# -ELEGTRONIC <br> DATABOOK 3RD EDITION 

Packed with vital, up-to-date facts on every aspect of electronics practice . . . for hobbyists and professionals!


BY RUDOLF F. GRAF

# ELECTRONIC DATABOOK 3RD EDITION 

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## THIRD EDITION

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The entire electromagnetic spectrum is presented. Then portions of this spectrum that are of particular interest to the electrical and electronic engineer are described in greater detail.

## 2. COMMUNICATION

18Information useful in all segments of communication, starting with propagation characteristics, modes, standards, and transmission data is given. Antenna, transmission line, and waveguide characteristics and performance data are presented. Modulation and international telecommunications standards, signals, signal reporting codes, radio amateur data, and emission information are also given, as is information on microphones.
3. PASSIVE COMPONENTS AND CIRCUITS

Resistors, amplifiers, attenuators, filters, inductors, transformers, and capacitors are covered and their characteristics and applications are treated in depth. Computer-calculated tabulations of modern filter designs based on network synthesis are given.

## 4. ACTIVE COMPONENTS AND CIRCUITS

Vacuum tubes, semiconductors, and integrated circuits are covered. Circuit configurations are given in which these components are employed together with definitions of integrated circuit, logic, and microelectronic terms. A tabulation that shows the characteristics of integrated circuit logic families currently in use is given. Solid-state sensor characteristics and semiconductor memories are covered.

## 5. MATHEMATICAL DATA, FORMULAS, SYMBOLS

This section covers reliability; mathematical signs, symbols, operations, and tables; charts and formulas; prefixes; geometric curves; solids; spherical as well as plane geometry; and trigonometry. Frequency, phase angle, and time relationships for recurrent wave forms are given. Power and voltage level determinations in signals circuits are explained. Letter symbols for all quantities encountered in the electronics, electrical field are defined. This section concludes with a comprehensive selection of conversion factors.

## 6. PHYSICAL DATA

This section covers the most often needed physical data and includes, among other items, laser radiation, motors, radioactivity, optical data, sound, incandescent lamps, cathode ray tubes, crystals, color codes, relay contact code, military nomenclature, atmospheric and space data, chemical data, plastics, temperature and humidity tables, energy conversion factors and equivalents, wire data, hardware, shock and vibration, cooling data, and characteristics of materials.

INDEX

## Preface

This revised and expanded edition includes a great deal of new material that has come to light since the second edition was published.

The filter section has been thoroughly updated and now includes computer-generated tabulations of modern filter design based on network synthesis. This major entry was especially prepared for this book by Mr . Ed Wetherhold, whose contribution I most gratefully acknowledge.

I also wish to thank my friends and colleagues Rich Myers and F. Raymond Dewey for giving so unselfishly of their time to review and comment on the previous edition of this work and for generously sharing with me much of their private source material.

The word knowledge brings to mind the staggering body of facts and data accumulated by mankind since his descent from the trees. Once, thousands of years ago, it was possible for a man to know all that his kind had discovered. But, time has added so greatly to our reservoir of wisdom, that knowledge, today, has assumed another meaning: knowing where to find the information needed.

This book humbly admits to being my attempt at simplifying the task of the busy engineer, technician, amateur, and student in locating the data he needs in the shortest possible time.

Gathered here, in one single volume, is a wealth of information in the form of timely and practical nomograms, tables, charts, and formulas.

Some of the material was available elsewhere, at some time or other, but never has all of it been gathered together under one cover. New and heretofore unpublished charts and nomograms are added because of what seemed to me an obvious need for such material.

The book is arranged in a most readily usable format. It contains only clear-cut, theory-free data and examples that are concise, accurate, and to the point. The user of this book will be looking for answers and he will find them, without having to fight his way through lengthy derivations and proofs.

In order to assist you in finding the data you seek, the book has been divided into six functional sections. That organization, together with a comprehensive index, quickly leads to the specific information needed. The
book maintains uniform terminology and format which assures that data found in one section can be easily and accurately related to those in the rest of the book.

Much new and up-dated material has been added to this current edition of the book. It has been my intention (and certainly my hope) that this new material makes the book still more useful and comprehensive.

The preparation of a reference book such as this is not possible without the cooperation and assistance of numerous industry sources who have so generously made their material available. I gratefully acknowledge, with special thanks, the contributions and critical efforts of Messrs. George J. Whalen, Arthur E. Fury, Rene Colen, and B. William Dudley, Jr.

If this book saves you many hours of tedious computations and search for information, it will indeed have served its intended purpose.

The author and publisher invite your comments and suggestions regarding any such other material as might have been included here, so that it may be considered for any subsequent edition or revision.

## Acknowledgments

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Data for Radio Engineers, 5th Edition, (0) 1968).
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TRW, Capacitor Division, page 242.
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# ELECTRONIC DATABOOK <br> 3RD EDITION 

## Section 1

## Frequency Data

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## THE ELECTROMAGNETIC SPECTRUM

This chart presents an overview of the complete electromagnetic radiation spectrum, extending from infrasonics to cosmic rays. The wavelength, the amount of energy required to radiate one photon, a general description, the band designation, and the normal occurrence or use are given. Some specific bands are described in more detail on the following pages.

$$
\begin{aligned}
& \lambda_{\mathrm{m}}=\frac{300,000}{f_{\mathrm{kHz}}}=\frac{300}{f_{\mathrm{MHz}}} \quad \lambda_{\mathrm{cm}}=\frac{30}{f_{\mathrm{GHz}}} \\
& \lambda_{\mathrm{Ht}}=\frac{984,000}{f_{\mathrm{kHz}}}=\frac{984}{f_{\mathrm{MHz}}} \quad \lambda_{\mathrm{in}}=\frac{11.8}{f_{\mathrm{GHz}}}
\end{aligned}
$$

WAVELENGTH BANDS AND FREQUENCY USED IN RADIOCOMMUNICATION
Nomenclature of the frequency and wavelength bands used in radiocommunication in accordance with Article 2, No. 12 of the "Radio Regulations," Geneva, 1959.

| Band Number | Frequency Range (lower limit exclusive, upper limit inclusive) |  |  | Corresponding Metric Subdivision | Adjectival Band Designation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $3-$ | $30 \mathrm{c} / \mathrm{s}$ | $(\mathrm{Hz})$ | Petametric waves | ELF Extremely-Low Frequency |
| 2 | 30- | $300 \mathrm{c} / \mathrm{s}$ | $(\mathrm{Hz})$ | Terametric waves | SLF Super-Low Frequency |
| 3 | 300- | $3000 \mathrm{c} / \mathrm{s}$ | $(\mathrm{Hz})$ | Gigametric waves | ULF Ultra-Low Frequency |
| 4 |  | $30 \mathrm{kc} / \mathrm{s}$ | (kHz) | Myriametric waves | VLF Very-Low Frequency |
| 5 |  | $300 \mathrm{kc} / \mathrm{s}$ | (kHz) | Kilometric Waves | LF Low Frequency |
| 7 | $300-$ | $3000 \mathrm{kc} / \mathrm{s}$ | (kHz) | Hectometric waves | MF Medium Frequency |
| 7 |  | $30 \mathrm{Mc} / \mathrm{s}$ | (MHz) | Decametric waves | HF High Frequency |
| 8 |  | $300 \mathrm{Mc} / \mathrm{s}$ | (MHz) | Metric waves | VHF Very High Frequency |
| 9 | 300- | $3000 \mathrm{Mc} / \mathrm{s}$ | (MHz) | Decimetric waves | UHF Uiltra-High Frequency |
| 10 |  | $30 \mathrm{Gc} / \mathrm{s}$ | ( GHz ) | Centimetric waves | SHF Super-High Frequency |
|  |  | $300 \mathrm{Gc} / \mathrm{s}$ | (GHz) | Millimetric waves | EHF Extremely-High Frequency |
| 12 | 300- | $3000 \mathrm{Gc} / \mathrm{s}$ or $3 \mathrm{Tc} / \mathrm{s}$ | $\begin{aligned} & (\mathrm{GHz}) \\ & (\mathrm{THz}) \end{aligned}$ | Decimillimetric waves | - |

## BROADCASTING FREQUENCY ASSIGNMENTS

This table shows the frequency range, number of available channels, and channel width for AM, FM, and TV service in the United States.

| Type of <br> Service | Frequency Range | Number of <br> Available <br> Channels | Width of <br> Each Channel |
| :---: | :---: | :---: | :---: |
| AM radio | $535-1605 \mathrm{kHz}$ | 107 | 10 kHz |
| FM radio | $88-108 \mathrm{MHz}$ 100 <br> $54-72 \mathrm{MHz}$ $76-88 \mathrm{MHz}$ <br> $174-216 \mathrm{MHz}$ 12 |  |  |
| VHF television | $470-890 \mathrm{MHz}$ | 70 | 6 kHz |
| UHF television |  |  | 6 MHz |



| Channel <br> Number | Frequency Limits (MHz) | Video Carrier ( MHz ) <br> Sound Carrier ( MHz ) | Channel Number | Frequency Limits (MHz) | Video Carrier ( MHz ) Sound Carrier ( MHz ) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ----- | --596 -- | ------- | -----------698 ----------------- |  |  |
| 35 |  | $\begin{aligned} & 597.25 \\ & 601.75 \end{aligned}$ | 52 | $\begin{aligned} & 699 \\ & 703 \end{aligned}$ |  |
| 36 |  | $\begin{aligned} & 603.25 \\ & 607.75 \end{aligned}$ | 53 |  | $\begin{aligned} & 5.25 \\ & 9.75 \end{aligned}$ |
| 37 |  | $\begin{aligned} & 609.25 \\ & 613.75 \end{aligned}$ | 54 |  |  |
| 38 |  | $\begin{aligned} & 615.25 \\ & 619.75 \end{aligned}$ | 55 |  |  |
| 39 |  | $\begin{aligned} & 621.25 \\ & 625.75 \end{aligned}$ | 56 |  |  |
| 40 |  | $\begin{aligned} & 627.25 \\ & 631.75 \end{aligned}$ | 57 |  |  |
| 41 |  | $\begin{aligned} & 633.25 \\ & 637.75 \end{aligned}$ | 58 |  |  |
| 42 | 638 | $\begin{aligned} & 639.25 \\ & 643.75 \end{aligned}$ | 59 | 741 745 | $\begin{aligned} & 1.25 \\ & 5.75 \end{aligned}$ |
| 43 |  | $\begin{aligned} & 645.25 \\ & 649.75 \end{aligned}$ | 60 |  | $\begin{aligned} & 7.25 \\ & 1.75 \end{aligned}$ |
| 44 |  | $\begin{aligned} & 651.25 \\ & 655.75 \end{aligned}$ | 61 | $\begin{aligned} & 753 \\ & 757 \end{aligned}$ | $\begin{aligned} & 3.25 \\ & 7.75 \end{aligned}$ |
| 45 |  | $\begin{aligned} & 657.25 \\ & 661.75 \end{aligned}$ | 62 |  | $\begin{array}{r} 39.25 \\ 33.75 \end{array}$ |
| 46 |  | $\begin{aligned} & 663.25 \\ & 667.75 \end{aligned}$ | 63 |  | $\begin{aligned} & 5.25 \\ & 39.75 \end{aligned}$ |
| 47 |  | $\begin{aligned} & 669.25 \\ & 673.75 \end{aligned}$ | 64 |  | $\begin{aligned} & 71.25 \\ & 75.75 \end{aligned}$ |
| 48 |  | $\begin{aligned} & 675.25 \\ & 679.75 \end{aligned}$ | 65 | $\begin{aligned} & 777 \\ & 78 \end{aligned}$ |  |
| 49 |  | $\begin{aligned} & 681.25 \\ & 685.75 \end{aligned}$ | 66 |  | $\begin{aligned} & 33.25 \\ & 37.75 \end{aligned}$ |
| 50 |  | $\begin{aligned} & 687.25 \\ & 691.75 \end{aligned}$ | 67 |  | $\begin{aligned} & 89.25 \\ & 93.75 \end{aligned}$ |
| 51 |  | $\begin{aligned} & 693.25 \\ & 697.75 \end{aligned}$ | 68 |  | $\begin{aligned} & 95.25 \\ & 99.75 \end{aligned}$ |


| Channel Number | Frequency Limits <br> ( MHz ) | Video Carrier ( MHz ) <br> Sound Carrier ( MHz ) |
| :---: | :---: | :---: |
| ----- | ----800 - | --------- |
| 69 |  | 801.25 |
|  |  | 805.75 |
| 70 (*) |  | 807.25 |
|  |  | 811.75 |
| 71 |  | 813.25 |
|  |  | 817.75 |
| 72 |  | 819.25 |
|  |  | 823.75 |
| 73 |  | 825.25 |
|  |  | 829.75 |
| 74 |  |  |
|  |  | 831.25 |
|  |  | 835.75 |
| 75 |  | 837.25 |
|  |  | 841.75 |
| 76 |  | 843.25 |
|  |  | 847.75 |
| 77 |  | 849.25 |
|  |  | 853.75 |
| 78 |  |  |
|  |  |  |
|  | -860 | ------ |
| 79 |  | 861.25 |
|  |  | 865.75 |
| 80 |  | 867.25 |
|  |  | $871.75$ |
| 81 |  | 873.25 |
|  |  | 877.75 |
|  | -878-- | -------- |
| 82 |  | 879.25 |
|  |  | 883.75 |
| 83 |  | 885.25 |
|  |  | 889.75 |

(*)Channels 70 to 83 were withdrawn and reassigned to TV translator station until licenses expire. License renewals will be granted only a secondary basis for land mobile radio operation.

FREQUENCIES IN USE AROUND THE WORLD IN THE AERONAUTICAL MOBILE BANDS

| WORLD AIR <br> ROUTE AREA | FREQUENCY ALLOCATION (kHz) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alaska | 2945 | 3411.5 | 4668.5 | 5611.5 | 6567 |  | 11,328 |  |
| Hawall |  | 3453.5 |  | 5559 | 6649.5 |  |  |  |
| West Indles | 2861 |  | 4689.5 |  |  |  |  |  |
| Cantral East Pacific |  | $\begin{aligned} & 3432.5 \\ & 3446.5 \\ & 3467.5 \\ & 3481.5 \end{aligned}$ |  | $\begin{aligned} & 5551.5 \\ & 5604 \end{aligned}$ | $\begin{aligned} & 6612 \\ & 6679.5 \end{aligned}$ | $\begin{aligned} & 8879.5 \\ & 8930.5 \end{aligned}$ | $\begin{aligned} & 10,048 \\ & 10,084 \\ & 11,299.5 \\ & 11,318.5 \end{aligned}$ | $\begin{aligned} & 13,304.5 \\ & 13,334.5 \\ & 17,926.5 \end{aligned}$ |
| Cantral West Pacific | 2966 |  |  | $\begin{aligned} & 5506.5 \\ & 5536.5 \end{aligned}$ |  | 8862.5 |  | $\begin{aligned} & 13,354.5 \\ & 17,906.5 \end{aligned}$ |
| North Pacific | 2987 |  |  | 5521.5 |  | 8939 |  | $\begin{aligned} & 13,274.5 \\ & 17,906.5 \end{aligned}$ |
| South Pacific | 2945 |  |  | 5641.5 |  | 8845.5 |  | $\begin{aligned} & 13,344.5 \\ & 17,946.5 \end{aligned}$ |
| North Atiantic | $\begin{aligned} & 2868 \\ & 2931 \\ & 2945 \\ & 2987 \end{aligned}$ |  |  | $\begin{aligned} & 5611.5 \\ & 5626.5 \\ & 5641.5 \\ & 5671.5 \end{aligned}$ |  | $\begin{aligned} & 8862.5 \\ & 8888 \\ & 8913.5 \\ & 8947.5 \end{aligned}$ |  | $\begin{aligned} & 13,264.5 \\ & 13,284.5 \\ & 13,324.5 \\ & 13,354.5 \\ & 17,966.5 \end{aligned}$ |
| Europe | $\begin{aligned} & 2889 \\ & 2910 \end{aligned}$ | $\begin{aligned} & 3467.5 \\ & 3481.5 \end{aligned}$ | $\begin{aligned} & 4654.5 \\ & 4689.5 \end{aligned}$ | 5551.5 | $\begin{aligned} & 6552 \\ & 6582 \end{aligned}$ | $\begin{aligned} & 8871 \\ & 8930.5 \end{aligned}$ | 11,299.5 | 17,906.5 |
| North-South Amarica | $\begin{aligned} & 2889 \\ & 2910 \\ & 2966 \end{aligned}$ | 3404.5 | 4696.5 | $\begin{aligned} & 5566.5 \\ & 5581.5 \end{aligned}$ | $\begin{aligned} & 6567 \\ & 6664.5 \end{aligned}$ | 8820 8845.5 8871 | $\begin{aligned} & 11,290 \\ & 11,337.5 \end{aligned}$ | $\begin{aligned} & 13,314.5 \\ & 13,344.5 \\ & 17,916.5 \end{aligned}$ |
| Far East | $\begin{aligned} & 2868 \\ & 2987 \end{aligned}$ |  |  | $\begin{aligned} & 5611.5 \\ & 5671.5 \end{aligned}$ |  | 8871 <br> 8879.5 <br> 8930.5 |  | $\begin{aligned} & 13,284.5 \\ & 13,324.5 \\ & 17,966.5 \end{aligned}$ |
| South Atiantic | 2875 | 3432.5 |  |  | $\begin{aligned} & 6597 \\ & 6612 \\ & 6679.5 \end{aligned}$ | $\begin{aligned} & 8879.5 \\ & 8939 \end{aligned}$ | 10,048 | $\begin{aligned} & 13,274.5 \\ & 17,946.5 \end{aligned}$ |
| Middla East |  | $\begin{aligned} & 3404.5 \\ & 3446.5 \end{aligned}$ |  | 5604 | 6627 | 8845.5 | 10,021 | $\begin{aligned} & 13,334.5 \\ & 17,926.5 \end{aligned}$ |
| North-South Africa | 2966 | 3411.5 |  | $\begin{aligned} & 5506.5 \\ & 5521.5 \end{aligned}$ |  | $\begin{aligned} & 8820 \\ & 8956 \end{aligned}$ |  | $\begin{aligned} & 13,304.5 \\ & 13,334.5 \\ & 17,926.5 \\ & 17,946.5 \end{aligned}$ |
| Carlbbean | $\begin{aligned} & 2875 \\ & 2952 \\ & 2966 \end{aligned}$ |  |  | 5499 <br> 5566.5 <br> 5619 | 6537 | $\begin{aligned} & 8837 \\ & 8871 \end{aligned}$ | 10,021 | $\begin{aligned} & 13,294.5 \\ & 13,344.5 \\ & 17,936.5 \end{aligned}$ |
| Canada | 2973 |  |  | 5499 |  | 8871 | 11,356.5 |  |

FREQUENCIES USED BY SHIP AND SHORE STATIONS

| Band (MHz) | SHIP STATIONS |  | SHORE STATIONS |
| :---: | :---: | :---: | :---: |
|  | Calling Frequencies (kHz) | Working Frequencies (kHz) | (Approximate Limits) |
| 2 | 2065-2107 | Same as calling | 2000-2065 |
| 4 | 4178-4186 | $\begin{aligned} & 4161-4176 \\ & 4188-4236 \end{aligned}$ | 4240-4400 |
| 6 | 6267-6279 | $\begin{aligned} & 6241-6264 \\ & 6282-6355 \end{aligned}$ | 6362-6523 |
| 8 | $8356-8372$ | $\begin{aligned} & 8322-8352 \\ & 8376-8473 \end{aligned}$ | 8478-8742 |
| 12 | 12,534-12,558 | $\begin{aligned} & 12,474-12,528 \\ & 12,564-12,709 \end{aligned}$ | 12,714-13,128 |
| 16 | 16,712-16,744 | $\begin{aligned} & 16,626-16,704 \\ & 16,752-16,946 \end{aligned}$ | $16,950-17,285$ |
| 22 | 22,225-22,265 | $\begin{aligned} & 22,151-22,217 \\ & 22,272-22,395 \end{aligned}$ | 22,400-22,670 |

INTERNATIONAL AMPLITUDE-MDDULATIDN BRDADCASTING FREqUENCIES
$5.950-\quad 6.200 \mathrm{MHz}$
$9.500-9.775$
$11.70-11.975$
$15.10-15.45$
$17.70-17.90$
$21.45-21.75$
$25.60-26.10$

AMATEUR RADID FREQUENCIES

| 1800 | -2000 kHz | $3.300-3.500 \mathrm{GHz}$ |
| ---: | ---: | ---: |
| $3.500-4.000 \mathrm{MHz}$ | $5.650-5.925$ |  |
| $7.000-7.300$ | $10.00-10.50$ |  |
| $14.00-14.35$ | $24.00-24.25$ |  |
| $21.00-21.45$ | $48.00-50.00$ |  |
| $28.00-29.70$ | $71.00-84.00$ |  |
| $50.00-54.00$ | $152.0-170.0$ |  |
| $144.0-148.0$ | $200.0-220.0$ |  |
| $220.0-225.0$ | $240.0-250.0$ |  |
| $420.0-450.0$ | Above 275.0 |  |
| 1215 |  |  |
| 2300 | -2450 |  |

CITIZINS RADID (PERSONAL RADIO) FREQUENCIES
$26.96 \quad 27.23 \mathrm{MHz}$
$462.5375-462.7375$
$467.5375-467.7375$

CDMMDNLY USED LETTER-CDDE DESIGNATIDNS FOR MICROWAVE FREQUENCY BANDS

| Band | Frequency | Wavelength | Typical Use |
| :---: | :---: | :---: | :---: |
| P | 225-390 MHz | $133.3-76.9 \mathrm{~cm}$ | Long range (over 200 miles) to very long range (beyond 1,000 miles) surface-to-air search. |
| L | $390-1550 \mathrm{MHz}$ | $76.9-19.3 \mathrm{~cm}$ | Very long through medium range surface-to-air missile and aircraft detection, tracking and air traffic control, IFF transponders, beacon systems. |
| S | $1.55-5.2 \mathrm{GHz}$ | $19.3-5.77 \mathrm{~cm}$ | Medium and long range surface-to-air surveillance, surfacebased weather radar, altimetry, missile-borne guidance, airbome bomb-navigation systems. |
| C | $3.9-6.2 \mathrm{MHz}$ | $7.69-4.84 \mathrm{~cm}$ | Airborne fire control, missile-borne beacons, recon, airborne weather avoidance, aircraft and missile target tracking. |
| X | $5.2-10.9 \mathrm{MHz}$ | $5.77-2.75 \mathrm{~cm}$ | Doppler navigation, airborne fire control, airbome and sur-face-based weather detection, bomb-navigation systems, missile-bome guidance, precision landing approach. |
| K | $10.9-36 \mathrm{GHz}$ | $2.75-0.834 \mathrm{~cm}$ | Doppler navigation, automatic landing systems, airborne fire control, radar fuzing, recon, missile-borne guidance. |
| Q | $36-46 \mathrm{GHz}$ | $0.834-0.652 \mathrm{~cm}$ | Recon, airport surface detection. |
| V | $46-56 \mathrm{GHz}$ | $0.652-0.536 \mathrm{~cm}$ | High-resolution experimental shortrange systems. |

## CTCS (CONTINUOUS TONE CODED SQUELCH) AND REMOTE CONTROL STANDARD FREQUENCY TABLE

The EIA Standard Tone Frequencies for remote (i.e., radio paging) and control applications have been established to allow adequate separation and minimum harmonic relationship for use in multiple frequency systems.

For optimum system performance it is best to choose the widest frequency spacing possible within the recommended range.

| Frequency | EIA | Frequency | EIA | Frequency | EIA |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hz 67.0 | Code | Hz 258.8 | Code 136 | Hz 651.9 | Code 153 |
| 71.9 | L 2 | 266.0 | 106 | 669.9 | 123 |
| 77.0 | L 3 | 273.3 | 137 | 688.3 | 154 |
| 82.5 | L 4 | 280.8 | 107 | 707.3 | 124 |
| 88.5 | L 4A | 288.5 | 138 | 726.8 | 155 |
| 94.8 | L 5 | 296.5 | 108 | 746.8 | 125 |
| 100.0 | 1 | 304.7 | 139 | 767.4 | 156 |
| 103.5 | 1A | 313.0 | 109 | 788.5 | 126 |
| 107.2 | 1B | 321.7 | 140 | 810.2 | 157 |
| 110.9 | 2 | 330.5 | 110 | 832.5 | 127 |
| 114.8 | 2A | 339.6 | 141 | 855.2 | 158 |
| 118.8 | 2B | 349.0 | 111 | 879.0 | 128 |
| 123.0 | 3 | 358.6 | 142 | 903.0 | 159 |
| 127.3 | 3A | 368.5 | 112 | 928.1 | 129 |
| 131.8 | 3B | 378.6 | 143 | 953.7 | 160 |
| 136.5 | 4 | 389.0 | 113 | 979.9 | 130 |
| 141.3 | 4 A | 399.8 | 144 | 1006.9 | 161 |
| 146.2 | 4B | 410.8 | 114 | 1049.6 | 131 |
| 151.4 | 5 | 422.1 | 145 | 1084.0 | P |
| 156.7 | 5A | 433.7 | 115 | 1120.0 | S11 |
| 162.2 | 5B | 445.7 | 146 | 1190.0 | S12 |
| 167.9 | 6 | 457.9 | 116 | 1220.0 | S2 |
| 173.8 | 6A | 470.5 | 147 | 1265.0 | S14 |
| 179.9 | 6B | 483.5 | 117 | 1291.4 | S3 |
| 186.2 | 7 | 496.8 | 148 | 1320.0 | S15 |
| 192.8 | 7A | 510.5 | 118 | 1355.0 | S16 |
| 203.5 | M1 | 524.6 | 149 | 1400.0 | S17 |
| 210.7 | M2 | 539.0 | 119 | 1430.5 | S7 |
| 218.1 | M3 | 553.9 | 150 | 1450.0 | S18 |
| 225.7 | M4 | 569.1 | 120 | 1500.0 | S20 |
| 233.6 | M5 | 582.1 | H | 1520.0 | S9 |
| 241.8 | M6 | 600.9 | 121 | 1550.0 | S21 |
| 250.3 | M7 | 617.4 | 152 | 1600.0 | S22 |
|  |  | 634.5 | 122 |  |  |

The table lists the ultrasonic transducer materials used in instrumentation, sensing and power applications.

| Piezoelectric Transducers |  |  |  |
| :---: | :---: | :---: | :---: |
| Material | Frequency Range | Maximum Safe Operating Temperature | Typical Applications |
| Quartz | $100 \mathrm{kHz}-35+\mathrm{MHz}$ | $550^{\circ} \mathrm{C}$ | Medical and non-destructive testing |
| Barium Titanate | $100 \mathrm{kHz}-10 \mathrm{MHz}$ | $100^{\circ} \mathrm{C}$ | Most cleaning and processing applications |
| Lead Zirconate Lead Titanate | $5 \mathrm{kHz}-10 \mathrm{MHz}$ | $320^{\circ} \mathrm{C}$ | Most cleaning and processing applications, (high temperature uses) |
| Rochelle Salt | $20 \mathrm{~Hz}-1 \mathrm{MHz}$ | $45^{\circ} \mathrm{C}$ | Sonar and depth finding |
| Magnetostrictive Transducers |  |  |  |
| Nickel | $10 \mathrm{kHz}-100 \mathrm{kHz}$ | - | Cleaning, drilling, machining, soldering, melt treatment, and applications where transducer has pressure applied |
| Venadium Permendur | $10 \mathrm{kHz}-100 \mathrm{kHz}$ | - | Same as nickel |

## ULTRASONIC FREQUENCY SPECTRUM

## Ultrasonic Frequency Spectrum



## NBS STANDARD FREQUENCY AND TIME BROADCAST SCHEDULES

The diagrams presented here, with explanatory notes, summarize the technical services provided by the National Bureau of Standards (NBS) radio stations WWV, WWVH, WWVB, and WWVL.

## WWV and WWVH Broadcast Services

Standard Radio Frequencies. WWV and WWVH transmit frequencies and time coordinated through the Bureau Intemational de l'Heure (BIH), Paris, France. Transmissions are based upon the International time scale, Universal Coordinated Time (UTC).

WWV broadcasts continuously on radio carrier frequencies of $2.5,5,10,15,20$, and 25 MHz . WWVH broadcasts continuously on radio carrier frequencies of $2.5,5,10,15$ and 20 MHz .

The broadcasts of WWV may also be heard via telephone by dialing (303) 499-7111, Boulder, Colorado.
Standard Audio Frequencies. Standard audio frequencies of $440 \mathrm{~Hz}, 500 \mathrm{~Hz}$, and 600 Hz are broadcast on each radio carnier frequency by the two stations. Duration of each transmitted standard tone is approximately 45 seconds. A $600-\mathrm{Hz}$ tone is broadcast during odd minutes by WWV and during even minutes by WWVH. A $500-\mathrm{Hz}$ tone is broadcast during alternate minutes unless voice announcements or silent periods are scheduled. The $440-\mathrm{Hz}$ tone is broadcast beginning one minute after the hour at WWVH and two minutes after the hour at WWV. The $440-\mathrm{Hz}$ tone period is omitted during the first hour of the UTC day.

Standard Musical Pitch. The $440-\mathrm{Hz}$ tone is broadcast for approximately 45 seconds beginning 1 minute after the hour at WWVH and 2 minutes after the hour at WWV. The tone is omitted during the zero hour of each UTC day.

Standard Time Intervals. Seconds pulses at precise intervals are derived from the same frequency standard that controls the radio carrier frequencies. Every minute, except the first of the hour, begins with a 800 -millisecond tone of $1,000 \mathrm{~Hz}$ at WWV and $1,200 \mathrm{~Hz}$ at WWVH. The first minute of every hour begins with an 800 -millisecond tone of $1,500 \mathrm{~Hz}$ at both stations.

The 1 -second markers are transmitted throughout all programs of WWV and WWVH except that the 29th of the 59th markers of each minute are omitted.

Time Signals. The time announcements of WWV and WWVH reference the Coordinated Universal Time Scale maintained by the National Bureau of Standards, UTC(NBS).

The 0 to 24 hour system is used starting with 0000 for midnight at the Greenwich Meridian (longitude zero). The first two figures give the hour, and the last two figures give the number of minutes past the hour when the tone returns.

At WWV a voice announcement of Greenwich Mean Time is given during the 7.5 seconds immediately preceding the minute.

At WWVH a voice announcement of Greenwich Mean Time occurs during the period 15 seconds to 7.5 seconds preceding the minute. The voice announcement for WWVH precedes that of WWV by 7.5 seconds. However, the tone markers referred to in both announcements occur simultaneously.

Propagation Forecasts. A forecast of radio propagation conditions is broadcast in voice from WWV at 14 minutes after every hour. The announcements are short-term forecasts and refer to propagation along paths in the North Atlantic area, such as Washington, D.C. to London or New York to Berlin.

The propagation forecast announcements are repeated in synoptic form comprised of a phonetic and a numeral. The phonetic (Whiskey, Uniform, or November) identifies the radio quality at the time the forecast is made. The numeral indicates on a scale of 1 to 9 the radio propagation quality expected during the six-hour period after the forecast is issued. The meaning of the phonetics and numerals are:

| Phonetic | Meaning |
| :--- | :--- |
| Whiskey | disturbed |
| Uniform | unsettled |
| November | normal |


| Numeral | Meaning |
| :--- | :--- |
| One | useless |
| Two | very poor |
| Three | poor |
| Four | poor-to-fair |
| Five | fair |
| Six | fair-to-good |
| Seven | good |
| Eight | very good |
| Nine | excellent |

If, for example, propagation conditions are normal and expected to be good during the next six hours, the coded forecast announcement would be "November Seven."

Geophysical Alerts. Current geophysical alerts (Geoalerts) as declared by the World Warning Agency of the International Ursigram and World Days Service (IUWDS) are broadcast in voice from WWV at 18 minutes after each hour and from WWVH at 45 minutes after each hour.

Weather Information. Weather information about major storms in the Atlantic and Pacific areas is broadcast from WWV and WWVH respectively.

Time Code. The time code is transmitted continuously by both WWV and WWVH on a $100-\mathrm{Hz}$ subcarrier. The code format is a modified IRIG-H time code produced at a $1-\mathrm{pps}$ rate and carried on $100-\mathrm{Hz}$ modulation. The $100-\mathrm{Hz}$ subcarrier is synchronous with the code pulses so that $10-$ millisecond resolution is readily obtained.

The code contains UTC time-of-year information in minutes, hours, and day of year. Seconds information may be obtained by counting pulses.

The binary coded decimal (BCD) system is used. Each minute contains seven BCD groups in this order: two groups for minutes, two groups for hours, and three groups for day of year. The code digit weighting is 1-2-4-8 for each BCD group multiplied by 1,10 , or 100 as the case may be. A complete time frame is 1 minute. The binary groups follow the 1-minute reference marker.

Modulation. At WWV and WWVH, double sideband amplitude modulation is employed with 50 percent modulation on the steady tones, 25 percent for the IRIG-H code, 100 percent for seconds pulses, and 75 percent for voice.

## WWVB Broadcast Services

WWVB transmits a standard radio frequency, standard time signals, time intervals, and UT1 corrections. The station is located near WWV on the same site.

Program. WWVB broadcasts a standard radio carrier frequency of 60 kHz with no offset. It also broadcasts a time code consistent with the internationally coordinated time scale UTC(NBS).

## WWVL Experimental Broadcasts

WWVL broadcasts experimental programs, usually involving multiple frequencies. The station is located in the same building with WWVB and on the same site with WWV.

Effective On UTC, 1 July 1972, regularly scheduled transmissions from WWVL were discontinued. Contingent upon need and availability of funds this station broadcasts experimental programs on an intermittent basis only.

WWVL transmits only carrier frequencies with no modulation. The format and frequencies used by WWVL are subject to change to meet the requirements of the particular experiment being conducted.


This scale is based on the formula

$$
\lambda_{m}=\frac{300}{f_{M H Z}}
$$

It shows the relationship between free space wavelength $\lambda$ and frequency $f$ and covers a frequency range extending from 300 Hz to 300 GHz , corresponding to wavelengths of $1000 \mathrm{~m}(1 \mathrm{~km})$ to 1 mm .

FOR EXAMPLE: A $60-\mathrm{MHz}$ signal has a wavelength of 5 m . A signal whose wavelength is 3 mm has a frequency of 100 GHz .


## Section 2

## Communication

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PROPAGATION CHARACTERISTICS OF ELECTROMAGNETIC WAVES

| Band | Frequency (Wavelength) | Characteristics | Applications |
| :---: | :---: | :---: | :---: |
| Very-low frequency (VLF) | $\begin{aligned} & 20-30 \mathrm{kHz} \\ & (20,000-10,000 \mathrm{~m}) \end{aligned}$ | Very stable; low attenuation at all times. Influenced by magnetic storms. Ground wave extends over long distances. (No fading out long-time variations occur.) | Continuously operating longdistance station-to-station communication service. |
| Low frequency (LF) | $\begin{aligned} & 30-300 \mathrm{kHz} \\ & (10,000-1,000 \mathrm{~m}) \end{aligned}$ | Seasonal and daily variations greater than that of VLF; daytime absorption also greater, increasing with frequency. At night similar to VLF although slightly less reliable. | Long-distance station-to-station service (marine, navigational aids). |
| Medium frequency (MF) | $\begin{aligned} & 300-3,000 \mathrm{kHz} \\ & (1,000-100 \mathrm{~m}) \end{aligned}$ | Less reliable over long distances than lower frequencies. Attenuation: low at night, high in daytime; greater in summer than in winter. Low attenuation at night is due to sky-wave reflection. Ground-wave attenuation is relatively high over land and low over salt water. | Commercial broadcasting police, marine and airplane navigation. |
| High frequency (HF) | $\begin{aligned} & 3-30 \mathrm{MHz} \\ & (100-10 \mathrm{~m}) \end{aligned}$ | Dependent on ionospheric conditions, leading to considerable variation from day to night and from season to season. Attenuation low under favorable conditions, and high under unfavorable conditions, at medium to very long distances. | Medium and long-distance communication service of all types. |
| Very-high frequency (VHF) | $\begin{aligned} & 30-300 \mathrm{MHz} \\ & (10-1 \mathrm{~m}) \end{aligned}$ | $30-60 \mathrm{MHz}$ sometimes affected by ionosphere. Quasi-optical transmission (similar to light, but subject to diffraction by surface of the earth). | Television, FM commercial broadcasting, radar airplane navigation, short-distance communications. |
| Ultra-high frequency (UHF) | $\begin{aligned} & 300-3,000 \mathrm{MHz} \\ & (100-10 \mathrm{~cm}) \end{aligned}$ | Substantially same as above; slightly less diffraction. Under abnormal conditions, can be refracted by troposphere similar to sky-wave refraction. This often results temporarily in abnormally long ranges of transmission. | Television, radar, microwave relay, short-distance communications. |
| Super-high frequency (SHF) | $\begin{aligned} & 3,000-30,000 \\ & \mathrm{MHz}(10-1 \mathrm{~cm}) \end{aligned}$ | Same as above. <br> 1-cm range has broad water-vapor absorption band (slight $\mathrm{O}_{2}$ absorption). | Radar, microwave relay, short distance communications. |

Principal ground-to-ground communication modes, utilizing the microwave ( 70 MHz to 20 GHz ) region of the spectrum. Characteristically wide-band ( 100 kHz to 20 MHz ) service.

|  <br> LIME OF SIGMT (Los) | 0 to 35 miles, depending on (h). | 0.1 to 10 W , two to $10-\mathrm{ft}$ antennas | Low-cost, high-performance wide band system; replaces costly right-of-way maintenance of coaxial or multiple cable or overhead wiring. |
| :---: | :---: | :---: | :---: |
|  | up to $1 / 2$ circum ference of earth depending on satellite orbit and ( $\Theta$ ) | 1 to 15 kW , 30 to $85-\mathrm{ft}$ antennas | Only practical system of global coverage using three active synchronous satellites ( 22,000 miles from earth) or a number of orbiting satellites (dependent on distance covered and altitude) in conjunction with multiple earth earth stations. |
| DIFFRACTIOM <br> (Plane Surface) | 30 to 70 miles, depending on (h) and $\mathrm{N}_{8}$ ) | 0.1 to 100 w , six to $28-\mathrm{ft}$ antennas | Diffraction mode is very specialized form of UHF used only rarely where rugged terrain prevents use of direct LOS and permits longer path with obstacle gain. |
| DIFFRACTIOM <br> (Knife Edge) | 30 to 120 miles, depending on $(\mathrm{h}),\left(\mathrm{N}_{\mathrm{B}}\right)$ and $\left(\mathrm{G}_{\mathrm{O}}\right)$ | 0.1 to 100 w , six to 28-ft antennas |  |
| DIFFRACTIOH ( housh Surface) | 30 to 120 miles, depending on (h), ( $\mathrm{N}_{\mathrm{g}}$ ), $\left(\mathrm{G}_{\mathrm{o}}\right)$, and ( $\mathrm{A}_{0}$ ) | 0.1 to 100 W , six to $28-\mathrm{ft}$ antennas | Great attention is being given to refining propagational computation in the diffraction region because of need for utilization in tropo path predictions. |
|  | 70 to 600 miles, depending on many factors | 1 to 100 kW , 10 to $120-\mathrm{ft}$ antennas, refined modulation and receiver techniques | Only practical wide-band, reliable ground-based method of achieving 70 to 600 mile hop where unsuitable intervening territory prevents use of LOS or diffraction modes. |
| (h) = helght of anteras center <br> $\left(\mathrm{N}_{3}\right)=$ relractive index <br> (Go)-conatele rain |  | ( $\mathrm{M}_{0}$ ) =obstacle absorption <br> (d) = diatasce between atstlons <br> ( $\Theta$ ) = nestter angle or angle of elevation |  |

## INTERNATIONAL TELEVISION STANDARDS

This table outlines pertinent characteristics of the current TV standards used throughout the world. The video frequency-channel arrangements are also shown. The systems have been designated by letter and are in use or proposed for use in the countries listed.

| Country | Standard Used ${ }^{\text {c }}$ | Country | Standard Used ${ }^{\text {c }}$ |
| :---: | :---: | :---: | :---: |
| Argentina | N | Mexico | M |
| Australa | B | Monaco | E, G |
| Austria | B, G | Morocco |  |
| Belgium | C, H | Natherlands | B, G |
| Brazil | M $\mathrm{D}, \mathrm{K}$ | Netharlands Antilles | M |
| Canada | D. M | New Zealand | B |
| Canada | M | Nigeria | B |
| China | M | Noway Pakistan | B |
| Columbia | M | Panama | M |
| Cuba | M | Panu | M |
| Czechosioveliae | D | Phillipines | M |
| Denmark | B | Poland | 0 |
| Egypt | B ${ }_{\text {B }}$ | Portugal | B, G |
| France | E, G | Phodesia | 8 |
| Garmany (East) | E, | Romania | K B |
| Germany (Wast) | B, G | Saudi Arebia | B |
| Greace | B | South Africa | 1 |
| Hong Kong | B. I | Spain | B, G |
| Hungary | D, K | Sweden | B, G |
| India | B | Switzarland | B, G |
| Iran | B | Turkey | 8 |
| Iraland | A | United Kingdom | A, 1 |
| Israel | B | United States of America | M |
| Italy | B, G | Union of Soviet Socialist |  |
| Japan | M | Republics | 0 |
| Korea | C, L | Unuguez, | N |
| Luxembourg | F | Yugosiavia | B, G |
| ${ }^{\text {c }}$ Letter designations corraspond to those in the following table. |  |  |  |


|  | A | M | $N$ | $B$ | c | $G$ | H | $I$ | D, K | $L$ | $F$ | E |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lines/frame | 405 | 525 | 625 | 625 | 625 | 625 | 625 | 625 | 625 | 625 | 819 | 819 |
| Fields/sec | 50 | 60 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| Interlace | 2/1 | 2/1 | $2 / 1$ | 2/1 | 2/1 | 2/1 | 2/1 | $2 / 1$ | 2/1 | 2/1 | $2 / 1$ | $2 / 1$ |
| Frames/sec | 25 | 30 | - | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 | 25 |
| Lines/sec | 10125 | 15750 | - | 15625 | 15625 | 15625 | 15625 | 15625 | 15625 | 15625 | ${ }^{20} 475$ | 20475 |
| Aspect ratio ${ }^{1}$ | 4/3 | 4/3 | - | 4/3 | $4 / 3$ | 4/3 | $4 / 3$ | 4/3 | 4/3 | 4/3 | 4/3 | 4/3 |
| Video band (MHz) | 3 | 4.2 | 4.2 | 5 | 5 | 5 | 5 | 5.5 | 6 | 6 | 5 | 10 |
| RF band ( MHz ) | 5 | 6 | 6 | 7 | 7 | 8 | 8 | 8 | 8 | 8 | 7 | 14 |
| Visual polarity ${ }^{2}$ | $+$ | - | - | - | + | - | - | - | - | + | + | + |
| Sound modulation | A3 | F3 | - | F3 | A3 | F3 | F3 | F3 | F3 | F3 | A3 | A3 |
| Pre-emphasis in microseconds | - | 75 | - | 50 | 50 | 50 | 50 | 50 | 50 | - | 50 | - |
| Deviation (kHz) | - | 25 | - | 50 | - | 50 | 50 | 50 | 50 | - | - | - |
| Gamma of picture signal | 0.45 | 0.45 | - | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 |
| Notes: <br> ${ }^{1}$ In all systems the scanning sequence is from left to right and top to bottom. <br> ${ }^{2}$ All visual carriers are amplitude modulated. Positive polarity indicates that an increase in light intensity causes an increase in radiated power. Negative polarity (as used in the US-Standard $M$ ) means that a decrease in light intensity causes an increase in radiated power. |  |  |  |  |  |  |  |  |  |  |  |  |



This nomogram relates receiver-transmitter distance, wavelength and free space attenuation. It can also be used to convert between nautical and statute miles and between frequency and wavelength.

