THE RADIO HANDBOOK

Table of Contents

PREFACE

The Publishers take pleasure in presenting the 14th edition of the RADIO HANDBOOK, written especially for the advanced radio amateur and the electronic engineer.

The field of electronics has made tremendous strides since World War II. Radar, television, semi-conductors and electronic computing devices have created million dollar industries that were mere dreams fifteen years ago.

This edition of RADIO HANDBOOK has been thoroughly revised and brought up to date, touching briefly on those aspects in the industrial and military electronic fields that are of immediate interest to the electronic engineer and the radio amateur. Many beginning amateurs must make the decision of whether or not to try to make a career in electronics. This Handbook should be of great help to them, as it presents an overall picture of the electronic techniques used in these fields.

The construction chapters of this Handbook have been completely re-edited. All items described therein are of up-to-date design, free of TVI problems and sundry parasitic oscillations. An attempt has been made not to duplicate items that have appeared in contemporary magazines.

The compilation and writing of this book would have been impossible without the lavish help that was tended the editor from fellow amateurs and interested electronic organizations. Time, ideas and encouragement were freely given in a joint effort to make the 14th edition of the RADIO HANDBOOK an outstanding success. The editor and publishers wish to thank the following individuals and organizations whose unselfish assistance made the publication of this book an interesting and inspired task:

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CHAPTER ONE

Introduction to Radio

The field of radio is a division of the much larger field of electronics. Radio itself is such a broad study that it is still further broken down into a number of smaller fields of which only shortwave or high-frequency radio is covered in this book. Specifically the field of communication on frequencies from 1.8 to 450 megacycles is taken as the subject matter for this work.

The largest group of persons interested in the subject of high-frequency communication is the more than 100,000 radio amateurs located in nearly all countries of the world. Strictly speaking, a radio amateur is anyone interested in radio non-commercially, but the term is ordinarily applied only to those hobbyists possessing transmitting equipment and a license from the government.

It was for the radio amateur, and particularly for the serious and more advanced amateur, that most of the equipment described in this book was developed. However, in each equipment group simple items also are shown for the student or beginner. The design principles behind the equipment for high-frequency radio communication are of course the same whether the equipment is to be used for commercial, military, or amateur purposes, the principal differences lying in construction practices, and in the tolerances and safety factors placed upon components.

With the increasing complexity of high-frequency communication, resulting primarily from increased utilization of the available spectrum, it becomes necessary to delve more deeply into the basic principles underlying radio communication, both from the standpoint of equipment design and operation and from the standpoint of signal propagation. Hence, it will be found that this edition of the RADIO HANDBOOK has been devoted in greater proportion to the teaching of the principles of equipment design and signal propagation. It is in response to requests from schools and agencies of the Department of Defense, in addition to persistent requests from the amateur radio fraternity, that coverage of these principles has been expanded.

1-1 Amateur Radio

Amateur radio is a fascinating hobby with many phases. So strong is the fascination offered by this hobby that many executives, engineers, and military and commercial operators enjoy amateur radio as an avocation even though they are also engaged in the radio field commercially. It captures and holds the interest of many people in all walks of life, and in all countries of the world where amateur activities are permitted by law.

Amateurs have rendered much public service through furnishing communications to and from the outside world in cases where disaster has isolated an area by severing all wire communications. Amateurs have a proud record of heroism and service in such occasion. Many expeditions to remote places have been kept in touch with home by communication with amateur stations on the high frequencies. The amateur's fine record of performance with the "wireless" equipment of World War I has been surpassed by his outstanding service in World War II.

By the time peace came in the Pacific in the summer of 1945, many thousand amateur operators were serving in the allied armed forces. They had supplied the army, navy, marines, coast guard, merchant marine, civil service, war plants, and civilian defense organizations with *trained* personnel for radio, radar, wire, and visual communications and for teaching. Even now, at the time of this writing, amateurs are being called back into the expanded defense forces, are returning to defense plants where their skills are critically needed, and are being organized into communication units as an adjunct to civil defense groups.

1-2 Station and Operator Licenses

Every radio transmitting station in the United States no matter how low its power must have a license from the federal government before being operated; some classes of stations must have a permit from the government even before being constructed. And every operator of a transmitting station must have an operator's license before operating a transmitter. There are no exceptions. Similar laws apply in practically every major country.

Classes of Amateur Operator Licenses There are at present *six* classes of amateur operator licenses which have been authorized by the Federal Communications Commission. These classes differ in many respects, so each will be discussed briefly.

(a) *Amateur Extra Class.* This class of license is available to any U. S. citizen who at any time has held for a period of two years or more a valid amateur license, issued by the FCC, excluding licenses of the Novice and Technician Classes. The examination for the license includes a code test at 20 words per minute, the usual tests covering basic amateur practice and general amateur regulations, and an additional test on advanced amateur practice. All amateur privileges are accorded the holders of this operator's license.

(b) *General Class.* This class of amateur license is equivalent to the old Amateur Class B license, and accords to the holders all amateur privileges except those which may be set aside for holders of the Amateur Extra Class license. This class of amateur operator's license is available to any U. S. citizen. The examination for the license includes a code test at 13 words per minute, and the usual examinations covering basic amateur practice and general amateur regulations.

(c) *Conditional Class.* This class of amateur license and the privileges accorded by it are equivalent to the General Class license. However, the license can be issued only to those whose residence is more than 125 miles airline from the nearest location at which FCC examinations are held at intervals of not more than three months for the General Class amateur operator license, or to those who for any of several specified reasons are unable to appear for examination.

(d) *Technician Class.* This is a new class of license which is available to any citizen of the United States. The examination is the same as that for the General Class license, except that the code test is at a speed of 5 words per minute. The holder of a Technician class license is accorded all authorized amateur privileges in the amateur frequency bands above 220 megacycles, and in the 50-Mc. band.

(e) *Novice Class.* This is a new class of license which is available to any U. S. citizen who has not previously held an amateur license of any class issued by any agency of the U. S. government, military or civilian. The examination consists of a code test at a speed of 5 words per minute, plus an examination on the rules and regulations essential to beginner's operation, including sufficient elementary radio theory for the understanding of those rules. The Novice Class of license affords severely restricted privileges, is valid for only a period of one year (as contrasted to all other classes of amateur licenses which run for a term of five years), and is not renewable.

All Novice and Technician class examinations are given by volunteer examiners, as regular examinations for these two classes are not given in FCC offices. Amateur radio clubs in the larger cities have established examining committees to assist would-be amateurs of the area in obtaining their Novice and Technician licenses.

1-3 The Amateur Bands

Certain small segments of the radio frequency spectrum between 1500 kc. and 10,000 Mc. are reserved for operation of amateur radio stations. These segments are in general agreement throughout the world, although certain parts of different amateur bands may be used for other purposes in various geographic regions. In particular, the 40-meter amateur band is used legally (and illegally) for short wave broadcasting by many countries in Europe, Africa and Asia. Parts of the 80-meter band are used for short distance marine work in Europe, and for broadcasting in South America. The amateur bands available to American radio amateurs are:

160 Meters (1800 Kc.-2000 Kc.) The 160-meter band is divided into 25-kilocycle segments on a regional basis, with day and night power limitations, and is available for amateur use provided no interference is caused to the Loran (Long Range Navigation) stations operating in this band. This band is least affected by the 11-

year solar sunspot cycle. The Maximum Usable Frequency (MUF) even during the years of decreased sunspot activity does not usually drop below 4 Mc., therefore this band is not subject to the violent fluctuations found on the higher frequency bands. DX contacts on on this band are limited by the ionospheric absorption of radio signals, which is quite high. During winter nighttime hours the absorption is often of a low enough value to permit trans-oceanic contacts on this band. On rare occasions, contacts up to 10,000 miles have been made. As a usual rule, however, 160-meter amateur operation is confined to ground-wave contacts or single-skip contacts of 1000 miles or less. Popular before World War II, the 160-meter band is now only sparsely occupied since many areas of the country are blanketed by the megawatt pulses of the Loran chains.

80 Meters (3500 Kc.-4000 Kc.) The 80-meter band is the most popular amateur band in the continental United States for local "rag-chewing" and traffic nets. During the years of minimum sunspot activity the ionospheric absorption on this band may be quite low, and long distance DX contacts are possible during the winter night hours. Daytime operation, in general, is limited to contacts of 500 miles or less. During the summer months, local static and high ionospheric absorption limit long distance contacts on this band. As the sunspot cycle advances and the MUF rises, increased ionospheric absorption will tend to degrade the long distance possibilities of this band. At the peak of the sunspot cycle, the 80-meter band becomes useful only for short-haul communication.

40 Meters (7000 Kc.-7300 Kc.) The 40-meter band is high enough in frequency to be severely affected by the 11-year sunspot cycle. During years of minimum solar activity, the MUF may drop below 7 Mc., and the band will become very erratic, with signals dropping completely out during the night hours. Ionospheric absorption of signals is not as large a problem on this band as it is on 80 and 160 meters. As the MUF gradually rises during the next few years, the skip-distance will increase on 40 meters, especially during the winter months. At the peak of the solar cycle, the daylight skip distance on 40 meters will be quite long, and stations within a distance of 500 miles or so of each other will not be able to hold communication. DX operation on the 40-meter band is considerably hampered by broadcasting stations, propaganda stations, and jamming transmitters. In Europe and Asia the band is in a chaotic state, and amateur operation in this region is severely hampered.

20 Meters (14,000 Kc.-14,350 Kc.) At the present time, the 20-meter band is by far the most popular band for long distance contacts. High enough in frequency to be almost obliterated at the bottom of the solar cycle, the band nevertheless provides good DX contacts during years of minimal sunspot activity. At the present time, the band is open to almost all parts of the world at some time during the year. During the summer months, the band is active until the late evening hours, but during the winter months the band is only good for a few hours during daylight. Extreme DX contacts are usually erratic, but the 20-meter band is the only band available for DX operation the year around during the bottom of the DX cycle. As the sunspot count increases and the MUF rises (as it will for the next few years), the 20-meter band will become open for longer hours during the winter. The maximum skip distance will increase, and DX contacts will be possible over paths other than the Great Circle route. Signals will be heard the "long path," 180 degrees opposite to the Great Circle path. During daylight hours, absorption may become apparent on the 20-meter band, and all signals except very short skip may disappear. On the other hand, the band will be open for worldwide DX contacts all night long. The 20-meter band is very susceptible to "fade-outs" caused by solar disturbances, and all except local signals may completely disappear for periods of a few hours to a day or so. In general, the 20-meter band will improve rapidly during the next few years, and it will support long distance DX contacts during most of the year.

15 Meters (21,000 Kc.-21,450 Kc.) This is a relatively new band for radio amateurs since it has only been available for amateur operation since 1952. Not too much is known about the characteristics of this band, since it has not been occupied for a full cycle of solar activity. However, it is reasonable to assume that it will have characteristics similar to both the 20 and 10-meter amateur bands. It should have a longer skip distance than 20 meters for a given time, and sporadic-E (short-skip) should be apparent during the winter months. During a period of low sunspot activity, the MUF will rarely rise as high as 15 meters, so this band will be "dead" for a large part of the year. During the next few years, 15-meter activity should pick up rapidly, and the band should support extremely long DX contacts. Activity on the 15-meter band is limited in some areas, since the older model TV receivers have a 21 Mc. i-f channel, which falls directly in the 15-meter band. The interference problems brought about by such an unwise choice of intermediate frequency often restrict operation on this band by amateur stations unfortunate enough to be situated near such an obsolete receiver.

10-11 Meters (26,960 Kc.-27,230 Kc.) (28,000 Kc.-29,700 Kc.) During the peak of the sunspot cycle, the 10-meter band is without doubt the most popular amateur band. The combination of long skip and low ionospheric absorption make reliable DX contacts with low powered equipment possible. The great width of the band (1700 kc.) provides room for a large number of amateurs. The long skip (1500 miles or so) prevents near-by amateurs from hearing each other, thus dropping the interference level. During the winter months, sporadic-E (short skip) signals up to 1200 miles or so will be heard. The 10-meter band is poorest in the summer months, even during a sunspot maximum. Extremely long daylight skip is common on this band, and in a few years the 10-meter band will support intercontinental DX contacts during daylight hours.

The second harmonic of stations operating in the 10-meter band falls directly into television channel 2, and the higher harmonics of 10-meter transmitters fall into the higher TV channels. This harmonic problem seriously curtailed amateur 10-meter operation during the late 40's. However, with the new circuit techniques and TVI precautionary measures stressed in this Handbook, 10-meter operation should cause little or no interference to near-by television receivers of modern design.

Six Meters (50 Mc.-54 Mc.) At the peak of the sunspot cycle, the MUF occasionally rises high enough to permit DX contacts up to 10,000 miles or so on 6 meters. Activity on this band during such a period is often quite high. Interest in this band wanes during a period of lesser solar activity, as contacts, as a rule, are restricted to short-skip work. The proximity of the 6-meter band to television channel 2 often causes interference problems to amateurs located in areas where channel 2 is active. As the sunspot cycle increases, activity on the 6-meter band will increase.

The V-H-F Bands (Two Meters and "Up") The v-h-f bands are the least affected by the vagaries of the sunspot cycle and the Heaviside layer. Their predominant use is for reliable communication over distances of 150 miles or less. These bands are sparsely occupied in the rural sections of the United States, but are quite heavily congested in the urban areas of high population.

In recent years it has been found that v-h-f signals are propagated by other means than by line-of-sight transmission. "Scatter signals," Aurora reflection, and air-mass boundary bending are responsible for v-h-f communication up to 1200 miles or so. Weather conditions will often affect long distance communication on the 2-meter band, and all the v-h-f bands are particularly sensitive to this condition.

The other v-h-f bands have had insufficient occupancy to provide a clear picture of their characteristics. In general, they behave much as does the 2-meter band, with the weather effects becoming more pronounced on the higher frequency bands.

1-4 Starting Your Study

When you start to prepare yourself for the amateur examination you will find that the circuit diagrams, tube characteristic curves, and formulas appear confusing and difficult of understanding. But after a few study sessions one becomes sufficiently familiar with the notation of the diagrams and the basic concepts of theory and operation so that the acquisition of further knowledge becomes easier and even fascinating.

As it takes a considerable time to become proficient in sending and receiving code, it is a good idea to intersperse technical study sessions with periods of code practice. Many short code practice sessions benefit one more than a small number of longer sessions. Alternating between one study and the other keeps the student from getting "stale" since each type of study serves as a sort of respite from the other.

When you have practiced the code long enough you will be able to follow the gist of the slower sending stations. Many stations send very slowly when working other stations at great distances. Stations repeat their calls many times when calling other stations before contact is established, and one need not have achieved much code proficiency to make out their calls and thus determine their location.

The Code The applicant for any class of amateur operator license must be able to send and receive the Continental Code (sometimes called the International Morse Code). The speed required for the sending and receiving test may be either 5, 13, or 20 words per minute, depending upon the class of license, assuming an average of five characters to the word in each case. The sending and re-

A	· —	N	— ·	1	· — — — —
B	— · · ·	O	— — —	2	· · — — —
C	— · — ·	P	· — — ·	3	· · · — —
D	— · ·	Q	— — · —	4	· · · · —
E	·	R	· — ·	5	· · · · ·
F	· · — ·	S	· · ·	6	— · · · ·
G	— — ·	T	—	7	— — · · ·
H	· · · ·	U	· · —	8	— — — · ·
I	· ·	V	· · · —	9	— — — — ·
J	· — — —	W	· — —	Ø	— — — — —
K	— · —	X	— · · —		
L	· — · ·	Y	— · — —		
M	— —	Z	— — · ·		

Ø MEANS ZERO, AND IS WRITTEN IN THIS WAY TO DISTINGUISH IT FROM THE LETTER "O". IT OFTEN IS TRANSMITTED INSTEAD AS ONE LONG DASH (EQUIVALENT TO 5 DOTS)

PERIOD (.)	· — · — · —	WAIT SIGN (AS)	· — · · ·
COMMA (,)	— — · · — —	DOUBLE DASH (BREAK)	— · · · —
INTERROGATION (?)	· · — — · ·	ERROR (ERASE SIGN)	· · · · · · · ·
QUOTATION MARK (")	· — · · — ·	FRACTION BAR (/)	— · · — ·
COLON (:)	— — — · · ·	END OF MESSAGE (AR)	· — · — ·
SEMICOLON (;)	— · — · — ·	END OF TRANSMISSION (SK)	· · · — · —
PARENTHESIS ( )	— · — — · —	INTERNAT. DISTRESS SIG. (SOS)	· · · — — — · · ·

Figure 1

The Continental (or International Morse) Code is used for substantially all non-automatic radio communication. DO NOT memorize from the printed page; code is a language of SOUND, and must not be learned visually; learn by listening as explained in the text.

ceiving tests run for five minutes, and one minute of errorless transmission or reception must be accomplished within the five-minute interval.

If the code test is failed, the applicant must wait at least one month before he may again appear for another test. Approximately 30% of amateur applicants fail to pass the test. It should be expected that nervousness and excitement will at least to some degree temporarily lower the applicant's code ability. The best prevention against this is to master the code at a little greater than the required speed under ordinary conditions. Then if you slow down a little due to nervousness during a test the result will not prove fatal.

Memorizing the Code There is no shortcut to code proficiency. To memorize the alphabet entails but a few evenings of diligent application, but considerable time is required to build up speed. The exact time required depends upon the individual's ability and the regularity of practice.

While the speed of learning will naturally vary greatly with different individuals, about 70 hours of practice (no practice period to be over 30 minutes) will usually suffice to bring a speed of about 13 w.p.m.; 16 w.p.m. requires about 120 hours; 20 w.p.m., 175 hours.

Since code reading requires that individual letters be recognized instantly, any memorizing scheme which depends upon orderly sequence, such as learning all *"dah"* letters and all *"dit"* letters in separate groups, is to be discouraged. Before beginning with a code practice set it is necessary to memorize the whole alphabet perfectly. A good plan is to study only two or three letters a day and to drill with those letters until they become part of your consciousness. Mentally translate each day's letters into their sound equivalent wherever they are seen, on signs, in papers, indoors and outdoors. Tackle two additional letters in the code chart each day, at the same time reviewing the characters already learned.

Avoid memorizing by routine. Be able to sound out any letter immediately without so much as hesitating to think about the letters preceding or following the one in question. Know *C*, for example, apart from the sequence *ABC*. Skip about among all the characters learned, and before very long sufficient letters will have been acquired to enable you to spell out simple words to yourself in *"dit dabs."* This is interesting exercise, and for that reason it is good to memorize all the vowels first and the most common consonants next.

Actual code practice should start only when the entire alphabet, the numerals, period, com-

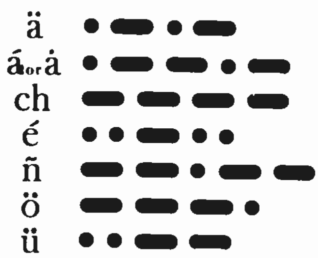


Figure 2

These code characters are used in languages other than English. They may occasionally be encountered so it is well to know them.

ma, and question mark have been memorized so thoroughly that any one can be sounded without the slightest hesitation. Do not bother with other punctuation or miscellaneous signals until later.

Sound — Not Sight Each letter and figure *must* be memorized by its *sound* rather than its appearance. Code is a system of sound communication, the same as is the spoken word. The letter *A*, for example, is one short and one long sound in combination sounding like *dit dah*, and it must be remembered as such, and not as "dot dash."

Practice Time, patience, and regularity are required to learn the code properly. Do not expect to accomplish it within a few days.

Don't practice too long at one stretch; it does more harm than good. Thirty minutes at a time should be the limit.

Lack of regularity in practice is the most common cause of lack of progress. Irregular practice is very little better than no practice at all. Write down what you have heard; then forget it; *do not look back.* If your mind dwells even for an instant on a signal about which you have doubt, you will miss the next few characters while your attention is diverted.

While various automatic code machines, phonograph records, etc., will give you practice, by far the best practice is to obtain a study companion who is also interested in learning the code. When you have both memorized the alphabet you can start sending to each other. Practice with a key and oscillator or key and buzzer generally proves superior to all automatic equipment. Two such sets operated between two rooms are fine—or between your house and his will be just that much better. Avoid talking to your partner while practicing. If you must ask him a question, do it in code. It makes more interesting practice than confining yourself to random practice material.

When two co-learners have memorized the code and are ready to start sending to each other for practice, it is a good idea to enlist the aid of an experienced operator for the first practice session or two so that they will get an idea of how properly formed characters sound.

During the first practice period the speed should be such that substantially solid copy can be made without strain. Never mind if this is only two or three words per minute. In the next period the speed should be increased slightly to a point where nearly all of the characters can be caught only through conscious effort. When the student becomes proficient at this new speed, another slight increase may be made, progressing in this manner until a speed of about 16 words per minute is attained if the object is to pass the amateur 13-word per minute code test. The margin of 3 w.p.m. is recommended to overcome a possible excitement factor at examination time. Then when you take the test you don't have to worry about the "jitters" or an "off day."

Speed should not be increased to a new level until the student finally makes solid copy with ease for at least a five-minute period at the old level. How frequently increases of speed can be made depends upon individual ability and the amount of practice. Each increase is apt to prove disconcerting, but remember "you are never learning when you are comfortable."

A number of amateurs are sending code practice on the air on schedule once or twice each week; excellent practice can be obtained after you have bought or constructed your receiver by taking advantage of these sessions.

If you live in a medium-size or large city, the chances are that there is an amateur radio club in your vicinity which offers free code practice lessons periodically.

Skill When you listen to someone speaking you do not consciously think how his words are spelled. This is also true when you read. In code you must train your ears to read code just as your eyes were trained in school to read printed matter. With enough practice you acquire skill, and from skill, speed. In other words, it becomes a *habit*, something which can be done without conscious effort. Conscious effort is fatal to speed; we can't think rapidly enough; a speed of 25 words a minute, which is a common one in commercial operations, means 125 characters per minute or more than two per second, which leaves no time for conscious thinking.

Perfect Formation of Characters When transmitting on the code practice set to your partner, concentrate on the *quality* of your sending, *not* on your speed. Your partner will appreciate it and he could not copy you if you speeded up anyhow.

If you want to get a reputation as having an excellent "fist" on the air, just remember that speed alone won't do the trick. Proper execution of your letters and spacing will make much more of an impression. Fortunately, as you get so that you can send evenly and accurately, your sending speed will automatically increase. Remember to try to see how *evenly* you can *send*, and how *fast* you can *receive*. Concentrate on making signals properly with your key. Perfect formation of characters is paramount to everything else. Make every signal right no matter if you have to practice it hundreds or thousands of times. Never allow yourself to vary the slightest from perfect formation once you have learned it.

If possible, get a good operator to listen to your sending for a short time, asking him to criticize even the slightest imperfections.

Timing It is of the utmost importance to maintain uniform spacing in characters and combinations of characters. Lack of uniformity at this point probably causes beginners more trouble than any other single factor. Every dot, every dash, and every space must be correctly timed. In other words, accurate timing is absolutely essential to intelligibility, and timing of the spaces between the dots and dashes is just as important as the lengths of the dots and dashes themselves.

The characters are timed with the dot as a "yardstick." A standard dash is three times as long as a dot. The spacing between parts of the same letter is equal to one dot; the space between letters is equal to three dots, and that between words equal to five dots.

The rule for spacing between letters and words is not strictly observed when sending slower than about 10 words per minute for the benefit of someone learning the code and desiring receiving practice. When sending at, say, 5 w.p.m., the individual letters should be made the same as if the sending rate were about 10 w.p.m., except that the spacing between letters and words is greatly exaggerated. The reason for this is obvious. The letter *L*, for instance, will then sound exactly the same at 10 w.p.m. as at 5 w.p.m., and when the speed is increased above 5 w.p.m. the student will not have to become familiar with what may seem to him like a new sound, although it is in reality only a faster combination of dots and dashes. At the greater speed he will merely have to learn the identification of the *same* sound without taking as long to do so.

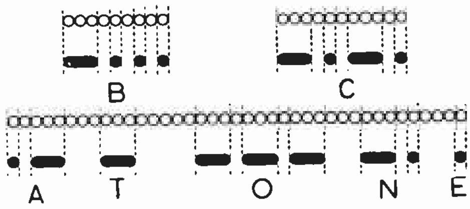


Figure 3

Diagram illustrating relative lengths of dashes and spaces referred to the duration of a dot. A dash is exactly equal in duration to three dots; spaces between parts of a letter equal one dot; those between letters, three dots; space between words, five dots. Note that a slight increase between two parts of a letter will make it sound like two letters.

Be particularly careful of letters like *B*. Many beginners seem to have a tendency to leave a longer space after the dash than that which they place between succeeding dots, thus making it sound like *TS*. Similarly, make sure that you do not leave a longer space after the first dot in the letter *C* than you do between other parts of the same letter; otherwise it will sound like *NN*.

Sending vs. Receiving Once you have memorized the code thoroughly you should concentrate on increasing your *receiving* speed. True, if you have to practice with another newcomer who is learning the code with you, you will both have to do some sending. But don't attempt to practice *sending* just for the sake of increasing your sending *speed*.

When transmitting on the code practice set to your partner so that he can get receiving practice, concentrate on the *quality* of your sending, not on your speed.

Because it is comparatively easy to learn to send rapidly, especially when no particular care is given to the quality of sending, many operators who have just received their licenses get on the air and send mediocre or worse code at 20 w.p.m. when they can barely receive good code at 13. Most oldtimers remember their own period of initiation and are only too glad to be patient and considerate if you tell them that you are a newcomer. But the surest way to incur their scorn is to try to impress them with your "lightning speed," and then to request them to send more slowly when they come back at you at the same speed.

Stress your copying ability; never stress your sending ability. It should be obvious that that if you try to send faster than you can receive, your ear will not recognize any mistakes which your hand may make.

Figure 4
PROPER POSITION OF THE FINGERS FOR OPERATING A TELEGRAPH KEY

The fingers hold the knob and act as a cushion. The hand rests lightly on the key. The muscles of the forearm provide the power, the wrist acting as the fulcrum. The power should not come from the fingers, but rather from the forearm muscles.

Using the Key Figure 4 shows the proper position of the hand, fingers and wrist when manipulating a telegraph or radio key. The forearm should rest naturally on the desk. It is preferable that the key be placed far enough back from the edge of the table (about 18 inches) that the elbow can rest on the table. Otherwise, pressure of the table edge on the arm will tend to hinder the circulation of the blood and weaken the ulnar nerve at a point where it is close to the surface, which in turn will tend to increase fatigue considerably.

The knob of the key is grasped lightly with the thumb along the edge; the index and third fingers rest on the top towards the front or far edge. The hand moves with a free up and down motion, the wrist acting as a fulcrum. The power must come entirely from the arm muscles. The third and index fingers will bend slightly during the sending but not because of deliberate effort to manipulate the finger muscles. Keep your finger muscles just tight enough to act as a cushion for the arm motion and let the slight movement of the fingers take care of itself. The key's spring is adjusted to the individual wrist and should be neither too stiff nor too loose. Use a moderately stiff tension at first and gradually lighten it as you become more proficient. The separation between the contacts must be the proper amount for the desired speed, being somewhat under 1/16 inch for slow speeds and slightly closer together (about 1/32 inch) for faster speeds. Avoid extremes in either direction.

Do not allow the muscles of arm, wrist, or fingers to become tense. Send with a full, free arm movement. Avoid like the plague any finger motion other than the slight cushioning effect mentioned above.

Stick to the regular hand key for learning code. No other key is satisfactory for this purpose. Not until you have thoroughly mastered both sending and receiving at the maximum speed in which you are interested should you tackle any form of automatic or semi-automatic key such as the Vibroplex ("bug") or an electronic key.

Difficulties Should you experience difficulty in increasing your code speed after you have once memorized the characters, there is no reason to become discouraged. It is more difficult for some people to learn code than for others, but there is no justification for the contention sometimes made that "some people just can't learn the code." It is not a matter of intelligence; so don't feel ashamed if you seem to experience a little more than the usual difficulty in learning code. Your reaction time may be a little slower or your coordination not so good. If this is the case, remember *you can still learn the code.* You may never learn to send and receive at 40 w.p.m., but you can learn sufficient speed for all non-commercial purposes and even for most commercial purposes if you have patience, and refuse to be discouraged by the fact that others seem to pick it up more rapidly.

When the sending operator is sending just a bit too fast for you (the best speed for practice), you will occasionally miss a signal or a small group of them. When you do, leave a blank space; do not spend time futilely trying to recall it; dismiss it, and center attention on the next letter; otherwise you'll miss more. Do not ask the sender any questions until the transmission is finished.

To prevent guessing and get equal practice on the less common letters, depart occasionally from plain language material and use a jumble of letters in which the usually less commonly used letters predominate.

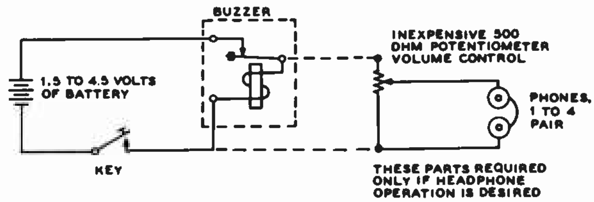
As mentioned before, many students put a greater space after the dash in the letter *B* than between other parts of the same letter so it sounds like *TS*. *C, F, Q, V, X, Y* and *Z* often give similar trouble. Make a list of words or arbitrary combinations in which these letters predominate and practice them, both sending and receiving until they no longer give you trouble. Stop everything else and stick at them. So long as they give you trouble you are not ready for anything else.

Follow the same procedure with letters which you may tend to confuse such as *F* and *L*, which are often confused by beginners.

Figure 5

THE SIMPLEST CODE PRACTICE SET CONSISTS OF A KEY AND A BUZZER

The buzzer is adjusted to give a steady, high-pitched whine. If desired, the phones may be omitted, in which case the buzzer should be mounted firmly on a sounding board. Crystal, magnetic, or dynamic earphones may be used. Additional sets of phones should be connected in parallel, not in series.



Keep at it until you *always* get them right without having to stop *even an instant* to think about it.

If you do not instantly recognize the sound of any character, you have not learned it; go back and practice your alphabet further. You should never have to omit writing down every signal you hear except when the transmission is too fast for you.

Write down what you hear, not what you think it should be. It is surprising how often the word which you guess will be wrong.

Copying Behind All good operators copy several words behind, that is, while one word is being received, they are writing down or typing, say, the fourth or fifth previous word. At first this is very difficult, but after sufficient practice it will be found actually to be easier than copying close up. It also results in more accurate copy and enables the receiving operator to capitalize and punctuate copy as he goes along. It is not recommended that the beginner attempt to do this until he can send and receive accurately and with ease at a speed of at least 12 words a minute.

It requires a considerable amount of training to dissociate the action of the subconscious mind from the direction of the conscious mind. It may help some in obtaining this training to write down two columns of short words. Spell the first word in the first column out loud while writing down the first word in the second column. At first this will be a bit awkward, but you will rapidly gain facility with practice. Do the same with all the words, and then reverse columns.

Next try speaking aloud the words in the one column while writing those in the other column; then reverse columns.

After the foregoing can be done easily, try sending with your key the words in one column while spelling those in the other. It won't be easy at first, but it is well worth keeping after if you intend to develop any real code proficiency. Do *not* attempt to catch up. There is a natural tendency to close up the gap, and you must train yourself to overcome this.

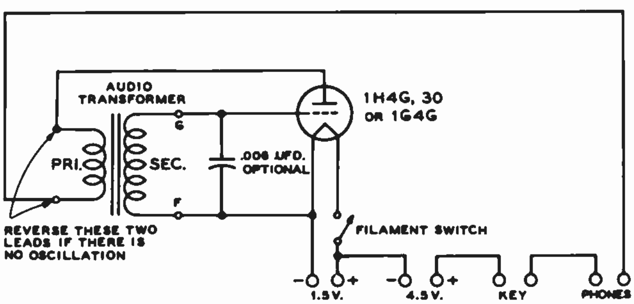
Next have your code companion send you a word either from a list or from straight text; do not write it down yet. Now have him send the next word; *after* receiving this second word, write down the first word. After receiving the third word, write the second word; and so on. Never mind how slowly you must go, even if it is only two or three words per minute. *Stay behind.*

It will probably take quite a number of practice sessions before you can do this with any facility. After it is relatively easy, then try staying two words behind; keep this up until it is easy. Then try three words, four words, and five words. The more you practice keep-

Figure 6

SIMPLE VACUUM-TUBE CODE PRACTICE OSCILLATOR

Power is furnished by a dry cell and a 4½-volt C battery. If the 0.006-µfd. capacitor is omitted, a higher pitched note will result. The note may have too low a pitch even without the capacitor unless the smallest, least expensive audio transformer available is used. The earphones must be of the magnetic or dynamic type since the plate current of the oscillator must flow through the phones.



ing received material in mind, the easier it will be to stay behind. It will be found easier at first to copy material with which one is fairly familiar, then gradually switch to less familiar material.

Automatic Code Machines The two practice sets which are described in this chapter are of most value when you have someone with whom to practice. Automatic code machines are not recommended to anyone who can possibly obtain a companion with whom to practice, someone who is also interested in learning the code. If you are unable to enlist a code partner and have to practice by yourself, the best way to get receiving practice is by the use of a tape machine (automatic code sending machine) with several practice tapes. Or you can use a set of phonograph code practice records. The records are of use only if you have a phonograph whose turntable speed is readily adjustable. The tape machine can be rented by the month for a reasonable fee.

Once you can copy about 10 w.p.m. you can also get receiving practice by listening to slow sending stations on your receiver. Many amateur stations send slowly particularly when working far distant stations. When receiving conditions are particularly poor many commercial stations also send slowly, sometimes repeating every word. Until you can copy around 10 w.p.m. your receiver isn't much use, and either another operator or a machine or records are necessary for getting receiving practice after you have once memorized the code.

Code Practice Sets If you don't feel too foolish doing it, you can secure a measure of code practice with the help of a partner by sending "dit-dah" messages to each other while riding to work, eating lunch, etc. It is better, however, to use a buzzer or code practice oscillator in conjunction with a regular telegraph key.

As a good key may be considered an investment it is wise to make a well-made key your first purchase. Regardless of what type code practice set you use, you will need a key, and later on you will need one to key your transmitter. If you get a good key to begin with, you won't have to buy another one later.

The key should be rugged and have fairly heavy contacts. Not only will the key stand up better, but such a key will contribute to the "heavy" type of sending so desirable for radio work. Morse (telegraph) operators use a "light" style of sending and can send somewhat faster when using this light touch. But, in radio work static and interference are often present, and a slightly heavier dot is desirable. If you use a husky key, you will find yourself automatically sending in this manner.

Figure 7

THE CIRCUIT OF FIGURE 6 IS USED IN THIS BATTERY-OPERATED CODE PRACTICE OSCILLATOR

A tube and audio transformer essentially comprise the oscillator. Fahnestock clips screwed to the base-board are used to make connection to the batteries, key, and phones.

To generate a tone simulating a code signal as heard on a receiver, either a mechanical buzzer or an audio oscillator may be used. Figure 5 shows a simple code-practice set using a buzzer which may be used directly simply by mounting the buzzer on a sounding board, or the buzzer may be used to feed from one to four pairs of conventional high-impedance phones.

An example of the audio-oscillator type of code-practice set is illustrated in figures 6 and 7. Any type of battery-filament tube may be used in this circuit to make up a satisfactory oscillator for code-practice work. The circuit is shown in figure 6.

CHAPTER TWO

Direct Current Circuits

All naturally occurring matter (excluding artifically produced radioactive substances) is made up of 92 fundamental constituents called *elements*. These elements can exist either in the free state such as iron, oxygen, carbon, copper, tungsten, and aluminum, or in chemical unions commonly called *compounds*. The smallest unit which still retains all the original characteristics of an element is the *atom*.

Combinations of atoms, or subdivisions of compounds, result in another fundamental unit, the *molecule*. The molecule is the smallest unit of any compound. All reactive elements when in the gaseous state also exist in the molecular form, made up of two or more atoms. The nonreactive gaseous elements helium, neon, argon, krypton, xenon, and radon are the only gaseous elements that ever exist in a stable monatomic state at ordinary temperatures.

2-1 The Atom

An atom is an extremely small unit of matter — there are literally billions of them making up so small a piece of material as a speck of dust. To understand the basic theory of electricity and hence of radio, we must go further and divide the atom into its main components, a positively charged nucleus and a cloud of negatively charged particles that surround the nucleus. These particles, swirling around the nucleus in elliptical orbits at an incredible rate of speed, are called *orbital electrons*.

It is upon the behavior of these electrons when freed from the atom, that depends the study of electricity and radio, as well as allied sciences. Actually it is possible to subdivide the nucleus of the atom into a dozen or so different particles, but this further subdivision can be left to quantum mechanics and atomic physics. As far as the study of electronics is concerned it is only necessary for the reader to think of the normal atom as being composed of a nucleus having a net positive charge that is exactly neutralized by the one or more orbital electrons surrounding it.

The atoms of different elements differ in respect to the charge on the positive nucleus and in the number of electrons revolving around this charge. They range all the way from hydrogen, having a net charge of one on the nucleus and one orbital electron, to uranium with a net charge of 92 on the nucleus and 92 orbital electrons. The number of orbital electrons is called the *atomic number* of the element.

Action of the Electrons From the above it must not be thought that the electrons revolve in a haphazard manner around the nucleus. Rather, the electrons in an element having a large atomic number are grouped into rings having a definite number of electrons. The only atoms in which these rings are completely filled are those of the inert gases mentioned before; all other elements have one or more uncompleted rings of electrons. If the uncompleted ring is nearly empty, the element is *metallic* in character, being most metallic when there is only one electron in the outer ring. If the incomplete ring lacks only one or two electrons, the element is usually *non-metallic*. Elements with a ring about half completed will exhibit both non-metallic and metallic characteristics; carbon, silicon, germanium, and arsenic are examples of this type of element.

In metallic elements these outer ring electrons are rather loosely held. Consequently, there is a continuous helter-skelter movement of these electrons and a continual shifting from one atom to another. The electrons which move about in a substance are called *free electrons*, and it is the ability of these electrons to drift from atom to atom which makes possible the *electric current*.

Conductors and Insulators If the free electrons are numerous and loosely held, the element is a good conductor. On the other hand, if there are few free electrons, as is the case when the electrons in an outer ring are tightly held, the element is a poor conductor. If there are virtually no free electrons, the element is a good insulator.

2-2 Fundamental Electrical Units and Relationships

Electromotive Force: Potential Difference The free electrons in a conductor move constantly about and change their position in a haphazard manner. To produce a drift of electrons or *electric current* along a wire it is necessary that there be a difference in "pressure" or *potential* between the two ends of the wire. This *potential difference* can be produced by connecting a source of *electrical potential* to the ends of the wire.

As will be explained later, there is an excess of electrons at the negative terminal of a battery and a deficiency of electrons at the positive terminal, due to chemical action. When the battery is connected to the wire, the deficient atoms at the positive terminal attract free electrons from the wire in order for the positive terminal to become neutral. The attracting of electrons continues through the wire, and finally the excess electrons at the negative terminal of the battery are attracted by the positively charged atoms at the end of the wire. Other sources of electrical potential (in addition to a battery) are: an electrical generator (dynamo), a thermocouple, an electrostatic generator (static machine), a photoelectric cell, and a crystal or piezoelectric generator.

Thus it is seen that a potential difference is the result of a difference in the number of electrons between the two (or more) points in question. The force or pressure due to a potential difference is termed the *electromotive force*, usually abbreviated *e.m.f.* or *E.M.F.* It is expressed in units called *volts*.

It should be noted that for there to be a potential difference between two bodies or points it is not necessary that one have a positive charge and the other a negative charge. If two bodies each have a negative charge, but one more negative than the other, the one with the lesser negative charge will act as though it were positively charged *with respect to the other body*. It is the *algebraic* potential difference that determines the force with which electrons are attracted or repulsed, the potential of the earth being taken as the zero reference point.

The Electric Current The flow of electrons along a conductor due to the application of an electromotive force constitutes an electric current. This drift is in addition to the irregular movements of the electrons. However, it must not be thought that each free electron travels from one end of the circuit to the other. On the contrary, each free electron travels only a short distance before colliding with an atom; this collision generally knocking off one or more electrons from the atom, which in turn move a short distance and collide with other atoms, knocking off other electrons. Thus, in the general drift of electrons along a wire carrying an electric current, each electron travels only a short distance and the excess of electrons at one end and the deficiency at the other are balanced by the source of the e.m.f. When this source is removed the state of normalcy returns; there is still the rapid interchange of free electrons between atoms, but there is no general trend or "net movement" in either one direction or the other.

Ampere and Coulomb There are two units of measurement associated with current, and they are often confused. The *rate of flow* of electricity is stated in *amperes*. The unit of *quantity* is the *coulomb*. A coulomb is equal to 6.28×10^{18} electrons, and when this quantity of electrons flows by a given point in every second, a current of one ampere is said to be flowing. An ampere is equal to one coulomb per second; a coulomb is, conversely, equal to one ampere-second. Thus we see that *coulomb* indicates *amount*, and *ampere* indicates *rate of flow* of electric current.

Older textbooks speak of current flow as being from the positive terminal of the e.m.f. source through the conductor to the negative terminal. Nevertheless, it has long been an established fact that the current flow in a metallic conductor is the *electronic* flow from the negative terminal of the source of voltage through the conductor to the positive terminal. The only exceptions to the electronic direction of flow occur in gaseous and electrolytic conductors where the flow of positive ions toward the cathode or negative electrode constitutes a positive flow in the opposite direction to the electronic flow. (An ion is an atom, molecule, or particle which either lacks one or more electrons, or else has an excess of one or more electrons.)

In radio work the terms "electron flow" and "current" are becoming accepted as being synonymous, but the older terminology is still accepted in the electrical (industrial) field. Because of the confusion this sometimes causes, it is often safer to refer to the direction of electron flow rather than to the direction of the "current." Since electron flow consists actually of a passage of *negative* charges, current flow and *algebraic* electron flow do pass in the same direction.

Resistance The flow of current in a material depends upon the ease with which electrons can be detached from the atoms of the material and upon its molecular structure. In other words, the easier it is to detach electrons from the atoms the more free electrons there will be to contribute to the flow of current, and the fewer collisions that occur between free electrons and atoms the greater will be the total electron flow.

The opposition to a steady electron flow is called the *resistance* of a material, and is one of its physical properties.

The unit of resistance is the *ohm*. Every substance has a *specific resistance*, usually expressed as *ohms per mil-foot*, which is determined by the material's molecular structure and temperature. A mil-foot is a piece of material one circular mil in area and one foot long. Another measure of resistivity frequently used is expressed in the units *microhms per centimeter cube*. The resistance of a uniform length of a given substance is directly proportional to its length and specific resistance, and inversely proportional to its cross-sectional area. A wire with a certain resistance for a given length will have twice as much resistance if the length of the wire is doubled. For a given length, doubling the cross-sectional area of the wire will *halve* the resistance, while doubling the *diameter* will reduce the resistance to *one fourth*. This is true since the cross-sectional area of a wire varies as the square of the diameter. The relationship between the resistance and the linear dimensions of a conductor may be expressed by the following equation:

$$R = \frac{r\,l}{A}$$

Where

R = resistance in ohms

r = resistivity in *Ohms per mil-foot*

l = length of conductor in feet

A = cross-sectional area in circular mils

TABLE OF RESISTIVITY		
Material	Resistivity in Ohms per Circular Mil-Foot	Temp. Coeff. of resistance per °C at 20° C.
Aluminum	17	0.0049
Brass	45	0.003 to 0.007
Cadmium	46	0.0038
Chromium	16	0.00
Copper	10.4	0.0039
Iron	59	0.006
Silver	9.8	0.004
Zinc	36	0.0035
Nichrome	650	0.0002
Constantan	295	0.00001
Manganin	290	0.00001
Monel	255	0.0019

FIGURE 1

The resistance also depends upon temperature, increasing with increases in temperature for most substances (including most metals), due to increased electron acceleration and hence a greater number of impacts between electrons and atoms. However, in the case of some substances such as carbon and glass the temperature coefficient is negative and the resistance decreases as the temperature increases. This is also true of electrolytes. The temperature may be raised by the external application of heat, or by the flow of the current itself. In the latter case, the temperature is raised by the heat generated when the electrons and atoms collide.

Conductors and Insulators In the molecular structure of many materials such as glass, porcelain, and mica all electrons are tightly held within their orbits and there are comparatively few free electrons. This type of substance will conduct an electric current only with great difficulty and is known as an *insulator*. An insulator is said to have a high electrical *resistance*.

On the other hand, materials that have a large number of free electrons are known as *conductors*. Most metals, those elements which have only one or two electrons in their outer ring, are good conductors. Silver, copper, and aluminum, in that order, are the best of the common metals used as conductors and are said to have the greatest *conductivity*, or lowest resistance to the flow of an electric current.

Fundamental Electrical Units These units are the *volt*, the *ampere*, and the *ohm*. They were mentioned in the preceding paragraphs, but were not completely defined in terms of fixed, known quantities.

The fundamental unit of *current*, or *rate of flow* of electricity is the ampere. A current of one ampere will deposit silver from a specified solution of silver nitrate at a rate of 1.118 milligrams per second.

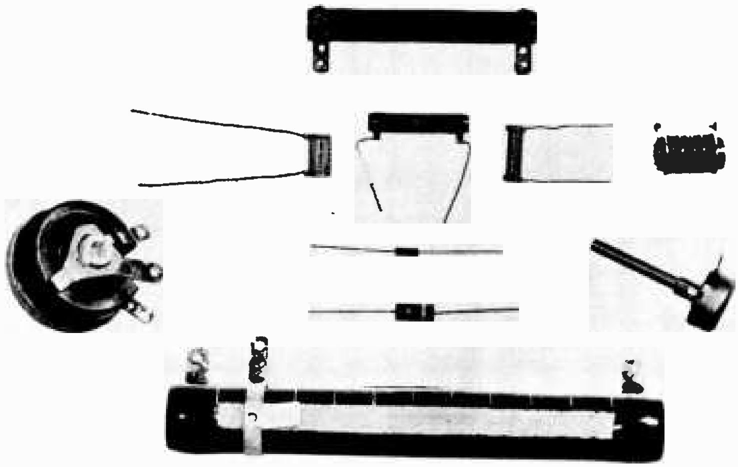


Figure 2
TYPICAL RESISTORS
Shown above are various types of resistors used in electronic circuits. The larger units are power resistors. On the left is a variable power resistor. Three precision-type resistors are shown in the center with two small composition resistors beneath them. At the right is a composition-type potentiometer, used for audio circuitry.

The international standard for the ohm is the resistance offered by a uniform column of mercury at 0° C., 14.4521 grams in mass, of constant cross-sectional area and 106.300 centimeters in length. The expression *megohm* (1,000,000 ohms) is also sometimes used when speaking of very large values of resistance.

A volt is the e.m.f. that will produce a current of one ampere through a resistance of one ohm. The standard of electromotive force is the Weston cell which at 20° C. has a potential of 1.0183 volts across its terminals. This cell is used only for reference purposes in a bridge circuit, since only an infinitesimal amount of current may be drawn from it without disturbing its characteristics.

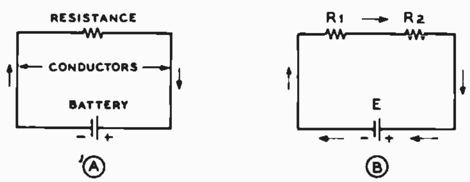


Figure 3
SIMPLE SERIES CIRCUITS
At (A) the battery is in series with a single resistor. At (B) the battery is in series with two resistors, the resistors themselves being in series. The arrows indicate the direction of electron flow.

Ohm's Law The relationship between the electromotive force (voltage), the flow of current (amperes), and the resistance which impedes the flow of current (ohms), is very clearly expressed in a simple but highly valuable law known as *Ohm's law.* This law states that *the current in amperes is equal to the voltage in volts divided by the resistance in ohms.* Expressed as an equation:

$$I = \frac{E}{R}$$

If the voltage (E) and resistance (R) are known, the current (I) can be readily found. If the voltage and current are known, and the resistance is unknown, the resistance (R) is equal to $\frac{E}{I}$. When the voltage is the unknown quantity, it can be found by multiplying I × R. These three equations are all secured from the original by simple transposition. The expressions are here repeated for quick reference:

$$I = \frac{E}{R} \qquad R = \frac{E}{I} \qquad E = IR$$

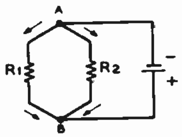
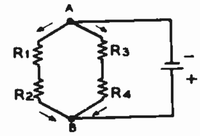


Figure 4
SIMPLE PARALLEL CIRCUIT

The two resistors R_1 and R_2 are said to be in parallel since the flow of current is offered two parallel paths. An electron leaving point A will pass either through R_1 or R_2, but not through both, to reach the positive terminal of the battery. If a large number of electrons are considered, the greater number will pass through whichever of the two resistors has the lower resistance.

Figure 5
SERIES-PARALLEL CIRCUIT



In this type of circuit the resistors are arranged in series groups, and these seriesed groups are then placed in parallel.

where I is the current in amperes,
R is the resistance in ohms,
E is the electromotive force in volts.

Application of Ohm's Law All electrical circuits fall into one of three classes: series circuits, parallel circuits, and series-parallel circuits. A series circuit is one in which the current flows in a single continuous path and is of the same value at every point in the circuit (figure 3). In a parallel circuit there are two or more current paths between two points in the circuit, as shown in figure 4. Here the current divides at A, part going through R_1 and part through R_2, and combines at B to return to the battery. Figure 5 shows a series-parallel circuit. There are two paths between points A and B as in the parallel circuit, and in addition there are two resistances in series in each branch of the parallel combination. Two other examples of series-parallel arrangements appear in figure 6. The way in which the current splits to flow through the parallel branches is shown by the arrows.

In every circuit, each of the parts has some resistance: the batteries or generator, the connecting conductors, and the apparatus itself. Thus, if each part has some resistance, no matter how little, and a current is flowing through it, there will be a voltage drop across it. In other words, there will be a potential difference between the two ends of the circuit element in question. This drop in voltage is equal to the product of the current and the resistance, hence it is called the *IR* drop.

The source of voltage has an *internal* resistance, and when connected into a circuit so that current flows, there will be an IR drop in the source just as in every other part of the circuit. Thus, if the terminal voltage of the source could be measured in a way that would cause no current to flow, it would be found to be more than the voltage measured when a current flows by the amount of the IR drop in the source. The voltage measured with no current flowing is termed the *no load* voltage; that measured with current flowing is the *load* voltage. It is apparent that a voltage source having a low internal resistance is most desirable.

Resistances in Series The current flowing in a series circuit is equal to the voltage impressed divided by the *total* resistance across which the voltage is impressed. Since the same current flows through every part of the circuit, it is merely necessary to add all the individual resistances to obtain the total resistance. Expressed as a formula:

$$R_{total} = R_1 + R_2 + R_3 + \ldots + R_N .$$

Of course, if the resistances happened to be all the same value, the total resistance would be the resistance of one multiplied by the number of resistors in the circuit.

Resistances in Parallel Consider two resistors, one of 100 ohms and one of 10 ohms, connected in parallel as in figure 4, with a voltage of 10 volts applied across each resistor, so the current through each can be easily calculated.

$$I = \frac{E}{R}$$

$$E = 10 \text{ volts} \quad R = 100 \text{ ohms} \qquad I_1 = \frac{10}{100} = 0.1 \text{ ampere}$$

$$E = 10 \text{ volts} \quad R = 10 \text{ ohms} \qquad I_2 = \frac{10}{10} = 1.0 \text{ ampere}$$

$$\text{Total current} = I_1 + I_2 = 1.1 \text{ ampere}$$

Until it divides at A, the entire current of 1.1 amperes is flowing through the conductor from the battery to A, and again from B through the conductor to the battery. Since this is more current than flows through the smaller resistor it is evident that the resistance of the parallel combination must be less than 10 ohms, the resistance of the smaller resistor. We can find this value by applying Ohm's law.

$$R = \frac{E}{I}$$

$$E = 10 \text{ volts} \qquad R = \frac{10}{1.1} = 9.09 \text{ ohms}$$
$$I = 1.1 \text{ amperes}$$

The resistance of the parallel combination is 9.09 ohms.

Mathematically, we can derive a simple formula for finding the effective resistance of two resistors connected in parallel.
This formula is:

$$R = \frac{R_1 \times R_2}{R_1 + R_2},$$

where R is the unknown resistance,
R_1 is the resistance of the first resistor,
R_2 is the resistance of the second resistor.

If the effèctive value required is known, and it is desired to connect one unknown resistor in parallel with one of known value, the following transposition of the above formula will simplify the problem of obtaining the unknown value:

$$R_2 = \frac{R_1 \times R}{R_1 - R}$$

where R is the effective value required,
R_1 is the known resistor,
R_2 is the value of the unknown resistance necessary to give R when in parallel with R_1.

The resultant value of placing a number of unlike resistors in parallel is equal to the reciprocal of the sum of the reciprocals of the various resistors. This can be expressed as:

$$R = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} + \cdots \frac{1}{R_n}}$$

The effective value of placing any number of unlike resistors in parallel can be determined from the above formula. However, it is commonly used only when there are three or more resistors under consideration, since the simplified formula given before is more convenient when only two resistors are being used.

From the above, it also follows that when two or more resistors of the same value are placed in parallel, the effective resistance of the paralleled resistors is equal to the value of one of the resistors divided by the number of resistors in parallel.

The effective value of resistance of two or more resistors connected in parallel is *always* less than the value of the lowest resistance in the combination. It is well to bear this simple rule in mind, as it will assist greatly in approximating the value of paralleled resistors.

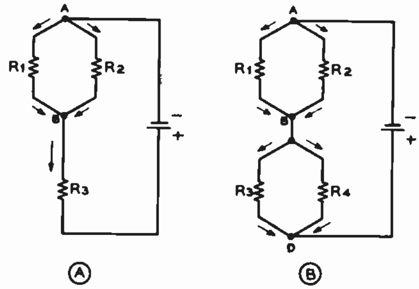


Figure 6
OTHER COMMON SERIES-PARALLEL CIRCUITS

Resistors in Series Parallel To find the total resistance of several resistors connected in series-parallel, it is usually easiest to apply either the formula for series resistors or the parallel resistor formula first, in order to reduce the original arrangement to a simpler one. For instance, in figure 5 the series resistors should be added in each branch, then there will be but two resistors in parallel to be calculated. Similarly in figure 7, although here there will be three parallel resistors after adding the series resistors in each branch. In figure 6B the paralleled resistors should be reduced to the equivalent series value, and then the series resistance values can be added.

Resistances in series-parallel can be solved by combining the series and parallel formulas into one similar to the following (refer to figure 7):

$$R = \frac{1}{\frac{1}{R_1 + R_2} + \frac{1}{R_3 + R_4} + \frac{1}{R_5 + R_6 + R_7}}$$

Voltage Dividers A voltage divider is exactly what its name implies: a resistor or a series of resistors connected across a source of voltage from which various lesser values of voltage may be obtained by connection to various points along the resistor.

A voltage divider serves a most useful purpose in a radio receiver, transmitter or amplifier, because it offers a simple means of obtaining plate, screen, and bias voltages of different values from a common power supply

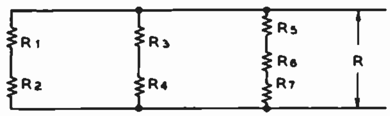


Figure 7
ANOTHER TYPE OF SERIES-PARALLEL CIRCUIT

source. It may also be used to obtain very low voltages of the order of .01 to .001 volt with a high degree of accuracy, even though a means of measuring such voltages is lacking. The procedure for making these measurements can best be given in the following example.

Assume that an accurately calibrated voltmeter reading from 0 to 150 volts is available, and that the source of voltage is exactly 100 volts. This 100 volts is then impressed through a resistance of exactly 1,000 ohms. It will, then, be found that the voltage along various points on the resistor, with respect to the grounded end, is exactly proportional to the resistance at that point. From Ohm's law, the current would be 0.1 ampere; this current remains unchanged since the original value of resistance (1,000 ohms) and the voltage source (100 volts) are unchanged. Thus, at a 500-ohm point on the resistor (half its entire resistance), the voltage will likewise be halved or reduced to 50 volts.

The equation ($E = I \times R$) gives the proof: $E = 500 \times 0.1 = 50$. At the point of 250 ohms on the resistor, the voltage will be one-fourth the total value, or 25 volts ($E = 250 \times 0.1 = 25$). Continuing with this process, a point can be found where the resistance measures exactly 1 ohm and where the voltage equals 0.1 volt. It is, therefore, obvious that if the original source of voltage and the resistance can be measured, it is a simple matter to predetermine the voltage at any point along the resistor, provided that the current remains constant, and provided that no current is taken from the tap-on point unless this current is taken into consideration.

Voltage Divider Calculations Proper design of a voltage divider for any type of radio equipment is a relatively simple matter. The first consideration is the amount of "bleeder current" to be drawn. In addition, it is also necessary that the desired voltage and the exact current at each tap on the voltage divider be known.

Figure 8 illustrates the flow of current in a simple voltage divider and load circuit. The light arrows indicate the flow of bleeder current, while the heavy arrows indicate the flow of the load current. The design of a combined

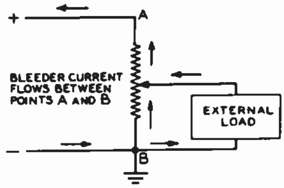


Figure 8
SIMPLE VOLTAGE DIVIDER CIRCUIT

The arrows indicate the manner in which the current flow divides between the voltage divider itself and the external load circuit.

bleeder resistor and voltage divider, such as is commonly used in radio equipment, is illustrated in the following example:

A power supply delivers 300 volts and is conservatively rated to supply all needed current for the receiver and still allow a bleeder current of 10 milliamperes. The following voltages are wanted: 75 volts at 2 milliamperes for the detector tube, 100 volts at 5 milliamperes for the screens of the tubes, and 250 volts at 20 milliamperes for the plates of the tubes. The required voltage drop across R_1 is 75 volts, across R_2 25 volts, across R_3 150 volts, and across R_4 it is 50 volts. These values are shown in the diagram of figure 9. The respective current values are also indicated. Apply Ohm's law:

$$R_1 = \frac{E}{I} = \frac{75}{.01} = 7{,}500 \text{ ohms.}$$

$$R_2 = \frac{E}{I} = \frac{25}{.012} = 2{,}083 \text{ ohms.}$$

$$R_3 = \frac{E}{I} = \frac{150}{.017} = 8{,}823 \text{ ohms.}$$

$$R_4 = \frac{E}{I} = \frac{50}{.037} = 1{,}351 \text{ ohms.}$$

$$R_{Total} = 7{,}500 + 2{,}083 + 8{,}823 + 1{,}351 = 19{,}757 \text{ ohms.}$$

A 20,000-ohm resistor with three sliding taps will be of the approximately correct size, and would ordinarily be used because of the difficulty in securing four separate resistors of the exact odd values indicated, and because no adjustment would be possible to compensate for any slight error in estimating the probable currents through the various taps.

When the sliders on the resistor once are set to the proper point, as in the above ex-

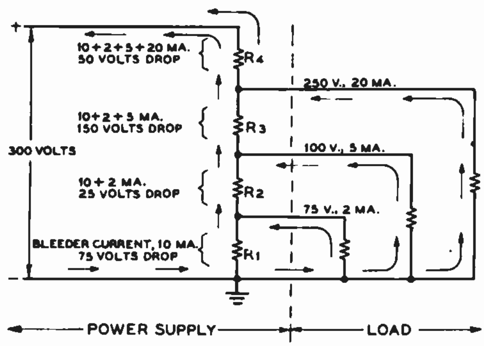


Figure 9
MORE COMPLEX VOLTAGE DIVIDER
The method for computing the values of the resistors is discussed in the accompanying text.

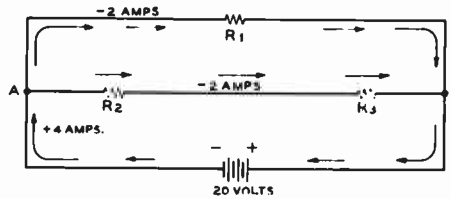


Figure 10
ILLUSTRATING KIRCHHOFF'S FIRST LAW
The current flowing toward point "A" is equal to the current flowing away from point "A."

ample, the voltages will remain constant at the values shown as long as the current remains a constant value.

Disadvantages of Voltage Dividers One of the serious disadvantages of the voltage divider becomes evident when the the current drawn from one of the taps changes. It is obvious that the voltage drops are interdependent and, in turn, the individual drops are in proportion to the current which flows through the respective sections of the divider resistor. The only remedy lies in providing a heavy steady bleeder current in order to make the individual currents so small a part of the total current that any change in current will result in only a slight change in voltage. This can seldom be realized in practice because of the excessive values of bleeder current which would be required.

Kirchhoff's Laws Ohm's law is all that is necessary to calculate the values in simple circuits, such as the preceding examples; but in more complex problems, involving several loops or more than one voltage in the same closed circuit, the use of *Kirchhoff's laws* will greatly simplify the calculations. These laws are merely rules for applying Ohm's law.

Kirchhoff's first law is concerned with net current to a point in a circuit and states that:

> *At any point in a circuit the current flowing toward the point is equal to the current flowing away from the point.*

Stated in another way: if currents flowing to the point are considered positive, and those flowing from the point are considered negative, the sum of all currents flowing toward and away from the point—taking signs into account—is equal to zero. Such a sum is known as an *algebraic sum;* such that the law can be stated thus: *The algebraic sum of all currents entering and leaving a point is zero.*

Figure 10 illustrates this first law. Since the effective resistance of the network of resistors is 5 ohms, it can be seen that 4 amperes flow toward point A, and 2 amperes flow away through the two 5-ohm resistors in series. The remaining 2 amperes flow away through the 10-ohm resistor. Thus, there are 4 amperes flowing to point A and 4 amperes flowing away from the point. If R is the effective resistance of the network (5 ohms), $R_1 = 10$ ohms, $R_2 = 5$ ohms, $R_3 = 5$ ohms, and $E = 20$ volts, we can set up the following equation:

$$\frac{E}{R} - \frac{E}{R_1} - \frac{E}{R_2 + R_3} = 0$$

$$\frac{20}{5} - \frac{20}{10} - \frac{20}{5+5} = 0$$

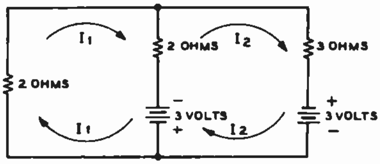
$$4 - 2 - 2 = 0$$

Kirchhoff's second law is concerned with net voltage drop around a closed loop in a circuit and states that:

> *In any closed path or loop in a circuit the sum of the IR drops must equal the sum of the applied e.m.f.'s.*

The second law also may be conveniently stated in terms of an algebraic sum as: *The algebraic sum of all voltage drops around a closed path or loop in a circuit is zero.* The applied e.m.f.'s (voltages) are considered positive, while IR drops taken in the direction of current flow (including the internal drop of the sources of voltage) are considered negative.

Figure 11 shows an example of the application of Kirchhoff's laws to a comparatively simple circuit consisting of three resistors and



1. SET VOLTAGE DROPS AROUND EACH LOOP EQUAL TO ZERO.
$I_1\,2_{(\text{OHMS})} + 2(I_1 - I_2) + 3 = 0$ (FIRST LOOP)
$-6 + 2(I_2 - I_1) + 3I_2 = 0$ (SECOND LOOP)

2. SIMPLIFY
$2I_1 + 2I_1 - 2I_2 + 3 = 0$ $\quad$ $2I_2 - 2I_1 + 3I_2 - 6 = 0$
$\frac{4I_1+3}{2} = I_2$ $\quad$ $5I_2 - 2I_1 - 6 = 0$
$\frac{2I_1+6}{5} = I_2$

3. EQUATE
$\frac{4I_1+3}{2} = \frac{2I_1+6}{5}$

4. SIMPLIFY
$20I_1 + 15 = 4I_1 + 12$
$I_1 = -\frac{3}{16}$ AMPERE

5. RE-SUBSTITUTE
$I_2 = \frac{-\frac{12}{16}+3}{2} = \frac{2\frac{1}{4}}{2} = 1\frac{1}{8}$ AMPERE

Figure 11
ILLUSTRATING KIRCHHOFF'S SECOND LAW
The voltage drop around any closed loop in a network is equal to zero.

two batteries. First assume an arbitrary direction of current flow in each closed loop of the circuit, drawing an arrow to indicate the assumed direction of current flow. Then equate the sum of all IR drops plus battery drops around each loop to zero. You will need one equation for each unknown to be determined. Then solve the equations for the unknown currents in the general manner indicated in figure 11. If the answer comes out positive the direction of current flow you originally assumed was correct. If the answer comes out negative, the current flow is in the opposite direction to the arrow which was drawn originally. This is illustrated in the example of figure 11 where the direction of flow of I_1 is opposite to the direction assumed in the sketch.

Power in Resistive Circuits In order to cause electrons to flow through a conductor, constituting a current flow, it is necessary to apply an electromotive force (voltage) across the circuit. Less power is expended in creating a small current flow through a given resistance than in creating a large one; so it is necessary to have a unit of power as a reference.

The unit of electrical power is the *watt*, which is the rate of energy consumption when an e.m.f. of 1 volt forces a current of 1 ampere through a circuit. The power in a resistive circuit is equal to the product of the voltage applied across, and the current flowing in, a given circuit. Hence: P (watts) = E (volts) × I (amperes).

Since it is often convenient to express power in terms of the resistance of the circuit and the current flowing through it, a substitution of IR for E (E = IR) in the above formula gives: P = IR × I or $P = I^2R$. In terms of voltage and resistance, $P = E^2/R$. Here, I = E/R and when this is substituted for I the original formula becomes P = E × E/R, or $P = E^2/R$. To repeat these three expressions:

$$P = EI,\ P = I^2R,\ \text{and}\ P = E^2/R,$$

where P is the power in watts,
E is the electromotive force in volts, and
I is the current in amperes.

To apply the above equations to a typical problem: The voltage drop across a cathode resistor in a power amplifier stage is 50 volts; the plate current flowing through the resistor is 150 milliamperes. The number of watts the resistor will be required to dissipate is found from the formula: P = EI, or 50 × .150 = 7.5 watts (.150 amperes is equal to 150 milliamperes). From the foregoing it is seen that a 7.5-watt resistor will safely carry the required current, yet a 10- or 20-watt resistor would ordinarily be used to provide a safety factor.

In another problem, the conditions being similar to those above, but with the resistance (R = 333⅓ ohms), and current being the *known* factors, the solution is obtained as follows: $P = I^2R = .0225 \times 333.33 = 7.5$. If only the voltage and resistance are known, $P = E^2/R = 2500/333.33 = 7.5$ watts. It is seen that all three equations give the same results; the selection of the particular equation depends only upon the known factors.

Power, Energy and Work It is important to remember that power (expressed in watts, horsepower, etc.), represents the *rate* of energy consumption or the *rate* of doing work. But when we pay our electric bill

Figure 12
MATCHING OF RESISTANCES

To deliver the greatest amount of power to the load, the load resistance R_L should be equal to the internal resistance of the battery R_1.

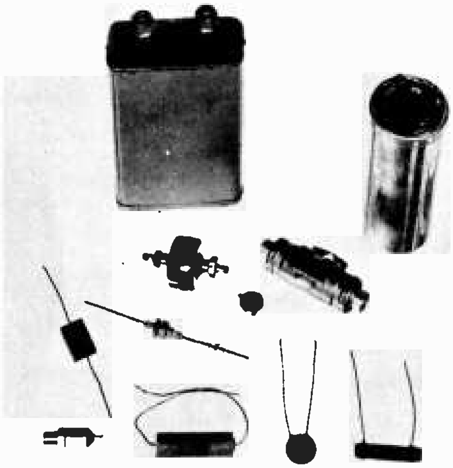


Figure 13
TYPICAL CAPACITORS
The two large units are high value filter capacitors. Shown beneath these are various types of by-pass capacitors for r-f and audio application.

to the power company we have purchased a specific *amount* of *energy* or *work* expressed in the common units of *kilowatt-hours*. Thus *rate* of energy consumption (watts or kilowatts) multiplied by *time* (seconds, minutes or hours) gives us total energy or work. Other units of energy are the watt-second, BTU, calorie, erg, and joule.

Heating Effect Heat is generated when a source of voltage causes a current to flow through a resistor (or, for that matter, through any conductor). As explained earlier, this is due to the fact that heat is given off when free electrons collide with the atoms of the material. More heat is generated in high resistance materials than in those of low resistance, since the free electrons must strike the atoms harder to knock off other electrons. As the heating effect is a function of the current flowing and the resistance of the circuit, the power expended in heat is given by the second formula: $P = I^2R$.

2-3 Electrostatics — Capacitors

Electrical energy can be stored in an electrostatic field. A device capable of storing energy in such a field is called *capacitor* (in earlier usage the term *condenser* was frequently used but the IRE standards call for the use of capacitor instead of condenser) and is said to have a certain *capacitance*. The *energy* stored in an electrostatic field is expressed in *joules* (watt seconds) and is equal to $CE^2/2$, where C is the capacitance in *farads* (a unit of capacitance to be discussed) and E is the potential in volts. The *charge* is equal to CE, the charge being expressed in coulombs.

Capacitance and Capacitors Two metallic plates separated from each other by a thin layer of insulating material (called a *dielectric*, in this case), becomes a *capacitor*. When a source of d-c potential is momentarily applied across these plates, they may be said to become charged. If the same two plates are then joined together momentarily by means of a switch, the capacitor will *discharge*.

When the potential was first applied, electrons immediately flowed from one plate to the other through the battery or such source of d-c potential as was applied to the capacitor plates. However, the circuit from plate to plate in the capacitor was *incomplete* (the two plates being separated by an insulator) and thus the electron flow ceased, meanwhile establishing a shortage of electrons on one plate and a surplus of electrons on the other.

Remember that when a deficiency of electrons exists at one end of a conductor, there is always a tendency for the electrons to move about in such a manner as to re-establish a state of balance. In the case of the capacitor herein discussed, the surplus quantity of electrons on one of the capacitor plates cannot move to the other plate because the circuit has been broken; that is, the battery or d-c potential was removed. This leaves the capacitor in a *charged* condition; the capacitor plate with the electron *deficiency* is *positively* charged, the other plate being *negative*.

In this condition, a considerable stress exists in the insulating material (dielectric) which separates the two capacitor plates, due to the mutual attraction of two unlike potentials on the plates. This stress is known as *electrostatic* energy, as contrasted with *electromagnetic* energy in the case of an inductor. This charge can also be called *potential energy* because it is capable of performing work when the charge is released through an external circuit. The charge is proportional to the voltage but the energy is proportional to the voltage squared, as shown in the following analogy.

The charge represents a definite amount of electricity, or a given number of electrons. The potential energy possessed by these electrons depends not only upon their number, but also upon their potential or voltage.

Compare the electrons to water, and two capacitors to standpipes, a 1 μfd. capacitor to

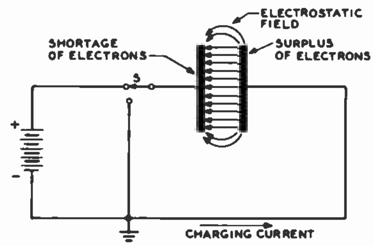


Figure 14
SIMPLE CAPACITOR
Illustrating the imaginary lines of force representing the paths along which the repelling force of the electrons would act on a free electron located between the two capacitor plates.

a standpipe having a cross section of 1 square inch and a 2 μfd. capacitor to a standpipe having a cross section of 2 square inches. The charge will represent a given volume of water, as the "charge" simply indicates a certain number of electrons. Suppose the water is equal to 5 gallons.

Now the potential energy, or capacity for doing work, of the 5 gallons of water will be twice as great when confined to the 1 sq. in. standpipe as when confined to the 2 sq. in. standpipe. Yet the volume of water, or "charge" is the same in either case.

Likewise a 1 μfd. capacitor charged to 1000 volts possesses twice as much potential energy as does a 2 μfd. capacitor charged to 500 volts, though the *charge* (expressed in *coulombs:* $Q = CE$) is the same in either case.

The Unit of Capacitance: The Farad If the external circuit of the two capacitor plates is completed by joining the terminals together with a piece of wire, the electrons will rush immediately from one plate to the other through the external circuit and establish a state of equilibrium. This latter phenomenon explains the *discharge* of a capacitor. The amount of stored energy in a charged capacitor is dependent upon the charging potential, as well as a factor which takes into account the *size* of the plates, *dielectric thickness*, *nature* of the dielectric, and the *number* of plates. This factor, which is determined by the foregoing, is called the *capacitance* of a capacitor and is expressed in *farads*.

The farad is such a large unit of capacitance that it is rarely used in radio calculations, and the following more practical units have, therefore, been chosen.

1 *microfarad* = 1/1,000,000 *of a farad, or* .000001 *farad, or* 10^{-6} *farads.*

1 *micro-microfarad* = 1/1,000,000 *of a microfarad, or* .000001 *microfarad, or* 10^{-6} *microfarads.*

1 *micro-microfarad = one-millionth of one-millionth of a farad, or* 10^{-12} *farads.*

If the capacitance is to be expressed in *microfarads* in the equation given for *energy storage*, the factor C would then have to be divided by 1,000,000, thus:

$$\text{Stored energy in joules} = \frac{C \times E^2}{2 \times 1{,}000{,}000}$$

This storage of energy in a capacitor is one of its very important properties, particularly in those capacitors which are used in power supply filter circuits.

Dielectric Materials Although any substance which has the characteristics of a good insulator may be used as a dielectric material, commercially manufactured capacitors make use of dielectric materials which have been selected because their characteristics are particularly suited to the job at hand. Air is a very good dielectric material, but an air-spaced capacitor does not have a high capacitance since the dielectric constant of air is only slightly greater than one. A group of other commonly used dielectric mateials is listed in figure 15.

Certain materials, such as bakelite, lucite, and other plastics dissipate considerable energy when used as capacitor dielectrics.

TABLE OF DIELECTRIC MATERIALS

MATERIAL	DIELECTRIC CONSTANT 10 MC.	POWER FACTOR 10 MC.	SOFTENING POINT FAHRENHEIT
ANILINE-FORMALDEHYDE RESIN	3.4	0.004	260°
BARIUM TITANATE	1200	1.0	—
CASTOR OIL	4.67		
CELLULOSE ACETATE	3.7	0.04	180°
GLASS, WINDOW	6-8	POOR	2000°
GLASS, PYREX	4.5	0.02	
KEL-F FLUOROTHENE	2.5	0.6	—
METHYL-METHACRYLATE—LUCITE	2.8	0.007	160°
MICA	5.4	0.0003	
MYCALEX, MYKROY	7.0	0.002	650°
PHENOL-FORMALDEHYDE, LOW-LOSS YELLOW	5.0	0.015	270°
PHENOL-FORMALDEHYDE BLACK BAKELITE	5.5	0.03	350°
PORCELAIN	7.0	0.005	2800°
POLYETHYLENE	2.25	0.0003	220°
POLYSTYRENE	2.55	0.0002	175°
QUARTZ, FUSED	4.2	0.0002	2600°
RUBBER, HARD-EBONITE	2.8	0.007	150°
STEATITE	6.1	0.003	2700°
SULFUR	3.8	0.003	236°
TEFLON	2.1	0.02	—
TITANIUM DIOXIDE	100-175	0.0006	2700°
TRANSFORMER OIL	2.2	0.003	
UREA-FORMALDEHYDE	5.0	0.05	260°
VINYL RESINS	4.0	0.02	200°
WOOD, MAPLE	4.4	POOR	

FIGURE 15

This energy loss is expressed in terms of the *power factor* of the capacitor, which represents the portion of the input volt-amperes lost in the dielectric material. Other materials including air, polystyrene and quartz have a very low power factor.

The new *ceramic* dielectrics such as steatite (talc) and titanium dioxide products are especially suited for high frequency and high temperature operation. Ceramics based upon titanium dioxide have an unusually high dielectric constant combined with a low power factor. The temperature coefficient with respect to capacity of units made with this material depends upon the mixture of oxides, and coefficients ranging from zero to over -700 parts per million per degree Centigrade may be obtained in commercial production.

Mycalex is a composition of minute mica particles and lead borate glass, mixed and fired at a relatively low temperature. It is hard and brittle, but can be drilled or machined when water is used as the cutting lubricant.

Mica dielectric capacitors have a very low power factor and extremely high voltage breakdown per unit of thickness. A mica and copper-foil "sandwich" is formed under pressure to obtain the desired capacity value. The effect of temperature upon the pressures in the "sandwich" causes the capacity of the usual mica capacitor to have large, non-cyclic variations. If the copper electrodes are plated directly upon the mica sheets, the temperature coefficient can be stablized at about 20 parts per million per degree Centigrade. A process of this type is used in the manufacture of "silver mica" capacitors.

Paper dielectric capacitors consist of strips of aluminum foil insulated from each other by a thin layer of paper, the whole assembly being wrapped in a circular bundle. The cost of such a capacitor is low, the capacity is high in proportion to the size and weight, and the power factor is good. The life of such a capacitor is dependent upon the moisture penetration of the paper dielectric and upon the applied d-c voltage.

Air dielectric capacitors are used in transmitting and receiving circuits, principally where a variable capacitor of high resetability is required. The dielectric strength is high, though somewhat less at radio frequencies than at 60 cycles. In addition, corona discharge at high frequencies will cause ionization of the air dielectric causing an increase in power loss. Dielectric strength may be increased by increasing the air pressure, as is done in hermetically sealed radar units. In some units, dry nitrogen gas may be used in place of air to provide a higher dielectric strength than that of air.

Likewise, the dielectric strength of an "air" capacitor may be increased by placing the unit in a vacuum chamber to prevent ionization of the dielectric.

The temperature coefficient of a variable air dielectric capacitor varies widely and is often non-cyclic. Such things as differential expansion of various parts of the capacitor, changes in internal stresses and different temperature coefficients of various parts contribute to these variances.

Dielectric Constant The capacitance of a capacitor is determined by the thickness and nature of the dielectric material between plates. Certain materials offer a greater capacitance than others, depending upon their physical makeup and chemical constitution. This property is expressed by a constant K, called the dielectric constant. (K = 1 for air.)

Dielectric Breakdown If the charge becomes too great for a given thickness of a certain dielectric, the capacitor will break down, i.e., the dielectric will puncture. It is for this reason that capacitors are rated in the manner of the amount of voltage they will safely withstand as well as the capacitance in microfarads. This rating is commonly expressed as the *d-c working voltage.*

Calculation of Capacitance The capacitance of two parallel plates is given with good accuracy by the following formula:

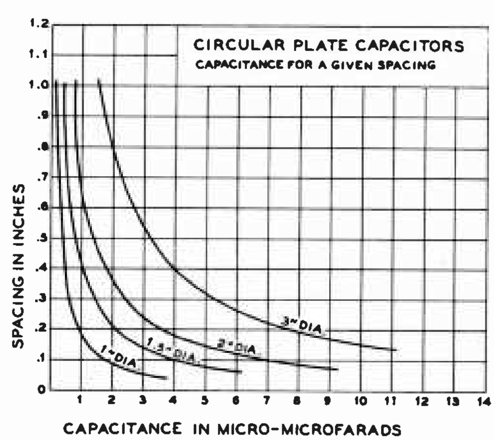


Figure 16

Through the use of this chart it is possible to determine the required plate diameter (with the the necessary spacing established by peak voltage considerations) for a circular-plate neutralizing capacitor. The capacitance given is for a dielectric of air and the spacing given is between adjacent faces of the two plates.

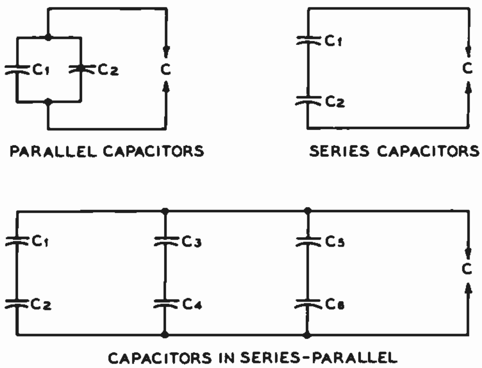


Figure 17
CAPACITORS IN SERIES, PARALLEL, AND SERIES-PARALLEL

$$C = 0.2248 \times K \times \frac{A}{t},$$

where C = capacitance in micro-microfarads,
K = dielectric constant of spacing material,
A = area of dielectric in square inches,
t = thickness of dielectric in inches.

This formula indicates that the capacitance is directly proportional to the area of the plates and inversely proportional to the thickness of the dielectric (spacing between the plates). This simply means that when the area of the plate is doubled, the spacing between plates remaining constant, the capacitance will be doubled. Also, if the area of the plates remains constant, and the plate spacing is doubled, the capacitance will be reduced to half.

The above equation also shows that capacitance is directly proportional to the dielectric constant of the spacing material. An air-spaced capacitor that has a capacitance of 100 $\mu\mu$fd. in air would have a capacitance of 467 $\mu\mu$fd. when immersed in castor oil, because the dielectric constant of castor oil is 4.67 times as great as the dielectric constant of air.

Where the area of the plates is definitely set, when it is desired to know the spacing needed to secure a required capacitance,

$$t = \frac{A \times 0.2248 \times K}{C}$$

where all units are expressed just as in the preceding formula. This formula is not confined to capacitors having only square or rectangular plates, but also applies when the plates are circular in shape. The only change will be the calculation of the *area* of such circular plates; this area can be computed by squaring the *radius* of the plate, then multiplying by 3.1416, or "pi." Expressed as an equation:

$$A = 3.1416 \times r^2$$

where r = radius in inches

The capacitance of a multi-plate capacitor can be calculated by taking the capacitance of one section and multiplying this by the number of dielectric spaces. In such cases, however, the formula gives no consideration to the effects of edge capacitance; so the capacitance as calculated will not be entirely accurate. These additional capacitances will be but a small part of the effective total capacitance, particularly when the plates are reasonably large and thin, and the final result will, therefore, be within practical limits of accuracy.

Capacitors in Parallel and in Series Equations for calculating capacitances of capacitors in *parallel* connections are the same as those for resistors in *series*.

$$C = C_1 + C_2 + \ldots + C_n$$

Capacitors in *series* connection are calculated in the same manner as are resistors in *parallel* connection.

The formulas are repeated: (1) For two or more capacitors of *unequal* capacitance in series:

$$C = \frac{1}{\frac{1}{C_1} + \frac{1}{C_2} + \frac{1}{C_3}},$$

$$\text{or } \frac{1}{C} = \frac{1}{C_1} + \frac{1}{C_2} + \frac{1}{C_3}$$

(2) *Two* capacitors of *unequal* capacitance in series:

$$C = \frac{C_1 \times C_2}{C_1 + C_2}$$

(3) Three capacitors of *equal* capacitance in series:

$C = \frac{C_1}{3}$ where C_1 is the common capacitance.

(4) Three or more capacitors of *equal* capacitance in series.

$$C = \frac{\text{Value of common capacitance}}{\text{Number of capacitors in series}}$$

(5) Six capacitors in series parallel:

$$C = \frac{1}{\frac{1}{C_1}+\frac{1}{C_2}} + \frac{1}{\frac{1}{C_3}+\frac{1}{C_4}} + \frac{1}{\frac{1}{C_5}+\frac{1}{C_6}}$$

Capacitors in A-C and D-C Circuits When a capacitor is connected into a direct-current circuit, it will block the d.c., or stop the flow of current. Beyond the initial movement of electrons during the period when the capacitor is being charged, there will be no flow of current because the circuit is effectively broken by the dielectric of the capacitor.

Strictly speaking, a very small current may actually flow because the dielectric of the capacitor may not be a perfect insulator. This minute current flow is the leakage current previously referred to and is dependent upon the internal d-c resistance of the capacitor. This leakage current is usually quite noticeable in most types of electrolytic capacitors.

When an alternating current is applied to a capacitor, the capacitor will charge and discharge a certain number of times per second in accordance with the frequency of the alternating voltage. The electron flow in the charge and discharge of a capacitor when an a-c potential is applied constitutes an alternating current, in effect. It is for this reason that a capacitor will pass an alternating current yet offer practically infinite opposition to a direct current. These two properties are repeatedly in evidence in a radio circuit.

Voltage Rating of Capacitors in Series Any good paper dielectric filter capacitor has such a high internal resistance (indicating a good dielectric) that the exact resistance will vary considerably from capacitor to capacitor even though they are made by the same manufacturer and are of the same rating. Thus, when 1000 volts d.c. is connected across two 1-μfd. 500-volt capacitors in series, the chances are that the voltage will divide unevenly and one capacitor will receive more than 500 volts and the other less than 500 volts.

Voltage Equalizing Resistors By connecting a half-megohm 1-watt carbon resistor across each capacitor, the voltage will be equalized because the resistors act as a voltage divider, and the internal resistances of the capacitors are so much higher (many megohms) that they have but little effect in disturbing the voltage divider balance.

Carbon resistors of the inexpensive type are not particularly accurate (not being designed for precision service); therefore it is advisable to check several on an accurate ohmmeter to find two that are as close as possible in resistance. The exact resistance is unimportant, just so it is the same for the two resistors used.

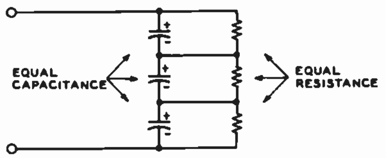


Figure 18
SHOWING THE USE OF VOLTAGE EQUALIZING RESISTORS ACROSS CAPACITORS CONNECTED IN SERIES

Capacitors in Series on A.C. When two capacitors are connected in series, *alternating* voltage pays no heed to the relatively high internal resistance of each capacitor, but divides across the capacitors in inverse proportion to the *capacitance*. Because, in addition to the d.c. across a capacitor in a filter or audio amplifier circuit there is usually an a-c or a-f voltage component, it is inadvisable to series-connect capacitors of unequal capacitance even if dividers are provided to keep the d.c. within the ratings of the individual capacitors.

For instance, if a 500-volt 1-μfd. capacitor is used in series with a 4-μfd. 500-volt capacitor across a 250-volt a-c supply, the 1-μfd. capacitor will have 200 volts a.c. across it and the 4-μfd. capacitor only 50 volts. An equalizing divider to do any good in this case would have to be of very low resistance because of the comparatively low impedance of the capacitors to a.c. Such a divider would draw excessive current and be impracticable.

The safest rule to follow is to use only capacitors of the same capacitance and voltage rating and to install matched high resistance proportioning resistors across the various capacitors to equalize the d-c voltage drop across each capacitor. This holds regardless of how many capacitors are series-connected.

Electrolytic Capacitors Electrolytic capacitors use a very thin film of oxide as the dielectric, and are polarized; that is, they have a positive and a negative terminal which must be properly connected in a circuit; otherwise, the oxide will break down and the capacitor will overheat. The unit then will no longer be of service. When electrolytic capacitors are connected in series, the positive terminal is always connected to the positive lead of the power supply; the negative terminal of the capacitor connects to the positive terminal of the *next* capacitor in the series combination. The method of connection for electrolytic capacitors in series is shown in figure 18. Electrolytic capacitors have very low cost per microfarad of capacity, but also have a large power factor and high leakage; both dependent upon applied voltage, temperature and the age of the capacitor. The modern electrolytic capacitor uses a dry paste electrolyte embedded in a gauze or paper dielectric. Aluminium foil and the dielectric are wrapped in a circular bundle and are mounted in a cardboard or metal box. Etched electrodes may be employed to increase the effective anode area, and the total capacity of the unit.

The capacity of an electrolytic capacitor is affected by the applied voltage, the usage of the capacitor, and the temperature and humidity of the environment. The capacity usually drops with the aging of the unit. The leakage current and power factor increase with age. At high frequencies the power factor becomes so poor that the electrolytic capacitor acts as a series resistance rather than as a capacity.

2-4 Magnetism and Electromagnetism

The common bar or horseshoe magnet is familiar to most people. The magnetic field which surrounds it causes the magnet to attract other magnetic materials, such as iron nails or tacks. Exactly the same kind of magnetic field is set up around any conductor carrying a current, but the field exists only while the current is flowing.

Magnetic Fields Before a potential, or voltage, is applied to a conductor there is no external field, because there is no general movement of the electrons in one direction. However, the electrons do progressively move along the conductor when an e.m.f. is applied, the direction of motion depending upon the polarity of the e.m.f. Since each electron has an electric field about it, the flow of electrons causes these fields to build up into a resultant external field which acts in a plane at right angles to the direction in which the current is flowing. This field is known as the *magnetic field.*

The magnetic field around a current-carrying conductor is illustrated in figure 19. The direction of this magnetic field depends entirely upon the direction of electron drift or current flow in the conductor. When the flow is toward the observer, the field about the conductor is clockwise; when the flow is away from the observer, the field is counter-clockwise. This is easily remembered if the left hand is clenched, with the thumb outstretched

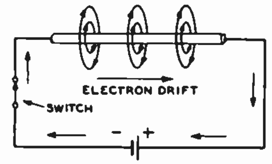


Figure 19
LEFT-HAND RULE
Showing the direction of the magnetic lines of force produced around a conductor carrying an electric current.

and pointing in the direction of electron flow. The fingers then indicate the direction of the magnetic field around the conductor.

Each electron adds its field to the total external magnetic field, so that the greater the number of electrons moving along the conductor, the stronger will be the resulting field.

One of the fundamental laws of magnetism is that *like poles repel one another and unlike poles attract one another.* This is true of current-carrying conductors as well as of permanent magnets. Thus, if two conductors are placed side by side and the current in each is flowing in the same direction, the magnetic fields will also be in the same direction and will combine to form a larger and stronger field. If the current flow in adjacent conductors is in opposite directions, the magnetic fields oppose each other and tend to cancel.

The magnetic field around a conductor may be considerably increased in strength by winding the wire into a coil. The field around each wire then combines with those of the adjacent turns to form a total field through the coil which is concentrated along the axis of the coil and behaves externally in a way similar to the field of a bar magnet.

If the left hand is held so that the thumb is outstretched and parallel to the axis of a coil, with the fingers curled to indicate the direction of electron flow around the turns of the coil, the thumb then points in the direction of the north pole of the magnetic field.

The Magnetic Circuit In the magnetic circuit, the units which correspond to current, voltage, and resistance in the electrical circuit are *flux, magnetomotive force,* and *reluctance.*

Flux, Flux Density As a current is made up of a drift of electrons, so is a magnetic field made up of lines of force, and the total number of lines of force in a given magnetic circuit is termed the *flux.* The flux depends upon the material, cross section, and length of the magnetic circuit, and it varies directly as the current flowing in the circuit.

The unit of flux is the *maxwell*, and the symbol is the Greek letter ϕ (phi).

Flux density is the number of lines of force per unit area. It is expressed in *gauss* if the unit of area is the square centimeter (1 gauss = 1 line of force per square centimeter), or in *lines per square incb*. The symbol for flux density is B if it is expressed in gausses, or B if expressed in lines per square inch.

Magnetomotive Force The force which produces a flux in a magnetic circuit is called *magnetomotive force*. It is abbreviated m.m.f. and is designated by the letter F. The unit of magnetomotive force is the *gilbert*, wbicb is equivalent to $1.26 \times$ NI, where N is the number of turns and I is the current flowing in the circuit in amperes.

The m.m.f. necessary to produce a given flux density is stated in gilberts per centimeter (oersteds) (H), or in ampere-turns per inch (H).

Reluctance Magnetic reluctance corresponds to electrical resistance, and is the property of a material that opposes the creation of a magnetic flux in the material. It is expressed in *rels*, and the symbol is the letter R. A material has a reluctance of 1 rel when an m.m.f. of 1 ampere-turn (NI) generates a flux of 1 line of force in it. Combinations of reluctances are treated the same as resistances in finding the total effective reluctance. The *specific reluctance* of any substance is its reluctance per unit volume.

Except for iron and its alloys, most common materials have a specific reluctance very nearly the same as that of a vacuum, which, for all practical purposes, may be considered the same as the specific reluctance of air.

Ohm's Law for Magnetic Circuits The relations between flux, magnetomotive force, and reluctance are exactly the same as the relations between current, voltage, and resistance in the electrical circuit. These can be stated as follows:

$$\phi = \frac{F}{R} \qquad R = \frac{F}{\phi} \qquad F = \phi R$$

where ϕ = flux, F = m.m.f., and R = reluctance.

Permeability Permeability expresses the ease with which a magnetic field may be set up in a material as compared with the effort required in the case of air. Iron, for example, has a permeability of around 2000 times that of air, which means that a given amount of magnetizing effect produced in an iron core by a current flowing through a coil of wire will produce 2000 times tbe *flux* density that the same magnetizing effect would produce in air. It may be expressed by the ratio B/H or B/H. In other words,

$$\mu = \frac{B}{H} \quad \text{or} \quad \mu = \frac{\mathrm{B}}{\mathrm{H}}$$

where μ is the premeability, B is the flux density in gausses, B is the flux density in lines per square inch, H is the m.m.f. in gilberts per centimeter (oersteds), and H is the m.m.f. in ampere-turns per inch. These relations may also be stated as follows:

$$H = \frac{B}{\mu} \quad \text{or} \quad \mathrm{H} = \frac{\mathrm{B}}{\mu}, \quad \text{and} \quad B = H\mu \quad \text{or} \quad \mathrm{B} = \mathrm{H}\mu$$

It can be seen from the foregoing that permeability is inversely proportional to the specific reluctance of a material.

Saturation Permeability is similar to *electric conductivity*. There is, however, one important difference: the permeability of magnetic materials is not independent of the magnetic current (flux) flowing through it, although electrical conductivity is substantially independent of the electric current in a wire. When the flux density of a magnetic conductor has been increased to tbe *saturation point*, a further increase in the magnetizing force will not produce a corresponding increase in flux density.

Calculations To simplify magnetic circuit calculations, a magnetization curve may be drawn for a given unit of material. Such a curve is termed a B-H curve, and may be determined by experiment. When the current in an iron core coil is first applied, the relation between the winding current and the core flux is sbown at A-B in figure 20. If the current is then reduced to zero, reversed, brought back again to zero and reversed to the

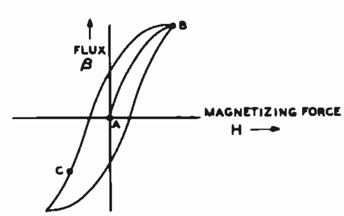


Figure 20
TYPICAL HYSTERESIS LOOP
(B-H CURVE = A-B)
Showing relationship between the current in the winding of an iron core inductor and the core flux. A direct current flowing through the inductance brings the magnetic state of the core to some point on the hysteresis loop, such as C.

original direction, the flux passes through a typical hysteresis loop as shown.

Residual Magnetism; Retentivity The magnetism remaining in a material after the magnetizing force is removed is called *residual magnetism. Retentivity* is the property which causes a magnetic material to have residual magnetism after having been magnetized.

Hysteresis; Coercive Force *Hysteresis* is the characteristic of a magnetic system which causes a loss of power due to the fact that a negative magnetizing force must be applied to reduce the residual magnetism to zero. This negative force is termed *coercive force.* By "negative" magnetizing force is meant one which is of the opposite polarity with respect to the original magnetizing force. Hysteresis loss is apparent in transformers and chokes by the heating of the core.

Inductance If the switch shown in figure 19 is opened and closed, a pulsating direct current will be produced. When it is first closed, the current does not instantaneously rise to its maximum value, but builds up to it. While it is building up, the magnetic field is expanding around the conductor. Of course, this happens in a small fraction of a second. If the switch is then opened, the current stops and the magnetic field contracts quickly. This expanding and contracting field will induce a current in any other conductor that is part of a continuous circuit which it cuts. Such a field can be obtained in the way just mentioned by means of a vibrator interruptor, or by applying a.c. to the circuit in place of the battery. Varying the resistance of the circuit will also produce the same effect. This inducing of a current in a conductor due to a varying current in another conductor not in acutal contact is called *electromagnetic induction.*

Self-Inductance If an alternating current flows through a coil the varying magnetic field around each turn cuts itself and the adjacent turn and *induces a voltage in the coil of opposite polarity to the applied e.m.f.* The amount of induced voltage depends upon the number of turns in the coil, the current flowing in the coil, and the number of lines of force threading the coil. The voltage so induced is known as a *counter-e.m.f.* or *back-e.m.f.*, and the effect is termed *self-induction.* When the applied voltage is building up, the counter-e.m.f. opposes the rise; when the applied voltage is decreasing, the counter-e.m.f. is of the same polarity and tends to maintain the current. Thus, it can be seen that self-induction tends to prevent any change in the current in the circuit.

The storage of energy in a magnetic field is expressed in *joules* and is equal to $(LI^2)/2$. (A joule is equal to 1 watt-second. L is defined immediately following.)

The Unit of Inductance; The Henry Inductance is usually denoted by the letter L, and is expressed in *henrys.* A coil has an inductance of 1 henry when a voltage of 1 volt is induced by a current change of 1 ampere per second. The henry, while commonly used in audio frequency circuits, is too large for reference to inductance coils, such as those used in radio frequency circuits; *millihenry* or *microhenry* is more commonly used, in the following manner:

1 *henry* = 1,000 *millihenrys,* or 10^3 *millihenrys.*

1 *millihenry* = 1/1,000 *of a henry,* .001 *henry, or* 10^{-3} *henry.*

1 *microhenry* = 1/1,000,000 *of a henry, or* .000001 *henry, or* 10^{-6} *henry.*

1 *microhenry* = 1/1,000 *of a millihenry,* .001 *or* 10^{-3} *millihenrys.*

1,000 *microhenrys* = 1 *millihenry.*

Mutual Inductance When one coil is near another, a varying current in one will produce a varying magnetic field which cuts the turns of the other coil, inducing a current in it. This induced current is also varying, and will therefore induce another current in the first coil. This reaction between two coupled circuits is called *mutual induction,* and can be calculated and expressed in henrys. The symbol for mutual inductance is M. Two circuits thus joined are said to be *inductively coupled.*

The magnitude of the mutual inductance depends upon the shape and size of the two circuits, their positions and distances apart, and the premeability of the medium. The extent to

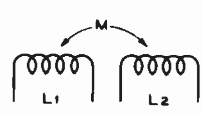
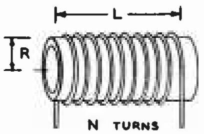


Figure 21
MUTUAL INDUCTANCE
The quantity M represents the mutual inductance between the two coils L_1 and L_2.



INDUCTANCE OF SINGLE-LAYER SOLENOID COILS

$$L = \frac{R^2 N^2}{9R + 10L} \text{ MICROHENRIES}$$

WHERE: R = RADIUS OF COIL TO CENTER OF WIRE
L = LENGTH OF COIL
N = NUMBER OF TURNS

Figure 22
FORMULA FOR CALCULATING INDUCTANCE

Through the use of the equation and the sketch shown above the inductance of single-layer solenoid coils can be calculated with an accuracy of about one per cent for the types of coils normally used in the h-f and v-h-f range.

which two inductors are coupled is expressed by a relation known as *coefficient of coupling.* This is the ratio of the mutual inductance actually present to the maximum possible value.

The formula for mutual inductance is $L = L_1 + L_2 + 2M$ when the coils are poled so that their fields add. When they are poled so that their fields buck, then $L = L_1 + L_2 - 2M$ (figure 21).

Inductors in Parallel Inductors in parallel are combined exactly as are resistors in parallel, provided that they are far enough apart so that the mutual inductance is entirely negligible.

Inductors in Series Inductors in series are additive, just as are resistors in series, again provided that no mutual inductance exists. In this case, the total inductance L is:

$$L = L_1 + L_2 + \ldots\ldots\ldots \text{etc.}$$

Where mutual inductance does exist:

$$L = L_1 + L_2 + 2M,$$

where M is the mutual inductance.

This latter expression assumes that the coils are connected in such a way that all flux linkages are in the same direction, i.e., additive. If this is not the case and the mutual linkages *subtract* from the self-linkages, the following formula holds:

$$L = L_1 + L_2 - 2M,$$

where M is the mutual inductance.

Core Material Ordinary magnetic cores cannot be used for radio frequencies because the *eddy current and hysteresis losses* in the core material becomes enormous as the frequency is increased. The principal use for conventional magnetic cores is in the audio-frequency range below approximately 15,000 cycles, whereas at very low frequencies (50 to 60 cycles) their use is mandatory if an appreciable value of inductance is desired.

An air core inductor of only 1 henry inductance would be quite large in size, yet values as high as 500 henrys are commonly available in small iron core chokes. The inductance of a coil with a magnetic core will vary with the amount of current (both a-c and d-c) which passes through the coil. For this reason, iron core chokes that are used in power supplies have a certain inductance rating at a *predetermined value of d-c.*

The premeability of air does not change with flux density; so the inductance of iron core coils often is made less dependent upon flux density by making part of the magnetic path air, instead of utilizing a closed loop of iron. This incorporation of an *air gap* is necessary in many applications of iron core coils, particularly where the coil carries a considerable d-c component. Because the permeability of air is so much lower than that of iron, the air gap need comprise only a small fraction of the magnetic circuit in order to provide a substantial proportion of the total reluctance.

Iron Cored Inductors at Radio Frequencies Iron-core inductors may be used at radio frequencies if the iron is in a very finely divided form, as in the case of the powdered iron cores used in some types of r-f coils and i-f transformers. These cores are made of extremely small particles of iron. The particles are treated with an insulating material so that each particle will be insulated from the others, and the treated powder is molded with a binder into cores. Eddy current losses are greatly reduced, with the result that these special iron cores are entirely practical in circuits which operate up to 100 Mc. in frequency.

2-5 RC and RL Transients

A voltage divider may be constructed as shown in figure 23. Kirchhoff's and Ohm's Laws hold for such a divider. This circuit is known as an RC circuit.

Time Constant-RC and RL Circuits When switch S in figure 23 is placed in position 1, a voltmeter across capacitor C will indicate the manner in which the capacitor will become charged through the resistor R from battery B. If relatively large values are used for R and C, and if a v-t voltmeter which draws negligible current is used

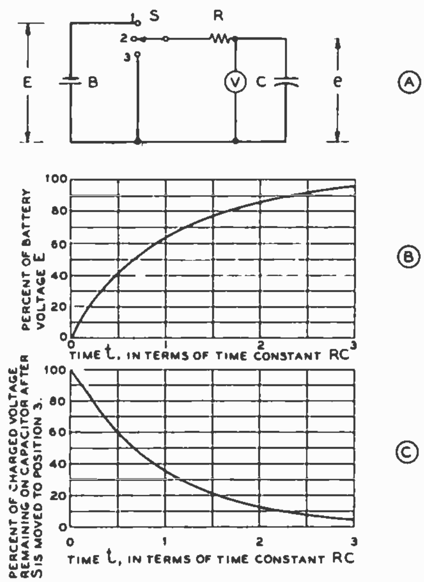


Figure 23
TIME CONSTANT OF AN R-C CIRCUIT
Shown at (A) is the circuit upon which is based the curves of (B) and (C). (B) shows the rate at which capacitor C will charge from the instant at which switch S is placed in position 1. (C) shows the discharge curve of capacitor C from the instant at which switch S is placed in position 3.

to measure the voltage *e*, the rate of charge of the capacitor may actually be plotted with the aid of a stop watch.

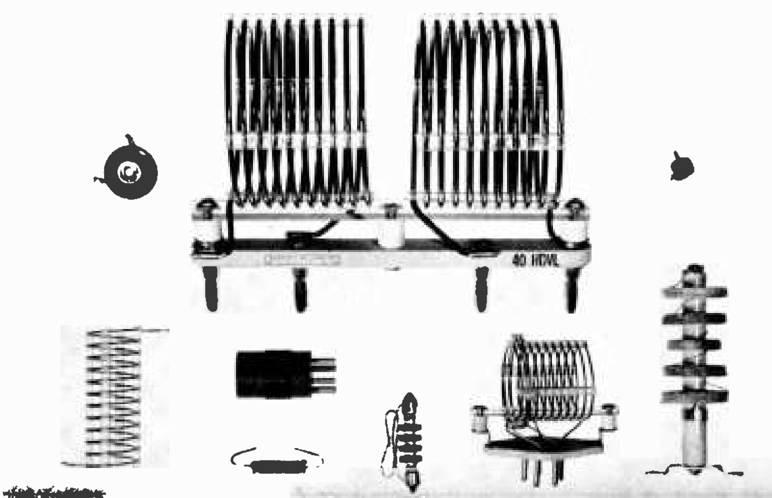
Voltage Gradient It will be found that the voltage *e* will begin to rise rapidly from zero the instant the switch is closed. Then, as the capacitor begins to charge, the rate of change of voltage across the capacitor will be found to decrease, the charging taking place more and more slowly as the capacitor voltage *e* approaches the battery voltage E. Actually, it will be found that in any given interval a constant percentage of the remaining difference between *e* and E will be delivered to the capacitor as an increase in voltage. A voltage which changes in this manner is said to increase *logarithmically*, or is said to follow an *exponential* curve.

Time Constant A mathematical analysis of the charging of a capacitor in this manner would show that the relationship between the battery voltage E and the voltage across the capacitor *e* could be expressed in the following manner:

$$e = E\,(1 - \epsilon^{-t/RC})$$

where *e*, E, R, and C have the values discussed above, $\epsilon = 2.716$ (the base of Naperian or natural logarithms), and t represents the time which has elapsed since the closing of the switch. With t expressed in seconds, R and C

Figure 24
TYPICAL INDUCTANCES
The large inductance is a 1000-watt transmitting coil. To the right and left of this coil are small r-f chokes. Several varieties of low power capability coils are shown below, along with various types of r-f chokes intended for high-frequency operation.



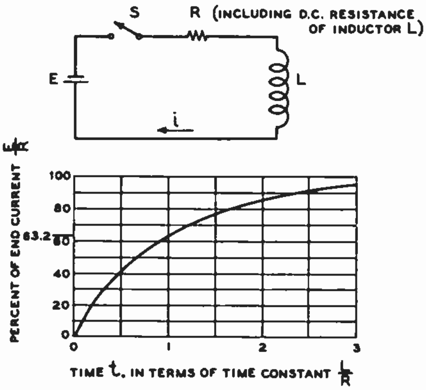


Figure 25
TIME CONSTANT OF AN R-L CIRCUIT
Note that the time constant for the increase in current through an R-L circuit is identical to the rate of increase in voltage across the capacitor in an R-C circuit.

may be expressed in farads and ohms, or R and C may be expressed in microfarads and megohms. The product RC is called the *time constant* of the circuit, and is expressed in seconds. As an example, if R is one megohm and C is one microfarad, the time constant RC will be equal to the product of the two, or one second.

When the elapsed time t is equal to the time constant of the RC network under consideration, the exponent of ϵ becomes –1. Now ϵ^{-1} is equal to $1/\epsilon$, or 1/2.716, which is 0.368. The quantity (1 - 0.368) then is equal to 0.632. Expressed as percentage, the above means that the voltage across the capacitor will have increased to 63.2 per cent of the battery voltage in an interval equal to the time constant or RC product of the circuit. Then, during the next period equal to the time constant of the RC combination, the voltage across the capacitor will have risen to 63.2 per cent of the remaining difference in voltage, or 86.5 per cent of the applied voltage E.

RL Circuit In the case of a series combination of a resistor and an inductor, as shown in figure 25, the current through the combination follows a very similar law to that given above for the voltage appearing across the capacitor in an RC series circuit. The equation for the current through the combination is:

$$i = \frac{E}{R}\left(1 - \epsilon^{-tR/L}\right)$$

where i represents the current at any instant through the series circuit, E represents the applied voltage, and R represents the total resistance of the resistor and the d-c resistance of the inductor in series. Thus the time constant of the RL circuit is L/R, with R expressed in ohms and L expressed in henrys.

Voltage Decay When the switch in figure 23 is moved to position 3 after the capacitor has been charged, the capacitor voltage will drop in the manner shown in figure 23-C. In this case the voltage across the capacitor will decrease to 36.8 per cent of the initial voltage (will make 63.2 per cent of the total drop) in a period of time equal to the time constant of the RC circuit.

CHAPTER THREE

Alternating Current Circuits

The previous chapter has been devoted to a discussion of circuits and circuit elements upon which is impressed a current consisting of a flow of electrons in one direction. This type of unidirectional current flow is called direct current, abbreviated *d.c.* Equally as important in radio and communications work, and power practice, is a type of current flow whose direction of electron flow reverses periodically. The reversal of flow may take place at a low rate, in the case of power systems, or it may take place millions of times per second in the case of communications frequencies. This type of current flow is called *alternating current,* abbreviated *a.c.*

3-1 Alternating Current

Frequency of an Alternating Current An alternating current is one whose amplitude of current flow periodically rises from zero to a maximum in one direction, decreases to zero, changes its direction, rises to maximum in the opposite direction, and decreases to zero again. This complete process, starting from zero, passing through two maximums in opposite directions, and returning to zero again, is called a *cycle.* The number of times per second that a current passes through the complete cycle is called the *frequency* of the current. One and one quarter cycles of an alternating current wave are illustrated diagrammatically in figure 1.

Frequency Spectrum At present the usable frequency range for alternating electrical currents extends over the enormous frequency range from about 15 cycles per second to perhaps 30,000,000,000 cycles per second. It is obviously cumbersome to use a frequency designation in c.p.s. for enormously high frequencies, so three common units which are multiples of one cycle per second have been established.

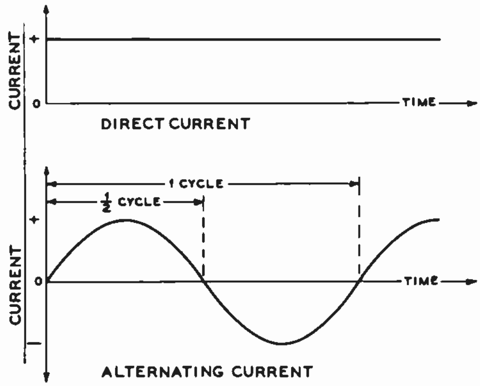


Figure 1
ALTERNATING CURRENT AND DIRECT CURRENT
Graphical comparison between unidirectional (direct) current and alternating current as plotted against time.

These units are:

(1) the kilocycle (abbr., kc.), 1000 c.p.s.
(2) the Megacycle (abbr., Mc.), 1,000,000 c.p.s. or 1000 kc.
(3) the kilo-Megacycle (abbr., kMc.), 1,000,000,000 c.p.s. or 1000 Mc.

With easily handled units such as these we can classify the entire usable frequency range into frequency bands.

The frequencies falling between about 15 and 20,000 c.p.s. are called *audio* frequencies, abbreviated *a.f.*, since these frequencies are audible to the human ear when converted from electrical to acoustical signals by a loudspeaker or headphone. Frequencies in the vicinity of 60 c.p.s. also are called *power* frequencies, since they are commonly used to distribute electrical power to the consumer.

The frequencies falling between 10,000 c.p.s. (10 kc.) and 30,000,000,000 c.p.s. (30 kMc.) are commonly called *radio* frequencies, abbreviated *r.f.*, since they are commonly used in radio communication and allied arts. The radio-frequency spectrum is often arbitrarily classified into seven frequency bands, each one of which is ten times as high in frequency as the one just below it in the spectrum (except for the v-l-f band at the bottom end of the spectrum). The present spectrum, with classifications, is given below.

Frequency	*Classification*	*Abbrev.*
10 to 30 kc.	Very-low frequencies	v.l.f
30 to 300 kc.	Low frequencies	l.f.
300 to 3000 kc.	Medium frequencies	m.f.
3 to 30 Mc.	High frequencies	h.f.
30 to 300 Mc.	Very-high frequencies	v.h.f.
300 to 3000 Mc.	Ultra-high frequencies	u.h.f.
3 to 30 kMc.	Super-high frequencies	s.h.f.
30 to 300 kMc.	Extremely-high frequencies	e.h.f.

Generation of Alternating Current Faraday discovered that if a conductor which forms part of a closed circuit is moved through a magnetic field so as to cut across the lines of force, a current will flow in the conductor. He also discovered that, if a conductor in a second closed circuit is brought near the first conductor and the current in the first one is varied, a current will flow in the second conductor. This effect is known as *induction*, and the currents so generated are *induced currents*. In the latter case it is the lines of force which are moving and cutting the second conductor, due to the varying current strength in the first conductor.

A current is induced in a conductor if there is a relative motion between the conductor and a magnetic field, its direction of flow depending upon the direction of the relative motion between the conductor and the field, and its strength depends upon the intensity of the field, the rate of cutting lines of force, and the number of turns in the conductor.

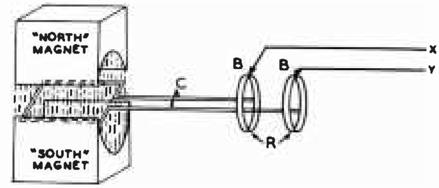


Figure 2
THE ALTERNATOR
Semi-schematic representation of the simplest form of the alternator.

Alternators A machine that generates an alternating current is called an *alternator* or *a-c* generator. Such a machine in its basic form is shown in figure 2. It consists of two permanent magnets, M, the opposite poles of which face each other and are machined so that they have a common radius. Between these two poles, north (N) and south (S), a substantially constant magnetic field exists. If a conductor in the form of C is suspended so that it can be freely rotated between the two poles, and if the opposite ends of conductor C are brought to collector rings, there will be a flow of alternating current when conductor C is rotated. This current will flow out through the collector rings R and brushes B to the external circuit, X-Y.

The field intensity between the two pole pieces is substantially constant over the entire area of the pole face However, when the conductor is moving parallel to the lines of force at the top or bottom of the pole faces, no lines are being cut. As the conductor moves on across the pole face it cuts more and more lines of force for each unit distance of travel, until it is cutting the maximum number of lines when opposite the center of the pole. Therefore, zero current is induced in the conductor at the instant it is midway between the two poles, and maximum current is induced when it is opposite the center of the pole face. After the conductor has rotated through 180° it can be seen that its position with respect to the pole pieces will be exactly opposite to that when it started. Hence, the second 180° of rotation will produce an alternation of current in the opposite direction to that of the first alternation.

The current does *not* increase directly as the angle of rotation, but rather as the *sine* of the angle; hence, such a current has the mathematical form of a *sine wave*. Although

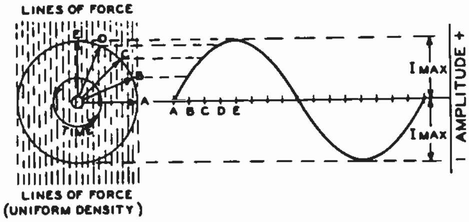


Figure 3
OUTPUT OF THE ALTERNATOR
Graph showing sine-wave output current of the alternator of figure 2.

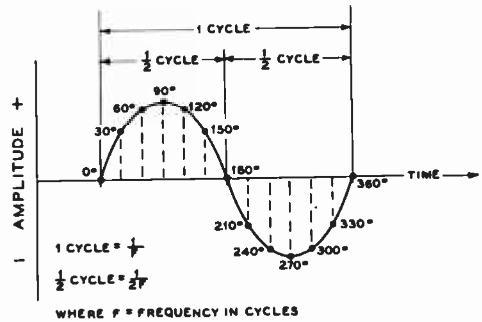


Figure 4
THE SINE WAVE
Illustrating one cycle of a sine wave. One complete cycle of alternation is broken up into 360 degrees. Then one-half cycle is 180 degrees, one-quarter cycle is 90 degrees, and so on down to the smallest division of the wave. A cosine wave has a shape identical to a sine wave but is shifted 90 degrees in phase — in other words the wave begins at full amplitude, the 90-degree point comes at zero amplitude, the 180-degree point comes at full amplitude in the opposite direction of current flow, etc.

most electrical machinery does not produce a strictly pure sine curve, the departures are usually so slight that the assumption can be regarded as fact for most practical purposes. All that has been said in the foregoing paragraphs concerning alternating current also is applicable to alternating voltage.

The rotating arrow to the left in figure 3 represents a conductor rotating in a constant magnetic field of uniform density. The arrow also can be taken as a *vector* representing the strength of the magnetic field. This means that the length of the arrow is determined by the strength of the field (number of lines of force), which is constant. Now if the arrow is rotating at a constant rate (that is, with constant *angular velocity*), then the voltage developed across the conductor will be proportional to the rate at which it is cutting lines of force, which rate is proportional to the vertical distance between the tip of the arrow and the horizontal base line.

If EO is taken as unity or a voltage of 1, then the voltage (vertical distance from tip of arrow to the horizontal base line) at point C for instance may be determined simply by referring to a table of sines and looking up the sine of the angle which the arrow makes with the horizontal.

When the arrow has traveled from A to point E, it has traveled 90 degrees or one quarter cycle. The other three quadrants are not shown because their complementary or mirror relationship to the first quadrant is obvious.

It is important to note that time units are represented by *degrees* or quadrants. The fact that AB, BC, CD, and DE are equal chords (forming equal quadrants) simply means that the arrow (conductor or vector) is traveling at a constant speed, because these points on the radius represent the passage of equal units of time.

The whole picture can be represented in another way, and its derivation from the foregoing is shown in figure 3. The time base is represented by a straight line rather than by angular rotation. Points A, B, C, etc., represent the same units of time as before. When the voltage corresponding to each point is projected to the corresponding time unit, the familiar *sine curve* is the result.

The frequency of the generated voltage is proportional to the speed of rotation of the alternator, and to the number of magnetic poles in the field. Alternators may be built to produce radio frequencies up to 30 kilocycles, and some such machines are still used for low frequency communication purposes. By means of multiple windings, three-phase output may be obtained from large industrial alternators.

Radian Notation From figure 1 we see that the value of an a-c wave varies continuously. It is often of importance to know the amplitude of the wave in terms of the total amplitude at any instant or at any time within the cycle. To be able to establish the instant in question we must be able to divide the cycle into parts. We could divide the cycle into eighths, hundredths, or any other ratio that suited our fancy. However, it is much more convenient mathematically to divide the cycle either into *electrical degrees* (360° represent one cycle) or into *radians*. A radian is an arc of a circle equal to the radius of the circle; hence there are 2π radians per cycle — or per circle (since there are π diameters per circumference, there are 2π radii).

Both radian notation and electrical degree notation are used in discussions of alternating current circuits. However, trigonometric tables are much more readily available in terms of degrees than radians, so the following simple conversions are useful.

$$2\pi \text{ radians} = 1 \text{ cycle} = 360°$$

$$\pi \text{ radians} = \tfrac{1}{2} \text{ cycle} = 180°$$

$$\frac{\pi}{2} \text{ radians} = \tfrac{1}{4} \text{ cycle} = 90°$$

$$\frac{\pi}{3} \text{ radians} = \tfrac{1}{6} \text{ cycle} = 60°$$

$$\frac{\pi}{4} \text{ radians} = \tfrac{1}{8} \text{ cycle} = 45°$$

$$1 \text{ radian} = \frac{1}{2\pi} \text{ cycle} = 57.3°$$

When the conductor in the simple alternator of figure 2 has made one complete revolution it has generated one cycle and has rotated through 2π radians. The expression $2\pi f$ then represents the number of radians in one cycle multiplied by the number of cycles per second (the frequency) of the alternating voltage or current. The expression then represents the number of radians per second through which the conductor has rotated. Hence $2\pi f$ represents the angular velocity of the rotating conductor, or of the rotating vector which represents any alternating current or voltage, expressed in radians per second.

In technical literature the expression $2\pi f$ is often replaced by ω, the lower-case Greek letter *omega*. Velocity multiplied by time gives the distance travelled. so $2\pi ft$ (or ωt) represents the angular distance through which the rotating conductor or the rotating vector has travelled since the reference time $t = 0$. In the case of a sine wave the reference time $t = 0$ represents that instant when the voltage or the current, whichever is under discussion, also is equal to zero.

Instantaneous Value of Voltage or Current The instantaneous voltage or current is proportional to the sine of the angle through which the rotating vector has travelled since reference time $t = 0$. Hence, when the peak value of the a-c wave amplitude (either voltage or current amplitude) is known, and the angle through which the rotating vector has travelled is established, the amplitude of the wave at this instant can be determined through use of the following expression:

$$e = E_{max} \sin 2\pi ft,$$

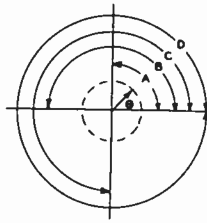


Figure 5
ILLUSTRATING RADIAN NOTATION

The radian is a unit of phase angle, equal to 57.324 degrees. It is commonly used in mathematical relationships involving phase angles since such relationships are simplified when radian notation is used.

where e = the instantaneous voltage

E = maximum crest value of voltage,

f = frequency in cycles per second, and

t = period of time which has elapsed since $t = 0$ expressed as a fraction of one second.

The instantaneous current can be found from the same expression by substituting i for e and I_{max} for E_{max}.

It is often easier to visualize the process of determining the instantaneous amplitude by ignoring the frequency and considering only one cycle of the a-c wave. In this case, for a sine wave, the expression becomes:

$$e = E_{max} \sin \theta$$

where θ represents the angle through which the vector has rotated since time (and amplitude) were zero. As examples:

when $\theta = 30°$
$\sin \theta = 0.5$
so $e = 0.5\ E_{max}$

. . . .

when $\theta = 60°$
$\sin \theta = 0.866$
so $e = 0.866\ E_{max}$

. . . .

when $\theta = 90°$
$\sin \theta = 1.0$
so $e = E_{max}$

. . . .

when $\theta = 1$ radian
$\sin \theta = 0.8415$
so $e = 0.8415\ E_{max}$

Effective Value of an Alternating Current The instantaneous value of an alternating current or voltage varies continuously throughout the cycle. So some value of an a-c wave must be chosen to establish a relationship between the effectiveness of an a-c and a d-c voltage or current. The heating value of an alternating current has been chosen to establish the reference between the *effective* values of a.c. and d.c. Thus an alternating current will have an effective value of 1 ampere when it produces the same heat in a resistor as does 1 ampere of direct current.

The effective value is derived by taking the instantaneous values of current over a cycle of alternating current, squaring these values, taking an average of the squares, and then taking the square root of the average. By this procedure, the effective value becomes known as the *root mean square* or r.m.s. value. This is the value that is read on a-c voltmeters and a-c ammeters. The r.m.s. value is 70.7 (for sine waves only) per cent of the peak or maximum instantaneous value and is expressed as follows:

$$E_{eff.} \text{ or } E_{r.m.s.} = 0.707 \times E_{max} \text{ or}$$

$$I_{eff.} \text{ or } I_{r.m.s.} = 0.707 \times I_{max}.$$

The following relations are extremely useful in radio and power work:

$$E_{r.m.s.} = 0.707 \times E_{max}, \text{ and}$$

$$E_{max} = 1.414 \times E_{r.m.s.}$$

Rectified Alternating Current or Pulsating Direct Current If an alternating current is passed through a rectifier, it emerges in the form of a current of *varying amplitude* which flows in *one* direction only. Such a current is known as *rectified a.c.* or *pulsating d.c.* A typical wave form of a pulsating direct current as would be obtained from the output of a full-wave rectifier is shown in figure 6.

Measuring instruments designed for d-c operation will not read the peak for instantaneous maximum value of the pulsating d-c output from the rectifier; they will read only the *average value*. This can be explained by assuming that it could be possible to cut off some of the peaks of the waves, using the cut-off portions to fill in the spaces that are open, thereby obtaining an *average* d-c value. A milliammeter and voltmeter connected to the adjoining circuit, or across the output of the rectifier, will read this average value. It is related to *peak* value by the following expression:

$$E_{avg} = 0.636 \times E_{max}$$

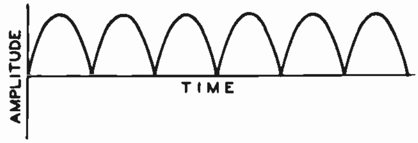


Figure 6
FULL-WAVE RECTIFIED SINE WAVE

Waveform obtained at the output of a fullwave rectifier being fed with a sine wave and having 100 per cent rectification efficiency. Each pulse has the same shape as one-half cycle of a sine wave. This type of current is known as pulsating direct current.

It is thus seen that the average value is 63.6 per cent of the peak value.

Relationship Between Peak, R.M.S. or Effective, and Average Values To summarize the three most significant values of an a-c sine wave: the peak value is equal to 1.41 times the r.m.s. or effective, and the r.m.s. value is equal to 0.707 times the peak value; the average value of a full-wave rectified a-c wave is 0.636 times the peak value, and the average value of a rectified wave is equal to 0.9 times the r.m.s. value.

R.M.S. = 0.707 × Peak
Average = 0.636 × Peak

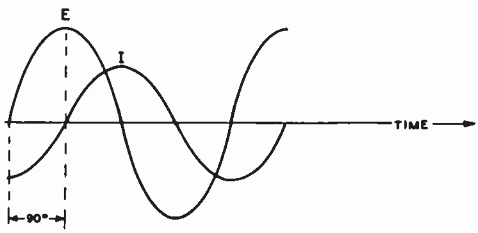
. . . .

Average = 0.9 × R.M.S.
R.M.S. = 1.11 × Average

. . . .

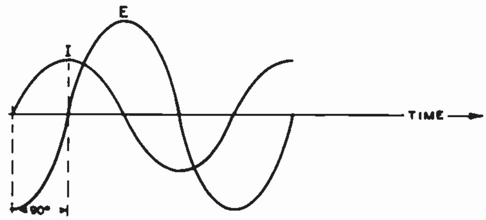
Peak = 1.414 × R.M.S.
Peak = 1.57 × Average

Applying Ohm's Law to Alternating Current Ohm's law applies equally to direct or alternating current, *provided* the circuits under consideration are purely resistive, that is, circuits which have neither inductance (coils) nor capacitance (capacitors). Problems which involve tube filaments, drop resistors, electric lamps, heaters or similar resistive devices can be solved from Ohm's law, regardless of whether the current is direct or alternating. When a capacitor or coil is made a part of the circuit, a property common to either, called *reactance*, must be taken into consideration. Ohm's law still applies to a-c circuits containing reactance, but additional considerations are involved; these will be discussed in a later paragraph.



CURRENT LAGGING VOLTAGE BY 90°
(CIRCUIT CONTAINING PURE INDUCTANCE ONLY)

Figure 7
LAGGING PHASE ANGLE
Showing the manner in which the current lags the voltage in an a-c circuit containing pure inductance only. The lag is equal to one-quarter cycle or 90 degrees.



CURRENT LEADING VOLTAGE BY 90°
(CIRCUIT CONTAINING PURE CAPACITANCE ONLY)

Figure 8
LEADING PHASE ANGLE
Showing the manner in which the current leads the voltage in an a-c circuit containing pure capacitance only. The lead is equal to one-quarter cycle or 90 degrees.

Inductive Reactance As was stated in Chapter Two, when a changing current flows through an inductor a back- or counter-electromotive force is developed; opposing any change in the initial current. This property of an inductor causes it to offer opposition or *impedance* to a change in current. The measure of impedance offered by an inductor to an alternating current of a given frequency is known as its *inductive reactance.* This is expressed as X_L.

$$X_L = 2\pi f L,$$

where X_L = inductive reactance expressed in ohms.

$\pi = 3.1416$ ($2\pi = 6.283$),
f = frequency in cycles,
L = inductance in henrys.

Inductive Reactance at Radio Frequencies It is very often necessary to compute inductive reactance at radio frequencies. The same formula may be used, but to make it less cumbersome the inductance is expressed in *millihenrys* and the frequency in *kilocycles.* For higher frequencies and smaller values of inductance, frequency is expressed in *megacycles* and inductance in *microhenrys.* The basic equation need not be changed, since the multiplying factors for inductance and frequency appear in numerator and denominator, and hence are cancelled out. However, it is not possible in the same equation to express L in millihenrys and f in cycles without conversion factors.

Capacitive Reactance It has been explained that inductive reactance is the measure of the ability of an inductor to offer impedance to the flow of an alternating current. Capacitors have a similar property although in this case the opposition is to any change in the voltage across the capacitor. This property is called *capacitive reactance* and is expressed as follows:

$$X_C = \frac{1}{2\pi f C},$$

where X_C = capacitive reactance in ohms,
$\pi = 3.1416$
f = frequency in cycles,
C = capacitance in farads.

Capacitive Reactance at Radio Frequencies Here again, as in the case of inductive reactance, the units of capacitance and frequency can be converted into smaller units for practical problems encountered in radio work. The equation may be written:

$$X_C = \frac{1{,}000{,}000}{2\pi f C},$$

where f = frequency in megacycles,
C = capacitance in micro-microfarads.

In the audio range it is often convenient to express frequency (f) in *cycles* and capacitance (C) in *microfarads,* in which event the same formula applies.

Phase When an alternating current flows through a purely resistive circuit, it will be found that the current will go through maximum and minimum in perfect step with the voltage. In this case the current is said to be in step or *in phase* with the voltage. For this reason, Ohm's law will apply equally well for *a.*c. or *d.*c. where pure resistances are concerned, provided that the same values of the wave (either peak or r.m.s.) for both voltage and current are used in the calculations.

However, in calculations involving alternating currents the voltage and current are not necessarily in phase. The current through the circuit may lag behind the voltage, in which case the current is said to have *lagging* phase. Lagging phase is caused by inductive reactance. If the current reaches its maximum value ahead of the voltage (figure 8) the current is said to have a leading phase. A leading phase angle is caused by capacitive reactance.

In an electrical circuit containing reactance only, the current will either lead or lag the voltage by 90°. If the circuit contains inductive reactance only, the current will lag the voltage by 90°. If only capacitive reactance is in the circuit, the current will lead the voltage by 90°.

Reactances in Combination Inductive and capacitive reactance have exactly opposite effects on the phase relation between current and voltage in a circuit. Hence when they are used in combination their effects tend to neutralize. The combined effect of a capacitive and an inductive reactance is often called the ***net reactance*** of a circuit. The net reactance (X) is found by subtracting the capacitive reactance from the inductive reactance, $X = X_L - X_C$.

The result of such a combination of pure reactances may be either positive, in which case the positive reactance is greater so that the net reactance is inductive, or it may be negative in which case the capacitive reactance is greater so that the net reactance is capacitive. The net reactance may also be zero in which case the circuit is said to be *resonant*. The condition of resonance will be discussed in a later section. Note that inductive reactance is always taken as being positive while capacitive reactance is always taken as being negative.

Impedance; Circuits Containing Reactance and Resistance Pure reactances introduce a phase angle of 90° between voltage and current; pure resistance introduces no phase shift between voltage and current. Hence we cannot add a reactance and a resistance directly. When a reactance and a resistance are used in combination the resulting phase angle of current flow with respect to the impressed voltage lies somewhere between plus or minus 90° and 0° depending upon the relative magnitudes of the reactance and the resistance.

The term *impedance* is a general term which can be applied to any electrical entity which impedes the flow of current. Hence the term may be used to designate a resistance, a pure reactance, or a complex combination of both reactance and resistance. The designation for impedance is Z. An impedance must be defined in such a manner that both its magnitude and its phase angle are established. The designation may be accomplished in either of two ways — one of which is convertible into the other by simple mathematical operations.

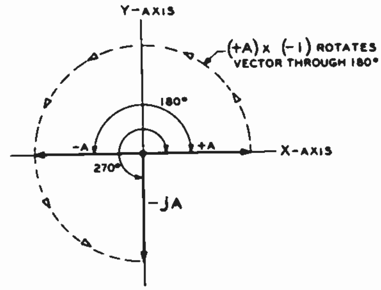


Figure 9

Operation on the vector (+A) by the quantity (−1) causes vector to rotate through 180 degrees.

The "J" Operator The first method of designating an impedance is actually to specify both the resistive and the reactive component in the form R + jX. In this form R represents the resistive component in ohms and X represents the reactive component. The "j" merely means that the X component is reactive and thus cannot be added directly to the R component. Plus jX means that the reactance is positive or inductive, while if minus jX were given it would mean that the reactive component was negative or capacitive.

In figure 9 we have a vector (+A) lying along the positive X-axis of the usual X-Y coordinate system. If this vector is multiplied by the quantity (−1), it becomes (−A) and its position now lies along the X-axis in the negative direction. The *operator* (−1) has caused the vector to rotate through an angle of 180 degrees. Since (−1) is equal to $(\sqrt{-1} \times \sqrt{-1})$, the same result may be obtained by operating on the vector with the operator $(\sqrt{-1} \times \sqrt{-1})$. However if the vector is operated on but once by the operator $(\sqrt{-1})$, it is caused to rotate only 90 degrees (figure 10). Thus the operator $(\sqrt{-1})$ rotates a vector by 90 degrees. For convenience, this operator is called the *j operator*. In like fashion, the operator (−j) rotates the vector of figure 9 through an angle of 270 degrees, so that the resulting vector (−jA) falls on the (−Y) axis of the coordinate system.

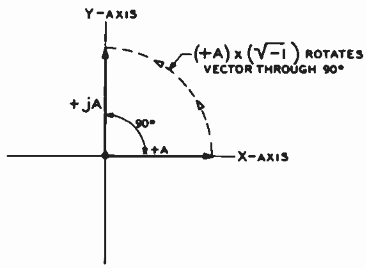


Figure 10

Operation on the vector (+A) by the quantity (j) causes vector to rotate through 90 degrees.

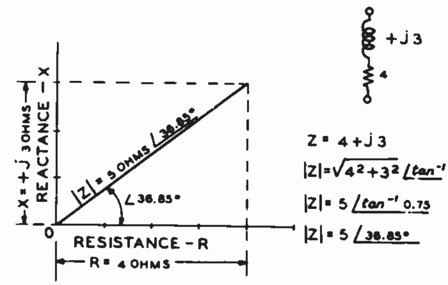


Figure 11

THE IMPEDANCE TRIANGLE

Showing the graphical construction of a triangle for obtaining the net (scalar) impedance resulting from the connection of a resistance and a reactance in series. Shown also alongside is the alternative mathematical procedure for obtaining the values associated with the triangle.

Polar Notation The second method of representing an impedance is to specify its absolute magnitude and the phase angle of current with respect to voltage, in the form $Z \angle \theta$. Figure 11 shows graphically the relationship between the two common ways of representing an impedance.

The construction of figure 11 is called an impedance diagram. Through the use of such a diagram we can add graphically a resistance and a reactance to obtain a value for the resulting impedance in the scalar form. With zero at the origin, resistances are plotted to the right, positive values of reactance (inductive) in the upward direction, and negative values of reactance (capacitive) in the downward direction.

Note that the resistance and reactance are drawn as the two sides of a right triangle, with the hypotenuse representing the resulting impedance. Hence it is possible to determine mathematically the value of a resultant impedance through the familiar right-triangle relationship — the square of the hypotenuse is equal to the sum of the squares of the other two sides:

$$Z^2 = R^2 + X^2$$

$$\text{or } |Z| = \sqrt{R^2 + X^2}$$

Note also that the angle θ included between R and Z can be determined from any of the following trigonometric relationships:

$$\sin \theta = \frac{X}{|Z|}$$

$$\cos \theta = \frac{R}{|Z|}$$

$$\tan \theta = \frac{X}{R}$$

One common problem is that of determining the *scalar magnitude* of the impedance, $|Z|$, and the phase angle θ, when resistance and reactance are known; hence, of converting from the $Z = R + jX$ to the $|Z| \angle \theta$ form. In this case we use two of the expressions just given:

$$|Z| = \sqrt{R^2 + X^2}$$

$$\tan \theta = \frac{X}{R}, \; (\text{or } \theta = \tan^{-1} \frac{X}{R})$$

The inverse problem, that of converting from the $|Z| \angle \theta$ to the $R + jX$ form is done with the following relationships, both of which are obtainable by simple division from the trigonometric expressions just given for determining the angle θ:

$$R = |Z| \cos \theta$$

$$jX = |Z| \, j \sin \theta$$

By simple addition these two expressions may be combined to give the relationship between the two most common methods of indicating an impedance:

$$R + jX = |Z| \, (\cos \theta + j \sin \theta)$$

In the case of impedance, resistance, or reactance, the unit of measurement is the ohm; hence, the ohm may be thought of as a unit of *opposition to current flow,* without reference to the relative phase angle between the applied voltage and the current which flows.

Further, since both capacitive and inductive reactance are functions of frequency, impedance will vary with frequency. Figure 12 shows the manner in which $|Z|$ will vary with frequency in an RL series circuit and in an RC series circuit.

Series RLC Circuits In a series circuit containing R, L, and C, the impedance is determined as discussed before except that the reactive component in the expressions becomes: (The net reactance — the difference between X_L and X_C.) Hence (X_L − X_C) may be substituted for X in the equations. Thus:

$$|Z| = \sqrt{R^2 + (X_L - X_C)^2}$$

$$\theta = \tan^{-1}\frac{(X_L - X_C)}{R}$$

A series RLC circuit thus may present an impedance which is capacitively reactive if the net reactance is capacitive, inductively reactive if the net reactance is inductive, or resistive if the capacitive and inductive reactances are equal.

Addition of Complex Quantities The addition of complex quantities (for example, impedances in series) is quite simple if the quantities are in the rectangular form. If they are in the polar form they only can be added graphically, unless they are converted to the rectangular form by the relationships previously given. As an example of the addition of complex quantities in the rectangular form, the equation for the addition of impedances is:

$$(R_1 + jX_1) + (R_2 + jX_2) = (R_1 + R_2) + j(X_1 + X_2)$$

For example if we wish to add the impedances (10 + j50) and (20 − j30) we obtain:

$$\begin{aligned}(10 + j50) + (20 - j30) &= (10 + 20) + j(50 + (-30))\\ &= 30 + j(50\text{-}30)\\ &= 30 + j20\end{aligned}$$

Multiplication and Division of Complex Quantities It is often necessary in solving certain types of circuits to multiply or divide two complex quantities. It is a much simplier mathematical operation to multiply or divide complex quantities if they are expressed in the polar form. Hence if they are given in the rectangular form they should be converted to the polar form before multiplication or division is begun. Then the multiplication is accomplished by multiplying the $|Z|$ terms together and *adding* algebraically the $\angle\theta$ terms, as:

$$(|Z_1| \angle\theta_1)(|Z_2| \angle\theta_2) = |Z_1|\,|Z_2|\,(\angle\theta_1 + \angle\theta_2)$$

For example, suppose that the two impedances $|20| \angle 43°$ and $|32| \angle -23°$ are to be multiplied. Then:

$$\begin{aligned}(|20| \angle 43°)(|32| \angle -23°) &= |20 \cdot 32|\,(\angle 43° + \angle -23°)\\ &= 640 \angle 20°\end{aligned}$$

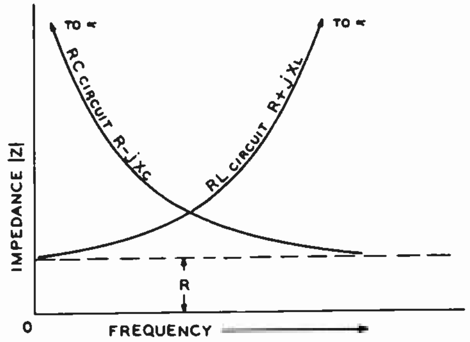


Figure 12
IMPEDANCE AGAINST FREQUENCY FOR R-L AND R-C CIRCUITS

The impedance of an R-C circuit approaches infinity as the frequency approaches zero (d.c.), while the impedance of a series R-L circuit approaches infinity as the frequency approaches infinity. The impedance of an R-C circuit approaches the impedance of the series resistor as the frequency approaches infinity, while the impedance of a series R-L circuit approaches the impedance of the resistor as the frequency approaches zero.

Division is accomplished by dividing the denominator into the numerator, and *subtracting* the angle of the denominator from that of the numerator, as:

$$\frac{|Z_1| \angle\theta_1}{|Z_2| \angle\theta_2} = \frac{|Z_1|}{|Z_2|}(\angle\theta_1 - \angle\theta_2)$$

For example, suppose that an impedance of $|50| \angle 67°$ is to be divided by an impedance of $|10| \angle 45°$. Then:

$$\frac{|50| \angle 67°}{|10| \angle 45°} = \frac{|50|}{|10|}(\angle 67° - \angle 45°) = |5|(\angle 22°)$$

Ohm's Law for Complex Quantities The simple form of Ohm's Law used for d-c circuits may be stated in a more general form for application to a-c circuits involving either complex quantities or simple resistive elements. The form is:

$$I = \frac{E}{Z}$$

in which, in the general case, I, E, and Z are complex (vector) quantities. In the simple case where the impedance is a pure resistance with an a-c voltage applied, the equation simplifies to the familiar I = E/R. In any case the applied voltage may be expressed either as peak, r.m.s., or average; the resulting

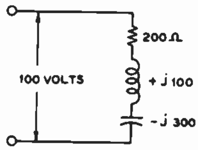


Figure 13
SERIES R-L-C CIRCUIT

current always will be in the same type of units as used to define the voltage.

In the more general case vector algebra must be used to solve the equation. And, since either division or multiplication is involved, the complex quantities should be expressed in the polar form. As an example, take the case of the series circuit shown in figure 13 with 100 volts applied. The impedance of the series circuit can best be obtained first in the rectangular form, as:

$$200 + j(100 - 300) = 200 - j200$$

Now, to obtain the current we must convert this impedance to the polar form.

$$|Z| = \sqrt{200^2 + (-200)^2}$$
$$= \sqrt{40{,}000 + 40{,}000}$$
$$= \sqrt{80{,}000}$$
$$= 282\ \Omega$$

$$\theta = \tan^{-1}\frac{X}{R} = \tan^{-1}\frac{-200}{200} = \tan^{-1} -1$$
$$= -45^\circ.$$

Therefore $Z = 282\ \angle{-45^\circ}$

Note that in a series circuit the resulting impedance takes the sign of the largest reactance in the series combination.

Where a slide-rule is being used to make the computations, the impedance may be found without any addition or subtraction operations by finding the angle θ first, and then using the trigonometric equation below for obtaining the impedance. Thus:

$$\theta = \tan^{-1}\frac{X}{R} = \tan^{-1}\frac{-200}{200} = \tan^{-1} -1$$
$$= -45^\circ$$

$$\text{Then } |Z| = \frac{R}{\cos\theta} \quad \cos -45^\circ = 0.707$$

$$|Z| = \frac{200}{0.707} = 282\ \Omega$$

Since the applied voltage will be the reference for the currents and voltages within the circuit, we may define it as having a zero phase angle: $E = 100\ \angle 0^\circ$. Then:

$$I = \frac{100\ \angle 0^\circ}{282\ \angle{-45^\circ}} = 0.354\ \angle 0^\circ-(-45^\circ)$$
$$= 0.354\ \angle 45^\circ \text{ amperes.}$$

This same current must flow through all three elements of the circuit, since they are in series and the current through one must already have passed through the other two. Hence the voltage drop across the resistor (whose phase angle of course is 0°) is:

$$E = I\,R$$
$$E = (0.354\ \angle 45^\circ)(200\ \angle 0^\circ)$$
$$= 70.8\ \angle 45^\circ \text{ volts}$$

The voltage drop across the inductive reactance is:

$$E = I\,X_L$$
$$E = (0.354\ \angle 45^\circ)(100\ \angle 90^\circ)$$
$$= 35.4\ \angle 135^\circ \text{ volts}$$

Similarly, the voltage drop across the capacitive reactance is:

$$E = I\,X_C$$
$$E = (0.354\ \angle 45^\circ)(300\ \angle{-90^\circ})$$
$$= 106.2\ \angle{-45^\circ}$$

Note that the voltage drop across the capacitive reactance is greater than the supply voltage. This condition often occurs in a series RLC circuit, and is explained by the fact that the drop across the capacitive reactance is cancelled to a lesser or greater extent by the drop across the inductive reactance.

It is often desirable in a problem such as the above to check the validity of the answer by adding vectorially the voltage drops across the components of the series circuit to make sure that they add up to the supply voltage — or to use the terminology of Kirchhoff's Second Law, to make sure that the voltage drops across all elements of the circuit, including the source taken as negative, is equal to zero.

In the general case of the addition of a number of voltage vectors in series it is best to resolve the voltages into their in-phase and out-of-phase components with respect to the supply voltage. Then these components may be added directly. Hence:

$$E_R = 70.8\ \angle 45^\circ$$
$$= 70.8\,(\cos 45^\circ + j \sin 45^\circ)$$
$$= 70.8\,(0.707 + j0.707)$$
$$= 50 + j50$$

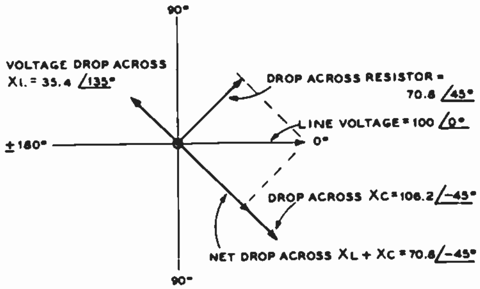


Figure 14

Graphical construction of the voltage drops associated with the series R-L-C circuit of figure 13.

$$
\begin{aligned}
E_L &= 35.4 \angle 135^\circ \\
&= 35.4\,(\cos 135^\circ + j \sin 135^\circ) \\
&= 35.4\,(-0.707 + j0.707) \\
&= -25 + j25
\end{aligned}
$$

. . . .

$$
\begin{aligned}
E_C &= 106.2 \angle 45^\circ \\
&= 106.2\,(\cos -45^\circ + j \sin -45^\circ) \\
&= 106.2\,(0.707 - j0.707) \\
&= 75 - j75
\end{aligned}
$$

. . . .

$$
\begin{aligned}
E_R + E_L + E_C &= (50 + j50) + (-25 + j25) \\
&\quad + (75 - j75) \\
&= (50 - 25 + 75) + j(50 + 25 - 75) \\
&= 100 + j0 \\
&= 100 \angle 0^\circ,
\end{aligned}
$$

which is equal to the supply voltage.

Checking by Construction on the Complex Plane It is frequently desirable to check computations involving complex quantities by constructing vectors representing the quantities on the complex plane. Figure 14 shows such a construction for the quantities of the problem just completed. Note that the answer to the problem may be checked by constructing a parallelogram with the voltage drop across the resistor as one side and the net voltage drop across the capacitor plus the inductor (these may be added algrebraically as they are 180° out of phase) as the adjacent side. The vector sum of these two voltages, which is represented by the diagonal of the parallelogram, is equal to the supply voltage of 100 volts at zero phase angle.

Resistance and Reactance in Parallel In a series circuit, such as just discussed, the current through all the elements which go to make up the series circuit is the same. But the voltage drops across each of the components are, in general, different from one another. Conversely, in a parallel RLC or RX circuit the voltage is, obviously, the same across each of the elements. But the currents through each of the elements are usually different.

There are many ways of solving a problem involving paralleled resistance and reactance; several of these ways will be described. In general, it may be said that the impedance of a number of elements in parallel is solved using the same relations as are used for solving resistors in parallel, except that complex quantities are employed. The basic relation is:

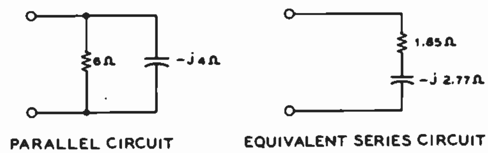


Figure 15

THE EQUIVALENT SERIES CIRCUIT

Showing a parallel R-C circuit and the equivalent series R-C circuit which represents the same net impedance as the parallel circuit.

$$\frac{1}{Z_{tot}} = \frac{1}{Z_1} + \frac{1}{Z_2} + \frac{1}{Z_3} + \ldots\ldots,$$

or when only two impedances are involved:

$$Z_{tot} = \frac{Z_1 Z_2}{Z_1 + Z_2}$$

As an example, using the two-impedance relation, take the simple case, illustrated in figure 15, of a resistance of 6 ohms in parallel with a capacitive reactance of 4 ohms. To simplify the first step in the computation it is best to put the impedances in the polar form for the numerator, since multiplication is involved, and in the rectangular form for the addition in the denominator.

$$
\begin{aligned}
Z_{tot} &= \frac{(6 \angle 0^\circ)\,(4 \angle -90^\circ)}{6 - j4} \\
&= \frac{24 \angle -90^\circ}{6 - j4}
\end{aligned}
$$

Then the denominator is changed to the polar form for the division operation:

$$\theta = \tan^{-1}\frac{-4}{6} = \tan^{-1} - 0.667 = -33.7^\circ$$

$$|Z| = \frac{6}{\cos - 33.7^\circ} = \frac{6}{0.832} = 7.21 \text{ ohms}$$

$$6 - j4 = 7.21 \angle -33.7^\circ$$

Then:

$$Z_{tot} = \frac{24 \angle -90^\circ}{7.21 \angle -33.7^\circ} = 3.33 \angle -56.3^\circ$$

$$= 3.33\,(\cos - 56.3^\circ + j \sin - 56.3^\circ)$$

$$= 3.33\,[0.5548 + j\,(-0.832)]$$

$$= 1.85 - j\,2.77$$

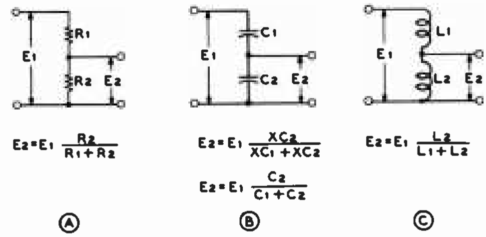


Figure 16
SIMPLE A-C VOLTAGE DIVIDERS

Equivalent Series Circuit Through the series of operations in the previous paragraph we have converted a circuit composed of two impedances in parallel into an *equivalent series circuit* composed of impedances in series. An equivalent series circuit is one which, as far as the terminals are concerned, acts identically to the original parallel circuit; the current through the circuit and the power dissipation of the resistive elements are the same for a given voltage at the specified frequency.

We can check the equivalent series circuit of figure 15 with respect to the original circuit by assuming that one volt a.c. (at the frequency where the capacitive reactance in the parallel circuit is 4 ohms) is applied to the terminals of both.

In the parallel circuit the current through the resistor will be 1/6 ampere (0.166a.) while the current through the capacitor will be j 1/4 ampere (+ j 0.25 a.). The total current will be the sum of these two currents, or 0.166 + j 0.25 a. Adding these vectorially we obtain:

$$|I| = \sqrt{0.166^2 + 0.25^2} = \sqrt{0.09} = 0.3 \text{ a.}$$

The dissipation in the resistor will be $1^2/6 =$ 0.166 watts.

In the case of the equivalent series circuit the current will be:

$$|I| = \frac{E}{|Z|} = \frac{1}{3.33} = 0.3 \text{ a.}$$

And the dissipation in the resistor will be:

$$W = I^2R = 0.3^2 \times 1.85$$
$$= 0.9 \times 1.85$$
$$= 0.166 \text{ watts}$$

So we see that the equivalent series circuit checks exactly with the original parallel circuit.

Parallel RLC Circuits In solving a more complicated circuit made up of more than two impedances in parallel we may elect to use either of two methods of solution. These methods are called the *admittance* method and the *assumed-voltage* method. However, the two methods are equivalent since both use the sum-of-reciprocals equation:

$$\frac{1}{Z_{tot}} = \frac{1}{Z_1} + \frac{1}{Z_2} + \frac{1}{Z_3} \cdots\cdots$$

In the admittance method we use the relation $Y = 1/Z$, where $Y = G + jB$; Y is called the *admittance*, defined above, G is the *conductance* or R/Z^2 and B is the *susceptance* or $-X/Z^2$. Then $Y_{tot} = 1/Z_{tot} = Y_1 + Y_2 + Y_3 \cdots\cdot$ In the assumed-voltage method we multiply both sides of the equation above by E, the assumed voltage, and add the currents, as:

$$\frac{E}{Z_{tot}} = \frac{E}{Z_1} + \frac{E}{Z_2} + \frac{E}{Z_3} \ldots = I_{Z_1} + I_{Z_2} + I_{Z_3} \ldots$$

Then the impedance of the parallel combination may be determined from the relation:

$$Z_{tot} = E/I_{Z\,tot}$$

AC Voltage Dividers Voltage dividers for use with alternating current are quite similar to d-c voltage dividers. However, since capacitors and inductors oppose the flow of a-c current as well as resistors, voltage dividers for alternating voltages may take any of the configurations shown in figure 16.

Since the impedances within each divider are of the same type, the output voltage is in phase with the input voltage. By using combinations of different types of impedances, the phase angle of the output may be shifted in relation to the input phase angle at the same time the amplitude is reduced. Several dividers of this type are shown in figure 17. Note that the ratio of output voltage to input voltage is equal to the ratio of the output impedance to the total divider impedance. This relationship is true only if negligible current is drawn by a load on the output terminals.

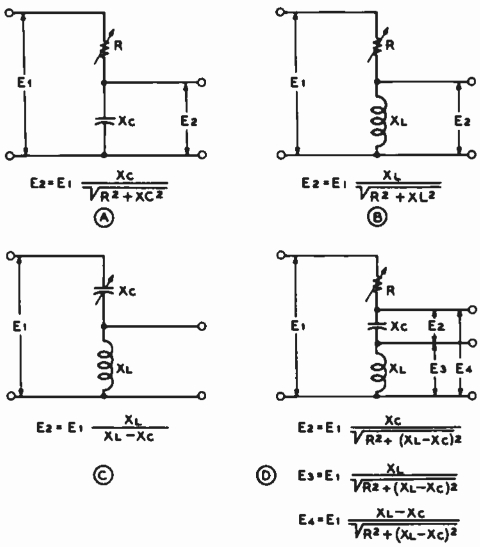


Figure 17
COMPLEX A-C VOLTAGE DIVIDERS

3-2 Resonant Circuits

A series circuit such as shown in figure 18 is said to be in *resonance* when the applied frequency is such that the capacitive reactance is exactly balanced by the inductive reactance. At this frequency the two reactances will cancel in their effects, and the impedance of the circuit will be at a minimum so that maximum current will flow. In fact, as shown in figure 19 the net impedance of a series circuit at resonance is equal to the resistance which remains in the circuit after the reactances have been cancelled.

Resonant Frequency Some resistance is always present in a circuit because it is possessed in some degree by both the inductor and the capacitor. If the frequency of the alternator E is varied from nearly zero to some high frequency, there will be one particular frequency at which the inductive reactance and capacitive reactance will be equal. This is known as the *resonant frequency,* and in a series circuit it is the frequency at which the circuit current will be a maximum. Such series resonant circuits are chiefly used when it is desirable to allow a certain frequency to pass through the circuit (low impedance to this frequency), while at the same time the circuit is made to offer considerable opposition to currents of other frequencies.

Figure 18
SERIES RESONANT CIRCUIT

If the values of inductance and capacitance both are fixed, there will be only one resonant frequency.

If both the inductance and capacitance are made variable, the circuit may then be changed or *tuned,* so that a number of combinations of inductance and capacitance can resonate at the same frequency. This can be more easily understood when one considers that inductive reactance and capacitive reactance travel in opposite directions as the frequency is changed. For example, if the frequency were to remain constant and the values of inductance and capacitance were then changed, the following combinations would have equal *reactance:*

Frequency is constant at 60 cycles.

L is expressed in henrys.
C is expressed in microfarads (.000001 farad.)

L	X_L	*C*	X_C
.265	100	26.5	100
2.65	1,000	2.65	1,000
26.5	10,000	.265	10,000
265.00	100,000	.0265	100,000
2,650.00	1,000,000	.00265	1,000,000

Frequency of Resonance From the formula for resonance, $2\pi f L = 1/2\pi f C$, the resonant frequency is determined:

$$f = \frac{1}{2\pi\sqrt{LC}},$$

where f = frequency in cycles,
L = inductance in henrys,
C = capacitance in farads.

It is more convenient to express L and C in smaller units, especially in making radio-frequency calculations; f can also be expressed in megacycles or kilocycles. A very useful group of such formulas is:

$$f^2 = \frac{25{,}330}{LC} \text{ or } L = \frac{25{,}330}{f^2C} \text{ or } C = \frac{25{,}330}{f^2L}$$

where f = frequency in megacycles,
L = inductance in microhenrys,
C = capacitance in micromicrofarads.

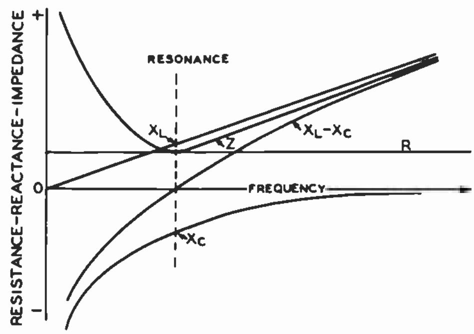


Figure 19
IMPEDANCE OF A SERIES-RESONANT CIRCUIT
Showing the variation in reactance of the separate elements and in the net impedance of a series resonant circuit (such as figure 18) with changing frequency. The vertical line is drawn at the point of resonance ($X_L - X_C = 0$) in the series circuit.

Impedance of Series Resonant Circuits The impedance across the terminals of a series resonant circuit (figure 18) is:

$$Z = \sqrt{r^2 + (X_L - X_C)^2},$$

where Z = impedance in ohms,
r = resistance in ohms,
X_C = capacitive reactance in ohms,
X_L = inductive reactance in ohms.

From this equation, it can be seen that the impedance is equal to the vector sum of the circuit resistance and the *difference* between the two reactances. Since at the resonant frequency X_L equals X_C, the difference between them (figure 19) is zero, so that at resonance the impedance is simply equal to the resistance of the circuit; therefore, because the resistance of most normal radio-frequency circuits is of a very low order, the impedance is also low.

At frequencies higher and lower than the resonant frequency, the difference between the reactances will be a definite quantity and will add with the resistance to make the impedance higher and higher as the circuit is tuned off the resonant frequency.

If X_C should be greater than X_L, then the term $(X_L - X_C)$ will give a negative number. However, when the difference is squared the product is always positive. This means that the smaller reactance is subtracted from the larger, regardless of whether it be capacitive or inductive, and the difference squared.

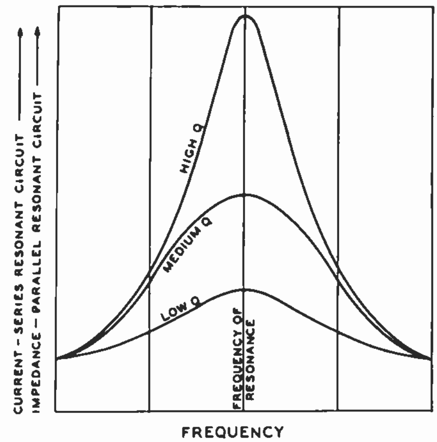


Figure 20
RESONANCE CURVE
Showing the increase in impedance at resonance for a parallel-resonant circuit, and similarly, the increase in current at resonance for a series-resonant circuit. The sharpness of resonance is determined by the Q of the circuit, as illustrated by a comparison between A, B, and C.

Current and Voltage in Series Resonant Circuits Formulas for calculating currents and voltages in a series resonant circuit are similar to those of Ohm's law.

$$I = \frac{E}{Z} \qquad E = IZ$$

The complete equations:

$$I = \frac{E}{\sqrt{r^2 + (X_L - X_C)^2}}$$

$$E = I\sqrt{r^2 + (X_L - X_C)^2}$$

Inspection of the above formulas will show the following to apply to series resonant circuits: When the impedance is low, the current will be high; conversely, when the impedance is high, the current will be low.

Since it is known that the impedance will be very low at the resonant frequency, it follows that the current will be a maximum at this point. If a graph is plotted of the current against the frequency either side of resonance, the resultant curve becomes what is known as a *resonance curve*. Such a curve is shown in figure 20, the frequency being plotted against *current* in the series resonant circuit.

Several factors will have an effect on the shape of this resonance curve, of which resistance and L-to-C ratio are the important considerations. The curves B and C in figure 20 show the effect of adding increasing values of resistance to the circuit. It will be seen that the peaks become less and less prominent as the resistance is increased; thus, it can be said that the *selectivity* of the circuit is thereby *decreased.* Selectivity in this case can be defined as the ability of a circuit to discriminate against frequencies adjacent to the resonant frequency.

Voltage Across Coil and Capacitor in Series Circuit Because the a.c. or r-f voltage across a coil and capacitor is proportional to the reactance (for a given current), the actual voltages across the coil and across the capacitor may be many times greater than the *terminal* voltage of the circuit. At resonance, the voltage across the coil (or the capacitor) is Q times the applied voltage. Since the Q (or merit factor) of a series circuit can be in the neighborhood of 100 or more, the voltage across the capacitor, for example, may be high enough to cause flashover, even though the applied voltage is of a value considerably below that at which the capacitor is rated.

Circuit Q — Sharpness of Resonance An extremely important property of a capacitor or an inductor is its factor-of-merit, more generally called its Q. It is this factor, Q, which primarily determines the sharpness of resonance of a tuned circuit. This factor can be expressed as the ratio of the reactance to the resistance, as follows:

$$Q = \frac{2\pi f L}{R},$$

where R = total resistance.

Skin Effect The actual resistance in a wire or an inductor can be far greater than the d-c value when the coil is used in a radio-frequency circuit; this is because the current does not travel through the entire cross-section of the conductor, but has a tendency to travel closer and closer to the surface of the wire as the frequency is increased. This is known as the *skin effect.*

The actual current-carrying portion of the wire is decreased, as a result of the skin effect, so that the ratio of a-c to d-c resistance of the wire, called the *resistance ratio,* is increased. The resistance ratio of wires to be used at frequencies below about 500 kc. may be materially reduced through the use of *litz* wire. Litz wire, of the type commonly used to wind the coils of 455-kc. i-f transformers, may consist of 3 to 10 strands of insulated wire, about No. 40 in size, with the individual strands connected together only at the ends of the coils.

Variation of Q with Frequency Examination of the equation for determining Q might give rise to the thought that even though the resistance of an inductor increases with frequency, the inductive reactance does likewise, so that the Q might be a constant. Actually, however, it works out in practice that the Q of an inductor will reach a relatively broad maximum at some particular frequency. Hence, coils normally are designed in such a manner that the peak in their curve of Q with frequency will occur at the normal operating frequency of the coil in the circuit for which it is designed.

The Q of a capacitor ordinarily is much higher than that of the best coil. Therefore, it usually is the merit of the coil that limits the overall Q of the circuit.

At audio frequencies the core losses in an iron-core inductor greatly reduce the Q from the value that would be obtained simply by dividing the reactance by the resistance. Obviously the core losses also represent circuit resistance, just as though the loss occurred in the wire itself.

Parallel Resonance In radio circuits, parallel resonance (more correctly termed *anti-resonance*) is more frequently encountered than series resonance; in fact, it is the basic foundation of receiver and transmitter circuit operation. A circuit is shown in figure 21.

The "Tank" Circuit In this circuit, as contrasted with a circuit for series resonance, L (inductance) and C (capacitance) are connected in *parallel,* yet the *combination* can be considered to be in series with the remainder of the circuit. This combination of L and C, in conjunction with R, the resistance which is principally included in L, is sometimes called a *tank* circuit because it effectively functions as a storage tank when incorporated in vacuum tube circuits.

Contrasted with series resonance, there are two kinds of current which must be considered in a parallel resonant circuit: (1) the line current, as read on the indicating meter M_1, (2) the circulating current which flows within the parallel L-C-R portion of the circuit. See figure 21.

At the resonant frequency, the line current (as read on the meter M_1) will drop to a very low value although the circulating current in the L-C circuit may be quite large. It is interesting to note that the parallel resonant circuit acts in a distinctly opposite manner to that of a series resonant circuit, in which the

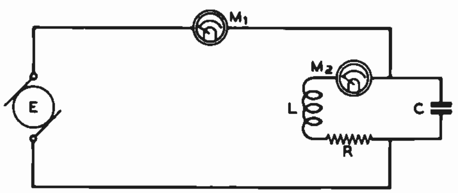


Figure 21
PARALLEL-RESONANT CIRCUIT
The inductance L and capacitance C comprise the reactive elements of the parallel-resonant (anti-resonant) tank circuit, and the resistance R indicates the sum of the r-f resistance of the coil and capacitor, plus the resistance coupled into the circuit from the external load. In most cases the tuning capacitor has much lower r-f resistance than the coil and can therefore be ignored in comparison with the coil resistance and the coupled-in resistance. The instrument M_1 indicates the "line current" which keeps the circuit in a state of oscillation—this current is the same as the fundamental component of the plate current of a Class C amplifier which might be feeding the tank circuit. The instrument M_2 indicates the "tank current" which is equal to the line current multiplied by the operating Q of the tank circuit.

current is at a maximum and the impedance is minimum at resonance. It is for this reason that in a parallel resonant circuit the principal consideration is one of impedance rather than current. It is also significant that the *impedance* curve for *parallel* circuits is very nearly identical to that of the *current* curve for *series* resonance. The impedance at resonance is expressed as:

$$Z = \frac{(2\pi f L)^2}{R},$$

where Z = impedance in ohms,
L = inductance in henrys,
f = frequency in cycles,
R = resistance in ohms.

Or, impedance can be expressed as a function of Q as:

$$Z = 2\pi f L Q,$$

showing that the impedance of a circuit is directly proportional to its effective Q at resonance.

The curves illustrated in figure 20 can be applied to parallel resonance. Reference to the curve will show that the effect of adding resistance to the circuit will result in both a broadening out and lowering of the peak of the curve. Since the voltage of the circuit is directly proportional to the impedance, and since it is this voltage that is applied to the grid of the vacuum tube in a detector or amplifier circuit, the impedance curve must have a sharp peak in order for the circuit to be *selective*. If the curve is broad-topped in shape, both the desired signal and the interfering signals at close proximity to resonance will give nearly equal voltages on the grid of the tube, and the circuit will then be *non-selective;* i.e., it will tune broadly.

Effect of L/C Ratio in Parallel Circuits In order that the highest possible voltage can be developed across a parallel resonant circuit, the impedance of this circuit must be very high. The impedance will be greater with conventional coils of limited Q when the ratio of inductance-to-capacitance is great, that is, when L is large as compared with C. When the resistance of the circuit is very low, X_L will equal X_C at maximum impedance. There are innumerable ratios of L and C that will have *equal* reactance, at a given resonant frequency, exactly as in the case in a series resonant circuit.

In practice, where a certain value of inductance is tuned by a variable capacitance over a fairly wide range in frequency, the L/C ratio will be small at the lowest frequency end and large at the high-frequency end. The circuit, therefore, will have unequal gain and selectivity at the two ends of the band of frequencies which is being tuned. Increasing the Q of the circuit (lowering the resistance) will obviously increase *both* the selectivity and gain.

Circulating Tank Current at Resonance The Q of a circuit has a definite bearing on the circulating tank current at resonance. This tank current is very nearly the value of the line current multiplied by the effective circuit Q. For example: an r-f line current of 0.050 amperes, with a circuit Q of 100, will give a circulating tank current of approximately 5 amperes. From this it can be seen that both the inductor and the connecting wires in a circuit with a high Q must be of very low resistance, particularly in the case of high power transmitters, if heat losses are to be held to a minimum.

Because the voltage across the tank at resonance is determined by the Q, it is possible to develop very high peak voltages across a high Q tank with but little line current.

Effect of Coupling on Impedance If a parallel resonant circuit is coupled to another circuit, such as an antenna output circuit, the impedance and the effective Q of the parallel circuit is decreased as the coupling becomes closer. The effect of closer (tighter) coupling is the same as though an

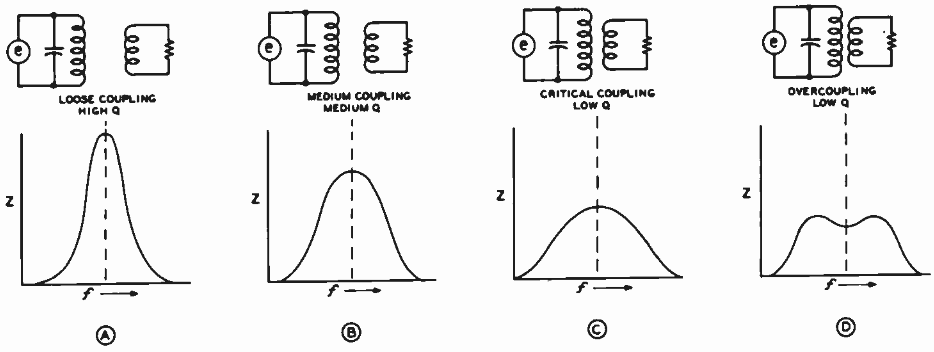


Figure 22
EFFECT OF COUPLING ON CIRCUIT IMPEDANCE AND Q

actual resistance were added in series with the parallel tank circuit. The resistance thus coupled into the tank circuit can be considered as being *reflected* from the output or load circuit to the driver circuit.

The behavior of coupled circuits depends largely upon the amount of coupling, as shown in figure 22. The coupled current in the secondary circuit is small, varying with frequency, being maximum at the resonant frequency of the circuit. As the coupling is increased between the two circuits, the secondary resonance curve becomes broader and the resonant amplitude increases, until the reflected resistance is equal to the primary resistance. This point is called the *critical coupling point.* With greater coupling, the secondary resonance curve becomes broader and develops double resonance humps, which become more pronounced and farther apart in frequency as the coupling between the two circuits is increased.

Tank Circuit Flywheel Effect When the plate circuit of a Class B or Class C operated tube is connected to a parallel resonant circuit tuned to the same frequency as the exciting voltage for the amplifier, the plate current serves to maintain this L/C circuit in a state of oscillation.

The plate current is supplied in short pulses which do not begin to resemble a sine wave, even though the grid may be excited by a sine-wave voltage. These spurts of plate current are converted into a sine wave in the plate tank circuit by virtue of the "Q" or "flywheel effect" of the tank.

If a tank did not have some resistance losses, it would, when given a "kick" with a single pulse, continue to oscillate indefinitely. With a moderate amount of resistance or "friction" in the circuit the tank will still have inertia, and continue to oscillate with decreasing amplitude for a time after being given a "kick." With such a circuit, almost pure sine-wave voltage will be developed across the tank circuit even though power is supplied to the tank in short pulses or spurts, so long as the spurts are evenly spaced with respect to time and have a frequency that is the same as the resonant frequency of the tank.

Another way to visualize the action of the tank is to recall that a resonant tank with moderate Q will discriminate strongly against harmonics of the resonant frequency. The distorted plate current pulse in a Class C amplifier contains not only the fundamental frequency (that of the grid excitation voltage) but also higher harmonics. As the tank offers low impedance to the harmonics and high impedance to the fundamental (being resonant to the latter), only the fundamental — a sine-wave voltage — appears across the tank circuit in substantial magnitude.

Loaded and Unloaded Q Confusion sometimes exists as to the relationship between the unloaded and the loaded Q of the tank circuit in the plate of an r-f power amplifier. In the normal case the loaded Q of the tank circuit is determined by such factors as the operating conditions of the amplifier, bandwidth of the signal to be emitted, permissible level of harmonic radiation, and such factors. The normal value of *loaded* Q for an r-f amplifier used for communications service is from perhaps 6 to 20. The *unloaded* Q of the tank circuit determines the efficiency of the output circuit and is determined by the losses in the tank coil, its leads and plugs and jacks if any, and by the losses in the tank capacitor which ordinarily are very low. The unloaded Q of a good quality large diameter tank coil in the high-frequency range may be as high as 500 to 800, and values greater than 300 are quite common.

Tank Circuit Efficiency Since the unloaded Q of a tank circuit is determined by the minimum losses in the tank, while the loaded Q is determined by useful loading of the tank circuit from the external load in addition to the internal losses in the tank circuit, the relationship between the two Q values determines the operating efficiency of the tank circuit. Expressed in the form of an equation, the loaded efficiency of a tank circuit is:

$$\text{Tank efficiency} = \left(1 - \frac{Q_u}{Q_l}\right) \times 100$$

where Q_u = unloaded Q of the tank circuit
Q_l = loaded Q of the tank circuit

As an example, if the unloaded Q of the tank circuit for a class C r-f power amplifier is 400, and the external load is coupled to the tank circuit by an amount such that the loaded Q is 20, the tank circuit efficiency will be: eff. = (1 − 400/20) × 100, or (1 − 0.05) × 100, or 95 per cent. Hence 5 per cent of the power output of the Class C amplifier will be lost as heat in the tank circuit and the remaining 95 per cent will be delivered to the load.

3-3 Nonsinusoidal Waves and Transients

Pure sine waves, discussed previously, are basic wave shapes. Waves of many different and complex shape are used in electronics, particularly square waves, saw-tooth waves, and peaked waves.

Wave Composition Any periodic wave (one that repeats itself in definite time intervals) is composed of sine waves of different frequencies and amplitudes, added together. The sine wave which has the same frequency as the complex, periodic wave is called the *fundamental.* The frequencies higher than the fundamental are called *harmonics,* and are always a whole number of times higher than the fundamental. For example, the frequency twice as high as the fundamental is called the second harmonic.

The Square Wave Figure 23 compares a square wave with a sine wave (A) of the same frequency. If another sine wave (B) of smaller amplitude, but three times the frequency of (A), called the third harmonic, is added to (A), the resultant wave (C) more nearly approaches the desired square wave.

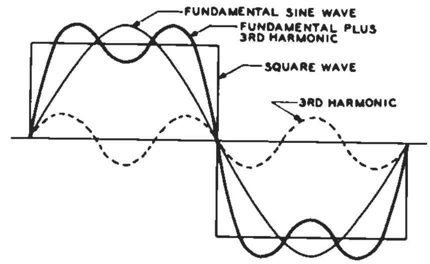


Figure 23
COMPOSITE WAVE-FUNDAMENTAL PLUS THIRD HARMONIC

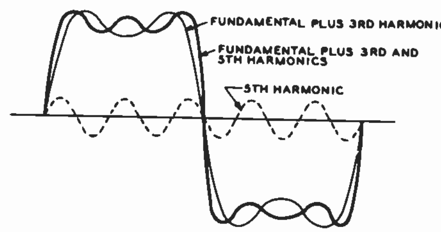


Figure 24
THIRD HARMONIC WAVE PLUS FIFTH HARMONIC

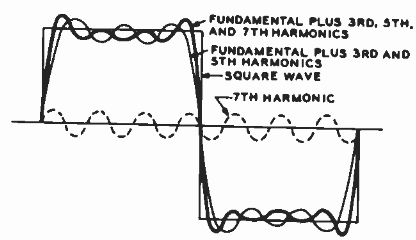


Figure 25
RESULTANT WAVE, COMPOSED OF FUNDAMENTAL, THIRD, FIFTH, AND SEVENTH HARMONICS

This resultant curve (figure 24) is added to a fifth harmonic curve (D), and the sides of the resulting curve (E) are steeper than before. This new curve is shown in figure 25 after a 7th harmonic component has been added to it, making the sides of the composite wave even steeper. Addition of more higher odd harmonics will bring the resultant wave nearer and nearer to the desired square wave shape. The square wave will be achieved if an infinite number of odd harmonics are added to the original sine wave.

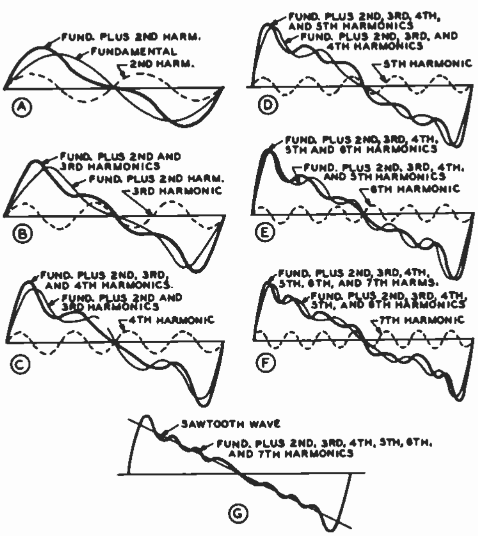


Figure 26
COMPOSITION OF A SAWTOOTH WAVE

The Sawtooth Wave In the same fashion, a sawtooth wave is made up of different sine waves (figure 26). The addition of all harmonics, odd and even, produces the sawtooth wave form.

The Peaked Wave Figure 27 shows the composition of a peaked wave. Note how the addition of each sucessive harmonic makes the peak of the resultant higher and the sides steeper.

Other Waveforms The three preceeding examples show how a complex periodic wave is composed of a fundamental wave and different harmonics. The shape of the resultant wave depends upon the harmonics that are added, their relative amplitudes, and relative phase relationships. In general, the steeper the sides of the waveform, the more harmonics it contains.

AC Transient Circuits If an a-c voltage is substituted for the d-c input voltage in the RC Transient circuits discussed in Chapter 2, the same principles may be applied in the analysis of the transient behavior. An RC coupling circuit is designed to have a long time constant with respect to the lowest frequency it must pass. Such a circuit is shown in figure 28. If a nonsinusoidal voltage is to be passed unchanged through the coupling circuit, the time constant

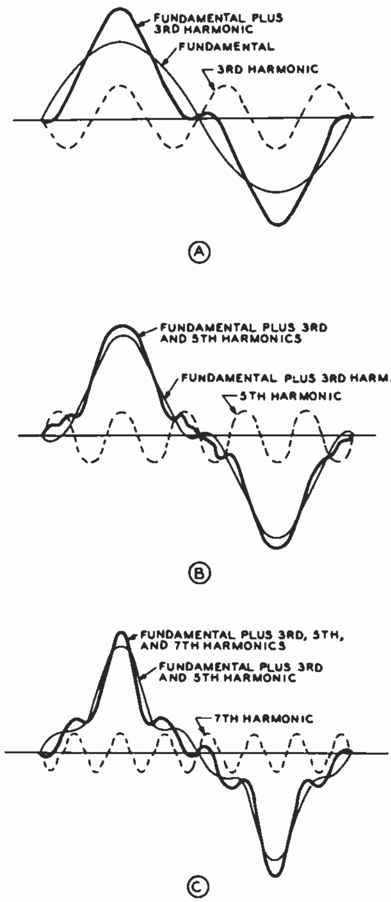


Figure 27
COMPOSITION OF A PEAKED WAVE

must be long with respect to the period of the lowest frequency contained in the voltage wave.

RC Differentiator and Integrator An RC voltage divider that is designed to distort the input waveform is known as a *differentiator* or *integrator*, depending upon the locations of the output taps. The output from a differentiator is taken across the resistance, while the output from an integrator is taken across the capacitor. Such circuits will change the shape of any complex a-c waveform that is impressed upon them. This distortion is a function of the value of the time constant of the circuit as compared to the period of the waveform. Neither a differentiator nor an integrator can change the

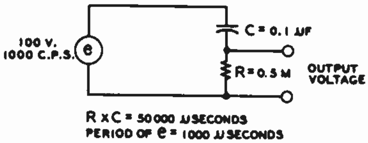


Figure 28
R-C COUPLING CIRCUIT WITH LONG TIME CONSTANT

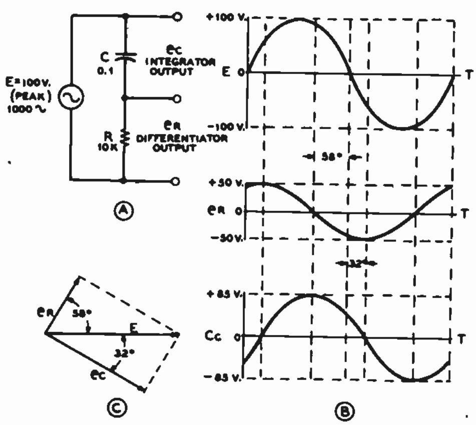


Figure 29
R-C DIFFERENTIATOR AND INTEGRATOR ACTION ON A SINE WAVE

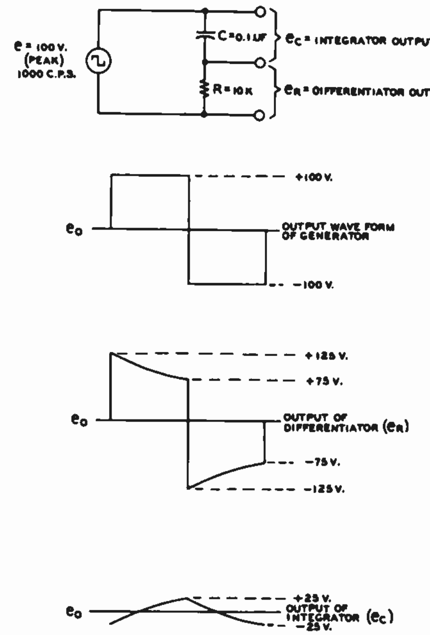


Figure 30
R-C DIFFERENTIATOR AND INTEGRATOR ACTION ON A SQUARE WAVE

shape of a pure sine wave, they will merely shift the phase of the wave (figure 29). The differentiator output is a sine wave leading the input wave, and the integrator output is a sine wave which lags the input wave. The sum of the two outputs at any instant equals the instantaneous input voltage.

Square Wave Input If a square wave voltage is impressed on the circuit of figure 30, a square wave voltage output may be obtained across the integrating capacitor if the time constant of the circuit allows the capacitor to become fully charged. In this particular case, the capacitor never fully charges, and as a result the output of the integrator has a smaller amplitude than the input. The differentiator output has a maximum value greater than the input amplitude, since the voltage left on the capacitor from the previous half wave will add to the input voltage. Such a circuit, when used as a differentiator, is often called a *peaker*. Peaks of twice the input amplitude may be produced.

Sawtooth Wave Input If a back-to-back sawtooth voltage is applied to an RC circuit having a time constant one-sixth the period of the input voltage, the result is shown in figure 31. The capacitor voltage will closely follow the input voltage, if the time constant is short, and the integrator output closely resembles the input. The amplitude is slightly reduced and there is a slight phase lag. Since the voltage across the capacitor is increasing at a constant rate, the charging and discharging current is constant. The output voltage of the differentiator, therefore, is constant during each half of the sawtooth input.

Miscellaneous Inputs Various voltage waveforms other than those represented here may be applied to short RC circuits for the purpose of producing across the resistor an output voltage with an amplitude *proportional to the rate of change* of the input signal. The shorter the RC time constant is made with respect to the period of the input wave, the more nearly the voltage across

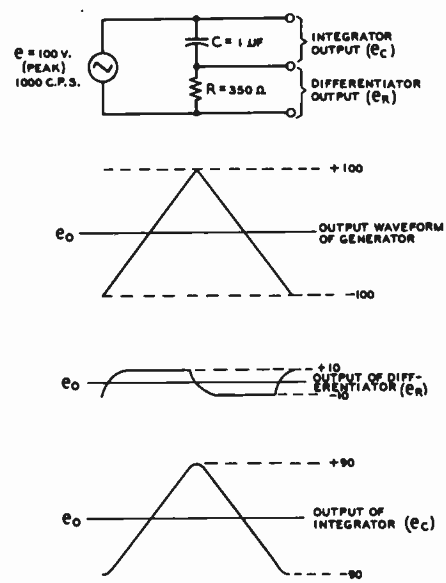


Figure 31
R-C DIFFERENTIATOR AND INTEGRATOR ACTION ON A SAWTOOTH WAVE

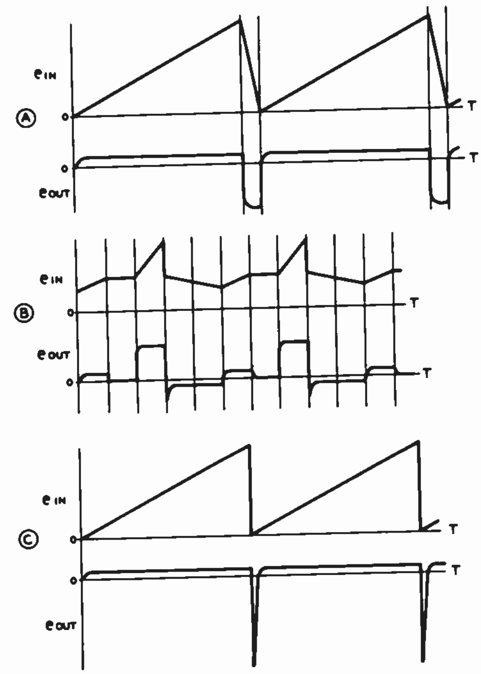


Figure 32

Differentiator outputs of short r-c circuits for various input voltage waveshapes. The output voltage is proportional to the rate of change of the input voltage.

the capacitor conforms to the input voltage. Thus, the differentiator output becomes of particular importance in very short RC circuits. Differentiator outputs for various types of input waves are shown in figure 32.

Square Wave Test for Audio Equipment The application of a square wave input signal to audio equipment, and the observation of the reproduced output signal on an oscilloscope will provide a quick and accurate check of the overall operation of audio equipment. Low-frequency and high-frequency response, as well as transient response can be examined easily. If the amplifier is deficient in low-frequency response, the flat top of the square wave will be canted, as in figure 33. If the high-frequency response is inferior, the rise time of the output wave will be retarded (figure 34). An amplifier with a limited high- and low-frequency response will turn the square wave into the approximation of a sawtooth wave (figure (35).

3-4 Transformers

When two coils are placed in such inductive relation to each other that the lines of force from one cut across the turns of the other inducing a current, the combination can be called a *transformer*. The name is derived from the fact that energy is transformed from one winding to another. The inductance in which the original flux is produced is called the *primary;* the inductance which *receives* the induced current is called the *secondary*. In a radio receiver power transformer, for example, the coil through which the 110-volt a.c. passes is the primary, and the coil from which a higher or lower voltage than the a-c line potential is obtained is the *secondary*.

Transformers can have either air or magnetic cores, depending upon the frequencies at which they are to be operated. The reader should thoroughly impress upon his mind the fact that current can be transferred from one circuit to another *only* if the primary current is changing or alternating. From this it can be seen that a power transformer cannot possibly function as such when the primary is supplied with non-pulsating d.c.

A power transformer usually has a magnetic core which consists of laminations of iron, built up into a square or rectangular form, with a center opening or window. The secondary windings may be several in number, each perhaps delivering a different voltage. The secondary voltages will be proportional to the turns ratio and the primary voltage.

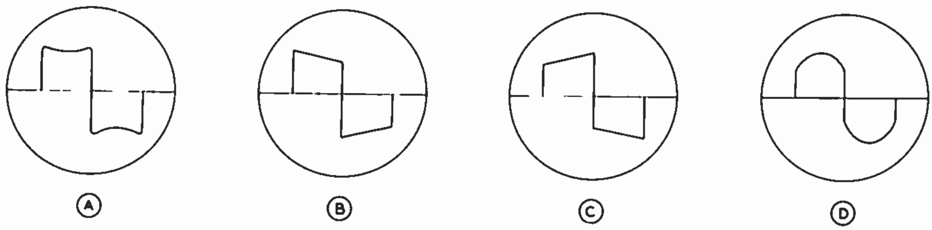


Figure 33

Amplifier deficient in low frequency response will distort square wave applied to the input circuit, as shown. A 60-cycle square wave may be used.

A: Drop in gain at low frequencies
B: Leading phase shift at low frequencies
C: Lagging phase shift at low frequencies
D: Accentuated low frequency gain

Types of Transformers Transformers are used in alternating-current circuits to transfer power at one voltage and impedance to another circuit at another voltage and impedance. There are three main classifications of transformers: those made for use in power-frequency circuits, those made for audio-frequency applications, and those made for radio frequencies.

The Transformation Ratio In a perfect transformer all the magnetic flux lines produced by the primary winding link every turn of the secondary winding. For such a transformer, the ratio of the primary and secondary voltages is exactly the same as the ratio of the number of turns in the two windings:

$$\frac{N_P}{N_S} = \frac{E_P}{E_S}$$

where N_P = number of turns in the primary winding
N_S = number of turns in the secondary winding
E_P = voltage across the primary winding
E_S = voltage across the secondary winding

In practice, the transformation ratio of a transformer is somewhat less than the turns ratio, since unity coupling does not exist between the primary and secondary windings.

Ampere Turns (NI) The current that flows in the secondary winding as a result of the induced voltage must produce a flux which exactly equals the primary flux. The magnetizing force of a coil is expressed as the product of the number of turns in the coil times the current flowing in it:

$$N_P \times I_P = N_S \times I_S\,, \quad \text{or} \quad \frac{N_P}{N_S} = \frac{I_S}{I_P}$$

where I_P = primary current
I_S = secondary current

It can be seen from this expression that when the voltage is stepped up, the current is stepped down, and vice-versa.

Leakage Reactance Since unity coupling does not exist in a practical

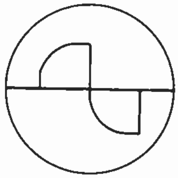


Figure 34

Output waveshape of amplifier having deficiency in high-frequency response. Tested with 10-kc. square wave.

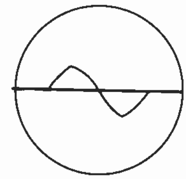


Figure 35

Output waveshape of amplifier having limited low-frequency and high-frequency response. Tested with 1-kc. square wave.

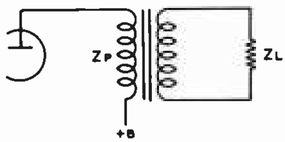


Figure 36
IMPEDANCE-MATCHING TRANSFORMER
The reflected impedance Z_p varies directly in proportion to the secondary load Z_L, and directly in proportion to the square of the primary-to-secondary turns ratio.

transformer, part of the flux passing from the primary circuit to the secondary circuit follows a magnetic circuit acted upon by the primary only. The same is true of the secondary flux. These leakage fluxes cause *leakage reactance* in the transformer, and tend to cause the transformer to have poor voltage regulation. To reduce such leakage reactance, the primary and secondary windings should be in close proximity to each other. The more expensive transformers have interleaved windings to reduce inherent leakage reactance.

Impedance Transformation In the ideal transformer, the impedance of the secondary load is reflected back into the primary winding in the following relationship:

$$Z_P = N^2 Z_S, \quad \text{or} \quad N = \sqrt{Z_P/Z_S}$$

where Z_P = reflected primary impedance
N = turns ratio of transformer
Z_S = impedance of secondary load

Thus any specific load connected to the secondary terminals of the transformer will be transformed to a different specific value appearing across the primary terminals of the transformer. By the proper choice of turns ratio, any reasonable value of secondary load impedance may be "reflected" into the primary winding of the transformer to produce the desired transformer primary impedance. The phase angle of the primary "reflected" impedance will be the same as the phase angle of the load impedance. A capacitive secondary load will be presented to the transformer source as a capacity, a resistive load will present a resistive "reflection" to the primary source. Thus the primary source "sees" a transformer load entirely dependent upon the secondary load impedance and the turns ratio of the transformer (figure 36).

The Auto Transformer The type of transformer in figure 37, when wound with heavy wire over an iron core, is a common device in primary power circuits for the purpose of increasing or decreasing the line voltage. In effect, it is merely a continuous winding with taps taken at various points along the winding, the input voltage being applied to the bottom and also to one tap on the winding. If the output is taken from this same tap, the voltage ratio will be 1-to-1; i.e., the input voltage will be the same as the output voltage. On the other hand, if the output tap is moved down toward the common terminal, there will be a step-down in the turns ratio with a consequent step-down in voltage. The initial setting of the middle input tap is chosen so that the number of turns will have sufficient reactance to keep the no-load primary current at a reasonably low value.

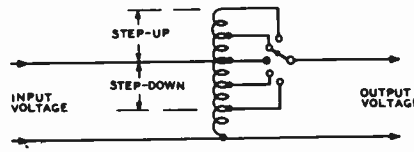


Figure 37
THE AUTO-TRANSFORMER
Schematic diagram of an auto-transformer showing the method of connecting it to the line and to the load. When only a small amount of step up or step down is required, the auto-transformer may be much smaller physically than would be a transformer with a separate secondary winding. Continuously variable auto-transformers (Variac and Powerstat) are widely used commercially.

3-5 Electric Filters

There are many applications where it is desirable to pass a d-c component without passing a superimposed a-c component, or to

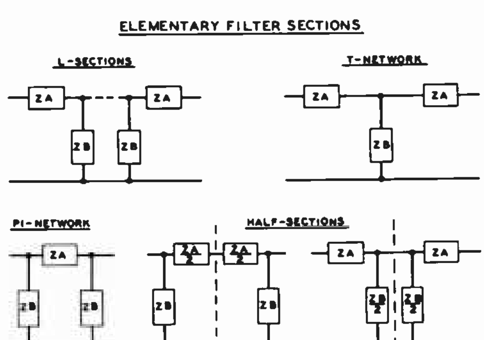


Figure 38
Complex filters may be made up from these basic filter sections.

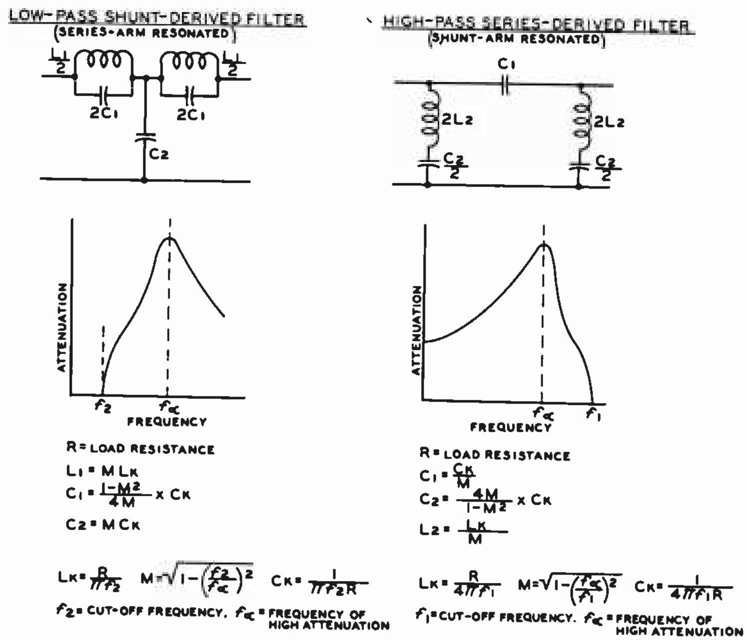


Figure 39

TYPICAL LOW-PASS AND HIGH-PASS FILTERS, ILLUSTRATING SHUNT AND SERIES DERIVATIONS

pass all frequencies above or below a certain frequency while rejecting or attenuating all others, or to pass only a certain band or bands of frequencies while attenuating all others.

All of these things can be done by suitable combinations of inductance, capacitance and resistance. However, as whole books have been devoted to nothing but electric filters, it can be appreciated that it is possible only to touch upon them superficially in a general coverage book.

Filter Operation A filter acts by virtue of its property of offering very high impedance to the undesired frequencies, while offering but little impedance to the desired frequencies. This will also apply to d.c. with a superimposed a-c component, as d.c. can be considered as an alternating current of zero frequency so far as filter discussion goes.

Basic Filters Filters are divided into four classes, descriptive of the frequency bands which they are designed to transmit: high pass, low pass, band pass and band elimination. Each of these classes of filters is made up of elementary filter sections called *L sections* which consist of a series element (Z_A) and a parallel element (Z_B) as illustrated in figure 38. A finite number of L sections may be combined into basic filter sections, called *T networks* or *pi networks*, also shown in figure 38. Both the T and pi networks may be divided in two to form *half-sections*.

Filter Sections The most common filter section is one in which the two impedances Z_A and Z_B are so related that their arithmetical product is a constant: $Z_A \times Z_B = K^2$ at all frequencies. This type of filter section is called a *constant-K section*.

A section having a sharper cutoff frequency than a constant-K section, but less attenuation at frequencies far removed from cutoff is the *M-derived section*, so called because the shunt or series element is resonated with a reactance of the opposite sign. If the complementary reactance is added to the series arm, the section is said to be *shunt derived;* if added to the shunt arm, *series derived.* Each impedance of the M-derived section is related to a corresponding impedance in the constant-K section by some factor which is a function of the constant *m*. *M*, in turn, is a function of the ratio between the cutoff frequency and the frequency of infinite attenuation, and will

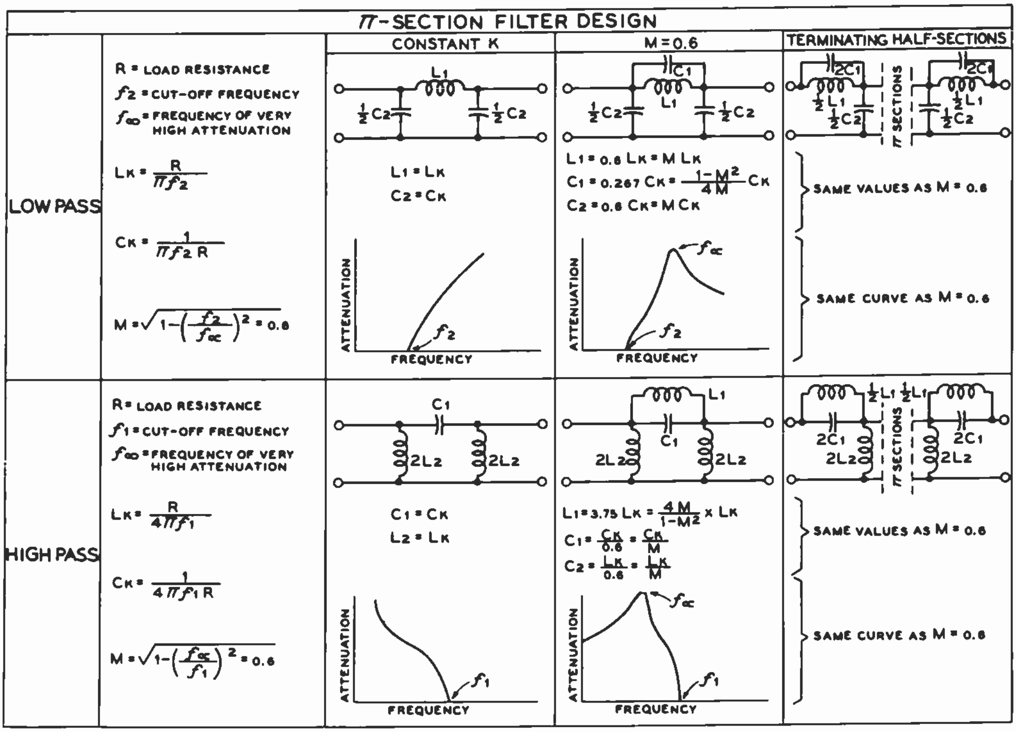


Figure 40

Through the use of the curves and equations which accompany the diagrams in the illustration above it is possible to determine the correct values of inductance and capacitance for the usual types of pi-section filters.

have some value between zero and one. As the value of *m* approaches zero, the sharpness of cutoff increases, but the less will be the attenuation at several times cutoff frequency. A value of 0.6 may be used for *m* in most applications. The "notch" frequency is determined by the resonant frequency of the tuned filter element. The amount of attenuation obtained at the "notch" when a derived section is used is determined by the effective Q of the resonant arm (figure 39).

Filter Assembly Constant-K sections and derived sections may be cascaded to obtain the combined characteristics of sharp cutoff and good remote frequency attenuation. Such a filter is known as a *composite* filter. The amount of attenuation will depend upon the number of filter sections used, and the shape of the transmission curve depends upon the type of filter sections used. All filters have some *insertion loss*. This attenuation is usually uniform to all frequencies within the pass band. The insertion loss varies with the type of filter, the Q of the components and the type of termination employed.

Electric Filter Design Electric wave filters have long been used in some amateur stations in the audio channel to reduce the transmission of unwanted high frequencies and hence to reduce the bandwidth occupied by a radiophone signal. The effectiveness of a properly designed and properly used filter circuit in reducing QRM and sideband splatter should not be underestimated.

In recent years, high frequency filters have become commonplace in TVI reduction. High-pass type filters are placed before the input stage of television receivers to reject the fundamental signal of low frequency transmitters. Low-pass filters are used in the output circuits of low frequency transmitters to prevent harmonics of the transmitter from being radiated in the television channels.

The chart of figure 40 gives design data and procedure on the pi-section type of filter. M-derived sections with an M of 0.6 will be found to be most satisfactory as the input section (or half-section) of the usual filter since the input impedance of such a section is most constant over the pass band of the filter section.

Simple filters may use either L, T, or π sections. Since the π section is the more commonly used type figure 40 gives design data and characteristics for this type of filter.

CHAPTER FOUR

Vacuum Tube Principles

In the previous chapters we have seen the manner in which an electric current flows through a metallic conductor as a result of an electron drift. This drift, which takes place when there is a difference in potential between the ends of the metallic conductor, is in addition to the normal random electron motion between the molecules of the conductor.

The electron may be considered as a minute negatively charged particle, having a mass of 9×10^{-28} gram, and a charge of 1.59×10^{-19} coulomb. Electrons are always identical, regardless of the source from which they are obtained.

An electric current can be caused to flow through other media than a metallic conductor. One such medium is an ionized solution, such as the sulfuric acid electrolyte in a storage battery. This type of current flow is called *electrolytic conduction*. Further, it was shown at about the turn of the century that an electric current can be carried by a stream of free electrons in an evacuated chamber. The flow of a current in such a manner is said to take place by *electronic conduction*. The study of electron tubes (also called vacuum tubes, or valves) is actually the study of the control and use of electronic currents within an evacuated or partially evacuated chamber.

Since the current flow in an electron tube takes place in an evacuated chamber, there must be located within the enclosure both a source of electrons and a collector for the electrons which have been emitted. The electron source is called the *cathode*, and the electron collector is usually called the *anode*. Some external source of energy must be applied to the cathode in order to impart sufficient velocity to the electrons within the cathode material to enable them to overcome the surface forces and thus escape into the surrounding medium. In the usual types of electron tubes the cathode energy is applied in the form of heat; electron emission from a heated cathode is called *thermionic emission*. In another common type of electron tube, the photoelectric cell, energy in the form of light is applied to the cathode to cause *photoelectric emission*.

4-1 Thermionic Emission

Electron Emission Emission of electrons from the cathode of a thermionic electron tube takes place when the cathode of the tube is heated to a temperature sufficiently high that the free electrons in the emitter have sufficient velocity to overcome the restraining forces at the surface of the material. These surface forces vary greatly with different materials. Hence different types of cathodes must be raised to different temperatures to obtain adequate quantities of electron emission. The several types of emitters found in common types of transmitting and receiving tubes will be described in the following paragraphs.

Cathode Types The emitters or cathodes as used in present-day thermionic electron tubes may be classified into two groups: the directly-heated or *filament type* and the indirectly-heated or *heater-cathode type*. Directly-heated emitters may be further subdivided into three important groups, all of which are commonly used in modern vacuum tubes. These classifications are: the pure-tungsten filament, the thoriated-tungsten filament, and the oxide-coated filament.

The Pure Tungsten Filament Pure tungsten wire was used as the filament in nearly all the earlier transmitting and

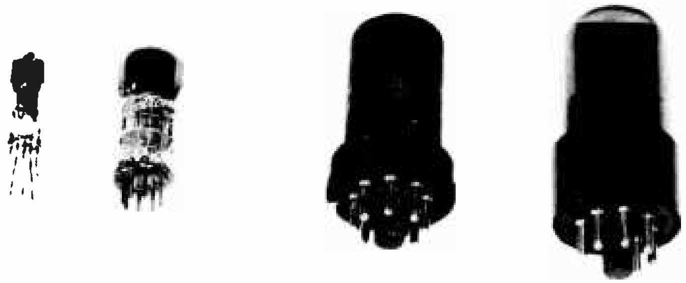


Figure 1
CONVENTIONAL ELECTRON-TUBE TYPES

receiving tubes. However, the thermionic efficiency of tungsten wire as an emitter (the number of milliamperes emission per watt of filament heating power) is quite low, the filaments become fragile after use, their life is rather short, and they are susceptible to burnout at any time. Pure tungsten filaments must be run at bright white heat (about 2500° Kelvin). For these reasons, tungsten filaments have been replaced in all applications where another type of filament could be used. They are, however, still universally employed in large water-cooled tubes and in certain large, high-power air-cooled triodes where another filament type would be unsuitable. Tungsten filaments are the most satisfactory for high-power, high-voltage tubes where the emitter is subjected to positive ion bombardment caused by the residual gas content of the tubes. Tungsten is not adversely affected by such bombardment.

The Thoriated-Tungsten Filament In the course of experiments made upon tungsten emitters, it was found that filaments made from tungsten having a small amount of thoria (thorium oxide) as an impurity had much greater emission than those made from the pure metal. Subsequent development has resulted in the highly efficient carburized thoriated-tungsten filament as used in virtually all medium-power transmitting tubes today.

Thoriated-tungsten emitters consist of a tungsten wire containing from 1% to 2% thoria. The activation process varies between different manufacturers of vacuum tubes, but it is essentially as follows: (1) the tube is evacuated; (2) the filament is burned for a short period at about 2800° Kelvin to clean the surface and reduce some of the thoria within the filament to metallic thorium; (3) the filament is burned for a longer period at about 2100° Kelvin to form a layer of thorium on the surface of the tungsten; (4) the temperature is reduced to about 1600° Kelvin and some pure hydrocarbon gas is admitted to form a layer of tungsten carbide on the surface of the tungsten. This layer of tungsten carbide reduces the rate of thorium evaporation from the surface at the normal operating temperature of the filament and thus increases the operating life of the vacuum tube. Thorium evaporation from the surface is a natural consequence of the operation of the thoriated-tungsten filament. The carburized layer on the tungsten wire plays another role in acting as a reducing agent to produce new thorium from the thoria to replace that lost by evaporation. This new thorium continually diffuses to the surface during the normal operation of the filament. The last process, (5), in the activation of a thoriated tungsten filament consists of re-evacuating the envelope and then burning or ageing the new filament for a considerable period of time at the normal operating temperature of approximately 1900° K.

One thing to remember about any type of filament, particularly the thoriated type, is that the emitter deteriorates practically as fast when "standing by" (no plate current) as it does with any normal amount of emission load. Also, a thoriated filament may be either temporarily or permanently damaged by a heavy overload which may strip the surface layer of thorium from the filament.

Reactivating Thoriated-Tungsten Filaments Thoriated-tungsten filaments (and *only* thoriated-tungsten filaments) which have lost emission as a result of insufficient filament voltage, a severe temporary overload, a less severe extended overload, or even normal operation

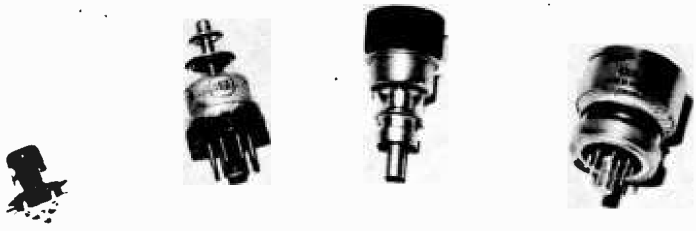


Figure 2
V-H-F and U-H-F TUBE TYPES

The tube to the left in this photograph is a 955 "acorn" triode. The 6F4 acorn triode is very similar in appearance to the 955 but has two leads brought out each for the grid and for the plate connection. The second tube is a 446A "lighthouse" triode. The 2C40, 2C43, and 2C44 are more recent examples of the same type tube and are essentially the same in external appearance. The third tube from the left is a 2C39 "oilcan" tube. This tube type is essentially the inverse of the lighthouse variety since the cathode and heater connections come out the small end and the plate is the large finned radiator on the large end. The use of the finned plate radiator makes the oilcan tube capable of approximately 10 times as much plate dissipation as the lighthouse type. The tube to the right is the 4X150A beam tetrode. This tube, a comparatively recent release, is capable of somewhat greater power output than any of the other tube types shown, and is rated for full output at 500 Mc. and at reduced output at frequencies greater than 1000 Mc.

may quite frequently be reactivated to their original characteristics by a process similar to that of the original activation. However, only filaments which have not approached too close to the end of their useful life may be successfully reactivated.

The actual process of reactivation is relatively simple. The tube which has gone "flat" is placed in a socket to which only the two filament wires have been connected. The filament is then "flashed" for about 20 to 40 seconds at about $1\frac{1}{2}$ times normal rated voltage. The filament will become extremely bright during this time and, if there is still some thoria left in the tungsten and if the tube did not originally fail as a result of an air leak, some of this thoria will be reduced to metallic thorium. The filament is then burned at 15 to 25 per cent overvoltage for from 30 minutes to 3 to 4 hours to bring this new thorium to the surface.

The tube should then be tested to see if it shows signs of renewed life. If it does, but is still weak, the burning process should be continued at about 10 to 15 per cent overvoltage for a few more hours. This should bring it back almost to normal. If the tube checks still very low after the first attempt at reactivation, the complete process can be repeated as a last effort.

The Oxide-Coated Filament The most efficient of all modern filaments is the oxide-coated type which consists of a mixture of barium and strontium oxides coated upon a nickel alloy wire or strip. This type of filament operates at a dull-red to orange-red temperature (1050° to 1170° K) at which temperature it will emit large quantities of electrons. The oxide-coated filament is somewhat more efficient than the thoriated-tungsten type in small sizes and it is considerably less expensive to manufacture. For this reason all receiving tubes and quite a number of the low-powered transmitting tubes use the oxide-coated filament. Another advantage of the oxide-coated emitter is its extremely long life — the average tube can be expected to run from 3000 to 5000 hours, and when loaded very lightly, tubes of this type have been known to give 50,000 hours of life before their characteristics changed to any great extent.

Oxide filaments are unsatisfactory for use at high continuous plate voltages because: (1) their activity is seriously impaired by the high temperature necessary to de-gas the high-voltage tubes and, (2) the positive ion bombardment which takes place even in the best evacuated high-voltage tube causes destruction of the oxide layer on the surface of the filament.

Oxide-coated emitters have been found capable of emitting an enormously large current pulse with a high applied voltage for a very short period of time without damage. This characteristic has proved to be of great value

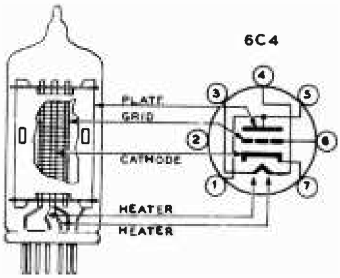


Figure 3
CUT-AWAY DRAWING OF A 6C4 TRIODE

in radar work. For example, the relatively small cathode in a microwave magnetron may be called upon to deliver 25 to 50 amperes at an applied voltage of perhaps 25,000 volts for a period in the order of one microsecond. After this large current pulse has been passed, plate voltage normally will be removed for 1000 microseconds or more so that the cathode surface may be restored in time for the next pulse of current. If the cathode were to be subjected to a continuous current drain of this magnitude, it would be destroyed in an exceedingly short period of time.

The activation of oxide-coated filaments also varies with tube manufacturers but consists essentially in heating the wire which has been coated with a mixture of barium and strontium carbonates to a temperature of about 1500° Kelvin for a time and then applying a potential of 100 to 200 volts through a protective resistor to limit the emission current. This process reduces the carbonates to oxides thermally, cleans the filament surface of foreign materials, and activates the cathode surface.

Reactivation of oxide-coated filaments is not possible since there is always more than sufficient reduction of the oxides and diffusion of the metals to the surface of the filament to meet the emission needs of the cathode.

The Heater Cathode The heater type cathode was developed as a result of the requirement for a type of emitter which could be operated from alternating current and yet would not introduce a-c ripple modulation even when used in low-level stages. It consists essentially of a small nickel-alloy cylinder with a coating of strontium and barium oxides on its surface similar to the coating used on the oxide-coated filament. Inside the cylinder is an insulated heater element consisting usually of a double spiral of tungsten wire. The heater may operate on any voltage from 2 to 117 volts, although 6.3 is the most common value. The heater is operated at quite a high temperature so that the cathode itself usually may be brought to operating temperature in a matter of 15 to 30 seconds. Heat-coupling between the heater and the cathode is mainly by radiation, although there is some thermal conduction through the insulating coating on the heater wire, as this coating is also in contact with the cathode thimble.

Indirectly heated cathodes are employed in all a-c operated tubes which are designed to operate at a low level either for r-f or a-f use. However, some receiver power tubes use heater cathodes (6L6, 6V6, 6F6, and 6K6-GT) as do some of the low-power transmitter tubes (802, 807, 815, 3E29, 2E26, 5763, etc.). Heater cathodes are employed almost exclusively when a number of tubes are to be operated in series as in an a.c.-d.c. receiver. A heater cathode is often called a *uni-potential cathode* because there is no voltage drop along its length as there is in the directly-heated or filament cathode.

The Bombardment Cathode A special bombardment cathode is employed in many of the new high powered television transmitting klystrons (Eimac 3K 20,000 LA). The cathode takes the form of a tantalum diode, heated to operating temperature by the bombardment of electrons from a directly heated filament. The cathode operates at a positive potential of 2000 volts with respect to the filament, and a d-c bombardment current of 0.66 amperes flows between filament and cathode. The filament is designed to operate under space-charge limited conditions. Cathode temperature is varied by changing the bombardment potential between the filament and the cathode.

The Emission Equation The emission of electrons from a heated cathode is quite similar to the evaporation of molecules from the surface of a liquid. The molecules which leave the surface are those having sufficient kinetic (heat) energy to overcome the forces at the surface of the liquid. As the temperature of the liquid is raised, the average velocity of the molecules is increased, and a greater number of molecules will acquire sufficient energy to be evaporated. The evaporation of electrons from the surface of a thermionic emitter is similarly a function of average electron velocity, and hence is a function of the temperature of the emitter.

Electron emission per unit area of emitting surface is a function of the temperature T in degrees Kelvin, the work function of the emitting surface b (which is a measure of the

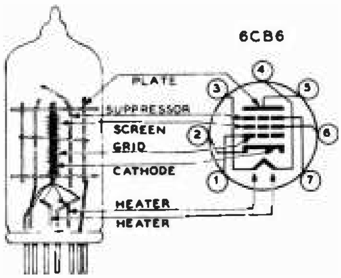


Figure 4
CUT-AWAY DRAWING OF A 6CB6 PENTODE

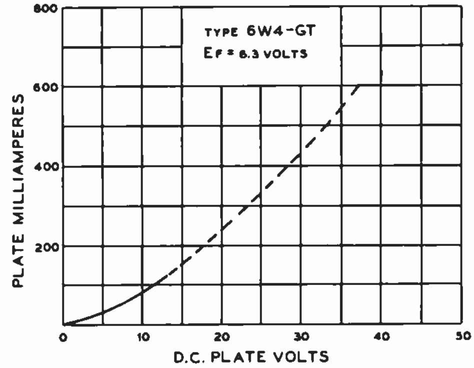


Figure 5
AVERAGE PLATE CHARACTERISTICS OF A POWER DIODE

surface forces of the material and hence of the energy required of the electron before it may escape), and of the constant A which also varies with the emitting surface. The relationship between emission current in amperes per square centimeter, I, and the above quantities can be expressed as:

$$I = AT^2\epsilon^{-b/T}$$

Secondary Emission The bombarding of most metals and a few insulators by electrons will result in the emission of other electrons by a process called *secondary emission.* The secondary electrons are literally knocked from the surface layers of the bombarded material by the primary electrons which strike the material. The number of secondary electrons emitted per primary electron varies from a very small percentage to as high as 5 to 10 secondary electrons per primary.

The phenomena of secondary emission is undesirable for most thermionic electron tubes. However, the process is used to advantage in certain types of electron tubes such as the image orthicon (TV camera tube) and the electron-multiplier type of photo-electric cell. In types of electron tubes which make use of secondary emission, such as the type 931 photo cell, the secondary-electron-emitting surfaces are specially treated to provide a high ratio of secondary to primary electrons. Thus a high degree of current amplification in the electron-multiplier section of the tube is obtained.

The Space Charge Effect As a cathode is heated so that it begins to emit, those electrons which have been discharged into the surrounding space form a negatively charged cloud in the immediate vicinity of the cathode. This cloud of electrons around the cathode is called the *space charge.* The electrons comprising the charge are continuously changing, since those electrons making up the original charge fall back into the cathode and are replaced by others emitted by it.

4-2 The Diode

If a cathode capable of being heated either indirectly or directly is placed in an evacuated envelope along with a plate, such a two-element vacuum tube is called a diode. The diode is the simplest of all vacuum tubes and is the fundamental type from which all the others are derived.

Characteristics of the Diode When the cathode within a diode is heated, it will be found that a few of the electrons leaving the cathode will leave with sufficient velocity to reach the plate. If the plate is electrically connected back to the cathode, the electrons which have had sufficient velocity to arrive at the plate will flow back to the cathode through the external circuit. This small amount of initial plate current is an effect found in all two-element vacuum tubes.

If a battery or other source of d-c voltage is placed in the external circuit between the plate and cathode so that it places a positive potential on the plate, the flow of current from the cathode to plate will be increased. This is due to the strong attraction offered by the positively charged plate for any negatively charged particles (figure 5).

Space-Charge Limited Current At moderate values of plate voltage the current flow from cathode to anode is limited by the space charge of electrons around the cathode. Increased values

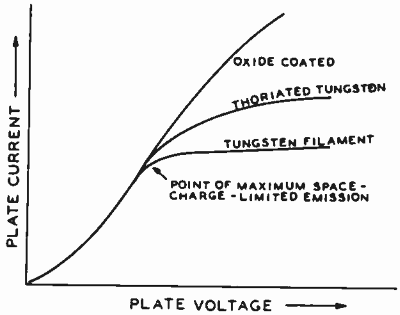


Figure 6
MAXIMUM SPACE-CHARGE-LIMITED EMISSION FOR DIFFERENT TYPES OF EMITTERS

of plate voltage will tend to neutralize a greater portion of the cathode space charge and hence will cause a greater current to flow.

Under these conditions, with plate current limited by the cathode space charge, the plate current is not linear with plate voltage. In fact it may be stated in general that the plate-current flow in electron tubes does not obey Ohm's Law. Rather, plate current increases as the three-halves power of the plate voltage. The relationship between plate voltage, E, and plate current, I, can be expressed as:

$$I = K\,E^{3/2}$$

where K is a constant determined by the geometry of the element structure within the electron tube.

Plate Current Saturation As plate voltage is raised to the potential where the cathode space charge is neutralized, all the electrons that the cathode is capable of emitting are being attracted to the plate. The electron tube is said then to have reached *saturation* plate current. Further increase in plate voltage will cause only a relatively small increase in plate current. The initial point of plate current saturation is sometimes called the point of Maximum Space-Charge-Limited Emission (MSCLE).

The degree of flattening in the plate-voltage plate-current curve after the MSCLE point will vary with different types of cathodes. This effect is shown in figure 6. The flattening is quite sharp with a pure tungsten emitter. With thoriated tungsten the flattening is smoothed somewhat, while with an oxide-coated cathode the flattening is quite gradual. The gradual saturation in emission with an oxide-coated emitter is generally considered to result from

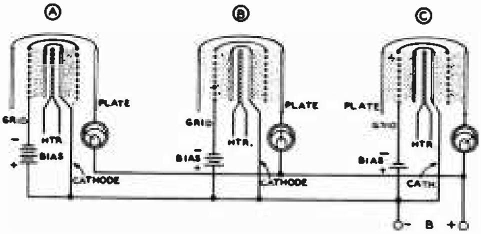


Figure 7
ACTION OF THE GRID IN A TRIODE

(A) shows the triode tube with cutoff bias on the grid. Note that all the electrons emitted by the cathode remain inside the grid mesh. (B) shows the same tube with an intermediate value of bias on the grid. Note the medium value of plate current and the fact that there is a reserve of electrons remaining within the grid mesh. (C) shows the operation with a relatively small amount of bias which with certain tube types will allow substantially all the electrons emitted by the cathode to reach the plate. Emission is said to be saturated in this case. In a majority of tube types a high value of positive grid voltage is required before plate-current saturation takes place.

a lowering of the surface work function by the field at the cathode resulting from the plate potential.

Electron Energy Dissipation The current flowing in the plate-cathode space of a conducting electron tube represents the energy required to accelerate electrons from the zero potential of the cathode space charge to the potential of the anode. Then, when these accelerated electrons strike the anode, the energy associated with their velocity is immediately released to the anode structure. In normal electron tubes this energy release appears as heating of the plate or anode structure.

4-3 The Triode

If an element consisting of a mesh or spiral of wire is inserted concentric with the plate and between the plate and the cathode, such an element will be able to control by electrostatic action the cathode-to-plate current of the tube. The new element is called a *grid*, and a vacuum tube containing a cathode, grid, and plate is commonly called a triode.

Action of the Grid If this new element through which the electrons must pass in their course from cathode to plate is made negative with respect to the cathode, the nega-

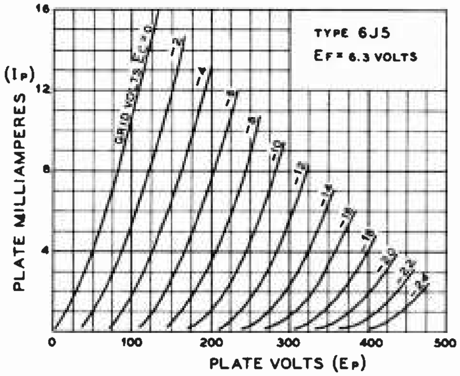


Figure 8

NEGATIVE-GRID CHARACTERISTICS (I_p VS. E_p CURVES) OF A TYPICAL TRIODE

Average plate characteristics of this type are most commonly used in determining the Class A operating characteristics of a triode amplifier stage.

tive charge on this grid will effectively repel the negatively charged electrons (like charges repel; unlike charges attract) back into the space charge surrounding the cathode. Hence, the number of electrons which are able to pass through the grid mesh and reach the plate will be reduced, and the plate current will be reduced accordingly. If the charge on the grid is made sufficiently negative, all the electrons leaving the cathode will be repelled back to it and the plate current will be reduced to zero. Any d-c voltage placed upon a grid is called a *bias* (especially so when speaking of a control grid). The smallest negative voltage which will cause cutoff of plate current at a particular plate voltage is called the value of *cutoff bias* (figure 7).

Amplification Factor The amount of plate current in a triode is a result of the net field at the cathode from interaction between the field caused by the grid bias and that caused by the plate voltage. Hence, both grid bias and plate voltage affect the plate current. In all normal tubes a small change in grid bias has a considerably greater effect than a similar change in plate voltage. The ratio between the change in grid bias and the change in plate current which will cause the same small change in plate current is called the *amplification factor* or μ of the electron tube. Expressed as an equation:

$$\mu = -\frac{\Delta E_p}{\Delta E_g}$$

with i_p constant (Δ represents a small increment).

The μ can be determined experimentally by making a small change in grid bias, thus slightly changing the plate current. The plate current is then returned to the original value by making a change in the plate voltage. The ratio of the change in plate voltage to the change in grid voltage is the μ of the tube under the operating conditions chosen for the test.

Current Flow in a Triode In a diode it was shown that the electrostatic field at the cathode was proportional to the plate potential, E_p, and that the total cathode current was proportional to the three-halves power of the plate voltage. Similiarly, in a triode it can be shown that the field at the cathode space charge is proportional to the equivalent voltage ($E_g + E_p/\mu$), where the amplification factor, μ, actually represents the relative effectiveness of grid potential and plate potential in producing a field at the cathode.

It would then be expected that the cathode current in a triode would be proportional to the three-halves power of ($E_g + E_p/\mu$). The cathode current of a triode can be represented with fair accuracy by the expression:

$$\text{Cathode current} = K\left(E_g + \frac{E_p}{\mu}\right)^{3/2}$$

where K is a constant determined by element geometry within the triode.

Plate Resistance The *plate resistance* of a vacuum tube is the ratio of a change in plate voltage to the change in plate current which the change in plate voltage produces. To be accurate, the changes should be very small with respect to the operating values. Expressed as an equation:

$$R_p = \frac{\Delta E_p}{\Delta I_p} \quad E_g = \text{constant},\ \Delta = \text{small increment}$$

The plate resistance can also be determined by the experiment mentioned above. By noting the change in plate current as it occurs when the plate voltage is changed (grid voltage held constant), and by dividing the latter by the former, the plate resistance can be determined. Plate resistance is expressed in Ohms.

Transconductance The mutual conductance, also referred to as *transconductance,* is the ratio of a change in the plate current to the change in grid voltage which brought about the plate current change, the plate voltage being held constant. Expressed as an equation:

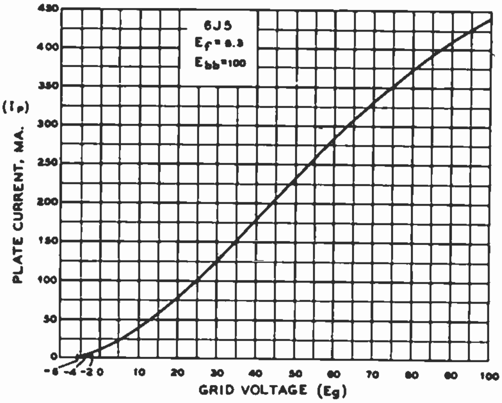


Figure 9

POSITIVE-GRID CHARACTERISTICS (I_p VS. E_g) OF A TYPICAL TRIODE

Plate characteristics of this type are most commonly used in determining the pulse-signal operating characteristics of a triode amplifier stage. Note the large emission capability of the oxide-coated heater cathode in tubes of the general type of the 6J5.

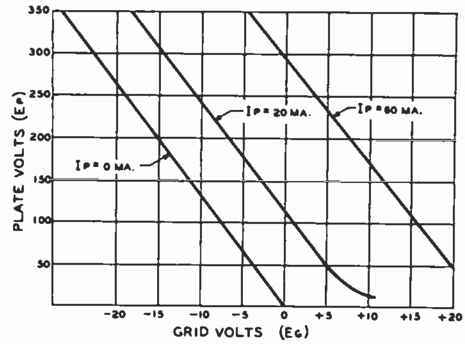


Figure 10

CONSTANT CURRENT (E_p VS. E_g) CHARACTERISTICS OF A TYPICAL TRIODE TUBE

This type of graphical representation is used for Class C amplifier calculations since the operating characteristic of a Class C amplifier is a straight line when drawn upon a constant current graph.

$$G_m = \frac{\Delta I_p}{\Delta E_g} \quad E_p = \text{constant}, \ \Delta = \text{small increment}$$

The transconductance is also numerically equal to the amplification factor divided by the plate resistance. $G_m = \mu / R_p$.

Transconductance is most commonly expressed in microreciprocal-ohms or *micromhos.* However, since transconductance expresses change in plate current as a function of a change in grid voltage, a tube is often said to have a transconductance of so many milliamperes-per-volt. If the transconductance in milliamperes-per-volt is multiplied by 1000 it will then be expressed in micromhos. Thus the transconductance of a 6A3 could be called either 5.25 ma./volt or 5250 micromhos.

Characteristic Curves of a Triode Tube The operating characteristics of a triode tube may be summarized in three sets of curves: The I_p vs. E_p curve (figure 8), the I_p vs. E_g curve (figure 9) and the E_p vs. E_g curve (figure 10). The *plate resistance* (R_p) of the tube may be observed from the I_p vs. E_p curve, the *transconductance* (G_m) may be observed from the I_p vs. E_g curve, and the *amplification factor* (μ) may be determined from the E_p vs. E_g curve.

The Load Line A *load line* is a graphical representation of the voltage on the plate of a vacuum tube, and the current passing through the plate circuit of the tube for various values of plate-load resistance and plate-supply voltage. Figure 11 illustrates a triode tube with a resistive plate load, and a supply voltage of 300 volts. The voltage at the plate of the tube (e_p) may be expressed as:

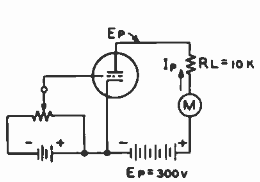
$$e_p = E_p - (i_p \times R_L)$$

where E_p is the plate supply voltage, i_p is the plate current, and R_L is the load resistance in ohms.

Assuming various values of i_p flowing in the circuit, controlled by the internal resistance of the tube, (a function of the grid bias) values of plate voltage may be plotted as shown for each value of plate current (i_p). The line connecting these points is called the *load line* for the particular value of plate-load resistance used. The *slope* of the load line is equal to the ratio of the lengths of the vertical and horizontal projections of any segment of the load line. For this example it is:

$$\text{Slope} = -\frac{.01 - .02}{100 - 200} = -.0001 = -\frac{1}{10{,}000}$$

The slope of the load line is equal to $-1/R_L$. At point A on the load line, the voltage across the tube is zero. This would be true for a perfect tube with zero internal voltage drop, or if the tube is short-circuited from cathode to plate. Point B on the load line corresponds to the cutoff point of the tube, where no plate current is flowing. The operating range of the tube lies between these two extremes. For additional information re-



IP (MA.)	EP
0	300
5	250
10	200
15	150
20	100
25	50
30	0

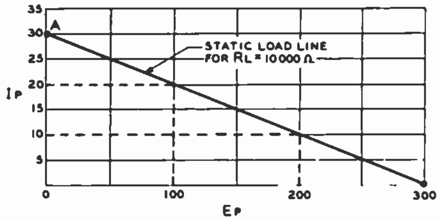


Figure 11

The static load line for a typical triode tube with a plate load resistance of 10,000 ohms.

garding *dynamic* load lines, the reader is referred to the *Radiotron Designer's Handbook*, 4th edition, distributed by Radio Corporation of America.

Application of Tube Characteristics As an example of the application of tube characteristics, the constants of the triode amplifier circuit shown in figure 12 may be considered. The plate supply is

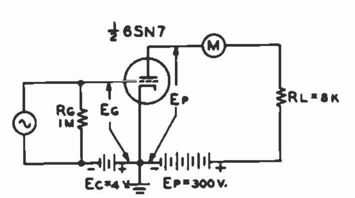


Figure 12

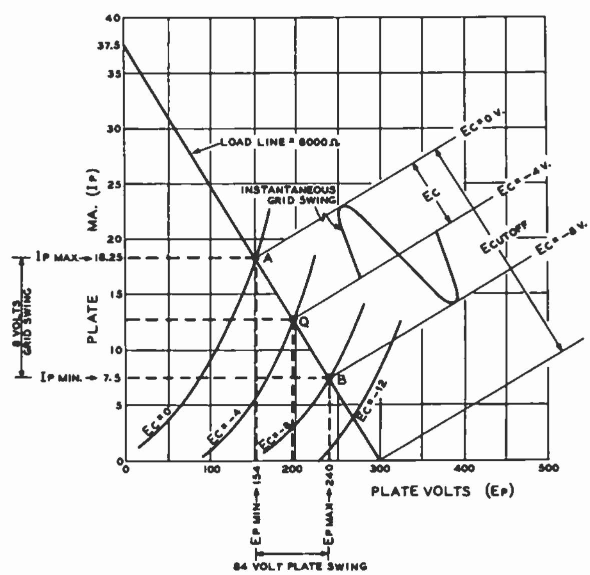
TRIODE TUBE CONNECTED FOR DETERMINATION OF PLATE CIRCUIT LOAD LINE, AND OPERATING PARAMETERS OF THE CIRCUIT

300 volts, and the plate load is 8,000 ohms. If the tube is considered to be an open circuit no plate current will flow, and there is no voltage drop across the plate load resistor, R_L. The plate voltage on the tube is therefore 300 volts. If, on the other hand, the tube is considered to be a short circuit, maximum possible plate current flows and the full 300 volt drop appears across R_L. The plate voltage is zero, and the plate current is 300/8,000, or 37.5 milliamperes. These two extreme conditions define the load line on the I_p vs. E_p characteristic curve, figure 13.

For this application the grid of the tube is returned to a steady biasing voltage of −4 volts. The steady or quiescent operation of the tube is determined by the intersection of the load line with the −4 volt curve at point Q. By projection from point Q through the plate

Figure 13

APPLICATION OF I_p VS. E_p CHARACTERISTICS OF VACUUM TUBE



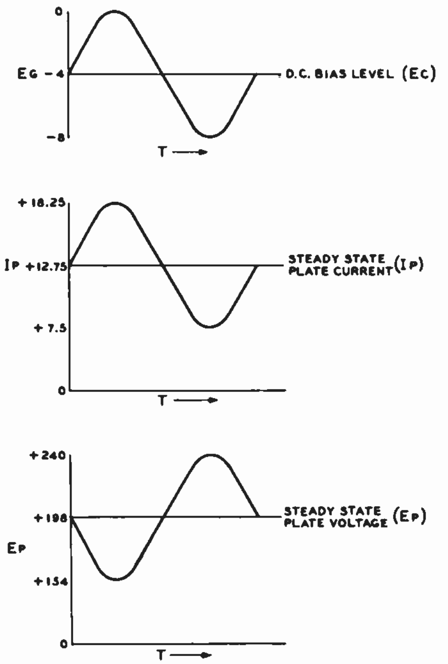


Figure 14
POLARITY REVERSAL BETWEEN GRID AND PLATE VOLTAGES

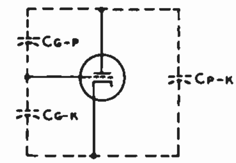


Figure 15
SCHEMATIC REPRESENTATION OF INTERELECTRODE CAPACITANCE

current axis it is found that the value of plate current with no signal applied to the grid is 12.75 milliamperes. By projection from point Q through the plate voltage axis it is found that the quiescent plate voltage is 198 volts. This leaves a drop of 102 volts across R_L which is borne out by the relation 0.01275 × 8,000 = 102 volts.

An alternating voltage of 4 volts maximum swing about the normal bias value of −4 volts is applied now to the grid of the triode amplifier. This signal swings the grid in a positive direction to 0 volts, and in a negative direction to −8 volts, and establishes the *operating region* of the tube along the load line between points A and B. Thus the maxima and minima of the plate voltage and plate current are established. By projection from points A and B through the plate current axis the maximum instantaneous plate current is found to be 18.25 milliamperes and the minimum is 7.5 milliamperes. By projections from points A and B through the plate voltage axis the minimum instantaneous plate voltage swing is found to be 154 volts and the maximum is 240 volts.

By this graphical application of the I_p vs. E_p characteristic of the 6SN7 triode the operation of the circuit illustrated in figure 12 becomes apparent. A voltage variation of 8 volts (peak-to-peak) on the grid produces a variation of 84 volts at the plate.

Polarity Inversion When the signal voltage applied to the grid has its maximum positive instantaneous value the plate current is also maximum. Reference to figure 12 shows that this maximum plate current flows through the plate load resistor R_L, producing a maximum voltage drop across it. The lower end of R_L is connected to the plate supply, and is therefore held at a constant potential of 300 volts. With maximum voltage drop across the load resistor, the upper end of R_L is at a minimum instantaneous voltage. The plate of the tube is connected to this end of R_L and is therefore at the same minimum instantaneous potential.

This polarity reversal between instantaneous grid and plate voltages is further clarified by a consideration of Kirchhoff's law as it applies to series resistance. The sum of the IR drops around the plate circuit must at all times equal the supply voltage of 300 volts. Thus when the instantaneous voltage drop across R_L is maximum, the voltage drop across the tube is minimum, and their sum must equal 300 volts. The variations of grid voltage,plate current and plate voltage about their steady state values is illustrated in figure 14.

Interelectrode Capacitance Capacitance always exists between any two pieces of metal separated by a dielectric. The exact amount of capacitance depends upon the size of the metal pieces, the dielectric between them, and the type of dielectric. The electrodes of a vacuum tube have a similar characteristic known as the *interelectrode capacitance*, illustrated in figure 15. These direct capacities in a triode are: grid-to-cathode capacitance, grid-to-plate capacitance, and plate-to-cathode capacitance. The interelectrode capacitance, though very small, has a coupling effect, and often can cause unbalance in a particular circuit. At very high

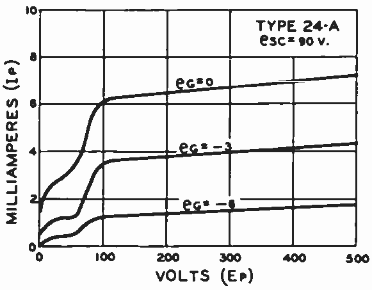


Figure 16

TYPICAL I_p VS. E_p TETRODE CHARACTERISTIC CURVES

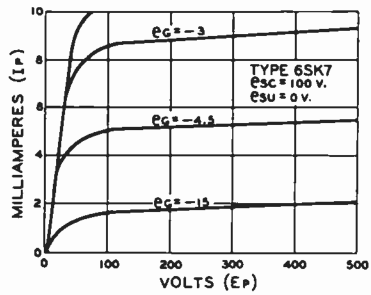


Figure 17

TYPICAL I_p VS. E_p PENTODE CHARACTERISTIC CURVES

frequencies (v-h-f), interelectrode capacities become very objectionable and prevent the use of conventional tubes at these frequencies. Special v-h-f tubes must be used which are characterized by very small electrodes and close internal spacing of the elements of the tube.

4-4 Tetrode or Screen Grid Tubes

Many desirable characteristics can be obtained in a vacuum tube by the use of more than one grid. The most common multi-element tube is the tetrode (four electrodes). Other tubes containing as many as eight electrodes are available for special applications.

The Tetrode The quest for a simple and easily usable method of eliminating the effects of the grid-to-plate capacitance of the triode led to the development of the *screen-grid* tube or *tetrode.* When another grid is added between the grid and plate of a vacuum tube the tube is called a tetrode, and because the new grid is called a *screen,* as a result of its screening or shielding action, the tube is often called a screen-grid tube. The interposed screen grid acts as an electrostatic shield between the grid and plate, with the consequence that the grid-to-plate capacitance is reduced. Although the screen grid is maintained at a positive voltage with respect to the cathode of the tube, it is maintained at ground potential with respect to r.f. by means of a by-pass capacitor of very low reactance at the frequency of operation.

In addition to the shielding effect, the screen grid serves another very useful purpose. Since the screen is maintained at a positive potential, it serves to increase or accelerate the flow of electrons to the plate. There being large openings in the screen mesh, most of the electrons pass through it and on to the plate. Due also to the screen, the plate current is largely independent of plate voltage, thus making for high amplification. When the screen voltage is held at a constant value, it is possible to make large changes in plate voltage without appreciably affecting the plate current, (figure 16).

When the electrons from the cathode approach the plate with sufficient velocity, they dislodge electrons upon striking the plate. This effect of *bombarding* the plate with high velocity electrons, with the consequent dislodgement of other electrons from the plate, gives rise to the condition of secondary emission which has been discussed in a previous paragraph. This effect can cause no particular difficulty in a triode because the secondary electrons so emitted are eventually attracted back to the plate. In the screen-grid tube, however, the screen is close to the plate and is maintained at a positive potential. Thus, the screen will attract these electrons which have been knocked from the plate, particularly when the plate voltage falls to a lower value than the screen voltage, with the result that the plate current is lowered and the amplification is decreased.

In the application of tetrodes, it is necessary to operate the plate at a high voltage in relation to the screen in order to overcome these effects of *secondary emission.*

The Pentode The undesirable effects of secondary emission from the plate can be greatly reduced if yet another element is added between the screen and plate. This additional element is called a *suppressor,* and tubes in which it is used are called *pentodes.* The suppressor grid is sometimes connected to the cathode within the tube; sometimes it is brought out to a connecting pin on the tube base, but in any case it is established nega-

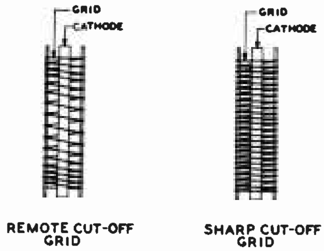


Figure 18
REMOTE CUTOFF GRID STRUCTURE

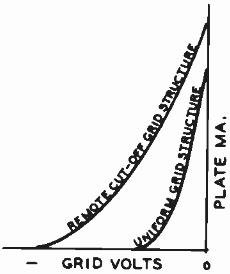


Figure 19
ACTION OF A REMOTE CUTOFF GRID STRUCTURE

tive with respect to the minimum plate voltage. The secondary electrons that would travel to the screen if there were no suppressor are diverted back to the plate. The plate current is, therefore, not reduced and the amplification possibilities are increased (figure 17).

Pentodes for audio applications are designed so that the suppressor increases the limits to which the plate voltage may swing; therefore the consequent power output and gain can be very great. Pentodes for radio-frequency service function in such a manner that the suppressor allows high voltage gain, at the same time permitting fairly high gain at low plate voltage. This holds true even if the plate voltage is the same or slightly lower than the screen voltage.

Remote Cutoff Tubes *Remote cutoff* tubes (variable mu) are screen grid tubes in which the control grid structure has been physically modified so as to cause the plate current of the tube to drop off gradually, rather than to have a well defined cutoff point (figure 18). A non-uniform control grid structure is used, so that the amplification factor is different for different parts of the control grid.

Remote cutoff tubes are used in circuits where it is desired to control the amplification by varying the control grid bias. The characteristic curve of an ordinary screen grid tube has considerable curvature near the plate current cutoff point, while the curve of a remote cutoff tube is much more linear (figure 19). The remote cutoff tube minimizes cross-talk interference that would otherwise be produced. Examples of remote cutoff tubes are: 6BD6, 6K7, 6SG7 and 6SK7.

Beam Power Tubes A beam power tube makes use of another method for suppressing secondary emission. In this tube there are four electrodes: a cathode, a grid, a screen, and a plate, so spaced and placed that secondary emission from the plate is suppressed without actual power loss. Because of the manner in which the electrodes are spaced, the electrons which travel to the plate are slowed down when the plate voltage is low, almost to zero velocity in a certain region between screen and plate. For this reason the electrons form a stationary cloud, or *space charge*. The effect of this space charge is to repel secondary electrons emitted from the plate and thus cause them to return to the plate. In this way, secondary emission is suppressed.

Another feature of the beam power tube is the low current drawn by the screen. The screen and the grid are spiral wires wound so that each turn in the screen is shaded from the cathode by a grid turn. This alignment of the screen and the grid causes the electrons to travel in sheets between the turns of the screen so that very few of them strike the screen itself. This formation of the electron stream into sheets or beams increases the charge density in the screen-plate region and assists in the creation of the space charge in this region.

Because of the effective suppressor action provided by the space charge, and because of the low current drawn by the screen, the beam power tube has the advantages of high power output, high power-sensitivity, and high efficiency. The 6L6 is such a beam power tube, designed for use in the power amplifier stages of receivers and speech amplifiers or modulators. Larger tubes employing the beam-power principle are being made by various manufacturers for use in the radio-frequency stages of transmitters. These tubes feature extremely high power-sensitivity (a very small amount of driving power is required for a large output), good plate efficiency, and low grid-to-plate capacitance. Examples of these tubes are 813, 4-250A, 4X150A, etc.

Grid-Screen Mu Factor The *grid-screen mu factor* (μ_{sg}) is analogous to the amplification factor in a triode, except that the screen of a pentode or tetrode is substituted for the plate of a triode. μ_{sg} denotes the ratio of a change in grid voltage to a change in screen voltage, each of which will produce the same change in screen current. Expressed as an equation:

$$\mu_{sg} = \frac{\Delta E_{sg}}{\Delta E_g} \quad I_{sg} = \text{constant}, \Delta = \text{small increment}$$

The grid-screen mu factor is important in determining the operating bias of a tetrode or pentode tube. The relationship between control-grid potential and screen potential determines the plate current of the tube as well as the screen current since the plate current is essentially independent of the plate voltage in tubes of this type. In other words, when the tube is operated at cutoff bias as determined by the screen voltage and the grid-screen mu factor (determined in the same way as with a triode, by dividing the operating voltage by the mu factor) the plate current will be substantially at cutoff, as will be the screen current. The grid-screen mu factor is numerically equal to the amplification factor of the same tetrode or pentode tube when it is triode connected.

Current Flow in Tetrodes and Pentodes The following equation is the expression for total cathode current in a triode tube. The expression for the total cathode current of a tetrode and a pentode tube is the same, except that the screen-grid voltage and the grid-screen μ-factor are used in place of the plate voltage and μ of the triode.

$$\text{Cathode current} = K\left(E_g + \frac{E_{sg}}{\mu_{sg}}\right)^{3/2}$$

Cathode current, of course, is the sum of the screen and plate current, plus control grid current in the event that the control grid is positive with respect to the cathode. It will be noted that total *cathode* current is independent of plate voltage in a tetrode or pentode. Also, in the usual tetrode or pentode the *plate* current is substantially independent of plate voltage over the usual operating range— which means simply that the effective plate resistance of such tubes is relatively high. However, when the plate voltage falls below the normal operating range, the plate current falls sharply, while the screen current rises to such a value that the total cathode current remains substantially constant. Hence, the screen grid in a tetrode or pentode will almost invariably be damaged by excessive dissipation if the plate voltage is removed while the screen voltage is still being applied from a low-impedance source.

The Effect of Grid Current The current equations show how the total cathode current in triodes, tetrodes, and pentodes is a function of the potentials applied to the various electrodes. If only one electrode is positive with respect to the cathode (such as would be the case in a triode acting as a class A amplifier) all the cathode current goes to the plate. But when both screen and plate are positive in a tetrode or pentode, the cathode current divides between the two elements. Hence the screen current is taken from the total cathode current, while the balance goes to the plate. Further, if the control grid in a tetrode or pentode is operated at a positive potential the total cathode current is divided between all three elements which have a positive potential. In a tube which is receiving a large excitation voltage, it may be said that the control grid robs electrons from the output electrode during the period that the grid is positive, making it always necessary to limit the peak-positive excursion of the control grid.

Coefficients of Tetrodes and Pentodes In general it may be stated that the amplification factor of tetrode and pentode tubes is a coefficient which is not of much use to the designer. In fact the amplification factor is seldom given on the design data sheets of such tubes. Its value is usually very high, due to the relatively high plate resistance of such tubes, but bears little relationship to the stage gain which actually will be obtained with such tubes.

On the other hand, the *grid-plate transconductance* is the most important coefficient of pentode and tetrode tubes. Gain per stage can be computed directly when the G_m is known. The grid-plate transconductance of a tetrode or pentode tube can be calculated through use of the expression:

$$G_m = \frac{\Delta I_p}{\Delta E_g}$$

with E_{sg} and E_p constant.

The plate resistance of such tubes is of less importance than in the case of triodes, though it is often of value in determining the amount of damping a tube will exert upon the impedance in its plate circuit. Plate resistance is calculated from:

$$R_p = \frac{\Delta E_p}{\Delta I_p}$$

with E_g and E_{sg} constant.

4-5 Mixer and Converter Tubes

The superheterodyne receiver always in-

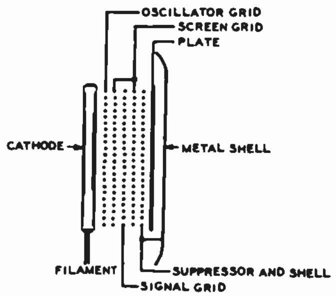


Figure 20
GRID STRUCTURE OF 6SA7 CONVERTER TUBE

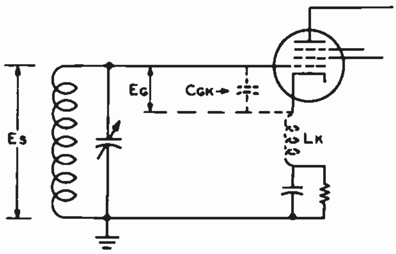


Figure 21
SHOWING THE EFFECT OF CATHODE LEAD INDUCTANCE

The degenerative action of cathode lead inductance tends to reduce the effective grid-to-cathode voltage with respect to the voltage available across the input tuned circuit. Cathode lead inductance also introduces undesirable coupling between the input and the output circuits.

cludes at least one stage for changing the frequency of the incoming signal to the fixed frequency of the main intermediate amplifier in the receiver. This frequency changing process is accomplished by selecting the beat-note difference frequency between a locally generated oscillation and the incoming signal frequency. If the oscillator signal is supplied by a separate tube, the frequency changing tube is called a *mixer*. Alternatively, the oscillation may be generated by additional elements within the frequency changer tube. In this case the frequency changer is commonly called a *converter* tube.

Conversion Conductance The *conversion conductance* (G_c) is a coefficient of interest in the case of mixer or converter tubes, or of conventional triodes, tetrodes, or pentodes operating as frequency changers. The conversion conductance is the ratio of a change in the signal-grid voltage at the input frequency to a change in the output current at the converted frequency. Hence G_c in a mixer is essentially the same as transconductance in an amplifier, with the exception that the input signal and the output current are on different frequencies. The value of G_c in conventional mixer tubes is from 300 to 1000 micromhos. The value of G_c in an amplifier tube operated as a mixer is approximately 0.3 the G_m of the tube operated as an amplifier. The voltage gain of a mixer stage is equal to $G_c Z_L$ where Z_L is the impedance of the plate load into which the mixer tube operates.

The Diode Mixer The simplest mixer tube is the diode. The noise figure, or figure of merit, for a mixer of this type is not as good as that obtained with other more complex mixers; however, the diode is useful as a mixer in u-h-f and v-h-f equipment where low interelectrode capacities are vital to circuit operation. Since the diode impedance is low, the local oscillator must furnish considerable power to the diode mixer. A good diode mixer has an overall gain of about 0.5.

The Triode Mixer A triode mixer has better gain and a better noise figure than the diode mixer. At low frequencies, the gain and noise figure of a triode mixer closely approaches those figures obtained when the tube is used as an amplifier. In the u-h-f and v-h-f range, the efficiency of the triode mixer deteriorates rapidly. The optimum local oscillator voltage for a triode mixer is about 0.7 as large as the cutoff bias of the triode. Very little local oscillator power is required by a triode mixer.

Pentode Mixers and Converter Tubes The most common multigrid converter tube for broadcast or shortwave use is the *penta grid converter*, typified by the 6SA7, 6SB7-Y and 6BA7 tubes (figure 20). Operation of these converter tubes and pentode mixers will be covered in the Receiver Fundamentals Chapter.

4-6 Electron Tubes at Very High Frequencies

As the frequency of operation of the usual type of electron tube is increased above about 20 Mc., certain assumptions which are valid for operation at lower frequencies must be re-examined. First, we find that lead inductances from the socket connections to the actual elements within the envelope no longer are negligible. Second, we find that electron transit time no longer may be ignored; an appreciable fraction of a cycle of input signal may be required for an electron to leave the cathode space charge, pass through the grid wires, and travel through the space between grid and plate.

Effects of Lead Inductance The effect of lead inductance is two-fold. First, as shown in figure 21, the combination of grid-lead inductance, grid-cathode capacitance, and cathode lead inductance tends to reduce the effective grid-cathode signal voltage for a constant voltage at the tube terminals as the frequency is increased. Second, cathode lead inductance tends to introduce undesired coupling between the various elements within the tube.

Tubes especially designed for v-h-f and u-h-f use have had their lead inductances minimized. The usual procedures for reducing lead inductance are: (1) using heavy lead conductors or several leads in parallel (examples are the 6SH7 and 6AK5), (2) scaling down the tube in all dimensions to reduce both lead inductances and interelectrode capacitances (examples are the 6AK5, 6F4, and other acorn and miniature tubes), and (3) the use of very low inductance extensions of the elements themselves as external connections (examples are lighthouse tubes such as the 2C40, oilcan tubes such as the 2C29, and many types of v-h-f transmitting tubes).

Effect of Transit Time When an electron tube is operated at a frequency high enough that electron transit time between cathode and plate is an appreciable fraction of a cycle at the input frequency, several undesirable effects take place. First, the grid takes power from the input signal even though the grid is negative at all times. This comes about since the grid will have changed its potential during the time required for an electron to pass from cathode to plate. Due to interaction, and a resulting phase difference between the field associated with the grid and that associated with a moving electron, the grid presents a resistance to an input signal in addition to its normal "cold" capacitance. Further, as a result of this action, plate current no longer is in phase with grid voltage.

An amplifier stage operating at a frequency high enough that transit time is appreciable:

(a) Is difficult to excite as a result of grid loss from the equivalent input grid resistance,

(b) Is capable of less output since transconductance is reduced and plate current is not in phase with grid voltage.

The effects of transit time increase with the square of the operating frequency, and they increase rapidly as frequency is increased above the value where they become just appreciable. These effects may be reduced by scaling down tube dimensions; a procedure which also reduces lead inductance. Further, transit-time effects may be reduced by the obvious procedure of increasing electrode potentials so that electron velocity will be increased. However, due to the law of electron-motion in an electric field, transit time is increased only as the square root of the ratio of operating potential increase; therefore this expedient is of limited value due to other limitations upon operating voltages of small electron tubes.

4-7 Special Microwave Electron Tubes

Due primarily to the limitation imposed by transit time, conventional negative-grid electron tubes are capable of affording worthwhile amplification and power output only up to a definite upper frequency. This upper frequency limit varies from perhaps 100 Mc. for conventional tube types to about 4000 Mc. for specialized types such as the lighthouse tube. Above the limiting frequency, the conventional negative-grid tube no longer is practicable and recourse must be taken to totally different types of electron tubes in which electron transit time is not a limitation to operation. Three of the most important of such microwave tube types are the ***klystron***, the ***magnetron***, and the ***travelling wave tube***.

The Power Klystron The klystron is a type of electron tube in which electron transit time is used to advantage, Such tubes comprise, as shown in figure 22, a cathode, a focussing electrode, a resonator connected to a pair of grids which afford *velocity modulation* of the electron beam (called the "buncher"), a *drift space*, and another resonator connected to a pair of grids (called the "catcher"). A *collector* for the expended electrons may be included at the end of the tube, or the catcher may also perform the function of electron collection.

The tube operates in the following manner: The cathode emits a stream of electrons which is focussed into a beam by the focussing electrode. The stream passes through the buncher where it is acted upon by any field existing between the two grids of the buncher cavity. When the potential between the two grids is zero, the stream passes through without change in velocity. But when the potential between the two grids of the buncher is increasingly positive in the direction of electron

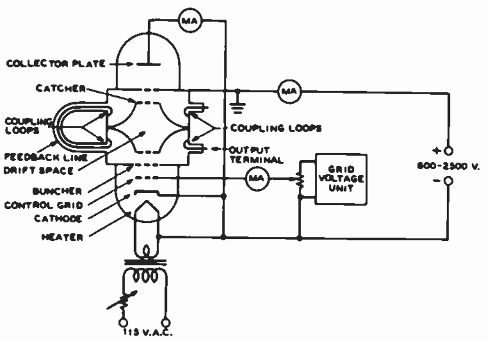


Figure 22

TWO-CAVITY KLYSTRON OSCILLATOR

A conventional two-cavity klystron is shown with a feedback loop connected between the two cavities so that the tube may be used as an oscillator.

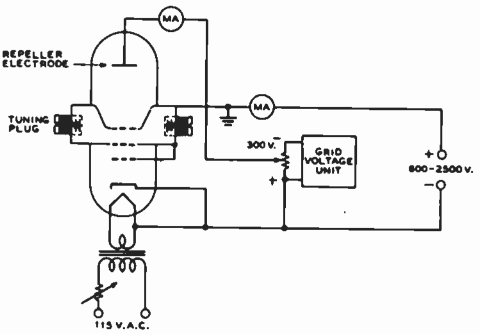


Figure 23

REFLEX KLYSTRON OSCILLATOR

A conventional reflex klystron oscillator of the type commonly used as a local oscillator in superheterodyne receivers operating above about 2000 Mc. is shown above. Frequency modulation of the output frequency of the oscillator, or a-f-c operation in a receiver, may be obtained by varying the negative voltage on the repeller electrode.

motion, the velocity of the electrons in the beam is increased. Conversely, when the field becomes increasingly negative in the direction of the beam (corresponding to the other half cycle of the exciting voltage from that which produced electron acceleration) the velocity of the electrons in the beam is decreased.

When the velocity-modulated electron beam reaches the drift space, where there is no field, those electrons which have been sped up on one half-cycle overtake those immediately ahead which were slowed down on the other half-cycle. In this way, the beam electrons become bunched together. As the bunched groups pass through the two grids of the catcher cavity, they impart pulses of energy to these grids. The catcher grid-space is charged to different voltage levels by the passing electron bunches, and a corresponding oscillating field is set up in the catcher cavity. The catcher is designed to resonate at the frequency of the velocity-modulated beam, or at a harmonic of this frequency.

In the klystron amplifier, energy delivered by the buncher to the catcher grids is greater than that applied to the buncher cavity by the input signal. In the klystron oscillator a feedback loop connects the two cavities. Coupling to either buncher or catcher is provided by small loops which enter the cavities by way of concentric lines.

The klystron is an electron-coupled device. When used as an oscillator, its output voltage is rich in harmonics. Klystron oscillators of various types afford power outputs ranging from less than 1 watt to many thousand watts. Operating efficiency varies between 5 and 30 per cent. Frequency may be shifted to some extent by varying the beam voltage. Tuning is carried on mechanically in some klystrons by altering (by means of knob settings) the shape of the resonant cavity.

The Reflex Klystron The two-cavity klystron as described in the preceding paragraphs is primarily used as a transmitting device since quite reasonable amounts of power are made available in its output circuit. However, for applications where a much smaller amount of power is required — power levels in the milliwatt range — for low-power transmitters, receiver local oscillators, etc., another type of klystron having only a single cavity is more frequently used.

The theory of operation of the single-cavity klystron is essentially the same as the multicavity type with the exception that the velocity-modulated electron beam, after having left the "buncher" cavity is reflected back into the area of the buncher again by a repeller electrode as illustrated in figure 23. The potentials on the various electrodes are adjusted to the value such that proper bunching of the electron beam will take place just as a particular portion of the velocity-modulated beam reenters the area of the resonant cavity. Since this type of klystron has only one circuit it can be used only as an oscillator and not as an amplifier. Effective modulation of the frequency of a single-cavity klystron for FM work can be obtained by modulating the repeller electrode voltage.

Figure 24
THE 723 A/B TUNABLE KLYSTRON TUBE
The tuning vane visible on the left side of the tube allows the volume of the tuning cavity to be varied by means of thin, flexible diaphragms within the metal shell of the klystron tube.

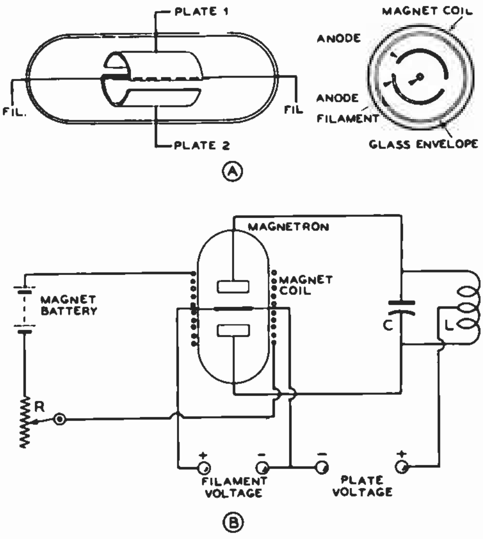


Figure 25
SIMPLE MAGNETRON OSCILLATOR
An external tank circuit is used with this type of magnetron oscillator for operation in the lower u-h-f range.

The Magnetron The magnetron is an s-h-f oscillator tube normally employed where very high values of peak power or moderate amounts of average power are required in the range from perhaps 700 Mc. to 30,000 Mc. Special magnetrons were developed for wartime use in radar equipments which had peak power capabilities of several million watts (megawatts) output at frequencies in the vicinity of 3000 Mc. The normal duty cycle of operation of these radar equipments was approximately 1/10 of one per cent (the tube operated about 1/1000 of the time and rested for the balance of the operating period) so that the average power output of these magnetrons was in the vicinity of 1000 watts.

In its simplest form the magnetron tube is a filament-type diode with two half-cylindrical plates or anodes situated coaxially with respect to the filament. The construction is illustrated in figure 25A. The anodes of the magnetron are connected to a resonant circuit as illustrated on figure 25B. The tube is surrounded by an electromagnet coil which, in turn, is connected to a low-voltage d-c energizing source through a rheostat R for controlling the strength of the magnetic field. The field coil is oriented so that the lines of magnetic force it sets up are parallel to the axis of the electrodes.

Under the influence of the strong magnetic field, electrons leaving the filament are deflected from their normal paths and move in circular orbits within the anode cylinder. This effect results in a negative resistance which sustains oscillations. The oscillation frequency is very nearly the value determined by L and C. In other magnetron circuits, the frequency may be governed by the electron rotation, no external tuned circuits being employed. Wavelengths of less than 1 centimeter have been produced with such circuits.

More complex magnetron tubes employ no external tuned circuit, but utilize instead one or more resonant cavities which are integral with the anode structure. Figure 26 shows a magnetron of this type having a multi-cellular

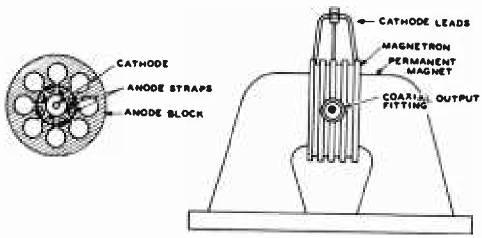


Figure 26
MODERN MULTI-CAVITY MAGNETRON
Illustrated is an external-anode strapped magnetron of the type commonly used in radar equipment for the 10-cm. range. A permanent magnet of the general type used with such a magnetron is shown in the right-hand portion of the drawing, with the magnetron in place between the pole pieces of the magnet.

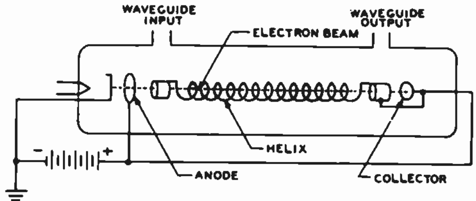


Figure 27
THE TRAVELLING WAVE TUBE
Operation of this tube is the result of interaction between the electron beam and wave travelling along the helix.

anode of eight cavities. It will be noted, also, that alternate cavities (which would operate at the same polarity when the tube is oscillating) are strapped together. Strapping was found to improve the efficiency and stability of high-power radar magnetrons. In most radar applications of magnetron oscillators a powerful permanent magnet of controlled characteristics is employed to supply the magnetic field rather than the use of an electromagnet.

The Travelling Wave Tube The *Travelling Wave Tube* (figure 27) consists of a helix located within an evacuated envelope. Input and output terminations are affixed to each end of the helix. An electron beam passes through the helix and interacts with a wave travelling along the helix to produce broad band amplification at microwave frequencies.

When the input signal is applied to the gun end of the helix, it travels along the helix wire at approximately the speed of light. However, the signal velocity measured along the axis of the helix is considerably lower. The electrons emitted by the cathode gun pass axially through the helix to the collector, located at the output end of the helix. The average velocity of the electrons depends upon the potential of the collector with respect to the cathode. When the average velocity of the electrons is greater than the velocity of the helix wave, the electrons become crowded together in the various regions of retarded field, where they impart energy to the helix wave. A power gain of 100 or more may be produced by this tube.

4-8 The Cathode-Ray Tube

The Cathode-Ray Tube The *cathode-ray tube* is a special type of electron tube which permits the visual observation of electrical signals. It may be incorporated into an oscilloscope for use as a test instrument or it may be the display device for radar equipment or a television receiver.

Operation of the CRT A cathode-ray tube always includes an electron gun for producing a stream of electrons, a grid for controlling the intensity of the electron beam, and a luminescent screen for converting the impinging electron beam into visible light. Such a tube always operates in conjunction with either a built-in or an external means for focussing the electron stream into a narrow beam, and a means for deflecting the electron beam in accordance with an electrical signal.

The main electrical difference between types of cathode-ray tubes lies in the means employed for focussing and deflecting the electron beam. The beam may be focussed and/or deflected either electrostatically or magnetically, since a stream of electrons can be acted upon either by an electrostatic or a magnetic field. In an electrostatic field the electron beam tends to be deflected toward the positive termination of the field (figure 28). In a magnetic field the stream tends to be deflected at right angles to the field. Further, an electron beam tends to be deflected so that it is normal (perpendicular) to the equipotential lines of an electrostatic field — and it tends to be deflected so that it is parallel to the lines of force in a magnetic field.

Large cathode-ray tubes used as *kinescopes* in television receivers usually are both focused and deflected magnetically. On the other hand, the medium-size CR tubes used in oscilloscopes and small television receivers usually are both focused and deflected electrostatically. But CR tubes for special applications may be focused magnetically and deflected electrostatically or vice versa.

There are advantages and disadvantages to

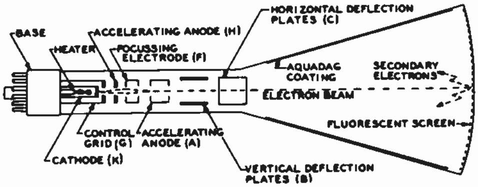


Figure 28
TYPICAL ELECTROSTATIC CATHODE-RAY TUBE

both types of focussing and deflection. However, it may be stated that electrostatic deflection is much better than magnetic deflection when high-frequency waves are to be displayed on the screen; hence the almost universal use of this type of deflection for oscillographic work. But when a tube is operated at a high value of accelerating potential so as to obtain a bright display on the face of the tube as for television or radar work, the use of magnetic deflection becomes desirable since it is relatively easier to deflect a high-velocity electron beam magnetically than electrostatically. However, an *ion trap* is required with magnetic deflection since the heavy negative ions emitted by the cathode are not materially deflected by the magnetic field and hence would burn an "ion spot" in the center of the luminescent screen. With electrostatic deflection the heavy ions are deflected equally as well as the electrons in the beam so that an ion spot is not formed.

Construction of Electrostatic CRT The construction of a typical electrostatic-focus, electrostatic-deflection cathode-ray tube is illustrated in the pictorial diagram of figure 28. The *indirectly heated cathode* K releases free electrons when heated by the enclosed filament. The cathode is surrounded by a cylinder G, which has a small hole in its front for the passage of the electron stream. Although this element is not a wire mesh as is the usual grid, it is known by the same name because its action is similar: it controls the electron stream when its negative potential is varied.

Next in order, is found the first *accelerating anode*, H, which resembles another disk or cylinder with a small hole in its center. This electrode is run at a high or moderately high positive voltage, to accelerate the electrons towards the far end of the tube.

The *focussing electrode*, F, is a sleeve which usually contains two small disks, each with a small hole.

After leaving the focussing electrode, the electrons pass through another *accelerating anode*, A, which is operated at a high positive potential. In some tubes this electrode is operated at a higher potential than the first accelerating electrode, H, while in other tubes both accelerating electrodes are operated at the same potential.

The electrodes which have been described up to this point constitute the *electron gun*, which produces the free electrons and focusses them into a slender, concentrated, rapidly-traveling stream for projecting onto the viewing screen.

Electrostatic Deflection To make the tube useful, means must be provided for deflecting the electron beam along two axes at right angles to each other. The more common tubes employ *electrostatic deflection plates*, one pair to exert a force on the beam in the vertical plane and one pair to exert a force in the horizontal plane. These plates are designated as B and C in figure 28.

Standard oscilloscope practice with small cathode-ray tubes calls for connecting one of the B plates and one of the C plates together and to the high voltage accelerating anode. With the newer three-inch tubes and with five-inch tubes and larger, all four deflecting plates are commonly used for deflection. The *positive* high voltage is grounded, instead of the negative as is common practice in amplifiers, etc., in order to permit operation of the deflecting plates at a d-c potential at or near ground.

An *Aquadag* coating is applied to the inside of the envelope to attract any secondary electrons emitted by the flourescent screen.

In the average electrostatic-deflection CR tube the spot will be fairly well centered if all four deflection plates are returned to the potential of the second anode (ground). However, for accurate centering and to permit moving the entire trace either horizontally or vertically to permit display of a particular waveform, horizontal and vertical centering controls usually are provided on the front of the oscilloscope.

After the spot is once centered, it is necessary only to apply a positive or negative voltage (with respect to ground) to one of the ungrounded or "free" deflector plates in order to move the spot. If the voltage is positive with respect to ground, the beam will be attracted toward that deflector plate, while if negative the beam and spot will be repulsed. The amount of deflection is directly proportional to the voltage (with respect to ground) that is applied to the free electrode.

With the larger-screen higher-voltage tubes it becomes necessary to place deflecting voltage on both horizontal and both vertical plates. This is done for two reasons: First, the amount of deflection voltage required by the high-

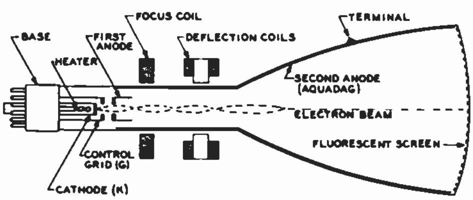


Figure 29
TYPICAL ELECTROMAGNETIC CATHODE-RAY TUBE

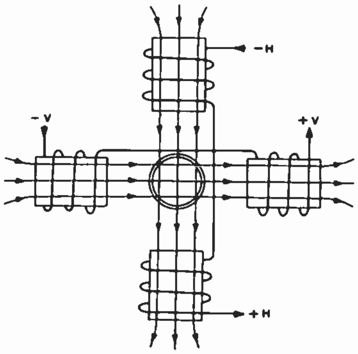


Figure 30
Two pairs of coils arranged for electromagnetic deflection in two directions.

voltage tubes is so great that a transmitting tube operating from a high voltage supply would be required to attain this voltage without distortion. By using push-pull deflection with two tubes feeding the deflection plates, the necessary plate supply voltage for the deflection amplifier is halved. Second, a certain amount of de-focussing of the electron stream is always present on the extreme excursions in deflection voltage when this voltage is applied only to one deflecting plate. When the deflecting voltage is fed in push-pull to both deflecting plates in each plane, there is no defocussing because the *average* voltage acting on the electron stream is zero, even though the *net* voltage (which causes the deflection) acting on the stream is twice that on either plate.

The fact that the beam is deflected by a magnetic field is important even in an oscilloscope which employs a tube using electrostatic deflection, because it means that precautions must be taken to protect the tube from the transformer fields and sometimes even the earth's magnetic field. This normally is done by incorporating a magnetic shield around the tube and by placing any transformers as far from the tube as possible, oriented to the position which produces minimum effect upon the electron stream.

Construction of Electromagnetic CRT The electromagnetic cathode-ray tube allows greater definition than does the electrostatic tube. Also, electromagnetic definition has a number of advantages when a rotating radial sweep is required to give polar indications.

The production of the electron beam in an electromagnetic tube is essentially the same as in the electrostatic tube. The grid structure is similar, and controls the electron beam in an identical manner. The elements of a typical electromagnetic tube are shown in figure 29. The *focus coil* is wound on an iron core which may be moved along the neck of the tube to focus the electron beam. For final adjustment, the current flowing in the coil may be varied. A second pair of coils, the *deflection coils* are mounted at right angles to each other around the neck of the tube. In some cases, these coils can rotate around the axis of the tube.

Two *anodes* are used for accelerating the electrons from the cathode to the screen. The second anode is a graphite coating (Aquadag) on the inside of the glass envelope. The function of this coating is to attract any secondary electrons emitted by the flourescent screen, and also to shield the electron beam.

In some types of electromagnetic tubes, a first, or *accelerating anode* is also used in addition to the Aquadag.

Electromagnetic Deflection A magnetic field will deflect an electron beam in a direction which is at right angles to both the direction of the field and the direction of motion of the beam.

In the general case, two pairs of deflection coils are used (figure 30). One pair is for horizontal deflection, and the other pair is for vertical deflection. The two coils in a pair are connected in series and are wound in such directions that the magnetic field flows from one coil, through the electron beam to the other coil. The force exerted on the beam by the field moves it to any point on the screen by application of the proper currents to these coils.

The Trace The human eye retains an image for about one-sixteenth second after viewing. In a CRT, the spot can be moved so quickly that a series of adjacent spots can be made to appear as a line, if the beam is swept over the path fast enough. As long as the electron beam strikes in a given place at least sixteen times a second, the spot will appear to the human eye as a source of continuous light with very little flicker.

Screen Materials — "Phosphors" At least five types of luminescent screen materials are commonly available on the various types of CR tubes commercially available. These screen materials are called *phosphors;* each of the five phosphors is best suited to a particular type of application. The P-1 phosphor, which has a green flourescence with medium persistence, is almost invariably used for oscilloscope tubes for visual observation. The P-4 phosphor, with white fluorescence and medium persistence, is used on television viewing tubes ("Kinescopes"). The P-5 and P-11 phosphors, with blue fluorescence and very short persistence, are used primarily in oscilloscopes where photographic recording of the trace is to be obtained. The P-7 phosphor, which has a blue flash and a long-persistence greenish-yellow persistence, is used primarily for radar displays where retention of the image for several seconds after the initial signal display is required.

4-9 Gas Tubes

The space charge of electrons in the vicinity of the cathode in a diode causes the plate-to-cathode voltage drop to be a function of the current being carried between the cathode and the plate. This voltage drop can be rather high when large currents are being passed, causing a considerable amount of energy loss which shows up as plate dissipation.

Action of Positive Ions The negative space charge can be neutralized by the presence of the proper density of positive ions in the space between the cathode and anode. The positive ions may be obtained by the introduction of the proper amount of gas or a small amount of mercury into the envelope of the tube. When the voltage drop across the tube reaches the ionization potential of the gas or mercury vapor, the gas molecules will become ionized to form positive ions. The positive ions then tend to neutralize the space charge in the vicinity of the cathode. The voltage drop across the tube then remains constant at the ionization potential of the gas up to a current drain equal to the maximum emission capability of the cathode. The voltage drop varies between 10 and 20 volts, depending upon the particular gas employed, up to the maximum current rating of the tube.

Mercury Vapor Tubes Mercury-vapor tubes, although very widely used, have the disadvantage that they must be operated within a specific temperature range (25° to 70° C.) in order that the mercury vapor pressure within the tube shall be within the proper range. If the temperature is too low, the drop across the tube becomes too high causing immediate overheating and possible damage to the elements. If the temperature is too high, the vapor pressure is too high, and the voltage at which the tube will "flash back" is lowered to the point where destruction of the tube may take place. Since the ambient temperature range specified above is within the normal room temperature range, no trouble will be encountered under normal operating conditions. However, by the substitution of xenon gas for mercury it is possible to produce a rectifier with characteristics comparable to those of the mercury-vapor tube except that the tube is capable of operating over the range from approximately –70° to 90° C. The 3B25 rectifier is an example of this type of tube.

Thyratron Tubes If a grid is inserted between the cathode and plate of a mercury-vapor gaseous-conduction rectifier, a negative potential placed upon the added element will increase the plate-to-cathode voltage drop required before the tube will ionize or "fire." The potential upon the control grid will have no effect on the plate-to-cathode drop after the tube has ionized. However, the grid voltage may be adjusted to such a value that conduction will take place only over the desired portion of the cycle of the a-c voltage being impressed upon the plate of the rectifier.

Voltage Regulator Tubes In a glow-discharge gas tube the voltage drop across the electrodes remains constant over a wide range of current passing through the tube. This property exists because the degree of ionization of the gas in the tube varies with the amount of current passing through the tube. When a large current is passed, the gas is highly ionized and the internal impedance of the tube is low. When a small current is passed, the gas is lightly ionized and the internal impedance of the tube is high. Over the operating range of the tube, the product (IR) of the current through the tube and the internal impedance of the tube is very nearly constant. Examples of this type of tube are VR-150, VR-105 and the old 874.

Vacuum Tube Classification Vacuum tubes are grouped into three major classifications: commercial, ruggedized, and premium (or reliable). Any one of these three groups may also be further classified for military duty (JAN classification). To qualify for JAN classification, sample lots of the particular tube must have passed special qualification tests at the factory. It should not be construed that a JAN-type tube is better than a commercial tube, since some commercial tests and specifications are more rigid than the corresponding JAN specifications. The JAN-stamped tube has merely been accepted under a certain set of conditions for military service.

Ruggedized or Premium Tubes Radio tubes are being used in increasing numbers for industrial applications, such as computing and control machinery, and in aviation and marine equipment. When a tube fails in a home radio receiver, it is merely inconvenient, but a tube failure in industrial applications may bring about stoppage of some vital process, resulting in financial loss, or even danger to life.

To meet the demands of these industrial applications, a series of tubes was evolved incorporating many special features designed to ensure a long and pre-determined operating life, and uniform characteristics among similar tubes. Such tubes are known as *ruggedized* or *premium* tubes. Early attempts to select reliable specimens of tubes from ordinary stock tubes proved that in the long run the selected tubes were no better than tubes picked at random. Long life and ruggedness had to be built into the tubes by means of proper choice and 100% inspection of all materials used in the tube, by critical processing inspection and assembling, and by conservative ratings of the tube.

Pure tungsten wire is used for heaters in preference to alloys of lower tensile strength. Nickel tubing is employed around the heater wires at the junction to the stem wires to reduce breakage at this point. Element structures are given extra supports and bracing. Finally, all tubes are given a 50 hour test run under full operating conditions to eliminate early failures. When operated within their ratings, ruggedized or premium tubes should provide a life well in excess of 10,000 hours.

Ruggedized tubes will withstand severe impact shocks for short periods, and will operate under conditions of vibration for many hours. The tubes may be identified in many cases by the fact that their nomenclature includes a "W" in the type number, as in 807W, 5U4W, etc. Some ruggedized tubes are included in the "5000" series nomenclature. The 5654 is a ruggedized version of the 6AK5, the 5692 is a ruggedized version of the 6SN7, etc.

CHAPTER FIVE

Semi-Conductors

One of the earliest detection devices used in radio was the galena crystal, a crude example of a *semiconductor*. More modern examples of semiconductors are the copper-oxide rectifier, the selenium rectifier and the germanium diode. All of these devices offer the interesting property of greater resistance to the flow of electrical current in one direction than in the opposite direction. Typical conduction curves for these semiconductors are shown in Figure 1. The copper oxide rectifier action results from the function of a thin film of cuprous oxide formed upon a pure copper disc. This film offers low resistance for positive voltages, and high resistance for negative voltages. The same action is observed in selenium rectifiers, where a film of selenium is deposited on an iron surface.

5-1 Atomic Structure of Germanium and Silicon

It has been previously stated that the electrons in an element having a large atomic number are grouped into rings, each ring having a definite number of electrons. Atoms in which these rings are completely filled are called *inert gases*, of which helium and argon are examples. All other elements have one or more incomplete rings of electrons. If the incomplete ring is loosely bound, the electrons may be easily removed, the element is called *metallic*, and is a conductor of electric current. If the incomplete ring is tightly bound, with only a few missing electrons, the element is called *non-metallic* and is an insulator of electric current. Germanium and silicon fall between these two sharply defined groups, and exhibit both metallic and non-metallic characteristics. Pure germanium or silicon may be considered to be a good insulator. The addition of certain impurities in carefully controlled amounts to the pure germanium will alter the conductivity of the material. In addition, the choice of the impurity can change the direction of conductivity through the crystal, some impurities increasing conductivity to positive voltages, and others increasing conductivity to negative voltages.

5-2 Mechanism of Conduction

As indicated by their name, semiconductors are substances which have a conductivity intermediate between the high values observed for metals and the low values observed for insulating materials. The mechanism of conduc-

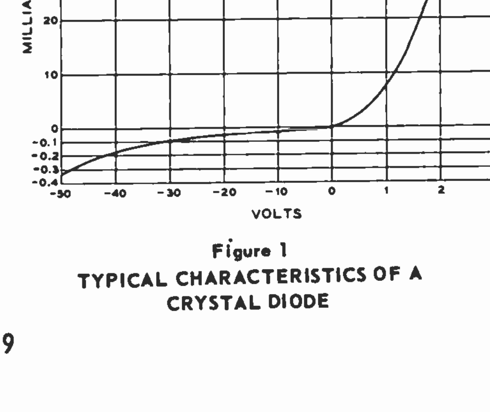


Figure 1
TYPICAL CHARACTERISTICS OF A CRYSTAL DIODE

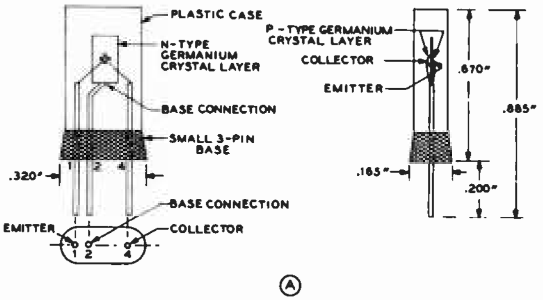


Figure 2A
CUT-AWAY VIEW OF JUNCTION TRANSSISTOR, SHOWING PHYSICAL ARRANGEMENT

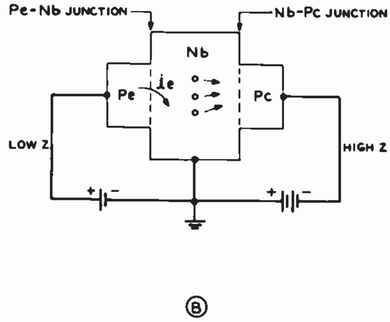


Figure 2B
PICTORIAL EQUIVALENT OF P-N-P JUNCTION TRANSISTOR

tion in semiconductors is different from that observed in metallic conductors. There exist in semiconductors both negatively charged electrons and positively charged particles, called *holes*, which behave as though they had a positive electrical charge equal in magnitude to the negative electrical charge on the electron. These holes and electrons drift in an electrical field with a velocity which is proportional to the field itself:

$$V_{dh} = \mu_h E$$

where V_{dh} = drift velocity of hole
E = magnitude of electric field
μ_h = mobility of hole

In an electric field the holes will drift in a direction opposite to that of the electron and with about one-half the velocity, since the hole mobility is about one-half the electron mobility. A sample of a semiconductor, such as germanium or silicon, which is both chemically pure and mechanically perfect will contain in it approximately equal numbers of holes and electrons and is called an *intrinsic* semiconductor. The intrinsic resistivity of the semiconductor depends strongly upon the temperature, being about 50 ohm/cm. for germanium at room temperature. The intrinsic resistivity of silicon is about 65,000 ohm/cm. at the same temperature.

If, in the growing of the semiconductor crystal, a small amount of an impurity, such as phosphorous, arsenic or antimony is included in the crystal, each atom of the impurity contributes one free electron. This electron is available for conduction. The crystal is said to be *doped* and has become electron-conducting in nature and is called *N (negative) type* germanium. The impurities which contribute electrons are called *donors*. N-type germanium has better conductivity than pure germanium in one direction, and a continuous stream of electrons will flow through the crystal in this direction as long as an external potential of the correct polarity is applied across the crystal.

Other impurities, such as aluminum, gallium or indium add one hole to the semiconducting crystal by accepting one electron for each atom of impurity, thus creating additional holes in the semiconducting crystal. The material is now said to be hole-conducting, or *P (positive) type* germanium. The impurities which create holes are called *acceptors*. P-type germanium has better conductivity than pure germanium in one direction. This direction is opposite to that of the N-type material. Either the N-type or the P-type germanium is called *extrinsic* conducting type. The doped materials have lower resistivities than the pure materials, and doped semiconductors in the resistivity range of .01 to 10 ohm/cm. are normally used in the production of transistors.

5-3 The Transistor

In the past few years an entire new technology has been developed for the application of certain semiconducting materials in production of devices having gain properties. These gain properties were previously found only in vacuum tubes. The elements germanium and silicon are the principal materials which exhibit the proper semiconducting properties permitting their application in the new amplifying devices called *transistors*. However, other semiconducting materials, including the compounds indium antimonide and lead sulfide have been used experimentally in the production of transistors.

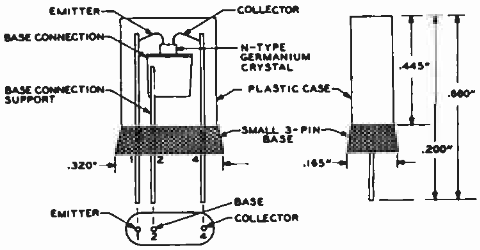


Figure 3
CONSTRUCTION DETAIL OF A POINT CONTACT TRANSISTOR

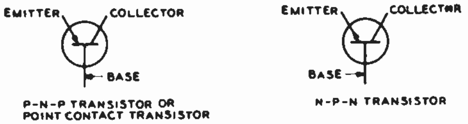


Figure 4
ELECTRICAL SYMBOLS FOR TRANSISTORS

Types of Transistors There are two basic types of transistors, the *point-contact* type and the *junction* type (figure 2). Typical construction detail of a point-contact transistor is shown in Figure 3, and the electrical symbol is shown in Figure 4. The *emitter* and *collector* electrodes make contact with a small block of germanium, called the *base*. The base may be either N-type or P-type germanium, and is approximately .05" long and .03" thick. The emitter and collector electrodes are fine wires, and are spaced about .005" apart on the germanium base. The complete assembly is usually encapsulated in a small, plastic case to provide ruggedness and to avoid contaminating effects of the atmosphere. The polarity of emitter and collector voltages depends upon the type of germanium employed in the base, as illustrated in figure 4.

The junction transistor consists of a piece of either N-type or P-type germanium between two wafers of germanium of the opposite type. Either N-P-N or P-N-P transistors may be made. In one construction called the *grown crystal process*, the original crystal, grown from molten germanium or silicon, is created in such a way as to have the two closely spaced junctions imbedded in it. In the other construction called the *fusion process*, the crystals are grown so as to make them a single conductivity type. The junctions are then produced by fusing small pellets of special metal alloys into minute plates cut from the original crystal. Typical construction detail of a junction transistor is shown in figure 2A.

The electrical schematic for the P-N-P junction transistor is the same as for the point-contact type, as is shown in figure 4.

Transistor Action Presently available types of transitors have three essential actions which collectively are called *transistor action*. These are: minority carrier injection, transport, and collection. Figure 2B shows a simplified drawing of a P-N-P junction-type transistor, which can illustrate this collective action. The P-N-P transistor consists of a piece of N-type germanium on opposite sides of which a layer of P-type material has been grown by the fusion process. Terminals are connected to the two P-sections and to the N-type base. The transistor may be considered as two P-N junction rectifiers placed in close juxaposition with a semi-conduction crystal coupling the two rectifiers together. The left-hand terminal is biased in the forward (or conducting) direction and is called the emitter. The right-hand terminal is biased in the back (or reverse) direction and is called the collector. The operating potentials are chosen with respect to the base terminal, which may or may not be grounded. If an N-P-N transistor is used in place of the P-N-P, the operating potentials are reversed.

The $P_e - N_b$ junction on the left is biased in the forward direction and holes from the P region are injected into the N_b region, producing therein a concentration of holes substantially greater than normally present in the material. These holes travel across the base region towards the collector, attracting neighboring electrons, finally increasing the available supply of conducting electrons in the collector loop. As a result, the collector loop possesses lower resistance whenever the emitter circuit is in operation. In junction transistors this *charge transport* is by means of diffusion wherein the charges move from a region of high concentration to a region of lower concentration at the collector. The collector, biased in the opposite direction, acts as a *sink* for these holes, and is said to collect them.

It is known that any rectifier biased in the forward direction has a very low internal impedance, whereas one biased in the back direction has a very high internal impedance. Thus, current flows into the transistor in a low impedance circuit, and appears at the output as current flowing in a high impedance circuit. The ratio of a change in collector current to a change in emitter current is called the *current amplification*, or *alpha:*

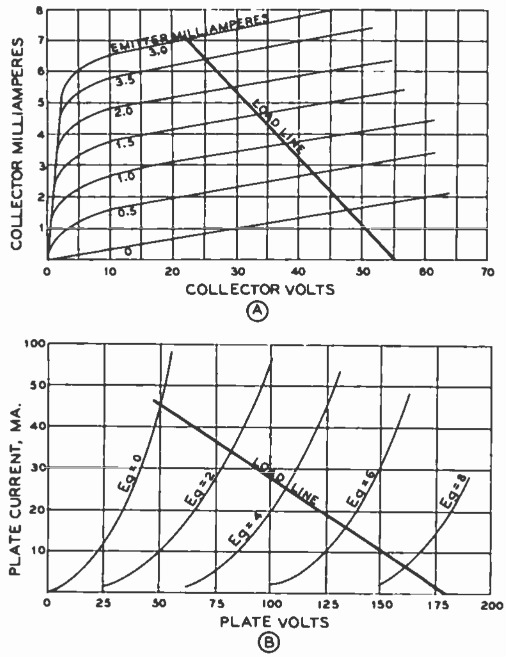


Figure 5
COMPARISON OF POINT-CONTACT TRANSISTOR AND VACUUM TUBE CHARACTERISTICS.

$$a = \frac{i_c}{i_e}$$

where a = current amplification
i_c = change in collector current
i_e = change in emitter current

Values of alpha up to 3 or so may be obtained in commercially available point-contact transistors, and values of alpha up to about 0.95 are obtainable in junction transistors.

The *resistance gain* of a transistor is expressed as the ratio of output resistance to input resistance. The input resistance of a typical transistor, is low, in the neighborhood of 300 ohms, while the output resistance is relatively high, usually over 20,000 ohms. For a point-contact transistor, the resistance gain is usually over 60.

The *voltage gain* of a transistor is the product of alpha times the resistance gain, and for a point-contact transistor is of the order of $3 \times 60 = 180$. A junction transistor which has a value of alpha less than unity nevertheless has a resistance gain of the order of 2000 because of its extremely high output resistance, and the resulting voltage gain is

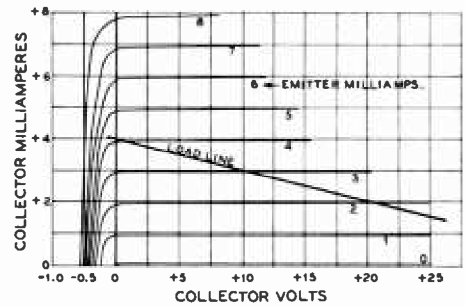


Figure 6
OUTPUT CHARACTERISTICS OF TYPICAL JUNCTION TRANSISTOR

about 1800 or so. For both types of transistors the *power gain* is the product of alpha squared times the resistance gain and is of the order of 400 to 500.

5-4 Transistor Characteristics

The transistor produces results that may be comparable to a vacuum tube, but there is a basic difference between the two devices. The vacuum tube is a voltage controlled device whereas the transistor is a current controlled device. A vacuum tube normally operates with its grid biased in the negative or high resistance direction, and its plate biased in the positive or low resistance direction. The tube conducts only by means of electrons, and has its conducting counterpart in the form of the N-P-N transistor, whose majority carriers are also electrons. There is no vacuum tube equivalent of the P-N-P transistor, whose majority carriers are holes.

The biasing conditions stated above provide the high input impedance and low output impedance of the vacuum tube. The transistor is biased in the positive or low resistance direction in the emitter circuit, and in the negative, or high resistance direction in the collector circuit resulting in a low input impedance and a high output impedance, contrary to and opposite from the vacuum tube. A comparison of point-contact transistor characteristics and vacuum tube characteristics is made in figure 5.

The output characteristics of the junction transistor are of great interest. A typical example is shown in figure 6. It is seen that the junction transistor has the characteristics of an ideal pentode vacuum tube. The collector current is practically independent of the collector voltage. The range of linear operation

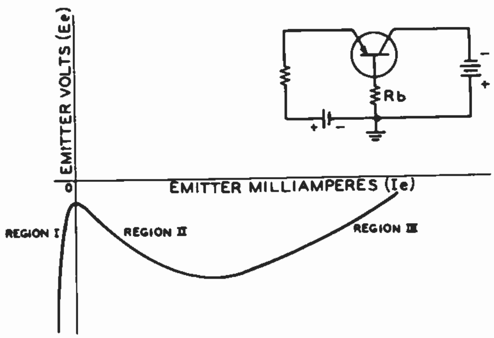
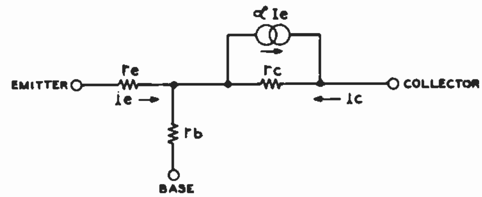


Figure 7
EMITTER CHARACTERISTIC CURVE FOR TYPICAL POINT CONTACT TRANSISTOR



VALUES OF THE EQUIVALENT CIRCUIT

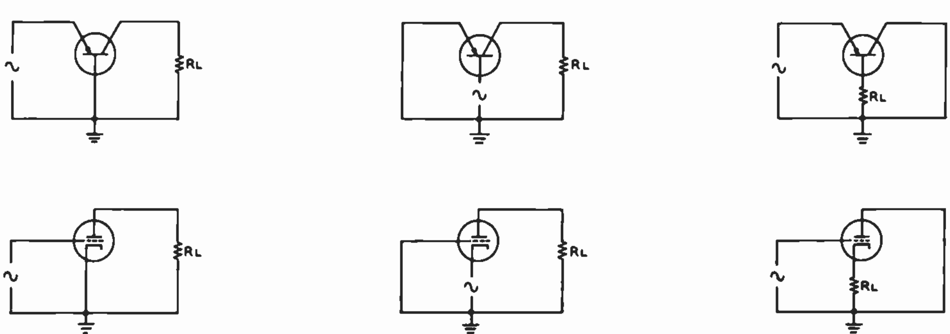
PARAMETER	POINT-CONTACT TRANSISTOR (i_e = 1 MA., V_c = 15 V.)	JUNCTION TRANSISTOR (i_e = 1 MA., V_c = 3 V.)
r_e - EMITTER RESISTANCE	100 Ω	30 Ω
r_b - BASE RESISTANCE	300 Ω	300 Ω
r_c - COLLECTOR RESISTANCE	20 000 Ω	1 MEGOHM
α - CURRENT AMPLIFICATION	2.0	0.97

Figure 8
LOW FREQUENCY EQUIVALENT CIRCUIT FOR POINT CONTACT AND JUNCTION TRANSISTOR

extends from a minimum voltage of about 0.2 volts up to the maximum rated collector voltage. A typical load line is shown, which illustrates the very high load impedance that would be required for maximum power transfer. A grounded emitter circuit is usually used, since the output impedance is not as high as when a grounded base circuit is used.

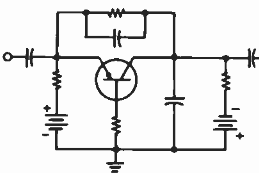
The output characteristics of a typical point-contact transistor are shown in figure 5. The pentode characteristics are less evident, and the output impedance is much lower, with the range of linear operation extending down to a collector voltage of 2 or 3. Of greater practical interest, however, is the input characteristic curve with short-circuited, or nearly short-circuited input, as shown in figure 7. It is this point-contact transistor characteristic of having a region of negative impedance that lends the unit to use in switching circuits. The transistor circuit may be made to have two, one or zero stable operating points, depending upon the bias voltages and the load impedance used.

Equivalent Circuit of a Transistor As is known from network theory, the small signal performance of any device in any network can be represented by means of an equivalent circuit. The most convenient equivalent circuit for the low frequency small signal performance of both point-contact and junction transistors is shown in figure 8. r_e, r_b, and r_c, are dynamic resistances which can be associated with the emitter, base and collector regions of the transistor. The current

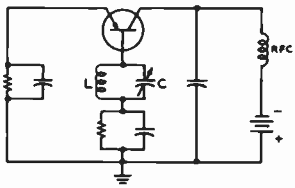


GROUNDED BASE CONNECTION GROUNDED EMITTER CONNECTION GROUNDED COLLECTOR CONNECTION

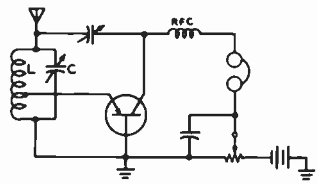
Figure 9
COMPARISON OF BASIC VACUUM TUBE AND TRANSISTOR CONFIGURATIONS.



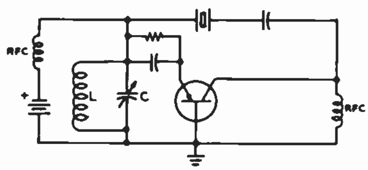
10A FLIP-FLOP COUNTER



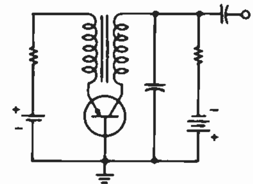
10B R.F. OSCILLATOR

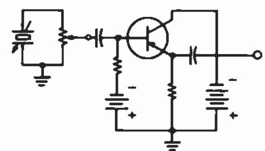


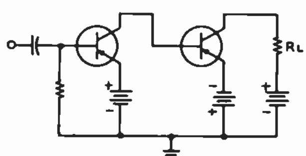
10C ONE-STAGE RECEIVER



10D CRYSTAL OSCILLATOR


10E BLOCKING OSCILLATOR


10F AUDIO AMPLIFIER



10G DIRECT-COUPLED AMPLIFIER

Figure 10
TYPICAL TRANSISTOR CIRCUITS.

generator aI_e, represents the transport of charge from emitter to collector. Typical values of the equivalent circuit are shown in figure 8.

Transistor Circuitry There are three basic transistor configurations: grounded base connection, grounded emitter connection, and grounded collector connection. These correspond roughly to grounded grid, grounded cathode, and grounded plate circuits in vacuum tube terminology (figure 9).

The grounded base circuit has a low input impedance and high output impedance, and no phase reversal of signal from input to output circuit. The grounded emitter circuit has a higher input impedance and a lower output impedance than the grounded base circuit, and a reversal of phase between the input and output signal occurs. This circuit usually provides maximum voltage gain from a transistor. The grounded collector circuit has relatively high input impedance, low output impedance, and no phase reversal of signal from input to output circuit. Power and voltage gain are both low.

Figure 10 illustrates some practical vacuum tube circuits, as applied to transistors.

5-5 A Transistor Frequency Standard

A 100 kilocycle crystal transistor oscillator for use as a secondary frequency standard is shown in figure 11.

In developing a transistor crystal oscillator with satisfactory characteristics for use as a frequency standard, a few difficulties must be considered. Chief among these is the loading effect of the transistor upon the crystal. The transistor presents a low impedance capacitive load to the crystal, which results in a lowering of the resonant frequency of the crystal. With commercial crystals it was found that the transistor loading will drop the resonant frequency of the crystal 30 to 100 cycles below the 100 kilocycle point. The simplest solution to this problem is to decouple the crystal by means of a series capacitor. This was found to bring the resonant frequency up to the desired point. However, this action also tends to decrease the coupling to the crystal to the point where oscillation may be marginal. Most all CK-722 (Raytheon) transistors oscillated well in this circuit and showed no signs of instability provided the output coupling was loose.

One desirable result of decoupling the crystal is that the oscillator is relatively independent of temperature variations in the transistor parameters. Temperature variation of this circuit is approximately 1 cycle/degree, which is satisfactory for room temperature limits.

The output of the 100 kilocycle is run through a 1N34 germanium diode to increase the strength of the higher oscillator harmonics. Power for the unit may be obtained from two or three of the smallest size *pen-lite* batteries, as the current drain of the unit is minute.

If the oscillator is placed in a receiver, the operating voltage may be obtained from a tap on the cathode resistor of the power audio tube of the receiver.

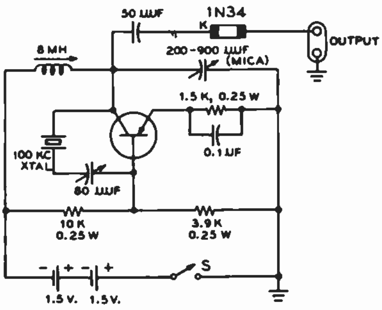


Figure 11
100-KILOCYCLE CRYSTAL TRANSITOR OSCILLATOR, USING CK-722 TRANSISTOR

CHAPTER SIX

Vacuum Tube Amplifiers

6-1 Vacuum Tube Parameters

The ability of the control grid of a vacuum tube to control large amounts of plate power with a small amount of grid energy allows the vacuum tube to be used as an amplifier. It is this ability of vacuum tubes to amplify an extremely small amount of energy up to almost any level without change in anything except amplitude which makes the vacuum tube such an extremely valuable adjunct to modern electronics and communication.

Symbols for Vacuum-Tube Parameters As an assistance in simplifying and shortening expressions involving vacuum-tube parameters, the following symbols will be used throughout this book:

Tube Constants

μ — amplification factor
R_p — plate resistance
G_m — transconductance
μ_{sg} — grid-screen mu factor
G_c — conversion transconductance (mixer tube)

Interelectrode Capacitances

C_{gk} — grid-cathode capacitance
C_{gp} — grid-plate capacitance
C_{pk} — plate-cathode capacitance
C_{in} — input capacitance (tetrode or pentode)
C_{out} — output capacitance (tetrode or pentode)

Electrode Potentials

E_{bb} — d-c plate supply voltage (a positive quantity)
E_{cc} — d-c grid supply voltage (a negative quantity)
E_{gm} — peak grid excitation voltage (½ total peak-to-peak grid swing)
E_{pm} — peak plate voltage (½ total peak-to-peak plate swing)
e_p — instantaneous plate potential
e_g — instantaneous grid potential
e_{pmin} — minimum instantaneous plate voltage
e_{gmp} — maximum positive instantaneous grid voltage
E_p — static plate voltage
E_g — static grid voltage
e_{co} — cutoff bias

Electrode Currents

I_b — average plate current
I_c — average grid current
I_{pm} — peak fundamental plate current
i_{pmax} — maximum instantaneous plate current
i_{gmax} — maximum instantaneous grid current
I_p — static plate current
I_g — static grid current

Other Symbols

P_i — plate power input
P_o — plate power output
P_p — plate dissipation
P_d — grid driving power (grid plus bias losses)

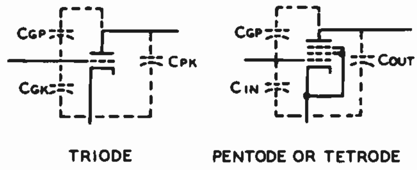


Figure 1

STATIC INTERELECTRODE CAPACITANCES WITHIN A TRIODE, PENTODE, OR TETRODE

P_g — grid dissipation
N_p — plate efficiency(expressed as a decimal)
θ_p — one-half angle of plate current flow
θ_g — one-half angle of grid current flow
R_L — load resistance
Z_L — load impedance

Vacuum-Tube Constants The relationships between certain of the electrode potentials and currents within a vacuum tube are reasonably constant under specified conditions of operation. These relationships are called *vacuum-tube constants* and are listed in the data published by the manufacturers of vacuum tubes. The defining equations for the basic vacuum-tube constants are given in Chapter Four.

Interelectrode Capacitances and Miller Effect The values of interelectrode capacitance published in vacuum-tube tables are the static values measured, in the case of triodes for example, as shown in figure 1. The static capacitances are simply as shown in the drawing, but when a tube is operating as amplifier there is another consideration known as *Miller Effect* which causes the dynamic input capacitance to be different from the static value. The output capacitance of an amplifier is essentially the same as the static value given in the published tube tables. The grid-to-plate capacitance is also the same as the published static value, but since the C_{gp} acts as a small capacitance coupling energy back from the plate circuit to the grid circuit, the dynamic input capacitance is equal to the static value plus an amount (frequently much greater in the case of a triode) determined by the gain of the stage, the plate load impedance, and the C_{gp} feedback capacitance. The total value for an audio amplifier stage can be expressed in the following equation:

$$C_{gk}^{(dynamic)} = C_{gk}^{(static)} + (A + 1)\, C_{gp}$$

where C_{gk} is the grid-to-cathode capacitance, C_{gp} is the grid-to-plate capacitance, and A is the stage gain. This expression assumes that the vacuum tube is operating into a resistive load such as would be the case with an audio stage working into a resistance plate load in the middle audio range.

The more complete expression for the input admittance (vector sum of capacitance and resistance) of an amplifier operating into any type of plate load is as follows:

$$\text{Input capacitance} = C_{gk} + (1 + A\cos\theta)\, C_{gp}$$

$$\text{Input resistance} = \frac{-\left(\dfrac{1}{\omega\, C_{gp}}\right)}{A \sin\theta}$$

Where: C_{gk} = grid-to-cathode capacitance
C_{gp} = grid-to-plate capacitance
A = voltage amplification of the tube alone
θ = phase angle of the plate load impedance, positive for inductive loads, negative for capacitive

It can be seen from the above that if the plate load impedance of the stage is capacitive or inductive, there will be a resistive component in the input admittance of the stage. The resistive component of the input admittance will be positive (tending to load the circuit feeding the grid) if the load impedance of the plate is capacitive, or it will be negative (tending to make the stage oscillate) if the load impedance of the plate is inductive.

Neutralization of Interelectrode Capacitance Neutralization of the effects of interelectrode capacitance is employed most frequently in the case of radio frequency power amplifiers. Before the introduction of the tetrode and pentode tube, triodes were employed as neutralized Class A amplifiers in receivers. This practice has been largely superseded in the present state of the art through the use of tetrode and pentode tubes in which the C_{gp} or feedback capacitance has been reduced to such a low value that neutralization of its effects is not necessary to prevent oscillation and instability.

6-2 Classes and Types of Vacuum-Tube Amplifiers

Vacuum-tube amplifiers are grouped into various classes and sub-classes according to the type of work they are intended to perform. The difference between the various classes is determined primarily by the value of average grid bias employed and the maximum value of the exciting signal to be impressed upon the grid.

Class A Amplifier A Class A amplifier is an amplifier biased and supplied with excitation of such amplitude that plate current flows continuously (360° of the exciting voltage waveshape) and grid current does not flow at any time. Such an amplifier is normally operated in the center of the grid-voltage plate-current transfer characteristic and gives an output waveshape which is a substantial replica of the input waveshape.

Class A_1 Amplifier This is another term applied to the Class A amplifier in which grid current does not flow over any portion of the input wave cycle.

Class A_2 Amplifier This is a Class A amplifier operated under such conditions that the grid is driven positive over a portion of the input voltage cycle, but plate current still flows over the entire cycle.

Class AB_1 Amplifier This is an amplifier operated under such conditions of grid bias and exciting voltage that plate current flows for more than one-half the input voltage cycle but for less than the complete cycle. In other words the operating angle of plate current flow is appreciably greater than 180° but less than 360°. The suffix 1 indicates that grid current does not flow over any portion of the input cycle.

Class AB_2 Amplifier A Class AB_2 amplifier is operated under essentially the same conditions of grid bias as the Class AB_1 amplifier mentioned above, but the exciting voltage is of such amplitude that grid current flows over an appreciable portion of the input wave cycle.

Class B Amplifier A Class B amplifier is biased substantially to cutoff of plate current (without exciting voltage) so that plate current flows essentially over one-half the input voltage cycle. The operating angle of plate current flow is essentially 180°. The Class B amplifier is almost always excited to such an extent that grid current flows.

Class C Amplifier A Class C amplifier is biased to a value greater than the value required for plate current cutoff and is excited with a signal of such amplitude that grid current flows over an appreciable period of the input voltage waveshape. The angle of plate current flow in a Class C amplifier is appreciably less than 180°, or in other words, plate current flows appreciably less than one-half the time. Actually, the conventional operating conditions for a Class C amplifier are such that plate current flows for 120° to 150° of the exciting voltage waveshape.

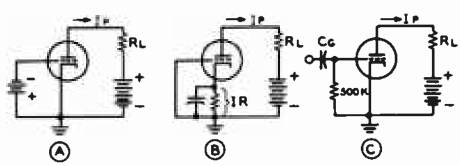


Figure 2
TYPES OF BIAS SYSTEMS

A - Grid bias
B - Cathode bias
C - Grid leak bias

Types of Amplifiers There are three general types of amplifier circuits in use. These types are classified on the basis of the *return* for the input and output circuits. Conventional amplifiers are called *cathode return* amplifiers since the cathode is effectively grounded and acts as the common return for both the input and output circuits. The second type is known as a plate return amplifier or *cathode follower* since the plate circuit is effectively at ground for the input and output signal voltages and the output voltage or power is taken between cathode and plate. The third type is called a *grid-return* or *grounded-grid* amplifier since the grid is effectively at ground potential for input and output signals and output is taken between grid and plate.

6-3 Biasing Methods

The difference of potential between grid and cathode is called the *grid bias* of a vacuum tube. There are three general methods of providing this bias voltage. In each of these methods the purpose is to establish the grid at a potential with respect to the cathode which will place the tube in the desired operating condition as determined by its characteristics.

Grid bias may be obtained from a source of voltage especially provided for this purpose, as a battery or other d-c power supply. This method is illustrated in figure 2A, and is known as *fixed bias*.

A second biasing method is illustrated in figure 2B which utilizes a cathode resistor across which an IR drop is developed as a result of plate current flowing through it. The cathode of the tube is held at a positive potential with respect to ground by the amount of the IR drop because the grid is at ground potential. Since the biasing voltage depends upon the flow of plate current the tube cannot be held in a cutoff condition by means of the *cathode bias* voltage developed across the cathode resistor. The value of this resistor is determined by the bias required and the plate current which flows at this value of bias, as found from the tube characteristic curves. A capacitor is shunted across the bias resistor to provide a low impedance path to ground for the a-c component of the plate current which results from an a-c input signal on the grid.

The third method of providing a biasing voltage is shown in figure 2C, and is called *grid-leak* bias. During the portion of the input cycle which causes the grid to be positive with respect to the cathode, grid current flows from cathode to grid, charging capacitor C_g. When the grid draws current, the grid-to-cathode resistance of the tube drops from an infinite value to a very low value, on the order of 1,000 ohms or so, making the charging time constant of the capacitor very short. This enables C_g to charge up to essentially the full value of the positive input voltage and results in the grid (which is connected to the low potential plate of the capacitor) being held essentially at ground potential. During the negative swing of the input signal no grid current flows and the discharge path of C_g is through the grid resistance which has a value of 500,000 ohms or so. The discharge time constant for C_g is, therefore, very long in comparison to the period of the input signal and only a small part of the charge on C_g is lost. Thus, the bias voltage developed by the discharge of C_g is substantially constant and the grid is not permitted to follow the positive portions of the input signal.

6-4 Distortion in Amplifiers

There are three main types of distortion that may occur in amplifiers: frequency distortion, phase distortion and amplitude distortion.

Frequency Distortion Frequency distortion may occur when some frequency components of a signal are amplified more than others. Frequency distortion occurs at low frequencies if coupling capacitors between stages are too small, or may occur at high frequencies as a result of the shunting effects of the distributed capacities in the circuit.

Phase Distortion In figure 3 an input signal consisting of a fundamental and a third harmonic is passed through a two stage amplifier. Although the amplitudes of both components are amplified by identical ratios, the output waveshape is considerably different from the input signal because the phase of the third harmonic signal has been shifted with respect to the fundamental signal. This phase shift is known as *phase distortion*, and is caused principally by the coupling circuits between the stages of the amplifier. Most coupling circuits shift the phase of a sine wave, but this has no effect on the shape of the output wave. However, when a complex wave is passed through the same coupling circuit, each component frequency of the waveshape may be shifted in phase by a different amount so that the output wave is not a faithful reproduction of the input waveshape.

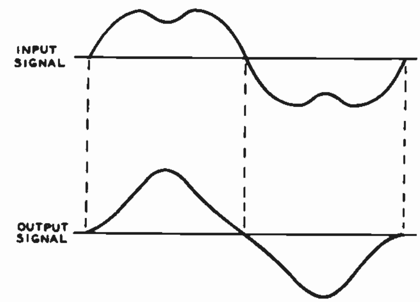


Figure 3

Illustration of the effect of phase distortion on input wave containing a third harmonic signal

Amplitude Distortion If a signal is passed through a vacuum tube that is operating on any non-linear part of its characteristic, amplitude distortion will occur. In such a region, a change in grid voltage does not result in a change in plate current which is directly proportional to the change in grid voltage. For example, if an amplifier is excited with a signal that overdrives the tubes, the resultant signal is distorted in amplitude, since the tubes operate over a non-linear portion of their characteristic.

6-5 Resistance-Capacitance Coupled Audio-Frequency Amplifiers

Present practice in the design of audio-frequency voltage amplifiers is almost exclusively to use resistance-capacitance coupling between the low-level stages. Both triodes and

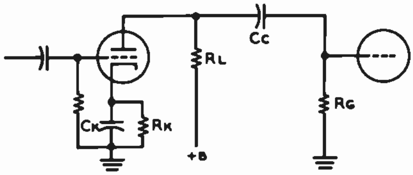


Figure 4

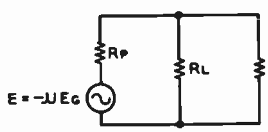
STANDARD CIRCUIT FOR RESISTANCE-CAPACITANCE COUPLED TRIODE AMPLIFIER STAGE

pentodes are used; triode amplifier stages will be discussed first.

R-C Coupled Triode Stages Figure 4 illustrates the standard circuit for a resistance-capacitance coupled amplifier stage utilizing a triode tube with cathode bias. In conventional audio-frequency amplifier design such stages are used at medium voltage levels (from 0.01 to 5 volts peak on the grid of the tube) and use medium-μ triodes such as the 6J5 or high-μ triodes such as the 6SF5 or 6SL7-GT. Normal voltage gain for a single stage of this type is from 10 to 70, depending upon the tube chosen and its operating conditions. Triode tubes are normally used in the last voltage amplifier stage of an R-C amplifier since their harmonic distortion with large output voltage (25 to 75 volts) is less than with a pentode tube.

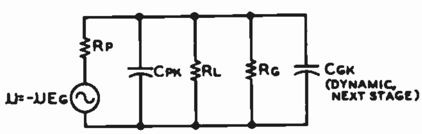
Voltage Gain per Stage The voltage gain per stage of a resistance-capacitance coupled triode amplifier can be calculated with the aid of the equivalent circuits and expressions for the mid-frequency, high-frequency, and low-frequency range given in figure 5.

A triode R-C coupled amplifier stage is normally operated with values of cathode resistor and plate load resistor such that the actual voltage on the tube is approximately one-half the d-c plate supply voltage. To



MID FREQUENCY RANGE

$$A = \frac{\mu R_L R_G}{R_P (R_L + R_G) + R_L R_G}$$

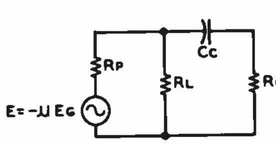


HIGH FREQUENCY RANGE

$$\frac{A_{\text{HIGH FREQ.}}}{A_{\text{MID FREQ.}}} = \frac{1}{\sqrt{1 + (R_{EQ}/X_S)^2}}$$

$$R_{EQ} = \frac{R_L}{1 + \frac{R_L}{R_G} + \frac{R_L}{R_P}}$$

$$X_S = \frac{1}{2\pi f\,(C_{PK} + C_{GK}\ (\text{DYNAMIC}))}$$



LOW FREQUENCY RANGE

$$\frac{A_{\text{LOW FREQ.}}}{A_{\text{MID FREQ.}}} = \frac{1}{\sqrt{1 + (X_C/R)^2}}$$

$$X_C = \frac{1}{2\pi f C_C}$$

$$R = R_G + \frac{R_L R_P}{R_L + R_P}$$

Figure 5

Equivalent circuits and gain equations for a triode R-C coupled amplifier stage. In using these equations, be sure to select the values of mu and R_p which are proper for the static current and voltages with which the tube will operate. These values may be obtained from curves published in the RCA Tube Handbook RC-16.

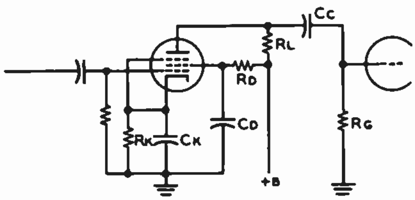


Figure 6

STANDARD CIRCUIT FOR RESISTANCE-CAPACITANCE COUPLED PENTODE AMPLIFIER STAGE

assist the designer of such stages, data on operating conditions for commonly used tubes is published in the RCA Tube Handbook RC-16. It is assumed, in the case of the gain equations of figure 5, that the cathode by-pass capacitor, C_k, has a reactance that is low with respect to the cathode resistor at the lowest frequency to be passed by the amplifier stage.

R-C Coupled Pentode Stages Figure 6 illustrates the standard circuit for a resistance-capacitance coupled pentode amplifier stage. Cathode bias is used and the screen voltage is supplied through a dropping resistor from the plate voltage supply. In conventional audio-frequency amplifier design such stages are normally used at low voltage levels (from 0.00001 to 0.1 volts peak on the grid of the tube) and use moderate-G_m pentodes such as the 6SJ7. Normal voltage gain for a stage of this type is from 60 to 250, depending upon the tube chosen and its operating conditions. Pentode tubes are ordinarily used the first stage of an R-C amplifier where the high gain which they afford is of greatest advantage and where only a small voltage output is required from the stage.

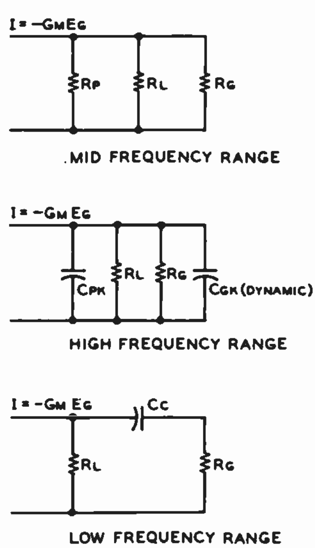
The voltage gain per stage of a resistance-capacitance coupled pentode amplifier can be calculated with the aid of the equivalent circuits and expressions for the mid-frequency, high-frequency, and low-frequency range given in figure 7.

To assist the designer of such stages, data on operating conditions for commonly used types of tubes is published in the RCA Tube Handbook RC-16. It is assumed, in the case of the gain equations of figure 7, that the cathode by-pass capacitor, C_k, has a reactance that is low with respect to the cathode resistor at the lowest frequency to be passed by the stage. It is additionally assumed that the reactance of the screen by-pass capacitor C_d, is low with respect to the screen dropping resistor, R_d, at the lowest frequency to be passed by the amplifier stage.

Cascade Voltage Amplifier Stages When voltage amplifier stages are operated in such a manner that the output voltage of the first is fed to the grid of the second, and so forth, such stages are said to be *cascaded.* The total voltage gain of cascaded amplifier

Figure 7

Equivalent circuits and gain equations for a pentode R-C coupled amplifier stage. In using these equations be sure to select the values of G_m and R_p which are proper for the static currents and voltages with which the tube will operate. These values may be obtained from curves published in the RCA Tube Handbook RC-16.



$$A = G_M R_{EQ}$$

$$R_{EQ} = \frac{R_L}{1 + \frac{R_L}{R_G} + \frac{R_L}{R_P}}$$

$$\frac{A_{\text{HIGH FREQ.}}}{A_{\text{MID FREQ.}}} = \frac{1}{\sqrt{1 + (R_{EQ}/X_S)^2}}$$

$$R_{EQ} = \frac{R_L}{1 + \frac{R_L}{R_G} + \frac{R_L}{R_P}}$$

$$X_S = \frac{1}{2\pi f\,(C_{PK} + C_{GK\,(\text{DYNAMIC})})}$$

$$\frac{A_{\text{LOW FREQ.}}}{A_{\text{MID FREQ.}}} = \frac{1}{\sqrt{1 + (X_C/R)^2}}$$

$$X_C = \frac{1}{2\pi f\,C_C}$$

$$R = R_G + \frac{R_L\ R_P}{R_L + R_P}$$

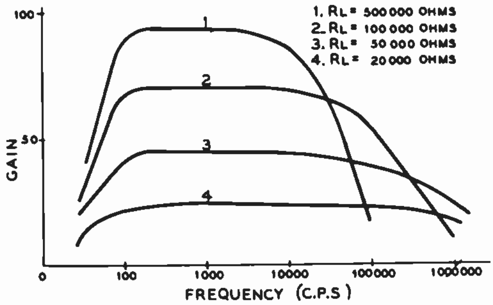
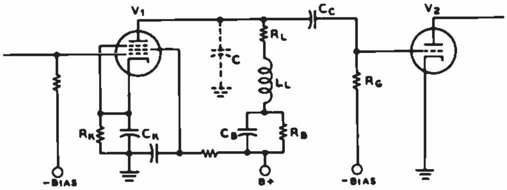


Figure 8

The variation of stage gain with frequency in an r-c coupled pentode amplifier for various values of plate load resistance



MID-FREQUENCY GAIN $= G_M V_1 R_L$

HIGH-FREQUENCY GAIN $= G_M V_1 Z_{\text{COUPLING NETWORK}}$

$C = C_{OUT} V_1 + C_{IN} V_2 + C_{\text{DISTRIBUTED}}$

FOR COMPROMISE HIGH FREQUENCY EQUALIZATION.

$X_{L_L} = 0.5 X_C$ AT f_C

$R_L = X_C$ AT f_C

WHERE. f_C = CUTOFF FREQUENCY OF AMPLIFIER

L_L = PEAKING INDUCTOR

FOR COMPROMISE LOW FREQUENCY EQUALIZATION:

$R_B = R_K (G_M V_1 R_L)$

$R_B C_B = R_K C_K$

C_K = 25 TO 50 μFD. IN PARALLEL WITH .001 MICA

C_B = CAPACITANCE FROM ABOVE WITH .001 MICA IN PARALLEL

Figure 9

SIMPLE COMPENSATED VIDEO AMPLIFIER CIRCUIT

Resistor R_L in conjunction with coil L_L serves to flatten the high-frequency response of the stage, while C_B and R_B serve to equalize the low-frequency response of this simple video amplifier stage.

stages is obtained by taking the product of the voltage gains of each of the successive stages.

Sometimes the voltage gain of an amplifier stage is rated in decibels. Voltage gain is converted into decibels gain through the use of the following expression: db = 20 $\log_{10}$ A, where A is the voltage gain of the stage. The total gain of cascaded voltage amplifier stages can be obtained by *adding* the number of decibels gain in each of the cascaded stages.

R-C Amplifier Response A typical frequency response curve for an R-C coupled audio amplifier is shown in figure 8. It is seen that the amplification is poor for the extreme high and low frequencies. The reduced gain at the low frequencies is caused by the loss of voltage across the coupling capacitor. In some cases, a low value of coupling capacitor is deliberately chosen to reduce the response of the stage to hum, or to attenuate the lower voice frequencies for communication purposes. For high fidelity work the product of the grid resistor in ohms times the coupling capacitor in microfarads should equal 25,000. (ie.: 500,000 ohms × 0.05 μfd = 25,000).

The amplification of high frequencies falls off because of the Miller effect of the subsequent stage, and the shunting effect of residual circuit capacities. Both of these effects may be minimized by the use of a low value of plate load resistor.

Grid Leak Bias for High Mu Triodes The correct operating bias for a high-mu triode such as the 6SL7, is fairly critical, and will be found to be highly variable from tube to tube because of minute variations in contact potential within the tube itself. A satisfactory bias method is to use grid leak bias, with a grid resistor of one to ten megohms connected directly between grid and cathode of the tube. The cathode is grounded. Grid current flows at all times, and the effective input resistance is about one-half the resistance value of the grid leak. This circuit is particularly well suited as a high gain amplifier following low output devices, such as crystal microphones, or dynamic microphones.

R-C Amplifier General Characteristics A resistance-capacity coupled amplifier can be designed to provide a good frequency response for almost any desired range. For instance, such an amplifier can be built to provide a fairly uniform amplification for frequencies in the audio range of about 100 to 20,000 cycles. Changes in the values of coupling capacitors and load resistors can extend this frequency range to cover the very wide range required for video service. However, extension of the range can only be obtained at the cost of reduced over-all amplification. Thus the R-C method of coupling allows good frequency response with minimum distortion, but low amplification. Phase distortion is less with R-C coupling than with other types, except direct coupling. The R-C amplifier may exhibit tendencies to "motorboat" or oscillate if it is used with a high impedance plate supply.

6-6 Video-Frequency Amplifiers

A video-frequency amplifier is one which has been designed to pass frequencies from the lower audio range (lower limit perhaps 50 cycles) to the middle r-f range (upper limit perhaps 4 to 6 megacycles). Such amplifiers, in addition to passing such an extremely wide frequency range, must be capable of amplifying this range with a minimum of amplitude, phase, and frequency distortion. Video amplifiers are commonly used in television, pulse communication, and radar work.

Tubes used in video amplifiers must have a high ratio of G_m to capacitance if a usable gain per stage is to be obtained. Commonly available tubes which have been designed for or are suitable for use in video amplifiers are: 6AU6, 6AG5, 6AK5, 6CB6, 6AC7, 6AG7, and 6K6-GT. Since, at the upper frequency limits of a video amplifier the input and output shunting capacitances of the amplifier tubes have rather low values of reactance, low values of coupling resistance along with peaking coils or other special interstage coupling impedances are usually used to flatten out the gain/frequency and hence the phase/frequency characteristic of the amplifier. Recommended operating conditions along with expressions for calculation of gain and circuit values are given in figure 9. Only a simple two-terminal interstage coupling network is shown in this figure.

The performance and gain-per-stage of a video amplifier can be improved by the use of increasingly complex two-terminal interstage coupling networks or through the use of four-terminal coupling networks or filters between successive stages. The reader is referred to Terman's *"Radio Engineer's Handbook"* for design data on such interstage coupling networks.

6-7 Other Interstage Coupling Methods

Figure 10 illustrates, in addition to resistance-capacitance interstage coupling, seven additional methods in which coupling between two successive stages of an audio-frequency amplifier may be accomplished. Although resistance-capacitance coupling is most commonly used, there are certain circuit conditions wherein coupling methods other than resistance capacitance are more effective.

Transformer Coupling Transformer coupling, as illustrated in figure 10B, is seldom used at the present time between two successive single-ended stages of an audio amplifier. There are several reasons why resistance coupling is favored over transformer coupling between two successive single-ended stages. These are: (1) a transformer having frequency characteristics comparable with a properly designed R-C stage is very expensive; (2) transformers, unless they are very well shielded, will pick up inductive hum from nearby power and filament transformers; (3) the phase characteristics of step-up interstage transformers are poor, making very difficult the inclusion of a transformer of this type within a feedback loop; and (4) transformers are heavy.

However, there is one circuit application where a step-up interstage transformer is of considerable assistance to the designer; this is the case where it is desired to obtain a large amount of voltage to excite the grid of a cathode follower or of a high-power Class A amplifier from a tube operating at a moderate plate voltage. Under these conditions it is possible to obtain a peak voltage on the secondary of the transformer of a value somewhat greater than the d-c plate supply voltage of the tube supplying the primary of the transformer.

Push-Pull Transformer Interstage Coupling Push-pull transformer coupling between two stages is illustrated in figure 10C. This interstage coupling arrangement is fairly commonly used. The system is particularly effective when it is desired, as in the system just described, to obtain a fairly high voltage to excite the grids of a high-power audio stage. The arrangement is also very good when it is desired to apply feedback to the grids of the push-pull stage by applying the feedback voltage to the low-potential sides of the two push-pull secondaries.

Impedance Coupling Impedance coupling between two stages is shown in figure 10D. This circuit arrangement is seldom used, but it offers one strong advantage over R-C interstage coupling. This advantage is the fact that, since the operating voltage on the tube with the impedance in the plate circuit is the plate supply voltage, it is possible to obtain approximately twice the peak voltage output that it is possible to obtain with R-C coupling. This is because, as has been

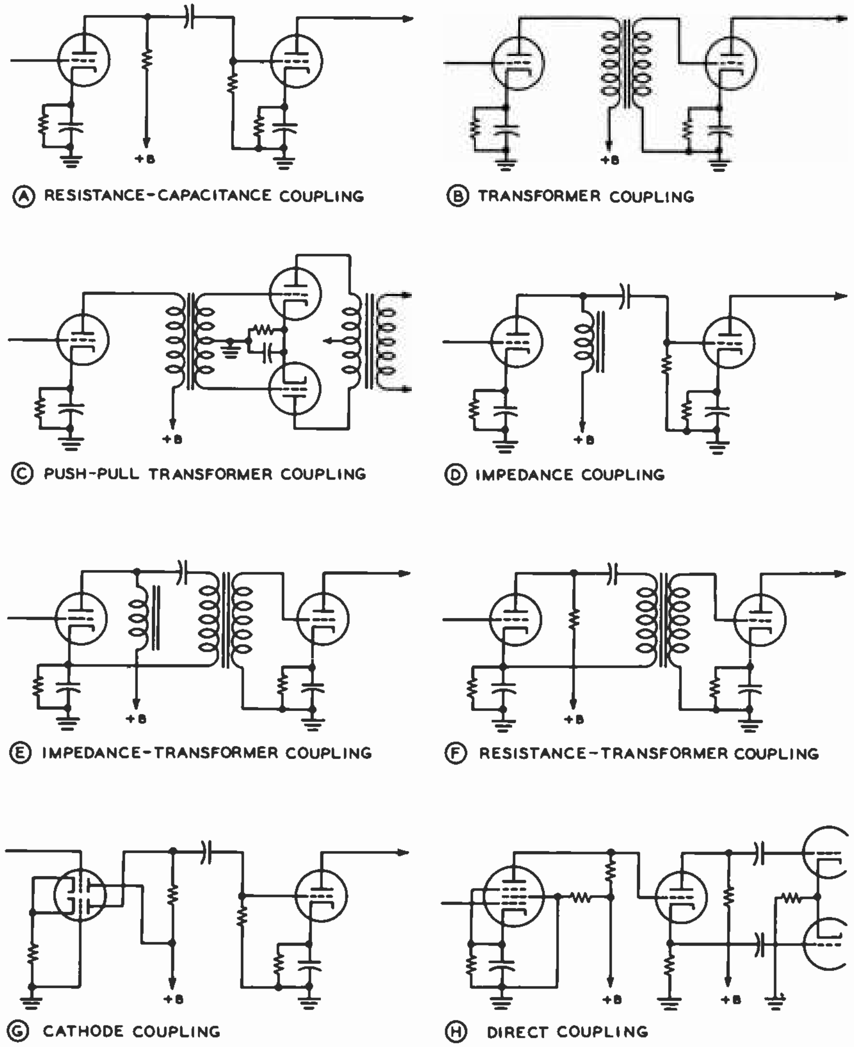
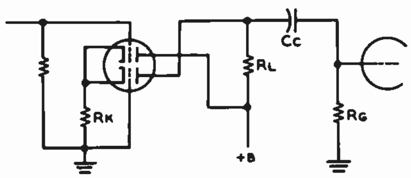


Figure 10
INTERSTAGE COUPLING METHODS FOR AUDIO FREQUENCY VOLTAGE AMPLIFIERS

mentioned before, the d-c plate voltage on an R-C stage is approximately one-half the plate supply voltage.

Impedance-Transformer and Resistance-Transformer Coupling These two circuit arrangements, illustrated in figures 10E and 10F, are employed when it is desired to use transformer coupling for the reasons cited above, but where it is desired that the d-c plate current of the amplifier stage be isolated from the primary of the coupling transformer. With most types of high-permeability wide-response transformers it is necessary that there be no direct-current flow through the windings of the transformer. The impedance-transformer arrangement of figure 10E will give a higher voltage output from the stage but is not often used since the plate coupling impedance (choke) must have very high inductance and very low distributed capacitance in order not to restrict the range of



$G_M' = -G_M \frac{G}{2G+1}$ $G = R_K G_M \left(1 + \frac{1}{\mu}\right)$

R_K = CATHODE RESISTOR

$R_P' = R_P \frac{2G+1}{G+1}$ G_M = G_M OF EACH TUBE

μ = μ OF EACH TUBE

$\mu' = -\mu \frac{G}{G+1}$ R_P = R_P OF EACH TUBE

EQUIVALENT FACTORS INDICATED ABOVE BY (′) ARE THOSE OBTAINED BY USING AN AMPLIFIER WITH A PAIR OF SIMILAR TUBE TYPES IN CIRCUIT SHOWN ABOVE.

Figure 11

Equivalent factors for a pair of similar triodes operating as a cathode-coupled audio-frequency voltage amplifier.

the transformer which it and its associated tube feed. The resistance-transformer arrangement of figure 10F is ordinarily quite satisfactory where it is desired to feed a transformer from a voltage amplifier stage with no d.c.in the transformer primary.

Cathode Coupling The cathode coupling arrangement of figure 10G has been widely used only comparatively recently. One outstanding characteristic of such a circuit is that there is no phase reversal between the grid and the plate circuit. All other common types of interstage coupling are accompanied by a 180° phase reversal between the grid circuit and the plate circuit of the tube.

Figure 11 gives the expressions for determining the appropriate factors for an equivalent triode obtained through the use of a pair of similar triodes connected in the cathode-coupled circuit shown. With these equivalent triode factors it is possible to use the expressions shown in figure 5 to determine the gain of the stage at different frequencies. The input capacitance of such a stage is less than that of one of the triodes, the effective grid-to-plate capacitance is very much less (it is so much less that such a stage may be used as an r-f amplifier without neutralization), and the output capacitance is approximately equal to the grid-to-plate capacitance of one of the triode sections. This circuit is particularly effective with tubes such as the 6J6, 6N7, and 6SN7-GT which have two similar triodes in one envelope. An appropriate value of cathode resistor to use for such a stage is the value which would be used for the cathode resistor of a conventional amplifier using *one* of the same type tubes with the values of plate voltage and load resistance to be used for the cathode-coupled stage.

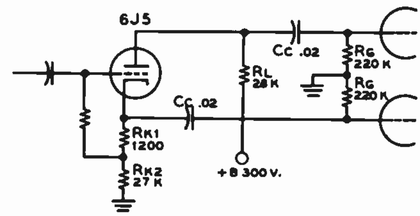
Inspection of the equations in figure 11 shows that as the cathode resistor is made smaller, to approach zero, the G_m approaches zero, the plate resistance approaches the R_p of one tube, and the mu approaches zero. As the cathode resistor is made very large the G_m approaches one half that of a single tube of the same type, the plate resistance approaches twice that of one tube, and the mu approaches the same value as one tube. But since the G_m of each tube decreases as the cathode resistor is made larger (since the plate current will decrease on each tube) the optimum value of cathode resistor will be found to be in the vicinity of the value mentioned in the previous paragraph.

Direct Coupling Direct coupling between successive amplifier stages (plate of first stage connected directly to the grid of the succeeding stage) is complicated by the fact that the grid of an amplifier stage must be operated at an average negative potential with respect to the cathode of that stage. However, if the cathode of the second amplifier stage can be operated at a potential more positive than the plate of the preceding stage by the amount of the grid bias on the second amplifier stage, this direct connection between the plate of one stage and the grid of the succeeding stage can be used. Figure 10H illustrates an application of this principle in the coupling of a pentode amplifier stage to the grid of a "hot-cathode" phase inverter. In this arrangement the values of cathode, screen, and plate resistor in the pentode stage are chosen such that the plate of the pentode is at approximately 0.3 times the plate supply potential. The succeeding phase-inverter stage then operates with conventional values of cathode and plate resistor (same value of resistance) in its normal manner. This type of phase inverter is described in more detail in the section to follow.

