach $63.2 \%$ of full value. During the next time constant, the capacitor is charged or the current builds
up to $63.2 \%$ of the remaining difference, or to $86.5 \%$ of the full value. Table II gives the per cent of full charge on a capacitor, or current buildup in an inductance after each time constant. Theoretically, the charge on the capacitor, or the current through the coil, can never reach $100 \%$. However, it is usually considered to be $100 \%$ after five time constants.

Table II. Time Constants versus Per Cent of Voltage or Current

| No. of <br> Time Constants | \% Charge <br> or Buildup | \% Discharge <br> or Decay |
| :---: | :---: | :---: |
| 1 | 63.2 | 36.8 |
| 2 | 86.5 | 13.5 |
| 3 | 95.0 | 5.0 |
| 4 | 98.2 | 1.8 |
| 5 | 99.3 | 0.7 |

Likewise, when the voltage source is removed, the capacitor will discharge or the current will decay $63.2 \%$, or to $36.8 \%$ of full value during the first time constant. Table II also gives the per cent of full voltage after each time constant for discharge of a capacitor or decay of the current through a coil.

The time per time constant is calculated as follows.
For an R-C circuit (Fig. 40) :

$$
\mathrm{T}=\mathrm{RC}
$$



Fig. 40
For an R-L circuit (Fig. 41) :

$$
T=\frac{L}{\mathrm{R}}
$$



Fig. 41
where,
T is the time in seconds,
R is the resistance in ohms,
C is the capacitance in farads,
L is the inductance in henries.

In addition, the values can also be expressed by the following relationships:

| T | R | C or L |
| :--- | :--- | :--- |
| seconds | megohms | microfarads |
| seconds | megohms | microhenries |
| microseconds | ohms | microfarads |
| microseconds | megohms | micromicrofarads |
| microseconds | ohms | microhenries |

## 20. TRANSFORMER FORMULAS

In a transformer, the relationships between the number of turns in the primary and secondary, the voltage across each winding, and the current through the windings are expressed by the equations:

$$
\frac{\mathrm{E}_{\mathrm{p}}}{\mathrm{E}_{\mathrm{s}}}=\frac{\mathrm{N}_{\mathrm{p}}}{\mathrm{~N}_{\mathrm{s}}} \quad \text { and } \quad \frac{\mathrm{E}_{\mathrm{p}}}{\mathrm{E}_{\mathrm{s}}}=\frac{\mathrm{I}_{\mathrm{s}}}{\mathrm{I}_{\mathrm{p}}}
$$

By rearranging these equations, any unknown can be determined from the following formulas:

$$
\begin{aligned}
& E_{p}=\frac{E_{s} N_{p}}{N_{s}}=\frac{E_{\mathrm{s}} I_{\mathrm{s}}}{\mathrm{I}_{\mathrm{p}}} \\
& \mathrm{E}_{\mathrm{s}}=\frac{\mathrm{E}_{\mathrm{p}} N_{\mathrm{s}}}{\mathrm{~N}_{\mathrm{p}}}=\frac{\mathrm{E}_{\mathrm{p}} \mathrm{I}_{\mathrm{p}}}{\mathrm{I}_{\mathrm{s}}} \\
& \mathrm{~N}_{\mathrm{p}}=\frac{\mathrm{E}_{\mathrm{p}} \mathrm{~N}_{\mathrm{s}}}{\mathrm{E}_{\mathrm{s}}}=\frac{\mathrm{N}_{\mathrm{s}}}{\mathrm{I}_{\mathrm{p}}} \\
& \mathrm{~N}_{\mathrm{s}}=\frac{\mathrm{E}_{\mathrm{s}} \mathrm{~N}_{\mathrm{p}}}{\mathrm{E}_{\mathrm{p}}}=\frac{\mathrm{N}_{\mathrm{p}}}{\mathrm{I}_{\mathrm{s}}} \\
& \mathrm{I}_{\mathrm{p}}=\frac{\mathrm{E}_{\mathrm{s}}}{\mathrm{E}_{\mathrm{p}}}=\frac{\mathrm{N}_{\mathrm{s}}}{\mathrm{~N}_{\mathrm{p}}} \\
& \mathrm{I}_{\mathrm{s}}=\frac{\mathrm{E}_{\mathrm{p}} \mathrm{I}_{\mathrm{p}}}{\mathrm{E}_{\mathrm{s}}}=\frac{\mathrm{N}_{\mathrm{p}} \mathrm{I}_{\mathrm{p}}}{\mathrm{~N}_{\mathrm{s}}}
\end{aligned}
$$



Fig. 42

The turns ratio of a transformer is determined by the following formulas:

For a step-up transformer:

$$
\mathrm{T}=\frac{\mathrm{N}_{\mathrm{s}}}{\mathrm{~N}_{\mathrm{p}}}
$$

For a step-down transformer:

$$
\mathrm{T}=\frac{\mathrm{N}_{\mathrm{p}}}{\mathrm{~N}_{\mathrm{s}}}
$$

The impedance ratio of a transformer is determined by :

$$
\mathrm{Z}=\mathrm{T}^{2}
$$

The impedance of an unknown winding is determined by the following:

For a step-up transformer:

$$
\begin{aligned}
& \mathrm{Z}_{\mathrm{p}}=\frac{\mathrm{Z}_{\mathrm{s}}}{\mathrm{Z}} \\
& \mathrm{Z}_{\mathrm{s}}=\mathrm{Z} \times \mathrm{Z}_{\mathrm{p}}
\end{aligned}
$$

For a step-down transformer:

$$
\begin{aligned}
& \mathrm{Z}_{\mathrm{p}}=\mathrm{Z} \times \mathrm{Z}_{\mathrm{s}} \\
& \mathrm{Z}_{\mathrm{s}}=\frac{\mathrm{Z}_{\mathrm{p}}}{\mathrm{Z}}
\end{aligned}
$$

where,
$\mathrm{E}_{\mathrm{p}}$ is the voltage across the primary winding,
$\mathrm{E}_{\mathrm{g}}$ is the voltage across the secondary winding,
$\mathrm{N}_{\mathrm{p}}$ is the number of turns in the primary winding,
$\mathrm{N}_{\mathrm{s}}$ is the number of turns in the secondary winding,
$\mathrm{I}_{\mathrm{p}}$ is the current through the primary winding,
$\mathrm{I}_{\mathrm{s}}$ is the current through the secondary winding,
T is the turns ratio,
Z is the impedance ratio,
$\mathrm{Z}_{\mathrm{p}}$ is the impedance of the primary winding,
$\mathrm{Z}_{\mathrm{s}}$ is the impedance of the secondary winding.

## 21. VOLTAGE REGULATION

When a load is connected to a power supply, the output voltage drops because more current flows through the resistive elements of the power supply. Voltage regulation is a measure of how much the voltage drops and is usually expressed as a percentage. It is determined by the following formula:

$$
\% \mathrm{R}=\frac{\mathrm{E}_{1}-\mathrm{E}_{2}}{\mathrm{E}_{2}} \times 100
$$

where,
$\% \mathrm{R}$ is the voltage regulation in per cent,
$\mathrm{E}_{1}$ is the no-load voltage,
$\mathrm{E}_{2}$ is the voltage under load.

## 22. DC METER FORMULAS

The basic instrument for testing current and voltage is the moving-coil meter. The meter can be either a DC milliammeter or a DC microammeter. A series resistor converts the meter to a DC voltmeter, and a parallel resistor converts the meter to a DC ammeter. The resistance of the meter movement is determined first, as follows. Connect a suitable variable resistor $\mathrm{R}_{\mathrm{a}}$ and a battery as shown in Fig. 43. Adjust resistor $\mathrm{R}_{\mathrm{a}}$ until full-scale deflection is obtained. Then connect a variable resistor $\mathrm{R}_{\mathrm{b}}$ in parallel with the meter, and adjust $R_{b}$ until half-scale deflection is obtained. Disconnect


Fig. 43
$R_{b}$ and measure its resistance. The measured value is the resistance of the meter movement.
(A) Voltage Multipliers

$$
\mathrm{R}=\frac{\mathrm{E}_{\mathrm{s}}}{\mathrm{I}_{\mathrm{s}}}-\mathrm{R}_{\mathrm{m}}
$$



Fig. 44
where,
R is the multiplier resistance in ohms, $\mathrm{E}_{\mathrm{s}}$ is the full-scale reading in volts, $\mathrm{I}_{\mathrm{s}}$ is the full-scale reading in amperes, $R_{m}$ is the meter resistance in ohms.
(B) Shunt-type Ohmmeter for Low Resistance

$$
\mathrm{R}_{\mathrm{x}}=\mathrm{R}_{\mathrm{m}} \frac{\mathrm{I}_{2}}{\mathrm{I}_{\mathbf{1}}-\mathrm{I}_{2}}
$$



Fig. 45
where,
$\mathrm{R}_{\mathrm{x}}$ is the unknown resistance,
$\mathrm{R}_{\mathrm{m}}$ is the meter resistance in ohms,
$\mathrm{I}_{1}$ is the current reading with probes open,
$I_{2}$ is the current reading with probes connected across unknown resistor,
$R_{1}$ is a variable resistance for current limiting to keep meter adjusted for full-scale reading with probes open.
(C) Series-type Ohmmeter for High Resistance

$$
\mathrm{R}_{\mathrm{x}}=\left(\mathrm{R}_{1}+\mathrm{R}_{\mathrm{m}}\right) \frac{\mathrm{I}_{1}-\mathrm{I}_{2}}{\mathrm{I}_{2}}
$$



Fig. 46
where,
$\mathrm{R}_{\mathrm{X}}$ is the unknown resistance,
$R_{1}$ is a variable resistance adjusted for full-scale reading with probes shorted together,
$R_{n 1}$ is the meter resistance in ohms,
$\mathrm{I}_{1}$ is the current reading with probes shorted,
$\mathrm{I}_{2}$ is the current reading with unknown resistor connected.
(D) Ammeter Shunts

$$
\mathrm{R}=\frac{\mathrm{R}_{\mathrm{m}}}{\mathrm{~N}-1}=\frac{\mathrm{I}_{\mathrm{m}} \mathrm{R}_{\mathrm{m}}}{\mathrm{I}_{\mathrm{s}}}
$$

where,


Fig. 47
$R$ is the resistance of the shunt, $\mathrm{R}_{\mathrm{m}}$ is the meter resistance in ohms,
N is the scale multiplication factor,
$\mathrm{I}_{\mathrm{m}}$ is the meter current,
$\mathrm{I}_{8}$ is the shunt current.
(E) Ammeter With Multirange Shunt

$$
\mathrm{R}_{2}=\frac{\left(\mathrm{R}_{1}+\mathrm{R}_{2}\right)+\mathrm{R}_{\mathrm{m}}}{\mathrm{~N}}
$$



Fig. 48
where,
$\mathrm{R}_{2}$ is the intermediate value in ohms,
$R_{1}+R_{2}$ is the total shunt resistance for lowest full-scale reading,
$\mathrm{R}_{\mathrm{m}}$ is the meter resistance in ohms,
N is the scale multiplication factor.

## 23. FREQUENCY AND WAVELENGTH

## (A) Formulas

Since the frequency is the number of complete cycles per second and since radio waves travel at a fixed speed, it follows that a complete cycle occupies a given distance in space. The distance between two corresponding parts of two waves (the two positive or negative crests or the points where the two waves cross the zero axis in a given direction) constitutes the wavelength. If either the frequency or the wavelength is known, the other can be computed as follows:

$$
\begin{aligned}
& f=\frac{300,000}{\lambda} \\
& \lambda=\frac{300,000}{f}
\end{aligned}
$$

where,
$f$ is the frequency in kilocycles,
$\lambda$ is the wavelength in meters.
If it is desired to calculate the wavelength in feet, the following formulas should be used:

$$
\begin{aligned}
& f=\frac{984,000}{\lambda} \\
& \lambda=\frac{984,000}{f}
\end{aligned}
$$

where,
f is the frequency in kilocycles,
$\lambda$ is the wavelength in feet.

## (B) Conversion Chart

The wavelength of any frequency from 30 kc to 3000 mc can be read directly from the chart in Fig. 49. Likewise, if the wavelength is known, the corresponding frequency can be obtained from the chart for wavelengths from 10 centimeters to 1000 meters. To use the chart, merely find the

## Frequency-Wavelength Conversion Chart


known value (either frequency or wavelength) on one of the scales, and then read the corresponding value from the opposite side of the scale.

Example-What is the wavelength of a 4 -mc signal?
ANSWER: 75 meters. (Find 4 mc on the third scale from the left. Opposite 4 mc on the frequency scale we find 75 meters on the wavelength scale.)

## 24. TRANSMISSION-LINE FORMULAS

The characteristic impedance of a transmission line is defined as the input impedance of a line of the same configuration and dimensions but of infinite length. When a line of finite length is terminated with an impedance equal to its own characteristic impedance, the line is said to be matched.

## (A) Coaxial Line

The characteristic impedance of a coaxial line is given by :

$$
\mathrm{Z}_{\mathrm{o}}=\frac{138}{\sqrt{\mathrm{k}}} \log \frac{\mathrm{D}}{\mathrm{~d}}
$$



Fig. 50
where,
$\mathrm{Z}_{\mathrm{o}}$ is the characteristic impedance,
D is the inside diameter of the outer conductor,
d is the outside diameter of the inner conductor expressed
in the same units as D,
k is the dielectric constant of the insulating material* ( $k$ equals 1 for dry air).

The attenuation of coaxial line in decibels per foot can be determined by the formula:

$$
a=\frac{4.6 \sqrt{f}(D+d)}{D \times d\left(\log \frac{D}{d}\right)} \times 10^{-\varepsilon}
$$

where,
a is the attenuation in decibels per foot of line,
$f$ is the frequency in megacycles,
$D$ is the inside diameter of the outer conductor in inches, d is the outside diameter of the inner conductor in inches.

[^1]
## (B) Parallel-Conductor Line

The characteristic impedance of parallel-conductor line (twin-lead) is determined by the formula:

$$
\mathrm{Z}_{\mathrm{o}}=\frac{276}{\sqrt{\mathrm{k}}} \log \frac{2 \mathrm{D}}{\mathrm{~d}}
$$

where,


Fig. 51
$\mathrm{Z}_{\mathrm{o}}$ is the characteristic impedance,
D is the center-to-center distance between conductors, d is the diameter of the conductors in the same units as $D$, k is the dielectric constant of the insulating material between conductors* (k equals 1 for dry air).

## 25. MODULATION FORMULAS

## (A) Amplitude Modulation

The amount of modulation of an amplitude-modulated carrier is referred to as the percentage of modulation. It can be determined by the following formulas:

$$
\% M=\frac{\mathrm{E}_{\mathrm{G}}-\mathrm{E}_{\mathrm{T}}}{2 \mathrm{E}_{\mathrm{AV}}} \times 100
$$

or,

$$
\% M=\frac{E_{C}-E_{T}}{E_{C}+E_{T}} \times 100
$$

where,
$\% \mathrm{M}$ is the percentage of modulation,
$\mathrm{E}_{\mathrm{C}}$ is the amplitude of the crest of the modulated carrier, $\mathrm{E}_{\mathrm{T}}$ is the amplitude of the trough of the modulated carrier, $\mathrm{E}_{\mathrm{Av}}$ is the average amplitude of the modulated carrier.

Also, the percentage of modulation can be determined by applying the modulated carrier wave to the vertical plates and the modulating voltage wave to the horizontal plates of an oscilloscope. This produces a trapezoidal wave, as shown in Fig. 53. The dimensions A and B are proportional to the crest and trough amplitudes, respectively. The percentage

[^2]of modulation can be determined by measuring the height of A and B , and using the formula:
$$
\% M=\frac{A-B}{A+B} \times 100
$$


Fig. 53
where,
$\% \mathrm{M}$ is the percentage of modulation,
A and B are the dimensions measured in Fig. 53.
The sideband power of an AM carrier is determined by:

$$
\mathrm{P}_{\mathrm{sB}}=\frac{\% \mathrm{M}^{2}}{2} \times \mathrm{P}_{\mathrm{C}}
$$

The total radiated power is the sum of the carrier and the radiated powers:

$$
P_{T}=P_{S B}+P_{C}
$$

where,
$\mathrm{P}_{\mathrm{sB}}$ is the sideband power (includes both sidebands),
$\% \mathrm{M}$ is the percentage of modulation,
$\mathrm{P}_{\mathrm{C}}$ is the carrier power,
$\mathrm{P}_{\mathrm{T}}$ is the total radiated power.
Note: The carrier power does not change with modulation.

## (B) Frequency Modulation

In a frequency-modulated carrier, the amount the carrier frequency changes is determined by the amplitude of the modulating signal, and the number of times the changes occur per second is determined by the frequency of the modulating signal.

The percentage of modulation of an FM carrier can be computed from:

$$
\% M=\frac{\Delta f}{\Delta f \text { for } 100 \% M} \times 100
$$

where,
$\% \mathrm{M}$ is the percentage of modulation,
$\Delta f$ is the change in frequency, or the deviation,
$\Delta \mathrm{f}$ for $100 \% \mathrm{M}$ is the change in frequency for a $100 \%$ modulated carrier. (For commercial FM, 75 kc ; for television sound, 25 kc ; and for two-way radio, 15 kc .)

The modulation index of an FM carrier is determined by :

$$
M=\frac{f_{d}}{f_{u}}
$$

where,
M is the modulation index,
$f_{d}$ is the deviation in frequency,
$f_{a}$ is the modulating audio frequency in the same units as $f_{d}$.

## 26. DECIBELS AND VOLUME UNITS

(A) Equations

The number of decibels corresponding to a given power ratio is 10 times the common logarithm of the ratio. Thus:

$$
\mathrm{db}=10 \log \frac{\mathrm{P}_{2}}{\mathrm{P}_{1}}
$$

The number of decibels corresponding to a given voltage or current ratio is 20 times the common logarithm of the ratio. Thus, when the impedances across which the signals are being measured are equal, the equations are:

$$
\begin{aligned}
& \mathrm{db}=20 \log \frac{\mathrm{E}_{2}}{\mathrm{E}_{1}} \\
& \mathrm{db}=20 \log \frac{\mathrm{I}_{2}}{\mathrm{I}_{1}}
\end{aligned}
$$

If the impedances across which the signals are measured are not equal, the equations become:

$$
\begin{aligned}
& \mathrm{db}=20 \log \frac{\mathrm{E}_{2} \sqrt{\mathrm{Z}_{1}}}{\mathrm{E}_{1} \sqrt{\mathrm{Z}_{2}}} \\
& \mathrm{db}=20 \log \frac{\mathrm{I}_{2} \sqrt{\mathrm{Z}_{2}}}{\mathrm{I}_{1} \sqrt{\mathrm{Z}_{1}}}
\end{aligned}
$$

## (B) Reference Levels

The decibel is not an absolute value; it is a means of stating the ratio of a level to a certain reference level. Usually, when no reference level is given, it is 6 millivolts across a 500 -ohm impedance. However, the reference level should be stated whenever a value in db's is given. Other units, which
do have specific reference levels, have been established. Some of the more common are:
dbk -1 kilowatt
dbm - 1 milliwatt, 600 ohms
dbv -1 volt
dbw -1 watt
dbvg —voltage gain
dbrap-decibels above a reference acoustical power of $10^{-16}$ watts
VU - 1 milliwatt, 600 ohms (complex waveforms varying in both amplitude and frequency).

## (C) Decibel Table

The decibel table on the following pages lists most of the current, voltage, and power ratios encountered, with their decibel values. If a db value is not listed and it is desired to find the corresponding ratio, first subtract one of the given values from the unlisted value (select a value so the remainder will also be listed). Then multiply the ratios given in the chart for each value. To convert a ratio which is not given in the table to a db value, first factor the ratio so that each factor will be a listed value; then find the db equivalents for each factor and add them.

Example 1-Find the db equivalent of a power ratio of . 631 .

ANSWER: 2-db loss.

Example 2-Find the current ratio corresponding to a gain of 43 db .

ANSWER: 141. [First find the current ratio for 40 db (100); then find the current ratio for 3 db (1.41). Multiplying, $100 \times 1.41=141$.

Example 3-Find the db value corresponding to a voltage ratio of $\mathbf{1 5 0}$.

ANSWER: 43.5. [First factor 150 into $1.5 \times 100$. The db value for a voltage ratio of 100 is 40 ; the db value for a voltage ratio of 1.5 is 3.5 (approximately). Therefore, the db value for a voltage ratio is $40+3.5$ or 43.5 db.$]$

Table III. Decibel Table (0 to 10.9 Db )

| Db | Current or Voltage Ratio |  | Power Ratio |  | Db | Current or Voltage Ratio |  | Power Ratio |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Gain | Loss | Gain | Loss |  | Gain | Loss | Gain | Loss |
| 0 | 1.000 | 1.0000 | 1.000 | 1.0000 | 5.5 | 1.884 | . 5309 | 3.548 | . 2818 |
| . 1 | 1.012 | . 9886 | 1.023 | . 9772 | 5.6 | 1.905 | . 5248 | 3.631 | . 2754 |
| . 2 | 1.023 | . 9772 | 1.047 | . 9550 | 5.7 | 1.928 | . 5188 | 3.715 | . 2692 |
| . 3 | 1.035 | . 9661 | 1.072 | . 9333 | 5.8 | 1.950 | . 5129 | 3.802 | . 2630 |
| . 4 | 1.047 | . 9550 | 1.096 | . 9120 | 5.9 | 1.972 | . 5070 | 3.890 | . 2570 |
| . 5 | 1.059 | . 9441 | 1.122 | . 8913 | 6.0 | 1.995 | . 5012 | 3.981 | . 2512 |
| . 6 | 1.072 | . 9333 | 1.148 | . 8710 | 6.1 | 2.018 | . 4955 | 4.074 | . 2455 |
| . 7 | 1.084 | . 9226 | 1.175 | . 8511 | 6.2 | 2.042 | . 4898 | 4.169 | . 2399 |
| . 8 | 1.096 | . 9120 | 1.202 | . 8318 | 6.3 | 2.065 | . 4842 | 4.266 | . 2344 |
| . 9 | 1.109 | . 9016 | 1.230 | . 8128 | 6.4 | 2.089 | . 4786 | 4.365 | . 2291 |
| 1.0 | 1.122 | . 8913 | 1.259 | . 7943 | 6.5 | 2.113 | . 4732 | 4.467 | . 2239 |
| 1.1 | 1.135 | . 8810 | 1.288 | . 7762 | 6.6 | 2.138 | . 4677 | 4.571 | . 2188 |
| 1.2 | 1.148 | . 8710 | 1.318 | . 7586 | 6.7 | 2.163 | . 4624 | 4.677 | . 2138 |
| 1.3 | 1.161 | . 8610 | 1.349 | . 7413 | 6.8 | 2.188 | . 4571 | 4.786 | . 2089 |
| 1.4 | 1.175 | .8511 | 1.380 | . 7244 | 6.9 | 2.213 | . 4519 | 4.898 | . 2042 |
| 1.5 | 1.189 | . 8414 | 1.413 | . 7079 | 7.0 | 2.239 | . 4467 | 5.012 | . 1995 |
| 1.6 | 1.202 | . 8318 | 1.445 | . 6918 | 7.1 | 2.265 | . 4416 | 5.129 | . 1950 |
| 1.7 | 1.216 | . 8222 | 1.479 | . 6761 | 7.2 | 2.291 | . 4365 | 5.248 | . 1905 |
| 1.8 | 1.230 | . 8128 | 1.514 | . 6607 | 7.3 | 2.317 | . 4315 | 5.370 | . 1862 |
| 1.9 | 1.245 | . 8035 | 1.549 | . 6457 | 7.4 | 2.344 | . 4266 | 5.495 | . 1820 |
| 2.0 | 1.259 | . 7943 | 1.585 | . 6310 | 7.5 | 2.371 | . 4217 | 5.623 | . 1778 |
| 2.1 | 1.274 | . 7852 | 1.622 | . 6166 | 7.6 | 2.399 | . 4169 | 5.754 | . 1738 |
| 2.2 | 1.288 | . 7762 | 1.660 | . 6026 | 7.7 | 2.427 | . 4121 | 5.888 | . 1698 |
| 2.3 | 1.303 | . 7674 | 1.698 | . 5888 | 7.8 | 2.455 | . 4074 | 6.026 | . 1660 |
| 2.4 | 1.318 | . 7586 | 1.738 | . 5754 | 7.9 | 2.483 | . 4027 | 6.166 | . 1622 |
| 2.5 | 1.334 | . 7499 | 1.778 | . 5623 | 8.0 | 2.512 | . 3981 | 6.310 | . 1585 |
| 2.6 | 1.349 | . 7413 | 1.820 | . 5495 | 8.1 | 2.541 | . 3936 | 6.457 | . 1549 |
| 2.7 | 1.365 | . 7328 | 1.862 | . 5370 | 8.2 | 2.570 | . 3890 | 6.607 | . 1514 |
| 2.8 | 1.380 | . 7244 | 1.905 | . 5248 | 8.3 | 2.600 | . 3846 | 6.761 | . 1479 |
| 2.9 | 1.396 | . 7161 | 1.950 | . 5129 | 8.4 | 2.630 | . 3802 | 6.918 | . 1445 |
| 3.0 | 1.413 | . 7079 | 1.995 | . 5012 | 8.5 | 2.661 | . 3758 | 7.079 | . 1413 |
| 3.1 | 1.429 | . 6998 | 2.042 | . 4898 | 8.6 | 2.692 | . 3715 | 7.244 | . 1380 |
| 3.2 | 1.445 | . 6918 | 2.089 | . 4786 | 8.7 | 2.723 | . 3673 | 7.413 | . 1349 |
| 3.3 | 1.462 | . 6839 | 2.138 | . 4677 | 8.8 | 2.754 | . 3631 | 7.586 | . 1318 |
| 3.4 | 1.479 | . 6761 | 2.188 | . 4571 | 8.9 | 2.786 | . 3589 | 7.762 | . 1288 |
| 3.5 | 1.496 | . 6683 | 2.239 | . 4467 | 9.0 | 2.818 | . 3548 | 7.943 | . 1259 |
| 3.6 | 1.514 | . 6607 | 2.291 | . 4365 | 9.1 | 2.851 | . 3508 | 8.128 | . 1230 |
| 3.7 | 1.531 | . 6531 | 2.344 | . 4266 | 9.2 | 2.884 | . 3467 | 8.318 | . 1202 |
| 3.8 | 1.549 | . 6457 | 2.399 | . 4169 | 9.3 | 2.917 | . 3428 | 8.511 | . 1175 |
| 3.9 | 1.567 | . 6383 | 2.455 | . 4074 | 9.4 | 2.951 | . 3388 | 8.710 | . 1148 |
| 4.0 | 1.585 | . 6310 | 2.512 | . 3981 | 9.5 | 2.985 | . 3350 | 8.913 | . 1122 |
| 4.1 | 1.603 | . 6237 | 2.570 | . 3890 | 9.6 | 3.020 | . 3311 | 9.120 | . 1096 |
| 4.2 | 1.622 | . 6166 | 2.630 | . 3802 | 9.7 | 3.055 | . 3273 | 9.333 | . 1072 |
| 4.3 | 1.641 | . 6095 | 2.692 | . 3715 | 9.8 | 3.090 | . 3236 | 9.550 | . 1047 |
| 4.4 | 1.660 | . 6026 | 2.754 | . 3631 | 9.9 | 3.126 | . 3199 | 9.772 | . 1023 |
| 4.5 | 1.679 | . 5957 | 2.818 | . 3548 | 10.0 | 3.162 | . 3162 | 10.000 | . 1000 |
| 4.6 | 1.698 | . 5888 | 2.884 | . 3467 | 10.1 | 3.199 | . 3126 | 10.23 | . 09772 |
| 4.7 | 1.718 | . 5821 | 2.951 | . 3388 | 10.2 | 3.236 | . 3090 | 10.47 | . 09550 |
| 4.8 | 1.738 | . 5754 | 3.020 | . 3311 | 10.3 | 3.273 | . 3055 | 10.72 | . 09333 |
| 4.9 | 1.758 | . 5689 | 3.090 | . 3236 | 10.4 | 3.311 | . 3020 | 10.96 | . 09120 |
| 5.0 | 1.778 | . 5623 | 3.162 | . 3162 | 10.5 | 3.350 | . 2985 | 11.22 | . 08913 |
| 5.1 | 1.799 | . 5559 | 3.236 | . 3090 | 10.6 | 3.388 | . $2951{ }^{\circ}$ | 11.48 | . 08710 |
| 5.2 | 1.820 | . 5495 | 3.311 | . 3020 | 10.7 | 3.428 | . 2917 | 11.75 | . 08511 |
| 5.3 | 1.841 | . 5433 | 3.388 | . 2951 | 10.8 | 3.467 | . 2884 | 12.02 | . 08318 |
| 5.4 | 1.862 | . 5370 | 3.467 | . 2884 | 10.9 | 3.508 | . 2851 | 12.30 | . 08128 |

Table III. Decibel Table-(Cont'd) (11.0 to 19.9 Db )

| Db | Current or Voltage Ratio |  | Power Ratio |  | Db | Current or Voltage Ratio |  | Power Ratio |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Gain | Loss | Gain | Loss |  | Gain | Loss | Gain | Loss |
| 11.0 | 3.548 | . 2818 | 12.59 | . 07943 | 15.5 | 5.957 | . 1679 | 35.48 | . 02818 |
| 11.1 | 3.589 | . 2786 | 12.88 | . 07762 | 15.6 | 6.026 | . 1660 | 36.31 | . 02754 |
| 11.2 | 3.631 | . 2754 | 13.18 | . 07586 | 15.7 | 6.095 | . 1641 | 37.15 | . 02692 |
| 11.3 | 3.673 | . 2723 | 13.49 | . 07413 | 15.8 | 6.166 | . 1622 | 38.02 | . 02630 |
| 11.4 | 3.715 | . 2692 | 13.80 | . 07244 | 15.9 | 6.237 | . 1603 | 38.90 | . 02570 |
| 11.5 | 3.758 | . 2661 | 14.13 | . 07079 | 16.0 | 6.310 | . 1585 | 39.81 | . 02512 |
| 11.6 | 3.802 | . 2630 | 14.45 | . 06918 | 16.1 | 6.383 | . 1567 | 40.74 | . 02455 |
| 11.7 | 3.846 | . 2600 | 14.79 | . 06761 | 16.2 | 6.457 | . 1549 | 41.69 | . 02399 |
| 11.8 | 3.890 | . 2570 | 15.14 | . 06607 | 16.3 | 6.531 | . 1531 | 42.66 | . 02344 |
| 11.9 | 3.936 | . 2541 | 15.49 | . 06457 | 16.4 | 6.607 | . 1514 | 43.65 | . 02291 |
| 12.0 | 3.981 | . 2512 | 15.85 | . 06310 | 16.5 | 6.683 | . 1496 | 44.67 | . 02239 |
| 12.1 | 4.027 | . 2483 | 16.22 | . 06166 | 16.6 | 6.761 | . 1479 | 45.71 | . 02188 |
| 12.2 | 4.074 | . 2455 | 16.60 | . 06026 | 16.7 | 6.839 | . 1462 | 46.77 | . 02138 |
| 12.3 | 4.121 | . 2427 | 16.98 | . 05888 | 16.8 | 6.918 | . 1445 | 47.86 | . 02089 |
| 12.4 | 4.169 | . 2399 | 17.38 | . 05754 | 16.9 | 6.998 | . 1429 | 48.98 | . 02042 |
| 12.5 | 4.217 | . 2371 | 17.78 | . 05623 | 17.0 | 7.079 | . 1413 | 50.12 | . 01995 |
| 12.6 | 4.266 | . 2344 | 18.20 | . 05495 | 17.1 | 7.161 | . 1396 | 51.29 | . 01950 |
| 12.7 | 4.315 | . 2317 | 18.62 | . 05370 | 17.2 | 7.244 | . 1380 | 52.48 | . 01905 |
| 12.8 | 4.365 | . 2291 | 19.05 | . 05248 | 17.3 | 7.328 | . 1365 | 53.70 | . 01862 |
| 12.9 | 4.416 | . 2265 | 19.50 | . 05129 | 17.4 | 7.413 | . 1349 | 54.95 | . 01820 |
| 13.0 | 4.467 | . 2239 | 19.95 | . 05012 | 17.5 | 7.499 | . 1334 | 56.23 | . 01778 |
| 13.1 | 4.519 | . 2213 | 20.42 | . 04898 | 17.6 | 7.586 | . 1318 | 57.54 | . 01738 |
| 13.2 | 4.571 | . 2188 | 20.89 | . 04786 | 17.7 | 7.674 | . 1303 | 58.88 | . 01698 |
| 13.3 | 4.624 | . 2163 | 21.38 | . 04677 | 17.8 | 7.762 | . 1288 | 60.26 | . 01660 |
| 13.4 | 4.677 | . 2138 | 21.88 | . 04571 | 17.9 | 7.852 | . 1274 | 61.66 | . 01622 |
| 13.5 | 4.732 | . 2113 | 22.39 | . 04467 | 18.0 | 7.943 | . 1259 | 63.10 | . 01585 |
| 13.6 | 4.786 | . 2089 | 22.91 | . 04365 | 18.1 | 8.035 | . 1245 | 64.57 | . 01549 |
| 13.7 | 4.842 | . 2065 | 23.44 | . 04266 | 18.2 | 8.128 | . 1230 | 66.07 | . 01514 |
| 13.8 | 4.898 | . 2042 | 23.99 | . 04169 | 18.3 | 8.222 | . 1216 | 67.61 | . 01479 |
| 13.9 | 4.955 | . 2018 | 24.55 | . 04074 | 18.4 | 8.318 | . 1202 | 69.18 | . 01445 |
| 14.0 | 5.012 | . 1995 | 25.12 | . 03981 | 18.5 | 8.414 | . 1189 | 70.79 | . 01413 |
| 14.1 | 5.070 | . 1972 | 25.70 | . 03890 | 18.6 | 8.511 | . 1175 | 72.44 | . 01380 |
| 14.2 | 5.129 | . 1950 | 26.30 | . 03802 | 18.7 | 8.610 | . 1161 | 74.13 | . 01349 |
| 14.3 | 5.188 | . 1928 | 26.92 | . 03715 | 18.8 | 8.710 | . 1148 | 75.86 | . 01318 |
| 14.4 | 5.248 | . 1905 | 27.54 | . 03631 | 18.9 | 8.811 | . 1135 | 77.62 | . 01288 |
| 14.5 | 5.309 | . 1884 | 28.18 | . 03548 | 19.0 | 8.913 | . 1122 | 79.43 | . 01259 |
| 14.6 | 5.370 | . 1862 | 28.84 | . 03467 | 19.1 | 9.016 | . 1109 | 81.28 | . 01230 |
| 14.7 | 5.433 | . 1841 | 29.51 | . 03388 | 19.2 | 9.120 | . 1096 | 83.18 | . 01202 |
| 14.8 | 5.495 | . 1820 | 30.20 | . 03311 | 19.3 | 9.226 | . 1084 | 85.11 | . 01175 |
| 14.9 | 5.559 | . 1799 | 30.90 | . 03236 | 19.4 | 9.333 | . 1072 | 87.10 | . 01148 |
| 15.0 | 5.623 | . 1778 | 31.62 | . 03162 | 19.5 | 9.441 | . 1059 | 89.13 | . 01122 |
| 15.1 | 5.689 | . 1758 | 32.36 | . 03090 | 19.6 | 9.550 | . 1047 | 91.20 | . 01096 |
| 15.2 | 5.754 | . 1738 | 33.11 | . 03020 | 19.7 | 9.661 | . 1035 | 93.33 | . 01072 |
| 15.3 | 5.821 | . 1718 | 33.88 | . 02951 | 19.8 | 9.772 | . 1023 | 95.50 | . 01047 |
| 15.4 | 5.888 | . 1698 | 34.67 | . 02884 | 19.9 | 9.886 | . 1012 | 97.72 | . 01023 |

Note: For values from 20 to 180 db , see next page.