FOR EXAMPLE: A signal from a $200-\mathrm{MHz}$ transmitter will be attenuated 125 dB before it reaches a receiver located 100 nautical miles away.

At a distance of 200 nautical miles, and a system gain of 130 dB , the highest usable frequency is 180 MHz .
The maximum distance between a transmitter-receiver-antenna system with a total gain of 125 dB operating at 500 MHz is 45 statute miles.


## SIGNAL-STRENGTH NOMOGRAM

This nomogram is used to compute signal-strength input at the receiver based on a formula that converts field intensity at the receiving antenna to receiver input voltage.

If field intensity $\epsilon$, in microvolts per meter, of a given signal $f$, in MHz , is known, the signal strength $\mathrm{E}_{\boldsymbol{r}}$, in microvolts, is determined for an input impedance of 50 ohms ( E , in $\mu \mathrm{V}$ for $R=50$ ) and may be adjusted for any value of input impedance between 30 and 5000 ohms ( $E_{r}$ in $\mu \mathrm{V}$ for $30 \leqslant R \leqslant 5,000$ ). An isotropic antenna, no-loss transmission line is assumed.

Signal strength for receiving antennas of gain >1 (0 dB) are solved first by finding from the chart the voltage input for a system with an isotropic antenna and then adjusting the answer using the relation: $G=20 \log \left(\mathrm{E}^{\prime}, / \mathrm{E}\right.$ ) where $G$ is the gain of the antenna referred to isotropic; $\mathrm{E}^{\prime}$, is the voltage input to be found; and E , is the voltage input.
(Reprinted from Electronics, June 6, 1958, copyright McGraw-Hill, Inc., 1958)

## NOMOGRAM RELATING TRANSMITTER OUTPUT, TRANSMISSION LOSS, AND RECEIVER INPUT

This nomogram shows the available input voltage (microvolts into 50 ohms), if transmitter output in watts and transmission loss in decibels are known. It can also show the maximum permissible transmission loss if transmitter power and receiver requirements are given, or it can be used to determine the required transmitter output for a given transmission loss and receiver input voltage. Microvolts (into 50 ohms ) may be directly converted to dBm on the left scale and watts may be converted to dBm on the center scale.

FOR EXAMPLE: (1) For a transmitter output of 5 W and a transmission loss of 90 dB , the receiver input will be $500 \mu \mathrm{~V}$. (2) For a minimum of $50 \mu \mathrm{~V}$ at the receiver, and a transmitter output of 5 W , the transmission loss may not exceed 110 dB .


## RECEIVER BANDWIDTH-SENSITIVITY-NOISE FIGURE NOMOGRAM

This nomogram is based on the noise figure of a receiver as given by the equation:

$$
N F=\frac{\left(m \mathrm{E}_{0} \sqrt{\left.P_{n} / P_{S}\right)^{2}}\right.}{2 R(4 K T \Delta f)}
$$

where $N F=$ noise figure; $m=$ modulation index; $P_{n}=$ noise power, $P_{s}=$ signal power; $K=$ Boltzmann's constant or $1.38 \times 10^{-23}$ joules $/^{\circ} \mathrm{K} ; R=$ antenna resistance; $T=$ degrees Kelvin; $\Delta f=6-\mathrm{dB}$ audio bandwidth, and $\mathrm{E}_{0}=$ signal generator output in $\mu \mathrm{V}$.

Nominal antenna impedance is 52 ohms and the temperature can be approximated at $300^{\circ} \mathrm{K}$.
To find the noise figure of a receiver, it is only necessary to place a straightedge across the sensitivity and audio bandwidth points, extending it to intersect the noise figure line.

FOR EXAMPLE: Sensitivity of $10 \mu \mathrm{~V}$ and bandwidth of 6 kHz gives a noise figure of 100 , or 20 dB .


## LINE-OF-SIGHT TRANSMISSION RANGE NOMOGRAM SHOWING THE APPROXIMATE TRANSMISSION RANGE OF SIGNALS IN THE VHF BAND

The theoretical maximum distance that can be covered is equal to the geometrical or "optical" horizon distance of each antenna, and is defined by the formula $D=1.23 \sqrt{H_{t}}+1.23 \sqrt{H_{t}}$, where $D$ is in miles and $H_{r}$ and $H_{t}$ are the height in feet, above effective ground level, of the receiving and transmitting antennas. Atmospheric diffraction increases the distance by a factor of $2 N \sqrt{3}$ which defines the "radio" path under normal or standard diffraction, by the formula $\mathrm{D}=1.41 \sqrt{H_{r}}+1.41 \sqrt{H_{r}}$

FOR EXAMPLE: With a receiving antenna height of 30 ft and a transmitting antenna height of 100 ft , the "optical" horizon is 19 miles and the "radio" horizon is 21.5 miles.

(Reprinted with permission from International Telephone and Telegraph Corporation.)

## RADAR POWER-ENERGY NOMOGRAM

The energy available from a radar transmitter is often the limiting factor in determining the maximum free space range. This nomogram relates the four interdependent radar equations involving peak power, average power, energy, duty cycle, pulse width, pulse repetition rate and pulse interval based on the following equations:

$$
\frac{P_{A V}}{P_{P}}=d=\tau f_{r} \text { and } P_{P} \tau=E=P_{A V} t
$$

where $P_{P}=$ peak power in watts
$P_{A V}=$ average power
$E=$ energy in joules
$d$ = duty cycle
$\tau=$ pulse width in microseconds
$f_{\text {f }}=$ pulse repetition rate in pulses $/ \mathrm{sec}$
$t$ = pulse interval in microseconds
FOR EXAMPLE: A pulse repetition rate of 1,000 pulses $/ \mathrm{sec}$ with a pulse width of $5 \mu \mathrm{sec}$ will give a duty cycle of 0.005 . For a peak power of 100 kW , join this value on the $P_{p}$ scale with 0.005 on the duty-cycle scale and read an average power of 500 W . Joining the 100 kW point with the pulse width of $5 \mu \mathrm{sec}$ shows the energy as 0.5 J . (To crosscheck, connect the average power of 500 W with $1,000 \mathrm{pps}$ rep rate, which also yields 0.5 J .)

 vided by position of signal in broad azimuthal trace.


Single signal only. Signal appears as "wingspot," position giving azimuth and elevation errors. Length of wings inversely proportional to range.


Signal appears as two dots. Left dot gives range and azimuth of target. Relative position of right dot gives rough indication of elevation.


Antenna scan is conical. Signal is a circle, the radius proportional to range. Brightest part indicates direction from axis of cone to target.


Same as type A, except time base is circular, and signals appear as radial pips.


Type A with lobe-switching antenna. Spread voltage splits signals from two lobes. When pips are of equal size, antenna is on target.


RANGE
Same as type K , but signals from two lobes are placed back to back.


Type A with range step or range notch. When pip is aligned with step or notch, range can be read from a dial or counter.


A combination of type $K$ and type M.


Range is measured radially from the center.

## ANTENNA REFERENCE CHART

Antennas may be classified as linear radiators or elements, apertures arrays, and traveling wave types. Basic information on a few types of antennas is tabulated. For each type the following is given: the antenna name, physical size in wavelengths, a line drawing superimposed on coordinate axis, the impedance $R$ in ohms at the resonant frequency $f_{r}$, the half-power ( 3 dB ) bandwidth in percent, the gain in dB above an isotropic radiator, as well as the conventional half-wavelength dipole, the polarization for the given configuration, and a set of Fraunhofer Zone field strength patterns for each of the three orthogonal planes of the axis system shown.

An isotropic radiator is given, even though such an antenna for electromagnetic waves does not exist. It is a convenient and frequent reference, however, for gain and pattern measurements.

The antennas tabulated may be vertically or horizontally polarized radiators. The configuration shown in the chart is the one most frequently used in practice. The antennas listed may be fed by balanced transmission lines, by coaxial lines and a balun (balanced-to-unbalanced transformer) when necessary, or in some cases by waveguides. Aperture antennas, such as parabolic dishes and horns, are usually fed by waveguides and, for such feed systems, impedance is not too meaningful.


## Brosdside Array

$L=\lambda / 2$
polerization: vertica
Theoretical Gain of Broadeide $1 / 2 \lambda$ sloments ot different spocinge $1 / 9^{+1}$.

| Spacing in <br> wevelengths "0" | Gain, dB <br> sbove Dipole |
| :---: | :---: |
| $5 / 4$ | 4.8 |
| $3 / 4$ | 4.6 |
| $1 / 2$ | 4.0 |
| $1 / 3$ | 2.4 |
| $1 / 3$ | 1.0 |

Theoretical Gsin of Brosdside $1 / 2 \lambda$ slements for different numbers of elemente.

| Number of <br> elements | Gain, dB <br> ebove Dipole |
| :---: | :---: |
| 2 | 4.0 |
| 3 | 5.5 |
| 4 | 7.0 |
| 5 | 8.0 |
| 8 | 9.0 |

End Firs Array

$$
L=\lambda / 2
$$

polerization: vertieal
Theoreticel Gain of Two End Fire $1 / 2 \lambda$ Eiemente for Verious Specings "o"


| $5 / 4$ | 1.7 |
| :--- | :--- |
| $1 / 2$ | 2.2 |
| $3 / 9$ | 3.0 |
| $1 / 4.20$ | 3.8 |
| $1 / 8$ | 4.1 |
|  | 4.3 |

Parasitic Arrey
$L=\lambda / 2$
polorization: horizontal

| Number of <br> Elemente | Gein, dB <br> sbove Dipole | Front to Beck <br> Rotio, dB |
| :---: | :---: | :---: |
| 2 | 4 to 5. | 10 to 15 |
| 3 | 8 to 7 | 15 to 25 |
| 4 | 7 to 9 | 20 to 30 |
| 5 | 9 | - |



Collineer Arrey

$$
L=\lambda / 2
$$



Number of $1 / 2 \lambda$ elements in arrey versue
Spacing "0" between centers of adjacent
$1 / 2 \times$ olemente
gein in dB ebove reference bipole

| $0=1 / 2 \lambda$ | 1.8 | 3.3 | 4.5 | 5.3 | 8.2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $9=3 / 4 \lambda$ | 3.2 | 4.8 | 8.0 | 7.0 | 7.8 |



|  | 票 |  | GAIN 8 above |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \frac{\pi}{6} \\ & \frac{\text { In }}{2} \end{aligned}$ | 葚 |  |  |  | Dipole aver small ground plane $L=\lambda / 4$ |
|  | E | V | 0 | 2.14 | 40 | 28 |  | $L / D=53$ $l=2 \lambda$ |
|  | E | V | 0 | 2.14 | 45 | 150 |  | $\begin{aligned} & \text { Folded Unipole } \\ & \text { over small } \\ & \text { ground plame } \\ & L=\lambda / 4 \\ & L / D=83 \\ & L=2 \lambda, \\ & L / d=13 \\ & \hline \end{aligned}$ |
|  | E | V | 0 | 2.14 | 16 | 50 |  | $\begin{aligned} & \text { Coosilal Dipole } \\ & L=\lambda / 4 \\ & L / D=10 \end{aligned}$ |
|  | E | v | 0 | 2.14 | 200 | 72 |  | $\begin{aligned} & \text { Bleconical } \\ & \text { Couxlal Dipole } \\ & L=\lambda / 2 \\ & d=\lambda / 8 \\ & D=3 \lambda / 8 \end{aligned}$ |
|  | E | V | 0 | 2.14 | 300 | 50 |  | Disc-Cone or Mod Disc-Cone $L=\lambda / 4$ $1=\lambda$ |
|  | E | V | 12 | 14.14 | 25 | 20 |  | $\begin{aligned} & \text { Bicenical Hiem } \\ & L=99 / 2 \\ & D=14 \mathrm{x} \end{aligned}$ |
|  | F | H | 0 | 2.14 | 70 | 350 |  | Slot In Large Ground Plane $\begin{aligned} & L=x / 2 \\ & 1 / d=29 \end{aligned}$ |
|  | B | H | 1 | 3.14 | 13 | 45 |  | Verfical Full Wave Loop $D=\frac{\lambda}{r}$ $D / d=36$ |
|  | G | Circ. | 8 | 10.14 | 200 | 130 |  | Hellical <br> over reflector screen, tube $6 \times$ long coiled Into 6 tums 2/4 apart |
|  | H | H | 14.5 | 16.74 | 100 | 600 |  | Rhombic $\begin{aligned} & L \\ & 1 \end{aligned}=9 \lambda / 2$ |
|  | H | H | 12.5 | 14.74 | 30 | 300 |  | Parabolic with folded clipole feed ( $1 / 2$ ) |
|  | H | H | 13 | 15.14 | 35 | 50 |  | Horn. coaxial feed $l=3 \lambda$ $L=3 \lambda$ |

## MICROWAVE ANTENNA CHART

Shown here is the relationship between circular antenna aperture size, frequency, and gain. Also listed are the antenna performance requirements for various system applications. Practical factors, such as whether the antenna is solid or perforated, the type of aperture illumination, accuracy of construction, and shadowing from the feed system will tend to reduce the gain somewhat.

FOR EXAMPLE: To achieve a gain of 40 dB at 10 GHz requires an antenna with a diameter of 10 m . An antenna with a diameter of 100 m has a gain of 100 dB at 100 GHz .

Antenna Performance Requirements

| APPLICATION | Pattern | POLARIZATION | GAIN <br> g. (dB) above leotrople rad. | BEAMWIOTH <br> (H) degrese | POINTING ACCURACY, to degreet | TYPICAL TYPES |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1. SATELLITE Link or Probe | Penell Beam | tny | 10 to 40 dB or maore | 60 to 2 or lase | 8 to 2 or better | Horn, Phased array, Parabela, Cassegreln |
| 2. POINT TO POINT RELAY <br> 1. On Earth <br> b. Earth to Setallite to Earth <br> c. Satellite to Satallite | Pencll Beam | any | e. 50 to 120 <br> b. 50 to 120 <br> c. 50 to 180 | $\begin{aligned} & 5.8 \times 10^{-1} \text { to } \\ & 1.8 \times 10^{-4} \\ & 5.8 \times 10^{-1} \text { to } \\ & 1.8 \times 10^{-1} \end{aligned}$ | $\begin{aligned} & 5.8 \times 10^{-2} 10 \\ & 1.8 \times 10^{-7} \end{aligned}$ | Horn, Perebole. Cessegrain |
| 3. BROAOCAST <br> a. Earth Trana. <br> b. Set. Trans. | omnidir. wide or fon beam | any | 6. 3 to 40 <br> b. 1 to 10 | $\begin{aligned} & 100 \text { to } 1.8 \\ & 180 \text { to } 80 \end{aligned}$ | 10 to. 13 | a. Vertleal rediator <br> b. Cylindricel perebole |
| 4. NAVIGATION | omnidir, or fon beam | eny | 3 to 30 | 100 to, 50 | 10 to .058 | Verlicel redletor, Hern, or Perabole |
| 5. RADAR <br> a. Seerch <br> b. Tratk | csez <br> Panell Beam | try | 40 to 120 | . 8 to $1.8 \times 10^{-4}$ | . 18 to $1.8 \times 10^{-3}$ | Horn, Parebola, Csssegrain, Phesed orrey |
| 8. RADIO ASTRONOMY <br> 0. Pasaive <br> b. Active | Pencli Beam | ony | 50 to 160 or grobler | . 58 to $1.8 \times 10^{-3}$ | . 057 to $1.8 \times 10^{-7}$ | Persbola, Cessegreln, Phased array |
| 7. RAOFOMETRY Industrial | eny | ary | unknown | unknown | unknown | Any |

Antenna Gain and Size vs Frequency for Uniformly Illuminated Circular Aperture


Antennas are judged on the basis of radiation efficiency or their VSWR. Radiation efficiency is the ratio of the radiated power to the total power fed into the antenna terminals. Total power is the sum of the radiated power and the power lost in ohmic losses in the form of heat. The power going into the antenna terminals is the power which a transmitter can put out less the power reflected due to antenna mismatch. Antenna effectiveness is the ratio of the radiated power to the power which a transmitter can put into a matched load, i.e., the forward or incident power.

$$
\text { Effectiveness }=\frac{4 \text { VSWR }}{(\text { VSWR }+1)^{2}} \times \text { efficiency }
$$

FOR EXAMPLE: A $60 \%$ efficient antenna with a 2.5:1 VSWR has an effectiveness of $48 \%$ compared to a perfectly matched $100 \%$ efficient antenna.

NOTE: In some cases an antenna can be made more effective by lessening its efficiency if this will produce a sufficient reduction in the VSWR.


Characteristics of Various Types of Transmission Lines Erected Parallel to a Perfectly Conducting Earth.

| logarithms to the base io |  |  | I, - oenerator Current |
| :---: | :---: | :---: | :---: |
| LINE CONFIGURATION |  | CHARACTERISTIC IMPEDANCE | MET OROUND-RETURN CURRETIT |
| Single wire |  | $z_{0}=138 \log \frac{2 h}{r}$ | Land $=I_{1}$ |
| 2-Wire balanced |  | $z_{0}=276 \log \frac{3}{r}$ | $\mathrm{I}_{\text {Ond }}=0$ |
| 2-Wire grounded |  | $\begin{aligned} & z_{0} \sim 276 \frac{\log \frac{3}{r} \log \left(\rho^{2} p\right]}{\log \left[\rho^{2}\left(\frac{s}{r}\right)^{2}\right]} \\ & \rho=\frac{2 h}{s} \end{aligned}$ | $I_{\text {Gnd }}=I_{1} \frac{\log \frac{3}{r}}{\log \frac{2 h}{r}}$ |
| 3-Wire 2 wires grounded |  | $Z_{0} 069\left[\log \frac{3^{3}}{2 r^{3}} \cdot \frac{\left(\log \frac{3}{2}\right)^{2}}{\log \frac{2 h^{2}}{72}}\right]$ | $\begin{aligned} & I_{G n d}=I_{1} \frac{\log \frac{s}{2 r}}{\operatorname{Lr}} \frac{\operatorname{sp}}{2 r} \\ & \rho=\frac{2 h}{3} \end{aligned}$ |
| 4-Wire balanced |  | $z_{0}=138\left(\log \frac{3}{r}\right)-21$ | ${ }^{1}$ Gnd $=0$ |
| 4-Wire 2 wires grounded |  | $\begin{aligned} & z_{0}=138\left[\frac{\log \frac{5}{\sqrt{2}} \log \left[\rho^{4} \frac{3}{n^{2}}\right.}{\log \left[\rho^{4}\left(\frac{5}{\sqrt{3}}\right)^{2}\right]}\right] \\ & \rho=\frac{2 h}{5} \end{aligned}$ | $1_{\text {ond }}=I_{1} \frac{\log \frac{s}{\sqrt{2}}}{\log \frac{\rho^{2} s}{\sqrt{2}}}$ |
| 5- Wire 4 wires grounded |  | $\begin{aligned} & z_{0}-138\left[\log \frac{2 h}{r} \frac{\left[\log 2 p^{2}\right]^{2}}{\log \left[\rho^{3} \frac{3 V_{2}}{r}\right.}\right] \\ & e^{\frac{2 h}{s}} \end{aligned}$ | $I_{\text {and }}=1, \frac{\log \frac{s}{r \Delta \sqrt{2}}}{\log \frac{s \rho^{4}}{r \sqrt{2}}}$ |
| Concentric (cooxial) |  | $\begin{aligned} & z_{0}=138 \frac{\log \frac{c}{b}}{\sqrt{1+\left(\frac{(b-1)}{s} \omega\right.}} \\ & \varepsilon=\text { Dielectric constant } \\ & \text { of insulating material } \end{aligned}$ |  |
| Double conxial bslanced |  | $\tau_{0}=276 \frac{\log \frac{c}{b}}{\sqrt{1+\frac{(\varepsilon-1) \omega}{5}}}$ |  |
| Shialded poir balanced |  | $\begin{aligned} & z_{0} \frac{120}{\sqrt{\varepsilon}}\left[2.303 \log \left(2 v \frac{1-\sigma^{2}}{1 \sigma^{2}}\right)-\right. \\ & \varepsilon=\text { Dieletric constant of } \\ & \varepsilon=\text { Unity for gaseous mec } \\ & v=\frac{h}{b} ; \sigma=t \end{aligned}$ | $\left.\frac{1+4 v^{2}}{6 v^{4}}\left(1-4 \sigma^{2}\right)\right]$ <br> medium ium |

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## CHARACTERISTIC IMPEDANCE OF BALANCED TWO-WIRE LINES

This nomogram determines the theoretical exact impedance of air-dielectric parallel lines in air or in a vacuum, and remote from any conducting plane. It covers conductors having diameters from 0.01 to 5 in ., spaced from 0.01 to 100 in . center-to-center.

$$
\begin{gathered}
z_{0}=276 \log _{10} \frac{2 D}{d} \\
D>2 d
\end{gathered}
$$

FOR EXAMPLE: (1) The impedance of a line using \#12 wire spaced $11 / 2$ in. is 430 ohms. (2) What is the wire diameter for a 300 -ohm line spaced $11 / 4 \mathrm{in}$.? Answer: 0.20 in .

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SC-silver plated copper, C-bore sopper. PE-polyethylene. NCV-non-contaminoting vinyl.
V-polyvinyichlaride, TC-tinned copper, CW-copperweld

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## ULTRA-HIGH FREQUENCY HALF-WAVE SHORTING-STUB NOMOGRAM

This nomogram is used to determine the length in inches of shorting stubs required to eliminate interference in the UHF television range.

FOR EXAMPLE: To eliminate an interfering signal at 575 MHz (channel 31) requires a $81 / 2 \mathrm{in}$. long half-wave shorting stub, if 300 -ohm twin lead is used. If 75 -ohm twin lead is used, the stub has to be $71 / 4 \mathrm{in}$. for the same frequency.


TRANSMISSION UNE NOMOGRAM
This nomogram gives the actual length of line in centimeters and inches when given the length in electrical degrees and the frequency provided that the velocity of propagation on the transmission line is equal to that in free space. The length is equal to that in free space and is given on the $L$ scale intersection by a line between $\lambda$ on $\ell^{\circ}$.

## FOR EXAMPLE:

$$
\begin{aligned}
& f=600 \mathrm{MHz} \quad \ell^{\circ}=30^{\circ} \\
& \text { Length } L=1.64^{\prime \prime} \text { or } 4.2 \mathrm{~cm}
\end{aligned}
$$

(

This nomogram is used to determine the VSWR and the magnitude of the reflection coefficient by the use of width-of-minimum measurement technique. This technique relies on the fact that there are two comparatively easy-to-find $3-\mathrm{dB}$ points straddling any minimum, as illustrated.

FOR EXAMPLE: A slotted-line width-of-minimum measurement of 0.18 cm , with a $1-\mathrm{GHz}$ source, indicates a VSWR of 53 or a reflection coefficient magnitude of 0.963 .

NOTE: The signal-to-noise ratio at the bottom of the minimum must be at least 10 dB for accurate results.


## SLOTTED LINE WIDTH-OF-MINIMUM ATTENUATION CALCULATION NOMOGRAM

This nomogram is used to determine the total attenuation between the probe position and the reference plane based on width-of-minimum measurements.

FOR EXAMPLE: With a short circuit termination at the reference plane, if the width-of-the-minimum measured 30 cm from the reference plane is 0.014 cm at 3.5 GHz , then the attenuation is 0.045 dB .

NOTE: The signal-to-noise ratio at the bottom of the minimum should be at least 10 dB for accurate results.


## WAVEGUIDE NOMOGRAM

This nomogram relates three significant waveguide characteristics:
waveguide wavelength ( $\lambda_{q}$ )
free space wavelength ( $\lambda_{0}$ ) or frequency ( $f$ )
cutoff wavelength $\left(\lambda_{c}\right)$
The vertical scale gives waveguide wavelength in centimeters. The horizontal scale is for the cutoff wavelength, and the points corresponding to the cutoff wavelength in the $\mathrm{TE}_{10}$ mode of three common waveguides are indicated. The sloping center scale is calibrated in free space wavelength and frequency.

FOR EXAMPLE: (1) The waveguide wavelength at 6 GHz ( 5 cm free space wavelength) in an RG-50 waveguide is 7.17 cm . (2) Measurement on an RG-51 waveguide whows the waveguide wavelength to be 6.5 cm . The frequency is 7 GHz , which corresponds to a free space wavelength of 4.27 cm .


If a transmission line is not terminated in its characteristic impedance, then some of the energy sent along the line will be reflected back, and standing waves form on the line. The ratio of the maximum to the minimum voltage of the standing waves is the VSWR (voltage standing wave ratio) and indicates the effectiveness of the match between line and load. For a perfectly matched line, the VSWR is 1 . The VSWR can be given in a number of ways:

$$
\text { VSWR }=\frac{Z_{L}}{Z_{0}}=\frac{E_{\max }}{E_{\min }}=\frac{1+\sqrt{\frac{\text { Reflected power }}{\text { Forward power }}}}{1-\sqrt{\frac{\text { Reflected power }}{\text { Forward power }}}}
$$

This nomogram is based on the last expression and solves for VSWR from measurements of reflected power and forward power.

FOR EXAMPLE: For a forward power of 180 W and a reflected power of 2.7 W , the VSWR is 1.27 .


## VSWR REDUCTION AS A RESULT OF ATTENUATION

This nomogram relates load VSWR, input VSWR, and attenuation. It can be used to find the resultant VSWR with a given amount of attenuation, or to determine the attenuation required for a given VSWR.

FOR EXAMPLE: (1) A $5-\mathrm{dB}$ attenuator will reduce input VSWR to 1.23 if the load VSWR is 2.0. (2) The required attenuation to reduce a load VSWR of 1.8 to an input VSWR of 1.06 is 10.0 dB .


## DOPPLER TO SPEED CONVERSION NOMOGRAM

Radar or sonar frequency may be converted to hundreds of miles per hour or knots per hour by using this chart. The base sonar frequency in kHz is given on the left scale and the base radar frequency in GHz is given on the right. Doppler frequency, in Hz for sonar and hundreds of Hz for radar, is shown at the bottom. The diagonals represent target rate of change of range, which is the velocity speed vector in the source's direction.

The basic formula for Doppler speed is:

$$
\text { Doppler frequency }=\frac{\text { base } f . \times \text { target range rate }}{\text { signal velocity in medium. }}
$$

The signal velocity in medium is $5,000 \mathrm{ft} / \mathrm{sec}$ for sonar and $186,000 \mathrm{mi} / \mathrm{sec}$ for radar.
FOR EXAMPLE: (1) The base frequency of a sonar system is 40 kHz and its Doppler frequency is 55 Hz . The speed vector is found by the intersection of these two lines on the chart to be approximately 4.1 knots. (2) The base frequency of a radar system is 11 GHz , and the Doppler frequency is $8,000 \mathrm{~Hz}$. The speed vector of the aircraft in miles per hour is found (from the intersection of these two lines) to be approximately 480 mph .


## DOPPLER FREQUENCY NOMOGRAM

This nomogram solves for the Doppler frequency, which is produced as a result of relative motion between a transmitter and its receiver or target. The Doppler frequency is a function of transmitted frequency and velocity of motion. The angle to the velocity vector determines the actual relative velocity. For a navigation system (Fig. A) in an airplane, the earth is the target, and the angle $A$ is the acute angle between the aircraft heading and the radar beam. In this case the Doppler shift is downward. A forward-looking radar will produce an upward Doppler shift. For surveillance-type radars (Fig. B), the angle A is the acute angle between the radar beam and target velocity. (Note that the nomogram is based on the Doppler equation for radar and that the Doppler shift for a passive listening device will be half the frequency indicated.)

FOR EXAMPLE: A helicopter navigation system transmits at 10 GHz at an angle of $70^{\circ}$. What is the audio bandwidth required for aircraft velocities of 10 through 200 mph ? On the left scales, connect 10 GHz and 10 mph to the turning scale. From that point on, the turning scale connecting through $70^{\circ}$ gives 100 Hz as the lowest frequency. Repeating the steps using 200 mph in place of 10 mph shows the highest frequency to be 2 kHz . Thus the required bandwidth is 100 to $2,000 \mathrm{~Hz}$. The nomogram is based on the formula

$$
f_{d}=89.4 \frac{V}{\lambda}
$$

where
$f_{d}=$ Doppler frequency $(\mathrm{Hz})$
$V=$ velocity in miles per hour
$\lambda=$ transmitted wavelength in centimeters
Angle-to-velocity vector depends on type of target.



This graph determines the combined signal level and shows the number of dB that must be added to the larger signal.

FOR EXAMPLE: Two in-phase signals are -25 dB and -27 dB respectively. The difference is 2 dB and, from the graph, 2.2 dB must be added to the larger signal. Thus, the combined signal power level is -25 dB plus 2.2 dB or -22.8 dB .

$\left(\frac{A}{B}\right)$

## GRAPH FOR SEPARATING SIGNAL POWER FROM NOISE POWER

When making transmission loss or crosstalk measurements, the presence of noise is a potential source of error. If the total voltage measured across the load resistance when a signal is being transmitted is 15 dB or more greater than the noise voltage alone, the error in the received voltage measurement will be negligible. If, however, the dB difference between the combined signal and noise voltage and the noise voltage alone is less than 15 dB , a correction must be made. To do so, two voltage measurements must be made. Namely, (1) the noise power in dBm , and (2) the combined noise and signal power in dBm . On the horizontal axis locate the point equal to the difference between the two powers and read on the vertical axis the number of dB to be subtracted from the noise plus signal power and obtain the power of the signal alone.

FOR EXAMPLE: The difference between the measurements of combined noise and crosstalk and noise alone is 5 dB . Thus, 1.7 dB must be subtracted from the combined signal and noise level to obtain the level of the signal alone.


FIELD POWER CONVERSION CHART
Power density is related to field strength by the equation

$$
P=\frac{E_{2}}{10 \pi}
$$

where

$$
\begin{aligned}
P & =\text { the power density } \\
E & =\text { the field strength } \\
120 \pi & =\text { the resistance of free space }
\end{aligned}
$$

and
This chart converts between field strength and power density.

FOR EXAMPLE: A field strength of $3,000 \mu \mathrm{~V} / \mathrm{m}$ corresponds to a poler density of $0.024 \mu \mathrm{~W} / \mathrm{m}^{2}$ and is 70.5 dB above $1 \mu \mathrm{~V}-\mathrm{m}$.

## Q SIGNALS (MNEMONIC CODE)

The Q code was first adopted in 1912 by international treaty agreement to overcome the language barriers faced by ship operators of all nations as they tried to communicate with shore stations all over the world. Many of the original list of 50 signals are still in use with their definitions unchanged. Many more have been added from time to time, and the official meanings of some signals have been changed. In addition, many signals have been informally adopted for use by amateurs in situations not covered by the official lists.

The list below includes virtually every Q signal which could, even remotely, be thought to have an application in amateur radio communication. To simplify the task of finding the definition of an unfamiliar signal, we have combined all the signals into a single alphabetical list, mixing "official" and unofficial signals. The definitions listed are, in most cases, the official ones, taken verbatim from the treaty. In other cases, where definitions are not the official ones, they are as amateurs universally understand them, for purposes of amateur communications. The QN signals, adopted by ARRL for traffic net use, have official definitions which refer to aeronautical situations.

QAM What is the latest available meterological observation for (place)?
The observation made at (time) was . . . .
QAP Shall I listen for you (or for . . .) on ... kH ? Listen for me (or for . . .) on . . . kHz .
QAR May I stop listening on the watch frequency for . . . minutes?
You may stop listening on the watch frequency for . . . minutes?
QBF Have we worked before in this contest? We have worked before in this contest.
QHM I will tune from the high end of the band toward the middle
(Used after a call or CQ.)
QIF What frequency is . . . using?
He is using . . . kHz .
QJA Is my RTTY (1-tape, $2-\mathrm{M} / \mathrm{S}$ ) reversed?
It is reversed.
QJB Shall I use (1-TTY, 2-reperf)? (For RTTY use.) Use (1-TTY, 2-reperf)
QJC Check your RTTY (1-7'C, 2-auto head, 3-reperf, 5-Printer, 7-keyboard).

QJD Shall I transmit (1-letters, 2-figs)? (For RTTY)
Transmit (1-letters, 2-1igs).
QJE Shall I send (1-wide, 2 -narrow, 3-correct) RTTY shift?
Your RTTY shift is (1-wide, 2-narrow, 3-correct).
QJF Does my RTTY signal check out OK? Your RTTY signal checks out OK.
QJH Shall I transmit (1-test tape, 2-test sentence) by RTTY?

Transmit (1-test tape, 2-test sentence) by RTTY.
QJI Shall I transmit continuous (1-mark, 2-space) RTTY signal?
Transmit continuous (1-mark, 2-space) signal.
QJK Are you receiving continuous (1-mark, 2-space, 3-mark bias, 4-space bias)? I am receiving continuous (1-mark, 2 space, 3 -mark bias, 4 -space bias).
QKF May I be relieved at . . . hours?
You may expect to be relieved at.. hours by. . . .
QLM I will tune for answers from the low end of the band toward the middle.
QMD I will tune for answers from my frequency down.
QMH I will tune for answers from the middle of the band toward the high end.
QML I will tune for answers from the middle of the band toward the low end.
QMU I will tune for answers from my frequency upward.
QMT Will you mail the traffic?
I will accept the traffic for delivery by mail.
QNA Answer in prearranged order.
QNB* Act as re ay between . . . and . . . .
QNC All net stations copy.
I have a inessage for all net stations.
QND* Net is directed (controlled by net control station).
QNE * Entire net stand by.
QNF Net is free (not controlled).
QNG Take over as net control station.
QNH Your net frequency is high.
QNI * Net stations report in."

- For use only by Net Control Station

I am reporting into the net. (Follow with list of traffic or QRU.)
QNJ Can you copy me?
Can you copy . . . ?
QNK* Transmit messages for . . . to . . . .
QNL Your net frequency is low.
QNM* You are QRMing the net. Stand by.
QNN Net control station is . . . .
What station has net control?
QNQ Station is leaving the net.
QNP Unable to copy you. Unable to copy . . . .
QNQ* QSY to . . . . . . . and wait for . . . to finish. Then send him traffic for . . . .
QNR* Answer . . . and receive traffic.
QNS Follow ng stations are in the net. " $\langle$ Follow with list.) Request list of stations in the net.
QNT I request permission to leave the net for . . . minutes.
QNU* The net has traffic for you. Stand by.
QNV Establish contact with . . . on this freq. If successful QSY to . . . and send traffic for . . .
QNW How do I route messages for . . . ?
QNX You are excused from the net." Request to be excused from the net.
QNY* Shift to another frequency (or to . . . kHz) to clear traffic with. . . .
QNZ* Zero beat your signal with mine.
QRA What is the name of your station? The name of my station is. . . .
QRB How far approximately are you from my station?
The approximate distance between our station is . . . nautical miles (or kilometers).
QRD Where are you bound for and where are you from?
I am bound for . . . from. . . .
QRE What is your estimated time of arrival at . . . (or over . . .) (place)?
My estimated time of arrival at . . . (or over . . .) (place) is . . . hours.
QRF Are you returning to . . . (place)? I am returning to . . . (place). or
Return to . . . (place).
QRG Will you tell me my exact frequency (or that of . . .)?
*For use only by Net Control Station

Your exact frequency (or that of . . .) is $\ldots \mathrm{kHz}_{2}$ (or $\mathrm{MHz}_{2}$ ).
QRH Does my frequency vary? Your frequency varies.
QRI How is the tone of my transmission?
The tone of your transmission is (1good, 2-variable, 3-bad.
QRJ Are you receiving me badly? Are my signals weak?
I am receiving you badly. Your signals are too weak.
QRK What is the intelligibility of my signals (or those of . . .)?
The intelligibility of your signals (or those of . . ) is 1-bad, 2-poor, 3-fair, 4-good, 5-excellent.
QRL Are you busy?
I am busy (or I am busy with. . .). Please do not interfere.
QRM Are you being interfered with?
I am being interfered with (1-nil, 2slightly, 3-moderately, 4-severely, 5extremely).
QRN Are you troubled by static?
I am troubled by static (1-nil, $2-$ slightly, 3-moderately, 4-severely, 5extremely).
QRQ Shall I increase transmitter power? Increase transmitter power.
QRP Shall I decrease transmitter power? Decrease transmitter power.
QRQ Shall I send faster?
Send faster (. . . words per minute).
QRR Are you ready for automatic operation? I am ready for automatic operation. Send at . . . words per minute.
QRRR Distress call signal for use by amateur c.w. and RTTY stations. To be used only in situations where there is danger to human life or safety.
QRS Shall I send more slowly? Send more slowly.
QRT Shall I stop sending? Stop sending.
QRU Have you anything for me? I have nothing for you.
QRV Are you ready? I am ready.
QRW Shall I inform... that you are calling him on . . . kHz ?

Please inform ... that I am calling him on . . . kHz.
QRX When will you call me again?
I will call you again at . . . hours (on . . . kHz ).
QRY What is my turn?
(Relates to communication)
Your turn is Number ... (or according to any other indication).
(Relates to communication)
QRZ Who is calling me?
You are being called by . . . (on . . kHz).
OSA What is the strength of my signals (or those of . . .)?
The strength of your signals (or those of ...) is (1-scarcely perceptible, 2-weak, 3 -fairly good, 4 -good, 5 -very good).
QSB Are my signals fading?
Your signals are fading.
QSD Is my keying defective?
Your keying is defective.
QSG Shall I send . . . messages at a time?
Send . . . messages at a time.
QSH Are you able to home on your D/F equipment?
I am able to home on my D/F equipment (on station . . .).
QSI I have been unable to break in on your transmission.
or
Will you inform . . . (call sign) that I have been unable to break in on his transmission (on ... kHz).
OSK Can you hear me between your signals and if so can I break in on your transmission?
I can hear you between my signals; break in on my transmission.
QSL Can you acknowledge receipt? 1 am acknowledging receipt.
OSM Shall I repeat the last telegram which I sent you (or some previous telegram)? Repeat the last telegram which you sent me for telegram(s) number(s) . . .).
QSN Did you hear me [or . . . (call sign)] on kHz ? I did hear you [or ... (call sign)] on ... kHz .
QSO Can you communicate with ... direct (or by relay)?

I can communicate with... direct (or by relay through . . .).
QSP Will you relay to ... free of charge? I will relay to ... free of charge.
QSQ Have you a doctor on board [or is ... (name of person) on board] ?
I have a doctor on board for . . . (name of person) is on board].
QSR Shall I repeat the call on the calling frequency?
Repeat your call on the calling frequency; did not hear you (or have interference).
QSS What working frequency will you use? I will use the working frequency . . kHz .
QST Calling all radio amateurs.
QSU Shall I send or reply on this frequency (or on . . . kHz?
Send or reply on this frequency (or on ... kHz .
QSV Shall I send a series of V's on this frequency (or . . . kHz)?
Send a series of V's on this frequency (or ... $k H z$ ).
QSW Will you send on this frequency (or on ... kHz )?
I am going to send on this frequency (or on .... kHz ).
OSX Will you listen to ... (call sign(s)) on . . $k \mathrm{kz}^{\text {? }}$
I am listening to ... (call sign(s)) on $\ldots \mathrm{kHz}$

QSY Shall 1 change to transmission on another frequency?
Change to transmission on another frequency (or on ... kHz).
QSZ Shall I send each word or group more than once?
Send each word or group twice for... times).
QTA Shall I cancel message number . . . ? Cancel niessage number. . . .
QTB Do you agree with my counting of words?
I do not agree with your counting of words; I will repeat the first letter or digit of each word or group.
OTC How many messages have you to send? I have . . . messages for you (or for . . .).
QTG. Will you send two dashes of ten seconds each followed by your call sign (re-
peated . . . times) (on . . . kHz)? or -Will you request . . . to send two dashes of ten seconds followed by his call sign (repeated . . . times) on . . . kHz ?
1 am going to send two dashes of ten seconds each followed by my call sign (repeated . . . times) (on . . . kHz). or I have requested . . . to send two dashes of ten seconds followed by his call sign (repeated . . . times) on . . . kHz.
QTH What is your position in latitude and longitude (or according to any other indication)?
My position is . . . latitude . . . longitude (or according to any other indication).
QTN At what time did you depart from . . . (place)?
I departed from . . . (place) at . . . hours.
QTO Have you left dock (or port)? or Are you airborne?
I have left dock (or port). or I am airborne.
Are you going to enter dock (or port)? or Are you going to alight (or land)?
I am going to enter dock (or port). or I am going to alight (or land).
QTQ Can you communicate with my station by means of the International Code of Signals?
I am going to communicate with your station by means of the International Code of Signals.
QTR What is the correct time?
The correct time is . . . hours.
QTS Will you send your call sign for tuning purposes or so that your frequency can be measured now (or at . . . hours) on ... $\mathrm{kHz}_{z}$ ?
I will send my call sign for tuning purposes or so that my frequency may be measured now (or at . . . hours) on ... kHz.
QTU What are the hours during which your station is open?
My station is open from . . . to . . . hours.
QTV Shall I stand guard for you on the frequency of . . . kHz (from . . . to . . . . hours)? Stand guard for me on the frequency of . . . kHz (from . . . to hours). Will you keep your station open for further communication with me until further notice (or until . . . hours)?

I will keep my station open for further communication with you until further: notice (or until . . . hours).
QTY Are you proceeding to the position of incident and if so when do you expect to arrive?
I am proceeding to the position of incident and expect to arrive at . . . hours on . . . (date).
QTZ Are you continuing the search?
I am continuing the search for .... (aircraft, ship, survival craft, survivors, or wreckage).
QUA Have you news of . . . (call sign)? Here is news of . . . (call sign).
QUB Can you give me in the following order information concerning: the direction in
degrees TRUE and speed of the surface wind; visibility; present weather; and amount, type, and height of base of cloud above surface elevation at ... (place of observation)?
Here is the information requested:
(The units used for speed and distances should be indicated.)
QUC What is the number (or other indication) of the last message you received from me [or from . . . (call sign)] ?
The number (or other indication) of the last message 1 received from you lor from . . . (call sign)] is . . . .
QUE Can you use telephony in . . . (language), with interpreter if necessary; if so, on what frequencies?
I can use telephony in . . . (language) on ... kHz.

QUF Have you received the distress signal sent by . . . (call sign of station)?
I have received the distress signal sent by . . . (call sign of station) at . . . hours.
QUH Will you give me the present barometric pressure at sea level?
The present barometric pressure at sea level is . . . (units).
QUK Can you tell me the condition of the sea observed at . . . (place or coordinates)? The sea at . . . (place or coordinates) is . . . .
QUM May I resume normal working? Normal working may be resumed.

## RADIO TELEPHONE CODE

General Station Operation
10-1 Receiving poorly.
10-2 Signals good.
10-3 Stop transmitting.
10-4 Okay-Affirmative-Acknowledged.
10-5 Relay this message.
10-6 Busy, stand by.
10-7 Leaving the air.
10-8 Back on the air and standing by.
10-9 Repeat message.
10-10 Transmission completed, standing by.
10-11 Speak slower.
10-13 Advise weather and road conditions.
10-18 Complete assignment as quickly as possible.
10-19 Retum to base.
10-20 What is your location? My location is . . . .
10-21 Call . . . by telephone.
10-22 Report in person to . . . .
10-23 Stand by.
10-24 Have you finished? I have finished.
10-25 Do you have contact with . . . ?
Emergency or Unusual
10-30 Does not conform to Rules and Regulations.
10-33 Emergency traffic this station.
10-35 Confidential information.
10-36 Correct time.
10-41 Tune to channel . . . for test, operation, or emergency service.
10-42 Out of service at home.
10-45 Call . . . by phone.
10-54 Accident.
10-55 Wrecker or tow truck needed.
10-56 Ambulance needed.