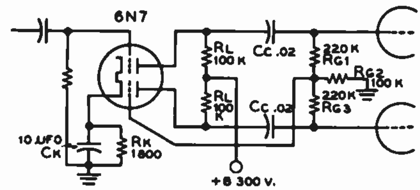
6-8 Phase Inverters

It is necessary in order to excite the grids of a push-pull stage that voltages equal in amplitude and opposite in polarity be applied to the two grids. These voltages may be obtained through the use of a push-pull input transformer such as is shown in figure 10C. It is possible also, without the attendant bulk and expense of a push-pull input transformer, to obtain voltages of the proper polarity and phase through the use of a so-called *phase-inverter* stage. There are a large number of phase inversion circuits which have been developed and applied but the three shown in figure 12 have been found over a period of time to be the most satisfactory from the point of view of the number of components required and from the standpoint of the accuracy with which the two out-of-phase voltages are held to the same amplitude with changes in supply voltage and changes in tubes.

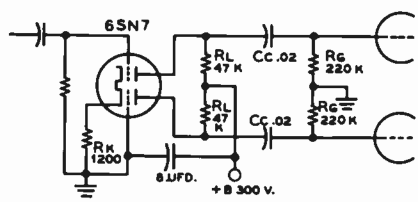
All of these vacuum tube phase inverters are based upon the fact that a 180° phase shift occurs within a vacuum tube between the grid input voltage and the plate output voltage. In certain circuits, the fact that the grid input voltage and the voltage appearing across the cathode bias resistor are in phase is used for phase inversion purposes.



Ⓐ "HOT CATHODE" PHASE INVERTER



Ⓑ "FLOATING PARAPHRASE" PHASE INVERTER



Ⓒ CATHODE COUPLED PHASE INVERTER

Figure 12

THREE POPULAR PHASE-INVERTER CIRCUITS WITH RECOMMENDED VALUES FOR CIRCUIT COMPONENTS

"Hot-Cathode" Phase Inverter Figure 12A illustrates the hot-cathode type of phase inverter. This type of phase inverter is the simplest of the three types since it requires only one tube and a minimum of circuit components. It is particularly simple when directly coupled from the plate of a pentode amplifier stage as shown in figure 10H. The circuit does, however, possess the following two disadvantages: (1) the cathode of the tube must run at a potential of approximately 0.3 times the plate supply voltage above the heater when a grounded common heater winding is used for this tube as well as the other heater-cathode tubes in a receiver or amplifier: (2) the circuit actually has a loss in voltage from its input to either of the output grids — about 0.9 times the input voltage will be applied to each of these grids. This does represent a voltage gain of about 1.8 in *total* voltage output with respect to input (grid-to-grid output voltage) but it is still small with respect to the other two phase inverter circuits shown.

Recommended component values for use with a 6J5 tube in this circuit are shown in figure 12A. If it is desired to use another tube in this circuit, appropriate values for the operation of that tube as a conventional amplifier can be obtained from manufacturer's tube data. The value of R_L obtained should be divided by two, and this new value of resistance placed in the circuit as R_L. The value of R_k from tube manual tables should then be used as R_{k1} in this circuit, and then the total of R_{k1} and R_{k2} should be equal to R_L.

"Floating Paraphrase" Phase Inverter An alternate type of phase inverter sometimes called the "floating paraphrase" is illustrated in figure 12B. This circuit is quite often used with a 6N7 tube, and appropriate values for the 6N7 tube in this application are shown. The circuit shown with the values given will give a voltage gain of approximately 21 from the input grid to each of the grids of the succeeding stage. It is capable of approximately 70 volts peak output to each grid.

The circuit inherently has a small unbalance in output voltage. This unbalance can be eliminated, if it is required for some special application, by making the resistor R_{g1} a few per cent lower in resistance value than R_{g3}.

Cathode-Coupled Phase Inverter The circuit shown in figure 12C gives approximately one-half the voltage gain from the input grid to either of the grids of the succeeding stage that would be obtained from a single tube of the same type operating as a conventional R-C amplifier stage. Thus, with a 6SN7-GT tube as shown (two 6J5's in one

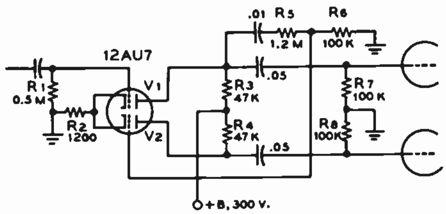


Figure 13
VOLTAGE DIVIDER PHASE INVERTER

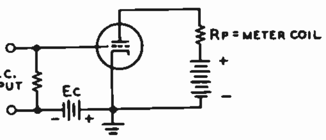


Figure 14
SIMPLE VACUUM TUBE VOLTMETER

envelope) the voltage gain from the input grid to either of the output grids will be approximately 7 — the gain is, of course, 14 from the input to both output grids. The phase characteristics are such that the circuit is commonly used in deriving push-pull deflection voltage for a cathode-ray tube from a signal ended input signal.

The first half of the 6SN7 is used as an amplifier to increase the amplitude of the applied signal to the desired level. The second half of the 6SN7 is used as an inverter and amplifier to produce a signal of the same amplitude but of opposite polarity. Since the common cathode resistor, R_k, is not by-passed the voltage across it is the algebraic sum of the two plate currents and has the same shape and polarity as the voltage applied to the input grid of the first half of the 6SN7. When a signal, e, is applied to the input circuit, the effective grid-cathode voltage of the first section is $Ae/2$, when A is the gain of the first section. Since the grid of the second section of the 6SN7 is grounded, the effect of the signal voltage across R_k (equal to $e/2$ if R_k is the proper value) is the same as though a signal of the same amplitude but of opposite polarity were applied to the grid. The output of the second section is equal to $-Ae/2$ if the plate load resistors are the same for both tube sections.

Voltage Divider Phase Inverter A commonly used phase inverter is shown in figure 13. The input section (V_1) is connected as a conventional amplifier. The output voltage from V_1 is impressed on the voltage divider R_5-R_6. The values of R_5 and R_6 are in such a ratio that the voltage impressed upon the grid of V_2 is 1/A times the output voltage of V_1, where A is the amplification factor of V_1. The output of V_2 is then of the same amplitude as the output of V_1, but of opposite phase.

6-9 D-C Amplifiers

Direct current amplifiers are special types used where amplification of very slow variations in voltage, or of d-c voltages is desired. A simple d-c amplifier consists of a single tube with a grid resistor across the input terminals, and the load in the plate circuit.

Basic D-C Amplifier Circuit A simple d-c amplifier circuit is shown in figure 14. The plate load may be a mechanical device, such as a relay or a meter, or the output voltage may be developed across a resistor and used for various control purposes. The tube is biased by E_c and, a fixed value of plate current flows, causing a fixed voltage drop across the plate load resistor, R_p. When a positive d-c voltage is applied to the input terminals it cancels part of the negative grid bias, making the grid more positive with respect to the cathode. This grid voltage change permits a greater amount of plate current to flow, and develops a greater voltage drop across the plate load resistor. A negative input voltage would decrease the plate current and decrease the voltage drop across R_p. The varying voltage drop across R_p may be employed as a control voltage for relays or other devices.

The D-C Vacuum Tube Voltmeter One of the most important applications of a d-c amplifier is as a d-c vacuum-tube voltmeter. A simple v.t.v.m. is shown in figure 15. The voltage to be measured is applied to the voltage divider, R_1, R_2, R_3, by means of the "voltage range" switch. Resistor R_4 is used to protect the meter from excessive input voltage to the v.t.v.m. In the plate circuit of the tube an additional battery and a variable resistor ("zero adjustment") are used to balance out the meter reading of the normal plate current of the tube. The zero adjustment potentiometer can be so adjusted that the meter M reads zero current with no input voltage to the v.t.v.m. When a d-c input voltage is applied to the circuit, current flows through

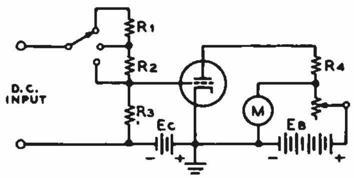


Figure 15
D-C VACUUM TUBE VOLTMETER

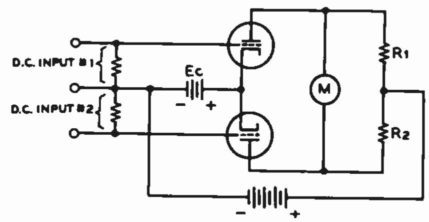


Figure 16
BRIDGE-TYPE VACUUM TUBE VOLTMETER

the meter, and the meter reading is proportional to the applied d-c voltage.

The Bridge-type V.T.V.M. Another important use of a d-c amplifier is to show the exact point of balance between two d-c voltages. This is done by means of a bridge circuit with two d-c amplifiers serving as two legs of the bridge (figure 16). With no input signal, and with matched triodes, no current will be read on meter M, since the IR drops across R_1 and R_2 are identical. When a signal is applied to one tube, the IR drops in the plate circuits become unbalanced, and meter M indicates the unbalance. In the same way, two d-c voltages may be compared if they are applied to the two input circuits. When the voltages are equal, the bridge is balanced and no current flows through the meter. If one voltage changes, the bridge becomes unbalanced and indication of this will be noted by a reading of the meter.

6-10 Single-ended Triode Amplifiers

Figure 17 illustrates five circuits for the operation of Class A triode amplifier stages. Since the cathode current of a triode Class A_1 (no grid current) amplifier stage is constant with and without excitation, it is common practice to operate the tube with cathode bias. Recommended operating conditions in regard to plate voltage, grid bias, and load impedance for conventional triode amplifier stages are given in the RCA Tube Manual, RC-16.

Extended Class A Operation It is possible, under certain conditions to operate single-ended triode amplifier stages (and pentode and tetrode stages as well) with grid excitation of sufficient amplitude that grid current is taken by the tube on peaks. This type of operation is called Class A_2 and is characterized by increased plate-circuit efficiency over straight Class A amplification without grid current. The normal Class A_1 amplifier power stage will operate with a plate circuit efficiency of from 20 per cent to perhaps 35 per cent. Through the use of Class A_2 operation it is possible to increase this plate circuit efficiency to approximately 38 to 45 per cent. However, such operation requires careful choice of the value of plate load impedance, a grid bias supply with good regulation (since the tube draws grid current on peaks although the plate current does not change with signal), and a driver tube with moderate power capability to excite the grid of the Class A_2 tube.

Figures 17D and 17E illustrate two methods of connection for such stages. Tubes such as the 845, 849, and 304TL are suitable for such a stage. In each case the grid bias is approximately the same as would be used for a Class A_1 amplifier using the same tube, and as mentioned before, fixed bias must be used along with an audio driver of good regulation — preferably a triode stage with a 1:1 or step-down driver transformer. In each case it will be found that the correct value of plate load impedance will be increased about 40 per cent over the value recommended by the tube manufacturer for Class A_1 operation of the tube.

Operation Characteristics of a Triode Power Amplifier A Class A power amplifier operates in such a way as to amplify as faithfully as possible the waveform applied to the grid of the tube. Large power output is of more importance than high voltage amplification, consequently gain characteristics may be sacrificed in power tube design to obtain more important power handling capabilities. Class A power tubes, such as the 45, 2A3 and 6AS7 are characterized by a low amplification factor, high plate dissipation and relatively high filament emission.

The operating characteristics of a Class A

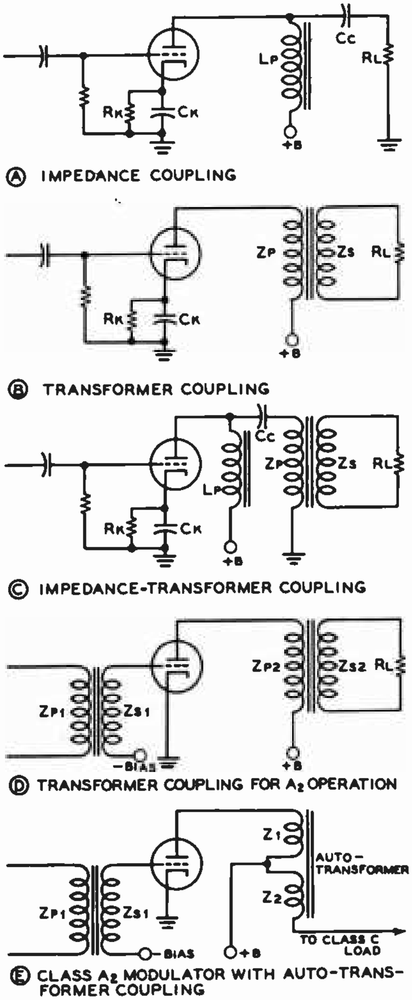


Figure 17

Output coupling arrangements for single-ended Class A triode audio-frequency power amplifiers.

triode amplifier employing an output transformer-coupled load may be calculated from the plate family of curves for the particular tube in question by employing the following steps:

1- The load resistance should be approximately twice the plate resistance of the tube for maximum undistorted power output. Remember this fact for a quick check on calculations.

2- Calculate the zero-signal bias voltage (E_g).

$$E_g = \frac{-(0.68 \times E_{bb})}{\mu}$$

Where E_{bb} is the actual plate voltage of the Class A stage, and μ is the amplification factor of the tube.

3- Locate the E_g bias point on the I_p vs. E_p graph where the E_g bias line crosses the plate voltage line, as shown in figure 18. Call this point P.

4- Locate on the plate family of curves the value of zero-signal plate current, I_p, corresponding to the operating point, P.

5- Locate $2 \times I_p$ (twice the value of I_p) on the plate current axis (Y-axis). This point corresponds to the value of maximum signal plate current, i_{max}.

6- Locate point x on the d-c bias curve at zero volts ($E_g = 0$), corresponding to the value of i_{max}.

7- Draw a straight line ($x - y$) through points x and P. This line is *the load resistance line*. Its slope corresponds to the value of the load resistance.

8- Load Resistance, (in ohms)

$$R_L = \frac{e_{max} - e_{min}}{i_{max} - i_{min}}$$

where e is in volts, i is in amperes, and R_L is in ohms.

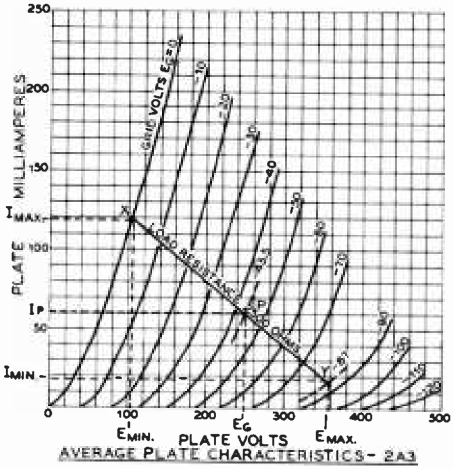
9- Check: Multiply the zero-signal plate current, I_p, by the operating plate voltage, E_p. If the plate dissipation rating of the tube is exceeded, it is necessary to increase the bias (E_g) on the tube so that the plate dissipation falls within the maximum rating of the tube. If this step is taken, operations 2 through 8 must be repeated with the new value of E_g.

10- For maximum power output, the peak a-c grid voltage on the tube should swing to $2E_g$ on the negative cycle, and to zero-bias on the positive cycle. At the peak of the negative swing, the plate voltage reaches e_{max} and the plate current drops to i_{min}. On the positive swing of the grid signal, the plate voltage drops to e_{min} and the plate current reaches i_{max}. The power output of the tube is:
Power Output (watts)

$$P_o = \frac{(i_{max} - i_{min}) \times (e_{max} - e_{min})}{8}$$

where i is in amperes and e is in volts.

11- The second harmonic distortion generated in a single-ended Class A triode amplifier, expressed as a percentage of the fundamental output signal is:



$\mu = 4.2$ $R_P = 800$ OHMS
PLATE DISSIPATION = 15 WATTS

LOAD RESISTANCE

$$R_L = \frac{E_{MAX.} - E_{MIN.}}{I_{MAX.} - I_{MIN.}} \text{ OHMS}$$

POWER OUTPUT

$$P_O = \frac{(I_{MAX.} - I_{MIN.})\ (E_{MAX.} - E_{MIN.})}{8} \text{ WATTS}$$

SECOND HARMONIC DISTORTION

$$D_2 = \frac{\frac{(I_{MAX.} + I_{MIN.})}{2} - I_P}{I_{MAX.} - I_{MIN.}} \times 100 \text{ PERCENT}$$

Figure 18

Formulas for determining the operating conditions for a Class A triode single-ended audio-frequency power output stage. A typical load line has been drawn on the average plate characteristics of a type 2A3 tube to illustrate the procedure.

% 2d harmonic =

$$\frac{\frac{(i_{max} - i_{min})}{2} - I_p}{i_{max} - i_{min}} (\times 100)$$

Figure 18 illustrates the above steps as applied to a single Class A 2A3 amplifier stage.

6-11 Single-ended Pentode Amplifiers

Figure 19 illustrates the conventional circuit for a single-ended tetrode or pentode amplifier stage. Tubes of this type have largely replaced triodes in the output stage of receivers and amplifiers due to the higher plate efficiency (30%–40%) with which they operate. Tetrode and pentode tubes do, however, introduce a considerably greater amount of harmonic distortion in their output circuit, particularly odd harmonics. In addition, their plate circuit impedance (which acts in an amplifier to damp loudspeaker overshoot and ringing, and acts in a driver stage to provide good regulation) is many times higher than that of an equivalent triode. The application of negative feedback acts both to reduce distortion and to reduce the effective plate circuit impedance of these tubes.

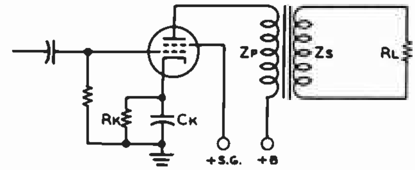


Figure 19

Normal single-ended pentode or beam tetrode audio-frequency power output stage.

Operating Characteristics of a Pentode Power Amplifier The operating characteristics of pentode power amplifiers may be obtained from the plate family of curves, much as in the manner applied to triode tubes. A typical family of pentode plate curves is shown in figure 20. It can be seen from these curves that the plate current of the tube is relatively independent of the applied plate voltage, but is sensitive to screen voltage. In general, the correct pentode load resistance is about

$$\frac{0.9\ E_p}{I_p},$$

and the power output is somewhat less than

$$\frac{E_p \times I_p}{2}.$$

These formulae may be used for a quick check on more precise calculations. To obtain the operating parameters for Class A pentode amplifiers, the following steps are taken:

1- The i_{max} point is chosen so as to fall on the zero-bias curve, just above the "knee" of the curve (point A, figure 20).

2- A preliminary operating point, P, is determined by the intersection of the plate voltage line, E_p, and the line of $i_{max}/2$.

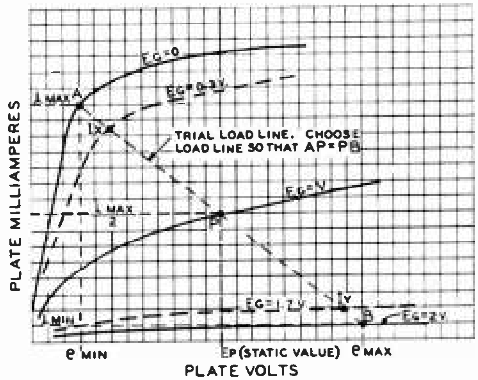


Figure 20

GRAPHIC DETERMINATION OF OPERATING CHARACTERISTICS OF A PENTODE POWER AMPLIFIER

"V" is the negative control grid voltage at the operating point P

The grid voltage curve that this point falls upon should be one that is about ½ the value of E_g required to cut the plate current to a very low value (Point B). Point B represents i_{min} on the plate current axis (y–axis). The line $i_{max}/2$ should be located half-way between i_{max} and i_{min}.

3- A trial load line is constructed about point P and point A in such a way that the lengths A-P and P-B are approximately equal.

4- When the most satisfactory load line has been determined, the load resistance may calculated:

$$R_L = \frac{e_{max} - e_{min}}{i_{max} - i_{min}}$$

5- The operating bias (E_g) is the bias at point P.

6- The power output is:

Power Output (watts)

$$P_o = \frac{(i_{max} - i_{min}) + 1.41\,(I_x - I_y)^2 \times R_L}{32}$$

Where I_x is the plate current at the point on the load line where the grid voltage, e_g, is equal to: $E_g - 0.7\ E_g$; and where I_y is the plate current at the point where e_g is equal to: $E_g + 0.7\ E_g$.

7- The percentage harmonic distortion is:

% 2d harmonic distortion

$$= \frac{i_{max} - i_{min} - 2\,I_p}{i_{max} - i_{min} + 1.41\,(I_x - I_y)} \times 100$$

Where I_p is the static plate current of of the tube.

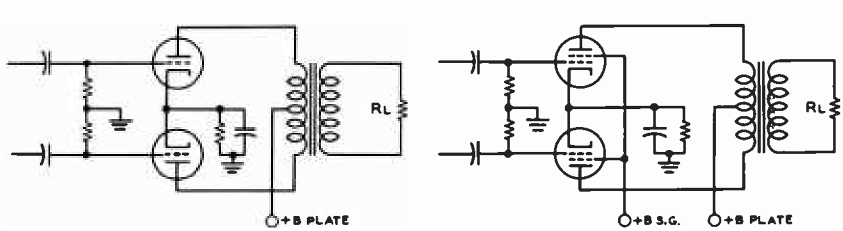
% 3d harmonic distortion

$$= \frac{i_{max} - i_{min} - 1.41\,(I_x - I_y)}{i_{max} - i_{min} + 1.41\,(I_x - I_y)} \times 100$$

6-12 Push-Pull Audio Amplifiers

A number of advantages are obtained through the use of the push-pull connection of two or four tubes in an audio-frequency power amplifier. Two conventional circuits for the use of triode and tetrode tubes in the push-pull connection are shown in figure 21. The two main advantages of the push-pull circuit arrangement are: (1) the magnetizing effect of the plate currents of the output tubes is cancelled in the windings of the output transformer; (2) even harmonics of the input signal (second and fourth harmonics primarily) generated in the push-pull stage are cancelled when the tubes are balanced.

The cancellation of even harmonics generated in the stage allows the tubes to be oper-



PUSH-PULL TRIODE AND TETRODE

FIGURE 21

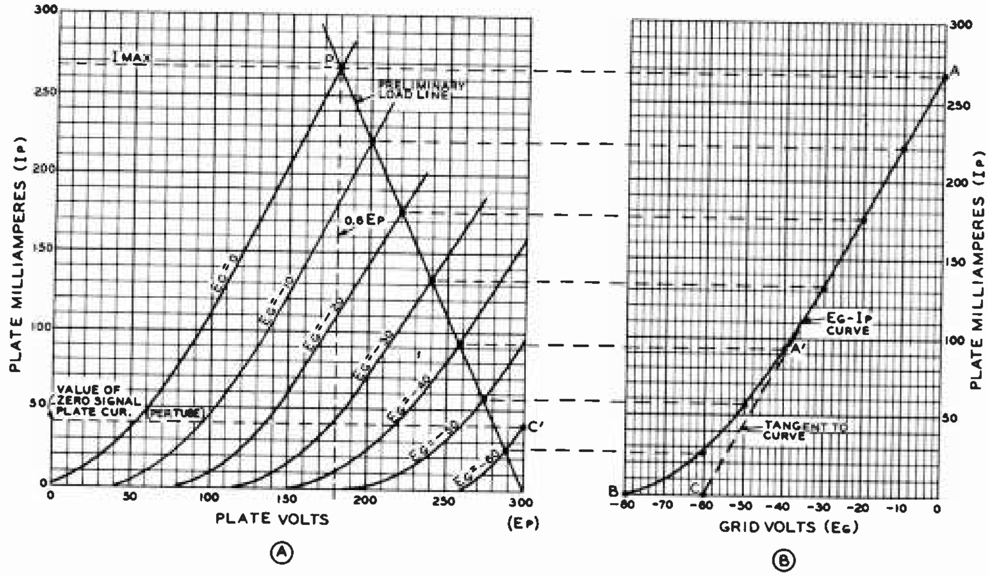


Figure 22

DETERMINATION OF OPERATING PARAMETERS FOR PUSH-PULL CLASS A TRIODE TUBES

ated Class AB — in other words the tubes may be operated with bias and input signals of such amplitude that the plate current of alternate tubes may be cut off during a portion of the input voltage cycle. If a tube were operated in such a manner in a single-ended amplifier the second harmonic amplitude generated would be prohibitively high.

Push-pull Class AB operation allows a plate circuit efficiency of from 45 to 60 per cent to be obtained in an amplifier stage depending upon whether or not the exciting voltage is of such amplitude that grid current is drawn by the tubes. If grid current is taken on input voltage peaks the amplifier is said to be operating Class AB_2 and the plate circuit efficiency can be as high as the upper value just mentioned. If grid current is not taken by the stage it is said to be operating Class AB_1 and the plate circuit efficiency will be toward the lower end of the range just quoted. In all Class AB amplifiers the plate current will increase from 40 to 150 per cent over the no-signal value when full signal is applied.

Operating Characteristics of Push-Pull Class A Triode Power Amplifier The operating characteristics of push-pull Class A amplifiers may also be determined from the plate family of curves for a particular triode tube by the following steps:

1- Erect a vertical line from the plate voltage axis (x-axis) at 0.6 E_p (figure 22), which intersects the $E_g = 0$ curve. This point of intersection (P), interpolated to the plate current axis (y-axis) may be taken as i_{max}. It is assumed for simplification that i_{max} occurs at the point of the zero-bias curve corresponding to 0.6 E_p.

2- The power output obtainable from the two tubes is:

$$\text{Power output } (P_o) = \frac{i_{max} \times E_p}{5}$$

where P_o is expressed in watts, i_{max} in amperes, and E_p is the applied plate voltage.

3- Draw a preliminary load line through point P to the E_P point located on the x-axis (the zero plate current line). This load line represents ¼ of the actual plate-to-plate load of the Class A tubes. Therefore:

$$R_L \text{ (plate-to-plate)} = 4 \times \frac{E_p - 0.6\, E_p}{i_{max}}$$

$$= \frac{1.6\, E_p}{i_{max}}.$$

where R_L is expressed in ohms, E_p in volts, and i_{max} in amperes.

Figure 22 illustrates the above steps applied to a push-pull Class A amplifier using two 2A3 tubes.

4- The average plate current is 0.636 i_{max}, and, multiplied by the plate voltage, E_p, will give the average watts input to the plates of the two tubes. The power output should be subtracted from this value to obtain the total operating plate dissipation of the two tubes. If the plate dissipation is excessive, a slightly higher value of R_L should be chosen to limit the plate dissipation.

5- The correct value of operating bias, and the static plate current for the push-pull tubes may be determined from the E_g vs. I_p curves, which are a derivation of the E_p vs. I_p curves for various values of E_g.

6- The E_g vs. I_p curve may be constructed in this manner: Values of grid bias are read from the intersection of each grid bias curve with the load line. These points are transferred to the E_g vs. I_p graph to produce a curved line, A-B. If the grid bias curves of the E_p vs. I_p graph were straight lines, the lines of the E_g vs. I_p graph would also be straight This is usually not the case. A tangent to this curve is therefore drawn, starting at point A′, and intersecting the grid voltage abscissa (x-axis). This intersection (C) is the operating bias point for fixed bias operation.

7- This operating bias point may now be plotted on the original E_g vs. I_p family of curves (C′), and the zero-signal current produced by this bias is determined.

This operating bias point (C′) does not fall on the operating load line, as in the case of a single-ended amplifier.

8- Under conditions of maximum power output, the exciting signal voltage swings from zero-bias voltage to zero-bias voltage for each of the tubes on each half of the signal cycle. Second harmonic distortion is largely cancelled out.

6-13 Class B Audio Frequency Power Amplifiers

The Class B audio-frequency power amplifier (figure 23) operates at a higher plate-circuit efficiency than any of the previously described types of audio power amplifiers. Full-signal plate-circuit efficiencies of 60 to 70 per cent are readily obtainable with the tube types at present available for this type of work. Since the plate circuit efficiency is higher, smaller tubes of lower plate dissipation may be used in a Class B power amplifier of a given power output than can be used in any other conventional type of audio amplifier. An additional factor in favor of the Class B audio amplifier is the fact that the power input to the stage is relatively low under no-signal conditions. It is for these reasons that this type of amplifier has largely superseded other types in the generation of audio-frequency levels from perhaps 100 watts on up to levels of approximately 150,000 watts as required for large short-wave-broadcast stations.

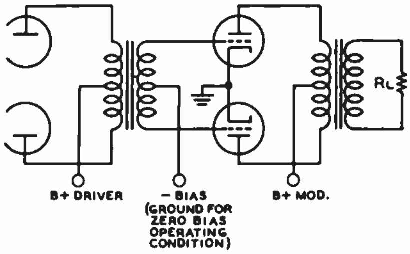


Figure 23
CLASS B AUDIO FREQUENCY POWER AMPLIFIER

Disadvantages of Class B Amplifier Operation There are attendant disadvantageous features to the operation of a power amplifier of this type; but all these disadvantages can be overcome by proper design of the circuits associated with the power amplifier stage. These disadvantages are: (1) The Class B audio amplifier requires driving power in its grid circuit; this disadvantage can be overcome by the use of an oversize power stage preceding the Class B stage with a step-down transformer between the driver stage and the Class-B grids. Degenerative feedback is sometimes employed to reduce the plate impedance of the driver stage and thus to improve the voltage regulation under the varying load presented by the Class B grids. (2) The Class B stage requires a constant value of average grid bias to be supplied in spite of the fact that the grid current on the stage is zero over most of the cycle but rises to values as high as one-third of the peak plate current on the peak of the exciting voltage cycle. Special regulated bias supplies have been used for this application, or B batteries can be used. However, a number of tubes especially designed for Class B audio amplifiers have been developed which require zero average grid bias for their operation. The 811A, 838, 805, 809, HY-5514, and TZ-40 are examples of this type of tube. All these so-called "zero-bias" tubes have rated operating conditions up to moderate plate voltages wherein they can be operated without grid bias. As the plate voltage is increased to to their maximum ratings, however, a small amount of grid bias, such as could be obtained from several 4 ½-volt C batteries, is required.

(3), A Class B audio-frequency power amplifier or modulator requires a source of plate supply voltage having reasonably good regulation. This requirement led to the development of the *swinging choke.* The swinging choke is essentially a conventional filter choke in which the core air gap has been reduced. This reduction in the air gap allows the choke to have a much greater value of inductance with low current values such as are encountered with no signal or small signal being applied to the Class B stage. With a higher value of current such as would be taken by a Class B stage with full signal applied the inductance of the choke drops to a much lower value. With a swinging choke of this type, having adequate current rating, as the input inductor in the filter system for a rectifier power supply, the regulation will be improved to a point which is normally adequate for a power supply for a Class B amplifier or modulator stage.

Calculation of Operating Conditions of Class B Power Amplifiers The following procedure can be used for the calculation of the operating conditions of Class B power amplifiers when they are to operate into a resistive load such as the type of load presented by a Class C power amplifier. This procedure will be found quite satisfactory for the application of vacuum tubes as Class B modulators when it is desired to operate the tubes under conditions which are not specified in the tube operating characteristics published by the tube manufacturer. The same procedure can be used with equal effectiveness for the calculation of the operating conditions of beam tetrodes as Class AB_2 amplifiers or modulators when the resting plate current on the tubes (no signal condition) is less than 25 or 30 per cent of the maximum-signal plate current.

1- With the average plate characteristics of the tube as published by the manufacturer before you, select a point on the $E_p = E_g$ (diode bend) line at about twice the plate current you expect the tubes to kick to under modulation. If beam tetrode tubes are concerned, select a point at about the same amount of plate current mentioned above, just to the right of the region where the I_b line takes a sharp curve downward. This will be the first trial point, and the plate voltage at the point chosen should be not more than about 20 per cent of the d-c voltage applied to the tubes if good plate-circuit efficiency is desired.
2- Note down the value of i_{pmax} and e_{pmin} at this point.
3- Subtract the value of e_{pmin} from the d-c plate voltage on the tubes.
4- Substitute the values obtained in the following equations:

$$P_o = \frac{i_{pmax}(E_{bb} - e_{pmin})}{2} = \text{Power output from 2 tubes}$$

$$R_L = 4\frac{(E_{bb} - e_{pmin})}{i_{pmax}}$$

$$= \text{Plate-to-plate load for 2 tubes}$$

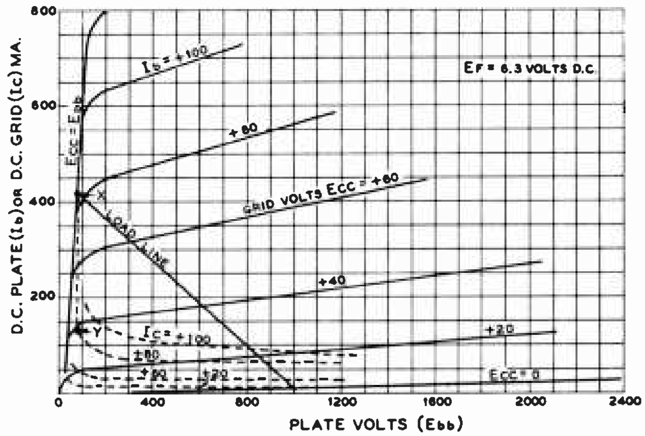
Full signal efficiency (N_p) =

$$78.5\left(1 - \frac{e_{pmin}}{E_{bb}}\right)$$

Effects of Speech Clipping All the above equations are true for sine-wave operating conditions of the tubes concerned. However, if a speech clipper is being used in the speech amplifier, or if it is desired to calculate the operating conditions on the basis of the fact that the ratio of peak power to average power in a speech wave is approximately 4-to-1 as contrasted to the ratio of 2-to-1 in a sine wave — in other words, when non-sinusoidal waves such as plain speech or speech that has passed through a clipper are concerned, we are no longer concerned with average power output of the modulator as far as its capability of modulating a Class-C amplifier is concerned; we are concerned with its *peak-power-output* capability.

Under these conditions we call upon other, more general relationships. The first of these is: It requires a *peak* power output *equal* to the Class-C stage input to modulate that input fully.

The second one is: The average power output required of the modulator is equal to the shape factor of the modulating wave multiplied by the input to the Class-C stage. The shape factor of unclipped speech is approximately 0.25. The shape factor of a sine wave is 0.5. The shape factor of a speech wave that



AVERAGE PLATE CHARACTERISTICS TYPE 811 AND 811-A

Figure 24

Typical Class B a-f amplifier load line. The load line has been drawn on the average characteristics of a type 811 tube.

has been passed through a clipper-filter arrangement is somewhere between 0.25 and 0.9 depending upon the amount of clipping that has taken place. With 15 or 20 db of clipping the shape factor may be as high as the figure of 0.9 mentioned above. This means that the audio power output of the modulator will be 90% of the input to the Class-C stage. Thus with a kilowatt input we would be putting 900 watts of audio into the Class-C stage for 100 per cent modulation as contrasted to perhaps 250 watts for unclipped speech modulation of 100 per cent.

Sample Calculation for 811A Tubes Figure 24 shows a set of plate characteristics for a type 811A tube with a load line for Class B operation. Figure 25 lists a sample calculation for determining the proper operating conditions for obtaining approximately 185 watts output from a pair of the tubes with 1000 volts d-c plate potential. Also shown in figure 25 is the method of determining the proper ratio for the modulation transformer to couple between the 811's or 811A's and the anticipated final amplifier which is to operate at 2000 plate volts and 175 ma. plate current.

Modulation Transformer Calculation The method illustrated in figure 25 can be used in general for the determination of the proper transformer ratio to couple between the modulator tube and the amplifier to be modulated. The procedure can be stated as follows: (1) Determine the proper plate-to-plate load impedance for the modulator tubes either by the use of the type of calculation shown in figure 25, or by reference to the published characteristics on the tubes to be used. (2) Determine the load impedance which will be presented by the Class C amplifier stage to be modulated by dividing the operating plate voltage on that stage by the operating value of plate current in *amperes*. (3) Divide the Class C load impedance determined in (2)

SAMPLE CALCULATION

CONDITION: 2 TYPE 811 TUBES, E_{bb} = 1000
INPUT TO FINAL STAGE, 350 W.
PEAK POWER OUTPUT NEEDED = 350 + 6% = 370 W.
FINAL AMPLIFIER E_{bb} = 2000 V.
FINAL AMPLIFIER I_b = .175 A.
FINAL AMPLIFIER $Z_L = \frac{2000}{.175} = 11400\ \Omega$

EXAMPLE: CHOSE POINT ON 811 CHARACTERISTICS JUST TO RIGHT OF $E_{bb} = E_{cc}$.
I_P MAX. = .410 A. E_P MIN. = +100
I_G MAX. = .100 A. E_G MAX. = +80

PEAK P_O = .410 X (1000−100) = .410 X 900 = 369 W.
$R_L = 4 \times \frac{900}{.410} = 8800\ \Omega$
$N_P = 78.5\ (1 - \frac{100}{1000}) = 78.5\ (.9) = 70.5\ \%$
W_O (AVERAGE WITH SINE WAVE) $= \frac{P_O(\text{PEAK})}{2} = 184.5$
$W_{IN} = \frac{184.5}{70.5} = 260$ W.
I_b (MAXIMUM WITH SINE WAVE) = 260 MA
W_G PEAK = .100 X 80 = 8 W.
DRIVING POWER $= \frac{W_G\ \text{PK}}{2} = 4$ W.

TRANSFORMER:
$\frac{Z_S}{Z_P} = \frac{11400}{8800} = 1.29$
TURNS RATIO $= \sqrt{\frac{Z_S}{Z_P}} = \sqrt{1.29} = 1.14$ STEP UP

Figure 25

Typical calculation of operating conditions for a Class B a-f power amplifier using a pair of type 811 or 811A tubes. Plate characteristics and load line shown in figure 24.

above by the plate-to-plate load impedance for the modulator tubes determined in (1) above. The ratio determined in this way is the secondary-to-primary *impedance* ratio. (4) Take the square root of this ratio to determine the secondary-to-primary *turns* ratio. If the turns ratio is greater than one the use of a step-up transformer is required. If the turns ratio as determined in this way is less than one a step-down transformer is called for.

If the procedure shown in figure 25 has been used to calculate the operating conditions for the modulator tubes, the transformer ratio calculation can be checked in the following manner: Divide the plate voltage on the modulated amplifier by the total voltage swing on the modulator tubes: $2(E_{bb} - e_{min})$. This ratio should be quite close numerically to the transformer turns ratio as previously determined. The reason for this condition is that the ratio between the total primary voltage and the d-c plate supply voltage on the modulated stage is equal to the turns ratio of the transformer, since a peak secondary voltage equal to the plate voltage on the modulated stage is required to modulate this stage 100 per cent.

Use of Clipper Speech Amplifier with Tetrode Modulator Tubes When a clipper speech amplifier is used in conjunction with a Class B modulator stage, the plate current on that stage will kick to a higher value with modulation (due to the greater average power output and input) but the plate dissipation on the tubes will ordinarily be less than with sine-wave modulation. However, when tetrode tubes are used as modulators, the screen dissipation will be much greater than with sine-wave modulation. Care must be taken to insure that the screen dissipation rating on the modulator tubes is not exceeded under full modulation conditions with a clipper speech amplifier. The screen dissipation is equal to screen voltage times screen current.

Practical Aspects of Class B Modulators As stated previously, a Class B audio amplifier requires the driving stage to supply well-regulated audio power to the grid circuit of the Class B stage. Since the performance of a Class B modulator may easily be impaired by an improperly designed driver stage, it is well to study the problems incurred in the design of the driver stage.

The grid circuit of a Class B modulator may be compared to a variable resistance which decreases in value as the exciting grid voltage is increased. This variable resistance appears across the secondary terminals of the driver transformer so that the driver stage is called upon to deliver power to a varying load. For best operation of the Class B stage, the grid excitation voltage should not drop as the power taken by the grid circuit increases. These opposing conditions call for a high order of voltage regulation in the driver stage plate circuit. In order to enhance the voltage regulation of this circuit, the driver tubes must have low plate resistance, the driver transformer must have as large a step-down ratio as possible, and the d-c resistance of both primary and secondary windings of the driver transformer should be low.

The driver transformer should reflect into the plate circuit of the driver tubes a load of such value that the required driving power is just developed with full excitation applied to the driver grid circuit. If this is done, the driver transformer will have as high a step-down ratio as is consistent with the maximum drive requirements of the Class B stage. If the step-down ratio of the driver transformer is too large, the driver plate load will be so high that the power required to drive the Class B stage to full output cannot be developed. If the step-down ratio is too small the regulation of the driver stage will be impaired.

Driver Stage Calculations The parameters for the driver stage may be calculated from the plate characteristic curve, a sample of which is shown in figure 24. The required positive grid voltage ($e_{g\text{-}max}$) for the 811A tubes used in the sample calculation is found at point X, the intersection of the load line and the peak plate current as found on the y-axis. This is +80 volts. If a vertical line is dropped from point X to intersect the dotted grid current curves, it will be found that the grid current for a single 811A at this value of grid voltage is 100 milliamperes (point Y). The peak grid driving power is therefore $80 \times 0.100 = 8$ watts. The approximate *average* driving power is 4 watts. This is an approximate figure because the grid impedance is not constant over the entire audio cycle.

A pair of 2A3 tubes will be used as drivers, operating Class A, with the maximum excitation to the drivers occuring just below the point of grid current flow in the 2A3 tubes. The driver plate voltage is 300 volts, and the grid bias is −62 volts. The peak power developed in the primary winding of the driver transformer is:

$$\underset{\text{(watts)}}{\text{Peak Power }(P_p)} = 2R_L\left(\frac{\mu E_g}{R_p + R_L}\right)^2$$

where μ is the amplification factor of the driver tubes (4.2 for 2A3). E_g is the peak grid swing of the driver stage (62 volts). R_p is the plate resistance of one driver tube (800 ohms). R_L is ½ the plate-to-plate load of the driver stage, and P_p is 8 watts.

Solving the above equation for R_L, we obtain a value of 14,500 ohms load, plate-to-plate for the 2A3 driver tubes.

The peak primary voltage is:

$$e_{pri} = 2R_L \times \frac{\mu E_g}{R_p + R_L} = 493 \text{ volts}$$

and the turns ratio of the driver transformer (primary to ½ secondary) is:

$$\frac{e_{pri}}{e_{g(max)}} = \frac{493}{80} = 6.15{:}1$$

Plate Circuit Impedance Matching One of the commonest causes of distortion in a Class B modulator is incorrect load impedance in the plate circuit. The purpose of the Class B modulation transformer is to take the power developed by the modulator (which has a certain operating impedance) and transform it to the operating impedance imposed by the modulated amplifier stage.

If the transformer in question has the same number of turns on the primary winding as it has on the secondary winding, the turns ratio is 1:1, and the impedance ratio is also 1:1. If a 10,000 ohm resistor is placed across the secondary terminals of the transformer, *a reflected load* of 10,000 ohms would appear across the primary terminals. If the resistor is changed to one of 2376 ohms, the reflected primary impedance would also be 2376 ohms.

If the transformer has twice as many turns on the secondary as on the primary, the turns ratio is 2:1. The impedance ratio is the square of the turns ratio, or 4:1. If a 10,000 ohm resistor is now placed across the secondary winding, a reflected load of 2,500 ohms will appear across the primary winding.

Effects of Plate Circuit Mis-match It can be seen from the above paragraphs that the Class B modulator plate load is entirely dependent upon the load placed upon the secondary terminals of the Class B modulation transformer. If the secondary load is incorrect, certain changes will take place in the operation of the Class B modulator stage.

When the modulator load impedance is too low, the efficiency of the Class B stage is reduced and the plate dissipation of the tubes is increased. Peak plate current of the modulator stage is increased, and saturation of the modulation transformer core may result. "Talk-back" of the modulation transformer may result if the plate load impedance of the modulator stage is too low.

When the modulator load impedance is too high, the maximum power capability of the stage is reduced. An attempt to increase the output by increasing grid excitation to the stage will result in peak-clipping of the audio wave. In addition, high peak voltages may be built up in the plate circuit that may damage the modulation transformer.

6-14 Cathode-Follower Power Amplifiers

The cathode-follower is essentially a power output stage in which the exciting signal is applied between grid and ground. The plate is maintained at ground potential with respect to input and output signals, and the output signal is taken between cathode and ground.

Types of Cathode-Follower Amplifiers Figure 26 illustrates four types of cathode-follower power amplifiers in common usage and figure 27 shows the output impedance (R_o), and stage gain (A) of both triode and pentode (or tetrode) cathode-follower stages. It will be seen by inspection of the equations that the stage voltage gain is always less than one, that the output impedance of the stage is much less than the same stage operated as a conventional cathode-return amplifier. The output impedance for conventional tubes will be somewhere between 100 and 1000 ohms, depending primarily on the transconductance of the tube.

This reduction in gain and output impedance for the cathode-follower comes about since the stage operates as though it has 100 per cent degenerative feedback applied between its output and input circuit. Even though the voltage gain of the stage is reduced to a value less than one by the action of the degenerative feedback, the power gain of the stage (if it is operating Class A) is not reduced. Although more voltage is required to excite a cathode-follower amplifier than appears across the load circuit, since the cathode "follows" along with the grid, the relative grid-to-cathode voltage is essentially the same as in a conventional amplifier.

Use of Cathode-Follower Amplifiers Although the cathode-follower gives no voltage gain, it is an effective power amplifier where it is desired to feed a low-impedance load, or where it is desired to feed a load of varying impedance with a signal having good regulation. This latter capability

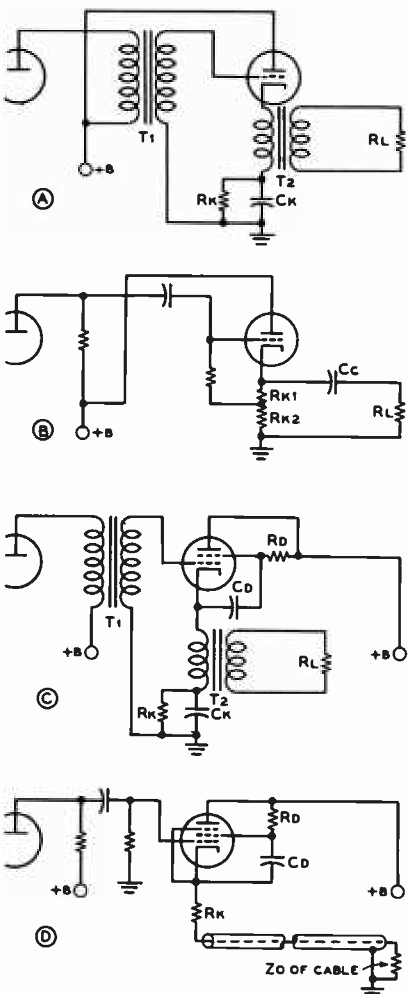


Figure 26

CATHODE-FOLLOWER OUTPUT CIRCUITS FOR AUDIO OR VIDEO AMPLIFIERS

TRIODE:

$$\mu_{cf} = \frac{\mu}{\mu+1} \qquad A = \frac{\mu R_L}{R_L(\mu+1) + R_P}$$

$$R_{O(CATHODE)} = \frac{R_P}{\mu+1} \qquad R_L = \frac{(R_{K1}+R_{K2})\,R_L'}{R_{K1}+R_{K2}+R_L'}$$

PENTODE:

$$R_{O(CATHODE)} = \frac{1}{G_M} \qquad R_{EQ} = \frac{R_L}{1+R_L G_M}$$

$$A = G_M R_{EQ}$$

Figure 27

Equivalent factors for pentode (or tetrode) cathode-follower power amplifiers.

makes the cathode follower particularly effective as a driver for the grids of a Class B modulator stage.

The circuit of figure 26A is the type of amplifier, either single-ended or push-pull, which may be used as a driver for a Class B modulator or which may be used for other applications such as feeding a loudspeaker where unusually good damping of the speaker is desired. If the d-c resistance of the primary of the transformer T_2 is approximately the correct value for the cathode bias resistor for the amplifier tube, the components R_k and C_k need not be used. Figure 26B shows an arrangement which may be used to feed directly a value of load impedance which is equal to or higher than the cathode impedance of the amplifier tube. The value of C_c must be quite high, somewhat higher than would be used in a conventional circuit, if the frequency response of the circuit when operating into a low-impedance load is to be preserved.

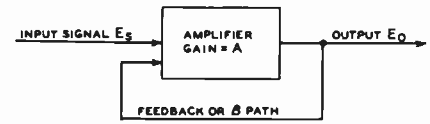
Figures 26C and 26D show cathode-follower circuits for use with tetrode or pentode tubes. Figure 26C is a circuit similar to that shown in 26A and essentially the same comments apply in regard to the components R_k and C_k and the primary resistance of the transformer T_2. Notice also that the screen of the tube is maintained at the same signal potential as the cathode by means of coupling capacitor C_d. This capacitance should be large enough so that at the lowest frequency it is desired to pass through the stage its reactance will be low with respect to the dynamic screen-to-cathode resistance in parallel with R_d T_2 in this stage as well as in the circuit of figure 26A should have the proper turns (or impedance) ratio to give the desired step-down or step-up from the cathode circuit to the load. Figure 26D is an arrangement frequently used in video systems for feeding a coaxial cable of relatively low impedance from a vacuum-tube amplifier. A pentode or tetrode tube with a cathode impedance as a cathode follower ($1/G_m$) approximately the same as the cable impedance should be chosen. The 6AG7 and 6AC7 have cathode impedances of the same order as the surge impedances of certain types of low-capacitance coaxial cable. An arrangement such as 26D is also usable for feeding coaxial cable with audio or r-f energy where it is desired to transmit the output signal over moderate distances. The resistor R_k is added to the circuit as shown if the cathode impedance of the tube used is lower than the characteristic impedance of the cable. If the output impedance of the stage is higher than the cable impedance a resistance of appropriate value is sometimes placed in parallel with the input end of the cable. The values of C_d and R_d should be chosen with the same considerations in mind as mentioned in the discussion of the circuit of figure 26C above.

The Cathode-Follower in R-F Stages The cathode follower may conveniently be used as a method of coupling r-f or i-f energy between two units separated a considerable distance. In such an application a coaxial cable should be used to carry the r-f or i-f energy. One such application would be for carrying the output of a v-f-o to a transmitter located a considerable distance from the operating position. Another application would be where it is desired to feed a single-sideband demodulator, an FM adaptor, or another accessory with intermediate frequency signal from a communications receiver. A tube such as a 6CB6 connected in a manner such as is shown in figure 26D would be adequate for the i-f amplifier coupler, while a 6L6 or a 6AG7 could be used in the output stage of a v-f-o as a cathode follower to feed the coaxial line which carries the v-f-o signal from the control unit to the transmitter proper.

6-15 Feedback Amplifiers

It is possible to modify the characteristics of an amplifier by feeding back a portion of the output to the input. All components, circuits and tubes included between the point where the feedback is taken off and the point where the feedback energy is inserted are said to be included within the feedback loop. An amplifier containing a feedback loop is said to be a *feedback amplifier.* One stage or any number of stages may be included within the feedback loop. However, the difficulty of obtaining proper operation of a feedback amplifier increases with the bandwidth of the amplifier, and with the number of stages and circuit elements included within the feedback loop.

Gain and Phase-shift in Feedback Amplifiers The gain and phase shift of any amplifier are functions of frequency. For any amplifier containing a feedback loop to be completely stable the gain of such an amplifier, as measured from the input back to the point where the feedback circuit connects to the input, must be less than one



VOLTAGE AMPLIFICATION WITH FEEDBACK = $\dfrac{A}{1-A\beta}$

A = GAIN IN ABSENCE OF FEEDBACK

β = FRACTION OF OUTPUT VOLTAGE FED BACK

β IS NEGATIVE FOR NEGATIVE FEEDBACK

FEEDBACK IN DECIBELS = 20 LOG $(1-A\beta)$

= 20 LOG $\dfrac{\text{MID FREQ. GAIN WITHOUT FEEDBACK}}{\text{MID FREQ. GAIN WITH FEEDBACK}}$

DISTORTION WITH FEEDBACK = $\dfrac{\text{DISTORTION WITHOUT FEEDBACK}}{(1-A\beta)}$

$$R_O = \frac{R_N}{1 - A\beta\left(1 + \frac{R_N}{R_L}\right)}$$

WHERE:

R_O = OUTPUT IMPEDANCE OF AMPLIFIER WITH FEEDBACK

R_N = OUTPUT IMPEDANCE OF AMPLIFIER WITHOUT FEEDBACK

R_L = LOAD IMPEDANCE INTO WHICH AMPLIFIER OPERATES

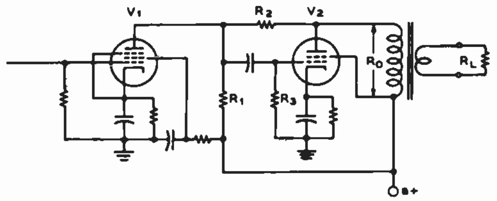
Figure 28

FEEDBACK AMPLIFIER RELATIONSHIPS

at the frequency where the feedback voltage is in phase with the input voltage of the amplifier. If the gain is equal to or more than one at the frequency where the feedback voltage is in phase with the input the amplifier will oscillate. This fact imposes a limitation upon the amount of feedback which may be employed in an amplifier which is to remain stable. If the reader is desirous of designing amplifiers in which a large amount of feedback is to be employed he is referred to a book on the subject by H. W. Bode.*

Types of Feedback Feedback may be either negative or positive, and the feedback voltage may be proportional either to output voltage or output current. The most commonly used type of feedback with a-f or video amplifiers is negative feedback proportional to output voltage. Figure 28 gives the general operating conditions for feedback amplifiers. Note that the reduction in distortion is proportional to the reduction in gain of the amplifier, also that the reduction in the output impedance of the amplifier is somewhat greater than the reduction in the gain by an amount which is a function of the ratio of the

* H. W. Bode, "Network Analysis and Feedback Amplifier Design," D. Von Nostrand Co., 250 Fourth Ave., New York 3, N. Y.



$$\text{DB FEEDBACK} = 20 \text{ LOG} \left[\frac{R_2 + R_A(G_M V_2 \; R_O)}{R_2}\right]$$

$$= 20 \text{ LOG} \left[\frac{R_2 + R_A(\text{VOLTAGE GAIN OF } V_2)}{R_2}\right]$$

$$\text{GAIN OF BOTH STAGES} = \left[G_M V_1 \left(\frac{R_B \times R_A}{R_B + R_A}\right)\right] \times (G_M V_2 \; R_O)$$

WHERE:

$$R_A = \frac{R_1 \times R_3}{R_1 + R_3}$$

$$R_B = \frac{R_2}{G_M V_2 \; R_O}$$

R_O = REFLECTED LOAD IMPEDANCE ON V_2

R_2 = FEEDBACK RESISTOR (USUALLY ABOUT 500 K)

$$\text{OUTPUT IMPEDANCE} = \frac{R_N \; R_2}{\left[R_2 + R_A(G_M V_2 \; R_O)\right] \times \left(1 + \frac{R_N}{R_O}\right)}$$

R_N = PLATE IMPEDANCE OF V_2

Figure 29

SHUNT FEEDBACK CIRCUIT FOR PENTODES OR TETRODES

This circuit requires only the addition of one resistor, R_2, to the normal circuit for such an application. The plate impedance and distortion introduced by the output stage are materially reduced.

output impedance of the amplifier without feedback to the load impedance. The reduction in noise and hum in those stages included within the feedback loop is proportional to the reduction in gain. However, due to the reduction in gain of the output section of the amplifier somewhat increased gain is required of the stages preceding the stages included within the feedback loop. Therefore the noise and hum output of the entire amplifier may or may not be reduced dependent upon the relative contributions of the first part and the latter part of the amplifier to hum and noise. If most of the noise and hum is coming from the stages included within the feedback loop the undesired signals will be reduced in the output from the complete amplifier. It is most frequently true in conventional amplifiers that the hum and distortion come from the latter stages, hence these will be reduced by feedback, but thermal agitation and microphonic noise come from the first stage and will not be reduced but may be increased by feedback unless the feedback loop includes the first stage of the amplifier.

Figure 29 illustrates a very simple and effective application of negative voltage feedback to an output pentode or tetrode amplifier stage. The reduction in hum and distortion may amount to 15 to 20 db. The reduction in the effective plate impedance of the stage will be by a factor of 20 to 100 dependent upon the operating conditions. The circuit is commonly used in commercial equipment with tubes such as the 6SJ7 for V_1 and the 6V6 or 6L6 for V_2.

CHAPTER SEVEN

Radio Frequency Vacuum Tube Amplifiers

TUNED RF VACUUM TUBE AMPLIFIERS

Tuned r-f voltage amplifiers are used in receivers for the amplification of the incoming r-f signal and for the amplification of intermediate frequency signals after the incoming frequency has been converted to the intermediate frequency by the mixer stage. Signal frequency stages are normally called *tuned r-f amplifiers* and intermediate-frequency stages are called *i-f amplifiers*. Both tuned r-f and i-f amplifiers are operated Class A and normally operate at signal levels from a fraction of a microvolt to amplitudes as high as 10 to 50 volts at the plate of the last i-f stage in a receiver.

7-1 Grid Circuit Considerations

Since the full amplification of a receiver follows the first tuned circuit, the operating conditions existing in that circuit and in its coupling to the antenna on one side and to the grid of the first amplifier stage on the other are of greatest importance in determining the signal-to-noise ratio of the receiver on weak signals.

First Tuned Circuit It is obvious that the highest ratio of signal-to-noise be impressed on the grid of the first r-f amplifier tube. Attaining the optimum ratio is a complex problem since noise will be generated in the antenna due to its equivalent radiation resistance (this noise is in addition to any noise of atmospheric origin) and in the first tuned circuit due to its equivalent coupled resistance at resonance. The noise voltage generated due to antenna radiation resistance and to equivalent tuned circuit resistance is similar to that generated in a resistor due to thermal agitation and is expressed by the following equation:

$$E_n^2 = 4kTR\Delta f$$

Where: E_n = r-m-s value of noise voltage over the interval Δf
k = Boltzman's constant = 1.374 $\times 10^{-22}$ joule per °K.
T = Absolute temperature °K.
R = Resistive component of impedance across which thermal noise is developed.
Δf = Frequency band across which voltage is measured.

In the above equation Δf is essentially the frequency band passed by the intermediate frequency amplifier of the receiver under consideration. This equation can be greatly simplified for the conditions normally encountered in communications work. If we assume the following conditions: T = 300° K or 27° C or 80.5° F, room temperature; Δf = 8000 cycles (the average pass band of a communications receiver or speech amplifier), the equation reduces to: $E_{r.m.s.} = 0.0115\sqrt{R}$ microvolts. Accordingly, the thermal-agitation voltage appearing in the center of half-wave antenna (assuming effective temperature to be 300° K) having a radiation resistance of 73 ohms is approximately 0.096 microvolts. Also, the thermal agitation voltage appearing across a 500,000-ohm grid resistor in the first stage of a speech amplifier is approximately 8 microvolts under the conditions cited above. Further, the voltage due to thermal agitation being impressed on the grid of the first r-f stage in a receiver by a first tuned circuit whose resonant resistance is 50,000 ohms is approximately 2.5 microvolts. Suffice to say, however, that the value of thermal agitation voltage appearing across the first tuned circuit when the antenna is properly coupled to this circuit will be very much less than this value.

It is common practice to match the impedance of the antenna transmission line to the input impedance of the grid of the first r-f amplifier stage in a receiver. This is the condition of antenna coupling which gives maximum gain in the receiver. However, when u-h-f tubes such as acorns and miniatures are used at frequencies somewhat less than their maximum capabilities, a significant improvement in *signal-to-noise* ratio can be attained by *increasing* the coupling between the antenna and first tuned circuit to a value greater than that which gives greatest signal amplitude out of the receiver. In other words, in the 10, 6, and 2 meter bands it is possible to attain somewhat improved signal-to-noise ratio by increasing antenna coupling to the point where the gain of the receiver is slightly reduced.

It is always possible, in addition, to obtain improved signal-to-noise ratio in a v-h-f receiver through the use of tubes which have improved input impedance characteristics at the frequency in question over conventional types.

Noise Factor The limiting condition for sensitivity in any receiver is the thermal noise generated in the antenna and in the first tuned circuit. However, with proper coupling between the antenna and the grid of the tube, through the first tuned circuit, the noise contribution of the first tuned circuit can be made quite small. Unfortunately, though, the major noise contribution in a properly designed receiver is that of the first tube. The noise contribution due to electron flow and due to losses in the tube can be lumped into an equivalent value of resistance which, if placed in the grid circuit of a perfect tube having the same gain but no noise would give the same noise voltage output in the plate load. The equivalent noise resistance of tubes such as the 6SK7, 6SG7, etc., runs from 5000 to 10,000 ohms. Very high G_m tubes such as the 6AC7 and 6AK5 have equivalent noise resistances as low as 700 to 1500 ohms. The lower the value of equivalent noise resistance, the lower will be the noise output under a fixed set of conditions.

The equivalent noise resistance of a tube must not be confused with the actual input loading resistance of a tube. For highest signal-to-noise ratio in an amplifier the input loading resistance should be as high as possible so that the amount of voltage that can be developed from grid to ground by the antenna energy will be as high as possible. The equivalent noise resistance should be as low as possible so that the noise generated by this resistance will be lower than that attributable to the antenna and first tuned circuit, and the losses in the first tuned circuit should be as low as possible.

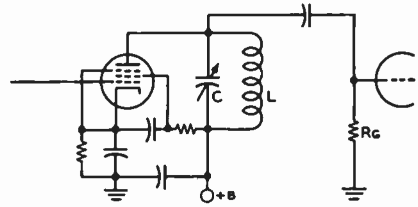
The absolute sensitivity of receivers has been designated in recent years in government and commercial work by an arbitrary dimensionless number known as "noise factor" or *N*. The noise factor is the ratio of noise output of a "perfect" receiver having a given amount of gain with a dummy antenna matched to its input, to the noise output of the receiver under measurement having the same amount of gain with the dummy antenna matched to its input. Although a perfect receiver is not a physically realizable thing, the noise factor of a receiver under measurement can be determined by calculation from the amount of additional noise (from a temperature-limited diode or other calibrated noise generator) required to increase the noise power output of a receiver by a predetermined amount.

Tube Input Loading As has been mentioned in a previous paragraph, greatest gain in a receiver is obtained when the antenna is matched, through the r-f coupling transformer, to the input resistance of the r-f tube. However, the higher the ratio of tube input resistance to equivalent noise resistance of the tube the higher will be the signal-to-noise ratio of the stage—and of course, the better will be the noise factor of the overall receiver. The input resistance of a tube is very high at frequencies in the broadcast band and gradually decreases as the frequency increases. Tube input resistance on conventional tube types begins to become an important factor at frequencies of about 25 Mc. and above. At frequencies above about 100 Mc. the use of conventional tube types becomes impracticable since the input resistance of the tube has become so much lower than the equivalent noise resistance that it is impossible to attain reasonable signal-to-noise ratio on any but very strong signals. Hence, special v-h-f tube types such as the 6AK5, 6AG5, and 6CB6 must be used.

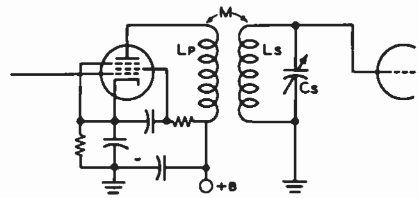
The lowering of the effective input resistance of a vacuum tube at higher frequencies is brought about by a number of factors. The first, and most obvious, is the fact that the dielectric loss in the internal insulators, and in the base and press of the tube increases with frequency. The second factor is due to the fact that a finite time is required for an electron to move from the space charge in the vicinity of the cathode, pass between the grid wires, and travel on to the plate. The fact that the electrostatic effect of the grid on the moving electron acts over an appreciable portion of a cycle at these high frequencies causes a current flow in the grid circuit which appears to the input circuit feeding the grid as a resistance. The decrease in input resistance of a tube due to electron transit time varies as the square of the frequency. The undesirable effects of transit time can be reduced in certain cases by the use of higher plate voltages. Transit time varies inversely as the square root of the applied plate voltage.

Cathode lead inductance is an additional cause of reduced input resistance at high frequencies. This effect has been reduced in certain tubes such as the 6SH7 and the 6AK5 by providing two cathode leads on the tube base. One cathode lead should be connected to the input circuit of the tube and the other lead should be connected to the by-pass capacitor for the plate return of the tube.

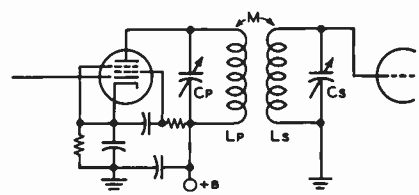
The reader is referred to the Radiation Laboratory Series, Volume 23: "Microwave Receivers" (McGraw-Hill, publishers) for additional information on noise factor and input loading of vacuum tubes.



(A) AMPLIFICATION AT RESONANCE (APPROX.) = $G_m \omega L Q$



(B) AMPLIFICATION AT RESONANCE (APPROX.) = $G_m \omega M Q$



(C) AMPLIFICATION AT RESONANCE (APPROX.) = $G_m K \dfrac{\omega\sqrt{L_P L_S}}{K^2 + \frac{1}{Q_P Q_S}}$

WHERE: 1. PRI. AND SEC. RESONANT AT SAME FREQUENCY
2. K IS COEFFICIENT OF COUPLING

IF PRI. AND SEC. Q ARE APPROXIMATELY THE SAME:

$$\frac{\text{TOTAL BANDWIDTH}}{\text{CENTER FREQUENCY}} = 1.2\,K$$

MAXIMUM AMPLITUDE OCCURS AT CRITICAL COUPLING - WHEN $K = \dfrac{1}{\sqrt{Q_P Q_S}}$

Figure 1

Gain equations for pentode r-f amplifier stages operating into a tuned load

7-2 Plate-Circuit Considerations

Noise is generated in a vacuum tube by the fact that the current flow within the tube is not a smooth flow but rather is made up of the continuous arrival of particles (electrons) at a very high rate. This *shot effect* is a source of noise in the tube, but its effect is referred back to the grid circuit of the tube since it is included in the *equivalent noise resistance* discussed in the preceding paragraphs.

Plate Circuit Coupling For the purpose of this section, it will be considered that the function of the plate load circuit of a tuned vacuum-tube amplifier is to deliver energy to the next stage with the greatest efficiency over the required band of frequencies. Figure 1 shows three methods of interstage coupling for tuned r-f voltage amplifiers. In figure 1A omega (ω) is 2π times the resonant frequency of the circuit in the plate of the amplifier tube, and L and Q are the inductance and Q of the inductor L. In figure 1B the notation is the same and M is the mutual inductance between the primary coil and the secondary coil. In figure 1C the notation is again the same and *k* is the coefficient of coupling between the two tuned circuits. As the coefficient of coupling between the circuits is increased the bandwidth becomes greater but the response over the band becomes progressively more double-humped. The response over the band is the most flat when the Q's of primary and secondary are approximately the same and the value of each Q is equal to $1.75/k$.

Variable-Mu Tubes in R-F Stages It is common practice to control the gain of a succession of r-f or i-f amplifier stages by varying the average bias on their control grids. However, as the bias is raised above the operating value on a conventional sharp-cutoff tube the tube becomes increasingly non-linear in operation as cutoff of plate current is approached. The effect of such non-linearity is to cause cross modulation between strong signals which appear on the grid of the tube. When a tube operating in such a manner is in one of the first stages of a receiver a number of signals are appearing on its grid simultaneously and cross modulation between them will take place. The result of this effect is to produce a large number of spurious signals in the output of the receiver—in most cases these signals will carry the modulation of both the carriers which have been cross modulated to produce the spurious signal.

The undesirable effect of cross modulation can be eliminated in most cases and greatly reduced in the balance through the use of a variable-mu tube in all stages which have a-v-c voltage or other large negative bias applied to their grids. The variable-mu tube has a characteristic which causes the cutoff of plate current to be gradual with an increase in grid bias, and the reduction in plate current is accompanied by a decrease in the effective amplification factor of the tube. Variable-mu tubes ordinarily have somewhat reduced G_m as compared to a sharp-cutoff tube of the same group. Hence the sharp-cutoff tube will perform best in stages to which a-v-c voltage is not applied.

RADIO-FREQUENCY POWER AMPLIFIERS

All modern transmitters in the medium-frequency range and an increasing percentage of those in the v-h-f and u-h-f ranges consist of a comparatively low-level source of radio-frequency energy which is multiplied in frequency and successively amplified to the desired power level. Microwave transmitters are still predominately of the self-excited oscillator type, but when it is possible to use r-f amplifiers in s-h-f transmitters the flexibility of their application will be increased. The following portion of this chapter will be devoted, however, to the method of operation and calculation of operating characteristics of r-f power amplifiers for operation in the range of approximately 3.5 to 500 Mc.

7-3 Class C R-F Power Amplifiers

The majority of r-f power amplifiers fall into the Class C category since such stages can be made to give the best plate circuit efficiency of any present type of vacuum-tube amplifier. Hence, the cost of tubes for such a stage and the cost of the power to supply that stage is least for any given power output. Nevertheless, the Class C amplifier gives less power gain than either a Class A or Class B amplifier under similar conditions since the grid of a Class C stage must be driven highly positive over the portion of the cycle of the exciting wave when the plate voltage on the amplifier is low, and must be at a large negative potential over a large portion of the cycle so that no plate current will flow except when plate voltage is very low. This, in fact, is the fundamental reason why the plate circuit efficiency of a Class C amplifier stage can be made high—plate current is cut off at all times except when the plate-to-cathode voltage drop across the tube is at its lowest value. Class C amplifiers almost invariably operate into a tuned tank circuit as a load, and as a result are used as amplifiers of a single frequency or of a comparatively narrow band of frequencies.

Relationships in Class C Stage Figure 2 shows the relationships between the various voltages and currents over one cycle of the exciting grid voltage for a Class C amplifier stage. The notation given in figure 2 and in the discussion to follow is the same as given at the first of Chapter Six under "Symbols for Vacuum-Tube Parameters."

The various manufacturers of vacuum tubes publish booklets listing in adequate detail alternative Class C operating conditions for the tubes which they manufacture. In addition, operating condition sheets for any particular type of vacuum tube are available for the asking from the different vacuum-tube manufacturers. It is, nevertheless, often desirable to determine optimum operating conditions for a tube under a particular set of circumstances. To assist in such calculations the following paragraphs are devoted to a method of calculating Class C operating conditions which is moderately simple and yet sufficiently accurate for all practical purposes.

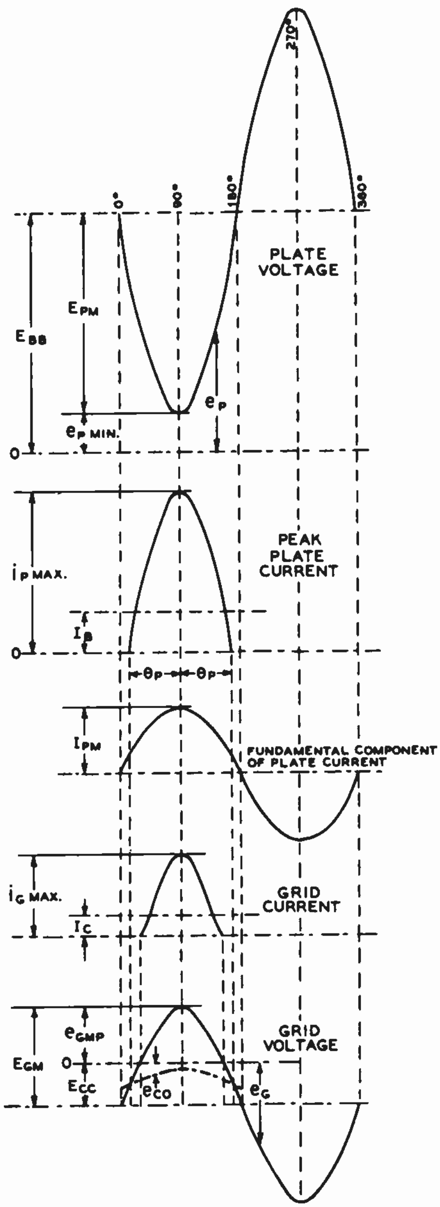


Figure 2

Instantaneous electrode and tank circuit voltages and currents for a Class C r-f power amplifier

Calculation of Class C Amplifier Operating Characteristics

Although Class C operating conditions can be determined with the aid of the more conventional grid voltage-plate current operating curves, the calculation is considerably simplified if the alternative "constant-current curve" of the tube in question is used. This is true since the operating line of a Class C amplifier is a straight line on a set of constant-current curves. A set of constant-current curves on the 250TH tube with a sample load line drawn thereon is shown in figure 5.

In calculating and predicting the operation of a vacuum tube as a Class C radio-frequency amplifier, the considerations which determine the operating conditions are plate efficiency, power output required, maximum allowable plate and grid dissipation, maximum allowable plate voltage and maximum allowable plate current. The values chosen for these factors will depend both upon the demands of a particular application and upon the tube chosen.

The plate and grid currents of a Class C amplifier tube are periodic pulses, the durations of which are always less than 180 degrees. For this reason the average grid current, average plate current, power output, driving power, etc., cannot be directly calculated but must be determined by a Fourier analysis from points selected at proper intervals along the line of operation as plotted upon the constant-current characteristics. This may be done either analytically or graphically. While the Fourier analysis has the advantage of accuracy, it also has the disadvantage of being tedious and involved.

The approximate analysis which follows has proved to be sufficiently accurate for most applications. This type of analysis also has the advantage of giving the desired information at the first trial. The system is direct in giving the desired information since the important factors, power output, plate efficiency, and plate voltage are arbitrarily selected at the beginning.

Method of Calculation

The first step in the method to be described is to determine the power which must be delivered by the Class C amplifier. In making this determination it is well to remember that ordinarily from 5 to 10 per cent of the power delivered by the amplifier tube or tubes will be lost in well-designed tank and coupling circuits at frequencies below 20 Mc. Above 20 Mc. the tank and circuit losses are ordinarily somewhat above 10 per cent.

The plate power input necessary to produce the desired output is determined by the plate efficiency: $P_{in} = P_{out}/N_p$.

For most applications it is desirable to operate at the highest practicable efficiency. High-efficiency operation usually requires less expensive tubes and power supplies, and the

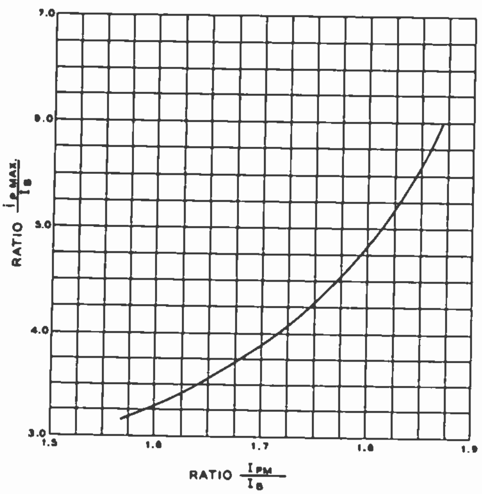


Figure 3

Relationship between the peak value of the fundamental component of the tube plate current, and average plate current; as compared to the ratio of the instantaneous peak value of tube plate current, and average plate current

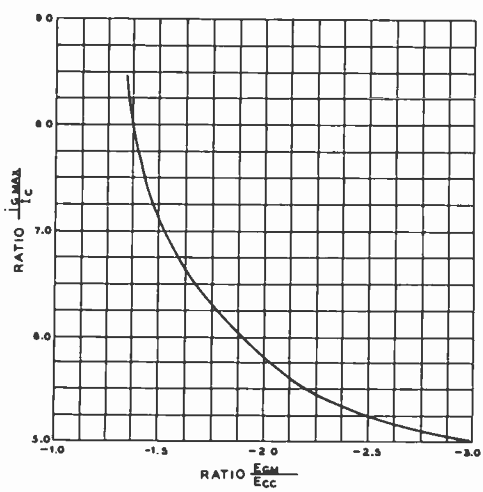


Figure 4

Relationship between the ratio of the peak value of the fundamental component of the grid excitation voltage, and the average grid bias; as compared to the ratio between instantaneous peak grid current and average grid current

amount of artificial cooling required is frequently less than for low-efficiency operation. On the other hand, high-efficiency operation usually requires more driving power and involves the use of higher plate voltages and higher peak tube voltages. The better types of triodes will ordinarily operate at a plate efficiency of 75 to 85 per cent at the highest rated plate voltage, and at a plate efficiency of 65 to 75 per cent at intermediate values of plate voltage.

The first determining factor in selecting a tube or tubes for a particular application is the amount of plate dissipation which will be required of the stage. The total plate dissipation rating for the tube or tubes to be used in the stage must be equal to or greater than that calculated from: $P_p = P_{in} - P_{out}$.

After selecting a tube or tubes to meet the power output and plate dissipation requirements it becomes necessary to determine from the tube characteristics whether the tube selected is capable of the desired operation and, if so, to determine the driving power, grid bias, and grid dissipation.

The complete procedure necessary to determine a set of Class C amplifier operating conditions is given in the following steps:

1. Select the plate voltage, power output, and efficiency.
2. Determine plate input from: $P_{in} = P_{out}/N_p$.
3. Determine plate dissipation from: $P_p = P_{in} - P_{out}$. P_p must not exceed maximum rated plate dissipation for tube or tubes selected.
4. Determine average plate current from: $I_b = P_{in}/E_{bb}$.
5. Determine approximate i_{pmax} from:
   $i_{pmax} = 4.9\ I_b$ for $N_p = 0.85$
   $i_{pmax} = 4.5\ I_b$ for $N_p = 0.80$
   $i_{pmax} = 4.0\ I_b$ for $N_p = 0.75$
   $i_{pmax} = 3.5\ I_b$ for $N_p = 0.70$
6. Locate the point on constant-current characteristics where the constant plate current line corresponding to the approximate i_{pmax} determined in step 5 crosses the line of equal plate and grid voltages (diode line). Read e_{pmin} at this point. In a few cases the lines of constant plate current will inflect sharply upward before reaching the diode line. In these cases e_{pmin} should not be read at the diode line but at the point where the plate current line intersects a line drawn from the origin through these points of inflection.

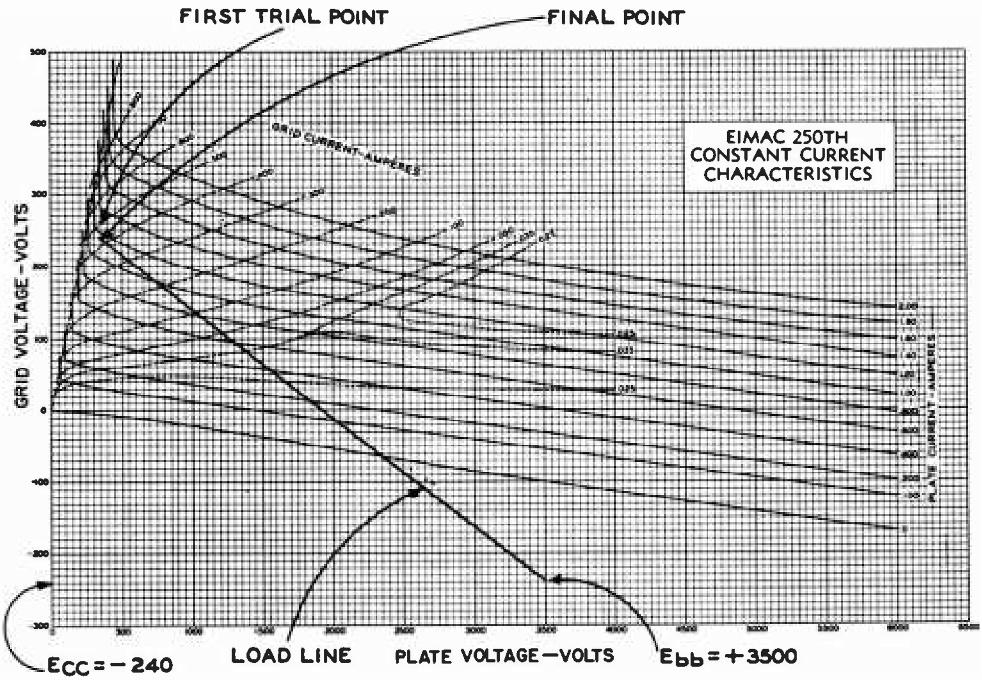


FIGURE 5

Active portion of the operating load line for an Eimac 250TH Class C r-f power amplifier, showing first trial point and the final operating point

7. Calculate E_{pm} from: $E_{pm} = E_{bb} - e_{pmin}$.

8. Calculate the ratio I_{pm}/I_b from:

$$\frac{I_{pm}}{I_b} = \frac{2\,N_p\,E_{bb}}{E_{pm}}$$

9. From the ratio of I_{pm}/I_b calculated in step 8 determine the ratio i_{pmax}/I_b from figure 3.

10. Calculate a new value for i_{pmax} from the ratio found in step 9.
i_{pmax} = (ratio from step 9) I_b

11. Read e_{gmp} and i_{gmax} from the constant-current characteristics for the values of e_{pmin} and i_{pmax} determined in steps 6 and 10.

12. Calculate the cosine of one-half the angle of plate current flow from:

$$\cos\theta_p = 2.32\left(\frac{I_{pm}}{I_b} - 1.57\right)$$

13. Calculate the grid bias voltage from:

$$E_{cc} = \frac{1}{1-\cos\theta_p} \times \left[\cos\theta_p\left(\frac{E_{pm}}{\mu} - e_{gmp}\right) - \frac{E_{bb}}{\mu}\right]$$

for triodes.

$$E_{cc} = \frac{1}{1-\cos\theta_p} \times \left[-\,e_{gmp}\cos\theta - \frac{E_{c2}}{\mu_{12}}\right]$$

for tetrodes, where μ_{12} is the grid-screen amplification factor, and E_{c2} is the d-c screen voltage.

14. Calculate the peak fundamental grid excitation voltage from:

$$E_{gm} = e_{gmp} - E_{cc}$$

15. Calculate the ratio E_{gm}/E_{cc} for the val-

ues of E_{cc} and E_{gm} found in steps 13 and 14.

16. Read i_{gmax}/I_c from figure 4 for the ratio E_{gm}/E_{cc} found in step 15.

17. Calculate the average grid current from the ratio found in step 16, and the value of i_{gmax} found in step 11:

$$I_c = \frac{i_{gmax}}{\text{Ratio from step 16}}$$

18. Calculate approximate grid driving power from:

$$P_d = 0.9\, E_{gm} I_c$$

19. Calculate grid dissipation from:

$$P_g = P_d + E_{cc} I_c$$

P_g must not exceed the maximum rated grid dissipation for the tube selected.

Sample Calculation A typical example of a Class C amplifier calculation is shown in the example below. Reference is made to figures 3, 4 and 5 in the calculation.

1. Desired power output—800 watts.
2. Desired plate voltage—3500 volts.
   Desired plate efficiency—80 per cent ($N_p = 0.80$)
   $P_{in} = 800/0.80 = 1000$ watts
3. $P_p = 1000 - 800 = 200$ watts
   Use 250TH; max. $P_p = 250$w; $\mu = 37$.
4. $I_b = 1000/3500 = 0.285$ ampere (285 ma.)
   Max. I_b for 250TH is 350 ma.
5. Approximate $i_{pmax} = 0.285 \times 4.5 = 1.28$ ampere
6. $e_{pmin} = 260$ volts (see figure 5 first trial point)
7. $E_{pm} = 3500 - 260 = 3240$ volts
8. $I_{pm}/I_b = 2 \times 0.80 \times 3500/3240 = 5600/3240 = 1.73$
9. $i_{pmax}/I_b = 4.1$ (from figure 3)
10. $i_{pmax} = 0.285 \times 4.1 = 1.17$
11. $e_{gmp} = 240$ volts
    $i_{gmax} = 0.430$ amperes
    (Both above from final point on figure 5)
12. $\cos\theta_p = 2.32\,(1.73 - 1.57) = 0.37$
    $(\theta_p = 68.3°)$
13. $$E_{cc} = \frac{1}{1-0.37} \times \left[0.37\left(\frac{3240}{37} - 240\right) - \frac{3500}{37}\right] = -240 \text{ volts}$$
14. $E_{gm} = 240 - (-240) = 480$ volts grid swing
15. $E_{gm}/E_{cc} = 480/-240 = -2$
16. $i_{gmax}/I_c = 5.75$ (from figure 4)
17. $I_c = 0.430/5.75 = 0.075$ amp. (75 ma. grid current)
18. $P_d = 0.9 \times 480 \times 0.075 = 32.5$ watts driving power
19. $P_g = 32.5 - (-240 \times 0.75) = 14.5$ watts grid dissipation
    Max. P_g for 250TH is 40 watts

The power output of any type of r-f amplifier is equal to:

$$I_{pm}E_{pm}/2 = P_o$$

I_{pm} can be determined, of course, from the ratio determined in step 8 above (in this type of calculation) by multiplying this ratio times I_b.

It is frequently of importance to know the value of load impedance into which a Class C amplifier operating under a certain set of conditions should operate. This is simply $R_L = E_{pm}/I_{pm}$. In the case of the operating conditions just determined for a 250TH amplifier stage the value of load impedance is:

$$R_L = \frac{E_{pm}}{I_{pm}} = \frac{3240}{.495} = 6600 \text{ ohms}$$

$$I_{pm} = \frac{I_{pm}}{I_b} \times I_b$$

Q of Amplifier Tank Circuit In order to obtain good plate tank circuit tuning and low radiation of harmonics from an amplifier it is necessary that the plate tank circuit have the correct Q. Charts giving compromise values of Q for Class C amplifiers are given in the chapter, *Generation of R-F Energy*. However, the amount of inductance required for a specified tank circuit Q under specified operating conditions can be calculated from the following expression:

$$\omega L = \frac{R_L}{Q}$$

ω = 2 π X operating frequency
L = Tank inductance
R_L = Required tube load impedance
Q = Effective tank circuit Q

A tank circuit Q of 12 to 20 is recommended for all normal conditions. However, if a balanced push-pull amplifier is employed the tank receives two impulses per cycle and the circuit Q may be lowered somewhat from the above values.

Quick Method of Calculating Amplifier Plate Efficiency The plate circuit efficiency of a Class B or Class C r-f amplifier can be determined from the following facts. The plate circuit efficiency of such an amplifier is equal to the product of two factors, F_1, which is equal to the ratio of E_{pm} to E_{bb} ($F_1 = E_{pm}/E_{bb}$) and F_2, which is proportional to the one-half angle of plate current flow, θ_p. A graph of F_2 against both θ_p and cos θ_p is given in figure 6. Either θ_p or cos θ_p may be used to determine F_2. Cos θ_p may be determined either from the procedure previously given for making Class C amplifier computations or it may be determined from the following expression:

$$\cos \theta_p = -\frac{\mu E_{cc} + E_{bb}}{\mu E_{gm} - E_{pm}}$$

Example of Method It is desired to know the one-half angle of plate current flow and the plate circuit efficiency for an 812 tube operating under the following conditions which have been assumed from inspection of the data and curves given in the RCA Transmitting Tube Handbook HB-3:

1. $E_{bb} = 1100$ volts
   $E_{cc} = -40$ volts
   $\mu = 29$
   $E_{gm} = 120$ volts
   $E_{pm} = 1000$ volts

2. $F_1 = E_{pm}/E_{bb} = 0.91$

3. $$\cos \theta_p = \frac{-29 \times 40 + 1100}{29 \times 120 - 1000} = \frac{60}{2480} = 0.025$$

4. $F_2 = 0.79$ (by reference to figure 6)

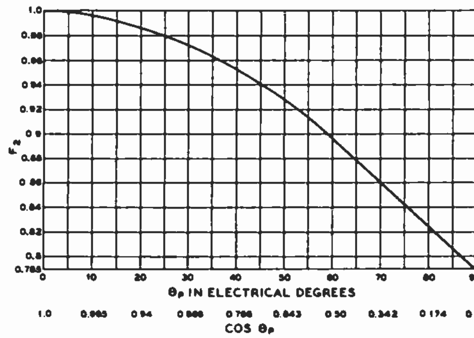


Figure 6

Relationship between Factor F_2 and the half-angle of plate current flow in an amplifier with sine-wave input and output voltage, operating at a grid-bias voltage greater than cut-off

5. $N_p = F_1 \times F_2 = 0.91 \times 0.79 = 0{,}72$
   (72 per cent efficiency)

F_1 could be called the plate-voltage-swing efficiency factor, and F_2 can be called the operating-angle efficiency factor or the maximum possible efficiency of any stage running with that value of half-angle of plate current flow.

N_p is, of course, only the ratio between power output and power input. If it is desired to determine the power input, exciting power, and grid current of the stage, these can be obtained through the use of steps 7, 8, 9, and 10 of the previously given method for power input and output; and knowing that i_{gmax} is 0.095 ampere the grid circuit conditions can be determined through the use of steps 15, 16, 17, 18 and 19.

7-4 Class B Radio Frequency Power Amplifiers

Radio frequency power amplifiers operating under Class B conditions of grid bias and excitation voltage are used in two general types of applications in transmitters. The first general application is as a buffer amplifier stage where it is desired to obtain a high value of power amplification in a particular stage. A particular tube type operated with a given plate voltage will be capable of somewhat greater output for a certain amount of excitation power when operated as a Class B ampli-

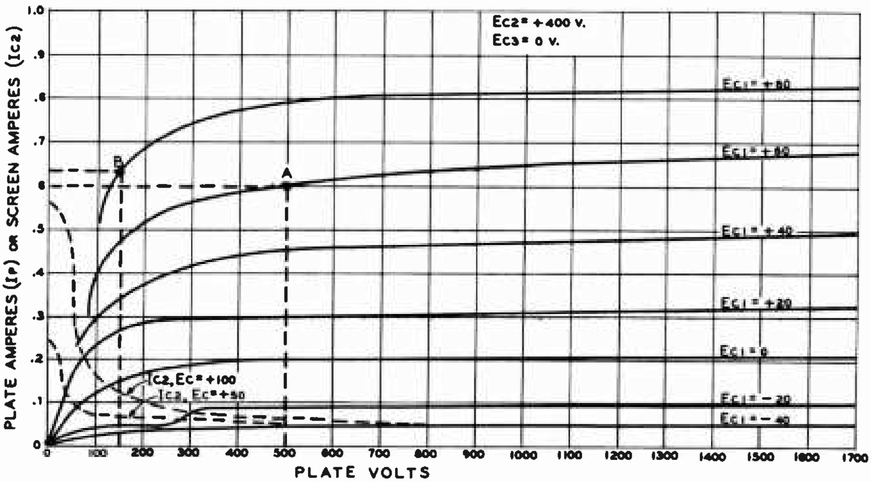


Figure 7
AVERAGE PLATE CHARACTERISTICS OF 813 TUBE

fier than when operated as a Class C amplifier.

Calculation of Operating Characteristics Calculation of the operating conditions for this type of Class B r-f amplifier can be carried out in a manner similar to that described in the previous paragraphs, except that the grid bias voltage is set on the tube before calculation at the value: $E_{cc} = -E_{bb}/\mu$. Since the grid bias is set at cutoff the one-half angle of plate current flow is 90°; hence cos θ_p is fixed at 0.00. The plate circuit efficiency for a Class B r-f amplifier operated in this manner can be determined in the following manner:

$$N_p = 78.5 \left(\frac{E_{pm}}{E_{bb}}\right)$$

The "Class B Linear" The second type of Class B r-f amplifier is the so-called *Class B linear amplifier* which is often used in transmitters for the amplification of a single-sideband signal or a conventional amplitude-modulated wave. Calculation of operating conditions may be carried out in a manner similar to that previously described with the following exceptions: The first trial operating point is chosen on the basis of the 100 per cent positive modulation peak of the modulated exciting wave. The plate circuit and grid peak voltages and currents can then be determined and the power input and output calculated. Then, with the exciting voltage reduced to one-half for the no-modulation condition of the exciting wave, and with the same value of load resistance reflected on the tube, the plate input and plate efficiency will drop to approximately one-half the values at the 100 per cent positive modulation peak and the power output of the stage will drop to one-fourth the peak-modulation value. On the negative modulation peak the input, efficiency, and output all drop to zero.

In general, the proper plate voltage, bias voltage, load resistance and power output listed in the tube tables for Class B audio work will also apply to Class B linear r-f application.

Calculation of Operating Parameters for a Class B Linear Amplifier Figure 7 illustrates the characteristic curves for an 813 tube. Assume the plate supply to be 2000 volts, and the screen supply to be 400 volts. To determine the operating parameters of this tube as a Class B linear r-f amplifier, the following steps should be taken:

1. The grid bias is chosen so that the resting plate current will produce approximately 1/3 of the maximum plate dissipation of the tube. The maximum dissipation of the 813 is 125 watts, so the bias is set to allow one-third of this value, or 42 watts of resting dissipation. At a plate potential of 2000 volts, a

plate current of 21 milliamperes will produce this figure. Referring to figure 7, a grid bias of −45 volts is approximately correct.

2. A practical Class B linear r-f amplifier runs at an efficiency of about 66% at full output, the efficiency dropping to about 33% with an unmodulated exciting signal. In the case of single-sideband suppressed carrier excitation, a no-excitation condition is substituted for the unmodulated excitation case, and the linear amplifier runs at the resting or quiescent input of 42 watts with no exciting signal. The peak allowable power input to the 813 is:

$$\text{Input Peak Power } (W_p) \text{ (watts)} = \frac{\text{Plate Dissipation} \times 100}{(100 - \%\text{ plate efficiency})} =$$

$$\frac{125}{33} \times 100 = 385 \text{ watts}$$

3. The maximum signal plate current is:

$$i_{p\,max} = \frac{W_p}{E_p} = \frac{385}{2000} = 0.193 \text{ ampere}$$

4. The plate current flow of the linear amplifier is 90°, and the plate current pulses have a peak of 3.14 times the maximum signal current:

$$3.14 \times 0.193 = 0.605 \text{ ampere}$$

5. Referring to figure 7, a current of 0.605 ampere (Point A) will flow at a positive grid potential of 60 volts and a minimum plate potential of 500 volts. The grid is biased at −45 volts, so a peak r-f grid voltage of 60 + 45 volts = 105 volts is required.

6. The grid driving power required for the Class B linear stage may be found by the aid of figure 8. It is one-quarter the product of the peak grid current times the peak grid voltage:

$$P_g = \frac{0.02 \times 105}{4} = 0.53 \text{ watt}$$

7. The peak power output of the 813 linear stage is:

$$385 - 125 = 260 \text{ watts}$$

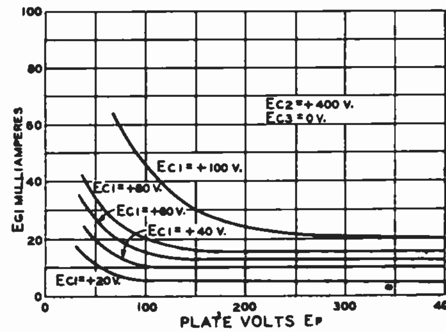


Figure 8

E_{g1} VS. E_p CHARACTERISTICS OF 813 TUBE

8. The plate load resistance is:

$$R_L = \frac{E_p - e_{p\,min}}{i_{p\,max}} = \frac{1500}{0.605} = 2500 \text{ ohms}$$

9. If a loaded plate tank circuit Q of 12 is desired, the reactance of the plate tank capacitor at the resonant frequency should be:

$$\text{Reactance (ohms)} = \frac{R_L}{Q} = \frac{2500}{12} = 208 \text{ ohms}$$

10. For an operating frequency of 4.0 Mc., the effective resonant capacity is:

$$C = \frac{1}{6.28 \times 4.0 \times 208} = 193\ \mu\mu\text{fd.}$$

11. The inductance required to resonate at 4.0 Mc. with this value of capacity is:

$$L = \frac{208}{6.28 \times 4.0} = 8.3 \text{ microhenries}$$

Grid Circuit Considerations

1. The maximum positive grid potential is 60 volts, and the peak r-f grid voltage is 105 volts. Required driving power is 0.53 watt. The equivalent grid resistance of this stage is:

$$R_g = \frac{(e_g)^2}{2 \times P_g} = \frac{105^2}{2 \times 0.53} = 10{,}400 \text{ ohms}$$

2. As in the case of the Class B audio amplifier the grid resistance of the linear amplifier varies from infinity to a low value when maximum grid current is drawn. To decrease the effect of this resistance excursion, a swamping resistor should be placed across the grid tank circuit. The value of the resistor should be dropped until a shortage of driving power begins to be noticed. For this example, a resistor of 3,000 ohms is used. The grid circuit load for no grid current is now 3,000 ohms instead of infinity, and drops to 2,300 ohms when maximum grid current is drawn.

3. A circuit Q of 15 is chosen for the grid tank. The capacitive reactance required is:

$$X_C = \frac{2300}{15} = 154 \text{ ohms}$$

4. At 4.0 Mc. the effective capacity is:

$$C = \frac{1}{6.28 \times 4 \times 154} = 225\ \mu\mu\text{fd.}$$

5. The inductive reactance required to resonate the grid circuit at 4.0 Mc. is:

$$L = \frac{154}{6.28 \times 4.0} = 6.1 \text{ microhenries}$$

6. By substituting the loaded grid resistance figure in the formula in the first paragraph, the grid driving power is now found to be approximately 2.5 watts.

Screen Circuit Considerations By reference to the plate characteristic curve of the 813 tube, it can be seen that at a minimum plate potential of 500 volts, and a maximum plate current of 0.6 ampere, the screen current will be approximately 30 milliamperes, dropping to one or two milliamperes in the quiescent state. It is necessary to use a well-regulated screen supply to hold the screen voltage at the correct potential over this range of current excursion. The use of an electronic regulated screen supply is recommended.

7-5 Special R-F Power Amplifier Circuits

The r-f power amplifier discussions of Sections 7-3 and 7-4 have been based on the assumption that a conventional grounded-cathode or cathode-return type of amplifier was in question. It is possible, however, as in the case of a-f and low-level r-f amplifiers to use circuits in which electrodes other than the cathode are returned to ground insofar as the signal potential is concerned. Both the plate-return or cathode-follower amplifier and the grid-return or grounded-grid amplifier are effective in certain circuit applications as tuned r-f power amplifiers.

Disadvantages of Grounded-Cathode Amplifiers An undesirable aspect of the operation of cathode-return r-f power amplifiers using triode tubes is that such amplifiers must be neutralized. Principles and methods of neutralizing r-f power amplifiers are discussed in the chapter *Generation of R-F Energy*. As the frequency of operation of an amplifier is increased the stage becomes more and more difficult to neutralize due to inductance in the grid and plate leads of the tubes and in the leads to the neutralizing capacitors. In other words the bandwidth of neutralization decreases as the frequency is increased. In addition the very presence of the neutralizing capacitors adds additional undesirable capacitive loading to the grid and plate tank circuits of the tube or tubes. To look at the problem in another way, an amplifier that may be perfectly neutralized at a frequency of 30 Mc. may be completely out of neutralization at a frequency of 120 Mc. Therefore, if there are circuits in both the grid and plate circuits which offer appreciable impedance at this high frequency it is quite possible that the stage may develop a "parasitic oscillation" in the vicinity of 120 Mc.

Grounded-Grid R-F Amplifiers This condition of restricted-range neutralization of r-f power amplifiers can be greatly alleviated through the use of a cathode-return or grounded-grid r-f stage. The grounded-grid amplifier has the following advantages:

1. The output capacitance of a stage is reduced to approximately one-half the value which would be obtained if the same tube or tubes were operated as a conventional neutralized amplifier.

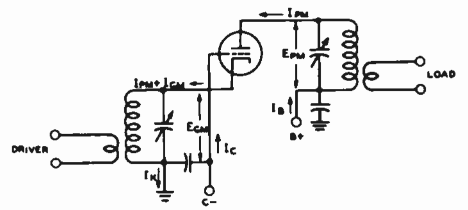
2. The tendency toward parasitic oscillations in such a stage is greatly reduced since the shielding effect of the control grid be-

tween the filament and the plate is effective over a broad range of frequencies.

3. The feedback capacitance within the stage is the plate-to-cathode capacitance which is ordinarily very much less than the grid-to-plate capacitance. Hence neutralization is ordinarily not required. If neutralization is required the neutralizing capacitors are very small in value and are cross connected between plates and cathodes in a push-pull stage, or between the opposite end of a split plate tank and the cathode in a single-ended stage.

The disadvantages of a grounded-grid amplifier are:

1. A large amount of excitation energy is required. However, only the normal amount of energy is lost in the grid circuit of the amplifier tube; all additional energy over this amount is delivered to the load circuit as useful output.
2. The cathode of a grounded-grid amplifier stage is "hot" to r.f. This means that the cathode must be fed through a suitable impedance from the filament supply, or the secondary of the filament transformer must be of the low-capacitance type and adequately insulated for the r-f voltage which will be present.
3. A grounded-grid r-f amplifier cannot be plate modulated 100 per cent unless the output of the exciting stage is modulated also. Approximately 70 per cent modulation of the exciter stage as the final stage is being modulated 100 per cent is recommended. However, the grounded-grid r-f amplifier is quite satisfactory as a Class B linear r-f amplifier for single sideband or conventional amplitude modulated waves or as an amplifier for a straight c-w or FM signal.



POWER OUTPUT TO LOAD = $\frac{(E_{GM}+E_{PM})\,I_{PM}}{2}$ OR $\frac{E_{PM}\,I_{PM}}{2}+\frac{E_{GM}\,I_{PM}}{2}$

POWER DELIVERED BY OUTPUT TUBE = $\frac{E_{PM}\,I_{PM}}{2}$

POWER FROM DRIVER TO LOAD = $\frac{E_{GM}\,I_{PM}}{2}$

TOTAL POWER DELIVERED BY DRIVER = $\frac{E_{GM}\,(I_{PM}+I_{GM})}{2}$

OR $\frac{E_{GM}\,I_{PM}}{2}+0.9\,E_{GM}\,I_C$

POWER ABSORBED BY OUTPUT TUBE GRID AND BIAS SUPPLY.

= $\frac{E_{GM}\,I_{GM}}{2}$ OR $0.9\,E_{GM}\,I_C$

Z_K = (APPROXIMATELY) = $\frac{E_{GM}}{I_{PM}+1.8\,I_C}$

Figure 9

GROUNDED-GRID CLASS B OR CLASS C AMPLIFIER

The equations in the above figure give the relationships between the fundamental components of grid and plate potential and current, and the power input and power output of the stage. An expression for the approximate cathode impedance is given

Figure 9 shows a simplified representation of a grounded-grid triode r-f power amplifier stage. The relationships between input and output power and the peak fundamental components of electrode voltages and currents are given below the drawing. The calculation of the complete operating conditions for a grounded-grid amplifier stage is somewhat more complex than that for a conventional amplifier because the input circuit of the tube is in series with the output circuit as far as the load is concerned. The primary result of this effect is, as stated before, that considerably more power is required from the driver stage. The normal power gain for a g-g stage is from 3 to 15 depending upon the grid circuit conditions chosen for the output stage. The higher the grid bias and grid swing required on the output stage, the higher will be the requirement from the driver.

Calculation of Operating Conditions of Grounded Grid R-F Amplifiers It is most convenient to determine the operating conditions for a Class B or Class C grounded-grid r-f power amplifier in a two-step process. The first step is to determine the plate-circuit and grid-circuit operating conditions of the tube as though it were to operate as a conventional cathode-return amplifier stage. The second step is then to add in the additional conditions imposed upon the operating conditions by the fact that the stage is to operate as a grounded-grid amplifier.

For the first step in the calculation the procedure given in Section 7-3 is quite satisfactory and will be used in the example to follow. Suppose we take for our example the case of a type 304TL tube operating at 2700 plate volts at a kilowatt input. Following through the procedure previously given:

1. Desired power output—850 watts
   Desired Plate voltage—2700 volts
   Desired plate efficiency—85 per cent
   (N_p = 0.85)

2. $P_{in} = 850/0.85 = 1000$ watts

3. $P_p = 1000 - 850 = 150$ watts
Type 304TL chosen; max. $P_p = 300$ watts, $\mu = 12$.

4. $I_b = 1000/2700 = 0.370$ ampere (370 ma.)

5. Approximate $i_{pmax} = 4.9 \times 0.370 = 1.81$ ampere

6. $e_{pmin} = 140$ volts (from 304TL constant-current curves)

7. $E_{pm} = 2700 - 140 = 2560$ volts

8. $I_{pm}/I_b = 2 \times 0.85 \times 2700/2560 = 1.79$

9. $i_{pmax}/I_b = 4.65$ (from figure 3)

10. $i_{pmax} = 4.65 \times 0.370 = 1.72$ amperes

11. $e_{gmp} = 140$ volts
$i_{gmax} = 0.480$ amperes

12. $\cos \theta_p = 2.32\,(1.79-1.57) = 0.51$
$\theta_p = 59°$

13. $$E_{cc} = \frac{1}{1-0.51} \times \left[0.51\left(\frac{2560}{12} - 140\right) - \frac{2700}{12}\right] = -385 \text{ volts}$$

14. $E_{gm} = 140-(-385) = 525$ volts

15. $E_{gm}/E_{cc} = -1.36$

16. $i_{gmax}/I_c =$ approx. 8.25 (extrapolated from figure 4)

17. $I_c = 0.480/8.25 = 0.058$ (58 ma. d-c grid current)

18. $P_d = 0.9 \times 525 \times 0.058 = 27.5$ watts

19. $P_g = 27.5 - (-385 \times 0.058) = 5.2$ watts
Max. P_g for 304TL is 50 watts

We can check the operating plate efficiency of the stage by the method described in Section 7-3 as follows:

$F_1 = E_{pm}/E_{bb} = 2560/2700 = 0.95$
F_2 for θ_p of 59° (from figure 6) $= 0.90$
$N_p = F_1 \times F_2 = 0.95 \times 0.90 =$ Approx. 0.85 (85 per cent plate efficiency)

Now, to determine the operating conditions as a grounded-grid amplifier we must also know the peak value of the fundamental components of plate current. This is simply equal to $(I_{pm}/I_b)\,I_b$, or:

$I_{pm} = 1.79 \times 0.370 = 0.660$ amperes (from 4 and 8 above)

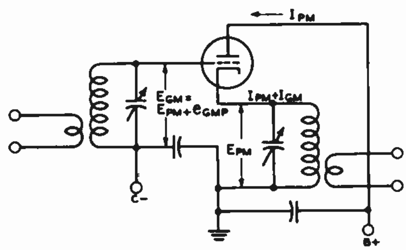
The total average power required of the driver (from figure 9) is equal to $E_{gm}I_{pm}/2$ (since the grid is grounded and the grid swing appears also as cathode swing) plus P_d which is 27.5 watts from 18 above. The total is:

$$\text{Total drive} = \frac{525 \times 0.660}{2} = 172.5 \text{ watts}$$
plus 27.5 watts or 200 watts

Therefore the total power output of the stage is equal to 850 watts (contributed by the 304TL) plus 172.5 watts (contributed by the driver) or 1022.5 watts. The cathode driving impedance of the 304TL (again referring to figure 7) is approximately:

$Z_k = 525/(0.660 + 0.116) =$ approximately 675 ohms.

Plate-Return or Cathode-Follower R-F Power Amplifier Circuit diagram, electrode potentials and currents, and operating conditions for a cathode-follower r-f power amplifier are given in figure 10. This circuit can be used, in addition to the grounded-grid circuit just discussed, as an r-f amplifier with a triode tube and no additional neutralization circuit. However, the circuit will oscillate if the impedance from cathode to ground is allowed to become capacitive rather than inductive or resistive with respect to the operating frequency. The circuit is not recommended except for v-h-f or u-h-f work with coaxial lines as tuned circuits since the peak grid swing required on the r-f amplifier stage is approximately equal to the plate voltage on the amplifier tube if high-efficiency operation is desired. This means, of course, that the grid tank must be able to withstand slightly more peak voltage than the plate tank. Such a stage may not be plate modulated unless the driver stage is modulated the same percentage as the final amplifier. However, such a stage may be used as an amplifier or modulated waves (Class B linear) or as a c-w or FM amplifier.



POWER OUTPUT TO LOAD $= \frac{E_{PM}(I_{PM}+I_{GM})}{2}$

POWER DELIVERED BY OUTPUT TUBE $= \frac{E_{PM} I_{PM}}{2}$

POWER FROM DRIVER TO LOAD $= \frac{E_{PM} I_{GM}}{2}$

TOTAL POWER FROM DRIVER $= \frac{E_{GM} I_{GM}}{2} = \frac{(E_{PM}+e_{GMP}) I_{GM}}{2}$

$=$ APPROX. $\frac{(E_{PM}+e_{GMP})\, 1.8\, I_C}{2}$

ASSUMING $I_{GM} \cong 1.8\, I_C$

POWER ABSORBED BY OUTPUT TUBE GRID AND BIAS SUPPLY:

$=$ APPROX. $0.9\,(E_{CC} + e_{GMP})\, I_C$

$Z_G = \frac{E_{GM}}{I_{GM}} =$ APPROX. $\frac{(E_{PM}+e_{GMP})}{1.8\, I_C}$

Figure 10

CATHODE-FOLLOWER R-F POWER AMPLIFIER

Showing the relationships between the tube potentials and currents and the input and output power of the stage. The approximate grid impedance also is given.

The design of such an amplifier stage is essentially the same as the design of a grounded-grid amplifier stage as far as the first step is concerned. Then, for the second step the operating conditions given in figure 10 are applied to the data obtained in the first step. As an example, take the 304TL stage previously described. The total power required of the driver will be (from figure 10) approximately (2700X0.58X1.8)/2 or 141 watts. Of this 141 watts 27.5 watts (as before) will be lost as grid dissipation and bias loss and the balance of 113.5 watts will appear as output. The total output of the stage will then be approximately 963 watts.

Cathode Tank for G-G or C-F Power Amplifier The cathode tank circuit for either a grounded-grid or cathode-follower r-f power amplifier may be a conventional tank circuit if the filament transformer for the stage is of the low-capacitance high-voltage type. Conventional filament transformers, however, will not operate with the high values of r-f voltage present in such a circuit. If a conventional filament transformer is to be used the cathode tank coil may consist of two parallel heavy conductors (to carry the high filament current) by-passed at both the ground end and at the tube socket. The tuning capacitor is then placed between filament and ground. It is possible in certain cases to use two r-f chokes of special design to feed the filament current to the tubes, with a conventional tank circuit between filament and ground. Coaxial lines also may be used to serve both as cathode tank and filament feed to the tubes for v-h-f and u-h-f work.

7-6 A Grounded-Grid 304TL Amplifier

The 304TL tube is capable of operating as an r-f amplifier of the conventional type with the full kilowatt input permitted amateur stations. The tube is characterized by an enormous reserve of filament emission, resulting from the fact that about 130 watts is required merely to light the four filaments. Where the heavy filament drain, plus the low amplification factor of about 12, does not impose hardship in the design of the transmitter, the 304TL is quite satisfactory for amateur service.

The 304TL offers an additional feature in that its plate-to-cathode capacitance is very low (about 0.6 $\mu\mu$fd.) for a tube of its size and power handling capabilities. This feature permits the tube to be operated, without neutralization, as a grounded-grid r-f power amplifier.

Characteristics of Grounded-Grid Operation Although the excitation power of the tube is only 27.5 watts (which would be the actual driving power required if the tube were operating as a neutralized amplifier) the driving power required into the cathode circuit from the exciter is about 200 watts. The extra 170 watts or so is not lost, however, since it appears directly in the output of the amplifier as additional energy. Thus while the 304TL itself will deliver about 850 watts to the load circuit, the extra 170 watts supplied by the driver over and above the 27.5 watts required to excite the 304TL appears added to the 850-watt output of the 304TL. Thus the total output of the stage would be about 1020 watts, even though the d-c input to the 304TL was only one kilowatt. Nevertheless, the tube itself operates only at its normal plate-circuit efficiency, the extra power output coming directly from the added excitation power taken from the driver.

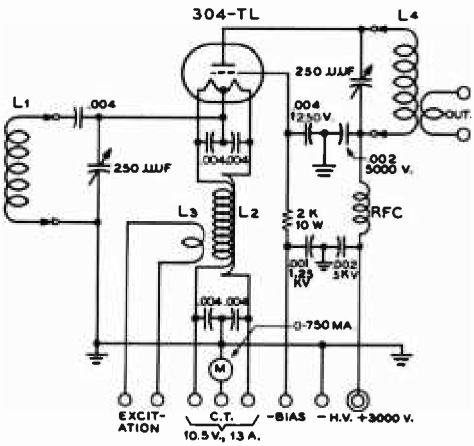


Figure 11
SCHEMATIC OF THE
304TL G-G AMPLIFIER

L_1—None required for 3.5 Mc., since cathode coil L_2 tunes to 3.5 Mc.
7 Mc.—20 turns no. 14 enam., 1¼" dia. by 3" long.
14 Mc.—10 turns no. 8 bare, 1¼" dia. by 3" long.
L_2—Two parallel lengths of no. 12 enam. close-wound to fill National type XR-10A coil form.
25 turns of the two wires in parallel.
L_3—5-turn link of no. 16 rubber and cotton covered wire.
L_4—3.5 Mc.: 18 turns no. 12 enam.; Nat. XR-10A form wound full, 4 t. link
7 Mc.: 10 turns no. 12 enam.; Nat. XR-10A form, 3 t. link
14 Mc.: 4 turns no. 8 bare; Nat. XR-10A form, 2 t. link
RFC—800-ma. r-f choke (National R-175)

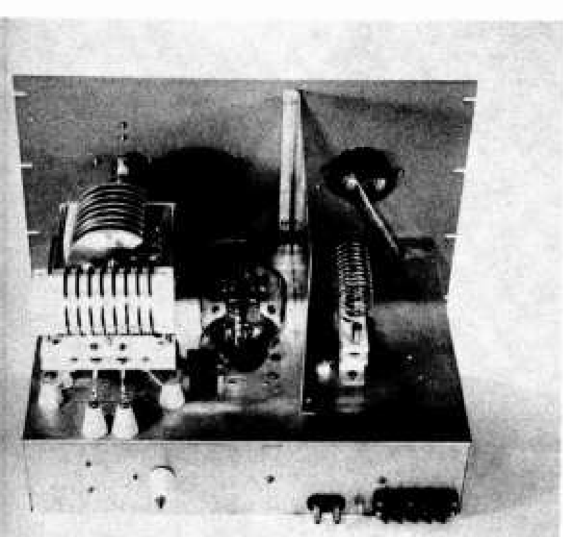


Figure 12
REAR OF THE GROUNDED-GRID
AMPLIFIER

Since 15 to 20 per cent of the output from a grounded-grid r-f stage passes directly through it from the driver, it is obvious that conventional plate modulation of the output stage only will give incomplete modulation. In fact, if the plate voltage is completely removed from the g-g (grounded-grid) stage and the plate return is grounded, the energy from the driver will pass directly through the tube and appear in the output circuit. So it becomes necessary to apply modulation to the driver tube simultaneously to that which is applied to the plate of the g-g stage. It is normal practice in commercial application to modulate the driver stage about 60 per cent as much as the g-g stage.

For straight c-w operation no special considerations are involved in the use of a g-g power amplifier except that it obviously is necessary that the driver stage be keyed simultaneously with the final amplifier, if the installation is such that the final amplifier is to be keyed. With excitation, keying the combination of the driver and output stage will operate quite normally.

The Grounded-Grid Class B Linear The g-g power amplifier is particularly well suited to use as a class B linear amplifier to build up the output of a lower powered SSB transmitter. Two advantages obtained through the use of the g-g stage as a class B linear amplifier are (1) no swamping is required in the input circuit of the g-g stage, and (2) nearly the full output of the exciter transmitter appears in the output of the g-g stage, being added to the output of the g-g amplifier.

Since operating impedances are lowered when a stage is operated as a Class B linear, rather high values of tank capacitance are required for a satisfactory operating circuit Q. The load impedance presented to one 304TL with the operating conditions specified above is about 2500 ohms; hence the plate tank circuit capacitance for an operating Q of 15 should be about 180 ohms. This represents an operating plate tank capacitance of about 240 μμfd. for 4 Mc., and proportionately smaller capacitances for the higher frequency bands. The cathode impedance for one 304TL under the operating conditions specified is about 700 ohms. Thus, for an operating cathode-circuit Q of 10 the cathode tank capacitance should have a reactance of 70 ohms. This value of reactance is represented by about 550 $\mu\mu$fd. at 4 Mc., and proportionately smaller capacitances for higher frequencies. Since the peak cathode voltage is only about 400, quite small spacing in the cathode tank capacitor can be used.

Figure 11 illustrates a practical grounded-grid amplifier, using a single 304TL tube. A bifilar wound coil is used to feed the filament voltage to the tube. Shunting inductors are used to tune the filament circuit to higher frequencies. When tuning the g-g stage, it must be remembered that the input tuned circuit is effectively in series with the output circuit as far as the output energy is concerned. Thus, it is not possible to apply full excitation power to the stage unless plate current is also flowing. If full excitation is applied in the absence of plate voltage, the grid of the output tube would be damaged from excessive excitation. Construction of the amplifier is illustrated in figures 12 and 13.

A 3000-volt plate supply is used which should have good regulation. An output filter condenser of at least 10 microfarads should be employed for Class B operation. Class B operating bias is -260 volts, obtained from a well regulated bias supply.

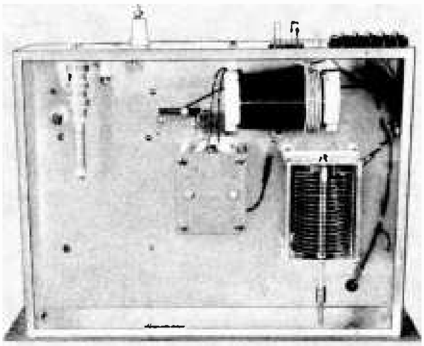


Figure 13
UNDERSIDE OF THE GROUNDED-GRID AMPLIFIER

For operation in TV areas, additional lead filtering is required, as well as complete screening of the amplifier.

CHAPTER EIGHT

The Oscilloscope

The cathode-ray oscilloscope (also called oscillograph) is an instrument which permits visual examination of various electrical phenomena of interest to the electronic engineer. Instantaneous changes in voltage, current and phase are observable if they take place slowly enough for the eye to follow, or if they are periodic for a long enough time so that the eye can obtain an impression from the screen of the cathode-ray tube. In addition, the cathode-ray oscilloscope may be used to study any variable (within the limits of its frequency response characteristic) which can be converted into electrical potentials. This conversion is made possible by the use of some type of *transducer*, such as a vibration pickup unit, pressure pickup unit, photoelectric cell, microphone, or a variable impedance. The use of such a transducer makes the oscilloscope a valuable tool in fields other than electronics.

8-1 A Typical Cathode-Ray Oscilloscope

For the purpose of analysis, the operation of a simple oscilloscope will be described. The Du Mont type 274-A unit is a fit instrument for such a description. The block diagram of the 274-A is shown in figure 1. The electron beam of the cathode-ray tube can be moved vertically or horizontally, or the vertical and horizontal movements may be combined to produce composite patterns on the tube screen. As shown in figure 1, the cathode-ray tube is the recipient of signals from two sources: the vertical and horizontal amplifiers. The operation of the cathode-ray tube itself has been covered in Chapter 4; the auxiliary circuits pertaining to the cathode-ray tube will be covered here.

The Vertical Amplifier The incoming signal which is to be examined is applied to the terminals marked *Vertical Input* and *Ground.* The Vertical Input terminal is connected through capacitor C_1 (figure 2) so that the a-c component of the input signal appears across the vertical amplifier gain control potentiometer, R_1. Thus the magnitude of the incoming signal may be controlled to provide the desired deflection on the screen of

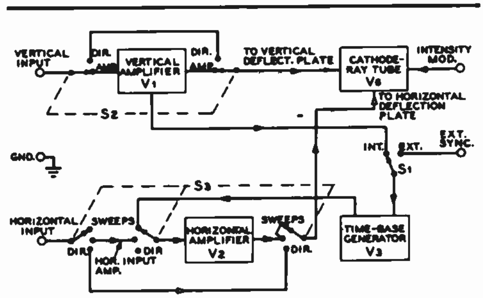


Figure 1

BLOCK DIAGRAM, TYPE 274-A CATHODE-RAY OSCILLOSCOPE

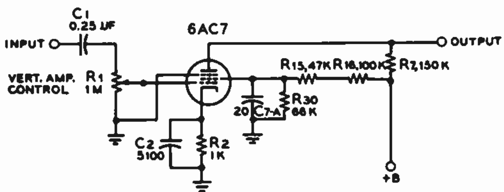


Figure 2
TYPICAL AMPLIFIER SCHEMATIC

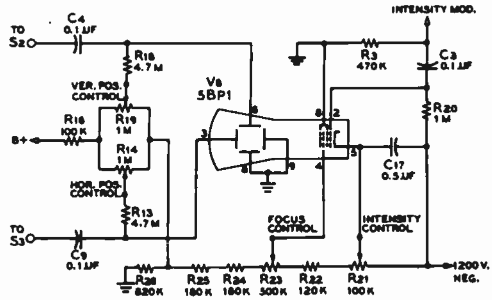


Figure 3
SCHEMATIC OF CATHODE-RAY TUBE CIRCUITS

A 5BP1A cathode-ray tube is used in this instrument. As shown, the necessary potentials for operating this tube are obtained from a voltage divider made up of resistors R_{21} through R_{26} inclusive. The intensity of the beam is adjusted by moving the contact on R_{21}. This adjusts the potential on the cathode more or less negative with respect to the grid which is operated at the full negative voltage—1200 volts. Focusing to the desired sharpness is accomplished by adjusting the contact on R_{23} to provide the correct potential for anode no. 1. Interdependency between the focus and the intensity controls is inherent in all electrostatically focused cathode-ray tubes. In short, there is an optimum setting of the focus control for every setting of the intensity control. The second anode of the 5BP1A is operated at ground potential in this instrument. Also one of each pair of deflection plates is operated at ground potential.

The cathode is operated at a high negative potential (approximately 1200 volts) so that the total overall accelerating voltage of this tube is regarded as 1200 volts since the second anode is operated at ground potential. The vertical and horizontal positioning controls which are connected to their respective deflection plates are capable of supplying either a positive or negative d-c potential to the deflection plates. This permits the spot to be positioned at any desired place on the entire screen.

the cathode-ray tube. Also, as shown in figure 1, S_2 has been incorporated to by-pass the vertical amplifier and capacitively couple the input signal directly to the vertical deflection plate if so desired.

In figure 2, V_1 is a 6AC7 pentode tube which is used as the vertical amplifier. As the signal variations appear on the grid of V_1, variations in the plate current of V_1 will take place. Thus signal variations will appear in opposite phase and greatly amplified across the plate resistor, R_7. Capacitor C_2 has been added across R_2 in the cathode circuit of V_1 to flatten the frequency response of the amplifier at the high frequencies. This capacitor because of its low value has very little effect at low input frequencies, but operates more effectively as the frequency of the signal increases. The amplified signal delivered by V_1 is now applied through the second half of switch S_2 and capacitor C_4 to the free vertical deflection plate of the cathode-ray tube (figure 3).

The Horizontal Amplifier The circuit of the horizontal amplifier and the circuit of the vertical amplifier, described in the above paragraph, are similar. A switch in the input circuit makes provision for the input from the *Horizontal Input* terminals to be capacitively coupled to the grid of the horizontal amplifier or to the free horizontal deflection plate thus by-passing the amplifier, or for the output of the sweep generator to be capacitively coupled to the amplifier, as shown in figure 1.

The Time Base Generator Investigation of electrical wave forms by the use of a cathode-ray tube frequently requires that some means be readily available to determine the variation in these wave forms with respect to time. When such a time base is required, the patterns presented on the cathode-ray tube screen show the variation in amplitude of the input signal with respect to time. Such an arrangement is made possible by the inclusion in the oscilloscope of a *Time Base-Generator*. The function of this generator is to move the spot across the screen at a constant rate from left to right between two selected points, to return the spot almost instantaneously to its original position, and to

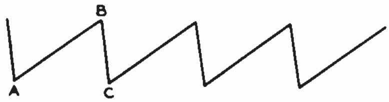


Figure 4
SAWTOOTH WAVE FORM

repeat this procedure at a specified rate. This action is accomplished by the voltage output from the time base (sweep) generator. The rate at which this voltage repeats the cycle of sweeping the spot across the screen is referred to as the *sweep frequency*. The sweep voltage necessary to produce the motion described above must be of a sawtooth waveform, such as that shown in figure 4.

The sweep occurs as the voltage varies from A to B, and the *return trace* as the voltage varies from B to C. If A-B is a straight line, the sweep generated by this voltage will be linear. It should be realized that the sawtooth sweep signal is only used to plot variations in the vertical axis signal with respect to time. Specialized studies have made necessary the use of sweep signals of various shapes which are introduced from an external source through the Horizontal Input terminals.

The Sawtooth Generator The sawtooth voltage necessary to obtain the linear time base is generated by the circuit of figure 5, which operates as follows:

A type 884 gas triode (V_3) is used for the sweep generator tube. This tube contains an inert gas which ionizes when the voltage between the cathode and the plate reaches a certain value. The ionizing voltage depends upon the bias voltage of the tube, which is determined by the voltage divider resistors R_{12}-R_{17}. With a specific negative bias applied to the 884 tube, the tube will ionize (or fire) at a specific plate voltage.

Capacitors C_{10}-C_{14} are selectively connected in parallel with the 884 tube. Resistor R_{11} limits the peak current drain of the gas triode. The plate voltage on this tube is obtained through resistors R_{28}, R_{27} and R_{11}. The voltage applied to the plate of the 884 tube cannot reach the power supply voltage because of the charging effect this voltage has upon the capacitor which is connected across the tube. This capacitor charges until the plate voltage becomes high enough to ionize the gas in the tube. At this time, the 884 tube starts to conduct and the capacitor discharges through the tube until its voltage falls to the extinction potential of the tube. When the tube stops conducting, the capacitor voltage builds up until the tube fires again. As this action continues, it results in the sawtooth wave form of figure 4 appearing at the junction of R_{11} and R_{27}.

Synchronization Provision has been made so the sweep generator may be synchronized from the vertical amplifier or from an external source. The switch S_1 shown in figure 5 is mounted on the front panel to be easily accessible to the operator.

If no synchronizing voltage is applied, the discharge tube will begin to conduct when the plate potential reaches the value of E_f (Firing Potential). When this breakdown takes place and the tube begins to conduct, the capacitor is discharged rapidly through the tube, and the plate voltage decreases until it reaches the extinction potential E_x. At this point conduction ceases, and the plate potential rises slowly as the capacitor begins to charge through R_{27} and R_{28}. The plate potential will again reach a point of conduction and the circuit will start a new cycle. The rapidity of the plate voltage rise is dependent upon the circuit constants R_{27}, R_{28}, and the capacitor selected,

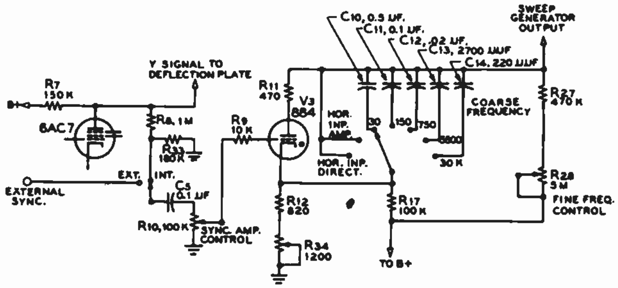


Figure 5
SCHEMATIC OF SWEEP GENERATOR

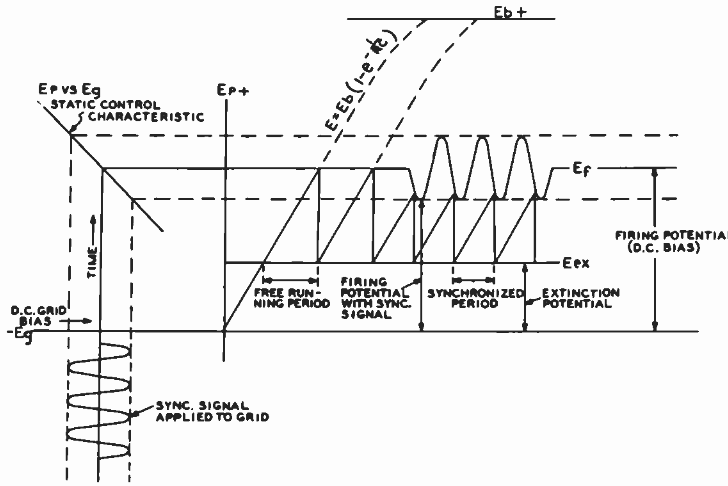


Figure 6

ANALYSIS OF SYNCHRONIZATION OF TIME-BASE GENERATOR

C10-C14, as well as the supply voltage E_b. The exact relationship is given by:

$$E_c = E_b\left(1 - e^{\frac{-t}{rc}}\right)$$

Where E_c = Capacitor voltage at time t
E_b = Supply voltage (B+ supply − cathode bias)
E_f = Firing potential or potential at which time-base gas triode fires
E_x = Extinction potential or potential at which time-base gas triode ceases to conduct
e = Base of natural logarithms
t = Time in seconds
r = Resistance in ohms (R_{27} + R_{28})
c = Capacity in farads ($C_{10, 11, 12, 13}$, or $_{14}$)

The frequency of oscillation will be approximately:

$$f = \frac{E_b}{rc}\left(\frac{1}{E_f - E_x}\right)$$

Under this condition (no synchronizing signal applied) the oscillator is said to be *free running*.

When a positive synchronizing voltage is applied to the grid, the firing potential of the tube is reduced. The tube therefore ionizes at a lower plate potential than when no grid signal is applied. Thus the applied snychronizing voltage fires the gas-filled triode each time the plate potential rises to a sufficient value, so that the sweep recurs at the same or an integral sub-multiple of the synchronizing signal rate. This is illustrated in figure 6.

Power Supply Figure 7 shows the power supply to be made up of two definite sections: a low voltage positive supply which provides power for operating the amplifiers, the sweep generator, and the positioning circuits of the cathode-ray tube; and the high voltage negative supply which provides the potentials necessary for operating the various

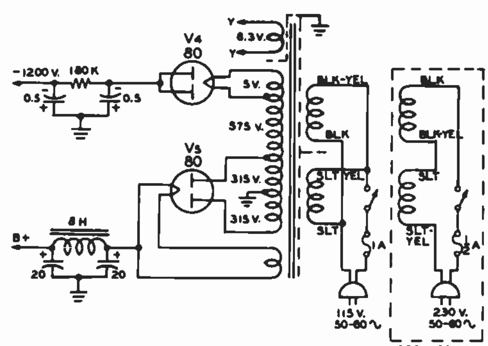


Figure 7

SCHEMATIC OF POWER SUPPLY

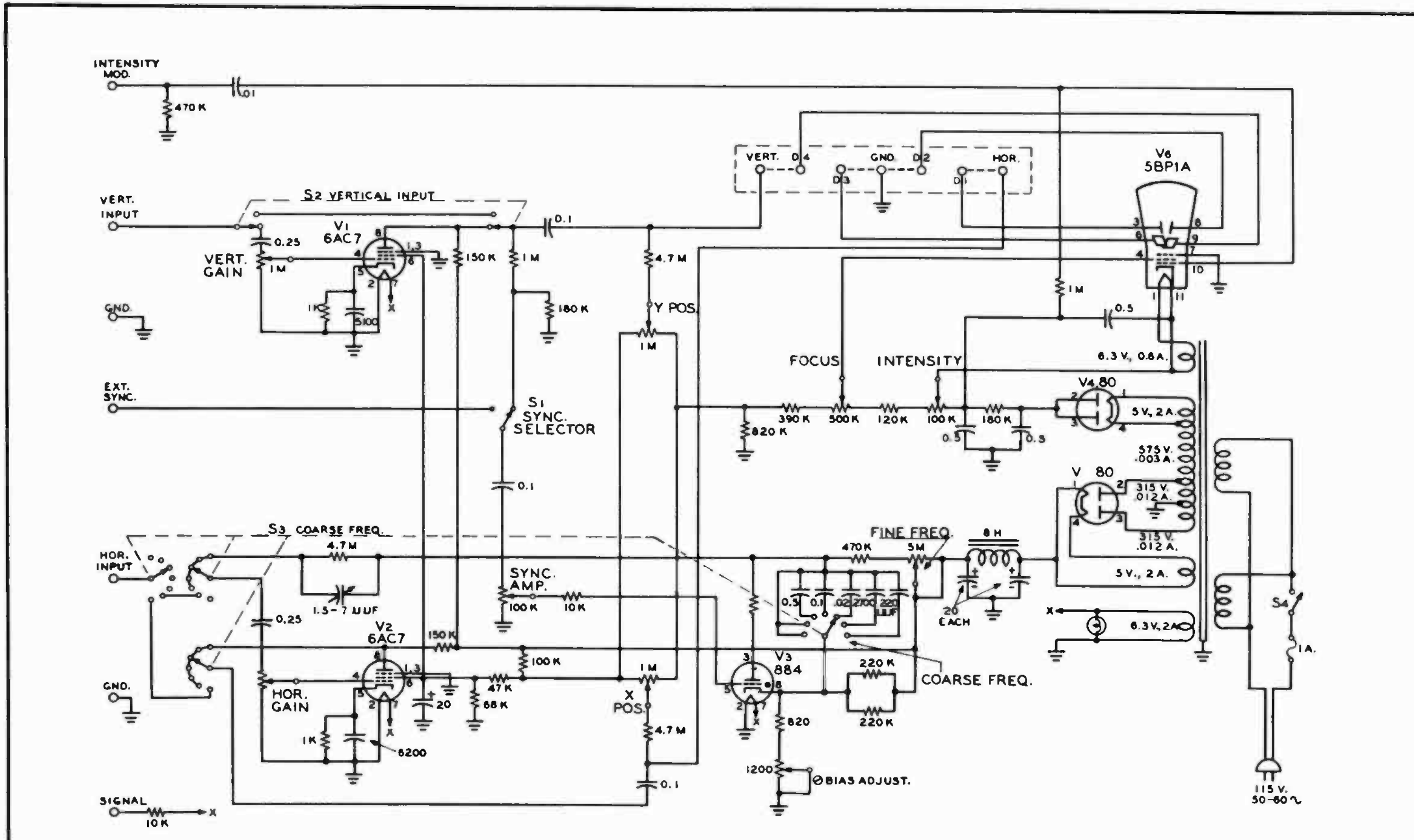


Figure 8

CIRCUIT OF TYPE 274-A CATHODE-RAY OSCILLOSCOPE

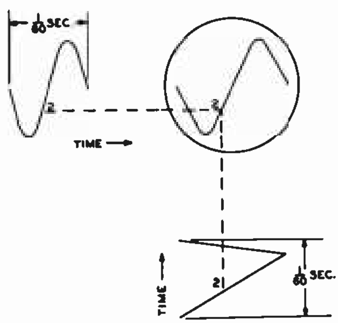


Figure 9

PROJECTION DRAWING OF A SINEWAVE APPLIED TO THE VERTICAL AXIS AND A SAWTOOTH WAVE OF THE SAME FREQUENCY APPLIED SIMULTANEOUSLY ON THE HORIZONTAL AXIS

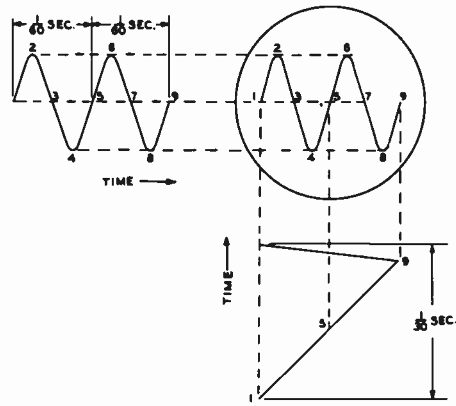


Figure 10

PROJECTION DRAWING SHOWING THE RESULTANT PATTERN WHEN THE FREQUENCY OF THE SAWTOOTH IS ONE-HALF OF THAT EMPLOYED IN FIGURE 9

electrodes of the cathode-ray tube, and for certain positioning controls.

The positive low voltage supply consists of full-wave rectifier (V_5), the output of which is filtered by a capacitor input filter (20-20 μfd. and 8 H). It furnishes approximately 400 volts. The high voltage power supply employs a half wave rectifier tube, V_4. The output of this rectifier is filtered by a resistance-capacitor filter consisting of 0.5-0.5 μfd. and .18 M. A voltage divider network attached from the output of this filter obtains the proper operating potentials for the various electrodes of the cathode-ray tube. The complete schematic of the Du Mont 274-A Oscilloscope is shown in figure 8.

8-2 Display of Waveforms

Together with a working knowledge of the controls of the oscilloscope, an understanding of how the patterns are traced on the screen must be obtained for a thorough knowledge of oscilloscope operation. With this in mind a careful analysis of two fundamental waveform patterns is discussed under the following headings:

a. Patterns plotted against time (using the sweep generator for horizontal deflection).
b. Lissajous Figures (using a sine wave for horizontal deflection).

Patterns Plotted Against Time A sine wave is typical of such a pattern and is convenient for this study. This wave is amplified by the vertical amplifier and impressed on the vertical (Y-axis) deflection plates of the cathode-ray tube. Simultaneously the sawtooth wave from the time base generator is amplified and impressed on the horizontal (X-axis) deflection plates.

The electron beam moves in accordance with the resultant of the sine and sawtooth signals. The effect is shown in figure 9 where the sine and sawtooth waves are graphically represented on time and voltage axes. Points on the two waves that occur simultaneously are numbered similarly. For example, point 2 on the sine wave and point 2 on the sawtooth wave occur at the same instant. Therefore the position of the beam at instant 2 is the resultant of the voltages on the horizontal and vertical deflection plates at instant 2. Referring to figure 9, by projecting lines from the two point 2 positions, the position of the electron beam at instant 2 can be located. If projections were drawn from every other instantaneous position of each wave to intersect on the circle representing the tube screen, the intersections of similarly timed projections would trace out a sine wave.

In summation, figure 9 illustrates the principles involved in producing a sine wave trace on the screen of a cathode-ray tube. Each intersection of similarly timed projections represents the position of the electron beam acting under the influence of the varying voltage waveforms on each pair of deflection plates. Figure 10 shows the effect on the pattern of decreasing the frequency of the sawtooth

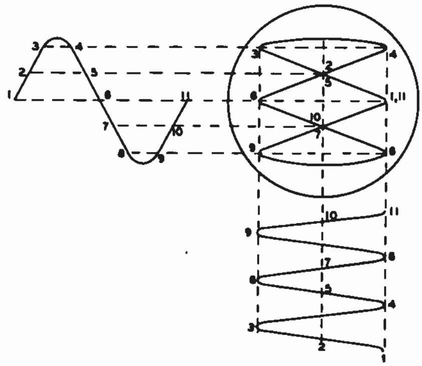


Figure 11

PROJECTION DRAWING SHOWING THE RESULTANT LISSAJOUS PATTERN WHEN A SINE WAVE APPLIED TO THE HORIZONTAL AXIS IS THREE TIMES THAT APPLIED TO THE VERTICAL AXIS

wave. Any recurrent waveform plotted against time can be displayed and analyzed by the same procedure as used in these examples.

The sine wave problem just illustrated is typical of the method by which any waveform can be displayed on the screen of the cathode-ray tube. Such waveforms as square wave, sawtooth wave, and many more irregular recurrent waveforms can be observed by the same method explained in the preceding paragraphs.

8-3 Lissajous Figures

Another fundamental pattern is the Lissajous figure, named after the 19th century French scientist. This type of pattern is of particular use in determining the frequency ratio between two sine wave signals. If one of these signals is known, the other can be easily calculated from the pattern made by the two signals upon the screen of the cathode-ray tube. Common practice is to connect the known signal to the horizontal channel and the unknown signal to the vertical channel.

The presentation of Lissajous figures can be analyzed by the same method as previously used for sine wave presentation. A simple example is shown in figure 11. The frequency ratio of the signal on the horizontal axis to the signal on the vertical axis is 3 to 1. If the known signal on the horizontal axis is 60 cycles per second, the signal on the vertical axis is 20 cycles.

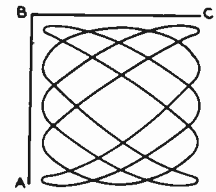


Figure 12

METHOD OF CALCULATING FREQUENCY RATIO OF LISSAJOUS FIGURES

Obtaining a Lissajous Pattern on the screen Oscilloscope Settings

1. The horizontal amplifier should be disconnected from the sweep oscillator. The signal to be examined should be connected to the horizontal amplifier of the oscilloscope.

2. An audio oscillator signal should be connected to the vertical amplifier of the oscilloscope.

3. By adjusting the frequency of the audio oscillator a stationary pattern should be obtained on the screen of the oscilloscope. It is not necessary to stop the pattern, but merely to slow it up enough to count the loops at the side of the pattern.

4. Count the number of loops which intersect an imaginary vertical line AB and the number of loops which intersect the imaginary horizontal line BC as in figure 12. The ratio of the number of loops which intersect AB is to

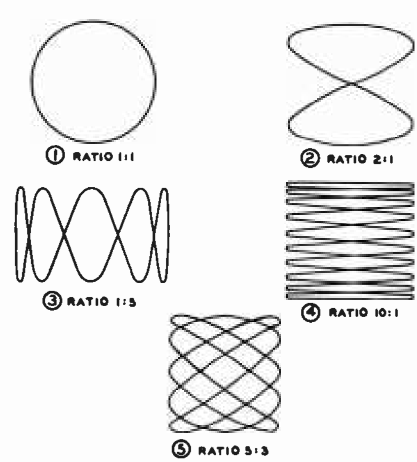


Figure 13

OTHER LISSAJOUS PATTERNS

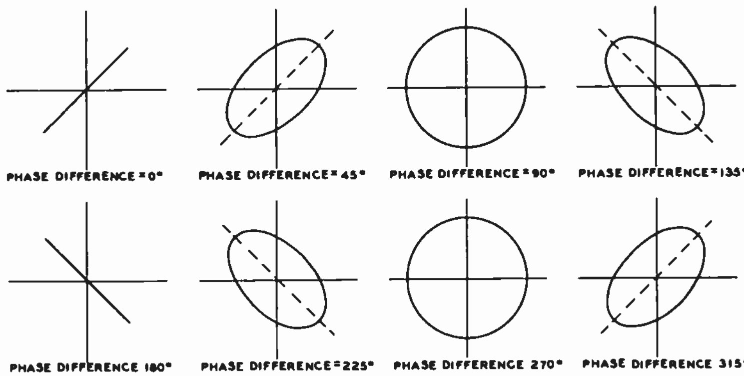


Figure 14
LISSAJOUS PATTERNS OBTAINED FROM THE MAJOR PHASE DIFFERENCE ANGLES

the number of loops which intersect BC as the frequency of the horizontal signal is to the frequency of the vertical signal.

Figure 13 shows other examples of Lissajous figures. In each case the frequency ratio shown is the frequency ratio of the signal on the horizontal axis to that on the vertical axis.

Phase Difference Patterns Coming under the heading of Lissajous figures is the method used to determine the phase difference between signals of the same frequency. The patterns involved take on the form of ellipses with different degrees of eccentricity.

The following steps should be taken to obtain a phase-difference pattern:

1. With no signal input to the oscilloscope, the spot should be centered on the screen of the tube.
2. Connect one signal to the vertical amplifier of the oscilloscope, and the other signal to the horizontal amplifier.
3. Connect a common ground between the two frequencies under investigation and the oscilloscope.
4. Adjust the vertical amplifier gain so as to give about 3 inches of deflection on a 5 inch tube, and adjust the calibrated scale of the oscilloscope so that the vertical axis of the scale coincides precisely with the vertical deflection of the spot.
5. Remove the signal from the vertical amplifier, being careful not to change the setting of the vertical gain control.
6. Increase the gain of the horizontal amplifier to give a deflection exactly the same as that to which the vertical amplifier control is adjusted (3 inches). Reconnect the signal to the vertical amplifier.

The resulting pattern will give an accurate picture of the exact phase difference between the two waves. If these two patterns are exactly the same frequency but different in phase and maintain that difference, the pattern on the screen will remain stationary. If, however, one of these frequencies is drifting slightly, the pattern will drift slowly through 360°. The phase angles of 0°, 45°, 90°, 135°, 180°, 225°, 270°, 315° are shown in figure 14.

Each of the eight patterns in figure 14 can be analyzed separately by the previously used

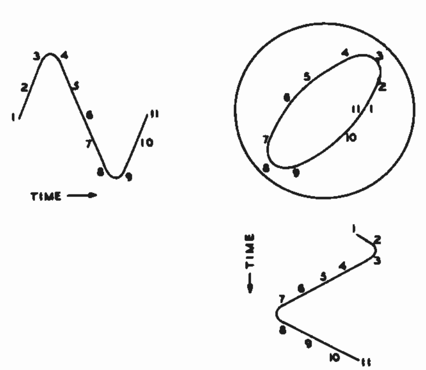


Figure 15
PROJECTION DRAWING SHOWING THE RESULTANT PHASE DIFFERENCE PATTERN OF TWO SINE WAVES 45° OUT OF PHASE

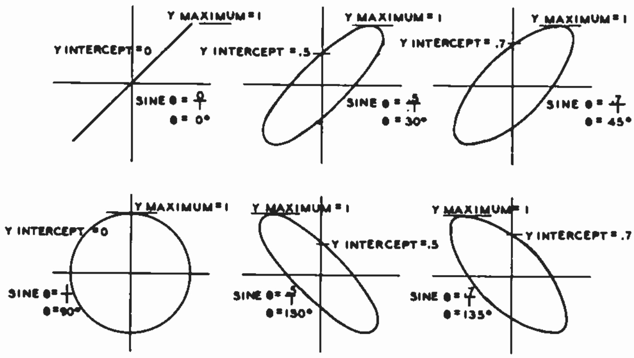


Figure 16
EXAMPLES SHOWING THE USE OF THE FORMULA FOR DETERMINATION OF PHASE DIFFERENCE

projection method. Figure 15 shows two sine waves which differ in phase being projected on to the screen of the cathode-ray tube. These signals represent a phase difference of 45°. It is extremely important: (1) that the spot has been centered on the screen of the cathode-ray tube, (2) that both the horizontal and vertical amplifiers have been adjusted to give exactly the same gain, and (3) that the calibrated scale be originally set to coincide with the displacement of the signal along the vertical axis. If the amplifiers of the oscilloscope are not used for conveying the signal to the deflection plates of the cathode-ray tube, the coarse frequency switch should be set to *horizontal input direct* and the vertical input switch to *direct* and the outputs of the two signals must be adjusted to result in exactly the same vertical deflection as horizontal deflection. Once this deflection has been set by either the oscillator output controls or the amplifier gain controls in the oscillograph, it should not be changed for the duration of the measurement.

Determination of the Phase Angle The relation commonly used in determining the phase angle between signals is:

$$\text{Sine } \theta = \frac{\text{Y intercept}}{\text{Y maximum}}$$

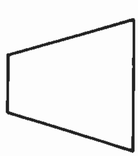


Figure 17
TRAPEZOIDAL MODULATION PATTERN

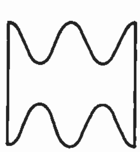


Figure 18
MODULATED CARRIER WAVE PATTERN

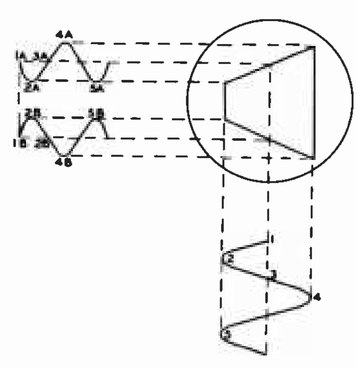


Figure 19
PROJECTION DRAWING SHOWING TRAPEZOIDAL PATTERN

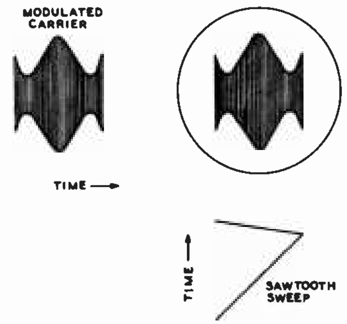


Figure 20

PROJECTION DRAWING SHOWING MODULATED CARRIER WAVE PATTERN

where θ = phase angle between signals
Y intercept = point where ellipse crosses vertical axis measured in tenths of inches. (Calibrations on the calibrated screen)
Y maximum = highest vertical point on ellipse in tenths of inches

Several examples of the use of the formula are given in figure 16. In each case the Y intercept and Y maximum are indicated together with the sine of the angle and the angle itself. For the operator to observe these various patterns with a single signal source such as the test signal, there are many types of phase shifters which can be used. Circuits can be obtained from a number of radio text books. The procedure is to connect the original signal to the horizontal channel of the oscilloscope and the signal which has passed through the phase shifter to the vertical channel of the oscilloscope, and follow the procedure set forth in this discussion to observe the various phase shift patterns.

8-4 Monitoring Transmitter Performance with the Oscilloscope

The oscilloscope may be used as an aid for the proper operation of a radiotelephone transmitter, and may be used as an indicator of the overall performance of the transmitter output signal, and as a modulation monitor.

Waveforms There are two types of patterns that can serve as indicators, the trapezoidal pattern (figure 17) and the modulated wave pattern (figure 18). The trapezoidal pattern is presented on the screen by impressing a modulated carrier wave signal on the vertical deflection plates and the signal that modulates the carrier wave signal (the modulating signal) on the horizontal deflection plates. The trapezoidal pattern can be analyzed by the method used previously in analyzing waveforms. Figure 19 shows how the signals cause the electron beam to trace out the pattern.

The modulated wave pattern is accomplished by presenting a modulated carrier wave on the vertical deflection plates and by using the time-base generator for horizontal deflection. The modulated wave pattern also can be used for analyzing waveforms. Figure 20 shows how the two signals cause the electron beam to trace out the pattern.

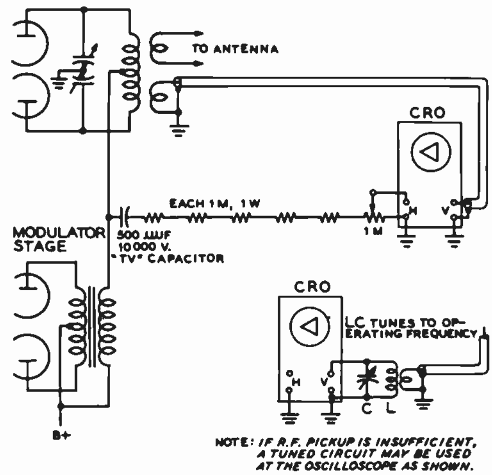
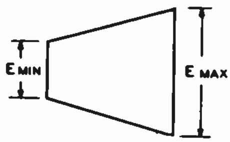
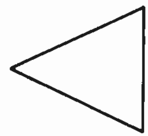


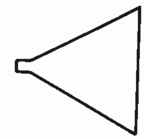
Figure 21

MONITORING CIRCUIT FOR TRAPEZOIDAL MODULATION PATTERN

The Trapezoidal Pattern The oscilloscope connections for obtaining a trapezoidal pattern are shown in figure 21. A portion of the audio output of the transmitter modulator is applied to the horizontal input of the oscilloscope. The vertical amplifier of the oscilloscope is disconnected, and a small amount of modulated r-f energy is coupled directly to the vertical deflection plates of the oscilloscope. A small pickup loop, loosely coupled to the final amplifier tank circuit and connected to the vertical de-







TRAPEZOIDAL WAVE PATTERN

Figure 22

(LESS THAN 100% MODULATION)

Figure 23

(100% MODULATION)

Figure 24

(OVER MODULATION)

flection plates by a short length of coaxial line will suffice. The amount of excitation to the plates of the oscilloscope may be adjusted to provide a pattern of convenient size. Upon modulation of the transmitter, the trapezoidal pattern will appear. By changing the degree of modulation of the carrier wave the shape of the pattern will change. Figures 22 and 23 show the trapezoidal pattern for various degrees of modulation. The percentage of modulation may be determined by the following formula:

Modulation percentage =

$$\frac{E_{max} - E_{min}}{E_{max} + E_{min}} \times 100$$

where E_{max} and E_{min} are defined as in figure 22.

An overmodulated signal is shown in figure 24.

The Modulated Wave Pattern The oscilloscope connections for obtaining a modulated wave pattern are shown in figure 25. The internal sweep circuit of the oscilloscope is applied to the horizontal plates, and the modulated r-f signal is applied to the vertical plates, as described before. If desired, the internal sweep circuit may be synchronized with the modulating signal of the transmitter by applying a small portion of the modulator output signal to the *external sync* post of the oscilloscope. The percentage of modulation may be determined in the same fashion as with a trapezoidal pattern. Figures 26, 27 and 28 show the modulated wave pattern for various degrees of modulation.

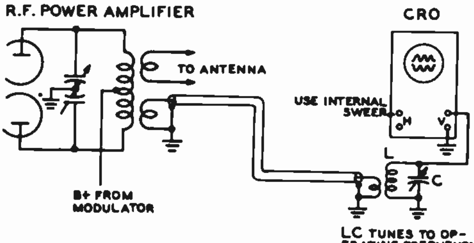


Figure 25

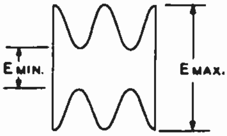
MONITORING CIRCUIT FOR MODULATED WAVE PATTERN

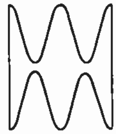
8-5 Receiver I-F Alignment with an Oscilloscope

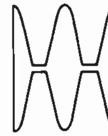
The alignment of the i-f amplifiers of a receiver consists of adjusting all the tuned circuits to resonance at the intermediate frequency and at the same time to permit passage of a predetermined number of side bands. The best indication of this adjustment is a resonance curve representing the response of the i-f circuit to its particular range of frequencies.

As a rule medium and low-priced receivers use i-f transformers whose bandwidth is about 5 kc. on each side of the fundamental frequency. The response curve of these i-f transformers is shown in figure 29. High fidelity receivers usually contain i-f transformers which have a broader bandwidth which is usually 10 kc. on each side of the fundamental. The response curve for this type transformer is shown in figure 30.

Resonance curves such as these can be displayed on the screen of an oscilloscope. For a complete understanding of the procedure it is important to know how the resonance curve is traced.







CARRIER WAVE PATTERN

Figure 26

(LESS THAN 100% MODULATION)

Figure 27

(100% MODULATION)

Figure 28

(OVER MODULATION)

The Resonance Curve on the Screen To present a resonance curve on the screen, a frequency-modulated signal source must be available. This signal source is a signal generator whose output is the fundamental i-f frequency which is frequency-modulated 5 to 10 kc. each side of the fundamental frequency. A signal generator of this type generally takes the form of an ordinary signal generator with a rotating motor driven tuned circuit capacitor, called a *wobbulator*, or its electronic equivalent, a reactance tube.

The method of presenting a resonance curve on the screen is to connect the vertical channel of the oscilloscope across the detector load of the receiver as shown in the detectors of figure 31 (between point A and ground) and the time-base generator output to the horizontal channel. In this way the d-c voltage across the detector load varies with the frequencies which are passed by the i-f system. Thus, if the time-base generator is set at the frequency of rotation of the motor driven capacitor, or the reactance tube, a pattern resembling figure 32, a double resonance curve, appears on the screen.

Figure 32 is explained by considering figure 33. In half a rotation of the motor driven capacitor the frequency increases from 445 kc. to 465 kc., more than covering the range of frequencies passed by the i-f system. Therefore, a full resonance curve is presented on the screen during this half cycle of rotation since only *half* a cycle of the voltage producing horizontal deflection has transpired. In the second half of the rotation the motor

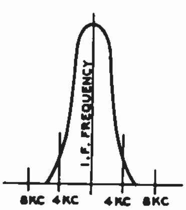


Figure 29

FREQUENCY RESPONSE CURVE OF THE I-F OF A LOW PRICED RECEIVER

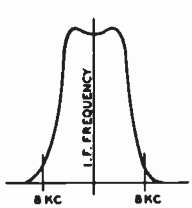
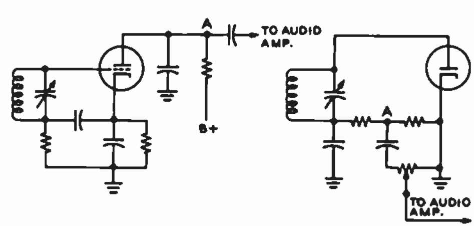


Figure 30

FREQUENCY RESPONSE OF HIGH-FIDELITY I-F SYSTEM



TRIODE DETECTOR DIODE DETECTOR

Figure 31

CONNECTION OF THE OSCILLOSCOPE ACROSS THE DETECTOR LOAD

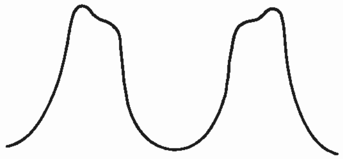


Figure 32
DOUBLE RESONANCE CURVE

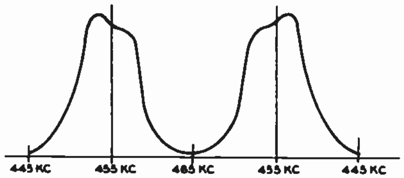


Figure 33
DOUBLE RESONANCE ACHIEVED BY COMPLETE ROTATION OF THE MOTOR DRIVEN CAPACITOR

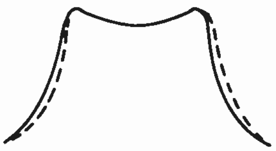


Figure 34
SUPER-POSITION OF RESONANCE CURVES

driven capacitor takes the frequency of the signal in the reverse order through the range of frequencies passed by the i-f system. In this interval the time-base generator sawtooth waveform completes its cycle, drawing the electron beam further across the screen and then returning it to the starting point. Subsequent cycles of the motor driven capacitor and the sawtooth voltage merely retrace the same pattern. Since the signal being viewed is applied through the vertical amplifier, the sweep can be synchronized internally.

Some signal generators, particularly those employing a reactance tube, provide a sweep output in the form of a sine wave which is synchronized to the frequency with which the reactance tube is swinging the fundamental frequency through its limits, usually 60 cycles per second. If such a signal is used for horizontal deflection, it is already synchronized. Since this signal is a sine wave, the response curve is observed as it sweeps the spot across the screen from left to right; and it is observed again as the sine wave sweeps the spot back again from right to left. Under these conditions the two response curves are superimposed on each other and the high frequency responses of both curves are at one end and the low frequency response of both curves is at the other end. The i-f trimmer capacitors are adjusted to produce a response curve which is symmetrical on each side of the fundamental frequency.

When using sawtooth sweep, the two response curves can also be superimposed. If the sawtooth signal is generated at exactly twice the frequency of rotation of the motor driven capacitor, the two resonance curves will be superimposed (figure 34) if the i-f transformers are properly tuned. If the two curves do not coincide the i-f trimmer capacitors should be adjusted. At the point of coincidence the tuning is correct. It should be pointed out that rarely do the two curves agree perfectly. As a result, optimum adjustment is made by making the peaks coincide. This latter procedure is the one generally used in i-f adjustment. When the two curves coincide, it is evident that the i-f system responds equally to signals higher and lower than the fundamental i-f frequency.

CHAPTER NINE

Special Vacuum Tube Circuits

A whole new concept of vacuum tube applications has been developed in recent years. No longer are vacuum tubes chained to the field of communication. This chapter is devoted to some of the more common circuits encountered in industrial and military applications of the vacuum tube.

9-1 Limiting Circuits

The term *limiting* refers to the removal or suppression by electronic means of the extremities of an electronic signal. Circuits which perform this function are referred to as *limiters* or *clippers*. Limiters are useful in wave-shaping circuits where it is desirable to square off the extremities of the applied signal. A sine wave may be applied to a limiter circuit to produce a rectangular wave. A peaked wave may be applied to a limiter circuit to eliminate either the positive or negative peaks from the output. Limiter circuits are employed in FM receivers where it is necessary to limit the amplitude of the signal applied to the detector. Limiters may be used to reduce automobile ignition noise in short-wave receivers, or to maintain a high average level of modulation in a transmitter. They may also be used as protective devices to limit input signals to special circuits.

Diode Limiters The characteristics of a diode tube are such that the tube conducts only when the plate is at a positive potential with respect to the cathode. A positive potential may be placed on the cathode, but the tube will not conduct until the voltage on the plate rises above an equally positive value. As the plate becomes more positive with respect to the cathode, the diode conducts and passes that portion of the wave that is more positive than the cathode voltage. Diodes may be used as either series or parallel limiters, as shown in figure 1. A diode may be so biased that only a certain portion of the positive or negative cycle is removed.

Audio Peak Limiting An audio peak clipper consisting of two diode limiters may be used to limit the amplitude of an audio signal to a predetermined value to provide a high average level of modulation without danger of overmodulation. An effective limiter for this service is the *series-diode gate clipper*. A circuit of this clipper is shown in figure 2. The audio signal to be clipped is coupled to the clipper through C_1. R_1 and R_2 are the clipper input and output load resistors. The clipper plates are tied together and are connected to the clipping level control, R_4, through the series resistor, R_3. R_4 acts as a voltage divider between the high voltage supply and ground. The exact point at which clip-

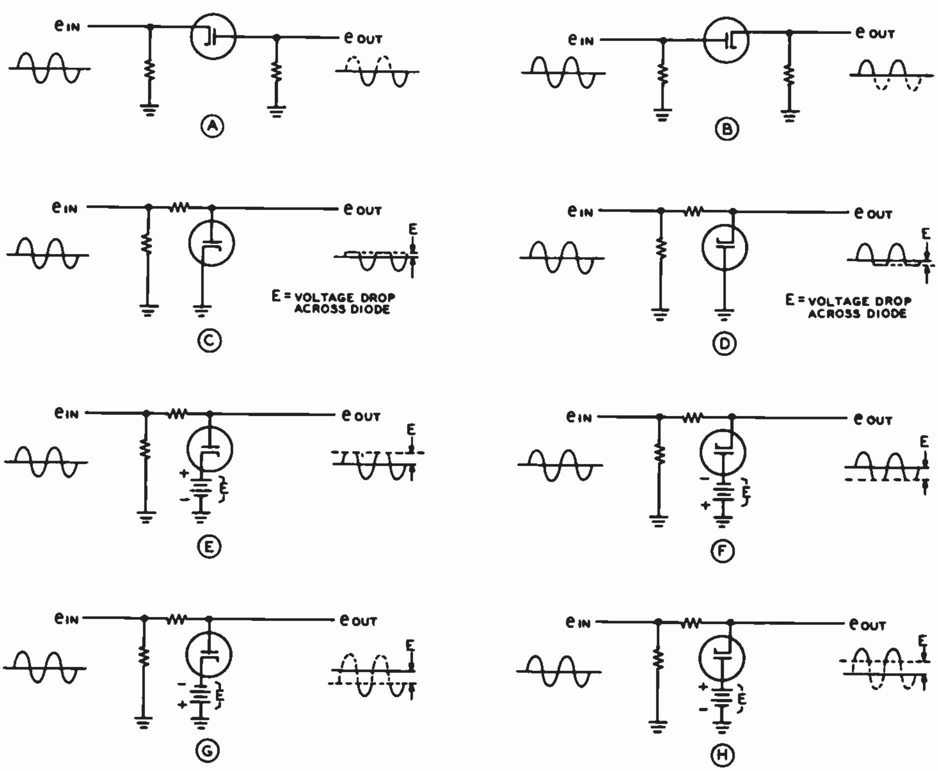


Figure 1

VARIOUS DIODE LIMITING CIRCUITS

Series diodes limiting positive and negative peaks are shown in A and B. Parallel diodes limiting positive and negative peaks are shown in C and D. Parallel diodes limiting above and below ground are shown in E and F. Parallel diode limiters which pass negative and positive peaks are shown in G and H.

ping will occur is set by R_4, which controls the positive potential applied to the diode plates.

Under static conditions, a d-c voltage is obtained from R_4 and applied through R_3 to both plates of the 6AL5 tube. Current flows through R_4, R_3, and divides through the two diode sections of the 6AL5 and the two load resistors, R_1 and R_2. All parts of the clipper circuit are maintained at a positive potential above ground. The voltage drop between the plate and cathode of each diode is very small compared to the drop across the 300,000-ohm resistor (R_3) in series with the diode plates. The plate and cathode of each diode are therefore maintained at approximately equal potentials as long as there is plate current flow. Clipping does not occur until the peak audio input voltage reaches a value greater than the static voltages at the plates of the diode.

Assume that R_4 has been set to a point that will give 4 volts at the plates of the 6AL5. When the peak audio input voltage is less than 4 volts, both halves of the tube conduct at all times. As long as the tube conducts, its resistance is very low compared with the plate resistor R_3. Whenever a voltage change occurs across input resistor R_1, the voltage at all of the tube elements increases or decreases by the same amount as the input voltage change, and the voltage drop across R_3 changes by an equal amount. As long as the peak input voltage is less than 4 volts, the 6AL5 acts merely as a conductor, and the output cathode is permitted to follow all voltage changes at the input cathode.

If, under static conditions, 4 volts appear at the diode plates, then twice this voltage (8 volts) will appear if one of the diode circuits

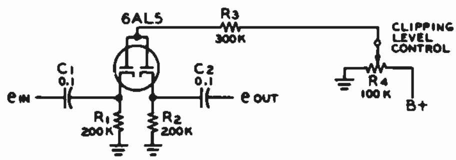


Figure 2
THE SERIES-DIODE GATE CLIPPER FOR AUDIO PEAK LIMITING

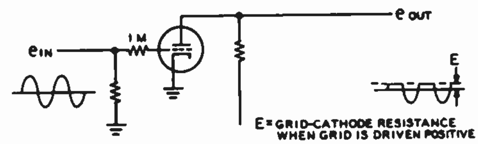


Figure 3
GRID LIMITING CIRCUIT

is opened, removing its d-c load from the circuit. As long as only one of the diodes continues to conduct, the voltage at the diode plates cannot rise above twice the voltage selected by R_4. In this example, the voltage cannot rise above 8 volts. Now, if the input audio voltage applied through C_1 is increased to any peak value between zero and plus 4 volts, the first cathode of the 6AL5 will increase in voltage by the same amount to the proper value between 4 and 8 volts. The other tube elements will assume the same potential as the first cathode. However, the 6AL5 plates cannot increase more than 4 volts above their original 4-volt static level. When the input voltage to the first cathode of the 6AL5 increases to more than plus 4 volts, the cathode potential increases to more than 8 volts. Since the plate circuit potential remains at 8 volts, the first diode section ceases to conduct until the input voltage across R_1 drops below 4 volts.

When the input voltage swings in a negative direction, it will subtract from the 4-volt drop across R_1 and decrease the voltage on the input cathode by an amount equal to the input voltage. The plates and the output cathode will follow the voltage level at the input cathode as long as the input voltage does not swing below minus 4 volts. If the input voltage does not change more than 4 volts in a negative direction, the plates of the 6AL5 will also become negative. The potential at the output cathode will follow the input cathode voltage and decrease from its normal value of 4 volts until it reaches zero potential. As the input cathode voltage decreases to less than zero, the plates will follow. However, the output cathode, grounded through R_2, will stop at zero potential as the plate becomes negative. Conduction through the second diode is impossible under these conditions. The output cathode remains at zero potential until the voltage at the input cathode swings back to zero.

The voltage developed across output resistor R_2 follows the input voltage variations as long as the input voltage does not swing to a peak value greater than the static voltage at the diode plates, determined by R_4. Effective clipping may thus be obtained at any desired level.

The square-topped audio waves generated by this clipper are high in harmonic content, but these higher order harmonics may be greatly reduced by a low-level speech filter.

Grid Limiters A triode grid limiter is shown in figure 3. On positive peaks of the input signal, the triode grid attempts to swing positive, and the grid-cathode resistance drops to a value on the order of 1000 ohms or so. The voltage drop across R (usually of the order of 1 megohm) is large compared to the grid-cathode drop, and the resulting limiting action removes the top part of the positive input wave.

9-2 Clamping Circuits

A circuit which holds either amplitude extreme of a waveform to a given reference level

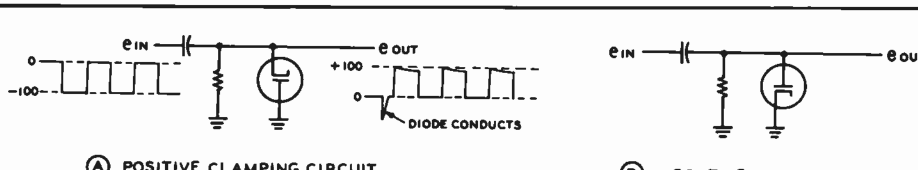


Figure 4
SIMPLE POSITIVE AND NEGATIVE CLAMPING CIRCUITS

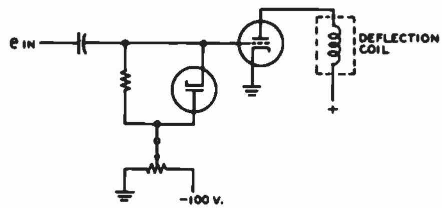


Figure 5
NEGATIVE CLAMPING CIRCUIT EMPLOYED IN ELECTROMAGNETIC SWEEP SYSTEM

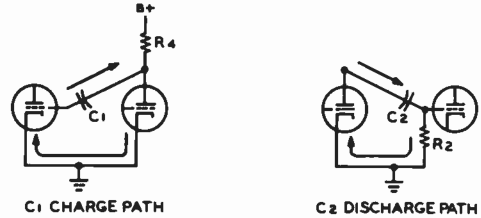


Figure 7
THE CHARGE AND DISCHARGE PATHS IN FREE-RUNNING MULTIVIBRATOR OF FIGURE 6

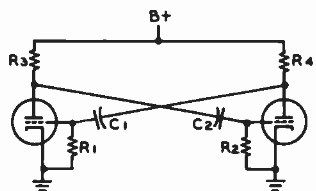


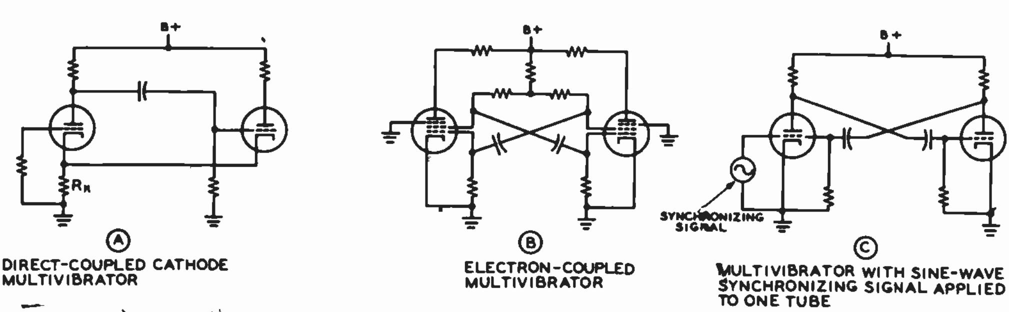
Figure 6
BASIC MULTIVIBRATOR CIRCUIT

of potential is called a *clamping circuit* or a *d-c restorer*. Clamping circuits are used after RC coupling circuits where the waveform swing is required to be either above or below the reference voltage, instead of alternating on both sides of it (figure 4). Clamping circuits are usually encountered in oscilloscope sweep circuits. If the sweep voltage does not always start from the same reference point, the trace on the screen does not begin at the same point on the screen each time the sweep is repeated and therefore is "jittery." If a clamping circuit is placed between the sweep amplifier and the deflection element, the start of the sweep can be regulated by adjusting the d-c voltage applied to the clamping tube (figure 5).

9-3 Multivibrators

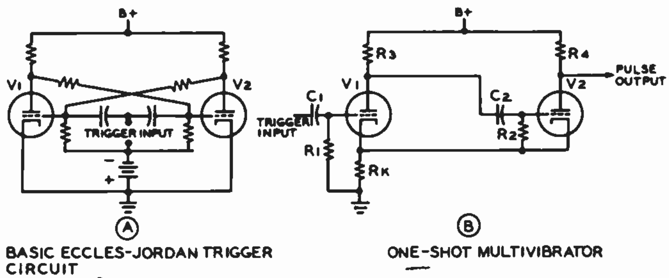
The multivibrator, or relaxation oscillator, is used for the generation of nonsinusoidal waveforms. The output is rich in harmonics, but the inherent frequency stability is poor. The multivibrator may be stabilized by the introduction of synchronizing voltages of harmonic or subharmonic frequency.

In its simplest form, the multivibrator is a simple two-stage resistance-capacitance coupled amplifier with the output of the second stage coupled through a capacitor to the grid of the first tube, as shown in figure 6. Since the output of the second stage is of the proper polarity to reinforce the input signal applied to the first tube, oscillations can readily take place, started by thermal agitation noise and



Fred Dunning

Figure 8
VARIOUS FORMS OF MULTIVIBRATOR CIRCUITS



(A) BASIC ECCLES-JORDAN TRIGGER CIRCUIT

flip-flop

(B) ONE-SHOT MULTIVIBRATOR

Figure 9

ECCLES-JORDAN MULTIVIBRATOR CIRCUITS

miscellaneous tube noise. Oscillation is maintained by the process of building up and discharging the store of energy in the grid coupling capacitors of the two tubes. The charging and discharging paths are shown in figure 7. Various forms of multivibrators are shown in figure 8.

The output of a multivibrator may be used as a source of square waves, as an electronic switch, or as a means of obtaining frequency division. Submultiple frequencies as low as one-tenth of the injected synchronizing frequency may easily be obtained.

The Eccles-Jordan Circuit The *Eccles-Jordan* trigger circuit is shown in figure 9A. This is not a true multivibrator, but rather a circuit that possesses two conditions of stable equilibrium. One condition is when V_1 is conducting and V_2 is cutoff; the other when V_2 is conducting and V_1 is cutoff. The circuit remains in one or the other of these two stable conditions with no change in operating potentials until some external action occurs which causes the nonconducting tube to conduct. The tubes then reverse their functions and remain in the new condition as long as no plate current flows in the cutoff tube. This type of circuit is known as a *flip-flop* circuit.

Figure 9B illustrates a modified Eccles-Jordan circuit which accomplishes a complete cycle when triggered with a positive pulse. Such a circuit is called a *one-shot* multivibrator. For initial action, V_1 is cutoff and V_2 is conducting. A large positive pulse applied to the grid of V_1 causes this tube to conduct, and the voltage at its plate decreases by virtue of the IR drop through R_3. Capacitor C_2 is charged rapidly by this abrupt change in V_1 plate voltage, and V_2 becomes cutoff while V_1 conducts. This condition exists until C_2 discharges, allowing V_2 to conduct, raising the cathode bias of V_1 until it is once again cutoff.

A direct, cathode-coupled multivibrator is shown in figure 8A. R_K is a common cathode resistor for the two tubes, and coupling takes place across this resistor. It is impossible for a tube in this circuit to completely cutoff the other tube, and a circuit of this type is called a *free-running* multivibrator in which the condition of one tube temporarily cuts off the other.

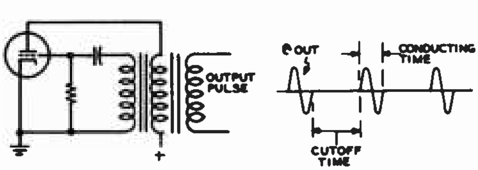


Figure 10

SINGLE-SWING BLOCKING OSCILLATOR

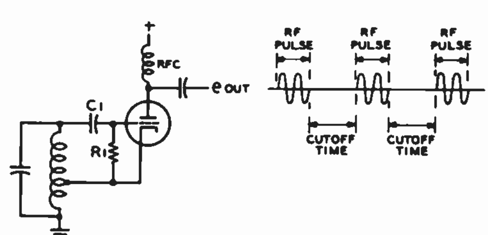
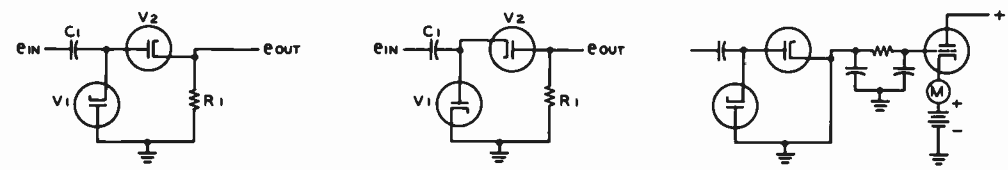


Figure 11

HARTLEY OSCILLATOR USED AS BLOCKING OSCILLATOR BY PROPER CHOICE OF R_1-C_1



Ⓐ POSITIVE COUNTING CIRCUIT

Ⓑ NEGATIVE COUNTING CIRCUIT

Ⓒ POSITIVE COUNTING CIRCUIT WITH METER INDICATION

Figure 12

POSITIVE AND NEGATIVE COUNTING CIRCUITS

9-4 The Blocking Oscillator

A blocking oscillator is any oscillator which cuts itself off after one or more cycles caused by the accumulation of a negative charge on the grid capacitor. This negative charge may gradually be drained off through the grid resistor of the tube, allowing the circuit to oscillate once again. The process is repeated and the tube becomes an intermittent oscillator. The rate of such an occurance is determined by the R-C time constant of the grid circuit. A *single-swing blocking oscillator* is shown in figure 10, wherein the tube is cutoff before the completion of one cycle. The tube produces single pulses of energy, the time between the pulses being regulated by the discharge time of the grid R-C network. The *self-pulsing* blocking oscillator is shown in figure 11, and is used to produce pulses of r-f energy, the number of pulses being determined by the timing network in the grid circuit of the oscillator. The rate at which these pulses occur is known as the *pulse-repetition frequency,* or *p.r.f.*

9-5 Counting Circuits

A *counting circuit,* or *frequency divider* is one which receives uniform pulses, representing units to be counted, and produces a voltage that is proportional to the frequency of the pulses. A counting circuit may be used in conjunction with a blocking oscillator to produce a trigger pulse which is a submultiple of of the frequency of the applied pulse. Either positive or negative pulses may be counted. A positive counting circuit is shown in figure 12A, and a negative counting circuit is shown in figure 12B. The positive counter allows a certain amount of current to flow through R_1 each time a pulse is applied to C_1.

The positive pulse charges C_1, and makes the plate of V_2 positive with respect to its cathode. V_2 conducts until the exciting pulse passes. C_1 is then discharged by V_1, and the circuit is ready to accept another pulse. The average current flowing through R_1 increases as the pulse-repetition frequency increases, and decreases as the p.r.f. decreases.

By reversing the diode connections, as shown in figure 12B, the circuit is made to respond to negative pulses. In this circuit, an increase in the p.r.f. causes a decrease in the average current flowing through R_1, which is opposite to the effect in the positive counter.

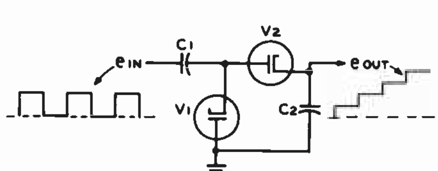


Figure 13

STEP-BY-STEP COUNTING CIRCUIT

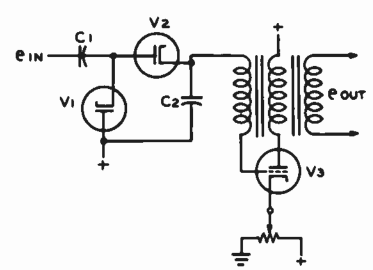


Figure 14

The step-by-step counter used to trigger a blocking oscillator. The blocking oscillator serves as a frequency divider.

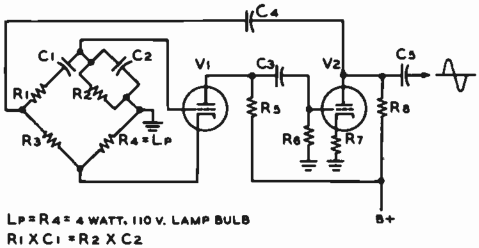


Figure 15
THE WIEN-BRIDGE AUDIO OSCILLATOR

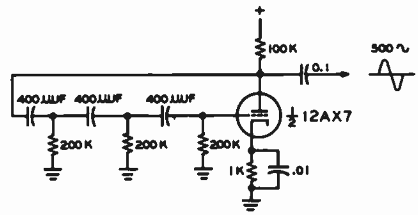


Figure 16
THE PHASE-SHIFT OSCILLATOR

A *step-counter* is similar to the circuits discussed, except that a capacitor which is large compared to C_1 replaces the diode load resistor. The charge of this condenser is increased during the time of each pulse, producing a step voltage across the output (figure 13). A blocking oscillator may be connected to a step-counter, as shown in figure 14. The oscillator is triggered into operation when the voltage across C_2 reaches a point sufficiently positive to raise the grid of V_3 above cutoff. Circuit parameters may be chosen so that a count division up to 1/20 may be obtained with reliability.

9-6 Resistance-Capacity Oscillators

In an R-C oscillator, the frequency is determined by a resistance capacity network that provides regenerative coupling between the output and input of a feedback amplifier. No use is made of a tank circuit consisting of inductance and capacitance to control the frequency of oscillation.

The *Wien-Bridge* oscillator employs a *Wien network* in the R-C feedback circuit and is shown in figure 15. Tube V_1 is the oscillator tube, and tube V_2 is an amplifier and phase-inverter tube. Since the feedback voltage through C_4 produced by V_2 is in phase with the input circuit of V_1 at all frequencies, oscillation is maintained by voltages of any frequency that exist in the circuit. The bridge circuit is used, then, to eliminate feedback voltages of all frequencies except the single frequency desired at the output of the oscillator. The bridge allows a voltage of only one frequency to be effective in the circuit because of the degeneration and phase shift provided by this circuit. The frequency at which oscillation occurs is:

$$f = \frac{1}{2\pi R_1 C_1}, \text{ when } R_1 \times C_1 = R_2 \times C_2$$

A lamp L_p is used as the cathode resistor of V_1 as a thermal stabilizer of the oscillator amplitude. The variation of the resistance with respect to current of the lamp bulb holds the oscillator output voltage at a nearly constant amplitude.

The *phase-shift* oscillator shown in figure 16 is a single tube oscillator using a three section phase shift network. Each section of the network produces a phase shift in proportion to the frequency of the signal that passes through it. For oscillations to be produced, the signal from the plate of the tube must be shifted 180°. Three successive phase shifts of 60° accomplish this, and the frequency of oscillation is determined by this phase shift. A high-mu triode or a pentode must be used in this circuit. In order to increase the frequency of oscillation, either the resistance or the capacitance must be decreased.

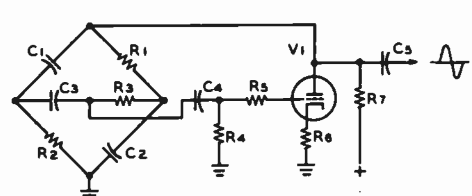


Figure 17
THE BRIDGE-TYPE PHASE-SHIFT OSCILLATOR

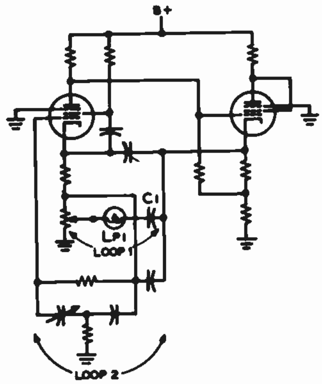


Figure 18
THE NBS BRIDGE-T OSCILLATOR CIRCUIT

A *bridge-type phase shift oscillator* is shown in figure 17. The bridge is so proportioned that at only one frequency is the phase shift through the bridge 180°. Voltages of other frequencies are fed back to the grid of the tube out of phase with the existing grid signal, and are cancelled by being amplified out of phase.

The *NBS Bridge-T* oscillator developed by the National Bureau of Standards consists of a two stage amplifier having two feedback loops, as shown in figure 18. Loop 1 consists of a regenerative cathode-to-cathode loop, consisting of L_{p1} and C_1. The bulb regulates the positive feedback, and tends to stabilize the output of the oscillator, much as in the manner of the Wien circuit. Loop 2 consists of a grid-cathode degenerative circuit, containing the bridge-T. Oscillation will occur at the null frequency of the bridge, at which frequency the bridge allows minimum degeneration in loop 2.

CHAPTER TEN

Radio Receiver Fundamentals

A conventional reproducing device such as a loudspeaker or a pair of earphones is incapable of receiving directly the intelligence carried by the *carrier* wave of a radio transmitting station. It is necessary that an additional device, called a *radio receiver,* be placed between the receiving antenna and the loudspeaker or headphones.

Radio receivers vary widely in their complexity and basic design, depending upon the intended application and upon economic factors. A simple radio receiver for reception of radiotelephone signals can consist of an earphone, a silicon or germanium crystal as a carrier rectifier or *demodulator,* and a length of wire as an antenna. However, such a receiver is highly insensitive, and offers no significant discrimination between two signals in the same portion of the spectrum.

On the other hand, a dual-diversity receiver designed for single-sideband reception and employing double or triple detection might occupy several relay racks and would cost many thousands of dollars. However, conventional communications receivers are intermediate in complexity and performance between the two extremes. This chapter is devoted to the principles underlying the operation of such conventional communications receivers.

10-1 Detection or Demodulation

A detector or demodulator is a device for removing the modulation (demodulating) or detecting the intelligence carried by an incoming radio wave.

Radiotelephony Demodulation Figure 1 illustrates an elementary form of radiotelephony receiver employing a diode detector. Energy from a passing radio wave will induce a voltage in the antenna and cause a radio-frequency current to flow from antenna to ground through coil L_1. The alternating magnetic field set up around L_1 links with the turns of L_2 and causes an r-f current to flow through the parallel-tuned circuit, L_2-C_1. When variable capacitor C_1 is adjusted so that the tuned circuit is resonant at the frequency of the applied signal, the r-f voltage is maximum. This r-f voltage is applied to the diode detector where it is rectified into a varying direct current and passed through the earphones. The variations in this current correspond to the voice modulation placed on the signal at the transmitter. As the earphone diaphragms vibrate back and forth in accord-

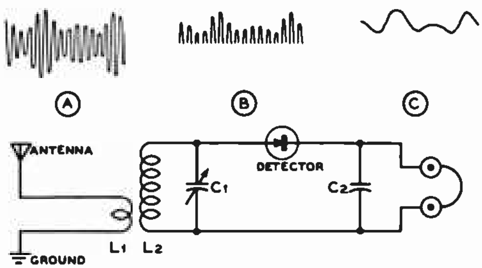


Figure 1
ELEMENTARY FORM OF RECEIVER
This is the basis of the "crystal set" type of receiver, although a vacuum diode may be used in place of the crystal diode. The tank circuit L_2-C_1 is tuned to the frequency it is desired to receive. The by-pass capacitor across the phones should have a low reactance to the carrier frequency being received, but a high reactance to the modulation on the received signal.

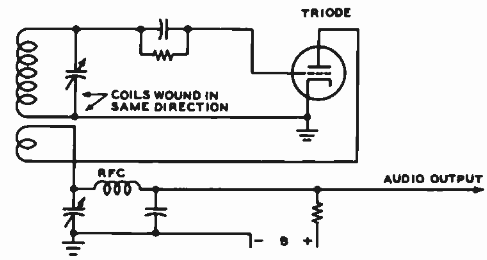
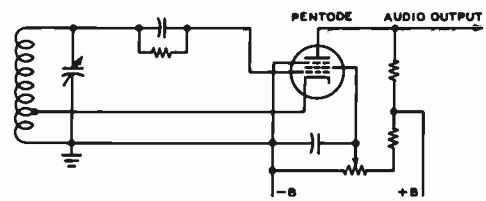


PLATE-TICKLER REGENERATION WITH "THROTTLE" CONDENSER REGENERATION CONTROL.



CATHODE-TAP REGENERATION WITH SCREEN VOLTAGE REGENERATION CONTROL.

Figure 2
REGENERATIVE DETECTOR CIRCUITS
Regenerative detectors are seldom used at the present time due to their poor selectivity. However, they do illustrate the simplest type of receiver which may be used either for radiophone or radiotelegraph reception.

ance with the pulsating current they audibly reproduce the modulation which was placed upon the carrier wave.

The operation of the detector circuit is shown graphically above the detector circuit in figure 1. The modulated carrier is shown at A, as it is applied to the antenna. B represents the same carrier, increased in amplitude, as it appears across the tuned circuit. In C the varying d-c output from the detector is seen.

Radiotelegraphy Reception Since a c-w telegraphy signal consists of an unmodulated carrier which is interrupted to form dots and dashes, it is apparent that such a signal would not be made audible by detection alone. While the keying is a form of modulation, it is composed of such low frequency components that the keying envelope itself is below the audible range for hand keying speeds. Some means must be provided whereby an audible tone is heard while the unmodulated carrier is being received, the tone stopping immediately when the carrier is interrupted.

The most simple means of accomplishing this is to feed a locally generated carrier of a slightly different frequency into the same detector, so that the incoming signal will *mix* with it to form an audible *beat note*. The difference frequency, or *heterodyne* as the beat note is known, will of course stop and start in accordance with the incoming c-w radiotelegraph signal, because the audible heterodyne can exist only when both the incoming and the locally generated carriers are present.

The Autodyne Detector The local signal which is used to beat with the desired c-w signal in the detector may be supplied by a separate low-power oscillator in the receiver itself, or the detector may be made to self-oscillate, and thus serve the dual purpose of detector and oscillator. A detector which self-oscillates to provide a beat note is known as an *autodyne* detector, and the process of obtaining feedback between the detector plate and grid is called *regeneration.*

An autodyne detector is most sensitive when it is barely oscillating, and for this reason a regeneration control is always included in the circuit to adjust the feedback to the proper amount. The regeneration control may be either a variable capacitor or a variable resistor, as shown in figure 2.

With the detector regenerative but not oscillating, it is also quite sensitive. When the circuit is adjusted to operate in this manner, modulated signals may be received with considerably greater strength than with a non-regenerative detector.

10-2 Superregenerative Receivers

At ultra-high frequencies, when it is desired to keep weight and cost at a minimum, a special form of the regenerative receiver known as the *superregenerator* is often used for radiotelephony reception. The superregenerator is essentially a regenerative receiver with a means provided to throw the detector rapidly in and out of oscillation. The frequency at which the detector is made to go in and out of oscillation varies with the frequency to be received, but is usually between 20,000 and 500,000 times a second. This superregenerative action considerably increases the sensitivity of the oscillating detector so that the usual "background hiss" is greatly amplified when no signal is being received. This hiss diminishes in proportion to the strength of the received signal, loud signals eliminating the hiss entirely.

Quench Methods There are two systems in common use for causing the detector to break in and out of oscillation rapidly. In one, a separate *interruption-frequency* oscillator is arranged so as to vary the voltage rapidly on one of the detector tube elements (usually the plate, sometimes the screen) at the high rate necessary. The interruption-frequency oscillator commonly uses a conventional tickler-feedback circuit with coils appropriate for its operating frequency.

The second, and simplest, type of superregenerative detector circuit is arranged so as to produce its own interruption frequency oscillation, without the aid of a separate tube. The detector tube damps (or "quenches") itself out of signal-frequency oscillation at a high rate by virtue of the use of a high value of grid leak and proper size plate-blocking and grid capacitors, in conjunction with an excess of feedback. In this type of "self-quenched" detector, the grid leak is quite often returned to the positive side of the power supply (through the coil) rather than to the cathode. A representative self-quenched superregenerative detector circuit is shown in figure 3.

Except where it is impossible to secure sufficient regenerative feedback to permit superregeneration, the self-quenching circuit is to be preferred; it is simpler, is self-adjusting as regards quenching amplitude, and can have good quenching wave form. To obtain as good results with a separately quenched superregenerator, very careful design is required. However, separately quenched circuits are useful when it is possible to make a certain tube oscillate on a very high frequency but it is impossible to obtain enough regeneration for self-quenching action.

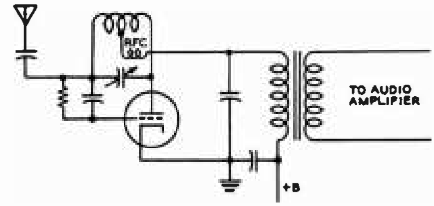


Figure 3
SUPERREGENERATIVE DETECTOR CIRCUIT
A self-quenched superregenerative detector such as illustrated above is capable of giving good sensitivity in the v-h-f range. However, the circuit has the disadvantage that its selectivity is relatively poor. Also, such a circuit should be preceded by an r-f stage to suppress the radiation of a signal by the oscillating detector.

The optimum quenching frequency is a function of the signal frequency. As the operating frequency goes up, so does the optimum quenching frequency. When the quench frequency is too low, maximum sensitivity is not obtained. When it is too high, both sensitivity and selectivity suffer. In fact, the optimum quench frequency for an operating frequency below 15 Mc. is in the audible range. This makes the superregenerator impracticable for use on the lower frequencies.

The high background noise or hiss which is heard on a properly designed superregenerator when no signal is being received is not the quench frequency component; it is tube and tuned circuit fluctuation noise, indicating that the receiver is extremely sensitive.

A moderately strong signal will cause the background noise to disappear completely, because the superregenerator has an inherent and instantaneous automatic volume control characteristic. This same a-v-c characteristic makes the receiver comparatively insensitive to impulse noise such as ignition pulses—a highly desirable feature. This characteristic also results in appreciable distortion of a received radiotelephone signal, but not enough to affect the intelligibility.

The selectivity of a superregenerator is rather poor as compared to a superheterodyne, but is surprisingly good for so simple a receiver when figured on a percentage basis rather than absolute kc. bandwidth.

FM Reception A superregenerative receiver will receive frequency modulated signals with results comparing favorably with amplitude modulation if the frequency swing of the FM transmitter is sufficiently high. For such reception, the receiver is detuned slightly to either side of resonance.

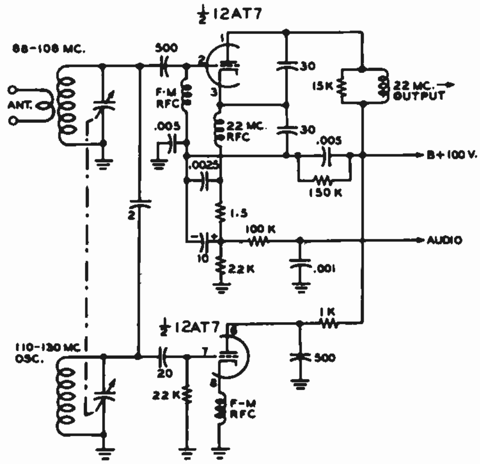


Figure 4
THE FREMODYNE SUPERREGENERATIVE SUPERHETERODYNE DETECTOR FOR FREQUENCY MODULATED SIGNALS

Superregenerative receivers radiate a strong, broad, and rough signal. For this reason, it is necessary in most applications to employ a radio frequency amplifier stage ahead of the detector, with thorough shielding throughout the receiver.

The Fremodyne Detector The Hazeltine-Fremodyne superregenerative circuit is expressly designed for reception of FM signals. This versatile circuit combines the action of the superregenerative receiver with the superhetrodyne, converting FM signals directly into audio signals in one double triode tube (figure 4). One section of the triode serves as a superregenerative mixer, producing an i-f of 22 Mc., an i-f amplifier, and a FM detector. The detector action is accomplished by *slope detection* tuning on the side of the i-f selectivity curve.

This circuit greatly reduces the radiated signal, characteristic of the superregenerative detector, yet provides many of the desirable features of the superregenerator. The passband of the Fremodyne detector is about 400 kc.

10-3 Superheterodyne Receivers

Because of its superiority and nearly universal use in all fields of radio reception, the

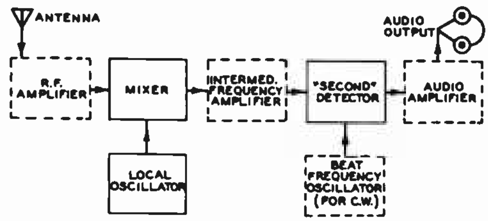


Figure 5
ESSENTIAL UNITS OF A SUPERHETERODYNE RECEIVER

The basic portions of the receiver are shown in solid blocks. Practicable receivers employ the dotted blocks and also usually include such additional circuits as a noise limiter, an a-v-c circuit, and a crystal filter in the i-f amplifier.

theory of operation of the superheterodyne should be familiar to every radio student and experimenter. The following discussion concerns superheterodynes for amplitude-modulation reception. It is, however, applicable in part to receivers for frequency modulation.

Principle of Operation In the superheterodyne, the incoming signal is applied to a *mixer* consisting of a non-linear impedance such as a vacuum tube or a diode. The signal is mixed with a steady signal generated locally in an oscillator stage, with the result that a signal bearing all the modulation applied to the original signal *but of a frequency equal to the difference between the local oscillator and incoming signal frequencies* appears in the mixer output circuit. The output from the mixer stage is fed into a fixed-tuned *intermediate-frequency amplifier,* where it is amplified and detected in the usual manner, and passed on to the audio amplifier. Figure 5 shows a block diagram of the fundamental superheterodyne arrangement. The basic components are shown in heavy lines, the simplest superheterodyne consisting simply of these three units. However, a good communications receiver will comprise all of the elements shown, both heavy and dotted blocks.

Superheterodyne Advantages The advantages of superheterodyne reception are directly attributable to the use of the fixed-tuned *intermediate-frequency* (i-f) *amplifier.* Since all signals are converted to the intermediate frequency, this section of the receiver may be designed for optimum selectivity and high amplification. High amplification is easily obtained in the intermediate-frequency amplifier, since it operates at a

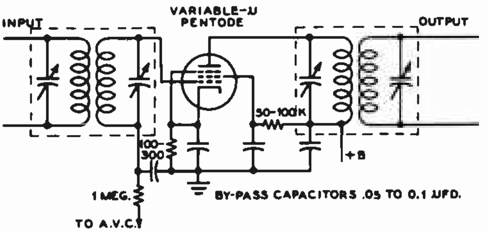


Figure 6
TYPICAL I-F AMPLIFIER STAGE

relatively low frequency, where conventional pentode-type tubes give adequate voltage gain. A typical i-f amplifier is shown in figure 6.

From the diagram it may be seen that both the grid and plate circuits are tuned. The tuned circuits used for coupling between i-f stages are known as *i-f transformers*. These will be more fully discussed later in this chapter.

Choice of Intermediate Frequency The choice of a frequency for the i-f amplifier involves several considerations. One of these considerations concerns selectivity; the lower the intermediate frequency the greater the obtainable selectivity. On the other hand, a rather high intermediate frequency is desirable from the standpoint of *image* elimination, and also for the reception of signals from television and FM transmitters and modulated self-controlled oscillators, all of which occupy a rather wide band of frequencies, making a broad selectivity characteristic desirable. Images are a pecularity common to all superheterodyne receivers, and for this reason they are given a detailed discussion later in this chapter.

While intermediate frequencies as low as 50 kc. are used where extreme selectivity is a requirement, and frequencies of 60 Mc. and above are used in some specialized forms of receivers, most present-day communications superheterodynes use intermediate frequencies around either 455 kc. or 1600 kc.

Home-type broadcast receivers almost always use an i-f in the vicinity of 455 kc., while auto receivers usually use a frequency of about 262 kc. The standard frequency for the i-f channel of FM receivers is 10.7 Mc. Television receivers use an i-f which covers the band between about 21.5 and 27 Mc., although a new band between 41 and 46 Mc. is coming into more common usage.

Arithmetical Selectivity Aside from allowing the use of fixed-tuned band-pass amplifier stages, the superheterodyne has an overwhelming advantage over the tuned radio frequency (t-r-f) type of receiver because of what is commonly known as *arithmetical selectivity*.

This can best be illustrated by considering two receivers, one of the t-r-f type and one of the superheterodyne type, both attempting to receive a desired signal at 10,000 kc. and eliminate a strong interfering signal at 10,010 kc. In the t-r-f receiver, separating these two signals in the tuning circuits is practically impossible, since they differ in frequency by only 0.1 per cent. However, in a superheterodyne with an intermediate frequency of, for example, 1000 kc., the desired signal will be converted to a frequency of 1000 kc. and the interfering signal will be converted to a frequency of 1010 kc., both signals appearing at the input of the i-f amplifier. In this case, the two signals may be separated much more readily, since they differ by 1 per cent, or 10 times as much as in the first case.

The Converter Stage The converter stage, or *mixer*, of a superheterodyne receiver can be either one of two types: (1) it may use a single envelope *converter* tube, such as a 6K8, 6SA7, or 6BE6, or (2) it may use two tubes, or two sets of elements in the same envelope, in an oscillator-mixer arrangement. Figure 7 shows a group of circuits of both types to illustrate present practice with regard to types of converter stages.

Converter tube combinations such as shown in figures 7A and 7B are relatively simple and inexpensive, and they do an adequate job for most applications. With a converter tube such as the 6SB7-Y or the 6BA7 quite satisfactory performance may be obtained for the reception of relatively strong signals (as for example FM broadcast reception) up to frequencies in excess of 100 Mc. However, the equivalent input noise resistance of such tubes is of the order of 200,000 ohms, which is a rather high value indeed. So such tubes are *not* suited for operation without an r-f stage in the high-frequency range if weak-signal reception is desired.

The 6L7 mixer circuit shown in figure 7C, and the 6BA7 circuit of figure 7D, also are characterized by an equivalent input noise resistance of several hundred thousand ohms, so that these also must be preceded by one or more r-f stages with a fairly high gain per stage if a low noise factor is desired of the complete receiver.

However, the circuit arrangements shown at figures 7F and 6F *are* capable of low-noise operation within themselves, so that these circuits may be fed directly from the antenna without an r-f stage and still provide a good noise factor to the complete receiver. Note

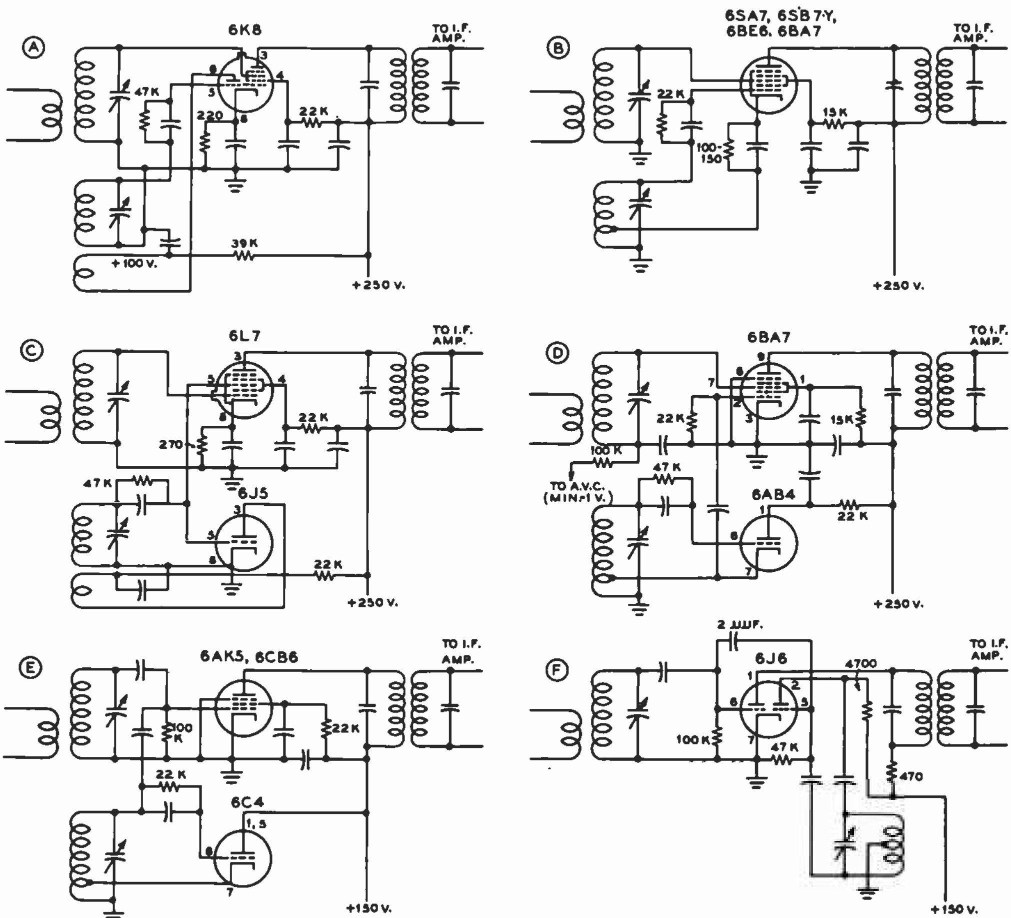


Figure 7

TYPICAL FREQUENCY-CONVERTER (MIXER) STAGES

The relative advantages of the different circuits are discussed in the text

that both these circuits use *control-grid injection* of both the incoming signal and the local-oscillator voltage. Hence, paradoxically, circuits such as these should be preceded by an r-f stage if local-oscillator radiation is to be held to any reasonable value of field intensity.

Diode Mixers As the frequency of operation of a superheterodyne receiver is increased above a few hundred megacycles the signal-to-noise ratio appearing in the plate circuit of the mixer tube when triodes or pentodes are employed drops to a prohibitively low value. At frequencies above the upper-frequency limit for conventional mixer stages, mixers of the diode type are most commonly employed. The diode may be either a vacuum-tube heater diode of a special u-h-f design such as the 9005, or it may be a crystal diode of the general type of the 1N21 through 1N28 series.

10-4 Mixer Noise and Images

The effects of *mixer noise* and *images* are troubles common to all superheterodynes. Since both these effects can largely be obviated by the same remedy, they will be considered together.

Mixer Noise Mixer noise of the shot-effect type, which is evidenced by a hiss in the audio output of the receiver, is caused by small irregularities in the plate current in the mixer stage and will mask weak signals. Noise of an identical nature is generated in an amplifier stage, but due to the fact that the conductance in the mixer stage is considerably lower than in an amplifier stage using the same tube, the proportion of inherent noise present in a mixer usually is considerably greater than in an amplifier stage using a comparable tube.

Although this noise cannot be eliminated, its effects can be greatly minimized by placing sufficient signal-frequency amplification having a high signal-to-noise ratio ahead of the mixer. This remedy causes the signal output from the mixer to be large in proportion to the noise generated in the mixer stage. Increasing the gain *after* the mixer will be of no advantage in eliminating mixer noise difficulties; greater selectivity after the mixer will help to a certain extent, but cannot be carried too far, since this type of selectivity decreases the i-f band-pass and if carried too far will not pass the sidebands that are an essential part of a voice-modulated signal.

Triode Mixers A triode having a high transconductance is the *quietest* mixer tube, exhibiting somewhat less gain but a better signal-to-noise ratio than a comparable multi-grid mixer tube. However, below 30 Mc. it is possible to construct a receiver that will get down to the atmospheric noise level without resorting to a triode mixer. The additional difficulties experienced in avoiding *pulling*, undesirable feedback, etc., when using a triode with control-grid injection tend to make multi-grid tubes the popular choice for this application on the lower frequencies.

On very high frequencies, where set noise rather than atmospheric noise limits the weak signal response, triode mixers are more widely used. A 6J6 miniature twin triode with grids in push-pull and plates in parallel makes an excellent mixer up to about 600 Mc.

Injection Voltage The amplitude of the injection voltage will affect the conversion transconductance of the mixer, and therefore should be made optimum if maximum signal-to-noise ratio is desired. If fixed bias is employed on the injection grid, the optimum injection voltage is quite critical. If cathode bias is used, the optimum voltage is not so critical; and if grid leak bias is employed, the optimum injection voltage is not at all critical just so it is adequate. Typical optimum injection voltages will run from 1 to 10 volts for control grid injection, and 45 volts or so for screen or suppressor grid injection.

Images There always are *two* signal frequencies which will combine with a given frequency to produce the same difference frequency. For example: assume a superheterodyne with its oscillator operating on a higher frequency than the signal, which is common practice in present superheterodynes, tuned to receive a signal at 14,100 kc. Assuming an i-f amplifier frequency of 450 kc., the mixer input circuit will be tuned to 14,100 kc., and the oscillator to 14,100 plus 450, or 14,550 kc. Now, a *strong* signal at the oscillator frequency plus the intermediate frequency (14,550 plus 450, or 15,000 kc.) will also give a difference frequency of 450 kc. in the mixer output and will be heard also. Note that the image is always *twice* the intermediate frequency away from the desired signal. Images cause *repeat points* on the tuning dial.

The only way that the image could be eliminated in this particular case would be to make the selectivity of the mixer input circuit, and any circuits preceding it, great enough so that the 15,000-kc. signal never reaches the mixer grid in sufficient amplitude to produce interference.

For any particular intermediate frequency, image interference troubles become increasingly greater as the frequency to which the signal-frequency portion of the receiver is tuned is increased. This is due to the fact that the percentage difference between the desired frequency and the image frequency decreases as the receiver is tuned to a higher frequency. The ratio of strength between a signal at the image frequency and a signal at the frequency to which the receiver is tuned producing equal output is known as the *image ratio*. The higher this ratio, the better the receiver in regard to image-interference troubles.

With but a single tuned circuit between the mixer grid and the antenna, and with 400-500 kc. i-f amplifiers, image ratios of 60 db and over are easily obtainable up to frequencies around 2000 kc. Above this frequency, greater selectivity in the mixer grid circuit through the use of additional tuned circuits between the mixer and the antenna is necessary if a good image ratio is to be maintained.

10-5 R-F Stages

Since the necessary tuned circuits between the mixer and the antenna can be combined with tubes to form r-f amplifier stages, the

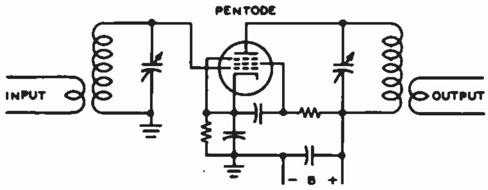


Figure 8
TYPICAL PENTODE R-F AMPLIFIER STAGE

reduction of the effects of mixer noise and the increasing of the image ratio can be accomplished in a single section of the receiver. When incorporated in the receiver, this section is known simply as an *r-f amplifier;* when it is a separate unit with a separate tuning control it is often known as a *preselector.* Either one or two stages are commonly used in the preselector or r-f amplifier. Some preselectors use regeneration to obtain still greater amplification and selectivity. An r-f amplifier or preselector embodying more than two stages rarely ever is employed since two stages will ordinarily give adequate gain to override mixer noise.

R-F Stages in the V-H-F Range Generally speaking, atmospheric noise in the frequency range above 30 Mc. is quite low—so low, in fact, that the noise generated within the receiver itself is greater than the noise received on the antenna. Hence it is of the greatest importance that internally generated noise be held to a minimum in a receiver. At frequencies much above 300 Mc. there is not too much that can be done at the present state of the art in the direction of reducing receiver noise below that generated in the converter stage. But in the v-h-f range, between 30 and 300 Mc., the receiver noise factor in a well designed unit is determined by the characteristics of the first r-f stage.

The usual v-h-f receiver, whether for communications or for FM or TV reception, uses a miniature pentode for the first r-f amplifier stage. The 6AK5 is the best of presently available types, with the 6CB6 and the 6DC6 closely approaching the 6AK5 in performance. But when gain in the first r-f stage is not so important, and the best noise factor must be obtained, the first r-f stage usually uses a triode.

Shown in figure 9 are four commonly used types of triode r-f stages for use in the v-h-f range. The circuit at (A) uses few components and gives a moderate amount of gain with very low noise. It is most satisfactory when the first r-f stage is to be fed directly from a low-

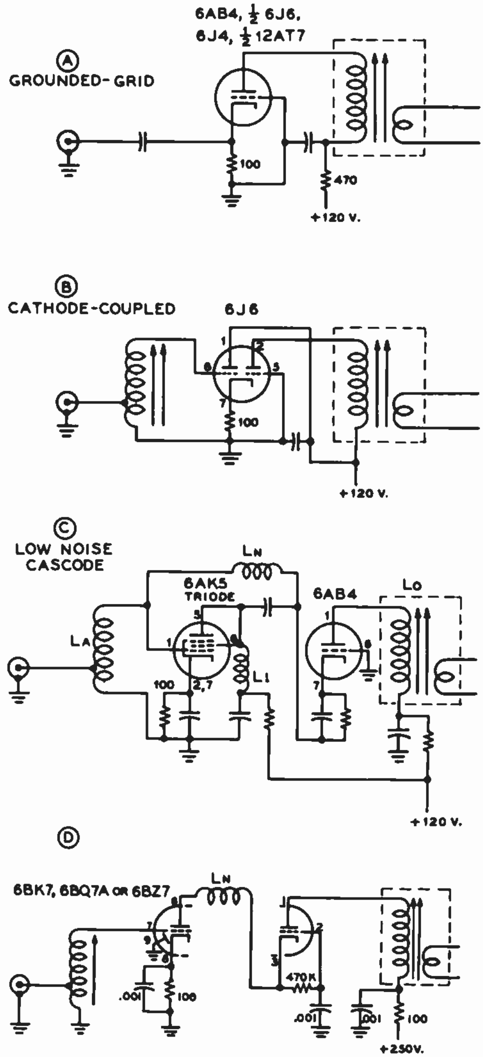


Figure 9
TYPICAL TRIODE V-H-F R-F AMPLIFIER STAGES
Triode r-f stages contribute the least amount of noise output for a given signal level, hence their frequent use in the v-h-f range.

impedance coaxial transmission line. Figure 9 (B) gives somewhat more gain than (A), but requires an input matching circuit. The effective gain of this circuit is somewhat reduced when it is being used to amplify a broad band of frequencies since the effective G_m of the cathode-coupled dual tube is somewhat less

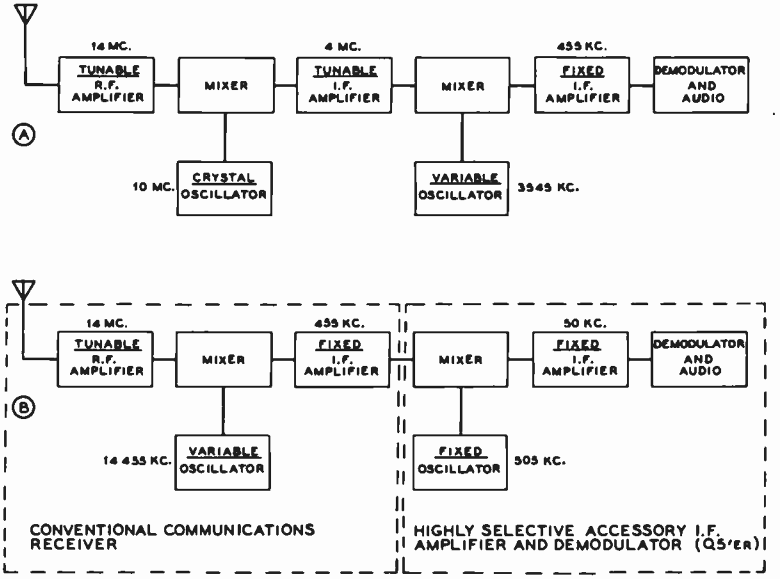


Figure 10

TYPICAL DOUBLE-CONVERSION SUPERHETERODYNE RECEIVERS

Illustrated at (A) is the basic circuit of a commercial double-conversion superheterodyne receiver. At (B) is illustrated the application of an accessory sharp i-f channel for obtaining improved selectivity from a conventional communications receiver through the use of the double-conversion principle.

than half the G_m of either of the two tubes taken alone.

The Cascode Amplifier The Cascode r-f amplifier, developed at the MIT Radiation Laboratory during World War II, is a low noise circuit employing a grounded cathode triode driving a grounded grid triode, as shown in figure 9C. The stage gain of such a circuit is about equal to that of a pentode tube, while the noise figure remains at the low level of a triode tube. Neutralization of the first triode tube is usually unnecessary below 50 Mc. Above this frequency, a definite improvement in the noise figure may be obtained through the use of neutralization. The neutralizing coil, L_N, should resonate at the operating frequency with the grid-plate capacity of the first triode tube.

The 6BQ7A and 6BZ7 tubes are designed for use in cascode circuits, and may be used to good advantage in the 144 Mc. and 220 Mc. amateur bands (figure 9D). For operation at higher frequencies, the 6AJ4 tube is recommended.

Double Conversion As previously mentioned, the use of a higher intermediate frequency will also improve the image ratio, at the expense of i-f selectivity, by placing the desired signal and the image farther apart. To give both good image ratio at the higher frequencies and good selectivity in the i-f amplifier, a system known as *double conversion* is sometimes employed. In this system, the incoming signal is first converted to a rather high intermediate frequency, and then amplified and again converted, this time to a much lower frequency. The first intermediate frequency supplies the necessary wide separation between the image and the desired signal, while the second one supplies the bulk of the i-f selectivity.

The double-conversion system, as illustrated in figure 10, is receiving two general types of application at the present time. The first application is for the purpose of attaining extremely good stability in a communications receiver through the use of crystal control of the first oscillator. In such an arrangement, as used in several types of Collins receivers, the first oscillator is crystal controlled and is followed by a tunable i-f amplifier which then is followed by a mixer stage and a fixed-tuned i-f amplifier on a much lower frequency. Through such a circuit arrangement the stability of the complete receiver is equal to the stability of the oscillator which feeds the second mixer, while the selectivity is determined by the bandwidth of the second, fixed i-f amplifier.

The second common application of the double-conversion principle is for the purpose of obtaining a very high degree of selectivity in the complete communications receiver. In this type of application, as illustrated in figure 10 (B), a conventional communications receiver is modified in such a manner that its normal i-f amplifier (which usually is in the 450 to 915 kc. range) instead of being fed to a demodulator and then to the audio system, is alternatively fed to a fixed-tune mixer stage and then into a much lower intermediate frequency amplifier before the signal is demodulated and fed to the audio system. The accessory i-f amplifier system (sometimes called a Q5'er) normally is operated on a frequency of 175 kc., 85 kc., or 50 kc.

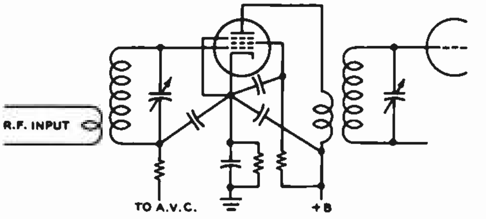


Figure 11
ILLUSTRATING "COMMON POINT" BY-PASSING

To reduce the detrimental effects of cathode circuit inductance in v-h-f stages, all by-pass capacitors should be returned to the cathode terminal at the socket. Tubes with two cathode leads can give improved performance if the grid return is made to one cathode terminal while the plate and screen by-pass returns are made to the cathode terminal which is connected to the suppressor within the tube.

10-6 Signal-Frequency Tuned Circuits

The signal-frequency tuned circuits in high-frequency superheterodynes and tuned radio frequency types of receivers consist of coils of either the solenoid or universal-wound types shunted by variable capacitors. It is in these tuned circuits that the causes of success or failure of a receiver often lie. The universal-wound type coils usually are used at frequencies below 2000 kc.; above this frequency the single-layer solenoid type of coil is more satisfactory.

Impedance and Q The two factors of greatest significance in determining the gain-per-stage and selectivity, respectively, of a tuned amplifier are tuned-circuit impedance and tuned-circuit Q. Since the resistance of modern capacitors is low at ordinary frequencies, the resistance usually can be considered to be concentrated in the coil. The resistance to be considered in making Q determinations is the r-f resistance, not the d-c resistance of the wire in the coil. The latter ordinarily is low enough that it may be neglected. The increase in r-f resistance over d-c resistance primarily is due to skin effect and is influenced by such factors as wire size and type, and the proximity of metallic objects or poor insulators, such as coil forms with high losses. Higher values of Q lead to better selectivity and increased r-f voltage across the tuned circuit. The increase in voltage is due to an increase in the circuit impedance with the higher values of Q.

Frequently it is possible to secure an increase in impedance in a resonant circuit, and consequently an increase in gain from an amplifier stage, by increasing the reactance through the use of larger coils and smaller tuning capacitors (higher L/C ratio).

Input Resistance Another factor which influences the operation of tuned circuits is the input resistance of the tubes placed across these circuits. At broadcast frequencies, the input resistance of most conventional r-f amplifier tubes is high enough so that it is not bothersome. But as the frequency is increased, the input resistance becomes lower and lower, until it ultimately reaches a value so low that no amplification can be obtained from the r-f stage.

The two contributing factors to the decrease in input resistance with increasing frequency are the transit time required by an electron traveling between the cathode and grid, and the inductance of the cathode lead common to both the plate and grid circuits. As the frequency becomes higher, the transit time can become an appreciable portion of the time required by an r-f cycle of the signal voltage, and current will actually flow into the grid. The result of this effect is similar to that which would be obtained by placing a resistance between the tube's grid and cathode.

Superheterodyne Tracking Because the oscillator in a superheterodyne operates "offset" from the other front end circuits, it is necessary to make special provisions to allow the oscillator to track when similar tuning capacitor sections are

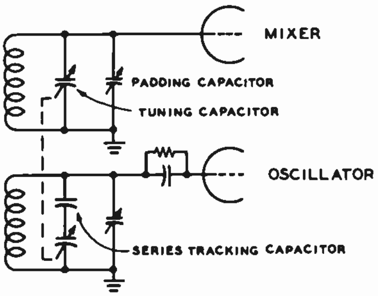


Figure 12
SERIES TRACKING EMPLOYED IN THE H-F OSCILLATOR OF A SUPERHETERODYNE

The series tracking capacitor permits the use of identical gangs in a ganged capacitor, since the tracking capacitor slows down the rate of frequency change in the oscillator so that a constant difference in frequency between the oscillator and the r-f stage (equal to the i-f amplifier frequency) may be maintained.

ganged. The usual method of obtaining good tracking is to operate the oscillator on the high-frequency side of the mixer and use a series *tracking capacitor* to slow down the tuning rate of the oscillator. The oscillator tuning rate must be slower because it covers a smaller range than does the mixer when both are expressed as a percentage of frequency. At frequencies above 7000 kc. and with ordinary intermediate frequencies, the difference in percentage between the two tuning ranges is so small that it may be disregarded in receivers designed to cover only a small range, such as an amateur band.

A mixer and oscillator tuning arrangement in which a series tracking capacitor is provided is shown in figure 12. The value of the tracking capacitor varies considerably with different intermediate frequencies and tuning ranges, capacitances as low as .0001 μfd. being used at the lower tuning-range frequencies, and values up to .01 μfd. being used at the higher frequencies.

Superheterodyne receivers designed to cover only a single frequency range, such as the standard broadcast band, sometimes obtain tracking between the oscillator and the r-f circuits by cutting the variable plates of the oscillator tuning section to a different shape from those used to tune the r-f stages.

Frequency Range Selection The frequency to which a receiver responds may be varied by changing the size of either the coils or the capacitors in the tuning circuits, or both. In short-wave receivers

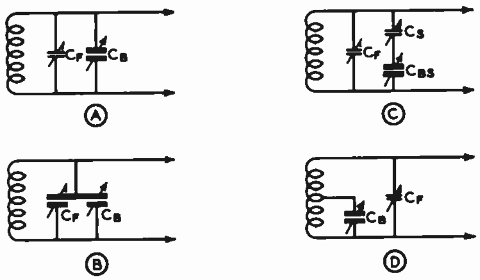


Figure 13
BANDSPREAD CIRCUITS

Parallel bandspread is illustrated at (A) and (B), series bandspread at (C), and tapped-coil bandspread at (D),

a combination of both methods is usually employed, the coils being changed from one band to another, and variable capacitors being used to tune the receiver across each band. In practical receivers, coils may be changed by one of two methods: a switch, controllable from the panel, may be used to switch coils of different sizes into the tuning circuits or, alternatively, coils of different sizes may be plugged manually into the receiver, the connection into the tuning circuits being made by suitable plugs on the coils. Where there are several *plug-in coils* for each band, they are sometimes arranged to a single mounting strip, allowing them all to be plugged in simultaneously.

Bandspread Tuning In receivers using large tuning capacitors to cover the short-wave spectrum with a minimum of coils, tuning is likely to be quite difficult, owing to the large frequency range covered by a small rotation of the variable capacitors. To alleviate this condition, some method of slowing down the tuning rate, or *bandspreading,* must be used.

Quantitatively, bandspread is usually designated as being inversely proportional to the range covered. Thus, a *large* amount of bandspread indicates that a *small* frequency range is covered by the bandspread control. Conversely, a *small* amount of bandspread is taken to mean that a *large* frequency range is covered by the bandspread dial.

Types of Bandspread Bandspreading systems are of two general types: electrical and mechanical. Mechanical systems are exemplified by high-ratio dials in which the tuning capacitors rotate much more slowly than the dial knob. In this system, there is often a separate scale or pointer either connected or geared to the dial knob to facilitate accurate dial readings. However, there is a practical limit to the amount of mechanical bandspread which can be obtained in a dial and capacitor before the speed-reduction unit and capacitor bearings become prohibitively expensive. Hence, most receivers employ a combination of electrical and mechanical bandspread. In such a system, a moderate reduction in the tuning rate is obtained in the dial, and the rest of the reduction obtained by *electrical bandspreading*.

Stray Circuit Capacitance In this book and in other radio literature, mention is sometimes made of *stray* or *circuit capacitance*. This capacitance is in the usual sense defined as the capacitance remaining across a coil when all the tuning, bandspread, and padding capacitors across the circuit are at their minimum capacitance setting.

Circuit capacitance can be attributed to two general sources. One source is that due to the input and output capacitance of the tube when its cathode is heated. The input capacitance varies somewhat from the static value when the tube is in actual operation. Such factors as plate load impedance, grid bias, and frequency will cause a change in input capacitance. However, in all except the extremely high-transconductance tubes, the published measured input capacitance is reasonably close to the effective value when the tube is used within its recommended frequency range. But in the high-transconductance types the effective capacitance will vary considerably from the published figures as operating conditions are changed.

The second source of circuit capacitance, and that which is more easily controllable, is that contributed by the minimum capacitance of the variable capacitors across the circuit and that due to capacitance between the wiring and ground. In well-designed high-frequency receivers, every effort is made to keep this portion of the circuit capacitance at a minimum since a large capacitance reduces the tuning range available with a given coil and prevents a good L/C ratio, and consequently a high-impedance tuned circuit, from being obtained.

A good percentage of stray circuit capacitance is due also to distributed capacitance of the coil and capacitance between wiring points and chassis.

Typical values of circuit capacitance may run from 10 to 75 $\mu\mu$fd. in high-frequency receivers, the first figure representing concentric-line receivers with acorn or miniature tubes and extremely small tuning capacitors, and the latter representing all-wave sets with bandswitching, large tuning capacitors, and conventional tubes.

10-7 I-F Tuned Circuits

I-f amplifiers usually employ bandpass circuits of some sort. A bandpass circuit is exactly what the name implies—a circuit for passing a band of frequencies. Bandpass arrangements can be designed for almost any degree of selectivity, the type used in any particular case depending upon the ultimate application of the amplifier.

I-F Transformers Intermediate frequency transformers ordinarily consist of two or more tuned circuits and some method of coupling the tuned circuits together. Some representative arrangements are shown in figure 14. The circuit shown at A is the conventional i-f transformer, with the coupling, M, between the tuned circuits being provided by inductive coupling from one coil to the other. As the coupling is increased, the selectivity curve becomes less peaked, and when a condition known as *critical coupling* is reached, the top of the curve begins to flatten out. When the coupling is increased still more, a dip occurs in the top of the curve.

The windings for this type of i-f transformer, as well as most others, nearly always consist of small, flat universal-wound pies mounted either on a piece of dowel to provide an air core or on powdered-iron for *iron core* i-f transformers. The iron-core transformers generally have somewhat more gain and better selectivity than equivalent air-core units.

The circuits shown at figure 14-B and C are quite similar. Their only difference is the type of mutual coupling used, an inductance being used at B and a capacitance at C. The operation of both circuits is similar. Three resonant circuits are formed by the components. In B, for example, one resonant circuit is formed by L_1, C_1, C_2 and L_2 all in series. The frequency of this resonant circuit is just the same as that of a single one of the coils and capacitors, since the coils and capacitors are similar in both sides of the circuit, and the resonant frequency of the two capacitors and the two coils all in series is the same as that of a single coil and capacitor. The second resonant frequency of the complete circuit is determined by the characteristics of each half of the circuit containing the mutual coupling device. In B, this second frequency will be lower than the first, since the resonant frequency of L_1, C_1 and the inductance, M, or L_2, C_2 and M is lower than that of a single coil and capacitor, due to the inductance of M being added to the circuit.

The opposite effect takes place at figure 14-C, where the common coupling impedance is a capacitor. Thus, at C the second resonant frequency is higher than the first. In either case, however, the circuit has two resonant frequencies, resulting in a flat-topped selectivity curve. The width of the top of the curve is controlled by the reactance of the mutual coupling component. As this reactance is increased (inductance made greater, capacitance made smaller), the two resonant frequencies become further apart and the curve is broadened.

In the circuit of figure 14-D, there is inductive coupling between the center coil and each of the outer coils. The result of this arrangement is that the center coil acts as a sharply tuned coupler between the other two. A signal somewhat off the resonant frequency of the transformer will not induce as much current in the center coil as will a signal of the correct frequency. When a smaller current is induced in the center coil, it in turn transfers a still smaller current to the output coil. The effective coupling between the outer coils increases as the resonant frequency is approached, and remains nearly constant over a small range and then decreases again as the resonant band is passed.

Another very satisfactory bandpass arrangement, which gives a very straight-sided, flat-topped curve, is the negative-mutual arrangement shown at figure 14-E. Energy is transferred between the input and output circuits in this arrangement by both the negative-mutual coils, M, and the common capacitive reactance, C. The negative-mutual coils are interwound on the same form, and connected *backward.*

Transformers usually are made tunable over a small range to permit accurate alignment in the circuit in which they are employed. This is accomplished either by means of a variable capacitor across a fixed inductance, or by means of a fixed capacitor across a variable inductance. The former usually employ either a mica-compression capacitor (designated "mica tuned"), or a small air dielectric variable capacitor (designated "air tuned"). Those which use a fixed capacitor usually employ a powdered iron core on a threaded rod to vary the inductance, and are known as "permeability tuned."

Shape Factor It is obvious that to pass modulation sidebands and to allow for slight drifting of the transmitter carrier frequency and the receiver local oscillator, the i-f amplifier must pass not a single frequency but a band of frequencies. The width of this pass band, usually 5 to 8 kc. at maximum width in a good communications receiver, is known as the *pass band,* and is arbitrarily taken as the width between the two frequencies at which the response is attenuated 6 db, or is "6 db down." However, it is apparent that to discriminate against an interfering signal which is stronger than the desired signal, much more than 6 db attenuation is required. The attenuation arbitrarily taken to indicate adequate discrimination against an interfering signal is 60 db.

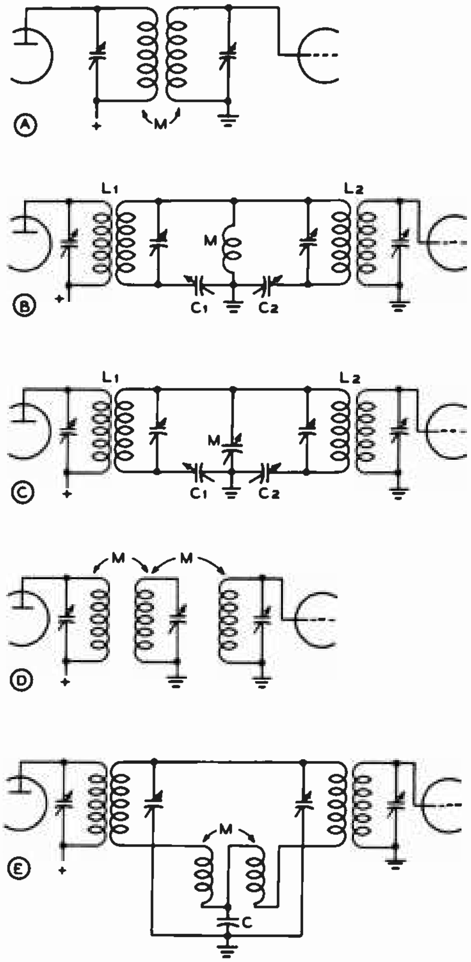


Figure 14
I-F AMPLIFIER COUPLING ARRANGEMENTS

The interstage coupling arrangements illustrated above give a better shape factor (more straight sided selectivity curve) than would the same number of tuned circuits coupled by means of tubes.

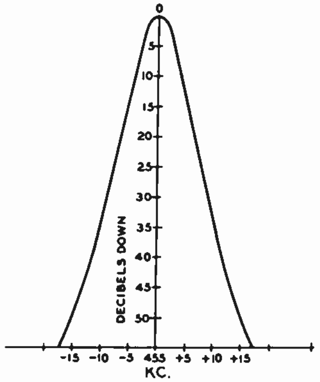


Figure 15
I-F PASS BAND OF TYPICAL COMMUNICATIONS RECEIVER

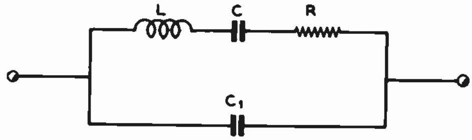


Figure 16
ELECTRICAL EQUIVALENT OF QUARTZ FILTER CRYSTAL

The crystal is equivalent to a very large value of inductance in series with small values of capacitance and resistance, with a larger though still small value of capacitance across the whole circuit (representing holder capacitance plus stray capacitances).

It is apparent that it is desirable to have the bandwidth at 60 db down as narrow as possible, but it must be done without making the pass band (6 db points) too narrow for satisfactory reception of the desired signal. The figure of merit used to show the ratio of bandwidth at 6 db down to that at 60 db down is designated *shape factor.* The ideal i-f curve, a rectangle, would have a shape factor of 1.0. The i-f shape factor in typical communications receivers runs from 3.0 to 5.5.

The most practicable method of obtaining a low shape factor for a given number of tuned circuits is to employ them in pairs, as in figure 14-A, adjusted to *critical coupling* (the value at which two resonance points just begin to become apparent). If this gives too sharp a "nose" or pass band, then coils of lower Q should be employed, with the coupling maintained at the critical value. As the Q is lowered, closer coupling will be required for critical coupling.

Conversely if the pass band is too broad, coils of higher Q should be employed, the coupling being maintained at critical. If the pass band is made more narrow by using looser coupling instead of raising the Q and maintaninig critical coupling, the shape factor will not be as good.

The *pass band* will not be much narrower for several pairs of identical, critically coupled tuned circuits than for a single pair. However, the *shape factor* will be greatly improved as each additional pair is added, up to about 5 pairs, beyond which the improvement for each additional pair is not significant. Commercially available communications receivers of good quality normally employ 3 or 4 double tuned transformers with coupling adjusted to critical or slightly less.

The pass band of a typical communication receiver having a 455 kc. i-f amplifier is shown in figure 15.

"Miller Effect" As mentioned previously, the dynamic input capacitance of a tube varies slightly with bias. As a-v-c voltage normally is applied to i-f tubes for radiotelephony reception, the effective grid-cathode capacitance varies as the signal strength varies, which produces the same effect as slight detuning of the i-f transformer. This effect is known as "Miller effect," and can be minimized to the extent that it is not troublesome either by using a fairly low L/C ratio in the transformers or by incorporating a small amount of degenerative feedback, the latter being most easily accomplished by leaving part of the cathode resistor unbypassed for r.f.

Crystal Filters The pass band of an intermediate frequency amplifier may be made very narrow through the use of a piezoelectric filter crystal employed as a series resonant circuit in a bridge arrangement known as a *crystal filter.* The shape factor is quite poor, as would be expected when the selectivity is obtained from the equivalent of a single tuned circuit, but the very narrow pass band obtainable as a result of the extremely high Q of the crystal makes the crystal filter useful for c-w telegraphy reception. The pass band of a 455 kc. crystal filter may be made as narrow as 50 cycles, while the narrowest pass band that can be obtained with a 455 kc. tuned circuit of practicable dimensions is about 5 kc.

The electrical equivalent of a filter crystal is shown in figure 16. For a given frequency, L is very high, C very low, and R (assuming

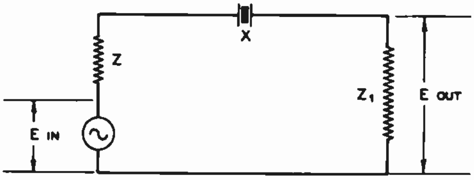


Figure 17
EQUIVALENT OF CRYSTAL FILTER CIRCUIT

For a given voltage out of the generator, the voltage developed across Z_1 depends upon the ratio of the impedance of X to the sum of the impedances of Z and Z_1. Because of the high Q of the crystal, its impedance changes rapidly with changes in frequency.

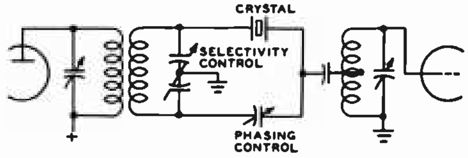


Figure 18
TYPICAL CRYSTAL FILTER CIRCUIT

a good crystal of high Q) is very low. Capacitance C_1 represents the shunt capacitance of the electrodes, plus the crystal holder and wiring, and is many times the capacitance of C. This makes the crystal act as a parallel resonant circuit with a frequency only slightly higher than that of its frequency of series resonance. For crystal filter use it is the series resonant characteristic that we are primarily interested in.

The electrical equivalent of the basic crystal filter circuit is shown in figure 17. If the impedance of Z plus Z_1 is low compared to the impedance of the crystal X at resonance, then the current flowing through Z_1, and the voltage developed across it, will be almost in inverse proportion to the impedance of X, which has a very sharp resonance curve.

If the impedance of Z plus Z_1 is made *high* compared to the resonant impedance of X, then there will be no appreciable drop in voltage across Z_1 as the frequency departs from the resonant frequency of X until the point is reached where the impedance of X approaches that of Z plus Z_1. This has the effect of broadening out the curve of frequency versus voltage developed across Z_1, which is another way of saying that the selectivity of the crystal filter (but not the crystal proper) has been reduced.

In practicable filter circuits the impedances Z and Z_1 usually are represented by some form of tuned circuit, but the basic principle of operation is the same.

Practical Filters It is necessary to balance out the capacitance across the crystal holder (C_1, in figure 16) to prevent bypassing around the crystal undesired signals off the crystal resonant frequency. The balancing is done by a *phasing* circuit which takes out-of-phase voltage from a balanced input circuit and passes it to the output side of the crystal in proper phase to neutralize that passed through the holder capacitance. A representative practical filter arrangement is shown in figure 18. The balanced input circuit may be obtained either through the use of a split-stator capacitor as shown, or by the use of a center-tapped input coil.

Variable-Selectivity Filters In the circuit of figure 18, the selectivity is *minimum* with the crystal input circuit tuned to resonance, since at resonance the impedance of the tuned circuit is maximum. As the input circuit is detuned from resonance, however, the impedance decreases, and the selectivity becomes greater. In this circuit, the output from the crystal filter is tapped down on the i-f stage grid winding to provide a low value of series impedance in the output circuit. It will be recalled that for maximum selectivity, the total impedance in series with the crystal (both input and output circuits) must be low. If one is made low and the other is made variable, then the selectivity may be varied at will from sharp to broad.

The circuit shown in figure 19 also achieves variable selectivity by adding a variable impedance in series with the crystal circuit. In this case, the variable impedance is in series with the crystal output circuit. The impedance of the output circuit is varied by varying the Q. As the Q is reduced (by adding resistance in series with the coil), the impedance decreases and the selectivity becomes greater. The input circuit impedance is made low by using a non-resonant secondary on the input transformer.

A variation of the circuit shown at figure 19 consists of placing the variable resistance across the coil and capacitor, rather than in series with them. The result of adding the resistor is a reduction of the output impedance, and an increase in selectivity. The circuit behaves oppositely to that of figure 19, however; as the resistance is lowered the selectivity becomes greater. Still another variation of figure 19 is to use the tuning capacitor across the output coil to vary the output impedance.

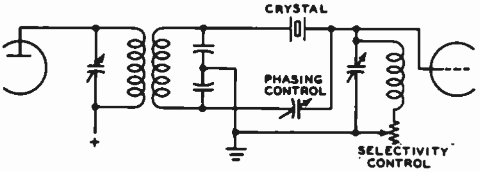


Figure 19
VARIABLE SELECTIVITY CRYSTAL FILTER
This circuit permits of a greater control of selectivity than does the circuit of figure 16, and does not require a split-stator variable capacitor.

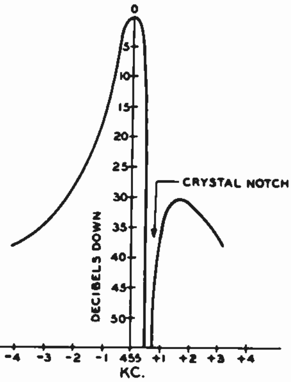


Figure 20
I-F PASS BAND OF TYPICAL CRYSTAL FILTER COMMUNICATIONS RECEIVER

As the output circuit is detuned from resonance, its impedance is lowered, and the selectivity increases. Sometimes a set of fixed capacitors and a multipoint switch are used to give step-by-step variation of the output circuit tuning, and thus of the crystal filter selectivity.

Rejection Notch As previously discussed, a filter crystal has both a resonant (series resonant) and an anti-resonant (parallel resonant) frequency, the impedance of the crystal being quite low at the former frequency, and quite high at the latter frequency. The anti-resonant frequency is just slightly higher than the resonant frequency, the difference depending upon the effective shunt capacitance of the filter crystal and holder. As adjustment of the phasing capacitor controls the effective shunt capacitance of the crystal, it is possible to vary the anti-resonant frequency of the crystal slightly without unbalancing the circuit sufficiently to let undesired signals *leak through* the shunt capacitance in appreciable amplitude. At the exact anti-resonant frequency of the crystal the attenuation is exceedingly high, because of the high impedance of the crystal at this frequency. This is called the *rejection notch,* and can be utilized virtually to eliminate the heterodyne image or *repeat tuning* of c-w signals. The beat frequency oscillator can be so adjusted and the phasing capacitor so adjusted that the desired beat note is of such a pitch that the image (the same audio note on the other side of zero beat) falls in the rejection notch and is inaudible. The receiver then is said to be adjusted for *single-signal* operation.

The rejection notch sometimes can be employed to reduce interference from an undesired *phone* signal which is very close in frequency to a desired phone signal. The filter is adjusted to "broad" so as to permit telephony reception, and the receiver tuned so that the carrier frequency of the undesired signal falls in the rejection notch. The modulation sidebands of the undesired signal still will come through, but the carrier heterodyne will be effectively eliminated and interference greatly reduced.

A typical crystal selectivity curve for a communications receiver is shown in figure 20.

Crystal Filter Considerations A crystal filter, especially when adjusted for *single signal* reception, greatly reduces interference and background noise, the latter feature permitting signals to be copied that would ordinarily be too weak to be heard above the background hiss. However, when the filter is adjusted for maximum selectivity, the pass band is so narrow that the received signal must have a high order of stability in order to stay within the pass band. Likewise, the local oscillator in the receiver must be highly stable, or constant retuning will be required. Another effect that will be noticed with the filter adjusted too "sharp" is a tendency for code characters to produce a ringing sound, and have a hangover or "tails." This effect limits the code speed that can be copied satisfactorily when the filter is adjusted for extreme selectivity.

The Mechanical Filter The Collins Mechanical Filter (figure 21) is a new concept in the field of selectivity. It is an electro-mechanical bandpass filter about half the size of a cigarette package. As shown in figure 22, it consists of an input transducer, a resonant mechanical section comprised of a number of metal discs, and an output transducer.

The frequency characteristics of the resonant mechanical section provide the almost rectangular selectivity curves shown in figure 23. The input and output transducers serve only as electrical to mechanical coupling devices and do not affect the selectivity characteristics which are determined by the metal discs. An electrical signal applied to the input terminals is converted into a mechanical vibration at the input transducer by means of magnetostriction. This mechanical vibration travels through the resonant mechanical section to the output transducer, where it is converted by magnetostriction to an electrical signal which appears at the output terminals.

In order to provide the most efficient electromechanical coupling, a small magnet in the mounting above each transducer applies a magnetic bias to the nickel transducer core. The electrical impulses then add to or subtract from this magnetic bias, causing vibration of the filter elements that corresponds to the exciting signal. There is no mechanical motion except for the imperceptible vibration of the metal discs.

Magnetostrictively-driven mechanical filters have several advantages over electrical equivalents. In the region from 100 kc. to 500 kc., the mechanical elements are extremely small, and a mechanical filter having better selectivity than the best of conventional i-f systems may be enclosed in a package smaller than one i-f transformer.

Since mechanical elements with Q's of 5000 or more are readily obtainable, mechanical filters may be designed in accordance with the theory for lossless elements. This permits filter characteristics that are unobtainable with electrical circuits because of the relatively high losses in electrical elements as compared with the mechanical elements used in the filters.

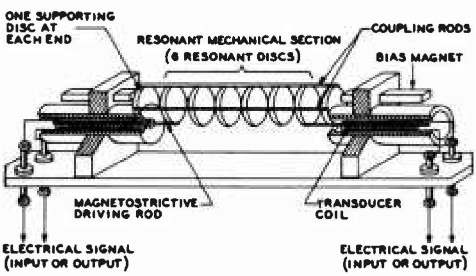


Figure 22
MECHANICAL FILTER
FUNCTIONAL DIAGRAM

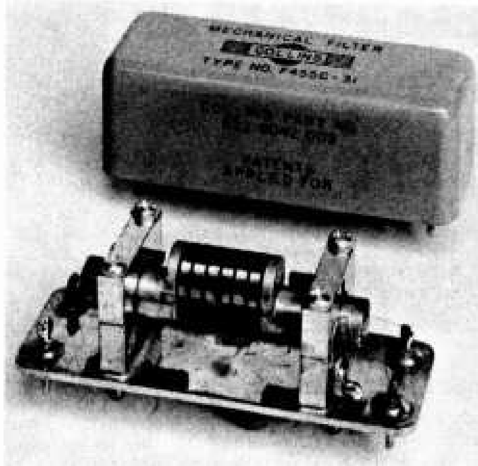


Figure 21
COLLINS MECHANICAL FILTER
Interior view of filter showing suspension of resonating discs.

The frequency characteristics of the mechanical filter are permanent, and no adjustment is required or is possible. The filter is enclosed in a hermetically sealed case.

In order to realize full benefit from the mechanical filter's selectivity characteristics, it is necessary to provide shielding between the external input and output circuits, capable of reducing transfer of energy external to the

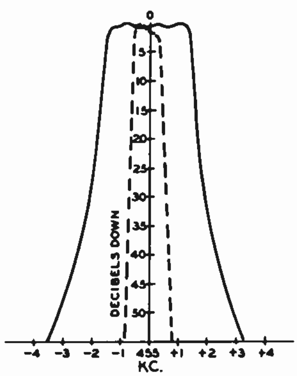


Figure 23

Selectivity curves of 455-kc. mechanical filters with nominal 0.8-kc. (dotted line) and 3.1-kc. (solid line) bandwidth at -6 db.

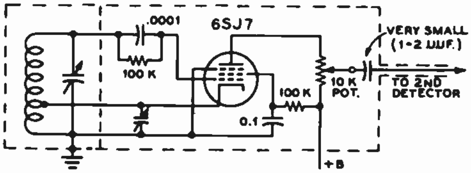


Figure 24
VARIABLE-OUTPUT B-F-O CIRCUIT
A beat-frequency oscillator whose output is controllable is of considerable assistance in copying c-w signals over a wide range of levels, and such a control is almost a necessity for satisfactory copying of single-sideband radiophone signals.

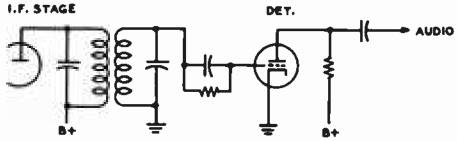
filter by a minimum value of 100 db. If the input circuit is allowed to couple energy into the output circuit external to the filter, the excellent skirt selectivity will deteriorate and the passband characteristics will be distorted.

As with almost any mechanically resonant circuit, elements of the mechanical filter have multiple resonances. These result in spurious modes of transmission through the filter and produce minor passbands at frequencies on other sides of the primary passband. Design of the filter reduces these sub-bands to a low level and removes them from the immediate area of the major passband. Two conventional i-f transformers supply increased attenuation to these spurious responses, and are sufficient to reduce them to an insignificant level.

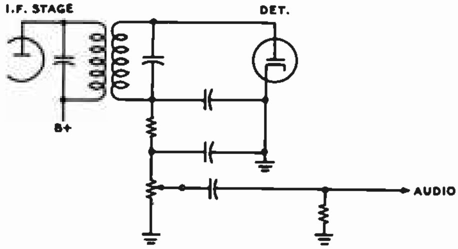
Beat-Frequency Oscillators The beat-frequency oscillator, usually called the *b.f.o.*, is a necessary adjunct for reception of c-w telegraph signals on superheterodynes which have no other provision for obtaining modulation of an incoming c-w telegraphy signal. The oscillator is coupled into or just ahead of second detector circuit and supplies a signal of nearly the same frequency as that of the desired signal from the i-f amplifier. If the i-f amplifier is tuned to 455 kc., for example, the b.f.o. is tuned to approximately 454 or 456 kc. to produce an audible (1000 cycle) beat note in the output of the second detector of the receiver. The carrier signal itself is, of course, inaudible. The b.f.o. is not used for voice reception, except as an aid in searching for weak stations.

The b-f-o input to the second detector need only be sufficient to give a good beat note on an average signal. Too much coupling into the second detector will give an excessively high hiss level, masking weak signals by the high noise background.

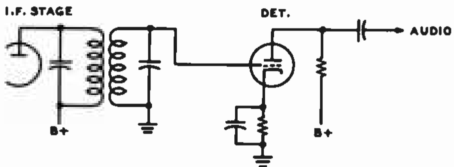
Figure 24 shows a method of manually adjusting the b-f-o output to correspond with the strength of received signals. This type of variable b-f-o output control is a useful adjunct to any superheterodyne, since it allows sufficient b-f-o output to be obtained to *beat* with strong signals or to allow single-sideband reception and at the same time permits the b-f-o output, and consequently the hiss, to be reduced when attempting to receive weak signals. The circuit shown is somewhat better than those in which one of the electrode volt-



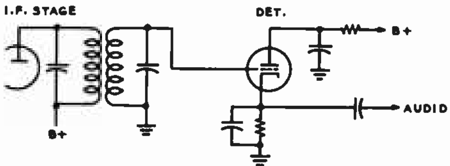
Ⓐ GRID LEAK DETECTOR



Ⓑ DIODE DETECTOR



Ⓒ PLATE DETECTOR



Ⓓ INFINITE IMPEDANCE DETECTOR

Figure 25
TYPICAL CIRCUITS FOR GRID-LEAK, DIODE, PLATE AND INFINITE IMPEDANCE DETECTOR STAGES

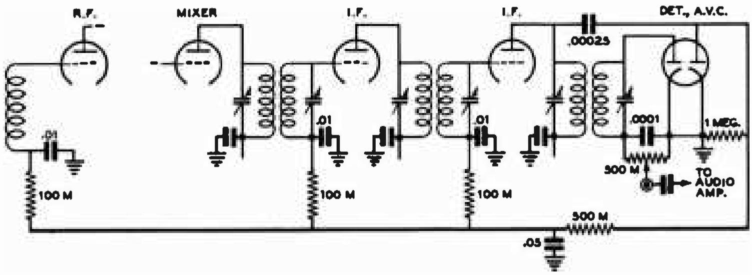


Figure 26
TYPICAL A-V-C CIRCUIT USING A DOUBLE DIODE

Any of the small dual-diode tubes may be used in this circuit. Or, if desired, a duo-diode-triode may be used, with the triode acting as the first audio stage. The left-hand diode serves as the detector, while the right-hand side acts as the a-v-c rectifier. The use of separate diodes for detector and a-v-c reduces distortion when receiving an AM signal with a high modulation percentage.

ages on the b-f-o tube is changed, as the latter circuits usually change the frequency of the b.f.o. at the same time they change the strength, making it necessary to reset the trimmer each time the output is adjusted.

The b.f.o. usually is provided with a small trimmer which is adjustable from the front panel to permit adjustment over a range of 5 or 10 kc. For single-signal reception the b.f.o. always is adjusted to the high-frequency side, in order to permit placing the heterodyne image in the rejection notch.

In order to reduce the b-f-o signal output voltage to a reasonable level which will prevent blocking the second detector, the signal voltage is delivered through a low-capacitance (high-reactance) capacitor having a value of 1 to 2 $\mu\mu$fd.

Care must be taken with the b.f.o. to prevent harmonics of the oscillator from being picked up at multiples of the b-f-o frequency. The complete b.f.o. together with the coupling circuits to the second detector, should be thoroughly shielded to prevent pickup of the harmonics by the input end of the receiver.

If b-f-o harmonics still have a tendency to give trouble after complete shielding and isolation of the b-f-o circuit has been accomplished, the passage of these harmonics from the b-f-o circuit to the rest of the receiver can be stopped through the use of a low-pass filter in the lead between the output of the b-f-o circuit and the point on the receiver where the b-f-o signal is to be injected.

10-8 Detector, Audio, and Control Circuits

Detectors Second detectors for use in superheterodynes are usually of the diode, plate, or infinite-impedance types. Occasionally, grid-leak detectors are used in receivers using one i-f stage or none at all, in which case the second detector usually is made regenerative.

Diodes are the most popular second detectors because they allow a simple method of obtaining automatic volume control to be used. Diodes load the tuned circuit to which they are connected, however, and thus reduce the selectivity slightly. Special i-f transformers are used for the purpose of providing a low-impedance input circuit to the diode detector.

Typical circuits for grid-leak, diode, plate and infinite-impedance detectors are shown in figure 25.

Automatic Volume Control The elements of an automatic volume control (a.v.c.) system are shown in figure 26. A dual-diode tube is used as a combination diode detector and a-v-c rectifier. The left-hand diode operates as a simple rectifier in the manner described earlier in this chapter. Audio voltage, superimposed on a d-c voltage, appears across the 500,000-ohm potentiometer (the volume control) and the .0001-μfd. capacitor, and is passed on to the audio amplifier. The right-hand diode receives signal voltage directly from the primary of the last i-f amplifier, and acts as the a-v-c rectifier. The pulsating d-c voltage across the 1-megohm a.v.c.-diode load resistor is filtered by a 500,000-ohm resistor and a .05-μfd. capacitor, and applied as bias to the grids of the r-f and i-f amplifier tubes; an increase or decrease in signal strength will cause a corresponding increase or decrease in a-v-c bias voltage, and thus the gain of the receiver is automatically adjusted to compensate for changes in signal strength.

A-C Loading of Second Detector By disassociating the a.v.c. and detecting functions through using separate diodes, as shown, most of the ill effects of *a-c shunt loading* on the detector diode are avoided. This type of loading causes serious distortion, and the additional components required to eliminate it are well worth their cost. Even with the circuit shown, a-c loading can occur unless a *very high* (5 megohms, or more) value of grid resistor is used in the following audio amplifier stage.

A.V.C. in B-F-O-Equipped Receivers In receivers having a beat-frequency oscillator for the reception of radiotelegraph signals, the use of a.v.c. can result in a great loss in sensitivity when the b.f.o. is switched on. This is because the beat oscillator output acts exactly like a strong received signal, and causes the a-v-c circuit to put high bias on the r-f and i-f stages, thus greatly reducing the receiver's sensitivity. Due to the above effect, it is necessary to provide a method of making the a-v-c circuit inoperative when the b.f.o. is being used. The simplest method of eliminating the a-v-c action is to short the a-v-c line to ground when the b.f.o. is turned on. A two-circuit switch may be used for the dual purpose of turning on the beat oscillator and shorting out the a.v.c. if desired.

Signal Strength Indicators Visual means for determining whether or not the receiver is properly tuned, as well as an indication of the relative signal strength, are both provided by means of *tuning indicators* (S meters) of the meter or vacuum-tube type. A d-c milliammeter can be connected in the plate supply circuit of one or more r-f or i-f amplifiers, as shown in figure 27A, so that the change in plate current, due to the action of the a-v-c voltage, will be indicated on the instrument. The d-c instrument MA should have a full-scale reading approximately equal to the total plate current taken by the stage or stages whose plate current passes through the instrument. The value of this current can be estimated by assuming a plate current on each stage (with no signal input to the receiver) of about 6 ma. However, it will be found to be more satisfactory to measure the actual plate current on the stages with a milliammeter of perhaps 0-100 ma. full scale before purchasing an instrument for use as an S meter. The 50-ohm potentiometer shown in the drawing is used to adjust the meter reading to full scale with no signal input to the receiver.

When an ordinary meter is used in the plate circuit of a stage, for the purpose of indicating signal strength, the meter reads backwards

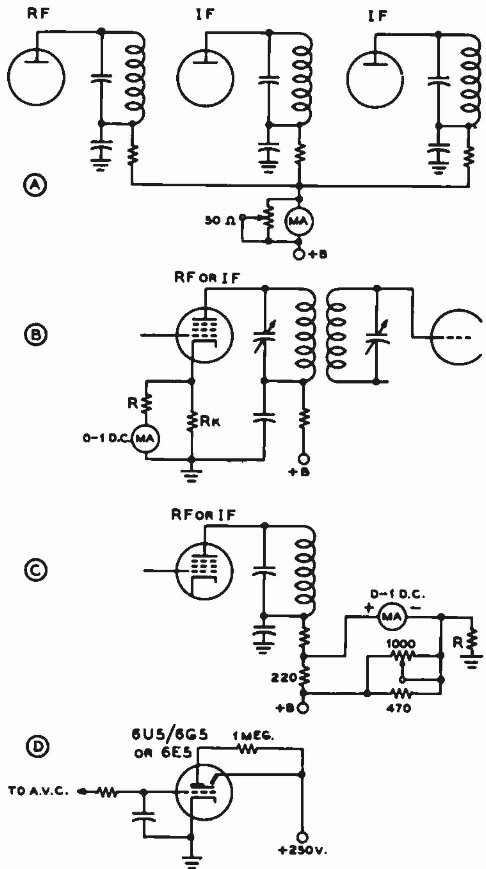


Figure 27
SIGNAL-STRENGTH-METER CIRCUITS
Shown above are four circuits for obtaining a signal-strength reading which is a function of incoming carrier amplitude. The circuits are discussed in the accompanying text.

with respect to strength. This is because increased a-v-c bias on stronger signals causes lower plate current through the meter. For this reason, special meters which indicate zero at the right-hand end of the scale are often used for signal strength indicators in commercial receivers using this type of circuit. Alternatively, the meter may be mounted upside down, so that the needle moves toward the right with increased strength.

The circuit of figure 27B can frequently be used to advantage in a receiver where the cathode of one of the r-f or i-f amplifier stages runs directly to ground through the cathode bias resistor instead of running through a cathode-voltage gain control. In this case a 0-1 d-c milliammeter in conjunction with a resistor from 1000 to 3000 ohms can be used as shown as a signal-strength meter. With this circuit the meter will read backwards with increasing signal strength as in the circuit previously discussed.

Figure 27C is the circuit of a forward-reading S meter as is often used in communications receivers. The instrument is used in an unbalanced bridge circuit with the d-c plate resistance of one i-f tube as one leg of the bridge and with resistors for the other three legs. The value of the resistor R must be determined by trial and error and will be somewhere in the vicinity of 50,000 ohms. Sometimes the screen circuits of the r-f and i-f stages are taken from this point along with the screen-circuit voltage divider.

Electron-ray tubes (sometimes called "magic eyes") can also be used as indicators of relative signal strength in a circuit similar to that shown in figure 27D. A 6U5/6G5 tube should be used where the a-v-c voltage will be from 5 to 20 volts and a type 6E5 tube should be used when the a-v-c voltage will run from 2 to 8 volts.

Audio Amplifiers Audio amplifiers are employed in nearly all radio receivers. The audio amplifier stage or stages are usually of the Class A type, although Class AB push-pull stages are used in some receivers. The purpose of the audio amplifier is to bring the relatively weak signal from the detector up to a strength sufficient to operate a pair of headphones or a loud speaker. Either triodes, pentodes, or beam tetrodes may be used, the pentodes and beam tetrodes usually giving greater output. In some receivers, particularly those employing grid leak detection, it is possible to operate the headphones directly from the detector, without audio amplification. In such receivers, a single audio stage with a beam tetrode or pentode tube is ordinarily used to drive the loud speaker.

Most communications receivers, either home-constructed or factory-made, have a single-ended beam tetrode (such as a 6L6 or 6V6) or pentode (6F6 or 6K6-GT) in the audio output stage feeding the loudspeaker. If precautions are not taken such a stage will actually bring about a decrease in the effective signal-to-noise ratio of the receiver due to the rising high-frequency characteristic of such a stage when feeding a loud-speaker. One way of improving this condition is to place a mica or paper capacitor of approximately 0.003 μfd. capacitance across the primary of the output transformer. The use of a capacitor in this manner tends to make the load impedance seen by the plate of the output tube more constant over the audio-frequency range. The speaker and transformer will tend to present a rising impedance to the tube as the frequency increases, and the parallel capacitor will tend to make the total impedance more constant since it will tend to present a decreasing impedance with increasing audio frequency.

A still better way of improving the frequency characteristic of the output stage, and at the same time reducing the harmonic distortion, is to use shunt feedback from the plate of the output tube to the plate of a tube such as a 6SJ7 acting as an audio amplifier stage ahead of the output stage.

10-9 Noise Suppression

The problem of noise suppression confronts the listener who is located in places where interference from power lines, electrical appliances, and automobile ignition systems is troublesome. This noise is often of such intensity as to swamp out signals from desired stations.

There are two principal methods for reducing this noise:

(1) A-c line filters at the source of interference, if the noise is created by an electrical appliance.

(2) Noise-limiting circuits for the reduction, in the receiver itself, of interference of the type caused by automobile ignition systems.

Power Line Filters Many household appliances, such as electric mixers, heating pads, vacuum sweepers, refrigerators, oil burners, sewing machines, doorbells, etc., create an interference of an intermittent nature. The insertion of a line filter near the source of interference often will effect a complete cure. Filters for small appliances can consist of a 0.1-μfd. capacitor connected across the 110-volt a-c line. Two capacitors in series across the line, with the midpoint connected to ground, can be used in conjunction with ultraviolet ray machines, refrigerators, oil burner furnaces, and other more stubborn offenders. In severe cases of interference, additional filters in the form of heavy-duty r-f choke coils must be connected in series with the 110-volt a-c line on both sides of the line right at the interfering appliance.

Peak Noise Limiters Numerous noise-limiting circuits which are beneficial in overcoming key clicks, automobile ignition interference, and similar noise impulses have become popular. They operate on the principle that each individual noise pulse is of very short duration, yet of very high amplitude. The popping or clicking type of noise from electrical ignition systems may produce a signal having a peak value ten to twenty times as great as the incoming radio signal, but an average power much less than the signal.

As the duration of this type of noise peak is short, the receiver can be made inoperative during the noise pulse without the human ear detecting the total loss of signal. Some noise limiters actually *punch a hole* in the signal, while others merely *limit* the maximum peak signal which reaches the headphones or loudspeaker.

The noise peak is of such short duration that it would not be objectionable except for the fact that it produces an over-loading effect on the receiver, which increases its time constant. A sharp voltage peak will give a kick to the diaphragm of the headphones or speaker, and the momentum or inertia keeps the diaphragm in motion until the dampening of the diaphragm stops it. This movement produces a popping sound which may completely obliterate the desired signal. If the noise pulse can be limited to a peak amplitude equal to that of the desired signal, the resulting interference is practically negligible for moderately low repetition rates, such as ignition noise.

In addition, the i-f amplifier of the receiver will also tend to lengthen the duration of the noise pulses because the relatively high-Q i-f tuned circuits will *ring* or oscillate when excited by a sharp pulse, such as produced by ignition noise. The most effective noise limiter would be placed before the high-Q i-f tuned circuits. At this point the noise pulse is the sharpest and has not been degraded by passage through the i-f transformers. In addition, the pulse is eliminated before it can produce ringing effects in the i-f chain.

The Lamb Noise Limiter An i-f noise limiter is shown in figure 28. This is an adaptation of the Lamb noise silencer circuit. The i-f signal is fed into a double grid tube, such as a 6L7, and thence into the i-f chain. A 6AB7 high gain pentode is capacity coupled to the input of the i-f system. This auxiliary tube amplifies both signal and noise that is fed to it. It has a minimum of selectivity ahead of it so that it receives the true noise pulse before it is degraded by the i-f strip. A broadly tuned i-f transformer is used to couple the noise amplifier to a 6H6 noise rectifier. The gain of the noise amplifier is controlled by a potentiometer in the cathode of the 6AB7 noise amplifier. This potentiometer controls the gain of the noise amplifier

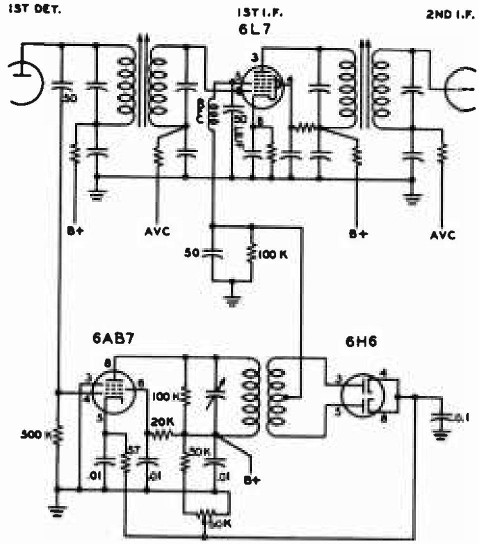


Figure 28
THE LAMB I-F NOISE SILENCER

stage and in addition sets the bias level on the 6H6 diode so that the incoming signal will not be rectified. Only noise peaks louder than the signal can overcome the resting bias of the 6H6 and cause it to conduct. A noise pulse rectified by the 6H6 is applied as a negative voltage to the control grid of the 6L7 i-f tube, disabling the tube, and punching a hole in the signal at the instant of the noise pulse. By varying the bias control of the noise limiter, the negative control voltage applied to the 6L7 may be adjusted until it is barely sufficient to overcome the noise impulses applied to the #1 control grid without allowing the modulation peaks of the carrier to become badly distorted.

The Bishop Noise Limiter Another effective i-f noise limiter is the Bishop limiter. This is a full-wave shunt type diode limiter applied to the primary of the last i-f transformer of a receiver. The limiter is self-biased and automatically adjusts itself to the degree of modulation of the received signal. The schematic of this limiter is shown in figure 29. The bias circuit time constant is determined by C_1 and the shunt resistance, which consists of R_1 and R_2 in series. The plate resistance of the last i-f tube and the capacity of C_1 determine the charging rate of the circuit. The limiter is disabled by opening S_1, which allows the bias to rise to the value of the i-f signal.

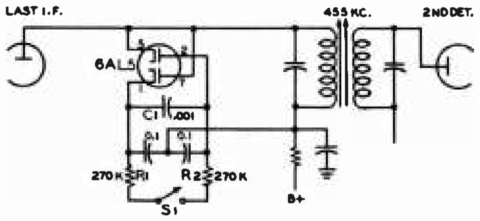


Figure 29
THE BISHOP I-F NOISE LIMITER

Audio Noise Limiters Some of the simplest and most practical peak limiters for radiotelephone reception employ one or two diodes either as shunt or series limiters in the audio system of the receiver. When a noise pulse exceeds a certain predetermined threshold value, the limiter diode acts either as a short or open circuit, depending upon whether it is used in a shunt or series circuit. The threshold is made to occur at a level high enough that it will not clip modulation peaks enough to impair voice intelligibility, but low enough to limit the noise peaks effectively.

Because the action of the peak limiter is needed most on very weak signals, and these usually are not strong enough to produce proper a-v-c action, a threshold setting that is correct for a strong phone signal is not correct for optimum limiting on very weak signals. For this reason the threshold control often is tied in with the a-v-c system so as to make the optimum threshold adjustment automatic instead of manual.

Suppression of impulse noise by means of an audio peak limiter is best accomplished at the very front end of the audio system, and for this reason the function of superheterodyne second detector and limiter often are combined in a composite circuit.

The amount of limiting that can be obtained is a function of the audio distortion that can be tolerated. Because excessive distortion will reduce the intelligibility as much as will background noise, the degree of limiting for which the circuit is designed has to be a compromise.

Peak noise limiters working at the second detector are much more effective when the i-f bandwidth of the receiver is broad, because a sharp i-f amplifier will lengthen the pulses by the time they reach the second detector, making the limiter less effective. V-h-f superheterodynes have an i-f bandwidth considerably wider than the minimum necessary for voice sidebands (to take care of drift and instability). Therefore, they are capable of better peak noise suppression than a standard communications receiver having an i-f bandwidth of perhaps 8 kc. Likewise, when a crystal filter is used on the "sharp" position an a-f peak limiter is of little benefit.

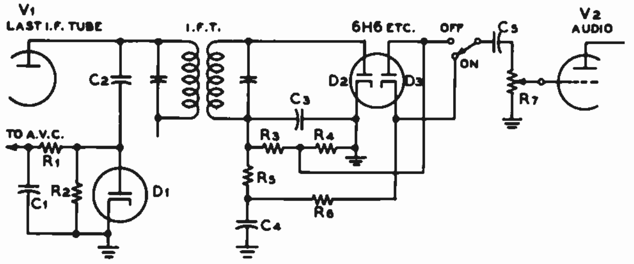
Practical Peak Noise Limiter Circuits Noise limiters range all the way from an audio stage running at very low screen or plate voltage, to elaborate affairs employing 5 or more tubes. Rather than attempt to show the numerous types, many of which are quite complex considering the results obtained, only two very similar types will be described. Either is just about as effective as the most elaborate limiter that can be constructed, yet requires the addition of but a single diode and a few resistors and capacitors over what would be employed in a good superheterodyne without a limiter. Both circuits, with but minor modifications in resistance and capacitance values, are incorporated in one form or another in different types of factory-built communications receivers.

Referring to figure 30, the first circuit shows a conventional superheterodyne second detector, a.v.c., and first audio stage with the addition of one tube element, D_3, which may be either a separate diode or part of a twin-diode as illustrated. Diode D_3 acts as a series gate, allowing audio to get to the grid of the a-f tube only so long as the diode is conducting. The diode is biased by a d-c voltage obtained in the same manner as a-v-c control voltage, the bias being such that pulses of short duration no longer conduct when the pulse voltage exceeds the carrier by approximately 60 per cent. This also clips voice modulation peaks, but not enough to impair intelligibility.

It is apparent that the series diode clips only *positive* modulation peaks, by limiting upward modulation to about 60 per cent. Negative or downward peaks are limited automatically to 100 per cent in the detector, because obviously the rectified voltage out of the diode detector cannot be less than zero. Limiting the downward peaks to 60 per cent or so instead of 100 per cent would result in but little improvement in noise reduction, and the results do not justify the additional components required.

It is important that the exact resistance values shown be used, for best results, and that 10 per cent tolerance resistors be used for R_3 and R_4. Also, the rectified carrier voltage developed across C_3 should be at least 5 volts for good limiting.

The limiter will work well on c-w telegraphy if the amplitude of beat frequency oscillator injection is not too high. Variable injection is to be preferred, adjustable from the front panel.



C_1—0.1-μfd. paper
C_2—50-μμfd. mica
C_3—100-μμfd. mica
C_4, C_5—0.01-μfd. paper
R_1, R_2—1 megohm, ½ watt
R_3, R_4—220,000 ohms, ½ watt
R_5, R_6—1 megohm, ½ watt
R_7—2-megohm potentiometer

Figure 30
NOISE LIMITER CIRCUIT, WITH ASSOCIATED A-V-C
This limiter is of the series type, and is self-adjusting to carrier strength for phone reception. For proper operation several volts should be developed across the secondary of the last i-f transformer (IFT) under carrier conditions.

If this feature is not provided, the b-f-o injection should be reduced to the lowest value that will give a satisfactory beat. When this is done, effective limiting and a good beat can be obtained by proper adjustment of the r-f and a-f gain controls. It is assumed, of course, that the a.v.c. is cut out of the circuit for c-w telegraphy reception.

Alternative Limiter Circuit The circuit of figure 31 is more effective than that shown in figure 30 under certain conditions and requires the addition of only one more resistor and one more capacitor than the other circuit. Also, this circuit involves a smaller loss in output level than the circuit of figure 30. This circuit can be used with equal effectiveness with a combined diode-triode or diode-pentode tube (6R7, 6SR7, 6Q7, 6SQ7 or similar diode-triodes, or 6B8, 6SF7, or similar diode-pentodes) as diode detector and first audio stage. However, a separate diode must be used for the noise limiter, D_2. This diode may be one-half of a 6H6, 6AL5, 7A6, etc., or it may be a triode connected 6J5, 6C4 or similar type.

Note that the return for the volume control must be made to the cathode of the detector diode (and not to ground) when a dual tube is used as combined second-detector first-audio. This means that in the circuit shown in figure 31 a connection will exist across the points where the "X" is shown on the diagram since a common cathode lead is brought out of the tube for D_1 and V_1. If desired, of course, a single dual diode may be used for D_1 and D_2 in this circuit as well as in the circuit of figure 30. Switching the limiter in and out with the switch S brings about no change in volume.

In any diode limiter circuit such as the ones shown in these two figures it is important that the mid-point of the heater potential for the noise-limiter diode be as close to ground potential as possible. This means that the center-tap of the heater supply for the tubes should be grounded wherever possible rather than grounding one side of the heater supply as is often done. Difficulty with hum pickup in the limiter circuit *may* be encountered when one side of the heater is grounded due to the high values of resistance necessary in the limiter circuit.

The circuit of figure 31 has been used with excellent success in several home-constructed receivers, and in the BC-312/BC-342 and BC-348 series of surplus communications receivers. It is also used in certain manufactured receivers.

An excellent check on the operation of the noise limiter in any communications receiver can be obtained by listening to the Loran signals in the 160-meter band. With the limiter out a sharp rasping buzz will be obtained when one of these stations is tuned in. With the noise limiter switched into the circuit the buzz should be greatly reduced and a low-pitched hum should be heard.

The Full-Wave Limiter The most satisafctory diode noise limiter is the series full-wave limiter, shown in figure 32. The positive noise peaks are clipped by diode A, the clipping level of which may be adjusted to clip at any modulation level between 25 per cent and 100 per cent. The negative noise peaks are clipped by diode B at a fixed level.

The TNS Limiter The *Twin Noise Squelch*, popularized by CQ magazine, is a combination of a diode noise clipper and an audio squelch tube. The squelch cir-

This circuit is of the self-adjusting type and gives less distortion for a given degree of modulation than the more common limiter circuits.

R_1, R_2—470K, ½ watt
R_3—100K, ½ watt
R_4, R_5—1 megohm, ½ watt
R_6—2-megohm potentiometer
C_1—0.00025 mica (approx.)
C_2—0.01-μfd. paper
C_3—0.01-μfd. paper
C_4—0.01-μfd. paper
D_1, D_2—6H6, 6AL5, 7A6, or diode sections of a 6S8-GT

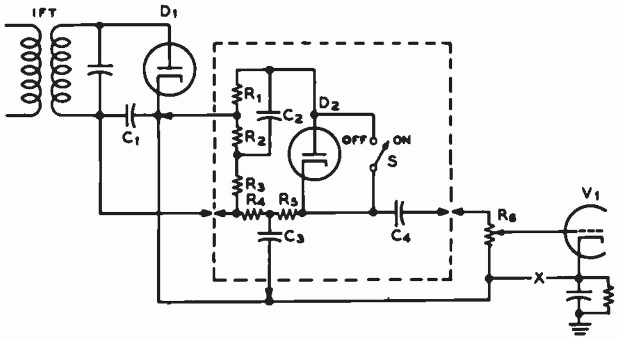


Figure 31
ALTERNATIVE NOISE LIMITER CIRCUIT

cuit is useful in eliminating the grinding background noise that is the residual left by the diode clipper. In figure 33, the setting of the 470K potentiometer determines the operating level of the squelch action and should be set to eliminate the residual background noise. Because of the low inherent distortion of the TNS, it may be left in the circuit at all times. As with other limiters, the TNS requires a high signal level at the second detector for maximum limiting effect.

10-10 Special Considerations in U-H-F Receiver Design

Transmission Line Circuits At increasingly higher frequencies, it becomes progressively more difficult to obtain a satisfactory amount of selectivity and impedance from an ordinary coil and capacitor used as a resonant circuit. On the other hand, quarter wavelength sections of parallel conductors or concentric transmission line are not only more efficient but also become of practical dimensions.

Tuning Short Lines Tubes and tuning capacitors connected to the open end of a transmission line provide a capacitance that makes the resonant length less than a quarter wave-length. The amount of shortening for a specified capacitive reactance is determined by the surge impedance of the line

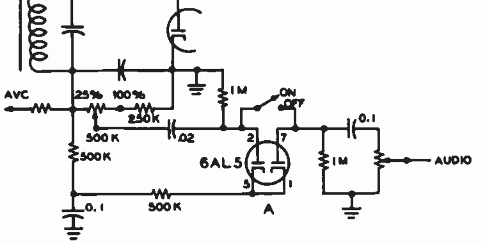


Figure 32
THE FULL-WAVE SERIES AUDIO NOISE LIMITER

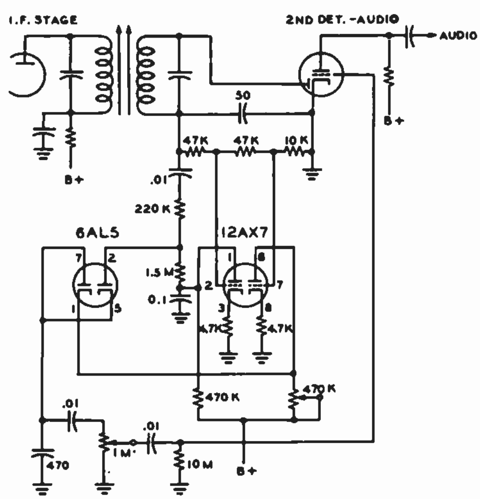


Figure 33
THE TNS AUDIO NOISE LIMITER

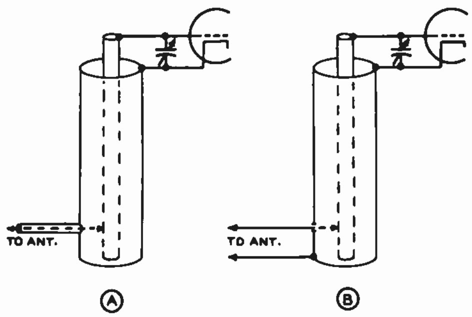


Figure 34
COUPLING AN ANTENNA TO A COAXIAL-RESONANT CIRCUIT
(A) shows the recommended method for coupling a coaxial line to a coaxial resonant circuit. (B) shows an alternative method for use with an open-wire type of antenna feed line.

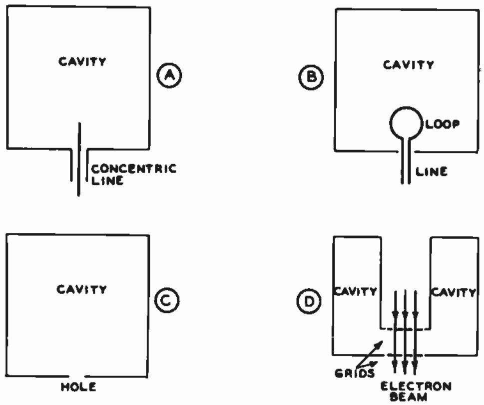


Figure 35
METHODS OF EXCITING A RESONANT CAVITY

section. It is given by the equation for resonance:

$$\frac{1}{2\,\pi\, f C} = Z_0 \tan l$$

in which $\pi = 3.1416$, f is the frequency, C the capacitance, Z_0 the surge impedance of the line, and tan l is the tangent of the electrical length in degrees.

The capacitive reactance of the capacitance across the end is $1/(2\pi\, f\, C)$ ohms. For resonance, this must equal the surge impedance of the line times the tangent of its electrical length (in degrees, where 90° equals a quarter wave). It will be seen that twice the capacitance will resonate a line if its surge impedance is halved; also that a given capacitance has twice the loading effect when the frequency is doubled.

Coupling Into Lines and Coaxial Circuits It is possible to couple into a parallel-rod line by tapping directly on one or both rods, preferably through blocking capacitors if any d.c. is present. More commonly, however, a *hairpin* is inductively coupled at the shorting bar end, either to the bar or to the two rods, or both. This normally will result in a balanced load. Should a loop unbalanced to ground be coupled in, any resulting unbalance reflected into the rods can be reduced with a simple Faraday screen, made of a few parallel wires placed between the hairpin loop and the rods. These should be soldered at only one end and grounded.

An unbalanced tap on a coaxial resonant circuit can be made directly on the inner conductor at the point where it is properly matched (figure 34). For low impedances, such as a concentric line feeder, a small one-half turn loop can be inserted through a hole in the outer conductor of the coaxial circuit, being in effect a half of the hairpin type recommended for coupling balanced feeders to coaxial resonant lines. The size of the loop and closeness to the inner conductor determines the impedance matching and loading. Such loops coupled in near the shorting disc do not alter the tuning appreciably, if not overcoupled.

Resonant Cavities A *cavity* is a closed resonant chamber made of metal. It is known also as a *rhumbatron.* The cavity, having both inductance and capacitance, supersedes coil-capacitor and capacitance-loaded transmission-line tuned circuits at extremely high frequencies where conventional L and C components, of even the most refined design, prove impractical because of the tiny electrical and physical dimensions they must have. Microwave cavities have high Q factors and are superior to conventional tuned circuits. They may be employed in the manner of an absorption wavemeter or as the tuned circuit in other r-f test instruments, and in microwave transmitters and receivers.

Resonant cavities usually are closed on all sides and all of their walls are made of electrical conductor. However, in some forms, small openings are present for the purpose of excitation. Cavities have been produced in several shapes including the plain sphere,

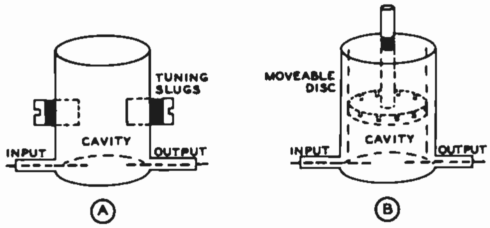


Figure 36
TUNING METHODS FOR CYLINDRICAL RESONANT CAVITIES

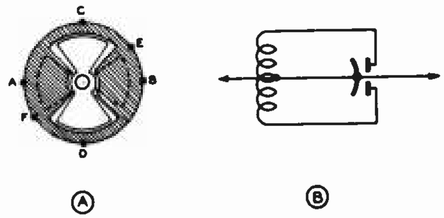


Figure 37
THE BUTTERFLY RESONANT CIRCUIT
Shown at (A) is the physical appearance of the butterfly circuit as used in the v-h-f and lower u-h-f range. (B) shows an electrical representation of the circuit.

dimpled sphere, sphere with reentrant cones of various sorts, cylinder, prism (including cube), ellipsoid, ellipsoid-hyperboloid, doughnut-shape, and various reentrant types. In appearance, they resemble in their simpler forms metal boxes or cans.

The cavity actually is a linear circuit, but one which is superior to a conventional coaxial resonator in the s-h-f range. The cavity resonates in much the same manner as does a barrel or a closed room with reflecting walls.

Because electromagnetic energy, and the associated electrostatic energy, oscillates to and fro inside them in one mode or another, resonant cavities resemble wave guides. The mode of operation in a cavity is affected by the manner in which micro-wave energy is injected. A cavity will resonate to a large number of frequencies, each being associated with a particular mode or standing-wave pattern. The lowest mode (lowest frequency of operation) of a cavity resonator normally is the one used.

The resonant frequency of a cavity may be varied, if desired, by means of movable plungers or plugs, as shown in figure 36A, or a movable metal disc (see figure 36B). A cavity that is too small for a given wavelength will not oscillate.

The resonant frequencies of simple spherical, cylindrical, and cubical cavities may be calculated simply for one particular mode. Wavelength and cavity dimensions (in centimeters) are related by the following simple resonance formulae:

For Cylinder $\lambda_r = 2.6 \times$ radius
" Cube $\lambda_r = 2.83 \times$ half of 1 side
" Sphere $\lambda_r = 2.28 \times$ radius

Butterfly Circuit Unlike the cavity resonator, which in its conventional form is a device which can tune over a relatively narrow band, the butterfly circuit is a tunable resonator which permits coverage of a fairly wide u-h-f band. The butterfly circuit is very similar to a conventional coil-variable capacitor combination, except that both inductance and capacitance are provided by what appears to be a variable capacitor alone. The Q of this device is somewhat less than that of a concentric-line tuned circuit but is entirely adequate for numerous applications.

Figure 37A shows construction of a single butterfly section. The butterfly-shaped rotor, from which the device derives its name, turns in relation to the unconventional stator. The two groups of stator "fins" or sectors are in effect joined together by a semi-circular metal band, integral with the sectors, which provides the circuit inductance. When the rotor is set to fill the loop opening (the position in which it is shown in figure 37A), the circuit inductance and capacitance are reduced to minimum. When the rotor occupies the position indicated by the dotted lines, the inductance and capacitance are at maximum. The tuning range of practical butterfly circuits is in the ratio of 1.5:1 to 3.5:1.

Direct circuit connections may be made to points A and B. If balanced operation is desired, either point C or D will provide the electrical mid-point. Coupling may be effected by means of a small singleturn loop placed near point E or F. The butterfly thus permits continuous variation of both capacitance and inductance, as indicated by the equivalent circuit in figure 37B, while at the same time eliminating all pigtails and wiping contacts.

Several butterfly sections may be stacked in parallel in the same way that variable capacitors are built up. In stacking these sections, the effect of adding inductances in parallel is to lower the total circuit inductance, while the addition of stators and rotors raises the total capacitance, as well as the ratio of maximum to minimum capacitance.

Butterfly circuits have been applied specifically to oscillators for transmitters, superheterodyne receivers, and heterodyne frequency meters in the 100-1000-Mc. frequency range.

Receiver Circuits The types of resonant circuits described in the previous paragraphs have largely replaced conventional coil-capacitor circuits in the range above 100 Mc. Tuned short lines and butterfly circuits are used in the range from about 100 Mc. to perhaps 3500 Mc., and above about 3500 Mc. resonant cavities are used almost exclusively. The resonant cavity is also quite generally employed in the 2000-Mc. to 3500-Mc. range.

In a properly designed receiver, thermal agitation in the first tuned circuit is amplified by subsequent tubes and predominates in the output. For good signal-to-set-noise ratio, therefore, one must strive for a high-gain low-noise r-f stage. Hiss can be held down by giving careful attention to this point. A mixer has about 0.3 of the gain of an r-f tube of the same type; so it is advisable to precede a mixer by an efficient r-f stage. It is also of some value to have good r-f selectivity before the first detector in order to reduce noises produced by beating noise at one frequency against noise at another, to produce noise at the intermediate frequency in a superheterodyne.

The frequency limit of a tube is reached when the shortest possible external connections are used as the tuned circuit, except for abnormal types of oscillation. Wires or sizeable components are often best considered as sections of transmission lines rather than as simple resistances, capacitances, or inductances.

So long as small triodes and pentodes will operate normally, they are generally preferred as v-h-f tubes over other receiving methods that have been devised. However, the input capacitance, input conductance, and transit time of these tubes limit the upper frequency at which they may be operated. The input resistance, which drops to a low value at very short wave-lengths, limits the stage gain and broadens the tuning.

V-H-F Tubes The first tube in a v-h-f receiver is most important in raising the signal above the noise generated in successive stages, for which reason small v-h-f types are definitely preferred.

Tubes employing the conventional grid-controlled and diode rectifier principles have been modernized, through various expedients, for operation at frequencies as high, in some new types, as 4000 Mc. Beyond that frequency, electron transit time becomes the limiting factor and new principles must be enlisted. In general, the improvements embodied in existing tubes have consisted of (1) reducing electrode spacing to cut down electron transit time, (2) reducing electrode areas to decrease interelectrode capacitances, and (3) shortening of electrode leads either by mounting the electrode assembly close to the tube base or by bringing the leads out directly through the glass envelope at nearby points. Through reduction of lead inductance and interelectrode capacitances, input and output resonant frequencies due to tube construction have been increased substantially.

Tubes embracing one or more of the features just outlined include the later loctal types, high-frequency acorns, button-base types, and the lighthouse types. Type 6J4 button-base triode will reach 500 Mc. Type 6F4 acorn triode is recommended for use up to 1200 Mc. Type 1A3 button-base diode has a resonant frequency of 1000 Mc., while type 9005 acorn diode resonates at 1500 Mc. Lighthouse type 2C40 can be used at frequencies up to 3500 Mc. as an oscillator.

Crystal Rectifiers More than two decades have passed since the crystal (mineral) rectifier enjoyed widespread use in radio receivers. Low-priced tubes completely supplanted the fragile and relatively insensitive crystal detector, although it did continue for a few years as a simple meter rectifier in absorption wavemeters after its demise as a receiver component.

Today, the crystal detector is of new importance in microwave communication. It is being employed as a detector and as a mixer in receivers and test instruments used at extremely high radio frequencies. At some of the frequencies employed in microwave operations, the crystal rectifier is the only satisfactory detector or mixer. The chief advantages of the crystal rectifier are very low capacitance, relative freedom from transit-time difficulties, and its two-terminal nature. No batteries or a-c power supply are required for its operation.

The crystal detector consists essentially of a small piece of silicon or germanium mounted in a base of low-melting-point alloy and contacted by means of a thin, springy feeler wire known as the *cat whisker*. This arrangement is shown in figure 38A.

The complex physics of crystal rectification is beyond the scope of this discussion. It is sufficient to state that current flows from several hundred to several thousand times more readily in one direction through the contact of cat whisker and crystal than in the opposite direction. Consequently, an alternating current (including one of microwave frequency) will

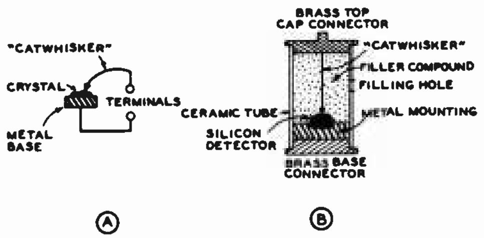


Figure 38
THE MICROWAVE CRYSTAL DIODE
(A) shows the essentials of a crystal diode, while (B) is a sketch to illustrate the construction of the common microwave crystal diode.

be rectified by the crystal detector. The load, through which the rectified currents flow, may be connected in series or shunt with the crystal, although the former connection is most generally employed.

The basic arrangement of a modern fixed crystal detector developed during World War II for microwave work, particularly radar, is shown in figure 38B. Once the cat whisker of this unit is set at the factory to the most sensitive spot on the surface of the silicon crystal and its pressure is adjusted, a filler compound is injected through the filling hole to hold the cat whisker permanently in position.

10-11 Receiver Adjustment

A simple regenerative receiver requires little adjustment other than that necessary to insure correct tuning and smooth regeneration over some desired range. Receivers of the tuned radio-frequency type and superheterodynes require precise alignment to obtain the highest possible degree of selectivity and sensitivity.

Good results can be obtained from a receiver only when it is properly aligned and adjusted. The most practical technique for making these adjustments is given below.

Instruments A very small number of instruments will suffice to check and align a communications receiver, the most important of these testing units being a modulated oscillator and a d-c and a-c voltmeter. The meters are essential in checking the voltage applied at *each* circuit point from the power supply. If the a-c voltmeter is of the oxide-rectifier type, it can be used, in addition, as an output meter when connected across the receiver output when tuning to a modulated signal. If the signal is a steady tone, such as from a test oscillator, the output meter will indicate the value of the detected signal. In this manner, alignment results may be visually noted on the meter.

T-R-F Receiver Alignment Alignment procedure in a multistage t-r-f receiver is exactly the same as aligning a single stage. If the detector is regenerative, each preceding stage is successively aligned while keeping the detector circuit tuned to the test signal, the latter being a station signal or one locally generated by a test oscillator loosely coupled to the antenna lead. During these adjustments, the r-f amplifier gain control is adjusted for maximum sensitivity, assuming that the r-f amplifier is stable and does not oscillate. Often a sensitive receiver can be roughly aligned by tuning for maximum noise pickup.

Superheterodyne Alignment Aligning a superhet is a detailed task requiring a great amount of care and patience. It should never be undertaken without a thorough understanding of the involved job to be done and then only when there is abundant time to devote to the operation. There are no short cuts; every circuit must be adjusted individually and accurately if the receiver is to give peak performance. The precision of each adjustment is dependent upon the accuracy with which the preceding one was made.

Superhet alignment requires (1) a good signal generator (modulated oscillator) covering the radio and intermediate frequencies and equipped with an attenuator; (2) the necessary socket wrenches, screwdrivers, or "neutralizing tools" to adjust the various i-f and r-f trimmer capacitors; and (3) some convenient type of tuning indicator, such as a copper-oxide or electronic voltmeter.

Throughout the alignment process, unless specifically stated otherwise, the r-f gain control must be set for maximum output, the beat oscillator switched off, and the a.v.c. turned off or shorted out. When the signal output of the receiver is excessive, either the attenuator or the a-f gain control may be turned down, but never the r-f gain control.

I-F Alignment After the receiver has been given a rigid electrical and mechanical inspection, and any faults which may have been found in wiring or the selection and assembly of parts corrected, the i-f amplifier may be aligned as the first step in the checking operations.

With the signal generator set to give a modulated signal on the frequency at which the i-f amplifier is to operate, clip the "hot" output lead from the generator to the last i-f stage through a small fixed capacitor to the control grid. Adjust both trimmer capacitors in the last i-f transformer (the one between the last i-f amplifier and the second detector) to resonance as indicated by maximum deflection of the output meter.

Each i-f stage is adjusted in the same manner, moving the hot lead, stage by stage, back toward the front end of the receiver and backing off the attenuator as the signal strength increases in each new position. The last adjustment will be made to the first i-f transformer, with the hot signal generator lead connected to the control grid of the mixer. Occasionally it is necessary to disconnect the mixer grid lead from the coil, grounding it through a 1,000- or 5,000-ohm resistor, and coupling the signal generator through a small capacitor to the grid.

When the last i-f adjustment has been completed, it is good practice to go back through the i-f channel, re-peaking all of the transformers. It is imperative that this recheck be made in sets which do not include a crystal filter, and where the simple alignment of the i-f amplifier to the generator is final.

I-F with Crystal Filter There are several ways of aligning an i-f channel which contains a crystal-filter circuit. However, the following method is one which has been found to give satisfactory results in every case: An unmodulated signal generator capable of tuning to the frequency of the filter crystal in the receiver is coupled to the grid of the stage which precedes the crystal filter in the receiver. Then, with the crystal filter switched in, the signal generator is tuned *slowly* to find the frequency where the crystal peaks. The receiver "S" meter may be used as the indicator, and the sound heard from the loudspeaker will be of assistance in finding the point. When the frequency at which the crystal peaks has been found, all the i-f transformers in the receiver should be touched up to peak at that frequency.

B-F-O Adjustment Adjusting the beat oscillator on a receiver that has no front panel adjustment is relatively simple. It is only necessary to tune the receiver to resonance with any signal, as indicated by the tuning indicator, and then turn on the b.f.o. and set its trimmer (or trimmers) to produce the desired beat note. Setting the beat oscillator in this way will result in the beat note being stronger on one "side" of the signal than on the other, which is what is desired for c-w reception. The b.f.o. should *not* be set to *zero beat* when the receiver is tuned to resonance with the signal, as this will cause an equally strong beat to be obtained on both sides of resonance.

Front-End Alignment Alignment of the front end of a home-constructed receiver is a relatively simple process, consisting of first getting the oscillator to cover the desired frequency range and then of peaking the various r-f circuits for maximum gain. However, if the frequency range covered by the receiver is very wide a fair amount of cut and try will be required to obtain satisfactory tracking between the r-f circuits and the oscillator. Manufactured communications receivers should always be tuned in accordance with the instructions given in the maintenance manual for the receiver.

CHAPTER ELEVEN

Generation of Radio Frequency Energy

A radio communication or broadcast transmitter consists of a source of radio frequency power, or *carrier;* a system for *modulating* the carrier whereby voice or telegraph keying or other modulation is superimposed upon it; and an antenna system, including feed line, for *radiating* the intelligence-carrying radio frequency power. The power supply employed to convert primary power to the various voltages required by the r-f and modulator portions of the transmitter may also be considered part of the transmitter.

Voice modulation usually is accomplished by varying either the amplitude or the frequency of the radio frequency carrier in accordance with the components of intelligence to be transmitted.

Radiotelegraph modulation (keying) normally is accomplished either by interrupting, shifting the frequency of, or superimposing an audio tone on the radio-frequency carrier in accordance with the dots and dashes to be transmitted.

The complexity of the radio-frequency generating portion of the transmitter is dependent upon the power, order of stability, and frequency desired. An oscillator feeding an antenna directly is the simplest form of radio-frequency generator. A modern high-frequency transmitter, on the other hand, is a very complex generator. Such an equipment usually comprises a very stable crystal-controlled or self-controlled oscillator to stabilize the output frequency, a series of frequency multipliers, one or more amplifier stages to increase the power up to the level which is desired for feeding the antenna system, and a filter system for keeping the harmonic energy generated in the transmitter from being fed to the antenna system.

11-1 Self-Controlled Oscillators

In Chapter Four, it was explained that the amplifying properties of a tube having three or more elements give it the ability to generate an alternating current of a frequency determined by the components associated with it. A vacuum tube operated in such a circuit is called an *oscillator,* and its function is essentially to convert direct current into radio-frequency alternating current of a predetermined frequency.

Oscillators for controlling the frequency of conventional radio transmitters can be divided into two general classes: self-controlled and crystal-controlled.

There are a great many types of self-controlled oscillators, each of which is best suited

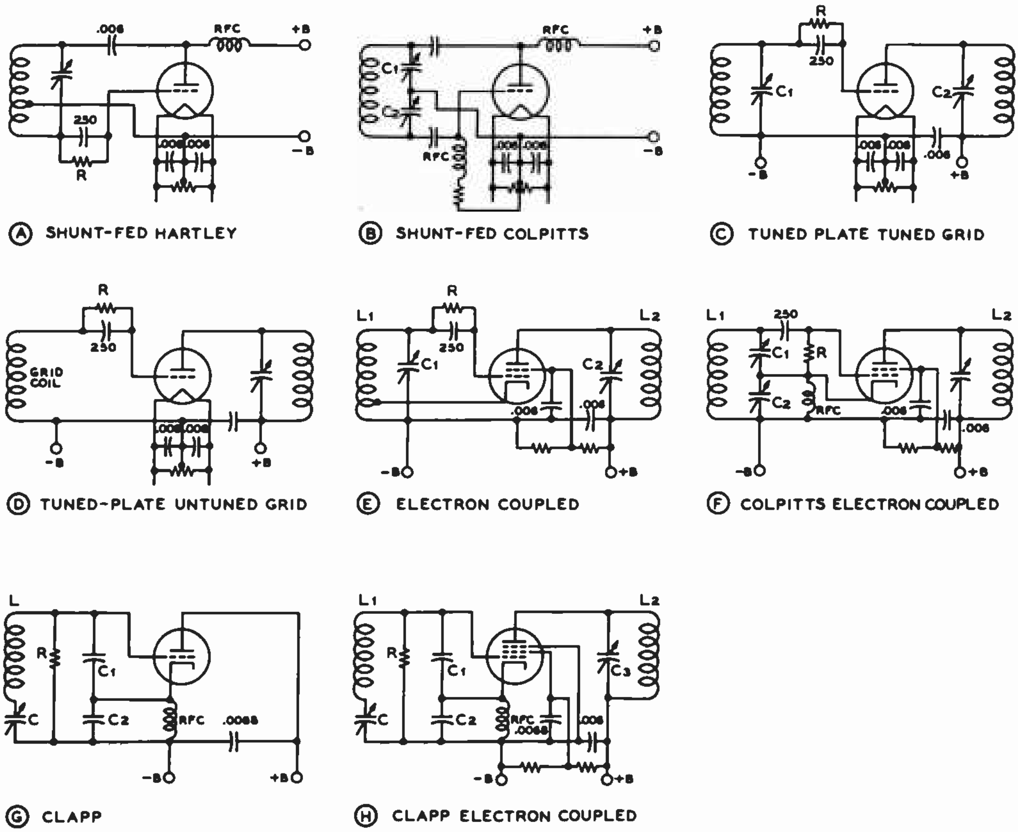


Figure 1

COMMON TYPES OF SELF-EXCITED OSCILLATORS

Fixed capacitor values are typical, but will vary somewhat with the application. In the Clapp oscillator circuits (G) and (H), capacitors C_1 and C_2 should have a reactance of 50 to 100 ohms at the operating frequency of the oscillator. Tuning of these two oscillators is accomplished by capacitor C. In the circuits of (E), (F), and (H), tuning of the tank circuit in the plate of the oscillator tube will have relatively small effect on the frequency of oscillation. The plate tank circuit also may, if desired, be tuned to a harmonic of the oscillation frequency, or a broadly resonant circuit may be used in this circuit position.

to a particular application. They can further be subdivided into the classifications of: negative-grid oscillators, electron-orbit oscillators, negative-resistance oscillators, velocity modulation oscillators, and magnetron oscillators.

Negative-Grid Oscillators A negative-grid oscillator is essentially a vacuum-tube amplifier with a sufficient portion of the output energy coupled back into the input circuit to sustain oscillation. The control grid is biased negatively with respect to the cathode. Common types of negative-grid oscillators are diagrammed in figure 1.

The Hartley Illustrated in figure 1 (A) is the oscillator circuit which finds the most general application at the present time; this circuit is commonly called the Hartley. The operation of this oscillator will be described as an index to the operation of all negative-grid oscillators; the only real difference between the various circuits is the manner in which energy for excitation is coupled from the plate to the grid circuit.

When plate voltage is applied to the Hartley oscillator shown at (A), the sudden flow of plate current accompanying the application of plate voltage will cause an electro-magnetic field to be set up in the vicinity of the coil. The building-up of this field will cause a potential drop to appear from turn-to-turn along the coil. Due to the inductive coupling between the portion of the coil in which the plate current is flowing and the grid portion, a potential will be induced in the grid portion.

Since the cathode tap is between the grid and plate ends of the coil, the induced grid voltage acts in such a manner as to increase further the plate current to the tube. This action will continue for a short period of time determined by the inductance and capacitance of the tuned circuit, until the *flywheel effect* of the tuned circuit causes this action to come to a maximum and then to reverse itself. The plate current then decreases, the magnetic field around the coil also decreasing, until a minimum is reached, when the action starts again in the original direction and at a greater amplitude than before. The amplitude of these oscillations, the frequency of which is determined by the coil-capacitor circuit, will increase in a very short period of time to a limit determined by the plate voltage of the oscillator tube.

The Colpitts Figure 1 (B) shows a version of the Colpitts oscillator. It can be seen that this is essentially the same circuit as the Hartley except that the ratio of a pair of capacitances in series determines the effective cathode tap, instead of actually using a tap on the tank coil. Also, the net capacitance of these two capacitors comprises the tank capacitance of the tuned circuit. This oscillator circuit is somewhat less susceptible to parasitic (spurious) oscillations than the Hartley.

For best operation of the Hartley and Colpitts oscillators, the voltage from grid to cathode, determined by the tap on the coil or the setting of the two capacitors, normally should be from 1/3 to 1/5 that appearing between plate and cathode.

The T.P.T.G. The tuned-plate tuned-grid oscillator illustrated at (C) has a tank circuit in both the plate and grid circuits. The feedback of energy from the plate to the grid circuits is accomplished by the plate-to-grid inter-electrode capacitance within the tube. The necessary phase reversal in feedback voltage is provided by tuning the grid tank capacitor to the low side of the desired frequency and the plate capacitor to the high side. A broadly resonant coil may be substituted for the grid tank to form the *T.N.T.* oscillator shown at (D).

Electron-Coupled Oscillators In any of the oscillator circuits just described it is possible to take energy from the oscillator circuit by coupling an external load to the tank circuit. Since the tank circuit determines the frequency of oscillation of the tube, any variations in the conditions of the external circuit will be coupled back into the frequency determining portion of the oscillator. These variations will result in frequency instability.

The frequency determining portion of an oscillator may be coupled to the load circuit only by an electron stream, as illustrated in (E) and (F) of figure 1. When it is considered that the screen of the tube acts as the plate to the oscillator circuit, the plate merely acting as a coupler to the load, then the similarity between the cathode-grid-screen circuit of these oscillators and the cathode-grid-plate circuits of the corresponding prototype can be seen.

The electron-coupled oscillator has good stability with respect to load and voltage variation. Load variations have a relatively small effect on the frequency, since the only coupling between the oscillating circuit and the load is through the electron stream flowing through the other elements to the plate. The plate is electrostatically shielded from the oscillating portion by the bypassed screen.

The stability of the e.c.o. with respect to variations in supply voltages is explained as follows: The frequency will shift in one direction with an increase in screen voltage, while an increase in plate voltage will cause it to shift in the other direction. By a proper proportioning of the resistors that comprise the voltage divider supplying screen voltage, it is possible to make the frequency of the oscillator substantially independent of supply voltage variations.

The Clapp Oscillator A relatively new type of oscillator circuit which is capable of giving excellent frequency stability is illustrated in figure 1G. Comparison between the more standard circuits of figure 1A through 1F and the Clapp oscillator circuits of figures 1G and 1H will immediately show one marked difference: the tuned circuit which controls the operating frequency in the Clapp oscillator is *series* resonant, while in all the more standard oscillator circuits the frequency controlling circuit is parallel resonant. Also, the capacitors C_1 and C_2 are relatively large in terms of the usual values for a Colpitts oscillator. In fact, the value of capacitors C_1 and C_2 will be in the vicinity of 0.001 μfd. to 0.0025 μfd. for an oscillator which is to be operated in the 1.8-Mc. band.

The Clapp oscillator operates in the following manner: at the resonant frequency of the oscillator tuned circuit (L, C) the impedance of this circuit is at minimum (since it operates in series resonance) and maximum current flows through it. Note however, that C_1 and C_2 also are included within the current path for the series resonant circuit, so that at the frequency of resonance an appreciable voltage drop appears across these capacitors. The voltage drop appearing across C_1 is applied to the grid of the oscillator tube as excitation, while the amplified output of the oscillator tube appears across C_2 as the driving power to keep the circuit in oscillation.

Capacitors C_1 and C_2 should be made as large in value as possible, while still permitting the circuit to oscillate over the full tuning range of C. The larger these capacitors are made, the smaller will be the coupling between the oscillating circuit and the tube, and consequently the better will be oscillator stability with respect to tube variations. High G_m tubes such as the 6AC7, 6AG7, and 6CB6 will permit the use of larger values of capacitance at C_1 and C_2 than will more conventional tubes such as the 6SJ7, 6V6, and such types. In general it may be said that the reactance of capacitors C_1 and C_2 should be on the order of 40 to 120 ohms at the operating frequency of the oscillator—with the lower values of reactance going with high-G_m tubes and the higher values being necessary to permit oscillation with tubes having G_m in the range of 2000 micromhos such as the 6SJ7.

It will be found that the Clapp oscillator will have a tendency to vary in power output over the frequency range of tuning capacitor C. The output will be greatest where C is at its largest setting, and will tend to fall off with C at minimum capacitance. In fact, if capacitors C_1 and C_2 have too large a value the circuit will stop oscillation near the *minimum* capacitance setting of C. Hence it will be necessary to use a slightly *smaller* value of capacitance at C_1 and C_2 (to provide an increase in the capacitive reactance at this point), or else the frequency range of the oscillator must be restricted by paralleling a fixed capacitor across C so that its effective capacitance at minimum setting will be increased to a value which will sustain oscillation.

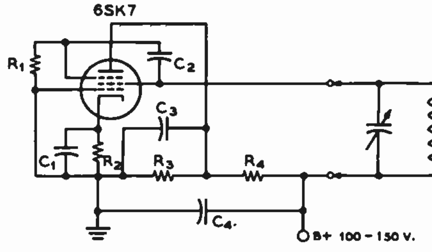
In the triode Clapp oscillator, such as shown at figure 1G, output voltage for excitation of an amplifier, doubler, or isolation stage normally is taken from the cathode of the oscillator tube by capacitive coupling to the grid of the next tube. However, where greater isolation of succeeding stages from the oscillating circuit is desired, the electron-coupled Clapp oscillator diagrammed in figure 1H may be used. Output then may be taken from the plate circuit of the tube by capacitive coupling with either a tuned circuit, as shown, or with an r-f choke or a broadly resonant circuit in the plate return. Alternatively, energy may be coupled from the output circuit L_2-C_3 by link coupling. The considerations with regard to C_1, C_2, and the grid tuned circuit are the same as for the triode oscillator arrangement of figure 1G.

Negative Resistance Oscillators Negative-resistance oscillators often are used when unusually high frequency stability is desired, as in a frequency meter. The *dynatron* of a few years ago and the newer *transitron* are examples of oscillator circuits which make use of the negative resistance characteristic between different elements in some multi-grid tubes.

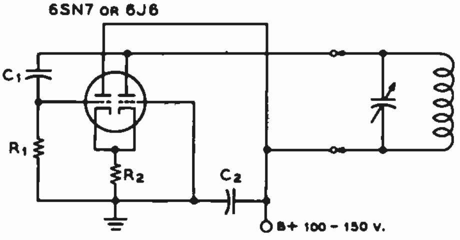
In the dynatron, the negative resistance is a consequence of secondary emission of electrons from the plate of a tetrode tube. By a proper proportioning of the electrode voltage, an increase in screen voltage will cause a decrease in screen current, since the increased screen voltage will cause the screen to attract a larger number of the secondary electrons emitted by the plate. Since the net screen current flowing from the screen supply will be decreased by an increase in screen voltage, it is said that the screen circuit presents a negative resistance.

If any type of tuned circuit, or even a resistance-capacitance circuit, is connected in series with the screen, the arrangement will oscillate—provided, of course, that the external circuit impedance is greater than the negative resistance. A negative resistance effect similar to the dynatron is obtained in the *transitron* circuit, which uses a pentode with the suppressor coupled to the screen. The negative resistance in this case is obtained from a combination of secondary emission and inter-electrode coupling, and is considerably more stable than that obtained from uncontrolled secondary emission alone in the dynatron. A representative transitron oscillator circuit is shown in figure 2.

The chief distinction between a conventional *negative grid oscillator* and a *negative resistance oscillator* is that in the former the tank circuit must act as a phase inverter in order to permit the amplification of the tube to act as a negative resistance, while in the latter the tube acts as its own phase inverter. Thus a negative resistance oscillator requires only an untapped coil and a single capacitor



Ⓐ TRANSITRON OSCILLATOR



Ⓑ CATHODE COUPLED OSCILLATOR

Figure 2

TWO-TERMINAL OSCILLATOR CIRCUITS

Both circuits may be used for an audio oscillator or for frequencies into the v-h-f range simply by placing a tank circuit tuned to the proper frequency where indicated on the drawing. Recommended values for the components are given below for both oscillators.

TRANSITION OSCILLATOR
C_1—0.01-μfd. mica for r.f. 10-μfd. elect. for a.f.
C_2—0.00005-μfd. mica for r.f. 0.1-μfd. paper for a.f.
C_3—0.003-μfd. mica for r.f. 0.5-μfd. paper for a.f.
C_4—0.01-μfd. mica for r.f. 8-μfd. elect. for a.f.
R_1—220K ½-watt carbon
R_2—1800 ohms ½-watt carbon
R_3—22K 2-watt carbon
R_4—22K 2-watt carbon

CATHODE-COUPLED OSCILLATOR
C_1—0.00005-μfd. mica for r.f. 0.1-μfd. paper for audio
C_2—0.003-μfd. mica for r.f. 8-μfd. elect. for audio
R_1—47K ½-watt carbon
R_2—1K 1-watt carbon

as the frequency determining tank circuit, and is classed as a *two terminal oscillator.* In fact, the time constant of an R/C circuit may be used as the frequency determining element and such an oscillator is rather widely used as a tunable audio frequency oscillator.

The Franklin Oscillator The Franklin oscillator makes use of two cascaded tubes to obtain the negative-resistance effect (figure 3). The tubes may be either a pair of triodes, tetrodes, or pentodes, a dual triode, or a combination of a triode and a multigrid tube. The chief advantage of this oscillator circuit is that the frequency determining tank only has two terminals, and one side of the circuit is grounded.

The second tube acts as a phase inverter to give an effect similar to that obtained with the dynatron or transitron, except that the effective transconductance is much higher. If the tuned circuit is omitted or is replaced by a resistor, the circuit becomes a relaxation oscillator or a multivibrator.

Oscillator Stability The Clapp oscillator has proved to be inherently the most stable of all the oscillator circuits discussed above, since minimum coupling between the oscillator tube and its associated tuned circuit is possible. However, this inherently good stability is with respect to tube variations; instability of the tuned circuit with respect to vibration or temperature will of course have as much effect on the frequency of oscillation as with any other type of oscillator circuit. Solid mechanical construction of the components of the oscillating circuit, along with a small negative-coefficient compensating capacitor included as an element of the tuned circuit, usually will afford an adequate degree of oscillator stability.

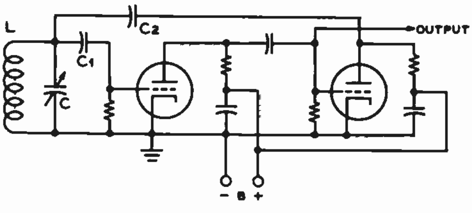


Figure 3

THE FRANKLIN OSCILLATOR CIRCUIT

A separate phase inverter tube is used in this oscillator to feed a portion of the output back to the input in the proper phase to sustain oscillation. The values of C_1 and C_2 should be as small as will permit oscillations to be sustained over the desired frequency range.

V.F.O. Transmitter Controls When used to control the frequency of a transmitter in which there are stringent limitations on frequency tolerance, several precautions are taken to ensure that a variable frequency oscillator will stay on frequency. The oscillator is fed from a voltage regulated power supply, uses a well designed and temperature compensated tank circuit, is of rugged mechanical construction to avoid the effects of shock and vibration, is protected against excessive changes in ambient room temperature, and is isolated from feedback or stray coupling from other portions of the transmitter by shielding, filtering of voltage supply leads, and incorporation of one or more buffer-amplifier stages. In a high power transmitter a small amount of stray coupling from the final amplifier to the oscillator can produce appreciable degradation of the oscillator stability if both are on the same frequency. Therefore, the oscillator usually is operated on a subharmonic of the transmitter output frequency, with one or more frequency multipliers between the oscillator and final amplifier.

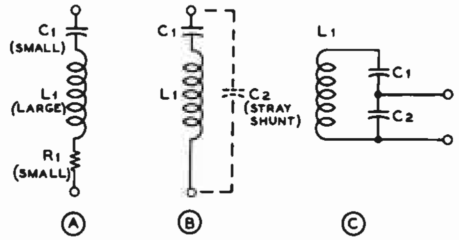


Figure 4

EQUIVALENT ELECTRICAL CIRCUIT OF QUARTZ PLATE IN A HOLDER

At (A) is shown the equivalent series-resonant circuit of the crystal itself, at (B) is shown how the shunt capacitance of the holder electrodes and associated wiring affects the circuit to the combination circuit of (C) which exhibits both series resonance and parallel resonance (anti-resonance), the separation in frequency between the two modes being very small and determined by the ratio of C_1 to C_2.

11-2 Quartz Crystal Oscillators

Quartz is a naturally occuring crystal having a structure such that when plates are cut in certain definite relationships to the crystallographic axes, these plates will show the *piezoelectric* effect—the plates will be deformed in the influence of an electric field, and, conversely, when such a plate is compressed or deformed in any way a potential difference will appear upon its opposite sides.

The crystal has mechanical resonance, and will vibrate at a very high frequency because of its stiffness, the natural period of vibration depending upon the dimensions, the method of electrical excitation, and crystallographic orientation. Because of the piezoelectric properties, it is possible to cut a quartz plate which, when provided with suitable electrodes, will have the characteristics of a series resonant circuit with a very high L/C ratio and very high Q. The Q is several times as high as can be obtained with an inductor-capacitor combination in conventional physical sizes. The equivalent electrical circuit is shown in figure 4A, the resistance component simply being an acknowledgment of the fact that the Q, while high, does not have an infinite value.

The shunt capacitance of the electrodes and associated wiring (crystal holder and socket, plus circuit wiring) is represented by the dotted portion of figure 4B. In a high frequency crystal this will be considerably greater than the capacitance component of an equivalent series L/C circuit, and unless the shunt capacitance is balanced out in a bridge circuit, the crystal will exhibit both resonant (series resonant) and anti-resonant (parallel resonant) frequencies, the latter being slightly higher than the series resonant frequency and approaching it as C_2 is increased.

The series resonance characteristic is employed in crystal filter circuits in receivers and also in certain oscillator circuits wherein the crystal is used as a selective feedback element in such a manner that the phase of the feedback is correct and the amplitude adequate only at or very close to the series resonant frequency of the crystal.

While quartz, tourmaline, Rochelle salts, ADP, and EDT crystals all exhibit the piezoelectric effect, quartz is the material widely employed for frequency control.

As the cutting and grinding of quartz plates has progressed to a high state of development and these plates may be purchased at prices which discourage the cutting and grinding by simple hand methods for one's own use, the procedure will be only lightly touched upon here.

The crystal blank is cut from the raw quartz at a predetermined orientation with respect to the optical and electrical axes, the orientation determining the activity, temperature coefficient, thickness coefficient, and other characteristics. Various orientations or "cuts" having useful characteristics are illustrated in figure 5.

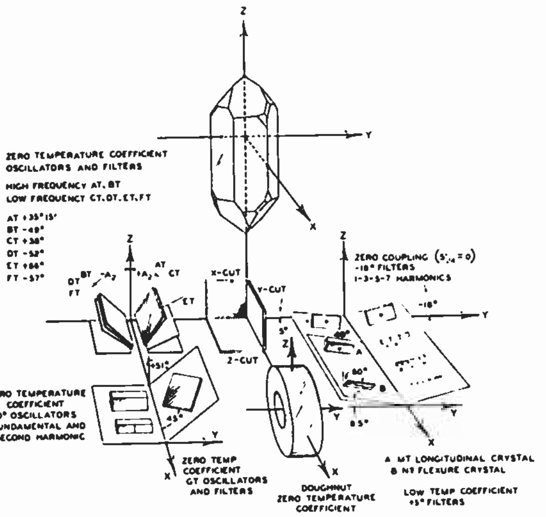


Figure 5

ORIENTATION OF THE COMMON CRYSTAL CUTS

The crystal blank is then rough-ground almost to frequency, the frequency increasing in inverse ratio to the oscillating dimension (usually the thickness). It is then finished to exact frequency either by careful lapping, by etching, or plating. The latter process consists of finishing it to a frequency slightly higher than that desired and then silver plating the electrodes right on the crystal, the frequency decreasing as the deposit of silver is increased. If the crystal is not etched, it must be carefully scrubbed and "baked" several times to stabilize it, or otherwise the frequency and activity of the crystal will change with time. Irradiation by X-rays recently has been used in crystal finishing.

Unplated crystals usually are mounted in pressure holders, in which two electrodes are held against the crystal faces under slight pressure. Unplated crystals also are sometimes mounted in an air-gap holder, in which there is a very small gap between the crystal and one or both electrodes. By making this gap variable, the frequency of the crystal may be altered over narrow limits (about 0.3% for certain types).

The temperature coefficient of frequency for various crystal cuts of the "-T" rotated family is indicated in figure 5. These angles are typical, but crystals of a certain cut will vary slightly. By controlling the orientation and dimensioning, the *turning point* (point of zero temperature coefficient) for a BT cut plate may be made either lower or higher than the 75 degrees shown. Also, by careful control of axes and dimensions, it is possible to get AT cut crystals with a very flat temperature-frequency characteristic.

The first quartz plates used were either Y cut or X cut. The former had a very high temperature coefficient which was discontinuous, causing the frequency to jump at certain critical temperatures. The X cut had a moderately bad coefficient, but it was more continuous, and by keeping the crystal in a temperature controlled oven, a high order of stability could be obtained. However, the X cut crystal was considerably less active than the Y cut, especially in the case of poorly ground plates.

For frequencies between 500 kc. and about 6 Mc., the AT cut crystal now is the most widely used. It is active, can be made free from spurious responses, and has an excellent temperature characteristic. However, above about 6 Mc. it becomes quite thin, and a difficult production job. Between 6 Mc. and about 12 Mc., the BT cut plate is widely used. It also works well between 500 kc. and 6 Mc., but the AT cut is more desirable when a high order of stability is desired and no crystal oven is employed.

For low frequency operation on the order of 100 kc., such as is required in a frequency standard, the GT cut crystal is recommended, though CT and DT cuts also are widely used for applications between 50 and 500 kc. The CT, DT, and GT cut plates are known as *contour* cuts, as these plates oscillate along the long dimension of the plate or bar, and are much smaller physically than would be the case for a regular AT or BT cut crystal for the same frequency.

Crystal Holders Crystals normally are purchased ready mounted. The best type mount is determined by the type crystal and its application, and usually an optimum mounting is furnished with the crystal. However, certain features are desirable in all holders. One of these is exclusion of moisture and prevention of electrode oxidization. The best means of accomplishing this is a metal holder, hermetically sealed, with glass insulation and a metal-to-glass bond. However, such holders are more expensive, and a ceramic or phenolic holder with rubber gasket will serve where requirements are not too exacting.

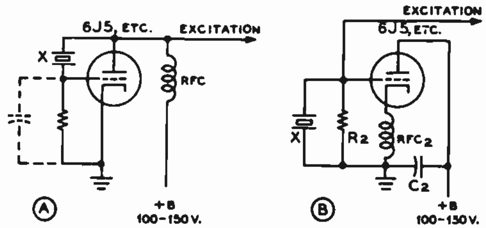
Temperature Control; Crystal Ovens Where the frequency tolerance requirements are not too stringent and the ambient temperature does not include extremes, an AT-cut plate, or a BT-cut plate with optimum (mean temperature) turning point, will often provide adequate stability without resorting to a temperature controlled oven. However, for broadcast stations and other applications where very close tolerances must be maintained, a thermostatically controlled oven, adjusted for a temperature slightly higher than the highest ambient likely to be encountered, must of necessity be employed.

Harmonic Cut Crystals Just as a vibrating string can be made to vibrate on its harmonics, a quartz crystal will exhibit mechanical resonance (and therefore electrical resonance) at harmonics of its fundamental frequency. When employed in the usual holder, it is possible to excite the crystal only on its odd harmonics (overtones).

By grinding the crystal especially for harmonic operation, it is possible to enhance its operation as a harmonic resonator. BT and AT cut crystals designed for optimum operation on the 3d, 5th and even the 7th harmonic are available. The 5th and 7th harmonic types, especially the latter, require special holder and oscillator circuit precautions for satisfactory operation, but the 3d harmonic type needs little more consideration than a regular fundamental type. A crystal ground for optimum operation on a particular harmonic may or may not be a good oscillator on a different harmonic or on the fundamental. One interesting characteristic of a harmonic cut crystal is that its harmonic frequency is not quite an exact multiple of its fundamental, though the disparity is very small.

The harmonic frequency for which the crystal was designed is the *working frequency*. It is not the fundamental since the crystal itself actually oscillates on this working frequency when it is functioning in the proper manner.

When a harmonic-cut crystal is employed, a selective tuned circuit must be employed somewhere in the oscillator in order to discriminate against the fundamental frequency or undesired harmonics. Otherwise the crystal might not always oscillate on the intended frequency. For this reason the Pierce oscillator, later described in this chapter, is not suitable for use with harmonic-cut crystals, because the only tuned element in this oscillator circuit is the crystal itself.



BASIC "PIERCE" OSCILLATOR

HOT-CATHODE "PIERCE" OSCILLATOR

Figure 6

THE PIERCE CRYSTAL OSCILLATOR CIRCUIT

Shown at (A) is the basic Pierce crystal oscillator circuit. A capacitance of 10 to 75 μμfd. normally will be required at C_1 for optimum operation. If a plate supply voltage higher than indicated is to be used, RFC_1 may be replaced by a 22,000-ohm 2-watt resistor. Shown at (B) is an alternative arrangement with the r-f ground moved to the plate, and with the cathode floating. This alternative circuit has the advantage that the full r-f voltage developed across the crystal may be used as excitation to the next stage, since one side of the crystal is grounded.

Crystal Current; Heating and Fracture For a given crystal operating as an anti-resonant tank in a given oscillator at fixed load impedance and plate and screen voltages, the r-f current through the crystal will increase as the shunt capacitance C_2 of figure 4 is increased, because this effectively increases the step-up ratio of C_1 to C_2. For a given shunt capacitance, C_2, the crystal current for a given crystal is directly proportional to the r-f voltage across C_2. This voltage may be measured by means of a vacuum tube voltmeter having a low input capacitance, and such a measurement is a more pertinent one than a reading of r-f current by means of a thermogalvanometer inserted in series with one of the leads to the crystal holder.

The function of a crystal is to provide accurate frequency control, and unless it is used in such a manner as to take advantage of its inherent high stability, there is no point in using a crystal oscillator. For this reason a crystal oscillator should not be run at high plate input in an attempt to obtain considerable power directly out of the oscillator, as such operation will cause the crystal to heat, with resultant frequency drift and possible fracture.

11-3 Crystal Oscillator Circuits

Considerable confusion exists as to nomenclature of crystal oscillator circuits, due to a tendency to name a circuit after its discoverer. Nearly all the basic crystal oscillator circuits were either first used or else developed independently by G. W. Pierce, but he has not been so credited in all the literature.

Use of the crystal oscillator in master oscillator circuits in radio transmitters dates back to about 1924 when the first application articles appeared.

The Pierce Oscillator The circuit of figure 6A is the simplest crystal oscillator circuit. It is one of those developed by Pierce, and is generally known among amateurs as the *Pierce oscillator.* The crystal simply replaces the tank circuit in a Colpitts or ultra-audion oscillator. The r-f excitation voltage available to the next stage is low, being somewhat less than that developed across the crystal. Capacitor C_1 will make more of the voltage across the crystal available for excitation, and sometimes will be found necessary to ensure oscillation. Its value is small, usually approximately equal to or slightly greater than the stray capacitance from the plate circuit to ground (including the grid of the stage being driven).

If the r-f choke has adequate inductance, a crystal (even a harmonic cut crystal) will almost invariably oscillate on its fundamental. The Pierce oscillator therefore cannot be used with harmonic cut crystals.

The circuit at (B) is the same as that of (A) except that the plate instead of the cathode is operated at ground r-f potential. All of the r-f voltage developed across the crystal is available for excitation to the next stage, but still is low for reasonable values of crystal current. For best operation a tube with low heater-cathode capacitance is required. Excitation for the next stage may also be taken from the cathode when using this circuit.

Tuned-Plate Crystal Oscillator The circuit shown in figure 7A is also one used by Pierce, but is more widely referred to as the "Miller" oscillator. To avoid confusion, we shall refer to it as the *tuned-plate crystal oscillator.* It is essentially an Armstrong or tuned plate-tuned grid oscillator with the crystal replacing the usual L-C grid tank. The plate tank must be tuned to a frequency slightly higher than the anti-resonant (parallel resonant) frequency of the crystal. Whereas the Pierce circuits of figure 6 will oscillate at (or very close to) the anti-resonant frequency of the crystal, the circuits of figure 7 will oscillate at a frequency a little above the anti-resonant frequency of the crystal.

The diagram shown in figure 7A is the basic circuit. The most popular version of the tuned-plate oscillator employs a pentode or beam tetrode with cathode bias to prevent excessive plate dissipation when the circuit is not oscillating. The cathode resistor is optional. Its omission will reduce both crystal current and oscillator efficiency, resulting in somewhat more output for a given crystal current. The tube usually is an audio or video beam pentode or tetrode, the plate-grid capacitance of such tubes being sufficient to ensure stable oscillation but not so high as to offer excessive feedback with resulting high crystal current. The 6AG7 makes an excellent all-around tube for this type circuit.

Pentode Harmonic Crystal Oscillator Circuits The usual type of crystal-controlled h-f transmitter operates, at least part of the time, on a frequency which is an integral multiple of the operating frequency of the controlling crystal. Hence, oscillator circuits which are capable of providing output on the crystal frequency if desired, but which also can deliver output energy on harmonics of the crystal frequency have come into wide use. Four such circuits which have found wide application are illustrated in figures 7C, 7D, 7E, and 7F.

The circuit shown in figure 7C is recommended for use with harmonic-cut crystals when output is desired on a multiple of the oscillating frequency of the crystal. As an example, a 25-Mc. harmonic-cut crystal may be used in this circuit to obtain output on 50 Mc., or a 48-Mc. harmonic-cut crystal may be used to obtain output on the 144-Mc. amateur band. The circuit is not recommended for use with the normal type of fundamental-frequency crystal since more output with fewer variable elements can be obtained with the circuits of 7D and 7F.

The Pierce-harmonic circuit shown in figure 7D is satisfactory for many applications which require very low crystal current, but has the disadvantage that both sides of the crystal are above ground potential. The Tri-tet circuit of figure 7E is widely used and can

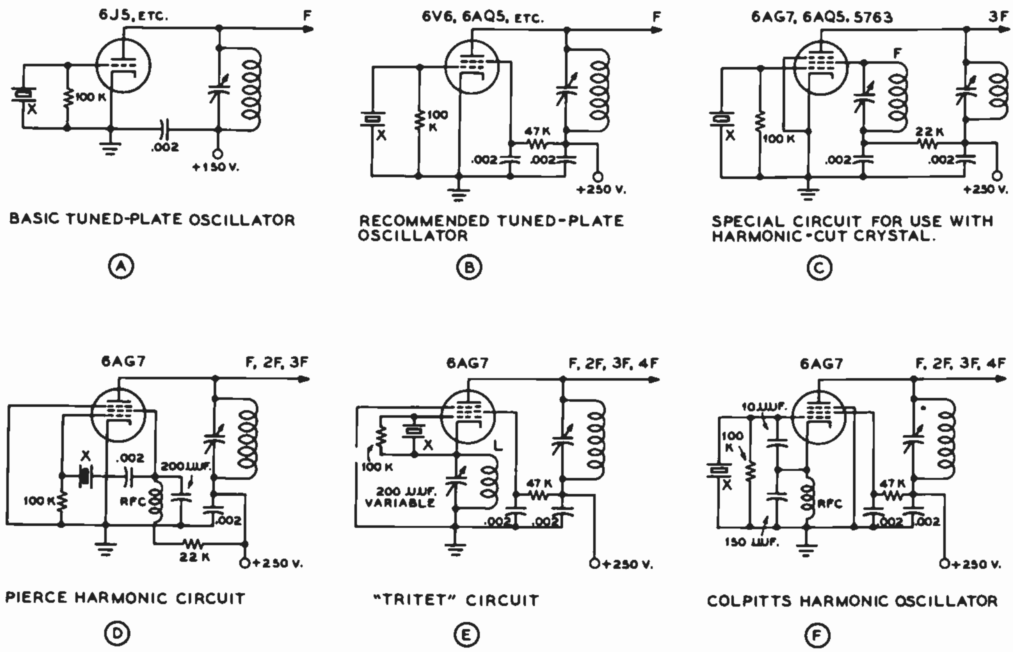


Figure 7

COMMONLY USED CRYSTAL OSCILLATOR CIRCUITS

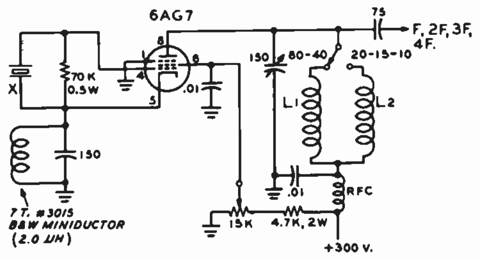
Shown at (A) is the basic tuned-plate crystal oscillator with a triode oscillator tube. The plate tank must be tuned on the low-capacitance side of resonance to sustain oscillation. (B) shows the tuned-plate oscillator as it is normally used, with an a-f power pentode to permit high output with relatively low crystal current.

Schematics (C), (D), (E), and (F) illustrate crystal oscillator circuits which can deliver moderate output energy on harmonics of the oscillating frequency of the crystal. (C) shows a special circuit which will permit use of a harmonic-cut crystal to obtain output energy well into the v-h-f range. (D) is valuable when extremely low crystal current is a requirement, but delivers relatively low output. (E) is commonly used, but is subject to crystal damage if the cathode circuit is mistuned. (F) is recommended as the most generally satisfactory from the standpoints of: low crystal current regardless of mis-adjustment, good output on harmonic frequencies, one side of crystal is grounded, will oscillate with crystals from 1.5 to 10 Mc. without adjustment, output tank may be tuned to the crystal frequency for fundamental output without stopping oscillation or changing frequency.

give excellent output with low crystal current. However, the circuit has the disadvantages of requiring a cathode coil, of requiring careful setting of the variable cathode capacitor to avoid damaging the crystal when changing frequency ranges, and of having both sides of the crystal above ground potential.

The Colpitts harmonic oscillator of figure 7F is recommended as being the most generally satisfactory harmonic crystal oscillator circuit since it has the following advantages: (1) the circuit will oscillate with crystals over a very wide frequency range with no change other than plugging in or switching in the desired crystal; (2) crystal current is extremely low; (3) one side of the crystal is grounded, which facilitates crystal-switching circuits; (4) the circuit will operate straight through without frequency pulling, or it may be operated with output on the second, third, or fourth harmonic of the crystal frequency.

Crystal Oscillator Tuning The tunable circuits of all oscillators illustrated should be tuned for maximum output as indicated by maximum excitation to the following stage, except that the oscillator tank of tuned-plate oscillators (figure 7A and figure 7B) should be backed off slightly towards the low capacitance side from



NOTES

1. L1 = 15 µH (2¼" OF B&W # 3015)
2. L2 = 1.6 µH (1" OF B&W # 3003)
3. FOR 160 METER OPERATION ADD 5 µµF. CONDENSER BETWEEN PINS 4 & 8 OF 6AG7. PLATE COIL = 55 µH, (2¼" OF B&W # 3016)
4. X = 7 MC. CRYSTAL FOR HARMONIC OPERATION

Figure 8

ALL-BAND 6AG7 CRYSTAL OSCILLATOR CAPABLE OF DRIVING BEAM PENTODE TUBE

maximum output, as the oscillator then is in a more stable condition and sure to start immediately when power is applied. This is especially important when the oscillator is keyed, as for break-in c-w operation.