Table III. Decibel Table-(Cont'd) ( 20 to 180 Db )

| Db | Current or Voltage Ratio |  | Power Ratio |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Gain | Loss | Gain | Loss |
| 20.0 | 10.00 | 0.1000 | 100.00 | 0.01000 |
| 25.0 | 17.78 | 0.0562 | $3.162 \times 10^{2}$ | $3.162 \times 10^{-31}$ |
| 30.0 | 31.62 | 0.0316 | $10^{\text {a }}$ | $10^{-3}$ |
| 35.0 | 56.23 | 0.0178 | $3.162 \times 10^{3}$ | $3.162 \times 10^{-4}$ |
| 40.0 | 100.00 | 0.0100 | $10^{4}$ | $10^{-4}$ |
| 45.0 | 177.8 | 0.0056 | $3.162 \times 10^{4}$ | $3.162 \times 10^{-5}$ |
| 50.0 | 316.2 | 0.0032 | $10^{5}$ | $10^{-5}$ |
| 55.0 | 562.3 | 0.0018 | $3.162 \times 10^{5}$ | $3.162 \times 10^{-6}$ |
| 60.0 | $10^{3}$ | $10^{-3}$ | $10^{11}$ | $10^{-6}$ |
| 65.0 | $1.778 \times 10^{3}$ | $5.623 \times 10^{-4}$ | $3.162 \times 10^{6}$ | $3.162 \times 10^{-7}$ |
| 70.0 | $3.162 \times 10^{8}$ | $3.162 \times 10^{-4}$ | $10^{7}$ | $10^{-7}$ |
| 75.0 | $5.623 \times 10^{9}$ | $1.78 \times 10^{-4}$ | $3.162 \times 10^{7}$ | $3.162 \times 10^{-8}$ |
| 80.0 | $10^{4}$ | $10^{-4}$ | $10^{6}$ | $10^{-8}$ |
| 85.0 | $1.778 \times 10^{4}$ | $5.623 \times 10^{-5}$ | $3.162 \times 10^{8}$ | $3.162 \times 10^{-9}$ |
| 90.0 | $3.162 \times 10^{4}$ | $3.162 \times 10^{-5}$ | $10^{\circ}$ | $10^{-9}$ |
| 95.0 | $5.632 \times 10^{4}$ | $1.78 \times 10^{-5}$ | $3.162 \times 10^{18}$ | $3.162 \times 10^{-10}$ |
| 100.0 | $10^{5}$ | $10^{-5}$ | $10^{10}$ | $10^{-10}$ |
| 110.0 | $3.162 \times 10^{5}$ | $3.162 \times 10^{-6}$ | $10^{11}$ | $10^{-11}$ |
| 120.0 | $10^{8}$ | $10^{-6}$ | $10^{12}$ | $10^{-12}$ |
| 130.0 | $3.162 \times 10^{8}$ | $3.162 \times 10^{-7}$ | $10^{13}$ | $10^{-13}$ |
| 140.0 | $10^{7}$ | $10^{-7}$ | $10^{14}$ | $10^{-14}$ |
| 150.0 | $3.162 \times 10^{7}$ | $3.162 \times 10^{-8}$ | $10^{15}$ | $10^{-15}$ |
| 160.0 | $10^{8}$ | $10^{-8}$ | $10^{16}$ | $10^{-16}$ |
| 170.0 | $3.162 \times 10^{8}$ | $3.162 \times 10^{-9}$ | $10^{17}$ | $10^{-17}$ |
| 180.0 | $10^{9}$ | $10^{-9}$ | $10^{18}$ | $10^{-18}$ |

## Constants and Standards

## 27. DIELECTRIC CONSTANTS OF MATERIALS

The dielectric constants of most materials vary for different temperatures and frequencies. Likewise, small differences in the composition of materials will cause differences in the dielectric constants. A list of materials, and the approximate range (where available) of their dielectric constants, are given in Table IV. The values shown are accurate enough for most applications. The dielectric constants of some materials (such as quartz, Styrofoam, and Teflon) do not change appreciably with frequency.

Table IV. Dielectric Constants of Materials

| Material | Dielectric <br> Constant <br> (Approx.) | Material | Dielectric <br> Constant <br> (Approx.) |
| :--- | :---: | :--- | :---: |
| Air | 1.0 | Nylon | $3.4-22.4$ |
| Amber | $2.6-2.7$ | Paper (dry) | $1.5-3.0$ |
| Bakelite (asbestos base) | $5.0-22$ | Paper (paraffin coated) | $2.5-4.0$ |
| Bakelite (mica filled) | $4.5-4.8$ | Paraffin (solid) | $2.0-3.0$ |
| Beeswax | $2.4-2.8$ | Plexiglass | $2.6-3.5$ |
| Cambric (varnished) | 4.0 | Polyethylene | 2.3 |
| Celluloid | 4.0 | Polystyrene | $2.4-3.0$ |
| Cellulose Acetate | $3.1-4.5$ | Porcelain (dry process) | $5.0-5.5$ |
| Durite | $4.7-5.1$ | Porcelain (wet process) | $5.8-6.5$ |
| Ebonite | 2.7 | Quartz | 5.0 |
| Fiber | 5.0 | Quartz (fused) | 3.78 |
| Formica | $3.6-6.0$ | Rubber (hard) | $2.0-4.0$ |
| Glass (electrical) | $3.8-14.5$ | Ruby Mica | 5.4 |
| Glass (photographic) | 7.5 | Shellac (natural) | $2.9-3.9$ |
| Glass (Pyrex) | $4.6-5.0$ | Silicone (glass) (molding) | $3.2-4.7$ |
| Glass (window) | 7.6 | Silicone (glass) (laminate) | $3.7-4.3$ |
| Gutta Percha | $2.4-2.6$ | Slate | 7.0 |
| Isolantite | 6.1 | Steatite (ceramic) | $5.2-6.3$ |
| Lucite | 2.5 | Steatite (low loss) | 4.4 |
| Mica (electrical) | $4.0-9.0$ | Styrofoam | 1.03 |
| Mica (clear India) | 7.5 | Teflon | 2.1 |
| Mica (filled phenolic) | $4.2-5.2$ | Vaseline | 2.16 |
| Micarta | $3.2-5.5$ | Vinylite | $2.7-7.5$ |
| Mycalex | $7.3-9.3$ | Water (distilled) | $34-78$ |
| Neoprene | $4.0-6.7$ | Wood (dry) | $1.4-2.9$ |

## 28. CONVERSION FACTORS

The following table lists the multiplying factors necessary to convert from one unit of measure to another, and vice versa. To use the table, locate the unit of measure you are converting from or the one you are converting to in the first column. Opposite this listing are the multiplying factors for converting either unit of measure to the other unit of measure.

Table V. Conversion Factors

| To Convert | Into | Multiply by | Conversely, Multiply by |
| :---: | :---: | :---: | :---: |
| Acres | Square feet | $4.356 \times 10^{4}$ | $2.296 \times 10^{-6}$ |
| Acres | Square meters | 4047 | $2.471 \times 10^{-4}$ |
| Acres | Square miles | $1.5625 \times 10^{-3}$ | 640 |
| Amperes | Microamperes | $10^{4}$ | $10^{-6}$ |
| Amperes | Micromicroamperes | $10^{12}$ | $10^{-12}$ |
| Amperes | Milliamperes | $10^{3}$ | $10^{-3}$ |
| Ampere-hours | Coulombs | 3600 | $2.778 \times 10^{-4}$ |
| Ampere-turns | Gilberts | 1.257 | 0.7958 |
| Ampere-turns per cm. | Ampere-furns per in. | 2.54 | 0.39 |
| Angstrom units | Inches | $3.937 \times 10^{-8}$ | $2.54 \times 10^{4}$ |
| Angstrom units | Meters | $10^{-10}$ | $10^{10}$ |
| Bars | Atmospheres | $9.870 \times 10^{-8}$ | 1.0133 |
| Bars | Dynes per sq. cm. |  | $10^{-4}$ |
| Bars | Pounds per sq. in. | 14.504 | $8947 \times$ |
| Bru | Ergs | $1.0548 \times 10^{10}$ | $9.486 \times 10^{-11}$ |
| Btu | Foot-pounds | 778.3 | $1.285 \times$ |
| Bru | Joules | 1054.8 | $9.480 \times 10^{-4}$ |
| Bru | Kilogram-calories | 0.252 | 3.969 |
| Btu per hour | Horsepower-hours | $3.929 \times 10$ | 2545 |
| Bushels | Cubic feet | 1.2445 | 0.8036 |
| Calories, gram | Joules | 4.185 | 0.2389 |
| Centigrade | Celsius |  | $\left.{ }^{1} \mathrm{~F}-32\right)$ |
| Centigrade | Fahrenheit | $\begin{array}{r} \left({ }^{\circ} \mathrm{C} \times 9 / 5\right) \\ +32={ }^{\circ} \mathrm{F} \end{array}$ | $\left.{ }^{\circ} \mathrm{F}-32\right)$ |
| Centigrade | Kelvin | ${ }^{\circ} \mathrm{C}+273.1={ }^{\circ} \mathrm{K}$ | ${ }^{\circ} \mathrm{K}-273.1{ }^{\circ} \mathrm{C}$ |
| Chains (surveyor's) | Feet | 66 | $1.515 \times 10^{-2}$ |
| Circular mils | Square centimeters | $5.067 \times 10^{-6}$ | $1.973 \times 10^{-3}$ |
| Circular mils | Square mils | 0.7854 | 1.273 |
| Cubic feet | Gallons (liq. U.S.) | 7.481 | $0.1337 \times 1{ }^{-2}$ |
| Cubic feet | Liters | 28.32 | $3.531 \times 10^{-2}$ |
| Cubic inches | Cubic centimeters | 16.39 | $6.102 \times 10^{-2}$ |
| Cubic inches | Cubic feet | $5.787 \times 10^{-4}$ | $1728 \times 10^{4}$ |
| Cubic inches | Cubic meters | $1.639 \times 10^{-5}$ | $6.102 \times 10^{4}$ |
| Cubic inches | Gallons (lia. U.S.) | $4.329 \times 10^{-3}$ 35.31 | 231 $2.832 \times 10^{-2}$ |
| Cubic meters | Cubic feet | 35.31 1.308 | $2.832 \times 10$ 0.7646 |
| Cubic meters | Cubic yards | 1.308 | $10^{3}$ |
| Cycles Cycles | Kilocycles Megacycles | $10^{-8}$ | $10^{\prime \prime}$ |

## Table V. Conversion Factors--(Cont'd)

| To Convert | Into | Multiply by | Conversely, Multiply by |
| :---: | :---: | :---: | :---: |
| Degrees (angle) | Mils | 17.45 | $5.73 \times 10^{-2}$ |
| Degrees (angle) | Radians | $1.745 \times 10^{-2}$ | 57.3 |
| Dynes | Pounds | $2.248 \times 10^{-5}$ | $4.448 \times 10^{5}$ |
| Ergs | Foot-pounds | $7.376 \times 10^{-8}$ | $1.356 \times 10^{7}$ |
| Fahrenheit | Rankine | ${ }^{\circ} \mathrm{F}+459.58={ }^{\circ} \mathrm{R}$ | ${ }^{\circ} \mathrm{R}-459.58={ }^{\circ} \mathrm{F}$ |
| Faradays | Ampere-hours | 26.8 | $3.731 \times 10^{-2}$ |
| Farads | Mierofarads | $10^{8}$ | $10^{-6}$ |
| Farads | Micromicrofarads | $10^{13}$ | $10^{-12}$ |
| Farads | Millifarads | $10^{3}$ | $10^{-3}$ |
| Fathoms | Feet | 6 | 0.16667 |
| Feet | Centimeters | 30.48 | $3.281 \times 10^{-2}$ |
| Feet | Meters | 0.3048 | 3.281 |
| Feet | Mils | $1.2 \times 10^{4}$ | $8.333 \times 10^{-5}$ |
| Foot-pounds | Gram-centimeters | $1.383 \times 10^{4}$ | $1.235 \times 10^{-5}$ |
| Foor-pounds | Horsepower-hours | $5.05 \times 10^{-7}$ | $1.98 \times 10^{8}$ |
| Foot-pounds | Kilogram-meters | 0.1383 | 7.233 |
| Foot-pounds | Kilowatt-hours | $3.766 \times 10^{-7}$ | $2.655 \times 10^{3}$ |
| Foot-pounds | Ounce-inches | 192 | $5.208 \times 10^{-3}$ |
| Gallons (liq. U.S.) | Cubic meters | $3.785 \times 10^{-3}$ | 264.2 |
| Gallons (liq. U.S.) | Gallons (liq. Br. Imp.) | 0.8327 | 1.201 |
| Gausses | Lines per sq. cm. | 1.0 | 1.0 |
| Gausses | Lines per sq. in. | 6.452 | 0.155 |
| Gausses | Webers per sq. in. | $6.452 \times 10^{-4}$ | $1.55 \times 10^{7}$ |
| Grams | Dynes | 980.7 | $1.02 \times 10^{-3}$ |
| Grams | Grains | 15.43 | $6.481 \times 10^{-2}$ |
| Grams | Ounces (avdp.) | $3.527 \times 10^{-2}$ | 28.35 |
| Grams | Poundals | $7.093 \times 10^{-2}$ | 14.1 |
| Grams per cm. | Pounds per in. | $5.6 \times 10^{-3}$ | 178.6 |
| Grams per cu. cm. | Pounds per cu. in. | $3.613 \times 10^{-2}$ | 27.68 |
| Henries | Microhenries | $10^{6}$ | $10^{-8}$ |
| Henries | Millihenries | $10^{3}$ | $10^{-3}$ |
| Horsepower | Biu per minute | 42.418 | $2.357 \times 10^{-2}$ |
| Horsepower | Foot-lbs. per minute | $3.3 \times 10^{4}$ | $3.03 \times 10^{-5}$ |
| Horsepower | Foot-lbs. per second | 550 | $1.182 \times 10^{-3}$ |
| Horsepower | Horsepower (metric) | 1.014 | 0.9863 |
| Horsepower | Kilowatts | 0.746 | 1.341 |
| Inches | Centimeters | 2.54 | 0.3937 |
| inches | Feet | $8.333 \times 10^{-2}$ |  |
| Inches | Meters | $2.54 \times 10^{-2}$ | 39.37 |
| Inches | Miles | $1.578 \times 10^{-5}$ | $6.336 \times 10^{4}$ |
| Inches | Mils |  | $10^{-3}$ |
| Inches | Yards | $2.778 \times 10^{-2}$ | 36 |
| Joules | Foot-pounds | 0.7376 | 1.356 |
| Joules | Ergs | $10^{7}$ | $10^{-7}$ |
| Joules | Watt-hours | $2.778 \times 10^{-4}$ | 3600 |
| Kilograms | Tonnes | $10^{3}$ |  |
| Kilograms | Tons (long) | $9.842 \times 10^{-4}$ | 1016 |
| Kilograms | Tons (short) | $1.102 \times 10^{-3}$ | 907.2 |
| Kilograms | Pounds (avdp.) | 2.205 | 0.4536 |
| Kilograms per sq. meter | Pounds per sq. feet | 0.2048 | 4.882 |

Table V. Conversion Factors-(Cont'd)

| To Çonvert | Into | Multiply by | Conversely, Multiply by |
| :---: | :---: | :---: | :---: |
| Kilometers | Feet | 3281 | $3.408 \times 10^{-4}$ |
| Kilometers | Inches | $3.937 \times 10^{4}$ | $2.54 \times 10^{-5}$ |
| Kilometers | Light years | $1.0567 \times 10^{-13}$ | $9.4637 \times 10^{12}$ |
| Kilometers per hr. | Feet per minute | 54.68 | $1.829 \times 10^{-2}$ |
| Kilometers per hr. | Knots | 0.5396 | 1.8532 |
| Kilowatt-hours | Btu | 3413 | $2.93 \times 10^{-4}$ |
| Kilowatt-hours | Foot-pounds | $2.655 \times 10^{6}$ | $3.766 \times 10^{-7}$ |
| Kilowatt-hours | Joules | $3.6 \times 10^{61}$ | $2.778 \times 10^{-7}$ |
| Kilowatt-hours | Horsepower-hours | 1.341 | 0.7457 |
| Kilowatt-hours | Pounds water evaporated from and at $212^{\circ} \mathrm{F}$. | 3.53 | 0.284 |
| Kilowatt-hours | Watt-hours | $10^{3}$ | $10^{-3}$ |
| Knots | Feet per second | 1.688 | 0.5925 |
| Knots | Meters per minute | 30.87 | 0.0324 |
| Knots | Miles per hour | 1.1508 | 0.869 |
| Lamberts | Candles per sq. cm. | 0.3183 | 3.142 |
| Lamberts | Candles per sq. in. | 2.054 | 0.4869 |
| Leagues | Miles | 3 | 0.33 |
| Links | Chains | 0.01 | 100 |
| Links (surveyor's) | Inches | 7.92 | 0.1263 |
| Liters | Bushels (dry U.S.) | $2.838 \times 10^{-2}$ | 35.24 |
| Liters | Cubic enntimeters | $10^{3}$ | $10^{-3}$ |
| Liters | Cubic meters | $10^{-3}$ | $10^{3}$ |
| Liters | Cubic inches | 61.02 | $1.639 \times 10^{-2}$ |
| Liters | Gallons (liq. U.S.) | 0.2642 | 3.785 |
| Liters | Pints (liq. U.S.) | 2.113 | 0.4732 |
| $\log _{\epsilon} N$ | $\log _{10} \mathrm{~N}$ | 0.4343 | 2.303 |
| Lumens per sq. ft . | Foot-candles | 1 | 1 |
| Lux | Foot-candles | 0.0929 | 10.764 |
| Maxwells | Kilolines | $10^{-3}$ | $10^{3}$ |
| Maxwells | Megalines | $10^{-6}$ | $10^{\text {s }}$ |
| Maxwells | Webers | $10^{-8}$ | $10^{8}$ |
| Meters | Centimeters | $10^{2}$ | $10^{-2}$ |
| Meters | Feet | 3.28 | $30.48 \times 10^{-2}$ |
| Meters | Inches | 39.37 | $2.54 \times 10^{-2}$ |
| Meters | Kilometers | $10^{-3}$ | $10^{3}$ |
| Meters | Miles | $6.214 \times 10^{-4}$ | 1609.35 |
| Meters | Yards | 1.094 | 0.9144 |
| Meters per minute | Feet per minute | 3.281 | 0.3048 |
| Meters per minute | Kilometers per hour | 0.06 | 16.67 |
| Mhos | Micromhos | $10^{63}$ | $10^{-6}$ |
| Mhos | Millimhos | $10^{3}$ | $10^{-3}$ |
| Microfarads | Micromicrofarads | $10^{\prime \prime}$ | $10^{-n}$ |
| Miles (nautical) | Feet | 6076.1 | $1.646 \times 10^{-4}$ |
| Miles (nautical) | Meters | 1852 | $5.4 \times 10^{-4}$ |
| Miles (statute) | Feet | 5280 | $1.894 \times 10^{-4}$ |
| Miles (statute) | Kilometers | 1.609 | 0.6214 |
| Miles (statute) | Light years | $1.691 \times 10^{-13}$ | $5.88 \times 10^{12}$ |
| Miles (statute) | Miles (nautical) | 0.869 | 1.1508 |

Table V. Conversion Factors-(Cont'd)

| To Convert | Into | Multiply by | Conversely, Multiply by |
| :---: | :---: | :---: | :---: |
| Miles (statute) | Yards | 1760 | $5.6818 \times 10^{-4}$ |
| Miles per hour | Feet per minute | 88 | $1.136 \times 10^{-2}$ |
| Miles per hour | Feet per second | 1.467 | 0.6818 |
| Miles per hour | Kilometers per hour | 1.609 | 0.6214 |
| Miles per hour | Knots | 0.8684 | 1.152 |
| Milliamperes | Microamperes | $10^{3}$ | $10^{-3}$ |
| Millihenries | Microhenries | $10^{3}$ | $10^{-3}$ |
| Millimeters | Centimeters | 0.1 | 10 |
| Millimeters | Inches | $3.937 \times 10^{-2}$ | 25.4 |
| Millimeters | Microns | $10^{3}$ | $10^{-3}$ |
| Millivolts | Microvolts | $10^{3}$ | $10^{-3}$ |
| Mils | Minutes | 3.438 | 0.2909 |
| Minutes (angle) | Degrees | $1.666 \times 10^{-2}$ | 60 |
| Nepers | Decibels | 8.686 | 0.1151 |
| Newtons | Dynes | $10^{5}$ | $10^{-5}$ |
| Newtons | Pounds (avdp.) | 0.2248 | 4.448 |
| Ohms | Milliohms | $10^{3}$ | $10^{-3}$ |
| Ohms | Micro-ohms | $10^{6}$ | $10^{-9}$ |
| Ohms | Micromicro-ohms | $10^{12}$ | $10^{-12}$ |
| Ohms | Megohms | $10^{-6}$ | $10^{\circ}$ |
| Ohms | Ohms(International) | 0.99948 | 1.00052 |
| Ohms per foot | Ohms per meter | 0.3048 | 3.281 |
| Ounces (fluid) | Quarts | $3.125 \times 10^{-2}$ | 32 |
| Ounces (avdp.) | Pounds | $6.25 \times 10^{-2}$ | 16 |
| Picofarad | Micromicrofarad | 1 | 1 |
| Pints | Quarts (liq. U.S.) | 0.50 | 2 |
| Pounds (force) | Newtons | 4.4482 | 0.2288 |
| Pounds carbon oxidized | Btu | 14,544 | $6.88 \times 10^{-5}$ |
| Pounds carbon oxidized | Horsepower-hours | 5.705 | 0.175 |
| Pounds carbon oxidized | Kilowatt-hours | 4.254 | 0.235 |
| Pounds of water (dist.) | Cubic feet | $1.603 \times 10^{-2}$ | 62.38 |
| Pounds of water (dist.) | Gallons | 0.1198 | 8.347 |
| Pounds per sq. in. | Dynes per sq. cm. | $6.8946 \times 10^{4}$ | $1.450 \times 10^{-5}$ |
| Poundals | Dynes | $1.383 \times 10^{4}$ | $7.233 \times 10^{-5}$ |
| Poundals | Pounds (avdp.) | $3.108 \times 10^{-2}$ | 32.17 |
| Quadrants | Degrees | 90 | $11.111 \times 10^{-2}$ |
| Quadrants | Radians | 1.5708 | 0.637 |
| Radians | Mils | $10^{3}$ | $10^{-3}$ |
| Radians | Minutes | $3.438 \times 10^{3}$ | $2.909 \times 10^{-4}$ |
| Radians | Seconds | $2.06265 \times 10^{5}$ | $4.848 \times 10^{-8}$ |
| Rods | Feet | 16.5 | $6.061 \times 10^{-2}$ |
| Rods | Miles | $3.125 \times 10^{-3}$ | 320 |
| Rods | Yards | 5.5 | 0.1818 |
| Rpm | Degrees per second | 6.0 | 0.1667 |
| Rpm | Radians per second | 0.1047 | 9.549 |

## Table V. Conversion Factors-(Cont'd)

| To Convert | Into | Multiply by | Conversely, Multiply by |
| :---: | :---: | :---: | :---: |
| Rpm | Rps | $1.667 \times 10^{-2}$ | 60 |
| Square feet | Acres | $2.296 \times 10^{-5}$ | 43.560 |
| Square feet | Square centimeters | 929.034 | $1.076 \times 10^{-3}$ |
| Square feet | Square inches | $144 \times 10^{-2}$ | $6.944 \times 10^{-3}$ |
| Square feet | Square meters | $9.29 \times 10^{-2}$ | 10.764 |
| Square feet | Square miles | $3.587 \times 10^{-8}$ | $27.88 \times 10^{8}$ |
| Square feet | Square yards | $11.11 \times 10^{-2}$ | 9 |
| Square inches | Circular mils | $1.273 \times 10^{n}$ | $7.854 \times 10^{-7}$ |
| Square inches | Square centimeters | 6.452 | 0.155 |
| Square inches | Square mils | $10^{8}$ | $10^{-6}$ |
| Square inches | Square millimeters | 645.2 | $1.55 \times 10^{-3}$ |
| Square kilometers | Square miles | 0.3861 | 2.59 |
| Square meters | Square yards | 1.196 | 0.8361 |
| Square miles | Acres | 640 | $1.562 \times 10^{-3}$ |
| Square miles | Square yards | $3.098 \times 10^{6}$ | $3.228 \times 10^{-7}$ |
| Square millimeters | Circular mils | 1973 | $5.067 \times 10^{-4}$ |
| Square millimeters | Square centimeters | . 01 | 100 |
| Square mils | Circular mils | 1.273 | 0.7854 |
| Tons (long) | Pounds (avdp.) | 2240 | $4.464 \times 10^{-4}$ |
| Tons (short) | Pounds | 2,000 | $5 \times 10^{-4}$ |
| Tonnes | Pounds | 2204.63 | $4.536 \times 10^{-4}$ |
| Varas | Feet | 2.7777 | 0.36 |
| Volts | Kilovolts | $10^{-3}$ | $10^{3}$ |
| Volts | Microvolts | $10^{6}$ | $10^{-16}$ |
| Volts | Millivolts | $10^{3}$ | $10^{-3}$ |
| Watts | Biu per hour | 3.413 | 0.293 |
| Watts | Btu per minute | $5.689 \times 10^{-2}$ | 17.58 |
| Watts | Ergs per second | $10^{7}$ |  |
| Watts | Foot-lbs per minute | 44.26 | $2.26 \times 10^{-2}$ |
| Watts | Foot-lbs per second | 0.7378 | 1.356 |
| Watts | Horsepower | $1.341 \times 10^{-3}$ | 746 |
| Watts | Kilogram-calories per minute | $1.433 \times 10^{-2}$ | 69.77 |
| Watts | Kilowatts | $10^{-3}$ | $10^{3}$ |
| Watts | Microwatts | $10^{8}$ | $10^{-6}$ |
| Watts | Milliwatts | $10^{3}$ | $10^{-3}$ |
| Watt-seconds | Joules | 1 |  |
| Webers | Maxwells | $10^{\mu}$ | $10^{-8}$ |
| Webers per sq. meter | Gausses | $10^{4}$ | $10^{-4}$ |
| Yards | Feet | 3 | . 3333 |
| Yards | Varas | 1.08 | 0.9259 |

## 29. METRIC PREFIXES

## (A) Unit Prefixes

The metric system, whereby a different prefix is assigned for each order of magnitude, is particularly suited for electronic values. In 1958 the International Committee on Weights and Measures assigned prefixes for the ninth and twelfth orders of magnitude (both positive and negative). (See Table VI.) This system eliminates the cumbersome double prefixes (micromicro-," "kilomega-," etc. In 1959 the National Bureau of Standards began using these terms; however, acceptance by industry in the United States has been slow, particularly in using the newer term "picofarad" instead of "micromicrofarad."

Table VI. Metric Prefixes

| Multiple | Prefix | Abbreviation | Multiple | Prefix | Abbreviation |
| :---: | :--- | :---: | :---: | :---: | :---: |
| $10^{12}$ | tera- | T | $10^{-1}$ | deci- | d |
| $10^{\mathrm{Q}}$ | giga- | G | $10^{-2}$ | centi- | c |
| $10^{\mathrm{B}}$ | mega- | M | $10^{-3}$ | milli- | m |
| $10^{4}$ | myria- | My | $10^{-n}$ | micro- | $\mu$ |
| $10^{3}$ | kilo- | K | $10^{-11}$ | nano- | n |
| $10^{2}$ | hecto- | H | $10^{-12}$ | pico- | p |
| 10 | deka- | D |  |  |  |

## (B) Conversion Table

Table VII gives the number of places, and the direction, the decimal point must be moved to convert from one metric notation to another. The value labeled "units" is the basic unit of measurement-e.g., ohms, farads, etc. To use the chart, find the desired value in the left-hand column; then follow the horizontal line across to the column with the prefix in which the original value is stated. The number and arrow at this point indicate the number of places and the direction the decimal point must be moved to change the original value to the desired value.

Table VII. Metric Conversion Table

| Desired Value | Original Value |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Tera- | Giga- | Mega- | Myria- | Kilo- | Hecto- | Deka- | Units | Deci- | Centi- | Milli- | Micro- | Nano- | Pico- |
| Tera- |  | $\leftarrow 3$ | $\leftarrow 6$ | $\leftarrow 8$ | $\leftarrow 9$ | $\leftarrow 10$ | $\leftarrow 11$ | $\leftarrow 12$ | $\leftarrow 13$ | $\leftarrow 14$ | $\leftarrow 15$ | $\leftarrow 18$ | $\longleftarrow 21$ | $\longleftarrow 24$ |
| Giga- | $3 \rightarrow$ |  | $\leftarrow 3$ | $\leftarrow 5$ | $\leftarrow 6$ | $\leftarrow 7$ | $\leftarrow 8$ | $\leftarrow 9$ | $\leftarrow 10$ | $\leftarrow 11$ | $\leftarrow 12$ | $\leftarrow 15$ | $\leftarrow 18$ | $\leftarrow 21$ |
| Mega- | $6 \rightarrow$ | $3 \rightarrow$ |  | $\leftarrow 2$ | $\leftarrow 3$ | $\leftarrow 4$ | $\leftarrow 5$ | $\leftarrow 6$ | $\leftarrow 7$ | $\leftarrow 8$ | $\leftarrow 9$ | $\leftarrow 12$ | $\leftarrow 15$ | $\leftarrow 18$ |
| Myria- | $8 \rightarrow$ | $5 \rightarrow$ | $2 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 2$ | $\leftarrow 3$ | $\leftarrow 4$ | $\leftarrow 5$ | $\leftarrow 6$ | $\leftarrow 7$ | $\leftarrow 10$ | $\leftarrow 13$ | $\leftarrow 16$ |
| Kilo- | $9 \rightarrow$ | $6 \rightarrow$ | $3 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 2$ | $\leftarrow 3$ | $\leftarrow 4$ | $\leftarrow 5$ | $\leftarrow 6$ | $\leftarrow 9$ | $\leftarrow 12$ | $\leftarrow 15$ |
| Hecto- | $10 \rightarrow$ | $7 \rightarrow$ | $4 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 2$ | $\leftarrow 3$ | $\leftarrow 4$ | $\leftarrow 5$ | $\leftarrow 8$ | $\leftarrow 11$ | $\leftarrow 14$ |
| Deka- | $11 \rightarrow$ | $8 \rightarrow$ | $5 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 2$ | $\leftarrow 3$ | $\leftarrow 4$ | $\leftarrow 7$ | $\leftarrow 10$ | $\leftarrow 13$ |
| Units | $12 \rightarrow$ | $9 \rightarrow$ | $6 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 2$ | $\leftarrow 3$ | $\leftarrow 6$ | $\leftarrow 9$ | $\leftarrow 12$ |
| Deci- | $13 \rightarrow$ | $10 \rightarrow$ | $7 \rightarrow$ | $5 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 2$ | $\leftarrow 5$ | $\leftarrow 8$ | $\leftarrow 11$ |
| Centi- | $14 \rightarrow$ | $11 \rightarrow$ | $8 \rightarrow$ | $6 \rightarrow$ | $5 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 4$ | $\leftarrow 7$ | $\leftarrow 10$ |
| Milli- | $15 \rightarrow$ | $12 \rightarrow$ | $9 \rightarrow$ | $7 \rightarrow$ | $6 \rightarrow$ | $5 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 3$ | $\leftarrow 6$ | $\leftarrow 9$ |
| Micro- | $18 \rightarrow$ | $15 \rightarrow$ | $12 \rightarrow$ | $10 \rightarrow$ | $9 \rightarrow$ | $8 \rightarrow$ | $7 \rightarrow$ | $6 \rightarrow$ | $5 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ |  | $\leftarrow 3$ | $\leftarrow 6$ |
| Nano- | $21 \rightarrow$ | $18 \rightarrow$ | $15 \rightarrow$ | $13 \rightarrow$ | $12 \rightarrow$ | $11 \rightarrow$ | $10 \rightarrow$ | $9 \rightarrow$ | $8 \rightarrow$ | $7 \rightarrow$ | $6 \longrightarrow$ | $3 \rightarrow$ |  | $\leftarrow 3$ |
| Pico. | $24 \rightarrow$ | $21 \rightarrow$ | $18 \rightarrow$ | $16 \rightarrow$ | $15 \rightarrow$ | $14 \rightarrow$ | $13 \rightarrow$ | $12 \rightarrow$ | $11 \rightarrow$ | $10 \rightarrow$ | $9 \rightarrow$ | $6 \rightarrow$ | $3 \rightarrow$ |  |

## 30. STANDARD FREQUENCIES AND TIME SIGNALS

## (A) WWV and WWVH

Time signals, audio frequencies, and a 36 -digit binary timing code are broadcast continuously day and night from WWV, operated by the National Bureau of Standards near Washington, D.C. The WWV broadcast frequencies are 2.5, $5,10,15,20$, and 25 megacycles; and its modulation consists of 1 -cps pulses and 440 - and $600-\mathrm{cps}$ tones. A similar station, WWVH, is located at Maui, Hawaii. It broadcasts on frequencies of 5,10 , and 15 megacycles.

Signals from WWV and WWVH are coordinated with Stations GBR and MSF at Rugby, England, and Station NBA in the Canal Zone. This coordination provides a more uniform system of time and frequency transmissions throughout the world. It also aids in the solution of many scientific and technical problems such as radiocommunications, geodesy, and tracking of artificial satellites.

WWV is silent for a four-minute period beginning approximately 45 minutes after each hour. The WWVH transmissions are silent for a four-minute period beginning approximately 15 minutes after the hour, and for 34 minutes beginning at 1900 Universal Time.

The frequencies transmitted from WWV and WWVH are accurate to within 1 part in 10 billion.

The drawing in Fig. 54 shows a breakdown of the transmissions during each hour. Each small division represents 1 minute; each large division, 5 minutes.

The audio-frequency signals are transmitted from WWV for precisely two minutes at the beginning of each fiveminute period except at the beginning of each hour, when the transmission is for three minutes, and at 45 minutes after the hour when WWV is silent. The audio-frequency signal from WWVH is for precisely three minutes during the periods indicated in Fig. 54.

The timing code (a 36 -bit, 100 -pulses-per-second code carried on $1,000-\mathrm{cps}$ modulation) is broadcast for one-minute intervals, 10 times per hour. This timing code is indicated by the shaded area in Fig. 54, and immediately follows the 440 and $600-\mathrm{cps}$ modulation except at the beginning of each hour. The 440 - and $600-\mathrm{cps}$ modulations are alternated as shown in Fig. 54.

The code is binary-coded decimal (BCD), as shown in Fig. 55, and contains the time-of-year information (in Universal Time) in seconds, minutes, hours, and days. The code consists of nine binary groups each second, as shown in Fig. 55A. The groups appear in the following order: two groups for seconds, two for minutes, two for hours, and three for day of year. The expanded drawing at the bottom of Fig. 55A shows the make-up of the pulse code. A " 0 " pulse is 2 milliseconds long (or 2 cycles at $1,000 \mathrm{cps}$ ), and the " 1 " pulse is 6 milliseconds ( 6 cycles at $1,000 \mathrm{cps}$ ). The code is locked in phase with the frequency and time signals.

A complete time frame is 1 second. Fig. 55B shows the make-up of a typical time code. The time code is amplitude-


* One Minute Announcement interval (See Fig. 56).
$\dagger$ North Atlantic Propagation Notice-WWV.
$\ddagger$ North Pacific Propagation Notice-WWVH.
- IWDS Warning-WWV.
- IWDS Warning-WWVH.

WWVH Silent Between 1900 and 1934 Universal Time
Fig. 54


Fig. 55A


Fig. 55B
modulated on $1,000 \mathrm{cps}$. The leading edge of the time-code pulses coincide with the zero axis of the positive-going 1,000cps signal. The least significant binary group and least significant binary digit in each group occur first. The binary groups follow the 1 -second reference marker. The start time occurs at the leading edge of all pulses.

The BCD contains a 100 -per-second clocking rate, 10 -persecond index markers, and 1-per-second reference markers. The 1,000-cps signal is locked to the code pulses so that millisecond resolution can be obtained easily.

The 10 -per-second index markers consist of " 1 " pulses preceding each code group except at the beginning of the second, where there is a " 0 " pulse.

Each second begins at the leading edge of the " 0 " pulse, as shown in Fig. 55.

The 1 -second reference marker is made up of five " 1 " pulses followed by a " 0 " pulse.

The code is spaced so that it follows each of the 10 -persecond index markers. The last index marker is followed by an unused four-bit group of " 0 " pulses immediately preceding the 1 -second reference marker.

A five-millisecond pulse spaced at intervals of one second is also transmitted. The pulse transmitted by WWV consists of five cycles of a 1,000 -cycle tone. The pulse transmitted by WWVH consists of six cycles of a 1,200 -cycle tone. The 440 - and $600-\mathrm{cps}$ tone signal is interrupted for .04 second for each seconds pulse. The pulse starts .01 second after commencement of the interruption, and resumes .025 second after the pulse. For identification, the fifty-ninth second pulse is omitted, and the zero-second pulse is followed by another pulse 100 milliseconds later.

A voice announcement of Eastern Standard Time and call letters is given each five minutes from station WWV. This is followed by a telegraph-code announcement of Universal Time and another voice announcement of Eastern Standard Time. WWVH broadcasts call letters and Universal Time (UT) in telegraphic code only. The time given is the time at the resumption of the tone.

The drawing in Fig. 56 shows a breakdown of the transmissions during the one-minute announcement intervals marked with an asterisk (*) in Fig. 54. Each division on this drawing represents one second.

During announcement intervals at $191 / 2$ and $491 / 2$ minutes past every hour，propagation notices applying to transmis－ sion paths over the North Atlantic are transmitted from WWV．Similar forecasts for the North Pacific are trans－ mitted from WWVH，during announcement intervals，at 9.4 and 39.4 minutes after the hour．

These notices，in telegraphic code，consist of a letter fol－ lowed by a number．The letter signifies the propagation conditions at the time of the broadcast．The following desig－ nations are used：


[^3]Fig． 56

N—Normal U—Unsettled W—Disturbance
The number following the letter applies to expected propagation conditions during the subsequent 6 or more hours. The following designations are used:

| 1-Useless | 4-Poor to Fair | 7-Good |
| :--- | :--- | :--- |
| 2-Very Poor | 5-Fair | 8-Very good |
| 3-Poor | 6-Fair to Good | 9—Excellent |

At 4.3 and 34.3 minutes past the hour on WWV, and at approximately 14.4 and 44.4 minutes past the hour on WWVH, the IWDS (International World Day Service) warning is broadcast. This message reveals to experimenters in radio, geophysical, and solar sciences the content of the warning message issued at 1600 UT by the world warning agency on days when an outstanding geophysical event has occurred during the preceding 24 hours. This message is first broadcast at 1604.3 UT on WWV and at 1714.4 UT on WWVH.

If the IWDS warning declares an alert, the letters AGI AAAA are broadcast very slowly in code. This means that a significant magnetic storm has started or that an outstanding auroral display or increase in cosmic-ray flux has been reported or observed.

If a special world interval is in progress, the code letters AGI are followed by three extra-long dashes. This again indicates that an alert has been declared and that the geophysical activity is of sufficient interest to warrant special attention and intensified observations. Special world intervals usually last two or three days.

When there is no "state of alert" or "special world interval" in progress, the letters AGI EEEEE are broadcast.

## (B) CHU

The Dominion Observatory at Ottawa, Canada, broadcasts time signals which can be heard throughout the North American continent and many other parts of the world. The frequencies are $3,330,7,335$, and $14,670 \mathrm{kc}$, and the transmission is continuous on all frequencies. The $3,330-\mathrm{kc}$ transmitter has a power of 0.75 kw and the other two, 3 kw .