## Net Message Handling

10-60 What is next message number?
10-62 Unable to copy, use CW.
10-63 Net clear.
10-64 Net is clear.
10-66 Cancellation.
10-68 Repeat dispatch on message.
10-69 Have you dispatched message . . . ?
10-70 Net message.
10-71 Proceed with transmission in sequence.

## Personal

10-82 Reserve room for
10-84 What is your telephone number?
10-88 Advise present phone number of

## Technical

10-89 Repairman needed.
10-90 Repairman will arrive at your station
10-92 Poor signal, have transmitter checked.
10-93 Frequency check.
10-94 Give a test without voice for frequency check.
10-95 Test with no modulation.
10-99 Unable to receive your signals.

## INTERNATIONAL MORSE CODE

## Alphabetical

| A - - | J.--- | S . . |
| :---: | :---: | :---: |
| B $-\cdots$ | K - - - | T- |
| C-* | L. - $\cdot$ | U $\cdot$ - |
| D - . | M - - | V...- |
| E. | N-* | W $\cdot$ - |
| F...* | O--- | X - $\cdot$ - |
| G - - | P.--* | Y-*- |
| H.... | Q - - - | Z - - |
| I. | R. - |  |

## By Groups

| Group One | Group Two | Group Three |
| :---: | :---: | :---: |
| E. | A - - | R •- |
| 1.. | W •-- | F••- |
| S . . | J•--- | L.-* |
| H. . . | N - . | U..- |
| T - | D - $\cdot$ | V $\cdot \cdots$ - |
| M - - | B $-\cdots$ |  |
| O-- |  |  |
| Group Four |  |  |
| K - - | Q - - - |  |
| X - $\cdot$ | G - - |  |
| C - - | Z - - ${ }^{\text {c }}$ |  |
| Y-*- | P - - - |  |

## Numerals and Punctuation

```
\(2 \cdots-\) - 7 - \(\cdot \cdots\)
\(3 \cdots-\) - 8 - -
\(4 \cdots \cdots-\quad 9-\) - \(\quad\).
\(5 \cdots \quad 0-\cdots \quad\) -
Period •—•- -
Comma - - . - -
Question mark . . - - .
Error
Double dash - ... -
Fraction bar -.. - .
Wait •- . . .
Invitation to transmit - -
End of message (AR) *-• - .
End of transmission . . . - • -
```


## Special Foreign Letters

Ä (German) • - • -
A or A (Spanish-Scandinavian) •- - -
CH (German-Spanish) - - - -
$E^{\prime}$ (French) $\cdots$ -
$\widetilde{N}$ (Spanish) $--\cdot--$
Ö (German) - - - .
Ü (German) • • - -

## SIGNAL REPORTING CODES

## RST Code

The standard amateur method of giving signal strength reports. For phone operation only the first two sets of numbers are used with the words "readability" and "strength."

Readability ( $\mathbf{R}$ )

1. Unreadable
2. Barely readable, occasional words distinguishable
3. Readable with considerable difficulty
4. Readable with practically no difficulty
5. Perfectly readable

## Signal Strength (\$)

1. Faint; signal barely perceptible
2. Very weak signal
3. Weak signal
4. Fair signal
5. Fairly good signal
6. Good signal
7. Moderately strong signal
8. Strong signal
9. Extremely strong signal

Tone ( T )

1. Extremely rough, hissing signal
2. Very rough ac signal
3. Rough, low-pitched ac signal
4. Rather rough ac signal
5. Musically modulated signal
6. Modulated signal, slight whistle
7. Near dc signal, smooth ripple
8. Good dc signal, trace of ripple
9. Purest dc signal

If the signal has the steadiness of crystal control, add "X" after the RST report; add " C " for a chirp; and " K " for a keying click.

A typical report might be: "RST579X," meaning "Your signals are perfectly readable, moderately strong, have a perfectly clear tone, and have the stability of a crystal-controlled transmitter."

This reporting system is used on both CW and voice, leaving out the "Tone" report on voice.

## SINPO Code

A reporting method used in the shortwave field. All the numbers after the letters range from one to five. Q-code equivalents for each characteristic are also shown.

FOR EXAMPLE: A typical report for a station that is coming in loud and clear would read: SINPO 55555.

| $S$ Signal Strength (QSA) | Interference (QRM) | N <br> Atmospheric Noise (QRN) | $P$ <br> Propagation Disturbance (QSB) | Overall Merit (QRK) |
| :---: | :---: | :---: | :---: | :---: |
| 5 Excellent | 5 None | 5 None | 5 None | 5 Excellent |
| 4 Good | 4 Slight | 4 Slight | 4 Slight | 4 Good |
| 3 Fair | 3 Moderate | 3 Moderate | 3 Moderate | 3 Fair |
| $2 \text { Poor }$ | 2 Severe | 2 Severe | 2 Severe | 2 Poor |
| 1 Barely audible | 1 Extreme | 1 Extreme | 1 Extreme | 1 Unusable |

## 555 Code

Another reporting code sometimes used in the shortwave field.

|  | Signal Strength | Interference | Overall Merit |
| :--- | :--- | :--- | :--- |
|  | 0 Inaudible | 0 Total | 0 Unusable |
| 1 Poor | 1 Very severe | 1 Poor |  |
| 2 Fair | 2 Severe | 2 Fair |  |
| 3 Good | 3 Moderate | 3 Good |  |
| 4 Very good | 4 Slight | 4 Very good |  |
|  | 5 Excellent | 5 None | 5 Excellent |

## SINPFEMO Code

This eight-figure signal reporting method rates eight characteristics of a signal. (If a characteristic is not rated, the letter " $x$ " is used instead of a numeral.)

| Rating | S | 1 | N | P | $F$ | E | M | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Signal Strength | Degrading Effect of |  |  | Frequency of Fading | Modulation |  | Overall Rating |
|  |  | $\begin{aligned} & \text { Interference } \\ & \text { (QRM) } \end{aligned}$ | $\begin{aligned} & \text { Noise } \\ & \text { (QRN) } \end{aligned}$ | Propagation Disturbance |  | Quality | Depth |  |
| 5 | Excellent | Nil | Nil | Nil | Nil | Excellent | Maximum | Excellent |
| 4 | Good | Slight | Slight | Slight | Slow | Good | Good | Good |
| 3 | Fair | Moderate | Moderate | Moderate | Moderate | Fair | Fair |  |
| 2 | Poor | Severe | Severe | Severe |  | Poor | Poor or nil | Poor |
| 1 | Barely audible | Extreme | Extreme | Extreme | Very fast | Very poor | Continuously overmodulated | Unusable |

COMMERCIAL RADIO OPERATOR AND AMATEUR OPERATOR LICENSES REQUIREMENTS
Amateur Operator Licenses

| Class | Prior Experience | Code Test | Written Examination | Privileges | Term |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Novice | None | 5 w.p.m. | Elementary theory and regulations | Al Telegraphy in 3.73.75, 7.1-7.15, 21.121.2, 28.1-28.2 MHz. 250 watts maximum input. | 5 years, renewable |
| Technician | None | 5 w.p.m. (Credit given to Novice Class Licensees) | General theory and regulations | All amateur privileges above 50 MHz . <br> Also novice privileges. | 5 years, renewable |
| General | None | 13 w.p.m. | General theory and regulations (Credit given to Technician Class Licensees) | $1.8-2$, ${ }^{\text {a }} 3.525-3.775$, <br> 3.89-4, 7.025-7.15, <br> 7.225-7.3, 14.025- <br> 14.2, 14.275-14.35, <br> 21.025-21.25, 21.35- <br> 21.45, 28.0-29.7 <br> MHz , and all amateur <br> privileges above <br> 50 MHz . | 5 years, renewable |
| Advanced | None | 13 w.p.m. (Credit is given to General Class Licensees) | Intermediate theory and regulations | $\begin{aligned} & 1.8-2,3.525-3.775, \\ & 3.8-4,7.025-7.3, \\ & 14.025-14.45,21.025- \\ & 21.25 \text {, and all ama- } \\ & \text { teur frequencies } \\ & \text { above } 21.27 \mathrm{MHz} \text {. } \end{aligned}$ | 5 years, renewable |
| Amateur Extra | None | 20 w.p.m. | Advanced theory and regulations | All amateur privileges | 5 years, renewable |
| ${ }^{\text {a }}$ The 1.8-2 band frequency and power assignments differ from state to state. Check with nearest FCC office. |  |  |  |  |  |

Commercial Radio Operator Licenses

| Type <br> of License | Age <br> Minimum | Code <br> Requirement | Written <br> Test | Term <br> of License |
| :--- | :--- | :--- | :--- | :--- |
| Restricted Radiotelephone Permit | 14 years | None | None; obtained <br> by declaration <br> (FCC Form 753) | Lifetime |

## Commercial Examination Elements

NO. 1, BASIC LAW-
Provisions of laws, treaties and regulations with which every marine operator should be familiar. ( 20 Questions, multiple choice type)
NO. 2, BASIC OPERATING PRACTICE-
Operating procedures and practices generally followed or required in communicating by marine radio-telephone stations. ( 20 Questions, multiple choice type)
NO. 3, BASIC RADIOTELEPHONE-
Technical, legal and other matters including basic operating practices and provisions of laws, treaties and regulations applicable to operating radiotelephone stations other than broadcast. ( 100 Questions, multiple choice type)
NO. 5, RADIOTELEGRAPH OPERATING PRACTICE-
Radio operating procedures and practices generally followed or required in communicating by radiotelegraph stations primarily other than in the maritime mobile services of public correspondence. ( 50 Questions, multiple choice type)

## NO. 6, ADVANCED RADIOTELEGRAPH-

Technical, legal matters applicable to operating all classes of radiotelegraph stations including maritime mobile services of public correspondence, message traffic routing and accounting, radio navigational aids, etc. (100 Questions)
NO. 7, AIRCRAFT RADIOTELEGRAPH-
Special endorsement on Radiotelegraph First and Second Class Operator Licenses. Theory and practice in operation of radio communication and navigational systems in use on aircraft. ( 100 Questions, multiple choice type; code test of 20 code groups per minute and 25 WPM plain language.)
NO. 8, SHIP RADAR TECHNIQUES-
Special endorsement on Radiotelegraph or Radiotelephone First or Second Class Operator Licenses. Specialized theory and practice applicable to proper installation, servicing and maintenance of ship radar equipment in use for marine navigational purposes. ( 50 Questions, multiple choice type)

To avoid errors or misunderstanding during voice communication, the new international phonetic alphabet has been adopted.

| Letter | Name | Pronunciation | Letter | Name | Pronunciation |
| :--- | :--- | :--- | :---: | :--- | :--- |
|  |  |  |  |  |  |
| A | Alfa | AL-fah | N | November | No-VEM-ber |
| B | Bravo | BRAH-voh | O | Oscar | OSS-cah |
| C | Charlie | CHAR-lee | P | Papa | Pah-PAH |
|  |  | (or SHAR-lee) | Q | Quebec | Keh-BECK |
| D | Delta | DELL-tah | R | Romeo | ROW-me-oh |
| E | Echo | ECK-oh | S | Sierra | See-AlR-rah |
| F | Foxtrot | FOKS-trot | T | Tango | TANG-go |
| G | Golf | GOLF | U | Uniform | YOU-nee-form |
| H | Hotel | HOH-tel |  |  | (or OO-nee-form) |
| I | India | IN-dee-ah | V | Victor | VIK-tah |
| J | Juliett | JEW-lee-ett | W | Whiskey | WISS-key |
| K | Kilo | KEY-loh | X | X-ray | ECKS-ray |
| L | Lima | LEE-mah | Y | Yankee | YANG-key |
| M | Mike | MIKE | Z | Zulu | ZOO-loo |

ARRL (AMERICAN RADIO RELAY LEAGUE) WORD UST FOR VOICE COMMUNICATION

| A-Adam | N-Nancy |
| :--- | :--- |
| B-Baker | O-Otto |
| C-Charlie | P-Peter |
| D-David | Q-Queen |
| E-Edward | R-Robert |
| F-Frank | S-Susan |
| G-George | T-Thomas |
| H-Henry | U-Union |
| I-Ida | V-Victor |
| J-John | W-William |
| K-King | X-X-Ray |
| L-Lewis | Y-Young |
| M-Mary | Z-Zebra |

Example: W1AW . . . W1
ADAM WILLIAM . . . W1AW

## TRANSMISSION TRAVEL TIME

The time required for electromagnetic energy to travel interplanetary distances is significant. Shown here are some typical times and distances related to the earth's position.

| Moon Venus | (overhead) | $=23.9 \times$ | 7 |
| :---: | :---: | :---: | :---: |
|  | (nearest) | $=22.4 \times 10^{6} \mathrm{~nm}$ | 139.00 sec one way |
|  | (farthest) | $139.0 \times 10^{6} \mathrm{n} \mathrm{mi}$ | 859.00 sec one way |
| Mars | (nearest) | $42.4 \times 10^{6} \mathrm{n} \mathrm{mi}$ | 262.00 sec one way |
|  | (farthest) | $=203.9 \times 10^{6} \mathrm{nmi}$ | 1259.00 sec one way |
| Jupiter | (nearest) | $=339.8 \times 10^{6} \mathrm{nmi}$ | 2099.00 sec one way |
|  | (farthest) | $=501.2 \times 10^{6} \mathrm{nmi}$ | 3096.00 sec one |

In accordance with Federal Communications Commission Rules and Regulations 2.201, Subpart C, the following system of designating emission, modulation, and transmission characteristics is employed.


| Class | Name | Code | Action of Modulating Signal |
| :---: | :---: | :---: | :---: |
| A | Pulse-time modulation | PTM | Varies some characteristic of pulse with respect to time. |
|  | Pulseposition modulation | PPM | Varies position (phase) of pulse on time base. |
|  | Pulseduration modulation | PDM | Varies width of pulse (also called PWM, or PulseWidth Modulation). |
|  | Pulse-shape modulation |  | Varies shape of pulse. |
|  | Pulsefrequency modulation | PFM | Varies pulse recurrence frequency. |
| B | Pulseamplitude modulation | PAM | Varies amplitude of pulse-consists of two types: one using unipolar pulses, the other using bipolar pulses. |
| C | Pulse-code modulation | PCM | Varies the makeup of a series of pulses and spaces. Individual systems are classified as follows: Binary-pulse and spaces, or positive and negative pulses. Ternary-positive pulses, negative pulses, and spaces. N -ary-more complex combinations of pulses and spaces. |

## MICROPHONE OUTPUT NOMOGRAM

This nomogram determines the output voltages for various microphone ratings and relates this output to actual sound pressure levels.

Two methods of specifying microphone levels are in general use. Acoustic input and electrical output are specified so that the microphone can be considered as a generator, with sound pressure input and voltage or power output.

For low-impedance microphones, output is given in decibels referenced to 1 mW for 10 dynes $/ \mathrm{cm}^{2}$ sound pressure. For high-impedance microphones, output is given in decibels referenced to 1 V for $1 \mathrm{dyne} / \mathrm{cm}^{2}$ sound pressure. (In both, output is into a resistive load equal to the impedance of the microphone.)

This nomogram is prepared for microphone preamplifiers with low input impedances matched to the microphone impedance. (Open-circuit voltage is 6 dB higher than the nomogram value.) Connecting the microphone impedance and the decibel rating solves for the voltage across a matched load for the standard 10 dynes $/ \mathrm{cm}^{2}$ sound pressure field. By referring to the absolute sound pressure vs decibel scale, any other sound pressure level can be found and the decibel difference (with respect to 10 dynes $/ \mathrm{cm}^{2}$ ) can be determined, and adjustments can be made in the output voltage by adding or subtracting decibels.

For high-impedance microphones, the nomogram is used in the same way, except that the impedance is always considered as $40,000 \mathrm{ohms}$, and the reading will be that for a 10 dynes $/ \mathrm{cm}^{2}$ field. These microphones are usually operated into a very high impedance circuit, hence 6 dB must be added to the output voltage. (Use of this method results in an error of approximately 2 dB .)


Sound pressure level


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## ATTENUATOR NOMOGRAMS

These two nomograms solve for the resistor values required for the following: $\mathrm{T}, \mathrm{Pi}, \mathrm{H}, \mathrm{O}$, lattice, bridged T , bridged H,L, and U-type attenuators. The nomograms are based on the equations shown. The keys next to the nomograms show which scales must be used for a particular type of attenuator.

FOR EXAMPLE:

1. $Z_{0}$ is 600 ohms and the required attenuation is 20 dB . Design $\mathrm{T}, \mathrm{H}$, and Pi attenuators. From nomogram 1 , for a T type, $R_{1}$ is 480 ohms and $R_{4}$ is 120 ohms . For an H type each of the four series arms would be 240 ohms . For Pi type (middle key) $R_{2}$ is 750 ohms and $R_{3}$ is 3,000 ohms.
2. A lattice attenuator (key three, nomogram 1) that gives 20 dB of attenuation at 500 ohms requires $R_{1}$ to be 410 ohms and $R_{2}$ to be 610 ohms.
3. A bridged $T$ attenuator (nomogram 2, first key) with an attenuation of 20 dB and terminal impedances of 450 ohms has $R_{5}$ as 4,000 ohms and $R_{6}$ as 50 ohms.
4. Design an L-type attenuator (middle key, nomogram) with an attenuation of 14 dB , and an impedance of 50 ohms with the shunt arm at the output end. In this case $R_{5}$ is 200 ohms and $R_{6}$ is 62.5 ohms.

NOTE: In all cases the input and output impedances are the same.

$$
\begin{aligned}
& R_{1}=Z_{0}\left(\frac{K-1}{K+1}\right) \quad R_{3}=Z_{0}\left(\frac{K^{2}-1}{2 K}\right) \quad R_{5}=Z_{0}(K-1) \quad R_{7}=Z_{0}\left(\frac{K-1}{K}\right) \\
& R_{2}=Z_{0}\left(\frac{K+1}{K-1}\right) \quad R_{4}=Z_{0}\left(\frac{2 K}{K^{2}-1}\right) \quad R_{6}=Z_{0}\left(\frac{1}{K-1}\right) \quad R_{8}=Z_{0}\left(\frac{K}{K-1}\right)
\end{aligned} \text { where } K=\frac{E_{\mathrm{in}}}{E_{\text {out }}}
$$

NOMOGRAM 1 FOR T, Pi, H, O, AND LATTICE TYPE ATTENUATORS.


## NOMOGRAM 2 FOR BRIDGED T, H, L, AND U TYPE ATTENUATORS.


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## TWIN-T FILTER NOMOGRAM

Twin-T filters with symmetrical response curves are frequently used to reject specific frequencies, or they may be included in the negative feedback loop of a frequency-selective amplifier as the tuning element. Other component combinations may be used, but the one selected here has the greatest possible selectivity. With this general configuration, any filter exhibits infinite attenuation at the notch frequency $\left(f_{0}\right)$ which is specified by the values of $R_{1}$ and $C_{1}$. If it is only desired to reject $f_{0}$, then the choice of these values is arbitrary. However, if it is desired to design a filter with a symmetrical response curve so the dc gain is equal to that at high frequencies, that is accomplished when $R_{1}=\sqrt{R_{8} R_{L} / 2}$, and the notch frequency is determined by the expression $f_{0}=1 / 4 \pi C_{1} R_{1}$. The nomograms are based on these two equations. Usually $R_{0,}, R_{L}$, and $f_{o}$ are known, and the values of $R_{1}$ and $C_{1}$ are to be determined. It is also possible to use chart 2 alone and select arbitrary values for $R_{1}$ or $C_{1}$ if symmetrical response is not essential.

FOR EXAMPLE: Design a filter with infinite attenuation at 800 Hz which is to be inserted between a 2,000 -ohm source impedance and a load resistance of 100,000 ohms. From nomogram 1 determine that $R_{1}$ should be 10,000 ohms, and with that value determine from nomogram 2 that $C_{1}$ must be $0.01 \mu \mathrm{~F}$ to achieve a symmetrical response curve.

Twin-T notch filter, with component values related as shown, yields maximum selectivity and symmetrical gain-frequency response.

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This nomogram solves for the resistance values needed for an impedance matching pad having a minimum of attenuation. $Z_{1}$ is the greater and $Z_{2}$ is the lesser terminal impedance in ohms. To use the nomogram, calculate the ratio of $Z_{2} / Z_{1}$ and connect that point on the center scale with $Z_{1}$ to find $R_{1}$, and with $Z_{2}$ to find $R_{3} 890$ ohms also read on the center scale.

FOR EXAMPLE: If $Z_{2}$ is 400 ohms and $Z_{1}$ is 500 ohms, the value of $R_{1}$ must be 225 ohms and of $R_{3} 890$ ohms for a minimum insertion loss pad that has 4.2 dB of insertion loss.

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## PREFERRED VALUES OF COMPONENTS

Preferred numbers for nominal values of resistance, capacitance, and inductance have been adopted by the electronics industry. Each value differs from its predecessor by step multiples of (10) $1 / 16,(10) 1 / 12$, or (10) $1 / 24$ resulting in incremental increase of approximately $40 \%, 20 \%$, and $10 \%$ per step as shown in the table, to yield an orderly progression of component values of $\pm 20 \%, \pm 10 \%$, and $\pm 5 \%$.

Standard values outside of the range listed can be obtained by multiplying by suitable multiples of 10 . (For example, 15 can represent $1.5,150,15 \mathrm{k}, 1.5 \mathrm{M}$, etc.)

MIL and EIA Standard for Component Values and Tolerances

| $\pm 20 \%$ | $\pm 10 \%$ | $\pm 5 \%$ |
| :---: | :---: | :---: |
| 10 | 10 | 10 |
|  |  | 11 |
|  | 12 | 12 |
| 15 | 15 | 13 |
|  |  | 15 |
|  | 18 | 16 |
|  |  | 18 |
| 22 | 22 | 20 |
|  |  | 22 |
|  | 27 | 24 |
|  |  | 27 |
| 33 | 33 | 30 |
|  |  | 33 |
|  |  | 36 |
| 47 |  | 39 |
|  |  | 43 |
|  |  | 43 |
|  |  | 47 |
| 68 |  | 51 |
|  |  | 56 |
|  |  | 62 |
|  |  | 68 |
| 100 |  | 75 |
|  |  | 82 |
|  |  | 91 |
|  |  | 100 |

Given frequency, input $C$, and amplifier input $Z$, only two operations are required to find the equivalent thermal noise voltage.

When an amplifier is fed from a capacitive source, the spot (one frequency) noise is generated by the real part of the impedance. This nomogram reduces the calculation required to arnive at the noise value. Impedance at the amplifier input is

$$
\begin{equation*}
z=\frac{R-j R^{2} \omega C}{R^{2} \omega^{2} C^{2}+1} \tag{1}
\end{equation*}
$$

Thermal noise is generated by the real part of this expression, which is

$$
\begin{equation*}
(\text { REAL } Z)=\frac{R}{R^{2} \omega^{2} C^{2}+1} \approx \frac{1}{R \omega^{2} C^{2}} \tag{2}
\end{equation*}
$$

The mean square thermal noise voltage associated with the real part of $Z$ is given by

$$
\begin{equation*}
\overline{\mathrm{e}}^{2}=4 k T d f(R E A L Z) \tag{3}
\end{equation*}
$$

For this case

$$
\begin{aligned}
& d f=1 \text { (spot frequency) } \\
& \quad T=25^{\circ} \mathrm{C}
\end{aligned}
$$

Combining (2) and (3)

$$
\begin{equation*}
\bar{e}^{2}=4 k T d f \frac{1}{R \omega^{2} C^{2}} \tag{4}
\end{equation*}
$$

Equation (4) forms the basis for the nomogram. Nomogram of equivalent spot thermal noise voltage of the parallel combination of a capacitor and an amplifier input resistance. Using the nomogram:

1. Choose $f, C$, and $R$ (in the example $f=10 \mathrm{kHz}, C=0.001 \mu F$, and $R=1 \mathrm{M}$ ohm).
2. Draw a line between the chosen $f$ and $C$.
3. Mark its intersection on the reference line.
4. Draw a line from the marked point on the reference scale to the chosen $R$.
5. The intersection of this line with the $\overline{\mathbf{e}}^{2}$ scale is the desired equivalent thermal noise voltage in dB re 1 V .


## THERMAL NOISE VOLTAGE NOMOGRAM (B)

Thermally produced noise voltage of any linear conductor is determined by Nyquist's equation

$$
E=2 \sqrt{R k T B}
$$

$$
\text { where } \begin{array}{rlrl}
E & =\text { noise voltage in rms microvolts } & T & =\text { absolute temperature }\left({ }^{\circ} \mathrm{K}\right) \\
k & =\text { Boltzmann's constant, } 1.38 \times 10^{-23} \mathrm{~J} /{ }^{\circ} \mathrm{K} & B=\text { bandwidth in hertz } \\
R & =\text { resistance } & &
\end{array}
$$

This nomogram solves the above equation if any three of the four variables are given.
FOR EXAMPLE: An amplifier has a voltage gain of 1,000 , and input resistance of 470,000 ohms, and a bandwidth of 2 kHz . Find the output noise level due to the input resistance if the amplifier is operated at an ambient temperature of $100^{\circ} \mathrm{C}$.

Connect $100^{\circ} \mathrm{C}$ ( $T$ scale) with 470 K ( $R$ scale) and note intersect point on turning scale. Connect that point with 2 kHz ( $B$ scale) and read noise voltage as $4.4 \mu \mathrm{~V}$ on E scale. The amplifier has a gain of 1,000 ; thus, the outside noise of the amplifier due to the input resistance is 4.4 mV .


This nomogram is based on the formula for the inductance of a single-layer coil

$$
L=\frac{a^{2} N^{2}}{9 a+10 b}
$$

$$
\text { where } \begin{aligned}
L & =\text { inductance in microhenries } \\
a & =\text { coil radius in inches } \\
b & =\text { coil length in inches } \\
N & =\text { number of turns }
\end{aligned}
$$



FOR EXAMPLE: (1). Find the inductance of a 100-turn coil with a diameter of 2 in . and a winding length of 0.8 in. Find K (diameter/length) $2 / 0.8$ to be 2.5 . Connecting 2.5 on the K scale to 100 on the N scale intersects the turning axis at 3.8 . Now connect 3.8 with 2 on the D scale, and read the inductance as $600 \mu \mathrm{H}$. (2) Determine the number of turns required for a $290-\mu \mathrm{H}$ coil 3 in . long with a diameter of 2.5 in . K is equal to 0.8 . Connect 290 on the L scale with 2.5 on the D scale, and read 4.6 on the turning axis. Connecting 4.6 and 0.8 on the K scale gives the answer as 90 turns on the N scale.


## SINGLE-LAYER COIL DESIGN NOMOGRAM (B)

This nomogram solves for the number of close-wound tums required to achieve inductances in the range of values required for television, fm , and radar if transformers. The nomogram is based on a slight modification of H.A. Wheeler's inductance formula that was used to construct nomogram A. The formula used here (with all dimensions in inches) is

$$
L=\frac{a^{2} N^{2}}{8.85 a+10 b}
$$

FOR EXAMPLE: Ten turns of number 30 AWG enameled wire closewound on a 0.25 -inch diameter coil form will produce an inductance of $0.7 \mu \mathrm{H}$.

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## INDUCTANCE OF STRAIGHT, ROUND WIRE AT HIGH FREQUENCIES

Above several megahertz the inductance of relatively short lengths of wire becomes important because of the effect on circuit performance. The chart shows the relationship between diameter, wire length, and inductance for various diameters. A more precise tabulation is also shown for short lengths of commonly used wire sizes.

FOR EXAMPLE: A straight piece of wire 4 in . long with a diameter of 25 mil has an inductance of $0.2 \mu \mathrm{H}$. At a frequency of 80 MHz , this represents an inductive reactance of about 100 ohms.

| AWG <br> Wire Size | Length <br> (in.) | Approx. <br> inductance <br> $(\mu \mathrm{H})$ |
| :---: | :---: | :---: |
| 20 | $1 / 4$ | 0.0031 |
|  | $1 / 2$ | 0.0064 |
|  | $3 / 4$ | 0.0115 |
|  | 1 | 0.019 |
|  | $11 / 2$ | 0.031 |
|  | 2 | 0.04 |
| 24 | $1 / 4$ | 0.0037 |
|  | $1 / 2$ | 0.0082 |
|  | $3 / 4$ | 0.014 |
|  | 1 | 0.022 |
|  | $11 / 2$ | 0.036 |
|  | 2 | 0.05 |


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TRANSFORMER IMPEDANCE NOMOGRAM
Tapped transformers provide standard impedances between the various taps and the common terminal. If a nonstandard impedance is required, it can often be found between the taps. This nomogram determines the impedance between terminals $B$ and $C$ if the impedance from $A$ to $B$ and $A$ to $C$ are known, and it is based on the following formula

$$
Z_{(B-C)}=\left(\sqrt{Z_{(A-C)}}-\sqrt{Z_{(A-B)}}\right)^{2 \cdot}
$$

FOR EXAMPLE: If the impedance from $A$ to $B$ is 15 ohms, and the impedance from $A$ to $C$ is 250 ohms, then the impedance from $B$ to $C$ is $\approx 145$ ohms.

$$
\text { *Derived from } Z_{(B-C)}=Z_{A-B}\left(\sqrt{\frac{Z_{(A-C)}}{Z_{(A-B)}}}-1\right)^{2}
$$



| 1 |
| ---: | ---: | ---: |
| 3 |
| 5 |

## ENERGY STORAGE NOMOGRAM

The nomogram relates capacitance, charging voltage, and stored energy in a capacitor in accordance with the formula

$$
J \text { or } W=\frac{C V^{2}}{2}
$$

$$
\begin{aligned}
\text { where } J \text { or } \begin{aligned}
W & =\text { energy in joules or watt-seconds } \\
C & =\text { capacitance in microfarad } \\
V & =\text { charging voltage }
\end{aligned}
\end{aligned}
$$

FOR EXAMPLE: The energy stored in a $525-\mu \mathrm{F}$ capacitor charged to 450 V is 53 W -sec or joules.

|  | Charging voltage <br> (de V) | CAPACITANCE <br> ( $\mu \mathrm{F}$ ) |
| :---: | :---: | :---: |

## POWER-FACTOR CORRECTION

Power factor is the ratio (usually given in percent) of the actual power used in a circuit to the power apparently drawn from the line.

$$
P F=\frac{\text { actual power }}{\text { apparent power }}
$$

A low power factor is undesirable, and it can be raised by the addition of power-factor correction capacitors which are rated in kVAR (kilovolt-ampere reactive). To determine the kVAR of the capacitors needed to correct from an existing to a higher power factor, multiply the proper value in the table by the average power consumption on kilowatts, of the load.

FOR EXAMPLE: Find the kVAR of capacitors that is required to raise the power factor of a $500-\mathrm{kW}$ load from $70 \%$ to $85 \%$.

From the table select the multiplying factor 0.400 which corresponds to the existing $70 \%$ and required $85 \%$ power factor. Multiplying 0.400 by 500 shows that 200 kVAR of capacitors are required.

| Existing <br> Power <br> Factor <br> $\%$ | $100 \%$ | $95 \%$ | $90 \%$ | $85 \%$ | $80 \%$ | $75 \%$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Corrected Power Factor |  |  |  |  |  |
| 50 | 1.732 | 1.403 | 1.247 | 1.112 | 0.982 | 0.850 |
| 52 | 1.643 | 1.314 | 1.158 | 1.023 | 0.893 | 0.761 |
| 54 | 1.558 | 1.229 | 1.073 | 0.938 | 0.808 | 0.676 |
| 55 | 1.518 | 1.189 | 1.033 | 0.898 | 0.768 | 0.636 |
| 56 | 1.479 | 1.150 | 0.994 | 0.859 | 0.729 | 0.597 |
| 58 | 1.404 | 1.075 | 0.919 | 0.784 | 0.654 | 0.522 |
| 60 | 1.333 | 1.004 | 0.848 | 0.713 | 0.583 | 0.451 |
| 62 | 1.265 | 0.936 | 0.780 | 0.645 | 0.515 | 0.383 |
| 64 | 1.201 | 0.872 | 0.716 | 0.581 | 0.451 | 0.319 |
| 65 | 1.168 | 0.839 | 0.683 | 0.548 | 0.418 | 0.286 |
| 66 | 1.139 | 0.810 | 0.654 | 0.519 | 0.389 | 0.257 |
| 68 | 1.078 | 0.749 | 0.593 | 0.458 | 0.328 | 0.196 |
| 70 | 1.020 | 0.691 | 0.535 | 0.400 | 0.270 | 0.138 |
| 72 | 0.964 | 0.635 | 0.479 | 0.344 | 0.214 | 0.082 |
| 74 | 0.909 | 0.580 | 0.424 | 0.289 | 0.159 | 0.027 |
| 75 | 0.882 | 0.553 | 0.397 | 0.262 | 0.132 |  |
| 76 | 0.855 | 0.526 | 0.370 | 0.235 | 0.105 |  |
| 78 | 0.802 | 0.473 | 0.317 | 0.182 | 0.052 |  |
| 80 | 0.750 | 0.421 | 0.265 | 0.130 |  |  |
| 82 | 0.698 | 0.369 | 0.213 | 0.078 |  |  |
| 84 | 0.646 | 0.317 | 0.161 |  |  |  |
| 85 | 0.620 | 0.291 | 0.135 |  |  |  |
| 86 | 0.594 | 0.265 | 0.109 |  |  |  |
| 88 | 0.540 | 0.211 | 0.055 |  |  |  |
| 90 | 0.485 | 0.156 |  |  |  |  |
| 92 | 0.426 | 0.097 |  |  |  |  |
| 94 | 0.363 | 0.034 |  |  |  |  |
| 9 | 0.329 |  |  |  |  |  |
| 9 |  |  |  |  |  |  |

The power factor $(\cos \phi)$ of a series RL or a parallel RC network is given by the following formulas

$$
\begin{aligned}
& \text { P.F. (inductive) }=\frac{R_{2}}{\sqrt{R_{s}^{2}+(\omega L)^{2}}} \\
& \text { P.F. (capacitive) }=\frac{1}{\sqrt{\left(R_{\mathrm{p}} \omega C\right)^{2}+1}}
\end{aligned}
$$

To use the nomogram connect frequency with the desired value of $L$ or $C$ and note the intersect point on the turning scale. Using this intersect point, connect to the resistance, and by extending this line, read power factor and phase angle.

## FOR EXAMPLE:

1. A $1-\mathrm{H}$ inductance in series with 100 ohms is connected to a $60-\mathrm{Hz}$ source. In this case $\phi$ is $75^{\circ}$ and $\cos \phi$ $=0.26$.
2. An inverter operating at 2 kHz is used to supply a 100 -ohm load which is in parallel with a capacitance of $0.047 \mu \mathrm{~F}$. In this case $\phi$ is $3.5^{\circ}$ and $\cos \phi=0.998$.

This nomogram is based on the formula

$$
k V A R=\frac{2 \pi f C E^{2}}{10^{9}}
$$

where $C$ is in microfarad $E$ in volts, and $f$ is 60 Hz .
FOR EXAMPLE: To provide 5 kVAR at 460 V requires $62 \mu \mathrm{~F}$.
(
kVAR


## SELF-RESONANT FREQUENCY OF PARALLEL LEAD CAPACITORS

The curves show the approximate self-resonant frequency of capacitors with various lead lengths. They apply to parallel lead wires of equal length \#20 to \#24 AWG, spaced no further than 0.375 in . apart.

FOR EXAMPLE: A $1,000-\mathrm{pF}$ capacitor with 2 -in. leads resonates at about 18 MHz . The same capacitor with $0.2-\mathrm{in}$. leads will resonate at 60 MHz .


## REACTANCE NOMOGRAMS

The set of three nomograms on the following pages covers the frequency range of 1 Hz to $1,000 \mathrm{MHz}$ in three ranges which give direct answers without the need for additional calculations to locate the decimal point. These nomograms may be used to find capacitive reactance, inductive reactance, as well as resonant frequency ( $X_{L}=$ $X_{c}$ ) of any combination of inductance and capacitance.

## FOR EXAMPLE:

1. The reactance of a $10-\mathrm{mH}$ inductor at $10-\mathrm{kHz}$ is 630 ohms.
2. The reactance of a $3-\mathrm{pF}$ capacitor at 5 MHz is 10,500 ohms.
3. A $5-\mu \mathrm{F}$ capacitor and a $1.4-\mathrm{H}$ inductance resonante at 60 Hz .








At very high frequencies current travels close to the outer surface of the conductor and eddy current losses increase beneath the surface. This effect is called "skin resistance" or "rf resistance." This chart shows the minimum required conductor depth related with frequency. The depth varies with the resistivity of the material and is least for silver. Therefore, a silver plating is frequently applied to conductors that are used at high frequencies so as to reduce the skin resistance.

FOR EXAMPLE: At 200 MHz a minimum thickness of 0.81 mils of cadmium is required, whereas only 0.18 mils of silver are needed at the same frequency.


IMPEDANCE OF SERIES-CONNECTED AND PARALLEL-CONNECTED COMBINATIONS OF L, C, AND R

| Circuit | Series combination | $\begin{aligned} & \text { Impedance } \\ & \mathbf{Z}=R+j X \end{aligned}$ | Magnutude of impedance $\|Z\|=\sqrt{R^{\prime}+X^{\prime}}$ | $\begin{gathered} \text { Phase sngle } \\ \phi=\operatorname{tin}^{-1}(X / R) \end{gathered}$ | $\begin{gathered} \text { Admiftance }^{a} \\ \mathbf{Y}=1 / \mathbf{Z} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\longrightarrow$ C-m | $R$ | ohm $R$ | ohms R | $\begin{gathered} \text { radians } \\ 0 \end{gathered}$ | $\begin{aligned} & \text { mhos } \\ & 1 / R \end{aligned}$ |
| mor | $L$ | +jwL | $\omega L$ | $+\pi / 2$ | $-f(1 / \omega L)$ |
| - 1 | C | $-j(1 / \omega C)$ | $1 / \omega C$ | - - $/ 2$ | $j \omega C$ |
| C-mm | $R_{1}+R_{3}$ | $R_{1}+R_{1}$ | $\boldsymbol{R}_{\mathbf{4}}+\mathrm{R}_{\mathbf{z}}$ | 0 | $1 /\left(R_{1}+R_{\mathrm{s}}\right)$ |
| $\sim_{\text {- }}^{\text {- }}$ | $L_{1}(M) L_{1}$ | $+j \omega\left(L_{1}+L_{1} \pm \mathbf{2 M}\right)$ | $\omega\left(L_{1}+L^{\prime} \pm 2 M\right)$ | + $\pi / 2$ | $-j / \omega\left(L_{1}+L_{1} \pm 2 M\right)$ |
| $\longrightarrow \mathrm{HH}$ | $C_{1}+C_{3}$ | $-j \frac{1}{\omega}\left(\frac{C_{1}+C_{3}}{C_{1} C_{3}}\right)$ | $\frac{1}{\omega}\left(\frac{C_{1}+C_{7}}{C_{4} C_{2}}\right)$ | $-\frac{\pi}{2}$ | $j \omega\left(\frac{C_{1} C_{3}}{C_{1}+C_{2}}\right)$ |
| mmon | $R+L$ | $R+j \omega L$ | $\sqrt{\overline{R^{3}}+\omega^{3} L^{3}}$ | $\tan ^{-1} \frac{\omega L}{R}$ | $\frac{R-j \omega L}{R^{3}+L^{*}}$ |
| $\longrightarrow$ - | $R+C$ | $R-j \frac{1}{\omega C}$ | $\sqrt{\frac{\omega^{2} C^{t} R^{2}+1}{\omega^{2} C^{t}}}$ | $-\tan ^{-1} \frac{1}{\omega R C}$ | $\frac{\omega^{3} C^{3} R+j \omega C}{\omega^{1} C^{3} R^{1}+1}$ |
| mel! | $L+C$ | $+j\left(\omega L+\frac{1}{\omega C}\right)$ | $\left(\omega L-\frac{1}{\omega C}\right)$ | $\pm \frac{\pi}{2}$ | $-\frac{j \omega C}{\omega^{2} L C-1}$ |
| $\rightarrow \sim$-mF | $R+L+C$ | $R+i\left(\omega L-\frac{1}{\omega C}\right)$ | $\sqrt{R^{1}+\left(\omega L-\frac{1}{\omega C}\right)^{3}}$ | $\tan ^{-1}\left(\frac{\omega L-1 / \omega C}{R}\right)$ | $\frac{R-j(\omega L}{R^{3}+(\omega L} \frac{-1 / \omega C)}{-1 / \omega C)^{t}}$ |


| Circuit | Parallel combination | $\begin{aligned} & \text { Impedance } \\ & \mathbf{z}=\boldsymbol{R}+j X \end{aligned}$ | Magnitude of impedance $\|Z\|=\sqrt{R^{v}+X^{y}}$ | Phase angle $\phi=\tan ^{-1}(X / R)$ | $\begin{aligned} & \text { Admitrance }{ }^{\text {a }} \\ & \mathbf{Y}=1 / \mathbf{Z} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $R_{3}, R_{1}$ | $\frac{\begin{array}{c}\text { ohms } \\ R_{1} R_{3}\end{array}}{R_{1}+R_{1}}$ | $\begin{gathered} \begin{array}{c} \text { ohms } \\ R_{1} R_{2} \end{array} \\ R_{1}+R_{3} \end{gathered}$ | radians | $\begin{aligned} & \text { mbot } \\ & \frac{R_{1}+R_{\mathrm{s}}}{R_{\mathrm{v}} R_{\mathrm{i}}} \end{aligned}$ |
|  | $C_{34} C_{3}$ | $-\frac{1}{0\left(C_{1}+C_{2}\right)}$ | $\frac{1}{w\left(C_{1}+\bar{G}_{2}\right)}$ | $-\frac{\pi}{2}$ | $+j \omega\left(C_{1}+C_{2}\right)$ |
|  | $L, R$ | $\frac{\omega^{3} L^{3} R+j \omega L R^{2}}{\omega^{2} L^{3}+R^{*}}$ | $\frac{\omega L R}{\sqrt{\omega^{2} L^{1}+R^{3}}}$ | $\tan ^{-1} \frac{R}{\omega L}$ | $\frac{1}{R}-\frac{j}{w L}$ |
|  | R, C | $\frac{R-j \omega R^{*} C}{1+\omega^{2} R^{2} C^{1}}$ | $\frac{R}{\sqrt{1+\omega^{*} R^{\prime} C^{i}}}$ | $\tan ^{-1}(-\omega R C)$ | $\frac{1}{R}+j \omega C$ |
|  | $L, C$ | $+j \frac{\omega L}{1-\omega^{2} L C}$ | $\frac{\omega L}{1-\omega^{0} L C}$ | $\pm \frac{17}{2}$ | $j\left(\omega C-\frac{1}{\omega L}\right)$ |
|  | $L_{4}(M) L_{i}$ | $+j \omega \frac{L_{1} L_{4}-M^{\prime}}{L_{1}+L_{1} \mp 2 M}$ | $\frac{L_{1} L_{1}-M^{2}}{L_{1}+L_{1} \mp 2 M}$ | $\pm \frac{\pi}{2}$ | $-j \frac{1}{\omega}\left(\frac{L_{1}+L_{0} \mp 2 M}{L_{1} L_{4}-M^{2}}\right)$ |
|  | L, C, R | $\frac{\frac{1}{R}-j\left(\omega C-\frac{1}{\omega L}\right)}{\left(\frac{1}{R}\right)^{\prime}+\left(\omega C-\frac{1}{\omega L}\right)^{1}}$ | $\frac{R}{\sqrt{1+R^{\prime}\left(\omega C-\frac{1}{\omega L}\right)^{2}}}$ | $\tan ^{-2}-R\left(\omega C-\frac{1}{\omega L}\right)$ | $\frac{1}{R}+j\left(\omega C-\frac{1}{\omega L}\right)$ |

## FREQUENCY CHARACTERISTICS OF RESISTORS, CAPACITORS, AND INDUCTORS

Tabulated here are the effects when potentials of increasing frequency are applied to resistors, capacitors, and inductors.