Crystal Switching It is desirable to keep stray shunt capacitances in the crystal circuit as low as possible, regardless of the oscillator circuit. If a selector switch is used, this means that both switch and crystal sockets must be placed close to the oscillator tube socket. This is especially true of harmonic-cut crystals operating on a comparatively high frequency. In fact, on the highest frequency crystals it is preferable to use a turret arrangement for switching, as the stray capacitances can be kept lower.

Crystal Oscillator Keying When the crystal oscillator is keyed, it is necessary that crystal activity and oscillator-tube transconductance be moderately high, and that oscillator loading and crystal shunt capacitance be low. Below 2500 kc. and above 6 Mc. these considerations become especially important. Keying of the plate voltage (in the negative lead) of a crystal oscillator, with the screen voltage regulated at about 150 volts, has been found to give satisfactory results.

A Versatile 6AG7 Crystal Oscillator The 6AG7 tube may be used in a modified Tri-tet crystal oscillator, capable of delivering sufficient power on all bands from 160 meters through 10 meters to fully drive a pentode tube, such as the 807, 2E26 or 6146. Such an oscillator is extremely useful for portable or mobile work, since it combines all essential exciter functions in one tube. The circuit of this oscillator is shown in figure 8. For 160, 80 and 40 meter operation the 6AG7 functions as a tuned-plate oscillator. Fundamental frequency crystals are used on these three bands. For 20, 15 and 10 meter operation the 6AG7 functions as a Tri-tet oscillator with a fixed-tuned cathode circuit. The impedance of this cathode circuit does not affect operation of the 6AG7 on the lower frequency bands so it is left in the circuit at all times. A 7-Mc. crystal is used for fundamental output on 40 meters, and for harmonic output on 20, 15 and 10 meters. Crystal current is extremely low regardless of the output frequency of the oscillator. The plate circuit of the 6AG7 is capable of tuning a frequency range of 2:1, requiring only two output coils: one for 80-40 meter operation, and one for 20, 15 and 10 meter operation. In some cases it may be necessary to add 5 micromicrofarads of external feedback capacity between the plate and control grid of the 6AG7 tube to sustain oscillation with sluggish 160 meter crystals.

Triode Overtone Oscillators The recent development of reliable overtone crystals capable of operation on the third, fifth, seventh (or higher) overtones has made possible v-h-f output from a low frequency crystal by the use of a double triode regenerative oscillator circuit. Some of the new twin triode tubes such as the 12AU7, 12AV7 and 6J6 are especially satisfactory when used in this type of circuit. Crystals that are ground for overtone service may be made to oscillate on odd overtone frequencies other than the one marked on the crystal holder. A 24-Mc. overtone crystal, for example, is a specially ground 8-Mc. crystal operating on its third overtone. In the proper circuit it may be made to oscillate on 40 Mc. (fifth overtone), 56 Mc. (seventh overtone), or 72 Mc. (ninth overtone). Even the ordinary 8-Mc. crystals not designed for overtone operation may be made to oscillate readily on 24 Mc. (third overtone) in these circuits.

A variety of overtone oscillator circuits is shown in figure 9. The oscillator of figure 9A is attributed to Frank Jones, W6AJF. The first section of the 6J6 dual triode comprises a regenerative oscillator, with output on either the third or fifth overtone of the crystal frequency. The regenerative loop of this oscillator consists of a condenser bridge made up of C_1 and C_2, with the ratio C_2/C_1 determining the amount of regenerative feedback in the circuit. With

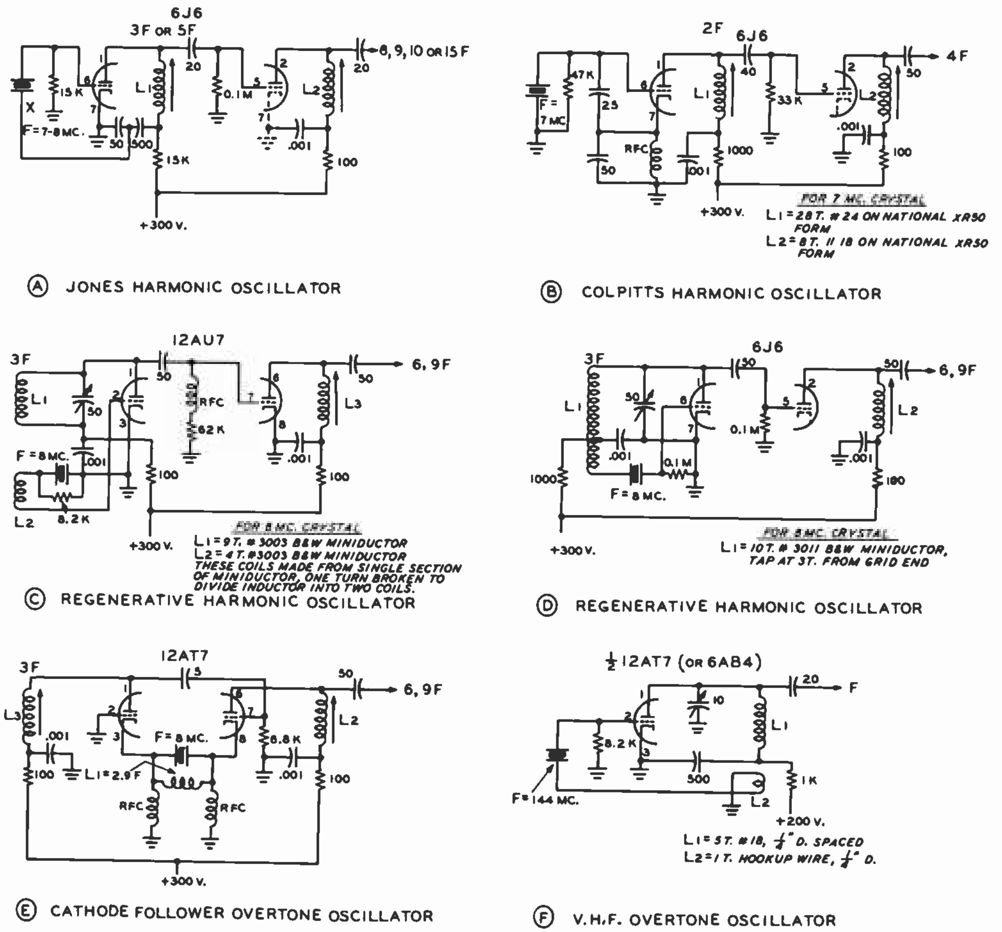


Figure 9
VARIOUS TYPES OF OVERTONE OSCILLATORS USING MINIATURE DOUBLE-TRIODE TUBES

an 8-Mc. crystal, output from the first section of the 6J6 tube may be obtained on either 24 Mc. or 40 Mc., depending upon the resonant frequency of the plate circuit inductor, L_1. The second half of the 6J6 acts as a frequency multiplier, its plate circuit, L_2, tuned to the sixth or ninth harmonic frequency when L_1 is tuned to the third overtone, or to the tenth harmonic frequency when L_1 is tuned to the fifth overtone.

Figure 9B illustrates a Colpitts overtone oscillator employing a 6J6 tube. This is an outgrowth of the Colpitts harmonic oscillator of figure 7F. The regenerative loop in this case consists of C_1, C_2 and RFC between the grid, cathode and ground of the first section of the 6J6. The plate circuit of the first section is tuned to the second overtone of the crystal, and the second section of the 6J6 doubles to the fourth harmonic of the crystal. This circuit is useful in obtaining 28-Mc. output from a 7-Mc. crystal and is highly popular in mobile work.

The circuit of figure 9C shows a typical regenerative overtone oscillator employing a 12AU7 double triode tube. Feedback is controlled by the number of turns in L_2, and the coupling between L_2 and L_1. Only enough feedback should be employed to maintain proper oscillation of the crystal. Excessive feedback will cause the first section of the 12AU7 to oscillate as a self-excited TNT oscillator, independent of the crystal. A variety of this circuit is shown in figure 9D, wherein a tapped coil, L_1, is used in place of the two separate coils. Operation of the circuit is the same in either case, regeneration now being controlled by the placement of the tap on L_1.

A cathode follower overtone oscillator is shown in figure 9E. The cathode coil, L_1, is chosen so as to resonate with the crystal and tube capacities *just below* the third overtone frequency of the crystal. For example, with an 8-Mc. crystal, L_3 is tuned to 24 Mc., L_1 resonates with the circuit capacities to 23.5 Mc., and the harmonic tank circuit of the second section of the 12AT7 is tuned either to 48 Mc. or 72 Mc. If a 24-Mc. overtone crystal is used in this circuit, L_3 may be tuned to 72 Mc., L_1 resonates with the circuit capacities to 70 Mc., and the harmonic tank circuit, L_2, is tuned to 144 Mc. If there is any tendency towards self-oscillation in the circuit, it may be eliminated by a small amount of inductive coupling between L_2 and L_3. Placing these coils near each other, with the winding of L_2 correctly polarized with respect to L_3 will prevent self-oscillation of the circuit.

The use of a 144-Mc. overtone crystal is illustrated in figure 9F. A 6AB4 or one-half of a 12AT7 tube may be used, with output directly in the 2-meter amateur band. A slight amount of regeneration is provided by the one turn link, L_2, which is loosely coupled to the 144-Mc. tuned tank circuit, L_1 in the plate circuit of the oscillator tube. If a 12AT7 tube and a 110-Mc. crystal are employed, direct output in the 220-Mc. amateur band may be obtained from the second half of the 12AT7.

11-4 Radio Frequency Amplifiers

The output of the oscillator stage in a transmitter (whether it be self-controlled or crystal controlled) must be kept down to a fairly low level to maintain stability and to maintain a factor of safety from fracture of the crystal when one is used. The low power output of the oscillator is brought up to the desired power level by means of radio-frequency amplifiers. The two classes of r-f amplifiers that find widest application in radio transmitters are the Class B and Class C types.

The Class B Amplifier Class B amplifiers are used in a radio-telegraph transmitter when maximum power gain and minimum harmonic output is desired in a particular stage. A Class B amplifier operates with cutoff bias and a comparatively small amount of excitation. Power gains of 20 to 200 or so are obtainable in a well-designed Class B amplifier. The plate efficiency of a Class B c-w amplifier will run around 65 per cent.

The Class B Linear Another type of Class B amplifier is the Class B linear stage as employed in radiophone work. This type of amplifier is used to increase the level of a modulated carrier wave, and depends for its operation upon the linear relation between excitation voltage and output voltage. Or, to state the fact in another manner, the power output of a Class B linear stage varies linearly with the square of the excitation voltage.

The Class B linear amplifier is operated with cutoff bias and a small value of excitation, the actual value of exciting power being such that the power output under carrier conditions is one-fourth of the peak power capabilities of the stage. Class B linears are very widely employed in broadcast and commercial installations, but are comparatively uncommon in amateur application, since tubes with high plate dissipation are required for moderate output. The carrier efficiency of such an amplifier will vary from approximately 30 per cent to 35 per cent.

The Class C Amplifier Class C amplifiers are very widely used in all types of transmitters. Good power gain may be obtained (values of gain from 3 to 20 are common) and the plate circuit efficiency may be, under certain conditions, as high as 85 per cent. Class C amplifiers operate with considerably more than cutoff bias and ordinarily with a large amount of excitation as compared to a Class B amplifier. The bias for a normal Class C amplifier is such that plate current on the stage flows for approximately 120° of the 360° excitation cycle. Class C amplifiers are used in transmitters where a fairly large amount of excitation power is available and good plate circuit efficiency is desired.

Plate Modulated Class C The characteristic of a Class C amplifier which makes it linear with respect to changes in plate voltage is that which allows such an amplifier to be *plate modulated* for radiotelephony. Through the use of higher bias than is required for a c-w Class C amplifier and greater excitation, the linearity of such an amplifier may be extended from zero plate voltage to twice the normal value. The output power of a Class C amplifier, adjusted for plate modulation, varies with the square of the plate voltage. This is the same condition that would take place if a resistor equal to the voltage on the amplifier, divided by its plate current, were substituted for the amplifier. Therefore, the stage presents a resistive load to the modulator.

Grid Modulated Class C If the grid current to a Class C amplifier is reduced to a low value, and the plate loading is increased to the point where the plate dissipation approaches the rated value, such an amplifier may be grid modulated for radiotelephony. If the plate voltage is raised to quite a high value and the stage is adjusted carefully, efficiencies as high as 40 to 43 per cent with good modulation capability and comparatively low distortion may be obtained. Fixed bias is required. This type of operation is termed Class C grid-bias modulation.

Grid Excitation Adequate grid excitation must be available for Class B or Class C service. The excitation for a plate-modulated Class C stage must be sufficient to produce a normal value of d-c grid current with rated bias voltage. The bias voltage preferably should be obtained from a combination of grid leak and fixed C-bias supply.

Cutoff bias can be calculated by dividing the amplification factor of the tube into the d-c plate voltage. This is the value normally used for Class B amplifiers (fixed bias, no grid resistor). Class C amplifiers use from 1½ to 5 times this value, depending upon the available grid drive, or excitation, and the desired plate efficiency. Less grid excitation is needed for c-w operation, and the values of fixed bias (if greater than cutoff) may be reduced, or the value of the grid leak resistor can be lowered until normal rated d-c grid current flows.

The values of grid excitation listed for each type of tube may be reduced by as much as 50 per cent if only moderate power output and plate efficiency are desired. When consulting the tube tables, it is well to remember that the power lost in the tuned circuits must be taken into consideration when calculating the available grid drive. At very high frequencies, the r-f circuit losses may even exceed the power required for actual grid excitation.

Link coupling between stages, particularly to the final amplifier grid circuit, normally will provide more grid drive than can be obtained from other coupling systems. The number of turns in the coupling link, and the location of the turns on the coil, can be varied with respect to the tuned circuits to obtain the greatest grid drive for allowable values of buffer or doubler plate current. Slight readjustments sometimes can be made after plate voltage has been applied to the driver tube.

Excessive grid current damages tubes by overheating the grid structure; beyond a certain point of grid drive, no increase in power output can be obtained for a given plate voltage.

11-5 Neutralization of R.F. Amplifiers

The plate-to-grid feedback capacitance of triodes makes it necessary that they be neutralized for operation as r-f amplifiers at frequencies above about 500 kc. Those screen-grid tubes, pentodes, and beam tetrodes which have a plate-to-grid capacitance of 0.1 $\mu\mu$fd. or less may be operated as an amplifier without neutralization in a well-designed amplifier up to 30 Mc.

Neutralizing Circuits The object of *neutralization* is to cancel or neutralize the capacitive feedback of energy from plate to grid. There are two general methods by which this energy feedback may be eliminated: the first, and the most common method, is through the use of a capacitance bridge, and the second method is through the use of a parallel reactance of equal and opposite polarity to the grid-to-plate capacitance, to nullify the effect of this capacitance.

Examples of the first method are shown in figure 10. Figure 10A shows a capacity neutralized stage employing a balanced tank circuit. Phase reversal in the tank circuit is obtained by grounding the center of the tank coil to radio frequency energy by condenser C. Points A and B are 180 degrees out of phase with each other, and the correct amount of out of phase energy is coupled through the neutralizing condenser NC to the grid circuit of the tube. The equivalent bridge circuit of this is shown in figure 11A. It is seen that the bridge is not in balance, since the plate-filament capacity of the tube forms one leg of the bridge, and there is no corresponding capacity from the neutralizing condenser (point B) to ground to obtain a complete balance. In addition, it is mechanically difficult to obtain a perfect electrical balance in the tank coil, and the potential between point A and ground and point B and ground in most cases is unequal. This circuit, therefore, holds neutralization over a very small operating range and unless tubes of low interelectrode capacity are used the inherent unbalance of the circuit will permit only approximate neutralization.

Split-Stator Plate Neutralization Figure 10B shows the neutralization circuit which is most widely used in single-ended r-f stages. The use of

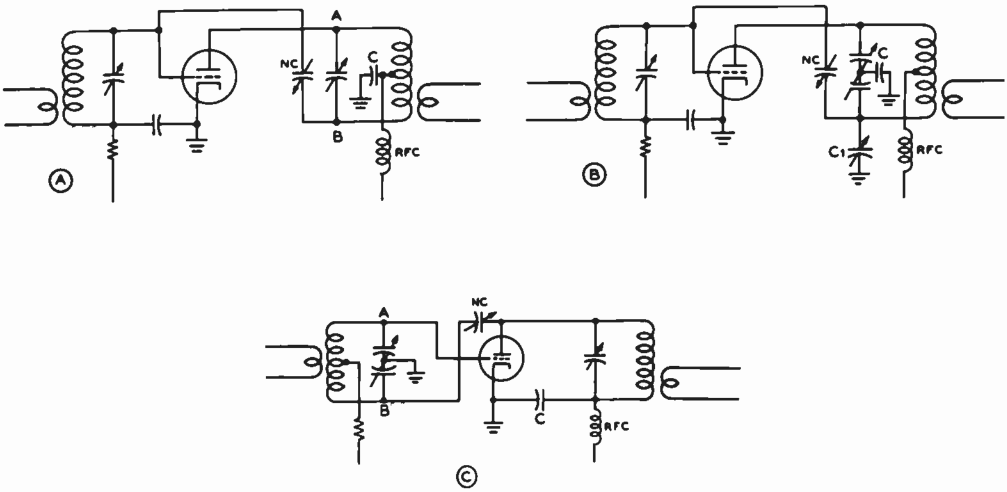


Figure 10
COMMON NEUTRALIZING CIRCUITS FOR SINGLE-ENDED AMPLIFIERS

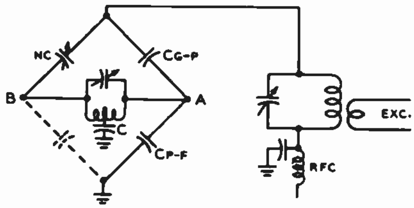
a split-stator plate capacitor makes the electrical balance of the circuit substantially independent of the mutual coupling within the coil and also makes the balance independent of the place where the coil is tapped. With conventional tubes this circuit will allow one neutralization adjustment to be made on, say, 28 Mc., and this adjustment usually will hold sufficiently close for operation on all lower frequency bands.

Condenser C_1 is used to balance out the plate-filament capacity of the tube to allow a perfect neutralizing balance at all frequencies. The equivalent bridge circuit is shown in figure 11B. If the plate-filament capacity of the tube is extremely low (100TH triode, for example), condenser C_1 may be omitted, or may merely consist of the residual capacity of NC to ground.

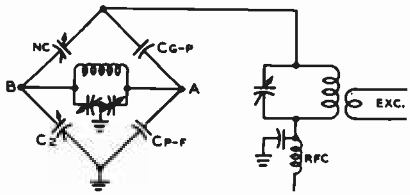
Grid Neutralization A split grid tank circuit may also be used for neutralization of a triode tube as shown in figure 10C. Out of phase voltage is developed across a balanced grid circuit, and coupled through NC to the single-ended plate circuit of the tube. The equivalent bridge circuit is shown in figure 11C. This circuit is in balance until the stage is in operation when the loading effect of the tube upon one-half of the grid circuit throws the bridge circuit out of balance. The amount of unbalance depends upon the grid-plate capacity of the tube, and the amount of mutual inductance between the two halves of the grid coil. If an r-f voltmeter is placed between point A and ground, and a second voltmeter placed between point B and ground the loading effect of the tube will be noticeable. When the tube is supplied excitation with no plate voltage, NC may be adjusted until the circuit is in balance. When plate voltage is applied to the stage, the voltage from point A to ground will decrease, and the voltage from point B to ground will increase, both in direct proportion to the amount of circuit unbalance. The use of this circuit is not recommended above 7 Mc., and it should be used below that frequency only with low internal capacity tubes.

Push-Pull Neutralization Two tubes of the same type can be connected for *push-pull* operation so as to obtain twice as much output as that of a single tube. A push-pull amplifier, such as that shown in figure 12 also has an advantage in that the circuit can more easily be balanced than a single-tube r-f amplifier. The various inter-electrode capacitances and the neutralizing capacitors are connected in such a manner that the reactances on one side of the tuned circuits are exactly equal to those on the opposite side. For this reason, push-pull r-f amplifiers can be more easily neutralized in very-high-frequency transmitters; also, they usually remain in perfect neutralization when tuning the amplifier to different bands.

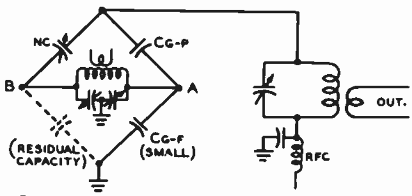
The circuit shown in figure 12 is perhaps



(A) BRIDGE EQUIVALENT OF FIGURE 10-A



(B) BRIDGE EQUIVALENT OF FIGURE 10-B



(C) BRIDGE EQUIVALENT OF FIGURE 10-C

Figure 11
EQUIVALENT NEUTRALIZING CIRCUITS

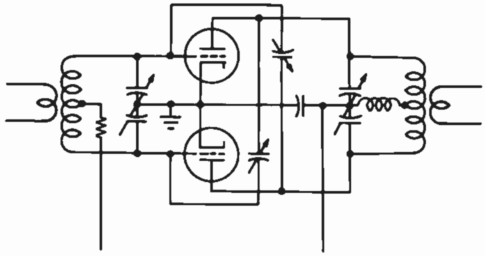


Figure 12
STANDARD CROSS-NEUTRALIZED PUSH-PULL TRIODE AMPLIFIER

the most commonly used arrangement for a push-pull r-f amplifier stage. The rotor of the grid capacitor is grounded, and the rotor of the plate tank capacitor is by-passed to ground.

Shunt or Coil Neutralization The feedback of energy from grid to plate in an unneutralized r-f amplifier is a result of the grid-to-plate capacitance of the amplifier tube. A neutralization circuit is merely an electrical arrangement for nullifying the effect of this capacitance. All the previous neutralization circuits have made use of a bridge circuit for balancing out the grid-to-plate energy feedback by feeding back an equal amount of energy of opposite phase.

Another method of eliminating the feedback effect of this capacitance, and hence of neutralizing the amplifier stage, is shown in figure 13. The grid-to-plate capacitance in the triode amplifier tube acts as a capacitive reactance, coupling energy back from the plate to the grid circuit. If this capacitance is paralleled with an inductance having the same value of reactance of opposite sign, the reactance of one will cancel the reactance of the other and a high-impedance tuned circuit from grid to plate will result.

This neutralization circuit can be used on ultra-high frequencies where other neutralization circuits are unsatisfactory. This is true because the lead length in the neutralization circuit is practically negligible. The circuit can also be used with push-pull r-f amplifiers. In this case, each tube will have its own neutralizing inductor connected from grid to plate.

The main advantage of this arrangement is that it allows the use of single-ended tank circuits with a single-ended amplifier.

The chief disadvantage of the shunt neutralized arrangement is that the stage must be reneutralized each time the stage is retuned to a new frequency sufficiently removed that the grid and plate tank circuits must be retuned to resonance. However, by the use of plug-in coils it is possible to change to a different band of operation by changing the neutralizing coil at the same time that the grid and plate coils are changed.

The 0.0001-μfd. capacitor in series with the neutralizing coil is merely a blocking capacitor to isolate the plate voltage from the grid circuit. The coil L will have to have a very large number of turns for the band of operation in order to be resonant with the comparatively small grid-to-plate capacitance. But since, in all ordinary cases with tubes operating on frequencies for which they were designed, the L/C ratio of the tuned circuit will be very high, the coil can use comparatively small wire, although it must be wound on air or very low loss dielectric and must be insulated for the sum of the plate r-f voltage and the grid r-f voltage.

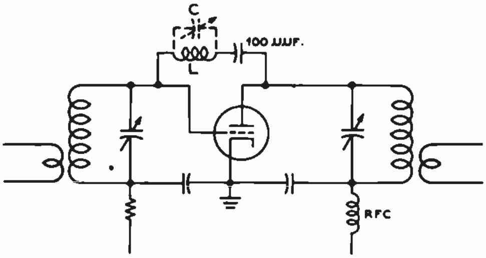


Figure 13

COIL NEUTRALIZED AMPLIFIER

This neutralization circuit is very effective with triode tubes on any frequency, but is particularly effective in the v-h-f range. The coil L is adjusted so that it resonates at the operating frequency with the grid-to-plate capacitance of the tube. Capacitor C may be a very small unit of the low-capacitance neutralizing type and is used to trim the circuit to resonance at the operating frequency. If some means of varying the inductance of the coil a small amount is available, the trimmer capacitor is not needed.

11-6 Neutralizing Procedure

An r-f amplifier is neutralized to prevent self-oscillation or regeneration. A neon bulb, a flashlight lamp and loop of wire, or an r-f galvanometer can be used as a *null indicator* for neutralizing low-power stages. *The plate voltage lead is disconnected from the r-f amplifier stage while it is being neutralized.* Normal grid drive then is applied to the r-f stage, the neutralizing indicator is coupled to the plate coil, and the plate tuning capacitor is tuned to resonance. The neutralizing capacitor (or capacitors) then can be adjusted until *minimum* r.f. is indicated for resonant settings of both grid and plate tuning capacitors. Both neutralizing capacitors are adjusted simultaneously and to approximately the same value of capacitance when a physically symmetrical push-pull stage is being neutralized.

A final check for neutralization should be made with a d-c milliammeter connected in the grid leak or grid-bias circuit. There will be no movement of the meter reading as the plate circuit is tuned through resonance (without plate voltage being applied) when the stage is completely neutralized.

Plate voltage should be *completely* removed by actually opening the d-c plate circuit. If there is a d-c return through the plate supply, a small amount of plate current will flow when grid excitation is applied, even though no primary a-c voltage is being fed to the plate transformer.

A further check on the neutralization of any r-f amplifier can be made by noting whether maximum grid current on the stage comes at the same point of tuning on the plate tuning capacitor as minimum plate current. This check is made with plate voltage on the amplifier and with normal antenna coupling. As the *plate* tuning capacitor is detuned *slightly* from resonance on either side the grid current on the stage should *decrease* the same amount and without any sudden jumps on either side of resonance. This will be found to be a very precise indication of accurate neutralization in either a triode or beam-tetrode r-f amplifier stage, so long as the stage is feeding a load which presents a resistive impedance at the operating frequency.

Push-pull circuits usually can be more completely neutralized than single-ended circuits at very high frequencies. In the intermediate range of from 3 to 15 Mc., single-ended circuits will give satisfactory results.

Neutralization of Screen-Grid R-F Amplifiers Radio-frequency amplifiers using screen-grid tubes can be operated without any additional provision for neutralization at frequencies up to about 15 Mc., provided adequate shielding has been provided between the input and output circuits. Special v-h-f screen-grid and beam tetrode tubes such as the 2E26, 807W, and 5516 in the low-power category and HK-257B, 4E27/8001, 4-125A, and 4-250A in the medium-power category can frequently be operated at frequencies as high as 100 Mc. without any additional provision for neutralization. Tubes such as the 807, 2E22, HY-69, and 813 can be operated with good circuit design at frequencies up to 30 Mc. without any additional provision for neutralization. The 815 tube has been found to require neutralization in many cases above 20 Mc., although the 829B tube will operate quite stably at 100 Mc. without neutralization.

None of these tubes, however, has perfect shielding between the grid and the plate, a condition brought about by the inherent inductance of the screen leads within the tube itself. In addition, unless "watertight" shielding is used between the grid and plate circuits of the tube a certain amount of external leakage between the two circuits is present. These difficulties may not be serious enough to require neutralization of the stage to prevent oscillation, but in many instances they show up in terms of key-clicks when the stage in question is keyed, or as parasitics when the stage is modulated. Unless the designer of the equipment can carefully check the tetrode

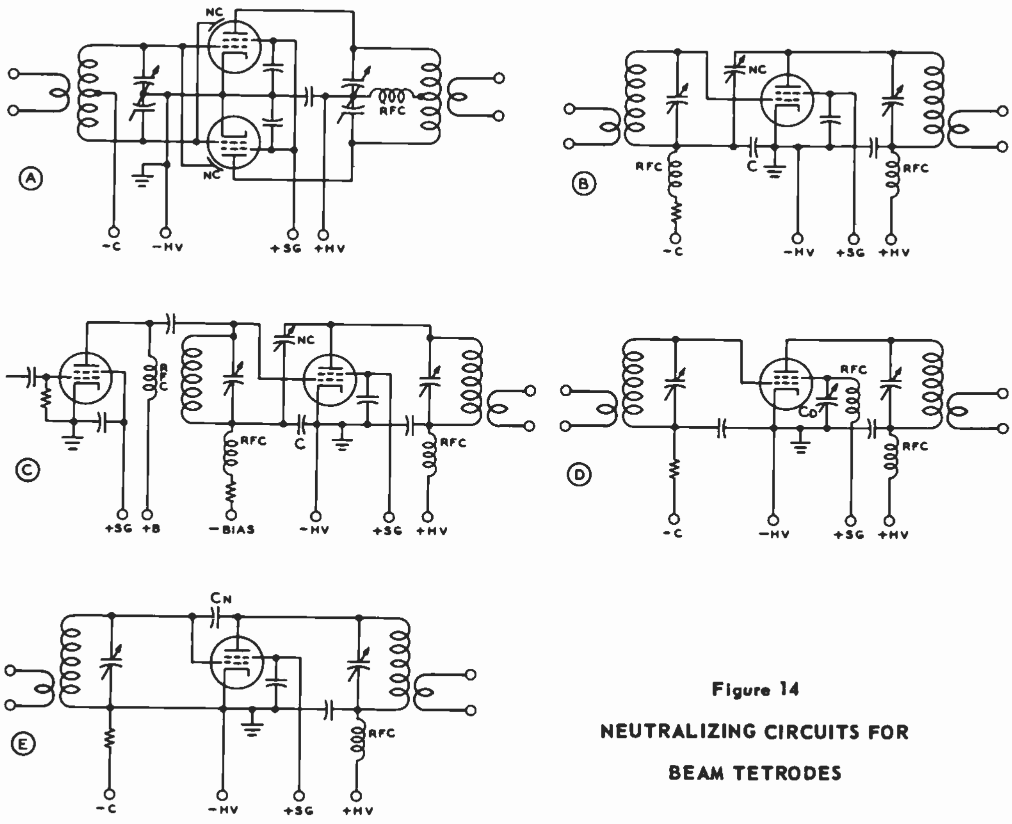


Figure 14

NEUTRALIZING CIRCUITS FOR BEAM TETRODES

A conventional cross neutralized circuit for use with push-pull beam tetrodes is shown at (A). The neutralizing capacitors (NC) usually consist of small plates or rods mounted alongside the plate elements of the tubes. (B) and (C) show "grid neutralized" circuits for use with a single-ended tetrode stage having either link coupling or capacitive coupling into the grid tank. (D) shows a method of tuning the screen-lead inductance to accomplish neutralization in a single-frequency v-h-f tetrode amplifier, while (E) shows a method of neutralizotion by increasing the grid-to-plate capacitance on o tetrode when the operating frequency is higher than that frequency where the tetrode is "self-neutralized" as a result of series resonance in the screen lead. Methods (D) and (E) normally are not practicable at frequencies below about 50 Mc. with the usual types of beam tetrode tubes.

stage for miscellaneous feedback between the grid and plate circuits, and make the necessary circuit revisions to reduce this feedback to an absolute minimum, it is wise to neutralize the tetrode just as if it were a triode tube.

In most push-pull tetrode amplifiers the simplest method of accomplishing neutralization is to use the cross-neutralized capacitance bridge arrangement as normally employed with triode tubes. The neutralizing capacitances, however, must be very much smaller than used with triode tubes, values of the order of 0.2 $\mu\mu$fd. normally being required with beam tetrode tubes. This order of capacitance is far less than can be obtained with a conventional neutralizing capacitor at minimum setting, so the neutralizing arrangement is most commonly made especially for the case at hand. Most common procedure is to bring a conductor (connected to the opposite grid) in the vicinity of the plate itself or of the plate tuning capacitor of one of the tubes. Either one or two such capacitors may be used, two being normally used on a higher frequency amplifier in order to maintain balance within the stage.

An example of this is shown in figure 14A.

Neutralizing Single-Ended Tetrode Stages A single-ended tetrode r-f amplifier stage may be neutralized in the same manner as illustrated for a push-pull stage in figure 14A, provided a split-stator tank capacitor is in use in the plate circuit. However, in the majority of single-ended tetrode r-f amplifier stages a single-section capacitor is used in the plate tank. Hence, other neutralization procedures must be employed when neutralization is found necessary.

The circuit shown in figure 14B is not a true neutralizing circuit, in that the plate-to-grid capacitance is not balanced out. However, the circuit can afford the equivalent effect by isolating the high resonant impedance of the grid tank circuit from the energy fed back from plate to grid. When NC and C are adjusted to bear the following ratio to the grid-to-plate capacitance and the total capacitance from grid-to-ground in the output tube:

$$\frac{NC}{C} = \frac{C_{gp}}{C_{gk}}$$

both ends of the grid tank circuit will be at the same voltage with respect to ground as a result of r-f energy fed back to the grid circuit. This means that the impedance from grid to ground will be effectively equal to the reactance of the grid-to-cathode capacitance in parallel with the stray grid-to-ground capacitance, since the high resonant impedance of the tuned circuit in the grid has been effectively isolated from the feedback path. It is important to note that the effective grid-to-ground capacitance of the tube being neutralized includes the rated grid-to-cathode or input capacitance of the tube, the capacitance of the socket, wiring capacitances and other strays, but it does *not* include the capacitances associated with the grid tuning capacitor. Also, if the tube is being excited by capacitive coupling from a preceding stage (as in figure 14C), the effective grid-to-ground capacitance includes the output capacitance of the preceding stage and its associated socket and wiring capacitances.

Cancellation of Screen-Lead Inductance The provisions discussed in the previous paragraphs are for neutralization of the small, though still important at the higher frequencies, grid-to-plate capacitance of beam-tetrode tubes. However, in the vicinity of the upper-frequency limit of each tube type the inductance of the screen lead of the tube becomes of considerable importance. With a tube operating at a frequency where the inductance of the screen lead is appreciable, the screen will allow a considerable amount of energy leak-through from plate to grid even though the socket terminal on the tube is carefully by-passed to ground. This condition takes place even though the socket pin is bypassed since the reactance of the screen lead will allow a moderate amount of r-f potential to appear on the screen itself inside the electrode assembly in the tube. This effect has been reduced to a very low amount in such tubes as the Hytron 5516, and the Eimac 4X150A and 4X500A but it is still quite appreciable in most beam-tetrode tubes.

The effect of screen-lead inductance on the stability of a stage can be eliminated at any particular frequency by one of two methods. These methods are: (1) Tuning out the screen-lead inductance by series resonating the screen lead inductance with a capacitor to ground. This method is illustrated in figure 14D and is commonly employed in commercially-built equipment for operation on a narrow frequency band in the range above about 75 Mc. The other method (2) is illustrated in figure 14E and consists in feeding back additional energy from plate to grid by means of a small capacitor connected between these two elements. Note that this capacitor is connected in such a manner as to *increase* the effective grid-to-plate capacitance of the tube. This method has been found to be effective with 807 tubes in the range above 50 Mc. and with tubes such as the 4-125A and 4-250A in the vicinity of their upper frequency limits.

Note that both these methods of stabilizing a beam-tetrode v-h-f amplifier stage by cancellation of screen-lead inductance are suitable only for operation over a relatively narrow band of frequencies in the v-h-f range. At lower frequencies both these expedients for reducing the effects of screen-lead inductance will tend to increase the tendency toward oscillation of the amplifier stage.

Neutralizing Problems When a stage cannot be completely neutralized, the difficulty usually can be traced to one or more of the following causes: (1) Filament leads not by-passed to the common ground of that particular stage. (2) Ground lead from the rotor connection of the split-stator tuning capacitor to filament open or too long. (3) Neutralizing capacitors in a field of excessive r.f. from one of the tuning coils. (4) Electromagnetic coupling between grid and plate coils, or between plate and preceding buffer or oscillator circuits. (5) Insufficient shielding or spacing between stages, or between grid and plate circuits in compact transmitters. (6) Shielding placed too close to plate circuit coils, causing induced currents in the shields. (7) Parasitic oscillations when plate voltage is applied. The cure for the latter is mainly a matter of cut and try—rearrange the parts,

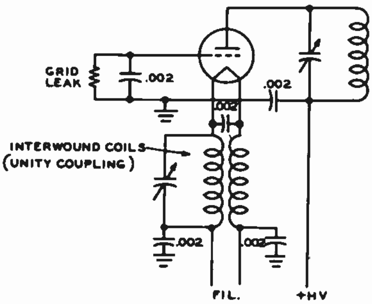


Figure 15
GROUNDED-GRID AMPLIFIER

This type of triode amplifier requires no neutralization, but can be used only with tubes having a relatively low plate-to-cathode capacitance

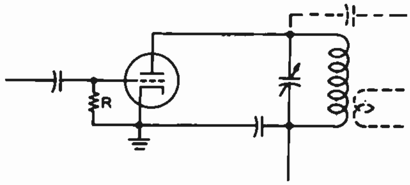


Figure 16
CONVENTIONAL TRIODE FREQUENCY MULTIPLIER

Small triodes such as the 6C4 operate satisfactorily as frequency multipliers, and can deliver output well into the v-h-f range. Resistor R normally will have a value in the vicinity of 100,000 ohms.

change the length of grid or plate or neutralizing leads, insert a parasitic choke in the grid lead or leads, or eliminate the grid r-f chokes which may be the cause of a low-frequency parasitic (in conjunction with plate r-f chokes).

11-7 Grounded Grid Amplifiers

Certain triodes have a grid configuration and lead arrangement which results in very low plate to filament capacitance when the control grid is grounded, the grid acting as an effective shield much in the manner of the screen in a screen-grid tube.

By connecting such a triode in the circuit of figure 15, taking the usual precautions against stray capacitive and inductive coupling between input and output leads and components, a stable power amplifier is realized which requires no neutralization.

At ultra-high frequencies, where it is difficult to obtain satisfactory neutralization with conventional triode circuits (particularly when a wide band of frequencies is to be covered), the grounded-grid arrangement is about the only practicable means of employing a triode amplifier.

Because of the large amount of degeneration inherent in the circuit, considerably more excitation is required than if the same tube were employed in a conventional grounded-cathode circuit. The additional power required to drive a triode in a grounded-grid amplifier is not lost, however, as it shows up in the output circuit and adds to the power delivered to the load. But nevertheless it means that a larger driver stage is required for an amplifier of given output, because a moderate amount of power is delivered to the amplifier load by the driver stage of a grounded-grid amplifier.

11-8 Frequency Multipliers

Quartz crystals and variable-frequency oscillators are not ordinarily used for direct control of the output of high-frequency transmitters. *Frequency multipliers* are usually employed to multiply the frequency to the desired value. These multipliers operate on exact multiples of the excitation frequency; a 3.6-Mc. crystal oscillator can be made to control the output of a transmitter on 7.2 or 14.4 Mc., or on 28.8 Mc., by means of one or more frequency multipliers. When used at twice frequency, they are often termed *frequency doublers*. A simple doubler circuit is shown in figure 16. It consists of a vacuum tube with its plate circuit tuned to *twice* the frequency of the grid driving circuit. This doubler can be excited from a crystal oscillator or another multiplier or amplifier stage.

Doubling is best accomplished by operating the tube with high grid bias. The grid circuit is driven approximately to the normal value of d-c grid current through the r-f choke and grid-leak resistor, shown in figure 16. The resistance value generally is from two to five times as high as that used with the same tube for straight amplification. Consequently, the grid bias is several times as high for the same value of grid current.

Neutralization is seldom necessary in a doubler circuit, since the plate is tuned to twice the frequency of the grid circuit. The impedance of the grid driving circuit is very low at the doubling frequency, and thus there is little tendency for self-excited oscillation.

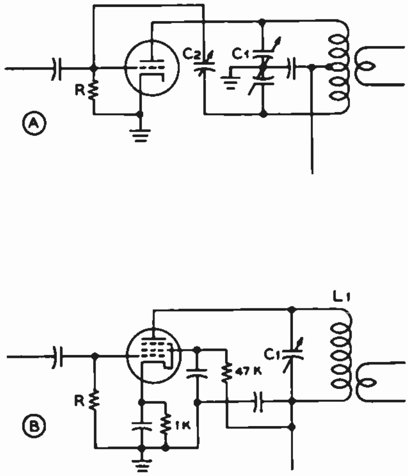


Figure 17
FREQUENCY MULTIPLIER CIRCUITS

The output of a triode v-h-f frequency multiplier often may be increased by neutralization of the grid-to-plate capacitance as shown at (A) above. Such a stage also may be operated as a straight amplifier when the occasion demands. A pentode frequency multiplier is shown at (B). Conventional power tetrodes operate satisfactorily as multipliers so long as the output frequency is below about 100 Mc. Above this frequency special v-h-f tetrodes must be used to obtain satisfactory output.

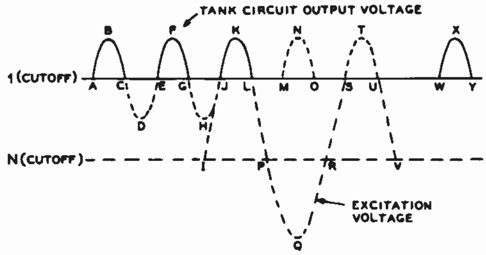


Figure 18
ILLUSTRATING THE ACTION OF A FREQUENCY DOUBLER

Frequency doublers require bias of several times cutoff; high-μ tubes therefore are desirable for this type of service. Tubes which have amplification factors from 20 to 200 are suitable for doubler circuits. Tetrodes and pentodes make excellent doublers. Low-μ triodes, having amplification constants of from 3 to 10, are not applicable for doubler service. In extreme cases the grid voltage must be as high as the plate voltage for efficient doubling action.

Angle of Flow in Frequency Multipliers The angle of plate current flow in a frequency multiplier is a very important factor in determining the efficiency. As the angle of flow is decreased for a given value of grid current, the efficiency increases. To reduce the angle of flow, higher grid bias is required so that the grid excitation voltage will exceed the cutoff value for a shorter portion of the exciting-voltage cycle. For a high order of efficiency, frequency doublers should have an angle of flow of 90 degrees or less, triplers 60 degrees or less, and quadruplers 45 degrees or less. Under these conditions the efficiency will be on the same order as the reciprocal of the harmonic on which the stage operates. In other words the efficiency of a doubler will be approximately ½ or 50 per cent, the efficiency of a tripler will be approximately ⅓ or 33 per cent and that of a quadrupler will be about 25 per cent. With good stage design the efficiency can be somewhat greater than these values, but as the angle of flow is made greater than these limiting values, the efficiency falls off rapidly. The reason is apparent from a study of figure 18.

The pulses ABC, EFG, JKL illustrate 180-degree excitation pulses under Class B operation, the solid straight line indicating cutoff bias. If the bias is increased by N times, to the value indicated by the dotted straight line, and the excitation increased until the peak r-f voltage with respect to ground is the same as before, then the excitation frequency can be cut in half and the effective excitation pulses will have almost the same shape as before. The only difference is that every other pulse is missing; MNO simply shows where the missing pulse would go. However, if the Q of the plate tank circuit is high, it will have sufficient *flywheel effect* to carry over through the missing pulse, and the only effect will be that the plate input and r-f output at optimum loading drop to approximately half. As the input frequency is half the output frequency, an efficient frequency doubler is the result.

By the same token, a tripler or quadrupler can be analyzed, the tripler skipping two excitation pulses and the quadrupler three. In each case the excitation pulse ideally should be short enough that it does not exceed 180 degrees at the output frequency; otherwise the excitation actually is *bucking* the output over a portion of the cycle.

In actual practice, it is found uneconomical to provide sufficient excitation to run a tripler or quadrupler in this fashion. Usually the ex-

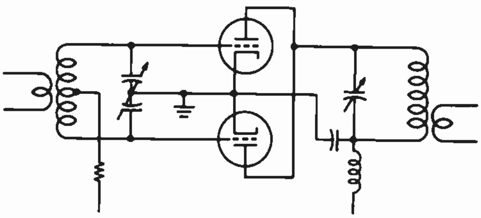


Figure 19
PUSH-PUSH FREQUENCY DOUBLER

The output of a doubler stage may be materially increased through the use of a push-push circuit such as illustrated above.

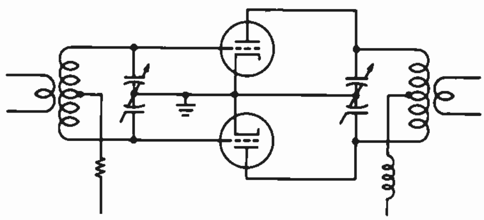


Figure 20
PUSH-PULL FREQUENCY TRIPLER

The push-pull tripler is advantageous in the v-h-f range since circuit balance is maintained both in the input and output circuits. If the circuit is neutralized it may be used either as a straight amplifier or as a tripler. Either triodes or tetrodes may be used; dual-unit tetrodes such as the 815, 832A, and 829B are particularly effective in the v-h-f range.

citation pulses will be at least 90 degrees at the exciting frequency, with correspondingly low efficiency, but it is more practicable to accept the low efficiency and build up the output in succeeding amplifier stages. The efficiency can become quite low before the power gain becomes less than unity.

Push-Push Multipliers Two tubes can be connected in parallel to give twice the output of a single-tube doubler. If the grids are driven *out* of phase instead of *in* phase, the tubes then no longer work simultaneously, but rather one at a time. The effect is to fill in the missing pulses (figure 18). Not only is the output doubled, but several advantages accrue which cannot be obtained by straight parallel operation.

Chief among these is the effective neutralization of the fundamental and all *odd* harmonics, an advantage when spurious emissions must be minimized. Another advantage is that when the available excitation is low and excitation pulses exceed 90 degrees, the output and efficiency will be greater than for the same tubes connected in parallel.

The same arrangement may be used as a quadrupler, with considerably better efficiency than for straight parallel operation, because seldom is it practicable to supply sufficient excitation to permit 45 degree excitation pulses. As pointed out above, the push-push arrangement exhibits better efficiency than a single ended multiplier when excitation is inadequate for ideal multiplier operation.

A typical push-push doubler is illustrated in figure 19. When high transconductance tubes are employed, it is necessary to employ a split-stator grid tank capacitor to prevent self oscillation; with well screened tetrodes or pentodes having medium values of transconductance, a split-coil arrangement with a single-section capacitor may be employed (the center tap of the grid coil being by-passed to ground).

Push-Pull Frequency Triplers It is frequently desirable in the case of u-h-f and v-h-f transmitters that frequency multiplication stages be balanced with respect to ground. Further it is just as easy in most cases to multiply the crystal or v-f-o frequency by powers of three rather than multiplying by powers of two as is frequently done on lower frequency transmitters. Hence the use of push-pull triplers has become quite prevalent in both commercial and amateur v-h-f and u-h-f transmitter designs. Such stages are balanced with respect to ground and appear in construction and on paper essentially the same as a push-pull r-f amplifier stage with the exception that the output tank circuit is tuned to three times the frequency of the grid tank circuit. A circuit for a push-pull tripler stage is shown in figure 20.

A push-pull tripler stage has the further advantage in amateur work that it can also be used as a conventional push-pull r-f amplifier merely by changing the grid and plate coils so that they tune to the same frequency. This is of some advantage in the case of operating the 50-Mc. band with 50-Mc. excitation, and then changing the plate coil to tune to 144 Mc. for operation of the stage as a tripler from excitation on 48 Mc. This circuit arrangement is excellent for operation with push-pull beam tetrodes such as the 6360 and 829B, although a pair of tubes such as the 2E26, or 5763 could just as well be used if proper attention were given to the matter of screen-lead inductance.

11-9 Tank Circuit Capacitances

It is necessary that the proper value of Q be used in the plate tank circuit of any r-f amplifier. The following section has been devoted to a treatment of the subject, and charts are given to assist the reader in the determination of the proper L/C ratio to be used in a radio-frequency amplifier stage.

A Class C amplifier draws plate current in the form of very distorted pulses of short duration. Such an amplifier is always operated into a tuned inductance-capacitance or tank circuit which tends to smooth out these pulses, by its storage or tank action, into a sine wave of radio-frequency output. Any wave-form distortion of the carrier frequency results in harmonic interference in higher-frequency channels.

A Class A r-f amplifier would produce a sine wave of radio-frequency output if its exciting waveform were also a sine wave. However, a Class A amplifier stage converts its d-c input to r-f output by acting as a variable resistance, and therefore heats considerably. A Class C amplifier when driven hard with short pulses at the peak of the exciting waveform acts more as an electronic switch, and therefore can convert its d-c input to r-f output with relatively good efficiency. Values of plate circuit efficiency from 65 to 85 per cent are common in Class C amplifiers operating under optimum conditions of excitation, grid bias, and loading.

Tank Circuit Q As stated before, the tank circuit of a Class C amplifier receives energy in the form of short pulses of plate current which flow in the amplifier tube. But the tank circuit must be able to store enough energy so that it can deliver a current essentially sine wave in form to the load. The ability of a tank to store energy in this manner may be designated as the effective Q of the tank circuit. The effective circuit Q may be stated in any of several ways, but essentially the Q of a tank circuit is the *ratio of the energy stored to 2π times the energy lost per cycle.* Further, the *energy lost per cycle* must, by definition, be equal to *the energy delivered* to the tank circuit by the Class C amplifier tube or tubes.

The Q of a tank circuit at resonance is equal to its parallel resonant impedance (the resonant impedance is resistive at resonance) divided by the reactance of either the capacitor or the inductor which go to make up the tank. The inductive reactance is equal to the capacitive reactance, by definition, at resonance. Hence we may state:

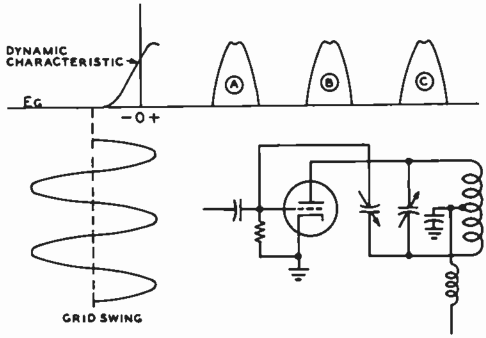


Figure 21

CLASS C AMPLIFIER OPERATION

Plate current pulses are shown at (A), (B), and (C). The dip in the top of the plate current waveform will occur when the excitation voltage is such that the minimum plate voltage dips below the maximum grid voltage. A detailed discussion of the operation of Class C amplifiers is given in Chapter Seven.

$$Q = \frac{R_L}{X_C} = \frac{R_L}{X_L}$$

where R_L is the resonant impedance of the tank and X_C is the reactance of the tank capacitor and X_L is the reactance of the tank coil. This value of resonant impedance, R_L, is the load which is presented to the Class C amplifier tube in a single-ended circuit such as shown in figure 21.

The value of load impedance, R_L, which the Class C amplifier tube sees may be obtained, looking in the other direction from the tank coil, from a knowledge of the operating conditions on the Class C tube. This load impedance may be obtained from the following expression, which is true in the general case of any Class C amplifier:

$$R_L = \frac{E_{pm}^2}{2\, N_p\, I_b\, E_{bb}}$$

where the values in the equation have the characteristics listed in the beginning of Chapter 6.

The expression above is academic, since the peak value of the fundamental component of plate voltage swing, E_{pm}, is not ordinarily known unless a high-voltage peak a-c voltmeter is available for checking. Also, the decimal value of plate circuit efficiency is not ordinarily known with any degree of accuracy. However, in a *normally operated* Class C amplifier

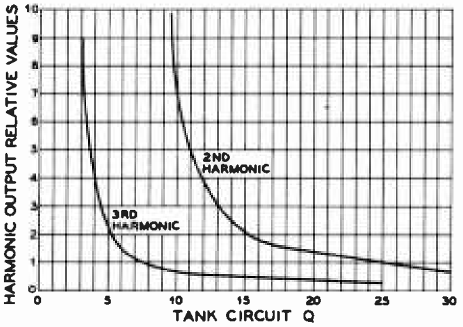


Figure 22
RELATIVE HARMONIC OUTPUT PLOTTED AGAINST TANK CIRCUIT Q

the plate voltage swing will be approximately equal to 0.85 to 0.9 times the d-c plate voltage on the stage, and the plate circuit efficiency will be from 70 to 80 per cent (N_p of 0.7 to 0.8), the higher values of efficiency normally being associated with the higher values of plate voltage swing. With these two assumptions as to the normal Class C amplifier, the expression for the plate load impedance can be greatly simplified to the following approximate but useful expression:

$$R_L \simeq \frac{R_{d.c.}}{2}$$

which means simply that the resistance presented by the tank circuit to the Class C tube is approximately equal to one-half the d-c load resistance which the Class C stage presents to the power supply (and also to the modulator in case high-level modulation of the stage is to be used).

Combining the above simplified expression for the r-f impedance presented by the tank to the tube, with the expression for tank Q given in a previous paragraph we have the following expression which relates the reactance of the tank capacitor or coil to the d-c input to the Class C stage:

$$X_C = X_L \simeq \frac{R_{d.c.}}{2\,Q}$$

The above expression is the basis of the usual charts giving tank capacitance for the various bands in terms of the d-c plate voltage and current to the Class C stage, including the charts of figure 23, figure 24 and figure 25.

Harmonic Radiation vs. Q The problem of harmonic radiation from transmitters has long been present, but it has become critical only relatively recently along with the extensive occupation of the v-h-f range. Television signals are particularly susceptible to interference from other signals falling within the pass band of the receiver, so that the TVI problem has received the major emphasis of all the services in the v-h-f range which are susceptible to interference from harmonics of signals in the h-f or lower v-h-f range.

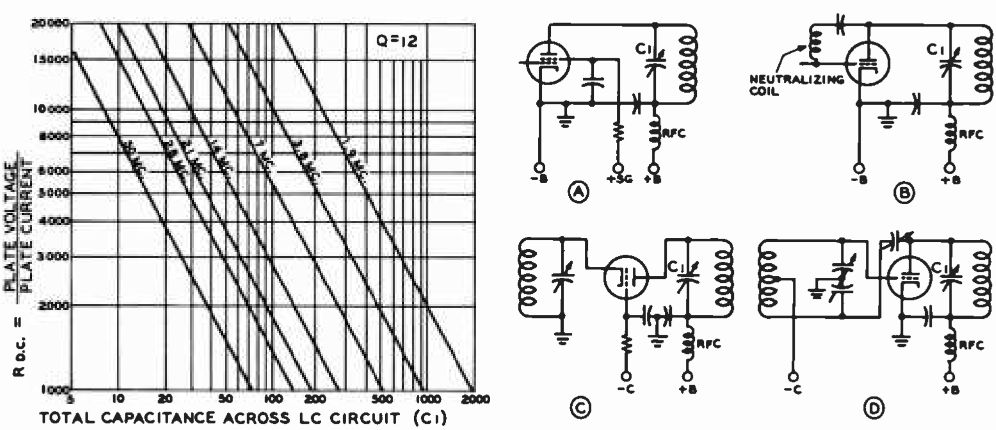
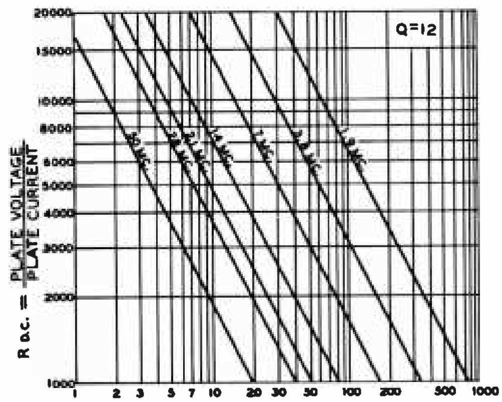


Figure 23
PLATE-TANK CIRCUIT ARRANGEMENTS

Shown above in the case of each of the tank circuit types is the recommended tank circuit capacitance. (A) is a conventional tetrode amplifier, (B) is a coil-neutralized triode amplifier, (C) is a grounded-grid triode amplifier, (D) is a grid-neutralized triode amplifier.



CORRECT VALUES OF TANK CIRCUIT CAPACITANCE (C) FOR OPERATING Q OF 12 WITH SINGLE-ENDED SPLIT TANK COILS

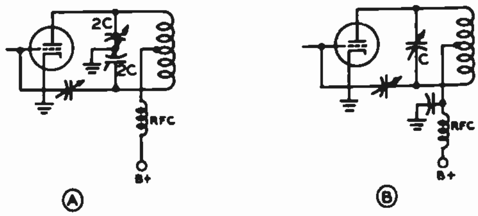


Figure 24

PLATE-TANK CIRCUIT ARRANGEMENTS

Shown above for each of the tank circuit types is the recommended tank circuit capacitance at the operating frequency for an operating Q of 12. (A) is a split-stator tank, each section of which is twice the capacity value read on the graph. (B) is circuit using tapped coil for phase reversal.

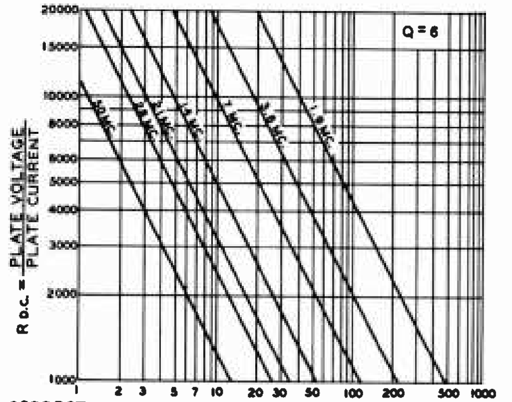
Inspection of figure 22 will show quickly that the tank circuit of a Class C amplifier should have an operating Q of 12 or greater to afford satisfactory rejection of second harmonic energy. The curve begins to straighten out above a Q of about 15, so that a considerable increase in Q must be made before an appreciable reduction in second-harmonic energy is obtained. Above a circuit Q of about 10 any increase will not afford appreciable reduction in the third-harmonic energy, so that additional harmonic filtering circuits external to the amplifier proper must be used if increased attenuation of higher order harmonics is desired. The curves also show that push-pull amplifiers may be operated at Q values of 6 or so, since the second harmonic is cancelled to a large extent if there is no unbalanced coupling between the output tank circuit and the antenna system.

Capacity Charts for Correct Tank Q Figures 23, 24 and 25 illustrate the correct value of tank capacity for various circuit configurations. A Q value of 12 has been chosen as optimum for single ended circuits, and a value of 6 has been chosen for push-pull circuits. Figure 23 is used when a single ended stage is employed, and the capacitance values given are for the total capacitance across the tank coil. This value includes the tube interelectrode capacitance (plate to ground), coil distributed capacitance, wiring capacities, and the value of any low-inductance plate-to-ground by-pass capacitor as used for reducing harmonic generation, in addition to the actual "in-use" capacitance of the plate tuning capacitor. Total circuit stray capacitance may vary from perhaps 5 micromicrofarads for a v-h-f stage to 30 micromicrofarads for a medium power tetrode h-f stage.

When a split plate tank coil is employed in the stage in question, the graph of figure 24 should be used. The capacity read from the graph is the total capacity across the tank coil. If the split-stator tuning capacitor is used, each section of the capacitor should have a value of capacity equal to *twice* the value indicated by the graph. As in the case of figure 23, the values of capacity read on the graph of figure 24 include all residual circuit capacities.

For push-pull operation, the correct values of tank circuit capacity may be determined with the aid of figure 25. The capacity values obtained from figure 25 are the effective values across the tank circuit, and if a split-stator tuning capacitor is used, each section of the capacitor should have a value of capacity equal to *twice* the value indicated by the graph. As in the case of figures 23 and 24, the values of capacity read on the graph of figure 25 include all residual circuit capacities.

The tank circuit operates in the same manner whether the tube feeding it is a pentode, beam tetrode, neutralized triode, grounded-grid triode, whether it is single ended or push-



CORRECT VALUES OF TANK CIRCUIT CAPACITANCE (C_1) FOR OPERATING Q OF 6 WITH PUSH-PULL TANK CIRCUITS

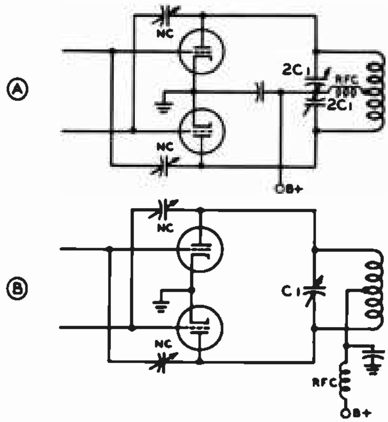


Figure 25

PLATE-TANK CIRCUIT ARRANGEMENTS FOR PUSH-PULL STAGES

Shown above is recommended tank circuit capacity at operating frequency for a Q of 6. (A) is split-stator tank, each section of which is twice the capacity value read on the graph. (B) is circuit using tapped coil for phase reversal.

pull, or whether it is shunt fed or series fed. The important thing in establishing the operating Q of the tank circuit is the ratio of the loaded resonant impedance across its terminals to the reactance of the L and the C which make up the tank.

Due to the unknowns involved in determining circuit stray capacitances it is sometimes more convenient to determine the value of L required for the proper circuit Q (by the method discussed earlier in this Section) and then to vary the tuned circuit capacitance until resonance is reached. This method is most frequently used in obtaining proper circuit Q in commercial transmitters.

The values of R_p for using the charts are easily calculated by dividing the d-c plate supply voltage by the total d-c plate current (expressed in amperes). Correct values of total tuning capacitance are shown in the chart for the different amateur bands. The shunt stray capacitance can be estimated closely enough for all practical purposes. The coil inductance should then be chosen which will produce resonance at the desired frequency with the total calculated tuning capacitance.

Effect of Loading on Q The Q of a circuit depends upon the resistance in series with the capacitance and inductance. This series resistance is very low for a low-loss coil not loaded by an antenna circuit. The value of Q may be from 100 to 600 under these conditions. Coupling an antenna circuit has the effect of increasing the series resistance, though in this case the power is consumed as useful radiation by the antenna. Mathematically, the antenna increases the value of R in the expression $Q = \omega L/R$ where L is the coil inductance in microhenrys and ω is the term $2\pi f$, f being in megacycles.

The coupling from the final tank circuit to the antenna or antenna transmission line can be varied to obtain values of Q from perhaps 3 at maximum coupling to a value of Q equal to the unloaded Q of the circuit at zero antenna coupling. This value of unloaded Q can be as high as 500 or 600, as mentioned in the preceding paragraph. However, the value of Q = 12 will not be obtained at values of normal d-c plate current in the Class C amplifier stage unless the C-to-L ratio in the tank circuit is correct for that frequency of operation.

Tuning Capacitor Air Gap To determine the required tuning capacitor air gap for a particular amplifier circuit it is first necessary to estimate the peak r-f voltage which will appear between the plates of the tuning capacitor. Then, using figure 26, it is possible to estimate the plate spacing which will be required.

The instantaneous r-f voltage in the plate circuit of a Class C amplifier tube varies from nearly zero to nearly twice the d-c plate voltage. If the d-c voltage is being 100 per cent modulated by an audio voltage, the r-f peaks will reach nearly four times the d-c voltage.

FIGURE 26

USUAL BREAKDOWN RATINGS OF COMMON PLATE SPACINGS

Air-gap in inches	Peak voltage breakdown
.030	1,000
.050	2,000
.070	3,000
.100	4,000
.125	4,500
.150	5,200
.170	6,000
.200	7,500
.250	9,000
.350	11,000
.500	15,000
.700	20,000

Recommended air-gap for use when no d-c voltage appears across plate tank condenser (when plate circuit is shunt fed, or when the plate tank condenser is insulated from ground).

D.C. PLATE VOLTAGE	C.W.	PLATE MOD.
400	.030	.050
600	.050	.070
750	.050	.084
1000	.070	.100
1250	.070	.144
1500	.078	.200
2000	.100	.250
2500	.175	.375
3000	.200	.500
3500	.250	.600

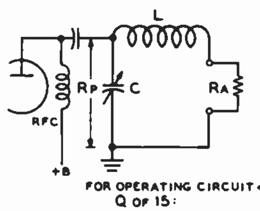
Spacings should be multiplied by 1.5 for same safety factor when d-c voltage appears across plate tank condenser.

These rules apply to a loaded amplifier or buffer stage. If either is operated without an r-f load, the peak voltages will be greater and can *exceed* the d-c plate supply voltage. For this reason no amplifier should be operated without load when anywhere near normal d-c plate voltage is applied.

If a plate blocking condenser is used, it must be rated to withstand the d-c plate voltage plus any audio voltage. This capacitor should be rated at a d-c working voltage of at least *twice the d-c plate supply in a plate modulated amplifier*, and at least *equal to the d-c supply* in any other type of r-f amplifier.

11-10 L and Pi Matching Networks

The L and pi networks often can be put to advantageous use in accomplishing an impedance match between two differing impedances. Common applications are the matching between a transmission line and an antenna, or between the plate circuit of a single-ended amplifier stage and an antenna transmission line. Such networks may be used to accomplish a match



$R_P = R_A(Q^2+1)$ (EXACT)

$R_P = Q^2 R_A$ (APPROX.)

$Q = \frac{X_L}{R_A} = \frac{X_C}{R_A} = \frac{R_P}{X_C} = \frac{R_P}{X_L}$

$X_L = X_C$

For operating circuit Q of 15:

$R_P =$ APPROX. $\frac{\text{PLATE VOLTAGE}}{\text{PLATE CURRENT}}$

$R_P = 225 R_A$

$X_C = \frac{R_P}{15}$

$X_L = \frac{R_P}{15}$

Figure 27

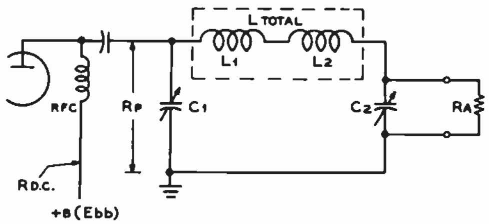
THE L NETWORK IMPEDANCE TRANSFORMER

The L network is useful with a moderate operating Q for high values of impedance transformation, and it may be used for applications other than in the plate circuit of a tube with relatively low values of operating Q for moderate impedance transformations. Exact and approximate design equations are given.

between the plate tank circuit of an amplifier and a transmission line, or they may be used to match directly from the plate circuit of an amplifier to the line without the requirement for a tank circuit—provided the network is designed in such a manner that it has sufficient operating Q for accomplishing harmonic attenuation.

The L Matching Network The L network is of limited utility in impedance matching since its ratio of impedance transformation is fixed at a value equal to (Q^2+1). The operating Q may be relatively low (perhaps 3 to 6) in a matching network between the plate *tank circuit* of an amplifier and a transmission line; hence impedance transformation ratios of 10 to 1 and even lower may be attained. But when the network also acts as the plate tank circuit of the amplifier stage, as in figure 27, the operating Q should be at least 12 and preferably 15. An operating Q of 15 represents an impedance transformation of 225; this value normally will be too high even for transforming from the 2000 to 10,000 ohm plate impedance of a Class C amplifier stage down to a 50-ohm transmission line.

However, the L network is interesting since it forms the basis of design for the pi network. Inspection of figure 27 will show that the L network in reality must be considered as a parallel-resonant tank circuit in which R_A represents the coupled-in load resistance; only in this case the load resistance is directly coupled into the tank circuit rather than being inductively coupled as in the conven-



$$R_{D.C.} = \frac{E_{bb}}{I_b}$$

$$R_P \approx \frac{R_{D.C.}}{2}$$

$$X_{C1} = \frac{R_P}{Q}$$

$$X_{L1} = \frac{R_P}{Q}$$

$$X_{C2} = -R_A \sqrt{\frac{R_P}{R_A(Q^2+1)-R_P}}$$

$$X_{L2} = -\frac{R_A^2\, X_{C2}}{R_A^2+X_{C2}^2}$$

$$X_{L\,TOT.} = X_{L1} + X_{L2}$$

Figure 28

THE PI NETWORK

The pi network is valuable for use as an impedance transformer over a wide ratio of transformation values. The operating Q should be at least 12 and preferably 15 to 20 when the circuit is to be used in the plate circuit of a Class C amplifier. Design equations are given above. The inductor L_{tot} represents a single inductance, usually variable, with a value equal to the sum of L_1 and L_2.

tional arrangement where the load circuit is coupled to the tank circuit by means of a link. When R_A is shorted, L and C comprise a conventional parallel-resonant tank circuit, since for proper operation L and C must be resonant in order for the network to present a resistive load to the Class C amplifier.

The Pi Network The pi impedance matching network, illustrated in figure 28, is much more general in its application than the L network since it offers greater harmonic attenuation, and since it can be used to match a relatively wide range of impedances while still maintaining any desired operating Q. The values of C_1 and L_1 in the pi network of figure 28 can be thought of as having the same values of the L network in figure 27 for the same operating Q, but what is more important from the comparison standpoint these values will be the *same as in a conventional tank circuit.*

The value of the capacitance may be determined by calculation, with the operating Q and the load impedance which should be reflected to the plate of the Class C amplifier as the two knowns—or the actual values of the capacitance may be obtained for an operating Q of 12 by reference to figures 23, 24 and 25.

The inductive arm in the pi network can be thought of as consisting of two inductances in series, as illustrated in figure 28. The first portion of this inductance, L_1, is that value of inductance which would resonate with C_1 at the operating frequency—the same as in a conventional tank circuit. However, the actual value of inductance in this arm of the pi network, L_{tot} will be greater than L_1 for normal values of impedance transformation. For high transformation ratios L_{tot} will be only slightly greater than L_1; for a transformation ratio of 1.0, L_{tot} will be twice as great as L_1. The amount of inductance which must be added to L_1 to restore resonance and maintain circuit Q is obtained through use of the expression for $X_{1,2}$ in figure 28.

The peak voltage rating of the main tuning capacitor C_1 should be the normal value for a Class C amplifier operating at the plate voltage to be employed. The inductor L_{tot} may be a plug-in coil which is changed for each band of operation, or some sort of variable inductor may be used. A continuously variable slider-type of variable inductor, such as used in certain items of surplus military equipment, may be used to good advantage if available, or a tapped inductor such as used in the ART-13 may be employed. However, to maintain good circuit Q on the higher frequencies when a variable or tapped coil is used on the lower frequencies, the tapped or variable coil should be removed from the circuit and replaced by a smaller coil which has been especially designed for the higher frequency ranges.

The peak voltage rating of the output or loading capacitor, C_2, is determined by the power level and the impedance to be fed. If a 50-ohm coaxial line is to be fed from the pi network, receiving-type capacitors will be satisfactory even up to the power level of a plate-modulated kilowatt amplifier. In any event, the peak voltage which will be impressed across the output capacitor is expressed by: $E_{pk}^2 = 2\ R_a\ W_o$, where E_{pk} is the peak voltage across the capacitor, R_a is the value of resistive load which the network is feeding, and W_o is the maximum value of the average power output of the stage. The harmonic attenuation of the pi network is quite good, although an external low-pass filter will be required to obtain harmonic attenuation value upward of 100 db such as normally required. The attenuation to second harmonic energy will be approximately 40 db for an operating Q of 15 for the pi network; the value increases to about 45 db for a 1:1 transformation and falls to about 38 db for an impedance step-down of 80:1, assuming that the operating Q is maintained at 15.

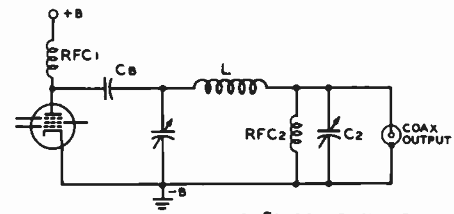


PLATE LOAD (OHMS) $\frac{E_B}{2 \times I_B}$ WHERE E_B IS PLATE VOLTAGE AND I_B IS PLATE CURRENT IN MILLIAMPERES.

CB — .00025 μF. MICA CAPACITOR RATED AT TWICE THE D.C. PLATE VOLTAGE.

RFC1 — Nº 28 ENAMELED, CLOSE-WOUND ON A CERAMIC INSULATOR 1" DIA., 4" LONG OR NATIONAL R-175A

RFC2 — $2\frac{1}{2}$ MH, NATIONAL R-100

Estimated Plate Load (ohms)		1,000	1,500	2,000	2,500	3,000	3,500	4,000	4,500	5,000	6,000*	NOTES
C_1 in μμf,	3.5 Mc	520	360	280	210	180	155	135	120	110	90	The actual capacitance setting for C_1 equals the value in this table minus the published tube output capacitance. Air gap approx. 10 mils/100 v E_b.
	7	260	180	140	105	90	76	68	60	56	45	
	14	130	90	70	52	45	38	34	30	28	23	
	21	85	60	47	35	31	25	23	20	19	15	
	28	65	45	35	26	23	19	17	15	14	11	
L in μh,	3.5 Mc	4.5	6.5	8.5	10.5	12.5	14	15.5	18	20	25	Inductance values are for a 50-ohm load. For a 70-ohm load, values are approx. 3% higher.
	7	2.2	3.2	4.2	5.2	6.2	7	7.8	9	10	12.5	
	14	1.1	1.6	2.1	2.6	3.1	3.5	3.9	4.5	5	6.2	
	21	0.73	1.08	1.38	1.7	2.05	2.3	2.6	3	3.3	4.1	
	28	0.55	0.8	1.05	1.28	1.55	1.7	1.95	2.25	2.5	3.1	
C_2 in μμf,	3.5 Mc	2,400	2,100	1,800	1,550	1,400	1,250	1,100	1,000	900	700	For 50-ohm transmission line. Air gap for C_2 is approx. 1 mil/100 v E_b.
	7	1,200	1,060	900	760	700	630	560	500	460	350	
	14	600	530	450	380	350	320	280	250	230	175	
	21	400	350	300	250	230	210	185	165	155	120	
	28	300	265	225	190	175	160	140	125	115	90	
C_2 in μμf,	3.5 Mc	1,800	1,500	1,300	1,100	1,000	900	800	720	640	500	For 70-ohm transmission line.
	7	900	750	650	560	500	450	400	360	320	250	
	14	450	370	320	280	250	220	200	180	160	125	
	21	300	250	215	190	170	145	130	120	110	85	
	28	225	185	160	140	125	110	100	90	80	65	

* Values given are approximations. All components shown in Table I are for a Q of 12. For other values of Q, use $\frac{Q_a}{Q_b} = \frac{C_a}{C_b}$ and $\frac{Q_a}{Q_b} = \frac{L_b}{L_a}$. When the estimated plate load is higher than 5,000 ohms, it is recommended that the components be selected for a circuit Q between 20 and 30.

Table I Components for Pi-Coupled Final Amplifiers

Component Chart for Pi-Networks To simplify design procedure, a pi-network chart, compiled by M. Seybold, W2RYI (reproduced by courtesy of R.C.A. Tube Division, Harrison, N.J.) is shown in table 1. This chart summarizes the calculations of figure 28 for various values of plate load.

11-11 Grid Bias

Radio-frequency amplifiers require some form of *grid bias* for proper operation. Practically all r-f amplifiers operate in such a manner that plate current flows in the form of short pulses which have a duration of only a fraction of an r-f cycle. To accomplish this with a sinusoidal excitation voltage, the operating grid bias must be at least sufficient to cut off the plate current. In very high efficiency Class C amplifiers the operating bias may be many times the cutoff value. Cutoff bias, it will be recalled, is that value of grid voltage which will reduce the plate current to zero at the plate voltage employed. The method for calculating it has been indicated previously. This theoretical value of cutoff will not reduce the plate current completely to zero, due to the variable-μ tendency or "knee" which is characteristic of all tubes as the cutoff point is approached.

Class C Bias Amplitude modulated Class C amplifiers should be operated with the grid bias adjusted to a value greater than twice cutoff at the operating plate volt-

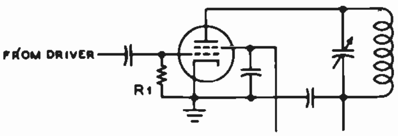


Figure 29

GRID-LEAK BIAS

The grid leak on an amplifier or multiplier stage may also be used as the shunt feed impedance to the grid of the tube when a high value of grid leak (greater than perhaps 20,000 ohms) is used. When a lower value of grid leak is to be employed, an r-f choke should be used between the grid of the tube and the grid leak to reduce r-f losses in the grid leak resistance.

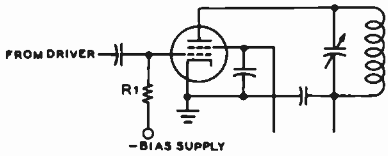


Figure 30

COMBINATION GRID-LEAK AND FIXED BIAS

Grid-leak bias often is used in conjunction with a fixed minimum value of power supply bias. This arrangement permits the operating bias to be established by the excitation energy, but in the absence of excitation the electrode currents to the tube will be held to safe values by the fixed-minimum power supply bias. If a relatively low value of grid leak is to be used, an r-f choke should be connected between the grid of the tube and the grid leak as discussed in figure 29.

age. This procedure will insure that the tube is operating at a bias greater than cutoff when the plate voltage is doubled on positive modulation peaks. C-w telegraph and FM transmitters can be operated with bias as low as cutoff, if only limited excitation is available and moderate plate efficiency is satisfactory. In a c-w transmitter, the bias supply or resistor should be adjusted to the point which will allow normal grid current to flow for the particular amount of grid driving r-f power available. This form of adjustment will allow more output from the under-excited r-f amplifier than when higher bias is used with corresponding lower values of grid current. In any event, the operating bias should be set at as low a value as will give satisfactory operation, since harmonic generation in a stage increases rapidly as the bias is increased.

Grid-Leak Bias A resistor can be connected in the grid circuit of a Class C amplifier to provide grid-leak bias. This resistor, R_1 in figure 29, is part of the d-c path in the grid circuit.

The r-f excitation applied to the grid circuit of the tube causes a pulsating direct current to flow through the bias supply lead, due to the rectifying action of the grid, and any current flowing through R_1 produces a voltage drop across that resistor. The grid of the tube is positive for a short duration of each r-f cycle, and draws electrons from the filament or cathode of the tube during that time. These electrons complete the circuit through the d-c *grid return*. The voltage drop across the resistance in the grid return provides a *negative bias* for the grid.

Grid-leak bias automatically adjusts itself over fairly wide variations of r-f excitation. The value of grid-leak resistance should be such that normal values of grid current will flow at the maximum available amount of r-f excitation. Grid-leak bias cannot be used for grid-modulated or linear amplifiers in which the average d-c grid current is constantly varying with modulation.

Safety Bias Grid-leak bias alone provides no protection against excessive plate current in case of failure of the source of r-f grid excitation. A *C-battery* or *C-bias* supply can be connected in series with the grid leak, as shown in figure 30. This fixed protective bias will protect the tube in the event of failure of grid excitation. "Zero-bias" tubes do not require this bias source in addition to the grid leak, since their plate current will drop to a safe value when the excitation is removed.

Cathode Bias A resistor can be connected in series with the cathode or center-tapped filament lead of an amplifier to secure *automatic bias*. The plate current flows through this resistor, then back to the cathode or filament, and the voltage drop across the resistor can be applied to the grid circuit by connecting the grid bias lead to the grounded or power supply end of the resistor R, as shown in figure 31.

The grounded (B-minus) end of the cathode resistor is negative relative to the cathode by an amount equal to the voltage drop across the resistor. The value of resistance must be so chosen that the sum of the desired grid and plate current flowing through the resistor will bias the tube for proper operation.

This type of bias is used more extensively in audio-frequency than in radio-frequency amplifiers. The voltage drop across the resistor

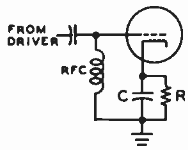


Figure 31
R-F STAGE WITH CATHODE BIAS
Cathode bias sometimes is advantageous for use in an r-f stage that operates with a relatively small amount of r-f excitation.

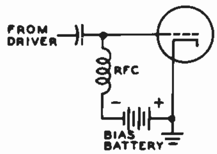


Figure 32
R-F STAGE WITH BATTERY BIAS
Battery bias is seldom used, due to deterioration of the cells by the reverse grid current. However, it may be used in certain special applications, or the fixed bias voltage may be supplied by a bias power supply.

must be subtracted from the total plate supply voltage when calculating the power input to the amplifier, and this loss of plate voltage in an r-f amplifier may be excessive. A Class A audio amplifier is biased only to approximately one-half cutoff, whereas an r-f amplifier may be biased to twice cutoff, or more, and thus the plate supply voltage loss may be a large percentage of the total available voltage when using low or medium μ tubes.

Oftentimes just enough cathode bias is employed in an r-f amplifier to act as safety bias to protect the tubes in case of excitation failure, with the rest of the bias coming from a grid leak.

Separate Bias Supply An external supply often is used for grid bias, as shown in figure 32. Battery bias gives very good voltage regulation and is satisfactory for grid-modulated or linear amplifiers, which operate at low grid current. In the case of Class C amplifiers which operate with high grid current, battery bias is not satisfactory. This direct current has a charging effect on the dry batteries; after a few months of service the cells will become unstable, bloated, and noisy.

A separate a-c operated power supply is commonly used for grid bias. The bleeder resistance across the output of the filter can be made sufficiently low in value that the grid current of the amplifier will not appreciably change the amount of negative grid-bias voltage. Alternately, a voltage regulated grid-bias supply can be used. This type of bias supply is used in Class B audio and Class B r-f linear amplifier service where the voltage regulation in the C-bias supply is important. For a Class C amplifier, regulation is not so important, and an economical design of components in the power supply, therefore, can be utilized. In this case, the bias voltage must be adjusted with normal grid current flowing, as the grid current will raise the bias considerably when it is flowing through the bias-supply bleeder resistance.

11-12 Protective Circuits for Tetrode Transmitting Tubes

The tetrode transmitting tube requires three operating voltages: grid bias, screen voltage, and plate voltage. The current requirements of these three operating voltages are somewhat interdependent, and a change in potential of one voltage will affect the current drain of the tetrode in respect to the other two voltages. In particular, if the grid excitation voltage is interrupted as by keying action, or if the plate supply is momentarily interrupted, the resulting voltage or current surges in the screen circuit are apt to permanently damage the tube.

The Series Screen Supply A simple method of obtaining screen voltage is by means of a dropping resistor from the high voltage plate supply, as shown in figure 33. Since the current drawn by the screen is a function of the exciting voltage applied to the tetrode, the screen voltage will rise to equal the plate voltage under conditions of no exciting voltage. If the control grid is overdriven, on the other hand, the screen current may become excessive. In either case, damage to the screen and its associated components may result. In addition, fluctuations in the plate loading of the tetrode stage will cause changes in the screen current of the tube. This will result in screen voltage fluctuations due to the inherently poor voltage regulation of the screen series dropping resistor. These effects become dangerous to tube life if the plate voltage is greater than the screen voltage by a factor of 2 or so.

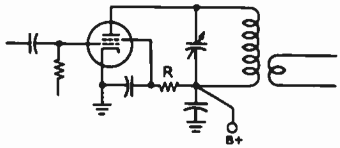


Figure 33
DROPPING-RESISTOR SCREEN SUPPLY

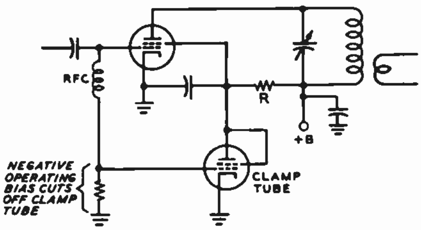


Figure 34
CLAMP-TUBE SCREEN SUPPLY

The Clamp Tube A clamp tube may be added to the series screen supply, as shown in figure 34. The clamp tube is normally cut off by virtue of the d-c grid bias drop developed across the grid resistor of the tetrode tube. When excitation is removed from the tetrode, no bias appears across the grid resistor, and the clamp tube conducts heavily, dropping the screen voltage to a safe value. When excitation is applied to the tetrode the clamp tube is inoperative, and fluctuations of the plate loading of the tetrode tube could allow the screen voltage to rise to a damaging value. Because of this factor, the clamp tube does not offer complete protection to the tetrode.

The Separate Screen Supply A low voltage screen supply may be used instead of the series screen dropping resistor. This will protect the screen circuit from excessive voltages when the other tetrode operating parameters shift. However, the screen can be easily damaged if plate or bias voltage is removed from the tetrode, as the screen current will reach high values and the screen dissipation will be exceeded. If the screen supply is capable of providing slightly more screen voltage than the tetrode requires for proper operation, a series wattage-limiting resistor may be added to the circuit as shown in figure 35. With this resistor in the circuit it is possible to apply excitation to the tetrode tube with screen voltage present (but in the absence of plate voltage) and still not damage the screen of the tube. The value of the resistor should be chosen so that the product of the voltage applied to the screen of the tetrode times the screen current never exceeds the maximum rated screen dissipation of the tube.

11-13 Interstage Coupling

Energy is usually coupled from one circuit of a transmitter into another either by *capacitive coupling*, *inductive coupling*, or *link coupling*. The latter is a special form of inductive coupling. The choice of a coupling method depends upon the purpose for which it is to be used.

Capacitive Coupling Capacitive coupling between an amplifier or doubler circuit and a preceding driver stage is shown in figure 36. The coupling capacitor, C, isolates the d-c plate supply from the next grid and provides a low impedance path for the r-f energy between the tube being driven and the driver tube. This method of coupling is simple and economical for low power amplifier or exciter stages, but has certain disadvantages, particularly for high frequency stages. The grid leads in an amplifier should be as short as possible, but this is difficult to attain in the physical arrangement of a high power amplifier with respect to a capacitively-coupled driver stage.

Disadvantages of Capacitive Coupling One significant disadvantage of capacitive coupling is the difficulty of adjusting the load on the driver stage. Impedance adjustment can be accomplished by tapping the coupling lead a part of the way down on the plate coil of the tuned stage of the driver circuit; but often when this is done

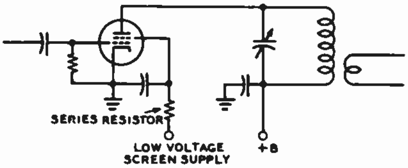


Figure 35
A PROTECTIVE WATTAGE-LIMITING RESISTOR FOR USE WITH LOW-VOLTAGE SCREEN SUPPLY

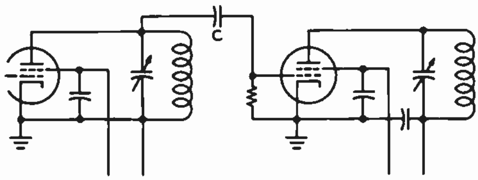


Figure 36
CAPACITIVE INTERSTAGE COUPLING

a parasitic oscillation will take place in the stage being driven.

One main disadvantage of capacitive coupling lies in the fact that the grid-to-filament capacitance of the driven tube is placed directly across the driver tuned circuit. This condition sometimes makes the r-f amplifier difficult to neutralize, and the increased minimum circuit capacitance makes it difficult to use a reasonable size coil in the v-h-f range. Difficulties from this source can be partially eliminated by using a center-tapped or split-stator tank circuit in the plate of the driver stage, and coupling capacitively to the opposite end from the plate. This method places the plate-to-filament capacitance of the driver across one-half of the tank and the grid-to-filament capacitance of the following stage across the other half. This type of coupling is shown in figure 37.

Capacitive coupling can be used to advantage in reducing the total number of tuned circuits in a transmitter so as to conserve space and cost. It also can be used to advantage between stages for driving beam tetrode or pentode amplifier or doubler stages.

Inductive Coupling *Inductive coupling* (figure 38) results when two coils are electromagnetically coupled to one another. The degree of coupling is controlled by varying the mutual inductance of the two coils, which is accomplished by changing the spacing or the relationship between the axes of the coils.

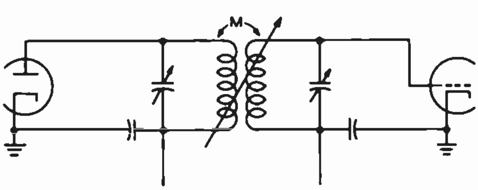


Figure 38
INDUCTIVE INTERSTAGE COUPLING

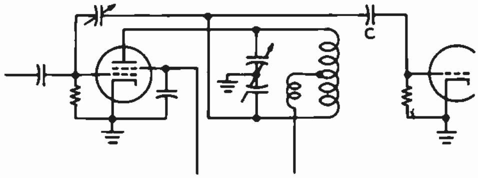


Figure 37
BALANCED CAPACITIVE COUPLING

Balanced capacitive coupling sometimes is useful when it is desirable to use a relatively large inductance in the interstage tank circuit, or where the exciting stage is neutralized as shown above.

Inductive coupling is used extensively for coupling r-f amplifiers in radio receivers. However, the mechanical problems involved in adjusting the degree of coupling limit the usefulness of direct inductive coupling in transmitters. Either the primary or the secondary or both coils may be tuned.

Unity Coupling If the grid tuning capacitor of figure 38 is removed and the coupling increased to the maximum practicable value by interwinding the turns of the two coils, the circuit insofar as r.f. is concerned acts like that of figure 36, in which one tank serves both as plate tank for the driver and grid tank for the driven stage. The inter-wound grid winding serves simply to isolate the d-c plate voltage of the driver from the grid of the driven stage, and to provide a return for d-c grid current. This type of coupling, illustrated in figure 39, is commonly known as *unity coupling.*

Because of the high mutual inductance, both primary and secondary are resonated by the one tuning capacitor.

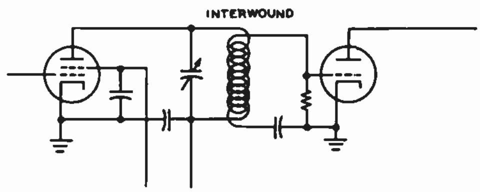


Figure 39
"UNITY" INDUCTIVE COUPLING

Due to the high value of coupling between the two coils, one tuning capacitor tunes both circuits. This arrangement often is useful in coupling from a single-ended to a push-pull stage.

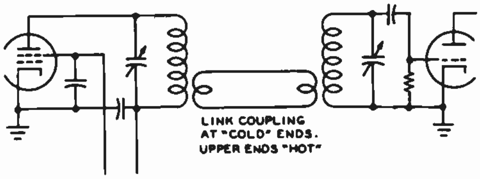


Figure 40
INTERSTAGE COUPLING BY MEANS OF A "LINK"

Link interstage coupling is very commonly used since the two stages may be separated by a considerable distance, since the amount of a coupling between the two stages may be easily varied, and since the capacitances of the two stages may be isolated to permit use of larger inductances in the v-h-f range.

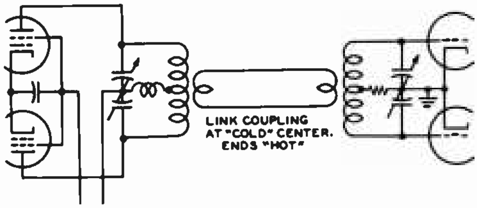


Figure 41
PUSH-PULL LINK COUPLING

Link Coupling A special form of inductive coupling which is widely employed in radio transmitter circuits is known as *link coupling.* A low impedance r-f transmission line couples the two tuned circuits together. Each end of the line is terminated in one or more turns of wire, or links, wound around the coils which are being coupled together. These links should be coupled to each tuned circuit at the point of zero r-f potential, or *nodal point.* A ground connection to one side of the link usually is used to reduce harmonic coupling, or where capacitive coupling between two circuits must be minimized. Coaxial line is commonly used to transfer energy between the two coupling links, although Twin-Lead may be used where harmonic attenuation is not so important.

Typical link coupled circuits are shown in figures 40 and 41. Some of the advantages of link coupling are the following:

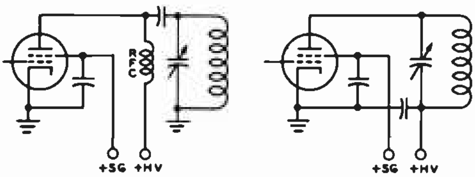
(1) It eliminates coupling taps on tuned circuits.
(2) It permits the use of series power supply connections in both tuned grid and tuned plate circuits, and thereby eliminates the need of shunt-feed r-f chokes.
(3) It allows considerable separation between transmitter stages without appreciable r-f losses or stray chassis currents.
(4) It reduces capacitive coupling and thereby makes neutralization more easily attainable in r-f amplifiers.
(5) It provides semi-automatic impedance matching between plate and grid tuned circuits, with the result that greater grid drive can be obtained in comparison to capacitive coupling.
(6) It effectively reduces the coupling of harmonic energy.

The link-coupling line and links can be made of no. 18 push-back wire for coupling between low-power stages. For coupling between higher powered stages the 150-ohm Twin-Lead transmission line is quite effective and has very low loss. Coaxial transmission is most satisfactory between high powered amplifier stages, and should always be used where harmonic attenuation is important.

11-14 Radio-Frequency Chokes

Radio-frequency chokes are connected in circuits for the purpose of stopping the passage of r-f energy while still permitting a direct current or audio-frequency current to pass. They consist of inductances wound with a large number of turns, either in the form of a solenoid, a series of solenoids, a single universal pie winding, or a series of pie windings. These inductors are designed to have as much inductance and as little distributed or shunt capacitance as possible. The unavoidable small amount of distributed capacitance resonates the inductance, and this frequency normally should be much lower than the frequency at which the transmitter or receiver circuit is operating. R-f chokes for operation on several bands must be designed carefully so that the impedance of the choke will be extremely high (several hundred thousand ohms) in each of the bands.

The direct current which flows through the r-f choke largely determines the size of wire to be used in the winding. The inductance of r-f chokes for the v-h-f range is much less than for chokes designed for broadcast and ordinary short-wave operation. A very high inductance r-f choke has more distributed capacitance than a smaller one, with the result



PARALLEL PLATE FEED SERIES PLATE FEED

Figure 42

ILLUSTRATING PARALLEL AND SERIES PLATE FEED

Parallel plate feed is desirable from a safety standpoint since the tank circuit is at ground potential with respect to d.c. However, a high-impedance r-f choke is required, and the r-f choke must be able to withstand the peak r-f voltage output of the tube. Series plate feed eliminates the requirement for a high-performance r-f choke, but requires the use of a relatively large value of by-pass capacitance at the bottom end of the tank circuit, as contrasted to the moderate value of coupling capacitance which may be used at the top of the tank circuit for parallel plate feed.

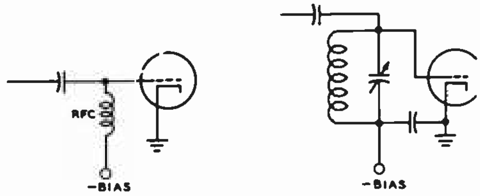
that it will actually offer *less* impedance at very high frequencies.

Another consideration, just as important as the amount of d.c. the winding will carry, is the r-f voltage which may be placed across the choke without its breaking down. This is a function of insulation, turn spacing, frequency, number and spacing of pies and other factors.

Some chokes which are designed to have a high impedance over a very wide range of frequency are, in effect, really two chokes: a u-h-f choke in series with a high-frequency choke. A choke of this type is polarized; that is, it is important that the correct end of the combination choke be connected to the "hot" side of the circuit.

Shunt and Series Feed Direct-current grid and plate connections are made either by *series* or *parallel feed* systems. Simplified forms of each are shown in figures 42 and 43.

Series feed can be defined as that in which the d-c connection is made to the grid or plate circuits at a point of very low r-f potential. Shunt feed always is made to a point of high r-f voltage and always requires a high impedance r-f choke or a relatively high resistance to prevent waste of r-f power.



PARALLEL BIAS FEED SERIES BIAS FEED

Figure 43

ILLUSTRATING SERIES AND PARALLEL BIAS FEED

11-15 Parallel and Push-Pull Tube Circuits

The comparative r-f power output from parallel or push-pull operated amplifiers is the same if proper impedance matching is accomplished, if sufficient grid excitation is available in both cases, and if the frequency of measurement is considerably lower than the frequency limit of the tubes.

Parallel Operation Operating tubes in parallel has some advantages in transmitters designed for operation below 10 Mc., particularly when tetrode or pentode tubes are to be used. Only one neutralizing capacitor is required for parallel operation of triode tubes, as against two for push-pull. Above about 10 Mc., depending upon the tube type, parallel tube operation is not ordinarily recommended with triode tubes. However, parallel operation of grounded-grid stages and stages using low-C beam tetrodes often will give excellent results well into the v-h-f range.

Push-Pull Operation The push-pull connection provides a well-balanced circuit insofar as miscellaneous capacitances are concerned; in addition, the circuit can be neutralized more completely, especially in high-frequency amplifiers. The L/C ratio in a push-pull amplifier can be made higher than in a plate-neutralized parallel-tube operated amplifier. Push-pull amplifiers, when perfectly balanced, have less second-harmonic output than parallel or single-tube amplifiers, but in practice undesired capacitive coupling and circuit unbalance more or less offset the theoretical harmonic-reducing advantages of push-pull r-f circuits.

CHAPTER TWELVE

Amplitude Modulation

If the output of a c-w transmitter is varied in amplitude at an audio frequency rate instead of interrupted in accordance with code characters, a tone will be heard on a receiver tuned to the signal. If the audio signal consists of a band of audio frequencies comprising voice or music intelligence, then the voice or music which is superimposed on the radio frequency carrier will be heard on the receiver.

When voice, music, video, or other intelligence is superimposed on a radio frequency carrier by means of a corresponding variation in the *amplitude* of the radio frequency output of a transmitter, *amplitude modulation* is the result. Telegraph keying of a c-w transmitter is the simplest form of amplitude modulation, while video modulation in a television transmitter represents a highly complex form. Systems for modulating the amplitude of a carrier envelope in accordance with voice, music, or similar types of complicated audio waveforms are many and varied, and will be discussed later on in this chapter.

12-1 Sidebands

Modulation is essentially a form of *mixing* or *combining* already covered in a previous chapter. To transmit voice at radio frequencies by means of amplitude modulation, the voice frequencies are mixed with a radio frequency carrier so that the voice frequencies are converted to radio frequency *sidebands.* Though it may be difficult to visualize, *the amplitude of the radio frequency carrier does not vary during conventional amplitude modulation.*

Even though the amplitude of radio frequency voltage representing the composite signal (resultant of the carrier and sidebands, called the *envelope*) will vary from zero to twice the unmodulated signal value during full modulation, the amplitude of the *carrier* component does not vary. Also, so long as the amplitude of the modulating voltage does not vary, the amplitude of the sidebands will remain constant. For this to be apparent, however, it is necessary to measure the amplitude of each component with a highly selective filter. Otherwise, the measured power or voltage will be a *resultant* of two or more of the components, and the amplitude of the resultant will vary at the modulation rate.

If a carrier frequency of 5000 kc. is modulated by a pure tone of 1000 cycles, or 1 kc., two sidebands are formed: one at 5001 kc. (the sum frequency) and one at 4999 kc. (the difference frequency). The frequency of each sideband is independent of the amplitude of the modulating tone, or *modulation percentage;* the frequency of each sideband is determined only by the frequency of the modulating tone. This assumes, of course, that the transmitter is not modulated in excess of its linear capability.

When the modulating signal consists of multiple frequencies, as is the case with voice or music modulation, two sidebands will be formed by each modulating frequency (one on each side of the carrier), and the radiated signal will consist of a *band* of frequencies. The *band width*, or *channel* taken up in the frequency spectrum by a conventional double-sideband amplitude-modulated signal, is equal to twice the highest modulating frequency. For example, if the highest modulating frequency is 5000 cycles, then the signal (assuming modulation of complex and varying waveform) will occupy a band extending from 5000 cycles below the carrier to 5000 cycles above the carrier.

Frequencies up to at least 2500 cycles, and preferably 3500 cycles, are necessary for good speech intelligibility. If a filter is incorporated in the audio system to cut out all frequencies above approximately 3000 cycles, the band width of a radio-telephone signal can be limited to 6 kc. without a significant loss in intelligibility. However, if harmonic distortion is introduced subsequent to the filter, as would happen in the case of an overloaded modulator or overmodulation of the carrier, new frequencies will be generated and the signal will occupy a band wider than 6 kc.

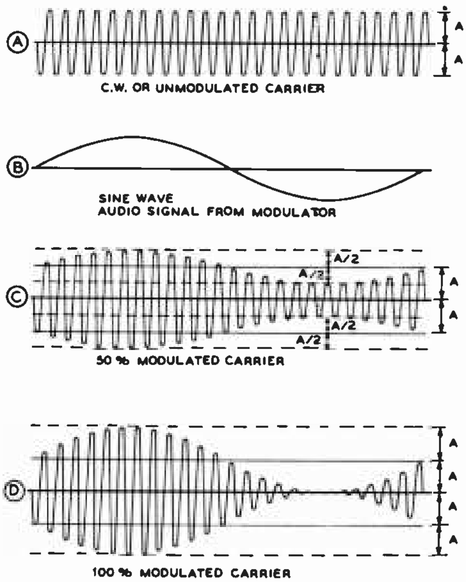


Figure 1
AMPLITUDE MODULATED WAVE

Top drawing (A) represents an unmodulated carrier wave; (B) shows the audio output of the modulator. Drawing (C) shows the audio signal impressed on the carrier wave to the extent of 50 per cent modulation; (D) shows the carrier with 100 per cent amplitude modulation.

12-2 Mechanics of Modulation

A c-w or unmodulated r-f carrier wave is represented in figure 1A. An audio frequency sine wave is represented by the curve of figure 1B. When the two are combined or "mixed," the carrier is said to be amplitude modulated, and a resultant similar to 1C or 1D is obtained. It should be noted that under modulation, each half cycle of r-f voltage differs slightly from the preceding one and the following one; therefore at no time during modulation is the r-f waveform a pure sine wave. This is simply another way of saying that during modulation, the transmitted r-f energy no longer is confined to a single radio frequency.

It will be noted that the *average* amplitude of the peak r-f voltage, or modulation envelope, is the same with or without modulation. This simply means that the modulation is symmetrical (assuming a symmetrical modulating wave) and that for distortionless modulation the upward modulation is limited to a value of twice the unmodulated carrier wave amplitude because the amplitude cannot go below zero on downward portions of the modulation cycle. Figure 1D illustrates the maximum obtainable distortionless modulation with a sine modulating wave, the r-f voltage at the peak of the r-f cycle varying from zero to twice the unmodulated value, and the r-f power varying from zero to four times the unmodulated value (the power varies as the square of the voltage).

While the average r-f *voltage* of the modulated wave over a modulation cycle is the same as for the unmodulated carrier, the average *power* increases with modulation. If the radio frequency power is integrated over the audio cycle, it will be found with 100 per cent sine wave modulation the average r-f power has increased 50 per cent. This additional power is represented by the sidebands, because as previously mentioned, the carrier power does not vary under modulation. Thus, when a 100-watt carrier is modulated 100 per cent by a sine wave, the total r-f power is 150 watts; 100 watts in the carrier and 25 watts in each of the two sidebands.

Modulation Percentage So long as the *relative proportion* of the various sidebands making up voice modulation is maintained, the signal may be received and detected without distortion. However, the higher the average amplitude of the sidebands, the greater the audio signal produced at the receiver. For this reason it is desirable to increase the *modulation percentage,* or degree of modulation, to the point where maximum peaks just hit 100 per cent. If the modulation percentage is increased so that the peaks exceed this value, distortion is introduced, and if carried very far, bad interference to signals on nearby channels will result.

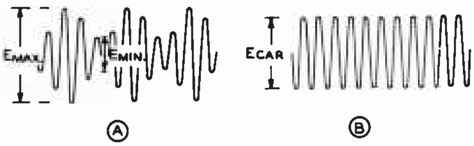


Figure 2

GRAPHICAL DETERMINATION OF MODULATION PERCENTAGE

The procedure for determining modulation percentage from the peak voltage points indicated is discussed in the text.

Modulation Measurement The amount by which a carrier is being modulated may be expressed either as a modulation factor, varying from zero to 1.0 at maximum modulation, or as a percentage. The percentage of modulation is equal to 100 times the modulation factor. Figure 2A shows a carrier wave modulated by a sine-wave audio tone. A picture such as this might be seen on the screen of a cathode-ray oscilloscope with sawtooth sweep on the horizontal plates and the modulated carrier impressed on the vertical plates. The same carrier without modulation would appear on the oscilloscope screen as figure 2B.

The percentage of modulation of the positive peaks and the percentage of modulation of the negative peaks can be determined separately from two oscilloscope pictures such as shown.

The modulation factor of the positive peaks may be determined by the formula:

$$M = \frac{E_{max} - E_{car}}{E_{car}}$$

The factor for negative peaks may be determined from this formula:

$$M = \frac{E_{car} - E_{min}}{E_{car}}$$

In the above two formulas E_{max} is the maximum carrier amplitude with modulation and E_{min} is the minimum amplitude; E_{car} is the steady-state amplitude of the carrier without modulation. Since the deflection of the spot on a cathode-ray tube is linear with respect to voltage, the relative voltages of these various amplitudes may be determined by measuring the deflections, as viewed on the screen, with a rule calibrated in inches or centimeters. The percentage of modulation of the carrier may be had by multiplying the modulation factor thus obtained by 100. The above procedure assumes that there is no *carrier shift,* or change in average amplitude, with modulation.

If the modulating voltage is symmetrical, such as a sine wave, and modulation is accomplished without the introduction of distortion, then the percentage modulation will be the same for both negative and positive peaks. However, the distribution and phase relationships of harmonics in voice and music waveforms are such that the percentage modulation of the negative modulation peaks may exceed the percentage modulation of the positive peaks, and vice versa. The percentage modulation when referred to without regard to polarity is an indication of the average of the negative and positive peaks.

Modulation Capability The modulation capability of a transmitter is the maximum percentage to which that transmitter may be modulated before spurious sidebands are generated in the output or before the distortion of the modulating waveform becomes objectionable. The highest modulation capability which *any* transmitter may have on the *negative* peaks is 100 per cent. The maximum permissible modulation of many transmitters is less than 100 per cent, especially on positive peaks. The modulation capability of a transmitter may be limited by tubes with insufficient filament emission, by insufficient excitation or grid bias to a plate-modulated stage, too light loading of any type of amplifier carrying modulated r.f., insufficient power output capability in the modulator, or too much excitation to a grid-modulated stage or a Class B linear amplifier. In any case, the FCC regulations specify that no transmitter be modulated in excess of its modulation capability. Hence, it is desirable to make the modulation capability of a transmitter as near as possible to 100 per cent so that the carrier power may be used most effectively.

Speech Waveform Dissymmetry The manner in which the human voice is produced by the vocal cords gives rise to a certain dissymmetry in the waveform of voice sounds when they are picked up by a good-quality microphone. This is especially pronounced in the male voice, and more so on certain voiced sounds than on others. The result of this dissymmetry in the waveform is that the voltage peaks on one side of the average value of the wave will be considerably greater, often two or three times as great, as the voltage excursions on the other side of the zero axis. The *average* value of voltage on both sides of the wave is, of course, the same.

As a result of this dissymmetry in the male voice waveform, there is an optimum polarity of the modulating voltage that must be observed if maximum sideband energy is to be obtained without negative peak clipping and generation of "splatter" on adjacent channels.

A double-pole double-throw "phase reversing" switch in the input or output leads of any transformer in the speech amplifier system will permit poling the extended peaks in the direction of maximum modulation capability. The optimum polarity may be determined easily by listening on a selective receiver tuned to a frequency 30 to 50 kc. removed from the desired signal and adjusting the phase reversing switch to the position which gives the least "splatter" when the transmitter is modulated rather heavily. If desired, the switch then may be replaced with permanent wiring, so long as the microphone and speech system are not to be changed.

A more conclusive illustration of the lopsidedness of a speech waveform may be obtained by observing the modulated waveform of a radiotelephone transmitter on an oscilloscope. A portion of the carrier energy of the transmitter should be coupled by means of a link directly to the vertical plates of the 'scope, and the horizontal sweep should be a sawtooth or similar wave occurring at a rate of approximately 30 to 70 sweeps per second.

With the speech signal from the speech amplifier connected to the transmitter in one polarity it will be noticed that negative-peak clipping—as indicated by bright "spots" in the center of the 'scope pattern whenever the carrier amplitude goes to zero—will occur at a considerably lower level of average modulation than with the speech signal being fed to the transmitter in the other polarity. When the input signal to the transmitter is polarized in such a manner that the "fingers" of the speech wave extend in the direction of positive modulation these fingers usually will be clipped in the plate circuit of the modulator at an acceptable peak modulation level.

The use of the proper polarity of the incoming speech wave in modulating a transmitter can afford an increase of approximately two to one in the amount of speech audio power which may be placed upon the carrier for an amplitude-modulated transmitter for the same amount of sideband splatter. More effective methods for increasing the amount of audio power on the carrier of an AM phone transmitter are discussed later in this chapter.

Single-Sideband Transmission Because the same intelligibility is contained in each of the sidebands associated with a modulated carrier, it is not necessary to transmit sidebands on both sides of the carrier. Also, because the carrier is simply a single radio frequency wave of unvarying amplitude, it is not necessary to transmit the carrier if some means is provided for inserting a locally generated carrier at the receiver.

When the carrier is suppressed but both upper and lower sidebands are transmitted, it is necessary to insert a locally generated carrier at the receiver of *exactly* the same frequency and phase as the carrier which was suppressed. For this reason, suppressed-carrier double-sideband systems have little practical application.

When the carrier is suppressed and only the upper *or* the lower sideband is transmitted, a highly intelligible signal may be obtained at the receiver even though the locally generated carrier differs a few cycles from the frequency of the carrier which was suppressed at the transmitter. A communications system utilizing but one group of sidebands with carrier suppressed is known as a *single sideband system*. Such systems are widely used for commercial point to point work, and are being used to an increasing extent in amateur communication. The two chief advantages of the system are: (1) an effective power gain of about 9 db results from putting all the radiated power in intelligence carrying sideband frequencies instead of mostly into radiated carrier, and (2) elimination of the selective fading and distortion that normally occurs in a conventional double-sideband system when the carrier fades and the sidebands do not, or the sidebands fade differently.

12-3 Systems of Amplitude Modulation

There are many different systems and methods for amplitude modulating a carrier, but most may be grouped under three general classifications: (1) *variable efficiency* systems in which the average input to the stage remains constant with and without modulation and the variations in the efficiency of the stage in accordance with the modulating signal accomplish the modulation; (2) *constant efficiency* systems in which the input to the stage is varied by an external source of modulating energy to accomplish the modulation; and (3) so-called *high-efficiency* systems in which circuit complexity is increased to ob-high plate circuit efficiency in the modulated stage without the requirement of an external high-level modulator. The various systems under each classification have individual characteristics which make certain ones best suited to particular applications.

Variable Efficiency Modulation Since the *average* input remains constant in a stage employing variable efficiency modulation, and since the average power output of the stage increases with modulation, the additional average power output from the stage *with* modulation must come from the plate dissipation of the tubes in the stage. Hence, for the best relation between tube cost and power output the tubes employed should have as high a plate dissipation rating per dollar as possible.

The plate efficiency in such an amplifier is doubled when going from the unmodulated condition to the peak of the modulation cycle. Hence, the unmodulated efficiency of such an amplifier *must always be less than 45 per cent,* since the maximum peak efficiency obtainable in a conventional amplifier is in the vicinity of 90 per cent. Since the peak efficiency in certain types of amplifiers will be as low as 60 per cent, the unmodulated efficiency in such amplifiers will be in the vicinity of 30 per cent.

Assuming a typical amplifier having a peak efficiency of 70 per cent, the following figures give an idea of the operation of an idealized efficiency-modulated stage adjusted for 100 per cent sine-wave modulation. It should be kept in mind that the plate voltage is constant at all times, even over the audio cycles.

Plate input without modulation........100 watts
Output without modulation.............. 35 watts
Efficiency without modulation......... 35%

Input on 100% positive modulation
peak (plate current doubles)........200 watts
Efficiency on 100% positive peak.... 70%
Output on 100% positive modulation peak................................140 watts

Input on 100% negative peak.......... 0 watts
Efficiency on 100% negative peak.... 0%
Output on 100% negative peak........ 0 watts

Average input with 100% modulation.............................100 watts
Average output with 100% modulation (35 watts carrier plus 17.5 watts sideband) ....52.5 watts
Average efficiency with 100% modulation.............................52.5%

Systems of Efficiency Modulation There are many systems of efficiency modulation, but they *all* have the general limitation discussed in the previous paragraph—so long as the carrier amplitude is to remain constant with and without modulation, the efficiency at carrier level must be not greater than one-half the peak modulation efficiency if the stage is to be capable of 100 per cent modulation.

The classic example of efficiency modulation is the Class B linear r-f amplifier, to be discussed below. The other three common forms of efficiency modulation are control-grid modulation, screen-grid modulation, and suppressor-grid modulation. In each case, including that of the Class B linear amplifier, note that the modulation, or the modulated signal, is impressed on a control electrode of the stage.

The Class B Linear Amplifier This is the simplest practicable type amplifier for an amplitude-modulated wave or a single-sideband signal. The system possesses the disadvantage that excitation, grid bias, and loading must be carefully controlled to preserve the linearity of the stage. Also, the grid circuit of the tube, in the usual application where grid current is drawn on peaks, presents a widely varying value of load impedance to the source of excitation. Hence it is necessary to include some sort of *swamping resistor* to reduce the effect of grid-impedance variations with modulation. If such a swamping resistance across the grid tank is not included, or is too high in value, the positive modulation peaks of the incoming modulated signal will tend to be flattened with resultant distortion of the wave being amplified.

The Class B linear amplifier has long been used in broadcast transmitters, but recently has received much more general usage in the h-f range for two significant reasons: (a) the Class B linear is an excellent way of increasing the power output of a single-sideband transmitter, since the plate efficiency with full signal will be in the vicinity of 70 per cent, while with no modulation the input to the stage drops to a relatively low value; and (b) the Class B linear amplifier operates with relatively low harmonic output since the grid bias on the stage normally is slightly less than the value which will cut off plate current to the stage in the absence of excitation.

Since a Class B linear amplifier is biased to *extended* cutoff with no excitation (the grid bias at extended cutoff will be approximately equal to the plate voltage divided by the amplification factor for a triode, and will be approximately equal to the screen voltage divided by the grid-screen mu factor for a tetrode or pentode) the plate current will flow essentially in 180-degree pulses. Due to the relatively large operating angle of plate current flow the theoretical peak plate efficiency is limited to 78.5 per cent, with 65 to 70 per cent representing a range of efficiency normally attainable, and the harmonic output will be low.

The carrier power output from a Class B linear amplifier of a normal 100 per cent modulated AM signal will be about one-half the rated plate dissipation of the stage, with optimum operating conditions. The peak output from a Class B linear, which represents the maximum-signal output as a single-sideband amplifier, or peak output with a 100 per cent AM signal, will be about twice the plate dissipation of the tubes in the stage. Thus the carrier-level input power to a Class B linear should be about 1.5 times the rated plate dissipation of the stage.

The schematic circuit of a Class B linear amplifier is the same as a conventional single-ended or push-pull stage, whether triodes or beam tetrodes are used. However, a swamping resistor, as mentioned before, must be placed across the grid tank of the stage if the operating conditions of the tube are such that appreciable grid current will be drawn on modulation peaks. Also, a *fixed* source of grid bias must be provided for the stage. A regulated grid-bias power supply is the usual source of negative bias voltage.

Adjustment of a Class B Linear Amplifier With grid bias adjusted to the correct value, and with provision for varying the excitation voltage to the stage and the loading of the plate circuit, a fully modulated signal is applied to the grid circuit of the stage. Then with an oscilloscope coupled to the output of the stage, excitation and loading are varied until the stage is drawing the normal plate input and the output waveshape is a good replica of the input signal. The adjustment procedure normally will require a succession of approximations, until the optimum set of adjustments is attained. Then the modulation being applied to the input signal should be removed to check the linearity. With modulation removed, in the case of a 100 per cent AM signal, the input to the stage should remain constant, and the peak output of the r-f envelope should fall to half the value obtained on positive modulation peaks.

Class C Grid Modulation One widely used system of efficiency modulation for communications work is Class C control-grid bias modulation. The distortion is slightly higher than for a properly operated Class B linear amplifier, but the efficiency is also higher, and the distortion can be kept within tolerable limits for communications work.

Class C grid modulation requires high plate voltage on the modulated stage, if maximum output is desired. The plate voltage is normally run about 50 per cent higher than for maximum output with plate modulation.

The driving power required for operation of a grid-modulated amplifier under these conditions is somewhat more than is required for operation at lower bias and plate voltage, but the increased power output obtainable overbalances the additional excitation requirement. Actually, almost half as much excitation is required as would be needed if the same stage were to be operated as a Class C plate-modulated amplifier. The resistor R across the grid tank of the stage serves as *swamping* to stabilize the r-f driving voltage. At least 50 per cent of the output of the driving stage should be dissipated in this swamping resistor under carrier conditions.

A comparatively small amount of audio power will be required to modulate the amplifier stage 100 per cent. An audio amplifier having 20 watts output will be sufficient to modulate an amplifier with one kilowatt input. Proportionately smaller amounts of audio will be required for lower powered stages. However, the audio amplifier that is being used as the grid modulator should, in any case, either employ low plate resistance tubes such as 2A3's, employ degenerative feedback from the output stage to one of the preceding stages of the speech amplifier, or be resistance loaded with a resistor across the secondary of the modulation transformer. This provision of low driving impedance in the grid modulator is to insure good regulation in the audio driver for the grid modulated stage. Good regulation of both the audio and the r-f drivers of a grid-modulated stage is quite important if distortion-free modulation approaching 100 per cent is desired, because the grid impedance of the modulated stage varies widely over the audio cycle.

A practical circuit for obtaining grid-bias modulation is shown in figure 3. The modulator and bias regulator tube have been combined in a single 6B4G tube.

The regulator-modulator tube operates as a cathode-follower. The average d-c voltage

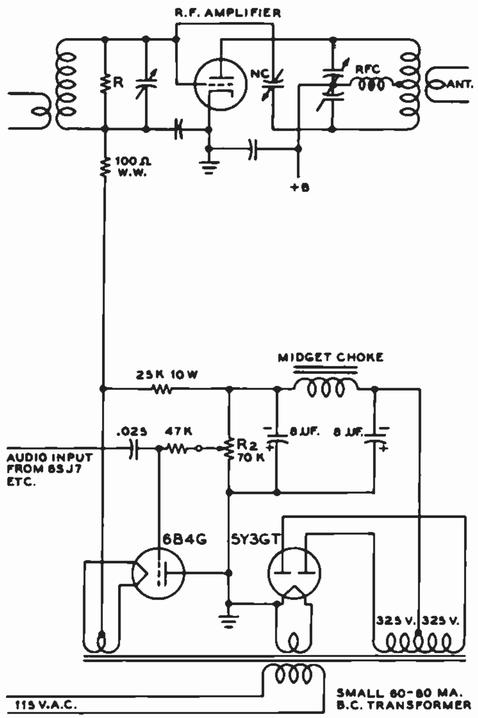


Figure 3
GRID-BIAS MODULATOR CIRCUIT

on the control grid is controlled by the 70,000-ohm wire-wound potentiometer and this potentiometer adjusts the average grid bias on the modulated stage. However, a-c signal voltage is also impressed on the control-grid of the tube and since the cathode follows this a-c wave the incoming speech wave is superimposed on the average grid bias, thus effecting grid-bias modulation of the r-f amplifier stage. An audio voltage swing is required on the grid of the 6B4G of approximately the same peak value as will be required as bias-voltage swing on the grid-bias modulated stage. This voltage swing will normally be in the region from 50 to 200 peak volts. Up to about 100 volts peak swing can be obtained from a 6SJ7 tube as a conventional speech amplifier stage. The higher voltages may be obtained from a tube such as a 6J5 through an audio transformer of 2:1 or 2½:1 ratio.

With the normal amount of comparatively tight antenna coupling to the modulated stage, a non-modulated carrier efficiency of 40 per cent can be obtained with substantially distortion-free modulation up to practically 100 per cent. If the antenna coupling is decreased slightly from the condition just described, and the excitation is increased to the point where the amplifier draws the same input, carrier efficiency of 50 per cent is obtainable with tolerable distortion at 90 per cent modulation.

Tuning the Grid-Bias Modulated Stage The most satisfactory procedure for tuning a stage for grid-bias modulation of the Class C type is as follows. The amplifier should first be neutralized, and any possible tendency toward parasitics under any condition of operation should be eliminated. Then the antenna should be coupled to the plate circuit, the grid bias should be run up to the maximum available value, and the plate voltage and excitation should be applied. The grid bias voltage should then be reduced until the amplifier draws the approximate amount of plate current it is desired to run, and modulation corresponding to about 80 per cent is then applied. If the plate current kicks up when modulation is applied, the grid bias should be reduced; if the plate meter kicks down, increase the grid bias.

When the amount of bias voltage has been found (by adjusting the fine control, R_2, on the bias supply) where the plate meter remains constant with modulation, it is more than probable that the stage will be drawing either too much or too little input. The antenna coupling should then be either increased or decreased (depending on whether the input was too little or too much, respectively) until the input is more nearly the correct value. The bias should then be readjusted until the plate meter remains constant with modulation as before. By slight jockeying back and forth of antenna coupling and grid bias, a point can be reached where the tubes are running at rated plate dissipation, and where the plate milliammeter on the modulated stage remains substantially constant with modulation.

The linearity of the stage should then be checked by any of the conventional methods; the trapezoidal pattern method employing a cathode-ray oscilloscope is probably the most satisfactory. The check with the trapezoidal pattern will allow the determination of the proper amount of gain to employ on the speech amplifier. Too much audio power on the grid of the modulated stage should not be used in the tuning-up process, as the plate meter will kick erratically and it will be impossible to make a satisfactory adjustment.

Screen-Grid Modulation Amplitude modulation may be accomplished by varying the screen-grid voltage in a Class C amplifier which employs a pentode, beam tetrode, or other type of screen-grid tube. The modulation obtained in this way is not especially linear, but screen-grid modulation does offer other advantages and the linearity is quite adequate for communications work.

There are two significant and worthwhile advantages of screen-grid modulation for communications work: (1) The excitation requirements for an amplifier which is to be modulated in the screen are not at all critical, and good regulation of the excitation voltage is not required. The normal rated grid-circuit operating conditions specified for Class C c-w operation are quite adequate for screen-grid modulation. (2) The audio modulating power requirements for screen-grid modulation are relatively low.

A screen-grid modulated r-f amplifier operates as an efficiency-modulated amplifier, the same as does a Class B linear amplifier and a grid-modulated stage. Hence, *plate circuit* loading is relatively critical as in any efficiency-modulated stage, and must be adjusted to the correct value if normal power output with full modulation capability is to be obtained. As in the case of any efficiency-modulated stage, the operating efficiency at the peak of the modulation cycle will be between 70 and 80 per cent, with efficiency at the carrier level (if the stage is operating in the normal manner with full carrier) about half of the peak-modulation value.

There are two main disadvantages of screen-grid modulation, and several factors which must be considered if satisfactory operation of the screen-grid modulated stage is to be obtained. The disadvantages are: (1) As mentioned before, the linearity of modulation with respect to screen-grid voltage of such a stage is satisfactory only for communications work, unless carrier-rectified degenerative feed-back is employed around the modulated stage to straighten the linearity of modulation. (2) The impedance of the screen grid to the modulating signal is non-linear. This means that the modulating signal must be obtained from a source of quite low impedance if audio distortion of the signal appearing at the screen grid is to be avoided.

Screen-Grid Impedance Instead of being linear with respect to modulating voltage, as is the plate circuit of a plate-modulated Class C amplifier, the screen grid presents approximately a square-law impedance to the modulating signal over the region of signal excursion where the screen is positive with respect to ground. This non-linearity may be explained in the following manner: At the carrier level of a conventional screen-modulated stage the plate-voltage swing of the modulated tube is one-half the voltage swing at peak-modulation level. This condition must exist in any type of conventional efficiency-modulated stage if 100 per cent positive modulation is to be attainable. Since the plate-voltage swing is at half amplitude, and since the screen voltage is at half its full-modulation value, the screen current is relatively low. But at the positive modulation peak the screen voltage is approximately doubled, and the plate-voltage swing also is at twice the carrier amplitude. Due to the increase in plate-voltage swing with increasing screen voltage, the screen current increases more than linearly with increasing screen voltage.

In a test made on an amplifier with an 813 tube, the screen current at carrier level was about 6 ma. with screen potential of 190 volts; but under conditions which represented a positive modulation peak the screen current measured 25 ma. at a potential of 400 volts. Thus instead of screen current doubling with twice screen voltage as would be the case if the screen presented a resistive impedance, the screen current became about four times as great with twice the screen voltage.

Another factor which must be considered in the design of a screen-modulated stage, if full modulation is to be obtained, is that the power output of a screen-grid stage with zero screen voltage is still relatively large. Hence, if anything approaching full modulation on negative peaks is to be obtained, the screen potential must be made negative with respect to ground on negative modulation peaks. In the usual types of beam tetrode tubes the screen potential must be 20 to 50 volts negative with respect to ground before cut-off of output is obtained. This condition further complicates the problem of obtaining good linearity in the audio modulating voltage for the screen-modulated stage, since the screen voltage must be driven negatively with respect to ground over a portion of the cycle. Hence the screen draws *no* current over a portion of the modulating cycle, and over the major portion of the cycle when the screen does draw current, it presents approximately a square-law impedance.

Circuits for Screen-Grid Modulation Laboratory analysis of a large number of circuits for accomplishing screen modulation has led to the conclusion that the audio modulating voltage *must* be obtained from a low-impedance source if low-distortion modulation is to be obtained. Figure 4 shows a group of sketches of the modulation envelope obtained with various types of modulators and also with insufficient antenna coupling. The result of this laboratory work led to the conclusion that the cathode-follower modulator of the basic circuit shown in figure

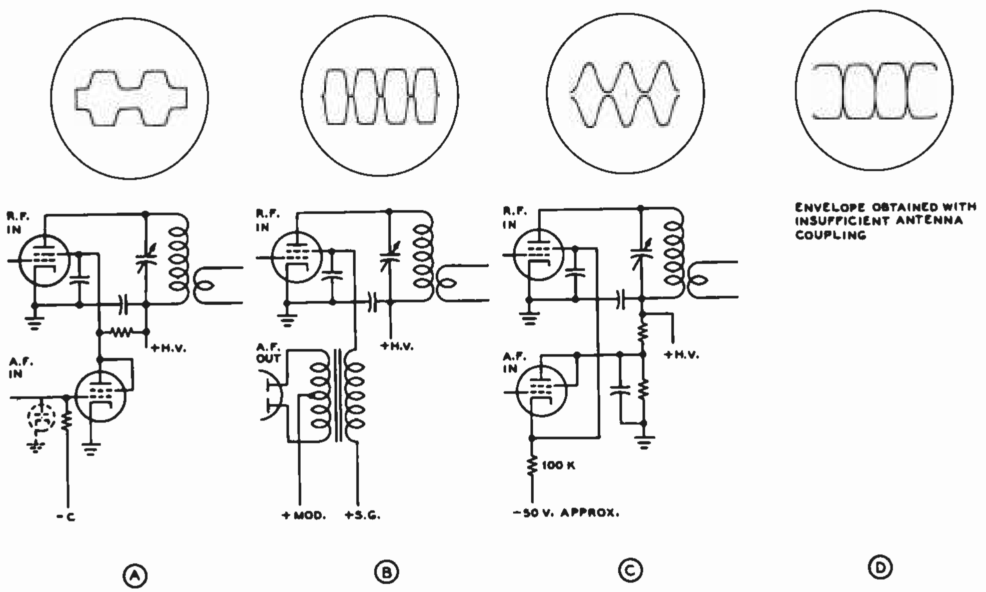


Figure 4

SCREEN-MODULATION CIRCUITS

Three common screen modulation circuits are illustrated above. All three circuits are capable of giving intelligible voice modulation although the waveform distortion in the circuits of (A) and (B) is likely to be rather severe. The arrangement at (A) is often called "clamp tube" screen modulation; by returning the grid leak on the clamp tube to ground the circuit will give controlled-carrier screen modulation. This circuit has the advantage that it is simple and is well suited to use in mobile transmitters. (B) is an arrangement using a transformer coupled modulator, and offers no particular advantages. The arrangement at (C) is capable of giving good modulation linearity due to the low impedance of the cathode-follower modulator. However, due to the relatively low heater-cathode ratings on tubes suited for use as the modulator, a separate heater supply for the modulator tube normally is required. This limitation makes application of the circuit to the mobile transmitter a special problem, since an isolated heater supply normally is not available. Shown at (D) as an assistance in the tuning of a screen-modulated transmitter (or any efficiency-modulated transmitter for that matter) is the type of modulation envelope which results when loading to the modulated stage is insufficient.

5 *is* capable of giving good-quality screen-grid modulation, and in addition the circuit provides convenient adjustments for the carrier level and the output level on *negative* modulation peaks. This latter control, P_2 in figure 5, allows the amplifier to be adjusted in such a manner that negative-peak clipping cannot take place, yet the negative modulation peaks may be adjusted to a level just above that at which sideband splatter will occur.

The Cathode-Follower Modulator The cathode follower is ideally suited for use as the modulator for a screen-grid stage since it acts as a relatively low-impedance source of modulating voltage for the screen-grid circuit. In addition the cathode-follower modulator allows the supply voltage both for the modulator and for the screen grid of the modulated tube to be obtained from the high-voltage supply for the plate of the screen-grid tube or beam tetrode. In the usual case the plate supply for the cathode follower, and hence for the screen grid of the modulated tube, may be taken from the bleeder on the high-voltage power supply. A tap on the bleeder may be used, or two resistors may be connected in series to make up the bleeder, with appropriate values such that the voltage applied to the plate of the cathode follower is appropriate for the tube to be modulated. It is important that a bypass capacitor be used from the plate of the cathode-follower modulator to ground.

The voltage applied to the plate of the cathode follower should be about 100 volts greater than the rated screen voltage for the tetrode tube as a c-w Class C amplifier. Hence the cathode-follower plate voltage should be about 350 volts for an 815, 2E26, or 829B, about 400 volts for an 807 or 4-125A, about 500 volts for an 813, and about 600 volts for a 4-250A or a 4E27. Then potentiometer P_1 in figure 5 should be adjusted until the carrier-level screen voltage on the modulated stage is about one-half the rated screen voltage specified for the tube as a Class C c-w amplifier. The current taken by the screen of the modulated tube under carrier conditions will be about one-fourth the normal screen current for c-w operation.

The only current taken by the cathode follower itself will be that which will flow through the 100,000-ohm resistor between the cathode of the 6L6 modulator and the negative supply. The current taken from the bleeder on the high-voltage supply will be the carrier-level screen current of the tube being modulated (which current passes of course through the cathode follower) plus that current which will pass through the 100,000-ohm resistor.

The loading of the modulated stage should be adjusted until the input to the tube is about 50 per cent greater than the rated plate dissipation of the tube or tubes in the stage. If the carrier-level screen voltage value is correct for linear modulation of the stage, the loading will have to be somewhat *greater* than that amount of loading which gives maximum output from the stage. The stage may then be modulated by applying an audio signal to the grid of the cathode-follower modulator, while observing the modulated envelope on an oscilloscope.

If good output is being obtained, and the modulation envelope appears as shown in figure 4C, all is well, except that P_2 in figure 5 should be adjusted until negative modulation peaks, even with excessive modulating signal, do not cause carrier cutoff with its attendant sideband splatter. If the envelope appears as at figure 4D, antenna coupling should be increased while the carrier level is backed down by potentiometer P_1 in figure 5 until a set of adjustments is obtained which will give a satisfactory modulation envelope as shown in figure 4C.

Changing Bands After a satisfactory set of adjustments has been obtained, it is *not* difficult to readjust the amplifier for operation on different bands. Potentiometers P_1 (carrier level), and P_2 (negative peak level) may be left fixed after a satisfactory adjustment, with the aid of the scope, has once been found. Then when changing bands it is only necessary to adjust excitation until the correct value of grid current is obtained, and then to adjust antenna coupling until correct plate current is obtained. Note that the correct plate current for an efficiency-modulated amplifier is only slightly less than the out-of-resonance plate current of the stage. Hence carrier-level screen voltage must be low so that the out-of-resonance plate current will not be too high, and relatively heavy antenna coupling must be used so that the operating plate current will be near the out-of-resonance value, and so that the operating input will be slightly greater than 1.5 times the rated plate dissipation of the tube or tubes in the stage. Since the carrier efficiency of the stage will be only 35 to 40 per cent, the tubes will be operating with plate dissipation of approximately the rated value without modulation.

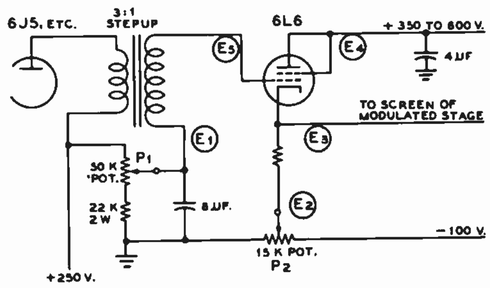


Figure 5

CATHODE-FOLLOWER SCREEN-MODULATION CIRCUIT

A detailed discussion of this circuit, which also is represented in figure 4C, is given in the accompanying text.

Speech Clipping in the Modulated Stage The maximum r-f output of an efficiency-modulated stage is limited by the maximum possible plate voltage swing on positive modulation peaks. In the modulation circuit of figure 5 the *minimum* output is limited by the minimum voltage which the screen will reach on a negative modulation peak, as set by potentiometer P_2. Hence the screen-grid-modulated stage, when using the modulator of figure 5, acts effectively as a speech clipper, provided the modulating signal amplitude is not too much more than that value which will accomplish full modulation. With correct adjustments of the operating conditions of the stage it can be made to clip positive and negative modulation peaks symmetrically. However, the inherent peak clipping ability of the stage should *not* be relied upon as a means of obtaining a large amount of speech compression, since excessive audio distortion and excessive screen current on the modulated stage will result.

Characteristics of a Typical Screen-Modulated Stage An important characteristic of the screen-modulated stage, when using the cathode-follower modulator, is that excessive plate voltage on the modulated stage is not required. In fact, full output usually may be obtained with the larger tubes at an operating plate voltage from one-half to two-thirds the maximum rated plate voltage for c-w operation. This desirable condition is the natural result of using a low-impedance source of modulating signal for the stage.

As an example of a typical screen-modulated stage, full output of 75 watts of carrier may be obtained from an 813 tube operating with a plate potential of only 1250 volts. No increase in output from the 813 may be obtained by increasing the plate voltage, since the tube may be operated with full rated plate dissipation of 125 watts, with normal plate efficiency for a screen-modulated stage, 37.5 per cent, at the 1250-volt potential.

The operating conditions of a screen-modulated 813 stage are as follows:

Plate voltage—1250 volts
Plate current—160 ma.
Plate input—200 watts
Grid current—11 ma.
Grid bias—110 volts
Carrier screen voltage—190 volts
Carrier screen current—6 ma.
Power output—approx. 75 watts

With full 100 per cent modulation the plate current decreases about 2 ma. and the screen current increases about 1 ma.; hence plate, screen, and grid current remain essentially constant with modulation. Referring to figure 5, which was the circuit used as modulator for the 813, (E_1) measured plus 155 volts, (E_2) measured −50 volts, (E_3) measured plus 190 volts, (E_4) measured plus 500 volts, and the r.m.s. swing at (E_5) for full modulation measured 210 volts, which represents a peak swing of about 296 volts. Due to the high positive voltage, and the large audio swing, on the cathode of the 6L6 (triode connected) modulator tube, it is important that the heater of of this tube be fed from a separate filament transformer or filament winding. Note also that the operating plate-to-cathode voltage on the 6L6 modulator tube does not exceed the 360-volt rating of the tube, since the operating potential of the cathode is considerably above ground potential.

Suppressor-Grid Modulation Still another form of efficiency modulation may be obtained by applying the audio modulating signal to the suppressor grid of a pentode Class C r-f amplifier. Basically, suppressor-grid modulation operates in the same general manner as other forms of efficiency modulation; carrier plate circuit efficiency is about 35 per cent, and antenna coupling must be rather tight. However, suppressor-grid modulation has one sizeable disadvantage, in addition to the fact that pentode tubes are not nearly so widely used as beam tetrodes which of course do not have the suppressor element. This disadvantage is that the screen-grid current to a suppressor-grid modulated amplifier is rather high. The high screen current is a natural consequence of the rather high negative bias on the suppressor grid, which reduces the plate-voltage swing and plate current with a resulting increase in the screen current.

In tuning a suppressor-grid modulated amplifier, the grid bias, grid current, screen voltage, and plate voltage are about the same as for Class C c-w operation of the stage. But the suppressor grid is biased negatively to a value which reduces the plate-circuit efficiency to about one-half the maximum obtainable from the particular amplifier, with antenna coupling adjusted until the plate input is about 1.5 times the rated plate dissipation of the stage. It is important that the input to the screen grid be measured to make sure that the rated screen dissipation of the tube is not being exceeded. Then the audio signal is applied to the suppressor grid. In the normal application the audio voltage swing on the suppressor will be somewhat greater than the negative bias on the element. Hence suppressor-grid current will flow on modulation peaks, so that the source of audio signal voltage must have good regulation. Tubes suitable for suppressor-grid modulation are: 2E22, 837, 4E27/8001, 5-125, 804 and 803. A typical suppressor-grid modulated amplifier is illustrated in figure 6.

12-4 Input Modulation Systems

Constant efficiency variable-input modulation systems operate by virtue of the addition

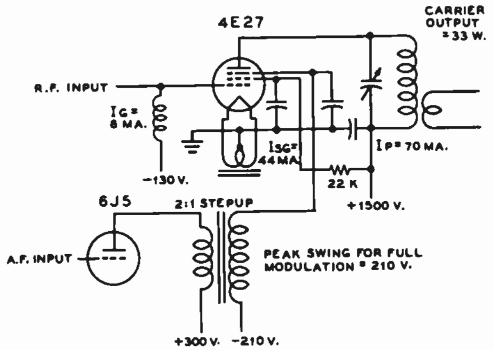


Figure 6

AMPLIFIER WITH SUPPRESSOR-GRID MODULATION

Recommended operating conditions for linear suppressor-grid modulation of a 4E27/257B/8001 stage are given on the drawing.

of external power to the modulated stage to effect the modulation. There are two general classifications that come under this heading; those systems in which the additional power is supplied as audio frequency energy from a modulator, usually called plate modulation systems, and those systems in which the additional power to effect modulation is supplied as direct current from the plate supply.

Under the former classification comes Heising modulation (probably the oldest type of modulation to be applied to a continuous carrier), Class B plate modulation, and series modulation. These types of plate modulation are by far the easiest to get into operation, and they give a very good ratio of power input to the modulated stage to power output; 65 to 80 per cent efficiency is the general rule. It is for these two important reasons that these modulation systems, particularly Class B plate modulation, are at present the most popular for communications work.

Modulation systems coming under the second classification are of comparatively recent development but have been widely applied to broadcast work. There are quite a few systems in this class. Two of the more widely used are the Doherty linear amplifier, and the Terman-Woodyard high-efficiency grid-modulated amplifier. Both systems operate by virtue of a carrier amplifier and a peak amplifier connected together by electrical quarter-wave lines. They will be described later in this section.

Plate Modulation Plate modulation is the application of the audio power to the *plate circuit* of an r-f amplifier. The r-f amplifier must be operated Class C for this type of modulation in order to obtain a radio-frequency output which changes in exact accordance with the variation in plate voltage. *The r-f amplifier is 100 per cent modulated when the peak a-c voltage from the modulator is equal to the d.c. voltage applied to the r-f tube.* The positive peaks of audio voltage increase the instantaneous plate voltage on the r-f tube to *twice* the d-c value, and the negative peaks reduce the voltage to zero.

The instantaneous plate *current* to the r-f stage also varies in accordance with the modulating voltage. The peak alternating current in the output of a modulator must be equal to the d-c plate current of the Class C r-f stage at the point of 100 per cent modulation. This combination of change in audio voltage and current can be most easily referred to in terms of *audio power in watts.*

In a sinusoidally modulated wave, the antenna current increases approximately 22 per cent for 100 per cent modulation with a pure tone input; an r-f meter in the antenna circuit indicates this increase in antenna current. The *average power* of the r-f wave increases 50 per cent for 100 per cent modulation, the efficiency remaining constant.

This indicates that in a plate-modulated radiotelephone transmitter, the audio-frequency channel must supply this additional 50 per cent increase in average power for sine-wave modulation. If the power input to the modulated stage is 100 watts, for example, the *average power* will increase to 150 watts at 100 per cent modulation, and this additional 50 watts of power must be supplied by the *modulator* when plate modulation is used. The actual antenna power is a constant percentage of the total value of input power.

One of the advantages of plate (or power) modulation is the ease with which proper adjustments can be made in the transmitter. Also, there is less plate loss in the r-f amplifier for a given value of carrier power than with other forms of modulation because the plate efficiency is higher.

By properly matching the plate impedance of the r-f tube to the output of the modulator, the ratio of voltage and current swing to d-c voltage and current is automatically obtained. The modulator should have a peak voltage output equal to the average d-c plate voltage on the modulated stage. The modulator should also have a *peak power* output equal to the d-c plate input power to the modulated stage.

The *average* power output of the modulator will depend upon the type of waveform. If the amplifier is being Heising modulated by a Class A stage, the modulator must have an average

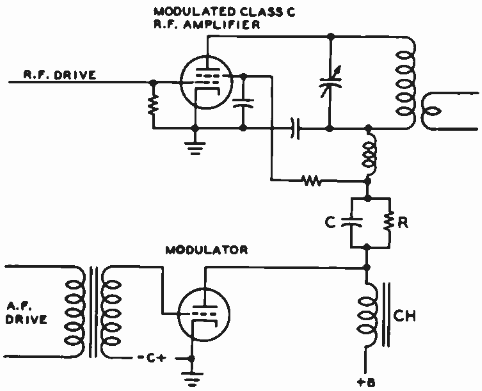


Figure 7
HEISING PLATE MODULATION

This type of modulation was the first form of plate modulation. It is sometimes known as "constant current" modulation. Because of the effective 1:1 ratio of the coupling choke, it is impossible to obtain 100 per cent modulation unless the plate voltage to the modulated stage is dropped slightly by resistor R. The capacitor C merely bypasses the audio around R, so that the full a-f output voltage of the modulator is impressed on the Class C stage.

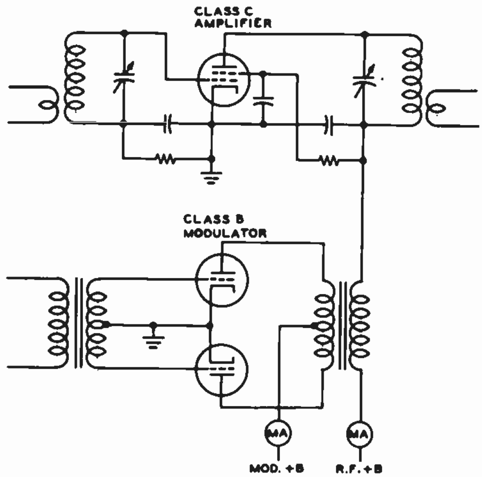


Figure 8
CLASS B PLATE MODULATION

This type of modulation is the most flexible in that the loading adjustment can be made in a short period of time and without elaborate test equipment after a change in operating frequency of the Class C amplifier has been made.

power output capability of one-half the input to the Class C stage. If the modulator is a Class B audio amplifier, the average power required of it may vary from one-quarter to more than one-half the Class C input depending upon the waveform. However, the *peak* power output of any modulator must be equal to the Class C input to be modulated.

Heising Modulation Heising modulation is the oldest system of plate modulation, and usually consists of a Class A audio amplifier coupled to the r-f amplifier by means of a modulation choke coil, as shown in figure 7.

The d.c. plate voltage and plate current in the r-f amplifier must be adjusted to a value which will cause the plate impedance to match the output of the modulator, since the modulation choke gives a 1-to-1 coupling ratio. A series resistor, by-passed for audio frequencies by means of a capacitor, must be connected in series with the plate of the r-f amplifier to obtain modulation up to 100 per cent. The peak output voltage of a Class A amplifier does not reach a value equal to the d-c voltage applied to the amplifier and, consequently, the d-c plate voltage impressed across the r-f tube must be reduced to a value equal to the maximum available a-c peak voltage if 100% modulation is to be obtained.

A higher degree of distortion can be tolerated in low-power emergency phone transmitters which use a pentode modulator tube, and the series resistor and by-pass capacitor are usually omitted in such transmitters.

Class B Plate Modulation High-level Class B plate modulation is the least expensive method of plate modulation. Figure 8 shows a conventional Class B plate-modulated Class C amplifier.

The statement that the modulator output power must be one-half the Class C input for 100 per cent modulation is correct only if the waveform of the modulating power is a *sine wave.* Where the modulator waveform is unclipped speech, the average modulator power for 100 per cent modulation is considerably less than one-half the Class C input.

Power Relations in Speech Waveforms It has been determined experimentally that the ratio of peak to average power in a speech waveform is approximately 4 to 1 as contrasted to a ratio of 2 to 1 in a sine wave. This is due to the high harmonic content of such a waveform, and to the fact that this high harmonic content manifests itself by making the wave unsymmetrical and causing sharp peaks or "fingers" of high energy content to appear. Thus for unclipped speech, the *average* modulator plate current, plate dissipation, and power output are approximately one-half the sine wave values for a given *peak* output power.

Both peak power and average power are necessarily associated with waveform. *Peak* power is just what the name implies; the power at the peak of a wave. Peak power, although of the utmost importance in modulation, is of no great significance in a-c power work, except insofar as the *average* power may be determined from the peak value of a known wave form.

There is no time element implied in the definition of peak power; peak power may be instantaneous—and for this reason average power, which is definitely associated with time, is the important factor in plate dissipation. It is possible that the peak power of a given waveform be several times the average value; for a sine wave, the peak power is twice the average value, and for unclipped speech the peak power is approximately four times the *average* value. For 100 per cent modulation, the *peak* (instantaneous) audio power must equal the Class C input, although the average power for this value of peak varies widely depending upon the modulator waveform, being greater than 50 per cent for speech that has been clipped and filtered, 50 per cent for a sine wave, and about 25 per cent for typical unclipped speech tones.

Modulation Transformer Calculations The modulation transformer is a device for matching the load impedance of the Class C amplifier to the recommended load impedance of the Class B modulator tubes. Modulation transformers intended for communications work are usually designed to carry the Class C plate current through their secondary windings, as shown in figure 8. The manufacturer's ratings should be consulted to insure that the d-c plate current passed through the secondary winding does not exceed the maximum rating.

A detailed discussion of the method of making modulation transformer calculations has been given in Chapter Six. However, to emphasize the method of making the calculation, an additional example will be given.

Suppose we take the case of a Class C amplifier operating at a plate voltage of 2000 with 225 ma. of plate current. This amplifier would present a load resistance of 2000 divided by 0.225 amperes or 8888 ohms. The plate power input would be 2000 times 0.225 or 450 watts. By reference to Chapter Six we see that a pair of 811 tubes operating at 1500 plate volts will deliver 225 watts of audio output. The plate-to-plate load resistance for these tubes under the specified operating conditions is 18,000 ohms. Hence our problem is to match the Class C amplifier load resistance of 8888 ohms to the 18,000-ohm load resistance required by the modulator tubes.

A 200-to-300 watt modulation transformer will be required for the job. If the taps on the transformer are given in terms of impedances it will only be necessary to connect the secondary for 8888 ohms (or a value approximately equal to this such as 9000 ohms) and the primary for 18,000 ohms. If it is necessary to determine the proper turns ratio required of the transformer it can be determined in the following manner. The square root of the impedance ratio is equal to the turns ratio, hence:

$$\sqrt{\frac{8888}{18000}} = \sqrt{0.494} = 0.703$$

The transformer must have a turns ratio of approximately 1-to-0.7 step down, total primary to total secondary. The greater number of turns always goes with the higher impedance, and vice versa.

Plate-and-Screen Modulation When *only* the plate of a screen-grid tube is modulated, it is impossible to obtain high-percentage linear modulation under ordinary conditions. The plate current of such a stage is not linear with plate voltage. However, if the screen is modulated simultaneously with the plate, the instantaneous screen voltage drops in proportion to the drop in the plate voltage, and linear modulation can then be obtained. Four satisfactory circuits for accomplishing combined plate and screen modulation are shown in figure 9.

The screen r-f by-pass capacitor C_2, should not have a greater value than 0.005 μfd., preferably not larger than 0.001 μfd. It should be large enough to bypass effectively all r-f voltage without short-circuiting high-frequency audio voltages. The plate by-pass capacitor can be of any value from 0.002 μfd. to 0.005 μfd. The screen-dropping resistor, R_1, should reduce the applied high voltage to the value specified for operating the particular tube in the circuit. Capacitor C_1 is seldom required yet some tubes may require this capacitor in order to keep C_2 from attenuating the high frequencies. Different values between .0002 and .002 μfd. should be tried for best results.

Figure 9C shows another method which uses a third winding on the modulation transformer, through which the screen-grid is connected to

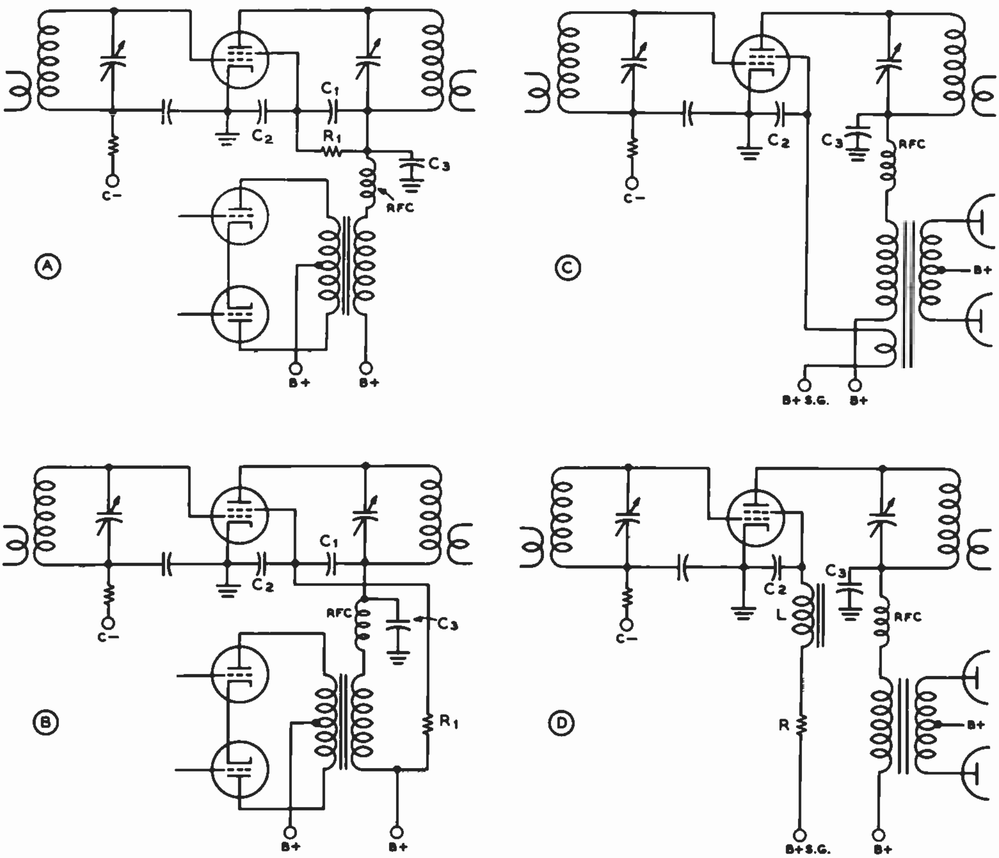


Figure 9

PLATE MODULATION OF A BEAM TETRODE OR SCREEN-GRID TUBE

These alternative arrangements for plate modulation of tetrodes or pentodes are discussed in detail in the text. The arrangements shown at (B) or (D) are recommended for most applications.

a low-voltage power supply. The ratio of turns between the two output windings depends upon the type of screen-grid tube which is being modulated. Normally it will be such that the screen voltage is being modulated 60 per cent when the plate voltage is receiving 100 per cent modulation.

If the screen voltage is derived from a dropping resistor (*not* a divider) that is bypassed for r.f. but not a.f., it is possible to secure quite good modulation by applying modulation only to the plate. Under these conditions, the screen tends to modulate itself, the screen voltage varying over the audio cycle as a result of the screen impedance increasing with plate voltage, and decreasing with a decrease in plate voltage. This circuit arrangement is illustrated in figure 9B.

A similar application of this principle is shown in figure 9D. In this case the screen voltage is fed directly from a low-voltage supply of the proper potential through a choke L. A conventional filter choke having an inductance from 10 to 20 henries will be satisfactory for L.

To afford protection of the tube when plate voltage is not applied but screen voltage is supplied from the exciter power supply, when using the arrangement of figure 9D, a resistor of 3000 to 10,000 ohms can be connected in series with the choke L. In this case the screen supply voltage should be at least 1½ times as much as is required for actual screen voltage, and the value of resistor is chosen such that with normal screen current the drop through the resistor and choke will be such that normal screen voltage will be applied to the tube. When the plate voltage is removed the screen current will increase greatly and the drop through resistor R will increase to such a value that the screen voltage will be lowered to the point where the screen dissipation on the tube will not be exceeded. However, the supply voltage and value of resistor R must be chosen carefully so that the maximum rated screen dissipation cannot be exceeded. The maximum possible screen dissipation using this arrangement is equal to: $W = E^2/4R$ where E is the screen supply voltage and R is the combined resistance of the resistor in figure 9D and the d-c resistance of the choke L. It is wise, when using this arrangement to check, using the above formula, to see that the value of W obtained is less than the maximum rated screen dissipation of the tube or tubes used in the modulated stage. This same system can of course also be used in figuring the screen supply circuit of a pentode or tetrode amplifier stage where modulation is not to be applied.

The modulation transformer for plate-and-screen-modulation, when utilizing a dropping resistor as shown in figure 9A, is similar to the type of transformer used for any plate modulated phone. The combined screen and plate current is divided into the plate voltage in order to obtain the Class C amplifier load impedance. The peak audio power required to obtain 100 per cent modulation is equal to the d-c power input to the screen, screen resistor, and plate of the modulated r-f stage.

12-5 Cathode Modulation

Cathode modulation offers a workable compromise between the good plate efficiency but expensive modulator of high-level plate modulation, and the poor plate efficiency but inexpensive modulator of grid modulation. Cathode modulation consists essentially of an admixture of the two.

The efficiency of the average well-designed plate-modulated transmitter is in the vicinity of 75 to 80 per cent, with a compromise perhaps at 77.5 per cent. On the other hand, the efficiency of a good grid-modulated transmitter may run from 28 to maybe 40 per cent, with the average falling at about 34 per cent. Now since cathode modulation consists of simultaneous grid and plate modulation, in phase with each other, we can theoretically obtain any efficiency from about 34 to 77.5 per cent from our cathode-modulated stage, depending upon the relative percentages of grid and plate modulation.

Since the system is a compromise between the two fundamental modulation arrangements, a value of efficiency approximately half way between the two would seem to be the best compromise. Experience has proved this to be the case. A compromise efficiency of about 56.5 per cent, roughly half way between the two limits, has proved to be optimum. Calculation has shown that this value of efficiency can be obtained from a cathode-modulated amplifier when the audio-frequency modulating power is approximately 20 per cent of the d-c input to the cathode-modulated stage.

An Economical Series Cathode Modulator Series cathode modulation is ideally suited as an economical modulating arrangement for a high-power triode c-w transmitter. The modulator can be constructed quite compactly and for a minimum component cost since no power supply is required for it. When it is desired to change over from c-w to 'phone, it is only necessary to cut the series modulator into the cathode return circuit of the c-w amplifier stage. The plate voltage for the modulator tubes and for the speech amplifier is taken from the cathode voltage drop of the modulated stage across the modulator unit.

Figure 10 shows the circuit of such a modulator, designed to cathode modulate a Class C amplifier using push-pull 810 tubes, running at a supply voltage of 2500, and with a plate input of 660 watts. The modulated stage runs at about 50% efficiency, giving a power output of nearly 350 watts, fully modulated. The voltage drop across the cathode modulator is 400 volts, allowing a net plate to cathode voltage of 2100 volts on the final amplifier. The plate current of the 810's should be about 330 ma., and the grid current should be approximately 40 ma., making the total cathode current of the modulated stage 370 ma. Four parallel 6L6 modulator tubes can pass this amount of plate current without difficulty. It must be remembered that the voltage drop across the cathode modulator is also the cathode bias of the modulated stage. In most cases, no extra grid bias is necessary. If a bias supply is used for c-w operation, it may be removed for cathode modulation, as shown in figure 11. With low-mu triodes, some extra grid bias (over and above that amount supplied by the cathode modulator) may be needed to achieve proper linearity of the modulated stage. In any case, proper operation of a cathode modulated stage should be determined by examining the modulated output waveform of the stage on an oscilloscope.

Excitation The r-f driver for a cathode-modulated stage should have about

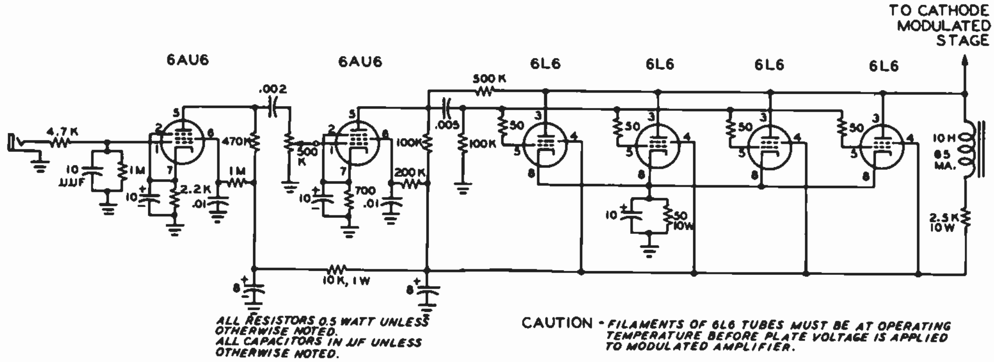


Figure 10

SERIES CATHODE MODULATOR FOR A HIGH-POWERED TRIODE R-F AMPLIFIER

the same power output capabilities as would be required to drive a c-w amplifier to the same input as it is desired to drive the cathode-modulated stage. However, some form of excitation control should be available since the amount of excitation power has a direct bearing on the linearity of a cathode-modulated amplifier stage. If link coupling is used between the driver and the modulated stage, variation in the amount of link coupling will afford ample excitation variation. If much less than 40% plate modulation is employed, the stage begins to resemble a grid-bias modulated stage, and the necessity for good r-f regulation will apply.

Cathode Modulation of Tetrodes Cathode modulation has not proved too satisfactory for use with beam tetrode tubes. This is a result of the small excitation and grid swing requirements for such tubes, plus the fact that some means for holding the screen voltage at the potential of the cathode as far as audio is concerned is usually necessary. Because of these factors, cathode modulation is not recommended for use with tetrode r-f amplifiers.

12-6 The Doherty and the Terman-Woodyard Modulated Amplifiers

These two amplifiers will be described together since they operate upon very similar principles. Figure 12 shows a greatly simplified schematic diagram of the operation of both types. Both systems operate by virtue of a carrier tube (V_1 in both figures 12 and 13) which supplies the unmodulated carrier, and whose output is reduced to supply negative peaks, and a peak tube (V_2) whose function is to supply approximately half the positive peak of the modulation cycle and whose additional function is to lower the load impedance on the carrier tube so that it will be able to supply the other half of the positive peak of the modulation cycle.

The peak tube is enabled to increase the output of the carrier tube by virtue of an impedance inverting line between the plate circuits of the two tubes. This line is designed to have a characteristic impedance of one-half the value of load into which the carrier tube operates under the carrier conditions. Then a load of one-half the characteristic impedance of the quarter-wave line is coupled into the output. By experience with quarter-wave lines in antenna-matching circuits we know that such a line will vary the impedance at one end of the line in such a manner that the geometric mean between the two terminal impedances will be equal to the characteristic impedance of the line. Thus, if we have a value of load of *one-half* the characteristic impedance of the line at one end, the other end of the line will present a value of *twice* the characteristic impedance of the lines to the carrier tube V_1.

This is the situation that exists under the carrier conditions when the peak tube merely floats across the load end of the line and contributes no power. Then as a positive peak of modulation comes along, the peak tube starts to contribute power to the load until at the peak of the modulation cycle it is contributing enough power so that the impedance at the load end of the line is equal to R, instead of

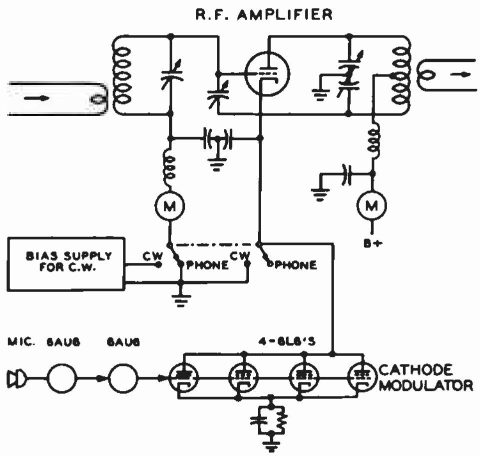


Figure 11
CATHODE MODULATOR INSTALLATION SHOWING PHONE-C.W. TRANSFER SWITCH

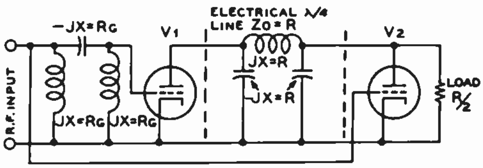


Figure 12
DIAGRAMMATIC REPRESENTATION OF THE DOHERTY LINEAR

the R/2 that is presented under the carrier conditions. This is true because at a positive modulation peak (since it is delivering full power) the peak tube subtracts a negative resistance of R/2 from the load end of the line.

Now, since under the peak condition of modulation the load end of the line is terminated in R ohms instead of R/2, the impedance at the *carrier-tube* will be *reduced* from 2R ohms to R ohms. This again is due to the impedance inverting action of the line. Since the load resistance on the carrier tube has been reduced to half the carrier value, its output at the peak of the modulation cycle will be doubled. Thus we have the necessary condition for a 100 per cent modulation peak; the amplifier will deliver four times as much power as it does under the carrier conditions.

On negative modulation peaks the peak tube does not contribute; the output of the carrier tube is reduced until on a 100 per cent negative peak its output is zero.

The Electrical Quarter-Wave Line While an electrical quarter-wave line (consisting of a pi network with the inductance and capacitance units having a reactance equal to the characteristic impedance of the line) does have the desired impedance-inverting effect, it also has the undesirable effect of introducing a 90° phase shift across such a line. If the shunt elements are capacitances, the phase shift across the line lags by 90°; if they are inductances, the phase shift leads by 90°. Since there is an undesirable phase shift of 90° between the plate circuits of the carrier and peak tubes, an equal and opposite phase shift must be introduced in the exciting voltage to the grid circuits of the two tubes so that the resultant output in the plate circuit will be in phase. This additional phase shift has been indicated in figure 12 and a method of obtaining it has been shown in figure 13.

Comparison Between Linear and Grid Modulator The difference between the Doherty linear amplifier and the Terman-Woodyard grid-modulated amplifier is the same as the difference between any linear and grid-modulated stages. Modulated r.f. is applied to the grid circuit of the Doherty linear amplifier with the carrier tube biased to cutoff and the peak tube biased to the point where it draws substantially zero plate current at the carrier condition.

In the Terman-Woodyard grid-modulated amplifier the carrier tube runs Class C with comparatively high bias and high plate efficiency, while the peak tube again is biased so that it draws almost no plate current. Unmodulated r.f. is applied to the grid circuits of the two tubes and the modulating voltage is inserted in series with the fixed bias voltages. From one-half to two-thirds as much *audio* voltage is required at the grid of the peak tube as is required at the grid of the carrier tube.

Operating Efficiencies The resting carrier efficiency of the grid-modulated amplifier may run as high as is obtainable in any Class C stage, 80 per cent or better. The resting carrier efficiency of the linear will be about as good as is obtainable in any Class B amplifier, 60 to 70 per cent. The overall efficiency of the bias-modulated amplifier at 100 per cent modulation will run about 75 per cent; of the linear, about 60 per cent.

In figure 13 the plate tank circuits are detuned enough to give an effect equivalent to the shunt elements of the quarter-wave "line" of figure 12. At resonance, the coils L_1 and L_2 in the grid circuits of the two tubes have

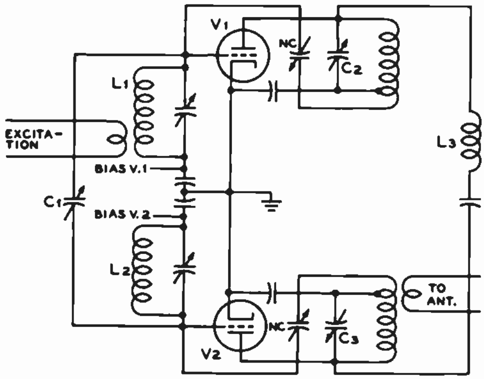


Figure 13

SIMPLIFIED SCHEMATIC OF A "HIGH EFFICIENCY" AMPLIFIER

The basic system, comprising a "carrier" tube and a "peak" tube interconnected by lumped-constant quarter-wave lines, is the same for either grid-bias modulation or for use as a linear amplifier of a modulated wave.

each an inductive reactance equal to the capacitive reactance of the capacitor C_1. Thus we have the effect of a pi network consisting of shunt inductances and series capacitance. In the plate circuit we want a phase shift of the same magnitude but in the opposite direction; so our series element is the inductance L_3 whose reactance is equal to the characteristic impedance desired of the network. Then the plate tank capacitors of the two tubes C_2 and C_3 are increased an amount past resonance, so that they have a capacitive reactance equal to the inductive reactance of the coil L_3. It is quite important that there be no coupling between the inductors.

Although both these types of amplifiers are highly efficient and require no high-level audio equipment, they are difficult to adjust—particularly so on the higher frequencies—and it would be an extremely difficult problem to design a multiband transmitter employing the circuit. However, the grid-bias modulation system has advantages for the high-power transmitter which will be operated on a single frequency band.

Other High-Efficiency Modulation Systems Many other high-efficiency modulation systems have been described since about 1936. The majority of these, however have received little application either by commercial interests or by amateurs. In most cases the circuits are difficult to adjust, or they have other undesirable features which make their use impracticable alongside the more conventional modulation systems. Nearly all these circuits have been published in the *I.R.E. Proceedings* and the interested reader can refer to them in back copies of that journal.

12-7 Speech Clipping

Speech waveforms are characterized by frequently recurring high-intensity peaks of very short duration. These peaks will cause overmodulation if the *average* level of modulation on loud syllables exceeds approximately 30 per cent. Careful checking into the nature of speech sounds has revealed that these high-intensity peaks are due primarily to the vowel sounds. Further research has revealed that the vowel sounds add little to intelligibility, the major contribution to intelligibility coming from the consonant sounds such as *v, b, k, s, t,* and *l*. Measurements have shown that the power contained in these consonant sounds may be down 30 db or more from the energy in the vowel sounds in the same speech passage. Obviously, then, if we can increase the relative energy content of the consonant sounds with respect to the vowel sounds it will be possible to understand a signal modulated with such a waveform in the presence of a much higher level of background noise and interference. Experiment has shown that it is possible to accomplish this desirable result simply by cutting off or *clipping* the high-intensity peaks and thus building up in a relative manner the effective level of the weaker sounds.

Such clipping theoretically can be accomplished simply by increasing the gain of the speech amplifier until the average level of modulation on loud syllables approaches 90 per cent. This is equivalent to increasing the speech power of the consonant sounds by about 10 times or, conversely, we can say that 10 db of clipping has been applied to the voice wave. However, the clipping when accomplished in this manner *will produce higher order sidebands known as "splatter,"* and the transmitted signal would occupy a relatively tremendous slice of spectrum. So another method of accomplishing the desirable effects of clipping must be employed.

A considerable reduction in the amount of splatter caused by a moderate increase in the gain of the speech amplifier can be obtained by poling the signal from the speech amplifier to the transmitter such that the high-intensity peaks occur on *upward* or positive modulation. Overloading on positive modulation peaks produces less splatter than the negative-peak clipping which occurs with overloading on the

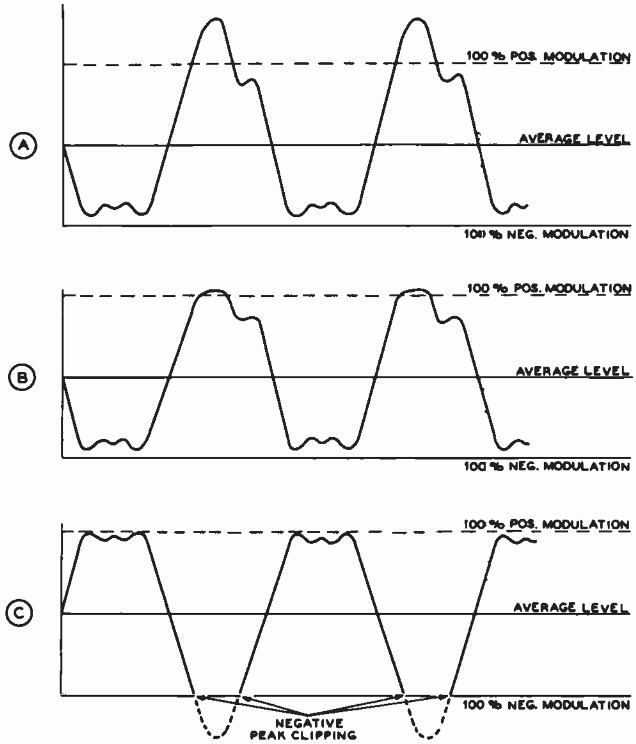


Figure 14
SPEECH-WAVEFORM AMPLITUDE MODULATION

Showing the effect of using the proper polarity of a speech wave for modulating a transmitter. (A) shows the effect of proper speech polarity on a transmitter having an upward modulation capability of greater than 100 per cent. (B) shows the effect of using proper speech polarity on a transmitter having an upward modulation capability of only 100 per cent. Both these conditions will give a clean signal without objectionable splatter. (C) shows the effect of the use of improper speech polarity. This condition will cause serious splatter due to negative-peak clipping in the modulated-amplifier stage.

negative peaks of modulation. This aspect of the problem has been discussed in more detail in the section on *Speech Waveform Dissymmetry* earlier in this chapter. The effect of feeding the proper speech polarity from the speech amplifier is shown in figure 14.

A much more desirable and effective method of obtaining speech clipping is actually to employ a clipper circuit in the earlier stages of the speech amplifier, and then to filter out the objectionable distortion components by means of a sharp low-pass filter having a cut-off frequency of approximately 3000 cycles. Tests on *clipper-filter* speech systems have shown that 6 db of clipping on voice is just noticeable, 12 db of clipping is quite acceptable, and values of clipping from 20 to 25 db are tolerable under such conditions that a high degree of clipping is necessary to get through heavy QRM or QRN. A signal with 12 db of clipping doesn't sound quite *natural* but it is not unpleasant to listen to and is much more readable than an unclipped signal in the presence of strong interference.

The use of a clipper-filter in the speech amplifier, to be completely effective, requires that phase shift between the clipper-filter stage and the final modulated amplifier be kept to a minimum. However, if there is phase shift after the clipper-filter the system does not completely break down. The presence of phase shift merely requires that the audio gain following the clipper-filter be reduced to the point where the *cant* applied to the clipped speech waves still cannot cause overmodulation. This effect is illustrated in figures 15 and 16.

The *cant* appearing on the tops of the square waves leaving the clipper-filter centers about the clipping level. Hence, as the frequency being passed through the system is lowered, the amount by which the peak of the *canted* wave exceeds the clipping level is increased.

Phase Shift Correction In a normal transmitter having a moderate amount of phase shift the *cant* applied to the tops of the waves will cause overmodulation on frequencies below those for which the gain following the clipper-filter has been adjusted unless remedial steps have been taken. The following steps are advised:

(1) Introduce bass *suppression* into the speech amplifier *ahead* of the clipper-filter.

(2) *Improve* the low-frequency response characteristic insofar as it is possible in the

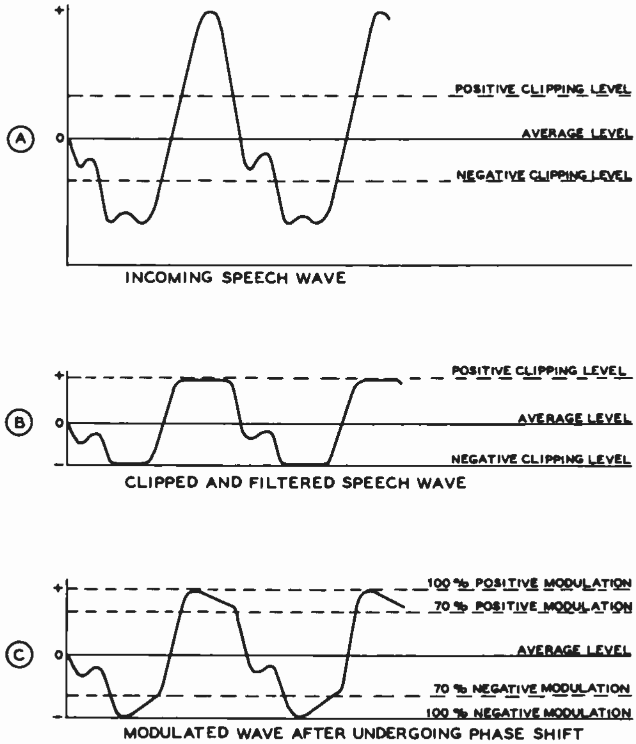


Figure 15

ACTION OF A CLIPPER-FILTER ON A SPEECH WAVE

The drawing (A) shows the incoming speech wave before it reaches the clipper stage. (B) shows the output of the clipper-filter, illustrating the manner in which the peaks are clipped and then the sharp edges of the clipped wave removed by the filter. (C) shows the effect of phase shift in the stages following the clipper-filter. (C) also shows the manner in which the transmitter may be adjusted for 100 per cent modulation of the "canted" peaks of the wave, the sloping top of the wave reaching about 70 per cent modulation.

stages *following* the clipper-filter. Feeding the plate current to the final amplifier through a choke rather than through the secondary of the modulation transformer will help materially.

Even with the normal amount of improvement which can be attained through the steps mentioned above there will still be an amount of wave cant which must be compensated in some manner. This compensation can be done in either of two ways. The first and simpler way is as follows:

(1) Adjust the speech gain *ahead* of the clipper-filter until with normal talking into the microphone the distortion being introduced by the clipper-filter circuit is quite apparent but not objectionable. This amount of distortion will be apparent to the normal listener when 10 to 15 db of clipping is taking place.

(2) Tune a selective communications receiver about 15 kc. to one side or the other of the frequency being transmitted. Use a short antenna or no antenna at all on the receiver so that the transmitter is not blocking the receiver.

(3) Again with the normal talking into the microphone adjust the gain *following* the clipper-filter to the point where the sideband splatter is being heard, and then slightly back off the gain after the clipper-filter until the splatter disappears.

If the phase shift in the transmitter or modulator is not excessive the adjustment procedure given above will allow a clean signal to be radiated regardless of any reasonable voice level being fed into the microphone.

If a cathode-ray oscilloscope is available the modulated envelope of the transmitter should be checked with 30 to 70 cycle sawtooth waves on the horizontal axis. If the upper half of the envelope appears in general the same as the drawing of figure 15C, all is well and phase-shift is not excessive. However, if much more slope appears on the tops of the waves than is illustrated in this figure, it will be well to apply the second step in compensation in order to insure that sideband splatter cannot take place and to afford a still higher average percentage of modulation. This second step consists of the addition of a high-level *splatter suppressor* such as is illustrated in figure 17.

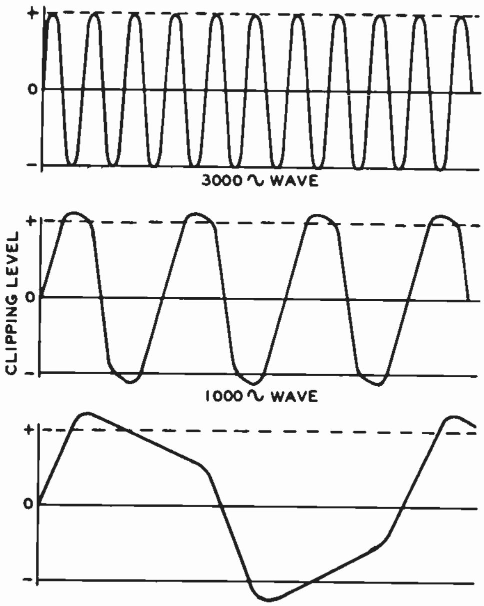


Figure 16

ILLUSTRATING THE EFFECT OF PHASE SHIFT AND FILTERED WAVES OF DIFFERENT FREQUENCY

Sketch (A) shows the effect of a clipper and a filter having a cutoff of about 3500 cycles on a wave of 3000 cycles. Note that no harmonics are present in the wave so that phase shift following the clipper-filter will have no significant effect on the shape of the wave. (B) and (C) show the effect of phase shift on waves well below the cutoff frequency of the filter. Note that the "cant" placed upon the top of the wave causes the peak value to rise higher and higher above the clipping level as the frequency is lowered. It is for this reason that bass suppression before the clipper stage is desirable. Improved low-frequency response following the clipper-filter will reduce the phase shift and therefore the canting of the wave at the lower voice frequencies.

The use of a high-level splatter suppressor after a clipper-filter system will afford the result shown in figure 18 since such a device will not permit the negative-peak clipping which the wave cant caused by audio-system phase shift can produce. The high-level splatter suppressor operates by virtue of the fact that it will not permit the plate voltage on the modulated amplifier to go completely to zero regardless of the incoming signal amplitude.

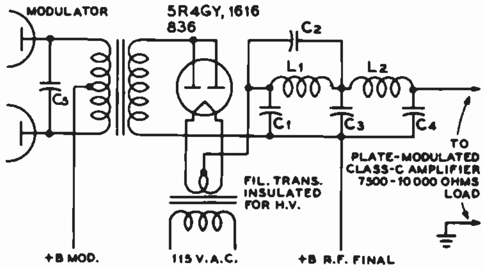


Figure 17

HIGH-LEVEL SPLATTER SUPPRESSOR

This circuit is effective in reducing splatter caused by negative-peak clipping in the modulated amplifier stage. The use of a two-section filter as shown is recommended, although either a single m-derived or a constant-k section may be used for greater economy. Suitable chokes, along with recommended capacitor values, are available from several manufacturers.

Hence negative-peak clipping with its attendant splatter cannot take place. Such a device can, of course, also be used in a transmitter which does not incorporate a clipper-filter system. However, the full increase in average modulation level without serious distortion, afforded by the clipper-filter system, will not be obtained.

A word of caution should be noted at this time in the case of tetrode final modulated amplifier stages which afford screen voltage modulation by virtue of a tap or a separate winding on the modulation transformer such as is shown in figure 9C of this chapter. If such a system of modulation is in use, the high-level splatter suppressor shown in figure 17 will not operate satisfactorily since negative-peak clipping in the stage can take place when the *screen* voltage goes too low.

Clipper Circuits Two effective low-level clipper-filter circuits are shown in figures 19 and 20. The circuit of figure 19 employs a 6J6 double triode as a clipper, each half of the 6J6 clipping one side of the impressed waveform. The optimum level at which the clipping operation begins is set by the value of the cathode resistor. A maximum of 12 to 14 db of clipping may be used with this circuit, which means that an extra 12 to 14 db of speech gain must precede the clipper. For a peak output of 8 volts from the clipper-filter, a peak audio signal of about 40 volts must be impressed upon the clipper input circuit. The 6C4 speech amplifier stage must therefore be considered as a part of the clipper circuit as

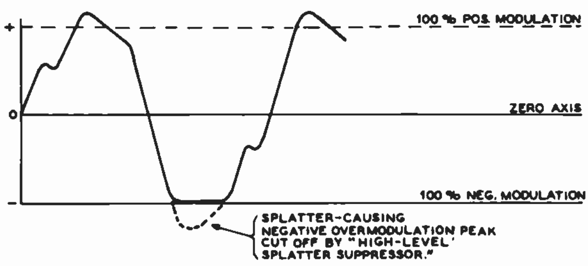


Figure 18

ACTION OF HIGH-LEVEL SPLATTER SUPPRESSOR

A high-level splatter suppressor may be used in a transmitter without a clipper-filter to reduce negative-peak clipping, or such a unit may be used following a clipper-filter to allow a higher average modulation level by eliminating the negative-peak clipping which the wave-cant caused by phase shift might produce.

it compensates for the 12 to 14 db loss of gain incurred in the clipping process. A simple low-pass filter made up of a 20 henry a.c. - d.c replacement type filter choke and two mica condensers follows the 6J6 clipper. This filter is designed for a cutoff frequency of about 3500 cycles when operating into a load impedance of ½ megohm. The output level of 8 volts peak is ample to drive a triode speech amplifier stage, such as a 6C4 or 6J5.

A 6AL5 double diode series clipper is employed in the circuit of figure 20, and a commercially made low-pass filter is used to give somewhat better high frequency cutoff characteristics. A double triode is employed as a speech amplifier ahead of the clipper circuit. The actual performance of either circuit is about the same.

To eliminate higher order products that may be generated in the stages following the clipper-filter, it is wise to follow the modulator with a high-level filter, as shown in figure 21.

Clipper Adjustment These clipper circuits have two adjustments: *Adjust Gain* and *Adjust Clipping.* The *Adj. Gain* control determines the modulation level of the transmitter. This control should be set so that over-modulation of the transmitter is impossible, regardless of the amount of clipping used. Once the *Adj. Gain* control has been roughly set, the *Adj. Clip.* control may be used to set the modulation level to any percentage below 100%. As the modulation level is decreased, more and more clipping is introduced into the circuit, until a full 12 db of clipping is used. This means that the *Adj. Gain* control may be advanced some 12 db past the point where the clipping action started. Clipping action should start at 85% to 90% modulation when a sine wave is used for circuit adjustment purposes.

High-Level Filters Even though we may have cut off all frequencies above 3000 or 3500 cycles through the use of a filter system such as is shown in the circuits of figures 19 and 20, higher frequencies may again be introduced into the modulated wave by distortion in stages following the speech amplifier. Harmonics of the incoming audio frequencies may be generated in the driver stage for the modulator; they may be generated in the plate circuit of the modulator; or they may be generated by non-linearity in the modulated amplifier itself.

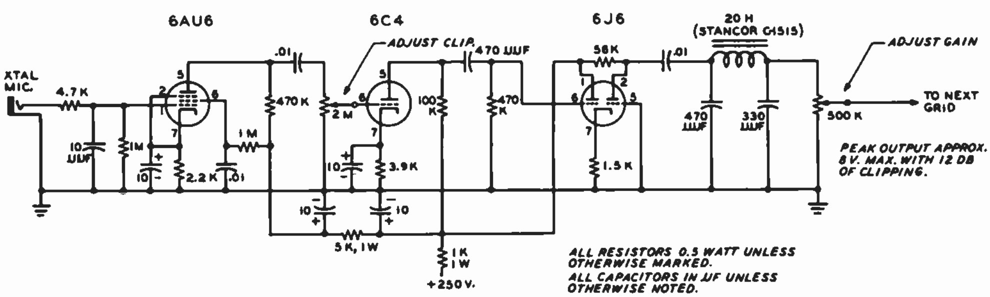


Figure 19

CLIPPER FILTER USING 6J6 DOUBLE TRIODE STAGE

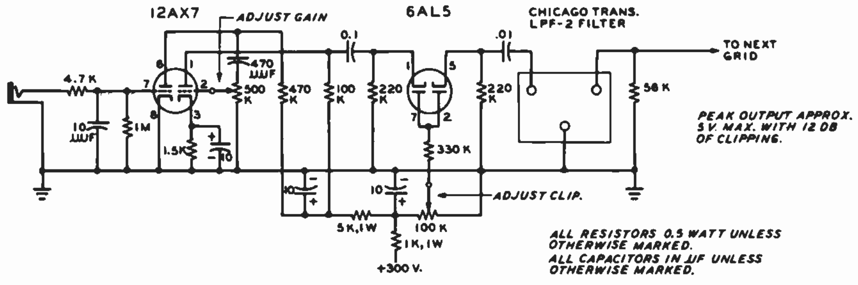


Figure 20
CLIPPER FILTER USING 6AL5 STAGE

Regardless of the point in the system following the speech amplifier where the high audio frequencies may be generated, these frequencies can still cause a broad signal to be transmitted even though all frequencies above 3000 or 3500 cycles have been cut off in the speech amplifier. The effects of distortion in the audio system *following* the speech amplifier can be eliminated quite effectively through the use of a *post-modulator* filter. Such a filter must be used between the modulator plate circuit and the r-f amplifier which is being modulated.

This filter may take three general forms in a normal case of a Class C amplifier plate modulated by a Class B modulator. The best method is to use a high level low-pass filter as shown in figure 21 and discussed previously. Another method which will give excellent results in some cases and poor results in others, dependent upon the characteristics of the modulation transformer, is to "build out" the modulation transformer into a filter section. This is accomplished as shown in figure 22 by placing mica capacitors of the correct value across the primary and secondary of the modulation transformer. The proper values for the capaci-

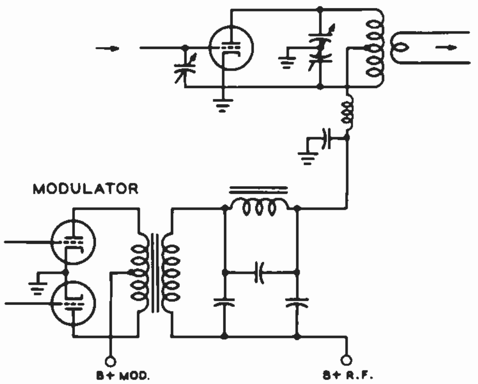


Figure 21
ADDITIONAL HIGH-LEVEL LOW-PASS FILTER TO FOLLOW MODULATOR WHEN A LOW-LEVEL CLIPPER FILTER IS USED

Suitable choke, along with recommended capacitor values, is available from several manufacturers.

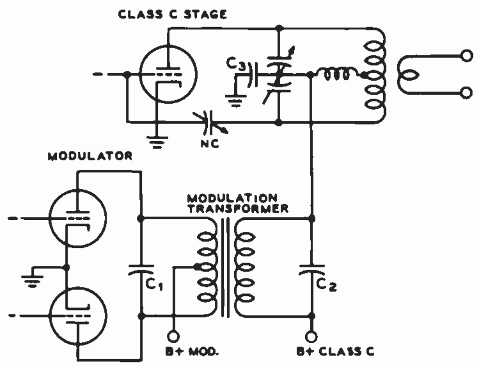


Figure 22
"BUILDING-OUT" THE MODULATION TRANSFORMER

This expedient utilizes the leakage reactance of the modulation transformer in conjunction with the capacitors shown to make up a single-section low-pass filter. In order to determine exact values for C_1 and C_2 plus C_3, it is necessary to use a measurement setup such as is shown in figure 23. However, experiment has shown in the case of a number of commercially available modulation transformers that a value for C_1 of 0.002-µfd. and C_2 plus C_3 of 0.004-µfd. will give satisfactory results.

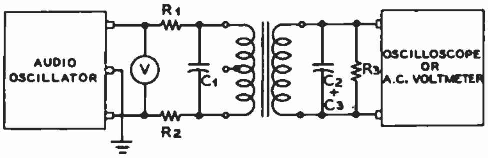


Figure 23

TEST SETUP FOR BUILDING-OUT MODULATION TRANSFORMER

Through the use of a test setup such as is shown and the method described in the text it is possible to determine the correct values for a specified filter characteristic in the built-out modulation transformer.

tors C_1 and C_2 must, in the ideal case, be determined by trial and error. Experiment with a number of modulators has shown, however, that if a 0.002 μfd. capacitor is used for C_1, and if the sum of C_2 and C_3 is made 0.004 μfd. (0.002 μfd. for C_2 and 0.002 for C_3) the ideal condition of cutoff above 3000 cycles will be approached in most cases with the "multiple-match" type of modulation transformer.

If it is desired to determine the optimum values of the capacitors across the transformer this can be determined in several ways, all of which require the use of a calibrated audio oscillator. One way is diagrammed in figure 23. The series resistors R_1 and R_2 should each be equal to ½ the value of the recommended plate-to-plate load resistance for the Class B modulator tubes. Resistor R_3 should be equal to the value of load resistance which the Class C modulated stage will present to the modulator. The meter V can be any type of a-c voltmeter. The indicating instrument on the secondary of the transformer can be either a cathode-ray oscilloscope or a high-impedance a-c voltmeter of the vacuum-tube or rectifier type.

With a set-up as shown in figure 23 a plot of output voltage against frequency is made, at all times keeping the voltage across V constant, using various values of capacitance for C_1 and C_2 plus C_3. When the proper values of capacitance have been determined which give substantially constant output up to about 3000 or 3500 cycles and decreasing output at all frequencies above, high-voltage mica capacitors can be substituted if receiving types were used in the tests and the transformer connected to the modulator and Class C amplifier.

With the transformer reconnected in the transmitter a check of the modulated-wave output of the transmitter should be made using an audio oscillator as signal generator and an oscilloscope coupled to the transmitter output. With an input signal amplitude fed to the speech amplifier of such amplitude that limiting does not take place, a substantially clean sine wave should be obtained on the carrier of the transmitter at all input frequencies up to the cutoff frequency of the filter system in the speech amplifier and of the filter which includes the modulation transformer. Above these cutoff frequencies very little modulation of the carrier wave should be obtained. To obtain a check on the effectiveness of the "built out" modulation transformer, the capacitors across the primary and secondary should be removed for the test. In most cases a marked deterioration in the waveform output of the modulator will be noticed with frequencies in the voice range from 500 to 1500 cycles being fed into the speech amplifier.

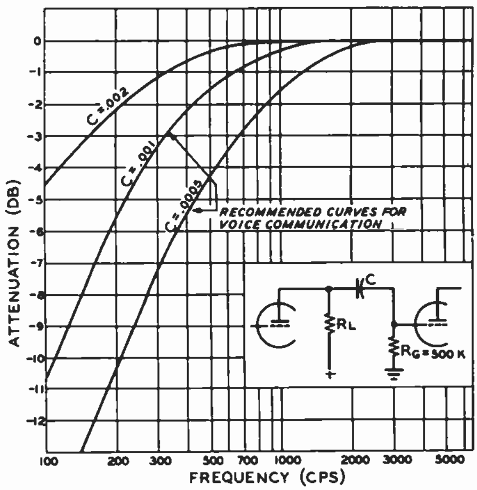


Figure 24

BASE ATTENUATION CHART

Frequency attenuation caused by various values of coupling capacitor with a grid resistor of 0.5 megohm in the following stage (R_G > R_L)

A filter system similar to that shown in figure 17 may be used between the modulator and the modulated circuit in a grid-modulated or screen-modulated transmitter. Lower-voltage capacitors and low-current chokes may of course be employed.

Bass Suppression Most of the power represented by ordinary speech (particularly the male voice) lies below 1000 cycles. If all frequencies below 400 or 500 cycles are eliminated or substantially attenuated, there is a considerable reduction in power but insignificant reduction in intelligibility. This means that the speech level may be increased considerably without overmodulation or overload of the audio system. In addition, if speech clipping is used, attenuation of the lower audio frequencies before the clipper will reduce phase shift and canting of the clipper output.

A simple method of bass suppression is to reduce the size of the interstage coupling capacitors in a resistance coupled amplifier. Figure 24 shows the frequency characteristics caused by such a suppression circuit. A second simple bass suppression circuit is to place a small a.c. - d.c. type filter choke from grid to ground in a speech amplifier stage, as shown in figure 25.

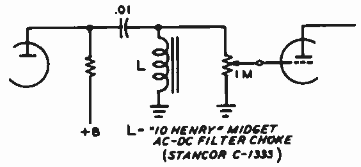


Figure 25
USE OF PARALLEL INDUCTANCE FOR BASS SUPPRESSION

Modulated Amplifier Distortion The systems described in the preceding paragraphs will have no effect in reducing a broad signal caused by non-linearity in the modulated amplifier. Even though the modulating waveform impressed upon the modulated stage may be distortion free, if the modulated amplifier is non-linear distortion will be generated in the amplifier. The only way in which this type of distortion may be corrected is by making the modulated amplifier more linear. Degenerative feedback which includes the modulated amplifier in the loop will help in this regard.

Plenty of grid excitation and high grid bias will go a long way toward making a plate-modulated Class C amplifier linear, although such operating conditions will make more difficult the problem of TVI reduction. If this still does not give adequate linearity, the preceding buffer stage may be modulated 50 per cent or so at the same time and in the same phase as the final amplifier. The use of a grid leak to obtain the majority of the bias for a Class C stage will improve its linearity.

The linearity of a grid-bias modulated r-f amplifier can be improved, after proper adjustments of excitation, grid bias, and antenna coupling have been made by modulating the stage which excites the grid-modulated amplifier. The preceding driver stage may be grid-bias modulated or it may be plate modulated. Modulation of the driver stage should be in the same phase as that of the final modulated amplifier.

CHAPTER THIRTEEN

Frequency Modulation Transmission

Exciter systems for FM and single sideband transmission are basically similar in that modification of the signal in accordance with the intelligence to be transmitted is normally accomplished at a relatively low level. Then the intelligence-bearing signal is amplified to the desired power level for ultimate transmission. True, amplifiers for the two types of signals are basically different; linear amplifiers of the Class A or Class B type being used for ssb signals, while Class C or non-linear Class B amplifiers may be used for FM amplification. But the principle of low-level generation and subsequent amplification is standard for both types of transmission.

13-1 Frequency Modulation

The use of frequency modulation and the allied system of phase modulation has become of increasing importance in recent years. For amateur communication frequency and phase modulation offer important advantages in the reduction of broadcast and TV interference and in the elimination of the costly high-level modulation equipment most commonly employed with amplitude modulation. For broadcast work FM offers an improvement in signal-to-noise ratio for the high field intensities available in the local-coverage area of FM and TV broadcast stations.

In this chapter various points of difference between FM and amplitude modulation transmission and reception will be discussed and the advantages of FM for certain types of communication pointed out. Since the distinguishing features of the two types of transmission lie entirely in the modulating circuits at the transmitter and in the detector and limiter circuits in the receiver, these parts of the communication system will receive the major portion of attention.

Modulation *Modulation* is the process of altering a radio wave in accordance with the intelligence to be transmitted. The nature of the intelligence is of little importance as far as the process of modulation is concerned; it is the *method* by which this intelligence is made to give a distinguishing characteristic to the radio wave which will enable the receiver to convert it back into intelligence that determines the type of modulation being used.

Figure 1 is a drawing of an r-f carrier amplitude modulated by a sine-wave audio voltage. After modulation the resultant modulated r-f wave is seen still to vary about the zero axis at a constant rate, but the strength of the individual r-f cycles is proportional to the amplitude of the modulation voltage.

In figure 2, the carrier of figure 1 is shown frequency modulated by the same modulating voltage. Here it may be seen that modulation voltage of one polarity causes the carrier frequency to decrease, as shown by the fact that the individual r-f cycles of the carrier are spaced farther apart. A modulating voltage of the opposite polarity causes the frequency to

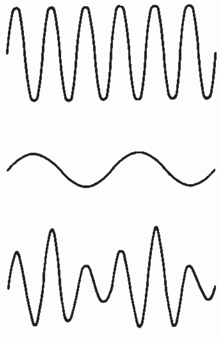


FIGURE 1

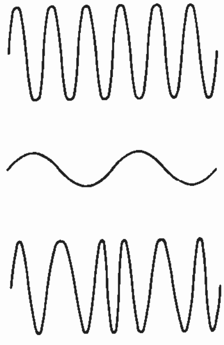


FIGURE 2

AM AND FM WAVES

Figure 1 shows a sketch of the scope pattern of an amplitude modulated wave at the bottom. The center sketch shows the modulating wave and the upper sketch shows the carrier wave.

Figure 2 shows at the bottom a sketch of a frequency modulated wave. In this case the center sketch also shows the modulating wave and the upper sketch shows the carrier wave. Note that the carrier wave and the modulating wave are the same in either case, but that the waveform of the modulated wave is quite different in the two cases.

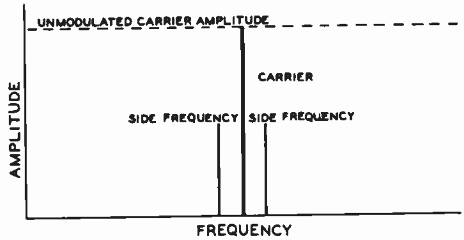


Figure 3
AM SIDE FREQUENCIES

For each AM modulating frequency, a pair of side frequencies is produced. The side frequencies are spaced away from the carrier by an amount equal to the modulation frequency, and their amplitude is directly proportional to the amplitude of the modulation. The amplitude of the carrier does not change under modulation.

increase, and this is shown by the r-f cycles being squeezed together to allow more of them to be completed in a given time interval.

Figures 1 and 2 reveal two very important characteristics about amplitude- and frequency-modulated waves. First, it is seen that while the amplitude (power) of the signal is varied in AM transmission, no such variation takes place in FM. In many cases this advantage of FM is probably of equal or greater importance than the widely publicized noise reduction capabilities of the system. When 100 per cent amplitude modulation is obtained, the average power output of the transmitter must be increased by 50 per cent. This additional output must be supplied either by the modulator itself, in the high-level system, or by operating one or more of the transmitter stages at such a low output level that they are capable of producing the additional output without distortion, in the low-level system. On the other hand, a frequency-modulated transmitter requires an insignificant amount of power from the modulator and needs no provision for increased power output on modulation peaks. All of the stages between the oscillator and the antenna may be operated as high-efficiency Class B or Class C amplifiers or frequency multipliers.

Carrier-Wave Distortion The second characteristic of FM and AM waves revealed by figures 1 and 2 is that both types of modulation result in distortion of the r-f carrier. That is, after modulation, the r-f cycles are no longer sine waves, as they would be if no frequencies other than the fundamental carrier frequency were present. It may be shown in the amplitude modulation case illustrated, that there are only two additional frequencies present, and these are the familiar *side frequencies*, one located on each side of the carrier, and each spaced from the carrier by a frequency interval equal to the modulation frequency. In regard to frequency and amplitude, the situation is as shown in figure 3. The strength of the carrier itself does not vary during modulation, but the strength of the side frequencies depends upon the percentage of modulation. At 100 per cent modulation the power in the side frequencies is equal to half that of the carrier.

Under frequency modulation, the carrier wave again becomes distorted, as shown in figure 2. But, in this case, many more than two additional frequencies are formed. The first two of these frequencies are spaced from the carrier by the modulation frequency, and the additional side frequencies are located out on each side of the carrier and are also spaced from each other by an amount equal to the modulation frequency. Theoretically, there are an infinite number of side frequencies formed, but, fortunately, the strength of those beyond the frequency *swing* of the transmitter under modulation is relatively low.

One set of side frequencies that might be formed by frequency modulation is shown in figure 4. Unlike amplitude modulation, the

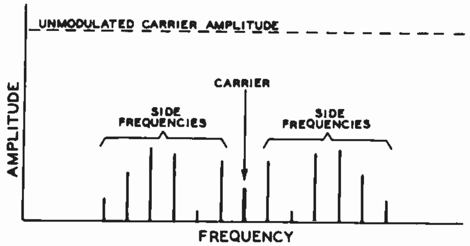


Figure 4
FM SIDE FREQUENCIES

With FM each modulation frequency component causes a large number of side frequencies to be produced. The side frequencies are separated from each other and the carrier by an amount equal to the modulation frequency, but their amplitude varies greatly as the amount of modulation is changed. The carrier strength also varies greatly with frequency modulation. The side frequencies shown represent a case where the deviation each side of the "carrier" frequency is equal to five times the modulating frequency. Other amounts of deviation with the same modulation frequency would cause the relative strengths of the various sidebands to change widely.

strength of the component at the carrier frequency varies widely in FM and it may even disappear entirely under certain conditions. The variation of strength of the carrier component is useful in measuring the amount of frequency modulation, and will be discussed in detail later in this chapter.

One of the great advantages of FM over AM is the reduction in noise at the receiver which the system allows. If the receiver is made responsive only to changes in frequency, a considerable increase in signal-to-noise ratio is made possible through the use of FM, when the signal is of greater strength than the noise. The noise reducing capabilities of FM arise from the inability of noise to cause appreciable frequency modulation of the noise-plus-signal voltage which is applied to the detector in the receiver.

FM Terms Unlike amplitude modulation, the term *percentage modulation* means little in FM practice, unless the receiver characteristics are specified. There are, however, three terms, *deviation, modulation index*, and *deviation ratio*, which convey considerable information concerning the character of the FM wave.

Deviation is the amount of frequency shift each side of the unmodulated carrier frequency which occurs when the transmitter is modulated. Deviation is ordinarily measured in kilocycles, and in a properly operating FM transmitter it will be directly proportional to the amplitude of the modulating signal. When a symmetrical modulating signal is applied to the transmitter, equal deviation each side of the resting frequency is obtained during each cycle of the modulating signal, and the total frequency range covered by the FM transmitter is sometimes known as the *swing*. If, for instance, a transmitter operating on 1000 kc. has its frequency shifted from 1000 kc. to 1010 kc., back to 1000 kc., then to 990 kc., and again back to 1000 kc. during one cycle of the modulating wave, the *deviation* would be 10 kc. and the *swing* 20 kc.

The *modulation index* of an FM signal is the ratio of the deviation to the audio modulating frequency, when both are expressed in the same units. Thus, in the example above if the signal is varied from 1000 kc. to 1010 kc. to 990 kc., and back to 1000 kc. at a rate (frequency) of 2000 times a second, the modulation index would be 5, since the deviation (10 kc.) is 5 times the modulating frequency (2000 cycles, or 2 kc.).

The relative strengths of the FM carrier and the various side frequencies depend directly upon the modulation index, these relative strengths varying widely as the modulation index is varied. In the preceding example, for instance, side frequencies occur on the high side of 1000 kc. at 1002, 1004, 1006, 1008, 1010, 1012, etc., and on the low frequency side at 998, 996, 994, 992, 990, 988, etc. In proportion to the unmodulated carrier strength (100 per cent), these side frequencies have the following strengths, as indicated by a modulation index of 5: 1002 and 998–33 per cent, 1004 and 996–5 per cent, 1006 and 994–36 per cent, 1008 and 992–39 per cent, 1010 and 990–26 per cent, 1012 and 988–13 per cent. The carrier strength (1000 kc.) will be 18 per cent of its unmodulated value. Changing the amplitude of the modulating signal will change the deviation, and thus the modulation index will be changed, with the result that the side frequencies, while still located in the same places, will have different strength values from those given above.

The *deviation ratio* is similar to the modulation index in that it involves the ratio between a modulating frequency and deviation. In this case, however, the deviation in question is the peak frequency shift obtained under full modulation, and the audio frequency to be considered is the maximum audio frequency to be transmitted. When the maximum audio frequency to be transmitted is 5000 cycles, for example, a deviation ratio of 3 would call for a peak deviation of 3 x 5000, or 15 kc. at full modulation. The noise-suppression capabilities of FM are directly related to the deviation ratio. As the deviation ratio is increased, the noise suppression becomes better *if* the signal is somewhat stronger than the noise. Where the noise approaches the signal in strength, however, low deviation ratios allow communication to be maintained in many cases where high-deviation-ratio FM and conventional AM are incapable of giving service. This assumes that a narrow-band FM receiver is in use. For each value of r-f signal-to-noise ratio at the receiver, there is a maximum deviation ratio which may be used, beyond which the output audio signal-to-noise ratio decreases. Up to this critical deviation ratio, however, the noise suppression becomes progressively better as the deviation ratio is increased.

For high-fidelity FM broadcasting purposes, a deviation ratio of 5 is ordinarily used, the maximum audio frequency being 15,000 cycles, and the peak deviation at full modulation being 75 kc. Since a swing of 150 kc. is covered by the transmitter, it is obvious that wide-band FM transmission must necessarily be confined to the v-h-f range or higher, where room for the signals is available.

In the case of television sound, the deviation ratio is 1.67; the maximum modulation frequency is 15,000 cycles, and the transmitter deviation for full modulation is 25 kc. The sound carrier frequency in a standard TV signal is located exactly 4.5 Mc. higher than the picture carrier frequency. In the *intercarrier* TV sound system, which recently has become quite widely used, this constant difference between the picture carrier and the sound carrier is employed within the receiver to obtain an FM sub-carrier at 4.5 Mc. This 4.5 Mc. sub-carrier then is demodulated by the FM detector to obtain the sound signal which accompanies the picture.

Narrow-Band FM Transmission Narrow-band FM transmission has become standardized for use by the mobile services such as police, fire, and taxicab communication, and also on the basis of a temporary authorization for amateur work in portions of each of the amateur radiotelephone bands. A maximum deviation of 15 kc. has been standardized for the mobile and commercial communication services, while a maximum deviation of 3 kc. is authorized for amateur NBFM communication.

Bandwidth Required by FM As the above discussion has indicated, many side frequencies are set up when a radio-frequency carrier is frequency modulated; theoretically, in fact, an infinite number of side frequencies is formed. Fortunately, however, the amplitudes of those side frequencies falling outside the frequency range over which the transmitter is *swung* are so small that most of them may be ignored. In FM transmission, when a complex modulating wave (speech or music) is used, still additional side frequencies resulting from a beating together of the various frequency components in the modulating wave are formed. This is a situation that does not occur in amplitude modulation and it might be thought that the large number of side frequencies thus formed might make the frequency spectrum produced by an FM transmitter prohibitively wide. Analysis shows, however, that the additional side frequencies are of very small amplitude, and, instead of increasing the bandwidth, modulation by a complex wave actually reduces the effective bandwidth of the FM wave. This is especially true when speech modulation is used, since most of the power in voiced sounds is concentrated at low frequencies in the vicinity of 400 cycles.

The bandwidth required in an FM receiver is a function of a number of factors, both theoretical and practical. Basically, the bandwidth required is a function of the deviation ratio and the maximum frequency of modulation, although the practical consideration of drift and ease of receiver tuning also must be considered. Shown in figure 5 are the frequency spectra (carrier and sideband frequencies) associated with the standard FM broadcast signal, the TV sound signal, and an amateur-band narrow-band FM signal with full modulation using the highest permissible modulating frequency in each case. It will be seen that for low deviation ratios the receiver bandwidth should be at least four times the maximum frequency deviation, but for a deviation ratio of 5 the receiver bandwidth need be only about 2.5 times the maximum frequency deviation.

13-2 Direct FM Circuits

Frequency modulation may be obtained either by the direct method, in which the frequency of an oscillator is changed directly by the modulating signal, or by the indirect method which makes use of phase modulation. Phase-modulation circuits will be discussed in section 13-3.

A successful frequency modulated transmitter must meet two requirements: (1) The frequency deviation must be symmetrical about a fixed frequency, for symmetrical modulation voltage. (2) The deviation must be directly proportional to the amplitude of the modulation, and independent of the modulation frequency. There are several methods of direct frequency modulation which will fulfill these

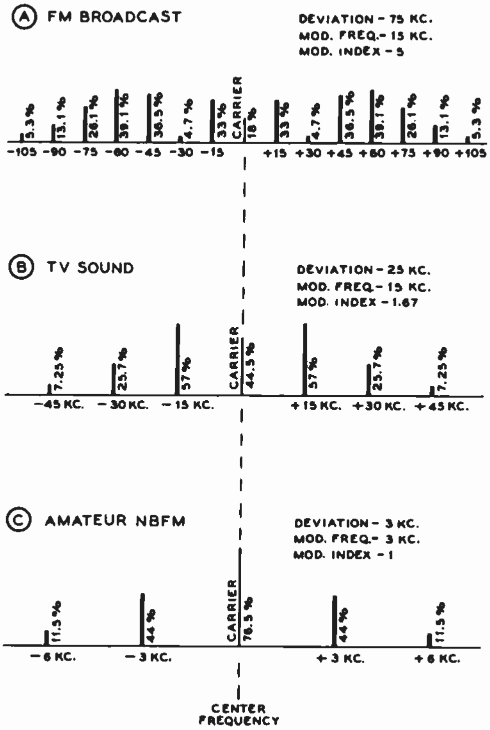


Figure 5
EFFECT OF FM MODULATION INDEX
Showing the side-frequency amplitude and distribution for the three most common modulation indices used in FM work. The maximum modulating frequency and maximum deviation are shown in each case.

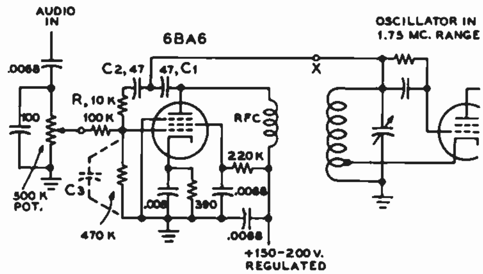


Figure 6
REACTANCE-TUBE MODULATOR
This circuit is convenient for direct frequency modulation of an oscillator in the 1.75-Mc. range. Capacitor C_3 may be only the input capacitance of the tube, or a small trimmer capacitor may be included to permit a variation in the sensitivity of the reactance tube.

requirements. Some of these methods will be described in the following paragraphs.

Reactance-Tube Modulators One of the most practical ways of obtaining direct frequency modulation is through the use of a *reactance-tube modulator.* In this arrangement the modulator plate-cathode circuit is connected across the oscillator tank circuit, and made to appear as either a capacitive or inductive reactance by exciting the modulator grid with a voltage which either leads or lags the oscillator tank voltage by 90 degrees. The leading or lagging grid voltage causes a corresponding leading or lagging plate current, and the plate-cathode circuit appears as a capacitive or inductive reactance across the oscillator tank circuit. When the transconductance of the modulator tube is varied, by varying one of the element voltages, the magnitude of the reactance across the oscillator tank is varied. By applying audio modulating voltage to one of the elements, the transconductance, and hence the frequency, may be varied at an audio rate. When properly designed and operated, the reactance-tube modulator gives linear frequency modulation, and is capable of producing large amounts of deviation.

There are numerous possible configurations of the reactance-tube modulator circuit. The difference in the various arrangements lies principally in the type of phase-shifting circuit used to give a grid voltage which is in phase quadrature with the r-f voltage at the modulator plate.

Figure 6 is a diagram of one of the most popular forms of reactance-tube modulators. The modulator tube, which is usually a pentode such as a 6BA6, 6AU6, or 6CL6, has its plate coupled through a blocking capacitor, C_1, to the "hot" side of the oscillator grid circuit. Another blocking capacitor, C_2, feeds r.f. to the phase shifting network R-C_3 in the modulator grid circuit. If the resistance of R is made large in comparison with the reactance of C_3 at the oscillator frequency, the current through the R-C_3 combination will be nearly in phase with the voltage across the tank circuit, and the voltage across C_3 will lag the oscillator tank voltage by almost 90 degrees. The result of the 90-degree lagging voltage on the modulator grid is that its plate current lags the tank voltage by 90 degrees, and the reactance tube appears as an inductance in shunt with the oscillator inductance, thus raising the oscillator frequency.

The phase-shifting capacitor C_3 can consist of the input capacitance of the modulator tube and stray capacitance between grid and ground.

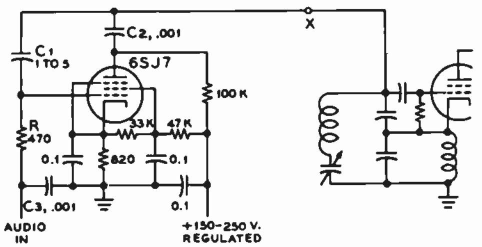


Figure 7
ALTERNATIVE REACTANCE-TUBE MODULATOR

This circuit is often preferable for use in the lower frequency range, although it may be used at 1.75 Mc. and above if desired. In the schematic above the reactance tube is shown connected across the voltage-divider capacitors of a Clapp oscillator, although the modulator circuit may be used with any common type of oscillator.

However, better control of the operating conditions of the modulator may be had through the use of a variable capacitor as C_3. Resistance R will usually have a value of between 4700 and 100,000 ohms. Either resistance or transformer coupling may be used to feed audio voltage to the modulator grid. When a resistance coupling is used, it is necessary to shield the grid circuit adequately, since the high impedance grid circuit is prone to pick up stray r-f and low frequency a-c voltage, and cause undesired frequency modulation.

An alternative reactance modulator circuit is shown in figure 7. The operating conditions are generally the same, except that the r-f excitation voltage to the grid of the reactance tube is obtained effectively through reversing the R and C_1 of figure 6. In this circuit a small capacitance is used to couple r.f. into the grid of the reactance tube, with a relatively small value of resistance from grid to ground. This circuit has the advantage that the grid of the tube is at relatively low impedance with respect to r.f. However, the circuit normally is not suitable for operation above a few megacycles due to the shunting capacitance within the tube from grid to ground.

Either of the reactance-*ube circuits may be used with any of the common types of oscillators. The reactance modulator of figure 6 is shown connected to the high-impedance point of a conventional hot-cathode Hartley oscillator, while that of figure 7 is shown connected across the low-impedance capacitors of a series-tuned Clapp oscillator.

There are several possible variations of the basic reactance-tube modulator circuits shown in figures 6 and 7. The audio input may be applied to the suppressor grid, rather than the control grid, if desired. Another modification is to apply the audio to a grid other than the control grid in a mixer or pentagrid converter tube which is used as the modulator. Generally, it will be found that the transconductance variation per volt of control-element voltage variation will be greatest when the control (audio) voltage is applied to the control grid. In cases where it is desirable to separate completely the audio and r-f circuits, however, applying audio voltage to one of the other elements will often be found advantageous despite the somewhat lower sensitivity.

Adjusting the Phase Shift One of the simplest methods of adjusting the phase shift to the correct amount is to place a pair of earphones in series with the oscillator cathode-to-ground circuit and adjust the phase-shift network until minimum sound is heard in the phones when frequency modulation is taking place. If an electron-coupled or Hartley oscillator is used, this method requires that the cathode circuit of the oscillator be inductively or capacitively coupled to the grid circuit, rather than tapped on the grid coil. The phones should be adequately bypassed for r.f. of course.

Stabilization Due to the presence of the reactance-tube frequency modulator, the stabilization of an FM oscillator in regard to voltage changes is considerably more involved than in the case of a simple self-controlled oscillator for transmitter frequency control. If desired, the oscillator itself may be made perfectly stable under voltage changes, but the presence of the frequency modulator destroys the beneficial effect of any such stabilization. It thus becomes desirable to apply the stabilizing arrangement to the modulator as well as the oscillator. If the oscillator itself is stable under voltage changes, it is only necessary to apply voltage-frequency compensation to the modulator.

Reactance-Tube Modulators Two simple reactance-tube modulators that may be applied to an existing v.f.o. are illustrated in figures 8 and 9. The circuit of figure 8 is extremely simple, yet effective. Only two tubes are used exclusive of the voltage regulator tubes which perhaps may be already incorporated in the v.f.o. A 6AU6 serves as a high-gain voltage amplifier stage, and a 6CL6 is used as the reactance modulator since its high value of transconductance will permit a large value of lagging current to be drawn under modulation swing. The unit should be

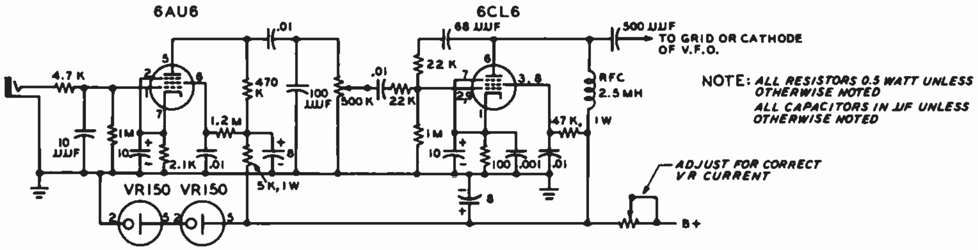


Figure 8
SIMPLE FM REACTANCE-TUBE MODULATOR

mounted in close proximity to the v.f.o. so that the lead from the 6CL6 to the grid circuit of the oscillator can be as short as possible. A practical solution is to mount the reactance modulator in a small box on the side of the v-f-o cabinet.

By incorporating speech clipping in the reactance modulator unit, a much more effective use is made of a given amount of deviation. When the FM signal is received on an AM receiver by means of slope detection, the use of speech clipping will be noticed by the greatly increased modulation level of the FM signal, and the attenuation of the center frequency null of no modulation. In many cases, it is difficult to tell a speech-clipped FM signal from the usual AM signal.

A more complex FM reactance modulator incorporating a speech clipper is shown in figure 9. A 12AX7 double triode speech amplifier provides enough gain for proper clipper action when a high level crystal microphone is used. A double diode 6AL5 speech clipper is used, the clipping level being set by the potentiometer controlling the plate voltage applied to the diode. A 6CL6 serves as the reactance modulator.

The reactance modulator may best be adjusted by listening to the signal of the v-f-o exciter at the operating frequency and adjusting the gain and clipping controls for the best modulation level consistent with minimum sideband splatter. Minimum clipping occurs when the *Adj. Clip.* potentiometer is set for maximum voltage on the plates of the 6AL5 clipper tube. As with the case of all reactance modulators, a voltage regulated plate supply is required.

Linearity Test It is almost a necessity to run a static test on the reactance-tube frequency modulator to determine its linearity and effectiveness, since small changes in the values of components, and in stray capacitances will almost certainly alter the modulator characteristics. A frequency-versus-control-voltage curve should be plotted to ascertain that equal increments in control voltage, both in a positive and a negative direction, cause equal changes in frequency. If the curve shows that the modulator has an appreciable amount of non-linearity, changes in bias, electrode voltages, r-f excitation, and resistance

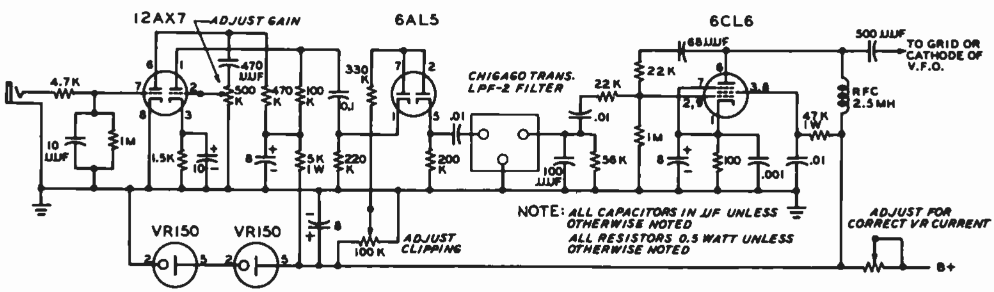


Figure 9
FM REACTANCE MODULATOR WITH SPEECH CLIPPER

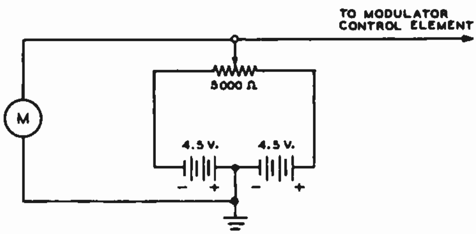


Figure 10
REACTANCE-TUBE LINEARITY CHECKER

values may be made to obtain a straight-line characteristic.

Figure 10 shows a method of connecting two 4½-volt C batteries and a potentiometer to plot the characteristic of the modulator. It will be necessary to use a zero-center voltmeter to measure the grid voltage, or else reverse the voltmeter leads when changing from positive to negative grid voltage. When a straight-line characteristic for the modulator is obtained by the static test method, the capacitances of the various by-pass capacitors in the circuit must be kept small to retain this characteristic when an audio voltage is used to vary the frequency in place of the d-c voltage with which the characteristic was plotted.

13-3 Phase Modulation

By means of phase modulation (PM) it is possible to dispense with self-controlled oscillators and to obtain directly crystal-controlled FM. In the final analysis, PM is simply frequency modulation in which the deviation is directly proportional to the modulation frequency. If an audio signal of 1000 cycles causes a deviation of ½ kc., for example, a 2000-cycle modulating signal of the same amplitude will give a deviation of 1 kc., and so on. To produce an FM signal, it is necessary to make the deviation independent of the modulation frequency, and proportional only to the modulating signal. With PM this is done by including a frequency correcting network in the transmitter. The audio correction network must have an attenuation that varies directly with frequency, and this requirement is easily met by a very simple resistance-capacity network.

The only disadvantage of PM, as compared to direct FM such as is obtained through the use of a reactance-tube modulator, is the fact that very little frequency deviation is produced directly by the phase modulator. The deviation produced by a phase modulator is independent of the actual carrier frequency on which the modulator operates, but is dependent only upon the phase deviation which is being produced and upon the modulation frequency. Expressed as an equation:

$$F_d = M_p \text{ modulating frequency}$$

Where F_d is the frequency deviation one way from the mean value of the carrier, and M_p is the phase deviation accompanying modulation expressed in radians (a radian is approximately 57.3°). Thus, to take an example, if the phase deviation is ½ radian and the modulating frequency is 1000 cycles, the frequency deviation applied to the carrier being passed through the phase modulator will be 500 cycles.

It is easy to see that an enormous amount of multiplication of the carrier frequency is required in order to obtain from a phase modulator the frequency deviation of 75 kc. required for commercial FM broadcasting. However, for amateur and commercial narrow-band FM work (NBFM) only a quite reasonable number of multiplier stages are required to obtain a deviation ratio of approximately one. Actually, phase modulation of approximately one-half radian on the output of a crystal oscillator in the 80-meter band will give adequate deviation for 29-Mc. NBFM radiotelephony. For example; if the crystal frequency is 3700 kc., the deviation in phase produced is ½ radian, and the modulating frequency is 500 cycles, the deviation in the 80-meter band will be 250 cycles. But when the crystal frequency is multiplied on up to 29,600 kc. the frequency deviation will also be multiplied by 8 so that the resulting deviation on the 10-meter band will be 2 kc. either side of the carrier for a total swing in carrier frequency of 4 kc. This amount of deviation is quite adequate for NBFM work.

Odd-harmonic distortion is produced when FM is obtained by the phase-modulation method, and the amount of this distortion that can be tolerated is the limiting factor in determining the amount of PM that can be used. Since the aforementioned frequency-correcting network causes the lowest modulating frequency to have the greatest amplitude, maximum phase modulation takes place at the lowest modulating frequency, and the amount of distortion that can be tolerated at this frequency determines the maximum deviation that can be obtained by the PM method. For high-fidelity broadcasting, the deviation produced by PM is limited to an amount equal to about one-third of the lowest modulating frequency. But for NBFM work the deviation may be as high as 0.6 of the modulating frequency before distortion becomes objectionable on voice modulation. In other terms this means that phase deviations as high as 0.6 radian may be used for amateur and commercial NBFM transmission.

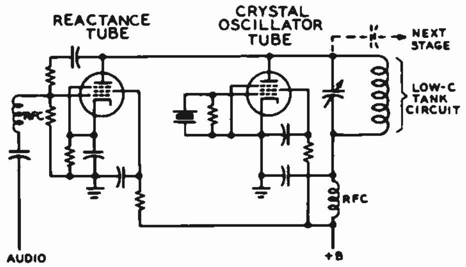


Figure 11
REACTANCE-TUBE MODULATION OF CRYSTAL OSCILLATOR STAGE

Phase-Modulation Circuits A simple reactance modulator normally used for FM may also be used for PM by connecting it to the plate circuit of a crystal oscillator stage as shown in figure 11.

Another PM circuit, suitable for operation on 20, 15 and 10 meters with the use of 80 meter crystals is shown in figure 12. A double triode 12AX7 is used as a combination Pierce crystal oscillator and phase modulator. C_1 should not be thought of as a neutralizing condenser, but rather as an adjustment for the phase of the r-f voltage acting between the grid and plate of the 12AX7 phase modulator. C_2 acts as a phase angle and magnitude control, and both these condensers should be adjusted for maximum phase modulation capabilities of the circuit. Resonance of the circuit is established by the iron slug of coil L_1-L_2. A 6CL6 is used as a doubler to 7 Mc. and delivers approximately 2 watts on this band. Additional doubler stages may be added after the 6CL6 stage to reach the desired band of operation.

Still another PM circuit, which is quite widely used commercially, is shown in figure 13. In this circuit L and C are made resonant at a frequency which is 0.707 times the operating frequency. Hence at the operating frequency the inductive reactance is twice the capacitive reactance. A cathode follower tube acts as a variable resistance in series with the L and C which go to make up the tank circuit. The operating point of the cathode follower should be chosen so that the effective resistance in series with the tank circuit (made up of the resistance of the cathode-follower tube in parallel with the cathode bias resistor of the cathode follower) is equal to the capacitive reactance of the tank capacitor at the operating frequency. The circuit is capable of about plus or minus ½ radian deviation with tolerable distortion.

Measurement of Deviation When a single-frequency modulating voltage is used with an FM transmitter, the relative amplitudes of the various sidebands and the carrier vary widely as the deviation is varied by increasing or decreasing the amount of modulation. Since the relationship between the amplitudes of the various sidebands and carrier to the audio modulating frequency and the deviation is known, a simple method of measuring the deviation of a frequency modulated transmitter is possible. In making the measurement, the result is given in the form of the modulation index for a certain amount of audio input. As previously described, the modulation index is the ratio of the peak frequency deviation to the frequency of the audio modulation.

The measurement is made by applying a sine-wave audio voltage of known frequency to the transmitter, and increasing the modulation until the amplitude of the carrier component of the frequency modulated wave reaches zero. The modulation index for zero carrier may then be determined from the table below. As may be seen from the table, the first point of zero carrier is obtained when the modulation index has a value of 2.405,—in other words, when the deviation is 2.405 times the modulation frequency. For example, if a modulation frequency of 1000 cycles is used, and the modulation is increased until the first carrier null is obtained, the deviation will then be 2.405 times the modulation frequency, or 2.405 kc. If the modulating frequency happened to be 2000 cycles, the deviation at the first null would be 4.810 kc. Other carrier nulls will be obtained when the index is 5.52, 8.654, and at increasing values separated approximately by π. The following is a listing of the modulation index at successive carrier nulls up to the tenth:

Zero carrier point no.	Modulation index
1	2.405
2	5.520
3	8.654
4	11.792
5	14.931
6	18.071
7	21.212
8	24.353
9	27.494
10	30.635

The only equipment required for making the measurements is a calibrated audio oscillator of good wave form, and a communication receiver equipped with a beat oscillator and crystal filter. The receiver should be used with its crystal filter set for minimum bandwidth to exclude sidebands spaced from the carrier by the modulation frequency. The un-

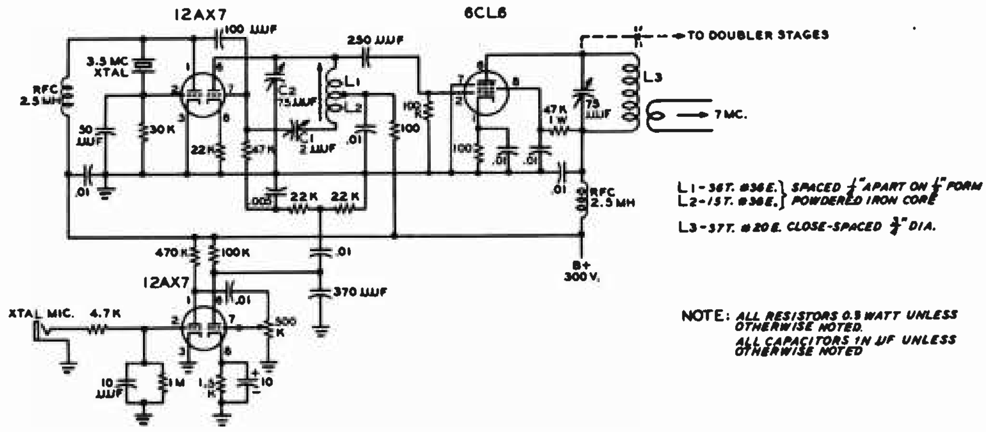


Figure 12
REACTANCE MODULATOR FOR 10, 15 AND 20 METER OPERATION

modulated carrier is accurately tuned in on the receiver with the beat oscillator operating. Then modulation from the audio oscillator is applied to the transmitter, and the modulation is increased until the first carrier null is obtained. This carrier null will correspond to a modulation index of 2.405, as previously mentioned. Successive null points will correspond to the indices listed in the table.

A volume indicator in the transmitter audio system may be used to measure the audio level required for different amounts of deviation, and the indicator thus calibrated in terms of frequency deviation. If the measurements are made at the fundamental frequency of the oscillator, it will be necessary to multiply the frequency deviation by the harmonic upon which the transmitter is operating, of course. It will probably be most convenient to make the determination at some frequency intermediate between that of the oscillator and that at which the transmitter is operating, and then to multiply the result by the frequency multiplication between that frequency and the transmitter output frequency.

13-4 Reception of FM Signals

A conventional communications receiver may be used to receive narrow-band FM transmissions, although performance will be much poorer than can be obtained with an NBFM receiver or adapter. However, a receiver specifically designed for FM reception must be used when it is desired to receive high deviation FM such as used by FM broadcast stations, TV sound, and mobile communications FM.

The FM receiver must have, first of all, a bandwidth sufficient to pass the range of frequencies generated by the FM transmitter. And since the receiver must be a superheterodyne if it is to have good sensitivity at the frequencies to which FM is restricted, i-f bandwidth is an important factor in its design.

The second requirement of the FM receiver is that it incorporate some sort of device for converting frequency changes into amplitude changes, in other words, a detector operating on frequency variations rather than amplitude variations. The third requirement, and one which is necessary if the full noise reducing capa-

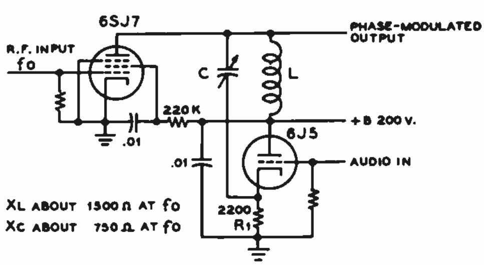


Figure 13
CATHODE-FOLLOWER PHASE MODULATOR

The phase modulator illustrated above is quite satisfactory when the stage is to be operated on a single frequency or over a narrow range of frequencies.

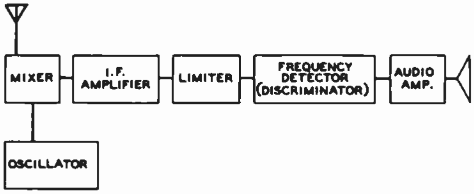


Figure 14
FM RECEIVER BLOCK DIAGRAM
Up to the amplitude limiter stage, the FM receiver is similar to an AM receiver, except for a somewhat wider i-f bandwidth. The limiter removes any amplitude modulation, and the frequency detector following the limiter converts frequency variations into amplitude variations.

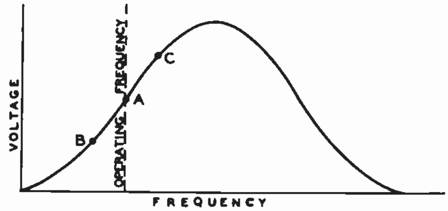


Figure 15
SLOPE DETECTION OF FM SIGNAL
One side of the response characteristic of a tuned circuit or of an i-f amplifier may be used as shown to convert frequency variations of an incoming signal into amplitude variations.

bilities of the FM system of transmission are desired, is a limiting device to eliminate amplitude variations before they reach the detector. A block diagram of the essential parts of an FM receiver is shown in figure 14.

The Frequency Detector The simplest device for converting frequency variations to amplitude variations is an "off-tune" resonant circuit, as illustrated in figure 15. With the carrier tuned in at point "A," a certain amount of r-f voltage will be developed across the tuned circuit, and, as the frequency is varied either side of this frequency by the modulation, the r-f voltage will increase and decrease to points "C" and "B" in accordance with the modulation. If the voltage across the tuned circuit is applied to an ordinary detector, the detector output will vary in accordance with the modulation, the amplitude of the variation being proportional to the deviation of the signal, and the rate being equal to the modulation frequency. It is obvious from figure 15 that only a small portion of the resonance curve is usable for linear conversion of frequency variations into amplitude variations, since the linear portion of the curve is rather short. Any frequency variation which exceeds the linear portion will cause distortion of the recovered audio. It is also obvious by inspection of figure 15 that an AM receiver used in this manner is wide open to signals on the peak of the resonance curve and also to signals on the other side of the resonance curve. Further, no noise limiting action is afforded by this type of reception. This system, therefore, is not recommended for FM reception, although widely used by amateurs for occasional NBFM reception.

Travis Discriminator Another form of frequency detector or *discriminator,* is shown in figure 16. In this arrangement two tuned circuits are used, one tuned on each side of the i-f amplifier frequency, and with their resonant frequencies spaced slightly more than the expected transmitter swing. Their outputs are combined in a differential rectifier so that the voltage across the series load resistors, R_1 and R_2, is equal to the algebraic sum of the individual output voltages of each rectifier. When a signal at the

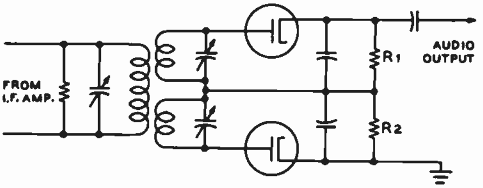


Figure 16
TRAVIS DISCRIMINATOR
This type of discriminator makes use of two off-tuned resonant circuits coupled to a single primary winding. The circuit is capable of excellent linearity, but is difficult to align.

At its "center" frequency the discriminator produces zero output voltage. On either side of this frequency it gives a voltage of a polarity and magnitude which depend on the direction and amount of frequency shift.

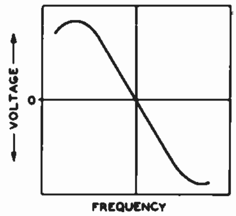


Figure 17
DISCRIMINATOR VOLTAGE-FREQUENCY CURVE

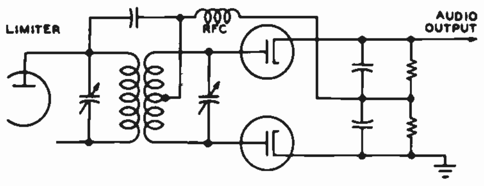


Figure 18
FOSTER-SEELEY DISCRIMINATOR
This discriminator is the most widely used circuit since it is capable of excellent linearity and is relatively simple to align when proper test equipment is available.

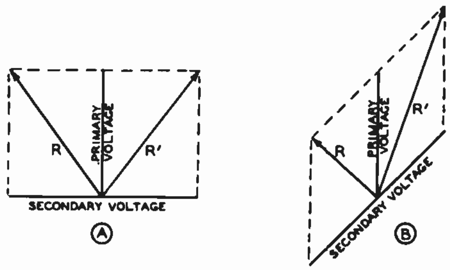


Figure 19
DISCRIMINATOR VECTOR DIAGRAM
A signal at the resonant frequency of the secondary will cause the secondary voltage to be 90 degrees out of phase with the primary voltage, as shown at A, and the resultant voltages R and R' are equal. If the signal frequency changes, the phase relationship also changes, and the resultant voltages are no longer equal, as shown at B. A differential rectifier is used to give an output voltage proportional to the difference between R and R'.

i-f mid-frequency is received, the voltages across the load resistors are equal and opposite, and the sum voltage is zero. As the r-f signal varies from the mid-frequency, however, these individual voltages become unequal, and a voltage having the polarity of the larger voltage and equal to the difference between the two voltages appears across the series resistors, and is applied to the audio amplifier. The relationship between frequency and discriminator output voltage is shown in figure 17. The separation of the discriminator peaks and the linearity of the output voltage vs. frequency curve depend upon the discriminator frequency, the Q of the tuned circuits, and the value of the diode load resistors. As the intermediate (and discriminator) frequency is increased, the peaks must be separated further to secure good linearity and output. Within limits, as the diode load resistance or the Q is reduced, the linearity improves, and the separation between the peaks must be greater.

Foster-Seeley Discriminator The most widely used form of discriminator is that shown in figure 18. This type of discriminator yields an output-voltage-versus-frequency characteristic similar to that shown in figure 19. Here, again, the output voltage is equal to the algebraic sum of the voltages developed across the load resistors of the two diodes, the resistors being connected in series to ground. However, this *Foster-Seeley* discriminator requires only two tuned circuits instead of the three used in the previous discriminator. The operation of the circuit results from the phase relationships existing in a transformer having a tuned secondary. In effect, as a close examination of the circuit will reveal, the primary circuit is in series, for r.f., with each half of the secondary to ground. When the received signal is at the resonant frequency of the secondary, the r-f voltage across the secondary is 90 degrees out of phase with that across the primary. Since each diode is connected across one half of the secondary winding and the primary winding in series, the resultant r-f voltages applied to each are equal, and the voltages developed across each diode load resistor are equal and of opposite polarity. Hence, the net voltage between the top of the load resistors and ground is zero. This is shown vectorially in figure 19A where the resultant voltages R and R' which are applied to the two diodes are shown to be equal when the phase angle between primary and secondary voltages is 90 degrees. If, however, the signal varies from the resonant frequency, the 90-degree phase relationship no longer exists between primary and secondary. The result of this effect is shown in figure 19B where the secondary r-f voltage is no longer 90 degrees out of phase with respect to the primary voltage. The resultant voltages applied to the two diodes are now no longer equal, and a d-c voltage proportional to the difference between the r-f voltages applied to the two diodes will exist across the series load resistors. As the signal frequency varies back and forth across the resonant frequency of the discriminator, an a-c voltage of the same frequency as the original modulation, and proportional to the deviation, is developed and passed on to the audio amplifier.

Ratio Detector One of the more recent types of FM detector circuits, called the *ratio detector* is diagrammed in figure 20. The input transformer can be designed so that the parallel input voltage to the diodes can be taken from a tap on the primary of the trans-

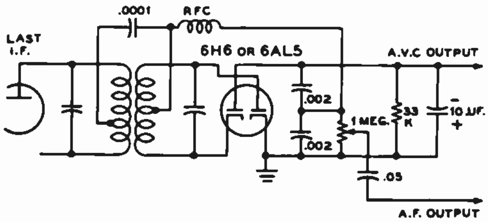


Figure 20
RATIO DETECTOR CIRCUIT

The parallel voltage to the diodes in a ratio detector may be obtained from a tap on the primary winding of the transformer or from a third winding. Note that one of the diodes is reversed from the system used with the Foster-Seeley discriminator, and that the output circuit is completely different. The ratio detector does not have to be preceded by a limiter, but is more difficult to align for distortion-free output than the conventional discriminator.

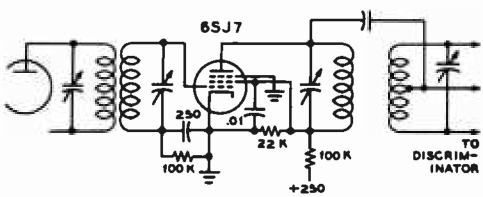


Figure 21
LIMITER CIRCUIT

One, or sometimes two, limiter stages normally precede the discriminator so that a constant signal level will be fed to the FM detector. This procedure eliminates amplitude variations in the signal fed to the discriminator, so that it will respond only to frequency changes.

former, or this voltage may be obtained from a tertiary winding coupled to the primary. The r-f choke used must have high impedance at the intermediate frequency used in the receiver, although this choke is not needed if the transformer has a tertiary winding.

The circuit of the ratio detector appears very similar to that of the more conventional discriminator arrangement. However, it will be noted that the two diodes in the ratio detector are poled so that their d-c output voltages add, as contrasted to the Foster-Seeley circuit wherein the diodes are poled so that the d-c output voltages buck each other. At the center frequency to which the discriminator transformer is tuned the voltage appearing at the top of the 1-megohm potentiometer will be one-half the d-c voltage appearing at the *a-v-c output* terminal—since the contribution of each diode will be the same. However, as the input frequency varies to one side or the other of the tuned value (while remaining within the pass band of the i-f amplifier feeding the detector) the relative contributions of the two diodes will be different. The voltage appearing at the top of the 1-megohm volume control will increase for frequency deviations in one direction and will decrease for frequency deviations in the other direction from the mean or tuned value of the transformer. The audio output voltage is equal to the ratio of the relative contributions of the two diodes, hence the name ratio detector.

The ratio detector offers several advantages over the simple discriminator circuit. The circuit does not require the use of a limiter preceding the detector since the circuit is inherently insensitive to amplitude modulation on an incoming signal. This factor alone means that the r-f and i-f gain ahead of the detector can be much less than the conventional discriminator for the same overall sensitivity. Further, the circuit provides a-v-c voltage for controlling the gain of the preceding r-f and i-f stages. The ratio detector is, however, susceptible to variations in the amplitude of the incoming signal as is any other detector circuit except the discriminator *with* a limiter preceding it, so that a-v-c should be used on the stages preceding the detector.

Limiters The limiter of an FM receiver using a conventional discriminator serves to remove amplitude modulation and pass on to the discriminator a frequency modulated signal of constant amplitude; a typical circuit is shown in figure 21. The limiter tube is operated as an i-f stage with very low plate voltage and with grid leak bias, so that it overloads quite easily. Up to a certain point the output of the limiter will increase with an increase in signal. Above this point, however, the limiter becomes overloaded, and further large increases in signal will not give any increase in output. To operate successfully, the limiter must be supplied with a large amount of signal, so that the amplitude of its output will not change for rather wide variations in amplitude of the signal. Noise, which causes little frequency modulation but much amplitude modulation of the received signal, is virtually wiped out in the limiter.

The voltage across the grid resistor varies with the amplitude of the received signal. For this reason, conventional amplitude modulated signals may be received on the FM receiver by connecting the input of the audio amplifier to the top of this resistor, rather than to the discriminator output. When properly filtered.

by a simple R-C circuit, the voltage across the grid resistor may also be used as a-v-c voltage for the receiver. When the limiter is operating properly, a.v.c. is neither necessary nor desirable, however, for FM reception alone.

Receiver Design Considerations One of the most important factors in the design of an FM receiver is the frequency swing which it is intended to handle. It will be apparent from figure 17 that if the straight portion of the discriminator circuit covers a wider range of frequencies than those generated by the transmitter, the audio output will be reduced from the maximum value of which the receiver is capable.

In this respect, the term "modulation percentage" is more applicable to the FM receiver than it is to the transmitter, since the modulation capability of the communication system is limited by the receiver bandwidth and the discriminator characteristic; full utilization of the linear portion of the characteristic amounts, in effect, to 100 per cent modulation. This means that some sort of standard must be agreed upon, for any particular type of communication, to make it unnecessary to vary the transmitter swing to accommodate different receivers.

Two considerations influence the receiver bandwidth necessary for any particular type of communication. These are the maximum audio frequency which the system will handle, and the deviation ratio which will be employed. For voice communication, the maximum audio frequency is more or less fixed at 3000 to 4000 cycles. In the matter of deviation ratio, however, the amount of noise suppression which the FM system will provide is influenced by the ratio chosen, since the improvement in signal-to-noise ratio which the FM system shows over amplitude modulation is equivalent to a constant *multiplied by the deviation ratio.* This assumes that the signal is somewhat stronger than the noise at the receiver, however, as the advantages of wideband FM in regard to noise suppression disappear when the signal-to-noise ratio approaches unity.

On the other hand, a low deviation ratio is more satisfactoty for strictly communication work, where readability at low signal-to-noise ratios is more important than additional noise suppression when the signal is already appreciably stronger than the noise.

As mentioned previously, broadcast FM practice is to use a deviation ratio of 5. When this ratio is applied to a voice-communication system, the total swing becomes 30 to 40 kc. With lower deviation ratios, such as are most frequently used for voice work, the swing becomes proportionally less, until at a deviation ratio of 1 the swing is equal to twice the highest audio frequency. Actually, however, the receiver bandwidth must be slightly greater than the expected transmitter swing, since for distortionless reception the receiver must pass the complete band of energy generated by the transmitter, and this band will always cover a range somewhat wider than the transmitter swing.

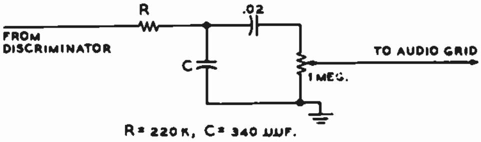


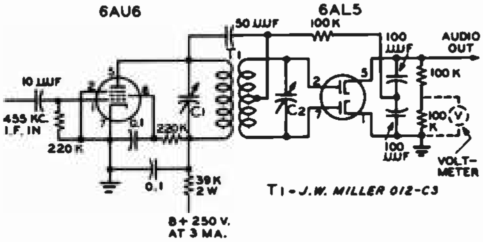
Figure 22
75-MICROSECOND DE-EMPHASIS CIRCUITS

The audio signal transmitted by FM and TV stations has received high-frequency pre-emphasis, so that a de-emphasis circuit should be included between the output of the FM detector and the input of the audio system.

Pre-Emphasis and De-Emphasis Standards in FM broadcast and TV sound work call for the pre-emphasis of all audio modulating frequencies above about 2000 cycles, with a rising slope such as would be produced by a 75-microsecond RL network. Thus the FM receiver should include a compensating de-emphasis RC network with a time constant of 75 microseconds so that the overall frequency response from microphone to loudspeaker will approach linearity. The use of pre-emphasis and de-emphasis in this manner results in a considerable improvement in the overall signal-to-noise ratio of an FM system. Appropriate values for the de-emphasis network, for different values of circuit impedance are given in figure 22.

A NBFM 455-kc. Adapter Unit The unit diagrammed in figure 23 is designed to provide NBFM reception when attached to any communication receiver having a 455-kc. i-f amplifier. Although NBFM can be received on an AM receiver by tuning the receiver to one side or the other of the incoming signal, a tremendous improvement in signal-to-noise ratio and in signal to amplitude ratio will be obtained by the use of a true FM detector system.

The adapter uses two tubes. A 6AU6 is used as a limiter, and a 6AL5 as a discriminator. The audio level is approximately 10



NOTE: *ALL CAPACITORS IN µF UNLESS OTHERWISE NOTED*
ALL RESISTORS 0.5 WATT UNLESS OTHERWISE NOTED

Figure 23
NBFM ADAPTER FOR 455-KC. I-F SYSTEM

volts peak for the maximum deviation which can be handled by a conventional 455-kc. i-f system. The unit may be tuned by placing a high resistance d-c voltmeter across R_1 and tuning the trimmers of the i-f transformer for maximum voltage when an unmodulated signal is injected into the i-f strip of the receiver. The voltmeter should next be connected across the audio output terminal of the discriminator. The receiver is now tuned back and forth across the frequency of the incoming signal, and the movement of the voltmeter noted. When the receiver is exactly tuned on the signal the voltmeter reading should be zero. When the receiver is tuned to one side of center, the voltmeter reading should increase to a maximum value and then decrease gradually to zero as the signal is tuned out of the passband of the receiver. When the receiver is tuned to the other side of the signal the voltmeter should increase to the same maximum value but in the opposite direction or polarity, and then fall to zero as the signal is tuned out of the passband. It may be necessary to make small adjustments to C_1 and C_2 to make the voltmeter read zero when the signal is tuned in the center of the passband.

CHAPTER FOURTEEN

Single-Sideband Transmission

While single-sideband transmission has attracted significant interest on amateur frequencies only in the past few years, the principles have been recognized and put to use in various commercial applications for many years. Expansion of single-sideband for both commercial and amateur communication has awaited the development of economical components possessing the required characteristics (such as sharp cutoff filters and high stability crystals) demanded by SSB techniques. The availability of such components and precision test equipment now makes possible the economical testing, adjustment and use of SSB equipment on a wider scale than before. Many of the seemingly insurmountable obstacles of past years no longer prevent the amateur from achieving the advantages of SSB for his class of operation.

14-1 Commercial Applications of SSB

Before discussion of amateur SSB equipment, it is helpful to review some of the commercial applications of SSB in an effort to avoid problems that are already solved.

The first and only large scale use of SSB has been for multiplexing additional voice circuits on long distance telephone toll wires. Carrier systems came into wide use during the 30's, accompanied by the development of high Q toroids and copper oxide ring modulators of controlled characteristics.

The problem solved by the carrier system was that of translating the 300-3000 cycle voice band of frequencies to a higher frequency (for example, 40.3 to 43.0 kc.) for transmission on the toll wires, and then to reverse the translation process at the receiving terminal. It was possible in some short-haul equipment to amplitude modulate a 40 kilocycle carrier with the voice frequencies, in which case the resulting signal would occupy a band of frequencies between 37 and 43 kilocycles. Since the transmission properties of wires and cable deteriorate rapidly with increasing frequency, most systems required the bandwidth conservation characteristics of single-sideband transmission. In addition, the carrier wave was generally suppressed to reduce the power handling capability of the repeater amplifiers and diode modulators. A substantial body of literature on the components and circuit techniques of SSB has been generated by the large and continuing development effort to produce economical carrier telephone systems.

The use of SSB for overseas radiotelephony has been practiced for several years though the number of such circuits has been numerically small. However, the economic value of such circuits has been great enough to warrant elaborate station equipment. It is from these stations that the impression has been obtained that SSB is too complicated for all but a corps of engineers and technicians to handle. Components such as lattice filters with 40 or more crystals have suggested astronomical expense.

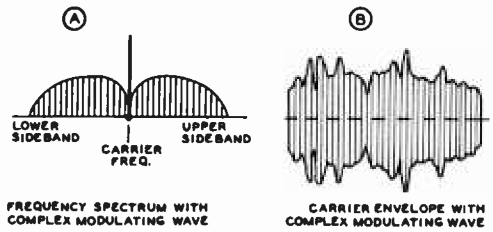


Figure 1
REPRESENTATION OF A CONVENTIONAL AM SIGNAL

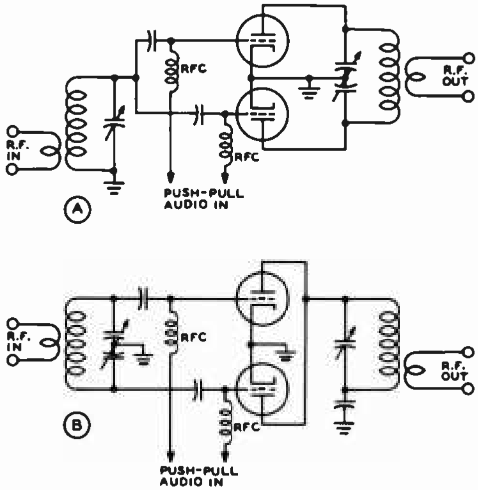


Figure 2
SHOWING TWO COMMON TYPES OF BALANCED MODULATORS

Notice that a balanced modulator changes the circuit condition from single ended to push-pull, or vice versa. Choice of circuit depends upon external circuit conditions since both the (A) and (B) arrangements can give satisfactory generation of a double-sideband suppressed-carrier signal.

More recently, SSB techniques have been used to multiplex large numbers of voice channels on a microwave radio band using equipment principally developed for telephone carrier applications. It should be noted that all production equipment employed in these services uses the *filter method* of generating the single-sideband signal, though there is a wide variation in the types of filters actually used. The SSB signal is generated at a low frequency and at a low level, and then translated and linearly amplified to a high level at the operating frequency.

Considerable development effort has been expended on high level phasing type transmitters wherein the problems of linear amplification are exchanged for the problems of accurately controlled phase shifts. Such equipment has featured automatic tuning circuits, servo-driven to facilitate frequency changing, but no transmitter of this type has been sufficiently attractive to warrant appreciable production.

14-2 Derivation of Single-Sideband Signals

The single-sideband method of communication is, essentially, a procedure for obtaining more efficient use of available frequency spectrum and of available transmitter capability. As a starting point for the discussion of single-sideband signals, let us take a conventional AM signal, such as shown in figure 1, as representing the most common method for transmitting complex intelligence such as voice or music.

It will be noted in figure 1 that there are three distinct portions to the signal: the carrier, and the upper and the lower sideband group. These three portions always are present in a conventional AM signal. Of all these portions the carrier is the least necessary and the most expensive to transmit. It is an actual fact, and it can be proved mathematically (and physically with a highly selective receiver) that the carrier of an AM signal remains unchanged in amplitude, whether it is being modulated or not. Of course the carrier *appears* to be modulated when we observe the modulated signal on a receiving system or indicator which passes a sufficiently wide band that the carrier and the modulation sidebands are viewed at the same time. This apparent change in the amplitude of the carrier with modulation is simply the result of the sidebands beating with the carrier. However, if we receive the signal on a highly selective receiver, and if we modulate the carrier with a sine wave of 3000 to 5000 cycles, we will readily see that the carrier, or either of the sidebands can be tuned in separately; the carrier amplitude, as observed on a signal strength meter, will remain constant, while the amplitude of the sidebands will vary in direct proportion to the modulation percentage.

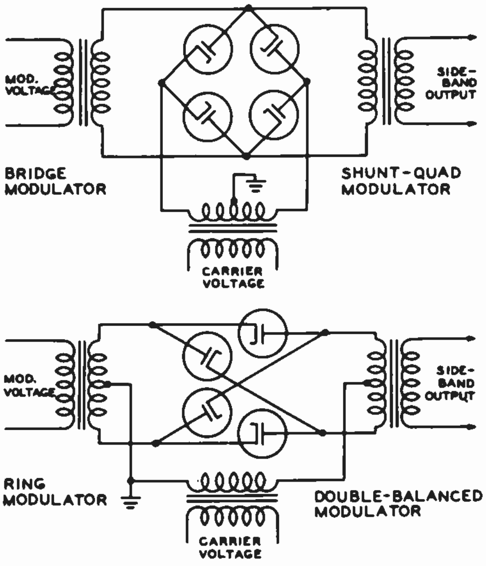


Figure 3

TWO TYPES OF DIODE BALANCED MODULATOR

Such balanced modulator circuits are commonly used in carrier telephone work and in single-sideband systems where the carrier frequency and modulating frequency are relatively close together. Vacuum diodes, copper-oxide rectifiers, or crystal diodes may be used in the circuits.

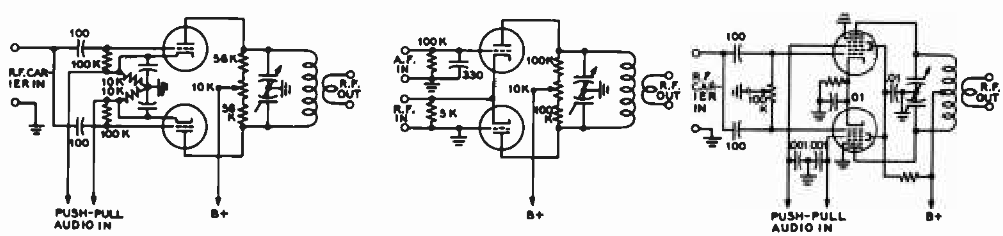
Elimination of the Carrier From the discussion in the previous paragraphs it is obvious that the carrier is superfluous so far as transmitting intelligence is concerned. It obviously is a *convenience,* however, since it provides a signal at the receiving end for the sidebands to beat with and thus to reproduce the original modulating signal.

Two modulated amplifiers may be connected with the carrier inputs 180° out of phase, and with the carrier outputs in parallel. The carrier will be balanced out of the output circuit, leaving only the two sidebands. Such a circuit is called a *balanced modulator.*

Any non-linear element will produce modulation. That is, if two signals are put in, sum and difference frequencies as well as the original frequencies appear in the output. This phenomenon is objectionable in amplifiers and desirable in modulators or mixers.

In addition to the sum and difference frequencies, other outputs (such as twice one frequency plus the other) may appear. All combinations of all harmonics of each input frequency may appear, but in general these are of decreasing amplitude with increasing order of harmonic. These outputs are usually rejected by selective circuits following the modulator. All modulators are not alike in the magnitude of these higher order outputs. Balanced diode rings operating in the square law region are fairly good; pentagrid converters much poorer. Excessive carrier level in tube mixers will increase the relative magnitude of the higher order outputs. Two types of triode balanced modulators are shown in figure 2, and two types of diode modulators are shown in figure 3. Balanced modulators employing vacuum tubes may be made to work very easily to a point. Circuits may be devised wherein both input signals may be applied to a high impedance grid, simplifying isolation and loading problems. The most important difficulties with these vacuum tube modulator circuits are: (1) Balance is not independent of signal level. (2) Balance drifts with time and environment. (3) The carrier level for low "high-order output" is critical, and (4) Such circuits have limited dynamic range.

A number of typical circuits are shown in



Ⓐ PLATE MODULATED BALANCED TRIODE MODULATOR

Ⓑ BALANCED TRIODE MODULATOR WITH SINGLE ENDED INPUT CIRCUITS

Ⓒ BALANCED PENTAGRID CONVERTER MODULATOR

Figure 4

BALANCED MODULATORS

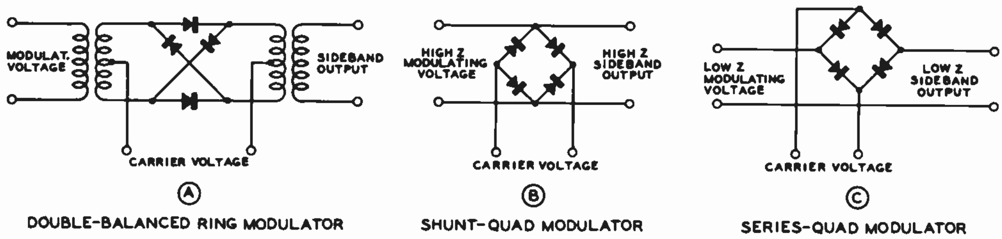


Figure 5
DIODE RING MODULATORS

figure 4. Of the group the most satisfactory performance is to be had from plate modulated triodes.

Diode Ring Modulators Modulation in telephone carrier equipment has been very successfully accomplished with copper-oxide double balanced ring modulators. More recently, germanium diodes have been applied to similar circuits. The basic diode ring circuits are shown in figure 5. The most widely applied is the double balanced ring (A). Both carrier and input are balanced with respect to the output, which is advantageous when the output frequency is not sufficiently different from the inputs to allow ready separation by filters. It should be noted that the carrier must pass through the balanced input and output transformers. Care must be taken in adapting this circuit to minimize the carrier power that will be lost in these elements. The shunt and series quad circuits are usable when the output frequencies are entirely different (i.e.: audio and r.f.). The shunt quad (B) is used with high source and load impedances and the series quad (C) with low source and load impedances. These two circuits may be adapted to use only two diodes, substituting a balanced transformer for one side of the bridge, as shown in figure 6. It should be noted that these circuits present a half-wave load to the carrier source. In applying any of these circuits, r-f chokes and capacitors must be employed to control the path of signal and carrier currents. In the shunt pair, for example, a blocking capacitor is used to prevent the r-f load from shorting the audio input.

To a first approximation, the source and load impedances should be the arithmetical mean of the forward and back resistances of the diodes employed. A workable rule of thumb is that the source and load impedances be ten to twenty times the forward resistance for semiconductor rings. The high frequency limit of operation in the case of junction and copper-oxide diodes may be appreciably extended by the use of very low source and load impedances.

Copper-oxide diodes suitable for carrier work are normally manufactured to order. They offer no particular advantage to the amateur, though their excellent long-term stability is important in commercial applications. Rectifier types intended to be used as meter rectifiers are not likely to have the balance or high frequency response desirable in amateur SSB transmitters.

Vacuum diodes such as the 6AL5 may be used as modulators. Balancing the heater-cathode capacity is a major difficulty except when the 6AL5 is used at low source and load impedance levels. In addition, contact potentials of the order of a few tenths of a volt may also disturb low level applications (figure 7).

The double diode circuits appear attractive, but in general it is more difficult to balance a transformer at carrier frequency than an additional pair of diodes. Balancing potentiometers may be employed, but the actual cause of the

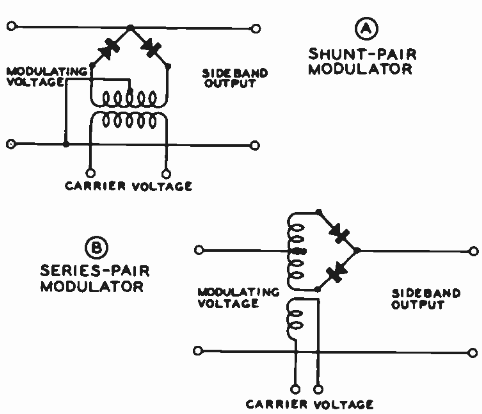
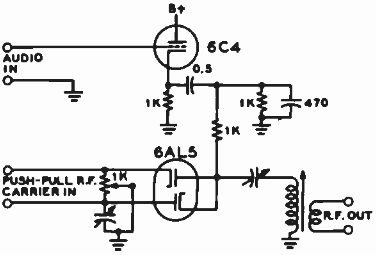
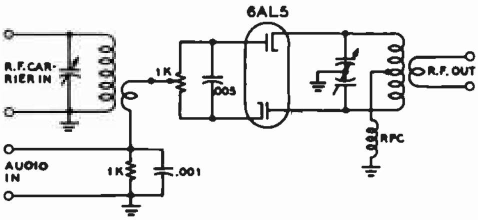


Figure 6
DOUBLE-DIODE PAIRED MODULATORS

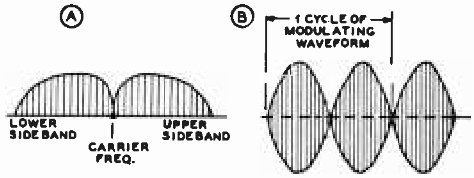


Ⓐ SERIES-BALANCED DIODE MODULATOR USING 6AL5 TUBE



Ⓑ RING-DIODE MODULATOR USING 6AL5 TUBE

Figure 7
VACUUM DIODE MODULATOR CIRCUITS



FREQUENCY SPECTRUM WITH COMPLEX MODULATING WAVE

DOUBLE SIDE-BAND OUTPUT FROM BALANCED MODULATOR WITH SINE-WAVE MODULATION

Figure 8
DOUBLE-SIDEBAND SUPPRESSED-CARRIER SIGNAL

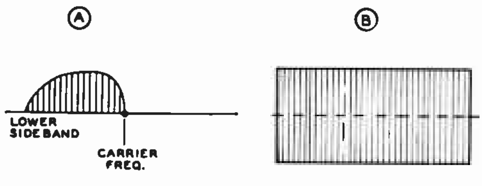
The envelope shown at B also is obtained on the oscilloscope when two audio frequencies of the same amplitude are fed to the input of a single-sideband transmitter.

unbalance is far more subtile, and cannot be adequately corrected with a single adjustment.

A signal produced by any of the above circuits may be classified as a *double sideband, suppressed-carrier* signal.

Re-insertion of the Carrier A representation of a double-sideband suppressed-carrier signal, such as would appear at the output of a balanced modulator, is shown in figure 8. Such signals can be, and have been used for communication on the amateur bands and other frequency ranges. When such a signal is being received on a conventional communications receiver, with a diode detector for example, the signal occupies the same amount of spectrum as a conventional AM signal, except that the carrier interference is not present—however, the rectified signal will have 100 per cent second harmonic distortion. This is to say that each of the original modulating frequencies will be doubled by the rectifying action of the diode second detector in the communications receiver.

If the carrier is re-inserted at the communications receiver, through use of the beat oscillator on the receiver or some other signal source such as a frequency-meter signal generator, the harmonic distortion will be reduced proportionately until the re-inserted carrier has twice the peak amplitude of the received signal; when the re-inserted carrier is more than twice the amplitude of the double-sideband suppressed-carrier received the distortion will be eliminated and the received signal will be quite normal in all respects. *However,* the re-inserted carrier must have exactly the correct frequency and *phase* to obtain distortion-free demodulation. This is not easily accomplished by any manual means. But if a small amount of carrier is transmitted with the double-sideband signal, say 2 to 5 per cent, the locally generated carrier at the receiver may be *locked* in frequency and phase to the received pilot carrier by electrical means so that normal distortion-free reception is possible.



FREQUENCY SPECTRUM WITH COMPLEX MODULATING WAVE

SIGNAL ENVELOPE WITH SINGLE-FREQUENCY MODULATING WAVE.

Figure 9
SINGLE-SIDEBAND SUPPRESSED-CARRIER SIGNAL

Note that the signal envelope, as viewed on an oscilloscope, appears as an unmodulated carrier with a single-frequency modulating tone; the frequency of the signal will be either the sum or the difference between the suppressed carrier frequency and the modulating frequency. In the absence of modulation the signal output is negligible.

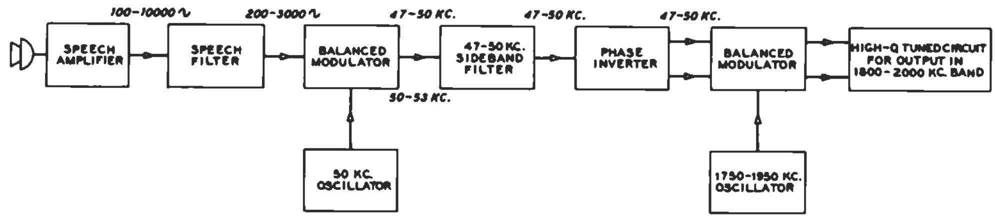


Figure 10

BLOCK DIAGRAM OF FILTER EXCITER EMPLOYING A 50-KC. SIDEBAND FILTER

Suppression of One Sideband The superfluity of the carrier, except as a convenience, has been discussed. But it is equally true that the transmission of both sidebands also is superfluous since identically the same intelligence is contained in both sidebands. And further, the transmission of both sidebands is an inconvenience since the re-inserted carrier must have identically the correct frequency and phase if both sidebands are transmitted; but if only one sideband is transmitted the re-inserted carrier need have a frequency only approximately correct (within a few cycles) for satisfactory demodulation of the single-sideband signal. This means that a single-sideband signal may be received on any good communications receiver whose high-frequency oscillator and beat-frequency oscillator have good stability.

A typical SSB signal is shown in figure 9.

Single-Sideband Power Gain and Signal Effectiveness A sizeable increase in the effectiveness of a transmitter with a specified peak power capability is attainable through the use of single-sideband transmission. Actually, when transmitters are compared on the basis of peak power capability alone, the effective signal improvement at a receiver is about 9 db for a single-sideband signal as compared to a conventional AM signal.

A further advantage of single-sideband transmission is that the undesirable effects of selective fading are greatly reduced as compared to AM. Completely satisfactory SSB communication can be had when propagation conditions are such that the intelligibility of conventional AM signals over the same signal path is almost unusable. Also, the average power input to a SSB transmitter is a very small fraction of the power input to a conventional AM transmitter of the same power rating. This is true since a signal is being emitted from the SSB transmitter only during the instants of modulation and the amount of power being taken from the line, as well as the signal being transmitted, is in direct proportion to the level of signal being transmitted. Further, since no signal is transmitted between speech passages, it is possible to operate duplex transmission on the same frequency. (This is true in general only of the filter method, unless extremely good shielding of the local carrier generator of the transmitter is being employed.)

14-3 Generation of Single-Sideband Signals

In general, there are two methods by which a single-sideband signal may be generated. These systems are: (1) The Filter Method, and (2) The Phasing Method. The systems

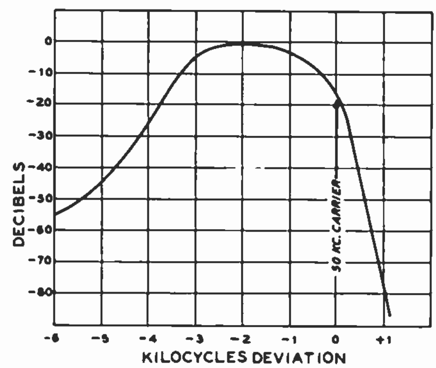


Figure 11

BANDPASS CHARACTERISTIC OF BURNELL S-15000 SINGLE SIDEBAND FILTER

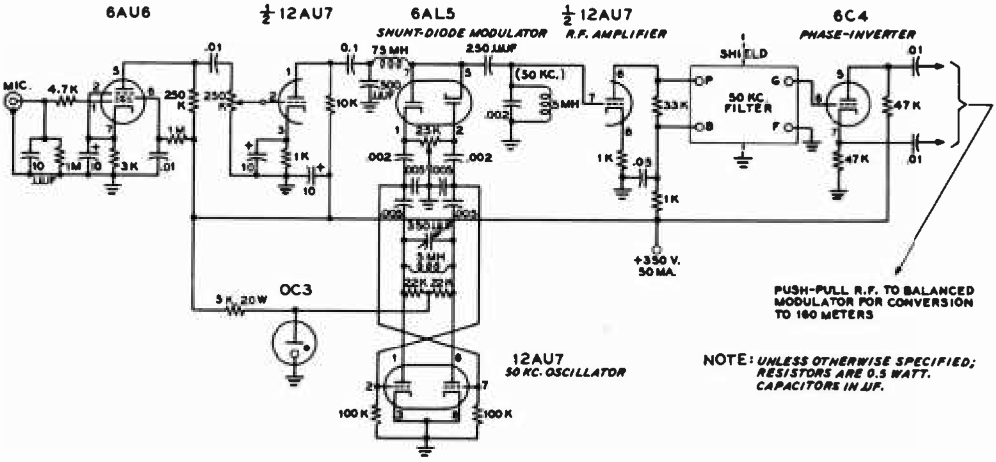


Figure 12
OPERATIONAL CIRCUIT FOR SSB EXCITER USING THE BURNELL 50-KC. SIDEBAND FILTER

may be used singly or in combination, and either method, in theory, may be used at the operating frequency of the transmitter or at some other frequency with the signal at the operating frequency being obtained through the use of frequency changers (mixers).

The Filter Method The filter method for obtaining a SSB signal is the classic method which has been in use by the telephone companies for many years both for landline and radio communications. The mode of operation of the filter method is diagrammed in figure 10, in terms of components and filters which normally would be available to the amateur or experimenter. The output of the speech amplifier passes through a conventional speech filter to limit the frequency range of the speech to about 200 to 3000 cycles. This signal then is fed to a balanced modulator along with a 50,000-cycle first carrier from a self-excited oscillator. A low-frequency balanced modulator of this type most conveniently may be made up of four diodes of the vacuum or crystal type cross connected in a balanced bridge or ring modulator circuit. Such a modulator passes only the sideband components resulting from the sum and difference between the two signals being fed to the balanced modulator. The audio signal and the 50-kc. carrier signal from the oscillator both cancel out in the balanced modulator so that a band of frequencies between 47 and 50 kc. and another band of frequencies between 50 and 53 kc. appear in the output.

The signals from the first balanced modulator are then fed through the most critical component in the whole system—the first sideband filter. It is the function of this first sideband filter to separate the desired 47 to 50 kc. sideband from the unneeded and undesired 50 to 53 kc. sideband. Hence this filter must have low attenuation in the region between 47 and 50 kc., a very rapid slope in the vicinity of 50 kc., and a very high attenuation to the sideband components falling between 50 and 53 kilocycles.

Burnell & Co., Inc., of Yonkers, New York produce such a filter, designated as *Burnell S-15,000*. The passband of this filter is shown in figure 11.

Appearing, then, at the output of the filter is a single sideband of 47 kc. to 50 kc. This sideband may be passed through a phase inverter to obtain a balanced output, and then fed to a balanced mixer. A local oscillator operating in the range of 1750 kc. to 1950 kc. is used as the conversion oscillator. Additional conversion stages may now be added to translate the SSB signal to the desired frequency. Since only linear amplification may be used, it is not possible to use frequency multiplying stages. Any frequency changing must be done by the beating-oscillator technique. An operational circuit of this type of SSB exciter is shown in figure 12.

A second type of filter-exciter for SSB may be built around the *Collins* Mechanical Filter. Such an exciter is diagrammed in figure 13.

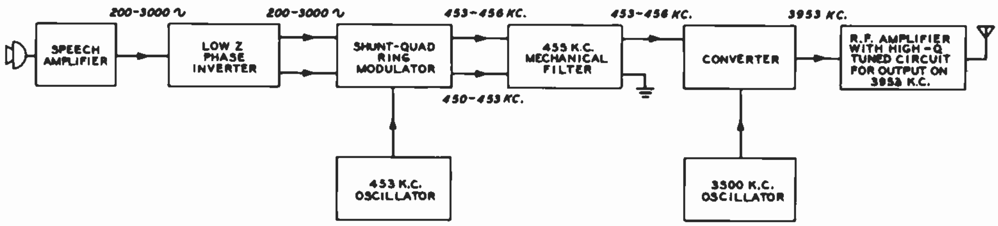


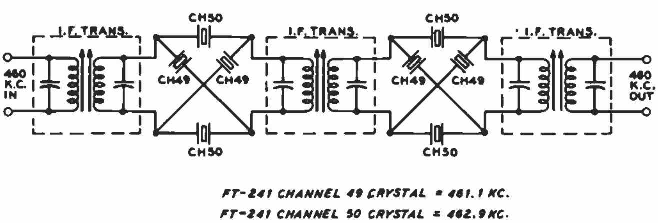
Figure 13

BLOCK DIAGRAM OF FILTER EXCITER EMPLOYING A 455-KC. MECHANICAL FILTER FOR SIDEBAND SELECTION

Voice frequencies in the range of 200-3000 cycles are amplified and fed to a low impedance phase-inverter to furnish balanced audio. This audio, together with a suitably chosen r-f signal are mixed in a ring modulator, made up of small germanium diodes. Depending upon the choice of frequency of the r-f oscillator, either the upper or lower sideband may be applied to the input of the mechanical filter. The carrier, to some extent, has been rejected by the ring modulator. Additional carrier rejection is afforded by the excellent passband characteristics of the mechanical filter. For simplicity, the mixing and filtering operation usually takes place at a frequency of 455 kilocycles. The single-sideband signal appearing at the output of the mechanical filter may be translated directly to a higher operating frequency. Suitable tuned circuits must follow the conversion stage to eliminate the signal from the conversion oscillator.

Wave Filters The heart of a filter-type SSB exciter is the sideband filter. Conventional coils and condensers may be used to construct a filter based upon standard wave filter techniques. The Q of the filter inductances must be high when compared with the reciprocal of the fractional bandwidth. If a bandwidth of 3 kc. is needed at a carrier frequency of 50 kc., the bandwidth expressed in terms of the carrier frequency is 3/50 or 6%. This is expressed in terms of fractional bandwidth as 1/16. For satisfactory operation, the Q of the filter inductances should be 10 times the reciprocal of this, or 160. Appropriate Q is generally obtained from toroidal inductances, though there is some possibility of using iron core solenoids between 10 kc. and 20 kc. A characteristic impedance below 1000 ohms should be selected to prevent distributed capacity of the inductances from spoiling overall performance. Paper capacitors intended for bypass work may not be trusted for stability or low loss and should not be used in filter circuits. Care should be taken that the levels of both accepted and rejected signals are low enough so that saturation of the filter inductances does not occur.

Crystal Filters The best known filter responses have been obtained with crystal filters. Types designed for program carrier service cut-off 80 db in less than 50 cycles. More than 80 crystals are used in this type of filter. The crystals are cut to con-



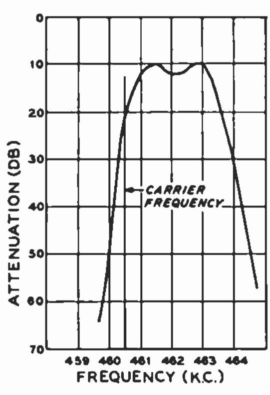


Figure 14

SIMPLE CRYSTAL LATTICE FILTER

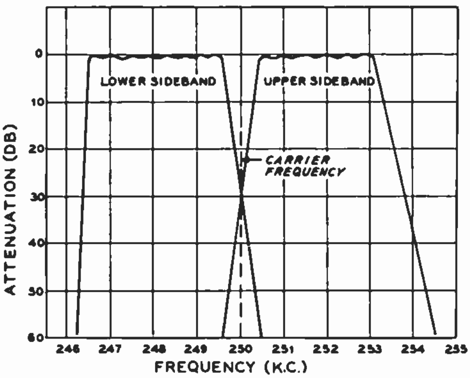


Figure 15
PASSBANDS OF LOWER AND UPPER SIDEBAND MECHANICAL FILTER

trol reactance and resistance as well as the resonant frequency. The circuits used are based on full lattices.

The war-surplus low frequency crystals may be adapted to this type of filter with some success. Experimental designs usually synthesize a selectivity curve by grouping sharp notches at the side of the passband. Where the width of the passband is greater than twice the spacing of the series and parallel resonance of the crystals, special circuit techniques must be used. A typical crystal filter using these surplus crystals, and its approximate passband is shown in figure 14.

Mechanical Filters Filters using mechanical resonators have been studied by a number of companies and are offered commercially by the *Collins Radio Co.* They are available in a variety of bandwidths at center frequencies of 250 kc. and 455 kc. The 250 kc. series is specifically intended for sideband selection. The selectivity attained by these filters is intermediate between good LC filters at low center frequencies and engineered quartz crystal filters. A passband of two 250 kc. filters is shown in figure 15. In application of the mechanical filters some special precautions are necessary. The driving and pick-up coils should be carefully resonated to the operating frequency. If circuit capacities are unknown, trimmer capacitors should be used across the coils. Maladjustment of these tuned coils will increase insertion loss and the peak-to-valley ratio. On high impedance filters (ten to twenty thousand ohms) signals greater than 2 volts at the input should be avoided. D.c. should be blocked out of the end coils. While the filters are rated for 5 ma. of coil current, they are not rated for d-c plate voltage.

The Phasing System There are a number of points of view from which the operation of the phasing system of SSB generation may be described. We may state that we generate two double-sideband suppressed carrier signals, each in its own balanced modulator, that both the r-f phase and the audio phase of the two signals differ by 90 degrees, and that the outputs of the two balanced modulators are added with the result

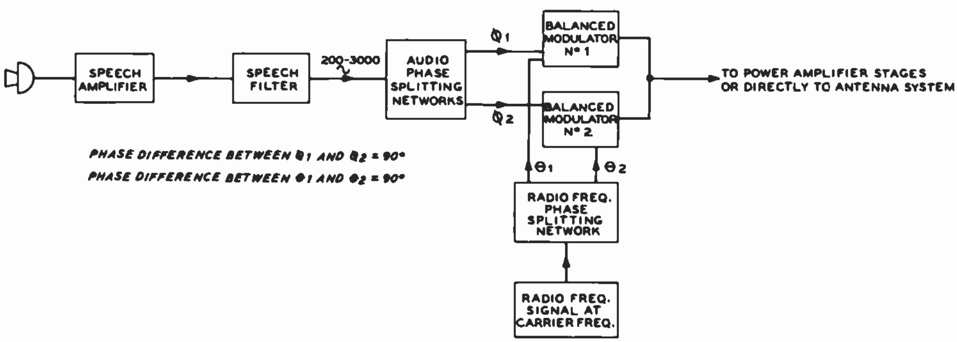


Figure 16
BLOCK DIAGRAM OF THE "PHASING" METHOD

The phasing method of obtaining a single-sideband signal is simpler than the filter system in regard to the number of tubes and circuits required. The system is also less expensive in regard to the components required, but is more critical in regard to adjustments for the transmission of a pure single-sideband signal.

that one sideband is increased in amplitude and the other one is cancelled. This, of course, is a true description of the action that takes place. But it is much easier to consider the phasing system as a method simply of adding (or of subtracting) the desired modulation frequency and the nominal carrier frequency. The carrier frequency of course is not transmitted, as is the case with all SSB transmissions, but only the sum or the difference of the modulation band from the nominal carrier is transmitted (figure 16).

The phasing system has the obvious advantage that all the electrical circuits which give rise to the single sideband can operate in a practical transmitter at the nominal output frequency of the transmitter. That is to say that if we desire to produce a single sideband whose nominal carrier frequency is 3.9 Mc., the balanced modulators are fed with a 3.9-Mc. signal and with the audio signal from the phase splitters. It is not necessary to go through several frequency conversions in order to obtain a sideband at the desired output frequency, as in the case with the filter method of sideband generation.

Assuming that we feed a speech signal to the balanced modulators along with the 3900-kc. carrier (3.9 Mc.) we will obtain in the output of the balanced modulators a signal which is either the sum of the carrier signal and the speech band, or the difference between the carrier and the speech band. Thus if our speech signal covers the band from 200 to 3000 cycles, we will obtain in the output a band of frequencies from 3900.2 to 3903 kc. (the sum of the two, or the "upper" sideband), or a band from 3897 to 3899.8 kc. (the difference between the two or the "lower" sideband). A further advantage of the phasing system of sideband generation is the fact that it is a very simple matter to select either the upper sideband or the lower sideband for transmission. A simple double-pole double-throw reversing switch in two of the four audio leads to the balanced modulators is all that is required.

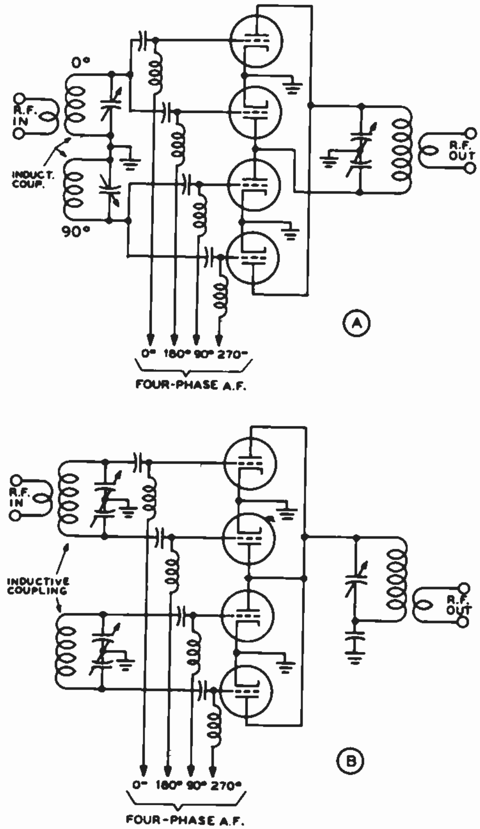


Figure 17

TWO CIRCUITS FOR SINGLE-SIDEBAND GENERATION BY THE PHASING METHOD

The circuit at (A) offers the advantages of simplicity in the single-ended input circuits plus a push-pull output circuit. Circuit (B) requires double-ended input circuits but allows all the plates to be connected in parallel for the output circuit.

High-Level Phasing Vs. Low-Level Phasing The plate-circuit efficiency of the four tubes usually used to make up the two balanced modulators of the phasing system may run as high as 50 to 70 per cent, depending upon the operating angle of plate current flow. Hence it is possible to operate the double balanced modulator directly into the antenna system as the output stage of the transmitter.

The alternative arrangement is to generate the SSB signal at a lower level and then to amplify this signal to the level desired by means of class A or class B r-f power amplifiers. If the SSB signal is generated at a level of a few milliwatts it is most common to make the first stage in the amplifier chain a class A amplifier, then to use one or more class B linear amplifiers to bring the output up to the desired level.

Balanced Modulator Circuits Illustrated in figure 2 are the two basic balanced modulator circuits which give good results with a radio frequency carrier and an audio modulating signal. Note that

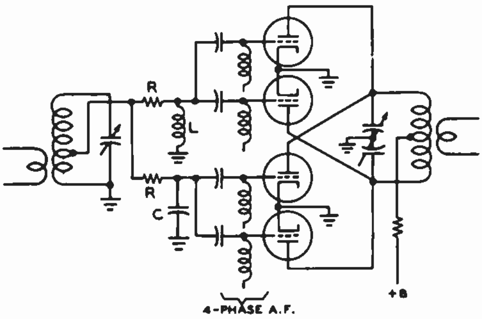


Figure 18

LOW-Q R-F PHASE-SHIFT NETWORK

The r-f phase-shift system illustrated above is convenient in a case where it is desired to make small changes in the operating frequency of the system without the necessity of being precise in the adjustment of two coupled circuits as used for r-f phase shift in the circuit of figure 17.

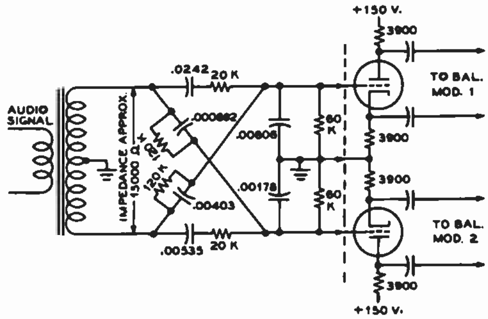


Figure 19

DOME AUDIO-PHASE-SHIFT NETWORK

This circuit arrangement is convenient for obtaining the audio phase shift when it is desired to use a minimum of circuit components and tube elements.

one push-pull and one single ended tank circuit is required, but that the push-pull circuit may be placed either in the plate or the grid circuit. Also, the audio modulating voltage always is fed into the stage in push-pull, and the tubes normally are operated Class A.

When combining two balanced modulators to make up a double balanced modulator as used in the generation of an SSB signal by the phasing system, only one plate circuit is required for the two balanced modulators. However, separate grid circuits are required since the grid circuits of the two balanced modulators operate at an r-f phase difference of 90 degrees. Shown in figure 17 are the two types of double balanced modulator circuits used for generation of an SSB signal. Note that the circuit of figure 17A is derived from the balanced modulator of figure 2A, and similarly figure 17B is derived from figure 2B.

Radio-Frequency Phasing A single-sideband generator of the phasing type requires that the two balanced modulators be fed with r-f signals having a 90-degree phase difference. This r-f phase difference may be obtained through the use of two loosely coupled resonant circuits, such as illustrated in figures 17A and 17B. The r-f signal is coupled directly or inductively to one of the tuned circuits, and the coupling between the two circuits is varied until, at resonance of both circuits, the r-f voltages developed across each circuit have the same amplitude and a 90-degree phase difference.

The 90-degree r-f phase difference also may be obtained through the use of a low-Q phase shifting network, such as illustrated in figure 18; or it may be obtained through the use of a lumped-constant quarter-wave line. The low-Q phase-shifting system has proved quite practicable for use in single-sideband systems, particularly on the lower frequencies. In such an arrangement the two resistances R have the same value, usually in the range between 100 and a few thousand ohms. Capacitor C, in shunt with the input capacitances of the tubes and circuit capacitances, has a reactance at the operating frequency equal to the value of the resistor R. Also, inductor L has a *net* inductive reactance equal in value at the operating frequency to resistance R.

The inductance chosen for use at L must take into account the cancelling effect of the input capacitance of the tubes and the circuit capacitance; hence the inductance should be variable and should have a *lower* value of inductance than that value of inductance which would have the same reactance as resistor R. Inductor L may be considered as being made up of two values of inductance in parallel; (a) a value of inductance which will resonate at the operating frequency with the circuit and tube capacitances, and (b) the value of inductance which is equal in reactance to the resistance R. In a network such as shown in figure 18, equal and opposite 45-degree phase shifts are provided by the RL and RC circuits, thus providing a 90-degree phase difference between the excitation voltages applied to the two balanced modulators.

Audio-Frequency Phasing The audio-frequency phase-shifting networks used in generating a single-side-

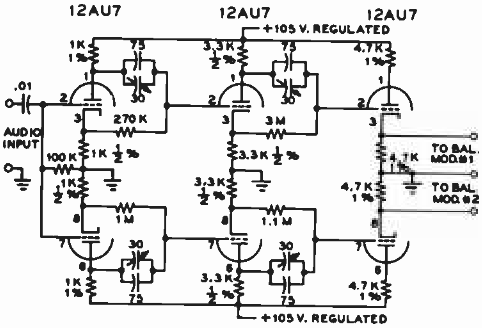


Figure 20
A VERSION OF THE DOME AUDIO-PHASE-SHIFT NETWORK

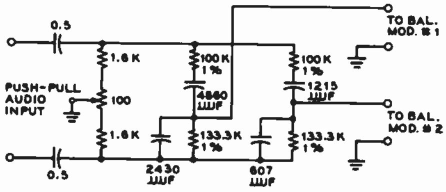


Figure 21
PASSIVE AUDIO-PHASE-SHIFT NETWORK, USEFUL OVER RANGE OF 300 TO 3000 CYCLES

band signal by the phasing method usually are based on those described by Dome in an article in the December, 1946, *Electronics*. A relatively simple network for accomplishing the 90-degree phase shift over the range from 160 to 3500 cycles is illustrated in figure 19. The values of resistance and capacitance must be carefully checked to insure minimum deviation from a 90-degree phase shift over the 200 to 3000 cycle range.

Another version of the Dome network is shown in figure 20. This network employs three 12AU7 tubes and provides balanced output for the two balanced modulators. As with the previous network, values of the resistances within the network must be held to very close tolerances. It is necessary to restrict the speech range to 300 to 3000 cycles with this network. Audio frequencies outside this range will not have the necessary phase-shift at the output of the network and will show up as spurious emissions on the sideband signal, and also in the region of the rejected sideband. A low-pass 3500 cycle speech filter, such as the *Chicago Transformer Co. LPF-2* should be used ahead of this phase-shift network.

A passive audio phase-shift network that employs no tubes is shown in figure 21. This network has the same type of operating restrictions as those described above. Additional information concerning phase-shift networks will be found in *Single Sideband Techniques* published by the Cowan Publishing Corp. of N.Y., and *The Single Sideband Digest* published by the American Radio Relay League.

Comparison of Filter and Phasing Methods of SSB Generation Either the filter or the phasing method of single-sideband generation is theoretically capable of a high degree of performance.

In general, it may be said that a high degree of unwanted signal rejection may be attained with less expense and circuit complexity with the filter method. The selective circuits for rejection of unwanted frequencies operate at a relatively low frequency, are designed for this one frequency and have a relatively high order of Q. Carrier rejection of the order of 50 db or so may be obtained with a relatively simple filter and a balanced modulator, and unwanted sideband rejection in the region of 60 db is economically possible.

The phasing method of SSB generation exchanges the problems of high-Q circuits and linear amplification for the problems of accurately controlled phase-shift networks. If the phasing method is employed on the actual transmitting frequency, change of frequency must be accompanied by a corresponding rebalance of the phasing networks. In addition, it is difficult to obtain a phase balance with ordinary equipment within 2% over a band of audio frequencies. This means that carrier suppression is limited to a maximum of 40 db or so. However, when a relatively simple SSB transmitter is needed for spot frequency operation, a phasing unit will perform in a satisfactory manner.

Where a high degree of performance in the SSB exciter is desired, the filter method and the phasing method may be combined. Through the use of the phasing method in the first balanced modulator those undesired sideband components lying within 1000 cycles of the carrier may be given a much higher degree of rejection than is attainable with the filter method alone, with any reasonable amount of complexity in the sideband filter. Then the sideband filter may be used in its normal way to attain very high attenuation of all undesired sideband components lying perhaps further than 500 cycles away from the carrier, and to restrict the sideband width on the *desired* side of the carrier to the specified frequency limit.

Requirement for Linearity In any type of single-sideband system there is a requirement for a high degree of linearity in the amplification and frequency conversion stages. This means that the low-level stages should be operated Class A, with the operating bias in the center of the dynamic characteristic. If this is not done, undesired cross-modulation products will be generated, and these undesired signals will be amplified along with the desired-signal output of the exciter unit. High level stages may be operated in the Class B region, but careful attention to establishing operating conditions which give good linearity is necessaty.

14-4 Reception of Single-Sideband Signals

Single-sideband signals may be received, after a certain degree of practice in the technique, in a quite adequate and satisfactory manner with a good communications receiver. However, the receiver must have quite good frequency stability both in the high-frequency oscillator and in the beat oscillator. For this reason, receivers which use a crystal-controlled first oscillator are likely to offer a greater degree of satisfaction than the more common type which uses a self-controlled oscillator.

Beat oscillator stability in most receivers is usually quite adequate, but many receivers do not have a sufficient amplitude of beat oscillator injection to allow reception of strong SSB signals without distortion. In such receivers it is necessary either to increase the amount of beat-oscillator injection into the diode detector, or the manual gain control of the receiver must be turned down quite low.

The tuning procedure for SSB signals is as follows: The SSB signals may first be located by tuning over the band with the receiver set for the reception of c.w.; that is, with the manual gain at a moderate level and with the beat oscillator operating. By tuning in this manner SSB signals may be *located* when they are far below the amplitude of conventional AM signals on the frequency band. Then after a signal has been located, the beat oscillator should be turned off and the receiver put on a.v.c. Following this the receiver should be tuned for maximum swing of the S meter with modulation of the SSB signal. It will not be possible to understand the SSB signal at this time, but the receiver may be tuned for maximum deflection. Then the receiver is put back on manual gain control, the beat oscillator is turned on again, the manual gain is turned down until the background noise level is quite low, and the *beat oscillator* control is varied until the signal sounds natural.

The procedure in the preceding paragraph may sound involved, but actually all the steps except the last one can be done in a moment. However, the last step is the one which will require some practice. In the first place, it is not known in advance whether the upper or lower sideband is being transmitted. So it will be best to start tuning the beat oscillator from one side of the pass band of the receiver to the other, rather than starting with the beat oscillator near the center of the pass band as is normal for c-w reception.

With the beat oscillator on the wrong side of the sideband, the speech will sound inverted; that is to say that low-frequency modulation tones will have a high pitch and high-frequency modulation tones will have a low pitch—and the speech will be quite unintelligible. With the beat oscillator on the correct side of the sideband but too far from the correct position, the speech will have some intelligibility but the voice will sound quite high pitched. Then as the correct setting for the beat oscillator is approached the voice will begin to sound natural but will have a background growl on each syllable. At the correct frequency for the beat oscillator the speech will clear completely and the voice will have a clean, crisp quality. It should also be mentioned that there is a narrow region of tuning of the beat oscillator a small distance on the wrong side of the sideband where the voice will sound quite bassy and difficult to understand.

With a little experience it will be possible to identify the sound associated with improper settings of the beat-oscillator control so that corrections in the setting of the control can be made. Note that the main tuning control of the receiver is not changed after the sideband once is tuned into the pass band of the receiver. All the fine tuning should be done with the beat oscillator control. Also, it is very important that the r-f gain control be turned to quite a low level during the tuning process. Then after the signal has been tuned properly the r-f gain may be increased for good signal level, or until the point is reached where best oscillator injection becomes insufficient and the signal begins to distort.

Single-Sideband Receivers and Adapters Greatly simplified tuning, coupled with strong attenuation of undesired signals, can be obtained through the use of a single-sideband receiver or receiver adapter. The exalted carrier principle usually is employed in such receivers, with a phase-sensitive system sometimes included for locking the local oscillator to the frequency of the carrier of the incoming signal. In order for the

Table I—Ratings and Operating Conditions for RCA Tubes Used as Linear RF Power Amplifiers

Maximum Ratings - Absolute Values										Typical Operation								
Tube Type	Class of Operation	Service	Plate Voltage (E_b)	Screen Voltage (E_{c2})	Max-Signal Plate Current (I_{bmo})—ma	Max-Signal Plate Input (PI)—watts	Max-Signal Screen Input (SI)—watts	Plate Dissipation (PD)—watts	Grid Resistance —ohms	Plate Voltage (E_b)	Screen Voltage (E_{c2})	Grid Voltage (E_{c1})	Peak Grid Voltage (E'_g)	Zero-Signal Plate Current (I_{bo})—ma	Max-Signal Plate Current (I_{bmo})—ma	Max-Signal Screen Current (I_{c2})—ma	Drive Power (DP) —watts	Max-Signal Power Output (PO)—watts
2E26	AB_1	CCS	400	200	75	30	2.5	10	30 K	400	200	-25	25	9	45	10		12
		ICAS	500	200	75	37.5	2.5	12.5	30 K	500	200	-25	25	9	45	10		15
	AB_2	CCS	400	200	75	30	2.5	10		400	125	-15	30	10	75	16	0.2	20
		ICAS	500	200	75	37.5	2.5	12.5		500	125	-15	30	11	75	16	0.2	25
4-65A	AB_1	CCS	3000	600	150		10	65	250 K	1000	500	-85	85	15	85	12		40
										1500	500	-85	85	15	90	7		70
										1750	500	-90	90	10	85	9		85
	AB_2	CCS	3000	600	150		10	65		1000	250	-30	105	30	150	22	2.5	85
										1500	250	-35	100	30	125	15	1.5	125
										1800	250	-35	90	25	110	13	1.0	135
4-125A	AB_1	CCS	3000	600	225		20	125	250 K	1500	600	-90	90	30	110	9		80
										2000	600	-94	94	25	120	3		115
										2500	600	-96	96	25	115	4		165
	AB_2	CCS	3000	400	225		20	125		1500	350	-41	141	44	200	17	5.0	175
										2000	350	-45	105	36	150	3	3.0	175
										2500	350	-43	138	47	130	3	2.5	200
4-250A	AB_1	CCS	4000	600	350		35	250		2000	500	-88	88	55	200	11		230
										2500	500	-90	90	60	215	7		310
										3000	500	-93	93	60	205	5		370
	AB_2	CCS	4000	600	350		35	250		2000	300	-48	100	60	255	13	5.5	325
										2500	300	-51	100	60	250	12	5.0	420
										3000	300	-53	100	62	236	16	4.5	520
807 1625	AB_1	CCS	600	300	120	60	3.5	25	100 K	500	300	-32	32	22	70	8		23
		ICAS	750	300	120	90	3.5	30	100 K	600	300	-34	34	18	70	8		28
										750	300	-35	35	15	70	8		35
	AB_2	CCS	600	300	120	60	3.5	25		500	300	-30	43	30	120	10	0.2	38
										600	300	-32	40	24	100	9	0.1	40
		ICAS	750	300	120	90	3.5	30		750	300	-35	48	15	120	10	0.2	80
811A	B	CCS	1250		175	165		45		750		0	100	16	175		10	90
										1250		0	78	25	130		4	120
		ICAS	1500		175	235		65		1000		0	93	22	175		7.5	125
										1250		0	88	27	175		6	155
813	AB_1	CCS	2250	1100	180	360	22	100		2000	750	-90	80	25	130	20		165
										2250	750	-95	85	25	125	28		190
		ICAS	2500	1100	225	450	22	125		2500	750	-95	90	25	145	27		245
6290 Natural Cooling	AB_1	CCS	750	225	250	100	7	30	100 K	500	200	-20	40	20	100	20		36
										600	200	-18	36	40	100	18		44
		ICAS	750	225	250	120	7	40	100 K	750	200	-21	42	20	100	20		56
	AB_2	CCS	750	225	250	100	7	30		500	200	-18	50	30	180	26	0.6	60
										600	200	-20	50	28	155	22	0.4	65
		ICAS	750	225	250	120	7	40		750	200	-19	50	32	180	25	0.5	85
832A	AB_1									500	180	-30	80	14	70	7		22
		CCS	750	250	90	36	5	15	100 K	600	150	-30	60	12	60	7		23
		ICAS	750	250	115	50	5	20	100 K	750	150	-32	64	12	60	7		30
833A	B	ICAS	3300		500	1300		350		3300		-80	190	60	300		20	710
6146 6150	AB_1	CCS	600	250	125	60	3	20	100 K	400	190	-40	40	32	114	13		27
										500	185	-40	40	29	108	13		35
										600	180	-45	45	13	100	12		40
		ICAS	750	250	135	85	3	25	100 K	600	200	-50	50	14	115	14		47
										750	195	-50	50	12	110	13		60
	AB_2									400	175	-41	48	17	116	9	0.2	31
		CCS	600	250	125	60	3	20		500	175	-44	51	14	121	9	0.3	41
										600	165	-44	49	11	104	9	0.2	45
		ICAS	750	250	135	85	3	25		600	190	-48	55	14	135	10	0.3	56
										750	165	-46	54	11	120	10	0.4	65
6524	AB_2	CCS	500	300	150	70	3	20	30 K	400	200	-23	72	25	145	10	0.1	39
										500	200	-26	70	20	116	10	0.1	40
		ICAS	600	300	150	85	3	20	30 K	500	200	-25	76	25	145	10	0.1	50
										600	200	-26	76	21	135	13	0.1	57

Courtesy of RCA and A. P. Sweet

Figure 22

locking system to operate, some carrier must be transmitted along with the SSB signal. Such receivers and adapters include a means for selecting the upper or lower sideband by the simple operation of a switch. For the reception of a single-sideband signal the switch obviously must be placed in the correct position. But for the reception of a conventional AM or phase-modulated signal, either sideband may be selected, allowing the sideband with the least interference to be used.

14-5 Adjustment of Class B Linear Amplifiers

The establishment of operating conditions and the adjustment of a Class B linear amplifier, or any type of efficiency-modulated amplifier, are somewhat more critical than for a similar Class C amplifier for one basic reason: the linear amplifier or efficiency-modulated amplifier must be linear as an *amplifier* with respect to the parameter which is to be varied to effect modulation. Hence, the operating value of bias, the amount of excitation, and the plate circuit loading must be approximately at the correct values before linear amplification or modulation may be attained. A Class C modulated amplifier must be linear only with respect to plate-voltage variation.

Establishing Operating Conditions Satisfactory operating conditions for use of many tube types as Class B linear amplifiers are included in the recommended operating conditions published by tube manufacturers.

Figure 22 (Table 1) shows the maximum ratings and typical operating conditions for many of the transmitting tubes commonly used in SSB linear work.

Basically, a Class B linear amplifier is operated at a grid-bias voltage such that with excitation removed the plate dissipation of the tube will be perhaps 10 to 20 per cent of the rated dissipation of the tube. Loading of the tube will be approximately twice as heavy as with the same tube operating as a Class C amplifier. This means that the effective load impedance which the tube sees will be about one-half the value which would be used if the tube were to operate as a Class C amplifier. Hence, in order that the loaded Q of the tank circuit in the plate circuit of the tube shall be 15 or higher, approximately *twice* as much tuning capacitance for a specified operating frequency will be required—as compared to the same tube with the same carrier input operating as a Class C amplifier.

An approximation to the correct value of load impedance for a single-sideband Class B linear amplifier may be determined as follows: (1) Assume a peak power output value for the tube. This value will be determined by the operating conditions chosen, and usually will lie between three and five times the rated plate dissipation of the tube, assuming that the tube will be operated at a relatively high plate voltage and that the maximum capabilities of the tube are to be used. (2) Assume a peak value of plate voltage swing at maximum output from the stage. This value will normally be about 0.9 times the operating voltage on the stage. (3) Determine the approximate R_L for the tube from:

$$R_L = (0.9\ E_{bb})^2 / 2\ W_{o\ pk}$$

The above is only an approximation, but it is of sufficient accuracy to be of value in establishing the correct value of tank circuit capacitance for a specified nominal value of circuit loaded Q. The reactance required in the tank capacitor or the tank coil at the operating frequency then is equal to: R_L/Q_L, where Q_L is the value of loaded Q desired in the tank circuit.

Adjustment of the Linear Amplifier An oscilloscope is practically a necessity in adjusting a Class B linear amplifier, or other type of efficiency-modulated amplifier, for proper operating conditions. The output signal from the amplifier to be adjusted is coupled to the vertical deflection plates of of the oscilloscope. Then the horizontal sweep oscillator on the oscilloscope is adjusted to a frequency which is appropriate for the audio modulation frequency which will be used to adjust the amplifier.

The adjustment of a linear amplifier of a single-sideband signal may be done in several ways. One satisfactory way, when the linear amplifier is to be operated relatively conservatively, is to insert a carrier signal in the single-sideband exciter of approximately one-half the peak output voltage capability of the exciter. Then an audio modulating tone of about 400 cycles is applied to the SSB exciter, and the excitation and loading adjustments to the linear amplifier are made.

Another method of adjustment of a linear amplifier for single-sideband signals is to apply two tones to the exciter, say 1000 cycles and 600 cycles, so that the difference frequency will be about 400 cycles. Then loading, excitation, and bias to the linear amplifier are adjusted until the waveform output of the exciter is undistorted in passing through the linear amplifier. The envelope of the amplified SSB signal should appear as in figure 23.

Due to the large signal excursions encountered in a Class B linear amplifier of single-sideband signals, it is important that the bias voltage and plate voltage have good regulation, and in the case of a tetrode amplifier the screen voltage must have extremely good regulation. Also, to obtain best linearity when using tetrode tubes as SSB linear amplifiers, it has been found best to operate with a grid bias somewhat less than that which would be used for straight Class B operation. The tube manual values specified for Class AB_1 or Class

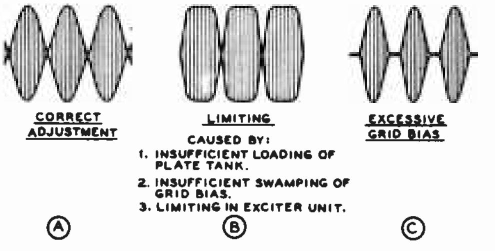


Figure 23

SSB LINEAR-AMPLIFIER OUTPUT WAVEFORMS

With improper adjustment the output envelope from a SSB linear amplifier appears similar to the analogous conditions obtained with a conventional AM linear amplifier. But when operating conditions are correct, with a two-tone modulating signal or with carrier and one sideband of full amplitude, the envelope has the appearance shown at (A) above.

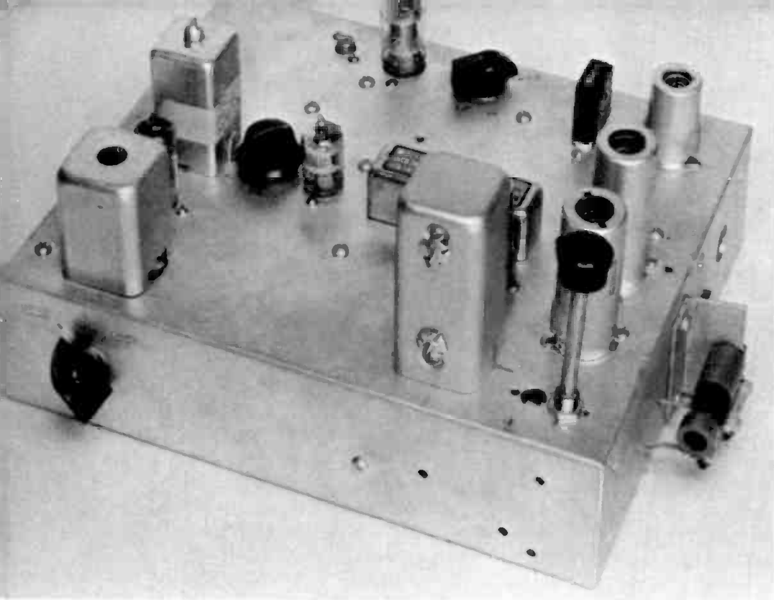


Figure 24

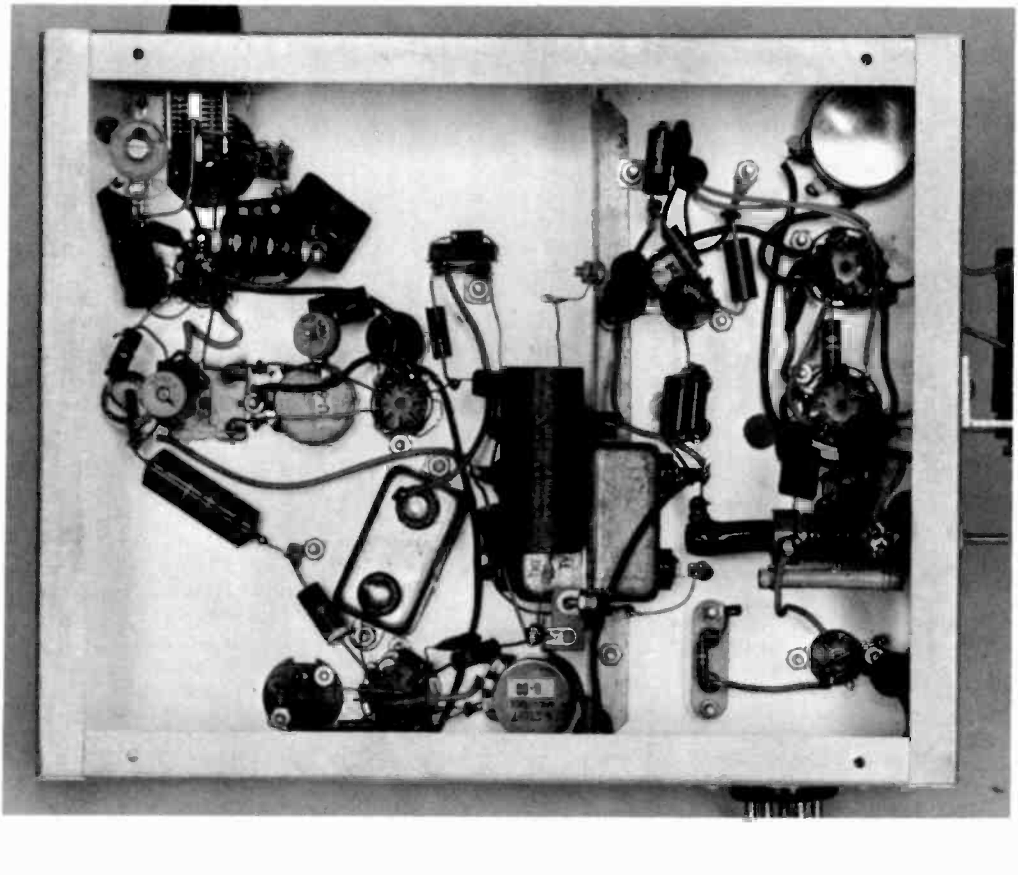
80-METER SINGLE-SIDEBAND EXCITER

Sideband selector control is at the left front. The mechanical filter may be seen behind the 455-kc. transformer. The modulator balance control is to the left of the 6AL5 series modulator tube. Audio gain control is at rear of the chassis. The 80-meter output tank is on the right of the chassis, with the two 6CL6 mixer tubes directly above it.

Figure 25

UNDERCHASSIS LAYOUT OF 80-METER SSB EXCITER

The shield partition dividing the low frequency and high frequency sections of the exciter passes across the mounting sockets of the mechanical filter. The sideband selector control is at upper left. The balancing potentiometer in the 6CL6 cathode circuit (upper right) was later removed and is not shown in the schematic.



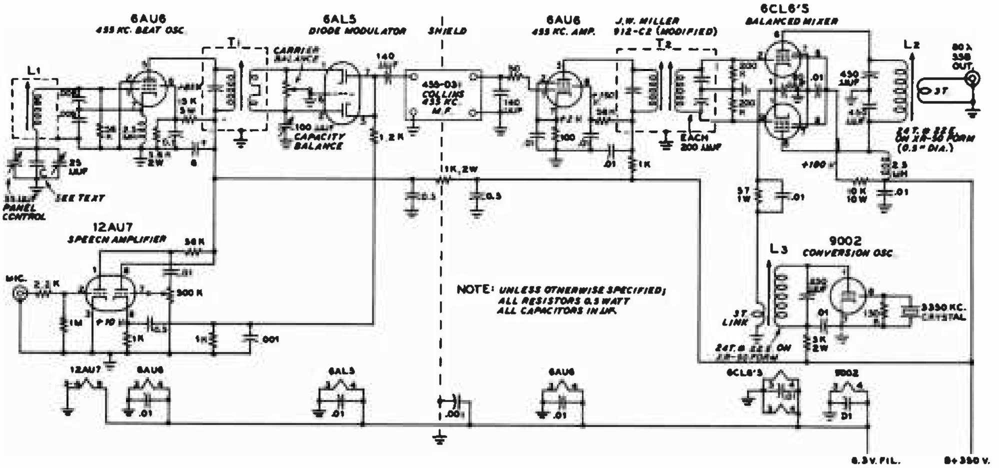


Figure 26
SCHEMATIC SSB FILTER EXCITER USING COLLINS 455-KC. MECHANICAL FILTER

AB_2 operation as an *audio* amplifier have proven most satisfactory for linear operation of tetrode tubes as single-sideband amplifiers.

14-6 A Simple Filter-Exciter for 80 Meters

A simple single-sideband filter-type exciter employing the Collins mechanical filter illustrates many of the basic principles of SSB generation. Such an exciter is shown in figures 24, 25 and 26. This exciter is designed for operation in the 80 meter phone band, and delivers sufficient output to drive a Class AB_1 tetrode such as the 2E26, 807 or 6146. At reduced output it may be used to drive a 6AG7 or 6CL6. This exciter is a basic unit, and such features as voice control and 80 meter VFO may be readily added to it. Its main purpose is to illustrate how simply a high-quality SSB exciter may be built with a minimum of tubes. The only piece of test equipment needed to align the exciter is a communications receiver equipped with an "S" meter.

The filter-exciter employs 7 tubes, exclusive of power supply. They are: 12AU7 speech amplifier and cathode follower, 6AU6 low frequency oscillator, 6AL5 balanced modulator, 6AU6 amplifier, two 6CL6 balanced mixers to 80 meters, and a 9002 80 meter conversion crystal oscillator. The heart of the exciter is the 6AL5 series balanced modulator and the 455 kc. mechanical filter. The input circuit of the mechanical filter is series resonated by a 140 $\mu\mu$fd. capacitor to 455 kc., providing a low impedance termination for the balanced modulator. A 6AU6 is employed as a beating oscillator to convert the voice frequencies to the 455 kc. region. For maximum frequency stability, a Clapp oscillator circuit is used. Transformer T_1 provides a source of low impedance r.f. for the 6AL5 modulator, and a 1000 ohm potentiometer is placed across the secondary winding of T_1 to balance out the 455 kc. carrier from the conversion oscillator. A small variable ceramic capacitor is employed to provide capacity balance in the circuit.

One half of a 12AU7 is used as a speech amplifier delivering sufficient output from a high level crystal microphone to drive the secone half of the tube as a low impedance cathode follower, which is coupled to the series balanced modulator. The 6AL5 acts as an electronic switch, impressing a double sideband suppressed carrier signal upon the mechanical filter. By the proper choice of frequency of the beating oscillator, the unwanted sideband may be made to fall outside the passband of the mechanical filter. Thus a single sideband suppressed carrier signal appears at the output of the mechanical filter. This 455 kc. SSB signal is amplified by a 6AU6 pentode amplifier stage and then converted to a frequency in the 80 meter band by a balanced mixer stage employing two 6CL6 tubes. The SSB signal is fed into the mixer tubes in

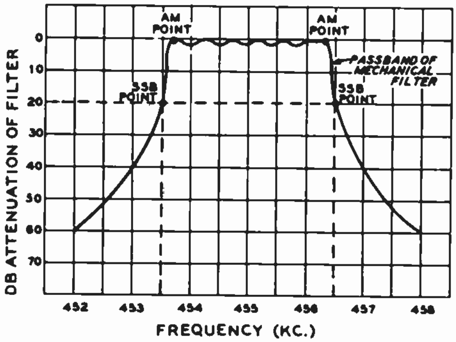


Figure 27

THE "TWENTY DB" CARRIER POINTS ON THE FILTER CURVE

The beating oscillator should be adjusted so that its frequency corresponds to the 20 db attenuation points of the mechanical filter passband. The carrier of the SSB signal is thus attenuated 20 db in addition to the inherent carrier attenuation of the balanced mixer. A total carrier attenuation of 50 db is achieved. Unwanted sideband rejection is of the same order.

push-pull, and the second beating oscillator signal is inductively coupled into the parallel cathode circuit of the converter tubes. The plate circuit of the 6CL6 tubes is a push-pull configuration and the beating oscillator signal injected into the mixer in a parallel connection is attenuated some 30 db in the push-pull output circuit of the mixer stage. A 9002 triode is used as the 80 meter beating oscillator, operating 455 kc. either above or below the desired output frequency. In this case, the transmitter was placed on a frequency of 3805 kc. and a conversion crystal of 3350 kc. was used.

The 80 meter tank circuit of the exciter, L_2, is link coupled to an output jack. The low impedance output (about 0.3 watt) may be coupled via coaxial line to the grid circuit of a medium power tetrode. A maximum of 100 volts peak-to-peak SSB signal will be developed across a high-Q grid circuit following the exciter. This is sufficient to drive a pair of 807 or 6146 tubes in Class AB_1, where a minimum of grid swamping is required.

Selection of the upper or lower sideband is accomplished by tuning the 6AU6 beating oscillator across the passband of the mechanical filter, as shown in figure 27. If the 80 meter conversion oscillator is on the low frequency side of the SSB signal, placing the 6AU6 beating oscillator on the low frequency side of the passband of the mechanical filter will produce the upper sideband on 80 meters. When the beating oscillator is placed on the high frequency side of the passband of the mechanical filter the lower sideband will be generated on 80 meters. If the 80 meter conversion oscillator is placed on the high frequency side of the SSB signal, the sidebands will be reversed from the above. The variable oscillator should be set at approximately the 20 db suppression point of the passband of the mechanical filter for best operation, as shown in figure 27. If the oscillator is closer in frequency to the filter passband than this, carrier rejection will suffer. If the oscillator is moved farther away in frequency from the passband, the lower voice frequencies will be attenuated, and the SSB signal will sound high-pitched and tinny. A little practice in setting the frequency of the beating oscillator while monitoring the 80 meter SSB signal in the station receiver will quickly acquaint the operator with the proper frequency setting of the beating oscillator control for transmission of either sideband.

If desired, an amplitude modulated signal with full carrier and one sideband may be transmitted by placing the 6AU6 low frequency oscillator just inside either edge of the passband of the filter (designated "AM point", figure 27).

Mechanical Layout The SSB exciter is built upon an 8"x 10"x 3" aluminum chassis. Since the rejection of the mechanical filter to unwanted frequencies is of the order of 70 db or so, it is important that there be no path by which low frequency signals can pass around the mechanical filter. It is necessary to place a three inch high shield across the underside of the chassis from front to back to isolate the input and output circuits of the filter. Only two leads pass through this partition: the filament lead to the 12AU7, 6AU6 and 6AL5 tubes and the high voltage lead for these tubes. The filament lead passes through a bulkhead type .001 $\mu\mu$fd. capacitor mounted on the shield, and the high voltage lead is filtered by a 1000 ohm resistor mounted through a hole in the shield, and bypassed on each side of the partition by a 0.5 μfd. capacitor.

The 455 kc. oscillator coil is mounted to the left front of the chassis with the 35 $\mu\mu$fd. sideband selector capacitor directly beneath it on the front edge of the chassis. Behind the oscillator coil can is the 6AU6 oscillator tube, and behind the 6AU6 is the oscillator transformer, T_1. Between T_1 and the mechanical filter are the 1000 ohm balancing control and the 6AL5 diode modulator tube. To the rear of the chassis in the low frequency compartment is the 12AU7 speech amplifier tube.

To the right of the mechanical filter is the 6AU6 amplifier stage, with the 455 kc. transformer (T_2) mounted at the front of the chassis. Along the right edge of the chassis are the 9002 conversion oscillator and the two 6CL6 converter tubes. The push-pull tank circuit for the 6CL6 tubes is mounted on the right outboard edge of the chassis. This is admittedly a poor arrangement, and if a 12" chassis was used, the output tank circuit could be placed above the chassis to the right of the 6CL6 tubes. Such a change is recommended if this unit is duplicated. On the rear lip of the chassis is placed a five prong power plug.

The Circuit Wiring No special finesse is required to wire and test the circuit. The filament wiring should be done first, using a .01 μfd. ceramic condenser at the ungrounded filament pin of each tube. This is mandatory, since both the 6AU6 low frequency oscillator and the 6AL5 diode modulator have "hot cathode" circuits, and a considerable amount of 455 kc. signal would be coupled into the filament line if this precaution was not observed.

The 455 kc. oscillator coil, L_1 is a 455 kc. permeability tuned BFO coil, such as the *J.W. Miller 912-C5*. The shunt capacitor used to tune the BFO coil is removed from the can and is used to series tune the coil in the Clapp circuit, and is shown as C in figure 26. A small 25 μμfd. ceramic padding capacitor is employed to set the range of the tuned circuit. Two .006 silver mica capacitors are used as the series capacitors in the grid-cathode circuit of the Clapp oscillator. The oscillator transformer, T_1, is made from a permeability tuned 455 kc. i-f transformer, such as the *J.W. Miller 612-C2*. This transformer is modified by removing the secondary winding and the secondary padding capacitor. 80 turns of no. 22 d-c-c wire are then wound on the transformer form as a new secondary winding. This winding is split into two coils of forty turns each. These coils are jumble wound, one on each side of the primary winding. The coils should be wound tightly against the primary winding. When completed, the new winding should be given a coat of nail polish or Duco cement to hold it in place. As a last step, the secondary tuning slug of the transformer should be removed.

The particular Mechanical Filter used in this exciter is the F455-D31, requiring capacitors of 140 μμfd. resonating both the input and output circuits.

The 12AU7 speech amplifier and cathode follower is conventional, and all parts may be mounted either on the socket or in close proximity to it.

Care should be taken in wiring the 6AU6 amplifier stage to prevent any unwanted regeneration. The 140 μμfd. resonating capacitor should be mounted between the terminals of the mechanical filter, and a short, direct lead run from the filter to pin no. 1 of the 6AU6. The .01 μfd. screen bypass capacitor should be mounted from pin no. 6 to pin no. 3 (ground) of the socket to act as a shield between the input and output pins of the socket. The lead from plate pin no. 5 to the i-f transformer should be short and direct and lie close against the chassis. Transformer T_2 is a slug-tuned 455 kc. interstage transformer, such as the *J.W. Miller 912-C2*. The secondary winding of this transformer is normally tuned by a 100 μμfd. capacitor. This is removed, and two 200 μμfd. capacitors are placed in series across the secondary winding. The junction of the two capacitors is grounded. This modification provides a balanced output from the transformer to feed out-of-phase signals to each 6CL6 converter tube.

Oscillator coil L_3 and its associated tuning capacitor are mounted on the side wall of the chassis between the 9002 tube socket and the nearest 6CL6 socket. The power plug is directly behind the 9002 tube socket. The plate circuit for the 6CL6 tubes is mounted on the side wall of the chassis, in close proximity to the 6CL6 sockets.

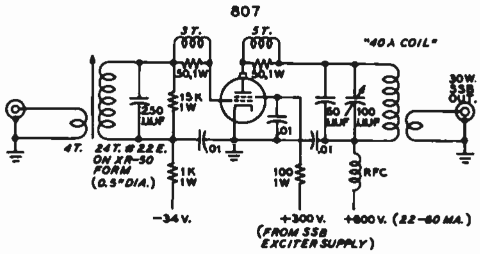
Testing and Aligning the Exciter The first step is to test the 6AU6 low frequency oscillator. All tubes except the 6AU6 should be removed from the exciter. Power should be applied to the exciter, and a wire should be run from the proximity of the plate pin (no. 5) of the 6AU6 to the 455 kc. amplifier of the auxiliary communications receiver. If the oscillator is operating, it should be possible to hear it in the receiver as the slug of L_1 is adjusted. If the oscillator cannot be heard, capacitor C may have to be adjusted slightly to bring the oscillator to the correct frequency. The panel control of the beating oscillator should vary the frequency from 450 kc. to 460 kc. The oscillator frequency may be checked on a BC-221 frequency meter if one is available. If trouble is encountered getting the oscillator to start the series Clapp capacitors may be reduced in value from .006 μμfd. to .003 μμfd. This will raise the impedance of the grid circuit and generally cure the trouble. After the oscillator is working the 6AL5 diode modulator should be plugged in its socket. With the balance potentiometer set at mid-scale and the oscillator tuned to the center of the filter passband a voltage of at least 4 volts RMS to ground should be read from each side of the potentiometer to ground with a vacuum-tube voltmeter.

This check is not necessary unless trouble is had with the oscillator circuit. The amount of r-f voltage across the balancing control may be varied by altering the value of the 5,600 ohm screen bleeder resistor of the 6AU6 tube.

The output terminals of the mechanical filter should now be coupled to the first i-f stage of the communications receiver by a short length of wire. It should be possible to tune the beating oscillator capacitor across the passband of the filter and obtain a reading on the S-meter of the receiver. The 1000 ohm balancing control and the 100 $\mu\mu$fd. balancing capacitor should be adjusted for a null reading of the S-meter when the oscillator is set in the middle of the filter passband. The slug of T_1 should be adjusted for ***maximum*** S-meter reading. If a null cannot be obtained, check to make sure the balancing capacitor is connected to pin no. 2 of the 6AL5 tube, since the capacitor balances the cathode-ground capacity of pin no. 1. It should be possible to obtain a very sharp null with the balancing potentiometer set near center position. Adjust the capacitor to enhance this null. When this has been done, the setting of the potentiometer should be marked, and the lead coupling the mechanical filter to the receiver should be removed.

The 6AU6 amplifier tube should next be plugged into its socket. A shielded lead from the i-f circuit of the communications receiver is temporarily brought near pin no. 2 of one 6CL6 and the slugs of T_2 adjusted for maximum S-meter reading of the receiver. Be careful not to overload the receiver. It may be necessary to temporarily unbalance the 1000 ohm potentiometer across the secondary winding of T_1 to obtain a test signal of sufficient amplitude for the alignment of T_2. When T_2 is aligned properly, rebalance the 1000 ohm carrier balance control for minimum carrier. Listen carefully to the received signal during this process and make sure that no trace of oscillation exists in the 6AU6 stage. Any spurious signal emanating from this stage is a sign of oscillation. This trouble should not show up if the grid and plate leads to the 6AU6 are short, and dressed closely against the chassis.

The 9002 conversion oscillator tube and the conversion crystal should be plugged into their respective sockets, and the slug of L_1 adjusted for oscillation. The conversion oscillator may be monitored by the communications receiver. Approximately 40 volts of r.f. should be measured by a VTVM at the plate end of L_1. The SSB signal at the plate of the 6AU6 amplifier should be about 18 volts, and about 4 volts of r.f. should be measured on each pin no. 2 of each 6CL6 tube socket.



NOTE: *ADJUST LINK COUPLING FOR 25 V. RMS MAXIMUM SSB SIGNAL AT GRID OF 807.*

Figure 28

30-WATT LINEAR AMPLIFIER FOR SSB EXCITER

The 6CL6 tubes should be placed in their sockets and the receiver should be tuned to the 80 meter SSB frequency and loosely coupled to L_2 by a short loop of wire. L_2 should be peaked for maximum S-meter reading, and the cathode coil of the mixer adjusted in relation to L_1 for maximum output at L_2. Fairly tight coupling is required between L_1 and the cathode link. The 6AL5 balancing potentiometer should now be reset for minimum S-meter reading.

When these adjustments have been completed, the 455 kc. beating oscillator should be moved just out of the passband of the mechanical filter and the 80 meter signal should disappear. If it does not, there is either signal leakage around the filter by some means, or the 6AU6 stage is oscillating. Careful attention to shielding in either case will cure the trouble.

If a frequency meter is available the correct frequency setting of the sideband control of the beating oscillator may be ascertained from the chart of figure 27. If no frequency meter is at hand the beating oscillator should be set so that its signal provides a weak carrier of about S-3 on 80 meters when the SSB signal is well over S-9. The 12AU7 speech amplifier tube should now be inserted in the socket and a microphone connected to the exciter. When modulation is applied to the exciter, the S-meter of the receiver should kick up with speech, but the audio output of the receiver should be unintelligible. As the sideband control of the beating oscillator is adjusted so as to bring the oscillator frequency within the passband of the mechanical filter, the modulation should become intelligible. A single sideband AM signal is now being transmitted. The BFO of the receiver should now be turned on and the sideband oscillator moved out of the filter passband. When the receiver is cor-

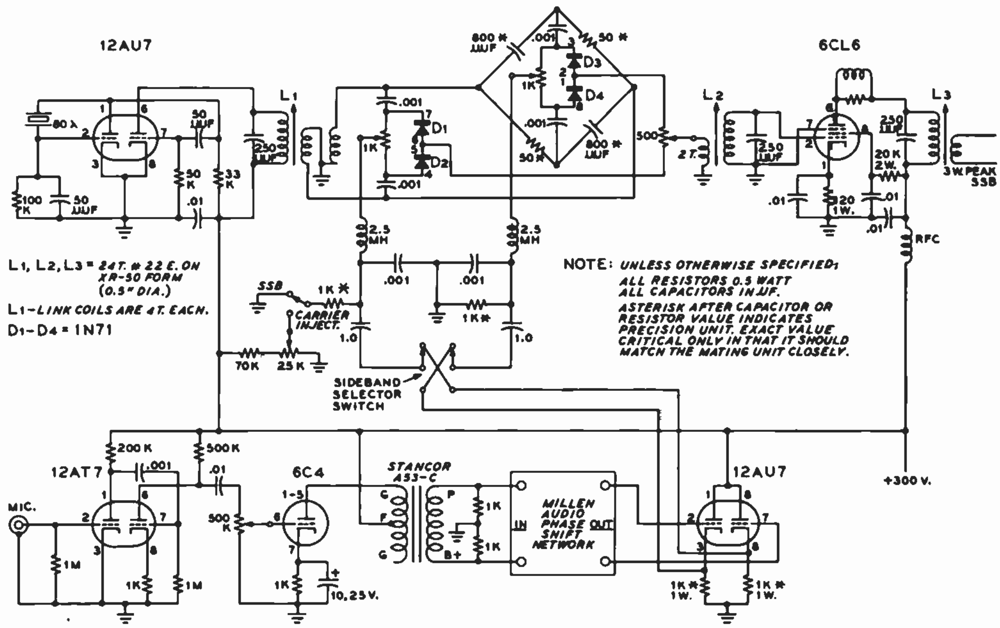


Figure 29

SIMPLE 3-WATT PHASING TYPE SSB EXCITER

rectly adjusted by the process explained earlier in this chapter, clean, crisp speech should be heard.

After the operator becomes familiar with the exciter, alignment should only take a matter of a few minutes. The exciter may be monitored in a nearby receiver if care is taken not to overload the receiver. A suitable linear amplifier capable of 30 watts peak output when driven by this exciter is shown in figure 28.

14-7 A Simple Phasing Exciter for 80 Meters

A SSB exciter employing r-f and audio phasing circuits is shown in figure 29. Since the r-f phasing circuits are balanced only at one frequency of operation, the phasing exciter is necessarily a single frequency transmitter unless provisions are made to re-balance the phasing circuits every time a frequency shift is made. However for mobile operation, or spot frequency operation a relatively simple phasing exciter may be made to perform in a satisfactory manner.

A 12AU7 is employed as a Pierce crystal oscillator, operating directly on the chosen SSB frequency in the 80 meter band. The second section of this tube is used as an isolation stage, with a tuned plate circuit, L_1. The output of the oscillator stage is link coupled to a 90° r-f phase-shift network wherein the audio signal from the audio phasing network is combined with the r-f signals. Carrier balance is accomplished by adjustment of the two 1000 ohm potentiometers in the r-f phase network. The output of the r-f phasing network is coupled through L_2 to a single 6CL6 linear amplifier which delivers a 3 watt peak SSB signal on 80 meters.

A cascade 12AT7 and a single 6C4 comprise the speech amplifier used to drive the audio phase shift network. A small inter-stage transformer is used to provide the necessary 180° audio phase shift required by the network. The output of the audio phasing network is coupled to a 12AU7 dual cathode follower which provides the necessary low impedance circuit to match the r-f phasing network. A double-pole double-throw switch in the output circuit of the cathode follower permits sideband selection.

A transmitter employing this circuit is shown in the Mobile Section of this Handbook.

CHAPTER FIFTEEN

Transmitter Design

The excellence of a transmitter is a function of the design, and is dependent upon the execution of the design and the proper choice of components. This chapter deals with the study of transmitter circuitry and of the basic components that go to make up this circuitry. Modern components are far from faultless. Resistors have inductance and distributed capacity. Capacitors have inductance and resistance, and inductors have resistance and distributed capacity. None of these residual attributes show up on circuit diagrams, yet they are as much responsible for the success or failure of the transmitter as are the necessary and vital bits of resistance, capacitance and inductance. Because of these unwanted attributes, the job of translating a circuit on paper into a working piece of equipment often becomes an impossible task to those individuals who disregard such important trivia. Rarely do circuit diagrams show such pitfalls as ground loops and residual inductive coupling between stages. Parasitic resonant circuits are rarely visible from a study of the schematic. Too many times radio equipment is rushed into service before it has been entirely checked. The immediate and only too apparent results of this enthusiasm are transmitter instability, difficulty of neutralization, r.f. wandering all over the equipment, and a general "touchiness" of adjustment. Hand in glove with these problems go the more serious ones of TVI, key-clicks, and parasitics. By paying attention to detail, with a good working knowledge of the limitations of the components, and with a basic conception of the actions of ground currents, the average amateur will be able to build equipment that will work "just like the book says."

The twin problems of TVI and parasitics are an outgrowth of the major problem of overall circuit design. If close attention is paid to the cardinal points of circuitry design, the secondary problems of TVI and parasitics will in themselves be solved.

15-1 Resistors

The resistance of a conductor is a function of the material, the form the material takes, the temperature of operation, and the frequency of the current passing through the resistance. In general, the variation in resistance due to temperature is directly proportional to the temperature change. With most wire-wound resistors, the resistance increases with temperature and returns to its original value when the temperature drops to normal. So-called composition or carbon resistors have less reliable temperature/resistance characteristics. They usually have a positive temperature coefficient, but the retrace curve as the resistor is cooled is often erratic, and in

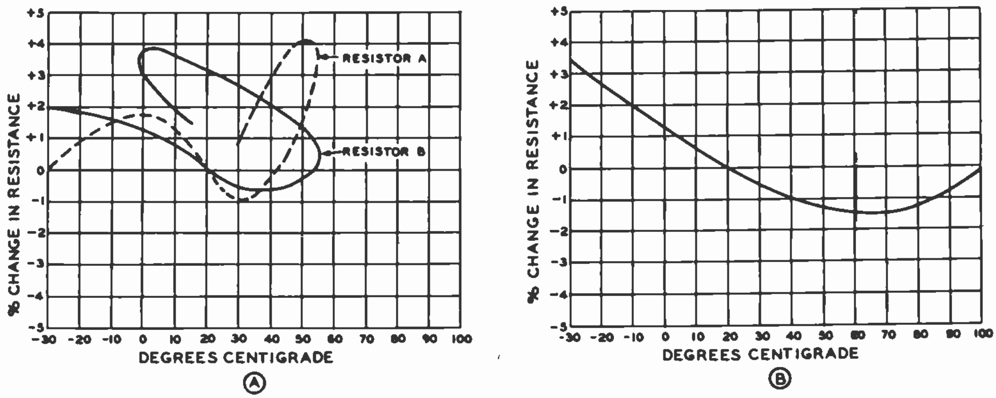


Figure 1

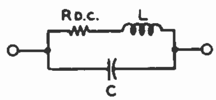
HEAT CYCLE OF UNCONDITIONED COMPOSITION RESISTORS

HEAT CYCLE OF CONDITIONED COMPOSITION RESISTORS

many cases the resistance does not return to its original value after a heat cycle. It is for this reason that care must be taken when soldering composition resistors in circuits that require close control of the resistance value. Matched resistors used in phase-inverter service can be heated out of tolerance by the act of soldering them into the circuit. Long leads should be left on the resistors and a long-nose pliers should grip the lead between the iron and the body of the resistor to act as a heat block. General temperature characteristics of typical carbon resistors are shown in figure 1. The behavior of an individual resistor will vary from these curves depending upon the manufacturer, the size and wattage of the resistor, etc.