The frequencies are synthesized from a 100 -kc crystal oscillator which is maintained accurate to within a few parts
in one billion. The "seconds" pips are also derived from this same oscillator and consist of 200 cycles of a $1,000-\mathrm{cps}$ tone.

The "seconds" pips are broadcast continuously except for the 29 th and the 51st through 59th pips, which are omitted each minute. In addition, the 1st to 29th pips are omitted during the first minute of the hour. The beginning of the pip marks the exact second. The zero pip has a duration of 0.5 second instead of the 0.2 second of the other pips.

During the first half-minute of each hour, CHU CANADA CHU is transmitted in code.

A voice announcement of the time is given each minute during the 10 -second interval between the 50 th and 60 th second when the pips are omitted. The announcement is as follows: "CHU, Dominion Observatory Canada, Eastern Standard Time, __ hours, minutes." The time given refers to the beginning of the minute pip which follows, and is on the 24 -hour system.

## (C) Other Standards Stations

Throughout the world, there are many other stations which broadcast similar data. Table VIII lists some of them, and other data about stations operating on the standards frequencies. Table IX lists some other stations in the LF and VLF bands which broadcast similar data, but not on the frequencies assigned for standard-frequency operation.

## 31. FREQUENCY AND OPERATING POWER TOLERANCES

## (A) AM Broadcast

The operating frequency tolerance of each station shall be maintained within $\pm 20$ cycles of the assigned frequency.

The operating power of each AM broadcast station shall be maintained as near as practicable to the licensed power and shall not exceed the limits of 5 per cent above and 10 per cent below the licensed power except in emergencies.

## (B) FM Broadcast

Operating frequency tolerance of each station shall be maintained within $\pm 2,000$ cycles of the assigned center frequency.

Table VIII. Other Standards Stations

| Call <br> Sign | Location | Carrier Freq. (mc) | Modulation (cps) | Power (kw) |
| :---: | :---: | :---: | :---: | :---: |
| ATA | New Delhi, India | 10 | 1;1000 | 1.0 |
| FFH | Paris, France | 2.5; 5; 10 | 1;440; 1000 | 0.3 |
| HBN | Neuchatel, Switzerland | 2.5; 5 | 1;500 | 0.5 |
| HBN IAM | Rome, Italy |  | 1; 440;600; 1000 | 1.0 |
| IBF | Turin, Italy |  | 1;440; 1000 | 0.3 |
|  |  | 2.5; 5; 10; 15 | 1;440; 1000 | 2.0 |
| JJY | Tokyo, Japan Buenos Aires, Argentina | 2.5; 5; 10; 15; 20; 25 | 1; 440; 1000 | 2.0 |
| MSF | Buenos Aires, Argentina Rugby, England | $2.5 ; 5 ; 10 ; 15 ; 20,25$ $2.5 ; 5 ; 10$ | 1; 1000 | 0.5 |
| OMA | Prague, Czechoslovakia | 2.5 | 1;1000 | 1.0 |
| ZLFS | Lower Hutt, New Zealand | 2.5 | - - - - - | 0.03 |
|  | Olifantsfontein, South Africa |  |  | 4.0 |
| WWVL | Fort Collins, Colorado | 20 kc | - - - - - | 1.0 |

Table IX. LF and VLF Stations

| Call Sign | Location | Carrier Freq. (ke) | Modulation (cps) | Power (kw) |
| :---: | :---: | :---: | :---: | :---: |
| WWVB <br> DCF77 <br> OMA <br> GBR <br> MSF <br> NBA | Fort Collins, Colorado <br> Federal German Republic <br> Czechoslovakia <br> Rugby, England <br> Rugby, England <br> Canal Zone (U. S. Navy) | 60 77.5 50 16 60 18 | $\begin{aligned} & 1 ; 200 ; 440 \\ & -----------1 \\ & 1 ; 1000 \\ & 1 \end{aligned}$ | $\begin{array}{r} 5 \\ 12 \\ 5 \\ 300 \\ 10 \\ 100 \end{array}$ |

The operating power of each station shall be maintained as near as practicable to the authorized operating power and shall not exceed the limits of 5 per cent above and 10 per cent below the authorized power except in emergencies.

## (C) TV Broadcast

The carrier frequency of the visual transmitter shall be maintained within $\pm 1,000$ cycles of the authorized carrier frequency.

The center frequency of the aural transmitter shall be maintained 4.5 megacycles $\pm 1,000$ cycles above the visual carrier frequency.

The peak power shall be monitored by a peak-reading device which reads proportionally to voltages, current, or power in the radio-frequency line. The operating power as so monitored shall be maintained as near as practicable to the authorized operating power and shall not exceed the limits of 10 per cent above and 20 per cent below the authorized power except in emergencies.

The operating power of the aural transmitter shall be maintained as near as practicable to the authorized operating power, and shall not exceed the limits of 10 per cent above and 20 per cent below the authorized power except in emergencies.

## (D) Industrial Radio Service

The carrier frequency of stations operating below 220 megacycles in the Industrial Radio Service shall be maintained within $\pm .01 \%$ of the authorized power for stations of 3 watts or less, and $\pm .005 \%$ for stations with an authorized power of more than 3 watts. The frequency tolerance of Industrial Radio Service stations operating between 220 and 1,000 megacycles is specified in the station authorization.

## (E) Citizens-Band Radio

The maximum plate power input to the anode (plate) circuit of the electron tube or tubes which supply energy to the radiating system of a station in this service shall not exceed the values given in Table $\mathbf{X}$.

Table X. Power Limits of Citizens-Band Stations

| Class of Station | Maximum Plate Power Input <br> (Watts) |
| :---: | :---: |
| A | 60 |
| B | 5 |
| C | $5 *$ |
| D | 5 |

* A maximum plate power input of 30 watts is permitted on 27.255 mc only.

The carrier frequency of a station in this service shall be maintained within the percentages of authorized frequency given in Table XI.

Table XI. Frequency Tolerances of Citizens-Band Stations

| Class | Maximum Authorized Plate <br> Power Input <br> (Watts) | Frequency <br> Tolerance $\%$ |  |
| :--- | :--- | :--- | :--- |
|  | 3 or less | Fixed and Base | Mobile |
| A | Over 3 | .001 | .005 |
| B | 3 or less | .001 | .001 |
| B | Over 3 | --- | .5 |
| C | 5 or less* | --- | .3 |
| C | Over 5 (27.255 me only) | --- | .005 |
| D | 5 or less | --- | .005 |

* Class-C stations which have a plate power input of 3 watts or less and are used solely for remote control of objects or devices by radio (other than devices used solely as a means of attracting attention) are permitted a frequency tolerance of $0.01 \%$.


## 32. COMMERCIAL OPERATOR LICENSES

The classes of commercial radio operator licenses issued by the Federal Communications Commission are classified basically as radiotelegraph and radiotelephone licenses.

## (A) Examination Elements

Written examinations are composed of questions from various categories called elements. These elements, and the types of questions in each, are:

Element 1. Basic Law. Provisions of laws, treaties, and regulations with which every operator should be familiar.
Element 2. Basic Operating Practice. Radio operating procedures and practices generally followed or required in communicating by means of radiotelephone stations.
Element 3. Basic Radiotelephone. Technical, legal, and other matters applicable to the operation of radiotelephone stations other than broadcast.
Element 4. Advanced Radiotelephone. Advanced technical, legal, and other matters particularly applicable to the operation of the various classes of broadcast stations.
Element 5. Radiotelegraph Operating Practice. Radio operating procedure and practices generally followed or required in communicating by means of radiotelegraph stations primarily other than in the maritime mobile services of public correspondences.
Element 6. Advanced Radiotelegraph. Technical, legal, and other matters applicable to the operation of all classes of radiotelegraph stations, including operating procedures and practices in the maritime mobile services of public correspondences, and associated matters such as radionavigational aids, message traffic routing and accounting, etc.
Element 7. Aircraft Radiotelegraph. Basic theory and practice in the operation of radiocommunications and radionavigational systems aboard aircraft.
Element 8. Ship Radar Techniques. Specialized theory and practice applicable to the proper installation, servicing, and maintenance of ship radar equipment in general use for marine navigational purposes.

## (B) Examination Requirements

Applicants for licenses must be able to transmit and receive spoken messages in English, and be able to pass the examination elements required for the license. The requirements for the various licenses are:

1. Radiotelephone second-class operator licenses. Written examination elements 1,2 , and 3 .
2. Radiotelephone first-class operator licenses. Written examination elements $1,2,3$, and 4.
3. Radiotelegraph second-class operator license. Transmitting and receiving code test of 16 code groups per minute. Written examination elements 1, 2, 5, and 6.
4. Radiotelegraph first-class operator license. Transmitting and receiving code test of 25 words per minute in conversational language and 20 groups per minute in code. Written examination elements $1,2,5$, and 6.
5. Radiotelephone third-class operator permit. Written examination elements 1 and 2.
6. Radiotelegraph third-class operator permit. Transmitting and receiving code test of 16 code groups per minute. Written examination elements 1,2 , and 5 .

## 33. AMATEUR OPERATOR PRIVILEGES

## (A) Examination Elements

Examinations for amateur operator privileges are composed of questions from various categories, called elements. The various elements and their requirements are:

Element 1(A): Beginner's Code Test. Code test at 5 words per minute.
Element 1(B): General Code Test. Code test at 13 words per minute.
Element 1(C): Expert's Code Test. Code test at 20 words per minute.
Element 2: Basic Amateur Practice. Amateur radio operation and apparatus, including radiotelephone and radiotelegraph.
Element 3(A): Basic Law. Rules and regulations essential to beginners' operation, including sufficient elementary radio theory to understand these rules.
Element 3(B): General Regulations. Provisions of treaties, statutes, and rules and regulations affecting all amateur stations and operators.
Element 4(B): Advanced Amateur Practice. Advanced radio theory and operation applicable to mod-
ern amateur techniques, including-but not limited to-radiotelephony, radiotelegraphy, and transmission of energy for (1) measurements and observations applied to propagation, (2) radio control of remote objects, and (3) similar experimental purposes.

## (B) Examination Requirements

Applicants for original licenses will be required to pass examinations as follows :

1. Amateur Extra Class. Elements 1(C), 2, 3(B), and 4 (B).
2. General Class. Elements 1 (B), 2, and 3(B).
3. Conditional Class. Elements 1(B), 2, and 3(B).
4. Technician Class. Elements 1 (A), 2, and 3 (B).
5. Novice Class. Elements $1(\mathrm{~A})$ and $3(\mathrm{~A})$.

Note: Examinations for licenses (1) and (2) above must be given by an FCC examiner. The examinations for licenses (3), (4), and (5) are taken by mail, under the supervision of a volunteer examiner.

## 34. AMATEUR ("HAM") BANDS

The various bands of frequencies used by amateur radio operators ("hams") are usually referred to in meters instead of the actual frequencies. The number of meters approximates the wavelength at the band of frequencies being designated. The meter bands and their frequency limits are given in Table XII. (Note: Frequencies between 220 and 225 mc are sometimes referred to as $11 / 4$ meters, and between 420 and 450 meters as $3 / 4$ meter.)

Table XII. "Ham" Bands

| Band | Frequency <br> (mc) |
| :---: | :---: |
| 80 Meters | $3.5-4.0$ |
| 40 Meters | $7.0-7.3$ |
| 20 Meters | $14.0-14.35$ |
| 15 Meters | $21.0-21.45$ |
| 10 Meters | $28.0-29.7$ |
| 6 Meters | $50-54$ |
| 2 Meters | $144-148$ |

Table XIII．Types of Emission

| Type of Modulation | Type of Transmission | Supplementary Characteristics | Symbol |
| :---: | :---: | :---: | :---: |
| 1．Amplitude | Absence of any modulation | －－－－－－－－－－－－ | A0 |
|  | Telegraphy without the use of modulating audio frequency（on－off keying） | －－－－－－－－－－－－ | Al |
|  | Telegraphy by the keying of a modulating audio frequency or frequencies or by the keying of the modulated emission（special case：an unkeyed modulated emission） | －－－－－－－－－－－－－－－－ | A2 |
|  | Telephony | Double sideband，full carrier | A3 |
|  |  | Single sideband，reduced carrier | A3a |
|  |  | Two independent sidebands，reduced car－ rier | A3b |
|  | Facsimile | －－－－－－－－－－－－－－ | A4 |
|  | Television | －－ー－ー－ーーーーーーー－ | A5 |
|  | Composite transmissions，and cases not cov－ ered by the above | －－－－－－－－－－ | A9 |
|  | Composite transmissions | Reduced carrier | A9c |
| 2．Frequency（or phase） modulated | Absence of any modulation | －－－－－－－－－－－－－ | FO |
|  | Telegraphy without the use of modulating audio frequency（frequency shift keying） | －－－－－－－－－－－ | F1 |


|  | Telegraphy by the keying of a modulating audio frequency or audio frequencies or by the keying of the modulated emission (special case: an unkeyed emission modulated by audio frequency) | - - - - - - - - - - - | F2 |
| :---: | :---: | :---: | :---: |
|  | Telephony | --------------- | F3 |
|  | Facsimile | - - - - - - - - - - - | F4 |
|  | Television | - - - - - - - - - - - - | F5 |
|  | Composite transmissions and cases not covered by the above | --------------- | F9 |
| 3. Pulsed emissions | Absence of any modulation carrying information | -------------- | PO |
|  | Telegraphy without the use of modulating audio frequency | - - - - - - - - - - - - | P1 |
|  | Telegraphy by the keying of a modulating audio frequency or of the modulated pulse (special case: an unkeyed modulated pulse) | Audio frequency or frequencies modulating the pulse in amplitude | P2d |
|  |  | Audio frequency or frequencies modulating the width of the pulse | P2c |
|  |  | Audio frequency or frequencies modulating the phase (or position) of the pulse | P2f |
|  | Telephony | Amplitude-modulated pulse | P3d |
|  |  | Width-modulated pulse | P3e |
|  |  | Phase-(or position-) modulated pulse | P3f |
|  | Composite transmissions and cases not covered by the above | - - - - - - - - - - - | P9 |

## 35. TYPES OF EMISSIONS

Emissions are classified according to their modulation, type of transmission, and supplementary characteristics. These classifications are given in Table XIII on pages 72 and 73. When a full designation of the emissions-including bandwidth-is necessary, the symbols in Table XIII are prefixed by a number indicating the bandwidth in kilocycles. Below 10 kc , this number is given to two significant figures.

## 36. TELEVISION CHANNEL FREQUENCIES

The chart in Fig. 57 (page 75) lists the frequency limits of all television channels and the frequency of the picture and sound carriers of each channel.

## 37. TELEVISION SIGNAL STANDARDS

The signal standards for television broadcasting are given in Figs. 58A and B (pages 76 and 77). Note: The standards given here are for color transmission. For monochrome transmission, the standards are the same except the color burst signal is omitted. Also, for color the vertical and horizontal scanning frequencies are 59.94 and $15,734.264 \mathrm{cps}$, respectively; for monochrome they are 60 and $15,750 \mathrm{cps}$.

## 38. AUDIO-FREQUENCY SPECTRUM

The audio-frequency spectrum is generally accepted as extending from 15 cps to $20,000 \mathrm{cps}$. Fig. 60 (page 79) gives the frequencies for each tone of the standard keyboard, based on the current musical pitch of $A=440$ cps. Fig. 59 (page 78) shows the frequency range of various musical instruments and of other sounds. The frequency range shown for each sound is the range needed for faithful reproduction, and includes the fundamental frequency and the necessary harmonic frequencies. The frequency range of the human ear, and the various broadcasting and recording media, are also included in Fig. 59.

## 39. RADIO-FREQUENCY SPECTRUM

(A) Frequency Classification

The radio-frequency spectrum from 3 kc to $3,000,000 \mathrm{mc}$ is divided into the various bands (shown in Table XIV on page 78) for easier identification.

Television Channel Frequencies


[^4][^5]


NOTES

1. H = Time from start of one line to start of next line.
2. $V=$ Time from start of one field to start of next field.
3. Leading and trailing edges of vertical blanking should be complete in less than 0.1 H
4. Leading and trailing slopes of horizontal blanking must be steep enough to preserve minimum and maximum values of $(x+y)$ and (z) under all conditions of picture content.
5. Dimensions marked with asterisk indicate that tolerances given are permitted only for long time variations and not for successive cycles.
6. Equalizing pulse area shall be between 0.45 and 0.5 of area of a horizontal sync pulse.
7. Color burst follows each horizontal pulse, but is omitted following the equalizing pulses and during the broad vertical pulses.
8. Color burst to be omitted during monochrome transmissions.
9. The burst frequency shall be 3.579545 mc . The tolerance on the frequency shall be $+0.0003 \%$ with a maximum rate of change of frequency shall be $\pm 0.0003 \%$ with a maximum rate of che
10. The horizontal scanning frequency shall be $2 / 455$ times the burst frequency.
11. The dimensions specified for the burst determine the times of starting and stopping the burst but not its phase. The color burst consists of amplitude modulation of a continuous sine wave.
12. Dimension " $P$ " represents the peak excursion of the luminance signal at blanking level but does not include the chrominance signal. Dimension " S " is the sync amplitude above blanking level. Dimension " C " is the peak carrier amplitude.


Fig. 59

## Table XIV. Frequency Classification

| Frequency | Band <br> No. | Classification | Abbreviation |
| :---: | :---: | :--- | :--- |
| $3-30 \mathrm{kc}$ | 4 | Very low frequencies | VLF |
| $30-300 \mathrm{kc}$ | 5 | Low frequencies | LF |
| $300-3000 \mathrm{kc}$ | 6 | Medium frequencies | MF |
| $3-30 \mathrm{mc}$ | 7 | High frequencies | HF |
| $30-300 \mathrm{mc}$ | 8 | Very high frequencies | VHF |
| $300-3000 \mathrm{mc}$ | 9 | Ultrahigh frequencies | UHF |
| $3000-30,000 \mathrm{mc}$ | 10 | Super-high frequencies | SHF |
| $30,000-300,000 \mathrm{mc}$ | 11 | Extremely high frequencies | EHF |
| $300,000-3,000,000 \mathrm{mc}$ | 12 | - | - |

## (B) FCC Allocations

The FCC allocations for the various services between 10 kc and $100,000 \mathrm{mc}$ are given in Fig. 61A and B (located on the fold-out page between pages 180 and 181.


Fig. 60

## Symbols and Codes

## 40. INTERNATIONAL Q SIGNALS

The international $Q$ signals were first adopted to enable ships at sea to communicate with each other or to foreign shores without experiencing language difficulties. The signals consist of a series of three-letter groups starting with $Q$ and having the same meaning in all languages. Today, $Q$ signals serve as a convenient means of abbreviation in communications between amateurs. Each $Q$ signal has both an affirmative and an interrogative meaning. The question is designated by the addition of the question mark after the $Q$ signal. The most common $Q$ signals are listed in Table XV.

Table XV. Q Signals

| Signal | Question | Answer or Advice |
| :---: | :---: | :---: |
| QRG | Will you tell me my exact frequency? | Your exact frequency is . . . kc (or mc). |
| QRH | Does my frequency vary? | Your frequency varies. |
| QRK | What is the readability of my signals? | The readability of your signals is |
| QRM | Are you being interfered with? | I am being interfered with. |
| QRN | Are you troubled by static? | I am troubled by static. |
| QRO | Shall I increase power? | Increase power. |
| QRP | Shall I decrease power? | Decrease power. |
| QRQ | Shall I send faster? | Send faster. |
| QRS | Shall I send more slowly? | Send more slowly (. . . . words per minute). |
| QRT | Shall I stop sending? | Stop sending. |
| QRU | Have you anything for me? | I have nothing for you. |
| QRV | Are you ready? | 1 am ready. |
| QRX | When will you call again? | I will call you again at . . hours [on . . . . kc (or mc)]. |
| QSA | What is the strength of my signals? | The strength of your signals is |
| QSB ${ }^{\text {- }}$ | Are my signals fading? | Your signals are fading. |
| QSL | Can you acknowledge receipt? | I am acknowledging receipt. |
| QSM | Shall I repeat the last message I sent you? | Repeat the last message you have sent me. |
| QSO | Can you communicate with . . . . direct or by relay? | I can communicate with . . . . direct (or by relay through . . . .). |
| QSV | Shall I send a series of V's? | Send a series of V's. |
| QSY | Shall I change to transmission on another frequency? | Change to transmission on another frequency [or on .... kc (or mc)]. |
| QSZ | Shall I send each word or group twice? | Send each word or group twice. |
| QTH | What is your location? | My location is |

## 41. "10" SIGNALS

The abbreviations based on the number 10 plus a suffix was originally used for communication between police units. Now they are often used in other forms of two-way communications. The most common signals are given in Table XVI.

Table XVI. " 10 " Signals

| Signal | Meaning | Signal | Meaning |
| :--- | :--- | :--- | :--- |
| $10-1$ | Unable to copy | $10-27$ | Operator on duty |
| $10-2$ | Signal good | $10-30$ | Does not conform to rules |
| $10-3$ | Affirmative-granted-will do | $10-33$ | Emergency traffic this station |
| $10-5$ | Relay | $10-36$ | Confidential information |
| $10-6$ | Busy | $10-41$ | Beginning tour of duty |
| $10-7$ | Off the air | $10-42$ | Ending tour of duty |
| $10-8$ | On the air | $10-44$ | Message received by all con- |
| $10-9$ | Repeat |  | cerned |
| $10-10$ | On detail, but subject to call | $10-60$ | What is next number? |
| $10-11$ | Remain in service | $10-61$ | CW traffic |
| $10-12$ | Visitors or officials present | $10-62$ | Teletype traffic |
| $10-13$ | Weather and road conditions | $10-63$ | Any answer our number . . . |
| $10-14$ | Correct time | $10-64$ | Message for local delivery |
| $10-16$ | Pick up (. .) | $10-65$ | Net message assignment |
| $10-17$ | Urgent-rush present detail | $10-66$ | Cancellation |
| $10-18$ | Anything for us? | $10-67$ | Clear for net message |
| $10-19$ | Nothing for you | $10-68$ | Dispatch information |
| $10-20$ | Location | $10-88$ | Advise present phone number |
| $10-21$ | Call ...by telephone |  | of . . |
| $10-22$ | Reporting in person to ... | $10-91$ | Too weak; talk closer to mike |
| $10-23$ | Arrived at scene | $10-92$ | Too loud; talk farther from mike |
| $10-24$ | Finished with last assignment | $10-93$ | Frequency check |
| $10-25$ | Disregard last information | $10-94$ | Give a test |

42. THE INTERNATIONAL CODE


## 43. GREEK ALPHABET

The Greek alphabet is given in Table XVII. The items for which each letter is a symbol are also listed. The small Greek letter is the symbol for all the items listed unless a capital letter is indicated (cap).

Table XVII. Greek Alphabet

| Letter |  | Name | Designates |
| :---: | :---: | :---: | :---: |
| Small | Capital |  |  |
| $a$ | A | Alpha | Angles, coefficients, attenuation constant, absorption factor, area. |
| $\beta$ | B | Beta | Angles, coefficients, phase constant. |
| $\gamma$ | $\Gamma$ | Gamma | Specific quantity, angles, electrical conductivity, propagation constant, complex propagation constant (cap). |
| $\delta$ | $\lambda$ | Delta | Density, angles, increment or decrement (cap or small), determinant (cap), permittivity (cap). |
| $\epsilon$ | E | Epsilon | Dielectric constant, permittivity, base of natural (Napierian) logarithms, electric intensity. |
| $\zeta$ | Z | Zeta | Co-ordinate, coefficients. |
| $\eta$ | H | Eta | Intrinsic impedance, efficiency, surface charge density, hysteresis, coordinates. |
| $\theta$ | $\theta$ | Theta | Angular phase displacement, time constant, reluctance, angles. |
| 6 | 1 | lota | Unit vector. |
| $\kappa$ | K | Kappa | Susceptibility, coupling coefficient. |
| $\lambda$ | $\Lambda$ | Lambda | Wavelength, attenuation constant, permeance (cap). |
| $\mu$ | M | Mu | Prefix micro-, permeability, amplification factor. |
| $\nu$ | N | Nu | Reluctivity, frequency. |
| $\xi$ | 3 | Xi | Co-ordinates. |
| 0 | $\bigcirc$ | Omicron | - |
| $\pi$ | TT | Pi | 3.1416 (circumference divided by diameter). |
| $\rho$ | P | Rho | Resistivity, volume charge density, co-ordinates. |
| $\sigma$ | $\Sigma$ | Sigma | Surface charge density, complex propagation constant, electrical conductivity, leakage coefficient, sign of summation (cap). |
| T | T | Tau | Time constant, volume resistivity, time-phase displacement, transmission factor, density. |
| $v$ | $\Upsilon$ | Upsilon | - |

## Table XVII. Greek Alphabet-(Cont'd)

| Letter |  |  |  |
| :---: | :---: | :--- | :--- |
| Small | Capital | Name | Designates |$|$| Phi |
| :--- |
| $\phi$ |
| $\psi$ |

## 44. ELECTRONIC SYMBOLS AND ABBREVIATIONS*

A-Ammeter; ampere; area
a-Ampere
AC, a.c., a-c, ac-Alternating current
AF, a.f., a-f, af-Audio frequency
AFC, afc-Automatic frequency control
AGC, age--Automatic gain control
AM, am—Amplitude modulation
Amp, amp., Amps, amps.-Ampere; amperes

Ant, ant.-Antenna
AVC, a.v.c., ave-Automatic volume control
B-Susceptance
b-Magnetic flux density
BC, be-Broadcas $\dagger$
BFO, bfo-Beat-frequency oscillator
C-Capacitance; capacitor
${ }^{\circ} \mathrm{C}$-Degrees Celsius or centigrade
cm-Centimeter
cps-Cycles per second
CW, cw-Continuous wave
db-Decibels
DC, d.c., d-c, dc—Direct current
d.c.c., dec-Double cotton-covered

DPDT, d.p.d.t., dpdt-Double-pole, dou-ble-throw
DPST, d.p.s.t., dpst-Double-pole, singlethrow
d.s.c., dsc-Double silk-covered

E, e-Voltage
e.c., ex-Enamel-covered

EMF, emf-Electromotive force
ERP—Effective radiated power

F, f-Farad
f-Frequency
${ }^{\circ}$ F--Degrees Fahrenheit
FM, f.m., fm-Frequency modulation
G-Conductance
$\mathbf{G}_{\mathrm{m}}, \boldsymbol{g} m, \mathbf{g}_{\mathrm{m}}$ —Mutual conductance
GCT-Greenwich Civil Time
gnd-Ground
H, h-Henry
HF, h.f., h.f, hf-High frequency
hp-Horsepower
hy.-Henry
I-Current
IF, i.f., i-f, if-Intermediate frequency
ips-Inches per second
i-Joule; an imaginary number; an operator to rotate a vector quantity $90^{\circ}$ counterclockwise
K—X 1000; dielectric constant; a numerical value that does not change during a given period
k-Dielectric constant
KC, ke—Kilocycle
kv-Kilovolt
kva-Kilovolt ampere
KW, kw-Kilowatt
KWH, kwh—Kilowatt hour
L-Inductance; inductor
--Length
LF, I.f., I-f, If-Low frequency
M—Mutual inductance; $\times 1000$
m-Meter
ma-Milliampere

[^6]MC, Mc, me-Megacycle
mew-Modulated continuous wave
meg-Megohm
MF, m.f., m-f, mf—Medium frequency
mf, mfd-Mierofarad
$\mathbf{m h}$-Millihenry
mm—Millimeter
mmf, mmfd—Micromicrofarad
mv—Millivoit (sometimes microvolt)
mw-Milliwatt (sometimes microwatt)
NC-No connection
OD-Outside diameter
P-Power
pf-Power factor
p-p-Peak-to-peak
Q-Merit of a coil or capacitor; quantity of electricity
R-Resistance; resistor
RC, R-C—Product of resistance time capacitance; resistor-capacitor
RF, r.f., r-f, rf—Radio frequency
RFC-Radio-frequency choke coil
rms-Root mean square
rpm-Revolutions per minute
s.c.c., sec-Single cotton-covered
s.c.e., sce-Single cotton enamel
sec-Second; secondary
s.s.c., sse—Single silk-covered

SHF; s.h.f., shf-Super-high frequencies
SW, sw-Short wave
†-Time
T-Temperature
trf-Tuned radio frequency
UHF, uhf-Ultrahigh frequencies
V, v-Volt; voltmeter
VHF, vhf-Very high frequencies
VOM, vom-Volt-ohm-milliammeter
VTVM, vivm-Vacuum-tube voltmeter
VU—Volume unit
W-Watt; work
w-Watt
wh, whr-Watt-hour
X—Reactance
$\mathrm{X}_{6}$-Capacitive reactance
$\mathrm{X}_{L}$,-Inductive reactance
$\mathbf{Y}$-Admittance
Z—Impedance
$\mu \mathrm{a}$-Microampere
$\mu \mathrm{f}$-Microfarad
$\mu \mathrm{h}$-Microhenry
$\mu \mu \mathbf{f}$-Micromicrofarad
$\sim$-Cycles per second

## 45. SEMICONDUCTOR ABBREVIATIONS

The following symbols and abbreviations have been adopted as standard by the Electronic Industries Association (EIA) and the National Electrical Manufacturers Association (NEMA).

B, b-Base electrode for units employing a single base
$\boldsymbol{b}_{1}, \boldsymbol{b}_{2}$, etc.-Base electrodes for more than one base
BV ${ }_{\text {cro-Breakdown }}$ voltage, collector to base, emitter open
BV ceo-Breakdown voltage, collector to emitter, base open
BV $\mathrm{Brin}^{\text {- Breakdown voltage, collector to }}$ emitter, with specified resistance between base and emitter
BVces-Breakdown voltage, collector to emitter, with base short-circuited to emitter
$\mathrm{BV}_{\text {fro }}-$ Breakdown voltage, emitter to base, collector open
$\mathrm{BV}_{\mathrm{R}}$-Breakdown voltage, reverse
C, c-Collector electrode
$C_{1 \downarrow}$-Input capacitance (common base)
$\mathbf{C i c}_{\text {ic }}$-Input capacitance (common collector)
$\mathbf{C}_{\text {te }}$-Input capacitance (common emitter)
$C_{\text {ol }}$-Output capacitance (common base)
$C_{\text {oc }}$-Output capacitance (common collector)
$C_{0 .}$-Output capacitance (common emitter)
E, e-Emitter electrode
$\mathbf{f}_{\text {hfl }}$-Small-signal, short-circuit, forwardcurrent, transfer-ratio cutoff frequency (common base)
$\mathbf{f l y r}$-Small-signal, short-circuit, forwardcurrent, transfer-ratio cutoff frequency (common collector)
$\mathbf{f}_{\text {hfe }}$-Small-signal, short-circuit, forwardcurrent, transfer-ratio cutoff frequency (common emitter)
$\mathbf{f}_{\text {max }}$-Maximum frequency of oscillation
$\mathbf{G p h}_{\mathrm{p}}$-Large-signal average power gain (common base)
$\mathbf{G}_{\mathrm{pb}}$-Small-signal average power gain (common base)
$\mathbf{G}_{\mathrm{rc}}$-Large-signal average power gain (common collector)
$\mathbf{G}_{\mathrm{p}}$-Small-signal average power gain (common collector)
$\mathbf{G}_{\mathrm{p}:}$-Large-signal average power gain (common emitter)
$\mathbf{G}_{\mathrm{pe}}$-Small-signal average power gain (common emitter)
$h_{F s}$-Static value of the forward-current transfer ratio (common base)
$h_{\text {fo }}$-Small-signal, short-circuit, forwardcurrent transfer ratio (common base)
hrc-Static value of the forward-current transfer ratio (common collector)
hec-Small-signal, short-sircuit, forwardcurrent transfer ratio (common collector)
$h_{\mathrm{FE}}-$ Static value of the forward-current transfer ratio (common emitter)
hes-Small-signal, short-circuit, forwardcurrent transfer ratio (common emitter)
$h_{\text {IR }}$-Static value of the input resistance (common base)
$h_{1 s}$-Small-signal value of short-circuit input impedance (common base)
$h_{1 c}-$ Static value of the input resistance (common collector)
$h_{i e}$-Small-signal value of short-circuit input impedance (common emitter)
$h_{1 E}-$ Static value of the input resistance (common emitter)
$h_{\text {ie }}$-Small-signal value of short-circuit input impedance (common emitter)
$h_{\text {se }}$ (real)-Real part of small-signal value of short-circuit input impedance (common emitter)
hos-Static value of open-circuit output conductance (common base)
$\mathbf{h}_{\text {ob }}$-Small-signal value of open-circuit output admittance (common base)
hoc-Static value of open-circuit output conductance (common collector)
$h_{\text {or }}$-Small-signal value of open-circuit output admittance (common collector)
hor-Static value of open-circuit output conductance (common emitter)
$h_{\text {oe }}$-Small-signal value of open-circuit output admittance (common emitter)
$h_{\text {rb }}-S m a l l-s i g n a l$ value of open-circuit, reverse-voltage transfer ratio (common base)
$h_{r u}$-Small-signal value of open-circuit, reverse-voltage transfer ratio (common collector)
$\mathbf{h}_{\text {re }}$-Small-signal value of open-circuit, reverse-voltage transfer ratio (common emitter)
I, i-Intrinsic region of a device (where neither holes nor electrons predominate)
$I_{s}$-Base current (DC)
$\mathrm{I}_{\mathrm{l}}$-Base current (rms)
$\mathrm{i}_{1}$-Base current (instantaneous)
I(-Collector current (DC)
I,-Collector current (rms)
$\mathrm{i}_{\mathrm{e}}$-Collector current (instantaneous)
$\mathbf{l}_{\text {cuo }}$-Collector cutoff current (DC), emitter open
$I_{\text {ceoo-Collector cutoff current ( }} \mathrm{DC}$ ), base open
$\mathbf{I}_{\text {(efi-h }}$ Collector cutoff current (DC), with specified resistance between base and emitter
$I_{\text {crix-Collector current ( }}$ (DC), with specified circuit between base and emitter
$\mathrm{I}_{\text {cess-Collector cutoff current ( }} \mathrm{DC}$ ), with base short-circuited to emitter
$1_{1}$ :-Emitter current (DC)
$1_{\text {e }}$-Emitter current (rms)
$\mathrm{i}_{\mathrm{p}}$-Emitter current (instantaneous)
$I_{\text {mio-Emitter cutoff }}$ current (DC), collec. tor open
IF-Forward current (DC)
if-Forward current (instantaneous)
lo-Average output (rectified) current
$I_{\mathrm{H}}$-Reverse current (DC)
$\mathbf{i}_{\boldsymbol{R}}$-Reverse current (instantaneous)
$\mathbf{K}_{\theta}$-Thermal derating factor
$\mathbf{L}_{\mathbf{c}}$-Conversion loss
$\mathrm{N}, \mathrm{n}$-Region of a device where electrons are the majority carriers
NF-Noise figure
P, p-Region of a device where holes are the majority carriers
$P_{11}$ i-Total power input (DC or average) to the base electrode with respect to the emitter electrode
pus-Total power input (instantaneous) to the base electrode with respect to the emitter electrode

Pcr-Total power input (DC or average)
to the collector electrode with respect to the base electrode
Per:-Total power input (instantaneous) to to the collector electrode with respect to the base electrode
P(es-Total power input (DC or average) to the collector electrode with respect to the emitter electrode
per-Total power input (instantaneous) to the collector electrode with respect to the emitter electrode
$\mathbf{P}_{\text {EH }}$-Total power input (DC or average) to the emitter electrode with respect to the base electrode
per-Total power input (instantaneous) to the emitter electrode with respect to the base electrode
$\mathbf{P}_{18}$-Large-signal input power (common base)
$\mathbf{P}_{10}$-Small-signal input power (common base)
$P_{\text {IC }}$-Large-signal input power (common collector)
$\mathbf{P}_{\mathrm{te}_{e}}$-Small-signal input power (common collector)
$\mathbf{P a}_{\text {IE }}$-Large-signal input power (common emitter)
$\mathbf{P}_{\text {ie }}$-Small-signal input power (common emitter)
$\mathbf{P}_{\text {os-Large-signal output power (common }}$ base)
$P_{\text {ob }}$-Small-signal output power (common base)
Poc-Large-signal output power (common coliector)
$\mathbf{P}_{\text {oc }}$-Small-signal output power (common coilector)
$\mathbf{P}_{\text {On:-Large-signal }}$ output power (common emitter)
$\mathbf{P}_{\text {ge }}$-Small-signal output power (common emitter)
$\mathrm{Pr}_{\mathrm{r}}$-Total power input (DC or average) to all electrodes

Pr-Total power input (instantaneous) to all electrodes
$\mathbf{R}_{\mathrm{R}}$-External base resistance
$R_{C}-$ External colfector resistance
res (sat)-Collector-to-emitter saturation resistance
$\mathbf{R}_{\mathrm{t}}$-External emitter resistance
$\mathbf{R}_{1}$-Load resistance
T-Temperature
$\mathrm{T}_{\mathrm{A}}$-Ambient temperature
$\mathrm{T}_{\mathrm{f}}$;-Case temperature
$\mathrm{t}_{\mathrm{d}}$-Delay time
$\mathrm{T}_{\mathrm{f}}$-Fall time
$\dagger_{\mathrm{rr}}$-Forward recovery time
$\mathrm{T}_{\mathbf{J}}$-Junction temperature
Topr-Operating temperature
$\dagger_{p}$-Pulse time
${ }^{1}$-Rise time
$\dagger_{\mathrm{r}}$-Reverse recovery time
$\mathrm{t}_{\mathrm{s}}$-Storage time
$\mathrm{T}_{\mathrm{st}} \mathrm{g}$-Storage temperature
${ }^{+}{ }_{w}$-Pulse average time
$\theta$-Thermal resistance
$\theta_{J-A}$-Thermal resistance, junction-toambient
$\theta_{\mathrm{J} \text {-c }}$-Thermal resistance, junction-to-case
$\mathbf{V}_{13}$-Base supply voltage (DC)
$\mathbf{V}_{\text {BC }}$-Base-to-collector voltage (DC)
$\mathbf{V}_{b,}$-Base-to-collector voltage ( rms )
$\mathbf{V}_{b e}$-Base-to-collector voltage (instantaneous)
$\mathbf{V}_{\text {BE:-Base-to-emitter voltage (DC) }}$
$\mathbf{V}_{\text {be }}$-Base-to-emitter voltage (rms)
$\mathbf{v}_{\mathrm{be}}$-Base-to-emitter voltage (instantaneous)
$\mathbf{V}_{\mathrm{CH}}$-Collector-to-base voltage (DC)
$\mathbf{V}_{\mathrm{eb}}$-Collector-to-base voltage (rms)
$\mathbf{v}_{\text {ch }}$-collector-to-base voltage (instantaneous)
$V_{\text {cc }}$-Collector supply voltage (DC)
$\mathbf{V}_{\text {Ce }}$-Collector-to-emitter voltage (DC)
$\mathbf{V}_{\text {ce }}$-Collector-to-emitter voltage $\langle\mathrm{rms}$ )

| $\mathrm{V}_{\mathrm{c}}$-Collector-to-emitter voltage (instantaneous) | $\mathbf{V}_{\mathbf{F}}$-Forward voltage (DC) <br> $\mathrm{V}_{\mathrm{F}}$-Forward voltage (instantaneous) |
| :---: | :---: |
| $\mathbf{V}_{\text {CE }}$ (sat)-Collector-to-emitter saturation voltage | $V_{\text {erf-DC }}$ open-circuit voltage (floating potential) between collector and base, |
| $\mathrm{V}_{\text {EB }}$-Emitter-to-base voltage (DC) | with emitter biased in reverse direc- |
| $\mathrm{V}_{\text {eb }}$-Emitter-to-base voltage (rms) | tion with respect to base |
| $V_{e b}$-Emitter-to-base voltage (instantaneous) | $V_{\text {ref-DC }}$ open-circuit voltage (floating potential) between emitter and collec- |
| $\mathbf{V}_{\text {EC }}$-Emitter-to-collector voltage ( DC ) | tor, with base biased in reverse direc- |
| $\mathbf{V}_{\mathrm{ec}}$-Emitter-to-collector voltage (rms) | tion with respect to collector |
| $\mathrm{v}_{\mathrm{ec}}$-Emitter-to-collector voltage (instan- | $\mathbf{V}_{\mathrm{RT}}-$ Reach-through voltage |
| taneous) | $\mathbf{V}_{\mathrm{H}}$-Reverse voltage (DC) |
| VEE-Emitter supply voltage (DC) | $\mathrm{V}_{\mathrm{K}}$-Reverse voltage (instantaneous) |

## 46. EIA TRANSFORMER COLOR CODE

The following diagrams illustrate the color code for transformers recommended by the EIA.