As the frequency increases from dc to above resonance, the effective "look" of the component changes as shown.


## RESISTANCE-VOLTAGE-CURRENT-POWER NOMOGRAM

This nomogram is based on Ohm's law, and one straight line will determine two unknown parameters if two others are given. Preferred ( $\pm 20 \%$ ) resistance values are marked in addition to the ordinary resistance scale divisions. The power scale is calibrated in watts and dBm with a reference level of $0 \mathrm{dBm}=1 \mathrm{~mW}$ into 600 ohms. This, direct conversion between dBm and watts can be made. To cover a wide range of values and yet maintain accuracy, a dual numbering system is used. To avoid confusion, all members should be read from either the regular or the gray-barred scales.

## FOR EXAMPLE:

1. The current through a $150-\mathrm{k}$ resistor with a potential drop of 300 V is 2 mA , and the power dissipated is 600 mW or 0.6 W .
2. When a 12,000 -ohm resistor has a current of 6 mA through it, the power dissipated is 0.43 W and the voltage across the resistor is 72 V .
3. The voltage across a 4.7 M ohm resistor with a signal level of -30 dBm is about 2.15 V rms.
4. The maximum allowable current through a 10 W 200 -ohm resistor is 0.22 A . Under these operating conditions there will be 45 V across the resistor.


This nomogram aids in the rapid selection of component values for the simple resistive and capacitive voltage dividers illustrated, where

$$
\frac{e_{0}}{e_{i}}=\frac{R_{g}}{R_{g}+R_{s}} \text { or } \quad \frac{e_{0}}{e_{i}}=\frac{C_{s}+C_{g}}{C_{s}}
$$

Only two decades are covered on the left and right scale to achieve maximum accuracy. The range of the nomogram can be extended by multiplying these two columns by the same power of ten without making any changes in the center column.

FOR EXAMPLE:

1. A blocking oscillator must be held at cutoff by means of a voltage divider between B - and ground. Cut-off bias is -15 V , the negative supply is 150 V , and the grid-to-ground resistor is 22,000 ohms. Thus, $e_{o} / \mathrm{e}$, is 0.1 . Joining that value with 2.2 on the $R_{g}$ scale gives 20 on the $R_{s}$ scale, which makes that resistor equal to 200,000 ohms since each scale had to be multiplied by $10^{4}$.
2. Design an rf probe with a $5: 1$ attenuator using standard capacitance values. Rotating about the 0.2 point on the center scale gives typical values of 30 pF for $\mathrm{C}_{g}$ and 7.5 pF for $C_{s}$.

NOTE: The longer lines outside the left and right columns locate standard $\pm 10 \%$ values and the shorter lines locate standard $\pm 5 \%$ values.

(a)

(b)



It is often necessary to know the portion of the input voltage that will appear across the load resistor in a capacitively coupled circuit. This is a function of frequency and a factor of the ratio of $R$ to $X_{c}$, the required ratio is shown on the center scale. It is interesting to note that any ratio of $R$ to $X_{c}$ greater than $7.4: 1$ yields over $99 \%$ output. The $X_{c}$ and $R$ scales can be multiplied by any common power of ten to extend the range of the nomogram.

FOR EXAMPLE: For $R=100 \mathrm{k}$ and $X_{c}=10 \mathrm{k}, V_{2}$ will be $99.4 \%$ of $V_{1}$.

(From Electronics and Communications, June, 1966.)

## R-C COUPLING NOMOGRAM

This nomogram is used to calculate phase shift and attenuation in R-C coupling networks. To use, connect capacitance with frequency and note the intersect point on the turning scale. Using this intersect point, connect to the resistance, and by extending this line, read attenuation and phase shift.

FOR EXAMPLE: At $60 \mathrm{~Hz}, \mathrm{a} 0.01-\mu \mathrm{F}$ capacitor and 10,000 -ohm resistor will exhibit a phase shift of $72^{\circ}$ and an attenuation factor of 0.35 .


This table illustrates how performance characteristics of an amplifier can be determined by observing the waveform of the output, when the input is a square wave.

| Output Waveform | Low Frequency |  | High Frequency |  | Damping |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Gain | Delay | Gain | Delay |  |
| --5 | Ideal | Ideal | Ideal | Ideal | Ideal |
|  | Inadequate | Good | Excessive | Good | High |
|  | Excessive | Good | Inadequate | Good | High |
|  | Good | Excessive | Good | Inadequate | High |
|  | Good | Inadequate | Good | Excessive | High |
| V | Excessive | Excessive | Inadequate | Inadequate | High |
| $5$ | Excessive | Inadequate | Inadequate | Excessive | High |
|  | Inadequate | Excessive | Excessive | Inadequate | High |
|  | Good | Good | Excessive | Good | Medium |
|  | Good | Good | Excessive | Good | Low |
|  | Good | Good | Excessive | Good | Poor |
| $\square$ | Good | Good | Sharp Cutoff or Peaked | Good | Low |

LOW-END AMPLIFIER RESPONSE
In an RC-coupled amplifier, the coupling capacitance ( $C$ ), combines with the output load ( $R$ ), to form a potential divider or filter.

The response curve of this combination usually is specified in terms of the relative gain -3 dB point which can be calculated from the equation:

$$
\frac{e_{2}}{e_{1}}=\frac{1}{\sqrt{1+\frac{1}{(2 \pi f T)^{2}}}}=0.708
$$

where $T=R C$ and 0.708 is used to calculate the 3 dB point.
The accompanying nomogram relates the parameters $R, \operatorname{Cor} f_{-3 \mathrm{~dB}}$. Given any two, the third term can be determined by a simple straight-line alignment.

EXAMPLE: With a load of 10 k , what capacitance will give a low cutoff frequency of 20 Hz ?
The alignment shows that a capacitor of $0.8 \mu \mathrm{~F}$ will yield the desired high-pass characteristic.


This nomogram is based on the formula $T=R C$ where $T$ (the time constant) is the time required for the capacitor in an RC series circuit to reach $63.2 \%$ of the applied voltage.

FOR EXAMPLE: The time constant of 10 msec can be achieved with a $1-\mathrm{M}$ ohm resistor and a $0.01-\mu \mathrm{F}$ capacitor.


## TIME-CONSTANT NOMOGRAM (B)

This chart is used to determine the time required in an RC series circuit to reach a given fraction of an applied step input, or to determine the percent of the applied input when the time constant is given.

The nomogram is based on the relationship.

$$
\frac{E_{\text {out }}}{E_{\text {in }}}=1-\mathrm{e}^{-t / A C}
$$

FOR EXAMPLE: Determine the time required to charge a $50-\mu \mathrm{F}$ capacitor to 400 V through 1,000 ohms from a 450 V supply. The percent of applied voltage is $88.5 \%(400 / 450)$ which requires 2.2 time constants. The time constant is 50 ms (from time-constant nomogram A), so the time required to charge to 400 V is 110 ms .


## FREQUENCY SELECTIVE NETWORK NOMOGRAM

The expression $f=1 / 2 \pi R C$, where $f$ is in hertz, $C$ and $R$ in ohms, is the expression for:

1. The 3-dB bandwidth of a single tuned circuit having parameters as shown in Figure 1.
2. The frequency at 3 dB relative attenuation of the parallel RC low-pass network shown in Figure 2.
3. The frequency at 3 dB relative transfer attenuation of the series RC high-pass network of Figure 3.
4. Wien bridge balance.

FOR EXAMPLE:

1. The circuit shown in Figure 1 is used to couple two successive stages of an amplifier. The 3-dB bandwidth of the circuit must be 3.4 MHz and the equivalent shunt capacitance of the circuit is 25 pF . What equivalent resonant resistance will the circuit exhibit? Connect 3.4 MHz and 25 pF and find the equivalent resonant resistance as 1,850 ohms.
2. The low-pass network of Figure 2 uses a $0.05-\mu \mathrm{F}$ capacitor. What value of resistance is required for the output to drop to 0.707 of the input at 5 kHz ? Connect $0.05-\mu \mathrm{F}$ with 5 kHz and read answer as 620 ohms.


Figure 1. Characteristics of a single tuned circuit.


Figure 2. Characteristics of a parallel RC low-pass network.


Figure 3. Transfer characteristics of an RC high-pass network.
3. It is required that the RC high-pass network in Figure 3 attenuate rapidly below 300 Hz . What value resistor must be used with a $0.1-\mu \mathrm{F}$ capacitor? Connect $0.1-\mu \mathrm{F}$ with $300 \mathrm{~Hz}(0.3 \mathrm{kHz})$ and read answer as 5,250 ohms.
4. Figure 4 shows an RC coupled amplifier and its equivalent circuits. It is assumed that the reactance of the bypass capacitors is negligible throughout the frequency range of the amplifier. If the equivalent circuit resistance has a value of 1,300 ohms and the equivalent capacitance is 25 pF , at what frequency is the amplification 0.707 of the midfrequency range of the amplifier? Connect 25 pF and 1,300 ohms and read frequency of 4.75 MHz at which amplifier gain is down 3 dB .
5. The Wien bridge circuit shown in Figure 5 has $R_{1}$ and $R_{2}$ equal to 10,000 ohms and $C_{1}$ and $C_{2}$ equal to $0.1-\mu \mathrm{F}$. With those values the balance frequency of the circuit is 1.59 kHz .

$$
\begin{aligned}
& R_{1}=R_{2}=R \\
& C_{1}=C_{2}=C \\
& \frac{R_{3}}{R_{4}}=2
\end{aligned}
$$

For the measurement of frequency, the unknown frequency is connected across A and B and a null detector, across C and D.

When used with an oscillator, the circuit is connected to a suitable amplifier with regenerative feedback.



Figure 5. Conventional Wien bridge circuit.

Figure 4. An RC-coupled amplifier and its equivalent circuits.


Figure 4. Circuit Diagram of N-Channel JFET Transistor Amplifer. (Continued from page 111.)


Note: Scales with corresponding letters (A or B) are used together.

## BANDWIDTH NOMOGRAM

This nomogram is used to compute the bandwidth of a tuned circuit at $70.7 \%(-3 \mathrm{~dB})$ of maximum gain. It is based on the equation

$$
\Delta f=\frac{f_{r}}{Q}
$$

where
$\Delta f=$ bandwidth in kilohertz
$f_{r}=$ resonant frequency in megahertz
$Q=$ figure of merit of the inductance

## FOR EXAMPLE:

1. A circuit that has a resonant frequency of 6 MHz , and uses an inductance with a $Q$ of 140 , will have a bandwidth of 43 kHz . NOTE: The range of the nomogram can be extended to cover other frequencies by multiplying or dividing both frequency scales by the same power of 10 .
2. To achieve a bandwidth of 2.5 kHz at a resonant frequency of 600 kHz the inductance must have a $Q$ of 240.
$f_{r}$
( $\mathrm{MHz}_{\mathrm{z}}$ )





Crossover curves showing 6,12, and 18 dB /octave crossover net work cutoff rate
(Reprinted from Radio-Eloctronics, copyright © Garnsback Publications, Inc., March, 1968.)

## PASSIVE LC FILTER DESIGN

Previous editions of the Electronic Databook used nomograms to determine the component values of image parameter lowpass and highpass filters. This edition provides computer-calculated tabulations of modern filter designs that are based on network synthesis. These modern designs are more versatile, less complicated and easier to build than the old image parameter designs. For example, to simplify construction, the tabulated modern filter designs require fewer components than comparable image parameter designs, and all (or most) of the capacitor values of the modern filter designs are standard values.

Most filtering applications do not require a precisely defined cutoff frequency, and as long as the actual cutoff frequency is within about five percent of the desired cutoff frequency, and the passband and stopband attenuation levels are satisfactory, the design will be acceptable. Of almost equal importance is finding a design that has the minimum number of components and that requires standard-value capacitors to simplify the ordering of parts and the assembly of the filter. Standard values for the inductors is less important because the inductors are usually hand-wound or ordered to specification from inductor manufacturers.

Each filter table provides many designs over one frequency decade in which the change in cutoff frequency from one design to the next is sufficiently small so that virtually any cutoff requirement can be satisfied within a few percent. The 50 -ohm impedance level for source and load was used for most of the tabulations because this impedance termination is most frequently needed by the electronics engineer. All component values and frequencies versus selected stopband attenuation levels have been computer-calculated for each design for the convenience of the user. Although the tabulated designs are only for the equally terminated condition at the listed impedance level and frequency decade, a simple scaling procedure allows the tables to be scaled to any equally terminated impedance level and any frequency decade, while keeping the important advantage of all designs requiring only standard-value capacitors. These pre-calculated filter tables are therefore universally applicable because they can be used to select a suitable design having standard-value capacitors for any impedance level or any cutoff frequency.

Only the passive LC filter was considered for tabulation because this filter type is capable of passing rf power, whereas the active filter is not. Also, the passive filter does not require a power supply, and it usually is easier to assemble in small quantities than the active filter.

## Filter Types and Responses

Only the lowpass and highpass filter types having the Chebyshev or elliptic attenuation responses are considered. For design information on other filter types (bandpass, bandstop, etc.), and responses (Butterworth, Bessel, etc.), see References 13-18. Only the 5th- and 7th-degree Chebyshev designs ( 5 and 7 elements each, respectively) and the 5th-degree elliptic design are included in the tables because these designs are suitable for almost all of the non-stringent filtering requirements encountered by the non-professional filter designer.

The Chebyshev attenuation response is characterized by attenuation ripples in the passband and a constantly (monotonic) increasing attenuation in the stopband. The level of maximum passband ripple ( $A_{p}$ ) is directly related to the filter reflection coefficient (RC) and VSWR (see Appendix A), and these parameters can be increased or decreased to get a corresponding increase or decrease in the rate of attenuation rise in the filter stopband in the vicinity of the filter cutoff frequency.

The elliptic attenuation response is characterized by attenuation ripple in the passband, attenuation peaks in the stopband, and a specific level of minimum stopband attenuation. The presence of the two resonant circuits in the elliptic filter configuration results in a more abrupt rise in attenuation than is possible with the Chebyshev configuration.

[^0]
## Filter Tables

Lowpass and highpass filter designs are listed in ten tables, with eight tables based on a 50 ohm impedance level, and two tables ( 5 B and 8 B ) based on 600 ohms. The schematic diagram and a typical attenuation response of each tabulated filter appears at the head of each table, except Tables $5 B$ and $8 B$, where the only difference is the impedance level. The component designations in the schematic diagram and the frequency designations ( $F_{c 0^{\prime}} F_{3}$, F20 and F50) in the attenuation response diagram correspond to similar designations in the table column headings.

Although there is passband ripple in all these designs, the amplitude of the ripple is so small that it is usually swamped out by the losses of the filter components. Consequently, when the completed design is measured, the passband response appears to be flat. For this reason, the passband in the response diagrams is shown flat.

The filter reflection coefficient (RC) provides an indication of the flatness of the passband and the VSWR of the filter. For if filtering applications where low VSWR is desired, designs with low reflection coefficients are preferred. For audio filtering applications, where a faster rise of attenuation is more important than minimizing VSWR, designs having high RC values are preferred.

## Lowpass Filters

Chebyshev Designs and Applications. Tables 1 through 4 list 5-and 7 -element Chebyshev lowpass designs. Use the 5 -element designs when about 30 dB of attenuation is needed at one octave above the cutoff frequency, and the filter component count must be minimized. Use the 7 -element designs when about 42 dB of attenuation is needed at one octave above the cutoff frequency. A typical application for these filters is to reduce the harmonic output of transistor amplifiers. Normally, the capacitive input/output configurations shown in Figures 1 and 3 are preferred to the altemative inductive input/output configurations in Figures 2 and 4 to minimize the number of inductors. Inductors are usually more bulky, more expensive and have higher losses than capacitors. Both filter types have identical attenuation responses, but the filter input impedances in the stopbands are markedly different. For the inductive input filter, the input impedance starts increasing between the 3 and $15-\mathrm{dB}$ attenuation level, and continues increasing with increasing stopband frequency. The reverse is true for the capacitive input filter. Under certain conditions, transistor if amplifiers may become unstable when looking into a decreasing or increasing reactive impedance (see Bibliography, Nos. 8 \& 15). Because of this, it is necessary that the rf filter designer be able to design lowpass filters having either capacitive or inductive input elements.

Elliptic Designs and Applications. Tables 5A and 5B list 5th-degree elliptic lowpass designs for 50 and 600 ohms, respectively. This type of filter is preferred where a more abrupt rise in attenuation is desired. This type is also useful because the attenuation peaks at F4 and F2 sometimes can be placed at the second and third harmonic frequencies of a constant-frequency if amplifier to provide more than 60 dB attenuation to the harmonics.

In this filter type, only capacitors C1, C3 and C5 are standard value. The fact that C2 and C4 are not standard values is not important because these capacitors should be tuned to precisely resonate L2 and L4 at F2 and F4. This is necessary if the minimum stopband attenuation level $\left(A_{s}\right)$ is to be achieved throughout the entire stopband. A slight variation in the values of C2, L2 and C4, L4 is not important as long as the F2 and F4 frequencies are as close as possible to the tabulated frequencies.

Table 5B is provided for audio filtering applications where this impedance level is very common. This table also serves to provide 600 -ohm designs that can be used to confirm the correctness of the impedance scaling procedure to be explained later.

## Highpass Filters

Chebyshev Designs and Applications. Tables 6 and 7 list 5-and 7 -element Chebyshev highpass filter designs, but unlike the lowpass designs only the capacitive input/output configuration is considered. This is because they are very few applications for the altemate L-input/output configuration. The C-input/output configuration has the important advantage of increasing input impedance with decreasing frequency. This configuration is therefore suitable as an isolation network between a signal source and a detection system being used to examine the harmonics of the signal source fundamental. The highpass filter passes the harmonic frequencies unattenuated,
but provides considerable attenuation to the fundamental signal. Also, the high input impedance of the filter will not cause excessive loading of the generator. This is not true for the alternate inductive input filter.

Elliptic Designs and Applications. Tables 8A and 8B list the 5th-degree elliptic highpass designs for 50 and 600 ohms, respectively. This type filter is preferred where a more abrupt increase in attenuation is desired as compared to the Chebyshev filter. The comments concerning the elliptic lowpass design relative to $\mathrm{C} 1, \mathrm{C} 3$ and C 5 being standard values and the importance of tuning C 2 and C 4 to F 2 and F 4 are equally applicable here. The concluding comments about the elliptic 600 -ohm lowpass filter are equally applicable to the highpass filter.

## How to Use the Precalculated Design Tables

For 50-0hm Impedance Levels. Before selecting a suitable filter design, the reader must know or be able to specify the important parameters of the filter, such as type (highpass or lowpass), cutoff frequency, impedance level, and an approximation of the required stopband attenuation. It is obvious as to which tables to use for lowpass or highpass applications, but it is not so obvious as to which one design of the many possible choices is optimum for the intended application. Generally, the Chebyshev is preferred over the elliptic because the Chebyshev does not require tuning of the inductors; however, if the gradual rise in attenuation of the Chebyshev is not satisfactory, then the elliptic should be considered. For audio frequency filtering, the elliptic designs with high values of RC are preferred because they have a much more abrupt rise in attenuation as compared to the Chebyshev. For if applications, RC values less than $8 \%$ are recommended to minimize VSWR. Low VSWR is also important when cascading high and lowpass designs to achieve a bandpass response of more than two octaves wide. Each filter will operate as expected if it is correctly terminated, but this condition will exist only if both designs have the relatively constant terminal impedance that is associated with low values of RC.

Knowing the filter type and the response needed, the table of designs most appropriate for the application is selected on a trial basis. Find the table and search the cutoff frequency column for a cutoff frequency nearest the desired cutoff frequency. After finding a possible design, examine the stopband attenuation levels to see if they are satisfactory. Then check the RC value to see if it is appropriate for the application. Finally, check the component values to see if they are convenient. Usually, it is easier to obtain capacitors with the ten-percent tolerance than the five-percent value. For example, in the audio frequency range, the capacitor values will probably be in the microfarad range, and capacitors in this size are available only in the ten-percent tolerance group.

Because all the important parameters of each design are listed, it is possible to quickly check many designs so the most suitable design can be selected. After the final choice has been made, interconnect the components in accordance with the schematic diagram above the table headings. Use good engineering practices in assembling the filter components as explained in listing number 12 of the bibliography.

For Impedance Levels Other Than 50 Ohms. All tabulated designs are easily scaled to impedance levels other than 50 ohms while maintaining the advantage of standard-value capacitors. If the impedance level differs from fifty ohms by a factor equal to an integral power of ten (such as .01, 1, 10 or 100), the design tables can be scaled by inspection (by shifting the decimal points of the component values). The tabulated frequency, $A_{\mathrm{s}}$ and RC values remain unchanged. For example, if the 50 -ohm impedance level is raised by a factor of ten to $500^{\circ}$ ohms, the new capacitance and inductance values are found by multiplying the tabulated inductance values by ten, and by dividing the capacitor values by ten. This means that the decimal points of the inductor values are shifted one place to the right, and the decimal points of the capacitor values are shifted one place to the left. The reverse is true if the impedance level is reduced from 50 to 5 ohms. For example, the impedance level of Design \#1, Table 1, can be increased to 500 ohms by shifting the decimal points of $L 2$ and $L 4$ one place to the right (to become $107.3 \mu \mathrm{H}$ ), and by shifting the decimal points of the capacitance values one place to the left (to become 300 pF and 560 pF ).

To change the tabulated frequency decades to another frequency decade differing by a factor equal to an integral power of ten, multiply all tabulated frequencies by the factor, and divide all capacitance and inductance values by the same factor. For example, the frequency decade of Table 1 can be reduced from $1-10 \mathrm{MHz}$ to $1-10$ kHz by multiplying all frequencies by .001 (the frequency units in the column headings become kHz ), and by
dividing the capacitance and inductance values by the same factor. (The units of capacitance and inductance become nanofarads and millihenries.)

Filter designs with standard-value capacitors may be found for impedance levels that differ from 50 ohms by a factor equal to a non-integral power of ten (such as 1.2, 12, etc.). To do this, use the following procedure:

1. Calculate the scaled impedance factor, $R=Z_{x} / 50$ where $Z_{x}$ is the desired new impedance level in ohms.
2. Calculate the cutoff frequency of a "trial" 50 -ohm filter using the equation: $F_{50}=R \cdot F_{x_{c \infty}}$ where $F_{x_{\infty}}$ is the desired cutoff frequency of the filter at the new impedance level.
3. From the 50 -ohm tables, select a design having its cutoff frequency closest to the calculated $\mathrm{F}_{50}$ value. The tabulated capacitor values will be used directly, and the frequencies and inductance values will be scaled.
4. Calculate the exact values of $F_{x_{\infty}}=F_{50}^{\prime} / R$, where $F_{50}^{\prime}$ is the tabulated cutoff frequency. In a similar manner, calculate all the other frequencies.
5. Calculate the new inductance values for the new filter from $L_{x}=R^{2} \cdot L_{50}$, where $L_{50}$ is the tabulated inductance value of the trial filter design, and $L_{x}$ is the inductance value of the scaled filter.

An example follows showing how the 50 -ohm design \#3 of Table 5A can be replaced with a 60 -ohm design having a similar cutoff frequency and other similar characteristics. Using the same previously numbered steps:

1. $R=60 / 50=1.2$
2. $F_{50_{\infty}}=1.2(1.06 \mathrm{MHz})=1.272 \mathrm{MHz}$
3. From Table 5A, design \#15 has a cutoff frequency closest to the calculated $F_{50}$ value. The $A_{s}$ and $R C$ values are similar to design \#3. Design \#28 is also suitable as a replacement. The tabulated capacitor values of design \#15 are copied directly. Thus, C1, 3,5,2 and $4=2,200,3,900,1,800,271$ and 779 pF , respectively.
4. The exact values of $F_{x_{c o}}, F_{x_{3}}$ and $F_{A_{s}}$ are calculated, and are equal to: $1.27 \mathrm{MHz} / 1.2=1.058 \mathrm{MHz}, 1.45$ $\mathrm{MHz} / 1.2=1.208 \mathrm{MHz}$ and $2.17 \mathrm{MHz} / 1.2=1.808 \mathrm{MHz}$.
5. The $L 2$ and $L 4$ inductance values of the 60 ohm filter are calculated: $L_{2}{ }_{x}=(1.2)^{2} \cdot 7.85 \mu \mathrm{H}=11.3 \mu \mathrm{H}$, $L 4_{x}=(1.2)^{2} \cdot 6.39 \mu \mathrm{H}=\mathrm{H}=9.20 \mu \mathrm{H}$. The validity of the scaling procedure can be confirmed by scaling the new 60 -ohm filter to an impedance level of 600 ohms , and scaling the frequency from 1 MHz to 1 kHz , and then comparing the $600-\mathrm{ohm}, 1 \mathrm{kHz}$ filter with design \#5 of Table 58. All parameters of the designs will be identical, thus confirming the correctness of the scaling procedure.

The validity of the pre-calculated tables may be confirmed by independently calculating the component values using previously published normalized tables from authoritative sources such as References 8-10 and 13 . This is done by finding a tabulated pre-calculated design that has a reflection coefficient nearly identical to that of a published normalized design. For example, design \#80, Table 3 is suitable to match a $10 \%$ RC Chebyshev design. The pre-calculated impedance level and the cutoff frequency are then used with the normalized values, and the inductance and capacitance component values are calculated in the usual manner. Because the pre-calculated tabulated values agree within less than $1 \%$ variation with the independently calculated values, the correctness of the tables is confirmed.

## APPENDIX A

Equations and Table Relating RC, $A_{p}$ and VSWR for all Modern Design Filters
$R C_{(F)}=100 * \operatorname{SQR}[1-(0.1 \uparrow x)]$
where 100 *SQR $=100$ times the square root of...
$x=0.1\left(A_{p}\right)$
$t=$ symbol for exponentiation

* = symbol for multiplication

$$
\begin{equation*}
A_{P_{(d B)}}=-4.3429 * \operatorname{LOG}[1-(.01 * \mathrm{RC}) \uparrow 2] \tag{2}
\end{equation*}
$$

VSWR $=[1+(.01 * R C)] /[1-(.01 * R C)]$
where $\quad A_{p}=$ Maximum passband ripple amplitude in $d B$
RC $=$ Reflection coefficient in percent
VSWR = Voltage standing wave ratio

Equations 1-3 are presented in a format suitable for computer programming. The LOG function in Eq. (2) is based on the natural log.

Table 1. Reflection Coefficient with Corresponding Values of $A_{p}$ and VSWR.

| REFLECTION COEFFICIENT (\%) | MAX. RIPPLE AMPLITUDE (dB) | MAX. VSWR -.-- | REFLECTION COEFFICIENT <br> (\%) | MAX. RIPPLE AMPLITUDE (dB) | MAX. <br> VSWR <br> ------ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1.0 | 0.000434 | 1.020 | 12.0 | 0.0630 | 1.273 |
| 2.0 | 0.001738 | 1.041 | 14.0 | 0.0860 | 1.326 |
| 3.0 | 0.003910 | 1.062 | 16.0 | 0.1126 | 1.381 |
| 4.0 | 0.006954 | 1.083 | 18.0 | 0.1430 | 1.439 |
| 5.0 | 0.010871 | 1.105 | 20.0 | 0.1773 | 1.500 |
| 6.0 | 0.015663 | 1.128 | 22.0 | 0.2155 | 1.564 |
| 7.0 | 0.021333 | 1.151 | 24.0 | 0.2576 | 1.632 |
| 8.0 | 0.027884 | 1.174 | 26.0 | 0.3040 | 1.703 |
| 9.0 | 0.035321 | 1.198 | 28.0 | 0.3546 | 1.778 |
| 10.0 | 0.043648 | 1.222 | 30.0 | 0.4096 | 1.857 |

## References

The first four references are recommended as authoritative sources on image parameter passive LC filter design.
References 5 through 18 are recommended as authoritative sources on passive LC modem filter design.

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Figure 1. Lowpass filter schemetic diagram and attenuation response, capacitive input and output.
Table $1.50-0 \mathrm{hm}$ 5-Element Chebyshev Lowpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output.
(Continued on page 124.)

| Filter - . . . - Frequency (MHz) - - - - |  |  |  |  | RC <br> (\%) | C1, C5 (pf) | $\begin{aligned} & \text { L2, L4 } \\ & (\mu \mathrm{H}) \end{aligned}$ | $\begin{gathered} \mathrm{C} 3 \\ (\mathrm{pF}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Cutoff | 3-dB | 20-dB | 50-dB |  |  |  |  |
| 1 | 1.016 | 1.209 | 1.652 | 3.038 | 9.58 | 3000 | 10.73 | 5600 |
| 2 | 1.101 | 1.320 | 1.809 | 3.334 | 8.93 | 2709 | 9.882 | 5100 |
| 3 | 1.039 | 1.371 | 1.944 | 3.657 | 4.06 | 2200 | 9.818 | 4700 |
| 4 | 1.146 | 1.409 | 1.951 | 3.618 | 7.19 | 2400 | 9.373 | 4700 |
| 5 | 1.127 | 1.496 | 2.125 | 4.0102 | 3.88 | 2000 | 9.003 | 4360 |
| 6 | 1.256 | 1.541 | 2.133 | 3.955 | 7.27 | 2200 | 8.564 | 4300 |
| 7 | 1.054 | 1.619 | 2.379 | 4.566 | 1.39 | 1690 | 8.351 | 3900 |
| 8 | 1.232 | 1.646 | 2.344 | 4.420 | 3.67 | 1800 | 8. 187 | 3900 |
| 9 | 1.388 | 1.701 | 2.353 | 4.360 | 7. 38 | 2060 | 7.754 | 3900 |
| 10 | 1.169 | 1.756 | 2.570 | 4.922 | 1.60 | 1500 | 7.703 | 3600 |
| 11 | 1.275 | 1.771 | 2.547 | 4.830 | 2.77 | 1600 | 7.635 | 3600 |
| 12 | 1.452 | 1.825 | 2.542 | 4.731 | 6.30 | 1800 | 7.281 | 3600 |
| 13 | 1.430 | 1.939 | 2.773 | 5.241 | 3.29 | 1500 | 6.960 | 3300 |
| 14 | 1.541 | 1.971 | 2.768 | 5.179 | 5.16 | 1600 | 6.789 | 3300 |
| 15 | 1.315 | 2.101 | 3.108 | 5.989 | 1.07 | 1200 | 6.424 | 3000 |
| 16 | 1.481 | 2.117 | 3.065 | 5.836 | 2.26 | 1300 | 6.393 | 3006 |
| 17 | 1.754 | 2.190 | 3.050 | 5.677 | 6.30 | 1500 | 6.067 | 3000 |
| 18 | 1.887 | 2.252 | 3.080 | 5.669 | 9.33 | 1600 | 5.773 | 3000 |
| 19 | 1.506 | 2.337 | 3.440 | 6. 611 | 1.29 | 1100 | 5.782 | 2700 |
| 20 | 1.706 | 2.361 | 3.396 | 6.441 | 2.77 | 1200 | 5.726 | 2700 |
| 21 | 1.868 | 2.483 | 3.383 | 6.336 | 4.93 | 1300 | 5.573 | 2700 |
| 22 | 1.753 | 2. 6.34 | 3.854 | 7.383 | 1.60 | 1000 | 5.135 | 2400 |
| 23 | 1.985 | 2.671 | 3.810 | 7.193 | 3.49 | 1100 | 5.049 | 2400 |
| 24 | 2.193 | 2.737 | 3.813 | 7.096 | 6.30 | 1200 | 4.854 | 2400 |
| 25 | 2.462 | 2.838 | 3.865 | 7.094 | 10.21 | 1390 | 4.549 | 2400 |
| 26 | 1.892 | 2.872 | 4.210 | 8.073 | 1.50 | 910 | 4.799 | 2200 |
| 27 | 2.145 | 2.989 | 4.159 | 7.861 | 3.29 | 1000 | 4.640 | 2200 |
| 28 | 2.392 | 2.986 | 4.159 | 7.741 | 6.30 | 1190 | 4.449 | 2200 |
| 29 | 2.053 | 3.157 | 4.639 | 8.906 | 1.38 | 820 | 4.283 | 2000 |
| 35 | 2.362 | 3.201 | 4.575 | 9.646 | 3.31 | 916 | 4.217 | 2000 |
| 31 | 2.6.31 | 3.284 | 4.575 | 8.515 | E. 30 | 1000 | 4.945 | 2000 |

Table 1. 50 -Ohm 5-Element Chebyshev Lowpass Filter designs Using Standard-Value Capacitors, Capacitive Input and Output. (Continued from Page 123.)

| Filter --- - Frequency (MHz) - - . . |  |  |  |  | RC | C1, C5 | L2, L4 | C3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Cutoff | 3-dB | $20-\mathrm{dB}$ | $50-\mathrm{dB}$ | (\%) |  | $(\mu \mathrm{H})$ | (pF) |
| 32 | 2.338 | 3.512 | 5.139 | 9.843 | 1.60 | 750 | 3.851 |  |
| 33 | 2.628 | 3.557 | 5.083 | 9.603 | 3.34 | 826 | 3.794 | 1800 |
| 34 | 2.960 | 3.664 | 5.089 | 9.453 | 6.76 | 910 | 3.614 | 1806 |
| 35 | 2.705 | 3.959 | 5.763 | 11.01 | 1.92 | 680 | 3.418 | 1609 |
| 36 | 3.058 | 4.027 | 5.710 | 10.74 | 4.10 | 750 | 3.346 | 1600 |
| 37 | 3. 381 | 4.145 | 5.734 | 10.63 | 7.35 | 820 | 3.182 | 1600 |
| 38 | 2. 772 | 4.212 | 6.176 | 11.84 | 1.49 | 620 | 3.211 | 1500 |
| 39 | 3.135 | 4.265 | 6.101 | 11.54 | 3.22 | 680 | 3.166 | 1500 |
| 40 | 3.508 | 4.379 | 6.100 | 11.35 | 6.30 | 750 | 3.633 | 1500 |
| 41 | 3.391 | 4.881 | ?.079 | 13.49 | 2.15 | 560 | 2.772 | 1309 |
| 42 | 3.838 | 4.979 | 7.026 | 13.18 | 4.62 | 620 | 2.695 | 1300 |
| 43 | 4.259 | 5.147 | 7.080 | 13.08 | 8.32 | 680 | 2.545 | 1300 |
| 44 | 3.607 | 5.279 | 7.684 | 14.6 ? | 1.92 | 510 | 2. 563 | 1200 |
| 45 | 4.056 | 5.364 | ?.614 | 14.33 | 3.98 | 560 | 2.509 | 1206 |
| 46 | 4.550 | 5.545 | 7.654 | 14.17 | 7.72 | 620 | 2.372 | 1200 |
| 47 | 3.963 | 5.762 | 8.376 | 15.98 | 2.61 | 470 | 2.348 | 1100 |
| 48 | 4.391 | 5.843 | 8.309 | 15.66 | 3.80 | 510 | 2.305 | 1100 |
| 49 | 4.881 | 6.012 | 8.334 | 15.46 | 7.05 | 560 | 2.198 | 1100 |
| 50 | 4.398 | 6.344 | 9.265 | 17.55 | 2.12 | 430 | 2.133 | 1000 |
| 51 | 4.987 | 6.448 | 9.135 | 17.18 | 4.18 | 470 | 2.085 | 1006 |
| 52 | 5.380 | 6.618 | 9.169 | 17.01 | 7. 13 | 510 | 1.996 | 1006 |
| 53 | 4.811 | 6.968 | 10.12 | 19.30 | 2.06 | 390 | 1.942 | 910 |
| 54 | 5.426 | 7.095 | 10.04 | 18.86 | 4.34 | 430 | 1.894 | 910 |
| 55 | 5.997 4.862 | 7.311 | 10.89 | 18.68 | 7.79 | 470 | 1.799 | 910 |
| 56 | 4.862 | 7.690 | 11.36 | 21.86 | 1.14 | 330 | 1.756 | 820 |
| 57 | 5.511 | 7.758 | 11.20 | 21.28 | 2.51 | 360 | 1.743 | 820 |
| 58 | 6.066 | 7.887 | 11.14 | 20.90 | 4.54 | 390 | 1.702 | 820 |
| 59 | 6.771 | 8.169 | 11.23 | 20.73 | 8.44 | 430 | 1.602 | 820 |
| 60 | 5.262 | 8.464 | 12.43 | 23.95 | 1.07 | 300 | 1.606 | 750 |
| 61 | 6.642 | 8.485 | 12.24 | 23.25 | 2.56 | 330 | 1.594 | 750 |
| 62 | 6.702 | 8.645 | 12.18 | 22.82 | 4.83 | 360 | 1.550 | 750 |
| 63 | 7.332 | 8.897 | 12.26 | 22.66 | 8.93 | 390 | 1.475 | 750 |
| 6.4 | 6.687 | 9.363 | 13.49 | 25.62 | 2.61 | 309 | 1.444 | 680 |
| 65 | 7.484 | 9.565 | 13.43 | 25.13 | 5.29 | 330 | 1.398 | 680 |
| 66 | 8.254 | 9.896 | 13.57 | 25.00 | 8.93 | 360 | 1.317 | 680 |
| 68 | 8. 181 | 10.48 | 14.82 14.73 | 28.20 | 2.35 | 276 | 1.320 | 626 |
| 69 | 9.109 | 10.88 | 14.90 | 27.43 | 9.22 | 330 | 1.195 | 629 |
| 70 | 7.818 | 11.32 | 16.45 | 31.37 | 2.06 | 240 | 1.195 | 560 |
| 71 | 9.021 | 11.59 | 16.31 | 36.54 | 4.98 | 270 | 1.155 | 560 |
| 72 | 10.16 | 12.89 | 16.52 | 30.38 | 9.58 | 304 | 1.073 | 560 |
| 73 | 8.659 | 12.44 | 18.04 | 34.38 | 2.17 | 220 | 1.087 | 510 |
| 74 | 9.636 | 12.65 | 17.91 | 33.67 | 4.22 | 240 | 1. 1.663 | 510 |
| 75 | 9.224 | 13.48 | 19.61 | 37.45 | 1.94 | 200 | 1.003 | 470 |
| 76 | 10.39 | 13.71 | 19.44 | 36.57 | 4.06 | 220 | 0.981 | 470 |
| 78 | 9.851 | 14.71 | 21.50 | 41.14 | 1.67 | 180 | 0.919 | 436 |
| 78 | 10.54 | 16.19 | 23.79 | 45.66 | 1.39 | 160 | 0.835 | 390 |



Figure 2. Lowpass filter schematic diagram and attenuation response, inductive input and output.
Table 2. 50-Ohm 5-Element Chebyshev Lowpass Fitter Designs Using Standard-Value Capacitors, Inductive Input and Output. (Continued on page 126.)

| Filter No. | Frequency (MHz) - . . . . |  |  | $50-\mathrm{dB}$ | RC <br> (\%) | $\begin{array}{r} \mathrm{L}, \mathrm{~L}, \mathrm{~L} \\ (\mu \mathrm{H}) \end{array}$ | $\begin{gathered} \mathrm{C} 2, \mathrm{C} 4 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{aligned} & \mathrm{L} 3 \\ & (\mu \mathrm{H}) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cutoff | 3-dB | $20-\mathrm{dB}$ |  |  |  |  |  |
| 1 | 0.74 | 1.15 | 1.69 | 3.25 | 1.32 | 5.6 | 4700 | 13.72 |
| 2 | 0.90 | 1.26 | 1.81 | 3.44 | 2.67 | 5.6 | 4300 | 12.66 |
| 3 | 1.86 | 1.38 | 1.94 | 3.64 | 4.60 | 5.6 | 3900 | 11.75 |
| 4 | 1.19 | 1.47 | 2.05 | 3.82 | 6.47 | 5.6 | 3600 | 11.15 |
| 5 | 1.32 | 1.58 | 2.17 | 4.69 | 8.76 | 5.6 | 3300 | 10. 61 |
| 6 | 0.91 | 1.39 | 2.03 | 3.90 | 1.47 | 4.7 | 3900 | 11.38 |
| 7 | 1.03 | 1. 50 | 2.16 | 4.10 | 2.71 | 4.7 | 3606 | 10.60 |
| 8 | 1.25 | 1.63 | 2.30 | 4.32 | 4.42 | 4.7 | 3301 | 9.92 |
| 9 | 1.42 | 1.77 | 2.46 | 4.56 | 6.65 | 4.7 | 3000 | 9.32 |
| 16 | 1. 61 | 1.92 | 2.63 | 4.84 | 9.47 | 4.7 | 2700 | 0.79 |
| 11 | 1.05 | 1.64 | 2.41 | 4.64 | 1.22 | 3.9 | 3300 | 9.63 |
| 12 | 1.29 | 1.80 | 2.60 | 4.93 | 2.64 | 3.9 | 3000 | 8.83 |
| 13 | 1.54 | 1.95 | 2.30 | 5.25 | 4.73 | 3.9 | 2700 | 8.15 |
| 1.4 | 1. 89 | 2.19 | 3.03 | 5.61 | 7.59 | $3 \times 9$ | 2406 | 7.57 |
| 15 | 1.99 | 2.35 | 3.21 | 5.89 | 10.010 | 3.5 | 2200 | 7.23 |
| 16 | 1.34 | 2.00 | 2.93 | 5.51 | 1.E6 | 3.3 | 2700 | 7.89 |
| 17 | 1. 68 | 2.25 | 3.20 | 6.93 | 3.69 | 3.3 | 2400 | 7.15 |
| 18 | 1.92 | 2.43 | 3.40 | 6.34 | 5.59 | 3.3 | 2200 | 6.72 |
| 19 | $2 \cdot 16$ | 2. 63 | 3.62 | 6.69 | 7.99 | 3.3 | 2006 | 6.35 |
| 28 | 2.43 | 2.85 | 3.87 | 7.09 | 10.98 | 3.3 | 1800 | 6.92 |
| 21 | 1.E6 | 2.46 | 3.59 | 6.87 | 1.72 | 2.7 | 2200 | 6.43 |
| 22 | 1.99 | 2.70 | 3.86 | 7.29 | 3.33 | 2.7 | 2006 | 5.93 |
| 23 | 2.34 | 2.97 | 4.15 | $7 \times 75$ | 5.59 | $2 \times 7$ | 1800 | 5.50 |
| $\geq 4$ | 2.71 | 3.27 | 4.49 | 8.28 | 8.61 | 2.7 | 1600 | 5.13 |
| 25 | 2.92 | 3.44 | 4.63 | 8.58 | 10.44 | 2.7 | 1500 | 4.97 |

Table 2. $50-0 \mathrm{hm}$ 5-Element Chebyshev Lowpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output. (Continued from Page 125.)

| Filter <br> No. | Cutoff | (MHz)3-dB | 20-dB | $50-\mathrm{dB}$ | $\begin{aligned} & \mathrm{RC} \\ & (\%) \end{aligned}$ | $\begin{gathered} \text { L1, L5 } \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \mathrm{C} 2, \mathrm{C} 4 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{aligned} & \mathrm{LB}_{2} \\ & (\mu \mathrm{H}) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |
| 26 | $2 \times 1$ | 3.01 | 4.35 | 8.41 | 1.6E | 2.2 | 1800 | 5.26 |
| 27 | $2 \times 52$ | 3.37 | 4.80 | 9.04 | 3.69 | 2.2 | 1600 | 4.76 |
| 28 | 2.78 | 3.57 | 5.62 | 9.39 | 5.07 | 2.2 | 1500 | 4.55 |
| 29 | 3.34 | 4.02 | 5.52 | 10.18 | 8.68 | 2.2 | 1309 | 4.18 |
| 36 | 3.65 | 4.28 | 5.80 | 10.63 | 10.98 | 2.2 | 1200 | 4.01 |
| 31 | 2.35 | 3.61 | 5.29 | 10.16 | 1.41 | 1.8 | 1500 | 4.38 |
| 32 | 3.12 | 4.14 | 5.89 | 11.10 | 3.83 | 1. 8 | 1300 | 3.88 |
| 33 | 3.51 | 4.45 | 6.23 | 11.63 | 5.59 | 1.8 | 1206 | 3.67 |
| 34 | 3.93 | 4.78 | 6.60 | 12.21 | 7.78 | 1.8 | 1100 | 3.48 |
| 35 | 4.37 | 5.16 | 7.01 | 12.86 | 10.44 | 1.8 | 1006 | 3.31 |
| 36 | 3.10 | 4.51 | 6.56 | 12.51 | 2.00 | 1.5 | 1206 | 3.51 |
| 37 | 3.65 | 4.90 | 6.99 | 13.20 | 3,52 | 1.5 | 1109 | 3.27 |
| 33 | 4.21 | 5.34 | 7.47 | 13.95 | 5.59 | 1.5 | 1000 | 3.016 |
| 39 | 4.75 | 5.77 | 7.96 | 14.71 | 7.97 | 1.5 | 910 | 2.89 |
| 40 | 5.34 | 6.26 | 8.50 | 15.57 | 10.92 | 1.5 | 826 | 2.74 |
| 41 | 3.53 | 5.41 | 7.94 | 15.24 | 1.41 | 1.2 | 1060 | 2.92 |
| 42 | 4.30 | 5.94 | 8. 53 | 16.17 | 2.89 | 1.2 | 910 | 2. 68 |
| 43 | 5.09 | 6. 53 | 9.19 | 17.20 | 5.02 | 1.2 | 829 | 2. 2.49 |
| 44 | 5.73 | 7.04 | 9.75 | 18.69 | 7.18 | 1.2 | 750 | 2.35 |
| 45 | 6.42 | 7.62 | 10.39 | 19.09 | 9.87 | 1.2 | 686 | 2.23 |
| 46 | 4.40 | 6.60 | 9.65 | 18.43 | 1. 63 | 1.0 | 820 | 2.40 |
| 47 | 5.27 | 7.20 | 10.32 | 19.53 | 3.69 | 1.0 | 750 | 2.22 |
| 48 | 6.15 | 7.87 | 11.06 | 20.70 | 5.13 | 1.6 | 680 | 2. 26 |
| 49 | 6.95 | 8.51 | 11.77 | 21.81 | 7.39 | 1.0 | 620 | 1.95 |
| 50 | 7.80 | 9.22 | 12.56 | 23.05 | 10.21 | 1.0 | 560 | 1.85 |
| 51 | 5.23 | 7.96 | 11.67 | 22.38 | 1.48 | 0.82 | 680 | 1.99 |
| 52 | 6.33 | 8.72 | 12.51 | 23.70 | 2.95 | 8.82 | 620 | 1.83 |
| 53 | 7.45 | 9.56 | 13.45 | 25.18 | 5.03 | 0.82 | 560 | 1.709 |
| 54 | 8.44 | 10.35 | 14.32 | 28.55 | 7.31 | 8.82 | 510 | 1.60 |
| 55 | 9.28 | 11.05 | 15.10 | 27.76 | 9.54 | 0.82 | 470 | 1.53 |
| 56 | 6.41 | 9.66 | 14.15 | 27.16 | 1. 57 | 0.68 | 560 | 1.64 |
| 57 | 7.75 | 10.59 | 15.18 | 28.73 | 3.69 | 6. 6.6 | 510 | 1.51 |
| 58 | E.83 | 11.41 | 16.98 | 30.15 | 4.76 | 0.68 | 470 | 1.42 |
| 59 | 9.97 | 12.31 | 17.08 | 31.72 | 6.88 | 0.68 | 430 | 1.34 |



Figure 3. Lowpass filter schematic diagram and attenuation response, capacitive input and output.