Inductance of Resistors Every resistor because of its physical size has in addition to its desired resistance, less desirable amounts of inductance and distributed capacitance. These quantities are illustrated in figure 2A, the general equivalent circuit of a resistor. This circuit represents the actual impedance network of a resistor at any frequency. At a certain specified frequency

Figure 2



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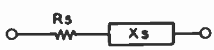
EQUIVALENT CIRCUIT OF A RESISTOR



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EQUIVALENT CIRCUIT OF A RESISTOR AT A PARTICULAR FREQUENCY

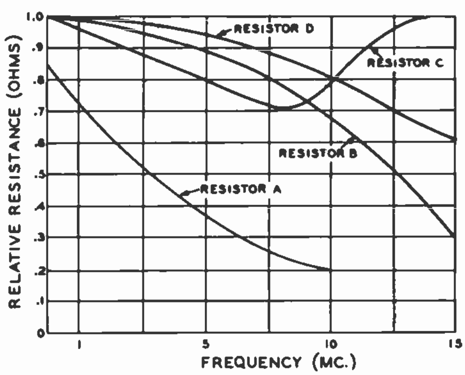


Figure 3

FREQUENCY EFFECTS ON SAMPLE COMPOSITION RESISTORS

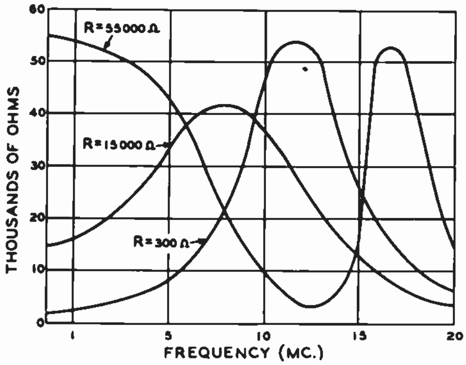


Figure 4

CURVES OF THE IMPEDANCE OF WIRE-WOUND RESISTORS AT RADIO FREQUENCIES

the impedance of the resistor may be thought of as a series reactance (X_s) as shown in figure 2B. This reactance may be either inductive or capacitive depending upon whether the residual inductance or the distributed capacitance of the resistor is the dominating factor. As a rule, skin effect tends to increase the reactance with frequency, while the capacity between turns of a wire-wound resistor, or capacity between the granules of a composition resistor tends to cause the reactance and resistance to drop with frequency. The behavior of various types of composition resistors over a large frequency range is shown in figure 3. By proper component design, non-inductive resistors having a minimum of residual reactance characteristics may be constructed. Even these have reactive effects that cannot be ignored at high frequencies.

Wirewound resistors act as low-Q inductors at radio frequencies. Figure 4 shows typical curves of the high frequency characteristics of cylindrical wirewound resistors. In addition to resistance variations wirewound resistors exhibit both capacitive and inductive reactance, depending upon the type of resistor and the operating frequency. In fact, such resistors perform in a fashion as low-Q r-f chokes below their parallel self-resonant frequency.

15-2 Capacitors

The inherent residual characteristics of capacitors include series resistance, series inductance and shunt resistance, as shown in figure 5. The series resistance and inductance

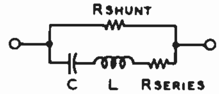


Figure 5

EQUIVALENT CIRCUIT OF A CAPACITOR

depend to a large extent upon the physical configuration of the capacitor and upon the material of which it is made. Of great interest to the amateur constructor is the series inductance of the capacitor. At a certain frequency the series inductive reactance of the capacitor and the capacitive reactance are equal and opposite, and the capacitor is in itself series resonant at this frequency. As the operating frequency of the circuit in which the capacitor is used is increased above the series resonant frequency, the effectiveness of the capacitor as a by-passing element deteriorates until the unit is about as effective as a block of wood.

By-Pass Capacitors The usual forms of by-pass capacitors have dielectrics of paper, mica, or ceramic. For audio work, and low frequency r-f work up to perhaps 2 Mc. or so, the paper capacitors are satisfactory as their relatively high internal inductance has little effect upon the proper operation of the circuit. The actual amount of internal inductance will vary widely with the manufacturing process, and some types of paper capacitors have satisfactory characteristics up to a frequency of 5 Mc. or so.

When considering the design of transmitting equipment, it must be remembered that while the transmitter is operating at some relatively low frequency of, say, 7 Mc., there will be harmonic currents flowing through the various by-pass capacitors of the order of 10 to 20 times the operating frequency. A capacitor that behaves properly at 7 Mc. however, may offer considerable impedance to the flow of these harmonic currents. For minimum harmonic generation and radiation, it is obviously of greatest importance to employ by-pass capacitors having the lowest possible internal inductance.

Mica dielectric capacitors have much less internal inductance than do most paper condensers. Figure 6 lists self-resonant frequencies of various mica capacitors having various lead lengths. It can be seen from inspection of this table that most mica capacitors become self-resonant in the 12-Mc. to 50-Mc. region. The inductive reactance they would offer to harmonic currents of 100 Mc. or so

CONDENSER	LEAD LENGTHS	RESONANT FREQ.
.02 μF MICA	NONE	44.5 MC.
.002 μF MICA	NONE	23.5 MC.
.01 μF MICA	1/4"	10 MC.
.0009 μF MICA	1/4"	55 MC.
.002 μF CERAMIC	3/8"	24 MC.
.001 μF CERAMIC	1/4"	55 MC.
500 μμF BUTTON	NONE	220 MC.
.001 μF CERAMIC	1/4"	90 MC.
.01 μF CERAMIC	1/2"	14.5 MC.

Figure 6

SELF-RESONANT FREQUENCIES OF VARIOUS CAPACITORS WITH RANDOM LEAD LENGTH

would be of considerable magnitude. In certain instances it is possible to deliberately series-resonate a mica capacitor to a certain frequency somewhat below its normal self-resonant frequency by trimming the leads to a critical length. This is sometimes done for maximum by-passing effect in the region of 40 Mc. to 60 Mc.

The recently developed button-mica capacitors shown in figure 7 are especially designed to have extremely low internal inductance. Certain types of button-mica capacitors of small physical size have a self-resonant frequency in the region of 600 Mc.

Ceramic dielectric capacitors in general have the lowest amount of series inductance per unit of capacitance of these three universally used types of by-pass capacitors. Typical resonant frequencies of various ceramic units are listed in figure 6. Ceramic capacitors are available in various voltage and capacity ratings and different physical configurations. Stand-off types such as shown in figure 7 are useful for by-passing socket and transformer terminals. Two of these capacitors may be mounted in close proximity on a chassis and connected together by an r-f choke to form a highly effective r-f filter. The inexpensive "clamshell" type of ceramic capacitor is recommended for general by-passing in r-f circuitry, as it is effective as a by-pass unit to well over 100 Mc.

The large TV "doorknob" capacitors are useful as by-pass units for high voltage lines. These capacitors have a value of 500 micro-microfarads, and are available in voltage ratings up to 40,000 volts. The dielectric of these capacitors is usually titanium-dioxide. This material exhibits piezo-electric effects, and capacitors employing it for a dielectric will tend to "talk-back" when a-c voltages are applied across them. When these capacitors are used as plate bypass units in a modulated transmitter they will cause acoustical noise. Otherwise they are excellent for general r-f work.

A recent addition to the varied line of capacitors is the coaxial or "Hypass" type of capacitor. These capacitors exhibit superior by-passing qualities at frequencies up to 200 Mc. and the bulkhead type are especially effective when used to filter leads passing through partition walls between two stages.

Variable Air Capacitors Even though air is the perfect dielectric, air capacitors exhibit losses because of the inherent resistance of the metallic parts that make up the capacitor. In addition, the leakage loss across the insulating supports may become of some consequence at high frequencies. Of greater concern is the inductance of the capacitor at high frequencies. Since the capacitor must be of finite size, it will have tie-rods and metallic braces and end plates, all of which contribute to the inductance of the unit. The actual amount of the inductance will depend upon the physical size of the capacitor and the method used to make contact to the stator and rotor plates. This inductance may be cut to a minimum value by using as small a capacitor as is practical, by using insulated tie-rods to prevent the formation of closed inductive loops in the frame of the unit, and by making connections to the centers of the plate assemblies rather than to the ends as is com-

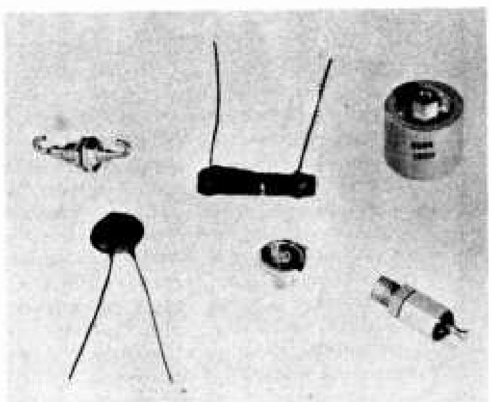


Figure 7

TYPES OF CERAMIC AND MICA CAPACITORS SUITABLE FOR HIGH-FREQUENCY BYPASSING

The Centralab 858S (1000 μμfd) is recommended for screen and plate circuits of tetrode tubes.

monly done. A large transmitting capacitor may have an inherent inductance as large as 0.1 microhenry, making the capacitor susceptible to parasitic resonances in the 50 Mc. to 150 Mc. range of frequencies.

The question of optimum C/L ratio and capacitor plate spacing is covered in Chapter Eleven. For all-band operation of a high-power stage, it is recommended that a capacitor just large enough for 40-meter phone operation be chosen. (This will have sufficient capacitance for phone operation on all higher frequency bands.) Then use fixed padding capacitors for operation on 80 meters. Such padding capacitors are available in air, ceramic, and vacuum types.

Specially designed variable capacitors are recommended for u-h-f work; ordinary capacitors often have "loops" in the metal frame which may resonate near the operating frequency.

Variable Vacuum Capacitors Variable vacuum capacitors because of their small physical size have less inherent inductance per unit of capacity than do variable air capacitors. Their losses are extremely low, and their dielectric strength is high. Because of increased production the cost of such units is now within the reach of the designer of amateur equipment, and their use is highly recommended in high power tank circuits.

15-3 Wire and Inductors

Any length of wire, no matter how short, has a certain value of inductance. This property is of great help in making coils and inductors, but may be of great hindrance when it is not taken into account in circuit design and construction. Connecting circuit elements (themselves having residual inductance) together with a conductor possessing additional inductance can often lead to puzzling difficulties. A piece of no. 10 copper wire ten inches long (a not uncommon length for a plate lead in a transmitter) can have a self-inductance of 0.15 microhenries. This inductance and that of the plate tuning capacitor together with the plate-to-ground capacity of the vacuum tube can form a resonant circuit which may lead to parasitic oscillations in the v-h-f regions. To keep the self-inductance at a minimum, all r-f carrying leads should be as short as possible and should be made out of as heavy material as possible.

At the higher frequencies, solid enamelled copper wire is most efficient for r-f leads. Tinned or stranded wire will show greater losses at these frequencies. Tank coil and tank capacitor leads should be of heavier wire than other r-f leads.

The best type of flexible lead from the envelope of a tube to a terminal is thin copper strip, cut from thin sheet copper. Heavy, rigid leads to these terminals may crack the envelope glass when a tube heats or cools.

Wires carrying only a.f. or d.c. should be chosen with the voltage and current in mind. Some of the low-filament-voltage transmitting tubes draw heavy current, and heavy wire must be used to avoid voltage drop. The voltage is low, and hence not much insulation is required. Filament and heater leads are usually twisted together. An initial check should be made on the filament voltage of all tubes of 25 watts or more plate dissipation rating. This voltage should be measured right at the tube sockets. If it is low, the filament transformer voltage should be raised. If this is impossible, heavier or parallel wires should be used for filament leads, cutting down their length if possible.

Coaxial cable may be used for high voltage leads when it is desirable to shield them from r-f fields. RG-8/U cable may be used at d-c potentials up to 8000 volts, and the lighter RG-17/U may be used to potentials of 3000 volts. Spark-plug type high-tension wire may be used for unshielded leads, and will withstand 10,000 volts.

If this cable is used, the high-voltage leads may be cabled with filament and other low-voltage leads. For high-voltage leads in low-power exciters, where the plate voltage is not over 450 volts, ordinary radio hookup wire of good quality will serve the purpose.

No r-f leads should be cabled; in fact it is better to use enamelled or bare copper wire for r-f leads and rely upon spacing for insulation. All r-f joints should be soldered, and the joint should be a good mechanical junction before solder is applied.

The efficiency and Q of air coils commonly used in amateur equipment is a factor of the shape of the coil, the proximity of the coil to other objects (including the coil form) and the material of which the coil is made. Dielectric losses in so-called "air wound" coils are low and the Q of such coils runs in the neighborhood of 300 to 500 at medium frequencies. Unfortunately, most of the transmitting type plug-in coils on the market designed for link coupling have far too small a pick up link for proper operation at 7 Mc. and 3.5 Mc. The coefficient of coupling of these coils is about 0.5, and additional means must be employed to provide satisfactory coupling at these low frequencies. Additional inductance in series with the pick up link, the whole being reso-

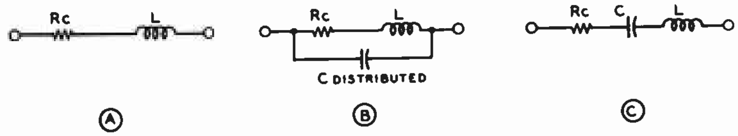


Figure 8

ELECTRICAL EQUIVALENT OF R-F CHOKE AT VARIOUS FREQUENCIES

nated to the operating frequency will often permit satisfactory coupling.

Coil Placement For best Q a coil should be in the form of a solenoid with length from one to two times the diameter. For minimum interstage coupling, coils should be made as small physically as is practicable. The coils should then be placed so that adjoining coils are oriented for minimum mutual coupling. To determine if this condition exists, apply the following test: the axis of one of the two coils must lie in the plane formed by the center turn of the other coil. If this condition is not met, there will be appreciable coupling unless the unshielded coils are very small in diameter or are spaced a considerable distance from each other.

Insulation On frequencies above 7 Mc., ceramic, polystyrene, or Mycalex insulation is to be recommended. Cold flow must be considered when using polystyrene (Amphenol 912, etc.). Bakelite has low losses on the lower frequencies but should never be used in the field of high-frequency tank circuits.

Lucite (or Plexiglas), which is available in rods, sheets, or tubing, is satisfactory for use at all radio frequencies *where the r-f voltages are not especially high.* It is very easy to work with ordinary tools and is not expensive. The loss factor depends to a considerable extent upon the amount and kind of plasticizer used.

The most important thing to keep in mind regarding insulation is that the best insulation is air. If it is necessary to reinforce air-wound coils to keep turns from vibrating or touching, use strips of Lucite or polystyrene cemented in place with Amphenol 912 coil dope. This will result in lower losses than the commonly used celluloid ribs and Duco cement.

Radio Frequency Chokes R-f chokes may be considered to be special inductances designed to have a high value of impedance over a large range of frequencies. A practical r-f choke has inductance, distributed capacitance, and resistance. At low frequencies, the distributed capacity has little effect and the electrical equivalent circuit of the r-f choke is as shown in figure 8A. As the operating frequency of the choke is raised the effect of the distributed capacity becomes more evident until at some particular frequency the distributed capacity resonates with the inductance of the choke and a parallel resonant circuit is formed. This point is shown in figure 8B. As the frequency of operation is further increased the overall reactance of the choke becomes capacitive, and finally a point of series resonance is reached (figure 8C.). This cycle repeats itself as the operating frequency is raised above the series resonant point, the impedance of the choke rapidly becoming lower on each successive cycle. A chart of this action is shown in figure 9. It can be seen that as the r-f choke approaches and leaves a condition of series resonance, the performance of the choke is seriously impaired. The condition of series resonance may easily be found by shorting the terminals of the r-f choke in question with a piece of wire and exploring the windings of the choke with a grid-dip oscillator. Most commercial transmitting type chokes have series resonances in the vicinity of 11 Mc. or 24 Mc.

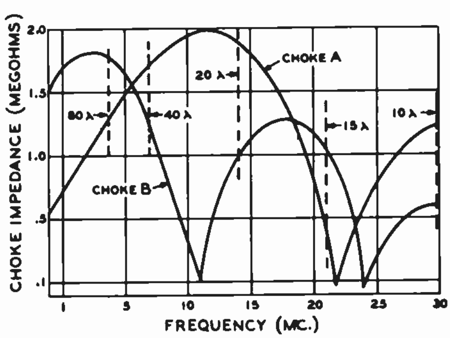


Figure 9

FREQUENCY-IMPEDANCE CHARACTERISTICS FOR TYPICAL PIE-WOUND R-F CHOKES

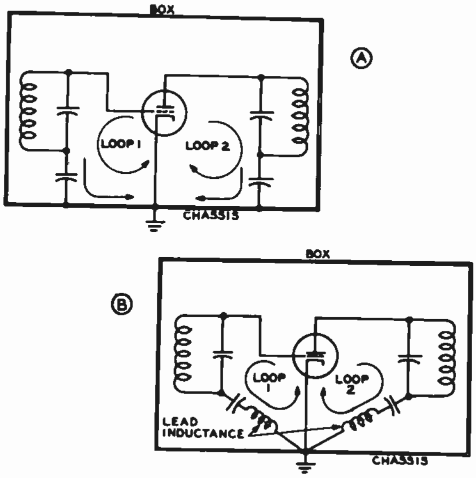


Figure 10
GROUND LOOPS IN AMPLIFIER STAGES
A. Using chassis return
B. Common ground point

15-4 Grounds

At frequencies of 30 Mc. and below, a chassis may be considered as a fixed ground reference, since its dimensions are only a fraction of a wavelength. As the frequency is increased above 30 Mc., the chassis must be considered as a conducting sheet on which there are points of maximum current and potential. However, for the lower amateur frequencies, an object may be assumed to be at ground potential when it is affixed to the chassis.

In transmitter stages, two important current loops exist. One loop consists of the grid circuit and chassis return, and the other loop consists of the plate circuit and chassis return. These two loops are shown in figure 10A. It can be seen that the chassis forms a return for both the grid and plate circuits, and that *ground currents* flow in the chassis towards the cathode circuit of the stage. For some years the theory has been to separate these ground currents from the chassis by returning all ground leads to one point, usually the cathode of the tube for the stage in question. This is well and good if the ground leads are of minute length and do not introduce cross couplings between the leads. Such a technique is illustrated in figure 10B. wherein all stage components are grounded to the cathode pin of the stage socket. However, in transmitter construction the physical size of the components prevent such close grouping. It is necessary to spread the components of such a stage over a fairly large area. In this case it is best to ground items directly to the chassis at the nearest possible point, with short, direct grounding leads. The ground currents will flow from these points through the low inductance chassis to the cathode return of the stage. Components grounded on the top of the chassis have their ground currents flow through holes to the cathode circuit which is usually located on the bottom of the chassis, since such currents travel on the surface of the chassis. The usual "top to bottom" ground path is through the hole cut in the chassis for the tube socket. When the gain per stage is relatively low, or there are only a small number of stages on a chassis this universal grounding system is ideal. It is only in high gain stages (i-f strips) where the "gain per inch" is very high that circulating ground currents will cause operational instability.

Intercoupling of Ground Currents It is important to prevent intercoupling of various different ground currents when the chassis is used as a common ground return. To keep this intercoupling at a minimum, the stage should be completely shielded. This will prevent external fields from generating spurious ground currents, and prevent the ground currents of the stage from upsetting the action of nearby stages. Since the ground currents travel on the surface of the metal, the stage should be enclosed in an electrically tight box. When this is done, all ground currents generated inside the box will remain in the box. The only possible means of escape for fundamental and harmonic currents are imperfections in this electrically tight box. Whenever we bring a wire lead into the box, make a ventilation hole, or bring a control shaft through the box we create an imperfection. It is important that the effect of these imperfections be reduced to a minimum.

15-5 Holes, Leads and Shafts

Large size holes for ventilation may be put in an electrically tight box provided they are properly screened. Perforated metal stock having many small, closely spaced holes is the best screening material. Copper wire screen may be used provided the screen wires are bonded together every few inches. As the wire corrodes, an insulating film prevents contact between the individual wires, and the attenuation of the screening suffers. The screening material should be carefully soldered to the

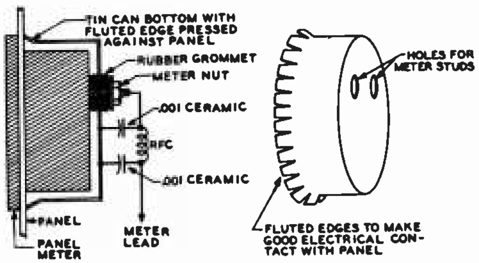


Figure 11A
SIMPLE METER SHIELD

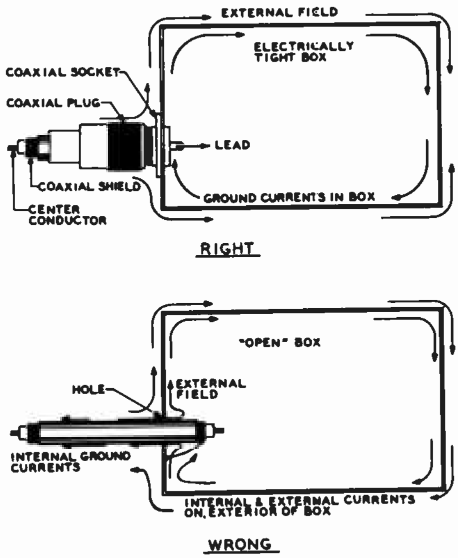


Figure 11B
Use of coaxial connectors on electrically tight box prevents escape of ground currents from interior of box. At the same time external fields are not conducted into the interior of the box.

box, or bolted with a spacing of not less than two inches between bolts. Mating surfaces of the box and the screening should be clean.

A screened ventilation opening should be roughly three times the size of an equivalent unscreened opening, since the screening represents about a 70 per cent coverage of the area. Careful attention must be paid to equipment heating when an electrically tight box is used.

Commercially available panels having half-inch ventilating holes may be used as part of the box. These holes have much less attenuation than does screening, but will perform in a satisfactory manner in all but the areas of weakest TV reception. If it is desired to reduce leakage from these panels to a minimum, the back of the grille must be covered with screening tightly bonded to the panel.

Doors may be placed in electrically tight boxes provided there is no r-f leakage around the seams of the door. Electronic weather-stripping or metal "finger stock" may be used to seal these doors. A long, narrow slot in a closed box has the tendency to act as a slot antenna and harmonic energy may pass more readily through such an opening than it would through a much larger circular hole.

Variable capacitor shafts or switch shafts may act as antennas, picking up currents inside the box and re-radiating them outside of the box. It is necessary either to ground the shaft securely as it leaves the box, or else to make the shaft of some insulating material.

A two or three inch panel meter requires a large leakage hole if it is mounted in the wall of an electrically tight box. To minimize leakage, the meter leads should be by-passed and shielded. The meter should be encased with a metal shield that makes contact to the box entirely around the meter. The connecting studs of the meter may project through the back of the metal shield. Such a shield may be made out of the end of a tin can of correct diameter, cut to fit the depth of the meter. This complete shield assembly is shown in figure 11A.

Careful attention should be paid to leads entering and leaving the electrically tight box. Harmonic currents generated within the box can easily flow out of the box on power or control leads, or even on the outer shields of coaxially shielded wires. Figure 11B illustrates the correct method of bringing shielded cables into a box where it is desired to preserve the continuity of the shielding.

Unshielded leads entering the box must be carefully filtered to prevent fundamental and harmonic energy from escaping down the lead. Combinations of r-f chokes and low inductance by-pass capacitors should be used in power leads. If the current in the lead is high, the chokes must be wound of large gauge wire. Composition resistors may be substituted for the r-f chokes in high impedance circuits. Bulkhead or feed-through type capacitors are preferable when passing a lead through a shield partition. A summary of lead leakage with various filter arrangements is shown in figure 12.

Internal Leads Leads that connect two points within an electrically tight box

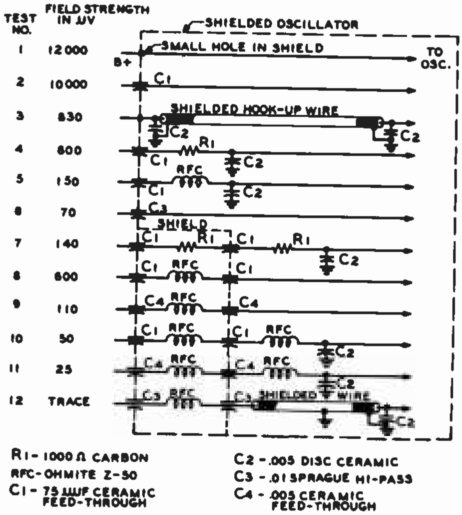


Figure 12
LEAD LEAKAGE WITH VARIOUS LEAD FILTERING SYSTEMS (COURTESY W1DBM)

may pick up fundamental and harmonic currents if they are located in a strong field of flux. Any lead forming a closed loop with itself will pick up such currents, as shown in figure 13. This effect is enhanced if the lead happens to be self-resonant at the frequency at which the exciting energy is supplied. The solution for all of this is to by-pass all internal power leads and control leads at each end, and to shield these leads their entire length. All filament, bias, and meter leads should be so treated. This will make the job of filtering the leads as they leave the box much easier, since normally "cool" leads within the box will not have picked up spurious currents from nearby "hot" leads.

15-6 Parasitic Resonances

Filament leads within vacuum tubes may resonate with the filament by-pass capacitors at some particular frequency and cause instability in an amplifier stage. Large tubes of the 810 and 250TH type are prone to this spurious effect. In particular, a push-pull 810 amplifier using .001-µfd. filament by-pass capacitors had a filament resonant loop that fell in the 7-Mc. amateur band. When the amplifier was operated near this frequency marked instability was noted, and the filaments of the 810 tubes increased in brilliance when plate voltage was applied to the amplifier, indicating the presence of r.f. in the filament circuit. Changing the filament by-pass capacitors to .01-µfd. lowered the filament resonance frequency to 2.2 Mc. and cured this effect. A ceramic capacitor of .01-µfd. used as a filament by-pass capacitor on each filament leg seems to be satisfactory from both a resonant and a TVI point of view. Filament by-pass capacitors smaller in value than .01-µfd. should be used with caution.

Various parasitic resonances are also found in plate and grid tank circuits. Push-pull tank circuits are prone to double resonances, as shown in figure 14. The parasitic resonance circuit is usually several megacycles higher than the actual resonant frequency of the full tank circuit. The cure for such a double resonance is the inclusion of an r-f choke in the center tap lead to the split coil.

Chassis Material From a point of view of electrical properties, aluminum is a poor chassis material. It is difficult to make a soldered joint to it, and all grounds must rely upon a pressure joint. These pres-

Figure 13

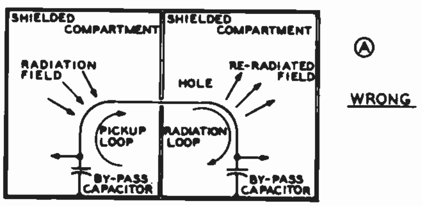


ILLUSTRATION OF HOW A SUPPOSEDLY GROUNDED POWER LEAD CAN COUPLE ENERGY FROM ONE COMPARTMENT TO ANOTHER

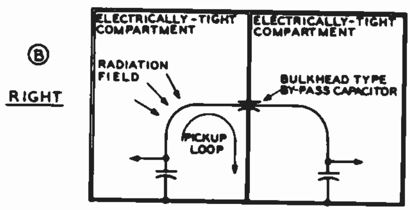


ILLUSTRATION OF LEAD ISOLATION BY PROPER USE OF BULKHEAD BYPASS CAPACITOR

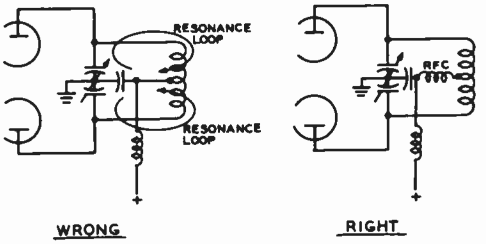


Figure 14
DOUBLE RESONANCE EFFECTS IN PUSH-PULL TANK CIRCUIT MAY BE ELIMINATED BY THE INSERTION OF ANY R-F CHOKE IN THE COIL CENTER TAP LEAD

sure joints are prone to give trouble at a later date because of high resistivity caused by the formation of oxides from eletrolytic action in the joint. However, the ease of working and forming the aluminum material far outweighs the electrical shortcomings, and aluminum chassis and shielding may be used with good results provided care is taken in making all grounding connections. Cadmium and zinc plated chassis are preferable from a corrosion standpoint, but are much more difficult to handle in the home workshop.

15-7 Parasitic Oscillation in R-F Amplifiers

Parasitics (as distinguished from *self-oscillation* on the normal tuned frequency of the amplifier) are undesirable oscillations either of very high or very low frequencies which may occur in radio-frequency amplifiers.

They may cause spurious signals (which are often rough in tone) other than normal harmonics, hash on each side of a modulated carrier, key clicks, voltage breakdown or flashover, instability or inefficiency, and shortened life or failure of the tubes. They may be damped and stop by themselves after keying or modulation peaks, or they may be undamped and build up during ordinary unmodulated transmission, continuing if the excitation is removed. They may result from series or parallel resonant circuits of all types. Due to neutralizing lead length and the nature of most parasitic circuits, the amplifier usually is not neutralized for the parasitic frequency.

Sometimes the fact that the plate supply is keyed will obscure parasitic oscillations in a final amplifier stage that might be very severe if the plate voltage were left on and the excitation were keyed.

In some cases, an all-wave receiver will prove helpful in locating v-h-f spurious oscillations, but it may be necessary to check from several hundred megacycles downward in frequency to the operating range. A normal harmonic is weaker than the fundamental but of good tone; a strong harmonic or a rough note at any frequency generally indicates a parasitic.

In general, the cure for parasitic oscillation is two-fold: The oscillatory circuit is damped until sustained oscillation is impossible, or it is detuned until oscillation ceases. An examination of the various types of parasitic oscillations and of the parasitic oscillatory circuits will prove handy in applying the correct cure.

Low Frequency Parasitic Oscillations One type of unwanted oscillation often occurs in shunt-fed circuits in which the grid and plate chokes resonate, coupled through the tube's interelectrode capacitance. This also can happen with series feed. This oscillation is generally at a much lower frequency than the operating frequency and will cause additional carriers to appear, spaced from perhaps twenty to a few hundred kilocycles on either side of the main wave. Such a circuit is illustrated in figure 15. In this case, RFC_1 and RFC_2 form the grid and plate inductances of the parasitic oscillator. The neutralizing capacitor, no longer providing out-of-phase feedback to the grid circuit actually enhances the low frequency oscillation. Because of the low Q of the r-f chokes, they will usually run warm when this type of parasitic oscillation is present and may actually char and burn up. A neon bulb held near the oscillatory circuit will glow a bright yellow, the color appearing near the glass of the neon bulb and not between the electrodes.

One cure for this type of oscillation is to change the type of choke in either the plate or the grid circuit. This is a marginal cure, because the amplifier may again break into the same type of oscillation when the plate voltage is raised slightly. The best cure is to remove the grid r-f choke entirely and replace it with a wirewound resistor of sufficient wattage to carry the amplifier grid current. If the inclusion of such a resistor upsets the operating bias of the stage, an r-f choke may be used, with a 100-ohm 2-watt carbon resistor in series with the choke to lower the operating Q of the choke. If this expedient does not eliminate the condition, and the stage under investigation uses a beam-tetrode tube, negative resistance can exist in the screen circuit

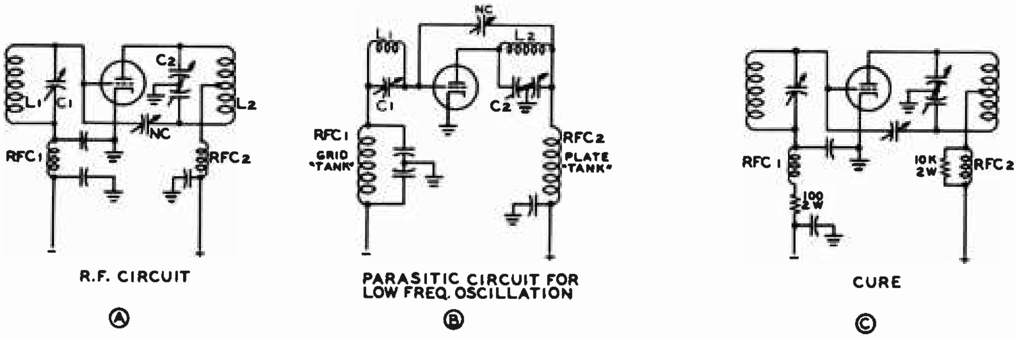


Figure 15

THE CAUSE AND CURE OF LOW FREQUENCY PARASITICS

of such tubes. Try larger and smaller screen by-pass capacitors to determine whether or not they have any effect. If the condition is coming from the screen circuit an audio choke with a resistor across it in series with the screen feed lead will often eliminate the trouble.

Low-frequency parasitic oscillations can often take place in the audio system of an AM transmitter, and their presence will not be known until the transmitter is checked on a receiver. It is easy to determine whether or not the oscillations are coming from the modulator simply by switching off the modulator tubes. If the oscillations are coming from the modulator, the stage in which they are being generated can be determined by removing tubes successively, starting with the first speech amplification stage, until the oscillation stops. When the stage has been found, remedial steps can be taken on that stage.

If the stage causing the oscillation is a low-level speech stage it is possible that the trouble is coming from r-f or power-supply feedback, or it may be coming about as a result of inductive coupling between two transformers. If the oscillation is taking place in a high-level audio stage, it is possible that inductive or capacitive coupling is taking place back to one of the low-level speech stages. It is also possible, in certain cases, that parasitic push-pull oscillation can take place in a Class B or Class AB modulator as a result of the grid-to-plate capacitance within the tubes and in the stage wiring. This condition is more likely to occur if capacitors have been placed across the secondary of the driver transformer and across the primary of the modulation transformer to act in the reduction of the amplitude of the higher audio frequencies. Relocation of wiring or actual neutralization of the audio stage in the manner used for r-f stages may be required.

It may be said in general that the presence of low-frequency parasitics indicates that somewhere in the oscillating circuit there is an impedance which is high at a frequency in the upper audio or low r-f range. This impedance may include one or more r-f chokes of the conventional variety, power supply chokes, modulation components, or the high impedance may be presented simply by an RC circuit such as might be found in the screen-feed circuit of a beam-tetrode amplifier stage.

15-8 Elimination of V-H-F Parasitic Oscillations

V-h-f parasitic oscillations are often difficult to locate and difficult to eliminate since their frequency often is only moderately above the desired frequency of operation. But it may be said that v-h-f parasitics always may be eliminated if the operating frequency is appreciably below the upper frequency limit for the tubes used in the stage. However, the elimination of a persistent parasitic oscillation on a frequency only moderately higher than the desired operating frequency will involve a sacrifice in either the power output or the power sensitivity of the stage, or in both.

Beam-tetrode stages, particularly those using 807 type tubes, will almost invariably have one or more v-h-f parasitic oscillations unless adequate precautions have been taken in advance. Many of the units described in the constructional section of this edition had parasitic oscillations when first constructed. But these oscillations were eliminated in each case; hence, the expedients used in these equipments should be studied. V-h-f parasitics may be readily identified, as they cause a neon lamp to have a purple glow close to the electrodes when it is excited by the parasitic energy.

Parasitic Oscillations with Triodes Triode stages are less subject to parasitic oscillations primarily because of the much lower power sensitivity of such tubes as compared to beam tetrodes. But such oscillations can and do take place. Usually, however, it is not necessary to incorporate losser resistors as normally is the case with beam tetrodes, unless the triodes are operated quite near to their upper frequency limit, or the tubes are characterized by a relatively high transconductance. Triode v-h-f parasitic oscillations normally may be eliminated by adjustment of the lengths and effective inductance of the leads to the elements of the tubes.

In the case of triodes, v-h-f parasitic oscillations often come about as a result of inductance in the neutralizing leads. This is particularly true in the case of push-pull amplifiers. The cure for this effect will usually be found in reducing the length of the neutralizing leads and increasing their diameter. Both the reduction in length and increase in diameter will reduce the inductance of the leads and tend to raise the parasitic oscillation frequency until it is out of the range at which the tubes will oscillate. The use of straightforward circuit design with short leads will assist in forestalling this trouble at the outset. Butterfly-type tank capacitors with the neutralizing capacitors built into the unit (such as the B&W type) are effective in this regard.

V-h-f parasitic oscillations may take place as a result of inadequate by-passing or long by-pass leads in the filament, grid-return and plate-return circuits. Such oscillations also can take place when long leads exist between the grids and the grid tuning capacitor or between the plates and the plate tuning capacitor. The grid and plate leads should be kept short, but the leads from the tuning capacitors to the tank coils can be of any reasonable length insofar as parasitic oscillations are concerned. In an amplifier where oscillations have been traced to the grid or plate leads, their elimination can often be effected by making the grid leads much longer than the plate leads or vice versa. Sometimes parasitic oscillations can be eliminated by using iron or nichrome wire for the grid or plate leads, or for the neutralizing leads. But in any event it will always be found best to make the neutralizing leads as short and of as heavy conductor as is practicable.

In cases where it has been found that increased length in the grid leads for an amplifier is required, this increased length can often be wound into the form of a small coil and still obtain the desired effect. Winding these small coils of iron or nichrome wire may sometimes be of assistance.

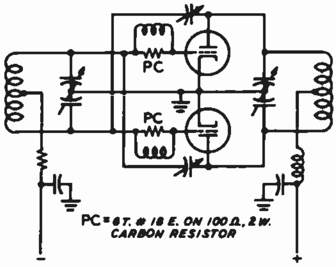


Figure 16

GRID PARASITIC SUPPRESSORS IN PUSH-PULL TRIODE STAGE

To increase losses at the parasitic frequency, the parasitic coils may be wound on 100-ohm 2-watt resistors. These "lossy" suppressors should be placed in the grid leads of the tubes close to the grid connection, as shown in figure 16.

Parasitics with Beam Tetrodes Where beam-tetrode tubes are used in the stage which has been found to be generating the parasitic oscillation, all the foregoing suggestions apply in general. However, there are certain additional considerations involved in elimination of parasitics from beam-tetrode amplifier stages. These considerations involve the facts that a beam-tetrode amplifier stage has greater power sensitivity than an equivalent triode amplifier, such a stage has a certain amount of screen-lead inductance which may give rise to trouble, and such stages have a small amount of feedback capacitance.

Beam-tetrode stages often will require the inclusion of a neutralizing circuit to eliminate oscillation on the operating frequency. However, oscillation on the operating frequency normally is not called a parasitic oscillation, and different measures are required to eliminate the condition.

Basically, parasitic oscillations in beam-tetrode amplifier stages fall into two classes: cathode-grid-screen oscillations, and cathode-screen-plate oscillations. Both these types of oscillation can be eliminated through the use of a parasitic suppressor in the lead between the screen terminal of the tube and the screen by-pass suppressor, as shown in figure 17. Such a suppressor has negligible effect on the by-passing effect of the screen at the operating frequency. The method of connecting this

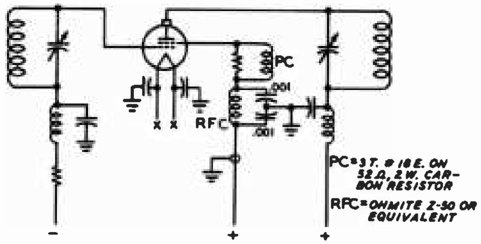


Figure 17
SCREEN PARASITIC SUPPRESSION CIRCUIT FOR TETRODE TUBES

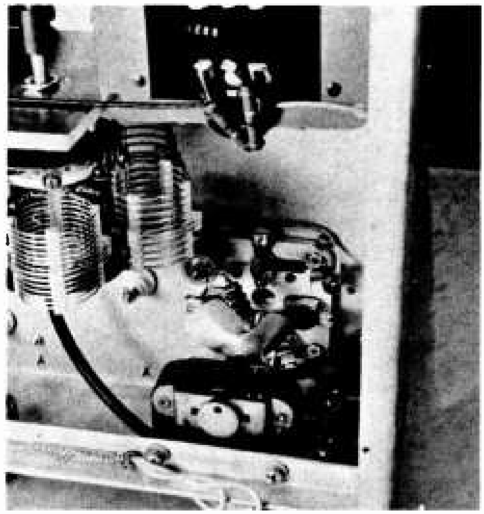


Figure 18
PHOTO OF APPLICATION OF SCREEN PARASITIC SUPPRESSION CIRCUIT OF FIGURE 17

suppressor to tubes having dual screen leads is shown in figure 18. At the higher frequencies at which parasitics occur, the screen is no longer at ground potential. It is therefore necessary to include an r-f choke by-pass condenser filter in the screen lead after the parasitic suppressor. The screen lead, in addition, should be shielded for best results.

During parasitic oscillations, considerable r-f voltage appears on the screen of a tetrode tube, and the screen by-pass condenser can easily be damaged. It is best, therefore, to employ screen by-pass condensers whose d-c working voltage is equal to twice the maximum applied screen voltage.

The grid-screen oscillations may occasionally be eliminated through the use of a parasitic suppressor in series with the grid lead of the tube. The screen plate oscillations may also be eliminated by inclusion of a parasitic suppressor in series with the plate lead of the tube. A suitable grid suppressor may be made of a 22-ohm 2-watt Ohmite or Allen-Bradley resistor wound with 8 turns of no. 18 enameled wire. A plate circuit suppressor is more of a problem, since it must dissipate a quantity of power that is dependent upon just how close the parasitic frequency is to the operating frequency of the tube. If the two frequencies are close, the suppressor will absorb some of the fundamental plate circuit power. For kilowatt stages operating no higher than 30 Mc. a satisfactory plate circuit suppressor may be made of five 570-ohm 2-watt carbon resistors in parallel, shunted by 5 turns of no. 16 enameled wire, ¾ inch diameter and ½ inch long (figure 19A and B).

The parasitic suppressor for the plate circuit of a small tube such as the 5763, 2E26, 807, 6146 or similar type normally may consist of a 47-ohm carbon resistor of 2-watt size with 6 turns of no. 18 enameled wire wound around the resistor. However, for operation above 30 Mc., special tailoring of the value of the resistor and the size of the coil wound around it will be required in order to attain satisfactory parasitic suppression without excessive power loss in the parasitic suppressor.

Tetrode Screening Isolation between the grid and plate circuits of a tetrode tube is not perfect. For maximum stability, it is recommended that the tetrode stage be neutralized. Neutralization is *absolutely necessary* unless the grid and plate circuits of the tetrode stage are each completely isolated from each other in electrically tight boxes. Even when this is done, the stage will show signs of regeneration when the plate and grid tank circuits are tuned to the same frequency. Neutralization will eliminate this regeneration. Any of the neutralization circuits described in the chapter *Generation of R-F Energy* may be used.

15-9 Checking for Parasitic Oscillations

It is an unusual transmitter which harbors no parasitic oscillations when first constructed

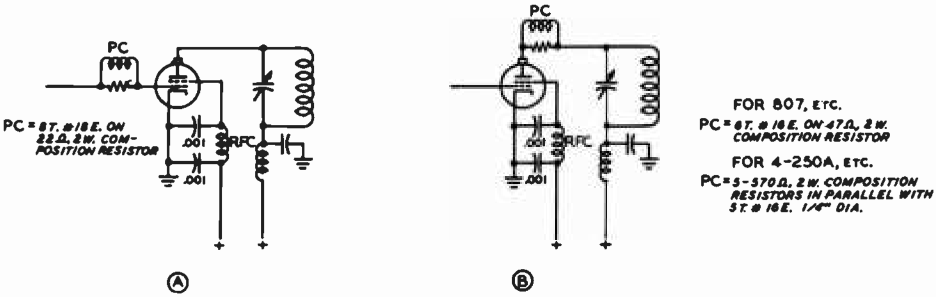


Figure 19

PLATE AND GRID PARASITIC SUPPRESSION IN TETRODE TUBES

and tested. Therefore it is always wise to follow a definite procedure in checking a new transmitter for parasitic oscillations.

Parasitic oscillations of all types are most easily found when the stage in question is running by itself, with full plate (and screen) voltage, sufficient protective bias to limit the plate current to a safe value, and no excitation. One stage should be tested at a time, and the complete transmitter should never be put on the air until all stages have been thoroughly checked for parasitics.

To protect tetrode tubes during tests for parasitics, the screen voltage should be applied through a series resistor which will limit the screen current to a safe value in case the plate voltage of the tetrode is suddenly removed when the screen supply is on. The correct procedure for parasitic testing is as follows (figure 20):

1. The stage in question should be coupled to a dummy load, and tuned up in correct operating shape. Sufficient protective bias should be applied to the tube at all times. For protection of the stage under test, a lamp bulb should be added in series with one leg of the primary circuit of the high voltage power supply. As the plate supply load increases during a period of parasitic oscillation, the voltage drop across the lamp increases, and the effective plate voltage drops. Bulbs of various size may be tried to adjust the voltage under testing conditions to the correct amount. If a Variac or Powerstat is at hand, it may be used in place of the bulbs for smoother voltage control. Don't test for parasitics unless some type of voltage control is used on the high voltage supply! When a stage breaks into parasitic oscillations, the plate current increases violently, and some protection to the tube under test *must* be used.

2. The r-f excitation to the tube should now be removed. When this is done, the grid, screen and plate currents of the tube should drop to zero. Grid and plate tuning condensers should be tuned to minimum capacity. No change in resting grid, screen or plate current should be observed. If a parasitic is present, grid current will flow, and there will be an abrupt increase in plate current. The size of the lamp bulb in series with the high voltage supply may be varied until the stage can oscillate continuously, without exceeding the rated plate dissipation of the tube.

3. The frequency of the parasitic may now be determined by means of an absorption wave meter, or a neon bulb. Low frequency oscillations will cause a neon bulb to glow yellow. High frequency oscillations will cause the bulb to have a soft, violet glow. Once the frequency of oscillation is determined, the cures suggested in this chapter may be applied to the stage.

4. When the stage can pass the above test with no signs of parasitics, the bias supply of the tube in question should be decreased until the tube is dissipating its full plate rating when full plate voltage is applied, with no r-f

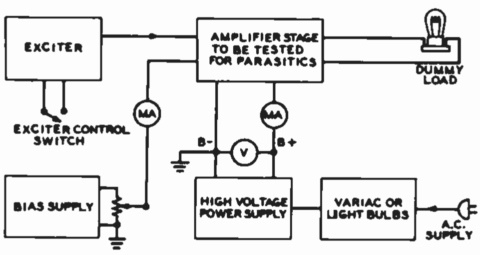


Figure 20

SUGGESTED TEST SETUP FOR PARASITIC TESTS

excitation. Excitation may now be applied and the stage loaded to full input into a dummy load. The signal should now be monitored in a nearby receiver which has the antenna terminals grounded or otherwise shorted out. A series of rapid dots should be sent, and the frequency spectrum for several megacycles each side of the carrier frequency carefully searched. If any vestige of parasitic is left, it will show up as an occasional "pop" on a keyed dot. This "pop" may be enhanced by a slight detuning of either the grid or plate circuit.

5. If such a parasitic shows up, it means that the stage is still not stable, and further measures must be applied to the circuit. Parasitic suppressors may be needed in both screen and grid leads of a tetrode, or perhaps in both grid and neutralizing leads of a triode stage. As a last resort, a 10,000-ohm 25-watt wirewound resistor may be shunted across the grid coil, or grid tuning condenser of a high powered stage. This strategy removed a keying pop that showed up in a commercial transmitter, operating at a plate voltage of 5000.

CHAPTER SIXTEEN

Television and Broadcast Interference

The problem of interference to television reception is best approached by the philosophy discussed in Chapter Fifteen. By correct design procedure, spurious harmonic generation in low frequency transmitters may be held to a minimum. The remaining problem is twofold: to make sure that the residual harmonics generated by the transmitter are not radiated, and to make sure that the fundamental signal of the transmitter does not overload the television receiver by reason of the proximity of one to the other.

In an area of high TV-signal field intensity the TVI problem is capable of complete solution with routine measures both at the amateur transmitter and at the affected receivers. But in fringe areas of low TV-signal field strength the complete elimination of TVI is a difficult and challenging problem. The fundamentals illustrated in Chapter Fifteen must be closely followed, and additional antenna filtering of the transmitter is required.

16-1 Types of Television Interference

There are three main types of TVI which may be caused singly or in combination by the emissions from an amateur transmitter. These types of interference are:

(1) Overloading of the TV set by the transmitter fundamental
(2) Impairment of the picture by spurious emissions
(3) Impairment of the picture by the radiation of harmonics

TV Set Overloading Even if the amateur transmitter were perfect and had no harmonic radiation or spurious emissions whatever, it still would be likely to cause overloading of TV sets whose antennas were within a few hundred feet of the transmitting antenna. This type of overloading is essentially the same as the common type of BCI encountered when operating a medium-power or high-power amateur transmitter within a few hundred feet of the normal type of BCL receiver. The field intensity in the immediate vicinity of the transmitting antenna is sufficiently high that the amateur signal will get into the BC or TV set either through overloading of the front end, or through the i-f, video, or audio system. A characteristic of this type of interference is that it always will be eliminated when the transmitter temporarily is operated into a dummy antenna. Another characteristic of this type of overloading is that its effects will be substantially continuous over the entire frequency coverage of the BC or TV receiver. Channels 2 through 13 will be affected in approximately the same manner.

With the overloading type of interference the problem is simply to keep the *fundamental* of the transmitter out of the affected receiver. Other types of interference may or may not show up when the fundamental is taken out of the TV set (they probably will appear), but at least the fundamental *must* be eliminated first.

The elimination of the transmitter fundamental from the TV set is normally the only operation performed on or in the vicinity of the TV receiver. After the fundamental has been elimi-

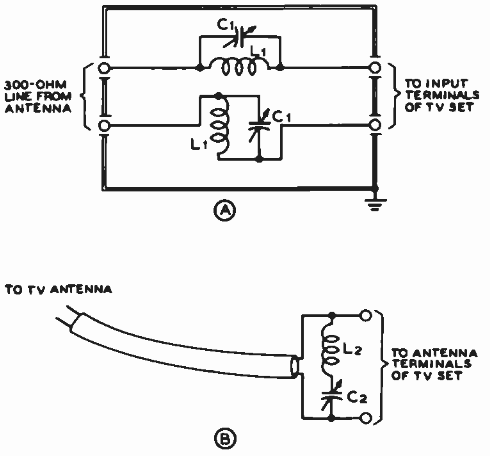


Figure 1

TUNED TRAPS FOR THE TRANSMITTER FUNDAMENTAL

The arrangement at (A) has proven to be effective in eliminating the condition of general blocking as caused by a 28-Mc. transmitter in the vicinity of a TV receiver. The tuned circuits L_1-C_1 are resonated separately to the frequency of transmission. The adjustment may be done at the station, or it may be accomplished at the TV receiver by tuning for minimum interference on the TV screen.

Shown at (B) is an alternative arrangement with a series-tuned circuit across the antenna terminals of the TV set. The tuned circuit should be resonated to the operating frequency of the transmitter. This arrangement gives less attenuation of the interfering signal than that at (A); the circuit has proven effective with interference from transmitters on the 50-Mc. band, and with low-power 28-Mc. transmitters.

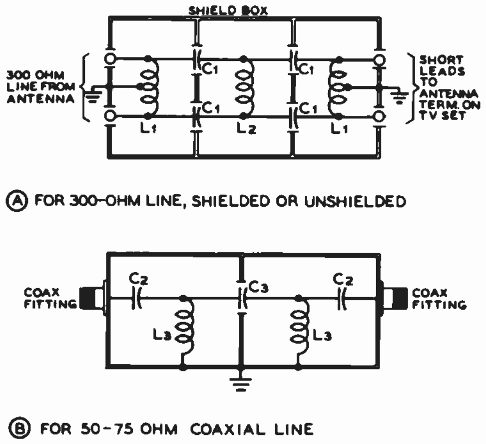


Figure 2

HIGH-PASS TRANSMISSION LINE FILTERS

The arrangement at (A) will stop the passing of all signals below about 45 Mc. from the antenna transmission line into the TV set. Coils L_1 are each 1.2 microhenrys (17 turns no. 24 enam. closewound on ¼-inch dia. polystyrene rod) with the center tap grounded. It will be found best to scrape, twist, and solder the center tap before winding the coil. The number of turns each side of the tap may then be varied until the tap is in the exact center of the winding. Coil L_2 is 0.6 microhenry (12 turns no. 24 enam. closewound on ¼-inch dia. polystyrene rod). The capacitors should be about 16.5 μμfd., but either 15 or 20 μμfd. ceramic capacitors will give satisfactory results. A similar filter for coaxial antenna transmission line is shown at (B). Both coils should be 0.12 microhenry (7 turns no. 18 enam. spaced to ½ inch on ¼-inch dia. polystyrene rod). Capacitors C_2 should be 75 μμfd. midget ceramics, while C_3 should be a 40-μμfd. ceramic.

nated as a source of interference to reception, work may then be begun on or in the vicinity of the transmitter toward eliminating the other two types of interference.

Taking Out the Fundamental More or less standard BCI-type practice is most commonly used in taking out fundamental interference. Wavetraps and filters are installed, and the antenna system may or may not be modified so as to offer less response to the signal from the amateur transmitter. In regard to a comparison between wavetraps and filters, the same considerations apply as have been effective in regard to BCI for many years; wavetraps are quite effective when properly installed and adjusted, but they must be readjusted whenever the band of operation is changed, or even when moving from one extreme end of a band to the other. Hence, wavetraps are not recommended except when operation will be confined to a relatively narrow portion of one amateur band. However, figure 1 shows two of the most common signal trapping arrangements.

High-Pass Filters High-pass filters in the antenna lead of the TV set have proven to be quite satisfactory as a means of eliminating TVI of the overloading type. In many cases when the interfering transmitter is operated only on the bands below 7.3 Mc., the use of a high-pass filter in the antenna lead has completely eliminated all

TVI. In some cases the installation of a high-pass filter in the antenna transmission line and an a-c line filter of a standard variety has proven to be completely effective in eliminating the interference from a transmitter operating in one of the lower frequency amateur bands.

In general, it is suggested that commercially manufactured high-pass filters be purchased. Such units are available from a number of manufacturers at a relatively moderate cost. However, such units may be home constructed; suggested designs are given in figures 2 and 3. Types for use both with coaxial and with balanced transmission lines have been shown. In most cases the filters may be constructed in one of the small shield boxes which are now on the market. Input and output terminals may be standard connectors, or the inexpensive type of terminal strips usually used on BC and TV sets may be employed. Coaxial terminals should of course be employed when a coaxial feed line is used to the antenna. In any event the leads from the filter box to the TV set should be very short, including both the antenna lead and the ground lead to the box itself. If the leads from the box to the set have much length, they may pick up enough signal to nullify the effects of the high-pass filter.

Blocking from 50-Mc. Signals Operation on the 50-Mc. amateur band in an area where channel 2 is in use for TV imposes a special problem in the matter of blocking. The input circuits of most TV sets are sufficiently broad so that an amateur signal on the 50-Mc. band will ride through with little attenuation. Also, the normal TV antenna will have a quite large response to a signal in the 50-Mc. band since the lower limit of channel 2 is 54 Mc.

High-pass filters of the normal type simply are not capable of giving sufficient attenuation to a signal whose frequency is so close to the necessary pass band of the filter. Hence, a resonant circuit element, as illustrated in figure 1, must be used to trap out the amateur field at the input of the TV set. The trap must be tuned or the section of transmission line cut, if a section of line is to be used for a particular frequency in the 50-Mc. band. This frequency will have to be near the lower frequency limit of the 50-Mc. band to obtain adequate rejection of the amateur signal while still not materially affecting the response of the receiver to channel 2.

Elimination of Spurious Emissions All spurious emissions from amateur transmitters (ignoring harmonic signals for the time being) must be eliminated to comply with FCC regulations. But in the past many amateur transmitters have emitted spurious signals as a result of key clicks, parasitics, and overmodulation transients. In most cases the operators of the transmitters were not aware of these emissions since they were radiated only for a short distance and hence were not brought to his attention. But with one or more TV sets in the neighborhood it is probable that such spurious signals will be brought quickly to his attention.

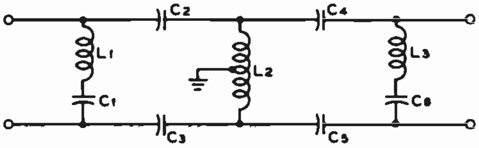


Figure 3

SERIES-DERIVED HIGH-PASS FILTER

This filter is designed for use in the 300-ohm transmission line from the TV antenna to the TV receiver. Nominal cut-off frequency is 36 Mc. and maximum rejection is at about 29 Mc.

C_1, C_6—15-μμfd. zero-coefficient ceramic

C_2, C_3, C_4, C_5—20-μμfd. zero-coefficient ceramic

L_1, L_3—2.0 μh. About 24 turns no. 28 d.c.c. wound to 5/8" on 1/4" diameter polystyrene rod. Turns should be adjusted until the coil resonates to 29 Mc. with the associated 15-μμfd. capacitor.

L_2—0.66 μh., 14 turns no. 28 d.c.c. wound to 5/8" on 1/4" dia. polystyrene rod. Adjust turns to resonate externally to 20 Mc. with an auxiliary 100-μμfd. capacitor whose value is accurately known.

16-2 Harmonic Radiation

After any condition of blocking at the TV receiver has been eliminated, and when the transmitter is completely free of transients and parasitic oscillations, it is probable that TVI will be eliminated in certain cases. Certainly general interference should be eliminated, particularly if the transmitter is a well designed affair operated on one of the lower frequency bands, and the station is in a high-signal TV area. But when the transmitter is to be operated on one of the higher frequency bands, and particularly in a marginal TV area, the job of TVI-proofing will just have begun. The elimination of harmonic radiation from the transmitter is a difficult and tedious job which must be done in an orderly manner if completely satisfactory results are to be obtained.

TRANSMITTER FUNDAMENTAL	2ND	3RD	4TH	5TH	6TH	7TH	8TH	9TH	10TH
7.0 – 7.3		21-21.9 TV I.F.			42-44 NEW TV I.F.		56-58.4 CHANNEL 2	63-65.7 CHANNEL 3	70-73 CHANNEL 4
14.0 – 14.4		42-43 NEW TV I.F.	56-57.6 CHANNEL 2	70-72 CHANNEL 4	84-86.4 CHANNEL 6	98-100.8 FM BROAD-CAST			
21.0 – 21.45 (TV I.F.)		63-64.35 CHANNEL 3	84-85.8 CHANNEL 6	105-107.25 FM BROAD-CAST				189-193 CHANNELS 9 10	210-214.5 CHANNEL 13
26.96 – 27.23	53.92-54.46 CHANNEL 2 ABOVE 27 MC. ONLY	80.88-81.69 CHANNEL 5	107.84-108.92 FM BROAD-CAST			189 CHANNEL 9	216 CHANNEL 13		
28.0 – 29.7	56-59.4 CHANNEL 2	84-89.1 CHANNEL 6			168-178.2 CHANNEL 7	196-207.9 CHANNELS 10 11 12			
50.0 – 54.0	100-108 FM BROAD-CAST		200-216 CHANNELS 11 12 13				POSSIBLE INTERFERENCE TO U-H-F CHANNELS	450-486	500-540

Figure 4
HARMONICS OF THE AMATEUR BANDS

Shown are the harmonic frequency ranges of the amateur bands between 7 and 54 Mc., with the TV channels (and TV i-f systems) which are most likely to receive interference from these harmonics. Under certain conditions amateur signals in the 1.8 and 3.5 Mc. bands can cause interference as a result of direct pickup in the video systems of TV receivers which are not adequately shielded.

First it is well to become familiar with the TV channels presently assigned, with the TV intermediate frequencies commonly used, and with the channels which will receive interference from harmonics of the various amateur bands. Figures 4 and 5 give this information.

Even a short inspection of figures 4 and 5 will make obvious the seriousness of the interference which can be caused by harmonics of amateur signals in the higher frequency bands. With any sort of reasonable precautions in the design and shielding of the transmitter it is not likely that harmonics higher than the 6th will be encountered. Hence the main offenders in the way of harmonic interference will be those bands above 14-Mc.

Nature of Harmonic Interference Investigations into the nature of the interference caused by amateur signals on the TV screen, assuming that blocking has been eliminated as described earlier in this chapter, have revealed the following facts:

1. An unmodulated carrier, such as a c-w signal with the key down or an AM signal without modulation, will give a cross-hatch or herringbone pattern on the TV screen. This same general type of picture also will occur in the case of a narrow-band FM signal either with or without modulation.
2. A relatively strong AM signal will give in addition to the herringbone a very serious succession of light and dark bands across the TV picture.
3. A moderate strength c-w signal without transients, in the absence of overloading of the TV set, will result merely in the turning on and off of the herringbone on the picture.

To discuss condition (1) above, the herringbone is a result of the beat note between the TV video carrier and the amateur harmonic. Hence the higher the beat note the less obvious will be the resulting cross-hatch. Further, it has been shown that a much stronger signal is required to produce a discernible herringbone when the interfering harmonic is as far away as possible from the video carrier, without running into the sound carrier. Thus, as a last resort, or to eliminate the last vestige of interference after all corrective measures have been taken, operate the transmitter on a frequency such that the interfer-

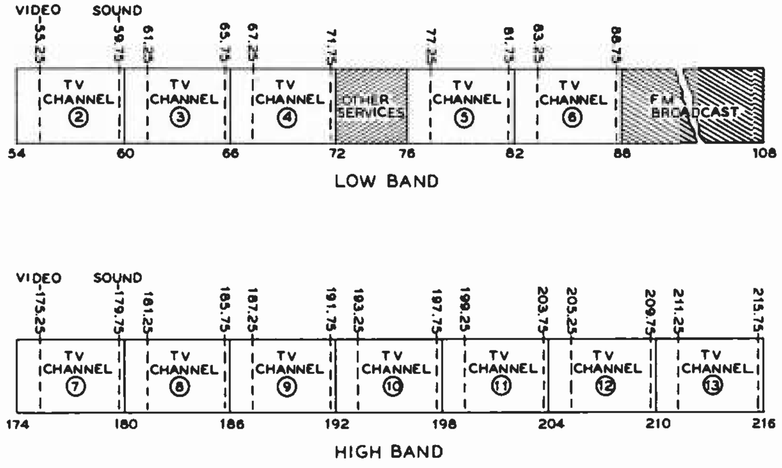


Figure 5
FREQUENCIES OF THE V-H-F TV CHANNELS.
Showing the frequency ranges of TV channels 2 through 13, with the picture carrier and sound carrier frequencies also shown.

ing harmonic will fall as far as possible from the picture carrier. The worst possible interference to the picture from a continuous carrier will be obtained when the interfering signal is very close in frequency to the video carrier.

Isolating the Source of the Interference Throughout the testing procedure it will be necessary to have some sort of indicating device as a means of determining harmonic field intensities. The best indicator for field intensities some distance from the transmitting antenna will probably be the TV receiver of some neighbor with whom friendly relations are still maintained. This person will then be able to give a check, occasionally, on the relative nature of the interference. But it will probably be necessary to go and check yourself periodically the results obtained, since the neighbor probably will not be able to give any sort of a quantitative analysis of the progress which has been made.

An additional device for checking relatively high field intensities in the vicinity of the transmitter will be almost a necessity. A simple crystal diode wavemeter, shown in figure 6 will accomplish this function. Also, it will be very helpful to have a receiver, with an S meter, capable of covering at least the 50 to 100 Mc. range and preferably the range to 216 Mc. This device may consist merely of the station receiver and a simple converter using the two halves of a 6J6 as oscillator and mixer.

The first check can best be made with the neighbor who is receiving the most serious or the most general interference. Turn on the transmitter and check all channels to determine the extent of the interference and the number of channels affected. Then disconnect the antenna and substitute a group of 100-watt lamps as a dummy load for the transmitter. Experience has shown that 8 100-watt lamps connected in two seriesed groups of four in parallel will take the output of a kilowatt transmitter on 28 Mc. if connections are made symmetrically to the group of lamps. Then note the interference. Now remove plate voltage from the final amplifier and determine the extent of interference caused by the exciter stages.

In the average case, when the final amplifier is a beam tetrode stage and the exciter is

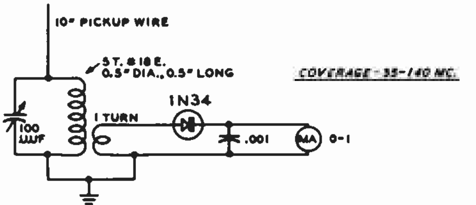


Figure 6
Crystal-diode wavemeter suitable for checking high-intensity harmonics in TV region.

relatively low powered and adequately shielded, it will be found that the interference drops materially when the antenna is removed and a dummy load substituted. It will also be found in such an average case that the interference will stop when the exciter only is operating.

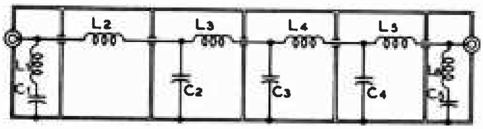
Transmitter Power Level It should be made clear at this point that the level of power used at the transmitter is not of great significance in the basic harmonic reduction problem. The difference in power level between a 20-watt transmitter and one rated at a kilowatt is only a matter of about 17 db. Yet the degree of harmonic attenuation required to eliminate interference caused by harmonic radiation is from 80 to 120 db, depending upon the TV signal strength in the vicinity. This is not to say that it is not a simpler job to eliminate harmonic interference from a low-power transmitter than from a kilowatt equipment. It is simpler to suppress harmonic radiation from a low-power transmitter simply because it is a much easier problem to shield a low-power unit, and the filters for the leads which enter the transmitter enclosure may be constructed less expensively and smaller for a low-power unit.

16-3 Low-Pass Filters

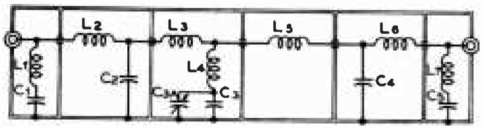
After the transmitter has been shielded, and all power leads have been filtered in such a manner that the transmitter shielding has not been rendered ineffective, the only remaining available exit for harmonic energy lies in the antenna transmission line. Hence the main burden of harmonic attenuation will fall on the low-pass filter installed between the output of the transmitter and the antenna system.

Experience has shown that the low-pass filter can best be installed externally to the main transmitter enclosure, and that the transmission line from the transmitter to the low-pass filter should be of the coaxial type. Hence the majority of low-pass filters are designed for a characteristic impedance of 52 ohms, so that RG-8/U cable (or RG-58/U for a small transmitter) may be used between the output of the transmitter and the antenna transmission line or the antenna tuner.

Transmitting-type low-pass filters for amateur use usually are designed in such a manner as to pass frequencies up to about 30 Mc. without attenuation. The nominal cutoff frequency of the filters is usually between 38 and 45 Mc., and *m*-derived sections with maximum attenuation in channel 2 usually are included. Well-designed filters capable of carrying any power level up to one kilowatt are



(A)



(B)

Figure 7
LOW-PASS FILTER SCHEMATIC DIAGRAMS

The filter illustrated at (A) uses m-derived terminating half sections at each end, with three constant-k mid-sections. The filter at (B) is essentially the same except that the center section has been changed to act as an m-derived section which can be designed to offer maximum attenuation to channels 2, 4, 5, or 6 in accordance with the constants given below. Cutoff frequency is 45 Mc. in all cases. All coils, except L_4 in (B) above, are wound ½" i.d. with 8 turns per inch.

The (A) Filter
C_1, C_5—41.5 μμfd. (40 μμfd. will be found suitable.)
C_2, C_3, C_4—136 μμfd. (130 to 140 μμfd. may be used.)
L_1, L_6—0.2 μh; 3½ t. no. 14
L_2, L_5—0.3 μh; 5 t. no. 12
L_3, L_4—0.37 μh; 6½ t. no. 12

The (B) Filter with Mid-Section tuned to Channel 2 (58 Mc..)
C_1, C_5—41.5 μfd.
C_2, C_4—136 μμfd.
C_3—87 μμfd. (50 μμfd. fixed and 75 μμfd. variable in parallel.)
L_1, L_7—0.2 μh; 3½ t. no. 14
L_2, L_3, L_5, L_6—0.3 μh; 5 t. no. 12
L_4—0.09 μh; 2 t. no. 14 ½" dia. by ¼" long

The (B) Filter with Mid-Section tuned to Channel 4 (71 Mc.). All components same except that:
C_3—106 μμfd.
L_3, L_5—0.33 μh; 6 t. no. 12
L_4—0.05 μh; 1½ t. no. 14, 3/8" dia. by 3/8" long.

The (B) Filter with Mid-Section tuned to Channel 5 (81 Mc.). Change the following:
C_3—113 μμfd.
L_3, L_5—0.34 μh; 6 t. no. 12
L_4—0.033 μh; 1 t. no. 14 3/8" dia.

The (B) Filter with Mid-Section tuned to Channel 6 (86 Mc.). All components are essentially the same except that the theoretical value of L_4 is changed to 0.03 μh., and the capacitance of C_3 is changed to 117 μμfd.

available commercially from several manufacturers. Alternatively, filters in kit form are available from several manufacturers at a somewhat lower price. Effective filters may be home constructed, if the test equipment is available and if sufficient care is taken in the construction of the assembly.

Construction of Low-Pass Filters Figures 7, 8 and 9 illustrate high-performance low-pass filters which are suitable for home construction. All are constructed in slip-cover aluminum boxes (ICA no. 29110) with dimensions of 17 by 3 by 2¾ inches. Five aluminum baffle plates have been installed in the chassis to make six shielded sections within the enclosure. Feed-through bushings between the shielded sections are Johnson no. 135-55.

Both the (A) and (B) filter types are designed for a nominal cut-off frequency of 45 Mc., with a frequency of maximum rejection at about 57 Mc. as established by the terminating half-sections at each end. Characteristic impedance is 52 ohms in all cases. The alternative filter designs diagrammed in figure 7B have provision for an additional rejection trap in the center of the filter unit which may be designed to offer maximum rejection in channel 2, 4, 5, or 6, depending upon which channel is likely to be received in the area in question. The only components which must be changed when changing the frequency of the maximum rejection notch in the center of the filter unit are inductors L_3, L_4, and L_5, and capacitor C_3. A trimmer capacitor has been included as a portion of C_3 so that the frequency of maximum rejection can be tuned accurately to the desired value. Reference to figures 5 and 6 will show the amateur bands which are most likely to cause interference to specific TV channels.

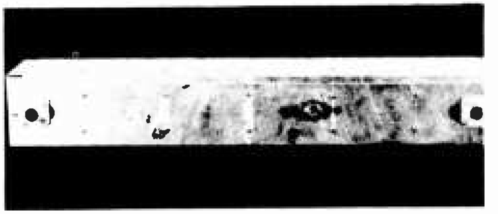


Figure 8

PHOTOGRAPH OF THE (B) FILTER WITH THE COVER IN PLACE

Either high-power or low-power components may be used in the filters diagrammed in figure 7. With the small Centralab TCZ zero-coefficient ceramic capacitors used in the filter units of figure 7A or figure 7B, power levels up to 200 watts output may be used without danger of damage to the capacitors, *provided* the filter is feeding a 52-ohm resistive load. It may be practicable to use higher levels of power with this type of ceramic capacitor in the filter, but at a power level of 200 watts on the 28-Mc. band the capacitors run just perceptibly warm to the touch. As a point of interest, it is the current rating which is of significance to the capacitors used in filters such as illustrated. Since current ratings for small capacitors such as these are not readily available, it is not possible to establish an accurate power rating for such a unit. The high-power unit illustrated in figure 9, which uses Centralab type 850S and 854S capacitors,

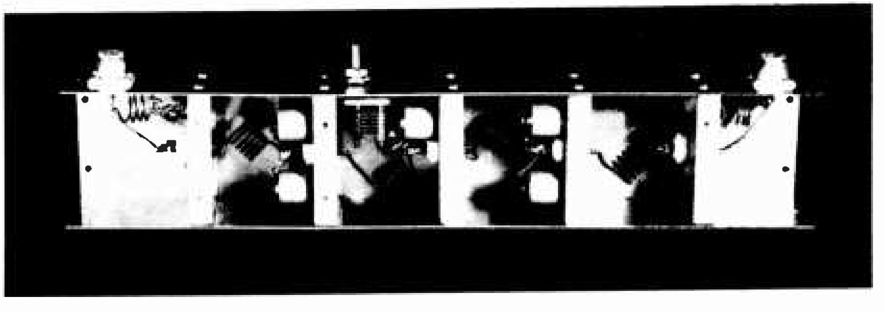


Figure 9

PHOTOGRAPH OF THE (B) FILTER WITH COVER REMOVED

The mid-section in this filter is adjusted for maximum rejection of channel 4. Note that the main coils of the filter are mounted at an angle of about 45 degrees so that there will be minimum inductive coupling from one section to the next through the holes in the aluminum partitions. Mounting the coils in this manner was found to give a measurable improvement in the attenuation characteristics of the filter.

has proven quite suitable for power levels up to one kilowatt.

Capacitors C_1, C_2, C_4, and C_5 can be standard manufactured units with normal 5 per cent tolerance. The coils for the end sections can be wound to the dimensions given (L_1, L_6, and L_7). Then the resonant frequency of the series resonant end sections should be checked with a grid-dip meter, after the adjacent input or output terminal has been shorted with a very short lead. The coils should be squeezed or spread until resonance occurs at 57 Mc.

The intermediate *m*-derived section in the filter of figure 7B may also be checked with a grid-dip meter for resonance at the correct rejection frequency, after the hot end of L_4 has been temporarily grounded with a low-inductance lead. The variable capacitor portion of C_3 can be tuned until resonance at the correct frequency has been obtained. Note that there is so little difference between the constants of this intermediate section for channels 5 and 6 that variation in the setting of C_3 will tune to either channel without materially changing the operation of the filter.

The coils in the intermediate sections of the filter (L_2, L_3, L_4, and L_5 in figure 7A, and L_2, L_3, L_5, and L_6 in figure 7B) may be checked most conveniently outside the filter unit with the aid of a small ceramic capacitor of known value and a grid-dip meter. The ceramic capacitor is paralleled across the small coil with the shortest possible leads. Then the assembly is placed atop a cardboard box and the resonant frequency checked with a grid-dip meter. A *Shure reactance slide rule* may be used to ascertain the correct resonant frequency for the desired L-C combination and the coil altered until the desired resonant frequency is attained. The coil may then be installed in the filter unit, making sure that it is not squeezed or compressed as it is being installed. However, if the coils are wound exactly as given under figure 10, the filter may be assembled with reasonable assurance that it will operate as designed.

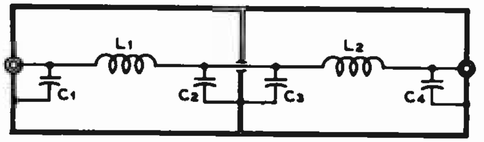


Figure 10

SCHEMATIC OF THE SINGLE-SECTION HALF-WAVE FILTER

The constants given below are for a characteristic impedance of 52 ohms, for use with RG-8/U and RG-58/U cable. Coil L_1 should be checked for resonance at the operating frequency with C_1, and the same with L_2 and C_4. This check can be made by soldering a low-inductance grounding strap to the lead between L_1 and L_2 where it passes through the shield. When the coils have been trimmed to resonance with a grid-dip meter, the grounding strap should of course be removed. This filter type will give an attenuation of about 30 db to the second harmonic, about 48 db to the third, about 60 db to the fourth, 67 to the fifth, and so on increasing at a rate of about 30 db per octave.

C_1,C_2,C_3,C_4—Silver mica or small ceramic for low power, transmitting type ceramic for high power. Capacitance for different bands is given below:
160 meters—1700 μμfd.
80 meters—850 μμfd.
40 meters—440 μμfd.
20 meters—220 μμfd.
10 meters—110 μμfd.
6 meters—60 μμfd.

L_1,L_2—May be made up of sections of B&W Miniductor for power levels below 250 watts, or of no. 12 enam. for power up to one kilowatt. Approximate dimensions for the coils are given below, but the coils should be trimmed to resonate at the proper frequency with a grid-dip meter as discussed above. All coils except the ones for 160 meters are wound 8 turns per inch.
160 meters—4.2 μh; 22 turns no. 16 enam., 1" dia. 2" long
80 meters—2.1 μh; 13 t. 1" dia. (No. 3014 Miniductor or no. 12)
40 meters—1.1 μh; 8 t. 1" dia. (No. 3014 or no. 12 at 8 t.p.i.)
20 meters—0.55 μh; 7 t. ¾" dia. (No. 3010 or no. 12 at 8 t.p.i.)
10 meters—0.3 μh; 6 t. ½" dia. (No. 3002 or no. 12 at 8 t.p.i.)
6 meters—0.17 μh; 4 t. ½" dia. (No. 3002 or no. 12 at 8 t.p.i.)

Using Low-Pass Filters The low-pass filter connected in the output transmission line of the transmitter is capable of affording an enormous degree of harmonic attenuation. However, the filter must be operated in the correct manner or the results obtained will not be up to expectations.

In the first place, all direct radiation from the transmitter and its control and power leads must be suppressed. This subject has been discussed in the previous section. Secondly, the filter must be operated into a load impedance approximately equal to its design characteristic impedance. The filter itself will have very low losses (usually less than 0.5 db) when operated into its nominal value of resistive load. But if the filter is mis-terminated its losses will become excessive, and it will not present the correct value of load impedance to the transmitter.

If a filter, being fed from a high-power transmitter, is operated into an incorrect termination it may be damaged; the coils may be overheated and the capacitors destroyed as a result of excessive r-f currents. Hence it is wise, when first installing a low-pass filter,

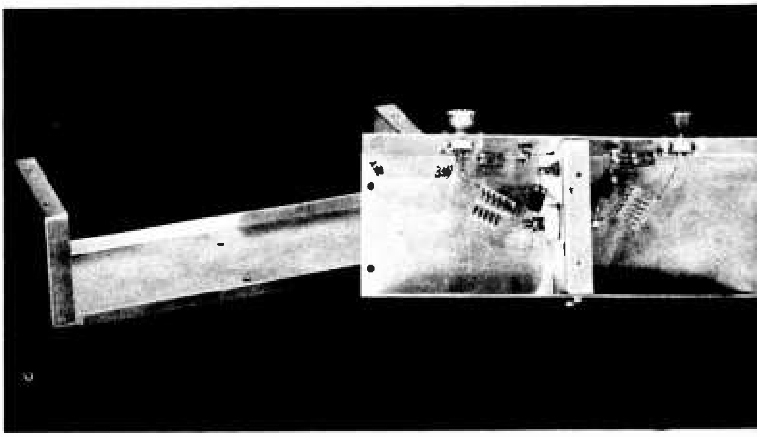


Figure 11
HALF-WAVE FILTER FOR THE 28-MC. BAND

Showing one possible type of construction of a 52-ohm half-wave filter for relatively low power operation on the 28-Mc. band.

to check the standing-wave ratio of the load being presented to the output of the filter with a standing-wave meter of any of the conventional types. Then the antenna termination or the antenna coupled should be adjusted, with low power on the transmitter, until the s.w.r. of the load being presented to the filter is less than 2.0, and preferably below 1.5.

Half-Wave Filters Half-wave filters ("Harmonikers") have been discussed in various publications including the Nov.-Dec. 1949 GE *Ham News*. Such filters are relatively simple and offer the advantage that they present the same value of impedance at their input terminals as appears as load across their output terminals. Such filters normally are used as one-band affairs, and they offer high attenuation only to the third and higher harmonics. Design data on the half-wave filter is given in figure 10. Construction of half-wave filters is illustrated in figure 11.

16-4 Broadcast Interference

Interference to the reception of signals in the broadcast band (540 to 1600 kc.) or in the FM broadcast band (88 to 108 Mc.) by amateur transmissions is a serious matter to those amateurs living in densely populated areas. Although broadcast interference has recently been overshadowed by the seriousness of television interference, the condition of BCI is still present.

In general, signals from a transmitter operating properly are not picked up by receivers tuned to other frequencies unless the receiver is of inferior design, or is in poor condition. Therefore, if the receiver is of good design and is in good repair, the burden of rectifying the trouble rests with the owner of the interfering station. Phone and c-w stations both are capable of causing broadcast interference, key-click annoyance from the code transmitters being particularly objectionable.

A knowledge of each of the several types of broadcast interference, their cause, and methods of eliminating them is necessary for the successful disposition of this trouble. An effective method of combating one variety of interference is often of no value whatever in the correction of another type. Broadcast interference seldom can be cured by "rule of thumb" procedure.

Broadcast interference, as covered in this section refers primarily to standard (amplitude modulated, 550-1600 kc.) broadcast. Interference with FM broadcast reception is much less common, due to the wide separation in frequency between the FM broadcast band and the more popular amateur bands, and due also to the limiting action which exists in all types of FM receivers. Occasional interference with FM broadcast by a harmonic of an amateur transmitter has been reported; if this condition is encountered, it may be eliminated by the procedures discussed in the first portion of this chapter under Television Interference.

The use of frequency-modulation transmission by an amateur station is likely to result in much less interference to broadcast reception than either amplitude-modulated telephony or straight keyed c.w. This is true because, insofar as the broadcast receiver is concerned, the amateur FM transmission will consist of a plain unmodulated carrier. There will be no key clicks or voice reception picked up by the b-c-l set (unless it happens to be an FM receiver which might pick up a harmonic of the signal), although there might be a slight click when the transmitter is put on or taken

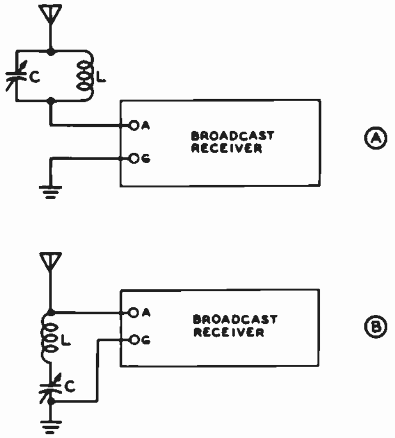


Figure 12

WAVE-TRAP CIRCUITS

The circuit at (A) is the most common arrangement, but the circuit at (B) may give improved results under certain conditions. Manufactured wave traps for the desired band of operation may be purchased or the traps may be assembled from the data given in figure 14.

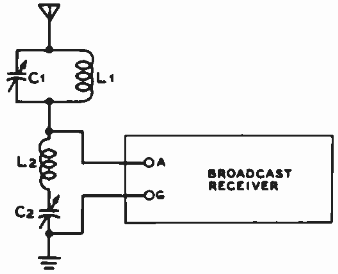


Figure 13

HIGH-ATTENUATION WAVE-TRAP CIRCUIT

The two circuits may be tuned to the same frequency for highest attenuation of a strong signal, or the two traps may be tuned separately for different bands of operation.

off the air. This is one reason why narrow-band FM has become so popular with phone enthusiasts who reside in densely populated areas.

Interference Classifications Depending upon whether it is traceable directly to causes within the *station* or within the *receiver*, broadcast interference may be divided into two main classes. For example, that type of interference due to transmitter over-modulation is at once listed as being caused by improper operation, while an interfering signal that tunes in and out with a broadcast station is probably an indication of cross modulation or image response in the receiver, and the poorly-designed input stage of the receiver is held liable. The various types of interference and recommended cures will be discussed in the following paragraphs.

Blanketing This is not a tunable effect, but a total blocking of the receiver. A more or less complete "washout" covers the entire receiver range when the carrier is switched on. This produces either a complete blotting out of all broadcast stations, or else knocks down their volume several decibels—depending upon the severity of the interference. Voice modulation of the carrier causing the blanketing will be highly distorted or even unintelligible. Keying of the carrier which produces the blanketing will cause an annoying fluctuation in the volume of the broadcast signals.

Blanketing generally occurs in the immediate neighborhood (inductive field) of a powerful transmitter, the affected area being directly proportional to the power of the transmitter. Also it is more prevalent with transmitters which operate in the 160-meter and 80-meter bands, as compared to those on the higher frequencies.

The remedies are to (1) shorten the receiving antenna and thereby shift its resonant frequency, or (2) remove it to the interior of the building, (3) change the direction of either the receiving or transmitting antenna to minimize their mutual coupling, or (4) keep the interfering signal from entering the receiver input circuit by installing a wavetrap tuned to the signal frequency (see figure 12) or a low-pass filter as shown in figure 21.

A suitable wave-trap is quite simple in construction, consisting only of a coil and midget variable capacitor. When the trap circuit is tuned to the frequency of the interfering signal, little of the interfering voltage reaches the grid of the first tube. Commercially manufactured wave-traps are available from several concerns, including the J. W. Miller Co. in Los Angeles. However, the majority of amateurs prefer to construct the traps from spare components selected from the "junk box."

The circuit shown in figure 13 is particularly effective because it consists of two traps. The shunt trap blocks or rejects the frequency to which it is tuned, while the series trap across the antenna and ground terminals of the receiver provides a very low impedance path to ground at the frequency to

BAND	COIL, L	CAPACITOR, C
1.8 Mc.	1 inch no. 30 enam. closewound on 1" form	75-μμfd. var.
3.5 Mc.	42 turns no. 30 enam. closewound on 1" form	50-μμfd. var.
7.0 Mc.	23 turns no. 24 enam. closewound on 1" form	50-μμfd. var.
14 Mc.	10 turns no. 24 enam. closewound on 1" form	50-μμfd. var.
21 Mc.	7 turns no. 24 enam. closewound on 1" form	50-μμfd. var.
28 Mc.	4 turns no. 24 enam. closewound on 1" form	25-μμfd. var.
50 Mc.	3 turns no. 24 enam. spaced ½" on 1" form	25-μμfd. var.

Figure 14
COIL AND CAPACITOR TABLE FOR AMATEUR-BAND WAVETRAPS

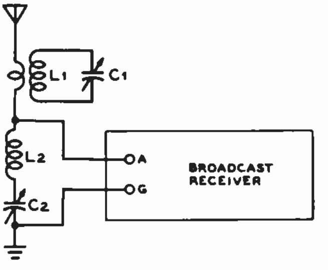


Figure 15
MODIFICATION OF THE FIGURE 13 CIRCUIT

In this circuit arrangement the parallel-tuned tank is inductively coupled to the antenna lead with a 3 to 6 turn link instead of being placed directly in series with the antenna lead.

which it is tuned and by-passes the signal to ground. In moderate interference cases, either the shunt or series trap may be used alone, while similarly, one trap may be tuned to one of the frequencies of the interfering transmitter and the other trap to a different interfering frequency. In either case, each trap is effective over but a small frequency range and must be readjusted for other frequencies.

The wave-trap must be installed as close to the receiver antenna terminal as practicable, hence it should be as small in size as possible. The variable capacitor may be a midget air-tuned trimmer type, and the coil may be wound on a 1-inch dia. form. The table of figure 14 gives winding data for wave-traps built around standard variable capacitors. For best results, both a shunt and a series trap should be employed as shown.

Figure 15 shows a two-circuit coupled wave-trap that is somewhat sharper in tuning and more efficacious. The specifications for the secondary coil L_1 may be obtained from the table of figure 14. The primary coil of the shunt trap consists of 3 to 5 closewound turns of the same size wire wound in the same direction on the same form as L_1 and separated from the latter by ¼ of an inch.

Overmodulation A carrier modulated in excess of 100 per cent acquires sharp cutoff periods which give rise to transients. These transients create a broad signal and generate spurious responses. Transients caused by overmodulation of a radio-telephone signal may at the same time bring about impact or shock excitation of nearby receiving antennas and power lines, generating interfering signals in that manner.

Broadcast interference due to overmodulation is frequently encountered. The remedy is to reduce the modulation percentage or to use a clipper-filter system or a high-level splatter suppressor in the speech circuit of the transmitter.

Cross Modulation Cross modulation or *cross talk* is characterized by the amateur signal *riding in* on top of a strong broadcast signal. There is usually no heterodyne note, the amateur signal being tuned in and out with the program carriers.

This effect is due frequently to a faulty input stage in the affected receiver. Modulation of the interfering carrier will swing the operating point of the input tube. This type of trouble is seldom experienced when a variable-μ tube is used in the input stage.

Where the receiver is too ancient to incorporate such a tube, and is probably poorly shielded at the same time, it will be better to attach a wave-trap of the type shown in figure 12 rather than to attempt rebuilding of the receiver. The addition of a good ground and a shield can over the input tube often adds to the effectiveness of the wave-trap.

Transmission via Capacitive Coupling A small amount of capacitive coupling is now widely used in receiver r.f. and antenna transformers as a gain booster at the high-frequency end of the tuning range. The coupling capacitance is obtained by means of a small loop of wire cemented close to the grid end of the secondary winding, with one end directly connected to the plate or antenna end of the primary winding. (See figure 16.)

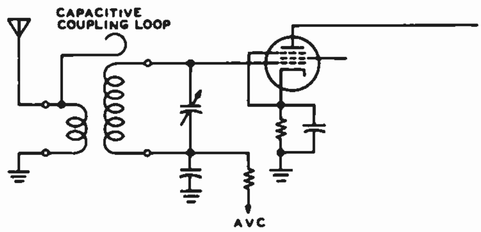


Figure 16
CAPACITIVE BOOST COUPLING CIRCUIT

Such circuits, included within the broadcast receiver to bring up the stage gain at the high-frequency end of the tuning range, have a tendency to increase the susceptibility of the receiver to interference from amateur-band transmissions.

It is easily seen that a small capacitor at this position will favor the coupling of the higher frequencies. This type of capacitive coupling in the receiver coils will tend to pass amateur high-frequency signals into a receiver tuned to broadcast frequencies.

The amount of capacitive coupling may be reduced to eliminate interference by moving the coupling turn further away from the secondary coil. However, a simple wave-trap of the type shown in figure 12, inserted at the antenna input terminal, will generally accomplish the same result and is more to be recommended than reducing the amount of capacitive coupling (which lowers the receiver gain at the high-frequency end of the broadcast band). Should the wave-trap alone not suffice, it will be necessary to resort to a reduction in the coupling capacitance.

In some simple broadcast receivers, capacitive coupling is obtained by closely coupled primary and secondary coils, or as a result of running a long primary or antenna lead close to the secondary coil of an unshielded antenna coupler.

Phantoms With two strong local carriers applied to a non-linear impedance, the beat note resulting from cross-modulation between them may fall on some frequency within the broadcast band and will be audible at that point. If such a "phantom" signal falls on a local broadcast frequency, there will be heterodyne interference as well. This is a common occurence with broadcast receivers in the neighborhood of two amateur stations, or an amateur and a police station. It also sometimes occurs when only one of the stations is located in the immediate vicinity.

As an example: an amateur signal on 3514 kc. might beat with a local 2414-kc. police carrier to produce a 1100-kc. phantom. If the two carriers are strong enough in the vicinity of a circuit which can cause rectification, the 1100-kc. phantom will be heard in the broadcast band. A poor contact between two oxidized wires can produce rectification.

Two stations must be transmitting simultaneously to produce a phantom signal; when either station goes off the air the phantom disappears. Hence, this type of interference is apt to be reported as highly intermittent and might be difficult to duplicate unless a test oscillator is used "on location" to simulate the missing station. Such interference cannot be remedied at the transmitter, and often the rectification takes place some distance from the receivers. In such occurrences it is most difficult to locate the source of the trouble.

It will also be apparent that a phantom might fall on the intermediate frequency of a simple superhet receiver and cause interference of the untunable variety if the manufacturer has not provided an i-f wave-trap in the antenna circuit.

This particular type of phantom may, in addition to causing i-f interference, generate harmonics which may be tuned in and out with heterodyne whistles from one end of the receiver dial to the other. It is in this manner that *birdies* often result from the operation of nearby amateur stations.

When one component of a phantom is a steady, unmodulated carrier, only the intelligence present on the other carrier is conveyed to the broadcast receiver.

Phantom signals almost always may be identified by the suddenness with which they are interrupted, signalizing withdrawal of one party to the union. This is especially baffling to the inexperienced interference-locater, who observes that the interference suddenly disappears, even though his own transmitter remains in operation.

If the mixing or rectification is taking place in the receiver itself, a phantom signal may be eliminated by removing either one of the contributing signals from the receiver input circuit. A wave-trap of the type shown in figure 12, tuned to either signal, will do the trick. If the rectification is taking place outside the receiver, the wave-trap should be tuned to the frequency of the phantom, instead of to one of its components. I-f wave-traps may be built around a 2.5-millihenry r-f choke as the inductor, and a compression-type mica padding capacitor. The capacitor should have a capacitance range of 250–525 $\mu\mu$fd. for the 175- and 206-kc. intermediate frequencies; 65–175 $\mu\mu$fd. for 260-kc. and other intermediates lying between 250- and 400-kc; and 17–80 $\mu\mu$fd. for 456-, 465-, 495-, and 500-kc. Slightly more capacitance will be required for resonance with a 2.1 millihenry choke.

Spurious Emissions This sort of interference arises from the transmitter itself. The radiation of any signal (other than the intended carrier frequency) by an amateur station is prohibited by FCC regulations. Spurious radiation may be traced to imperfect neutralization, parasitic oscillations in the r-f or modulator stages, or to "broadcast-band" variable-frequency oscillators or e.c.o.'s.

Low-frequency parasitics may actually occur on broadcast frequencies or their near subharmonics, causing direct interference to programs. An all-wave monitor operated in the vicinity of the transmitter will detect these spurious signals.

The remedy will be obvious in individual cases. Elsewhere in this book are discussed methods of complete neutralization and the suppression of parasitic oscillations in r-f and audio stages.

A-c/d-c Receivers Inexpensive table-model a-c/d-c receivers are particularly susceptible to interference from amateur transmissions. In fact, it may be said with a fair degree of assurance that the majority of BCI encountered by amateurs operating in the 1.8-Mc. to 29-Mc. range is a result of these inexpensive receivers. In most cases the receivers are at fault; but this does not absolve the amateur of his responsibility in attempting to eliminate the interference.

Stray Receiver Rectification In most cases of interference to inexpensive receivers, particularly those of the a-c/d-c type, it will be found that stray receiver rectification is causing the trouble. The offending stage usually will be found to be a high-mu triode as the first audio stage following the second detector. Tubes of this type are quite non-linear in their grid characteristic, and hence will readily rectify any r-f signal appearing between grid and cathode. The r-f signal may get to the tube as a result of direct signal pickup due to the lack of shielding, but more commonly will be fed to the tube from the power line as a result of the series heater string.

The remedy for this condition is simply to insure that the cathode and grid of the high-mu audio tube (usually a 12SQ7 or equivalent) are at the same r-f potential. This is accomplished by placing an r-f by-pass capacitor with the shortest possible leads directly from grid to cathode, and then adding an impedance in the lead from the volume control to the grid of the audio tube. The impedance may be an amateur band r-f choke (such as a National R-100U) for best results, but for a majority of cases it will be found that a 47,000-ohm ½-watt resistor in series with this lead will give satisfactory operation. Suitable circuits for such an operation on the receiver are given in figure 17.

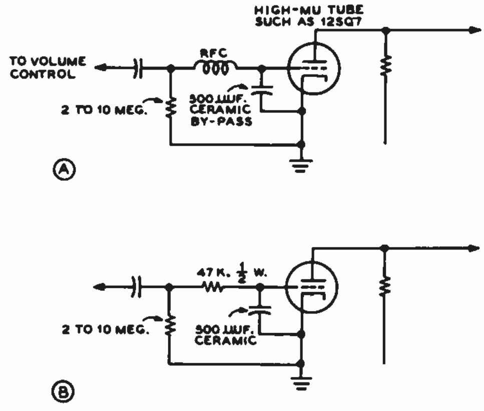


Figure 17

CIRCUITS FOR ELIMINATING AUDIO-STAGE RECTIFICATION

In many a.c.-d.c. receivers there is no r-f by-pass included across the plate supply rectifier for the set. If there is an appreciable level of r-f signal on the power line feeding the receiver, r-f rectification in the power rectifier of the receiver can cause a particularly bad type of interference which may be received on other broadcast receivers in the vicinity in addition to the one causing the rectification. The soldering of a 0.01-μfd. disc ceramic capacitor directly from anode to cathode of the power rectifier (whether it is of the vacuum-tube or selenium-rectifier type) usually will by-pass the r-f signal across the rectifier and thus eliminate the difficulty.

"Floating" Volume Control Shafts Several sets have been encountered where there was only a slightly interfering signal; but, upon placing one's hand up to the volume control, the signal would greatly increase. Investigation revealed that the volume control was installed with its shaft insulated from ground. The control itself was connected to a critical part of a circuit, in many instances to the grid of a high-gain audio stage. The cure is to install a volume control with *all* the terminals insulated from the shaft, and then to ground the shaft.

BAND	COIL, L	CAPACITOR, C
3.5 Mc.	17 turns no. 14 enameled 3-inch diameter 2¼-inch length	100-$\mu\mu$fd. variable
7.0 Mc.	11 turns no. 14 enameled 2½-inch diameter 1½-inch length	100-$\mu\mu$fd. variable
14 and 21 Mc.	4 turns no. 10 enameled 3-inch diameter 1⅛-inch length	100-$\mu\mu$fd. variable
27 and 28 Mc.	3 turns ¼-inch o.d. copper tubing 2-inch diameter 1-inch length	100-$\mu\mu$fd. variable

Figure 18

COIL AND CAPACITOR TABLE FOR A-C LINE TRAPS

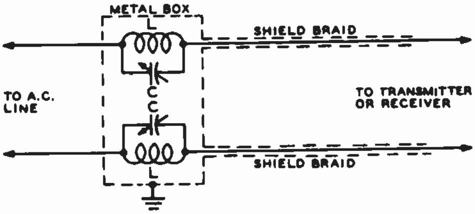


Figure 19

RESONANT POWER-LINE WAVE-TRAP CIRCUIT

The resonant type of power-line filter is more effective than the more conventional "brute force" type of line filter, but requires tuning to the operating frequency of the transmitter.

Power-Line Pickup When radio-frequency energy from a radio transmitter enters a broadcast receiver through the a-c power lines, it has either been fed back into the lighting system by the offending transmitter, or picked up from the air by over-head power lines. Underground lines are seldom responsible for spreading this interference.

To check the path whereby the interfering signals reach the line, it is only necessary to replace the transmitting antenna with a dummy antenna and adjust the transmitter for maximum output. If the interference then ceases, overhead lines have been picking up the energy. The trouble can be cleared up by installing a wave-trap or a commercial line filter in the power lines at the receiver. If the receiver is reasonably close to the transmitter, it is very doubtful that changing the direction of the transmitting antenna to right angles with the overhead lines will eliminate the trouble.

If, on the contrary, the interference continues when the transmitter is connected to the dummy antenna, radio-frequency energy is being fed directly into the power line by the transmitter, and the station must be inspected to determine the cause.

One of the following reasons for the trouble will usually be found: (1) the r-f stages are not sufficiently bypassed and/or choked, (2) the antenna coupling system is not performing efficiently, (3) the power transformers have no electrostatic shields; or, if shields are present, they are ungrounded, (4) power lines are running too close to an antenna or r-f circuits carrying high currents. If none of these causes apply, wave-traps must be installed in the power lines at the transmitter to remove r-f energy passing back into the lighting system.

The wave-traps used in the power lines at transmitter or receiver must be capable of passing relatively high current. The coils are accordingly wound with heavy wire. Figure 18 lists the specifications for power line wave-trap coils, while figure 19 illustrates the method of connecting these wave-traps. Observe that these traps are enclosed in a shield box of heavy iron or steel, well grounded.

All-Wave Receivers Each complete-coverage home receiver is a potential source of annoyance to the transmitting amateur. The novice short-wave broadcast-listener who tunes in an amateur station often considers it an interfering signal, and complains accordingly.

Neither selectivity nor image rejection in most of these sets is comparable to those properties in a communication receiver. The result is that an amateur signal will occupy too much dial space and appear at more than one point, giving rise to interference on adjacent channels and distant channels as well.

If carrier-frequency harmonics are present in the amateur transmission, serious interference will result at the all-wave receiver. The harmonics may, if the carrier frequency has been so unfortunately chosen, fall directly upon a favorite short-wave broadcast station and arouse warranted objection.

The amateur is apt to be blamed, too, for transmissions for which he is not responsible, so great is the public ignorance of short-wave allocations and signals. Owners of all-wave receivers have been quick to ascribe to amateur stations all signals they hear from tape machines and V-wheels, as well as stray tones and heterodyne flutters.

The amateur cannot be held responsible when his carrier is deliberately tuned in on an all-wave receiver. Neither is he accountable for the width of his signal on the receiver dial, or for the strength of image repeat points, if it can be proven that the receiver design does not afford good selectivity and image rejection.

If he so desires, the amateur (or the owner of the receiver) might sharpen up the received signal somewhat by shortening the receiving antenna. Set retailers often supply quite a sizeable antenna with all-wave receivers, but most of the time these sets perform almost as well with a few feet of inside antenna.

The amateur *is* accountable for harmonics of his carrier frequency. Such emissions are unlawful in the first place, and he must take all steps necessary to their suppression. Practical suggestions for the elimination of harmonics have been given earlier in this chapter under Television Interference.

Image Interference In addition to those types of interference already discussed, there are two more which are common to superhet receivers. The prevalence of these types is of great concern to the amateur, although the responsibility for their existence more properly rests with the broadcast receiver.

The mechanism whereby image production takes place may be explained in the following manner: when the first detector is set to the frequency of an incoming signal, the high-frequency oscillator is operating on another frequency which differs from the signal by the number of kilocycles of the intermediate frequency. Now, with the setting of these two stages undisturbed, there is another signal which will beat with the high-frequency oscillator to produce an i-f signal. This other signal is the so-called *image,* which is separated from the desired signal by twice the intermediate frequency.

Thus, in a receiver with 175-kc. i.f., tuned to 1000 kc.: the h-f oscillator is operating on 1175 kc., and a signal on 1350 kc. (1000 kc. plus 2 x 175 kc.) will beat with this 1175 kc. oscillator frequency to produce the 175-kc. i-f signal. Similarly, when the same receiver is tuned to 1400 kc., an amateur signal on 1750 kc. can come through.

If the image appears only a few cycles or kilocycles from a broadcast carrier, heterodyne interference will be present as well. Otherwise, it will be tuned in and out in the manner of a station operating in the broadcast band. Sharpness of tuning will be comparable to that of broadcast stations producing the same a-v-c voltage at the receiver.

The second variety of superhet interference is the result of harmonics of the receiver h-f oscillator beating with amateur carriers to produce the intermediate frequency of the receiver. The amateur transmitter will always be found to be on a frequency equal to some harmonic of the receiver h-f oscillator, *plus or minus the intermediate frequency.*

As an example: when a broadcast superhet with 465-kc. i.f. is tuned to 1000 kc., its high-frequency oscillator operates on 1465 kc. The third harmonic of this oscillator frequency is 4395 kc., which will beat with an amateur signal on 3930 kc. to send a signal through the i-f amplifier. The 3930 kc. signal would be tuned in at the 1000-kc. point on the dial.

Some oscillator harmonics are so related to amateur frequencies that more than one point of interference will occur on the receiver dial. Thus, a 3500-kc. signal may be tuned in at six points on the dial of a nearby broadcast superhet having 175 kc. i.f. and no r-f stage.

Insofar as remedies for image and harmonic superhet interference are concerned, it is well to remember that *if* the amateur signal did not in the first place reach the input stage of the receiver, the annoyance would not have been created. It is therefore good policy to try to eliminate it by means of a wave-trap or low-pass filter. Broadcast superhets are not always the acme of good shielding, however, and the amateur signal is apt to enter the circuit through channels other than the input circuit. If a wave-trap or filter will not cure the trouble, the only alternative will be to attempt

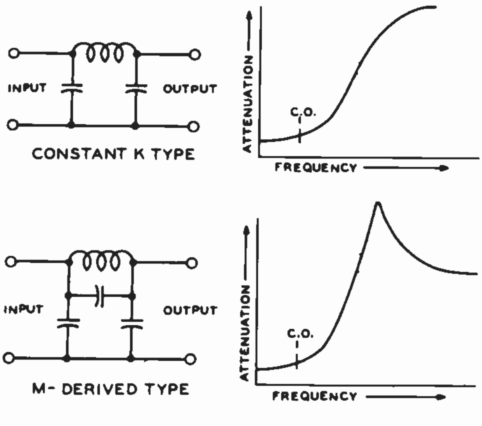


Figure 20

TYPES OF LOW-PASS FILTERS

Filters such as these may be used in the circuit between the antenna and the input of the receiver.

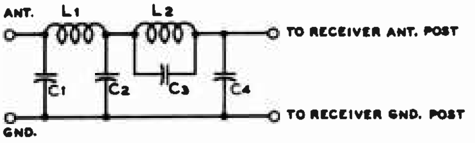


Figure 21
COMPOSITE LOW-PASS FILTER CIRCUIT

This filter is highly effective in reducing broadcast interference from all high frequency stations, and requires no tuning. Constants for 400 ohm terminal impedance and 1600 kc. cutoff are as follows: L_1, 65 turns no. 22 d.c.c. closewound on 1½ in. dia. form. L_2, 41 turns ditto, not coupled to L_1. C_1, 250 μμfd. fixed mica capacitor. C_2, 400 μμfd. fixed mica capacitor. C_3 and C_4, 150 μμfd. fixed mica capacitors, former of 5% tolerance. With some receivers, better results will be obtained with a 200 ohm carbon resistor inserted between the filter and antenna post on the receiver. With other receivers the effectiveness will be improved with a 600 ohm carbon resistor placed from the antenna post to the ground post on the receiver. The filter should be placed as close to the receiver terminals as possible.

to select a transmitter frequency such that neither image nor harmonic interference will be set up on favorite stations in the susceptible receivers. The equation given earlier may be used to determine the proper frequencies.

Low Pass Filters The greatest drawback of the wave-trap is the fact that it is a single-frequency device; i.e.—it may be set to reject at one time only one frequency (or, at best, an extremely narrow band of frequencies). Each time the frequency of the interfering transmitter is changed, every wave-trap tuned to it must be retuned. A much more satisfactory device is the *wave filter* which requires no tuning. One type, the low-pass filter, passes all frequencies below one critical frequency, and eliminates all higher frequencies. It is this property that makes the device ideal for the task of removing amateur frequencies from broadcast receivers.

A good low-pass filter designed for maximum attenuation around 1700 kc. will pass all broadcast carriers, but will reject signals originating in any amateur band. Naturally such a device should be installed only in standard broadcast receivers, never in all-wave sets.

Two types of low-pass filter sections are shown in figure 20. A composite arrangement comprising a section of each type is more effective than either type operating alone. A composite filter composed of one K-section and one shunt-derived M-section is shown in figure 21, and is highly recommended. The M-section is designed to have maximum attenuation at 1700 kc., and for that reason C_3 should be of the "close tolerance" variety. Likewise, C_3 should not be stuffed down inside L_2 in the interest of compactness, as this will alter the inductance of the coil appreciably, and likewise the resonant frequency.

If a fixed 150 μμfd. mica capacitor of 5 per cent tolerance is not available for C_1, a compression trimmer covering the range of 125–175 μμfd. may be substituted and adjusted to give maximum attenuation at about 1700 kc.

CHAPTER SEVENTEEN

Transmitter Keying and Control

17-1 Power Systems

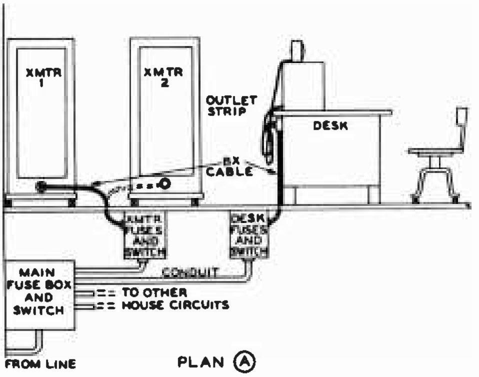
It is probable that the average amateur station that has been in operation for a number of years will have at least two transmitters available for operation on different frequency bands, at least two receivers or one receiver and a converter, at least one item of monitoring or frequency measuring equipment and probably two, a v.f.o., a speech amplifier, a desk light, and a clock. In addition to the above 8 or 10 items, there must be an outlet available for a soldering iron and there should be one or two additional outlets available for plugging in one or two pieces of equipment which are being worked upon.

It thus becomes obvious that 10 or 12 outlets connected to the 115-volt a-c line should be available at the operating desk. It may be practicable to have this number of outlets installed as an outlet strip along the baseboard at the time a new home is being planned and constructed. Or it might be well to install the outlet strip on the operating desk so as to have the flexibility of moving the operating desk from one position to another. Alternatively, the outlet strip might be wall mounted just below the desk top.

Power Drain Per Outlet When the power drain of all the items of equipment, other than transmitters, used at the operating position is totalled, you probably will find that 350 to 600 watts will be required. Since the usual home outlet is designed to handle only about 600 watts maximum, the transmitter, unless it is of relatively low power, should be powered from another source. This procedure is desirable in any event so that the voltage supplied to the receiver, frequency control, and frequency monitor will be substantially constant with the transmitter on or off the air.

So we come to two general alternative plans with their variations. Plan (A) is the more desirable and also the most expensive since it involves the installation of two separate lines from the meter box to the operating position either when the house is constructed or as an alteration. One line, with its switch, is for the transmitters and the other line and switch is for receivers and auxiliary equipment. Plan (B) is the more practicable for the average amateur, but its use requires that all cords be removed from the outlets whenever the station is not in use in order to comply with the electrical codes.

Figure 1 shows a suggested arrangement for carrying out Plan (A). In most cases an installation such as this will require approval of the plans by the city or county electrical inspector. Then the installation itself will also require inspection after it has been completed. It will be necessary to use approved outlet boxes at the rear of the transmitter where the cable is connected, and also at the operating bench where the other BX cable connects to the outlet strip. Also, the connectors at the rear of the transmitter will have to be of an approved



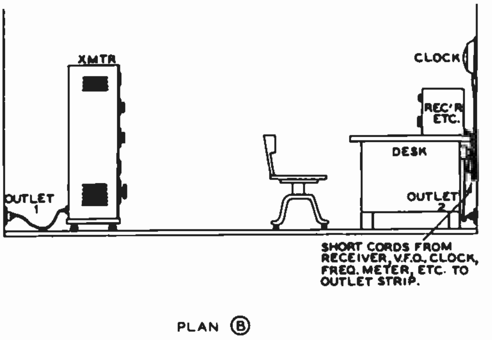


Figure 1

THE PLAN (A) POWER SYSTEM

A-c line power from the main fuse box in the house is run separately to the receiving equipment and to the transmitting equipment. Separate switches and fuse blocks then are available for the transmitters and for the auxiliary equipment. Since the fuses in the boxes at the operating room will be in series with those at the main fuse box, those in the operating room should have a lower rating than those at the main fuse box. Then it will always be possible to replace blown fuses without leaving the operating room. The fuse boxes can conveniently be located alongside one another on the wall of the operating room.

Figure 2

THE PLAN (B) POWER SYSTEM

This system is less convenient than the (A) system, but does not require extensive rewiring of the electrical system within the house to accommodate the arrangement. Thus it is better for a temporary or semi-permanent installation. In most cases it will be necessary to run an extra conduit from the main fuse box to the outlet from which the transmitter is powered, since the standard arrangement in most houses is to run all the outlets in one room (and sometimes all in the house) from a single pair of fuses and leads.

type. It is possible also that the BX cable will have to be permanently affixed to the transmitter with the connector at the fuse-box end. These details may be worked out in advance with the electrical inspector for your area.

The general aspects of Plan (B) are shown in figure 2. The basic difference between the two plans is that (A) represents a *permanent* installation even though a degree of mobility is allowed through the use of BX for power leads, while plan (B) is definitely a *temporary* type of installation as far as the electrical inspector is concerned. While it will be permissible in most areas to leave the transmitter cord plugged into the outlet even though it is turned off, the Fire Insurance Underwriters codes will make it necessary that the cord which runs to the group of outlets at the back of the operating desk be removed whenever the equipment is not actually in use.

Whether the general aspects of plans (A) or (B) are used it will be necessary to run a number of control wires, keying and audio leads, and an excitation cable from the operating desk to the transmitter. Control and keying wires can best be grouped into a multiple-wire rubber-covered cable between the desk and the transmitter. Such an arrangement gives a good appearance, and is particularly practical if cable connectors are used at each end. High-level audio at a moderate impedance level (600 ohms or below) may be run in the same control cable as the other leads. However, low-level audio can best be run in a small coaxial cable. Small coaxial cable such as RG-58/U or RG-59/U also is quite satisfactory and quite convenient for the signal from the v.f.o. to the r-f stages in the transmitter. Coaxial-cable connectors of the UG series are quite satisfactory for the terminations both for the v-f-o lead and for any low-level audio cables.

Checking an Outlet with a Heavy Load To make sure that an outlet will stand the full load of the entire transmitter, plug in an electric heater rated at about 50 per cent greater wattage than the power you expect to draw from the line. If the line voltage does not drop more than 5 volts (assuming a 117-volt line) under load and the wiring does not overheat, the wiring is adequate to supply the transmitter. About 600 watts total drain is the maximum that should be drawn from a 117-volt *lighting* outlet or circuit. For greater power, a separate pair of heavy conductors should be run right from the meter box. For a 1-kw. phone transmitter the total drain is so great that a 230-volt "split" system ordinarily will be required. Most of the newer homes are wired with this system, as are homes utilizing electricity for cooking and heating.

With a three-wire system, be sure there is no fuse in the neutral wire at the fuse box. A neutral fuse is not required if both "hot" legs are fused, and, should a neutral fuse blow, there is a chance that damage to the radio transmitter will result.

If you have a high power transmitter and do a lot of operating, it is a good idea to check on your local power rates if you are on a straight *lighting* rate. In some cities a lower rate can be obtained (but with a higher "minimum") if electrical equipment such as an electric heater drawing a specified amount of current is permanently wired in. It is not required that you use this equipment, merely that it be permanently wired into the electrical system. Naturally, however, there would be no saving unless you expect to occupy the same dwelling for a considerable length of time.

Outlet Strips The *outlet strips* which have been suggested for installation in the baseboard or for use on the rear of a desk are obtainable from the large electrical supply houses. If such a house is not in the vicinity it is probable that a local electrical contractor can order a suitable type of strip from one of the supply house catalogs. These strips are quite convenient in that they are available in varying lengths with provision for inserting a-c line plugs throughout their length. The a-c plugs from the various items of equipment on the operating desk then may be inserted in the outlet strip throughout its length. In many cases it will be desirable to reduce the equipment cord lengths so that they will plug neatly into the outlet strip without an excess to dangle behind the desk.

Contactors and Relays The use of power-control contactors and relays often will add considerably to the operating convenience of the station installation. The most practicable arrangement usually is to have a main a-c line switch on the front of the transmitter to apply power to the filament transformers and to the power control circuits. It also will be found quite convenient to have a single a-c line switch on the operating desk to energize or cut the power from the outlet strip on the rear of the operating desk. Through the use of such a switch it is not necessary to remember to switch off a large number of separate switches on each of the items of equipment on the operating desk. The alternative arrangement, and that which is approved by the Underwriters, is to remove the plugs from the wall both for the transmitter and for the operating-desk outlet strip when a period of operation has been completed.

While the insertion of plugs or operation of switches usually will be found best for applying the a-c line power to the equipment, the changing over between transmit and receive can best be accomplished through the use of relays. Such a system usually involves three relays, or three groups of relays. The relays and their functions are: (1) power control relay for the transmitter—applies 115-volt line to the primary of the high-voltage transformer and turns on the exciter; (2) control relay for the receiver—makes the receiver inoperative by any one of a number of methods when closed, also may apply power to the v.f.o. and to a keying or a phone monitor; and (3) the antenna changeover relay—connects the antenna to the transmitter when the transmitter is energized and to the receiver when the transmitter is not operating. Several circuits illustrating the application of relays to such control arrangements are discussed in the paragraphs to follow in this chapter.

Controlling Transmitter Power Output It is necessary, in order to comply with FCC regulations, that transmitter power output be limited to the minimum amount necessary to sustain communication. This requirement may be met in several ways. Many amateurs have two transmitters; one is capable of relatively high power output for use when calling, or when interference is severe, and the other is capable of considerably less power output. In many cases the lower powered transmitter acts as the exciter for the higher powered stage when full power output is required. But the majority of the amateurs using a high powered equipment have some provision for reducing the plate voltage on the high-level stages when rednced power output is desired.

One of the most common arrangements for obtaining two levels of power output involves the use of a plate transformer having a double primary for the high-voltage power supply. The majority of the high-power plate transformers of standard manufacture have just such a dual-primary arrangement. The two primaries are designed for use with either a 115-volt or 230-volt line. When such a transformer is to be operated from a 115-volt line, operation of both

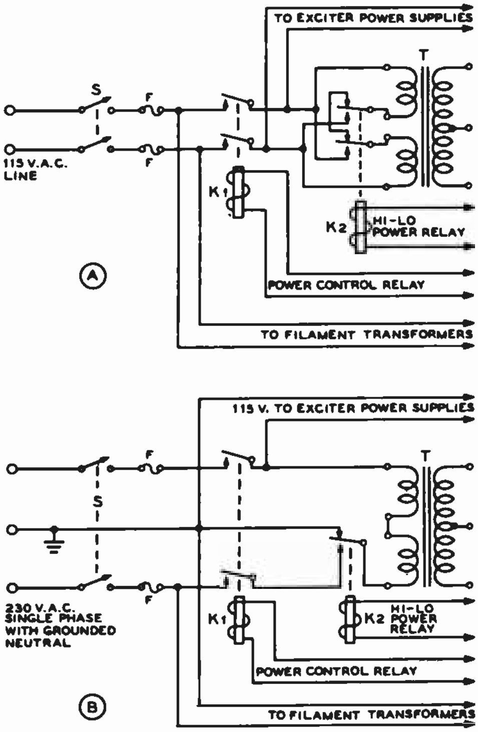


Figure 3

FULL-VOLTAGE/HALF-VOLTAGE POWER CONTROL SYSTEMS

The circuit at (A) is for use with a 115-volt a-c line. Transformer T is of the standard type having two 115-volt primaries; these primaries are connected in series for half-voltage output when the power control relay K_1 is energized but the hi-lo relay K_2 is not operated. When both relays are energized the full output voltage is obtained. At (B) is a circuit for use with a standard 230-volt residence line with grounded neutral. The two relays control the output of the power supplies the same as at (A).

primaries in parallel will deliver full output from the plate supply. Then when the two primaries are connected in series and still operated from the 115-volt line the output voltage from the supply will be reduced approximately to one half. In the case of the normal class C amplifier, a reduction in plate voltage to one half will reduce the power input to the stage to one quarter.

If the transmitter is to be operated from a 230-volt line, the usual procedure is to operate the filaments from one side of the line, the low-voltage power supplies from the other side, and the primaries of the high-voltage transformer across the whole line for full power output. Then when reduced power output is required, the primary of the high-voltage plate transformer is operated from one side to center tap rather than across the whole line. This procedure places 115 volts across the 230-volt winding the same as in the case discussed in the previous paragraph. Figure 3 illustrates the two standard methods of power reduction with a plate transformer having a double primary; (A) shows the connections for use with a 115-volt line and (B) shows the arrangement for a 230-volt a-c power line to the transmitter.

The full-voltage/half-voltage methods for controlling the power input to the transmitter, as just discussed, are subject to the limitation that only two levels of power input (full power and quarter power) are obtainable. In many cases this will be found to be a limitation to flexibility. When tuning the transmitter, the antenna coupling network, or the antenna system itself it is desirable to be able to reduce the power input to the final stage to a relatively low value. And it is further convenient to be able to vary the power input continuously from this relatively low input up to the full power capabilities of the transmitter. The use of a variable-ratio auto-transformer in the circuit from the line to the primary of the plate transformer will allow a continuous variation in power input from zero to the full capability of the transmitter.

Variable-Ratio Auto-Transformers There are several types of variable-ratio auto-transformers available on the market. Of these, the most common are the *Variac* manufactured by the General Radio Company, and the *Powerstat* manufactured by the Superior Electric Company. Both these types of variable-ratio transformers are excellently constructed and are available in a wide range of power capabilities. Each is capable of controlling the line voltage from zero to about 15 per cent above the nominal line voltage. Each manufacturer makes a single-phase unit capable of handling an output power of about 175 watts, one capable of about 750 to 800 watts, and a unit capable of about 1500 to 1800 watts. The maximum power-output capability of these units is available only at approximately the nominal line voltage, and must be reduced to a maximum current limitation when the output voltage is somewhat above or below the input line voltage. This, however, is not an important limitation for this type of application since the output voltage seldom will be raised above the line voltage, and when the output voltage is reduced below the line voltage the input to the transmitter is reduced accordingly.

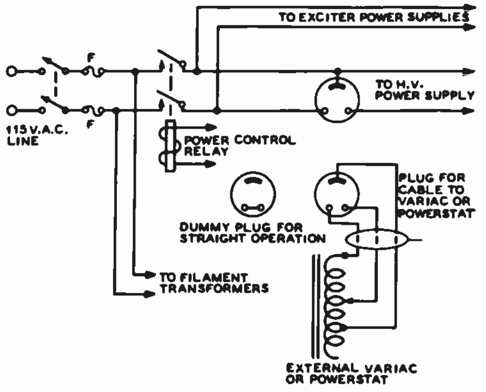


Figure 4

CIRCUIT WITH VARIABLE-RATIO AUTO-TRANSFORMER

When the dummy plug is inserted into the receptacle on the equipment, closing of the power control relay will apply full voltage to the primaries. With the cable from the Variac or Powerstat plugged into the socket the voltage output of the high-voltage power supply may be varied from zero to about 15 per cent above normal.

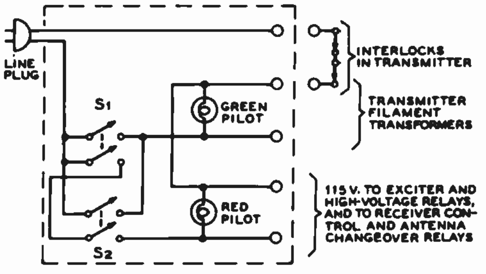


Figure 5

PROTECTIVE CONTROL CIRCUIT

With this circuit arrangement either switch may be closed first to light the heaters of all tubes and the filament pilot light. Then when the second switch is closed the high voltage will be applied to the transmitter and the red pilot will light. With a 30-second delay between the closing of the first switch and the closing of the second, the rectifier tubes will be adequately protected. Similarly, the opening of either switch will remove plate voltage from the rectifiers while the heaters remain lighted.

One convenient arrangement for using a Variac or Powerstat in conjunction with the high-voltage transformer of a transmitter is illustrated in figure 4. In this circuit a heavy three-wire cable is run from a plug on the transmitter to the Variac or Powerstat. The Variac or Powerstat then is installed so that it is accessible from the operating desk so that the input power to the transmitter may be controlled during operation. If desired, the cable to the Variac or Powerstat may be unplugged from the transmitter and a dummy plug inserted in its place. With the dummy plug in place the transmitter will operate at normal plate voltage. This arrangement allows the transmitter to be wired in such a manner that an external Variac or Powerstat may be used if desired, even though the unit is not available at the time that the transmitter is constructed.

Notes on the Use of the Variac or Powerstat Plate voltage to the modulators may be controlled at the same time as the plate voltage to the final amplifier is varied if the modulator stage uses beam tetrode tubes; variation in the plate voltage on such tubes used as modulators causes only a moderate change in the standing plate current. Since the final amplifier plate voltage is being controlled simultaneously with the modulator plate voltage, the conditions of impedance match will not be seriously upset. In several high power transmitters using this system, and using beam-tetrode modulator tubes, it is possible to vary the plate input from about 50 watts to one kilowatt without a change other than a slight increase in audio distortion at the adjustment which gives the lowest power output from the transmitter.

With triode tubes as modulators it usually will be found necessary to vary the grid bias at the same time that the plate voltage is changed. This will allow the tubes to be operated at approximately the same relative point on their operating characteristic when the plate voltage is varied. When the modulator tubes are operated with zero bias at full plate voltage, it will usually be possible to reduce the modulator voltage along with the voltage on the modulated stage, with no apparent change in the voice quality. However, it will be necessary to reduce the audio gain at the same time that the plate voltage is reduced.

17-2 Transmitter Control Methods

Almost everyone, when getting a new trans-

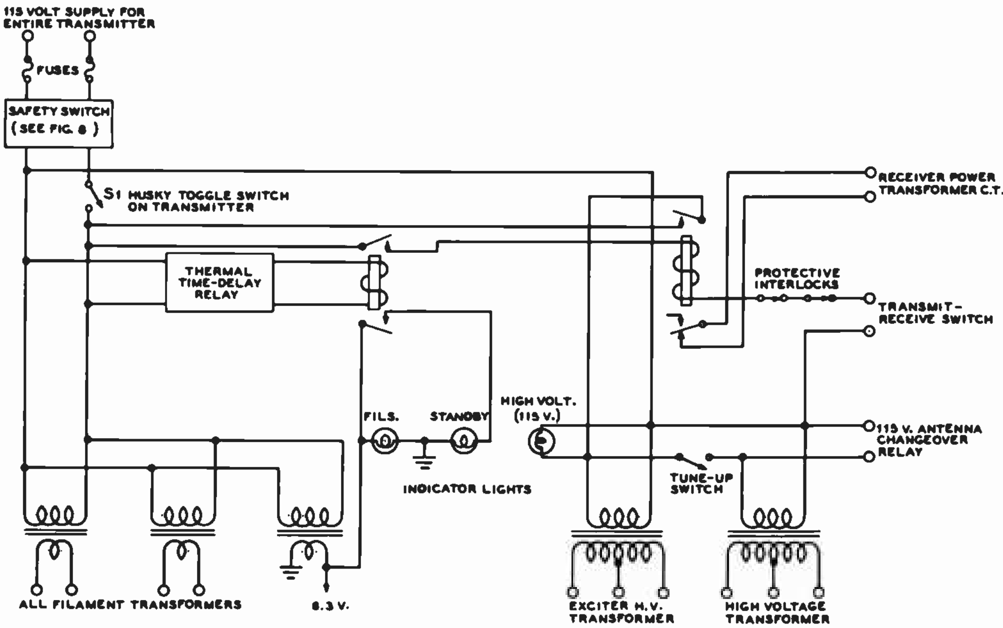


Figure 6

TRANSMITTER CONTROL CIRCUIT

Closing S_1 lights all filaments in the transmitter and starts the time-delay relay in its cycle. When the time-delay relay has operated, closing the transmit-receive switch at the operating position will apply plate power to the transmitter and disable the receiver. A tune-up switch has been provided so that the exciter stages may be tuned without plate voltage on the final amplifier.

mitter on the air, has had the experience of having to throw several switches and pull or insert a few plugs when changing from receive to transmit. This is one extreme in the direction of how *not* to control a transmitter. At the other extreme we find systems where it is only necessary to speak into the microphone or touch the key to change both transmitter and receiver over to the transmit condition. Most amateur stations are intermediate between the two extremes in the control provisions and use some relatively simple system for transmitter control.

In figure 5 is shown an arrangement which protects mercury-vapor rectifiers against premature application of plate voltage without resorting to a time-delay relay. No matter which switch is thrown first, the filaments will be turned on first and off last. However, double-pole switches are required in place of the usual single-pole switches.

When assured time delay of the proper interval and greater operating convenience are desired, a group of inexpensive a-c relays may be incorporated into the circuit to give a control circuit such as is shown in figure 6. This arrangement uses a 115-volt thermal (or motor-operated) time-delay relay and a d-p-d-t 115-volt control relay. Note that the protective interlocks are connected in series with the coil of the relay which applies high voltage to the transmitter. A tune-up switch has been included so that the transmitter may be tuned up as far as the grid circuit of the final stage is concerned before application of high voltage to the final amplifier. Provisions for operating an antenna-changeover relay and for cutting the plate voltage to the receiver when the transmitter is operating have been included.

A circuit similar to that of figure 6 but incorporating push-button control of the transmitter is shown in figure 7. The circuit features a set of START-STOP and TRANSMIT-RECEIVE buttons at the transmitter and a separate set at the operating position. The control push buttons operate independently so that either set may be used to control the transmitter. It is only necessary to push the START

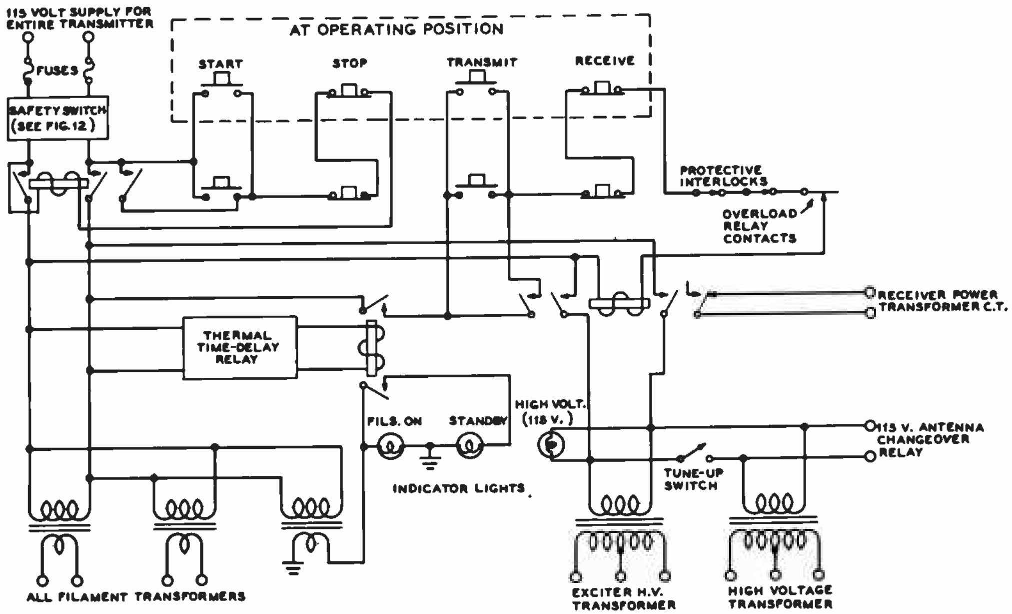


Figure 7

PUSH-BUTTON TRANSMITTER-CONTROL CIRCUIT

Pushing the START button either at the transmitter or at the operating position will light all filaments and start the time-delay relay in its cycle. When the cycle has been completed, a touch of the TRANSMIT button will put the transmitter on the air and disable the receiver. Pushing the RECEIVE button will disable the transmitter and restore the receiver. Pushing the STOP button will instantly drop the entire transmitter from the a-c line. If desired, a switch may be placed in series with the lead from the RECEIVE button to the protective interlocks; opening the switch will make it impossible for any person accidentally to put the transmitter on the air. Various other safety provisions, such as the protective-interlock arrangement described in the text have been incorporated.

With the circuit arrangement shown for the overload-relay contacts, it is only necessary to use a simple normally-closed d-c relay with a variable shunt across the coil of the relay. When the current through the coil becomes great enough to open the normally-closed contacts the hold-circuit on the plate-voltage relay will be broken and the plate voltage will be removed. If the overload is only momentary, such as a modulation peak or a tank flashover, merely pushing the TRANSMIT button will again put the transmitter on the air. This simple circuit provision eliminates the requirement for expensive overload relays of the mechanically-latching type, but still gives excellent overload protection.

button momentarily to light the transmitter filaments and start the time-delay relay in its cycle. When the standby light comes on it is only necessary to touch the TRANSMIT button to put the transmitter on the air and disable the receiver. Touching the RECEIVE button will turn off the transmitter and restore the receiver. After a period of operation it is only necessary to touch the STOP button at either the transmitter or the operating position to shut down the transmitter. This type of control arrangement is called an electrically-locking push-to-transmit control system. Such systems are frequently used in industrial electronic control.

17-3 Safety Precautions

The best way for an operator to avoid serious accidents from the high voltage supplies of a transmitter is for him to use his head, act only with deliberation, and not take unnecessary chances. However, no one is infallible, and chances of an accident are greatly lessened if certain factors are taken into consideration in the design of a transmitter, in order to protect the operator in the event of a lapse of caution. If there are too many things one must "watch out for" or keep in mind there is a good chance that sooner or later there will be a mishap; and it only takes *one*. When designing or constructing a transmitter, the following safety considerations should be given attention.

Grounds For the utmost in protection, everything of metal on the front panel of a transmitter capable of being touched by the operator should be at ground potential. This includes dial set screws, meter *zero adjuster* screws, meter cases if of metal, meter jacks, *everything* of metal protruding through the front panel or capable of being touched or *nearly* touched by the operator. This applies whether or not the panel itself is of metal. Do not rely upon the insulation of meter cases or tuning knobs for protection.

The B negative or chassis of all plate power supplies should be connected together, and to an external ground such as a waterpipe.

Exposed Wires and Components It is not necessary to resort to rack and panel construction in order to provide complete enclosure of all components and wiring of the transmitter. Even with metal-chassis construction it is possible to arrange things so as to incorporate a protective shielding housing which will not interfere with ventilation yet will prevent contact with all wires and components carrying high voltage d.c. or a.c., in addition to offering shielding action.

If everything on the front panel is at ground potential (with respect to external ground) and all units are effectively housed with protective covers, then there is no danger except when the operator must reach into the interior part of the transmitter, as when changing coils, neutralizing, adjusting coupling, or shooting trouble. The latter procedure can be made safe by making it possible for the operator to be *absolutely certain* that all voltages have been turned off and that they cannot be turned on either by short circuit or accident. This can be done by incorporation of the following system of main primary switch and safety signal lights.

Combined Safety Signal and Switch The common method of using red pilot lights to show when a circuit is *on* is useless except from an ornamental standpoint. When the red pilot is not lit it *usually* means that the circuit is turned off, but it *can* mean that the circuit is on but the lamp is burned out or not making contact.

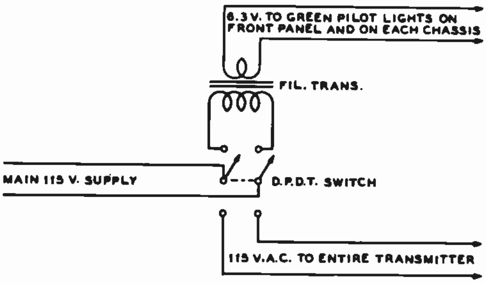


Figure 8

COMBINED MAIN SWITCH AND SAFETY SIGNAL

When shutting down the transmitter, throw the main switch to neutral. If work is to be done on the transmitter, throw the switch all the way to "pilot," thus turning on the green pilot lights on the panel and on each chassis, and insuring that no voltage can exist on the primary of any transformer, even by virtue of a short or accidental ground.

To enable you to touch the tank coils in your transmitter with absolute assurance that it is impossible for you to obtain a shock except from possible undischarged filter condensers (see following topic for elimination of this hazard), it is only necessary to incorporate a device similar to that of figure 8. It is placed near the point where the main 110-volt leads enter the room (preferably near the door) and in such a position as to be inaccessible to small children. Notice that this switch breaks *both* leads; switches that open just one lead do not afford complete protection, as it is sometimes possible to complete a primary circuit through a short or accidental ground. Breaking just one side of the line may be all right for turning the transmitter on and off, but when you are going to place an arm inside the transmitter, *both* 110-volt leads should be broken.

When you are all through working your transmitter for the time being, simply throw the main switch to neutral.

When you find it necessary to work on the transmitter or change coils, throw the switch so that the green pilots light up. These can be ordinary 6.3-volt pilot lamps behind green bezels or dipped in green lacquer. One should be placed on the front panel of the transmitter; others should be placed so as to be easily visible when changing coils or making adjustments requiring the operator to reach inside the transmitter.

For 100 per cent protection, just obey the following rule: *never work on the transmitter or reach inside any protective cover except when the green pilots are glowing.* To avoid confusion, no other green pilots should be used on the transmitter; if you want an indicator jewel to show when the filaments are lighted, use amber instead of green.

Safety Bleeders Filter capacitors of good quality hold their charge for some time, and when the voltage is more than 1000 volts it is just about as dangerous to get across an undischarged 4-μfd. filter capacitor as it is to get across a high-voltage supply that is turned on. Most power supplies incorporate bleeders to improve regulation, but as these are generally wire-wound resistors, and as wire-wound resistors occasionally open up without apparent cause, it is desirable to incorporate an auxiliary safety bleeder across each heavy-duty bleeder. Carbon resistors will not stand much dissipation and sometimes change in value slightly with age. However, the chance of their opening up when run well within their dissipation rating is very small.

To make *sure* that all capacitors are bled, it is best to short each one with an insulated screwdriver. However, this is sometimes awkward and always inconvenient. One can be virtually sure by connecting auxiliary carbon bleeders across all wire-wound bleeders used on supplies of 1000 volts or more. For every 500 volts, connect in series a 500,000-ohm 1-watt carbon resistor. The drain will be negligible (1 ma.) and each resistor will have to dissipate only 0.5 watt. Under these conditions the resistors will last indefinitely with little chance of opening up. For a 1500-volt supply, connect three 500,000-ohm resistors in series. If the voltage exceeds an integral number of 500 volt divisions, assume it is the next higher integral value; for instance, assume 1800 volts as 2000 volts and use four resistors.

Do *not* attempt to use fewer resistors by using a higher value for the resistors; not over 500 volts should appear across any single 1-watt resistor.

In the event that the regular bleeder opens up, it will take several seconds for the auxiliary bleeder to drain the capacitors down to a safe voltage, because of the very high resistance. Therefore, it is best to allow 10 or 15 seconds after turning off the plate supply before attempting to work on the transmitter.

If a 0-1 d-c milliammeter is at hand, it may be connected in series with the auxiliary bleeder to act as a high voltage voltmeter.

"Hot" Adjustments Some amateurs contend that it is almost impossible to make certain adjustments, such as coupling and neutralizing, unless the transmitter is running. The best thing to do is to make all neutralizing and coupling devices adjustable from the front panel by means of flexible control shafts which are broken with insulated couplings to permit grounding of the panel bearing.

If your particular transmitter layout is such that this is impracticable and you refuse to throw the main switch to make an adjustment—throw the main switch—take a reading—throw the main switch—make an adjustment—and so on, then protect yourself by making use of long adjusting rods made from ½-inch dowel sticks which have been wiped with oil when perfectly free from moisture.

If you are addicted to the use of pickup loop and flashlight bulb as a resonance and neutralizing indicator, then fasten it to the end of a long dowel stick and use it in that manner.

Protective Interlocks With the increasing tendency toward construction of transmitters in enclosed steel cabinets a transmitter becomes a particularly lethal device unless adequate safety provisions have been incorporated. Even with a combined safety signal and switch as shown in figure 8 it is still conceivable that some person unfamiliar with the transmitter could come in contact with high voltage. It is therefore recommended that the transmitter, wherever possible, be built into a complete metal housing or cabinet and that *all* doors or access covers be provided with protective interlocks (all interlocks must be connected in *series)* to remove the high voltage whenever these doors or covers are opened. The term "high voltage" should mean any voltage above approximately 150 volts, although it is still possible to obtain a serious burn from a 150-volt circuit under certain circumstances. The 150-volt limit usually will mean that grid-bias packs as well as high-voltage packs should have their primary circuits opened when any interlock is opened.

17-4 Transmitter Keying

The carrier from a c-w telegraph transmitter must be broken into dots and dashes for the transmission of code characters. The carrier signal is of constant amplitude while the key is closed, and is entirely removed when the key is open. When code characters are being transmitted, the carrier may be considered as being modulated by the keying. If the change from the no-output condition to full-output, or vice versa, occurs too rapidly, the rectangular pulses which form the keying characters contain high-frequency components which take up a wide frequency band as sidebands and are heard as clicks.

The cure for transient key clicks is relatively simple, although one would not believe it, judging from the hordes of clicky, "snappy" signals heard on the air.

To be capable of transmitting code characters and at the same time not splitting the eardrums of neighboring amateurs, the c-w transmitter MUST meet two important specifications.

1- It must have no parasitic oscillations either in the stage being keyed or in any succeeding stage.

2- It must have some device in the keying circuit capable of shaping the leading and trailing edge of the waveform.

Both these specifications must be met before the transmitter is capable of c-w operation. Merely turning a transmitter on and off by the haphazard insertion of a telegraph key in some power lead is an invitation to trouble.

The two general methods of keying a transmitter are those which control the excitation to the keyed amplifier, and those which control the plate or screen voltage applied to the keyed amplifier.

Key-Click Elimination Key-click elimination is accomplished by preventing a too-rapid make-and-break of power to the antenna circuit, rounding off the keying characters so as to limit the sidebands to a value which does not cause interference to adjacent channels. Too much lag will prevent fast keying, but fortunately key clicks can be practically eliminated without limiting the speed of manual (hand) keying. Some circuits which eliminate key clicks introduce too much time-lag and thereby add *tails* to the dots. These tails may cause the signals to be difficult to copy at high speeds.

Location of Keyed Stage Considerable thought should be given as to which stage in a transmitter is the proper one to key. If the transmitter is keyed in a stage close to the oscillator, the change in r-f loading of the oscillator will cause the oscillator to shift frequency with keying. This will cause the signal to have a distinct chirp. The chirp will be multiplied as many times as the frequency of the oscillator is multiplied. A chirpy oscillator that would be passable on 80 meters would be unusable on 28 Mc. c.w.

Keying the oscillator itself is an excellent way to run into keying difficulties. If no key click filter is used in the keying circuit, the transmitter will have bad key clicks. If a key click filter is used, the slow rise and decay of oscillator voltage induced by the filter action will cause a keying chirp. This action is

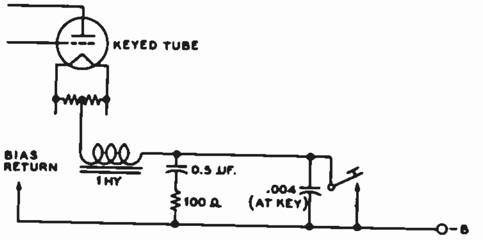


Figure 9

CENTER-TAP KEYING WITH CLICK FILTER

The constants shown above are suggested as starting values; considerable variation in these values can be expected for optimum keying of amplifiers of different operating conditions. It is suggested that a keying relay be substituted for the key in the circuit above wherever practicable.

true of all oscillators, whether electron coupled or crystal controlled.

The more amplifier or doubler stages that follow the keyed stage, the more difficult it is to hold control of the shape of the keyed waveform. A heavily excited doubler stage or class C stage acts as a peak clipper, tending to square up a rounded keying impulse, and the cumulative effect of several such stages cascaded is sufficient to square up the keyed waveform to the point where bad clicks are reimposed on a clean signal.

A good rule of thumb is to never key back farther than one stage removed from the final amplifier stage, and never key closer than one stage removed from the frequency controlling oscillator of the transmitter. Thus there will always be one isolating stage between the keyed stage and the oscillator, and one isolating stage between the keyed stage and the antenna. At this point the waveform of the keyed signal may be most easily controlled.

Keyer Circuit Requirements In the first place it may be established that the majority of new design transmitters, and many of those of older design as well, use a medium power beam tetrode tube either as the output stage or as the exciter for the output stage of a high power transmitter. Thus the transmitter usually will end up with a tube such as type 2E26, 807, 6146, 813, 4-65A, 4E27/257B, 4-125A or similar, or one of these tubes will be used as the stage just ahead of the output stage.

Second, it may be established that it is undesirable to key further down in the transmitter chain than the stage just ahead of the final

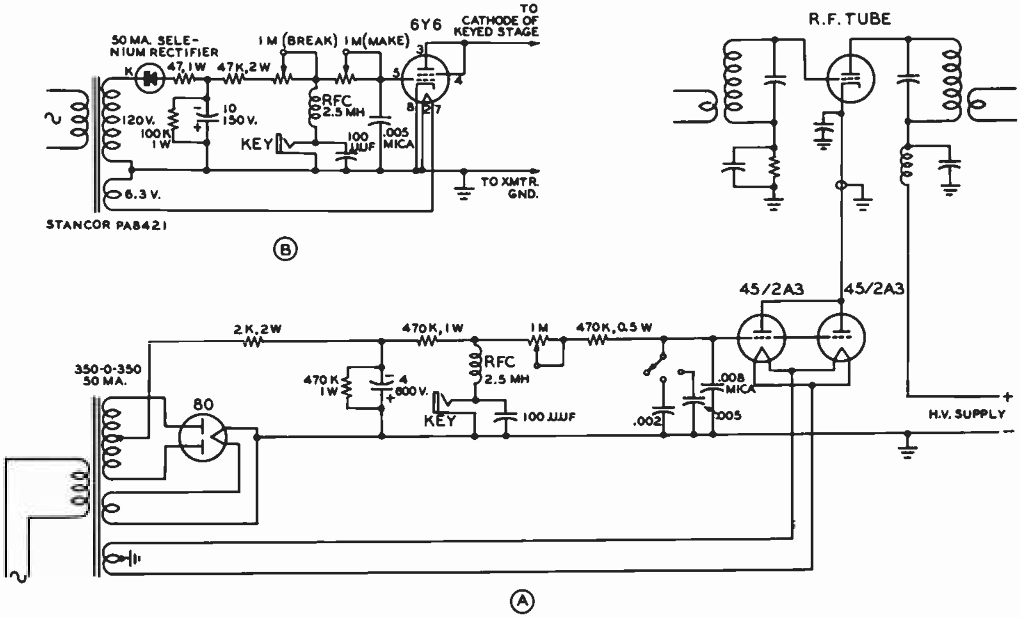


Figure 10

VACUUM TUBE KEYERS FOR CENTER-TAP KEYING CIRCUITS

The type A keyer is suitable for keying stages running up to 1250 volts on the plate. Two 2A3 or 6A3 tubes can safely key 160 milliamperes of cathode current. The simple 6Y6 keyer in figure B is for keying stages running up to 650 volts on the plate. A single 6Y6 can key 80 milliamperes. Two in parallel may be used for plate currents under 160 ma. If softer keying is desired, the 500-μμfd. mica condenser should be increased to .001 μfd.

amplifier. If a low-level stage, which is followed by a series of class C amplifiers, is keyed, serious transients will be generated in the output of the transmitter even though the keyed stage is being turned on and off very smoothly. This condition arises as a result of *pulse sharpening,* which has been discussed previously.

Third, the output from the stage should be completely cut off when the key is up, and the time constant of the rise and decay of the keying wave should be easily controllable.

Fourth, it should be possible to make the rise period and the decay period of the keying wave approximately equal. This type of keying envelope is the only one tolerable for commercial work, and is equally desirable for obtaining clean cut and easily readable signals in amateur work.

Fifth, it is desirable that the keying circuit be usable without a keying relay, even when a high-power stage is being keyed.

Last, for the sake of simplicity and safety, it should be possible to ground the frame of the key, and yet the circuit should be such that placing the fingers across the key will not result in an electrical shock. In other words, the keying circuit should be inherently safe.

All these requirements have been met in the keying circuits to be described.

17-5 Cathode Keying

The lead from the cathode or center-tap connection of the filament of an r-f amplifier can be opened and closed for a keying circuit. Such a keying system opens the plate voltage circuit and at the same time opens the grid bias return lead. For this reason, the grid circuit is blocked at the same time the plate circuit is opened. This helps to reduce the backwave that might otherwise leak through the keyed stage.

The simplest cathode keying circuit is illustrated in figure 9, where a key-click filter is employed, and a hand key is used to break the circuit. This simple keying circuit is not

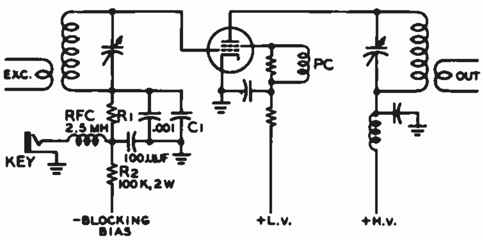


Figure 11

SIMPLE BLOCKED-GRID KEYING SYSTEM

The blocking bias must be sufficient to cut-off plate current to the amplifier stage in the presence of the excitation voltage. R_1 is normal bias resistor for the tube. R_2 and C_1 should be adjusted for correct keying waveform.

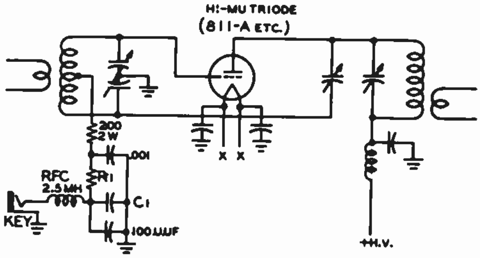


Figure 12

SELF-BLOCKING KEYING SYSTEM FOR HIGH-MU TRIODE

R_1 and C_1 adjusted for correct keying waveform. R_1 is bias resistor of tube.

recommended for general use, as considerable voltage will be developed across the key when it is open.

An electronic switch can take the place of the hand key. This will remove the danger of shock. At the same time, the opening and closing characteristics of the electronic switch may easily be altered to suit the particular need at hand. Such an electronic switch is called a *vacuum tube keyer*. Low internal resistance triode tubes such as the 45, 6A3, or 6AS7 are used in the keyer. These tubes act as a very high resistance when sufficient blocking bias is applied to them, and as a very low resistance when the bias is removed. The desired amount of lag or *cushioning effect* can be obtained by employing suitable resistance and capacitance values in the grid of the keyer tube(s). Because very little spark is produced at the key, due to the small amount of power in the key circuit, sparking clicks are easily suppressed.

One type 45 tube should be used for every 50 ma. of plate current. Type 6B4G or 2A3 tubes may also be used; allow one 6B4G tube for every 80 ma. of plate current.

Because of the series resistance of the keyer tubes, the plate voltage at the keyed tube will be from 30 to 60 volts less than the power supply voltage. This voltage appears as cathode bias on the keyed tube, assuming the bias return is made to ground, and should be taken into consideration when providing bias.

Some typical cathode circuit vacuum tube keying units are shown in figure 10.

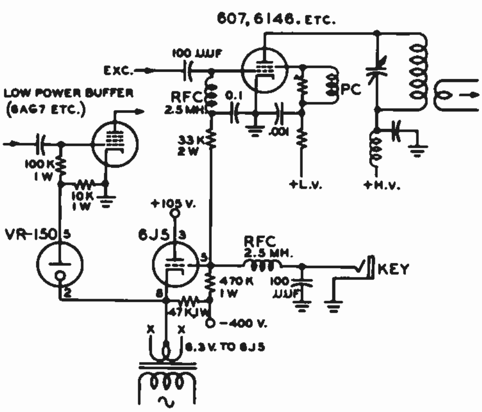


Figure 13

TWO-STAGE BLOCKED-GRID KEYER

A separate filament transformer must be used for the 6J5, as its filament is at a potential of −400 volts.

17-6 Grid Circuit Keying

Grid circuit, or blocked grid keying is another effective method of keying a c-w transmitter. A basic blocked grid keying circuit is shown in figure 11. The time constant of the keying is determined by the RC circuit, which also forms part of the bias circuit of the tube. When the key is closed, operating bias is developed by the flow of grid current through R_1. When the key is open, sufficient fixed bias is applied to the tube to block it, preventing the stage from functioning. If an un-neutralized

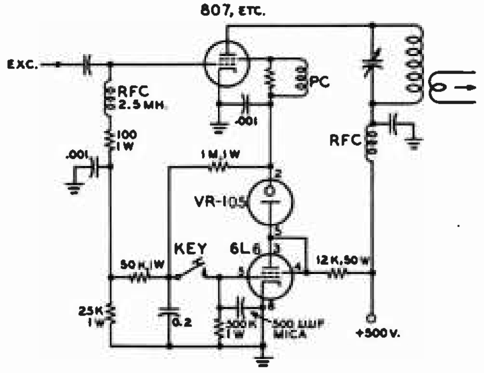


Figure 14
SINGLE-STAGE SCREEN GRID KEYER FOR TETRODE TUBES

tetrode is keyed by this method, there is the possibility of a considerable backwave caused by r-f leakage through the grid-plate capacity of the tube.

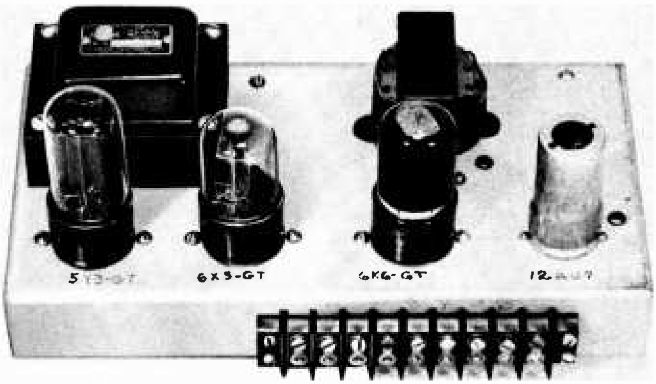
Certain hi-μ triode tubes, such as the 811-A and the 805, automatically block themselves when the grid return circuit is opened. It is merely necessary to insert a key and associated key click filter in the grid return lead of these tubes. No blocking bias supply is needed. This circuit is shown in figure 12.

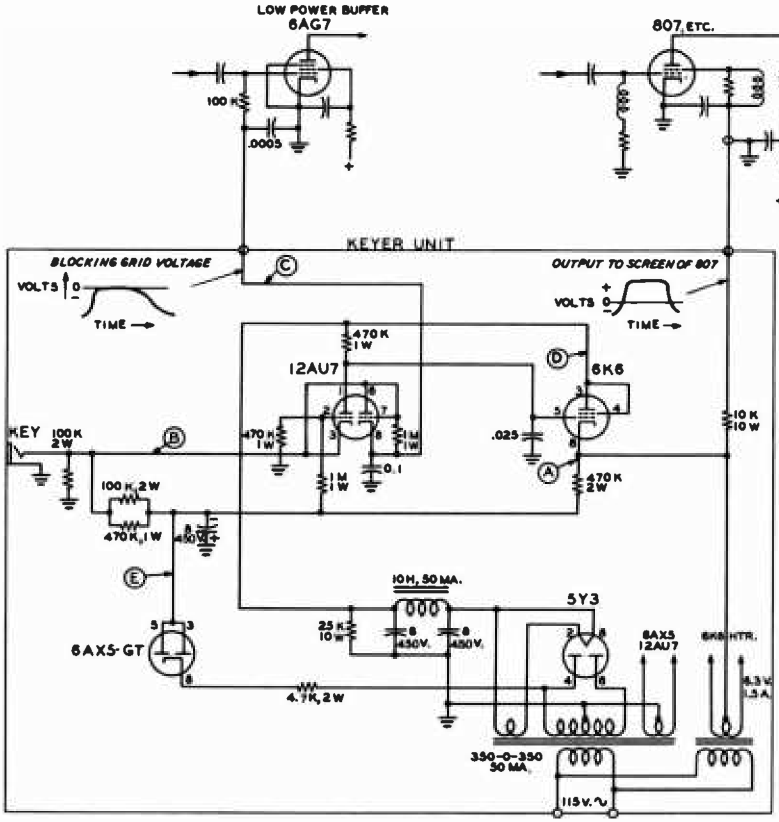
A more elaborate blocked-grid keying system has been developed by W1DX, and was shown in the February, 1954 issue of QST magazine. This highly recommended circuit is shown in figure 13. Two stages are keyed, preventing any backwave emission. The first keyed stage may be the oscillator, or a low powered buffer. The last keyed stage may be the driver stage to the power amplifier, or the amplifier itself. Since the circuit is so proportioned that the lower powered stage comes on *first* and goes off *last*, any keying chirp in the oscillator is not emitted on the air. Keying lag is applied to the high powered keyed stage only.

17-7 Screen Grid Keying

The screen circuit of a tetrode tube may be keyed for c-w operation. Unfortunately, when the screen grid of a tetrode tube is brought to zero potential, the tube still delivers considerable output. Thus it is necessary to place a negative blocking voltage on the screen grid to reduce the backwave through the tube. A suitable keyer circuit that will achieve this was developed by W6DTY, and was described in the February, 1953 issue of CQ magazine. This circuit is shown in figure 14. A 6L6 is used as a combined clamper tube and keying tube. When the key is closed, the 6L6 tube has blocking bias applied to its control grid. This bias is obtained from the rectified grid bias of the keyed tube. Screen voltage is applied to the keyed stage through a screen dropping resistor and a VR-105 regulator tube. When the key is open, the 6L6 is no longer cut-off, and conducts heavily. The voltage drop across the dropping resistor caused by the heavy plate current of the 6L6 lowers the voltage on the VR-105 tube until it is extin-

Figure 15
TOP VIEW OF SCREEN GRID KEYER SHOWN IN FIGURE 16





REFERENCE VOLTAGES		
POINT	KEY UP	KEY DOWN
A	-35	380
B	-110	0
C	-110	0
D	375	375
E	-275	-275

Figure 16
TWO-STAGE SCREEN GRID KEYER UNIT

guished, removing the screen voltage from the tetrode r-f tube. At the same time, rectified grid bias is applied to the screen of the tetrode through the 1 megohm resistor between screen and key. This voltage effectively cuts off the screen of the tetrode until the key is closed again. The RC circuit in the grid of the 6L6 tube determines the keying characteristic of the tetrode tube.

A more elaborate screen grid keyer is shown in figures 15 and 16. This keyer is designed to block-grid key the oscillator or a low powered buffer stage, and to screen key a medium powered tetrode tube such as an 807, 2E26 or 6146. The unit described includes a simple dual voltage power supply for the positive screen voltage of the tetrode, and a negative supply for the keyer stages. A 6K6 is used as the screen keyer, and a 12AU7 is used as a cathode follower and grid block keyer. As in the W1DX keyer, this keyer turns on the exciter a moment before the tetrode stage is turned on. The tetrode stage goes off an instant before the exciter does. Thus any keying chirp of the oscillator is effectively removed from the keyed signal.

By listening in the receiver one can hear the exciter stop operating a fraction of a second after the tetrode stage goes off. In fact, during rapid keying, the exciter may be heard as a steady signal in the receiver, as it has appreciable time lag in the keying circuit. The clipping effect of following stages has a definite hardening effect on this, however.

CHAPTER EIGHTEEN

Radiation, Propagation and Transmission Lines

Radio waves are electromagnetic waves similar in nature but much lower in frequency than light waves or heat waves. Such waves represent electric energy traveling through space. Radio waves travel in free space with the velocity of light and can be reflected and refracted much the same as light waves.

18-1 Radiation from an Antenna

Alternating current passing through a conductor creates an alternating electromagnetic field around that conductor. Energy is alternately stored in the field, and then returned to the conductor. As the frequency is raised, more and more of the energy does not return to the conductor, but instead is radiated off into space in the form of electromagnetic waves, called radio waves. Radiation from a wire, or wires, is materially increased whenever there is a sudden *change* in the *electrical constants* of the line. These sudden changes produce reflection, which places *standing waves* on the line.

When a wire in space is fed radio frequency energy having a wavelength of approximately 2.1 times the length of the wire in meters, the wire *resonates* as a *half-wave dipole* antenna at that wavelength or frequency. The greatest possible change in the electrical constants of a line is that which occurs at the open end of a wire. Therefore, a dipole has a great mismatch at each end, producing a high degree of reflection. We say that the ends of a dipole are terminated in an infinite impedance.

A returning wave which has been reflected meets the next incident wave, and the voltage and current at any point along the antenna are the vector sum of the two waves. At the ends of the dipole, the voltages add, while the currents of the two waves cancel, thus producing *high voltage* and *low current* at the *ends* of the dipole or half wave section of wire. In the same manner, it is found that the currents add while the voltages cancel at the center of the dipole. Thus, at the *center* there is *high current* but *low voltage*.

Inspection of figure 1 will show that the current in a dipole decreases sinusoidally towards either end, while the voltage similarly increases. The voltages at the two ends of the antenna are 180° out of phase, which means that the polarities are opposite, one being plus while the other is minus at any instant. A curve representing either the voltage or current on a dipole represents a *standing wave* on the wire.

Radiation from Sources other than Antennas Radiation can and does take place from sources other than antennas. Undesired radiation can take place from open-wire

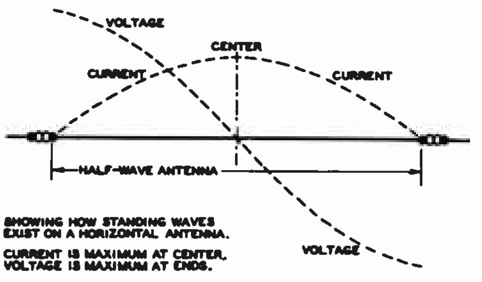


Figure 1
STANDING WAVES ON A RESONANT ANTENNA

transmission lines, both from single-wire lines and from lines comprised of more than one wire. In addition, radiation can be made to take place in a very efficient manner from electromagnetic horns, from plastic lenses or from electromagnetic lenses made up of spaced conducting planes, from slots cut in a piece of metal, from dielectric wires, or from the open end of a wave guide.

Directivity of Radiation The radiation from any physically practicable radiating system is directive to a certain degree. The degree of directivity can be enhanced or altered when desirable through the combination of radiating elements in a prescribed manner, through the use of reflecting planes or curved surfaces, or through the use of such systems as mentioned in the preceding paragraph. The construction of directive antenna arrays is covered in detail in the chapters which follow.

Polarization Like light waves, radio waves can have a definite polarization. In fact, while light waves ordinarily have to be reflected or passed through a polarizing medium before they have a definite polarization, a radio wave leaving a simple radiator will have a definite polarization, the polarization being indicated by the orientation of the electric-field component of the wave. This, in turn, is determined by the orientation of the radiator itself, as the magnetic-field component is always at right angles to a linear radiator, and the electric-field component is always in the same plane as the radiator. Thus we see that an antenna that is vertical with respect to the earth will transmit a vertically polarized wave, as the electrostatic lines of force will be vertical. Likewise, a simple horizontal antenna will radiate horizontally polarized waves.

Because the orientation of a simple linear radiator is the same as the polarization of the waves emitted by it, the radiator itself is referred to as being either vertically or horizontally polarized. Thus, we say that a horizontal antenna is horizontally polarized.

Figure 2A illustrates the fact that the polarization of the electric field of the radiation from a vertical dipole is vertical. Figure 2B, on the other hand, shows that the polarization of electric-field radiation from a vertical *slot* radiator is horizontal. This fact has been utilized in certain commercial FM antennas where it is desired to have horizontally polarized radiation but where it is more convenient to use an array of vertically stacked slot arrays. If the metallic sheet is bent into a cylinder with the slot on one side, substantially omnidirectional horizontal coverage is obtained with horizontally-polarized radiation when the cylinder with the slot in one side is oriented vertically. An arrangement of this type is shown in figure 2C. Several such cylinders may be stacked vertically to reduce high-angle radiation and to concentrate the radiated energy at the useful low radiation angles.

In any event the polarization of radiation from a radiating system is parallel to the electric field as it is set up inside or in the vicinity of the radiating system.

18-2 General Characteristics of Antennas

All antennas have certain general characteristics to be enumerated. It is the result of differences in these general characteristics which makes one type of antenna system most suitable for one type of application and another type best for a different application. Six of the more important characteristics are: (1) polarization, (2) radiation resistance, (3) horizontal directivity, (4) vertical directivity, (5) bandwidth, and (6) effective power gain.

The *polarization* of an antenna or radiating system is the direction of the electric field and has been defined in Section 18-1.

The *radiation resistance* of an antenna system is normally referred to the feed point in an antenna fed at a current loop, or it is referred to a current loop in an antenna system fed at another point. The radiation resistance is that value of resistance which, if inserted in series with the antenna at a current loop, would dissipate the same energy as is actually radiated by the antenna if the antenna current at the feed point were to remain the same.

The *horizontal* and *vertical directivity* can best be expressed as a *directive pattern* which

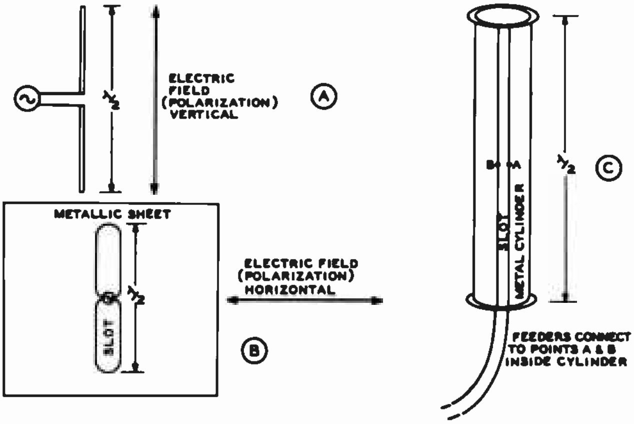


Figure 2

ANTENNA POLARIZATION

The polarization (electric field) of the radiation from a resonant dipole such as shown at (A) above is parallel to the length of the radiator. In the case of a resonant slot cut in a sheet of metal and used as a radiator, the polarization (of the electric field) is perpendicular to the length of the slot. In both cases, however, the polarization of the radiated field is parallel to the potential gradient of the radiator; in the case of the dipole the electric lines of force are from end to end, while in the case of the slot the field is across the sides of the slot. The metallic sheet containing the slot may be formed into a cylinder to make up the radiator shown at (C). With this type of radiator the radiated field will be horizontally polarized even though the radiator is mounted vertically.

is a graph showing the relative radiated field intensity against *azimuth* angle for horizontal directivity and field intensity against *elevation* angle for vertical directivity.

The *bandwidth* of an antenna is a measure of its ability to operate within specified limits over a range of frequencies. Bandwidth can be expressed either "operating frequency plus-or-minus a specified per cent of operating frequency" or "operating frequency plus-or-minus a specified number of megacycles" for a certain standing-wave-ratio limit on the transmission line feeding the antenna system.

The *effective power gain* or *directive gain* of an antenna is the ratio between the power required in the specified antenna and the power required in a reference antenna (usually a half-wave dipole) to attain the same field strength in the favored direction of the antenna under measurement. Directive gain may be expressed either as an actual power ratio, or as is more common, the power ratio may be expressed in decibels.

Physical Length of a Half-Wave Antenna If the cross section of the conductor which makes up the antenna is kept very small with respect to the antenna length, an electrical half wave is a fixed percentage shorter than a physical half-wavelength. This percentage is approximately 5 per cent. Therefore, most linear half-wave antennas are close to 95 per cent of a half wavelength long physically. Thus, a half-wave antenna resonant at exactly 80 meters would be one-half of 0.95 times 80 meters in length. Another way of saying the same thing is that a wire resonates at a wavelength of about 2.1 times its length in meters. If the diameter of the conductor begins to be an appreciable fraction of a wavelength, as when tubing is used as a v-h-f radiator, the factor becomes slightly less than 0.95. For the use of wire and not tubing on frequencies below 30 Mc., however, the figure of 0.95 may be taken as accurate. This assumes a radiator removed from surrounding objects, and with *no bends*.

Simple conversion into feet can be obtained by using the factor 1.56. To find the physical length of a half-wave 80-meter antenna, we multiply 80 times 1.56, and get 124.8 feet for the length of the radiator.

It is more common to use frequency than wavelength when indicating a specific spot in the radio spectrum. For this reason, the relationship between wavelength and frequency must be kept in mind. As the velocity of radio waves through space is constant at the speed of light, it will be seen that the more waves that pass a point per second (higher frequency), the closer together the peaks of those waves must be (shorter wavelength). Therefore, the higher the frequency, the lower will be the wavelength.

A radio wave in space can be compared to a wave in water. The wave, in either case, has peaks and troughs. One peak and one trough constitute a *full wave*, or *one wavelength*.

Frequency describes the number of wave cycles or peaks passing a point per second. Wavelength describes the distance the wave travels through space during one cycle or oscillation of the antenna current; it is the distance in meters between adjacent peaks or adjacent troughs of a wave train.

As a radio wave travels 300,000,000 meters a second (speed of light), a frequency of 1 cycle per second corresponds to a wavelength of 300,000,000 meters. So, if the frequency is multiplied by a million, the wavelength must be divided by a million, in order to maintain their correct ratio.

A frequency of 1,000,000 cycles per second (1,000 kc.) equals a wavelength of 300 meters. Multiplying frequency by 10 and dividing wavelength by 10, we find: a frequency of 10,000 kc. equals a wavelength of 30 meters. Multiplying and dividing by 10 again, we get: a frequency of 100,000 kc. equals 3 meters wavelength. Therefore, to change wavelength to frequency (in kilocycles), simply divide 300,000 by the wavelength in meters (λ).

$$F_{kc} = \frac{300{,}000}{\lambda}$$

$$\lambda = \frac{300{,}000}{F_{kc}}$$

Now that we have a simple conversion formula for converting wavelength to frequency and vice versa, we can combine it with our wavelength versus antenna length formula, and we have the following:

Length of a half-wave radiator made from wire (no. 14 to no. 10):

3.5-Mc. to 30-Mc. bands

$$\text{Length in feet} = \frac{468}{\text{Freq. in Mc.}}$$

50-Mc. band

$$\text{Length in feet} = \frac{460}{\text{Freq. in Mc.}}$$

$$\text{Length in inches} = \frac{5600}{\text{Freq. in Mc.}}$$

144-Mc. band

$$\text{Length in inches} = \frac{5500}{\text{Freq. in Mc.}}$$

Length-to-Diameter Ratio When a half-wave radiator is constructed from tubing or rod whose diameter is an appreciable fraction of the length of the radiator, the resonant length of a half-wave antenna will be shortened. The amount of shortening can be determined with the aid of the chart of figure 3, In this chart the amount of additional shortening over the values given in the previous paragraph is plotted against the ratio of the length to the diameter of the half-wave radiator.

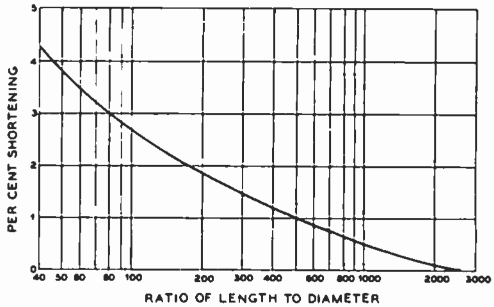


Figure 3
CHART SHOWING SHORTENING OF A RESONANT ELEMENT IN TERMS OF RATIO OF LENGTH TO DIAMETER

The use of this chart is based on the basic formula where radiator length in feet is equal to 468/frequency in Mc. This formula applies to frequencies below perhaps 30 Mc. when the radiator is made from wire. On higher frequencies, or on 14 and 28 Mc. when the radiator is made of large-diameter tubing, the radiator is shortened from the value obtained with the above formula by an amount determined by the ratio of length to diameter of the radiator. The amount of this shortening is obtainable from the chart shown above.

The length of a wave in free space is somewhat longer than the length of an antenna for the same frequency. The actual free-space wavelength is given by the following expressions:

$$\text{Wavelength} = \frac{492}{\text{Freq. in Mc.}} \text{ in feet}$$

$$\text{Wavelength} = \frac{5905}{\text{Freq. in Mc.}} \text{ in inches}$$

Harmonic Resonance A wire in space can resonate at more than one frequency. The *lowest* frequency at which it resonates is called its *fundamental* frequency, and at that frequency it is approximately a half wavelength long. A wire can have two, three, four, five, or more standing waves on it, and thus it resonates at approximately the integral harmonics of its fundamental frequency. However, the higher harmonics are not exactly integral multiples of the lowest resonant frequency as a result of *end effects*.

A harmonic operated antenna is somewhat longer than the corresponding integral number of dipoles, and for this reason, the dipole length formula cannot be used simply by multiplying by the corresponding harmonic. The intermediate half wave sections do not have *end effects*. Also, the current distribution is disturbed by the fact that power can reach some of the half wave sections only by flowing through other sections, the latter then acting not only as radiators, but also as transmission lines. For the latter reason, the resonant length will be dependent to an extent upon the method of feed, as there will be less attenuation of the current along the antenna if it is fed at or near the center than if fed towards or at one end. Thus, the antenna would have to be somewhat longer if fed near one end than if fed near the center. The difference would be small, however, unless the antenna were many wavelengths long.

The length of a center fed harmonically operated doublet may be found from the formula:

$$L = \frac{(K-.05) \times 492}{\text{Freq. in Mc.}}$$

where K = number of ½ waves on antenna
L = length in feet

Under conditions of severe current attenuation, it is possible for some of the nodes, or loops, actually to be slightly greater than a physical half wavelength apart. Practice has shown that the most practical method of resonating a harmonically operated antenna accurately is by cut and try, or by using a feed system in which both the feed line and antenna are resonated at the station end as an integral system.

A dipole or half-wave antenna is said to operate on its fundamental or first harmonic. A full wave antenna, 1 wavelength long, operates on its second harmonic. An antenna with five half-wavelengths on it would be operating on its fifth harmonic. Observe that the fifth harmonic antenna is *2½ wavelengths* long, *not* 5 wavelengths.

Antenna Resonance Most types of antennas operate most efficiently when tuned or *resonated* to the frequency of operation. This consideration of course does not apply to the rhombic antenna and to the parasitic elements of arrays employing parasitically excited elements. However, in practically every other case it will be found that increased efficiency results when the entire antenna system is resonant, whether it be a simple dipole or an elaborate array. The radiation efficiency of a resonant wire is many times that of a wire which is not resonant.

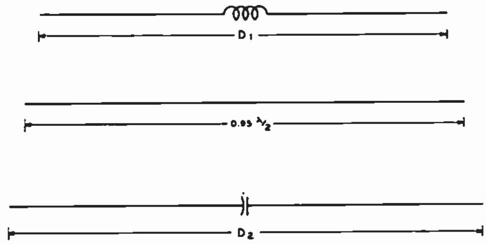


Figure 4

EFFECT OF SERIES INDUCTANCE AND CAPACITANCE ON THE LENGTH OF A HALF-WAVE RADIATOR

The top antenna has been electrically lengthened by placing a coil in series with the center. In other words, an antenna with a lumped inductance in its center can be made shorter for a given frequency than a plain wire radiator. The bottom antenna has been capacitively shortened electrically. In other words, an antenna with a capacitor in series with it must be made longer for a given frequency since its effective electrical length as compared to plain wire is shorter.

If an antenna is slightly too long, it can be resonated by series insertion of a variable capacitor at a high current point. If it is slightly too short, it can be resonated by means of a variable inductance. These two methods, illustrated schematically in figure 4, are generally employed when part of the antenna is brought into the operating room.

With an antenna array, or an antenna fed by means of a transmission line, it is more common to cut the elements to exact resonant length by "cut and try" procedure. Exact antenna resonance is more important when the antenna system has low radiation resistance; an antenna with low radiation resistance has higher Q (tunes sharper) than an antenna with high radiation resistance. The higher Q does not indicate greater efficiency; it simply indicates a sharper resonance curve.

18-3 Radiation Resistance and Feed-Point Impedance

In many ways, a half-wave antenna is like a tuned tank circuit. The main difference lies in the fact that the elements of inductance, capacitance, and resistance are *lumped* in the tank circuit, and are *distributed* throughout the length of an antenna. The center of a half-wave radiator is effectively at ground potential as far as r-f voltage is concerned, although the current is highest at that point.

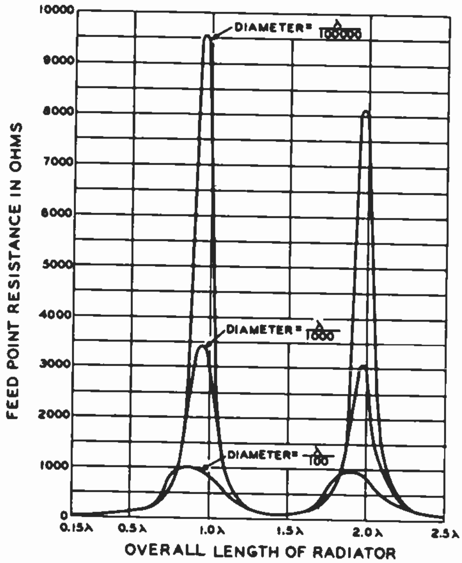


Figure 5

FEED POINT RESISTANCE OF A CENTER DRIVEN RADIATOR AS A FUNCTION OF PHYSICAL LENGTH IN TERMS OF FREE SPACE WAVELENGTH

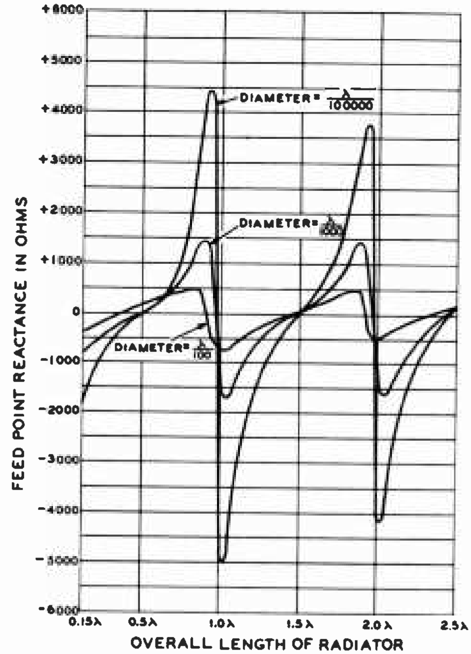


Figure 6

REACTIVE COMPONENT OF THE FEED POINT IMPEDANCE OF A CENTER DRIVEN RADIATOR AS A FUNCTION OF PHYSICAL LENGTH IN TERMS OF FREE SPACE WAVELENGTH

When the antenna is resonant, and it always should be for best results, the impedance at the center is substantially resistive, and is termed the radiation resistance. Radiation resistance is a fictitious term; it is that value of resistance (referred to the current loop) which would dissipate the same amount of power as being radiated by the antenna, when fed with the current flowing at the current loop.

The radiation resistance depends on the antenna length and its proximity to nearby objects which either absorb or re-radiate power, such as the ground, other wires, etc.

The Marconi Antenna Before going too far with the discussion of radiation resistance, an explanation of the Marconi (grounded quarter wave) antenna is in order. The Marconi antenna is a special type of Hertz antenna in which the earth acts as the "other half" of the dipole. In other words, the current flows into the earth instead of into a similar quarter-wave section. Thus, the current loop of a Marconi antenna is at the *base* rather than in the *center*. In either case it is a quarter wavelength from the end.

A half-wave dipole far from ground and other reflecting objects has a radiation resistance at the center of about 73 ohms. A Marconi antenna is simply one-half of a dipole. For that reason, the radiation resistance is roughly half the 73-ohm impedance of the dipole or 36.5 ohms. The radiation resistance of a Marconi antenna such as a mobile whip will be lowered by the proximity of the automobile body.

Antenna Impedance Because the power throughout the antenna is the same, the *impedance* of a resonant antenna at any point along its length merely expresses the ratio between voltage and current at that point. Thus, the lowest impedance occurs where the current is highest, namely, at the center of a dipole, or a quarter wave from the end of a Marconi. The impedance rises uniformly toward each end, where it is about 2000 ohms for a dipole remote from ground, and about twice as high for a vertical Marconi.

If a vertical half-wave antenna is set up so that its lower end is at the ground level, the effect of the ground reflection is to increase

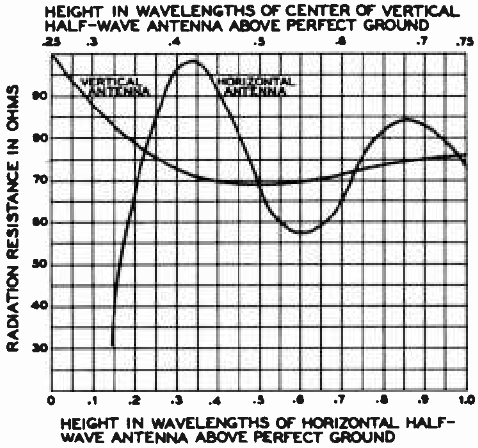


Figure 7

EFFECT OF HEIGHT ON THE RADIATION RESISTANCE OF A DIPOLE SUSPENDED ABOVE PERFECT GROUND

the radiation resistance to approximately 100 ohms. When a horizontal half-wave antenna is used, the radiation resistance (and, of course, the amount of energy radiated for a given antenna current) depends on the height of the antenna above ground, since the height determines the phase and amplitude of the wave reflected from the ground back to the antenna. Thus the resultant current in the antenna for a given power is a function of antenna height.

Center-fed Feed Point Impedance When a linear radiator is series fed at the center, the resistive and reactive components of the driving point impedance are dependent upon both the length and diameter of the radiator in wavelengths. The manner in which the resistive component varies with the physical dimensions of the radiator is illustrated in figure 5. The manner in which the reactive component varies is illustrated in figure 6.

Several interesting things will be noted with respect to these curves. The reactive component disappears when the overall physical length is slightly less than any number of half waves long, the differential increasing with conductor diameter. For overall lengths in the vicinity of an odd number of half wavelengths, the center feed point looks to the generator or transmission line like a series-resonant lumped circuit, while for overall lengths in the vicinity of an *even* number of half wavelengths, it looks like a parallel-resonant or anti-resonant lumped circuit. Both the feed point resistance and the feed point reactance *change more slowly* with overall radiator length (or with frequency with a fixed length) *as the conductor diameter is increased,* indicating that the effective "Q" is lowered as the diameter is increased. However, in view of the fact that the damping resistance is nearly all "radiation resistance" rather than loss resistance, the lower Q does not represent lower efficiency. Therefore, the lower Q is desirable, because it permits use of the radiator over a wider frequency range without resorting to means for eliminating the reactive component. Thus, the use of a large diameter conductor makes the overall system less frequency sensitive. If the diameter is made sufficiently large in terms of wavelengths, the Q will be low enough to qualify the radiator as a "broad-band" antenna.

The curves of figure 7 indicate the theoretical center-point radiation resistance of a half-wave antenna for various heights above perfect ground. These values are of importance in matching untuned radio-frequency feeders to the antenna, in order to obtain a good impedance match and an absence of standing waves on the feeders.

Ground Losses Above *average* ground, the actual radiation resistance of a dipole will vary from the exact value of figure 7 since the latter assumes a hypothetical, perfect ground having no loss and perfect reflection. Fortunately, the curves for the radiation resistance over most types of earth will correspond rather closely with those of the chart, except that the radiation resistance for a horizontal dipole does not fall off as rapidly as is indicated for heights below an eighth wavelength. However, with the antenna so close to the ground and the soil in a strong field, much of the radiation resistance is actually represented by ground loss; this means that a good portion of the antenna power is being dissipated in the earth, which, unlike the hypothetical perfect ground, has resistance. In this case, an appreciable portion of the *radiation resistance* actually is loss resistance. The type of soil also has an effect upon the radiation *pattern,* especially in the vertical plane, as will be seen later.

The radiation resistance of an antenna generally increases with length, although this increase varies up and down about a constantly increasing average. The peaks and dips are caused by the reactance of the antenna, when its length does not allow it to resonate at the operating frequency.

Antenna Efficiency Antennas have a certain loss resistance as well as a radiation resistance. The loss resistance defines the power lost in the antenna due to ohmic resistance of the wire, ground resistance (in the case of a Marconi), corona discharge, and insulator losses.

The approximate effective radiation efficiency (expressed as a decimal) is equal to: $N_r = R_a/(R_a + R_L)$ where R_a is equal to the radiation resistance and R_L is equal to the effective loss resistance of the antenna. The loss resistance will be of the order of 0.25 ohm for large-diameter tubing conductors such as are most commonly used in multi-element parasitic arrays, and will be of the order of 0.5 to 2.0 ohms for arrays of normal construction using copper wire.

When the radiation resistance of an antenna or array is very low, the current at a voltage node will be quite high for a given power. Likewise, the voltage at a current node will be very high. Even with a heavy conductor and excellent insulation, the losses due to the high voltage and current will be appreciable if the radiation resistance is sufficiently low.

Usually, it is not considered desirable to use an antenna or array with a radiation resistance of less than approximately 5 ohms unless there is sufficient directivity, compactness, or other advantage to offset the losses resulting from the low radiation resistance.

Ground Resistance The radiation resistance of a Marconi antenna, especially, should be kept as high as possible. This will reduce the antenna current for a given power, thus minimizing loss resulting from the series resistance offered by the earth connection. The radiation resistance can be kept high by making the Marconi radiator somewhat longer than a quarter wave, and shortening it by series capacitance to an electrical quarter wave. This reduces the current flowing in the earth connection. It also should be removed from ground as much as possible (vertical being ideal). Methods of minimizing the resistance of the earth connection will be found in the discussion of the Marconi antenna.

18-4 Antenna Directivity

All practical antennas radiate better in some directions than others. This characteristic is called *directivity*. The more *directive* an antenna is, the more it concentrates the radiation in a certain direction, or directions. The more the radiation is concentrated in a certain direction, the greater will be the field strength produced in that direction for a given amount of total radiated power. Thus the use of a directional antenna or *array* produces the same result in the favored direction as an increase in the power of the transmitter.

The increase in radiated power in a certain direction with respect to an antenna in free space as a result of inherent directivity is called the *free space directivity power gain* or just *space directivity gain* of the antenna (referred to a hypothetical *isotropic radiator* which is assumed to radiate equally well in all directions). Because the fictitious isotropic radiator is a purely academic antenna, not physically realizable, it is common practice to use as a reference antenna the simplest ungrounded resonant radiator, the half-wave *Hertz,* or resonant doublet. As a half-wave doublet has a space directivity gain of 2.15 db over an isotropic radiator, the use of a resonant dipole as the comparison antenna reduces the *gain figure* of an array by 2.15 db. However, it should be understood that power gain can be expressed with regard to *any* antenna, just so long as it is specified.

As a matter of interest, the directivity of an *infinitesimal dipole* provides a free space directivity power gain of 1.5 (or 1.76 db) over an isotropic radiator. This means that *in the direction of maximum radiation* the infinitesimal dipole will produce the same field of strength as an isotropic radiator which is radiating 1.5 times as much total power.

A half-wave resonant doublet, because of its different current distribution and significant length, exhibits slightly more free space power gain as a result of directivity than does the infinitesimal dipole, for reasons which will be explained in a later section. The space directivity power gain of a half-wave resonant doublet is 1.63 (or 2.15 db) referred to an isotropic radiator.

Horizontal Directivity When choosing and orienting an antenna system, the radiation patterns of the various common types of antennas should be given careful consideration. The directional characteristics are of still greater importance when a directive antenna array is used.

Horizontal directivity is always desirable on any frequency for point-to-point work. However, it is not always attainable with reasonable antenna dimensions on the lower frequencies. Further, when it is attainable, as on the frequencies above perhaps 7 Mc., with reasonable antenna dimensions, operating convenience is greatly furthered if the maximum lobe of the horizontal directivity is controllable. It is for this reason that rotatable antenna arrays have come into such common usage.

Considerable horizontal directivity can be used to advantage when: (1) only point-to-point work is necessary, (2) several arrays are available so that directivity may be changed by selecting or reversing antennas, (3) a single rotatable array is in use. Signals follow the

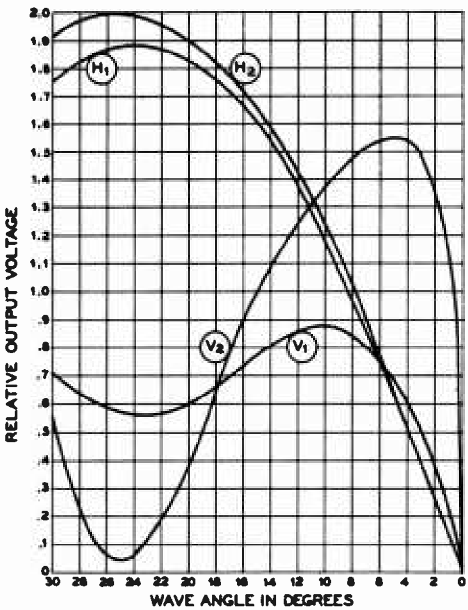


Figure 8

VERTICAL-PLANE DIRECTIONAL CHARACTERISTICS OF HORIZONTAL AND VERTICAL DOUBLETS ELEVATED 0.6 WAVELENGTH AND ABOVE TWO TYPES OF GROUND

H_1 represents a horizontal doublet over typical farmland. H_2 over salt water. V_1 is a vertical pattern of radiation from a vertical doublet over typical farmland, V_2 over salt water. A salt water ground is the closest approach to an extensive ideally perfect ground that will be met in actual practice.

great-circle path, or within 2 or 3 degrees of that path under all normal propagation conditions. However, under turbulent ionosphere conditions, or when unusual propagation conditions exist, the deviation from the great-circle path for greatest signal intensity may be as great as 90°. Making the array rotatable overcomes these difficulties, but arrays having extremely high horizontal directivity become too cumbersome to be rotated, except perhaps when designed for operation on frequencies above 50 Mc.

Vertical Directivity Vertical directivity is of the greatest importance in obtaining satisfactory communication above 14 Mc. whether or not horizontal directivity is used. This is true simply because *only* the energy radiated between certain definite *elevation* angles is useful for communication. Energy radiated at other elevation angles is lost and performs no useful function.

Optimum Angle of Radiation The optimum angle of radiation for propagation of signals between two points is dependent upon a number of variables. Among these significant variables are: (1) height of the ionosphere layer which is providing the reflection, (2) distance between the two stations, (3) number of hops for propagation between the two stations. For communication on the 14-Mc. band it is often possible for different modes of propagation to provide signals between two points. This means, of course, that more than one angle of radiation can be used. If *no* elevation directivity is being used under this condition of propagation, selective fading will take place because of interference between the waves arriving over the different paths.

On the 28-Mc. band it is by far the most common condition that only one mode of propagation will be possible between two points at any one time. This explains, of course, the reason why rapid fading in general and selective fading in particular are almost absent from signals heard on the 28-Mc. band (except for fading caused by local effects).

Measurements have shown that the angles useful for communication on the 14-Mc. band are from 3° to about 30°; angles above about 15° being useful only for local work. On the 28-Mc. band measurements have shown that the useful angles range from about 3° to 18°; angles above about 12° being useful only for local (less than 3000 miles) work. These figures assume normal propagation by virtue of the F_2 layer.

Angle of Radiation of Typical Antennas and Arrays It now becomes of interest to determine the amount of radiation available at these useful lower angles of radiation from commonly used antennas and antenna arrays. Figure 8 shows relative output voltage plotted against elevation angle (wave angle) in degrees above the horizontal, for horizontal and vertical doublets elevated 0.6 wavelength above two types of ground. It is obvious by inspection of the curves that a horizontal dipole mounted at this height above ground (20 feet on the 28-Mc. band) is radiating only a small amount of energy at angles useful for communication on the 28-Mc. band. Most of the energy is being radiated uselessly upward. The vertical antenna above a good reflecting surface appears much better in this respect—and this fact has been proven many times by actual installations.

It might immediately be thought that the amount of radiation from a horizontal or vertical

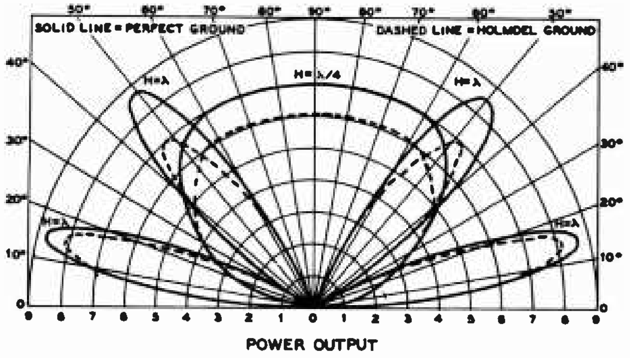


Figure 9

VERTICAL RADIATION PATTERNS

Showing the vertical radiation patterns for half-wave antennas (or colinear half-wave or extended half-wave antennas) at different heights above average ground and perfect ground. Note that such antennas one-quarter wave above ground concentrate most radiation at the very high angles which are useful for communication only on the lower frequency bands. Antennas one-half wave above ground are not shown, but the elevation pattern shows one lobe on each side at an angle of 30° above horizontal.

dipole could be increased by raising the antenna higher above the ground. This is true to an extent in the case of the horizontal dipole; the low-angle radiation does increase *slowly* after a height of 0.6 wavelength is reached but at the expense of greatly increased high-angle radiation and the formation of a number of nulls in the elevation pattern. No signal can be transmitted or received at the elevation angles where these nulls have been formed. Tests have shown that a center height of 0.6 wavelength for a vertical dipole (0.35 wavelength to the bottom end) is about optimum for this type of array.

Figure 9 shows the effect of placing a horizontal dipole at various heights above ground. It is easily seen by reference to figure 9 (and figure 10 which shows the radiation from a dipole at ¾ wave height) that a large percentage of the total radiation from the dipole is being radiated at relatively high angles which are useless for communication on the 14-Mc. and 28-Mc. bands. Thus we see that in order to obtain a worthwhile increase in the ratio of low-angle radiation to high-angle radiation it is necessary to place the antenna high above ground, *and in addition* it is necessary to use additional means for suppressing high-angle radiation.

Suppression of High-angle Radiation High-angle radiation can be suppressed, and this radiation can be added to that going out at low angles, only through the use of some sort of *directive* antenna system. There are three general types of antenna arrays composed of dipole elements commonly used which concentrate radiation at the lower more effective angles for high-frequency communication. These types are: (1) The close-spaced out-of-phase system as exemplified by the "flat-top" beam or W8JK array. Such configurations are classified as *end fire arrays.* (2) The wide-spaced in-phase arrays, as exemplified by the "Lazy H" antenna. These configurations are classified as *broadside arrays.* (3) The close-spaced parasitic systems, as exemplified by the three element rotary beam.

A comparison between the radiation from a dipole, a "flat-top beam" and a pair of dipoles stacked one above the other (half of a "lazy H"), in each case with the top of the antenna at a height of ¾ wavelength is shown in figure 11. The improvement in the amplitude of low-

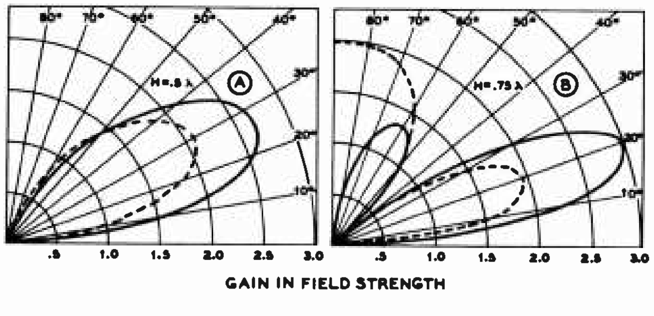


Figure 10

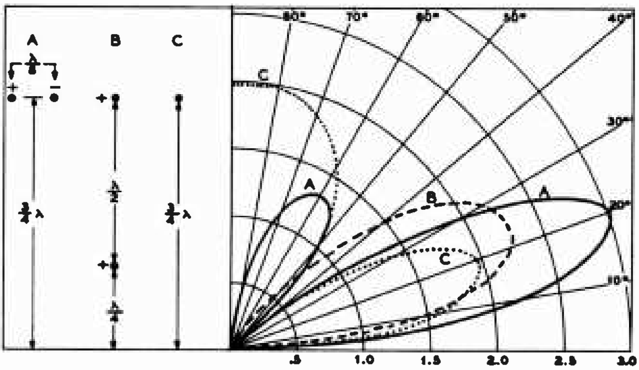
VERTICAL RADIATION PATTERNS

Showing vertical-plane radiation patterns of a horizontal single-section flat-top beam with one-eighth wave spacing (solid curves) and a horizontal half-wave antenna (dashed curves) when both are 0.5 wavelength (A) and 0.75 wavelength (B) above ground.

Figure 11

COMPARATIVE VERTICAL RADIATION PATTERNS

Showing the vertical radiation patterns of a horizontal single-section flat-top beam (A), an array of two stacked horizontal in-phase half-wave elements—half of a "Lazy H"—(B), and a horizontal dipole (C). In each case the top of the antenna system is 0.75 wavelength above ground, as shown to the left of the curves.



angle radiation at the expense of the useless high-angle radiation with these simple arrays as contrasted to the dipole is quite marked.

Figure 12 compares the patterns of a 3 element beam and a dipole radiator at a height of 0.75 wavelength. It will be noticed that although there is more energy in the lobe of the beam as compared to the dipole, the axis of the beam is at the same angle above the horizontal. Thus, although more radiated energy is provided by the beam at low angles, the average angle of radiation of the beam is no lower than the average angle of radiation of the dipole.

18-5 Bandwidth

The bandwidth of an antenna or an antenna array is a function primarily of the radiation resistance and of the shape of the conductors which make up the antenna system. For arrays of essentially similar construction the bandwidth (or the deviation in frequency which the system can handle without mismatch) is increased with increasing radiation resistance, and the bandwidth is increased with the use of conductors of larger diameter (smaller ratio of length to diameter). This is to say that if an array of any type is constructed of large diameter tubing or spaced wires, its bandwidth will be greater than that of a similar array constructed of single wires.

The radiation resistance of antenna arrays of the types mentioned in the previous paragraphs may be increased through the use of wider spacing between elements. With increased radiation resistance in such arrays the *radiation efficiency* increases since the ohmic losses within the conductors become a smaller percentage of the radiation resistance, and the bandwidth is increased proportionately.

18-6 Propagation of Radio Waves

The preceding sections have discussed the manner in which an electromagnetic-wave or radio-wave field may be set up by a radiating system. However, for this field to be useful for communication it must be propagated to some distant point where it may be received, or where it may be reflected so that it may be received at some other point. Radio waves may be propagated to a remote point by either or both of two general methods. Propagation

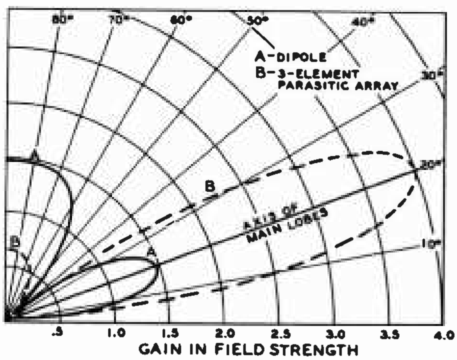


Figure 12

VERTICAL RADIATION PATTERNS

Showing vertical radiation patterns of a horizontal dipole (A) and a horizontal 3-element parasitic array (B) at a height above ground of 0.75 wavelength. Note that the axis of the main radiation lobes are at the same angle above the horizontal. Note also the suppression of high angle radiation by the parasitic array.

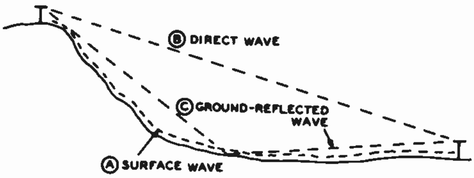


Figure 13
GROUND-WAVE SIGNAL PROPAGATION

The illustration above shows the three components of the ground wave: (A), the surface wave; (B), the direct wave; and (C), the ground-reflected wave. The direct wave and the ground-reflected wave combine at the receiving antenna to make up the space wave.

may take place as a result of the *ground wave*, or as a result of the *sky wave* or *ionospheric wave*.

The Ground Wave The term *ground wave* actually includes several different types of waves which usually are called: (1) the *surface wave*, (2) the *direct wave*, and (3) the *ground-reflected wave*. The latter two waves combine at the receiving antenna to form the *resultant wave* or the *space wave*. The distinguishing characteristic of the components of the ground wave is that all travel along or over the surface of the earth, so that they are affected by the conductivity and terrain of the earth's surface.

The Ionospheric Wave or Sky Wave Intense bombardment of the upper regions of the atmosphere by radiations from the sun results in the formation of ionized layers. These ionized layers, which form the *ionosphere*, have the capability of reflecting or refracting radio waves which impinge upon them. A radio wave which has been propagated as a result of one or more reflections from the ionosphere is known as an *ionospheric wave* or a *sky wave*. Such waves make possible long distance radio communication. Propagation of radio signals by ionospheric waves is discussed in detail in Section 18-8.

18-7 Ground-Wave Communication

As stated in the preceding paragraph, the term *ground wave* applies both to the *surface wave* and to the *space wave* (the resultant wave from the combination of the direct wave and the ground-reflected wave) or to a combination of the two. The three waves which may combine to make up the ground wave are illustrated in figure 13.

The Surface Wave The surface wave is that wave which we normally receive from a standard broadcast station. It travels directly along the ground and terminates on the earth's surface. Since the earth is a relatively poor conductor, the surface wave is attenuated quite rapidly. The surface wave is attenuated less rapidly as it passes over sea water, and the attenuation decreases for a specific distance as the frequency is decreased. The rate of attenuation with distance becomes so large as the frequency is increased above about 3 Mc. that the surface wave becomes of little value for communication.

The Space Wave The resultant wave or space wave is illustrated in figure 13 by the combination of (B) and (C). It is this wave path, which consists of the combination of the direct wave and the ground-reflected wave at the receiving antenna, which is the *normal* path of signal propagation for line-of-sight or near line-of-sight communication or FM and TV reception on frequencies above about 40 Mc.

Below line-of-sight over plane earth or water, when the signal source is effectively at the horizon, the ground-reflected wave does not exist, so that the *direct* wave is the only component which goes to make up the space wave. But when both the signal source and the receiving antenna are elevated with respect to the intervening terrain, the ground-reflected wave is present and adds vectorially to the direct wave at the receiving antenna. The vectorial addition of the two waves, which travel over different path lengths (since one of the waves has been reflected from the ground) results in an interference pattern. The interference between the two waves brings about a cyclic variation in signal strength as the receiving antenna is raised above the ground. This effect is illustrated in figure 14. From this figure it can be seen that best space-wave reception of a v-h-f signal often will be obtained with the receiving antenna quite close to the ground. This subject, along with other aspects of v-h-f signal propagation and reception, are discussed in considerable detail in a book on fringe-area TV reception.*

The distance from an elevated point to the geometrical horizon is given by the approximate equation: $d = 1.22\sqrt{H}$ where the distance

* "Better TV Reception," by W. W. Smith and R. L. Dawley, published by Editors and Engineers, Ltd., Summerland, Calif.

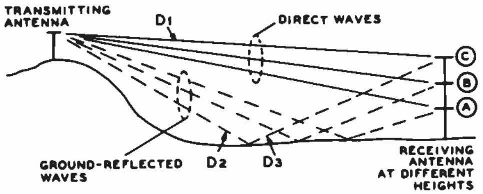


Figure 14

WAVE INTERFERENCE WITH HEIGHT

When the source of a horizontally-polarized space-wave signal is above the horizon, the received signal at a distant location will go through a cyclic variation as the antenna height is progressively raised. This is due to the difference in total path length between the direct wave and the ground-reflected wave, and to the fact that this path length difference changes with antenna height. When the path length difference is such that the two waves arrive at the receiving antenna with a phase difference of 360° or some multiple of 360°, the two waves will appear to be in phase as far as the antenna is concerned and maximum signal will be obtained. On the other hand, when the antenna height is such that the path length difference for the two waves causes the waves to arrive with a phase difference of an odd multiple of 180° the two waves will substantially cancel, and a null will be obtained at that antenna height. The difference between D_1 and D_2 plus D_3 is the path-length difference. Note also that there is an additional 180° phase shift in the ground-reflected wave at the point where it is reflected from the ground. It is this latter phase shift which causes the space-wave field intensity of a horizontally polarized wave to be zero with the receiving antenna at ground level.

d is in miles and the antenna height H is in feet. This equation must be applied separately to the transmitting and receiving antennas and the results added. However, refraction and diffraction of the signal around the spherical earth cause a smaller reduction in field strength than would occur in the absence of such bending, so that the average radio horizon is somewhat beyond the geometrical horizon. The equation $d = 1.4\sqrt{H}$ is sometimes used for determining the radio horizon.

Tropospheric Propagation Propagation by signal bending in the lower atmosphere, called *tropospheric propagation,* can result in the reception of signals over a much greater distance than would be the case if the lower atmosphere were homogeneous. In a homogeneous or well-mixed lower atmosphere, called a *normal* or *standard* atmosphere, there is a gradual and uniform decrease in index of refraction with height. This effect is due to the combined effects of a decrease in temperature, pressure, and water-vapor content with height.

This gradual decrease in refractive index with height causes waves radiated at very low angles with respect to the horizontal to be bent downward slightly in a curved path. The result of this effect is that such waves will be propagated beyond the *true* or *geometrical* horizon. In a so-called standard atmosphere the effect of the curved path is the same as though the radius of the earth were increased by approximately one third. This condition extends the horizon by approximately 30 per cent for normal propagation, and the extended-horizon is known as the *radio path horizon,* mentioned before.

Conditions Leading to Tropospheric Stratification When the temperature, pressure, or water-vapor content of the atmosphere does not change smoothly with rising altitude, the discontinuity or stratification will result in the reflection or refraction of incident v-h-f signals. Ordinarily this condition is more prevalent at night and in the summer. In certain areas, such as along the west coast of North America, it is frequent enough to be considered normal. Signal strength decreases slowly with distance and, if the favorable condition in the lower atmosphere covers sufficient area, the range is limited only by the transmitter power, antenna gain, receiver sensitivity, and signal-to-noise ratio. There is no skip distance. Usually, transmission due to this condition is accompanied by slow fading, although fading can be violent at a point where direct waves of about the same strength are also received.

Bending in the troposphere, which refers to the region from the earth's surface up to about 10 kilometers, is more likely to occur on days when there are stratus clouds than on clear, cool days with a deep blue sky. The temperature or humidity discontinuities may be broken up by vertical convection currents over land in the daytime but are more likely to continue during the day over water. This condition is in some degree predictable from weather information several days in advance. It does not depend on the sunspot cycle. Like direct communication, best results require similar antenna polarization or orientation at both the transmitting and receiving ends, whereas in transmission via reflection in the ionosphere (that part of the atmosphere between about 50 and 500 kilometers high) it makes little difference whether antennas are similarly polarized.

Duct Formation When bending conditions are particularly favorable they

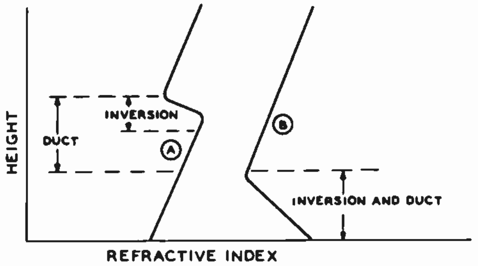


Figure 15

ILLUSTRATING DUCT TYPES

Showing two types of variation in refractive index with height which will give rise to the formation of a duct. An elevated duct is shown at (A), and a ground-based duct is shown at (B). Such ducts can propagate ground-wave signals far beyond their normal range.

may give rise to the formation of a *duct* which can propagate waves with very little attenuation over great distances in a manner similar to the propagation of waves through a wave guide. *Guided propagation* through a duct in the atmosphere can give quite remarkable transmission conditions (figure 15). However, such ducts usually are formed only on an over-water path. The depth of the duct over the water's surface may be only 20 to 50 feet, or it may be 1000 feet deep or more. Ducts exhibit a low-frequency cutoff characteristic similar to a wave guide. The cutoff frequency is determined by depth of the duct and by the strength of the discontinuity in refractive index at the upper surface of the duct. The lowest frequency that can be propagated by such a duct seldom goes below 50 Mc., and usually will be greater than 100 Mc. even along the Pacific Coast.

Stratospheric Reflection Communication by virtue of stratospheric reflection can be brought about during magnetic storms, aurora borealis displays, and during meteor showers. Dx communication during extensive meteor showers is characterized by frequent bursts of great signal strength followed by a rapid decline in strength of the received signal. The motion of the meteor forms an ionized trail of considerable extent which can bring about effective reflection of signals. However, the ionized region persists only for a matter of seconds so that a shower of meteors is necessary before communication becomes possible.

The type of communication which is possible during visible displays of the aurora borealis and during magnetic storms has been called *aurora-type dx.* These conditions reach a maximum somewhat after the sunspot cycle peak, possibly because the spots on the sun are nearer to its equator (and more directly in line with the earth) in the latter part of the cycle. Ionospheric storms generally accompany magnetic storms. The normal layers of the ionosphere may be churned or broken up, making radio transmission over long distances difficult or impossible on high frequencies. Unusual conditions in the ionosphere sometimes modulate v-h-f waves so that a definite tone or noise modulation is noticed even on transmitters located only a few miles away.

A pecularity of this type of auroral propagation of v-h-f signals in the northern hemisphere is that directional antennas usually must be pointed in a northerly direction for best results for transmission or reception, regardless of the direction of the other station being contacted. Distances out to 700 or 800 miles have been covered during magnetic storms, using 30 and 50 Mc. transmitters, with little evidence of any silent zone between the stations communicating with each other. Generally, voice-modulated transmissions are difficult or impossible due to the tone or noise modulation on the signal. Most of the communication of this type has taken place by c.w. or by tone modulated waves with a keyed carrier.

18-8 Ionospheric Propagation

Propagation of radio waves for communication on frequencies between perhaps 3 and 30 Mc. is normally carried out by virtue of *ionospheric reflection* or *refraction.* Under conditions of abnormally high ionization in the ionosphere, communication has been known to have taken place by ionospheric reflection on frequencies higher than 50 Mc.

The ionosphere consists of layers of ionized gas located above the stratosphere, and extending up to possibly 300 miles above the earth. Thus we see that high-frequency radio waves may travel over short distances in a direct line from the transmitter to the receiver, or they can be radiated upward into the ionosphere to be bent downward in an indirect ray, returning to earth at considerable distance from the transmitter. The wave reaching a receiver via the ionosphere route is termed a *sky wave.* The wave reaching a receiver by traveling in a direct line from the transmitting antenna to the receiving antenna is commonly called a *ground wave.*

The amount of bending at the ionosphere

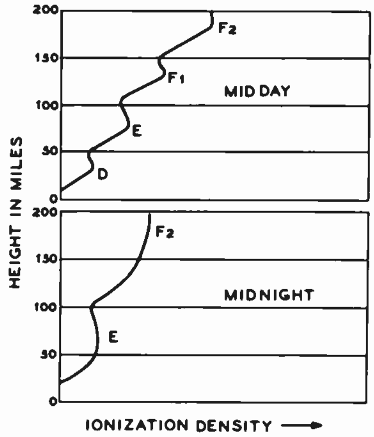


Figure 16

IONIZATION DENSITY IN THE IONOSPHERE

Showing typical ionization density of the ionosphere in mid-summer. Note that the F_1 and D layers disappear at night, and that the density of the E layer falls to such a low value that it is ineffective.

which the sky wave can undergo depends upon its frequency, and the amount of *ionization* in the ionosphere, which is in turn dependent upon radiation from the sun. The sun increases the density of the ionosphere layers (figure 16) and lowers their effective height. For this reason, the ionosphere acts very differently at different times of day, and at different times of the year.

The higher the frequency of a radio wave, the farther it penetrates the ionosphere, and the less it tends to be bent back toward the earth. The lower the frequency, the more easily the waves are bent, and the less they penetrate the ionosphere. 160-meter and 80-meter signals will usually be bent back to earth even when sent straight up, and may be considered as being *reflected* rather than *refracted*. As the frequency is raised beyond about 5,000 kc. (dependent upon the critical frequency of the ionosphere at the moment), it is found that waves transmitted at angles higher than a certain critical angle *never return to earth*. Thus, on the higher frequencies, it is necessary to confine radiation to low angles, since the high angle waves simply penetrate the ionosphere and are lost.

The F_2 Layer The higher of the two major reflection regions of the ionosphere is called the F_2 layer. This layer has a virtual height of approximately 175 miles at night, and in the daytime it splits up into two layers, the upper one being called the F_2 layer and the lower being called the F_1 layer. The height of the F_2 layer during daylight hours is normally about 250 miles on the average and the F_1 layer often has a height of as low as 140 miles. It is the F_2 layer which supports all nighttime dx communication and nearly all daytime dx propagation.

The E Layer Below the F_2 layer is another layer, called the *E* layer, which is of importance in daytime communication over moderate distances in the frequency range between 3 and 8 Mc. This layer has an almost constant height at about 70 miles. Since the re-combination time of the ions at this height is rather short, the *E* layer disappears almost completely a short time after local sunset.

The D Layer Below the *E* layer at a height of about 35 miles is an *absorbing* layer, called the *D* layer, which exists in the middle of the day in the summertime. The layer also exists during midday in the winter time during periods of high solar activity, but the layer disappears completely at night. It is this layer which causes high absorption of signals in the medium and high-frequency range during the middle of the day.

Critical Frequency The *critical frequency* of an ionospheric layer is the highest frequency which will be reflected when the wave strikes the layer at vertical incidence. The critical frequency of the most highly ionized layer of the ionosphere may be as low as 2 Mc. at night and as high as 12 to 13 Mc. in the middle of the day. The critical frequency is directly of interest in that a *skip-distance zone* will exist on all frequencies *greater* than the highest critical frequency at that time. The critical frequency is a measure of the density of ionization of the reflecting layers. The higher the critical frequency the greater the density of ionization.

Maximum Usable Frequency The *maximum usable frequency* or *m.u.f.* is of great importance in long-distance communication since this frequency is the highest that can be used for communication *between any two specified areas*. The m.u.f. is the highest frequency at which a wave projected into space in a certain direction will be returned to earth in a specified region by ionospheric reflection. The m.u.f. is highest at noon or in the early afternoon and is highest in periods of greatest sunspot activity, often going to frequencies higher than 50 Mc. (figure 17).

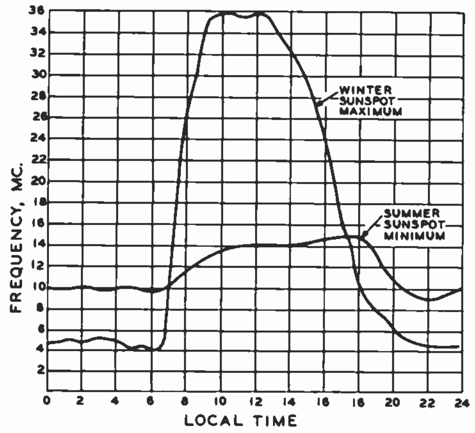


Figure 17

TYPICAL CURVES SHOWING CHANGE IN M.U.F. AT MAXIMUM AND MINIMUM POINTS IN SUNSPOT CYCLE

The m.u.f. often drops to frequencies below 10 Mc. in the early morning hours. The high m.u.f. in the middle of the day is brought about by reflection from the F_2 layer. M.u.f. data is published periodically in the magazines devoted to amateur work, and the m.u.f. can be calculated with the aid of *Basic Radio Propagation Predictions,* CRPL-D, published monthly by the Government Printing Office, Washington, D.C.

Absorption and Optimum Working Frequency The optimum working frequency for any particular direction and distance is usually about 15 per cent less than the m.u.f. for contact with that particular location. The absorption by the ionosphere becomes greater and greater as the operating frequency is progressively lowered below the m.u.f. It is this condition which causes signals to increase tremendously in strength on the 14-Mc. and 28-Mc. bands just before the signals drop completely out. At the time when the signals are greatest in amplitude the operating frequency is equal to the m.u.f. Then as the signals drop out the m.u.f. has become lower than the operating frequency.

Skip Distance The shortest distance from a transmitting location at which signals reflected from the ionosphere can be returned to the earth is called the *skip distance.* As was mentioned above under *Critical Frequency* there is no skip distance for a frequency below the critical frequency of the most highly ionized layer of the ionosphere at the time of transmission. However, the skip distance is always present on the 14-Mc. band and is almost always present on the 3.5-Mc. and 7-Mc. bands at night. The actual measure of the skip distance is the distance between the point where the ground wave falls to zero and the point where the sky wave begins to return to earth. This distance may vary from 40 to 50 miles on the 3.5-Mc. band to thousands of miles on the 28-Mc. band.

The Sporadic-E Layer Occasional patches of extremely high ionization density appear at intervals throughout the year at a height approximately equal to that of the *E* layer. These patches, called the *sporadic-E* layer may be very small or may be up to several hundred miles in extent. The critical frequency of the *sporadic-E* layer may be greater than twice that of the normal ionosphere layers which exist at the same time.

It is this *sporadic-E* condition which provides "short-skip" contacts from 400 to perhaps 1200 miles on the 28-Mc. band in the evening. It is also the *sporadic-E* condition which provides the more common type of "band opening" experienced on the 50-Mc. band when very loud signals are received from stations from 400 to 1200 miles distant.

Cycles in Ionosphere Activity The ionization density of the ionosphere is determined by the amount of radiation (probably ultra violet) which is being received from the sun. Consequently, ionosphere activity is a function of the amount of radiation of the proper character being emitted by the sun and is also a function of the relative aspect of the regions in the vicinity of the location under discussion to the sun. There are four main cycles in ionosphere activity. These cycles are: the daily cycle which is brought about by the rotation of the earth, the 27-day cycle which is caused by the rotation of the sun, the seasonal cycle which is caused by the movement of the earth in its orbit, and the 11-year cycle which is a cycle in sunspot activity. The effects of these cycles are superimposed insofar as ionosphere activity is concerned. Also, the cycles are subject to short term variations as a result of magnetic storms and similar terrestrial disturbances.

The most recent minimum of the 11-year sunspot cycle occured during the winter of 1954-1955, and we are currently moving up the slope of a new cycle, the maximum of which will probably occur during the year 1958. The current cycle is pictured in figure 18.

Fading The lower the angle of radiation of the wave, with respect to the hori-

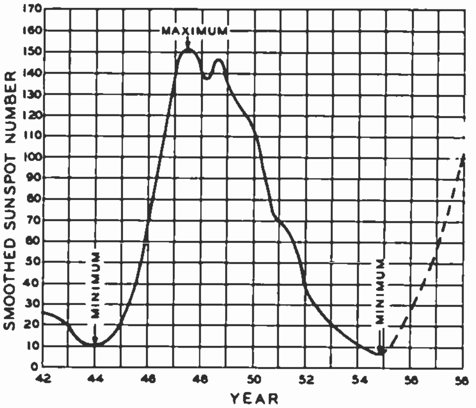


Figure 18

THE YEARLY TREND OF THE 11-YEAR SUNSPOT CYCLE. RADIO CONDITIONS IN GENERAL WILL IMPROVE DURING 1955-1958 AS THE CYCLE ADVANCES

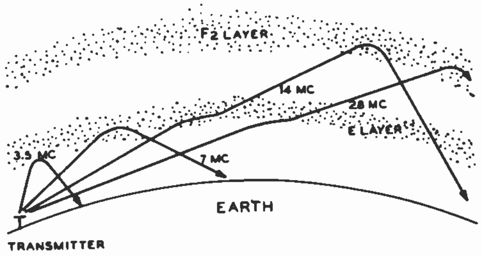


Figure 19

IONOSPHERE-REFLECTION WAVE PATHS

Showing typical ionosphere-reflection wave paths during daylight hours when ionization density is such that frequencies as high as 28 Mc. will be returned to earth. The distance between ground-wave range and that range where the ionosphere-reflected wave of a specific frequency first will be returned to earth is called the skip distance.

zon, the farther away will the wave return to earth, and the greater the skip distance. The wave can be reflected back up into the ionosphere by the earth, and then be reflected back down again, causing a second skip distance area. The drawing of figure 19 shows the multiple reflections possible. When the receiver receives signals which have traveled over more than one path between transmitter and receiver, the signal impulses will not all arrive at the same instant, as they do not all travel the same distance. When two or more signals arrive in the same phase at the receiving antenna, the resulting signal in the receiver will be quite strong. On the other hand, if the signals arrive 180° out of phase, so they tend to cancel each other, the received signal will drop—perhaps to zero if perfect cancellation occurs. This explains why high-frequency signals are subject to fading.

Fading can be greatly reduced on the high frequencies by using a transmitting antenna with sharp vertical directivity, thus cutting down the number of possible paths of signal arrival. A receiving antenna with similar characteristics (sharp vertical directivity) will further reduce fading. It is desirable, when using antennas with sharp vertical directivity, to use the lowest vertical angle consistent with good signal strength for the frequency used.

Scattered Reflections Scattered reflections are random, diffused, substantially isotropic reflections which are partly responsible for reception within the skip zone, and for reception of signals from directions off the great circle path.

In a heavy fog or mist, it is difficult to see the road at night because of the bright glare caused by scattered reflection of the headlight beam by the minute droplets. In fact, the road directly to the side of the car will be weakly illuminated under these conditions, whereas it would not on a clear night (assuming flat, open country). This is a good example of propagation of waves by scattered reflections into a zone which otherwise would not be illuminated.

Scattering occurs in the ionosphere at all times, because of irregularities in the medium (which result in "patches" corresponding to the water droplets) and because of random-phase radiation due to the collision or recombination of free electrons. However, the nature of the scattering varies widely with time, in a random fashion. Scattering is particularly prevalent in the *E* region, but scattered reflections may occur at any height, even well out beyond the virtual height of the F_2 layer.

There is no "critical frequency" or "lowest perforating frequency" involved in the scattering mechanism, though the intensity of the scattered reflections due to typical scattering in the *E* region of the ionosphere decreases with frequency.

When the received signal is due primarily to scattered reflections, as is the case in the skip zone or where the great circle path does not provide a direct sky wave (due to low critical or perforation frequency, or to an ionosphere storm) very bad distortion will be evident, particularly a "flutter fade" and a characteristic "hollow" or echo effect.

Deviations from a great circle path are especially noticeable in the case of great circle paths which cross or pass near the auroral zones, because in such cases there often is complete or nearly complete absorption of the direct sky wave, leaving off-path scattered reflections the only mechanism of propagation. Under such conditions the predominant wave will appear to arrive from a direction closer to the equator, and the signal will be noticeably if not considerably weaker than a direct sky wave which is received under favorable conditions.

Irregular reflection of radio waves from "scattering patches" is divided into two categories: "short scatter" and "long scatter".

Short scatter is the scattering that occurs when a radio wave first reaches the scattering patches or media. Ordinarily it is of no particular benefit, as in most cases it only serves to fill in the inner portion of the skip zone with a weak, distorted signal.

Long scatter occurs when a wave has been refracted from the F_2 layer and strikes scattering patches or media on the way down. When the skip distance exceeds several hundred miles, long scatter is primarily responsible for reception within the skip zone, particularly the outer portion of the skip zone. Distortion is much less severe than in the case of short scatter, and while the signal is likewise weak, it sometimes can be utilized for satisfactory communication.

During a severe ionosphere disturbance in the north auroral zone, it sometimes is possible to maintain communication between the Eastern United States and Northern Europe by the following mechanism: That portion of the energy which is radiated in the direction of the great circle path is completely absorbed upon reaching the auroral zone. However, the portion of the wave leaving the United States in a *southeasterly* direction is refracted downward from the F_2 layer and encounters scattering patches or media on its downward trip at a distance of approximately 2000 miles from the transmitter. There it is reflected by "long scatter" in all directions, this scattering region acting like an isotropic radiator fed with a very small fraction of the original transmitter power. The great circle path from this southerly point to northern Europe does not encounter unfavorable ionosphere conditions, and the wave is propagated the rest of the trip as though it had been radiated from the scattering region.

Another type of scatter is produced when a sky wave strikes certain areas of the earth. Upon striking a comparatively smooth surface such as the sea, there is little scattering, the wave being shot up again by what could be considered specular or mirror reflection. But upon striking a mountain range, for instance, the reradiation or reflected energy is scattered, some of it being directed back towards the transmitter, thus providing another mechanism for producing a signal within the skip zone.

Meteors and "Bursts" When a meteor strikes the earth's atmosphere, a cylindrical region of free electrons is formed at approximately the height of the E layer. This slender ionized column is quite long, and when first formed is sufficiently dense to reflect radio waves back to earth most readily, *including v-h-f waves which are not ordinarily returned by the F_2 layer.*

The effect of a single meteor, of normal size, shows up as a sudden "burst" of signal of short duration at points not ordinarily reached by the transmitter. After a period of from 10 to 40 seconds, recombination and diffusion have progressed to the point where the effect of a *single* fairly large meteor is not perceptible. However, there are many *small* meteors impinging upon earth's atmosphere every minute, and the *aggregate* effect of their transient ionized trails, including the small amount of residual ionization that exists for several minutes after the original flash but is too weak and dispersed to prolong a "burst", is believed to contribute to the existence of the "nighttime E" layer, and perhaps also to sporadic E patches.

While there are many of these very small meteors striking the earth's atmosphere every minute, meteors of normal size (sufficiently large to produce individual "bursts") do not strike nearly so frequently except during some of the comparatively rare meteor "showers". During one of these displays a "quivering" ionized layer is produced which is intense enough to return signals in the lower v-h-f range with good strength, but with a type of "flutter" distortion which is characteristic of this type of propagation.

18-9 Transmission Lines

For many reasons it is desirable to place an antenna or radiating system as high and in the clear as is physically possible, utilizing some form of nonradiating transmission line to carry energy with as little loss as possible from the transmitter to the radiating antenna, and conversely from the antenna to the receiver.

There are many different types of transmission lines and, generally speaking, practically any type of transmission line or feeder system may be used with any type of antenna. However, mechanical or electrical considerations often make one type of transmission line better adapted for use to feed a particular type of antenna than any other type.

Transmission lines for carrying r-f energy are of two general types: ***non-resonant*** and ***resonant.*** A non-resonant transmission line is one on which a successful effort has been made to eliminate reflections from the termination (the antenna in the transmitting case and the receiver for a receiving antenna) and hence one on which standing waves do not exist or are relatively small in magnitude. A resonant line, on the other hand, is a transmission line on which standing waves of appreciable magnitude do appear, either through inability to match the characteristic impedance of the line to the termination or through intentional design.

The principal types of transmission line in use or available at this time include the open-wire line (two-wire and four-wire types), two-wire solid-dielectric line ("Twin-Lead" and similar ribbon or tubular types), two-wire polyethylene-filled shielded line, coaxial line of the solid-dielectric, beaded, stub-supported, or pressurized type, rectangular and cylindrical wave guide, and the single-wire feeder operated against ground. The significant characteristics of the more popular types of transmission line available at this time are given in the chart of figure 21.

18-10 Non-Resonant Transmission Lines

A non-resonant or untuned transmission line is a line with negligible standing waves. Hence, a non-resonant line is a line carrying r-f power only in one direction—from the source of energy to the load.

Physically, the line itself should be ***identical throughout its length.*** There will be a smooth distribution of voltage and current throughout its length, both tapering off very slightly towards the load end of the line as a result of line losses. The attenuation (loss) in certain types of untuned lines can be kept very low for line lengths up to several thousand feet. In other types, particularly where the dielectric is not air (such as in the twisted-pair line), the losses may become excessive at the higher frequencies, unless the line is relatively short.

Transmission-Line Impedance All transmission lines have distributed inductance, capacitance and resistance. Neglecting the resistance, as it is of minor importance in short lines, it is found

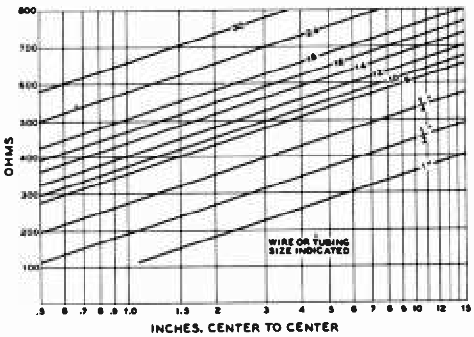


Figure 20

CHARACTERISTIC IMPEDANCE OF TYPICAL TWO-WIRE OPEN LINES

that the ***inductance and capacitance per unit length*** determine the characteristic or surge impedance of the line. Thus, the surge impedance depends upon the nature and spacing of the conductors, and the dielectric separating them.

Speaking in electrical terms, the characteristic impedance of a transmission line is simply the ratio of the voltage across the line to the current which is flowing, the same as is the case with a simple resistor: $Z_o = E/I$. Also, in a substantially loss-less line (one whose attenuation per wavelength is small) the energy stored in the line will be equally divided between the capacitive field and the inductive field which serve to propagate the energy along the line. Hence the characteristic impedance of a line may be expressed as:

$$Z_o = \sqrt{L/C}.$$

Two-Wire Open Line A two-wire transmission system is easy to construct. Its surge impedance can be calculated quite easily, and when properly adjusted and balanced to ground, with a conductor spacing which is negligible in terms of the wavelength of the signal carried, undesirable feeder radiation is minimized; the current flow in the adjacent wires is in opposite directions, and the magnetic fields of the two wires are in opposition to each other. When a two-wire line is terminated with the equivalent of a pure resistance equal to the characteristic impedance of the line, the line becomes a non-resonant line.

Expressed in physical terms, the characteristic impedance of a two-wire open line is equal to:

CHARACTERISTICS OF COMMON TRANSMISSION LINES

	ATTENUATION db/100 FEET VSWR = 1.0			VELOCITY FACTOR V	µµFD PER FT.	REMARKS
	30 MC	100 MC	300 MC			
OPEN WIRE LINE, Nº 12 COPPER.	0.15	0.3	0.6	0.96-0.99	—	BASED UPON 4" SPACING BELOW 50 MC.; 2" SPACING ABOVE 50 MC. RADIATION LOSSES INCLUDED. CLEAN, LOW LOSS CERAMIC INSULATION ASSUMED. RADIATION HIGH ABOVE 150 MC.
RIBBON LINE, REC. TYPE, 300 OHMS. (7/28 CONDUCTORS)	0.86	2.2	5.3	0.82 ✓	6 ✓	FOR CLEAN, DRY LINE. WET WEATHER PERFORMANCE RATHER POOR. BEST LINE IS SLIGHTLY CONVEX. AVOID LINE THAT HAS CONCAVE DIELECTRIC. SUITABLE FOR LOW POWER TRANSMITTING APPLICATIONS. LOSSES INCREASE AS LINE WEATHERS. HANDLES 400 WATTS AT 30 MC. IF VSWR IS LOW.
TUBULAR "TWIN-LEAD" REC. TYPE, 300 OHMS, 5/16" O.D., (AMPHENOL TYPE 14-271)	—	—	—	—	—	CHARACTERISTICS SIMILAR TO RECEIVING TYPE RIBBON LINE EXCEPT FOR MUCH BETTER WET WEATHER PERFORMANCE.
RIBBON LINE, TRANS. TYPE, 300 OHMS.	—	—	—	—	—	CHARACTERISTICS VARY SOMEWHAT WITH MANUFACTURER, BUT APPROXIMATE THOSE OF RECEIVING TYPE RIBBON EXCEPT FOR GREATER POWER HANDLING CAPABILITY AND SLIGHTLY BETTER WET WEATHER PERFORMANCE.
TUBULAR "TWIN-LEAD" TRANS. TYPE, 7/16 O.D. (AMPHENOL 14-076)	0.65	2.3	5.4	0.79	6.1	FOR USE WHERE RECEIVING TYPE TUBULAR "TWIN-LEAD" DOES NOT HAVE SUFFICIENT POWER HANDLING CAPABILITY. WILL HANDLE 1 KW AT 30 MC. IF VSWR IS LOW.
RIBBON LINE, RECEIVE. TYPE, 150 OHMS.	1.1	2.7	6.0	0.77 ✓	10 ✓	USEFUL FOR QUARTER WAVE MATCHING SECTIONS. NO LONGER WIDELY USED AS A LINE.
RIBBON LINE, RECEIVE. TYPE, 75 OHMS.	2.0	5.0	11.0	0.68 ✓	19 ✓	USEFUL MAINLY IN THE H-F RANGE BECAUSE OF EXCESSIVE LOSSES AT V-H-F AND U-H-F. LESS AFFECTED BY WEATHER THAN 300 OHM RIBBON.
RIBBON LINE, TRANS. TYPE, 75 OHMS.	1.5	3.9	8.0	0.71 ✓	18 ✓	VERY SATISFACTORY FOR TRANSMITTING APPLICATIONS BELOW 30 MC. AT POWERS UP TO 1 KW. NOT SIGNIFICANTLY AFFECTED BY WET WEATHER.
RG-8/U COAX (52 OHMS)	1.0	2.1	4.2	0.66	29.5	WILL HANDLE 2 KW AT 30 MC. IF VSWR IS LOW. 0.4" O.D. 7/21 CONDUCTOR.
RG-11/U COAX (75 OHMS)	0.94	1.9	3.8	0.66	20.5	WILL HANDLE 1.4 KW AT 30 MC. IF VSWR IS LOW. 0.4" O.D. 7/26 CONDUCTOR.
RG-17/U COAX (52 OHMS)	0.38	0.85	1.6	0.66	29.5	WILL HANDLE 7.8 KW. AT 30 MC. IF VSWR IS LOW. 0.87" O.D. 0.19" DIA. CONDUCTOR
RG-58/U COAX (53 OHMS)	1.95	4.1	8.0	0.66	28.5	WILL HANDLE 430 WATTS AT 30 MC. IF VSWR IS LOW. 0.2" O.D. Nº 20 CONDUCTOR.
RG-59/U COAX (73 OHMS)	1.9	3.8	7.0	0.66	21	WILL HANDLE 680 WATTS AT 30 MC. IF VSWR IS LOW. 0.24" O.D. Nº 22 CONDUCTOR.
TV-59 COAX (72 OHMS)	2.0	4.0	7.0	0.66	22	"COMMERCIAL" VERSION OF RG-59/U FOR LESS EXACTING APPLICATIONS. LESS EXPENSIVE.
RG-22/U SHIELDED PAIR (95 OHMS)	1.7	3.0	5.5	0.66	16	FOR SHIELDED, BALANCED-TO-GROUND APPLICATIONS. VERY LOW NOISE PICK UP. 0.4" O.D.
K-111 SHIELDED PAIR (300 OHMS)	2.0	3.5	6.1	—	4	DESIGNED FOR TV LEAD-IN IN NOISY LOCATIONS. LOSSES HIGHER THAN REGULAR 300 OHM RIBBON, BUT DO NOT INCREASE AS MUCH FROM WEATHERING.

✓ APPROXIMATE. EXACT FIGURE VARIES SLIGHTLY WITH MANUFACTURER.

FIGURE 21

$$Z_0 = 276 \log_{10} \frac{2S}{d}$$

Where:

S is the exact distance between wire centers in some convenient unit of measurement, and

d is the diameter of the wire measured in the same units as the wire spacing, S.

Since $\frac{2S}{d}$ expresses a ratio only, the units of measurement may be centimeters, millimeters, or inches. This makes no difference in the answer, so long as the substituted values for S and d are in the *same units.*

The equation is accurate *so long as the wire spacing is relatively large as compared to the wire diameter.*

Surge impedance values of less than 200 ohms are seldom used in the open-type two-wire line, and, even at this rather high value of Z_0 the wire spacing S is uncomfortably close, being only 5.3 times the wire diameter d.

Figure 20 gives in graphical form the surge impedance of practicable two-wire lines. The chart is self-explanatory, and is sufficiently accurate for practical purposes.

Ribbon and Tubular Transmission Line Instead of using spacer insulators placed periodically along the transmission line it is possible to mold the line conductors into a ribbon or tube of flexible low-loss dielectric material. Such line, with polyethylene dielectric, is used in enormous quantities as the lead-in transmission line for FM and TV receivers. The line is available from several manufacturers in the ribbon and tubular configuration, with characteristic impedance values from 75 to 300 ohms. Receiving types, and transmitting types for power levels up to one kilowatt in the h-f range, are listed with their pertinent characteristics, in the table of figure 21.

Coaxial Line Several types of coaxial cable have come into wide use for feeding power to an antenna system. A cross-sectional view of a coaxial cable (sometimes called concentric cable or line) is shown in figure 22.

As in the parallel-wire line, the power lost in a properly terminated coaxial line is the sum of the effective resistance losses along the length of the cable and the dielectric losses between the two conductors.

Of the two losses, the effective resistance loss is the greater; since it is largely due to the skin effect, the line loss (all other conditions the same) will increase directly as the square root of the frequency.

Figure 22 shows that, instead of having two conductors running side by side, one of the conductors is placed *inside* of the other. Since the outside conductor completely shields the inner one, no radiation takes place. The conductors may both be tubes, one within the other; the line may consist of a solid wire within a tube, or it may consist of a stranded or solid inner conductor with the outer conductor made up of one or two wraps of copper shielding braid.

In the type of cable most popular for military and non-commercial use the inner conductor consists of a heavy stranded wire, the outer conductor consists of a braid of copper wire, and the inner conductor is supported within the outer by means of a semi-solid dielectric of exceedingly low loss characteristics called polyethylene. The Army-Navy designation on one size of this cable suitable for power levels up to one kilowatt at frequencies as high as 30 Mc. is AN/RG-8/U. The outside diameter of this type of cable is approximately one-half inch. The characteristic impedance of this cable type is 52 ohms, but other similar types of greater and smaller power-handling capacity are available in impedances of 52, 75, and 95 ohms.

When using solid dielectric coaxial cable it is necessary that precautions be taken to insure that moisture cannot enter the line. If the better grade of connectors manufactured for the line are employed as terminations, this condition is automatically satisfied. If connectors are not used, it is necessary that some type of moisture-proof sealing compound be applied to the end of the cable where it will be exposed to the weather.

Nearby metallic objects cause no loss, and coaxial cable may be run up air ducts or elevator shafts, inside walls, or through metal conduit. Insulation troubles can be forgotten. The coaxial cable may be buried in the ground or suspended above ground.

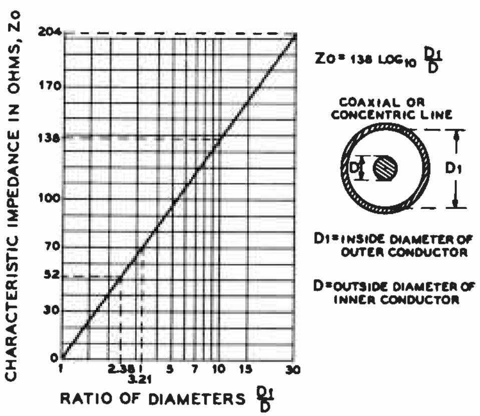


Figure 22

CHARACTERISTIC IMPEDANCE OF AIR-FILLED COAXIAL LINES

If the filling of the line is a dielectric material other than air, the characteristic impedance of the line will be reduced by a factor proportional to the square-root of the dielectric constant of the material used as a dielectric within the line.

Standing Waves Standing waves on a transmission line *always* are the result of the reflection of energy. The only significant reflection which takes place in a normal installation is that at the load end of the line. But reflection can take place from discontinuities in the line, such as caused by insulators, bends, or metallic objects adjacent to an unshielded line.

When a uniform transmission line is terminated in an impedance equal to its surge impedance, reflection of energy does not occur, and no standing waves are present. When the load termination is exactly the same as the line impedance, it simply means that the load takes energy from the line just as fast as the line delivers it, no slower and no faster.

Thus, for proper operation of an untuned line (with standing waves eliminated), some form of impedance-matching arrangement must be used between the transmission line and the antenna, so that the radiation resistance of the antenna is reflected back into the line as a nonreactive impedance equal to the line impedance.

The termination at the antenna end is the only critical characteristic about the untuned line fed by a transmitter. It is the reflection from the antenna end which starts waves moving back toward the transmitter end. When waves moving in both directions along a conductor meet, standing waves are set up.

Semi-Resonant Parallel-Wire Lines A well-constructed open-wire line has acceptably low losses when its length is less than about two wavelengths even when the voltage standing-wave ratio is as high as 10 to 1. A transmission line constructed of ribbon or tubular line, however, should have the standing-wave ratio kept down to not more than about 3 to 1 both to reduce power loss and because the energy dissipation on the line will be localized, causing overheating of the line at the points of maximum current.

Because moderate standing waves can be tolerated on open-wire lines without much loss, a standing-wave ratio of 2/1 or 3/1 is considered acceptable with this type of line, *even when used in an untuned system.* Strictly speaking, a line is untuned, or non-resonant, only when it is perfectly *flat,* with a standing-wave ratio of 1 (no standing waves). However, some mismatch can be tolerated with open-wire untuned lines, so long as the reactance is not objectionable, or is eliminated by cutting the line to approximately resonant length.

18-11 Tuned or Resonant Lines

If a transmission line is terminated in its *characteristic surge impedance,* there will be no reflection at the end of the line, and the current and voltage distribution will be uniform along the line. If the end of the line is either open-circuited or short-circuited, the reflection at the end of the line will be 100 per cent, and *standing waves* of very great amplitude will appear on the line. There will still be practically no radiation from the line if it is closely spaced, but voltage nodes will be found every half wavelength, the voltage loops corresponding to current nodes (figure 23).

If the line is terminated in some value of resistance other than the characteristic surge impedance, there will be some reflection, the amount being determined by the amount of mismatch. With reflection, there will be standing waves (excursions of current and voltage) along the line, though not to the same extent as with an open-circuited or short-circuited line. The current and voltage loops will occur at the same *points* along the line as with the open or short-circuited line, and as the terminating impedance is made to approach the characteristic impedance of the line, the current and voltage along the line will become more uniform. The foregoing assumes, of course, a purely resistive (non-reactive) load. If the load is reactive, standing waves also will be formed. But with a reactive load the nodes will occur at different locations from the node locations encountered with wrong-value resistive termination.

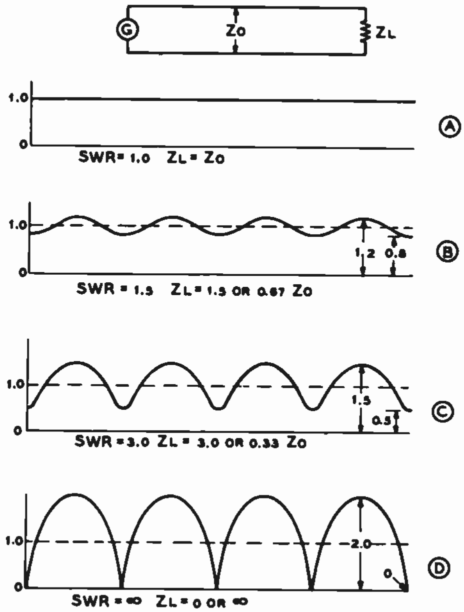


Figure 23
STANDING WAVES ON A TRANSMISSION LINE

As shown at (A), the voltage and current are constant on a transmission line which is terminated in its characteristic impedance, assuming that losses are small enough so that they may be neglected. (B) shows the variation in current or in voltage on a line terminated in a load with a reflection coefficient of 0.2 so that a standing wave ratio of 1.5 to 1 is set up. At (C) the reflection coefficient has been increased to 0.5, with the formation of a 3 to 1 standing-wave ratio on the line. At (D) the line has been terminated in a load which has a reflection coefficient of 1.0 (short, open circuit, or a pure reactance) so that all the energy is reflected with the formation of an infinite standing-wave ratio.

A well built 500- to 600-ohm transmission line may be used as a resonant feeder for lengths up to several hundred feet with very low loss, so long as the amplitude of the standing waves (ratio of maximum to minimum voltage along the line) is *not too great.* The amplitude, in turn, depends upon the mismatch at the line termination. A line of no. 12 wire, spaced 6 inches with good ceramic or plastic spreaders, has a surge impedance of approximately 600 ohms, and makes an excellent tuned feeder for feeding anything between 60 and 6000 ohms (at frequencies below 30 Mc.). If used to feed a load of higher or lower impedance than this, the standing waves become great enough in amplitude that some loss will occur unless the feeder is kept short. At frequencies above 30 Mc., the spacing becomes an appreciable fraction of a wavelength, and radiation from the line no longer is negligible. Hence, coaxial line or close-spaced parallel-wire line is recommended for v-h-f work.

If a transmission line is not perfectly matched, it should be made *resonant*, even though the amplitude of the standing waves (voltage variation) is not particularly great. This prevents reactance from being coupled into the final amplifier. A feed system having moderate standing waves may be made to present a non-reactive load to the amplifier either by tuning or by pruning the feeders to approximate resonance.

Usually it is preferable with tuned feeders to have a current loop (voltage minimum) at the transmitter end of the line. This means that when voltage-feeding an antenna, the tuned feeders should be made an odd number of quarter wavelengths long, and when current-feeding an antenna, the feeders should be made an even number of quarter wavelengths long. Actually, the feeders are made about 10 per cent of a quarter wave longer than the calculated value (the value given in the tables) when they are to be series tuned to resonance by means of a capacitor, instead of being trimmed and pruned to resonance.

When tuned feeders are used to feed an antenna on more than one band, it is necessary to compromise and make provision for both series and parallel tuning, inasmuch as it is impossible to cut a feeder to a length that will be optimum for several bands. If a voltage loop appears at the transmitter end of the line on certain bands, parallel tuning of the feeders will be required in order to get a transfer of energy. It is impossible to transfer energy by inductive coupling unless current is flowing. This is effected at a voltage loop by the presence of the resonant tank circuit formed by parallel tuning of the antenna coil.

CHAPTER NINETEEN

Antennas and Antenna Matching

Antennas for the lower frequency portion of the h-f spectrum (perhaps from 1.8 to 7.0 Mc.), and temporary or limited use antennas for the upper portion of the h-f range, usually are of a relatively simple type in which directivity is not a prime consideration. Also, it often is desirable, in amateur work, that a single antenna system be capable of operation at least on the 3.5-Mc. and 7.0-Mc. range, and preferably on other frequency ranges. Consequently, the first portion of this chapter will be devoted to a discussion of such antenna systems. The latter portion of the chapter is devoted to the general problem of matching the antenna transmission line to antenna systems of the fixed type. Matching the antenna transmission line to the rotatable directive array is discussed in Chapter Twenty-two.

19-1 End-Fed Half-Wave Horizontal Antennas

The half-wave horizontal dipole is the most common and the most practical antenna for the 3.5-Mc. and 7-Mc. amateur bands. The form of the dipole, and the manner in which it is fed are capable of a large number of variations. Figure 2 shows a number of practicable forms of the simple dipole antenna along with methods of feed.

Usually a high-frequency doublet is mounted as high and as much in the clear as possible, for obvious reasons. However, it is sometimes justifiable to bring part of the radiating system directly to the transmitter, feeding the antenna without benefit of a transmission line. This is permissible when (1) there is insufficient room to erect a 75- or 80-meter horizontal dipole and feed line, (2) when a long wire is also to be operated on one of the higher frequency bands on a harmonic. In either case, it is usually possible to get the main portion of the antenna in the clear because of its length. This means that the power lost by bringing the antenna directly to the transmitter is relatively small.

Even so, it is not best practice to bring the high-voltage end of an antenna into the operating room because of the increased difficulty in eliminating BCI and TVI. For this reason one should dispense with a feed line in conjunction with a Hertz antenna only as a last resort.

End-Fed Antennas The end-fed antenna has no form of transmission line to couple it to the transmitter, but brings the radiating portion of the antenna right down to the transmitter, where some form of coupling system is used to transfer energy to the antenna.

Figure 1 shows two common methods of feeding the *Fuchs antenna or end-fed Hertz.*

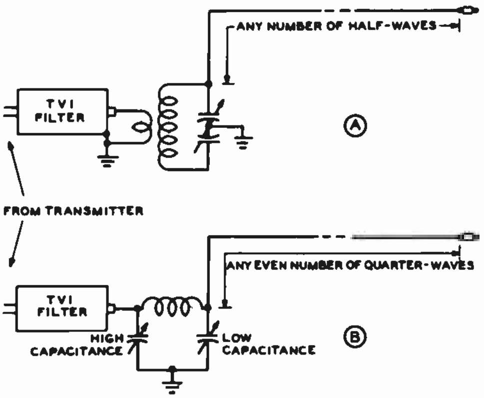


Figure 1
THE END-FED HERTZ ANTENNA

Showing the manner in which an end-fed Hertz antenna may be fed through a low-impedance line and low-pass filter by using a resonant tank circuit as at (A), or through the use of a reverse-connected pi network as at (B).

Some harmonic-attenuating provision (in addition to the usual low-pass TVI filter) must be included in the coupling system, as an end-fed antenna itself offers no discrimination against harmonics, either odd or even.

The end-fed Hertz antenna has rather high losses unless at least three-quarters of the radiator can be placed outside the operating room and in the clear. As there is r-f voltage at the point where the antenna enters the operating room, the insulation at that point should be several times as effective as the insulation commonly used with low-voltage feeder systems. This antenna can be operated on all of its higher harmonics with good efficiency, and can be operated at half frequency against ground as a quarter-wave Marconi.

As the frequency of an antenna is raised slightly when it is bent anywhere except at a voltage or current loop, an end-fed Hertz antenna usually is a few per cent longer than a straight half-wave doublet for the same frequency, because, ordinarily, it is impractical to bring a wire in to the transmitter without making several bends.

The Zepp Antenna System The *zeppelin* or *zepp antenna system,* illustrated in figure 2A is very convenient when it is desired to operate a single radiating wire on a number of harmonically related frequencies.

The zepp antenna system is easy to tune, and can be used on several bands by merely retuning the feeders. The overall efficiency of the zepp antenna system is not quite as high for long feeder lengths as for some of the antenna systems which employ non-resonant transmission lines, but where space is limited and where operation on more than one band is desired, the zepp has some decided advantages.

As the radiating portion of the zepp antenna system must always be some multiple of a half wave long, there is always high voltage present at the point where the live zepp feeder attaches to the end of the radiating portion of the antenna. Thus, this type of zepp antenna system is *voltage fed.*

Stub-Fed Zepp-Type Radiator Figure 2C shows a modification of the zepp-type antenna system to allow the use of a non-resonant transmission line between the radiating portion of the antenna and the transmitter. The *zepp* portion of the antenna is resonated as a quarter-wave stub and the non-resonant feeders are connected to the stub at a point where standing waves on the feeder are minimized. The procedure for making these adjustments is described in detail in Section 19-8. This type of antenna system is quite satisfactory when it is necessary physically to end feed the antenna, but where it is necessary also to use non-resonant feeder between the transmitter and the radiating system.

19-2 Center-Fed Half-Wave Horizontal Antennas

The center feeding of a half-wave antenna system is usually to be desired over an end-fed system since the center-fed system is inherently balanced to ground and is therefore less likely to be troubled by feeder radiation. A number of center-fed systems are illustrated in figure 2.

The Tuned Doublet The current-fed doublet with spaced feeders, sometimes called a *center-fed zepp,* is an inherently balanced system if the two legs of the radiator are electrically equal. This fact holds true regardless of the frequency, or of the harmonic, on which the system is operated. The system can successfully be operated over a wide range of frequencies if the system as a whole (both tuned feeders and the center-fed flat top) can be resonated to the operating frequency. It is usually possible to tune such an antenna system to resonance with the aid of a tapped coil and a tuning capacitor that can optionally be placed either

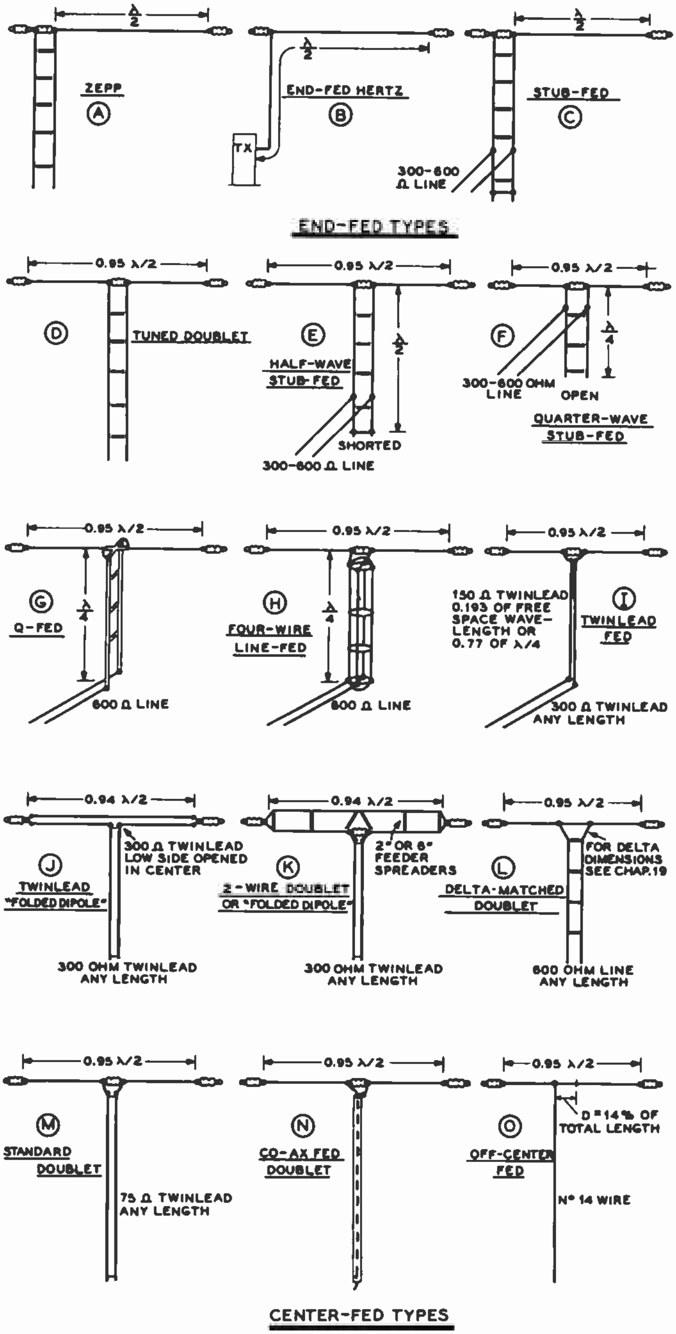


Figure 2

ALTERNATIVE METHODS OF FEEDING A HALF-WAVE DIPOLE

in series with the antenna coil or in parallel with it. A series tuning capacitor can be placed in series with one feeder leg without unbalancing the system.

The tuned-doublet antenna is shown in figure 2D. The antenna is a current-fed system when the radiating wire is a half wave long electrically, or when the system is operated on its odd harmonics, but becomes a voltage-fed radiator when operated on its even harmonics.

The antenna has a different radiation pattern when operated on its harmonics, as would be expected. The arrangement used on the second harmonic is better known as the *Franklin colinear array* and is described in Chapter Twenty. The pattern is similar to a half-wave dipole except that it is sharper in the broadside direction. On higher harmonics of operation there will be multiple lobes of radiation from the system.

Figures 2E and 2F show alternative arrangements for using an untuned transmission line between the transmitter and the tuned-doublet radiator. In figure 2E a half-wave shorted line is used to resonate the radiating system, while in figure 2F a quarter-wave open line is utilized. The adjustment of quarter-wave and half-wave stubs is discussed in Section 19-8.

Doublets with Quarter-Wave Transformers The average value of feed impedance for a center-fed half-wave doublet is 75 ohms. The actual value varies with height and is shown in Chapter Eighteen. Alternative methods of matching this rather low value of impedance to a medium-impedance transmission line are shown in (G), (H), and (I) of figure 2. Each of these three systems uses a quarter-wave transformer to accomplish the impedance transformation. The only difference between the three systems lies in the type of transmission line used in the quarter-wave transformer. (G) shows the *Johnson Q system* whereby a line made up of ½-inch dural tubing is used for the low-impedance linear transformer. A line made up in this manner is frequently called a set of *Q bars.* Illustration (H) shows the use of a four-wire line as the linear transformer, and (I) shows the use of a piece of 150-ohm Twin-Lead electrically ¼-wave in length as the transformer between the center of the dipole and a piece of 300-ohm Twin-Lead. In any case the impedance of the quarter-wave transformer will be of the order of 150 to 200 ohms. The use of sections of transmission line as linear transformers is discussed in detail in Section 19-8.

Multi-Wire Doublets An alternative method for increasing the feed-point impedance of a dipole so that a medium-impedance transmission line may be used is shown in figures 2J and 2K. This system utilizes more than one wire in parallel for the radiating element, but only one of the wires is broken for attachment of the feeder. The most common arrangement uses two wires in the flat top of the antenna so that an impedance multiplication of four is obtained.

The antenna shown in figure 2J is the so-called *Twin-Lead folded dipole* which is a commonly used antenna system on the medium-frequency amateur bands. In this arrangement both the antenna and the transmission line to the transmitter are constructed of 300-ohm Twin-Lead. The flat top of the antenna is made slightly less than the conventional length ($462/F_{Mc.}$ instead of $468/F_{Mc.}$ for a single-wire flat top) and the two ends of the Twin-Lead are joined together at each end. The center of one of the conductors of the Twin-Lead flat top is broken and the two ends of the Twin-Lead feeder are spliced into the flat top leads. As a protection against moisture pieces of flat polyethylene taken from another piece of 300-ohm Twin-Lead may be molded over the joint between conductors with the aid of an electric iron or soldering iron.

Better bandwidth characteristics can be obtained with a folded dipole made of ribbon line if the two conductors of the ribbon line are shorted a distance of 0.82 (the velocity factor of ribbon line) of a free-space quarter wavelength from the center or feed point. This procedure is illustrated in figure 3A. An alternative arrangement for a Twin-Lead folded dipole is illustrated in figure 3B. This type of half-wave antenna system is convenient for use on the 3.5-Mc. band when the 116 to 132 foot distance required for a full half-wave is not quite available in a straight line, since the single-wire end pieces may be bent away or downward from the direction of the main section of the antenna.

Figure 2K shows the basic type of 2-wire doublet or *folded dipole* wherein the radiating section of the system is made up of standard antenna wire spaced by means of feeder spreaders. The feeder again is made of 300-ohm Twin-Lead since the feed-point impedance is approximately 300 ohms, the same as that of the Twin-Lead folded dipole.

The folded-dipole type of antenna has the broadest response characteristic (greatest bandwidth) of any of the conventional half-wave antenna systems constructed of small wires or conductors. Hence such an antenna may be operated over the greatest frequency range without serious standing waves of any common half-wave antenna type.

The increased bandwidth of the multi-wire doublet type of radiator, and the fact that the feed-point resistance is increased several

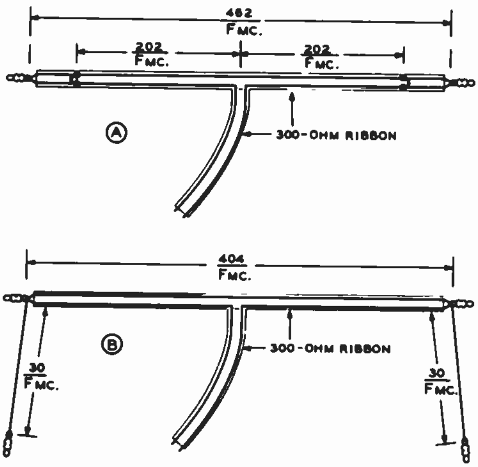


Figure 3

FOLDED DIPOLE WITH SHORTING STRAPS

The impedance match and bandwidth characteristics of a folded dipole may be improved by shorting the two wires of the ribbon a distance out from the center equal to the velocity factor of the ribbon times the half-length of the dipole as shown at (A). An alternative arrangement with bent down ends for space conservation is illustrated at (B).

times over the radiation resistance of the element, have both contributed to the frequent use of the multi-wire radiator as the driven element in a parasitic antenna array.

Delta-Matched Doublet and Standard Doublet These two types of radiating elements are shown in figure 2L and figure 2M. The delta-matched doublet is described in detail in Section 19-8 of this chapter. The standard doublet, shown in figure 2M, is fed in the center by means of 75-ohm Twin-Lead, either the transmitting or the receiving type, or it may be fed by means of twisted-pair feeder or by means of parallel-wire lamp-cord. Any of these types of feed line will give an approximate match to the center impedance of the dipole, but the 75-ohm Twin-Lead is far to be preferred over the other types of low-impedance feeder due to the much lower losses of the polyethylene-dielectric transmission line.

The coaxial-cable-fed doublet shown in figure 2N is a variation on the system shown in figure 2M. Either 52-ohm coaxial cable or 75-ohm coaxial cable may be used to feed the center of the dipole, although the 75-ohm type

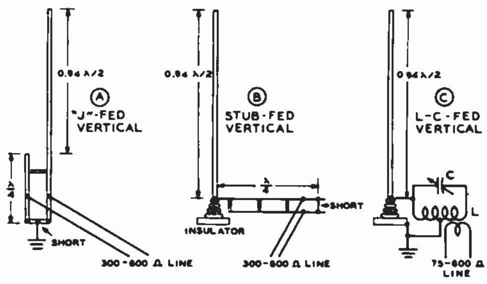


Figure 4

HALF-WAVE VERTICAL ANTENNA SHOWING ALTERNATIVE METHODS OF FEED

will give a somewhat better impedance match at normal antenna heights. Due to the asymmetry of the coaxial feed system difficulty may be encountered with waves traveling on the outside of the coaxial cable. For this reason the use of Twin-Lead is normally to be preferred over the use of coaxial cable for feeding the center of a half-wave dipole.

Off-Center Fed Doublet The system shown in figure 2(O) is sometimes used to feed a half-wave dipole, especially when it is desired to use the same antenna on a number of harmonically-related frequencies. The feeder wire (no. 14 enamelled wire should be used) is tapped a distance of 14 per cent of the total length of the antenna either side of center. The feeder wire, operating against ground for the return current, has an impedance of approximately 600 ohms. The system works well over highly conducting ground, but will introduce rather high losses when the antenna is located above rocky or poorly conducting soil. The off-center fed antenna has a further disadvantage that it is highly responsive to harmonics fed to it from the transmitter.

The effectiveness of the antenna system in radiating harmonics is of course an advantage when operation of the antenna on a number of frequency bands is desired. But it is necessary to use a harmonic filter to insure that only the desired frequency is fed from the transmitter to the antenna.

19-3 The Half-Wave Vertical Antenna

The half-wave vertical antenna with its bottom end from 0.1 to 0.2 wavelength above

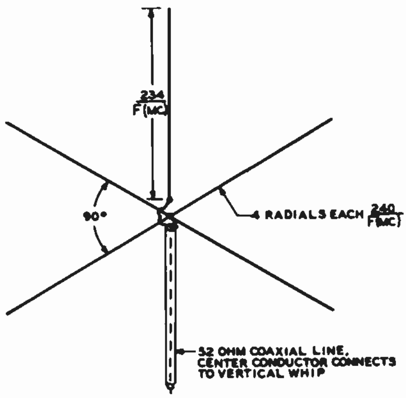


Figure 5

THE LOW-FREQUENCY GROUND PLANE ANTENNA

The radials of the ground plane antenna should lie in a horizontal plane, although slight departures from this caused by nearby objects is allowable. The whip may be mounted on a short post, or on the roof of a building. The wire radials may slope downwards towards their tips, acting as guy wires for the installation.

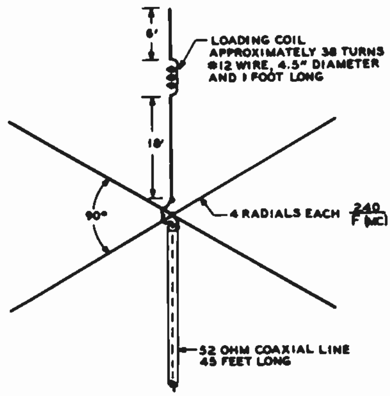


Figure 6

80 METER LOADED GROUND PLANE ANTENNA

Number of turns in loading coil to be adjusted until antenna system resonates at desired frequency in 80 meter band.

ground is an effective transmitting antenna for low-angle radiation, where ground conditions in the vicinity of the antenna are good. Such an antenna is not good for short-range *sky*-wave communication, such as is the normal usage of the 3.5-Mc. amateur band, but is excellent for short-range *ground*-wave communication such as on the standard broadcast band and on the amateur 1.8-Mc. band. The vertical antenna normally will cause greater BCI than an equivalent horizontal antenna, due to the much greater ground-wave field intensity. Also, the vertical antenna is poor for receiving under conditions where man-made interference is severe, since such interference is predominantly vertically polarized.

Three ways of feeding a half-wave vertical antenna from an untuned transmission line are illustrated in figure 4. The J-fed system shown in figure 4A is obviously not practicable except on the higher frequencies where the extra length for the stub may easily be obtained. However, in the normal case the ground-plane vertical antenna is to be recommended over the J-fed system for high frequency work.

19-4 The Ground Plane Antenna

An effective low angle radiator for any amateur band is the *ground-plane antenna,* shown in figure 5. So called because of the radial ground wires, the ground-plane antenna is not affected by soil conditions in its vicinity due to the creation of an artificial ground system by the radial wires. The base impedance of the ground plane is of the order of 30 to 35 ohms, and it may be fed with 52-ohm coaxial line with only a slight impedance mis-match. For a more exact match, the ground-plane antenna may be fed with a 72-ohm coaxial line and a quarter-wave matching section made of 52-ohm coaxial line.

The angle of radiation of the ground-plane antenna is quite low, and the antenna will be found less effective for contacts under 1000 miles or so on the 80 and 40 meter bands than a high angle radiator, such as a dipole. However, for DX contacts of 1000 miles or more, the ground-plane antenna will prove to be highly effective.

The 80-Meter Loaded Ground-Plane A vertical antenna of 66 feet in height presents quite a problem on a small lot, as the supporting guy wires will tend to take up quite a large portion of the lot. Under such conditions, it is possible to shorten the length of the vertical radiator of the ground-plane by the inclusion of a loading coil in the vertical whip section. The ground-plane antenna may be artificially loaded in this manner so that a 25-foot vertical whip may be used for the radiator. Such an antenna is shown in figure 6. The loaded ground-plane tends to have a rather high operating Q and operates only over a narrow band of frequencies. An operating range of about 100 kilocycles with a low SWR is possible on 80 meters. Operation over a larger frequency range is possible if a higher standing wave ratio is tolerated on the transmission line. The radiation resistance of a loaded 80-meter ground-plane is about 15 ohms. A quarter wavelength (45 feet) of 52-ohm coaxial line will act as an efficient feed line, presenting a load of approximately 180 ohms to the transmitter.

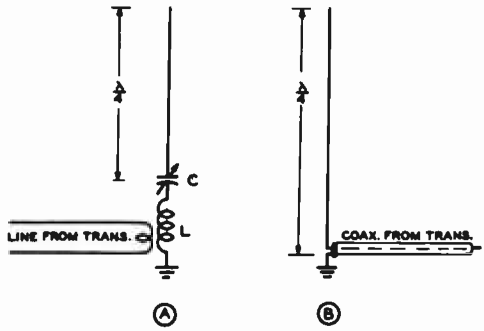


Figure 7
FEEDING A QUARTER-WAVE MARCONI ANTENNA

When an open-wire line is to be used, it may be link coupled to a series-resonant circuit between the bottom end of the Marconi and ground, as at (A). Alternatively, a reasonably good impedance match may be obtained between 52-ohm coaxial line and the bottom of a resonant quarter-wave antenna, as illustrated at (B) above.

19-5 The Marconi Antenna

A grounded quarter-wave Marconi antenna, widely used on frequencies below 3 Mc., is sometimes used on the 3.5-Mc. band, and is also used in v-h-f mobile services where a compact antenna is required. The Marconi type antenna allows the use of half the length of wire that would be required for a half-wave Hertz radiator. The ground acts as a mirror, in effect, and takes the place of the additional quarter-wave of wire that would be required to reach resonance if the end of the wire were not returned to ground.

The fundamental practical form of the Marconi antenna system is shown in figure 7. Other Marconi antennas differ from this type primarily in regard to the method of feeding the energy to the radiator. The feed method shown in figure 7B can often be used to advantage, particularly in mobile work.

Variations on the basic Marconi antenna are shown in the illustrations of figure 8. Figures 8B and 8C show the "L"-type and "T"-type Marconi antennas. These arrangements have been more or less superseded by the top-loaded forms of the Marconi antenna shown in figures 8D, 8E, and 8F. In each of these latter three figures an antenna somewhat less than one quarter wave in length has been *loaded* to increase its effective length by the insertion of a *loading coil* at or near the top of the radiator. The arrangement shown at figure 8D gives the least loading but is the most practical mechanically. The system shown at figure 8E gives an intermediate amount of loading, while that shown at figure 8F, utilizing a "hat" just above the loading coil, gives the greatest amount of loading. The object of all the top-loading methods shown is to produce an increase in the effective length of the radiator, and thus to raise the point of maximum current in the radiator as far as possible above ground. Raising the maximum-current point in the radiator above ground has two desirable results: The percentage of low-angle radiation is increased and the amount of ground current at the base of the radiator is reduced, thus reducing the ground losses.

To estimate whether a loading coil will probably be required, it is necessary only to note if the length of the antenna wire and ground lead is over a quarter wavelength; if so, no loading coil is needed, provided the series tuning capacitor has a high maximum capacitance.

Amateurs primarily interested in the higher frequency bands, but who like to work 80 meters occasionally, can usually manage to resonate one of their antennas as a Marconi by working the whole system, feeders and all, against a water pipe ground, and resorting to a loading coil if necessary. A high-frequency-rotary, zepp, doublet, or single-wire-fed antenna will make quite a good 80-meter Marconi if high and in the clear, with a rather long feed line to act as a radiator on 80 meters. Where two-wire feeders are used, the feeders should be tied together for Marconi operation.

Importance of Ground Connection With a quarter-wave antenna and a ground, the antenna current generally is measured with a meter placed in the antenna circuit close to the ground connection. If this

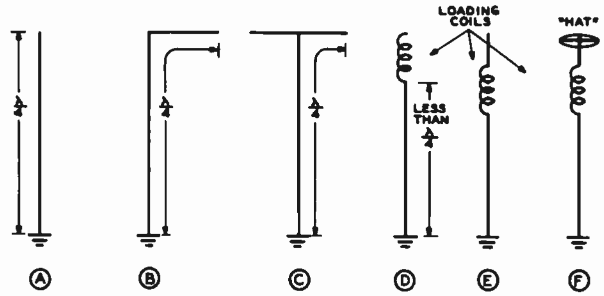


Figure 8
LOADING THE MARCONI ANTENNA
The various loading systems are discussed in the accompanying text.

current flows through a resistor, or if the ground itself presents some resistance, there will be a power loss in the form of heat. Improving the ground connection, therefore, provides a definite means of reducing this power loss, and thus increasing the radiated power.

The best possible ground consists of as many wires as possible, each at least a quarter wave long, buried just below the surface of the earth, and extending out from a common point in the form of radials. Copper wire of any size larger than no. 16 is satisfactory, though the larger sizes will take longer to disintegrate. In fact, the radials need not even be buried; they may be supported just above the earth, and insulated from it. This arrangement is called a *counterpoise,* and operates by virtue of its high capacitance to ground.

If the antenna is physically shorter than a quarter wavelength, the antenna current is higher, due to lower radiation resistance. Consequently, the power lost in resistive soil is greater. The importance of a good ground with short, inductive-loaded Marconi radiators is, therefore, quite obvious. With a good ground system, even very short (one-eighth wavelength) antennas can be expected to give a high percentage of the efficiency of a quarter-wave antenna used with the same ground system. This is especially true when the short radiator is *top loaded* with a high Q (low loss) coil.

Water-Pipe Grounds Water pipe, because of its comparatively large surface and cross section, has a relatively low r-f resistance. If it is possible to attach to a junction of several water pipes (where they branch in several directions and run for some distance under ground), a satisfactory ground connection will be obtained. If one of the pipes attaches to a lawn or garden sprinkler system in the immediate vicinity of the antenna, the effectiveness of the system will approach that of buried copper radials.

The main objection to water-pipe grounds is the possibility of high resistance joints in the pipe, due to the "dope" put on the coupling threads. By attaching the ground wire to a junction with three or more legs, the possibility of requiring the main portion of the r-f current to flow through a high resistance connection is greatly reduced.

The presence of water in the pipe adds nothing to the conductivity; therefore it does not relieve the problem of high resistance joints. Bonding the joints is the best insurance, but this is, of course, impracticable where the pipe is buried. Bonding together with copper wire the various water faucets above the surface of the ground will improve the effectiveness of a water-pipe ground system hampered by high-resistance pipe couplings.

Marconi Dimensions A Marconi antenna is an odd number of electrical quarter waves long (usually only one quarter wave in length), and is always resonated to the operating frequency. The correct loading of the final amplifier is accomplished by varying the coupling, *rather than by detuning the antenna from resonance.*

Physically, a quarter-wave Marconi may be made anywhere from one-eighth to three-eighths wavelength overall, meaning the total length of the antenna wire and ground lead from the end of the antenna to the point where the ground lead attaches to the junction of the radials or counterpoise wires, or where the water pipe enters the ground. The longer the antenna is made physically, the lower will be the current flowing in the ground connection, and the greater will be the overall radiation efficiency. However, when the antenna length exceeds three-eighths wavelength, the antenna becomes difficult to resonate by means of a series capacitor, and it begins to take shape as an end-fed Hertz, requiring a method of feed such as a pi network.

A radiator physically much shorter than a

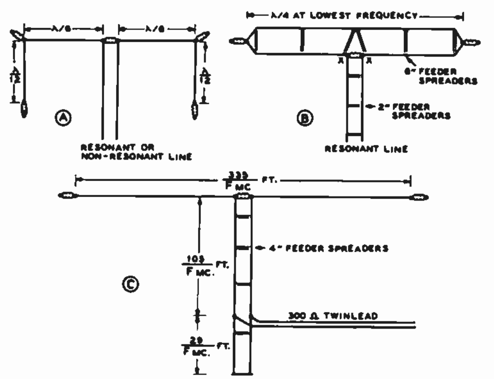


Figure 9

THREE EFFECTIVE SPACE CONSERVING ANTENNAS

The arrangements shown at (A) and (B) are satisfactory where resonant feed line can be used. However, non-resonant 75-ohm feed line may be used in the arrangement at (A) when the dimensions in wavelengths are as shown. In the arrangement shown at (B) low standing waves will be obtained on the feed line when the overall length of the antenna is a half wave. The arrangement shown at (C) may be tuned for any reasonable length of flat top to give a minimum of standing waves on the transmission line.

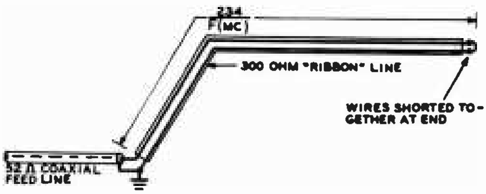


Figure 10

TWIN-LEAD MARCONI ANTENNA FOR THE 80 AND 160 METER BANDS

quarter wavelength can be lengthened electrically by means of a series loading coil, and used as a quarter-wave Marconi. However, if the wire is made shorter than approximately one-eighth wavelength, the radiation resistance will be quite low. This is a special problem in mobile work below about 20-Mc. (see mobile chapter).

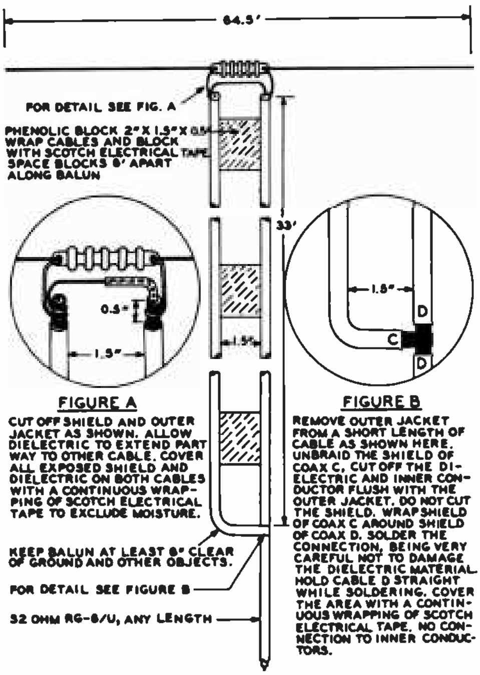
19-6 Space-Conserving Antennas

In many cases it is desired to undertake a considerable amount of operation on the 80-meter or 40-meter band, but sufficient space is simply not available for the installation of a half-wave radiator for the desired frequency of operation. This is a common experience of apartment dwellers. The shortened Marconi antenna operated against a good ground *can* be used under certain conditions, but the shortened Marconi is notorious for the production of broadcast interference, and a good ground connection is usually completely unobtainable in an apartment house.

Essentially, the problem in producing an antenna for lower frequency operation in restricted space is to erect a short radiator which is balanced with respect to ground and which is therefore independent of ground for its operation. Several antenna types meeting this set of conditions are shown in figure 9. Figure 9A shows a conventional center-fed doublet with bent-down ends. This type of antenna can be fed with 75-ohm Twin-Lead in the center, or it may be fed with a resonant line for operation on several bands. The overall length of the radiating wire will be a few per cent greater than the normal length for such an antenna since the wire is bent at a position intermediate between a current loop and a voltage loop. The actual length will have to be determined by the cut-and-try process because of the increased effect of interfering objects on the effective electrical length of an antenna of this type.

Figure 9B shows a method for using a two-wire doublet on one half of its normal operating frequency. It is recommended that spaced open conductor be used both for the radiating portion of the folded dipole and for the feed line. The reason for this recommendation lies in the fact that the two wires of the flat top are *not* at the same potential throughout their length when the antenna is operated on one-half frequency. Twin-Lead may be used for the feed line if operation on the frequency where the flat top is one-half wave in length is most common, and operation on one-half frequency is infrequent. However, if the antenna is to be used primarily on one-half frequency as shown, it should be fed by means of an open-wire line. If it is desired to feed the antenna with a non-resonant line, a quarter-wave stub may be connected to the antenna at the points X, X in figure 9B. The stub should be tuned and the transmission line connected to it in the normal manner.

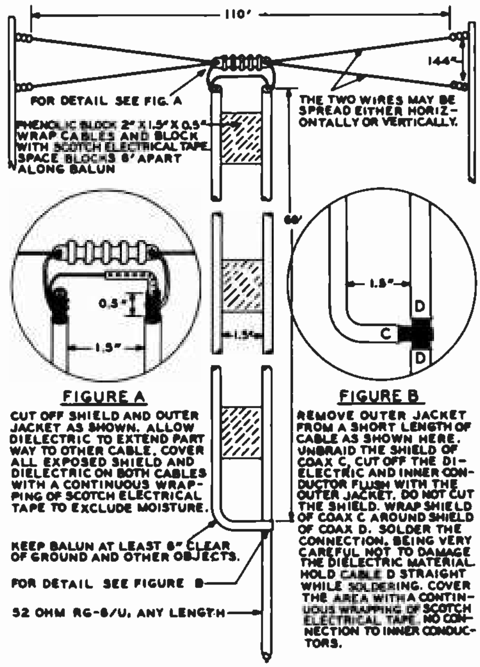
The antenna system shown in figure 9C may be used when not quite enough length is available for a full half-wave radiator. The dimen-



DIMENSIONS SHOWN HERE ARE FOR THE 40 METER BAND. THIS ANTENNA MAY BE BUILT FOR OTHER BANDS BY USING DIMENSIONS THAT ARE MULTIPLES OR SUBMULTIPLES OF THE DIMENSIONS SHOWN. BALUN SPACING IS 1.5" ON ALL BANDS.

Figure 11

HALF-WAVE ANTENNA WITH QUARTER-WAVE UNBALANCED TO BALANCED TRANSFORMER (BALUN) FEED SYSTEM FOR 40-METER OPERATION



DIMENSIONS SHOWN HERE ARE FOR THE 80 METER BAND. THIS ANTENNA MAY BE BUILT FOR OTHER BANDS BY USING DIMENSIONS THAT ARE MULTIPLES OR SUBMULTIPLES OF THE DIMENSIONS SHOWN. BALUN SPACING IS 1.5" ON ALL BANDS.

Figure 12

BROADBAND ANTENNA WITH QUARTER-WAVE UNBALANCED TO BALANCED TRANSFORMER (BALUN) FEED SYSTEM FOR 80-METER OPERATION

sions in terms of frequency are given on the drawing. An antenna of this type is 93 feet long for operation on 3600 kc. and 86 feet long for operation on 3900 kc. This type of antenna has the additional advantage that it may be operated on the 7-Mc. and 14-Mc. bands, when the flat top has been cut for the 3.5-Mc. band, simply by changing the position of the shorting bar and the feeder line on the stub.

A sacrifice which must be made when using a shortened radiating system, as for example the types shown in figure 9, is in the bandwidth of the radiating system. The frequency range which may be covered by a shortened antenna system is approximately in proportion to the amount of shortening which has been employed. For example, the antenna system shown in figure 9C may be operated over the range from 3800 kc. to 4000 kc. without serious standing waves on the feed line. If the antenna had been made full length it would be possible to cover about half again as much frequency range for the same amount of mismatch on the extremes of the frequency range.

The Twin-Lead Marconi Antenna Much of the power loss in the Marconi antenna is a result of low radiation resistance and high ground resistance. In some cases, the ground resistance may even be be higher than the radiation resistance, causing a loss of 50 per cent or more of the transmitter power output. If the radiation resistance of the Marconi antenna is raised, the amount of power lost in the ground resistance is proportionately less. If a Marconi antenna is made out of 300 ohm TV-type ribbon line, as shown in figure 10, the radiation resistance of the antenna is raised from a low value of 10 or 15 ohms to a more reasonable value of 40 to 60

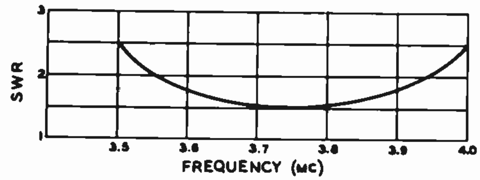


Figure 13
SWR CURVE OF 80-METER BROAD-BAND DIPOLE

ohms. The ground losses are now reduced by a factor of 4. In addition, the antenna may be directly fed from a 50-ohm coaxial line, or directly from the unbalanced output of a pi- network transmitter.

Since a certain amount of power may still be lost in the ground connection, it is still of greatest importance that a good, low resistance ground be used with this antenna.

The Collins Broad-band Dipole System Shown in figures 11 and 12 are broad-band dipoles for the 40 and 80 meter amateur bands, designed by Collins Radio Co. for use with the Collins 32V-3 and KW-1 transmitters. These fan-type dipoles have excellent broad-band response, and are designed to be fed with a 52-ohm unbalanced coaxial line, making them suitable for use with many of the other modern transmitters, such as the Barker and Williamson 5100, Johnson Ranger, and Viking. The antenna system consists of a fan-type dipole, a balun matching section, and a suitable coaxial feedline. The Q of the half-wave 80 meter doublet is lowered by decreasing the effective length-to-diameter ratio. The frequency range of operation of the doublet is increased considerably by this change. A typical SWR curve for the 80 meter doublet is shown in figure 13.

The balanced doublet is matched to the unbalanced coaxial line by the one-quarter wave balun. If desired, a shortened balun may be used (figure 14). The short balun is capacity loaded at the junction between the balun and the broad-band dipole.

19-7 Multi-Band Antennas

The availability of a multi-band antenna is a great operating convenience to an amateur station. In most cases it will be found best to install an antenna which is optimum for the band which is used for the majority of the

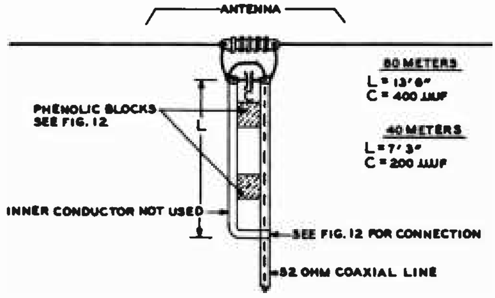


Figure 14
SHORT BALUN FOR 40 AND 80 METERS

available operating time, and then to have an additional multi-band antenna which may be pressed into service for operation on another band when propagation conditions on the most frequently used band are not suitable. Most amateurs use, or plan to install, at least one directive array for one of the higher-frequency bands, but find that an additional antenna which may be used on the 3.5-Mc. and 7.0-Mc. band, or even up through the 28-Mc. band is almost indispensable.

The choice of a multi-band antenna depends upon a number of factors such as the amount of space available, the band which is to be used for the majority of operating with the antenna, the radiation efficiency which is desired, and the type of antenna tuning network to be used at the transmitter. A number of recommended types are shown in the next pages.

The ¾-Wave Folded Doublet Figure 15 shows an antenna type which will be found to be very effective when a moderate amount of space is available, when most of the operating will be done on one band with occasional operation on the second harmonic. The system is quite satisfactory for use with high-power transmitters since a 600-ohm non-resonant line is used from the antenna to the transmitter and since the antenna system is balanced with respect to ground. With operation on the fundamental frequency of the antenna where the flat top is ¾ wave long the switch SW is left open. The system affords a very close match between the 600-ohm line and the feed point of the antenna. Kraus has reported a standing-wave ratio of approximately 1.2 to 1 over the 14-Mc. band when the antenna was located approximately one-half wave above ground.

For operation on the second harmonic the switch SW is *closed*. The antenna is still an

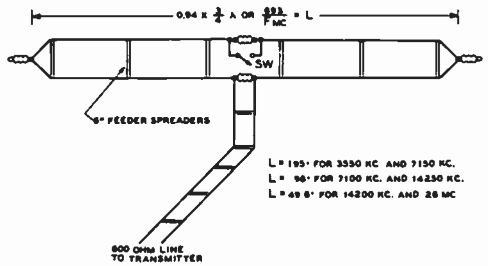


Figure 15

THE THREE-QUARTER WAVE FOLDED DOUBLET

This antenna arrangement will give very satisfactory operation with a 600-ohm feed line for operation with the switch open on the fundamental frequency and with the switch closed on twice frequency.

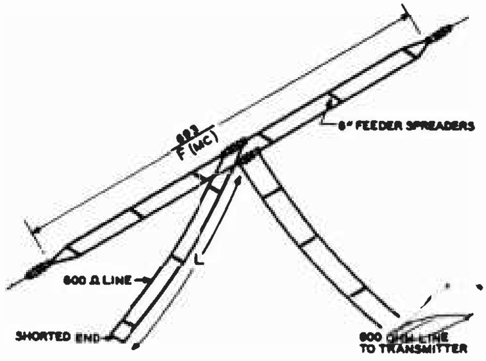


Figure 16

AUTOMATIC BANDSWITCHING STUB FOR THE THREE-QUARTER WAVE FOLDED DOUBLET

The antenna of Figure 15 may be used with a shorted stub line in place of the switch normally used for second harmonic operation.

effective radiator on the second harmonic but the pattern of radiation will be different from that on the fundamental, and the standing-wave ratio on the feed line will be greater. The flat top of the antenna must be made of open wire rather than ribbon or tubular line.

For greater operating convenience, the shorting switch may be replaced with a section of transmission line. If this transmission line is made one-quarter wavelength long for the fundamental frequency, and the free end of the line is shorted, it will act as an open circuit across the center insulator. At the second harmonic, the transmission line is one-half wavelength long, and reflects the low impedance of the shorted end across the center insulator. Thus the switching action is automatic as the frequency of operation is changed. Such an installation is shown in figure 16.

The End-Fed Hertz The end-fed Hertz antenna shown in figure 17 is not as effective a radiating system as many other antenna types, but it is particularly convenient when it is desired to install an antenna in a hurry for a test, or for field-day work. The flat top of the radiator should be as high and in the clear as possible. In any event at least three quarters of the total wire length should be in the clear. Dimensions for optimum operation on various amateur bands are given in addition in figure 17.

The End-Fed Zepp The end-fed Zepp has long been a favorite for multi-band operation. It is shown in figure 18 along with recommended dimensions for operation on various amateur band groups.

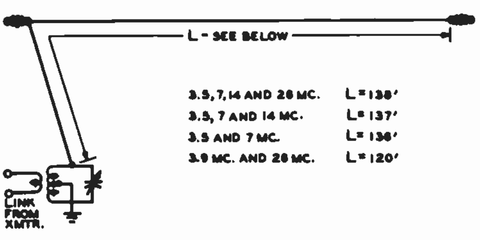
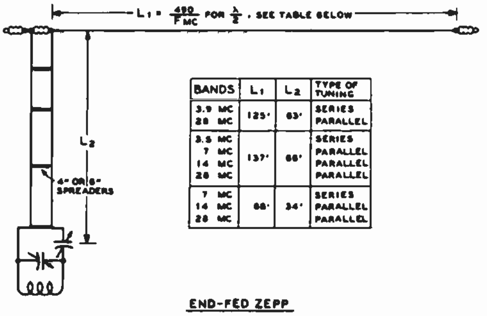


Figure 17

RECOMMENDED LENGTHS FOR THE END-FED HERTZ



BANDS	L_1	L_2	TYPE OF TUNING
3.9 MC 28 MC	125'	63'	SERIES PARALLEL
3.5 MC 7 MC 14 MC 28 MC	137'	68'	SERIES PARALLEL PARALLEL PARALLEL
7 MC 14 MC 28 MC	68'	34'	SERIES PARALLEL PARALLEL

END-FED ZEPP

FIGURE 18

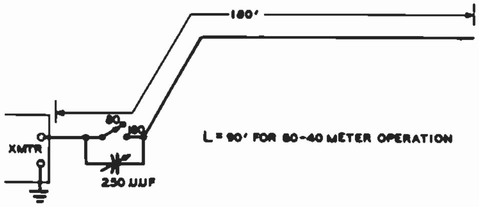


Figure 19

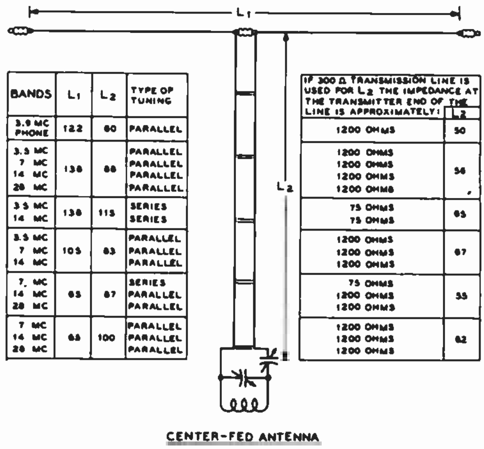
A TWO-BAND MARCONI ANTENNA FOR 160-80 METER OPERATION

Since this antenna type is an unbalanced radiating system, its use is not recommended with high-power transmitters where interference to broadcast listeners is likely to be encountered. The r-f voltages encountered at the end of zepp feeders and at points an electrical half wave from the end are likely to be quite high. Hence the feeders should be supported an adequate distance from surrounding objects and sufficiently in the clear so that a chance encounter between a passerby and the feeder is unlikely.

The coupling coil at the transmitter end of the feeder system should be link coupled to the output of the low-pass TVI filter in order to reduce harmonic radiation.

The Two-Band Marconi Antenna A three-eighths wavelength Marconi antenna may be operated on its harmonic frequency, providing good two band performance from a simple wire. Such an arrangement for operation on 160-80 meters, and 80-40 meters is shown in figure 19. On the fundamental (lowest) frequency, the antenna acts as a three-eighths wavelength series-tuned Marconi. On the second harmonic, the antenna is a current-fed three-quarter wavelength antenna operating against ground. For proper operation, the antenna should be resonated on its second harmonic by means of a grid-dip oscillator to the operating frequency most used on this particular band. The Q of the antenna is relatively low, and the antenna will perform well over a frequency range of several hundred kilocycles.

The overall length of the antenna may be varied slightly to place its self-resonant frequency in the desired region. Bends or turns in the antenna tend to make it resonate higher in frequency, and it may be necessary to lengthen it a bit to resonate it at the chosen frequency. For fundamental operation, the series condenser is inserted in the circuit, and the antenna may be resonated to any point in the lower frequency band. As with any Marconi



BANDS	L_1	L_2	TYPE OF TUNING	IF 300 Ω TRANSMISSION LINE IS USED FOR L_2 THE IMPEDANCE AT THE TRANSMITTER END OF THE LINE IS APPROXIMATELY:	L_2
3.9 MC PHONE	122	80	PARALLEL	1200 OHMS	50
3.5 MC 7 MC 14 MC 28 MC	138	88	PARALLEL PARALLEL PARALLEL PARALLEL	1200 OHMS 1200 OHMS 1200 OHMS 1200 OHMS	56
3.5 MC 14 MC	138	115	SERIES SERIES	75 OHMS 75 OHMS	65
3.5 MC 7 MC 14 MC	105	83	PARALLEL PARALLEL PARALLEL	1200 OHMS 1200 OHMS 1200 OHMS	67
7 MC 14 MC 28 MC	85	87	SERIES PARALLEL PARALLEL	75 OHMS 1200 OHMS 1200 OHMS	55
7 MC 14 MC 28 MC	68	100	PARALLEL PARALLEL PARALLEL	1200 OHMS 1200 OHMS 1200 OHMS	62

Figure 20

DIMENSIONS FOR CENTER-FED MULTI-BAND ANTENNA

type antenna, the use of a good ground is essential. This antenna works well with transmitters employing coaxial antenna feed, since its transmitting impedance on both bands is in the neighborhood of 40 to 60 ohms. It may be attached directly to the output terminal of such transmitters as the Collins 32V and the Viking II. The use of a low-pass TVI filter is of course recommended.

The Center-Fed Multi-Band Antenna For multi-band operation, the center fed antenna is without doubt the best compromise. It is a balanced system on all bands, it requires no ground return, and when properly tuned has good rejection properties for the higher harmonics generated in the transmitter. It is well suited for use with the various multi-band 150-watt transmitters that are currently so popular. For proper operation with these transmitters, an antenna tuning unit *must* be used with the center-fed antenna. In fact, some sort of tuning unit is necessary for any type of efficient, multi-band antenna. The use of such questionable antennas as the "off-center fed" doublet is an invitation to TVI troubles and improper operation of the transmitter. A properly balanced antenna is the best solution to multi-band operation. When used in conjunction with an antenna tuning unit, it will perform with top efficiency on all of the major amateur bands.

Several types of center-fed antenna systems are shown in figure 20. If the feed line is made up in the conventional manner of no. 12 or no.

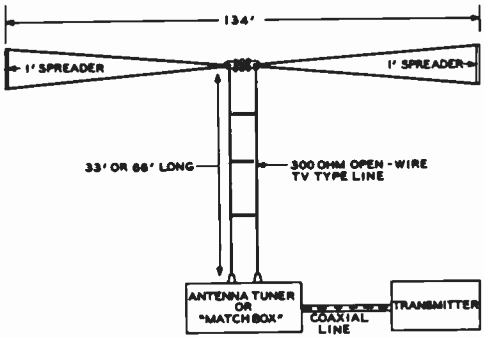


Figure 21
MULTI-BAND ANTENNA USING FAN-DIPOLE TO LIMIT IMPEDANCE EXCURSIONS ON HARMONIC FREQUENCIES

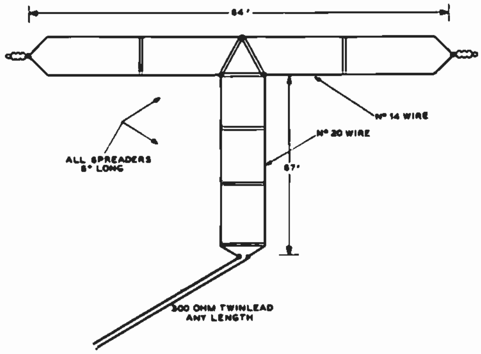


Figure 22
FOLDED-TOP DUAL-BAND ANTENNA

14 wire spaced 4 to 6 inches the antenna system is sometimes called a center-fed zepp. With this type of feeder the impedance at the transmitter end of the feeder varies from about 70 ohms to approximately 5000 ohms, the same as is encountered in an end-fed zepp antenna. This great impedance ratio requires provision for either series or parallel tuning of the feeders at the transmitter, and involves quite high r-f voltages at various points along the feed line.

If the feed line between the transmitter and the antenna is made to have a characteristic impedance of approximately 300 ohms the excursions in end-of-feeder impedance are greatly reduced. In fact the impedance then varies from approximately 75 ohms to 1200 ohms. With this much lowered impedance variation it is usually possible to use series tuning on all bands, or merely to couple the antenna directly to the output tank circuit or the harmonic reduction circuit without any separate feeder tuning provision.

There are several practicable types of transmission line which can give an impedance of approximately 300 ohms. The first is, obviously, 300-ohm Twin-Lead. Twin-Lead of the receiving type *may* be used as a resonant feed line in this case, but its use is not recommended with power levels greater than perhaps 150 watts, and it should not be used when lowest loss in the transmission line is desired.

For power levels up to 250 watts or so, the transmitting type tubular 300-ohm line may be used, or the open-wire 300-ohm TV line may be employed. For power levels higher than this, a 4- wire transmission line, or a line built of one-quarter inch tubing should be used.

Even when a 300-ohm transmission line is used, the end-of-feeder impedance may reach a high value, particularly on the second harmonic of the antenna. To limit the impedance excursions, a two-wire flat-top may be employed for the radiator, as shown in figure 21. The use of such a radiator will limit the impedance excursions on the harmonic frequencies of the antenna and make the operation of the antenna matching unit much less critical. The use of a two-wire radiator is highly recommended for any center-fed multi-band antenna.

Folded Flat-Top Dual-Band Antenna As has been mentioned earlier, there is an increasing tendency among amateur operators to utilize rotary or fixed arrays for the 14-Mc. band and those higher in frequency. In order to afford complete coverage of the amateur bands it is then desirable to have an additional system which will operate with equal effectiveness on the 3.5-Mc. and 7-Mc. bands, but this low-frequency antenna system will not be required to operate on any bands higher in frequency than the 7-Mc. band. The antenna system shown in figure 22 has been developed to fill this need.

This system consists essentially of an open-line folded dipole for the 7-Mc. band with a special feed system which allows the antenna to be fed with minimum standing waves on the feed line on both the 7-Mc. and 3.5-Mc. bands. The feed-point impedance of a folded dipole on its fundamental frequency is approximately 300 ohms. Hence the 300-ohm Twin-Lead shown in figure 22 can be connected directly into the center of the system for operation only on the 7-Mc. band and standing waves on the feeder will be very small. However, it is possible to insert an electrical half-wave of transmission line of any characteristic impedance into a feeder system such as this and the impedance at the far end of the line will be exactly the same value of impedance which the half-wave line sees at its termination. Hence this has been done in the antenna system shown in figure 22; an electrical half wave of line has been inserted between the feed point of the antenna and the 300-ohm transmission line to the transmitter.

The characteristic impedance of this additional half-wave section of transmission line has been made about 715 ohms (no. 20 wire spaced 6 inches), but since it is an electrical half wave long at 7 Mc. and operates into a load of 300 ohms at the antenna the 300-ohm Twin-Lead at the bottom of the half-wave section still sees an impedance of 300 ohms. The additional half-wave section of transmission line introduces a negligible amount of loss since the current flowing in the section of line is the same which would flow in a 300-ohm line at each end of the half-wave section, and at all other points it is *less* than the current which would flow in a 300-ohm line since the effective impedance is *greater* than 300 ohms in the center of the half-wave section. This means that the loss is less than it would be in an equivalent length of 300-ohm Twin-Lead since this type of manufactured transmission line is made up of conductors which are equivalent to no. 20 wire.

So we see that the added section of 715-ohm line has substantially no effect on the operation of the antenna system on the 7-Mc. band. However, when the flat top of the antenna is operated on the 3.5-Mc. band the feed-point impedance of the flat top is approximately 3500 ohms. Since the section of 715-ohm transmission line is an electrical *quarter-wave* in length on the 3.5-Mc. band, this section of line will have the effect of transforming the approximately 3500 ohms feed-point impedance of the antenna down to an impedance of about 150 ohms which will result in a 2:1 standing-wave ratio on the 300-ohm Twin-Lead transmission line from the transmitter to the antenna system.

The antenna system of figure 22 operates with very low standing waves over the entire 7-Mc. band, and it will operate with moderate standing waves from 3500 to 3800 kc. in the 3.5-Mc. band and with sufficiently low standing-wave ratio so that it is quite usable over the entire 3.5-Mc. band.

This antenna system, as well as all other types of multi-band antenna systems, must be used in conjunction with some type of harmonic-reducing antenna tuning network even though the system does present a convenient impedance value on both bands.

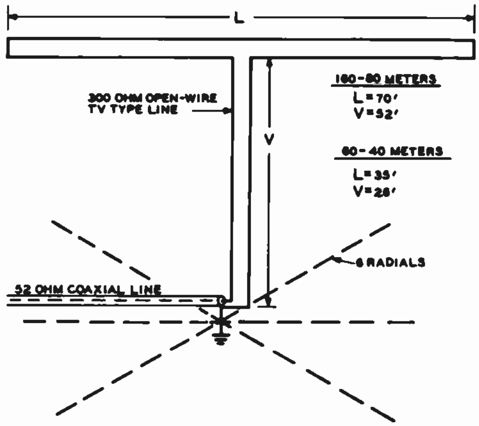


Figure 23

THE MULTEE TWO-BAND ANTENNA

This compact antenna can be used with excellent results on 160/80 and 80/40 meters. The feedline should be held as vertical as possible, since it radiates when the antenna is operated on its fundamental frequency.

The "Multee" Antenna An antenna that works well on 160 and 80 meters, or 80 and 40 meters and is sufficiently compact to permit erection on the average city lot is the *W6BCX Multee* antenna, illustrated in figure 23. The antenna evolves from a vertical two wire radiator, fed on one leg only. On the low frequency band the top portion does little radiating, so it is folded down to form a radiator for the higher frequency band. On the lower frequency band, the antenna acts as a top loaded vertical radiator, while on the higher frequency band, the flat-top does the radiating rather than the vertical portion. The vertical portion acts as a quarter-wave linear transformer, matching the 6000 ohm antenna impedance to the 50 ohm impedance of the coaxial transmission line.

The earth below a vertical radiator must be of good conductivity not only to provide a low resistance ground connection, but also to provide a good reflecting surface for the waves radiated downward towards the ground. For best results, a radial system should be installed beneath the antenna. For 160-80 meter operation, six radials 50 feet in length, made of no. 16 copper wire should be buried just below the surface of the ground. While an ordinary water pipe ground system with no radials may be used, a system of radials will provide a worthwhile increase in signal strength. For 80-40 meter operation, the length

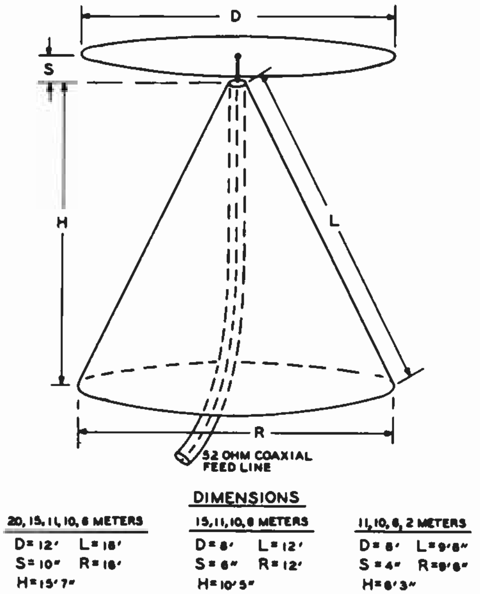


Figure 24

DIMENSIONS OF LOW-FREQUENCY DISCONE ANTENNA FOR LOW FREQUENCY CUTOFF AT 13.2 MC., 20.1 MC., AND 26 MC.

The Discone is a vertically polarized radiator, producing an omnidirectional pattern similar to a ground plane. Operation on several amateur bands with low SWR on the coaxial feed line is possible. Additional information on L-F Discone by W2RYI in July, 1950 CQ magazine.

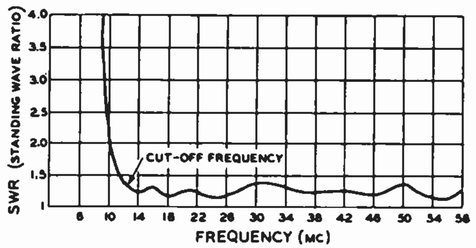


Figure 25

SWR CURVE FOR A 13.2 MC. DISCONE ANTENNA. SWR IS BELOW 1.5 TO 1 FROM 13.0 MC. TO 58 MC.

of the radials may be reduced to 25 feet. As with all multi-band antennas that employ no lumped tuned circuits, this antenna offers no attenuation to harmonics of the transmitter. When operating on the lower frequency band, it would be wise to check the transmitter for second harmonic emission, since this antenna will effectively radiate this harmonic.

The Low-Frequency Discone The *discone* antenna is widely used on the v-h-f bands, but until recently it has not been put to any great use on the lower frequency bands. Since the discone is a broad-band device, it may be used on several harmonically related amateur bands. Size is the limiting factor in the use of a discone, and the 20 meter band is about the lowest practical frequency for a discone of reasonable dimensions. A discone designed for 20 meter operation may be used on 20, 15, 11, 10 and 6 meters with excellent results. It affords a good match to a 50 ohm coaxial feed system on all of these bands. A practical discone antenna is shown in figure 24, with a SWR curve for its operation over the frequency range of 13-55 Mc. shown in figure 25. The discone antenna radiates a vertically polarized wave and has a very low angle of radiation. For v-h-f work the discone is constructed of sheet metal, but for low frequency work it may be made of copper wire and aluminum angle stock. A suitable mechanical layout for a low frequency discone is shown in figure 26. Smaller versions of this antenna may be constructed for 15, 11, 10 and 6 meters, or for 11, 10, 6 and 2 meters as shown in the chart of figure 24.

For minimum wind resistance, the top "hat" of the discone is constructed from three-quarter inch aluminum angle stock, the rods being bolted to an aluminum plate at the center of the structure. The tips of the rods are all connected together by lengths of no. 12 enamelled copper wire. The cone elements are made of no. 12 copper wire and act as guy wires for the discone structure. A very rigid arrangement may be made from this design; one that will give no trouble in high winds. A 4" x 4" post can be used to support the discone structure.

The discone antenna may be fed by a length of 50-ohm coaxial cable directly from the transmitter, with a very low SWR on all bands.

The Single-Wire-Fed Antenna The old favorite *single-wire-fed* antenna system is quite satisfactory for an impromptu all band antenna system. It is widely used for portable installations and "Field Day" contests where a simple, multi-band antenna is required. A single wire feeder has a characteristic impedance of some 500 ohms, de-

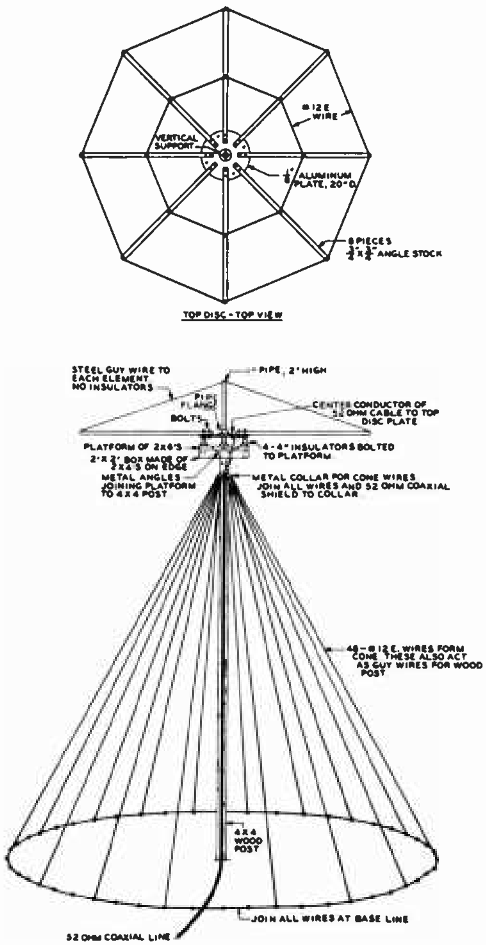


Figure 26

MECHANICAL CONSTRUCTION OF 20-METER DISCONE

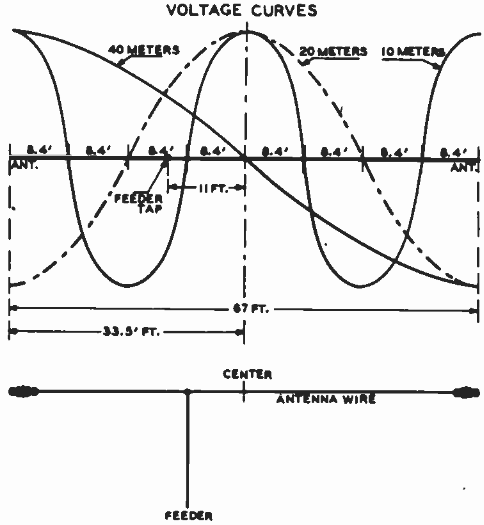


Figure 27

SINGLE-WIRE-FED ANTENNA FOR ALL-BAND OPERATION

An antenna of this type for 40-, 20- and 10-meter operation would have a radiator 67 feet long, with the feeder tapped 11 feet off center. The feeder can be 33, 66 or 99 feet long. The same type of antenna for 80-, 40-, 20- and 10-meter operation would have a radiator 134 feet long, with the feeder tapped 22 feet off center. The feeder can be either 66 or 132 feet long. This system should be used only with those coupling methods which provide good harmonic suppression.

pending upon the wire size and the point of attachment to the antenna. The earth losses are comparatively low over ground of good conductivity. Since the single wire feeder radiates, it is necessary to bring it away from the antenna at right angles to the antenna wire for at least one-half the length of the antenna.

The correct point for best impedance match on the fundamental frequency is not suitable for harmonic operation of the antenna. In addition, the correct length of the antenna for fundamental operation is not correct for harmonic operation. Consequently, a compromise must be made in antenna length and point of feeder connection to enable the single-wire-fed antenna to operate on more than one band. Such a compromise introduces additional reactance into the single wire feeder, and might cause loading difficulties with pi-network transmitters. To minimize this trouble, the single wire feeder should be made a multiple of 33 feet long.

Two typical single-wire-fed antenna systems are shown in figure 27 with dimensions for multi-band operation.

19-8 Matching Non-Resonant Lines to the Antenna

Present practice in regard to the use of transmission lines for feeding antenna systems on the amateur bands is about equally divided

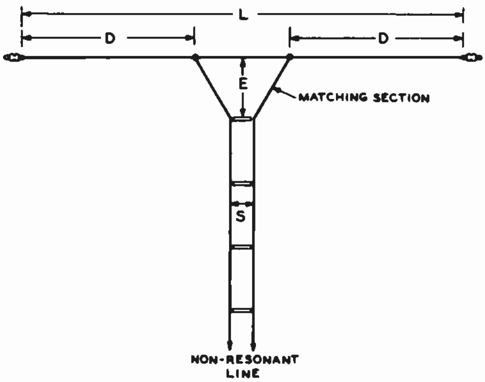


Figure 28
THE DELTA-MATCHED DIPOLE ANTENNA
The dimensions for the portions of the antenna are given in the text.

between three types of transmission line: (1) Ribbon or tubular molded 300-ohm line is widely used up to moderate power levels (the "transmitting" type is useable up to the kilowatt level). (2) Open-wire 400 to 600 ohm line is most commonly used when the antenna is some distance from the transmitter, because of the low attenuation of this type of line. (3) Coaxial line (usually RG-8/U with a 52-ohm characteristic impedance) is widely used in v-h-f work and also on the lower frequencies where the feed line must run underground or through the walls of a building. Coaxial line also is of assistance in TVI reduction since the r-f field is entirely enclosed within the line. Molded 75-ohm line is sometimes used to feed a doublet antenna, but the doublet has been largely superseded by the folded-dipole antenna fed by 300-ohm ribbon or tubular line when an antenna for a single band is required.

Standing Waves As was discussed earlier, standing waves on the antenna transmission line, in the transmitting case, are a result of reflection from the point where the feed line joins the antenna system. The magnitude of the standing waves is determined by the degree of mismatch between the characteristic impedance of the transmission line and the input impedance of the antenna system. When the feed-point impedance of the antenna is resistive and of the same value as the characteristic impedance of the feed line, standing waves will not exist on the feeder. It may be well to repeat at this time that there is no adjustment which can be made at the transmitter end of the feed line which will change the magnitude of the standing waves on the antenna transmission line.

Delta-Matched Antenna System The delta type matched-impedance antenna system is shown in figure 28. The impedance of the transmission line is transformed gradually into a higher value by the fanned-out Y portion of the feeders, and the Y portion is tapped on the antenna at points where the antenna impedance is a compromise between the impedance at the ends of the Y and the impedance of the unfanned portion of the line.

The constants of the system are rather critical, and the antenna must resonate at the operating frequency in order to minimize standing waves on the line. Some slight readjustment of the taps on the antenna is desirable, if appreciable standing waves persist in appearing on the line.

The constants for a doublet are determined by the following formulas:

$$L_{feet} = \frac{467.4}{F_{megacycles}}$$

$$D_{feet} = \frac{175}{F_{megacycles}}$$

$$E_{feet} = \frac{147.6}{F_{megacycles}}$$

Where L is antenna length; D is the distance *in from each end* at which the Y taps on; E is the height of the Y section.

Since these constants are correct only for a 600-ohm transmission line, the spacing S of the line must be approximately 75 times the diameter of the wire used in the transmission line. For no. 14 B & S wire, the spacing will be slightly less than 5 inches. This system should never be used on either its even or odd harmonics, as entirely different constants are required when more than a single half wavelength appears on the radiating portion of the system.

Multi-Wire Doublets When a doublet antenna or the driven element in an array consists of more than one wire or tubing conductor the radiation resistance of the antenna or array is increased slightly as a result of the increase in the effective diameter of the element. Further, if we split just one

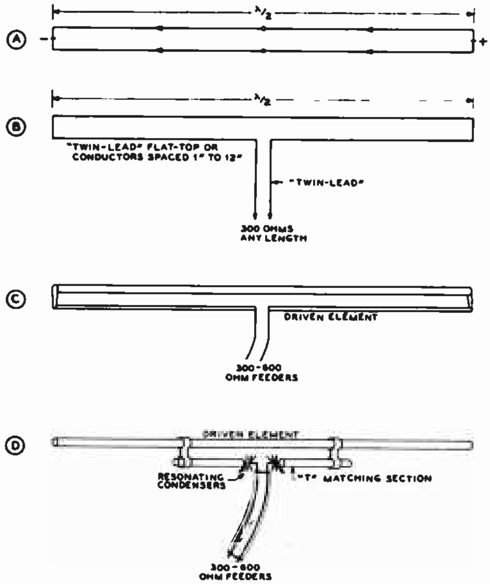


Figure 29

FOLDED-ELEMENT MATCHING SYSTEMS

Drawing (A) above shows a half-wave made up to two parallel wires. If one of the wires is broken as in (B) and the feeder connected, the feed-point impedance is multiplied by four; such an antenna is commonly called a "folded doublet." The feed-point impedance for a simple half-wave doublet fed in this manner is approximately 300 ohms, depending upon antenna height. Drawing (C) shows how the feed-point impedance can be multiplied by a factor greater than four by making the half of the element that is broken smaller in diameter than the unbroken half. An extension of the principles of (B) and (C) is the arrangement shown at (D) where the section into which the feeders are connected is considerably shorter than the driven element. This system is most convenient when the driven element is too long (such as for a 28-Mc. or 14-Mc. array) for a convenient mechanical arrangement of the system shown at (C).

wire of such a radiator, as shown in figure 29, the effective *feed-point* resistance of the antenna or array will be increased by a factor of N^2 where N is equal to the number of conductors, all in parallel, of the same diameter in the array. Thus if there are two conductors of the same diameter in the driven element or the antenna the feed-point resistance will be multiplied by 2^2 or 4. If the antenna has a radiation resistance of 75 ohms its feed-point resistance will be 300 ohms, this is the case

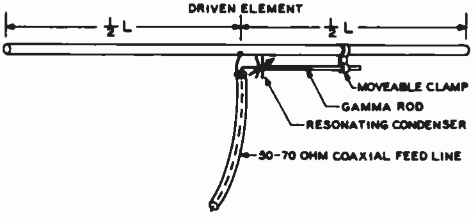


Figure 30

THE GAMMA MATCH FOR CONNECTING AN UNBALANCED COAXIAL LINE TO A BALANCED DRIVEN ELEMENT

of the conventional *folded-dipole* as shown in figure 29B.

If three wires are used in the driven radiator the feed-point resistance is increased by a factor of 9; if four wires are used the impedance is increased by a factor of 16, and so on. In certain cases when feeding a parasitic array it is desirable to have an impedance step up different from the value of 4:1 obtained with two elements of the same diameter and 9:1 with three elements of the same diameter. Intermediate values of impedance step up may be obtained by using two elements of different diameter for the complete driven element as shown in figure 29C. If the conductor that is broken for the feeder is of *smaller* diameter than the other conductor of the radiator, the impedance step up will be *greater* than 4:1. On the other hand if the *larger* of the two elements is broken for the feeder the impedance step up will be *less* than 4:1.

The "T" Match A method of matching a balanced low-impedance transmission line to the driven element of a parasitic array is the *T match* illustrated in figure 29D. This method is an adaptation of the multi-wire doublet principle which is more practicable for lower-frequency parasitic arrays such as those for use on the 14-Mc. and 28-Mc. bands. In the system a section of tubing of approximately one-half the diameter of the driven element is spaced about four inches below the driven element by means of clamps which hold the T-section mechanically and which make electrical connection to the driven element. The length of the T-section is normally between 15 and 30 inches each side of the center of the dipole for transmission lines of 300 to 600 ohms impedance, assuming 28-Mc. operation. In series with each leg of the T-section and the transmission line is a series resonating capacitor. These two capacitors tune out the reactance of the T-section. If they are not used, the T-section will detune the dipole when the T-section is attached to it. The two capacitors may be ganged together, and once adjusted for minimum detuning action, they may be locked. A suitable housing should be devised to protect these capacitors from the weather. Additional information on the adjustment of the T-match is given in the chapter covering rotary beam antennas.

The "Gamma" Match An unbalanced version of the T-match may be used to feed a dipole from an unbalanced coaxial line. Such a device is called a *Gamma Match*, and is illustrated in figure 30.

The length of the Gamma rod and the spacing of it from the dipole determine the impedance level at the transmission line end of the rod. The series capacitor is used to tune out the reactance introduced into the system by the Gamma rod. The adjustment of the Gamma Match is discussed in the chapter covering rotary beam antennas.

Matching Stubs By connecting a resonant section of transmission line (called a *matching stub*) to either a voltage or current loop and attaching parallel-wire nonresonant feeders to the resonant stub at a suitable voltage (impedance) point, standing waves on the line may be virtually eliminated. The stub is made to serve as an auto-transformer. Stubs are particularly adapted to matching an open line to certain directional arrays, as will be described later.

Voltage Feed When the stub attaches to the antenna at a voltage loop, the stub should be a quarter wavelength long electrically, and be shorted at the bottom end. The stub can be resonated by sliding the shorting bar up and down before the non-resonant feeders are attached to the stub, the antenna being shock-excited from a separate radiator during the process. Slight errors in the length of the radiator can be compensated for by adjustment of the stub if both sides of the stub are connected to the radiator in a symmetrical manner. Where only one side of the stub connects to the radiating system, as in the Zepp and in certain antenna arrays, the radiator length must be exactly right in order to prevent excessive unbalance in the untuned line.

A dial lamp may be placed in the center of the shorting stub to act as an r-f indicator.

Current Feed When a stub is used to current-feed a radiator, the stub should either be left *open* at the bottom end instead of shorted, or else made a *half wave* long.

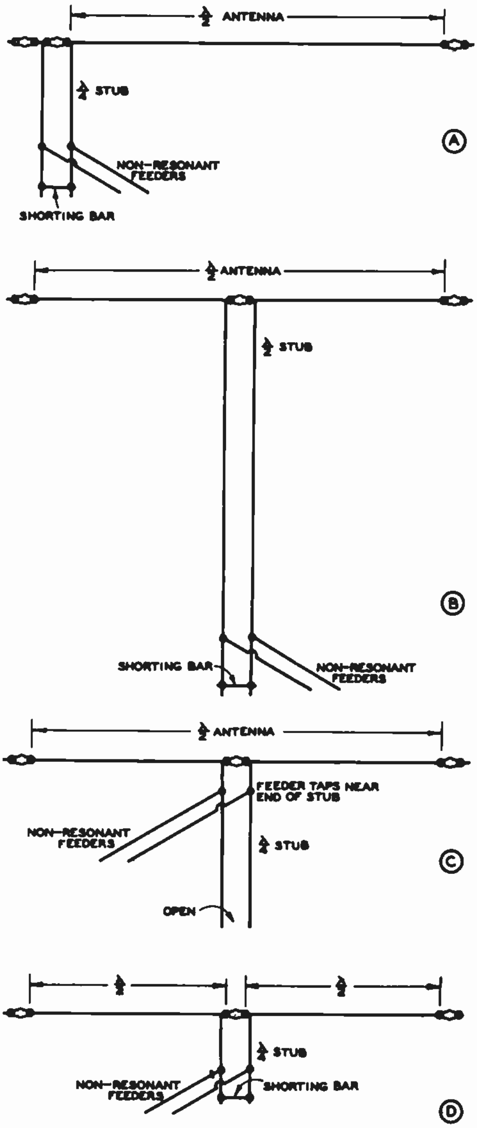


Figure 31

MATCHING-STUB APPLICATIONS

An end-fed half-wave antenna with a quarter-wave shorted stub is shown at (A). (B) shows the use of a half-wave shorted stub to feed a relatively low impedance point such as the center of the driven element of a parasitic array, or the center of a half-wave dipole. The use of an open-ended quarter-wave stub to feed a low impedance is illustrated at (C). (D) shows the conventional use of a shorted quarter-wave stub to voltage feed two half-wave antennas with a 180° phase difference.

The open stub should be resonated in the same manner as the shorted stub before attaching the transmission line; however, in this case, it is necessary to prune the stub to resonance, as there is no shorting bar.

Sometimes it is handy to have a stub hang from the radiator to a point that can be reached from the ground, in order to facilitate adjustment of the position of the transmission-line attachment. For this reason, a quarter-wave stub is sometimes made three-quarters wavelength long at the higher frequencies, in order to bring the bottom nearer the ground. Operation with any *odd* number of quarter waves is the same as for a quarter-wave stub.

Any number of *half waves* can be added to either a quarter-wave stub or a half-wave stub without disturbing the operation, though losses and frequency sensitivity will be lowest if the shortest usable stub is employed. See figure 31.

Stub Length (Electrical)	Current-Fed Radiator	Voltage-Fed Radiator
¼-¾-1¼-etc. wavelengths	Open Stub	Shorted Stub
½-1-1½-2-etc. wavelengths	Shorted Stub	Open Stub

Linear R-F Transformers A resonant quarter-wave line has the unusual property of acting much as a transformer. Let us take, for example, a section consisting of no. 12 wire spaced 6 inches, which happens to have a surge impedance of 600 ohms. Let the far end be terminated with a pure resistance, and let the near end be fed with radio-frequency energy at the frequency for which the line is a *quarter wavelength* long. If an impedance measuring set is used to measure the impedance at the near end while the impedance at the far end is varied, an interesting relationship between the 600-ohm characteristic surge impedance of this particular quarter-wave matching line, and the impedance at the ends will be discovered.

When the impedance at the far end of the line is the same as the characteristic surge impedance of the line itself (600 ohms), the impedance measured at the near end of the quarter-wave line will also be found to be 600 ohms.

Under these conditions, the line would not have any standing waves on it, since it is terminated in its characteristic impedance. Now, let the resistance at the far end of the line be doubled, or changed to 1200 ohms. The impedance measured at the near end of the line will be found to have been cut in half, to 300 ohms. If the resistance at the far end is made half the original value of 600 ohms or 300 ohms, the impedance at the near end doubles the original value of 600 ohms, and becomes 1200 ohms. As one resistance goes up, the other goes down proportionately.

It will always be found that the characteristic surge impedance of the quarter-wave matching line is the geometric mean between the impedance at both ends. This relationship is shown by the following formula:

$$Z_{MS} = \sqrt{Z_A Z_L}$$

where

Z_{MS} = Impedance of matching section.

Z_A = Antenna resistance.

Z_L = Line impedance.

Quarter-Wave Matching Transformers The impedance inverting characteristic of a quarter-wave section of transmission line is widely used by making such a section of line act as a *quarter-wave transformer*. The *Johnson Q* feed system is a widely known application of the quarter-wave transformer to the feeding of a dipole antenna and array consisting of two dipoles. However, the quarter-wave transformer may be used in a wide number of applications wherever a transformer is required to match two impedances whose geometric mean is somewhere between perhaps 25 and 750 ohms when transmission line sections can be used. Paralleled coaxial lines may be used to obtain the lowest impedance mentioned, and open-wire lines composed of small conductors spaced a moderate distance may be used to obtain the higher impedance. A short list of impedances, which may be matched by quarter-wave sections of transmission line having specified impedances, is given below.

Load or Ant. Impedance ↓	300	480	600	← Feed-Line Impedance
20	77	98	110	Quarter-
30	95	120	134	Wave
50	110	139	155	Transformer
75	150	190	212	Impedance
100	173	220	245	

Johnson-Q Feed System The standard form of *Johnson-Q* feed to a doublet is shown in figure 32. An impedance match is obtained by utilizing a matching section, the surge impedance of which is the geometric mean between the transmission line surge impedance and the radiation resistance of the radiator. A sufficiently good match usu-

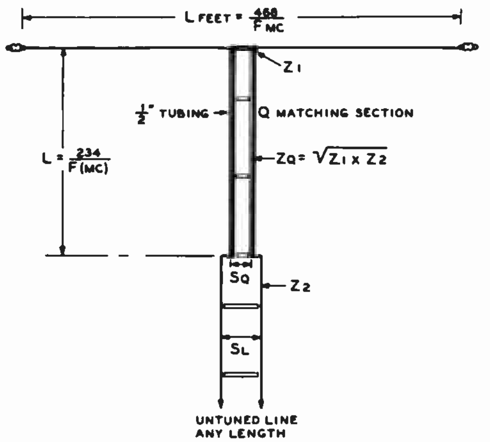


Figure 32

HALF-WAVE RADIATOR FED BY "Q BARS"

The Q matching section is simply a quarter-wave transformer whose impedance is equal to the geometric mean between the impedance at the center of the antenna and the impedance of the transmission line to be used to feed the bottom of the transformer. The transformer may be made up of parallel tubing, a four-wire line, or any other type of transmission line which has the correct value of impedance.

ally can be obtained by either designing or adjusting the matching section for a dipole to have a surge impedance that is the geometric mean between the line impedance and 72 ohms, the latter being the theoretical radiation resistance of a half-wave doublet either infinitely high or a half wave above a perfect ground.

Though the radiation resistance may depart somewhat from 72 ohms under actual conditions, satisfactory results will be obtained with this assumed value, so long as the dipole radiator is more than a quarter wave above effective earth, and reasonably in the clear. The small degree of standing waves introduced by a slight mismatch will not increase the line losses appreciably, and any *small* amount of reactance present can be tuned out at the transmitter termination with no bad effects. If the reactance is objectionable, it may be minimized by making the untuned line an integral number of quarter waves long.

A Q-matched system can be adjusted precisely, if desired, by constructing a matching section to the calculated dimensions with provision for varying the spacing of the Q section conductors slightly, after the untuned line has been checked for standing waves.

Center to Center Spacing in Inches	Impedance in Ohms for ½" Diameters	Impedance in Ohms for ¼" Diameters
1	170	250
1.25	188	277
1.5	207	298
1.75	225	318
2	248	335

PARALLEL TUBING SURGE IMPEDANCE FOR MATCHING SECTIONS

The Collins Transmission Line Matching System

The advantage of unbalanced output networks for transmitters are numerous; however this output system becomes awkward when it is desired to feed an antenna system utilizing a balanced input. For some time the *Collins Radio* Co. has been experimenting with a balun and tapered line system for matching a coaxial output transmitter to an open-wire balanced transmission line. Considerable success has been obtained and matching systems good over a frequency range as great as four to one have been developed. Illustrated in figure 33 is one type of matching system which is proving satisfactory over this range. Z_1 is the transmitter end of the system and may be any length of 52-ohm coaxial cable. Z_2 is one-quarter wavelength long at the *mid-frequency* of the range to be covered and is made of 75 ohm coaxial cable. Z_A is a quarter-wavelength shorted section of cable at the mid-frequency. Z_0 (Z_A and Z_2) forms a 200-ohm quarter-wave section. The Z_A section is formed of a conductor of the same diameter as Z_2. The difference in length between Z_A and Z_2 is accounted for by the fact that Z_2 is a coaxial conductor with a solid dielectric, whereas the dielectric for Z_0 is air. Z_3 is one-quarter wavelength long at the *mid-frequency* and has an imped-

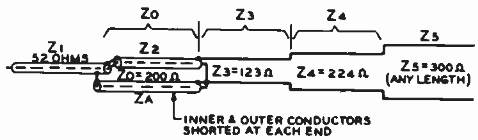


Figure 33

COLLINS TRANSMISSION LINE MATCHING SYSTEM

A wide-band system for matching a 52-ohm coaxial line to a balanced 300-ohm line over a 4:1 wide frequency range.

ance of 123 ohms. Z_4 is one-quarter wavelength long at the *mid-frequency* and has an impedance of 224 ohms. Z_5 is the balanced line to be matched (in this case 300 ohms) and may be any length.

Other system parameters for different output and input impedances may be calculated from the following:
Transformation ratio (r) for each section is:

$$r = \sqrt[N]{\frac{Z_{out}}{Z_{in}}}$$

Where N is the number of sections. In the above case,

$$r = \sqrt[3]{\frac{Z_5}{Z_1}}$$

Impedance between sections, as Z_{2-3}, is r times the preceding section. $Z_{2-3} = r \times Z_1$, and $Z_{3-4} = r \times Z_{2-3}$.
Mid-frequency (m):

$$m = \frac{F_1 + F_2}{2}$$

$$\text{For 40-20-10 meters} = \frac{7 + 30}{2} = 18.5 \text{ Mc.}$$

and one-quarter wavelength = 12 feet.

$$\text{For 20-10-6 meters} = \frac{14 + 54}{2} = 34 \text{ Mc.}$$

and one-quarter wavelength = 5.5 feet.

The impedances of the sections are:

$$Z_2 = \sqrt{Z_1 \times Z_{2-3}}$$

$$Z_3 = \sqrt{Z_{2-3} \times Z_{3-4}}$$

$$Z_4 = \sqrt{Z_{3-4} \times Z_5}$$

$$Z_6 = \tfrac{2}{3} \times Z_5$$

Generally, the larger number of taper sections the greater will be the bandwidth of the system.

19-9 Antenna Construction

The foregoing portion of this chapter has been concerned primarily with the *electrical* characteristics and considerations of antennas. Some of the physical aspects and mechanical problems incident to the actual erection of antennas and arrays will be discussed in the following section.

Up to 60 feet, there is little point in using mast-type antenna supports unless guy wires either must be eliminated or kept to a minimum. While a little more difficult to erect, because of their floppy nature, fabricated wood poles of the type to be described will be just as satisfactory as more rigid types, *provided* many guy wires are used.

Rather expensive when purchased through the regular channels, 40- and 50-foot telephone poles sometimes can be obtained quite reasonably. In the latter case, they are hard to beat, inasmuch as they require no guying if set in the ground six feet (standard depth), and the resultant pull in any lateral direction is not in excess of a hundred pounds or so.

For heights of 80 to 100 feet, either three-sided or four-sided lattice type masts are most practicable. They can be made self-supporting, but a few guys will enable one to use a smaller cross section without danger from high winds. The torque exerted on the base of a high self-supporting mast is terrific during a strong wind.

The "A-Frame" Mast Figures 34A and 34B show the standard method of construction of the *A-frame* type of mast. This type of mast is quite frequently used since there is only a moderate amount of work involved in the construction of the assembly and since the material cost is relatively small. The three pieces of selected 2 by 2 are first set up on three sawhorses or boxes and the holes drilled for the three ¼-inch bolts through the center of the assembly. Then the base legs are spread out to about 6 feet and the bottom braces installed. Then the upper braces and the cross pieces are installed and the assembly given several coats of good-quality paint as a protection against weathering.

Figure 34C shows another common type of mast which is made up of sections of 2 by 4 placed end-to-end with stiffening sections of 1 by 6 bolted to the edge of the 2 by 4 sections. Both types of masts will require a set of top guys and another set of guys about one-third of the way down from the top. Two guys spaced about 90 to 100 degrees and pulling against the load of the antenna will normally be adequate for the top guys. Three guys are usually used at the lower level, with one directly behind the load of the antenna and two more spaced 120 degrees from the rear guy.

The raising of the mast is made much easier

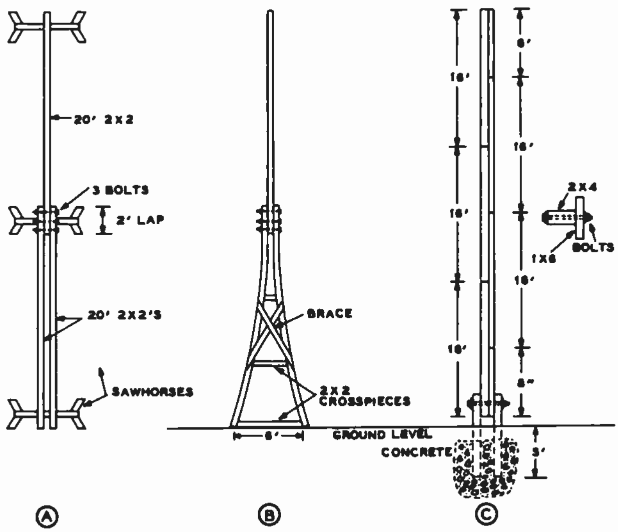


Figure 34
TWO SIMPLE WOOD MASTS
Shown at (A) is the method of assembly, and at (B) is the completed structure, of the conventional "A-frame" antenna mast. At (C) is shown a structure which is heavier but more stable than the A-frame for heights above about 40 feet.

if a gin pole about 20 feet high is installed about 30 or 40 feet to the rear of the direction in which the antenna is to be raised. A line from a pulley on the top of the gin pole is then run to the top of the pole to be raised. The gin pole comes into play when the center of the mast has been raised 10 to 20 feet above the ground and an additional elevated pull is required to keep the top of the mast coming up as the center is raised further above ground.