## (A) Power Transformers



Fig. 62
(B) IF Transformers


## (C) Audio Output and Interstage Transformers



## 47. RESISTOR AND CAPACITOR COLOR CODES

The present method and some of the older methods of color-coding resistors and capacitors are given in Figs. 65A and B (pages 89 and 90 ).

## 48. ELECTRONIC SCHEMATIC SYMBOLS

The most common schematic symbols are illustrated in Figs. 66A, B, C, and D (pages 91, 92, 93, and 94).


Resistor and Capacitor Color Codes-(Cont'd)

## Electronic Schematic Symbols

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Fig. 66A

## Electronic Schematic Symbols-(Cont'd)



Fig. 66B

Electronic Schematic Symbols-(Cont'd)


Fig. 66C


Fig. 66D

## Service and Installation Data

## 49. COAXIAL CABLE CHARACTERISTICS

Table XVIII lists the most frequently-used coaxial cables. The electrical specifications include the impedance in ohms, capacitance in micromicrofarads per foot, attenuation in db per 100 feet, and the outside diameter. (See page 43 for formulas.)

Table XVIII. Coaxial Cable Characteristics

| Type RG... <br> /U | Imp. (ohms) | Cap. (mmf perft.) | Diam. (inches) | Atrenuation-db per 100 ft . |  |  |  |  | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\underset{\mathrm{m}}{1}$ | $\begin{aligned} & 10 \\ & \mathrm{me} \end{aligned}$ | $\begin{gathered} 100 \\ \mathbf{m e} \end{gathered}$ | $\begin{aligned} & 400 \\ & \mathrm{mc} \end{aligned}$ | $\begin{gathered} 1000 \\ \mathrm{mc} \end{gathered}$ |  |
| 5 | 52.5 | 28.5 | . 332 | . 21 | . 77 | 2.9 | 6.5 | 11.5 | Small, double braid |
| 5A | 50 | 29 | . 328 | . 16 | . 66 | 2.4 | 5.25 | 8.8 | Small, low loss |
| 6 | 76 | 20 | . 332 | . 21 | . 78 | 2.9 | 6.5 | 11.2 | IF \& video |
| 8 | 52 | 29.5 | . 405 | . 16 | . 55 | 2.0 | 4.5 | 8.5 | General purpose |
| 9 | 51 | 30 | . 420 | . 12 | . 47 | 1.9 | 4.4 | 8.5 | General purpose |
| 9 A | 51 | 30 | . 420 | . 16 | . 59 | 2.3 | 5.2 | 8.6 | Stable attenuation |
| 11 | 75 | 20.5 | . 405 | . 18 | . 62 | 2.2 | 4.7 | 8.2 | Community TV |
| 13 | 74 | 20.5 | . 420 | . 18 | . 62 | 2.2 | 4.7 | 8.2 | IF |
| 14 | 52 | 29.5 | . 545 | . 10 | . 38 | 1.5 | 3.5 | 6.0 | RF power |
| 16 | 52 | 29.5 | . 630 | - | - | - | - | - | RF power |
| 17 | 52. | 29.5 | . 870 | . 06 | . 24 | . 95 | 2.4 | 4.4 | RF power |
| 19 | 52 | 29.5 | 1.120 | . 04 | . 17 | . 68 | 1.28 | 3.5 | Low-loss RF |
| 21 | 53 | 29 | . 332 | 1.4 | 4.4 | 14.0 | 29.0 | 46.0 | Attenuating cable |
| 22 | 95 | 16 | . 405 | . 41 | 1.3 | 4.3 | 8.8 | 46.0 | Twin conductors |
| 23 | 125 | 12 | . $65 \times .945$ | - | . 4 | 1.7 | . | - | Twin conductors (balanced) |
| 25 | 48 | 50 | . 565 | - | - | - | - | - | Pulse |
| 26 | 48 | 50 | . 525 | - | - | - | - | - | Pulse |
| 27 | 48 | 50 | . 675 | - | - | - | - | - | Pulse |
| 28 | 48 | 50 | . 805 | - | - | - | - | - | Pulse |
| 33 | 51 | 30 | . 470 | - | - | - | - | - | Pulse |
| 34 | 71 | 21.5 | . 625 | . 065 | . 29 | 1.3 | 3.3 | 6.0 | Flexible, medium |
| 35 | 71 | 21.5 | . 945 | . 064 | . 22 | . 85 | 2.3 | 4.2 | Low-loss video |
| 36 | 69 | 22 | 1.180 | - | - | - | - | - | -- |
| 41 | 67.5 | 27 | . 425 | - | 7 | - | - | - | Special twist |
| 54A | 58 | 26.5 | . 250 | . 18 | . 74 | 3.1 | 6.7 | 11.5 | Flexible, small |

Table XVIII. Coaxial Cable Characteristics-(Cont'd)

| Type RG... <br> /U | Imp. (ohms) | Cap. (mmf perft.) | Diam. (inches) | Attenuation-db per 100 ft . |  |  |  |  | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} \mathbf{1} \\ \mathbf{m c} \end{gathered}$ | $\begin{aligned} & 10 \\ & \mathrm{mc} \end{aligned}$ | $\begin{array}{r} 100 \\ \mathrm{mc} \end{array}$ | $\begin{aligned} & 400 \\ & \mathrm{mc} \end{aligned}$ | $\begin{gathered} 1000 \\ \mathrm{me} \end{gathered}$ |  |
| 55 | 53.5 | 28.5 | . 206 | . 36 | 1.3 | 4.8 | 10.4 | 17.0 | Flexible, small |
| 56 | - | - | . 535 | - | - | - | - | - | Pulse |
| 57 | 95 | 17 | . 625 | . 18 | . 71 | 3.0 | 7.3 | 13.0 | Twin conductors |
| 58 | 53.5 | 30 | . 195 | . 38 | 1.4 | 5.2 | 11.2 | 20.0 | General purpose |
| 58A | 50 | 30 | . 195 | . 42 | 1.6 | 6.2 | 14.0 | 24.0 | Test leads |
| 59 | 73 | 21 | . 242 | . 30 | 1.1 | 3.8 | 8.5 | 14.0 | TV lead-in |
| 60 | 50 | - | . 425 | - | - | - | - | - | Pulse cable |
| 61 | 500 | - | - | - | - | - | - | - | Special 500 -ohm twin-lead |
| 62 | 93 | 13.5 | . 242 | . 25 | . 83 | 2.7 | 5.6 | 9.0 | Low capacity, small |
| 63 | 125 | 10 | . 405 | . 19 | . 61 | 2.0 | 4.0 | 6.3 | Low capacity |
| 64 | 48 | 50 | . 495 | - | - | - | - | - | Pulse |
| 65 | 950 | 44 | . 405 | - | - | - | - | - | Coaxial delay line |
| 71 | 93 | 13.5 | . 250 | . 25 | . 83 | 2.7 | 5.6 | 9.0 | Low capacity, small |
| 77 | 48 | 50 | . 415 | - | - | - | - | - | Pulse |
| 78 | 48 | 50 | . 385 | - | - | - | - | - | Pulse |
| 87A | 50 | 29.5 | . 425 | . 13 | . 52 | 2.0 | 4.4 | 7.6 | Teflon dielectric |
| 88 | 48 | 50 | . 490 | - | - | - | - | - | Pulse |
| 101 | 75 | - | . 588 | - | - | - | - | - |  |
| 102 | 140 | - | 1.088 | - | - | - | - | - |  |
| 108 | 76 | 25 | . 245 | - | - | - | - | - | Twin conductors |
| 114 | 185 | 6.5 | . 405 | - | - | - | - | - | Extra flexible |
| 117 | 50 | 29 | . 730 | . 05 | . 20 | . 85 | 2.0 | 3.6 | Teflon \& Fiberglas |
| 119 | 50 | 29 | . 470 | - | - | - | - | - | Teflon \& Fiberglas |
| 122 | 50 | 29.3 | . 160 | . 40 | 1.70 | 7.0 | 16.5 | 29.0 |  |
| 126 | 50 | 29 | . 290 | 3.20 | 9.0 | 25.0 | 47.0 | 72.0 | Teflon \& Fiberglas |
| 140 | 73 | 21 | . 242 | . 33 | 1.03 | 3.3 | 6.9 | 11.7 | Teflon \& Fiberglas |
| 141 | 50 | 29 | . 195 | . 35 | 1.12 | 3.8 | 8.0 | 13.8 | Teflon \& Fiberglas |
| 142 | 50 | 29 | . 206 | . 35 | 1.12 | 3.8 | 8.0 | 13.8 | Teflon \& Fiberglas |
| 143 | 50 | 29 | . 325 | . 24 | . 77 | 2.5 | 5.3 | 9.0 | Teflon \& Fiberglas |
| 144 | 72 | 21 | . 395 | . 16 | . 53 | 1.8 | 3.9 | 7.0 | Teflon \& Fiberglas |
| 174 | 50 | 30 | . 10 | - | - | - | 19.0 | - | Miniature coaxial |

## 50. TEST-PATTERN INTERPRETATION

The Indian Head test pattern in Fig. 67 is transmitted by many TV stations and is also used in the flying-spot scanner type of video pattern generators. In addition, many of the features of this pattern are incorporated in the individual test patterns of TV stations. The test pattern is a quick and accurate way of checking receiver adjustments and operating conditions.

In the following explanation, the significance of each point indicated by an arrow and letter on the test pattern is


Fig. 67
explained. For example, the letter $A$ indicates the circles at each corner and the two circles in the center of the pattern.
A. The six circles serve as a check for the adjustment of the Height, Width, Vertical Linearity, Horizontal Linearity, and Horizontal Drive controls and the ion-trap magnets, as well as the over-all operation of the vertical, horizontal, and power-supply circuits. All circles should be round and should not overlap the sides of the picture tube by more than three-fourths of an inch.
B. The eight squares along the horizontal axis and the six squares along the vertical axis indicate the standard aspect ratio of $4: 3$. These squares serve as a check for rectangular distortion caused by misadjusted or missing anti-pincushion magnets or by defects in the deflection yoke.
C. The four diagonal lines are used to check interlace. Poor interlace due to improper operation of the verticaloscillator circuit will make the lines appear jagged.
D. The horizontal wedges located at each corner and in the center of the pattern serve as a check of the vertical resolution and interlace. Note the point where the horizontal lines are no longer clear and straight. The breaks in the
center line indicate 50 -line intervals. That is, starting from the left (on the center and left-hand wedges), the first break indicates vertical resolution of 150 lines; the others, 200, 250,300 , and 350 . The first break to the right of the center circles indicates 500 lines, then $450,400,350$, and 300 . The wedges at the top and bottom of the right side of the pattern give the same information except that the wedge is reversed. The numbers ( $20,30,35$, and 45 ) between the vertical and horizontal wedges in each circle indicate these vertical resolution check points, with the last zero omitted.
$E$. The vertical wedges at each corner and at the center of the pattern indicate the horizontal resolution. Hence, they serve as a check on all video-amplifying circuits and alignment. Note the point where the vertical lines are no longer clear. Each break in the center line of the vertical wedge indicates 50 lines, as explained for D . The horizontal resolution can be converted to bandwidth by dividing the number of lines by 80 . For example, if the lines are no longer clear at the 300 -line point, the bandwidth equals 300 divided by 80 , or 3.75 mc .
F. The two diagonal wedges and the Indian head indicate the contrast ratio. Therefore, they can be used to check the adjustment of the Contrast, Brightness, and AGC controls, as well as the video-amplifying and picture-tube circuits. When video-amplifier and picture-tube circuits are operating properly and the controls are properly adjusted, four degrees of shading should be observed, ranging from black at the center to light gray at the outermost point on the wedge.
G. The bull's-eyes at each corner and at the center of the pattern indicate receiver focus. Hence, they serve to check the adjustment of the focusing device or, if electromagnetic focusing is employed, of the low-voltage power supply.
$H$. The eleven horizontal bars represent half cycles of square-wave signals, and are used to check the low-frequency response or phase shift of the receiver. The bars, from top to bottom, represent the following video signals: 19 kc , $28 \mathrm{kc}, 38 \mathrm{kc}, 56 \mathrm{kc}, 75 \mathrm{kc}, 113 \mathrm{kc}, 150 \mathrm{kc}, 225 \mathrm{kc}, 300 \mathrm{kc}$, 450 kc , and 600 kc . If the low-frequency response is satisfactory, the bars will be sharply defined. However, if the receiver has poor low-frequency response due to a defect in the video-amplifier circuit or misadjustment of the Fine

Tuning, Contrast, or AGC controls, the bars will have trailing black or white edges.
I. The single resolution lines at each side of the center circle represent the width of a single line ranging from 50 to 575 lines, in steps of 25 . These lines are used to check for ringing in the video amplifier at frequencies from approximately 600 kc to 7 mc . When ringing occurs at any frequency, the resolution line corresponding to that frequency will be repeated several times at evenly spaced intervals. To convert the resolution lines to the frequency, divide the number of lines by 80 , as explained in the foregoing for $E$.

## 51. CLASSES OF VACUUM-TUBE OPERATION

Class-A amplifiers are biased so that the AC input signal is on the linear portion of their characteristic curve, as shown in Fig. 68.

The output signal is a faithful reproduction of the input signal. The only difference is in the amplification. Plate current flows at all times in a Class-A amplifier. Class-A amplifiers are used in audio or other applications where distortion cannot be tolerated. Their efficiency is around 20 to $25 \%$.


Input Signal Voltage

Class-AB amplifiers are biased as shown in Fig. 69. Here, plate current will flow more than one half but less than a full cycle. Higher plate voltages and currents can be employed than for Class-A amplifiers because the increased negative grid bias will hold the plate current within the plate-dissipation rating. For this reason, more power output can be obtained from Class-AB operation. Class-AB amplifiers may be operated either single-ended or in push-pull.

Class-AB amplifiers are subdivided into two classes, $\mathrm{AB}_{1}$ and $\mathrm{AB}_{2}$. In a Class- $\mathrm{AB}_{1}$ amplifier, no grid current will flow.


Fig. 70


Input Signal Voltage

Fig. 71
That is, the peak signal voltage applied to each grid is never greater than the negative grid bias; therefore, the grid is never driven positive. In a Class-AB 2 amplifier, grid current will flow because the peak signal is greater than the negative grid bias and the grid is driven positive during a portion of the cycle, as shown in Fig. 70. The efficiency of Class-AB amplifiers varies from 40 to $75 \%$, depending on the bias voltage.

Class-B amplifiers are biased at or near cutoff, as shown in Fig. 71. When on exciting grid voltage is applied, plate current is near zero; therefore, it will flow only during approximately half of a cycle. Because plate current flows for only one half the cycle, Class-B amplifiers must be operated in push-pull. More power can be obtained from Class-B amplifiers than from Class-A or Class-AB amplifiers without


Fig. 72
excessive plate dissipation. The efficiency of Class-B amplifiers is around 40 to $60 \%$.

Class-C amplifiers are biased below cutoff, as shown in Fig. 72. Therefore, plate current flows for less than half of a cycle. More power can be obtained from Class-C than Class-B amplifiers. Usually, Class-C amplifiers are used in a selective-tuned circuit, such as those employed in RF amplifiers. The high distortion, characteristic of Class-C amplifiers, is overcome by the flywheel effect of the tuned circuits. The efficiency of Class-C amplifiers is around 50 to $80 \%$.

## 52. MINIATURE LAMP DATA

Table XIX (page 102) lists the most common miniature lamps and their characteristics. The outline drawings for each lamp are given in Fig. 73 below.


B


D





Fig. 73

Table XIX. Miniature Lamp Data

| Lamp No. | Voits | Amps | Bead Color | Base | Bulb Type | Fig. No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PR2 | 2.4 | 0.50 | Blue | Flange | B-31/2 | A |
| PR3 | 3.6 | 0.50 | Green | Flange | B-31/2 | A |
| PR4 | 2.3 | 0.27 | Yellow | Flange | B-31/2 | A |
| PR6 | 2.5 | 0.30 | Brown | Flange | B-31/2 | A |
| PR12 | 5.95 | 0.50 | White | Flange | B-31/2 | A |
| 12 | 6.3 | 0.15 | - - | 2-Pin | G-31/2 | H |
| 13 | 3.8 | 0.30 | Green | Screw | G-31/2 | B |
| 14 | 2.5 | 0.30 | Blue | Screw | G-31/2 | B |
| 40 | 6.3 | 0.15 | Brown | Screw | T-31/4 | C |
| 41 | 2.5 | 0.50 | White | Screw | T-31/4 | C |
| 42 | 3.2 | 0.35* | Green | Screw | T-31/4 | C |
| 43 | 2.5 | 0.50 | White | Bayonet | T-31/4 | D |
| 44 | 6.3 | 0.25 | Blue | Bayonet | T-31/4 | D |
| 45 | 3.2 | $0.35 \dagger$ | Green $\dagger$ | Bayonet | T-31/4 | D |
| 46 | 6.3 | 0.25 | Blue | Screw | T-31/4 $\ddagger$ | C |
| 47 | 6.3 | 0.15 | Brown | Bayonet | T-31/4 | D |
| 48 | 2.0 | 0.06 | Pink | Screw | T-31/4 | C |
| 49 | 2.0 | 0.06 | Pink | Bayonet | T-31/4 | D |
| 50 | 6.3 | 0.20 | White | Screw | G-31/2 | B |
| 51 | 6.3 | 0.20 | White | Bayonep | G-31/2 | E |
| 55 | 6.3 | 0.40 | White | Bayonet | G-41/2 | F |
| 57 | 14.0 | 0.24 | White | Bayonet | G-41/2 | F |
| 112 | 1.1 | 0.22 | Pink | Screw | TL-3 | G |
| 222 | 2.2 | 0.25 | White | Screw | TL-3 | G |
| 233 | 2.3 | 0.27 | Purple | Screw | G-31/2 | B |
| 291 | 2.9 | 0.17 | White | Screw | T-31/4 | C |
| 292 | 2.9 | 0.17 | White | Screw | T-31/4 | C |
| 1490 | 3.2 | 0.16 | White | Bayonet | T-31/4 | D |
| 1891 | 14.0 | 0.23 | Pink | Bayonet | T-31/4 | D |
| 1892 | 14.0 | 0.12 | White | Screw | T-31/4 | C |

* Some brands are .50 amp .
$\dagger$ Some brands are .50 amp and white bead.
$\ddagger$ Frosted.


## 53. GAS-FILLED LAMP DATA

The characteristics of the more common gas-filled lamps are given in Table XX. The value of external resistance needed for operation with circuit voltages from 110 to 600 volts is given in Table XXI.

Table XX. Gas-Filled Lamps

| Number | Hours of Average Useful Life* | Type Gas | Max. Length In inches | Base | Amps | Volts | Watts $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AR-1 | 3,000 | Argon | $31 / 2$ | Medium Screw | 0.018 | 110-125 | 2 |
| AR-3 | 1,000 | Argon | $15 / 8$ | Cand. Screw | 0.0035 | 110-125 | 1/4 |
| AR-4 | 1,000 | Argon | $11 / 2$ | Double-Contact Bayonet | 0.0035 | 110-125 | 1/4 |
| NE-2 | Over 25,000 | Neon | 1 1/16 | Unbased | 0.003 | 110-125 | 1/25 |
| NE-2A | Over 25,000 | Neon | 27/32 $\ddagger$ | Unbased | 0.003 | 110-125 | 1/25 |
| NE-17 | 5,000 | Neon | $11 / 2$ | Double-Contact Bayonet§ | 0.002 | 110-125 | 1/4 |
| NE-30 | 10,000 | Neon | $21 / 4$ | Medium Screw§ | 0.012 | 110-125 | 1 |
| NE-32 | 10,000 | Neon | $21 / 16$ | Double-Contact Bayonet§ | 0.012 | 110-125 | 1 |
| NE-34 | 8,000 | Neon | $31 / 2$ | Medium Screw | 0.018 | 110-125 | 2 |
| NE-40 | 8,000 | Neon | $31 / 2$ | Medium Screw§ | 0.030 | 110-125 | 3 |
| NE-45 | Over 7,500 | Neon | $15 / 8$ | Cand. Screw | 0.002 | 110-125 | 1/4 |
| NE-48 | Over 7,500 | Neon | $11 / 2$ | Double-Contact Bayonet | 0.002 | 110-125 | 1/4 |
| NE-51 | Over 15,000 | Neon | $13 / 16$ | Miniature Bayonet | 0.0003 | 110-125 | 1/25 |
| NE-56 | 10,000 | Neon | $21 / 4$ | Medium Screw§ | 0.005 | 220-250 | 1 |
| NE-57 | 5,000 | Neon | $15 / 8$ | Cand. Screw§ | 0.002 | 110-125 | 1/4 |
| NE-58 | Over 7,500 | Neon | $15 / 8$ | Cand. Screw | 0.002 | 220-250 | 1/2 |

* Life on DC is approximately $60 \%$ of AC values.
$\dagger$ For $110-125 \mathrm{~V}$ operation.
$\ddagger$ The dimension is for glass only.
\& On DC circuits the base should be negative.

Table XXI. External Resistances Needed For Gas-Filled Lamps

| Type | 110-125V | 220-300V | 300-375V | 375-450V | 450-600V |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AR-1 | Included in Base | 10,000 | 18,000 | 24,000 | 30,000 |
| AR-3 | Included in Base | 68,000 | 91,000 | 150,000 | 160,000 |
| AR-4 | 15,000 | 82,000 | 100,000 | 160,000 | 180,000 |
| NE-2 | 200,000 | 750,000 | 1,000,000 | 1,200,000 | 1,600,000 |
| NE-2A | 200,000 | 750,000 | 1,000,000 | 1,200,000 | 1,600,000 |
| NE-17 | 30,000 | 110,000 | 150,000 | 180,000 | 240,000 |
| NE-30 | Included in Base | 10,000 | 20,000 | 24,000 | 36,000 |
| NE-32 | 7.500 | 18,000 | 27,000 | 33,000 | 43,000 |
| NE-34 | Included in Base | 9,100 | 13,000 | 16,000 | 22,000 |
| NE-40 | Included in Base | 6,200 | 8,200 | 11,000 | 16,000 |
| NE-45 | Included in Base | 82,000 | 120,000 | 150,000 | 200,000 |
| NE-48 | 30,000 | 110,000 | 150,000 | 180,000 | 240,000 |
| NE-51 | 200,000 | 750,000 | 1,000,000 | 1,200,000 | 1,600,000 |
| NE-56 | Included in Base |  |  |  |  |
| NE-57 | Included in Base | 82,000 | 120,000 | 150,000 | 200,000 |
| NE-58 | Included in Base |  |  |  |  |

## 54. LIGHT PROPERTIES OF COLOR TV

When we speak of light, we usually think of light coming from the sun or the light emitted from some artificial lighting source, such as electrical lighting. This light is referred to as direct light. Another type of light is indirect or reflected light, which is given off by an object when direct light strikes it. The difference between these two types of light is that the indirect light depends upon the direct light. When light is not shining upon an object, no light will be given off unless the object contains self-luminating properties.

White light is made up of different colors. This composition can be shown by passing light through a prism. The light spectrum is broken up into its constituent wavelengths, each representing a different color. The ability to disperse the light by a prism stems from the fact that light of shorter wavelengths travels slower through glass than does light of longer wavelengths. The spectrum ranges from violet on the lower end to red on the upper end. In between fall blue, green, yellow, and orange. A total of six distinct colors are visible when white light passes through a prism. Since the colors of the spectrum pass gradually from one to the other, the theoretical number of colors becomes infinite.

There are three color attributes used to describe any one color or to differentiate between several colors. These are (1) hue, (2) saturation, and (3) brightness. Hue is the quality used to identify any color under consideration, such as red, blue, or yellow. Saturation is a measure of the absence of dilution by white light, and can be expressed with such terms as rich, deep, vivid, or pure. Brightness defines the amount of light energy contained within a given color.

Color may be produced by either of two processes. When working with paint pigments, the subtractive process is employed. The other process of mixing colors is called the additive process. This process is used in color television. The colors in the additive process do not depend upon an incident light source. Self-luminous properties are characteristic of the additive colors. Phosphorescent signs which glow in the dark are good examples of this process. Cathoderay tubes contain self-luminance properties; so it is only logical that the additive process would be employed in color television.

The three primaries for the additive process of color mixing are red, green, and blue. Two requirements for the primary colors are that each primary must be different and that the combination of any two primaries must not be capable of producing the third. Red, green, and blue were chosen for the additive primaries because they fulfilled these requirements and because it was determined that the greatest number of colors could be produced by the combination of these three colors.


Fig. 74

The three additive primaries used in color television are shown in Fig. 74. From the illustration we can see that by mixing colors in certain proportions, we can obtain the following :

$$
\begin{aligned}
& \text { Red + Green = Yellow } \\
& \text { Red }+ \text { Blue }=\text { Magenta } \\
& \text { Blue }+ \text { Green = Cyan } \\
& \text { Yellow }+ \text { Blue }=\text { White } \\
& \text { Cyan }+ \text { Red }=\text { White } \\
& \text { Magenta }+ \text { Green }=\text { White } \\
& \text { Red }+ \text { Blue }+ \text { Green }=\text { White } \\
& \text { Cyan }+ \text { Magenta }+ \text { Yellow }=\text { White }
\end{aligned}
$$

It is not necessary to overlap the primary colors in the additive process to produce a different color. They may be placed close to each other, and at a certain viewing distance the two colors will blend and produce the new color.

To be compatible, the composite color signal must contain a complete black-and-white signal to which an additional signal is added to convey the color information. The black-and-white signal (also called the luminance signal) carries all the information pertaining to the brightness of the scene being televised, by means of amplitude modulation of the carrier envelope. The other color attributes-hue and satu-ration-are carried by the color signal.

To keep the color signal from interfering with black-and-white reception of the composite color signal, the color information is included within the $4.25-\mathrm{mc}$ video band by an interleaving process. This process is possible because the energy of the luminance signal concentrates at specific intervals in the frequency spectrum. The spaces between these intervals are relatively void of energy, and the energy of the chrominance signal can be caused to concentrate in these spaces.

The color or chrominance signal is conveyed by means of a subcarrier at 3.579 megacycles. This frequency was chosen so that the interleaving process could be accomplished. This chrominance signal is modulated in both phase and amplitude. A change in the phase of this signal represents a change in the hue of the scene, and a change in amplitude
represents a change of color saturation. A color sync signal which keeps the receiver circuits synchronized to the color information is included in the composite signal. This signal is placed on the "back porch" of the horizontal blanking pedestal and is transmitted at a fixed or reference phase. This signal is known as the "color burst" signal.

## 55. RELAY REWINDING DATA

The following nomograph can be used if it is desired to rewind a relay for operation on a different voltage. To calculate the wire size needed for operation on the desired voltage, first lay a straightedge across the points where the present voltage and the desired voltage appear on the first


Fig. 75
two columns, and note the point where the straightedge intersects the ratio column. Then lay the straightedge across this point on the ratio column and the present wire gauge column. Read the wire gauge needed for the desired voltage from the fifth column. Directly opposite this point, the wire diameter (in inches) is also given.

Example-What size wire is needed to rewind a relay wound with No. 23 wire and designed for 12 -volt operation, for operation on 24 volts?

ANSWER: No. 26 ( 0.0159 inch diameter). [First lay the straightedge across 12 in the first column and 24 in the second column. Note the point where the straightedge crosses the third column (.5), and lay the straightedge across this point and across 23 on the fourth column. Read the desired size from the fifth and sixth columns.]

## 56. SPEAKER CONNECTIONS

The following diagrams show the proper connection methods for single- or multiple-speaker operation.
(A) Single Speaker


Fig. 76
(B) Two Speakers in Series


Fig. 77
(C) Speakers in Parallel


Fig. 78
(D) 70.7-Volt Hook-up Using Matching Transformers


Fig. 79

## 57. MACHINE SCREW AND DRILL SIZES

The most common screw sizes and threads, together with the tap and clearance drill sizes, are given in Table XXII. The number listed under the "Type" column is actually a combination of the screw size and the number of threads per inch. For example, a No. 6-32 screw denotes a size No. 6 screw with 32 threads per inch.

Table XXII. Machine Screw and Drill Sizes

| Type | Tap Drill | Clearance Drill | Type | Tap Drill | Clearance Drill |
| :---: | :---: | :---: | :--- | :---: | :---: |
| $1-64$ | 53 | 47 | $10-24$ | 25 | $13 / 64$ |
| $1-72$ | 53 | 47 | $10-32$ | 21 | $13 / 64$ |
| $2-56$ | 50 | 42 | $12-24$ | 16 | $7 / 32$ |
| $2-64$ | 50 | 42 | $12-28$ | 14 | $7 / 32$ |
| $3-48$ | 47 | 36 | $1 / 4-20$ | 7 | $17 / 64$ |
| $3-56$ | 45 | 36 | $1 / 4-28$ | 3 | $17 / 64$ |
| $4-40$ | 43 | 31 | $5 / 16-18$ | $F$ | $21 / 64$ |
| $4-48$ | 42 | 31 | $5 / 16-24$ | 1 | $21 / 64$ |
| $5-40$ | 38 | 29 | $3 / 8-16$ | $5 / 16$ | $25 / 64$ |
| $5-44$ | 37 | 29 | $3 / 8-24$ | $Q$ | $25 / 64$ |
| $6-32$ | 36 | 25 | $7 / 16-14$ | $U$ | $29 / 64$ |
| $6-40$ | 33 | 25 | $7 / 16-20$ | $25 / 64$ | $29 / 64$ |
| $8-32$ | 29 | 16 | $1 / 2-13$ | $27 / 64$ | $33 / 64$ |
| $8-36$ | 29 | 16 | $1 / 2-20$ | $29 / 64$ | $33 / 64$ |



FLAT


BINDING


ROUND


STOVE


OVAL


FILLISTER


HEX


WASHER

PHILLIPS


ALLEN RECESS


BRISTO


CLUTCH

Fig. 80

## 58. TYPES OF SCREW HEADS

The most common types of screw heads are listed and illustrated in Fig. 80 on the preceeding page.

## 59. RESISTANCE OF METALS AND ALLOYS

The resistance for a given length of wire is determined by :

$$
\mathrm{R}=\frac{\mathrm{KL}}{\mathrm{~d}^{2}}
$$

where,
R is the resistance, in ohms, of the length of wire.
K is the resistance, in ohms per circular mil foot, of the material,
L is the length of the wire in feet,
d is the diameter of the wire in mils.
The resistance, in ohms per circular mil foot, of many of the materials used for conductors or heating elements is given in Table XXIII. The resistance shown is for $20^{\circ} \mathrm{C}$ ( $68^{\circ} \mathrm{F}$ ).

Table XXIII. Resistance of Metals and Alloys

| Material | Symbol | Resistance <br> (ohms per cir. mil foot) |
| :--- | :--- | :--- |
| Nichrome | $\mathrm{Ni}-\mathrm{Fe}-\mathrm{Cr}$ | 675 |
| Nichrome V | Ni Cr | 650 |
| Manganese Nickel | $\mathrm{Ni}-\mathrm{Mu}$ | 85 |
| Pure Nickel | Ni | 60 |
| High Brass | $\mathrm{Cu}-\mathrm{Zn}$ | 50 |
| Commercial Bronze | $\mathrm{Cu}-\mathrm{Zn}$ | 25 |
| Platinum | Pt | 63.8 |
| Iron | Fe | 60.14 |
| Zinc | Zn | 35.58 |
| Molybdenum | Mo | 34.27 |
| Tungsten | W | 33.22 |
| Aluminum | Al | 16.06 |
| Gold | Au | 14.55 |
| Copper | Cu | 10.37 |
| Silver | Ag | 9.796 |

## 60. COPPER WIRE TABLE

Copper wire sizes ranging from American wire gauge (B \& S) 0000 to 40 are listed in Table XXIV (pages 112 and 113). The turns per linear inch, diameter, area in circular mils, current-carrying capacity, feet per pound, and resistance per 1000 feet are included in the table.