Table 3. 50-ohm 7-Element Chebyshev Lowpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output.

| Filter No. | - Fr | quency | Hz) |  | RC | C1, C7 | L2, L6 | C3, C5 | L4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cutoff | 3-dB | $20-\mathrm{dB}$ | $50-\mathrm{dB}$ | (\%) | (pF) | $(\mu \mathrm{H})$ | (pF) | $(\mu \mathrm{H})$ |
| 1 | 1.037 | 1.162 | 1.401 | 2.006 | 16. 63 | 2,901 | 10.90 | 5609 | 12.57 |
| 2 | 1.047 | 1.229 | 1.511 | 2. 2666 | 3.41 | 2200 | 10.29 | 5198 | 12.29 |
| 3 | 1.118 | 1.264 | 1. 530 | 2.256 | 5.78 | 2406 | 10.04 | 5100 | 11.66 |
| 4 | 1.033 | 1.299 | 1. 6.33 | 2. 480 | 1.46 | 1890 | 9.518 | 4700 | 11.88 |
| 5 | 1. 124 | 1.329 | 1. 098 | 2. 455 | 3.12 | 2800 | 9.502 | 4700 | 11.40 |
| 5 | 1. 2118 | 1.358 | 1.658 | 2. 450 | 5.80 | 2209 | 9.270 | 4700 | 10.78 |
| $\stackrel{7}{7}$ | 1.294 | 1.423 | 1.697 | 2.434 | 9.8. | 2.406 | 8.824 | 4708 | 10.01 |
| 3 | 1.151 | 1.412 | 1.785 | 2. 331 | 1.16 | 1505 | 8. 5131 | 4390 | 10.97 |
| 9 | 1. 214 | 1. 4.446 | 1.783 | 2. 687 | 2.80 | 18918 | B. 709 | 4360 | 10.51 |
| 19 | 1.314 | 1.492 | 1.810 | 2. 6773 | 5.481 | 20010 | 8.502 | 4300 | 9.910 |
| 11 | 1.41? | 1.556 | 1.85 ? | 2.705 | 9.17 | 2.319 | 8.561 | 4306 | 9.138 |
| 12 | 1.256 | 1.56E | 1.9E7 | 2.194 | 1.51 | 15061 | 7.961 | 3960 | 9.846 |
| 13 | 1.318 | 1.58? | 1.979 | 2.468 | 2.44 | 1604 | 7.910 | 3900 | 9.617 |
| 14 | 1.449 | 1.E41 | 1.943 | 2. 951 | 5.16 | 18 BW | 7.733 | 3900 | 9.035 |
| 15 | 1. 5455 | 1.718 | 2.1949 | 2.984 | 9.88 | 26514 | 7. 298 | 3900 | 8.268 |
| $10^{\circ}$ | 1.445 | 1.726 | 2.135 | 3.216 | 2. 71 | 1569 | ?.294 | 3600 | 8.819 |
| 17 | 1.517 | 1.756 | 3.148 | 3.197 | 4.11 | 1609 | 7.219 | 3600 | 8.537 |
| 18 | 1. Ebil | 1.837 | 2. 2t1 | 3.218 | 8.119 | 1808 | 6.860 | 36001 | 7.826 |
| 19 | 1.513? | 1.8601 | 2.325 | 3. 525 | 1.82 | 1364 | 6.694 | 3300 | 8.265 |
| 28 | 1.082 | 1.329 | ㄹ.350 | 3.487 | 4.71 | 15.619 | 6.517 | 3390 | 7.721 |
| 31 | 1.767 | 1.976 | 2. 3861 | 3.49 | 15. 54 | 1640 | 6.403 | 3360 | 7.370 |
| $\therefore 2$ | 1.556 | 2.020 | 2. 560 | 8.925 | 1.612 | 1160 | E.043 | 30180 | 7.682 |
| 13 | 1.679 | 2.052 | 2. 5.518 | 3.879 | 2.114 | 1269 | 6.9188 | 3040 | 7. 472 |
| 24 | 1.786 | 2.952 | 2.5013 | 3.841 | 3. 51 | 1208 | 6. 048 | 3000 | 7.213 |
| 25 | 1.993 | 2.205 | 2.E.41 | 3.852 | 3.16 | 1549 | 5.718 | 3000 | 6.522 |
| 26 | 1. 3.45 | 2. 248 | 2.1944 | 4.35:i | 1.11 | 10619 | 5.447 | 2799 | 5.894 |
| $\therefore$ | 1.843 | 2. 289 | 2.844 | 4.391 | $\therefore .32$ | 1100 | 5, 4 ${ }^{\text {a }}$, | 27813 | 6.677 |
| 378 | 2.0 .2 | 2.341 | 2. 85, | 4.253 | 4. 11 | 1200 | 5.414 | 2790 | 6.493 |
| \% 4 | $\therefore 1.48$ | 2.409 | 2. 514 | 4.27:2 | 5.58 | 1396 | 5.258 | 2700 | 6.064 |
| 31 | $\therefore$ - 0150 | 2.539 | 3.174 | 4.87 ? | 1.35 | 918 | 4.856 | 2480 | 5.086 |
| 11 | $\because 147$ | 2. 888 | 3. 2113 | 4.815 | 2.11 | 1, 12106 | 4.363 | 2400 | 5.879 |
| 3. | $\therefore 3.13$ | $\therefore .6511$ | 3. ${ }^{\text {a }} 15$ | 4.7.95 | 4.95 | 1106 | 4.730 | 2400 | 5.586 |
| 3 | $\therefore 4^{\prime 31}$ | $\therefore 156$ | 3. 311 | 4.82, | 5.10 | 1204 | 4.513 | 2494 | 5.217 |
| 4 | $\therefore 155$ | $\therefore$ 为 | 1.4.49 | 5.336 | 1.17 | 820 | 4.442 | 2200 | 5.507 |
| 35 | .351 | $\therefore 131 \%$ | 2. 4 93 | 5. 25 | 2.58 | 418 | 4.45 cal | 2200 | 5.406 |
| 3 . | . $5,+$ | $\therefore 394$ | 3.5.5 | 5. 23.19 | 4.11 | 1050 | 4.264 | 2290 | 5.147 |
| -17 | A1i | 4. 61610 | 3. 5181 | 5. Atit | 9.10 | 11 ¢4 | 4.192 | 2200 | 4.782 |

Table 3. 50-ohm 7-Element Chebysher Lowpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output. (Continued from Page 127.)

| Filter - . . . . Frequency ( MHz ) . . . . . |  |  |  |  | RC <br> (\%) | C1, C7 (pF) | $\begin{gathered} \text { L2, L6 } \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \mathrm{C} 3, \mathrm{C} 5 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{gathered} \mathrm{L} 4 \\ (\mu \mathrm{H}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Cutoff | 3-dB | 20-dB | $50-\mathrm{dB}$ |  |  |  |  |  |
| 28 | 2.384 | 3.041 | 3.838 | 5.863 | 1.24 | 756 |  |  |  |
| 39 | 2.568 | 3.0994 | 3.840 | 5.788 | 2.43 | 829 | 4.041 | 2009 | 5.089 4.933 |
| 40 | 2.778 | 3.184 | 3.878 | 5.753 | 4.74 | 910 | 3.985 | 2060 | 4.933 4.676 |
| 42 | 2.989 | 3.307 | 3.961 | 5.792 | 8.10 | 1500 | 3.811 | 2060 | 4.378 4.348 |
| 43 | 2.686 2.889 | 3.383 3.451 | 4.264 4.271 | 6.507 | 1.31 | 689 | 3.640 | 1800 | 4.570 |
| 44 | 3.090 | 3.539 | 4.316 | 6. 5.393 | 2.1 | 750 | 3. 647 | 1800 | 4.409 |
| 45 | 3.351 | 3.695 | 4.417 | 6.44? | 8.60 | 820 | 3.585 | 1800 | 4.205 |
| 46 | 3.056 | 3.823 | 4.795 | 7.299 | 1.61 | 520 | 3.484 | 1890 | 3.871 |
| 48 | 3.300 | 3.902 | 4.811 | 7.211 | 3.09 | 689 | 3.235 | 1600 | 4.029 |
| 49 | 3.552 | 4.922 | 4.873 | 7.196 | 5.65 | 750 | 3.154 | 1609 | 3.667 |
| 50 | 3.166 | 4.186 4.051 | 4.992 | 7.272 | 9.25 | 820 | 2.995 | 1600 | 3.394 |
| 51 | 3.445 | 4.133 | 5.122 | 7.824 | 2. 57 | 560 | 3.029 | 1500 | 3.821 |
| 52 | 3.694 | 4.249 | 5.168 | 7.571 | 4. 6.4 | 680 | 3.041 | 1500 | 3.687 |
| 54 | 3.985 3.813 | 4.409 | 5.282 | 7.723 | 8.10 | 750 | 2.858 | 1508 | 3.515 |
| 55 | 4.193 | 4.717 4.819 | 5.902 5.927 | 8.955 | 1.76 | 510 | 2.636 | 1300 | 3.266 |
| 56 | 4.429 | 4.983 | 6.819 | 8.867 | 3.38 | 569 | 2. 623 | 1390 | 3.135 |
| 57 | 4.125 | 5.108 | 6.394 | 9.704 | 1.74 | 620 | 2.543 | 1300 | 2.941 |
| 58 | 4.490 | 5.202 | 6.414 | 9.615 | 3.619 | 510 | 2.433 | 1200 | 3.011 |
|  | 4.719 | 5.354 | 6.491 | 9.593 | 5.59 | 560 | 2. 369 | 12 Ab | 2.913 |
| E1 | 4.493 | 5.606 | 6.677 | 9.713 | 9.66 | 620 | 2. 232 | 1206 | 2.524 |
| 62 | 4.819 | 5.683 | 7.9180 | 10.59 | 1.72 | 430 | 2.230 | 1100 | 2.762 |
| 6.3 | 5.123 | 5.827 | 7.073 | 18.46 | 5.30 | 470 | 2.222 | 1100 | 2.663 |
| 64 | 5.516 | 6.067 | 7.245 | 10.56 | 8.93 | 560 | 2.177 | 1160 | 2.540 |
| 5 | 4.933 5.326 | 6.125 | 7.673 | 11.65 | 1. 69 | 390 | 2.027 | 1608 | 2.349 |
| 67 | 5.694 | 6.262 | 7.754 | 11.53 | 3.34 | 430 | 2.018 | 1000 | 2.413 |
| 68 | 6.017 | 6. 689 | 7.801 | 11.52 | 5.7 | 470 | 1.969 | 10010 | 2.287 |
| 69 | 5.485 | 6.749 | 8.432 | 12.78 | 1.88 | 510 | 1.879 | 1000 | 2.132 |
| 71 | 5.838 | 6.875 | 8. 464 | 12.67 | 3.27 | 390 | 1.846 | 910 | 2.275 |
| 1 | E. 288 | ?.693 | 8.581 | 12.66 | 5.91 | 436 | 1.787 | 918 | 2. 200 |
| 13 | 6.158 5.582 | ¢. 391 | 8.803 | 12.81 | 9.64 | 470 | 1.693 | 910 | 1.914 |
| -4 | 6.172 | 7.516 | 9.368 | 14.37 | 1.00 | 360 | 1.651 | 820 | 2.181 |
| 15 | 6.597 | 7.681 | 9.415 | 14.04 | 2.13 | 330 | 1.664 | 820 | 2.037 |
| 76 | 7.067 | 7.892 | 9.536 | 14.65 | E. 214 | 360 | 1. 649 | 820 | 1.958 |
| $\therefore 7$ | 6.715 | 8.298 | 10.23 | 15.48 | 2.64 | 300 | 1.522 | 820 | 1.859 |
| 18 | 7.225 | 8.493 | 10.30 | 15.35 | 3.86 | 330 | 1.587 | T50 | 1.868 |
| 19 | 7.716 | 8.660 | 10.45 | 15.37 | 6. 46 | 369 | 1.462 | 750 | 1.788 |
| 31 | 8.238 | 9.002 | 10.71 | 15. 55 | 9.99 | 394 | 1.387 | 750 | 1.588 |
| 81 | $\therefore .362$ | 9.039 | 11.29 | 17.09 | 1.93 | 270 | 1.379 | 680 | 1.698 |
| 82 | 1.985 | 9.275 | 11.36 | 16.93 | 3.93 | 3016 | 1.366 | 688 | 1.619 |
|  | 8.583 | 9.595 | 11.55 | 16.97 | 6.87 | 336 | 1.318 | 680 | 1.517 |
| 85 | ¢. 9.573 | 9.865 | 12.38 | 18.82 | 1.59 | 240 | 1.256 | 6,20 | 1.562 |
| 86 | 9. 392 | 10.13 | 12.44 | 18.58 | 3.62 | 270 | 1.248 | 620 | 1.486 |
| 87 | 8,852 | 19.95 | 12.68 | 18.61 | 6. 76 | 306 | 1.204 | 620 | 1.387 |
| 88 | 9,4:77 | 11.17 | 13.18 | 20.78 | 1.78 | 220 | 1.135 | 560 | 1.403 |
| 89 | 10.37 | 11.62 | 14. 91 | 20.68 | 3. ${ }_{5}$, | 2401 | 1.131 | 560 | 1.353 |
| 96 | 9.717 | 12.02 | 15.134 | 22.83 | 1.73 | 2701 | 1.069 | 568 | 1.256 |
| 91 | 11.47 | 12.29 | 15.11 | 22. 60 | 3, 41 | 26131 | 1.034 | 510 | 1.279 |
| 92 | 19.33 | 12.99 | 16.33 | 24.84 | 1.46 | 2201 | 1.029 | 510 | 1.229 |



Figure 4. Lowpass filter schematic diagram and attenuation response, inductive input and output.

Table 4. 50-ohm 7-Element Chebyshev Lowpass Fitter Designs Using Standard-Value Capacitors, Inductive Input and Output.

| Filter No. | - - Freq Cutoff | $\begin{gathered} \mathrm{cy}(\mathrm{MH} \\ 3-\mathrm{dB} \end{gathered}$ | 20-dB | 50-dB | RC <br> (\%) | $\begin{gathered} \mathrm{L}, \mathrm{~L} 7 \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \mathrm{C} 2, \mathrm{C} 6 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{array}{r} \text { L3, L5 } \\ (\mu \mathrm{H}) \end{array}$ | $\begin{aligned} & \mathrm{C4} \\ & (\mathrm{pF}) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.014 | 1.179 | 1.444 | 2.152 | 3.89 | 5.890 | 4300 | 13.37 | 5100 |
| 2 | 1.087 | 1.293 | 1.597 | 2.398 | 2.88 | 5.062 | 3900 | 12.04 | 4700 |
| 3 | 1.197 | 1.405 | 1.728 | 2.584 | 3. 41 | 4.810 | 3600 | 11.15 | 4360 |
| 4 | 1.328 | 1.537 | 1.879 | 2.797 | 4.16 | 4.581 | 3300 | 10.29 | 3900 |
| 5 | 1.425 | 1.683 | 2.075 | 3.110 | 3.12 | 3.947 | 3009 | 9.274 | 3600 |
| 6 | 1.528 | 1.855 | 2.308 | 3.486 | 2.21 | 3.363 | 2700 | 8.316 | 3300 |
| 7 | 1.634 | 2.059 | 2.589 | 3.945 | 1.43 | 2.828 | 2400 | 7.408 | 3000 |
| 8 | 1.859 | 2.271 | 2.832 | 4.284 | 2.04 | 2.710 | 2200 | 6.775 | 2700 |
| 9 | 2.137 | 2.525 | 3.113 | 4.665 | 3.12 | 2. 631 | 2000 | 6.182 | 2408 |
| 10 | 2.291 | 2.782 | 3.462 | 5.228 | 2.21 | 2.242 | 1800 | 5. 544 | 2200 |
| 11 | 2.452 | 3.088 | 3.884 | 5.918 | 1.43 | 1.885 | 1600 | 4.939 | 2000 |
| 12 | 2.849 | 3.367 | 4.150 | 6.219 | 3.12 | 1.973 | 1500 | 4.637 | 1800 |
| 13 | 3.126 | 3.838 | 4.791 | 7.256 | 1.93 | 1.589 | 1300 | 4.004 | 1600 |
| 14 | 3.269 | 4.117 | 5.179 | 7.890 | 1. 43 | 1.414 | 1200 | 3.704 | 1500 |
| 15 | 3.475 | 3.897 | 4.701 | 6.915 | 6.53 | 2.004 | 1300 | 4.169 | 1500 |
| 16 | 3.985 | 4.610 | 5.637 | 8.390 | 4.16 | 1.527 | 1100 | 3.4.29 | 1300 |
| 17 | 4.274 | 5.050 | 6.225 | 9.329 | 3.12 | 1.315 | 1000 | 3.091 | 1200 |
| 18 | 4.633 | 5.533 | 6.846 | 10.29 | 2.72 | 1.170 | 910 | 2.807 | 1100 |
| 19 | 5.053 | 6.115 | 7.600 | 11.47 | 2.30 | 1.027 | 820 | 2.525 | 1000 |
| 29 | 5.581 | 6.702 | 8.309 | 12.51 | 2.53 | 0.953 | 750 | 2.311 | 910 |
| 21 | 6.229 | 7.412 | 9.160 | 13.76 | 2.85 | 0.880 | 680 | 2.098 | 820 |
| 22 | 6.791 | 8.119 | 10.05 | 15.11 | 2.68 | 0.795 | 620 | 1.912 | 750 |
| 23 | 7.463 | 8.973 | 11.13 | 16.76 | 2.50 | 0.710 | 560 | 1.725 | 680 |
| 24 | 8.176 | 9.847 | 12.22 | 18.41 | 2.44 | 0. 644 | 510 | 1.571 | 620 |
| 25 | 9.207 | 10.77 | 13.23 | 19.76 | 3.57 | 0.633 | 470 | 1.457 | 560 |
| 26 | 10.14 | 11.79 | 14.44 | 21.52 | 3.89 | 0.589 | 430 | 1.337 | 510 |
| 27 | 10.87 | 12.93 | 15.97 | 23.98 | 2.88 | 0.506 | 390 | 1.203 | 470 |



Figure 5. 50-ohm 5th-degree elliptic lowpass filter designs using standard-value capacitors for C1, C3, and C5

Table 5A. 50-ohm 5th-Degree Elliptic Lowpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output.

| Filter No. | $\begin{gathered} \text { F-CO } \\ \cdots \end{gathered}$ | F-3dB <br> (MHz) | $\mathrm{F}-\mathrm{A}_{\mathrm{S}}$ | $\mathrm{A}_{\mathrm{s}}$ <br> (dB) | RC <br> (\%) | C1 | C3 | $\begin{array}{r} \mathrm{C} 5 \\ -(\mathrm{pF}) \end{array}$ | C2 | C4 | $\begin{aligned} & \text { L2 L4 } \\ & \cdots(\mu \mathrm{H})-- \end{aligned}$ | F2 <br> - (MHz) | F4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.80 | 0.99 | 1.57 | 47.4 | 4.40 | 2790 | 56800 | 2200 | 324 | 937 | 12.110 .1 | 2.54 | 1.64 |
| 2 | 0.93 | 1.89 | 1.67 | 46.7 | 7.16 | 2789 | 5100 | 2200 | 333 | 960 | 10.68 .74 | 2.67 | 1.17 |
| 3 | 1.46 | 1.20 | 1.72 | 46.2 | 10.5 | 2790 | 4796 | 2000 | 341 | 982 | 9.36 ․ 56 | 2.82 | 1.85 |
| 4 | 1.23 | 1.35 | 1.92 | 45.8 | 15.3 | 2700 | 4300 | 2200 | 352 | 1010 | 7.936 .27 | 3.12 | 2.00 |
| 5 | 1.47 | 1. 57 | 2.15 | 45.4 | 22.7 | 2796 | 3960 | 2200 | 364 | 1045 | $6.32 \quad 4.33$ | 3.32 | 2.23 |
| 6 | 0.87 | 1.10 | 1.83 | 49.7 | 3.84 | 2400 | 5106 | 20100 | 257 | 735 | 11.09 .41 | 2.99 | 1.91 |
| 7 | 1.99 | 1.20 | 1.93 | 49.2 | 6. 94 | 2490 | 4704 | 2008 | 262 | 748 | 9.31 8.36 | 3.12 | 2.81 |
| 8 | 1.15 | 1.33 | 2. 615 | 48.6 | 9.37 | 2490 | 43018 | 2000 | 269 | 765 | 8.67 ? 2.19 | 3.30 | 2. 15 |
| 9 | 1.37 | 1. 51 | 2. 25 | 48.1 | 14.5 | 2490 | 3700 | 2060 | 276 | 735 | 7.255 .90 | 3.55 | 2.34 |
| 10 | 1.39 | 1.60 | 3.11] | 61.5 | 161.8 | 2200 | 3903 | 2000 | 136 | 355 | 7.536 .80 | 5.09 | 5. 24 |
| 11 | 1.58 | 1.71 | 2.45 | 47.8 | 201. 2 | 24818 | 3696 | 2090 | 284 | 865 | 6.064 .85 | 3.84 | 2.55 |
| 12 | 1.62 | 1.80 | 3.37 | 61.3 | 15.91 | 22610 | $3 \mathrm{Fig6}$ | 2900 | 132 | 359 | 6.365 .69 | 5.49 | 3.52 |
| 13 | 18.93 | 1.18 | 1.91 | 48.4 | 3.71 | 22904 | 4 ? g ใ | 1800 | $25{ }^{\circ}$ | 74.3 | 19.28 .59 | 3.11 | 1.99 |
| 14 | 1.98 | 1.36 | 2.02 | 47.3 | 6.815 | 22610 | 43013 | 1360 | 2.5. | 759 | 9.097 .55 | 3.25 | 2.10 |
| 15 | 1. 27 | 1.45 | 2.17 | 46.7 | 9.63 | 2300 | 35018 | 1800 | 271 | 779 | ?.85 6. 39 | 3.45 | 2.26 |
| 15 | 1.45 | 1.51 | 2,3 ? | 45.3 | 13, 8 | $\geq 2190$ | 36.j¢ | 1806 | 278 | 796 | 6.805 .44 | 3.66 | 2. 42 |
| 17 | 1.47 | 1.70 | 3.36 | 51.5 | 9.41 | 20990 | 366461 | 1869 | 130 | 357 | 7.0776 .33 | 5.24 | 3.35 |
| 18 | 1.69 | 1.82 | 2.54 | $4{ }^{3} .9$ | 19.1 | $\therefore 290$ | 3.809 | 18 A | 237 | 821 | 5.644 .42 | 3.96 | 2.64 |
| 19 | 1.13 | 1.93 | 3.45 | 57.2 | 15.1 | 21096 | 9300 | 18 ¢0 | 132 | 362 | $5.94 \quad 5.25$ | 5.61 | 3.64 |
| 20 | 1.00 | 1.27 | 2. 919 | 46.1 | 3.54 | 2090 | 4.369 | 1689 | 258 | 752 | 9.35 7.76 | 3.24 | 2.03 |
| 21 | 1.18 | 1.41 | 2. 12 | 45.4 | 5.91? | 2009 | 3'100 | 1609 | 265 | 771 | 8.27 6.73 | 3.40 | 2.21 |
| 32 | 1.34 | 1.54 | 2.24 | 44.8 | 8.8'\% | 2009 | 3609 | 16010 | 272 | 779 | 7. $36 \quad 5.89$ | 3.56 | 2.33 |
| 23 | 1. 55 | 1.71 | 2.41 | 44.3 | 13.19 | 2609 | 3.3001 | 1600 | 286 | 812 | 6.354 .97 | 3.78 | 2.50 |
| 24 | 1.56 | 1.82 | 3.32 | 57.3 | 8.91 | 1606 | 3300 | 16010 | 130 | 360 | 6.615 .85 | 5.42 | 3.47 |
| 25 | 1.82 | 1.95 | 2.65 | 43.8 | 19.1 | 20ืbด | З可近 | 1600 | 290 | 841 | 5.213 .97 | 4.09 | 2. 75 |
| 26 | 1.86 | 2.08 | 3.62 | 57.0 | 14.1 | 1806 | 3 bug | 1660 | 133 | 366 | 5.524 .83 | 5.88 | 3.79 |


| Filter <br> No. | $\mathrm{F}-\mathrm{CO}$ | F-3 dB $(\mathrm{MHz})$ | $\mathrm{F}-\mathrm{A}_{\mathrm{S}}$ | $\begin{aligned} & A_{S} \\ & (\mathrm{~dB}) \end{aligned}$ | RC <br> (\%) | C1 | C3 | (pF) | C2 | C4 | 12 | $\begin{gathered} \mathrm{L} 4 \\ (\mu \mathrm{H}) \cdots \end{gathered}$ |  | F4 <br> z) -- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 27 | 1.12 | 1.44 | 2.41 | 49.8 | 3.42 | 1809 | 3900 | 1500 | 192 | 549 | 8. 45 | 7.25 | 3.95 | 2.52 |
| 28 | 1.28 | 1.56 | 2.53 | 49.3 | 5. 41 | 1300 | 3600 | 15018 | 196 | 558 | 7.65 | 6.47 | 4.11 | 2.65 |
| 29 | 1.49 | 1.73 | 2.70 | 43.8 | 8.45 | 1800 | 3300 | 1500 | 200 | 570 | 6.75 | 5.62 | 4.33 | 2.81 |
| 30 | 1.75 | 1.95 | 2.92 | 48.2 | 13.01 | 1800 | 3000 | 1500 | 206 | 585 | 5.72 | 4.68 | 4.64 | 3.04 |
| 31 | 2.11 | 2.27 | 3.27 | 47.8 | 20.2 | 1800 | 2706 | 1500 | 213 | 604 | 4.55 | 3.64 | 5.12 | 3.40 |
| 32 | 1.15 | 1.54 | 2.51 | 47.7 | 2.70 | 1660 | 35090 | 1300 | 191 | 553 | 7.86 | 6.65 | 4.11 | 2.63 |
| 33 | 1.35 | 1.68 | 2.64 | 47.1 | 4.53 | 1600 | 3300 | 1300 | 195 | 564 | ?. 10 | 5.92 | 4.28 | 2.75 |
| 34 | 1.58 | 1.86 | 2. 81 | 46.4 | ㄱ. 41 | 1606 | 3010 | 1300 | 200 | 578 | 6.24 | 5.11 | 4.50 | 2.93 |
| 35 | 1.57 | 1.93 | 3.40 | 53.9 | 5.51 | 1500 | 3080 | 1308 | 129 | 362 | 6.33 | 5.54 | 5.57 | 3.55 |
| 36 | 1.88 | 2.11 | 3.95 | 45.8 | 12.8 | 1600 | 2791 | 1300 | 207 | 596 | 5.26 | 4.21 | 4.82 | 3.18 |
| 37 | 1.89 | 2. 19 | 3.68 | 53.3 | 9.50 | 1500 | 2709 | 1300 | 132 | 369 | 5.39 | 4.65 | 5.96 | 3.84 |
| 38 | 2.31 | 2. 48 | 3.44 | 45.3 | 19.5 | 1600 | 24013 | 1300 | 216 | 620 | 4.12 | 3.21 | 5.33 | 3.57 |
| 39 | 2.35 | 2.58 | 4.12 | 52.9 | 16.3 | 1500 | 2400 | 1300 | 136 | 379 | 4.28 | 3.62 | 6.59 | 4.30 |
| 40 | 1. 28 | 1.66 | 2.63 | 46.3 | 3.11 | 1500 | 3300 | 1200 | 192 | 561 | 7.20 | 6.00 | 4.28 | 2.74 |
| 41 | 1.51 | 1.83 | 2.78 | 45.6 | 5.33 | 1500 | 3000 | 1200 | 197 | 574 | 6.42 | 5.25 | 4.47 | 2.90 |
| 42 | 1.79 | 2.06 | 2.99 | 44.8 | 8.89 | 1500 | 2706 | 1200 | 204 | 592 | 5.52 | 4.42 | 4.75 | 3.11 |
| 43 | 2.17 | 2.38 | 3. 31 | 44.2 | 14.7 | 1500 | 2400 | 1200 | 212 | 616 | 4.49 | 3.49 | 5.16 | 3.43 |
| 44 | 2.52 | 2.70 | 3.63 | 43.8 | 20.8 | 1500 | 22000 | 1200 | 220 | 636 | 3.71 | 2.82 | 5.58 | 3.76 |
| 45 | 1.68 | 2.10 | 3.56 | 51.2 | 4. 41 | 1300 | 2790 | 1100 | 129 | 365 | 5.79 | 4.99 | 5.83 | 3.73 |
| 46 | 2.35 | 2. 40 | 3.87 | 50.5 | 8. 22 | 1360 | 2406 | 1100 | 133 | 375 | 4.90 | 4.15 | 6.24 | 4.04 |
| 47 | 2.39 | 2.68 | 4.16 | 50.0 | 12.3 | 1300 | 2206 | 1100 | 136 | 383 | 4.22 | 3.52 | 6.65 | 4.34 |
| 48 | 2.84 | 3.08 | 4.80 | 49.7 | 18.6 | 1300 | 2006 | 1100 | 140 | 393 | 3.45 | 2.82 | 7.26 | 4.78 |
| 49 | 1.56 | 2.08 | 3.55 | 50.1 | 2.69 | 1200 | 2700 | 1090 | 127 | 363 | 5.88 | 5.07 | 5.83 | 3.71 |
| 50 | 1.92 | 2.35 | 3.80 | 49.3 | 5,41 | 1200 | 2496 | 1990 | 130 | 372 | 5.10 | 4.32 | 6.17 | 3.97 |
| 51 | 2.23 | 2.59 | 4.194 | 48.8 | 8.40 | 1200 | 2200 | 1900 | 133 | 380 | 4.50 | 3.75 | 6.50 | 4.22 |
| 52 | 2.62 | 2.92 | 4.38 | 48.2 | 13.0 | 1200 | 2006 | 1000 | 137 | 390 | 3.81 | 3.12 | 6.96 | 4.56 |
| 53 | 3.24 | 3. 60 | 6. 34 | 61.3 | 16.0 | 1100 | 1806 | 1090 | 65.9 | 180 | 3.18 | 2.85 | 11.0 | ?.04 |
| 54 | 3.17 | 3.41 | 4.96 | 47.8 | 20.2 | 1200 | 1800 | 1000 | 142 | 402 | 3.03 | 2.42 | 7.68 | 5.10 |
| 55 | 1.80 | 2. 33 | 3.97 | 49.1 | 3.27 | 1100 | 2400 | 910 | 121 | 349 | 5.21 | 4.45 | 6.33 | 4.04 |
| 56 | 2.09 | 2. 55 | 4.07 | 48.6 | 5.39 | 1100 | 2206 | 910 | 124 | 355 | 4.68 | 3.94 | 6.60 | 4.25 |
| 57 | 2.45 | 2. 84 | 4.36 | 48.6 | 8,69 | 1109 | 2006 | 910 | 127 | 364 | 4. 115 | 3.37 | 6.99 | 4.54 |
| 58 | 2.93 | 3.25 | 4. 17 | 47.4 | 13.9 | 1100 | 1800 | 910 | 131 | 375 | 3.38 | 2.74 | 7.55 | 4.97 |
| 59 | 3.64 | 3.88 | 5.45 | 47.0 | 22.6 | 1100 | 16019 | 910 | 137 | 389 | 2.58 | 2.04 | 8.46 | 5.65 |
| 80 | 1.94 | 2.52 | 4.15 | 48.4 | 3.11 | 1060 | 2206̆ | 820 | 115 | 331 | 4.79 | 4.06 | 6.78 | 4.34 |
| 61 | 2.29 | 2.79 | 4.39 | 47.7 | 5.37 | 1009 | 2006 | 820 | 118 | 339 | 4.26 | 3.56 | 7.10 | 4.58 |
| 62 | 2.73 | 3.14 | 4.73 | 47.0 | 9.615 | 1609 | 1806 | 820 | 121 | 348 | 3. 66 | 2.99 | 7.56 | 4.93 |
| 63 | 3.33 | 3.65 | 5.25 | 46.4 | 15.2 | 16109 | 1600 | 820 | 126 | 361 | 2.95 | 2.36 | 8.25 | 5.46 |
| 64 | 3.37 | 3.87 | 7.23 | 59.6 | 11.2 | 910 | 1603 | 820 | 53.8 | 161 | 3.08 | 2.75 | 11.8 | 7.55 |
| 65 | 3.73 | 4.02 | 5.53 | 46.2 | 19.7 | 1000 | 1500 | 820 | 129 | 368 | 2.56 | 2.01 | 8.76 | 5.85 |
| E. 6 | 3.82 | 4.26 | 7.72 | 59.5 | 15.2 | 919 | 1506 | 820 | 59.6 | 163 | 2.70 | 2.39 | 12.6 | 8.07 |
| 67 | 2.14 | 2.79 | 4.61 | 48.8 | 3.13 | 919 | 2004 | 750 | 102 |  | 4.35 | 3.71 | 7.55 | 4.82 |
| 68 | 2.57 | 3.11 | 4.92 | 48.1 | 5.71 | 910 | 1800 | 750 | 105 | 301 | 3.82 | 3.19 | 7.95 | 5.13 |
| 69 | 3.13 | 3.56 | 5.36 | 47.4 | 16.1 | 910 | 1600 | 750 | 108 | 315 | 3.20 | 2.62 | 8.55 | 5.59 |
| 70 | 3.49 | 3.87 | 5.68 | 47.1 | 13.4 | 910 | 1500 | 750 | 111 | 316 | 2.84 | 2.30 | 8.97 | 5.91 |
| 71 | 4.53 | 4.81 | E. 67 | 46.5 | 24.1 | 910 | 1300 | 750 | 116 | 331 | 2.04 | 1. 60 | 10.3 | 6.92 |

Table 5A. 50-ohm 5th-Degree Elliptic Lowpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output. (Continued from Page 131.)