Using TV Masts Steel tubing masts of the telescoping variety are widely available at a moderate price for use in supporting television antenna arrays. These masts usually consist of several 10-foot lengths of electrical metal tubing (EMT) of sizes such that the sections will telescope. The 30-foot and 40-foot lengths are well suited as masts for supporting antennas and arrays of the types used on the amateur bands. The masts are constructed in such a manner that the bottom 10-foot length may be guyed permanently before the other sections are raised. Then the upper sections may be extended, beginning with the top-mast section, until the mast is at full length (provided a strong wind is not blowing) following which all the guys may be anchored. It is important that there be no load on the top of the mast when the "vertical" raising method is to be employed.

Guy Wires Guy wires should never be pulled taut; a *small* amount of slack is desirable. Galvanized wire, somewhat heavier than seems sufficient for the job, should be used. The heavier wire is a little harder to handle, but costs only a little more and takes longer to rust through. Care should be taken to make sure that no kinks exist when the pole or tower is ready for erection, as the wire will be greatly weakened at such points if a kink is pulled tight, even if it is later straightened.

If "dead men" are used for the guy wire terminations, the wire or rod reaching from the dead men to the surface should be of non-rusting material, such as brass, or given a heavy coating of asphalt or other protective substance to prevent destructive action by the damp soil. Galvanized iron wire will last only a short time when buried in moist soil.

Only strain-type (compression) insulators should be used for guy wires. Regular ones might be sufficiently strong for the job, but it is not worth taking chances, and egg-type strain halyard insulators are no more expensive.

Only a brass or bronze pulley should be used for the halyard, as a high pole with a rusted pulley is truly a sad affair. The bearing of the pulley should be given a few drops of heavy machine oil before the pole or tower is raised. The halyard itself should be of good material, preferably water-proofed. Hemp rope of good quality is better than window sash cord from several standpoints, and is less expensive. Soaking it thoroughly in engine oil of medium viscosity, and then wiping it off with a rag, will not only extend its life but minimize shrinkage in wet weather. Because of the difficulty of replacing a broken halyard it is a good idea to replace it periodically, without waiting for it to show excessive wear or deterioration.

It is an excellent idea to tie both ends of the halyard line together in the manner of a flag-pole line. Then the antenna is tied onto the place where the two ends of the halyard are joined. This procedure of making the halyard into a loop prevents losing the top end of the halyard should the antenna break near the end, and it also prevents losing the halyard completely should the end of the halyard carelessly be allowed to go free and be pulled through the pulley at the top of the mast by the antenna load. A somewhat longer piece of line is required but the insurance is well worth the cost of the additional length of rope.

Trees as Supports Often a tall tree can be called upon to support one end of an antenna, but one should not attempt to attach anything to the top, as the swaying of the top of the tree during a heavy wind will complicate matters.

If a tree is utilized for support, provision should be made for keeping the antenna taut without submitting it to the possibility of being severed during a heavy wind. This can be done by the simple expedient of using a pulley and halyard, with weights attached to the lower end of the halyard to keep the antenna taut. Only enough weight to avoid excessive sag in the antenna should be tied to the halyard, as the continual swaying of the tree submits the pulley and halyard to considerable wear.

Galvanized iron pipe, or steel-tube conduit, is often used as a vertical radiator, and is quite satisfactory for the purpose. However, when used for supporting antennas, it should be remembered that the grounded supporting poles will distort the field pattern of a vertically polarized antenna unless spaced some distance from the radiating portion.

Painting The life of a wood mast or pole can be increased several hundred per cent by protecting it from the elements with a coat or two of paint. And, of course, the appearance is greatly enhanced. The wood should first be given a primer coat of flat white outside house paint, which can be thinned down a bit to advantage with second-grade linseed oil. For the second coat, which should not be applied until the first is thoroughly dry, *aluminum paint* is not only the best from a preservative standpoint, but looks very well. This type of paint, when purchased in quantities, is considerably cheaper than might be gathered from the price asked for quarter-pint cans.

Portions of posts or poles below the surface of the soil can be protected from termites and moisture by painting with creosote. While not so strong initially, redwood will deteriorate much more slowly when buried than will the white woods, such as pine.

Antenna Wire The antenna or array itself presents no especial problem. A few considerations should be borne in mind, however. For instance, soft-drawn copper should not be used, as even a short span will stretch several per cent after whipping around in the wind a few weeks, thus affecting the resonant frequency. Enameled-copper wire, as ordinarily available at radio stores, is usally soft drawn, but by tying one end to some object such as a telephone pole and the other to the frame of an auto, a few husky tugs can be given and the wire, after stretching a bit, is equivalent to hard drawn.

Where a long span of wire is required, or where heavy insulators in the center of the span result in considerable tension, copper-clad steel wire is somewhat better than hard-drawn copper. It is a bit more expensive, though the cost is far from prohibitive. The use of such wire, in conjunction with strain insulators, is advisable, where the antenna would endanger persons or property should it break.

For transmission lines and tuning stubs steel-core or hard-drawn wire will prove awkward to handle, and soft-drawn copper should, therefore, be used. If the line is long, the strain can be eased by supporting it at several points.

More important from an electrical standpoint than the actual size of wire used is the soldering of joints, especially at current loops in an antenna of low radiation resistance. In fact, it is good practice to solder *all* joints, thus insuring quiet operation when the antenna is used for receiving.

Insulation A question that often arises is that of insulation. It depends, of course, upon the r-f voltage at the point at which the insulator is placed. The r-f voltage, in turn, depends upon the distance from a current node, and the radiation resistance of the antenna. Radiators having low radiation resistance have very high voltage at the voltage loops; consequently, better than usual insulation is advisable at those points.

Open-wire lines operated as non-resonant lines have little voltage across them; hence the most inexpensive ceramic types are sufficiently good electrically. With tuned lines, the voltage depends upon the amplitude of the standing waves. If they are very great, the voltage will reach high values at the voltage loops, and the best spacers available are none too good. At the current loops the voltage is quite low, and almost anything will suffice.

When insulators are subject to very high r-f voltages, they should be cleaned occasionally if in the vicinity of sea water or smoke. Salt scum and soot are not readily dislodged by rain, and when the coating becomes heavy enough, the efficiency of the insulators is greatly impaired.

If a very pretentious installation is to be made, it is wise to check up on both underwriter's rules and local ordinances which might be applicable. If you live anywhere near an airport, and are contemplating a tall pole, it is best to investigate possible regulations and ordinances pertaining to towers in the district, before starting construction.

19-10 Coupling to the Antenna System

When coupling an antenna feed system to a transmitter the most important considerations are as follows: (1) means should be provided for varying the load on the amplifier; (2) the two tubes in a push-pull amplifier should be equally loaded; (3) the load presented to the final amplifier should be resistive (non-reactive) in character; and (4) means should be provided to reduce harmonic coupling between the final amplifier plate tank circuit and the antenna or antenna transmission line to an *extremely low* value.

The Transmitter-Loading Problem The problem of coupling the power output of a high-frequency or v-h-f transmitter to the radiating portion of the antenna system has been materially complicated by the virtual necessity for eliminating interference to TV reception. However, the TVI-elimination portion of the problem may *always* be accomplished by adequate shielding of the transmitter, by filtering of the control and power leads which enter the transmitter enclosure, and by the inclusion of a harmonic-attenuating filter between the output of the transmitter and the antenna system.

Although TVI may be eliminated through inclusion of a filter between the output of a shielded transmitter and the antenna system, the fact that such a filter must be included in the link between transmitter and antenna makes it necessary that the transmitter-loading problem be re-evaluated in terms of the necessity for inclusion of such a filter.

Harmonic-attenuating filters must be operated at an impedance level which is close to their design value; therefore they must operate *into* a resistive termination substantially equal to the characteristic impedance of the filter. If such filters are operated into an impedance which is not resistive and approximately equal to their characteristic impedance: (1) the capacitors used in the filter sections will be subjected to high peak voltages and may be damaged, (2) the harmonic-attenuating properties of the filter will be decreased, and (3) the impedance at the input end of the filter will be different from that seen by the filter at the load end (except in the case of the half-wave type of filter). It is therefore important that the filter be included in the transmitter-to-antenna circuit at a point where the impedance is close to the nominal value of the filter, and at a point where this impedance is likely to remain fairly constant with variations in frequency.

Block Diagrams of Transmitter-to-Antenna Coupling Systems There are two basic arrangements which include all the provisions required in the transmitter-to-antenna coupling system, and which permit the harmonic-attenuating filter to be placed at a position in the coupling system where it can be operated at an impedance level close to its nominal value. These arrangements are illustrated in block-diagram form in figures 35 and 36.

The arrangement of figure 35 is recommended for use with a single-band antenna system, such as a dipole or a rotatable array, wherein an impedance matching system is included

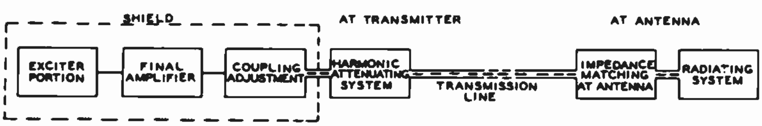


Figure 35

ANTENNA COUPLING SYSTEM

The harmonic suppressing antenna coupling system illustrated above is for use when the antenna transmission line has a low standing-wave ratio, and when the characteristic impedance of the antenna transmission line is the same as the nominal impedance of the low-pass harmonic-attenuating filter.

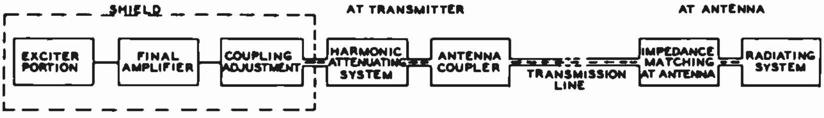


Figure 36

ANTENNA COUPLING SYSTEM

The antenna coupling system illustrated above is for use when the antenna transmission line does not have the same characteristic impedance as the TVI filter, and when the standing-wave ratio on the antenna transmission line may or may not be low.

within or adjacent to the antenna. The feed line coming down from the antenna system should have a characteristic impedance equal to the nominal impedance of the harmonic filter, and the impedance matching at the antenna should be such that the standing-wave ratio on the antenna feed line is less than 2 to 1 over the range of frequency to be fed to the antenna. Such an arrangement may be used with open-wire line, ribbon or tubular line, or with coaxial cable. The use of coaxial cable is to be recommended, but in any event the impedance of the antenna transmission line should be the same as the nominal impedance of the harmonic filter. The arrangement of figure 35 is more or less standard for commercially manufactured equipment for amateur and commercial use in the h-f and v-h-f range.

The arrangement of figure 36 merely adds an antenna coupler between the output of the harmonic attenuating filter and the antenna transmission line. The antenna coupler will have some harmonic-attenuating action, but its main function is to transform the impedance at the station end of the antenna transmission line to the nominal value of the harmonic filter. Hence the arrangement of figure 36 is more general than the figure 35 system, since the inclusion of the antenna coupler allows the system to feed an antenna transmission line of any reasonable impedance value, and also without regard to the standing-wave ratio which might exist on the antenna transmission line. Antenna couplers are discussed in a following section.

Output Coupling Adjustment It will be noticed by reference to both figure 35 and figure 36 that a box labeled *Coupling Adjustment* is included in the block diagram. Such an element is necessary in the complete system to afford an adjustment in the value of load impedance presented to the tubes in the final amplifier stage of the transmitter. The impedance at the input terminal of the harmonic filter is established by the antenna, through its matching system and the antenna coupler, if used. In any event the impedance at the input terminal of the harmonic filter should be very close to the nominal impedance of the filter. Then the Coupling Adjustment provides means for transforming this impedance value to the correct operating value of load impedance which should be presented to the final amplifier stage.

There are two common ways for accomplishing the antenna coupling adjustment, as illustrated in figures 37 and 38. Figure 37 shows the variable-link arrangement most commonly used in home-constructed equipment, while the pi-netowrk coupling arrangement commonly used in commercial equipment is illustrated in figure 38. Either method may be used, and each has its advantages.

Variable-Link Coupling The variable-link method illustrated in figure 37 has the advantage that standard manufactured components may be used with no changes. However, for greatest bandwidth of operation of the coupling circuit, the reactance of the link coil, L, and the reactance of the link tuning capacitor, C, should both be between 3 and 4 times the nominal load impedance of the harmonic filter. This is to say that the inductive reactance of the coupling link L should be tuned out or resonated by capacitor C, and the operating Q of the L-C link circuit should be between 3 and 4. If the link coil is not variable with respect to the tank coil of the final amplifier, capacitor C *may* be used as a loading control; however, this system is not recommended since its use will require adjustment of C whenever a frequency change is made at the transmitter. If L and C are made resonant at the center of a band, with a link circuit Q of 3 to 4, and coupling adjustment is made by physical adjustment of L with respect to the final amplifier tank coil, it usually will be possible to operate over an entire amateur band without change in the coupling system. Capacitor C normally may have a low voltage rating, even with a high power transmitter, due to the low Q and low impedance of the coupling circuit.

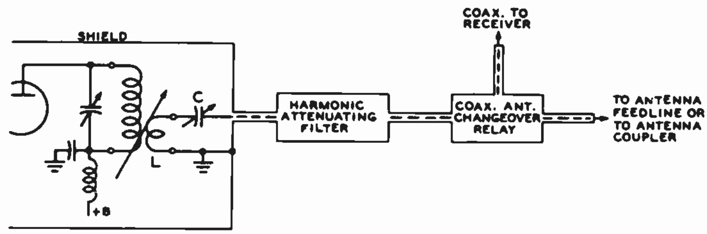


Figure 37

TUNED-LINK OUTPUT CIRCUIT

Capacitor C should be adjusted so as to tune out the inductive reactance of the coupling link, L. Loading of the amplifier then is varied by physically varying the coupling between the plate tank of the final amplifier and the antenna coupling link.

Pi-Network Coupling The pi-network coupling system offers two advantages: (1) a *mechanical* coupling variation is not required to vary the loading of the final amplifier, and (2) the pi network (if used with an operating Q of about 15) offers within itself a harmonic attenuation of 40 db or more, in addition to the harmonic attenuation provided by the additional harmonic attenuating filter. Some commercial equipments (such as the Collins amateur transmitters) incorporate an L network in addition to the pi network, for accomplishing the impedance transformation in two steps and to provide additional harmonic attenuation.

Tuning the Pi-Section Coupler Tuning of a pi-network coupling circuit such as illustrated in figure 38 is accomplished in the following manner: First remove the connection between the output of the amplifier and the harmonic filter (load). Tune C_2 to a capacitance which is large for the band in use, adding suitable additional capacitance by switch S if operation is to be on one of the lower frequency bands. Apply reduced plate voltage to the stage and dip to resonance with C_1. It may be necessary to vary the inductance in coil L, but in any event resonance should be reached with a setting of C_1 which is approximately correct for the desired value of operating Q of the pi network.

Next, couple the load to the amplifier (through the harmonic filter), apply reduced plate voltage again and dip to resonance with C_1. If the plate current dip with load is too low (taking into consideration the reduced plate voltage), *decrease* the capacitance of C_2 and again dip to resonance, repeating the procedure until the correct value of plate current is obtained with full plate voltage on the stage. There should be a relatively small change required in the setting of C_1 (from the original setting of C_1 without load) if the operating Q of the network is correct and if a large value of impedance transformation is being employed—as would be the case when transforming from the plate impedance of a single-

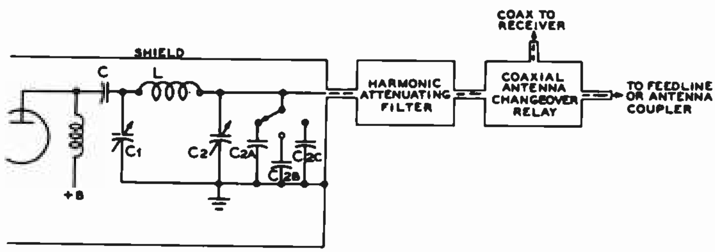


Figure 38

PI-NETWORK ANTENNA COUPLER

The design of pi-network output circuits is discussed in Chapter Eleven. The additional output-end shunting capacitors selected by switch S are for use on the lower frequency ranges. Inductor L may be selected by a tap switch, it may be continuously variable, or plug-in inductors may be used.

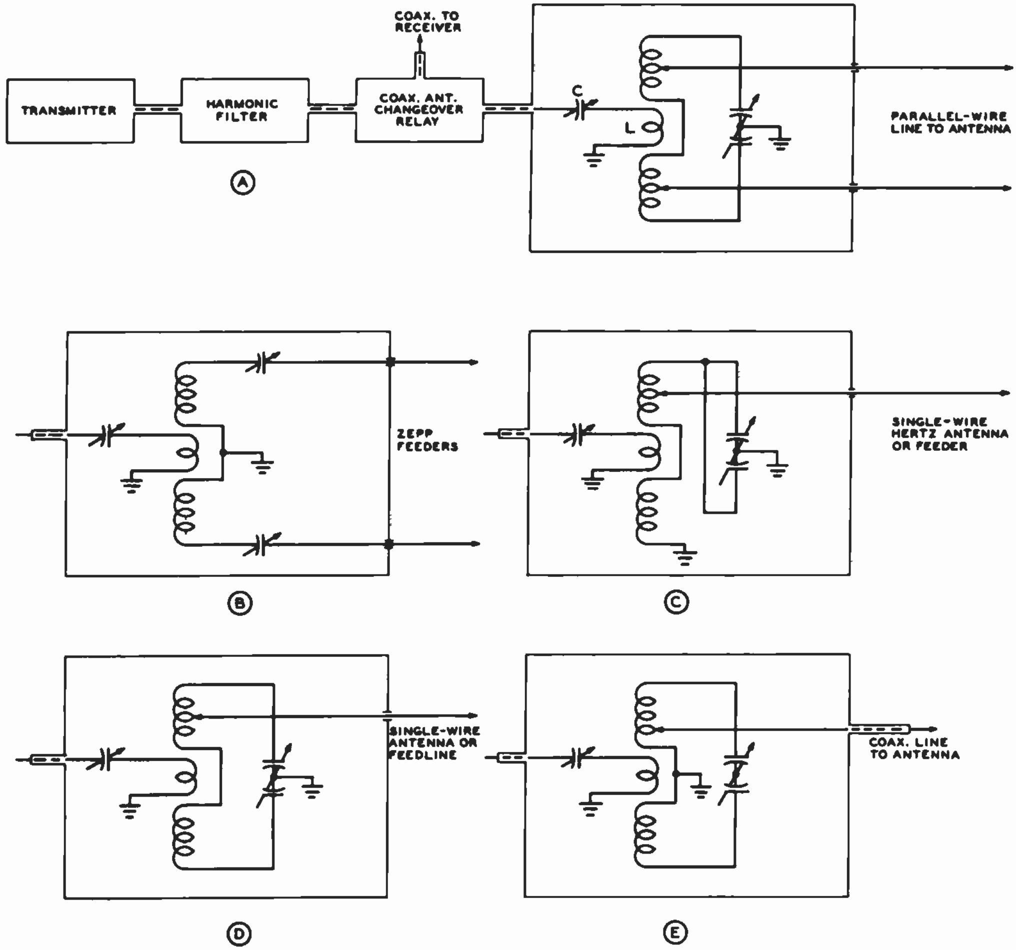


Figure 39

ALTERNATIVE ANTENNA-COUPLER CIRCUITS

Plug-in coils, one or two variable capacitors of the split-stator variety, and a system of switches or plugs and jacks may be used in the antenna coupler to accomplish the feeding of different types of antennas and antenna transmission lines from the coaxial input line from the transmitter or from the antenna changeover relay. Link L should be resonated with capacitor C at the operating frequency of the transmitter so that the harmonic filter will operate into a resistive load impedance of the correct nominal value.

ended output stage down to the 50-ohm impedance of the usual harmonic filter and its subsequent load.

In a pi network of this type the harmonic attenuation of the section will be adequate when the correct value of C_1 and L are being used and when the resonant dip in C_1 is sharp. If the dip in C_1 is broad, or if the plate current persists in being too high with C_2 at maximum setting, it means that a *greater* value of capacitance is required at C_2, assuming that the values of C_1 and L are correct.

19-11 Antenna Couplers

As stated in the previous section, an antenna coupler is not required when the impedance of the antenna transmission line is the same as the nominal impedance of the harmonic filter, assuming that the antenna feed line is being operated with a low standing-wave ratio. However, there are many cases where it is desirable to feed a multi-band antenna from the output of the harmonic filter, where a tuned line is being used to feed the antenna, or where a long wire without a separate feed line is to be fed from the output of the harmonic filter. In such cases an *antenna coupler* is required.

Some harmonic attenuation will be provided by the antenna coupler, particularly if it is well shielded. In certain cases when a pi network is being used at the output of the transmitter, the addition of a shielded antenna coupler will provide sufficient harmonic attenuation. But in all normal cases it will be necessary to include a harmonic filter between the output of the transmitter and the antenna coupler. When an adequate harmonic filter is being used, it will not be necessary in normal cases to shield the antenna coupler, except from the standpoint of safety or convenience.

Function of an Antenna Coupler The function of the antenna coupler is, basically, to transform the impedance of the antenna system being used to the correct value of *resistive* impedance for the harmonic filter, and hence for the transmitter. Thus the antenna coupler may be used to resonate the feeders or the radiating portion of the antenna system, in addition to its function of impedance transformation.

It is important to remember that there is *nothing* that can be done at the antenna coupler which will eliminate standing waves on the antenna transmission line. Standing waves are the result of reflection from the antenna, and the coupler can do nothing about this condition. However, the antenna coupler can resonate the feed line (by introducing a conjugate impedance) in addition to providing an impedance transformation. Thus, a resistive impedance of the correct value can be presented to the harmonic filter, as in figure 36, regardless of any *reasonable* value of standing-wave ratio on the antenna transmission line.

Types of Antenna Couplers All usual types of antenna couplers fall into two classifications: (1) inductively coupled resonant systems as exemplified by those shown in figure 39, and (2) conductively coupled pi-network systems such as shown in figure 40. The inductively-coupled system is much more commonly used, since it is convenient for feeding a balanced line from the coaxial output of the usual harmonic filter. The pi-network system is most useful for feeding a length of wire from the output of a transmitter.

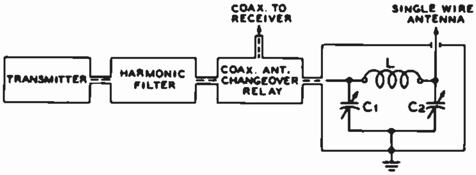


Figure 40
PI-NETWORK ANTENNA COUPLER

An arrangement such as illustrated above is convenient for feeding an end-fed Hertz antenna, or a random length of wire for portable or emergency operation, from the nominal value of impedance of the harmonic filter.

Several general methods for using the inductively-coupled resonant type of antenna coupler are illustrated in figure 39. The coupling between the link coil L and the main tuned circuit need not be variable; in fact it is preferable that the correct link size and placement be determined for the tank coil which will be used for each band, and then that the link be made a portion of the plug-in coil. Capacitor C then can be adjusted to a pre-determined value for each band such that it will resonate with the link coil for that band. The reactance of the link coil (and hence the reactance of the capacitor setting which will resonate the coil) should be about 3 or 4 times the impedance of the transmission line between the antenna coupler and the harmonic filter, so that the link coupling circuit will have an operating Q of 3 or 4. The use of capacitor C to resonate with the inductance of the link coil L will make it easier to provide a low standing-wave ratio to the output of the harmonic filter, simply by adjustment of the antenna-coupler tank circuit to resonance. If this capacitor is not included, the system still will operate satisfactorily, but the tank circuit will have to be detuned slightly from resonance so as to cancel the inductive reactance of the coupling link and thus provide a resistive load to the output of the harmonic filter. Variations in the loading of the final amplifier should be made by the coupling adjustment at the final amplifier, not at the antenna coupler.

The pi-network type of antenna coupler, as shown in figure 40 is useful for certain applications, but is primarily useful in feeding a single-wire antenna from a low-impedance transmission line. In such an application the operating Q of the pi network may be somewhat lower than that of a pi network in the plate circuit of the final amplifier of a transmitter, as shown in figure 38. An operating Q of 3 or 4

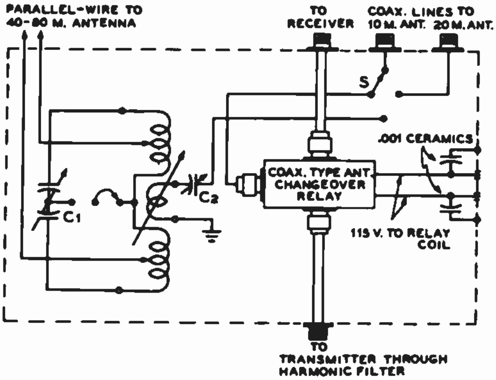


Figure 41

ALTERNATIVE COAXIAL ANTENNA COUPLER

This circuit is recommended not only as being most desirable when coaxial lines with low s.w.r. are being used to feed antenna systems such as rotatable beams, but when it also is desired to feed through open-wire line to some sort of multi-band antenna for the lower frequency ranges. The tuned circuit of the antenna coupler is operative only when using the open-wire feed, and then it is in operation both for transmit and receive.

in such an application will be found to be adequate, since harmonic attenuation has been accomplished ahead of the antenna coupler. However, the circuit will be easier to tune, although it will not have as great a bandwidth, if the operating Q is made higher.

An alternative arrangement shown in figure 41 utilizes the antenna coupling tank circuit only when feeding the coaxial output of the transmitter to the open-wire feed line (or similar multi-band antenna) of the 40-80 meter antenna. The coaxial lines to the 10-meter beam and to the 20-meter beam would be fed directly from the output of the coaxial antenna changeover relay through switch S.

CHAPTER TWENTY

High Frequency Directive Antennas

It is becoming of increasing importance in most types of radio communication to be capable of concentrating the radiated signal from the transmitter in a certain desired direction and to be able to discriminate at the receiver against reception from directions other than the desired one. Such capabilities involve the use of directive antenna arrays.

Few simple antennas, except the single vertical element, radiate energy equally well in all azimuth (horizontal or compass) directions. All horizontal antennas, except those specifically designed to give an omnidirectional azimuth radiation pattern such as the turnstile, have some directive properties. These properties depend upon the length of the antenna in wavelengths, the height above ground, and the slope of the radiator.

The various forms of the half-wave horizontal antenna produce maximum radiation at right angles to the wire, but the directional effect is not great. Nearby objects also minimize the directivity of a dipole radiator, so that it hardly seems worth while to go to the trouble to rotate a simple half-wave dipole in an attempt to improve transmission and reception in any direction.

The half-wave doublet, folded dipole, zepp, single-wire-fed, matched impedance, and Johnson Q antennas all have practically the same radiation pattern *when properly built and adjusted.* They all are dipoles, and the feeder system, if it does not radiate in itself, will have no effect on the radiation pattern.

20-1 Directive Antennas

When a multiplicity of radiating elements is located and phased so as to reinforce the radiation in certain desired directions and to neutralize radiation in other directions, a *directive antenna array* is formed.

The function of a directive antenna when used for transmitting is to give an increase in signal strength in some direction at the expense of radiation in other directions. For reception, one might find useful an antenna giving little or no gain in the direction from which it is desired to receive signals if the antenna is able to discriminate against interfering signals and static arriving from other directions. A good directive transmitting antenna, however, can also be used to good advantage for reception.

If radiation can be confined to a narrow beam, the signal intensity can be increased a great many times in the desired direction of transmission. This is equivalent to increasing the power output of the transmitter. On the higher frequencies, it is more economical to

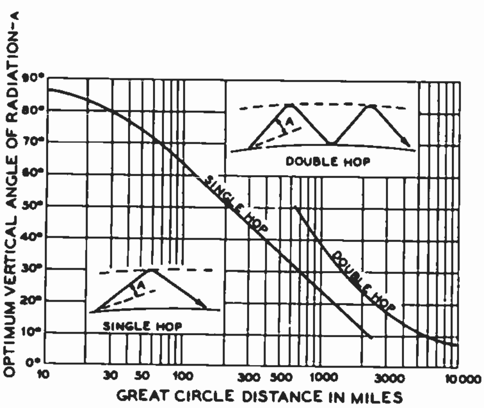


Figure 1

OPTIMUM ANGLE OF RADIATION WITH RESPECT TO DISTANCES

Shown above is a plot of the optimum angle of radiation for one-hop and two-hop communication. An operating frequency close to the optimum working frequency for the communication distance is assumed.

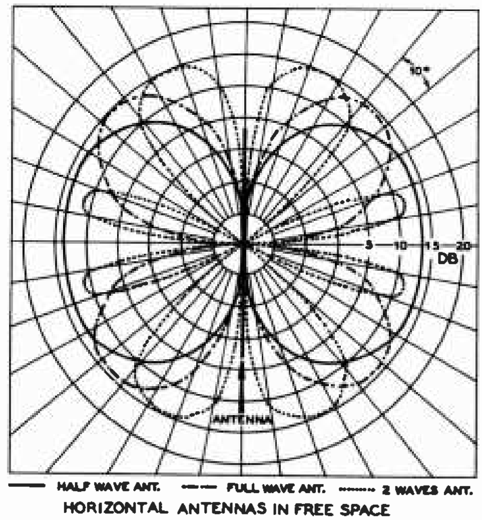


Figure 2

FREE-SPACE FIELD PATTERNS OF LONG-WIRE ANTENNAS

The presence of the earth distorts the field pattern in such a manner that the azimuth pattern becomes a function of the elevation angle.

use a directive antenna than to increase transmitter power, if more than a few watts of power is being used.

Directive antennas for the high-frequency range have been designed and used commercially with gains as high as 23 db over a simple dipole radiator. Gains as high as 35 db are common in direct-ray microwave communication and radar systems. A gain of 23 db represents a power gain of 200 times and a gain of 35 db represents a power gain of almost 3500 times. However, an antenna with a gain of only 15 to 20 db is so sharp in its radiation pattern that it is usable to full advantage only for point-to-point work.

The increase in radiated power in the desired direction is obtained at the expense of radiation in the undesired directions. Power gains of 3 to 12 db seem to be most practicable for amateur communication, since the width of a beam with this order of power gain is wide enough to sweep a fairly large area. Gains of 3 to 12 db represent effective transmitter power increases from 2 to 16 times.

Horizontal Pattern vs. Vertical Angle There is a certain optimum vertical angle of radiation for sky-wave communication, this angle being dependent upon distance, frequency, time of day, etc. Energy radiated at an angle much lower than this optimum angle is largely lost, while radiation at angles much higher than this optimum angle oftentimes is not nearly so effective.

For this reason, the horizontal directivity pattern as measured on the ground is of no import when dealing with frequencies and distances dependent upon sky-wave propagation. It is the horizontal directivity (or gain or discrimination) *measured at the most useful vertical angles of radiation* that is of consequence. The horizontal radiation pattern, as measured on the ground, is considerably different from the pattern obtained at a vertical angle of 15°, and still more different from a pattern obtained at a vertical angle of 30°. In general, the energy which is radiated at angles higher than approximately 30° above the earth is effective at any frequency only for local work.

For operation at frequencies in the vicinity of 14 Mc., the most effective angle of radiation is usually about 15° above the horizon, from *any* kind of antenna. The most effective angles for 10-meter operation are those in the vicinity of 10°. Figure 1 is a chart giving the optimum vertical angle of radiation for sky-wave propagation in terms of the great-circle distance between the transmitting and receiving antennas.

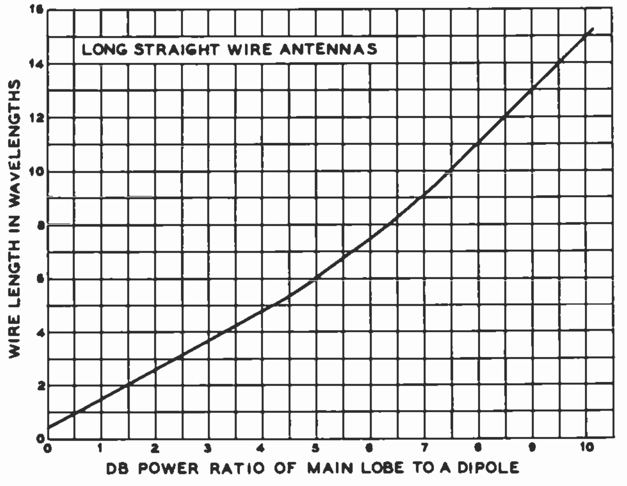


Figure 3
DIRECTIVE GAIN OF LONG-WIRE ANTENNAS

Types of Directive Arrays There is an enormous variety of directive antenna arrays that can give a substantial power gain in the desired direction of transmission or reception. However, some are more effective than others requiring the same space. In general it may be stated that long-wire antennas of various types, such as the single long wire, the V beam, and the rhombic, are less effective for a given space than arrays composed of resonant elements, but the long-wire arrays have the significant advantage that they may be used over a relatively large frequency range while resonant arrays are usable only over a quite narrow frequency band.

20-2 Long Wire Radiators

Harmonically operated long wires radiate better in certain directions than others, but cannot be considered as having appreciable directivity unless several wavelengths long. The current in adjoining half-wave elements flows in opposite directions at any instant, and thus, the radiation from the various elements adds in certain directions and cancels in others.

A half-wave doublet in free space has a "doughnut" of radiation surrounding it. A full wave has 2 lobes, 3 half waves 3, etc. When the radiator is made more than 4 half wavelengths long, the *end* lobes (cones of radiation) begin to show noticeable power gain over a half-wave doublet, while the broadside lobes get smaller and smaller in amplitude, even though numerous (figure 2).

The horizontal radiation pattern of such antennas depends upon the vertical angle of radiation being considered. If the wire is more than 4 wavelengths long, the maximum radiation at vertical angles of 15° to 20° (useful for dx) is in line with the wire, being slightly greater a few degrees either side of the wire than directly off the ends. The directivity of the main lobes of radiation is not particularly sharp, and the minor lobes fill in between the main lobes to permit working stations in nearly all directions, though the power radiated broadside to the radiator will not be great if the radiator is more than a few wavelengths long. The directive gain of long-wire antennas, in terms of the wire length in wavelengths is given in figure 3.

To maintain the out-of-phase condition in adjoining half-wave elements throughout the length of the radiator, it is necessary that a harmonic antenna be fed either at *one end* or at a *current* loop. If fed at a voltage loop, the adjacent sections will be fed *in* phase, and a different radiation pattern will result.

The directivity of a long wire does not increase very much as the length is increased beyond about 15 wavelengths. This is due to the fact that all long-wire antennas are adversely affected by the r-f resistance of the wire, and because the current amplitude begins to become unequal at different current loops, as a result of attenuation along the wire caused by radiation and losses. As the length is increased, the tuning of the antenna becomes quite broad. In fact, a long wire about 15 waves long is practically aperiodic, and works almost equally well over a wide range of frequencies.

LONG-ANTENNA DESIGN TABLE.

Approximate Length in Feet — End-Fed Antennas

Frequency in Mc.	1λ	1½λ	2λ	2½λ	3λ	3½λ	4λ	4½λ
30	32	48	65	81	97	104	130	146
29	33	50	67	84	101	118	135	152
28	34	52	69	87	104	122	140	157
14.4	66½	100	134	169	203	237	271	305
14.2	67½	102	137	171	206	240	275	310
14.0	68½	103½	139	174	209	244	279	314
7.3	136	206	276	346	416	486	555	625
7.15	136½	207	277	347	417	487	557	627
7.0	137	207½	277½	348	418	488	558	628
4.0	240	362	485	618	730	853	977	1100
3.9	246	372	498	625	750	877	1000	1130
3.8	252	381	511	640	770	900	1030	1160
3.7	259	392	525	658	790	923	1060	1190
3.6	266	403	540	676	812	950	1090	1220
3.5	274	414	555	696	835	977	1120	
2.0	480	725	972	1230	1475			
1.9	504	763	1020	1280				
1.8	532	805	1080					

One of the most practical methods of feeding a long-wire antenna is to bring one end of it into the radio room for direct connection to a tuned antenna circuit which is link-coupled through a harmonic-attenuating filter to the transmitter. The antenna can be tuned effectively to resonance for operation on any harmonic by means of the tuned circuit which is connected to the end of the antenna. A ground is sometimes connected to the center of the tuned coil.

If desired, the antenna can be opened and current-fed at a point of maximum *current* by means of low-impedance ribbon line, or by a quarter-wave matching section and open line.

20-3 The V Antenna

If two long-wire antennas are built in the form of a V, it is possible to make two of the maximum lobes of one leg shoot in the same direction as two of the maximum lobes of the other leg of the V. The resulting antenna is bidirectional (two opposite directions) for the main lobes of radiation. Each side of the V can be made any odd or even number of quarter wavelengths, depending on the method of feeding the apex of the V. The complete system must be a multiple of half waves. If each leg is an even number of quarter waves long, the antenna must be voltage-fed at the apex; if an odd number of quarter waves long, current feed must be used.

By choosing the proper apex angle, figure 4 and figure 5, the lobes of radiation from the two long-wire antennas aid each other to form a bidirectional beam. Each wire by itself would have a radiation pattern similar to that

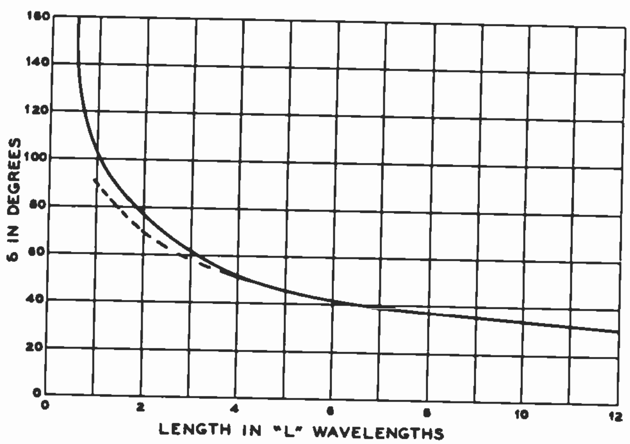


Figure 4

INCLUDED ANGLE FOR A "V" BEAM

Showing the included angle between the legs of a V beam for various leg lengths. For optimum alignment of the radiation lobe at the correct vertical angle with leg lengths less than three wavelengths, the optimum included angle is shown by the dashed curve.

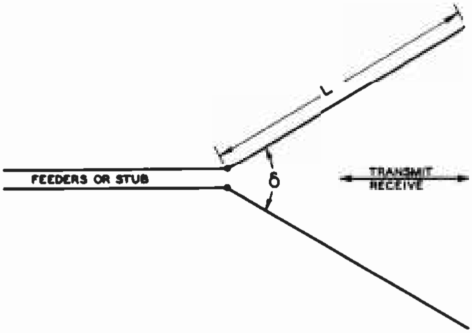


Figure 5

TYPICAL "V" BEAM ANTENNA

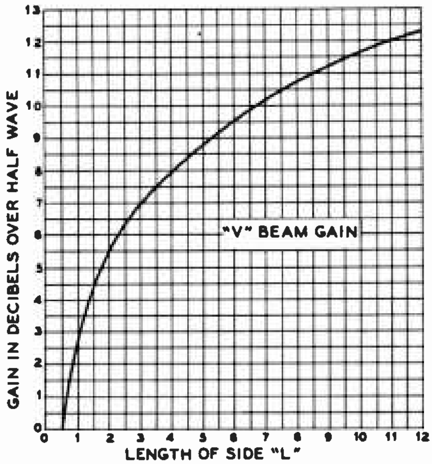


Figure 6

DIRECTIVE GAIN OF A "V" BEAM

This curve shows the approximate directive gain of a V beam with respect to a half-wave antenna located the same distance above ground, in terms of the side length L.

for a long wire. The reaction of one upon the other removes two of the four main lobes, and increases the other two in such a way as to form two lobes of still greater magnitude.

The correct wire lengths and the degree of the angle δ are listed in the *V-Antenna Design Table* for various frequencies in the 10-, 20- and 40-meter amateur bands. Apex angles for all side lengths are given in figure 4. The gain of a "V" beam in terms of the side length when optimum apex angle is used is given in figure 6.

The legs of a very long V antenna are usually so arranged that the included angle is twice the angle of the major lobe from a single wire if used alone. This arrangement concentrates the radiation of each wire along the bisector of the angle, and permits part of the other lobes to cancel each other.

With legs shorter than 3 wavelengths, the best directivity and gain are obtained with a somewhat smaller angle than that determined by the lobes. Optimum directivity for a one-wave V is obtained when the angle is 90° rather than 180°, as determined by the ground pattern alone.

If very long wires are used in the V, the angle between the wires is almost unchanged when the length of the wires in wavelengths is altered. However, an error of a few degrees causes a much larger loss in directivity and gain in the case of the longer V than in the shorter one.

The vertical angle at which the wave is best transmitted or received from a horizontal V antenna depends largely upon the included angle. The sides of the V antenna should be at least a half wavelength above ground; commercial practice dictates a height of approximately a full wavelength above ground.

V-ANTENNA DESIGN TABLE.

Frequency in Kilocycles	$L = \lambda$, $\delta = 90°$	$L = 2\lambda$, $\delta = 70°$	$L = 4\lambda$, $\delta = 52°$	$L = 8\lambda$, $\delta = 39°$
28000	34'8"	69'8"	140'	280'
28500	34'1"	68'6"	137'6"	275'
29000	33'6"	67'3"	135'	271'
29500	33'	66'2"	133'	266'
14050	69'	139'	279'	558'
14150	68'6"	138'	277'	555'
14250	68'2"	137'	275'	552'
14350	67'7"	136'	273'	548'
7020	138'2"	278'	558'	1120'
7100	136'8"	275'	552'	1106'
7200	134'10"	271'	545'	1090'
7280	133'4"	268'	538'	1078'

20-4 The Rhombic Antenna

The terminated *rhombic* or *diamond* is probably the most effective directional antenna that is practical for amateur communication. This antenna is non-resonant, with the result that it can be used on three amateur bands, such as 10, 20, and 40 meters. When the antenna is non-resonant, i.e., properly terminated, the system is undirectional, and the wire dimensions are not critical.

Rhombic Termination When the free end is terminated with a resistance of a value between 700 and 800 ohms the backwave is eliminated, the forward gain is increased, and the antenna can be used on several bands without changes. The terminating resistance should be capable of dissipating one-third the power output of the transmitter, and should have very little reactance. For medium or low power transmitters, the non-inductive *plaque* resistors will serve as a satisfactory termination. Several manufacturers offer special resistors suitable for terminating a rhombic antenna. The terminating device should, for technical reasons, present a small amount of inductive reactance at the point of termination.

A compromise terminating device commonly used consists of a terminated 250-foot or longer length of line, made of resistance wire which *does not have too much resistance per unit length.* If the latter qualification is not met, the reactance of the line will be excessive. A 250-foot line consisting of no. 25 nichrome wire, spaced 6 inches and terminated with 800 ohms, will serve satisfactorily. Because of the attenuation of the line, the lumped resistance at the end of the line need dissipate but a few watts even when high power is used. A half-dozen 5000-ohm 2-watt carbon resistors in parallel will serve for all except very high power. The attenuating line may be folded back on itself to take up less room.

The determination of the best value of terminating resistor may be made while receiving, if the input impedance of the receiver is approximately 800 ohms. The value of resistor which gives the best directivity on reception will not give the most gain when transmitting, but there will be little difference between the two conditions.

The input resistance of the rhombic which is reflected into the transmission line that feeds it is always somewhat less than the terminating resistance, and is around 700 to 750 ohms when the terminating resistor is 800 ohms.

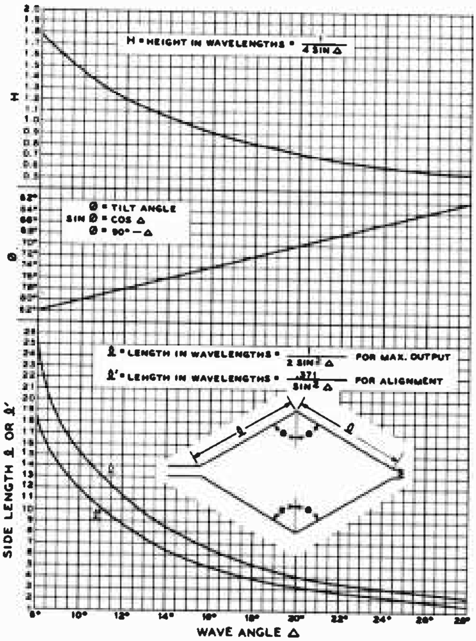


Figure 7

RHOMBIC ANTENNA DESIGN TABLE

Design data is given in terms of the wave angle (vertical angle of transmission and reception) of the antenna. The lengths l are for the "maximum output" design; the shorter lengths l' are for the "alignment" method which gives approximately 1.5 db less gain with a considerable reduction in the space required for the antenna. The values of side length, tilt angle, and height for a given wave angle are obtained by drawing a vertical line upward from the desired wave angle.

The antenna should be fed with a non-resonant line having a characteristic impedance of 650 to 700 ohms. The four corners of the rhombic should be at least one-half wavelength above ground for the lowest frequency of operation. For three-band operation the proper tilt angle ϕ for the center band should be observed.

The rhombic antenna transmits a horizontally-polarized wave at a relatively low angle above the horizon. The angle of radiation (wave angle) decreases as the height above ground is increased in the same manner as with a dipole antenna. The rhombic should not be tilted in any plane. In other words, the poles should all be of the same height and the plane of the antenna should be parallel with the ground.

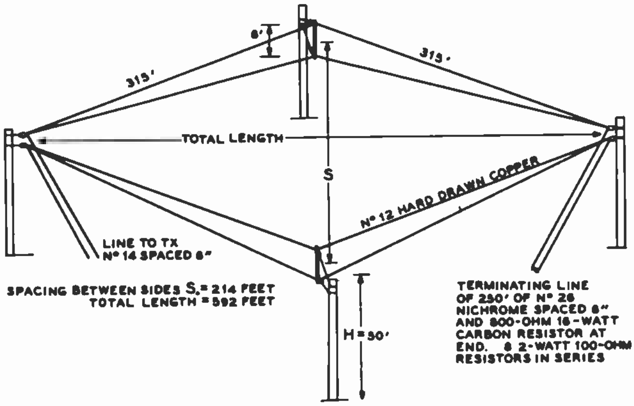


Figure 8

TYPICAL RHOMBIC ANTENNA DESIGN

The antenna system illustrated above may be used over the frequency range from 7 to 29 Mc. without change. The directivity of the system may be reversed by the system discussed in the text.

A considerable amount of directivity is lost when the terminating resistor is left off the end and the system is operated as a resonant antenna. If it is desired to reverse the direction of the antenna it is much better practice to run transmission lines to both ends of the antenna, and then run the terminating line to the operating position. Then with the aid of two d-p-d-t switches it will be possible to connect either feeder to the antenna changeover switch and the other feeder to the terminating line, thus reversing the direction of the array and maintaining the same termination for either direction of operation.

Figure 7 gives curves for optimum-design rhombic antennas by both the maximum-output method and the alignment method. The alignment method is about 1.5 db down from the maximum output method but requires only about 0.74 as much leg length. The height and tilt angle is the same in either case. Figure 8 gives construction data for a recommended rhombic antenna for the 7.0 through 29.7 Mc. bands. This antenna will give about 11 db gain in the 14.0-Mc. band. The approximate gain of a rhombic antenna over a dipole, both above normal soil, is given in figure 9.

20-5 Stacked-Dipole Arrays

The characteristics of a half-wave dipole already have been described. When another dipole is placed in the vicinity and excited either directly or parasitically, the resultant radiation pattern will depend upon the spacing and phase differential, as well as the relative magnitude of the currents. With spacings less than 0.65 wavelength, the radiation is mainly broadside to the two wires (bidirectional) when there is no phase difference, and *through* the wires (end fire) when the wires are 180° out of phase. With phase differences between 0°

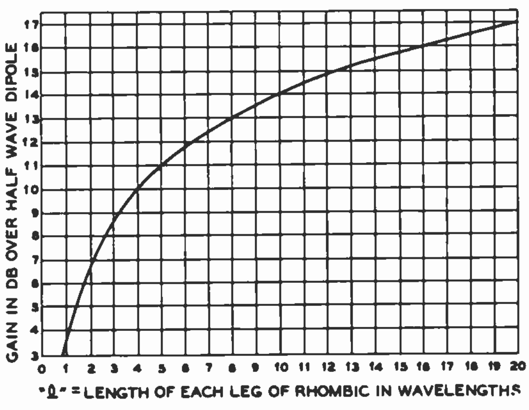


Figure 9

RHOMBIC ANTENNA GAIN

Showing the theoretical gain of a rhombic antenna, in terms of the side length, over a half-wave antenna mounted at the same height above the same type of soil.

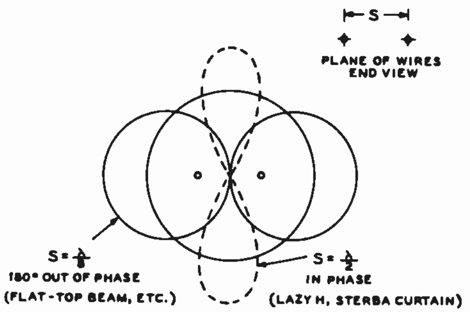


Figure 10

RADIATION PATTERNS OF A PAIR OF DIPOLES OPERATING WITH IN-PHASE EXCITATION, AND WITH EXCITATION 180° OUT OF PHASE

If the dipoles are oriented horizontally most of the directivity will be in the vertical plane; if they are oriented vertically most of the directivity will be in the horizontal plane.

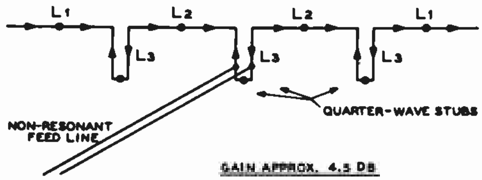


Figure 11

THE FRANKLIN OR COLINEAR ANTENNA ARRAY

An antenna of this type, regardless of the number of elements, attains all of its directivity through sharpening of the horizontal or azimuth radiation pattern; no vertical directivity is provided. Hence a long antenna of this type has an extremely sharp azimuth pattern, but no vertical directivity.

and 180° (45°, 90°, and 135° for instance), the pattern is unsymmetrical, the radiation being *greater in one direction* than in the opposite direction.

With spacings of more than 0.8 wavelength, more than two main lobes appear for all phasing combinations; hence, such spacings are seldom used.

In-Phase Spacing With the dipoles driven so as to be in phase, the most effective spacing is between 0.5 and 0.7 wavelength. The latter provides greater gain, but minor lobes are present which do not appear at 0.5-wavelength spacing. The radiation is broadside to the plane of the wires, and the gain is slightly greater than can be obtained from two dipoles out of phase. The gain falls off rapidly for spacings less than 0.375 wavelength, and there is little point in using spacing of 0.25 wavelength or less with in-phase dipoles, except where it is desirable to increase the radiation resistance. (See *Multi-Wire Doublet.*)

Out of Phase Spacing When the dipoles are fed 180° *out of phase*, the directivity is through the plane of the wires, and is greatest with *close spacing*, though there is but little difference in the pattern after the spacing is made less than 0.125 wavelength. The radiation resistance becomes so low for spacings of less than 0.1 wavelength that such spacings are not practicable.

In the three foregoing examples, most of the directivity provided is in a plane at a right angle to the wires, though when out of phase, the directivity is in a line *through* the wires, and when in phase, the directivity is *broadside* to them. Thus, if the wires are oriented vertically, mostly horizontal directivity will be provided. If the wires are oriented horizontally, most of the directivity obtained will be *vertical* directivity.

To increase the sharpness of the directivity in all planes that include one of the wires, additional identical elements are added *in the line of the wires*, and fed so as to be *in phase*. The familiar H array is one array utilizing both types of directivity in the manner prescribed. The two-section Kraus flat-top beam is another.

These two antennas in their various forms are directional in a horizontal plane, in addition to being low-angle radiators, and are perhaps the most practicable of the *bidirectional* stacked-dipole arrays for amateur use. More phased elements can be used to provide greater directivity in planes including one of the radiating elements. The H then becomes a Sterba-curtain array.

For unidirectional work the most practicable stacked-dipole arrays for amateur-band use are parasitically-excited systems using relatively close spacing between the reflectors and the directors. Antennas of this type are described in detail in Chapter Twenty-two. The next most practicable unidirectional array is an H or a Sterba curtain with a similar system placed approximately one-quarter wave behind. The use of a reflector system in conjunction with any type of stacked-dipole broadside array will increase the gain by 3 db.

COLINEAR ANTENNA DESIGN CHART			
FREQUENCY IN MC.	L_1	L_2	L_3
14.4	33'4"	34'3"	17'1"
14.2	33'8"	34'7"	17'3"
14.0	34'1"	35'	17'6"
7.3	65'10"	67'6"	33'9"
7.15	67'	68'8"	34'4"
7.0	68'5"	70'2"	35'1"
4.0	120'	123'	61'6"
3.9	123'	126'	63'
3.6	133'	136'5"	68'2"

Colinear Arrays The simple colinear antenna array is a very effective radiating system for the 3.5-Mc. and 7.0-Mc. bands, but its use is not recommended on higher frequencies since such arrays do not possess any vertical directivity. The elevation radiation pattern for such an array is essentially the same as for a half-wave dipole. This consideration applies whether the elements are of normal length or are extended.

The colinear antenna consists of two or more radiating sections from 0.5 to 0.65 wavelengths long, with the current in phase in each section. The necessary phase reversal between sections is obtained through the use of resonant tuning stubs as illustrated in figure 11. The gain of a colinear array using half-wave elements (in decibels) is approximately equal to the number of elements in the array. The exact figures are as follows:

Number of Elements	2	3	4	5	6
Gain in Decibels	1.8	3.3	4.5	5.3	6.2

As additional in-phase colinear elements are added to a doublet, the radiation resistance goes up much faster than when additional half waves are added out of phase (harmonic operated antenna).

For a colinear array of from 2 to 6 elements, the terminal radiation resistance in ohms at any current loop is approximately 100 times the number of elements.

It should be borne in mind that the *gain* from a colinear antenna depends upon the *sharpness* of the horizontal directivity since no vertical directivity is provided. An array with several colinear elements will give considerable gain, but will have a sharp horizontal radiation pattern.

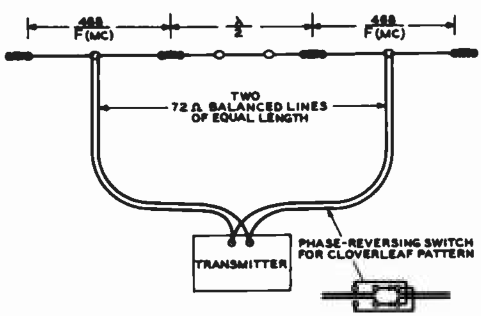


Figure 13

TWO COLINEAR HALF-WAVE ANTENNAS IN PHASE PRODUCE A 3 DB GAIN WHEN SEPARATED ONE-HALF WAVELENGTH

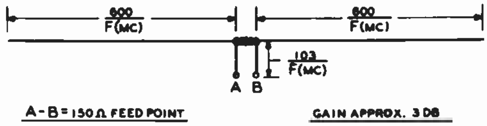


Figure 12

DOUBLE EXTENDED ZEPP ANTENNA

For best results, antenna should be tuned to operating frequency by means of grid-dip oscillator.

Double Extended Zepp The gain of a conventional two-element Franklin colinear antenna can be increased to a value approaching that obtained from a three-element Franklin, simply by making the two radiating elements 230° long instead of 180° long. The phasing stub is shortened correspondingly to maintain the whole array in resonance. Thus, instead of having 0.5-wavelength elements and 0.25-wavelength stub, the elements are made 0.64 wavelength long and the stub is approximately 0.11 wavelength long.

Dimensions for the double extended Zepp are given in figure 12.

The *vertical* directivity of a colinear antenna having 230° elements is the same as for one having 180° elements. There is little advantage in using extended sections when the total length of the array is to be greater than about 1.5 wavelength overall since the gain

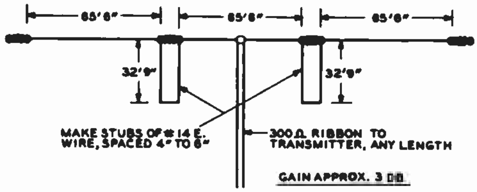


Figure 14

PRE-CUT LINEAR ARRAY FOR 40-METER OPERATION

of a colinear antenna is proportional to the overall length, whether the individual radiating elements are ¼ wave, ½ wave or ¾ wave in length.

Spaced Half Wave Antennas The gain of two colinear half waves may be increased by increasing the physical spacing between the elements, up to a maximum of about one half wavelength. If the half wave elements are fed with equal lengths of transmission line, poled correctly, a gain of about 3.3 db is produced. Such an antenna is shown in figure 13. By means of a phase reversing switch, the two elements may be operated out of phase, producing a cloverleaf pattern with slightly less maximum gain.

A three element "precut" array for 40 meter operation is shown in figure 14. It is fed directly with 300 ohm "ribbon line," and may be matched to a 52 ohm coaxial output transmitter by means of a Balun, such as the Barker & Williamson 3975. The antenna has a gain of about 3.2 db, and a beam width at half-power points of 40 degrees.

20-6 Broadside Arrays

Colinear elements may be stacked above or below another string of colinear elements to produce what is commonly called a *broadside* array. Such an array, when horizontal elements are used, possesses vertical directivity in proportion to the number of broadsided (vertically stacked) sections which have been used. Since broadside arrays do have good vertical directivity their use is recommended on the 14-Mc. band and on those higher in frequency. One of the most popular of simple broadside arrays is the "Lazy H" array of figure 15. Horizontal colinear elements stacked two above two make up this antenna system which is highly recommended for work on frequencies above perhaps 14-Mc. when moderate gain without too much directivity is desired. It has high radiation resistance and a gain of approximately 5.5 db. The high radiation resistance results in low voltages and a broad resonance curve, which permits use of inexpensive insulators and enables the array to be used over a fairly wide range in frequency. For dimensions, see the stacked dipole design table.

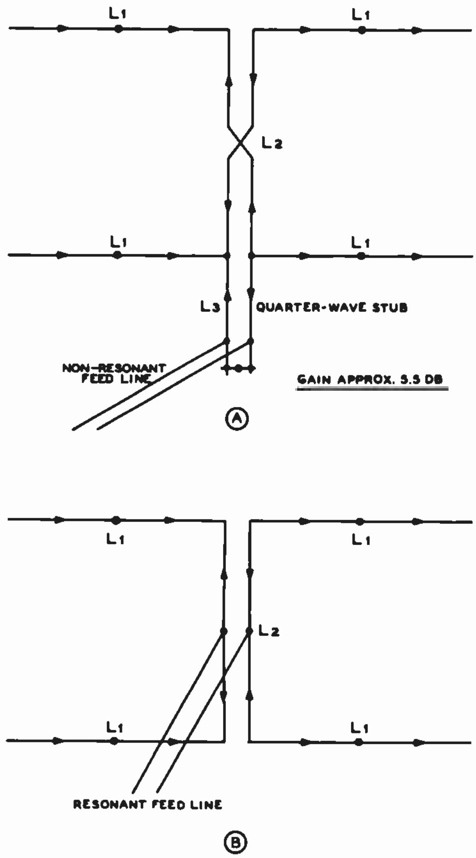


Figure 15
THE "LAZY H" ANTENNA SYSTEM

Stacking the colinear pairs gives both horizontal and vertical directivity. As shown, the array will give about 5.5 db gain. Note that the array may be fed either at the center of the phasing section or at the bottom; if fed at the bottom the phasing section must be twisted through 180°.

Stacked Dipoles Vertical stacking may be applied to strings of colinear elements longer than two half waves. In such arrays, the end quarter wave of each string of radiators usually is bent in to meet a similar bent quarter wave from the opposite end radiator. This provides better balance and better coupling between the upper and lower elements when the array is current-fed. Arrays of this type are shown in figure 16, and are commonly known as *curtain arrays*.

Correct length for the elements and stubs can be determined for any stacked dipole array from the *Stacked-Dipole Design Table*.

In the sketches of figure 16 the arrowheads represent the direction of current flow at any given instant. The dots on the radiators repre-

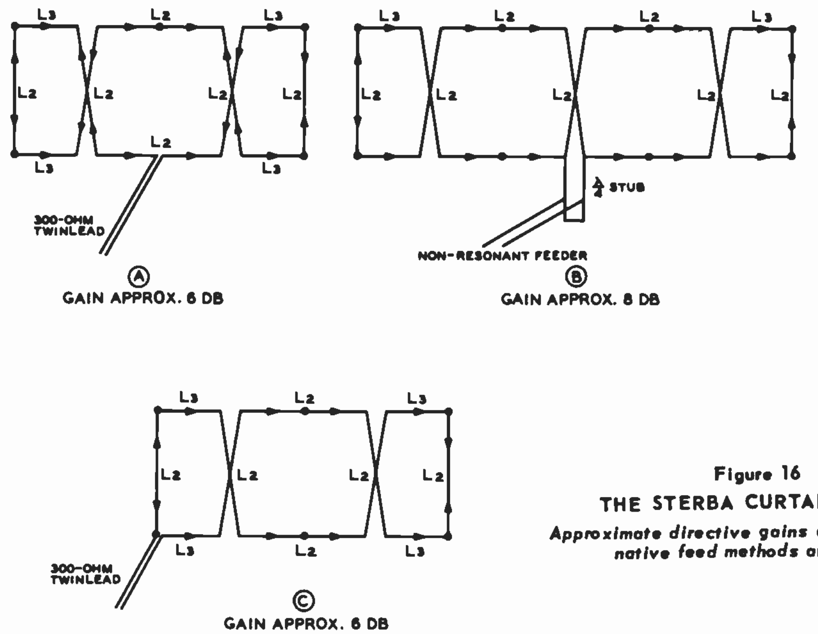


Figure 16
THE STERBA CURTAIN ARRAY
Approximate directive gains along with alternative feed methods are shown.

sent points of maximum current. All arrows should point in the same direction in each portion of the radiating sections of an antenna in order to provide a field in phase for broadside radiation. This condition is satisfied for the arrays illustrated in figure 16. Figures 16A and 16C show simple methods of feeding a short Sterba curtain, while an alternative method of feed is shown in the higher gain antenna of figure 16B.

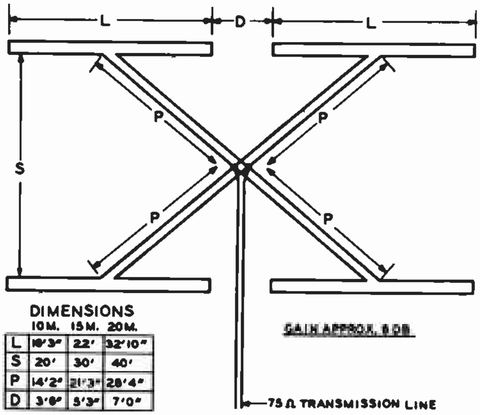
In the case of each of the arrays of figure 16, and also the "Lazy H" of figure 15, the array may be made unidirectional and the gain increased by 3 db if an exactly similar array is constructed and placed approximately ¼ wave behind the driven array. A screen or mesh of wires slightly greater in area than the antenna array may be used instead of an additional array as a reflector to obtain a unidirectional system. The spacing between the reflecting wires may vary from 0.05 to 0.1 wavelength with the spacing between the reflecting wires the smallest directly behind the driven elements. The wires in the untuned reflecting system should be parallel to the radiating elements of the array, and the spacing of the complete reflector system should be approximately 0.2 to 0.25 wavelength behind the driven elements.

On frequencies below perhaps 100 Mc. it normally will be impracticable to use a wire-screen reflector behind an antenna array such as a Sterba curtain or a "Lazy H." Parasitic elements may be used as reflectors or directors, but parasitic elements have the disadvantage that their operation is selective with respect to relatively small changes in frequency. Nevertheless, parasitic reflectors for such arrays are quite widely used.

The X-Array In section 20-5 it was shown how two dipoles may be arranged in phase to provide a power gain of (some) 3 db. If two such pairs of dipoles are stacked

LAZY-H AND STERBA
(STACKED DIPOLE) DESIGN TABLE

FREQUENCY IN MC.	L_1	L_2	L_3
7.0	68'2"	70'	35'
7.3	65'10"	67'6"	33'9"
14.0	34'1"	35'	17'6"
14.2	33'8"	34'7"	17'3"
14.4	33'4"	34'2"	17'
21.0	22'9"	23'3"	11'8"
21.5	22'3"	22'9"	11'5"
27.3	17'7"	17'10"	8'11"
28.0	17'	17'7"	8'9"
29.0	16'6"	17'	8'6"
50.0	9'7"	9'10"	4'11"
52.0	9'3"	9'5"	4'8"
54.0	8'10"	9'1"	4'6"
144.0	39.8"	40.5"	20.3"
146.0	39"	40"	20"
148.0	38.4"	39.5"	19.8"



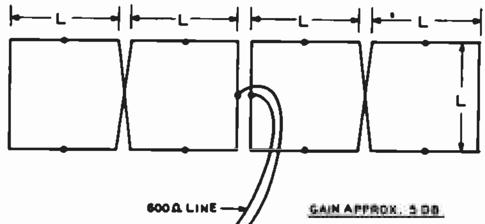
DIMENSIONS

	10M.	15M.	20M.
L	10'3"	22'	32'10"
S	20'	30'	40'
P	14'2"	21'3"	28'4"
D	3'6"	5'3"	7'0"

Figure 17

THE X-ARRAY FOR 28 MC., 21 MC., OR 14 MC.

The entire array (with the exception of the 75-ohm feed line) is constructed of 300-ohm ribbon line. Be sure phasing lines (P) are poled correctly, as shown.



DIMENSION L

10M.	15M.	20/10M.
8'9"	13'	17'6"

Figure 18

THE DOUBLE-BRUCE ARRAY FOR 10, 15, AND 20 METERS

If a 600-ohm feed line is used, the 20-meter array will also perform on 10 meters as a Sterba curtain, with an approximate gain of 9 db.

in a vertical plane and properly phased, a simplified form of in-phase curtain is formed, providing an overall gain of about 6 db. Such an array is shown in figure 17. In this X-array, the four dipoles are all in phase, and are fed by four sections of 300-ohm line, each one-half wavelength long, the free ends of all four lines being connected in parallel. The feed impedance at the junction of these four lines is about 75 ohms, and a length of 75-ohm Twin-Lead may be used for the feedline to the array.

An array of this type is quite small for the 28-Mc. band, and is not out of the question for the 21-Mc. band. For best results, the bottom section of the array should be one-half wavelength above ground.

The Double-Bruce Array The Bruce Beam consists of a long wire folded so that vertical elements carry in-phase currents while the horizontal elements carry out of phase currents. Radiation from the horizontal sections is low since only a small current flows in this part of the wire, and it is largely phased-out. Since the height of the Bruce Beam is only one-quarter wavelength, the gain per linear foot of array is quite low. Two Bruce Beams may be combined as shown in figure 18 to produce the *Double Bruce* array. A four section Double Bruce will give a vertically polarized emission, with a power gain of 5 db over a simple dipole, and is a very simple beam to construct. This antenna, like other so-called "broadside" arrays, radiates maximum power at right angles to the plane of the array.

The feed impedance of the Double Bruce is about 750 ohms. The array may be fed with a one-quarter wave stub made of 300-ohm ribbon line and a feedline made of 150-ohm ribbon line. Alternatively, the array may be fed directly with a wide-spaced 600-ohm transmission line (figure 18). The feedline should be brought away from the Double Bruce for a short distance before it drops downward, to prevent interaction between the feedline and the lower part of the center phasing section of the array. For best results, the bottom sections of the array should be one-half wavelength above ground.

Arrays such as the X-array and the Double Bruce are essentially high impedance devices, and exhibit relatively broad-band characteristics. They are less critical of adjustment than a parasitic array, and they work well over a wide frequency range such as is encountered on the 28-29.7 Mc. band.

The "Bi-Square" Broadside Array Illustrated in figure 19 is a simple method of feeding a small broadside array first described by W6BCX several years ago as a practical method of suspending an effective array from a single pole. As two arrays of this type can be supported at right angles from a single pole without interaction, it offers a solution to the problem of suspending two arrays in a restricted space with a minimum of erection work. The free space directivity gain is slightly less than that of a Lazy H, but is

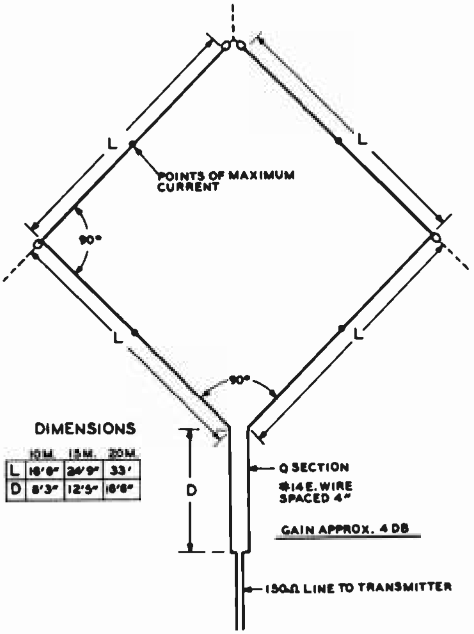


Figure 19

THE "BI-SQUARE" BROADSIDE ARRAY

This bidirectional array is related to the "Lazy H," and in spite of the oblique elements, is horizontally polarized. It has slightly less gain and directivity than the Lazy H, the free space directivity gain being approximately 4 db. Its chief advantage is the fact that only a single pole is required for support, and two such arrays may be supported from a single pole without interaction if the planes of the elements are at right angles. A 600-ohm line may be substituted for the Twin-Lead, and either operated as a resonant line, or made non-resonant by the incorporation of a matching stub.

still worthwhile, being approximately 4 db over a half-wave horizontal dipole at the same average elevation.

When two Bi-Square arrays are suspended at right angles to each other (for general coverage) from a single pole, the Q sections should be well separated or else symmetrically arranged in the form of a square (the diagonal conductors forming one Q section) in order to minimize coupling between them. The same applies to the line if open construction is used instead of Twin-Lead, but if Twin-Lead is used the coupling can be made negligible simply by separating the two Twin-Lead lines by at least two inches and twisting one Twin-Lead so as to effect a transposition every foot or so.

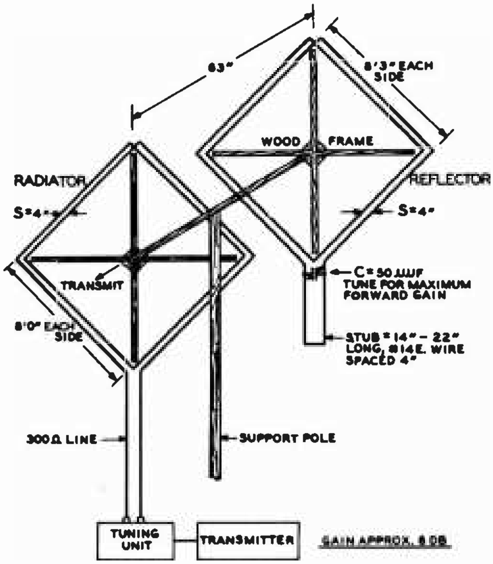


Figure 20

THE CUBICAL-QUAD ANTENNA FOR THE 10-METER BAND

When tuned feeders are employed, the Bi-Square array can be used on half frequency as an end-fire vertically polarized array, giving a slight practical dx signal gain over a vertical half-wave dipole at the same height.

A second Bi-Square serving as a reflector may be placed 0.15 wavelength behind this antenna to provide an overall gain of 8.5 db. The reflector may be tuned by means of a quarter-wave stub which has a moveable shorting bar at the bottom end. The stub is used as a substitute for the Q-section, since the reflector employs no feed line.

The "Cubical-Quad" Antenna A smaller version of the Bi-Square antenna is the Cubical-Quad antenna. Four half-waves of wire are folded into a square that is one-quarter wavelength on a side, as shown in figure 20. The array radiates a horizontally polarized signal. A reflector placed 0.15 wavelength behind the antenna provides an overall gain of some 8 db. A shorted stub with a paralleled tuning condenser is used to resonate the reflector.

The Cubical-Quad is fed with a 300-ohm line, and should employ some sort of antenna tuner at the transmitter end of the line if a pi-network type transmitter is used. There is a small standing wave on the line, and an open

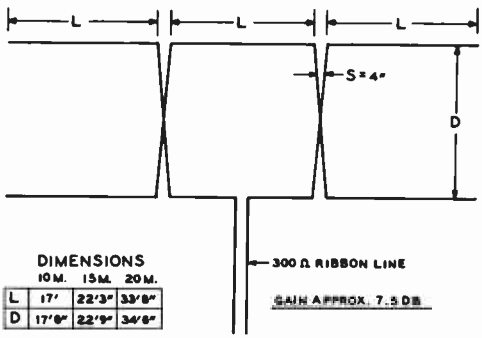


Figure 21

THE "SIX-SHOOTER" BROADSIDE ARRAY

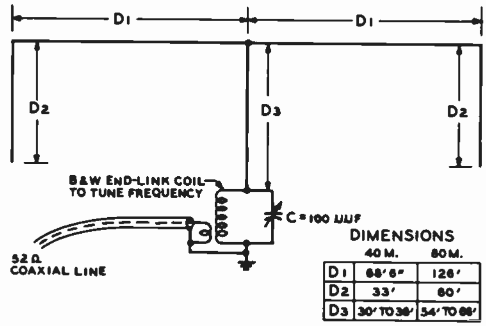


Figure 22

"BOBTAIL" BIDIRECTIONAL BROADSIDE CURTAIN FOR THE 7-MC. OR THE 4.0-MC. AMATEUR BANDS

This simple vertically polarized array provides low angle radiation and response with comparatively low pole heights, and is very effective for dx work on the 7-Mc. band or the 4.0-Mc. phone band. Because of the phase relationships, radiation from the horizontal portion of the antenna is effectively suppressed. Very little current flows in the ground lead to the coupling tank; so an elaborate ground system is not required, and the length of the ground lead is not critical so long as it uses heavy wire and is reasonably short.

wire line should be employed if the antenna is used with a high power transmitter.

To tune the reflector, the antenna is aimed at a nearby field-strength meter or receiver, and the stub condenser adjusted for maximum received signal.

This antenna provides high gain for its small size, and is recommended for 28-Mc. work. The elements may be made of number 14 enamel wire, and the array may be built on a light wood frame.

The "Six-Shooter" Broadside Array As a good compromise between gain, directivity, compactness, mechanical simplicity, ease of adjustment, and band width the array of figure 21 is recommended for the 10 to 30 Mc. range when the additional array width and greater directivity are not obtainable. The free space directivity gain is approximately 7.5 db over one element, and the practical dx signal gain over one element at the same average elevation is of about the same magnitude when the array is sufficiently elevated. To show up to best advantage the array should be elevated sufficiently to put the lower elements well in the clear, and preferably at least 0.5 wavelength above ground.

The "Bobtail" Bidirectional Broadside Curtain Another application of vertical orientation of the radiating elements of an array in order to obtain low-angle radiation at the lower end of the h-f range with low pole heights is illustrated in figure 22. When precut to the specified dimensions this single pattern array will perform well over the 7-Mc. amateur band or the 4-Mc. amateur phone band. For the 4-Mc. band the required two poles need be only 70 feet high, and the array will provide a practical signal gain averaging from 7 to 10 db over a horizontal half-wave dipole utilizing the same pole height when the path length exceeds 2500 miles.

The horizontal directivity is only moderate, the beam width at the half power points being slightly greater than that obtained from three cophased vertical radiators fed with equal currents. This is explained by the fact that the current in each of the two outer radiators of this array carries only about half as much current as the center, driven element. While this "binomial" current distribution suppresses the end-fire lobe that occurs when an odd number of parallel radiators with half-wave spacing are fed equal currents, the array still exhibits some high-angle radiation and response off the ends as a result of imperfect cancellation in the flat top portion. This is not sufficient to affect the power gain appreciably, but does degrade the discrimination somewhat.

A moderate amount of sag can be tolerated at the center of the flat top, where it connects to the driven vertical element. The poles and antenna tank should be so located with respect to each other that the driven vertical element drops approximately straight down from the flat top.

Normally the antenna tank will be located in the same room as the transmitter, to facilitate adjustment when changing frequency. In this case it is recommended that the link coupled tank be located across the room from the transmitter if much power is used, in order to minimize r-f feedback difficulties which might occur as a result of the asymmetrical high impedance feed. If tuning of the antenna tank from the transmitter position is desired, flexible shafting can be run from the antenna tank condenser to a control knob at the transmitter.

The lower end of the driven element is quite "hot" if much power is used, and the lead-in insulator should be chosen with this in mind. The ground connection need not have very low resistance, as the current flowing in the ground connection is comparatively small. A stake or pipe driven a few feet in the ground will suffice. However, the ground lead should be of heavy wire and preferably the length should not exceed about 10 feet at 7 Mc. or about 20 feet at 4 Mc. in order to minimize reactive effects due to its inductance. If it is impossible to obtain this short a ground lead, a piece of screen or metal sheet about four feet square may be placed parallel to the earth in a convenient location and used as an artificial ground. A fairly high C/L ratio ordinarily will be required in the antenna tank in order to obtain adequate coupling and loading.

20-7 End-Fire Directivity

By spacing two half-wave dipoles, or colinear arrays, at a distance of from 0.1 to 0.25 wavelength and driving the two 180° out of phase, directivity is obtained *through the two wires* at right angles to them. Hence, this type of bidirectional array is called *end fire.* A better idea of end-fire directivity can be obtained by referring to figure 10.

Remember that *end-fire* refers to the radiation with *respect to the two wires* in the array rather than with respect to the array as a whole.

The vertical directivity of an end-fire bidirectional array which is oriented horizontally can be increased by placing a similar end-fire array a half wave below it, and excited in the same phase. Such an array is a combination broadside and end-fire affair.

Kraus Flat-Top Beam A very effective bidirectional end-fire array is the Kraus or 8JK *Flat-Top Beam.* Essentially, this antenna consists of two close-spaced dipoles or colinear arrays. Because of the close spacing, it is possible to obtain the proper phase relationships in multi-section flat tops by crossing the wires at the voltage loops, rather than by resorting to phasing stubs. This greatly simplifies the array. (See figure 23.) Any number of sections may be used, though the one- and two-section arrangements are the most popular. Little extra gain is obtained by using more than four sections, and trouble from phase shift may appear.

A center-fed single-section flat-top beam cut according to the table, can be used quite successfully on its second harmonic, the pattern being similar except that it is a little sharper. The single-section array can also be used on its fourth harmonic with some success, though there then will be four cloverleaf lobes, much the same as with a full-wave antenna.

If a flat-top beam is to be used on more than one band, tuned feeders are necessary.

The radiation resistance of a flat-top beam is rather low, especially when only one section is used. This means that the voltage will be high at the voltage loops. For this reason, especially good insulators should be used for best results in wet weather.

The exact lengths for the radiating elements are not especially critical, because slight deviations from the correct lengths can be compensated in the stub or tuned feeders. Proper stub adjustment is covered in Chapter Twenty-two. Suitable radiator lengths and approximate stub dimensions are given in the accompanying design table.

Figure 23 shows *top views* of eight types of flat-top beam antennas. The dimensions for using these antennas on different bands are given in the design table. The 7- and 28-Mc. bands are divided into two parts, but the dimensions for either the low- or high-frequency ends of these bands will be satisfactory for use over the entire band.

In any case, the antennas are tuned to the frequency used, by adjusting the shorting wire on the stub, or tuning the feeders, if no stub is used. The data in the table may be extended to other bands or frequencies by applying the proper factor. Thus, for 50 to 52 Mc. operation, the values for 28 to 29 Mc. are divided by 1.8.

All of the antennas have a bidirectional horizontal pattern on their fundamental frequency. The maximum signal is broadside to the flat top. The single-section type has this pattern on both its fundamental frequency and second harmonic. The other types have four main lobes of radiation on the second and higher harmonics. The nominal gains of the different types over a half-wave comparison antenna are as follows: single-section, 4 db; two-section, 6 db; four-section, 8 db.

The maximum spacings given make the beams less critical in their adjustments. Up

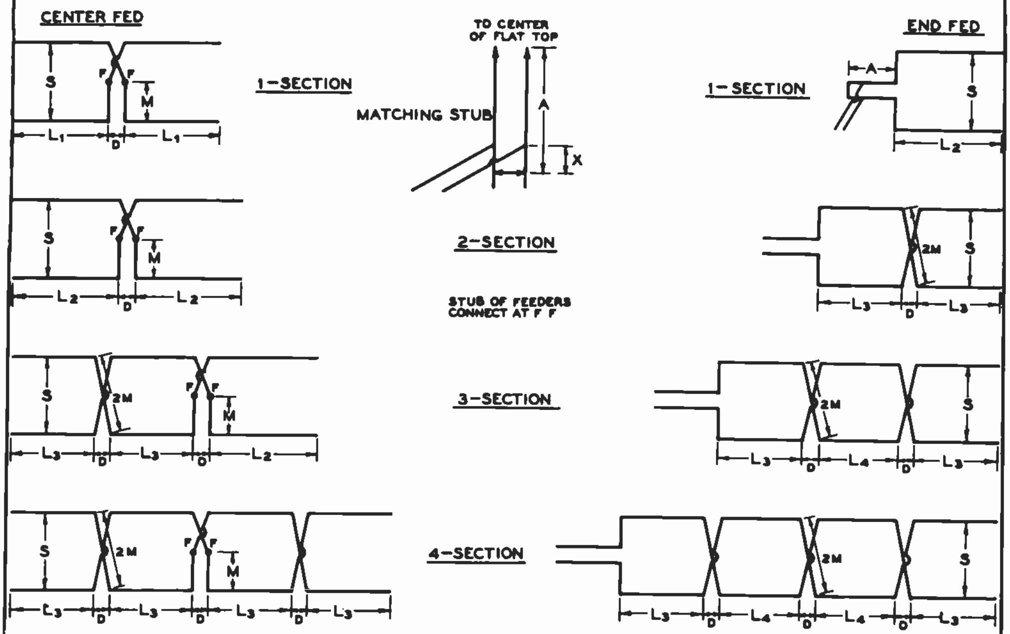


FIGURE 23

FLAT-TOP BEAM (8JK ARRAY) DESIGN DATA.

FREQUENCY	Spacing	S	L_1	L_2	L_3	L_4	M	D	A (¼) approx.	A (½) approx.	A (¾) approx.	X approx.
7.0-7.2 Mc.	λ/8	17'4"	34'	60'	52'8"	44'	8'10"	4'	26'	60'	96'	4'
7.2-7.3	λ/8	17'0"	33'6"	59'	51'8"	43'1"	8'8"	4'	26'	59'	94'	4'
14.0-14.4	λ/8	8'8"	17'	30'	26'4"	22'	4'5"	2'	13'	30'	48'	2'
14.0-14.4	.15λ	10'5"	17'	30'	25'3"	20'	5'4"	2'	12'	29'	47'	2'
14.0-14.4	.20λ	13'11"	17'	30'	22'10"	.....	7'2"	2'	10'	27'	45'	3'
14.0-14.4	λ/4	17'4"	17'	30'	20'8"	.....	8'10"	2'	8'	25'	43'	4'
28.0-29.0	.15λ	5'2"	8'6"	15'	12'7"	10'	2'8"	1'6"	7'	15'	24'	1'
28.0-29.0	λ/4	8'8"	8'6"	15'	10'4"	.....	4'5"	1'6"	5'	13'	22'	2'
29.0-30.0	.15λ	5'0"	8'3"	14'6"	12'2"	9'8"	2'7"	1'6"	7'	15'	23'	1'
29.0-30.0	λ/4	8'4"	8'3"	14'6"	10'0"	.....	4'4"	1'6"	5'	13'	21'	2'

Dimension chart for flat-top beam antennas. The meanings of the symbols are as follows:

L_1, L_2 L_3 and L_4, the lengths of the sides of the flat-top sections as shown. L_1 is length of the sides of single-section center-fed, L_2 single-section end-fed and 2-section center-fed, L_3 4-section center-fed and end-sections of 4-section end-fed, and L_4 middle sections of 4-section end-fed.

S, the spacing between the flat-top wires.

M, the wire length from the outside to the center of each cross-over.

D, the spacing lengthwise between sections.

A (¼), the approximate length for a quarter-wave stub.

A (½), the approximate length for a half-wave stub.

A (¾), the approximate length for a three-quarter wave stub.

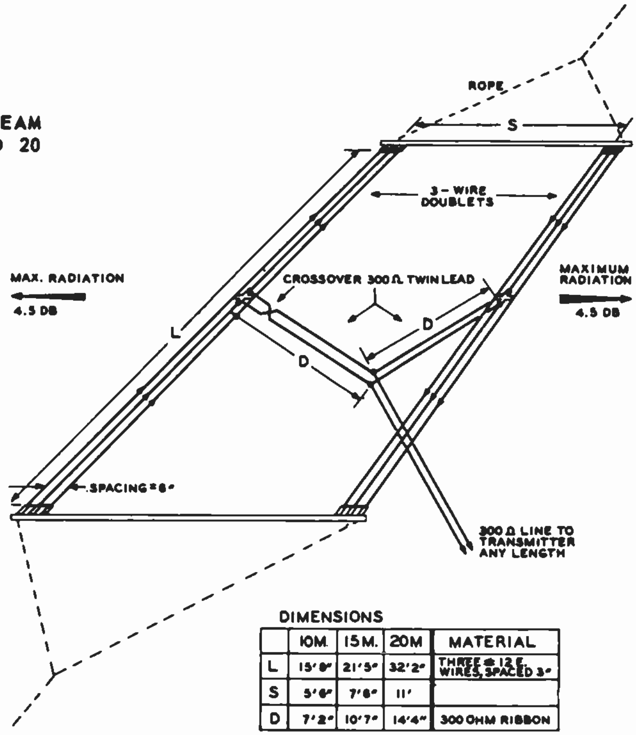
X, the approximate distance above the shorting wire of the stub for the connection of a 600-ohm line. This distance, as given in the table, is approximately correct only for 2-section flat-tops.

For single-section types it will be smaller and for 3- and 4-section types it will be larger.

The lengths given for a half-wave stub are applicable only to single-section center-fed flat-tops. To be certain of sufficient stub length, it is advisable to make the stub a foot or so longer than shown in the table, especially with the end-fed types. The lengths, A, are measured from the point where the stub connects to the flat-top.

Both the center and end-fed types may be used horizontally. However, where a vertical antenna is desired, the flat-tops can be turned on end. In this case, the end-fed types may be more convenient, feeding from the lower end.

Figure 24
THE TRIPLEX FLAT-TOP BEAM ANTENNA FOR 10, 15 AND 20 METERS



DIMENSIONS

	10M.	15M.	20M	MATERIAL
L	15'8"	21'5"	32'2"	THREE #12 E. WIRES, SPACED 3"
S	5'6"	7'8"	11'	
D	7'2"	10'7"	14'4"	300 OHM RIBBON

to one-quarter wave spacing may be used on the fundamental for the one-section types and also the two-section center-fed, but it is not desirable to use more than 0.15 wavelength spacing for the other types.

Although the center-fed type of flat-top generally is to be preferred because of its symmetry, the end-fed type often is convenient or desirable. For example, when a flat-top beam is used vertically, feeding from the lower end is in most cases more convenient.

If a multisection flat-top array is end-fed instead of center-fed, and tuned feeders are used, stations off the ends of the array can be worked by tying the feeders together and working the whole affair, feeders and all, as a long-wire harmonic antenna. A single-pole double-throw switch can be used for changing the feeders and directivity.

The Triplex Beam The Triplex beam is a modified version of the W8JK antenna which uses folded dipoles for the half wave elements of the array. The use of folded dipoles results in higher radiation resistance of the array, and a high overall system performance. Three wire dipoles are used for the elements, and 300-ohm Twin-Lead is used for the two phasing sections. A recommended assembly for Triplex beams for 28 Mc., 21 Mc., and 14 Mc. is shown in figure 24. The gain of a Triplex beam is about 4.5 db over a dipole.

20-8 Combination End-Fire and Broadside Arrays

Any of the end-fire arrays previously described may be stacked one above the other or placed end to end (side by side) to give greater directivity gain while maintaining a bidirectional characteristic. However, it must be kept in mind that to realize a worthwhile increase in directivity and gain while maintaining a bidirectional pattern the individual arrays must be spaced sufficiently to reduce the mutual impedances to a negligible value.

When two flat top beams, for instance, are placed one above the other or end to end, a center spacing on the order of one wavelength is required in order to achieve a worthwhile increase in gain, or approximately 3 db.

Thus it is seen that, while maximum gain occurs with two stacked dipoles at a spacing of about 0.7 wavelength and the space directivity gain is approximately 5 db over one element under these conditions; the case of two flat top or parasitic arrays stacked one above the other is another story. Maximum gain will occur at a greater spacing, and the gain over one array will not appreciably exceed 3 db.

When two broadside curtains are placed one ahead of the other in end-fire relationship, the aggregate mutual impedance between the two curtains is such that considerable spacing is required in order to realize a gain approaching 3 db (the required spacing being a function of the size of the curtains). While it is true that a space directivity gain of approximately 4 db can be obtained by placing one, half-wave dipole an eighth wavelength ahead of another and feeding them 180 degrees out of phase, a gain of less than 1 db is obtained when the same procedure is applied to two large broadside curtains. To obtain a gain of approximately 3 db and retain a bidirectional pattern, a spacing of many wavelengths is required between two large curtains placed one ahead of the other.

A different situation exists, however, when one driven curtain is placed ahead of an identical one and the two are phased so as to give a unidirectional pattern. When a unidirectional pattern is obtained, the gain over one curtain will be approximately 3 db regardless of the spacing. For instance, two large curtains placed one a quarter wavelength ahead of the other may have a space directivity gain of only 0.5 db over one curtain when the two are driven 180 degrees out of phase to give a bidirectional pattern (the type of pattern obtained with a single curtain). However, if they are driven in phase quadrature (and with equal currents) the gain is approximately 3 db.

The directivity gain of a composite array also can be explained upon the basis of the directivity patterns of the component arrays alone, but it entails a rather complicated picture. It is sufficient for the purpose of this discussion to generalize and simplify by saying that the greater the directivity of an end-fire array, the farther an identical array must be spaced from it in broadside relationship to obtain optimum performance; and the greater the directivity of a broadside array, the farther an identical array must be spaced from it in end-fire relationship to obtain optimum performance and retain the bidirectional characteristic.

It is important to note that while a bidirectional end-fire pattern is obtained with two driven dipoles when spaced anything under a half wavelength, and while the proper phase relationship is 180 degrees regardless of the spacing for all spacings not exceeding one half wavelength, the situation is different in the case of two curtains placed in end-fire relationship to give a bidirectional pattern. For maximum gain at zero wave angle, the curtains should be spaced an odd multiple of one half wavelength and driven so as to be 180 degrees out of phase, or spaced an even multiple of one half wavelength and driven in the same phase. The optimum spacing and phase relationship will depend upon the directivity pattern of the individual curtains used alone, and as previously noted the optimum spacing increases with the size and directivity of the component arrays.

A concrete example of a combination broadside and end-fire array is two Lazy H arrays spaced along the direction of maximum radiation by a distance of four wavelengths and fed in phase. The space directivity gain of such an arrangement is slightly less than 9 db. However, approximately the same gain can be obtained by juxtaposing the two arrays side by side or one over the other in the same plane, so that the two combine to produce, in effect, one broadside curtain of twice the area. It is obvious that in most cases it will be more expedient to increase the area of a broadside array than to resort to a combination of end-fire and broadside directivity. One exception, of course, is where two curtains are fed in phase quadrature to obtain a unidirectional pattern and space directivity gain of approximately 3 db with a spacing between curtains as small as one quarter wavelength. Another exception is where very low angle radiation is desired and the maximum pole height is strictly limited. The two aforementioned Lazy H arrays when placed in end-fire relationship will have a considerably lower radiation angle than when placed side by side if the array elevation is low, and therefore may *under some conditions* exhibit appreciably more practical signal gain.

CHAPTER TWENTY ONE

V-H-F and U-H-F Antennas

The *very-high-frequency* or *v-h-f* frequency range is defined as that range falling between 30 and 300 Mc. The *ultra-high-frequency* or *u-h-f* range is defined as falling between 300 and 3000 Mc. This chapter will be devoted to the design and construction of antenna systems for operation on the amateur 50-Mc., 144-Mc., 235-Mc., and 420-Mc. bands. Although the basic principles of antenna operation are the same for all frequencies, the shorter physical length of a wave in this frequency range and the differing modes of signal propagation make it possible and expedient to use antenna systems different in design from those used on the range from 3 to 30 Mc.

21-1 Antenna Requirements

Any type of antenna system useable on the lower frequencies *may* be used in the v-h-f and u-h-f bands. In fact, simple non-directive half-wave or quarter-wave vertical antennas are very popular for general transmission and reception from all directions, especially for short-range work. But for serious v-h-f or u-h-f work the use of some sort of directional antenna array is a necessity. In the first place, when the transmitter power is concentrated into a narrow beam the apparent transmitter power at the receiving station is increased many times. A "billboard" array or a Sterba curtain having a gain of 16 db will make a 25-watt transmitter sound like a kilowatt at the other station. Even a much simpler and smaller three- or four-element parasitic array having a gain of 7 to 10 db will produce a marked improvement in the received signal at the other station.

However, as all v-h-f and u-h-f workers know, the most important contribution of a high-gain antenna array is in reception. If a remote station cannot be heard it obviously is impossible to make contact. The limiting factor in v-h-f and u-h-f reception is in almost every case the noise generated within the receiver itself. Atmospheric noise is almost nonexistent and ignition interference can almost invariably be reduced to a satisfactory level through the use of an effective noise limiter. Even with a grounded-grid or neutralized triode first stage in the receiver the noise contribution of the first tuned circuit in the receiver will be relatively large. Hence it is desirable to use an antenna system which will deliver the greatest signal voltage to the first tuned circuit for a given field strength at the receiving location.

Since the field intensity being produced at the receiving location by a remote transmitting station may be assumed to be constant, the receiving antenna which intercepts the greatest amount of wave front, assuming that the polarization and directivity of the receiving antenna is proper, will be the antenna which gives the best received signal-to-noise ratio. An antenna which has two square wavelengths effective area will pick up twice as much signal power as one which has one square wavelength area, assuming the same general type of antenna and that both are directed at the station being received. Many instances have been reported where a frequency band sounded completely dead with a simple dipole receiving antenna but when the receiver was switched to a three-element or larger array a considerable amount of activity from 80 to 160 miles distant was heard.

Angle of Radiation The useful portion of the signal in the v-h-f and u-h-f range for short or medium distance communication is that which is radiated at a very low angle with respect to the surface of the earth; essentially it is that signal which is radiated parallel to the surface of the earth. A vertical antenna transmits a portion of its radiation at a very low angle and is effective for this reason; its radiation is not necessarily effective simply because it is vertically polarized. A simple horizontal dipole radiates very little low-angle energy and hence is not a satisfactory v-h-f or u-h-f radiator. Directive arrays which concentrate a major portion of the radiated signal at a low radiation angle will prove to be effective radiators whether their signal is horizontally or vertically polarized.

In all cases, the radiating system for v-h-f and u-h-f work should be as high and in the clear as possible. Increasing the height of the antenna system will produce a very marked improvement in the number and strength of the signals heard, regardless of the actual type of antenna used.

Transmission Lines Transmission lines to v-h-f and u-h-f antenna systems may be either of the parallel-conductor or coaxial conductor type. Coaxial line is recommended for short runs and closely spaced open-wire line for longer runs. Wave guides may be used under certain conditions for frequencies greater than perhaps 1500 Mc. but their dimensions become excessively great for frequencies much below this value. Non-resonant transmission lines will be found to be considerably more efficient on these frequencies than those of the resonant type. It is wise to to use the very minimum length of transmission line possible since transmission line losses at frequencies above about 100 Mc. mount very rapidly.

Open lines should preferably be spaced closer than is common for longer wavelengths, as 6 inches is an appreciable fraction of a wavelength at 2 meters. Radiation from the line will be greatly reduced if 1-inch or 1½-inch spacing is used, rather than the more common 6-inch spacing.

Ordinary TV-type 300-ohm ribbon may be used on the 2-meter band for feeder lengths of about 50 feet or less. For longer runs, either the u-h-f or v-h-f TV open-wire lines may be used with good overall efficiency. The v-h-f line is satisfactory for use on the amateur 420-Mc. band.

Antenna Changeover It is recommended that the same antenna be used for transmitting and receiving in the v-h-f and u-h-f range. An ever-present problem in this connection, however, is the antenna changeover relay. Reflections at the antenna changeover relay become of increasing importance as the frequency of transmission is increased. When coaxial cable is used as the antenna transmission line, satisfactory coaxial antenna changeover relays with low reflection can be used. One type manufactured by *Advance Electric & Relay Co.*, Los Angeles 26, Calif., will give a satisfactorily low value of reflection.

On the 235-Mc. and 420-Mc. amateur bands, the size of the antenna array becomes quite small, and it is practical to mount two identical antennas side by side. One of these antennas is used for the transmitter, and the other antenna for the receiver. Separate transmission lines are used, and the antenna relay may be eliminated.

Effect of Feed System on Radiation Angle A vertical radiator for general coverage u-h-f use should be made either ¼ or ½ wavelength long. Longer vertical antennas do not have their maximum radiation at right angles to the line of the radiator (unless co-phased), and, therefore, are not practicable for use where greatest possible radiation parallel to the earth is desired.

Unfortunately, a feed system which is not perfectly balanced and does some radiating, not only robs the antenna itself of that much power, but *distorts the radiation pattern of the antenna.* As a result, the pattern of a vertical radiator may be so altered that the radiation is bent upwards slightly, and the amount of power leaving the antenna parallel to the earth is greatly reduced. A vertical half-wave radiator fed at the bottom by a quarter-wave stub is a good example of this; the slight radiation from the matching section decreases the power radiated parallel to the earth by nearly 10 db.

The only cure is a feed system which does not disturb the radiation pattern of the antenna itself. This means that if a 2-wire line is used, the current and voltages must be exactly the same (though 180° out of phase) at any point on the feed line. It means that if a concentric feed line is used, there should be no current flowing on the outside of the outer conductor.

Radiator Cross Section There is no point in using copper tubing for an antenna on the medium frequencies. The reason is that considerable tubing would be required, and the cross section still would not be a sufficiently large fraction of a wavelength to improve the antenna bandwidth characteristics. At very high and ultra high frequencies, however, the radiator length is so short that the expense of large diameter conductor is relatively small, even though copper pipe of 1 inch cross section is used. With such conductors, the antenna will tune much more broadly, and often a broad resonance characteristic is desirable. This is particularly true when an antenna or array is to be used over an entire amateur band.

It should be kept in mind that with such large cross section radiators, the resonant length of the radiator will be somewhat shorter, being only slightly greater than 0.90 of a half wavelength for a dipole when heavy copper pipe is used above 100 Mc.

Insulation The matter of insulation is of prime importance at very high frequencies. Many insulators that have very low losses as high as 30 Mc. show up rather poorly at frequencies above 100 Mc. Even the low loss ceramics are none too good where the r-f voltage is high. One of the best and most practical insulators for use at this frequency is polystyrene. It has one disadvantage, however, in that it is subject to fracture and to deformation in the presence of heat.

It is common practice to design v-h-f and u-h-f antenna systems so that the various radiators are supported only at points of relatively low voltage; the best insulation, obviously, is air. The voltages on properly operated untuned feed lines are not high, and the question of insulation is not quite so important, though insulation still should be of good grade.

TABLE OF WAVELENGTHS

Frequency in Mc.	1/4 Wave Free Space	1/4 Wave Antenna	1/2 Wave Free Space	1/2 Wave Antenna
50.0	59.1	55.5	118.1	111.0
50.5	58.5	55.0	116.9	109.9
51.0	57.9	54.4	115.9	108.8
51.5	57.4	53.9	114.7	107.8
52.0	56.8	53.4	113.5	106.7
52.5	56.3	52.8	112.5	105.7
53.0	55.7	52.4	111.5	104.7
54.0	54.7	51.4	109.5	102.8
144	20.5	19.2	41.0	38.5
145	20.4	19.1	40.8	38.3
146	20.2	18.9	40.4	38.0
147	20.0	18.8	40.0	37.6
148	19.9	18.6	39.9	37.2
235	12.6	11.8	25.2	23.6
236	12.5	11.8	25.1	23.5
237	12.5	11.7	25.0	23.5
238	12.4	11.7	24.9	23.4
239	12.4	11.6	24.8	23.3
240	12.3	11.6	24.6	23.2
420	7.05	6.63	14.1	13.25
425	6.95	6.55	13.9	13.1
430	6.88	6.48	13.8	12.95

All dimensions are in inches. Lengths have in most cases been rounded off to three significant figures. "1/2-Wave Free-Space" column shown above should be used with Lecher wires for frequency measurement.

Antenna Polarization Commercial broadcasting in the U.S.A. for both FM and television in the v-h-f range has been standarized on horizontal polarization. One of the main reasons for this standardization is the fact that ignition interference is reduced through the use of a horizontally polarized receiving antenna. Amateur practice, however, is divided between horizontal and vertical polarization in the v-h-f and u-h-f range. Mobile stations are invariably vertically polarized due to the physical limitations imposed by the automobile antenna installation. Most of the stations doing intermittent or occasional work on these frequencies use a simple ground-plane vertical antenna for both transmission and reception. However, those stations doing serious work and striving for maximum-range contacts on the 50-Mc. and 144-Mc. bands almost invariably use horizontal polarization.

Experience has shown that there is a great attenuation in signal strength when using crossed polarization (transmitting antenna with one polarization and receiving antenna with the other) for all normal ground-wave contacts on these bands. When contacts are being made through sporadic-*E* reflection, however, the use of crossed polarization seems to make no discernible difference in signal strength. So the operator of a station doing v-h-f work (particularly on the 50-Mc. band) is faced with a problem: If contacts are to be made with all stations doing work on the same band, provision must be made for operation on both horizontal and vertical polarization. This problem has been solved in many cases through the construction of an antenna array that may be revolved in the plane of polarization in addition to being capable of rotation in the azimuth plane.

An alternate solution to the problem which involves less mechanical construction is simply to install a good ground-plane vertical antenna for all vertically-polarized work, and then to use a multi-element horizontally-polarized array for dx work.

21-2 Simple Horizontally-Polarized Antennas

Antenna systems which do not concentrate

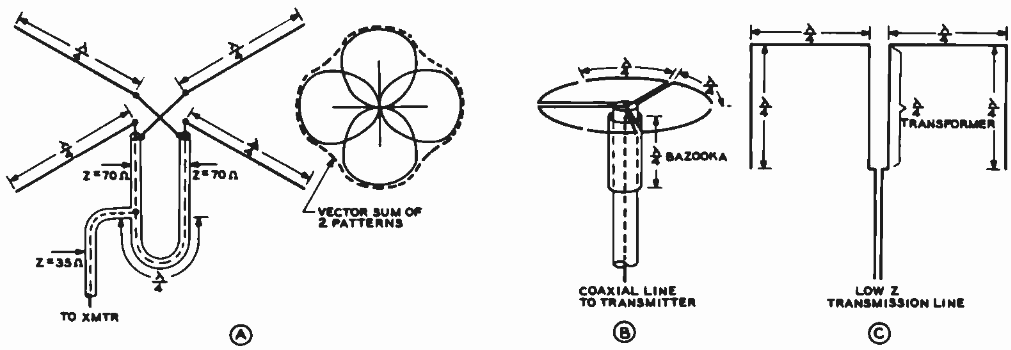


Figure 1
THREE NONDIRECTIONAL, HORIZONTALLY POLARIZED ANTENNAS

radiation at the very low elevation angles are not recommended for v-h-f and u-h-f work. It is for this reason that the horizontal dipole and horizontally-disposed colinear arrays are generally unsuitable for work on these frequencies. Arrays using broadside or end-fire elements do concentrate radiation at low elevation angles and are recommended for v-h-f work. Arrays such as the lazy-H, Sterba curtain, flat-top beam, and arrays with parasitically excited elements are recommended for this work. Dimensions for the first three types of arrays may be determined from the data given in the previous chapter, and reference may be made to the *Table of Wavelengths* given in this chapter.

Arrays using vertically-stacked horizontal dipoles, such as are used by commercial television and FM stations, are capable of giving high gain *without* a sharp horizontal radiation pattern. If sets of crossed dipoles, as shown in figure 1A, are fed 90° out of phase the resulting system is called a *turnstile* antenna. The 90° phase difference between sets of dipoles may be obtained by feeding one set of dipoles with a feed line which is one-quarter wave longer than the feed line to the other set of dipoles. The field strength broadside to one of the dipoles is equal to the field from that dipole alone. The field strength at a point at any other angle is equal to the vector sum of the fields from the two dipoles at that angle. A nearly circular horizontal pattern is produced by this antenna.

A second antenna producing a uniform, horizontally polarized pattern is shown in figure 1B. This antenna employs three dipoles bent to form a circle. All dipoles are excited in phase, and are center fed. A bazooka is included in the system to prevent unbalance in the coaxial feed system.

A third nondirectional antenna is shown in figure 1C. This simple antenna is made of two half-wave elements, of which the end quarter-wavelength of each is bent back 90 degrees. The pattern from this antenna is very much like that of the turnstile antenna. The field from the two quarter-wave sections that are bent back are additive because they are 180 degrees out of phase and are a half wavelength apart. The advantage of this antenna is the simplicity of its feed system and construction.

21-3 Simple Vertical-Polarized Antennas

For general coverage with a single antenna, a single vertical radiator is commonly employed. A two-wire open transmission line is not suitable for use with this type antenna, and coaxial polyethylene feed line such as RG-8/U is to be recommended. Three practical methods of feeding the radiator with concentric line, with a minimum of current induced in the outside of the line, are shown in figure 2. Antenna (A) is known as the *sleeve antenna*, the lower half of the radiator being a large piece of pipe up through which the concentric feed line is run. At (B) is shown the ground-plane vertical, and at (C) a modification of this latter antenna.

The radiation resistance of the ground-plane vertical is approximately 30 ohms, which is not a standard impedance for coaxial line. To obtain a good match, the first quarter wavelength of feeder may be of 52 ohms surge impedance, and the remainder of the line of approximately 75 ohms impedance. Thus, the first quarter-wave section of line is used as a

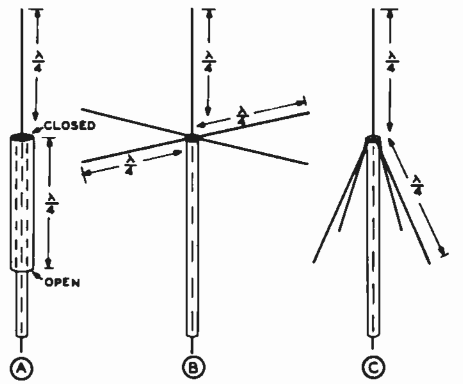


Figure 2
THREE VERTICALLY-POLARIZED LOW-ANGLE RADIATORS

Shown at (A) is the "sleeve" or "hypodermic" type of radiator. At (B) is shown the ground-plane vertical, and (C) shows a modification of this antenna system which increases the feed-point impedance to a value such that the system may be fed directly from a coaxial line with no standing waves on the feed line.

matching transformer, and a good match is obtained.

In actual practice the antenna would consist of a quarter-wave rod, mounted by means of insulators atop a pole or pipe mast. Elaborate insulation is not required, as the voltage at the lower end of the quarter-wave radiator is very low. Self-supporting rods from 0.25 to 0.28 wavelength would be extended out, as in the illustration, and connected together. As the point of connection is effectively at ground potential, no insulation is required; the horizontal rods may be bolted directly to the supporting pole or mast, even if of metal. The coaxial line should be of the low loss type especially designed for v-h-f use. The outside connects to the junction of the radials, and the inside to the bottom end of the vertical radiator. An antenna of this type is moderately simple to construct and will give a good account of itself when fed at the lower end of the radiator directly by the 52-ohm RG-8/U coaxial cable. Theoretically the standing-wave ratio will be approximately 1.5-to-1 but in practice this moderate s-w-r produces no deleterious effects, even on coaxial cable.

The modification shown in figure 2C permits matching to a standard 50- or 70-ohm flexible coaxial cable without a linear transformer. If the lower rods hug the line and supporting mast rather closely, the feed-point impedance is about 70 ohms. If they are bent out to form an angle of about 30° with the support pipe the impedance is about 50 ohms.

The number of radial legs used in a ground-plane antenna of either type has an important effect on the feed-point impedance and upon the radiation characteristics of the antenna system. Experiment has shown that three radials is the minimum number that should be used, and that increasing the number of radials above six adds substantially nothing to the effectiveness of the antenna and has no effect on the feed-point impedance. Experiment has shown, however, that the radials should be slightly longer than one-quarter wave for best results. A length of 0.28 wavelength has been shown to be the optimum value. This means that the radials for a 50-Mc. ground-plane vertical antenna should be 65" in length.

Double Skeleton Cone Antenna The bandwidth of the antenna of figure 2C can be increased considerably by substituting several space-tapered rods for the single radiating element, so that the "radiator" and skirt are similar. If a sufficient number of rods are used in the skeleton cones and the angle of revolution is optimized for the particular type of feed line used, this antenna exhibits a very low SWR over a 2 to 1 frequency range. Such an arrangement is illustrated schematically in figure 3.

A Nondirectional Vertical Array Half-wave elements may be stacked in the vertical plane to provide a non-directional pattern with good horizontal gain. An array made up of four half-wave vertical elements is shown in figure 4A. This antenna provides a circular pattern with a gain of about 4.5 db over a vertical dipole. It may be fed with 300-ohm TV-type line. The feedline should be conducted in such a way that the vertical portion of the line is at least one-half wavelength away from the vertical antenna elements. A suitable mechanical assembly is shown in figure 4B for the 144-Mc. and 235-Mc. amateur bands.

21-4 The Discone Antenna

The Discone antenna is a vertically polarized omnidirectional radiator which has very broad band characteristics and permits a simple, rugged structure. This antenna presents a substantially uniform feed-point impedance, suitable for direct connection of a coaxial line, over a range of several octaves. Also, the vertical pattern is suitable for ground-wave

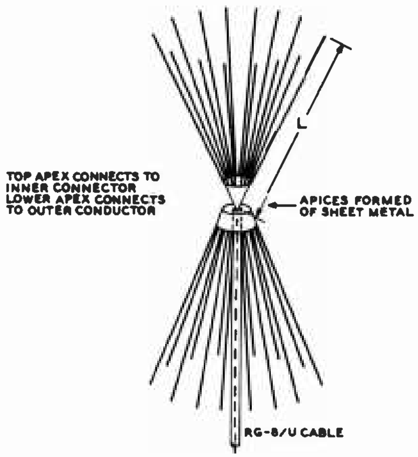


Figure 3

THE DOUBLE SKELETON CONE ANTENNA

A skeleton cone has been substituted for the single element radiator of figure 2C. This greatly increases the bandwidth. If at least 10 elements are used for each skeleton cone and the angle of revolution and element length are optimized, a low SWR can be obtained over a frequency range of at least two octaves. To obtain this order of bandwidth, the element length L should be approximately 0.2 wavelength at the lower frequency end of the band, and the angle of revolution optimized for the lowest maximum VSWR within the frequency range to be covered. A greater improvement in the impedance-frequency characteristic can be achieved by adding elements than by increasing the diameter of the elements. With only 3 elements per "cone" and a much smaller angle of revolution a low SWR can be obtained over a frequency range of approximately 1.3 to 1.0 when the element lengths are optimized.

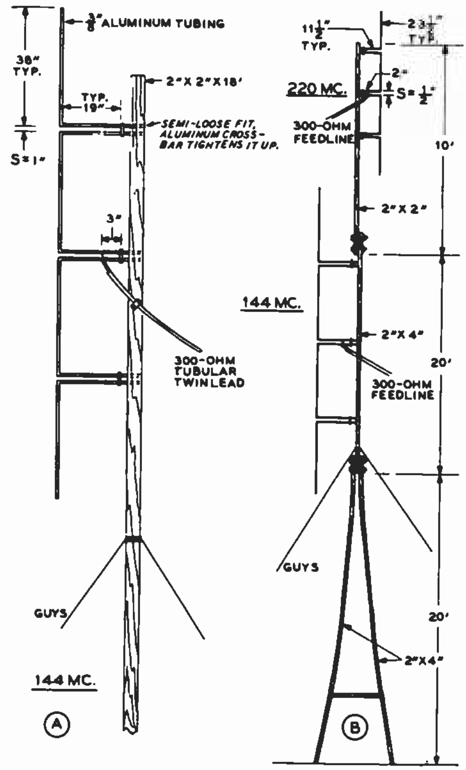


Figure 4

NONDIRECTIONAL ARRAYS FOR 144 MC. AND 235 MC.

On right is shown two band installation. The whole system may easily be dissembled and carried on a ski-rack atop a car for portable use.

work over several octaves, the gain varying only slightly over a very wide frequency range.

Commercial versions of the Discone antenna for various applications are manufactured by the *Federal Telephone and Radio Corporation*. A Discone type antenna for amateur work can be fabricated from inexpensive materials with ordinary hand tools.

A Discone antenna suitable for multi-band amateur work in the v-h/u-h-f range is shown schematically in figure 5A. The distance D should be made approximately equal to a free-space quarter wavelength at the lowest operating frequency. The antenna then will perform well over a frequency range of at least 8 to 1. At certain frequencies within this range the vertical pattern will tend to "lift" slightly, causing a slight reduction in gain at zero angular elevation, but the reduction is very slight.

Below the frequency at which the slant height of the conical skirt is equal to a free-space quarter wavelength the standing-wave ratio starts to climb, and below a frequency approximately 20 per cent lower than this the standing-wave ratio climbs very rapidly. This is termed the *cut off frequency* of the antenna. By making the slant height approximately equal to a free-space quarter wavelength at the lowest frequency employed (refer to chart), a

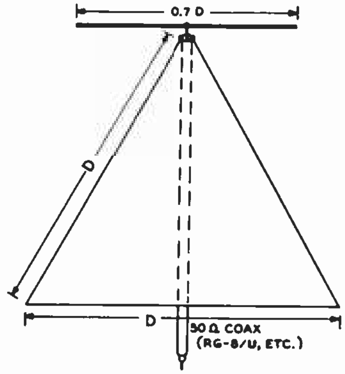


Figure 5A
THE "DISCONE" BROAD-BAND RADIATOR

This antenna system radiates a vertically polarized wave over a very wide frequency range. The "disc" may be made of solid metal sheet, a group of radials, or wire screen; the "cone" may best be constructed by forming a sheet of thin aluminum. A single antenna may be used for operation on the 50, 144, and 220 Mc. amateur bands. The dimension D is determined by the lowest frequency to be employed, and is given in the chart of figure 5B.

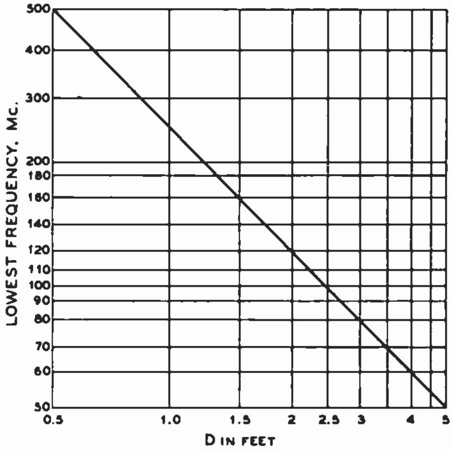


Figure 5B
DESIGN CHART FOR THE "DISCONE" ANTENNA

VSWR of less than 1.5 will be obtained throughout the operating range of the antenna.

The Discone antenna may be considered as a cross between an electromagnetic horn and an inverted ground plane unipole antenna. It looks to the feed line like a properly terminated high-pass filter.

Construction Details The top disk and the conical skirt may be fabricated either from sheet metal, screen (such as "hardware cloth"), or 12 or more "spine" radials. If screen is used a supporting framework of rod or tubing will be necessary for mechanical strength except at the higher frequencies. If spines are used, they should be terminated on a stiff ring for mechanical strength except at the higher frequencies.

The top disk is supported by means of three insulating pillars fastened to the skirt. Either polystyrene or low-loss ceramic is suitable for the purpose. The apex of the conical skirt is grounded to the supporting mast and to the outer conductor of the coaxial line. The line is run down through the supporting mast. An alternative arrangement, one suitable for certain mobile applications, is to fasten the base of the skirt directly to an effective ground plane such as the top of an automobile.

21-5 Helical Beam Antennas

Most v-h-f and u-h-f antennas are either vertically polarized or horizontally polarized (plane polarization). However, *circularly* polarized antennas have interesting characteristics which may be useful for certain applications. The installation of such an antenna can effectively solve the problem of horizontal vs. vertical polarization.

A circularly polarized wave has its energy divided equally between a vertically polarized component and a horizontally polarized component, the two being 90 degrees out of phase. The circularly polarized wave may be either "left handed" or "right handed," depending upon whether the vertically polarized component leads or lags the horizontal component.

A circularly polarized antenna will respond to any plane polarized wave whether horizontally polarized, vertically polarized, or diagonally polarized. Also, a circular polarized wave can be received on a plane polarized antenna, regardless of the polarization of the latter. When using circularly polarized antennas at *both* ends of the circuit, however, both must be left handed or both must be right handed. This offers some interesting possibilities with regard to reduction of QRM. At

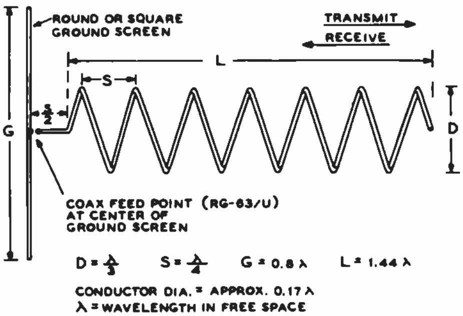


Figure 6

THE "HELICAL BEAM" ANTENNA

This type of directional antenna system gives excellent performance over a frequency range of 1.7 to 1.8 to 1. Its dimensions are such that it ordinarily is not practicable, however, for use as a rotatable array on frequencies below about 100 Mc. The center conductor of the feed line should pass through the ground screen for connection to the feed point. The outer conductor of the coaxial line should be grounded to the ground screen.

the time of writing, there has been no standardization of the "twist" for general amateur work.

Perhaps the simplest antenna configuration for a directional beam antenna having circular polarization is the helical beam popularized by Dr. John Kraus, W8JK. The antenna consists simply of a helix working against a ground plane and fed with coaxial line. In the u-h-f and the upper v-h-f range the physical dimensions are sufficiently small to permit construction of a rotatable structure without much difficulty.

When the dimensions are optimized, the characteristics of the helical beam antenna are such as to qualify it as a broad band antenna. An optimized helical beam shows little variation in the pattern of the main lobe and a fairly uniform feed point impedance averaging approximately 125 ohms over a frequency range of as much as 1.7 to 1. The direction of "electrical twist" (right or left handed) depends upon the direction in which the helix is wound.

A six-turn helical beam is shown schematically in figure 6. The dimensions shown will give good performance over a frequency range of plus or minus 20 per cent of the design frequency. This means that the dimensions are not especially critical when the array is to be used at a single frequency or over a narrow band of frequencies, such as an amateur band. At the design frequency the beam width is about 50 degrees and the power gain about 12 db, referred to a non-directional circularly polarized antenna.

The Ground Screen For the frequency range 100 to 500 Mc. a suitable ground screen can be made from "chicken wire" poultry netting of 1-inch mesh, fastened to a round or square frame of either metal or wood. The netting should be of the type that is galvanized *after* weaving. A small, sheet metal ground plate of diameter equal to approximately D/2 should be centered on the screen and soldered to it. Tin, galvanized iron, or sheet copper. is suitable. The outer conductor of the RG-63/U (125 ohm) coax is connected to this plate, and the inner conductor contacts the helix through a hole in the center of the plate. The end of the coax should be taped with *Scotch* electrical tape to keep water out.

The Helix It should be noted that the beam proper consists of six full turns. The start of the helix is spaced a distance of S/2 from the ground screen, and the conductor goes directly from the center of the ground screen to the start of the helix.

Aluminum tubing in the "SO" (soft) grade is suitable for the helix. Alternatively, lengths of the relatively soft aluminum electrical conduit may be used. In the v-h-f range it will be necessary to support the helix on either two or four wooden longerons in order to achieve sufficient strength. The longerons should be of as small cross section as will provide sufficient rigidity, and should be given several coats of varnish. The ground plane butts against the longerons and the whole assembly is supported from the balance point if it is to be rotated.

Aluminum tubing in the larger diameters ordinarily is not readily available in lengths greater than 12 feet. In this case several lengths can be spliced by means of short telescoping sections and sheet metal screws.

The tubing is close wound on a drum and then spaced to give the specified pitch. Note that the length of one complete turn when spaced is somewhat greater than the circumference of a circle having the diameter D.

Broad-Band 144 to 225 Mc. Helical Beam A highly useful v-h-f helical beam which will receive signals with good gain over the complete frequency range from 144 through 225 Mc. may be constructed by using the following dimensions (180 Mc. design center):

D........................22 in.
S.......................16½ in.
G........................53 in.
Tubing o.d.................1 in.

The D and S dimensions are to the center of the tubing. These dimensions must be held rather closely, since the range from 144 through 225 Mc. represents just about the practical limit of coverage of this type of antenna system.

High-Band TV Coverage Note that an array constructed with the above dimensions will give unusually good high-band TV reception in addition to covering the 144-Mc. and 220-Mc. amateur bands and the taxi and police services.

On the 144-Mc. band the beam width is approximately 60 degrees to the half-power points, while the power gain is approximately 11 db over a non-directional circularly polarized antenna. For high-band TV coverage the gain will be 12 to 14 db, with a beam width of about 50 degrees, and on the 220-Mc. amateur band the beam width will be about 40 degrees with a power gain of approximately 15 db.

The antenna system will receive vertically polarized or horizontally polarized signals with equal gain over its entire frequency range. Conversely, it will transmit signals over the same range, which then can be received with equal strength on either horizontally polarized or vertically polarized receiving antennas. The standing-wave ratio will be very low over the complete frequency range if RG-63/U coaxial feed line is used.

21-6 The Corner-Reflector and Horn-Type Antennas

The corner-reflector antenna is a good directional radiator for the v-h-f and u-h-f region. The antenna may be used with the radiating element vertical, in which case the directivity is in the horizontal or azimuth plane, or the system may be used with the driven element horizontal in which case the radiation is horizontally polarized and most of the directivity is in the vertical plane. With the antenna used as a horizontally polarized radiating system the array is a very good low-angle beam array although the nose of the horizontal pattern is still quite sharp. When the radiator is oriented vertically the corner reflector operates very satisfactorily as a direction-finding antenna.

Design data for the corner-reflector antenna is given in figure 7 and in the chart *Corner-Reflector Design Data.* The planes which make up the reflecting corner may be made of solid sheets of copper or aluminum for the u-h-f bands, although spaced wires with the ends soldered together at top and bottom may be used as the reflector on the lower frequencies.

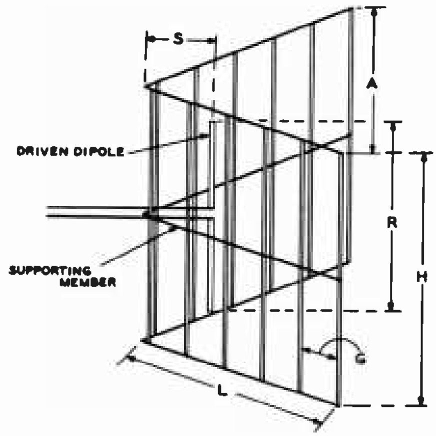


Figure 7
CONSTRUCTION OF THE "CORNER REFLECTOR" ANTENNA

Such an antenna is capable of giving high gain with a minimum of complexity in the radiating system. It may be used either with horizontal or vertical polarization. Design data for the antenna is given in the Corner-Reflector Design Table.

CORNER-REFLECTOR DESIGN DATA

Corner Angle	Freq. Band, Mc.	R	S	H	A	L	G	Feed Imped.	Approx. Gain, db
90	50	110"	82"	140"	200"	230"	18"	72	10
60	50	110"	115"	140"	230"	230"	18"	70	12
60	144	38"	40"	48"	100"	100"	5"	70	12
60	220	24.5"	25"	30"	72"	72"	3"	70	12
60	420	13"	14"	18"	36"	36"	screen	70	12

NOTE: Refer to figure 7 for construction of corner-reflector antenna.

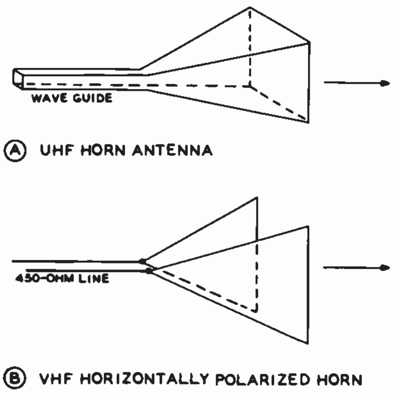
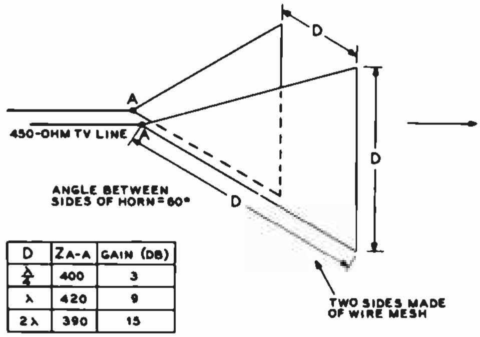


Figure 8
TWO TYPES OF HORN ANTENNAS
The "two sided horn" of Figure 8B may be fed by means of an open-wire transmission line.



D	Z_{A-A}	GAIN (DB)
$\frac{\lambda}{4}$	400	3
λ	420	9
2λ	390	15

Figure 9
THE 60° HORN ANTENNA FOR USE ON FREQUENCIES ABOVE 144 MC.

Copper screen may also be used for the reflecting planes.

The values of spacing given in the corner-reflector chart have been chosen such that the center impedance of the driven element would be approximately 70 ohms. This means that the element may be fed directly with 70-ohm coaxial line, or a quarter-wave matching transformer such as a "Q" section may be used to provide an impedance match between the center-impedance of the element and a 460-ohm line constructed of no. 12 wire spaced 2 inches.

In many v-h-f antenna systems, waveguide transmission lines are terminated by pyramidal horn antennas. These horn antennas (figure 8A) will transmit and receive either horizontally or vertically polarized waves. The use of waveguides at 144 Mc. and 235 Mc., however, is out of the question because of the relatively large dimensions needed for a waveguide operating at these low frequencies.

A modified type of horn antenna may still be used on these frequencies, since only one particular plane of polarization is of interest to the amateur. In this case, the horn antenna can be simplified to two triangular sides of the pyramidal horn. When these two sides are insulated from each other, direct excitation at the apex of the horn by a two-wire transmission line is possible.

In a normal pyramidal horn, all four triangular sides are covered with conducting material, but when horizontal polarization alone is of interest (as in amateur work) only the *vertical* areas of the horn need be used. If vertical polarization is required, only the *horizontal* areas of the horn are employed. In either case, the system is unidirectional, away from the apex of the horn. A typical horn of this type is shown in figure 8B. The two metallic sides of the horn are insulated from each other, and the sides of the horn are made of small mesh "chicken wire" or copper window screening.

A pyramidal horn is essentially a high-pass device whose low frequency cut-off is reached when a side of the horn is ½ wavelength. It will work up to infinitely high frequencies, the gain of the horn increasing by 6 db every time the operating frequency is doubled. The power gain of such a horn compared to a ½ wave dipole at frequencies higher than cut-off is:

$$\text{Power gain (db)} = \frac{8.4\ A^2}{\lambda^2}$$

where A is the frontal area of the mouth of the horn. For the 60 degree horn shown in figure 8B the formula simplifies to:

Power gain (db) = $8.4\ D^2$, when D is expressed in terms of wavelength

When D is equal to one wavelength, the power gain of the horn is approximately 9 db. The gain and feed point impedance of the 60 degree horn are shown in figure 9. A 450 ohm open wire TV-type line may be used to feed the horn.

21-7 VHF Horizontal Rhombic Antenna

For v-h-f transmission and reception in a fixed direction, a horizontal rhombic permits

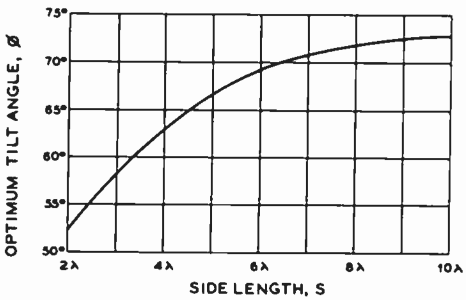


Figure 10
V-H-F RHOMBIC ANTENNA DESIGN CHART

The optimum tilt angle (see figure 11) for "zero-angle" radiation depends upon the length of the sides.

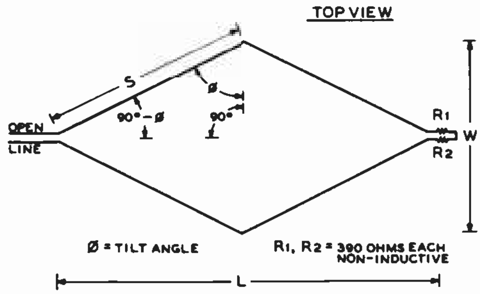


Figure 11
V-H-F RHOMBIC ANTENNA CONSTRUCTION

10 to 16 db gain with a simpler construction than does a phased dipole array, and has the further advantage of being useful over a wide frequency range.

Except at the upper end of the v-h-f range a rhombic array having a worthwhile gain is too large to be rotated. However, in locations 75 to 150 miles from a large metropolitan area a rhombic array is ideally suited for working into the city on extended (horizontally polarized) ground-wave while at the same time making an ideal antenna for TV reception.

The useful frequency range of a v-h-f rhombic array is about 2 to 1, or about plus 40% and minus 30% from the *design frequency*. This coverage is somewhat less than that of a high-frequency rhombic used for sky-wave communication. For ground-wave transmission or reception the only effective vertical angle is that of the horizon, and a frequency range greater than 2 to 1 cannot be covered with a rhombic array without an excessive change in the vertical angle of maximum radiation or response.

The dimensions of a v-h-f rhombic array are determined from the design frequency and figure 10, which shows the proper *tilt angle* (see figure 11) for a given leg length. The gain of a rhombic array increases with leg length. There is not much point in constructing a v-h-f rhombic array with legs shorter than about 4 wavelengths, and the beam width begins to become excessively sharp for leg lengths greater than about 8 wavelengths. A leg length of 6 wavelengths is a good compromise between beam width and gain.

The tilt angle given in figure 10 is based upon a wave angle of zero degrees. For leg lengths of 4 wavelengths or longer, it will be necessary to elongate the array a few per cent (pulling in the sides slightly) if the horizon elevation exceeds about 3 degrees.

Table I gives dimensions for two dual purpose rhombic arrays. One covers the 6-meter amateur band and the "low" television band. The other covers the 2-meter amateur band, the "high" television band, and the 1¼-meter amateur band. The gain is approximately 12 db over a matched half wave dipole and the beam width is about 6 degrees.

The Feed Line The recommended feed line is an open-wire line having a surge impedance between 450 and 600 ohms. With such a line the VSWR will be less than 2 to 1. A line with two-inch spacing is suitable for frequencies below 100 Mc., but one-inch spacing (such as used in the *Gonset Line* for TV installations) is recommended for higher frequencies.

The Termination If the array is to be used only for reception, a suitable termination consists of two 390-ohm carbon re-

	6 METERS AND LOW BAND TV	2 METERS, HIGH BAND TV, AND 1¼ METERS
S (side)	90′	32′
L (length)	166′ 10″	59′ 4″
W (Width)	67′ 4″	23′ 11″

S=6 wavelenths at design frequency
Tilt angle =68°

TABLE I.

sistors in series. If 2-watt resistors are employed, this termination also is suitable for transmitter outputs of 10 watts or less. For higher powers, however, resistors having greater dissipation with negligible reactance in the upper v-h-f range are not readily available.

For powers up to several hundred watts a suitable termination consists of a "lossy" line consisting of stainless steel wire (corresponding to no. 24 or 26 B&S gauge) spaced 2 inches, which in turn is terminated by two 390-ohm 2-watt carbon resistors. The dissipative line should be at least 6 wavelengths long.

21-8 Multi-Element V-H-F Beam Antennas

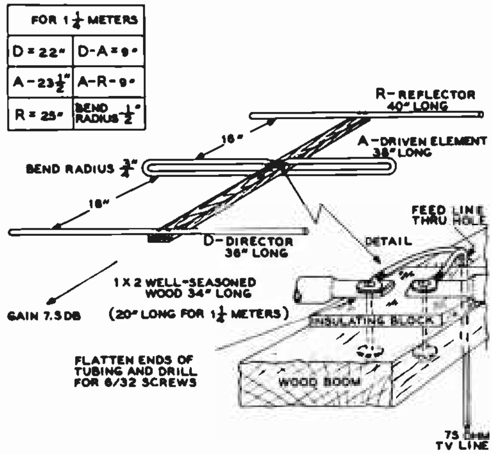


Figure 12

SIMPLE 3-ELEMENT BEAM FOR 2 AND 1¼ METERS

The rotary multi-element beam is undoubtedly the most popular type of v-h-f antenna in use. In general, the design, assembly and tuning of these antennas follows a pattern similar to the larger types of rotary beam antennas used on the lower frequency amateur bands. The characteristics of these low frequency beam antennas are discussed in the next chapter of this Handbook, and the information contained in that chapter applies in general to the v-h-f beam antennas discussed herewith.

A Simple Three Element Beam Antenna The simplest v-h-f beam for the beginner is the three-element Yagi array illustrated in figure 12. Dimensions are given for Yagis cut for the 2-meter and 1¼-meter bands. The supporting boom for the Yagi may be made from a smoothed piece of 1" x 2" wood. The wood should be reasonably dry and should be painted to prevent warpage from exposure to sun and rain. The director and reflector are cut from lengths of ¼" copper tubing, obtainable from any appliance store that does service work on refrigerators. They should be cut to length as noted in figure 12. The elements should then be given a coat of aluminum paint. Two small holes are drilled at the center of the reflector and director and these elements are bolted to the wood boom by means of two 1" wood screws. These screws should be of the plated, or rust-proof variety.

The driven element is made of a 78" length of ¼" copper tubing, the ends bent back upon each other to form a folded dipole. If the tubing is packed with fine sand and the bending points heated over a torch, no trouble will be had in the bending process. If the tubing does collapse when it is bent, the break may be repaired with a heavy-duty soldering iron. The driven element is next attached to the center of the wood boom, mounted atop a small insulating plate made of bakelite, micarta or some other non-conducting material. It is held in place in the same manner as the parasitic elements. The two free ends of the folded dipole are hammered flat and drilled for a 6-32 bolt. These bolts pass through both the insulating block and the boom, and hold the free tips of the element in place.

A length of 75-ohm Twin-Lead TV-type line should be used with this beam antenna. It is connected to each of the free ends of the folded dipole. If the antenna is mounted in the vertical plane, the 75-ohm line should be brought away from the antenna for a distance of four to six feet before it drops down the tower to lessen interaction between the antenna elements and the feed line. The complete antenna is light enough to be turned by a TV rotator.

A simple Yagi antenna of this type will provide a gain of 7 db over the entire 2-meter or 1¼-meter band, and is highly recommended as an "easy-to-build" beam for the novice or beginner.

An 8-Element "Tippable" Array for 144 Mc. Figures 13 and 14 illustrate an 8-element rotary array for use on the 144-Mc. amateur band. This array is "tippable" to obtain either horizontal or vertical polarization. It is necessary that the transmitting and receiving station use the same polarization for the ground-wave signal propagation which is characteristic of this fre-

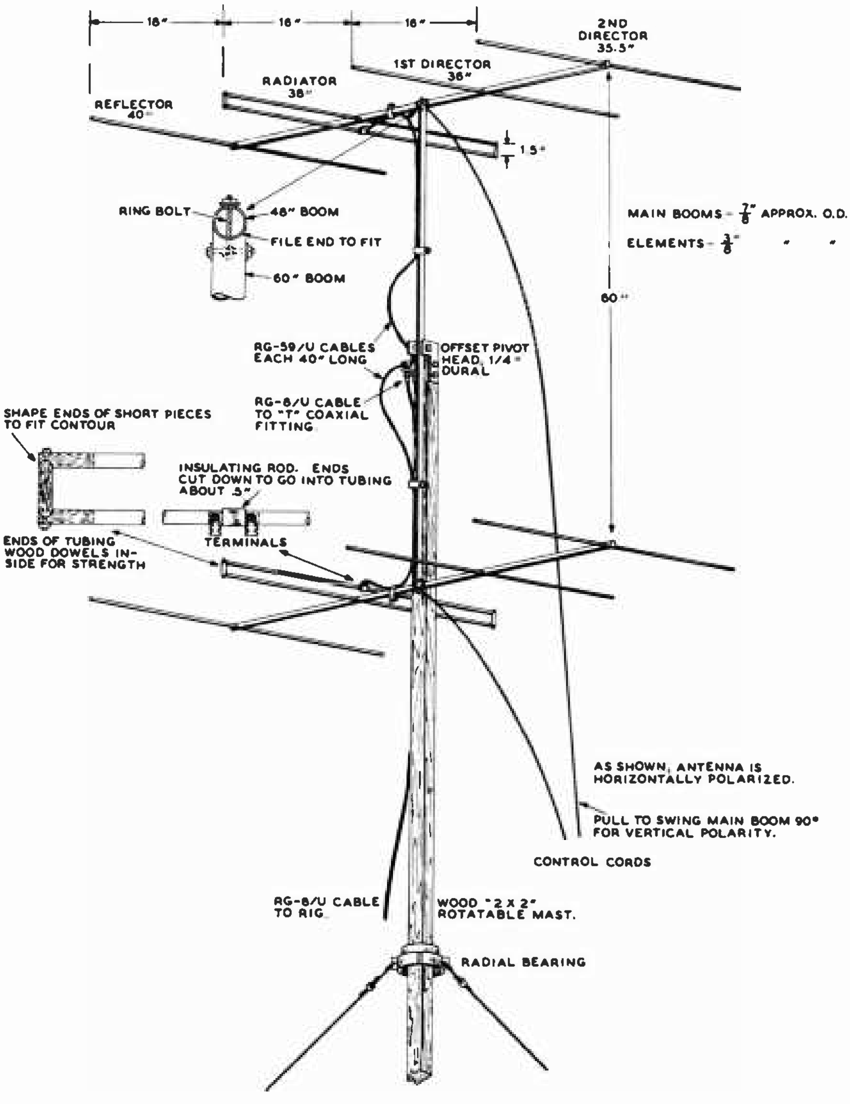


Figure 13
CONSTRUCTIONAL DRAWING OF AN EIGHT-ELEMENT TIPPABLE 144-MC. ARRAY

quency range. Although polarization has been loosely standardized in various areas of the country, exceptions are frequent enough so that it is desirable that the polarization of antenna radiation be easily changeable from horizontal to vertical.

The antenna illustrated has shown a signal gain of about 11 db, representing a power gain of about 13. Although the signal gain of the antenna is the same whether it is oriented for vertical or horizontal polarization, the horizontal beam width is smaller when the antenna is oriented for vertical polarization. Conversely, the vertical pattern is the sharper when the antenna system is oriented for horizontal polarization.

The changeover from one polarization to the other is accomplished simply by pulling on the

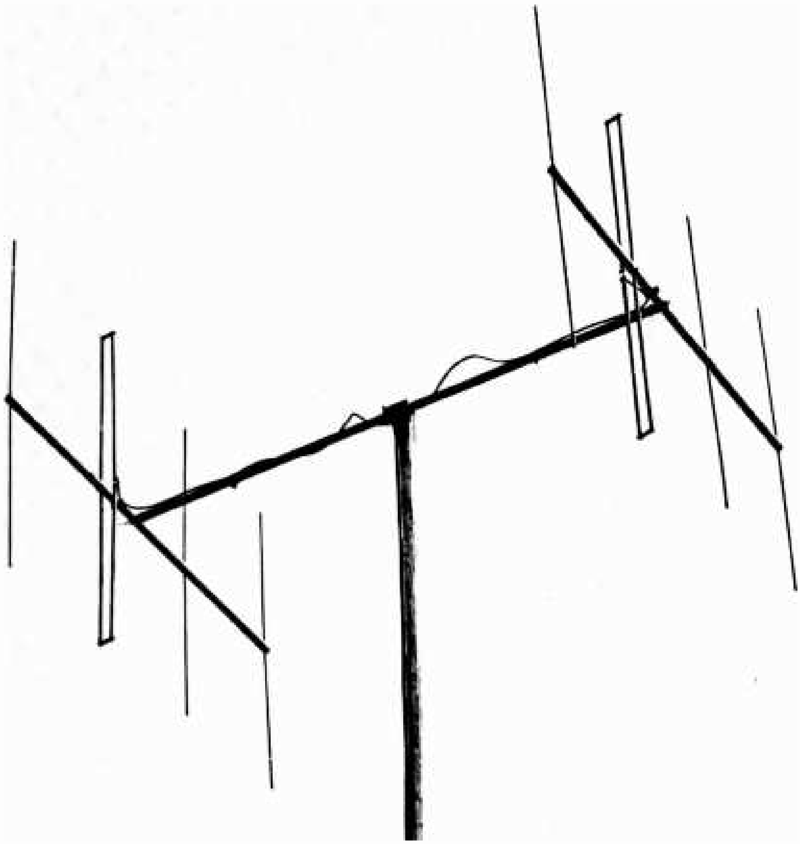


Figure 14
THE EIGHT-ELEMENT 144-MC. ARRAY IN A HORIZONTAL POSITION

appropriate cord. Hence, the operation is based on the offset head sketched in figure 13. Although a wood mast has been used, the same system may be used with a pipe mast.

The 40-inch lengths of RG-59/U cable (electrically ¾ wavelength) running from the center of each folded dipole driven element to the coaxial T-junction allow enough slack to permit free movement of the main boom when changing polarity. Type RG-8/U cable is run from the T-junction to the operating position. Measured standing-wave ratio was less than 2:1 over the 144 to 148 Mc. band, with the lengths and spacings given in figure 13.

Construction of the Array Most of the constructional aspects of the antenna array are self-evident from figure 13. However, the pointers given in the following paragraphs will be of assistance to those wishing to reproduce the array.

The drilling of holes for the small elements should be done carefully on accurately marked centers. A small angular error in the drilling of these holes will result in a considerable misalignment of the elements after the array is assembled. The same consideration is true of the filing out of the rounded notches in the ends of the main boom for the fitting of the two antenna booms.

Short lengths of wood dowel are used freely in the construction of the array. The ends of the small elements are plugged with an inch or so of dowel, and the ends of the antenna booms are similarly treated with larger discs pressed into place.

The ends of the folded dipoles are made in the following manner: Drive a length of dowel into the short connecting lengths of aluminum tubing. Then drill down the center of the dowel with a clearance hole for the connecting screw. Then shape the ends of the connecting pieces to fit the sides of the element ends. After assembly the junctions may be dressed with a file and sandpaper until a smooth fit is obtained.

The mast used for supporting the array is a 30-foot spliced 2 by 2. A large discarded ball bearing is used as the radial load bearing and guy-wire termination. Enough of the upper-mast corners were removed with a draw-knife to permit sliding the ball bearing down about 9 feet from the top of the mast. The bearing then was encircled by an assembly of three pieces of dural ribbon to form a clamp, with ears for tightening screws and attachment of the guy wires. The bearing then was greased and covered with a piece of auto inner tube to serve as protection from the weather. Another junk-box bearing was used at the bottom of the mast as a thrust bearing.

The main booms were made from ¾-inch aluminum electrical conduit. Any size of small tubing will serve for making the elements. Note that the main boom is mounted at the balance center and not necessarily at the physical center. The pivot bolt in the offset head should be tightened sufficiently that there will be adequate friction to hold the array in position. Then an additional nut should be placed on the pivot bolt as a lock.

In connecting the phasing sections between the T-junction and the centers of the folded dipoles, it is important that the center conductors of the phasing sections be connected to the same side of the driven elements of the antennas. In other words, when the antenna is oriented for horizontal polarization and the center of the coaxial phasing section goes to the left side of the top antenna, the center conductor of the other coaxial phasing section should go to the left side of the bottom antenna.

The "Screen Beam" for 2 Meters This highly effective rotary array for the 144 Mc. amateur band was designed by the staff of the Experimental Physics Laboratory, The Hague, Netherlands for use at the 2 meter experimental station PE1PL. The array consists of 10 half wave radiators fed in phase, and arranged in two stacked rows of five radiators. 0.2 wavelength behind this plane of radiators is a reflector screen, measuring approximately 15' x 9' in size. The antenna provides a power gain of 15 db, and a front to back ratio of approximately 28 db.

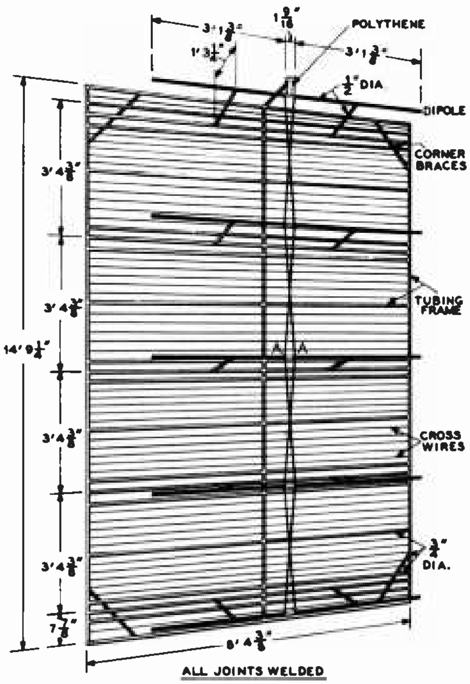


Figure 15
DETAIL OF LAYOUT AND DIMENSIONS OF BEAM ASSEMBLY OF PE1PL

The 10 dipoles are fed in phase by means of a length of balanced transmission line, a quarter-wave matching transformer, and a balun. A 72-ohm coaxial line couples the array to the transmitter. A drawing of the array is shown in figure 15.

The reflecting screen measures 14' 9" high by 8' 4" wide, and is made of welded ½" diameter steel tubing. Three steel reinforcing bars are welded horizontally across the framework directly behind each pair of horizontal dipoles. The intervening spaces are filled with lengths of no. 12 enamel-coated copper wire to complete the screen. The spacing between the wires is 2". Four cross braces are welded to the corners of the frame for additional bracing, and a single vertical ½" rod runs up the middle of the frame. The complete, welded frame is shown in figure 15. The no. 12 screening wires are run between 6-32 bolts placed in holes drilled in each outside vertical member of the frame.

The antenna assembly is supported away from the reflector screen by means of ten lengths of ½" steel tubing, each 1' 3¼" long.

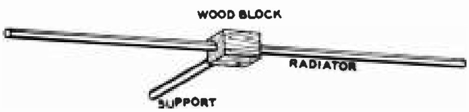


Figure 16

THE MOUNTING BLOCK FOR EACH SET OF ELEMENTS

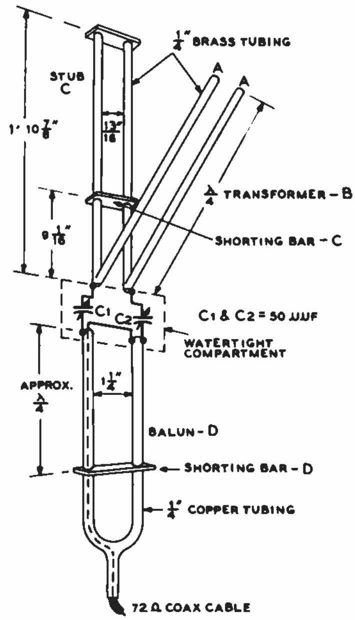


Figure 17

THE MATCHING UNIT IN DETAIL FOR THE PE1PL BEAM DESIGN, WHICH ALLOWS THE USE OF 72-OHM COAX

These tubes are welded onto the center tube of each group of three horizontal bracing tubes, and are so located to support the horizontal dipole at its exact center. The dipoles are attached to the supporting rods by means of small phenolic insulating blocks, as shown in figure 16. The radiators are therefore insulated from the screen reflector. The inner tips of the radiators are held by small polystyrene blocks for rigidity, and are cross connected to each other by a transposed length of TV-type 400 ohm open wire line. The entire array is fed at the point A-A, illustrated in figure 15.

The matching system for the beam is mounted behind the reflector screen, and is shown in figure 17. A quarter-wave transformer (B) drops the relatively high impedance of the antenna array to a suitable value for the low impedance balun (D). An adjustable matching stub (C) and two variable capacitors (C_1 and C_2) are employed for impedance matching. The two variable capacitors are mounted in a watertight box, with the balun and matching stubs entering the bottom and top of the box, respectively.

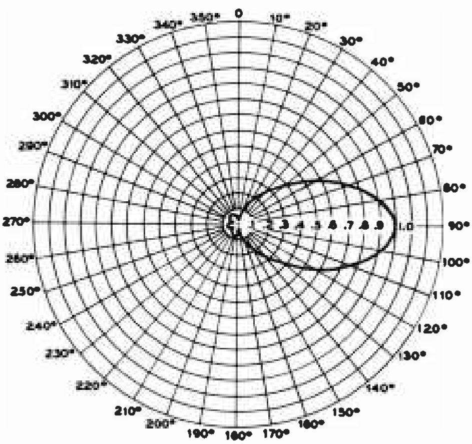


Figure 18

HORIZONTAL RADIATION PATTERN OF THE PE1PL ARRAY. THE FRONT-TO-BACK RATIO IS ABOUT 28 db IN AMPLITUDE, AND THE FORWARD GAIN APPROXIMATELY 15 db.

The matching procedure is carried out by the use of a standing wave meter (SWR bridge). A few watts of power are fed to the array through the SWR meter, and the setting of the shorting stub on C and the setting of the two variable capacitors are adjusted for lowest SWR at the chosen operating frequency. The capacity settings of the two variable capacitors should be equal. The final adjustment is to set the shorting stub of the balun (D) to remove any residual reactance that might appear on the transmission line. With proper adjustment, the VSWR of the array may be held to less than 1.5 to 1 over a 2 megacycle range of the 2-meter band.

The horizontal radiation pattern of this array is shown in figure 18.

A Simple 50 Mc. 3-element Array Shown in figure 19 is a 3-element array for the six-meter band. A simple wooden frame may be made from a ten-foot ladder as

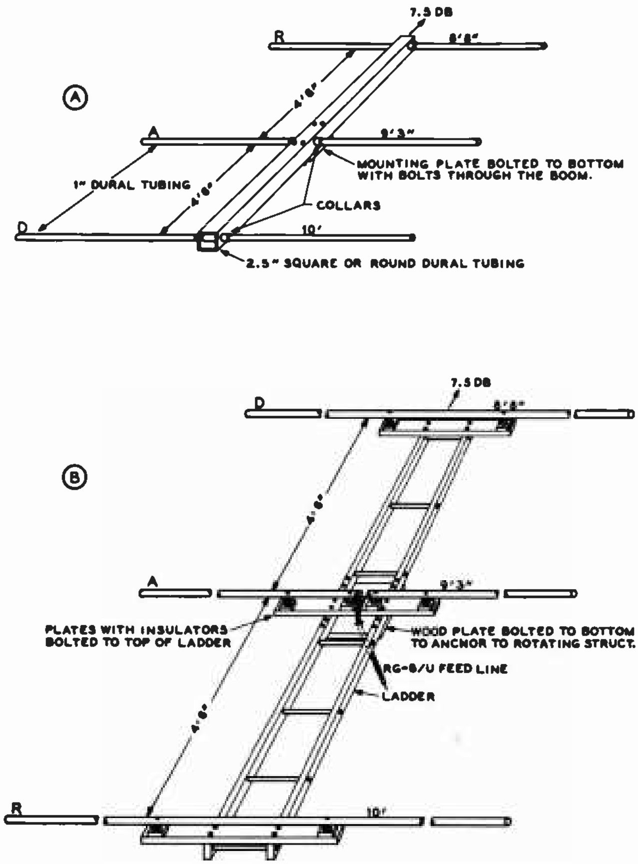


Figure 19

THE 6-METER BEAM. SUPPORTING BOOM ARRANGEMENTS

(A) shows the use of a section of dural tubing (either rectangular or round cross section) for supporting a moderate size array. At (B) is shown the use of a ladder for supporting a relatively large array.

illustrated, or a lighter (but more expensive) assembly may be made from a section of two-inch aluminum irrigation tubing used for the boom.

All elements are made of ten-foot lengths of 1" diameter EMT electrician's conduit, available at most large electrical supply houses. Since quarter-wave spacing is used between the driven element and the two parasitic elements, the feed-impedance of the array is of the order of 40 ohms or so. It is thus practical to split the driven element in the center and feed it directly with RG-8/U coaxial line; the inner conductor is connected directly to one side of the radiator while the outer conductor of the line is connected to the other half of the radiator. This provides a low value of SWR on the transmission line.

With the all-metal configuration, it is necessary to use a gamma-match for a coaxial feed system, or to use a folded dipole as the radiator of the beam. The folded dipole may be made up of two aluminum tubes, connected at their extreme ends. The main tube (which is attached to the boom) may be 1"-diameter EMT tubing. The second tube should be made of ½"-diameter aluminum tubing. It is split at the center and fed with a balanced 300 ohm TV-type line.

CHAPTER TWENTY TWO

Rotary Beams

The rotatable antenna array has become almost standard equipment for operation on the 28-Mc. and 50-Mc. bands and is commonly used on the 14-Mc. and 21-Mc. bands and on those frequencies above 144 Mc. The rotatable array offers many advantages for both military and amateur use. The directivity of the antenna types commonly employed, particularly the unidirectional arrays, offers a worthwhile reduction in interference from undesired directions. Also, the increase in the ratio of low-angle radiation plus the theoretical gain of such arrays results in a relatively large increase in both the transmitted signal and the signal intensity from a station being received.

A significant advantage of a rotatable antenna array in the case of the normal station is that a relatively small amount of space is required for erection of the antenna system. In fact, one of the best types of installation uses a single telephone pole with the rotating structure holding the antenna mounted atop the pole. To obtain results in all azimuth directions from fixed arrays comparable to the gain and directivity of a single rotatable three-element parasitic beam would require several acres of surface.

There are two normal configurations of radiating elements which, when horizontally polarized, will contribute to obtaining a low angle of radiation. These configurations are the end-fire array and the broadside array. The conventional three- or four-element rotary beam may properly be called a ***unidirectional parasitic end-fire array***, and is actually a type of ***yagi*** array. The flat-top beam is a type of ***bi-directional end-fire array***. The ***broadside type*** of array is also quite effective in obtaining low-angle radiation, and although widely used in FM and TV broadcasting has seen little use by amateur stations in rotatable arrays.

22-1 Unidirectional Parasitic End-Fire Arrays (Yagi Type)

If a single parasitic element is placed on one side of a driven dipole at a distance of from 0.1 to 0.25 wavelength the parasitic element can be tuned to make the array substantially unidirectional.

This simple array is termed a ***two element parasitic beam.***

22-2 The Two Element Beam

The two element parasitic beam provides the greatest amount of gain per unit size of any array commonly used by radio amateurs.

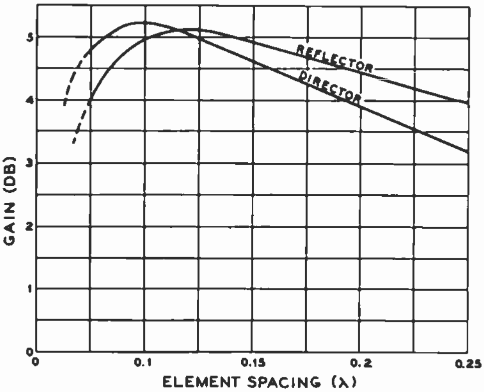


Figure 1

GAIN VS ELEMENT SPACING FOR A TWO-ELEMENT CLOSE-SPACED PARASITIC BEAM ANTENNA WITH PARASITIC ELEMENT OPERATING AS A DIRECTOR OR REFLECTOR

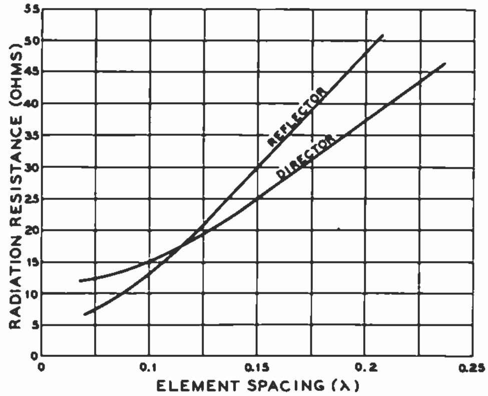


Figure 2

RADIATION RESISTANCE AS A FUNCTION OF ELEMENT SPACING FOR A TWO-ELEMENT PARASITIC ARRAY

Such an antenna is capable of a signal gain of 5 db over a dipole, with a front-to-back ratio of 7 db to 15 db, depending upon the adjustment of the parasitic element. The parasitic element may be used either as a director or as a reflector.

The optimum spacing for a reflector in a two-element array is approximately 0.13 wavelength and with optimum adjustment of the length of the reflector a gain of approximately 5 db will be obtained, with a feed-point resistance of about 25 ohms.

If the parasitic element is to be used as a director the optimum spacing between it and the driven element is 0.11 wavelength. The gain will theoretically be slightly greater than with the optimum adjustment for a reflector (about 5.5 db) and the radiation resistance will be in the vicinity of 17 ohms.

The general characteristics of a two-element parasitic array may be seen in figures 1, 2 and 3. The gain characteristics of a two-element array when the parasitic element is used as a director or as a reflector are shown. It can be seen that the director provides a maximum of 5.3 db gain at a spacing of slightly greater than 0.1 wavelength from the antenna. In the interests of greatest power gain and size conservation, therefore, the choice of a parasitic director would be wiser than the choice of a parasitic reflector, although the gain difference between the two is small.

Figure 2 shows the relationship between the element spacing and the radiation resistance for the two element parasitic array for both the reflector and the director case. Since the optimum antenna-director spacing for maximum gain results in an antenna radiation resistance of about 17 ohms, and the optimum antenna-reflector spacing for maximum gain results in an antenna radiation resistance of about 25 ohms, it may be of advantage in some instances to choose the antenna with the higher radiation resistance, assuming other factors to be equal.

Figure 3 shows the front-to-back ratio for the two element parasitic array for both the reflector and director cases. To produce these curves, the elements were tuned for maximum gain of the array. Better front-to-back ratios may be obtained at the expense of array gain, if desired, but the general shape of the curves remains the same. It can be readily observed that operation of the parasitic element as a reflector produces relatively poor front-to-back ratios except when the element spacing is greater than 0.15 wavelength. However, at this element spacing, the gain of the array begins to suffer.

Since a radiation resistance of 17 ohms is not unduly hard to match, it can be argued that the best all-around performance may be obtained from a two element parasitic beam employing 0.11 element spacing, with the parasitic element tuned to operate as a director. This antenna will provide a forward gain of 5.3 db, with a front-to-back ratio of 10 db, or slightly greater. Closer spacing than 0.11

wavelength may be employed for greater front-to-back ratios, but the radiation resistance of the array becomes quite low, the bandwidth of the array becomes very narrow, and the tuning becomes quite critical. Thus the Q of the antenna system will be *increased* as the spacing between the elements is *decreased*, and smaller optimum frequency coverage will result.

Element Lengths When the parasitic element of a two-element array is used as a director, the following formulas may be used to determine the lengths of the driven element and the parasitic director, assuming an element diameter-to-length ratio of 200 to 400:

$$\text{Driven element length (feet)} = \frac{476}{F_{Mc.}}$$

$$\text{Director length (feet)} = \frac{450}{F_{Mc.}}$$

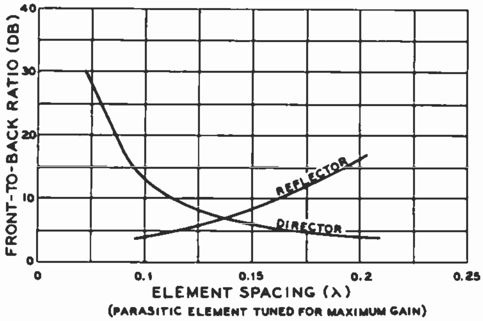


Figure 3

FRONT-TO-BACK RATIO AS A FUNCTION OF ELEMENT SPACING FOR A TWO-ELEMENT PARASITIC ARRAY

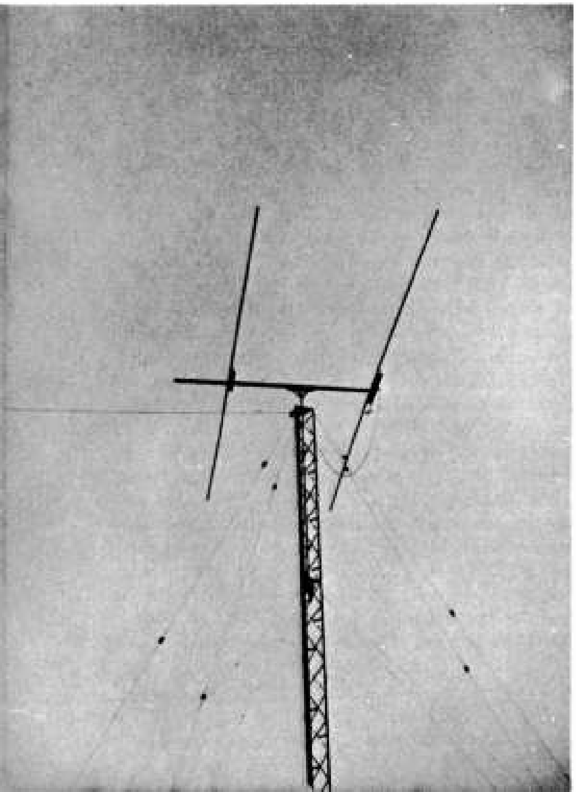


Figure 4

TWO ELEMENT 14-MC. BEAM ANTENNA AT W6SAI

The effective bandwidth taken between the 1.5/1 standing wave points of an array cut to the above dimensions is about 2.5% of the operating frequency. This means that an array pre-cut to a frequency of 14,150 kilocycles would have a bandwidth of 350 kilocycles (plus or minus 175 kilocycles of the center frequency), and therefore would be effective over the whole 20 meter band. In like fashion, a 15 meter array should be pre-cut to 21,200 kilocycles.

A beam designed for use on the 10-meter band would have an effective bandwidth of some 700 kilocycles. Since the 10-meter band is 1700 kilocycles in width, the array should either be cut to 28,500 kilocycles for operation in the low frequency portion of the band, or to 29,200 kilocycles for operation in the high frequency portion of the band. Operation of the antenna outside the effective bandwidth will increase the SWR on the transmission line, and noticeably degrade both the gain and front-to-back ratio performance. Figure 4 illustrates an all-metal 2-element 14 Mc. array.

22-3 The Three-Element Array

The three-element array using a director, driven element, and reflector will exhibit as much as 30 db front-to-back ratio and 20 db front-to-side ratio for *low-angle radiation*. The theoretical gain is about 9 db over a dipole in free space. In actual practice, the array will often show 7 to 10 db apparent gain over a horizontal dipole placed the same height above ground (at 28 and 14 Mc.).

The use of more than three elements is desirable when the length of the supporting structure is such that spacings of approximately

0.2 wavelength between elements becomes possible. Four-element arrays are quite common on the 28-Mc. and 50-Mc. bands, and five elements are sometimes used for increased gain and discrimination. As the number of elements is increased the gain and front-to-back ratio increases but the radiation resistance decreases and the bandwidth or frequency range over which the antenna will operate without reduction in effectiveness is decreased.

Material for Elements While the elements may consist of wire supported on a wood framework, self-supporting elements of tubing are much to be preferred. The latter type array is easier to construct, looks better, is no more expensive, and avoids the problem of getting sufficiently good insulation at the ends of the elements. The voltages reach such high values towards the ends of the elements that losses will be excessive, unless the insulation is excellent.

The elements may be fabricated of thin-walled steel conduit, or hard drawn thin-walled copper tubing, but dural tubing is much better. Or, if you prefer, you may purchase tapered copper-plated steel tubing elements designed especially for the purpose. Kits are available complete with rotating mechanism and direction indicator, for those who desire to purchase the whole system ready to put up.

Element Spacing The optimum spacing for a two-element array is, as has been mentioned before, approximately 0.11 wavelength for a director and 0.13 wavelength for a reflector. However, when both a director and a reflector are combined with the driven element to make up a three-element array the optimum spacing is established by the bandwidth which the antenna will be required to cover. Wide spacing (of the order of 0.25 wavelength between elements) will result in greater bandwidth for a specified maximum standing-wave ratio on the antenna transmission line. Smaller spacings may be used when boom length is an important consideration, but for a specified standing-wave ratio and forward gain the frequency coverage will be smaller. Thus the Q of the antenna system will be *increased* as the spacing between the elements is *decreased,* resulting in smaller frequency coverage, and at the same time the feed-point impedance of the driven element will be decreased.

For broad-band coverage, such as the range from 26.96 to 29.7 Mc. or from 50 to 54 Mc., 0.2 wavelength spacing from the driven element to each of the parasitic elements is recommended. For narrower bandwidth, such as would be adequate for the 14.0 to 14.4 Mc. band or the 144 to 148 Mc. band, the radiator to parasitic element spacing may be reduced to 0.12 wavelength, while still maintaining adequate array bandwidth for the amateur band in question.

Length of the Parasitic Elements Experience has shown that it is practical to cut the prarsitic elements of a three-elementparasitic array to a predetermined length before the installation of such an antenna. A pre-tuned antenna such as this will give good signal gain, adequate front-to-back ratio, and good bandwidth factor. By carefully tuning the array after it is in position the gain may be increased by a fraction of a db, and the front-to-back ratio by several db. However the slight improvement in performance is usually not worth the effort expended in tuning time.

The closer the lengths of the parasitic elements are to the resonant length of the driven element, the lower will be the feed-point resistance of the driven element, and the smaller will be the bandwidth of the array. Hence, for wide frequency coverage the director should be considerably shorter, and the reflector considerably longer than the driven element. For example, the director should still be less than a resonant half wave at the upper frequency limit of the range wherein the antenna is to be operated, and the reflector should still be long enough to act as a reflector at the lower frequency limit. Another way of stating the same thing is to say, in the case of an array to cover a wide frequency range such as the amateur range from 26.96 to 29.7 Mc. or the width of a low-band TV channel, that the director should be cut for the upper end of the band and the reflector for the lower end of the band. In the case of the 26.96 to 29.7 Mc. range this means that the director should be about 8 per cent shorter than the driven element and the reflector should be about 8 per cent longer. Such an antenna will show a relatively constant gain of about 6 db over its range of coverage, and the pattern will not reverse at any point in the range.

Where the frequency range to be covered is somewhat less, such as a high-band TV channel, the 14.0 to 14.4 Mc. amateur band, or the lower half of the amateur 28-Mc. phone band, the reflector should be about 5 per cent longer than the driven element, and the director about 5 per cent shorter. Such an antenna will perform well over its rated frequency band, will not reverse its pattern over this band, and will show a signal gain of 7 to 8 db. See figure 5 for design figures for 3-element arrays.

TYPE	DRIVEN ELEMENT LENGTH	REFLECTOR LENGTH	1ST DIRECTOR LENGTH	2ND DIRECTOR LENGTH	3RD DIRECTOR LENGTH	SPACING BETWEEN ELEMENTS	APPROX. GAIN DB	APPROX. RADIATION RESISTANCE (Ω)
3-ELEMENT	$\frac{472}{F(MC)}$	$\frac{500}{F(MC)}$	$\frac{445}{F(MC)}$	—	—	.15-.15	7.0	20
3-ELEMENT	$\frac{472}{F(MC)}$	$\frac{495}{F(MC)}$	$\frac{450}{F(MC)}$	—	—	.25-.25	8.5	35
4-ELEMENT	$\frac{472}{F(MC)}$	$\frac{497}{F(MC)}$	$\frac{450}{F(MC)}$	$\frac{440}{F(MC)}$	—	.2-.2-.2	9.5	20
5-ELEMENT	$\frac{472}{F(MC)}$	$\frac{497}{F(MC)}$	$\frac{450}{F(MC)}$	$\frac{440}{F(MC)}$	$\frac{430}{F(MC)}$	.2-.2-.2-.2	10.0	15

Figure 5

DESIGN CHART FOR PARASITIC ARRAYS (DIMENSIONS GIVEN IN FEET)

More Than Three Elements A small amount of additional gain may be obtained through use of more than two parasitic elements, at the expense of reduced feed-point impedance and lessened bandwidth. One additional director will add about 1 db, and a second additional director (making a total of five elements including the driven element) will add slightly less than one db more. In the v-h-f range, where the additional elements may be added without much difficulty, and where required bandwidths are small, the use of more than two parasitic elements is quite practicable.

Stacking of Yagi Arrays Parasitic arrays (yagis) may be stacked to provide additional gain in the same manner that dipoles may be stacked. Thus if an array of six dipoles would give a gain of 10 db. the substitution of yagi arrays for each of the dipoles would add the gain of *one* yagi array to the gain obtained with the dipoles. However, the yagi arrays *must be more widely spaced* than the dipoles to obtain this theoretical improvement. As an example, if six 5-element yagi arrays having a gain of about 10 db were substituted for the dipoles, with appropriate increase in the spacing between the arrays, the gain of the whole system would approach the sum of the two gains, or 20 db. A group of arrays of yagi antennas, with recommended spacing and approximate gains, are illustrated in figure 6.

22-4 Feed Systems for Parasitic (Yagi) Arrays

The table of figure 5 gives, in addition to other information, the approximate radiation resistance referred to the center of the driven element of multi-element parasitic arrays. It is obvious, from these low values of radiation resistance, that especial care must be taken in materials used and in the construction of the elements of the array to insure that ohmic losses in the conductors will not be an appreciable percentage of the radiation resistance. It is also obvious that some method of impedance transformation must be used in many cases to match the low radiation resistance of these antenna arrays to the normal range of characteristic impedance used for antenna transmission lines.

A group of possible methods of impedance matching is shown in figures 7, 8, 9 and 10. All these methods have been used but certain of them offer advantages over some of the other methods. Generally speaking it is not mechanically desirable to break the center of the driven element of an array for feeding the system. Breaking the driven element rules out the practicability of building an all-metal or "plumber's delight" type of array, and imposes mechanical limitations with any type of construction. However, when continuous rotation is desired, an arrangement such as shown in figure 9D utilizing a broken driven element with a rotatable transformer for coupling from the antenna transmission line to the driven element has proven to be quite satisfactory. In fact the method shown in figure 9D is probably the most practicable method of feeding the driven element when continuous rotation of the antenna array is required.

The feed systems shown in figure 7 will, under normal conditions, show the lowest losses of any type of feed system since the currents flowing in the matching network are the lowest of all the systems commonly used. The "Folded Element" match shown in figure 7A and the "Yoke" match shown in figure 7B are the most satisfactory electrically of all standard feed methods. However, both methods require the extension of an additional conductor out to the end of the driven element as a portion of the matching system. The folded-element match is best on the 50-Mc. band and

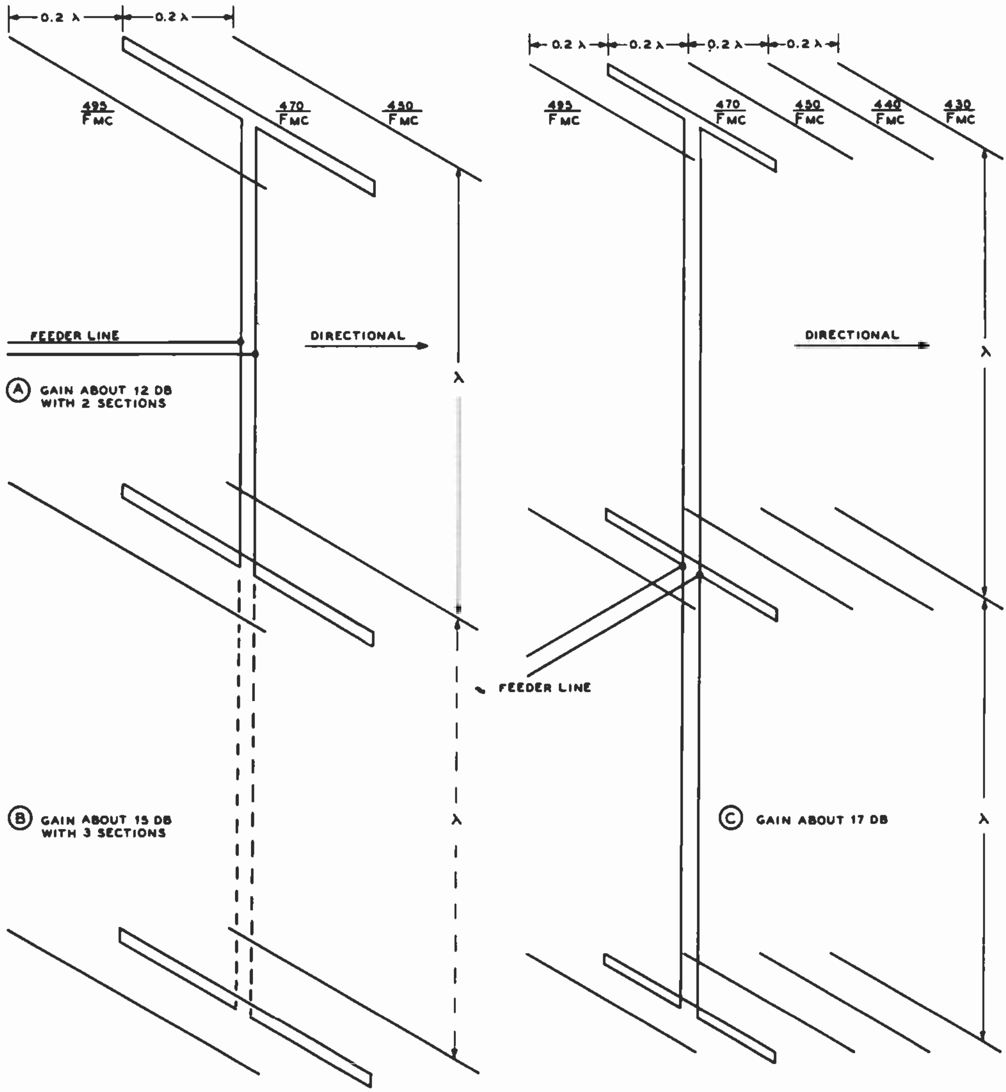


Figure 6

STACKED YAGI ARRAYS

It is possible to attain a relatively large amount of gain over a limited bandwidth with stacked yagi arrays. The two-section array at (A) will give a gain of about 12 db, while adding a third section will bring the gain up to about 15 db. Adding two additional parasitic directors to each section, as at (C) will bring the gain up to about 17 db.

higher where the additional section of tubing may be supported below the main radiator element without undue difficulty. The yoke-match is more satisfactory mechanically on the 28-Mc. and 14-Mc. bands since it is only necessary to suspend a wire below the driven element proper. The wire may be spaced below the self-supporting element by means of several

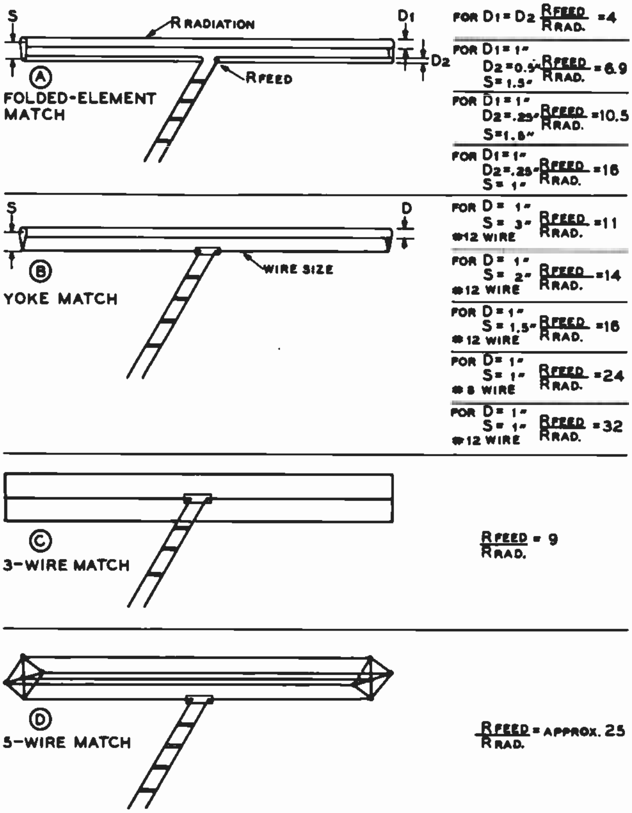


Figure 7
DATA FOR FOLDED-ELEMENT MATCHING SYSTEMS

In all normal applications of the data given the main element as shown is the driven element of a multi-element parasitic array. Directors and reflectors have not been shown for the sake of clarity.

small strips of polystyrene which have been drilled for both the main element and the small wire and threaded on the main element.

The Folded-Element Match Calculations The calculation of the operating conditions of the folded-element matching system and the yoke match, as shown in figures 7A and 7B is relatively simple. A selected group of operating conditions has been shown on the drawing of figure 7. In applying the system it is only necessary to multiply the ratio of feed to radiation resistance (given in the figures to the right of the suggested operating dimensions in figure 7) by the radiation resistance of the antenna system to obtain the impedance of the cable to be used in feeding the array. Approximate values of radiation resistance for a number of commonly used parasitic-element arrays are given in figure 5.

As an example, suppose a 3-element array with 0.15D-0.15R spacing between elements is to be fed by means of a 465-ohm line constructed of no. 12 wire spaced 2 inches. The approximate radiation resistance of such an antenna array will be 20 ohms. Hence we need a ratio of impedance step up of 23 to obtain a match between the characteristic impedance of the transmission line and the radiation resistance of the driven element of the antenna array. Inspection of the ratios given in figure 7 shows that the fourth set of dimensions given under figure 7B will give a 24-to-1 step up, which is sufficiently close. So it is merely necessary to use a 1-inch diameter driven element with a no. 8 wire spaced on 1 inch centers (½ inch below the outside wall of the 1-inch tubing) below the 1-inch element. The no. 8 wire is broken and a 2-inch insulator placed in the center. The feed line then carries from this insulator down to the transmitter. The center insulator should be supported rigidly from the 1-inch tube so that the spacing between the piece of tubing and the no. 8 wire will be accurately maintained.

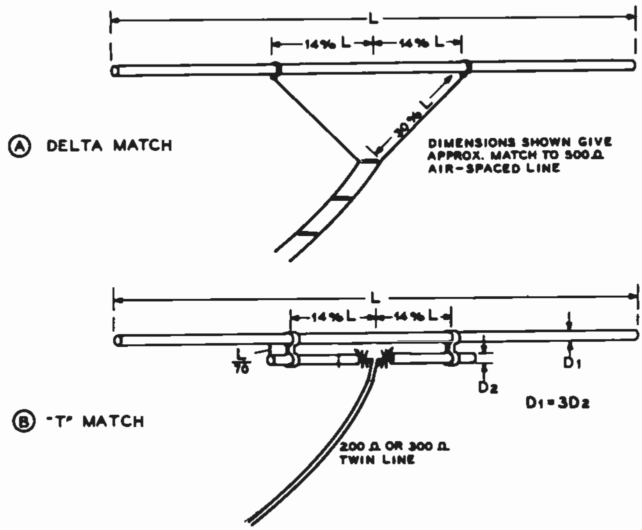


Figure 8
AVERAGE DIMENSIONS FOR THE DELTA AND "T" MATCH

In many cases it will be desired to use the folded-element or yoke matching system with different sizes of conductors or different spacings than those shown in figure 7. Note, then, that the impedance transformation ratio of these types of matching systems is dependent *both upon the ratio of conductor diameters* and *upon their spacing.* The following equation has been given by Roberts (*RCA Review,* June, 1947) for the determination of the impedance transformation when using different diameters in the two sections of a folded element:

$$\text{Transformation ratio} = \left(1 + \frac{Z_1}{Z_2}\right)^2$$

In this equation Z_1 is the characteristic impedance of a line made up of the smaller of the two conductor diameters spaced the center-to-center distance of the two conductors in the antenna, and Z_2 is the characteristic impedance of a line made up of two conductors the size of the larger of the two. This assumes that the feed line will be connected in series with the *smaller* of the two conductors so that an impedance step up of greater than four will be obtained. If an impedance step up of less than four is desired, the feed line is connected in series with the *larger* of the two conductors and Z_1 in the above equation becomes the impedance of a hypothetical line made up of the larger of the two conductors and Z_2 is made up of the smaller. The folded v-h-f unipole is an example where the transmission line is connected in series with the larger of the two conductors.

The conventional 3-wire match to give an impedance multiplication of 9 and the 5-wire match to give a ratio of approximately 25 are shown in figures 7C and 7D. The 4-wire match, not shown, will give an impedance transformation ratio of approximately 16.

The Delta Match and T-Match The Delta match and the T-match are shown in figure 8. The delta match has been largely superseded by the newer T-match, however both these systems can be adjusted to give a low value of SWR on 50 to 600-ohm balanced transmission lines. In the case of the systems shown it will be necessary to make adjustments in the tapping distance along the driven radiator until minimum standing waves on the antenna transmission line are obtained. Since it is sometimes impracticable to eliminate completely the standing waves from the antenna transmission line when using these matching systems, it is common practice to cut the feed line, after standing waves have been reduced to a minimum, to a length which will give satisfactory loading of the transmitter over the desired frequency range of operation.

The inherent reactance of the T-match is tuned out by the use of two identical resonating capacitors in series with each leg of the T-rod. These capacitors should each have a maximum capacity of 8 $\mu\mu$fd. per meter of wavelength. Thus for 20 meters, each capacitor should have a maximum capacity of at least 160 $\mu\mu$fd. For power up to a kilowatt, 1000 volt spacing of the capacitors is adequate.

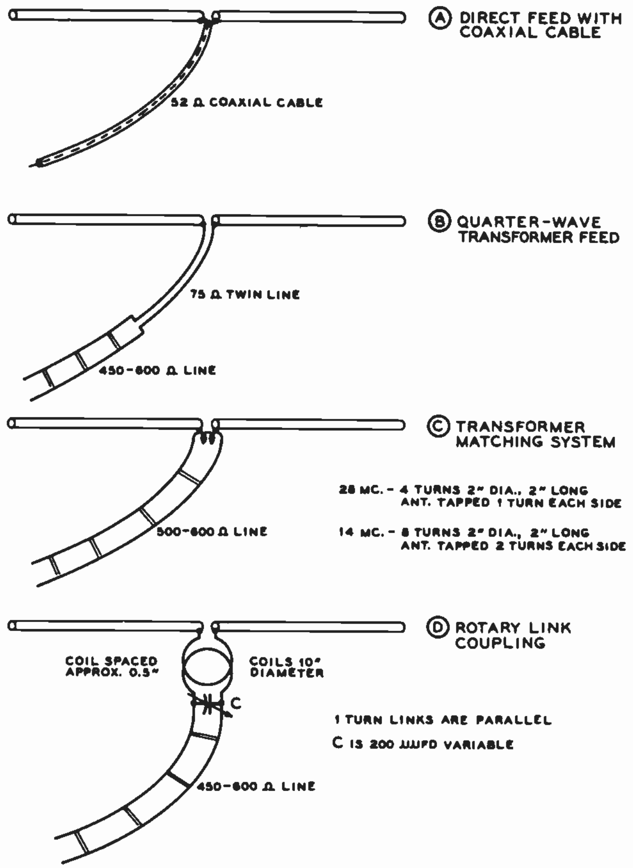


Figure 9
ALTERNATE FEED METHODS WHERE THE DRIVEN ELEMENT MAY BE BROKEN IN THE CENTER

These capacitors should be tuned for minimum SWR on the transmission line. The adjustment of these capacitors should be made at the same time the correct setting of the T-match rods is made as the two adjustments tend to be interlocking. The use of the standing wave meter (described in Test Equipment chapter) is recommended for making these adjustments to the T-match.

Feed Systems Using a Driven Element with Center Feed Four methods of exciting the driven element of a parasitic array are shown in figure 9. The system shown at (A) has proven to be quite satisfactory in the case of an antenna-reflector two-element array or in the case of a three-element array with 0.2 to 0.25 wavelength spacing between the elements of the antenna system. The feed-point impedance of the center of the driven element is close enough to the characteristic impedance of the 52-ohm coaxial cable so that the standing-wave ratio on the 52-ohm coaxial cable is less than 2-to-1. (B) shows an arrangement for feeding an array with a broken driven element from an open-wire line with the aid of a quarter-wave matching transformer. With 465-ohm line from the transmitter to the antenna this system will give a close match to a 12-ohm impedance at the center of the driven element. (C) shows an arrangement which uses an untuned transformer with lumped inductance for matching the transmission line to the center impedance of the driven element.

Rotary Link Coupling In many cases it is desirable to be able to allow the antenna array to rotate continuously without regard to snarling of the feed line. If this is to be done some sort of slip rings or rotary joint must be made in the feed line. One relatively simple method of allowing unrestrained rotation of the antenna is to use the method of rotary link coupling shown in figure 9D. The two cou-

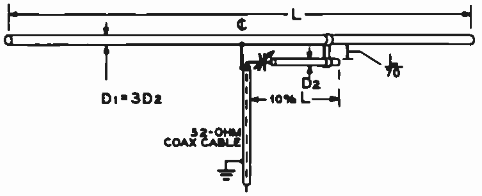


Figure 10
THE GAMMA MATCHING SYSTEM
See text for details of resonating capacitor

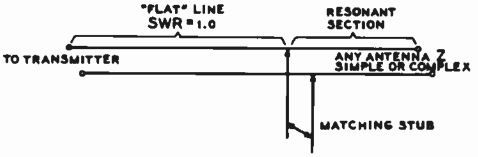


Figure 11
IMPEDANCE MATCHING WITH A CLOSED STUB ON A TWO WIRE TRANSMISSION LINE

pling rings are 10 inches in diameter and are usually constructed of ¼-inch copper tubing supported one from the rotating structure and one from the fixed structure by means of stand-off insulators. The capacitor C in figure 9D is adjusted, after the antenna has been tuned, for minimum standing-wave ratio on the antenna transmission line. The dimensions shown will allow operation with either 14-Mc. or 28-Mc. elements, with appropriate adjustment of the capacitor C. The rings must of course be parallel and must lie in a plane normal to the axis of rotation of the rotating structure.

The Gamma Match The use of coaxial cable to feed the driven element of a yagi array is becoming increasingly popular. One reason for this increased popularity lies in the fact that the TVI-reduction problem is simplified when coaxial feed line is used from the transmitter to the antenna system. Radiation from the feed line is minimized when coaxial cable is used, since the outer conductor of the line may be grounded at several points throughout its length and since the intense field is entirely confined within the outer conductor of the coaxial cable. Other advantages of coaxial cable as the antenna feed line lie in the fact that coaxial cable may be run within the structure of a building without danger, or the cable may be run underground without disturbing its operation. Also, transmitting-type low-pass filters for 52 ohm impedance are more widely available and are less expensive than equivalent filters for two-wire line.

The gamma-match is illustrated in figure 10, and may be looked upon as one-half of a T-match. One resonating capacitor is used, placed in series with the gamma rod. The capacitor should have a capacity of 7 $\mu\mu$fd. per meter of wavelength. For 15-meter operation the capacitor should have a maximum capacity of 105 $\mu\mu$fd. The *length* of the gamma rod determines the impedance transformation between the transmission line and the driven element of the array, and the gamma capacitor tunes out the inductance of the gamma rod. By adjustment of the length of the gamma rod, and the setting of the gamma capacitor, the SWR on the coaxial line may be brought to a very low value at the chosen operating frequency. The use of an Antennascope, described in the Test Equipment chapter is recommended for precise adjustment of the gamma match.

The Matching Stub If an open-wire line is used to feed a low impedance radiator, a section of the transmission line may be employed as a matching stub as shown in figure 11. The matching stub can transform any complex impedance to the characteristic impedance of the transmission line. While it is possible to obtain a perfect match and good performance with either an open stub or a shorted one by observing appropriate dimensions, a shorted stub is much more readily adjusted. Therefore, the following discussion will be confined to the problem of using a closed stub to match a low impedance load to a high impedance transmission line.

If the transmission line is so elevated that adjustment of a "fundamental" shorted stub cannot be accomplished easily from the ground, then the stub length may be increased by exactly one or two electrical half wavelengths, without appreciably affecting its operation.

While the correct position of the shorting bar and the point of attachment of the stub to the line can be determined entirely by experimental methods, the fact that the two adjustments are interdependent or interlocking makes such a cut-and-try procedure a tedious one. Much time can be saved by determining the approximate adjustments required by reference to a chart such as figure 12 and using them as a starter. Usually only a slight "touching up" will produce a perfect match and flat line.

In order to utilize figure 12, it is first necessary to locate accurately a voltage node or current node on the line in the vicinity that

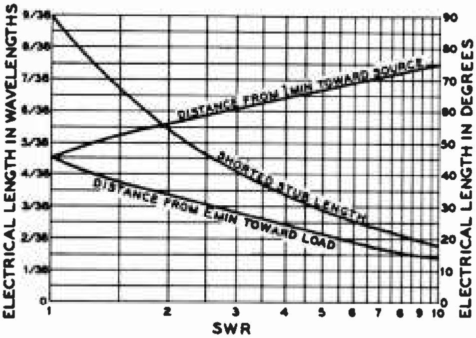


Figure 12

SHORTED STUB LENGTH AND POSITION CHART

From the standing wave ratio and current or voltage null position it is possible to determine the theoretically correct length and position of a shorted stub. In actual practice a slight discrepancy usually will be found between the theoretical and the experimentally optimized dimensions; therefore it may be necessary to "touch up" the dimensions after using the above data as a starting point.

has been decided upon for the stub, and also to determine the SWR.

Stub adjustment becomes more critical as the SWR increases, and under conditions of high SWR the current and voltage nulls are more sharply defined than the current and voltage maxima, or loops. Therefore, it is best to locate either a current null or voltage null, depending upon whether a current indicating device or a voltage indicating device is used to check the standing wave pattern.

The SWR is determined by means of a "directional coupler," or by noting the ratio of E_{max} to E_{min} or I_{max} to I_{min} as read on an indicating device.

It is assumed that the characteristic impedance of the section of line used as a stub is the same as that of the transmission line proper. It is preferable to have the stub section identical to the line physically as well as electrically.

22-5 Unidirectional Driven Arrays

Three types of unidirectional driven arrays are illustrated in figure 13. The array shown in figure 13A is an end-fire system which may be used in place of a parasitic array of similar dimensions when greater frequency coverage than is available with the yagi type is desired. Figure 13B is a combination end-fire and co-

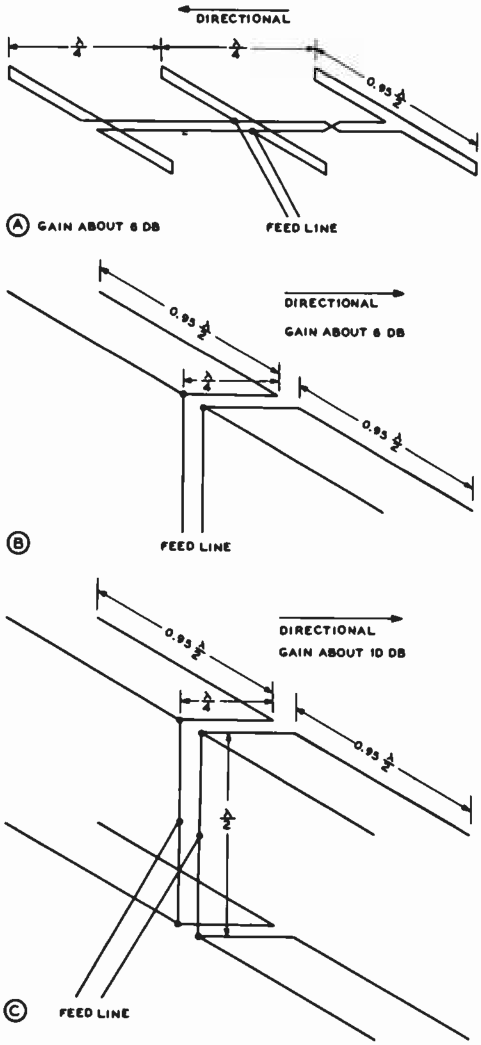


Figure 13

UNIDIRECTIONAL ALL-DRIVEN ARRAYS

A unidirectional all-driven end-fire array is shown at (A). (B) shows an array with two half waves in phase with driven reflectors. A Lazy-H array with driven reflectors is shown at (C). Note that the directivity is through the elements with the greatest total feed-line length in arrays such as shown at (B) and (C).

linear system which will give approximately the same gain as the system of figure 13A, but which requires less boom length and greater total element length. Figure 13C illustrates the familiar lazy-H with driven reflectors (or directors, depending upon the point of view) in a combination which will show wide bandwidth with a considerable amount of forward gain and good front-to-back ratio over the entire frequency coverage.

Unidirectional Stacked Broadside Arrays Three practicable types of unidirectional stacked broadside arrays are shown in figure 14. The first type, shown at figure 14A, is the simple "lazy H" type of antenna with parasitic reflectors for each element. (B) shows a simpler antenna array with a pair of folded dipoles spaced one-half wave vertically, operating with reflectors. In figure 14C is shown a more complex array with six half waves and six reflectors which will give a very worthwhile amount of gain.

In all three of the antenna arrays shown the spacing between the driven elements and the reflectors has been shown as one-quarter wavelength. This has been done to eliminate the requirement for tuning of the reflector, as a result of the fact that a half-wave element spaced exactly one-quarter wave from a driven element will make a unidirectional array when both elements are the same length. Using this procedure will give a gain of 3 db with the reflectors over the gain without the reflectors, with only a moderate decrease in the radiation resistance of the driven element. Actually, the radiation resistance of a half-wave dipole goes down from 73 ohms to 60 ohms when an identical half-wave element is placed one-quarter wave behind it.

A very slight increase in gain for the entire array (about 1 db) may be obtained at the expense of lowered radiation resistance, the necessity for tuning the reflectors, and decreased bandwidth by placing the reflectors 0.15 wavelength behind the driven elements and making them somewhat longer than the driven elements. The radiation resistance of each element will drop approximately to one-half the value obtained with untuned half-wave reflectors spaced one-quarter wave behind the driven elements.

Antenna arrays of the type shown in figure 14 require the use of some sort of lattice work for the supporting structure since the arrays occupy appreciable distance in space in all three planes.

Feed Methods The requirements for the feed systems for antenna arrays of the type shown in figure 14 are less critical than those for the close-spaced parasitic arrays shown in the previous section. This is a natural result of the fact that a larger number of the radiating elements are directly fed with energy, and of the fact that the effective radiation resistance of each of the driven elements of the array is much higher than the feed-point resistance of a parasitic array. As a consequence of this fact, arrays of the type shown in figure 14 can be expected to cover a somewhat greater frequency band for a specified value of standing-wave ratio than the parasitic type of array.

In most cases a simple open-wire line may be coupled to the feed point of the array without any matching system. The standing-wave ratio with such a system of feed will often be less than 2-to-1. However, if a more accurate match between the antenna transmission line and the array is desired a conventional quarter-wave stub, or a quarter-wave matching transformer of appropriate impedance, may be used to obtain a low standing-wave ratio.

22-6 Bi-Directional Rotatable Arrays

The bi-directional type of array is sometimes used on the 28-Mc. and 50-Mc. bands where signals are likely to be coming from only one general direction at a time. Hence the sacrifice of discrimination against signals arriving from the opposite direction is likely to be of little disadvantage. Figure 15 shows two general types of bi-directional arrays. The flat-top beam, which has been described in detail earlier, is well adapted to installation atop a rotating structure. When self-supporting elements are used in the flat-top beam the problem of losses due to insulators at the ends of the elements is somewhat reduced. With a single-section flat-top beam a gain of approximately 4 db can be expected, and with two sections a gain of approximately 6 db can be obtained.

Another type of bi-directional array which has seen less use than it deserves is shown in figure 15B. This type of antenna system has a relatively broad azimuth or horizontal beam, being capable of receiving signals with little diminution in strength over approximately 40°, but it has a quite sharp elevation pattern since substantially all radiation is concentrated at the lower angles of radiation if more than a total of four elements is used in the antenna system. Figure 15B gives the approximate gain over a half-wave dipole at the height of the center of the array which can be expected. Also shown in this figure is a type of "rotating mast" structure which is well suited to rotation of this type of array.

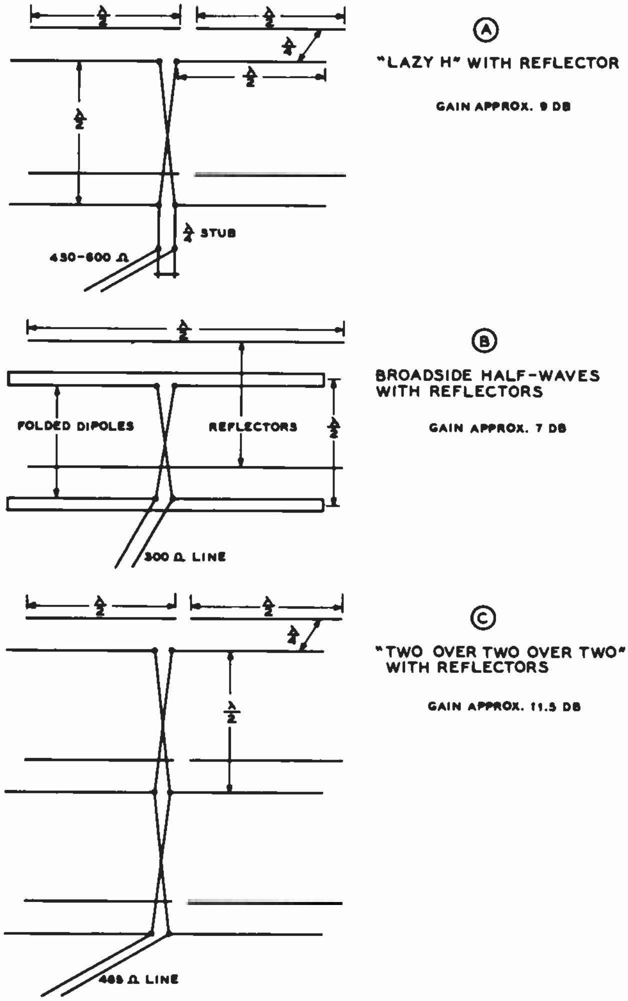


Figure 14
BROADSIDE ARRAYS WITH PARASITIC REFLECTORS

The apparent gain of the arrays illustrated will be greater than the values given due to concentration of the radiated signal at the lower elevation angles.

If six or more elements are used in the type of array shown in figure 15B no matching section will be required between the antenna transmission line and the feed point of the antenna. When only four elements are used the antenna is the familiar "lazy H" and a quarter-wave stub should be used for feeding from the antenna transmission line to the feed point of the antenna system.

If desired, and if mechanical considerations permit, the gain of the arrays shown in figure 15B may be increased by 3 db by placing a half-wave reflector behind each of the elements at a spacing of one-quarter wave. The array then becomes essentially the same as that shown in figure 14C and the same considerations in regard to reflector spacing and tuning will apply. However, the factor that a bi-directional array need be rotated through an angle of less than 180° should be considered in this connection.

22-7 Construction of Rotatable Arrays

A considerable amount of ingenuity may be exercised in the construction of the supporting structure for a rotatable array. Every person has his own ideas as to the best method of construction. Often the most practicable method of construction will be dictated by the

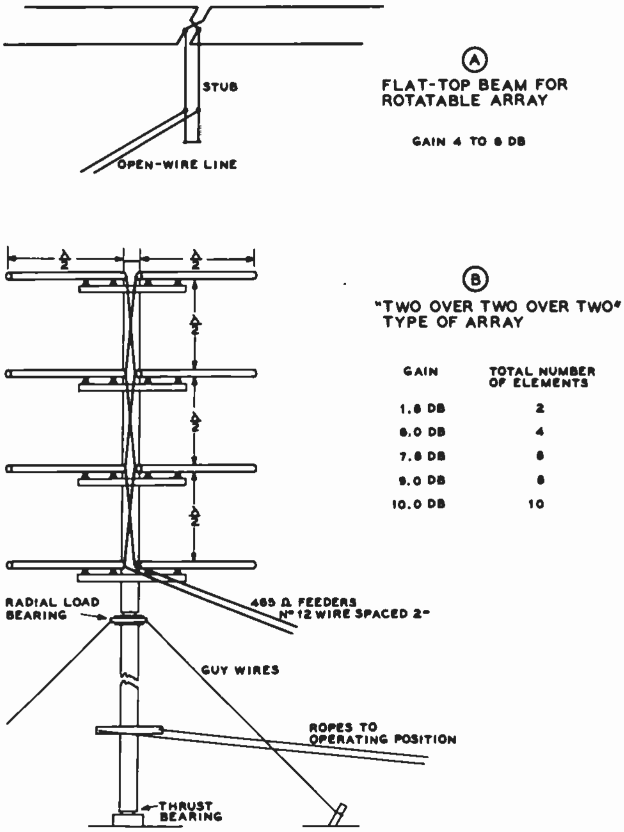


Figure 15
TWO GENERAL TYPES OF BI-DIRECTIONAL ARRAYS

Average gain figures are given for both the flat-top beam type of array and for the broadside-colinear array with different numbers of elements.

availability of certain types of constructional materials. But in any event be sure that sound mechanical engineering principles are used in the design of the supporting structure. There are few things quite as discouraging as the picking up of pieces, repairing of the roof, etc., when a newly constructed rotary comes down in the first strong wind. If the principles of mechanical engineering are understood it is wise to calculate the loads and torques which will exist in the various members of the structure with the highest wind velocity which may be expected in the locality of the installation. If this is not possible it will usually be worth the time and effort to look up a friend who understands these principles.

Radiating Elements One thing more or less standard about the construction of rotatable antenna arrays is the use of dural tubing for the self-supporting elements. Other materials may be used but an alloy known as 24ST has proven over a period of time to be quite satisfactory. Copper tubing is too heavy for a given strength, and steel tubing, unless copper plated, is likely to add an undesirably large loss resistance to the array. Also, steel tubing, even when plated, is not likely to withstand salt atmosphere such as encountered along the seashore for a satisfactory period of time. Do not use a soft aluminum alloy for the elements unless they will be quite short; 24ST is a hard alloy and is best although there are several other alloys ending in "ST" which will be found to be satisfactory. Do not use an alloy ending in "SO" or "S" in a position in the array where structural strength is important, since these letters designate a metal which has not been heat treated for strength and rigidity. However, these softer alloys, and aluminum electrical conduit, may be used for short radiating elements such as would be used for the 50-Mc. band or as interconnecting conductors in a stacked array.

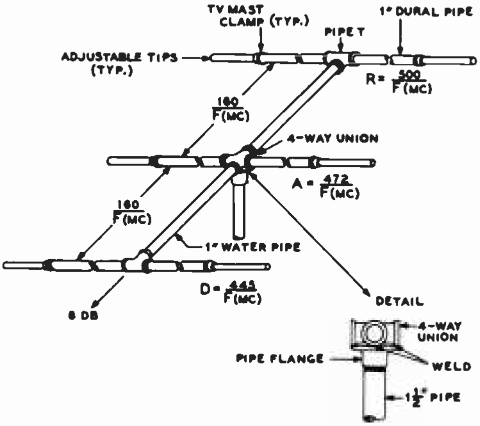


Figure 16

"PLUMBERS DELIGHT" BEAM FOR 21 MC. OR 28 MC. THIS ANTENNA IS FED WITH 52-OHM COAXIAL TRANSMISSION LINE AND THE GAMMA MATCH SYSTEM OF FIGURE 10.

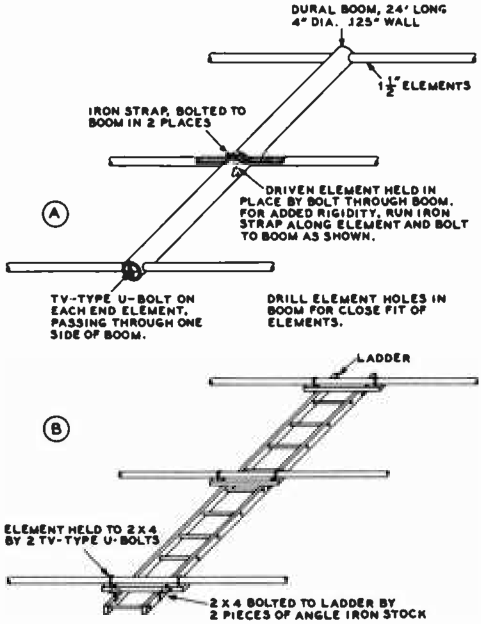


Figure 17

ALTERNATIVE SUPPORTING BOOM ARRANGEMENTS

(A) shows the use of a section of dural tubing for supporting a 20-meter array. At (B) is shown the use of a ladder for supporting a relatively large array.

"Plumber's Delight" Construction It is characteristic of the conventional type of multi-element parasitic array such as discussed previously and outlined that the centers of all the elements are at zero r-f potential with respect to ground. Hence it is possible to use a metallic structure without insulators for supporting the various elements of the array. A 28-Mc. three-element array of this type is shown in figure 16. In this particular array pipe-fitting "T's" have been used at either end to support the 1-inch dural tubing reflector and director, with pieces of standard water pipe as spacers on either side between the parasitic elements and the driven element. The fitting at the center of the structure was made from a four-way pipe union welded to a larger pipe flange. Two opposite sides of the union receive the threaded pipe sections which act as the antenna boom. The two other sides of the union are drilled out to pass the driven element of the array. If one inch dural tubing is used for the parasitic elements and also for the driven element, so-called "one inch" pipe T's and unions may be used in the assembly, since this size water pipe is approximately one inch in inside diameter. A 1½ inch pipe flange is welded to the bottom of the union, and threads into a length of 1½ inch water pipe which is used as the supporting mast. If desired, TV-type mast sections may be used instead of the water pipe mast. This type of construction may be used equally well for the 15-meter band.

Supporting Structures Figure 17 shows two commonly used types of center main boom for a larger array such as is required on the lower-frequency bands. Figure 17A shows a metal-boom type of construction which is quite satisfactory for construction of a plumber's delight type of structure. If the rectangular type of tubing is available it will be found somewhat easier to manage than the round dural tubing, but both types are relatively simple to use in making such a structure. For anchoring the radiating elements to the dural boom either a set of collars on either side of the boom may be used, or bolts may be run through both the boom and the elements. Any of the shunt feeding systems shown in figures 8, or 10 may be used to feed an array of this type.

A conventional ladder makes a satisfactory supporting boom for an array in the general manner illustrated in figure 17B. Ladders are relatively inexpensive, and produce a strong and stable type of mounting platform. The ladder, and for that matter any type of wood supporting structure, should be given several coats of a good grade outside paint to protect it from the elements.

22-8 Tuning the Array

Although satisfactory results may be obtained by pre-cutting the antenna array to the dimensions given earlier in this chapter, the occasion might arise when it is desired to make a check on the operation of the antenna before calling the job complete.

The process of tuning an array may fairly satisfactorily be divided into two more or less distinct steps: the actual tuning of the array for best front-to-back ratio or for maximum forward gain, and the project of obtaining the best possible impedance match between the antenna transmission line and the feed point of the array.

Tuning the Array Proper The actual tuning of the array for best front-to-back ratio or maximum forward gain may best be accomplished with the aid of a low-power transmitter feeding a dipole antenna (polarized the same as the array being tuned) at least four or five wavelengths away from the antenna being tuned and located at the same elevation as that of the antenna under test. A calibrated field-strength meter of the remote-indicating type is then coupled to the feed point of the antenna array being tuned. The transmissions from the portable transmitter should be made as short as possible and the call sign of the station making the test should be transmitted at least every ten minutes.

It is, of course, possible to tune an array with the receiver connected to it and with a station a mile or two away making transmissions on your request. But this method is more cumbersome and is not likely to give complete satisfaction. It is also possible to carry out the tuning process with the transmitter connected to the array and with the field-strength meter connected to the remote dipole antenna. In this event the indicating instrument of the remote-indicating field-strength meter should be visible from the position where the elements are being tuned. However, when the array is being tuned with the transmitter connected to it there is always the problem of making continual adjustments to the transmitter so that a constant amount of power will be fed to the array under test. Also, if you use this system, use very low power (5 or 10 watts of power is usually sufficient) and make sure that the antenna transmission line is effectively grounded as far as d-c plate voltage is concerned. The use of the method described in the previous paragraph of course eliminates these problems.

One satisfactory method for tuning the array proper, assuming that it is a system with several parasitic elements, is to set the directors to the dimensions given in figure 5 and then to adjust the reflector for maximum forward signal. Then the first director should be varied in length until maximum forward signal is obtained, and so on if additional directors are used. Then the array may be reversed in direction and the reflector adjusted for best front-to-back ratio. Subsequent small adjustments may then be made in both the directors and the reflector for best forward signal with a reasonable ratio of front-to-back signal. The adjustments in the directors and the reflector will be found to be interdependent to a certain degree, but if small adjustments are made after the preliminary tuning process a satisfactory set of adjustments for maximum performance will be obtained. It is usually best to make the end sections of the elements smaller in diameter so that they will slip inside the larger tubing sections. The smaller sliding sections may be clamped inside the larger main sections.

In making the adjustments described, it is best to have the rectifying element of the remote-indicating field-strength meter directly at the feed point of the array, with a resistor at the feed point of the estimated value of feed-point impedance for the array.

Matching to the Antenna Transmission Line The problem of matching the impedance of the antenna transmission line to the array is much simplified if the pro-

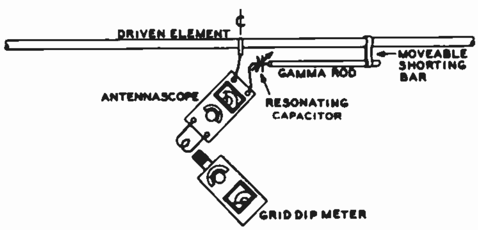
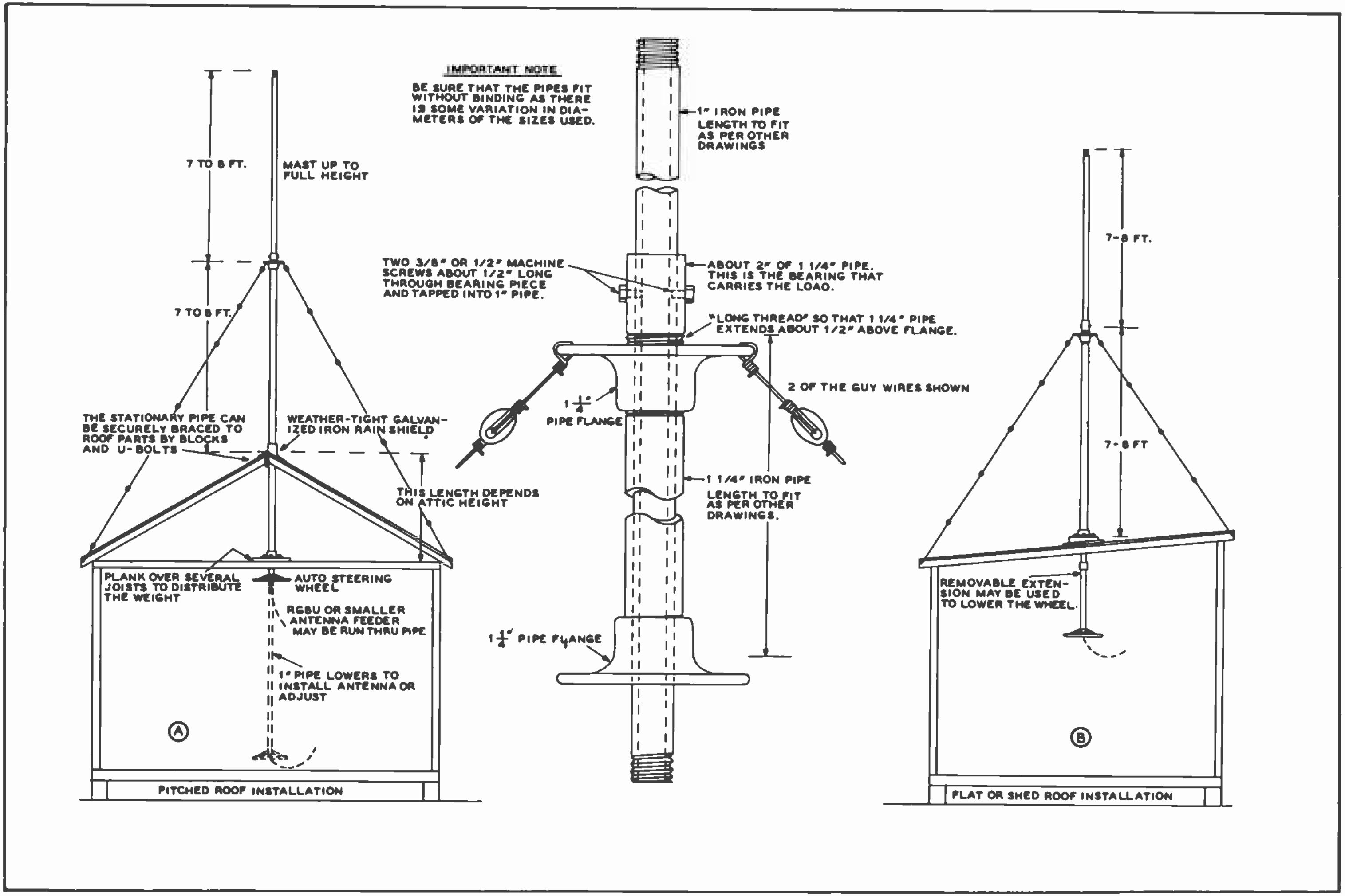


Figure 18

ADJUSTMENT OF GAMMA MATCH BY USE OF ANTENNASCOPE AND GRID-DIP METER



IMPORTANT NOTE
BE SURE THAT THE PIPES FIT WITHOUT BINDING AS THERE IS SOME VARIATION IN DIAMETERS OF THE SIZES USED.
7 TO 8 FT.
MAST UP TO FULL HEIGHT
7 TO 8 FT.
THE STATIONARY PIPE CAN BE SECURELY BRACED TO ROOF PARTS BY BLOCKS AND U-BOLTS
WEATHER-TIGHT GALVANIZED IRON RAIN SHIELD
THIS LENGTH DEPENDS ON ATTIC HEIGHT
PLANK OVER SEVERAL JOISTS TO DISTRIBUTE THE WEIGHT
AUTO STEERING WHEEL
RG8U OR SMALLER ANTENNA FEEDER MAY BE RUN THRU PIPE
1" PIPE LOWERS TO INSTALL ANTENNA OR ADJUST
A
PITCHED ROOF INSTALLATION
1" IRON PIPE LENGTH TO FIT AS PER OTHER DRAWINGS
TWO 3/8" OR 1/2" MACHINE SCREWS ABOUT 1/2" LONG THROUGH BEARING PIECE AND TAPPED INTO 1" PIPE.
ABOUT 2" OF 1 1/4" PIPE. THIS IS THE BEARING THAT CARRIES THE LOAD.
"LONG THREAD" SO THAT 1 1/4" PIPE EXTENDS ABOUT 1/2" ABOVE FLANGE.
2 OF THE GUY WIRES SHOWN
1 1/4" PIPE FLANGE
1 1/4" IRON PIPE LENGTH TO FIT AS PER OTHER DRAWINGS.
1 1/4" PIPE FLANGE
7-8 FT.
7-8 FT
REMOVABLE EXTENSION MAY BE USED TO LOWER THE WHEEL.
B
FLAT OR SHED ROOF INSTALLATION

cess of tuning the array is made a substantially separate process as just described. *After* the tuning operation is complete, the resonant frequency of the driven element of the antenna should be checked, directly at the center of the driven element if practicable, with a grid-dip meter. It is important that the resonant frequency of the antenna be at the *center* of the frequency band to be covered. If the resonant frequency is found to be much different from the desired frequency, the length of the driven element of the array should be altered until this condition exists. A relatively small change in the length of the driven element will have only a second order effect on the tuning of the parasitic elements of the array. Hence, a moderate change in the length of the driven element may be made without repeating the tuning process for the parasitic elements.

When the resonant frequency of the antenna system is correct, the antenna transmission line, with impedance-matching device or network between the line and antenna feed point, is then attached to the array and coupled to a low-power exciter unit or transmitter. Then, preferably, a standing-wave meter is connected in series with the antenna transmission line at a point relatively much more close to the transmitter than to the antenna. However, for best indication there should be 10 to 15 feet of line between the transmitter and the standing-wave meter. If a standing-wave meter is not available the standing-wave ratio may be checked approximately by means of a neon lamp or a short fluorescent tube if twin transmission line is being used, or it may be checked with a thermomilliammeter and a loop, a neon lamp, or an r-f ammeter and a pair of clips spaced a fixed distance for clipping onto one wire of a two-wire open line.

If the standing-wave ratio is below 1.5 to 1 it is satisfactory to leave the installation as it is. If the ratio is greater than this range it will be best when twin line or coaxial line is being used, and advisable with open-wire line, to attempt to decrease the s.w.r.

It must be remembered that no adjustments made at the *transmitter* end of the transmission line will alter the SWR on the line. All adjustments to better the SWR must be made at the *antenna* end of the line and to the device which performs the impedance transformation necessary to match the characteristic impedance of the antenna to that of the transmission line.

Before any adjustments to the matching system are made, the resonant frequency of the driven element must be ascertained, as explained previously. If all adjustments to correct impedance mismatch are made at this frequency, the problem of reactance termination of the transmission line is eliminated, greatly simplifying the problem. The following steps should be taken to adjust the impedance transformation:

1. The output impedance of the matching device should be measured. An Antennascope and a grid-dip oscillator are required for this step. The Antennascope is connected to the output terminals of the matching device. If the driven element is a folded dipole, the Antennascope connects directly to the split section of the dipole. If a gamma match or T-match are used, the Antennascope connects to the transmission-line end of the device. If a Q-section is used, the Antennascope connects to the bottom end of the section. The grid-dip oscillator is coupled to the input terminals of the Antennascope as shown in figure 18.
2. The grid-dip oscillator is tuned to the resonant frequency of the antenna, which

Figure 19

ALL-PIPE ROTATING MAST STRUCTURE FOR ROOF INSTALLATION

An installation suitable for a building with a pitched roof is shown at (A). At (B) is shown a similar installation for a flat or shed roof. The arrangement as shown is strong enough to support a lightweight 3-element 28-Mc. array and a light 3-element 50-Mc. array above the 28-Mc. array on the end of a 4-foot length of ½-inch pipe.

The lengths of pipe shown were chosen so that when the system is in the lowered position one can stand on a household ladder and put the beam in position atop the rotating pipe. The lengths may safely be revised upward somewhat if the array is of a particularly lightweight design with low wind resistance.

Just before the mast is installed it is a good idea to give the rotating pipe a good smearing of cup grease or waterproof pump grease. To get the lip of the top of the stationary section of 1¼-inch pipe to project above the flange plate, it will be necessary to have a plumbing shop cut a slightly deeper thread inside the flange plate, as well as cutting an unusually long thread on the end of the 1¼-inch pipe. It is relatively easy to waterproof this assembly through the roof since the 1¼-inch pipe is stationary at all times. Be sure to use pipe compound on all the joints and then really tighten these joints with a pair of pipe wrenches.

has been determined previously, and the Antennascope control is turned for a null reading on the meter of the Antennascope. The impedance presented to the Antennascope by the matching device may be read directly on the calibrated dial of the Antennascope.

3. Adjustments should be made to the matching device to present the desired impedance transformation to the Antennascope. If a folded dipole is used as the driven element, the transformation ratio of the dipole must be varied as explained previously in this chapter to provide a more exact match. If a T-match or gamma match system is used, the length of the matching rod may be changed to effect a proper match. If the Antennascope ohmic reading is *lower* than the desired reading, the length of the matching rod should be *increased*. If the Antennascope reading is higher than the desired reading, the length of the matching rod should be *decreased*. After each change in length of the matching rod, the series capacitor in the matching system should be re-resonated for best null on the meter of the Antennascope.

Raising and Lowering the Array A practical problem always present when tuning up and matching an array is the physical location of the structure. If the array is atop the mast it is inaccessible for adjustment, and if it is located on stepladders where it can be adjusted easily it cannot be rotated. One encouraging factor in this situation is the fact that experience has shown that if the array is placed 8 or 10 feet above ground on some stepladders for the preliminary tuning process, the raising of the system to its full height will not produce a serious change in the adjustments. So it is usually possible to make preliminary adjustments with the system located slightly greater than head height above ground, and then to raise the antenna to a position where it may be rotated for final adjustments. If the position of the sliding sections as determined near the ground is marked so that the adjustments will not be lost, the array may be raised to rotatable height and the fastening clamps left loose enough so that the elements may be slid in by means of a long bamboo pole. After a series of trials a satisfactory set of lengths can be obtained. But the end results usually come so close to the figures given in figure 5 that a subsequent array is usually cut to the dimensions given and installed as-is.

The matching process does not require rotation, but it does require that the antenna proper be located at as nearly its normal oper-

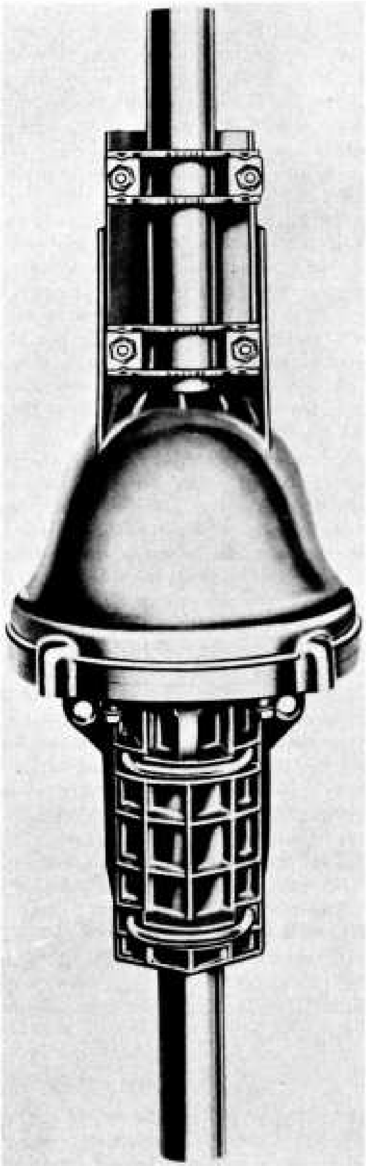


Figure 20

HEAVY DUTY TV ROTATOR SUITABLE FOR 10 AND 15-METER BEAMS

The Cornell-Dubilier type TR-4 television rotor has sufficiently heavy motor and gearing system to withstand the weight of a light amateur array under the buffeting of heavy winds. This rotor may be used with miniature 20-meter loaded beams.

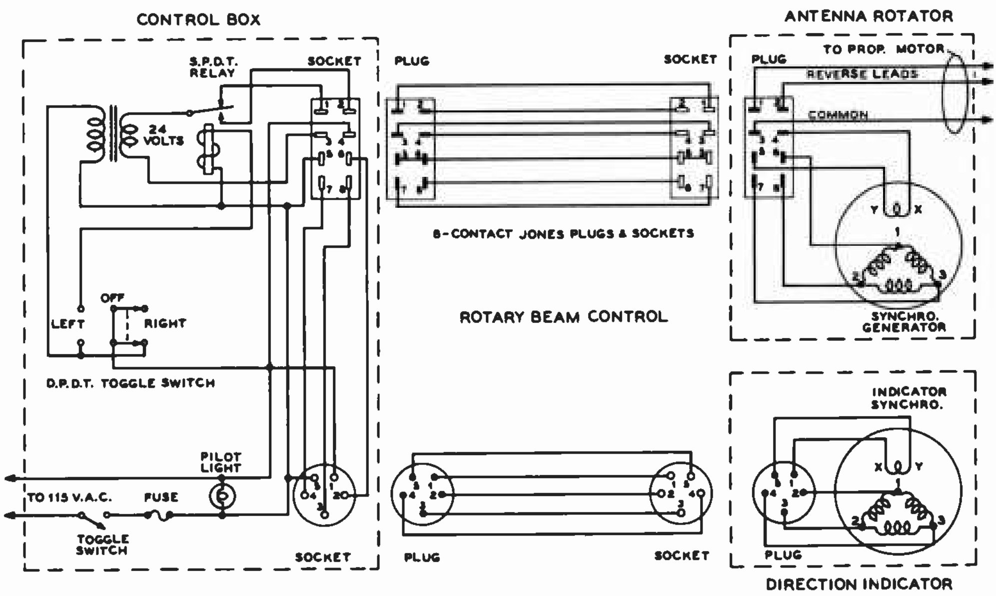


Figure 21

SCHEMATIC OF A COMPLETE ANTENNA CONTROL SYSTEM

ating position as possible. However, on a particular installation the positions of the current minimums on the transmission line near the transmitter may be checked with the array in the air, and then the array may be lowered to ascertain whether or not the positions of these points have moved. If they have not, and in most cases if the feeder line is strung out back and forth well above ground as the antenna is lowered they will not change, the positions of the last few toward the antenna itself may be determined. Then the calculation of the matching quarter-wave section may be made, the section installed, the standing-wave ratio again checked, and the antenna re-installed in its final location.

22-9 Antenna Rotation Systems

Structures for the rotation of antenna arrays may be divided into two general classes: the rotating mast and the rotating platform. The rotating mast is especially suitable where the transmitting equipment is installed in the garage or some structure away from the main house. Such an installation is shown in figure 19. A very satisfactory rotation mechanism is obtained by the use of a large steering wheel located on the bottom pipe of the rotating mast, with the thrust bearing for the structure located above the roof.

If the rotating mast is located a distance from the operating position, a system of pulleys and drive rope may be used to turn the antenna, or a slow speed electric motor may be employed.

The rotating platform system is best if a tower or telephone pole is to be used for antenna support. A number of excellent rotating platform devices are available on the market for varying prices. The larger and more expensive rotating devices are suitable for the rotaof a rather sizeable array for the 14-Mc. band while the smaller structures, such as those designed for rotating a TV antenna are designed for less load and should be used only with a 28-Mc. or 50-Mc. array. Most common practice is to install the rotating device atop a platform built at the top of a telephone pole or on the top of a lattice mast of sizeable cross section so that the mast will be self-supporting and capable of withstanding the torque imposed upon it by the rotating platform.

A *heavy duty* TV rotator suitable for rotation of 6, 10 or 15 meter arrays is shown in figure 20. This rotator may also be used with some of the miniature 20 meter rotary beams now available on the market.

22-10 Indication of Direction

The most satisfactory method for indicating the direction of transmission of a rotatable array is that which uses Selsyns or synchros for the transmission of the data from the rotating structure to the indicating pointer at the operating position. A number of synchros and Selsyns of various types are available on the surplus market. Some of them are designed for operation on 115 volts at 60 cycles, some are designed for operation on 60 cycles but at a lowered voltage, and some are designed for operation from 400-cycle or 800-cycle energy. This latter type of high-frequency synchro is the most generally available type, and the high-frequency units are smaller and lighter than the 60-cycle units. Since the indicating synchro must deliver an almost negligible amount of power to the pointer which it drives, the high-frequency types will operate quite satisfactorily from 60-cycle power if the voltage on them is reduced to somewhere between 6.3 and 20 volts. In the case of many of the units available, a connection sheet is provided along with a recommendation in regard to the operating voltage when they are run on 60 cycles. In any event the operating voltage should be held as low as it may be and still give satisfactory transmission of data from the antenna to the operating position. Certainly it should not be necessary to run such a voltage on the units that they become overheated.

A suitable Selsyn indicating system is shown in figure 21.

Systems using a potentiometer capable of continuous rotation and a milliammeter, along with a battery or other source of direct current, may also be used for the indication of direction. A commercially-available potentiometer (Ohmite RB-2) may be used in conjunction with a 0-1 d-c milliammeter having a hand-calibrated scale for direction indication.

CHAPTER TWENTY THREE

Mobile Equipment and Installation

Mobile operation is permitted on all amateur bands. Tremendous impetus to this phase of the hobby was given by the suitable design of compact mobile equipment. Complete mobile installations may be purchased as packaged units, or the whole mobile station may be home built, according to the whim of the operator.

The problems involved in achieving a satisfactory two-way installation vary somewhat with the band, but many of the problems are common to all bands. For instance, ignition noise is more troublesome on 10 meters than on 75 meters, but on the other hand an efficient antenna system is much more easily accomplished on 10 meters than on 75 meters. Also, obtaining a worthwhile amount of transmitter output without excessive battery drain is a problem on all bands.

23-1 Mobile Reception

When a broadcast receiver is in the car, the most practical receiving arrangement involves a converter feeding into the auto set. The advantages of good selectivity with good image rejection obtainable from a double conversion superheterodyne are achieved in most cases without excessive "birdie" troubles, a common difficulty with a double conversion superheterodyne constructed as an integral receiver in one cabinet. However, it is important that the b-c receiver employ an r-f stage in order to provide adequate isolation between the converter and the high frequency oscillator in the b-c receiver. The r-f stage also is desirable from the standpoint of image rejection if the converter does not employ a tuned output circuit (tuned to the frequency of the auto set, usually about 1500 kc.). A few of the late model auto receivers, even in the better makes, do not employ an r-f stage.

The usual procedure is to obtain converter plate voltage from the auto receiver. Experience has shown that if the converter does not draw more than about 15 or at most 20 ma. total plate current no damage to the auto set or loss in performance will occur other than a slight reduction in vibrator life. The converter drain can be minimized by avoiding a voltage regulator tube on the converter h-f oscillator. On 10 meters and lower frequencies it is possible to design an oscillator with sufficient stability so that no voltage regulator is required in the converter.

With some cars satisfactory 75-meter operation can be obtained without a noise clipper if resistor type spark plugs (such as those made by Autolite) are employed. However, a noise clipper is helpful if not absolutely necessary, and it is recommended that a noise clipper be installed without confirming the necessity therefor. It has been found that quiet reception sometimes may be obtained on 75 meters simply by the use of resistor type plugs, but after a few thousand miles these plugs often become less effective and no longer do a fully adequate job. Also, a noise clipper insures against ignition noise from passing trucks and "un-suppressed" cars. On 10 meters a noise clipper is a "must" in any case.

Modifying the Auto Receiver There are certain things that should be done to the auto set when it is to be used with a converter, and they might as well be done all at the same time, because "dropping" an auto receiver and getting into the chassis to work on it takes quite a little time.

First, however, check the circuit of the auto receiver to see whether it is one of the few receivers which employ circuits which complicate connection of a noise clipper or a converter. If the receiver is yet to be purchased, it is well to investigate these points ahead of time.

If the receiver uses a negative B resistor strip for bias (as evidenced by the cathode of the audio output stage being grounded), then the additional plate current drain of the converter will upset the bias voltages on the various stages and probably cause trouble. Because the converter is not on all the time, it is not practical simply to alter the resistance of the bias strip, and major modification of the receiver probably will be required.

The best type of receiver for attachment of a converter and noise clipper uses an r-f stage; permeability tuning; single unit construction (except possibly for the speaker); push button tuning rather than a tuning motor; a high vacuum rectifier such as a 6X4 (rather than an 0Z4 or a synchronous rectifier); a 6SQ7 (or miniature or Loctal equivalent) with *grounded cathode* as second detector, first audio, and a.v.c.; power supply negative grounded directly (no common bias strip); a PM speaker (to minimize battery drain); and an internal r-f gain control (indicating plenty of built-in reserve gain which may be called upon if necessary). Many current model auto radios have all of the foregoing features, and numerous models have most of them, something to keep in mind if the set is yet to be purchased.

Noise Limiters A noise limiter either may be built into the set or purchased as a commercially manufactured unit for "outboard" connection via shielded wires. If the receiver employs a 6SQ7 (or Loctal or miniature equivalent) in a conventional circuit, it is a simple matter to build in a noise clipper by

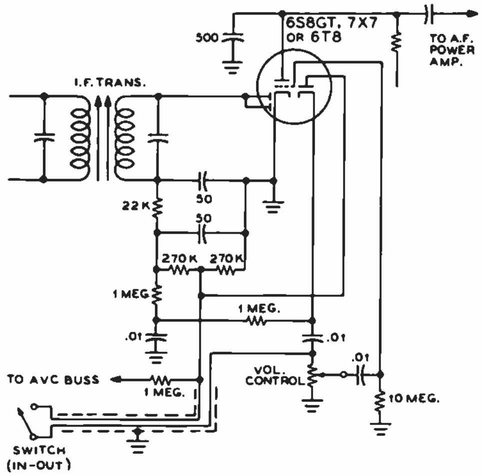


Figure 1

SERIES-GATE NOISE LIMITER FOR AUTO RECEIVER

Auto receivers using a 6SQ7, 7B6, 7X7, or 6AT6 as second detector and a.v.c. can be converted to the above circuit with but few wiring changes. The circuit has the advantage of not requiring an additional tube socket for the limiter diode.

substituting a 6S8 octal, 7X7 Loctal, or a 6T8 9-pin miniature as shown in figure 1. When substituting a 6T8 for a 6AT6 or similar 7-pin miniature, the socket must be changed to a 9-pin miniature type. This requires reaming the socket hole slightly.

If the receiver employs cathode bias on the 6SQ7 (or equivalent), and perhaps delayed a.v.c., the circuit usually can be changed to the grounded-cathode circuit of figure 1 without encountering trouble.

Some receivers take the r-f excitation for the a-v-c diode from the plate of the i-f stage. In this case, leave the a.v.c. alone and ignore the a-v-c buss connection shown in figure 1 (eliminating the 1-megohm decoupling resistor). If the set uses a separate a-v-c diode which receives r-f excitation via a small capacitor connected to the detector diode, then simply change the circuit to correspond to figure 1.

In case anyone might be considering the use of a crystal diode as a noise limiter in conjunction with the tube already in the set, it might be well to point out that crystal diodes perform quite poorly in series-gate noise clippers of the type shown.

It will be observed that no tone control is shown. Multi-position tone controls tied in with the second detector circuit often permit excessive "leak through." Hence it is recommended that the tone control components be completely removed unless they are confined to the grid of the a-f output stage. If removed, the highs can be attenuated any desired amount by connecting a mica capacitor from plate to screen on the output stage. Ordinarily from .005 to .01 μfd. will provide a good compromise between fidelity and reduction of background hiss on weak signals.

Usually the switch SW will have to be mounted some distance from the noise limiter components. If the leads to the switch are over approximately 1½ inches long, a piece of shield braid should be slipped over them and grounded. The same applies to the "hot" leads to the volume control if not already shielded. Closing the switch disables the limiter. This may be desirable for reducing distortion on broadcast reception or when checking the intensity of ignition noise to determine the effectiveness of suppression measures taken on the car. The switch also permits one to check the effectiveness of the noise clipper.

The 22,000-ohm decoupling resistor at the bottom end of the i-f transformer secondary is not critical, and if some other value already is incorporated inside the shield can it may be left alone so long as it is not over 47,000 ohms, a common value. Higher values must be replaced with a lower value even if it requires a can opener, because anything over 47,000 ohms will result in excessive loss in gain. There is some loss in a-f gain inherent in this type of limiter anyhow (slightly over 6 db), and it is important to minimize any additional loss.

It is important that the total amount of capacitance in the RC decoupling (r-f) filter not exceed about 100 μμfd. With a value much greater than this "pulse stretching" will occur and the effectiveness of the noise clipper will be reduced. Excessive capacitance will reduce the amplitude and increase the duration of the ignition pulses before they reach the clipper. The reduction in pulse amplitude accomplishes no good since the pulses are fed to the clipper anyhow, but the greater duration of the lengthened pulses increases the audibility and the blanking interval associated with each pulse. If a shielded wire to an external clipper is employed, the r-f by-pass on the "low" side of the RC filter may be eliminated since the capacitance of a few feet of shielded wire will accomplish the same result as the by-pass capacitor.

The switch SW is connected in such a manner that there is practically no change in gain with the limiter in or out. If the auto set does not have any reserve gain and more gain is needed on weak broadcast signals, the switch can be connected from the hot side of the volume control to the junction of the 22,000, 270,000 and 1 megohm resistors instead of as shown. This will provide approximately 6 db more gain when the clipper is switched out.

Many late model receivers are provided with an internal r-f gain control in the cathode of the r-f and/or i-f stage. This control should be advanced full on to provide better noise limiter action and make up for the loss in audio gain introduced by the noise clipper.

Installation of the noise clipper often detunes the secondary of the last i-f transformer. This should be repeaked before the set is permanently replaced in the car unless the trimmer is accessible with the set mounted in place.

Additional clipper circuits will be found in Chapter Ten of this Handbook.

Selectivity While not of serious concern on 10 meters, the lack of selectivity exhibited by a typical auto receiver will result in QRM difficulty on 20 and 75 meters. A typical auto set has only two i-f transformers of relatively low-Q design, and the second one is loaded by the diode detector. The skirt selectivity often is so poor that a strong local will depress the a.v.c. when listening to a weak station as much as 15 kc. different in frequency.

One solution is to add an outboard i-f stage employing two good quality double-tuned transformers (not the midget variety) connected "back-to-back" through a small coupling capacitance. The amplifier tube (such as a 6BA6) should be biased to the point where the gain of the outboard unit is relatively small (1 or 2), assuming that the receiver already has adequate gain. If additional gain is needed, it may be provided by the outboard unit. Low-capacitance shielded cable should be used to couple into and out of the outboard unit, and the unit itself should be thoroughly shielded.

Such an outboard unit will sharpen the nose selectivity slightly and the skirt selectivity greatly. Operation then will be comparable to a home-station communications receiver, though selectivity will not be as good as a receiver employing a 50-kc. or 85-kc. "Q5'er."

Obtaining Power for the Converter While the set is on the bench for installation of the noise clipper, provision should be made for obtaining filament and plate voltage for the converter, and for the exciter and speech amplifier of the transmitter, if such an arrangement is to be used. To permit removal of either the converter or the auto set from the car without removing the other, a connector should be provided. The best method

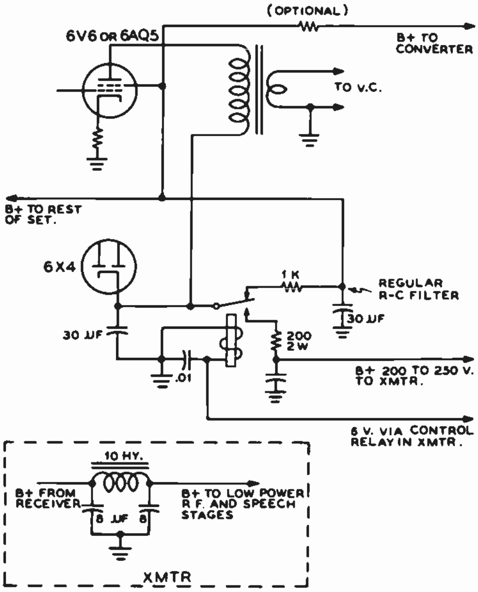


Figure 2

USING THE RECEIVER PLATE SUPPLY FOR THE TRANSMITTER

This circuit silences the receiver on transmit, and in addition makes it possible to use the receiver plate supply for feeding the exciter and speech amplifier stages in the transmitter.

is to mount a small receptacle on the receiver cabinet or chassis, making connection via a matching plug. An Amphenol type 77-26 receptacle is compact enough to fit in a very small space and allows four connections (including ground for the shield braid). The matching plug is a type 70-26.

To avoid the possibility of vibrator hash being fed into the converter via the heater and plate voltage supply leads, it is important that the heater and plate voltages be taken from points well removed from the power supply portion of the auto receiver. If a single-ended audio output stage is employed, a safe place to obtain these voltages is at this tube socket, the high voltage for the converter being taken from the screen. In the case of a push-pull output stage, however, the screens sometimes are fed from the input side of the power supply filter. The ripple at this point, while sufficiently low for a push-pull audio output stage, is not adequate for a converter without additional filtering. If the schematic shows that the screens of a push-pull stage are connected to the input side instead of the output side of the power supply filter (usually two electrolytics straddling a resistor in an R-C filter), then follow the output of the filter over into the r-f portion of the set and pick it up there at a convenient point, before it goes through any additional series dropping or isolating resistors, as shown in figure 2.

The voltage at the output of the filter usually runs from 200 to 250 volts with typical converter drain and the motor not running. This will increase perhaps 10 per cent when the generator is charging. The converter drain will drop the B voltage slightly at the output of the filter, perhaps 15 to 25 volts, but this reduction is not enough to have a noticeable effect upon the operation of the receiver. If the B voltage is higher than desirable or necessary for proper operation of the converter, a 2-watt carbon resistor of suitable resistance should be inserted in series with the plate voltage lead to the power receptacle. Usually something between 2200 and 4700 ohms will be found about right.

Receiver Disabling on Transmit When the battery drain is high on transmit, as is the case when a PE-103A dynamotor is run at maximum rating and other drains such as the transmitter heaters and auto headlights must be considered, it is desirable to disable the vibrator power supply in the receiver during transmissions. The vibrator power supply usually draws several amperes, and as the receiver must be disabled in some manner anyhow during transmissions, opening the 6-volt supply to the vibrator serves both purposes. It has the further advantage of introducing a slight delay in the receiver recovery, due to the inertia of the power supply filter, thus avoiding the possibility of a feedback "yoop" when switching from transmit to receive.

To avoid troubles from vibrator hash, it is best to open the ground lead from the vibrator by means of a midget s.p.d.t. 6-volt relay and thus isolate the vibrator circuit from the external control and switching circuit wires. The relay is hooked up as shown in figure 3; Standard 8-ampere contacts will be adequate for this application.

The relay should be mounted as close to the vibrator as practicable. Ground one of the coil terminals and run a shielded wire from the other coil terminal to one of the power receptacle connections, grounding the shield at both ends. By-pass each end of this wire to ground with .01 µfd., using the shortest possible leads. A lead is run from the corresponding terminal on the mating plug to the control circuits, to be discussed later.

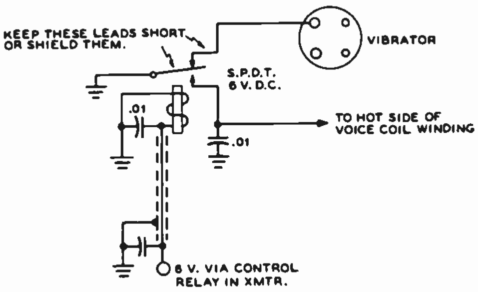


Figure 3

METHOD OF ELIMINATING THE BATTERY DRAIN OF THE RECEIVER VIBRATOR PACK DURING TRANSMISSION

If the receiver chassis has room for a midget s.p.d.t. relay, the above arrangement not only silences the receiver on transmit but saves several amperes battery drain.

If the normally open contact on the relay is connected to the hot side of the voice coil winding as shown in figure 3 (assuming one side of the voice coil is grounded in accordance with usual practice), the receiver will be killed instantly when switching from receive to transmit, in spite of the fact that the power supply filter in the receiver takes a moment to discharge. However, if a "slow start" power supply (such as a dynamotor or a vibrator pack with a large filter) is used with the transmitter, shorting the voice coil probably will not be required.

Using the Receiver Plate Supply On Transmit An alternative and highly recommended procedure is to make use of the receiver B supply on transmit, instead of disabling it. One disadvantage of the popular PE-103A dynamotor is the fact that its 450-500 volt output is too high for the low power r-f and speech stages of the transmitter. Dropping this voltage to a more suitable value of approximately 250 volts by means of dropping resistors is wasteful of power, besides causing the plate voltage on the oscillator and any buffer stages to vary widely with tuning. By means of a midget 6-volt s.p.d.t. relay mounted in the receiver, connected as shown in figure 2, the B supply of the auto set is used to power the oscillator and other low power stages (and possibly screen voltage on the modulator). On transmit the B voltage is removed from the receiver and converter, automatically silencing the receiver. When switching to receive the transmitter oscillator is killed instantly, thus avoiding trouble from dynamotor "carry over."

The efficiency of this arrangement is good because the current drain on the main high voltage supply for the modulated amplifier and modulator plate(s) is reduced by the amount of current borrowed from the receiver. At least 80 ma. can be drawn from practically all auto sets, at least for a short period, without damage.

It will be noted that with the arrangement of figure 2, plate voltage is supplied to the audio output stage at all times. However, when the screen voltage is removed, the plate current drops practically to zero.

The 200-ohm resistor in series with the normally open contact is to prevent excessive sparking when the contacts close. If the relay feeds directly into a filter choke or large capacitor there will be excessive sparking at the contacts. Even with the arrangement shown, there will be considerable sparking at the contacts; but relay contacts can stand such sparking quite a while, even on d.c., before becoming worn or pitted enough to require attention. The 200-ohm resistor also serves to increase the effectiveness of the .01-μfd. r-f by-pass capacitor.

Auxiliary Antenna Trimmer One other modification of the auto receiver which may or may not be desirable depending upon the circumstances is the addition of an auxiliary antenna trimmer capacitor. If the converter uses an untuned output circuit and the antenna trimmer on the auto set is peaked with the converter cut in, then it is quite likely that the trimmer adjustment will not be optimum for broadcast-band reception when the converter is cut out. For reception of strong broadcast band signals this usually will not be serious, but where reception of weak broadcast signals is desired the loss in gain often cannot be tolerated, especially in view of the fact that the additional length of antenna cable required for the converter installation tends to reduce the strength of broadcast band signals.

If the converter has considerable reserve gain, it may be practicable to peak the antenna trimmer on the auto set for broadcast-band reception rather than resonating it to the converter output circuit. But oftentimes this results in insufficient converter gain, excessive image troubles from loud local amateur stations, or both.

The difficulty can be circumvented by incorporation of an auxiliary antenna trimmer connected from the "hot" antenna lead on the auto receiver to ground, with a switch in series for cutting it in or out. This capacitor and switch can be connected across either the converter end or the set end of the cable between the converter and receiver. This auxiliary trimmer should have a range of about 3 to 50 $\mu\mu$fd., and may be of the inexpensive compression mica type.

With the trimmer cut out and the converter turned off (by-passed by the "in-out" switch), peak the regular antenna trimmer on the auto set at about 1400 kc. Then turn on the converter, with the receiver tuned to 1500 kc., switch in the auxiliary trimmer, and peak this trimmer for maximum background noise. The auxiliary trimmer then can be left switched in at all times except when receiving very weak broadcast band signals.

Some auto sets, particularly certain General Motors custom receivers, employ a high-Q high-impedance input circuit which is very critical as to antenna capacitance. Unless the shunt capacitance of the antenna (including cable) approximates that of the antenna installation for which the set was designed, the antenna trimmer on the auto set cannot be made to hit resonance with the converter cut out. This is particularly true when a long antenna cable is used to reach a whip mounted at the rear of the car. Usually the condition can be corrected by unsoldering the internal connection to the antenna terminal connector on the auto set and inserting in series a 100-$\mu\mu$fd. mica capacitor. Alternatively an adjustable trimmer covering at least 50 to 150 $\mu\mu$fd. may be substituted for the 100-$\mu\mu$fd. fixed capacitor. Then the adjustment of this trimmer and that of the regular antenna trimmer can be juggled back and forth until a condition is achieved where the input circuit of the auto set is resonant with the converter either in or out of the circuit. This will provide maximum gain and image rejection under all conditions of use.

Reducing Battery Drain of the Receiver When the receiving installation is used frequently, and particularly when the receiver is used with the car parked, it is desirable to keep the battery drain of the receiver-converter installation at an absolute minimum. A substantial reduction in drain can be made in many receivers, without appreciably affecting their performance. The saving of course depends upon the design of the particular receiver and upon how much trouble and expense one is willing to go to. Some receivers normally draw (without the converter connected) as much as 10 amperes. In many cases this can be cut to about 5 amperes by incorporating all practicable modifications. Each of the following modifications is applicable to many auto receivers.

If the receiver uses a speaker with a field coil, replace the speaker with an equivalent PM type.

Practically all 0.3-ampere r-f and a-f voltage amplifier tubes have 0.15-ampere equivalents. In many cases it is not even necessary to change the socket wiring. However, when substituting i-f tubes it is recommended that the i-f trimmer adjustments be checked. Generally speaking it is not wise to attempt to substitute for the converter tube or a-f power output tube.

If the a-f output tube employs conventional cathode bias, substitute a cathode resistor of twice the value originally employed, or add an identical resistor in series with the one already in the set. This will reduce the B drain of the receiver appreciably without seriously reducing the maximum undistorted output. Because the vibrator power supply is much less than 100 per cent efficient, a saving of one watt of B drain results in a saving of nearly 2 watts of battery drain. This also minimizes the overload on the B supply when the converter is switched in, assuming that the converter uses B voltage from the auto set.

If the receiver uses push-pull output and if one is willing to accept a slight reduction in the maximum volume obtainable without distortion, changing over to a single ended stage is simple if the receiver employs conventional cathode bias. Just pull out one tube, double the value of cathode bias resistance, and add a 25-μfd. by-pass capacitor across the cathode resistor if not already by-passed. In some cases it may be possible to remove a phase inverter tube along with one of the a-f output tubes.

If the receiver uses a motor driven station selector with a control tube (d-c amplifier), usually the tube can be removed without upsetting the operation of the receiver. One then must of course use manual tuning.

While the changeover is somewhat expensive, the 0.6 ampere drawn by a 6X4 or 6X5 rectifier can be eliminated by substituting six 115-volt r-m-s 50-ma. selenium rectifiers (such as Federal type 402D3200). Three in series are substituted for each half of the full-wave rectifier tube. Be sure to observe the correct polarity. The selenium rectifiers also make a good substitution for an 0Z4 or 0Z4-GT which is causing hash difficulties when using the converter.

Offsetting the total cost of nearly $4.00 is the fact that these rectifiers probably will last for the entire life of the auto set. Before purchasing the rectifiers, make sure that there is room available for mounting them. While these units are small, most of the newer auto sets employ very compact construction.

Two-Meter Reception For reception on the 144-Mc. amateur band, and those higher in frequency, the simple converter-auto-set combination has not proven very satisfactory. The primary reason for this is the fact that the relatively sharp i-f channel of the auto set imposes too severe a limitation on the stability of the high-frequency oscillator in the converter. And if a crystal-controlled beating oscillator is used in the converter, only a portion of the band may be covered by tuning the auto set.

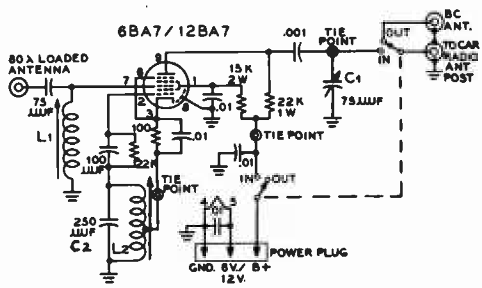
The most satisfactory arrangement has been found to consist of a separately mounted i.f., audio, and power supply system, with the converter mounted near the steering column. The i-f system should have a bandwidth of 30 to 100 kc. and may have a center frequency of 10.7 Mc. if standard i-f transformers are to be used. The control head may include the 144-Mc. r-f, mixer, and oscillator sections, and sometimes the first i-f stage. Alternatively, the control head may include only the h-f oscillator, with a broadband r-f unit included within the main receiver assembly along with the i.f. and audio system. Commercially manufactured kits and complete units using this general lineup are available.

An alternative arrangement is to build a converter, 10.7-Mc. i-f channel, and second detector unit, and then to operate this unit in conjunction with the auto-set power supply, audio system, and speaker. Such a system makes economical use of space and power drain, and can be switched to provide normal broadcast-band auto reception or reception through a converter for the h-f amateur bands.

23-2 A One Tube Mobile Converter for 75 Meters

The simple converter shown in figures 4, 5 and 6 provides reception over the frequency range of 3750 kc. to 4050 kc. when operated into a standard broadcast-band auto radio receiver. The converter uses a single 6BA7 (12BA7 for 12 volt automobiles) and operates into a tunable intermediate frequency in the range of 500-1500 kc. Power requirements for the converter are low enough so that the voltages necessary for converter operation may be taken from the auto receiver.

Circuit of the Converter A type 6BA7 tube is employed as a simple frequency converter with the 75 meter signal impressed upon the no. 3 grid of the tube. Grids no. 1, 2 and 4 form a fixed tuned hot-cathode conversion oscillator. The output of the converter is the beat frequency between this oscillator and the incoming signal. This beat frequency must fall in the tuning range of the



L1 = XR-50 FORM, 0.5" DIA., 48T. # 28 E.
L2 = XR-50 FORM, 0.5" DIA., 31T. # 28E. CATHODE TAP 6T. FROM GROUND.
C1 = CENTRALAB 823-BN

Figure 4
SCHEMATIC OF 80-METER CONVERTER

broadcast receiver (500-1500 kc.) so to receive signals in the 3750-4050 kc. spectrum the frequency of the oscillator must fall within the range shown in Table 1. To receive signals in the 75 meter phone band, it is only necessary to tune the broadcast receiver over 200 kc. of the broadcast band. By the proper setting of the oscillator slug, L_2, a 200 kc. spectrum of the broadcast band may be chosen in which there are relatively few strong local BC stations. This will prevent "leak through" of the BC signals during reception on the 75 meter band.

The input circuit of the converter is designed to work in conjunction with the usual 75 meter loaded whip antenna which may be connected to the input jack of the converter by a length of 52 ohm coaxial line. The converter employs a broadband output circuit, relying upon the inherent r.f. selectivity of the car radio for rejection of signals adjacent to the received signal.

Converter Assembly The converter is simple enough so that all components may be mounted within a small aluminum box chassis measuring 6½"x 3½"x 2" *(L.M.B. #138)*. All components except the converter switch are mounted on the back lip of the box, as shown in figure 6. The switch that places the converter in the circuit is mounted in the center of the front of the box. The complete assembly is small enough so that it may be mounted beneath the car radio as shown in figure 5.

Wiring the converter is simple. Pin no. 4 of the socket is grounded and the screen bypass capacitor is connected between pins 1 and 4 of

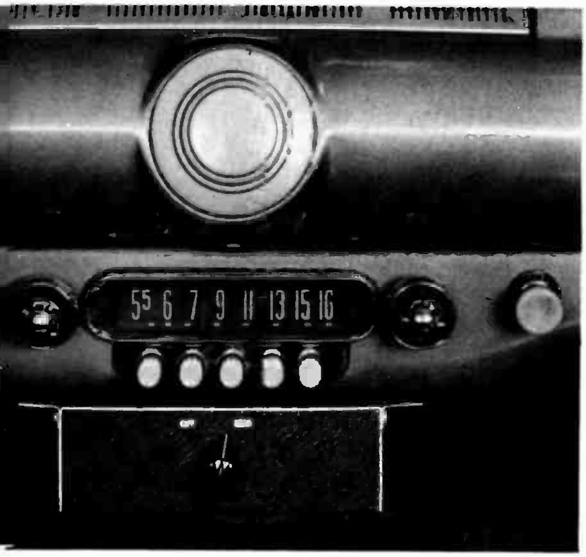


Figure 5

SINGLE TUBE CONVERTER MOUNTED BENEATH AUTO RADIO

Two small angle brackets are bolted to the ends of the converter case. Sheet metal screws hold the brackets to the dash of the automobile.

the socket. A jumper is placed between pins 3 and 6. The cathode bias network is placed between pin 3 and an adjacent insulated tie-point. A second insulated tie-point is used at the junction of the plate and screen resistors.

The oscillator padding capacitor, C_2 is mounted directly across the terminals of L_2. The lead from L_2 to the grid resistor and capacitor and to pin no. 2 of the 6BA7 socket should be made of no. 14 solid wire, as any vibration of this lead would lead to frequency instability in the conversion oscillator.

Alignment and Installation When the wiring has been completed and checked, a jumper should be placed across the 80 meter antenna jack, grounding the 75 $\mu\mu$fd. coupling condenser, and coil L_1 peaked to 3900 kc. with the aid of a grid-dip oscillator. Power should next be applied to the converter, and the slug of L_2 tuned so as to place the conversion oscillator on the chosen frequency as shown in Table 1. The frequency of the oscillator may be monitored in a nearby shortwave receiver. The converter should now be mounted in the car and all power and antenna connections made. The auto receiver should be tuned to the middle of the "75 meter" tuning range, and the antenna trimmer of the broadcast receiver peaked for maximum noise output when the converter switch is in the *off* position. The converter should now be turned on, and C_1

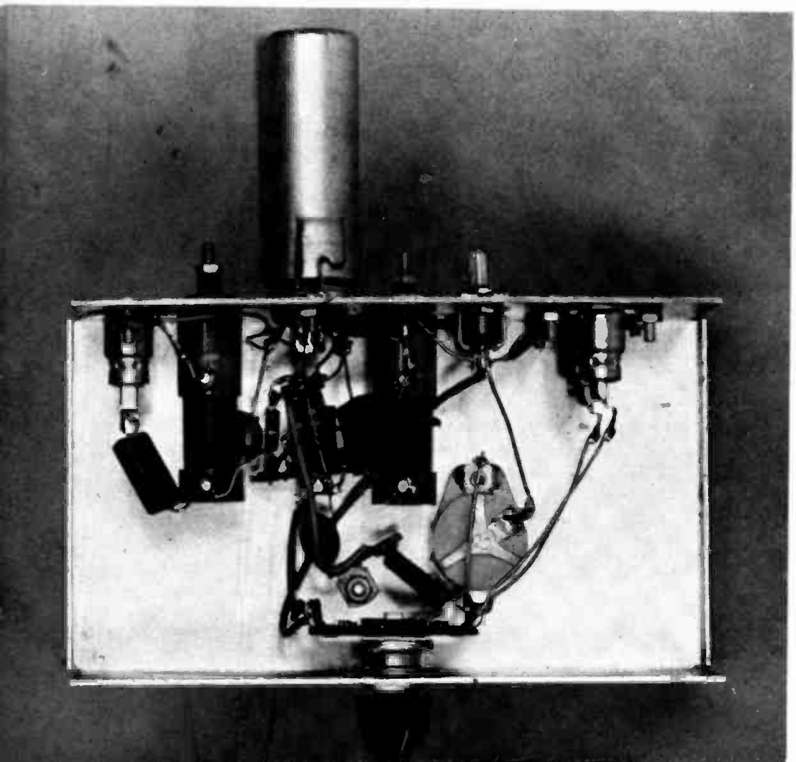


Figure 6

INTERIOR VIEW OF ONE-TUBE CONVERTER

The antenna coil is mounted between the 6BA7 tube and the antenna receptacle. To the right of the tube socket is the oscillator coil. The output tuning capacitor is mounted on the bottom chassis deck at the right.

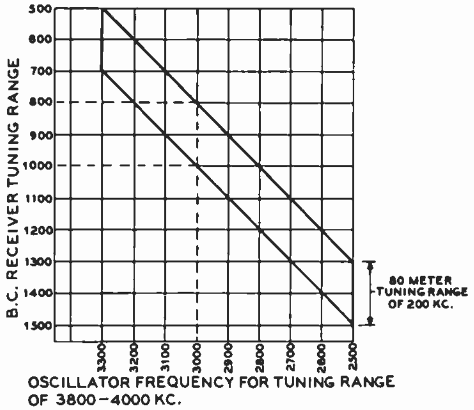


TABLE 1

CONVERSION OSCILLATOR FREQUENCY CHART

peaked for maximum response of 75 meter signals. Coil L_1 may be left peaked at 3900 kc., or it may be retuned to peak at the chosen frequency of operation in the 75 meter band.

It must be remembered that the 75 meter loaded whip antenna with which this converter is used is a very high-Q device, and best reception will be had only at the resonant frequency of the antenna. A whip with some sort of variable loading coil is recommended for optimum results with this converter.

The leads supplying filament and high voltage power to the converter should be shielded, with the shields grounded at each end of the lead for minimum noise pickup of the converter. Care should be taken that the box of the converter is firmly grounded to the chassis of the auto radio. As a final step, the slug of L_2 should be fixed in place with a spot of nail polish or *Duco Cement* to prevent frequency instability caused by a slight motion of the slug within the coil form.

23-3 Mobile Transmitters

As in the case of transmitters for fixed-station operation, there are many schools of thought as to the type of transmitter which is most suitable for mobile operation. One school states that the mobile transmitter should have very low power drain, so that no modification of the electrical system of the automobile will be required, and so that the equipment may be operated without serious regard to discharging the battery when the car is stopped, or overloading the generator when the car is in motion. A total transmitter power drain of about 80 watts from the car battery (6 volts at 13 amperes, or 12 volts at 7 ampetes) is about the maximum that can be allowed under these conditions. For maximum power efficiency it is recommended that a vibrator type of supply be used as opposed to a dynamotor supply, since the conversion efficiency of the vibrator unit is high compared to that of the dynamotor.

A second school of thought states that the mobile transmitter should be of relatively high power to overcome the poor efficiency of the usual mobile whip antenna. In this case, the mobile power should be drawn from a system that is independent from the electrical system of the automobile. A belt driven high voltage generator is often coupled to the automobile engine in this type of installation.

Three examples are given in this chapter of installations requiring different primary power levels. The first is a simple 12 watt all-band transmitter that operates from a 300 volt, 100 milliampere vibrator supply. The second is a 20 watt 2 meter mobile transmitter operating from a 300 volt, 200 milliampere vibrator supply. The third installation is a one kilowatt Single Sideband mobile transmitter operating from a three-phase alternating current supply provided by a belt driven generator. Each installation illustrates a separate set of power problems and requirements that must be met for proper operation of the equipment.

23-4 A 12 Watt All-Band Mobile Transmitter

This little 12 watt all-band mobile transmitter shown in figures 7 and 8 is designed for the amateur interested in starting mobile operation without too much capital investment. Both the component cost and the power drain of this unit are modest; yet it runs 12 watts input to the final stage, fully modulated and is capable of operation on the 80, 40, 20, 15, 11 and 10 meter amateur bands. It is designed for operation from a single 300 volt 100-ma. power unit such as incorporated in the Universal Mobile Modulator and Power unit to be described later.

Circuit Design Only two tubes are used in the r.f. portion of the 12 watt transmitter (figure 9). A 6CL6 is used as a conventional crystal oscillator for operation on the 80-meter and 40-meter bands. Fundamental frequency crystals ate employed on these bands. When the transmittet is used on the 20, 15, 11 and 10 meter bands, 7-megacycle crystals are used in a harmonic oscilla-

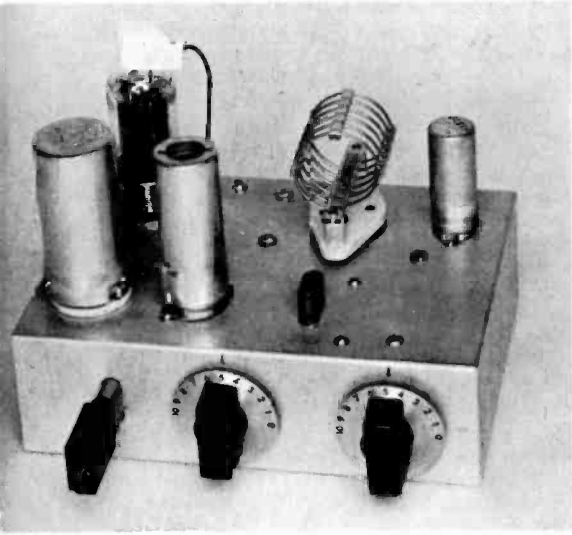


Figure 7

12-WATT ALL-BAND MOBILE TRANSMITTER USING 2E26 AMPLIFIER STAGE

Operating all amateur bands from 10 to 80 meters, this transmitter is powered by the modulator-supply unit of figure 10. A 6CL6 harmonic crystal oscillator is used to drive the 2E26 amplifier.

tor circuit. The changeover from one oscillator circuit to the other is accomplished automatically when the plug-in oscillator plate coil is changed (Table 2). The cathode coil of the oscillator is permanently tuned to 10.5-Mc. for correct harmonic operation and left in the circuit at all times, as it does not hinder operation on 80 or 40 meters. The oscillator is capacity coupled to a 2E26 tetrode, which serves as an amplifier on all bands. The plate circuit of the 2E26 stage is shunt fed so as to remove dangerous d.c. potentials from the pi-network output circuit of the 2E26. The output circuit is designed to operate into a loaded whip on each band except on 10 and 11 meters. On these two bands a conventional eight foot unloaded antenna should be employed.

The antenna relay is a small sealed single pole-double throw unit which mounts in a seven pin miniature tube socket. Only 150 milliwatts of power are required for relay operation. The coil resistance of the relay is 8,000 ohms and power for relay operation is obtained from the high voltage supply by means of a dropping resistor.

Transmitter Construction The transmitter is constructed upon a 5"x 7"x 2" aluminum chassis (Bud #AC-402), and the layout of the major components may be seen in figures 7 and 8. Along the rear of the chassis are the 2E26 tube, the plug-in pi-net-

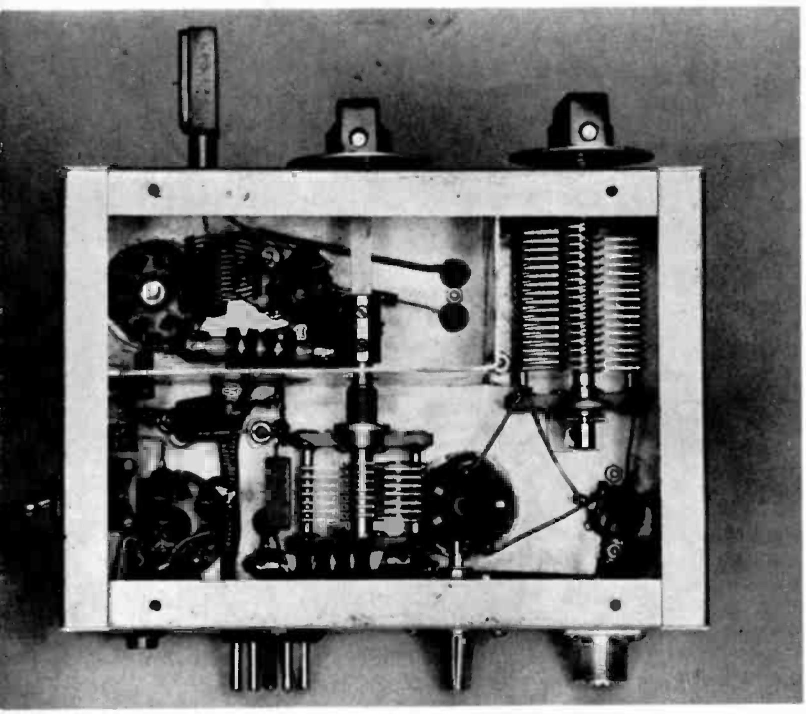


Figure 8

BELOW CHASSIS VIEW OF THE 12-WATT TRANSMITTER

A simple shield plate divides the sub-chassis area into two compartments for the oscillator and amplifier stages.

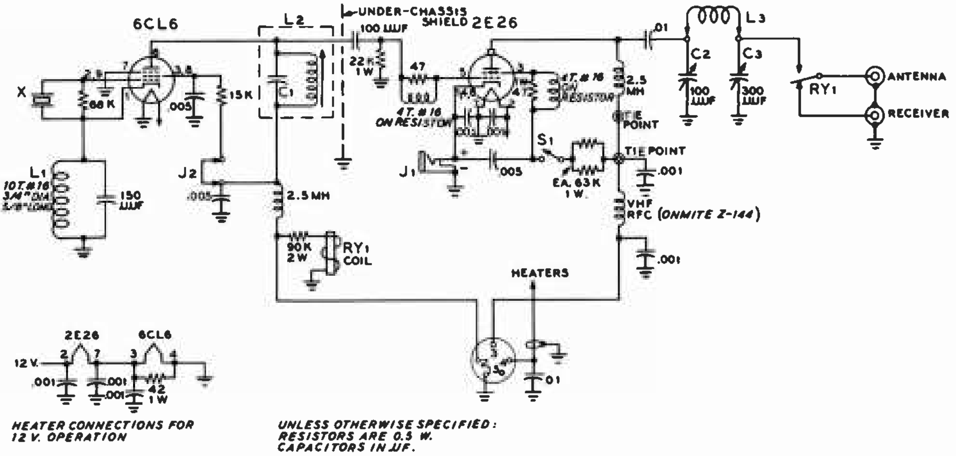


Figure 9

SCHEMATIC OF 2E26 ALL-BAND TRANSMITTER FOR 6 OR 12 VOLT OPERATION

Ry_1 is a "Terado Micro-Relay," manufactured by Terado Co., St. Paul. 14. Minn.

work coil and the antenna relay. The oscillator plate coil, the 6CL6 tube and the oscillator screen jack are along the front edge of the chassis. Directly below the oscillator plate coil on the front of the chassis is located the crystal socket, and to the right of this are the plate tuning and loading controls for the 2E26 stage. Across the back lip of the chassis (figure 8) are the coaxial output connector, the receiver antenna jack, the power plug and the microphone jack. On the extreme end of the chassis just below the 2E26 tube socket is located S_1, the screen control switch of the amplifier stage.

It is necessary to place a shield plate beneath the chassis between the oscillator stage and the components of the final amplifier. This shield may be cut from a piece of soft aluminum and should enclose a space 4¾" long and 2⅛" wide. The shield should be approximately 1⅞" high. Small mounting feet should be formed from the edges of the shield to allow it to be fastened to the underside of the chassis by 4-40 machine screws. The antenna loading capacitor, C_3, is mounted in the free space adjacent to the shield and is fastened by the front bearing bolt and the rear foot to the chassis. The amplifier tuning capacitor, C_2, is mounted at the rear of the chassis between the 2E26 socket and the socket for L_3 by means of two 6-32 machine screws through the threaded holes in the mounting feet of the capacitor. An extension to the shaft of C_2 passes through the oscillator shield to the tuning knob on the front of the chassis.

Wiring is accomplished with stranded hookup wire for all leads within the shielded compartment except for the filament lead, which is run in shielded wire. The lead to the relay coil is also run in shielded wire. The r-f circuits are wired with no. 14 tinned wire. Coil L_1 is a ten turn section of B & W #3011 Miniductor, and is self-supporting between pin no. 1 of the 6CL6 socket and the ground terminal of the crystal socket.

Tuning Procedure After the transmitter is wired and checked the tubes and coils may be plugged in their respective sockets, and a crystal of the correct operating frequency plugged into the crystal socket. A 0-50 ma. d-c meter should be plugged into J_1 and switch S_1 opened. A temporary short should be placed across C_3, grounding the antenna end of L_3. The transmitter should be connected to an a.c. operated power supply capable of delivering 300 volts at 50 ma. A jumper should be placed in the screen jack (J_2) of the 6CL6 oscillator stage. Power may be applied to the unit, and the slug of L_2 tuned for indication of grid current on the meter plugged into J_1. When the oscillator is operating properly, approximately 2½ ma. of grid current should be observed on the meter. On the 80-meter and 40-meter bands the rectified grid current may perhaps run as high as 6 ma. This exceeds the maximum grid current rating of the 2E26. To lower the grid current to the proper value, the shorting jumper should be removed from the screen socket of the 6CL6 stage and various values of resistance should be inserted in the socket until a value is found that will allow a maximum of 3 ma. grid current to the 6CL6. This resistor should be

TABLE 2

COILS FOR 12-WATT MOBILE TRANSMITTER

BAND	L_2 (*MILLEN 74001 COIL FORM*)	C_1 (*SILVER MICA*)
80	40 T. #24 E., CLOSEWOUND	80 μμF
40	20 T. #28 E., CLOSEWOUND	50 μμF
20	13 T. #28 E., CLOSEWOUND	20 μμF
15	10 T. #28 E., CLOSEWOUND	15 μμF
10-11	8 T. #28 E., CLOSEWOUND	15 μμF
L_3 = *35 WATT PLUG-IN COILS, NO LINK*		

used in place of the shorting jumper for operation on 80 and 40 meters.

When the correct grid current has been obtained in the 2E26 stage, switch S_1 should be closed, applying screen voltage to the amplifier tube. C_2 should then be tuned for the usual resonance dip on the meter plugged into J_1. When S_1 is closed, the off-resonance meter reading of J_1 will increase to 50 or 60 milliamperes, so care must be taken not to damage the meter. When the resonance dip is found, operation of the amplifier stage may be checked by removing the short across C_3 and connecting an automobile headlight lamp to the antenna jack as a dummy load. When C_2 is resonated, C_3 may be adjusted so that a reading of 45 milliamperes is obtained on the cathode meter. C_2 should always be re-resonated after the setting of C_3 is changed.

For operation on 80 and 40 meters it will be necessary to shunt C_3 with additional capacity in order to match center-loaded antennas presenting low values of load impedance. For a first test, a 300 μμfd. ceramic capacitor should be temporarily shunted across C_3. Then with the antenna connected, C_2 should be resonated and the minimum plate current noted. The object is to obtain the rated value of 45 ma. of cathode current in the 2E26 stage with the largest possible value of shunting capacitance across C_3. If the minimum plate current dip is too high, the shunting capacitor should be increased to 600 μμfd. or 900 μμfd. If operation is contemplated on the low frequency end of the 80-meter band with a high-Q loaded antenna, the shunt capacity may approach 1500 μμfd. When the correct capacitor values are found for 80 and 40 meter operation, the capacitors may be permanently connected to the base of the plug-in coil for that particular band. One of the blank socket pins may be grounded, and the capacitor connected to the corresponding pin on the coil base. The selection of the proper shunting capacitor should be done after the transmitter is placed in the automobile and connected to the car antenna.

Figure 10

POWER SUPPLY-MODULATOR UNIT FOR THE 12-WATT TRANSMITTER

A standard 300-volt, 100-milliampere vibrator pack is used to supply power for both the modulator and r-f sections of the transmitter.

23-5 Universal Modulator and Power Unit

The Modulator and Power (MP) unit to be discussed was designed for use with the 2E26 transmitter previously described. However, it may be used with any transmitter running approximately 12 watts input at 300 volts. The MP unit will supply plate and filament voltages for any two stage transmitter using a 2E26, 5763 or 6360 tube in the amplifier stage, and will supply a full six watts of audio power to fully modulate the amplifier. Top and bottom views of the MP unit are shown in figures 10 and 11 and the schematic is given in figure 12.

Circuit Design Three tubes are used in the MP universal unit. A 6U8 is employed as a high gain speech amplifier, for use with either crystal or carbon microphones. The carbon microphone is connected in the cathode circuit of the triode section of the 6U8 and switch S_1 is thrown to the "carbon"

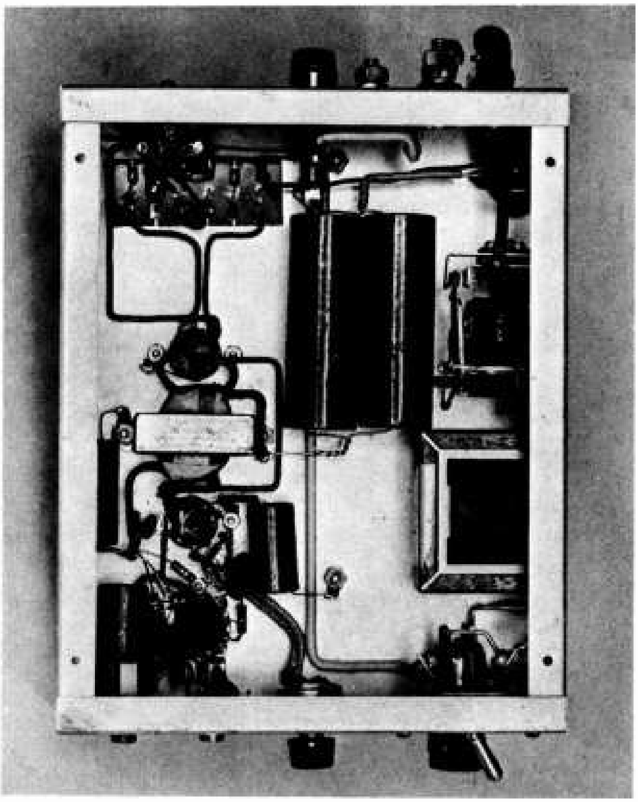


Figure 11
BOTTOM VIEW OF MODULATOR-POWER UNIT FOR 12-WATT TRANSMITTER

position. The triode section of the 6U8 is then operating as a grounded-grid amplifier. When the carbon microphone is removed, a crystal microphone plugged in the grid circuit jack and S_1 thrown to "crystal," the triode section operates as a conventional amplifier stage.

The pentode section of the 6U8 acts as a voltage amplifier, driving a parallel connected 12AU7. This in turn is transformer coupled to a single 12AX7 Class B modulator. The plate-to-plate load impedance of the 12AX7 is 18,000 ohms, and the tube will deliver almost 7 watts of sine-wave audio under this condition.

Three-circuit microphone jacks are used to allow "push-to-talk" microphones to be employed. For testing purposes a single pole-single throw "test switch" is placed across the control line. When this line is grounded, the coil circuit of Ry_1 is completed and 6 volts is supplied to the high voltage vibrator supply. Either a 6 volt or 12 volt vibrator supply should be used, depending upon the voltage of the electrical system of the car. Changes in filament wiring to accommodate either 6 or 12 volt systems are shown in figure 12.

The high voltage output from the vibrator supply is filtered by a low inductance high-capacity network to provide good dynamic regulation of the high voltage under modulation. The supply is capable of intermittent loads of up to 120 milliamperes at 300 volts without danger to the components of the vibrator package. The resting current of the 12AX7 modulator is 10 ma., rising to about 40 ma. under modulation peaks. This may be checked by inserting a meter in the cathode leads of the 12AX7. Total current drain of the modulator unit is 50 ma. when supplying six watts of audio. This leaves about 60 ma. for the r.f. section which is connected to the MP unit by means of P_1 and a four wire cable.

Construction The MP unit is built upon a cadmium plated steel chassis measuring 9"x 7"x 2" in size (Bud #CB-1192). *A Radiart Model 453* non-synchronous vibrator supply is used, which measures 7"x 3½" in area and occupies the left side of the chassis. If a different make or model vibrator supply is employed, it may be necessary to alter the

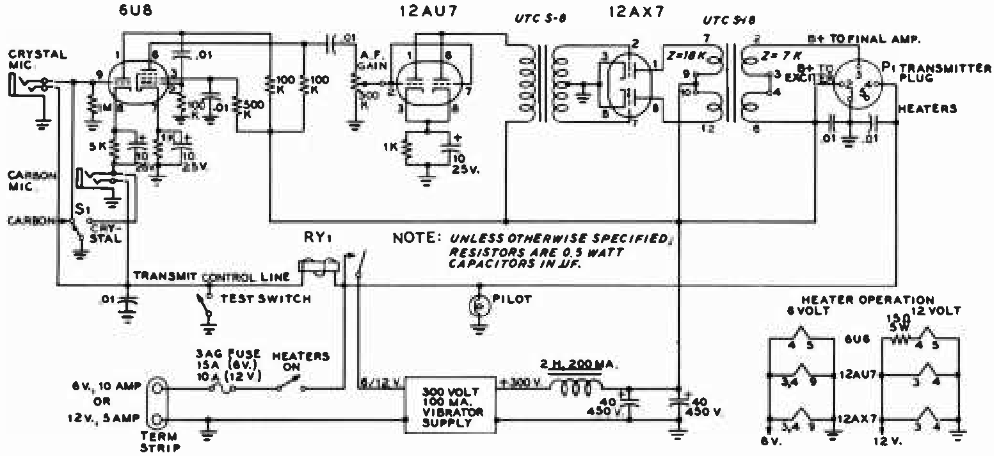


Figure 12

SCHEMATIC OF UNIVERSAL MOBILE MODULATOR AND POWER UNIT FOR 6 OR 12 VOLT OPERATION

chassis size slightly to hold the vibrator supply, which should be firmly bolted to the steel chassis. The three speech stages are aligned along the right side of the chassis, with the modulation transformer to the rear. Along the back edge of the chassis are the output plug, P_1, the primary fuse and the input terminal strip. On the front edge of the chassis are located the pilot light, the filament switch, the gain control and the two microphone jacks. Directly behind the jacks is the 6U8 stage, followed by the 12AU7 and the 12AX7. Placement of the underside components may be seen in figure 11.

No difficulty should be encountered in getting the modulator to operate properly. Either a carbon or crystal microphone may be used when S_1 is placed in the proper position, and full modulator output may be obtained from either type of microphone.

23-6 An 832-A Transmitter for 144 Mc.

The transmitter illustrated in figures 13 and 14 is an improved version of the 2 meter transmitter that was featured in the thirteenth edition of this Handbook. This has proven to be a very popular design, and the present version is a result of a series of changes in the original unit that allow more efficient circuit operation and greater output from the 832-A. The transmitter may be used with a dynamotor or vibrator supply for mobile use, or with an a-c operated power pack for use at the home station. In either event a power unit capable of delivering 300 volts at about 150 milliamperes is required.

The transmitter is crystal controlled and uses an 832-A at the output stage, running at an input of 300 volts and 70 ma., or 20 watts. The transmitter is designed to be operated with a low level carbon microphone, and is capable of 100% modulation.

Circuit Details The schematic of the transmitter is shown in figure 15. A 12AT7 is used as a harmonic oscillator with 24-Mc. crystals. However, 8-Mc. crystals of the surplus variety may be used with equal facility. The oscillator actually operates on the third harmonic of the 8-Mc. crystal frequency.

TABLE 3
COIL SPECIFICATIONS FOR 832A TRANSMITTER

L_1—16½ turns no. 20, ¾" dia., 1⅛" long, cut into two coils by breaking one turn. Plate coil has 12 turns, grid coil has 4 turns

L_2—4 turns no. 16, ½" dia., ⅝" long

L_3, L_4—4 turns no. 14, ½" dia., spaced to ⅞" long

L_5—1 turn pickup link, no. 14, ½" dia.

The data given for the oscillator coil, L_1, in table 3 has proven to be satisfactory for use with the normal run of surplus 8-Mc. crystals for third overtone use. However, if a high frequency crystal designed for 24-Mc. operation (such as the Bliley AX-3) is to be used, the number of turns on the grid winding of L_1 should be reduced to the amount which is just sufficient to sustain normal oscillation.

The second section of the 12AT7 is capacitively coupled to the output of the crystal oscillator stage. This second section of the tube acts as a frequency tripler to the 72-Mc. region. A 5763 high-frequency pentode is employed as a doubler from 72-Mc. to 144-Mc. This tube supplies ample excitation for proper operation of the 832-A at that frequency. Over 4 ma. of grid current is delivered to the 832-A by the exciter circuit illustrated.

The 832-A Class C final amplifier is plate modulated by a pair of 6V6-GT tubes operating as a class AB_1 amplifier. The 832-A stage is conventional, with the plate tank circuit and antenna coupling coil mounted on a bracket atop the chassis. A coaxial output fitting is employed for unbalanced feed systems, but a two-terminal output fitting may be substituted if it is desired to feed the antenna system with balanced transmission line. A miniature butterfly capacitor is used in the plate circuit of the 832-A as well as in the plate circuit of the 5763 doubler.

Metering Provision is included for checking the cathode current of the 832-A final amplifier, and for measuring the grid currents of the 5763 doubler and the 832-A amplifier. A 0-100 d-c milliammeter will be suitable for metering all three circuits. The indication in the two grid current positions will be small (1.5 and 4 ma.) but the deflection is sufficiently great to permit tuning the stages.

Construction The transmitter is constructed upon a 9"x 7"x 2" aluminum chassis (Bud #AC-406). The modulation system occupies the back half of the chassis. The 12AU7 speech amplifier tube is in the rear left corner, and in line with it are the driver transformer, the 6V6-GT modulator tubes and the modulation transformer. The microphone jack, the grid current jack, the audio level control and the power plug are located on the rear lip of the chassis.

The r-f section occupies the front of the chassis. At the extreme left is the 12AT7 crystal oscillator tube. L_1-C_1 is located directly in front of this tube, and L_2-C_2 behind it. The crystal socket is located between 12AT7 and the 5763. The butterfly plate circuit of the doubler stage is placed in front of the 5763

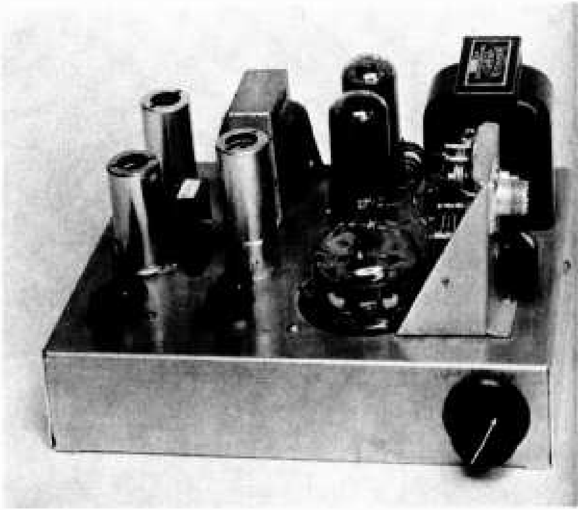


Figure 13
2-METER TRANSMITTER USING 832-A AMPLIFIER

tube socket, and the socket so aligned that pin no. 1 (plate pin) is located near one stator terminal of the butterfly capacitor. The doubler coil, L_3 is mounted directly between the stator connections of the butterfly capacitor, in close proximity to the 832-A socket.

The 832-A tube socket is mounted with pin no. 4 facing the doubler stage. All the ceramic bypass capacitors for the amplifier stage are mounted atop the socket and grounded to the socket shell with the shortest possible leads. If the socket is the type that has the ceramic base riveted to the shell, small 4-40 machine screws may be passed through the rivet holes and used for ground terminals. RFC_1 and RFC_2 are small air-wound chokes which connect directly from the no. 2 and no. 6 pins of the 832-A socket to a small terminal strip mounted on the socket between pins no. 1 and no. 7.

A small Centralab NPO-type ceramic capacitor of 5 $\mu\mu$fd. is connected from the end of L_3 opposite to the 5763 tube to balance out the internal capaciry of the doubler tube. This insures that each section of the 832-A receives grid drive from the doubler stage.

A bracket cut from a soft piece of aluminum is mounted atop the chassis to support the amplifier tank circuit, the output link coil and tuning condenser and the coaxial antenna receptacle. The plate r-f choke is supported to this bracket by an insulated terminal strip.

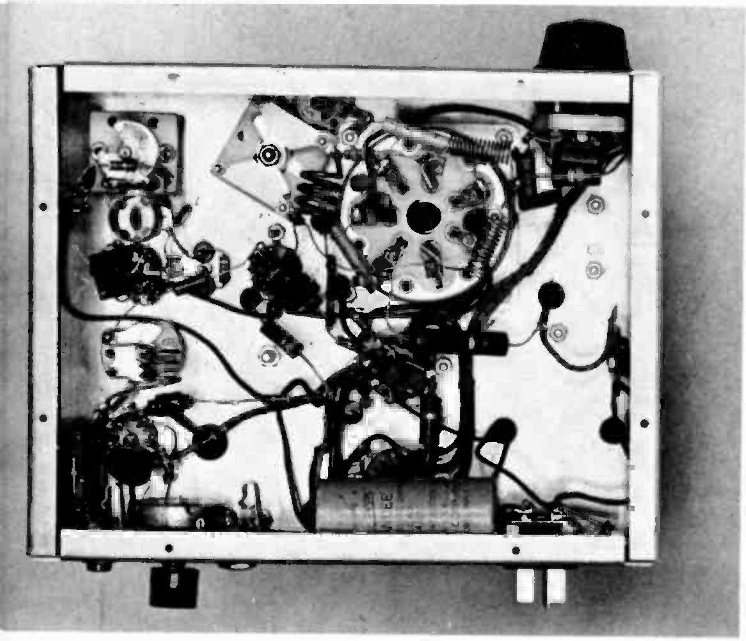


Figure 14
UNDER-CHASSIS VIEW OF 832-A TRANSMITTER

Bypass capacitors of the 832A stage are mounted directly between the tube socket pins and the grounding shell of the socket. The coils for the low level stages are self-supporting and mount to the tuning capacitors by their wire leads.

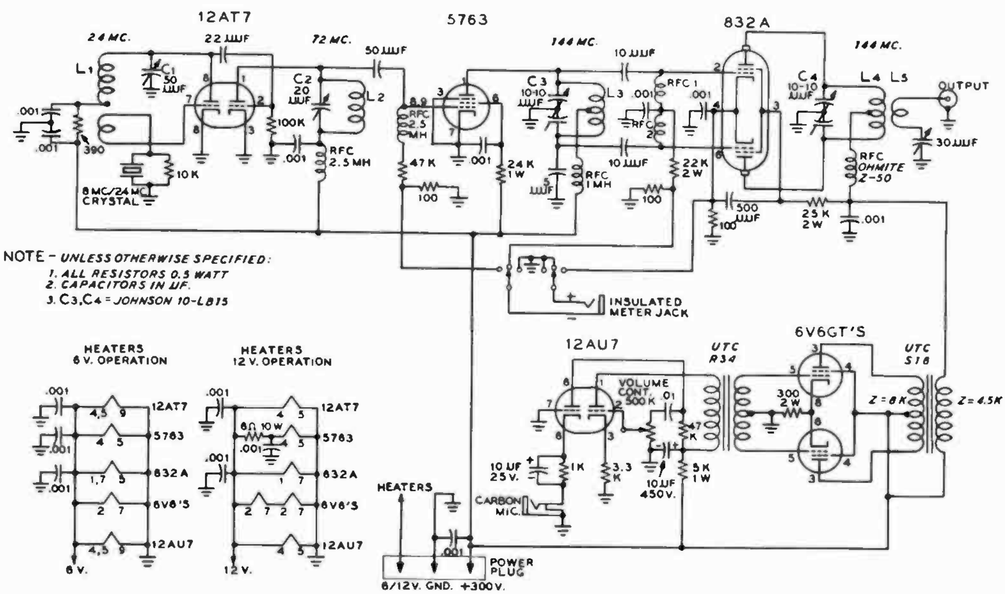


Figure 15
SCHEMATIC OF 832A 2 METER TRANSMITTER

Short, flexible copper leads are used for the plate connections to the 832-A tube.

It is important to note that all ground leads and bypass capacitor leads should be kept as short as possible at these frequencies. For example, the screen bypass capacitor on the 5763 doubler stage should be connected directly between pin no. 6 (screen) and ground (pin no. 7). Pin no. 7 should be grounded with a short piece of no. 14 wire directly to the socket rim. All components should be mounted as close to their respective socket pins as is possible. A neat, workman-like wiring job will do much to eliminate the instability that occasionally plagues the builder of v.h.f. equipment.

Alignment When the transmitter is wired and checked, the 12AT7 and the 5763 tubes should be placed in their sockets. If a grid-dip oscillator is handy the resonant frequency of the oscillator circuit, the tripler circuit and the doubler circuit should be checked. Coils L_2 and L_3 may be squeezed slightly to change the resonant frequency of the respective circuits if it is found to be in error. An 8-Mc. crystal should be plugged in the crystal socket and power applied to the transmitter. Oscillation should be heard when a receiver is tuned to the third harmonic of the crystal. When the tripler stage is tuned to resonance, a grid current reading of 1.5 ma. or more should be observed when the meter switch is turned to the 5763 grid current position. The switch should be turned to read the grid current of the 832-A, and the amplifier tube should be plugged in its socket. C_3 should be tuned for maximum grid current of the 832-A, the meter switch should be switched to read the 832-A cathode current, and the plate circuit of the 832-A should be tuned to resonance. An automobile headlight lamp may next be connected to the coaxial antenna receptacle and the antenna resonating capacitor tuned for maximum brilliance of the lamp. Cathode current of the 832-A should be limited to 70 milliamperes.

The last step is to plug the 6V6-GT modulator tubes and the 12AU7 speech amplifier tubes into their respective sockets. When the transmitter is modulated, the lamp bulb antenna should increase sharply in brilliance.

144-Mc. Mobile Antennas The most satisfactory antenna system for mobile operation on the 144-Mc. band has been found to be a ground-plane vertical. The most satisfactory antenna installation, if there is no objection to cutting a hole in the roof of a metal-top car, is that which uses a vertical rod operating against the car roof as a ground plane. A variety of such antennas designed for police car use are available, or one of the military surplus antenna bases designed for installation through the skin of an airplane may be used. In any event the length of the radiating rod should be about 20 inches. The tapered rods furnished with the surplus aircraft-type antennas usually are several inches shorter than 20 inches. But in most cases an extension may be machined to fit between the large base of the tapered rod and the antenna mounting unit. Coaxial feed, either with RG-8/U or RG-58/U cable should be used between the base of the antenna and the coaxial antenna changeover relay.

If it is desired not to cut a hole in the roof of the car for installation of the antenna at this point, the ground-plane vertical may be mounted atop a steel tube supported from the rear bumper. The height of the vertical radiator, when installed in this manner, should be at least as great as the car top to avoid strong directional effects.

23-7 A 12 Watt Fixed/Mobile Transmitter for 225 Mc.

With the advent of the Technician Grade Amateur License, there has been renewed interest in the 1¼ meter amateur band. Illustrated in figures 16 and 17 is a compact 12 watt crystal controlled transmitter designed for efficient operation in this band. The transmitter requires a power supply capable of supplying 300 volts at 200 milliamperes, and delivers a fully modulated carrier of ten watts in the frequency range of 200-Mc. to 225-Mc. This unit may also be used as an exciter to drive a high powered amplifier using an 829-B or AX-5894/9903 to an input of about 100 watts.

Circuit Description The r-f portion of the transmitter uses four tubes: A 6CL6 functions as an overtone oscillator on about 25-Mc. It is recommended that overtone crystals in the 25-Mc. range be used with this circuit, although many surplus FT-243 or CR-6/U 8.3-Mc. crystals will operate in a satisfactory fashion on their third overtone frequency. The 6CL6 is capacity coupled to a 5763 power pentode which doubles to 74.7-Mc. and which is inductively coupled through a double tuned circuit to an Amperex 6360 push-pull miniature beam tetrode. The 6360 is a frequency tripler from 74.7-Mc. to 224.1-Mc. Sufficient output is developed by the tripler stage to drive the 6360 amplifier for Class C plate modulation. A double tuned circuit is used between the 6360 tripler stage and the final amplifier to provide adequate attenuation

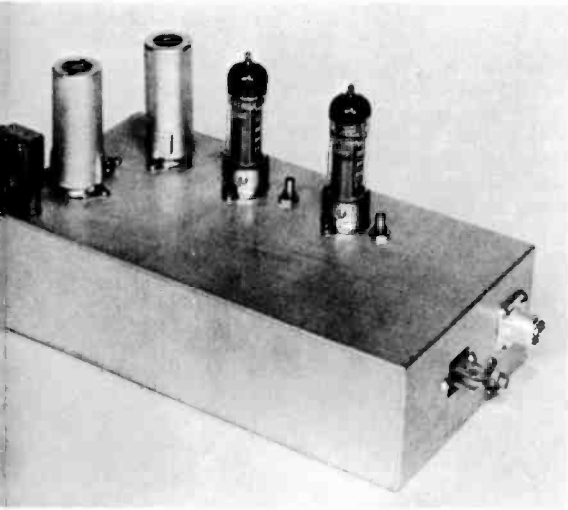
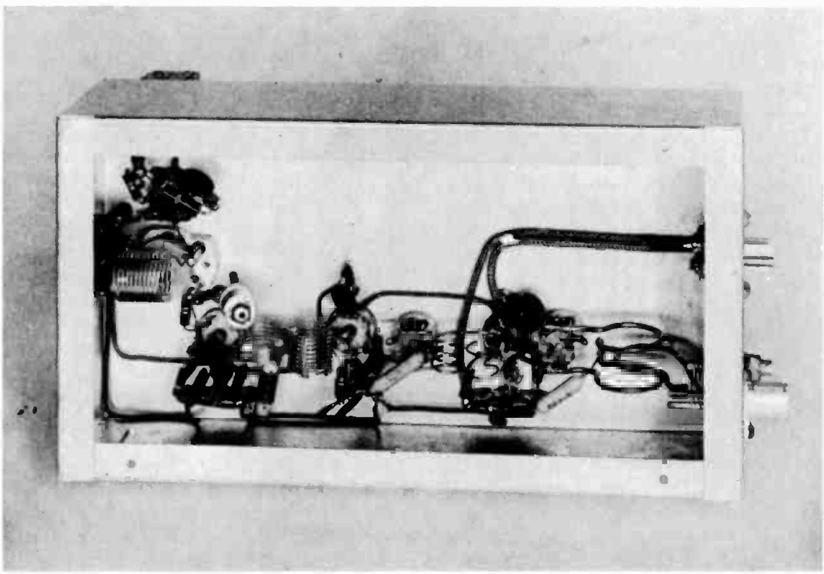


Figure 16
220-MC. TRANSMITTER
A 6360 dual tetrode is used in this miniature 1¼ meter transmitter. An 8-Mc. crystal is used for frequency control in an overtone oscillator circuit.

of other multiples of the fundamental frequency which may appear in the output of the tripler stage. The plate circuit of the 6360 amplifier stage is link coupled to a coaxial output connector for use with low loss coaxial line. If a balanced output is desired, the coaxial connector may be replaced with a two terminal output connector.

Construction The transmitter is built upon a 9½"x 5"x 3" aluminum chassis (Bud AC-421). The placement of the tubes is visible in figure 16, and the placement of the major components may be seen in the bottom view of figure 17. The schematic of the unit is given in figure 18. The crystal socket is placed in the front left corner of the chassis with the 6CL6 oscillator socket directly behind it. The 6CL6 socket is oriented so that prong no. 2 is facing the crystal socket. The plate tuning capacitor, C_1, of the oscillator is mounted directly behind the 6CL6 tube socket. Be sure to ground the rotor of this capacitor. A three terminal insulated tie-point strip is mounted on the side chassis wall next to C_1. This strip supports the B-plus end of L_1, the .001 $\mu\mu$fd. plate blocking capacitor and one end of the screen dropping resistor. Also supported by this strip are the 270 ohm plate iso-

Figure 17
UNDERCHASSIS VIEW OF 220-MC. TRANSMITTER



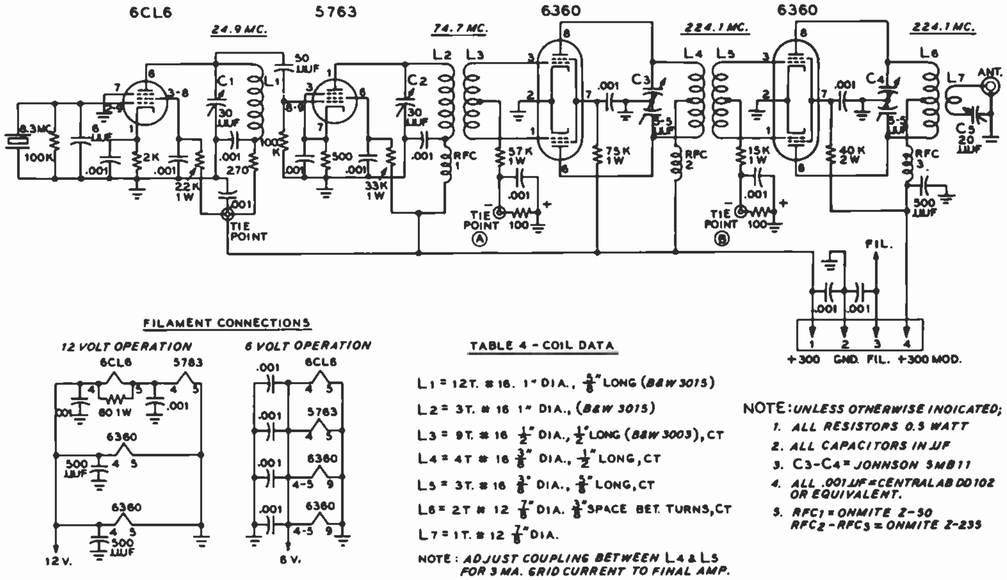


Figure 18
SCHEMATIC OF 224-MC. TRANSMITTER

lation resistor and the high voltage .001 $\mu\mu$fd. bypass capacitor.

The 5763 tripler socket is mounted a little to the side of the oscillator socket, with the no. 9 pin facing the oscillator socket. A three terminal insulated tie-point strip is affixed under the socket bolt next to the no. 5 pin. The components for the doubler stage are mounted between the socket pins and the terminals of this strip. Both L_1 and L_2 are mounted in position by their leads. L_1 is mounted atop C_1, and L_2 is connected between pin no. 1 of the 5763 socket and a small insulated tie-point that supports RFC_1 and the plate bypass capacitor. The grid coil of the tripler, L_3, mounts directly on pins no. 1 and no. 3 of the 6360 socket which is placed so that pins no. 1 and no. 3 are next to the plate coil, L_2, of the 5763 stage. A two terminal insulated tie-point strip is mounted beneath the socket bolt next to pin no. 9. This strip supports the grid resistor network and the screen circuit components of the 6360 stage. The miniature butterfly capacitor, C_3, which tunes the plate circuit of the tripler is mounted next to pins no. 6 and no. 8 of the 6360 socket. Connections are made to C_3 by means of short lengths of 1/8" wide flexible copper ribbon that run from the socket pins to the stators of C_3. The plate coil, L_4, is fastened directly to the stator connections of C_3. RFC_2 connects from the center of L_4 to the insulated terminal strip of the tripler socket.

The socket for the final amplifier stage is mounted 2⅜" to the right of the tripler socket. The grid coil, L_5, is fastened directly to pins no. 1 and no. 3 of the amplifier socket. A three terminal tie-point strip is attached to the socket bolt next to pin no. 9. The screen and grid components of the amplifier stage are attached to this tie-point strip. The butterfly tuning capacitor of the amplifier plate circuit, C_4, is mounted close to pins no. 6 and no. 8 of the amplifier socket, and connections are made between the capacitor and the socket pins by means of short lengths of 1/8" wide flexible copper ribbon. The plate coil, L_6, is attached directly to the stator rods of C_4.

The coaxial output plug and the antenna resonating capacitor, C_5 are fastened to the end lip of the chassis, and the pick-up link, L_7 is placed in between the turns of L_6.

The filament and plate supply leads to the power plug are made of shielded wire, as shown in the bottom chassis photograph.

Transmitter Tuning When the wiring is completed and checked, all tuned circuits should be set to the approximate operating frequency with the aid of a grid-dip oscillator. One stage at a time should be

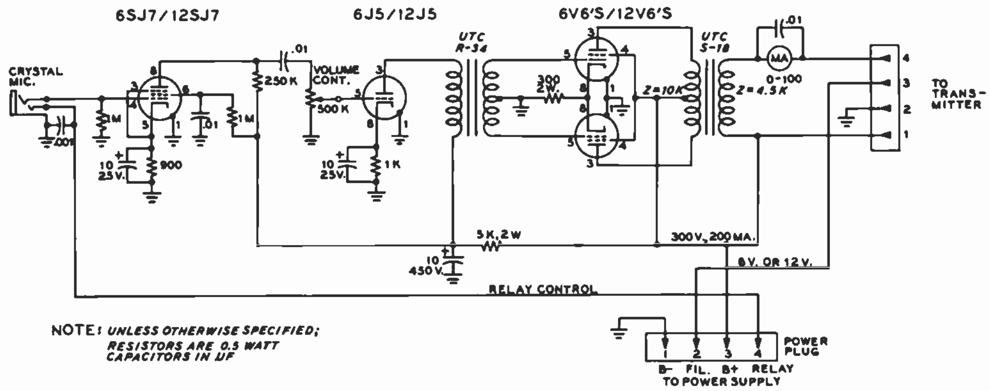
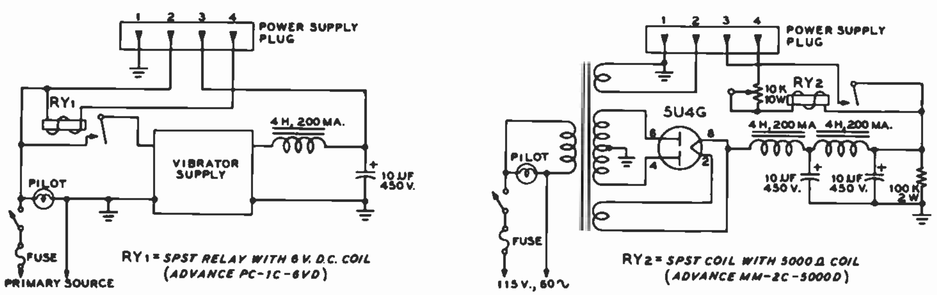


Figure 19
MODULATOR FOR 1¼-METER TRANSMITTER

tested starting with the oscillator stage. When it is working properly, the 5763 tripler stage should be put into operation. A milliammeter is connected between point "A" (figure 18) and ground and the grid current of the 6360 should be observed. A minimum of 1 ma. of grid current is needed for correct operation. When the 6360 tripler stage is operating, the grid current of the final amplifier should be checked by connecting the meter between point "B" and ground. A minimum of 3 ma. of grid current should be observed when the exciter circuits are properly tuned. Plate voltage should be applied to the 6360 amplifier and an automobile headlight lamp connected to the coaxial output plug. A 100 ma. d-c milliammeter should be placed in the plate voltage lead to the 6360 amplifier. C_4 should be tuned for resonance or minimum plate current indication, and the antenna resonating capacitor, C_5 should be adjusted for maximum bulb brilliance with an amplifier plate current not exceeding 70 ma. The coupling between L_6 and L_7 should be adjusted for proper plate current reading. Always re-resonate C_4 after changes are made to C_5 or the coupling between L_6 and L_7.

As a final check for stability, remove the plate and screen voltages from the 6360 amplifier tube. Apply excitation to the tube and closely watch the grid current as measured at point "B" when the plate tuning capacitor is tuned through resonance. If any flicker of the grid meter is noted, it will be necessary to place a small shield across the socket of the 6360 between the grid and the plate coils. This shield should be 3" long and 2" high and may be made of thin flashing copper. It should be fastened to the center socket con-



D.C. CIRCUIT A.C. CIRCUIT

Figure 20
RELAY CIRCUITS FOR MODULATOR UNIT

nection and grounded to each side socket bolt. In this particular transmitter, no such shield was needed.

Modulator Unit for the 1¼ Meter Transmitter The modulator unit for the 1¼ transmitter is built upon a separate 9½"x 5"x 3" chassis, and it may be used with any piece of low power transmitting equipment. It is capable of an output of 12 watts, and may be used to modulate amplifiers running a maximum input of 25 watts. The modulator and transmitter may be powered by a 300 volt, 200 ma. vibrator supply, or by an a-c operated supply delivering the same voltage and current. Either six volt filament or twelve volt filament tubes may be used in the modulator, the choice depending upon the available primary source of power. The modulator unit has sufficient gain for operation from a crystal microphone, and a three circuit microphone jack is used to permit "push-to-talk" operation of the transmitter. The circuit of the modulator is shown in figure 19, and the relay control circuits for both a-c and d-c operation are shown in figure 20. A 0-100 d-c milliammeter is incorporated in the plate voltage lead to the final amplifier stage for use in tuning and loading the transmitter.

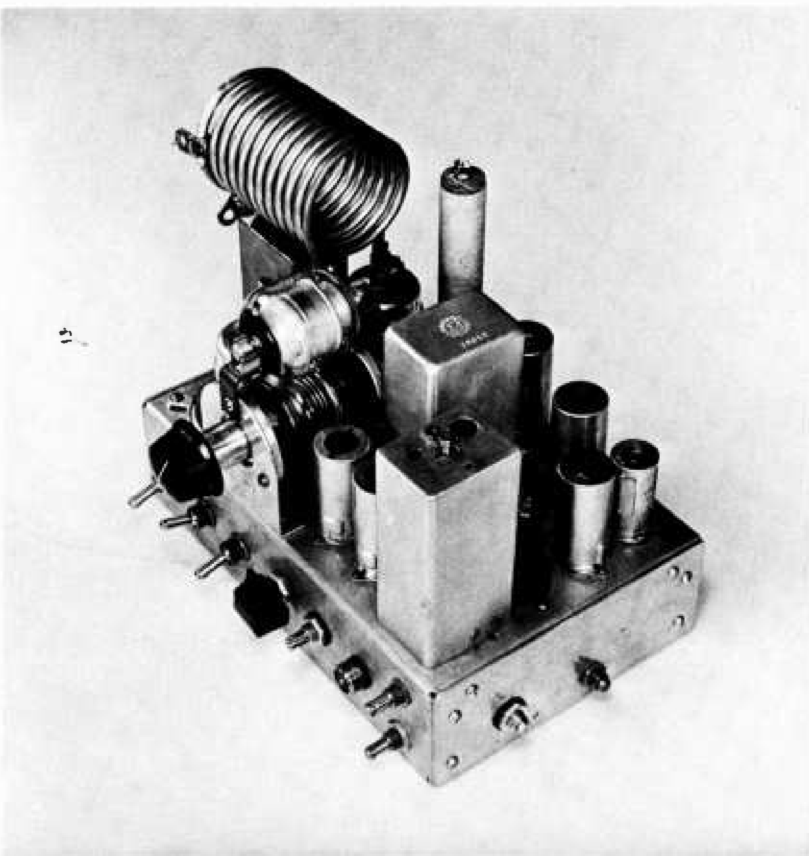
23-8 A One Kilowatt SSB Mobile Transmitter

The transmitter illustrated in figures 21, 22 and 23 was designed by Jo E. Jennings, W6EI and built by E. Alvernaz, W6DMN. It is designed to deliver a one kilowatt peak power single-sideband signal for mobile 75 meter phone operation. The transmitter employs a low powered phasing exciter driving two *Eimac*

Figure 21

A ONE KILOWATT SINGLE SIDEBAND TRANSMITTER USING THE NEW EIMAC X-531 (4W-300B) WATER COOLED TETRODES

The entire transmitter is built on a 7" x 12" x 2" chassis



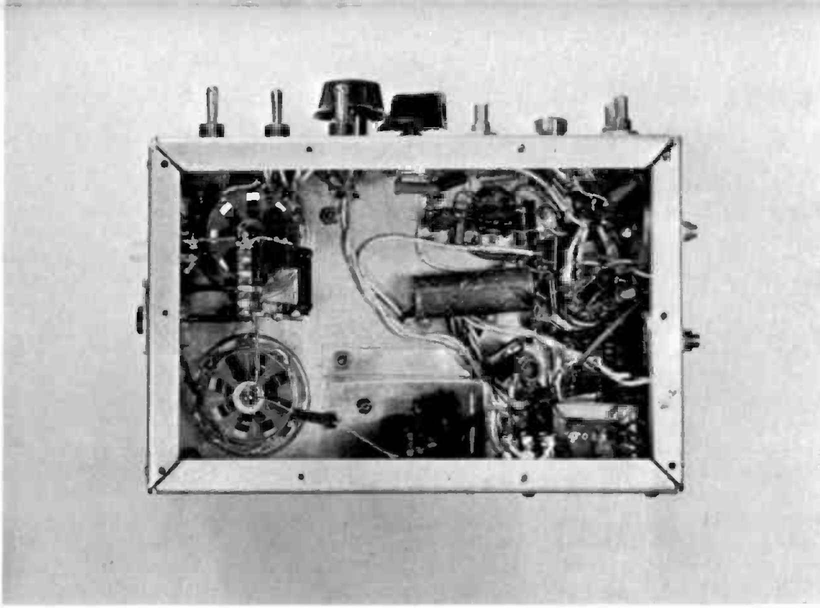


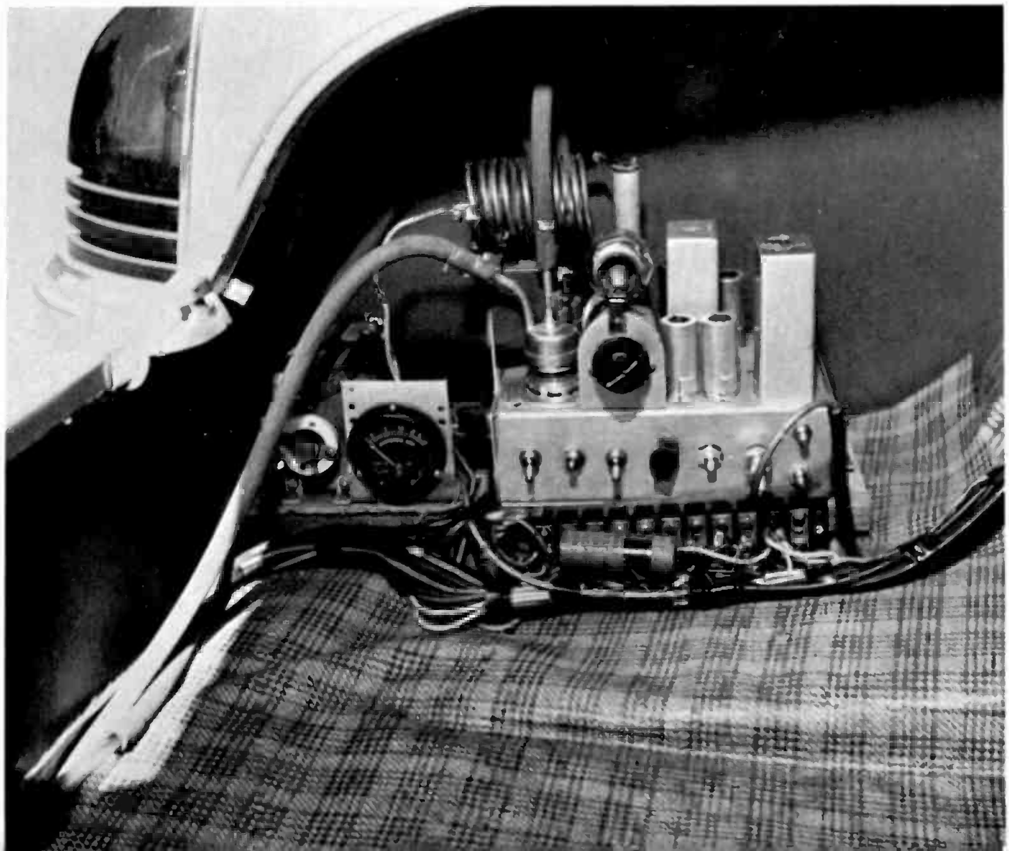
Figure 22

BOTTOM VIEW OF TRANSMITTER WITH BOTTOM COVER REMOVED TO SHOW PLACEMENT OF PARTS

Figure 23

THE ONE-KILOWATT TRANSMITTER INSTALLED IN THE TURTLEBACK

An antenna ammeter and rotary loading coil facilitate optimum tuning of the center loaded whip antenna. The two water cooled X-531 tubes are mounted on the left of the transmitter chassis.



X-531 water-cooled tetrodes in parallel as a linear amplifier. The power supply is a Leece-Neville three-phase alternator driven by a fan belt directly from the automobile engine. The three-phase voltage is stepped up to 3000 volts d.c. for operation of the linear amplifier. Power for the SSB exciter is obtained from a 300 volt, 100 ma. a-c power supply. With the exception of the control relays, filaments of the tubes, and the mobile receiver, all primary power is supplied by the three-phase supply. Approximately 70 watts of power are required from the car battery, and an auxiliary rectifier and voltage regulator operating from the three-phase alternator insure that the car battery is under proper charge at all times.

The Transmitter Layout A general view of the transmitter is shown in figure 21. The transmitter is completely constructed on a 7"x 12"x 2" aluminum chassis, as shown in figures 22 and 23. From left to right along the back edge of the chassis (figure 24) are the 6CL6 linear buffer stage, the 12AT7 low level audio stage and the 6C4 speech amplifier. Directly in front of the 6C4 is the 12AT7 cathode follower, and in front of this tube is the 1N71 plug-in diode assembly. At the front right hand corner is the oscillator coil, L_1. To the left of this is the 12AU7 oscillator and the 75 meter crystal which is placed within a tube shield as isolation from the r-f field of the high powered tank circuit to the left of it.

Parallel to the left side of the chassis are the two Eimac X-531 water cooled tetrodes. Directly to the right of the back tetrode is mounted the high voltage choke. The output tank circuit is mounted above and to the right of the tetrodes. The circuit of the complete transmitter is shown in figure 25.

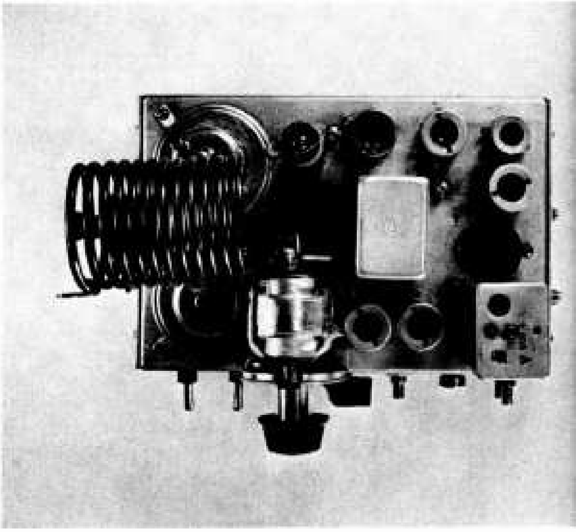
The Linear Amplifier The linear amplifier is unusual in that it employs two of the new Eimac X-531 water cooled tetrodes. These tubes are similar to the 4X-150A in construction and in electrical rating, and two of them will handle a peak input of one kilowatt SSB with ease. The X-531 tubes were chosen in place of the more widely known 4X-150A's since an air blower for the proper operation of the 4X-150A tubes would require 8 amperes of current at 6 volts. In addition, the plate dissipation of the X-531 tubes is almost double that of the air cooled version. The water cooling system, although unfamiliar to most amateurs is relatively simple. A Stewart-Warner fuel pump is employed to pump the water from a reservoir through rubber tubes to the X-531 tetrodes and back through other tubes to the reservoir. The reservoir is made from a surplus G.I. gasoline can, and 5/8" high-vacuum rubber tubing is used for the hoses which carry distilled water to the tubes. The temperature of the water is under 100° F even when the transmitter is operated for extended periods of time. The water jackets of the tubes are connected in series as shown in figure 26. It was found by experiment that it was not necessary to have any other form of cooling medium to operate the tubes at a safe temperature. The Stewart-Warner fuel pump draws a current of 0.2 amperes at maximum pumping speed. It is mounted in a rear corner of the turtle-back, along with the G.I. water can. The pump motor is connected so that it starts as soon as filament voltage is applied to the two X-531 tubes.

The plate circuit of the linear amplifier is composed of a Jennings UCS-3-250 variable vacuum capacitor shunted with a Jennings JCS-250 fixed vacuum capacitor providing a circuit capacitance of 450 $\mu\mu$fd. at resonance in the 75 meter band. A tap is taken off this coil about two turns from the ground end to match the 52 ohm coaxial feed line for the loaded whip antenna. The rubber hoses isolate the r-f and d-c circuits from ground.

The High Voltage Supply Shown in figure 27 is the Leece-Neville three-phase alternator mounted atop the engine block, and driven with a fan belt. The

Figure 24

TOP VIEW OF THE SSB TRANSMITTER



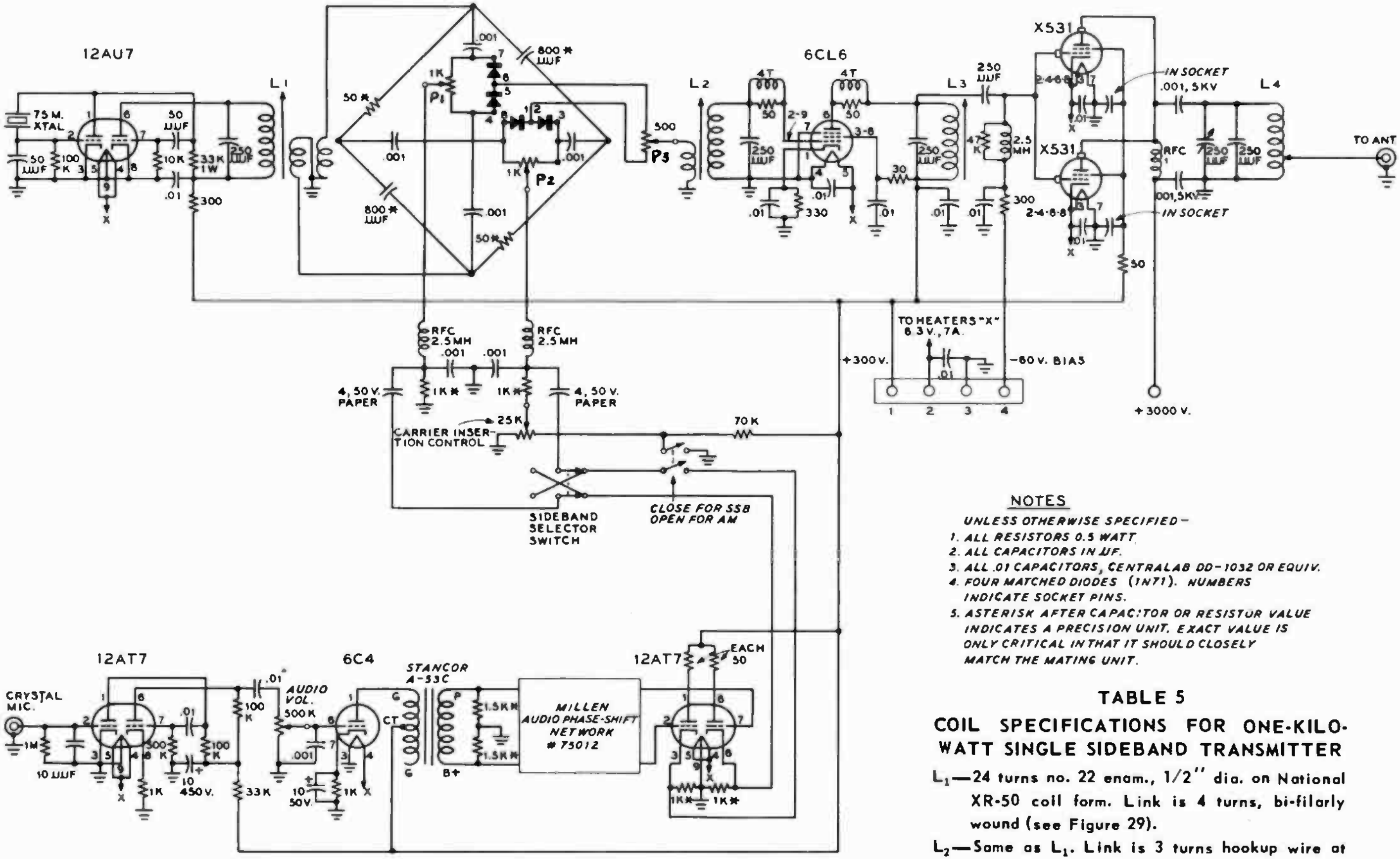


Figure 25
SCHEMATIC OF ONE-KILOWATT SINGLE SIDEBAND TRANSMITTER

TABLE 5
COIL SPECIFICATIONS FOR ONE-KILOWATT SINGLE SIDEBAND TRANSMITTER

L_1—24 turns no. 22 enam., 1/2" dia. on National XR-50 coil form. Link is 4 turns, bi-filarly wound (see Figure 29).

L_2—Same as L_1. Link is 3 turns hookup wire at ground end of L_2.

L_3—Same as L_1. No link.

L_4—12 turns 3/16" copper tubing, 3" i.d., 4" long.

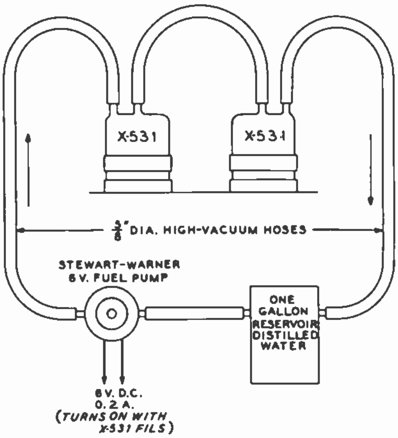


Figure 26

WATER CIRCULATION SYSTEM FOR X-531 (4W-300B) TUBES

voltage regulator and rectifier for charging the battery from the a-c system are mounted in the front of the car radiator. The alternator provides a balanced delta output circuit (figure 28). In such a system the line voltage is equal to the coil voltage, but the line current is $\sqrt{3}$ times the coil current. The coil voltage of the alternator is a nominal 6 volts RMS, and three conventional 6.3 volt 25 ampere filament transformers may be connected in delta on the primary and secondary windings to step the 6 volts up to three-phase 110 volts. In this installation, a special three-phase 6 volt to 110 volt step-up transformer was wound, since insufficient space under the hood of the car prevented the use of three filament transformers connected in delta. The three-phase 110 volts is carried through a standard 3-conductor rubber covered cable to the high voltage power supply located in the back of the car.

The three-phase high voltage supply (figure 28) uses three plate transformers, each having a 120 volt primary and a 2200 volt center

Figure 27

THE LEECE-NEVILLE THREE-PHASE ALTERNATOR IS DRIVEN BY THE AUTOMOBILE ENGINE VIA AN AUXILIARY FAN BELT

Visible at right is the three-phase 6-volt step-up transformer. The battery charging rectifier is located in front of the radiator at right.

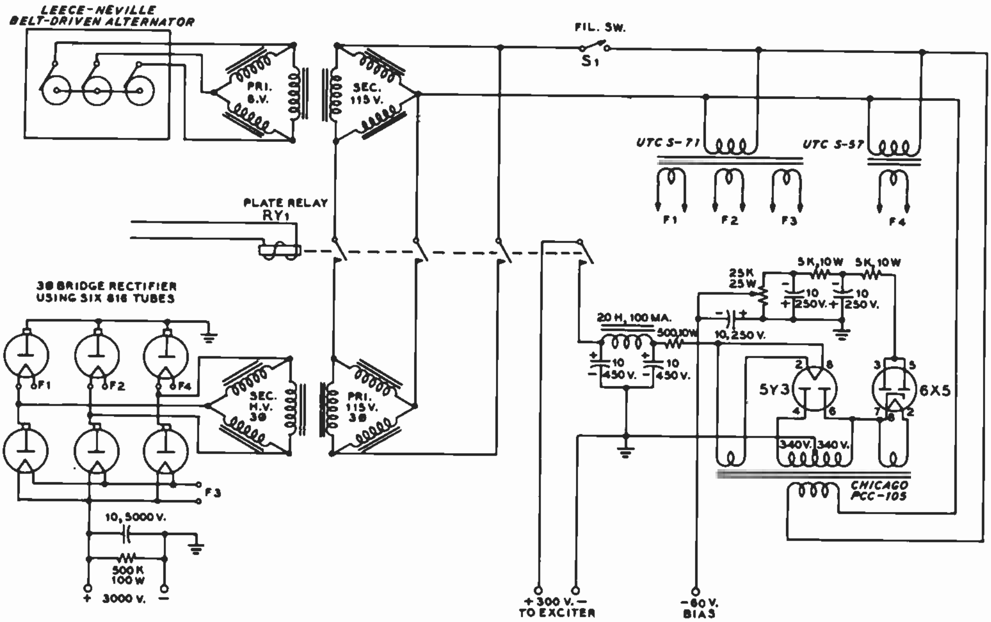


Figure 28
THREE-PHASE HIGH VOLTAGE SUPPLY FOR SSB TRANSMITTER

tapped secondary. The center tap is not used. Each transformer should be capable of supplying 100 milliamperes, or 1/3 of the peak load on the power supply. The U.T.C. type S-46 is acceptable for this service, although the output voltage of the supply will be slightly less than 3000 volts when these transformers are employed.

Since the ripple frequency is quite high in this type of supply no filter choke is necessary. A 10 μfd., 3000 volt filter capacitor is employed to prevent the heavy peak current of the linear stage from impairing the dynamic regulation of the power supply.

Four filament transformers are needed for the six type 816 rectifier tubes used in the three-phase rectifier. A U.T.C. type S-71 filament transformer may be used to energize the three 816's in the positive leg of the bridge supply, and two of the other 816's. A U.T.C. type S-57 filament transformer may be used to energize the remaining 816 tube.

It is necessary to determine the correct phasing of both the primary and secondary windings of all transformers that are used in the delta connection. When the transformers are phased properly, there will be very little primary current drawn from the three phase circuit with no secondary load. If one of the transformers is phased improperly, the load current will be excessive, and the transformer will be damaged quickly.

To correctly phase the 6 volt/110 volt transformers, a headlight bulb should be placed in series with each of the 6 volt leads to the transformer. The secondary windings should then be connected in delta, and three-phase power applied to the primary circuit. If the primary lamps light unevenly, it is a sign that the secondary windings are not phased properly. The connections to one secondary winding at a time should be reversed until the three lamps are equally (and dimly) illuminated. The same procedure may be applied to the high voltage transformers. 200 watt lamp bulbs should be placed in series with each primary lead to the delta, and the secondary windings connected in such a way as to produce minimum primary current with no secondary load on the transformers. CAUTION! Do not touch the secondary terminals when the three-phase supply is in operation as these terminals are at extremely high potential!

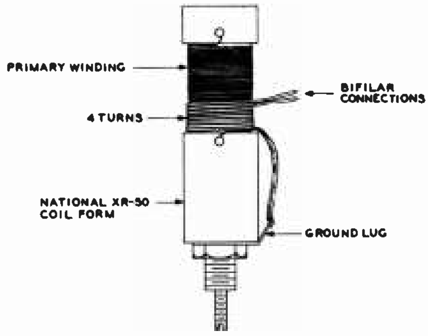
The SSB Exciter The SSB exciter is a low power phasing-type unit, previously described in Chapter 14 of this

Handbook. A balanced diode (1N71) is employed as a modulator unit, operating directly in the 75 meter region. A 12AU7 tube is employed as a Pierce crystal oscillator using a 75 meter crystal. The second half of this tube is used as a tuned buffer-amplifier. A low impedance bifilar winding is employed between the tuned circuit of the buffer and the low impedance 1N71 modulator. Construction of this bifilar coil is shown in figure 29. The output of the modulator is link coupled to a 6CL6 tube operating as a Class AB_1 amplifier stage. The peak output of the 6CL6 stage is about 3 watts.

Construction and Alignment Figures 22 and 24 show the placement of the major parts in this transmitter. Since space is at a premium, most small components are mounted by their leads directly to the pins of the associated tube sockets, or are mounted on insulated terminal strips placed adjacent to the sockets. A small shield is placed around the grid circuit of the 6CL6 buffer to isolate the low power audio circuits from the r-f field. The X-531 tubes are mounted in Eimac 4X150A/4011 Air system sockets (grounded cathode type).

The variable vacuum capacitor is mounted on a small aluminum angle bracket, and the fixed vacuum capacitor is attached to the top of this bracket by means of small fuse clips. The "hot" end of the plate coil is attached to a clip joining the two vacuum capacitors, and the opposite end of the coil is grounded to the transmitter chassis by a wide copper strap.

When the transmitter is wired and checked, the exciter portion is tested with the X-531 tubes left out of their sockets. The transmitter should be tested from a suitable 110 volt power supply on the workbench before any attempt is made to put it in the car. Coils L_1, L_2 and L_3 should be adjusted for maximum output from the 6CL6 stage, which may be temporarily loaded into a link coupled 6 volt flashlight bulb. Potentiometers P_1, P_2 and P_3 should be adjusted for maximum carrier suppression. A sine wave of 1500 cycles or so should be impressed upon the audio system and the resulting SSB carrier should be monitored in a receiver, using *no BFO*. The percentage of modulation heard upon the SSB carrier is an indication of the state of unbalance or non-linearity of the SSB system. Potentiometers P_1, P_2 and P_3 should now be touched up for minimum audio modulation, and the gain control of the speech amplifier set below the overload point of the system when the audio oscillator is adjusted to provide the same voltage level as the microphone intended for use with the SSB transmitter.



NOTE: *TWO PARALLEL PIECES OF HOOKUP WIRE ARE WOUND SIMULTANEOUSLY OVER PRIMARY WINDING TO MAKE BIFILAR SECONDARY. BOTTOM END OF EACH WINDING GROUNDED TO MOUNTING LUG ON COIL FORM.*

Figure 29
BIFILAR COIL FOR SSB TRANSMITTER

When a clean SSB is produced by the 6CL6 stage, attention may be turned to the linear amplifier.

The water cooling system should first be turned on, and left running during all tests to the linear amplifier. The bias supply to the X-531 tubes should be set at approximately -60 volts and 300 volts should be taken from the SSB exciter plate supply for the screen circuit of the linear amplifier. If possible, the linear amplifier should also be bench tested with a 3000 volt supply before the transmitter is run from the three-phase automobile system. The plate circuit of the linear amplifier should be resonated with a grid-dip oscillator and connected to a dummy load. The exciter should be modulated with a sine audio signal and plate and screen voltages should be applied to the linear amplifier which may be then tuned up much in the manner of a conventional Class C amplifier. The plate circuit may be loaded to 3000 volts at 300 ma. for a short period of time. When the audio modulation to the exciter is removed, the plate current of the X-531 tubes should drop from 300 ma. to approximately 50 milliamperes. The exact value of the resting current is dependent to a large extent upon the actual value of grid bias applied to the linear amplifier tubes. The reader is referred to the book "Single Sideband Techniques" published by Cowan Publishing Corp., 67 West 44th St., N.Y. 36, N.Y. for additional information regarding the testing and adjustment of linear amplifiers.