Table XXIV. Copper Wire Table

| AWG B \& 5 Gauge | Turns Per Linear Inch |  |  |  | Diameter (Inches) | Circular Mils | Current <br> Carrying Capacity <br> @700 CM <br> Per Amp | Feet Per lb. (Bare) | Ohms Per $1,000 \mathrm{Fr}$. <br> @ 20 ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Enamel | D.C.C. | s.c.c. | Nylon |  |  |  |  |  |
| 0000 | - | - | - | - | . 4600 | 211,600 | 302.3 | 1.561 | 0.04901 |
| 000 | - | - | - | - | . 4096 | 167,800 | 239.7 | 1.968 | 0.06180 |
| 00 | - | - | $\cdots$ | - | . 3648 | 133,100 | 190.1 | 2.482 | 0.07793 |
| 0 | - | $\cdots$ | - | - | . 3249 | 105,500 | 150.7 | 3.130 | 0.09827 |
| 1 | - | 3.3 | 3.3 | - | . 2893 | 83,690 | 119.6 | 3.947 | 0.1239 |
| 2 | - | 3.6 | 3.8 | - | . 2576 | 66,370 | 94.8 | 4.977 | 0.1563 |
| 3 | - | 4.0 | 4.2 | - | . 2294 | 52,640 | 75.2 | 6.276 | 0.1970 |
| 4 | - | 4.5 | 4.7 | - | . 2043 | 41,740 | 59.6 | 7.914 | 0.2485 |
| 5 | - | 5.0 | 5.2 | - | . 1819 | 33,100 | 47.3 | 9.980 | 0.3133 |
| 6 | - | 5.6 | 5.9 | - | . 1620 | 26,250 | 37.5 | 12.58 | 0.3951 |
| 7 | - | 6.2 | 6.5 | - | . 1443 | 20,820 | 29.7 | 15.87 | 0.4982 |
| 8 | 7.6 | 7.1 | 7.4 | - | . 1285 | 16,510 | 23.6 | 20.01 | 0.6282 |
| 9 | 8.6 | 7.8 | 8.2 | - | . 1144 | 13,090 | 18.7 | 25.23 | 0.7921 |
| 10 | 9.6 | 8.9 | 9.3 | - | . 1019 | 10,380 | 14.8 | 31.82 | 0.9989 |
| 11 | 10.7 | 9.8 | 10.3 | - | . 09074 | 8,234 | 11.8 | 40.12 | 1.260 |
| 12 | 12.0 | 10.9 | 11.5 | - | . 08081 | 6,530 | 9.33 | 50.59 | 1.588 |
| 13 | 13.5 | 12.0 | 12.8 | - | . 07196 | 5,178 | 7.40 | 63.80 | 2.003 |
| 14 | 15.0 | 13.8 | 14.2 | 14.9 | . 06408 | 4,107 | 5.87 | 80.44 | 2.525 |
| 15 | 16.8 | 14.7 | 15.8 | - | . 05707 | 3,257 | 4.65 | 101.4 | 3.184 |


| 16 | 18.9 | 16.4 | 17.9 | 18.6 | . 05082 | 2,583 | 3.69 | 127.9 | 4.016 | n m $<$ $<$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 17 | 21.2 | 18.1 | 19.9 | - | . 04526 | 2,048 | 2.93 | 161.3 | 5.064 | $\leq$ |
| 18 | 23.6 | 19.8 | 22.0 | 23.2 | . 04030 | 1,624 | 2.32 | 203.4 | 6.385 | m |
| 19 | 26.4 | 21.8 | 24.4 | - | . 03589 | 1,288 | 1.84 | 256.5 | 8.051 | $\$$ |
| 20 | 29.4 | 23.8 | 27.0 | 28.9 | . 03196 | 1,022 | 1.46 | 323.4 | 10.15 | 2 |
| 21 | 33.1 | 26.0 | 29.8 | - | . 02846 | 810.1 | 1.16 | 407.8 | 12.80 | $\bar{z}$ |
| 22 | 37.0 | 30.0 | 34.1 | 36.0 | . 02535 | 642.4 | . 918 | 514.2 | 16.14 | $\xrightarrow{\square}$ |
| 23 | 41.3 | 31.6 | 37.6 | - | . 02257 | 509.5 | . 728 | 648.4 | 20.36 | $\underset{\sim}{7}$ |
| 24 | 46.3 | 35.6 | 41.5 | 44.7 | . 02010 | 404.0 | . 577 | 817.7 | 25.67 | 2 |
| 25 | 51.7 | 38.6 | 45.6 | - | . 01790 | 320.4 | . 458 | 1,031 | 32.37 | $\cdots$ |
| 26 | 58.0 | 41.8 | 50.2 | 55.7 | . 01594 | 254.1 | . 363 | 1,300 | 40.81 | 2 |
| 27 | 64.9 | 45.0 | 55.0 | - | . 01420 | 201.5 | . 288 | 1,639 | 51.47 | 8 |
| 28 | 72.7 | 48.5 | 60.2 | 69.4 | . 01264 | 159.8 | . 228 | 2,067 | 64.90 | -1 |
| 29 | 81.6 | 51.8 | 65.4 | - | . 01126 | 126.7 | . 181 | 2,607 | 81.83 |  |
| 30 | 90.5 | 55.5 | 71.5 | 86.2 | . 01003 | 100.5 | . 144 | 3,287 | 103.2 |  |
| 31 | 101.0 | 59.2 | 77.5 | - | . 008928 | 79.70 | . 114 | 4,145 | 130.1 |  |
| 32 | 113.0 | 62.6 | 83.6 | 106.0 | . 007950 | 63.21 | . 090 | 5,227 | 164.1 |  |
| 33 | 127.0 | 66.3 | 90.3 | - | . 007080 | 50.13 | . 072 | 6,591 | 206.9 |  |
| 34 | 143.0 | 70.0 | 97.0 | 133.0 | . 006305 | 39.75 | . 057 | 8,310 | 260.9 |  |
| 35 | 158.0 | 73.5 | 104.0 | - | . 005615 | 31.52 | . 045 | 10,480 | 329.0 |  |
| 36 | 175.0 | 77.0 | 111.0 | 167.0 | . 005000 | 25.00 | . 036 | 13,210 | 414.8 |  |
| 37 | 198.0 | 80.3 | 118.0 | - | . 004453 | 19.83 | . 028 | 16,660 | 523.1 |  |
| 38 | 224.0 | 83.6 | 126.0 | 206.0 | . 003965 | 15.72 | . 022 | 21,010 | 659.6 |  |
| 39 | 248.0 | 86.6 | 133.0 | - | . 003531 | 12.47 | . 018 | 26,500 | 831.8 |  |
| 40 | 282.0 | 89.7 | 140.0 | 263.0 | . 003145 | 9.89 | . 014 | 33,410 | 1,049.0 | $\bar{\omega}$ |

## Design Data

## 61. VACUUM-TUBE FORMULAS

The following formulas can be used to calculate the vacuum-tube properties listed.

Amplification factor:

$$
\mu=\frac{\Delta \mathrm{E}_{\mathrm{p}}}{\Delta \mathrm{E}_{\mathrm{g}}}\left(\text { with } \mathrm{I}_{\mathrm{p}} \text { constant }\right)
$$

AC (dynamic) plate resistance:

$$
r_{p}=\frac{\Delta E_{p}}{\Delta I_{p}}\left(\text { with } E_{g} \text { constant }\right)
$$

Mutual conductance (transconductance) :

$$
\mathrm{g}_{\mathrm{m}}=\frac{\Delta \mathrm{I}_{\mathrm{p}}}{\Delta \mathrm{E}_{\mathrm{g}}}\left(\text { with } \mathrm{E}_{\mathrm{p}} \text { constant }\right)
$$

Gain of an amplifier stage:

$$
\text { Gain }=\mu \frac{\mathrm{R}_{\mathrm{L}}}{\mathrm{R}_{\mathrm{L}}+\mathrm{r}_{\mathrm{p}}}
$$

where,
$\mu$ is the amplification factor, $\Delta$ is the variation or change in value, $\mathrm{E}_{\mathrm{p}}$ is the plate voltage in volts, $\mathrm{E}_{\mathrm{g}}$ is the grid voltage in volts, $\mathrm{I}_{\mathrm{p}}$ is the plate current in amperes, $\mathrm{R}_{\mathrm{L}}$ is the plate-load resistance in ohms, $r_{p}$ is the AC plate resistance in ohms, $\mathrm{g}_{\mathrm{m}}$ is the mutual conductance in mhos.

## 62. TRANSISTOR FORMULAS

The following formulas can be used to calculate the transistor properties listed.

Input Resistance:

$$
\mathrm{R}_{\mathrm{i}}=\frac{\Delta \mathrm{V}_{\mathrm{i}}}{\Delta \mathrm{I}_{\mathrm{i}}}
$$

Current Gain :

$$
A_{i}=\frac{\Delta I_{\mathrm{c}}}{\Delta \mathrm{I}_{\mathrm{b}}}\left(\text { with } \mathrm{V}_{\mathrm{c}} \text { constant }\right)
$$

Voltage Gain:

$$
A_{v}=\frac{\Delta V_{\mathrm{e}}}{\Delta \mathbf{V}_{\mathrm{b}}}\left(\text { with } \mathrm{I}_{\mathrm{c}} \text { constant }\right)
$$

Output Resistance:

$$
\mathrm{R}_{0}=\frac{\Delta \mathbf{V}_{0}}{\Delta \mathbf{I}_{\mathrm{o}}}
$$

Power Gain:

$$
\mathbf{A}_{\mathrm{p}}=\frac{\Delta \mathbf{P}_{0}}{\Delta \mathbf{P}_{\mathrm{i}}}
$$

The current gain of the common-base configuration is alpha:

$$
a=\frac{\Delta \mathrm{I}_{\mathrm{c}}}{\Delta \mathrm{I}_{\mathrm{e}}}\left(\text { with } \mathrm{V}_{\mathrm{c}} \text { constant }\right)
$$

The current gain of the common emitter is beta:

$$
\beta=\frac{\Delta \mathrm{I}_{\mathrm{e}}}{\Delta \mathrm{I}_{\mathrm{b}}}\left(\text { with } \mathrm{V}_{\mathrm{e}} \text { constant }\right)
$$

A direct relationship exists between the alpha and beta of a transistor :

$$
a=\frac{\beta}{1+\beta} \quad \beta=\frac{a}{1-a}
$$

where,
$a$ is the current gain of a common-base configuration, $A_{v}$ is the voltage gain,
$A_{1}$ is the current gain,
$A_{p}$ is the power gain,
$\beta$ is the current gain in a common-emitter configuration,
$I_{b}$ is the base current,
$I_{c}$ is the collector current,
$I_{e}$ is the emitter current,
$I_{1}$ is the input current,
$I_{0}$ is the output current,
$P_{1}$ is the input power,
$\mathrm{P}_{\mathrm{o}}$ is the output power,
$R_{1}$ is the input resistance,
$\mathrm{R}_{0}$ is the output resistance,
$\mathrm{V}_{\mathrm{b}}$ is the base voltage,
$\mathrm{V}_{\mathrm{c}}$ is the collector voltage,
$V_{1}$ is the input voltage,
$\mathrm{V}_{0}$ is the output voltage.

## 63. THREE-PHASE POWER FORMULAS

In a three-phase system, there are three voltages, each separated by a phase difference of $120^{\circ}$ : The power-supply input transformers may be connected in either a delta or a Y (star). Fig. 81 shows how the terminals are placed in relationship to the coils. In the delta connection, there is one coil between each pair of terminals; and in the Y connection, there are two. The voltage between two terminals of the Y-connected coil is equal to $\sqrt{3}$ times the voltage across one winding.


Fig. 81
The formulas for determining the voltage across the secondary winding for each of the four possible connections are as follows:
$\Delta$ to Y :

$$
E_{s}=E_{p} \times N \times \sqrt{3}
$$

Y to $\Delta$ :

$$
\mathrm{E}_{\mathrm{s}}=\frac{\mathrm{E}_{\mathrm{p}} \times \mathrm{N}}{\sqrt{3}}
$$

$\Delta$ to $\Delta$ :

$$
\mathrm{E}_{\mathrm{s}}=\mathrm{E}_{\mathrm{p}} \times \mathrm{N}
$$

Y to Y :

$$
\mathrm{E}_{\mathrm{s}}=\mathrm{E}_{\mathrm{p}} \times \mathrm{N}
$$

where,
$\mathrm{E}_{\mathrm{s}}$ is the secondary voltage,
$\mathrm{E}_{\mathrm{p}}$ is the primary voltage, N is the turns ratio.

## 64. COIL WINDINGS

## (A) Single-Layer Coils

The inductance of single-layer coils can be calculated to an accuracy of approximately $1 \%$ with the formula:

$$
\mathrm{L}=\frac{(\mathrm{N} \times \mathrm{A})^{2}}{9 \mathrm{~A}+10 \mathrm{~B}}
$$



Fig. 82

To find the number of turns required for a single-layer coil with a given inductance, the foregoing formula is rearranged as follows:

$$
N=\frac{\sqrt{L(9 A+10 B)}}{A}
$$

where,
L is the inductance in microhenries,
N is the number of turns,
$A$ is the mean radius in inches,
$B$ is the length of the coil in inches.
(B) Multilayer Coils

The inductance of a multilayer coil of rectangular cross section can be computed from the formula:

$$
\mathrm{L}=\frac{0.8(\mathrm{~N} \times \mathrm{A})^{2}}{6 \mathrm{~A}+9 \mathrm{~B}+10 \mathrm{C}}
$$



A
Fig. 83
where,
L is the inductance in microhenries,
N is the number of turns,
$A$ is the mean radius in inches,
$B$ is the length of the coil in inches,
C is the depth of the coil in inches.

## (C) Single-Layer Coil Chart

The chart on the following page provides an easy method for determining either the inductance or the number of turns for single-layer coils. When the length of the winding, the diameter, and the number of turns of the coil are known, the inductance can be found by placing a straightedge from the "Turns" scale to the "Ratio" (diameter $\div$ length) scale and noting the point where the straightedge intersects the "Axis" scale. Then lay the straightedge from the point of intersection of the "Axis" scale to the "Diameter" scale. The point at which this line intersects the "Inductance" scale indicates the inductance (in microhenries) of the coil. The number of turns can be determined by reversing the procedure.

After finding the number of turns, consult the wire table in $\S 60$ to determine the size of wire to be used.

Example-What is the inductance of a single-layer coil having 80 turns wound to 4 inches in length on a coil form 2 inches in diameter?
ANSWER: 130 microhenries. (First lay the straightedge as indicated by the line labeled "Example 1A." Then lay the straightedge as indicated by the line labeled "Example 1B.")

## 65. FILTER FORMULAS

## (A) Constant-k Filters

A constant-k filter presents an impedance match to the line at only one frequency, and a mismatch at all others. The three basic configurations are the $\mathrm{T}, \mathrm{L}$ (half-section), and pi.

A constant-k low-pasis filter will pass frequencies below and attenuate those above a set frequency. Fig. 85 gives the circuit configurations, attenuation characteristics, and impedance characteristics of the three types of constant-k lowpass filters.

The attenuation of the $L$ section is equal to half that of the T or pi sections. The impedance of the filter is equal to

## Single-Layer Coil Chart



Fig. 84
the characteristic impedance of the line ( $\mathrm{Z}_{0}$ ) at zero frequency only. For all other frequencies, the input and output impedance of the filter are equal to $\mathrm{Z}_{\mathrm{I}}$ or $\mathrm{Z}_{\mathrm{I}}^{\prime}$, as shown in Fig. 85.


T-SECTION


L-SECTION


PI-SECTION
Fig. 85
The values for $L_{1}, C_{2}, Z_{o}$, and $f_{c}$ can be computed from the following formulas:

$$
\begin{aligned}
\mathrm{L}_{1} & =\frac{\mathrm{Z}_{0}}{\pi \mathrm{f}_{\mathrm{c}}} \\
\mathrm{C}_{2} & =\frac{1}{\pi \mathrm{f}_{\mathrm{c}} \mathrm{Z}_{\mathrm{o}}} \\
\mathrm{Z}_{\mathrm{o}} & =\sqrt{\frac{\mathrm{L}_{1}}{\mathrm{C}_{2}}} \\
\mathrm{f}_{\mathrm{c}} & =\frac{1}{\pi \sqrt{\mathrm{~L}_{1} \mathrm{C}_{2}}}
\end{aligned}
$$

The values computed for $L_{1}$ and $C_{2}$ must be divided in half, where specified in Fig. 85. That is, the coils in the T


T-SECTION


L-SECTION


PI-SECTION
Fig. 86
and $L$ sections, and the capacitors in the $L$ and pi sections, are equal to one-half the computed value.

A high-pass filter will pass all frequencies above and attenuate all those below a set frequency.

The circuit configurations, attenuation characteristics, and impedance characteristics of constant-k high-pass filltars are given in Fig. 86. The formulas for computing $L_{2}$, $\mathrm{C}_{1}, \mathrm{Z}_{\mathrm{o}}$, and $\mathrm{f}_{\mathrm{c}}$ are as follows:

$$
\begin{aligned}
\mathrm{L}_{2} & =\frac{\mathrm{Z}_{0}}{4 \pi f_{\mathrm{c}}} \\
\mathrm{C}_{1} & =\frac{1}{4 \pi f_{\mathrm{c}} \mathrm{Z}_{o}} \\
\mathrm{Z}_{0} & =\sqrt{\frac{\mathrm{L}_{2}}{\mathrm{C}_{1}}} \\
\mathrm{f}_{\mathrm{c}} & =\frac{1}{4 \pi \sqrt{\mathrm{~L}_{2} \mathrm{C}_{1}}}
\end{aligned}
$$

Notice that the values computed for C in the foregoing formulas must be doubled in the T and L sections. Likewise, the value computed for $L$ must be doubled in the $L$ and $p i$ sections.



Transmission Characteristics

Fig. 87
Bandpass filters will pass frequencies of a certain band and reject all others. The configuration and the transmission characteristics for a constant-k bandpass filter are given in Fig. 87. The formulas for computing the various values are:

$$
\begin{gathered}
L_{1}=\frac{Z_{o}}{\pi\left(f_{2}-f_{1}\right)} \\
L_{2}=\frac{\left(f_{2}-f_{1}\right) Z_{0}}{4 \pi f_{1} f_{2}} \\
C_{1}=\frac{\left(f_{2}-f_{1}\right)}{4 \pi f_{1} f_{2} Z_{o}} \\
C_{2}=\frac{1}{\pi\left(f_{2}-f_{1}\right) Z_{o}} \\
f_{m}=\sqrt{f_{1} f_{2}}=\frac{1}{2 \pi \sqrt{L_{1} C_{1}}=\frac{1}{2 \pi \sqrt{L_{2} C_{2}}}} \\
Z_{0}=\sqrt{\frac{L_{1}}{C_{2}}}=\sqrt{\frac{L_{2}}{C_{1}}}
\end{gathered}
$$

As before, some values must be doubled or halved, as shown in Fig. 87.

A band-rejection filter will reject a certain band of frequencies and pass all others. The configuration and the transmission characteristics of a constant-k band-rejection filter



Transmission Characteristics

Fig. 88
are given in Fig. 88. The formulas for computing the component values, frequencies, and line impedance are:

$$
\begin{aligned}
& \mathrm{L}_{1}=\frac{\left(\mathrm{f}_{2}-\mathrm{f}_{1}\right) \mathrm{Z}_{0}}{\pi \mathrm{f}_{1} \mathrm{f}_{2}} \\
& \mathrm{~L}_{2}=\frac{\mathrm{Z}_{o}}{4 \pi\left(\mathrm{f}_{2}-\mathrm{f}_{1}\right)} \\
& \mathrm{C}_{1}=\frac{1}{4 \pi\left(\mathrm{f}_{2}-\mathrm{f}_{1}\right) \mathrm{Z}_{o}} \\
& \mathrm{C}_{2}=\frac{\left(\mathrm{f}_{2}-\mathrm{f}_{1}\right)}{\pi \mathrm{f}_{1} \mathrm{f}_{2} \mathrm{Z}_{o}} \\
& \mathrm{f}_{\mathrm{m}}=\sqrt{\mathrm{f}_{1} \mathrm{f}_{2}}=\frac{1}{2 \pi \sqrt{\mathrm{~L}_{1} \mathrm{C}_{1}}}=\frac{1}{2 \pi \sqrt{\mathrm{~L}_{2} \mathrm{C}_{2}}} \\
& \mathrm{Z}_{o}=\sqrt{\frac{\mathrm{L}_{1}}{\mathrm{C}_{2}}}=\sqrt{\frac{\mathrm{L}_{2}}{\mathrm{C}_{1}}}
\end{aligned}
$$

where,
$\mathrm{L}_{1}$ and $\mathrm{L}_{2}$ are the inductances of the coils in henries,
$\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ are the capacitances of the capacitors in farads,
$f_{1}$ and $f_{2}$ are the frequencies at the edge of the passband, in cycles per second,
$f_{m}$ is the frequency at the center of the passband, in cycles per second,
$f_{1} \infty$ and $f_{2} \infty$ are the frequencies of infinite attenuation, in cycles per second,
$\mathrm{Z}_{0}$ is the line impedance in ohms.

## (B) M-Derived Filters

In an $m$-derived filter, the designer can control either the impedance or the attenuation characteristics. The values are first computed as for a constant-k filter and then modified by an algebraic expression containing the constant $m$. The


Fig. 89
term $m$ will be a positive number between zero and one, and its value governs the characteristics of the filter.

Two frequencies-the cutoff and the frequency of infinite attenuation-are involved in the design of $m$-derived filters. By selecting the proper value for $m$, it is possible to control the spacing between the two frequencies. Fig. 89 shows the effect which different values of $m$ have on the impedance


Fig. 90
characteristics. Note that the best impedance match is obtained when $m$ is equal to 0.6 ; hence this value is usually employed.

The attenuation characteristics for the various values of $m$ are given in Fig. 90. The attenuation rises to maximum and then drops on all curves. This graph applies to both lowand high-pass filters.

The value of $m$ is determined from the formulas:

$$
m=\sqrt{1-\left(\frac{f_{c}}{f_{\infty}}\right)^{2}}
$$

or,

$$
m=\sqrt{1-\left(\frac{f_{\infty}}{f_{\mathrm{c}}}\right)^{2}}
$$

Select the formula which will give a positive number.


T-SECTION


L-SECTION


PI-SECTION

Fig. 91
The configurations for $m$-derived filters are classified as either series or shunt. Those for the series $m$-derived lowpass filters are given in Fig. 91. The formulas are as follows:

$$
\begin{aligned}
& \mathbf{L}_{1}=m\left(\frac{\mathbf{Z}_{.,}}{2 \pi f_{4}}\right) \\
& \mathbf{L}_{2}=\left(\frac{1-m^{2}}{4 m}\right)\left(\frac{\mathbf{Z}_{b}}{2 \pi f_{c}}\right) \\
& \mathrm{C}_{2}=m\left(\frac{1}{\pi f_{\mathrm{c}} \mathbf{Z}_{0}}\right)
\end{aligned}
$$

For a series $m$-derived high-pass filter (Fig. 92), the formulas are:

$$
\mathrm{L}_{2}=\frac{\left(\frac{\mathbf{Z}_{o}}{4 \pi \mathbf{f}_{s}}\right)}{m}
$$

$$
\begin{aligned}
& \mathrm{C}_{1}=\frac{\left(\frac{1}{4 \pi \mathrm{f}_{\mathrm{r}} \mathrm{Z}_{\mathrm{o}}}\right)}{m} \\
& \mathrm{C}_{2}=\left(\frac{4 m}{1-m^{2}}\right)\left(\frac{1}{4 \pi \mathrm{f}_{\mathrm{c}} \mathrm{Z}_{\mathrm{o}}}\right)
\end{aligned}
$$



T-SECTION


L-SECTION

Fig. 92


Fig. 93
The configurations for shunt $m$-derived low-pass filters are given in Fig. 93. The formulas for computing the component values are:

$$
\begin{aligned}
& \mathrm{L}_{1}=m\left(\frac{\mathrm{Z}_{0}}{\pi \mathrm{f}_{\mathrm{c}}}\right) \\
& \mathrm{C}_{1}=\left(\frac{1-m^{2}}{4 m}\right)\left(\frac{1}{\pi \mathrm{f}_{\mathrm{c}} \mathbf{Z}_{\circ}}\right) \\
& \mathrm{C}_{2}=m\left(\frac{1}{\pi \mathrm{f}_{\mathrm{c}} \mathrm{Z}_{\mathrm{o}}}\right)
\end{aligned}
$$



Fig. 94
For shunt $m$-derived high-pass filters (Fig. 94), the formulas are:

$$
\begin{aligned}
& \mathbf{L}_{1}=\left(\frac{4 m}{1-m^{2}}\right)\left(\frac{\mathbf{Z}_{0}}{4 \pi \mathrm{f}_{\mathrm{e}}}\right) \\
& \mathbf{L}_{2}=\frac{\left(\frac{\mathrm{Z}_{0}}{4 \pi \mathrm{f}_{\mathrm{c}}}\right)}{m} \\
& \mathrm{C}_{1}=\frac{\left(\frac{1}{4 \pi f_{\mathrm{k}} \mathrm{Z}_{0}}\right)}{m}
\end{aligned}
$$

where,
$\mathrm{L}_{1}$ and $\mathrm{L}_{2}$ are the inductances of the coils in henries, $\mathrm{C}_{1}$ and $\mathrm{C}_{2}$ are the capacitances of the capacitors in farads, $m$ is a constant between 0 and 1 ,
$\mathrm{Z}_{0}$ is the line impedance in ohms, $\mathrm{f}_{\mathrm{c}}$ is the cutoff frequency in cycles per second.

## 66. ATTENUATOR FORMULAS

## (A) General

An attenuator is an arrangement of noninductive resistors used in an electrical circuit to reduce the audio- or radiosignal strength without introducing distortion. The resistors may be fixed or variable. Attenuators can be designed to
work between equal or unequal impedances; hence, they are often used as impedance-matching networks.

Any attenuator working between unequal impedances must introduce a certain minimum loss. These values are given in the graph of Fig. 95. The impedance ratio is the input impedance divided by the output impedance, or vice versa-whichever gives a value of more than one.

A factor is used in the calculation of resistor values in attenuator networks. Called K , it is the ratio of current, voltage, or power corresponding to a given value of attenuation in decibels. Table XXV gives the value of " $K$ " for the more common loss values.


Fig. 95
The four steps in the design of a pad are: (1) Determine the type of network required. (2) If impedances are unequal, calculate the ratio of input to output impedance (or output to input impedance) and refer to Fig. 95 for the minimum loss value. (3) From Table XXV find the value of K for the desired loss. (4) Calculate the resistor values, using the following formulas.

Table XXV. K Factors for Calculating Attenuator Loss

| db | K | db | K | db | K | db | K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| . 05 | 1.0058 | 9.5 | 2.9854 | 29.0 | 28.184 | 49.0 | 281.84 |
| . 1 | 1.0116 | 10.0 | 3.1623 | 30.0 | 31.623 | 50.0 | 316.23 |
| . 5 | 1.0593 | 11.0 | 3.5481 | 31.0 | 35.481 | 51.0 | 354.81 |
| 1.0 | 1.1220 | 12.0 | 3.9811 | 32.0 | 39.811 | 52.0 | 398.11 |
| 1.5 | 1.1885 | 13.0 | 4.4668 | 33.0 | 44.668 | 54.0 | 501.19 |
| 2.0 | 1.2589 | 14.0 | 5.0119 | 34.0 | 50.119 | 55.0 | 562.34 |
| 2.5 | 1.3335 | 15.0 | 5.6234 | 35.0 | 56.234 | 56.0 | 630.96 |
| 3.0 | 1.4125 | 16.0 | 6.3096 | 36.0 | 63.096 | 57.0 | 707.95 |
| 3.5 | 1.4962 | 17.0 | 7.0795 | 37.0 | 70.795 | 58.0 | 794.33 |
| 4.0 | 1.5849 | 18.0 | 7.9433 | 38.0 | 79.433 | 60.0 | 1000.0 |
| 4.5 | 1.6788 | 19.0 | 8.9125 | 39.0 | 89.125 | 65.0 | 1778.3 |
| 5.0 | 1.7783 | 20.0 | 10.0000 | 40.0 | 100.000 | 70.0 | 3162.3 |
| 5.5 | 1.8837 | 21.0 | 11.2202 | 41.0 | 112.202 | 75.0 | 5623.4 |
| 6.0 | 1.9953 | 22.0 | 12.589 | 42.0 | 125.89 | 80.0 | 10,000 |
| 6.5 | 2.1135 | 23.0 | 14.125 | 43.0 | 141.25 | 85.0 | 17,783 |
| 7.0 | 2.2387 | 24.0 | 15.849 | 44.0 | 158.49 | 90.0 | 31,623 |
| 7.5 | 2.3714 | 25.0 | 17.783 | 45.0 | 177.83 | 95.0 | 56,234 |
| 8.0 | 2.5119 | 26.0 | 19.953 | 46.0 | 199.53 | 100.0 | $10^{6}$ |
| 8.5 | 2.6607 | 27.0 | 22.387 | 47.0 | 223.87 |  |  |
| 9.0 | 2.8184 | 28.0 | 25.119 | 48.0 | 251.19 |  |  |

(B) Combining or Dividing Network
$\mathrm{R}_{\mathrm{B}}=\left(\frac{\mathrm{N}-1}{\mathrm{~N}+1}\right) \mathrm{Z}$


Fig. 96
where,
$\mathrm{R}_{\mathrm{B}}$ is the resistance of the building-out resistors in ohms, N is the number of circuits fed by the source impedance, Z is the source impedance in ohms.
(C) T-Type Attenuator (Between Equal Impedances)

$$
\begin{aligned}
\mathrm{R}_{1} \text { and } \mathrm{R}_{2} & =\left(\frac{\mathrm{K}-1}{\mathrm{~K}+1}\right) \mathrm{Z} \\
\mathrm{R}_{3} & =\left(\frac{\mathrm{K}}{\mathrm{~K}^{2}-1}\right) 2 \mathrm{Z}
\end{aligned}
$$



Fig. 97

## (D) H -Type Attenuator (Balanced-T Attenuator)

Calculate the values for $R_{1}$, $R_{2}$, and $R_{3}$ as for an unbalanced T-attenuator (Fig. 97). Then halve the values of $\mathrm{R}_{1}$ and $R_{2}$, as shown in Fig. 98. The tap on $R_{3}$ is exactly in the center.


Fig. 98
(E) Taper Pad (T-Type Attenuator Between Unequal Impedances)

$$
\begin{aligned}
& \mathrm{R}_{1}=\mathrm{Z}_{1}\left(\frac{\mathrm{~K}^{2}+1}{\mathrm{~K}^{2}-1}\right)-2 \sqrt{\mathrm{Z}_{1} \mathrm{Z}_{2}}\left(\frac{\mathrm{~K}}{\mathrm{~K}^{2}-1}\right) \\
& \mathrm{R}_{2}=\mathrm{Z}_{2}\left(\frac{\mathrm{~K}^{2}+1}{\mathrm{~K}^{2}-1}\right)-2 \sqrt{\mathrm{Z}_{1} \mathrm{Z}_{2}}\left(\frac{\mathrm{~K}}{\mathrm{~K}^{2}-1}\right) \quad \mathrm{Z}_{1} \rightarrow \\
& R_{3}=2 \sqrt{Z_{1} Z_{2}}\left(\frac{K}{K^{2}-1}\right)
\end{aligned}
$$

where,
$\mathrm{Z}_{1}$ is the larger impedance.
(F) Bridged-T Attenuator (Unbalanced)
$\mathrm{R}_{1}=\mathrm{Z}$
$\mathrm{R}_{5}=(\mathrm{K}-1) \mathrm{Z}$
$\mathrm{R}_{6}=\left(\frac{1}{\mathrm{~K}-1}\right) \mathrm{Z}$


Fig. 100
$R_{5}$ and $R_{6}$ are connected to a common shaft, and each varies inversely in value with respect to the other.

## (G) Balanced Bridged-T Attenuator

Calculate the values for $R_{1}, R_{5}$, and $R_{6}$ as for an unbalanced bridged-T attenuator (Fig. 100). Then halve the values as shown in Fig. 101.


Fig. 101

## (H) L-Type Attenuators

An L-type attenuator can supply an impedance match in only one direction. If the impedances it works out of and into are unequal, it can be made to match either-but not both-impedances. The arrows in the following illustrations indicate the direction of impedance match.

Between equal impedances and with the impedance match in the direction of the series arm:

$$
\begin{aligned}
& \mathrm{R}_{1}=\mathrm{Z}\left(\frac{\mathrm{~K}-1}{\mathrm{~K}}\right) \\
& \mathrm{R}_{2}=\mathrm{Z}\left(\frac{1}{\mathrm{~K}-1}\right)
\end{aligned}
$$



Fig. 102

Between equal impedances and with the impedance match in the direction of the shunt arm:

$$
\begin{aligned}
& \mathrm{R}_{1}=\mathrm{Z}(\mathrm{~K}-1) \\
& \mathrm{R}_{2}=\mathrm{Z}\left(\frac{\mathrm{~K}}{\mathrm{~K}-1}\right)
\end{aligned}
$$



Fig. 103

Between unequal impedances and with the impedance match toward the larger value:

$$
\begin{aligned}
& \mathrm{R}_{1}=\left(\frac{\mathrm{Z}_{1}}{\mathrm{~S}}\right)\left(\frac{\mathrm{KS}-1}{\mathrm{~K}}\right) \\
& \mathrm{R}_{2}=\left(\frac{\mathrm{Z}_{1}}{\mathrm{~S}}\right)\left(\frac{1}{\mathrm{~K}-\mathrm{S}}\right)
\end{aligned}
$$

where,

$$
\mathrm{S}=\sqrt{\frac{\mathrm{Z}_{1}}{\mathrm{Z}_{2}}}
$$



Fig. 104

Between unequal impedances and with the impedance match toward the smaller value:

$$
\begin{aligned}
& \mathrm{R}_{1}=\left(\frac{\mathrm{Z}_{1}}{\mathrm{~S}}\right)(\mathrm{K}-\mathrm{S}) \\
& \mathrm{R}_{2}=\left(\frac{\mathrm{Z}_{1}}{\mathrm{~S}}\right)\left(\frac{\mathrm{K}}{\mathrm{KS}-1}\right)
\end{aligned}
$$

where,

$$
S \text { equals } \sqrt{\frac{Z_{1}}{Z_{2}}}
$$



Fig. 105
(I) Pi-Type Attenuator (Between Equal Impedances)

$$
\begin{aligned}
& \mathrm{R}_{\mathrm{L}}=\mathrm{Z}\left(\frac{\mathrm{~K}+1}{\mathrm{~K}-1}\right) \\
& \mathrm{R}_{2}=\left(\frac{\mathrm{Z}}{2}\right)\left(\frac{\mathrm{K}^{2}-1}{\mathrm{~K}}\right)
\end{aligned}
$$



Fig. 106
(J) Pi-Type Attenuator (Between Unequal Impedances)

$$
\begin{aligned}
& \mathrm{R}_{1}=\mathrm{Z}_{1}\left(\frac{\mathrm{~K}^{2}-1}{\mathrm{~K}^{2}-2 \mathrm{KS}+1}\right) \\
& \mathrm{R}_{2}=\left(\frac{\sqrt{\mathrm{Z}_{1} \mathrm{Z}_{2}}}{2}\right)\left(\frac{\mathrm{K}^{2}-1}{\mathrm{~K}}\right) \\
& \mathrm{R}_{3}=\mathrm{Z}_{2}\left(\frac{\mathrm{~K}^{2}-1}{\mathrm{~K}_{2}-2 \frac{\mathrm{~K}}{\mathrm{~S}}+1}\right)
\end{aligned}
$$

where,


Fig. 107

S equals $\sqrt{\frac{\mathrm{Z}_{1}}{\mathrm{Z}_{2}}}$

## e Attenuators

culate the values for a pi-type attenuator (Figs. 106 and 107), then halve the values for the series resistors as shown in Figs. 108 (balanced) and 109 (unbalanced).


Fig. 108


Fig. 109

## (L) U-Type Attenuator

For impedance match in the direction of the series arms:

$$
\begin{aligned}
& \mathrm{R}_{1}=\left(\frac{\mathrm{Z}_{1}}{2 \mathrm{~S}}\right)\left(\frac{\mathrm{KS}-1}{\mathrm{~K}}\right) \\
& \mathrm{R}_{2}=\left(\frac{\mathrm{Z}_{1}}{\mathrm{~S}}\right)\left(\frac{1}{\mathrm{~K}-\mathrm{S}}\right)
\end{aligned}
$$



Fig. 110

For impedance match in the direction of the shunt arm:

$$
\begin{aligned}
& \mathrm{R}_{1}=\left(\frac{\mathrm{Z}_{1}}{2 \mathrm{~S}}\right)(\mathrm{K}-\mathrm{S}) \\
& \mathrm{R}_{2}=\left(\frac{\mathrm{Z}_{1}}{\mathrm{~S}}\right)\left(\frac{\mathrm{K}}{\mathrm{KS}-1}\right)
\end{aligned}
$$



Fig. 111
where,
The arrows indicate the direction of the impedance match,
S equals $\sqrt{\frac{\mathrm{Z}_{1}}{\mathrm{Z}_{2}}}$
(M) Lattice-Type Attenuator

$$
\begin{aligned}
& \mathrm{R}_{1}=\left(\frac{\mathrm{K}-1}{\mathrm{~K}+1}\right) \mathrm{Z} \\
& \mathrm{R}_{2}=\left(\frac{\mathrm{K}+1}{\mathrm{~K}-1}\right) \mathrm{Z}
\end{aligned}
$$



Fig. 112
(N) Ladder-Type Attenuator


Fig. 113
$\mathrm{R}_{1}=\left(\frac{\mathrm{K}^{2}-1}{2 \mathrm{~K}}\right) \mathrm{Z}$
$\mathrm{R}_{2}=\left(\frac{\mathrm{K}+1}{\mathrm{~K}-1}\right) \mathrm{Z}$
$\mathrm{R}_{3}=\frac{\mathrm{R}_{2} \times \mathrm{Z}}{\mathrm{R}_{2}+\mathrm{Z}}$
$R_{4}=\frac{Z}{2}$
$\mathrm{Z}_{\mathrm{in}}=\mathrm{Z}_{\text {ont }}$
where,
K depends on the loss per step-not on the total loss.

## Mathematical Tables and

## Formulas

$$
\begin{array}{rlrl}
\text { 67. MATHEMATICAL CONSTANTS } \\
\pi & =3.1416 & (2 \pi)^{2} & =39.4786 \\
\pi^{2} & =9.8696 & 4 \pi & =12.5664 \\
\pi^{3} & =31.0063 & \frac{\pi}{2} & =1.5708 \\
\frac{1}{\pi} & =0.3183 & \frac{\sqrt{\pi}}{2} & =1.2533 \\
\frac{1}{\pi^{2}} & =0.1013 & \sqrt{2} & =1.4142 \\
\frac{1}{\pi^{3}} & =0.0323 & \sqrt{3} & =1.7321 \\
\sqrt{\pi} & =1.7725 & \frac{1}{\sqrt{2}} & =0.7071 \\
\frac{1}{\sqrt{\pi}} & =0.5642 & \frac{1}{\sqrt{3}} & =0.5773 \\
\frac{1}{2 \pi} & =0.1592 & \log \pi & =0.4971 \\
\left(\frac{1}{2 \pi}\right)^{2} & =0.0253 & \log \pi^{2} & =0.9943 \\
2 \pi & =6.2832 & \log \sqrt{\pi} & =0.2486 \\
& \log \frac{\pi}{2} & =0.1961
\end{array}
$$

## 68. MATHEMATICAL SYMBOLS

$\times$ or $\cdot \quad$ Multiplied by. $\quad+$ Positive, add, and plus.
$\div$ Divided by.
$=$ Equals.
$\neq$ Does not equal.

- Negative, subtract, and minus.
$>$ Is greater than.
$<$ Is less than.
$\pm$ Plus or minus.
$\equiv$ Identical with.
$\therefore$ Therefore.
|| Parallel to.
$\angle$ Angle.
\& Is much less than.
$\Rightarrow$ Is much greater than.
$\geqq$ Equal to or greater than.
$\leqq$ Equal to or less than.
$\perp$ Perpendicular to.
$|n| \quad$ Absolute value of $n$.
$\cong$ Is approximately equal to.

Square root.

## 69. DECIMAL EQUIVALENTS OF FRACTIONS

The decimal equivalents to four places of fractions by 64ths are given in Table XXVI.