| Filter <br> No. |  |  |  | $A_{S}$ (dB) |  | C1 | C3 | $\begin{gathered} \mathrm{C} 5 \\ (\mathrm{pF}) \end{gathered}$ | C2 | C4 | L2 | $\begin{gathered} L 4 \\ -(\mu H) \end{gathered}$ | $\begin{aligned} & \text { F2 } \\ & \cdots(M H z) \end{aligned}$ | $\begin{gathered} \text { F4 } \\ \text { z) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 72 | 2.39 | 3.11 | 5.20 | 49.4 | 3.15 | 820 | 1800 | 680 | 89.3 | 256 | 3.91 | 3.35 | 8.51 | 5.44 |
| 73 | 2.93 | 3.52 | 5.59 | 48.6 | 6.14 | 820 | 1606 | 689 | 92.0 | 263 | 3.37 | 2.83 | 9.04 | 5.83 |
| 74 | 3.26 | 3.79 | 5.85 | 48.2 | 8.45 | 820 | 1506 | ES0 | 93.6 | 267 | 3.617 | 2.54 | 9.39 | 6.10 |
| 75 | 4.17 | 4.57 | 6.65 | 47.5 | 16.0 | 820 | 1309 | 630 | 97.7 | 278 | 2.36 | 1.90 | 10.5 | 6.92 |
| 76 | 4.23 | 4.82 | 9.15 | 60.8 | 12.1 | 750 | 1309 | 680 | 45.8 | 125 | 2.46 | 2.21 | 15.9 | 9.58 |
| 77 | 4.83 | 5.17 | 7.30 | 47.2 | 22.1 | 820 | 1296 | 680 | 100 | 286 | 1.95 | 1. 54 | 11.4 | 7.58 |
| 78 | 4.97 | 5.47 | 10.6 | 60.7 | 17.7 | 750 | 1206 | 680 | 48.4 | 127 | 2.06 | 1.83 | 16.3 | 10.5 |
| 79 | 2.74 | 3.49 | 5.73 | 48.9 | 3.75 | 750 | 1600 | 520 | 83.6 | 248 | 3.46 | 2.94 | 9.36 | 5.99 |
| 89 | 3.07 | 3.73 | 5.97 | 48.5 | 5.39 | 750 | 1500 | 620 | 84.9 | 243 | 3.19 | 2.68 | 9.67 | 6.23 |
| 81 | 3.96 | 4.41 | 6. 63 | 47.6 | 10.8 | 750 | 1390 | 629 | 88,4 | 252 | 2.57 | 2.10 | 18.6 | 6.91 |
| 82 | 4.47 | 4.91 | ?. 15 | 47.2 | 15.3 | 750 | 1209 | 620 | 90.6 | 258 | 2.21 | 1.77 | 11.3 | 7.43 |
| 83 | 5.24 | 5.61 | 7.89 | 46.9 | 21.8 | 750 | 1100 | 620 | 93.4 | 266 | 1.80 | 1. 42 | 12.3 | 8.19 |
| 84 | 2.85 | 3.71 | 6. 15 | 48.8 | 3. 65 | 680 | 1500 | 560 | 76.6 | 220 |  | 2.78 | 10.1 | 6.43 |
| 85 | 3.64 | 4.32 | 6.72 | 47.8 | 6.79 | 680 | 1306 | 560 | 79.4 | 223 | 2.72 | 2.26 | 15.8 | 7.01 |
| 86 | 4.16 | 4.74 | 7. 14 | 47.3 | 9.95 | 684 | 1260 | 560 | 81.3 | 233 | 2.46 | 1.97 | 11.4 | 7.44 |
| 87 | 4.82 | 5.31 | 7.72 | 46.9 | 14.5 | 680 | 1109 | 560 | 83.5 | 239 | 2.05 | 1.65 | 12.2 | 8.03 |
| 88 | 4.88 | 5. 62 | 10.6 | 60.1 | 10.7 | 628 | 1100 | 560 | 39.1 | 107 | 2.13 | 1.91 | 17.4 | 11.1 |
| 89 | 5.72 | 6.13 | 8.58 | 46.5 | 21.5 | 688 | 1006 | 560 | 86.3 | 245 | 1. 65 | 1.30 | 13.3 | 8.91 |
| 90 | 5.88 | 6.49 | 11.8 | 59.9 | 16.9 | 620 | 10001 | 560 | 39.8 | 109 | 1.74 | 1.55 | 19.1 | 12.3 |
| 9 | 3.41 | 4.28 | 6.93 | 49,3 | 4. 15 | 620 | 1309 | 516 | 71.1 | 204 | 2.80 | 2.37 | 11.3 |  |
| 93 | 3.91 | 4.6 ? | 7.29 | 47.8 | 6.38 | 629 | 12013 | 510 | 72.6 | 208 | 2.53 | 2.10 | 11.8 | 7.61 |
| 93 | 4.52 | 5.17 | 7.78 | 47.3 | 9.69 | 620 | 1100 | 510 | 74.4 | 213 | 2.21 | 1.81 | 12.4 | 8.16 |
| 95 | 5.31 | 5.85 | 8.47 | 46.8 | 14.7 | 629 | 16168 | 510 | 76.7 | 219 | 1.85 | 1.49 | 13.3 | 8.81 |
| 95 | 6. 29 | 6.73 | 9.40 | 46.4 | 21.6 | 620 | 916 | 510 | 79.3 | 226 | 1.50 | 1.18 | 14.6 | 9.76 |
| 96 | 3.67 | 4. 69 | 7.95 | 50.5 | 3.55 | 560 | 1200 | 470 | 57.6 | 16.4 | 2.59 | 2.23 | 13.0 | 8.31 |
| 97 | 4.27 | 5.15 | 8. 410 | 49.9 | 5.97 | 560 | 1100 | 470 | 58.8 | 167 | 2.32 | 1.97 | 13.6 | 8.77 |
| 98 | 5.92 | 5.77 | 9.191 | 49.4 | 9.57 | 56.8 | 1961 | 470 | 60.3 | 171 | 2.01 | 1.68 | 14.5 | 9.40 |
| 99 | 5.91 | 6.53 | 9.82 | 48.9 | 14.6 | 560 | 910 | 470 | 62.13 | 175 | 1.59 | 1.38 | 15.6 | 10.2 |
| 100 | 7. 18 | 7.68 | 11.1 | 48.6 | 22.5 | 560 | 829 | 470 | 64.1 | 181 | 1.32 | 1. 46 | 17.3 | 11.5 |
| 101 | 3.99 | 5.13 | 8.30 | 51.0 | 3.52 | 510 | 1100 | 439 | 51.1 | 145 | 2.38 | 2.96 | 14.4 | 9.20 |
| 1024 | 4.71 | 5.69 | 9.34 | 51, 4 | 6. 04 | 510 | 1000 | 430 | 52.3 | 148 | 2.11 | 1.79 | 15.2 | 9.76 |
| 1035 | 5.54 | 6.36 | 10.0 | 49.9 | 9.65 | 510 | 918 | $4: 30$ | 53.5 | 152 | 1.82 | 1.53 | 16.1 | 10.5 |
| 194 | 6. 64 | 7.32 | 11.0 | 49.4 | 15.4 | 510 | 826 | 4.30 | 55.2 | 156 | 1.50 | 1. 23 | 17.5 | 11.5 |
| 105 ? | ?.87 | 8.42 | 12.3 | 49.1 | 22.3 | 510 | 750 | 430 | 56.8 | 160 | 1.21 | 0.98 | 19.2 | 12.7 |
| 106 | 4.40 | 5.60 | 9.24 | 49.3 | 3.81 | 478 | 1060 | 390 | 51.4 | 147 | 2.16 | 1.84 | 15.1 | 9.66 |
| 107 | 5.18 | 6.19 | 9.82 | 48.6 | 6.39 | 476 | 910 | 398 | 52.6 | 151 | 1.91 | 1.60 | 15.9 | 10.2 |
| 1086 | 6.17 | $\xrightarrow{7} .01$ | 10.6 | 48.8 | 10.5 | 479 | 820 | 398 | 54.2 | 155 | 1.63 | 1.34 | 17.0 | 11.1 |
| 109 ? | 7.19 | 7.98 | 11.5 | 47.6 | 15.5 | 470 | 750 | 398 | 55.7 | 159 | 1.37 | 1.11 | 18.2 | 12.0 |
| 110 | 7.30 | 8.34 | 15.9 | 60.9 | 11. ? | 430 | 750 | 396 | 26.1 | 71.3 | 1.43 | 1.28 | 26.1 | 16.6 |
| 11112 | 8.63 | 9.26 9.78 | 12.9 | 47.3 | 23.2 | 470 | 680 | 390 | 57.6 | 164 | 1. 69 | 0.86 | 20.1 | 13.4 |
| 11.28 | 8.88 | 9.73 | 17.7 | 60.8 | 18.7 | 430 | 680 | 390 | 26.6 | 72.4 | 1.15 | 1.02 | 28.8 | 18.5 |


| Filter No. |  |  | $\mathrm{F}-\mathrm{A}_{\mathrm{S}}$ | $\begin{gathered} \mathrm{A}_{\mathrm{S}} \\ \text { (dB) } \end{gathered}$ | RC <br> (\%) | C1 | C3 | C5 | C2 | C4 | $\begin{aligned} & 12 \\ & \cdots(\mu \end{aligned}$ | L4 $(\mu H) \cdots$ | F2 $--(M)$ | $\begin{gathered} \text { F4 } \\ \text { z) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 113 | 4.88 | 6.18 | 10.4 | 50.1 | 3.94 | 430 | 916 | 360 | 45.0 | 128 | 1.96 | 1.68 | 16.9 | 10.8 |
| 114 | 5.84 | 6.93 | 11.1 | 49.5 | 6.94 | 430 | 820 | 360 | 46.1 | 131 | 1.71 | 1.44 | 17.9 | 11.6 |
| 115 | 6.79 | 7.72 | 11.9 | 49.0 | 10.6 | 430 | 750 | 360 | 47.3 | 134 | 1.48 | 1.23 | 19.0 | 12.4 |
| 116 | 8.06 | 8.83 | 13.1 | 48,5 | 16.3 | 439 | 680 | 360 | 48.7 | 138 | 1.22 | 1.00 | 20.6 | 13.6 |
| 117 | 9,61 | 10.2 | 14.6 | 48.3 | 23.9 | 430 | 520 | 360 | 50.2 | 142 | 0.97 | 0.78 | 22.8 | 15.2 |
| 118 | 5.47 | 6.91 | 11.8 | 51.3 | 4.11 | 390 | 829 | 330 | 38.5 | 109 | 1.76 | 1.52 | 19.3 | 12.3 |
| 119 | 6.39 | 7.53 | 12.5 | 50.7 | 6.70 | 390 | 756 | 330 | 39.3 | 111 | 1.57 | 1.33 | 20.3 | 13.1 |
| 120 | 7.55 | 8.59 | 13.5 | 50.2 | 10.8 | 390 | 680 | 330 | 40.4 | 114 | 1.34 | 1.12 | 21.7 | 14.1 |
| 121 | 8.90 | 9.77 | 14.8 | 49.8 | 16.2 | 390 | 620 | 330 | 41.4 | 117 | 1.11 | 0.92 | 23.4 | 15.4 |
| 122 | 10.9 | 11.5 | 16.8 | 49.5 | 24.8 | 390 | 560 | 338 | 42.8 | 120 | 0.86 | 0.70 | 26.2 | 17.4 |
| 123 | 9.87 | 10.7 | 15.7 | 48.0 | 17.4 | 360 | 560 | 300 | 42.9 | 119 | 0.99 | 0.80 | 24.7 | 16.3 |
| 124 | 10.1 | 11.3 | 21.6 | 61.4 | 13.4 | 330 | 560 | 300 | 19.7 | 53.6 | 1.03 | 0.93 | 35.3 | 22.6 |
| 125 | 8.26 | 9.33 | 14.2 | 48.4 | 11.2 | 360 | 620 | 300 | 40.7 | 116 | 1.22 | 1.00 | 22.6 | 14.8 |
| 126 | 8.28 | 9.84 | 19,6 | $61 . ?$ | 8.03 | 330 | 620 | 300 | 19.3 | 52.8 | 1.25 | 1.14 | 32.4 | 20.6 |
| 127 | 7.97 | 8.34 | 13.2 | 49.9 | 7.26 | 360 | 680 | 300 | 39.7 | 113 | 1.41 | 1.18 | 21.3 | 13.8 |
| 128 | 5.98 | 7.49 | 12.3 | 49.6 | 4.31 | 360 | 750 | 390 | 38.7 | 111 | 1.61 | 1.37 | 20.1 | 12.9 |
| 129 | 7.69 | 9.03 | 13.8 | 47.1 | 7.37 | 330 | B20 | 270 | 40.0 | 115 | 1.27 | 1.06 | 22.2 | 14.4 |
| 130 | 6.59 | 8,1? | 13.6 | 47.7 | 4.57 | 330 | 680 | 270 | 39.9 | 112 | 1.46 | 1.22 | 21.1 | 13.6 |
| 131 | 9.10 | 10.2 | 15.9 | 45.5 | 11.8 | 330 | 560 | 270 | 41.2 | 118 | 1.09 | 0,88 | 23.7 | 15.6 |
| 132 | 9.15 | 10.8 | 25.7 | 59.6 | 8.23 | 300 | 56.3 | 270 | 19.4 | 53.3 | 1.13 | 1.01 | 34.0 | 21.6 |
| 133 | 10.7 | 11.6 | 16.4 | 46.0 | 17.4 | 330 | 510 | 270 | 42.6 | 122 | 0.91 | 0.72 | 25.6 | 17.0 |
| 134 | 10.9 | 12.3 | 22.5 | 59.3 | 13.1 | 300 | 510 | 278 | 19.7 | 54.1 | 0.95 | 0.85 | 36.7 | 23.5 |
| 135 | 12.4 | 13.2 | 18.1 | 45.8 | 24,1 | 330 | 478 | 278 | 43.9 | 125 | 0.74 | 0.57 | 27.9 | 18.8 |
| 136 | 12.8 | 14.0 | 24.7 | 59.2 | 19.2 | 300 | 470 | 270 | 20,1 | 54.9 | 0.79 | 0.69 | 40.1 | 25.8 |
| 137 | ?. 14 | 8.134 | 13.6 | 45.8 | 4.47 | 3001 | 620 | 240 | 39.1 | 114 | 1.34 | 1.10 | 22.6 | 14.2 |
| 138 | 8.44 | 9.86 | 14.6 | 45.1 | 7. 51 | 369 | 5610 | 240 | 40.3 | 117 | 1.17 | 0.94 | 23.2 | 15.2 |
| 139 | 9.81 | 11.9 | 15.6 | 44.5 | 11.4 | 300 | 510 | 248 | 41.6 | 121 | 1.00 | 0.79 | 24.6 | 16.3 |
| 140 | 9.85 | 11.7 | 21.6 | 57.4 | 7. 64 | 270 | 516 | 240 | 19.5 | 53.8 | 1.04 | 0.93 | 35.4 | 22.6 |
| 141 | 11.2 | 12.2 | 16.9 | 44.1 | 16.9 | 300 | 478 | 240 | 42.8 | 124 | 0.86 | 0.67 | 26.2 | 17.5 |
| 142 | 11.4 | 13.0 | 23.1 | 57.1 | 11.5 | 270 | 470 | 240 | 19.8 | 54,5 | 0.90 | 0.79 | 37.7 | 24.2 |
| 143 | 13.1 | 14.0 | 18.6 | 43.7 | 22.7 | 300 | 430 | 240 | 44.3 | 128 | 0.70 | 0.53 | 28.6 | 19.3 |
| 144 | 13.6 | 14.9 | 25.4 | 56.9 | 17.4 | 270 | 436 | 245 | 20.2 | 55.4 | 0.75 | 0.65 | 41.0 | 26.5 |

Table 5B. 600-Ohm 5th-0egree Elliptic Lowpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output.

| Filter No. |  | F-3 dB <br> - (kHz) - | $\mathrm{F}-\mathrm{A}_{\mathrm{S}}$ | $\begin{gathered} \mathrm{A}_{\mathrm{S}} \\ (\mathrm{~dB}) \end{gathered}$ | $\begin{aligned} & \mathrm{RC} \\ & \text { (\%) } \end{aligned}$ | C1 | C3 | $\begin{aligned} & \text { C5 } \\ & (\mathrm{nF}) \end{aligned}$ | C2 | C4 | $\begin{gathered} L 2 \\ \cdots \end{gathered}$ | $\begin{gathered} 14 \\ (\mathrm{mH})-- \end{gathered}$ | $\begin{aligned} & \text { F2 } \\ & \cdots(\mathrm{kHz} \end{aligned}$ | $\begin{gathered} F^{\prime} \\ \text { (z) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 9.66 | 10.82 | 1. 31 | 47.4 | 4.49 | 270 | 55 ts | 20 | F2, 4 | 93.1 | 174 | 145 | 2.12 | 1.36 |
| 2 | 6.89 | 1.00 | 1.48 | 46.2 | 10.5 | 270 | 475 | . 220 | 34.1 | 98.2 | 135 | 109 | 2.35 | 1.54 |
| 3 | 1.23 | 1.31 | 1.79 | 45.4 | 22.1 | 270 | 398 | 220 | 36.4 | 105 | 91.6 | 70.3 | 2.76 | 1.86 |
| 4 | 0.77 | 0.98 | 1.51 | 48.0 | 3.11 | 220 | 470 | 180 | 25.7 | 74.3 | 147 | 124 | 2.59 | 1.66 |
| 5 | 1. 1.81 | 1.21 | 1.80 | 46.7 | 9.83 | 220 | 376 | 130 | 27.1 | 77.9 | 113 | 92.9 | 2.87 | 1.88 |
| 6 | 1.41 | 1.52 | 2. 12 | 45.9 | 19.7 | 220 | 336 | 180 | 28.7 | 82.1 | 81.2 | 63.7 | 3.30 | 2.20 |
| $?$ | 6.93 | 1.20 | 2.191 | 49.8 | 3.42 | 180 | 396 | 159 | 19.2 | 54.9 | 122 | 104 | 3.29 | 2.10 |
| 8 | 1.24 | 1.44 | 2.25 | 48.8 | S.48 | 180 | 336 | 150 | 20.0 | 57.6 | 97.1 | 81.0 | 3.61 | 2.34 |
| 9 | 1.76 | 1.90 | 2.72 | 47.8 | 20.2 | 180 | 270 | 150 | 21.3 | 66.4 | 65.5 | 52.4 | 4.26 | 2.83 |
| 10 | 1.07 | 1.38 | 2.19 | 46.3 | 3.11 | 150 | 330 | 120 | 19.2 | 56.1 | 104 | 86.4 | 3.57 | 2.29 |
| 11 | 1.49 | 1.71 | 2. 49 | 44.8 | 8.89 | 150 | 270 | 120 | 20.4 | 59.2 | 79.5 | 63.6 | 3.95 | 2.59 |
| 12 | 2.10 | 2.25 | 3,02 | 43.8 | 20.8 | 159 | 220 | 128 | 22.0 | 63.6 | 53.4 | 40.6 | 4.65 | 3.13 |
| 13 | 1.30 | 1.73 | 2.95 | 50.1 | 2.69 | 120 | 270 | 100 | 12. 7 | 36.3 | 84.7 | 73.0 | 4.86 | 3.09 |
| 14 | 1.86 | 2. 16 | 3.37 | 48.8 | 8.49 | 120 | 220 | 100 | 13.3 | 38.0 | 64.8 | 54.0 | 5.41 | 3.51 |
| 15 | 2.64 | 2.84 | 4.09 | 47.8 | 20.2 | 120 | 186 | 100 | 14.2 | 40.2 | 43.6 | 34.9 | 6.40 | 4.25 |
| 16 | 1.82 | 2.10 | 3.46 | 48.4 | 3.11 | 100 | 220 | 82 | 11.5 | 33.1 | 68.9 | 58.5 | 5.65 | 3.61 |
| 17 | 2.27 | 2.62 | 3.94 | 47.6 | 9.05 | 100 | 180 | 82 | 12.1 | 34.8 | 52.6 | 43.1 | 6.30 | 4.11 |
| 18 | 3.11 | 3.35 | 4.69 | 46.2 | 19.7 | 100 | 150 | 82 | 12.9 | 36.8 | 36.9 | 29.0 | 7.30 | 4.87 |
| 19 | 1.99 | 2. 5.59 | 4.33 | 49.4 | 3.15 | 82 | 180 | 68 | 8.93 | 25.6 | 56.3 | 48.2 | 7.10 | 4.53 |
| 20 | 2.72 | 3.16 | 4.88 | 48.2 | 8.45 | 82 | 150 | 68 | 9.36 | $26 . ?$ | 44.2 | 36.6 | 7.83 | 5.09 |
| 21 | 4.03 | 4.31 | 5. 08 | 47.2 | 22.1 | 82. | 120 | 68 | 10.0 | 28.6 | 28.1 | 22.2 | 9.47 | 6.32 |
| 22 | 2.37 | 3.09 | 5.12 | 48.8 | 3.06 | 68 | 150 | 56 | 7. 66 | 22.9 | 47.0 | 40.0 | 8.39 | 5.36 |
| 23 | 3.46 | 3.95 | 5.95 | 47.3 | 9.95 | 68 | 126 | 56 | 8.13 | 23.3 | 34.6 | 28.3 | 9.49 | 6.20 |
| 24 | 4.77 | 5.11 | 7.15 | 46.5 | 21.5 | 68 | 100 | 56 | 8.63 | 24.6 | 23.8 | 18.7 | 11.1 | 7.42 |
| 25 | 3.06 | 3.91 | 6.62 | 50.5 | 3.66 | 56 | 120 | 47 | 5.76 | 16.4 | 37.4 | 32.1 | 18.8 | 6.93 |
| 26 | 4.18 | 4.80 | 7. 51 | 49.4 | 9.57 | 56 | 100 | 47 | 6.03 | 17.1 | 28.9 | 24.1 | 12.1 | 7.83 |
| 27 | 5.98 | E. 40 | 9.22 | 48.6 | 22.5 | 56 | 82 | 47 | 6.41 | 18.1 | 19.0 | 15.2 | 14.4 | 9.58 |
| 28 | 3.67 | 4.66 | 7.70 | 49.3 | 3.81 | 47 | 100 | 39 | 5.14 | 14.7 | 31.1 | 26.5 | 12.6 | 8.05 |
| 29 | 5.14 | 5.84 | 8.86 | 48.0 | 10.5 | 47 | 82 | 39 | 5.42 | 15.5 | 23.4 | 19.2 | 14.1 | 9.23 |
| 30 | 7.19 | 7.67 | 10.8 | 47.3 | 23.2 | 47 | 68 | 39 | 5.76 | 16.4 | 15.6 | 12.3 | 16.8 | 11.2 |
| 31 | 4.56 | 5.76 | 9.83 | 51.3 | 4. 11 | 39 |  |  | 3.85 | 10.9 | 25.4 | 21.9 | 16.1 | 10.3 |
| 32 | 6. 30 | 7.16 | 11.3 | 56.2 | 10.8 | 39 | 68 | 33 | 4.04 | 11.4 | 19.3 | 16.1 | 18.1 | 11.7 |
| 33 | 9.05 | 3.62 | 14.8 | 49.5 | 24.8 | 39 | 56 | 33 | 4.28 | 12.0 | 12.4 | 10.8 | 21.8 | 14.5 |
| 34 | 5.149 | 6. 81 | 10.6 | 47.7 | 4.57 | 33 | 68 | 27 | 3.90 | 11.2 | 21.1 | 17.6 | 17.6 | 11.3 |
| 35 | T. 58 | 8. 51 | 12.5 | 46.5 | 11.8 | 33 | 56 | 27 | 4.12 | 11.8 | 15.7 | 12.7 | 19.8 | 13.0 |
| 36 | 10.4 | 11.0 | 15.1 | 45.8 | 24.1 | 33 | 47 | 27 | 4.39 | 12.5 | 10.7 | 8.25 | 23.3 | 15.6 |

$.100 \mathrm{nF}=.1 \mu \mathrm{~F}$


Figure 6. Highpass filter schematic diagram and attenuation response, capacitive input and output.
Table 6. 50-ohm 5-Element Chebyshev Highpass Filter Designs, Using Standard-Value Capacitors, Capacitive Input and Output. (Continued on Page 136.)

| $\begin{aligned} & \text { Filter } \\ & \text { No. } \\ & \hline \end{aligned}$ | Cutoff | Frequenc 3-dB | $\begin{gathered} \hline(\mathrm{MHz})- \\ 20-\mathrm{dB} \\ \hline \end{gathered}$ | $50 \mathrm{~dB}$ | $\begin{aligned} & \hline \mathrm{RC} \\ & (\%) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline \mathrm{C1,C5} \\ \text { (pF) } \end{gathered}$ | $\begin{gathered} \mathrm{L}, \mathrm{L4} \\ (\mu \mathrm{H}) \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{C}, \\ & \text { (pF) } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.043 | 9. 726 | 0.501 | 0.263 | 2.17 | 5109 | 6.447 | 2200 |
| 2 | 1.045 | 0.788 | 0.554 | 0.294 | 3.88 | 4300 | 5.969 | 2060 |
| 3 | 1.169 | 0.800 | 9. 550 | 0.288 | 1.94 | 4700 | 5.851 | 2000 |
| 4 | 1.070 | 0.857 | 0. 6.15 | 0.331 | 6.30 | 3600 | 5.562 | 1800 |
| 5 | 1.172 | 0.877 | 0.616 | 0.327 | 3.67 | 39010 | 5.358 | 1800 |
| 6 | 1.329 | 9.899 | 0.609 | 0.318 | 1.67 | 4300 | 5.258 | 1809 |
| 7 | 1.119 | 0.936 | 0.685 | 0.372 | 9.33 | 3000 | 5.195 | 1606 |
| 8 | 1.246 | 0.974 | 0.693 | 0.371 | 5.16 | 3300 | 4.860 | 1600 |
| 9 | 1:380 | 0.993 | 0.691 | 0.364 | 2.77 | 3650 | 4.714 | 1600 |
| 10 | 1. 541 | 1.003 | 9.683 | 0. 356 | 1.39 | 3900 | 4.669 | 1606 |
| 11 | 1. 284 | 1.828 | 0. 738 | 0.397 | 6.30 | 309日 | 4.635 | 1509 |
| 12 | 1.432 | 1.055 | 0.738 | 0.391 | 3.29 | 3300 | 4.444 | 1500 |
| 13 | 1.655 | 1.068 | 0.730 | 0.381 | 1.60 | 3600 | 4.380 | 1500 |
| 14 | 1.352 | 1.144 | 0.840 | 0.458 | 10.21 | 2406 | 4.286 | 136 |
| 15 | 1. 5.45 | 1.201 | 0.853 | 0. 4.45 | 4.93 | 2700 | 3.935 | 1308 |
| 16 | 1.754 | 1.22? | 0.848 | 0. 445 | 2.26 | 3000 | 3.812 | 1306 |
| 17 | 1.453 | 1.235 | 0.908 | 6. 496 | 15.63 | 2209 | 3.985 | 1200 |
| 18 | 1.604 | 1.285 | 0.923 | 0.496 | 6.30 | 2400 | 3.708 | 1209 |
| 19 | 1.840 | 1.325 | 0.921 | 0.486 | 2.77 | 2700 | 3.536 | 1200 |
| 20 | 2.140 | 1.340 | 0.906 | 0.476 | 1.07 | 3060 | 3.501 | 1200 |
| 21 | 1.569 | 1.348 | 0.988 | 0.540 | 11.14 | 2000 | 3.686 | 1100 |
| 22 | 1.750 | 1.402 | 1.007 | 0. 5.51 | 6.30 | 22810 | 3.399 | 1100 |
| 23 | 1.933 | 1.437 | 1.610? | 0. 534 | 3.49 | 2409 | 3.267 | 1190 |
| 24 | 2.265 | 1.460 | 0.992 | b. 516 | 1.29 | 2700 | 3.269 | 1100 |
| 25 | 1.925 | 1.542 | 1.167 | 0. 595 | 6.30 | 2006 | 3.990 | 1000 |
| 26 | 2.148 | 1.583 | 1.107 | 0.586 | 3.29 | 2201 | 2.963 | 1090 |
| 27 | 2.408 | 1.603 | 1. 695 | 0.572 | 1.60 | 2400 | 2.920 | 1009 |
| 28 | 2.090 | 1.688 | 1.216 | 0. 654 | 6.76 | 1809 | 2.832 | 910 |
| 29 | 2.357 | 1.739 | 1.217 | 日. 644 | 3.31 | 2006 | 2.697 | 910 |
| 910 | 2.675 | 1.762 | 1.252 | 6.627 | 1.519 | 2200 | 2.656 | 916 |
| 31 | 2.120 | 1.805 | 1.328 | 0.725 | 10.76 | 1506 | 2.729 | 820 |
| 32 | 2.284 | 1.863 | 1.347 | 0.727 | 7.35 | 1600 | 2.576 | 829 |
| 33 | 2.612 | 1.930 | 1.351 | 9. 315 | 3.34 | 1800 | 2.431 | 820 |
| 34 | 3.689 | 1.957 | 1.332 | 0.694 | 1,88 | 2000 | 2.393 | 820 |

Table 6. 50-ohm 5-Element Chebyshev Highpass Filter Designs
Using Standard-Value Capacitors, Capacitive Input and Output. (Continued from Page 135.)

| Filter No. | -- - - Frequency (MHz) - . - . . |  |  |  | RC$(\%)$ | $\begin{gathered} \mathrm{C1}, \mathrm{C} 5 \\ (\mathrm{pF}) \end{gathered}$ | $\begin{gathered} \mathrm{L} 2, \mathrm{~L} 4 \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \mathrm{C} \\ \text { (pF) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cutoff | 3-dB | $20-\mathrm{dB}$ | 50 dB |  |  |  |  |
| 35 | 2.567 | 2.057 | 1.476 | 0.793 | 6,301 | 1506 | 2.317 | 750 |
| 36 | 2.762 | 2.097 | 1.479 | 0.786 | 4.10 | 1600 | 2.245 | 750 |
| 37 | 3.211 | 2. 137 | 1.469 | 0.762 | 1.69 | 1890 | 2.190 | 756 |
| 38 | 2.691 | 2.227 | 1.619 | 0.877 | 8.32 | 1354 | 2.170 | 680 |
| 39 | 3.168 | 2.329 | 1.628 | 0.861 | 3.22 | 1500 | 2.813 | 680 |
| 40 | 3.443 | 2.352 | 1. 616 | 0.846 | 1.92 | 1600 | 1.989 | 680 |
| 41 | 2.993 | 2.456 | 1.779 | 0.961 | 7.72 | 1280 | 1.959 | 620 |
| 42 | 3.275 | 2.525 | 1.789 | 0. 954 | 4.62 | 1300 | 1.869 | 620 |
| 43 | 3.931 | 2.587 | 1.764 | 0.920 | 1.49 | 1560 | 1.869 | 620 |
| 44 | 3.370 | 2.736 | 1.974 | 1.064 | 7.05 | 1100 | 1.751 | 560 |
| 45 | 3.718 | 2.811 | 1.980 | 1.052 | 3.98 | 1206 | 1. 673 | 56 b |
| 45 | 4.155 | 2.852 | 1.966 | 1.032 | 2.15 | 1300 | 1.640 | 560 |
| 47 | 3.693 | 3.002 | 2. 167 | 1.168 | 7.13 | 1080 | 1.596 | 510 |
| 48 | 4.113 | 3.091 | 2.174 | 1.154 | 3.80 | 1100 | 1.520 | 510 |
| 49 | 4.596 | 3.136 | 2.155 | 1.128 | 1.92 | 1200 | 1.491 | 510 |
| 50 | 3.950 | 3.240 | 2.347 | 1.268 | 7.70 | 910 | 1.485 | 470 |
| 51 | 4.393 | 3.343 | 2.360 | 1.255 | 4.18 | 1000 | 1.408 | 470 |
| 52 | 4.945 | 3.401 | 2.340 | 1.226 | 2.01 | 1100 | 1.375 | 470 |
| 53 | 4.244 | 3.517 | 2.559 | 1.386 | 8.44 | 820 | 1.375 | 430 |
| 54 | 4.772 | 3.650 | 2.580 | 1.373 | 4.34 | 910 | 1.291 | 430 |
| 55 | 5.358 | 3.714 | 2.560 | 1.343 | 2.12 | 1009 | 1.259 | 430 |
| 56 | 4.724 | 3.893 | 2.826 | 1.528 | 8.03 | 750 | 1.239 | 390 |
| 57 | 5.223 | 4.017 | 2.844 | 1.516 | 4.54 | 820 | 1.174 | 390 |
| 58 | 5.934 | 4.097 | 2.821 | 1.479 | 2.46 | 910 | 1.142 | 390 |
| 59 | 5.014 | 4.182 | 3.051 | 1.655 | 8.93 | 680 | 1.161 | 360 |
| 60 | 5.599 | 4.341 | 3.081 | 1.645 | 4.83 | 750 | 1.088 | 360 |
| 61 | 6.228 | 4.424 | 3.066 | 1.613 | 2.51 | 820 | 1.058 | 360 |
| 62 | 5.437 | 4.550 | 3.324 | 1.806 | 9.22 | 620 | 1.069 | 330 |
| 63 | 6.033 | 4.720 | 3.361 | 1.797 | 5.20 | 680 | 1.002 | 330 |
| 64 | 6.775 | 4.825 | 3.345 | 1.761 | 2.56 | 750 | 0.970 | 330 |
| 65 | 7.702 | 4.869 | 3.297 | 1.713 | 1.14 | 820 | 0.962 | 330 |
| 66 | 5.936 | 4.988 | 3.651 | 1.985 | 9.58 | 560 | 0.978 | 300 |
| 67 | 6.658 | 5.197 | 3.697 | 1.976 | 5.10 | 620 | 0.910 | 300 |
| 68 | 7.427 | 5.395 | 3.681 | 1.938 | 2.61 | 680 | 0.882 | 300 |
| 69 | 8.558 | 5.358 | 3.622 | 1.880 | 1.07 | 750 | 0.875 | 300 |
| 70 | 6.686 | 5.576 | 4.0668 | 2.207 | 8.93 | 510 | 0.870 | 270 |
| 71 | 7.428 | 5.780 | 4.108 | 2.194 | 4.98 | 560 | 9.817 | 270 |
| 72 | 8.392 | 5.986 | 4.084 | 2.146 | 2.35 | 620 | 0.792 | 270 |
| 73 | 7.836 | 6.376 | 4.604 | 2.482 | 7.19 | 470 | 0.752 | 240 |
| 74 | 8.591 | 6.546 | 4.622 | 2.459 | 4.22 | 510 | 0.719 | 249 |
| 75 | 9.643 | 6.658 | 4.584 | 2.494 | 2.06 | 560 | 0.702 | 240 |
| 76 | 8.529 | 6.950 | 5.021 | 2.708 | 7.27 | 430 | 0.690 | 220 |
| 77 | 9.430 | 7.150 | 5.941 | 2.679 | 4.06 | 476 | 0.658 | 220 |
| 78 | 10.43 | 7.257 | 5.0106 | 2.627 | 2.17 | 510 | 0.644 | 220 |
| 79 | 9.358 | ? 6.637 | 5.521 | 2.979 | 7. 38 | 396 | 0. 628 | 200 |
| 89 | 10.45 | 7.877 | 5.544 | 2.944 | 3.88 | 430 | 0. 596 | 290 |
| 81 | 9.686 | 8.232 | 6.056 | 3. 304 | 10.63 | 339 | 0.597 | 180 |
| 82 | 10.70 | 8.569 | 6.152 | 3.305 | 6.30 | 560 | 0.556 | 180 |


(A) Schematic diagram

(B) Typical attenuation response

Figure 7. Highpass filter schematic diagram and attenuation response, capacitive input and output.
Table 7. 50-ohm 7-Element Chebyshev Highpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output. (Continued on Page 138.)

| Filter No. | - .-. - Frequency (MHz) ----- |  |  |  | $\begin{aligned} & \hline \mathrm{RC} \\ & (\%) \end{aligned}$ | $\begin{gathered} \hline \mathrm{Cl}, \mathrm{C7} \\ (\mathrm{pF}) \end{gathered}$ | $\begin{array}{r} \hline \text { L2, L6 } \\ (\mu \mathrm{H}) \\ \hline \end{array}$ | $\begin{gathered} \hline \mathrm{C} 3, \mathrm{C5} \\ (\mathrm{pF}) \end{gathered}$ | $\begin{gathered} \mathrm{L} 4 \\ (\mu \mathrm{H}) \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.022 | 0.826 | 0.660 | 0.435 | 1.76 | 5100 | 6.162 | 2000 | 4.982 |
| 2 | 1.002 | 0.880 | 0.724 | 0.489 | 5.16 | 3900 | 5.673 | 1800 | 4.855 |
| 3 | 1.079 | 0.905 | 0.732 | 0.487 | 2.80 | 4300 | 5.554 | 1800 | 4.601 |
| 4 | 1.159 | 0.922 | 0.734 | 0.482 | 1.46 | 4700 | 5.554 | 1890 | 4.449 |
| 5 | 1.086 | 0.971 | 0.806 | 0.549 | 6.84 | 3300 | 5.153 | 1600 | 4.477 |
| 6 | 1.160 | 1.002 | 0.819 | 0.559 | 4.11 | 3600 | 4.986 | 1600 | 4.216 |
| 7 | 1.232 | 1.023 | 0.824 | 0.547 | 2.44 | 3900 | 4.930 | 1600 | 4.055 |
| 8 | 1.338 | 1.043 | 0.825 | 0.539 | 1.16 | 4308 | 4.953 | 1690 | 3.921 |
| 9 | 1.139 | 1.021 | 0.853 | 0.583 | 8.10 | 3600 | 4.919 | 1590 | 4.312 |
| 10 | 1.217 | 1.061 | 0.871 | 0.587 | 4.71 | 3300 | 4.703 | 1509 | 4.006 |
| 11 | 1.299 | 1.087 | 0.879 | 0.584 | 2.71 | 3600 | 4.626 | 1500 | 3.826 |
| 12 | 1.386 | 1.106 | 0.880 | 0.578 | 1.51 | 3909 | 4.627 | 1506 | 3.713 |
| 13 | 1.344 | 1.198 | 0.994 | 0.676 | 6.58 | 2700 | 4.171 | 1300 | 3.617 |
| 14 | 1.455 | 1.242 | 1.011 | 0.676 | 3.51 | 3000 | 4.029 | 1300 | 3.379 |
| 15 | 1.567 | 1.270 | 1.016 | 0.670 | 1.82 | 3300 | 4.004 | 1300 | 3.244 |
| 16 | 1.413 | 1.277 | 1.066 | 0.729 | 8.10 | 2400 | 3.935 | 1200 | 3.449 |
| 17 | 1.546 | 1.336 | 1.092 | 0.734 | 4.11 | 2700 | 3.739 | 1299 | 3.162 |
| 18 | 1.677 | 1.372 | 1.100 | 0.727 | 2.04 | 3000 | 3.695 | 1200 | 3.011 |
| 19 | 1.541 | 1.393 | 1.163 | 0.795 | 8.10 | 2200 | 3.607 | 1190 | 3.162 |
| 20 | 1.649 | 1.443 | 1.186 | 0.800 | 4.95 | 2400 | 3.458 | 1190 | 2.953 |
| 21 | 1.802 | 1.490 | 1.200 | 0.795 | 2.32 | 2709 | 3.388 | 1190 | 2.779 |
| 22 | 1.973 | 1.520 | 1.199 | 0.782 | 1.02 | 3000 | 3.412 | 1100 | 2.684 |
| 23 | 1. 695 | 1.532 | 1.279 | 0.875 | 8.10 | 2009 | 3.279 | 1800 | 2.874 |
| 24 | 1.825 | 1.592 | 1.307 | 0.881 | 4.71 | 2206 | 3.135 | 1064 | 2.671 |
| 25 | 1.948 | 1.631 | 1.318 | 0.877 | 2.71 | 2409 | 3.684 | 1000 | 2.551 |
| 26 | 2.159 | 1.669 | 1.320 | 0.862 | 1.11 | 2700 | 3.097 | 1090 | 2.447 |
| 27 | 1.846 | 1. 674 | 1.400 | 6. 959 | 8.60 | 1800 | 3.507 | 910 | 2.644 |
| 28 | 2.004 | 1.748 | 1.436 | 0.968 | 4.74 | 2000 | 2.854 | 910 | 2.432 |
| 29 | 2.153 | 1.795 | 1.449 | 0.963 | 2.58 | 2296 | 2.805 | 919 | 2.314 |
| 30 | 2.312 | 1.827 | 1.451 | 0.951 | 1.35 | 2406 | 2.810 | 910 | 2.242 |
| 31 | 2.025 | 1.845 | 1. 547 | 1.062 | 9.25 | 1600 | 2.737 | 820 | 2.415 |
| 32 | 2.222 | 1.940 | 1.593 | 1.074 | 4.78 | 1806 | 2.573 | 820 | 2.193 |
| 33 | 2.496 | 1.997 | 1.609 | 1.067 | 2. 43 | 2009 | 2.525 | 820 | 2.077 |
| 34 | 2.606 | 2.934 | 1.610 | 1.053 | 1.17 | 2209 | 2.538 | 829 | 2.910 |
| 35 | 2.260 | 2.043 | 1.705 | 1.166 | 8.10 | 1598 | 2.459 | 750 | 2.156 |
| 36 | 2.377 | 2.099 | 1.733 | 1.173 | 5.65 | 1600 | 2.377 | 750 | 2.045 |
| 3 | 2.598 | 2.175 | 1.757 | 1.169 | 2.71 | 1806 | 2.313 | 750 | 1.913 |
| 38 | 2.834 | 2.221 | 1. 760 | 1.152 | 1.24 | 2056 | 2.319 | 750 | 1.842 |

Table 7. 50-ohm 7-Element Chehyshev Highpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output. (Continued from Page 137.)

| Filter No. | . .-. . . Frequency (MHz) - . . . . . |  |  |  | RC <br> (\%) | $\begin{gathered} (\mathrm{pF}) \\ \mathrm{C} 1, \mathrm{C} 7 \end{gathered}$ | $\begin{gathered} \text { L2, L6 } \\ (\mu \mathrm{H}) \end{gathered}$ | $\begin{gathered} \text { C3, C5 } \\ (\mathrm{pF}) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{L4} \\ (\mu \mathrm{H}) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Cutoff | 3-dB | 20-dB | 50-dB |  |  |  |  |  |
| 39 | 2.689 | 2.343 | 1.922 | 1.295 | 4.6 .4 | 1506 | 2.130 | 680 | 1.813 |
| 40 | 2.822 | 2.387 | 1.936 | 1.291 | 3.69 | 1606 | 2.161 | 689 | 1.750 |
| 41 | 3.105 | 2.447 | 1.941 | 1.272 | 1.31 | 1800 | 2.101 | 680 | 1. 673 |
| 42 | 2. 660 | 2.429 | 2.040 | 1.402 | 9.66 | 1200 | 2.082 | 620 | 1.842 |
| 43 | 2.838 | 2. 523 | 2.089 | 1.418 | 6.23 | 1300 | 1.986 | 620 | 1.712 |
| 44 | 3.162 | 2. 636 | 2.127 | 1. 413 | 2.57 | 1509 | 1.911 | 620 | 1. 576 |
| 45 | 3.331 | 2. 671 | 2.130 | 1.401 | 1. 61 | 1600 | 1.911 | 620 | 1.538 |
| 46 | 2.982 | 2.711 | 2.270 | 1. 557 | 8.93 | 1100 | 1.859 | 560 | 1. 6.38 |
| 47 | 3.195 | 2.816 | 2.323 | 1.572 | 5.50 | 1200 | 1.772 | 560 | 1. 522 |
| 48 | 3.392 | 2.888 | 2.348 | 1.570 | 3.38 | 1309 | 1.734 | 560 | 1.451 |
| 49 | 3.810 | 2.977 | 2.357 | 1.542 | 1.19 | 1500 | 1.732 | 560 | 1.373 |
| 50 | 3.269 | 2.974 | 2.491 | 1.709 | 9.01 | 1600 | 1.696 | 510 | 1.494 |
| 51 | 3.525 | 3.160 | 2. 553 | 1.726 | 5.30 | 1100 | 1.610 | 510 | 1.380 |
| 52 | 3.763 | 3.183 | 2.581 | 1.722 | 3.69 | 1200 | 1.576 | 510 | 1.312 |
| 53 | 4.008 | 3.240 | 2.589 | 1.786 | 1.76 | 1300 | 1.571 | 510 | 1.270 |
| 54 | 3.510 | 3.205 | 2.691 | 1.850 | 9.64 | 910 | 1.578 | 470 | 1.396 |
| 55 | 3.786 | 3.347 | 2,764 | 1.872 | 5.73 | 1000 | 1.491 | 470 | 1.283 |
| 56 | 4.067 | 3.449 | 2.800 | 1.869 | 3.20 | 1100 | 1. 453 | 470 | 1.213 |
| 57 | 4.355 | 3.517 | 2.810 | 1.851 | 1.74 | 1200 | 1.448 | 470 | 1.170 |
| 58 | 4.121 | 3.651 | 3.017 | 2.045 | 5.91 | 910 | 1.367 | 430 | 1.179 |
| 59 | 4.424 | 3.763 | 3.058 | 2.044 | 3.34 | 1003 | 1.331 | 430 | 1.113 |
| 60 | 4.768 | 3.846 | 3.071 | 2.023 | 1.72 | 1100 | 1.325 | 430 | 1.070 |
| 61 | 4.205 | 3.848 | 3.235 | 2.226 | 9.99 | 750 | 1.317 | 390 | 1.167 |
| 62 | 4.521 | 4.015 | 3.322 | 2.255 | 6.14 | 820 | 1.244 | 390 | 1.074 |
| 63 | 4.890 | 4.153 | 3.373 | 2.253 | 3.27 | 910 | 1.206 | 390 | 1.008 |
| 64 | 5.267 | 4.242 | 3.386 | 2.230 | 1.69 | 1000 | 1.202 | 390 | 0.969 |
| 65 | 4.864 | 4.333 | 3.592 | 2.441 | 6.46 | 759 | 1.153 | 360 | 0.999 |
| 66 | 5.202 | 4.469 | 3.646 | 2.444 | 3.81 | 820 | 1.118 | 360 | 0.942 |
| 67 | 5.639 | 4.582 | 3.668 | 2.420 | 1.88 | 910 | 1.108 | 360 | 0.899 |
| 68 | 5.260 | 4.706 | 3.908 | 2.660 | 6.87 | 680 | 1.963 | 330 | 0.924 |
| 69 | 5. 666 | 4.872 | 3.976 | 2. 667 | 3.86 | 750 | 1.926 | 330 | 0.864 |
| 70 | 6.067 | 4.981 | 4.000 | 2. 646 | 2.13 | 820 | 1.916 | 330 | 0.829 |
| 71 | 5.809 | 5.183 | 4.302 | 2.927 | 6.76 | 620 | 0. 965 | 300 | 0.838 |
| 72 | 6.220 | 5.355 | 4.372 | 2.934 | 3.93 | 680 | 0.933 | 300 | 0.787 |
| 73 | 6.706 | 5.487 | 4.401 | 2.909 | 2.04 | 750 | 0.923 | 300 | 0.752 |
| 74 | 7. 249 | 5.576 | 4.397 | 2.867 | 1.00 | 820 | 0.931 | 300 | 0.731 |
| 75 | 6.462 | 5.767 | 4.784 | 3.253 | 6.63 | 560 | 0.867 | 270 | 0.752 |
| 76 | 6.979 | 5.972 | 4.865 | 3. 258 | 3.62 | 620 | 9.837 | 270 | 0.703 |
| 77 | 7.496 | 6.105 | 4.890 | 3.229 | 1.93 | 680 | 0.831 | 279 | 0.675 |
| 78 | 6.940 | 6.315 | 5.292 | 3.631 | 9.07 | 470 | 0.798 | 246 | 0.704 |
| 79 | 7.407 | 6.551 | 5.411 | 3.666 | 5.78 | 510 | 0.762 | 240 | 0.656 |
| 80 | 7.946 | 6.748 | 5. 481 | 3.661 | 3.27 | 569 | 0.742 | 240 | 0.620 |
| 81 | 8. 612 | 6.903 | 5.592 | 3.619 | 1.59 | 520 | 0.740 | 240 | 0. 595 |
| 82 | 7.559 | 6.883 | 5.769 | 3.960 | 9.17 | 430 | 0.733 | 220 | 0. 0.646 |
| 83 | 8.113 | 7.161 | 5.909 | 4.0005 | 5.60 | 470 | 0.697 | 220 | 0. 599 |
| 84 | 8.626 | ?. 349 | 5.976 | 3.996 | 3.41 | 510 | 0.681 | 220 | 0.570 |
| 85 | 9. 280 | 7.509 | 6.002 | 3.957 | 1.78 | 560 | 0. 677 | 220 | 0.548 |
| 86 | 8.298 | 7.561 | 6.341 | 4.353 | 9.28 | 395 | 0. 067 | 200 | 0.589 |
| 87 | 8.968 | 7.895 | 6.508 | 4.401 | 5.45 | 430 | 0.632 | 200 | 0.542 |
| 88 | 9.587 | 8.113 | 6.581 | 4.391 | 3.12 | 479 | 0.618 | 2010 | 0.515 |
| 89 | 10.22 | 8.263 | 6.603 | 4.351 | 1.75 | 510 | 0.616 | 260 | 0.498 |
| 95 | 9.417 | 8.511 | 7.195 | 4.859 | 8.10 | 364 | 0. 596 | 180 | 0. 517 |
| 91 | 15.62 | 8.796 | 7. 241 | 4.891 | 5.16 | 399 | 0. 567 | 180 | 0.485 |
| 92 | 10.79 | 9.051 | 7. 321 | 4.873 | 2.80 | 436 | 5.555 | 180 | 5.460 |



Figure 8. 50-ohm 5-th degree elliptic highpass filter designs using standard-value capacitors for C1, C3 and C5.