When the transmitter is operating properly, and the three-phase supply of the car has been tested with light bulb loads, the transmitter may be placed in the car and properly loaded

Figure 30
A CENTER LOADED 80-METER WHIP IS USED WITH THE SSB TRANSMITTER. NOTE THE ANTI-CORONA DISC AT THE TOP OF THE WHIP.

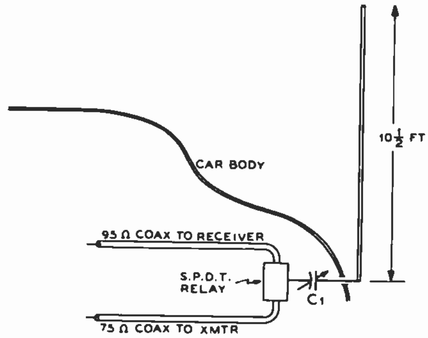


Figure 31
5/16-WAVE WHIP RADIATOR FOR 10 METERS

If a whip antenna is made slightly longer than one-quarter wave it acts as a slightly better radiator than the usual quarter-wave whip, and it can provide a better match to the antenna transmission line if the reactance is tuned out by a series capacitor close to the base of the antenna. Capacitor C_1 may be a 100-μμfd. midget variable.

to the whip antenna of the car. Care must be taken that a high efficiency antenna loading coil is used, or the high peak power of the transmitter will destroy the insulation of the coil. To prevent corona discharge from the tip of the whip antenna, copper wires formed into a ball should be soldered to the top of the whip. The ball should be about three inches in diameter (figure 30).

23-9 Antennas for Mobile Work

10-Meter Mobile Antennas The most popular mobile antenna for 10-meter operation is a rear-mounted whip approximately 8 feet long, fed with coaxial line. This is a highly satisfactory antenna, but a few remarks are in order on the subject of feed and coupling systems.

The feed point resistance of a resonant quarter-wave rear-mounted whip is approximately 20 to 25 ohms. While the standing-wave ratio when using 50-ohm coaxial line will not be much greater than 2 to 1, it is nevertheless desirable to make the line to the transmitter exactly one quarter wavelength long electrically at the center of the band. This procedure will minimize variations in loading over the band. The physical length of RG-8/U cable, from antenna base to antenna coupling coil, should be approximately 5 feet 3 inches. The antenna changeover relay preferably should be located either at the antenna end or the transmitter end of the line, but if it is more convenient physically the line may be broken anywhere for insertion of the relay.

If the same rear-mounted whip is used for broadcast-band reception, attenuation of broadcast-band signals by the high shunt capacitance of the low impedance feed line can be reduced by locating the changeover relay right at the antenna lead in, and by running 95-ohm coax (instead of 50 or 75 ohm coax) from the relay to the converter. Ordinarily this will produce negligible effect upon the operation of the converter, but usually will make a worthwhile improvement in the strength of broadcast-band signals.

A more effective radiator and a better line match may be obtained by making the whip approximately 10½ feet long and feeding it with 75-ohm coax (such as RG-11/U) via a series capacitor, as shown in figure 31. The relay and series capacitor are mounted inside the trunk, as close to the antenna feedthrough or base-mount insulator as possible. The 10½-foot length applies to the overall length from the tip of the whip to the point where the lead in passes through the car body. The leads inside the car (connecting the coaxial cable, relay, series capacitor and antenna lead) should be as short as possible. The outer conductor of both coaxial cables should be grounded to the car body at the relay end with short, heavy conductors.

A 100-$\mu\mu$fd. midget variable capacitor is suitable for C_1. The optimum setting should be determined experimentally at the center of the band. This setting then will be satisfactory over the whole band.

One suitable coupling arrangement for either a ¼-wave or 5/16-wave whip on 10 meters is to use a conventional tank circuit, inductively coupled to a "variable link" coupling loop which feeds the coaxial line. Alternatively, a pi-network output circuit may be used. If the input impedance of the line is very low and the tank circuit has a low C/L ratio, it may be necessary to resonate the coupling loop with series capacitance in order to obtain sufficient coupling. This condition often is encountered with a ¼-wave whip when the line length approximates an electrical half wavelength.

If an all-band center-loaded mobile antenna is used, the loading coil at the center of the antenna may be shorted out for operation of the antenna on the 10-meter band. The usual type of center-loaded mobile antenna will be between 9 and 11 feet long, including the center-loading inductance which is shorted out. Hence such an antenna may be shortened to an electrical quarter-wave for the 10-meter band by using a series capacitor as just discussed. Alternatively, if a pi-network is used in the plate circuit of the output stage of the mobile transmitter, any reactance presented at the antenna terminals of the transmitter by the antenna may be tuned out with the pi-network.

The All-Band Center-Loaded Mobile Antenna The great majority of mobile operation on the 14-Mc. band and below is with center loaded whip antennas. These antennas use an insulated bumper or body mount, with provision for coaxial feed from the base of the antenna to the transmitter, as shown in figure 32.

The center-loaded whip antenna must be tuned to obtain optimum operation on the desired frequency of operation. These antennas will operate at maximum efficiency over a range of perhaps 20 kc. on the 75-meter band, covering a somewhat wider range on the 40-meter band, and covering the whole 20-meter phone band. The procedure for tuning the antennas is discussed in the instruction sheet which is furnished with them, but basically the procedure is as follows:

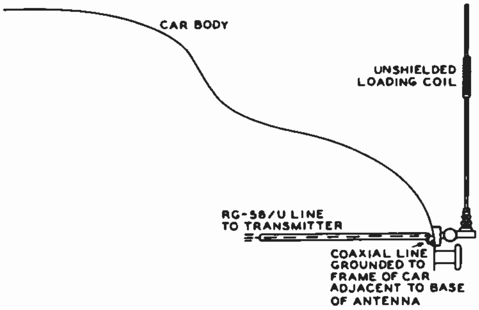


Figure 32

THE CENTER-LOADED WHIP ANTENNA

The center-loaded whip antenna, when provided with a tapped loading coil or a series of coils, may be used over a wide frequency range. The loading coil may be shorted for use of the antenna on the 10-meter band.

The antenna is installed, fully assembled, with a coaxial lead of RG-58/U from the base of the antenna to the place where the transmitter is installed. The rear deck of the car should be closed, and the car should be parked in a location as clear as possible of trees, buildings, and overhead power lines. Objects within 15 or 20 feet of the antenna can exert a considerable detuning effect on the antenna system due to its relatively high operating Q. The end of the coaxial cable which will plug into the transmitter is terminated in a link of 3 or 4 turns of wire. This link is then coupled to a grid-dip meter and the resonant frequency of the antenna determined by noting the frequency at which the grid current fluctuates. The coils furnished with the antennas normally are too large for the usual operating frequency, since it is much easier to remove turns than to add them. Turns then are removed, *one at a time*, until the antenna resonates at the desired frequency. If too many turns have been removed, a length of wire may be spliced on and soldered. Then, with a length of insulating tubing slipped over the soldered joint, turns may be added to lower the resonant fre-

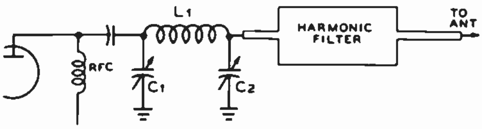


Figure 33
PI-NETWORK ANTENNA COUPLER

The pi-network antenna coupler is particularly satisfactory for mobile work since the coupler affords some degree of harmonic reduction, provides a coupling variation to meet varying load conditions caused by frequency changes, and can cancel out reactance presented to the transmitter at the end of the antenna transmission line.

For use of the coupler on the 3.9-Mc. band C_1 should have a maximum capacitance of about 250 μμfd., L_1 should be about 9 microhenrys (30 turns 1" dia. by 2" long), and C_2 may include a fixed and a variable element with maximum capacitance of about 1400 μμfd. A 100-μμfd. variable capacitor will be suitable at C_1 for the 14-Mc. and 28-Mc. bands, with a 350-μμfd. variable at C_2. Inductor L_1 should have an inductance of about 2 microhenrys (11 turns 1" dia. by 1" long) for the 14-Mc. band, and about 0.8 microhenry (6 turns 1" dia. by 1" long) for the 28-Mc. band.

quency. Or, if the tapped type of coil is used, taps are changed until the proper number of turns for the desired operating frequency is found. This procedure is repeated for the different bands of operation.

Feeding the Center-Loaded Antenna After much experimenting it has been found that the most satisfactory method for feeding the coaxial line to the base of a center-loaded antenna is with the pi-network coupler. Figure 33 shows the basic arrangement, with recommended circuit constants. It will be noted that relatively large values of capacitance are required for all bands of operation, with values which seem particularly large for the 75-meter band. But reference to the discussion of pi-network tank circuits in Chapter Eleven will show that the values suggested are normal for the values of impedance, impedance transformation, and operating Q which are encountered in a mobile installation of the usual type.

23-10 Construction and Installation of Mobile Equipment

It is recommended that the following measures be taken when constructing mobile equipment, either transmitting or receiving, to ensure trouble-free operation over long periods:

Use only a stiff, heavy chassis unless the chassis is quite small.

Use lock washers or lock nuts when mounting components by means of screws.

Use stranded hook-up wire except where r-f considerations make it inadvisable (such as for instance the plate tank circuit leads in a v-h-f amplifier). Lace and tie leads wherever necessary to keep them from vibrating or flopping around.

Unless provided with gear drive, tuning capacitors in the large sizes will require a rotor lock.

Filamentary (quick heating) tubes should be mounted only in a vertical position.

The larger size carbon resistors and mica capacitors should not be supported from tube socket pins, particularly from miniature sockets. Use tie points and keep the resistor and capacitor "pigtails" short.

Generally speaking, rubber shock mounts are unnecessary or even undesirable with passenger car installations, or at least with full size passenger cars. The springing is sufficiently "soft" that well constructed radio equipment can be bolted directly to the vehicle without damage from shock or vibration. Unless shock mounting is properly engineered as to the stiffness and placement of the shock mounts, mechanical-resonance "amplification" effects may actually cause the equipment to be shaken more than if the equipment were bolted directly to the vehicle.

Surplus military equipment provided with shock or vibration mounts was intended for use in aircraft, jeeps, tanks, gun-firing Naval craft, small boats, and similar vehicles and craft subject to severe shock and vibration. Also, the shock mounting of such equipment is very carefully engineered in order to avoid harmful resonances.

To facilitate servicing of mobile equipment, all interconnecting cables between units should be provided with separable connectors on at least one end.

Control Circuits The send-receive control circuits of a mobile installation are dictated by the design of the equipment, and therefore will be left to the ingenuity of the reader. However, a few generalizations and suggestions are in order.

Do not attempt to control too many relays, particularly heavy duty relays with large coils, by means of an ordinary push-to-talk switch on a microphone. These contacts are not designed for heavy work, and the inductive kick will cause more sparking than the contacts on the microphone switch are designed to handle. It is better to actuate a single relay with the push-to-talk switch and then control all other relays, including the heavy duty contactor for the dynamotor or vibrator pack, with this relay.

The procedure of operating only one relay directly by the push-to-talk switch, with all other relays being controlled by this control relay, will eliminate the often-encountered difficulty where the shutting down of one item of equipment will *close* relays in other items as a result of the coils of relays being placed in series with each other and with heater circuits. A recommended general control circuit, where one side of the main control relay is connected to the hot 6-volt circuit, but all other relays have one side connected to ground, is illustrated in figure 34. An additional advantage of such a circuit is that only one control wire need be run to the coil of each additional relay, the other side of the relay coils being grounded.

The heavy-duty 6-volt solenoid-type contactor relays such as provided on the PE-103A and used for automobile starter relays usually draw from 1.5 to 2 amperes. While somewhat more expensive, heavy-duty 6-volt relays of conventional design, capable of breaking 30 amperes at 6 volts d.c., are available with coils drawing less than 0.5 ampere.

When purchasing relays keep in mind that the current rating of the contacts is not a fixed value, but depends upon (1) the voltage, (2) whether it is a.c. or d.c., and (3) whether the circuit is purely resistive or is inductive. If in doubt, refer to the manufacturer's recommendations. Also keep in mind that a dynamotor presents almost a dead short until the armature starts turning, and the starting relay should be rated at considerably more than the normal dynamotor current.

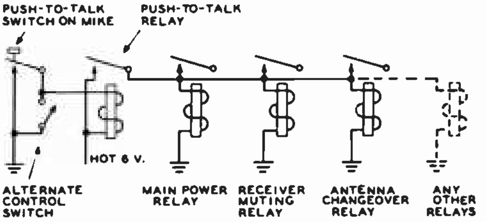


Figure 34

RELAY CONTROL CIRCUIT

Simplified schematic of the recommended relay control circuit for mobile transmitters. The relatively small push-to-talk relay is controlled by the button on the microphone or the communications switch. Then one of the contacts on this relay controls the other relays of the transmitter; one side of the coil of all the additional relays controlled should be grounded.

Microphones and Circuits The most generally used microphone for mobile work is the single-button carbon. With a high-output-type microphone and a high-ratio microphone transformer, it is possible when "close talking" to drive even a pair of push-pull 6L6's without resorting to a speech amplifier. However, there is a wide difference in the output of the various type single button microphones, and a wide difference in the amount of step up obtained with different type microphone transformers. So at least one speech stage usually is desirable.

One of the most satisfactory single button microphones is the standard Western Electric type F-1 unit (or Automatic Electric Co. equivalent). This microphone has very high output when operated at 6 volts, and good fidelity on speech. When used without a speech amplifier stage the microphone transformer should have a 50-ohm primary (rather than 200 or 500 ohms) and a secondary of at least 150,000 ohms and preferably 250,000 ohms.

The widely available surplus type T-17 microphone has higher resistance (200 to 500 ohms) and lower output, and usually will require a stage of speech amplification except when used with a very low power modulator stage.

Unless an F-1 unit is used in a standard housing, making contact to the button presents somewhat of a problem. No serious damage will result from soldering to the button if the connection is made to one edge and the soldering is done very rapidly with but a small amount of solder, so as to avoid heating the whole button.

A sound-powered type microphone removed from one of the chest sets available in the surplus market will deliver almost as much voltage to the grid of a modulator stage when used with a high-ratio microphone transformer as will an F-1 unit, and has the advantage of not requiring button current or a "hash filter." This is simply a dynamic microphone designed for high output rather than maximum fidelity.

The standardized connections for a single-button carbon microphone provided with push-to-talk switch are shown in figure 35. Practically all hand-held military-type single-button

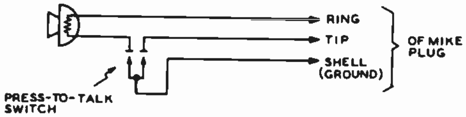


Figure 35
STANDARD CONNECTIONS FOR THE PUSH-TO-TALK SWITCH ON A HAND-HELD SINGLE-BUTTON CARBON MICROPHONE

microphones on the surplus market use these connections.

There is an increasing tendency among mobile operators toward the use of microphones having better frequency and distortion characteristics than the standard single-button type. The high-impedance dynamic type is probably the most popular, with the *ceramic*-crystal type next in popularity. The conventional crystal type is not suitable for mobile use since the crystal unit will be destroyed by the high temperatures which can be reached in a closed car parked in the sun in the summer time.

The use of low-level microphones in mobile service requires careful attention to the elimination of common-ground circuits in the microphone lead. The ground connection for the shielded cable which runs from the transmitter to the microphone should be made at only one point, preferably directly adjacent to the grid of the first tube in the speech amplifier. The use of a low-level microphone usually will require the addition of two speech stages (a pentode and a triode), but these stages will take only a milliampere or two of plate current, and 150 ma. per tube of heater current.

PE-103A Dynamotor Power Unit Because of its availability on the surplus market at a low price and its suitability for use with about as powerful a mobile transmitter as can be employed in a passenger car without resorting to auxiliary batteries or a special generatof, the PE-103A is probably the most widely used dynamotor for amateur work. Therefore some useful information will be given on this unit.

The nominal rating of the unit is 500 volts and 160 ma., but the output voltage will of course vary with load and is slightly higher with the generator charging. Actually the 160 ma. rating is conservative, and about 275 ma. can be drawn intermittently without overheating, and without damage or excessive brush or commutator wear. At this current the unit should not be run for more than 10 minutes at a time, and the average "on" time should not be more than half the average "off" time.

The output voltage vs. current drain is shown approximately in figure 36. The exact voltage will depend somewhat upon the loss resistance of the primary connecting cable and whether or not the battery is on charge. The primary current drain of the dynamotor proper (excluding relays) is approximately 16 amperes at 100 ma., 21 amperes at 160 ma., 26 amperes at 200 ma., and 31 amperes at 250 ma.

Only a few of the components in the base are absolutely necessary in an amateur mobile installation, and some of them can just as well be made an integral part of the transmitter if desired. The base can be removed for salvage components and hardware, or the dynamotor may be purchased without base.

To remove the base proceed as follows: Loosen the four thumb screws on the base plate and remove the cover. Remove the four screws holding the dynamotor to the base plate. Trace the four wires coming out of the dynamotor to their terminals and free the lugs. Then these four wires can be pulled through the two rubber grommets in the base plate when the dynamotor is separated from the base plate. It may be necessary to bend the eyelets in the large lugs in order to force them through the grommets.

Next remove the two end housings on the dynamotor. Each is held with two screws. The high-voltage commutator is easily identified by its narrower segments and larger diameter. Next to it is the 12-volt commutator. The 6-volt commutator is at the other end of the armature. The 12-volt brushes should be removed when only 6-volt operation is planned, in order to reduce the drag.

If the dynamotor portion of the PE-103A power unit is a Pioneer type VS-25 or a Russell type 530- (most of them are), the wires to the 12-volt brush holder terminals can be cross connected to the 6-volt brush holder terminals with heavy jumper wires. One of the wires disconnected from the 12-volt brush terminals is the primary 12-volt pigtail and will come free. The other wire should be connected to the opposite terminal to form one of the jumpers.

With this arrangement it is necessary only to remove the 6-volt brushes and replace the 12-volt brushes in case the 6-volt commutator becomes excessively dirty or worn or starts throwing solder. No difference in output voltage will be noted, but as the 12-volt brushes are not as heavy as the 6-volt brushes it is not permissible to draw more than about 150 ma. except for emergency use until the 6-volt commutator can be turned down or repaired.

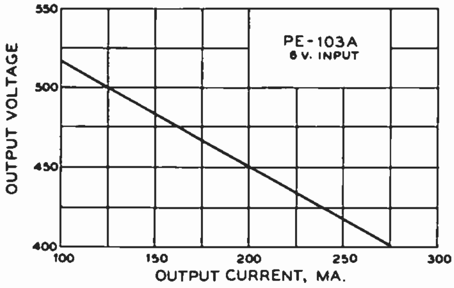


Figure 36
APPROXIMATE OUTPUT VOLTAGE VS. LOAD CURRENT FOR A PE-103A DYNAMOTOR

At 150 ma. or less the 12-volt brushes will last almost as long as the 6-volt brushes.

The reason that these particular dynamotors can be operated in this fashion is that there are two 6-volt windings on the armature, and for 12-volt operation the two are used in series with both commutators working. The arrangement described above simply substitutes for the regular 6-volt winding the winding and commutator which ordinarily came into operation only on 12-volt operation. Some operators have reported that the regulation of the PE-103A may be improved by operating both commutators in parallel with the 6-volt line.

The three wires now coming out of the dynamotor are identified as follows: The smaller wire is the positive high voltage. The heavy wire leaving the same grommet is positive 6 volts and negative high voltage. The single heavy wire leaving the other grommet is negative 6 volts. Whether the car is positive or negative ground, negative high voltage can be taken as car-frame ground. With the negative of the car battery grounded, the plate current can return through the car battery and the armature winding. This simply puts the 6 volts in series with the 500 volts and gives 6 extra volts plate voltage.

The trunk of a car gets very warm in summer, and if the transmitter and dynamotor are mounted in the trunk it is recommended that the end housings be left off the dynamotor to facilitate cooling. This is especially important in hot climates if the dynamotor is to be loaded to more than 200 ma.

When replacing brushes on a PE-103A check to see if the brushes are marked negative and positive. If so, be sure to install them accordingly, because they are not of the same material. The dynamotor will be marked to show which holder is negative.

When using a PE-103A, or any dynamotor for that matter, it may be necessary to devote one set of contacts on one of the control relays to breaking the plate or screen voltage to the transmitter oscillator, if these are supplied by the dynamotor, because the output of a dynamotor takes a moment to fall to zero when the primary power is removed.

23-11 Vehicular Noise Suppression

Satisfactory reception on frequencies above the broadcast band usually requires greater attention to noise suppression measures. The required measures vary with the particular vehicle and the frequency range involved.

Most of the various types of noise that may be present in a vehicle may be broken down into the following main categories:

(1) Ignition noise.

(2) Wheel static (tire static, brake static, and intermittent ground via front wheel bearings).

(3) "Hash" from voltage regulator contacts.

(4) "Whine" from generator commutator segment make and break.

(5) Static from scraping connections between various parts of the car.

There is no need to suppress ignition noise completely, because at the higher frequencies ignition noise from passing vehicles makes the use of a noise limiter mandatory anyway. However, the limiter should not be given too much work to do, because at high engine speeds a noisy ignition system will tend to mask weak signals, even though with the limiter working, ignition "pops" may appear to be completely eliminated.

Another reason for good ignition suppression at the source is that strong ignition pulses contain enough energy when integrated to block the a-v-c circuit of the receiver, causing the gain to drop whenever the engine is speeded up. Since the a-v-c circuits of the receiver obtain no benefit from a noise clipper, it is important that ignition noise be suppressed enough at the source that the a-v-c circuits will not be affected even when the engine is running at high speed.

Ignition Noise The following procedure should be found adequate for reducing the ignition noise of practically any passenger car to a level which the clipper can handle satisfactorily at any engine speed at any frequency from 500 kc. to 148 Mc. Some of the measures may already have been taken when the auto receiver was installed.

First either install a spark plug suppressor on each plug, or else substitute Autolite resistor plugs. The latter are more effective than suppressors, and on some cars ignition noise is reduced to a satisfactory level simply by installing them. However, they may not do an adequate job alone after they have been in use for a while, and it is a good idea to take the following additional measures.

Check all high tension connections for gaps, particularly the "pinch fit" terminal connectors widely used. Replace old high tension wiring that may have become leaky.

Check to see if any of the high tension wiring is cabled with low tension wiring, or run in the same conduit. If so, reroute the low tension wiring to provide as much separation as practicable.

By-pass to ground the 6-volt wire from the ignition coil to the ignition switch at each end with a 0.1-μfd. molded case paper capacitor in parallel with a .001-μfd. mica or ceramic, using the shortest possible leads.

Check to see that the hood makes a good ground contact to the car body at several points. Special grounding contactors are available for attachment to the hood lacings on cars that otherwise would present a grounding problem.

If the high-tension coil is mounted on the dash, it may be necessary to shield the high tension wire as far as the bulkhead, unless it already is shielded with armored conduit.

Wheel Static Wheel static is either static electricity generated by rotation of the tires and brake drums, or is noise generated by poor contact between the front wheels and the axles (due to the grease in the bearings). The latter type of noise seldom is caused by the rear wheels, but tire static may of course be generated by all four tires.

Wheel static can be eliminated by insertion of grounding springs under the front hub caps, and by inserting "tire powder" in all inner tubes. Both items are available at radio parts stores and from most auto radio dealers.

Voltage Regulator Hash Certain voltage regulators generate an objectionable amount of "hash" at the higher frequencies, particularly in the v-h-f range. A large by-pass will affect the operation of the regulator and possibly damage the points. A small by-pass can be used, however, without causing trouble. At frequencies above the frequency at which the hash becomes objectionable (approximately 20 Mc. or so) a small by-pass is quite effective. A 0.001-μfd. mica capacitor placed from the field terminal of the regulator to ground with the shortest possible leads often will produce sufficient improvement. If not, a choke consisting of about 60 turns of no. 18 d.c.c. or bell wire wound on a ¾-inch form can be added. This should be placed right at the regulator terminal, and the 0.001-μfd. by-pass placed from the generator side of the choke to ground.

Generator Whine Generator "whine" often can be satisfactorily suppressed from 550 kc. to 148 Mc. simply by by-passing the armature terminal to ground with a special "auto radio" by-pass of 0.25 or 0.5 μfd. in parallel with a 0.001-μfd. mica or ceramic capacitor. The former usually is placed on the generator when an auto radio is installed, but must be augmented by a mica or ceramic capacitor with short leads in order to be effective at the higher frequencies as well as on the broadcast band.

When more drastic measures are required, special filters can be obtained which are designed for the purpose. These are recommended for stubborn cases when a wide frequency range is involved. For reception only over a comparatively narrow band of frequencies, such as the 10-meter amateur band, a highly effective filter can be improvised by connecting between the previously described parallel by-pass capacitors and the generator armature terminal a resonant choke. This may consist of no. 10 enamelled wire wound on a suitable form and shunted with an adjustable trimmer capacitor to permit resonating the combination to the center of the frequency band involved. For the 10-meter band 11 turns close wound on a one-inch form and shunted by a 3-30 $\mu\mu$fd. compression-type mica trimmer is suitable. The trimmer should be adjusted experimentally at the center frequency.

When generator whine shows up after once being satisfactorily suppressed, the condition of the brushes and commutator should be checked. Unless a by-pass capacitor has opened up, excessive whine usually indicates that the brushes or commutator are in need of attention in order to prevent damage to the generator.

Body Static Loose linkages or body or frame joints anywhere in the car are potential static producers when the car is in motion, particularly over a rough road. Locating the source of such noise is difficult, and the simplest procedure is to give the car a thorough tightening up in the hope that the offending poor contacts will be caught by the procedure. The use of braided bonding straps between the various sections of the body of the car also may prove helpful.

Miscellaneous There are several other potential noise sources on a passenger vehicle, but they do not necessarily give trouble and therefore require attention only in some cases.

The heat, oil pressure, and gas gauges can cause a rasping or scraping noise. The gas gauge is the most likely offender. It will cause trouble only when the car is rocked or is in motion. The gauge units and panel indicators should both be by-passed with the 0.1-μfd. paper and 0.001-μfd. mica or ceramic combination previously described.

At high car speeds under certain atmospheric conditions corona static may be encountered unless means are taken to prevent it. The receiving-type auto whips which employ a plastic ball tip are so provided in order to minimize this type of noise, which is simply a discharge of the frictional static built up on the car. A whip which ends in a relatively sharp metal point makes an ideal discharge point for the static charge, and will cause corona trouble at a much lower voltage than if the tip were hooded with insulation. A piece of Vinylite sleeving slipped over the top portion of the whip and wrapped tightly with heavy thread will prevent this type of static discharge under practically all conditions. An alternative arrangement is to wrap the top portion of the whip with *Scotch* brand *electrical* tape.

Generally speaking it is undesirable from the standpoint of engine performance to use both spark-plug suppressors *and* a distributor suppressor. Unless the distributor rotor clearance is excessive, noise caused by sparking of the distributor rotor will not be so bad but what it can be handled satisfactorily by a noise limiter. If not, it is preferable to shield the hot lead between ignition coil and distributor rather than use a distributor suppressor.

In many cases the control rods, speedometer cable, etc., will pick up high-tension noise under the hood and conduct it up under the dash where it causes trouble. If so, all control rods and cables should be bonded to the fire wall (bulkhead) where they pass through, using a short piece of heavy flexible braid of the type used for shielding.

In some cases it may be necessary to bond the engine to the frame at each rubber engine mount in a similar manner. If a rear mounted whip is employed the exhaust tail pipe also should be bonded to the frame if supported by rubber mounts.

Locating Noise Sources Determining the source of certain types of noise is made difficult when several things are contributing to the noise, because elimination of one source often will make little or no apparent difference in the total noise. The following procedure will help to isolate and identify various types of noise.

Ignition noise will be present only when the ignition is on, even though the engine is turning over.

Generator noise will be present when the motor is turning over, regardless of whether the ignition switch is on. Slipping the drive belt off will kill it.

Gauge noise usually will be present only when the ignition switch is on or in the "left" position provided on some cars.

Wheel static when present will persist when the car clutch is disengaged and the ignition switch turned off (or to the left position), with the car coasting.

Body noise will be noticeably worse on a bumpy road than on a smooth road, particularly at low speeds.

CHAPTER TWENTY FOUR

Receiving Equipment

Receiver construction has just about become a lost art. Excellent general coverage receivers are available on the market in many price ranges. However, even the most modest of these receivers is relatively expensive, and most of the receivers are designed as a compromise—they must suit the majority of users, and they must be designed with an eye to the price.

It is a tribute to the receiver manufacturers that they have done as well as they have. Even so, the c-w man must often pay for a high-fidelity audio system and S-meter he never uses, and the phone man must pay for the c-w man's crystal filter. For one amateur, the receiver has too much bandspread; for the next, too little. For economy's sake and for ease of alignment, low-Q coils are often found in the r-f circuits of commercial receivers, making the set a victim of cross-talk and overloading from strong local signals. Rarely does the purchaser of a commercial receiver realize that he could achieve the results he desires in a home-built receiver *if* he left off the frills and trivia which he does not need but which he must pay for when he buys a commercial product.

The ardent experimenter, however, needs no such arguments. He builds his receiver merely for the love of the game, and the thrill of using a product of his own creation.

It is hoped that the receiving equipment to be described in this chapter will awaken the experimenter's instinct, even in those individuals owning expensive commercial receivers. These lucky persons have the advantage of comparing their home-built product against the best the commercial market has to offer. Sometimes such a comparison is surprising.

When the builder has finished the wiring of a receiver it is suggested that he check his wiring and connections carefully for possible errors before any voltages are applied to the circuits. If possible, the wiring should be checked by a second party as a safety measure. Some tubes can be permanently damaged by having the wrong voltages applied to their electrodes. Electrolytic capacitors can be ruined by hooking them up with the wrong voltage polarity across the capacitor terminals. Transformer, choke and coil windings may be damaged by incorrect wiring of the high-voltage leads.

The problem of meeting and overcoming such

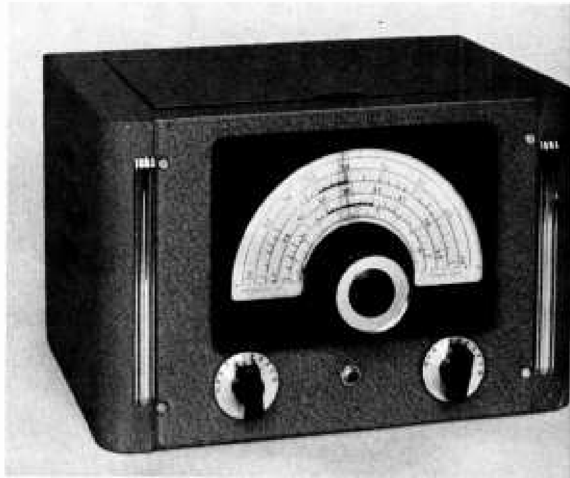


Figure 1
"SUPER GAINER" RECEIVER
A 3-tube superheterodyne combining circuit simplicity and high sensitivity. R-f tuning control is to the left, and regeneration control is at the right. Phone jack is in center, under main tuning dial.

obstacles is just part of the game. A true radio amateur (as opposed to an amateur broadcaster) should have adequate knowledge of the art of communication. He should know quite a bit about his equipment (even if purchased) and, if circumstances permit, he should build a portion of his own equipment. Those amateurs that do such construction work are convinced that half of the enjoyment of the hobby may be obtained from the satisfaction of building and operating their own receiving and transmitting equipment.

24-1 The "Super-Gainer" Receiver

Illustrated in figures 1, 3, and 4 is an up-to-date version of the now famous "Super-Gainer" receiver, originally designed by Frank Jones, W6AJF in 1934. The Super-Gainer is a basic superheterodyne receiver, with all the frills and gadgets omitted. Shown in block form in figure 2, this 3 tube receiver retains all the important advantages of more complicated superheterodyne receivers, yet is an ideal set for the beginner to start with. The receiver covers the 80 and 40-meter amateur bands, using but two coils, only one of which has to be wound. It is sensitive and selective, and serves well in any amateur station as a "stand-by" receiver.

Circuit Description Operation of the receiver may be easily understood by referring to figures 2 and 5. A 6U8 high-conductance mixer tube is used as a combined first detector and high-frequency oscillator. The detector section of the 6U8 is directly coupled to the receiving antenna. The r-f tuned circuit of the detector employs a high-Q 25-watt transmitting type plug-in coil, and tunes from 3.5 Mc. to 7.6 Mc. continuously with a 140-$\mu\mu$fd. variable capacitor. Excellent image rejection is obtained by the use of such a high-Q coil in the r-f circuit. For the frequency range covered, no additional r-f stage is necessary. The oscillator section of the 6U8 tunes from 5150 kc. to 5950 kc. If the proper intermediate frequency is chosen, the two detector responses will cover both the 80 and 40-meter bands. Using an i.f. of 1650 kc. (chosen so that no i-f interference will occur from broadcast stations), the response ranges of the r-f section of the 6U8 are equal to the oscillator tuning range plus or minus the intermediate frequency. In this particular case, the two tuning ranges are:

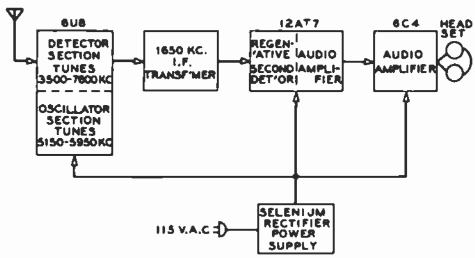


Figure 2
BLOCK DIAGRAM OF "SUPER GAINER" RECEIVER

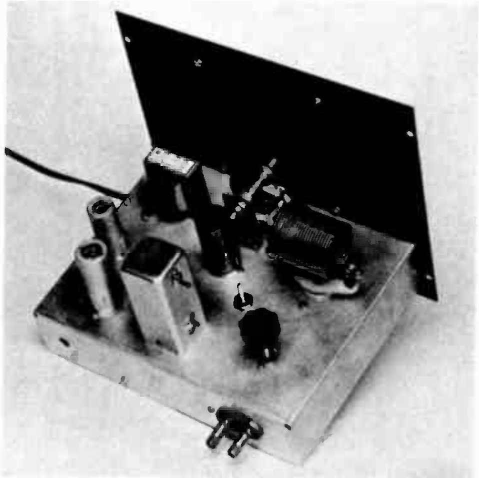


Figure 3
REAR VIEW OF "SUPER GAINER" RECEIVER

The 6U8 mixer tube is directly behind the main tuning capacitor. The slug of L_2 projects through the chassis between the 6U8 tube and C_5, the antenna trimmer. The antenna terminals are mounted on the back of the chassis behind C_5. Rear center is the i-f transformer T_1, with the 12AT7 tube to the left. In front of the 12AT7 socket is the 6C4 stage. T_2 is mounted directly behind the front panel.

Low Frequency Tuning Range (oscillator minus i.f.)

5150		5950	
−1650		−1650	
3500	to	4300	kilocycles ("80 meters")

High Frequency Tuning Range (oscillator plus i.f.)

5150		5950	
+1650		+1650	
6800	to	7600	kilocycles ("40 meters")

It can be seen from the above that one tuning range is the "image" of the other. Ordinarily this would be cause for concern, but the use of a high-Q r-f tuned circuit between the 6U8 and the antenna solves the image problem. Both of the above ranges are covered by the r-f tuned circuit. The low-frequency range (containing the 80-meter band) is covered with the tuning capacitor, C_1, near maximum capacity. The high frequency tuning range (containing the 40-meter band) is covered with the tuning capacitor, C_1, near minimum capacity.

It will be observed from figure 5 that while the receiver is a true superhet, there is no intermediate frequency amplifier stage. By utilizing a grid-leak second detector and incorporating regeneration in this stage to increase the sensitivity and selectivity, no i-f stage is required. A single 1650-kc. iron core i-f

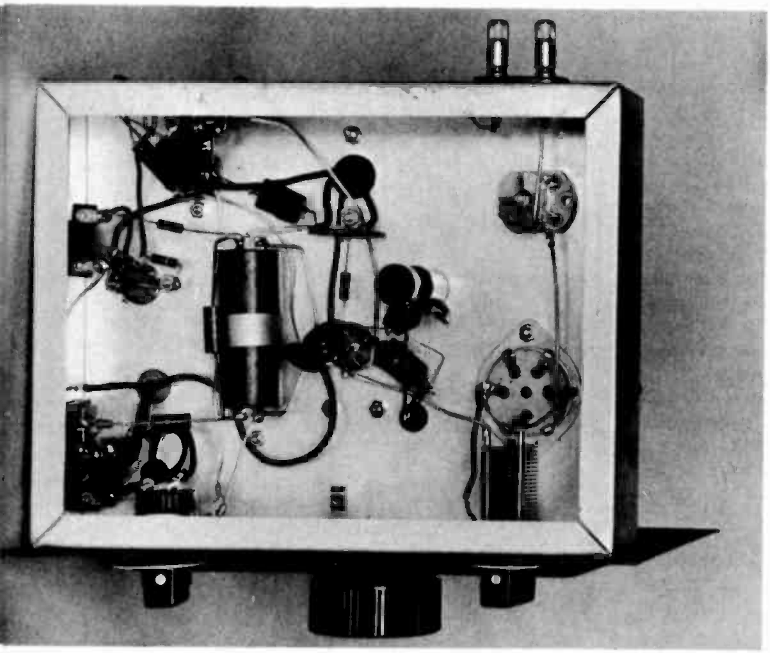


Figure 4
UNDER CHASSIS VIEW OF "SUPER GAINER" RECEIVER

L_2 is mounted to the chassis at the right of center. The dual electrolytic is mounted in center of chassis by short aluminum strap. The selenium power rectifier is bolted to the left side of the chassis.

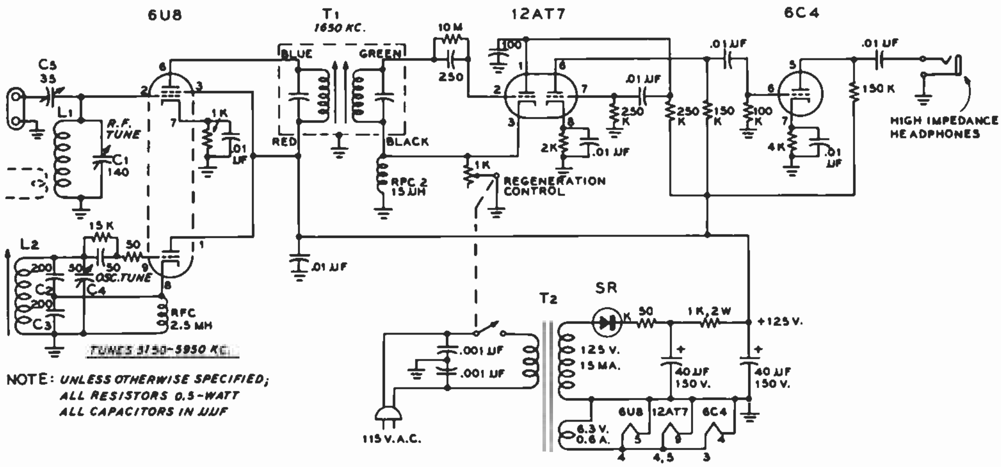


Figure 5

SCHEMATIC OF 3-TUBE SUPERHETERODYNE RECEIVER FOR 80 AND 40 METERS

C_1—140 $\mu\mu$fd. midget, Hammarlund HF-140
C_2, C_3—200 $\mu\mu$fd. silver mica
C_4—50 $\mu\mu$fd., Bud MC-903
C_5—35 $\mu\mu$fd., Bud LC-1644
L_1—B & W 40 MEL
L_2—26 t. no. 22 enam. on National XR-50 form
RFC_1—2½ mh., J.W. Miller 4666
RFC_2—15 μhy., J.W. Miller 4624

T_1—1500 kc. i-f trans., J.W. Miller 912-W1
T_2—Stancor PS-8415, 120 v. 15 ma., 6.3 v. 0.5 a.
Dial—National 1CN
Cabinet—Bud 1781 (8 x 10 panel)
Chassis—7x9x2 Bud AC-406
SR—Selectron 8J1, 50 ma. selenium rectifier
Note: All .01-μfd. capacitors Centralab DD1032 disc ceramic

transformer is used to couple the 6U8 mixer tube to the first section of a 12AT7 double triode which serves as a regenerative detector at 1650 kc. The second section of the 12AT7 is an audio amplifier stage. Cathode regeneration is used in the 12AT7 detector section, the amount of regeneration being controlled by the setting of the 1000-ohm regeneration control potentiometer. When this control is advanced enough to allow the second detector to oscillate, reception of c-w signals (or single sideband phone) is possible, obviating the need for a beat oscillator.

The audio amplifier section of the 12AT7 is resistance coupled to a 6C4 audio output stage which delivers sufficient power to operate a high impedance headset at comfortable volume level.

A half-wave rectifier power supply using a midget selenium rectifier is used in conjunction with a capacitor input filter system to provide 125 volts d.c. at 15 milliamperes. Filament power for the receiver is obtained from the half-wave plate transformer from a separate winding.

Construction The receiver is built upon a 7"x 9"x 2" aluminum chassis (Bud #AC-406) with a front panel measuring 8"x 10". The placement of parts is not critical, and major components may easily be recognized from the photographs of the unit. The antenna trimmer, C_5, is mounted on the chassis near the antenna terminal, and both the rotor and stator of the capacitor must be insulated from the chassis. The main tuning capacitor, C_4, is reversed and mounts directly to the vernier dial by its rear shaft extension. It is supported at the back by a small "L" shaped aluminum bracket 1¾" high which attaches to the capacitor panel bearing, and is bolted to the chassis. This provides a rigid mount for the capacitor. The connecting lead from C_4 to L_2 and the other oscillator components is a short length of no. 14 solid wire, which runs through a ¼" rubber grommet mounted in a chassis hole near the stator connection of C_4. Transformer T_1 is mounted above the chassis at the rear-center, its leads passing through a ½" rubber grommet, centered directly below the transformer on the chassis. Transformer T_2

is also mounted above the chassis in the right-front corner, its leads passing through two ½" rubber grommets in the chassis to the components beneath the chassis.

The r-f tuning coil, L_1, mounts in a five prong ceramic socket which is located to the left of C_4 and just behind C_1. Allow sufficient clearance between C_1 and the coil socket so that the two do not occupy the same space! The socket is oriented so that the axis of the coil is parallel to the front panel, and the coil is about midway between the panel and the antenna trimming capacitor, C_5, which is behind the coil socket. The 6U8 tube socket is placed directly behind C_4, the main tuning capacitor, and is placed in such a way that pin no. 2 of the socket is nearest the front panel. Behind and to the left of the 6U8 socket is L_2, the oscillator coil. The r-f tuning capacitor, C_1, mounts on the front lip of the chassis, and requires a 3/8" hole through both the chassis and front panel. Alignment of the panel to the chassis is made by the positioning of C_1, the regeneration potentiometer, and the phone jack. The bushings of these three controls hold the chassis to the panel. The a-c control switch is mounted on the back of the regeneration potentiometer.

The dual 40-μfd. filter capacitor is mounted below deck in the area between the three tube sockets by means of a strap made from scrap aluminum. The selenium rectifier is mounted to the side wall of the chassis by a single 6-32 bolt. The miscellaneous small parts are mounted directly to the pins of the tube sockets, or are supported by small phenolic tie-point strips. The chassis is used for a ground return, with grounding lugs mounted beneath the tube socket retaining bolts.

The cathode regeneration coil of the 12AT7 (RFC_2) is mounted directly on the tube socket between pin no. 3 (cathode) and no. 9 (ground). The grid-leak and capacitor (10 megohms and 250 μμfd.) are mounted between pin no. 2 of the 12AT7 and one terminal of a phenolic strip which is attached under the front mounting bolt of T_1.

Wiring The wiring is simple and straightforward. First of all, the filament grounds should be made on each socket. Next, the filament wiring and power supply wiring should be done. Cathode resistors and cathode bypass capacitors should be wired in place. The i-f transformer, regenerative circuit, and audio wiring should be installed. Capacitors C_2 and C_3 are mounted in series between the two terminal points on the coil, L_2. The ground lug of L_2 is used as a common ground point for the oscillator tuned circuit components. The oscillator grid capacitor, resistor and 50-ohm parasitic suppressor mount directly between pin 9 of the 6U8 socket and the no. 14 wire connecting L_2 to C_4. When all the wiring has been completed it should be carefully checked for opens, shorts and transpositions before the receiver is turned on.

Adjustment of the Receiver When the receiver is wired and checked, the tubes and coil should be placed in their respective sockets, and the a-c voltage to the receiver turned on. The positive voltage at the output of the rectifier supply should measure 125 volts under load. If another receiver is available, it should be tuned to the 5150-5950 kc. region and placed near the Super-Gainer. It should then be possible to hear the 6U8 oscil-

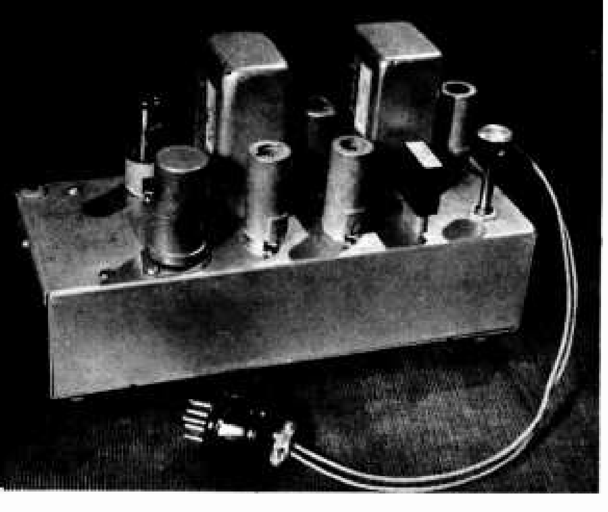


Figure 6

THE UNIVERSAL "Q-5ER" UNIT

The placement of major components may be seen in this view. From left to right across the back are: 6X4 rectifier T_2, 6AU6 i-f tube T_1, and 6C4 mixer. Across the front of the chassis from left to right are: filter capacitor can, 6BE6 mixer, 6AU6 crystal oscillator, low frequency crystal and gain control. The adapter plug is shown in the foreground.

lator somewhere in this region. The slug in coil L_2 should then be adjusted until the oscillator covers the above mentioned range as the main tuning capacitor of the Super-Gainer is tuned from maximum to minimum capacity. When the oscillator of the Super-Gainer covers the correct range, both the tuning ranges are correctly positioned on the dial.

The next step is to align the i-f transformer to 1650 kc. This may be done with the aid of a signal generator. A close approximation may be made by setting the tuning slugs of the transformer so that they project about ¼" from the case of the transformer. The transformer should be peaked for loudest reception on a local signal.

Tuning the Receiver A high, single wire about 30 to 60 feet long should be used as a receiving antenna. No ground connection is necessary. The r-f tuning capacitor, C_1, should be set near maximum capacity for 80-meter reception, and near minimum capacity for 40-meter reception. The regeneration control should be advanced until the regenerative rush is heard in the headset. Capacitor C_3, the antenna trimming control should be peaked for maximum background noise, and the receiver is ready for operation.

The receiver may be calibrated by means of a signal generator, or by careful listening to the received signals. The edges of the 80 and 40-meter phone bands may be readily found, as well as the edges of the two novice bands. When the low frequency edges of the 40 and 80-meter bands are found, a calibration scale for each band may be made and placed upon the blank dial scale provided for that purpose. For best results, high impedance earphones (2000 ohms or so) should be used with this receiver.

24-2 The Universal Q-5'er

Almost all of the less-expensive communications receivers can stand extra i-f selectivity. For c-w operation, it is essential that extreme selectivity be at hand for maximum utilization of the already overcrowded amateur bands. The most widely known method of obtaining additional selectivity has been the addition of the war-surplus BC-453 "Q-5'er" unit to the i-f strip of a standard communications receiver. This low frequency receiver has an 85-kc. i-f strip, and commendable selectivity. Unfortunately, this receiver is almost unobtainable now, and the cost is exorbitant. Even when available, the BC-453 is not the most effective way of obtaining i-f selectivity. It must be converted to operate at 6 volts, and usually will couple a good deal of hum and noise into the regular station receiver.

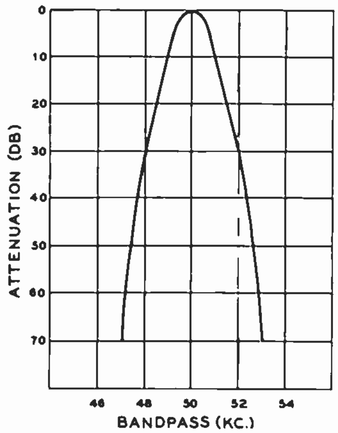


Figure 7
SELECTIVITY CURVE OF UQ-5 UNIT

The Universal Q-5'er (UQ5) is a highly selective i-f strip designed to take the place of the BC-453 and other less selective i-f strips (figure 6). It is a completely self-contained unit, having its own power supply, and no modifications need be made to the receiver when the UQ5 is used. It has a bandpass characteristic as shown in figure 7, and will operate with any receiver (not an a.c.-d.c. set) having a single ended pentode tube as an i-f amplifier. The i-f tube (such as a 6SG7 or a 6SK7) is removed and the adapter plug of the UQ5 is inserted into the empty socket. The i-f signal is removed from the receiver and converted to 50 kilocycles and passes through two high-Q i-f transformers operating on this frequency. The sharpened 50-kilocycle signal is then reconverted back to the original intermediate frequency of the receiver, and injected back into the plate circuit of the i-f system. A block diagram of the entire operation is shown in figure 9, and the complete schematic is shown in figure 10.

Circuit Description The intermediate frequency signal is removed from the receiver by replacing the i-f tube in the receiver by the adapter plug of the UQ5. The i-f signal is picked up from the grid connection (pin no. 4) of the receiver i-f tube socket and fed via a shielded lead to a 6C4 triode converter tube. A 6C4 was chosen for the con-

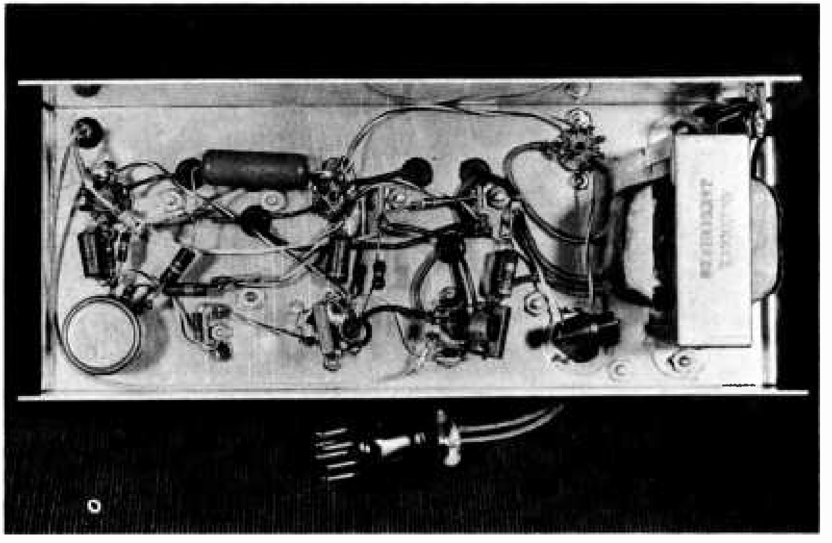


Figure 8
BOTTOM VIEW OF UQ-5 UNIT

verter tube because gain is not needed, and if two 6BE6 tubes are used as input and output converters in the UQ5 unit, there is a possibility of 50-kilocycle feedback from grid no. 1 of the input tube to grid no. 1 of the output tube through the conversion oscillator injection circuit. The conversion oscillator is a 6AU6, operating as a plate-tuned crystal oscillator and employing surplus FT-241 crystals. The correct crystal for a particular receiver i-f frequency may be found from the chart in figure 11. A small amount of external feedback is added between the grid and plate of the 6AU6 to sustain oscillation when these somewhat sluggish crystals are used.

The converted i-f signal is fed through two sharply tuned 50-kc. intermediate frequency transformers, coupled to each other by a single stage of i-f amplification using a 6AU6. The cathode bias of this stage is adjustable, so that the UQ5 may be made to have an overall gain slightly greater than unity. This will prevent overloading the rest of the tuned circuits of the receiver.

A 6BE6 converter tube is used to change the 50-kc. signal back to the original intermediate frequency of the receiver. The same crystal oscillator is used for both conversions, so the addition of the UQ5 unit brings no new problems of stability into the picture. The plate circuit of the 6BE6 converter tube has a broadly tuned circuit adjustable to the receiver intermediate frequency. The output from the 6BE6 is capacitively coupled back into the intermediate frequency system of the re-

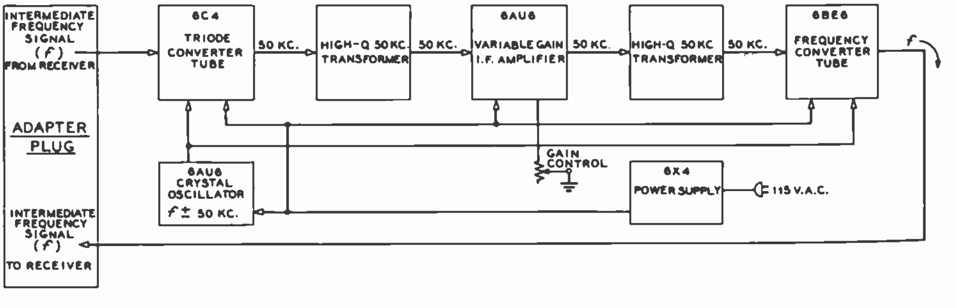
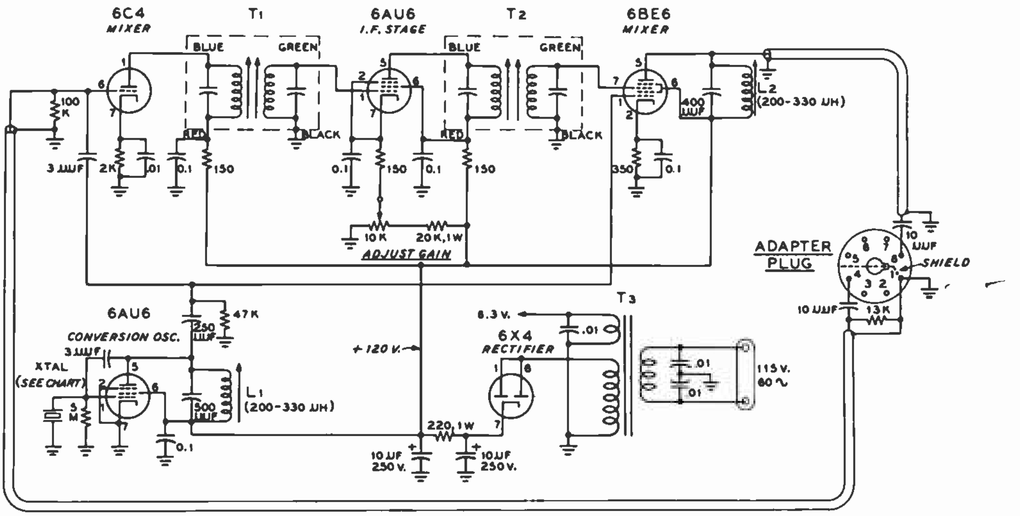


Figure 9
BLOCK DIAGRAM OF UNIVERSAL Q-5'ER



NOTE: *UNLESS OTHERWISE SPECIFIED—ALL RESISTORS 0.5 W., ALL CAPACITORS IN UF.*

Figure 10
SCHEMATIC OF UNIVERSAL Q-5'ER

L_1-L_2—J.W. Miller choke 4565 or equivalent
T_1-T_2—50 kc. i-f transformer J.W. Miller 1898-AX or equivalent
T_3—125 v. 50 ma.; 6.3 v. 2 a., Stancor PA-8421

ceiver via a shielded lead and pin no. 8 of the adapter plug.

Since the UQ5 draws some 30 milliamperes of plate current, it is not advisable to use the power supply of the receiver to supply extra power for the UQ5. A small built-in half wave supply using a 6X4 miniature rectifier tube and a resistance-capacity filter is included in the UQ5 to cover the demands of the plate current and filament current drain of the unit.

Construction The UQ5 is built upon a small aluminum box-chassis, measuring 10"x 4"x 2¼" in size. Figures 6 and 8, showing top and bottom views illustrate the placement of the various parts. Input and output leads are made of shielded wire. The two small 10-$\mu\mu$fd. capacitors mounted in the adapter plug in conjunction with the capacity of the shielded cables form a capacity divider, so that the relatively large internal capacity of the shielded leads does not detune the i-f transformers in the receiver. A small brass shield plate is mounted across the center of the adapter plug and grounded to pin no. 1 of the plug. This shield helps to reduce capacity feedback across the plug itself. The usable gain of the UQ5'er is determined by the feedback between the input and output circuits, so the shields on the "hot" wires to the adapter plug should be brought as close as possible to the plug pins. With a little care a tight-fitting shield plate can be made and soldered into position, using pin no. 1 of the adapter plug as a ground terminal for the shield plate and the shield braids of the two leads. A small tongue of the shield plate can slip down inside the hollow centering pin of the adapter plug to provide a little additional shielding between pins no. 4 and no. 8. Finally, the metal shield cover of the adapter plug should also be grounded to pin no. 1.

All small circuit components of the UQ5 should be mounted on the pins of their respective tube sockets wherever possible, or on small phenolic tie points. The input and output leads enter the chassis-box through a ½" rubber grommet mounted atop the box in the corner near the 6C4. These leads should have their shields grounded close to their termination points.

The two 50-kc. transformers are mounted along the rear edge of the chassis-box, with the 6AU6 i-f tube between them. The slugs of the transformers are oriented towards the outside edge of the chassis to facilitate adjustment. At the end of the chassis opposite the shielded leads is located the power transformer, the 6X4 rectifier and the dual 10-μfd. filter capacitor. The 115-volt line cord is brought out through the top of the chassis by means of a 1/4" rubber grommet.

The holder for the FT-241 crystal is located between the 6AU6 crystal oscillator tube and the 10,000-ohm gain control. It should be positioned at least 2" away from any tubes if possible, to prevent thermal pickup from the tubes, and consequent heat drift of the conversion frequency.

A small variable inductance r-f choke is used in the plate tank circuit of the crystal oscillator, as well as in the plate output circuit of the 6BE6 mixer. Circuit tuning is done by adjustment of the miniature slug. The small padding capacitor for each choke may be mounted directly to the terminal lugs of the choke, and the whole assembly supported on its leads directly above the respective tube socket. The chassis of the UQ5'er is used for the common ground return, and soldering lugs should be placed under each tube socket retaining nut as common ground points for each stage.

Wiring The power supply and filament circuits should be wired first. All wiring except the shielded leads and L_1 and L_2 should then be done. The shielded leads should be put in next, and L_1 and L_2 connected as a last step. This will prevent damage to the fragile windings of the coils by an accidental contact with a hot soldering iron. The UQ5 unit should next be temporarily placed into position near the receiver with which it will operate, and the two shielded leads dressed into position to the correct i-f tube socket in the receiver. The leads may then be cut to length and the adapter plug soldered to the leads.

Alignment When completed, the UQ5'er should be carefully checked for wiring errors, and 115 volts a.c. applied to it. Under load the power supply should deliver 120 volts. The slug of L_1 should be adjusted for oscillation of the converter stage. This may be determined by listening on the crystal frequency with a nearby receiver or frequency meter, or the plate voltage lead to the 6AU6 crystal stage may be temporarily broken and a 0-25 ma. meter inserted in the lead and used for tuning. The slug should be adjusted so that the oscillator starts easily each time the unit is turned on. When the oscillator is operating properly, the arm of the gain control should be set at ground potential, and the adapter plug of the UQ5 should be inserted in the i-f tube socket of the receiver. If the receiver has two i-f stages, the UQ5 should replace the tube of the first i-f stage. The gain control of the UQ5 should now be advanced until the unit breaks into spurious oscillation which may be heard in the speaker of the receiver. The gain control should be backed off until oscillation stops, and the receiver tuned until a signal is heard. The two 50-kc. transformers of the UQ5 unit should now be peaked for maximum signal. The gain control of the UQ5 should be retarded if the unit shows any signs of breaking into oscillation. A stable signal, such as a local oscillator should be used for final alignment of the 50-kc. transformers, peaking each slug for maximum signal strength through the UQ5 unit. The gain control of the UQ5 should be adjusted so that the signal gain through the UQ5 is substantially the same as the receiver gain when the i-f tube replaces the UQ5 adapter plug.

As a last step, the receiver i-f trimmers of the transformers on each side of the adapter plug socket should be repeaked for maximum gain with the UQ5 in operation.

The UQ5 requires no adjustments once it is set up for correct operation. It may be left connected to the receiver permanently when c-w operation is desired. The unit has too high a selectivity characteristic for phone operation unless exalted carrier reception using the receiver beat-frequency oscillator is employed. The UQ5'er may be used in this manner for single-sideband reception.

I.F. FREQUENCY	CONVERSION CRYSTAL FREQUENCY	FT241 CRYSTAL (SURPLUS)	
		CHANNEL	FREQ. (KC.)
455 KC.	405 ± 1 KC.	19 292	405.5 405.5
500 KC.	450 ± 1 KC.	43 324	450 450

Figure 11

CONVERSION CHART FOR FT-241 TYPE CRYSTALS

24-3 A Simple Preselector for 15 and 10 Meters

The performance of many receivers suffers greatly at frequencies above the 20-meter band. In most of these cases, the addition of a simple preselector stage will do much to improve the signal-to-noise ratio and image rejection of an otherwise satisfactory receiver. Such a preselector is shown in figure 12. It is designed to operate from the power supply of the receiver and will provide a noise figure of 6 db when operated into a receiver having one r-f stage. The preselector uses a single 12AT7 tube in a modified cascode circuit that is capable of sufficient sensitivity to enable

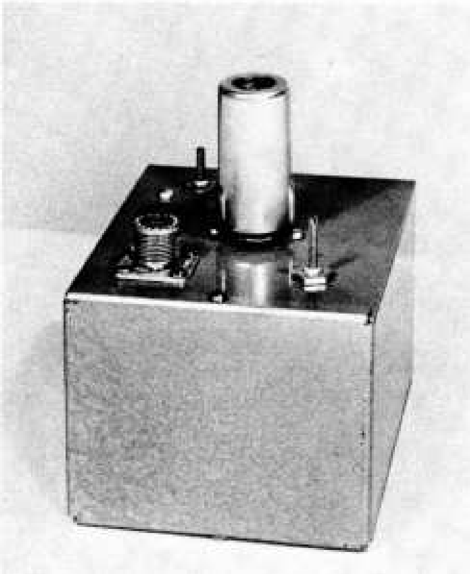
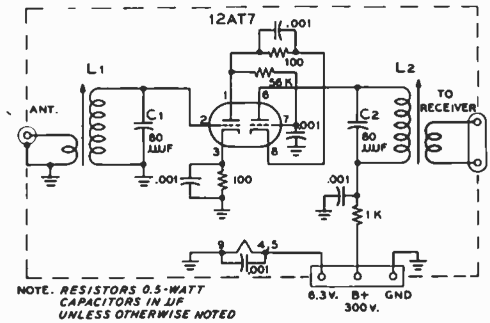


Figure 12
FRONT VIEW OF THE HIGH-FREQUENCY ONE-TUBE PRESELECTOR



L1	10 METERS	6T. #14E., SPACED WIRE DIA. ON NATIONAL XR-50 FORM (0.5" DIA.) LINK IS 2T. HOOKUP WIRE AT GROUND END OF L1.
	15 METERS	8T. #22E., SPACED TO FILL WINDING AREA ON NATIONAL XR-50 FORM (0.5" DIA.) SAME LINK AS ON 10 METER COIL.
L2	10 METERS	6T. #14E., SPACED WIRE DIA. ON NATIONAL XR-50 COIL FORM (0.5" DIA.) LINK IS 3T. HOOKUP WIRE AT GROUND END OF L2.
	15 METERS	8T. #22E. SPACED TO FILL WINDING AREA ON NATIONAL XR-50 COIL FORM (0.5" DIA.) SAME LINK AS ON 10 METER COIL.

Figure 13
SCHEMATIC OF HIGH-FREQUENCY PRESELECTOR

the receiver to easily reach the residual atmospheric noise present at 10 and 15 meters.

Circuit of the Preselector The circuit of the preselector is shown in figure 13. The preselector uses the first half of a double triode tube as the cascode input stage. The input circuit is tuned by a parallel resonant tank, L_1-C_1. The Q of this circuit is adjusted so that the preselector covers a frequency range of 400 kc. at 21 Mc. and a range of 700 kc. at 28 Mc. For 15-meter operation, therefore, the input circuit of the preselector is peaked at the middle of the band, and need not be retuned as the receiver is tuned across the 15-meter band. For 10-meter operation, the preselector input circuit should be peaked at 28.4 Mc. for operation at the low frequency end of the 10-meter band, or at 29.2 Mc. for operation at the high frequency end of the band.

The output section of the 12AT7 tube employs a plate tuned circuit that is resonant in the same manner as the antenna input circuit. The plate circuit is link coupled to the receiver by means of a low impedance link on coil L_2. The 12AT7 tube draws a plate current of approximately 10 milliamperes at a plate potential of 300 volts. This voltage may be obtained from the screen terminal of the power output tube in the communications receiver.

Assembly The preselector is constructed in a 3"x 4"x 5" aluminum utility box (Bud CU-3005) which acts as both chassis and circuit shield. The 12AT7 tube socket is centered on the top of the box, with the output terminal strip and the power plug located on the back end of the box. Between the 12AT7 socket and the output terminal strip the plate inductor, L_2, is placed. C_2 is connected across the terminal points of the XR-50 coil form. L_1 and the coaxial input plug are located in front of the tube socket, as shown in figure 12. The 12AT7 socket is oriented so that prong no. 2 faces coil L_1. C_1 is connected across the tie-points of L_1. The other components associated with the 12AT7 may be connected directly to the socket pins by the leads of the components. The plate bypass capacitor and the 1000-ohm decoupling resistor are connected directly to the XR-50 tie-point and a nearby insulated terminal strip. Placement of the smaller components may be seen in the interior view of figure 14.

Preselector Alignment Since the preselector is a one band unit, L_1 and L_2 should be wound for either 10 or 15 meters. When the preselector wiring has been checked,

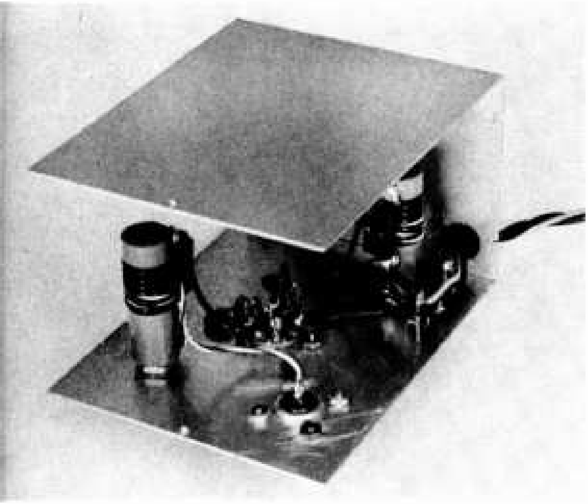


Figure 14
PRESELECTOR INTERIOR
Grid circuit is at left, plate circuit at right. All components for the cascode stage may be mounted directly on the tube socket pins.

it should be connected to the communications receiver as shown in figure 15. An antenna should be connected to the preselector, and the communication receiver tuned to approximately the center of the amateur band. Coils L_1 and L_2 of the preselector should be tuned for maximum received signal at this frequency. On ten meters, the preselector may be adjusted to cover the complete band with a slight loss of gain if L_1 is peaked at a received frequency of 28.5 Mc. and L_2 peaked at 29.2 Mc.

If it is desired to employ a 300-ohm input circuit with the preselector, the coaxial input plug should be replaced with a two terminal connector strip and one additional turn added to the link winding of L_1.

24-4 All-Triode Converter for 144 Mc.

The converter illustrated in figures 16, 17, and 18 will give a good account of itself when operating into the regular station communications receiver for the reception of stabilized signals on the 144-Mc. band. It employs three tubes and a voltage regulator, may be operated into an intermediate frequency from 17 to 30 Mc., and requires 250 volts of plate potential at about 45 milliamperes.

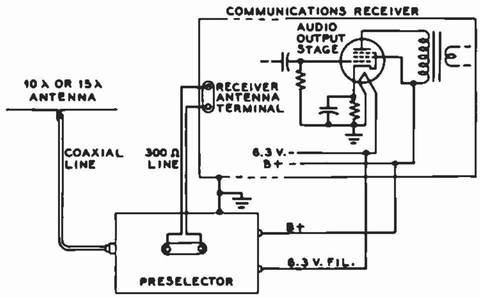


Figure 15
PRESELECTOR CONNECTIONS TO COMMUNICATIONS RECEIVER

Circuit Description The converter uses a 6BQ7-A as a cascode r-f amplifier operating into a 6AB4 mixer tube. A push-pull connected 6J6 tube acts as the high frequency conversion oscillator. The antenna input circuit of the converter is broadly resonant in the 144-Mc. region, and once the slug of L_1 is tuned for optimum performance at the middle of the 2-meter band, the r-f stage requires no further adjustment. The plate circuit of the cascode stage is also resonant in the 2-meter band, peaked by adjustment of C_1. The plate circuit of the mixer tube may be tuned to cover a 4-Mc. range in the region between 17 and 30 Mc., and the i-f output of the converter may be set anywhere within this range. The actual choice of intermediate frequency should be made on the basis of the tuning range of the receiver. The oscillator control is not ganged to the r-f tracking controls so that there is no tracking problem introduced by the selection of a different intermediate frequency.

The conversion oscillator is operated on the low frequency side of the incoming signal and covers a frequency range somewhat greater than the 4-Mc. spread of the 144-Mc. band. Therefore the oscillator range may be moved about to accommodate a change in the output intermediate frequency. A push-pull conversion oscillator circuit is used for maximum stability, and a split-stator tuning capacitor (C_3) is employed to tune the oscillator. The rotor of the capacitor is left ungrounded. The plate potential to the 6J6 oscillator stage is held constant by an OB2 regulator tube.

Filament voltage to the 6BQ7-A r-f amplifier is fed through a bifilar wound r-f choke, L_7,

Figure 16
TWO METER CONVERTER

while the "hot" filament pins of the 6J6 and the 6AB4 are bypassed to ground at their respective sockets.

Construction The converter is constructed upon an aluminum chassis measuring 7"x 7"x 2" in size (Bud # AC-405). A cabinet 8"x 8"x 7" is used (Bud # C-973) to house the unit. As may be seen in figure 17, the 6J6 oscillator is centrally located on the chassis. C_3 is mounted about 7/8" above the chassis on a rigid metal brace, and is coupled to the National dial by means of an insulated, flexible coupling. To the left of the oscillator is located the OB2 voltage regulator tube. The oscillator plate inductor, L_6, is formed of a loop of heavy wire and mounted directly on the top stator terminals of the tuning capacitor. Also connected to these stator terminals is the oscillator padding capacitor, C_4.

The r-f and mixer stages of the converter are mounted at the rear of the chassis. L_1, L_3 and L_4 are mounted beneath the chassis in a horizontal position, the forms being bolted to the rear lip of the chassis. The coaxial input plug is located between L_1 and L_3. The power cord leaves the chassis between L_3 and L_4. The coaxial output connector is mounted on the top of the chassis in the far corner.

Beneath the chassis (figure 18) the positioning of the three coils may be seen. Also visible is the small partition between L_1 and

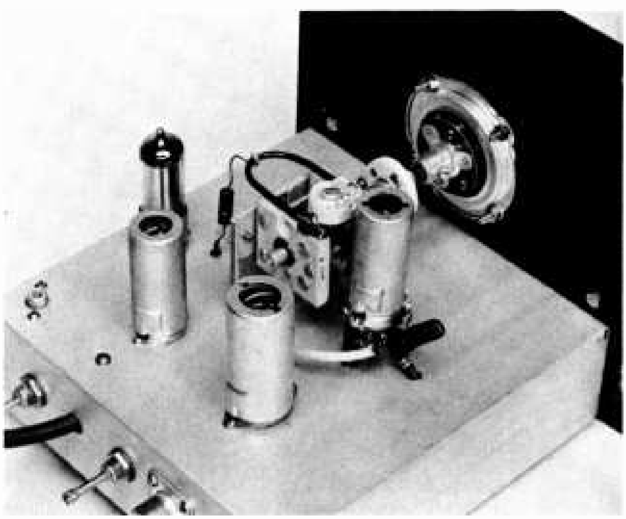


Figure 17
CHASSIS VIEW OF 2-METER CONVERTER

R-f coil slugs are adjustable through rear of chassis. Oscillator tube is mounted above chassis on short metal spacers.

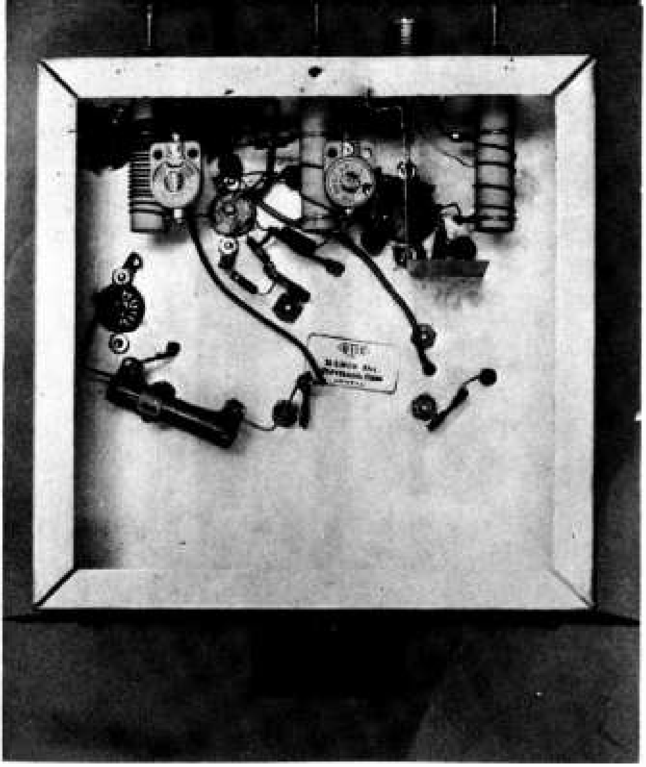


Figure 18
BOTTOM VIEW OF CONVERTER

Components are mounted on pins of tube sockets wherever possible. Observe shield mounted across r-f tube socket, to left.

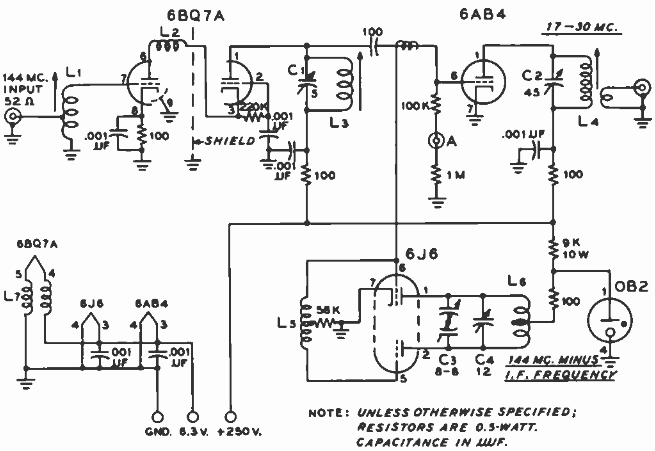


Figure 19
SCHEMATIC OF 2-METER CONVERTER

C_1—5 µµfd. Centralab NPO ceramic trimmer

C_2—45 µµfd. Centralab ceramic trimmer

C_3—8-8 µµfd. dual section capacitor (Bud LC-1659)

C_4—12 µµfd. Centralab NPO ceramic trimmer

L_1—4 t. no. 18 enam. on Millen 69046 slug-tuned form. Turns spaced to fill form. Input tap 1 t. from ground.

L_2—24 t. no. 22 d.c.c. wire closewound on 3/16" form.

L_3—2 t. no. 18 enam. on Millen 69046 slug-tuned form. Turns spaced to fill form.

L_4—13 t. no. 22 enam. on Millen 69046 slug-tuned form. Turns spaced to fill form.

L_5—12 t. no. 22 enam. closewound 1/8" i.d.

L_6—"Hairpin." Single loop no. 12 enam. 1" dia. 1¾" long. See top view photo for detail.

L_7—Wound on form ¼" dia. 1" long. Two parallel wires. 24 t. closewound no. 22 enam.

Note: All .001 µfd. capacitors are Centralab DD-102 or equivalent

L_3. Capacitors C_1 and C_2 are mounted on their respective coil terminals. The 6BQ7-A neutralizing coil L_2 is mounted through a 3/8" hole cut in the shield plate. This shield plate passes through the middle of the 6BQ7-A tube socket, and is grounded to the center stud of the socket and to pin no. 9. The bifilar coils are wound from two parallel lengths of enameled wire. The winding is placed on a 1-watt resistor which is mounted beneath and at right angles to L_3.

The oscillator coupling lead goes from pin no. 6 of the 6J6 socket through a 1/8" chassis hole and wraps twice around the no. 6 grid lead of the 6AB4 oscillator. This coupling is adjusted until 2 volts may be measured between point "A" and ground when a high resistance voltmeter is employed. This test should be made after the converter is in operation and has been aligned.

Alignment of the Converter As a first step, L_1 and L_3 should be tuned to approximately 145 Mc. with the aid of a grid-dip oscillator. The intermediate frequency should be chosen, and C_2 tuned so that the output circuit of the converter resonates to the intermediate frequency. The oscillator padding capacitor, C_4 is then adjusted to place the frequency of the oscillator lower in frequency than the 144-Mc. band by the amount of the intermediate frequency. If the i.f. is, for example, 20 Mc., the oscillator should be set to approximately 124 Mc. When this has been done, all circuit tuning may be optimized by actually peaking the various adjustments on a 2-meter signal. Squeezing or spacing the turns of L_5 will control excitation to the 6J6 oscillator and regulate to some extent the injection voltage measured at point "A."

Once the converter has been placed within the cabinet, adjustments to C_1 and C_2 may best be made through small holes drilled in the bottom of the cabinet. It will be found that changes in the intermediate frequency of several hundred kilocycles may be made without the necessity of repeaking any adjustments of the converter. The sensitivity of the converter will compare with all but the very best 2-meter receivers, and the stability is good enough so that 2-meter c-w stations may be copied with ease.

24-5 A De Luxe 2-Meter Superheterodyne

This receiver was designed with the idea of completely divorcing v-h-f reception from the regular station communications receiver, and with the idea of incorporating in one package the more desirable and suitable characteristics needed in a v-h-f receiver.

Using a good communications receiver with a 6-kc. bandwidth in conjunction with a 2-meter crystal controlled converter is one of the better ways of covering this band, but tuning the complete band with such a combination is time-consuming, and weak stations may eas-

Figure 20
FRONT VIEW OF 2-METER SUPERHETERODYNE

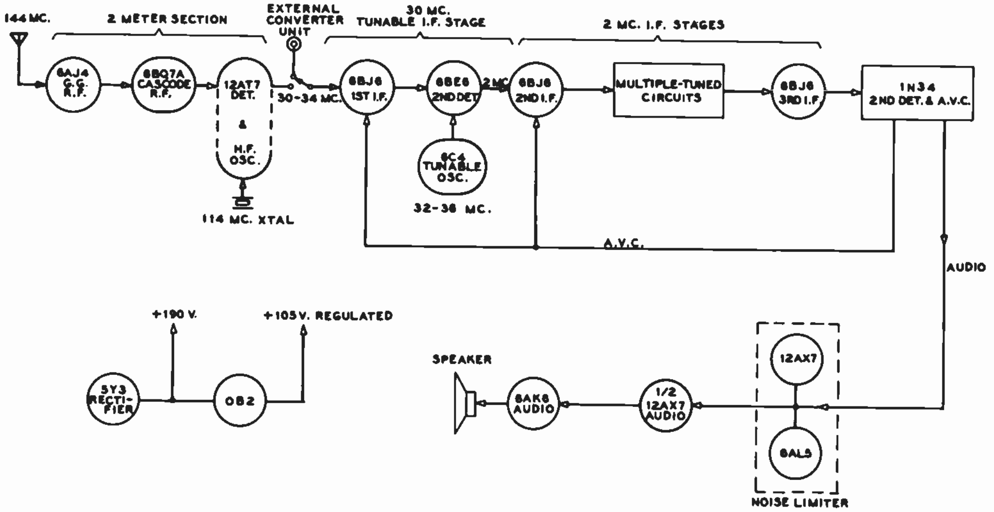


Figure 21

BLOCK DIAGRAM OF DE LUXE 2-METER SUPERHETERODYNE RECEIVER

ily be missed. Then, too, the problems of "birdies" or spurious images is always at hand when a converter-receiver combination is used. It was felt that a completely new approach was needed for the ultimate in v-h-f reception. This receiver is the result of many preliminary designs, and it is felt that it will provide outstanding performance on the 2-meter band.

Circuit Description The De Luxe receiver is a double conversion superhetrodyne, tuning 144-148 Mc. The first conversion oscillator is crystal controlled on 114 Mc. (figure 21). A 6AJ4 high-transconductance grounded-grid triode r-f stage is directly fed from a coaxial input at 2 meters. A second r-f stage using a 6BQ7-A follows the grounded-grid stage. The noise figure of the receiver is approximately 4 db at an input impedance of either 52 or 75 ohms. A 12AT7 is used as a combination first detector and local oscillator. A special overtone crystal is cut for 114 Mc., and is used in a regenerative circuit. The stability of this crystal oscillator approaches that obtained with lower frequency crystals. Circuitry is simplified, since no frequency multipliers need be used between the overtone oscillator and the mixer stage. Spurious responses are held to a minimum when the oscillator operates directly at the conversion frequency instead of a sub-multiple of it.

The two r-f stages are ganged tuned, and in turn are ganged to the tunable i-f section resulting in extremely high image rejection; so high, in fact, that in view of the high frequency of the first i-f stage, the ganging of the r-f might be dispensed with, if desired.

The first intermediate frequency stage uses a 6BJ6 and tunes from 30 to 34-Mc. This first i.f. is high enough in frequency so that it may be used with external converters for the 220-Mc. and 420-Mc. bands. A switch (S_3) is incorporated in the input circuit of the 30-Mc. i-f strip to permit switching auxiliary converters into the receiver. A 6BE6 second detector stage in conjunction with a 6C4 oscillator converts the 30-Mc. i-f signal to the second intermediate frequency of 2-Mc. The 6C4 oscillator tunes from 32 to 36 Mc. and uses a voltage regulated plate supply. The 3-gang tuning capacitor for this section (C_2) is enclosed in a standard aluminum utility box, keeping the rotor contacts free from dirt and dust. The box also acts as a heat baffle, and reduces radiation from the oscillator circuits. The tuning inductances (L_7-L_{10}) are enclosed beneath the chassis in a similar utility box, with flashing copper partitions between the stages. Although not shown on the schematic, each filament, a.v.c. and B plus lead entering this sub-chassis enclosure passes through a 1500 $\mu\mu$fd. feed-through bypass capacitor (Centralab FT-1500). The shielding and filtering contains the oscillator signal where it belongs, and permits the use of external converters without the usual "birdie" problems. The oscillator signal is so completely contained that no trace of it may be detected outside the enclosure with a TV-type signal strength meter.

The 6C4 conversion oscillator is temperature stabilized by C_4 and C_5. These are alternately adjusted to balance out oscillator drift. Both are mounted flat on the chassis, inside the top enclosure.

The second intermediate frequency of 2-Mc. was chosen so that the secondary images from the tunable i.f. would fall outside the 30 to 34-Mc. tuning range. The 50-$\mu\mu$fd. padding capacitors in transformers T_1-T_5 are removed and replaced with 30-$\mu\mu$fd. zero temperature ceramic units. The 1500-kc. transformers then tune to the 2-Mc. intermediate frequency with the slugs in normal position. It will be noted that the capacitors across the secondaries of T_1 and T_4 are returned directly to the cathodes of the tubes. The unbypassed 20-ohm cathode resistors cancel out the detuning effect caused by variations in a.v.c. grid bias on these stages, which otherwise can be quite violent with the relatively low tuning capacities used. An output connection from the 2-Mc. i-f detector is provided for connection to an oscilloscope or pan-adapter.

Two 1N34 crystal diodes are used for the second detector and the a.v.c. rectifier. A 12AU7 tube serves as a combination b.f.o. and a balanced bridge S-meter. Sensitivity of the meter is controlled by R_3 and zero-set is afforded by R_2. Ten turns are removed from the grid end of the winding of L_{11} to move the b.f.o. to 2-Mc. Switch S_2 positions are: "Manual–A.V.C.–B.F.O."

The overall gain level of the receiver is set by R_1. This should be adjusted for best noise limiter action, as too much or too little receiver gain degrades the effectiveness of the noise limiter stage. There is more gain than necessary for 2-meter operation, but the extra gain is useful with external converters of low output.

Excellent skirt selectivity is provided by five double tuned circuits at the 2-Mc. intermediate frequency. The coupling capacitors between T_2-T_3 and T_3-T_4 are each 2 $\mu\mu$fd. and may be increased or decreased in size to alter the selectivity to some degree. The bandwidth of the receiver is 8 kc. at 2 times down, 25 kc. at 10 times down, and 42 kc. at 100 times down. Total warm-up drift is such that a station tuned in from a cold start is still in the passband of the receiver one hour or more later.

A version of the popular TNS noise squelch circuit is used in the receiver, followed by two audio stages. Both low and high impedance output circuits are provided. A special plug (P_2) is placed in the positive voltage lead to the receiver to allow the unit to be rendered inoperative during transmission periods. The whole receiver runs at a plate voltage of only 190 volts. This reduces power consumption, and allows the receiver to run reasonably cool.

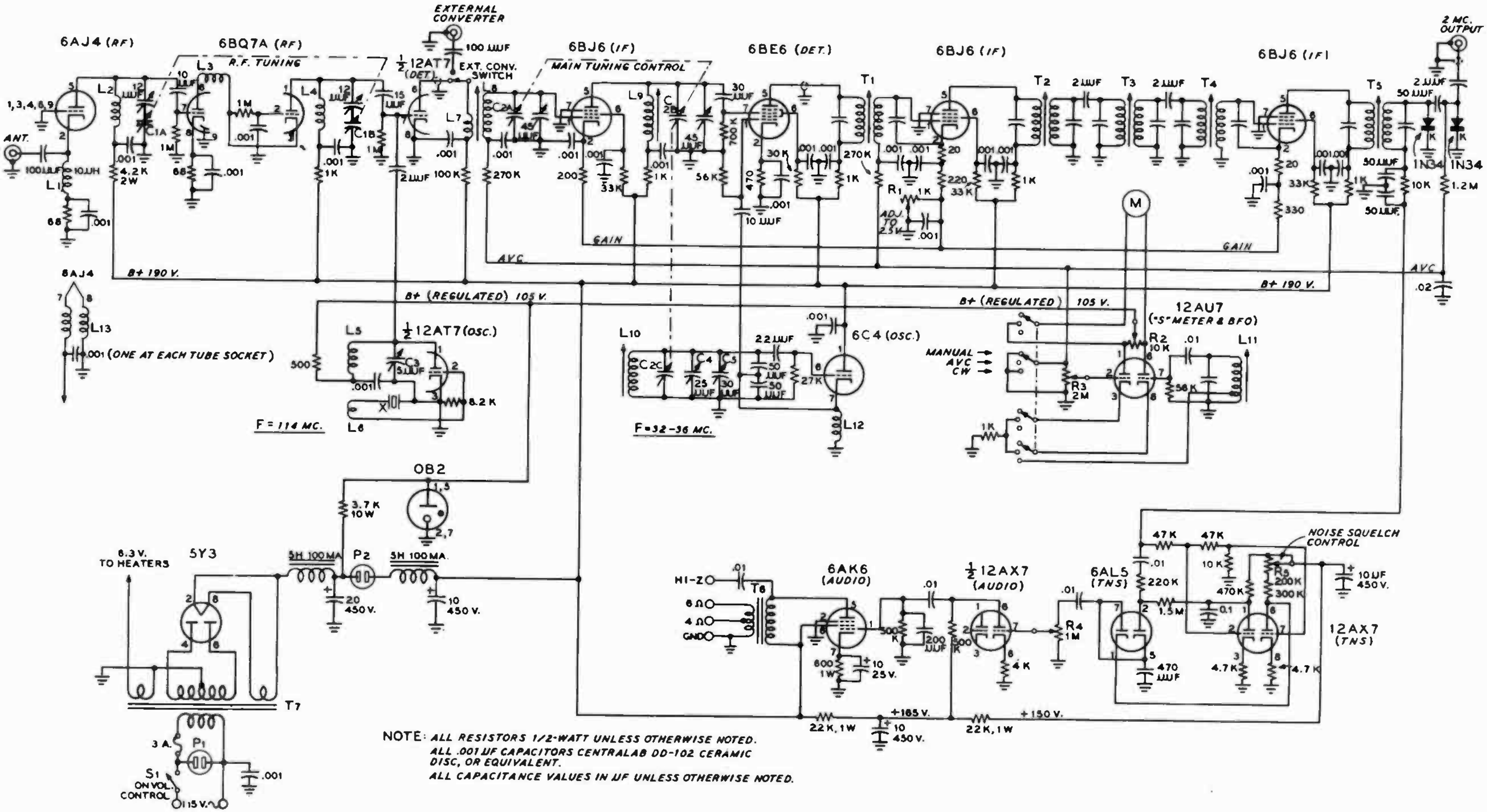
Construction of the Receiver A receiver such as this is a complex device, and its construction should only be undertaken by a person familiar with v-h-f equipment and who has a grid-dip oscillator and a frequency meter at his disposal.

The receiver is built upon an 8" x 15" x 2½" aluminum chassis, and fits within an 8" x 16" cabinet (Bud #C-1790). The main tuning capacitor box measures 3" x 4" x 5" (Bud AU-1028) and the 30-Mc. coil enclosure box beneath the chassis is 2" x 4" x 4" (Bud AU-1083). The 6AJ4, 6BQ7-A and 12AT7 front end tubes are mounted upon a thin copper plate measuring 4" x 5½". All components are mounted upon this plate which is completely wired before it is placed over a matching hole in the receiver chassis. Two flashing copper partitions are arranged to cross the middle of the 6AJ4 and 6BQ7-A tube sockets. The neutralizing coil, L_3, passes through a hole in one partition. High voltage and filament leads from the r-f section are run in shielded wires. The front end may be tested separately as a converter by operating it into a receiver that tunes the 30 to 34-Mc. range.

A Crowe #232 assembly is used for the slide-rule portion of the dial, and the drum parts. The vernier dial is a National AM dial assembly with a 0-200 (360 degree) scale. The knob is drilled and the scale fastened to it, rather than to the vernier as originally supplied. This provides a mechanical bandspread of about 10-kc. per dial division, which is consistent with the i-f passband used. The vernier scale permits excellent signal resetability, using the slide-rule scale for general tuning. The dial escutcheon plate was made from a modified push-button plate from an old receiver. If desired, a National or Millen dial may be substituted for the homemade dial with good results.

The two condenser gangs are connected together by dial cord and pulleys. If desired, the r-f stage condenser (C_{1A}-C_{1B}) may be separately controlled from the front panel and not ganged with the main tuning control.

Alignment of the Receiver When the wiring has been completed and checked, the 2-Mc. i-f strip should be aligned with the aid of a signal generator. Care should be taken not to overload the various i-f stages with the signal generator. The next step is to adjust L_{10} and C_4-C_5 so that



NOTE: ALL RESISTORS 1/2-WATT UNLESS OTHERWISE NOTED.
ALL .001 µF CAPACITORS CENTRALAB DD-102 CERAMIC DISC, OR EQUIVALENT.
ALL CAPACITANCE VALUES IN µF UNLESS OTHERWISE NOTED.

Figure 22

SCHEMATIC OF DE LUXE 2-METER SUPERHETERODYNE RECEIVER

C_{1a}, C_{1b}—8-8 μμfd. Bud LC-1659 or equivalent
C_{2a}, C_{2b}, C_{2c}—25-25-25 μμfd. J.W. Miller 1461 or Bud LC-1847
C_3—5 μμfd. Johnson 5M11
C_4—25 μμfd. NPO ceramic trimmer
C_5—30 μμfd. N500 ceramic trimmer
CH_1—Stancor C-2305
L_1—10 μhy. choke J.W. Miller 4612
L_2—3 t. no. 8 enam. 3/8" dia. spaced 1/2" long
L_3—10 t. no. 20 enam. 1/8" dia. closewound
L_4—same as L_2
L_5—5 t. no. 18 enam. 1/2" dia. 3/8" long
L_6—1 t. hookup wire pushed between t. 4 and 5 of L_5
L_7—3 t. hookup wire at bottom of L_8
L_8—6 t. no. 18 enam. on 3/8" dia. ceramic slug form Millen 69041
L_9—same as L_8
L_{10}—same as L_8 (see text)
L_{11}—1500 kc. b-f-o trans. Miller 912-W5
L_{12}—39 mhy. J.W. Miller 4628
L_{13}—5 t. each no. 18 enam. on 1/16" dia. forms closewound
T_1, T_2, T_3, T_4, T_5—J.W. Miller 1493-W 1500 kc. i-f trans.
T_6—10 K to voice coil Stancor A-3831
T_7—Power trans. 550 v. ct at 110 ma., 6.3 v. at 5 a., 5 v. at 2 a. Triad R-12A or Stancor PC-8405
X—114-Mc. crystal Precision Crystal Lab., Santa Monica, Cal.
M—De-Jur Amsco 1½" 1-ma. meter

the conversion oscillator covers the range of 32 to 34 Mc. The oscillator may be monitored in a nearby receiver. Adjust the slugs of L_8 and L_9 at 30 Mc. and trimmers at 34 Mc. for proper tracking of the 6BJ6 and 6BE6 stages. Tracking this small range presents no problem. If switch S_3 is thrown to the "converter" position and a short antenna placed in the converter jack, signals and ignition noise in the 30 to 34 Mc. range should be heard.

If the front end of the receiver has been tested as a converter, it is only necessary to hook it into the rest of the receiver and align L_2 and L_4 for best signal-to-noise ratio in the 2-meter band. The coupling between L_5 and L_6 should finally be adjusted for ease of starting of the crystal conversion oscillator.

Image Response The tunable oscillator range is such that no birdies occur

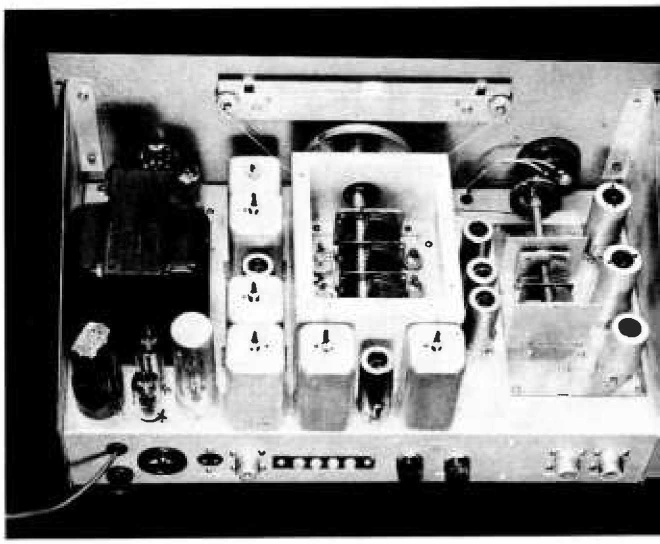


Figure 23

REAR VIEW OF 2-METER RECEIVER

The covers for the capacitor boxes have been removed to show the tuning gangs. At the right of the chassis is the r-f section, mounted on a copper plate. The 6AJ4 tube is to the rear of the chassis, the 6BQ7 directly in front of it, and the 12AT7 nearest the front panel. The 114-Mc. crystal is mounted in front of the box containing C_1. Between the copper plate and the main tuning box are the 6BJ6, 6BE6 and 6C4 tubes, the 6BJ6 tube being nearest the front panel. The i-f stages are to the left and to the rear of the main tuning box. At the left of the chassis are the audio stages, the B.F.O. (near panel) and the noise limiter tube.

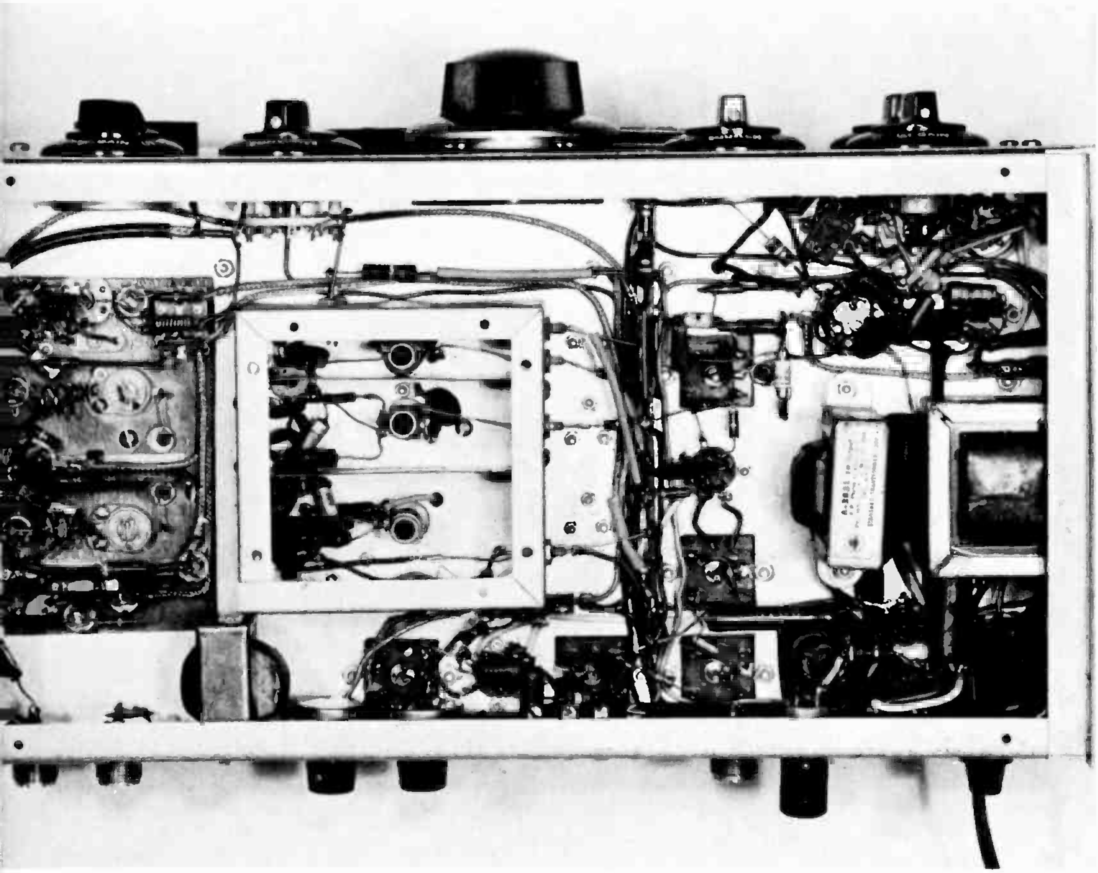


Figure 24

BOTTOM VIEW OF 2-METER SUPERHETERODYNE

To the left of the chassis is the copper r-f plate which mounts all components of the front-end section. All power leads to this section are shielded. At the center chassis is the coil box containing L_7-L_{10}. Directly behind this (bottom of photo) is T_6, R_3 and R_2. At the left rear edge of the chassis are the antenna and "converter input" coaxial plugs. Audio and power supply components are mounted along right hand side of chassis.

at any point in the 2-meter range. Using the 114-Mc. crystal simplifies this problem. Any higher order beats are too far below the noise level to be detected. The primary image tuning range is 80 to 84-Mc. With a grid-dip oscillator tuning this range placed directly at the antenna connection of the receiver with a two turn link, no signal should be heard in the receiver. The secondary image range of 34 to 48 Mc. (translated to 148 to 152 Mc.) presents a negligible response. There is no observable signal leak-through in the 30 to 34 Mc. range.

24-6 The C-W Man's Superheterodyne

Illustrated in figures 25, 27 and 29 is a straightforward double-conversion superhetrodyne having no "frills" or expensive refinements, but capable of excellent performance for the c-w operator. The receiver is designed around the Collins 455-kc. mechanical filter that has the "800 cycle" selectivity curve (figure 28). The receiver employs ten tubes, including the rectifier and voltage regulator. A simplified coil switching configuration is used, resulting in an extremely simple front-end design.

Circuit of the Receiver The "C-W Super" uses a 12AT7 cascode tuned r-f stage which operates on 80, 40, 20, 15 and 10 meters. The antenna input coil, L_1, is nominally tuned to 40 meters, and is in the circuit at all times. For 80-meter operation, band-switch section S_{1A} pads this coil with additional fixed capacity so that the circuit tunes to the 3.5-Mc. band. For 20-meter operation, a secondary inductor, L_2 is shunted across L_1, decreasing the inductance of the tuned circuit to a value suitable for 14-Mc. operation. Inductors L_3 and L_4 tune the input circuit to the 21-Mc. and 28-Mc. band respectively. By the use of such a coil-shunting method, only one switch segment is needed for the antenna input circuit, greatly simplifying the assembly and wiring of this stage. A single antenna link is used for all bands.

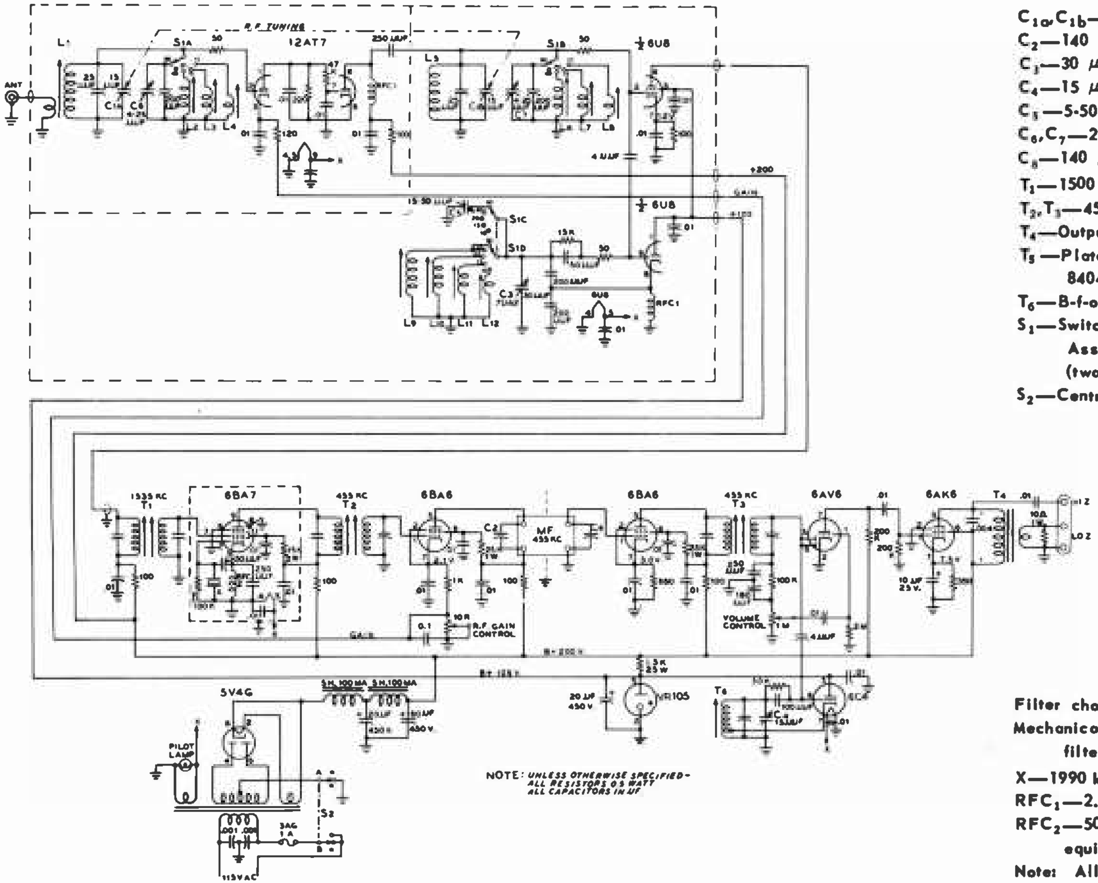
The plate circuit of the cascode r-f stage is band-switched in much the same manner as is the input circuit. L_6, L_7 and L_8 are the high-frequency shunting coils for the main 40-meter coil, L_5. Switch segment S_{1B} shunts sufficient capacity across L_5 for 80-meter operation of this circuit, in addition to selecting the proper shunting coil for the higher frequency bands. A 6U8 dual purpose tube is used for the frequency converter as well as for the high frequency oscillator.

The triode section of the 6U8 is used as a "hot cathode" oscillator. Feedback is sustained by a capacity bridge between ground, cathode and grid of the triode. No cathode tap or feedback winding is needed on the oscillator coils (L_9-L_{12}) when such a capacity feedback circuit is used.

To reduce images on the high frequency band, a double conversion i-f system is used in the receiver. The second intermediate frequency is 455 kc., and the first i.f. operates on 1535 kc. A 6BA7 is used as a combination mixer/conversion oscillator tube, with a conversion crystal of 1990 kc. The oscillator section of the 6U8 therefore is tuned either 1535 kilocycles higher or lower than the received signal. The low frequency tuning limits of the conversion oscillator are shown in figure 30, Table 2. Tuning of the receiver is accomplished by C_3, the oscillator tuning capacitor, and r-f tracking is accomplished by C_1, a two gang capacitor which simultaneously tunes the antenna and mixer r-f circuits.

After conversion from 1535 kc. the signal is amplified by a 6BA6 455 kc. amplifier before passing to the Collins 455 kc. mechanical filter. This filter has a bandwidth of 800 cycles at 10 db attenuation, and a bandwidth of 2500 cycles at 60 db attenuation (figure 28). Such a form factor is ideal for the advanced c-w operator, and the use of such a filter has proven itself many times in DX contests. The bandpass of the filter, of course, is much too sharp for reception of phone signals, but this receiver is designed strictly for the amateur

Figure 25
FRONT VIEW OF THE C-W MAN'S SUPERHETERODYNE



C_{1a}, C_{1b}—each 15 μμfd. Bud MC-1850
C_2—140 μμfd.
C_3—30 μμfd. Bud MC-1852
C_4—15 μμfd. Bud LC-1641
C_5—5-50 μμfd.
C_6, C_7—25 μμfd. ceramic trimmer
C_8—140 μμfd.
T_1—1500 kc. trans. J.W. Miller 1312-W1
T_2, T_3—455 kc. trans. J.W. Miller 912-C2
T_4—Output trans. Stancor A-3822
T_5—Plate trans. 520 v. ct at 90 ma. Stancor PC-8404
T_6—B-f-o trans. J.W. Miller 912-C5
S_1—Switch S_1 is made from a Centralab Index Assembly P-123 with three type K decks (two-pole, 2-5 positions)
S_2—Centralab 1405

Filter chokes—5 hy. at 100 ma. Stancor C-2305
Mechanical filter—Collins F455C-08 800 cycle filter
X—1990 kc. crystal
RFC_1—2.5 mhy. r-f choke
RFC_2—50 μhy. r-f choke J.W. Miller 4509 or equivalent
Note: All .01 μfd. capacitors are Centralab DD-1032 or equivalent

Figure 26
SCHEMATIC OF C-W MAN'S RECEIVER

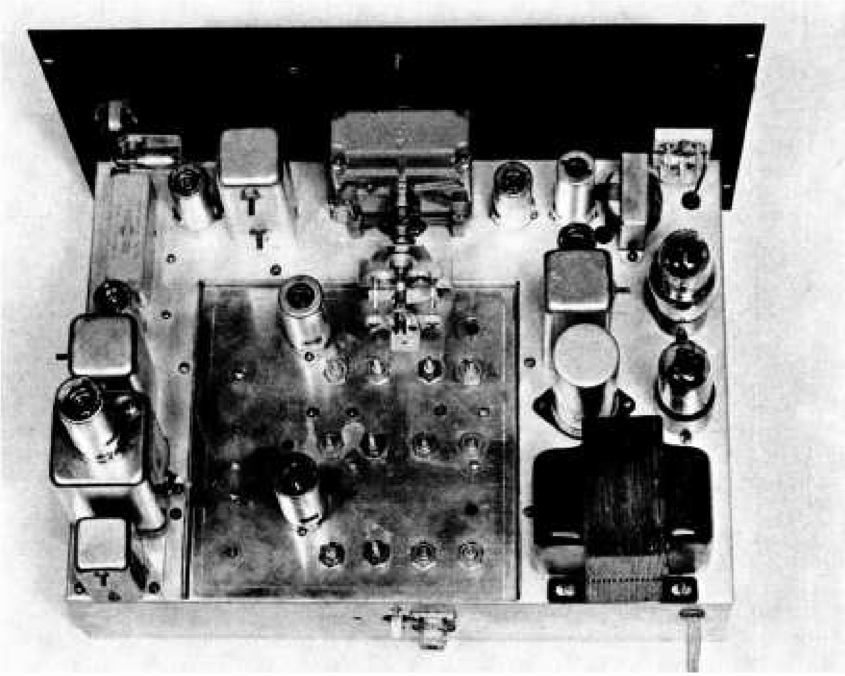


Figure 27

REAR VIEW OF C-W MAN'S RECEIVER

The r-f deck may be seen at the middle of the receiver with the 12AT7 r-f tube at the rear, near the coaxial antenna plug. At the left is the Vector plug-in unit that houses the 6BA7 converter tube. The mechanical filter is mounted to the chassis at the upper left. To the right of the mechanical filter is the second 6BA6 i-f tube and T_3. The 6AV6 is to the right of the dial mechanism, with the 6AK6 and T_4 beside it. The B.F.O. tuning control, C_4 is mounted to the panel at the extreme right. Between C_4 and the power transformer are the VR-105 tube and the 5V4-G rectifier.

interested in top-notch c-w reception at a modest cost, and no attempt has been made to modify the passband of the i-f system for phone reception.

The overall gain of the receiver is controlled by a variable cathode resistor that regulates the bias of the r-f stage and the first i-f stage. The i-f stage following the mechanical filter is run at maximum gain at all times. For proper receiver operation, a balance between r-f gain and i-f gain must be secured. Too much i-f gain will tend to make the receiver noisy and will mask some of the weaker signals. Too much r-f gain will make the receiver susceptible to cross-talk and overloading. For best operation, the receiver should be operated with the minimum amount of gain needed to hear the signal that the receiver is tuned to. Adjustment of the gain level in the receiver will be discussed later in this chapter.

Following the 455-kc. intermediate frequency stages is a 6AV6 detector and audio amplifier, a 6C4 B.F.O. and a 6AK6 audio output stage. A 5V4-G is used as a full-wave rectifier. A separate section of the power switch, S_2, is used as a stand-by switch, breaking the negative of the power supply to render the receiver inoperative during periods of transmission.

Mechanical Layout of the Receiver The main part of the receiver is built upon an aluminum chassis measuring 10"x 14"x 3" in size (Bud #AC-414). The r-f section of the receiver which includes the

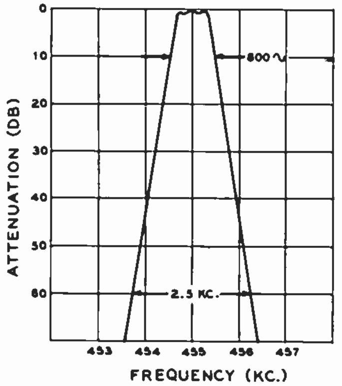


Figure 28
PASSBAND OF "800 CYCLE" MECHANICAL FILTER

12AT7 r-f stage and the 6U8 mixer/oscillator is built upon a sub-chassis measuring 7"x 7" x 2" (Bud #AC-405). The 6BA7 converter stage is built into a Vector Plug-in unit (#C12-N). For ease of assembly, the three sub-units are wired separately and then connected together for final testing and alignment. The receiver is housed in a sheet-metal cabinet measuring 15"x 11"x 9" (Bud #C-975).

A square hole is cut in the main chassis of the receiver to receive the sub-chassis which contains the r-f assembly. This smaller chassis is held in place by means of three lengths of small dural angle stock. The angle stock is bolted to the top edge of the sub-chassis by means of 4-40 machine screws and bolts, forming a ½" lip that passes around the front and the two sides of the sub-chassis. When the sub-chassis is positioned correctly, both the main chassis and the dural lip of the sub-chassis are drilled for 6-32 machine screws that will hold the two units together. The top of the sub-chassis is recessed below the level of the main chassis deck about ¼". This allows the bandswitch shaft and the r-f tuning shaft (C_1) to line up properly with the other controls which are centered on the front edge of the main chassis.

The placement of the main controls on the front panel may be seen in the front view of the receiver, figure 25. The National HRO-type dial is centered on the panel, with the shaft about 5⅛" above the bottom of the panel. Since the dial gear drive is bolted to the main chassis of the receiver, positioning the dial fixes the relationship between the panel and the chassis. At the extreme left are the b.f.o. panel control (C_4) and the stand-by switch (S_2). To the right of S_2 is the audio gain control. Directly below the main tuning dial and to the right of the audio gain control is the bandswitch (S_1). To the right of S_1 is the r-f tuning control (C_1) and the r-f gain control. Above the gain control are the 6.3 volt pilot lamp and the earphone jack. The placement of the main parts above and below the chassis may be seen in figures 27 and 29.

The R-F Deck The placement of components in the r-f deck may be seen in figures 29 and 31. In the underneath view, the main bandswitch (S_1) is to the left, positioned so that the tie-rods of the switch are aligned vertically. Before the switch is assembled, the two shield partitions are cut to shape and drilled to pass the tie-rods and rotation shaft of S_1. The two shield partitions are grounded to the r-f deck by means of a right-angle bend along the length of the partition that fastens to the underneath side of the deck. A second bend along the end of the partition nearest the deck wall allows the partition to be fastened to the wall of the sub-chassis by means of 4-40 machine screws. Additional rigidity is given to the two shields by the bracing action of the switch tie-rods where they pass through the matching holes in the partitions. It is mandatory that the tie-rods of the switch be grounded to the shield partitions, as the tie-rods will introduce undesirable coupling between the various stages in the r-f deck if this is not done.

To prevent other undesired intercoupling, the ganged tuning capacitors (C_{1A} and C_{1B}) are connected together by a flexible insulated coupling.

The twelve coils used in the r-f deck are grouped in three rows of four coils each. The rows are separated from each other by the shielded partitions. The 28-Mc. and 21-Mc. coils are placed nearest the switch decks so that their leads to the switch contacts may be as short as possible. The 80-meter variable ceramic padding capacitors (C_5, C_6, C_7) are mounted directly from the switch points of the bandswitch to the nearest ground point, as seen in the bottom view, figure 29.

The various bypass capacitors and resistors associated with the r-f and mixer stages are mounted directly on the tube socket pins, or on insulated phenolic tie-point strips immediately adjacent to the sockets. The two r-f chokes (RFC_1) are National R-100U chokes that mount directly upon the inner side wall of the r-f deck. All of the power wiring may be done with flexible hook-up wire, but it is advised that the r-f wiring to the switch decks be done with no. 14 tinned copper wire for maximum stability.

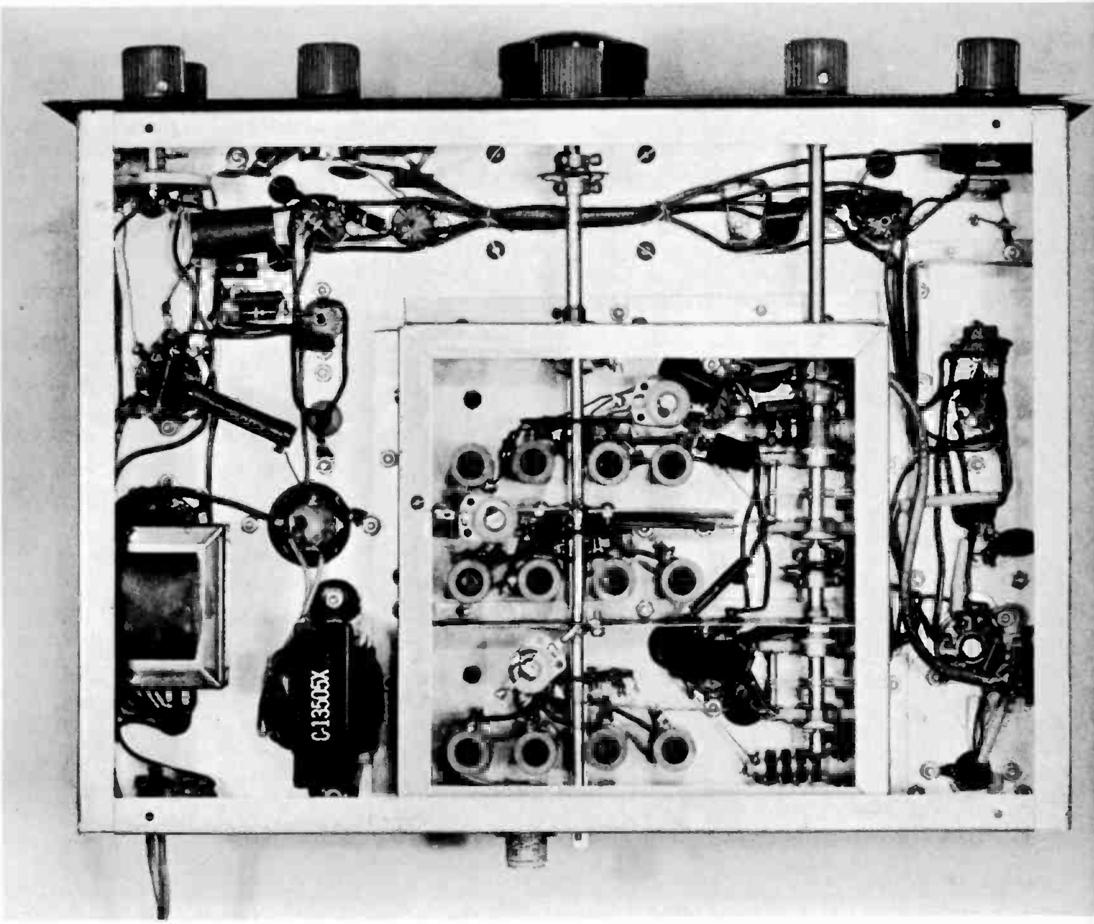


Figure 29

BOTTOM VIEW OF C-W RECEIVER

Power supply components and audio stages are to the left of the r-f deck; the i-f stages to the right. Insulated couplings are used on the control shafts of S_1 and C_1 which are both mounted on the r-f deck.

The main tuning capacitor, C_3, is mounted above the chassis after the receiver is completed. A ½" grommeted hole is used to bring up a no. 14 lead from the rotor arm of S_{1D} to to the stator of C_3 and return to socket pin 4 of the 6U8 tube, serving as a common ground return for the oscillator stage tuning capacitor.

All coils should be wound according to the coil table (figure 30) and connected into the switching circuits of the r-f deck before the deck is placed in the receiver.

Receiver Assembly and Wiring The receiver wiring should be completed before the r-f deck is placed in the receiver. All components should be mounted in place before any wiring is done. The Vector Plug-in Unit that contains the 6BA7 second mixer stage may be wired as a separate unit. It is placed within the shielded Vector box to reduce radiation from the crystal oscillator to a minimum. The crystal is mounted within the box, and the input, output and power leads are

TABLE I COIL TABLES

NOTE: 1. *ALL COILS WOUND ON NATIONAL XR-50 SLUG-TUNED FORMS, WINDING LENGTH – 11/16", DIA. 1/2", IRON SLUG.*
2. *ALL COIL WINDINGS SHOULD BE MADE WITH WIRE UNDER TENSION.*

$L_1 = L_5 =$	24 TURNS # 22 E., CLOSE WOUND. ANTENNA LINK OF L_1 IS 3 TURNS OF HOOKUP WIRE AT GROUND OF L_1. (*8 µH, APPROX.*)
$L_2 = L_6 =$	12 TURNS # 22 E., SPACED TO FILL FORM. (*2.6 µH, APPROX*)
$L_3 = L_7 =$	8 TURNS # 22 E., SPACED TO FILL FORM. (*1.2 µH, APPROX.*)
$L_4 = L_8 =$	5 TURNS # 22 E., SPACED TO FILL FORM. (*0.7 µH, APPROX.*)
$L_9 =$	24 TURNS # 28 E., CLOSE WOUND. (*7.0 µH, APPROX.*)
$L_{10} =$	11 TURNS # 22 E., SPACED TO FILL FORM. (*1.3 µH, APPROX.*)
$L_{11} =$	6 TURNS # 22 E., SPACED TO FILL FORM (*0.6 µH, APPROX.*)
$L_{12} =$	3 TURNS # 22 E., SPACED TO FILL FORM. (*0.3 µH, APPROX.*)

TABLE II

OSCILLATOR FREQUENCY WITH C_3 AT MAXIMUM CAPACITY (TO BE TUNED WITH GRID-DIP OSCILLATOR)

ADJUST	BANDSWITCH	FREQUENCY
L_9	40 METERS	5.4 MC.
L_{10}	20 METERS	12.3 MC.
L_{11}	15 METERS	18.3 MC.
L_{12}	10 METERS	26.4 MC.
C_5	80 METERS	5.0 MC.

TABLE III

R.F. AND MIXER COIL FREQUENCIES WITH C_{1A}, C_{1B} SET AT 75% MAXIMUM CAPACITY (TO BE TUNED WITH GRID-DIP OSCILLATOR)

ADJUST	BANDSWITCH	FREQUENCY
L_1, L_5	40 METERS	7.0 MC.
L_2, L_6	20 METERS	14.0 MC.
L_3, L_7	15 METERS	21.0 MC.
L_4, L_8	10 METERS	28.0 MC.
C_6, C_7	80 METERS	3.5 MC.

ADJUST B.F.O. TRANSFORMER SLUG TO 455.0 KC. WITH C_4 SET AT HALF-CAPACITY.

Figure 30

brought through the octal plug in the bottom of the unit. Since there is considerable inductance in the ground lead through the socket pin, the Vector box is strapped directly to the chassis by two short lengths of ¼" brass shim-stock. These brass strips are grounded to the lower assembly bolts of the Vector unit and connect to the machine screws that hold the octal socket to the receiver chassis. If these grounding straps are omitted, there is danger of self-oscillation in the 6BA7 mixer stage.

It is necessary to place a small aluminum partition across the under side of the mechanical filter to provide some isolation between the input and output circuits. This shield is 1½" high and 2" long.

The only leads that must be shielded in the receiver are the plate lead of the 6U8 and the diode lead of the 6AV6. Both of these leads are several inches long and should be shielded to prevent receiver instability. The shielded wire used in the receiver should be of the low capacity type to prevent detuning the primary of T_1 and the secondary of T_3. It may also be necessary to shield the lead from the volume control to the .01-µfd. audio coupling capacitor of the 6AV6 stage. This is a high impedance circuit, and some trouble from hum pickup may be had, especially if the six volt filament lead passes near the volume control. All components of the 6AV6 stage should be mounted in close proximity to the tube socket to minimize hum pickup. The filament lead to the 6AV6 tube should be spaced away from these components. If trouble is encountered with audio hum, the filament leads to the 6AV6 tube should be made with shielded wire.

The mounting of the tuning capacitor C_3 affects the stability of the receiver to a large degree. Since the receiver selectivity is less than one kilocycle, and the bandspread over an amateur band is of the order of 400 degrees on the main tuning dial, it is important that the utmost stability be achieved. A double bearing capacitor, such as the Bud MC-1850 should be used for C_3. It should be driven through a *good* flexible coupling that imparts no backlash to the drive. The front bearing of the capacitor is supported by an aluminum bracket to the edge of the chassis in front of the r-f deck. The rear of the capacitor is supported by a metal spacer mounted in the tapped hole in the foot of the capacitor. This spacer mounts C_3 firmly to the r-f deck. The leads to C_3 should be made of heavy solid wire to prevent vibration. A slight instability will be noted when the receiver is out of the cabinet since an aluminum chassis is used for ease of construction. Better mechanical stability may be had if a steel chassis is used; however, the steel chassis is much harder to drill and cut. When the receiver is firmly mounted in the case, and the rear lip of the chassis bolted to the case, the slight instability will vanish.

All capacitors and resistors associated with a particular stage of the receiver should be mounted on or near the tube socket of that stage, and care should be taken to keep the wiring to all components short and direct.

Receiver Alignment The first step is to align the i-f system of the receiver. After all wiring has been checked, all tubes except the 12AT7, the 6U8 and the 6C4 should be plugged in their sockets. Bias voltages should be checked against those shown in the schematic of figure 26. The signal generator should be tuned to 455 kc. and coupled to the plate prong of the 6BA7 through a .001-µfd. capacitor. Primary and secondary windings of T_2 and T_3 should be resonated for greatest audio output from the receiver when the signal generator is modulated with a tone signal. The passband of the mechanical filter is extremely sharp, and care must be taken in setting the frequency of the signal generator. The generator should be set to the center frequency of the mechanical filter, and T_2 and T_3 peaked for maximum output at that frequency.

The signal generator should now be clipped to the plate lead of the 6U8 tube socket through the .001-μfd. condenser, and a 1535 kc. signal injected into the primary of T_1. The primary and secondary of T_1 may be given a preliminary alignment. Alignment should be made with a minimum of signal output from the signal generator to prevent spurious responses in the receiver.

The next step is to align the r-f deck of the receiver. The 12AT7 and 6U8 tubes should be plugged in their sockets and the bandswitch set to the 40-meter position. The main tuning capacitor, C_3, should be set with the plates fully meshed. The r-f tuning capacitors, C_{1A} and C_{1B} should be set about 75% meshed. Using a grid-dip oscillator, the 6U8 oscillator inductances should be tuned until the tuned circuits resonate at the frequencies indicated in Table 2 figure 30 for the 40, 20, 15 and 10 meter bands. The bandswitch should then be set to the 80-meter position, and the 80-meter oscillator padding condenser set for an indicated frequency of 5.0-Mc. on the grid-dip oscillator.

When the oscillator inductances have been set to the approximate frequencies indicated in Table 2, the bandswitch should be returned to the 40-meter position and the r-f and mixer coils should be tuned by means of the grid-dip oscillator as shown in Table 3 figure 30. The 80 meter adjustments should be made last.

After these preliminary adjustments have been made, the receiver may be accurately aligned and calibrated by means of a good frequency meter, such as the BC-221. Oscillator coils L_9-L_{12} and padding capacitor C_8 should be adjusted to make the lower edge of each amateur band fall at about 50° on the HRO-type tuning dial. The r-f and mixer adjustments of L_1-L_8 and C_6, C_7 should be made so that the r-f and mixer circuits track at the low frequency end of each amateur band at the same setting of C_{1A}-C_{1B}. Under these conditions, this control need never be touched except for a slight "peaking-up" when the receiver is switched from band to band.

If more bandspread is desired, particularly on the 10, 15 and 20-meter bands, C_3 may be reduced in value to 15 $\mu\mu$fd. This will allow the receiver to cover only the bottom 200 kc. of the 80-meter c-w band, but will greatly increase the bandspread on the higher frequency bands.

As a final step, it is wise to place a drop of nail polish or Duco Cement on each one of the powdered iron slugs of the high frequency oscillator coils. This prevents any oscillator instability caused by random movement of the slugs within the coil form. The oscillator coil windings should be given a thin coat of cement.

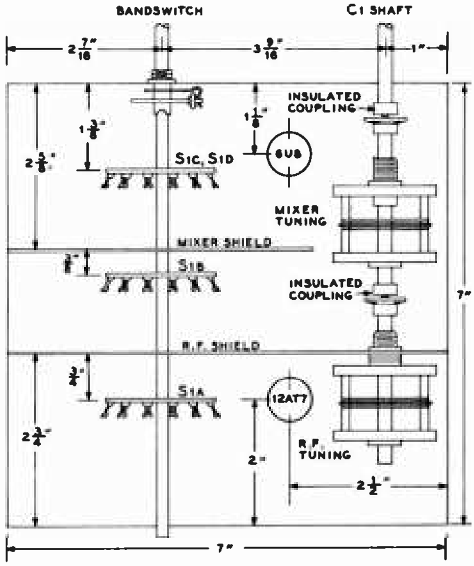


Figure 31
UNDER-CHASSIS
Layout of R.F. section

During operation of the receiver it will be noticed that there are two second order "birdies" from the 6BA7 conversion oscillator: one falls in the middle of the 80-meter band and is quite weak. The other falls in the middle of the 40-meter band and is of medium strength. Once recognized, they cause a minimum of trouble. They could be cured by the use of more complete shielding within the r-f sections of the receiver, but it is felt that they are of minor importance and may be ignored.

The last adjustment that may have to be made to the receiver is a balancing of the gain of the r-f and i-f stages. Under normal operating conditions, the residual noise picked up by the antenna system should mask out the internal noise of the receiver. If the antenna is removed from the receiver, and the internal noise does not drop appreciably, it is usually a sign that the receiver's i-f gain is too high and the r-f gain too low. The i-f gain of the receiver may be decreased by increasing the values of the cathode resistor and the screen resistor of the first 6BA6 i-f amplifier stage. Receiver gain may be increased by decreasing the value of the cathode resistor of the second 6BA6 i-f amplifier tube to about 150 ohms.

CHAPTER TWENTY FIVE

Exciters and Low Power Transmitters

Several different types of equipment designed to meet a range of needs have been described in this chapter. There is a simple all-band 40 watt phone and c-w transmitter, and several v-f-o units and exciters for the lower frequency bands. Of particular interest to the VHF man is a 2 meter transmitter employing the new AX-6360 miniature double tetrode.

For the Technician or beginner there is a simple 220-Mc. transceiver, and for the DX-man a high stability VFO unit. To the amateur who is interested in the construction phase of his hobby, these units should offer interesting ideas which might well fit in with the design of his basic transmitting equipment.

25-1 40-Watt All-Band Transmitter

This 40 watt phone-c.w. transmitter is an ideal unit for the beginning amateur. At the same time, it makes a fine stand-by transmitter for the advanced amateur who is interested in a small, compact piece of equipment. It is completely self-contained, and operates on all bands from 160 meters to 10 meters.

Circuit Description A block diagram of the transmitter is shown in figure 1 and the complete schematic in figure 3. A single 6146 tetrode tube is used as a class C amplifier on all bands, running at approximately 400 volts at 100 milliamperes. A 6AG7 is employed as a crystal oscillator. When the transmitter is operated on 160, 80 or 40 meters the 6AG7 functions as a straight crystal oscillator, using fundamental frequency crystals. On 160 meters, section S_{1B} of the oscillator plate circuit switch adds 15 $\mu\mu$fd. of capacity between the grid and plate circuits of the 6AG7, introducing sufficient feedback to sustain oscillation with the more sluggish low frequency crystals. When the transmitter is operated on the 20, 15, 11 and 10 meter bands, the 6AG7 functions as a tri-tet oscillator with the plate circuit of the oscillator tuned to the desired harmonic. The cathode tri-tet coil and capacitor are so proportioned that they may be left in the oscillator circuit at all times, with no detrimental effect upon the operation of the oscillator at lower frequencies.

Switch section S_{1A} selects the proper oscillator coil. Each oscillator coil is slug tuned to the approximate output frequency, and oscillator tuning is accomplished by C_1. The 160

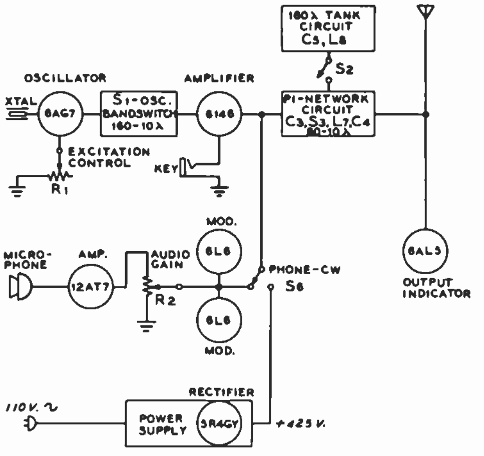


Figure 1
BLOCK DIAGRAM OF 40-WATT PHONE-C.W. ALL-BAND TRANSMITTER

meter oscillator coil, L_6, has an additional 100 μμfd. padding capacitor connected across it.

Excitation to the 6146 stage is controlled by varying the screen voltage on the 6AG7 oscillator tube. The excitation control, R_1, allows the oscillator screen voltage to be set to any value between zero and 200 volts.

The oscillator is capacitively coupled to the grid circuit of the 6146 class C amplifier. Grid leak bias is used on the 6146, and the tube is protected by a 6AQ5 clamper tube in the screen circuit. Screen voltage for the 6AQ5 clamper tube is obtained from a dropping resistor from the 300 volt supply, rather than by tying the screen of the 6AQ5 to the screen of the 6146. This allows greater clamping action, and the 6146 tube is fully protected during periods of no excitation. Screen voltage may be removed from the 6146 by means of switch S_5. This switch disables the final amplifier stage, and allows tuning adjustments to be made to the 6AG7 oscillator without fear of damage to the 6146 tube. Cathode keying is used in the 6146 stage to minimize keying effects or "yoops" which may result if the 6AG7 crystal oscillator is keyed.

A pi-network tank is employed in the plate circuit of the 6146 amplifier stage. The resonating capacitor is C_3 and the loading capacitor is C_4. A tapped plate coil, L_7, allows the pi circuit to resonate on any band between 80 and 10 meters. Switch S_2 is thrown for 160 meters and additional capacitance and inductance are added to the pi-network circuit to allow operation on this band. Switch S_4 adds additional capacity to the output side of the pi-network to allow operation into loads of low ohmic resistance on the low frequency bands.

For ease in tuning, an output meter is connected to the antenna circuit of the transmitter. A 6AL5 is used in a half-wave circuit to deliver a rectified voltage that is proportional to the r-f voltage at the antenna terminal of the transmitter. Such an indication is of great assistance when the transmitter is tuned up into different antenna systems. Switch S_9 permits the 0-15 milliampere d-c meter to read this output voltage.

A 12AT7 tube provides two stages of speech amplification, which is ample for use of a low

Figure 2
40-WATT ALL-BAND PHONE-C.W. TRANSMITTER

The various controls (from left to right) across the bottom of the transmitter are: microphone and key jacks, gain control R_2, crystal socket, oscillator switch S_1, oscillator tuning capacitor C_1, excitation potentiometer R_1, antenna loading switch S_4, antenna loading capacitor C_4. Across the top of the panel (from left to right): red pilot lamp S_8, meter switch S_9, phone-c.w. switch S_6, green pilot lamp, 160-meter switch S_2, main tuning capacitor C_3, and amplifier band switch S_3.

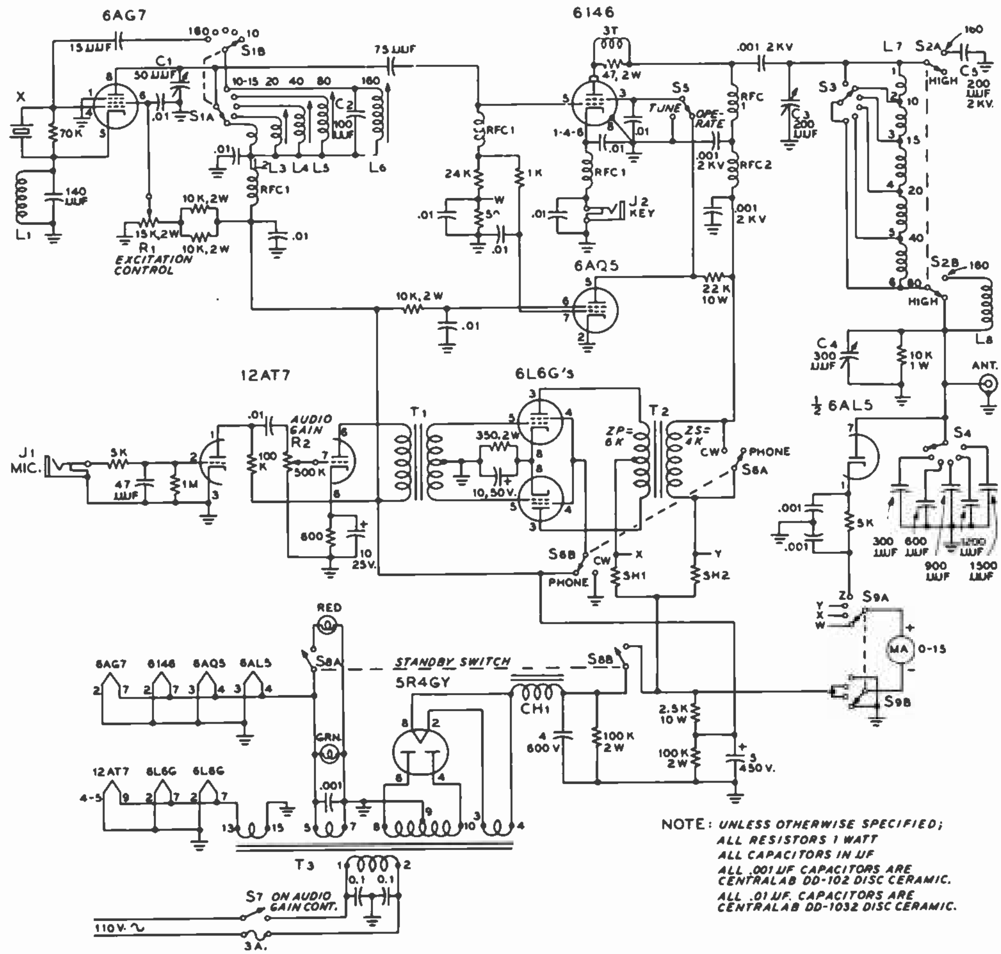


Figure 3

SCHEMATIC OF 40-WATT ALL-BAND TRANSMITTER

C_1—50 $\mu\mu$fd. Bud MC-903
C_2—100 $\mu\mu$fd. ceramic
C_3—200 $\mu\mu$fd. Bud MC-908
C_4—300 $\mu\mu$fd. Bud MC-910
C_5—200 $\mu\mu$fd. mica 2 kv.
R_1—15,000 ohms, 2 watts
R_2—0.5 megohm, audio taper, with switch S_7
RFC_1—2.5 mh. National R-100
RFC_2—10 μh. J.W. Miller 4612
J_1, J_2—Closed circuit jack
S_1—2 pole, 5 position switch Centralab 2505
S_2—2 pole, 2 position switch Centralab 2543
S_3—Centralab Index Assembly P-121 and switch section P1S
S_4—1 pole, 6 position switch Centralab 2501
S_5—s.p.d.t. toggle switch
S_6—d.p.d.t. toggle switch
S_7—See R_2
S_8—d.p.s.t. toggle switch
S_9—2 pole, 4 position switch Centralab 1405
T_1—Interstage transformer Merit A-2914
T_2—60 watt modulation trans. Merit A-3110
T_3—525-0-525 volts at 250 ma. 5 v. at 3 a., 6.3 v. at 3 a., 6.3 v. at 3 a. UTC S-40
CH_1—20 hy. at 225 ma. UTC-S31
By-pass capacitors on 110-volt line are Sprague "Hy-pass" type 80P3.

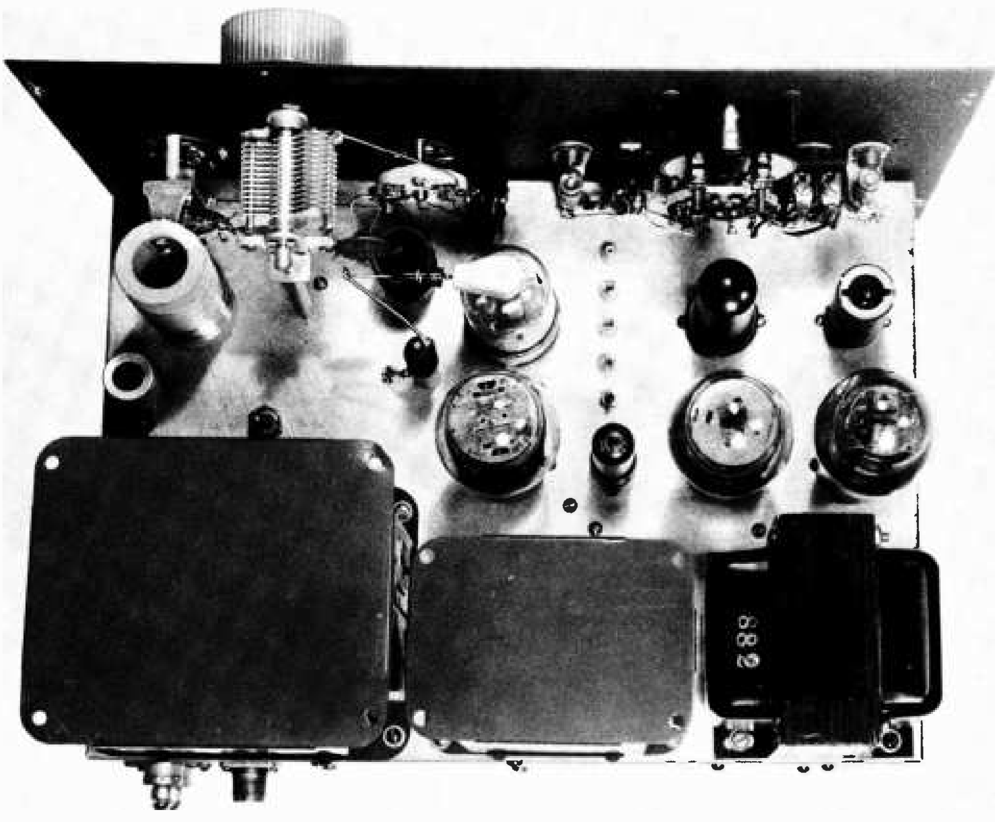
level crystal microphone. The second section of the 12AT7 has the audio level control, R_2, in its grid circuit and is transformer coupled to the two 6L6-G class AB_2 modulators.

A single heavy duty power supply using a 5R4-GY rectifier tube supplies 400 volts to the final amplifier and modulator stage, and 300 volts to the other stages of the transmitter. Switch S_{8B} breaks the B-plus lead of the power supply for stand-by purposes. Switch S_{8A} turns on a red pilot jewel when the B-plus circuits are closed, serving as a "transmit" indicator lamp.

Choice of phone or c-w operation is made possible by switch S_6. When c-w operation is desired, S_{6A} shorts out the secondary of the modulation transformer T_2 and S_{6B} grounds the screen circuit of the 6L6-G modulators. The transmitter may then be keyed by inserting a key in jack J_2.

A 0-15 milliampere d-c meter is used to measure various currents in the transmitter, selected by switch S_9. Position 1 of S_9 connects the meter (via lead W) to the grid circuit of the 6146 tube to measure rectified grid current of this stage. In this position, maximum scale reading of the meter is 15 milliamperes. Position 2 of S_9 (lead X) connects the meter in the plate circuit of the class AB_2 modulator stage. The meter is connected across shunt SH_1 which increases the maximum scale reading of the meter to 150 milliamperes. Position 3 of S_9 (lead Y) connects the meter in the plate circuit of the 6146 stage. The meter

Figure 4
TOP VIEW OF THE 40-WATT TRANSMITTER
Placement of the various components is discussed in the text



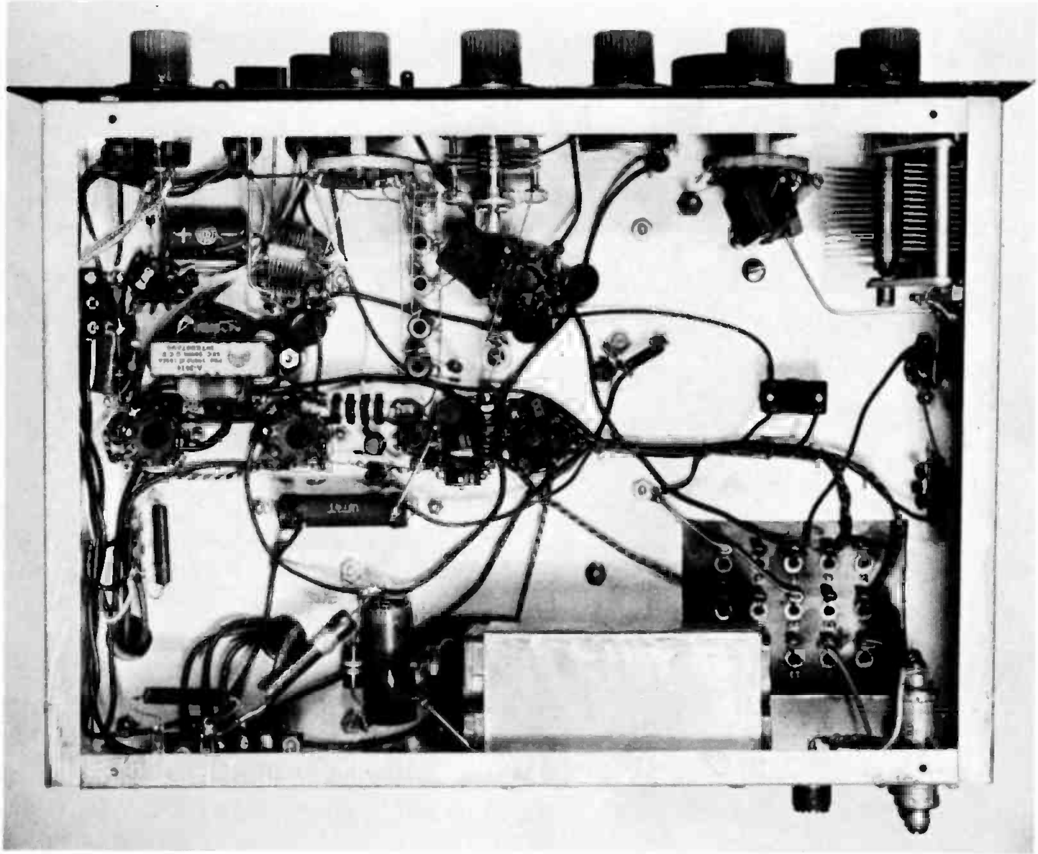


Figure 5
BOTTOM VIEW OF CHASSIS OF THE 40-WATT TRANSMITTER

is connected across shunt SH_2 which increases the maximum scale reading of the meter to 150 milliamperes. Position 4 of the meter switch connects the meter to the 6AL5 output indicator. The full scale reading of the meter is 15 milliamperes in this switch position.

Transmitter Assembly The transmitter is built upon an aluminum chassis measuring 10"x 14"x 3" in size (Bud AC-414). The transmitter cabinet measures 9" high by 15" wide by 11" deep (Bud C-975). The aluminum chassis is attached to the panel by means of the control shafts of the various condensers and potentiometers mounted along the front lip of the chassis. The steel cabinet has a 1/2" flange that runs around the four sides of the front to which the front panel attaches. It is necessary to leave a space of about 1/16" between the chassis and the front panel, into which gap the lower cabinet lip will fit. This is easily done by fastening the front panel controls to the chassis by means of the shaft nuts before the front panel is placed over the control shafts. After the panel has been placed in position, a second set of shaft nuts holds the panel to the chassis, spaced the required distance by the first set of shaft nuts between the panel and the chassis. Placement of the major components is shown in figures 2, 4, 5, 6 and 7. Transformer T_1 is mounted below deck in the area between the 6L6-G sockets and the 6AG7 socket. The 4 μfd., 600 volt filter capacitor (made up of two 2 μfd. oil capacitors in parallel) is bolted

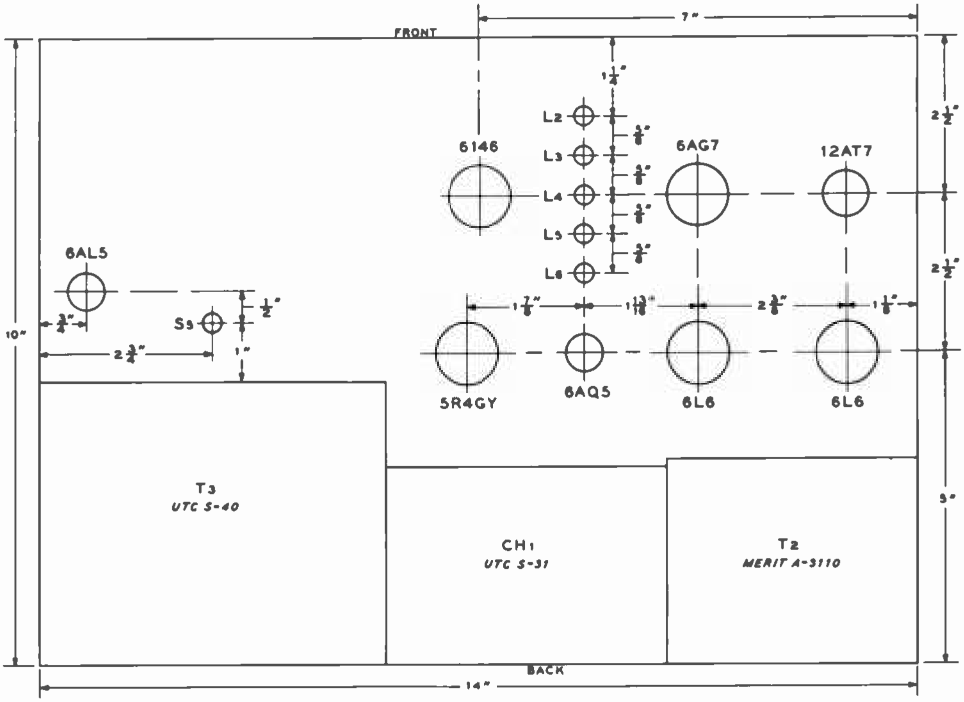
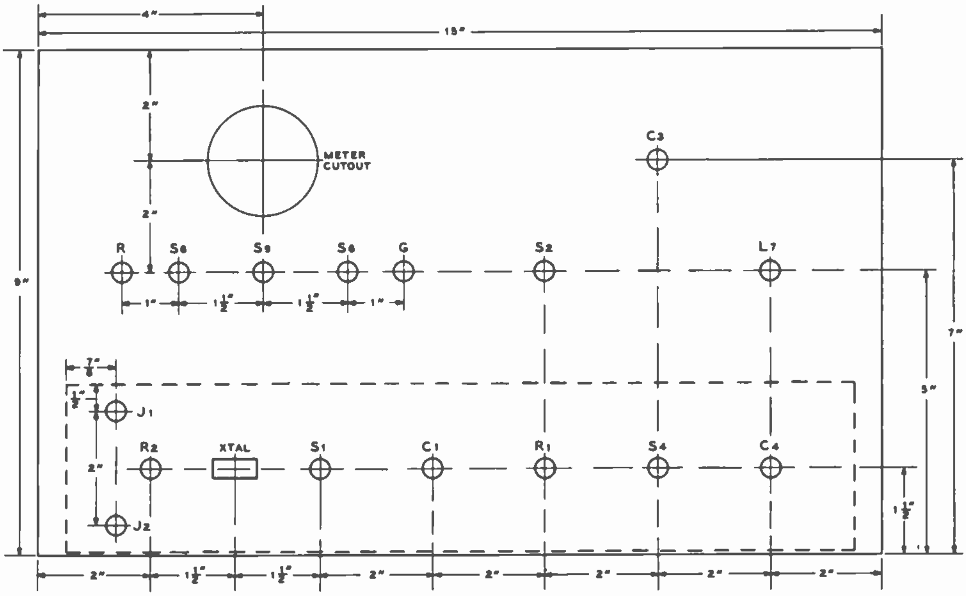


Figure 6
PLACEMENT OF MAJOR COMPONENTS ABOVE CHASSIS OF 40-WATT TRANSMITTER

Figure 7
PANEL LAYOUT OF 40-WATT TRANSMITTER



SOCKET CONNECTION CHART

TUBE	6AC7	6146	6AQ5	12AT7	6L6-G	6AL5
GROUND SOCKET PINS	1,2	7,8	2,3	3,4,5	1,2	3,6
FILAMENT PIN *	7	2	4	9	7	4

* *EACH FILAMENT PIN BYPASSED TO GROUND BY A .001 UF. CERAMIC CAPACITOR (CENTRALAB DD-102)*

Figure 8

COIL TABLE

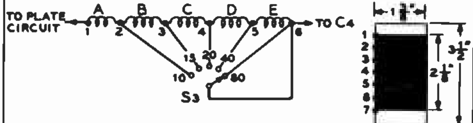
L1 = 8 TURNS # 20, 1" DIA., 1/2" LONG. (2.4 UH) *B&W # 3015*
L2 = (10-15 METERS) 11.5 TURNS # 22 E., 1/4" DIA., 3/8" LONG (1 UH) *J.W. MILLER R.F. COIL # 4502* WITH SLUG REMOVED
L3 = (20 METERS) 23 TURNS # 28 E., 1/4" DIA., 3/8" LONG (3 UH) *J.W. MILLER R.F. COIL # 4504* WITH POWDERED IRON SLUG
L4 = (40 METERS) APPROX. 38 TURNS # 32 E., 1/4" DIA., 3/8" LONG (9 UH) *J.W. MILLER R.F. COIL # 4506* WITH POWDERED IRON SLUG
L5 = (80 METERS) (45 UH) *J.W. MILLER R.F. COIL # 4509 WITN POWDERED IRON SLUG*
L6 = (160 METERS) (50 UH SHUNTED WITH 100 UUF) *J.W. MILLER R.F. COIL # 4509* WITH POWDERED IRON SLUG
L7 - TOTAL INDUCTANCE 12 UH, SWITCHED AS FOLLOWS: 80 METERS - 12 UH (*SECTION A+B+C+D+E*) 40 METERS - 6.5 UH (*SECTION A+B+C+D*) 20 METERS - 2.0 UH (*SECTION A+B+C*) 15 METERS - 1.3 UH (*SECTION A+B*) 10 METERS - 0.7 UH (*SECTION A*) COIL IS WOUND ON CERAMIC FORM, 1 3/8" DIA. AND 3 1/2" LONG. L7 IS MOUNTED BY ITS LEADS TO CONTACTS OF S3.  SECTION A - 4 TURNS # 16. SPACED TO 1/2" LONG SECTION B - 2 TURNS # 16. SPACED TO 1/4" LONG SECTION C - 2 TURNS # 16, SPACED TO 1/4" LONG SECTION D - 4 TURNS # 16, SPACED TO 3/8" LONG SECTION E - 13 TURNS # 20. SPACED TO 3/4" LONG
L8 - WOUND ON PHENOLIC FORM. 1" DIA. AND 1 1/2" LONG. 30 TURNS # 20 E., CLOSEWOUND

Figure 9

to the back wall of the chassis by means of a U-clamp made of dural. The coaxial connector for the antenna and the two 110-volt "Hy-pass" capacitors are mounted on the back wall of the chassis directly below T_3.

The amplifier plate circuit tuning capacitor, C_3, is held to the front panel by means of the threaded front bearing of the capacitor. In addition, a 1/4" rod (cut from a section of extension shaft) about 2¾" long is used as a rear mounting stud for the capacitor. The rod is tapped at both ends for a 6-32 machine screw. One end of the rod is bolted to the chassis deck and the top end is fastened to the rear mounting foot of C_3. Inductor L_8 is mounted behind switch S_2. The coil form of L_8 is bolted directly to the chassis deck. Capacitor C_5 is mounted behind S_2. The plate choke (RFC_1) of the 6146 has a ceramic mounting pillar (National R-100U) and is mounted between the 6146 socket and C_3. Pilot lamps G and R, and switches S_6, S_8 and S_9 are mounted on the front panel of the transmitter, as is the 2" d-c milliammeter.

Wiring the Transmitter Pilot lamps G and R, and switches S_6, S_8 and S_9 should be wired first. Since most of the leads from these components pass through a 1/2" rubber grommet mounted in the top deck of the chassis directly below S_9, it is best to use color coded wire for these leads, otherwise the identity of the leads will be lost after they pass through the rubber grommet. After the panel components have been wired, the panel should be attached to the chassis.

The next step is to ground certain socket pins of each socket, as shown in figure 8. These connections should be made to the socket ground lugs with short, direct leads. Lock washers should be employed on all socket bolts to insure that a good ground connection to the chassis is obtained. Each filament pin of each socket should be bypassed to ground as shown in figure 8 with a .001 μfd. ceramic capacitor (Centralab DD-102). After these preliminary connections have been made the filament wiring and power supply wiring should be done. The 110 volt leads to S_7 (on the back of R_2) should be run in shielded wire as these leads pass near the low level audio stages of the transmitter.

Wiring of the 6AG7 and 12AT7 sockets should be done first. The tri-tet cathode coil and capacitor should be placed across the 6AG7 socket between pins 5 and 1 after the rest of the oscillator stage wiring has been completed.

The leads from coils L_2-L_6 to the bandswitch S_1 are made of tinned no. 20 wire, as are the leads between C_4, S_4 and S_2. The lead from C_4 to the coaxial antenna receptacle mounted on the rear of the chassis is made from a short length of RG-59/U coaxial line. Both ends of the shield of this line are grounded.

The meter shunts SH_1 and SH_2 multiply the meter range by 10. Therefore 1/10 of the total circuit current should flow through the meter and 9/10 of the current through the shunt. The shunts, therefore, should have about 1/10 the resistance of the meter movement. A Triplett type 227-T meter is used which has an internal resistance of about 6.6 ohms. SH_1 and SH_2 should each be about 0.66 ohms. Two 5 per cent IRC type BW resistors (0.62 ohms) may be used for the shunts, or the shunts may be

TUNING CHART

OUTPUT FREQUENCY	CRYSTAL FREQUENCY	OSC. COIL	S3 SETTING	S4 SETTING	S2 SETTING
160 M.	160 M.	L6	TAP 6	1500 μμF	160
80 M	80 M	L5	TAP 6	800-1200 μμF	HI
40 M.	40 M.	L4	TAP 5	300 μμF	HI
20 M	40 M	L3	TAP 4	300 μμF	HI
15 M.	40 M.	L2	TAP 3	0	HI
10 M	40 M	L2	TAP 2	0	HI

TABLE I

wound out of suitable lengths of resistance wire, if desired.

Choke RFC_2 is mounted below the chassis and in combination with the .001 μfd. capacitors on each side of it makes an effective harmonic filter for the plate voltage lead of the 6146. The .001 μfd. capacitor located between RFC_1 and RFC_2 is a Centralab type FT feed-through unit. The v-h-f lead inductance of this capacitor is virtually zero.

When all components have been mounted and the wiring has been completed *and checked* the transmitter is ready for a preliminary check-out.

Transmitter Check-out 1. A d-c ohmmeter should be connected between the positive terminal of the high voltage filter capacitor and ground. After the capacitor charges, the resistance to ground should read 100,000 ohms with S_8 open, and approximately 20,000 ohms with S_8 closed.

2. The test meter should be switched to read high voltage, and the 5R4-GY rectifier tube plugged in its socket. S_7 should be closed, S_8 open. 110 volts should be applied to the transmitter. A plate voltage reading of 450 should be obtained on the meter. The transmitter should now be turned off.

3. The 6AG7 and 6146 tubes should be plugged in their sockets. The oscillator tuning capacitor, C_1 should be set to mid-scale. Using a grid-dip oscillator, coils L_3-L_6 should be resonated to the middle of their respective bands by means of their adjustable slugs. The slug should be removed from L_2. Switch S_5 should then be set to "tune" position.

4. Transmitter controls should be set as shown in Table I for the band in use, and the proper crystal should be inserted in the oscillator socket. The 6146 stage is disabled by switch S_5 set to "tune." The transmitter is turned on and C_1 tuned for indication of oscillation when S_9 is set to position 1 to read grid current of the 6146. Maximum grid current should be held to less than 3 milliamperes by adjustment of the excitation control, R_1.

5. A suitable antenna or dummy load should be connected to the antenna coaxial receptacle and loading capacitor C_4 set at maximum capacity. S_5 is thrown to "operate" position and S_8 closed, putting the transmitter in operation. Capacitor C_3 is tuned for plate circuit resonance (minimum reading of meter when S_9 is in third position). Capacitor C_4 and switch S_4 should be adjusted for a resonance plate current of 100 milliamperes to the 6146. R-f output into the antenna system may be read on position 4 of S_9.

6. After the transmitter is performing on c.w., the audio tubes should be plugged in their respective sockets and switch S_6 set to

Figure 10
HIGH STABILITY V.F.O. AND POWER SUPPLY

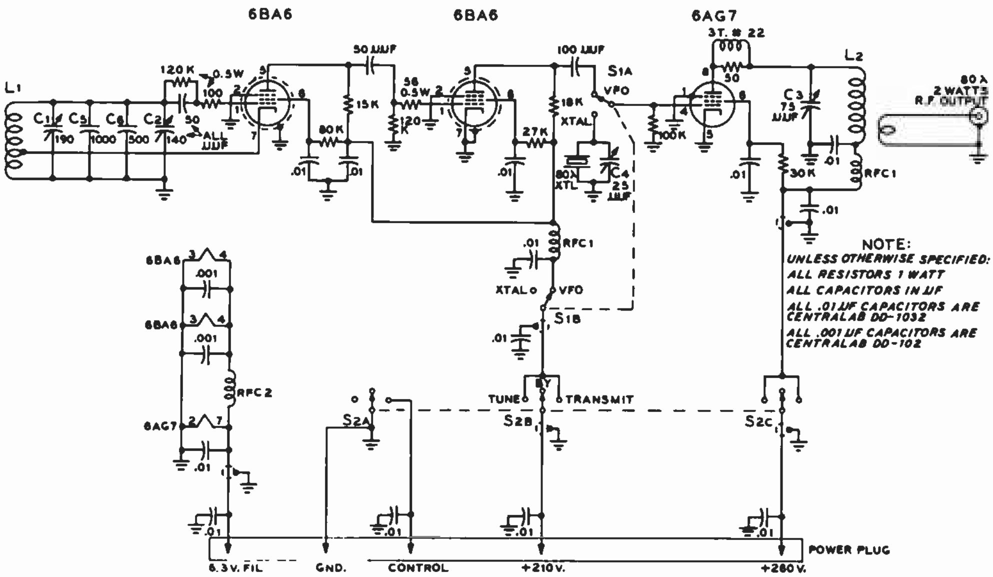


Figure 11
SCHEMATIC OF HIGH STABILITY V.F.O.

C_1—190 μμfd. Bud MC-1858
C_2—140 μμ fd. Bud MC-906
C_3—75 μμfd. Bud LC-1645
C_4—25 μμfd. Bud LC-2077
C_5—1000 μμfd. Centralab 950
C_6—500 μμfd. Centralab 950
RFC_1—2.5 mh. National R-100
RFC_2—15 μh. J.W. Miller 4624
S_1—2p.d.t. Centralab 1462
S_2—3p.3t. Centralab 1407

"phone." When S_9 is set to position 2, the modulator plate current should kick to approximately 90 milliamperes for 100 per cent modulation.

7. The transmitter is very nearly TVI-proof. To prevent excessive harmonic radiation from the antenna system, a TV filter such as described in Chapter 16 should be placed in the coaxial line from the transmitter to the antenna system.

8. When the operator has become familiar with the controls of the transmitter, white panel "decals" should be placed above all controls as shown in figure 2. The decals may be affixed permanently by brushing them with a *light* coat of nail-polish remover after they are thoroughly dry.

25-2 A High Stability V.F.O. Unit

The v.f.o. shown in figures 10, 12 and 13 is the end result of considerable experimentation in an effort to develop a simple operating-table v.f.o. having high frequency stability, and still be simple enough for home construction.

The outstanding problem in any variable frequency oscillator is to obtain adequate frequency stability for the use of a crystal filter at the receiving position on the 28-Mc. band. This may be taken as the limiting factor in so far as absolute frequency stability is concerned for amateur band work. The v.f.o. frequency must be stable with respect to warm-up, ambient temperature variations, line voltage shift, vibration and the presence of a strong r-f field in the vicinity of the v.f.o.

To achieve these requirements in actual practice requires great care in the design of the v.f.o. circuit and in the physical construction of the unit.

Frequency Stability The perfect v.f.o. has the frequency determining elements completely isolated both electrically and physically from the rest of the transmitting equipment. Unfortunately this goal cannot be reached, since a vacuum tube must be coupled to the frequency determining circuit to maintain oscillation. This deteriorates the electrical isolation of the frequency determining circuit.

The frequency determining circuit is also subject to temperature variations in the atmosphere, changes in the relative humidity, and absorption of the radiated heat of nearby objects. By using temperature and humidity resistive materials and removing as many tubes as possible from the vicinity of the frequency determining circuits, a good degree of stability in the v.f.o. may be obtained.

Finally, steps must be taken to insure that the oscillator of the v.f.o. unit is completely free from parasitics, and that the output waveform of the oscillator is low in harmonic content. The v.f.o. unit to be described meets these fundamental requirements.

The V.F.O. Circuit The circuit of the high stability v.f.o. is shown in figure 11, and the physical layout of the complete v.f.o. unit is illustrated in figures 10, 12 and 13.

A 6BA6 remote cutoff pentode is used as the oscillator tube. The oscillatory circuit operates in the 160 meter band and consists of a high-Q oscillator coil resonated to frequency by two precision ceramic capacitors. These capacitors (Centralab type 950) have a measured temperature coefficient of less than plus or minus ten parts per million over the temperature range of −40 degrees to plus 60 degrees centigrade. The use of ordinary ceramic or silver mica capacitors as a substitute for these units is not recommended, since the temperature coefficient of such units cannot be closely controlled in production.

The oscillator coil, L_1, is wound upon a phenolic coil form that has approximately the same coefficient of expansion as does the copper wire. A ceramic coil form should not be used here. The coil turns are spaced to insure low inter-turn capacity. The wire is wound upon the form under tension so that for all practical purposes the wire and the form have the same coefficient of expansion with regard to temperature changes. This will decrease the possibility of the oscillator developing random frequency jumps with changes in temperature and humidity.

A 100 ohm series resistor is inserted in the grid lead to the 6BA6 oscillator tube. This

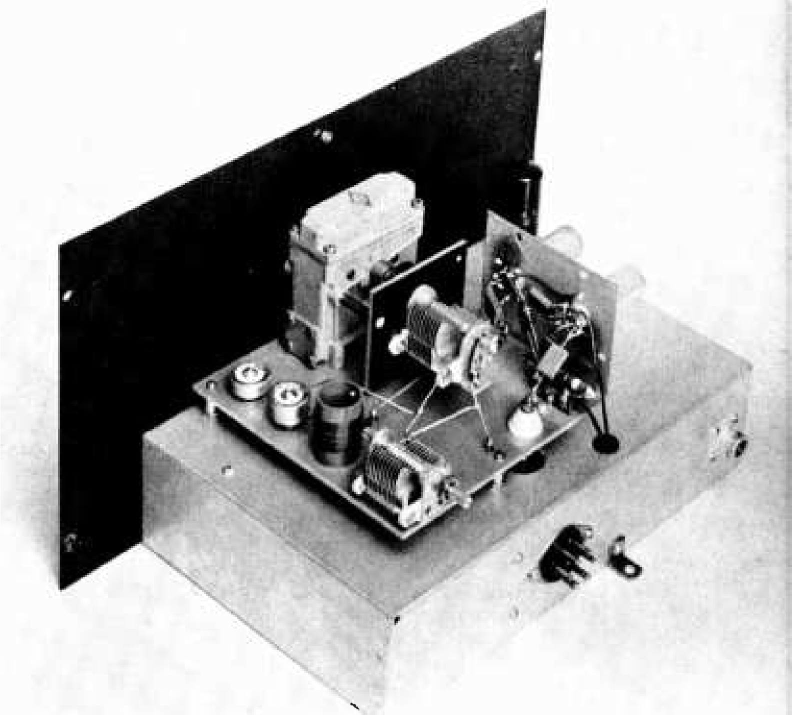


Figure 12
REAR VIEW OF V.F.O.
The high stability ceramic padding capacitors for the oscillator tank are on the left corner of the chassis. The two 6BA6 tubes are mounted horizontally at the right. The main tuning capacitor is firmly attached to the gear drive unit.

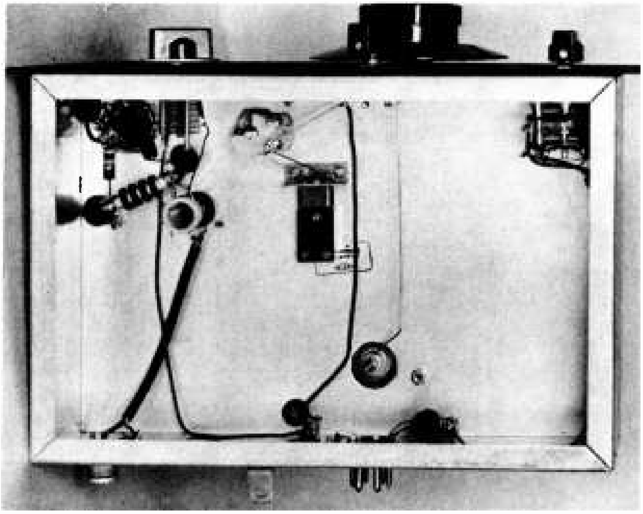


Figure 13
UNDER-CHASSIS VIEW OF V.F.O.
The crystal is mounted on a small angle bracket at the center of the chassis. All power leads are by-passed at power plug on rear of chassis.

eliminates a weak parasitic oscillation that is common to this type of oscillator circuit. The parasitic tends to make fundamental oscillation unstable at certain settings of the oscillator tuning capacitor. This is probably caused by a variation in the internal inductance of the tuning capacitor at the frequency of the parasitic oscillation.

All components of the oscillator circuit are spaced clear of the oscillator tube to prevent heat transfer from the oscillator tube to the frequency determining components.

The 6BA6 oscillator is R-C coupled to a second 6BA6 which serves as an isolation amplifier. The plate and screen voltage supply of both 6BA6 tubes is regulated at 210 volts. The filament terminal of each 6BA6 is by-passed to ground by a .001 μfd. ceramic capacitor, and the filament lead to these tubes passes through a r-f choke to insure maximum lead isolation.

The output of the 6BA6 isolation stage is capacity coupled to a 6AG7 stage which serves either as a frequency doubler or as a crystal oscillator. The v.f.o. covers the frequency range of 1750 kc. to 2000 kc., and the plate circuit of the 6AG7 doubler stage tunes 3500 kc. to 4000 kc. Switch S_1 disables the v.f.o. circuits and connects the 6AG7 as an 80 meter crystal oscillator. A 3500.1-kc. crystal serves as a low frequency band-edge marker. The exact frequency of the crystal may be varied about 50 cycles by means of a small variable padding capacitor (C_4) connected across it. The output of the 6AG7 stage on 80 meters is about two watts which is sufficient to drive a tetrode buffer such as an 807 or 6146.

Transmitter keying for c-w operation is done in the stages following the v.f.o. exciter to allow maximum stability and freedom from frequency shift with keying. A stand-by switch, S_2, is incorporated in the v.f.o. unit which has auxiliary contacts to control the other transmitting circuits.

Mechanical Design of the V.F.O. The mechanical design of the v.f.o. is equally as important as the electrical design if maximum stability and reliability are to be achieved. Provision must be made for dissipation of the heat of the vacuum tubes, and the v.f.o. components should be mounted on a thick slab of conducting material which will act as a heat "sink" and which will tend to resist rapid changes in the temperature of the various components.

The main components of the v.f.o. and the two 6BA6 tubes are mounted upon a 6½"x 6½" piece of dural plate, 0.125" in thickness. The 6BA6 tubes are mounted horizontally on a steel bracket that is positioned above the dural plate. The bracket is 3" high and 4" long with a 1" flange that is bolted to the dural plate.

The gear box of the National HRO-type dial is bolted to the front of the dural plate. The main tuning capacitor, C_1, is affixed by its front bearing to a 3"x 3"x 0.125" dural plate which is bolted to the gear box by means of three long machine screws and three 1¼" metal spacers. The tuning capacitor is driven through a high-quality flexible coupling. This coupling should be free of back-lash, and should not permit end pressure on the shaft of the tuning capacitor. A Johnson type 104-250 coupling is recommended.

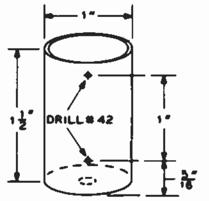
Output from the v.f.o. section is taken through the dural plate by a 3/4" feed-through insulator, and through a 1" hole in the sub-chassis. The dural plate is bolted to the sub-chassis by means of three 1/2" spacers and 6-32 machine screws.

The sub-chassis of the v.f.o. unit is a dural chassis measuring 8"x 12"x 3" (Bud AC-424). The complete unit is encased in a steel cabinet measuring 9"x 11"x 15" (Bud C-975). The sub-chassis is bolted to the 9"x 15" panel by means of the 3/8" collar nuts on C_3, S_1 and S_2. A small right angle foot is mounted at the rear of the chassis (figure 12) and fastens the rear of the chassis securely to the bottom of the cabinet. This eliminates a slight waver in the note of the v.f.o. caused by the movement of the v.f.o. chassis with respect to the cabinet.

The 6AG7 output tube is mounted in the front corner of the chassis, away from the frequency determining circuits. The output tuning capacitor, C_3, is a panel control and is mounted close to the 6AG7 socket. All components of the 6AG7 stage are mounted beneath the chassis for maximum isolation from the v.f.o. circuits. The 80 meter crystal is mounted in a holder attached to a small bracket, and may be seen in the middle of the chassis (figure 13).

All control leads to the v.f.o. unit pass through a 5-prong male plug mounted on the rear lip of the chassis. Each lead is bypassed with a .01 ceramic capacitor (Centralab DD-1032) as it passes through the plug. The SO-239 coaxial output connector is also mounted on the rear lip of the chassis, directly behind the 6AG7 output stage.

Wiring the V.F.O. The v.f.o. components on the dural plate should be wired first. The first step is to wind coil, L_1. A Millen low-loss mica filled bakelite form (45000) measuring 1½" long by 1" diameter is used for the form of L_1, and is drilled according to figure 14. Two 4-40 machine screws are passed through the holes to act as anchor points for the coil winding. A length of enameled wire is cut, and one end fastened to a bench vise or other solid object. The other end is soldered to one of the 4-40 machine screws projecting through the coil form. Tension is put on the wire, and the coil is then wound. If care is taken, the turns spacing may be approximated in the winding process. When the winding is completed, the wire should be cut, the end cleaned and soldered to the remaining 4-40



L1 – 15 TURNS # 22 E., 1" DIA., 1" LONG, TAPPED 5 TURNS FROM BOTTOM END.

L2 – 52 TURNS # 22 E., ½" DIA., 1" LONG. NATIONAL XR-72 FORM WITH SLUG REMOVED.

Figure 14
COIL TABLE

machine screw. A knifeblade may then be used to even-up the spacing of the turns of the coil until the winding is spaced properly.

The turn having the cathode tap should then be cleaned with the knife and a short length of no. 22 wire soldered to the coil winding at this place. When these steps are completed, the coil should be mounted to the dural plate by means of a 6-32 screw through the base.

The tuned circuit of the v.f.o. is wired with no. 16 solid tinned wire. A 1/2" ceramic post is placed adjacent to L_1 and the cathode tap of the coil is attached to a soldering lug screwed to the top of the post. A no. 16 lead goes from the post to the cathode pin of the 6BA6 oscillator tube socket. All grounds in the oscillator circuit are brought to a single ground lug securely fastened to the dural plate. A separate ground lead is run from this lug to the rotor of the main tuning capacitor, C_1. This prevents an intermittent ground path through the capacitor mounting assembly from affecting the stability of the oscillator.

RFC_1 is mounted on a two terminal phenolic strip below the second 6BA6 tube. The voltage lead from this choke passes through a 1/2" rubber grommet mounted on the aluminum sub-chassis to switch S_1. The filament lead for the 6BA6 tubes also passes through this grommet. The dural plate should now be mounted on the chassis and the small components beneath the chassis are now wired.

V.F.O. Power Supply The schematic of the v.f.o. power supply is shown in figure 15. The power supply is constructed as a separate item, since it is desired to keep the heat generated by the supply and the minute vibration of the transformers and chokes away from the v.f.o. circuits. The power supply construction is straightforward, with all leads bypassed to prevent r-f pickup

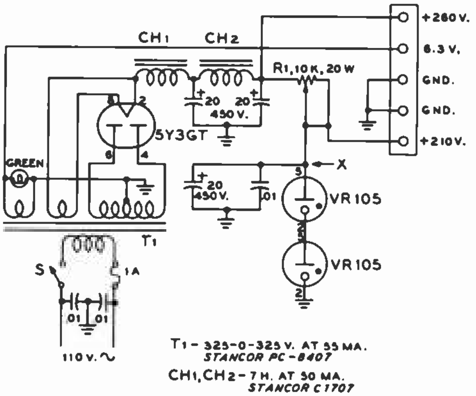


Figure 15

V.F.O. POWER SUPPLY

from the transmitter. The supply is built upon a 7½"x 5½" miniature amplifier foundation (Bud CA-1754). Resistor R_1 is adjusted so that a current of 15 milliamperes passes through the voltage regulator tubes. The regulator circuit is broken between point "X" (figure 15) and pin 5 of the VR105 and a d-c milliammeter inserted to measure the regulator tube current while the tap on R_1 is adjusted.

V.F.O. Alignment and Adjustment After the v.f.o. wiring has been checked, oscillator padding capacitor C_2 should be set to about 3/4 capacity and the two 6BA6 tubes plugged in their sockets. Switch S_1 should be set to "V.F.O." position. Filament and plate power should be applied to the unit, and the output of the v.f.o. should be monitored in a nearby BC-221 frequency meter or calibrated receiver. By varying the capacity of C_2 and possibly moving the turns of L_1 slightly, the main tuning capacitor, C_1, should cover the range of 1750 kc. to 2000 kc. If it is desired to have more bandspread on the 20, 15 and 10 meter bands, C_1 may be reduced to 100 $\mu\mu$fd., although full coverage on the 80 meter band will be lost.

Once the calibration of the oscillator has been set, the turns of L_1 may be permanently fixed in place by means of four vertical strips of colorless nail polish applied to the coil. Use the minimum of polish possible. The 6AG7 tube should be placed in its socket, and a dummy load made up of two parallel 6.3 volt 150-ma. pilot lamps (brown bead) is connected to the coaxial output plug. The setting of C_3 is adjusted to resonate the output circuit of the v.f.o. unit to 80 meters. The lamp load should glow brightly when C_3 is resonated.

The 80 meter crystal is next plugged in its holder, and S_1 thrown to the "crystal" position. C_3 should be readjusted for stable oscillation, and the oscillator padding capacitor adjusted for the desired frequency of the crystal oscillator.

As a last step, a variable voltage transformer should be inserted between the v.f.o. power supply and the power line to make sure the voltage regulator tubes are holding the v.f.o. plate voltage to a constant 210 volts.

Temperature Stabilization of the V.F.O. When completed, the v.f.o. should be placed in the operating position and run for a period of several hours. During this time, the frequency of the v.f.o. should be checked for long-term drift. Under normal conditions, the v.f.o. should have a very slow positive drift (lower in frequency) of less than 200 cycles on 80 meters over four hours. If the drift is greater than this, it may be caused by temperature changes in the room. To eliminate

Figure 16

THE 220-MC. TRANSCEIVER

A one-quarter wave vertical radiator is mounted in the antenna receptacle atop the transceiver case

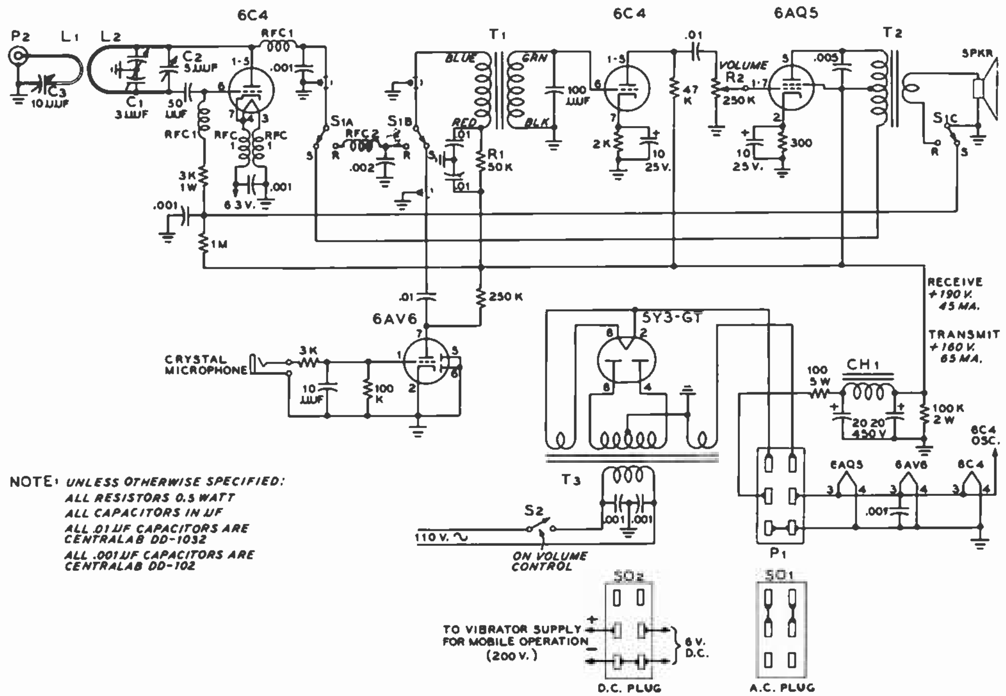


Figure 17
SCHEMATIC OF 220-MC. TRANSCEIVER

C_1—3 μμfd. butterfly Johnson 3MB11
C_2—5 μμfd. Centralab 822EZ
C_3—10 μμfd. Centralab 822BZ
RFC_1—1.8 μh. Ohmite Z-144 or J.W. Miller 4604
RFC_2—50 mh. J.W. Miller 958
S_1—3P3 position Centralab 2506 ceramic switch
T_1—interstage trans. Stancor A-53
T_2—universal output Stancor A-3822
T_3—240-0-240 v. at 55 ma. Stancor PM-8402
CH_1—7 hy. at 50 ma. Stancor C-1707
Speaker—3" Utah SP3A
L_1—Same as L_2 with leads long enough to reach C_3, P_2
L_2—3½" length of no. 12 enam., forming circle 1⅛" i.d. ½" opening between leads
P_1—Cinch S-306AB
SO_1, SO_2—Cinch S-306FHT

the last bit of drift, a small negative temperature coefficient variable ceramic capacitor of 20 μμfd. may be connected across C_2. The capacity of this padder should be slowly increased as the capacity of C_2 is decreased a like amount until a minimum warmup drift of the v.f.o. is observed.

To prevent frequency changes during operation, the lid of the v.f.o. cabinet should be fastened shut by means of two sheet metal screws run through the front corners of the lid into the cabinet.

25-3 A 220-Mc. Transceiver

The Federal Communications Commission allows amateurs to use modulated oscillators on frequencies above 220 Mc. The simple transceiver (so popular on "five meters" during the late "thirties") employing a single tube as both modulated oscillator and super-regenerative detector may be used on the 220-Mc. band to make a simple and inexpensive station for the Novice or Technician.

Shown in figures 16, 18 and 19 is such a transceiver. It covers the 220-Mc. to 225-Mc. range and uses only 5 tubes. The unit is a complete 1¼ meter phone station, with a carrier power of just over 1 watt.

Circuit Description The Transceiver employs a single 6C4 miniature triode which functions either as a modulated oscillator for transmission, or as a super-regenerative detector for reception of modulated

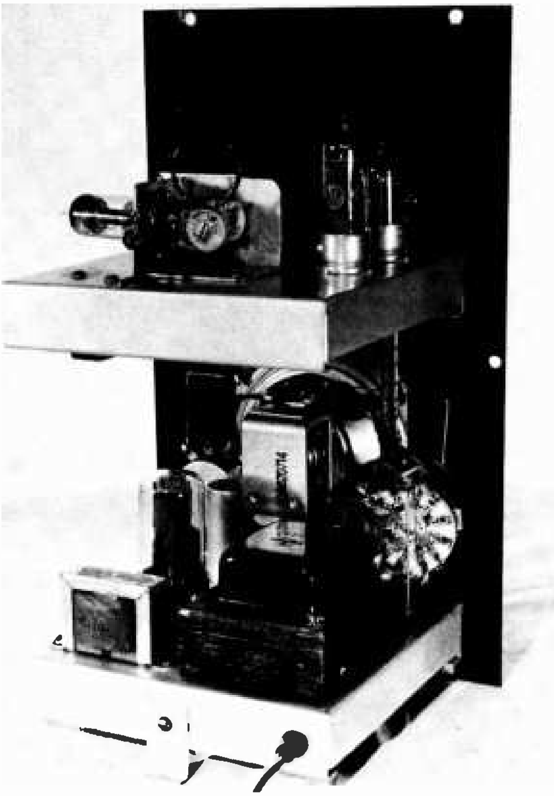


Figure 18
REAR VIEW
OF TRANSCEIVER
The 6C4 oscillator-detector components are mounted on a small bracket on the top deck

waves (figure 17). During periods of transmission, the "send-receive" switch S_{1A} connects the plate circuit of the 6C4 to the output of the 6AQ5 audio amplifier stage. Segment C of S_1 decreases the grid bias on the 6C4 allowing it to oscillate. Segment B of S_1 connects the output of the 6AV6 microphone amplifier stage to the input circuit of the audio amplifier. Enough gain is available in the audio system for the use of a crystal microphone.

During periods of reception, S_{1A} connects the plate circuit of the 6C4 detector to the input of the audio amplifier, and S_{1C} completes the speaker circuit by grounding one end of T_2. At the same time, S_{1C} unblocks the bias system of the 6C4. The 1 megohm grid resistor returns the grid circuit to B-plus, turning the 6C4 stage into a super-regenerative detector. A filter network consisting of RFC_2 and a .002 μfd. capacitor prevents the quench frequency of the detector from blocking the audio amplifier during reception.

The detector-oscillator input circuit of the transceiver consists of a high-C tank composed of a single turn inductance in parallel with a miniature 3 $\mu\mu$fd. split-stator "butterfly" type tuning capacitor (C_1) and a 5 $\mu\mu$fd. NPO ceramic padding capacitor. An insulated shaft connects the butterfly capacitor rotor to the tuning dial.

The 6AQ5 tube acts as a modulator when transmitting and as an audio amplifier when receiving. The output in the latter condition is sufficient to drive a small PM speaker to loud volume.

Transceiver Construction The Transceiver is built in a metal carrying case measuring 7" wide by 12" high by 6" deep (Bud CC-1096). Two chassis decks 5¾" x 5½" (Bud CB-525) support the major components of the unit, as shown in figure 18. The top deck of the transceiver holds the 6C4 oscillator-detector assembly, T_1 and T_2 and the 6C4 and 6AQ5 tubes. The lower deck holds T_3, CH_1, the 5Y3-GT and 6AV6 tubes and the power supply components. Volume control R_2 and switch S_1 are mounted on the front panel on either side of the 3-inch PM speaker.

A small plate of soft aluminum is bent into a double angle bracket (figure 19) to support the 6C4 oscillator tube socket. The bracket measures about 1¾" on a side. Capacitor C_1 is mounted close enough to the 6C4 socket so that the interconnecting leads consist only of the socket prongs. Coil L_2 is connected between the stator terminals of C_1, and C_2 connects to the same terminals, directly behind L_2. The four r-f chokes in the 6C4 circuit are brought away at right angles to L_2. A 1/2" rubber grommet is placed in a chassis hole directly behind the r-f chokes, and the power leads from these chokes pass through this hole. All the leads in the 6C4 circuit should be kept as short as possible.

An SO-239 coaxial receptacle (P_2) is mounted in the top of the metal carrying case, with C_3 next to it. Antenna pickup loop, L_1, has mounting leads that are long enough to permit L_1 to lie parallel to L_2, with L_2 positioned behind L_1 about 1/4" away. The coupling between these two loops may be adjusted after the transceiver has been placed in the cabinet.

Transformer T_1 is mounted above deck between the 6C4 oscillator-detector tube and the front panel, and T_2 is mounted below deck, directly under the 6C4 oscillator-detector tube. Placement of leads below the chassis is not critical, although all small components should be mounted as close to the tube sockets of the 6C4 and 6AQ5 as is practical.

RFC_2 and the .002 μfd. bypass capacitor are mounted directly on the back of switch S_1, and the remaining circuit components are mounted beneath the lower chassis deck. Plug P_1 is mounted on one side of the lower deck. To assure good bonding between the two decks, a wire jumper connects the two decks together, and also grounds one end of R_2. Leads to the rotor arm of S_{1A} and two points of S_{1B} are run in shielded wire, with the shield grounded at both ends of the leads.

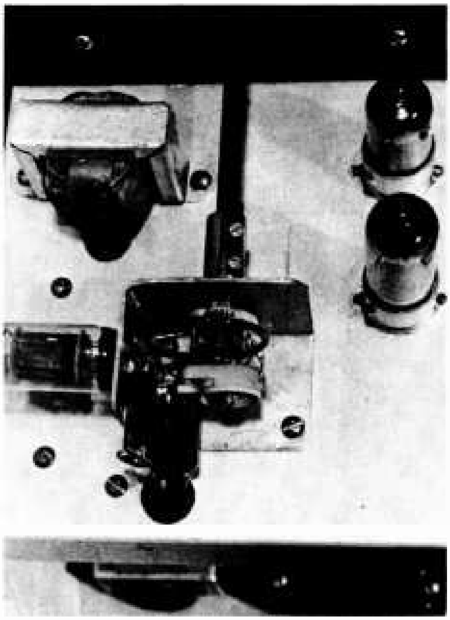


Figure 19
CLOSEUP OF OSCILLATOR-DETECTOR
Coil L_2 and padding capacitor C_2 are mounted on the back of C_1. To the right are the 6C4 audio tube (near panel) and the 6AQ5 output tube.

Transceiver Alignment After checking the wiring of the transceiver, all tubes may be placed in their sockets. A 6-volt pilot lamp (brown bead) should be loosely coupled to L_2 with a single turn pickup link. S_1 should be set to "receive." After a short warm-up period, a loud super-regenerative "rush" should be heard from the loudspeaker. If a short antenna is brought near L_2, and C_1 and C_2 set to maximum capacity any nearby television stations on channels 12 or 13 should be heard. With C_2 set to about 30 per cent capacity (see figure 18) the transceiver should be in the immediate vicinity of the 220-Mc. band. When S_1 is thrown to the "transmit" position, the pilot lamp serving as the dummy load should light, and should increase in brilliance under modulation. The plate voltage of the transceiver should measure 190 volts under "receive" conditions and 160 volts under "transmit" conditions. Plate voltage may be adjusted by changing the value of the 10 watt resistor connected between P_1 and CH_1.

The transceiver should now be placed in its case. The lamp load should be connected to the SO-239 coaxial receptacle on the top of the transceiver case, and the coupling between L_1 and L_2 and the setting of C_3 adjusted for maximum output from the transmitter, while still allowing smooth super-regeneration of the receiver. A PL-258 coaxial plug may be fitted with an 11 inch length of no. 12 wire to act as a 1/4 wave vertical whip, using the case of the transceiver as a ground plane. Contacts of up to 40 miles have been made with this unit using such a simple ground plane antenna. The setting of C_3 and the coupling between L_1 and L_2 should of course be readjusted for any change in the antenna system of the transceiver.

As a final step, resistor R_1 should be increased after 220-Mc. signals have been re-

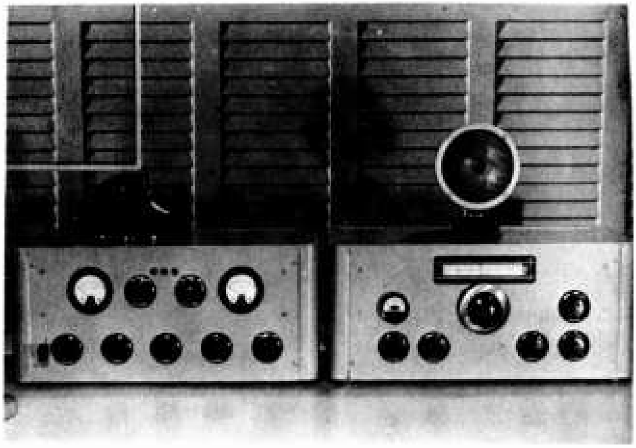


Figure 20
A COMPLETE 20-WATT 2-METER STATION

ceived. As this resistor is increased in value, the receiver radiation is reduced, resulting in less interference to nearby stations. Values of R_1 up to 0.25 megohm may be used, depending upon the degree of coupling between L_1 and L_2 and the type of antenna system in use.

It must be remembered that a super-regenerative receiver, under the best of conditions, radiates a portion of the energy of oscillation. Receivers of this type, in general, are not recommended in congested areas where the 220-Mc. population may be quite large since the QRM caused by such receiver circuits may be excessive.

This transceiver may be used for mobile operation by replacing SO_1 with SO_2 and employing a 200 volt 60 milliampere vibrator supply to deliver high voltage for the transceiver.

25-4 A 20 Watt 2-Meter Transmitter

This 20-watt 2 meter phone transmitter is designed as a companion item for the 2 meter receiver described in Chapter 24 of this Handbook. The two items form a complete 2 meter station, and are shown together in figure 20.

The transmitter uses two type 6360 miniature double-beam tetrodes, one as a push-pull final amplifier stage, and the other as a frequency tripler. By changing the coils in the transmitter, operation is possible in the 220-Mc. amateur band.

Circuit Description General layout of the transmitter may be seen in figures 21, 23 and 24. The complete schematic is given in figure 22. The transmitter was designed with continuous operation in mind. All tubes and components are operated at or below CCS ratings. The comparative lack of crowding of components results in low operating temperatures of the transmitter, and makes for easy servicing and adjustment should trouble develop.

Standard 8-Mc. crystals are used in an overtone crystal oscillator operating at 24-Mc. The tuning range of the 24-Mc. tank circuit, L_1-C_1, is limited by a 15 $\mu\mu$fd. padding capacitor which prevents parasitic oscillations from taking place when the tuning capacitor C_1 is at minimum capacity. Such oscillation is a characteristic of these overtone circuits when a large amount of feed-back is used for standard crystals. A 12AV7 double triode tube is used as the 24-Mc. overtone oscillator and as a doubler to 48-Mc. The plate circuit of the 12AV7 is split to provide balanced output for the 6360 stage. Padding capacitors are placed across the 48-Mc. tank circuit to provide a vernier tuning effect for this stage. These capacitors should be close tolerance units to avoid unbalancing the circuit. Feeding the d.c. plate voltage to this circuit from the end opposite the tube provides enough stray capacity to ground to balance the output capacity of the 12AV7 tube. For 220-Mc. operation, the padding capacitors are disconnected and a new coil tunes the stage to 72-Mc.

A 12AV7 tripler will furnish sufficient drive for the final stage, but the tube must be run at full rating with maximum plate dissipation. It was felt that operating the tube under such conditions would greatly shorten the tube life, so a 6360 was used in place of a 12AV7 tripler. The 6360 tripler furnishes over 6 milliamperes of grid current to the final stage, whereas only 3.5 milliamperes is required. Excitation to the final stage is controlled by R_1. For 220-Mc. operation, the 6360 stage triples from 72 Mc. to the 1¼ meter band, driving the grid circuit of the 6360 amplifier to more than 4 milliamperes.

The output coil of the 6360 tripler stage is inductively coupled to the self-resonant grid coil, L_5, of the amplifier stage. A double tuned circuit is necessary at this point to attenuate other harmonics of the 24-Mc. oscillator which may be present in the output circuit of the 6360 tripler stage.

Cathode bias is employed on both sections of the 12AV7 tube, and also on the 6360 tripler tube to protect the tubes in case of excitation failure. The 6360 final amplifier employs only grid-leak bias, but the tube is protected by a 6AQ5 clamper tube in the screen circuit.

The very low output capacity of the 6360 tube permits a good L/C ratio to be used in the amplifier plate tank circuit which affords excellent modulation linearity. The 6360 amplifier stage is both plate and screen modulated to provide maximum modulation capability of this stage. The antenna circuit is coupled to the plate tank of the amplifier by means of a series tuned link coil, L_7. Provision is made for coaxial feed to the antenna system, using either 52 or 72 ohm coaxial line.

The modulator section of the transmitter is designed to work from a crystal microphone. Two stages of high-gain R-C amplification use a 12AX7 to drive push-pull 6AQ5 pentode tubes, operating in class AB_2. The degree of modulation is controlled by potentiometer R_2 in the grid circuit of the second half of the 12AX7.

Separate grid and plate meters are used in the transmitter. A 0-5 d-c milliammeter measures the grid current of the 12AV7 doubler, the grid current of the 6360 tripler, or the grid current of the 6360 power amplifier. Switch S_2 selects the desired circuit. 100-ohm resistors are used as meter shunts in each circuit so that the meter may be switched from circuit to circuit without actually breaking any one of the circuits. The 100-ohm shunting resistor has little observable effect on the meter calibration, since the internal resistance of the meter is only 8.5 ohms. A 0-100 d-c milliammeter measures the plate current of each section of the 12AV7, the plate current of the 6360 tripler, the plate current of the 6360 power amplifier, or the plate current of the 6AQ5 modulator stage. Switch S_3 selects the desired circuit for this meter. 50-ohm shunting resistors are used in each plate lead and the meter is placed across these resistors by switch S_3.

A heavy-duty power supply using a 5U4-GA supplies 300 volts at the maximum transmitter current drain of 180 milliamperes. A choke input filter provides good regulation, reduces transformer heating and extends rectifier tube life.

A three position switch (S_1) is used as the "tune-standby-transmit" switch. Section A of this switch switches the antenna circuit from the transmitter to a coaxial jack mounted on the rear apron of the transmitter from which a coaxial line runs to the receiver input terminal. Section B of S_1 disables the high voltage supply on the "standby" and "tune" positions, and section C position 1 applies reduced voltage to the exciter stages for tune-up purposes. By this sequence of switching the transmitter is not put on the air during tune-up procedure, nor is there danger of modulation transformer damage.

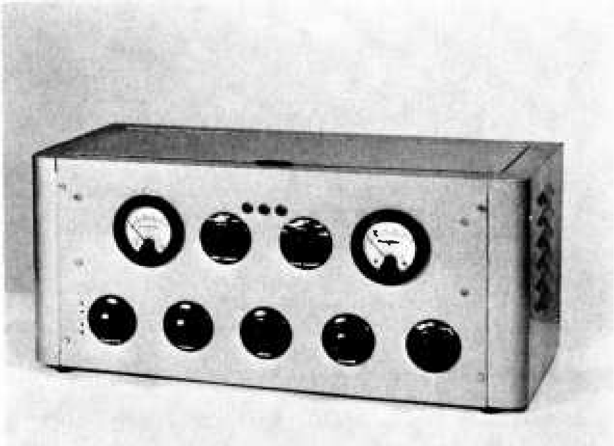


Figure 21
THE 2-METER TRANSMITTER
This transmitter has an input of 20 watts fully modulated and operates in either the 144-Mc. or 220-Mc. amateur band

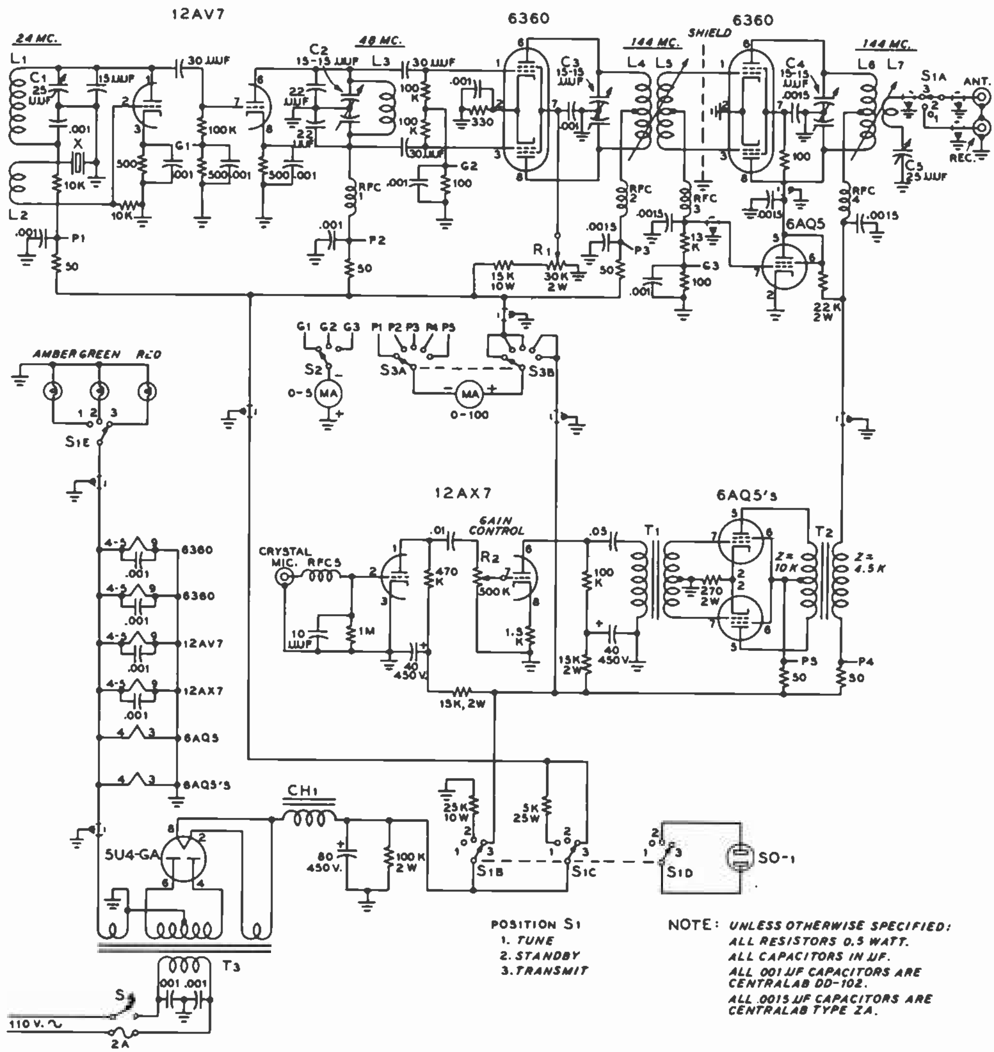


Figure 22

SCHEMATIC OF 20-WATT 2-METER TRANSMITTER

C_1—25 µµfd. Bud LC-1642
C_2, C_3, C_4—15-15 µµfd. Hammarlund HFD-15X
C_5—25 µµfd. Bud LC 2077
RFC_1—7 µh. Ohmite Z-50
RFC_2, RFC_3, RFC_4, RFC_5—1.8 µh. Ohmite Z-144
T_1—10 K primary to 90 K grid-to-grid Triad A-31X
T_2—10 K primary to Class C load, 25 watts Stancor A-3845
T_3—400-0-400 v. at 200 ma. Thordarson TS-24R07
CH_1—10 hy., 250 ma. Stancor C-1402
S_1—6p.3t. Centralab 2517 ceramic
S_2—1p.3t. Centralab 1401
S_3—2p.5t. Centralab 1405

SO_1—2 prong Jones receptacle
L_1, L_2—17 t. B&W Miniductor 3003 ½" dia., 16 t. per inch no. 20 wire. Remove one center t. to make two coils of 11 t. and 5 t., spaced one t. apart.
L_3—10 t. no. 14, ½" dia. spaced between terminals of C_2 (approx. 1¼")
L_4—4 t. no. 14, ½" dia. spaced between terminals of C_3 (approx. 1¼")
L_5—3 t. no. 18 at center of L_4, ⅜" dia. ¼" long
L_6—same as L_4
L_7—2 t. no. 14, ½" dia. at center of L_6

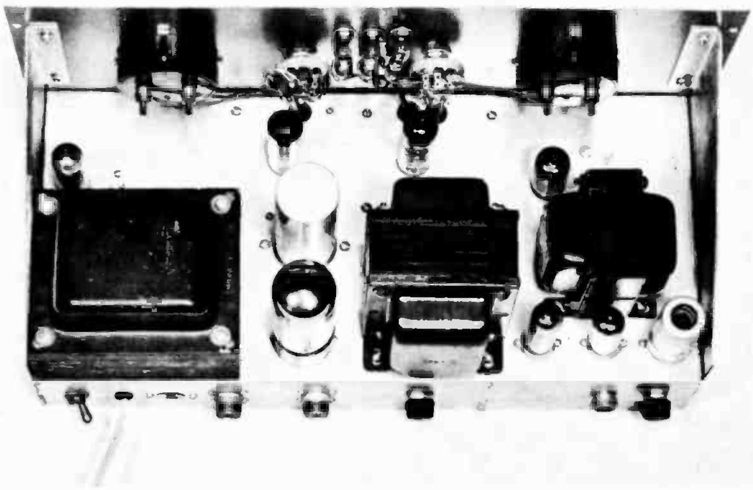
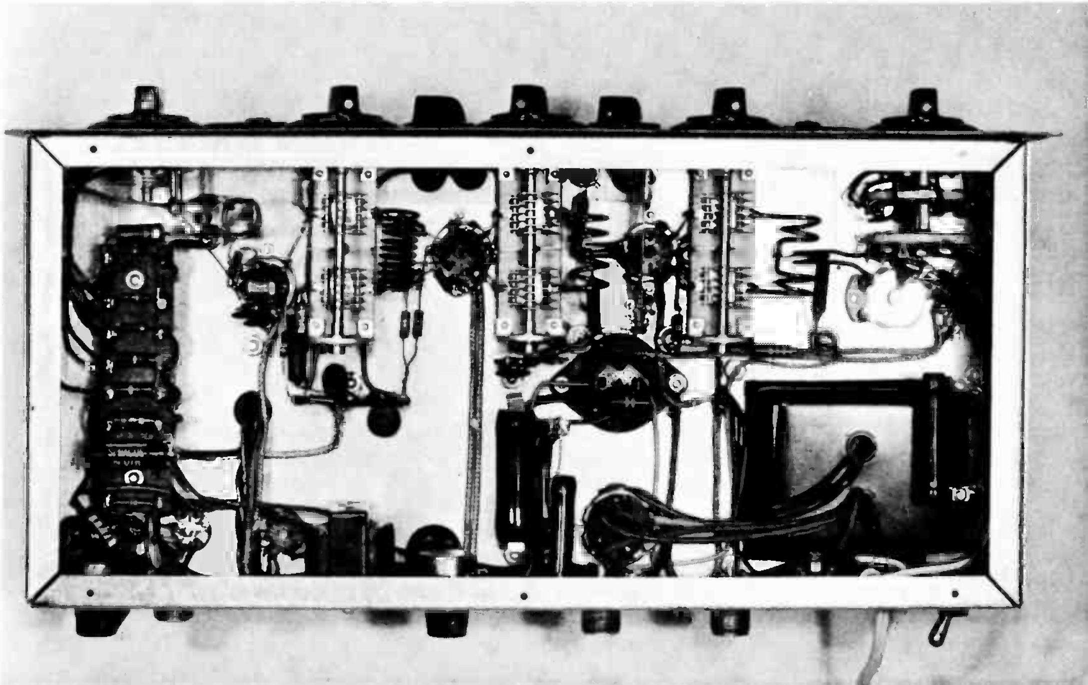


Figure 23
TOP VIEW OF 2-METER TRANSMITTER

Figure 24
BOTTOM VIEW OF 2-METER TRANSMITTER
The r-f circuits are at the top of the chassis next to the front panel. The multiplier stages are at the left and the 6360 amplifier stage at the right. Control switch S_1 is at the upper right corner. Antenna leads to this switch are run in lengths of RG-59/U coaxial line.



Transmitter Layout The transmitter is built upon a 7" x 15" x 2½" aluminum chassis (Bud AC-411) and fits inside a steel cabinet measuring 8" x 18½" x 8¼" (Bud C-1790). Two Bud MB-458 chassis mounting brackets hold the chassis to the 16" panel of the cabinet. The placement of major components above the chassis may be seen in figure 23. In the left corner of the chassis is the power transformer, T_3. In front of T_3 is the 6AQ5 clamper tube and the antenna resonating capacitor, C_5. To the right of T_3 are situated the 5U4-GA and the 80 μfd. upright-type filter capacitor. Next to the rectifier tube is choke CH_1. To the right of the choke are the two 6AQ5 modulator tubes and the 12AX7 speech amplifier tube, which is shielded. In front of these three tubes is the modulation transformer, T_2. The 12AV7 tube is in front of T_2, and the 6360 tripler tube is in front of CH_1. The 6360 power amplifier is in front of the 80 μfd. filter capacitor.

The placement of the panel controls may be seen in figure 21. From left to right along the bottom of the panel are the crystal socket, oscillator, doubler, tripler and amplifier tuning and the send-receive switch, S_1. Between the two meters are the grid current switch S_2 on the left, and the plate current selector switch, S_3 on the right. The three indicator lamps are placed between the switches and slightly above them.

On the back apron of the chassis (figure 23) are the 110-volt line switch, the auxiliary socket, SO_1, the two coaxial receptacles, the excitation control, R_1, and finally the microphone jack and audio gain control, R_2.

Transmitter Wiring The filament and power wiring is done first. All filament and power leads leaving the r-f stages are in shielded braid, which helps materially in attenuating harmonics and in keeping the r.f. of various frequencies where it belongs. Audio components and various d-c resistors are mounted on a terminal board situated below the chassis parallel to the left edge. Solid no. 18 tinned wire is used for all r-f circuitry. Coils L_1 and L_2 are made from a single piece of B & W Miniductor (#3003) with one turn cut out to make the center connections to the two separate windings. A shield partition is placed across the socket of the 6360 power amplifier stage which measures 2½" high by 3" wide, plus a 1/2" fold on each end. Pins 1, 2 and 3 are on one side of the shield, which passes between pins 3 and 4. A 1/2" foot should be made on each end of the shield to bolt it to the chassis with 4-40 machine screws.

Coils L_3, L_4 and L_6 are mounted directly to their respective tuning capacitors by their leads, which should be cut as short as possible. Coil L_5 is mounted directly to pins 1 and 3 of the 6360 amplifier tube socket. The center turns of L_4 are spread apart slightly to permit L_5 to slip partly inside of L_4. All bypass capacitors associated with the r-f circuitry should be positioned with as short leads as is possible. The button-mica capacitor used to bypass the screen grid of the 6360 amplifier stage should be mounted directly beside pin 7 of the tube socket, and the lug of the capacitor connected directly to pin 7 of the socket. The connections between L_7, S_{1A} and the two coaxial plugs are made with short lengths of RG-59/U coaxial line. All wiring in the r-f circuits should be done in accordance with the usual v.h.f. techniques.

METER READINGS		
STAGE	GRID CURRENT	PLATE CURRENT
OSCILLATOR	—	10 MA.
DOUBLER	0.5 MA.	10 MA.
TRIPLER	1.0 MA.	18 MA.
AMPLIFIER	3.5 MA. (MAX.)	70 MA.
MODULATOR	—	70 MA.
PLATE SUPPLY VOLTAGE = 290-300 VOLTS		
220 MC. OPERATION		
1. *REMOVE 22 μμF PADDERS ON 12AV7 DOUBLER PLATE CIRCUIT. RETUNE STAGE TO 72 MC.*		
2. *REPLACE L4 AND L6 WITH TWO TURN COILS OF SAME DIAMETER. SPACE TURNS TO RESONATE CIRCUITS WITH CAPACITORS HALF OPEN.*		

Figure 25

Transmitter Alignment The preliminary alignment of the tuned circuits of the transmitter is best done with the aid of a grid-dip oscillator. The frequencies to which the circuits should be set are shown in figure 22. Switch S_1 should be set to "tune" and capacitors C_1, C_2 and C_3 tuned for maximum grid current in each of the following stages. Coupling between L_4 and L_5 is adjusted for maximum grid drive to the 6360 grid circuit as read on S_2, position 3. The grid coil, L_5 is self-resonant at about 160 Mc. and need not be changed when the transmitter is moved to the 220-Mc. band. Coupling between L_6 and L_7 and the tuning of C_5 determine the degree of loading of the amplifier stage. One setting of C_5 will usually hold across the entire 144-Mc. band unless there is an unusually high value of SWR on the transmission line to the antenna. Current readings for the "transmit" position of S_1 are shown in figure 25. The transmitter input under these conditions is 21 watts, with a carrier power of approximately 13 watts, 100 per cent modulated.

When the final tank capacitor is tuned

Figure 26
75-WATT 2-METER TRANSMITTER

through resonance (high voltage off) there is no change in grid current in the amplifier stage, and the stage exhibits no instability, loaded or unloaded. The plate leads of the 6360 tube are crisscrossed within the tube to make the tube self-neutralizing in the 144-Mc. range. Without the inter-stage shield, a small degree of neutralization is necessary, due to the fact that there is a small degree of coupling between L_5 and L_6 when the shield partition is missing.

25-5 A 75 Watt 2-Meter Transmitter

The type 5894 (formerly Amperex AX-9903) tube is a twin five electrode tube designed for use as a radio-frequency power amplifier in the v-h-f region. Maximum CCS power input of 75 watts plate modulated may be run at frequencies up to 250 Mc. and the tube may be operated at reduced ratings up to 500 Mc. The tube has built-in cross neutralizing capacitors, which insure neutralization in the 100-Mc. to 250-Mc. region. The tube makes an ideal amplifier for a medium powered 2-meter telephone transmitter, delivering high output with a minimum of driving power.

The transmitter described in this section employs a single 5894 tube as a push-pull amplifier in the 144-Mc. band, running at a plate input of 75 watts.

Circuit Description The exciter stages of this transmitter are quite similar to the exciter stages of the 20 watt 2-meter transmitter described in section 25-4 of this chapter. A 12AT7 serves as a 24-Mc. overtone oscillator using 8-Mc. crystals. The second section of the 12AT7 acts as a frequency doubler to 48 Mc. The plate circuit of the 48-Mc. doubler stage is split to provide balanced excitation to the 6360 push-pull tripler stage. The 144-Mc. output of the tripler stage is link coupled to the grid circuit of the 5894 push-pull amplifier stage. The 5894 is both plate and screen modulated by a pair of 6L6-G tubes, working as class AB_2 modulators. The screen circuit of the 5894 is self-modulated by the action of the choke CH_1 (figure 27) in the screen supply lead. Three stages of resistance coupled amplification provide sufficient audio gain for proper operation of a crystal microphone with this transmitter.

Three power supplies are used to provide bias voltage for the r-f and modulator stages, 300 volts for the speech amplifier and doubler stages, and 500 volts for the power amplifier and modulator stages. Two meters are incorporated in the transmitter. A 0-300 d-c milliammeter is used to indicate modulator plate current, and a 0-3 d-c milliammeter with suitable shunts is used to read various grid and plate currents in the r-f section of the transmitter.

The transmitter is designed to operate into either a 52 or 72 ohm unbalanced feedline.

Transmitter Construction The transmitter is divided into two basic units. The r-f stages and bias supply are constructed upon a 7" x 11" x 2" aluminum chassis (Bud AC-407), mounted within a steel cabinet measur-

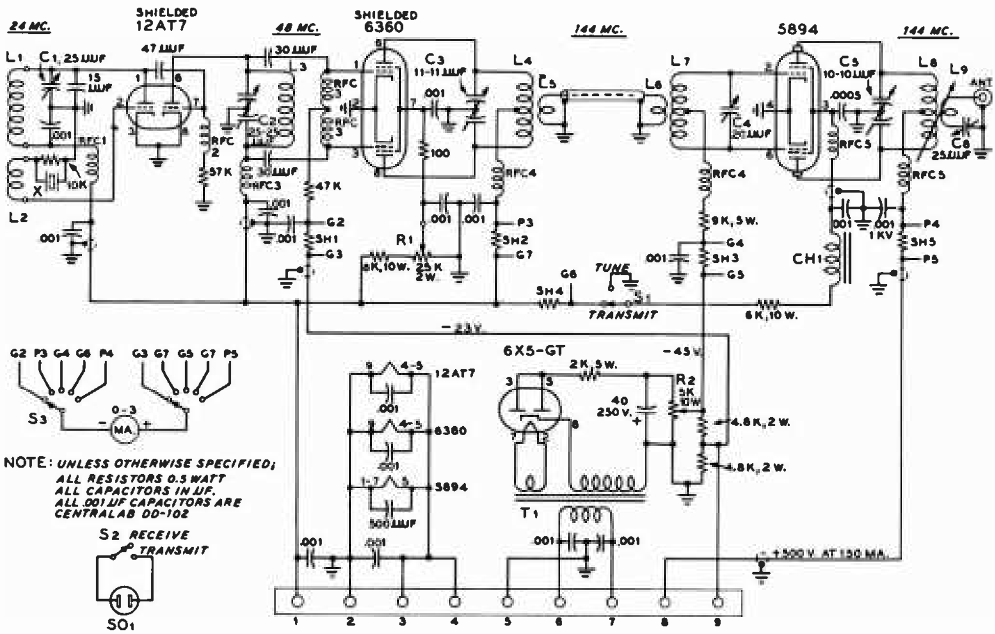


Figure 27

SCHEMATIC OF 75-WATT 2-METER TRANSMITTER

C_1—25 µµfd. Bud LC-1642
C_2—25-25 µµfd. butterfly Johnson 25LB15
C_3—10-10 µµfd. butterfly Johnson 10LB15
C_4—20 µµfd. ceramic Centralab 822AZ
C_5—same as C_3
C_6—same as C_1
RFC_1,RFC_2—2.5 mh. National R-100
RFC_3—7 µh. Ohmite Z-50
RFC_4,RFC_5—1.8 µh. Ohmite Z-144
T_1—125 v. at 50 ma. Stancor PA-8421
CH_1—4.5 hy. at 50 ma. Stancor C-1706
S_1,S_2—s.p.d.t. toggle switch
S_3—2p.5t. Centralab 1405
SH_1—100 ohms, 1 watt (meter reads 0-3 ma.)
SH_2—0.3 ohms, 1 watt (meter reads 0-100 ma.)
SH_3—9 ohms, 1 watt (meter reads 0-6 ma.)
SH_4—0.9 ohms, 1 watt (meter reads 0-30 ma.)
SH_5—approx. .09 ohms (meter reads 0-300 ma.)
Meter—Triplett 227-T. Internal resistance 9 ohms. Shunt resistances given above are approximate.
L_1,L_2—17 t. B&W Miniductor 3003, 1/2" dia. 16 t. per inch no. 20 wire. Remove one center t. to make two coils of 11 t. and 5 t. spaced one t. apart
L_3—9 t. B&W Miniductor 3003, 1/2" dia. 16 t. per inch no. 20 wire. Grid dip to 48 Mc. with C_2 about half meshed
L_4—4 t. no. 14, 1/2" dia. 1/2" long
L_5,L_6—2 t. hookup wire placed in centers of L_4 and L_7
L_7—3 t. no. 14, 3/8" dia. Resonates to 144 Mc. with C_4 at mid-capacity
L_8—4 t., same as L_4
L_9—2 t. no. 14, 1/2" dia. at center of L_8

ing 7" high by 12" long by 8" deep (Bud C-994). The transmitting unit is designed to sit upon the operating desk, next to the station receiver. A nine wire cable connects the transmitting unit to the power supply and modulator unit which sits upon the floor beneath the desk, or which may be put in a drawer of the desk. The latter unit is built upon an amplifier foundation and dust-cover combination, measuring 17" long by 10" wide by 10" high (Bud CA-1753).

By use of this physical arrangement, an absolute minimum of equipment is placed upon the operating table. The front view of the transmitter is shown in figure 26, and the top and bottom views are shown in figures 28 and 29. The oscillator, doubler and tripler tuning capacitors (C_1, C_2 and C_3) are mounted in a line beneath the chassis, along with the crystal socket and the transmit switch, S_2. For panel symmetry, the power amplifier tuning capaci-

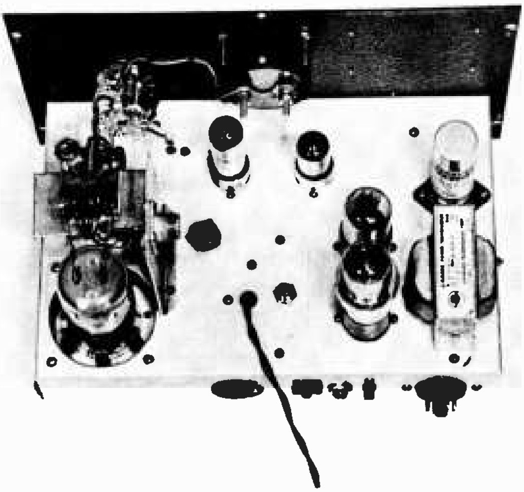


Figure 28

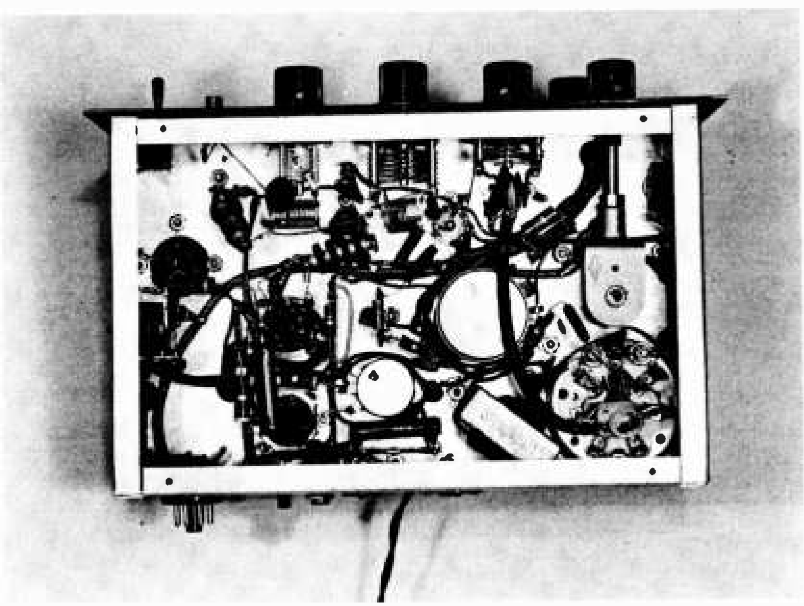
TOP VIEW OF THE 75-WATT 2-METER TRANSMITTER

The 12AT7 and 6360 tube shields have been removed for the photograph. The VR-150 regulator tube is not used. The antenna coaxial plug is mounted on the side of the amplifier plate circuit bracket, to the right of the 5894 tube. Meter shunts are mounted on the back of S_3.

Figure 29

BOTTOM VIEW OF THE 75-WATT 2-METER TRANSMITTER

R-f tuned circuits are at the front-center of the chassis. Inductors L_1, L_2, L_3 and L_4 are mounted directly to the stator supports of the tuning capacitors. Potentiometers R_1 and R_2 are mounted on the chassis deck, as is CH_1.



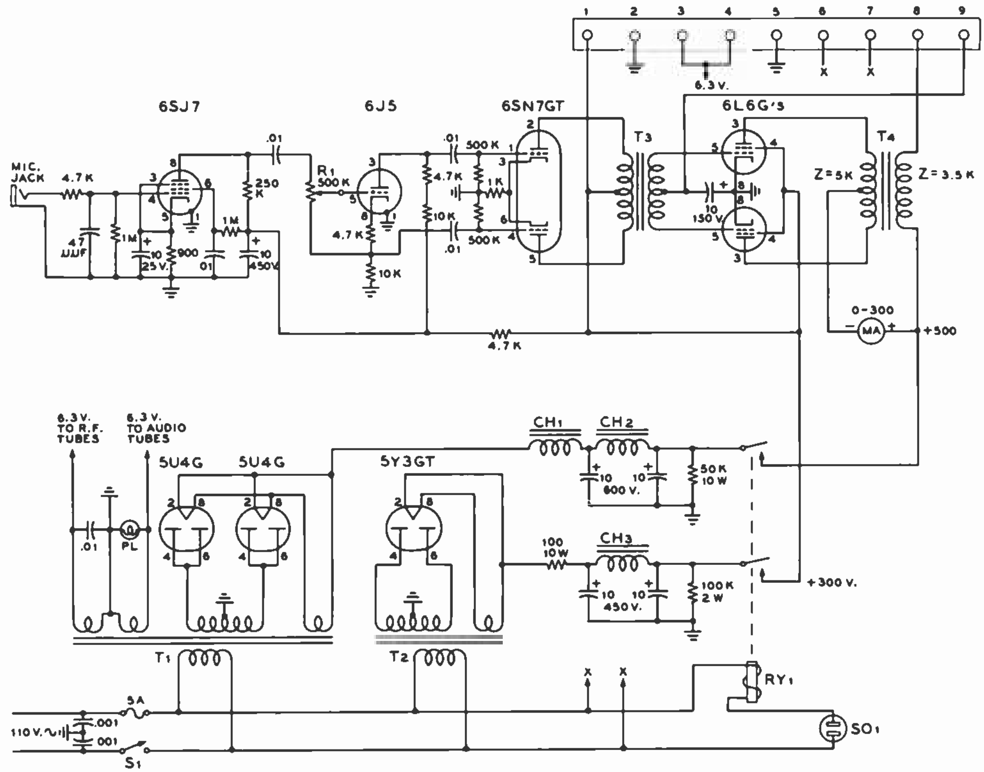


Figure 30

SCHEMATIC OF MODULATOR AND POWER SUPPLY FOR 75-WATT 2-METER TRANSMITTER

T_1—600-0-600 v. at 300 ma. UTC S-42
T_2—325-0-325 v. at 55 ma. Stancor PC-8407
T_3—push-pull interstage Stancor A-4155
T_4—universal modulation trans. UTC S-20

CH_1, CH_2—20 hy. at 300 ma. UTC S-33
CH_3—13 hy. at 65 ma. Stancor C-1708
Ry_1—d.p.s.t. relay with 110 v. a-c coil Advance PC-2C-115 VA

tor, C_5, is mounted vertically next to the plate connections of the 5894 tube. The shaft of C_5 projects downward through the chassis, and is driven from the panel by means of a National right-angle drive unit. The 0-3 d-c milliammeter is centered above the doubler tuning control, C_2, and meter switch S_3 is located to the right of the meter.

Placement of parts on the chassis may be seen in figure 28. The 5894 tube is submounted on the chassis in a Johnson 122-101 7-pin steatite socket. Directly in front of the 5894 tube is the mounting bracket which supports the output tuned circuit (C_5 and L_8), the plate r-f choke (RFC_5) and bypass capacitor, the antenna pickup coil and tuning capacitor (L_9 and C_6) and the coaxial antenna receptacle. The butterfly capacitor is mounted in a horizontal position, with two of the stator terminals positioned adjacent to the plate pins of the 5894 tube. Short, flexible leads run from the plate pins of the 5894 to each stator connection. The plate coil, L_8, is soldered to these stator terminals.

In front of the mounting bracket for the plate assembly, switch S_1 is mounted on the chassis. To the right of the bracket the excitation control, R_1, is mounted on the chassis. Directly behind the panel meter are the 6360 tripler tube (to the left) and the 12AT7 exciter tube (to the right). Care must be taken to position these tubes on the chassis so that the sockets are near the respective tuning circuits, but not so close to the front panel that the glass envelopes of the tubes hit the meter terminals. At the right side of the chassis are the components for the bias power supply. A VR-150 voltage regulator tube is shown in the photograph which is not used in the transmitter circuitry. This tube and the twisted leads running from center chassis in figure 28 were later removed. Bias potentiometer, R_2, is mounted in the chassis deck to the right of the 5894 tube.

Inductances L_1, L_2, L_3 and L_4 are mounted directly to their respective tuning capacitors by their leads (figure 29). Inductor L_7 and capacitor C_4 are mounted directly to pins 2 and 6 of the 5894 tube socket. A short length of RG-59/U coaxial line couples these tuned circuits through links L_5 and L_6. The plate voltage to the final amplifier stage also runs through a length of RG-59/U coaxial line reaching from the power plug to meter shunt SH_3. The screen lead to the 5894 is run in a short length of shielded braid.

Modulation choke CH_1 is mounted between the 5894 tube socket and R_1. Bias supply components occupy the corner of the chassis beneath transformer, T_1.

Wiring of the transmitter is in accord with the usual v-h-f wiring techniques. All r-f leads are of no. 18 solid wire, and their length is kept to a minimum. All bypass capacitors are mounted directly to the respective socket pins and their leads are cut to a length of 1/8" or less. The filament and screen bypass capacitors of the 5894 stage are button mica types (Centralab type ZA) which mount directly to holes in the socket shell of the 5894 tube.

A nine-prong male power plug is mounted on the rear apron of the r-f chassis and each power lead that passes through the plug is bypassed at the plug with a .001 μfd. ceramic capacitor.

In order to provide proper ventilation of the r-f unit, a 2" x 11" slot is cut along the top of the back of the cabinet. The edges of this slot are cleaned with paint remover, and a piece of copper screening is soldered over the opening.

Power Supply-Modulator Construction Construction of the power supply-modulator unit is straightforward. The output leads from this unit terminate in a nine-pin receptacle mounted on the back of the chassis. The transmit switch, S_2, on the r-f unit controls the coil of relay Ry_1 to place the transmitter on the air. The 0-300 d-c milliammeter is mounted on the front of the 3" chassis, as are the microphone jack, the gain control, R_1, the primary switch, S_1 and the pilot lamp assembly.

OPERATING CURRENTS		
STAGE	GRID CURRENT	PLATE CURRENT
OSCILLATOR	—	10 MA.
DOUBLER	1 MA.	10 MA.
TRIPLER	1 MA.	25 MA.
AMPLIFIER	5 MA. SCREEN = 15 MA.	150 MA.
MODULATOR	—	80–150 MA.

Figure 31

The audio stages are mounted at one end of the chassis, and the power supply components at the other end to minimize any hum pickup from transformers T_1 and T_2. Since the bias voltage for the 6L6-G tubes comes from the r-f unit, care must be taken never to run the power supply with the 6L6-G tubes in their sockets unless the r-f unit is attached to the power supply and the bias supply in the r-f unit is working.

Transmitter Testing and Alignment After the wiring of the transmitter has been checked, the 6X5 bias rectifier should be placed in its socket, and 110 volts a.c. applied to pins 6 and 7 of the power plug of the r-f unit. R_2 should be set so that the voltage from arm to ground is −45 volts.

110 volts a.c. should now be applied to the power supply unit, and the two 5U4-G tubes should be plugged in their sockets. About 600 volts should be measured at the output of the high voltage supply, and about 380 volts at the output of the low voltage supply. The 6SJ7, 6J5 and 6SN7-GT tubes should be plugged in their sockets.

The 12AT7, 6360 and 5894 tubes should now be plugged in their sockets in the r-f unit. S_1 should be set to "tune," a crystal of the proper frequency should be placed in the panel holder, and the two units connected together by a length of 9-wire cable. Socket SO_1 should be connected to the corresponding socket in the power supply unit by a length of two wire rubber covered cable. Filament voltage at the 5894 socket should be checked. Each tuned circuit in the transmitter should next be set to the approximate operating frequency with the aid of a grid-dip oscillator. Power is now applied to the transmitter and the exciter circuits tuned for maximum grid current to the 5894 stage. Maximum grid current is controlled by the setting of the excitation potentiometer, R_1.

A suitable dummy load or antenna should be connected to the coaxial antenna receptacle of the transmitter before switch S_1 is set to the "transmit" position. The screen grid current of the 5894 tube is a very sensitive indication of plate circuit loading, and if the amplifier is operated without adequate loading, the screen current of the 5894 will rise to excessive values. The 6000 ohm 10 watt series screen resistor, however, will protect the screen grid of the tube from damage caused by improper loading conditions. The proper current readings for full input to the transmitter are shown in figure 31.

The 6L6-G modulator tubes may now be plugged in their sockets and the audio system tested out.

The amount of antenna loading may be controlled by the coupling between L_8 and L_9 and the setting of C_6. The resonating capacitor, C_6, should always be tuned so that proper loading is had with a minimum of coupling between L_8 and L_9.

25-6 A 120-Watt 2-Meter Transmitter for Use With the Collins and Viking Transmitters

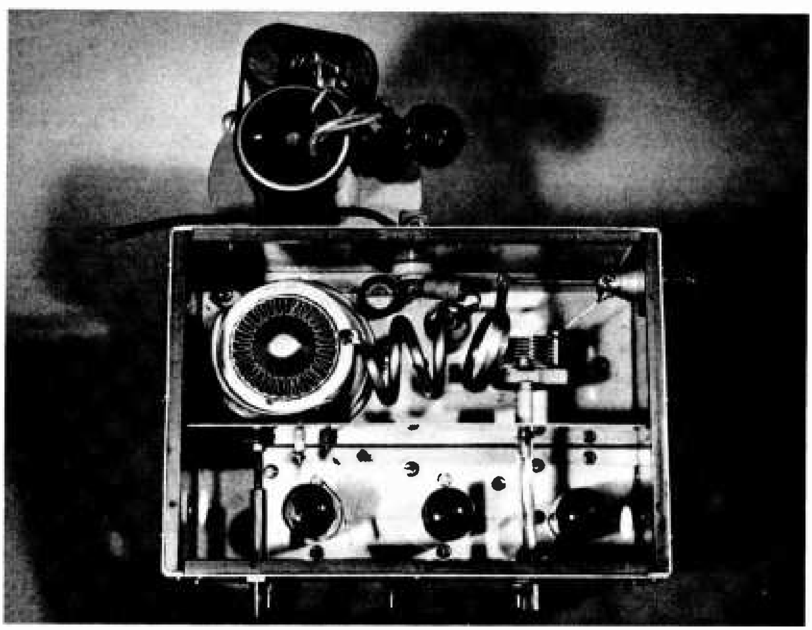
Both the Collins 32V series transmitters and the Johnson Viking transmitters are arranged so that the modulator and power supply may be used in conjunction with an external r-f unit. Many owners of these fine transmitters have often wished for an auxiliary r-f unit that would permit the low frequency transmitter to "operate" on the 144-Mc. amateur band.

The stumbling block to such an arrangement has been the lack of a suitable amplifier tube that would run the required power input at the low voltage, high plate current requirements of these transmitters. Both the Collins 32V and the Viking transmitters operate at a plate potential of about 650 volts, and the final amplifier stage runs at a plate current of approximately 200 milliamperes. The final amplifier of a 2-meter r-f unit for these transmitters would have to run at the same values of plate voltage and current. Under conditions of 100 per cent plate modulation the 6146, the 5894, 829B and such similar tubes could not long stand such excessive input. A satisfactory tube for this power level is the 4X150A radial-beam tetrode. This tube has an external anode and requires 7½ cubic feet of cooling air per minute flowing through its special socket. This requirement is easily met by a miniature 110-

Figure 32

TOP VIEW OF 4X-150A 2-METER TRANSMITTER

The 4X-150A plate tank circuit is at the center, with the tuned pickup link to the right. A small 115-volt blower is mounted on the rear of the chassis to provide circulating air for the 4X-150A. A perforated metal cabinet top allows maximum tube ventilation.



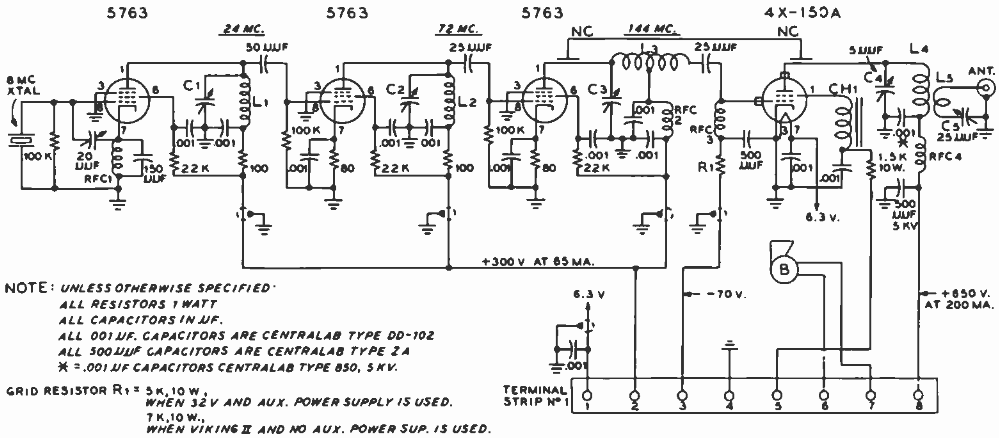


Figure 33
SCHEMATIC OF 120-WATT 2-METER TRANSMITTER

C_1,C_2—20 µµfd. Johnson 20M11
C_3—15 µµfd. Johnson 15M11
C_4—5 µµfd. (see text)
C_5—25 µµfd. Bud LC-1642

RFC_1—2.5 mh. choke National R-100
RFC_2,RFC_3,RFC_4—7 µh. Ohmite Z-50
B—110 v. blower L-R Mfg. Co. no. 2, Torrington, Conn.
CH_1—7 hy. at 50 ma. Stancor C-1707

L_1—8½ t. no. 20, ¾" dia. ½" long B&W Miniductor 3011
L_2—5 t. no. 20, ½" dia. ⅜" long B&W Miniductor 3003
L_3—4½ t. 3/16" copper strap, ¼" dia., 1¼" long, silver plated
L_4—2¼ t. 3/16" copper tubing, 1½" i.d., 2" long, silver plated
L_5—1½ t. 3/16" copper strap, 1½" dia., silver plated

volt radial-type blower. Now that the 4X150A is available for general amateur use, the design of a suitable 2-meter r-f section for the above-mentioned transmitters is greatly simplified.

Circuit Description Top and bottom views of the 4X150A transmitter are shown in figures 32 and 34, and the schematic is given in figure 33. A 5763 harmonic oscillator delivers 24 Mc. output from a 8-Mc. crystal. The oscillator is capacity coupled to a second 5763 working as a tripler to 72 Mc. Cathode bias is employed on the tripler stage to protect the tube in the event the crystal oscillator stage should cease oscillation. A third 5763 doubles frequency from 72 Mc. to 144 Mc.

An unusual and efficient coupling system is used between the 5763 frequency doubler and the 4X150A final amplifier stage. The tuned circuit L_3-C_3 is resonant to 144 Mc., and out of phase voltages are developed at each end of the circuit. The center tap of L_3 is bypassed to ground to obtain this effect. The input capacity of the 4X150A is 15.5 µµfd., and this is equal in value to the output capacity of the 5763 doubler stage (4.5 µµfd.) plus the resonant capacity of C_3. A neutralizing circuit for the 4X150A tube consists of a small variable capacity connected between the plate of the 4X150A and the plate of the 5763. Adjustment of this neutralizing circuit is not at all critical. A special air-system socket (Eimac 4X150A-4010) is employed with the 4X150A tube. The socket is designed to provide adequate air cooling and efficient circuit arrangement for the special base of the external anode tetrode. The cathode pins of the socket are internally grounded, and a low impedance path between screen grid and ground is provided by a bypass capacitor of 2500 µµfd. built into the socket flange. No additional bypass capacitor is necessary on the screen circuit of the tube.

The plate circuit of the 4X150A is composed of a homemade tubing capacitor C_4 and a copper tubing inductance L_4. A single turn loop L_5 and resonating capacitor C_5 are used to

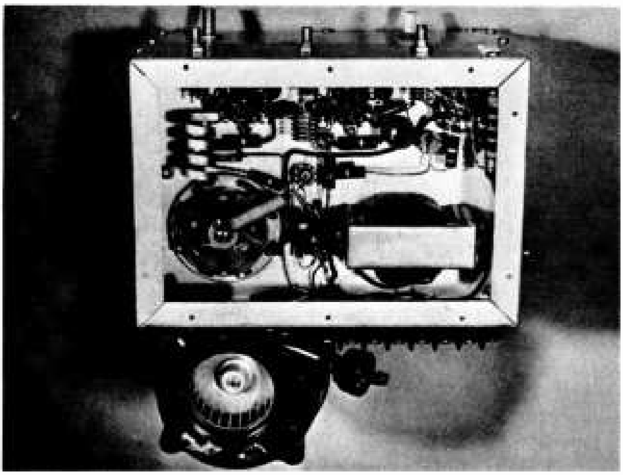


Figure 34

BOTTOM VIEW OF 4X-150A 2-METER TRANSMITTER

4X-150A socket and grid coil are to the left. Screen choke is to the right of the 4X-150A socket. Low frequency stages are along front of the chassis.

load the transmitter to a 52 or 72-ohm transmission line.

In addition to plate power for the 4X150A which is to be supplied by the 120-watt low frequency transmitter, the 2-meter transmitter requires 300 volts at 65 milliamperes for the exciter stages, and a bias supply of −70 volts for the grid of the 4X150A. A power supply

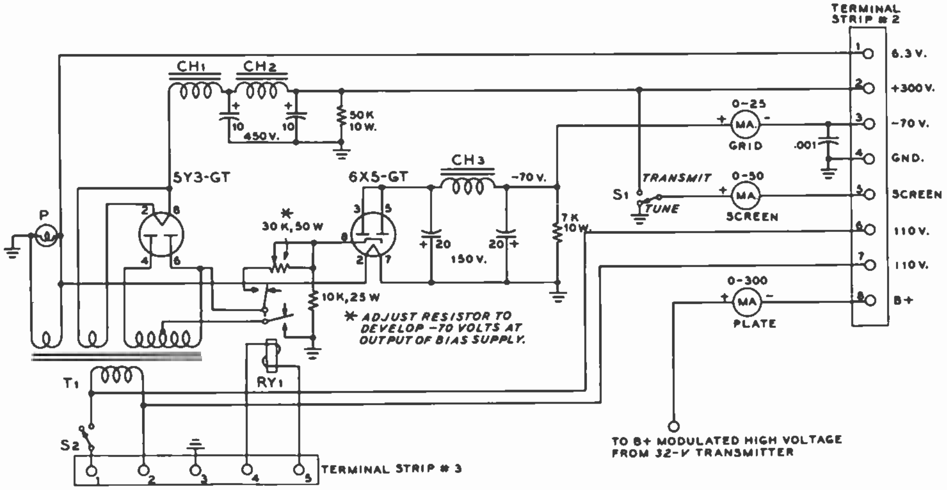


Figure 35

AUXILIARY POWER SUPPLY FOR USE WITH 2-METER R-F UNIT AND COLLINS 32V TRANSMITTER

CH_1, CH_2—10 hy. 100 ma. Stancor C-1001 or Triad C-7X

CH_3—16 hy. 50 ma. Stancor C-1003 or Triad C-3X

T_1—350-0-350 v. 90 ma. Stancor PC-8409 or Triad R-11a

Ry_1—d.p.s.t. relay with 100 v. a-c coil Advance PC-2C-115VA

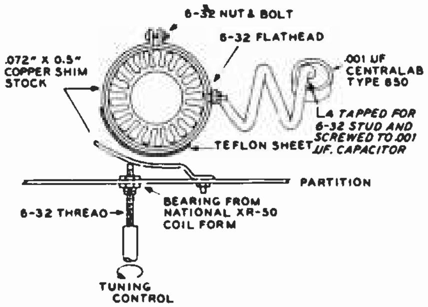


Figure 36

SIMPLIFIED PLATE CLAMP FOR 4X-150A TUBE

CURRENT DRAIN, 120-WATT, 2 METER TRANSMITTER		
CIRCUIT	GRID CURRENT	PLATE CURRENT
OSCILLATOR	—	15 MA.
5763 TRIPLER	1 MA.	20 MA.
5763 DOUBLER	1 MA.	25 MA.
4X-150A	GRID = 8 MA. SCREEN = 30 MA.	200 MA.

Figure 37

that meets these requirements is shown in figure 35. This supply also incorporates a 0-25 d-c milliammeter to measure the grid current of the 4X150A, and a 0-300 d-c milliammeter to measure the plate current of the tube. This supply is not needed when the r-f unit is used in conjunction with the Viking II transmitter.

Transmitter Construction The complete r-f section of the transmitter is constructed upon an aluminum chassis measuring 5" x 7" x 3" (Bud AC-429). A small surplus 110-volt blower is mounted on the rear of the chassis, and a bottom plate is affixed to the chassis by ten sheet metal screws to make the under-chassis area reasonably airtight. The air is thus forced out through the 4X150A tube socket which is flush mounted on the top of the chassis.

An enclosure 5" high is constructed atop the chassis from soft aluminum. This enclosure is divided into two compartments. The front compartment contains the three 5763 tubes. The rear compartment contains the 4X150A tube and associated plate circuit components. The cover of the enclosure is cut from a piece of perforated aluminum stock to allow air circulation in the two compartments.

Plate connection to the 4X150A tube is made by means of a machined copper ring which encircles the anode of the tube. The plate tuning capacitor, C_4, is made of a thin copper spring-shim, one end of which is grounded to the shield separating the two compartments. The distance between this shim and the plate ring of the 4X150A may be varied by means of a threaded shaft reaching through the front compartment to the panel of the transmitter. A sheet of Teflon is placed between the shim and the plate ring to act as dielectric for the variable capacitor (figure 36).

The neutralizing capacitor, NC, is merely a subminiature feedthrough insulator mounted in the intercompartment wall with a small tab on each end to offer a slight capacity to the plates of the 4X150A amplifier and the 5763 doubler. Neutralization is accomplished by varying the size of the tabs and the distance of the tabs from the envelopes of the tubes.

The antenna resonating capacitor C_5 is mounted to the intercompartment wall by insulated spacers, and is controlled from the front panel of the transmitter by means of a short length of insulated shaft coupling. The stator of the capacitor is grounded directly at the shell of the coaxial antenna plug.

The doubler plate coil, L_3, and the antenna pickup link, L_5, are wound from lengths of 3/16" copper strap. Coils L_3, L_4 and L_5 should be silver plated after they are wound for highest circuit efficiency.

Transmitter Tuning Care should be taken that the cooling blower for the 4X150A is turned on at the same time the filament of the tube is lighted. The circuits of the exciter stages should be resonated to their approximate operating frequencies, and final tuning may be done with the aid of an 0-25 d-c milliammeter in the grid circuit of the 4X150A. Screen voltage should be removed from the 4X150A during preliminary tuneup. When sufficient grid drive is applied to the grid of the 4X150A, the plate circuit should be resonated with the aid of a grid-dip oscillator. Neutralization procedure should start with a piece of 3/16" copper strap 1¾" long connected to the side of the feedthrough insulator projecting into the exciter cavity. This strap should be bent near the glass envelope of the 5763 doubler tube. When the plate circuit of the 4X150A is tuned through resonance, there should be no change of grid current as observed on the grid meter of the 4X150A. If neutralization is incomplete, a short tab should be soldered to the side of the feedthrough insulator that projects into the power amplifier compartment. The size of this tab should be increased in

TERMINAL STRIP E-308 OF 32 V	2 METER TRANSMITTER
REMOVE JUMPER 1-2	—
TERMINAL 1	H.V. TERMINAL ON POWER SUPPLY CHASSIS
TERMINAL 6	TERMINAL 3, STRIP 3
TERMINALS 22 AND 23 (*TERMINALS 7 AND 10 ON 32V-1*)	TERMINALS 4,5, STRIP 3

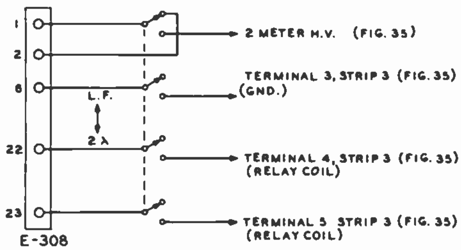


Figure 38
INTERCONNECTIONS BETWEEN 32V TRANSMITTER AND AUXILIARY POWER SUPPLY

small increments until neutralization of the 4X150A is complete. This neutralization adjustment is not critical, and is easily made.

A dummy load or suitable antenna may be connected to the antenna receptacle of the transmitter and plate and screen voltage applied to the 4X150A. Do not apply screen voltage *before* plate voltage is on the tube, or the 4X150A may be injured by excessive screen dissipation. The 1500-ohm series screen resistor will protect the tube during short periods of excessive screen current. The transmitter operating currents are tabulated in figure 37.

2-Meter Operation with Collins 32V Transmitter The 2-meter transmitter and auxiliary power supply are connected together by a cable between terminal strips 1 and 2. Connections between terminal strip 3 of the auxiliary power unit and terminal strip E-308 of the 32V transmitter are tabulated in figure 38. These connections remove the high voltage supply from the final amplifier of the 32V and apply the modulated high voltage to the plate circuit of the 2 meter transmitter. In addition, the push-to-talk circuit of the 32V operates the transmit relay, Ry_1, in the auxiliary power supply of the 2-meter section. No internal changes need be made to the 32V. The exciter stages of the 32V are left in normal condition, and only the 4D32 stage is disconnected. The modulator stages of the 32V transmitter will now modulate the 2-meter r-f section. If desired, the 4D32 tube in the 32V transmitter may be removed from its socket to keep

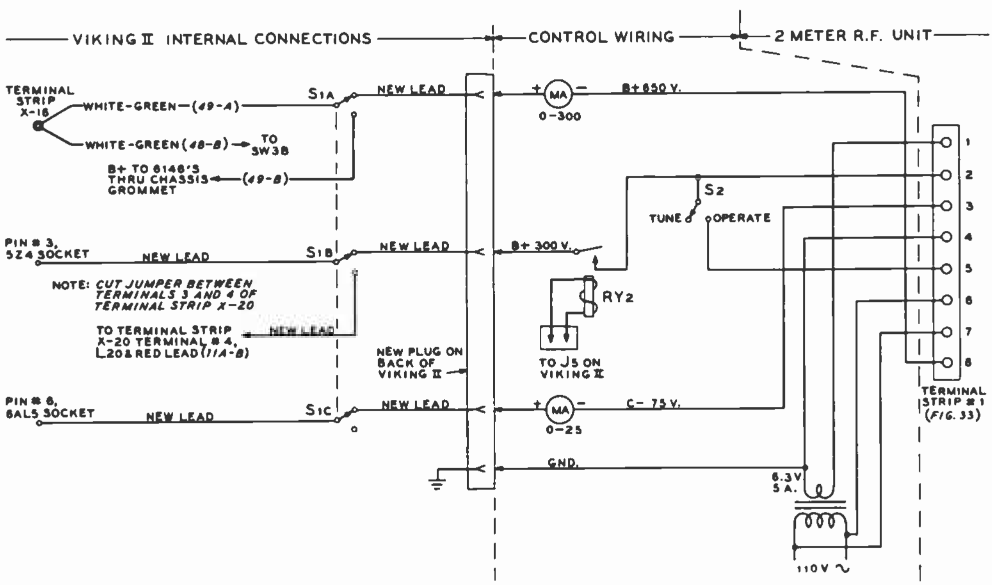


Figure 39
VIKING II CONNECTIONS FOR 2-METER R-F UNIT

the filament from lighting when the 2-meter transmitter is in operation.

Since the 110-volt control circuits of the 32V cannot be reached without internal wiring changes in the cabinet, a separate 110-volt control switch, S_2, is placed in the primary circuits of the auxiliary power supply. S_2 should be turned on at the same time the low voltage switch of the 32V transmitter is turned on. If desired, a three-pole double-throw switch may be connected as shown in figure 38 to allow rapid changeover between the 2-meter transmitter and normal operation of the 32V.

Transmitter Operation with Viking II Transmitter The Viking II transmitter has no auxiliary connections on the rear of the chassis other than the v-f-o plug. Therefore it is necessary to mount a connector plug and transfer switch on the rear of the Viking chassis, immediately behind the 8-μfd. 1000-volt filter capacitor, The auxiliary power supply of figure 35 need not be used when the 2-meter transmitter is run in conjunction with a Viking II transmitter, since all operating voltages may be obtained from the power supply of the Viking transmitter.

Connections between the 2-meter transmitter and the Viking II are shown in figure 39. Switch S_1 and plug P_1 are mounted as described above. Switch S_1 disconnects the high voltage, low voltage and bias circuits from the r-f section of the Viking and connects these circuits to P_1 for connection to the 2-meter r-f unit. Current drain of the 2-meter r-f section is indicated in figure 37. Since it is not feasible to control the 300-volt supply by the "transmit" switch on the Viking II, one additional relay (Ry_2) must be added in the 300-volt lead to the 2-meter transmitter to turn on the low voltage supply when the high voltage supply is turned on by the Viking II "transmit" switch. The coil of Ry_2 is connected to the antenna relay jack (J_5) of the Viking II transmitter. The two meters, Ry_2 and the filament transformer may be mounted in a small box and placed next to the 2-meter r-f unit.

25-7 A Versatile V.F.O.-Exciter Unit

The unit shown in figures 40 through 48 has been designed for those amateurs who desire a v.f.o. exciter with a high degree of operating flexibility, combined with maximum frequency stability. The unit may be operated on any band between 10 meters and 80 meters with complete coverage of each band. A 2E26 tube is used in the output stage, and the v.f.o. exciter has a power output of 12 watts. The a-c power supplies for the exciter unit are built upon a separate chassis designed to be placed beneath the operating table. Connections between the two units are made via a multi-conductor cable.

General Circuit Description A Collins 70E-20 precision oscillator is the heart of this exciter unit. The 70E-20 per-

Figure 40
15-WATT ALL-BAND EXCITER USING COLLINS 70E-20 V.F.O.

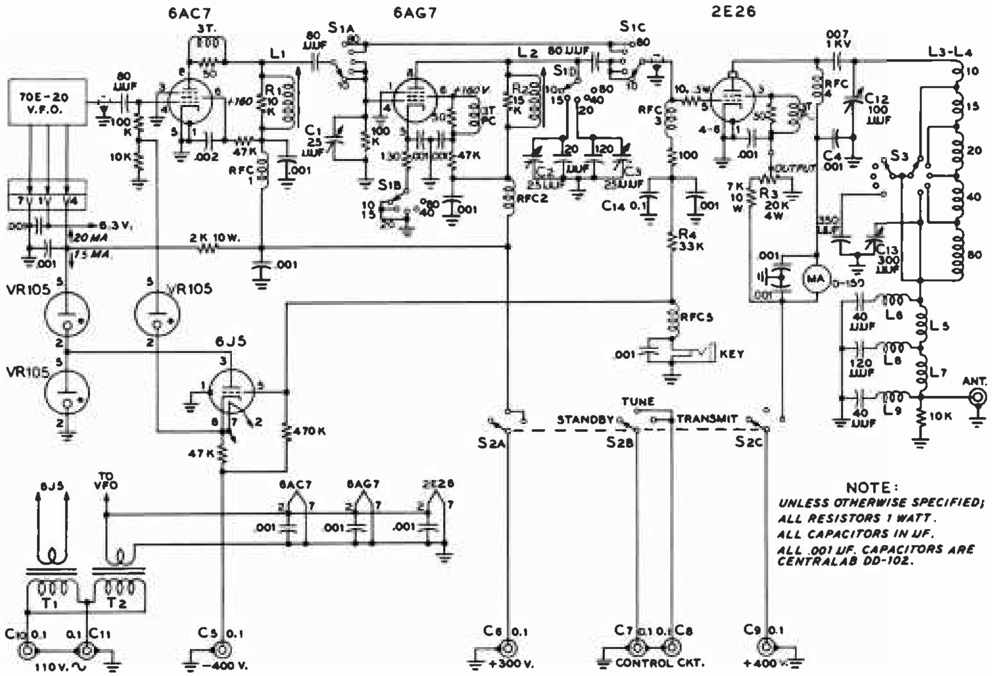


Figure 41
SCHEMATIC OF V.F.O.-EXCITER UNIT

C_1, C_2, C_3—25 $\mu\mu$fd. Centralab 822-AZ
C_4—.001 μfd. Centralab type FT-1000
C_5-C_{11}—.01 μfd. Sprague type 80P3 Hy-pass
C_{12}—100 $\mu\mu$fd. Bud MC-1865
C_{13}—300 $\mu\mu$fd. Bud MC-1860
C_{14}—0.1 μfd. 600 v. oil-filled
Parasitic chokes—3 t. no. 18 enam. on 50 ohm, 1 watt resistor
Note: 47K resistor in cathode circuit of 6J5 Keyer tube has a 5-watt rating.

RFC_1, RFC_2, RFC_3—2.5 mh. National R-100
RFC_4—2.5 mh. National R-100U
RFC_5—v.h.f. choke Ohmite Z-50
T_1, T_2—6.3 v. at 3 a. UTC S-55
S_1—Centralab Index Assembly P-123 with two type 2505 ceramic decks
S_2—3p.3t. Centralab 1407
S_3—Centralab type PA-2042 modified as shown in Figure 44

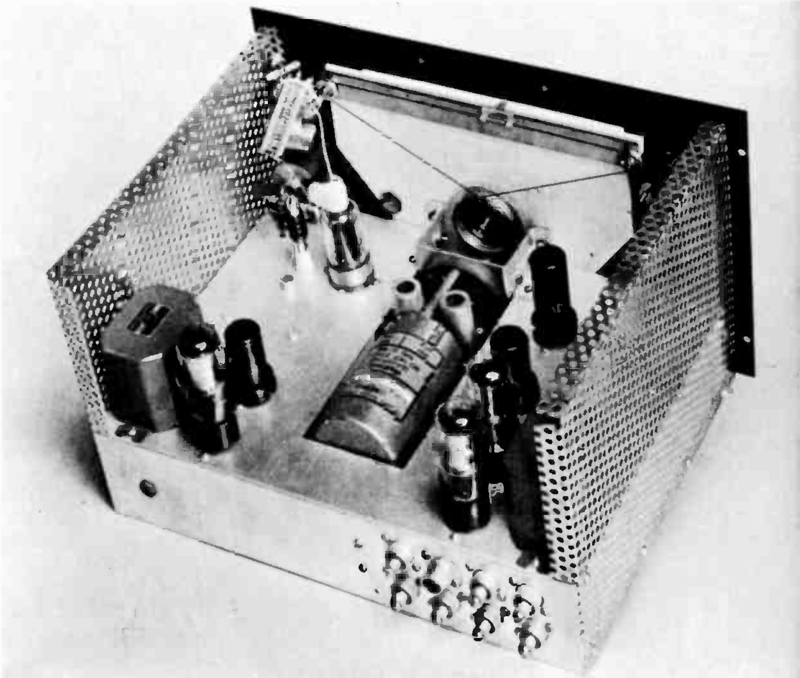
meability-tuned oscillator is continuously variable in the range of 1.65 Mc. to 2.05 Mc. The oscillator calibration is essentially linear and accurate to 500 cycles. Maximum frequency drift in the range of temperature from 40 degrees Farenheit to 120 degrees Farenheit is 400 cycles, and the maximum drift with 10 per cent plate voltage variation is 75 cycles. The 70E-20 utilizes two type 5749 pentode tubes. One tube serves as a buffer which minimizes frequency change due to varying load conditions. The screen grid of the other 5749 tube is used as the oscillator plate which is maintained at r-f ground potential. Feedback is applied via the cathode of the tube which is connected to a tap on the oscillator coil.

The tank circuit is permeability tuned by insertion of a ferromagnetic core into the coil. This coil has a specially developed variable-pitch winding to provide excellent tuning linearity. An internal corrector controls the rate at which the tuning core advances into the coil to maintain calibration linearity to less than 500 cycles.

The 70E-20 oscillator is sealed at the factory and humidity changes in the atmosphere do not affect the performance of the unit. The oscillator unit is supplied with 210 volts, regulated by series connected gas regulator tubes. The output signal of the oscillator has excellent stability characteristics and negligible drift on all bands.

Figure 42
REAR VIEW OF 15-WATT V-F-O EXCITER

The Collins 70E-20 v-f-o unit is mounted in a rectangular cutout at center of chassis. Keyer tubes and filament transformer are mounted at left rear corner of chassis. The homemade all-band tank assembly is mounted directly above the 2E26 stage.



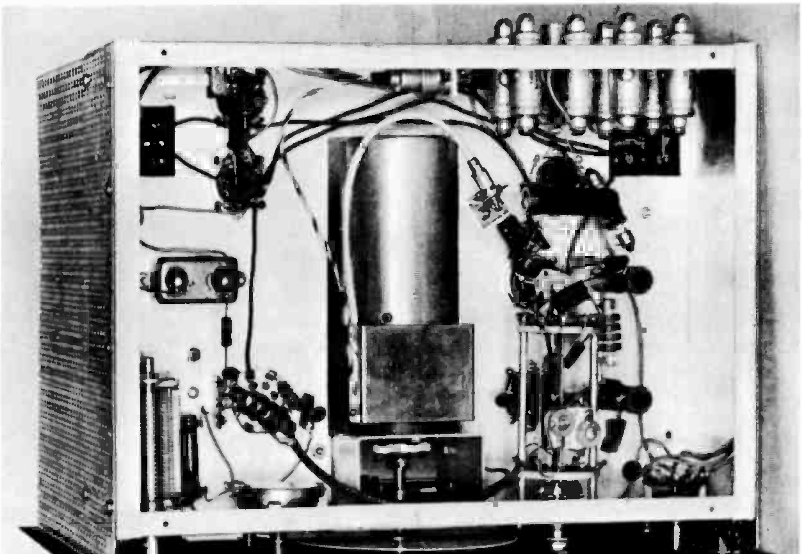
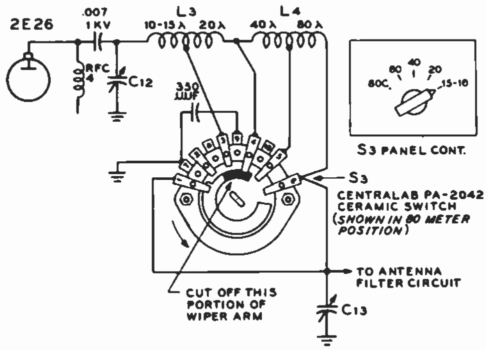


Figure 43
UNDER CHASSIS VIEW OF V-F-O EXCITER

The bandswitch assembly for the doubler stages is at the right. A short length of coaxial cable connects the 2E26 grid circuit to the bandswitch. The v-f-o power plug is visible at back of the chassis.



COIL TABLE

L_1 - NATIONAL XR-50 COIL FORM. ONE LAYER #30 CLOSEWOUND PLUS TEN TURNS OVERWOUND AT BOTTOM END. ONE LAYER PAPER TAPE BETWEEN WINDINGS.

L_2 - NATIONAL XR-50 FORM. 19 TURNS # 24E.

L_3 - 16 TURNS, 3/4" DIA., 2" LONG # 16 E. B&W MINIDUCTOR 3010. 10–15 METER COIL 7 TURNS. 20 METER COIL 9 TURNS.

L_4 - 34 TURNS, 1" DIA., 1 1/8" LONG # 24 E. B&W MINIDUCTOR 3016. 40 METER COIL 17 TURNS. 80 METER COIL 17 TURNS.

L_5-L_7 - 8 TURNS # 14 WIRE, 1/2" I.D., 1" LONG

L_6-L_9 - 6 TURNS # 14 WIRE, 1/2" I.D., 3/4" LONG

L_8 - 1 TURN # 14 WIRE, 1/2" I.D.

Figure 44

2E26 PLATE CIRCUIT LAYOUT AND COIL TABLE

The first 6AC7 doubler stage operates into a broadly resonant slug-tuned coil L_1. When tuning the exciter unit this coil is peaked at 3.6 Mc. The stage then will deliver substantially constant output over the range from 3.2 to 4.0 Mc. The 2E26 stage operates as an amplifier on the 3.5-Mc. band and as a doubler on the 7-Mc. band, driven directly from the 6AC7 stage.

For operation on 20, 15 and 10 meters, switch S_1 disconnects the 2E26 from the 6AC7 stage, and connects it to an auxiliary 6AG7 frequency multiplier. The 6AG7 multiplier operates either as a doubler, a tripler or a quadrupler. Its output circuit, therefore, is either tuned to 7 Mc., 10.5 Mc., or 14 Mc. Coil L_2 in the plate circuit of the 6AG7 resonates with residual circuit capacities to 14 Mc. Switch section S_{2B} of the bandswitch adds additional capacity to lower the resonant frequency of this circuit to 10.5 Mc. or 7 Mc.

The 2E26 stage operates as a doubler to 14 Mc., receiving 7 Mc. excitation from the 6AG7 stage. When the 6AG7 is tuned to 10.5 Mc., the 6AG7 acts as a doubler to 21 Mc. For 28 Mc. output from the 2E26, 14-Mc. excitation is received from the 6AG7 stage, and the 2E26 again functions as a doubler.

To prevent higher order harmonics generated by the 2E26 doubler stage from creating TVI problems, a low-pass filter is connected in the coaxial output lead from the exciter. The filter is designed to reject all frequencies above 36 Mc. that may appear in the output circuit of the exciter.

The power supply for the v.f.o. exciter is built upon a separate chassis and may be placed beneath the operating table or put in the main cabinet of the transmitter. An eight-wire cable connects the power supply unit to the exciter. An a-c operated relay, Ry_1, is actuated by switch S_2 of the exciter and serves to turn on the two high voltage power supplies when S_2 is set in the "tune" or "transmit" position. The complete schematic of the exciter is shown in figure 41, and the auxiliary power supply schematic is shown in figure 45.

The power supply is designed around the U.T.C. type S-39 power transformer. This transformer has a dual voltage winding that will provide 400 volts d.c. at 100 milliamperes, and 300 volts d.c. at 75 milliamperes. Three filament windings are also provided: 5 volts for a 5U4-G, 6.3 volts for a 6X5-G and 2.5 volts which is used for the filament of a 2A3 connected as a half-wave rectifier for the 400-volt bias supply.

Two filament transformers are incorporated in the exciter unit. T_2 is used for all tubes except the 6J5 keyer tube. The cathode of this tube is at a negative potential of 400 volts, and if a grounded filament circuit is used the maximum cathode-filament breakdown potential of the tube will be greatly exceeded. A separate filament transformer T_1 is used for the 6J5 keyer tube. Pins 7 and 8 of the 6J5 tube are strapped together removing the 400-volt filament-cathode potential difference from the tube and placing it across the primary-secondary insulation of T_1. This transformer is insulated for 1500 volts d.c. The 6J5 and the VR-105 tube connected in the grid circuit of the 6AC7 form a vacuum tube keying circuit that is very effective. This circuit has been discussed in Chapter 17 of this Handbook.

Exciter Construction The exciter is built upon an aluminum chassis measuring 10"x 14"x 3" (Bud AC-414) and fits within a steel cabinet measuring 11"x 15" x 9" (Bud C-975). To reduce TVI to an absolute minimum, all power leads leaving the chassis pass through Sprague type 80P3 Hypass capacitors. To prevent direct radiation of harmonics from the exciter circuits, an aluminum enclosure is made of perforated metal stock. This enclosure fits over the top of the exciter and is fastened to the aluminum chassis and the front panel by means of self-tapping sheet metal screws. A sheet of the same material covers the bottom of the chassis. The steel cabinet contributes little or nothing to the all-enclosing shield; it is merely a decorative dust cover.

It is well to build up the shielding enclosure before any work is started on the exciter. The enclosure is formed out of a sheet of 36" x 36" Reynolds "Do-it-yourself" (round hole perforated stock) aluminum sheet which is available in most hardware stores, department stores, or building supply houses. The enclosure is made out of four pieces: two end pieces and two mating pieces that form the top and the back. The dimensions for these pieces are shown in figure 46, and shielding construction information is contained in Chapter 30.

A 7/8" space is left between the aluminum chassis and the front panel to allow clearance for the dial mechanism of the 70E-20 variable frequency oscillator. All panel controls except C_{12} are attached to the chassis and have shafts 1¼" long that protrude through the front panel. Capacitor C_{12} is, however, attached directly to the front panel by its 3/8" shaft nut. The rear end of the capacitor is bolted to the deck of the aluminum chassis.

Placement of the major components may be seen in the rear view photograph, figure 42. The v.f.o. unit is mounted in a cutout in the center of the chassis. It is held to the chassis by means of two small aluminum angle brackets bolted to the frame that holds the v.f.o. unit to the dial assembly. The tuning shaft of the v.f.o. is 2¾" above the bottom edge of the chassis. To the right of the v.f.o. are the

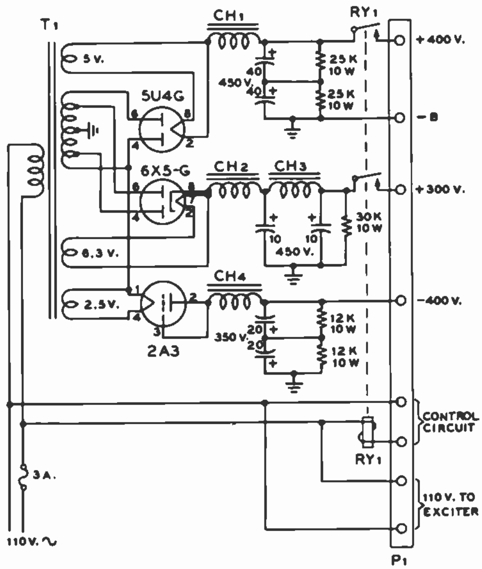


Figure 45

POWER SUPPLY FOR R-F UNIT

T_1—490,400-0-400,490 volts, 5 v. at 3 a., 6.3 v. at 4 a., 2.5 v. at 6 a. UTC S-39

CH_1,CH_2,CH_3—20 hy. at 100 ma. UTC S-28

CH_4—30 hy. at 75 ma. UTC S-27

RY_1—d.p.s.t. with 110 volt a-c coil. Advance PC-2C-115VA

P_1—Cinch-Jones S-310AB and P-310CCT

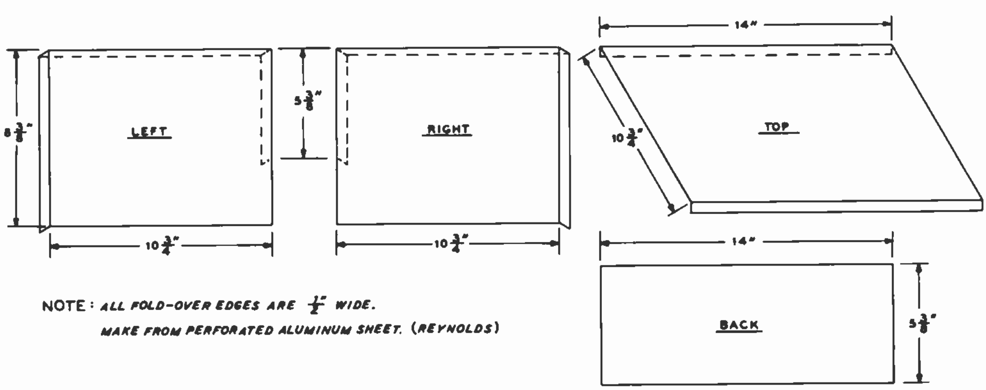


Figure 46

SHIELD PIECES FOR V-F-O EXCITER

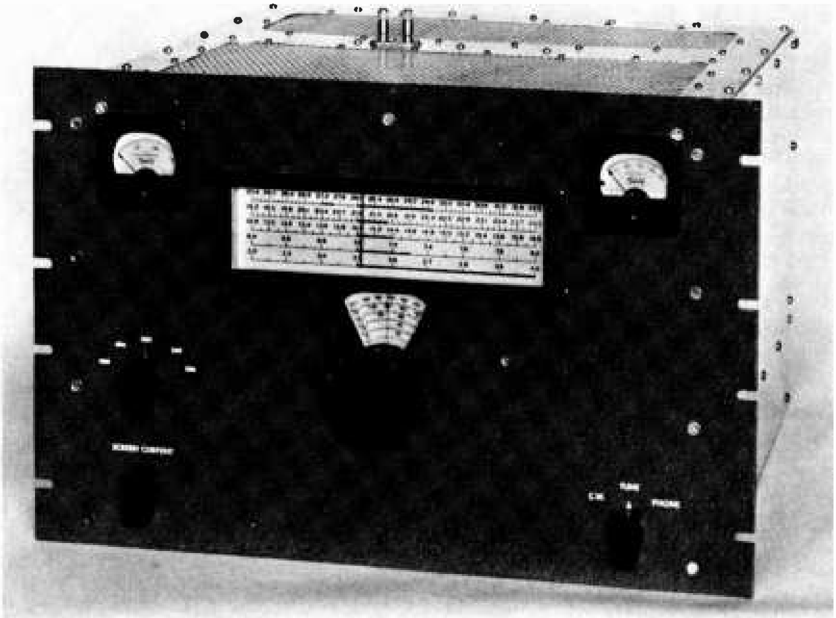


Figure 47
RACK MOUNTED V-F-O EXCITER
The exciter unit of Figure 41 and the power supply of Figure 45 are combined into one rack mounting unit. An 807 tube is used in the output stage which is capacitively coupled to the grid circuit of the power amplifier as shown in Figure 48.

6AC7 and 6AG7 doubler tubes, the two voltage regulators and transformer T_2. To the right of the v.f.o. is the 2E26 output stage, the 6J6 and VR-105 keyer tubes, and T_1. The location of the below-chassis components is shown in figure 43.

Electrical Assembly Power leads for the 70E-20 oscillator unit are terminated in a miniature 7-prong plug. A matching socket is mounted on the rear inside wall of the chassis on a small angle bracket. The doubler stage components for both the 6AC7 and the 6AG7 are connected directly between the socket prongs of the respective tubes and sections A and D of bandswitch S_1. The lead from the arm of S_{1C} to pin 5 of the 2E26 tube socket is made of a 6½" length of RG-59/U coaxial line. The capacity of this line appears across the tuned circuits of the 6AG7 stage when S_{1C} is in the 20, 15 and 10 meter positions, and across the 6AC7 tuned circuits when S_{1C} is in the 80 and 40-meter positions. Trimming capacitor C_1 compensates for the change in circuit capacity as switch S_1 removes the residual capacity of the coaxial line from the 6AC7 tuned circuit.

All bypass capacitors should be mounted as closely to the respective tube sockets as is possible. The plate bypass capacitor of the 2E26 stage, C_4, is a Centralab type FT feedthrough unit mounted on the deck of the chassis.

The all-band tank assembly of the 2E26 stage is made up from a Centralab PA-2042 Ceramic progressively shorting 10 pole switch, modified as shown in figure 44. The main portion of the switch shorts out sections of L_3-L_4 as the switch is advanced from 80 meters. An auxiliary pair of contacts adds additional output capacity to the loading section of the pi-network for 80 meter operation. An additional switch setting designated "80-C" adds this extra capacity to the circuit. Coil L_3 mounts between contact 4 of S_3 and the junction between C_{12} and the .007-$\mu\mu$fd. plate blocking capacitor. The coil is mounted at right angles to the front panel of the exciter. Below L_3 and parallel to the exciter panel is coil L_4. This coil is mounted between contacts 4 and 1 of S_3. A jumper connects contacts 1 and 6 of S_3. The output lead from the network passes through a chassis grommet to the loading capacitor, C_{13} and then through the low-pass filter and a short length of RG-59/U coaxial line to the coaxial plug on the rear wall of the exciter chassis.

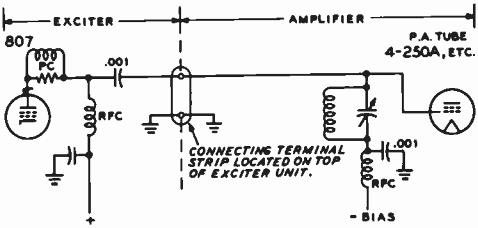


Figure 48
CAPACITIVE COUPLING CIRCUIT BETWEEN V-F-O EXCITER AND FINAL AMPLIFIER STAGE

Power Supply Assembly The exciter power supply is built upon an amplifier foundation measuring 7"x 17"x 8½" (Bud CA-1126). Connections are made to the exciter via a length of eight wire cable and a low resistance plug and socket located on the rear wall of the power supply chassis. When the power supply has been wired and tested, all connections between the supply and the exciter may be made with the exception of the 400-volt lead to the plate circuit of the 2E26 stage.

Testing the Exciter All tubes should be plugged in the exciter and switch S_1 placed in the 80-meter position. A high resistance voltmeter should be placed across the 33,000-ohm grid resistor R_4 of the 2E26 stage (positive lead of the meter attaches to the lead from R_4 to RFC_3). The oscillator should be monitored in a nearby receiver, and the two voltage regulator tubes should glow when S_2 is placed in either the "tune" or "transmit" position. The slug of L_1 should be adjusted for maximum meter reading when the frequency of the variable oscillator is set at 3.6 Mc. A reading of not less than 50 volts nor more than 90 volts should be obtained as the v.f.o. is tuned across the 80-meter band. If the voltage across R_4 is excessive, padding resistor R_1 may be decreased in value. Grid voltage should remain relatively constant across the entire band.

Bandswitch S_1 should now be set to the 10-meter position. The slug of L_2 and padding capacitor C_1 are adjusted for the above value of grid voltage across the 28-Mc. band. The v.f.o. should be set to 28.5 Mc. for initial adjustment. The bandswitch is next set to the 15-meter position and the v.f.o. tuned to 21.2 Mc. Padding capacitor C_2 is adjusted for correct value of grid voltage across the 15-meter band. As a last step, the bandswitch is set for 20 meters, the v.f.o. tuned to 14.2 Mc. and capacitor C_3 adjusted for uniform grid drive across the 20-meter band.

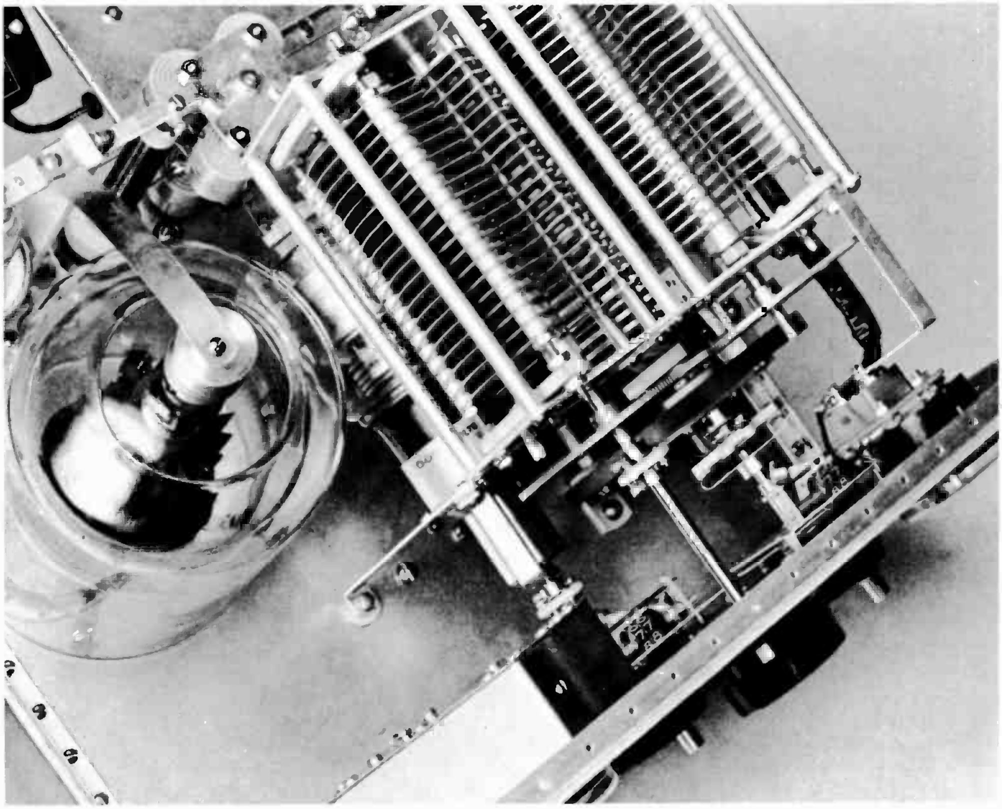
The consistency of grid drive across the various amateur bands is controlled by the padding resistors R_1 and R_2 across coils L_1 and L_2. The lower value of these resistors, the more uniform is the grid drive across the various bands. At the same time, the drive to the 2E26 drops as these resistors are lowered in value. The values shown in figure 41 give satisfactory results on all bands, since the grid voltage of the 2E26 may vary almost 2:1 across an amateur band with little change in the output from the 2E26 stage.

A 50-ohm dummy load should now be connected to the coaxial output plug of the exciter, the output control R_3 is set for minimum output (ground end) and plate voltage is applied to the 2E26 stage. Circuit resonance is set by C_{12} and loading is controlled by C_{13}. If loading is excessive on the 80-meter band, the 350-$\mu\mu$fd. shunting capacitor across C_{13} should be increased in value.

The power output from this exciter is sufficient to drive any of the newer power tetrodes to 1-kilowatt input on all bands covered by the exciter. On the 15 and 10-meter bands it may be necessary to prune the length of coaxial line connecting the exciter to the power amplifier stage in order to obtain maximum output from the 2E26 stage. This precaution is necessary if a high order of SWR exists on the interconnecting coaxial line between the exciter and the power amplifier.

Keying of the exciter is smooth and clickless. The addition of a high powered amplifier following the exciter will sharpen the keying to some extent. Wave forming capacitor C_{14} may be increased in value to soften the exciter keying to compensate for the sharpening action of the stages following the exciter. Care must be taken that the amplifier stage following the exciter is free of parasitics and completely stable, or parasitic key-clicks will be reintroduced upon an otherwise clean signal.

It is possible to combine the power supply and exciter into one unit, suitable for mounting in a standard 19" relay rack. Such an assembly is shown in figure 47. A 14"x 17"x 3" chassis is used and the power supply components are mounted along the back of the chassis. This particular exciter is designed to be used with the push-pull 4-250A amplifier of Chapter 26. The plate circuit of the 2E26 stage of the exciter is shunt fed, and the band switching circuit of the 4-250A amplifier is used as a common circuit for both the 2E26 and the grid circuit of the amplifier. The plate connection of the 2E26 exciter appears at the two terminal plug located on the top of the exciter. A matching plug on the bottom of the 4-250A amplifier connects the two units when they are placed in the rack; the amplifier mounted directly above the exciter. A typical inter-connecting circuit is shown in figure 48.



High Frequency Power Amplifiers

The trend in design of transmitters for operation on the high frequency bands is toward the use of a single high-level stage. The most common and most flexible arrangement includes a compact bandswitching exciter unit, with 15 to 100 watts output on all the high-frequency bands, followed by a single power amplifier stage. In many cases the exciter unit is placed upon the operating table, with a coaxial cable feeding the drive to the power amplifier, although some operators prefer to have the exciter unit included in the main transmitter housing.

This trend is a natural outgrowth of the increasing importance of v-f-o operation on the amateur bands. It is not practical to make a quick change in the operating frequency of a transmitter when a whole succession of stages must be retuned to resonance following the frequency change. Another significant factor in implementing the trend has been the wide acceptance of commercially produced 75 and 150-watt transmitters. These units, such as the Johnson Ranger and Viking II and the Collins 32V, provide r-f excitation and audio driving power for high-level amplifiers running up to the 1000-watt power limit. The amplifiers discussed in this chapter were specifically designed for use with these exciters, and complete installations employing these commercial transmitters as exciters are shown and discussed in Chapter 28 of this Handbook.

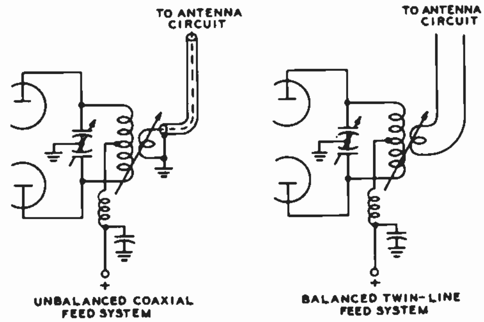


Figure 1
LINK COUPLED OUTPUT CIRCUITS FOR PUSH-PULL AMPLIFIERS

26-1 Power Amplifier Design-Choice of Tubes

Either tetrode or triode tubes may be used in high-frequency power amplifiers. The choice is usually dependent upon the amount of driving power that is available for the power amplifier. If a transmitter-exciter of 100-watt power capability is at hand (such as the Viking II) it would be wise to employ a power amplifier whose grid driving requirements were to fall in the same range as the output power of the exciter. Triode tubes running 1-kilowatt input (plate modulated) generally require some 50 to 80 watts of grid driving power. Such a requirement is easily met by the output level of the 100-watt transmitter which should be employed as the exciter. Tetrode tubes (such as the 4-250A) require only 10 to 15 watts of actual drive from the exciter for proper operation of the amplifier stage at 1-kilowatt input. This means that the output from the 100-watt transmitter has to be cut down to the 15 watt driving level. This is a nuisance, as it requires the addition of swamping resistors to the output circuit of the transmitter-exciter. The triode tubes, therefore, would lend themselves to a much more convenient driving arrangement than would the tetrode tubes, simply because their grid drive requirements fall within the power output range of the exciter unit.

On the other hand, if the transmitter-exciter output level is in the range of 15-50 watts (the exciter of Chapter 25, section 7, or the Johnson Ranger) sufficient drive for triode tubes running 1-kilowatt input would be lacking. Tetrode tubes requiring low grid driving power would have to be employed in a high-level stage, or smaller triode tubes requiring modest grid drive and running 250 watts or so would have to be used.

Power Amplifier Design-Choice of Circuits Either push-pull or single ended circuits may be employed in the power amplifier. Using modern tubes and properly designed circuits, either type is capable of high efficiency operation and low harmonic output. Push-pull circuits, whether using triode or tetrode tubes usually employ link coupling between the amplifier stage and the feed line running to the antenna or the antenna tuner.

It is possible to use the link circuit in either an unbalanced or balanced configuration, as shown in figure 1, using unbalanced coaxial line, or balanced twin-line.

Common technique is to employ plug-in plate coils with the push-pull amplifier stage. This necessitates some kind of opening for coil changing purposes in the "electrically tight" enclosure surrounding the amplifier stage. Care must be used in the design and construction of the door for this opening or leakage of harmonics through the opening will result, with the attendant TVI problems.

Single ended amplifiers may also employ link-coupled output devices, although the trend is to use pi-network circuits in conjunction with single ended tetrode stages. A tapped or otherwise variable tank coil may be used which is adjustable from the front panel, eliminating the necessity of plug-in coils and openings into the shielded enclosure of the amplifier. Pi-network circuits are becoming increasingly popular as coaxial feed systems are coming into use to couple the output circuits of transmitters directly to the antenna.

26-2 Push-Pull Triode Amplifiers

Figure 2 shows a conventional push-pull amplifier circuit. While variations in the method of applying plate and filament voltages and bias are sometimes found, the basic circuit remains the same in all amplifiers.

Filament Supply The amplifier filament transformer should be placed right on the amplifier chassis in close proximity to the tubes. Short filament leads are necessary to prevent excessive voltage drop in the connecting leads, and also to prevent r-f pickup in the filament circuit. Long filament leads can often induce instability in an otherwise stable amplifier circuit, especially if the leads are exposed to the radiated field of the plate circuit of the amplifier stage. The filament voltage should be the correct value specified by the tube manufacturer when measured *at the tube sockets*. A filament transformer having a tapped primary often will be found useful in adjusting the filament voltage. When there is a choice of having the filament voltage slightly higher or slightly lower than normal, the higher voltage is preferable. If the amplifier is to be overloaded, a filament voltage slightly higher than the rated value will give greater tube life.

Plate Feed The series plate voltage feed shown in figure 2 is the most satisfactory method for push-pull stages. This method of feed puts high voltage on the plate tank coil, but since the r-f voltage on the coil is in itself sufficient reason for protecting the coil from accidental bodily contact, no additional protective arrangements are made necessary by the use of series feed.

The insulation in the plate supply circuit should be adequate for the voltages encountered. In general, the insulation should be rated to withstand at least four times the maximum d-c plate voltage. For safety, the plate meter should be placed in the cathode return lead, since there is danger of voltage breakdown between a metal panel and the meter movement at plate voltages much higher than one thousand.

Grid Bias The recommended method of obtaining bias for c-w or plate modulated telephony is to use just sufficient fixed bias to protect the tubes in the event of excitation failure, and to obtain the rest by the voltage drop caused by flow of rectified grid current through a grid resistor. If desired, the bias supply may be omitted for telephony if an overload relay is incorporated in the plate circuit of the amplifier, the relay being adjusted to trip immediately when excitation is removed from the stage.

The grid resistor R_1 serves effectively as an r-f choke in the grid circuit because the impressed r-f voltage is low, and the Q of the resistor is poor. No r-f choke need be used in the grid bias return lead of the amplifier, other than those necessary for harmonic suppression.

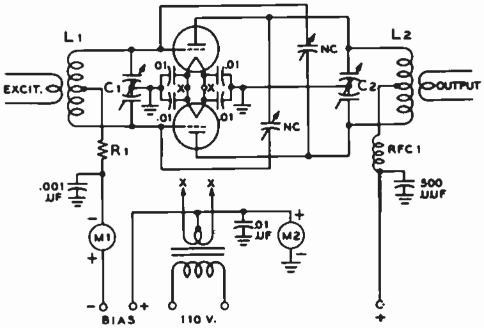


Figure 2

CONVENTIONAL PUSH-PULL AMPLIFIER CIRCUIT

The mechanical layout should be symmetrical and the output coupling provision must be evenly balanced with respect to the plate coil

C_1—Approx. 1.5 $\mu\mu$fd. per meter of wavelength per section

C_2—Refer to plate tank capacitor design in Chapter 11

C_3—May be 500-$\mu\mu$fd., 10,000-volt type ceramic capacitor

NC—Max. usable capacitance should be greater, and min. capacitance less than rated grid-plate capacity of tubes in amplifier. 50% greater air gap than C_2.

R_1—100 ohms, 20 watts. This resistor serves as low Q r-f choke.

RFC_1—All-band r-f choke suitable for plate current of tubes

M_1,M_2—Suitable meters for d-c grid and plate currents

All low voltage .001-μfd. and .01-μfd. by-pass capacitors are ceramic disc units (Centrolab DD or equiv.)

L_1—50-watt plug-in coil, center link

L_2—Plug-in coil, center link, of suitable power rating

Parasitics and TVI Problems Any power amplifier, push-pull or otherwise makes an excellent oscillator at some frequency higher than the operating frequency of the amplifier. Such an oscillation is termed a *parasitic oscillation*. General design precautions to eliminate parasitics were discussed in Chapter 15. It must be emphasized that parasitic loops are normally present in even the most well engineered circuits, and definite steps must be taken to eliminate them.

It is always best and safest to assume the presence of parasitic oscillations in amplifier stages, until it is *proven* that they are absent.

Two basic methods of eliminating parasitics are at hand: First, the inductance of the various leads of the amplifier may be decreased by making the leads shorter and heavier until the resonant parasitic frequency is moved up and out of the operating range of the amplifier tubes. Second, certain leads in the amplifier may be made long enough to lower the parasitic frequency until it is within the range in which the amplifier is self-neutralized by the neutralizing capacitors. In addition, the leads may be swamped with resistors to act as loading devices at the parasitic frequency of oscillation. Such long leads and swamping resistors are generally referred to as *parasitic chokes*. The elimination of parasitic oscillations in the amplifier stage will do much to lessen the TVI problem. Simple shielding and lead filtering will suffice to eliminate TVI from a stable, parasitic-free amplifier. TVI elimination from an amplifier containing one or more parasitic oscillations is an almost impossible task.

The Grid Circuit As the power in the grid circuit is much lower than in the plate circuit, it is customary to use a close-spaced split-stator grid capacitor with sufficient capacitance for operation on the lowest frequency band. A physically small capacitor has a greater ratio of maximum to minimum capacitance, and it is possible to obtain a unit that will be satisfactory on all bands from 10 to 80 meters without the need for auxiliary padding capacitors. The rotor of the grid capacitor is grounded, simplifying mounting of the capacitor and providing circuit balance and electrical symmetry. Grounding the rotor also helps to retard v-h-f parasitics by by-passing them to ground in the grid circuit. The L/C ratio in the grid circuit should be fairly low, and care should be taken that circuit resonance is not reached with the grid capacitor at minimum capacitance. That is a direct invitation for instability and parasitic oscillations in the stage. The grid coil may be wound of no. 14 wire for driving powers of up to 100 watts. To restrict the field and thus aid in neutralizing, the grid coil should be physically no larger than absolutely necessary.

Circuit Layout The most important consideration in constructing a push-pull amplifier is to maintain electrical symmetry on both sides of the balanced circuit. Of utmost importance in maintaining electrical balance is the control of stray capacitance between each side of the circuit and ground.

Large masses of metal placed near one side of the grid or plate circuits can cause serious unbalance, especially at the higher frequencies, where the tank capacitance between one side of the tuned circuit and ground is often quite small in itself. Capacitive unbalance most often occurs when a plate or grid coil is located with one of its ends close to a metal panel. The solution to this difficulty is to mount the coil parallel to the panel to make the capacitance to ground equal from each end of the coil, or to place a grounded piece of metal opposite the "free" end of the coil to accomplish a capacity balance.

Whenever possible, the grid and plate coils should be mounted at right angles to each other, and should be separated far enough apart to reduce coupling between them to a minimum. Coupling between the grid and plate coils will tend to make neutralization frequency sensitive, and it will be necessary to readjust the neutralizing capacitors of the stage when changing bands.

All r-f leads should be made as short and direct as possible. The leads from the tube grids or plates should be connected directly to their respective tank capacitors, and the leads between the tank capacitors and coils should be as heavy as the wire that is used in the coils themselves. Plate and grid leads to the tubes may be made of flexible tinned braid or flat copper strip. Neutralizing leads should run directly to the tube grids and plates and should be separate from the grid and plate leads to the tank circuits. Having a portion of the plate or grid connections to their tank circuits serve as part of a neutralizing lead can often result in amplifier instability at certain operating frequencies.

Excitation Requirements In general it may be stated that the overall power requirement for grid circuit excitation to a push-pull triode amplifier is approximately 10 per cent of the amount of the power output of the stage. Tetrodes require about 1 per cent to 3 per cent excitation, referred to the power output of the stage. Excessive excitation to pentodes or tetrodes will often result in reduced power output and efficiency.

26-3 A Push-Pull 811-A Triode Amplifier

A 350-watt push-pull 811-A triode amplifier is shown in figures 3 to 6. The 811-A tube offers an advantage for r-f work that is not found

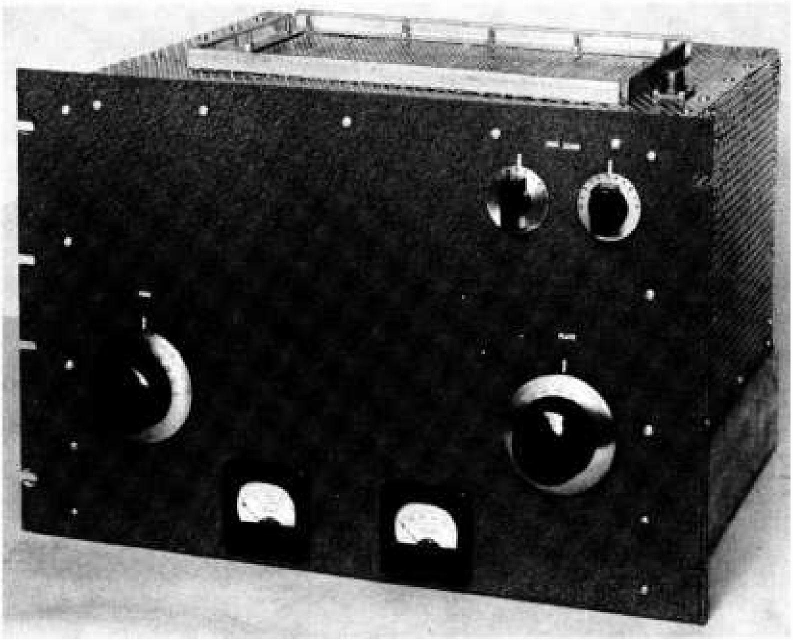


Figure 3

THE 811-A AMPLIFIER. A TVI-PROOF DESIGN SUITABLE FOR OPERATION ON ALL AMATEUR BANDS BETWEEN 10 METERS AND 80 METERS

Plate and grid coils may be removed through the top of the amplifier enclosure when the cover plate is taken off. The amplifier is placed in a cabinet (see Chapter 28, Section 1) which has a matching door in the top.

in other tubes of similar power capabilities. The amplification factor of the 811-A is 160 which means that this tube may be operated in a zero-bias condition with plate potentials up to 1250 volts. The elimination of a bias supply in the design of an amplifier stage greatly simplifies the stage and makes it an ideal arrangement for the beginner. When the excitation is removed from the 811-A tube, the plate current drops to an exceedingly low value and no harm is done to the tube. The 811-A may, in fact, be keyed by merely opening the ground return lead of the grid circuit.

This final amplifier may be operated at a maximum input of 1500 volts and 350 milliamperes, or 525 watts. However, at this input a fixed bias of 5 volts is required by the 811-A tubes. If the plate voltage is held below 1250 volts, no such safety bias is needed.

Commercial plug-in coils are employed in the grid and plate circuits of the amplifier, and the input and output circuits are link coupled. A 25-$\mu\mu$fd. fixed air capacitor C_4 is clipped across the plate tank circuit for 80-meter operation.

Amplifier Construction The 811-A amplifier is built upon an aluminum chassis measuring 12" x 17" x 3" (Bud AC-418) and uses a standard 19" relay rack panel 12¼" high. The above-chassis area of the amplifier is enclosed in a housing measuring 11¾" deep by 16¾" long by 8¾" high. The enclosure frame is made of 3/4" Reynolds "Do-it-yourself" aluminum angle stock. The end pieces, back and top pieces are made from perforated sheet stock furnished by the same manufacturer. The construction of such an enclosure is covered in Chapter 30. A sheet of aluminum measuring 12" x 17" is attached to the bottom of the chassis to enclose the components mounted beneath the chassis.

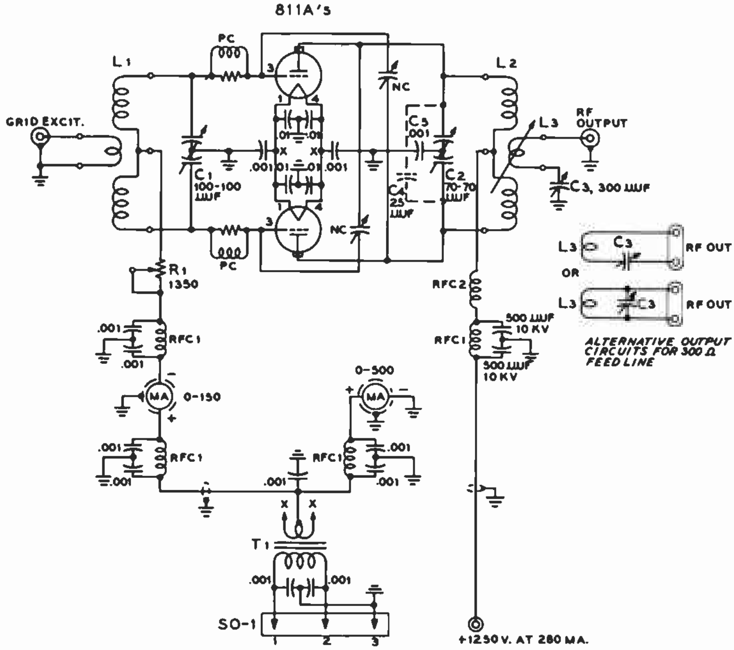


Figure 4
SCHEMATIC OF THE 811-A POWER AMPLIFIER

C_1—100-100 $\mu\mu$fd., National STHD-100
C_2—70-70 $\mu\mu$fd., 4500 volts, Johnson 70ED45
C_3—300 $\mu\mu$fd., Bud MC-1860. One corner of a rotor plate of C_3 is bent so that C_3 shorts itself out at full capacity.
C_4—25 $\mu\mu$fd., Bud FA-778 (80 meters only)
C_5—Two 500 $\mu\mu$fd., 10K volt TV type
R_1—2000-ohm, 50-watt resistor with slider
RFC_1—4 μh., National R-60
RFC_2—1 mh., National R-154U
L_1—B&W JCL series coils
L_2,L_3—B&W TVL series coils
NC—National NC-800 disc type capacitors
T_1—6.3 volts at 10 amp. Stancor P-6308
PC—50-ohm, 2-watt resistor wound with 4 T no. 18 enam.
SO_1—Amphenol 86CP4 plug, 4 prong
All .001-μfd. capacitors Centralab type DD-102
All .01-μfd. capacitors Centralab type DD-1032
Erie type 327 (.001 μfd.) feedthrough capacitors used on each filament lead

Meter shields are cut from the end of a "tin can" measuring three inches in diameter. The open edge of the can is fluted with tin snips and bent out to form a spring fit to the chassis edge. The meter shields are held in position by the meter studs and nuts. Construction of these shields is shown in Chapter 15. A 6" x 12" opening is cut in the top enclosure plate directly above the amplifier tubes. The grid and plate coils of the amplifier may be changed through this access hole. During operation of the amplifier, the hole is covered by a piece of Reynolds perforated aluminum stock.

The amplifier is designed to mount in the top section of a standard 19" rack-cabinet, such as the Bud CR-1745. This cabinet has a hinged door in the top which aligns with the opening in the top of the amplifier enclosure. When the hinged door is opened, access may be had to the interior of the enclosure for the purpose of changing coils.

Filament pins 1 and 4 of each 811-A socket are bypassed to ground by means of .01-μfd. ceramic capacitors. The filament leads for each tube socket, in addition, pass through Erie type 327 feedthrough ceramic capacitors (.001

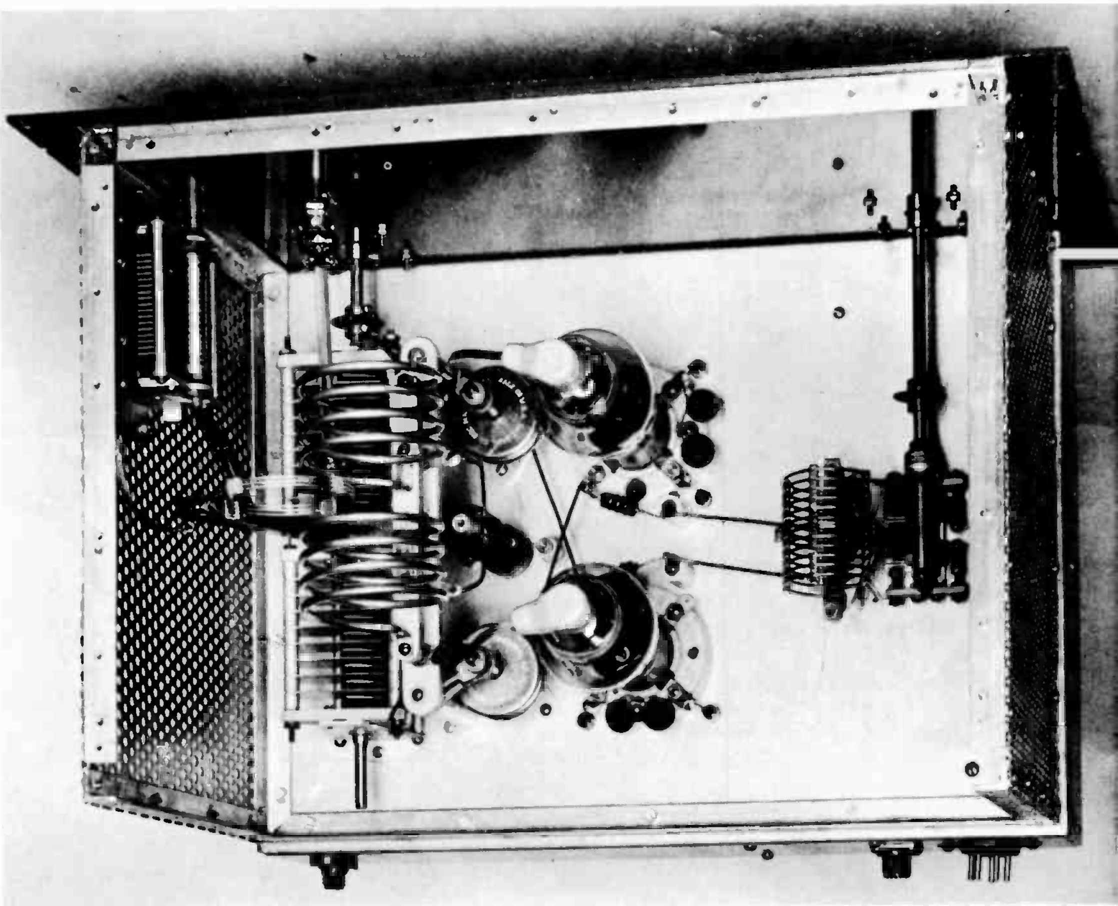


Figure 5

TOP VIEW OF 350-WATT AMPLIFIER

The antenna circuit tuning capacitor is to the top left of the front panel. One corner of a rotor plate of this capacitor is bent so that the capacitor shorts itself out at maximum capacitance, since occasions arise when this capacitor is not required in the circuit. The panel control to the right of the antenna tuning capacitor is the swinging link drive. The plate circuit r-f choke is mounted directly on the top post of a 500-μμfd. TV type ceramic bypass capacitor.

μfd.) into the area below the chassis where the filament transformer T_1 is located (figure 6).

TV-type 500-μμfd., 10,000-volt ceramic capacitors are used as by-pass capacitors in the high voltage lead in conjunction with a v-h-f choke. The high voltage lead from this harmonic filter to the high voltage terminal is made of a short length of RG-59/U coaxial cable.

The plate circuit tuning capacitor C_2 is driven from the panel through an insulated coupling, and is mounted to the chassis on 1/2" ceramic insulators. Each end of the frame of the capacitor is by-passed to ground by means of a 500-μμfd., 10,000-volt TV-type ceramic capacitor (C_5). If the amplifier is operated at a maximum plate voltage of 1000 instead of 1250, the plate tuning capacitor C_2 may be mounted directly to the metal chassis and the

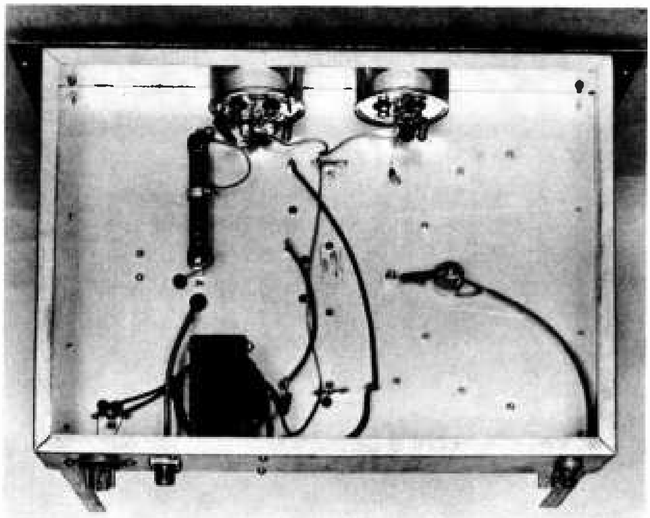


Figure 6

SIMPLICITY OF WIRING MAY BE OBSERVED IN THE UNDER CHASSIS VIEW OF THE 811-A AMPLIFIER

The filament transformer for the amplifier tubes is mounted to the rear wall of the chassis, as are the input and output coaxial plugs, and the power connector. The two meters are covered by shield cans, and the TVI filter components for these circuits are mounted on the back of the cans. The variable grid resistor is directly behind the left-hand meter.

two capacitors making up C_5 may be eliminated.

Small parasitic chokes are placed in each lead from the grids of the 811-A tubes to the grid network, C_1-L_1. These chokes are supported between the grid terminals of the 811-A sockets and two one inch ceramic insulators mounted adjacent to the tube sockets. The operation of the amplifier is completely stable under all conditions up to plate potentials of 2500 volts when these chokes are employed.

The variable link of the Barker and Williamson TVL series plate coils is driven from the front panel by means of two Millen 39005 universal coupling joints and a short length of 1/4" phenolic shafting. The link tuning control C_3 is also located on the front panel above and to the right of the main tuning capacitor C_2.

Amplifier Adjustment After the amplifier has been wired and checked, the tubes should be inserted in their sockets and the filaments turned on. Excitation should be applied to the stage, and C_1 resonated until the grid meter indicates approximately 50 milliamperes of rectified grid current. The amplifier should next be neutralized according to the procedure given in Chapter 11, Section 6.

If a 52-ohm or 72-ohm coaxial feed system is employed, the coaxial line may be coupled directly to the coaxial output jack mounted atop the amplifier enclosure. Capacitor C_3 should be adjusted for maximum loading at the minimum amount of coupling possible between L_2 and L_3. The coaxial output receptacle may be removed and replaced with a two terminal connector if a 300-ohm feed system is to be employed. The rotor of C_3 should then be ungrounded and attached to the free terminal of the connector. In some instances, C_3 should be connected across L_3 instead of in series with the link when a 300-ohm feed system is used. The amplifier may be run at a maximum input of 1250 volts and 280 milliamperes (350 watts) for phone, and 1250 volts and 360 milliamperes (450 watts) for c.w. Grid current, in either case should be 90 milliamperes. This amplifier is shown with a companion modulator and power unit in Chapter 28.

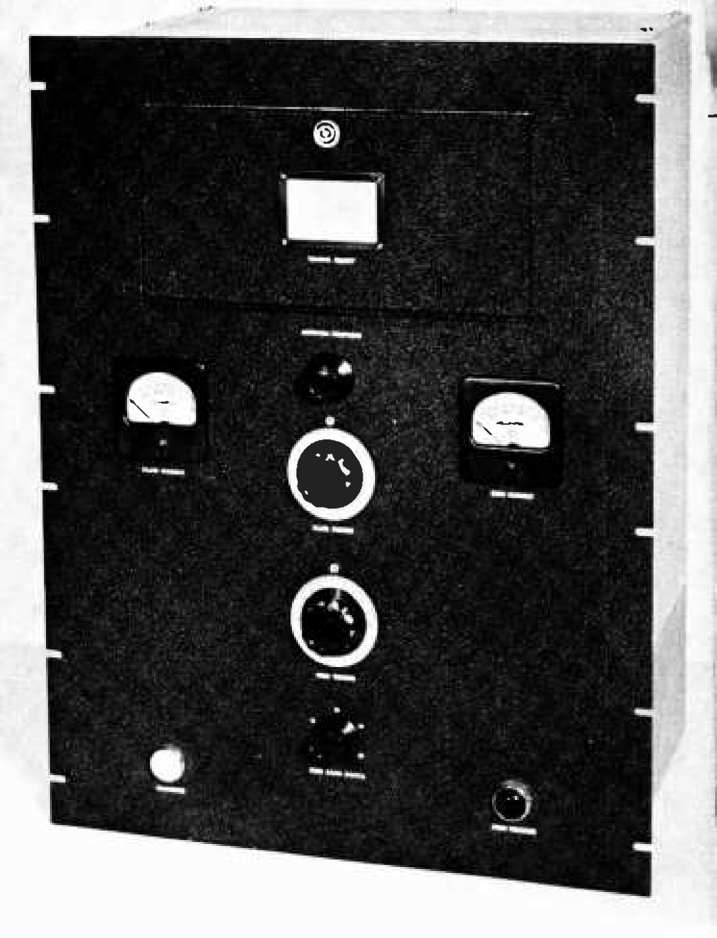


Figure 7
A PUSH-PULL 1-KILOWATT TRIODE AMPLIFIER STAGE
Employing either 8000, 810, 806 or 250-TH triodes, this amplifier is capable of 1-kilowatt operation on all amateur bands from 80 to 10 meters, inclusive.

26-4 Push-Pull Kilowatt Triode Amplifier

The amplifier illustrated in figures 7 through 12 is an excellent example of the style of equipment that may be built if the services of a machine shop are at hand. Special machine work and fittings make this unit an outstanding assembly.

Covering all amateur bands between 80 meters and 10 meters, this amplifier is designed to work with either 810, 8000, 806 or 250TH type tubes. Type 250TH or 806 tubes are recommended if the amplifier is to be employed to a great extent on 10 meters. The extremely low inter-electrode capacities of these tubes allow efficient tank circuits at this high frequency. Type 8000 tubes will also perform well on the 10 meter band, although their inter-electrode capacities are markedly higher.

The amplifier is designed for operation at a plate potential of 2500 volts and a plate current of 400 milliamperes. The type 810 and 8000 tubes may be operated at 2000 volts and a plate current of 500 milliamperes for a 1-kilowatt plate input.

Amplifier Circuit A front view of the amplifier is shown in figure 7 and the schematic is shown in figure 8. A 100-watt Barker & Williamson type BCL turret is employed in the grid circuit of the amplifier, and 1-kilowatt heavy duty plug-in coils are employed in the plate circuit. On 80 meters, the plate circuit of the amplifier is padded with a 12 $\mu\mu$fd. vacuum capacitor to obtain the correct L/C ratio on this band. A separate bias supply (figure 12) is employed with this amplifier and is mounted on a chassis directly below the amplifier in the relay rack.

For flash-over protection, the rotor of the plate tuning capacitor, C_2, is insulated from ground and is returned to the center tap of the plate coil, L_2, through a 35,000-ohm, 2-watt resistor. The rotor of C_2 is driven through a high-voltage insulated coupling.

Small parasitic chokes are included in the leads to the grid tank circuit to suppress v-h-f

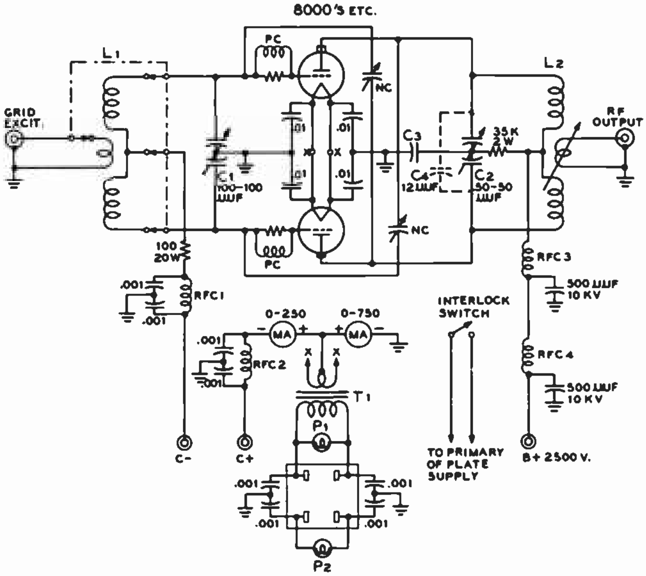


Figure 8

SCHEMATIC OF PUSH-PULL 1-KILOWATT TRIODE AMPLIFIER

C_1—100-100 $\mu\mu$fd. split stator Johnson 100FD20
C_2—50-50 $\mu\mu$fd. 9000 volt Johnson 50DD90
C_3—2000 $\mu\mu$fd. 10,000 volt. Four 500 $\mu\mu$fd. TV type ceramic capacitors in parallel
C_4—12 $\mu\mu$fd. 20,000 volt fixed vacuum capacitor Jennings type VC (80 meters)
RFC_1,RFC_2,RFC_4—4 μh. National R-60
RFC_3—1.9 mh. Johnson 102-754
PC—50 ohm 2 watt resistor, wound with 4 t. no. 18 enam.
NC—10 $\mu\mu$fd. Johnson type N-250
T_1—10 volts at 10 amp. Chicago F-1010. For 250-TH tubes: 5 volts at 20 amp. Chicago F-516
P_1—110 volt pilot lamp, green
P_2—110 volt pilot lamp, red
L_1—B&W BCL turret, modified as per Table I
L_2—1000 watt plug-in inductors. See Table I
All .001 μfd. capacitors Centralab DD-102
All .01 μfd. capacitors Centralab DD-1032

parasitic oscillations which usually occur in push-pull amplifier stages.

The grid turret must be modified as shown in Table 1 to resonate with the proper amount of capacitance in the 10, 15 and 20 meter bands. The use of a high-C grid tank circuit greatly simplifies the problem of coupling driving power to the amplifier on the higher frequency bands through a random length of 52 ohm coaxial line.

Amplifier Construction The amplifier is built upon a 13" x 17" x 5" cadmium plated steel chassis (California Chassis Co., 5445 Century Blvd., Lynwood, Calif.). Centered atop this chassis is a second cadmium plated steel chassis measuring 13" x 5" x 3". The axis of this second chassis is at right angles to the front panel of the amplifier. Grid tuning capacitor C_1 is located within this smaller chassis, bolted upside down to the top of the chassis. A cutout is made in the main amplifier chassis, matching the opening in the bottom of the smaller unit as shown in figure 11. The grid turret sits astride this cutout, mounted on two small aluminum brackets. The turret is oriented so that the 10-meter coil drops into the cutout area. Also located within the cutout is the plate r-f choke, RFC_3 (figure 11).

The panel of the amplifier is made from a single sheet of duraluminum and measures 19" wide by 24½" high. A door measuring 6" x 12" is cut in the top of the panel, the top of the door being 2" below the upper edge of the panel. A short section of piano hinge is riv-

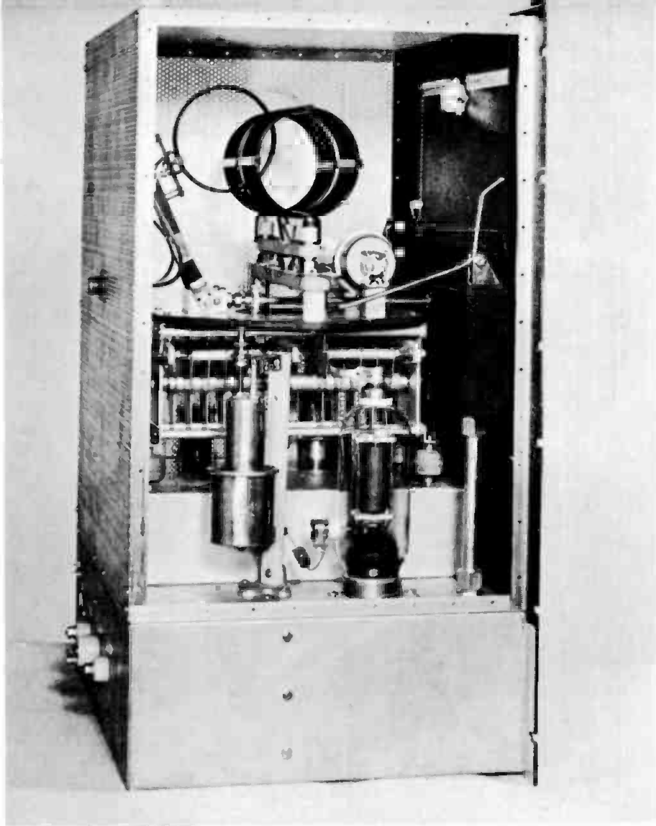


Figure 9
TOP RIGHT-HAND VIEW OF AMPLIFIER

The shorting rod which grounds the plate circuit of the amplifier when the panel door is opened may be seen in the foreground. A grid parasitic choke is visible next to the grid terminal of the 8000 tube.

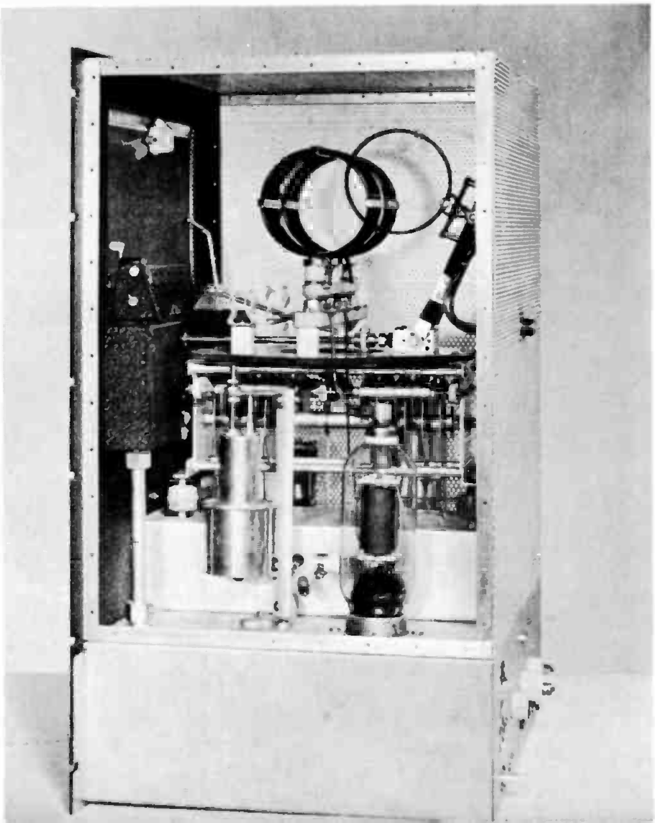


Figure 10
TOP LEFT-HAND VIEW OF AMPLIFIER

The plate tuning capacitor is supported by four TV type ceramic capacitors, and is driven through an insulated shaft coupling. Above the shielded meter box is located the protective micro-switch which opens the primary power circuits when the panel door is not closed tightly. The swinging link circuit is panel driven by a right-angle coupling and extension shaft.

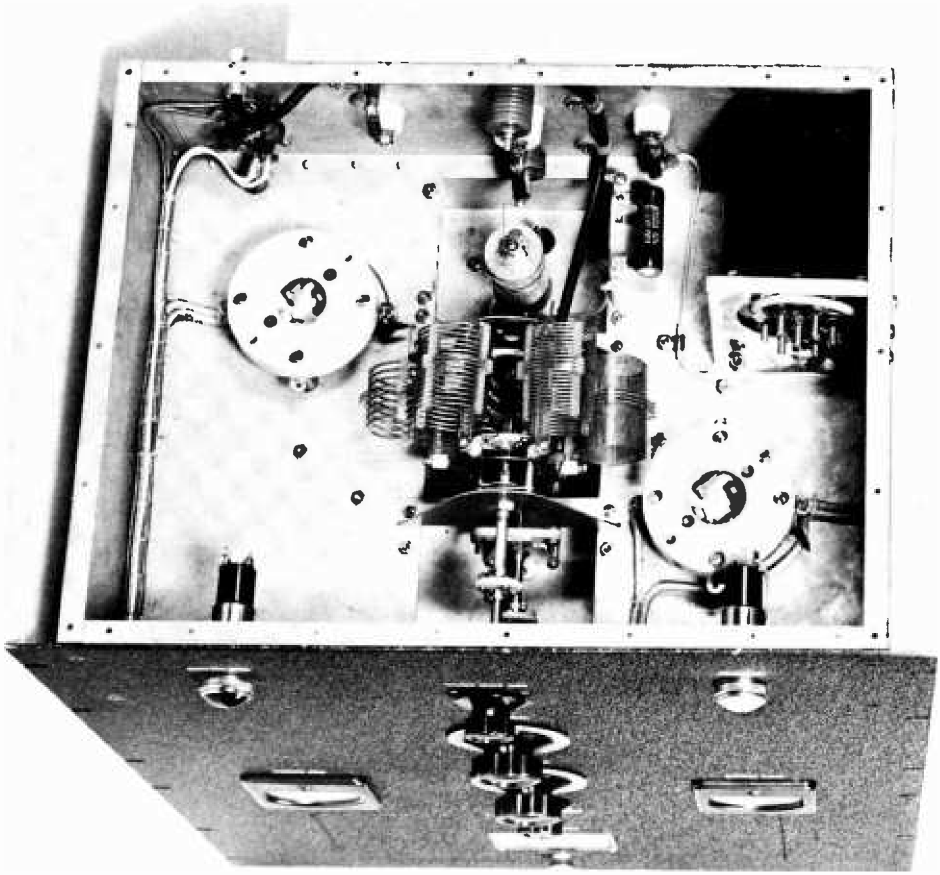


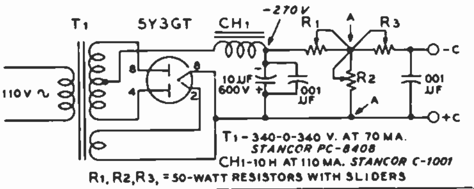
Figure 11

UNDER CHASSIS VIEW OF 1-KILOWATT TRIODE AMPLIFIER

The grid circuit tuning capacitor and plate circuit r-f choke are contained in the below chassis enclosure formed by a small chassis mounted at right angles to the front panel. The bandswitch coil assembly for the grid circuit is mounted on two brackets above this cutout. A metal screen attached to the bottom of the amplifier completes the TVI proof enclosure.

eted to the panel and to the door to form a joint. The edges of the door are lined with Eimac finger stock to prevent harmonic leakage through the cracks. The two three-inch panel meters are mounted above the chassis on the main panel, and are shielded by enclosing them in 4" x 4" x 2" utility boxes (Bud AU-1083). The leads to the meters are run from the under-chassis area in short lengths of copper tubing, the ends of which are affixed with automobile gas line couplings to the meter enclosures and to the chassis.

The plate circuit tuning capacitor, C_2, is mounted atop the grid box. It is fastened to the grid box by using four TV-type 500 $\mu\mu$fd., 20,000 volt ceramic capacitors as combination standoff insulators and blocking capacitors. The total value of C_3, therefore, is the sum capacity of these units, or 2000 $\mu\mu$fd. On each side of the plate tuning capacitor are located one amplifier tube and one neutralizing capacitor. The tube sockets are recessed in the chassis so that the top of the socket shell projects 1/2" above the chassis. On the right side



PROTECTIVE BIAS (VOLTS AT A-A)	TUBES	R1 (Ω)	R2 (Ω)	R3 (Ω)	GRID CUR. (MA.)	OPERATING BIAS (VOLTS)
-155	8000	2300	3100	2200	70	-370
-80	810	3800	1600	900	140	-350
-210	806	1200	4200	3300	80	-600
-80	250TH	3800	1600	900	100	-250

TABLE I - PLATE COILS

HDVL = BARKER & WILLIAMSON LCS = JOHNSON

TUBES	PLATE CKT. CMAX-CMIN	80M	40M	20M	15M	10M
810'S	41-24	[illegible] + 12 µµF [illegible]	40HDVL	[illegible]CS20 1/2 TURN OFF [illegible]	15HDVL 1 TURN OFF [illegible]	—
8000'S	37-20	80HDVL + 12 µµF [illegible]	40HDVL	1000LCS20 1/2 [illegible] EACH END [illegible]	15HDVL 1/2 TURN OFF [illegible]	10HDVL 1/2 TURN OFF [illegible]
250TH'S 808'S	33-16	80HDVL + 12 µµF VACUUM PADDER	1000HCS40	1000LCS20	1000LCS14	10HDVL 1/2 TURN OFF EACH END JUMPER CENTER PLUGS

GRID TURRET MODIFICATIONS

10 METERS - REMOVE COIL. REPLACE WITH NEW COIL, 4 T. # 12 E. 1 3/4" LONG, 1" I.D., CENTER-TAPPED. LINK IS 2 TURNS #14 INSULATED, 1 3/8" DIA. WOUND ON TOP CENTER OF GRID COIL.

15 METERS - REMOVE 2 TURNS FROM EACH END OF COIL.

20 METERS - REMOVE 2 TURNS FROM EACH END OF COIL.

Figure 12

BIAS SUPPLY AND COIL TABLE FOR KILOWATT AMPLIFIER

of the amplifier (facing it from the rear) the tube socket is nearest the panel (figure 9), and the neutralizing capacitor is directly behind it. On the left side of the amplifier the neutralizing capacitor is nearest the panel (figure 10) with the tube directly behind it. This layout transposition results in very short neutralizing leads since the connections may be made through the stator plates of C_2.

Mounted atop C_2 is a hexagonal piece of 1/4" micarta, cut from a square 11" on one side. The jack bar for L_2 is mounted to this plate, as are the two heavy-duty fuse clips that hold the 80 meter padding capacitor, C_4. The variable link is attached by a special bracket to a Millen 10012 right angle drive unit which allows panel control of the coupling between the plate coil and the pickup link.

Mounted atop one meter shield is a micro-switch that is actuated when the panel door is opened. The switch is connected so as to break the primary of the plate supply during the coil changing process. Atop the other meter shield is a spring-loaded shorting switch made of a length of 1/4" shafting. When the door opens this switch shorts one end of the plate tank circuit to ground as a precautionary measure.

Amplifier Wiring All low voltage d-c leads and the filament leads are run in shielded loom, the shielding being grounded at both ends of the leads. Connections are made to the tube caps by short pieces of flexible braid, or 1/4" copper strip. The leads from the output link to the coaxial receptacle mounted on the rear screen are made of flexible braid, run in lengths of neoprene tubing.

Plate Coil Adjustment Table 1 lists the ratio of maximum to minimum tank circuit capacity when various tubes are used in the amplifier. In each case, it is necessary to pad the 80-meter coil with a fixed vacuum capacitor to establish resonance. On 40 meters, the low-C 250TH or 806 type tubes require the use of a Johnson HCS inductor, as the Barker & Williamson 40-HDVL coils will not resonate to frequency when low-C tubes are used without additional padding capacity. On 20 meters, Johnson LCS type coils are used, 1/2 turn being removed from each end if either 810 or 8000 type tubes are employed in the amplifier. The simplest way to make this modification is to reduce the outer turn on each end of the inductor to one-half the diameter of the other turns. Additional modifications must be made to the 15 and 10 meter coils, as shown in Table 1.

26-5 Push-Pull 250TH Amplifier

A simplified version of the kilowatt amplifier of section 4 is illustrated in figures 13 to 16. This construction requires no extensive metal work and may easily be duplicated in the home workshop.

Two low capacity 250TH triodes are used in this amplifier. It is designed to work at 1-kilowatt input at 3000 volts for c.w., and 2500 volts for phone on all amateur bands between 10 meters and 80 meters. For 80-meter operation, the plate tank circuit is padded with a 20-µµfd. vacuum capacitor to maintain optimum L/C ratio.

Amplifier Layout The amplifier is built upon a 17" x 13" x 4" aluminum chassis (Bud AC-428) and uses a second aluminum chassis 17" x 13" x 2" (Bud AC-419) mounted upside down beneath the first to complete the grid circuit enclosure. The panel of the unit is 22¾" high and is made of two separate panels: a 12¼" panel having a hinged door (Bud PS-815), and a 10½" panel. The two panels are held together by the aluminum angle

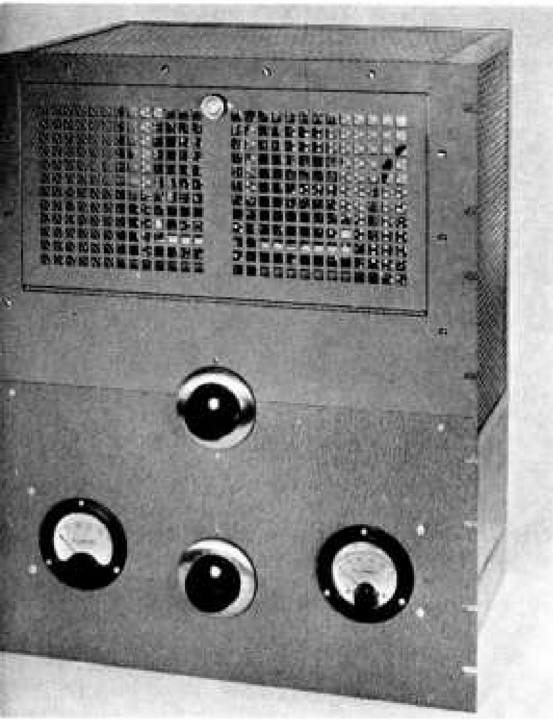
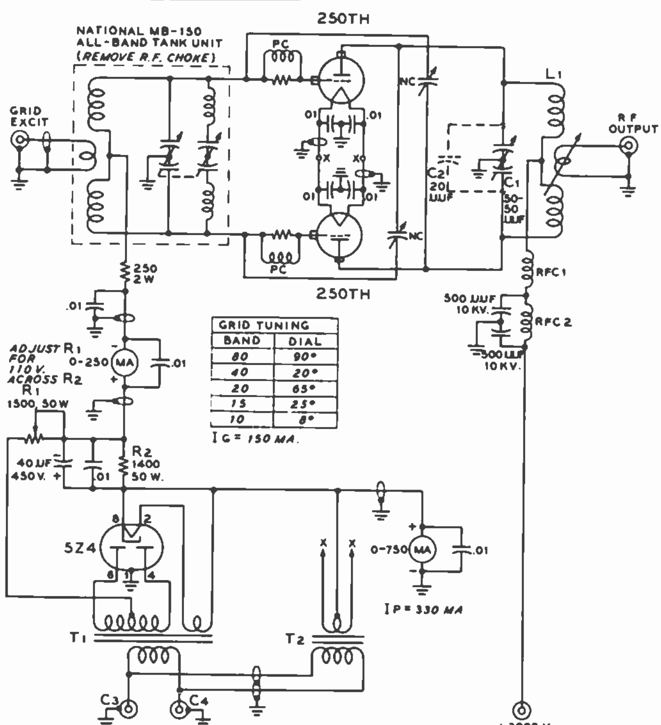


Figure 13
PUSH-PULL 250-TH AMPLIFIER
The plate coils of the amplifier may be changed through the door in the top section of the front panel

Figure 14
SCHEMATIC OF PUSH-PULL 250-TH AMPLIFIER

C_1—50-50 $\mu\mu$fd. Johnson 50CD110
C_2—20 $\mu\mu$fd. fixed vacuum capacitor Jennings type VC (80 meters)
C_3,C_4—0.1 μfd. Sprague Hy-pass capacitor 80P3
L_1—1 kw. B&W HDVL coils. Use Johnson 1000 HCS-40 coil for 40-meter operation, Johnson 1000 HCS-20 for 20-meter operation
RFC_1—1 mh. National R-154 or Johnson 102-752
RFC_2—4 μh. National R-60
T_1—250-0-250 volts at 70 ma. Stancor PC-8403
T_2—5 volts at 20 amp. Chicago FV-520H
NC—5 $\mu\mu$fd. disc type capacitor Millen 15011
PC—50 ohm 2 watt resistor, wound with 4 t. no. 18 enam.
All .01 μfd. capacitors Centralab D-1032 or equivalent



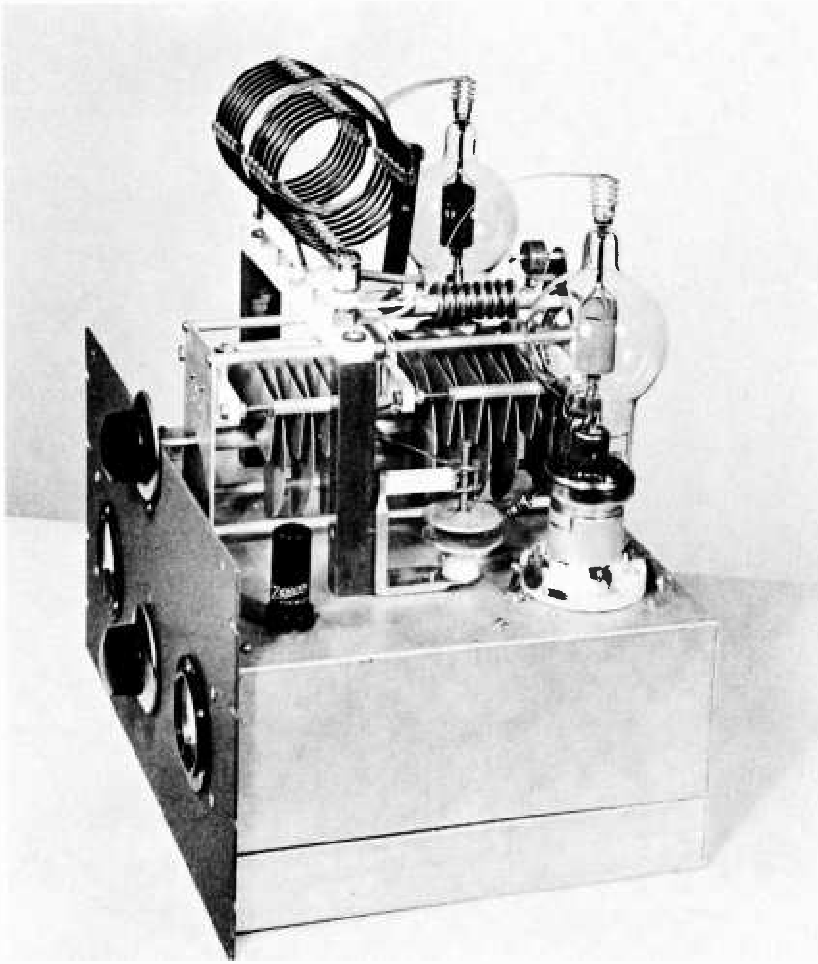


Figure 15

PUSH-PULL 250-TH AMPLIFIER WITH TVI SHIELD REMOVED

The phenolic mounting rod for the plate coil assembly is bolted to the frame of the neutralizing capacitor

strips that form the front part of the TVI-proof enclosure. The reader is referred to Chapter 30 for construction information concerning enclosures of this type.