Table XXVI. Decimal Equivalents of Fractions

| Fraction |  |  |  | Decimal | Fraction |  |  |  | Decimal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1/64 | 1/32 | 1/16 | 1/8 | $\begin{aligned} & 0.0156 \\ & 0.0313 \end{aligned}$ | 33/64 | 17/32 | 9/16 | 5/8 | 0.5156 |
|  |  |  |  |  |  |  |  |  | 0.5313 |
| 3/64 |  |  |  | 0.0469 | 35/64 |  |  |  | 0.5469 |
|  |  |  |  | 0.0625 |  |  |  |  | 0.5625 |
| 5/64 | 3/32 |  |  | 0.0781 | 37/64 | 19/32 |  |  | 0.5781 |
|  |  |  |  | 0.0938 |  |  |  |  | 0.5938 |
| 7/64 |  |  |  | 0.1094 | 39/64 |  |  |  | 0.6094 |
|  |  |  |  | 0.1250 |  |  |  |  | 0.6250 |
| 9/64 | 5/32 | 3/16 |  | 0.1406 | 41/64 | 21/32 | 11/16 |  | 0.6406 |
|  |  |  |  | 0.1563 |  |  |  |  | 0.6563 |
| 11/64 |  |  |  | 0.1719 | 43/64 |  |  |  | 0.6719 |
|  |  |  |  | 0.1875 |  |  |  |  | 0.6875 |
| 13/64 | 7/32 |  |  | 0.2031 | 45/64 |  |  |  | 0.7031 |
| 15/64 |  |  |  | 0.2188 |  | 23/32 |  |  | 0.7188 |
|  |  |  |  | 0.2344 | 47/64 |  |  |  | 0.7344 |
|  |  |  | 1/4 | 0.2500 |  |  |  | 3/4 | 0.7500 |
| 17/64 | 9/32 | 5/16 | 3/8 | 0.2656 | 49/64 | 25/32 | 13/16 |  | 0.7656 |
| 19/64 |  |  |  | 0.2813 |  |  |  |  | 0.7813 |
|  |  |  |  | 0.2969 | 51/64 |  |  |  | 0.7969 |
|  |  |  |  | 0.3125 |  |  |  |  | 0.8125 |
| 21/64 | 11/32 |  |  | 0.3281 | 53/64 | 27/32 |  |  | 0.8281 |
|  |  |  |  | 0.3438 |  |  |  |  | 0.8438 |
| 23/64 |  |  |  | 0.3594 | 55/64 |  |  |  | 0.8594 |
|  |  |  |  | 0.3750 |  |  |  | 7/8 | 0.8750 |
| 25/64 | 13/32 | 7/16 |  | 0.3906 | 57/64 | 29/32 | 15/16 |  | 0.8906 |
|  |  |  |  | 0.4063 | 59/64 |  |  |  | 0.9063 |
| 27/64 |  |  |  | 0.4219 |  |  |  |  | 0.9219 |
|  |  |  |  | 0.4375 | 61/64 |  |  |  | 0.9375 |
| 29/64 | 15/32 |  |  | 0.4531 |  |  |  |  | 0.9531 |
| 31/64 |  |  |  | 0.4688 | 63/64 | 31/32 |  |  | 0.9688 |
|  |  |  |  | 0.4844 |  |  |  |  | 0.9844 |
|  |  |  | 1/2 | 0.5000 |  |  |  | 1 | 1.0000 |

## 70. POWERS OF TEN

## (A) Exponent Determination

Large numbers can be simplified by using powers of ten. For example, some of the multiples of ten from 1 to $1,000,000$, with their equivalents in powers of ten are:

$$
\begin{aligned}
1 & =10^{0 *} \\
10 & =10^{1} \\
100 & =10^{2} \\
1000 & =10^{3} \\
10,000 & =10^{4} \\
100,000 & =10^{5} \\
1,000,000 & =10^{6}
\end{aligned}
$$

Likewise, powers of ten can be used to simplify decimal expressions. Some of the submultiples of ten from 0.1 to 0.000001 , with their equivalents in powers of ten are:

$$
\begin{aligned}
0.1 & =10^{-1} \\
0.01 & =10^{-2} \\
0.001 & =10^{-3} \\
0.0001 & =10^{-4} \\
0.00001 & =10^{-5} \\
0.000001 & =10^{-6}
\end{aligned}
$$

Any whole number can be expressed as a smaller whole number, and any decimal can be expressed as a whole number, by moving the decimal point to the left or right and expressing the number as a power of ten. If the decimal point is moved to the left, the power is positive and is equal to the number of places the decimal point was moved. If the decimal point is moved to the right, the power is negative and is equal to the number of places the decimal point was moved.

For example:

$$
\begin{aligned}
123 & =1.23 \times 10^{2} \\
456.7 & =4.567 \times 10^{2} \\
78,900 & =78.9 \times 10^{3} \\
0.00012 & =1.2 \times 10^{-4} \\
0.0345 & =34.5 \times 10^{-3} \\
.678 & =67.8 \times 10^{-2}
\end{aligned}
$$

[^7]
## (B) Addition and Subtraction

To add or subtract using powers of ten, first convert all numbers to the same power of ten. The numbers can then be added or subtracted, and the answer will be in the same power of ten. For example:

$$
\begin{aligned}
& 9.32 \times 10^{2}+17.63 \times 10^{3}+297=? \\
& 9.32 \times 10^{2}=0.932 \times 10^{3} \\
& 17.63 \times 10^{3}= 17.630 \times 10^{3} \\
& 297=\frac{0.297 \times 10^{3}}{18.859 \times 10^{3}}=18,859 \\
& 18.47 \times 10^{2}-1.59 \times 10^{3}=? \\
& 18.47 \times 10^{2}= 1.847 \times 10^{3} \\
& 1.59 \times 10^{3}= \frac{1.590 \times 10^{3}}{.257 \times 10^{3}}=257
\end{aligned}
$$

## (C) Multiplication

To multiply using powers of ten, add the exponents. Thus:

$$
\begin{aligned}
1000 \times 3721 & =10^{3} \times 37.21 \times 10^{2} \\
& =37.21 \times 10^{3+2} \\
& =37.21 \times 10^{5} \\
& =3,721,000 \\
225 \times .00723 & =2.25 \times 10^{2} \times 7.23 \times 10^{-3} \\
& =2.25 \times 7.23 \times 10^{2+(-3)} \\
& =2.25 \times 7.23 \times 10^{-1} \\
& =16.2675 \times 10^{-1} \\
& =1.62675
\end{aligned}
$$

(D) Division

To divide using powers of ten, subtract the exponent of the denominator from the exponent of the numerator. Thus:

$$
\begin{aligned}
\frac{10^{5}}{10^{3}} & =10^{5-3} \\
& =10^{2} \\
& =100
\end{aligned}
$$

$$
\begin{aligned}
\frac{72,600}{.002} & =\frac{72.6 \times 10^{3}}{2 \times 10^{-3}} \\
& =\frac{72.6 \times 10^{3+3}}{2} \\
& =36.3 \times 10^{6} \\
& =36,300,000
\end{aligned}
$$

(E) Combination Multiplication and Division

Problems involving a combination of multiplication and division can be solved using powers of ten by multiplying and dividing, as called for, until the problem is completed. For example:

$$
\begin{aligned}
\frac{3900 \times .007 \times 420}{142,000 \times .00005} & =\frac{3.9 \times 10^{3} \times 7 \times 10^{-3} \times 4.2 \times 10^{2}}{1.42 \times 10^{5} \times 5 \times 10^{-5}} \\
& =\frac{3.9 \times 7 \times 4.2 \times 10^{2}}{1.42 \times 5} \\
& =\frac{114.66 \times 10^{2}}{7.1} \\
& =16.1493 \times 10^{2} \\
& =1614.93
\end{aligned}
$$

## (F) Reciprocal

To take the reciprocal of a number using powers of ten, first (if necessary) state the number so the decimal point precedes the first significant figure of the number. Then divide this number into 1 . The power of 10 in the answer will be the same value as in the original number, but will have the opposite sign. For example:

$$
\begin{aligned}
& \text { Reciprocal of } \begin{aligned}
& 400=\frac{1}{400} \\
& \begin{aligned}
\frac{1}{400} & =\frac{1}{.4 \times 10^{3}} \\
& =2.5 \times 10^{-3} \\
& =.0025
\end{aligned}
\end{aligned}=\text {. }
\end{aligned}
$$

$$
\text { Reciprocal of } .0025=\frac{1}{.0025}
$$

$$
\frac{1}{.0025}=\frac{1}{.25 \times 10^{-2}}
$$

$$
=4 \times 10^{2}
$$

$$
=400
$$

## (G) Square and Square Root

To square a number using powers of ten, multiply the number by itself, and double the exponent. Thus:

$$
\begin{aligned}
\left(7 \times 10^{3}\right)^{2} & =49 \times 10^{6} \\
& =49,000,000 \\
\left(9.2 \times 10^{-4}\right)^{2} & =84.64 \times 10^{-8} \\
& =.0000008464
\end{aligned}
$$

To extract the square root of a number using powers of ten, do the opposite. (If the number is an odd power of 10 , first convert it to an even power of ten.) Extract the square root of the number, and divide the power of ten by 2 . Thus:

$$
\begin{aligned}
\sqrt{36 \times 10^{10}} & =6 \times 10^{5} \\
& =600,000 \\
\sqrt{5.72 \times 10^{3}} & =\sqrt{57.2 \times 10^{2}} \\
& =7.56 \times 10 \\
& =75.6
\end{aligned}
$$

## 71. OPERATION OF THE SLIDE RULE

The slide rule (Fig. 114) is an instrument designed to perform mathematical calculations with a high degree of accuracy. For example, the common 10 -inch slide rule has an accuracy of one-tenth of one per cent. Operations such as multiplication, division, extraction of square and cube roots, and finding trigonometric functions such as sine, cosine, and tangent can all be performed on the slide rule.

There are six scales on the front of the slide rule. The letter $A$, in the upper left-hand corner of the body, denotes the $A$ scale. On the left side of the slide, the letters $B, C I$, and $C$ denote their respective scales. The letters $D$ and $K$, at the lower left corner of the body, indicate these scales.


Fig. 114


Fig. 115
The number 1 on the left end of the slide is called the left index, and the number 1 on the right end is the right index.

The $C$ and $D$ scales, which are identical, are used for multiplication and division. As a sample problem in multiplication, let us multiply 136 by 27 . First place the left index of the slide on 136 on the $D$ scale. Then slide the runner to 27 on the $C$ scale, and read your answer (3672) on the $D$ scale, as shown in Fig. 115.

Notice that the slide rule is accurate to three places, as illustrated by the sample problem. The fourth number can be estimated close enough for practical purposes.

As a sample problem in division, let us divide 390 by 0.7 . Place the runner on 390 on the $D$ scale; then push the slide to the left until 7 on the $C$ scale is over the 390 , as shown in Fig. 116. Finally, place the runner at the right index, and read the answer (557) on the $D$ scale.

The $C I$, or reciprocal, scale is the same as the $C$ scale except its numbers increase from right to left. Hence, any number on the $C I$ scale is the reciprocal of the number directly below it on the $C$ scale. The $C I$ scale can be used with


Fig. 116
the $C$ and $D$ scales for multiplication and division, including problems involving several multiplication and division operations in sequence.

As a sample problem in multiplication, take $26 \times 32 \times 6$. Place the left index of the slide on 26 of the $D$ scale. Then slide the runner to 32 on the $C$ scale, as shown in Fig. 117. Multiplying by 6 is the same as dividing by the reciprocal of 6 . To do this, place the 6 on the $C I$ scale under the hairline of the runner (Fig. 118), and read the answer (4992) under the left index.


Fig. 117


Fig. 118

The $A$ and $B$ scales, which are identical, are located on the upper portion of the body and slide. The $A$ and/or $B$ scales are used with the $C$ and/or $D$ scales for finding the square or square root of a number.

Example problem: Find the square root of 625 . First place the runner at 625 on the $A$ scale. Then read the answer (25) on the $D$ scale (Fig. 119).

The slide rule can be used for finding the square root of the sum of two squares, as you might wish to do if you were


Fig. 119


Fig. 120
solving a right triangle. For example, if the two sides of a right triangle are 3 and 5 , find the hypotenuse in the following manner:

Divide the 5 by the 3 , by placing 3 on the $C$ scale opposite 5 on the $D$ scale. Square the quotient by reading 2.78 on the $A$ scale opposite the left index of the $B$ scale (Fig. 120). Mentally add 1 to get 3.78, and set the left index of the $B$ scale to 3.78 on the $A$ scale. Extract the square root by going to the $D$ scale and reading 1.945 opposite the $C$ index mark. Without changing the slide, multiply by 3 (the number by which you originally divided) to obtain the answer (5.83) on the $D$ scale (Fig. 121).

The $K$ scale is used with the $D$ scale for finding the cube and cube root. Each number on the $K$ scale is equal to the cube of the number above it on the $D$ scale. Conversely, to extract the cube root of a number, set the runner to this number on the $K$ scale, and read the cube root on the $D$ scale.

The back of the slide is shown in Fig. 122. On it are the sine, $\log$, and tangent scales. The sine scale is at the top and is designated by the letter $S$ on the right side of the


Fig. 121
slide. The $\log$ scale, designated by the letter $L$, is in the middle; and the tangent scale, designated by the letter $T$, is at the bottom.

The "inch" and "centimeter" scales on the rule are only a convenience-they are not used in any slide-rule operations.


Fig. 122

## 72. ALGEBRAIC OPERATIONS

## (A) Transposition of Terms

The following rules apply to the transposition of terms in algebraic equations:

$$
\begin{array}{r}
\text { If } A=\frac{B}{C} \text {, then : } \\
B=A C \\
C=\frac{B}{A} \\
\text { If } \frac{A}{B}=\frac{C}{D}, \text { then }: \\
A=\frac{B C}{D} \\
B=\frac{A D}{C} \\
C=\frac{A D}{B} \\
D=\frac{B C}{A}
\end{array}
$$

$$
\begin{aligned}
& \text { If } \mathrm{A}=\frac{1}{\mathrm{D} \sqrt{\mathrm{BC}}}, \text { then }: \\
& \mathrm{A}^{2}=\frac{1}{\mathrm{D}^{2} \mathrm{BC}} \\
& \mathrm{~B}=\frac{1}{\mathrm{D}^{2} \overline{\mathrm{~A}^{2} \mathrm{C}}} \\
& \mathrm{C}=\frac{1}{\mathrm{D}^{2} \mathrm{~A}^{2} \mathrm{~B}} \\
& \mathrm{D}=\frac{1}{\mathrm{~A} \sqrt{\mathrm{BC}}} \\
& \text { If } \mathrm{A}=\sqrt{\mathrm{B}^{2}+\mathrm{C}^{2}}, \text { then } \\
& \mathrm{A}^{2}=\mathrm{B}^{2}+\mathrm{C}^{2} \\
& \mathrm{~B}=\sqrt{\mathrm{A}^{2}-\mathrm{C}^{2}} \\
& \mathrm{C}=\sqrt{\mathrm{A}^{2}-\mathrm{B}^{2}}
\end{aligned}
$$

## (B) Laws of Exponents

A power of a fraction is equal to that power of the numerator divided by the same power of the denominator.

$$
\left(\frac{a}{b}\right)^{x}=\frac{a^{x}}{b^{x}}
$$

The product of two powers of the same base is also a power of that base; the exponent of the product is equal to the sum of the exponents of the two factors.

$$
\mathrm{a}^{\mathrm{x}} \cdot \mathrm{a}^{y}=\mathrm{a}^{\mathrm{x}+\mathrm{y}}
$$

The quotient of two powers of the same base is also a power of that base; the exponent of the quotient is equal to the numerator exponent minus the denominator exponent.

$$
\frac{a^{x}}{a^{x}}=a^{x-2}
$$

The power of a power of a base is also a power of that base; the exponent of the product is equal to the product of the exponents.

$$
\left(\mathrm{a}^{\mathrm{x}}\right)^{y}=\mathrm{a}^{x y}
$$

A negative exponent of a base is equal to the reciprocal of that base, with a positive exponent numerically equal to the original exponent.

$$
\mathrm{a}^{-\mathrm{x}}=\frac{1}{\mathrm{a}^{\mathrm{x}}}
$$

A fractional exponent indicates that the base should be raised to the power indicated by the numerator of the fraction; the root indicated by the denominator should then be extracted.

$$
a^{\frac{x}{y}}=\sqrt[y]{a^{x}}
$$

A root of a fraction is equal to the identical root of the numerator divided by the identical root of the denominator.

$$
\sqrt[x]{\frac{a}{b}}=\frac{\sqrt[x]{a}}{\sqrt{b}}
$$

A root of a product is equal to the product of the roots of the individual factors.

$$
\sqrt[x]{a b}=\sqrt[x]{a} \times \sqrt[x]{b}
$$

(C) Quadratic Equation

The general quadratic equation:

$$
a x^{2}+b x+c=0
$$

may be solved by:

$$
x=\frac{-b \pm \sqrt{b^{2}-4 a c}}{2 a}
$$

## 73. GEOMETRIC FORMULAS

(A) Triangle

$$
\operatorname{area}(\mathrm{A})=\frac{\mathrm{bh}}{2}
$$


(B) Square

$$
\operatorname{area}(\mathrm{A})=\mathrm{b}^{2}
$$



Fig. 124
(C) Rectangle

$$
\operatorname{area}(\mathrm{A})=a b
$$



Fig. 125
(D) Parallelogram

$$
\operatorname{area}(A)=\operatorname{ah}
$$

(E) Trapezoid

$$
\operatorname{area}(\mathrm{A})=\frac{\mathrm{h}}{2}(\mathrm{a}+\mathrm{b})
$$

(F) Trapezium

$$
\begin{aligned}
\operatorname{area}(\mathrm{A})= & 1 / 2[\mathrm{~b}(\mathrm{H}+\mathrm{h}) \\
& +\mathrm{ah}+\mathrm{cH}]
\end{aligned}
$$

(G) Regular Pentagon

$$
\operatorname{area}(\mathrm{A})=1.720 \mathrm{a}^{2}
$$

(H) Regular Hexagon

$$
\operatorname{area}(\mathrm{A})=2.598 \mathrm{a}^{2}
$$

(I) Regular Octagon

$$
\operatorname{area}(\mathrm{A})=4.828 \mathrm{a}^{2}
$$



Fig. 126


Fig. 127


Fig. 128


Fig. 129


Fig. 130


Fig. 131
(J) Circle

$$
\text { circumference } \begin{aligned}
(\mathrm{C}) & =2 \pi \mathrm{R} \\
& =\pi \mathrm{D} \\
\text { area }(\mathrm{A}) & =\pi \mathrm{R}^{2}
\end{aligned}
$$



Fig. 132
(K) Segment

$$
\begin{aligned}
& \text { chord }(\mathrm{c})=\sqrt{4\left(2 \mathrm{hR}-\mathrm{h}^{2}\right)} \\
& \text { area }(\mathrm{A})=\pi \mathrm{R}^{2}\left(\frac{\theta}{360}\right)-\left(\frac{\mathrm{c}(\mathrm{R}-\mathrm{h})}{2}\right)
\end{aligned}
$$



Fig. 133
(L) Sector

$$
\begin{aligned}
\operatorname{area}(\mathrm{A}) & =\frac{\mathrm{bR}}{2} \\
& =\pi \mathrm{R}^{2}\left(\frac{\theta}{360}\right)
\end{aligned}
$$



Fig. 134
(M) Circular Ring

$$
\text { area } \begin{aligned}
(\mathrm{A}) & =\pi\left(\mathrm{R}^{2}-\mathrm{r}^{2}\right) \\
& =7854\left(\mathrm{D}^{2}-\mathrm{d}^{2}\right)
\end{aligned}
$$



Fig. 135
(N) Ellipse

$$
\text { circumference }(C)=\pi(a+b)\left[\frac{64-3\left(\frac{b-a}{b+a}\right)^{4}}{64-16\left(\frac{b-a}{b+a}\right)^{2}}\right]
$$

$$
\operatorname{area}(\mathrm{A})=\pi \mathrm{ab}
$$



Fig. 136

## (O) Sphere

$$
\begin{aligned}
\text { area }(\mathrm{A}) & =4 \pi \mathrm{R}^{2} \\
& =\pi \mathrm{D}^{2} \\
\text { volume }(\mathrm{V}) & =\frac{4}{3} \pi \mathrm{R}^{3} \\
& =1 / 6 \pi \mathrm{D}^{3}
\end{aligned}
$$



Fig. 137
(P) Cube

$$
\begin{aligned}
\operatorname{area}(\mathrm{A}) & =6 \mathrm{~b}^{2} \\
\text { volume }(\mathrm{V}) & =\mathrm{b}^{3}
\end{aligned}
$$



Fig. 138
(Q) Rectangular Solid
$\operatorname{area}(A)=2(a b+b c+a c)$
volume $(\mathrm{V})=\mathrm{abc}$


Fig. 139
(R) Cone

$$
\begin{aligned}
\operatorname{area}(\mathrm{A}) & =\pi \mathrm{RS} \\
& =\pi \mathrm{R} \sqrt{\mathrm{R}^{2}+\mathrm{h}^{2}} \\
\text { volume }(\mathrm{V}) & =\frac{\pi \mathrm{R}^{2} \mathrm{~h}}{3} \\
& =1.047 \mathrm{R}^{2} \mathrm{~h} \\
& =0.2618 \mathrm{D}^{2} \mathrm{~h}
\end{aligned}
$$



Fig. 140
(S) Cylinder
cylindrical surface $=\pi \mathrm{Dh}$

$$
\begin{aligned}
\text { total surface } & =2 \pi R(R+h) \\
\text { volume }(V) & =\pi R^{2} h \\
& =\frac{c^{2} h}{4 \pi}
\end{aligned}
$$



Fig. 141
(T) Ring of Rectangular Cross Section

$$
\begin{aligned}
\text { volume }(V) & =\frac{\pi c}{4}\left(D^{2}-d^{2}\right) \\
& =\left(\frac{D+d}{2}\right) \pi b c
\end{aligned}
$$



Fig. 142
(U) Torus (Ring of Circular Cross Section)

$$
\begin{aligned}
\text { total surface } & =4 \pi^{2} \mathrm{Rr} \\
& =\pi^{2} \mathrm{Dd} \\
\text { volume }(\mathrm{V}) & =2 \pi^{2} \mathrm{R} \times \mathrm{r}^{2} \\
& =2.463 \mathrm{D} \times \mathrm{d}^{2}
\end{aligned}
$$



Fig. 143

## 74. TRIGONOMETRIC FUNCTIONS

(A) Plane Trigonometry

In any right triangle, the values in Table XXVII are valid if we let:


Fig. 144
a equal the acute angle formed by the hypotenuse and the altitude leg,
b equal the acute angle formed by the hypotenuse and the base leg,

A equal the side adjacent to $\angle \mathrm{b}$ and opposite $\angle \mathrm{a}$,

B equal the side opposite $\angle \mathrm{b}$ and adjacent to $\angle \mathrm{a}$,
$C$ equal the hypotenuse.

Table XXVII. Trigonometric Formulas

| Known Values | Formulas for Unknown Values of |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | 8 | C | $\angle b$ | $\angle \mathrm{a}$ |
| A \& B | - | - | $\sqrt{A^{2}+B^{2 \prime}}$ | $\arctan \frac{B}{A}$ | $\arctan \frac{A}{B}$ |
| $A \& C$ | - | $\sqrt{C^{2}-A^{2}}$ | - | $\arccos \frac{A}{C}$ | $\arcsin \frac{A}{C}$ |
| $A \& \angle b$ | - | $A \tan \angle b$ | $\frac{A}{\cos \angle b}$ | - | $90^{\circ}-\angle b$ |
| A \& $\angle \mathrm{a}$ | - | $\frac{A}{\tan \angle a}$ | $\frac{A}{\sin \angle a}$ | $90^{\circ}-\angle a$ | - |
| $B \& C$ | $\sqrt{C^{2}-B^{2}}$ | - | - | $\arcsin \frac{B}{C}$ | $\arccos \frac{B}{C}$ |
| B \& $\angle b$ | $\frac{B}{B \tan \angle b}$ | - | $\frac{B}{\sin \angle b}$ | - | $90^{\circ}-\angle b$ |
| B \& $\angle$ a | $B \tan \angle a$ | - | $\frac{B}{\cos \angle a}$ | $90^{\circ}-\angle a$ | - |
| $C \& \angle b$ | $C \cos \angle b$ | $C \sin \angle b$ | - | - | $90^{\circ}-\angle b$ |
| $C \& \angle a$ | $C \sin \angle a$ | $C \cos \angle a$ | - | $90^{\circ}-\angle \mathrm{a}$ | - |

The expression "arc sin" or "sin"" indicates an angle whose sine is. . . Similarly, "arc tan" or "tan"" indicates the angle whose tangent is . . . , etc.

## (B) Table of Trigonometric Functions

Table XXVIII gives the natural sines, cosines, tangents, and cotangents of angles. To find these values for angles from $0^{\circ}$ to $45^{\circ}$, use the headings at the top of the table and the degree listings in the left-hand column. For angles from $45^{\circ}$ to $90^{\circ}$, use the headings at the bottom of the table and the degree listings in the right-hand column. Note: Read the degree listings in the right-hand column from bottom to top; thus, the $10^{\prime}$ listing directly above $89^{\circ}$ signifies $89^{\circ} 10^{\prime}$.

Table XXVIII. Natural Trigonometric Functions

| Degrees |  | Sin | Cos | Tan | Cot |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $00^{\prime}$ | 0.0000 | 1.0000 | 0.0000 | $\infty$ | $90^{\circ}$ | $00^{\prime}$ |
|  | 10 | . 0029 | 1.0000 | . 0029 | 343.77 |  | 50 |
|  | 20 | . 0058 | 1.0000 | . 0058 | 171.89 |  | 40 |
|  | 30 | . 0087 | 1.0000 | . 0087 | 114.59 |  | 30 |
|  | 40 | . 0116 | . 9999 | . 0116 | 85.940 |  | 20 |
|  | 50 | . 0145 | . 9999 | . 0145 | 68.750 |  | 10 |
|  |  | 0.0175 | 0.9998 | 0.0175 | 57.290 | $89^{\circ}$ | 00' |
|  | 10 | . 0204 | . 9998 | . 0204 | 49.104 |  | 50 |
|  | 20 | . 0233 | . 9997 | . 0233 | 42.964 |  | 40 |
|  | 30 | . 0262 | . 9997 | . 0262 | 38.188 |  | 30 |
|  | 40 | . 0291 | . 9996 | .0291 | 34.368 |  | 20 |
|  | 50 | . 0320 | . 9995 | . 0320 | 31.242 |  | 10 |
| $2{ }^{\circ}$ |  | 0.0349 | 0.9994 | 0.0349 | 28.636 | $88^{\circ}$ | 00' |
|  | 10 | . 0378 | . 9993 | . 0378 | 26.432 |  | 50 |
|  | 20 | . 0407 | . 9992 | . 0407 | 24.542 |  | 40 |
|  | 30 | . 0436 | . 9990 | . 0437 | 22.904 |  | 30 |
|  | 40 | . 0465 | . 9989 | . 0466 | 21.470 |  | 20 |
|  | 50 | . 0494 | . 9988 | . 0495 | 20.206 |  | 10 |
| $3^{\circ}$ |  | 0.0523 | 0.9986 | 0.0524 | 19.081 | $87^{\circ}$ | $00^{\circ}$ |
|  | 10 | . 0552 | . 9985 | . 0553 | 18.075 |  | 50 |
|  | 20 | . 0581 | . 9983 | . 0582 | 17.169 |  | 40 |
|  | 30 | . 0610 | . 9981 | . 0612 | 16.350 |  | 30 |
|  | 40 | . 0640 | . 9980 | . 0641 | 15.605 |  | 20 |
|  | 50 | . 0669 | . 9978 | . 0670 | 14.924 |  | 10 |
| $4^{\circ}$ | $00^{\prime}$ | 0.0698 | 0.9976 | 0.0699 | 14.301 | $86^{\circ}$ | 00' |
|  | 10 | . 0727 | . 9974 | . 0729 | 13.727 |  | 50 |
|  | 20 | . 0756 | . 9971 | . 0758 | 13.197 |  | 40 |
|  | 30 | . 0785 | . 9969 | . 0787 | 12.706 |  | 30 |
|  | 40 | . 0814 | . 9967 | . 0816 | 12.251 |  | 20 |
|  | 50 | . 0843 | . 9964 | . 0846 | 11.826 |  | 10 |
| $5{ }^{\circ}$ | 00' | 0.0872 | 0.9962 | 0.0875 | 11.430 | $85^{\circ}$ | 00' |
|  | 10 | . 0901 | . 9959 | . 0904 | 11.059 |  | 50 |
|  | 20 | . 0929 | . 9957 | . 0934 | 10.712 |  | 40 |
|  | 30 | . 0958 | . 9954 | . 0963 | 10.385 |  | 30 |
|  | 40 | . 0987 | . 9951 | . 0992 | 10.078 |  | 20 |
|  | 50 | .1016 | . 9948 | . 1022 | 9.7882 |  | 10 |
| $6^{\circ}$ | 00' | 0.1045 | 0.9945 | 0.1051 | 9.5144 | $84^{\circ}$ | $00^{\circ}$ |
|  | 10 | . 1074 | . 9942 | . 1080 | 9.2553 |  | 50 |
|  | 20 | . 1103 | . 9939 | . 1110 | 9.0098 |  | 40 |
|  | 30 | . 1132 | . 9936 | .1139 | 8.7769 |  | 30 |
|  | 40 | . 1161 | . 9932 | . 1169 | 8.5555 |  | 20 |
|  | 50 | . 1190 | . 9929 | . 1198 | 8.3450 |  | 10 |
| $7{ }^{\circ}$ | 00' | 0.1219 | 0.9925 | 0.1228 | 8.1443 | $83^{\circ}$ | $00^{\circ}$ |
|  | 10 | . 1248 | . 9922 | . 1257 | 7.9530 |  | 50 |
|  | 20 | . 1276 | . 9918 | . 1287 | 7.7704 |  | 40 |
|  | 30 | . 1305 | . 9914 | . 1317 | 7.5958 |  | 30 |
|  | 40 | . 1334 | . 9911 | . 1346 | 7.4287 |  | 20 |
|  | 50 | . 1363 | . 9907 | . 1376 | 7.2687 |  | 10 |
|  |  | Cos | Sin | Cot | Tan | Deg | ees |

Table XXVIII. Natural Trigonometric Functions-(Cont'd)

| Degrees |  | Sin | Cos | Tan | Cot |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $00^{\prime}$ | 0.1392 | 0.9903 | 0.1405 | 7.1154 | $82^{\circ}$ |  |
|  | 10 | . 1421 | . 9899 | . 1435 | 6.9682 |  | 50 |
|  | 20 | . 1449 | . 9894 | . 1465 | 6.8269 |  | 40 |
|  | 30 | . 1478 | . 9890 | . 1495 | 6.6912 |  | 30 |
|  | 40 | . 1507 | . 9886 | . 1524 | 6.5606 |  | 20 |
|  | 50 | . 1536 | . 9881 | . 1554 | 6.4348 |  | 10 |
| $9{ }^{\circ}$ | 00' | 0.1564 | 0.9877 | 0.1584 | 6.3138 | $81{ }^{\circ}$ | 00' |
|  | 10 | . 1593 | . 9872 | . 1614 | 6.1970 |  | 50 |
|  | 20 | . 1622 | . 9868 | . 1644 | 6.0844 |  | 40 |
|  | 30 | . 1650 | . 9863 | . 1673 | 5.9758 |  | 30 |
|  | 40 | . 1679 | . 9858 | . 1703 | 5.8708 |  | 20 |
|  | 50 | . 1708 | . 9853 | . 1733 | 5.7694 |  | 10 |
| $10^{\circ}$ |  | 0.1736 | 0.9848 | 0.1763 | 5.6713 | $80^{\circ}$ |  |
|  | 10 | . 1765 | . 9843 | . 1793 | 5.5764 |  | 50 |
|  | 20 | . 1794 | . 9838 | . 1823 | 5.4845 |  | 40 |
|  | 30 | . 1822 | . 9833 | . 1853 | 5.3955 |  | 30 |
|  | 40 | . 1851 | . 9827 | . 1883 | 5.3093 |  | 20 |
|  | 50 | . 1880 | . 9822 | . 1914 | 5.2257 |  | 10 |
| $11^{\circ}$ | $00^{\prime}$ | 0.1908 | 0.9816 | 0.1944 | 5.1446 | $79^{\circ}$ | $00^{\prime}$ |
|  | 10 | . 1937 | . 9811 | . 1974 | 5.0658 |  | 50 |
|  | 20 | . 1965 | . 9805 | . 2004 | 4.9894 |  | 40 |
|  | 30 | . 1994 | . 9799 | . 2035 | 4.9152 |  | 30 |
|  | 40 | . 2022 | . 9793 | . 2065 | 4.8430 |  | 20 |
|  | 50 | . 2051 | . 9787 | . 2095 | 4.7729 |  | 10 |
| $12{ }^{\circ}$ | 00' | 0.2079 | 0.9781 | 0.2126 | 4.7046 | $78^{\circ}$ | $00^{\prime}$ |
|  | 10 | . 2108 | . 9775 | . 2156 | 4.6382 |  | 50 |
|  | 20 | . 2136 | . 9769 | . 2186 | 4.5736 |  | 40 |
|  | 30 | . 2164 | . 9763 | . 2217 | 4.5107 |  | 30 |
|  | 40 | . 2193 | . 9757 | . 2247 | 4.4494 |  | 20 |
|  | 50 | . 2221 | . 9750 | . 2278 | 4.3897 |  | 10 |
| $13^{\circ}$ |  | 0.2250 | 0.9744 | 0.2309 | 4.3315 | $77^{\circ}$ |  |
|  | 10 | . 2278 | . 9737 | . 2339 | 4.2747 |  | 50 |
|  | 20 | . 2306 | . 9730 | . 2370 | 4.2193 |  | 40 |
|  | 30 | . 2334 | . 9724 | . 2401 | 4.1653 |  | 30 |
|  | 40 | . 2363 | . 9717 | . 2432 | 4.1126 |  | 20 |
|  | 50 | . 2391 | . 9710 | . 2462 | 4.0611 |  | 10 |
| $14^{\circ}$ | $00^{\prime}$ | 0.2419 | 0.9703 | 0.2493 | 4.0108 | $76^{\circ}$ | 00' |
|  | 10 | . 2447 | . 9696 | . 2524 | 3.9617 |  | 50 |
|  | 20 | . 2476 | . 9689 | . 2555 | 3.9136 |  | 40 |
|  | 30 | 2504 | . 9681 | . 2586 | 3.8667 |  | 30 |
|  | 40 | . 2532 | . 9674 | . 2617 | 3.8208 |  | 20 |
|  | 50 | . 2560 | . 9667 | . 2648 | 3.7760 |  | 10 |
|  | $00^{\prime}$ | 0.2588 | 0.9659 | 0.2679 | 3.7321 | $75^{\circ}$ | 00' |
|  | 10 | . 2616 | . 9652 | . 2711 | 3.6891 |  | 50 |
|  | 20 | . 2644 | . 9644 | . 2742 | 3.6470 |  | 40 |
|  | 30 | . 2672 | . 9636 | . 2773 | 3.6059 |  | 30 |
|  | 40 | . 2700 | . 9628 | . 2805 | 3.5656 |  | 20 |
|  | 50 | . 2728 | . 9621 | . 2836 | 3.5261 |  | 10 |
|  |  | Cos | Sin | Cot | Tan | Deg | ees |