Table 8A. 50 -ohm 5th-Degree Elliptic Highpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output. (Continued on Page 140.)

| Filter No. |  |  |  | $\begin{gathered} \mathrm{A}_{\mathrm{s}} \\ (\mathrm{~dB}) \end{gathered}$ | RC <br> (\%) | C1 | C3 |  | C2 | C4 | $\begin{aligned} & \mathrm{L} 2 \\ & \cdots(\mu \mathrm{H}) \end{aligned}$ | $\stackrel{L 4}{(H)-}$ | $\begin{aligned} & \text { F2 } \\ & \text { (M1 } \end{aligned}$ | F4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.79 | 0.74 | 0.50 | 49.6 | 20.7 | 3.3 | 2.2 | 3.9 | 30.5 | 10.8 | 8.28 | 10.2 | 0.32 | 0.48 |
| 2 | 0.93 | 0.84 | 0.63 | 41.0 | 12.9 | 3.6 | 2.2 | 4.7 | 21.5 | 7.26 | 7.09 | 9.46 | 0.41 | 0.61 |
| 3 | 0.92 | 0.80 | 0.53 | 48.1 | 9.80 | 3.9 | 2.2 | 4.? | 34.6 | 11.9 | 6.86 | 8.32 | 0.33 | 0.51 |
| 4 | 1.02 | 0.86 | 0.60 | 42.4 | 5.92 | 4.3 | 2.2 | 5.6 | 27.7 | 9.34 | 6.44 | 8.18 | 0.38 | 0.58 |
| 5 | 1.04 | 0.82 | 0.48 | 50.5 | 3.73 | 4.7 | 2.2 | 5.6 | 45.6 | 16.0 | 6.36 | 7.49 | 0. 30 | 0. 46 |
| 6 | 1.15 | 0.86 | 0.58 | 42.3 | 2.27 | 5.1 | 2.2 | 6.8 | 32.1 | 10.7 | 6.26 | 7.77 | 0.36 | 0.55 |
| 7 | 0.97 | 0.90 | 0.69 | 40.8 | 18.2 | 3.0 | 2.0 | 3.9 | 17.6 | 5.93 | 7.03 | 9.58 | 0. 45 | 0.67 |
| 8 | 0.95 | 0.85 | 0.55 | 49.9 | 13.8 | 3.3 | 2.6 | 3.9 | 31.4 | 11.1 | 6.67 | 8.04 | 0.35 | 0.53 |
| 9 | 1.08 | 0.94 | 0.68 | 41.6 | 8.67 | 3.6 | 2.0 | $4 . ?$ | 22.4 | 7. 53 | 6.06 | 7.87 | 0.43 | 0.65 |
| 10 | 1.98 | 0.90 | 0.57 | 48.7 | 6.17 | 3.9 | 2.0 | 4.7 | 34.9 | 12.2 | 5.93 | 7.07 | 0.35 | 0.54 |
| 11 | 1.19 | 0.94 | 0.63 | 43.1 | 3.57 | 4.3 | 2.0 | 5. 6 | 28.6 | 3.62 | 5.73 | 7.12 | 6. 39 | 0.61 |
| 12 | 1.28 | 0.94 | 0.62 | 43.0 | 2.06 | 4.7 | 2.6 | 6.2 | 30.7 | 10.3 | 5.69 | 7.00 | 0.38 | 0.59 |
| 13 | 1.01 | 0.94 | 0.67 | 45.9 | $19 . ?$ | $2 . ?$ | 1.8 | 3.3 | 20.7 | 7.24 | 6.58 | 8.40 | 0.43 | 0.65 |
| 14 | 0.98 | 0.88 | 0.47 | 61.3 | 14.7 | 3.6 | 1.8 | 3.3 | 50.2 | 18.4 | 6.22 | 6.94 | 0.28 | 0.45 |
| 15 | 1.14 | 0.98 | 0.61 | 50.4 | 8.50 | 3.3 | 1.8 | 3.9 | 32.3 | 11.4 | 5.53 | 6.54 | 0.38 | 0.58 |
| 16 | 1.27 | 1.05 | 0.73 | 42.4 | 5.27 | 3.6 | 1.8 | 4.7 | 23.2 | 7.80 | 5.23 | 6.62 | 0.46 | 0.79 |
| 17 | 1.39 | 1.01 | 0.60 | 49.4 | 3.42 | 3.9 | 1.8 | $4 . ?$ | 35.8 | 12.5 | 5.19 | 6.07 | 0.37 | 0.58 |
| 18 | 1.33 | 1.05 | 0.71 | 42.9 | 3.42 | 3.9 | 1.8 | 5.1 | 25.6 | 8.60 | 5.15 | 6.40 | 0.44 | 0.68 |
| 19 | 1.02 | 0.94 | 0.57 | 56.8 | $22 . ?$ | 2.4 | 1.6 | 2.7 | 31.7 | 11.5 | 6.36 | 7.38 | 9. 35 | 9.55 |
| 20 | 1.13 | 1.01 | 0.55 | 59.3 | 13.6 | 2.7 | 1.6 | 3.0 | 40.9 | 15.8 | 5.41 | 6.09 | 9.34 | 0.53 |
| 21 | 1.24 | 1.11 | 0.76 | 46.5 | 12.1 | 2.7 | 1.6 | 3.3 | 21.6 | 7.52 | 5.15 | 6.39 | 9. 48 | 9.73 |
| 22 | 1.37 | 1.18 | 0.83 | 42.2 | 7.22 | 3.8 | 1.6 | 3.9 | 19.2 | 6.47 | 4.76 | 6.09 | 0.53 | 0.80 |
| 23 | 1.39 | 1.12 | 0.66 | 51.1 | 4.59 | 3.3 | 1.6 | 3.9 | 33.2 | 11.7 | 4.67 | 5.43 | 9. 46 | 9. 63 |
| 24 | 1.54 | 1.18 | 0.78 | 43.3 | 2.73 | 3.6 | 1.6 | 4.7 | 24.9 | 8.08 | 4.56 | 5.62 | 0.48 |  |
| 25 | 1.19 | 1.11 | 0.81 | 45.4 | 21.3 | 2.2 | 1.5 | $2 . ?$ | 16.4 | 5.71 | 5.65 | 7.28 | 9.52 | 9. 78 |
| 26 | 1.16 | 1.06 | 0.62 | 56.9 | 17.9 | 2.4 | 1.5 | $2 . ?$ | 32.2 | 11.7 | 5.37 | 6.17 | 0.38 | 0.59 |
| 27 | 1.38 | 1.20 | 0.80 | 46.8 | 9.03 | $2 . ?$ | 1.5 | 3.3 | 22.1 | 7.66 | 4.61 | 5.65 | 0.50 | 0.77 |
| 28 | 1.45 | 1.27 | 0.94 | 40.3 | 8.59 | 2.7 | 1.5 | 3.6 | 15.6 | 5.20 | 4.53 | 5.99 | 9. 54 | 0.98 0.83 |
| 29 | 1.52 | 1.26 | 0.87 | $42 . ?$ | 5.28 | 3.0 | 1.5 | 3.9 3.9 |  | 6.61 11.9 |  |  |  | 0.86 |
| 30 | 1.56 | 1.19 | 0.69 | 51.6 | 3.11 | 3.3 | 1.5 | 3. | 33.7 | 11.9 | 4.32 | 4.97 | 0.42 | 0.66 |

Table BA. 50-0hm 5-th Degree Elliptic Highpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output.
(Continued from Page 139.)

| Filter F <br> No. |  |  | $\begin{gathered} \mathrm{A}_{\mathrm{S}} \\ (\mathrm{~dB}) \end{gathered}$ | RC <br> (\%) | C1 | C3 |  | C2 | C4 | L2 | $\begin{gathered} \mathrm{L4} \\ (\mu \mathrm{H}) \cdots \end{gathered}$ | F2 $\cdots(1)$ | $\begin{gathered} \mathrm{F} 4 \\ \mathrm{~Hz}) \\ \cdots \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 311.29 | 1.23 | 0.91 | 45.7 | 26.9 | 1.8 | 1.3 | 2. |  |  |  |  |  |  |
| 321.25 | 1.15 | 0.63 | 61.3 | 21.3 | 2.0 | 1.3 | 2.2 | 33.6 | 12 | 5.07 | 5. | 10. 39 |  |
| 331.53 | 1.37 | 0.94 | 46.1 | 11.9 | 2.2 | 1.3 | 2.7 | 17.2 | 6.00 | 4.17 | 5.19 | 9.59 |  |
| 341.64 | 1.41 | 0.96 | 45,0 | 7.91 | 2.4 | 1.3 | 3.0 | 17.8 | 6.13 | 3.92 | 4.87 | 0.69 | 9.92 |
| 351.75 | 1.40 | 0.88 | 47.8 | 4.37 | 2.7 | 1.3 | 3.3 | 22.9 | 7.95 | 3.77 | 4.50 | 9.54 | 9.84 |
| 361.81 | 1.47 | 1.03 | 41.4 | 4.33 | 2.7 | 1.3 | 3.6 | 16.4 | 5.47 | 3.74 | 4.76 | 0.64 | 0.99 |
| 371.51 | 1.40 | 1.01 | 45.9 | 19.7 | 1.8 | 1.2 | 2.2 | 13.8 | 4.82 | 4.39 | 5.60 | 9. 65 |  |
| 381.47 | 1.32 | 0.70 | 61.3 | 14.7 | 2.0 | 1.2 | 2.2 | 33.5 | 12.3 | 4.15 | 4.62 | 9.43 | 9.67 |
| 391.61 | 1.44 | 0.96 | 48.2 | 13.8 | 2.9 | 1.2 | 2.4 | 17.5 | 6.16 | 3.93 | 4.81 | 9. 51 | 9.93 |
| $40 \quad 1.75$ | 1.51 | 1.000 | 46.6 | 8.27 | 2.2 | 1.2 | 2.7 | 17.7 | 6.14 | 3.65 | 4.47 | 0.63 | 0.96 |
| 411.87 | 1.54 | 1.01 | 45.6 | 5.33 | 2.4 | 1.2 | 3.0 | 18.2 | 6.27 | 3.51 | 4.29 | 0.63 | 0.97 |
| 422.02 | 1.52 | 6.92 | 48.3 | 2.69 | 2.7 | 1.2 | 3.3 | 23.4 | 8.69 | 3.44 | 4.04 | 0.56 | 0.88 |
| 431.42 | 1.33 | 0.81 | 56.9 | 26.01 | 1.6 | 1.1 | 1.8 | 21.9 | 7.65 | 4.66 | 5.43 | 0. 51 | 0.78 |
| $44 \quad 1.65$ | 1.55 | 1.15 | 43.7 | 21.5 | 1.6 | 1.1 | 2.0 | 10.9 | 3.76 | 4.13 | 5.45 | 0.75 | 1.11 |
| 451.60 | 1.44 | 0.80 | 59.2 | 15.7 | 1.8 | 1.1 | 2.0 | 27.1 | 9.92 | 3.86 | 4.36 | 0.49 | 9.77 |
| 461.76 | 1.59 | 1.10 | 46.3 | 13.8 | 1.8 | 1.1 | 2.2 | 14.2 | 4.96 | 3.64 | 4.55 | 9.70 | 1.06 |
| $\begin{array}{lll}47 & 1.87 \\ 48 & 2.87\end{array}$ | 1.61 | 1.04 | 48.? | 8.74 | 2.9 | 1.1 | 2.4 | 17.9 | 6.30 | 3.38 | 4.06 | 0.65 | 0.99 |
| $48 \quad 2.02$ | 1.66 | 1.06 | 47.1 | 5.36 | 2.2 | 1.1 | 2.7 | 18.1 | 6.28 | 3.22 | 3.88 | 9.66 | 1.02 |
| $49 \quad 1.48$ | 1.38 | 0.66 | 69.6 | 25.8 | 1.5 | 1.0 | 1.6 | 36.6 | 13.7 | 4.32 | 4.69 | 9.40 |  |
| 501.78 | 1.65 | 1.15 | 47.8 | 20.2 | 1.5 | 1.0 | 1.8 | 12.7 | 4.47 | 3.71 | 4.64 | 9.73 | 1.10 |
| 511.92 | 1.65 | 0.88 | 59.5 | 9.91 | 1.8 | $1 . \square$ | 2.0 | 27.6 | 10.1 | 3.18 | 3.55 | 9. 54 | 0.84 |
| $52 \quad 2.07$ | 1.80 | 1.20 | 46.8 | 9.03 | 1.8 | 1.0 | 2.2 | 14.7 | 5.11 | 3.07 | 3.77 | 9.75 | 1.15 |
| 532.18 | 1.91 | 1.41 | 40.3 | 8.59 | 1.8 | 1.0 | 2.4 | 10.4 | 3.47 | 3.02 | 3.99 | 0.96 | 1.35 |
| 542.45 | 1.93 | 1.34 | 40.6 | 3.15 | 2.2 | 1.6 | 3.0 | $12 . ?$ | 4.20 | 2.85 | 3.63 | 9.84 | 1.29 |
| 551.93 | 1.81 | 1.34 | 45.1 | 23.5 | 1.3 | 0.91 | 1.6 | 9.45 | 3.29 | 3.56 | 4.64 | 9.87 | 1.29 |
| 56.2 .11 | 1.98 | 1.27 | 48.2 | 13.6 | 1.5 | 0.91 | 1.8 | 13.1 | 4.60 | 3.02 | 3.69 | 9.80 | 1.22 |
| 572.69 | 1.82 | 1.02 | 57.1 | 11.0 | 1.6 | 0.91 | 1.8 | 21.9 | 7.94 | 2.93 | 3.33 | 0. 6.6 | 6.98 |
| 582.42 | 2.00 | 1.28 | 47.4 | 5.69 | 1.8 | 0.91 | 2.2 | 15.1 | 5.24 | 2.68 | 3.22 | 0.79 | 1.23 |
| 592.51 | 2.10 | 1.50 | 41.0 | 5.55 | 1.8 | 0.91 | 2.4 | 10.8 | 3.59 | 2.65 | 3.41 | 0.94 | 1.44 |
| $60 \quad 2.84$ | 2.00 | 1.18 | 48.5 | 1.62 | 2.2 | 0.91 | 2.7 | 19.0 | 6.56 | 2.60 | 3.93 | 0.72 | 1.1 .3 |
| 612.22 | 2.08 | 1.55 | 43.7 | 21.0 | 1.2 | 0.82 | 1.5 | 8.19 | 2.83 | 3.05 | 4.02 | 1.01 | 1.49 |
| $62 \quad 2.33$ | 2.12 | 1.50 | 45.5 | 15.6 | 1.3 | 0.82 | 1.6 | 9.83 | 3.42 | 2.79 | 3.54 | 8.96 | 1.45 |
| $63 \quad 2.52$ | 2.17 | 1.39 | 48.7 | 8.49 | 1.5 | 0.82 | 1.8 | 13.5 | 4.73 | 2.51 | 3.01 | 0.87 | 1.33 |
| 642.69 | 2.25 | 1.50 | 45.4 | 6.05 | 1.6 | 0.82 | 2.0 | 12.1 | 4.15 | 2.42 | 2.97 | 6.93 | 1.43 |
| 652.89 | 2.23 | 1.36 | 48.2 | 3.15 | 1.8 | 0.82 | 2.2 | 15.5 | 5.37 | 2.36 | 2.78 | 9.83 | 1.30 |
| $66 \quad 2.97$ | 2.33 | 1.59 | 41.8 | 3.18 | 1.8 | 0.82 | 2.4 | 11.1 | 3.71 | 2.34 | 2.94 | 0.99 | 1.52 |
| 67. 2. 27 | 2.12 | 1.45 | 49.6 | 22.7 | 1.1 | Q. 75 | 1.3 | 10.1 | 3.59 | 2.93 | 3,62 |  | 1.40 |
| 68.2 .60 | 2.37 | 1.79 | 44.2 | 14.? | 1.2 | 0.75 | 1.5 | 8.48 | 2.92 | 2. 51 | 3.22 | 1.99 | 1.64 |
| 69 2.56 | 2.26 | 1.37 | 53.2 | 11.4 | 1.3 | 0.75 | 1.5 | 14.6 | 5.24 | 2.42 | 2.82 | 0.85 | 1.31 |
| 70.2 .93 | 2.40 | 1.48 | 49.2 | 5.35 | 1.5 | 0. 75 | 1.8 | 13.8 | 4.82 | 2.20 | 2.61 | 0.91 | 1.42 |
| $? 17.3 .12$ | 2.47 | 1.58 | 46.6 | 3.74 | 1. 6 | Q. 75 | 2.8 | 12.4 | 4.25 | 2.16 | 2.61 | 0.97 | 1.51 |
| $72 \quad 3.42$ | 2.43 | 1.43 | 48.8 | 1.71 | 1.8 | 0.75 | 2.2 | 15.8 | 5.47 | 2.14 | 2.50 | 0.86 | 1.36 |
| $73 \quad 2.57$ | 2.40 | 1.68 | 47.8 | 21.9 | 1.0 | 0.68 | 1.2 | 8.40 | 2.96 | 2.60 | 3.27 | 1.08 |  |
| 742.49 | 2.26 | 1.17 | 63.2 | 17.1 | 1.1 | 0. 68 | 1.2 | 20.1 | 7.40 | 2.46 | 2.73 | 0.72 | 1.12 |
| $75 \quad 3.05$ | 2.68 | 1.85 | $44 . ?$ | 9.72 | 1.2 | 0.68 | 1.5 | 8.77 | 3.02 | 2.19 | 2.64 | 1.1? | 1.78 |
| 763.05 | 2.56 | 1.48 | 53.6 | 7.02 | 1.3 | 0.68 | 1.5 | 14.9 | 5.34 | 2.05 | 2.36 | 0.91 | 1.42 |



Table 8A. 50-0hm 5-th Degree Elliptic Highpass Filter Designs Using Standard-Value Capacitors, Capacitive Input and Output. (Continued from Page 141.)

| Filter No. | $\mathrm{F}-\mathrm{CO}$ | $\begin{aligned} & \text { F-3 dB } \quad \text { F-A } \\ & =(\mathrm{MHz}) \end{aligned}$ | $\begin{gathered} \mathrm{A}_{\mathrm{S}} \\ (\mathrm{~dB}) \end{gathered}$ | RC <br> (\%) | C1 | C3 | $\begin{aligned} & \text { C5 } \\ & -(n F) \end{aligned}$ | C2 | C4 |  | L4 $\mu \mathrm{H})=$ | $\begin{aligned} & \text { F2 F4 } \\ & -(\mathrm{MHz})= \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 123 | 5.99 | 5.343 .60 | 47.1 | 11.8 | 0.56 | 0.33 | 0.68 | 4.63 | 1.62 | 1.06 | 1.31 | 2.273 .46 |
| 124 | 6.72 | 5.764 .15 | 41.1 | 7.11 | 0.62 | 0.33 | 0.82 | 3.74 | 1.25 | 0.98 | 1.27 | 2.633 .99 |
| 125 | 6.81 | 5.483 .37 | 49.0 | 4.58 | 0.68 | 0.33 | 0.82 | 6. 15 | 2.15 | 0.96 | 1.13 | 2.073 .22 |
| 126 | 8.07 | 5.503 .17 | 49.3 | 1.301 | 0.82 | 0.33 | 1.0 | 7.33 | 2.54 | 0.94 | 1.09 | 1.913 .02 |
| 127 | 6.25 | 5.884 .61 | 40.4 | 21.5 | 0.43 | 0.30 | 9. 56 | 2.45 | 0.83 | 1.12 | 1.55 | 3.054 .45 |
| 128 | 5.40 | 4.952 .54 | 64.5 | 20.2 | 0.47 | 0.30 | 0. 51 | 9.09 | 3.36 | 1.15 | 1.27 | 1.562 .43 |
| 129 | 6.10 | 5.593 .77 | 48.8 | 17.1 | 0.47 | 0.30 | 0. 0.56 | 4.20 | 1.48 | 1.06 | 1.30 | 2.393 .63 |
| 130 | 6.00 | 5.312 .77 | 61.7 | 13.4 | 0. 0.51 | 0.38 | 0. 5.56 | 8.73 | 3.21 | 1.01 | 1.13 | 1.692 .65 |
| 131 | 7.03 | 6.003 .89 | 47.7 | 7.64 | 0.56 | 0.36 | 0.68 | 4.76 | 1. 66 | 0.91 | 1.69 | 2. 423.73 |
| 132 | 8.08 | 6.043 .56 | 49.7 | 2.56 | 0.68 | 0.30 | 0.82 | 6.29 | 2.19 | 0.86 | 1.00 | 2.163 .40 |
| 133 | 6.38 | 5.994 .26 | 47.3 | 23.3 | 0. 39 | 0.27 | 0.47 | 3.18 | 1.12 | 1.06 | 1.34 | 2.744 .10 |
| 134 | 6.19 | 5.632 .97 | 62.7 | 18.4 | 6.43 | 0.27 | 0.47 | 7.65 | 2.82 | 1. 0.06 | 1.11 | 1.822 .84 |
| 135 | 7.34 | 6.474 .18 | 49.2 | 10.8 | 0. 47 | 0.27 | 0. 56 | 4.33 | 1.53 | 0.86 | 1.03 | 2.614 .01 |
| 136 | 8.26 | 7.085 .13 | 40.6 | 6.92 | 0.51 | 0.27 | 0. 68 | 3.09 | 1.60 | 0.80 | 1.04 | 3.254 .93 |
| 137 | 8.39 | 6.734 .17 | 48.4 | 4.41 | 0.56 | 0.27 | 0.68 | 4.90 | 1.71 | 0.78 | 0.93 | 2.574 .00 |
| 138 | 9.30 | 7.024 .67 | 42.7 | 2.40 | 10.62 | 0.27 | 0.82 | 3.99 | 1.33 | 0.77 | 0.95 | 2.874 .47 |
| 139 | E. 36 | 5.923 .08 | 65.0 | 24.8 | 0.36 | 0. 24 | 0. 39 | 7.06 | 2. 62 | 1.01 | 1.12 | 1.892 .94 |
| 140 | 8. 68 | 7.525 .81 | 40.4 | 18.1 | 0.36 | 0.24 | 0. 47 | 2.07 | 9. 70 | 0.84 | 1.15 | 3.815 .61 |
| 141 | 7.94 | 7.184 .87 | 47.7 | 14.4 | 0.39 | 0. 24 | 0. 47 | 3:31 | 1.16 | 0.80 | 0.99 | 3.084 .68 |
| 142 | 8.40 | 7.304 .62 | 49.9 | 9.46 | 0.1 .43 | 0.24 | 0. 51 | 4:10 | 1.45 | 0.75 | 0.89 | 2.884 .43 |
| 143 | 8.97 | 7.444 .58 | 49.9 | 6. 06 | 0.47 | 0.24 | 0. 56 | 4.47 | 1.57 | 0.71 | 日. 84 | 2.824 .38 |
| 144 | 9.94 | 7.965 .51 | 41.6 | 3.82 | 0.51 | 0.24 | 0.68 | 3.13 | 1.04 | 0.69 | 0.87 | 3.435 .29 |

Table 8B. 600-ahm 5th-Degree Elliptic Highpass-Filter Designs Using Stanard-Value Capacitors, Capacitor Input and Output.

| $\begin{aligned} & \text { Filter } \\ & \text { No. } \end{aligned}$ |  | $\begin{gathered} \mathrm{F}-3 \mathrm{~dB} \\ -(\mathrm{kHz}) \end{gathered}$ | $\mathrm{F}-\mathrm{A}_{\mathrm{S}}$ | $\begin{aligned} & \mathrm{A}_{\mathrm{S}} \\ & (\mathrm{~dB}) \end{aligned}$ | $\begin{aligned} & \mathrm{RC} \\ & (\%) \end{aligned}$ |  | C3 | C5 | $\mathrm{C} 2$ | C4 |  | $\begin{gathered} \mathrm{L} 4 \\ (\mathrm{mH}) \ldots \end{gathered}$ | $\begin{array}{cc} \hline \text { F2 } & \text { F4 } \\ --(k H z) & \cdots \\ \hline \end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | E. 60 | 6.13 | 4.15 | 49.6 | 20.7 | 33 | 22 | 39 | 305 | 168 | 11.9 | 14.6 | 2.64 | 3.99 |
| 2 | 7. 8.7 | 6.71 | 4.39 | 48.1 | 9.80 | 39 | 22 | 47 | 346 | 119 | 9.88 | 12.0 | 2.75 | 4.21 |
| 3 | 8.70 | 5.81 | 4.93 | 50.5 | 3.73 | 47 | 22 | 56 | 456 | 160 | 9.17 | 10.7 | 2.46 | 3.85 |
| 4 | 8.401 | 7.80 | 5.59 | 45.9 | 19.7 | 27 | 18 | 33 | 207 | 72.4 | 9.48 | 12.1 | 3.59 | 5.38 |
| 5 | 9.47 | 8.13 | 5, 06 | 50.4 | 8.501 | 33 | 18 | 39 | 323 | 114 | 7.96 | 9.42 | 3.14 | 4.85 |
| 5 | 10.8 | 8. 39 | 5.514 | 49.4 | 3.42 | 39 | 18 | 47 | 358 | 125 | 7.47 | 8.74 | 3.08 | 4.82 |
| 7 | 11.1 | 8.76 | 5.96 | 42.9 | 3.42 | 39 | 18 | 51 | 256 | 86.0 | 7.42 | 9.22 | 3.65 | 5.65 |
| 8 | 9.94 | 9.29 | 6.75 | 45.4 | 21.3 | 22 | 15 | 27 | 164 | 57.1 | 8.13 | 10.5 | 4.36 | 6. 50 |
| 9 | 11.5 | 9.98 | E. 64 | 46.8 | 9.80 | 27 | 15 | 33 | 220 | 76.E | 6. 64 | 8.13 | 4.16 | 6.38 |
| 19 | 12.1 | 18.6 | 7.81 | 40.3 | 8.59 | 27 | 15 | 36 | 156 | 52.0 | 6.52 | 8.62 | 4.99 | 7.52 |
| 11 | 13.5 | 9.95 | 5.71 | 51.6 | 3.11 | 33 | 15 | 39 | 337 | 119 | 6.22 | 7.16 | 3.47 | 5.46 |
| 12 | 12.5 | 11.7 | B.38 | 45.9 | 19.7 | 18 | 12 | 22 | 138 | 48.2 | 6.32 | 8. 0.6 | 5.39 | 8.07 |
| 13 | 14.6 | 12.6 | 8.35 | 46.6 | 8.27 | 22 | 12 | 27 | 177 | 61.4 | 5.25 | 6.43 | 5.22 | 8.01 |
| 14 | 16.8 | 12.7 | 7.67 | 48.3 | 2.69 | 27 | 12 | 33 | 234 | 80.9 | 4.95 | 5.82 | 4.68 | 7.33 |
| 15 | 12.3 | 11.5 | 5.48 | 69.6 | 25.8 | 15 | 19 | 16 | 366 | 137 | 6.21 | 6.75 | 3.34 | 5.24 |
| 16 | 14.8 | 13.7 | 9.57 | 47.8 | 20.2 | 15 | 10 | 18 | 127 | 44.7 | 5.35 | 6.68 | 6.11 | 9.21 |
| 17 | 16.19 | 13.8 | 7.33 | 59. 5 | 9.91 | 18 | 10 | 20 | 276 | 101 | 4.58 | 5.12 | 4.47 | 7.01 |
| 18 | 17.2 | 15.0 | 9.96 | 46.8 | 9.93 | 19 | 10 | 22 | 147 | 51.1 | 4.43 | 5.42 | 6.24 | 9.56 |
| 19 | 18.1 | 15.9 | 11.7 | 40.3 | 8.59 | 18 | 10 | 24 | 194 | 34.7 | 4.34 | 5.75 | 7.49 | 11.3 |
| 20 | 20.5 | 16.1 | 11.2 | 49.6 | 3.15 | 22 | 16 | 50 | 127 | 42.0 | 4.10 | 5.23 | 6.96 | 10.7 |
| 21 | 18.5 | 17.3 | 12.9 | 43.7 | 21.0 | 12 | 8.2 | 158 | 81.9 | 28.3 | 4.39 | 5.79 | 8.39 | 12.4 |
| 22 | 21.0 | 18.1 | 11.6 | 48.7 | $8: 49$ | 15 | 8.2 | 18 | 135 | 47.3 | 3.61 | 4.34 | 7.21 | 11.1 |
| 23 | 24.1 | 18.6 | 11.4 | 48.2 | 3.15 | 18 | 8.2 | 22 | 155 | 53.7 | 3.39 | 4.00 | 6.94 | 10.9 |
| 24 | 24.8 | 19.4 | 13.2 | 41.8 | 3.18 | 18 | 8.2 | 24 | 111 | 37.1 | 3.37 | 4.24 | 8.21 | 12.7 |
| ${ }^{\prime} 25$ | 21.4 | 20.0 | 14.018 | 47.8 | 21.9 | 10 | E. 8 | 128 | 84.0 | 29.6 | 3.75 | 4.71 | 8.97 | 13.5 |
| 26 | 25.4 | 22.3 | 15.5 | 44.7 | 9.72 | 12 | 6.8 | 158 | 87.7 | 39.2 | 3. 03 | 3.80 | 9.76 | 14.8 |
| 27 | 29.0 | 22.2 | 13.1 | 49.9 | 3.86 | 15 | E. 8 | 18 | 141 | 49.4 | 2.82 | 3.28 | 7.98 | 12.5 |
| 28 | 26.4 | 24.7 | 17.8 | 46.1 | 21.7 | 8.2 | 5.6 | 106 | 63.1 | 22.1 | 3.06 | 3.92 | 11.5 | 17.1 |
| 29 | 30.2 | 26.3 | 17.8 | 48.6 | 9.51 | 19 | 5.6 | 128 | 89.3 | 31.4 | 2. 51 | 3.02 | 10.6 | 16.4 |
| 30 | 34.9 | 27.5 | 17.E | 46.1 | 3.64 | 12 | 5.6 | 159 | 93.0 | 31.9 | 2.32 | 2.80 | 10.8 | 16.8 |
| 31 | 30.5 | 28.7 | 20.4 | 47.2 | 23,2 | 6.8 | 4.7 | 8.25 | 55.3 | 19.5 | 2.65 | 3.36 | 13.2 | 19.7 |
| 32 | 35.8 | 31.6 | 21.2 | 46.9 | 16, 4 | 8.2 | 4.7 | 106 | 66.9 | 23.3 | 2.13 | 2.61 | 13.3 | 20.4 |
| 33 | 40.7 | 32.6 | 19.2 | 49.7 | 3.81 | 19 | 4.7 | 129 | 93.4 | 32.7 | 1.96 | 2. 29 | 11.8 | 18.4 |
| 34 | 49.0 | 32.5 | 19.2 | 47.4 | 1. 25 | 12 | 4.7 | 159 | 97.1 | 33.2 | 1.94 | 2.27 | 11.6 | 18.3 |
| 35 | 37.6 | 34.8 | 25.1 | 46.5 | 23.6 | 5.6 |  | E. 84 | 43.7 |  | 2.21 | 2.83 | 16.2 | 24.2 |
| 35 | 42.8 | 37.7 | 24.9 | 48.0 | 16.6 | 6.8 | 3.9 | 8.25 | 58.8 | 20.6 | 1.77 | 2.16 | 15,6 | $23.9$ |
| 37 | 49.0 | 39, 6 | 24.2 | 48.0 | 4.198 | 8.2 | 3.9 | 107 | 70.5 | 24.5 | 1.63 | 1.93 | 14.9 | 23.2 |
| 38 | 42.2 | 39.8 | 27.9 | 48.5 | 25.2 | 4.7 | 3,3 | 5. 64 | 40.7 | 14.4 | 1.94 | 2.43 | 17.9 | 26.9 |
| 39 | 49.9 | 44.5 | 361, 0 | 47.1 | 11.8 | 5.6 | 3.3. | 6.8 | 4E, 3 | 16.2 | 1.53 | 1.88 | 18.9 | 28.8 |
| 49 | 56.7 | 45.7 | 38.1 | 49.6 | 4.59 | 6.9 | 3,3 | 8.26 | 61.5 | 21.5 | 1.38 | 1.63 | 17.3 | 26.9 |
| 41 | 67.3 | 45,8 | 26.4 | 49.3 | 1.30 | 8.2 | 3.3 | 107 | 73.3. | 25.4 | 1.36 | 1.57 | 15.9 | 25.2 |
| 42 | 53.2 | 49.9 | 35.5 | 47.3 | 23.3 | 3.9 | 2. | 4.73 | 31.8 | 11.2 | 1.53 | 1.94 | 22.8 | 34.2 |
| 43 | 1.1.2 | 53.9 | 34.8 | 49.2 | 10.3 | 4.7 | 2. 7 | 5.64 | 43.3 | 15.3 | 1.23 | 1. 1.48 | 21.8 | 33.4 |
| 44 | 69.9 | 56.1 | 34.8 | 48.4 | 4.41 | 5,6 | $2 . \vec{i}$ | 6.8 .4 | 49.0 | 17.1 | 1.13 | 1.34 | 21.4 | 33.3 |

FILTER CHARACTERISTICS AND DESIGN FORMULAS


|  |  |  |  |  |  | цим pesn 'oul 'Kuedu |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | నేచేకే <br> 111 <br> న్కరల |  |  |  |  | yoog II! $\mathrm{H}^{- \text {Meigo }}$ |
|  |  |  |  |  |  | $\begin{aligned} & \text { n } \\ & \text { in } \\ & \frac{0}{5} \\ & \frac{1}{6} \\ & 9 \\ & \frac{5}{0} \end{aligned}$ |
|  |  <br> 1111 <br> 550 |  |  |  |  |  |
|  |  |  |  | $\frac{1}{5}$ |  |  |
| (\%) | $\frac{\sim}{4}$ |  |  |  |  |  |
| $\begin{aligned} & 5: \\ & \text { 日i } \\ & 989 \end{aligned}$ | $\begin{array}{r} 08 \\ 18 \\ 18 \\ y \end{array}$ | $>$ | $E$ | Ei | Ei |  |

## COMB-FILTER DESIGN

Comb filters consist of a chain of narrow-band filters which pass spectral lines over the frequency spectrum of the signal. They pass discrete frequency components and discriminate against noise. Such filters are used to separate a composite input signal into a number of channels before data processing in telemetry systems and radar. The spacing between channels may be expressed as a frequency ratio which depends on the number of channels needed to cover one octave, or " $n$." Thus $f / f_{c}=2^{n}$, where $f_{c}$ is the reference, $f$ is the unknown frequency of the adjacent channel, and $n$ is any positive or negative real number. For $n= \pm 1, f$ equals $2 f_{c}$ and $1 / 2 f_{c}$. These values are the center frequencies of channels, one octave away from the reference frequency.

The nomogram solves for positive or negative fractional values of $n$. The frequency scales, $f_{\mathrm{c}}$ and $f$, are normalized so that the nomogram can be used for any frequency by shifting the decimal point. The ratio scale, $n$, has a decimal range as well as fractional values.

To use the nomogram, place a straight-edge from the octave fraction or decimal on the $n$ scale to the reference frequency on the $f_{c}$ scale. Read the center frequency of the next channel on the $f$ scale. Hold the $n$-scale value as a pivot point and shift the straight-edge to the same frequency on the $f_{c}$ scale as the first answer. Read the next bandpass center frequency on the $f$ scale. Continue the process until all center frequencies are obtained. For negative $n$ values, divide the reference frequency by two to obtain the lower octave. After this step, proceed as for a positive $n$ value.

FOR EXAMPLE: Calculate the center frequencies for $1 / 3$ octave filters, starting at 100 Hz (see illustration).
Set the straight-edge from $1 / 3$ or 0.33 on the $n$ scale to the one (for 100 Hz ) on the $f_{c}$ scale and read 1.26 on the $f$ scale; the center frequency of the next channel bandpass filter is 126 Hz . Pivot at $1 / 3$ on the $n$ scale and shift the straightedge to 126 on the $f_{c}$ scale. Read 160 Hz on the $f$ scale. When $1,260 \mathrm{~Hz}$ on the $f$ scale and 1,000 Hz on $f_{c}$ is reached, shift back to the lower portion of the $f_{c}$ scale and continue.





Bandpass filter array shown requires three
channals to cover one octave. Therefore $n=1 / 3$.

Pulse-forming networks supply high-voltage pulses to magnetrons and lasers. This nomogram relates the pulse width and characteristic impedance to the network's inductances and capacitances. It is based on the formulas:

$$
\begin{aligned}
Z_{o}=\sqrt{\frac{L}{C}} ; P_{w} & =2 n \sqrt{L C} \\
n & =\frac{P_{w}}{2 r}
\end{aligned}
$$

where

$$
\begin{aligned}
Z_{0} & =\text { characteristic impedance } \\
L & =\text { inductance per section } \\
C & =\text { capacitance per section } \\
n & =\text { number of sections } \\
P_{w} & =\text { pulse width } \\
r & =\text { rise time }
\end{aligned}
$$

FOR EXAMPLE: Designa PFN that delivers a $4-\mathrm{kV}, 500-\mu \mathrm{sec}$ pulse with a $25-\mu \mathrm{sec}$ rise time into a 1-ohm load: The numbers of sections ( $\mathrm{P}_{\mathrm{w}} / 2 r$ ) is 10. Connecting 1 ohm to $500 \mu \mathrm{sec}$ on the left and right scales yields $250 \mu \mathrm{~F}$ and $250 \mu \mathrm{H}$ as total capacitive $C_{N}$ and total inductance $L_{N}$. Dividing by 10 gives $25 \mu \mathrm{~F}$ and $25 \mu \mathrm{H}$ per section. The two end inductances are 1.15 the value of each section or $2.875 \mu \mathrm{H}$.


A pulse applied to the input of a delay line is continuously delayed by a predetermined amount as it travels along the line. The artificial or lumped parameter type of delay line consists of a series of low pass LC filters. The delay for $n$ sections is given by the formula

$$
t=n \sqrt{L C}
$$

where $t=$ time delay in microseconds
$L=$ inductance in microhenries
$n=$ number of sections
$C=$ capacitance in microfarad
The characteristic impedance $Z_{0}$ must be matched to reduce reflections within the delay line and is given by the formula

$$
z_{0}=\sqrt{U C}
$$

where $Z_{0}$ is in ohms
The cutoff frequency of each section must be higher than the operating frequency $f_{c}=\frac{1}{\pi \sqrt{L C}}$
where $f_{c}$ is the cutoff frequency in megahertz


This nomogram solves for the delay per foot as well as the total delay of a coaxial cable when the relative dielectric constant of the insulation is known. The nomogram is based on the relationship

$$
T=1.108 \sqrt{E} n \mathrm{sec} / \mathrm{ft}
$$

The relative dielectric constant and delay per foot are plotted on the left-hand index and can be related directly. The chart gives the approximate ranges of dielectric constants of commonly used insulating materials. Some dielectric properties are a function of composition, frequency, and temperature, and the values shown should be used accordingly.

FOR EXAMPLE: A 4-ft cable with a polystyrene dielectric will produce a total delay of about 6.3 to 6.5 nsec .

## DIELECTRIC CONSTANTS

Bokalite ${ }^{\text {' ............................. . . . . ............... } 3.95}$
Fluarinated athylene prapyiene ..... 2.2
lrrodiated polyethylane ..... 2.3
Lueite ${ }^{2}$ ..... 2.7
Mognesium oxade ..... 9 .7
Nylan. ..... 30
Pelyethylene ..... 2.25-2.32
Pelystyrene ..... 2.4.26
Polytetrefluoroethylene ..... 20.2 .3
Pelyurethens ..... 64.76
Polywinylehloride (nanerigid) ..... 7.0
Rubber (netural). ..... 24.46
Rubber (silicone) ..... 2.9.3.7
1.TM Unien Carbide Corp.
2.TM DVPent


Inv $\overrightarrow{\text { In }}$



Circuit diagrams are given and the minimum voltage ratings of the capacitors are shown as related to $V_{m}$. The minimum PIV of the diodes is $2 V_{m}$.



FULL-WAVE VOLTAGE TRIPLER


FULL-WAVE VOLTAGE QUADRUPLER


HALF-WAVE VOLTAGE QUADRUPLER

$n$-SECTION VOLTAGE MULTIPLIER

This tabulation shows the transfer function, switching transistor currents and voltages, diode currents and voltages as well as voltage and current waveforms for ten different converter circuit configurations used in switching power supplies.

The advantages and disadvantages of each circuit configuration are also given.



AND CURRENT RATINGS BE INCREASED TO $125 \%$ OF THE REQUIRED MAXIMUM.


|  |  |  |
| :---: | :---: | :---: |
| (4) PUSH-PULL | Ćuk (Boost - Buck invertimg) | cux (with transfonmer) |
| $\frac{V_{0}}{V_{\text {IN }}}=2 \frac{\mathrm{Nz}}{\mathrm{NI}}\left(\frac{\mathrm{T}}{\mathrm{T}}\right)$ | $\frac{V_{0}}{V_{\text {IE }}} \cdot\left(\frac{\tau}{T-T}\right)(t-1)$ | $\frac{v_{0}}{v_{i n}} \cdot \frac{r}{T-\tau}, 0=\frac{T}{T}, 0 \leq 0 \leq 1$ |
| $I_{C \text { max }}=\frac{N 2}{\text { WI }}$ ( $\left(I_{m L}+\frac{\Delta I_{\text {LI }}}{2}\right)+I_{\text {mac }}$ | $I_{\text {cmax }}=I_{1}+I_{2}=I_{1}\left(\frac{T}{T}\right)$ |  |
| $\mathrm{vcxo}=2 \mathrm{v}_{\mathrm{m}}$ | $\mathrm{v}_{\text {ceo }} \geq 2 \mathrm{v}_{\text {m }}$ | $v_{\text {cEO }}=\underbrace{15 v_{m}}_{0.33} \cdot \underbrace{2 v_{\text {Im }}}_{0.5} \cdot \underbrace{2.5 v_{m}}_{0.5}$ |
| $\begin{aligned} & I_{C n 1} * \frac{I_{n L}}{2} \\ & I_{C n 2} * \frac{I_{n L}}{2} \end{aligned}$ | $\begin{aligned} I_{\text {CH }} & =I_{1}+I_{2} \\ I_{1} & +I_{2}=I_{1}\left(\frac{T}{r}\right) \end{aligned}$ | $\begin{aligned} & I_{C R 1}=1,5 I_{m L} \text { FOR } 0=33 \\ & I_{C N 1}=2 I_{m L} \text { FON } D=50 \\ & I_{C N 1}=25 I_{R L} \text { FON } 0=60 \end{aligned}$ |
| $v_{\text {Ru }}\left\{\begin{array}{l}v_{\text {CRI }}=2 v_{\text {IM }}\left(\frac{N 2}{N 1}\right) \\ v_{C R 2}=2 v_{\text {IW }}\left(\frac{N 2}{N 1}\right)\end{array}\right.$ | $v_{0}+1$ | $15 V_{\text {IM }}$ FOR $0=.33$ <br> $2 V_{\text {IW }}$ FOR O = SO <br> $2 S V_{i m}$ FOR $0=60$ |
|  |  |  |
| Sample, goob Thansformer UTILI2ATION COLLECTOA CURRENT REOUCED AS A FUNCTION OF $\frac{M 2}{\mathrm{NI}}$ G000 AT LOW values of $\mathrm{v}_{\mathrm{m}}$. | CONTWNOUS DPUT ANO OUTPUT CURMENT, HIGHEST EFFICIENCY, LOW MPPLE, SMALLEST RUMEER OF SWITCHING COMPONENTS, SWTCHING LOSSES CUT IN HALF, ONIVE CIRCUIT REFENENCED TO GROUNO hiGREST OPERATIWG PREOUENCY | COMTINUOUS INPUT ANO OUTPUT CURNEMT, MGHEST EFFICIENCY, VEAY LOW RIPMLE, SMALLEST MUMBER OF SWITCANG COMPONENTS, SWITCHNG Losses low, orive cunnemt referenceo to grouno highest OPEAATMG FREOUENCY. |
| CROSS COWDUCTION OF OL, oz POSSUBLE,MGBH PARTS COUNT TRUWSFONMER DESICN CPITICAL POON OTMANC RANGE, POOR TRANSENT RESPONSE | HIGH COLLECTOR CUFRENT CI MAS HIGM MIPPLE CURRENT REOUREMENT MiGH VOLTAGE REDURED FOR OI PGWER OUTPUT LIMITEO | CI ano Cz have hich ripple CUnRent reouifements transformer dESIGN CRITICAL. POWER OUTPUT IS LIMITEO. |

(From General Electric Application Note 200.87, "Power Transistor Applications for Switching Regulators and Motor Control," copyrighted © by and reprinted with permission of General Electric Company.)