An 11,000-volt spacing tuning capacitor, C_1, is mounted at right-angles to the front panel. Above this capacitor, the jack bar for the plate circuit inductors is mounted parallel to the front panel, supported on two phenolic posts 6½" high. These posts are rigidly braced by being bolted to the channel frame of the disc-type neutralizing capacitors (Millen 15011). The plate choke (RFC_1) is mounted in a horizontal position between an aluminum bracket affixed to the rear frame of C_1 and the jumper connecting the center coil jacks of L_1.

The grid circuit of the amplifier uses a National 150-watt all-band tank unit, shown in the under-chassis photograph figure 16. The grid bias return lead for the amplifier stage is

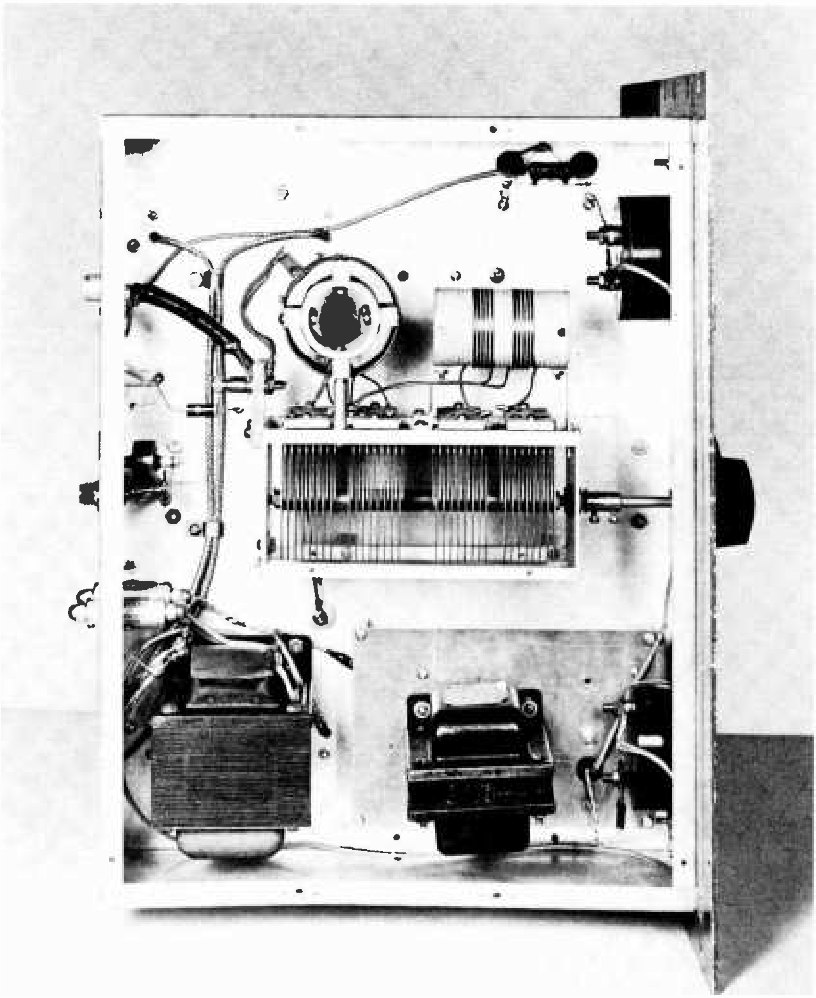


Figure 16

UNDER CHASSIS VIEW OF PUSH-PULL 250-TH AMPLIFIER

The bias supply and filament transformer are located at the bottom of the photo. The National MB-150 all-band tank unit is centered on the chassis and supported on metal pillars. All power wiring is run in shielded loom.

taken from the point on the assembly which serves as the plate connection when the tank is used in the plate circuit of an amplifier. The frame of the MB-150 tank assembly should be grounded to the amplifier chassis, and the r-f choke must be removed from the circuit, since the MB-150 is designed to operate with the frame of the unit "above ground."

The plate and neutralizing leads of the amplifier are made of 1/2" copper strap and other r-f leads are made with no. 12 wire. All d-c and filament leads below the chassis pass through braided loom, which is grounded at each end of the lead.

Bias Supply When the 250-TH tubes operate at a plate potential of 3000 volts, it is reasonable to assume the plate voltage will reach a value of 3500 volts when the plate power supply is lightly loaded. A cutoff bias of about 100 volts is required under these circumstances. A simple R-C filter bias pack is built on a small metal plate in one corner of the under-chassis compartment. The 5Z4 rectifier projects up through the chassis into the plate circuit compartment of the amplifier. A metal 5Z4 rectifier is used, with the shell grounded, preventing r-f pickup by the rectifier tube circuit. Normal grid current for both phone and c-w operation is 150 milliamperes with 210 volts of operating bias. Approximately 70 watts of driving power are required for either c-w or plate modulated operation of the amplifier at one kilowatt level.

26-6 Push-Pull 4X-150A Amplifier for the 144-Mc. Band

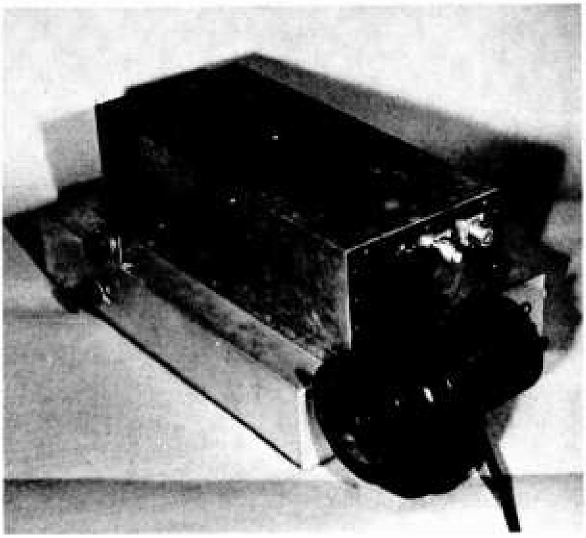
The design of amplifiers for very high frequency operation is, in general, much the same as for the lower frequency amateur bands. Greater attention must be paid to details of design, since at these higher frequencies the design of efficient electrical circuits becomes more subtle. Components having low lead inductance must be employed, and care must be taken to make sure that the circuit inductance remains where it belongs: in the grid and plate tank circuits.

Special v-h-f tubes have been produced during the past few years featuring low lead inductance and minimum electron transit time. Of these tubes, one of the most effective for general amateur use is the 4X-150A. An amplifier using a pair of 4X-150A tetrode tubes may be run at a plate modulated input of 400 watts in the 144-Mc. amateur band. The same tubes may be run at a plate voltage of 1250, delivering 200 peak watts as a linear amplifier. Under these conditions, the amplifier makes an excellent linear stage for either a SCR-522 transmitter or a Gonset "Communicator."

Circuit of the Linear Amplifier A general view of the push-pull 4X-150A 144-Mc. amplifier is shown in figure 17. This unit was designed and built by W6WV. It employs quarter-wave linear lines in both the plate and grid circuits. The plate lines are shown in figures 19 and 20, and the grid arrangement is shown in figure 21. The schematic of the amplifier is shown in figure 18.

The plate circuit of the 4X-150A amplifier is completely enclosed to reduce radiation loss from the plate lines. The grid circuit is mounted in the below-chassis enclosure, which is sealed and pressurized by a 115-volt 40-

Figure 17
PUSH-PULL 4X-150A TWO-METER AMPLIFIER



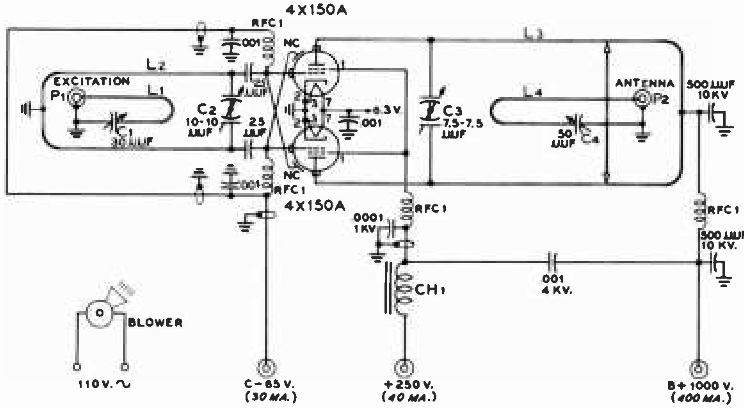


Figure 18
SCHEMATIC PUSH-PULL 4X-150A AMPLIFIER

C_1—30 μμfd. Bud LC-1642
C_2—10-10 μμfd. Bud LC-1664
C_3—7½-7½ μμfd. Hammarlund HFD-30X with alternate plates removed
C_4—50 μμfd. Bud LC-1644

L_1,L_2,L_3,L_4—See coil table, figure 22
RFC_1—4 μh. National R-60
CH_1—16 henry at 50 ma. Stancor C-1003
All .001 μfd. capacitors Centralab DD-102 or equivalent

watt blower. The air passes through the 4X-150A sockets into the plate circuit enclosure. Two ventilation holes are cut in the top of the plate circuit box to insure proper circulation of air. These holes are covered with copper screening to electrically seal the box.

Particular attention must be paid to the mounting of the 4X-150A tubes. Special sockets available from the manufacturer (Eimac 4X-150/4010) are used to simplify the cooling problem and to provide proper low-inductance screen connections. A built-in by-pass capacitor insures that the screen of the tubes is at ground potential when these special sockets are employed. No other screen by-pass capacitor is required.

A simple connection to the external anode of the 4X-150A tubes may be made from a 5 inch length of Eimac 17/32" finger stock. This pre-formed contact material is pressed tightly around the 4X-150A anode and wrapped with a length of no. 14 tinned copper wire. This

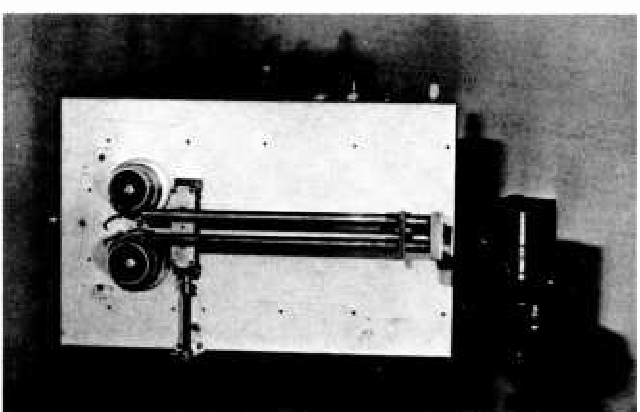


Figure 19
TOP VIEW OF 4X-150A TWO-METER AMPLIFIER

connector is then removed from the tube, and the wire is soldered to the finger stock.

The plate and grid circuits of this amplifier are resonant lines, tuned at the high-impedance end by small variable capacitors. The grid circuit is shunt fed, and the driving circuit is link coupled to the grid line. Power output from the plate line is also taken from a tuned link circuit.

Amplifier Assembly The amplifier is constructed upon an aluminum chassis 17"x 10" x 3" (Bud AC-416). The plate circuit box measures 6"x 16"x 4". This particular box was formed out of a piece of galvanized iron, obtained from a local sheet-metal shop. Dimensions of the grid and plate linear tank circuits are given in figure 22.

The coaxial input plug P_1 and the excitation link resonating capacitor C_1 are mounted on the wall of the chassis directly next to the grid line L_2. The coaxial output plug P_2 and the output link resonating capacitor C_4 are mounted on the wall of the plate circuit box nearest the far end of the plate line, as shown in figure 20. A threaded phenolic shaft passes through the top of the plate circuit box to which a tuning knob is attached. The shaft turns in a threaded bushing mounted in the top of the box, and presses against pickup link L_4. By turning the knob it is possible to vary the spacing between L_4 and L_3 until optimum coupling conditions are reached.

The plate circuit capacitor is mounted upside down beneath the plate rods, and is supported at each end by a short length of bakelite strip which is attached to the chassis. The grid capacitor C_2 is mounted upon two short ceramic insulators, and is attached to the grid circuit as shown in figure 21.

A minor amount of circuit instability, noticed only when the amplifier was run in class AB_1 linear condition was cured by neutralizing the tubes. Two sub-miniature chassis-type feedthrough bushings are mounted adjacent to the plate of each 4X-150A tube. These bushings are cross-connected beneath the chassis to the grid terminal of each tube. A length of wire about 3/4" long is soldered to the top side of each bushing, and the spacing between each wire and rhe plate of the adjacent 4X-150A is varied until there is no change in grid current when the plate circuit of the amplifier stage is tuned through resonance. No plate or screen voltage is applied to the amplifier for this test.

Amplifier Adjustment For Class C operation, the amplifier may be operated under the voltage and current conditions set forth in the instruction sheet of the 4X-150A. Maximum input under plare modulated conditions is 400 watts. The following steps should be taken for adjustment of the amplifier as a class AB_1 linear amplifier:

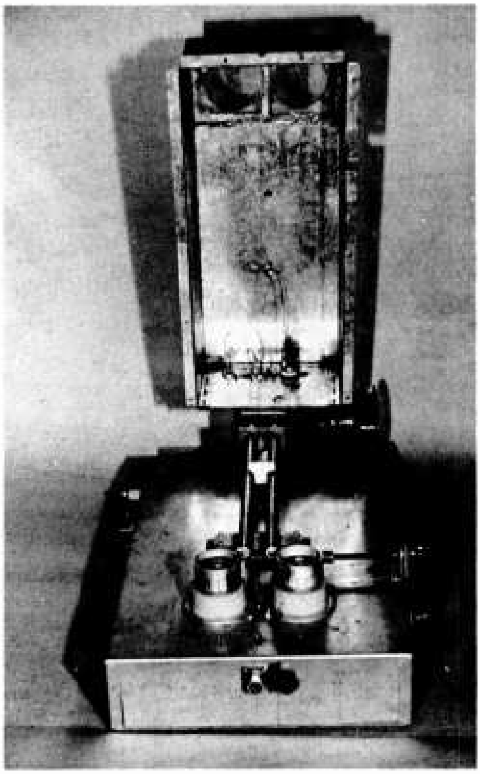


Figure 20

4X-150A AMPLIFIER WITH PLATE SHIELD OPEN, SHOWING LINEAR TANK ARRANGEMENT

1. The amplifier is operated at a plate potential of 1250 volts, and a screen potential of 350 volts. The grid bias of the tubes is adjusted until the amplifier plate current is 100 milliamperes, with no input signal.
2. Excitation is applied to the amplifier and the coupling to the grid circuit and the coupling to the antenna circuit are adjusted until the grids are driven to the point where grid current barely begins to flow (about 0.2 ma.). The plate coupling is now adjusted until 30 ma. of screen current is drawn by the amplifier. Plate current will be 500 ma.
3. The coupling and excitation to the grid circuit is now reduced until the d-c plate

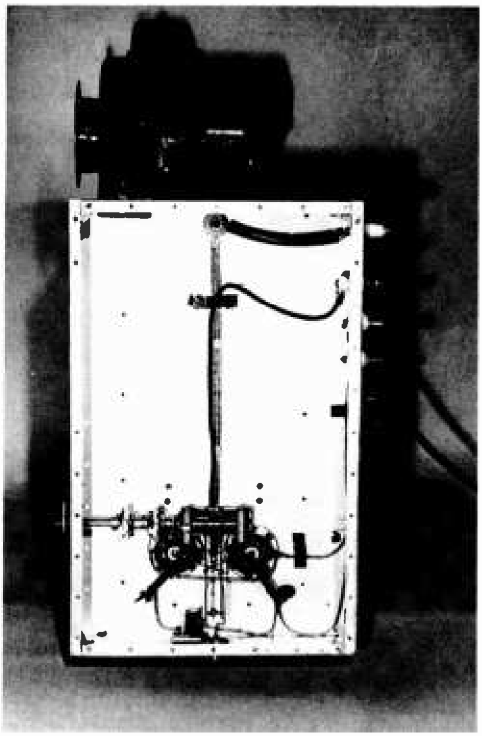


Figure 21
BOTTOM VIEW OF PUSH-PULL 4X-150A AMPLIFIER

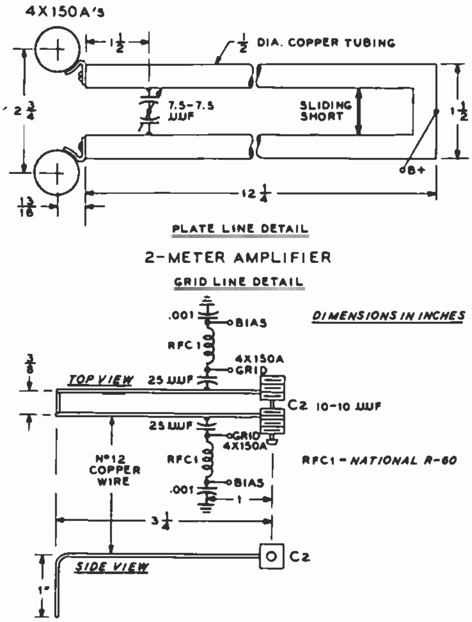


Figure 22
GRID AND PLATE LINE DETAIL OF 4X-150A TWO-METER AMPLIFIER

current drops to 0.55 of the plate current obtained in step 2, above.

4. Specific operating conditions for the unit, operating as a linear amplifier for a Gonset "Communicator" are:

D-C Plate Voltage	1250
D-C Screen Voltage	350
Zero-Signal Plate Current	100 ma.
Carrier Plate Current	275 ma.
Peak Modulated Plate Current	500 ma.
Screen Current	0-30 ma.
Carrier Output	50 watts
Peak Power Output	200 watts

26-7 A Push-Pull 813 Amplifier

One of the most popular and rugged tubes available to the radio amateur today is the 813. Two of these tubes, operating under ICAS ratings in c-w service can run one kilowatt input at a plate voltage of only 2250. With 2000 volts on the plates, the push-pull 813 amplifier can run a maximum input of 800 watts, plate modulated.

Many amateurs have had bad luck with these tubes and have been plagued with parasitics and spurious oscillations. It must be remembered with high gain tubes such as the 813 almost full output can be obtained with practically zero grid excitation. Any minute amount of energy fed back from the plate circuit to the grid circuit can cause instability or oscillation. *Unless suitable precautions are incorporated in the electrical and mechanical design of the amplifier, this energy feedback will inevitably occur.*

Fortunately these precautions are simple. The grid and filament circuits must be isolated from the plate circuit. This is done by placing these circuits in an "electrically tight" box. All leads departing from this box are by-passed and filtered so that no r-f energy can pass along the leads into the box. This restricts the energy leakage path between the plate and grid circuits to the residual plate-to-grid capacity

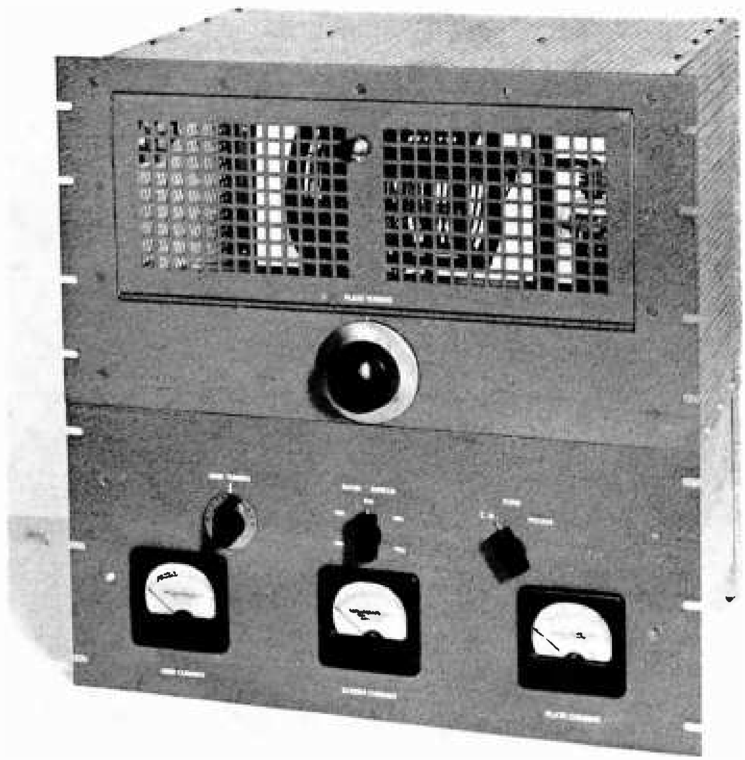


Figure 23
PUSH-PULL 813 AMPLIFIER
A TVI proof enclosure allows kilowatt operation of this amplifier from 10 to 80 meters, even in regions of weak TV signals. The complete absence of parasitics aids in reducing TVI producing harmonics to a minimum.

of the 813 tubes. This capacity is of the order of 0.25 $\mu\mu$fd. per tube, and under normal conditions is sufficient to produce a highly regenerative condition in the amplifier. Whether or not the amplifier will actually break into oscillation is dependent upon circuit losses and residual lead inductance of the stage. Suffice to say that unless the tubes are actually neutralized a condition exists that will lead to circuit instability and oscillation under certain operating conditions. With luck, and a heavily loaded plate circuit, one might be able to use an un-neutralized push-pull 813 amplifier stage and suffer no ill effects from the residual grid-plate feedback of the tubes. In fact, a minute amount of external feedback in the power leads to the amplifier may just (by chance) cancel out the inherent feedback of the amplifier circuit. Such a condition, however, results in an amplifier that is not "reproducable." There is no guarantee that a duplicate amplifier will perform in the same, stable manner. This is the one, great reason that many amateurs having built a tetrode amplifier that "looks just like the one in the book" find out to their sorrow that it does not "work like the one in the book."

This borderline situation can easily be over-

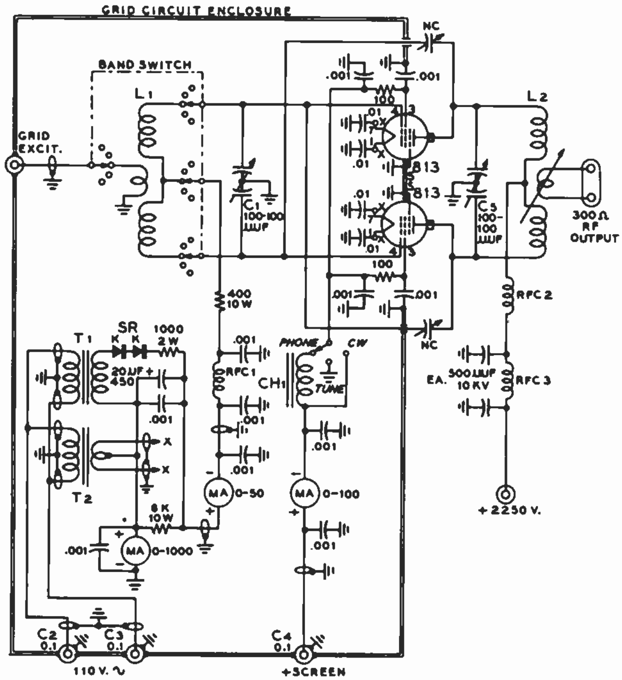


Figure 24

SCHEMATIC OF PUSH-PULL 813 AMPLIFIER

C_1—100-100 μμfd. Johnson 100LD15
C_2,C_3,C_4—0.1 μfd. Sprague 80P3 Hypass
C_5—100-100 μμfd., 9000 v. Johnson 100DD90
L_1—B&W BTCL turret, 35 watt. Remove 1 t. from each end of 10, 15 and 20 meter coils.
L_2—B&W series 3400 (BC-610) coils. Remove 1/2 t. from each end of 10 and 15 meter coil. Minimum tank circuit capacity is approximately 25 μμfd.
RFC_1,RFC_3—4 μhy. National R-60
RFC_2—1 mhy. National R-154
CH_1—8 hy. 85 ma. Chicago R-885 or Triad C-7X
T_1—125 v. 50 ma. Stancor PA-8421
T_2—10 v. 10 a. Chicago FV-1010 or Thordarson 21F-19
SR—Two 50 ma. "replacement type" selenium rectifiers connected in series
NC—3/4" x 1 3/4" aluminum tab, mounted about 1" away from tube env.
All .001 μfd. capacitors Centralab DD-102
All .01 μfd. capacitors Centralab DD-1032

come by the simple process of neutralizing the high-gain tetrode tubes. Once this is done, and the amplifier is tested for parasitic oscillations (and the oscillations eliminated if they occur) the tetrode amplifier will perform in an excellent manner on all bands. In a word, it will be "reproducable."

As a summation, three requirements must be met for proper operation of tetrode tubes—whether in a push-pull or parallel mode:

1. Complete isolation must be achieved between the grid and plate circuits.
2. The tubes must be neutralized.
3. The circuit must be parasitic-free.

The Amplifier Circuit Shown in figure 24 is the schematic of a stable push-pull 813 power amplifier. All components within the heavy box lines are mounted below the chassis deck in the "electrically tight" grid box. The 110-volt leads and the screen supply lead that leave this area pass through the box wall via three Sprague type 80P3 Hypass capacitors, which provide excellent lead isolation. The grid, screen and plate current meters are mounted on the front of this box. It was felt that it might be necessary to shield the meter cases to prevent an r-f path

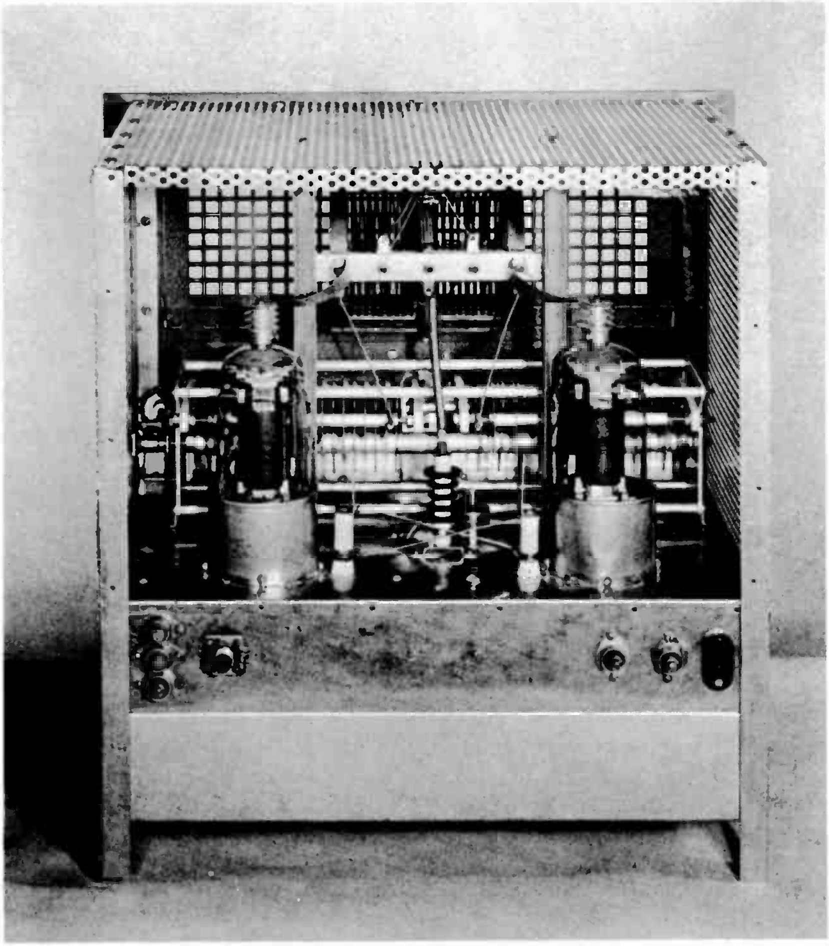


Figure 25

REAR VIEW OF THE PUSH-PULL 813 AMPLIFIER

The two neutralizing plates are mounted between and adjacent to the 813 tubes. The gear drive for the plate tuning capacitor may be seen at the left of the capacitor.

between the inside and outside of the box, but this precaution was not necessary.

All low voltage d-c wiring is made with shielded leads. This is done, since it is very easy for a power lead to have an unknown loop resonance at some frequency of operation of the amplifier. Belden 8652 shielded wire may be used for all low voltage leads except the filament circuit. A heavier wire, such as Belden 8650 should be used for these low voltage, high current leads. The outer braid of each lead should be grounded at each end of the wire.

A small protective bias supply is built into the below-chassis compartment of the amplifier. This supply protects the tubes in case of excitation failure, and permits the exciter to be keyed for c-w operation. A simple half-wave rectifier circuit is used, with a 50-milliampere selenium replacement-type rectifier stack and an R-C filter (figure 26).

A modified Barker & Williamson BTCL 35-watt bandswitching turret is employed in the grid circuit of the amplifier for coverage of all amateur bands from 10 to 80 meters. Barker & Williamson type 3400 series inductors (popu-

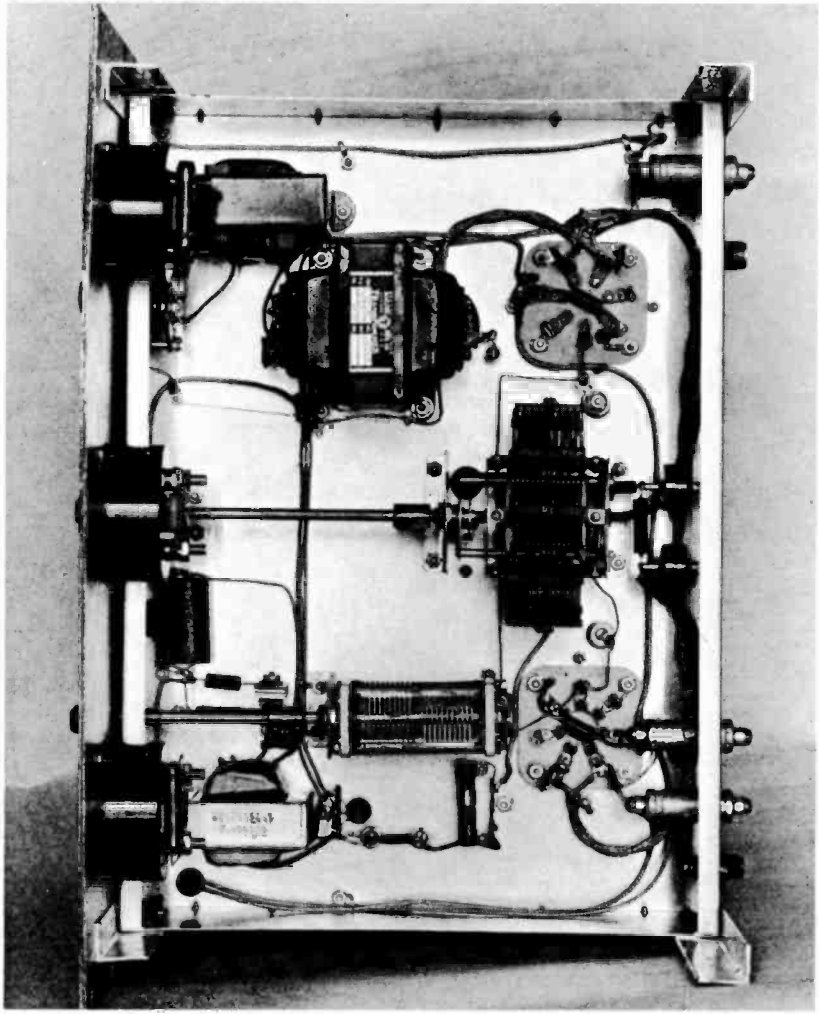


Figure 26

UNDER CHASSIS VIEW OF 813 AMPLIFIER

The screen choke and filament transformer are located at the top of the photograph. The bias transformer is at the bottom, between the grid tuning capacitor and the panel meter. All low voltage leads are run in shielded loom, each end of which is grounded to the chassis.

larly known as "BC-610" tank coils) are used in the plate circuit. A hinged door is located in the front panel, (figure 23) through which the plate inductors of the amplifier may be inserted and removed from the ceramic mounting bar. The usual method of removing plate coils is to grasp the windings of the coil and remove the coil from the mounting bar by a prying movement. The series 3400 coils have a pair of heavy phenolic end rings that protect the windings of the coil. These rings may be grasped to remove the coil, preventing eventual damage to the relatively fragile coil winding. If desired, the less expensive type TVL series inductors may be substituted for the 3400 series coils.

The plate tuning capacitor C_5 is mounted parallel to the front panel and is driven by means of a National RAD right-angle drive unit and a gear chain from the centrally located plate tuning control. A National type AMT capacitor having a right-angle center drive may be substituted for the one used in this amplifier and the built-up drive mechanism may be eliminated. The AMT capacitor, however, must be insulated from the chassis, since the maximum voltage breakdown of this unit is only 6000 volts. The frame of the AMT capacitor should be by-passed to ground at each end with a 500-$\mu\mu$fd., 10,000-volt TV-type ceramic capacitor.

For proper shielding of the 813 tubes, shield cans 2" high and 2½" in diameter surround the lower portion of the tubes. These shields are cut from "tin cans" and are given a coat of silver paint. They are each affixed to the chassis by four spade-bolts.

The plate coil of the amplifier is positioned with its mounting bar so placed that the mounting jacks are horizontal. Thus the coil is pulled toward the operator to remove it. The jack bar is mounted on two pieces of 1/2" x 1/2" square aluminum bar stock which run from the chassis up to the perforated metal sheet at the top of the screened compartment.

Mechanical Assembly The push-pull 813 amplifier foundation is based upon the use of a 10½" relay rack panel having a 6½" x 15" hinged door running horizontally across the panel (Bud PS-814). The plate inductors of the amplifier may be changed through this access door. If the mating surfaces of the door and the panel are free of paint, a fair bond between the two may be achieved, and the radiation of TVI producing harmonics will not be too severe in an area of strong TV signals. In a weak signal area it is necessary to place several wire jumpers across the door hinge and to line the edges of the opening with Eimac finger stock to produce a good ground between the door and the panel. This is simple to do, and will produce a "TV-tight" opening in the panel.

The panel height of the amplifier is 19¼". An 8¾" panel is placed below the 10½" panel to make the total height required. As seen in figure 25, the two panels are held together by means of two 18" lengths of Reynolds "Do-it-yourself" angle aluminum stock. The paint is removed from the rear of the panels where the angle-stock contacts the panel to provide good grounding between the panels and the rack frame. The horizontal crack between the panels requires two jumper bonds spaced equidistant between the two pieces of angle stock to prevent the crack from acting as a slot antenna for VHF harmonics. Assembly of the shielding is discussed in Chapter 30.

813 AMPLIFIER—OPERATING CHARACTERISTICS

ITEM	PHONE	CW
PLATE VOLTAGE	2000	2250
PLATE CURRENT	400 MA.	440 MA.
SCREEN CURRENT	60 MA	70 MA.
GRID CURRENT	32 MA.	30 MA.
SCREEN VOLTAGE	350	350
POWER INPUT	800 W	1000 W
PROTECTIVE BIAS	-85	-85
OPERATING BIAS	-180	-175

NOTE: FOR PROTECTION OF THE 813 TUBES, SCREEN VOLTAGE SHOULD BE OBTAINED FROM A 450-VOLT SUPPLY, THROUGH A 1250Ω, 25W. RESISTOR.

Figure 27

The amplifier is built upon an aluminum chassis measuring 12" x 17" x 3" (Bud AC-418). A second chassis is mounted upside down beneath the main chassis to act as the bottom section of the "electrically tight box" required by the grid circuitry. The four legs of the angle-stock aluminum frame extend below the main chassis, and it is to these legs that the lower chassis is fastened by means of no. 6 self-tapping screws. The front of this lower chassis is cut out to clear the three meters mounted on the lower section of the 8¾" panel.

Phone-C.W. Selection A single pole, three position switch S_1 in the screen lead of the 813 tubes serves as the "phone-tune-c.w." switch. In the tune position, the screen grids of the 813 tubes are grounded. The amplifier delivers enough output under this condition to establish resonance in the plate tank circuit and to permit preliminary tuneup without danger to the 813 tubes. In the c-w position of S_1 full screen voltage is applied to the screens of the 813 tubes. Screen voltage should never be applied to the amplifier unless the plate circuit is loaded and plate voltage is applied to the amplifier. It is easy to damage the screens of any tetrode tubes by excessive screen dissipation during loading adjustments. S_1 should be placed in the "tune" position at any time tuning adjustments are being made.

The screens of the 813 tubes are self-modulated for plate modulated phone operation when S_1 is set to the "phone" position. Screen voltage required by the amplifier is 350 volts. Operating voltages and currents for the amplifier are shown in figure 27.

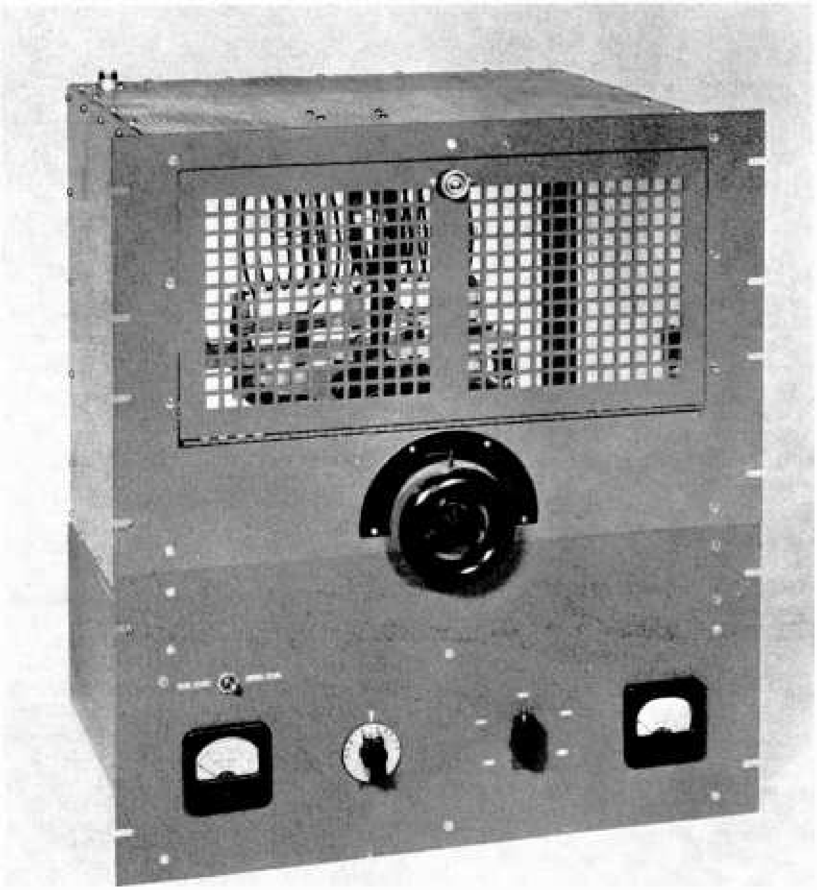


Figure 28

PUSH-PULL 4-250A AMPLIFIER

The plate circuit inductors may be changed through the hinged panel door. At lower left is the grid current-screen current meter with the selector switch above it. To the right is the grid tuning capacitor and grid bandswitch. At the extreme right is the plate current meter. The coaxial antenna connector is located atop the shielded compartment at the rear.

26-8 A Push-Pull 4-250A Kilowatt Amplifier

The push-pull 4-250A amplifier design given in the past issues of this Handbook has proven to be a most popular and widely duplicated piece of equipment. The amplifier illustrated herewith lives up to the excellent operational standards set by its predecessors. In addition, this latest version is completely TVI-proof, and is compact enough so that it may be mounted upon a standard size chassis, and placed within a standard relay rack cabinet.

The amplifier runs one kilowatt input on all amateur bands from 10 meters to 80 meters, inclusive. A bandswitching turret is used in the grid circuit, and heavy-duty plug-in inductors in the plate circuit. These inductors may be removed through a door in the upper portion of the shielded enclosure.

All tendencies towards parasitic oscillation in the amplifier have been eliminated. The amplifier is neutralized in the frequency range of

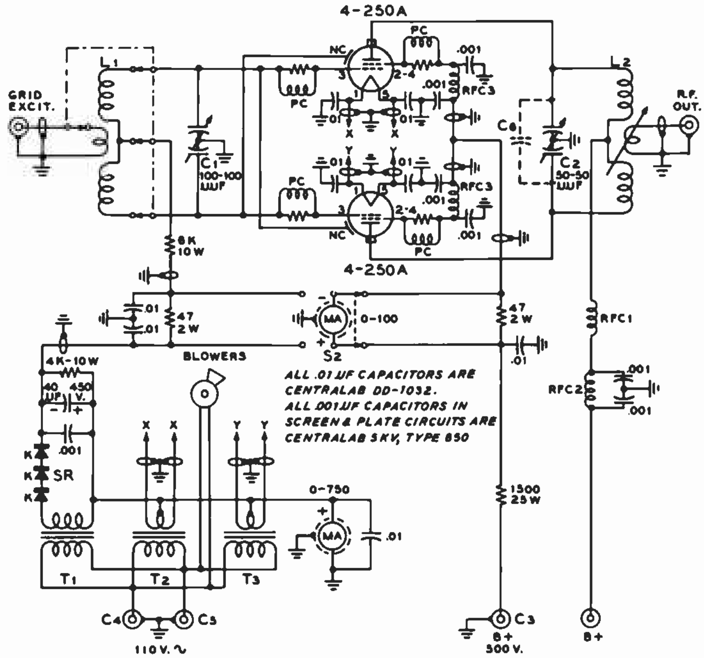


Figure 29
SCHEMATIC OF PUSH-PULL 4-250A AMPLIFIER

C_1—100-100 $\mu\mu$fd. Bud MC-1882A
C_2—50-50 $\mu\mu$fd. Butterfly B&W CX49A
C_3,C_4,C_5—0.1 μfd. 600 v. Sprague Hypass 80P3
C_6—10,000 v. vacuum capacitor, 10 $\mu\mu$fd. for 7 Mc., 20 $\mu\mu$fd. for 3.5 Mc.
RFC_1—2 mhy. National R-175A
RFC_2—4 μhy. National R-60
RFC_3—v-h-f choke Ohmite Z-50 or equivalent
T_1—125 v. 50 ma. Stancor PA-8421
T_2,T_3—5 v. 12 a. UTC S-59 or Triad F-9U
NC—see text
PC—50 ohm 2 watt resistor, wound with 3 t. no. 18 enam.
SR—three 50 ma. "replacement" type selenium rectifiers connected in series
L_1—B&W 35 watt BTCL turret
L_2—B&W HDVL series inductors

3.0 Mc. to 35 Mc., and operation is completely stable in this range at plate voltages up to 4500. The amplifier may, if desired, be used for Class B single-sideband operation on any band with no signs of instability.

The amplifier normally operates at 3000 volts and 330 milliamperes for c-w operation, or 2500 volts and 400 milliamperes for phone operation. Under these operating conditions, the 4-250A tubes show no visible color in a lighted room. In a darkened room the dull cherry red color of the plates becomes visible.

Circuit Description The complete schematic of the amplifier is shown in figure 29. The general layout design used for the push-pull 813 amplifier described in Section 7 of this chapter is used for this unit. The grid, filament and metering circuits of the amplifier are enclosed beneath the chassis in an "electrically tight" box. All leads leaving this box are suitably filtered to prevent leakage of energy into (or out of) the enclosure. The plate circuit of the amplifier is contained in a separate enclosure above the main chassis deck.

As stated in section 7 of this chapter, the feedback within tetrode tubes due to the small grid-plate capacity is a minute but highly important item. In the case of most tetrodes having internal screen support lead rods (such as the 4-250A and the 813) the need for neutralization in the high frequency region is necessary when the tube is used in an amplifier cir-

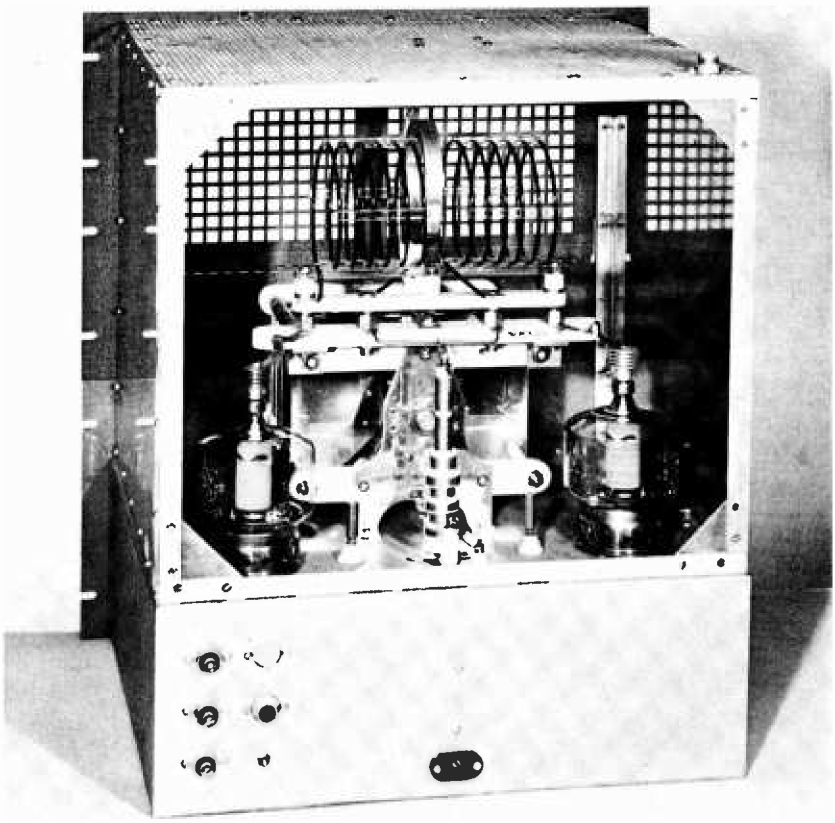


Figure 30
REAR VIEW OF PUSH-PULL 4-250A AMPLIFIER

The neutralizing rods are mounted on ceramic feedthrough insulators adjacent to each tube socket. Low voltage power leads leave the grid circuit compartment via Hypass capacitors located on the lower left corner of the chassis. A screen plate covers the rear of the amplifier during operation. This plate was removed for the photograph.

cuit operating with high power gain and high screen voltage. As the operating frequency of the tube is increased, the inductance of the screen support lead becomes an important part of the screen ground return circuit. At some critical frequency (about 45 Mc. for the 4-250A tube) the screen lead inductance causes a series-resonant condition and the tube is said to be "self-neutralized" at this frequency. Above this frequency the screen of the tetrode tube cannot be held at ground potential by the usual screen by-pass capacitors. With normal circuitry, the tetrode tube will have a tendency to self-oscillate somewhere in the 120 Mc. to 160 Mc. region. Low capacity tetrodes that can operate efficiently at such a high frequency are capable of generating robust parasitic oscillations in this region while the operator is vainly trying to get them operating at some lower frequency. The solution is to introduce enough

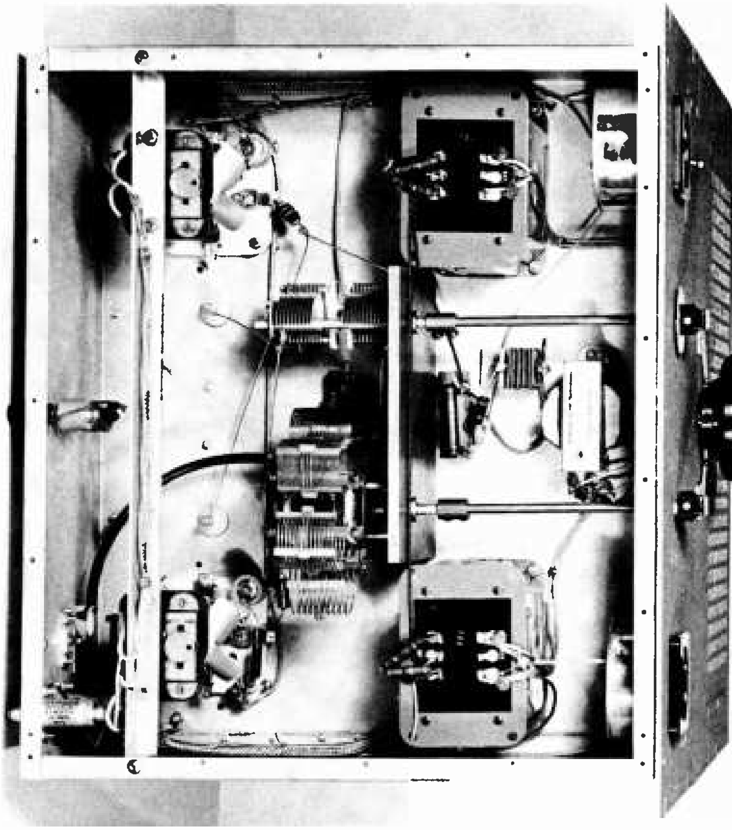


Figure 31
UNDER CHASSIS VIEW OF 4-250A AMPLIFIER

The bias supply for the amplifier is mounted at the front of the chassis between the two control shafts. A blower motor is mounted beneath each tube socket. A screened plate is placed on the bottom of the chassis to complete the under-chassis shielding.

loss in the circuit at the frequency of the parasitic so as to render oscillation impossible. This procedure has been followed in this amplifier.

During a long series of experiments designed to stabilize large tetrode tubes, it was found that suppression circuits were most effective when inserted in the *screen lead* of the tetrode. The screen, it seemed, would have r-f potentials measuring into the thousands of volts upon it during a period of parasitic oscillation. By-passing the screen to ground with copper strap connections and multiple by-pass capacitors did little to decrease the amplitude of the oscillation. Excellent parasitic suppression was brought about by strapping the screen leads of the 4-250A socket together (figure 32) and inserting a parasitic choke between the screen terminal of the socket and the screen by-pass capacitor.

After this was done, a very minor tendency towards self-oscillation was noted at extremely high plate voltages. A small parasitic choke in each grid lead of the 4-250A tubes eliminated this completely.

The 4-250A tubes are neutralized by two 1/4" rods mounted upon two feedthrough insulators and cross-connected to the 4-250A control grids beneath the chassis. These rods are threaded so that they may be run up and down the insulator bolt for neutralizing adjustment.

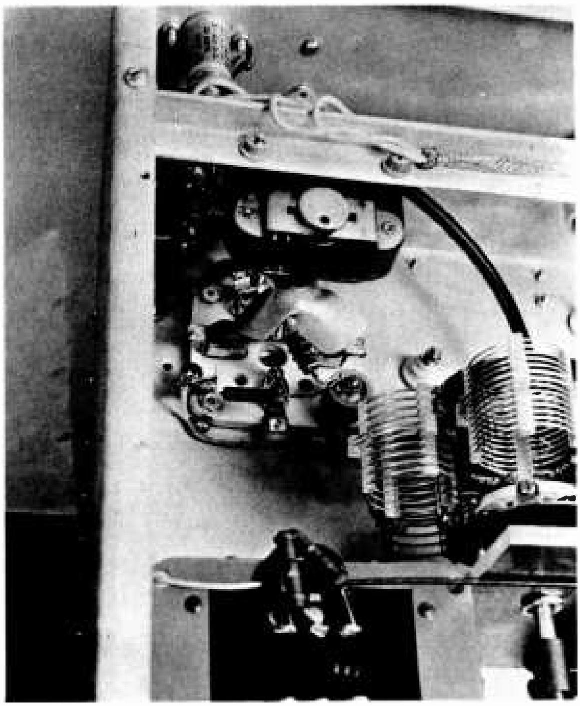


Figure 32
4-250A PARASITIC SUPPRESSION CIRCUIT

The two screen grid terminals of the socket are connected by a short copper strap. The .001-μfd. ceramic screen bypass capacitor is mounted on a corner socket bolt, and is connected to the screen strap through a small parasitic choke. Screen voltage is fed through a shielded cable and v-h-f choke to the terminal of the screen bypass capacitor. This installation is duplicated on the other 4-250A tube socket.

It is necessary to cool the filament seals of the 4-250A tubes. A small 115-volt a-c blower mounted beneath each tube socket, with the fan blade directing the air blast at the socket cooling holes will suffice. It is also necessary (although rarely mentioned) to ground the metal base ring of the 4-250A tube since this ring forms part of the screen shielding circuit. If grounding clips are not furnished with the tube socket, they may be made out of a short length of 3/8" brass strap formed to spring against the base ring.

Excellent circuit symmetry is achieved by the use of a "Butterfly" type tuning capacitor in the plate circuit of the amplifier. The heavy duty ceramic inductor jack-bar is attached to the capacitor by clips furnished by the manufacturer of the capacitor.

For operation in the 80-meter and 40-meter bands, a vacuum capacitor is placed across the plate tank circuit to provide proper circuit Q for phone operation. The vacuum capacitor is mounted in two clips placed atop the Butterfly capacitor.

The two 2" meters that indicate grid, screen and plate current are mounted below the chassis deck to remove them from the intense field of the plate circuit of the amplifier. Shield cans for the meters are cut from ends of "tin cans." The front edges of these cans are fluted, and the shield is pressed tightly against the front of the chassis and held in place by the stud-bolts on the back of the meter which pass through the end of the shield can. Construction of these meter shields is discussed in Chapter 15.

Grid tuning capacitor C_1 and the 35-watt B & W BTCL grid turret are mounted to a piece

4-250A AMPLIFIER—OPERATING CHARACTERISTICS

ITEM	PHONE	CW
PLATE VOLTAGE	2500	3000
PLATE CURRENT	400 MA.	330 MA.
SCREEN VOLTAGE	500	500
SCREEN CURRENT	60 MA.	70 MA.
GRID CURRENT	20 MA.	20 MA.
PROTECTIVE BIAS	−120	−120
OPERATING BIAS	−200	−200

Figure 33

of 1/4" dural plate measuring 5" high and 7" long. The edge of the plate is tapped for 6-32 screws and it is screwed to the underside of the chassis.

Mechanical Assembly The same mechanical configuration used in the push-pull 813 amplifier is employed in the push-pull 4-250A unit. A 12" relay rack panel with hinged door (Bud PS-815) and a 8¾" panel are joined together to form a 20¾" panel. The amplifier is constructed upon a cadmium plated steel chassis measuring 15"x 17"x 6" (California Chassis Co., 5445 Century Blvd., Lynwood, Calif.). A 14¼" high enclosure atop the chassis contains the plate circuit components of the amplifier. The bottom of the amplifier chassis is covered with a piece of perforated Reynolds "Do-it-yourself" aluminum. Construction of the amplifier enclosure is discussed in Chapter 30. The sides of this enclosure are made of solid sheet aluminum, and the top and back are made of perforated stock. An SO-239 coaxial receptacle is mounted in one corner of the top of the enclosure as the antenna output connector. Placement of the major components may be seen in figures 28, 30, and 31. The two feedthrough insulators which are used as mounting studs for the neutralizing rods are each located 3⅞" from the center of the tube socket, and each neutralizing rod is 1¼" long.

Plate leads to the 4-250A tubes are made of short sections of 1/2" copper strap and all r-f wiring beneath the chassis is done with no. 14 tinned copper wire. All low voltage d-c leads and a-c wiring is done in shielded braid; the braid being grounded to the chassis at each end of the lead. A short length of RG-59/U coaxial line is used for the connection between the coaxial input plug P_1 and the link circuit of the grid turret L_1.

Amplifier Operation Excitation should be applied to the amplifier and a 2-volt, 60-milliampere flashlight lamp connected to the link output connections. Starting with no rods on the neutralizing feedthrough insulators, a definite indication should be obtainable in the lamp when the grid and plate circuits are in resonance and excitation is applied to the amplifier. Makeshift neutralizing rods may be built up out of 6-32 nuts, held together by a long bolt. These rods should be lengthened bit by bit until the amplifier becomes perfectly neutralized. This will happen at a rod length of slightly over 1". When the proper length is found, two rods may be cut from a length of 1/4" brass extension shaft. These rods should be drilled and tapped to fit the threaded bolt of the feedthrough insulator. Correct operating voltages and currents for the amplifier are shown in figure 33.

26-9 A Pi-Network Amplifier Using a 4-125A

The pi-network is an effective means of obtaining an impedance match between a source of r-f energy and a low value of load impedance. A properly designed pi-network is capable of transformation ratios greater than 10 to 1, and will provide approximately 30 db or more attenuation to the second-harmonic output of the r-f stage than to the desired signal output. Since the second harmonic output of the amplifier tube already may be down some 20 db, the second harmonic output of the network should be down perhaps 50 db from the fundamental output level of the transmitter. Attenuation to the third harmonic of the r-f stage will be even greater.

The peak voltages to be expected across the input capacitor of the pi-network are the same as would be encountered across the plate tuning capacitor of a single-ended tank used in the same circuit configuration. The peak voltage to be expected across the output capacitor of the network will be less than the voltage across the input capacitor by the square root of the ratio of impedance transformation by the network. Thus if the network is transforming from 5000 ohms to 50 ohms, the ratio of impedance transformation is 100 and the square root of this ratio is 10, so that the voltage across the output capacitor in the network is 1/10 that across the input capacitor.

A considerably greater maximum capacitance is required of the output capacitor than of the input capacitor of a pi-network when transformation to a low load impedance is required.

Figure 34
4-125A PI-NETWORK FINAL AMPLIFIER

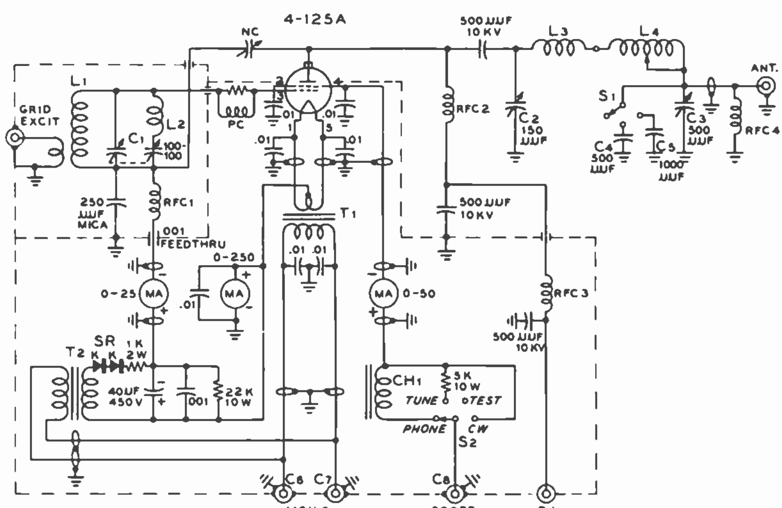


Figure 35

SCHEMATIC OF 4-125A PI-NETWORK AMPLIFIER

C_1—100-100 µµfd. Millen type 28000
C_2—150 µµfd. 7000 v. Johnson 150D70
C_3—500 µµfd. Johnson 500E20
C_4—500 µµfd. 3000 v. mica
C_5—1000 µµfd. v. mica
C_6, C_7, C_8—0.1 µfd. 600 v. Sprague Hypass 80P3
L_1—34 t. 1" dia. 2" long B&W 3015, link 3 t.
L_2—12 t., same as L_1
L_3—4 t. 1" dia. 1" long no. 12 enam.
L_4—B&W Rotary Inductor 229-201
RFC_1—2½ mhy. National R-100
RFC_2—1 mhy. National R-175A
RFC_3—4 µhy. National R-60
T_1—5 v. at 6 a. Stancor P-3062 or Triad F-8X
T_2—125 v. at 50 ma. Stancor PA-8421
CH_1—16 hy. at 50 ma. Stancor C-1003 or Triad C-3X
SR—two 50 ma. selenium "replacement type" rectifiers in series
NC—National NC-800 disc type capacitor
PC—3 t. no. 18 enam. on 50 ohm 1 watt resistor

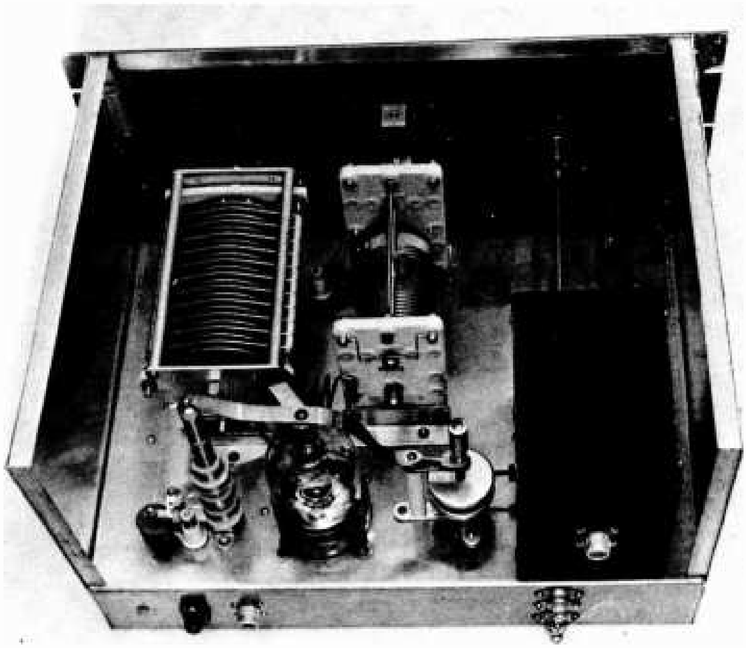


Figure 36

REAR VIEW OF 4-125A AMPLIFIER

The 10-meter plate circuit inductance is mounted between the rotary coil (center) and the plate tuning capacitor (left)

For 3.5-Mc. operation, maximum values of output capacitance may run from 500 $\mu\mu$fd. to well over 1500 $\mu\mu$fd., depending upon the ratio of transformation. Design information on pi-network circuits is given in Chapter 11.

Illustrated in figures 34, 36, and 37 is a modern version of an all-band pi-network power amplifier, employing a 4-125A tetrode tube. The amplifier is capable of an input of 500 watts at 3000 volts on c.w., and 380 watts at 2500 volts on phone. The amplifier employs a rotary inductor in the output tank circuit for full frequency coverage between 3.5 Mc. and 30 Mc., and the unit is designed for TVI-free operation over this range.

Circuit Description The 4-125A amplifier is capable of operation at any frequency within the range of 3.5 Mc. to 30 Mc. A so-called *multi-band* tank circuit is employed in the grid input of the amplifier. This special resonant circuit tunes a ten to one frequency range, eliminating the need of various grid coils for the different amateur bands. A 500-watt roller-type variable inductor in conjunction with a 150-$\mu\mu$fd. variable capacitor provides a nine to one frequency range for the pi-network plate circuit. The pi-network output capacitor has sufficient maximum capacity to match 50 or 70-ohm load circuits within the frequency range of the amplifier.

A small 50-ma. selenium rectifier supply provides protective bias for the 4-125A tube, and a selector switch in the screen circuit allows the screen voltage to be modified as dictated by the operating requirements of the amplifier (figure 39).

The amplifier is neutralized by a capacitor-bridge system, and all signs of parasitic oscillations are removed by a small parasitic suppressor mounted at the grid terminal of the 4-125A socket.

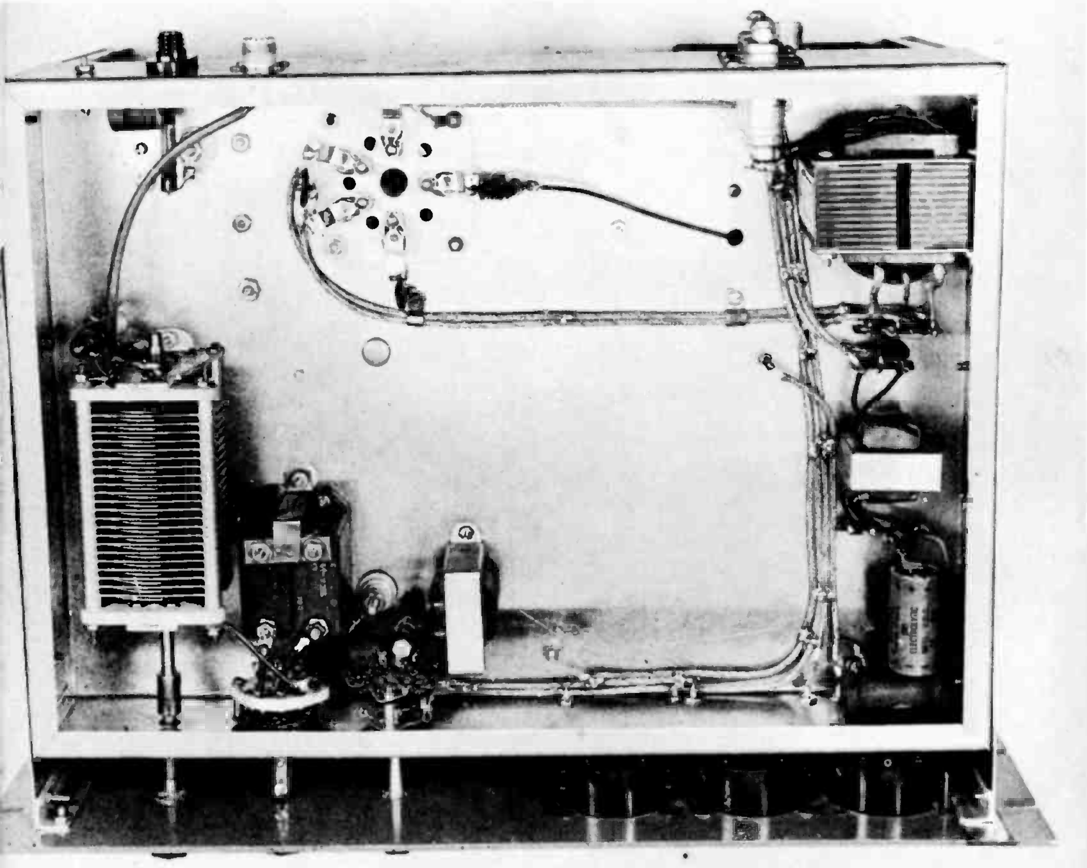


Figure 37
UNDER CHASSIS VIEW OF 4-125A AMPLIFIER
All low voltage leads are run in shielded wires, banded at intervals to the chassis. A chassis plate fits over the bottom of the amplifier to complete the TVI proof enclosure.

Amplifier Construction The complete amplifier stage is built upon an aluminum chassis measuring 10" x 17" x 3" (Bud AC-416). A standard 10" aluminum relay rack panel is used. The chassis is spaced away from the panel two inches to allow mounting room for the three meters. These meters measure the grid, screen and plate current of the 4-125A tube.

As shown in figure 36, the rotary inductor is placed in the center of the chassis, and is driven by a Barker & Williamson 3902 counter-type dial through an insulated coupling. The plate tuning capacitor C_2 and the grid tuning capacitor C_1 are spaced equidistant each side of the axis of the rotary inductor. The grid circuit of the amplifier is mounted above chassis in an aluminum box measuring 5" x 4" x 3" (Bud AU-1028). An interior view of this box, showing the arrangement of the grid circuit is shown in figure 38. The shaft connecting the grid capacitor to the panel control is a section of 1/4" phenolic rod, since it is necessary to insulate the rotor of the grid capacitor from ground. To the left of the grid circuit box is mounted the neutralizing capacitor for the 4-125A tube. The connections between the neutralizing capacitor, the tube and the plate r-f choke and coupling capacitor are made from 1/2" brass shim stock.

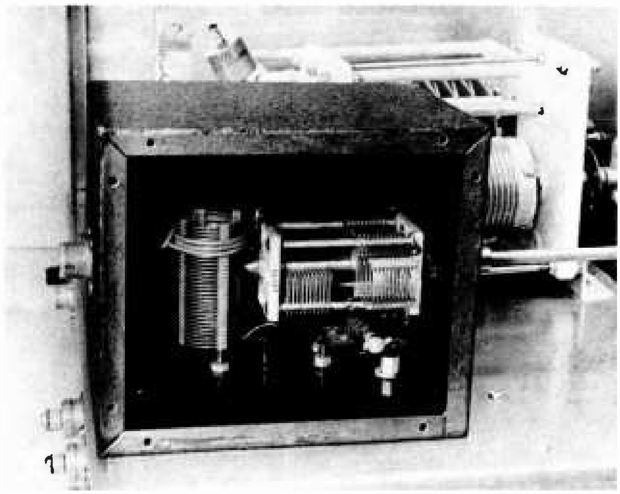


Figure 38

THE GRID CIRCUIT ENCLOSURE OF THE 4-125A AMPLIFIER

Coil L_1 is mounted vertically at the left of capacitor C_1. RFC_1 and the 250-μμfd. by-pass capacitor are located below C_1. The bias lead enters the grid circuit enclosure through a .001-μfd. feedthrough capacitor at the right. The coaxial connector for excitation is mounted on the back of the box.

The section of the plate circuit inductor that resonates to 10 meters takes the form of a small inductor (L_3) wound of no. 10 enameled wire and mounted between the plate tuning capacitor and the main rotary inductor.

Beneath the chassis are located the output capacitors and loading circuit of the pi-network and the bias supply for the 4-125A tube. Placement of these components may be seen in figure 37.

Amplifier Wiring As with the push-pull type of amplifier, all d-c and low voltage a-c leads in this amplifier are run in shielded braid. The leads that pass through the front of the chassis to the meters run through Centralab type FT ceramic feedthrough capacitors mounted in the front wall of the chassis. Power connections to the amplifier are made through Sprague type 80P3 Hypass capacitors mounted on the rear wall of the chassis. The high voltage lead to the shunt-fed plate tank circuit passes through the rear wall via a Millen type 37001 safety terminal and is filtered by a VHF filter composed of two 500 μμfd. TV-type ceramic capacitors and an Ohmite Z-50 r-f choke. The output lead from the antenna loading capacitor C_3 consists of a short length of RG-59/U coaxial line.

The two auxiliary antenna padding capacitors are mounted directly behind the antenna loading switch S_1 and are connected to the switch with short, direct leads. The other capacitor leads are strapped together and grounded by lengths of 1/2" brass shim stock.

Grid inductors L_1 and L_2 are mounted to the grid tuning capacitor C_1 by their leads. A three turn link wound of hookup wire is placed around the ground end of L_1. The coaxial input plug is mounted on the rear wall of the grid box directly behind L_1. Coils L_1 and L_2 are mounted at right angles to each other. The paint is removed from the bottom of the box and it is firmly bolted to the amplifier chassis.

Amplifier Neutralization The amplifier stage may be neutralized by supplying excitation to the input circuit until rectified grid current flows. A jumper is next placed across the antenna output jack, and the plate tuning capacitor C_2 is resonated to frequency. Neutralizing capacitor NC is now adjusted until the tuning of the plate capacitor

4-125A AMPLIFIER—OPERATING CHARACTERISTICS

ITEM	PHONE	CW
GRID VOLTAGE	−220	−200
GRID CURRENT	10 MA.	12 MA.
SCREEN VOLTAGE	350	350
SCREEN CURRENT	33 MA.	50 MA.
PLATE VOLTAGE	2000	2000
PLATE CURRENT	150 MA	200 MA.

Figure 39

has no effect upon the reading of the rectified grid current.

The output tank circuit has two variables: The plate capacitor C_2 and the rotary inductor L_4. To obtain the correct L/C ratio rotary inductor L_4 should be set with all turns in the circuit for 80 meter operation, 12 turns active for 40 meters, 5 turns for 20 meters, 2½ turns for 15 meters, and zero turns for 10 meters. Resonance may now be set in the usual manner by the tuning of C_2.

26-10 A Kilowatt Pi-Network Amplifier

A single 4-250A or 4-400A tetrode tube may be employed in a pi-coupled amplifier capable of running 1-kilowatt input on all frequencies between 3.5 Mc. and 30 Mc. Such an amplifier is shown in figures 40 to 43 inclusive. Basically, this amplifier follows the design of the 4-125A amplifier in Section 8 of this chapter, except that heavy-duty components are employed, and the amplifier is designed to work at plate potentials up to 4000 volts.

Amplifier Circuit The plate circuit of this kilowatt amplifier is built around a Jennings type UCS 300-$\mu\mu$fd. vacuum variable capacitor and a Barker & Williamson type 850 1-kw. Bandswitching Inductor.

Using a 4-250A tube the amplifier operates at 3000 volts and 330 milliamperes for c.w., and 3000 volts and 225 milliamperes (675 watts) for phone. A 4-400A tube in the amplifier runs at the same input on c.w. and at 3000

Figure 40

4-250A AMPLIFIER USING BANDSWITCHING TURRET

This amplifier may be used with either a single 4-250A or 4-400A tube. It is capable of one kilowatt input on all frequencies between 3.0 Mc. and 30 Mc. The output impedance is 50 to 75 ohms. Complete shielding and parasitic suppression make this unit TVI proof at all frequencies.

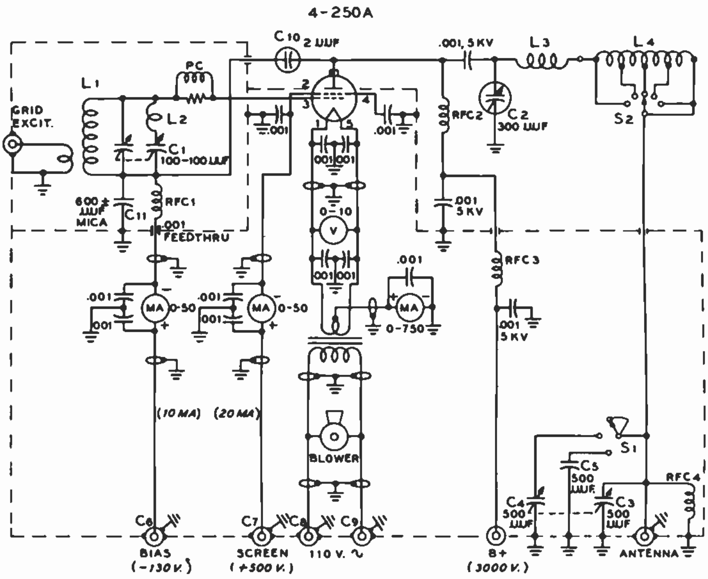


Figure 41
SCHEMATIC OF 4-250A PI-NETWORK AMPLIFIER

C_1—100-100 $\mu\mu$fd. Bud MC-1882A
C_2—300 $\mu\mu$fd. variable vacuum capacitor Jennings UCS-300
C_3,C_4—500 $\mu\mu$fd. Johnson 500E20
C_5—500 $\mu\mu$fd. 3000 v. mica
C_6,C_7,C_8,C_9—0.1 μfd. 600 v. Sprague Hypass 80P3
C_{10}—2 $\mu\mu$fd. fixed vacuum capacitor Jennings
C_{11}—see text
L_1,L_2—same as figure 35
L_3—4 t. 3/16" dia. copper tubing 1¼" dia. 2" long
L_4—B&W 850 bandswitching inductor
RFC_1—2½ mhy. National R-100
RFC_2—2 mhy. National R-175A
RFC_3—4 μhy. National R-60 or Ohmite Z-50
RFC_4—same as RFC_1
T_1—5 v. at 10 a. Stancor P-6135 or Triad F-9A
PC—50 ohm 2 watt resistor, wound with 4 t. no. 18 enam.
All .001, 5KV capacitors are Centralab 850

volts and 275 milliamperes (825 watts) on phone.

The same type of multi-range grid circuit as employed in the 4-125A amplifier is used here. Bridge neutralization is used with a 2-$\mu\mu$fd. fixed vacuum capacitor as one leg of the bridge, and a hand-picked mica capacitor C_{11} as the other leg of the bridge.

Amplifier Construction The amplifier is built upon an aluminum chassis measuring 13" x 17" x 3" (Bud AC-420) and has a 12¼" standard relay rack panel. The grid circuit components are mounted in an aluminum box measuring 4" x 5" x 6" (Bud AU-1029). The screen covering of this amplifier is made of Reynolds "Do-it-yourself" perforated aluminum stock. The construction of the screened enclosure is discussed in Chapter 30. The counter dial used on this amplifier is a surplus item, but a Johnson type 3902 counter dial may be used as an equivalent substitute. The three main tuning controls drive the inductor switch, the vacuum variable capacitor and the grid tuning capacitor through flexible insulated couplings. The vacuum capacitor is mounted in a piece of 1/2" aluminum stock that is bolted to the chassis. A hole is drilled in the stock to pass the neck of the capacitor. The top portion of the aluminum bracket is split, and a long bolt draws the sides of the bracket tightly against the neck of the capacitor. A mounting frame is supplied by the manufacturer of the capacitor which would serve equally as well.

The shaft height above the chassis of the

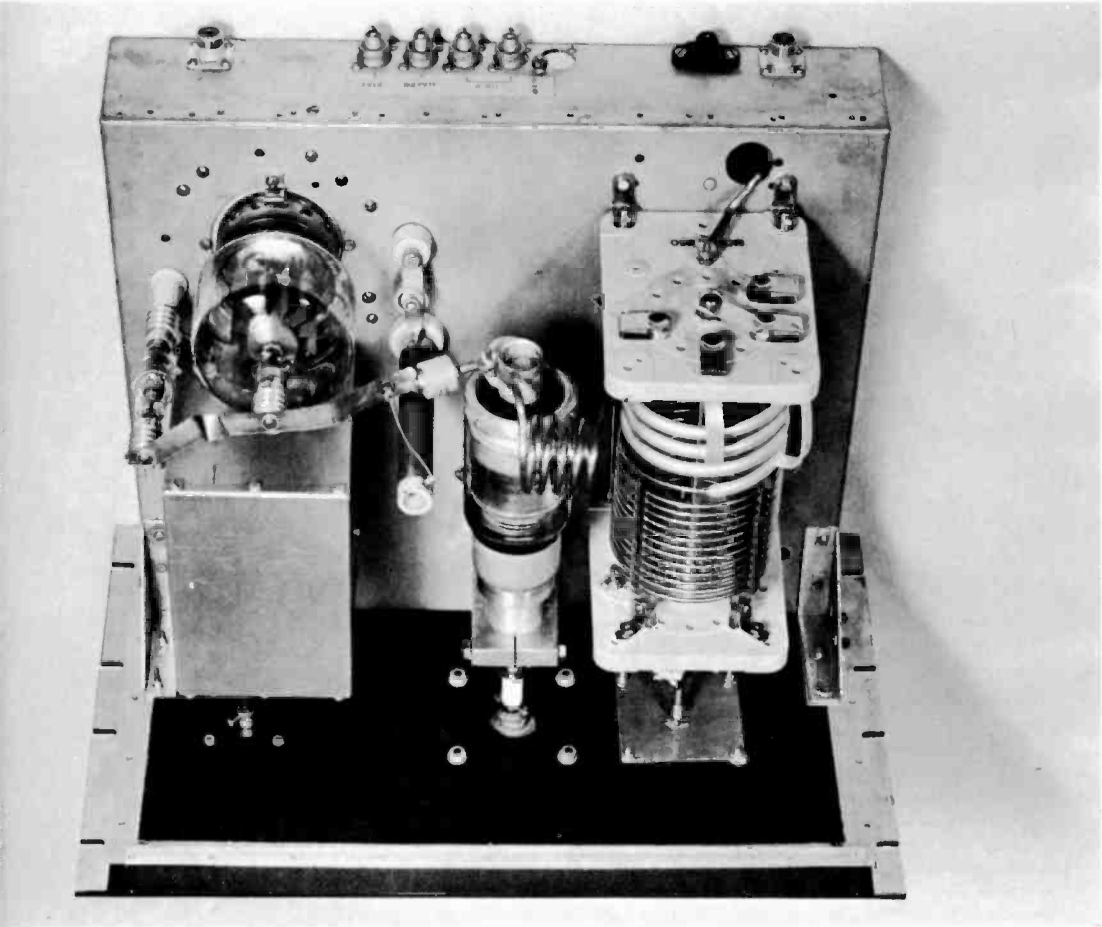


Figure 42
TOP VIEW OF 4-250A AMPLIFIER

Because of limited panel height, the 10-meter coil supplied with the B&W model 850 all-band tank circuit was removed and a new coil was wound out of copper tubing and mounted between the tank circuit switch and the variable vacuum capacitor. The vacuum neutralizing capacitor is directly to the right of the amplifier tube.

inductor determines the placement of the variable vacuum capacitor and the placement of the grid circuit tuning capacitor within the grid box. All shafts should fall on the same horizontal line for panel symmetry. The components within the grid box are arranged in the same manner as those in the 4-125A stage, shown in figure 38.

A small blower fan is mounted beneath the tube socket to provide cooling air for the base seal of the 4-250A. The motor is mounted on a length of angle aluminum that bolts to the under lip of the chassis at the front and back.

The meter leads are by-passed by Erie type 327 feedthrough ceramic capacitors mounted on one side of an aluminum angle strip 10" long. The strip is affixed to the chassis by 1" brass spacers and machine bolts. The two

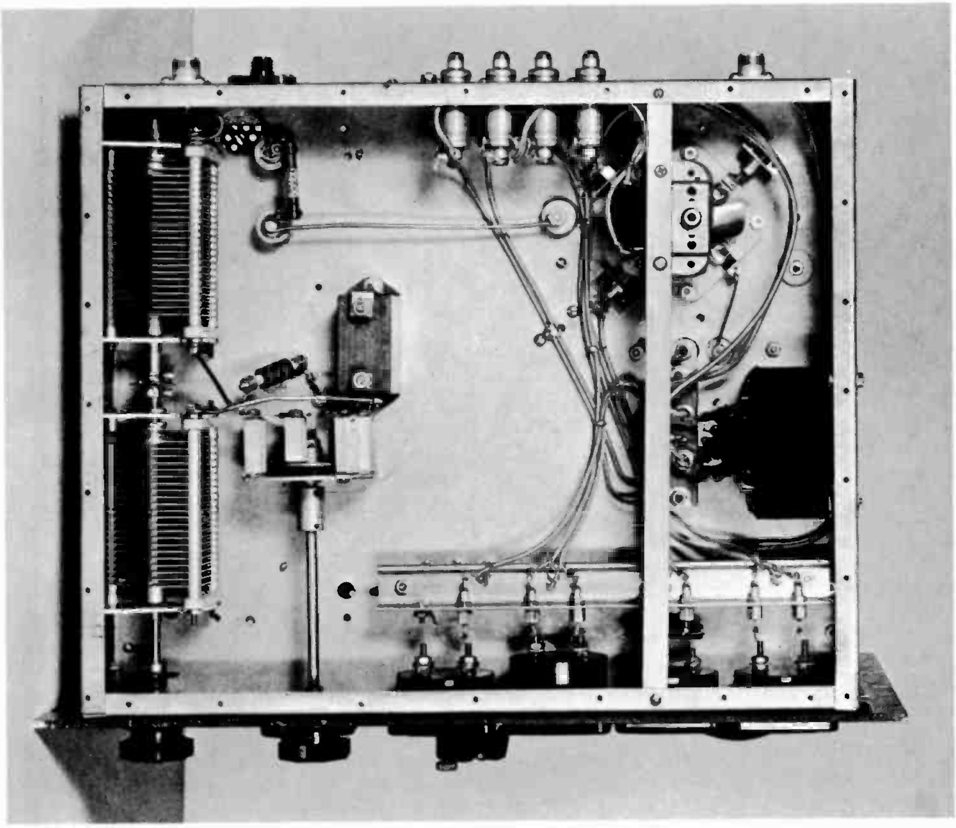


Figure 43
UNDER CHASSIS VIEW OF 4-250A PI-NETWORK AMPLIFIER

screen terminals of the amplifier tube socket are by-passed directly to ground by means of two .001-μfd. type 327 Erie feedthrough capacitors mounted on 1" lengths of aluminum angle. The inductance of the screen grounding lead is thus reduced to an extremely low value.

The output section of the plate pi-network is tuned by a 500-$\mu\mu$fd. variable capacitor C_2. Switch S_1 shunts an additional air capacitor across C_2 for low frequency operation. A third position of S_1 adds a 620-$\mu\mu$fd., 3000-volt mica capacitor to the circuit, used for operation of the amplifier with low impedance antenna systems on the 80-meter band.

Amplifier Neutralization The amplifier tube is neutralized by a bridge system, composed of the 2-$\mu\mu$fd. fixed vacuum capacitor and C_{11}, the grid circuit by-pass capacitor. The amplifier is neutralized by varying the capacity of C_{11} which will fall somewhere between 250 $\mu\mu$fd. and 700 $\mu\mu$fd.

To accomplish this, about 10 watts of 14-Mc. r-f energy is fed into the *plate circuit* of the amplifier, via the coaxial output plug. The plate circuit of the amplifier as well as the grid circuit is resonated to the frequency of the exciting voltage. A sensitive device, such as a 0-1 d-c milliammeter in series with a 1N34 crystal diode, is connected to the *grid input receptacle* of the amplifier. This meter will indicate the degree of unbalance in the bridge neutralizing circuit. For test purposes, a three section b-c type variable capacitor is used for C_{11}, the three sections being strapped in parallel to provide a variable capacitor of approximately 1000 $\mu\mu$fd. This capacitor is

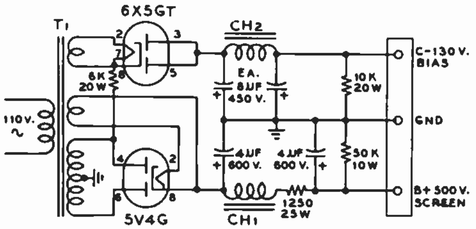


Figure 44
SAFETY SCREEN AND BIAS SUPPLY

T_1—450-0-450 v. at 105 ma. Chicago PSR-105
CH_1—12 hy. at 85 ma. Chicago RS-1285
CH_2—15 hy. at 40 ma. Chicago RS-1540

varied until the reading of the indicating device is at a minimum. Each change in C_{11} should be accompanied by re-resonating the plate and grid tank circuits. When a point of minimum indication is found, the variable capacitor may be removed, and a 1000-volt mica capacitor of the correct value substituted in its place. Under normal conditions, the capacity of C_{11} will be in the neighborhood of 700 $\mu\mu$fd.

A second amplifier built along the lines of this one showed slight signs of instability in the region of the 21-Mc. band. This tendency towards oscillation was cured by removing the two .001 μfd. screen by-pass capacitors, and strapping the number 2 and 4 screen pins of the socket together with a piece of half-inch copper strap. A parasitic choke was connected to the center of this strap (as shown in figure 32) and the free end of the suppressor was attached to a .001-μfd., 5-Kv. ceramic capacitor mounted to one of the socket bolts. Screen voltage was fed to the capacitor via a v-h-f choke, in the manner shown in figure 29. This modification allowed the amplifier to be run class AB_1 for single-sideband operation with no signs of instability. Such a screen circuit modification is recommended for those who wish to duplicate this amplifier.

Bias and Screen Supply A separate bias and screen supply (figure 44) is employed with this amplifier. The screen supply furnishes slightly higher than normal voltage which is dropped to the correct value by an adjustable series resistor. With this current limiting resistor in the circuit, it is possible to apply excitation to the 4-250A with screen voltage present but in the absence of plate voltage and still not damage the screen of the tube.

Grid Resonance If a 0-100 degree dial is used on the grid tank circuit (with minimum capacitance at zero dial setting) the following dial settings are the approximate readings for the various bands: 80 meters, 25 degrees; 40 meters, 80 degrees; 20 meters, 24 degrees; 15 meters, 61 degrees; 10 meters, 74 degrees.

26-11 A 4-1000A Pi-Network Amplifier

The amplifier illustrated in figures 45 through 49 is of great academic interest to amateurs, although the power rating of 3.5 kilowatts is in excess of the maximum level permitted by the Federal Communications Commission. Custom built for commercial applications in the 3.5-Mc. to 25-Mc. range, this unit exhibits many interesting features that may well be applied to amplifiers of more modest rating.

Amplifier Circuit The schematic of the power amplifier is shown in figure 46. A single 4-1000A tetrode is employed in a straightforward pi-network circuit, running at 5000 volts and 700 ma. The symmetrical panel arrangement of the amplifier is shown in the front view (figure 45) and the rear view (figure 48). A standard heavy-duty variable inductor and a 10,000-volt, 300-$\mu\mu$fd. variable vacuum capacitor form the plate tank circuit. The plate blocking capacitor C_1 is made of four 500-$\mu\mu$fd., 30KV TV-type ceramic capacitors connected in parallel. The capacitors are mounted between two copper plates to insure equal distribution of r-f current between them. Two 500-$\mu\mu$fd. variable air capacitors are ganged by means of a gear drive to form the output capacitor of the pi-network.

The 4-1000A is mounted in a special air socket which is connected to a 115-volt blower motor mounted on the back of the amplifier chassis. Beneath the chassis are located the filament transformer and the National MB-40SL all band grid turret, modified as shown in figure 46. All below chassis wiring is run in shielded loom, grounded at both ends.

To insure a short, direct plate-cathode ground circuit, a length of 1/2" copper strap is run from the rotor of the plate circuit tuning capacitor C_2 through a feedthrough insulator directly to a point at the center of the tube socket. All socket grounds are made directly to this point.

The plate current meter located above the

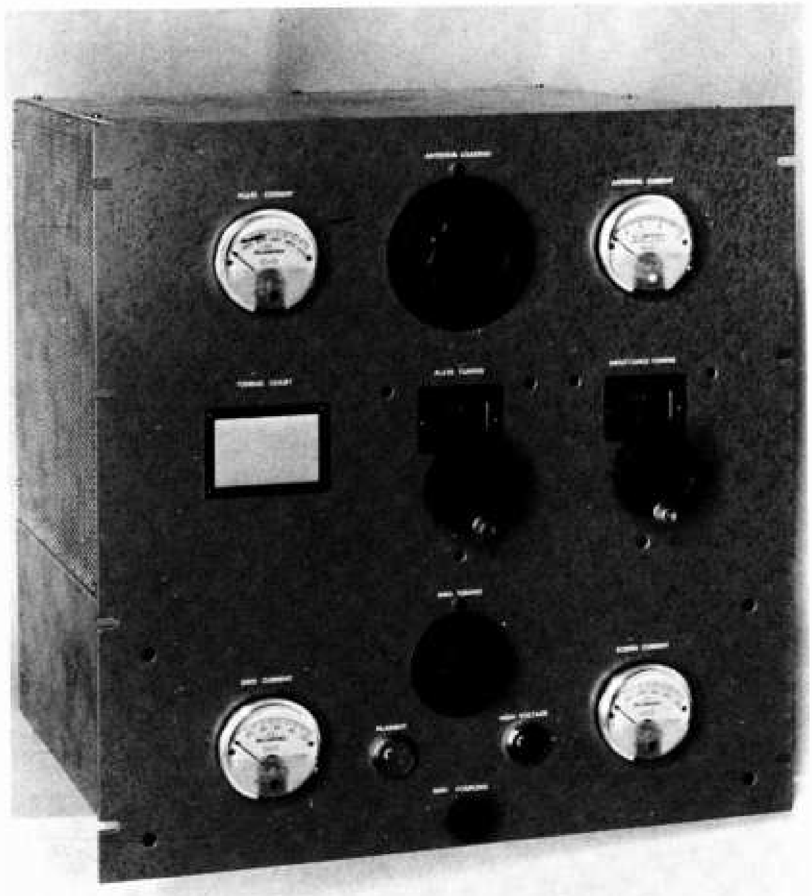


Figure 45
SINGLE 4-1000A PI-NETWORK AMPLIFIER

chassis is enclosed in an aluminum shield box, and the leads to the meter are run from the below chassis area in copper conduit. The meters mounted below chassis are enclosed in aluminum shield cans to remove them from the r-f field surrounding the grid circuit components.

R-f line filters are located in a separate box affixed to the rear of the amplifier chassis next to the blower motor.

The plate r-f choke is a critical item in a transmitter of this power capability. The most satisfactory choke found is a surplus item, wound on a 1" ceramic form that was used in the plate circuit of the AN/ART-13 airborne transmitter. Four turns are removed from the top of the choke winding to eliminate a resonant spot that fell in the vicinity of 21 Mc.

This amplifier was tested at plate potentials of up to 6000 volts with no signs of instability. Another amplifier of like power capability but slightly different physical configuration required the screen terminals of the 4-1000A to be strapped together with a 1/2" copper strap, and a single .001-μfd., 5000-volt ceramic capacitor connected to the screen terminal through a parasitic choke, much as in the manner as the screen connection of the push-pull

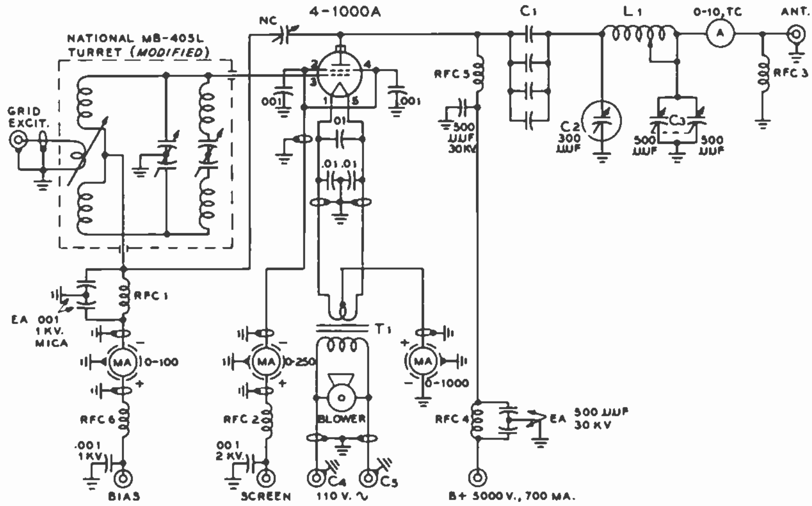


Figure 46
SCHEMATIC OF 4-1000A PI-NETWORK AMPLIFIER

C_1—four 500 $\mu\mu$fd. 30 KV TV-type capacitors in parallel
C_2—300 $\mu\mu$fd. 10,000 v. variable vacuum capacitor Jennings UCS
C_3—two 500 $\mu\mu$fd. capacitors in parallel Johnson 500D35
C_4,C_5—0.1 μfd. 600 v. Sprague Hypass 80P3
NC—10 $\mu\mu$fd. Johnson N-375
RFC_1,RFC_2,RFC_3,RFC_6—2½ mhy. National R-100U
RFC_4—4 μhy. National R-60
RFC_5—surplus plate choke from ART-13 transmitter
T_1—7.5 v. at 21 a. Chicago FV-720
L_1—Johnson rotary inductor 226-3
Filament bypass capacitors are Centralab DD-1032

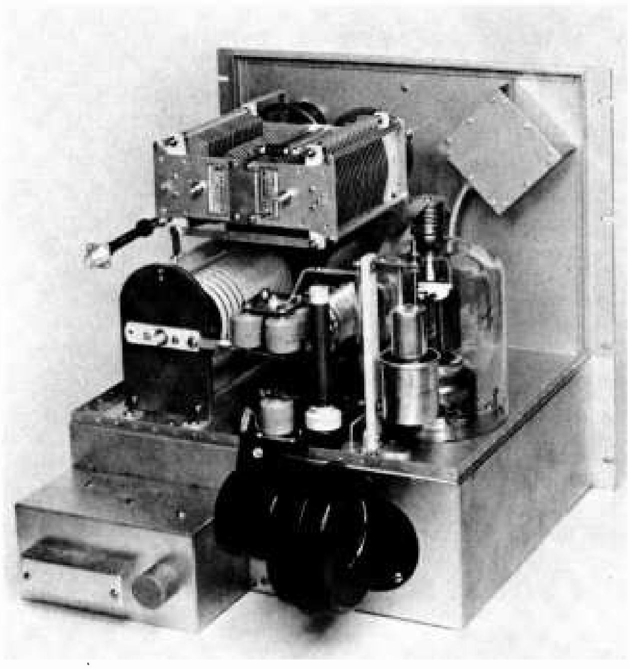


Figure 47
REAR VIEW OF 4-1000A AMPLIFIER

The plate r-f choke is mounted upon a 1-inch phenolic block to prevent flashover between the choke winding and the chassis. All tank circuit connections are made with half-inch copper strap.

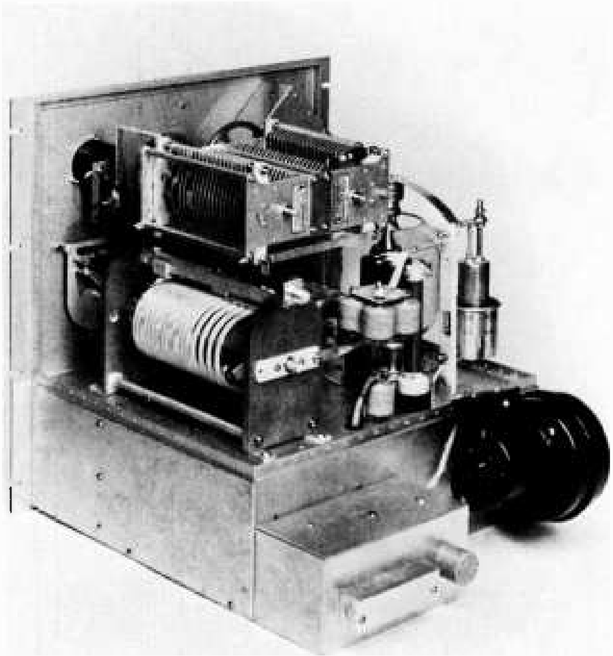


Figure 48
SIDE VIEW OF 4-1000A AMPLIFIER
Low voltage lead filters are contained in the small box mounted on the rear of the amplifier chassis. The pi-network output capacitors are mounted above the rotary inductor. They are geared together and driven from the front panel. The neutralizing capacitor is at the extreme right of the chassis.

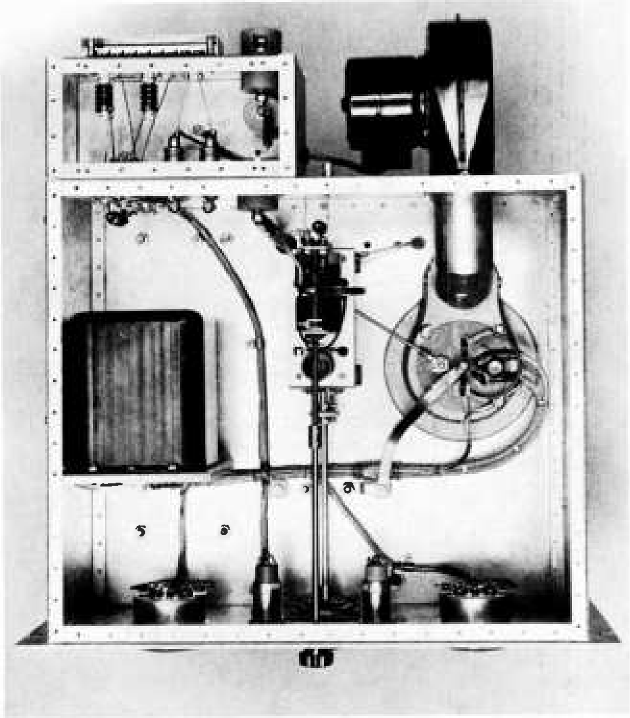


Figure 49
UNDER CHASSIS VIEW OF 4-1000A AMPLIFIER
All low voltage leads are run in shielded loom. A metal plate covers the bottom of the amplifier to complete the TVI proof enclosure. A short length of aluminum tubing conducts the forced air from the blower motor to the 4-1000A tube socket. Filament transformer is mounted at left.

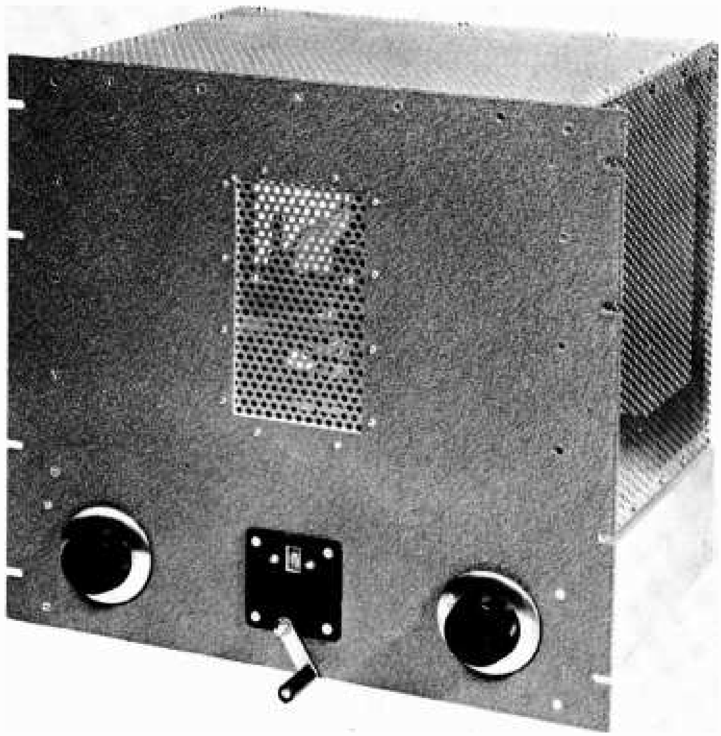


Figure 50
PI-NETWORK TRIODE AMPLIFIER
A single 450-TH triode tube operates in a unique circuit providing a single-ended pi-network coupling to the antenna. TVI proof design is employed in both the electrical circuit and the mechanical layout.

4-250A amplifier shown in figure 29 of this chapter. The choke consisted of a 50-ohm, 2-watt carbon resistor wound with three turns of no. 18 enamelled wire spaced the length of the resistor.

26-12 1-Kilowatt Triode Pi-Network Amplifier

Chapter 11, section 5 (Amplifier Neutralization) states that grid neutralization of triode amplifiers is in general unsatisfactory since the degree of neutralization is a function of the operating parameters of the stage. As the triode stage begins to draw grid current, one section of the split grid coil is heavily loaded, upsetting the balance of the neutralizing bridge.

If a triode tube having low internal capacities (such as the 450TH) is used in a grid neutralized circuit, and if the L/C ratio in the grid network is held at a low value, an amplifier employing this tube may be used over a 2:1 frequency range with a satisfactory degree

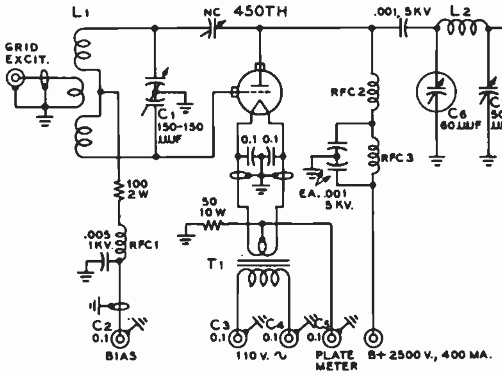


Figure 51
SCHEMATIC OF 450-TH PI-NETWORK AMPLIFIER

C_1—Johnson 150FD20
C_2,C_3,C_4,C_5—0.1 μfd. Sprague Hypass capacitor 80P3
C_6—Eimac VVC 60-20 variable vacuum capacitor
C_7—Johnson 500E20
NC—National NC-150 disc type capacitor
RFC_1,RFC_4—2½ mhy. National R-100
RFC_2—National R-175A
RFC_3—4 mhy. National R-60
L_1—B&W 10JCL (for 14 Mc.)
L_2—5 t. 1/4" copper tubing, 3 1/4" i.d. 3" long (14 Mc.)
L_3,L_7—6 t. no. 12, 1/2" i.d., 3/4" long
L_4,L_6—8 t. no. 12, 1/2" i.d., 1" long
L_5—1½ t. no. 12, 1/2" i.d., 1/8" long
T_1—7.5 v. at 20 a. Chicago FV-720
Filament capacitors are Sprague Hypass 80P3
.001 μfd., 5KV capacitors are Centralab 854
Capacitors in low-pass filter are Centralab 850

of neutralization. This neutralization configuration allows the use of a single-ended pi-network plate tank circuit, usually only employed with tetrode tubes.

The amplifier shown in figures 50 to 53 employs a single 450TH triode tube, running at either 2500 volts and 400 milliamperes or 3000 volts and 330 milliamperes. It is designed for operation on a single band: 20 meters. A surprising number of amateurs are single band operators, either by choice or because of insufficient space for more than one antenna. An amplifier of this type is an inexpensive solution to their high power problem.

Amplifier Circuit The schematic of the triode amplifier is shown in figure 51. The grid circuit is composed of a 10-meter B & W JCL inductor tuned by a 150-μμfd. split stator capacitor to 20 meters. The effective circuit capacity is 70 μμfd. This is sufficient to provide stable neutralization of the stage under all operating conditions. The plate voltage for the amplifier is shunt fed through a National R-175A choke in combination with a v-h-f filter.

It is necessary to employ a high-C plate tank circuit with a single ended stage, and yet at the same time have a reasonably low inductance ground return path for harmonic frequencies. An Eimac 60-μμfd., 20,000-volt vacuum variable capacitor is well suited for this purpose and therefore is employed as the input capacitor in the pi-network. The output capacitor is a 500-μμfd., 2000-volt air unit, suitable for matching load impedances in the range of 50 to 75 ohms.

Included in the overall plate circuit of a single-ended amplifier are the filament by-pass capacitors which must carry the r-f current flowing in the plate-filament circuit of the stage. The most satisfactory capacitors for this service were found to be Sprague Hypass units, type 80P3. Small mica or ceramic capacitors invariably failed after a few hours use carrying the heavy current that flows in this circuit when the amplifier is delivering full output.

As a final TVI precaution, a low-pass 50-ohm filter is incorporated in the output lead from the pi-network circuit. This filter is mounted below deck and is built with no interstage shields. The attenuation of the filter is not quite up to the best standards, but it is sufficient to reduce the higher harmonics of

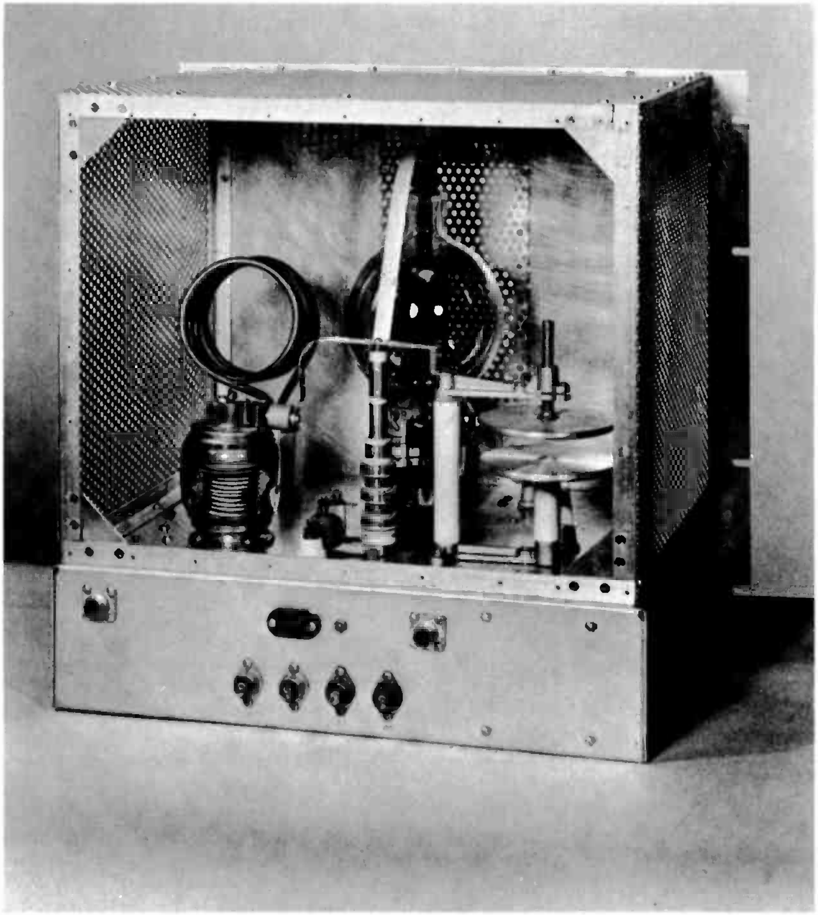


Figure 52
The circuit simplicity may be seen in the rear view of the 450-TH pi-network amplifier

the amplifier stage to insignificant proportions. If higher attenuation of harmonics is desired, the filter should be removed from the amplifier and placed in a separate compartmented box.

The bias and metering circuits for the amplifier are built upon a separate chassis, which is mounted beneath the amplifier. The schematic for this unit is shown in figure 54.

Amplifier Construction The amplifier is built upon an aluminum chassis 13" x 17" x 3" in size (Bud AC-420) and uses a 17½" aluminum relay rack panel. A 4" x 7" port is cut in the panel through which the 450-TH tube may be observed. This opening is covered with a piece of perforated aluminum stock, firmly bolted to the panel. The 450-TH tube socket is centered behind this port and sub-mounted on the chassis so that the rim of the socket is flush with the top of the chassis. The 450-TH socket is mounted on a "U" shaped aluminum bracket 6" long, 3½" wide and 2⅞" high. The Hypass filament capacitors are mounted on the side of this bracket, forming a short, low inductance path to ground for the plate return circuit.

Spaced symmetrically on each side of the tube socket are the grid tuning capacitor C_1 and the antenna loading capacitor C_7. These may be seen in figure 53. Directly behind C_1 is mounted the 7.5-volt filament transformer for the 450-TH. The grid inductor L_1 is mounted

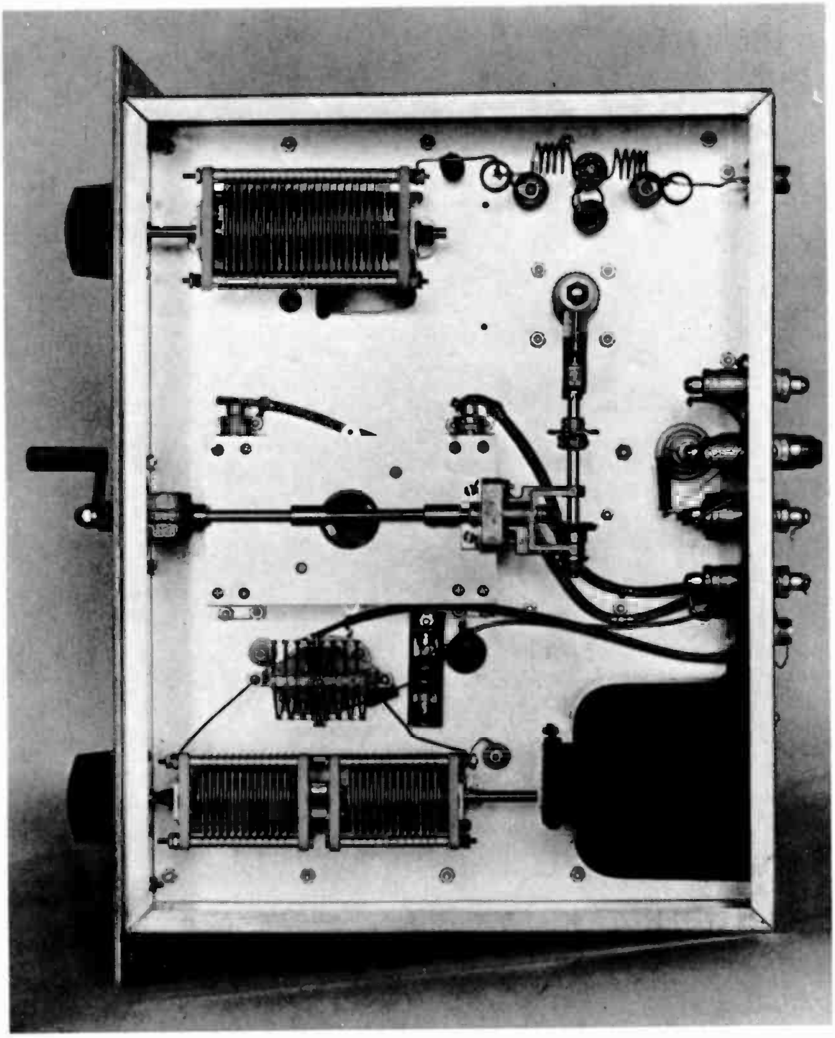


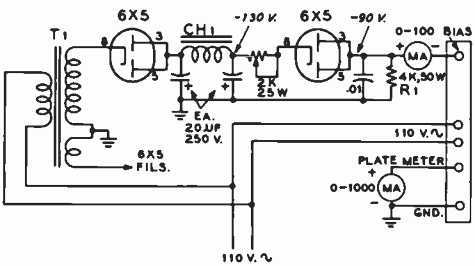
Figure 53

UNDER CHASSIS LAYOUT OF 450-TH AMPLIFIER

Shown at the top of the photograph are the pi-network loading capacitor and the 52-ohm low-pass filter. The gear drive for the variable vacuum capacitor is located at the center of the chassis. Directly below the mount for the 450-TH tube socket is the 50-watt grid inductor and the split-stator grid tuning capacitor. The filament transformer is mounted to the rear edge of the chassis. A perforated aluminum bottom plate completes the TVI-proof enclosure.

in a five prong ceramic socket positioned between C_1 and the tube socket bracket.

Atop the chassis (figure 52), the plate r-f choke is mounted directly behind the 450-TH tube. On each side of the choke are placed the plate circuit components. To the right is the disc-type neutralizing capacitor NC; to the left is the variable vacuum capacitor, mounted in a vertical position. A 60-ampere fuse clip is used to make a low resistance connection to



T1 - 125 V. AT 50 MA - *STANCOR PA-8421*
CH1 - 13 H. AT 65 MA. - *STANCOR C-1708*

Figure 54
BIAS SUPPLY FOR 450-TH PI-NETWORK AMPLIFIER

the stator post of the capacitor. The 5000-volt ceramic plate blocking capacitor is attached to this fuse clip, as is one end of the plate coil, L_2.

The opposite end of L_2 is affixed to a 2" ceramic insulator, and a 1/2" silver plated copper strap runs through a chassis hole connecting L_2 with the loading capacitor C_7 mounted beneath the chassis.

The variable vacuum tuning capacitor is driven by means of a B & W type 3902 cyclometer-type counter dial mounted in the center of the panel, directly below the view port for the 450-TH. Two B & W type 3903 right angle drive units connect the counter dial to the variable vacuum capacitor. The first right angle unit is mounted at the rear of the U-bracket holding the 450-TH tube socket, and the second is mounted between the bracket and the vacuum capacitor.

All under-chassis wiring of the amplifier is enclosed in shielded loom, the shield being grounded to the chassis at each end of the lead. R-f wiring is done with no. 12 enamelled wire, except in the plate circuit of the amplifier, where 1/2" silver plated copper strap is employed. The plate coil L_2 is wound of 1/4" copper tubing. Construction of the shielded enclosure is covered in Chapter 30 of this handbook. The bottom of the amplifier chassis is covered with a 13" x 17" aluminum plate to complete the grid circuit enclosure. A series of 1/4" ventilation holes are drilled in this plate directly below the 450-TH tube socket permitting cooling of the base seal of the 450-TH by convection air currents.

Bias Supply For 2500 or 3000 volt operation, the 450-TH requires a cutoff bias of −90 volts, and an operating bias of −210 volts. Shown in figure 54 is a bias supply capable of meeting these operating conditions. A half-wave supply with a 6X5 rectifier and a capacitor input filter is used to produce −90 volts across the bias resistor R_1. The exact cutoff bias voltage may be set by adjusting the slider of the 2000-ohm series resistor. When the amplifier stage is in operation, the voltage across R_1 rises to −210 volts. A second 6X5 automatically disconnects the bias supply from the grid circuit of the amplifier whenever the voltage across R_1 exceeds the supply voltage of −130 volts. This action protects the filter capacitors in the supply from excessive bias voltage that may perhaps be developed during tuneup of the 450-TH stage. Operation of the cutout circuit is entirely automatic. The only adjustment needed to the supply is to set the voltage across R_1 before the supply is attached to the amplifier stage.

Amplifier Adjustment The bias supply should be connected to the amplifier, and excitation supplied to the 450TH stage until approximately 50 milliamperes of grid current is flowing. A short circuit should be placed across the antenna connector of the amplifier, and the plate tuning capacitor C_6 tuned to resonance as indicated by a kick in the reading of the grid meter. A flashlight bulb coupled to L_2 should indicate presence of r.f. in the plate tank circuit of the amplifier. The neutralizing capacitor NC should be adjusted until minimum r.f. is present in the plate circuit, and no deflection is noted on the grid meter of the amplifier as the plate circuit is tuned through resonance.

The plate voltage lead should now be connected and the amplifier loaded to an antenna. If the amplifier is correctly neutralized, detuning the plate circuit either side of resonance will cause the grid current reading to drop. If grid current increases when the plate tuning capacitor is detuned either side of resonance, the neutralizing capacitor should be varied a small amount until this action ceases. *All adjustments to the amplifier should be made with plate voltage removed from the stage.* Under correct operating conditions, grid current will run 55 milliamperes, and the cathode current 455 milliamperes for 2500 volt operation. Plate current (the difference between these two) will be 400 milliamperes.

Operation on Other Bands As stated before, this amplifier was designed for one band service. It can be operated on other bands, however, by changing the plate and grid circuit inductors. Operation on 15 and 40 meters is possible if the grid inductor L_1 is cut so as to require maximum capacity setting of C_1 for 15 meters. For 40-meter operation L_1 should be cut so as to resonate to 40 meters when each section of C_1 is shunted with a 100-$\mu\mu$fd. 5000-volt ceramic capacitor (Centralab type 850). L_2 should be cut so as to resonate to the desired frequency with C_6 at near maximum capacity. It will be necessary to shunt C_7 with a 500-$\mu\mu$fd., 5000-volt mica capacitor for 40-meter operation. Operation of the amplifier has not been attempted on 10 meters or on 80 meters.

CHAPTER TWENTY SEVEN

Speech and Amplitude Modulation Equipment

Amplitude modulation of the output of a transmitter for radiotelephony may be accomplished either at the plate circuit of the final amplifier, commonly called high-level AM or simply plate modulation of the final stage, or it may be accomplished at a lower level. Low-level modulation is accompanied by a plate-circuit efficiency in the final stage of 30 to 45 per cent, while the efficiency obtainable with high-level AM is about twice as great, running from 60 to 80 per cent. Intermediate values of efficiency may be obtained by a combination of low-level and high-level modulation; cathode modulation of the final stage is a common way of obtaining combined low-level and high-level modulation.

High-level AM is characterized by a requirement for an amount of audio power approximately equal to one-half the d-c input to the plate circuit of the final stage. Low-level modulation, as for example grid-bias modulation of the final stage, requires only a few watts of audio power for a medium power transmitter and 10 to 15 watts for modulation of a stage with one kilowatt input. Cathode modulation of a stage normally is accomplished with an audio power capability of about 20 per cent of the d-c input to the final stage. A detailed discussion of the relative advantages of the different methods for accomplishing amplitude modulation of the output of a transmitter is given in Chapter Twelve.

Two trends may be noted in the design of systems for obtaining high-level AM of the final stage of amateur transmitters. The first is toward the use of tetrodes in the output stage of the high-power audio amplifier which is used as the modulator for a transmitter. The second trend is toward the use of a ***high-level splatter suppressor*** in the high-voltage circuit between the secondary of the modulation transformer and the plate circuit of the modulated stage.

27-1 Modulation

Tetrode Modulators In regard to the use of tetrodes, the advantages of these tubes have long been noted for use in modulators having from 10 to 100 watts output. The 6V6, 6L6, and 807 tubes have served well in providing audio power outputs in this range. Recently the higher power tetrodes such as the 4-65A, 813, 4-125A, and 4-250A have come into more general use as high-level audio amplifiers. The beam tetrodes offer the advantages of low driving power (even down to zero driving power for many applications) as compared to the moderate driving power requirements of the usual triode tubes having equivalent power-output capabilities.

On the other hand, beam tetrode tubes require both a screen-voltage power supply and a grid-bias source. So it still is expedient in many cases to use zero-bias triodes or even low-mu triodes such as the 304TL in many modulators for the medium-power and high-power range. A list of suggested modulator combinations for a range of power output capabilities is given in conjunction with several of the modulators to be described.

Increasing the Effective Modulation Percentage It has long been known that the effective modulation percentage of a transmitter carrying unaltered speech waves was necessarily limited to a rather low value by the frequent high-amplitude peaks which occur in a speech waveform. Many methods for increasing the effective modulation percentage in terms of the peak modulation percentage have been suggested in various publications and subsequently tried in the field by the amateur fraternity. Two of the first methods suggested were Automatic Modulation Control and Volume Compression. Both these methods were given extensive trials by operating amateurs; the systems do give a degree of improvement as evidenced by the fact that such arrangements still are used in many amateur stations. But these systems fall far short of the optimum because there is no essential modification of the speech waveform. Some method of actually modifying the speech waveform to improve the ratio of peak amplitude to average amplitude must be used before significant improvement is obtained.

It has been proven that the most serious effect on the radiated signal accompanying overmodulation is the strong spurious-sideband radiation which accompanies negative-peak clipping. Modulation in excess of 100 per cent in the positive direction is accompanied by no undesirable effects as far as the radiated signal is concerned, at least so long as the linear modulation capability of the final amplifier is not exceeded. So the problem becomes mainly one of constructing a modulator-final amplifier combination such that negative-peak clipping (modulation in excess of 100 per cent in a negative direction) cannot normally take place regardless of any reasonable speech input level.

The speech waveform of the normal male voice is characterized, as was stated before, by high-amplitude peaks of short duration. But it is also a significant characteristic of this wave that these high-amplitude peaks are poled in one direction with respect to the average amplitude of the wave. This is the "lopsided" or assymetrical speech which has been discussed and illustrated in Chapter Twelve.

The simplest method of attaining a high average level of modulation without negative peak clipping may be had merely by insuring that these high-amplitude peaks always are poled in a positive direction at the secondary of the modulation transformer. This adjustment may be achieved in the following manner: Couple a cathode-ray oscilloscope to the output of the transmitter in such a manner that the carrier and its modulation envelope may be viewed on the scope. Speak into the microphone and note whether the sharp peaks of modulation are poled upward or whether these peaks tend to cut the baseline with the "bright spot" in the center of the trace which denotes negative-peak clipping. If it is not obvious whether or not the existing polarity is correct, reverse the polarity of the modulating signal and again look at the envelope. Since a push-pull modulator almost invariably is used, the easiest way of reversing signal polarity is to reverse either the leads which go to the grids or the leads to the plates of the modulator tubes.

When the correct adjustment of signal polarity is obtained through the above procedure, it is necessarily correct only for the specific microphone which was used while making the tests. The substitution of another microphone may make it necessary that the polarity be reversed, since the new microphone may be connected internally in the opposite polarity to that of the original one.

Low-Level Speech Clipping The low-level speech clipper is, in the ideal case, a very neat method for obtaining an improved ratio of average-to-peak amplitude. Such systems, used in conjunction with a voice-frequency filter, can give a very worthwhile improvement in the effective modulation percentage. But in the normal amateur transmitter their operation is often less than ideal. The excessive phase shift between the

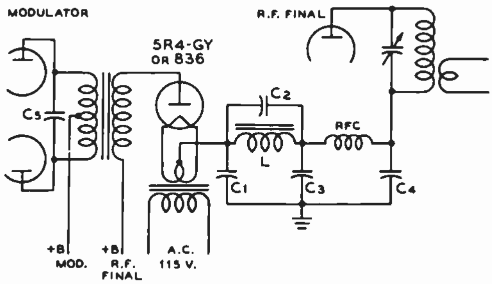


Figure 1
HIGH-LEVEL SPLATTER SUPPRESSOR

The high-vacuum diode acts as a series limiter to suppress negative-peak clipping in the modulated r-f amplifier as a result of large amplitude negative-peak modulating signals. In addition, the low-pass filter following the diode suppresses the transients which result from the peak-clipping action of the diode. Further, the filter attenuates all harmonics generated within the modulator system whose frequency lies above the cut-off frequency of the filter. The use of an appropriate value of capacitor, determined experimentally as discussed in Chapter Twelve, across the primary of the modulation transformer (C_5) introduces further attenuation to high-frequency modulator harmonics. Chokes suitable for use at L_1 are manufactured by Thordarson. The correct values of capacitance for C_1, C_2, C_3, and C_4 are specified on the installation sheet for the splatter suppressor chokes for a wide variety of operating conditions.

low-level clipper and the plate circuit of the final amplifier in the normal transmitter results in a severe alteration in the square-wave output of the clipper-filter which results from a high degree of clipping. The square-wave output of the clipper ends up essentially as a double saw-tooth wave by the time this wave reaches the plate of the modulated amplifier. The net result of the rather complex action of the clipper, filter, and the phase shift in the succeeding stages is that the low-level speech clipper system *does* provide an improvement in the effective modulation percentage, but it *does not* insure against overmodulation. An extensive discussion of these factors, along with representative waveforms, is given in Chapter Twelve. Circuits for some recommended clipper-filter systems will also be found in Chapter Twelve.

High-Level Splatter Suppressor One practicable method for the substantial elimination of negative-peak clipping in a high-level AM transmitter is the so-called *high-level splatter suppressor.* As figure 1 shows it is only necessary to add a high-vacuum rectifier tube socket, a filament transformer and a simple low-pass filter to an existing modulator-final amplifier combination to provide high-level suppression.

The tube, V_1, serves to act as a switch to cut off the circuit from the high-voltage power supply to the plate circuit of the final amplifier as soon as the peak a-c voltage across the secondary of the modulation transformer has become equal and opposite to the d-c voltage being applied to the plate of the final amplifier stage. A single-section low-pass filter serves to filter out the high-frequency components resulting from the clipping action.

Tube V_1 may be a receiver rectifier with a 5-volt filament for any but the highest power transmitters. The 5Y3-GT is good for 125 ma. plate current to the final stage, the 5R4-GY and the 5U4-G are satisfactory for up to 250 ma. For high-power high-voltage transmitters the best tube is the high-vacuum transmitting tube type 836. This tube is equivalent in shape, filament requirements, and average-current capabilities to the 866A. However, it is a vacuum rectifier and utilizes a large-size heater-type dual cathode requiring a warm-up time of at least 40 seconds before current should be passed. The tube is rated at an average current of 250 ma. For greater current drain by the final amplifier, two or more 836 tubes may be placed in parallel.

The filament transformer for the cathode of the splatter-suppressor tube must be insulated for somewhat more than twice the operating d-c voltage on the plate modulated stage, to allow for a factor of safety on modulation peaks. A filament transformer of the type normally used with high-voltage rectifier tubes will be suitable for such an application.

27-2 Design of Speech Amplifiers and Modulators

A number of representative designs for speech amplifiers and modulators is given in this chapter. Still other designs are included in the descriptions of other items of equipment in other chapters. However, those persons who wish to design a speech amplifier or modulator to meet their particular needs are referred to Chapter Six, *Vacuum Tube Amplifiers,* for a detailed discussion of the factors involved in

Figure 2
TOP VIEW OF THE
6L6 MODULATOR

the design of such amplifiers, and for tabular material on recommended operating conditions for voltage and power amplifiers.

15 to 50 Watt Modulator with 6L6 Tubes It is difficult to surpass the capabilities of the reliable 6L6 tube when an audio power output of 25 to 50 watts is required of a modulator. A pair of 6L6 tubes operating in such a modulator will deliver good plate circuit efficiency, require only a very small amount of driving power, and they impose no serious grid-bias problems.

Circuit Description Included on the chassis of the modulator shown in figures 2 and 3 are the speech amplifier, the driver and modulation transformers for the output tubes, and a plate current milliammeter. The power supply has not been included. The 6SJ7 pentode first stage is coupled through the volume control to the grid of a 6J5 phase inverter. The output of the phase inverter is capacitively coupled to the grids of a 6SN7-GT which acts as a push-pull driver for the output tubes. Transformer coupling is used between the driver stage and the grids of the output tubes so that the output stage may be operated either as a class AB_1 or class AB_2 amplifier.

The Output Stage Either 6L6, 6L6-G or 1614 tubes may be used in the output stage of the modulator. As a matter of fact, either 6V6-GT or 6F6-G tubes could be used in the output stage if somewhat less power output is required. The 1614 tube is the transmitting-tube counterpart of the 6L6 and carries the same ratings and recommended operating conditions as the 6L6 within the ratings of the 6L6. But the 1614 does have

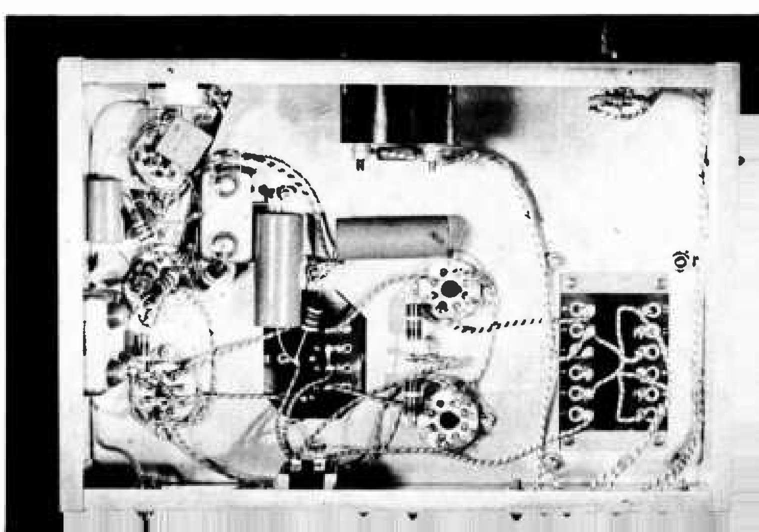


Figure 3
UNDERCHASSIS OF THE
6L6 MODULATOR

A 4-connector plug is used for filaments and plate voltage to the speech amplifier, while a 6-wire terminal strip is used for the high-voltage connections and the transmitter-control switch.

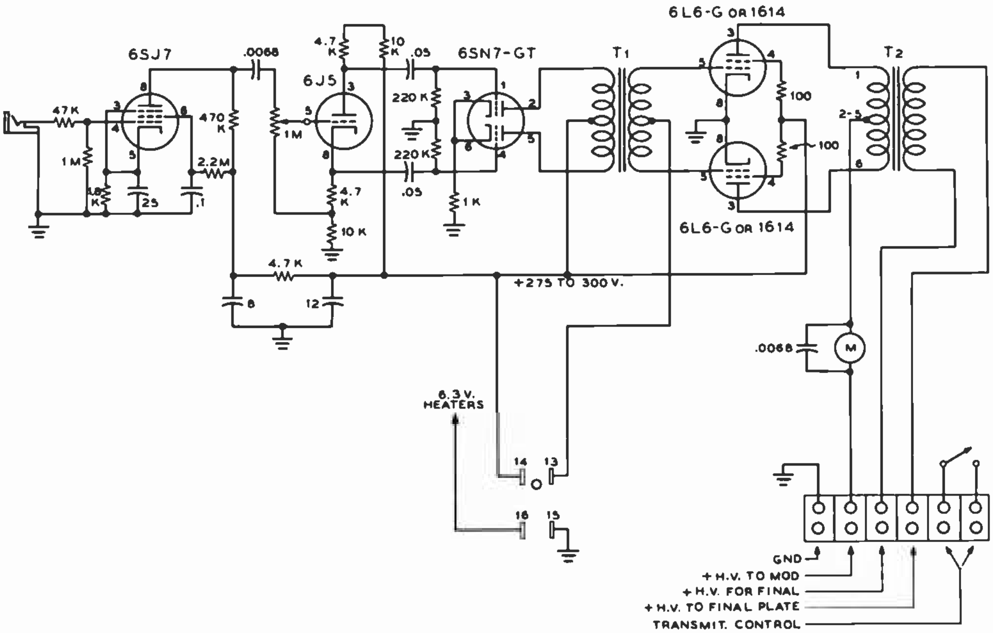


Figure 4

SCHEMATIC OF THE 6L6 MODULATOR

M—0-250 d-c milliammeter (Simpson model 127)
T_1—Driver transformer to 6L6 grids (UTC S-10)
T_2—60-watt modulation transformer (UTC S-20)

somewhat greater maximum ratings when the tube is to be used for ICAS (Intermittent Commercial and Amateur Service) operation. The 6L6 and 1614 retail to the amateur for essentially the same price, although the 1614 is available only from transmitting tube distributors. The 6L6-G tube retails for a somewhat lower price; hence it is expedient to purchase 6L6-G tubes if 360 to 400 volts is the maximum to be used on the output stage, or to purchase 1614 tubes if up to 550 volts will be applied.

Tabulated below are a group of recommended operating conditions for different tube types in the output stage of the modulator. In certain sets of operating conditions the tubes will be operated class AB_1, that is with increased plate current with signal but with no grid current. Other operating conditions specify class

Tubes	Class	Plate Voltage	Screen Voltage	Grid Bias	Plate-to-Plate Load	Zero-Sig. Plate Cur.	Max.-Sig. Plate Cur.	Power Output
6V6-GT	AB_1	285	285	-19	8000	70	92	14
6F6-G	AB_2	375	250	-26	10000	34	82	20
6L6-G	AB_1	360	270	-22.5	6600	88	132	26.5
6L6-G	AB_2	400	275	-22.5	3800	90	210	50
1614	AB_1	530	340	-36	7200	60	160	50
1614 or 807	AB_2	500	300	-30	4250	60	240	75
807	AB_2	750	300	-32	6950	60	240	120

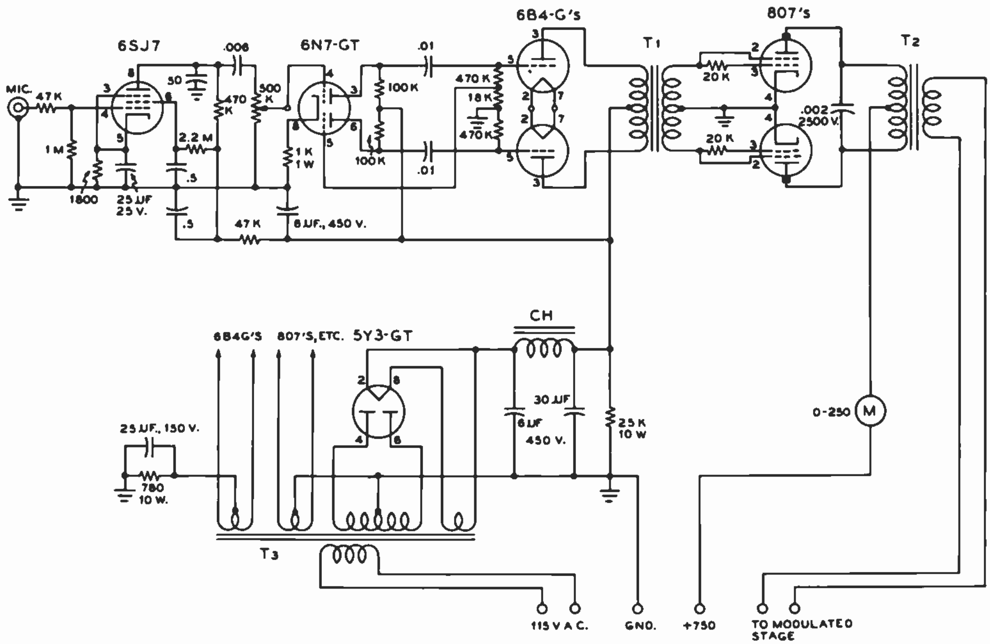


Figure 5
SCHEMATIC OF AN 807-TRIODE 120-WATT CLASS B MODULATOR

T_1—Step-up driver transformer; 1 to 1 total pri. to ½ sec. approx. (UTC type S-9, reverse connected, may be used.)

T_2—125-watt modulation transformer (UTC CVM-3)
T_3—750 v. c.t., 100 ma.; 5 v. 3 a., 6.3 v. 2 a.; 6.3 v. 4 a. (UTC R-12)
CH—14-hy. 100-ma. filter choke (UTC R-19)

AB_2 operation, in which the plate current increases with signal and grid current flows on peaks. Either type of operation is quite satisfactory for communication work. All operating conditions for 50 watts output and less are suitable for use with the output transformer specified. The operating conditions for power outputs greater than 50 watts are shown to illustrate the fact that the driver stages are capable of exciting the specified tubes to the greater power outputs; however, an output transformer with a power-handling rating greater than the unit specified (see caption to figure 4) will be required.

27-3 120-Watt Modulator With Triode-Connected 807's

Through use of the principles disclosed by Seybold in his patent no. 2,494,317 it is possible to operate beam-tetrode tubes such as the 6AQ5, 7C5, 6V6, 6L6, and 807 in such a manner that neither a grid-bias supply nor a screen-voltage supply is required. Yet the tubes operate with moderate driving power and with excellent plate circuit efficiency. The tubes essentially are operated as high-mu zero-bias triodes, with the excitation voltage applied to the screen grids, and through resistors to the control grids.

The system also is well suited to use with type 807 tubes in a modulator with a power output capability of about 120 watts. The schematic of the modulator is given in figure 5. Note that the peak audio signal voltage per grid is about 280 volts. This means that a step-up transformer must be used between the plates of the 6B4-G drivers and the screens of the 807's, even though the 807 tubes operate in true Class B. The effective driving impedance of the 807's is about 30,000 ohms, screen-to-screen. Hence, for optimum opera-

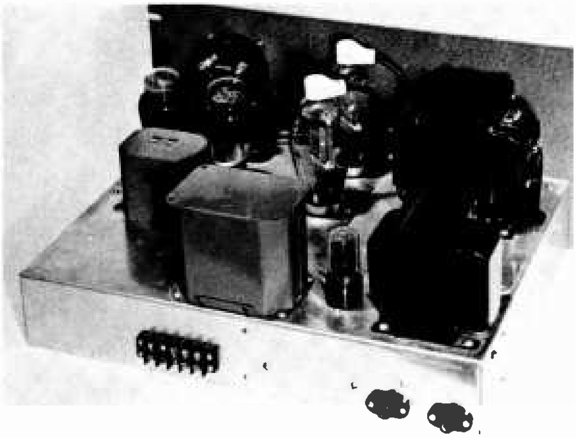


Figure 6
REAR VIEW OF THE GENERAL-PURPOSE MODULATOR

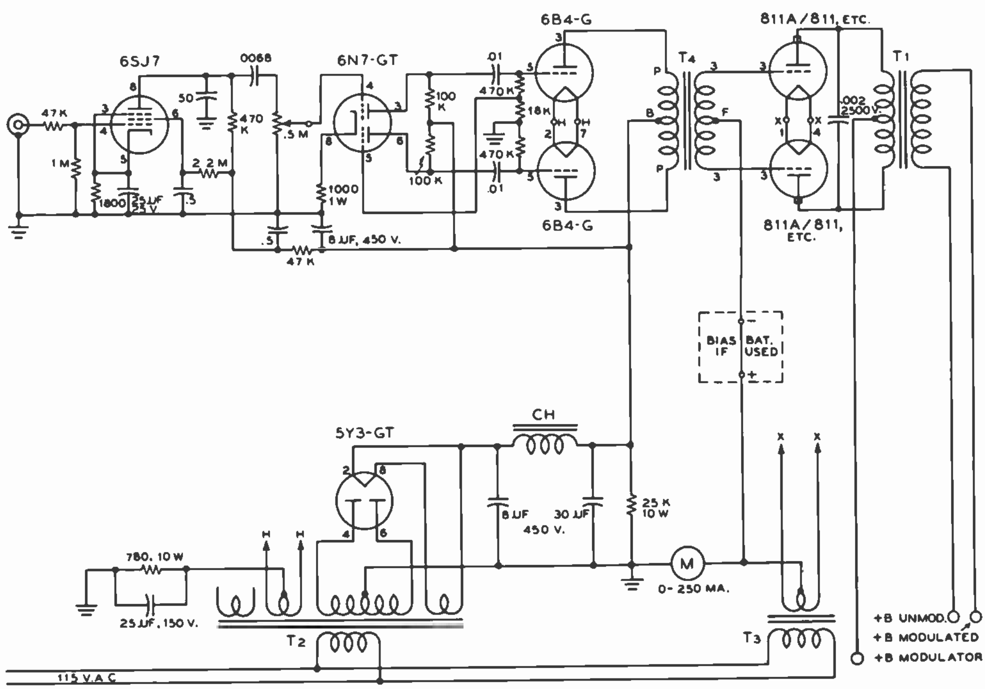


Figure 7
SCHEMATIC OF THE GENERAL-PURPOSE CLASS B MODULATOR

T_1—125 to 400 watt modulation transformer, depending upon tubes used

T_2—750 v. c.t., 100 ma.; 5 v. 3 a.; 6.3 v. 2 a.; 6.3 v. 4 a. (UTC R-19)

T_3—Suitable for tubes used. (UTC S-70 used with windings in parallel for type 811 or 811A tubes)

T_4—Push-pull drivers to Class B grids (UTC S-9)

CH—14-hy. 100-ma. filter choke (UTC R-19)

Figure 8

SUGGESTED OPERATING CONDITIONS

TUBE TYPE	PLATE VOLTAGE	GRID BIAS	ZERO-SIG. PLATE CUR.	MAX.-SIG. PLATE CUR.	PLATE-TO PLATE LOAD	SINE-WAVE POWER OUTPUT
807 (hi-μ triode)	750	0	10	230	7500	120
809	500	0	40	250	3750	85
809	600	0	55	210	6000	85
809	700	0	70	250	6200	120
809	750	-4.5	40	200	8400	105
809	1000	-9	40	200	11,600	145
811	1250	0	48	200	14,400	175
811	1250	0	48	240	12,000	210
811	1500	-9	20	200	17,600	220
811A	750	0	32	350	5100	178
811A	1000	0	44	350	7400	248
811A	1250	0	50	260	12,400	235
811A	1250	0	50	350	9200	310
811A	1500	-4.5	32	313	12,400	340
805	1250	0	148	400	6700	300
805	1500	-16	84	400	8200	370
5514	1000	0	64	350	6500	260
5514	1250	0	84	350	8400	320
5514	1500	-4.5	50	350	10,500	400

tion of the 2A3 or 6B4-G driver tubes, the driver transformer should have a step-up ratio, total primary to total secondary, of approximately 2 to 1. Driving power required at the input of the 807's is about 5.5 watts.

The 807's operate at a plate-circuit efficiency slightly greater than 70 per cent with full signal. No-signal plate current will be in the vicinity of 10 ma., and full-signal plate current with sine-wave output of 120 watts will be about 230 ma. Maximum-signal plate current with a voice signal will depend upon the amount of clipping which precedes the driver stage.

27-4 General Purpose Class B Modulator

High-level Class B modulators with power outputs in the 125 to 400 watt range usually make use of zero-bias triodes such as the 809, 811, 805 or 5514, with operating plate voltages between 750 and 1500 volts. Figures 6 and 7 illustrate a modulator unit designed for operation in this power range. Figure 8 gives a group of suggested operating conditions for the tubes specified above. The driver unit and driver power supply are adequate for any of the operating conditions specified, including the use of the 807 tubes as high-mu Class B triodes.

Circuit Description The modulator unit is complete as diagrammed in figure 7 except for the high-voltage power supply which feeds the modulator tubes. A speech amplifier-driver, suitable for operation from a crystal microphone, is included on the chassis along with its power supply. The 6SJ7 preamplifier stage feeds a 6N7-GT phase inverter which in turn supplies signal to the grids of the push-pull 6B4-G drivers. The driver stage is coupled to the grids of the modulator tubes through a conventional multi-purpose driver transformer.

The modulator chassis includes a filament supply for the modulator tubes, and a plate supply for the speech amplifier and driver. No grid bias supply for the modulators is included since all the modulator tubes specified operate either with zero bias, or with a value of bias low enough so that it may conveniently be supplied by one or two small C batteries of the 4½-volt type, or from a tapped 22½-volt battery.

27-5 An Outboard Clipper-Filter for the Phone Transmitter

It is very hard to maintain a high level of modulation with an audio signal having such irregular peaks as a voice wave without the danger of persistent overmodulation. It is usually necessary to keep the average modulation level of the transmitter below 40 per cent to prevent the voice peaks from overmodulating the transmitter. In addition, with some of the more inexpensive commercially produced amateur transmitters enough audio harmonic distortion is generated even at low modulation levels to produce a broad signal with many kilocycles of sidebands. When such a transmitter is overmodulated, the results are intolerable to amateurs living within a radius of several miles of the offending transmitter.

It is possible by the combined use of low-level clipping and filtering and high-level filtering to restrict the sidebands of a normal transmitter to less than 8 or 10 kilocycles. Since most home-built and commercial transmitters do not incorporate any means to limit the modulation level, an auxiliary unit must be added to the transmitter to accomplish this action. In addition to limiting the "nuisance bandwidth" of the transmitter, such a unit will increase the useable modulation level of the transmitter, adding a worthwhile 8 to 10-db of audio "punch" to the signal that is extremely effective under QRM-conditions.

A practical low-level clipper-filter unit is illustrated in figures 9, 10 and 11.

Circuit of the Low-Level Clipper-Filter The outboard clipper-filter unit employs two tubes. A 12AX7 is used as a two stage resistance coupled amplifier to build up the voltage output of a low level crystal microphone to a level sufficient for clipping purposes. An audio level control, R_1, in the grid circuit of the second half of the 12AX7 controls the gain of the clipper-filter unit. A very small value of coupling capacitor (470 $\mu\mu$fd.) is employed between the two sections of the 12AX7 to limit the low frequency response of the unit. This tends to maintain a proper level of balance between the high and low frequencies present in the normal human voice, and also tends to reduce the effects of low frequency phase-shift in stages following the clipper-filter. A r-f filter network is incorporated in the 12AX7 input circuit to reduce any tendency towards r-f feedback in the clipper audio system.

A 6AL5 double diode is used as a series clipper tube. The clipping level may be adjusted by varying the plate potential of the diodes by means of R_2. The output from the clipper is smoothed and filtered by LPF-2, a low-pass audio filter, having a cut-off frequency of approximately 3500 cycles. The particular filter used in this unit is a Chicago Transformer Co. model LPF-2. Other filters may be used in its place, but it would be wise to test any substitution with a square wave audio oscillator and an oscilloscope. Some makes of low-pass audio filters are not designed to follow a clipping stage, and they have a tendency to "ring," or to put "spikes" on the clipped waveform. This action will cause a very violent sideband splatter to appear on the transmitted signal and will make the sidebands of the transmitter broader with the clipper-filter in the circuit than when it is removed!

The clipper-filter requires a plate supply of approximately 170 volts at 25 milliamperes. This is easily provided by a broadcast replacement-type selenium rectifier and a midget half-

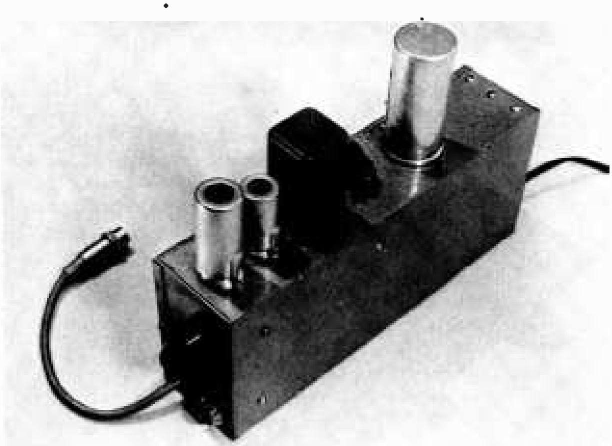


Figure 9
THE CLIPPER FILTER UNIT

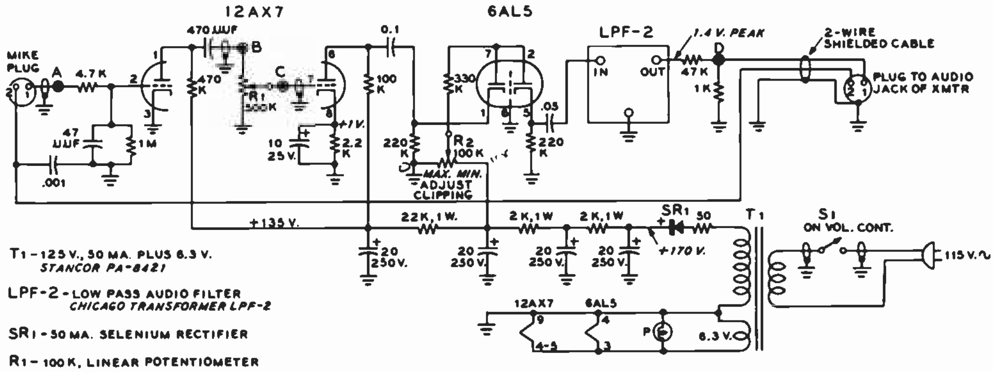


Figure 10
OUTBOARD SPEECH CLIPPER-FILTER UNIT

wave power supply transformer. Since a high degree of ripple is passed by a half-wave rectification system, it is necessary to employ a three section R-C filter to completely eliminate any hum from the low level stages of the clipper-filter unit.

The clipper-filter unit has an audio signal output of about 1.4 volts peak-to-peak under conditions of maximum clipping. Since the clipper is intended to be placed between the crystal microphone and the microphone jack of the transmitter, it is necessary to reduce the output of the unit to the level of the crystal microphone. This is easily done with a simple voltage divider placed after the low-pass filter.

Since many of the modern transmitters are equipped with a two circuit microphone jack for a push-to-talk circuit, a similar installation was made in the clipper-filter unit. The push-to-talk circuit (pin no. 2 of microphone jack) is merely routed around the clipper-filter unit and connected directly to pin no. 2 of the output plug of the unit. If possible, the clipper-filter unit should be connected to the transmitter in such a way so that when the filament circuits of the transmitter are energized, the primary power is applied to the clipper-filter. If this is done, the primary switch, S_1, of the clipper-filter unit may be omitted.

Construction The complete clipper-filter unit is built within an aluminum box measuring 10"x 4"x 2½" (California Chassis Co.) and is designed to be bolted to the side of either a Collins 32V or Johnson Viking transmitter. If it is desired to make the unit a table item, it may be built on a Bud 7"x 7"x 1½" chassis (CB-41) and placed within a Bud C-973 cabinet. However, the type of construction shown in figure 9 makes a very compact unit which may be bolted to the side of an existing transmitter by means of four 6-32 machine screws.

The placement of parts may be seen in figures 9 and 11. On the front of the unit are the pilot lamp, the two wire shielded connector cord that goes to the microphone jack of the transmitter, the audio level control, R_1, and the microphone jack. Atop the box are the 12AX7 and 6AL5 tubes followed by the LPF-2 filter-unit. Behind the filter is the clipping level control, R_2, and the four section 20-μfd. filter capacitor can. The 110-volt power cable comes out the back of the box.

Interior placement of parts is shown in figure 11. Connections between the panel controls which are located on one half of the box, and the rest of the components on the other half of the box are made by means of leads that terminate in a six point phenolic tie-point strip. The leads that terminate on this strip are designated A, B, C and D in figure 10. Another tie-point terminal is used for the ground lead from the removable box side. Audio leads A, B and C are run in shielded wire to prevent hum pick-up from the six volt lead to the pilot lamp mounted on the front panel, or hum from the 110-volt leads to S_1 which is mounted on the back of R_1.

The half-wave power transformer, T_1, is mounted within the box on one wall, and the selenium rectifier, SR_1, is mounted on a small angle bracket to the bottom of the box. Most of the small resistors and capacitors may be mounted directly to the pins of the respective tube sockets, or to small phenolic tie-point strips mounted adjacent to the sockets. The resistors comprising the R-C network in the

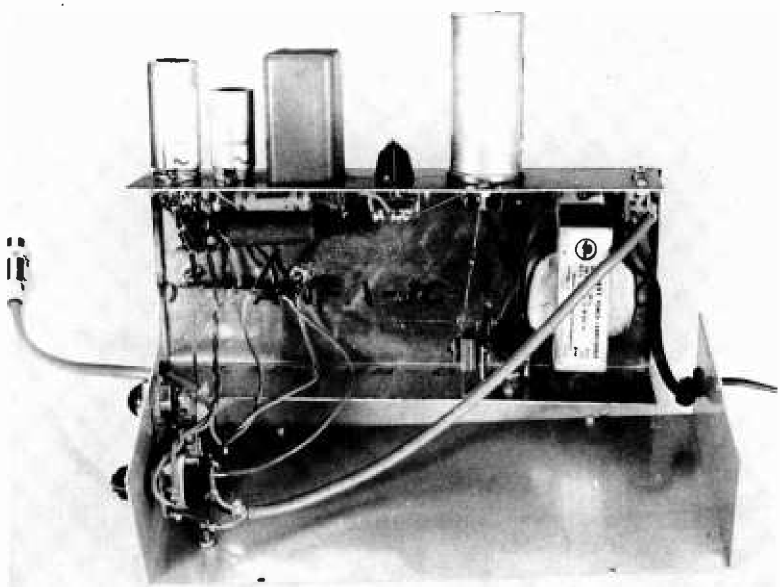


Figure 11
INTERIOR VIEW OF CLIPPER-FILTER UNIT

high voltage supply may be mounted directly on the terminals of the four section filter capacitor.

Adjustment When the unit has been wired and tested, it is attached to the transmitter it will be used with, and power should be applied to the filter-clipper unit. The clipping level control should be set for *minimum clipping* (see figure 10) and R_1 set at the ground end. The audio gain control of the transmitter should be set at the position used under normal conditions. The microphone should be plugged into the microphone jack of the clipper-filter unit. The transmitter should be put on the air, and if an oscilloscope is not handy, the services of a nearby amateur should be enlisted to help adjust the correct modulation and clipping level of the transmitter.

As the first step, R_1 should be advanced until normal modulation of the transmitter takes place. (R_2 is adjusted for minimum clipping.) The spread of the sidebands of the transmitter should be carefully noted. As the transmitter is voice modulated, R_2 should be advanced, bringing the clipping circuit into play. It will be noticed that as more clipping is brought into action, the maximum reading of the modulation meter in the transmitter will tend to decrease. When R_2 is set for maximum clipping, the modulation meter of the transmitter may only advance to perhaps 1/3 of the usual reading encountered with no clipping. At the same time, the modulation will sound boomy and unpleasant. R_2 should be backed off from maximum clipping until a point is found at which the sidebands are sharp, and splatter is at a minimum. This point is a function of the setting of R_2 and the setting of the gain control *of the transmitter.* The gain control of the transmitter should be adjusted so that proper sideband limitation starts with R_2 set at about mid-scale. Once this adjustment has been found, the transmitter gain control should be locked and all gain adjustments made with R_1 of the clipper-filter.

When this procedure is followed, R_2 and the transmitter gain control put an upper limit on the modulation level. No matter how heavily the operator tries to modulate the transmitter, only a pre-set maximum modulation level will be possible. The actual microphone gain will be set by R_1, and not by the gain control of the transmitter.

It must be remembered that the operator is at the mercy of the individual who is monitor-

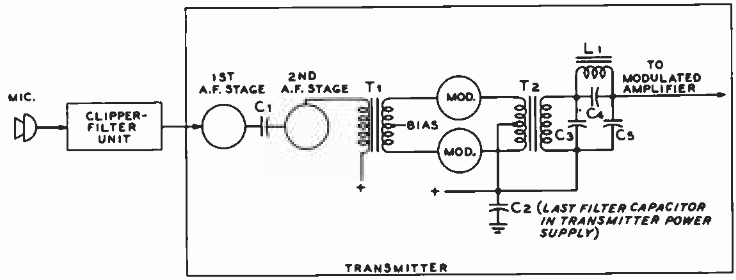


Figure 12

TRANSMITTER MODIFICATIONS FOR EFFECTIVE SPEECH CLIPPING ACTION

ing the signal when this adjustment process is followed. Care should be taken that the monitor chosen is a good judge of when a signal sounds "broad" and when it does not. The monitor should also be careful that his receiver is not being overloaded when these tests are being conducted. If an oscilloscope is available, it should be connected to the transmitter to provide a trapezoidal pattern as explained in Chapter Eight, and the clipper-filter unit adjusted for 90 per cent modulation of the transmitter with a sine-wave audio signal impressed upon the clipper. It will be found from on-the-air checks that when the clipper circuit is adjusted either by ear or by the oscilloscope, a final "touching up" of R_2 will drop the sideband splatter to a minimum level. In addition, the modulation level will sound full and heavy with the clipper-filter in use, and "flat" when the unit is removed from the circuit.

Unfortunately, not all transmitters are capable of 100 per cent modulation, regardless of whether or not the clipper-filter is used. One popular commercial amateur transmitter was only capable of 30 per cent modulation before the sideband splatter became objectionable. In such a case, modifications must be made to the transmitter to make the use of the clipper-filter worthwhile.

Practical Use of the Clipper-Filter It will be found that the advantages of clipping and filtering are diluted to a greater or less extent by the audio equipment of the transmitter with which the clipper-filter unit is used. With some transmitters, the addition of the unit makes a marked difference. The speech is crisp and clear, the modulation is heavy and the transmitter sidebands are noticeably narrow when compared to sidebands of unclipped signals. With other transmitters the improvement in modulation level and the sharpening of the sidebands is not so apparent. The results, then, are a function of the excellence of the audio system of the transmitter. A typical modulation system for a 120 watt transmitter is shown in figure 12. The clipper-filter unit is to be added to this transmitter. What portions of the transmitter audio system might cause the excellent clipping action to deteriorate, and what can be done to alleviate the trouble?

The first step should be to examine the audio coupling capacitors (C_1) in the speech amplifier of the transmitter. These should be removed and replaced with 0.1 μfd. coupling capacitors, if they are smaller in value than this. Low frequency phase-shift in the speech amplifier will be lessened by such action. The coupling transformer (T_1) between the modulators and the driver stage should be examined. If it is a puny transformer with little iron, it should be removed and replaced with a higher grade unit. If the modulation transformer, T_2, "talks back" under modulation, it should be replaced with a better unit.

Attention should be turned to the output filter capacitor, C_2, in the modulator plate supply. If the capacity of this unit is insufficient, the modulator will not be able to deliver the required audio power on modulation peaks. It should be shunted with a capacitor of 10 μfd. to 20 μfd. to provide a low impedance source of plate voltage for the modulator stage.

The final, and most important step is to see that any audio harmonic distortion generated *after* the low level filter is suitably attenuated before the audio signal is impressed upon the r-f amplifier stage. A single section low pass filter between the modulator stage and the modulated stage will attenuate audio harmonics above 3500 cycles some 15 db to 25 db. L_1,

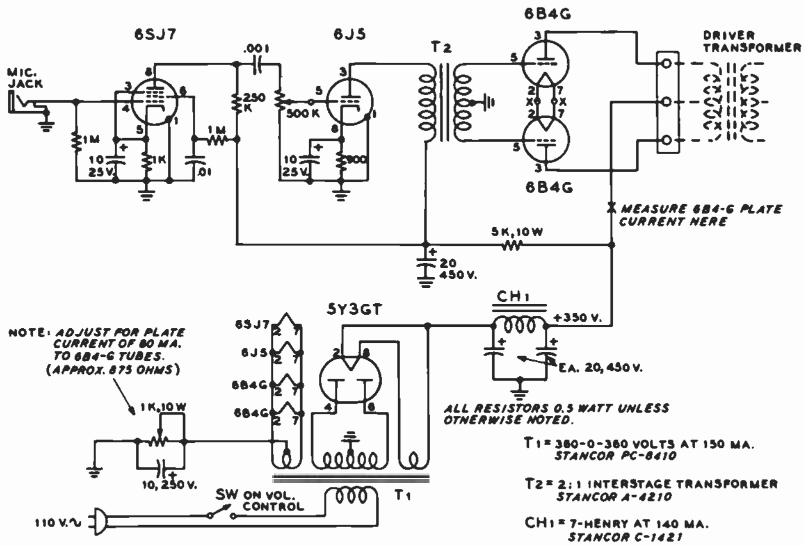


Figure 13

10-WATT SPEECH AMPLIFIER-DRIVER

C_3, C_4 and C_5 comprise such a filter. This filter will "clean up" most of the sideband components generated in the modulator of the transmitter.

Just such a housecleaning program was tried on a 120 watt phone transmitter. Under observation on the air, the operator of the transmitter was modulating approximately 150 per cent as near as could be observed on an oscilloscope, and the transmitter blanketed a radius of more than five miles with several hundred kilocycles of sideband splatter. Upon reducing the modulation to a point where the sideband splatter was only 20 kilocycles or so, it was found that the transmitter was only being modulated about 30 per cent. Any modulation over this value produced excessive sidebands. A clipper-filter was tried, with no success. A high level filter of the type shown in figure 12 was added, which allowed modulation up to about 70 per cent before sideband splatter was excessive. The other circuit changes shown in figure 12 allowed approximately 90 per cent modulation with 10 db of clipping. At this level, the signal was extremely clean and sharp. The main cause for the distressing action of this transmitter was the generation in the audio system of excessive harmonics, which when applied to the r-f amplifier produced sideband splatter. The illustrated changes reduced the audio harmonic distortion to an acceptable value.

27-6 A 10-Watt Amplifier-Driver

A simple speech amplifier-driver for a medium powered class B modulator is shown in figure 13. The amplifier is designed to work with a crystal microphone. The first stage utilizes a 6SJ7. The gain control is between the 6SJ7 plate circuit and the grid of the 6J5 second stage amplifier. The output tubes are a pair of 6B4-G low-mu tubes operating with a self-bias resistor in their common filament return circuit. Operating in this manner the 6B4's have an undistorted output of approximately 10 watts. This is sufficient power to drive most class-B modulators whose output is 400 watts or less. The driver transformer for coupling the plates of the 6B4-G tubes to the grids of the Class B stage is not shown, as it had been found more convenient to locate this transformer at the grids of the modulator tubes rather than in the speech amplifier. The correct transformer step-down ratio for driving

Figure 14
DE LUXE 15-WATT SPEECH AMPLIFIER-DRIVER

most class B tubes has been set down in tabular form by the various transformer manufacturers. When the driver transformer is purchased one should be obtained which has the proper turns ratio for the class B tubes to be used.

A three wire shielded cable should be used to connect the 6B4-G tubes to the driver transformer located at the grids of the class B tubes. This cable may be any reasonable length up to 25 or 30 feet. Any of the modulator configurations shown in figure 8 may be driven with this simple speech amplifier.

27-7 A De-Luxe 15 Watt Amplifier-Driver

Illustrated in figures 14, 15 and 16 is a 15-watt speech amplifier-driver which incorporates a low level clipper-filter circuit of the type described in section 27-3. This unit was specifically designed to drive a pair of push-pull 810 modulator tubes delivering 500 watts of clipped and filtered audio. A pair of fixed biased 6B4-G tubes are used as drivers for the class B modulator stage.

Circuit Description The speech amplifier schematic is shown in figure 15. A 12AX7 tube is used as a two stage microphone pre-amplifier and delivers approximately 20 volts (r.m.s.) audio signal to the 6AL5 series clipper tube. The clipping level is adjustable between 0 db and 15 db by clipping control, R_2. Amplifier gain is controlled by R_1, in the grid circuit of the second section of the 12AX7. A low pass filter having a 3500 cycle cut-off follows the 6AL5 clipper stage, with an output of 5 volts peak audio signal under maximum clipping conditions. A double-triode 12AU7 cathode follower phase-inverter follows the clipper stage and delivers a 125 volt r.m.s. signal to the push-pull grids of the 6B4-G audio driver tubes. The 6B4-G tubes operate at a plate potential of 330 volts and have a -68 volt bias voltage developed by a

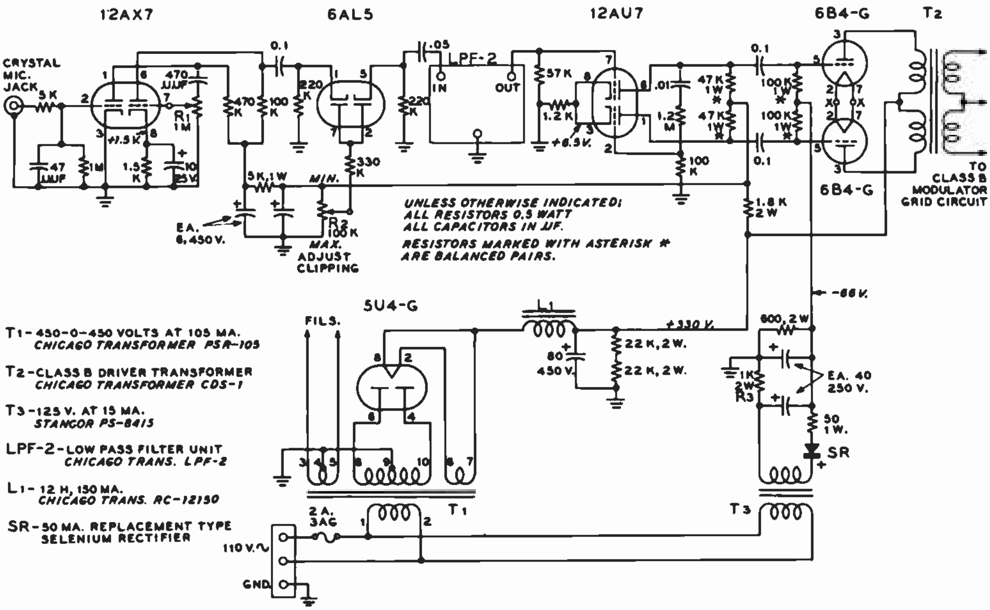


Figure 15

SCHEMATIC OF DE LUXE 15-WATT SPEECH AMPLIFIER

small selenium rectifier supply applied to their grid circuit. An audio output of 15 watts is developed across the secondary terminals of the class B driver transformer with less than 5 per cent distortion under conditions of no clipping. A 5U4-G and a choke input filter network provide unusually good voltage regulation of the high voltage plate supply.

Construction The De-Luxe speech amplifier is constructed upon a 10" x 17" x 3" aluminum chassis (Bud AC-416). An 8¾" aluminum panel (Bud PA-1105) is affixed to the chassis by two triangular mounting brackets (Bud MB-1266). Placement of parts above the chassis may be seen in figure 14. The power supply components are to the rear of the chassis. At the extreme left is the plate transformer. Next to it is the 5U4-G rectifier tube, and to the right of the tube are the high voltage filter choke and the 80-μfd. filter capacitor.

The audio components are arranged along the front of the chassis. From right to left are the 12AX7 speech amplifier, the 6AL5 clipper tube with R_2 between it and the filter capacitor, the low pass filter, the 12AU7 phase inverter and the 6B4-G driver tubes. In the far left corner is the class B driver transformer.

Mounting of the below deck components is shown in figure 16. To the right are the cutouts in the chassis for the leads to the driver transformer and the power transformer. At the lower left of the chassis is the bias rectifier transformer, T_3. The audio gain control knob (R_1) is visible directly above the 6AL5 tube socket, next to the microphone jack on the front panel. Placement of parts beneath the chassis is not particularly critical, except that the power supply components should be grouped around the rear of the chassis to separate them as far as possible from the low level stages of the speech amplifier. All capacitors and resistors of the audio section should be mounted as close to the respective sockets as is practical. The 0.1 μfd. coupling capacitors between the 12AU7 phase inverter and the grid terminals of the 6B4-G tube sockets may be mounted directly to the socket pins of the 12AU7 and 6B4-G sockets. For minimum hum pick-up, the filament leads to all audio tubes should be twisted and dressed closely to the chassis.

Those resistors in the 12AU7 phase inverter plate circuit and the grid circuit of the 6B4-G tubes should be matched for best phase inverter balance. The exact value of the paired

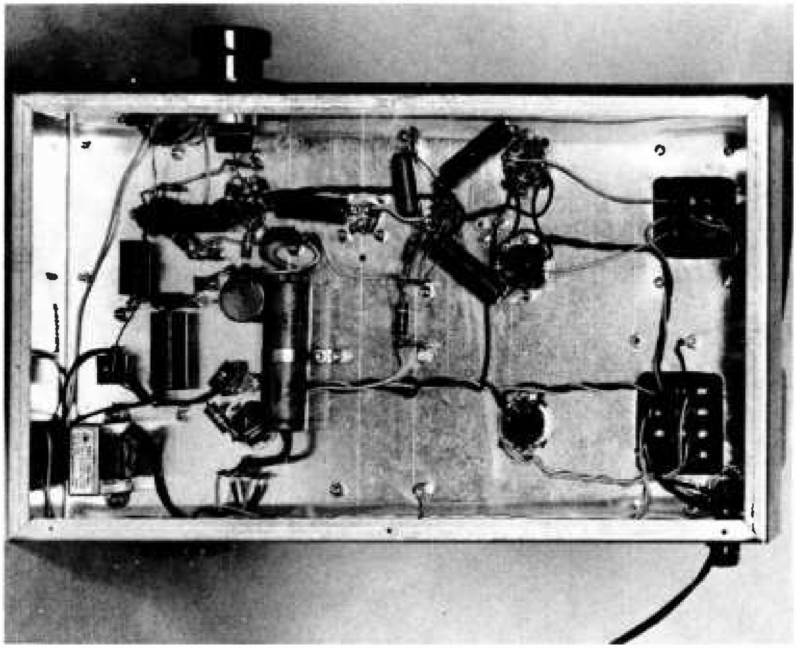


Figure 16
BOTTOM VIEW OF 15-WATT SPEECH AMPLIFIER

resistors is not important, but care should be taken that the values are equal. Random resistors may be matched on an ohmmeter to find two units that are alike in value. When these matched resistors are soldered in the circuit, care should be taken that the heat of the soldering iron does not cause the resistors to shift value. The resistors should be held firmly by the lead to be soldered with a long nose pliers, which will act as a heat-sink between the soldered joint and the body of the resistor. If this precaution is taken the two phase inverter outputs will be in close balance.

Adjustment of the Speech Amplifier When the wiring of the speech amplifier has been completed and checked, the unit is ready to be tested. Before the tubes are plugged in the amplifier, the bias supply should be energized and the voltage across the 600 ohm bleeder resistor should be measured. It should be −68 volts. If it is not, slight changes in the value of the series resistor, R_3, should be made until the correct voltage appears across the bleeder resistor. The tubes may now be inserted in the amplifier and the positive and cathode voltages checked in accordance with the measurements given in figure 15. After the unit has been tested and is connected with the modulator, R_2 should be set so that it is impossible to overmodulate the transmitter regardless of the setting of R_1. The gain control (R_1) may then be adjusted to provide the desired level of clipping consistent with the setting of R_2.

27-8 A 200 Watt 811-A Modulator

One of the most popular medium power r-f amplifier stages consists of a single tetrode power amplifier tube, such as the 4-125A, 813 or 4E27 operating at a plate voltage of 2000 and a plate current of 150 to 200 milliamperes. Such an amplifier requires a minimum of r-f driving power, allows an input of 300 to 400 watts, and yet employs power supply components that are relatively modest in price. The

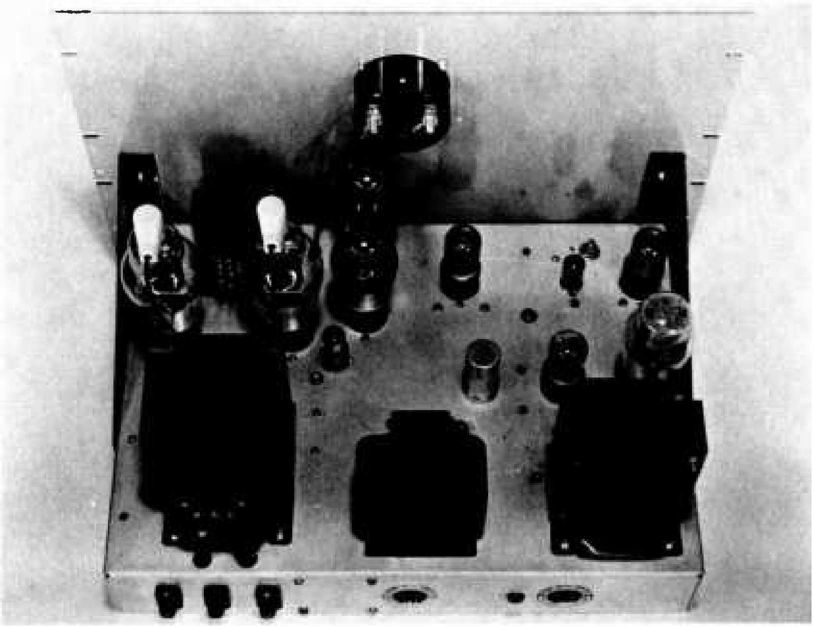


Figure 17
TOP REAR VIEW OF THE 811-A AMPLIFIER-MODULATOR UNIT

5-db signal increase between a 300 watt transmitter and a 1000 watt transmitter is very expensive when one considers the additional cost of modulator and power supply equipment.

Additional economy may be achieved if the modulator and final amplifier may be operated from the same power supply. Unfortunately, this is not so simple. There are few modulator tubes designed to deliver 150 to 200 watts of audio power at a plate voltage of 2000. It is poor economy to use tubes of the 810 calibre (which will operate at 2000 volts) when only 200 watts of audio are needed. Other triodes, such as the 75TH and the 100TH require plate-to-plate load impedances of the order of 21,000 ohms or so for proper operation at this voltage. Modulation transformers to match such a high value of plate load impedance are both rare and expensive. If a cheap modulation transformer is used for such a purpose as this, the leakage reactance of the transformer may provide a match for the modulator tubes without any secondary load applied to the transformer.

The modulator to be described avoids these difficulties, and will provide over 200 watts of audio power. It is designed to work with the new series of *Stancor* plate transformers which are tapped to provide two output voltages. The transformer used for the power supply of this modulator provides 2000 volts d-c at 200 milliamperes for operation of the r-f power amplifier, and also 1750 volts d.c. at an intermittent load of 200 milliamperes for operation of the class B modulator.

This is a satisfactory compromise, since there are many types of tubes which will deliver 200 watts of audio at 1750 plate volts. Of the group, the 811-A is an excellent choice. Maximum rated plate voltage for the 811-A is 1500 volts for class B operation, but experience has shown that the tubes perform in a satisfactory manner with no observable shortening of life when operated at plate voltages in excess of 2000. When the 811-A is operated at a plate potential of 1750 volts, it requires 9 volts of negative bias for class B operation. This voltage may be obtained from flashlight batteries or other low impedance source.

The Modulator Circuit The 200 watt modulator is illustrated in figures 17 and 18, and the schematic is shown

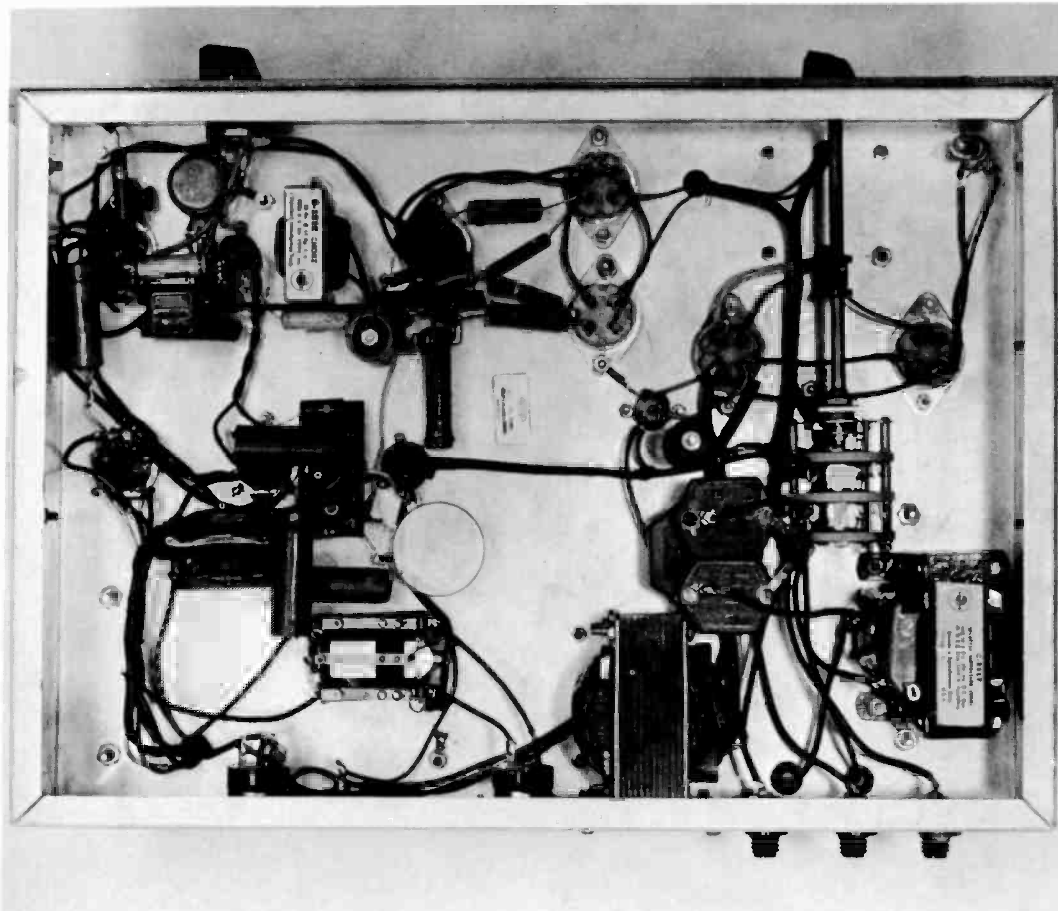
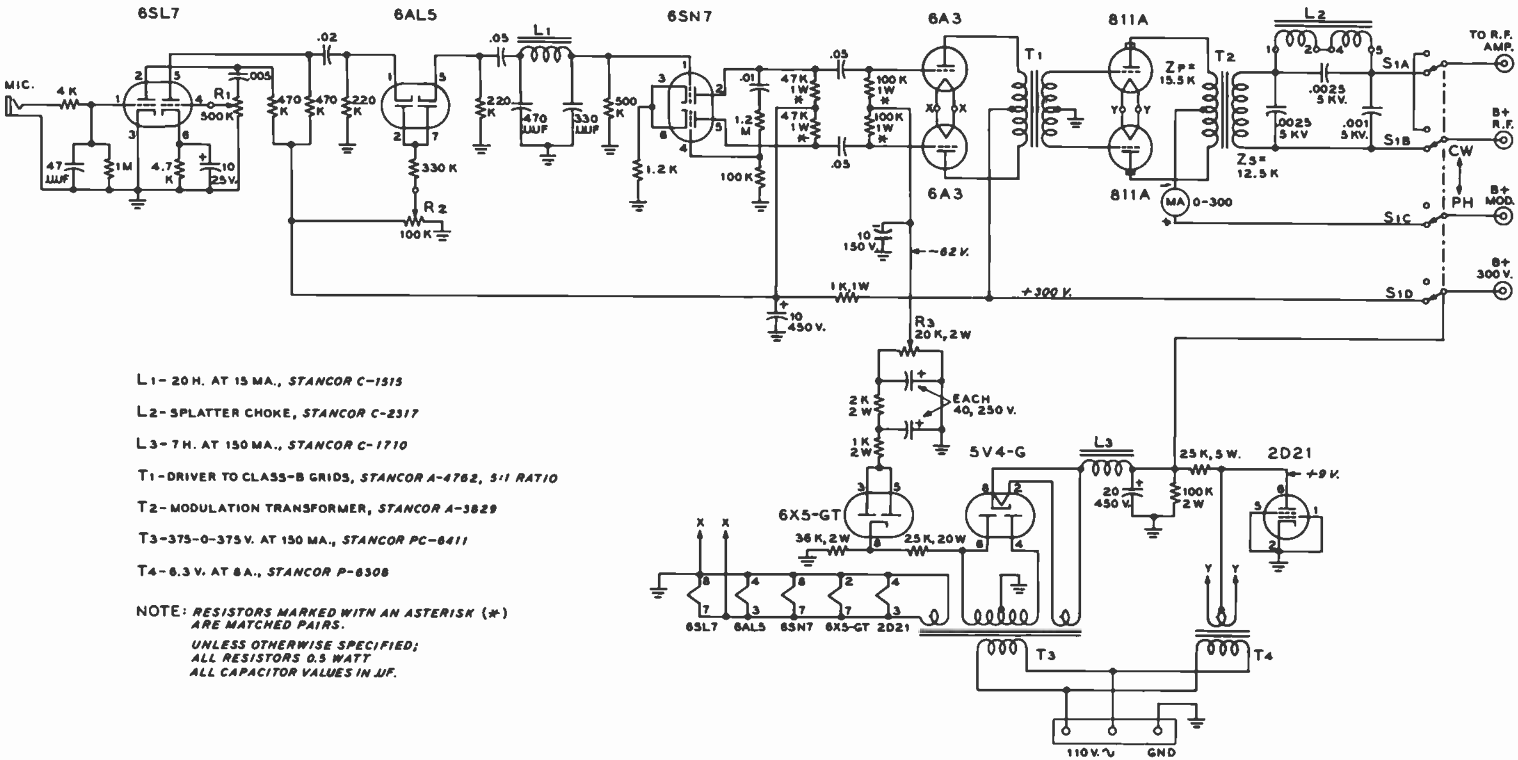


Figure 18
BOTTOM VIEW OF 811-A AMPLIFIER-MODULATOR UNIT

in figure 19. The low level audio stages and modulator driver are similar to the 15 watt speech amplifier described in section 27-5 of this chapter. A 6SL7 double triode tube is employed as two stages of R-C amplification, and a 6AL5 is used as a speech clipper tube. A simple L-C audio filter made up of an inexpensive a.c-d.c. filter choke and two mica capacitors follows the clipper stage. The roll-off of this filter is not as steep as the more expensive filter shown in section 27-5 of this chapter, but it performs in a satisfactory manner, considering its initial cost. A 6SN7 phase inverter follows the filter circuit, driving two 6A3 low-mu triodes connected in push-pull. Bias voltage for the 6A3's is obtained from a simple half-wave rectifier using a 6X5-GT and a two section R-C filter network.

The 6A3 driver tubes are transformer coupled to two 811-A tubes, operating class B at a plate potential of 1750 volts. The 9 volt bias source is obtained from a voltage divider composed of a 25,000 ohm, 5 watt resistor and a 2D21 thyratron tube. When the miniature 2D21 is connected as a triode, it acts as a voltage regulator tube, with a constant voltage drop of 9 volts from plate to cathode. The tube will regulate over 300 milliamperes of current while maintaining a voltage drop of 9 volts between the electrodes. The center tap of the 811-A



L1- 20 H. AT 15 MA., *STANCOR C-1515*

L2- SPLATTER CHOKE, *STANCOR C-2317*

L3- 7 H. AT 150 MA., *STANCOR C-1710*

T1-DRIVER TO CLASS-B GRIDS, *STANCOR A-4762, 5:1 RATIO*

T2-MODULATION TRANSFORMER, *STANCOR A-3829*

T3-375-0-375 V. AT 150 MA., *STANCOR PC-8411*

T4-6.3 V. AT 8 A., *STANCOR P-6308*

NOTE: *RESISTORS MARKED WITH AN ASTERISK (*) ARE MATCHED PAIRS.*

UNLESS OTHERWISE SPECIFIED;
ALL RESISTORS 0.5 WATT
ALL CAPACITOR VALUES IN μF.

Figure 19

200-WATT 811-A MODULATOR

filament transformer (T_4) is thus held at a positive potential of 9 volts with respect to ground. Since the center tap of the 811-A driver transformer (T_1) is grounded, the 811-A tubes are biased at a constant negative voltage equal to the voltage drop across the 2D21 regulator tube in the cathode circuit of the class B stage.

The plate-to-plate load impedance of the 811-A tubes when operating at 1750 volts is 15,500 ohms. A Vari-Match transformer such as the UTC type CVM-4 may be used if desired. In this particular case, a Stancor type A-3829 was employed. This unit is designed to match a plate-to-plate load of 9,000 ohms to a secondary load of 6,250 ohms. With the 15,500 ohm load of the 811-A tubes, a secondary load of 11,500 ohms should be used to maintain the same primary to secondary impedance ratio. This secondary load is closely matched by a single 4-125A tube operating at 2000 volts and 165 milliamperes of plate current.

The audio output from the push-pull 811-A class B modulator is passed through a high-level "splatter suppressor" which attenuates all audio frequencies above 3500 cycles. The use of both low level and high level audio filters does much to reduce the broad sidebands and co-channel interference that seems to be so common on the amateur phone bands.

A ceramic switch, S_1, is used to switch the modulator unit out of the operational circuit for c-w operation of the transmitter.

Construction of the Modulator The modulator is constructed upon a 10"x 17"x 3" aluminum chassis (Bud AC-416). A 12¼" aluminum panel (Bud PS-1256G) and a pair of 6½" chassis mounting brackets (Bud MB-458) complete the assembly. Placement of the major parts may be seen in the top view of the unit, figure 17. The modulation transformer (T_2) is mounted to the left rear of the chassis, with the modulator tubes and the driver transformer (T_1) directly in front. To the right of the 811-A tubes are the push-pull 6A3 tubes, and the 2D21 bias regulator. To the right of these are the speech amplifier tubes. The clipping level control, R_2, is mounted on the top deck of the chassis between the 6SL7 and the 6AL5 tubes. The gain control, R_1, is located on the front panel directly in front of R_2.

To the right rear of the chassis are located the power transformer, T_3, and the filter choke, L_3. In front of these are the 5V4-G and the 6X5-GT rectifier tubes.

The low level audio filter choke, L_1, may be seen at the upper left corner of the chassis in figure 18. T_4 and L_2 are mounted at the lower right of the chassis, directly behind S_1.

Wiring and Testing the Modulator Since the 811-A tubes operate from a separate filament supply from the other tubes in the modulator unit, it is permissible to ground one side of the filament circuit in the speech amplifier stages. The filament lead to the 6SL7 tube should be shielded. The 811-A filament circuit, however, is a part of the bias system, and both filament leads must be balanced to ground, as shown in figure 19. Choke L_1 should be kept clear of the large inductive fields created by T_4. L_1 is therefore mounted close to the front panel of the modulator between the 6AL5 socket and the 6SN7 socket.

All leads to T_2, S_1 and the L_2 assembly should be carefully insulated from the chassis. High voltage 5000 volt cable should be employed for these connections. The capacitors that make up the high level low pass audio filter are mounted on one inch ceramic insulators. High voltage connections to the modulator unit are made through Millen 37001 safety terminals.

When the wiring has been completed and checked, the 6SL7, 6AL5, 6SN7, 6X5-GT and 5V4-G tubes should be inserted in their sockets and power applied to the primary circuit of T_3 and T_4. Plate voltage as measured at the center tap of T_1 (S_1 set to "phone") should be about 310 volts. Bias control R_3 should be set to show −62 volts between the arm of R_3 and ground, when measured with a high resistance d-c voltmeter. The 6A3 tubes and 811-A tubes may now be plugged in their sockets. A 12,000 ohm, 200 watt resistor should be placed between the two output safety terminals, and 1750 volts applied to the "B-plus Mod." terminal. With no audio signal, the resting plate current of the 811-A stage should be approximately 30 milliamperes, kicking up to approximately 160 milliamperes under full output conditions of the modulator. The clipping level control, R_2, may be set as previously described in sections 27-3 and 27-5 of this chapter.

27-9 500-Watt 810 Modulator

Illustrated in figures 20 and 21 is a modulator unit capable of high-level amplitude modulation of a one kilowatt r-f amplifier stage. This modulator is designed to be driven by the modulator section of either a Collins 32V or a Viking II transmitter. Both of these 120 watt transmitters employ push-pull class AB 807 modulators capable of delivering over 50 watts of audio into a 500 ohm tap of the modulation transformer of the transmitter.

Either of these two transmitters is capable of driving a kilowatt r-f amplifier stage as il-

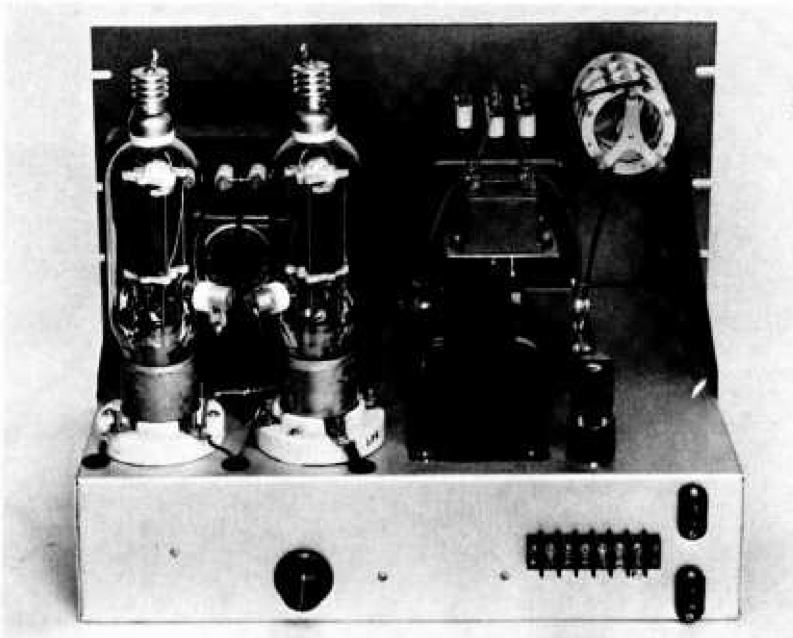


Figure 20
REAR VIEW OF 810 500-WATT CLASS B MODULATOR
Bias control is directly below the 810 tubes with bias supply to right

lustrated in Chapter 28. In addition, the audio section of the 120 watt transmitter, with proper care, may be employed to drive a high-level modulator for the kilowatt r-f amplifier, as shown herein.

The Modulator Circuit The circuit of this modulator is shown in figure 21. Push-pull class B 810 triode tubes operating at a plate potential of 2500 volts are used to deliver a clean 500 watt audio signal. A small low-impedance bias supply is built into the modulator unit to deliver approximately −75 volts of bias under the varying load conditions imposed upon the supply by the variable grid circuit impedance of the class B modulator. Since the 60 watt class AB modulator of the 120 watt transmitter will now be used as a driver stage for this high powered class B 810 modulator, it is wise to artificially load the output circuit of the 807 driver unit with a resistor to provide a constant load impedance for the driver. In addition, a portion of the excess driving power may be swamped out in this load resistor, R_1.

To attenuate harmonics developed in the 807 driver stage, a low pass audio filter network is placed in the 500 ohm input circuit of the high level modulator. This "splatter suppressor" attenuates frequencies higher than 3500 c.p.s.

A similar low pass audio filter network is placed *after* the push-pull 810 stage to reduce any harmonics that may be generated in the modulator itself. The use of these two audio filter networks, plus resistive loading of the 807 driver stage results in unusually clean and crisp audio up to and including the 500 watt output level. In general, the use of a class AB 807 driver for a class B high level plate modulator is to be frowned upon, since the driver stage is working into the variable load impedance of the 810 modulator grid circuit. However, this is the only way that the aforementioned transmitters may be used as audio drivers for high powered modulation equipment, and they will perform in a very satisfactory manner if the low pass audio networks and grid circuit loading are incorporated in the high level modulator.

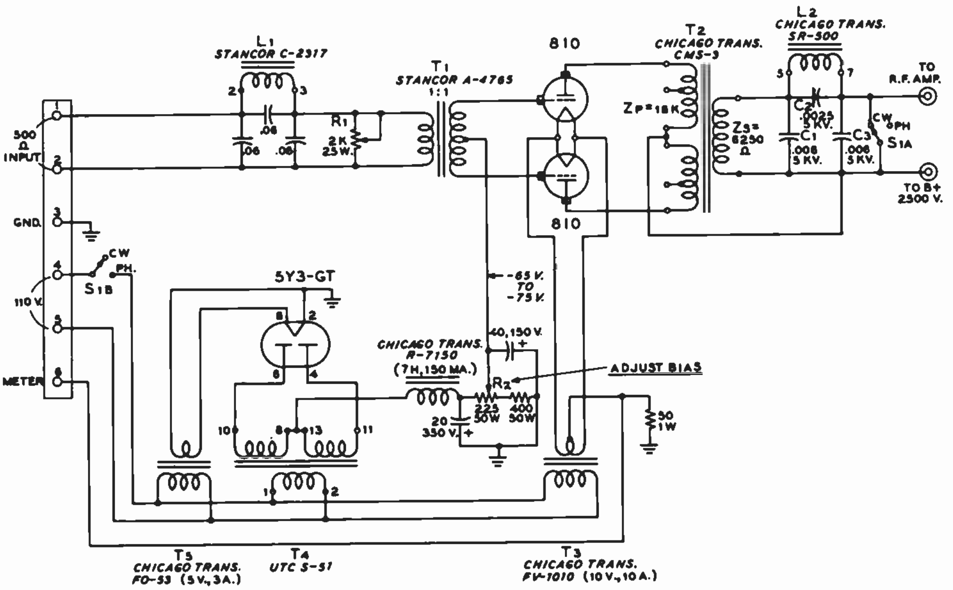


Figure 21
SCHEMATIC OF 500-WATT MODULATOR

For c-w operation, the secondary of the class B modulator transformer is shorted out, and the filament and bias circuits of the modulator are disabled. Switch S_{1A} should have 10,000 volt insulation. A suitable switch may be found in the war-surplus BC-306A antenna loading unit. This switch may be seen in figure 20.

All low voltage connections to the modulator are brought out to a six terminal phenolic strip on the back of the chassis. A 0-500 ma. d-c meter is placed in the filament circuit of the 810 tubes. The meter is placed across a 50 ohm, 1 watt resistor so that the filament return circuit of the modulator is not broken if the meter is removed.

The modulation transformer, T_2, is designed for plate-to-plate loads of either 12,000 ohms or 18,000 ohms when a 6250 ohm load is placed across the secondary terminals. The 810 tubes are correctly matched when the 18,000 ohm taps are used at a plate potential of 2500 volts, or when the 12,000 ohm taps are used at a plate potential of 2000 volts or 2250 volts.

Modulator Construction Because of the great weight of the modulator components it is best to use a heavy-duty steel chassis. A 13"x 17"x 4" chassis (Bud CB-643), a 14" steel panel (Bud PS-1257G) and a pair of Bud MB-449 mounting brackets make up the assembly for this particular modulator. As seen in figure 20, the CMS-3 modulation transformer is mounted in the left-front corner of the unit. The secondary terminals of T_2 are to the front of the chassis, clearing the front panel by about 1/2". To the right of T_2 is placed the high level audio filter choke, L_2. The two 810 tubes are mounted in back of T_2. To the right of the 810 tubes is the 10 volt filament transformer, T_3. To the right of T_3 is the 5Y3-GT bias rectifier tube. Between T_3 and L_2 are mounted the mica bypass capacitors which make up the high level filter network. Two .003 μfd., 5000 volt mica capacitors are paralleled for C_1 and also for C_3. C_2 is made from a .001 μfd. capacitor and a .0015 μfd. capacitor which are connected in parallel. All of these capacitors are mounted upon a plywood bracket which insulates them from the metal chassis. This prevents insulation breakdown within the capacitors which might occur if they were fastened directly to the metal chassis.

The bias supply components, T_1, and the low level filter components are mounted beneath the four inch deep chassis. Placement

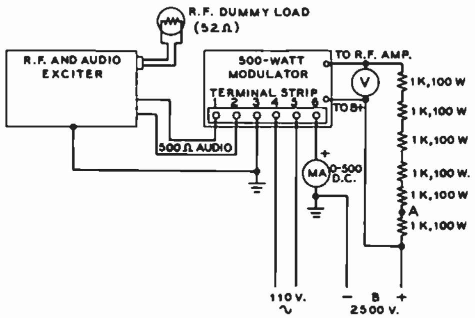


Figure 22
TEST SETUP FOR THE 500-WATT MODULATOR

of these parts is not critical. The bias adjustment control, R_2, is mounted on the back lip of the chassis as are the two high voltage terminals. Millen 37001 high voltage connectors are used for the two high voltage leads. High-voltage TV wire should be employed for all leads in the 810 plate circuit.

Modulator Adjustment When the modulator has been wired and checked, it should be tested before being used with an r-f unit. A satisfactory test set-up is shown in figure 22. The transmitter that is to be used as the r-f and audio driving unit should be connected to a 100 watt 52 ohm dummy load to dissipate the r-f signal, and the 500 ohm audio leads from the transmitter-exciter should be connected to terminals 1 and 2 of the modulator. A common ground lead should be run between the transmitter-exciter and the modulator. Six 1000 ohm 100 watt resistors should be connected in series and placed across the high voltage terminals of the modulator unit to act as an audio load. The first step is to place the 810 tubes in their sockets and turn switch S_1 to the "phone" position. The 810 filaments should light, and switch section S_{1A} should remove the short across the secondary of T_2. R_2 should be adjusted to show −75 volts from each 810 grid terminal to ground as measured with a high resistance voltmeter. Resistor R_1 should be set to approximately 1000 ohms. If an oscilloscope is available, it should be coupled to point "A" on the load resistor (figure 22) through a 500 $\mu\mu$fd. ceramic TV capacitor of 10,000 volts rating. The case of the oscilloscope should be grounded to the common ground point of the modulator.

A plate potential of 2500 volts should be applied to the modulator, and R_2 adjusted for a resting plate current of 50 milliamperes as read on the 500 milliampere meter in the cathode circuit of the modulator. *Be extremely careful during these adjustments, since the plate supply of the modulator is a lethal weapon. Never touch the modulator when the plate voltage supply is on! Be sure you employ the TV blocking capacitor between the oscilloscope and the plate load resistors, as these load resistors are at high voltage potential! If a high resistance a-c voltmeter is available that has a 2000 volt scale, it should be clipped between the high voltage terminals of the modulator, directly across the dummy load. Do not touch the meter when the high voltage supply is in operation!* An audio oscillator should be connected to the audio input circuit of the exciter-transmitter and the audio excitation to the high level modulator should be increased until the a-c voltmeter across the dummy load resistor indicates an R-M-S reading that is equal to 0.7 (70%) of the plate voltage applied to the modulator. If the modulator plate voltage is 2500 volts, the a-c meter should indicate 1750 volts developed across the 6000 ohm dummy load resistor. This is equivalent to an audio output of 500 watts. With sine wave modulation at 1000 c.p.s. and no speech clipping ahead of the modulator, this voltage should be developed at a cathode meter current of about 350 ma. when the plate-to-plate modulator impedance of the modulator is 18,000 ohms. Under these conditions, the oscilloscope may be used to observe the audio waveform of the modulator when coupled to point "A" through the 10,000 volt coupling capacitor. Load resistor R_1 should be adjusted to give best sine-wave output as observed on the oscilloscope when the 810 modulator is delivering maximum output. When the frequency of the audio oscillator is advanced above 3500 cycles, the output of the modulator as measured on the a-c voltmeter should drop sharply, indicating that the low pass audio networks are functioning properly.

If the waveform on the oscilloscope does not closely resemble a sine wave, the oscilloscope should be removed from point "A" and connected across R_1, with .01 μfd., 1000 volt capacitors in series with each lead to the oscilloscope. The output waveform of the transmitter-exciter should then be observed to determine if the distortion is being generated in the exciter or in the modulator. If the trouble is in the audio exciter, certain modifications to the exciter may be necessary as explained in section 27-3 of this chapter.

Audio distortion in the modulator may be caused by maladjustment of R_1 and the turns ratio of T_1. It may be necessary to change the taps on the secondary of T_1 to provide a 1:2

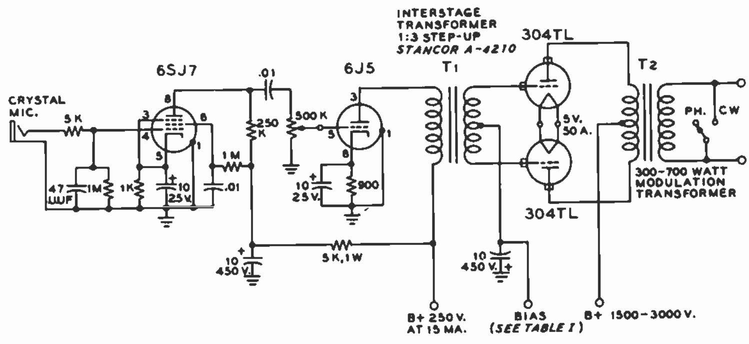


Figure 23
PUSH-PULL 304TL CLASS AB_1 MODULATOR

step-up ratio, with a corresponding readjustment of R_1 to provide minimum driver distortion, as observed at point "A" with the oscilloscope. The adjustment of R_1 and T_1 is not especially critical, and a setting of R_1 at 1000 ohms and T_1 at a 1:1 turns ratio seems to be nearly optimum with the 120 watt transmitters that were used as drivers for the modulator.

With speech waveforms and no clipping, the modulator meter will swing to about 150 to 200 ma. under 100 per cent modulation at a plate potential of 2500 volts. With speech waveforms and moderate low level clipping, the modulator meter will swing to about 275 ma. under 100 per cent modulation.

27-10 500-Watt 304TL Modulator

Ordinarily, few amateurs would be inclined to design the high-level stages of their transmitters around type 304TL tubes. Although the 304TL unquestionably is an excellent tube, with its extremely high transconductance and power sensitivity, its price and capabilities are in excess of those required even for a kilowatt amateur transmitter. But with enormous supplies of these tubes available at a relatively low price on the surplus market it becomes economical to consider their use in high-power amateur transmitters. In fact, with the use of these 304TL's the cost of heating power for filaments becomes a much more significant figure than the cost of the tubes.

The 304TL is ideally suited for use as a modulator for a high-power amateur transmitter. In fact, due to the relatively low amplification factor of the tube (about 12) the 304TL may even be used as a class A triode Heising modulator. Such an arrangement is practicable for modulating a medium-power transmitter when a 1500 to 2000 volt plate supply is available.

The class AB_1 operating characteristics of the 304TL tube are shown in Table 1. An interesting fact to be observed is that under these conditions no grid driving power is required by the 304TL tubes. It is necessary only to supply the correct amount of grid driving voltage. The amounts shown may easily be obtained from a single 6J5 tube, and the usual push-pull triode driver stage for the high powered modulator may be eliminated. A suit-

TABLE 1

304TL OPERATING CHARACTERISTICS, CLASS AB1
(NO DRIVING POWER REQUIRED)

D.C. PLATE VOLTS	1500	2000	2500	3000
GRID BIAS *	−118	−170	−230	−290
ZERO-SIGNAL PLATE CURRENT (MA.)	270	200	160	130
MAX. SIGNAL PLATE CURRENT (MA.) **	572	546	483	444
PLATE-TO-PLATE LOAD (OHMS)	2540	5300	8500	12000
PEAK A.F. GRID VOLTS (PER TUBE)	118	170	230	290
MAX. POWER OUTPUT (WATTS)	256	490	610	730

* ADJUST TO GIVE STATED ZERO-SIGNAL PLATE CURRENT

** VALUES GIVEN FOR SINE-WAVE MODULATION. FOR VOICE WAVE FORMS, MAXIMUM CURRENT WILL BE APPROXIMATELY TWO-THIRDS SINE-WAVE VALUES.

able modulator-driver unit which will deliver 500 watts of audio from two 304TL tubes operating class AB_1 is shown in figure 23.

The filaments of the 304TL tubes may be connected either in series or parallel for either 5 volt, 50 ampere operation, or 10 volt, 25 ampere operation. To conserve filament power during standby periods, the filaments of the 304TL tubes may be either turned off, or may be dropped to one-half voltage by means of a dropping resistor in the primary circuit of the filament transformer. This resistor may be shorted out during periods of transmission by a small relay actuated by the transmitting control system.

The gain of the speech amplifier is sufficient so that an inexpensive crystal microphone may be used with the modulator. The "phone-c.w." switch is connected so as to short the modulation transformer and to open the filament circuit of the 304TL tubes during c-w operation.

W6HX

Transmitter Construction

The equipments described in this chapter are complete transmitters which have been assembled from units described earlier in this Handbook, working in conjunction with commercial transmitter-exciters, such as the Johnson Ranger, Viking II, or Collins 32V. These medium power phone-c.w. transmitters make excellent station equipment for the amateur, as they may be used by themselves, or may be made to function as a driver unit for a more powerful amplifier stage.

The Johnson Ranger, for example, is capable of driving the push-pull 811-A amplifier of Chapter 26, Section 2; or any of the push-pull or pi-network tetrode amplifiers of Chapter 26. In addition, the Ranger unit will supply screen voltage for the tetrode amplifier, and will supply sufficient audio power to drive a high power class-B modulator stage.

120-watt transmitters, such as the Viking II or the Collins 32V series are capable of providing driving power for any of the triode 1-kilowatt amplifiers of Chapter 26, in addition to supplying audio driving power for the class-B modulator stage.

When these commercial transmitters are used for exciter stages for high powered transmitters, the overall cost of the kilowatt station is reduced to a reasonable figure, as the driver-exciter always retains a high resale value. In addition, it allows the amateur to get on the air with a respectable signal while he is in the process of building his high powered equipment.

Figure 1
THE VIKING RANGER FEATURED IN A 350-WATT PHONE-CW INSTALLATION
The Ranger transmitter makes an excellent exciter for an all-band medium power transmitter

28-1 A 350-Watt Amplifier Unit for the Ranger Transmitter

The Ranger transmitter is an excellent unit for the beginning amateur, and it may be made the heart of a 350-watt phone-c.w. transmitter at a modest additional expense. Shown in figure 1 is a complete 350-watt installation based upon the Viking Ranger transmitter-exciter unit.

The Ranger transmitter is used to drive the push-pull 811-A amplifier illustrated in Section 2 of Chapter 26. A modulator-power supply unit described herewith is, used in conjunction with the Ranger exciter and the 811-A amplifier, and these three units form a complete 350 watt all-band phone-c.w. transmitter. This amplifier-modulator-power supply package effectively adds a boost of 5 decibels to the Ranger transmitter, greatly increasing its "punch" and effectiveness.

The amplifier may be connected to the Ranger transmitter without the need of any internal wiring changes in the Ranger. It is only necessary to attach the power cables of the amplifier unit to the proper receptacles on the Ranger transmitter and the 350-watt transmitter is on the air.

The Modulator-Power Unit Assembly and tuning information has been given for the 811-A amplifier in Chapter 26. The following information deals with the assembly and testing of the modulator-power unit.

A block diagram of the interconnecting leads between the various units is shown in figure 2. Three cables connect the Ranger transmitter to the amplifier package: (1) The r-f output of the Ranger is coupled to the tuned grid circuit of the amplifier by a length of RG-8/U or RG-59/U coaxial cable. PL-259 (Amphenol 83-1SP) plugs are placed on each end of this line. (2) The modulator is disconnected from the 6146 r-f stage in the Ranger and coupled through a 4-wire cable and PL_2 to the modulator-supply unit. Plug PL_2 is a matching plug

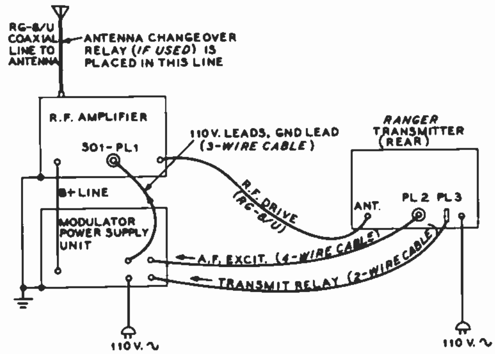


Figure 2

INTERCONNECTING CABLES BETWEEN RANGER TRANSMITTER AND R-F AMPLIFIER PACKAGE

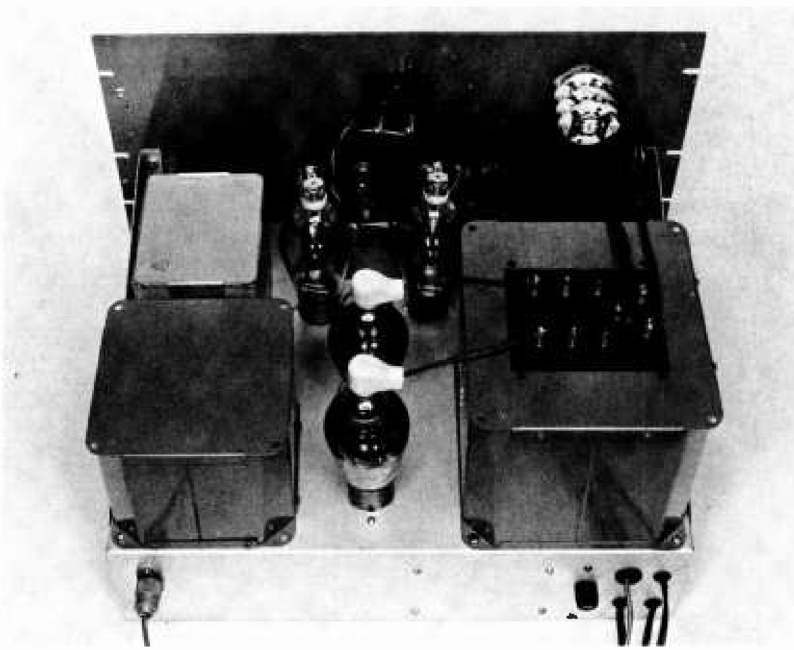


Figure 3

THE MODULATOR-POWER SUPPLY UNIT

Two 811-A Class B modulators provide 100 per cent modulation for the 811-A r-f amplifier stage described in Chapter 26, Section 2. A single power supply employing two 866 rectifier tubes provides 1200 volts for the operation of both the r-f amplifier and modulator. R.f. and audio excitation are supplied by the Ranger transmitter.

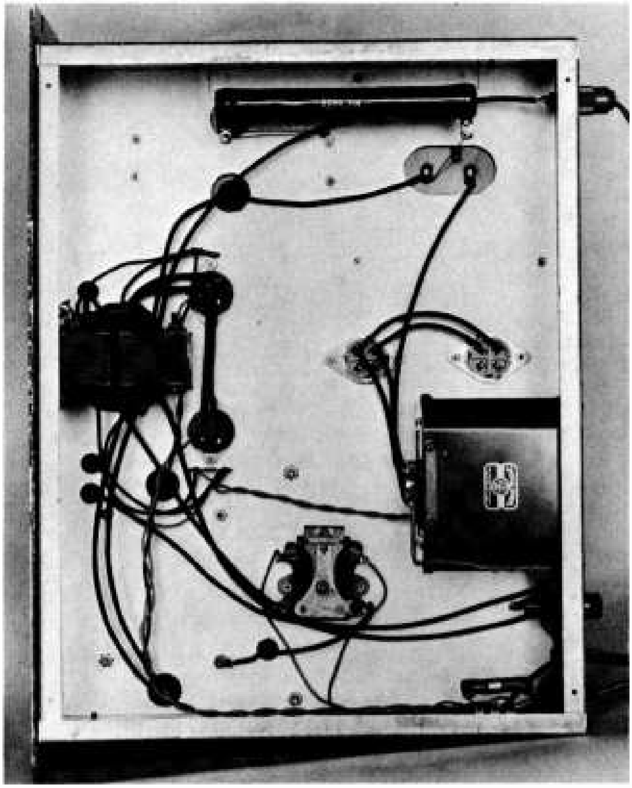


Figure 4
UNDER CHASSIS VIEW OF MODULATOR-POWER UNIT

The filament transformer for the 811 modulator tubes is to the front (left) of the chassis. To the right is the filament transformer for the 866 rectifier tubes. Next to this is the "transmit" relay.

for the nine pin socket on the rear of the Ranger transmitter. This plug is similar to the one supplied with the Ranger. Two jumpers inside PL_2 automatically make the necessary circuit changes to allow the audio section of the Ranger to serve as a driver for the high powered modulator stage of figure 5. (3) A two wire cable terminating in PL_3 connects the "transmit" relay of the modulator unit to the control circuits of the Ranger transmitter. If an external antenna relay is to be used with the r-f amplifier package, the coil of this relay is connected across the terminals of PL_3.

There are two interconnecting cables between the modulator-power supply unit and the r-f unit. A three-wire cable connects the two common grounds together and also supplies 110 volts a.c. for the filament transformer of the amplifier. A separate well-insulated lead connects the high voltage terminals of the two units.

Modulator-Power Unit Circuitry The circuit of the modulator-power unit (MP unit) is shown in figure 5. Two 811-A tubes are connected as zero bias class B modulators, operating at a plate potential of 1250 volts. A 3000-ohm, 10-watt resistor is connected between the grid terminals of the 811-A sockets to provide a stabilizing load for the 1614 audio tubes in the Ranger exciter.

No audio driver transformer is needed in the MP unit, as the modulation transformer in the Ranger serves as the class-B driver transformer.

The plate to plate load impedance required by the 811-A modulators is in the neighborhood of 9000 ohms. The 811-A r-f amplifier operates at 1250 volts and 280 milliamperes, presenting a load impedance of 4500 ohms. A 2:1 impedance step-down is required for an impedance match. A .004-μfd., 2500-volt mica capacitor is connected across the primary of the modulation transformer, and an identical capacitor across the secondary winding. These capacitors, plus the leakage reactance of the transformer form a low pass filter which attenuates audio frequencies above 5000 cycles.

A pair of 866-A rectifiers and a choke input filter network provides 1250 volts for the operation of both the modulator stage and the r-f amplifier. Ten microfarads of filter capacitance and the use of a swinging filter choke insure that the power supply has good regulation and high dynamic stability.

The change from phone to c-w operation is made by S_3. When the switch is in the "phone" position, plate voltage is applied to the 811-A modulators, and the primary of the modulator filament transformer T_2 is energized. Upon switching S_3 to the c-w position, plate voltage is removed from the modulator tubes, and T_1. At the same time, the primary circuit of T_2 is opened, turning off the filaments of the modulator tubes.

Switch S_1 turns on the filament circuits of the MP unit, and S_2 applies power to the contacts of the "transmit" relay, Ry_1. The energizing coil of Ry_1 is connected to the "transmit" circuit of the Ranger through a two wire cable and PL_3. Thus, when the Ranger is put on the air, the amplifier is also put on the air without the necessity of the operator closing additional switches.

A 0-250 d-c milliammeter is placed in the filament return circuit of the modulator stage. Under 100 per cent modulation, this meter should kick to about 200 milliamperes.

Modulator-Power Unit Construction The modulator unit (figure 3) is built upon an aluminum chassis measuring 13" x 17" x 4" (Bud AC-428) and uses a 12" aluminum relay rack panel. A pair of mounting brackets (Bud MB-459) securely fasten the panel to the chassis. The plate transformer T_3 and the filter choke CH_1 are mounted in the two rear corners of the chassis. If metal working tools are not available, the cutouts for these units may be done by a sheet metal shop. Directly in front of T_3 is located the modulation transformer T_1 with S_3 above it, mounted on the front panel. Filter capacitor C_3 is located in front of CH_1. Transformers T_2 and T_4 are placed below the chassis, close to their respective tube sockets.

All high voltage wiring should be done with heavily insulated wire (such as Belden 8899) and ceramic safety caps should be used on the 866-A rectifier tubes.

Capacitors C_1 and C_2 may be mounted directly to the lugs on T_1 by means of short pieces of solid copper wire. All leads passing through the chassis should pass through rubber grommets mounted in the chassis holes. The cables to PL_1, PL_2 and PL_3 should be cut to length to suit the particular installation.

Testing the MP Unit Before power is applied to the MP unit, an ohmmeter should be placed across the 10-μfd., 1500-volt filter capacitor. After the capacitor charges, the ohmmeter should read 50,000 ohms (the resistance of the bleeder) regardless of the position of S_3. The six ampere line fuse and the tubes should be inserted in their sockets and S_1 closed. The green pilot lamp should light, and all filaments should come on. PL_1 may now be inserted in the SO_1 socket in the r-f unit and the 811-A tubes in this deck should light. All connec-

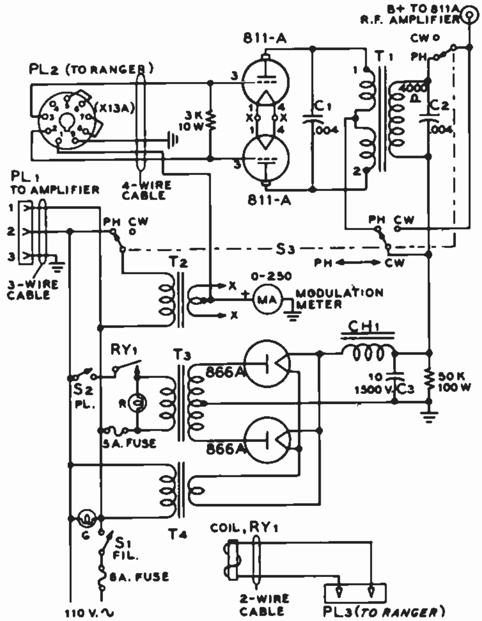


Figure 5

SCHEMATIC OF 811-A MODULATOR-POWER UNIT

C_1, C_2—.004 μfd. mica 2.5 Kv. Sprague ZFM-22
C_3—10 μfd. 1500 v. oil capacitor Sprague CR-1015
T_1—175 watt modulation trans. Stancor A-3829
T_2—6.3 v. at 10 a. Stancor P-6308
T_3—1500-0-1500 v. at 500 ma. UTC S-48
T_4—2.5 v. at 10 a. 10 Kv. insulation Stancor P-3060
CH_1—5/25 hy. at 500 ma. UTC S-38
PL_1—4 prong receptacle to fit SO-1 on amplifier chassis Amphenol 78-PF4-11
PL_2—9 prong plug Amphenol 86-PM9-11
PL_3—Antenna relay plug supplied with Viking Ranger transmitter
R—110 v. pilot lamp assembly, red
G—110 v. pilot lamp assembly, green
Ry_1—s.p.s.t. 100 v. relay Advance PC-1C-115VA
S_3—d.p.d.t. ceramic switch Centralab 2544
866-A sockets—Millen high voltage 33004

tions between the Ranger and the amplifier package should be made. Switch S_2 on the MP unit should remain open. The Ranger is now turned on, and excitation applied to the 811-A r-f section. The antenna loading control of the Ranger transmitter should be adjusted in conjunction with the excitation control until 90 milliamperes of grid current is indicated on the grid meter of the 811-A stage. The 811-A stage should now be neutralized according to the instructions given in Chapter 11. The five ampere plate fuse may now be placed in its receptacle and S_2 closed. When the Ranger control switch is turned to "transmit," the high voltage will be applied to the 811-A r-f amplifier. The amplifier may now be loaded to the antenna until a resonant plate current of 280 milliamperes is reached. If the Ranger is switched to phone operation, and S_3 thrown to phone, the Ranger transmitter audio section will now excite the 811-A modulators in the MP unit. It is necessary to retard the Ranger gain control to position 1 or 2 to prevent overmodulation. Modulator plate current of the 811-A tubes should rest at about 55 milliamperes, rising to 200 milliamperes under 100 per cent modulation. The modulator plate current of the Ranger transmitter should remain perfectly constant, perhaps kicking up a milliampere or two under heavy modulation. The modulator stage in the Ranger is now working as a class-AB_1 driver stage for the 811-A tubes, and delivers about six watts to excite the 811-A tubes to full output. Since the 1614 modulator tubes in the Ranger are capable of generating over 30 watts of audio power, care must be taken not to overdrive the 811-A modulator stage.

Amplifier Operation Once the initial tuning adjustments have been completed, the operation of the amplifier is completely controlled by the Ranger switching circuits. The amplifier is ready to operate shortly after S_1 and S_2 are turned on. It is necessary to allow the filaments of the 866-A rectifiers to heat for a period of 30 seconds before the plate voltage is applied to the tubes.

It must be remembered that the amplifier stage amplifies the signal that is put into it. If the Ranger transmitter has key-clicks (some of the early models of the Ranger had no vacuum tube keying circuit) the amplifier will reproduce these clicks. The keying of the Ranger should be slightly soft, as the amplifier has a natural tendency to "harden" the keyed exciting signal.

If it is desired to use the Ranger without the amplifier, plugs PL_2 and PL_3 should be removed from the Ranger, and the original 9-pin plug replaced in the Ranger PL_2 socket. The coaxial cable connecting the Ranger to the am-

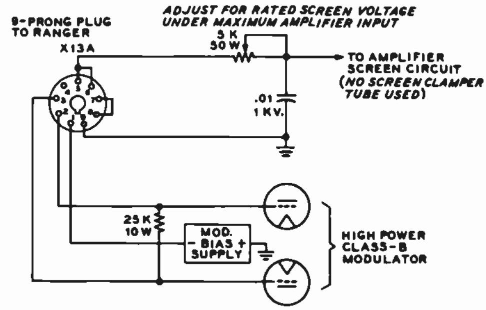


Figure 6

POWER CONNECTIONS TO JOHNSON RANGER FOR USE AS KILOWATT DRIVER

plifier should now be spliced to the antenna line to by-pass the amplifier. An M-259 coaxial cable splice may be used for this operation.

28-2 The Ranger Transmitter as a Driver for Tetrode Amplifiers

The Ranger transmitter may also be employed as a driver stage for tetrode amplifiers, as shown in figure 6. The screen voltage for the amplifier is taken from the power supply of the Ranger through a series protective resistor. Protective bias must be used on the tetrode amplifier since the screen voltage is applied to the amplifier when the Ranger is switched to "transmit," even though the keying circuit of the Ranger may be open. Suitable amplifiers for this type of service are the push-pull 813 amplifier of Chapter 26, Section 6, and the push-pull 4-250A amplifier of Section 7. If a pi network amplifier is to be used with the Ranger, the 4-250A amplifier of Section 9 will work in a satisfactory manner.

The audio section of the Ranger may be used to drive a class B audio amplifier such as the push-pull 810 modulator of Chapter 27. Since the plate current of the Ranger's modulator does not increase with speech when the Ranger is driving the grid circuit of a class B modulator, sufficient power supply capacity is available for the screen circuit of a tetrode class C amplifier without danger of overloading the power supply of the Ranger transmitter.

Figure 7

THE JOHNSON VIKING II TRANSMITTER MAKES AN EXCELLENT DRIVER FOR A 1-KILOWATT ALL-BAND PHONE-CW STATION

Push-pull 8000 tubes modulated by Class B 810's provide a compact 1000-watt amplifier package to work with a 120-watt exciter, such as the Collins 32V, the Viking or the B&W 5100

28-3 Viking II as Exciter for a Kilowatt Transmitter

The Viking II or the Collins 32V makes an excellent exciter unit for an all-triode kilowatt amplifier package. A complete station installation employing this configuration is shown in figure 7. Three additional basic units are added to the Viking transmitter to complete the kilowatt transmitter: (1) A triode amplifier capable of 800 to 1000 watts input on all bands between 10 meters and 80 meters. (2) A triode modulator capable of being driven by the Viking audio system, and delivering a peak audio power output of 500 watts. (3) A heavy-duty power unit to supply high voltage for both the modulator and the power amplifier. A block diagram of such an assembly is shown in figure 8.

These three units are mounted in a 66" relay rack cabinet (Bud CR-1772-G) to form a single assembly which may be placed adjacent to the operating table. The complete kilowatt transmitter is controlled by the Viking switches during changeover from receive to transmit, and both the audio and r-f section of the amplifier unit incorporate protective bias supplies. As an added factor to aid in preliminary tune-up, the plate voltage on the modulator and power supply may be cut in half by means of a "hi-

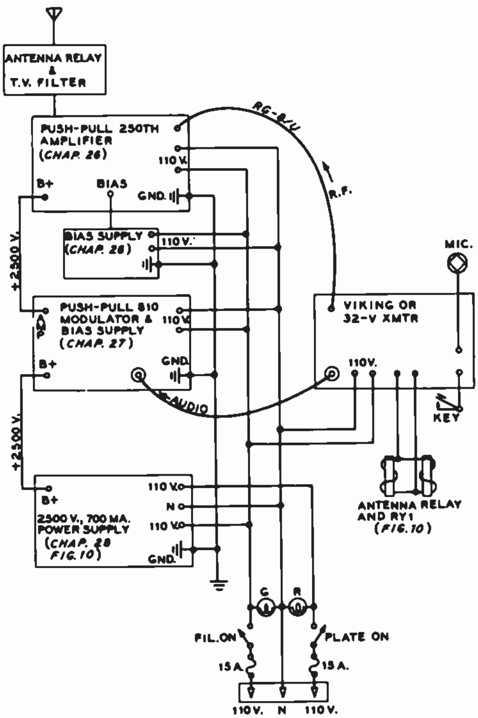


Figure 8

BLOCK DIAGRAM OF KILOWATT TRANSMITTER

lo" switch in the primary circuit of the high voltage plate supply.

The R-F Amplifier Either 250-TH, 810, or 8000 type tubes may be employed in the r-f amplifier of this transmitter. Type 810 tubes are recommended for class B modulator service. The r-f amplifiers of Sections 3 or 4 of Chapter 26 can be used in this application. The particular installation shown in figure 7 uses the amplifier of Section 3, Chapter 26, with push-pull 8000 tubes. These tubes run at 2000 volts and 450 milliamperes for a plate input of 900 watts. If 250-TH type tubes are employed in this amplifier, 2500 volts and 400 milliamperes may be run for a plate input of 1000 watts. The 810 modulator tubes will operate properly at either voltage provided the bias voltage is adjusted for the chosen plate voltage.

The bias supply for the 8000 r-f amplifier tubes is mounted on a small chassis directly below the amplifier. The schematic and pertinent information concerning this supply is given in figure 12, Chapter 26.

The P-P 810 Modulator The complete schematic for the 500-watt modulator is shown in figure 9. Two 810 tubes are employed in class B service, with low pass audio networks in both the plate and grid circuits.

The modulator stage in the Viking II transmitter employs a pair of 807 tubes in class AB_2. This arrangement makes an excellent low power modulator stage, but a rather mediocre driver stage for a high power class B modulator. The plate impedance of the 807 tubes is quite high, and the resulting voltage regulation of the tubes when operated as an exciting stage is quite poor. Two of the prerequisites for good class B modulator operation are good regulation in the bias supply of the modulator, and a source of low impedance audio excitation. The bias supply of figure 9 furnishes bias voltage of adequate regulation, but the regulation of the 807 audio driver tubes in the Viking transmitter cannot be improved without drastic changes in the audio section of the Viking. The distortion arising in the 810 modulator stage from this marginal driving situation can be almost completely eliminated by the use of low level and high level audio filters. These filters are designed to attenuate by some 15 db audio frequencies above 4000 cycles. When they are placed in the input and output circuits of the 810 modulator unit, a clean 500 watts of sine-wave audio output is obtained at the terminal posts of the modulator, when the microphone circuit of the Viking transmitter is excited with a .02-volt, 1500-cycle signal.

A 25,000-ohm swamping resistor is placed across the grid circuit of the 810 tubes. This tends to improve the driver regulation a bit, and also lessens the chances of audio feedback within the Viking transmitter.

A low impedance bias supply delivers 60 to 80 volts of negative bias, well filtered by a 40-μfd. capacitor connected between the bias supply arm of the adjustment potentiometer and ground. Bias is applied to the modulator tubes through the driver transformer in the Viking, and through the low level audio filter in the 810 grid circuit.

The grid circuit filter is composed of two 100 milliampere "splatter chokes" (Triad C-26C) connected in each grid lead, in conjunction with two .005-μfd., 1250-volt mica capacitors. The filter is terminated by the grid impedance of the 810 tubes in parallel with the 25,000-ohm 10-watt loading resistor.

A heavy duty splatter suppressor, using a 500 milliampere iron-core inductor is placed in the secondary circuit of T_1. 5000-volt mica capacitors are used in this circuit, although

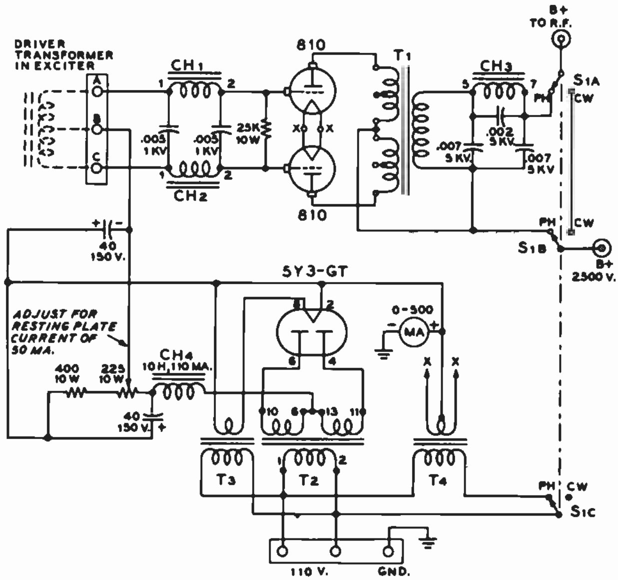


Figure 9
PUSH-PULL 810 MODULATOR

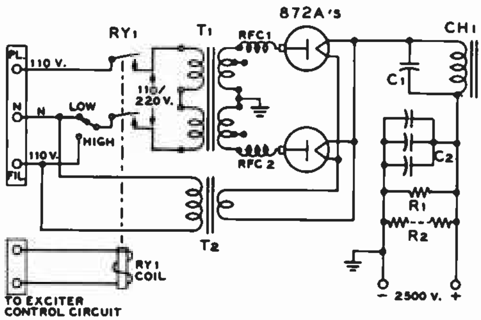
T_1—500 watt modulation trans. 18,000 ohms primary, 6250 ohms secondary Chicago CMS-3
T_2—Bias trans. UTC S-51
T_3—5 v. at 3 a. UTC FT-6
T_4—10 v. at 10 a. UTC S-62
CH_1,CH_2—100 ma. splatter choke Triad C-26X
CH_3—500 ma. splatter choke Chicago SR-500
CH_4—10 hy. 100 ma. Chicago R-23110
S_1—3 pole double throw high voltage switch

some of the new 5000-volt TV paper capacitors should be less expensive and just as effective. The capacitors are returned to the opposite side of the secondary winding instead of to ground, thus removing the plate potential of the amplifier stage from the capacitor.

The proper plate to plate impedance for 810 class B modulator tubes at a potential of 2500 volts is approximately 18,000 ohms. When the plate voltage is dropped to 2000 volts, the plate to plate impedance decreases to 13,000 ohms. The Chicago Transformer Co. type CMS-3 modulation transformer is specifically designed for just this situation. With a secondary load impedance of 6250 ohms (2500 volts at 400 ma.) the reflected primary load impedance is 18,000 ohms. With a secondary load impedance of 4500 ohms (2000 volts at 450 ma.) the reflected primary impedance is 13,000 ohms. Thus no connections need be changed on the modulation transformer when going from one plate potential to another.

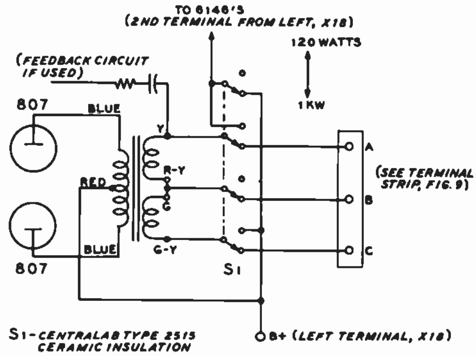
A three-pole two position switch of high insulation qualities is needed to cut the modulator stage in and out of the circuit. The switch used in this modulator is a surplus ceramic unit taken from the antenna loading unit (BC-306A) of a defunct Signal Corps transmitter.

Construction of the Modulator The modulator is built upon a 13"x 17"x 4" cadmium plated steel chassis, and uses a 12¼" steel panel. The modulator follows the exact chassis layout of the 810 modulator described in Chapter 27, except that the input transformer is removed from below the chassis and the two grid circuit chokes (CH_1 and CH_2) are mounted in its place. It must be remembered that peak voltages in excess of 5000 may occur in the plate circuit of the modulator, and extreme care should be taken with leads in this part of the assembly. Wiring should be done with high voltage wire, such as Belden 8833. The capacitors comprising the low pass filter following T_1 are mounted on a small bracket made of plywood, to insulate them from the chassis. The two high voltage leads are



T1-3450-0-3450 VOLTS AT 700 MA., ICAS. *CHICAGO P-2126*
T2-5 VOLTS, 10 AMP., *CHICAGO F-510H*
CH1-6 HENRIES, 700 MA. *CHICAGO R-67*
C1-0.15 UF, 3000-VOLT.
C2-THREE 4-UF 3000-VOLT
R1-100,000 OHMS, 200-WATT.
R2-ELEVEN 0.5 MEG. 2-WATT RESISTORS IN SERIES
RY1-DPST RELAY, 110 V. COIL, 20 A. CONTACTS. *POTTER & BRUMFIELD PR7A*
RFC1, RFC2-HASH FILTER, *J.W. MILLER CO. Nº 7868*

Figure 10
HIGH VOLTAGE POWER SUPPLY



S1-*CENTRALAB TYPE 2515 CERAMIC INSULATION*

SEE VIKING INSTRUCTION MANUAL FOR ADDITIONAL DETAILS

Figure 11
VIKING II AUDIO SWITCHING CIRCUIT

brought through the rear chassis wall by means of Millen 37001 high voltage terminals. Leads running through the chassis to T_1 are made of Belden 8833 wire, passing through 1/2" rubber grommets mounted in the chassis.

Construction of the Power Supply The high voltage power supply (figure 10) is mounted directly to the bottom of the relay rack. No chassis is employed, the parts being bolted directly to the steel bottom plate of the rack.

The r-f hash suppression chokes RFC_1 and RFC_2 are fastened directly to the high voltage terminals of the plate transformer. The two 872-A rectifier tubes are so located that the leads from the r-f chokes to the plate caps are only about three inches long. The use of these r-f chokes removes a parasitic buzz from the sidebands of the carrier that is often noticeable on phone stations employing mercury vapor rectifier tubes.

A 0.15-μfd., 2500-volt paper capacitor is used to resonate the filter choke to approximately 120 cycles at bleeder current drain from the supply. When full load current is drawn, the inductance of the filter choke drops, detuning the parallel resonant circuit. Improved voltage regulation is gained by this action, the no load voltage increasing only 200 volts when the transmitter is keyed for c-w operation.

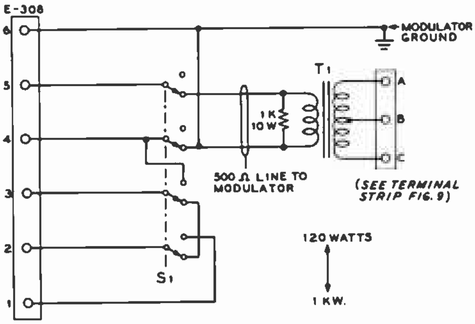
Ceramic safety caps are used on the 872-A tubes, and all exposed connections on the plate transformer, the filter choke and the high voltage capacitors are carefully wrapped with electrical tape to prevent accidental contact with these points of high voltage. A safety bleeder, R_2, is connected in parallel with R_1 to insure that the filter capacitor will be discharged even if R_1 should open up.

The power supply delivers 2500 volts when the power selector switch is in the "hi" position, and 1250 volts when the selector switch is in the "lo" position. These voltages may be dropped to 2000 and 1000 by changing the secondary taps of T_1.

Preliminary Transmitter Adjustment After the units have been wired and checked, they should be placed in the rack-cabinet as shown in figure 8, and all interconnections made. The 810 modulator should be switched out of the circuit, and all filaments in the high power units lighted. Excitation should be applied to the amplifier, which should then be neutralized according to the procedure outlined in Chapter 11.

Low plate voltage should be applied to the amplifier, which may then be loaded to about 200 milliamperes of plate current. The full voltage should next be applied to the transmitter, and amplifier loading readjusted for a plate current of 450 to 500 milliamperes. The modulator stage should now be switched into the circuit, and the bias control potentiometer adjusted for the correct resting plate current of the modulator stage.

The audio level control of the Viking II exciter may now be advanced until the plate cur-



S1-CENTRALAB TYPE 2515, CERAMIC INSULATION

T1-LINE-TO-GRID TRANSFORMER, STANCOR A-4765

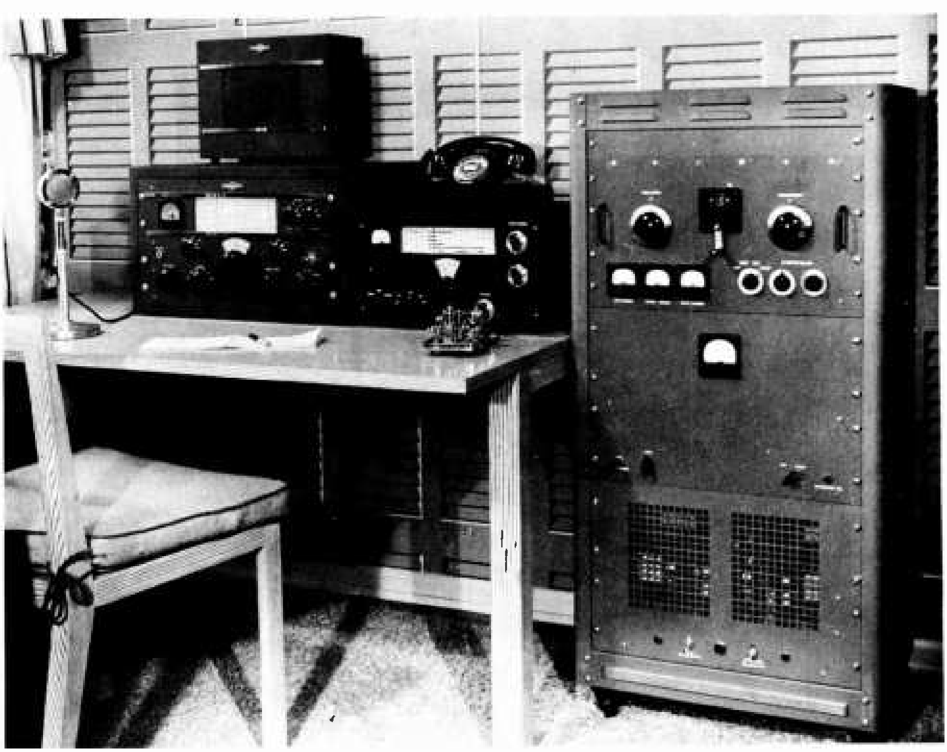
Figure 12
COLLINS 32V AUDIO SWITCHING CIRCUIT

rent of the 810 modulator stage rises to approximately 150 to 200 milliamperes under modulation. This corresponds to approximately 100 per cent modulation when no low level audio clipping is used. Under these conditions, the modulator plate current of the 807 tubes in the Viking unit will remain stationary. Care must be taken to prevent overmodulation of the transmitter, since the Viking possesses an excess of driving power for the 810 modulator stage.

The switching circuit for the Viking II exciter is shown in figure 11. If desired, the switch may be mounted on the rear apron of the chassis of the Viking, along with a suitable terminal strip for connections to the grid circuit of the 810 modulator.

The Collins 32V used as Exciter-Driver The Collins 32V series transmitters may also be employed as an r-f and audio driving unit for the kilowatt amplifier

Figure 13
VFO CONTROLLED 300-WATT PHONE-CW STATION USING 4-125A AMPLIFIER OF CHAPTER 26, SECTION 8



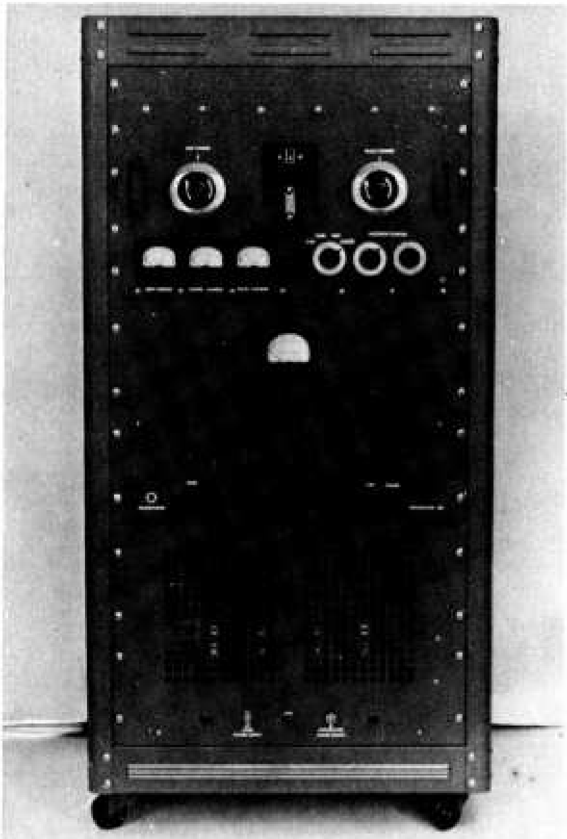


Figure 14
THE 300-WATT TRANSMITTER INSTALLATION IS MOUNTED IN A 36-INCH RACK CABINET
The dual power supply occupies the bottom of the rack, the modulator the center section, and the r-f amplifier is at the top

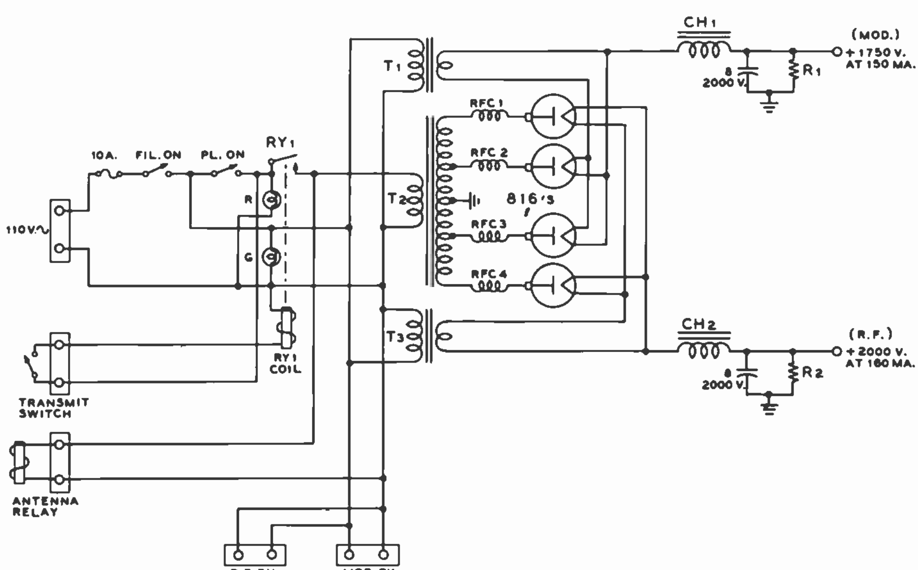


Figure 15
POWER SUPPLY FOR 4-125A TRANSMITTER

T_1, T_3—2.5 v. at 5 a. Stancor P-6133
T_2—2400-2100-0-2100-2400 v. at 375 ma. ICAS Stancor P-8032
CH_1—3-17 hy. 300 ma. Stancor C-1403
CH_2—8 hy. 300 ma. Stancor C-1413
RFC_1, RFC_4—Hash filters J.W. Miller Co. 7865, twin chokes
R_1, R_2—70,000 ohms 100 watts
Ry_1—s.p.s.t. relay 110 v. coil Advance PG-2C-115VA

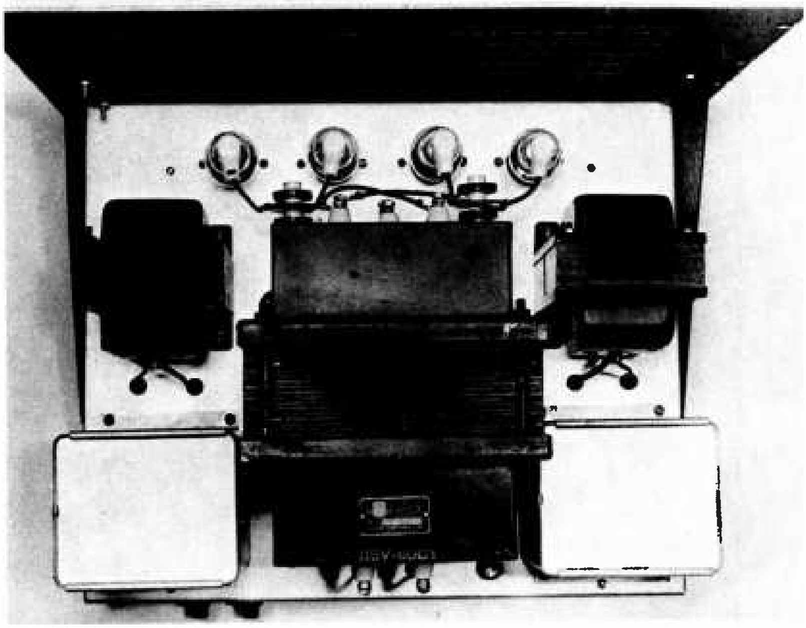


Figure 16
TOP VIEW OF DUAL-VOLTAGE POWER SUPPLY

package. The interconnecting wiring between the 32V and the kilowatt stages are shown in figure 12. Since the audio output impedance of the 32V modulator for this type of service is 500 ohms, an additional matching transformer is required in the grid circuit of the 810 modulator stage. The audio loading network for the 32V is placed across the 500-ohm line between the 32V and the matching transformer, which is located on the chassis of the 810 modulator unit.

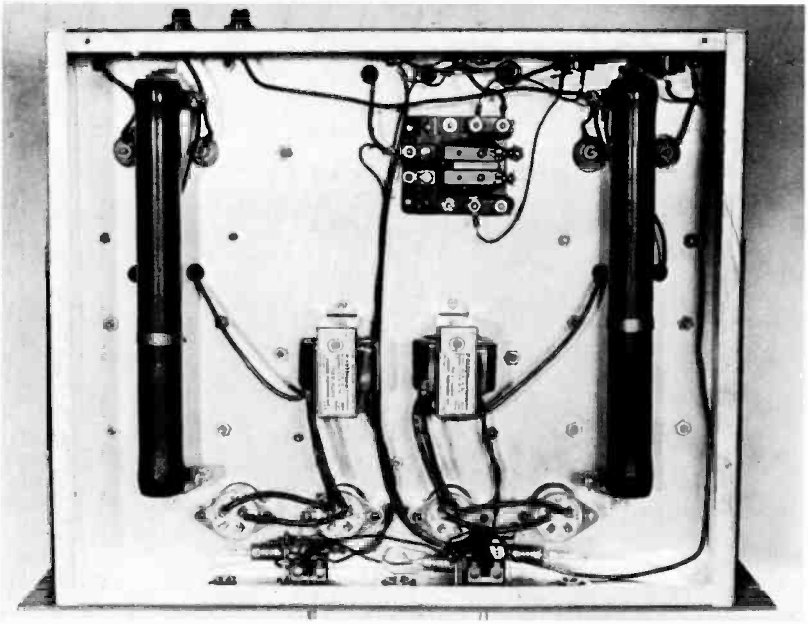
28-4 A 300-Watt Phone/ C.W. Transmitter

The 4-125A all-band amplifier of Chapter 26, Section 8; the 811-A modulator of Chapter 27, Section 8; and the power supply unit described herewith form a complete 300-watt all-band phone/c.w. transmitter. The complete installation may be mounted in a 36¾" relay rack (Bud CR-1774-G), as shown in figure 13. The PTO exciter of Chapter 25, Section 7 is employed to drive the 4-125A amplifier. If desired, a Johnson Ranger transmitter may be run at reduced output to provide excitation for this 300-watt power unit.

A close-up of the complete installation is shown in figure 14, and the schematic of the power unit is given in figure 15.

The Power Supply A dual winding transformer is used with four 816 rectifier tubes to provide 2000 volts at 150 milliamperes for the 4-125A amplifier, and 1750 volts at 150 milliamperes for the 811-A modulator. The 110-volt primary circuit is relay-controlled by the "transmit" switch located in the exciter unit.

The power supply is constructed upon a 13"x 17"x 3" aluminum chassis (Bud AC-420) and uses a 12¼" grille panel (Bud PS-812). A pair of 8½" mounting brackets (Bud MB-450) complete the assembly. The above chassis parts layout is shown in figure 16. The plate transformer is centered at the rear of the chassis with a filter choke and capacitor on each side of it. The four 816 rectifiers are mounted



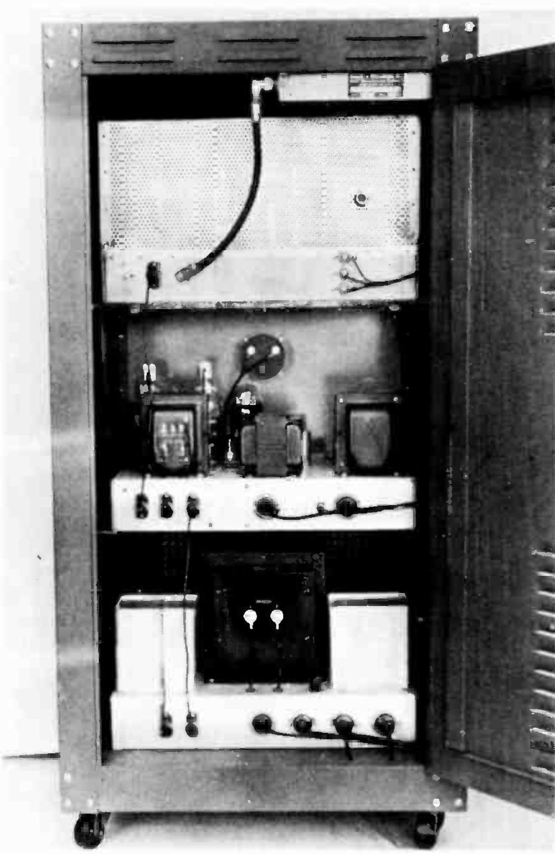


Figure 17

UNDER CHASSIS VIEW OF DUAL-VOLTAGE SUPPLY

Note: Since photograph was taken, the 816 tube sockets have been replaced with Millen 33004 sockets to reduce arcing in damp weather

Figure 18

REAR VIEW OF TRANSMITTER CABINET SHOWS SIMPLE INTERCONNECTING WIRES. A B&W TVI FILTER IS MOUNTED IN THE TOP OF THE RACK-CABINET.

between the grille panel and the plate transformer. The r-f hash chokes for the 816 tubes are mounted to the frame of the plate transformer by means of 1/2" ceramic insulators.

Under the chassis (figure 17) are located the filament transformers for the rectifier tubes, the bleeder resistors and the plate circuit relay. Along the front edge of the chassis are placed the 110-volt control switches and the pilot lamps.

The simplicity of the inter-chassis wiring is shown in the rear view, figure 18. Located in the space above the 4-125A amplifier stage is a Barker & Williamson model 426 low-pass coaxial line filter to prevent the harmonics of the amplifier stage from reaching the antenna. The case of the filter is firmly bolted to the underside of the top of the cabinet rack, and is connected to the coaxial plug of the amplifier by a short length of RG-8/U coaxial line.

Transmitter Adjustment The preliminary tuning and neutralizing procedure for the 4-125A amplifier stage is covered in Chapter 26, Section 8. Operation of the 811-A modulator stage is discussed in Chapter 27, Section 8.

Sufficient time should be allowed before transmissions to permit the 816 mercury-vapor tubes to reach operating temperatures. The first time these tubes are turned on, the filaments should burn for 15 minutes before plate voltage is applied to them. After this initial heating, the tubes need only be warmed up for one minute before subsequent application of plate voltage.

28-5 Other Transmitter Assemblies

It is obvious that other assemblies may be built up from the equipment described in Chapter 26. A transmitter of 100 watts output makes an excellent driver for the single 450-TH amplifier of Chapter 26, Section 11. A Collins 310B exciter unit is now being used to drive the push-pull 813 amplifier of Chapter 26, Section 6. It will be found that these amplifiers are flexible enough in driving requirements that, with proper care, they will work properly with almost any medium power transmitter capable of supplying a minimum of grid driving power.

CHAPTER TWENTY NINE

Power Supplies

In view of the high cost of iron-core components such as go to make up the bulk of a power supply, it is well to consider carefully the design of a new or rebuilt transmitter in terms of the minimum power supply requirements which will permit the desired performance to be obtained from the transmitter. Careful evaluation of the power supply requirements of alternative transmitter arrangements will permit the selection of that transmitter arrangement which requires the minimum of power supply components, and which makes most efficient use of such power supplies as are required.

29-1 Power Supply Requirements

A power supply for a transmitter or for a unit of station equipment should be designed in such a manner that it is capable of delivering the required current at a specified voltage, that it has a degree of regulation consistent with the requirements of the application, that its ripple level at full current is sufficiently low for the load which will be fed, that its internal impedance is sufficiently low for the job, and that none of the components shall be overloaded with the type of operation contemplated.

The meeting of all the requirements of the previous paragraph is not always a straightforward and simple problem. In many cases compromises will be involved, particularly when the power supply is for an amateur station and a number of components already on hand must be fitted into the plan. As much thought and planning should be devoted to the power-supply complement of an amateur station as usually is allocated to the r-f and a-f components of the station.

The arrival at the design for the power supply for use in a particular application may best be accomplished through the use of a series of steps, with reference to the data in this chapter by determining the values of components to be used. The first step is to establish the operating requirements of the power supply. In general these are:

1. Output voltage required under full load.

2. Minimum, normal, and peak output current.

3. Voltage regulation required over the current range.

4. Ripple voltage limit.

5. Rectifier circuit to be used.

The output voltage required of the power supply is more or less established by the operating conditions of the tubes which it will supply. The current rating of the supply, however, is not necessarily tied down by a particular tube combination. It is always best to design a power supply in such a manner that it will have the greatest degree of flexibility; this procedure will in many cases allow an existing power supply to be used without change as a portion of a new transmitter or other item of station equipment. So the current rating of a new power supply should be established by taking into consideration not only the requirements of the tubes which it immediately will feed, but also with full consideration of the best matching of power supply components in the most economical current range which still will meet the requirements. It is often long-run economy, however, to allow for any likely additional equipment to be added in the near future.

Current-Rating Considerations The minimum current drain which will be taken from a power supply will be, in most cases, merely the bleeder current. There are many cases where a particular power supply will always be used with a moderate or heavy load upon it, but when the supply is a portion of a transmitter it is best to consider the minimum drain as that of the bleeder. The minimum current drain from a power supply is of importance since it, in conjunction with the nominal voltage of the supply determines the minimum value of inductance which the input choke must have to keep the voltage from soaring when the external load is removed.

The normal current rating of a power supply usually is a round-number value chosen on the basis of the transformers and chokes on hand or available from the catalog of a reliable manufacturer. The current rating of a supply to feed a steady load such as a receiver, a speech amplifier, or a continuously-operating r-f stage should be at least equal to the steady drain of the load. However, other considerations come into play in choosing the current rating for a keyed amplifier, an amplifier of SSB signals, or a class B modulator. In the case of a supply which will feed an intermittent load such as these, the current ratings of the transformers and chokes may be *less* than the maximum current which will be taken; but the current ratings of the rectifier tubes to be used should be at least equal to the maximum current which will be taken. That is to say that 300-ma. transformers and chokes may be used in the supply for a modulator whose resting current is 100 ma. but whose maximum current at peak signal will rise to 500 ma. However, the rectifier tubes should be capable of handling the full 500 ma.

The iron-core components of a power supply which feeds an intermittent load may be chosen on the basis of the current as averaged over a period of several minutes, since it is *heating* effect of the current which is of greatest importance in establishing the ratings of such components. Since iron-core components have a relatively large amount of thermal inertia, the effect of an intermittent heavy current is offset to an extent by a key-up period or a period of low modulation in the case of a modulator. However, the current rating of a rectifier tube is established by the magnitude of the emission available from the filament of the tube; the maximum emission must not be exceeded even for a short period or the rectifier tube will be damaged. The above considerations are predicated, however, on the assumption that none of the iron-core components will become saturated due to the high intermittent current drain. If good-quality components of generous weight are chosen, saturation will not be encountered.

Voltage Regulation The general subject of voltage regulation can really be divided into two sub-problems, which differ greatly in degree. The first, and more common, problem is the case of the normal power supply for a transmitter modulator, where the current drain from the supply may vary over a ratio of four or five to one. In this case we desire to keep the voltage change under this varying load to a matter of 10 or 15 per cent of the operating voltage under full load. This is a quite different problem from the design of a power supply to deliver some voltage in the vicinity of 250 volts to an oscillator which requires two or three milliamperes of plate current; but in this latter case the voltage delivered to the oscillator must be constant within a few volts with small variations in oscillator current and with large variations in the a-c line voltage which feeds the oscillator power supply. An additional voltage regulation problem, intermediate in degree between the other two, is the case where a load must be fed with 10 to 100 watts of power at a voltage below 500 volts, and still the voltage variation with changes in load and changes in a-c line voltage must be held to a few volts at the output terminals.

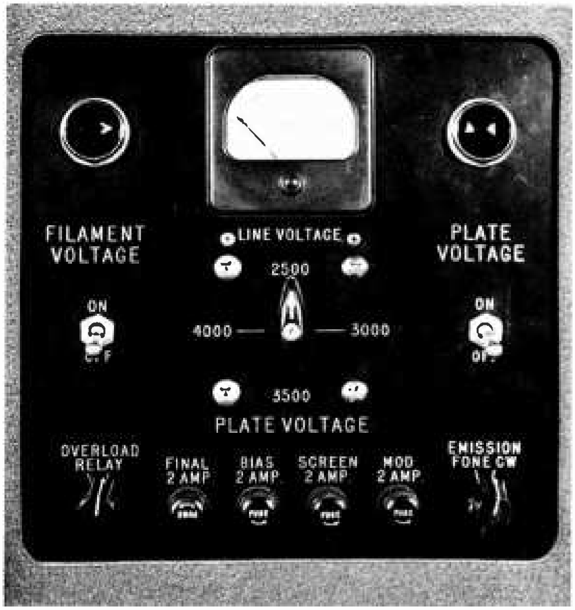


Figure 1

POWER SUPPLY CONTROL PANEL

A well designed supply control panel has separate primary switches and indicator lamps for the filament and plate circuits, overload circuit breaker, plate voltage control switch and primary circuit fuses.

These three problems are solved in the normal type of installation in quite different manners. The high-power case where output voltage must be held to within 10 to 20 per cent is normally solved by using the proper value of inductance for the input choke and proper value of bleeder at the output of the power supply. The calculations are simple: the inductance of the power-supply input choke at minimum current drain from the supply should be equal in henries to the load resistance on the supply (at minimum load current) divided by 1000. This value of inductance is called the *critical* inductance and it is the minimum value of inductance which will keep the output voltage from soaring in a choke-input power supply with minimum load upon the output. The minimum load current may be that due to the bleeder resistor alone, or it may be due to the bleeder plus the minimum drain of the modulator or amplifier to which the supply is connected.

The low-voltage low-current supply, such as would be used for a v.f.o. or the high-frequency oscillator in a receiver, usually is regulated with the aid of glow-discharge gaseous-regulator tubes. These regulators are usually called "VR tubes." Their use in various types of power supplies is discussed in Section 7. The electronically-regulated power supply, such as is used in the 20 to 100 watts power output range, also is discussed later on in this chapter and examples are given.

Ripple Considerations The ripple-voltage limitation imposed upon a power supply is determined by the load which will be fed by the supply. The tolerable ripple voltage from a supply may vary from perhaps 5 per cent for a class B or class C amplifier which is to be used for a c-w stage or amplifier of an FM signal down to a few hundredths of one per cent for the plate-voltage supply to a low-level voltage amplifier in a speech amplifier. The usual value of ripple voltage which may be tolerated in the supply for the majority of stages of a phone transmitter is between 0.1 and 2.0 per cent.

In general it may be stated that, with 60-cycle line voltage and a single-phase rectifier circuit, a power supply for the usual stages in the amateur transmitter will be of the choke-input type with a single pi-section filter following the input choke. A c-w amplifier or other stage which will tolerate up to 5 per cent ripple may be fed from a power supply whose filter consists merely of an adequate-size input choke and a single filter capacitor.

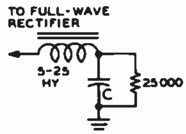
A power supply with input choke and a single capacitor also will serve in most cases to feed a class B modulator, provided the output capacitor in the supply is sufficiently large. The output capacitor in this case must be capable of storing enough energy to supply the peak-current requirement of the class B tubes on modulation peaks. The output capacitor for such a supply normally should be between 4 μfd. and 10 μfd.

Capacitances larger than 10 μfd. involve a high initial charging current when the supply is first turned on, so that an unusually large input choke should be used ahead of the capacitor to limit the peak-current surge through the rectifier tubes. A capacitance of less than 4 μfd. may reduce the power output capability of a class B modulator when it is passing the lower audio frequencies, and in addition may superimpose a low-frequency "growl" on the output signal. This growl will be apparent only when the supply is delivering a relatively high power output; it will not be present when modulation is at a low level.

When a stage such as a low-level audio amplifier requires an extremely low value of ripple voltage, but when regulation is not of importance to the operation of the stage, the high degree of filtering usually is obtained through the use of a resistance-capacitance filter. This filter usually is employed in addition to the choke-capacitor filter in the power supply for the higher-level stages, but in some cases when the supply is to be used only to feed low-current stages the entire filter of the power supply will be of the resistance-capacitance type. Design data for resistance-capacitance filters is given in a following paragraph.

When a low-current stage requires very low ripple in addition to excellent voltage regulation, the power supply filter often will end with one or more gaseous-type voltage-regulator tubes. These VR tubes give a high degree of filtering in addition to their voltage-regulating action, as is obvious from the fact that the tubes tend to hold the voltage drop across their elements to a very constant value regardless of the current passing through the tube. The VR tube is quite satisfactory for improving both the regulation and ripple characteristics of a supply when the current drain will not exceed 25 to 35 ma. depending upon the type of VR tube. Some types are rated at a maximum current drain of 30 ma. while others are capable of passing up to 40 ma. without damage. In any event the minimum current through the VR tube will occur when the associated circuit is taking maximum current. This minimum current requirement is 5 ma. for all types of gaseous-type voltage-regulator tubes.

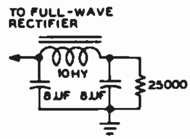
Other types of voltage-regulation systems, in addition to VR tubes, exhibit the added characteristic of offering a low value of ripple across their output terminals. The electronic-type of voltage-regulated power supply is capable of delivering an extremely small value of ripple across its output terminals, even though the rectifier-filter system ahead of the regulator delivers a relatively high value of ripple, such as in the vicinity of 5 to



RIPPLE IN TERMS OF C AT FULL LOAD

CAPACITANCE, C	PERCENT RIPPLE
2 µF	13.1
3 µF	8.5
4 µF	6.2
6 µF	4.0

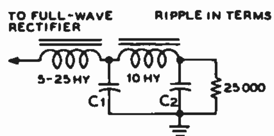
FIGURE 2



RIPPLE IN TERMS OF LOAD RESISTANCE

LOAD, OHMS	PERCENT RIPPLE
25000 (BLEEDER ONLY)	0.02
15000	0.04
10000	0.06
5000	0.1
3000	0.17
2000	0.25

FIGURE 3



RIPPLE IN TERMS OF C1 AND C2 AT FULL LOAD

C1	C2	PERCENT RIPPLE
2	2	1.2
3	2	0.7
4	4	0.25
8	8	0.06

FIGURE 4

10 per cent. In fact, it is more or less self evident that the better the regulation of such a supply, the better will be its ripple characteristic. It must be remembered that the ripple output of a voltage-regulated power supply of any type will rise rapidly when the load upon the supply is so high that the regulator begins to lose control. This will occur in a supply of the electronic type when the voltage ahead of the series regulator tube falls below a value equal to the sum of the minimum drop across the tube at that value of current, plus the output voltage. In the case of a shunt regulator of the VR-tube type, the regulating effect will fail when the current through the VR tube falls below the usual minimum value of about 5 ma.

Calculation of Ripple Although figures 2, 3 and 4 give the value of ripple voltage for several more or less standard types of filter systems, it is often of value to be able to calculate the value of ripple voltage to be expected with a particular set of filter components. Fortunately, the approximate ripple percentage for normal values of filter components may be calculated with the aid of rather simple formulas. In the two formulas to follow it is assumed that the line frequency is 60 cycles and that a full wave or a full-wave bridge rectifier is being used. For the case of a single-section choke-input filter as illustrated in figure 1, or for the ripple at the output of the first section of a two-section choke input filter the equation is as follows:

$$\text{Per cent ripple} = \frac{118}{LC-1}$$

where LC is the product of the input choke inductance in henrys (at the operating current to be used) and the capacitance which follows this choke expressed in microfarads.

In the case of a two-section filter, the per cent ripple at the output of the first section is determined by the above formula. Then this percentage is multiplied by the filter reduction factor of the following section of filter. This reduction factor is determined through the use of the following formula:

$$\text{Filter reduction factor} = \frac{LC-1}{1.76}$$

Where LC again is the product of the inductance and capacitance of the filter section. The reduction factor will turn out to be a decimal value, which is then multiplied by the percentage ripple obtained from the use of the preceding formula.

As an example, take the case of the filter diagrammed in figure 5. The LC product of the first section is 16. So the ripple to be expected at the output of the first section will be: 118/(16−1) or 118/15, which gives 7.87 per cent. Then the second section, with an LC product of 48, will give a reduction factor of: 1.76/(48−1) or 1.76/47 or 0.037. Then the ripple percentage at the output of the total filter will be: 7.87 times 0.037 or slightly greater than 0.29 per cent ripple.

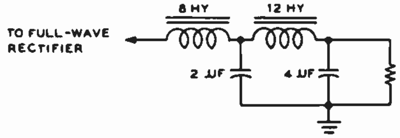


Figure 5
SAMPLE FILTER FOR CALCULATION OF RIPPLE

Resistance-Capacitance Filters In many applications where the current drain is relatively small, so that the voltage drop across the series resistors would not be excessive, a filter system made up of resistors and capacitors only may be used to advantage. In the normal case, where the reactance of the shunting capacitor is very much smaller than the resistance of the load fed by the filter system, the ripple reduction per section is equal to $1/(2\pi RC)$. In terms of the 120-cycle ripple from a full-wave rectifier the ripple-reduction factor becomes: 1.33/RC where R is expressed in thousands of ohms and C in microfarads. For 60-cycle ripple the expression is: 2.66/RC with R and C in the same quantities as above.

Filter System Resonance Many persons have noticed, particularly when using an input choke followed by a 2-µfd. first filter capacitor, that at some value of load current the power supply will begin to hum excessively and the rectifier tubes will tend to flicker or one tube will seem to take all the load while the other tube dims out. If the power supply is shut off and then again started, it may be the other tube which takes the load; *or* first one tube and then the other will take the load as the current drain is varied. This condition, as well as other less obvious phenomena such as a tendency for the first filter capacitor to break down regardless of its voltage rating or for rectifier tubes to have short life, results from resonance in the filter system following the high-voltage rectifier.

The condition of resonance is seldom encountered in low-voltage power supplies since the capacitors used are usually high enough so that resonance does not occur. But in high-voltage power supplies, where both choke inductance and filter capacitance are more expensive, the condition of resonance happens frequently. The product of inductance and capacitance which resonates at 120 cycles is 1.77. Thus a 1-µfd. capacitor and a 1.77-henry choke will resonate at 120 cycles. In almost any normal case the LC product of any section in the filter system will be somewhat greater than 1.77, so that resonance at 120 cycles will seldom take place. But the LC product for resonance at 60 cycles is about 7.1. This is a value frequently encountered in the input section of a high-voltage power supply. It occurs with a 2-µfd. capacitor and a choke which has 3.55 henrys of inductance at some current value. With a 2-µfd. filter capacitor following this choke, resonance will occur at the current value which causes the inductance of the choke to be 3.55 henrys. When this resonance does occur, one rectifier tube (assuming mercury-vapor types) will dim and the other will become much brighter.

Thus we see that we must avoid the LC products of 1.77 and 7.1. With a swinging-type input choke, whose inductance varies over a 5-to-1 range, we see that it is possible for resonance to occur at 60 cycles at a low value of current drain, and then for resonance to occur at 120 cycles at approximately full load on the power supply. Since the LC product must certainly be greater than 1.77 for satisfactory filtering along with peak-current limitation on the rectifier tubes, we see that with a swinging-type input choke the LC product must still be greater than 7.1 at maximum current drain from the power supply. To allow a reasonable factor of safety, it will be well to keep the LC product at maximum current drain above the value 10.

From the above we see that we can just get by with a 2-μfd. first capacitor following the input choke when this choke is of the more-or-less standard 5-25 henry swinging variety. Some of the less expensive types of chokes swing from about 3 to 12 henrys, so we see that the first capacitor must be greater than 2 μfd. to avoid resonance with these chokes. A 3-μfd. capacitor may be used if available, but a standard 4-μfd. unit will give a greater safety factor.

29-2 Rectification Circuits

There are a large number of rectifier circuits that may be used in the power supplies for station equipment. But the simpler circuits are more satisfactory for the power levels up to the maximum permitted the radio amateur. Figure 6 shows the three most common circuits used in power supplies for amateur equipment.

Half-Wave Rectifiers A half-wave rectifier, as shown in figure 6A, passes one half of the wave of each cycle of the alternating current and blocks the other half. The output current is of a *pulsating* nature, which can be smoothed into pure, direct current by means of filter circuits. Half-wave rectifiers produce a pulsating current which has zero output during one-half of each a-c cycle; this makes it difficult to filter the output properly into d.c. and also to secure good voltage regulation for varying loads.

Full-Wave Rectifiers A full-wave rectifier consists of a pair of half-wave rectifiers working on opposite halves of the cycle, connected in such a manner that each half of the rectified a-c wave is combined in the output as shown in figure 7. This pulsating unidirectional current can be filtered to any desired degree, depending upon the particular application for which the power supply is designed.

A full-wave rectifier may consist of two plates and a filament, either in a single glass or metal envelope for low-voltage rectification or in the form of two separate tubes, each having a single plate and filament for high-voltage rectification. The plates are connected across the high-voltage a-c power transformer winding, as shown in figure 6B. The power transformer is for the purpose of transforming the 110-volt a-c line supply to the desired secondary a-c voltages for filament and plate supplies. The transformer delivers alternating current to the two plates of the rectifier tube; one of these plates is positive at any instant during which the other is negative. The center point of the high-voltage transformer winding

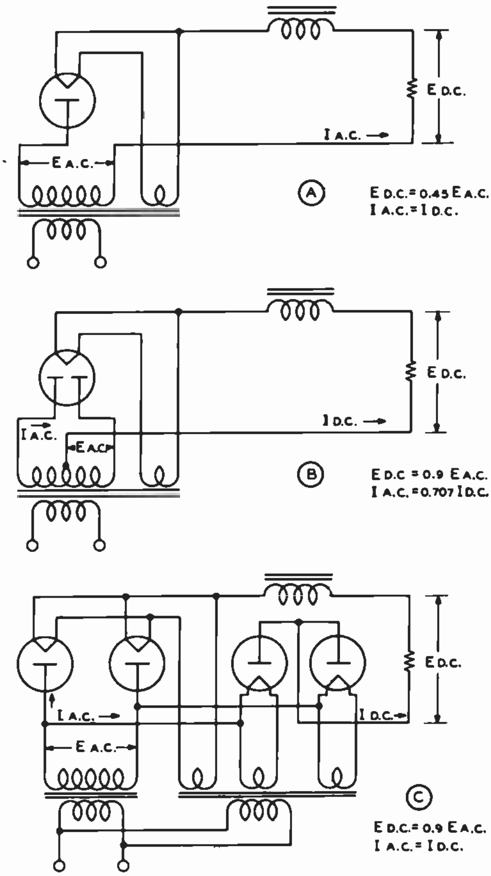


Figure 6
MOST COMMON RECTIFIER CIRCUITS
(A) shows a half-wave rectifier circuit, (B) is the standard full-wave rectifier circuit used with a dual rectifier or two rectifier tubes, and (C) is the bridge rectifier circuit.

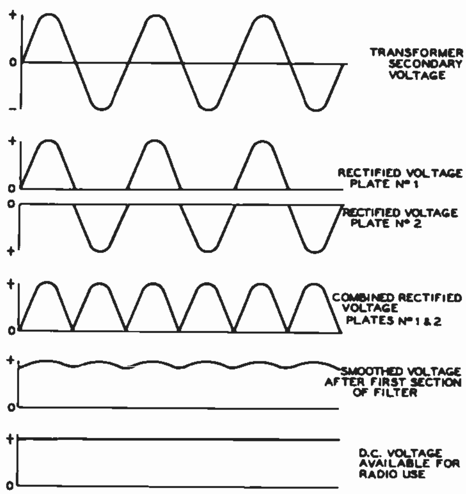


Figure 7

FULL-WAVE RECTIFICATION

Showing transformer secondary voltage, the rectified output of each tube, the combined output of the rectifier, the smoothed voltage after one section of filter, and the substantially pure d.c. output of the rectifier-filter after additional sections of filter.

is usually grounded and is, therefore, at zero voltage, thereby constituting the negative B connection.

While one plate of the rectifier tube is conducting, the other is inoperative, and vice versa. The output voltages from the rectifier tubes are connected together through the common rectifier filament circuit. Thus the plates alternately supply pulsating current to the output (load) circuit. The rectifier tube filaments or cathodes are always positive in polarity with respect to the plate transformer in this type of circuit.

The output current pulsates 120 times per second for a full-wave rectifier connected to a 60-cycle a-c line supply; hence the output of the rectifier must pass through a filter to smooth the pulsations into direct current. Filters are designed to select or reject alternating currents; those most commonly used in a-c power supplies are of the *low-pass* type. This means that pulsating currents which have a frequency below the cutoff frequency of the filter will pass through the filter to the load. Direct current can be considered as alternating current of zero frequency; this passes through the low-pass filter. The 120-cycle pulsations are similar to alternating current in characteristic, so that the filter must be designed to have a *cutoff* at a frequency *lower than 120 cycles* (for a 60 cycle a-c supply).

Bridge Rectification The bridge rectifier (figure 6C) is a type of full-wave circuit in which four rectifier elements or tubes are operated from a single high-voltage winding on the power transformer.

While twice as much output voltage can be obtained from a bridge rectifier as from a center-tapped circuit, the permissible output current is only one-half as great for a given power transformer. In the bridge circuit, four rectifiers and three filament heating transformer windings are needed, as against two rectifiers and one filament winding in the center-tapped full-wave circuit. In a bridge rectifier circuit, the inverse peak voltage impressed on any one rectifier tube is halved, which means that tubes of lower peak inverse voltage rating may be used for a given voltage output.

29-3 The Standard Power Supply Circuits

Choke input is shown for all three of the standard circuits of figure 6, since choke input gives the best utilization of rectifier-tube and power transformer capability, and in addition gives much better regulation. Where greater output voltage is a requirement, where the load is relatively constant so that regulation is not of great significance, and where the rectifier tubes will be operated well within their peak-current ratings, the capacitor-input type of filter may be used.

The capacitor-input filter gives a no-load output voltage equal approximately to the peak voltage being applied to the rectifier tubes. At full load, the d-c output voltage is usually slightly above one-half the secondary a-c voltage of the transformer, with the normal values of capacitance at the input to the filter. With large values of input capacitance, the output voltage will run somewhat higher than the r-m-s secondary voltage applied to the tubes, but the peak current flowing through the rectifier tubes will be many times as great as the d-c output current of the power supply. The half-wave rectifier of figure 6A is commonly used with capacitor input and resistance-capacitance filter as a high-voltage supply for a cathode-ray tube. In this case the current drain is very small so that the peak-current rating of the rectifier tube seldom will be exceeded.

The circuit of figure 6B is most commonly used in medium-voltage power supplies since this circuit is the most economical of filament transformers, rectifier tubes and sockets, and space. But the circuit of figure 6C, commonly called the *bridge rectifier*, gives better transformer utilization so that the circuit is most commonly used in higher powered supplies. The circuit has the advantage that the entire secondary of the transformer is in use at all times, instead of each side being used alternately as in the case of the full-wave rectifier. As a point of interest, the current flow through the secondary of the plate transformer is a substantially pure a-c wave as a result of better transformer utilization, instead of the pulsating d-c wave through each half of the power transformer secondary in the case of the full-wave rectifier.

The circuit of figure 6C will give the greatest value of output power for a given transformer weight and cost in a single-phase power supply as illustrated. But in attempting to bridge rectify the whole secondary of a transformer designed for a *full-wave* rectifier, in order to obtain doubled output voltage, make sure that the insulation rating of the transformer to be used is adequate. In the bridge rectifier circuit the center of the high-voltage winding is at a d-c potential of one-half the total voltage output from the rectifier. In a normal full-wave rectifier the center of the high-voltage winding is grounded. So in the bridge rectifier the entire high-voltage secondary of the transformer is subjected to twice the peak-voltage stress that would exist if the same transformer were used in a full-wave rectifier. High-quality full-wave transformers will withstand bridge operation quite satisfactorily so long as the total output voltage from the supply is less than perhaps 4500 volts. But inexpensive transformers, whose insulation is just sufficient for full-wave operation, will break down when bridge rectification of the entire secondary is attempted.

Special Single-Phase Rectification Circuits Figure 8 shows six circuits which may prove valuable when it is desired to obtain more than one output voltage from one plate transformer or where some special combination of voltages is required. Figure 8A shows a more or less common method for obtaining full voltage and half voltage from a bridge rectification circuit. With this type of circuit separate input chokes and filter systems are used on both output voltages. If a transformer designed for use with a full-wave rectifier is used in this circuit, the current drain from the full-voltage tap is doubled and added to the drain from the half-voltage tap to determine whether the rating of the transformer is being exceeded. Thus if the transformer is rated at 1250 volts at 500 ma. it will be permissible to pull 250 ma. at 2500 volts with no drain from the 1250-volt tap, or the drain from the 1250-volt tap may be 200 ma. if the drain from the 2500-volt tap is 150 ma., and so forth.

Figure 8B shows a system which may be convenient for obtaining two voltages which are not in a ratio of 2 to 1 from a bridge-type rectifier; a transformer with taps along the winding is required for the circuit however. With the circuit arrangement shown the voltage from the tap will be greater than one-half the voltage at the top. If the circuit is changed so that the plates of the two rectifier tubes are connected to the outside of the winding instead of to the taps, and the cathodes of the other pair are connected to the taps instead of to the outside, the total voltage output of the rectifier will be the same, but the voltage at the tap position will be *less* than half the top voltage.

An interesting variable-voltage circuit is shown in figure 8C. The arrangement may be used to increase or decrease the output voltage of a conventional power supply, as represented by transformer T_1, by adding another filament transformer to isolate the filament circuits of the two rectifier tubes and adding another plate transformer between the filaments of the two tubes. The voltage contribution of the added transformer T_2 may be subtracted from or added to the voltage produced by T_1 simply by reversing the double-pole double-throw switch S. A serious disadvantage of this circuit is the fact that the entire secondary winding of transformer T_2 must be insulated for the total output voltage of the power supply.

An arrangement for operating a full-wave rectifier from a plate transformer not equipped with a center tap is shown in figure 8D. The two chokes L_1 must have high inductance ratings at the operating current of the plate supply to hold down the *a-c* current load on the secondary of the transformer since the *total* peak voltage output of the plate transformer is impressed across the chokes alternately. However, the chokes need only have half the current rating of the filter choke L_2 for a certain current drain from the power supply since only half the current passes through each choke. Also, the two chokes L_1 act as input chokes so that an additional swinging choke is not required for such a power supply.

A conventional two-voltage power supply with grounded transformer center tap is shown in figure 8E. The output voltages from this circuit are separate and not additive as in the circuit of figure 8B. Figure 8F is of ad-

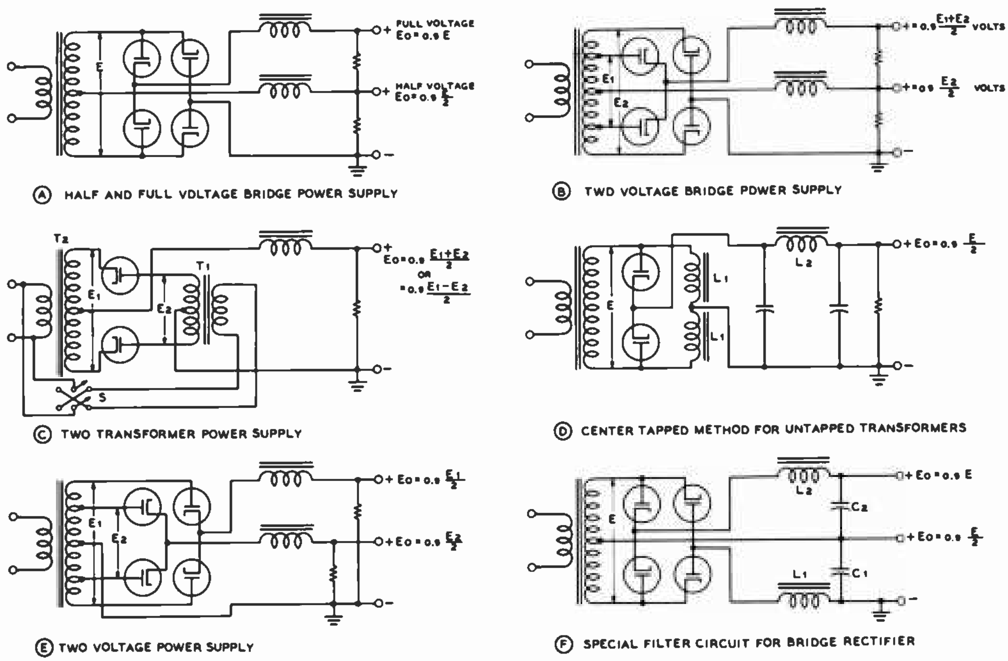


Figure 8

SPECIAL SINGLE-PHASE RECTIFICATION CIRCUITS

A description of the application and operation of each of these special circuits is given in the accompanying text.

vantage when it is desired to operate Class B modulators from the half-voltage output of a bridge power supply and the final amplifier from the full voltage output. Both L_1 and L_2 should be swinging chokes but the total drain from the power supply passes through L_1 while only the drain of the final amplifier passes through L_2. Capacitors C_1 and C_2 need be rated at only half the maximum output voltage of the power supply, plus the usual safety factor. This arrangement is also of advantage in holding down the "key-up" voltage of a c-w transmitter since both L_1 and L_2 are in series, and their inductances are additive, insofar as the "critical inductance" of a choke-input filter is concerned. If 4 μfd. capacitors are used at both C_1 and C_2 adequate filter will be obtained on both plate supplies for hum-free radiophone operation.

Polyphase Rectification Circuits It is usual practice in commercial equipment installations when the power drain from a plate supply is to be greater than about one kilowatt to use a polyphase rectification system. Such power supplies offer better transformer utilization, less ripple output and better power factor in the load placed upon the a-c line. However, such systems require a source of three-phase (or two-phase with Scott connection) energy. Several of the more common polyphase rectification circuits with their significant characteristics are shown in figure 9. The increase in ripple frequency and decrease in percentage of ripple is apparent from the figures given in figure 9. The circuit of figure 9C gives the best transformer utilization as does the bridge circuit in the single-phase connection. The circuit has the further advantage that there is no average d-c flow in the transformer, so that three single-phase transformers may be used. A tap at half-voltage may be taken at the junction of the star transformers, but there will be d-c flow in the transformer secondaries with the power supply center tap in use. The circuit of figure 9A has the disadvantage that there is an average d-c flow in each of the windings.

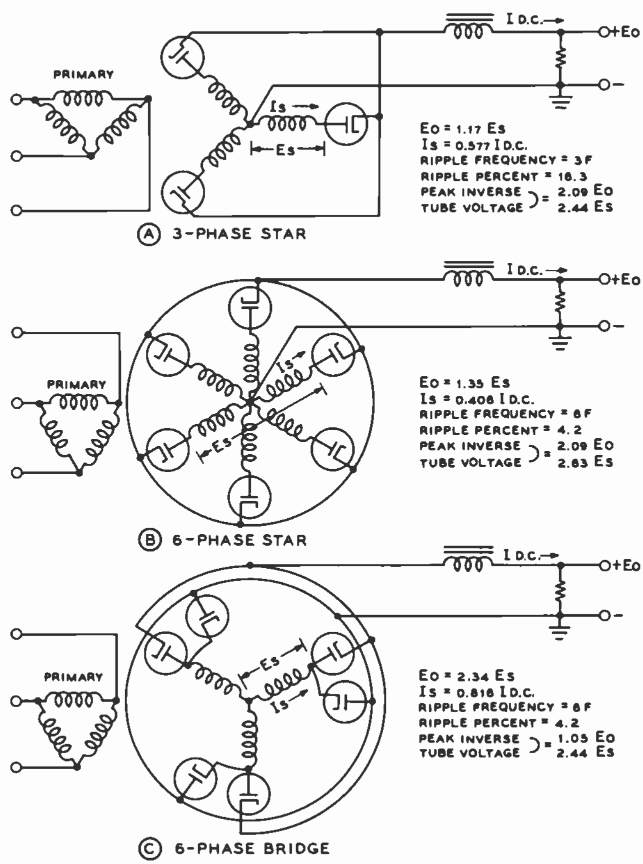


Figure 9

COMMON POLYPHASE-RECTIFICATION CIRCUITS

These circuits are used when polyphase power is available for the plate supply of a high-power transmitter. The circuit at (B) is also called a three-phase full-wave rectification system. The circuits are described in the accompanying text.

Rectifiers Rectifying elements in high-voltage plate supplies are almost invariably electron tubes of either the high-vacuum or mercury-vapor type, although selenium rectifier stacks containing a large number of elements are often used. Low-voltage high-current supplies may use argon gas rectifiers (Tungar tubes), selenium rectifiers, or other types of dry-disc rectification elements. The *xenon* rectifier tubes offer some advantage over mercury-vapor rectifiers for high-voltage applications where extreme temperature ranges are likely to be encountered. However, such rectifiers (3B25 for example) are considerably more expensive than their mercury-vapor counterparts.

Peak Inverse Plate Voltage and Peak Plate Current In an a-c circuit, the maximum peak voltage or current is $\sqrt{2}$ or 1.41 times that indicated by the a-c meters in the circuit. The meters read the *root-mean-square* (r.m.s.) values, which are the peak values divided by 1.41 for a sine wave.

If a potential of 1,000 r.m.s. volts is obtained from a high-voltage secondary winding of a transformer, there will be 1,410-volts peak potential from the rectifier plate to ground. In a single-phase supply the rectifier tube has this voltage impressed on it, either positively when the current flows or *"inverse"* when the current is blocked on the other half-cycle. The *inverse peak voltage* which the tube will stand safely is used as a rating for rectifier tubes. At higher voltages the tube is liable to arc back, thereby destroying or damaging it. The relations between peak inverse voltage, total transformer voltage and filter output voltage depend upon the characteristics of the filter and rectifier circuits (whether full- or half-wave, bridge, single-phase or polyphase, etc.).

Rectifier tubes are also rated in terms of *peak plate current.* The actual direct load current which can be drawn from a given rectifier tube or tubes depends upon the type of filter circuit. A full-wave rectifier with capacitor input passes a peak current several times the direct load current.

In a filter with choke input, the peak current is not much greater than the load current if the inductance of the choke is fairly high (assuming full-wave rectification).

A full-wave rectifier with two rectifier elements requires a transformer which delivers twice as much a-c voltage as would be the case with a half-wave rectifier or bridge rectifier.

Mercury-Vapor Rectifier Tubes The inexpensive mercury-vapor type of rectifier tube is almost universally used in the high-voltage plate supplies of amateur and commercial transmitters. Most amateurs are quite familiar with the use of these tubes but it should be pointed out that when new or long-unused mercury-vapor tubes are first placed in service, the filaments should be operated at normal temperature for approximately twenty minutes before plate voltage is applied, in order to remove all traces of mercury from the cathode and to clear any mercury deposit from the top of the envelope. After this preliminary warm-up with a new tube, plate voltage may be applied within 20 to 30 seconds after the time the filaments are turned on, each time the power supply is used. If plate voltage should be applied before the filament is brought to full temperature, active material may be knocked from the oxide-coated filament and the life of the tube will be greatly shortened.

Small r-f chokes must sometimes be connected in series with the plate leads of mercury-vapor rectifier tubes in order to prevent the generation of radio-frequency hash. These r-f chokes must be wound with sufficiently heavy wire to carry the load current and must have enough inductance to attenuate the r-f parasitic noise current to prevent it from flowing in the filter supply leads and then being radiated into nearby receivers. Manufactured mercury-vapor rectifier hash chokes are available in various current ratings from the James Millen Manufacturing Company in Malden, Mass., and from the J.W. Miller Company in Los Angeles.

When mercury-vapor rectifier tubes are operated in parallel in a power supply, small resistors or small iron-core choke coils should be connected in series with the plate lead of each tube. These resistors or inductors tend to create an equal division of plate current between parallel tubes and prevent one tube from carrying the major portion of the current. When high vacuum rectifiers are operated in parallel, these chokes or resistors are not required.

Transformerless Power Supplies Figure 10 shows a group of five different types of transformerless power supplies which are operated directly from the a-c line. Circuits of the general type are normally found in a.c.-d.c. receivers but may be used in low-powered exciters and in test instruments. When circuits such as shown in (A) and (B) are operated directly from the a-c line, the rectifier element simply rectifies the line current and delivers the alternate half cycles of energy to the filter network. With the normal type of rectifier tube, load currents up to approximately 75 ma. may be employed. The d-c voltage output of the filter will be slightly less than the r-m-s line voltage, depending upon the particular type of rectifier tube employed. With the introduction of the miniature selenium rectifier, the transformerless power supply has become a very convenient source of moderate voltage at currents up to perhaps 500 ma. A number of advantages are offered by the selenium rectifier as compared to the vacuum tube rectifier. Outstanding among these are the factors that the selenium rectifier operates instantly, and that it requires no heater power in order to obtain emission. The amount of heat developed by the selenium rectifier is very much less than that produced by an equivalent vacuum-tube type of rectifier.

In the circuits of figure 10 (A), (B) and (C), capacitors C_1 and C_2 should be rated at approximately 150 volts and for a normal degree of filtering and capacitance, should be between 15 to 60 μfd. In the circuit of figure 10D, capacitor C_1 should be rated at 150 volts and capacitor C_2 should be rated at 300 volts. In the circuit of figure 10E, capacitors C_1 and C_2 should be rated at 150 volts and C_3 and C_4 should be rated at 300 volts.

The d-c output voltage of the line rectifier may be stabilized by means of a VR tube. However, due to the unusually low internal resistance of the selenium rectifier, transformerless

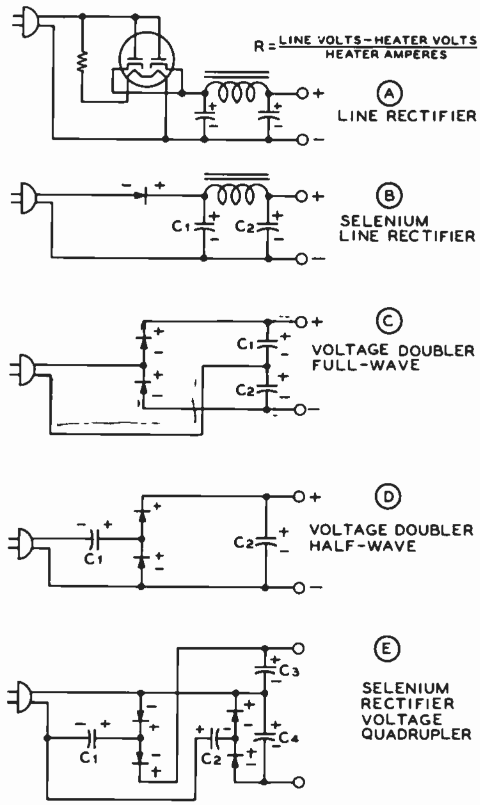


Figure 10

TRANSFORMERLESS POWER-SUPPLY CIRCUITS

Circuits such as shown above are also frequently called line-rectifier circuits. Selenium rectifiers, vacuum diodes, or gas diodes may be used as the rectifying elements in these circuits.

power supplies using this type of rectifying element can normally be expected to give very good regulation.

Voltage-Doubler Circuits Figures 10C and 10D illustrate two simple voltage-doubler circuits which will deliver a d-c output voltage equal approximately to twice the r-m-s value of the power line voltage. The no-load d-c output voltage is equal to 2.82 times the r-m-s line voltage value. At high current levels, the output voltage will be slightly under twice the line voltage. The circuit of figure 10C is of advantage when the lowest level of ripple is required from the power supply, since its ripple frequency is equal to twice the line frequency. The circuit of figure 10D is of advantage when it is desired to use the grounded side of the a-c line in a permanent installation as the return circuit for the power supply. However, with the circuit of figure 10D the ripple frequency is the same as the a-c line frequency.

Voltage Quadrupler The circuit of figure 10E illustrates a voltage quadrupler circuit for miniature selenium rectifiers. In effect this circuit is equivalent to two voltage doublers of the type shown in figure 10D with their outputs connected in series. The circuit delivers a d-c output voltage under light load approximately equal to four times the r-m-s value of the line voltage. The no-load d-c output voltage delivered by the quadrupler is equal to 5.66 times the r-m-s line voltage value and the output voltage decreases rather rapidly as the load current is increased.

In each of the circuits in figure 10 where selenium rectifiers have been shown, conventional high-vacuum rectifiers may be substituted with their filaments connected in series and an appropriate value of the line resistor added in series with the filament string.

29-4 Simple Transformer-Operated Power Supplies

Most of the newer high-G_m pentodes operate quite effectively at plate voltages in the vicinity of 110 to 130 volts. Such voltages can be obtained through use of the transformerless power supplies just described, but it is better in many cases to isolate the power supply from the a-c line by means of a transformer especially designed for such an application, or by means of two filament transformers connected back-to-back.

Figure 11A shows two filament transformers connected back-to-back in a simple low-voltage power supply arrangement. The output power available from such a power supply is limited by the leakage inductance and current capability of the two filament transformers. The more complex circuits of figure 10 may be used with such an arrangement when higher voltage at relatively low current is required from such a supply.

When greater current capability is required of such a supply, one of the small isolation transformers designed for such an application, such as shown in figure 11B and in several

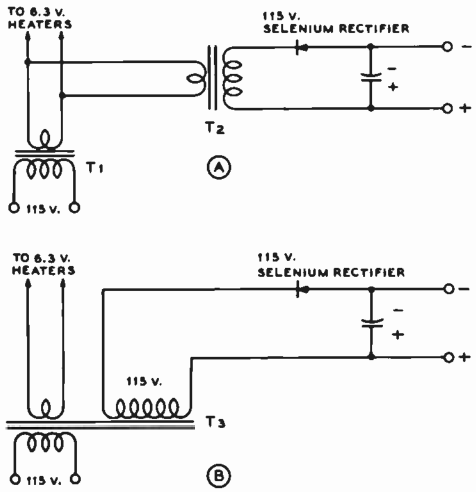


Figure 11
SIMPLE SELENIUM-RECTIFIER LOW-VOLTAGE SUPPLIES

The circuit at (A) may be used to deliver either positive or negative voltage at a relatively low current drain with output voltage in the vicinity of 100 volts. Transformers T_1 and T_2 are 6.3-volt filament transformers, T_2 being back-connected with respect to T_1. The (B) circuit is commonly used in small items of test equipment, converters, boosters, and such. With a 1:1 transformer at T_3, the output voltage will be between 115 and 135 under full load, depending upon the capacitance of the input filter capacitor. The current rating is dependent upon the current rating of the transformer and the selenium rectifier.

of the small units described in other chapters, may be used with good results.

29-5 Power Supply Components

The usual components which go to make up a power supply, in addition to rectifiers which have already been discussed, are filter capacitors, bleeder resistors, transformers, and chokes. These components normally will be purchased especially for the intended application, taking into consideration the factors discussed earlier in this chapter.

Filter Capacitors There are two types of filter capacitors: (1) paper dielectric type, (2) electrolytic type.

Paper capacitors consist of two strips of metal foil separated by several layers of special paper. Some types of paper capacitors are wax-impregnated, but the better ones, especially the high-voltage types, are oil-impregnated and oil-filled. Some capacitors are rated both for *flash* test and normal operating voltages; the latter is the important rating and is the maximum voltage which the capacitor should be required to withstand in service.

The capacitor across the rectifier circuit in a capacitor-input filter should have a working voltage rating equal at *least* to 1.41 times the r-m-s voltage output of the rectifier. The remaining capacitors may be rated more nearly in accordance with the d-c voltage.

The electrolytic capacitor consists of two aluminum electrodes in contact with a conducting paste or liquid which acts as an *electrolyte*. A very thin film of oxide is formed on the surface of one electrode, called the *anode*. This film of oxide acts as the dielectric. The electrolytic capacitor must be correctly connected in the circuit so that the anode always is at a positive potential with respect to the electrolyte, the latter actually serving as the other electrode (plate) of the capacitor. A reversal of the polarity for any length of time will ruin the capacitor.

The dry type of electrolytic capacitor uses an electrolyte in the form of paste. The dielectric in electrolytic capacitors is not perfect; these capacitors have a much higher direct current leakage than the paper type.

The high capacitance of electrolytic capacitors results from the thinness of the film which is formed on the plates. The maximum voltage that can be safely impressed across the average electrolytic filter capacitor is between 450 and 600 volts; the working voltage is usually rated at 450. When electrolytic capacitors are used in filter circuits of high-voltage supplies, the capacitors should be connected in series. The positive terminal of one capacitor must connect to the negative terminal of the other, in the same manner as dry batteries are connected in series.

It is not necessary to connect shunt resistors across each electrolytic capacitor section as it is with paper capacitors connected in series, because electrolytic capacitors have fairly low internal d-c resistance as compared to paper capacitors. Also, if there is any variation in resistance, it is that electrolytic unit in the poorest condition which will have the highest leakage current, and therefore the voltage across this capacitor will be lower than that across one of the series connected units in better condition and having higher internal resistance. Thus we see that equalizing resistors are not only unnecessary across series-connected electrolytic capacitors but are actually undesirable. This assumes, of course, similar capacitors by the same manufacturer and of the same capacitance and voltage rating. It is *not advisable* to connect in series electrolytic capacitors of different make or ratings.

There is very little economy in using electrolytic capacitors in series in circuits where more than two of these capacitors would be required to prevent voltage breakdown.

Electrolytic capacitors can be greatly reduced in size by the use of etched aluminum foil for the anode. This greatly increases the surface area, and the dielectric film covering it, but raises the power factor slightly. For this reason, ultra-midget electrolytic capacitors ordinarily should not be used at full rated d-c voltage when a high a-c component is present, such as would be the case for the input capacitor in a capacitor-input filter.

Bleeder Resistors A heavy duty resistor should be connected across the output of a filter in order to draw some load current at all times. This resistor avoids soaring of the voltage at no load when swinging choke input is used, and also provides a means for discharging the filter capacitors when no external vacuum-tube circuit load is connected to the filter. This *bleeder* resistor should normally draw approximately 10 per cent of the full load current.

The power dissipated in the bleeder resistor can be calculated by dividing the square of the d-c voltage by the resistance. This power is dissipated in the form of heat, and, if the resistor is not in a well-ventilated position, the wattage rating should be higher than the actual wattage being dissipated. High-voltage, high-capacitance filter capacitors can hold a dangerous charge if not bled off, and wire-wound resistors occasionally open up without warning. Hence it is wise to place carbon resistors in series across the regular wire-wound bleeder.

When purchasing a bleeder resistor, be sure that the resistor will stand not only the required wattage, but also the *voltage*. Some resistors have a voltage limitation which makes it impossible to force sufficient current through them to result in rated wattage dissipation. This type of resistor usually is provided with slider taps, and is designed for voltage divider service. An untapped, non-adjustable resistor is preferable as a high voltage bleeder, and is less expensive. Several small resistors may be connected in series, if desired, to obtain the required wattage and voltage rating.

Transformers Power transformers and filament transformers normally will give no trouble over a period of many years if purchased from a reputable manufacturer, and if given a reasonable amount of care. Transformers must be kept dry; even a small amount of moisture in a high-voltage unit will cause quick failure. A transformer which is operated continuously, within its ratings, seldom will give trouble from moisture, since an economically designed transformer operates at a moderate temperature rise above the temperature of the surrounding air. But an unsealed transformer which is inactive for an appreciable period of time in a highly humid location can absorb enough moisture to cause early failure.

Filter Choke Coils Filter inductors consist of a coil of wire wound on a laminated iron core. The size of wire is determined by the amount of direct current which is to flow through the choke coil. This direct current magnetizes the core and reduces the inductance of the choke coil; therefore, filter choke coils of the "smoothing" type are built with an air gap of a small fraction of an inch in the iron core, for the purpose of preventing saturation when maximum d.c. flows through the coil winding. The "air gap" is usually in the form of a piece of fiber inserted between the ends of the laminations. The air gap reduces the initial inductance of the choke coil, but keeps it at a higher value under maximum load conditions. The coil must have a great many more turns for the same initial inductance when an air gap is used.

The d-c resistance of any filter choke should be as low as practicable for a specified value of inductance. Smaller filter chokes, such as those used in radio receivers, usually have an inductance of from 6 to 15 henrys, and a d-c resistance of from 200 to 400 ohms. A high d-c resistance will reduce the output voltage, due to the voltage drop across each choke coil. Large filter choke coils for radio transmitters and Class B amplifiers usually have less than 100 ohms d-c resistance.

29-6 Transformer Design

The most important factor in determining the capability of any transformer is the amount of core material. The electrical rating, as well as the physical size, is determined almost entirely by the size of the core. The type of core material is also important. The present practice is to use high-grade silicon-steel sheet.

It will be assumed that this type of material is to be employed in all construction herein described. Soft sheet-iron or stovepipe iron is sometimes substituted, but transformers made from such materials will have about 50 to 60 per cent of the power rating, pound for pound of core, as those made from silicon-steel.

The Core The core size determines the performance of a transformer because the entire energy circulating in the transformer (except small amounts of energy dissipated in resistance losses in the primary) must be transformed from electrical energy in the primary winding to magnetic energy in the core, and reconverted into electrical energy in the secondary. The amount of core material determines quite definitely the power that any transformer will handle.

Transformer cores are often designed so that if the losses per cubic inch of core material are determined, these losses can be used as a basis for calculating the rating of the transformer. These losses exist in watts, and are divided between the eddy current loss and the hysteresis loss. The eddy current loss is the loss due to the lines of force moving across the core, just as if it were a conductor, and setting up currents in it.

Induced currents of this type are very undesirable and they are merely wasted in heating the core, which then tends to heat the windings, increase the resistance of the coils, and reduce the overall power handling ability of the transformer. To reduce such losses, transformer cores are made of thin sheets. These sheets are insulated from each other by a coat of thin varnish, shellac or japan, or by the iron-oxide scale which forms on the sheets during the manufacturing process and which acts as a good insulator between sheets.

Hysteresis The magnetic flux in the core lags behind the magnetizing force that produces it, which is, of course, the primary supply. Because all transformers operate on alternating current, the core is subjected to continuous magnetizing and demagnetizing force, due to alternating effect of the a-c field. This *hysteresis* (meaning "to lag") heats the iron, due to molecular friction caused by the iron molecules re-orienting themselves as the direction of the magnetizing flux changes.

Saturation The higher the field strength, the greater the heat produced. A condition can be reached where a further increase in magnetizing force does not produce a corresponding increase in the flux density. This is called *saturation*, and is a condition which will cause considerable heat in a core. In the normal transformer, all core material must be operated with the magnetic flux well below saturation.

Core Losses All core losses manifest themselves as heat, and these losses are the determining factor in transformer rating. They are spoken of as *total core loss*, generally used as a single figure, and for common use a core loss of from 0.75 watt to 2.5 watts per pound of core material can be assumed for 60 cycles. The lower figure is for the better grades of thin sheet, while the higher loss is for heavier grades.

About 1 watt per pound is a very satisfactory rating for common grades of material. This rating is also dependent on the manner in which the transformer is built and mounted, and on the ease with which the heat is radiated or conducted from the core. Transformers with higher losses may be used for intermittent service.

The transformer core loss can be assumed to be from 5 to 10 per cent of the total rating for small transformers. Thus, if the core loss is known, the rating of the transformer can be easily determined. If 1 watt per pound is assumed, the problem is further simplified. To determine the rating of the transformer, weigh the core. If, for example, the core weighs 10 pounds, the transformer will handle from 100 to 200 watts. Such a transformer core can be assumed to have about 150 watts nominal rating.

If the weighing of the core is inconvenient, the weight can be calculated from the cubic content or volume. Silicon-steel core laminations weigh approximately one-fourth pound per cubic inch.

The usual commercially manufactured transformer uses the shell-type core, as illustrated on the left in figure 12. Home constructed transformers often use the core-type core, as illustrated to the right in figure 12. Also, most of the newer light-weight high-efficiency transformers used in aircraft make use of the "Hypersil" type of wound core illustrated in figure 13. This latter type of core is made by winding a thin strip of *grain-oriented silicon steel* around a mandrel until the desired size is obtained, and then sawing the built-up core in half for mounting of the windings.

Both core-type and shell-type cores are assembled from strips. The shell type normally is assembled from "E" and "I" pieces, although it may be assembled from strips in the same manner as the core type. For the shell-type core, the area is taken as the square section of the center leg, (2¼ by 4¼ inches in the example shown in figure 12) and in the core-type the area taken as the section of one leg. The actual area of both cores shown in figure 12 is

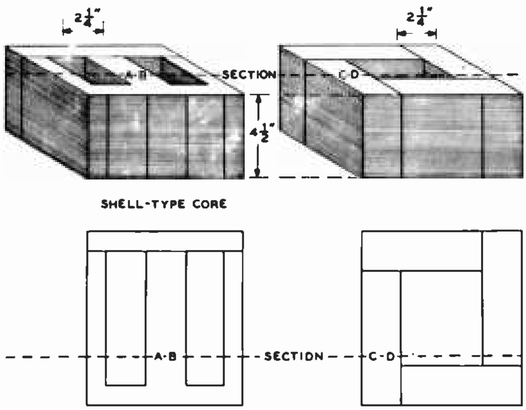


Figure 12

TYPES OF TRANSFORMER CORES

The shell-type core is shown on the left. The "E" and "I" pieces are stacked from alternate sides for a transformer which has no net d.c. in the windings. For a choke or a transformer which will have a substantial d-c winding current, the "E" and "I" pieces are stacked in the same direction so that an air gap may be inserted between the "E" assembly and the "I" stack. The seldom used core-type core is shown on the right.

10.1 square inches, which is large enough for a comparatively large transformer.

Turns Per Volt To determine the number of turns for a given voltage, apply the following formula.

$$E = \frac{4.44\,N\,B\,A\,T}{10^8}$$

Where E equals the voltage of the circuit; N, the frequency in cycles of the circuit; B, the number of magnetic lines per square inch of the magnetic circuit; A, the number of square inches of the magnetic circuit; and T, the number of turns.

The proper value for B, for small transformers and for ordinary grades of sheet-iron, such as are now being considered, is 75,000 for 25 cycles and 50,000 for 50 or 60 cycles.

Rewriting the above formula

$$T = \frac{E \times 10^8}{4.44\,N\,B\,A}$$

and since N and B are known

$$T = \frac{10^8}{4.44 \times 60 \times 50{,}000} \times \frac{E}{A}$$

from which

$$T = 7.5 \times \frac{E}{A}$$

That is, for a transformer to be used on a 60-cycle circuit, the proper number of turns for the primary coil is obtained by multiplying the line voltage by 7.5 and dividing this product by the number of square inches cross section of the magnetic circuit.

On a 25-cycle circuit, the 7.5 becomes 12, and on 50 cycles it becomes 9.

Copper Loss It should be kept in mind that there is a *copper or resistance loss* in all transformers. This is caused by the passage of the current through the windings, and is commonly spoken of as the "I^2R" loss. It manifests itself directly as heat and varies as the load is varied; the heavier the load, the more heat is developed.

This heat, as well as other heat losses, must be removed, or the transformer will overheat. Most transformers are arranged so that both the core and windings can radiate heat into the surrounding air and thus cool themselves. Large transformers are mounted in oil for cooling, and also for the purpose of increasing the insulation factor.

Turns Ratio In any transformer, the voltage ratio is directly proportional to the turns ratio. This means that if the transformer is to have 110-volts input and 250 turns for the primary, and if the output is to be 1,100 volts, 2,500 turns will be needed. This may be expressed:

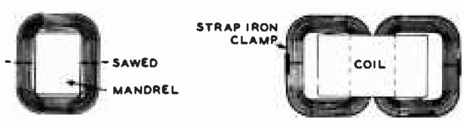


Figure 13

SHOWING USE OF THE "HYPERSIL" TYPE OF CORE

$$\frac{E_p}{E_s} = \frac{T_p}{T_s}$$

It is often more convenient to take the figure obtained for the primary winding and, by dividing by the supply voltage, the number of turns per volt is calculated. This accomplished, the number of turns for any given voltage can be calculated by simple multiplication.

Radio transformers are generally of small size. The matter of power factor can therefore be disregarded, more especially because they work into a substantially resistive load. In the design of radio transformers, the power factor can be safely assumed as unity, in which case the apparent watts and the actual watts are the same. Admittedly, this is not always a correct assumption, but it will suffice for common applications.

The size of the wire to be used in any transformer depends upon the amperage to be carried. For a continuous load, at least 1,000 circular mils per ampere must be allowed. For transformers which have poor ventilation, or continuous heavy load service, or where price is not the first consideration, 1,500 circular mils per ampere is a preferable figure.

Insulation Allowance should always be made for the insulation and size of the windings. Good insulation should be provided between the core and the windings and also between each winding and between turns. Numerous materials are satisfactory for this purpose; varnished paper or cloth, called empire, is satisfactory, although costly. Good bond paper will serve well as an insulating medium for small transformer windings.

Insulation between primary and secondary and to the core must be exceptionally good, as well as the insulation between windings. Thin mica or micanite sheet is very good. Thin fibre, commonly called fish paper, is also a good insulator; bristol board, or strong, thin cardboard may also be used. In all cases, the completed coil should be impregnated with insulating varnish (preferably in a vacuum), and either dried in air or baked in an oven. Common varnishes or shellac are unsatisfactory on account of the moisture content of these materials. Air-drying insulating varnish is practical for all-around purposes; baking varnish may be substituted, but the fumes given off are inflammable and often explosive. Care must be exercised in the handling of this type of material. Collodion and banana oil lacquer are quite dangerous; in the event of a short circuit or transformer burn-out, a serious fire may result.

Construction of Filter Chokes A choke is assembled on a silicon-steel core similar to a transformer core, but is wound with only a single winding. The size of the core and the number of turns of wire, together with the air gap which must be provided to prevent the core from saturating, are factors which determine the inductance of a choke. The relative sizes of the core and coil determine the amount of d-c which can flow through the choke without reducing the inductance to an undesirable low value due to magnetization.

The same core material which is used in ordinary radio power transformers, or from those which are burned out, is satisfactory for all general purposes.

In construction, the choke winding must be insulated from the core with a sufficient quantity of insulating material so that the highest peak voltages which are to be experienced in service will not rupture the insulation.

29-7 Special Power Supplies

A complete transmitter usually includes one or more power supplies such as grid-bias packs, voltage-regulated supplies, or transformerless supplies having some special characteristic.

Regulated Supplies—V-R Tubes Where it is desired in a circuit to stabilize the voltage supply to a load requiring not more than perhaps 20 to 25 ma., the glow-discharge type of voltage-regulator tube can be used to great advantage. Examples of such circuits are the local oscillator circuit in a receiver, the tuned oscillator in a v-f-o, the oscillator in a frequency meter, or the bridge circuit in a vacuum-tube voltmeter. A number of tubes are available for this application including the OA3/VR75, OB3/VR90, OC3/VR105, OD3/VR150, and the OA2 and OB2 miniature types. These tubes stabilize the voltage across their terminals to 75, 90, 105, or 150 volts. The miniature types OA2 stabilize to 150 volts and OB2 to 108 volts. The types OA2, OB2, and OB3/VR90 have a maximum current rating of 30 ma. and the other three types have a maximum current rating of 40 ma. The minimum current required by all six types to sustain a constant discharge is 5 ma.

A VR tube (common term applied to all glow-discharge voltage regulator tubes) may be used to stabilize the voltage across a variable load or the voltage across a constant load fed from a varying voltage. Two or more VR tubes may be connected in series to provide exactly 180, 210, 255 volts or other combinations of the voltage ratings of the tubes. It is not recommended, however, that VR tubes be connected in parallel since both the striking and the regulated voltage of the paralleled tubes normally will be sufficiently different so that only one of the tubes will light. The remarks following apply generally to all the VR types although some examples apply specifically to the OD3/VR150 type.

A device requiring say, only 50 volts can be stabilized against *supply voltage* variations by means of a VR-105 simply by putting a suitable resistor in series with the regulated voltage and the load, dropping the voltage from 105 to 50 volts. However, it should be borne in mind that under these conditions the device will *not* be regulated for *varying load;* in other words, if the *load resistance* varies, the voltage across the load will vary, even though the regulated voltage remains at 105 volts.

To maintain constant voltage across a *varying load resistance* there must be *no* series resistance between the regulator tube and the load. This means that the device must be operated exactly at one of the voltages obtainable by seriesing two or more similar or different VR tubes.

A VR-150 may be considered as a stubborn variable resistor having a range of from 30,000 to 5000 ohms and so intent upon maintaining a fixed voltage of 150 volts across its terminals that when connected across a voltage source having *very poor regulation* it will instantly vary its own resistance within the limits of 5000 and 30,000 ohms in an attempt to maintain the same 150 volt drop across its terminals when the supply voltage is varied. The theory upon which a VR tube operates is covered under the subject of gaseous conduction in Chapter Six and will not be discussed here.

It is paradoxical that in order to do a good job of regulating, the regulator tube must be fed from a voltage source having poor regulation (high series resistance). The reason for this presently will become apparent.

If a high resistance is connected across the VR tube, it will not impair its ability to maintain a fixed voltage drop. However, if the load is made too low, a variable 5000 to 30,000 ohm shunt resistance (the VR-150) will not exert sufficient effect upon the resulting resistance to provide constant voltage except over a *very limited* change in supply voltage or load resistance. The tube will supply maximum regulation, or regulate the largest load, when the source of supply voltage has high internal or high series resistance, because a variation in the effective internal resistance of the VR tube will then have more controlling effect upon the load shunted across it.

In order to provide greatest range of regulation, a VR tube (or two in series) should be used with a series resistor (to effect a poorly regulated voltage source) of such a value that it will permit the VR tube to draw from 8 to 20 ma. under normal or average conditions of supply voltage and load impedance. For maximum control range, the series resistance should be not less than approximately 20,000 ohms, which will necessitate a source of voltage considerably in excess of 150 volts. However, where the supply voltage is limited, good control over a *limited range* can be obtained with as little as 3000 ohms series resistance. If it takes less than 3000 ohms series resistance to make the VR tube draw 15 to 20 ma. when the VR tube is connected to the load, then the supply voltage is not high enough for proper operation.

Should the current through a VR-150, VR-105, or VR-75 be allowed to exceed 40 ma., the life of the tube will be shortened. If the current falls below 5 ma., operation will become unstable. Therefore, the tube must operate within this range, and within the two extremes will maintain the voltage within 1.5 per cent. It takes a voltage excess of at least 10 to 15 per cent to "start" a VR type regulator; and to insure positive starting each time the voltage supply should preferably exceed the regulated output voltage rating about 20 per cent or more. This usually is automatically taken care of by the fact that if sufficient series resistance for good regulation is employed, the voltage impressed across the VR tube before the VR tube ionizes and starts passing current is quite a bit higher than the starting voltage of the tube.

When a VR tube is to be used to regulate the voltage applied to a circuit drawing *less than 15 ma.* normal or average current, the simplest method of adjusting the series resistance is to remove the load and vary the series resistor until the VR tube draws about 30 ma. Then connect the load, and that is all there is to it. This method is particularly recommended when the load is a heater type vacuum tube, which may not draw current for several seconds after the power supply is turned on. Under these conditions, the current through the VR tube will never exceed 40 ma. even when it is running unloaded (while the heater tube is warming up and the power supply rectifier has already reached operating temperature).

Figure 14 illustrates the standard glow discharge regulator tube circuit. The tube will maintain the voltage across R_L constant to

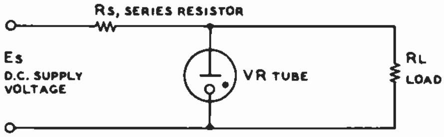


Figure 14
STANDARD VR-TUBE REGULATOR CIRCUIT

The VR-tube regulator will maintain the voltage across its terminals constant within a few volts for moderate variations in R_L or E_S. See text for discussion of the use of VR tubes in various circuit applications.

within 1 or 2 volts for moderate variations in R_L or E_S.

Voltage Regulated Power Supplies When it is desired to stabilize the potential across a circuit drawing more than a few milliamperes it is advisable to use a voltage-regulated power supply of the type illustrated in figure 15 rather than glow discharge tubes.

A 6AS7-G is employed as the series control element, and type 816 mercury vapor rectifiers are used in the power supply section. The 6AS7-G acts as a variable series resistance which is controlled by a separate regulator tube much in the manner of a-v-c circuits or inverse feedback as used in receivers and a-f amplifiers. A 6SH7 controls the operating bias on the 6AS7-G, and therefore controls the internal resistance of the 6AS7-G. This, in turn, controls the output voltage of the supply, which controls the plate current of the 6SH7, thus completing the cycle of regulation. It is apparent that under these conditions any change in the output voltage will tend to "resist itself," much as the a-v-c system of a receiver resists any change in signal strength delivered to the detector.

Because it is necessary that there always be a moderate voltage drop through the 6AS7-G in order for it to have proper control, the rest of the power supply is designed to deliver as much output voltage as possible. This calls for a low resistance full-wave rectifier, a high capacitance output capacitor in the filter system and a low resistance choke.

Reference voltage in the power supply is obtained from a VR-150 gaseous regulator. Note that the 6.3-volt heater winding for the 6SH7 and the 6AS7-G tubes is operated at a potential of plus 150 volts by connecting the winding to the plate of the VR-150. This procedure causes the heater-cathode voltage of the 6SH7 to be

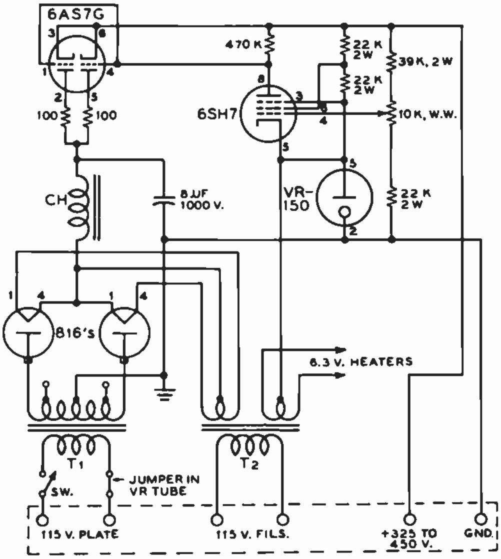


Figure 15
SCHEMATIC OF THE VOLTAGE-REGULATED POWER SUPPLY

CH—10-hy. 250 ma. choke (Merit C-3182)
T_1—660 or 550 v. each side, 250 ma. (Merit P-3157)
T_2—5 v. 3 a., 6.3 v. 3.6 a. (Merit P-3041)

zero, and permits an output voltage of up to 450 since the 300-volt heater-to-cathode rating of the 6AS7-G is not exceeded with an output voltage of 450 from the power supply.

The 6SH7 tube was used in place of the more standard 6SJ7 after it was found that the regulation of the power supply could be improved by a factor of two with the 6SH7 in place of the 6SJ7. The original version of the power supply used a 5R4-GY rectifier tube in place of the 816's which now are used. The excessive drop of the 5R4-GY resulted in loss of control by the regulator portion with an output voltage of about 390 with a 225-ma. drain. Satisfactory regulation can be obtained, however, at up to 450 volts if the maximum current drain is limited to 150 ma. when using a 5R4-GY rectifier. If the power transformer is used with the taps giving 550 volts each side of center, and if the maximum drain is limited to 225 ma., a type 83 rectifier may be used as the power supply rectifier. The 660-volt taps on the power transformer deliver a voltage in excess of the maximum ratings of the 83 tube. With the 83 in the power supply, excellent regulation may be obtained with up to about 420 volts output if the output current is limited to 225 ma. But with the 816's as rectifiers the full capabilities of all the components in the power supply may be utilized.

If the power supply is to be used with an output voltage of 400 to 450 volts, the full 660 volts each side of center should be applied to the 816's. However, the maximum plate dissipation rating of the 6AS7-G will be exceeded, due to the voltage drop across the tube, if the full current rating of 250 ma. is used with an output voltage below 400 volts. If the power supply is to be used with full output current at voltages below 400 volts the 550-volt taps on the plate transformer should be connected to the 816's. Some variation in the output range of the power supply may be obtained by varying the values of the resistors and the potentiometer across the output. However, be sure that the total plate dissipation rating of 26 watts on the 6AS7-G series regulator is not exceeded at maximum current output from the supply. The total dissipation in the 6AS7-G is equal to the current through it (output current plus the current passing through the two bleeder strings) multiplied by the drop through the tube (voltage across the filter capacitor minus the output voltage of the supply).

Auxiliary Grid-Bias Power Supplies In the construction of a transmitter, an exciter, or other items of station equipment the operating conditions of one of the stages often require a low-current source of negative potential at from perhaps 50 to 300 volts. In many cases this value of voltage may be obtained without the installation of another transformer through the use of the circuit arrangement of figure 16. In this circuit the 6X5-GT has its heater lighted from the 6.3-volt winding on the power transformer, and due to the heater-cathode rating of 450 volts the cathode may be connected to one side of the secondary of the high-voltage winding. If a negative-voltage output approximately equal to the voltage output of the positive supply is required, the cathode may be connected directly to one side of the secondary. If a lower value of output voltage is required of the negative supply, a resistor of 1000 to 10,000 ohms (10-watt rating) may be connected in series with the lead from the secondary winding to the cathode of the 6X5-GT. The 6X5-GT tube requires 0.6 ampere of heater current at 6.3 volts.

Bias Pack Considerations It should be borne in mind that when a conventional power supply is used "inverted" in order to provide bias to a stage drawing grid current, the grid current flows in the *same direction as the bleeder current.* This means that the grid current does not flow through the power pack as when a pack is used to supply the plate voltage, but rather through the bleeder.

Bear in mind that the bleeder always acts as a grid leak when grid current is flowing, and while the effect can be minimized by making the resistance quite low, all grid current *must flow through the bleeder,* as it cannot flow back through the bias pack.

Class C amplifiers, both c-w and plate modulated, require high grid current and considerably more than cutoff bias, the bias sometimes being as high as 4 or 5 times cutoff. To protect the tubes against excitation failure, it is desirable that fixed bias sufficient to limit the plate current to a safe value be used. This is normally the amount of bias that would be used on the same tubes at the same plate voltage in a Class B modulator. It is best practice to obtain only this amount of bias from a bias pack, the additional required amount being obtained from a variable grid leak which is adjusted for correct bias and grid current while the stage is running under normal conditions.

This condition is such that the voltage divider tap on the bias pack will be delivering only a portion of the full bias pack voltage when the biased stage is inoperative. Then, when grid current flows to the biased stage, there is no danger of the voltage rising to dangerously high values across the filter capacitors in the bias pack.

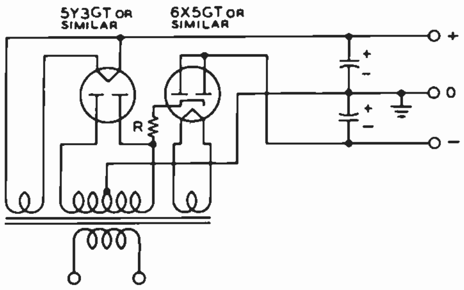
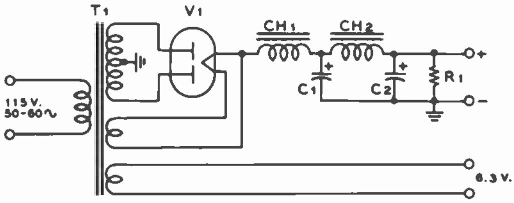


Figure 16

AUXILIARY BIAS SUPPLY OPERATING FROM THE POWER TRANSFORMER

This arrangement may be used to deliver a negative voltage up to the magnitude of the positive voltage output of the supply, but at a much lower current drain. The value of the negative voltage may be varied by changing the value of resistor R.



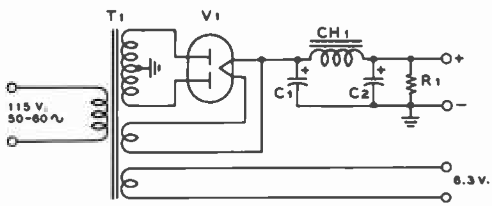
COMPONENTS							APPROXIMATE OUTPUT VOLTAGE		MAX. CURRENT	6.3 V. FILAMENT
T_1	V_1	CH_1	CH_2	C_1	C_2	R_1	NO LOAD	FULL LOAD		
350-0-350 *STANCOR PC-8409* *MERIT P-3152*	5Y3-GT	10 H. *STANCOR C-1001* *MERIT C-2995*	10 H. *STANCOR C-1001* *MERIT C-2993*	10 μF, 450 V. *CORNELL-DUBILIER BR-1045*	20 μF, 450 V. *CORNELL-DUBILIER BR-2045*	35 K, 10 W	310	240	80 MA.	3 A.
375-0-375 *STANCOR PC-8411* *MERIT P-2954*	5Y3-GT	3-13 H *STANCOR C-1718* *MERIT C-3187*	7 H. *STANCOR C-1421* *MERIT C-3180*	10 μF, 450 V. *CORNELL-DUBILIER BR-1045*	20 μF, 450 V. *CORNELL-DUBILIER BR-2045*	35 K, 10 W	330	230	140 MA.	4.5 A.
400-0-400 *STANCOR PC-8413*	5U4-G	2-12 H. *STANCOR C-1402* *MERIT C-3189*	4 H. *STANCOR C-1412* *MERIT C-3182*	10 μF 450 V. *CORNELL-DUBILIER BR-1045*	10 μF, 450 V. *CORNELL-DUBILIER BR-1045*	35 K, 10 W	380	270	250 MA.	5 A.
525-0-525 *UTC S-40*	5U4-GB	5-25 H. *UTC S-32*	20 H. *UTC S-31*	10 μF, 600 V. *MALLORY TC-92*	10 μF, 600 V. *MALLORY TC-92*	35 K, 10 W	460	375	240 MA.	4 A.
600-0-600 *UTC S-41*	5R4-GY	5-25 H. *UTC S-32*	20 H. *UTC S-31*	8 μF, 600 V. *SPRAGUE CR-86*	8 μF, 600 V. *SPRAGUE CR-86*	35 K, 25 W	540	410	200 MA.	4 A.
900-0-900 *UTC S-45*	5R4-GY	5-25 H. *UTC S-32*	20 H. *UTC S-31*	4 μF, 1 KV. *SPRAGUE CR-41*	8 μF, 1 KV. *SPRAGUE CR-81*	50 K, 25 W	830	650	175 MA.	—

Figure 17

DESIGN CHART FOR CHOKE-INPUT POWER SUPPLIES

Figure 18

DESIGN CHART FOR CAPACITOR-INPUT POWER SUPPLIES



COMPONENTS						APPROXIMATE OUTPUT VOLTAGE		MAX. CURRENT	6.3 V. FILAMENT
T_1	V_1	CH_1	C_1	C_2	R_1	NO LOAD	FULL LOAD		
260-0-260 *STANCOR PC-8404* *MERIT P-3148*	5Y3-GT	10 H. *STANCOR C-1001* *MERIT C-2993*	20 μF, 450 V. *CORNELL-DUBILIER BR-2045*	20 μF, 450 V. *CORNELL-DUBILIER BR-2045*	35 K, 10 W	340	240	80 MA.	3 A.
375-0-375 *STANCOR PC-8411* *MERIT P-2954*	5Y3-GT	7 H. *STANCOR C-1421* *MERIT C-3180*	10 μF, 600 V. *MALLORY TC-92*	10 μF, 600 V. *MALLORY TC-92*	35 K, 10 W	480	350	125 MA.	4.5 A.
435-0-435 *MERIT P-3156*	5U4-G	4 H. *STANCOR C-1412* *MERIT C-3182*	8 μF, 600 V. *SPRAGUE CR-86*	8 μF, 600 V. *SPRAGUE CR-86*	35 K, 25 W	600	400	225 MA.	6 A.
600-0-600 *STANCOR PC-8414*	5R4-GY	4 H. *STANCOR C-1412* *MERIT C-3182*	4 μF, 1 KV. *SPRAGUE CR-41*	8 μF, 1 KV. *SPRAGUE CR-81*	50 K, 25 W	800	600	200 MA.	6 A.
900-0-900 *UTC S-45*	5R4-GY	20 H. *UTC S-31*	4 μF, 1.5 KV. *SPRAGUE CR-415*	8 μF, 1.5 KV. *SPRAGUE CR-815*	75 K 25 W	1200	910	150 MA.	—

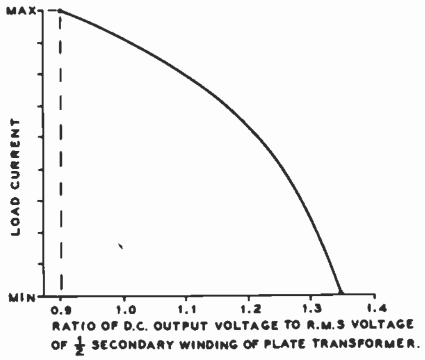


Figure 19

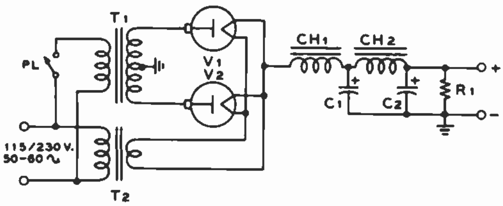
APPROXIMATE REGULATION OF CAPACITOR-INPUT FILTER SYSTEM

29-8 Power Supply Design

Power supplies may either be of the choke input type illustrated in figure 17, or the capacitor input type, illustrated in figure 18. Capacitor input filter systems are characterized by a d-c supply output voltage that runs from 0.9 to about 1.3 times the r.m.s. voltage of one-half of the high voltage secondary winding of the transformer. The approximate regulation of a capacitor input filter system is shown in figure 19. Capacitor input filter systems are not recommended for use with mercury vapor rectifier tubes, as the peak rectifier current may run as high as five or six times the d-c load current of the power supply. It is possible, however, to employ type 872-A mercury vapor rectifier tubes in capacitor input circuits wherein the load current is less than 600 milliamperes or so, and where a low resistance bleeder is used to hold the minimum current drain of the supply to a value greater than 50 milliamperes or so. Under these conditions the peak plate current of the 872-A mercury vapor tubes will not be exceeded if the input filter capacitor is 4 μfd. or less.

Choke input filter systems are characterized by lower peak load currents (1.1 to 1.3 times the average load current) than the capacitor input filter, and by better voltage regulation. Design Charts for capacitor and choke input filter supplies for various voltages and load currents are shown in figures 17, 18, and 20.

The construction of power supplies for transmitters, receivers and accessory equipment is a relatively simple matter electrically since lead lengths and placement of parts are of minor importance and since the circuits themselves are quite simple. Physical layouts for several power supplies of different power capabilities are shown in figures 21, 22 and 33.