Table XXVIII. Natural Trigonometric Functions-(Cont'd)

| Degrees |  | Sin | Cos | Tan | Cot |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $16^{\circ}$ | $00^{\prime}$ | 0.2756 | 0.9613 | 0.2867 | 3.4874 | $74^{\circ}$ | 00' |
|  | 10 | . 2784 | . 9605 | . 2899 | 3.4495 |  | 50 |
|  | 20 | . 2812 | . 9596 | . 2931 | 3.4124 |  | 40 |
|  | 30 | . 2840 | . 9588 | . 2962 | 3.3759 |  | 30 |
|  | 40 | . 2868 | . 9580 | . 2994 | 3.3402 |  | 20 |
|  | 50 | . 2896 | . 9572 | . 3026 | 3.3052 |  | 10 |
| $17^{\circ}$ | $00^{\circ}$ | 0.2924 | 0.9563 | 0.3057 | 3.27C7 | $73^{\circ}$ | $00^{\prime}$ |
|  | 10 | . 2952 | . 9555 | . 3089 | 3.2371 |  | 50 |
|  | 20 | . 2979 | . 9546 | . 3121 | 3.2041 |  | 40 |
|  | 30 | . 3007 | . 9537 | . 3153 | 3.1716 |  | 30 |
|  | 40 | . 3035 | . 9528 | . 3185 | 3.1397 |  | 20 |
|  | 50 | . 3062 | . 9520 | . 3217 | 3.1084 |  | 10 |
| $18^{\circ}$ | $00^{\prime}$ | 0.3090 | 0.9511 | 0.3249 | 3.0777 | $72^{\circ}$ | 00' |
|  | 10 | . 3118 | . 9502 | . 3281 | 3.0475 |  | 50 |
|  | 20 | . 3145 | . 9492 | . 3314 | 3.0178 |  | 40 |
|  | 30 | . 3173 | . 9483 | . 3346 | 2.9887 |  | 30 |
|  | 40 | . 3201 | . 9474 | . 3378 | 2.9600 |  | 20 |
|  | 50 | . 3228 | . 9465 | . 3411 | 2.9319 |  | 10 |
| $19^{\circ}$ | 00' | 0.3256 | 0.9455 | 0.3443 | 2.9042 | $71^{\circ}$ | 00' |
|  | 10 | . 3283 | . 9446 | . 3476 | 2.8770 |  | 50 |
|  | 20 | . 3311 | . 9436 | . 3508 | 2.8502 |  | 40 |
|  | 30 | . 3338 | . 9426 | . 3541 | 2.8239 |  | 30 |
|  | 40 | . 3365 | . 9417 | . 3574 | 2.7980 |  | 20 |
|  | 50 | . 3393 | . 9407 | . 3607 | 2.7725 |  | 10 |
| $20^{\circ}$ | $00^{\prime}$ | 0.3420 | 0.9397 | 0.3640 | 2.7475 | $70^{\circ}$ | 00' |
|  | 10 | . 3448 | . 9387 | . 3673 | 2.7228 |  | 50 |
|  | 20 | . 3475 | . 9377 | . 3706 | 2.6985 |  | 40 |
|  | 30 | . 3502 | . 9367 | . 3739 | 2.6746 |  | 30 |
|  | 40 | . 3529 | . 9356 | . 3772 | 2.6511 |  | 20 |
|  | 50 | . 3557 | . 9346 | . 3805 | 2.6279 |  | 10 |
| $21^{\circ}$ | 00' | 0.3584 | 0.9336 | 0.3839 | 2.6051 | $69^{\circ}$ | 00' |
|  | 10 | . 3611 | . 9325 | . 3872 | 2.5826 |  | 50 |
|  | 20 | . 3638 | . 9315 | . 3906 | 2.5605 |  | 40 |
|  | 30 | . 3665 | . 9304 | . 3939 | 2.5386 |  | 30 |
|  | 40 | . 3692 | . 9293 | . 3973 | 2.5172 |  | 20 |
|  | 50 | . 3719 | . 9283 | . 4006 | 2.4960 |  | 10 |
| $22^{\circ}$ | 00' | 0.3746 | 0.9272 | 0.4040 | 2.4751 | $68^{\circ}$ | 00' |
|  | 10 | . 3773 | . 9261 | . 4074 | 2.4545 |  | 50 |
|  | 20 | . 3800 | . 9250 | . 4108 | 2.4342 |  | 40 |
|  | 30 | . 3827 | . 9239 | . 4142 | 2,4142 |  | 30 |
|  | 40 | . 3854 | . 9228 | . 4176 | 2.3945 |  | 20 |
|  | 50 | . 3881 | . 9216 | . 4210 | 2.3750 |  | 10 |
| $23^{\circ}$ | 00' | 0.3907 | 0.9205 | 0.4245 | 2.3559 | $67^{\circ}$ | $00^{\prime}$ |
|  | 10 | . 3934 | . 9194 | . 4279 | 2.3369 |  | 50 |
|  | 20 | . 3961 | . 9182 | . 4314 | 2.3183 |  | 40 |
|  | 30 | . 3987 | . 9171 | . 4348 | 2.2998 |  | 30 |
|  | 40 | . 4014 | . 9159 | . 4383 | 2.2817 |  | 20 |
|  | 50 | .4041 | .9147 | . 4417 | 2.2637 |  | 10 |
|  |  | Cos | Sin | Cot | Tan | Deg | rees |

Table XXVIII. Natural Trigonometric Functions-(Cont'd)

\begin{tabular}{|c|c|c|c|c|c|}
\hline Degrees \& Sin \& Cos \& Tan \& Cot \& <br>
\hline $24^{\circ} 00^{\prime}$ \& 0.4067 \& 0.9135 \& 0.4452 \& 2.2460 \& $66^{\circ} 00{ }^{\prime}$ <br>
\hline \multirow{5}{*}{$24^{\circ}$} \& . 4094 \& . 9124 \& . 4487 \& 2.2286 \& 50 <br>
\hline \& . 4120 \& . 9112 \& . 4522 \& 2.2113 \& 40 <br>
\hline \& . 4147 \& . 9100 \& . 4557 \& 2.1943 \& 30 <br>
\hline \& . 4173 \& . 9088 \& . 4592 \& 2.1775 \& 20 <br>
\hline \& . 4200 \& . 9075 \& . 4628 \& 2.1609 \& 10 <br>
\hline \multirow[t]{6}{*}{$25^{\circ}$} \& 0.4226 \& 0.9063 \& 0.4663 \& 2.1445 \& $65^{\circ} 00{ }^{\prime}$ <br>
\hline \& . 4253 \& . 9051 \& . 4699 \& 2.1283 \& 50 <br>
\hline \& . 4279 \& . 9038 \& . 4734 \& 2.1123 \& 40 <br>
\hline \& . 4305 \& . 9026 \& . 4770 \& 2.0965 \& 30 <br>
\hline \& . 4331 \& . 9013 \& . 4806 \& 2.0809 \& 20 <br>
\hline \& . 4358 \& . 9001 \& . 4841 \& 2.0655 \& 10 <br>
\hline \multirow[t]{6}{*}{$26^{\circ}$} \& 0.4384 \& 0.8988 \& 0.4877 \& 2.0503 \& $64^{\circ} 00^{\prime}$ <br>
\hline \& . 4410 \& . 8975 \& . 4913 \& 2.0353 \& 50 <br>
\hline \& . 4436 \& . 8962 \& . 4950 \& 2.0204 \& 40 <br>
\hline \& . 4462 \& . 8949 \& . 4986 \& 2.0057 \& 30 <br>
\hline \& . 4488 \& . 8936 \& . 5022 \& 1.9912 \& 20 <br>
\hline \& . 4514 \& . 8923 \& . 5059 \& 1.9768 \& 10 <br>
\hline \multirow[t]{6}{*}{$27^{\circ}$
0
10
20
30
40
50} \& 0.4540 \& 0.8910 \& 0.5095 \& 1.9626 \& $63^{\circ} 00^{\prime}$ <br>
\hline \& . 4566 \& . 8897 \& . 5132 \& 1.9486 \& 50 <br>
\hline \& . 4592 \& . 8884 \& . 5169 \& 1.9347 \& 40 <br>
\hline \& . 4617 \& . 8870 \& . 5206 \& 1.9210 \& 30 <br>
\hline \& . 4643 \& . 8857 \& . 5243 \& 1.9074 \& 20 <br>
\hline \& . 4669 \& . 8843 \& . 5280 \& 1.8940 \& 10 <br>
\hline \multirow[t]{6}{*}{28

10

20
30
40
50} \& 0.4695 \& 0.8829 \& 0.5317 \& 1.8807 \& $62^{\circ} 00{ }^{\prime}$ <br>
\hline \& . 4720 \& . 8816 \& . 5354 \& 1.8676 \& 50 <br>
\hline \& . 4746 \& . 8802 \& . 5392 \& 1.8546 \& 40 <br>
\hline \& . 4772 \& . 8788 \& . 5430 \& 1.8418 \& 30 <br>
\hline \& . 4797 \& . 8774 \& . 5467 \& 1.8291 \& 20 <br>
\hline \& . 4823 \& . 8760 \& . 5505 \& 1.8165 \& 10 <br>
\hline \multirow[t]{6}{*}{$29^{\circ}-$} \& 0.4848 \& 0.8746 \& 0.5543 \& 1.8040 \& $61^{\circ} 00{ }^{\prime}$ <br>
\hline \& . 4874 \& . 8732 \& . 5581 \& 1.7917 \& 50 <br>
\hline \& . 4899 \& . 8718 \& . 5619 \& 1.7796 \& 40 <br>
\hline \& . 4924 \& . 8704 \& . 5658 \& 1.7675 \& 30 <br>
\hline \& . 4950 \& . 8689 \& . 5696 \& 1.7556 \& 20 <br>
\hline \& . 4975 \& . 8675 \& . 5735 \& 1.7437 \& 10 <br>
\hline \multirow[t]{6}{*}{$30^{\circ}$} \& 0.5000 \& 0.8660 \& 0.5774 \& 1.7321 \& $60^{\circ} 00^{\prime}$ <br>
\hline \& . 5025 \& . 8646 \& . 5812 \& 1.7205 \& 50 <br>
\hline \& . 5050 \& . 8631 \& . 5851 \& 1.7090 \& 40 <br>
\hline \& . 5075 \& . 8616 \& . 5890 \& 1.6977 \& 30 <br>
\hline \& . 5100 \& . 8601 \& . 5930 \& 1.6864 \& 20 <br>
\hline \& . 5125 \& . 8587 \& . 5969 \& 1.6753 \& 10 <br>
\hline \multirow[t]{6}{*}{$31^{\circ}$} \& 0.5150 \& 0.8572 \& 0.6009 \& 1.6643 \& $59^{\circ} 00^{\prime}$ <br>
\hline \& . 5175 \& . 8557 \& . 6048 \& 1.6534 \& 50 <br>
\hline \& . 5200 \& . 8542 \& . 6088 \& 1.6426 \& 40 <br>
\hline \& . 5225 \& . 8526 \& . 6128 \& 1.6319 \& 30 <br>
\hline \& . 5250 \& . 8511 \& . 6168 \& 1.6212 \& 20 <br>
\hline \& . 5275 \& . 8496 \& . 6208 \& 1.6107 \& 10 <br>
\hline \& Cos \& Sin \& Cot \& Tan \& Degrees <br>
\hline
\end{tabular}

Table XXVIII. Natural Trigonometric Functions-(Cont'd)

| Degrees |  | Sin | Cos | Tan | Cot |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $32^{\circ}$ | 00' | 0.5299 | 0.8480 | 0.6249 | 1.6003 | $58^{\circ}$ | 00' |
|  | 10 | . 5324 | . 8465 | . 6289 | 1.5900 |  | 50 |
|  | 20 | . 5348 | . 8450 | . 6330 | 1.5798 |  | 40 |
|  | 30 | . 5373 | . 8434 | . 6371 | 1.5697 |  | 30 |
|  | 40 | . 5398 | . 8418 | . 6412 | 1.5597 |  | 20 |
|  | 50 | . 5422 | . 8403 | . 6453 | 1.5497 |  | 10 |
| $33^{\circ}$ | $00^{\prime}$ | 0.5446 | 0.8387 | 0.6494 | 1.5399 | $57^{\circ}$ | 00' |
|  | 10 | . 5471 | . 8371 | . 6536 | 1.5301 |  | 50 |
|  | 20 | . 5495 | . 8355 | . 6577 | 1.5204 |  | 40 |
|  | 30 | . 5519 | . 8339 | . 6619 | 1.5108 |  | 30 |
|  | 40 | . 5544 | . 8323 | . 6661 | 1.5013 |  | 20 |
|  | 50 | . 5568 | . 8307 | . 6703 | 1.4919 |  | 10 |
| $34^{\circ}$ | $00^{\prime}$ | 0.5592 | 0.8290 | 0.6745 | 1.4826 | $56^{\circ}$ | 00' |
|  | 10 | . 5616 | . 8274 | . 6787 | 1.4733 |  | 50 |
|  | 20 | . 5640 | . 8258 | . 6830 | 1.4641 |  | 40 |
|  | 30 | . 5664 | . 8241 | . 6873 | 1.4550 |  | 30 |
|  | 40 | . 5688 | . 8225 | . 6916 | 1.4460 |  | 20 |
|  | 50 | . 5712 | . 8208 | . 6959 | 1.4370 |  | 10 |
| $35^{\circ}$ | 00' | 0.5736 | 0.8192 | 0.7002 | 1.4281 | $55^{\circ}$ | $00^{\prime}$ |
|  | 10 | . 5760 | . 8175 | . 7046 | 1.4193 |  | 50 |
|  | 20 | . 5783 | . 8158 | . 7089 | 1.4106 |  | 40 |
|  | 30 | . 5807 | . 8141 | . 7133 | 1.4019 |  | 30 |
|  | 40 | . 5831 | . 8124 | . 7177 | 1.3934 |  | 20 |
|  | 50 | . 5854 | . 8107 | . 7221 | 1.3848 |  | 10 |
| $36^{\circ}$ | 00' | 0.5878 | 0.8090 | 0.7265 | 1.3764 | $54^{\circ}$ | 00' |
|  | 10 | . 5901 | . 8073 | . 7310 | 1.3680 |  | 50 |
|  | 20 | . 5925 | . 8056 | . 7355 | 1.3597 |  | 40 |
|  | 30 | . 5948 | . 8039 | . 7400 | 1.3514 |  | 30 |
|  | 40 | . 5972 | . 8021 | . 7445 | 1.3432 |  | 20 |
|  | 50 | . 5995 | . 8004 | . 7490 | 1.3351 |  | 10 |
| $37^{\circ}$ | $00^{\prime}$ | . 6018 | . 7986 | . 7536 | 1.3270 | $53^{\circ}$ | 00' |
|  | 10 | . 6041 | . 7969 | . 7581 | 1.3190 |  | 50 |
|  | 20 | . 6065 | . 7951 | . 7627 | 1.3111 |  | 40 |
|  | 30 | . 6088 | . 7934 | . 7673 | 1.3032 |  | 30 |
|  | 40 | . 6111 | . 7916 | . 7720 | 1.2954 |  | 20 |
|  | 50 | . 6134 | . 7898 | . 7766 | 1.2876 |  | 10 |
| $38^{\circ}$ | 00' | 0.6157 | 0.7880 | 0.7813 | 1.2799 | $52^{\circ}$ | 00' |
|  | 10 | . 6180 | . 7862 | . 7860 | 1.2723 |  | 50 |
|  | 20 | . 6202 | . 7844 | . 7907 | 1.2647 |  | 40 |
|  | 30 | . 6225 | . 7826 | . 7954 | 1.2572 |  | 30 |
|  | 40 | . 6248 | . 7808 | . 8002 | 1.2497 |  | 20 |
|  | 50 | . 6271 | . 7790 | . 8050 | 1.2423 |  | 10 |
| $39^{\circ}$ | 00' | 0.6293 | 0.7771 | 0.8098 | 1.2349 | $51^{\circ}$ | 00' |
|  | 10 | . 6316 | . 7753 | . 8146 | 1.2276 |  | 50 |
|  | 20 | . 6338 | . 7735 | . 8195 | 1.2203 |  | 40 |
|  | 30 | . 6361 | . 7716 | . 8243 | 1.2131 |  | 30 |
|  | 40 | . 6383 | . 7698 | . 8292 | 1.2059 |  | 20 |
|  | 50 | . 6406 | . 7679 | . 8342 | 1.1988 |  | 10 |
|  |  | Cos | Sin | Cot | Tan | Deg | ees |

Table XXVIII. Natural Trigonometric Functions-(Cont'd)

| Degrees | Sin | Cos | Tan | Cot |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $40^{\circ} 00$ | 0.6428 | 0.7660 | 0.8391 | 1.1918 | $50^{\circ} 00{ }^{\prime}$ |
| 10 | . 6450 | . 7642 | . 8441 | 1.1847 | 50 |
| 20 | . 6472 | . 7623 | . 8491 | 1.1778 | 40 |
| 30 | . 6494 | . 7604 | . 8541 | 1.1708 | 30 |
| 40 | . 6517 | . 7585 | . 8591 | 1.1640 | 20 |
| 50 | . 6539 | . 7566 | . 8642 | 1.1571 | 10 |
| $41^{\circ} 00$ | 0.6561 | 0.7547 | 0.8693 | 1.1504 | $49^{\circ} 00{ }^{\prime}$ |
| 10 | . 6583 | . 7528 | . 8744 | 1.1436 | 50 |
| 20 | . 6604 | . 7509 | . 8796 | 1.1369 | 40 |
| 30 | . 6626 | . 7490 | . 8847 | 1.1303 | 30 |
| 40 | . 6648 | . 7470 | . 8899 | 1.1237 | 20 |
| 50 | . 6670 | . 7451 | . 8952 | 1.1171 | 10 |
| $42^{\circ} 00$ | 0.6691 | 0.7431 | 0.9004 | 1.1106 | $48^{\circ} 00{ }^{\prime}$ |
| 10 | . 6713 | . 7412 | . 9057 | 1.1041 | 50 |
| 20 | . 6734 | . 7392 | . 9110 | 1.0977 | 40 |
| 30 | . 6756 | . 7373 | . 9163 | 1.0913 | 30 |
| 40 | . 6777 | . 7353 | . 9217 | 1.0850 | 20 |
| 50 | . 6799 | . 7333 | . 9271 | 1.0786 | 10 |
| $43^{\circ} 00{ }^{\prime}$ | 0.6820 | 0.7314 | 0.9325 | 1.0724 | $47^{\circ} 00^{\prime}$ |
| 10 | . 6841 | . 7294 | . 9380 | 1.0661 | 50 |
| 20 | . 6862 | . 7274 | . 9435 | 1.0599 | 40 |
| 30 | . 6884 | . 7254 | . 9490 | 1.0538 | 30 |
| 40 | . 6905 | . 7234 | . 9545 | 1.0477 | 20 |
| 50 | . 6926 | . 7214 | . 9601 | 1.0416 | 10 |
| $44^{\circ} 00{ }^{\prime}$ |  | 0.7193 | 0.9657 | 1.0355 | $46^{\circ} 00{ }^{\prime}$ |
| 10 | . 6967 | . 7173 | . 9713 | 1.0295 | 50 |
| 20 | . 6988 | . 7163 | . 9770 | 1.0235 | 40 |
| 30 | . 7009 | . 7133 | . 9827 | 1.0176 | 30 |
| 40 | . 7030 | . 7112 | . 9884 | 1.0117 | 20 |
| 50 | . 7050 | . 7092 | . 9942 | 1.0058 | 10 |
| $45^{\circ} 00{ }^{\prime}$ | 0.7071 | 0.7071 | 1.0000 | 1.0000 | $45^{\circ} 00{ }^{\prime}$ |
|  | Cos | Sin | Cot | Tan | Degrees |

## 75. BINARY NUMBERS

## (A) Binary Digits

In the binary system of numbers, there are only two digits -0 and 1 . All numbers are written as successive powers of 2 . Actually, in the decimal system, all numbers are written as successive powers of 10 , although we don't normally think of them in this way. For example, decimal 3487 is actually :

$$
\begin{aligned}
& 3 \times 10^{3}=3000 \\
& 4 \times 10^{2}=400 \\
& 8 \times 10^{1}=80 \\
& 7 \times 10^{0}=\frac{7}{3487}
\end{aligned}
$$

With binary numbers, a like system is used except the base (radix) is 2 instead of 10 . For example, the binary numbers corresponding to decimal numbers 0 through 10 are $0,1,10$, $11,100,101,110,111,1000,1001,1010$. Each number is written as a succession of powers of 2 . For example, binary 1010 actually means:

$$
\begin{array}{r}
1 \times 2^{3}=8 \\
+1 \times 2^{1}=\frac{2}{10}
\end{array}
$$

The powers of 2, from 0 to 20, are given in Table XXIX. Thus, to write a number above decimal $1,048,056$ using binary numbers requires a minimum of 21 digits!

Table XXIX. Powers of 2

| Power | Decimal | Power | Decimal | Power | Decimal |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $2^{0}$ | 1 | $2^{7}$ | 128 | $2^{14}$ | 16,384 |
| $2^{1}$ | 2 | $2^{8}$ | 256 | $2^{15}$ | 32,768 |
| $2^{2}$ | 4 | $2^{9}$ | 512 | $2^{19}$ | 65,536 |
| $2^{3}$ | 8 | $2^{10}$ | 1,024 | $2^{17}$ | 131,072 |
| $2^{4}$ | 16 | $2^{11}$ | 2,048 | $2^{19}$ | 262,144 |
| $2^{5}$ | 32 | $2^{19}$ | 4,096 | $2^{19}$ | 524,288 |
| $2^{0}$ | 64 | $2^{13}$ | 8,192 | $2^{20}$ | $1,048,576$ |

## (B) Conversion

To convert from binary to decimal or from decimal to binary, you could use Table XXIX and compute the equivalent in the other numbering system as was done in the previous section. However, there are simpler methods. To convert from decimal to binary, successively divide the decimal number by 2. Write down a 1 if there is a remainder and a 0 if not, until the division gives a 0 . For example, to convert decimal 22 to binary :
2) 22

| 2) 11 | $\mathrm{R}=0$ |
| :--- | :--- |
| 2) | $\mathrm{R}=1$ |
| 2) | $\mathrm{R}=1$ |
| 2) | $\mathrm{R}=0$ |
| 2 | $\mathrm{R}=1$ |

The least significant figure is at the top; thus, the binary number corresponding to decimal 22 is 10110.

To convert from binary to decimal, take the first binary digit, double it, and add your answer to the second digit. Write this sum under the second digit. Then double this number, add it to the third digit, and write the sum under the third digit. Continue this process up to and including the last digit, as follows:

| 1 | 0 | 1 | 1 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 5 | 11 | 22 | 45 |

The number under the last digit (45) is the decimal equivalent of binary 101101.

## (C) Addition

Binary addition has only four rules:

$$
\begin{array}{cccc}
0 & 0 & 1 & 1 \\
\frac{0}{0} & \frac{1}{1} & \frac{0}{1} & \frac{1}{10}
\end{array}
$$

Following these rules, any binary number can be added. Thus:

$$
\begin{array}{r}
1011 \\
110 \\
\hline 10001
\end{array}
$$

To simplify the carry when $1+1=10$, place the carry under the next digit. Then add the partial total and the carries, as follows:

$$
\begin{aligned}
& 111101 \\
& 10110 \\
& \hline 101011 \\
& \hline 11
\end{aligned}
$$

## (D) Subtraction

Binary numbers can be subtracted directly, as follows:

$$
\begin{array}{r}
1111 \\
-\quad 111 \\
\hline 1000
\end{array}
$$

However, a simpler method is to complement the subtracted number and add. In the binary system, a number is
complemented by merely changing all 0 's to 1 's and all 1 's to 0 's and adding 1 to the final digit. Thus:

$$
\begin{array}{r}
1111 \\
-0111 \\
\hline
\end{array} \text { complemented } \begin{array}{r}
1111 \\
+1001 \\
\hline 11000
\end{array}
$$

The first digit in the answer is disregarded. Hence, the answer is 1000 (decimal 8), the same as before.

## (E) Multiplication

Binary multiplication is similar to decimal multiplication. All products are the same as in decimal multiplication. That is:

$$
\begin{aligned}
& 0 \times 0=0 \\
& 1 \times 0=0 \\
& 1 \times 1=1
\end{aligned}
$$

To multiply 1011 by 101:
1011
$\frac{0101}{1011}$
0000
$\frac{1011}{110111}$

## (F) Division

Binary division is similar to decimal division. Thus, to divide 1101001 by 101 :

$$
\begin{aligned}
& \text { 101 } \begin{array}{l}
\frac{10101}{1101001} \\
\frac{101}{110} \\
\frac{101}{101} \\
\underline{101}
\end{array}
\end{aligned}
$$

## 76. FUNDAMENTALS OF BOOLEAN ALGEBRA

Boolean algebra is based on symbolic logic, which states that an idea must be either true or false-it can be nothing else. The symbols $\mathrm{A}, \mathrm{B}$, and C are used to designate the various conditions (or computer inputs). Two connectivesAND and OR-express the relationship between two statements.

OR is the logical equivalent of a parallel switch circuit. That is, a statement is true if any switch is closed, or if they are all closed. OR is symbolized by a + sign. Thus, "A OR B" is written "A + B."

AND is the logical equivalent of a series switch circuitall switches must be closed to satisfy the condition. AND is symbolized by a multiplication sign (A $\cdot \mathrm{B}$ ) or no sign at all. For example, A • B and AB both mean A AND B. The various symbols are given in Table XXX. Table XXXI summarizes the various logical statements, explains their meanings, and shows the equivalent switch circuit for the statement.

Table XXX. Basic Rules of Symbolic Logic

| Symbol | Logic | Switch | Meaning | Circuit |
| :---: | :---: | :---: | :---: | :---: |
| 1 | True | Closed | The statement is true, the circuit is closed. | $\rightarrow 0$ |
| 0 | False | Open | The statement is false, the circuit is open. | $\cdots$ |
| - | Series | A and B | A is in series with B. | $\xrightarrow[A]{\rightarrow 0}$ |
| + | Parallel | A or B | A is in paraliel with B. |  |
| $\bar{A}$ or $A^{\prime}$ | Not A |  | Opposite of $A$ (If $A=0$, $\bar{A}=1$; if $A=1, \bar{A}=0$ ). |  |

Table XXXI. Summary of Logical Statements

| Logic | Meaning | Circuir |
| :---: | :---: | :---: |
| $0 \cdot 0=0$ | An open in series with an open is open. | $\ldots$ |
| $0 \cdot 1=0$ | An open in series with a closed is open. | $\cdots \infty$ |
| $1 \cdot 1=1$ | A closed in series with a closed is closed. | $\longrightarrow \infty$ |
| $A \cdot \bar{A}=0$ | A switch in series with its negation is open. | $-\infty$ |
| $0+0=0$ | An open in parallel with an open is open. |  |
| $0+1=1$ | An open in parallel with a closed is closed. |  |
| $1+1=1$ | A closed in parallel with a closed is closed. |  |
| $A+\bar{A}=1$ | A switch in parallel with its negation is closed. | $\left[\begin{array}{c} -\infty \\ -\infty \\ -\infty \\ -\infty \end{array}\right]$ |

## 77. COMMON LOGARITHMS

The logarithm of a quantity is the power to which a given number (base) must be raised in order to equal that quantity. Thus, any number may be used as the base. The most common system is the base 10 . Logarithms with the base 10 are known as common, or Briggs, logarithms; they are written $\log _{10}$, or simply log. When the base is omitted, the base 10 is understood.

A common logarithm of a given number is the number which, when applied to the number 10 as an exponent, will produce the given number. Thus, 2 is the common logarithm of 100 , since $10^{2}$ equals $100 ; 3$ is the logarithm of 1000 , since $10^{3}$ equals 1000 , etc. From this we can see that the logarithm of any number except a whole number power of 10 consists of a whole number and a decimal fraction.

## (A) Characteristic of a Logarithm

The whole-number portion of a logarithm is called the characteristic. The characteristic of a whole number, or of
a whole number and a fraction, has a positive value equal to one less than the number of digits preceding the decimal point. The characteristic of a decimal fraction has a negative value equal to one more than the number of zeros immediately following the decimal point. The characteristics of numbers between .0001 and 99,999 are:

| $\quad$ Numbers | Characteristic |
| :--- | :---: |
| .0001 to .0009 | -4 |
| .001 to .009 | -3 |
| .01 to .09 | -2 |
| .1 to .9 | -1 |
| 1 to 9 | 0 |
| 10 to 99 | 1 |
| 100 to 999 | 2 |
| 1,000 to 9,999 | 3 |
| 10,000 to 99,999 | 4 |

## (B) Use of Logarithm Table

The mantissa, or decimal-fraction portion, of a logarithm is obtained from Table XXXII. To find the mantissa for the logarithm of any number, locate the first two figures of the number in the left-hand column ( N ) ; then, in the column under the third figure of the number, the mantissa for that number will be found.

For example, to find the logarithm of 6673, first locate 66 in the left-hand column ( N ) ; then follow across to the column numbered 7 . The mantissa for 667 (.8241) is located at this point. The characteristic for the logarithm of 6673 is 3 . Therefore, the logarithm of 6670 is 3.8241 . For most computations, greater accuracy will not be required.

If accuracy to four places is desired, the columns labeled Proportional Parts may be used. These columns list the numbers to be added to the logarithm to obtain four-place accuracy. In the foregoing, we obtained the logarithm for 6670 (3.8241), but we wanted the logarithm for 6673 ; therefore, we use the proportional parts column to find the proportional part for 3. This is 2 . Therefore, the logarithm for 6673 is 3.8241 plus .0002 , or 3.8243 .

The mantissa of a logarithm is usually positive, whereas a characteristic may be either positive or negative. The total logarithm is the sum of the mantissa and the characteristic.

Thus, the mantissa of .0234 is .3692 , and the characteristic is $\mathbf{- 2}$. The total logarithm is $-2+.3692$, or -1.6308 . A negative logarithm is difficult to use; therefore, it is more convenient to convert the logarithm to a positive number. This is possible by adding 10, or a multiple thereof, to the characteristic when it is negative, and compensating for this by indicating the subtraction of 10 from the entire logarithm. Thus, the logarithm of .0234 would be written $8.3692-10$, since $-2+.3692$ equals $8+.3692-10$. This logarithm may now be used like any other positive logarithm, except that the -10 must be considered in determining the characteristic of the answer.

## (C) Antilogarithms

An antilogarithm (abbreviated antilog or $\log ^{-1}$ ) is a number corresponding to a given logarithm. To find an antilog, locate in the logarithm table the mantissa closest to that of the given logarithm. Record the number in the $N$ column directly opposite the mantissa located, and annex to this the number on the top line immediately above the mantissa. Next determine where the decimal point is located, by counting off the number of places indicated by the characteristic. Starting between the first and second digits, count to the right if the characteristic is positive, and to the left if it is negative. If greater accuracy is desired, the proportional parts columns of the logarithm table can be used, in the same manner described in the foregoing for finding the mantissa.

To find the antilog of 3.4548 , locate 4548 in the table. Then read the first two figures of the antilog from the $N$ column (28) and the third figure directly above the mantissa (5). Thus, the three figures of the antilog are 285 . Locate the decimal point by counting off three places to the right, from the point between the 2 and the 8 , to obtain $2850.0-$ the antilog of 3.4548 .

In the foregoing example, if the logarithm had been -2 +.4548 , the procedure would have been the same except for the location of the decimal point. The decimal point in this example would be located by starting at the point between the 2 and the 8 , and counting two places to the left to obtain 0.0285 -the antilog of $-2+.4548$.

## (D) Multiplication

Numbers are multiplied by adding their logarithms and finding the antilog of the sum. For example, to multiply $682 \times 497$, proceed as follows:

$$
\begin{aligned}
\log N & =\log 682+\log 497 \\
\log 682 & =2.8338 \\
+\log 497 & =\underline{2.6964} \\
\log N & =5.5302
\end{aligned}
$$

antilog $5.5302=339,000$.
To multiply $.02 \times .03 \times .5$, proceed as follows:

$$
\begin{aligned}
& \log \mathrm{N}=\log .02+\log .03+\log .5 \\
& \log .02=-2+.3010=8.3010-10 \\
& +\log .03=-2+.4771=8.4771-10 \\
& +\log .5=-1+.6990=\underline{9.6990-10} \\
& \log \mathrm{~N}=26.4771-30 \\
& =-4+.4771
\end{aligned}
$$

$$
\text { antilog }-4+.4771=.0003
$$

## (E) Division

Numbers are divided by subtracting the logarithm of the divisor from the logarithm of the dividend, and finding the antilog of the difference. For example, to divide 39,200 by 27.2, proceed as follows:

$$
\begin{aligned}
\log N & =\log 39,200-\log 27.2 \\
\log 39,200 & =4.5933 \\
-\log 27.2 & =\underline{1.4346} \\
\log N & =\underline{3.1587}
\end{aligned}
$$

antilog $3.1587=1441$

To divide .3 by .007 , proceed as follows:

$$
\begin{aligned}
& \log \mathrm{N}=\log .3-\log .007 \\
& \log .3=-1+.4771=9.4771-10 \\
& -\log .007=-3+.8451=7.8451-10 \\
& \log N=1.6320-0 \\
& \text { antilog } 1.6320=42.86
\end{aligned}
$$

## (F) Raising to Powers

A given number can be raised to any power by multiplying the logarithm of the given number by the power to which the number is to be raised, and finding the antilog of the product. For example, to raise 39.7 to the third power, proceed as follows:

$$
\begin{aligned}
\log \mathrm{N} & =\log 39.7 \times 3 \\
\log 39.7 & =1.5988 \\
\log \mathrm{~N} & =1.5988 \times 3 \\
& =4.7964 \\
\text { antilog } 4.7964 & =62,570
\end{aligned}
$$

## (G) Extracting Roots

Any root can be extracted from a given number by dividing the logarithm of the given number by the index of the root, and finding the antilog of the quotient. For example, to extract the cube root of 149 , proceed as follows:

$$
\log N=\log 149 \div 3
$$

$\log 149=2.1732$

$$
\begin{aligned}
\log \mathrm{N} & =2.1732 \div 3 \\
& =0.7244
\end{aligned}
$$

antilog $0.7244=5.301$

Table XXXII. Common Logarithms

| $\mathbf{N}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 10 | 0000 | 0043 | 0086 | 0128 | 0170 | 0212 | 0253 | 0294 | 0334 | 0374 | 4 | 8 | 12 | 17 | 21 | 25 | 29 | 33 | 37 |
| 11 | 0414 | 0453 | 0492 | 0531 | 0569 | 0607 | 0645 | 0682 | 0719 | 0755 | 4 | 8 | 11 | 15 | 19 | 23 | 26 | 30 | 34 |
| 12 | 0792 | 0828 | 0864 | 0899 | 0934 | 0969 | 1004 | 1038 | 1072 | 1106 | 3 | 7 | 10 | 14 | 17 | 21 | 24 | 28 | 31 |
| 13 | 1139 | 1173 | 1206 | 1239 | 1271 | 1303 | 1335 | 1367 | 1399 | 1430 | 3 | 6 | 10 | 13 | 16 | 19 | 23 | 26 | 29 |
| 14 | 1461 | 1492 | 1523 | 1553 | 1584 | 1614 | 1644 | 1673 | 1703 | 1732 | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 24 | 27 |
| 15 | 1761 | 1790 | 1818 | 1847 | 1875 | 1903 | 1931 | 1959 | 1987 | 2014 | 3 | 6 | 8 | 11 | 14 | 17 | 20 | 22 | 25 |
| 16 | 2041 | 2068 | 2095 | 2122 | 2148 | 2175 | 2201 | 2227 | 2253 | 2279 | 3 | 5 | 8 | 11 | 13 | 16 | 18 | 21 | 24 |
| 17 | 2304 | 2330 | 2355 | 2380 | 2405 | 2430 | 2455 | 2480 | 2504 | 2529 | 2 | 5 | 7 | 10 | 12 | 15 | 17 | 20 | 22 |
| 18 | 2553 | 2577 | 2601 | 2625 | 2648 | 2672 | 2695 | 2718 | 2742 | 2765 | 2 | 5 | 7 | 9 | 12 | 14 | 16 | 19 | 21 |
| 19 | 2788 | 2810 | 2833 | 2856 | 2878 | 2900 | 2923 | 2945 | 2967 | 2989 | 2 | 4 | 7 | 9 | 11 | 13 | 16 | 18 | 20 |
| 20 | 3010 | 3032 | 3054 | 3075 | 3096 | 3118 | 3139 | 3160 | 3181 | 3201 | 2 | 4 | 6 | 8 | 11 | 13 | 15 | 17 | 19 |
| 21 | 3222 | 3243 | 3263 | 3284 | 3304 | 3324 | 3345 | 3365 | 3385 | 3404 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 |
| 22 | 3424 | 3444 | 3464 | 3483 | 3502 | 3522 | 3541 | 3560 | 3579 | 3598 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 15 | 17 |
| 23 | 3617 | 3636 | 3655 | 3674 | 3692 | 3711 | 3729 | 3747 | 3766 | 3784 | 2 | 4 | 6 | 7 | 9 | 11 | 13 | 15 | 17 |
| 24 | 3802 | 3820 | 3838 | 3856 | 3874 | 3892 | 3909 | 3927 | 3945 | 3962 | 2 | 4 | 5 | 7 | 9 | 11 | 12 | 14 | 16 |
| 25 | 3979 | 3997 | 4014 | 4031 | 4048 | 4065 | 4082 | 4099 | 4116 | 4133 | 2 | 3 | 5 | 7 | 9 | 10 | 12 | 14 | 15 |
| 26 | 4150 | 4166 | 4183 | 4200 | 4216 | 4232 | 4249 | 4265 | 4281 | 4298 | 2 | 3 | 5 | 7 | 8 | 10 | 11 | 14 13 | 15 |
| 27 | 4314 | 4330 | 4346 | 4362 | 4378 | 4393 | 4409 | 4425 | 4440 | 4456 | 2 | 3 | 5 | 6 | 8 | 9 | 11 | 13 | 14 |
| 28 | 4472 | 4487 | 4502 | 4518 | 4533 | 4548 | 4564 | 4579 | 4594 | 4609 | 2 | 3 | 5 | 6 | 8 | 9 | 11 | 12 | 14 14 |
| 29 | 4624 | 4639 | 4654 | 4669 | 4683 | 4698 | 4713 | 4728 | 4742 | 4757 | 1 | 3 | 4 | 6 | 7 | 9 | 10 | 12 | 13 |
| 30 | 4771 | 4786 | 4800 | 4814 | 4829 | 4843 | 4857 | 4871 | 4886 | 4900 | 1 | 3 | 4 | 6 | 7 | 9 | 10 | 11 | 13 |
| 31 | 4914 | 4928 | 4942 | 4955 | 4969 | 4983 | 4997 | 5011 | 5024 | 5038 | 1 | 3 | 4 | 6 | 7 | 8 | 10 | 11 | 12 |
| 32 | 5051 | 5065 | 5079 | 5092 | 5105 | 5119 | 5132 | 5145 | 5159 | 5172 | 1 | 3 | 4 | 5 | 7 | 8 | 9 | 11 | 12 |
| 33 | 5185 | 5198 | 5211 | 5224 | 5237 | 5250 | 5263 | 5276 | 5289 | 5302 | 1 | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 12 12 |
| 34 | 5315 | 5328 | 5340 | 5353 | 5366 | 5378 | 5391 | 5403 | 5416 | 5428 | 1 | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 11 |
| $\mathbf{N}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | po | ion | Par |  |  |  |