COMPONENTS								APPROXIMATE OUTPUT VOLTAGE		MAX. CURRENT (ICAS)
T1	T2	V1-V2	CH1	CH2	C1	C2	R1	NO LOAD	FULL LOAD	
1150-0-1150 CHICAGO TRANS. P-107	2.5 V., 10 A. CHI. TRAN. F-210	866-A 866-A	6 H. CHI. TRAN. R-63	10 H. CHI. TRAN. R-103	4 UF, 1.5 KV. SANGAMO 7115-4	8 UF, 1.5 KV. SANGAMO 7115-8	40K, 75 W	1150	1000	350 MA.
1710-0-1710 CHICAGO TRANS. P-1512	2.5 V., 10 A. CHI. TRAN. F-210H	866-A 866-A	6 H. CHI. TRAN. R-65	10 H. CHI. TRAN. R-105	4 UF, 2 KV. SANGAMO 7120-4	8 UF, 2 KV. SANGAMO 7120-8	50 K, 75 W	1700	1500	425 MA.
2900-0-2900 CHICAGO TRANS. P-2126	5 V., 10 A. CHI. TRAN. F-510H	872-A 872-A	6 H. CHI. TRAN. R-67	6 H. CHI. TRAN. R-67	4 UF, 3 KV. SANGAMO 7130-4	4 UF, 3 KV. SANGAMO 7130-4	75 K 200 W	2750	2500	700 MA.
3500-0-3500 UTC CG-309	5 V., 10 A. UTC LS-82	872-A 872-A	10 H. UTC CG-15	10 H. UTC CG-15	4 UF, 4 KV. CORNELL-DUBILIER T40040-A	4 UF, 4 KV. CORNELL-DUBILIER T40040-A	100 K 200 W	3400	3000	1000 MA
4600-0-4600 UTC CG-310 CHICAGO TRANS. P-4353	5 V., 20 A. UTC LS-83	575-A 575-A	10 H. UTC CG-15	10 H. UTC CG-15	4 UF, 5 KV. AEROVOX JP-09	4 UF, 5 KV. AEROVOX JP-09	100 K 300 W	4400	4000	800 MA.

Figure 20

DESIGN CHART FOR CHOKE-INPUT HIGH VOLTAGE SUPPLIES

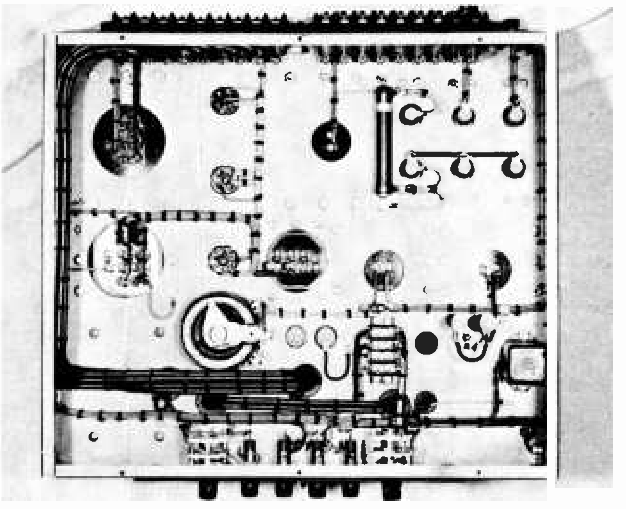


Figure 21
UNDER-CHASSIS POWER SUPPLY ASSEMBLY

All components are firmly mounted to the steel chassis and all wiring is cabled. High voltage leads are run in automobile ignition cables. Heavy-duty terminal strips are mounted along the rear edge of the chassis. The control panel of this supply is shown in figure 1 of this chapter.

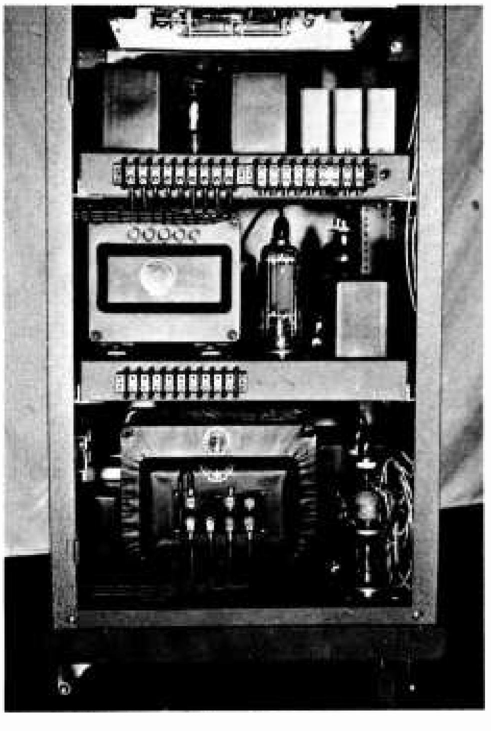
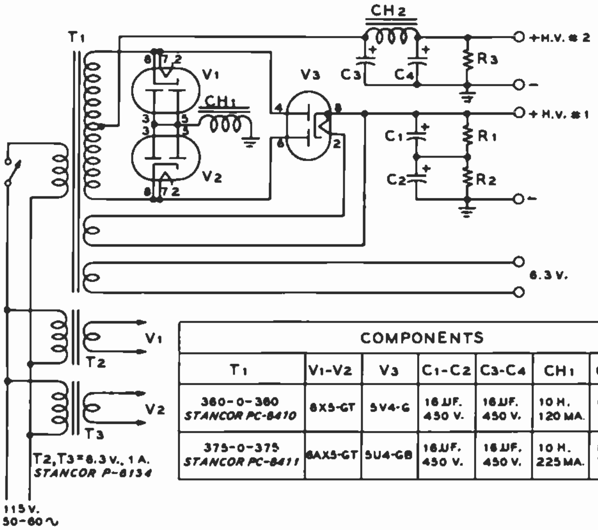


Figure 22
POWER SUPPLY — MODULATOR RACK INSTALLATION

The heavy-duty components of a high-power transmitter are mounted on steel chassis in a standard 19 inch relay rack cabinet. On the bottom shelf are the 4000-volt plate transformer, the 575-A rectifier tubes, filament transformer and associated filter chokes and capacitors. The next higher shelf has the push-pull 810 modulator stage, including modulation transformer and high-level audio clipper. Above this is the push-pull 6A3 speech amplifier, incorporating low level speech clipping and filtering. Each deck is supported on angle-stock bolted to the sides of the rack, taking the weight of the deck off the front panel, and allowing easy insertion and removal of the decks from the rack-cabinet.



COMPONENTS									FULL LOAD VOLT.		MAX. CURRENT	
T1	V1-V2	V3	C1-C2	C3-C4	CH1	CH2	R1-R2	R3	HV#1	HV#2	#1	#2
360-0-360 *STANCOR PC-8410*	6X5-GT	5V4-G	16 µF. 450 V.	16 µF. 450 V.	10 H. 120 MA.	6 H. 50 MA.	20K,10W.	100 K 1 W	600	240	100 MA.	40 MA.
375-0-375 *STANCOR PC-8411*	6AX5-GT	5U4-GB	16 µF. 450 V.	16 µF. 450 V.	10 H. 225 MA.	8 H. 75 MA.	20K 10W.	100 K 1 W	625	280	200 MA.	50 MA.

Figure 23
DUAL VOLTAGE BRIDGE POWER SUPPLIES

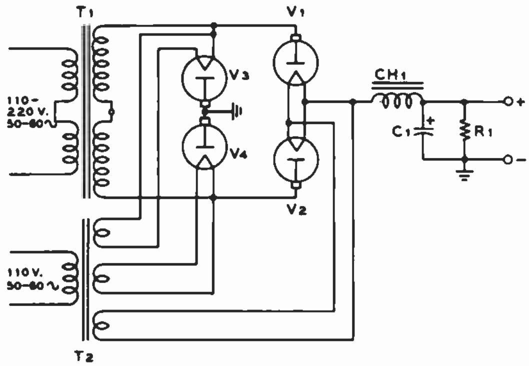
Bridge Supplies Some practical variations of the common bridge rectifier circuit of figure 5 are illustrated in figures 23 and 24. In many instances a transmitter or modulator requires two different supply voltages, differing by a ratio of about 2:1. A simple bridge supply such as shown in figure 23 will provide both of these voltages from a simple broadcast "replacement-type" power transformer. The first supply of figure 23 is ample to power a transmitter of the 6CL6-807 type to an input of 60 watts. The second supply will run a transmitter running up to 120 watts, such as one employing a pair of 6146 tetrodes in the power amplifier stage. It is to be noted that separate filament transformers are used for rectifier tubes V_1 and V_2, and that one leg of each filament is connected to the cathode of the respective tube, which is at a high potential with respect to ground. The choke CH_1 in the negative lead of the supply serves as a common filter choke for both output voltages. Each portion of the supply may be considered as having a choke input filter system. Filaments of V_1 and V_2 should be energized before the primary voltage is applied to T_1.

Bridge supplies may also be used to advantage to obtain relatively high plate voltages for high powered transmitting equipment. Type 866-A and 872-A rectifier tubes can only serve in a supply delivering under 3500 volts in a full-wave circuit. Above this voltage, the peak inverse voltage rating of the rectifier tube will be exceeded, and danger of flash-back within the rectifier tube will be present. However, with bridge circuits, the same tubes may deliver up to as much as 7000 volts d.c. without exceeding the peak inverse voltage rating.

The bridge circuit also permits the use of the so-called "pole transformer" in high voltage power supplies. Two KVA transformers of this type having a 110/220 volt secondary winding and a split 2200 volt primary winding may often be picked up in salvage yards for a dollar or two. If reversed, and either 110 or 220 volts applied to the "primary" winding approximately 2200 volts r.m.s. will be developed across the new "secondary" winding. If used in a bridge circuit as shown in figure 24, a d-c supply voltage of about 1900 volts at a current of 500 milliamperes may be drawn from such a transformer. Do not attempt to use a smaller transformer than the 2-KVA rating, as the voltage regulation of the unit will be too poor for practical purposes.

For higher voltages, a pole transformer with a 4400 volt primary and a 110/220 volt secondary may be reversed to provide a d-c plate supply of about 3800 volts.

Commercial plate transformers intended for full wave rectifier service may also be used in bridge service *provided* that the insulation at the center-tap point of the high voltage winding is sufficient to withstand one-half of



COMPONENTS						FULL LOAD VOLTAGE	FULL LOAD CURRENT (ICAS)
T1	T2	V1-V4	CH1	C1	R1		
2200-VOLT "POLE TRANSFORMER" 2 KVA	*UTC S-71*	866-A	20 H. 500 MA. *UTC S-37*	10 µF. 2500 V.	75 K. 200 W.	1900	500 MA.
3500-0-3500 *UTC CG-308*	*UTC LS-121-Y*	872-A	10 H. 500 MA. *UTC CG-108*	8 µF 6600 V.	200 K 300 W.	6000	500 MA.

Figure 24
HIGH VOLTAGE POWER SUPPLY

the r.m.s. voltage of the secondary winding. Many high voltage transformers are specifically designed for operation with the center-tap of the secondary winding at ground potential; consequently the insulation of the winding at this point is not designed to withstand high voltage. It is best to check with the manufacturer of the transformer and find out if the insulation will withstand the increased voltage before a full wave-type transformer is utilized in bridge rectifier service.

29-9 Power Supply Construction

The construction of power supplies for transmitters, receivers, and accessory equipments is a relatively simple matter electrically since lead lengths are of minor importance and since the circuits themselves are quite simple. There are two factors which do complicate power supply construction, both essentially mechanical problems; these are the problem of mounting the massive and heavy components, and the problem of maintaining adequate voltage insulation in the leads.

An abundance of power supply circuits has been described in the earlier sections of this chapter, and the construction details on a few power supplies of differing degrees of complexity will be shown to illustrate the conventional manner of construction of such units.

29-10 Low-Drain Power Supply

There are many applications in the laboratory and amateur station for a simple low-drain power supply. The most common application in the amateur station for such a supply is for items of test equipment such as the LM and BC-221 frequency meters, for frequency converters to be operated in conjunction with the station receiver, and for high-selectivity i-f channels such as the BC-453A. Items of equipment such as these may be operated from a plate supply delivering 200 to 250 volts at up to 50 ma. of plate current. Heater supply either is already 6.3 or 12.6 volts, or the heaters in the equipment may be rewired to either of these voltages with relatively little difficulty.

The simple supply illustrated in figures 25 and 26 is capable of meeting the requirements discussed in the paragraph above. Figure 25 shows the schematic diagram of the supply, with the 5-volt and 6.3-volt windings con-

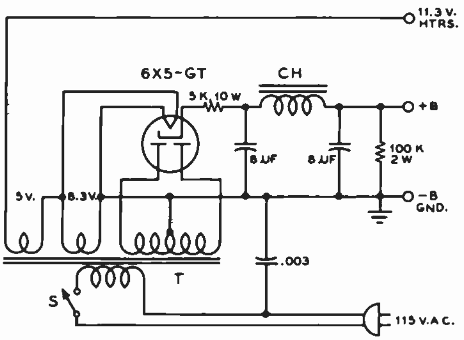


Figure 25

SCHEMATIC OF THE LOW-DRAIN POWER SUPPLY

The supply is shown connected for supplying heater voltage to a 12.6-volt heater string. For use with a 6.3-volt heater string the lead to the external heaters should be connected to the ungrounded side of the heater for the 6X5-GT rectifier tube. CH—16-hy. 50 ma. choke (Stancor C-1003). T—600 v. c.t., 55 ma.; 5 v. 2 a., 6.3 v. 2.7 a. (Stancor P-6119)

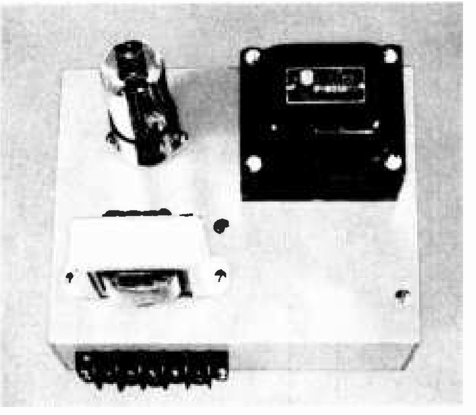


Figure 26

LOW-DRAIN POWER SUPPLY

nected in series so as to deliver 11.3 volts (nominal) to the heaters of the unit fed by the supply. The 11.3-volt output of the supply will be found to be adequate for operation of 12.6-volt tubes or for operation of a string consisting of two 6.3 volt tubes in series. The 11.3-volt heater supply is just about at the lower limit of the permissible plus or minus 10 per cent variation in heater voltage for conventional tube types.

It is recommended that a 6X5 rectifier be used in place of the more common 5Y3-GT type. This is particularly to be recommended when the power supply is to be installed in some space with limited ventilation such as the bottom compartment of a frequency meter. The 6X5-GT rectifier requires about one-third as much heater power as the 5Y3-GT, and in addition the 6X5-GT has less internal drop than the 5Y3-GT. The 6X4 miniature type may be used alternatively to the 6X5-GT when the reduced space requirements of the miniature tube envelope would be important. Further, where heater power and dissipation must be held to a minimum, the 6ZY5-G with its 6.3-volt 0.3 ampere heater may be used in place of the 6X5-GT if the output current is limited to 40 ma.

Some variation in the loaded output voltage of the power supply may be had by varying the value of the resistor from the rectifier tube to the first filter capacitor. The 5000-ohm 10-watt resistor shown in figure 25 will be found adequate for most limited-drain applications. For an application where less output voltage is required, this resistor may be increased in value; for increased voltage the resistor may be reduced in value, or eliminated entirely. When reduced output voltage from the power supply is required, as is normally the case with accessory test equipment, it is best to place the drop resistor in the position shown in the schematic of figure 25; when the drop resistor is used in this circuit position it serves additionally as a filter element to reduce the ripple-voltage output of the power supply, and it reduces the peak-emission requirement imposed on the cathode of the rectifier tube.

29-11 350-Volt 110-Ma. Power Supply

Figures 27 and 28 illustrate a general-purpose power supply suitable for operating a good size receiver, a low-power transmitter, or the exciter stages of a larger transmitter. The power supply is perfectly conventional, with a 5Y3-GT rectifier and a single-section capacitor-input filter. The two switches mounted on the front of the chassis are, respectively, the plate-voltage switch in the center tap of the power transformer high-voltage secondary, and the a-c line switch. A pair of leads, in parallel with the plate-voltage switch, are

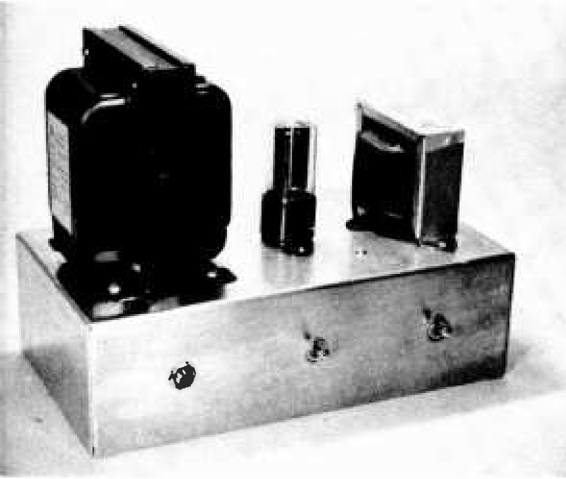


Figure 27
TOP OF THE 350-VOLT 110-MA. POWER SUPPLY

brought out for external control of the plate-voltage output of the supply. A key jack and key-click filter are also included in the chassis of the supply for use with center tap keying systems incorporated in many novice transmitters.

29-12 Variable Voltage Power Supply

Figures 29 through 32 show a multi-purpose power supply unit designed for general testing in the amateur station or in the laboratory. The chassis of the equipment actually contains two separate units. One unit is a 200 ma. variable-voltage power supply whose output voltage can be varied from approximately 100 volts to 400 volts under full load. The other unit is a dual-output regulated grid-bias pack with provisions for modulating one or both of the bias voltages for grid-bias modulation of an r-f amplifier. Although the two power supplies are mounted contiguously they will be described separately.

Variable Voltage Power Supply A pair of 2050 grid-controlled gas thyratrons are used as rectifiers in the variable-voltage power supply. These rectifier tubes have an inverse peak rating of 1300 volts and can deliver an average output current of 100 ma. each or 200 ma. for the pair. A 1300-volt inverse-peak rating on the tubes limits the maximum secondary voltage of the power transformer to about 460 each side of center. The particular transformer used in the unit illustrated furnishes 400 volts each side of center tap and is rated to carry an output current of 200 ma. A capacitor input filter is used so that the full load voltage with the con-

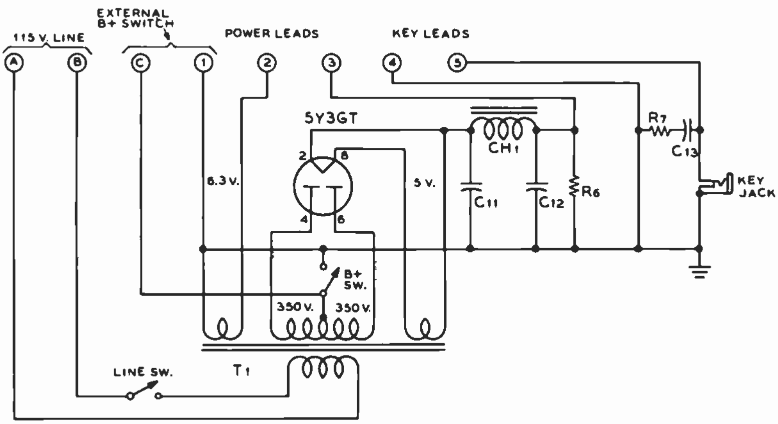


Figure 28
SCHEMATIC OF THE 350-VOLT SUPPLY

C_{11}, C_{12}—8-μfd. 500-volt electrolytics
C_{13}—0.5-μfd. 400-volt tubular
R_6—30,000-ohm 25-watt fixed bleeder
R_7—100-ohm 2-watt resistor
CH_1—10.5-hy. 110-ma. choke (Merit C-2993)
T_1—700 v. c.t. 110 ma., 5 v. 3 a., 6.3 v. 4.5 a. (Merit P-3153)
Switches—S.p.s.t. toggle switches

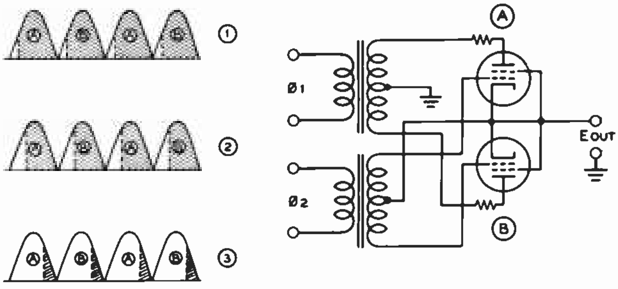


Figure 29

SHOWING THE OPERATION OF THE THYRATRON RECTIFIER CIRCUIT

Tubes (A) and (B) are type 2050 tetrode thyratrons. Phase 1 is the reference phase of the 115-volt line fed to the primary of the plate transformer. Phase 2 is controlled and varies the angle of the plate-supply voltage over which the thyratron tubes will conduct. The output voltage from the supply is taken from the cathodes of the tubes as in the case of any rectifier circuit. The cross-hatched area in (1), (2), and (3) represents the portion of the plate-voltage cycle during which tubes (A) and (B) are conducting. Condition (1) takes place when the grid voltage is substantially in phase with the plate voltage, so that conduction takes place over nearly the whole cycle. In (2) the phase of the grid voltage lags somewhat, while in (3) the phase of the grid voltage lags almost one-half cycle behind the plate voltage. (1) represents nearly full output voltage, (2) will give about half-voltage output, while (3) will give about the lower limit of stable output from the supply.

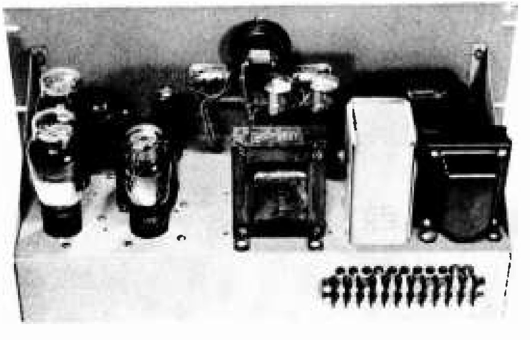
trol at maximum is about 400. Due to the peak current limitation of 1 ampere on the rectifier tubes, it is necessary to insert resistors in series with the plate leads. In the unit shown it was found convenient to combine the function of peak current limiting and hash suppression by placing a resistor in series with the plate lead of each tube. In addition a buffer capacitor is placed across each half of the primary of the plate transformer. Resistors R_3 and R_4 in conjunction with capacitors C_1 and C_2 serve the dual function of peak current limitation and hash suppression.

A unique feature of this power supply is the fact that the rectifier tubes are grid-controlled gas thyratrons. Hence it is possible to vary the output voltage of the power supply by varying the phase angle of the a-c voltage applied to the grids of the thyratrons. The use of thyratron tubes in this manner as controlled rectifiers is quite common in industrial practice but is seldom found in amateur equipment.

The mechanism of the action of the grids of the thyratron tubes in controlling the output voltage of the power supply is diagrammed in figure 29. The phase angle of the a-c line feeding the plates of the rectifiers, $\phi 1$, remains constant, as the reference phase,

Figure 30

REAR OF THE VARIABLE-VOLTAGE THYRATRON POWER SUPPLY



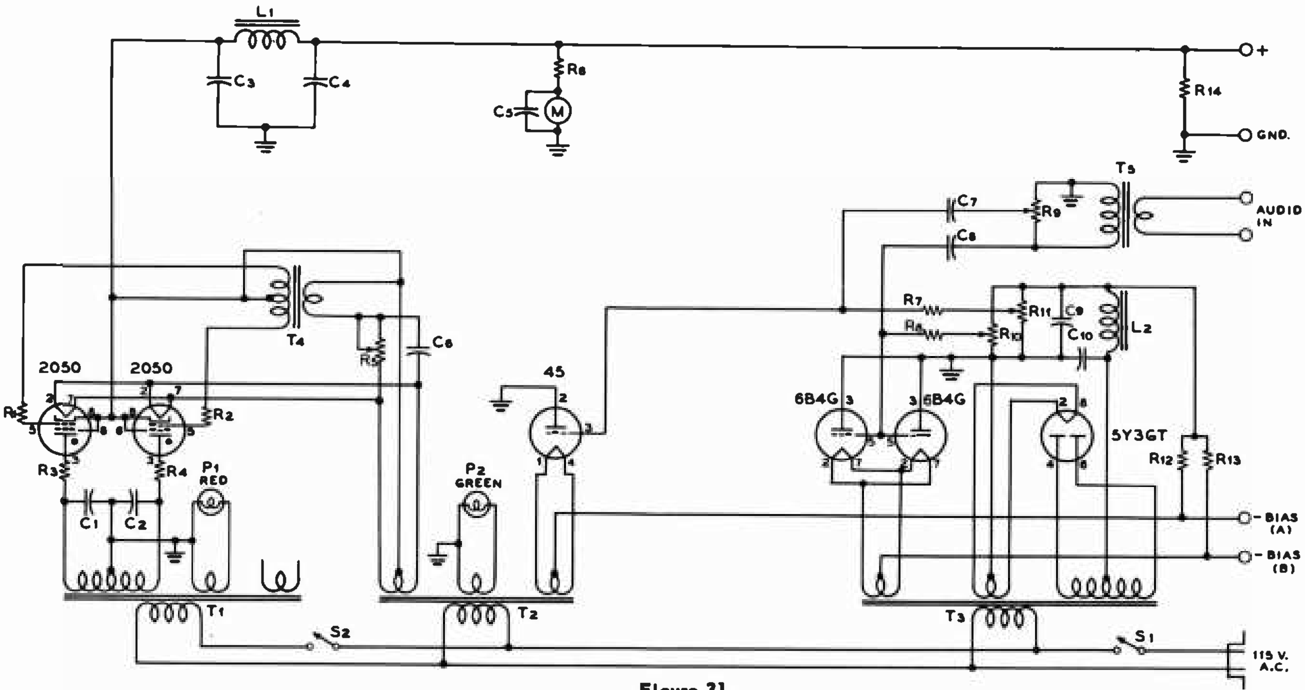


Figure 31

SCHEMATIC OF THE VARIABLE-VOLTAGE DUAL POWER SUPPLY

C_1, C_2—0.002-μfd. 1250-volt mica
C_3—4-μfd. 600-volt oil filled
C_4—8-μfd. 600-volt oil filled
C_5—0.003-μfd. mica
C_6—8-μfd. 150-volt elect.
C_7, C_8—0.05-μfd. 400-volt
C_9, C_{10}—8-μfd. 450-volt elect.
L_1—8.5-hy. 200-ma. choke (Stancor C-1721)
L_2—16-hy. 50-ma. choke (Stancor C-1003)
M—0-5 d-c milliammeter (Marion HM-2)

R_1, R_2—100,000 ohms ½ watt (Ohmite Little Devil)
R_3, R_4—200 ohms 10 watts (Ohmite Brown Devil)
R_5—10,000-ohm wire-wound potentiometer
R_6—Group of 2-watt resistors in series to make 100,000 ohms
R_7, R_8—100,000 ohms ½ watt (Ohmite Little Devil)
R_9—50,000-ohm potentiometer
R_{10}, R_{11}—70,000-ohm wire-wound potentiometers (Mallory 470MP)
R_{12}, R_{13}—25,000 ohms 10 watts (Ohmite Brown Devil)

R_{14}—50,000 ohms 20 watts (Ohmite Brown Devil)
S_1, S_2—S.p.s.t. toggle switches
T_1—400 volts to 460 volts each side center at 200 ma. (Stancor P-6165 used)
T_2—2.5 v. 3.5 a., 5 v. 3 a., 6.3 v. 3 a. (Stancor P-6144)
T_3—600 v. c.t. 55 ma., 5 v. 2 a., 6.3 v. 2.7 a. (Stancor P-6119)
T_4—Push-pull input, 3:1 ratio (Stancor A-4750)
T_5—Line to grid (Stancor A-4351)

throughout this discussion. However, the phase angle of the voltage applied to the grids of the thyratrons, $\phi 2$, is varied by means of the phase-shifting network with its control R_5 in figure 31. When the phase of the voltage applied to the grids is essentially the same as that applied to the plates, the tube conducts over substantially the entire cycle as is the case with any mercury-vapor or gas-type rectifier tube. This condition is illustrated by figure 29 (1). However, when the phase angle of the voltage applied to the grids is retarded, as in (2), the tube will not conduct until the actual negative grid voltage becomes more positive than the critical value for the applied plate voltage. When the critical value is reached, the tube ionizes and current flows through the remaining portion of the half-cycle. The portion of each half cycle during which conduction occurs is indicated by the cross-hatch lines in figure 29.

It is important to remember that a thyratron tube continues to conduct, after once having been fired, so long as the plate is positive with respect to the cathode; the grid loses control completely over the flow of current once its peak potential has exceeded the critical value and ionization has taken place. Hence thyratrons must be used in a type of circuit where voltages are periodically applied, with a short resting period between operating cycles. The power supply circuit of figure 31 is an example of such an arrangement since the plate voltage on each tube becomes negative after each period of conduction.

When the phase angle of the voltage on the grid is made to lag far behind that applied to the plate, the tube conducts over only a small portion of the half cycle during which the plate is positive with respect to the cathode. (See figure 29 (3).) In a power supply such as that illustrated, this type of operation results in the lowest value of output voltage which may be obtained from the power supply.

The phase-shifting network in the power supply illustrated is made up of R_5 and C_6. These two components are connected across the 6.3-volt winding for the 2050 heaters in such a manner that the phase of the voltage across the primary of T_4 may be varied over a wide angle. The phase-shifted voltage then is fed to the grids of the 2050 tubes from the push-pull secondary transformer T_4. Type 2D21 miniature thyratrons may be used in place of 2050's since their characteristics are similar. The balance of the circuit for the power supply is conventional, with a 0-5 milliammeter connected in series with the bleeder on the output of the power supply in such a manner that the milliammeter acts as a voltmeter. The output voltage is obtained by multiplying the milliammeter reading by 100.

Specifications for the 2050 tube call for a delay of at least 10 seconds after the application of heater voltage before the tube is required to conduct. This requirement is met by isolating the transformer which supplies heater power from the plate transformer. When S_1 is closed, heater power is applied to all tubes, and the bias supply becomes operative. Green pilot lamp P_2 lights whenever the heaters of the tubes are energized. Then when S_2 is closed the red pilot lamp P_1 lights, and plate voltage is applied to the 2050's. The output voltage of the power supply indicated by the milliammeter/voltmeter on the front panel, and

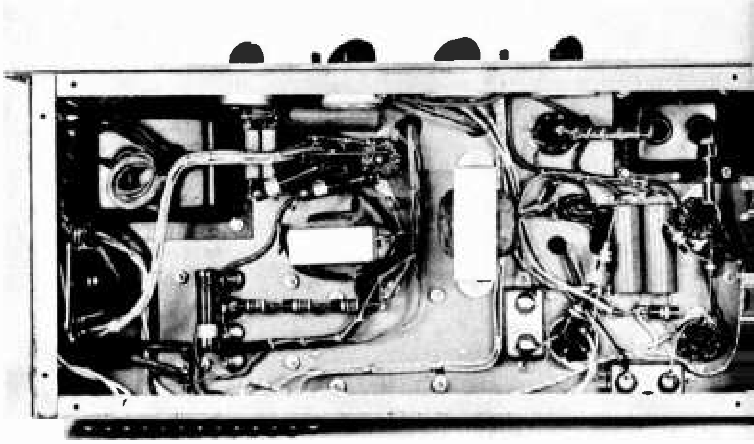


Figure 32
UNDERCHASSIS OF THE THYRATRON POWER SUPPLY

the value of the output voltage may be varied by the front-panel control of the potentiometer R_5.

The Regulated Bias Supply The balance of the chassis of the unit is taken up by the regulated bias supply. Two separately controlled bias outputs are provided, either one of which may be varied from a few volts to about −300 volts. Bias output (A), which uses a type 45 tube as the regulator, is capable of handling a maximum grid current into the bias pack of about 50 ma. Bias output (B), using a pair of 6B4-G tubes in parallel, is capable of handling up to 200 ma. of grid current from the tubes to which it feeds bias.

The circuit of the bias supply uses a 5Y3-GT as a rectifier, with the tubes specified in the previous paragraph as reverse-connected bias regulators. Potentiometers R_{10} and R_{11}, which are brought out to the front panel, serve to control separately the output voltage from each of the bias channels. Provision has been included with the components T_5, R_7, R_8, R_9, C_7, and C_8 for modulation of the grid-bias voltage by means of an audio signal from an external speech amplifier. Since potentiometer R_9 permits controlling the ratio of the audio voltage on channel (A) with respect to that on bias channel (B), the bias pack may be used for simultaneous cascade grid-bias modulation of two successive stages in an AM transmitter. Such an arrangement would be particularly convenient when grid-bias modulating a grounded-grid output stage (such as with one or two 304TL's) while simultaneously grid-bias modulating the stage which excites the final amplifier (which might be an 812A, 35TG, or similar type).

Obviously the bias-modulating portion of the regulated grid-bias pack may be omitted if this provision never will be needed. But if a bias supply such as the one described is to be used as a portion of a c-w transmitter, the inclusion of the few components for grid-bias modulation will allow the transmitter to be used for AM phone with little difficulty, should the occasion demand. Also, the bias supply may be separated from the variable-voltage power supply in the event that only one or the other is required simply by separating the functions of the filament transformer T_2.

29-13 400-Volt 250-Ma. Power Supply

Illustrated in figures 33, and 34 is a 400-volt power supply capable of delivering 250 ma. of current to the load. Type 816 tubes are used as rectifiers to feed a two-section choke-input filter. A high degree of filtering is obtained through use of two 10-μfd. 600-volt oil-filled capacitors in the filter system. Ripple percentage at full output from the power supply is about 0.25 per cent. The regulation from the supply is sufficiently good so that the one

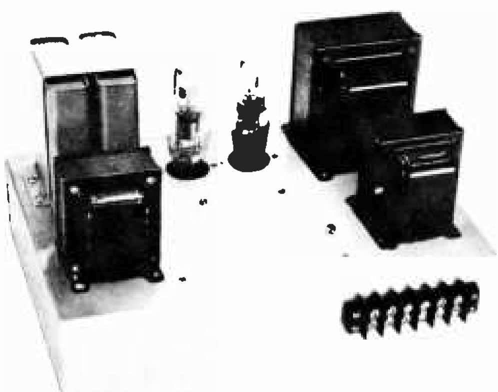


Figure 33
FRONT OF THE 400-VOLT 250-MA. SUPPLY

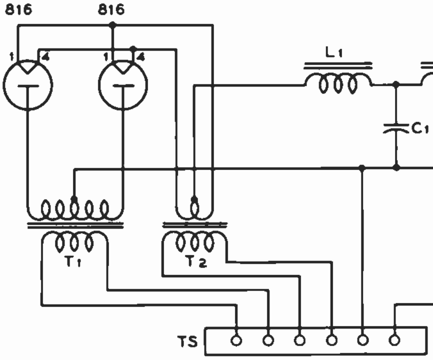


Figure 34
SCHEMATIC OF THE 400-VOLT 250-MA. SUPPLY

C_1, C_2—10-μfd. 600-volt oil filled
L_1—2-12 hy. 250-ma. swinging choke (Stancor C-1402)
L_2—4-hy. 250-ma. filter choke (Stancor C-1412)
T_1—1000 v. c.t., 300 ma. max. (Stancor P-8040)
T_2—2.5 v. 5 a., 7500 v. insulation (Stancor P-6133)
R—25,000 ohms, 25 watts fixed (Ohmite 0219)

power supply may be used to feed both the final amplifier and a class AB_2 or class B modulator for the r-f amplifier. The primary of the plate transformer is brought out to a separate pair of terminals from the primary of the rectifier filament transformer. The separation of the two primary circuits allows a greater degree of flexibility in the control circuits of the transmitter of which the power supply is a unit.

29-14 1250-Volt 250-Ma. Power Supply

One of the most popular and also one of the most convenient power ranges for amateur equipment is that which can be supplied from a 1250-volt power unit with a current capability of 200 to 300 ma. Figures 35, 36 and 37 illustrate such a power unit. The power supply has been assembled using the new "CG" series of components manufactured by UTC. Nearly all the components in this series are housed in cylindrical drawn-metal cans fitted with bottom terminals and finished in a medium grey enamel.

The supply is designed to provide plate voltage for a class C amplifier stage and a class B modulator. Plate voltage for the modu-

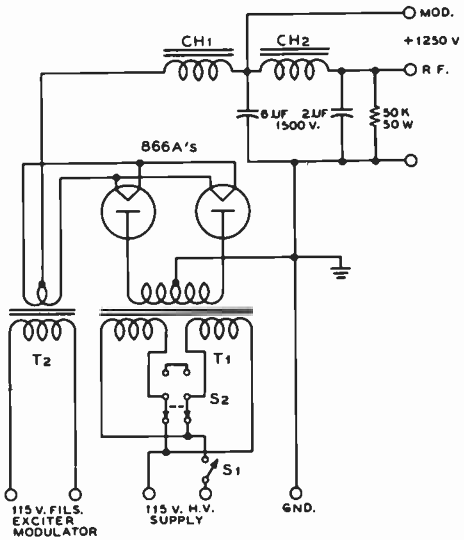


Figure 35
SCHEMATIC OF THE 1250-VOLT SUPPLY

CH_1—5-25 hy. 250-ma. swinging choke (UTC CG-103)
CH_2—12-hy. 250-ma. filter choke (UTC CG-102)
T_1—3000, 2470, and 800 c.t., 260 ma. (UTC CG-303)
T_2—2½ volts, 10 amps., 2500-volt working (UTC CG-34)
S_1—D.p.s.t. toggle switch (contacts in parallel)
S_2—10-amp. d.p.d.t. toggle switch

COPPER WIRE TABLE

Gauge No. B. & S.	Diam. in Mils[1]	Circular Mil Area	Turns per Linear Inch[2]				Turns per Square Inch[2]			Feet per Lb.		Ohms per 1000 ft. 25° C.	Correct Capacity at 1500 C.M. per Amp.[3]	Diam. in mm.
			Enamel	S.S.C.	D.S.C. or S.C.C.	D.C.C.	S.C.C.	Enamel	D.C.C.	Bare	D.C.C.			
1	289.3	82690	—	—	—	—	—	—	—	3.947	—	.1264	55.7	7.348
2	257.6	66370	—	—	—	—	—	—	—	4.977	—	.1593	44.1	6.544
3	229.4	52640	—	—	—	—	—	—	—	6.276	—	.2009	35.0	5.827
4	204.3	41740	—	—	—	—	—	—	—	7.914	—	.2533	27.7	5.189
5	181.9	33100	—	—	—	—	—	—	—	9.980	—	.3195	22.0	4.621
6	162.0	26250	—	—	—	—	—	—	—	12.58	—	.4028	17.5	4.115
7	144.3	20820	—	—	—	—	—	—	—	15.87	—	.5080	13.8	3.665
8	128.5	16510	7.6	—	7.4	7.1	—	—	—	20.01	19.6	.6405	11.0	3.264
9	114.4	13090	8.6	—	8.2	7.8	—	—	—	25.23	24.6	.8077	8.7	2.906
10	101.9	10380	9.6	—	9.3	8.9	87.5	84.8	80.0	31.82	30.9	1.018	6.9	2.588
11	90.74	8234	10.7	—	10.3	9.8	110	105	97.5	40.12	38.8	1.284	5.5	2.305
12	80.81	6530	12.0	—	11.5	10.9	136	131	121	50.59	48.9	1.619	4.4	2.053
13	71.96	5178	13.5	—	12.8	12.0	170	162	150	63.80	61.5	2.042	3.5	1.828
14	64.08	4107	15.0	—	14.2	13.8	211	198	183	80.44	77.3	2.575	2.7	1.628
15	57.07	3257	16.8	—	15.8	14.7	262	250	223	101.4	97.3	3.247	2.2	1.450
16	50.82	2583	18.9	18.9	17.9	16.4	321	306	271	127.9	119	4.094	1.7	1.291
17	45.26	2048	21.2	21.2	19.9	18.1	397	372	329	161.3	150	5.163	1.3	1.150
18	40.30	1624	23.6	23.6	22.0	19.8	493	454	399	203.4	188	6.510	1.1	1.024
19	35.89	1288	26.4	26.4	24.4	21.8	592	553	479	256.5	237	8.210	.86	.9116
20	31.96	1022	29.4	29.4	27.0	23.8	775	725	625	323.4	298	10.35	.68	.8118
21	28.46	810.1	33.1	32.7	29.8	26.0	940	895	754	407.8	370	13.05	.54	.7230
22	25.35	642.4	37.0	36.5	34.1	30.0	1150	1070	910	514.2	461	16.46	.43	.6438
23	22.57	509.5	41.3	40.6	37.6	31.6	1400	1300	1080	648.4	584	20.76	.34	.5733
24	20.10	404.0	46.3	45.3	41.5	35.6	1700	1570	1260	817.7	745	26.17	.27	.5106
25	17.90	320.4	51.7	50.4	45.6	38.6	2060	1910	1510	1031	903	33.00	.21	.4547
26	15.94	254.1	58.0	55.6	50.2	41.8	2500	2300	1750	1300	1118	41.62	.17	.4049
27	14.20	201.5	64.9	61.5	55.0	45.0	3030	2780	2020	1639	1422	52.48	.13	.3606
28	12.64	159.8	72.7	68.6	60.2	48.5	3670	3350	2310	2067	1759	66.17	.11	.3211
29	11.26	126.7	81.6	74.8	65.4	51.8	4300	3900	2700	2607	2207	83.44	.084	.2859
30	10.03	100.5	90.5	83.3	71.5	55.5	5040	4660	3020	3287	2534	105.2	.067	.2546
31	8.928	79.70	101.	92.0	77.5	59.2	5920	5280	—	4145	2768	132.7	.053	.2268
32	7.950	63.21	113.	101.	83.6	62.6	7060	6250	—	5227	3137	167.3	.042	.2019
33	7.080	50.13	127.	110.	90.3	66.3	8120	7360	—	6591	4697	211.0	.033	.1798
34	6.305	39.75	143.	120.	97.0	70.0	9600	8310	—	8310	6168	266.0	.026	.1601
35	5.615	31.52	158.	132.	104.	73.5	10900	8700	—	10480	6737	335.0	.021	.1426
36	5.000	25.00	175.	143.	111.	77.0	12200	10700	—	13210	7877	423.0	.017	.1270
37	4.453	19.83	198.	154.	118.	80.3	—	—	—	16660	9309	533.4	.013	.1131
38	3.965	15.72	224.	166.	126.	83.6	—	—	—	21010	10666	672.6	.010	.1007
39	3.531	12.47	248.	181.	133.	86.6	—	—	—	26500	11907	848.1	.008	.0897
40	3.145	9.88	282.	194.	140.	89.7	—	—	—	33410	14222	1069	.006	.0799

[1]A mil is 1/1000 (one thousandth) of an inch.
[2]The figures given are approximate only, since the thickness of the insulation varies with different manufacturers.
[3]The current-carrying capacity at 1000 C.M. per ampere is equal to the circular-mil area (Column 3) divided by 1000.

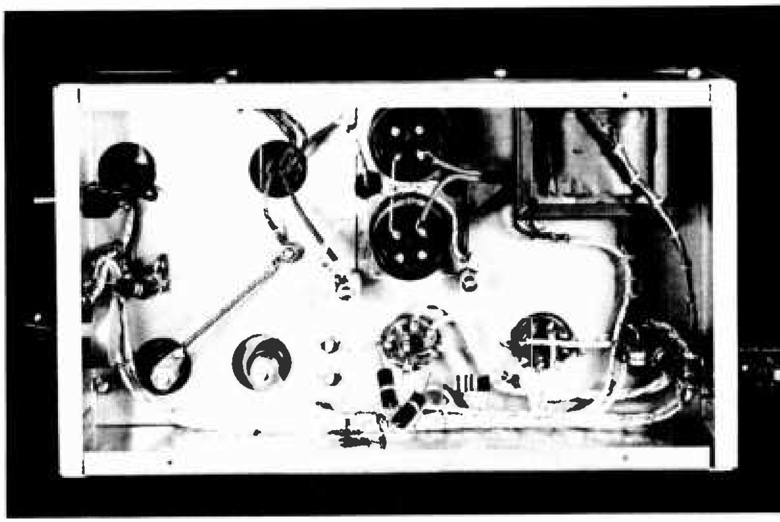


Figure 36
UNDERCHASSIS OF THE 1250-VOLT SUPPLY

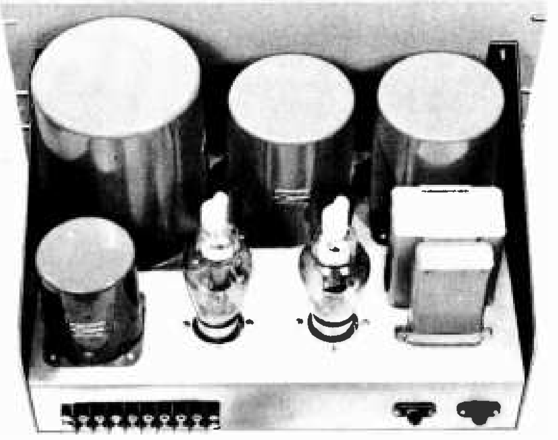
Note the manner in which cut-outs have been made to allow for mounting the "CG" series transformers, filter capacitors, and rectifier sockets. A socket-hole punch was used for the filter capacitors and the chokes, while a "Bruno" adjustable hole cutter was used for tube sockets and transformers. Plate leads to the tubes are ignition cable, while all other leads are no. 14 "Deltabeston" gray switchboard wire (available from G. E. Supply Co.).

lators is taken from the power supply after the first section of filter since less filtering is required for the push-pull modulators. Note that a 6-μfd. filter capacitor is used at this position so that ample storage capacity will be available to meet the peak-current requirements of the modulator tubes. Plate voltage for the final amplifier is taken off after an additional stage of filter, with a 2-μfd. filter capacitor used in this case since the peak current requirements of the final amplifier stage are less stringent.

Since the CG-303 plate transformer was provided with dual primaries for either 115-volt or 230-volt operation, it was deemed desirable to take advantage of this feature so as to make available either full voltage or half-voltage from the power supply. The two primaries are connected in series for half-voltage operation and they are connected in parallel for full-voltage output. Switch S_2 accomplishes the changeover from half to full voltage from the power unit. Switch S_1 acts as the local plate-voltage control switch. As in the case of all power supplies which use mercury-vapor rectifiers and yet do not have a time-delay relay, it is necessary to wait at least 30 seconds after application of filament voltage before the primary of the plate transformer is energized.

Figure 37
REAR VIEW OF THE 1250-VOLT 250-MA POWER SUPPLY

The unit is constructed on an 11 by 17 by 3 inch steel chassis with a 10½ by 19 inch steel panel. The two high-voltage output terminals can be seen on the right of the rear drop of the chassis.



CHAPTER THIRTY

Workshop Practice

With a few possible exceptions, such as fixed air capacitors, neutralizing capacitors and transmitting coils, it hardly pays one to attempt to build the components required for the construction of an amateur transmitter. This is especially true when the parts are of the type used in construction and replacement work on broadcast receivers, as mass production has made these parts very inexpensive.

Transmitters Those who have and wish to spend the necessary time can effect considerable monetary saving in their transmitters by building them from the component parts. The necessary data are given in the construction chapters of this handbook.

To many builders, the construction is as fascinating as the operation of the finished transmitter; in fact, many amateurs get so much satisfaction out of building a well-performing piece of equipment that they spend more time constructing and rebuilding equipment than they do operating the equipment on the air.

30-1 Tools

Beautiful work can be done with metal chassis and panels with the help of only a few inexpensive tools. However, the time required for construction will be greatly reduced if a fairly complete assortment of metal-working tools is available. Thus, it can be seen that while an array of tools will speed up the work, excellent results may be accomplished with but few tools, if one has the time and patience.

The investment one is justified in making in tools is dependent upon several factors. If you like to tinker, there are many tools useful in radio construction that you would probably buy anyway, or perhaps already have, such as screwdrivers, hammer, saws, square, vise, files, etc. This means that the money taken for tools from your radio budget can be used to buy the more specialized tools, such as socket punches or hole saws, taps and dies, etc.

The amount of construction work one does determines whether buying a large assortment of tools is an economical move. It also determines if one should buy the less expensive type offered at surprisingly low prices by the familiar mail order houses, "five and ten" stores and chain auto-supply stores, or whether one should spend more money and get first-grade tools. The latter cost considerably more and work but little better when new, but will outlast several sets of the cheaper tools. Therefore they are a wise investment for the experimenter who does lots of construction work (if he can afford the initial cash outlay). The amateur who constructs only an occasional piece of apparatus need not be so concerned with tool life, as even the cheaper grade tools will last him several years, if they are given proper care.

The hand tools and materials in the accompanying lists will be found very useful around the home workshop. Materials not listed but ordinarily used, such as paint, can best be purchased as required for each individual job.

ESSENTIAL HAND TOOLS AND MATERIALS

1 *Good* electric soldering iron, about 100 watts
1 Spool rosin-core wire solder
1 Each large, medium, small, and midget screwdrivers
1 *Good* hand drill (eggbeater type), preferably two speed
1 Pair regular pliers, 6 inch
1 Pair long nose pliers, 6 inch
1 Pair cutting pliers (diagonals), 5 inch or 6 inch
1 1⅛-inch tube-socket punch
1 "Boy Scout" knife
1 Combination square and steel rule, 1 foot
1 Yardstick or steel pushrule
1 Scratch awl or ice pick scribe
1 Center punch
1 Dozen or more assorted round shank drills (as many as you can afford between no. 50 and ¼ or ⅜ inch, depending upon size of hand drill chuck)
1 Combination oil stone
Light machine oil (in squirt can)
Friction tape
1 Hacksaw and blades
1 Medium file and handle
1 Cold chisel (½ inch tip)
1 Wrench for socket punch
1 Hammer

HIGHLY DESIRABLE HAND TOOLS AND MATERIALS

1 Bench vise (jaws at least 3 inch)
1 Spool plain wire solder
1 Carpenter's brace, ratchet type
1 Square-shank countersink bit
1 Square-shank taper reamer, small
1 Square-shank taper reamer, large (the two reamers should overlap; ½ inch and ⅞ inch size will usually be suitable)
1 ⅞ inch tube-socket punch (for electrolytic capacitors)
1 1-3/16 inch tube-socket punch
1 ⅝-inch tube-socket punch
1 Adjustable circle cutter for holes to 3 inch
1 Set small, inexpensive, open-end wrenches
1 Pair tin shears, 10 or 12 inch
1 Wood chisel (½ inch tip)
1 Pair wing dividers

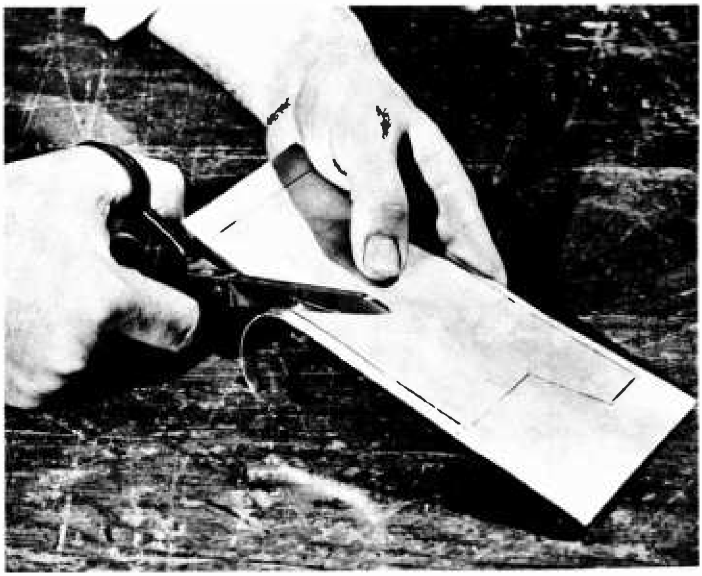


Figure 1
SOFT ALUMINUM SHEET MAY BE CUT WITH HEAVY KITCHEN SHEARS

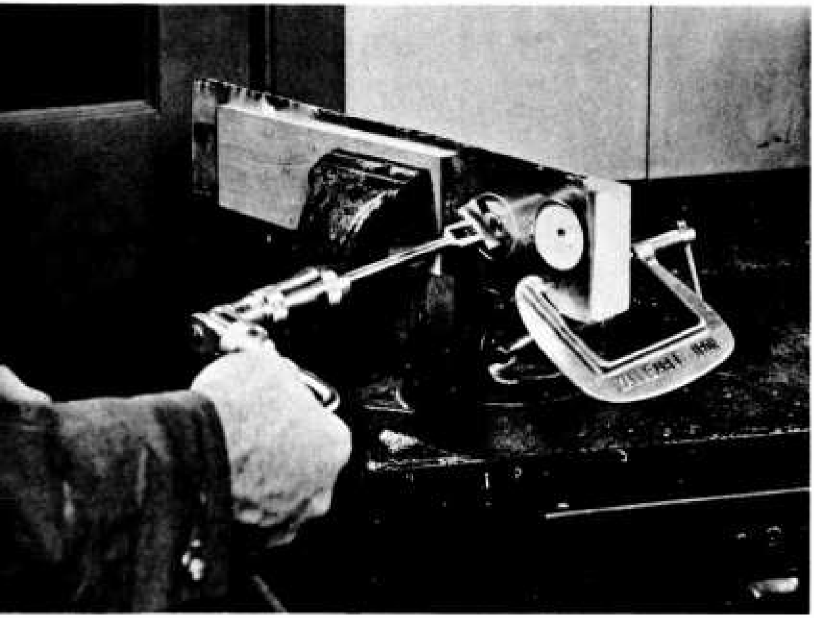


Figure 2
CONVENTIONAL WOOD EXPANSION BIT IS EFFECTIVE IN DRILLING SOCKET HOLES IN REYNOLDS DO-IT-YOURSELF ALUMINUM

1 Coarse mill file, flat 12 inch
1 Coarse bastard file, round, ½ or ¾ inch
1 Set allen and spline-head wrenches
6 or 8 Assorted small files; round, half-round, triangular, flat, square, rat-tail
4 Small "C" clamps
Steel wool, coarse and fine
Sandpaper and emery cloth, coarse, medium, and fine
Duco cement
File brush

USEFUL BUT NOT ESSENTIAL TOOLS AND MATERIALS

1 Jig or scroll saw (small) with metal-cutting blades
1 Small wood saw (crosscut teeth)
1 Each square-shank drills: ⅜, 7/16, and ½ inch
1 Tap and die outfit for 6-32, 8-32, 10-32 and 10-24 machine screw threads
4 Medium size "C" clamps
Lard oil (in squirt can)
Kerosene
Empire cloth
Clear lacquer ("industrial" grade)
Lacquer thinner
Dusting brush
Paint brushes
Sheet celluloid, Lucite, or polystyrene
1 Carpenter's plane
1 Each "Spintite" wrenches, ¼, 5/16, 11/32 to fit the standard 6-32 and 8-32 nuts used in radio work
1 Screwdriver for recessed head type screws

The foregoing assortment assumes that the constructor does not want to invest in the more expensive power tools, such as drill press, grinding head, etc. If power equipment is purchased, obviously some of the hand tools and accessories listed will be superfluous. A drill press greatly facilitates construction work, and it is unfortunate that a good one costs as much as a small transmitter.

Not listed in the table are several special-purpose radio tools which are somewhat of a luxury, but are nevertheless quite handy, such as various around-the-corner screwdrivers and wrenches, special soldering iron tips, etc. These can be found in the larger radio parts stores and are usually listed in their mail order catalogs.

If it is contemplated to use the newer and very popular miniature series of tubes (6AK5, 6C4, 6BA6, etc.) in the construction of equipment certain additional tools will be required to mount the smaller components. Miniature tube sockets mount in a ⅝-inch hole, while 9-pin sockets mount in a ¾-inch hole. Greenlee socket punches can be obtained in these sizes, or a smaller hole may be reamed to the

Figure 3
SOFT ALUMINUM TUBING MAY BE BENT AROUND WOODEN FORM BLOCKS. TO PREVENT THE TUBE FROM COLLAPSING ON SHARP BENDS, IT IS PACKED WITH WET SAND.

proper size. Needless to say, the punch is much the more satisfactory solution. Mounting screws for miniature sockets are usually of the 4-40 size.

Metal Chassis Though quite a few more tools and considerably more time will be required for metal chassis construction, much neater and more satisfactory equipment can be built by mounting the parts on sheet metal chassis instead of breadboards. This type of construction is necessary when shielding of the apparatus is required. A front panel and a back shield minimizes the danger of shock and completes the shielding of the enclosure.

30-2 The Material

Electronic equipment may be built upon foundations of wood, steel or aluminum. The choice of foundation material is governed by the requirements of the electrical circuit, the weight of the components of the assembly, and the financial cost of the project when balanced against the pocketbook contents of the constructor.

Breadboard The simplest method of constructing equipment is to lay it out in breadboard fashion, which consists of fastening the various components to a board of suitable size with wood screws or machine bolts, arranging the parts so that important leads will be as short as possible.

Breadboard construction is suitable for testing an experimental layout, or sometimes for assembling an experimental unit of test equipment. But no permanent item of station equipment should be left in the breadboard form. Breadboard construction is dangerous, since components carrying dangerous voltages are left exposed. Also, breadboard construction is never suitable for any r-f portion of a transmitter, since it would be substantially impossible to shield such an item of equipment for the elimination of TVI resulting from harmonic radiation.

Dish type construction is practically the same as metal chassis construction, the main difference lying in the manner in which the chassis is fastened to the panel.

Special Frameworks For high-powered r-f stages, many amateur constructors prefer to discard the more conventional types of construction and employ instead special metal frameworks and brackets which they design specially for the parts which they intend to use. These are usually arranged to give the shortest possible r-f leads and to fasten directly behind a relay rack panel by means of a few bolts, with the control shafts projecting through corresponding holes in the panel.

Working with Aluminum The necessity of employing "electrically tight enclosures" for the containment of TVI-producing harmonics has led to the general use of aluminum for chassis, panel, and enclosure construction. If the proper type of aluminum material is used, it may be cut and worked with the usual woodworking tools found in the home shop. Hard, brittle aluminum alloys such as 24ST and 61ST should be avoided, and the

Figure 4
A WOODWORKING PLANE MAY BE USED TO SMOOTH OR TRIM THE EDGES OF REYNOLDS DO-IT-YOURSELF ALUMINUM STOCK

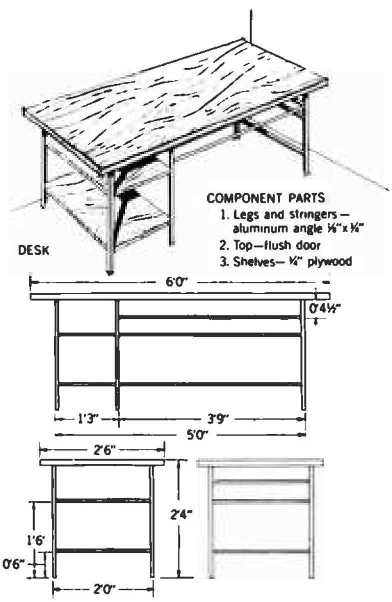


Figure 5
INEXPENSIVE OPERATING DESK MADE FROM ALUMINUM ANGLE STOCK, PLYWOOD AND A FLUSH-TYPE DOOR

softer materials such as 2S or ½H should be employed.

A new market product is Reynold's *Do-it-yourself* aluminum, which is being distributed on a nationwide basis through hardware stores, lumber yards and building material outlets. This material is an alloy which is temper selected for easy working with ordinary tools. Aluminum sheet, bar and angle stock may be obtained, as well as perforated sheets for ventilated enclosures.

Figures 1 through 4 illustrate how this soft material may be cut and worked with ordinary shop tools, and figure 5 shows a simple operating desk that may be made from aluminum angle stock, plywood and a flush-type six foot door.

30-3 TVI-Proof Enclosures

Armed with a right-angle square, a tin-snips and a straight edge, the home constructor will find the assembly of aluminum enclosures an easy task. This section will show simple construction methods, and short cuts in producing enclosures.

The simplest type of aluminum enclosure is used on the VFO exciter of Chapter 25. This enclosure is shown in figure 6. An aluminum chassis forms the base of the enclosure. Two

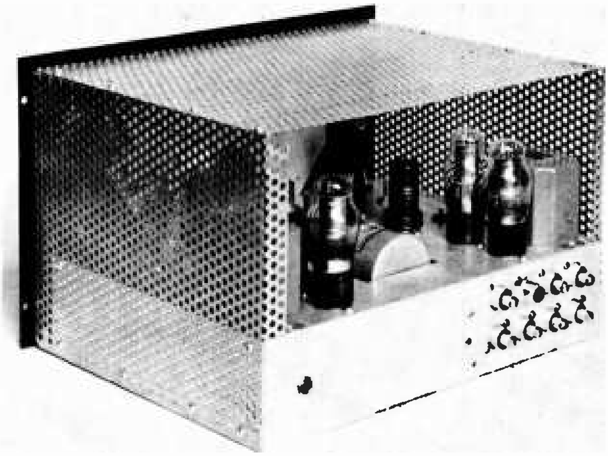


Figure 6

TVI-PROOF ENCLOSURE FORMED FROM FOUR PIECES OF PERFORATED ALUMINUM STOCK. A FIFTH PIECE IS USED TO SHIELD THE BOTTOM OF THE CHASSIS.

sides are cut from a sheet of perforated metal stock and fastened to each side of the chassis by means of no. 6 self-tapping sheet metal screws. One-half inch folds are made on the back, front and top sides of the end pieces. These two pieces are mirror images in that the folds in each piece are reversed in direction, forming a "right hand" and a "left hand" side.

The folds may be made in a large vise, but lacking such an object, the aluminum may be grasped between two wooden slats which are held firmly together by means of two adjustable "C-clamps." A light hammer is used to bend the soft aluminum around the edge of the wood. Care should be taken that all angles are square, and the two sides are the same size, otherwise the completed enclosure will not be symmetrical.

When the sides are completed, they are attached to the ends of the aluminum chassis, and the front panel is bolted to the chassis and to the sides. The top plate may now be cut. It is fastened to the panel by a 1/2 inch fold at the front, and is bolted to the top folds on the side pieces by 6-32 machine screws. For maximum TVI suppression, the screws holding the enclosure together should not be more than 2 inches apart. It is necessary to scrape the front panel free of paint at the joint between the panel and the enclosure.

The back plate is now formed. It should have a 1/2 inch lip at the bottom to facilitate attachment to the rear edge of the chassis. A strip of angle stock is bolted to the top edge of the back plate. The top edge of this strip is then tapped for 6-32 screws at about 2 inch intervals along its length. These holes should line up with the existing holes in the perforated material that forms the top plate. It is necessary to use this tapped angle strip, since it is next to impossible to get your hand inside the enclosure to hold nuts in position along the top edge of the back plate when the back plate is being bolted into position.

The enclosure for the 811-A amplifier of Chapter 26 is built up in much the same way (figure 7). This enclosure is quite a bit larger in size than that of figure 6, and is therefore built upon a frame made of 1/2 inch aluminum angle-stock. Strips of angle stock are attached to the two sides, and the rear of the chassis by means of no. 6 sheet metal screws. The strips are set back from the edge of the chassis about 1/4 inch. Two additional 1/2 inch angle strips run up each side of the front panel, and are attached to the front panel by 6-32 flat-head machine screws. A third strip runs across the front panel about 1/4 inch below the top of the panel. The two end pieces are now cut and attached to the angle strips at each end of the chassis. Next, the back side pieces of angle stock are cut and affixed to the perforated end pieces by means of sheet metal screws. Finally, the top pieces of angle stock are fastened in place. A rigid box is now formed of angle stock, each piece being held in place by being attached to the perforated end pieces, and the perforated top plate.

As seen in figure 7, this construction provides a frame around the rear opening which may be closed by covering it with a piece of perforated material. The four sides of the opening that are formed by the angle material are

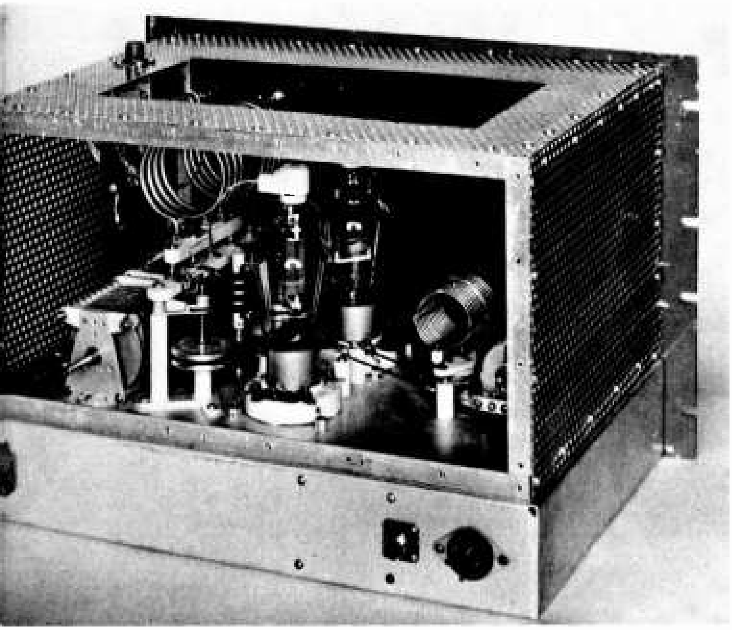


Figure 7
ALUMINUM ANGLE STOCK FORMS THE FRAMEWORK FOR THE ENCLOSURE OF THE 811-A AMPLIFIER

In this particular amplifier, it is necessary to have a top opening through which it is possible to change both the plate and grid circuit inductors. Accordingly, a square hole is cut in the top of the enclosure, which is covered by a slightly larger piece of perforated material during amplifier operation. This cover piece is affixed to the top of the cabinet by means of two pieces of spring brass. When the top of the cabinet is opened to change coils, the shielded enclosure is opened at the same time.

The perforated metal enclosure for the 4-250A amplifier of Chapter 26, Section 9 is shown in figure 8. This is a simplified version of the enclosure of figure 7. The two side pieces of the enclosure and the back are bolted directly to the aluminum chassis by means of sheet metal screws. The only angle-stock used in the enclosure are two vertical pieces in the rear corners which form the joint between the sides and the back. A lip is bent inwards on the top of the back shield and is bolted directly to the top piece by means of 6-32 machine screws. A 1/4 inch lip is formed around the front edge of the top and side pieces. This lip is bolted to the front panel by means of flathead screws. The enclosure forms a complete unit and may be lifted off the amplifier in one piece, if desired.

The push-pull 250-TH amplifier of Chapter 26, Section 4 has a more sophisticated type of enclosure. Here, the aluminum angle pieces are machined to length and are fixed in position by means of triangular gusset plates at each joint, as shown in figure 9. Each piece of perforated material is fitted inside the angle pieces, and the whole assembly is held to-tapped at intervals for 6-32 machine screws, which hold the back plate in position.

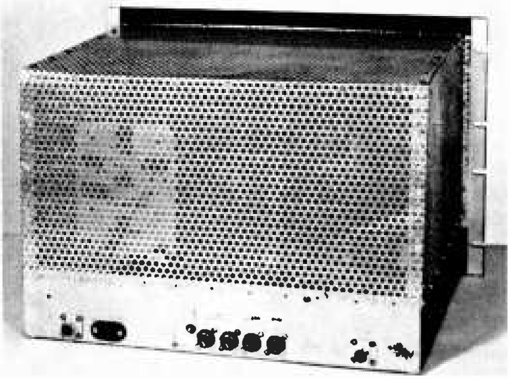


Figure 8
THE SIMPLE ENCLOSURE FOR THE 4-250A AMPLIFIER

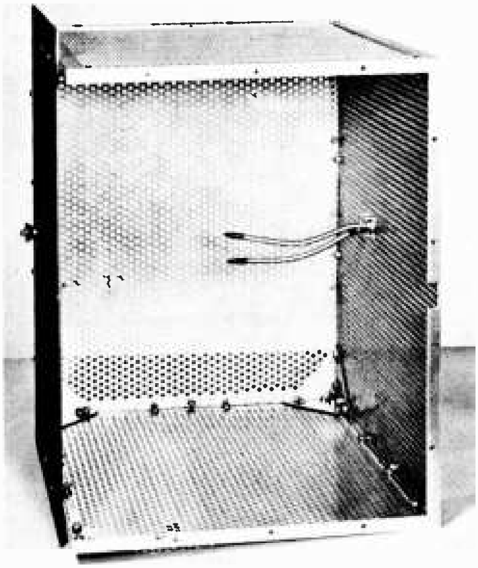


Figure 9

THE PERFORATED ALUMINUM SHEET OF THIS ENCLOSURE IS MOUNTED INSIDE THE ALUMINUM ANGLE STOCK. TRIANGULAR GUSSET PLATES ARE USED AT EACH JOINT. THIS ENCLOSURE FITS ATOP THE 250-TH AMPLIFIER OF CHAPTER 26, FIGURE 13

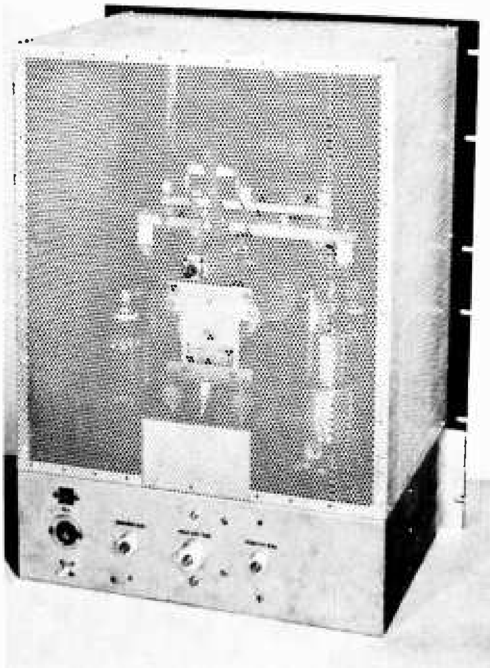


Figure 10

TVI-PROOF ENCLOSURE OF ONE-KILOWATT AMPLIFIER OF CHAPTER 26, SECTION 3

gether by means of elastic stop-nuts. The coaxial antenna receptacle is mounted to the center of the rear enclosure plate, and flexible leads connect this receptacle to the swinging link assembly of the plate tank circuit of the amplifier.

The shielded enclosure of the 1-kilowatt amplifier of Chapter 26, Section 3 is made up of a frame constructed of 1/2 inch aluminum angle stock, and the shield pieces are held in place by no. 6 sheet metal screws. A thicker grade of perforated stock with smaller holes is employed here. The rear of this enclosure is shown in figure 10.

30-4 Enclosure Openings

Openings into shielded enclosures may be made simply by covering them by a piece of shielding which can be removed by hand, as was done in the cover port of the 811-A amplifier of Chapter 26, Section 2.

Openings through vertical panels, however, usually require a bit more attention to prevent the leakage of harmonic energy through the cracks of the door which is supposed to seal the opening. Most of the amplifiers of Chapter 26 that require a panel opening make use of the Bud Radio Co. ventilated door rack panel (PS-814 or PS-815). The grille opening in this panel has holes small enough in area to prevent serious harmonic leakage. The actual door opening, however, does not seal tightly enough to be called TVI-proof. In areas of high TV signal strength where a minimum of operation on 28 Mc. is contemplated, the door is satisfactory as is. To accomplish more complete harmonic suppression, the edges of the opening should be lined with preformed con-

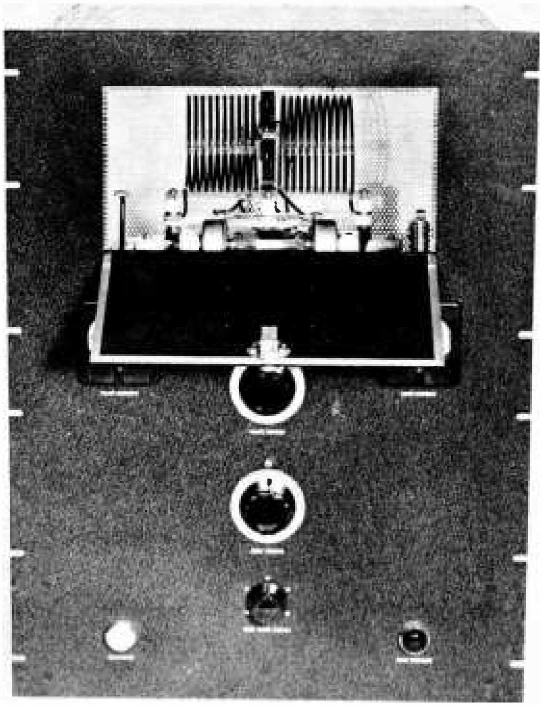


Figure 11
EIMAC FINGER STOCK IS USED TO LINE THE PANEL OPENING OF THE ONE-KILOWATT AMPLIFIER OF CHAPTER 26, SECTION 3

tact finger stock manufactured by Eitel-McCullough, Inc. of San Bruno, Calif. Eimac finger stock is an excellent means of providing good contact continuity when using components with adjustable or moving contact surfaces, or in acting as electrical "weather-strip" around access doors in enclosures. The access port of the 1-kilowatt amplifier of Chapter 26, Section 3 is lined with this material (figure 11). Harmonic leakage through such a sealed opening is reduced to a negligible level. The mating surface to the finger stock should be free of paint, and should provide a good electrical connection to the stock.

A second method of re-establishing electrical continuity across an access port is to employ Metex shielding around the mating edges of the opening. Metex is a flexible, knitted wire mesh which may be obtained in various sizes and shapes. This r-f gasket material is produced by Metal Textile Corp., Roselle, N. J. Metex is both flexible and resilient and conforms to irregularities in mating surfaces with a minimum of closing pressure.

30-5 Summation of the Problem

The creation of r-f energy is accompanied by harmonic generation and leakage of fundamental and harmonic energy from the generator source. For practical purposes, radio frequency power may be considered as a form of both electrical and r-f energy. As electrical energy, it will travel along any convenient conductor. As r-f energy, it will radiate directly from the source or from any conductor connected to the source. In view of this "dual personality" of r-f emanations, there is no panacea for all forms of r-f energy leakage. The cure involves both filtering and shielding: one to block the paths of conducted energy, the other to prevent the leakage of radiated energy. The proper combination of filtering and shielding can reduce the radiation of harmonic energy from a signal source some 80 decibels. In most cases, this is sufficient to eliminate interference caused by the generation of undesirable harmonics.

30-6 Construction Practice

Chassis Layout The chassis first should be covered with a layer of wrapping paper, which is drawn tightly down on all sides and fastened with scotch tape. This allows any number of measurement lines and hole centers to be spotted in the correct positions without making any marks on the chassis itself. Place on it the parts to be mounted and play a game of chess with them, trying different arrangements until all the grid and plate leads are made as short as possible, tubes are clear of coil fields, r-f chokes are in safe positions, etc. Remember, especially if you are going to use a panel, that a good mechanical layout often can accompany sound electrical design, but that the electrical design should be given first consideration.

All too often parts are grouped to give a symmetrical panel, irrespective of the arrangement behind. When a satisfactory arrangement has been reached, the mounting holes may be marked. The same procedure now must be followed for the underside, always being careful to see that there are no clashes between the two (that no top mounting screws come down into the middle of a paper capacitor on the underside, that the variable capacitor rotors do not hit anything when turned, etc.).

When all the holes have been spotted, they should be center-punched *through* the paper into the chassis. Don't forget to spot holes for leads which must also come through the chassis.

For transformers which have lugs on the bottoms, the clearance holes may be spotted by pressing the transformer on a piece of paper to obtain impressions, which may then be transferred to the chassis.

Punching In cutting socket holes, one can use either a fly-cutter or socket punches. These punches are easy to operate and only a few precautions are necessary. The guide pin should fit snugly in the guide hole. This increases the accuracy of location of the socket. If this is not of great importance, one may well use a drill of 1/32 inch larger diameter than the guide pin. Some of the punches will operate without guide holes, but the latter always make the punching operations simpler and easier. The only other precaution is to be sure the work is properly lined up before applying the hammer. If this is not done, the punch may slide sideways when you strike and thus not only shear the chassis but also take off part of the die. This is easily avoided by always making sure that the piece is parallel to the faces of the punch, the die, and the base. The latter should be an anvil or other solid base of heavy material.

A punch by *Greenlee* forces socket holes through the chassis by means of a screw turned with a wrench. It is noiseless, and works much more easily and accurately than most others.

The male part of the punch should be placed

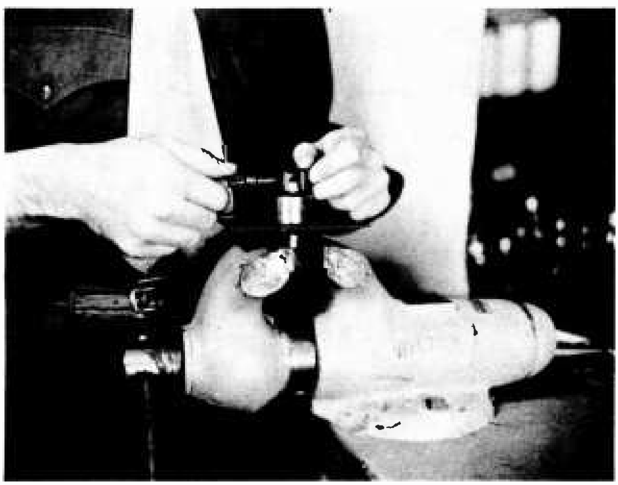
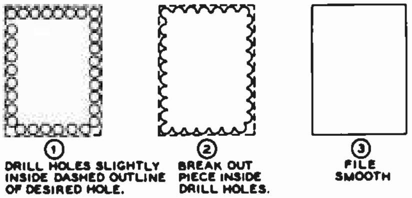


Figure 12
PROPER METHOD OF USING A SOCKET PUNCH OF THE "GREENLEE" TYPE



MAKING RECTANGULAR CUTOUT

Figure 13

in the vise, cutting edge up and the female portion forced against the metal with a wrench as in figure 12. These punches can be obtained in sizes to accommodate all tube sockets and even large enough to be used for meter holes. In the octal socket sizes they require the use of a 3/8 inch center hole to accommodate the bolt.

Transformer Cutouts Cutouts for transformers and chokes are not so simply handled. After marking off the part to be cut, drill about a ¼-inch hole on each of the inside corners and tangential to the edges. After burring the holes, clamp the piece and a block of cast iron or steel in the vise. Then, take your burring chisel and insert it in one of the corner holes. Cut out the metal by hitting the chisel with a hammer. The blows should be light and numerous. The chisel acts against the block in the same way that the two blades of a pair of scissors work against each other. This same process is repeated for the other sides. A file is used to trim up the completed cutout.

Another method is to drill the four corner holes large enough to take a hack saw blade, then saw instead of chisel. The four holes permit nice looking corners.

Still another method is shown in figure 13. When heavy panel steel is used and a drill press or electric drill is available, this is the most satisfactory method.

Removing Burrs In both drilling and punching, a burr is usually left on the work. There are three simple ways of removing these. Perhaps the best is to take a chisel (be sure it is one for use on metal) and set it so that its bottom face is parallel to the piece. Then gently tap it with a hammer. This usually will make a clean job with a little practice. If one has access to a counterbore, this will also do a nice job. A countersink will work, although it bevels the edges. A drill of several sizes larger is a much used arrangement. The third method is by filing off the burr, which does a good job but scratches the adjacent metal surfaces badly.

Mounting Components There are two methods in general use for the fastening of transformers, chokes, and similar pieces of apparatus to chassis or breadboards. The first, using nuts and machine screws, is slow, and the commercial manufacturing practice of using self-tapping screws is gaining favor. For the mounting of small parts such as resistors and capacitors, "tie points" are very useful to gain rigidity. They also contribute materially to the appearance of finished apparatus.

Rubber grommets of the proper size, placed in all chassis holes through which wires are to be passed, will give a neater appearing job and also will reduce the possibility of short circuits.

Soldering Making a strong, low-resistance solder joint does not mean just dropping a blob of solder on the two parts to be joined and then hoping that they'll stick. There are several definite rules that *must* be observed.

All parts to be soldered must be absolutely clean. To clean a wire, lug, or whatever it may be, take your pocket knife and scrape it thoroughly, until fresh metal is laid bare. It is not enough to make a few streaks; scrape until the part to be soldered is bright.

Make a good mechanical joint before applying any solder. Solder is intended primarily to make a good *electrical* connection; mechanical rigidity should be obtained by bending the wire into a small hook at the end and nipping it firmly around the other part, so that it will hold well even before the solder is applied.

Keep your iron properly tinned. It is impossible to get the work hot enough to take the solder properly if the iron is dirty. To tin your iron, file it, while hot, on one side until a full surface of clean metal is exposed. Immediately apply rosin core solder until a thin layer flows completely over the exposed surface. Repeat for the other faces. Then take a clean rag and wipe off all excess solder and rosin. The iron should also be wiped frequently while the actual construction is going on; it helps prevent pitting the tip.

Apply the solder to the work, not to the iron. The iron should be held against the parts to be joined until they are thoroughly heated. The solder should then be applied against the parts, and the iron should be held in place until the solder flows smoothly and envelops the work. If it acts like water on a greasy plate, and forms a ball, the work is not sufficiently clean.

The completed joint must be held perfectly still until the solder has had time to solidify. If the work is moved before the solder has become *completely* solid, a "cold" joint will result. This can be identified immediately, because the solder will have a dull "white" appearance rather than one of shiny "silver." Such joints tend to be of high resistance, and will very likely have a bad effect upon a circuit. The cure is simple: merely reheat the joint and do the job correctly.

Wipe away all surplus flux when the joint has cooled if you are using a paste type flux. Be sure it is non-corrosive, and use it with plain (not rosin core) solder.

Finishes If the apparatus is constructed on a painted chassis (commonly available in black wrinkle and gray wrinkle), there is no need for application of a protective coating when the equipment is finished, assuming that you are careful not to scratch or mar the finish while drilling holes and mounting parts. However, many amateurs prefer to use unpainted (zinc or cadmium plated) chassis, because it is much simpler to make a chassis ground connection with this type of chassis. A thin coat of clear "linoleum" lacquer may be applied to the whole chassis after the wiring is completed to retard rusting. In localities near the sea coast it is a good idea to lacquer the various chassis cutouts even on a painted chassis, as rust will get a good start at these points unless the metal is protected where the drill or saw has exposed it. If too thick a coat is applied, the lacquer will tend to peel. It may be thinned with lacquer thinner to permit application of a light coat. A thin coat will adhere to any *clean* metal surface that is not too shiny.

An attractive dull gloss finish, almost velvety can be put on aluminum by sand-blasting it with a very weak blast and fine particles and then lacquering it. Soaking the aluminum in a solution of lye produces somewhat the same effect as a fine grain sand blast.

There are also several brands of dull gloss black enamels on the market which adhere well to metals and make a nice appearance. Air-drying wrinkle finishes are sometimes successful, but a bake job is usually far better. Wrinkle finishes, properly applied, are very durable and are pleasing to the eye. If you live in a large community, there is probably an enamelling concern which can wrinkle your work for you at a reasonable cost. A very attractive finish, for panels especially, is to spray a wrinkle finish with aluminum paint. In any painting operation (or plating, either, for that matter), the work should be very thoroughly cleaned of all greases and oils.

To protect brass from tarnish, thoroughly cleanse and remove the last trace of grease by the use of potash and water. The brass must be carefully rinsed with water and dried; but in doing it, care must be taken not to handle any portion with the bare hands or anything else that is greasy. Then lacquer.

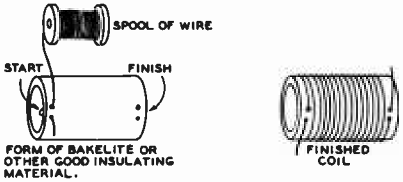
Drilling Glass This is done with a common drill by using a mixture of turpentine and camphor. When the point of the drill has come through, it should be taken out and the hole worked through with the point of a three-cornered file, having the edges ground sharp. Use the corners of the file, scraping the glass rather than using the file as a reamer. Great care must be taken not to crack the glass or flake off parts of it in finishing the hole after the point of the drill has come through. Use the mixture freely during the

NUMBERED DRILL SIZES

DRILL NUMBER	Diameter (In.)	Clears Screw	Correct for Tapping Steel or Brass†
1	.228	—	—
2	.221	12-24	—
3	.213	—	14-24
4	.209	12-20	—
5	.205	—	—
6	.204	—	—
7	.201	—	—
8	.199	—	—
9	.196	—	—
10*	.193	10-32	—
11	.191	10-24	—
12*	.189	—	—
13	.185	—	—
14	.182	—	—
15	.180	—	—
16	.177	—	12-24
17	.173	—	—
18*	.169	8-32	—
19	.166	—	12-20
20	.161	—	—
21*	.159	—	10-32
22	.157	—	—
23	.154	—	—
24	.152	—	—
25*	.149	—	10-24
26	.147	—	—
27	.144	—	—
28*	.140	6-32	—
29*	.136	—	8-32
30	.128	—	—
31	.120	—	—
32	.116	—	—
33*	.113	4-36 4-40	—
34	.111	—	—
35*	.110	—	6-32
36	.106	—	—
37	.104	—	—
38	.102	—	—
39*	.100	3-48	—
40	.098	—	—
41	.096	—	—
42*	.093	—	4-36 4-40
43	.089	2-56	—
44	.086	—	—
45*	.082	—	3-48

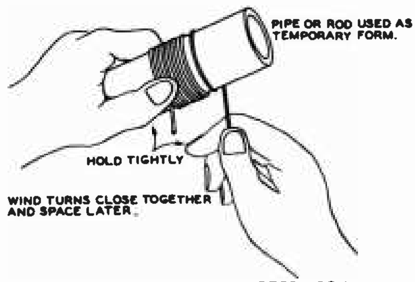
†Use next size larger drill for tapping bakelite and similar composition materials (plastics, etc.).

*Sizes most commonly used in radio construction.



WINDING COIL ON INSULATING FORM

Figure 14



WINDING "AIR-SUPPORTED" COIL

Figure 15

drilling and scraping. The above mixture will also be found useful in drilling hard cast iron. Drilling glass must be done very slowly. It is a good idea to practice by drilling several holes in scrap glass before tackling the actual piece to be drilled, to acquire the knack.

Etching Solution Add three parts nitric acid to one part muriatic acid. Cover the piece to be etched with beeswax. This can be done by heating the piece in a gas or alcohol flame and rubbing the wax over the surface. Use a sharp steel point or hard lead pencil point as a stylus. A pointed glass dropper can be used to put the solution at the place needed. After the solution foams for two or three minutes, remove with blotting paper and put oil on the piece, and then heat and remove the wax.

Chromium Polish So much chromium is now used in radio sets and on panels that it is well to know that this finish may be polished. The only materials required are absorbent cotton or soft cloth, alcohol, and ordinary lampblack.

A wad of cotton or the cloth is moistened in the alcohol and pressed into the lampblack. The chromium is then polished by rubbing the lampblack adhering to the cotton briskly over its surface. The mixture dries almost instantly and may be wiped off with another wad of cotton.

The alcohol serves merely to moisten the lampblack to a paste and make it stick to the cotton. The mixture cleans and polishes very quickly and cannot scratch the chromium surface. It polishes nickel-work just as effectively as it does chromium. Care should be taken to see that the lampblack does not contain any hard, gritty particles which might produce scratching during the polishing.

Winding Coils Coils are of two general types, those using a form and "air-wound" types. Neither type offers any particular constructional difficulties. Figure 14 illustrates the procedure used in form winding a coil. If the winding is to be spaced, the spacing can be done either by eye or a string or another piece of wire may be wound simultaneously with the coil wire and removed after the winding is in place. The usual procedure is to clamp one end of the wire in a vise, attaching the other end to the coil form and with the coil form in hand, walk slowly towards the vise winding the wire but at the same time keeping a strong tension on the wire as the form is rotated. After the coil is wound, if there is any possibility of the turns slipping, the completed coil is either entirely coated with a coil or Duco cement or cemented in those spots where slippage might occur.

V-h-f and u-h-f coils are commonly wound of heavy enameled wire on a form and then removed from the form as in figure 15. If the coil is long or has a tendency to buckle, strips of polystyrene or a similar material may be cemented longitudinally inside the coil. Due allowance must be made for the coil springing out when removed from the form, when selecting the diameter of the form.

On air wound coils of this type, spacing between turns is accomplished after removal from the form, by running a pencil, the shank of a screwdriver or other round object spirally between the turns from one end of the coil to the other, again making due allowance for spring.

Air-wound coils approaching the appearance of commercially manufactured ones, can be constructed by using a round wooden form which has been sawed diagonally from end to end. Strips of insulating material are temporarily attached to this mandrel, the wire then being wound over these strips with the desired separation between turns and cemented to the strips. When dry, the split mandrel may be removed by unwedging it.

CHAPTER THIRTY

Test Equipment

All amateur stations are required by law to have certain items of test equipment available within the station. A c-w station is required to have a frequency meter or other means in addition to the transmitter frequency control for insuring that the transmitted signal is on a frequency within one of the frequency bands assigned for such use. A radiophone station is required in addition to have a means of determining that the transmitter is not being modulated in excess of its modulation capability, and in any event not more than 100 per cent. Further, any station operating with a power input greater than 900 watts is required to have a means of determining the exact input to the final stage of the transmitter, so as to insure that the power input to the plate circuit of the output stage does not exceed 1000 watts.

The additional test and measurement equipment required by a station will be determined by the type of operation contemplated. It is desirable that all stations have an accurately calibrated volt-ohmmeter for routine transmitter and receiver checking and as an assistance in getting new pieces of equipment into operation. An oscilloscope and an audio oscillator make a very desirable adjunct to a phone station using AM or FM transmission, and are a necessity if single-sideband operation is contemplated. A calibrated signal generator is almost a necessity if much receiver work is contemplated, although a frequency meter of LM or BC-221 type, particularly if it includes internal modulation, will serve in place of the signal generator. Extensive antenna work invariably requires the use of some type of field-strength meter, and a standing-wave meter of some type is very helpful. Lastly, if much v-h-f work is to be done, a simple grid-dip meter will be found to be one of the most used items of test equipment in the station.

31-1 Voltage, Current and Power

The measurement of voltage and current in radio circuits is very important in proper maintenance of equipment. Vacuum tubes of the types used in communications work must be operated within rather narrow limits in regard to filament or heater voltage, and they must be operated within certain maximum limits in regard to the voltage and current on other electrodes.

Both direct current and voltage are most commonly measured with the aid of an instrument consisting of a coil that is free to rotate in a constant magnetic field (d'Arsonval type instrument). If the instrument is to be used for the measurement of current it is called an ammeter or milliammeter. The current flowing through the circuit is caused to flow through the moving coil of this type of instrument. If the current to be measured is greater than 10 milliamperes or so it is the usual practice to cause the majority of the current to flow through a by-pass resistor called a shunt, only a specified portion of the current flowing through the moving coil of the instrument. The calculation of shunts for extending the range of d-c milliammeters and ammeters is discussed in Chapter Two.

A direct current voltmeter is merely a d-c milliammeter with a *multiplier* resistor in series with it. If it is desired to use a low-range milliammeter as a voltmeter the value to the multiplier resistor for any voltage range may be determined from the following formula:

$$R = \frac{1000\ \ E}{I}$$

where: R = multiplier resistor in ohms
E = desired full scale voltage
I = full scale current of meter in ma.

The sensitivity of a voltmeter is commonly expressed in *ohms per volt.* The higher the ohms per volt of a voltmeter the greater its sensitivity. When the full-scale current drain of a voltmeter is known, its sensitivity rating in ohms per volt may be determined by:

$$\text{Ohms per volt} = \frac{1000}{I}$$

Where I is the full-scale current drain of the indicating instrument in milliamperes.

Multi-Range Meters It is common practice to connect a group of multiplier resistors in the circuit with a single indicating instrument to obtain a *multi-range voltmeter.* There are several ways of wiring such a meter, the most common ones of which are indicated in figure 1. With all these methods of connection, the sensitivity of the meter in ohms per volt is the same on all scales. With a 0-1 milliammeter as shown the sensitivity is 1000 ohms per volt.

Volt-Ohmmeters An extremely useful piece of test equipment which should be found in every laboratory or radio station is the *volt-ohmmeter.* It consists of a multi-range voltmeter with an additional fixed resistor, a variable resistor, and a battery. A typical example of such an instrument is diagrammed in figure 2. Tap 1 is used to permit use of the instrument as an 0-1 d-c milliammeter. Tap 2 permits accurate reading of resistors up to 100,000 ohms; taps 3, 4, 5, and 6 are for making voltage measurements, the full scale voltages being 10, 50, 250, and 500 volts respectively.

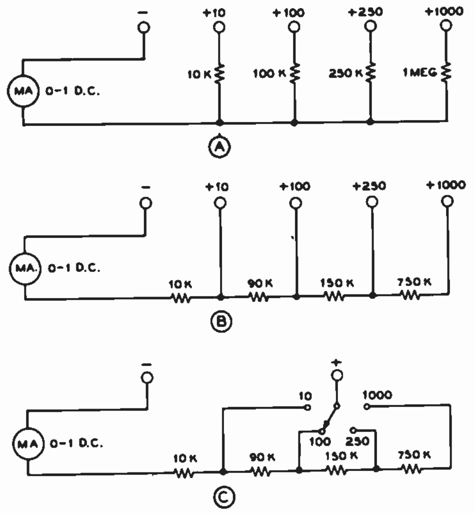


Figure 1

MULTI-VOLTMETER CIRCUITS

(A) shows a circuit whereby individual multiplier resistors are used for each range. (B) is the more economical "series multiplier" circuit. The same number of resistors is required, but those for the higher ranges have less resistance, and hence are less expensive when precision wirewound resistors are to be used. (C) shows a circuit essentially the same as at (A), except that a range switch is used. With a 0-500 d-c microammeter substituted for the 0-1 milliammeter shown above, all resistor values would be multiplied by two and the voltmeter would have a "2000-ohm-per-volt" sensitivity. Similarly, if a 0-50 d-c microammeter were to be used, all resistance values would be multiplied by twenty, and the voltmeter would have a sensitivity of 20,000 ohms per volt.

The 1000-ohm potentiometer is used to bring the needle to zero ohms when the terminals are shorted; this adjustment should always be made before a resistance measurement is taken. Higher voltages than 500 can be read if a higher value of multiplier resistor is added to an additional tap on the switch. The proper value for a given full scale reading can be determined from Ohm's law.

Resistances higher than 100,000 ohms cannot be measured accurately with the circuit constants shown; however, by increasing the ohmmeter battery to 45 volts and multiplying the 4000-ohm resistor and 1000-ohm potentiometer by 10, the ohms scale also will be mul-

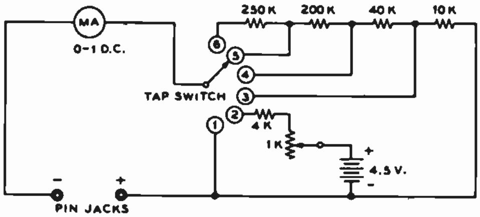


Figure 2
VOLT-OHMMETER CIRCUIT

With the switch in position 1, the 0-1 milliammeter would be connected directly to the terminals. In position 2 the meter would read from 0-100,000 ohms, approximately, with a resistance value of 4500 ohms at half scale. (Note: The half-scale resistance value of an ohmmeter using this circuit is equal to the resistance in series with the battery inside the instrument.) The other four taps are voltage ranges with 10, 50, 250, and 500 volts full scale.

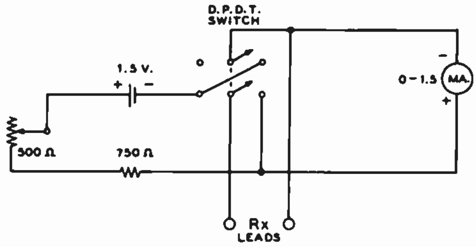


Figure 3
SCHEMATIC OF A LOW-RANGE OHMMETER

A description of the operation of this circuit is given in the text. With the switch in the left position the half-scale reading of the meter will occur with an external resistance of 1000 ohms. With the switch in the right position, half-scale deflection will be obtained with an external resistance equal to the d-c resistance of the milliammeter (20 to 50 ohms depending upon the make of instrument).

tiplied by 10. This would permit accurate measurements up to 1 megohm.

0-1 d-c milliammeters are available with special volt-ohmmeter scales which make individual calibration unnecessary. Or, special scales can be purchased separately and substituted for the original scale on the milliammeter.

Obviously, the accuracy of the instrument either as a voltmeter or as an ammeter can be no better than the accuracy of the milliammeter and the resistors.

Because volt-ohmmeters are so widely used and because the circuit is standardized to a considerable extent, it is possible to purchase a factory-built volt-ohmmeter for no more than the component parts would cost if purchased individually. For this reason no construction details are given. However, anyone already possessing a suitable milliammeter and desirous of incorporating it in a simple volt-ohmmeter should be able to build one from the schematic diagram and design data given here. Special, precision (accurately calibrated) multiplier resistors are available if a high degree of accuracy is desired. Alternatively, good quality carbon resistors whose actual resistance has been checked may be used as multipliers where less accuracy is required.

Medium- and Low-Range Ohmmeter Most ohmmeters, including the one just described, are not adapted for accurate measurement of low resistances—in the neighborhood of 100 ohms, for instance.

The ohmmeter diagrammed in figure 3 was especially designed for the reasonably accurate reading of resistances down to 1 ohm. Two scales are provided, one going in one direction and the other scale going in the other direction because of the different manner in which the milliammeter is used in each case. The low scale covers from 1 to 100 ohms and the high scale from 100 to 10,000 ohms. The high scale is in reality a medium-range scale. For accurate reading of resistances over 10,000 ohms, an ohmmeter of the type previously described should be used.

The 1-100 ohm scale is useful for checking transformers, chokes, r-f coils, etc., which often have a resistance of only a few ohms.

The calibration scale will depend upon the internal resistance of the particular make of 1.5-ma. meter used. The instrument can be calibrated by means of a Wheatstone bridge or a few resistors of known accuracy. The latter can be series-connected and parallel-connected to give sufficient calibration points. A hand-drawn hand-calibrated scale can be cemented over the regular meter scale to give a direct reading in ohms.

Before calibrating the instrument or using it, the test prods should always be touched together and the zero adjuster set accurately.

Measurement of Alternating Current and Voltage The measurement of alternating current and voltage is complicated by two factors; first, the frequency range covered in ordinary communication channels is so great that calibration of an instrument becomes extremely difficult; second, there is no single type of instrument which is suitable for all a-c measurements—as the d'Arsonval type of movement is suitable for d-c. The d'Arsonval movement will not operate on a-c since it indicates the average value of current flow, and the average value of an a-c wave is zero.

As a result of the inability of the reliable d'Arsonval type of movement to record an alternating current, either this current must be rectified and then fed to the movement, or a special type of movement which will operate from the *effective* value of the current can be used.

For the usual measurements of power frequency a.c. (25-60 cycles) the *iron-vane* instrument is commonly used. For audio frequency a.c. (50-20,000 cycles) a d'Arsonval instrument having an integral copper oxide or selenium rectifier is usually used. Radio frequency voltage measurements are usually made with some type of vacuum-tube voltmeter, while r-f current measurements are almost invariably made with an instrument containing a thermocouple to convert the r.f. into d.c. for the movement.

Since an alternating current wave can have an almost infinite variety of shapes, it can easily be seen that the ratios between the three fundamental quantities of the wave (peak, r.m.s. effective, and average after rectification) can also vary widely. So it becomes necessary to know beforehand just which quality of the wave under measurement our instrument is going to indicate. For the purpose of simplicity we can list the usual types of a-c meters in a table along with the characteristic of an a-c wave which they will indicate:

Iron-vane, thermocouple—r.m.s.

Rectifier type (copper oxide or selenium) —average after rectification.

V.t.v.m.—r.m.s., average or peak, depending upon design and calibration.

Vacuum-Tube Voltmeters A *vacuum-tube voltmeter* is essentially a detector in which a change in the signal placed upon the input will produce a change in the indicating instrument (usually a d'Arsonval meter) placed in the output circuit. A vacuum-tube voltmeter may use a diode, a triode, or a multielement tube, and it may be used either for the measurement of a.c. or d.c.

When a v.t.v.m. is used in d-c measurement it is used for this purpose primarily because of the very great input resistance of the device. This means that a v.t.v.m. may be used for the measurement of a-v-c, a-f-c, and discriminator output voltages where no loading of the circuit can be tolerated.

A-C V-T Voltmeters There are many different types of a-c vacuum-tube voltmeters, all of which operate as some type of rectifier to give an indication on a d-c instrument. There are two general types; those which give an indication of the r-m-s value of the wave (or approximately this value of a complex wave), and those which give an indication of the peak or crest value of the wave.

Since the setting up and calibration of a wide-range vacuum-tube voltmeter is rather tedious, in most cases it will be best to purchase a commercially manufactured unit. Several excellent commercial units are on the market at the present time; also, kits for home construction of a quite satisfactory v.t.v.m. are available from several manufacturers. These feature a wide range of a-c and d-c voltage scales at high sensitivity, and in addition several feature a built-in vacuum-tube ohmmeter which will give indications up to 500 or 1000 megohms.

Peak A-C V-T Voltmeters There are two common types of peak-indicating vacuum-tube voltmeters. The first is the so-called *slide-back* type in which a simple v.t.v.m is used along with a conventional d-c voltmeter and a source of bucking bias in series with the input. With this type of arrangement (figure 4) leads are connected to the voltage to be measured and the slider resistor R across the bucking voltage is backed down until an indication on the meter (called a false zero) equal to that value given with the prods shorted and the bucking voltage reduced to zero is obtained. Then the value of the bucking voltage (read on V) is equal to the peak value of the voltage under measurement. The slide-back voltmeter has the disadvantage that it is not instantaneous in its indication—adjustments must be made for every voltage measurement. For this reason the slide-back v.t.v.m is not commonly used, being supplanted by the diode-rectifier type of peak v.t.v.m for most applications.

High-Voltage Diode Peak Voltmeter A diode vacuum-tube voltmeter suitable for the measurement of high values of a-c voltage is diagrammed in figure 5. With the constant shown, the voltmeter has two ranges: 500 and 1500 volts *peak* full scale.

Capacitors C_1 and C_2 should be able to withstand a voltage in excess of the highest peak voltage to be measured. Likewise, R_1 and R_2 should be able to withstand the same amount of voltage. The easiest and least expensive

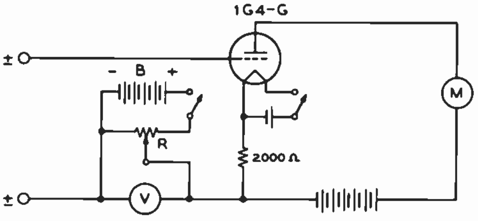


Figure 4
SLIDE-BACK V-T VOLTMETER

By connecting a variable source of voltage in series with the input to a conventional v-t voltmeter, or in series with the simple triode voltmeter shown above, a slide-back a-c voltmeter for peak voltage measurement can be constructed. Resistor R should be about 1000 ohms per volt used at battery B. This type of v-t voltmeter has the advantage that it can give a reading of the actual peak voltage of the wave being measured, without any current drain from the source of voltage.

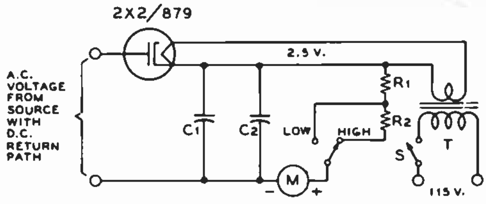


Figure 5
SCHEMATIC OF A HIGH-VOLTAGE PEAK VOLTMETER

A peak voltmeter such as diagrammed above is convenient for the measurement of peak voltages at fairly high power levels from a source of moderately low impedance.

C_1—.001-μfd. high-voltage mica
C_2—1.0μfd. high-voltage paper
R_1—500,000 ohms (two 0.25-megohm ½-watt in series)
R_2—1.0 megohm (four 0.25-megohm ½-watt in series)
T—2.5 v., 1.75 a. filament transformer
M—0-1 d-c milliammeter
S_{HI-LO}—S-p-d-t toggle switch
S—S-p-s-t toggle switch
(Note: C_1 is a by-pass around C_2, the inductive reactance of which may be appreciable at high frequencies.)

way of obtaining such resistors is to use several low-voltage resistors in series, as shown in figure 5. Other voltage ranges can be obtained by changing the value of these resistors, but for voltages less than several hundred volts a more linear calibration can be obtained by using a receiving-type diode. A calibration curve should be run to eliminate the appreciable error due to the high internal resistance of the diode, preventing the capacitor from charging to the full peak value of the voltage being measured.

A direct reading diode peak voltmeter of the type shown in figure 5 will load the source of voltage by approximately *one-half* the value of the load resistance in the circuit (R_1, or R_1 plus R_2, in this case). Also, the peak voltage reading on the meter will be slightly less than the actual peak voltage being measured. The amount of lowering of the reading is determined by the ratio of the reactance of the storage capacitance to the load resistance. If a cathode-ray oscilloscope is placed across the terminals of the v.t.v.m when a voltage is being measured, the actual amount of the lowering in voltage may be determined by inspection of the trace on the c-r tube screen. The peak positive excursion of the wave will be slightly flattened by the action of the v.t.v.m. Usually this flattening will be so small as to be negligible.

An alternative arrangement, shown in figure 6, is quite convenient for the measurement of high a-c voltages such as are encountered in the adjustment and testing of high-power audio amplifiers and modulators. The arrangement consists simply of a 2X2 rectifier tube and a filter capacitor of perhaps 0.25-μfd. capacitance, but with a voltage rating high enough that it is not likely to be punctured as a result of any tests made. Cathode-ray oscilloscope capacitors, and those for electrostatic-deflection TV tubes often have ratings as high as 0.25 μfd. at 7500 to 10,000 volts. The indicating instrument is a conventional multi-scale d-c voltmeter of the high-sensitivity type, preferably with a sensitivity of 20,000 or 50,000 ohms per volt. The higher the sensitivity of the d-c voltmeter used with the rectifier, the smaller will be the amount of flattening of the a-c wave as a result of the rectifier action.

Measurement of Power Audio frequency or radio frequency power in a resistive circuit is most commonly and most easily determined by the indirect method, i.e., through the use of one of the following formulas:

$$P = EI \qquad P = E^2/R \qquad P = I^2R$$

These three formulas mean that if any two of

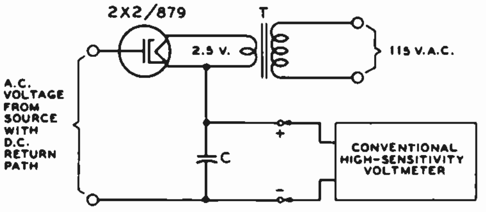


Figure 6
PEAK-VOLTAGE MEASUREMENT CIRCUIT

Through use of the arrangement shown above it is possible to make accurate measurements of peak a-c voltages, such as across the secondary of a modulation transformer, with a conventional d-c multi-voltmeter. Capacitor C and transformer T should, of course, be insulated for the highest peak voltage likely to be encountered. A capacitance of 0.25-μfd. at C has been found to be adequate. The higher the sensitivity of the indicating d-c voltmeter, the smaller will be the error between the indication on the meter and the actual peak voltage being measured.

the three factors determining power are known (resistance, current, voltage) the power being dissipated may be determined. In an ordinary 120-volt a-c line circuit the above formulas are not strictly true since the power factor of the load must be multiplied into the result—or a direct method of determining power such as a wattmeter may be used. But in a resistive a-f circuit and in a resonant r-f circuit the power factor of the load is taken as being unity.

For accurate measurement of a-f and r-f power, a *thermogalvanometer* or *thermocouple* ammeter in series with a non-inductive resistor of known resistance can be used. The meter should have good accuracy, and the exact value of resistance should be known with accuracy. Suitable dummy load resistors are available in various resistances in both 100 and 250-watt ratings. These are virtually non-inductive, and may be considered as a pure resistance up to 30 Mc. The resistance of these units is substantially constant for all values of current up to the maximum dissipation rating, but where extreme accuracy is required, a correction chart of the dissipation coefficient of resistance (supplied by the manufacturer) may be employed. This chart shows the exact resistance for different values of current through the resistor.

Sine-wave power measurements (r-f or single-frequency audio) may also be made through the use of a v.t.v.m and a resistor of known value. In fact a v.t.v.m of the type shown in figure 6 is particularly suited to this work. The formula, $P = E^2/R$ is used in this case. However, it must be remembered that a v.t.v.m of the type shown in figure 6 indicates the *peak* value of the a-c wave. This reading must be converted to the r-m-s or *heating* value of the wave by multiplying it by 0.707 before substituting the voltage value in the formula. The same result can be obtained by using the formula $P = E^2/2R$.

Thus all three methods of determining power: ammeter-resistor, voltmeter-resistor, and voltmeter-ammeter, give an excellent cross-check upon the accuracy of the determination and upon the accuracy of the *standards*.

Power may also be measured through the use of a calorimeter, by actually measuring the amount of heat being dissipated. Through the use of a water-cooled dummy load resistor this method of power output determination is being used by some of the most modern broadcast stations. But the method is too cumbersome for ordinary power determinations.

Power may also be determined photometrically through the use of a voltmeter, ammeter, incandescent lamp used as a load resistor, and a photographic exposure meter. With this method the exposure meter is used to determine the relative visual output of the lamp running as a dummy load resistor and of the lamp running from the 120-volt a-c line. A rheostat in series with the lead from the a-c line to the lamp is used to vary its light intensity to the same value (as indicated by the exposure meter) as it was putting out as a dummy load. The a-c voltmeter in parallel with the lamp and ammeter in series with it is then used to determine lamp power input by: $P = EI$. This method of power determination is satisfactory for audio and low frequency r.f. but is not satisfactory for v-h-f work because of variations in lamp efficiency due to uneven heating of the filament.

Dummy Loads Lamp bulbs make poor dummy loads for r-f work, in general, as they have considerable reactance above 2 Mc., and the resistance of the lamp varies with the amount of current passing through it.

A suitable r-f load for powers up to a few watts may be made by paralleling 2-watt composition resistors of suitable value to make a 50-ohm resistor of 5 or 10 watts dissipation. The resistors should be mounted in a compact bundle, with short interconnecting leads.

For powers of 100 and 250 watts, the Ohmite models D-101 and D-251 low inductance resistors may be used as dummy antennas. A D-101

Figure 7
100-WATT DUMMY LOAD SUITABLE FOR VIKING II, OR SIMILAR TYPE TRANSMITTER

resistor mounted on a small metal chassis, with a r-f ammeter and coaxial plug is shown in figure 7. A unit such as this may be used with transmitters of the Viking II and Collins 32V power rating. The Ohmite D-250 resistor may be employed in such a configuration for higher power.

A dummy load capable of taking the output of a plate-modulated 1-kilowatt transmitter is shown in figure 8. The load is made up of ten 160-watt, 500-ohm Ohmite type 2409 non-inductive resistors. These resistors are mounted between two aluminum end plates measuring 4 inches in diameter. The assembly is then end mounted by means of 1" ceramic insulators to an aluminum chassis containing the r-f ammeter and an SO-239 coaxial receptacle.

This dummy load presents a good approximation of a 50-ohm, 1600-watt resistor up to approximately 8 Mc. Above this frequency, it becomes increasingly reactive. It may be used up to 30 Mc., if it is remembered that the reading of the r-f ammeter no longer is an absolute indication of the resistive power dissipation of the load. For use on the 20, 15 and 10 meter bands, it is recommended that the coaxial line coupling the dummy load to the transmitter either be restricted to a length of two feet or less, or else be made an electrical half-wavelength long. This will insure that a minimum of reactance will be coupled back into the transmitter. The schematic of this dummy load is shown in figure 9.

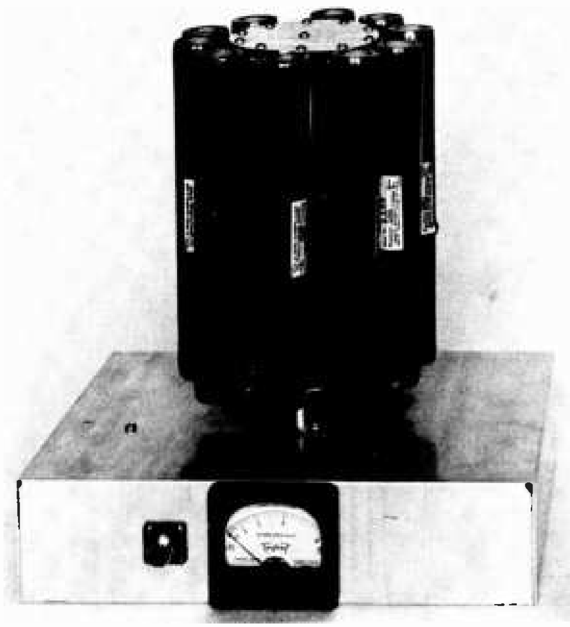
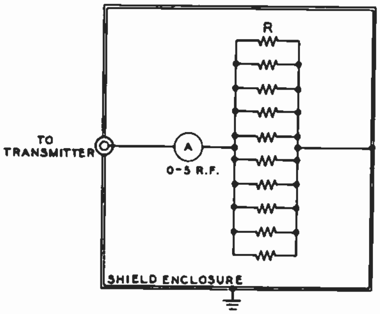


Figure 8
1600-WATT DUMMY LOAD, WITH ENCLOSURE REMOVED



R — TEN 500-OHM, 160-WATT NON-INDUCTIVE RESISTORS IN PARALLEL (*OHMITE 2409*)

Figure 9
1.6-KILOWATT DUMMY LOAD SCHEMATIC

31-2 Measurement of Circuit Constants

The measurement of the resistance, capacitance, inductance, and Q (figure of merit) of the components used in communications work can be divided into three general methods: the impedance method, the substitution or resonance method, and the bridge method.

The Impedance Method The impedance method of measuring inductance and capacitance can be likened to the ohmmeter method for measuring resistance. An a-c voltmeter, or milliammeter in series with a resistor, is connected in series with the inductance or capacitance to be measured and the a-c line. The reading of the meter will be inversely proportional to the impedance of the component being measured. After the meter has been calibrated it will be possible to obtain the approximate value of the impedance directly from the scale of the meter. If the component is a capacitor, the value of impedance may be taken as its reactance at the measurement frequency and the capacitance determined accordingly. But the d-c resistance of an inductor must also be taken into consideration in determining its inductance. After the d-c resistance and the impedance have been determined, the reactance may be determined from the formula: $X_L = \sqrt{Z^2-R^2}$. Then the inductance may be determined from: $L = X_L/2\pi f$.

The Substitution Method The substitution method is a satisfactory system for obtaining the inductance or capacitance of high-frequency components. A large variable capacitor with a good dial having an accurate calibration curve is a necessity for making determinations by this method. If an unknown inductor is to be measured, it is connected in parallel with the standard capacitor and the combination tuned accurately to some known frequency. This tuning may be accomplished either by using the tuned circuit as a wavemeter and coupling it to the tuned circuit of a reference oscillator, or by using the tuned circuit in the controlling position of a two terminal oscillator such as a dynatron or transitron. The capacitance required to tune this first frequency is then noted as C_1. The circuit or the oscillator is then tuned to the *second harmonic* of this first frequency and the amount of capacitance again noted, this time as C_2. Then the distributed capacitance across the coil (including all stray capacitances) is equal to: $C_0 = (C_1 - 4C_2)/3$.

This value of distributed capacitance is then substituted in the following formula along with the value of the standard capacitance for either of the two frequencies of measurement:

$$L = \frac{1}{4\pi^2 f_1^2 (C_1 + C_0)}$$

The determination of an unknown capacitance is somewhat less complicated than the above. A tuned circuit including a coil, the unknown capacitor and the standard capacitor, all in parallel, is resonated to some convenient frequency. The capacitance of the standard capacitor is noted. Then the unknown capacitor is removed and the circuit re-resonated by means of the standard capacitor. The difference between the two readings of the standard capacitor is then equal to the capacitance of the unknown capacitor.

31-3 Capacitance-Inductance Meter

A convenient instrument for the measurement of relatively small values of capacitance by the method just discussed is shown in figures 10, 11 and 12. The schematic diagram of the instrument is given in figure 13.

The device consists of a crystal oscillator operating in range between 3.5 and 4 Mc., with the output of the crystal oscillator inductively coupled to a separate tuned circuit. Resonance in the separate tuned circuit is indicated by a diode voltmeter using a crystal diode. Plate voltage for crystal oscillator is obtained from a small self-contained power supply using a type 6AL5 tube as a half-wave rectifier.

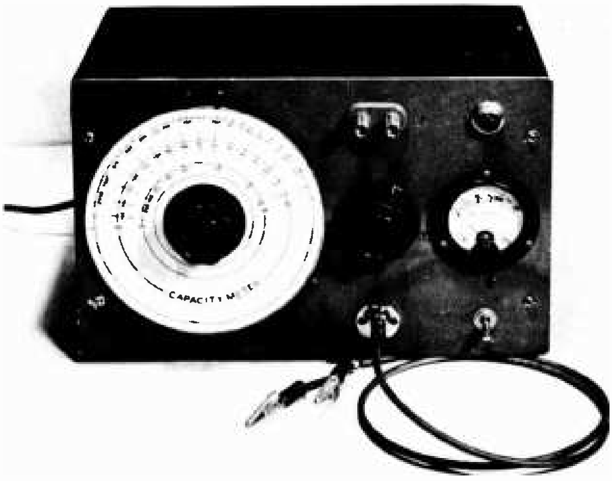


Figure 10
FRONT OF THE
CAPACITANCE METER

Measurement of Capacitance Referring to figure 13, it is seen that L_2 is resonated to the frequency of the crystal oscillator by capacitors C_2 and C_3 plus stray circuit capacitances. If C_3 has a capacitance range of 150 $\mu\mu$fd. (maximum capacitance minus minimum capacitance), any capacitance up to 150 $\mu\mu$fd. may be measured using the main tuning range of the instrument. The procedure is as follows: (1) C_3 is adjusted to maximum capacitance ("O" on the main dial); (2) the zero-set capacitor, C_2, then is adjusted for resonance as indicated by maximum deflection of the milliammeter; (3) the unknown capacitance then is placed across terminals "A"; and (4), C_3 is tuned until resonance in the tuned circuit is restored as indicated by maximum meter deflection. The amount by which C_3 is changed from its setting of maximum capacitance then is equal to the capacitance of the unknown capacitor which was placed at "A."

The capacitor used at C_3 should be of the straight-line-capacitance type with semi-circle plates so that the capacitance calibration on the main dial scale will be linear with rotation. For moderate accuracy the main dial may be calibrated directly with a knowledge of the maximum and minimum capacitance of C_3. But when a more precise calibration of the instrument is desired, the main dial should be cali-

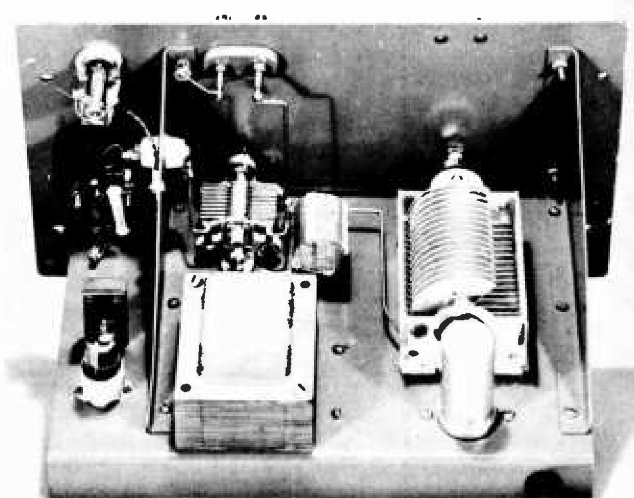


Figure 11
REAR VIEW OF THE
CAPACITANCE METER

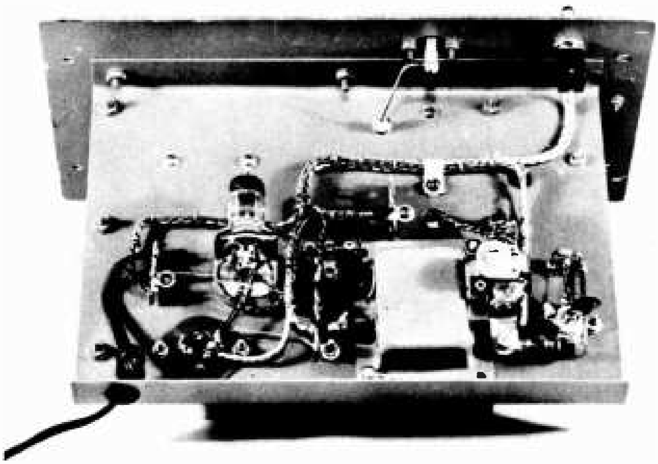


Figure 12
UNDER CHASSIS OF THE CAPACITANCE METER

brated by substituting known values of capacitance at "A."

Use of the Coaxial Lead It often is desirable to measure capacitors which are mounted in a circuit without mechanically removing them from the equipment. If one side of the capacitor is grounded and the other side is free, the capacitance may be measured with the aid of the coaxial lead shown in figure 10. The coaxial connector "B" on the panel of the instrument provides for connection of a two-foot length of RG-59/U cable which has been equipped with alligator clips on the free end. Coaxial cable of this type has a nominal capacitance of 21 μμfd. per foot, so approximately 45 μμfd. (including strays) must be removed from the circuit when the coaxial lead is to be used. This compensation is accomplished simply by changing the "zero set" capacitor, C_2, to restore resonance in the circuit when the coaxial lead is in use. The instrument then operates normally. However, when initially adjusting the inductance of L_2 at the chosen crystal frequency, the main capacitor C_3 must be at its maximum setting, and the "zero set" capacitor C_2 must be near its maximum setting, so that sufficient capacitance may be removed from the circuit to compensate for the added capacitance of the coaxial lead.

The High-Capacitance Scale The measuring range of the instrument may be increased by placing a known capacitance of 150 μμfd. in series with the unknown capacitor. The effective capacitance of the series combination will be:

$$C = \frac{150 \quad C_x}{C_x + 150}$$

or in terms of C_x:

$$C_x = \frac{150 \quad C}{150 - C}$$

remembering that C is the dial reading.

A new scale may be drawn on the dial for this type of measurement simply by choosing values of C and marking values of C_x opposite the basic calibration scale of the instrument. It should be noted that the scale of capacitance thus obtained is non-linear, and that readings above about 2000 μμfd. are not reliable due to compression of the scale.

Measurement of Inductance A limited range of inductance values may be measured through the following procedure: (1) Place the known 150-μμfd. fixed capacitor across terminals "A." (2) Adjust the main capacitance dial to resonance at its full-scale setting of 150 μμfd. (3) Place the unknown inductor also across terminals "A." (4) Readjust the main capacitance dial to resonance. Values of inductance between about 13 μh. and 200 μh. can be measured in this manner. The relationship between the value of the unknown inductance and the basic capacitance scale is:

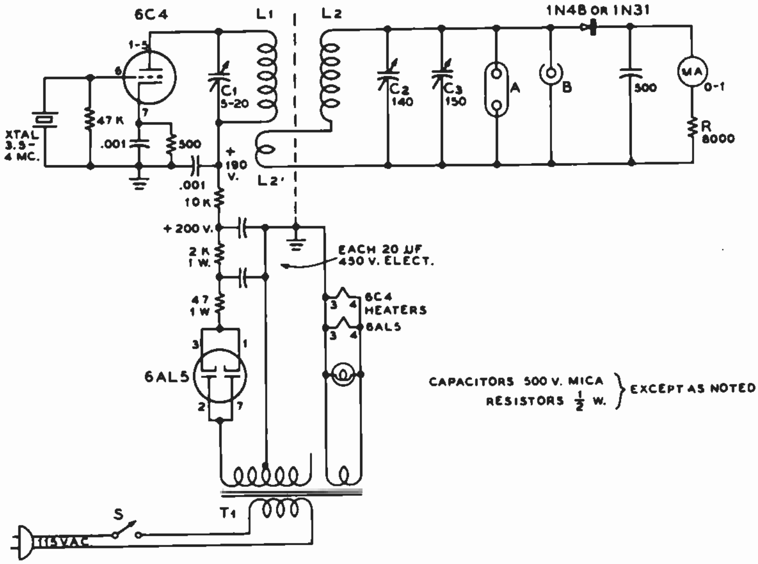


Figure 13
SCHEMATIC OF THE CAPACITANCE METER

C_1—5-20 $\mu\mu$fd. ceramic trimmer
C_2—140-$\mu\mu$fd. small variable
C_3—150 $\mu\mu$fd. capacitance range variable: removed from the output circuit of a 274N transmitter
L_1—100 t. no. 32 enam. closewound on 7/8-inch polystyrene rod
L_2—19 t. 1-inch dia. 16 turns per inch (B&W 3015 Miniductor)
L_2'—4-turn link around low-potential end of L_1
S—S.p.s.t. toggle a-c line switch
T_1—Small receiver power transformer; 420 v. c.t., 6.3 v. 2 a., and 5 v. 2 a. winding which is unused (Stancor P-6289)

$$L_x = \frac{1}{4\pi^2 f^2 C} = \frac{1}{39.5 f^2 C}$$

$$\text{or,} \quad C = \frac{1}{39.5 f^2 L_x}$$

Again, calibration of the dial scale may be made directly from the basic capacitance scale using the equations given above. Clearly the maximum inductance end of the scale will be infinity, with the high-inductance range squeezed; the minimum inductance will be that value which has an inductive reactance equal to the capacitive reactance of 150 $\mu\mu$fd. at the crystal frequency—the minimum inductance value is 13 μh. for the instrument illustrated.

The Resonance Indicator The diode-voltmeter resonance indicator is a relatively low impedance device. Hence the operating Q of the tuned circuit will be lowered by the shunting effect of the diode voltmeter. Since the overall Q of the measurement circuit thus is relatively low, the effective Q of the components being measured may vary through wide limits without appreciable effect on the voltage developed across the tuned circuit. Thus air capacitors, mica capacitors, and paper capacitors may be measured with equal facility. The proper series resistance for the diode voltmeter, R, can be found by trial. The value chosen for the unit illustrated gives about 3/4-scale deflection at resonance.

31-4 Measurements with a Bridge

Experience has shown that one of the most satisfactory methods for measuring circuit constants (resistance, capacitance, and induct-

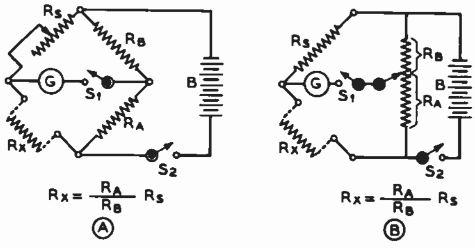


Figure 14

TWO WHEATSTONE BRIDGE CIRCUITS

These circuits are used for the measurement of d-c resistance. In (A) the "ratio arms" R_B and R_A are fixed and balancing of the bridge is accomplished by variation of the standard R_S. The standard in this case usually consists of a decade box giving resistance in 1-ohm steps from 0 to 1110 or to 11,110 ohms. In (B) a fixed standard is used for each range and the ratio arm is varied to obtain balance. A calibrated slide-wire or potentiometer calibrated by resistance in terms of degrees is usually employed as R_A and R_B. It will be noticed that the formula for determining the unknown resistance from the known is the same in either case.

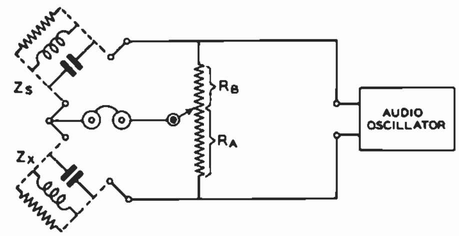
ance) at audio frequencies is by means of the a-c bridge. The *Wheatstone (d-c) bridge* is also one of the most accurate methods for the measurement of d-c resistance. With a simple bridge of the type shown at figure 14A it is entirely practical to obtain d-c resistance determinations accurate to four significant figures. With an a-c bridge operating within its normal rating as to frequency and range of measurement it is possible to obtain results accurate to three significant figures.

Both the a-c and the d-c bridges consist of a source of energy, a standard or reference of measurement, a means of balancing this standard against the unknown, and a means of indicating when this balance has been reached. The source of energy in the d-c bridge is a battery; the indicator is a sensitive galvanometer. In the a-c bridge the source of energy is an audio oscillator (usually in the vicinity of 1000 cycles), and the indicator is usually a pair of headphones. The standard for the d-c bridge is a resistance, usually in the form of a decade box. Standards for the a-c bridge can be resistance, capacitance, and inductance in varying forms.

Figure 14 shows two general types of the Wheatstone or d-c bridge. In (A) the so-called "ratio arms" R_A and R_B are fixed (usually in a ratio of 1-to-1, 1-to-10, 1-to-100, or 1-to-1,000) and the standard resistor R_S is varied until the bridge is in balance. In commercially manufactured bridges there are usually two or more buttons on the galvanometer for progressively increasing its sensitivity as balance is approached. Figure 14B is the *slide wire* type of bridge in which fixed standards are used and the ratio arm is continuously variable. The slide wire may actually consist of a moving contact along a length of wire of uniform cross section in which case the ratio of R_A to R_B may be read off directly in centimeters or inches, or in degrees of rotation if the slide wire is bent around a circular former. Alternatively, the slide wire may consist of linear-wound potentiometer with its dial calibrated in degrees or in resistance from each end.

Figure 15A shows a simple type of a-c bridge for the measurement of capacitance and inductance. It can also, if desired, be used for the measurement of resistance. The four arms of the bridge may be made up in a variety of ways. As before, R_B and R_A make up the ratio arms of the device and may be either of the slide wire type, as indicated, or they may be fixed and a variable standard used to obtain balance. In any case it is always necessary with this type of bridge to use a standard which presents the same type of impedance as the unknown being measured: resistance standard for a resistance measurement, capacitance standard for capacitance, and inductance standard for inductance determination. Also, it is a great help in obtaining an accurate balance of the bridge if a standard of approximately the same value as the assumed value of the unknown is employed. Also, the standard should be of the same general type and should have approximately the same power factor as the unknown impedance. If all these precautions are observed, little trouble will be experienced in the measurement of resistance and in the measurement of impedances of the values usually used in audio and low radio frequency work.

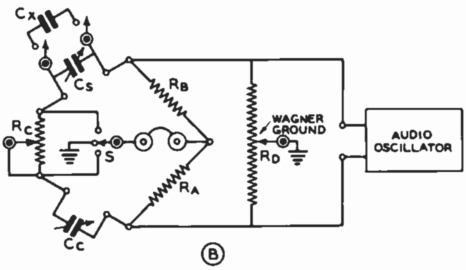
However, the bridge shown at 15A will not be satisfactory for the measurement of capacitances smaller than about 1000 $\mu\mu$fd. For the measurement of capacitances from a few micromicrofarads to about 0.001 μfd. a Wagner grounded substitution capacitance bridge of the type shown in figure 15B will be found satisfactory. The ratio arms R_A and R_B should be of the same value within 1 per cent; any value between 2500 and 10,000 ohms for them both will be satisfactory. The two resistors R_C and R_D should be 1000-ohm wire-wound potentiometers. C_S should be a straight-line capacitance capacitor with an accurate vernier dial; 500 to 1000 $\mu\mu$fd. will be satisfactory. C_C can be a two or three gang broadcast ca-



$Z_X = \frac{R_A}{R_B} Z_S$ $X_X = \frac{R_A}{R_B} X_S$ $R_X = \frac{R_A}{R_B} R_S$

Z_X = IMPEDANCE BEING MEASURED, R_S = RESISTANCE COMPONENT OF Z_S
Z_S = IMPEDANCE OF STANDARD, X_X = REACTANCE COMPONENT OF Z_X
R_X = RESISTANCE COMPONENT OF Z_X, X_S = REACTANCE COMPONENT OF Z_S

(A)



(B)

Figure 15
TWO A-C BRIDGE CIRCUITS

The operation of these bridges is essentially the same as those of figure 14 except that a.c. is fed into the bridge instead of d.c. and a pair of phones is used as the indicator instead of the galvanometer. The bridge shown at (A) can be used for the measurement of resistance, but it is usually used for the measurement of the impedance and reactance of coils and capacitors at frequencies from 200 to 1000 cycles. The bridge shown at (B) is used for the measurement of small values of capacitance by the substitution method. Full description of the operation of both bridges is given in the accompanying text.

pacitor from 700 to 1000 $\mu\mu$fd. maximum capacitance.

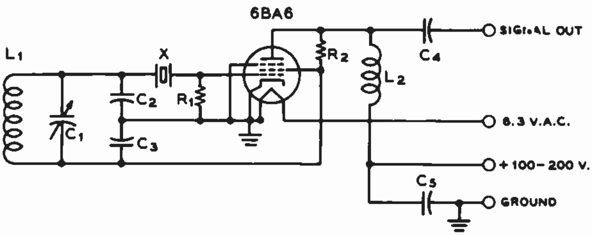
The procedure for making a measurement is as follows: The unknown capacitor C_X is placed in parallel with the standard capacitor C_S. The Wagner ground R_D is varied back and forth a small amount from the center of its range until no signal is heard in the phones with the switch S in the center position. Then the switch S is placed in either of the two outside positions, C_C is adjusted to a capacitance somewhat greater than the assumed value of the unknown C_X, and the bridge is brought into balance by variation of the standard capacitor C_S. It may be necessary to cut some resistance in at R_C and to switch to the other outside position of S before an exact balance can be obtained. The setting of C_S is then noted, C_X is removed from the circuit (but the leads which went to it are not changed in any way which would alter their mutual capacitance), and C_S is readjusted until balance is again obtained. The difference in the two settings of C_S is equal to the capacitance of the unknown capacitor C_X.

There are many other types of a-c bridge circuits in common use for measuring inductance with a capacitance standard, frequency in terms of resistance and capacitance, and so forth. Terman's *Radio Engineers' Handbook* gives an excellent discussion of common types of a-c bridge circuits.

31-5 Frequency Measurements

All frequency measurement within the United States is based on the transmissions of Station WWV of the National Bureau of Standards. This station operates continuously on frequencies of 2.5, 5, 10, 15, 20, 25, 30, and 35 Mc. The carriers of those frequencies below 30 Mc. are modulated alternately by a 440-cycle tone or a 600-cycle tone for periods of four minutes each. This tone is interrupted at the beginning of the 59th minute of each hour and each five minutes thereafter for a period of precisely one minute. Greenwich Civil Time is given in code during these one-minute intervals, followed by a voice announcement giving Eastern Standard Time. The accuracy of all radio and audio frequencies is better than one part in 50,000,000. A 5000 microsecond pulse (5 cycles of a 1000-cycle wave) may be heard as a tick for every second except the 59th second of each minute.

These standard-frequency transmissions of station WWV may be used for accurately determining the limits of the various amateur bands with the aid of the station communications receiver and a 50-kc., 100-kc., or 200-kc. bandedge spotter. The low-frequency oscillator may be self-excited if desired, but low-frequency standard crystals have become so relatively inexpensive that a reference crystal may be purchased for very little more than the cost of the components for a self-excited oscillator. The crystal has the additional advantage that it may be once set so that its harmonics are zero beat with WWV and then left with only an occasional check to see that the frequency has not drifted more than a few cycles. The self-



C_1—100-$\mu\mu$fd. air trimmer
C_2, C_3—0.0003-μfd. midget mica
C_4—50-$\mu\mu$fd. midget mica
C_5—0.002-μfd. midget mica
R_1, R_2—100,000 ohms ½ watt
L_1—10-mh. shielded r-f choke
L_2—2.1-mh. r-f choke
X—100-kc. crystal

Figure 16
SCHEMATIC OF A 100-KC. FREQUENCY SPOTTER

excited oscillator, on the other hand, must be monitored very frequently to insure that it is on frequency.

Using a Frequency Spotter To use a frequency spotter it is only necessary to couple the output of the oscillator unit to the antenna terminal of the receiver through a very small capacitance such as might be made by twisting two pieces of insulated hookup wire together. Station WWV is then tuned in on one of its harmonics, 15 Mc. will usually be best in the daytime and 5 or 10 Mc. at night, and the trimmer adjustment on the oscillator is varied until zero beat is obtained between the harmonic of the oscillator and WWV. With a crystal reference oscillator no difficulty will be had with using the wrong harmonic of the oscillator to obtain the beat, but with a self-excited oscillator it will be wise to insure that the reference oscillator is operating exactly on 50, 100, or 200 kc. (whichever frequency has been chosen) by making sure that zero beat is obtained simultaneously on all the frequencies of WWV that can be heard, and by noting whether or not the harmonics of the oscillator in the amateur bands fall on the approximate calibration marks of the receiver.

A simple frequency spotter is diagrammed in figure 16.

31-6 The Grid-Dip Meter

A *grid-dip meter* is a piece of test equipment which will be found invaluable in circuit alignment work. Basically, a grid-dip meter is simply a low-power oscillator with a meter for indicating rectified grid current. Some provision is always included in the design for coupling the tank circuit of the oscillator to the circuit under test.

The main application of the grid-dip meter is as a means of indicating the resonant frequency of a circuit to which it is coupled. For making a measurement of this type the tank circuit is coupled to the circuit under test, either directly or by means of a link, and the frequency of oscillation of the grid-dip meter is then varied over the frequency range where the external tank circuit is expected to resonate. When the frequency of oscillation of the grid-dip meter coincides with the resonant frequency of the external tank, power is extracted from the tank circuit of the grid-dip meter and the grid current of the oscillator tube takes a sudden dip. Hence the descriptive name for the instrument.

Since the basic application of the grid-dip meter is as a means of determining the resonant frequency of a tank circuit, it is fairly obvious that the meter will be more convenient to operate if it is capable of covering a relatively large frequency range. A frequency range on each coil of two to one is generally considered to be adequate.

Another use of the grid-dip meter is as an unshielded signal generator for the preliminary alignment of receivers in the v-h-f range. For this type of job the dip meter is coupled relatively tightly to the receiver until the signal can be tuned in by the detector stage. Then the coupling is backed off for the rough alignment of the r-f stages. After the r-f stages have been aligned roughly the dip meter may be turned off and the final alignment made on noise from the first tuned circuit, from an antenna, or on a signal from a shielded generator, if one should be available.

Measurement of Capacitance Since the grid-dip meter indicates resonance of an external circuit to its frequency of oscillation, the dip meter may be used in conjunction with a calibrated capacitor for the measurement of an unknown capacitance. This capability is convenient when it becomes necessary to determine the capacitance of a small

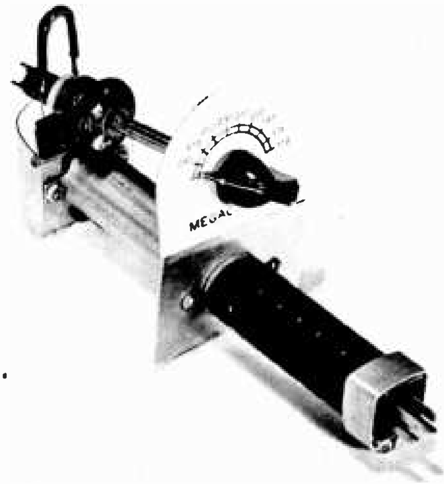


Figure 17
THE V-H-F GRID DIP METER

ceramic or mica capacitor when its markings have been obscured—or were obscure in the first place. Many of the fixed capacitors available from surplus stocks do not conform to RMA or ASA color-code markings, hence their capacitance must be measured before they are used in a circuit.

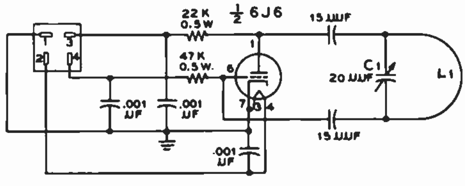
Since a high degree of accuracy will not be required for a rough capacitance check of this type, the calibrated capacitor may consist of a small straight-line-capacitance variable such as a National UM-100 or Johnson 100H15 with a simple 0-100 dial. A small coil of 5 or 6 turns with one-inch diameter is then soldered to the capacitor, the capacitor is set full in with its dial at 100, and the resonant frequency of the circuit checked with the grid-dip meter. The grid-dip meter is left set at this frequency and the unknown capacitor (whose capacitance is assumed to be less than the maximum capacitance of the variable capacitor) is soldered across the variable capacitor. Then, with the dip meter operating at the same frequency, the capacitance of the "calibrated" capacitor is decreased until the circuit again resonates at the frequency of operation of the dip meter. The amount by which the capacitance of the "calibrated" capacitor has been decreased is equal to the capacitance of the unknown capacitor which has been added. For the purpose of a simple check such as this, with a 0-100 dial and a variable capacitor with 100 $\mu\mu$fd. maximum, the reading of the 0-100 dial may be taken as the capacitance of the variable.

A V-H-F Grid-Dip Meter The oscillator unit illustrated in figures 17 and 18 was designed to cover a span of frequencies not normally covered by the less expensive grid-dip meters. For medium frequency work, it is best to buy a commercially produced grid-dip meter, such as the Millen 90651 or the less expensive Heathkit GD-1. For the v-h-f man, such a unit may perhaps not be necessary, since he is only interested in frequencies above 100 Mc.

This grid-dip meter covers the range of 90-Mc. to 175-Mc., or 170-Mc. to 290-Mc., depending upon the size of the coil used in the oscillator tuned circuit.

The unit and its handle are constructed on and inside a 7-inch length of aluminum tubing as a "chassis." The tubing has an inside diameter of 7/8 inch. A small rectangular piece of aluminum at the end carries the 6J6 socket, all the resistors and capacitors, a 3-lug tie point, and a small piece of insulating material on which is mounted the tuning capacitor. A third piece of aluminum carries the knob and dial scale.

At the oscillator end of the tubing two 1/4-inch ears are bent back to serve as mounting points for the plate which carries the 6J6 and its wiring. The 6J6 tube itself extends inside the tubing toward the handle end. The handle end of the tubing has four saw slots cut into it 90 degrees apart and 1/2 inch deep. This end then is formed into four flat sides to fit the rectangular base of a Jones four-point plug.



C1 - 20 µµF, JOHNSON 20 M11
L1 - 90-175 MC. = 2 T. # 14 E. ½" DIA., ¼" LONG
170-290 MC. = LOOP # 14 E. 1" LONG ½" WIDE

Figure 18
SCHEMATIC OF V-H-F GRID DIP METER

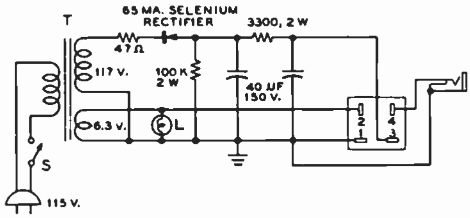


Figure 19
THE MINIATURE POWER SUPPLY
Transformer T is a Merit P-3045 power transformer, which was expressly designed for small power supplies of this general type.

A clamp secures the power plug in place as shown in figure 17. The wiring to the oscillator from the plug leaves the inside of the tubing through a grommet just beyond the dial scale, to clear the 6J6 tube envelope, and terminates on the 3-lug tie point below the socket. The dial scale is mounted half-way down the tubing by means of two angle brackets and sheet-metal screws.

The coil for the oscillator is mounted directly on the solder lugs of the tuning capacitor. A short length of plastic tubing is slipped over the coil just before mounting it on the tuning capacitor to reduce the possibility of grounding the coil when the unit is in use. A small piece of celluloid or plastic sheet may be formed and fastened over the end of the unit to protect the oscillator wiring.

Calibration of the oscillator may be accomplished with the aid of a pair of Lecher wires with a total length of about 6 feet. Some inaccuracy in the Lecher-wire calibration is unavoidable, since the oscillator must be coupled to the Lecher wires to obtain an indication. However, the range below 225 Mc. may be calibrated with the aid of a TV receiver on those channels which are in use.

A suitable power supply for this grid-dip meter is shown in figure 19.

31-7 One-Tube Sine-Wave Audio Oscillator

The miniature audio-oscillator shown in figures 20, 21 and 22 delivers several volts of sine-wave audio over the frequency range from 150 to 3500 cycles per second. The wave form is acceptable at 150 cycles and is a quite good sine wave above about 300 cycles. The circuit uses a 12AU7 as a cathode-coupled amplifier with the grid of the first section acting additionally as a diode to furnish automatic-level-control voltage to the second section.

An RC phase-shifting network, connected between the plate of the second section and the grid of the first, determines the frequency of oscillation. A one-megohm potentiometer is the variable element in the phase-shift network which controls the frequency of operation. The 3000-ohm potentiometer serving as plate load for the output section of the 12AU7 acts as a regeneration control. Its setting is not critical except to obtain the very best waveform at the low-frequency end of the audio range.

The output voltage from the oscillator varies somewhat with frequency. But for routine modu-

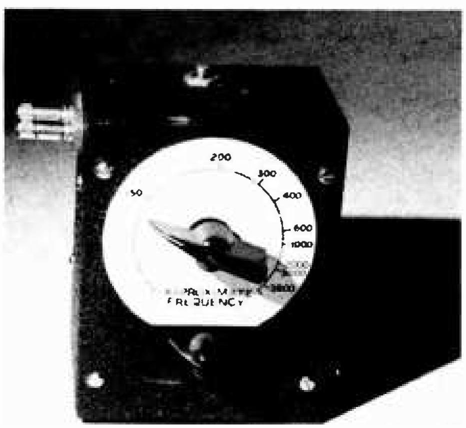


Figure 20
THE MINIATURE AUDIO OSCILLATOR

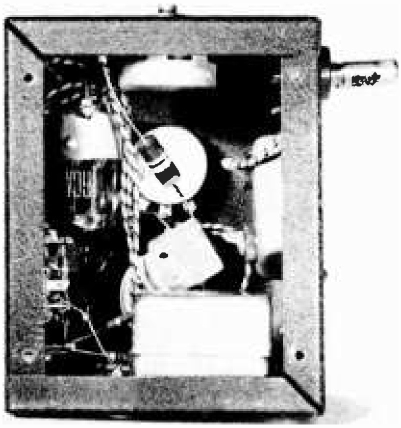


Figure 21
INSIDE THE MINIATURE AUDIO OSCILLATOR
The 12AU7 tube and its socket are mounted in an inverted position inside the housing.

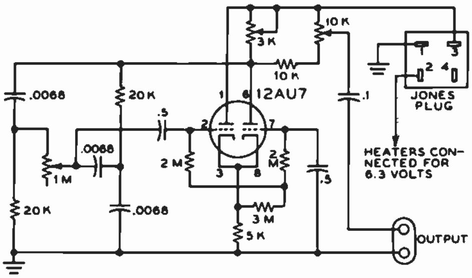


Figure 22
SCHEMATIC OF THE MINIATURE AUDIO OSCILLATOR
The one-megohm potentiometer acts as the frequency control, the 10,000-ohm potentiometer serves as output level control, and the 3000-ohm potentiometer controls the amplitude of oscillation and hence the output waveform of the unit. The power supply of figure 19 may be used with this oscillator.

lation testing where some waveform distortion on the lower frequencies may be tolerated, a single setting of the regeneration control will suffice. The 10,000-ohm potentiometer serves as an output attenuator.

This simple oscillator is adequate for the tuning of AM, FM, and single-sideband transmitters over the voice frequency range. The frequency range of the oscillator may be shifted by making a proportionate change in all three of the 0.0068-μfd. capacitors. An increase in capacitance will move both the upper frequency and lower frequency limits downward, though the ratio between the two extremes will remain the same as in the unit illustrated—approximately 20 to 1.

31-8 Antenna and Transmission Line Measurements

The degree of adjustment of any amateur antenna can be judged by the study of the standing-wave ratio on the transmission line feeding the antenna. Various types of instruments have been designed to measure the s.w.r. present on the transmission line, or to measure the actual radiation resistance of the antenna in question. The most important of these instruments are the *slotted line*, the *bridge-type s-w-r meter*, and the *antennascope*.

The Slotted Line It is obviously impractical to measure the voltage-standing-wave ratio in a length of coaxial line since the voltages and currents inside the line are completely shielded by the outer conductor of the cable. Hence it is necessary to insert some type of instrument into a section of the line in order to be able to ascertain the conditions which are taking place inside the shielded line. Where measurements of a high degree of accuracy are required, the *slotted line* is the instrument most frequently used. Such an instrument, diagrammed in figure 23, is an item of test equipment which could be constructed in a home workshop which included a lathe and other metal working tools. Commercially built slotted lines are very expensive since they are constructed with a high degree of accuracy for precise laboratory work.

The slotted line consists essentially of a section of air-dielectric line having the same characteristic impedance as the transmission line into which it is inserted. Tapered fittings for the transmission line connectors at each end of the slotted line usually are required due to differences in the diameters of the slotted line and the line into which it is inserted. A narrow slot from 1/8-inch to 1/4-inch in width is cut into the outer conductor of the line. A

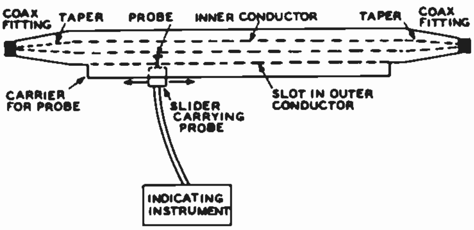


Figure 23

DIAGRAMMATIC REPRESENTATION OF A SLOTTED LINE

The conductor ratios in the slotted line, including the tapered end sections should be such that the characteristic impedance of the equipment is the same as that of the transmission line with which the equipment is to be used. The indicating instrument may be operated by the d-c output of the rectifier coupled to the probe, or it may be operated by the a-c components of the rectified signal if the signal generator or transmitter is amplitude modulated by a constant percentage.

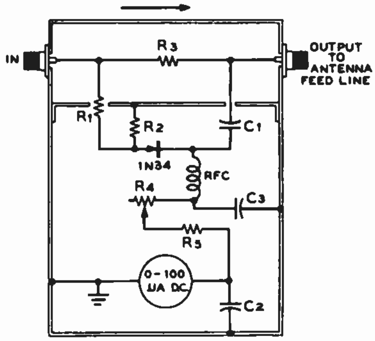


Figure 24

RESISTOR-BRIDGE STANDING-WAVE INDICATOR

This type of test equipment is suit- for use with coaxial feed lines.

C_1—0.001-μfd. midget ceramic capacitor
C_2, C_3—.001 disc ceramic
R_1, R_2—22-ohm 2-watt carbon resistors
R_3—Resistor equal in resistance to the characteristic impedance of the coaxial transmission line to be used (1 watt)
R_4—5000-ohm wire-wound potentiometer
R_5—10,000-ohm 1-watt resistor
RFC—R-f choke suitable for operation at the measurement frequency

probe then is inserted into the slot so that it is coupled to the field inside the line. Some sort of accurately machined track or lead screw must be provided to insure that the probe maintains a constant spacing from the inner conductor as it is moved from one end of the slotted line to the other. The probe usually includes some type of rectifying element whose output is fed to an indicating instrument alongside the slotted line.

The unfortunate part of the slotted-line system of measurement is that the line must be somewhat over one-half wavelength long at the test frequency, and for best results should be a full wavelength long. This requirement is easily met at frequencies of 420 Mc. and above where a full wavelength is 28 inches or less. But for the lower frequencies such an instrument is mechanically impracticable.

Bridge-Type Standing-Wave Indicators The bridge type of standing-wave indicator is used quite generally for making measurements on commercial coaxial transmission lines. A simplified version is available from M. C. Jones Electronics Co., Bristol, Conn. ("Micro-Match").

One type of bridge standing-wave indicator is diagrammed in figure 24. This type of instrument compares the electrical impedance of the transmission line with that of the resistor R_3 which is included within the unit. Experience with such units has shown that the resistor R_3 should be a good grade of non-inductive carbon type. The Ohmite "Little Devil" type of resistor in the 2-watt rating has given good performance. The resistance at R_3 should be equal to the characteristic impedance of the antenna transmission line. In other words, this resistor should have a value of 52 ohms for lines having this characteristic impedance such as RG-8/U and RG-58/U. For use with lines having a nominal characteristic impedance of 70 ohms, a selected "68 ohm" resistor having an actual resistance of 70 ohms may be used.

Balance within the equipment is checked by mounting a resistor, equal in value to the nominal characteristic impedance of the line to be used, on a coaxial plug of the type used on the end of the antenna feed line. Then this plug is inserted into the *input* receptacle of the instrument and a power of 2 to 4 watts applied to the *output* receptacle on the desired frequency of operation. Note that the signal is passed through the bridge in the direction opposite to normal for this test. The resistor R_4 is adjusted for full-scale deflection on the 0-100 microammeter. Then the plugs are reversed so that the test signal passes through the instrument in the direction indicated by the arrow

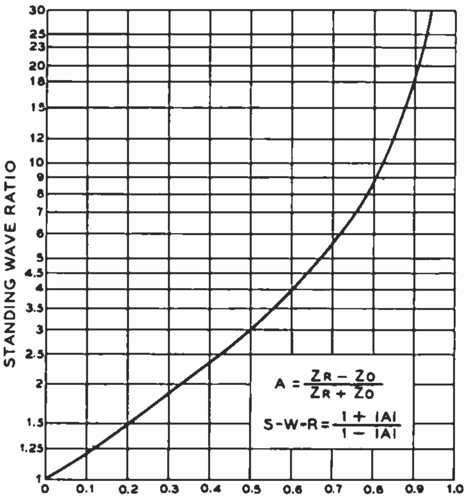


Figure 25

RELATION BETWEEN STANDING-WAVE RATIO AND REFLECTION COEFFICIENT

This chart may be used to convert reflection-coefficient indications such as are obtained with a bridge-type standing-wave indicator or an indicating twin lamp into values of standing-wave ratio.

on figure 24, and the power level is maintained the same as before. If the test resistor is matched to R_3, and stray capacitances have been held to low values, the indication on the milliammeter will be very small. The test plug with its resistor is removed and the plug for the antenna transmission line is inserted. The meter indication now will read the reflection coefficient which exists on the antenna transmission line at the point where the indicator has been inserted. From this reading of reflection coefficient the actual standing-wave ratio on the transmission line may be determined by reference to the chart of figure 25.

Measurements of this type are quite helpful in determining whether or not the antenna is presenting a good impedance match to the transmission line being used to feed it. However, a test instrument of the type shown in figure 24 must be inserted into the line for a measurement, and then removed from the line when the equipment is to be operated. Also, the power input to the line feeding the input terminal of the standing-wave indicator must not exceed 4 watts. The power level which the unit can accept is determined by the dissipation limitation of resistors R_1 plus R_2.

It is also important, for satisfactory operation of the test unit, that resistors R_1 and R_2 be exactly equal in value. The actual resistance of these two is not critically important, and deviations up to 10 per cent from the value given in figure 24 will be satisfactory. But the two resistors must have the same value, whether they are both 21 ohms or 24 ohms, or some value in between.

31-9 Construction of a Coaxial S-W-R Indicator

A suggested method of constructing an RC-bridge type of standing-wave indicator which can be left in the line with the transmitter operating is illustrated in figures 26 and 27. The unit is constructed in a 4 by 4 by 2 inch metal box with a shield baffle installed across the center of the box. The unit may be constructed in a relatively short period of time, using the general layout shown in the illustrations. However, the assembly of the actual bridge element is relatively critical for good performance.

The first step in the construction of the bridge assembly is to form two rings of no. 14 bus wire to a diameter of 3/4 inch. Then the nine 10-ohm 1-watt resistors, with leads on the resistors cut to a length of about one-quarter inch, are soldered to the two rings to form a cage. Following this, a shielding cone with length, not including leads, of 1¾ inches is formed of six lengths of no. 18 bus wire. Then an "X" of wire is placed across one end of the resistor cage, as shown to the left in figure 27. The center of this "X" is connected to the left-hand (antenna) coaxial terminal, while a lead about an inch long from the crystal rectifier also is connected to the center of the "X." However, it is important that the rectifier be mounted so that it extends *outward* from the *open* end of the resistor cage, with its inner end adjacent to the open end of the resistor cage. This method of mounting, which can be seen in figure 26, isolates the rectifier from the capacitive coupling to the voltage drop across the resistor cage.

The 750-$\mu\mu$fd. ceramic capacitor is then installed, the two leads from the junction between the rectifier and the 750-$\mu\mu$fd. capacitor are attached, and the shielding cone of wires is installed over the rectifier-capacitor assembly. Through this type of construction the rectifier and series capacitor are shielded from the fields which exist inside the upper

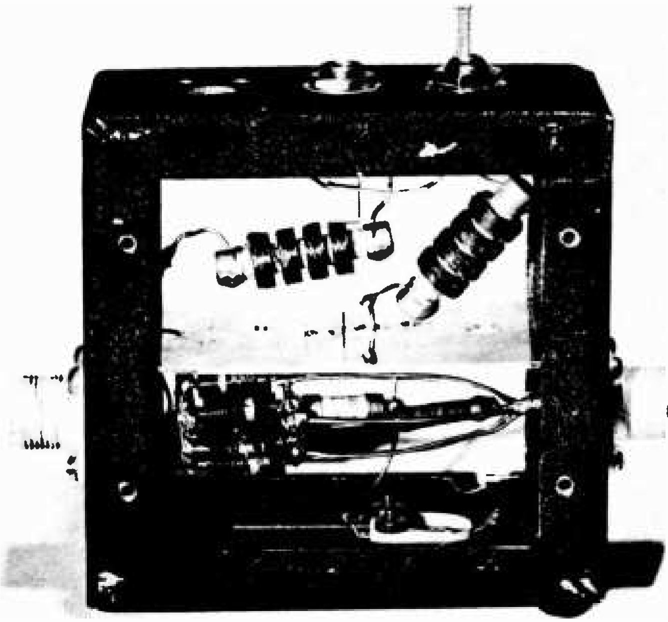


Figure 26
R-C BRIDGE STANDING-WAVE METER
The front and rear covers for the housing have been removed in this photograph. Note the shield baffle across the center of the housing. The mounting of the crystal rectifier and series capacitor with respect to the resistor cage and the cage of shielding wires also can be seen in the lower portion of the housing.

portion of the instrument, thus extending the operating range of the instrument well into the v-h-f range.

The bridge unit may be used with any type of d-c instrument, so long as the indicator has sufficient sensitivity for the power level to be used. Although measurements normally are made at a relatively low power level (10 to 50 watts in the transmission line) the unit illustrated may be used in a 52-ohm transmission line operating at a low s.w.r. with a power level as high as 500 watts.

Adjustment and Calibration Initial adjustment of the instrument for operation in a 52-ohm line is quite simple. A low-power transmitter is connected to the transmitter terminal. Then a 52-ohm 2-watt carbon resistor (with known good r-f characteristics) is connected with *short* leads to a coaxial plug. The plug with resistive termination then is inserted into the antenna terminal, and the 4.5-25 $\mu\mu$fd. ceramic trimmer capacitor is adjusted for minimum deflection. A very sharp null at frequencies as high as 50 Mc. will be obtained at the proper setting of the trimmer capacitor.

Calibration of the instrument may then be accomplished by reversing the instrument end for end, applying a resistive termination of value different from the nominal impedance of the unit, adjusting the power level and the sensitivity control (20,000-ohm rheostat shown on figure 27) until a full-scale deflection is obtained. Then the instrument is reversed again so that the transmitter and load are connected as shown in figure 27, and the deflection obtained on the meter is noted. If the sensitivity of the indicating instrument is high, so that a large value of series resistance is in use, the meter will read quite close to the theoretical value of reflection coefficient which would be obtained with the termination

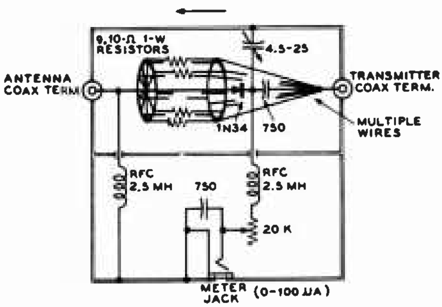


Figure 27

SCHEMATIC OF THE R-C STANDING-WAVE INDICATOR

This semi-pictorial illustration shows the manner of construction. Power flow in the direction of the arrow does not read on the indicator; flow in the other direction, resulting from reflected power or from intentional reversal of the instrument, does read on the indicator.

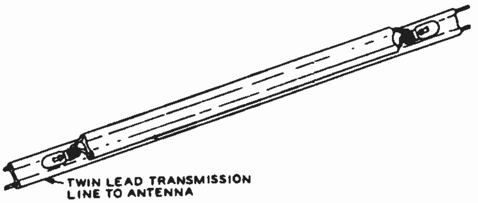


Figure 28

SKETCH OF THE "TWIN-LAMP" TYPE OF S-W-R INDICATOR

The short section of line with lamps at each end usually is taped to the main transmission line with plastic electrical tape.

under test. Conversion from reflection coefficient to standing-wave ratio may be obtained from the chart of figure 25.

The use of the instrument is normal for bridge-type indicators of this general type. The instrument is first connected into the antenna transmission line in the reverse direction. Then, with a large value of series resistance to the indicating meter, power is applied to the transmitter and the series resistor is adjusted until the meter reads full scale. Then the instrument is reversed end for end and reconnected back into the transmission line as shown in figure 27. When power is applied to the transmitter, the deflection on the meter is noted. The meter reading will be in reflection coefficient of the load, with a fair degree of accuracy even without calibration, so that the s.w.r. can be obtained by reference to figure 25.

Measurements on Molded Parallel-Wire Lines One of the most satisfactory and least expensive devices for obtaining a rough idea of the standing-wave ratio on a transmission line of the molded parallel-wire type is the *twin-lamp* which was first described by Wright in the October, 1947, issue of the magazine *QST*. This ingenious instrument may be constructed of new components for a total cost of about 25 cents; this fact alone places the twin-lamp in a class by itself as far as test instruments are concerned.

Figure 28 shows a sketch of a twin-lamp indicator. The indicating portion of the system consists merely of a length of 300-ohm Twin-Lead about 10 inches long with a dial lamp at each end. In the unit illustrated the dial lamps are standard 6.3-volt 150-ma. bayonet-base lamps. The lamps are soldered to the two leads at each end of the short section of Twin-Lead.

To make a measurement the short section of line with the lamps at each end is merely taped to the section of Twin-Lead (or other similar transmission line) running from the transmitter or from the antenna changeover relay to the antenna system. When there are no standing waves on the antenna transmission line the lamp toward the transmitter will light while the one toward the antenna will not light. With 300-ohm Twin-Lead running from the antenna changeover relay to the antenna, and with about 200 watts input on the 28-Mc. band, the dial lamp toward the transmitter will light nearly to full brilliancy. With a standing-wave ratio of about 1.5 to 1 on the transmission line to the antenna the lamp toward the antenna will just begin to light. With a high standing-wave ratio on the antenna feed line both lamps will light nearly to full brilliancy. Hence the instrument gives an indication of relatively low standing waves, but when the standing-wave ratio is high the twin-lamp merely indicates that they are high without giving any idea of the actual magnitude.

Operation of the Twin-Lamp The twin lamp operates by virtue of the fact that the capacitive and inductive coupling of the wire making up one side of the twin-lamp is much greater to the transmission-line lead immediately adjacent to it than to the transmission-line lead on the other side. The same is of course true of the wire on the other side of the twin-lamp and the transmission-line lead adjacent to it. A further condition which must be met for the twin-lamp to

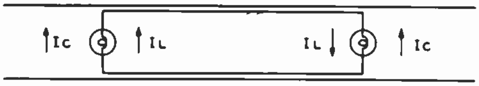


Figure 29
OPERATION OF THE "TWIN LAMP" INDICATOR
Showing current flow resulting from inductive and capacitive fields in a "twin lamp" attached to a line with a low standing-wave ratio.

operate is that the section of line making up the twin-lamp must be short with respect to a quarter wavelength. Then the current due to capacitive coupling passes through both lamps in the same direction, while the current due to inductive coupling between the leads of the twin-lamp and the leads of the antenna transmission line passes through the two lamps in opposite directions. Hence, in a line without reflections, the two currents will cancel in one lamp while the other lamp is lighted due to the sum of the currents (figure 29).

The basic fact which makes the twin-lamp a *directional coupler* is a result of the condition whereby the capacitive coupling is a *scalar* action not dependent upon the direction of the waves passing down the line, yet the inductive coupling is a *vector* action which *is* dependent upon the direction of wave propagation down the line. Thus the capacitive current is the same and is in the same phase for energy travelling in either direction down the line. But the inductive current travels in one direction for energy travelling in one direction and in the other direction for energy going the other direction. Hence the two currents add at one end of the line for a wave passing toward the antenna, while the currents add at the other end of the twin-lamp for the waves reflected from the antenna. When the waves are strongly reflected upon reaching the antenna, the reflected wave is nearly the same as the direct wave, and both lamps will light. This condition of strong reflection from the antenna system is that which results in a high standing-wave ratio on the antenna feed line.

Use of the Twin Lamp with Various Feed Lines The twin-lamp is best suited for use with antenna transmission lines of the flat ribbon type. Lines with a high power rating are available in impedances of 75 ohms, 205 ohms, and 300 ohms in the flat ribbon type. In addition, one manufacturer makes a 300-ohm line in two power-level ratings with a tubular cross section. A twin-lamp made from flat 300-ohm line may be used with this tubular line by taping the twin-lamp tightly to the tubular line so that the conductors of the twin-lamp are as close as possible on each side of the conductors of the antenna line.

The Antennoscope The *Antennascope,* first described by W2AEF in September, 1950, CQ magazine, is a modified SWR bridge in which one leg of the bridge is composed of a non-inductive variable resistor. This resistor is calibrated in ohms, and when its setting is equal to the radiation resistance of the antenna under test the bridge is in a balanced state. If a sensitive voltmeter is connected across the bridge, it will indicate a voltage null at bridge balance. The radiation resistance of the antenna may then be read directly from the calibrated resistor of the instrument.

When the antenna under test is in a non-resonant or reactive state, the null indication on the meter of the Antennascope will be incomplete. The frequency of the exciting signal must then be moved to the resonant frequency of the antenna to obtain accurate readings of radiation resistance from the dial of the instrument.

A typical Antennascope is shown in figures 30 and 31, and the schematic is shown in figure 32. A 100 ohm non-inductive carbon poten-

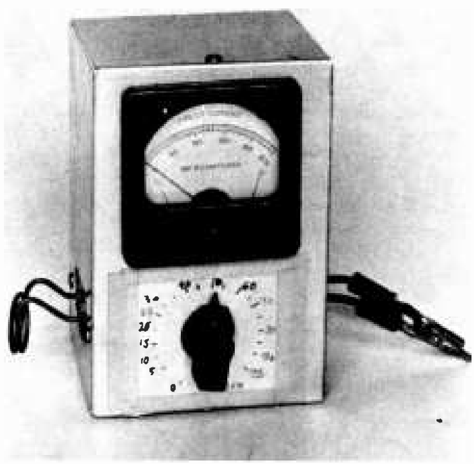


Figure 30
THE ANTENNASCOPE
The radiation resistance of r-f loads connected across the clips of this instrument may be quickly determined by a direct dial reading.

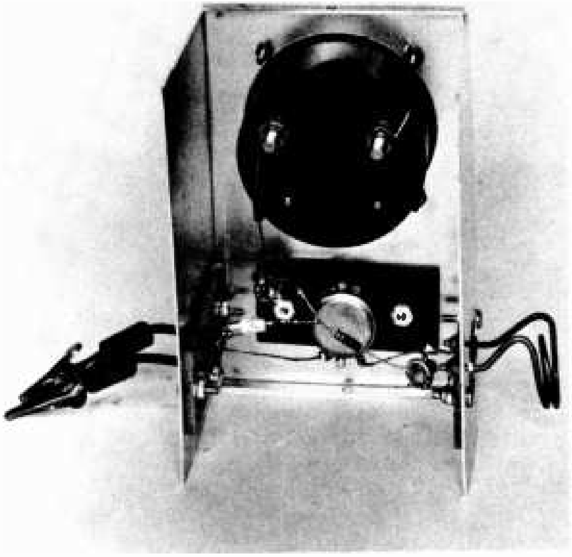


Figure 31
PLACEMENT OF PARTS IN THE ANTENNASCOPE
With the length of leads shown this model is useful up to about 40 Mc. For operation on 6 and 2 meters, the interconnecting leads should be shorter and made of one-eighth inch copper strap.

tiometer serves as the variable leg of the bridge. The other two legs are made of 200 ohm *composition* resistors in series with 500 $\mu\mu$fd. button mica capacitors. Since the tolerance of these capacitors is plus or minus 20 per cent of the marked capacity value, a number of the units should be checked on a capacity bridge to find two units of equal capacitance. The exact capacity value is unimportant, it is only necessary that the two values of capacitance be equal. If the Antennascope is not to be used above 30 Mc., 2 per cent silver-mica capacitors may be used for C_1 and C_2.

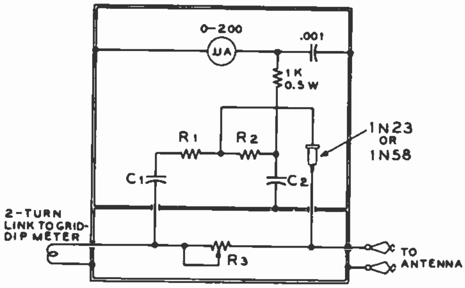
Resistors R_1 and R_2 should be matched on an ohmmeter and care should be taken when they are soldered in the circuit to see that they do not become overheated, causing the resistance value to change. In like manner, the 1N23 crystal should be soldered in the circuit with a minimum of applied heat, or it should be mounted in a miniature fuse clip. All leads in the r-f section of the Antennascope should be as short as possible.

A one inch hole is drilled in the front of the case, and R_3 is mounted in this hole on a thin piece of insulating material, such as bakelite or micarta. All terminals of R_3 are at r-f potential, so it is essential for good bridge operation to have a minimum of capacity between the case of R_3 and ground. The two output leads are brought out through a second insulating strip mounted on the side of the Antennascope. These connections to the alligator clips should not be over two inches long, since most of the residual inductance of the Antennascope will be found in these leads.

Testing the Antennascope When the instrument is completed, a grid-dip meter may be coupled to the input link of the Antennascope. If the 0-200 d-c microammeter in the Antennascope reads backward, the leads to the meter should be reversed. The grid-dip meter should be set somewhere in the 10-Mc. to 20-Mc. range and coupled to the Antennascope to obtain a half-scale reading on the meter. Various values of 1-watt composition resistors up to 100 ohms should be placed between the alligator clip terminals, and R_3 adjusted for a null on the meter. The settings of R_3 may then be calibrated in this manner, until, by interpolation, 5 ohm points are marked on a paper dial scale for the complete rotation of R_3.

This calibration should hold to frequencies well above the 6-meter amateur band if button mica capacitors are used for C_1 and C_2. As the inherent inductance of the instrument starts to become a factor, it will no longer be possible to obtain a complete null on the meter of the Antennascope.

Using the Antennascope The Antennascope is coupled to the grid-dip meter by means of a two or three turn link. Enough coupling should be obtained to allow



C1, C2 – 500 UUF BUTTON MICA CAPACITORS, MATCHED (*CENTRALAB ZA-501*)
R1 R2 – 200 OHMS, 0.5-WATT CARBON RESISTORS
R3 – 100 OHMS, NON-INDUCTIVE RESISTOR (*ALLEN-BRADLEY TYPE J OR OHMITE TYPE AB*)
BOX – 3 X 4 X 5-INCH ALUMINUM CASE (*BUD CU-3005*)

Figure 32

ANTENNASCOPE SUITABLE FOR USE WITH PARASITIC BEAM ANTENNAS (IMPEDANCE RANGE OF 0-100 OHMS)

at least a 3/4 scale reading on the meter of the Antennascope with no load connected to the measuring terminals. The Antennascope may be considered to be a low range r-f ohmmeter and may be employed to determine the electrical length of quarter-wave lines, surge impedance of transmission lines, and antenna resonance and radiation resistance.

In general, the measuring terminals of the Antennascope are connected in series with the load at a point of maximum current. This means the center of a dipole, or the base of a vertical 1/4-wave ground plane antenna. Excitation is supplied to the Antennascope, and the frequency of excitation and the resistance control of the Antennascope are both varied until a complete null is obtained on the indicating meter of the Antennascope. The frequency of the source of excitation is now the resonant frequency of the load, and the radiation resistance of the load may be read upon the dial of the Antennascope.

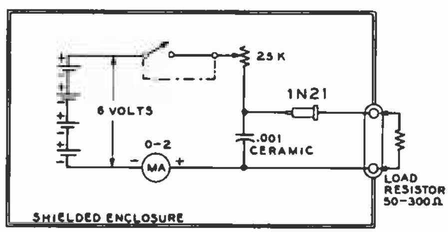
On measurements on 80 and 40 meters, it might be found that it is impossible to obtain a complete null on the Antennascope. This is usually caused by pickup of a nearby broadcast station, the rectified signal of the broadcast station obscuring the null indication on the Antennascope. This action is only noticed when antennas of large size are being checked.

31-10 A Silicon Crystal Noise Generator

The limiting factor in signal reception above 25 Mc. is usually the thermal noise generated in the receiver. At any frequency, however, the tuned circuits of the receiver must be accurately aligned for best signal-to-noise ratio. Circuit changes (and even alignment changes) in the r-f stages of a receiver may do much to either enhance or degrade the noise figure of the receiver. It is exceedingly hard to determine whether changes of either alignment or circuitry are really providing a boost in signal-

Figure 33

SIMPLE SILICON CRYSTAL NOISE GENERATOR



A SILICON CRYSTAL NOISE GENERATOR

Figure 34

SCHEMATIC OF SILICON CRYSTAL NOISE GENERATOR

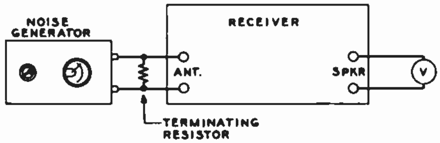
to-noise ratio of the receiver, or are merely increasing the gain (and noise) of the unit.

A simple means of determining the degree of actual sensitivity of a receiver is to inject a minute signal in the input circuit and then measure the amount of this signal that is needed to overcome the inherent receiver noise. The less injected signal needed to override the receiver noise by a certain, fixed amount, the more sensitive is the receiver.

A simple source of minute signal may be obtained from a silicon crystal diode. If a small d-c current is passed through a silicon crystal in the direction of highest resistance, a small but constant r-f noise (or hiss) is generated. The voltage necessary to generate this noise may be obtained from a few flashlight cells. The generator is a broad band device and requires no tuning. If built with short leads, it may be employed for receiver measurements well above 150 Mc. The noise generator should be used for comparative measurements only, since calibration against a high quality commercial noise generator is necessary for absolute measurements.

A Practical Noise Generator Shown in figure 33 is a simple silicon crystal noise generator. The schematic of this unit is illustrated in figure 34. The 1N21 crystal and .001 μfd. ceramic capacitor are connected in series directly across the output terminals of the instrument. Three small flashlight batteries are wired in series and mounted inside the case, along with the 0-1 d-c milliammeter and the noise level potentiometer.

To prevent heat damage to the 1N21 crystal during the soldering process, the crystal should be held with a damp rag, and the connections soldered to it quickly with a very hot iron. Across the terminals (and in parallel with the equipment to be attached to the generator) is a 1-watt carbon resistor whose resistance is equal to the impedance level at which measurements are to be made. This will usually be either 50 or 300 ohms. If the noise generator is to be used at one impedance level only, this resistor may be mounted permanently inside of the case.



TEST SET-UP FOR NOISE GENERATOR

RECEIVER SENSITIVITY CHECK

Using the Noise Generator The test setup for use of the noise generator is shown in figure 35. The noise generator is connected to the antenna terminals of the receiver under test. The receiver is turned on, the a.v.c. turned off, and the r-f gain control placed full on. The audio volume control is adjusted until the output meter advances to one-quarter scale. This reading is the basic receiver noise. The noise generator is turned on, and the noise level potentiometer adjusted until the noise output voltage of the receiver is doubled. The more resistance in the diode circuit, the better is the signal-to-noise ratio of the receiver under test. The r-f circuits of the receiver may be aligned for maximum signal-to-noise ratio with the noise generator by aligning for a 2/1 noise ratio at minimum diode current.

CHAPTER THIRTY TWO

Radio Mathematics and Calculations

Radiomen often have occasion to calculate sizes and values of required parts. This requires some knowledge of mathematics. The following pages contain a review of those parts of mathematics necessary to understand and apply the information contained in this book. It is assumed that the reader has had some mathematical training; this chapter is not intended to teach those who have never learned anything of the subject.

Fortunately only a knowledge of fundamentals is necessary, although this knowledge must include several branches of the subject. Fortunately, too, the majority of practical applications in radio work reduce to the solution of equations or formulas or the interpretation of graphs.

Arithmetic

Notation of Numbers In writing numbers in the Arabic system we employ ten different symbols, digits, or figures: 1, 2, 3, 4, 5, 6, 7, 8, 9, and 0, and place them in a definite sequence. If there is more than one figure in the number the *position* of each figure or digit is as important in determining its value as is the digit itself. When we deal with whole numbers the righthandmost digit represents units, the next to the left represents tens, the next hundreds, the next thousands, from which we derive the rule that every time a digit is placed one space further to the left its value is multiplied by ten.

8	1	4	3
thousands	hundreds	tens	units

It will be seen that any number is actually a sum. In the example given above it is the sum of eight thousands, plus one hundred, plus four tens, plus three units, which could be written as follows:

8	thousands (10 x 10 x 10)
1	hundreds (10 x 10)
4	tens
3	units
8143	

The number in the units position is sometimes referred to as a *first order* number, that in the tens position is of the *second order*, that in the hundreds position the *third order*, etc.

The idea of letting the position of the symbol denote its value is an outcome of the abacus. The abacus had only a limited number of wires with beads, but it soon became apparent that the quantity of symbols might be continued indefinitely towards the left, each further space multiplying the digit's value by ten. Thus any quantity, however large, may readily be indicated.

It has become customary for ease of reading to divide large numbers into groups of three digits, separating them by commas.

6,000,000 rather than 6000000

Our system of notation then is characterized by two things: the use of positions to indicate the value of each symbol, and the use of ten symbols, from which we derive the name *decimal system.*

Retaining the same use of positions, we might have used a different number of symbols, and displacing a symbol one place to the left might multiply its value by any other factor such as 2, 6 or 12. Such other systems have been in use in history, but will not be discussed here. There are also systems in which displacing a symbol to the left multiplies its value by

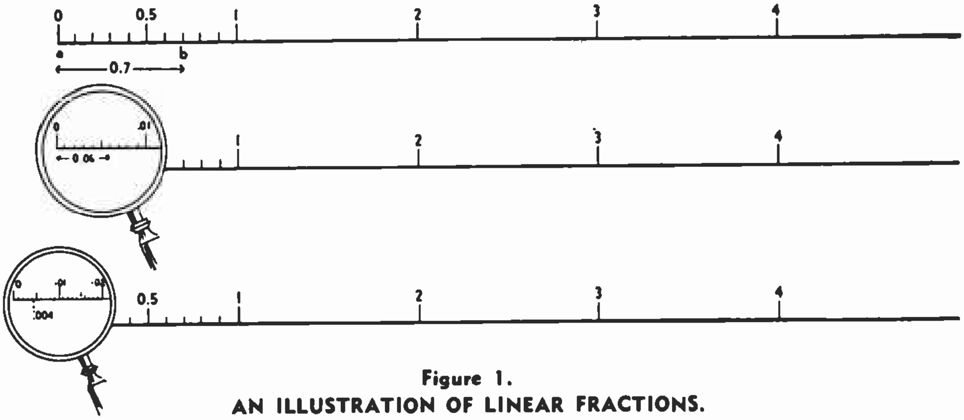


Figure 1.
AN ILLUSTRATION OF LINEAR FRACTIONS.

varying factors in accordance with complicated rules. The English system of measurements is such an inconsistent and inferior system.

Decimal Fractions Since we can extend a number indefinitely to the left to make it bigger, it is a logical step to extend it towards the right to make it smaller. Numbers smaller than unity are *fractions* and if a displacement one position to the right divides its value by ten, then the number is referred to as a *decimal fraction*. Thus a digit to the right of the units column indicates the number of *tenths*, the second digit to the right represents the number of *hundredths*, the third, the number of *thousandths*, etc. Some distinguishing mark must be used to divide unit from tenths so that one may properly evaluate each symbol. This mark is the *decimal point*.

A decimal fraction like *four-tenths* may be written .4 or 0.4 as desired, the latter probably being the clearer. Every time a digit is placed one space further to the right it represents a ten times smaller part. This is illustrated in Figure 1, where each large division represents a unit; each unit may be divided into ten parts although in the drawing we have only so divided the first part. The length *ab* is equal to seven of these tenth parts and is written as 0.7.

The next smaller divisions, which should be written in the second column to the right of the decimal point, are each one-tenth of the small division, or one one-hundredth each. They are so small that we can only show them by imagining a magnifying glass to look at them, as in Figure 1. Six of these divisions is to be written as 0.06 (six hundredths). We need a microscope to see the next smaller division, that is those in the third place, which will be a tenth of one one-hundredth, or a thousandth; four such divisions would be written as 0.004 (four thousandths).

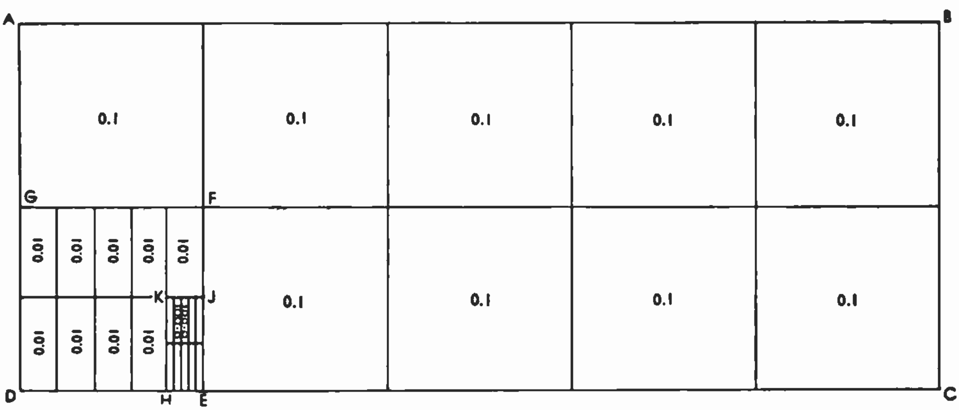


Figure 2.
IN THIS ILLUSTRATION FRACTIONAL PORTIONS ARE REPRESENTED IN THE FORM OF RECTANGLES RATHER THAN LINEARLY.
ABCD = 1.0; GFED = 0.1; KJEH = 0.01; each small section within KJEH equals 0.001.

It should not be thought that such numbers are merely of academic interest for very small quantities are common in radio work.

Possibly the conception of fractions may be clearer to some students by representing it in the form of rectangles rather than linearly (see Figure 2).

Addition When two or more numbers are to be added we sometimes write them horizontally with the plus sign between them. + is the sign or *operator* indicating addition. Thus if 7 and 12 are to be added together we may write $7+12=19$.

But if larger or more numbers are to be added together they are almost invariably written one under another in such a position that the decimal points fall in a vertical line. If a number has no decimal point, it is still considered as being just to the right of the units figure; such a number is a whole number or *integer*. Examples:

$$\begin{array}{r} 654 \\ 32 \\ 53041 \\ \hline 53727 \end{array} \qquad \begin{array}{r} 0.654 \\ 3.2 \\ 53.041 \\ \hline 56.895 \end{array} \qquad \begin{array}{r} 654 \\ 32 \\ 5304.1 \\ \hline 5990.1 \end{array}$$

The result obtained by adding numbers is called the *sum*.

Subtraction Subtraction is the reverse of addition. Its operator is − (the *minus* sign). The number to be subtracted is called the *minuend*, the number from which it is subtracted is the *subtrahend*, and the result is called the *remainder*.

$$\begin{array}{r} \text{subtrahend} \\ -\,\text{minuend} \\ \hline \text{remainder} \end{array}$$

Examples:

$$\begin{array}{r} 65.4 \\ -32 \\ \hline 33.4 \end{array} \qquad \begin{array}{r} 65.4 \\ -32.21 \\ \hline 33.19 \end{array}$$

Multiplication When numbers are to be multiplied together we use the ×, which is known as the *multiplication* or the *times* sign. The number to be multiplied is known as the *multiplicand* and that by which it is to be multiplied is the *multiplier*, which may be written in words as follows:

$$\begin{array}{r} \text{multiplicand} \\ \times\ \text{multiplier} \\ \hline \text{partial product} \\ \text{partial product} \\ \hline \text{p r o d u c t} \end{array}$$

The result of the operation is called the *product*.

From the examples to follow it will be obvious that there are as many partial products as there are digits in the multiplier. In the following examples note that the righthandmost digit of each partial product is placed one space farther to the left than the previous one.

$$\begin{array}{r} 834 \\ \times\ 26 \\ \hline 5004 \\ 1668 \\ \hline 21684 \end{array} \qquad \begin{array}{r} 834 \\ \times\ 206 \\ \hline 5004 \\ 000 \\ 1668 \\ \hline 171804 \end{array}$$

In the second example above it will be seen that the inclusion of the second partial product was unnecessary; whenever the multiplier contains a cipher (zero) the next partial product should be moved an *additional* space to the left.

Numbers containing decimal fractions may first be multiplied exactly as if the decimal point did not occur in the numbers at all; the position of the decimal point in the product is determined after all operations have been completed. It must be so positioned in the product that the number of digits to its right is equal to the number of decimal places in the multiplicand plus the number of decimal places in the multiplier.

This rule should be well understood since many radio calculations contain quantities which involve very small decimal fractions. In the examples which follow the explanatory notations "2 places," etc., are not actually written down since it is comparatively easy to determine the decimal point's proper location mentally.

$$\begin{array}{rl} 5.43 & \text{2 places} \\ \times 0.72 & \text{2 places} \\ \cline{1-1} 1086 & \\ 3\ 801 & \\ \cline{1-1} 3.9096 & 2+2=4 \text{ places} \end{array}$$

$$\begin{array}{rl} 0.04 & \text{2 places} \\ \times 0.003 & \text{3 places} \\ \cline{1-1} 0.00012 & 2+3=5 \text{ places} \end{array}$$

Division Division is the reverse of multiplication. Its operator is the ÷, which is called the *division sign*. It is also common to indicate division by the use of the fraction bar (/) or by writing one number over the other. The number which is to be divided is called the *dividend* and is written before the division sign or fraction bar or over the horizontal line indicating a fraction. The number by which the dividend is to be divided is called the *divisor* and follows the division sign or fraction bar or comes under the horizontal line of the fraction. The answer or result is called the *quotient.*

divisor) dividend (with **quotient** written above the dividend)

or

$$\text{dividend} \div \text{divisor} = \text{quotient}$$

or

$$\frac{\text{dividend}}{\text{divisor}} = \text{quotient}$$

Examples:

```
        126               49
834 ) 105084       49 ) 2436
      834                196
      ----               ---
      2168               476
      1668               441
      ----               ---
       5004               35 remainder
       5004
       ----
```

Note that one number often fails to divide into another evenly. Hence there is often a quantity left over called the *remainder.*

The rules for placing the decimal point are the reverse of those for multiplication. The number of decimal places in the quotient is equal to the difference between the number of decimal places in the dividend and that in the divisor. It is often simpler and clearer to remove the decimal point entirely from the divisor by multiplying both dividend and divisor by the necessary factor; that is we move the decimal point in the divisor as many places to the right as is necessary to make it a whole number and then we move the decimal point in the dividend exactly the same number of places to the right regardless of whether this makes the dividend a whole number or not. When this has been done the decimal point in the quotient will automatically come directly above that in the dividend as shown in the following example.

Example: Divide 10.5084 by 8.34. Move the decimal point of both dividend and divisor two places to the right.

```
         1.26
834 ) 1050.84
       834
       ----
       2168
       1668
       ----
        5004
        5004
        ----
```

Another example: Divide 0.000325 by 0.017. Here we must move the decimal point three places to the right in both dividend and divisor.

```
     0.019
17 ) 0.325
       17
       --
       155
       153
       ---
         2
```

In a case where the dividend has fewer decimals than the divisor the same rules still may be applied by adding ciphers. For example to divide 0.49 by 0.006 we must move the decimal point three places to the right. The 0.49 now becomes 490 and we write:

```
     81
6 ) 490
    48
    --
     10
      6
     --
      4
```

When the division shows a remainder it is sometimes necessary to continue the work so as to obtain more figures. In that case ciphers may be annexed to the dividend, brought down to the remainder, and the division continued as long as may be necessary; be sure to place a decimal point in the dividend before the ciphers are annexed if the dividend does not already contain a decimal point. For example:

```
     80.33
6 ) 482.00
    48
    --
      20
      18
      --
       20
       18
       --
        2
```

This operation is not very often required in radio work since the accuracy of the measurements from which our problems start seldom justifies the use of more than three significant figures. This point will be covered further later in this chapter.

Fractions Quantities of less than one (unity) are called *fractions.* They may be expressed by decimal notation as we have seen, or they may be expressed as *vulgar fractions.* Examples of vulgar fractions:

$$\frac{\text{numerator}}{\text{denominator}} \quad \frac{3}{4} \quad \frac{6}{7} \quad \frac{1}{5}$$

The upper position of a vulgar fraction is called the *numerator* and the lower position the *denominator*. When the numerator is the smaller of the two, the fraction is called a *proper fraction;* the examples of vulgar fractions given above are proper vulgar fractions. When the numerator is the larger, the expression is an *improper fraction,* which can be reduced to an integer or whole number with a proper fraction, the whole being called a mixed number. In the following examples improper fractions have been reduced to their corresponding mixed numbers.

$$\frac{7}{4} = 1\frac{3}{4} \qquad \frac{5}{3} = 1\frac{2}{3}$$

Adding or Subtracting Fractions Except when the fractions are very simple it will usually be found much easier to add and subtract fractions in the form of decimals. This rule likewise applies for practically all other operations with fractions. However, it is occasionally necessary to perform various operations with vulgar fractions and the rules should be understood.

When adding or subtracting such fractions the denominators must be made equal. This may be done by multiplying both numerator and denominator of the first fraction by the denominator of the other fraction, after which we multiply the numerator and denominator of the second fraction by the denominator of the first fraction. This sounds more complicated than it usually proves in practice, as the following examples will show.

$$\frac{1}{2} + \frac{1}{3} = \left[\frac{1 \times 3}{2 \times 3} + \frac{1 \times 2}{3 \times 2}\right] = \frac{3}{6} + \frac{2}{6} = \frac{5}{6}$$

$$\frac{3}{4} - \frac{2}{5} = \left[\frac{3 \times 5}{4 \times 5} - \frac{2 \times 4}{5 \times 4}\right] = \frac{15}{20} - \frac{8}{20} = \frac{7}{20}$$

Except in problems involving large numbers the step shown in brackets above is usually done in the head and is not written down.

Although in the examples shown above we have used proper fractions, it is obvious that the same procedure applies with improper fractions. In the case of problems involving mixed numbers it is necessary first to convert them into improper fractions. Example:

$$2\frac{3}{7} = \frac{2 \times 7 + 3}{7} = \frac{17}{7}$$

The numerator of the improper fraction is equal to the whole number multiplied by the denominator of the original fraction, to which the numerator is added. That is in the above example we multiply 2 by 7 and then add 3 to obtain 17 for the numerator. The denominator is the same as is the denominator of the original fraction. In the following example we have added two mixed numbers.

$$2\frac{3}{7} + 3\frac{3}{4} = \frac{17}{7} + \frac{15}{4} = \left[\frac{17 \times 4}{7 \times 4} + \frac{15 \times 7}{4 \times 7}\right]$$

$$= \frac{68}{28} + \frac{105}{28} = \frac{173}{28} = 6\frac{5}{28}$$

Multiplying Fractions All vulgar fractions are multiplied by multiplying the numerators together and the denominators together, as shown in the following example:

$$\frac{3}{4} \times \frac{2}{5} = \left[\frac{3 \times 2}{4 \times 5}\right] = \frac{6}{20} = \frac{3}{10}$$

As above, the step indicated in brackets is usually not written down since it may easily be performed mentally. As with addition and subtraction any mixed numbers should be first reduced to improper fractions as shown in the following example:

$$\frac{3}{23} \times 4\frac{1}{3} = \frac{3}{23} \times \frac{13}{3} = \frac{39}{69} = \frac{13}{23}$$

Division of Fractions Fractions may be most easily divided by inverting the divisor and then multiplying. Example:

$$\frac{2}{5} \div \frac{3}{4} = \frac{2}{5} \times \frac{4}{3} = \frac{8}{15}$$

In the above example it will be seen that to divide by ¾ is exactly the same thing as to multiply by 4/3. Actual division of fractions is a rather rare operation and if necessary is usually postponed until the final answer is secured when it is often desired to reduce the resulting vulgar fraction to a decimal fraction by division. It is more common and usually results in least overall work to reduce vulgar fractions to decimals at the beginning of a problem. Examples:

$$\frac{3}{8} = 0.375 \qquad \frac{5}{32} = 0.15625$$

```
       0.15625
32 ) 5.00000
     3 2
     1 80
     1 60
       200
       192
         80
         64
        160
        160
```

It will be obvious that many vulgar fractions cannot be reduced to exact decimal equivalents. This fact need not worry us, however, since the degree of equivalence can always be as much as the data warrants. For instance, if we know that one-third of an ampere is flowing in a given circuit, this can be written as 0.333 amperes. This is not the exact equivalent of 1/3 but is close enough since it shows the value to the nearest thousandth of an ampere and it is probable that the meter from which we secured our original data was not accurate to the nearest thousandth of an ampere.

Thus in converting vulgar fractions to a decimal we unhesitatingly stop when we have reached the number of significant figures warranted by our original data, which is very seldom more than three places (see section *Significant Figures* later in this chapter).

When the denominator of a vulgar fraction contains only the factors 2 or 5, division can be brought to a finish and there will be no remainder, as shown in the examples above.

When the denominator has other factors such as 3, 7, 11, etc., the division will seldom come out even no matter how long it is continued but, as previously stated, this is of no consequence in practical work since it may be carried to whatever degree of accuracy is necessary. The digits in the quotient will usually repeat either singly or in groups, although there may first occur one or more digits which do not repeat. Such fractions are known as *repeating fractions*. They are sometimes indicated by an oblique line (fraction bar) through the digit which repeats, or through the first and last digits of a repeating group. Example:

$$\frac{1}{3} = 0.3333 \ldots = 0.\cancel{3}$$

$$\frac{1}{7} = 0.142857142857 \ldots = 0.\cancel{1}4285\cancel{7}$$

The foregoing examples contained only repeating digits. In the following example a non-repeating digit precedes the repeating digit:

$$\frac{7}{30} = 0.2333 \ldots = 0.2\cancel{3}$$

While repeating decimal fractions can be converted into their vulgar fraction equivalents, this is seldom necessary in practical work and the rules will be omitted here.

Powers and Roots When a number is to be multiplied by itself we say that it is to be *squared* or to be *raised to the second power*. When it is to be multipled by itself once again, we say that it is *cubed* or *raised to the third power*.

In general terms, when a number is to be multipled by itself we speak of *raising to a power* or *involution;* the number of times which the number is to be multiplied by itself is called the *order of the power*. The standard notation requires that the order of the power be indicated by a small number written after the number and above the line, called the *exponent*. Examples:

$2^2 = 2 \times 2$, or 2 **squared**, or the **second power of 2**

$2^3 = 2 \times 2 \times 2$, or 2 **cubed**, or the **third power of 2**

$2^4 = 2 \times 2 \times 2 \times 2$, or the **fourth power of 2**

Sometimes it is necessary to perform the reverse of this operation, that is, it may be necessary, for instance, to find that number which multiplied by itself will give a product of nine. The answer is of course 3. This process is known as *extracting the root* or *evolution*. The particular example which is cited would be written:

$$\sqrt{9} = 3$$

The sign for extracting the root is $\sqrt{\ }$, which is known as the *radical sign;* the order of the root is indicated by a small number above the radical as in $\sqrt[4]{\ }$, which would mean the fourth root; this number is called the *index*. When the radical bears no index, the square or second root is intended.

Restricting our attention for the moment to square root, we know that 2 is the square root of 4, and 3 is the square root of 9. If we want the square root of a number between 3 and 9, such as the square root of 5, it is obvious that it must lie between 2 and 3. In general the square root of such a number cannot be *exactly* expressed either by a vulgar fraction or a decimal fraction. However, the square root can be carried out decimally as far as may be necessary for sufficient accuracy. In general such a decimal fraction will contain a never-ending series of digits without repeating groups. Such a number is an *irrational number*, such as

$$\sqrt{5} = 2.2361 \ldots$$

The extraction of roots is usually done by tables or logarithms the use of which will be described later. There are longhand methods of extracting various roots, but we shall give only that for extracting the square root since the others become so tedious as to make other methods almost invariably preferable. Even the longhand method for extracting the square root will usually be used only if logarithm tables, slide rule, or table of roots are not handy.

Extracting the Square Root First divide the number the root of which is to be extracted into groups of two digits starting at the decimal point and going in both directions. If the lefthandmost group proves to have only one digit instead of two, no harm will be done. The righthandmost group may be made to have two digits by annexing a zero if necessary. For example, let it be required to find the square root of 5678.91. This is to be divided off as follows:

$$\sqrt{56'\,78.91}$$

The mark used to divide the groups may be anything convenient, although the prime-sign (′) is most commonly used for the purpose.

Next find the largest square which is contained in the first group, in this case 56. The largest square is obviously 49, the square of 7. Place the 7 above the first group of the number whose root is to be extracted, which is sometimes called the *dividend* from analogy to ordinary division. Place the square of this figure, that is 49, under the first group, 56, and subtract leaving a remainder of 7.

$$\begin{array}{l} \;\;7 \\ \sqrt{56'\,78.91} \\ \;\;49 \\ \;\;\overline{\;\;7} \end{array}$$

Bring down the next group and annex it to the remainder so that we have 778. Now to the left of this quantity write down twice the root so far found (2 × 7 or 14 in this example), annex a cipher as a trial divisor, and see how many times the result is contained in 778. In our example 140 will go into 778 5 times. Replace the cipher with a 5, and multiply the resulting 145 by 5 to give 725. Place the 5 directly above the second group in the dividend and then subtract the 725 from 778.

$$\begin{array}{rl} & \;\;7\;\;\;5 \\ & \sqrt{56'\,78.91} \\ & \;\;49 \\ 140 & \;\;\;\;7\;78 \\ 145 \times 5 = & \;\;\;\;7\;25 \\ & \;\;\;\;\;\;\;\;53 \end{array}$$

The next step is an exact repetition of the previous step. Bring down the third group and annex it to the remainder of 53, giving 5391. Write down twice the root already found and annex the cipher (2 x 75 or 150 plus the cipher, which will give 1500). 1500 will go into 5391 3 times. Replace the last cipher with a three and multiply 1503 by 3 to give 4509. Place 3 above the third group. Subtract to find the remainder of 882. The quotient 75.3 which has been found so far is not the exact square root which was desired; in most cases it will be sufficiently accurate. However, if greater accuracy is desired groups of two ciphers can be brought down and the process carried on as long as necessary.

$$\begin{array}{rl} & \;\;7\;\;\;5.\;\;3 \\ & \sqrt{56'\,78.91} \\ & \;\;49 \\ 140 & \;\;\;\;7\;78 \\ 145 \times 5 = & \;\;\;\;7\;25 \\ 1500 & \;\;\;\;\;\;\;\;53\;91 \\ 1503 \times 3 = & \;\;\;\;\;\;\;\;45\;09 \\ & \;\;\;\;\;\;\;\;\;\;8\;82 \end{array}$$

Each digit of the root should be placed directly above the group of the dividend from which it was derived; if this is done the decimal point of the root will come directly above the decimal point of the dividend.

Sometimes the remainder after a square has been subtracted (such as the 1 in the following example) will not be sufficiently large to contain twice the root already found even after the next group of figures has been brought down. In this case we write a cipher above the group just brought down and bring down another group.

$$\begin{array}{rl} & \;\;7.\;\;0\;\;\;8\;\;\;2 \\ & \sqrt{50.16'\,00'\,00} \\ & \;\;49 \\ 1400 & \;\;\;\;1\;16\;00 \\ 1408 \times 8 = & \;\;\;\;1\;12\;64 \\ 14160 & \;\;\;\;\;\;\;\;3\;36\;00 \\ 14162 \times 2 = & \;\;\;\;\;\;\;\;2\;83\;24 \\ & \;\;\;\;\;\;\;\;\;\;\;52\;76 \end{array}$$

In the above example the amount 116 was not sufficient to contain twice the root already found with a cipher annexed to it; that is, it was not sufficient to contain 140. Therefore we write a zero above 16 and bring down the next group, which in this example is a pair of ciphers.

Order of Operations One frequently encounters problems in which several of the fundamental operations of arithmetic which have been described are to be performed. The order in which these operations must be performed is important. First all powers and roots should be calculated; multiplication and division come next; adding and subtraction come last. In the example

$$2 + 3 \times 4^2$$

we must first square the 4 to get 16; then we multiply 16 by 3, making 48, and to the product we add 2, giving a result of 50.

If a different order of operations were followed, a different result would be obtained. For instance, if we add 2 to 3 we would obtain 5, and then multiplying this by the square of 4 or 16, we would obtain a result of 80, which is incorrect.

In more complicated forms such as fractions whose numerators and denominators may both be in complicated forms, the numerator and denominator are first found separately before the division is made, such as in the following example:

$$\frac{3 \times 4 + 5 \times 2}{2 \times 3 + 2 + 3} = \frac{12 + 10}{6 + 2 + 3} = \frac{22}{11} = 2$$

Problems of this type are very common in dealing with circuits containing several inductances, capacities, or resistances.

The order of operations specified above does not always meet all possible conditions; if a series of operations should be performed in a different order, this is always indicated by *parentheses* or *brackets*, for example:

$$2 + 3 \times 4^2 = 2 + 3 \times 16 = 2 + 48 = 50$$
$$(2 + 3) \times 4^2 = 5 \times 4^2 = 5 \times 16 = 80$$
$$2 + (3 \times 4)^2 = 2 + 12^2 = 2 + 144 = 146$$

In connection with the radical sign, brackets may be used or the "hat" of the radical may be extended over the entire quantity whose root is to be extracted. Example:

$$\surd 4 + 5 = \sqrt{4} + 5 = 2 + 5 = 7$$
$$\surd (4 + 5) = \sqrt{4 + 5} = \sqrt{9} = 3$$

It is recommended that the radical always be extended over the quantity whose root is to be extracted to avoid any ambiguity.

Cancellation In a fraction in which the numerator and denominator consist of several factors to be multiplied, considerable labor can often be saved if it is found that the same factor occurs in both numerator and denominator. These factors cancel each other and can be removed. Example:

$$\frac{\cancel{2} \times \cancel{3} \times \overset{5}{\cancel{25}}}{\underset{\cancel{2}}{\cancel{6}} \times \cancel{5} \times 7} = \frac{5}{7}$$

In the foregoing example it is obvious that the 3 in the numerator goes into the 6 in the denominator twice. We may thus cross out the three and replace the 6 by a 2. The 2 which we have just placed in the denominator cancels the 2 in the numerator. Next the 5 in the denominator will go into the 25 in the numerator leaving a result of 5. Now we have left only a 5 in the numerator and a 7 in the denominator, so our final result is 5/7. If we had multiplied $2 \times 3 \times 25$ to obtain 150 and then had divided this by $6 \times 5 \times 7$ or 210, we would have obtained the same result but, with considerably more work.

Algebra

Algebra is not a separate branch of mathematics but is merely a form of *generalized arithmetic* in which letters of the alphabet and occasional other symbols are substituted for numbers, from which it is often referred to as *literal notation*. It is simply a shorthand method of writing operations which could be spelled out.

The laws of most common electrical phenomena and circuits (including of course radio phenomena and circuits) lend themselves particularly well to representation by literal notation and solution by algebraic equations or formulas.

While we may write a particular problem in Ohm's Law as an ordinary division or multiplication, the general statement of all such problems calls for the replacement of the numbers by symbols. We might be explicit and write out the names of the units and use these names as symbols:

$$\text{volts} = \text{amperes} \times \text{ohms}$$

Such a procedure becomes too clumsy when the expression is more involved and would be unusually cumbersome if any operations like multiplication were required. Therefore as a short way of writing these generalized relations the numbers are represented by letters. Ohm's Law then becomes

$$E = I \times R$$

In the statement of any particular problem the significance of the letters is usually indicated directly below the equation or formula using them unless there can be no ambiguity. Thus the above form of Ohm's Law would be more completely written as:

$$E = I \times R$$

where E = e.m.f. in volts
I = current in amperes
R = resistance in ohms

Letters therefore represent numbers, and for any letter we can read "any number." When the same letter occurs again in the same expression we would mentally read "the same number," and for another letter "another number of any value."

These letters are connected by the usual operational symbols of arithmetic, +, −, ×, ÷, and so forth. In algebra, the sign for division is seldom used, a division being usually written as a fraction. The multiplication sign, ×, is usually omitted or one may write a period only. Examples:

$$2 \times a \times b = 2ab$$
$$2.3.4.5a = 2 \times 3 \times 4 \times 5 \times a$$

In practical applications of algebra, an expression usually states some physical law and each letter represents a variable quantity which is therefore called a *variable.* A fixed number in front of such a quantity (by which it is to be multiplied) is known as the *coefficient.* Sometimes the coefficient may be unknown, yet to be determined; it is then also written as a letter; *k* is most commonly used for this purpose.

The Negative Sign In ordinary arithmetic we seldom work with negative numbers, although we may be "short" in a subtraction. In algebra, however, a number may be either negative or positive. Such a thing may seem *academic* but a negative quantity can have a real existence. We need only refer to a *debt* being considered a negative possession. In electrical work, however, a result of a problem might be a negative number of amperes or volts, indicating that the direction of the current is opposite to the direction chosen as positive. We shall have illustrations of this shortly.

Having established the existence of negative quantities, we must now learn how to work with these negative quantities in addition, subtraction, multiplication and so forth.

In addition, a negative number added to a positive number is the same as subtracting a positive number from it.

$$\begin{array}{r} 7 \\ -3 \\ \hline 4 \end{array} \text{ (add) is the same as } \begin{array}{r} 7 \\ 3 \\ \hline 4 \end{array} \text{ (subtract)}$$

or we might write it

$$7 + (-3) = 7 - 3 = 4$$

Similarly, we have:

$$a + (-b) = a - b$$

When a minus sign is in front of an expression in brackets, this minus sign has the effect of reversing the signs of every term within the brackets:

$$-(a - b) = -a + b$$
$$-(2a + 3b - 5c) = -2a - 3b + 5c$$

Multiplication. When both the multiplicand and the multiplier are negative, the product is positive. When only one (either one) is negative the product is negative. The four possible cases are illustrated below:

$$+ \times + = + \qquad + \times - = -$$
$$- \times + = - \qquad - \times - = +$$

Division. Since division is but the reverse of multiplication, similar rules apply for the sign of the quotient. When both the dividend and the divisor have the same sign (both negative or both positive) the quotient is positive. If they have unlike signs (one positive and one negative) the quotient is negative.

$$\frac{+}{+} = + \qquad \frac{+}{-} = -$$
$$\frac{-}{+} = - \qquad \frac{-}{-} = +$$

Powers. Even powers of negative numbers are positive and *odd* powers are negative. Powers of positive numbers are always positive. Examples:

$$-2^2 = -2 \times -2 = +4$$
$$-2^3 = -2 \times -2 \times -2 = +4 \times -2 = -8$$

Roots. Since the square of a negative number is positive and the square of a positive number is also positive, it follows that a positive number has two square roots. The square root of 4 can be either +2 or −2 for (+2) × (+2) = +4 and (−2) × (−2) = +4.

Addition and Subtraction *Polynomials* are quantities like $3ab^2 + 4ab^3 - 7a^2b^4$ which have several terms of different *names.* When adding polynomials, only terms of the same name can be taken together.

$$\begin{array}{rrrrr} 7a^3 + & 8\,ab^2 + & 3\,a^2b & & + 3 \\ a^3 - & 5\,ab^2 & & - b^3 & \\ \hline 8a^3 + & 3\,ab^2 + & 3\,a^2b & - b^3 & + 3 \end{array}$$

Collecting terms. When an expression contains more than one term of the same name, these can be added together and the expression made simpler:

$$5x^2 + 2xy + 3xy^2 - 3x^2 + 7xy =$$

$$5x^2 - 3x^2 + 2xy + 7xy + 3xy^2 =$$

$$2x^2 + 9xy + 3xy^2$$

Multiplication Multiplication of single terms is indicated simply by writing them together.

$a \times b$ is written as ab

$a \times b^2$ is written as ab^2

Bracketed quantities are multiplied by a single term by multiplying each term:

$$a(b + c + d) = ab + ac + ad$$

When two bracketed quantities are multiplied, each term of the first bracketed quantity is to be multiplied by each term of the second bracketed quantity, thereby making every possible combination.

$$(a + b)(c + d) = ac + ad + bc + bd$$

In this work particular care must be taken to get the signs correct. Examples:

$$(a + b)(a - b) = a^2 + ab - ab - b^2 = a^2 - b^2$$

$$(a + b)(a + b) = a^2 + ab + ab + b^2 = a^2 + 2ab + b^2$$

$$(a - b)(a - b) = a^2 - ab - ab + b^2 = a^2 - 2ab + b^2$$

Division It is possible to do longhand division in algebra, although it is somewhat more complicated than in arithmetic. However, the division will seldom come out even, and is not often done in this form. The method is as follows: Write the terms of the dividend in the order of descending powers of one variable and do likewise with the divisor. Example:

Divide $5a^2b + 21b^3 + 2a^3 - 26ab^2$ by $2a - 3b$

Write the dividend in the order of descending powers of a and divide in the same way as in arithmetic.

$$\begin{array}{r|l}
 & a^2 + 4ab - 7b^2 \\
2a - 3b & 2a^3 + 5a^2b - 26ab^2 + 21b^3 \\
 & 2a^3 - 3a^2b \\ \hline
 & + 8a^2b - 26ab^2 \\
 & + 8a^2b - 12ab^2 \\ \hline
 & - 14ab^2 + 21b^3 \\
 & - 14ab^2 + 21b^3 \\ \hline
\end{array}$$

Another example: Divide $x^3 - y^3$ by $x - y$

$$\begin{array}{r|l}
x - y & x^3 + 0 + 0 - y^3 \ (\ x^2 + xy + y^2 \\
 & x^3 - x^2y \\ \hline
 & + x^2y \\
 & x^2y - xy^2 \\ \hline
 & + xy^2 - y^3 \\
 & xy^2 - y^3 \\ \hline
\end{array}$$

Factoring Very often it is necessary to simplify expressions by finding a factor. This is done by collecting two or more terms having the same factor and bringing the factor outside the brackets:

$$6ab + 3ac = 3a(2b + c)$$

In a four term expression one can take together two terms at a time; the intention is to try getting the terms within the brackets the same after the factor has been removed:

$$30ac - 18bc + 10ad - 6bd =$$
$$6c(5a - 3b) + 2d(5a - 3b) =$$
$$(5a - 3b)(6c + 2d)$$

Of course, this is not always possible and the expression may not have any factors. A similar process can of course be followed when the expression has six or eight or any even number of terms.

A special case is a three-term polynomial, which can sometimes be factored by writing the middle term as the sum of two terms:

$x^2 - 7xy + 12y^2$ may be rewritten as

$$x^2 - 3xy - 4xy + 12y^2 =$$
$$x(x - 3y) - 4y(x - 3y) =$$
$$(x - 4y)(x - 3y)$$

The middle term should be split into two in such a way that the sum of the two new terms equals the original middle term and that their product equals the product of the two outer terms. In the above example these conditions are fulfilled for $-3xy - 4xy = -7xy$ and $(-3xy)(-4xy) = 12x^2y^2$. It is not always possible to do this and there are then no simple factors.

Working with Powers and Roots When two powers of the same number are to be multiplied, the exponents are *added.*

$$a^2 \times a^3 = aa \times aaa = aaaaa = a^5 \text{ or}$$
$$a^2 \times a^3 = a^{(2+3)} = a^5$$

$$b^3 \times b = b^4$$

$$c^5 \times c^7 = c^{12}$$

Similarly, dividing of powers is done by subtracting the exponents.

$$\frac{a^3}{a^2} = \frac{aaa}{aa} = a \text{ or } \frac{a^3}{a^2} = a^{(3-2)} = a^1 = a$$

$$\frac{b^5}{b^3} = \frac{bbbbb}{bbb} = b^2 \text{ or } \frac{b^5}{b^3} = b^{(5-3)} = b^2$$

Now we are logically led into some important new ways of notation. We have seen that when dividing, the exponents are subtracted. This can be continued into negative exponents. In the following series, we successively divide by *a* and since this can now be done in two ways, the two ways of notation must have the same meaning and be identical.

a^5	a^2	$a^{-1} = \frac{1}{a}$
a^4	$a^1 = a$	$a^{-2} = \frac{1}{a^2}$
a^3	$a^0 = 1$	$a^{-3} = \frac{1}{a^3}$

These examples illustrate two rules: (1) any number raised to "zero" power equals one or unity; (2) any quantity raised to a negative power is the inverse or reciprocal of the same quantity raised to the same positive power.

$$n^0 = 1 \qquad a^{-n} = \frac{1}{a^n}$$

Roots. The product of the square root of two quantities equals the square root of their product.

$$\sqrt{a} \times \sqrt{b} = \sqrt{ab}$$

Also, the quotient of two roots is equal to the root of the quotient.

$$\frac{\sqrt{a}}{\sqrt{b}} = \sqrt{\frac{a}{b}}$$

Note, however, that in addition or subtraction the square root of the sum or difference is *not* the same as the sum or difference of the square roots.

$$\text{Thus, } \sqrt{9} - \sqrt{4} = 3 - 2 = 1$$
$$\text{but } \sqrt{9-4} = \sqrt{5} = 2.2361$$
$$\text{Likewise } \sqrt{a} + \sqrt{b} \text{ is not the same as } \sqrt{a+b}$$

Roots may be written as fractional powers. Thus $\sqrt{a}$ may be written as $a^{1/2}$ because

$$\sqrt{a} \times \sqrt{a} = a$$
$$\text{and, } a^{1/2} \times a^{1/2} = a^{1/2+1/2} = a^1 = a$$

Any root may be written in this form

$$\sqrt{b} = b^{1/2} \quad \sqrt[3]{b} = b^{1/3} \quad \sqrt[3]{b^2} = b^{2/3}$$

The same notation is also extended in the negative direction:

$$b^{-1/2} = \frac{1}{b^{1/2}} = \frac{1}{\sqrt{b}} \qquad c^{-1/3} = \frac{1}{c^{1/3}} = \frac{1}{\sqrt[3]{c}}$$

Following the previous rules that exponents add when powers are multiplied,

$$\sqrt[3]{a} \times \sqrt[3]{a} = \sqrt[3]{a^2}$$
$$\text{but also } a^{1/3} \times a^{1/3} = a^{2/3}$$
$$\text{therefore } a^{2/3} = \sqrt[3]{a^2}$$

Powers of powers. When a power is again raised to a power, the exponents are multiplied;

$$(a^2)^3 = a^6 \qquad (b^{-1})^3 = b^{-3}$$
$$(a^3)^4 = a^{12} \qquad (b^{-2})^{-4} = b^8$$

This same rule also applies to roots of roots and also powers of roots and roots of powers because a root can always be written as a fractional power.

$$\sqrt[3]{\sqrt{a}} = \sqrt[6]{a} \text{ for } (a^{1/2})^{1/3} = a^{1/6}$$

Removing radicals. A root or radical in the denominator of a fraction makes the expression difficult to handle. If there must be a radical it should be located in the numerator rather than in the denominator. The removal of the radical from the denominator is done by multiplying both numerator and denominator by a quantity which will remove the radical from the denominator, thus *rationalizing* it:

$$\frac{1}{\sqrt{a}} = \frac{\sqrt{a}}{\sqrt{a} \times \sqrt{a}} = \frac{1}{a}\sqrt{a}$$

Suppose we have to rationalize

$\dfrac{3a}{\sqrt{a} + \sqrt{b}}$ In this case we must multiply numerator and denominator by $\sqrt{a} - \sqrt{b}$, the same terms but with the second having the opposite sign, so that their product will not contain a root.

$$\frac{3a}{\sqrt{a} + \sqrt{b}} = \frac{3a(\sqrt{a} - \sqrt{b})}{(\sqrt{a}+\sqrt{b})(\sqrt{a} - \sqrt{b})} = \frac{3a(\sqrt{a} - \sqrt{b})}{a - b}$$

Imaginary Numbers Since the square of a negative number is positive and the square of a positive number is also positive, the square root of a negative number can be neither positive nor negative. Such a number is said to be *imaginary;* the most common such number ($\sqrt{-1}$) is often represented by the letter i in mathematical work or j in electrical work.

$$\sqrt{-1} = i \text{ or } j \text{ and } i^2 \text{ or } j^2 = -1$$

Imaginary numbers do not exactly correspond to anything in our experience and it is best not to try to visualize them. Despite this fact, their interest is much more than academic, for they are extremely useful in many calculations involving alternating currents.

The square root of any other negative number may be reduced to a product of two roots, one positive and one negative. For instance:

$$\sqrt{-57} = \sqrt{-1}\ \sqrt{57} = i\sqrt{57}$$

or, in general

$$\sqrt{-a} = i\sqrt{a}$$

Since $i = \sqrt{-1}$, the powers of i have the following values:

$$i^2 = -1$$
$$i^3 = -1 \times i = -i$$
$$i^4 = +1$$
$$i^5 = +1 \times i = i$$

Imaginary numbers are different from either positive or negative numbers; so in addition or subtraction they must always be accounted for separately. Numbers which consist of both real and imaginary parts are called *complex* numbers. Examples of complex numbers:

$$3 + 4i = 3 + 4\sqrt{-1}$$
$$a + bi = a + b\sqrt{-1}$$

Since an imaginary number can never be equal to a real number, it follows that in an equality like

$$a + bi = c + di$$

a must equal c and bi must equal di

Complex numbers are handled in algebra just like any other expression, considering i as a known quantity. Whenever powers of i occur, they can be replaced by the equivalents given above. This idea of having in one equation two separate sets of quantities which must be accounted for separately, has found a symbolic application in vector notation. These are covered later in this chapter.

Equations of the First Degree Algebraic expressions usually come in the form of equations, that is, one set of terms equals another set of terms. The simplest example of this is Ohm's Law:

$$E = IR$$

One of the three quantities may be unknown but if the other two are known, the third can be found readily by substituting the known values in the equation. This is very easy if it is E in the above example that is to be found; but suppose we wish to find I while E and R are given. We must then rearrange the equation so that I comes to stand alone to the left of the equality sign. This is known as *solving the equation for I.*

Solution of the equation in this case is done simply by transposing. If two things are equal then they must still be equal if both are multiplied or divided by the same number. Dividing both sides of the equation by R:

$$\frac{E}{R} = \frac{IR}{R} = I \text{ or } I = \frac{E}{R}$$

If it were required to solve the equation for R, we should divide both sides of the equation by I.

$$\frac{E}{I} = R \text{ or } R = \frac{E}{I}$$

A little more complicated example is the equation for the reactance of a condenser:

$$X = \frac{1}{2\pi f C}$$

To solve this equation for C, we may multiply both sides of the equation by C and divide both sides by X

$$X \times \frac{C}{X} = \frac{1}{2\pi f C} \times \frac{C}{X}, \text{ or}$$
$$C = \frac{1}{2\pi f X}$$

This equation is one of those which requires a good knowledge of the placing of the decimal point when solving. Therefore we give a few examples: What is the reactance of a 25 $\mu\mu$fd. capacitor at 1000 kc.? In filling in the given values in the equation we must remember that the units used are farads, cycles, and ohms. Hence, we must write 25 $\mu\mu$fd. as 25 millionths of a millionth of a farad or 25×10^{-12} farad; similarly, 1000 kc. must be converted to 1,000,000 cycles. Substituting these values in the original equation, we have

$$X = \frac{1}{2 \times 3.14 \times 1{,}000{,}000 \times 25 \times 10^{-12}}$$

$$X = \frac{1}{6.28 \times 10^{6} \times 25 \times 10^{-12}} = \frac{10^{6}}{6.28 \times 25}$$
$$= 6360 \text{ ohms}$$

A bias resistor of 1000 ohms should be bypassed, so that at the lowest frequency the reactance of the condenser is 1/10th of that of the resistor. Assume the lowest frequency to be 50 cycles, then the required capacity should have a reactance of 100 ohms, at 50 cycles:

$$C = \frac{1}{2 \times 3.14 \times 50 \times 100} \text{ farads}$$

$$C = \frac{10^{6}}{6.28 \times 5000} \text{ microfarads}$$

$$C = 32 \ \mu\text{fd.}$$

In the third possible case, it may be that the frequency is the unknown. This happens for instance in some tone control problems. Suppose it is required to find the frequency which makes the reactance of a 0.03 μfd. condenser equal to 100,000 ohms.

First we must solve the equation for f. This is done by transposition.

$$X = \frac{1}{2\pi f C} \qquad f = \frac{1}{2\pi C X}$$

Substituting known values

$$f = \frac{1}{2 \times 3.14 \times 0.03 \times 10^{-6} \times 100{,}000} \text{ cycles}$$

$$f = \frac{1}{0.01884} \text{ cycles} = 53 \text{ cycles}$$

These equations are known as first degree equations with one unknown. First degree, because the unknown occurs only as a first power. Such an equation always has one possible solution or *root* if all the other values are known.

If there are two unknowns, a single equation will not suffice, for there are then an infinite number of possible solutions. In the case of two unknowns we need *two independent* simultaneous equations. An example of this is:

$$3x + 5y = 7 \qquad 4x - 10y = 3$$

Required, to find x and y.

This type of work is done either by the *substitution method* or by the *elimination method*. In the substitution method we might write for the first equation:

$$3x = 7 - 5y \therefore x = \frac{7 - 5y}{3}$$

(The symbol $\therefore$ means *therefore* or *hence*).

This value of x can then be substituted for x in the second equation making it a single equation with but one unknown, y.

It is, however, simpler in this case to use the elimination method. Multiply both sides of the first equation by two and add it to the second equation:

$$\begin{aligned} 6x + 10y &= 14 \\ 4x - 10y &= 3 \quad \text{add} \\ \hline 10x \quad &= 17 \qquad x = 1.7 \end{aligned}$$

Substituting this value of x in the first equation, we have

$$5.1 + 5y = 7 \therefore 5y = 7 - 5.1 = 1.9 \therefore$$
$$y = 0.38$$

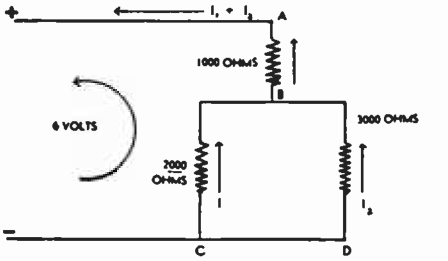


Figure 3.

In this simple network the current divides through the 2000-ohm and 3000-ohm resistors. The current through each may be found by using two simultaneous linear equations. Note that the arrows indicate the direction of electron flow as explained on page 18.

An application of two simultaneous linear equations will now be given. In Figure 3 a simple network is shown consisting of three resistances; let it be required to find the currents I_1 and I_2 in the two branches.

The general way in which all such problems can be solved is to assign directions to the currents through the various resistances. When these are chosen wrong it will do no harm for the result of the equations will then be negative, showing up the error. In this simple illustration there is, of course, no such difficulty.

Next we write the equations for the meshes, in accordance with Kirchhoff's second law. All voltage drops in the direction of the curved arrow are considered positive, the reverse ones negative. Since there are two unknowns we write two equations.

$$1000\ (I_1 + I_2) + 2000\ I_1 = 6$$

$$-2000\ I_1 + 3000\ I_2 = 0$$

Expand the first equation

$$3000\ I_1 + 1000\ I_2 = 6$$

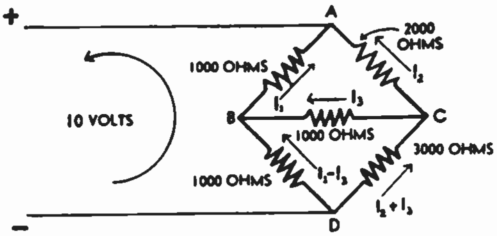


Figure 4.

A MORE COMPLICATED PROBLEM REQUIRING THE SOLUTION OF CURRENTS IN A NETWORK.

This problem is similar to that in Figure 3 but requires the use of three simultaneous linear equations.

Multiply this equation by 3

$$9000\, I_1 + 3000\, I_2 = 18$$

Subtracting the second equation from the first

$$11000\, I_1 = 18$$
$$I_1 = 18/11000 = 0.00164 \text{ amp.}$$

Filling in this value in the second equation

$$3000\, I_2 = 3.28 \qquad I_2 = 0.00109 \text{ amp.}$$

A similar problem but requiring three equations is shown in Figure 4. This consists of an unbalanced bridge and the problem is to find the current in the bridge-branch, I_3. We again assign directions to the different currents, guessing at the one marked I_3. The voltages around closed loops ABC [eq. (1)] and BDC [eq. (2)] equal zero and are assumed to be positive in a counterclockwise direction; that from D to A equals 10 volts [eq. (3)].

(1)

$$-1000\, I_1 + 2000\, I_2 - 1000\, I_3 = 0$$

(2)

$$-1000\,(I_1 - I_3) + 1000\, I_3 + 3000\,(I_2 + I_3) = 0$$

(3)

$$1000\, I_1 + 1000\,(I_1 - I_3) - 10 = 0$$

Expand equations (2) and (3)

(2)

$$-1000\, I_1 + 3000\, I_2 + 5000\, I_3 = 0$$

(3)

$$2000\, I_1 - 1000\, I_3 - 10 = 0$$

Subtract equation (2) from equation (1)

(a)

$$-1000\, I_2 - 6000\, I_3 = 0$$

Multiply the second equation by 2 and add it to the third equation

(b)

$$6000\, I_2 + 9000\, I_3 - 10 = 0$$

Now we have but two equations with two unknowns.

Multiplying equation (a) by 6 and adding to equation (b) we have

$$-27000\, I_3 - 10 = 0$$
$$I_3 = -10/27000 = -0.00037 \text{ amp.}$$

Note that now the solution is negative which means that we have drawn the arrow for I_3 in Figure 4 in the wrong direction. The current is 0.37 ma. in the other direction.

Second Degree or Quadratic Equations A somewhat similar problem in radio would be, if power in watts and resistance in ohms of a circuit are given, to find the voltage and the current. Example: When lighted to normal brilliancy, a 100 watt lamp has a resistance of 49 ohms; for what line voltage was the lamp designed and what current would it take.

Here we have to use the simultaneous equations:

$$P = EI \quad \text{and} \quad E = IR$$

Filling in the known values:

$$P = EI = 100 \text{ and } E = IR = I \times 49$$

Substitute the second equation into the first equation

$$P = EI = (I) \times I \times 49 = 49\, I^2 = 100$$

$$\therefore\ I = \sqrt{\frac{100}{49}} = \frac{10}{7} = 1.43 \text{ amp.}$$

Substituting the found value of 1.43 amp. for I in the first equation, we obtain the value of the line voltage, 70 volts.

Note that this is a *second degree* equation for we finally had the second power of I. Also, since the current in this problem could only be positive, the negative square root of 100/49 or $-10/7$ was not used. Strictly speaking, however, there are two more values that satisfy both equations, these are -1.43 and -70.

In general, a second degree equation in one unknown has two roots, a third degree equation three roots, etc.

The Quadratic Equation Quadratic or second degree equations with but one unknown can be reduced to the general form

$$ax^2 + bx + c = 0$$

where x is the unknown and a, b, and c are constants.

This type of equation can sometimes be solved by the method of factoring a three-term expression as follows:

$$2x^2 + 7x + 6 = 0$$

$$2x^2 + 4x + 3x + 6 = 0$$

factoring:

$$2x(x + 2) + 3(x + 2) = 0$$

$$(2x + 3)(x + 2) = 0$$

There are two possibilities when a product is zero. Either the one or the other factor equals zero. Therefore there are two solutions.

$$2x_1 + 3 = 0 \qquad x_2 + 2 = 0$$

$$2x_1 = -3 \qquad x_2 = -2$$

$$x_1 = -1\tfrac{1}{2}$$

Since factoring is not always easy, the following general solution can usually be employed; in this equation a, b, and c are the coefficients referred to above.

$$x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

Applying this method of solution to the previous example:

$$x = \frac{-7 \pm \sqrt{49 - 8 \times 6}}{4} = \frac{-7 \pm \sqrt{1}}{4} = \frac{-7 \pm 1}{4}$$

$$x_1 = \frac{-7 + 1}{4} = -1\tfrac{1}{2}$$

$$x_2 = \frac{-7 - 1}{4} = -2$$

A practical example involving quadratics is the law of impedance in a.c. circuits. However, this is a simple kind of quadratic equation which can be solved readily without the use of the special formula given above.

$$Z = \sqrt{R^2 + (X_L - X_C)^2}$$

This equation can always be solved for R, by squaring both sides of the equation. It should now be understood that squaring both sides of an equation as well as multiplying both sides with a term containing the unknown *may add a new root.* Since we know here that Z and R are positive, when we square the expression there is no ambiguity.

$$Z^2 = R^2 + (X_L - X_C)^2$$

$$\text{and } R^2 = Z^2 - (X_L - X_C)^2$$

$$\text{or } R = \sqrt{Z^2 - (X_L - X_C)^2}$$

$$\text{Also: } (X_L - X_C)^2 = Z^2 - R^2$$

$$\text{and } \pm (X_L - X_C) = \sqrt{Z^2 - R^2}$$

But here we do not know the sign of the solution unless there are other facts which indicate it. To find either X_L or X_C alone it would have to be known whether the one or the other is the larger.

Logarithms

Definition and Use A logarithm is the power (or exponent) to which we must raise one number to obtain another. Although the large numbers used in logarithmic work may make them seem difficult or complicated, in reality the principal use of logarithms is to *simplify* calculations which would otherwise be extremely laborious.

We have seen so far that every operation in arithmetic can be reversed. If we have the addition:

$$a + b = c$$

we can reverse this operation in two ways. It may be that b is the unknown, and then we reverse the equation so that it becomes

$$c - a = b$$

It is also possible that we wish to know a, and that b and c are given. The equation then becomes

$$c - b = a$$

We call both of these reversed operations *subtraction,* and we make no distinction between the two possible reverses.

Multiplication can also be reversed in two manners. In the multiplication

$$ab = c$$

we may wish to know a, when b and c are given, or we may wish to know b when a and c are given. In both cases we speak of *division,* and we make again no distinction between the two.

In the case of powers we can also reverse the operation in two manners, but now they are not equivalent. Suppose we have the equation

$$a^b = c$$

If a is the unknown, and b and c are given, we may reverse the operation by writing

$$\sqrt[b]{c} = a$$

This operation we call *taking the root.* But there is a third possibility: that a and c are given, and that we wish to know b. In other words, the question is "to which power must we raise a so as to obtain c?". This operation is known as *taking the logarithm*, and b is the logarithm of c to the base a. We write this operation as follows:

$$\log_a c = b$$

Consider a numerical example. We know $2^3=8$. We can reverse this operation by asking "to which power must we raise *2* so as to obtain *8?*" Therefore, the logarithm of *8* to the base *2* is *3*, or

$$\log_2 8 = 3$$

Taking any single base, such as *2*, we might write a series of all the powers of the base next to the series of their logarithms:

Number:	2	4	8	16	32	64	128	256	512	1024
Logarithm:	1	2	3	4	5	6	7	8	9	10

We can expand this table by finding terms between the terms listed above. For instance, if we let the logarithms increase with ½ each time, successive terms in the upper series would have to be multiplied by the square root of 2. Similarly, if we wish to increase the logarithm by 1/10 at each term, the ratio between two consecutive terms in the upper series would be the tenth root of 2. Now this short list of numbers constitutes a small logarithm table. It should be clear that one could find the logarithm of any number to the base 2. This logarithm will usually be a number with many decimals.

Logarithmic Bases The fact that we chose 2 as a base for the illustration is purely arbitrary. Any base could be used, and therefore there are many possible systems of logarithms. In practice we use only two bases: The most frequently used base is 10, and the system using this base is known as the system of *common* logarithms, or Briggs' logarithms. The second system employs as a base an odd number, designated by the letter e; $e = 2.71828\ldots$ This is known as the *natural* logarithmic system, also as the Napierian systèm, and the hyperbolic system. Although different writers may vary on the subject, the usual notation is simply *log a* for the common logarithm of a, and $\log_e a$ (or sometimes *ln a)* for the natural logarithm of a. We shall use the common logarithmic system in most cases, and therefore we shall examine this system more closely.

Common Logarithms In the system wherein *10* is the base, the logarithm of *10* equals *1*; the logarithm of *100* equals *2*, etc., as shown in the following table:

$$\log\ 10 = \log 10^1 = 1$$
$$\log\ 100 = \log 10^2 = 2$$
$$\log\ 1{,}000 = \log 10^3 = 3$$
$$\log\ 10{,}000 = \log 10^4 = 4$$
$$\log\ 100{,}000 = \log 10^5 = 5$$
$$\log\ 1{,}000{,}000 = \log 10^6 = 6$$

This table can be extended for numbers less than 10 when we remember the rules of powers discussed under the subject of algebra. Numbers less than unity, too, can be written as powers of ten.

$$\log 1 = \log 10^0 = 0$$
$$\log 0.1 = \log 10^{-1} = -1$$
$$\log 0.01 = \log 10^{-2} = -2$$
$$\log 0.001 = \log 10^{-3} = -3$$
$$\log 0.0001 = \log 10^{-4} = -4$$

From these examples follow several rules: The logarithm of any number between zero and + 1 is negative; the logarithm of zero is minus infinity; the logarithm of a number greater than + 1 is positive. *Negative numbers have no logarithm.* These rules are true of common logarithms and of logarithms to any base.

The logarithm of a number between the powers of ten is an irrational number, that is, it has a never ending series of decimals. For instance, the logarithm of 20 must be between 1 and 2 because 20 is between 10 and 100; the value of the logarithm of 20 is 1.30103. . . . The part of the logarithm to the left of the decimal point is called the *characteristic*, while the decimals are called the *mantissa*. In the case of 1.30103 . ., the logarithm of 20, the characteristic is 1 and the mantissa is .30103 . .

Properties of Logarithms If the base of our system is ten, then, by definition of a logarithm:

$$10^{\log a} = a$$

or, if the base is raised to the power having an exponent equal to the logarithm of a number, the result is that number.

The logarithm of a *product* is equal to the *sum* of the logarithms of the two factors.

$$\log ab = \log a + \log b$$

This is easily proved to be true because, it

Figure 5. FOUR PLACE LOGARITHM TABLES.

N	0	1	2	3	4	5	6	7	8	9
10	0000	0043	0086	0128	0170	0212	0253	0294	0334	0374
11	0414	0453	0492	0531	0569	0607	0645	0682	0719	0755
12	0792	0828	0864	0899	0934	0969	1004	1038	1072	1106
13	1139	1173	1206	1239	1271	1303	1335	1367	1399	1430
14	1461	1492	1523	1553	1584	1614	1644	1673	1703	1732
15	1761	1790	1818	1847	1875	1903	1931	1959	1987	2014
16	2041	2068	2095	2122	2148	2175	2201	2227	2253	2279
17	2304	2330	2355	2380	2405	2430	2455	2480	2504	2529
18	2553	2577	2601	2625	2648	2672	2695	2718	2742	2765
19	2788	2810	2833	2856	2878	2900	2923	2945	2967	2989
20	3010	3032	3054	3075	3096	3118	3139	3160	3181	3201
21	3222	3243	3263	3284	3304	3324	3345	3365	3385	3404
22	3424	3444	3464	3483	3502	3522	3541	3560	3579	3598
23	3617	3636	3655	3674	3692	3711	3729	3747	3766	3784
24	3802	3820	3838	3856	3874	3892	3909	3927	3945	3962
25	3979	3997	4014	4031	4048	4065	4082	4099	4116	4133
26	4150	4166	4183	4200	4216	4232	4249	4265	4281	4298
27	4314	4330	4346	4362	4378	4393	4409	4425	4440	4456
28	4472	4487	4502	4518	4533	4548	4564	4579	4594	4609
29	4624	4639	4654	4669	4683	4698	4713	4728	4742	4757
30	4771	4786	4800	4814	4829	4843	4857	4871	4886	4900
31	4914	4928	4942	4955	4969	4983	4997	5011	5024	5038
32	5051	5065	5079	5092	5105	5119	5132	5145	5159	5172
33	5185	5198	5211	5224	5237	5250	5263	5276	5289	5302
34	5315	5328	5340	5353	5366	5378	5391	5403	5416	5428
35	5441	5453	5465	5478	5490	5502	5514	5527	5539	5551
36	5563	5575	5587	5599	5611	5623	5635	5647	5658	5670
37	5682	5694	5705	5717	5729	5740	5752	5763	5775	5786
38	5798	5809	5821	5832	5843	5855	5866	5877	5888	5899
39	5911	5922	5933	5944	5955	5966	5977	5988	5999	6010
40	6021	6031	6042	6053	6064	6075	6085	6096	6107	6117
41	6128	6138	6149	6160	6170	6180	6191	6201	6212	6222
42	6232	6243	6253	6263	6274	6284	6294	6304	6314	6325
43	6335	6345	6355	6365	6375	6385	6395	6405	6415	6425
44	6435	6444	6454	6464	6474	6484	6493	6503	6513	6522
45	6532	6542	6551	6561	6571	6580	6590	6599	6609	6618
46	6628	6637	6646	6656	6665	6675	6684	6693	6702	6712
47	6721	6730	6739	6749	6758	6767	6776	6785	6794	6803
48	6812	6821	6830	6839	6848	6857	6866	6875	6884	6893
49	6902	6911	6920	6928	6937	6946	6955	6964	6972	6981
50	6990	6998	7007	7016	7024	7033	7042	7050	7059	7067
51	7076	7084	7093	7101	7110	7118	7126	7135	7143	7152
52	7160	7168	7177	7185	7193	7202	7210	7218	7226	7235
53	7243	7251	7259	7267	7275	7284	7292	7300	7308	7316
54	7324	7332	7340	7348	7356	7364	7372	7380	7388	7396

N	0	1	2	3	4	5	6	7	8	9
55	7404	7412	7419	7427	7435	7443	7451	7459	7466	7474
56	7482	7490	7497	7505	7513	7520	7528	7536	7543	7551
57	7559	7566	7574	7582	7589	7597	7604	7612	7619	7527
58	7634	7642	7649	7657	7664	7672	7679	7686	7694	7701
59	7709	7716	7723	7731	7738	7745	7752	7760	7767	7774
60	7782	7789	7796	7803	7810	7818	7825	7832	7839	7846
61	7853	7860	7868	7875	7882	7889	7896	7903	7910	7917
62	7924	7931	7938	7945	7952	7959	7966	7973	7980	7987
63	7993	8000	8007	8014	8021	8028	8035	8041	8048	8055
64	8062	8069	8075	8082	8089	8096	8102	8109	8116	8122
65	8129	8136	8142	8149	8156	8162	8169	8176	8182	8189
66	8195	8202	8209	8215	8222	8228	8235	8241	8248	8254
67	8261	8267	8274	8280	8287	8293	8299	8306	8312	8319
68	8325	8331	8338	8344	8351	8357	8363	8370	8376	8382
69	8388	8395	8401	8407	8414	8420	8426	8432	8439	8445
70	8451	8457	8463	8470	8476	8482	8488	8494	8500	8506
71	8513	8519	8525	8531	8537	8543	8549	8555	8561	8567
72	8573	8579	8585	8591	8597	8603	8609	8615	8621	8627
73	8633	8639	8645	8651	8657	8663	8669	8675	8681	8686
74	8692	8698	8704	8710	8716	8722	8727	8733	8739	8745
75	8751	8756	8762	8768	8774	8779	8785	8791	8797	8802
76	8808	8814	8820	8825	8831	8837	8842	8848	8854	8859
77	8865	8871	8876	8882	8887	8893	8899	8904	8910	8915
78	8921	8927	8932	8938	8943	8949	8954	8960	8965	8971
79	8976	8982	8987	8993	8998	9004	9009	9015	9020	9025
80	9031	9036	9042	9047	9053	9058	9063	9069	9074	9079
81	9085	9090	9096	9101	9106	9112	9117	9122	9128	9133
82	9138	9143	9149	9154	9159	9165	9170	9175	9180	9186
83	9191	9196	9201	9206	9212	9217	9222	9227	9232	9238
84	9243	9248	9253	9258	9263	9269	9274	9279	9284	9289
85	9294	9299	9304	9309	9315	9320	9325	9330	9335	9340
86	9345	9350	9355	9360	9365	9370	9375	9380	9385	9390
87	9395	9400	9405	9410	9415	9420	9425	9430	9435	9440
88	9445	9450	9455	9460	9465	9469	9474	9479	9484	9489
89	9494	9499	9504	9509	9513	9518	9523	9528	9533	9538
90	9542	9547	9552	9557	9562	9566	9571	9576	9581	9586
91	9590	9595	9600	9605	9609	9614	9619	9624	9628	9633
92	9638	9643	9647	9652	9657	9661	9666	9671	9675	9680
93	9685	9689	9694	9699	9703	9708	9713	9717	9722	9727
94	9731	9736	9741	9745	9750	9754	9759	9763	9768	9773
95	9777	9782	9786	9791	9795	9800	9805	9809	9814	9818
96	9823	9827	9832	9836	9841	9845	9850	9854	9859	9863
97	9868	9872	9877	9881	9886	9890	9894	9899	9903	9908
98	9912	9917	9921	9926	9930	9934	9939	9943	9948	9952
99	9956	9961	9965	9969	9974	9978	9983	9987	9991	9996

was shown before that when multiplying to powers, the exponents are added; therefore,

$$a \times b = 10^{\log a} \times 10^{\log b} = 10^{(\log a + \log b)}$$

Similarly, the logarithm of a quotient is the difference between the logarithm of the dividend and the logarithm of the divisor.

$$\log \frac{a}{b} = \log a - \log b$$

This is so because by the same rules of exponents:

$$\frac{a}{b} = \frac{10^{\log a}}{10^{\log b}} = 10^{(\log a - \log b)}$$

We have thus established an easier way of multiplication and division since these operations have been reduced to adding and subtracting.

The logarithm of a power of a number is equal to the logarithm of that number, multiplied by the exponent of the power.

$$\log a^2 = 2 \log a \text{ and } \log a^3 = 3 \log a$$

or, in general:

$$\log a^n = n \log a$$

Also, the logarithm of a root of a number is equal to the logarithm of that number divided by the index of the root:

$$\log \sqrt[n]{a} = \frac{1}{n} \log a$$

It follows from the rules of multiplication, that numbers having the same digits but different locations for the decimal point, have logarithms with the same mantissa:

$$\log 829 = 2.918555$$

$$\log 82.9 = 1.918555$$

$$\log 8.29 = 0.918555$$

$$\log 0.829 = -1.918555$$

$$\log 0.0829 = -2.918555$$

$$\log 829 = \log (8.29 \times 100) = \log 8.29 + \log 100 = 0.918555 + 2$$

Logarithm tables give the mantissas of logarithms only. The characteristic has to be determined by inspection. The characteristic is equal to the number of digits to the left of the decimal point *minus one*. In the case of logarithms of numbers less than unity, the characteristic is negative and is equal to the number of ciphers to the right of the decimal point *plus one*.

For reasons of convenience in making up logarithm tables, it has become the rule that the mantissa should always be positive. Such notations above as -1.918555 really mean $(+0.918555 \;\; -1)$ and -2.981555 means $(+0.918555 - 2)$. There are also some other notations in use such as

$$\bar{1}.918555 \text{ and } \bar{2}.918555$$

$$\text{also } 9.918555 - 10 \quad 8.918555 - 10 \quad 7.918555 - 10, \text{ etc.}$$

When, after some addition and subtraction of logarithms a mantissa should come out negative, one cannot look up its equivalent number or *anti-logarithm* in the table. The mantissa must first be made positive by adding and subtracting an appropriate integral number. Example: Suppose we find that the logarithm of a number is -0.34569, then we can transform it into the proper form by adding and subtracting 1

$$\begin{array}{ll} 1 & -1 \\ -0.34569 & \\ \hline 0.65431 & -1 \text{ or } -1.65431 \end{array}$$

Using Logarithm Tables

Logarithms are used for calculations involving multiplication, division, powers, and roots. Especially when the numbers are large and for higher, or fractional powers and roots, this becomes the most convenient way.

Logarithm tables are available giving the logarithms to three places, some to four places, others to five and six places. The table to use depends on the accuracy required in the result of our calculations. The four place table, printed in this chapter, permits the finding of answers to problems to four significant figures which is good enough for most constructional purposes. If greater accuracy is required a five place table should be consulted. The five place table is perhaps the most popular of all.

Referring now to the four place table, to find a common logarithm of a number, proceed as follows. Suppose the number is 5576. First, determine the characteristic. An inspection will show that the characteristic should be 3. This figure is placed to the left of the decimal point. The mantissa is now found by reference to the logarithm table. The first two numbers are 55; glance down the *N* column until coming to these figures. Advance to the right until coming in line with the column headed 7; the mantissa will be 7459. (Note that the column headed 7 corresponds to the *third figure* in the number 5576.) Place the mantissa 7459 to the right of the decimal point, making the logarithm of 5576 now read 3.7459. *Important:* do not consider the last figure 6 in the

N	L.	0*	1	2	3	4	5	6	7	8	9	P.P.
250	39	794	811	829	846	863	881	898	915	933	950	
251		967	985	*002	*019	*037	*054	*071	*088	*106	*123	18
252	40	140	157	175	192	209	226	243	261	278	295	1 1.8
253		312	329	346	364	381	398	415	432	449	466	2 3.6
254		483	500	518	535	552	569	586	603	620	637	3 5.4
												4 7.2
255		654	671	688	705	722	739	756	773	790	807	etc.

Figure 6.

A SMALL SECTION OF A FIVE PLACE LOGARITHM TABLE.

Logarithms may be found with greater accuracy with such tables, but they are only of use when the accuracy of the original data warrants greater precision in the figure work. Slightly greater accuracy may be obtained for intermediate points by interpolation, as explained in the text.

number 5576 when looking for the mantissa in the accompanying four place tables; in fact, one may usually disregard all digits beyond the first three when determining the mantissa. *(Interpolation.* sometimes used to find a logarithm more accurately, is unnecessary unless warranted by unusual accuracy in the available data.) However, be doubly sure to include all figures when ascertaining the magnitude of the characteristic.

To find the anti-logarithm, the table is used in reverse. As an example, let us find the anti-logarithm of 1.272 or, in other words, find the number of which 1.272 is the logarithm. Look in the table for the mantissa closest to 272. This is found in the first half of the table and the nearest value is 2718. Write down the first two significant figures of the anti-logarithm by taking the figures at the beginning of the line on which 2718 was found. This is 18; add to this, the digit above the column in which 2718 was found; this is 7. The anti-logarithm is 187 but we have not yet placed the decimal point. The characteristic is 1, which means that there should be two digits to the left of the decimal point. Hence, 18.7 is the anti-logarithm of 1.272.

For the sake of completeness we shall also describe the same operation with a five-place table where interpolation is done by means of tables of proportional parts (P.P. tables). Therefore we are reproducing here a small part of one page of a five-place table.

Finding the logarithm of 0.025013 is done as follows: We can begin with the characteristic, which is -2. Next find the first three digits in the column, headed by *N* and immediately after this we see 39, the first two digits of the mantissa. Then look among the headings of the other columns for the next digit of the number, in this case *1*. In the column, headed by *1* and on the line headed *250,* we find the next three digits of the logarithm, 811. So far, the logarithm is -2.39811 but this is the logarithm of 0.025010 and we want the logarithm of 0.025013. Here we can interpolate by observing that the difference between the log of 0.02501 and 0.02502 is $829 - 811$ or 18, in the last two significant figures. Looking in the P.P. table marked *18* we find after 3 the number 5.4 which is to be added to the logarithm.

$$\begin{array}{l} -2.39811 \\ 5.4 \\ \hline -2.39816\text{, the logarithm of } 0.025013 \end{array}$$

Since our table is only good to five places, we must eliminate the last figure given in the P.P. table if it is less than 5, otherwise we must add one to the next to the last figure, rounding off to a whole number in the P.P. table.

Finding the anti-logarithm is done the same way but with the procedure reversed. Suppose it is required to find the anti-logarithm of 0.40100. Find the first two digits in the column headed by L. Then one must look for the next three digits or the ones nearest to it, in the columns after 40 and on the lines from 40 to 41. Now here we find that numbers in the neighborhood of 100 occur only with an asterisk on the line just before 40 and still after 39. The asterisk means that instead of the 39 as the first two digits, these mantissas should have 40 as the first two digits. The logarithm 0.40100 is between the logs 0.40088 and 0.40106; the anti-logarithm is between 2517 and 2518. The difference between the two logarithms in the table is again 18 in the last two figures and our logarithm 0.40100 differs with the lower one 12 in the last figures. Look in the P.P. table of 18 which number comes closest to 12. This is found to be 12.6 for $7 \times 1.8 = 12.6$. Therefore we may add the digit 7 to the anti-logarithm already found; so we have 25177. Next, place the decimal point according to the rules: There are as many digits to the left of the decimal point as indicated in the characteristic plus one. The anti-logarithm of 0.40100 is 2.5177.

In the following examples of the use of logarithms we shall use only three places from the tables printed in this chapter since a greater degree of precision in our calculations would not be warranted by the accuracy of the data given.

In a 375 ohm bias resistor flows a current of 41.5 milliamperes; how many watts are dissipated by the resistor?

We write the equation for power in watts:

$$P = I^2R$$

and filling in the quantities in question, we have:

$$P = 0.0415^2 \times 375$$

Taking logarithms,

$$\log P = 2 \log 0.0415 + \log 375$$

$$\log 0.0415 = -2.618$$

$$\text{So } 2 \times \log 0.0415 = -3.236$$

$$\log \quad 375 = \quad 2.574$$

$$\log P \qquad = -1.810$$

antilog = 0.646. Answer = 0.646 watts

Caution: Do not forget that the negative sign before the characteristic belongs to the characteristic only and that mantissas are *always* positive. Therefore we recommend the other notation, for it is less likely to lead to errors. The work is then written:

$$\log 0.0415 = \;\; 8.618-10$$

$$2 \times \log 0.0415 = 17.236-20 = 7.236-10$$

$$\log 375 \qquad = 2.574$$

$$\log P \qquad = 9.810-10$$

Another example follows which demonstrates the ease in handling powers and roots. Assume an all-wave receiver is to be built, covering from 550 kc. to 60 mc. Can this be done in five ranges and what will be the required tuning ratio for each range if no overlapping is required? Call the tuning ratio of one band, x. Then the total tuning ratio for five such bands is x^5. But the total tuning ratio for all bands is 60/0.55. Therefore:

$$X^5 = \frac{60}{0.55} \text{ or : } x = \sqrt[5]{\frac{60}{0.55}}$$

Taking logarithms:

$$\log x = \frac{\log 60 - \log 0.55}{5}$$

log 60	1.778	
log 0.55	−1.740	subtract
	2.038	

Remember again that the mantissas are positive and the characteristic alone can be negative. Subtracting −1 is the same as adding +1.

$$\log x = \frac{2.038}{5} = 0.408$$

$$x = \text{antilog } 0.408 = 2.56$$

The tuning ratio should be 2.56.

db	Power Ratio
0	1.00
1	1.26
2	1.58
3	2.00
4	2.51
5	3.16
6	3.98
7	5.01
8	6.31
9	7.94
10	10.00
20	100
30	1,000
40	10,000
50	100,000
60	1,000,000
70	10,000,000
80	100,000,000

db R
13-20
16 40
19-80
22-160

Figure 7.
A TABLE OF DECIBEL GAINS VERSUS POWER RATIOS.

The Decibel

The decibel is a unit for the comparison of power or voltage levels in sound and electrical work. The sensation of our ears due to sound waves in the surrounding air is roughly proportional to the logarithm of the energy of the sound-wave and not proportional to the energy itself. For this reason a logarithmic unit is used so as to approach the reaction of the ear.

The decibel represents a *ratio* of two power levels, usually connected with gains or loss due to an amplifier or other network. The decibel is defined

$$N_{db} = 10 \log \frac{P_o}{P_i}$$

where P_o stands for the output power, P_i for the input power and N_{db} for the number of decibels. When the answer is positive, there is a gain; when the answer is negative, there is a loss.

The gain of amplifiers is usually given in decibels. For this purpose both the input power and output power should be measured. Example: Suppose that an intermediate amplifier is being driven by an input power of 0.2 watt and after amplification, the output is found to be 6 watts.

$$\frac{P_o}{P_i} = \frac{6}{0.2} = 30$$

$$\log 30 = 1.48$$

Therefore the gain is 10 × 1.48 = 14.8 decibels. The decibel is a logarithmic unit; when the power was multiplied by 30, the power level in decibels was increased by 14.8 decibels, or 14.8 decibels *added.*

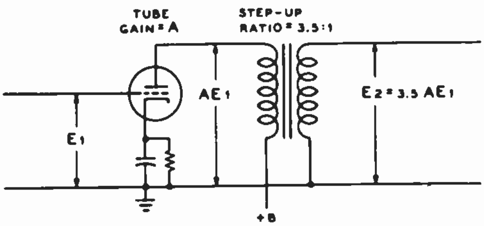


Figure 8.
STAGE GAIN.

The voltage gain in decibels in this stage is equal to the amplification in the tube plus the step-up ratio of the transformer, both expressed in decibels.

When one amplifier is to be followed by another amplifier, power gains are multiplied but the decibel gains are added. If a main amplifier having a gain of 1,000,000 (power ratio is 1,000,000) is preceded by a pre-amplifier with a gain of 1000, the total gain is 1,000,000,000. But in decibels, the first amplifier has a gain of 60 decibels, the second a gain of 30 decibels and the two of them will have a gain of 90 decibels when connected in cascade. (This is true only if the two amplifiers are properly matched at the junction as otherwise there will be a reflection loss at this point which must be subtracted from the total.)

Conversion of power ratios to decibels or vice versa is easy with the small table shown on these pages. In any case, an ordinary logarithm table will do. Find the logarithm of the power ratio and multiply by ten to find decibels.

Sometimes it is more convenient to figure decibels from voltage or current ratios or gains rather than from power ratios. This applies especially to voltage amplifiers. The equation for this is

$$N_{db} = 20 \log \frac{E_o}{E_i} \text{ or } 20 \log \frac{I_o}{I_i}$$

where the subscript, $_o$, denotes the output voltage or current and $_i$ the input voltage or current. Remember, this equation is true only if the voltage or current gain in question represents a power gain which is the square of it and not if the power gain which results from this is some other quantity due to impedance changes. This should be quite clear when we consider that a matching transformer to connect a speaker to a line or output tube does not represent a gain or loss; there is a voltage change and a current change yet the power remains the same for the impedance has changed.

On the other hand, when dealing with voltage amplifiers, we can figure the gain in a stage by finding the voltage ratio from the grid of the first tube to the grid of the next tube.

Example: In the circuit of Figure 8, the gain in the stage is equal to the amplification in the tube and the step-up ratio of the transformer. If the amplification in the tube is 10 and the step-up in the transformer is 3.5, the voltage gain is 35 and the gain in decibels is:

$$20 \times \log 35 = 20 \times 1.54 = 30.8 \text{ db}$$

Decibels as Power Level The original use of the decibel was only as a *ratio* of power levels—not as an absolute measure of power. However, one may use the decibel as such an absolute unit by fixing an arbitrary "zero" level, and to indicate any power level by its number of decibels above or below this arbitrary zero level. This is all very good so long as we agree on the zero level.

Any power level may then be converted to decibels by the equation:

$$N_{db} = 10 \log \frac{P_o}{P_{ref.}}$$

where N_{db} is the desired power level in decibels, P_o the output of the amplifier, $P_{ref.}$ the arbitrary reference level.

The zero level most frequently used (but not always) is 6 milliwatts or 0.006 watts. For this zero level, the equation reduces to

$$N_{db} = 10 \log \frac{P_o}{0.006}$$

Example: An amplifier using a 6F6 tube should be able to deliver an undistorted output of 3 watts. How much is this in decibels?

$$\frac{P_o}{P_{ref.}} = \frac{3}{.006} = 500$$

$$10 \times \log 500 = 10 \times 2.70 = 27.0$$

Therefore the power level at the output of the 6F6 is 27.0 decibels. When the power level to be converted is less than 6 milliwatts, the level is noted as negative. Here we must remember all that has been said regarding logarithms of numbers less than unity and the fact that the characteristic is negative but not the mantissa.

A preamplifier for a microphone is feeding 1.5 milliwatts into the line going to the regular speech amplifier. What is this power level expressed in decibels?

$$\text{decibels} = 10 \log \frac{P_o}{0.006} = 10 \log \frac{0.0015}{0.006} = 10 \log 0.25$$

Log 0.25 = $\bar{1}.398$ (from table). Therefore, 10 × $\bar{1}.398$ = (10 × −1 = −10) + (10 × .398 = 3.98); adding the products algebraically, gives −6.02 db.

The conversion chart reproduced in this chapter will be of use in converting decibels to watts and vice versa.

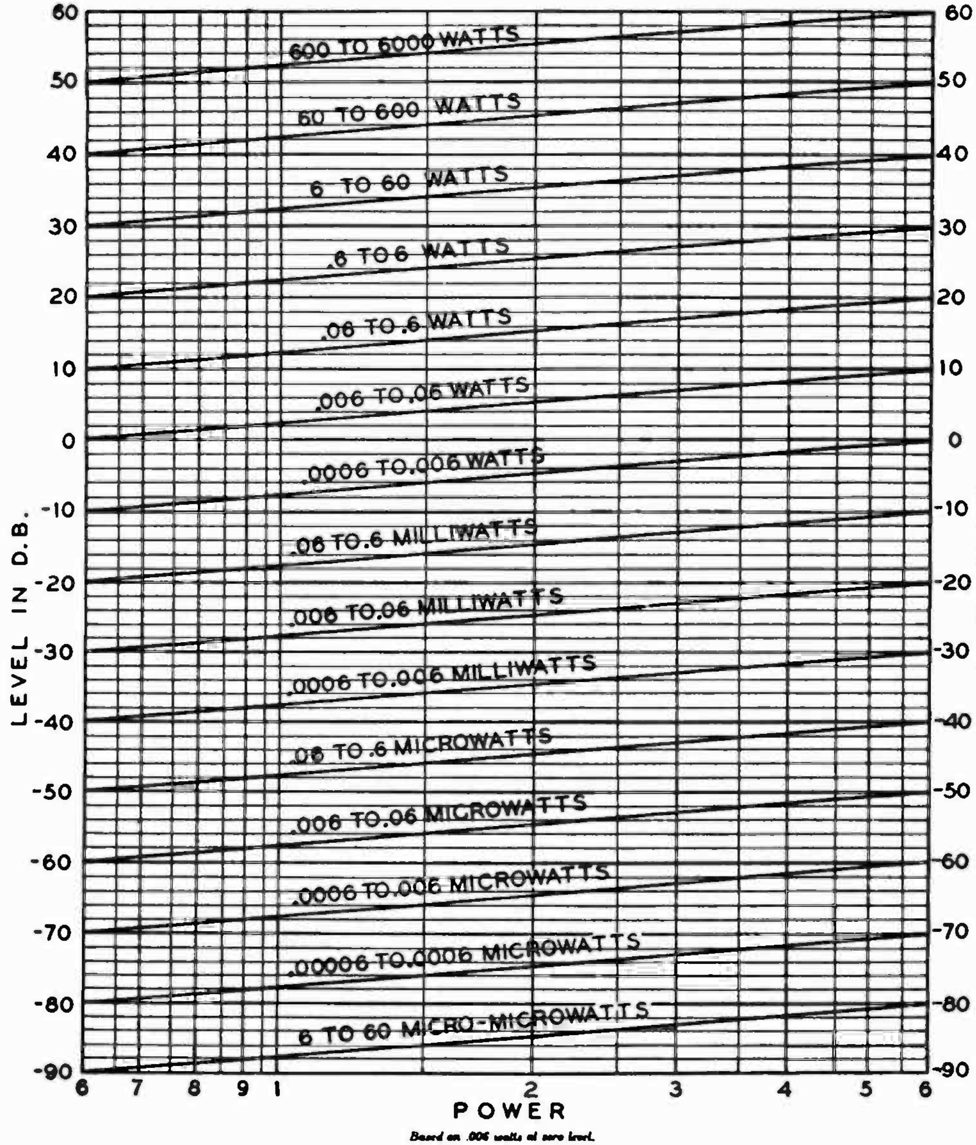


Figure 9.

CONVERSION CHART: POWER TO DECIBELS

Power levels between 6 micromicrowatts and 6000 watts may be referred to corresponding decibel levels between -90 and 60 db, and vice versa, by means of the above chart. Fifteen ranges are provided. Each curve begins at the same point where the preceding one ends, enabling uninterrupted coverage of the wide db and power ranges with condensed chart. For example: the lowermost curve ends at -80 db or 60 micromicrowatts and the next range starts at the same level. Zero db level is taken as 6 milliwatts (.006 watt).

Converting Decibels to Power It is often convenient to be able to convert a decibel value to a power equivalent. The formula used for this operation is

$$P = 0.006 \times \text{antilog} \frac{N_{db}}{10}$$

where P is the desired level in watts and N_{db} the decibels to be converted.

To determine the power level P from a decibel equivalent, simply divide the decibel value by 10; then take the number comprising the antilog and multiply it by 0.006; the product gives the level in watts.

Note: In problems dealing with the conversion of *minus* decibels to power, it often happens that the decibel value $-N_{db}$ is not divisible by 10. When this is the case, the numerator in the factor $-\frac{N_{db}}{10}$ must be made evenly divisible by 10, the negative signs must be observed, and the quotient labeled accordingly.

To make the numerator evenly divisible by 10 proceed as follows: Assume, for example, that $-N_{db}$ is some such value as -38; to make this figure evenly divisible by 10, we must add -2 to it, and, since we have added a negative 2 to it, we must also add a positive 2 so as to keep the net result the same.

Our decibel value now stands, $-40 + 2$. Dividing both of these figures by 10, as in the equation above, we have -4 and $+0.2$. Putting the two together we have the logarithm -4.2 with the negative characteristic and the positive mantissa as required.

The following examples will show the technique to be followed in practical problems.

(a) The output of a certain device is rated at -74 db. What is the power equivalent? Solution:

$$\frac{N_{db}}{10} = \frac{-74}{10} \text{ (not evenly divisible by 10)}$$

Routine:

$$\begin{array}{rr} -74 & \\ -\ 6 & +6 \\ \hline -80 & +6 \end{array}$$

$$\frac{N_{db}}{10} = \frac{-80+6}{10} = -8.6$$

$$\text{antilog } -8.6 = 0.000\,000\,04$$

$$.006 \times 0.000\,000\,04 = 0.000\,000\,000\,24 \text{ watt or } 240 \text{ micro-microwatt}$$

(b) This example differs somewhat from that of the foregoing one in that the mantissas are added differently. A low-powered amplifier has an input signal level of -17.3 db. How many milliwatts does this value represent?

Solution:

$$\begin{array}{rr} -17.3 & \\ -\ 2.7 & +2.7 \\ \hline -20 & +2.7 \end{array}$$

$$\frac{N_{db}}{10} = \frac{-20+2.7}{10} = -2.27$$

$$\text{Antilog } -2.27 = 0.0186$$

$$0.006 \times 0.0186 = 0.000\,1116 \text{ watt or } 0.1116 \text{ milliwatt}$$

Input voltages: To determine the required input voltage, take the peak voltage necessary to drive the last class A amplifier tube to maximum output, and divide this figure by the total overall voltage gain of the preceding stages.

Computing Specifications: From the preceding explanations the following data can be computed with any degree of accuracy warranted by the circumstances:

(1) Voltage amplification
(2) Overall gain in db
(3) Output signal level in db
(4) Input signal level in db
(5) Input signal level in watts
(6) Input signal voltage

When a power level is available which must be brought up to a new power level, the gain required in the intervening amplifier is equal to the difference between the two levels in decibels. If the required input of an amplifier for full output is -30 decibels and the output from a device to be used is but -45 decibels, the pre-amplifier required should have a gain of the difference, or 15 decibels. Again this is true only if the two amplifiers are properly matched and no losses are introduced due to mismatching.

Push-Pull Amplifiers To double the output of any cascade amplifier, it is only necessary to connect in push-pull the last amplifying stage, and replace the interstage and output transformers with push-pull types.

To determine the voltage gain (voltage ratio) of a push-pull amplifier, take the ratio of one *half* of the secondary winding of the push-pull transformer and multiply it by the μ of one of the output tubes in the push-pull stage; the product, *when doubled*, will be the voltage amplification, or step-up.

Other Units and Zero Levels When working with decibels one should not immediately take for granted that the zero level is 6 milliwatts for there are other zero levels in use.

In broadcast stations an entirely new system is now employed. Measurements made in acoustics are now made with the standard zero level of 10^{-16} watts per square cm.

Microphones are often rated with reference to the following zero level: *one volt at open circuit when the sound pressure is one millibar.* In any case, the rating of the microphone must include the loudness of the sound. It is obvious that this zero level does not lend itself readily for the calculation of required gain in an amplifier.

The VU: So far, the decibel has always referred to a type of signal which can readily be measured, that is, a steady signal of a single frequency. But what would be the power level of a signal which is constantly varying in volume and frequency? The measurement of voltage would depend on the type of instrument employed, whether it is measured with a thermal square law meter or one that shows average values; also, the inertia of the movement will change its indications at the peaks and valleys.

After considerable consultation, the broadcast chains and the Bell System have agreed on the *VU*. The level in VU is the level in decibels above *1 milliwatt* zero level and measured with a carefully defined type of instrument across a 600 ohm line. So long as we deal with an unvarying sound, the level in VU is equal to decibels above 1 milliwatt; but when the sound level varies, the unit is the VU and the special meter must be used. There is then no equivalent in decibels.

The Neper: We might have used the natural logarithm instead of the common logarithm when defining our logarithmic unit of sound. This was done in Europe and the unit obtained is known as the *neper* or *napier*. It is still found in some American literature on filters.

1 neper = 8.686 decibels
1 decibel = 0.1151 neper

AC Meters With Decibel Scales Many test instruments are now equipped with scales calibrated in decibels which is very handy when making measurements of frequency characteristics and gain. These meters are generally calibrated for connection across a 500 ohm line and for a zero level of 6 milliwatts. When they are connected across another impedance, the reading on the meter is no longer correct for the zero level of 6 milliwatts. A correction factor should be applied consisting in the addition or subtraction of a steady figure to all readings on the meter. This figure is given by the equation:

$$\text{db to be added} = 10 \log \frac{500}{Z}$$

where Z is the impedance of the circuit under measurement.

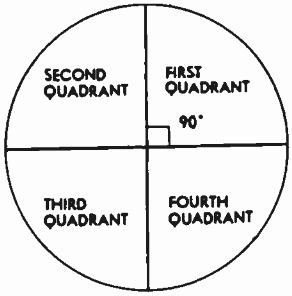


Figure 10.
THE CIRCLE IS DIVIDED INTO FOUR QUADRANTS BY TWO PERPENDICULAR LINES AT RIGHT ANGLES TO EACH OTHER.
The "northeast" quadrant thus formed is known as the first quadrant; the others are numbered consecutively in a counterclockwise direction.

Trigonometry

Definition and Use Trigonometry is the science of mensuration of *triangles*. At first glance triangles may seem to have little to do with electrical phenomena; however, in a.c. work most currents and voltages follow laws equivalent to those of the various trigonometric relations which we are about to examine briefly. Examples of their application to a.c. work will be given in the section on *Vectors*.

Angles are measured in *degrees* or in *radians*. The circle has been divided into 360 degrees, each degree into 60 minutes, and each minute into 60 seconds. A decimal division of the degree is also in use because it makes calculation easier. Degrees, minutes and seconds are indicated by the following signs: °, ′ and ″. Example: 6° 5′ 23″ means six degrees, five minutes, twenty-three seconds. In the decimal notation we simply write 8.47°, eight and forty-seven hundredths of a degree.

When a circle is divided into four quadrants by two perpendicular lines passing through the center (Figure 10) the angle made by the two lines is 90 degrees, known as a *right angle*. Two right angles, or 180° equals a *straight angle*.

The radian: If we take the radius of a circle and bend it so it can cover a part of the circumference, the arc it covers subtends an angle called a *radian* (Figure 11). Since the circumference of a circle equals 2 times the radius, there are 2π radians in 360°. So we have the following relations:

1 radian = 57° 17′ 45″ = 57.2958° $\pi = 3.14159$
1 degree = 0.01745 radians
π radians = 180° $\pi/2$ radians = 90°
$\pi/3$ radians = 60°

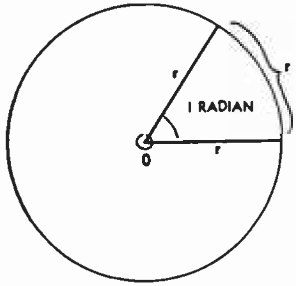


Figure 11.
THE RADIAN.
A radian is an angle whose arc is exactly equal to the length of either side. Note that the angle is constant regardless of the length of the side and the arc so long as they are equal. A radian equals 57.2958°.

In trigonometry we consider an angle *generated* by two lines, one stationary and the other rotating as if it were hinged at 0, Figure 12. Angles can be greater than 180 degrees and even greater than 360 degrees as illustrated in this figure.

Two angles are complements of each other when their sum is 90°, or a right angle. *A* is the complement of *B* and *B* is the complement of *A* when

$$A=(90°-B)$$

and when

$$B=(90°-A)$$

Two angles are supplements of each other when their sum is equal to a straight angle, or 180°. A is the supplement of B and B is the supplement of A when

$$A=(180°-B)$$

and

$$B=(180°-A)$$

In the angle *A*, Figure 13A, a line is drawn from *P*, perpendicular to *b*. Regardless of the point selected for *P*, the *ratio a/c* will always be the same for any given angle, *A*. So will all the other proportions between *a*, *b*, and *c* remain constant regardless of the position of point *P* on *c*. The six possible ratios each are named and defined as follows:

$$\text{sine A} = \frac{a}{c} \qquad \text{cosine A} = \frac{b}{c}$$

$$\text{tangent A} = \frac{a}{b} \qquad \text{cotangent A} = \frac{b}{a}$$

$$\text{secant A} = \frac{c}{b} \qquad \text{cosecant A} = \frac{c}{a}$$

Let us take a special angle as an example. For instance, let the angle *A* be 60 degrees as in Figure 13B. Then the relations between the sides are as in the figure and the six functions become:

$$\sin. 60° = \frac{a}{c} = \frac{\frac{1}{2}\sqrt{3}}{1} = \tfrac{1}{2}\sqrt{3}$$

$$\cos 60° = \frac{b}{c} = \frac{\frac{1}{2}}{1} = \tfrac{1}{2}$$

$$\tan 60° = \frac{a}{b} = \frac{\frac{1}{2}\sqrt{3}}{\frac{1}{2}} = \sqrt{3}$$

$$\cot 60° = \frac{\frac{1}{2}}{\frac{1}{2}\sqrt{3}} = \frac{1}{\sqrt{3}} = \tfrac{1}{3}\sqrt{3}$$

$$\sec 60° = \frac{c}{b} = \frac{1}{\frac{1}{2}} = 2$$

$$\csc 60° = \frac{c}{a} = \frac{1}{\frac{1}{2}\sqrt{3}} = \tfrac{2}{3}\sqrt{3}$$

Another example: Let the angle be 45°, then the relations between the lengths of *a*, *b*, and *c* are as shown in Figure 13C, and the six functions are:

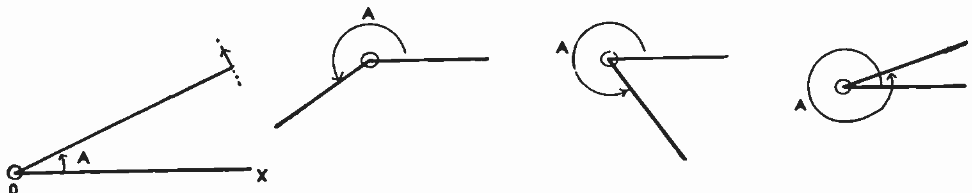


Figure 12.
AN ANGLE IS GENERATED BY TWO LINES, ONE STATIONARY AND THE OTHER ROTATING.
The line OX is stationary; the line with the small arrow at the far end rotates in a counterclockwise direction. At the position illustrated in the lefthandmost section of the drawing it makes an angle, A, which is less than 90° and is therefore in the first quadrant. In the position shown in the second portion of the drawing the angle A has increased to such a value that it now lies in the third quadrant; note that an angle can be greater than 180°. In the third illustration the angle A is in the fourth quadrant. In the fourth position the rotating vector has made more than one complete revolution and is hence in the fifth quadrant; since the fifth quadrant is an exact repetition of the first quadrant, its values will be the same as in the lefthandmost portion of the illustration.

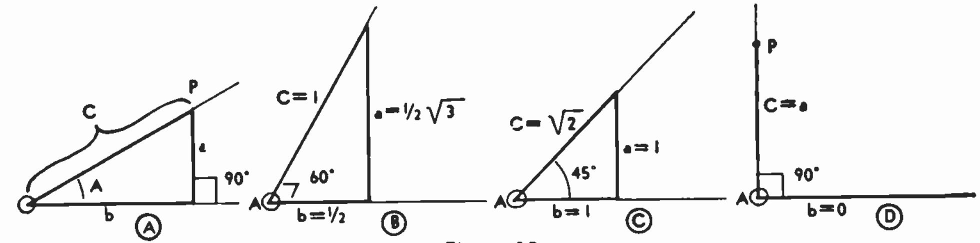


Figure 13.

THE TRIGONOMETRIC FUNCTIONS.

In the right triangle shown in (A) the side opposite the angle A is a, while the adjoining sides are b and c; the trigonometric functions of the angle A are completely defined by the ratios of the sides a, b and c. In (B) are shown the lengths of the sides a and b when angle A is 60° and side c is 1. In (C) angle A is 45°; a and b equal 1, while c equals $\sqrt{2}$. In (D) note that c equals a for a right angle while b equals 0.

$$\sin 45° = \frac{1}{\sqrt{2}} = \tfrac{1}{2}\sqrt{2}$$

$$\cos 45° = \frac{1}{\sqrt{2}} = \tfrac{1}{2}\sqrt{2}$$

$$\tan 45° = \frac{1}{1} = 1 \qquad \cot 45° = \frac{1}{1} = 1$$

$$\sec 45° = \frac{\sqrt{2}}{1} = \sqrt{2}$$

$$\operatorname{cosec} 45° = \frac{\sqrt{2}}{1} = \sqrt{2}$$

There are some special difficulties when the angle is zero or 90 degrees. In Figure 13D an angle of 90 degrees is shown; drawing a line perpendicular to b from point P makes it fall on top of c. Therefore in this case $a = c$ and $b = 0$. The six ratios are now:

$$\sin 90° = \frac{a}{c} = 1 \qquad \cos 90° = \frac{b}{c} = \frac{0}{c} = 0$$

$$\tan 90° = \frac{a}{b} = \frac{a}{0} = \infty \qquad \cot 90° = \frac{0}{a} = 0$$

$$\sec 90° = \frac{c}{b} = \frac{c}{0} = \infty \qquad \operatorname{cosec} 90° = \frac{c}{a} = 1$$

When the angle is zero, $a=0$ and $b=c$. The values are then:

$$\sin 0° = \frac{a}{c} = \frac{0}{c} = 0 \qquad \cos 0° = \frac{b}{c} = 1$$

$$\tan 0° = \frac{a}{b} = \frac{0}{b} = 0 \qquad \cot 0° = \frac{b}{a} = \frac{b}{0} = \infty$$

$$\sec 0° = \frac{c}{b} = 1 \qquad \operatorname{cosec} 0° = \frac{c}{a} = \frac{c}{0} = \infty$$

In general, for every angle, there will be definite values of the six functions. Conversely, when any of the six functions is known, the angle is defined. Tables have been calculated giving the value of the functions for angles.

From the foregoing we can make up a small table of our own (Figure 14), giving values of the functions for some common angles.

Relations Between Functions It follows from the definitions that

$$\sin A = \frac{1}{\operatorname{cosec} A} \qquad \cos A = \frac{1}{\sec A}$$

$$\text{and } \tan A = \frac{1}{\cot A}$$

From the definitions also follows the relation

$$\cos A = \sin(\text{complement of } A) = \sin(90° - A)$$

because in the right triangle of Figure 15, $\cos A = b/c = \sin B$ and $B = 90° - A$ or the complement of A. For the same reason:

$$\cot A = \tan\ (90° - A)$$

$$\csc A = \sec\ (90° - A)$$

Relations in Right Triangles In the right triangle of Figure 15, $\sin A = a/c$ and by transposition

$$a = c \sin A$$

For the same reason we have the following identities:

$$\tan A = a/b \qquad a = b \tan A$$
$$\cot A = b/a \qquad b = a \cot A$$

In the same triangle we can do the same for functions of the angle B

Angle	Sin	Cos.	Tan	Cot	Sec.	Cosec.
0	0	1	0	∞	1	∞
30°	½	$\frac{1}{2}\sqrt{3}$	$\frac{1}{3}\sqrt{3}$	$\sqrt{3}$	$\frac{2}{3}\sqrt{3}$	2
45°	$\frac{1}{2}\sqrt{2}$	$\frac{1}{2}\sqrt{2}$	1	1	$\sqrt{2}$	$\sqrt{2}$
60°	$\frac{1}{2}\sqrt{3}$	½	$\sqrt{3}$	$\frac{1}{3}\sqrt{3}$	2	$\frac{2}{3}\sqrt{3}$
90°	1	0	∞	0	∞	1

Figure 14.

Values of trigonometric functions for common angles in the first quadrant.

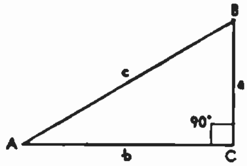


Figure 15.

In this figure the sides a, b, and c are used to define the trigonometric functions of angle B as well as angle A.

$\sin B = b/c$	$b = c \sin B$
$\cos B = a/c$	$a = c \cos B$
$\tan B = b/a$	$b = a \tan B$
$\cot B = a/b$	$a = b \cot B$

Functions of Angles Greater than 90 Degrees

In angles greater than 90 degrees, the values of *a* and *b* become negative on occasion in accordance with the rules of Cartesian coordinates. When *b* is measured from 0 towards the left it is considered negative and similarly, when *a* is measured from 0 downwards, it is negative. Referring to Figure 16, an angle in the *second quadrant* (between 90° and 180°) has some of its functions negative:

$$\sin A = \frac{a}{c} = \text{pos.} \qquad \cos A = \frac{-b}{c} = \text{neg.}$$

$$\tan A = \frac{a}{-b} = \text{neg.} \qquad \cot A = \frac{-b}{a} = \text{neg.}$$

$$\sec A = \frac{c}{-b} = \text{neg.} \qquad \text{cosec } A = \frac{c}{a} = \text{pos.}$$

For an angle in the third quadrant (180° to 270°), the functions are

$$\sin A = \frac{-a}{c} = \text{neg.} \qquad \cos A = \frac{-b}{c} = \text{neg.}$$

$$\tan A = \frac{-a}{-b} = \text{pos.} \qquad \cot A = \frac{-b}{-a} = \text{pos.}$$

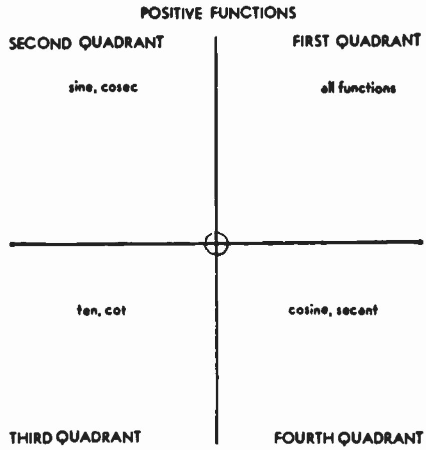


Figure 17.

SIGNS OF THE TRIGONOMETRIC FUNCTIONS.

The functions listed in this diagram are positive; all other functions are negative.

$$\sec A = \frac{c}{-b} = \text{neg.} \qquad \text{cosec } A = \frac{c}{-a} = \text{neg.}$$

And in the fourth quadrant (270° to 360°):

$$\sin A = \frac{-a}{c} = \text{neg.} \qquad \cos A = \frac{b}{c} = \text{pos.}$$

$$\tan A = \frac{-a}{b} = \text{neg.} \qquad \cot A = \frac{b}{-a} = \text{neg.}$$

$$\sec A = \frac{c}{b} = \text{pos.} \qquad \text{cosec } A = \frac{c}{-a} = \text{neg.}$$

Summarizing, the sign of the functions in each quadrant can be seen at a glance from Figure 17, where in each quadrant are written the names of functions which are positive; those not mentioned are negative.

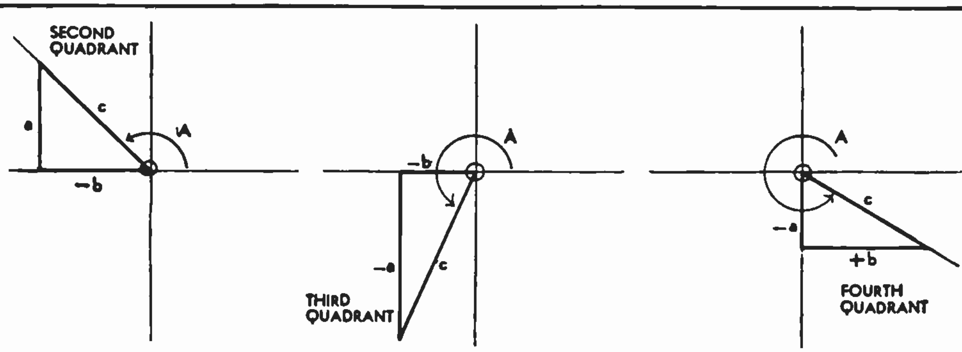


Figure 16.

TRIGONOMETRIC FUNCTIONS IN THE SECOND, THIRD, AND FOURTH QUADRANTS.

The trigonometric functions in these quadrants are similar to first quadrant values, but the signs of the functions vary as listed in the text and in Figure 17.

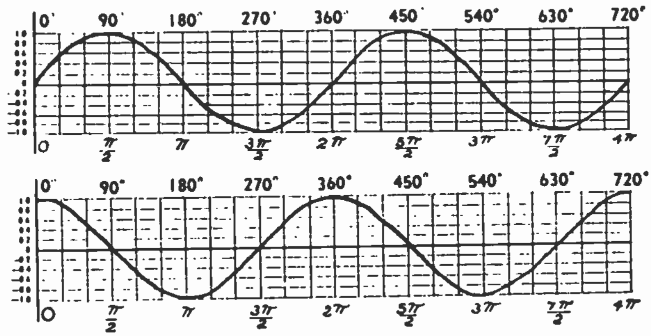


Figure 18.
SINE AND COSINE CURVES.
In (A) we have a sine curve drawn in Cartesian coordinates. This is the usual representation of an alternating current wave without substantial harmonics. In (B) we have a cosine wave; note that it is exactly similar to a sine wave displaced by 90° or π/2 radians.

Graphs of Trigonometric Functions

The sine wave. When we have the relation $y = \sin x$, where x is an angle measured in radians or degrees, we can draw a curve of y versus x for all values of the independent variable, and thus get a good conception how the sine varies with the magnitude of the angle. This has been done in Figure 18A. We can learn from this curve the following facts.

1. The sine varies between $+1$ and -1
2. It is a periodic curve, repeating itself after every multiple of 2π or $360°$
3. $\sin x = \sin(180° - x)$ or $\sin(\pi - x)$
4. $\sin x = -\sin(180° + x)$, or $-\sin(\pi + x)$

The cosine wave. Making a curve for the function $y = \cos x$, we obtain a curve similar to that for $y = \sin x$ except that it is displaced by 90° or $\pi/2$ radians with respect to the Y-axis. This curve (Figure 18B) is also periodic but it does not start with zero. We read from the curve:

1. The value of the cosine never goes beyond $+1$ or -1
2. The curve repeats, after every multiple of 2π radians or $360°$
3. $\cos x = -\cos(180° - x)$ or $-\cos(\pi - x)$
4. $\cos x = \cos(360° - x)$ or $\cos(2\pi - x)$

The graph of the tangent is illustrated in Figure 19. This is a discontinuous curve and illustrates well how the tangent increases from zero to infinity when the angle increases from zero to 90 degrees. Then when the angle is further increased, the tangent starts from minus infinity going to zero in the second quadrant, and to infinity again in the third quadrant.

1. The tangent can have any value between $+\infty$ and $-\infty$
2. The curve repeats and the period is π radians or $180°$, not 2π radians
3. $\tan x = \tan(180° + x)$ or $\tan(\pi + x)$
4. $\tan x = -\tan(180° - x)$ or $-\tan(\pi - x)$

The graph of the cotangent is the inverse of that of the tangent, see Figure 20. It leads us to the following conclusions:

1. The cotangent can have any value between $+\infty$ and $-\infty$
2. It is a periodic curve, the period being π radians or $180°$
3. $\cot x = \cot(180° + x)$ or $\cot(\pi + x)$
4. $\cot x = -\cot(180° - x)$ or $-\cot(\pi - x)$

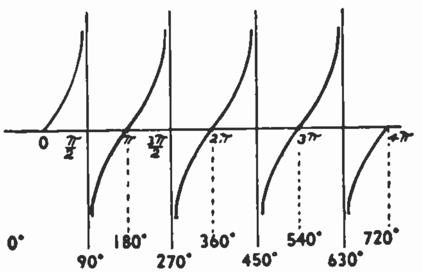


Figure 19.
TANGENT CURVES.
The tangent curve increases from 0 to ∞ with an angular increase of 90°. In the next 180° it increases from −∞ to +∞.

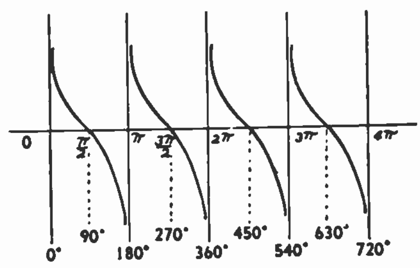


Figure 20.
COTANGENT CURVES.
Cotangent curves are the inverse of the tangent curves. They vary from +∞ to −∞ in each pair of quadrants.

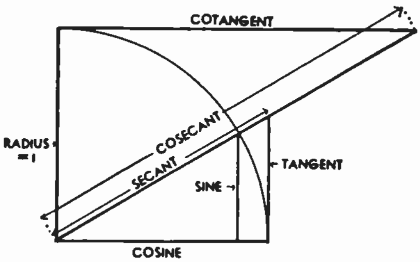


Figure 21.
ANOTHER REPRESENTATION OF TRIGONOMETRIC FUNCTIONS.
If the radius of a circle is considered as the unit of measurement, then the lengths of the various lines shown in this diagram are numerically equal to the functions marked adjacent to them.

The graphs of the secant and cosecant are of lesser importance and will not be shown here. They are the inverse, respectively, of the cosine and the sine, and therefore they vary from +1 to infinity and from −1 to −infinity.

Perhaps another useful way of visualizing the values of the functions is by considering Figure 21. If the radius of the circle is the unit of measurement then the lengths of the lines are equal to the functions marked on them.

Trigonometric Tables There are two kinds of trigonometric tables. The first type gives the functions of the angles, the second the logarithms of the functions. The first kind is also known as the table of *natural* trigonometric functions.

These tables give the functions of all angles between 0 and 45°. This is all that is necessary for the function of an angle between 45° and 90° can always be written as the co-function of an angle below 45°. Example: If we had to find the sine of 48°, we might write

$$\sin 48° = \cos (90° - 48°) = \cos 42°$$

Tables of the logarithms of trigonometric functions give the common logarithms ($\log_{10}$) of these functions. Since many of these logarithms have negative characteristics, one should add −10 to all logarithms in the table which have a characteristic of 6 or higher. For instance, the log sin 24° = 9.60931 −10. Log tan 1° = 8.24192 −10 but log cot 1° = 1.75808. When the characteristic shown is less than 6, it is supposed to be positive and one should not add −10.

Vectors

A *scalar* quantity has *magnitude* only; a *vector* quantity has both *magnitude* and *direction*. When we speak of a speed of 50 miles per hour, we are using a scalar quantity, but when we say the wind is Northeast and has a velocity of 50 miles per hour, we speak of a vector quantity.

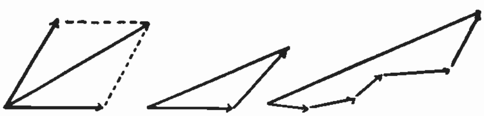


Figure 22.
Vectors may be added as shown in these sketches. In each case the long vector represents the vector sum of the smaller vectors. For many engineering applications sufficient accuracy can be obtained by this method which avoids long and laborious calculations.

Vectors, representing forces, speeds, displacements, etc., are represented by arrows. They can be added graphically by well known methods illustrated in Figure 22. We can make the parallelogram of forces or we can simply draw a triangle. The addition of many vectors can be accomplished graphically as in the same figure.

In order that we may define vectors algebraically and add, subtract, multiply, or divide them, we must have a logical notation system that lends itself to these operations. For this purpose vectors can be defined by coordinate systems. Both the Cartesian and the polar coordinates are in use.

Vectors Defined by Cartesian Coordinates Since we have seen how the sum of two vectors is obtained, it follows from Figure 23, that the vector $\dot{Z}$ equals the sum of the two vectors $\dot{x}$ and $\dot{y}$. In fact, any vector can be resolved into vectors along the *X*- and *Y*-axis. For convenience in working with these quantities we need to dis-

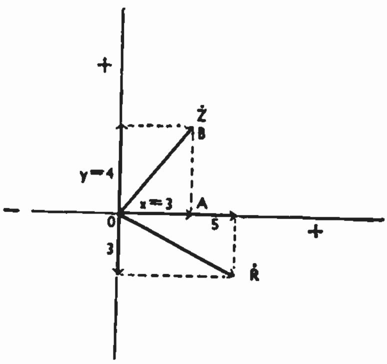


Figure 23.
RESOLUTION OF VECTORS.
Any vector such as Ż may be resolved into two vectors, x and y, along the X- and Y-axes. If vectors are to be added, their respective x and y components may be added to find the x and y components of the resultant vector.

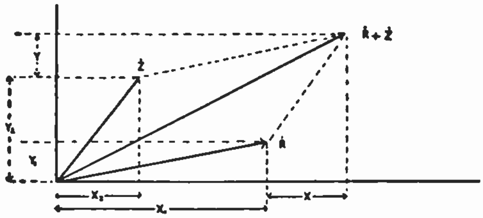


Figure 24.
ADDITION OR SUBTRACTION OF VECTORS.
Vectors may be added or subtracted by adding or subtracting their x or y components separately.

tinguish between the X- and Y-component, and so it has been agreed that the Y-component alone shall be marked with the letter j. Example (Figure 23):

$$\dot{Z} = 3 + 4j$$

Note again that the sign of components along the X-axis is positive when measured from 0 to the right and negative when measured from 0 towards the left. Also, the component along the Y-axis is positive when measured from 0 upwards, and negative when measured from 0 downwards. So the vector, $\dot{R}$, is described as

$$\dot{R} = 5 - 3j$$

Vector quantities are usually indicated by some special typography, especially by using a point over the letter indicating the vector, as $\dot{R}$.

Absolute Value of a Vector The absolute or scalar value of vectors such as $\dot{Z}$ or $\dot{R}$ in Figure 23 is easily found by the theorem of Pythagoras, which states that in any right-angled triangle the square of the side opposite the right angle is equal to the sum of the squares of the sides adjoining the right angle. In Figure 23, OAB is a right-angled triangle; therefore, the square of OB (or Z) is equal to the square of OA (or x) plus the square of AB (or y). Thus the absolute values of Z and R may be determined as follows:

$$|Z| = \sqrt{x^2 + y^2}$$

$$|Z| = \sqrt{3^2 + 4^2} = 5$$

$$|R| = \sqrt{5^2 + 3^2} = \sqrt{34} = 5.83$$

The vertical lines indicate that the absolute or scalar value is meant without regard to sign or direction.

Addition of Vectors An examination of Figure 24 will show that the two vectors

$$\dot{R} = x_1 + j\,y_1$$

$$\dot{Z} = x_2 + j\,y_2$$

can be added, if we add the X-components and the Y-components separately.

$$\dot{R} + \dot{Z} = x_1 + x_2 + j\,(y_1 + y_2)$$

For the same reason we can carry out subtraction by subtracting the horizontal components and subtracting the vertical components

$$\dot{R} - \dot{Z} = x_1 - x_2 + j\,(y_1 - y_2)$$

Let us consider the operator j. If we have a vector a along the X-axis and add a j in front of it (multiplying by j) the result is that the direction of the vector is rotated forward 90 degrees. If we do this twice (multiplying by j^2) the vector is rotated forward by 180 degrees and now has the value $-a$. Therefore multiplying by j^2 is equivalent to multiplying by -1. Then

$$j^2 = -1 \text{ and } j = \sqrt{-1}$$

This is the imaginary number discussed before under algebra. In electrical engineering the letter j is used rather than i, because i is already known as the symbol for current.

Multiplying Vectors When two vectors are to be multiplied we can perform the operation just as in algebra, remembering that $j^2 = -1$.

$$\dot{R}\dot{Z} = (x_1 + jy_1)\,(x_2 + jy_2)$$

$$= x_1\,x_2 + jx_1\,y_2 + j\,x_2\,y_1 + j^2\,y_1\,y_2$$

$$= x_1\,x_2 - y_1\,y_2 + j\,(x_1\,y_2 + x_2\,y_1)$$

Division has to be carried out so as to remove the j-term from the denominator. This can be done by multiplying both denominator and numerator by a quantity which will eliminate j from the denominator. Example:

$$\frac{\dot{R}}{\dot{Z}} = \frac{x_1 + jy_1}{x_2 + jy_2} = \frac{(x_1 + jy_1)\,(x_2 - jy_2)}{(x_2 + jy_2)\,(x_2 - jy_2)}$$

$$= \frac{x_1x_2 + y_1y_2 + j\,(x_2y_1 - x_1y_2)}{x_2^2 + y_2^2}$$

Polar Coordinates A vector can also be defined in polar coordinates by its magnitude and its vectorial angle with an arbitrary reference axis. In Figure 25

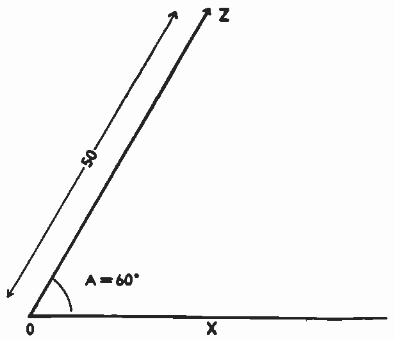


Figure 25.

IN THIS FIGURE A VECTOR HAS BEEN REPRESENTED IN POLAR INSTEAD OF CARTESIAN CO-ORDINATES.

In polar coordinates a vector is defined by a magnitude and an angle, called the vectorial angle, instead of by two magnitudes as in Cartesian coordinates.

the vector $\dot{Z}$ has a magnitude 50 and a vectorial angle of 60 degrees. This will then be written

$$\dot{Z} = 50\angle 60°$$

A vector $a + jb$ can be transformed into polar notation very simply (see Figure 26)

$$\dot{Z} = a + jb = \sqrt{a^2 + b^2}\,\angle \tan^{-1}\frac{b}{a}$$

In this connection tan^{-1} means *the angle of which the tangent is.* Sometimes the notation *arc tan b/a* is used. Both have the same meaning.

A polar notation of a vector can be transformed into a Cartesian coordinate notation in the following manner (Figure 27)

$$\dot{Z} = p\angle A = p\cos A + jp\sin A$$

A sinusoidally alternating voltage or current is symbolically represented by a rotating vector, having a magnitude equal to the peak voltage or current and rotating with an angular velocity of $2\pi f$ radians per second or as many revolutions per second as there are cycles per second.

The instantaneous voltage, *e*, is always equal to the sine of the vectorial angle of this rotating vector, multiplied by its magnitude.

$$e = E\sin 2\pi ft$$

The alternating voltage therefore varies with time as the sine varies with the angle. If we plot time horizontally and instantaneous voltage vertically we will get a curve like those in Figure 18.

In alternating current circuits, the current

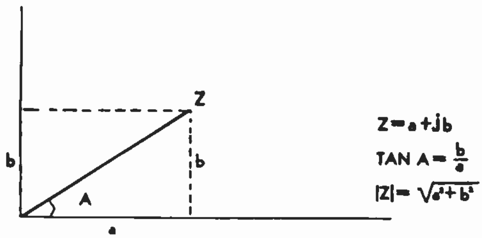


Figure 26.

Vectors can be transformed from Cartesian into polar notation as shown in this figure.

which flows due to the alternating voltage is not necessarily in step with it. The rotating current vector may be ahead or behind the voltage vector, having a *phase difference* with it. For convenience we draw these vectors as if they were standing still, so that we can indicate the difference in phase or the *phase angle.* In Figure 28 the current lags behind the voltage by the angle θ, or we might say that the voltage leads the current by the angle θ.

Vector diagrams show the phase relations between two or more vectors (voltages and currents) in a circuit. They may be added and subtracted as described; one may add a voltage vector to another voltage vector or a current vector to a current vector but not a current vector to a voltage vector (for the same reason that one cannot add a force to a speed). Figure 28 illustrates the relations in the simple series circuit of a coil and resistor. We know that the current passing through coil and resistor must be the same and in the same phase, so we draw this current *I* along the *X*-axis. We know also that the voltage drop *IR* across the resistor is in phase with the current, so the vector *IR* representing the voltage drop is also along the *X*-axis.

The voltage across the coil is 90 degrees ahead of the current through it; *IX* must therefore be drawn along the *Y*-axis. $\dot{E}$ the applied voltage must be equal to the vectorial sum of the two voltage drops, *IR* and *IX*, and we have so constructed it in the drawing. Now expressing the same in algebraic notation, we have

$$\dot{E} = IR + jIX$$

$$I\dot{Z} = IR + jIX$$

Dividing by *I*

$$\dot{Z} = R + jX$$

Due to the fact that a *reactance* rotates the voltage vector ahead or behind the current vector by 90 degrees, we must mark it with a *j* in vector notation. Inductive reactance will have a plus sign because it shifts the voltage vector forwards; a capacitive reactance is neg-

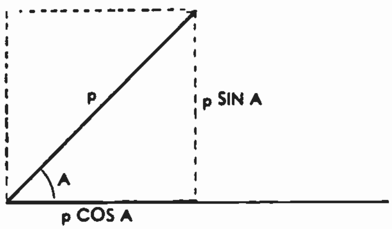


Figure 27.
Vectors can be transformed from polar into Cartesian notation as shown in this figure.

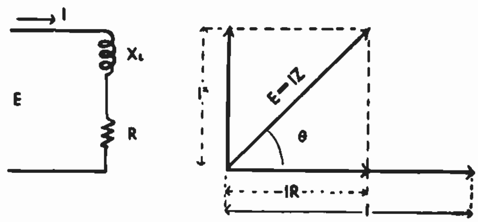


Figure 28.
VECTOR REPRESENTATION OF A SIMPLE SERIES CIRCUIT.
The righthand portion of the illustration shows the vectors representing the voltage drops in the coil and resistance illustrated at the left. Note that the voltage drop across the coil X_L leads that across the resistance by 90°.

ative because the voltage will lag behind the current. Therefore:

$$X_L = + j\, 2\pi f L$$

$$X_C = - j\, \frac{1}{2\pi f C}$$

In Figure 28 the angle θ is known as the phase angle between E and I. When calculating power, only the real components count. The power in the circuit is then

$$P = I\,(IR)$$

$$\text{but } IR = E \cos\theta$$

$$\therefore P = EI \cos\theta$$

This *cos θ* is known as the power factor of the circuit. In many circuits we strive to keep the angle θ as small as possible, making *cos θ* as near to unity as possible. In tuned circuits, we use reactances which should have as low a power factor as possible. The merit of a coil or condenser, its *Q*, is defined by the tangent of this phase angle:

$$Q = \tan\theta = X/R$$

For an efficient coil or condenser, *Q* should be as large as possible; the phase-angle should then be as close to 90 degrees as possible, making the power factor nearly zero. *Q* is almost but not quite the inverse of *cos θ*. Note that in Figure 29

$$Q = X/R \qquad \text{and} \qquad \cos\theta = R/Z$$

When Q is more than 5, the power factor is less than 20%; we can then safely say $Q = 1/\cos\theta$ with a maximum error of about 2½ percent, for in the worst case, when $\cos\theta = 0.2$, *Q* will equal $\tan\theta = 4.89$. For higher values of Q, the error becomes less.

Note that from Figure 29 can be seen the simple relation:

$$\dot{Z} = R + jX_L$$

$$|Z| = \sqrt{R^2 + X_L^2}$$

Graphical Representation

Formulas and physical laws are often presented in graphical form; this gives us a "bird's eye view" of various possible conditions due to the variations of the quantities involved. In some cases graphs permit us to solve equations with greater ease than ordinary algebra.

Coordinate Systems All of us have used coordinate systems without realizing it. For instance, in modern cities we have numbered streets and numbered avenues. By this means we can define the location of any spot in the city if the nearest street crossings are named. This is nothing but an application of Cartesian coordinates.

In the Cartesian coordinate system (named after Descartes), we define the location of any point in a plane by giving its distance from each of two perpendicular lines or *axes*. Figure 30 illustrates this idea. The vertical axis is called the *Y-axis*, the horizontal axis is the *X-axis*. The intersection of these two axes is called the *origin, O*. The location of a point, P, (Figure 30) is defined by measuring the respective distances, *x* and *y* along the X-axis and the Y-axis. In this example the distance along the X-axis is 2 units and along the Y-axis is 3 units. Thus we define the point as

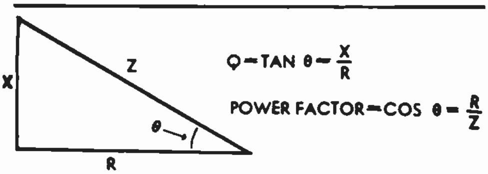


Figure 29.
The figure of merit of a coil and its resistance is represented by the ratio of the inductive reactance to the resistance, which as shown in this diagram is equal to $\frac{X_L}{R}$ which equals tan θ. For large values of θ (the phase angle) this is approximately equal to the reciprocal of the cos θ.

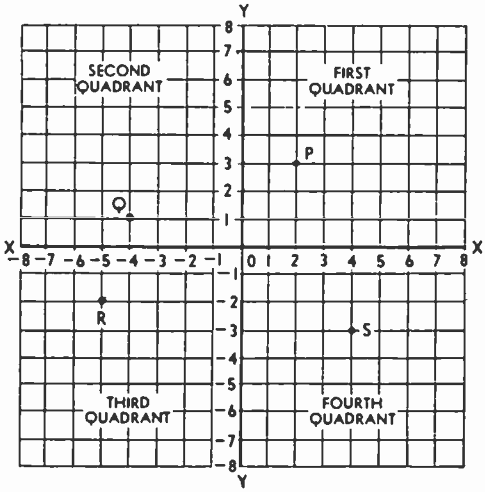


Figure 30.
CARTESIAN COORDINATES.
The location of any point can be defined by its distance from the X and Y axes.

P 2, 3 or we might say $x = 2$ and $y = 3$. The measurement x is called the *abscissa* of the point and the distance y is called its *ordinate.* It is arbitrarily agreed that distances measured from 0 to the right along the X-axis shall be reckoned positive and to the left negative. Distances measured along the Y-axis are positive when measured upwards from 0 and negative when measured downwards from 0. This is illustrated in Figure 30. The two axes divide the plane area into four parts called quadrants. These four quadrants are numbered as shown in the figure.

It follows from the foregoing statements, that points lying within the first quadrant have both x and y positive, as is the case with the point P. A point in the second quadrant has a negative abscissa, x, and a positive ordinate, y. This is illustrated by the point Q, which has the coordinates $x = -4$ and $y = +1$. Points in the third quadrant have both x and y negative. $x = -5$ and $y = -2$ illustrates such a point, R. The point S, in the fourth quadrant has a negative ordinate, y and a positive abscissa or x.

In practical applications we might draw only as much of this plane as needed to illustrate our equation and therefore, the scales along the X-axis and Y-axis might not start with zero and may show only that part of the scale which interests us.

Representation of Functions

In the equation:

$$f = \frac{300{,}000}{\lambda}$$

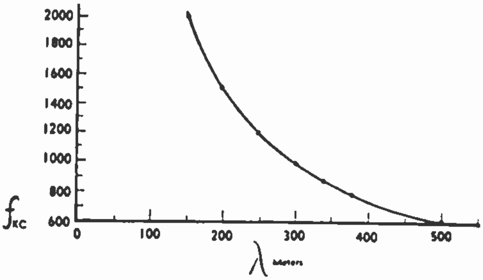


Figure 31.
REPRESENTATION OF A SIMPLE FUNCTION IN CARTESIAN COORDINATES.
In this chart of the function $f_{kc} = \frac{300{,}000}{\lambda_{meters}}$ distances along the X axis represent wavelength in meters, while those along the Y axis represent frequency in kilocycles. A curve such as this helps to find values between those calculated with sufficient accuracy for most purposes.

f is said to be a function of λ. For every value of f there is a definite value of λ. A variable is said to be a function of another variable when for every possible value of the latter, or *independent* variable, there is a definite value of the first or *dependent* variable. For instance, if $y = 5x^2$, y is a function of x and x is called the independent variable. When $a = 3b^3 + 5b^2 - 25b + 6$ then a is a function of b.

A function can be illustrated in our coordinate system as follows. Let us take the equation for frequency versus wavelength as an example. Given different values to the independent variable find the corresponding values of the dependent variable. Then plot the *points* represented by the different sets of two values.

$f_{kc.}$	λ_{meters}
600	500
800	375
1000	300
1200	250
1400	214
1600	187
1800	167
2000	150

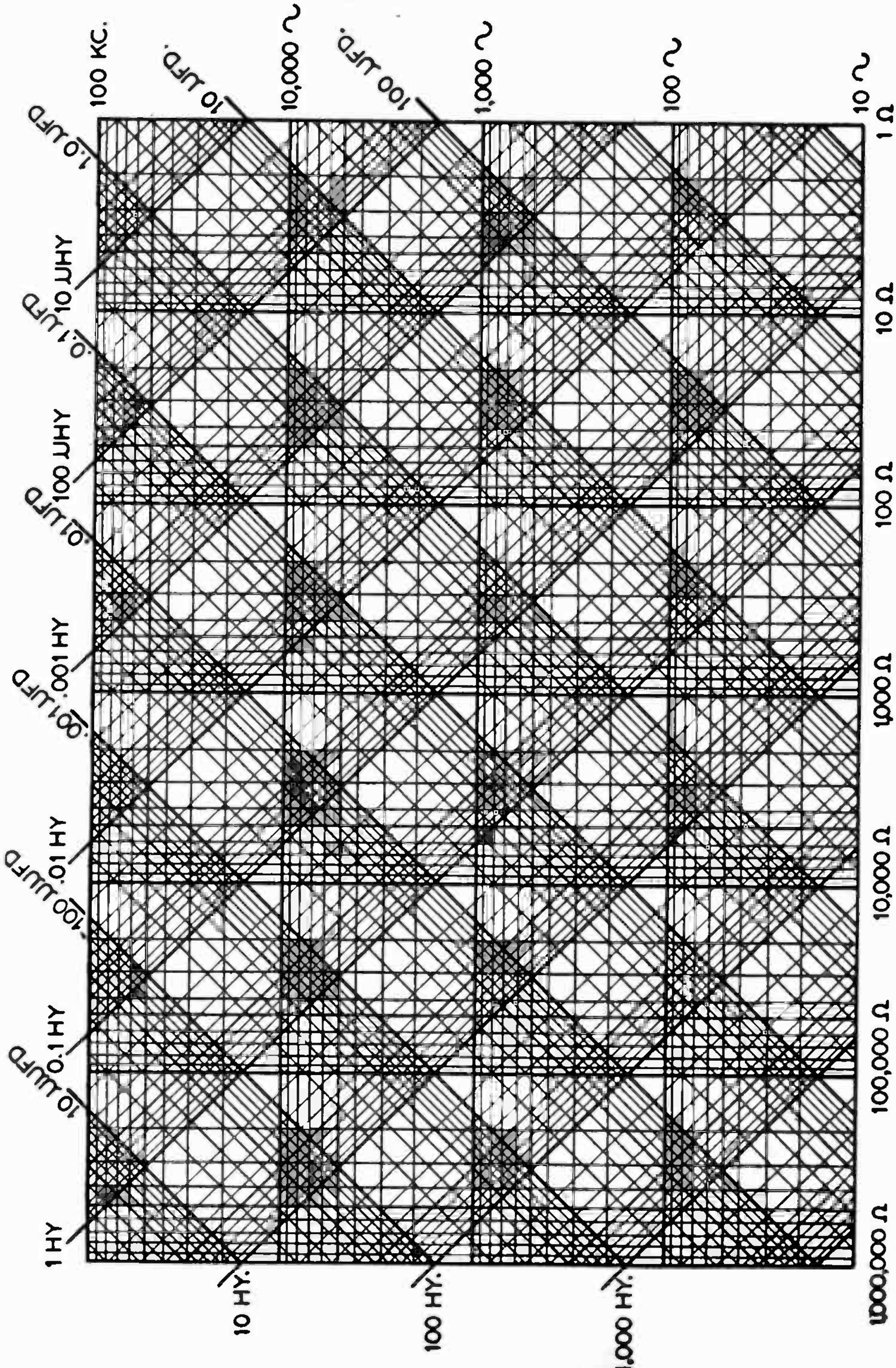
Plotting these points in Figure 31 and drawing a smooth curve through them gives us the *curve* or *graph* of the equation. This curve will help us find values of f for other values of λ (those in between the points calculated) and so a curve of an often-used equation may serve better than a table which always has gaps.

When using the coordinate system described so far and when measuring linearly along both axes, there are some definite rules regarding

Figure 40.

REACTANCE-FREQUENCY CHART FOR AUDIO FREQUENCIES

See text for applications and instructions for use.



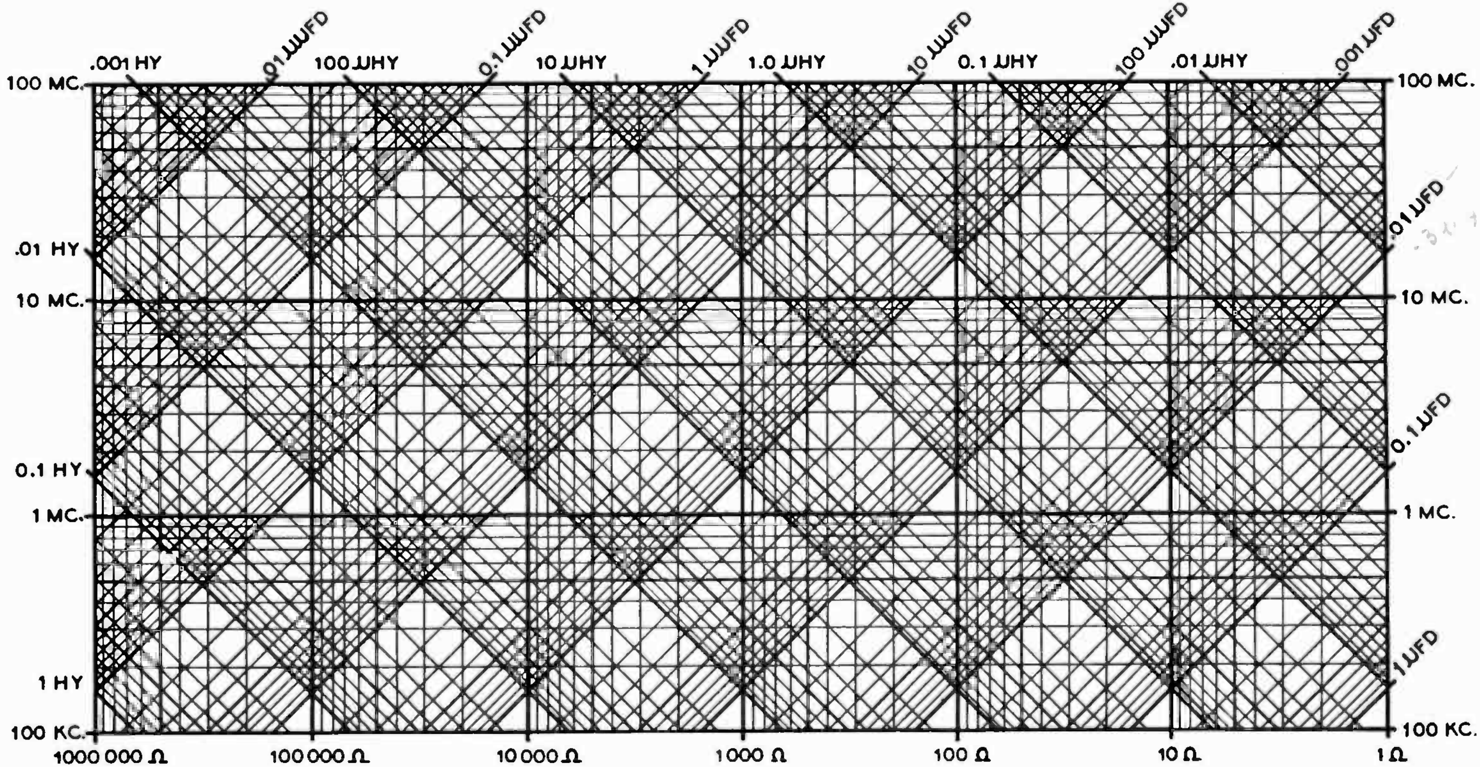


Figure 41.

REACTANCE-FREQUENCY CHART FOR R.F.

This chart is used in conjunction with the nomograph on page 569 for radio frequency tank coil computations.

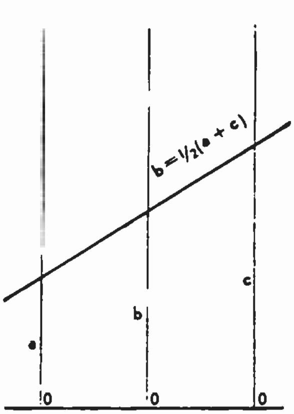


Figure 42.
THE SIMPLEST FORM OF NOMOGRAM.

plest form, it is somewhat like the lines in Figure 42. If the lines *a*, *b*, and *c* are parallel and equidistant, we know from ordinary geometry, that b = ½ (a + c). Therefore, if we draw a scale of the same units on all three lines, starting with zero at the bottom, we know that by laying a straight-edge across the chart at any place, it will connect values of *a*, *b*, and *c*, which satisfy the above equation. When any two quantities are known, the third can be found.

If, in the same configuration we used logarithmic scales instead of linear scales, the relation of the quantities would become

$$\log b = \tfrac{1}{2} (\log a + \log c) \text{ or } b = \sqrt{ac}$$

By using different kinds of scales, different units, and different spacings between the scales, charts can be made to solve many kinds of equations.

If there are more than three variables it is generally necessary to make a double chart, that is, to make the result from the first chart serve as the given quantity of the second one. Such an example is the chart for the design of coils illustrated in Figure 45. This nomogram is used to convert the inductance in microhenries to physical dimensions of the coil and vice versa. A pin and a straight edge are required. The method is shown under "R. F. Tank Circuit Calculations" later in this chapter.

Polar Coordinates Instead of the Cartesian coordinate system there is also another system for defining algebraically the location of a point or line in a plane. In this, the polar coordinate system, a point is determined by its distance from the origin, *O*, and by the angle it makes with the axis *O-X*. In Figure 43 the point *P* is defined by the length of *OP*, known as the radius vector and

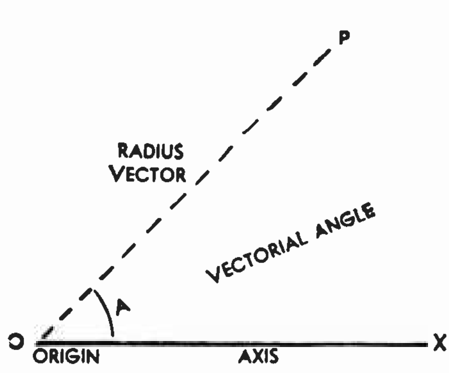


Figure 43.
THE LOCATION OF A POINT BY POLAR COORDINATES.
In the polar coordinate system any point is determined by its distance from the origin and the angle formed by a line drawn from it to the origin and the 0-X axis.

by the angle *A* the vectorial angle. We give these data in the following form

$$P = 3 \angle 60^\circ$$

Polar coordinates are used in radio chiefly for the plotting of directional properties of microphones and antennas. A typical example of such a directional characteristic is shown in Figure 44. The radiation of the antenna represented here is proportional to the distance of the characteristic from the origin for every possible direction.

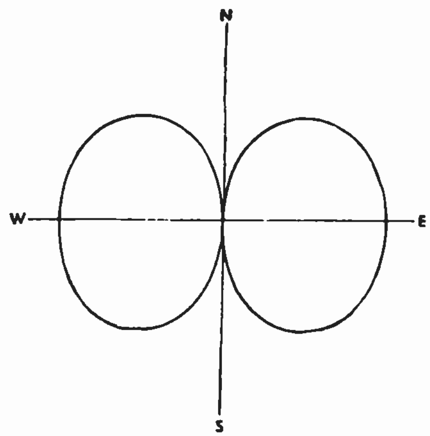


Figure 44.
THE RADIATION CURVE OF AN ANTENNA.
Polar coordinates are used principally in radio work for plotting the directional characteristics of an antenna where the radiation is represented by the distance of the curve from the origin for every possible direction.

Reactance Calculations

In audio frequency calculations, an accuracy to better than a few per cent is seldom required, and when dealing with calculations involving inductance, capacitance, resonant frequency, etc., it is much simpler to make use of reactance-frequency charts such as those on pages 667-668 rather than to wrestle with a combination of unwieldy formulas. From these charts it is possible to determine the reactance of a condenser or coil if the capacitance or inductance is known, and vice versa. It follows from this that resonance calculations can be made directly from the chart, because resonance simply means that the inductive and capacitive reactances are equal. The capacity required to resonate with a given inductance, or the inductance required to resonate with a given capacity, can be taken directly from the chart.

While the chart may look somewhat formidable to one not familiar with charts of this type, its application is really quite simple, and can be learned in a short while. The following example should clarify its interpretation.

For instance, following the lines to their intersection, we see that 0.1 hy. and 0.1 μfd. intersect at approximately 1,500 cycles and 1,000 ohms. Thus, the reactance of either the coil or condenser taken alone is about 1000 ohms, and the resonant frequency about 1,500 cycles.

To find the reactance of 0.1 hy. at, say, 10,000 cycles, simply follow the inductance line diagonally up towards the upper left till it intersects the horizontal 10,000 kc. line. Following vertically downward from the point of intersection, we see that the reactance at this frequency is about 6000 ohms.

To facilitate use of the chart and to avoid errors, simply keep the following in mind: The vertical lines indicate reactance in ohms, the horizontal lines always indicate the frequency, the diagonal lines sloping to the lower right represent inductance, and the diagonal lines sloping toward the lower left indicate capacitance. Also remember that the scale is *logarithmic*. For instance, the next horizontal line above 1000 cycles is *2000* cycles. Note that there are 9, not 10, divisions between the heavy lines. This also should be kept in mind when interpolating between lines when best possible accuracy is desired; halfway between the line representing 200 cycles and the line representing 300 cycles is *not* 250 cycles, but approximately 230 cycles. The 250 cycle point is approximately 0.7 of the way between the 200 cycle line and the 300 cycle line, rather than halfway between.

Use of the chart need not be limited by the physical boundaries of the chart. For instance, the 10-$\mu\mu$fd. line can be extended to find where it intersects the 100-hy. line, the resonant frequency being determined by projecting the intersection horizontally back on to the chart. To determine the reactance, the logarithmic ohms scale must be extended.

R. F. Tank Circuit Calculations When winding coils for use in radio receivers and transmitters, it is desirable to be able to determine in advance the full coil specifications for a given frequency. Likewise, it often is desired to determine how much capacity is required to resonate a given coil so that a suitable condenser can be used.

Fortunately, extreme accuracy is not required, except where fixed capacitors are used across the tank coil with no provision for trimming the tank to resonance. Thus, even though it may be necessary to estimate the stray circuit capacity present in shunt with the tank capacity, and to take for granted the likelihood of a small error when using a chart instead of the formula upon which the chart was based, the results will be sufficiently accurate in most cases, and in any case give a reasonably close point from which to start "pruning."

The inductance required to resonate with a certain capacitance is given in the chart on page 668. By means of the r.f. chart, the inductance of the coil can be determined, or the capacitance determined if the inductance is known. When making calculations, be sure to allow for stray circuit capacity, such as tube interelectrode capacity, wiring, sockets, etc. This will normally run from 5 to 25 micromicrofarads, depending upon the components and circuit.

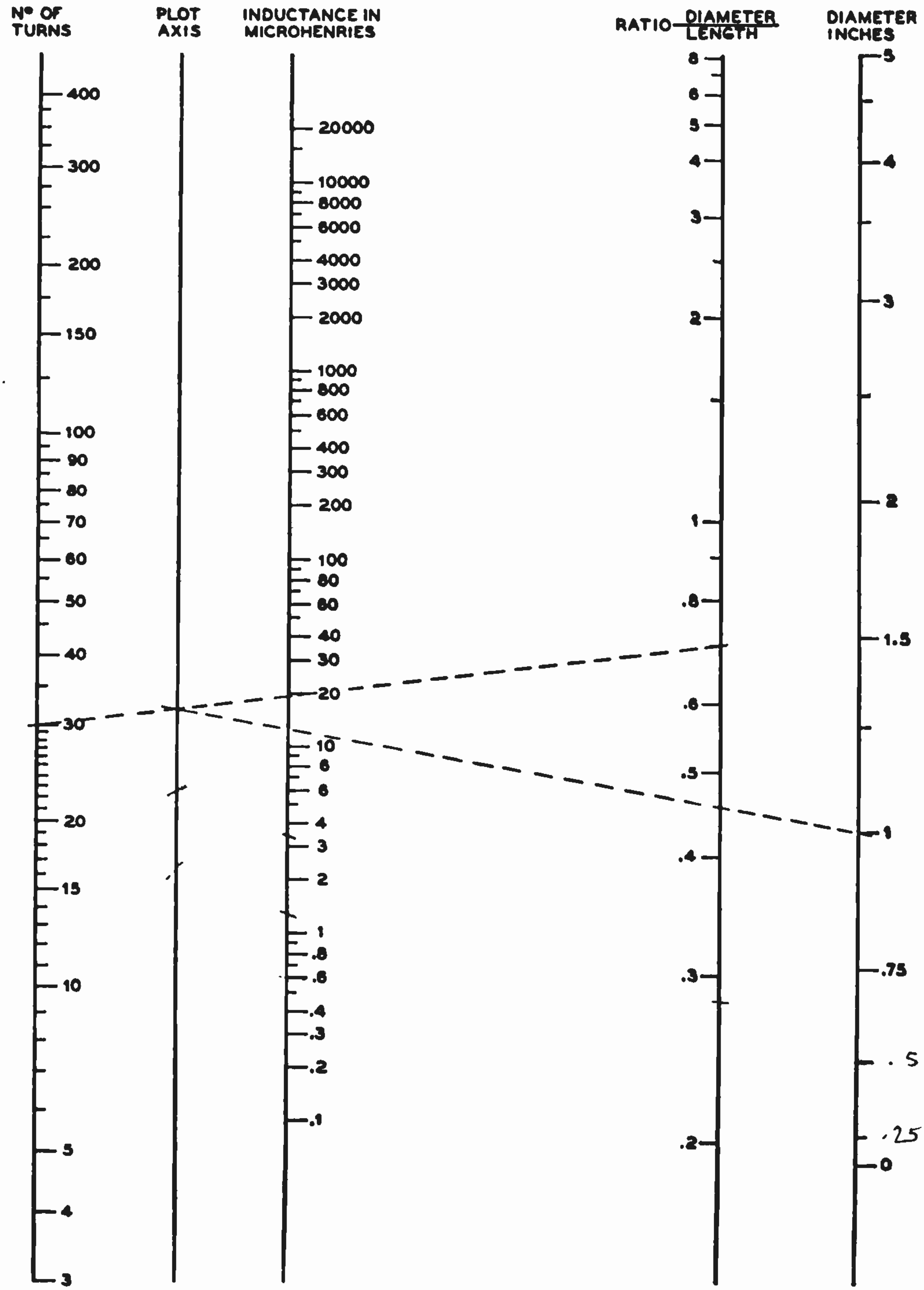
To convert the inductance in microhenries to physical dimensions of the coil, or vice versa, the nomograph chart on page 671 is used. A pin and a straightedge are required. The inductance of a coil is found as follows:

The straightedge is placed from the correct point on the turns column to the correct point on the diameter-to-length ratio column, the latter simply being the diameter divided by the length. Place the pin at the point on the plot axis column where the straightedge crosses it. From this point lay the straightedge to the correct point on the diameter column. The point where the straightedge intersects the inductance column will give the inductance of the coil.

From the chart, we see that a 30 turn coil having a diameter-to-length ratio of 0.7 and a diameter of 1 inch has an inductance of approximately 12 microhenries. Likewise any one of the four factors may be determined if the other three are known. For instance, to determine the number of turns when the desired in-

Figure 45. COIL CALCULATOR NOMOGRAPH

For single layer solenoid coils, any wire size. See text for instructions.



ductance, the D/L ratio, and the diameter are known, simply work backwards from the example given. In all cases, remember that the straightedge reads either turns and D/L ratio, *or* it reads inductance and diameter. It can read no other combination.

The actual wire size has negligible effect upon the calculations for commonly used wire sizes (no. 10 to no. 30). The number of turns of insulated wire that can be wound per inch (solid) will be found in the copper wire table on page 579.

Significant Figures

In most radio calculations, numbers represent quantities which were obtained by measurement. Since no measurement gives absolute accuracy, such quantities are only approximate and their value is given only to a few significant figures. In calculations, these limitations must be kept in mind and one should not finish for instance with a result expressed in more significant figures than the given quantities at the beginning. This would imply a greater accuracy than actually was obtained and is therefore misleading, if not ridiculous.

An example may make this clear. Many ammeters and voltmeters do not give results to closer than ¼ ampere or ¼ volt. Thus if we have 2¼ amperes flowing in a d.c. circuit at 6¾ volts, we can obtain a theoretical answer by multiplying 2.25 by 6.75 to get 15.1875 watts. But it is misleading to express the answer down to a ten-thousandth of a watt when the original measurements were only good to ¼ ampere or volt. The answer should be expressed as 15 watts, not even 15.0 watts. If we assume a possible error of ⅛ volt or ampere (that is, that our original data are only correct to the *nearest* ¼ volt or ampere) the true power lies between 14.078 (product of 2⅛ and 6⅝) and 16.328 (product of 2⅜ and 6⅞). Therefore, any third significant figure would be misleading as implying an accuracy which we do not have.

Conversely, there is also no point to calculating the value of a part down to 5 or 6 significant figures when the actual part to be used cannot be measured to better than 1 part in one hundred. For instance, if we are going to use 1% resistors in some circuit, such as an ohmmeter, there is no need to calculate the value of such a resistor to 5 places, such as 1262.5 ohm. Obviously, 1% of this quantity is over 12 ohms and the value should simply be written as 1260 ohms.

There is a definite technique in handling these approximate figures. When giving values obtained by measurement, no more figures are given than the accuracy of the measurement permits. Thus, if the measurement is good to two places, we would write, for instance, 6.9 which would mean that the true value is somewhere between 6.85 and 6.95. If the measurement is known to three significant figures, we might write 6.90 which means that the true value is somewhere between 6.895 and 6.905. In dealing with approximate quantities, the added cipher at the right of the decimal point has a meaning.

There is unfortunately no standardized system of writing approximate figures with many ciphers to the left of the decimal point. *69000* does not necessarily mean that the quantity is known to 5 significant figures. Some indicate the accuracy by writing 69×10^3 or 690×10^2 etc., but this system is not universally employed. The reader can use his own system, but whatever notation is used, the number of significant figures should be kept in mind.

Working with approximate figures, one may obtain an idea of the influence of the doubtful figures by marking all of them, and products or sums derived from them. In the following example, the doubtful figures have been underlined.

$$\begin{array}{r} 60\underline{3} \\ 34.\underline{6} \\ 0.120 \\ \hline 63\underline{7}.\underline{720} \end{array} \quad \textbf{answer: 638}$$

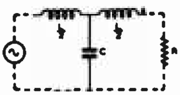
Multiplication:

$$\begin{array}{r} 65\underline{4} \\ 0.34\underline{2} \\ \hline 130\underline{8} \\ 261\underline{6} \\ 196\underline{2} \\ \hline 22\underline{3}.\underline{668} \end{array} \quad \textbf{answer: 224} \qquad \begin{array}{r} 65\underline{4} \\ 0.34\underline{2} \\ \hline 196|2 \\ 26|16 \\ 1|308 \\ \hline 224 \end{array}$$

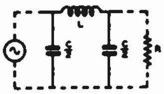
It is recommended that the system at the right be used and that the figures to the right of the vertical line be omitted or guessed so as to save labor. Here the partial products are written in the reverse order, the most important ones first.

In division, labor can be saved when after each digit of the quotient is obtained, one figure of the divisor be dropped. Example:

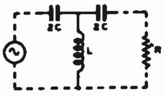
$$\begin{array}{r} 1.28 \\ 527\,)\overline{673} \\ 527 \\ \hline 53\,)\overline{146} \\ 106 \\ \hline 5\,)\overline{40} \\ 40 \\ \hline \end{array}$$



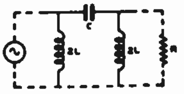
LOW-PASS T SECTION



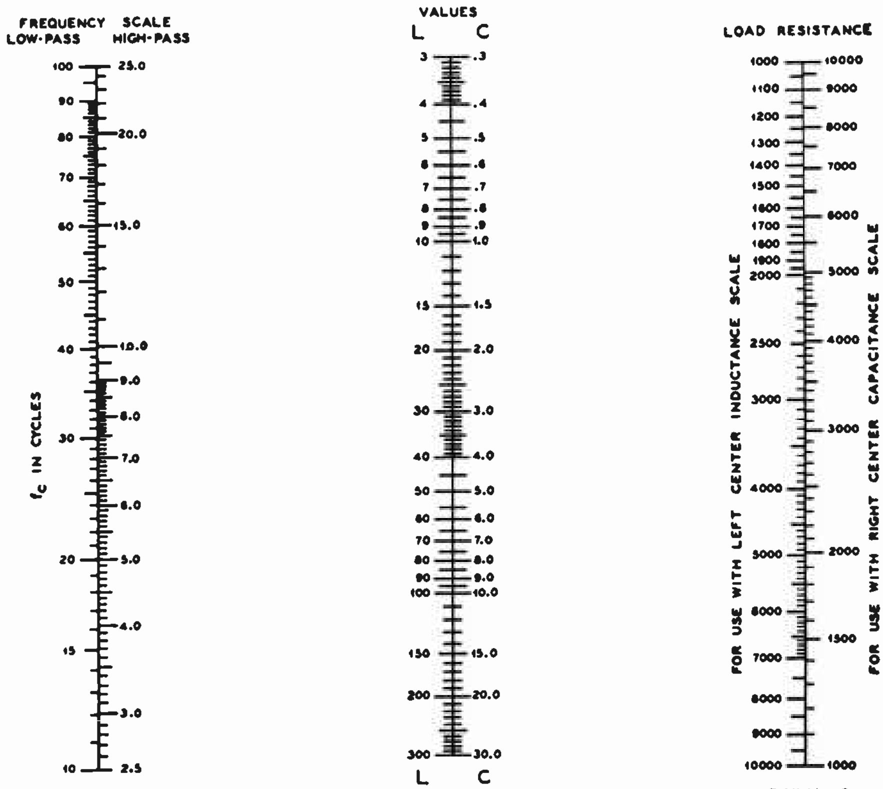
LOW-PASS π SECTION



HIGH-PASS T SECTION



HIGH-PASS π SECTION



Courtesy, Pacific Radio Publishing Co.

FILTER DESIGN CHART

For both Pi-type and T-type Sections

To find L, connect cut-off frequency on left-hand scale (using left-side scale for low-pass and right-side scale for high-pass) with load on left-hand side of right-hand scale by means of a straight-edge. Then read the value of L from the point where the edge intersects the left side of the center scale. Readings are in henries for frequencies in cycles per second.

To find C, connect cut-off frequency on left-hand scale (using left-side scale for low-pass and right-side scale for high pass) with the load on the right-hand side of the right-hand scale. Then read the value of C from the point where the straightedge cuts the right side of the center scale. Readings are in microfarads for frequencies in cycles per second.

For frequencies in kilocycles, C is expressed in thousands of micromicrofarads, L is expressed in millihenries. For frequencies in megacycles, L is expressed in microhenries and C is expressed in micromicrofarads.

For each tenfold increase in the value of load resistance multiply L by 10 and divide C by 10. For each tenfold decrease in frequency multiply L by 10 and multiply C by 10.

INDEX

A

B

C

D

E

F

G

H

I

J

K

L

M

N

O

P

Q

R

S

T

U

V

W

X

Y

Z

Every

ELECTRONIC TUBE IN 3 MANUALS

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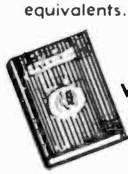

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