Table XXXII. Common Logarithms-(Cont'd)

| $\mathbf{N}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 35 | 5441 | 5453 | 5465 | 5478 | 5490 | 5502 | 5514 | 5527 | 5539 | 5551 | 1 | 2 | 4 | 5 | 6 | 7 | 9 | 10 | 11 |
| 36 | 5563 | 5575 | 5587 | 5599 | 5611 | 5623 | 5635 | 5647 | 5658 | 5670 | 1 | 2 | 4 | 5 | 6 | 7 | 8 | 10 | 11 |
| 37 | 5682 | 5694 | 5705 | 5717 | 5729 | 5740 | 5752 | 5763 | 5775 | 5786 | 1 | 2 | 3 | 5 | 6 | 7 | 8 | 9 | 10 |
| 38 | 5798 | 5809 | 5821 | 5832 | 5843 | 5855 | 5866 | 5877 | 5888 | 5899 | 1 | 2 | 3 | 5 | 6 | 7 | 8 | 9 | 10 |
| 39 | 5911 | 5922 | 5933 | 5944 | 5955 | 5966 | 5977 | 5988 | 5999 | 6010 | 1 | 2 | 3 | 4 | 5 | 7 | 8 | 9 | 10 |
| 40 | 6021 | 6031 | 6042 | 6053 | 6064 | 6075 | 6085 | 6096 | 6107 | 6117 | 1 | 2 | 3 | 4 | 5 | 6 | 8 | 9 | 10 |
| 41 | 6128 | 6138 | 6149 | 6160 | 6170 | 6180 | 6191 | 6201 | 6212 | 6222 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 42 | 6232 | 6243 | 6253 | 6263 | 6274 | 6284 | 6294 | 6304 | 6314 | 6325 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 43 | 6335 | 6345 | 6355 | 6365 | 6375 | 6385 | 6395 | 6405 | 6415 | 6425 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 44 | 6435 | 6444 | 6454 | 6464 | 6474 | 6484 | 6493 | 6503 | 6513 | 6522 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 45 | 6532 | 6542 | 6551 | 6561 | 6571 | 6580 | 6590 | 6599 | 6609 | 6618 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 46 | 6628 | 6637 | 6646 | 6656 | 6665 | 6675 | 6684 | 6693 | 6702 | 6712 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 7 | 8 |
| 47 | 6721 | 6730 | 6739 | 6749 | 6758 | 6767 | 6776 | 6785 | 6794 | 6803 | 1 | 2 | 3 | 4 | 5 | 5 | 6 | 7 | 8 |
| 48 | 6812 | 6821 | 6830 | 6839 | 6848 | 6857 | 6866 | 6875 | 6884 | 6893 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 8 |
| 49 | 6902 | 6911 | 6920 | 6928 | 6937 | 6946 | 6955 | 6964 | 6972 | 6981 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 8 |
| 50 | 6990 | 6998 | 7007 | 7016 | 7024 | 7033 | 7042 | 7050 | 7059 | 7067 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 7 | 8 |
| 51 | 7076 | 7084 | 7093 | 7101 | 7110 | 7118 | 7126 | 7135 | 7143 | 7152 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 7 | 8 |
| 52 | 7160 | 7168 | 7177 | 7185 | 7193 | 7202 | 7210 | 7218 | 7226 | 7235 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 7 | 7 |
| 53 | 7243 | 7251 | 7259 | 7267 | 7275 | 7284 | 7292 | 7300 | 7308 | 7316 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 6 | 7 |
| 54 | 7324 | 7332 | 7340 | 7348 | 7356 | 7364 | 7372 | 7380 | 7388 | 7396 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 6 | 7 |
| 55 | 7404 | 7412 | 7419 | 7427 | 7435 | 7443 | 7451 | 7459 | 7466 | 7474 | 1 | 2 | 2 | 3 | 4 | 5 | 5 | 6 | 7 |
| 56 | 7482 | 7490 | 7497 | 7505 | 7513 | 7520 | 7528 | 7536 | 7543 | 7551 | 1 | 2 | 2 | 3 | 4 | 5 | 5 | 6 | 7 |
| 57 | 7559 | 7566 | 7574 | 7582 | 7589 | 7597 | 7604 | 7612 | 7619 | 7627 | 1 | 2 | 2 | 3 | 4 | 5 | 5 | 6 | 7 |
| 58 | 7634 | 7642 | 7649 | 7657 | 7664 | 7672 | 7679 | 7686 | 7694 | 7701 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 |
| 59 | 7709 | 7716 | 7723 | 7731 | 7738 | 7745 | 7752 | 7760 | 7767 | 7774 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 |
|  |  |  |  |  |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| $\mathbf{N}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |  |  |  | Pr |  | Pa |  |  |  |

Table XXXII. Common Logarithms-(Cont'd)

| $\mathbf{N}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Paris |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 60 | 7782 | 7789 | 7796 | 7803 | 7810 | 7818 | 7825 | 7832 | 7839 | 7846 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 6 |
| 61 | 7853 | 7860 | 7868 | 7875 | 7882 | 7889 | 7896 | 7903 | 7910 | 7917 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 6 |
| 62 | 7924 | 7931 | 7938 | 7945 | 7952 | 7959 | 7966 | 7973 | 7980 | 7987 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 6 |
| 63 | 7993 | 8000 | 8007 | 8014 | 8021 | 8028 | 8035 | 8041 | 8048 | 8055 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 64 | 8062 | 8069 | 8075 | 8082 | 8089 | 8096 | 8102 | 8109 | 8116 | 8122 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 65 | 8129 | 8136 | 8142 | 8149 | 8156 | 8162 | 8169 | 8176 | 8182 | 8189 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 66 | 8195 | 8202 | 8209 | 8215 | 8222 | 8228 | 8235 | 8241 | 8248 | 8254 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 67 | 8261 | 8267 | 8274 | 8280 | 8287 | 8293 | 8299 | 8306 | 8312 | 8319 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 68 | 8325 | 8331 | 8338 | 8344 | 8351 | 8357 | 8363 | 8370 | 8376 | 8382 | 1 | 1 | 2 | 3 | 3 | 4 | 4 | 5 | 6 |
| 69 | 8388 | 8395 | 8401 | 8407 | 8414 | 8420 | 8426 | 8432 | 8439 | 8445 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 6 |
| 70 | 8451 | 8457 | 8463 | 8470 | 8476 | 8482 | 8488 | 8494 | 8500 | 8506 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 6 |
| 71 | 8513 | 8519 | 8525 | 8531 | 8537 | 8543 | 8549 | 8555 | 8561 | 8567 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 72 | 8573 | 8579 | 8585 | 8591 | 8597 | 8603 | 8609 | 8615 | 8621 | 8627 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 73 | 8633 | 8639 | 8645 | 8651 | 8657 | 8663 | 8669 | 8675 | 8681 | 8686 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 74 | 8692 | 8698 | 8704 | 8710 | 8716 | 8722 | 8727 | 8733 | 8739 | 8745 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 75 | 8751 | 8756 | 8762 | 8768 | 8774 | 8779 | 8785 | 8791 | 8797 | 8802 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 5 | 5 |
| 76 | 8808 | 8814 | 8820 | 8825 | 8831 | 8837 | 8842 | 8848 | 8854 | 8859 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 5 | 5 |
| 77 | 8865 | 8871 | 8876 | 8882 | 8887 | 8893 | 8899 | 8904 | 8910 | 8915 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 78 | 8921 | 8927 | 8932 | 8938 | 8943 | 8949 | 8954 | 8960 | 8965 | 8971 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 79 | 8976 | 8982 | 8987 | 8993 | 8998 | 9004 | 9009 | 9015 | 9020 | 9025 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 80 | 9031 | 9036 | 9042 | 9047 | 9053 | 9058 | 9063 | 9069 | 9074 | 9079 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 81 | 9085 | 9090 | 9096 | 9101 | 9106 | 9112 | 9117 | 9122 | 9128 | 9133 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 82 | 9138 | 9143 | 9149 | 9154 | 9159 | 9165 | 9170 | 9175 | 9180 | 9186 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 83 | 9191 | 9196 | 9201 | 9206 | 9212 | 9217 | 9222 | 9227 | 9232 | 9238 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 84 | 9243 | 9248 | 9253 | 9258 | 9263 | 9269 | 9274 | 9279 | 9284 | 9289 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | - | 9 |  |  |  | op | ion | Pa |  |  |  |

Table XXXII. Common Logarithms-(Cont'd)

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional Parts |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 85 | 9294 | 9299 | 9304 | 9309 | 9315 | 9320 | 9325 | 9330 | 9335 | 9340 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 86 | 9345 | 9350 | 9355 | 9360 | 9365 | 9370 | 9375 | 9380 | 9385 | 9390 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 87 | 9395 | 9400 | 9405 | 9410 | 9415 | 9420 | 9425 | 9430 | 9435 | 9440 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 88 | 9445 | 9450 | 9455 | 9460 | 9465 | 9469 | 9474 | 9479 | 9484 | 9489 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 89 | 9494 | 9499 | 9504 | 9509 | 9513 | 9518 | 9523 | 9528 | 9533 | 9538 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 90 | 9542 | 9547 | 9552 | 9557 | 9562 | 9566 | 9571 | 9576 | 9581 | 9586 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 91 | 9590 | 9595 | 9600 | 9605 | 9609 | 9614 | 9619 | 9624 | 9628 | 9633 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 92 | 9638 | 9643 | 9647 | 9652 | 9657 | 9661 | 9666 | 9671 | 9675 | 9680 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 93 | 9685 | 9689 | 9694 | 9699 | 9703 | 9708 | 9713 | 9717 | 9722 | 9727 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 94 | 9731 | 9736 | 9741 | 9745 | 9750 | 9754 | 9759 | 9763 | 9768 | 9773 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 95 | 9777 | 9782 | 9786 | 9791 | 9795 | 9800 | 9805 | 9809 | 9814 | 9818 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 96 | 9823 | 9827 | 9832 | 9836 | 9841 | 9845 | 9850 | 9854 | 9859 | 9863 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 97 | 9868 | 9872 | 9877 | 9881 | 9886 | 9890 | 9894 | 9899 | 9903 | 9908 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | $4$ | $4$ |
| 98 | 9912 | 9917 | 9921 | 9926 | 9930 | 9934 | 9939 | 9943 | 9948 | 9952 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 99 | 9956 | 9961 | 9965 | 9969 | 9974 | 9978 | 9983 | 9987 | 9991 | 9996 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 3 | 4 |
| $\mathbf{N}$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | op | ion | Par |  |  |  |

## Miscellaneous

## 78. POWER CONSUMPTION OF HOME ELECTRICAL EQUIPMENT

The power consumption for many items of home electrical equipment by an average family is given in Table XXXIII. The approximate usage of each item is also listed where applicable.

Table XXXIII. Power Consumption of Home Electrical Equipment

| Item | Approx. Kwh per Month | Remarks |
| :---: | :---: | :---: |
| Blanket (automatic) | 15 | 8 hr . per day (used 7 mo .) |
| Clock | $11 / 2$ |  |
| Coffee Maker | 15 | 25 hr . per mo. |
| Dishwasher | 25 | $11 / 2$ washings per day |
| Dryer (clothes) | 50 | 10 hr . per mo. (family of 4) |
| Fan (10-inch) | 1 | 25 hr . per mo. |
| Food Freezer | 40 | $8 \mathrm{cu} . \mathrm{ft}$. |
| Garbage Disposal Unit | 3/4 | 4 min . per day |
| Iron | 6 | 12 hr . per mo. |
| Ironer | 10 | 10 hr . per mo. (family of 4) |
| Lighting | 65 |  |
| Mixer | 3/4 | 5 hr . per mo. |
| culator fan) | 30 | (200-500 KW-hours per year) |
| Radio | 10 | 130 hr . per mo. |
| Range | 90 | (Family of 4) |
| Refrigerator | 22 | $8 \mathrm{cu} . \mathrm{ft}$. |
| Roaster | 12 | 16 hr . per mo. |
| Sandwich Grill | 4 | 5 hr . per mo. |
| Sewing Machine | 1 |  |
| Television | 18 | 90 hr . per mo. |
| Toaster | 3 | 3 hr . per mo. |
| Vacuum Cleaner (upright) | 21/4 | 6 hr . per mo. |
| Vacuum Cleaner (tank) | $31 / 4$ | 6 hr . per mo. |
| Washer (wringer-type) | 2 | 12 hr . per mo. (family of 4) |
| Washer (automatic) | 3 | 12 hr . per mo. (family of 4) |
| Water Heater | 350 | (Family of 4) |

## 79. TEMPERATURE CONVERSION

The nomograph in Fig. 145 can be used to convert from degrees Fahrenheit to degrees Celsius (or vice versa) for any temperature between absolute zero and $540^{\circ} \mathrm{F}$. $\left(281^{\circ} \mathrm{C}\right)$. The term Celsius was officially adopted, in place of centigrade, by international agreement in 1948; however, acceptance of the new term has been slow in Europe, and still slower in the United States. Actually, Celsius and centigrade scales differ slightly-the Celsius scale is based on $0^{\circ}$ at the triple point of water $\left(.01^{\circ} \mathrm{C}\right)$, and centigrade has $0^{\circ}$ at the freezing point of water. For all practical purposes, though, the two terms are interchangeable.

Two absolute temperature scales are also in use. The Fahrenheit absolute scale is called the Rankine- $0^{\circ}$ Rankine equals $-459.67^{\circ}$ Fahrenheit. The Celsius absolute scale is the Kelvin- $0^{\circ}$ Kelvin equals $-273.16^{\circ}$ Celsius (or centigrade).

The following formulas can be used to convert from any temperature to the other:

$$
\begin{aligned}
{ }^{\circ} \mathrm{F} . & =\left({ }^{\circ} \mathrm{C} . \times 9 / 5\right)+32 \\
{ }^{\circ} \mathrm{F} . & ={ }^{\circ} \mathrm{R} .-459.67 \\
{ }^{\circ} \mathrm{F} . & =9 / 5\left({ }^{\circ} \mathrm{K} .-273.16\right)+32 \\
{ }^{\circ} \mathrm{C} . & =5 / 9\left({ }^{\circ} \mathrm{F} .-32\right) \\
{ }^{\circ} \mathrm{C} . & ={ }^{\circ} \mathrm{K} .-273.16 \\
{ }^{\circ} \mathrm{C} . & =5 / 9\left({ }^{\circ} \mathrm{R} .-491.67\right) \\
{ }^{\circ} \mathrm{R} . & ={ }^{\circ} \mathrm{F} .+459.67 \\
{ }^{\circ} \mathrm{R} . & =\left({ }^{\circ} \mathrm{C} . \times 9 / 5\right)+491.67 \\
{ }^{\circ} \mathrm{R} . & =9 / 5\left({ }^{\circ} \mathrm{K} .-273.16\right)+491.67 \\
{ }^{\circ} \mathrm{K} . & ={ }^{\circ} \mathrm{C} .+273.16 \\
{ }^{\circ} \mathrm{K} . & =5 / 9\left({ }^{\circ} \mathrm{F}-32\right)+273.16 \\
{ }^{\circ} \mathrm{K} . & =5 / 9\left({ }^{\circ} \mathrm{R} .-491.67\right)+273.16
\end{aligned}
$$

## Temperature Nomograph

(200

Fig. 145

## 80. CHARACTERISTICS OF THE ELEMENTS

A list of all the known elements (103) is given in Table XXXIV. The symbol, atomic number, and atomic weight are included for each element. Where known, the melting and boiling point of each element is also given. A value shown in parentheses indicates the value is approximated; the asterisk (*) indicates the mass number of the longest-lived of the known available forms of the element, usually synthetic; < indicates the value may be lower; > indicates the value may be higher.

Table XXXIV. Characteristics of the Elements

| Element | Symbol | Atomic Number | Atomic Weight | Melting <br> Point ${ }^{\circ} \mathrm{C}$ | Boiling Point ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Actinium | Ac | 89 | *227 |  |  |
| Aluminum | Al | 13 | 26.97 | 660.1 | 1800 |
| Americium | Am | 95 | *243 |  |  |
| Antimony | Sb | 51 | 121.76 | 630.5 | 1380 |
| Argon | A | 18 | 39.944 | -189.2 | $-185.7$ |
| Arsenic | As | 33 | 74.91 | (820) | 615 |
| Astatine | At | 85 | *210 |  |  |
| Barium | Ba | 56 | 137.36 | 850 | 1140 |
| Berkelium | Bk | 97 | *249 |  |  |
| Beryllium | Be | 4 | 9.013 | 1350 | (1500) |
| Bismuth | Bi | 83 | 209.00 | 271.3 | 1450 |
| Boron | B | 5 | 10.82 | 2300 | 2550 |
| Bromine | Br | 35 | 79.916 | -7.2 | 58.8 |
| Cadmium | Cd | 48 | 112.41 | 320.9 | 766 |
| Calcium | Ca | 20 | 40.08 | 810 | 1170 |
| Californium | Cf | 98 | *249 |  |  |
| Carbon | C | 6 | 12.01 | $>3500$ | (4200) |
| Cerium | Ce | 58 | 140.13 | 640 | 1400 |
| Cesium | Cs | 55 | 132.91 | 28 | 670 |
| Chlorine | Cl | 17 | 35.457 | -101.6 | -34.7 |
| Chromium | Cr | 24 | 52.01 | 1615 | 2200 |
| Cobalt | Co | 27 | 58.94 | 1492 | 3000 |
| Copper | Cu | 29 | 63.54 | 1083 | 2300 |
| Curium | Cm | 96 | 247 | - |  |
| Dysprosium | Dy | 66 | 162.46 | - |  |
| Einsteinium | E | 99 | *254 | - |  |
| Erbium | Er | 68 | 167.2 | - | - |
| Europium | Eu | 63 | 152.0 | - |  |
| Fermium | Fm | 100 | *255 |  | - |
| Fluorine | F | 9 | 19.00 | -223 | $-187$ |
| Francium | Fr | 87 | *223 |  | - |
| Gadolinium | Gd | 64 | 156.9 |  |  |
| Gallium | Ga | 31 | 69.72 | 29.7 | $>1600$ |
| Germanium | Ge | 32 | 72.60 | 958.5 | (2700) |
| Gold | Au | 79 | 197.0 | 1063 | 2600 |

Table XXXIV. Characteristics of the Elements-(Cont'd)

| Element | Symbol | Atomic Number | Atomic Weight | Melting Point ${ }^{\circ} \mathrm{C}$ | Boiling <br> Point ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Halfnium | Hf | 72 | 178.6 | 1500 | ( $>3200$ ) |
| Helium | He | 2 | 4.003 | $<-271.4$ | -268.94 |
| Holmium | Ho | 67 | 164.94 |  | , |
| Hydrogen | H | 1 | 1.0080 | -259.14 | -252.8 |
| Indium | In | 49 | 114.76 | 155 | $>1450$ |
| lodine | 1 | 53 | 126.91 | 113.5 | 184.35 |
| Iridium | Ir | 77 | 192.2 | 2443 | ( $>4800$ ) |
| Iron | Fe | 26 | 55.85 | 1533 | 3000 |
| Krypton | Kr | 36 | 83.8 | -169 | $-151.8$ |
| Lanthanum | La | 57 | 138.92 | 826 | 1800 |
| Lawrencium | Lw | 103 | - |  |  |
| Lead | Pb | 82 | 207.21 | 327.4 | 1620 |
| Lithium | Li | 3 | 6.940 | 186 | $>1200$ |
| Lutetium | Lu | 71 | 174.99 |  |  |
| Magnesium | Mg | 12 | 24.32 | 651 | 1100 |
| Manganese | Mn | 25 | 54.94 | 1260 | 1800 |
| Mendelevium | Mr | 101 | *256 | -38.87 |  |
| Mercury | Hg | 80 | 200.61 | $-38.87$ | 356.9 |
| Molybdenum | Mo | 42 | 95.95 | 2620 | 3700 |
| Neodymium | Nd | 60 | 144.27 | 840 |  |
| Neon | Ne | 10 | 20.183 | -248.67 | -245.9 |
| Neptunium | Np | 93 | *237 | 639 | 2900 |
| Nickel | Ni | 28 | 58.69 | 1453 | 2900 |
| Niobium | Nb | 41 | 92.91 | 2500 | 3200 |
| Nitrogen | N | 7 | 14.008 | -209.86 | -195.81 |
| Nobelium | No | 102 | 251 | - |  |
| Osmium | Os | 76 | 190.2 | 2700 | ( $>5300$ ) |
| Oxygen | $\bigcirc$ | 8 | 16.000 | -218.4 | -183 |
| Palladium | Pd | 46 | 106.7 | 1552 | 2200 |
| Phosphorus | P | 15 | 30.975 | 44.1 | 280 |
| Platinum | Pt | 78 | 195.23 | 1769 | 4300 |
| Plutonium | Pu | 94 | 242 |  |  |
| Polonium | Po | 84 | 210 |  |  |
| Potassium | K | 19 | 39.100 | 62.3 | 760 |
| Praseodymium | Pr | 59 | 140.92 | 940 |  |
| Promethium | Pm | 61 | *145 | - | - |
| Protactinium | Pa | 91 | *231 |  |  |
| Radium | Ra | 88 | 226.05 | 960 | 1140 |
| Radon | Rn | 86 | 222 | -110 |  |
| Rhenium | Re | 75 | 186.31 | (3000) |  |
| Rhodium | Rh | 45 | 102.91 | 1960 | $>2500$ |
| Rubidium | Rb | 37 | 85.48 | 38.5 | 700 |
| Ruthenium | Ru | 44 | 101.1 | 2500 | $>2700$ |
| Samarium | Sm | 62 | 150.43 | $>1300$ |  |
| Scandium | Sc | 21 | 44.96 | 1200 | (2400) |
| Selenium | Se | 34 | 78.96 | 220 | 688 |
| Silicon | Si | 14 | 28.09 | 1420 | 2600 |
| Silver | Ag | 47 | 107.880 | 960.8 | 1950 |
| Sodium | Na | 11 | 22.997 | 97.5 | 880 |
| Strontium | Sr | 38 | 87.63 | 800 | 1150 |

Table XXXIV. Characteristics of the Elements-(Cont'd)

| Element | Symbol | Atomic <br> Number | Atomic <br> Weight | Melting <br> Point ${ }^{\circ} \mathbf{C}$ | Boiling <br> Point ${ }^{\circ} \mathrm{C}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Sulfur | S | 16 | 32.066 | 113.119 | 444.6 |
| Tantalum | Ta | 73 | 180.95 | 3005 | $(>4100)$ |
| Technetium | Tc | 43 | $* 99$ | - | -1390 |
| Tellurium | Te | 52 | 127.61 | 452 | 1390 |
| Terbium | Tb | 65 | 158.93 | 327 | - |
| Thallium | TI | 81 | 204.39 | 303.5 | 1650 |
| Thorium | Th | 90 | 232.12 | 1845 | $>3000$ |
| Thulium | Tm | 69 | 168.94 | - | 3500 |
| Tin | Sn | 50 | 118.70 | 231.9 | 2260 |
| Titanium | Ti | 22 | 47.90 | 1820 | $>3000)$ |
| Tungsten | W | 74 | 183.92 | 3380 | 5900 |
| Uranium | $\mathbf{U}$ | 92 | 238.07 | 1133 | -50.95 |
| Vanadium | $\mathbf{V}$ | 23 | 1735 | $(3000)$ |  |
| Xenon | Xe | 54 | 131.3 | -140 | -109.1 |
| Ytterbium | Yb | 70 | 173.04 | - |  |
| Yttrium | Y | 39 | 88.92 | 1490 | $(2500)$ |
| Zinc | Zn | 30 | 65.38 | 419.47 | $\mathbf{9 0 7}$ |
| Zirconium | Zr | 40 | 91.22 | 1750 | $>2900$ |

## 81. MEASURES AND WEIGHTS

## (A) Linear Measure

| 1 inch $=1000$ mils | 1 furlong $=40$ rods |
| :--- | :--- | :--- |
| 1 hand $=4$ inches | 1 statute mile $=8$ furlongs |
| 1 foot $=12$ inches | 1 statute mile $=5,280$ feet |
| 1 yard $=3$ feet | 1 nautical mile $=6076.1$ feet $\dagger$ |
| 1 fathom $=6$ fee $\dagger$ | 1 nautical mile $=1.1508$ statute miles |
| 1 rod $=51 / 2$ yards | 1 league $=3$ miles |

(B) Square Measure

| 1 sq. foot | $=144$ sq. inches | 1 township $=6$ miles sq. ( 36 sq. miles) |
| :---: | :---: | :---: |
| 1 sq. yard | $=9 \mathrm{sq}$. feet | 1 acre $=160$ sq. rods |
| 1 sq. rod | $=301 / 4$ sq. yards | 1 acre $=43,560$ sq. feet |
| 1 section (o | $=1 \mathrm{sq}$. mile | 1 sq. mile $=640$ acres |
| (C) Volume Measure |  |  |
| 1 cu. fo | . 728 cu . inches | 1 cu. yard $=27 \mathrm{cu}$. feet |

1 U.S. gallon $=231 \mathrm{cu}$. inches
(D) Liquid Measure

| 1 pint | $=4$ gills | 1 barrel $=311 / 2$ gallons |
| :--- | :--- | :--- |
| 1 quart | $=2$ pints | 1 hogshead $=2$ barrels ( 63 gallons) |
| 1 gallon | $=4$ quarts | 1 tun |
| 1 barrel (petroleum) | $=42$ gallons |  |

## (E) Dry Measure

1 quart $=2$ pints $=67.2006 \mathrm{cu}$. in. $\quad 1$ bushel $=4$ pecks $=2150.419 \mathrm{cu}$. in.
1 peck $=8$ quarts $=537.605 \mathrm{cu} . \mathrm{in} . \quad 1$ barrel $=2.381$ bushels $=7056 \mathrm{cu} . \mathrm{in}$.

## (F) Avoirdupois Weight

(For other than drugs, gold, silver, etc.)

| 1 dram (dr.) $=27.3437$ grains* | 1 hundredweight (cwt.) $=4$ quarters |
| :---: | :---: |
| 1 ounce (oz.) $=16$ drams | 1 ton (tn.) = 20 cwts . |
| 1 pound (lb.) = 16 ounces | 1 short ton $=2000$ pounds |
| 1 quarter $=25$ pounds | 1 long ton $=2240$ pounds |

1 pound avdp. $=7000$ grains $=453.59$ grams $=1.2153$ pounds troy

## (G) Troy Weight

(For gold, silver, etc.)
1 pennyweight (dwt.) $=24$ grains* $\quad 1$ ounce troy (oz.t.) $=20$ pennyweights
1 pound troy (lb.t.) $=12$ ounces troy $=240$ pennyweights $=5760$ grains
(H) Apothecaries' Weight
(For drugs)
1 scruple (s. ap.) $=20$ grains* $\quad 1$ dram apoth. (dr. ap.) $=3$ scruples
1 ounce apoth. (oz. ap.) $=8$ drams apoth.
1 pound apoth. (lb. ap.) $=12$ ounces apoth.
$=96$ drams apoth.
$=288$ scruples
$=5760$ drams

## 82. METRIC EQUIVALENTS

(A) Length

| 1 centimeter | $=0.3937$ inch |  | 1 inch |
| :--- | :--- | :--- | :--- |
| 1 meter | $=3.2808$ feet |  | $=2.5400$ centimeters (cm.) |
| 1 meter | $=1.0936$ yards |  | 1 yard |
| 1 kilometer | $=0.6214$ miles |  | $=0.3048$ meter |
|  | 1 mile (statute) | $=1.6093$ kilometers $(k m)$. |  |

(B) Area

| 1 sq. $\mathrm{cm} .=0.1550$ sq. inch | 1 sq. inch $=6.4516$ sq. cm. |
| :--- | :--- |
| 1 sq. meter $=10.7639$ sq. feet | 1 sq. foot $=0.0929$ sq. meter |
| 1 sq. meter $=1.1960$ sq. yards | 1 sq. yard $=0.8361$ sq. meter |
| 1 hectare $=2.4710$ acres | l acre $=0.4047$ hectare |
| 1 sq. $\mathrm{km} .=0.3861$ sq. mile | l sq. mile $=2.5900$ sq. km. |

[^8]
## (C) Volume

$1 \mathrm{cu} . \mathrm{cm} .=0.0610 \mathrm{cu}$. inch
1 cu. inch $=16.3872 \mathrm{cu} . \mathrm{cm}$.
1 cu. meter $=35.3145 \mathrm{cu}$. feet
1 cu . foot $=0.0283 \mathrm{cu}$. meter
1 cu. meter $=1.3079 \mathrm{cu}$. yards
1 cu. yard $=0.7646 \mathrm{cu}$. meter

## (D) Capacity

| 1 liter $=61.0250 \mathrm{cu}$. inches | 1 liter $=0.9081$ quart (dry) |
| :--- | :--- |
| 1 liter $=0.0353 \mathrm{cu}$. feet | 1 liter $=2.2046$ pounds of water @ $4^{\circ} \mathrm{C}$ |
| 1 liter $=0.2642$ gallon (U.S.) | 1 cu. inch $=0.0164$ liter |
| 1 liter $=0.0284$ bushel (U.S.) | 1 cu. foot $=28.3162$ liters |
| 1 liter $=1000.027 \mathrm{cu} . \mathrm{cm}$. | 1 gallon $=3.7853$ liters |
| 1 liter $=1.056$ quarts (liquid) | 1 bushel $=35.2383$ liters |

## (E) Weight

| 1 gram | $=15.4324$ grains | 1 grain | $=0.0648 \mathrm{gram}$ |
| :---: | :---: | :---: | :---: |
| 1 gram | $=0.0353$ ounce avdp. | 1 ounce (avd | $=28.3495 \mathrm{grams}$ |
| 1 kg . | $=2.2046$ pounds avdp. | 1 pound (avo | $)=0.4536 \mathrm{~kg}$. |
| 1 kg . | $=0.0011$ ton (short) | 1 ton (short) | $=907.1848 \mathrm{~kg}$. |
| 1 ton (me | $=1.1023$ tons (short) | 1 ton (short) | $=0.9072$ ton (metric) |
| 1 ton (me | $=0.9842$ ton (long) | 1 ton (long) | $=1.0160$ ton (metric) |

## (F) Pressure

$$
\begin{array}{ll}
1 \text { kg. per sq. } \mathrm{cm} . & =14.223 \mathrm{lbs} . \text { per sq. } \mathrm{inch} \\
1 \mathrm{lb} . \text { per sq. } \mathrm{inch} & =0.0703 \mathrm{~kg} . \text { per sq. } \mathrm{cm} . \\
1 \mathrm{~kg} . \text { per sq. meter } & =0.2048 \mathrm{lb} . \text { per sq. foot } \\
1 \mathrm{lb} . \text { per sq. foot } & =4.8824 \mathrm{~kg} . \text { per sq. meter } \\
1 \mathrm{~kg} . \text { per sq. } \mathrm{cm} . & =0.9678 \text { normal atmosphere } \\
1 \text { normal atmosphere }=1.0332 \mathrm{~kg} . \text { per sq. } \mathrm{cm} . \\
1 \text { normal atmosphere }=1.01325 \text { bars } \\
1 \text { normal atmosphere }=14.696 \mathrm{lbs} . \text { per sq. inch }
\end{array}
$$

## 83. WINDS

Table XXXV. Wind Designations

| Designation | Miles per hour | Designation | Miles per hour |
| :--- | :---: | :--- | :--- |
| Calm | Less than 1 | Moderate gale | 32 to 38 |
| Light air | 1 to 3 | Fresh gale | 39 to 46 |
| Light breeze | 4 to 7 | Strong gale | 47 to 54 |
| Gentle breeze | 8 to 12 | Whole gale | 55 to 63 |
| Moderate breeze | 13 to 18 | Storm | 64 to 72 |
| Fresh breeze | 19 to 24 | Hurricane | Above 72 |
| Strong breeze | 25 to 31 |  |  |

## 84. WEIGHT OF WATER

| 1 cubic inch | $=.0360$ pound |  | 1 imperial gallon $=10.0$ pounds |
| :--- | :--- | :--- | :--- |
| 12 cubic inches | $=.433$ pound |  | 11.2 imperial gallons $=112.0$ pounds |
| 1 cubic foot $=62.4$ pounds |  | 224 imperial gallons | $=2240.0$ pounds |
| 1 cubic foot $=7.48052$ U.S. gallons |  | 1 U.S. gallon | $=8.33$ pounds |
| 1.8 cubic feet $=112.0$ pounds |  | 13.45 U.S. gallons $=112.0$ pounds |  |
| 35.96 cubic feet $=2240.0$ pounds |  | 269.0 U.S. gallons $=2240.0$ pounds |  |

## 85. HYDRAULIC EQUATIONS

Lbs. per sq. in. $=0.434 \times$ head of water in feet
Head in feet $=2.31 \times$ lbs. per sq. inch
Approximate loss of head due to friction in clean iron pipes is:

$$
\frac{0.02 \times \mathrm{L} \times \mathrm{V}^{2}}{64.4 \mathrm{D}} \mathrm{ft}
$$

where,
L is the length of pipe in feet,
V is the velocity of flow in foot-pounds per second,
D is the diameter in feet.
In calculating the total head to be pumped against, it is common to consider this value as being equal to the sum of the friction head and the actual head.

$$
\text { Horsepower of waterfall }=\frac{62 \times \mathrm{A} \times \mathrm{V} \times \mathrm{H}}{33,000}
$$

where,
A is the cross section of water in square feet,
V is the velocity of flow in foot-pounds per minute,
$H$ is the head of fall in feet.

## 86. MISCELLANEOUS

## (A) Falling Object

The speed acquired by a falling object is determined by the formula:

$$
\mathrm{V}=32 \mathrm{t}
$$

where,
V is the velocity in feet per second, $t$ is the time in seconds.

The distance traveled by a falling object is determined by the formula:

$$
\mathrm{d}=16 \mathrm{t}^{2}
$$

where,
d is the distance traveled in feet,
t is the time in seconds.
(B) Speed of Sound

The speed of sound through air at $0^{\circ} \mathrm{C}$. is usually considered to be 1087.42 feet per second, and at normal temperature, 1130 feet per second. The speed of sound through any given temperature of air is determined by the formula:

$$
V=\frac{1087 \sqrt{(273+t)}}{16.52}
$$

where,
V is the speed in feet per second,
t is the temperature in degrees Celsius.

## (C) Cost of Operation

The cost per hour of operation of an electrical device is determined by the formula:

$$
\mathrm{C}=\frac{\mathrm{Wtc}}{1000}
$$

where,
C is the cost per hour of operation, $W$ is the wattage of the device,
$t$ is the time in hours,
c is the cost per kilowatt hour of electricity.

## (D) Conversion of Matter Into Energy

The conversion of matter into energy (Einstein's theorem) is expressed by:

$$
\mathrm{E}=\mathrm{mc}^{2}
$$

where,
E is the energy in ergs,
$m$ is the mass of the matter in grams,
c is the speed of light in centimeters per second ( $\mathrm{c}^{2}=$ $9.10^{20}$ ).



## Key to Abbreviations for FCC Allocation Chart

A-Amateur
AC—Airdrome Control
AF-Aeronautical Fixed
AFF-Aviation (Flight Test and Aeronautical Fixed Only)
AM-Aeronautical Mobile
AR-Aeronautical Radionavigation
ARO-Aeronautical Radionavigation
(Omnidirectional Radio Range)
C-Citizens Radio
CC-Common Carrier
CAP—Civil Air Patrol (Land and Mobile)
DP—Domestic Public
F-Fixed
FA-Fixed (Alaska)
FAP—Fixed (Alaska and Puerto Rico)
G-Government
I-Industrial
IAF-International Aeronautical Fixed
IAFP-International Aeronautical Fixed (Alaska, Hawaii, and U.S. Possessions)

IB-International Broadcasting
IC-International Control
IFP—International Fixed Public
IFPT-International Fixed Public (Puerto Rico and Virgin Islands)

ISM-Industrial, Scientific, and Medical Equipment
LT-Land Transportation
M-Mobile
MA—Meteorological Aids
MM—Maritime Mobile
MMCP-Maritime Mobile Coastal Telephony
MMCT-Maritime Mobile Coastal Telegraphy

MMDCP-Maritime Mobile Distress and Calling (Telephony)
MMDCT-Maritime Mobile Distress and Calling (Telegraphy)
MMIP-Maritime Mobile (Intership Telephony)

MMSCP-Maritime Mobile Ship Calling (Telephony)

MMSCT—Maritime Mobile Ship Calling (Telegraphy)
MMSP—Maritime Mobile Ship (Telephony)

MMST—Maritime Mobile Ship (Telegraphy)
MMT-Maritime Mobile (Telegraphy)
MRDF-Maritime Radionavigation (Radio Direction Finding)
(NIB)-Noninterference Basis
OF-Operational Fixed
P-Police
PS—Public Safety
R-Radiosonde
RA-Racon
RL--Radiolocation
RN—Radionavigation
RNAL—Radionavigation (Aeronautical and Land)

RP—Remote Pickup
RPT—Remote Pickup (Television)
SF—Standard Frequency
STLA—Studio Transmitter Link (AM Broadcast)

STLF—Studio Transmitter Link (FM Broadcast)
STLT—Studio Transmitter Link
(Television)
TM-Telemetering

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[^0]:    * For a list of dielectric constants of materials, see § 27 .

[^1]:    * For a list of dielectric constants of materials, see $\$ 27$.

[^2]:    * For a list of dielectric constants of materials, see $\S 27$.

[^3]:    Universal Time and Call Letters（Code）．
    IWDS Warning（Code）－WWV．（4．3 and 34．3 Minutes After Hour Only．）
    N North Pacific Propagation Forecast．（Approx． 9.4 and 39.4 Minutes After Hour Only．）
    IWDS Warning（Code）－WWVH．（Approx． 14.4 and 44.4 Minutes After Hour Only．）
    North Atlantic Propagation Forecast．（19．5 and 49．5 Minutes After Hour Only．）
    Call Letters and EST（Voice）－UT（Code）－EST（Voice）．

[^4]:    $\mathbf{p}=$ Picture Carrier Freq.

[^5]:    All frequencies in mc.

[^6]:    * For Greek letters used as symbols (such as $\Omega, \omega$, and $\psi$ ), see the Greek alphabet in § 43.

[^7]:    * Any number to the zero power is 1 .

[^8]:    * The grain is the same in avoirdupois, troy, and apothecaries' weights.