## PERCENT REGULATION OF POWER SUPPLIES

The percent regulation of a power supply is found by the change in output voltage between Full Load and No Load voltage as given by the formula:

$$
\% \text { regulation }=\frac{\text { No Load Voltage }- \text { Full Load Voltage }}{\text { Full Load Voltage }} \times 100 .
$$

## FOR EXAMPLE:

1. What is percent regulation if No Load Voltage is 500 V and Full Load Voltage is 492 V ? The difference is 8 V. Answer: Connecting 492 and 8 gives a regulation of about $1.6 \%$.
2. For $0.04 \%$ regulation what is maximum allowable change in output voltage if required Full Load Voltage is 15 V . Answer: 0.006 V .


## POWER LOSS DUE TO IMPEDANCE MISMATCH

This chart shows the power loss resulting from inequality in the absolute magnitude of two impedances connected so as to transfer power from one to the other. The figures on the curves are the number of degrees of algebraic phase difference between the two impedances.

FOR EXAMPLE: Find the resulting power loss when a loudspeaker with an impedance of 10 ohms and a phase angle of $60^{\circ}$ is fed from a generator with a 100 -ohm internal impedance. The impedance mismatch ratio is $10: 1$, and at the $60^{\circ}$ line the loss due to mismatch is read as 5.7 dB .


## SEVEN COMMONLY USED BRIDGE CIRCUITS AND THEIR BALANCE EQUATIONS

A bridge consists essentially of four arms connected in series and so arranged, that when an electromotive force is applied across one pair of opposite junctions, the response of a detecting and /or indicating device connected between the outer pair of junctions may be zeroed by adjusting one or more of the elements of the arms of the bridge. Seven commonly used bridge circuits and their balance equations are shown.


This nomogram is used to find the effective resistance of resistors connected in parallel or the capacitance of capacitors connected in series. The range of the nomogram may be extended by multiplying the three scales by the same factor $10^{n}$, where $n$ may be positive or negative.

FOR EXAMPLE: (1) The effective resistance of a 150 k and 120 k resistor in parallel is 67 k . (2) A $6.8 \mu$ f and $5.6 \mu \mathrm{f}$ capacitor connected in series present an effective capacitance of $3 \mu \mathrm{~F}$.

(From "Parallel-Resistance Chart," EDN, September 14, 1966 by perimission of EDN.)

## Section 4

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| NAME OF Device | CIRCUTT symbol | $\begin{aligned} & \text { COMMONLY USED } \\ & \text { JUKCTION } \\ & \text { SCHEMATIC } \\ & \hline \end{aligned}$ | ELECTRICAL CHARACTERISTICS | MAJOR APPLICATIONS | $\begin{gathered} \text { ROUGHLY } \\ \text { ANALOGOUS } \\ \text { TO } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Diode <br> or <br> Rectifier |  |  | AmODE I <br> YAMDDE $(-1)$ | Rectification <br> Blocking <br> Detecting <br> Steering | Check valve <br> Drade tube <br> Gas diode |
| Avalanche <br> (Zener) <br> Diode |  |  | Constant voltage characteriatic in negative quadrant | Regulation <br> Beference <br> Clipping | $\mathrm{V}-\mathrm{R}$ tube |
| Integrated Voltage Regulator (IVR) |  |  | Programmed to deair ed $\mathrm{V}_{21}$ by two resiatora | Shum voltage regulator <br> Reference element Error madifler Level senamp Level shifting | Avalanche Diode |
| Tunnel <br> Diode |  |  |  | UHF comerter <br> Logic circuits <br> Microwave elreuita <br> Levet sensing | None |
| Back Diode | CATHODE |  |  <br> Similar characterlatice to conventionsl difode except very low forward voltage drop | Mierowave mixer: and low power oncillators | None |


| NAME OF DEvice | cIRCUIT symbol. | COMMONLY USED JUNCTION SCHEMATIC | Electrical characteristics |  | MAJOR APPLICATIONS | $\begin{gathered} \text { ROUGGLY } \\ \text { ANALOCOUS } \\ \text { TO- } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| rtyrector |  |  |  | Rupudly Increasing current above rated voltage in either direction | Tramsient voltage suppression and are suppression | Thythe <br> Two avalanche diodes in inverne-weries connection |
| $\begin{aligned} & \text { n-p-n } \\ & \text { Tranaistor } \end{aligned}$ |  |  |  | Constant collector current for ziven bate drive | Amplification <br> Switehing <br> Oscillation | Pentode Tube |
| $\begin{aligned} & \mathrm{p}=\mathrm{m}-\mathrm{p} \\ & \text { Tramistor } \end{aligned}$ |  |  |  | Complement to n-p-n tranalator <br> Lecton (-) | Amplification Switching Oscillation | None |
| Photo <br> Tranmastor |  |  | $\underbrace{2}_{V E E}$ | Incident light acts as base current of the photo transistor | Tape readers <br> Card reader: <br> Position sensor <br> Tachometers | None |
| Unjuametion Fransistor (tu) I) |  |  |  | Unijunctlon emitter blocks uat!! its voltage reacher $\mathrm{V}_{\mathrm{p}}$. then conducts | Interval timiag <br> Oseltlation <br> Level Detector <br> SCR Trugger | Nome |


| NAME OF DEVICE | CIRCIIT <br> SYMBOL | COMMONLY USFB JNCTIOS SCHFMATIC | ELECTRICAL CIIARACTERISTICS | MA.JOR <br> APPLICATIONS | $\begin{aligned} & \text { Heviculir } \\ & \text { ANALOGOUS } \\ & \text { TO } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Complementary <br> Ual junction Tranaistor (CUST) | BASE 2 |  | Functionsl complement to DJST | High atabilet? tumere <br> Oscillators and level detectors | None |
| Programmable <br> Unijunction <br> Transistor (PUT) | ANODE: <br> CATHODE |  | Programmed by two resilatora for $\mathrm{V}_{p}$. $\mathrm{I}_{\mathrm{p}}$. $\mathrm{I}_{\mathrm{v}}$. Function equivalent to normal UJT, | L.ow cont timere and osclllators <br> Long period timers SCR trigger <br> Level detector | UJT |
| Silicon Controlled Rectifier (5CR) | CATHODE |  |  | Power awitching <br> Phase control <br> Inverter: <br> Chopperif | Gas thyratron of Igntron |
| Complementary <br> Silicon <br> Controlled <br> Hectifier <br> (CSCR) | ANODE <br> CATHODE |  | $\xrightarrow[(2)]{\text { ANDDE }}$ | Fung counters <br> Low mpeed logic <br> Lamp. driver | None |
| Laght <br> Activated <br> SCR <br> (LABCR) | CATHODE |  |  | Relay Replacement <br> Poeition costrola <br> Photcelectrif applications <br> Sisve flashea | None |


| NAME OF DEVICE | CIRCUIT SYMBOL | COMMONLY USED JUNCTION SCHEMATIC | ELECTRICAL CHA | ARACTERISTICS | MAJOR <br> APPLJCATIONS | $\begin{gathered} \text { ROUGHLY } \\ \text { ANALOGOUS } \\ \text { TO. } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| suicon Controlied Switch" (SCS) |  | ANODE |  | Operatea similar to SCR except can also be triggered on by a negative signal on anode-gate. Alao eeveral other specialized modea of operation | Lagic applications <br> Countera <br> Nixie drivers <br> Lamp drivers | Complementary transistor part |
| Silicon <br> Unilateral <br> Switch <br> (5U5) | CATHODE | ANODE <br> CATHOOE |  | Similar to scs but zener added to anode gate to trigger device Into conduction at $\sim B$ volts. Can also be triggered by negative pulae at gate lead. | Switching Circuite Counters SCR Trigger Oacilistor | Shockley or 4-layer diode |
| Silioon <br> Bilateral <br> Switch <br> (SBS) |  |  |  | Symmetrleal blateral veraion of the SUS. Breake down in both directions as SUS does in forwa d. | Swltching Cireults Counters TRIAC Phase Control | Two tiverke Shockley dilodea |
| Trise | ANOOE 1 |  |  | Operates aimiliar to SCR except ean be triggered Into conduction in either direction by ( + ) or ( -1 gate alynai | AC awltching <br> Phare control <br> Relay replacement | Two SCR' In inverse parallel |
| Dise Trlgerer |  | $n$ <br> $n$ <br> $n$ <br> $n$ |  | When voltage reaches tragger level \{about 35 voltin), abruptly swithehea down shout 10 volts. | Trlice and SCR trigger Owcillator | Neen lamp |

## LETTER SYMBOLS AND ABBREVIATIDNS FDR SEMICDNDUCTOR DEVICES

Table 1: General Semiconductor Symbols

| $l, i$ | region of a device which is intrinsic and in which neither holes nor electrons <br> predominate |
| :--- | :--- |
| $N, n$ | region of a device where electrons are the majority carriers |
| $N F$ | noise figure |

Table 2: Signal Diode and Rectifier Diode Symbols

| $V_{(B R)}$ or $V_{(B R) R}$ | reverse breakdown voltage, dc |
| :---: | :---: |
| $v_{\text {(BR) }}$ or $v_{\text {(BR)R }}$ | reverse breakdown voltage, instantaneous total value |
| $I_{\text {F }}$ | forward current, dc |
| $I_{\text {F }(A V) ~}$ | forward current, average value |
| ${ }^{\prime}{ }_{\text {F }}$ | forward current, instantaneous total value |
| $I_{\text {f }}$ | forward current, rms value of alternating component |
| $I_{\text {F(RMS })}$ | forward current, rms total value |
| $I_{\text {FM }}$ | forward current, maximum (peak) total value |
| $I_{\text {FM }}$ (rep) | forward current, repetitive, maximum (peak), total value |
| IFM(surge) | forward current, maximum (peak), total value of surge |
| Io | output current, average rectified |
| $I_{\text {R }}$ | reverse current, dc |
| $i_{\text {R }}$ | reverse current, instantaneous total value |
| $I_{\text {R(AV) }}$ | reverse current, average value |
| $I_{\text {RM }}$ | reverse current, maximum (peak) total value |
| $I_{r}$ | reverse current, rms value of alternating component |
| $I_{\text {R(RMS }}$ | reverse current, rms total value |
| $L_{\text {c }}$ | conversion loss (microwave diodes) |
| $P_{\text {F }}$ | forward power dissipation, dc |
| $P_{\text {F(AV) }}$ | forward power dissipation, average value |
| $P_{\text {FM }}$ | forward power dissipation, maximum (peak) total value |
| $p_{\text {F }}$ | forward power dissipation, instantaneous total value |


| $P_{\text {R }}$ | reverse power dissipation, dc |
| :---: | :---: |
| $P_{\text {R(AV) }}$ | reverse power dissipation, average value |
| $P_{\text {RM }}$ | reverse power dissipation, maximum (peak) total value |
| $p_{\text {R }}$ | reverse power dissipation, instantaneous total value |
| $V_{F}$ | forward voltage drop, dc |
| $v_{F}$ | forward voltage drop, instantaneous total value |
| $V_{\text {F (AV) }}$ | forward voltage drop, average value |
| $V_{\text {FM }}$ | forward voltage drop, maximum (peak) total value |
| $V_{\text {F (RMS }}$ ) | forward voltage drop, total rms value |
| $V_{\text {f }}$ | forward voltage drop, rms value of alternating component |
| $V_{\text {R }}$ | reverse voiltage, dc |
| $V_{\text {R }}$ | reverse voltage, instantaneous total value |
| $V_{\text {R(AV) }}$ | reverse voltage, average value |
| $V_{\text {RM }}$ | reverse voltage, maximum (peak) total value |
| $V_{\text {RM ( }}$ (wkg) | working peak reverse voltage, maximum (peak) total value |
| $V_{\text {RM (rep) }}$ | repetitive peak reverse voltage, maximum (peak) total value |
| $V_{\text {RM (nonrep) }}$ | nonrepetitive peak reverse voltage, maximum (peak) total value |
| $V_{\text {R(RMS })}$ | reverse voltage, total rms value |
| $V_{r}$ | reverse voltage, rms value of alternating component |

Table 3: Transistor Symbols

| $B V_{\text {cso }}$ | obsolete-see $V_{\text {(BR)ceo }}$ |
| :---: | :---: |
| $B V_{\text {CEE }}$ | obsolete-see $V_{\text {(BR)CEO }}$ |
| $B V_{\text {CER }}$ | obsolete-see $V_{\text {(BA)CER }}$ |
| $B V_{\text {CES }}$ | obsolete-see $V_{\text {(BR)CES }}$ |
| $B V_{\text {cex }}$ | obsolete-see $V_{\text {(BR)CEx }}$ |
| $B V_{\text {EBo }}$ | obsolete-see $V_{\text {(BR)EBo }}$ |
| $B V_{R}$ | obsolete-see $V_{\text {(BR) }}$ |
| $C_{\text {ibo }}$ | open-circuit input capacitance, common base |
| $C_{\text {ibs }}$ | short-circuit input capacitance, common base |
| $C_{\text {eo }}$ | open-circuit input capacitance, common emitter |
| $C_{\text {ies }}$ | short-circuit input capacitance, common emitter |
| $C_{\text {obo }}$ | open-circuit output capacitance, common base |
| $C_{\text {obs }}$ | short-circuit output capacitance, common base |
| $C_{\text {oso }}$ | open-circuit output capacitance, common emitter |
| $C_{\text {oes }}$ | short-circuit output capacitance, common emitter |
| $f_{\text {hto }}$ | small-signal short-circuit forward current transfer ratio cutoff frequency (common base) |
| $f_{\text {hite }}$ | small-signal short-circuit forward current transfer ratio cutoff frequency (common collector) |
| $f$ hfe | small-signal short-circuit forward current transfer ratio cutoff frequency (common emitter, |
| $f_{\text {max }}$ | maximum frequency of oscillation |
| $f_{T}$ | frequency at which small-signal forward current transfer ratio (common emitter) extrapolates to unity |
| $g_{\text {ME }}$ | static transconductance (common emitter) |
| $g_{\text {me }}$ | small-signal transconductance (common emitter) |
| $G_{P B}$ | large-signal average power gain (common base) |
| $G_{\text {pb }}$ | small-signal average power gain (common base) |
| $G_{P C}$ | large-signal average power gain (common collector) |
| $G_{p c}$ | small-signal average power gain (common collector) |
| $G_{\text {PE }}$ | large-signal average power gain (common emitter) |
| $G_{\text {pe }}$ | small-signal average power gain (common emitter) |


| $h_{\text {FB }}$ | ratio (common base) |
| :---: | :---: |
| $h_{\text {fo }}$ | small-signal short-circuit forward current transfer ratio (common base) |
| $h_{\text {FC }}$ | static forward current transfer ratio (common collector) |
| $h_{\text {fc }}$ | small-signal short-circuit forward current transfer ratio (common collector) |
| $h_{\text {FE }}$ | static forward current transfer ratio (common emitter) |
| $h_{\text {fo }}$ 。 | small-signal short-circuit forward current transfer ratio (common emitter) |
| $h_{18}$ | static input resistance (common base) |
| $h_{\text {ib }}$ | small-signal short-circuit input impedance (common base) |
| $h_{\text {IC }}$ | static input resistance (common collector) |
| $h_{\text {ic }}$ | small-signal short-circuit input impedance (common collector) |
| $h_{\text {IE }}$ | static input resistance (common emitter) |
| $h_{\text {i }}$ 。 | small-signal short-circuit input impedance (common emitter) |
| $h_{\text {ob }}$ | small-signal open-circuit output admittance (common base) |
| $h_{\text {oc }}$ | small-signal open-circuit output admittance (common collector) |
| $h_{\text {oo }}$ | small-signal open-circuit output admittance (common emitter) |
| $h_{\text {ro }}$ | small-signal open-circuit reverse voltage transfer ratio (common base) |
| $h_{r c}$ | small-signal open-circuit reverse voltage transfer ratio (common collector) |
| $h_{r e}$ | small-signal open-circuit reverse voltage transfer ratio (common emitter) |
| $I_{B}$ | base current, dc |
| $I_{6}$ | base current, rms value of alternating component |
| $i_{B}$ | base current, instantaneous total value |
| 1 C | collector current, dc |
| $t_{c}$ | collector current, rms value of alternating component |
| $i_{c}$ | collector current, instantaneous total value |
| $I_{\text {CBO }}$ | collector cutoff current, dc, emitter open |
| $I_{\text {Ceo }}$ | collector cutoff current, dc, base open |
| ICER | collector cutoff current, dc, with specified resistance between base and emitter |
| I'CEV | collector cutoff current, dc, with specified voltage between base and emitter |
| ${ }^{\prime}$ CEX | collector current, dc, with specified circuit between base and emitter |
| ICES | collector cutoff current, dc, with base short circuited to emitter |
| I oss | drain current, dc, with gate shorted to emitter |
| $I_{E}$ | emitter current, dc. |
| 1. | emitter current, rms value of alternating component |
| $\begin{aligned} & I_{\mathrm{EBO}} \\ & P_{\mathrm{BE}} \end{aligned}$ | emitter cutoff current (dc), collector open power input (dc) to the base (common emitter) |
| $p_{\text {BE }}$ | power input (instantaneous total) to the base (common emitter) |
| $P_{\text {CB }}$ | power input (dc) to the collector (common base) |
| $P_{\text {CB }}$ | power input (instantaneous total) to the collector (common base) |
| $P_{\text {ce }}$ | power input (dc) to the collector (common emitter) |
| $p_{\text {ce }}$ | power input (instantaneous total) to the collector (common emitter) |
| $P_{\text {eb }}$ | power input (dc) to the emitter (common base) |
| $p_{\text {EB }}$ | power input (instantaneous total) to the emitter (common base) |
| $P_{\text {18 }}$ | large-signal input power (common base) |
| $p_{\text {ib }}$ | small-signal input power (common base) |
| $P_{\text {Ic }}$ | large-signal input power (common collector) |
| $p_{\text {Ic }}$ | small-signal input power (common collector) |
| $P_{\text {IE }}$ | large-signal input power (common emitter) |
| $p_{\text {ie }}$ | small-signal input power (common emitter) |
| $P_{\text {OB }}$ | large-signal output power (common base) |
| $p_{\text {ob }}$ | small-signal output power (common base) |
| $P_{\text {OC }}$ | large-signal output power (common collector) |
| $p_{\text {oc }}$ | small-signal output power (common collector) |
| $P_{\text {OE }}$ | large-signal output power (common emitter) |

$\rho_{\text {on }} \quad$ small-signal output power (common emitter)
$P_{T} \quad$ total nonreactive power input (dc) to all terminals
$p_{T} \quad$ nonreactive power input (instantaneous total) to all terminals
$R_{\mathrm{B}} \quad$ external base resistance
$R_{\mathrm{C}}$ external collector resistance
$r_{\text {CE (sant) }}$ collector-to-emitter saturation resistance
$R_{E}$
$R e\left(h_{i d}\right)$ real part of the small-signal short-circuit input impedance (common emitter)
$V_{\text {(BR)CBO }}$ breakdown voltage, collector-to-base, emitter open
$V_{\text {(BR)CEO }}$ breakdown voltage, collector-to-emitter, base open
$V_{\text {(BR)CER }}$ breakdown voltage, collector-to-emitter, with specified resistance between base and emitter
$V_{\text {(BA)CES }}$ breakdown voltage, collector-to-emitter, with base short-circuited to emitter
$V_{\text {(BA)CEX }}$ breakdown voltage, collector-to-emitter, with specified circuit between base and emitter
$V_{\text {(BR)OGO }}$ breakdown voltage, drain-to-gate, source open
$V_{\text {(BR)EBO }}$ breakdown voltage, emitter-to-base, collector open
$V_{\text {(BR)R }}$ breakdown voltage, reverse
$V_{\mathrm{BB}} \quad$ base supply voltage
$V_{\mathrm{BC}} \quad$ base-to-collector voltage, dc
$V_{\mathrm{bc}} \quad$ base-to-collector voltage, rms value of alternating component
$V_{\mathrm{bc}} \quad$ base-to-collector voltage, instantaneous value of ac component
$V_{\text {BE }}$ base-to-emitter voltage, dc
$V_{\text {be }} \quad$ base-to-emitter voltage, rms value of alternating component
$v_{\text {be }}$ base-to-emitter voltage, instantaneous value of ac component
$V_{C B} \quad$ collector-to-base voltage, dc
$V_{\mathrm{cb}} \quad$ collector-to-base voltage, rms value of alternating component
$V_{c b}$ collector-to-base voltage, instantaneous value of ac component
$V_{C B}$ (t1) dc open-circuit voltage (floaking potential) between the collector and base, with the emitter biased with respect to the base
VCC collector supply voltage, dc
$V_{C E} \quad$ collector-to-emitter voltage, dc
$V_{c e} \quad$ collector-to-emitter voltage, rms value of alternating component
$V_{\text {ce }} \quad$ collector-to-emitter voltage, instantaneous value of ac component
$V_{C E(f)}$ dc open-circuit voltage (floating potential) between the collector and emitter, with the base biased with respect to the emitter
$V_{\text {CEO }} \quad$ collector-to-emitter voltage, dc, with base open
$V_{\text {CEO(sus) }}$ collector-to-emitter (breakdown) sustaining voltage with base open
$V_{\text {CER }} \quad$ collector-to-emitter voltage, dc with specified resistor between base emitter
$V_{\text {CER(sus) }}$ collector-to-emitter (breakdown) sustaining voltage with specified resistor between base and emitter
VCES collector-to-emitter voltage, dc with base short circuited to emitter
$V_{\text {CES(sus) }}$ collector-to-emitter (breakdown) sustaining voltage with base short-circuited to emitter
$V_{\text {CEX }} \quad$ collector-to-emitter voltage, dc with specified circuit between base and emitter
$V_{\text {CEX (wn) }}$ collector-to-emitter (breakdown) sustaining voltage with specified circuit between base and emitter
$V_{\text {CE (sat) }}$ collector-to-emitter saturation voltage, dc
$V_{E B}$
$V_{E B(f)}$ emitter-to-base voltage, dc
dc open-circuit voltage (floating potential) between the emitter and base, with the collector biased with respect to the base
$V_{\text {eb }} \quad$ emitter-to-base voltage, rms value of alternating component
$v_{\mathrm{ab}} \quad$ emitter-to-base voltage, instantaneous value of ac component
$V_{E C}$ emitter-to-collector voltage, dc
$V_{E C(f)}$ dc open-circuit voltage (floating potential) between the emitter and collector, with the base biased with respect to the collector
$V_{\text {ec }} \quad$ emitter-to-collector voltage, rms value of alternating component
$V_{\text {ec }}$ emitter-to-collector voltage, instantaneous value of ac component
$V_{E E} \quad$ emitter supply voltage
$V_{R T}$ reach-through voltage
Table 4: Tunnel Diode Symbols
I/ inflection point current
/p peak point current
Iv valley point current
$r_{i}$ dynamic resistance at inflection point
$V_{\text {pp }}$ projected peak point voltage
[forward voltage point (greater than the peak voltage), at which the current is equal to the peak current]
$V_{1}$ inflection point voltage
$V_{\mathrm{p}}$ peak point voltage
$V_{v}$ valley point voltage

## Typical Characteristics



| Characteristic | Vacuum Tube | Small-Signal Transistor | High-Power Transistor | Junction Fet | Mosfet |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Input impedance | High | * | Very low | High | Very high |
| Output impedance | High | $a$ | Low/moderate | High | High |
| Noise | Low | Low | Moderate | Low | Unpredictable |
| Warm-up time | Long | Short | Short | Short | Short |
| Power consumption | Large | Small | Moderate | Very Small | Very small |
| Aging | Appreciable | Low | Low | Low | Moderate |
| Reliability | Poor | Excellent | Very good | Excellent | Very good |
| Overload sensitivity | Excellent | Good | Fair | Good | Poor |
| Size | Large | Small | Moderate | Small | Small |

almpedances depend on circuit arrangement:

| For common base | Input Impedance |  |
| :--- | :--- | :--- |
| For common emitter | Mew (10's of ohms) |  |

## SUMMARY OF INTEGRATED CIRCUIT PROPERTIES

This table compares pertinent characteristics of present day and future ICs.

| Propertles | Current technotogles |  |  |  |  |  |  |  | $\begin{array}{lc} \hline \text { Future (1985-1990) } \\ \text { sos GeAs } \\ \hline \end{array}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 12 | LSTM | ECL | 12. | PMOS | NMOS | BULK CMOS | CM0s/30s |  |  |
| Relative process meturity $(1-10)$ | $\begin{array}{r} 10 \\ (8)^{*} \\ \hline \end{array}$ | $\begin{gathered} 9 \\ (4 \text { to } 5)^{\circ} \\ \hline \end{gathered}$ | $\begin{aligned} & 8 \text { to } 9 \\ & \text { (3 to } 5) \\ & \hline \end{aligned}$ | 4 | 10 | 9 | 8 | 4 | 2 | 1 |
| Process complexity (No proceasing steps) | 18 to 22t | 18 to $23 t$ | 19 to 23t | 13 to 17 | 8 to 14 | 9 to 15 | 14 to 17 | 14 to 20 | 14 to 20 | 18 |
| Logic complexity (No componente, 2 -input gete) | 12 | 12 | 8 | 3 to 4 | 3 | 3 | 4 | 4 | 3 to 4 | 2 |
| Pecking Density (gates/mm*) | 10 to 20 | 20 to 40 | 15 to 20 | 75 to 150 | 75 to 150 | 100 to 200 | 40 to 90 | 100 to 500 | 200 to 500 | 300 to 1000 |
| Propagation dalay, ne (typicel velue) | $8 \text { to } 30$ (10) | 2 to 10 (5) | 0.7 to 2 <br> (2) | 7 to 50 (20) | $\begin{gathered} 30 \text { to } 200 \\ (100) \end{gathered}$ | 4 to 25 (15) | $\begin{gathered} 10 \text { to } 35 \\ \text { (20) } \end{gathered}$ | 4 to 20 (10) | $\begin{gathered} 0.2 \text { to } 0.4 \\ (0.3) \end{gathered}$ | $\begin{gathered} 0.05 \text { to } 0.1 \\ (0.07) \end{gathered}$ |
| Speed-power product ( P ) | 30 to 150 | 10 to 60 | 15 to 60 | 0.2 to 2.0 | 50 to 500 | 5 to 50 | 2 to 40 | 0.5 to 30 | 0.1 to 0.2 | 0.01 to 0.1 |
| Typicel supply volteges (volts) | +5.0 | +5.0 | -5.2 | $\begin{gathered} +0.8 \text { to } \\ +1.0 \end{gathered}$ | -15 to +20 | +5.0 | +10.0 | +10.0 | +2.0 | +1.2 |
| Signel swing (volts) | 0.2 to 3.4 | 0.2 to 3.4 | -0.8 to -1.7 | 0.2 to 0.8 | 0.0 to -15.0 | 0.2 to 3.4 | 0.0 to 10.0 | 0.0 to 10.0 | 0.0 to 2.0 | 0.0 to 0.8 |
| Guarenteed noise margin (volls) | 0.3 to 0.4 | 0.3 to 0.4 | 0.125 | <0.1 | 1 to 2 | 0.5 to 20 | 3.5 to 4.5 | 3.5 to 4.5 | 0.2 to 0.8 | 0.2 to 0.3 |
| Neutron hardness cepebility ( $\mathrm{n} / \mathrm{cm}^{2}$ ) | 0.2 to 108 | 0.2 to $10^{18}$ | 0.5 to $2 \times 10^{14}$ | $\begin{array}{r} 1 \text { to } 5 \\ \times 1013 \\ \hline \end{array}$ | $\begin{gathered} >10^{15} \text { to } \\ 10^{10} \end{gathered}$ | $\begin{gathered} >10^{45} \text { to } \\ 10^{15} \end{gathered}$ | $\begin{gathered} >10^{15} \text { to } \\ 10^{15} \\ \hline \end{gathered}$ | $\begin{gathered} >10^{15} \text { to } \\ 10^{13} \end{gathered}$ | $\begin{gathered} >10^{15} \text { to } \\ 10^{15} \end{gathered}$ | $>1048$ |
| Total dose (h) hardness cepebility (rads) | $10^{\circ}$ to 100 | $10^{0}$ to $10^{\circ}$ | $\begin{gathered} 10^{r} \text { to } \\ 10^{5} \\ \hline \end{gathered}$ | $\begin{gathered} 100 \text { to } \\ 100 \\ \hline \end{gathered}$ | $10^{\prime}$ | $\begin{gathered} 1 \text { to } 5 \times \\ 100^{3} \\ \hline \end{gathered}$ | $\begin{gathered} 10^{4} \text { to } \\ 10^{7} \\ \hline \end{gathered}$ | $\begin{gathered} 100^{5} \text { to } \\ 100^{2} \\ \hline \end{gathered}$ | $10^{\circ}$ to $10^{\circ}$ | $>10^{\prime}$ |
| Dose rate (r) or pnotocurrent hardness cepebility (tacsis) | $\left\|\begin{array}{c} 0.5 \text { to } 2 x \\ 10^{15} \end{array}\right\|$ | 0.2 to $10^{10}$ | 0.2 to $10^{10}$ | 0.1 to 4 $\times 10^{18}$ | $\begin{aligned} & 0.1 \text { to } \\ & 5 \times 10^{0} \end{aligned}$ | $\begin{gathered} 0.1 \text { to } \\ 5 \times 10^{40} \end{gathered}$ | $\begin{gathered} 0.5 \text { to } \\ 2 \times 100 \end{gathered}$ | 0.2 to $10^{11}$ | 0.5 to $10^{11}$ | $>10^{10}$ |

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## ANALOGY BETWEEN THE THREE BASIC JUNCTION TRANSISTOR CIRCUITS AND THEIR EQUIVALENT ELECTRON TUBE CIRCUITS

A transistor can be operated with the input signal applied to the base and the output taken from the collector (common emitter), with the input signal applied to the emitter and the output taken from the collector (common base), or with the input signal applied to the base and the output taken from the emitter (common collector or emitter follower). The performance characteristics of these three connections correspond roughly to the three tube connections shown below, with the exception that the input impedance is generally lower in the transistor circuit. General characteristics of these three connections are given in the table.

| Common Emitter | Common Base | Common Collector |
| :--- | :--- | :--- |
| Large current gain | Approximate unity current gain | Large current gain |
| Large voltage gain | Large voltage gain | Approximate unity voltage gain |
| Highest power gain | Intermediate power gain | Lowest power gain |
| Low input resistance | Very low input resistance | High input resistance |
| High oututut resistance | Very high output resistance | Low output resistance |
| Analogous to grounded cathode | Anaiogous to grounded grid | Analogous to cathode follower generally |



## definitions of equivalent circuit parameters

| Common | Common <br> Base | Common <br> Collector | Definition |
| :---: | :---: | :---: | :---: | :---: | :---: |

## Typical Transistor Parameters

| Common Base | Common Emitter |  |
| :--- | :--- | :--- |
| Common Collector |  |  |
| $h_{11}=39$ ohms | $h_{11}=2,000$ ohms |  |
| $h_{12}=380 \times 10^{-6}$ | $h_{12}=-600 \times 10^{-6}$ | $h_{12}=1$ |
| $h_{21}=-0.98$ | $h_{21}=50$ | $h_{21}=-51$ |
| $h_{22}=0.49 \mu$ mho | $h_{22}=25 \mu$ mhos | $h_{22}=25 \mu$ mhos |

## EQUIVALENT CIRCUITS FOR SMALL-SIGNAL LOW-FREQUENCY TRANSISTOR STAGES

Small-signal, low-frequency, T-equivalent circuits for transistor stages


Common-base configuration (a) and hybrid equivalent circuit (b).


Common-emitter configuration (a) and hybrid equivalent circuit (b).


Common-collector configuration (a) and hybrid equivalent circuit (b).


(a)

(b)
$y$-Parameter equivalent circuit.


T-equivalent circuit, common base.


T-equivalent circuit, common emitter.

TRANSISTOR PARAMETER CONVERSION TABLES
(A) Common-base $h$ parameters in terms of common-emitter, common-collector, and $T$ parameters.
(B) Common-collector $h$ parameters in terms of common-emitter, common-base, and $T$ parameters.
(C) Common-emitter $h$ parameters in terms of common-base, common-collector, and T parameters.
(D) T parameters in terms of common-emitter, common-base, and common-collector parameters.

(E) Input impedance and output impedance in terms of $h$ and T parameters.
(F) Insertion power gain and transducer power gain in terms of $h$ parameters.
(G) Current gain and voltage gain in terms of $h$ and T parameters.
(H) Available power gain and operating power gain in terms of $h$ parameters.

(I) $Z$ parameters in terms of $h$ parameters.
(J) $Y$ parameters in terms of $h$ parameters.
(K) Common emitter z parameters in terms of common collector and common base z parameters and T parameters.
(L) Common emitter $y$ parameters in terms of common collector and common base $y$ parameters and $T$ parameters.

|  | Common amitter | Common base | Common collector |
| :---: | :---: | :---: | :---: |
| $z_{11 b}$ | $\frac{\Delta h}{h_{o e}}$ | $\frac{\Delta h}{h_{o b}}$ | $\frac{1}{h_{o c}}$ |
| $\text { (ii) }\left\{\begin{array}{l} z_{12 b} \\ \hline \end{array}\right.$ | $\frac{\Delta h-h_{r o}}{h_{o e}}$ | $\frac{h_{\text {do }}}{h_{o b}}$ | $\frac{1+h_{f c}}{h_{o c}}$ |
| $z_{21 b}$ | $\frac{\Delta h+h_{\text {fe }}}{h_{\text {o }}}$ | $\frac{{ }^{-h_{f b}}}{h_{\text {ob }}}$ | $\frac{1-h_{r c}}{h_{o c}}$ |
| $z^{22 b}$ | $\frac{d}{h_{00}}$ | $\frac{1}{h_{\text {ob }}}$ | $\frac{d}{h_{o c}}$ |
| $y_{11 b}$ | $\frac{d}{h_{i j}}$ | $\frac{1}{h_{16}}$ | $\frac{d}{h_{i c}}$ |
| (a) $\left\{\begin{array}{l}y_{12 b}\end{array}\right.$ | $\frac{h_{r e}+h_{f e}}{h_{\text {ie }}}$ | $-\frac{h_{\text {d }}}{h_{\text {b }}}$ | $-\frac{1+h_{f e}}{h_{k}}$ |
| \{ $y_{21 b}$ | $-\frac{\Delta h+h_{f 0}}{h_{0}}$ | $\frac{h_{\text {fb }}}{h_{\text {ib }}}$ | $\frac{h_{r c}-1}{h_{i c}}$ |
| $V^{22 b}$ | $\frac{\Delta h}{h_{i o}}$ | $\frac{\Delta h}{h_{b}}$ | $\frac{1}{h_{k}}$ |
| $\begin{aligned} \Delta h & =h_{i} h_{0}-h_{r} h_{f} \\ d & =\left(1+h_{f}\right)\left(1-h_{r}\right)+h_{i} h_{0} \cong 1+h_{f} \end{aligned}$ |  |  |  |
| $z$ parameiter | Common collector | Common base | $T$ equivelent-circuit |
| $z_{11}$ | $z_{11}-z_{12}-z_{21}+z_{22}$ | $z_{11}$ | $r_{e}+r_{b}$ |
| (K) $\left\{\begin{array}{l}\text { z } 2 \mathrm{e} \\ z_{21}\end{array}\right.$ | $z_{22}-z_{12}$ | $z_{11}-z_{12}$ | $r_{0}$ |
| (1) $z_{210}$ | $z_{22}-z_{21}$ | $z_{11}-z_{21}$ | $r_{e}-a r c_{c}$ |
| $z_{22}$ | $2_{22}$ | $z_{11}-z_{12}-z_{21}+z_{22}$ | $r_{e}+r_{c}(1-a)$ |
| $y$ parameter | Common collector | Common bese | $T$ equivalént-circuit |
| $v_{11}$ | $V_{11}$ | $y_{11}+y_{12}+y_{21} y_{22}$ | $\frac{r_{b}+r_{c}(1-a)}{\Delta}$ |
| (L) $\left\{\begin{array}{l}y_{120}\end{array}\right.$ | $-\left(y_{11}+y_{12}\right)$ | $-\left\langle y_{12}+y_{22}\right)$ | $-\frac{r_{e}}{\Delta}$ |
| (L) $V_{210}$ | $-\left(y_{11}+y_{21}\right)$ | $-\left\langle y_{21}+y_{22}\right\}$ | $-\frac{r_{a}-a r_{c}}{\Delta}$ |
| $r_{220}$ | $y_{11}+y_{12}+y_{21}+y_{22}$ | $V_{22}$ | $\frac{r_{0}+r_{b}}{\Delta}$ |
| $\Delta=r_{s} r_{b}+r_{c}$ |  |  |  |

(M) Common base z parameters in terms of common emitter and common collector z parameters and T parameters.
(N) Common base $y$ parameters in terms of common emitter and common collector $y$ parameters and $T$ parameters.
(O) Common collector $z$ parameters in terms of common emitter and common base $z$ parameters and T parameters.
(P) Common collector $y$ parameters in terms of common emitter and common base $y$ parameters and $T$ parameters.
(Q) Input impedance, output impedance, voltage gain, and current gain in terms of $z$ and $y$ parameters.

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## MULTIVIBRATOR DESIGN CURVES

The accompanying curves permit an easy and rapid determination of the frequency of oscillation of a symmetrical-astable (free-running) multivibrator, and the pulse duration ( $t_{p}$ ) of a monostable (one-shot) multivibrator. The pulse duration of the astable multivibrator output also can be read from the curve.

The expressions on which the curves are based are derived readily. The expression for the voltage at the base of the "off" transistor is

$$
e_{b}=E_{c c}\left(1-2 \epsilon^{-t R G}\right)+V_{b b}
$$

where $V_{b e}$ is the base-to-emitter voltage of an "on" transistor. The above equation assumes that base-to-emitter breakdown is prevented by using transistors whose base-to-emitter breakdown voltage is greater than $E_{c c}$ volts, or by connecting a diode in either the base or emitter lead.

The "off" transistor tums on when $e_{b}=V_{b 0^{\prime}}$ or $\epsilon^{-t / A C}=1 / 2$ where $t$ is the "off" time ( $t_{p}$ ) at the end of which time $e_{b}=V_{b e}$. Solving the equation yields $t_{b}=0.69$ RC. The curves in graph ( $A$ ) are plots of this equation. For the monostable multivibrator, $t_{p}$ is the pulse duration. The period of the symmetrical-astable multivibrator is equal to $2 t$.

Graph (B) is a family of curves of frequency of the symmetrical-astable multivibrator versus capacitance Cfor various values of resistance $R$. Since the period of the output wave is $2 t_{p}$, the equation for frequency is given as $f=1 / 1.38 \mathrm{RC}$, from which the curves were plotted.

FOR EXAMPLE: Find the value of $C$ required to generate a frequency of 500 Hz from a free-running multivibrator, or a 1 msec pulse from a monostable. In both cases the value of $R$ is limited to 100,000 ohms by the beta of the transistor selected. The curves indicated a value of $0.0145 \mu \mathrm{~F}$ for the capacitor.


## OPERATIONAL AMPLIFIERS

An operational amplifier is essentially a very high gain dc amplifier whose open-loop gain is generally high enough when compared with the closed-loop gain so that the closed-loop characteristics depend solely on the feedback element. Circuit applications for which operational amplifiers can be used are illustrated below.



Canstant Current Saurce
(Large Current Levels)


Current Canstant Saurce
(Flaating Laad)


Current ta Valtage Converter


Valtage Follawer with Gain


$$
\frac{e_{0}}{e_{i}}=+1
$$



High-impedance Low-voltoge Voltmeter



Voltage Comporator Circuit


Polority Separotor


Lagarithmic Transconductor


Modulator-Demodulator (Half-Wave)


Floating Load

$e_{0}=\left(e_{1}-e_{2}\right)\left(1+\frac{R_{2}+R_{3}}{R_{1}}\right)$


Frequency Divider

Crystal Oscillatar(Square Wave)


## GLOSSARY OF OPERATIONAL AMPLIFIER TERMS

Common-mode gain Ratio of output voltage over input voltage applied to (+) and ( - ) terminal in parallel. Common-mode rejection ratio (CMRR) Ratio of an op amp's open-loop gain to its common-mode gain. Differential-input voltage range Range of voltages that may be applied between input terminals without forcing the op amp to operate outside its specifications.
Differential Input Impedance ( $Z_{\text {if }}$ diff) Impedance measured between $(+)$ and ( - ) input terminals.
Drift, input voltage Change in output voltage divided by open-loop gain, as a function of temperature or time.
Input voltage offset Dc potential required at the differential input to produce an output voltage of zero.
Input bias current Input current required by $(+)$ and $(-)$ inputs for normal operation.
Input offset current Difference between $(+)$ and $(-)$ input bias currents.
Offset Measure of unbalance between halves of a symmetrical circuit.
Open-loop bandwidth Without feedback, frequency at which amplifier gain falls 3 dB below its low-frequency value.
Open-loop voltage gain ( $A_{\text {vol }}$ ) Differential gain of an op amp with no external feedback.
Slew rate Maximum rate at which output voltage can change with time; usually given in volts per microsecond.

| First Letter | Second Letter | Third, Fourth, and Fifth Character |
| :---: | :---: | :---: |
| Material | Type | Senal Code |
| A Germanium <br> B Silicon <br> C Compound materials, such as cadmium sulfide or gallium arsenide used in semiconductor devices. (Energy gap band of 1.3 or more electron-volts) <br> D Materials with an energy gap band of less than 0.6 elec-tron-volts such as indium antimonide <br> R Radiation detectors, photoconductive cells. Hall effect generators, etc. | A Low-power diode, voltage-variable capacitor <br> B Varicap <br> C Small-signal audio transistor <br> D Audio power transistor <br> E Tunnel diode <br> F Small-signal if transistor <br> G Miscellaneous <br> H Field probe <br> K Hall generator <br> L Rf-power transistor <br> M Hall modulators and multipliers <br> P Photodiode, phototransistor, photoconductive cell (LDR), radiation device <br> R Low-power controlled rectifier <br> S Low-power switching transistor <br> T Breakdown devices, high-power controlled rectifier, Shockley diode, Thyristor, pnpn diodes <br> U High-power switching transistor <br> X Multiplier diode <br> Y High-power rectifier (diode) <br> Z Zener diode | Three figuresserial codes used on devices for domestic and commercial applications <br> One letter and two figuresserial codes used on devices for use in military, industrial, scientific, and pulse, equipment |

The third letter-if there is one-indicates industrial device and is a $Y$. If there is no third letter, the device is for consumer or entertainment use. The digits that follow the letters for industrial units indicate how many devices of that particular type have been registered. The digits start at 10 and go up to 99 . When 99 is reached-i.e., after 89 devices-the last letter changes from a Y to an X and the numbering begins anew, working back towards A . There is no Z . For consumer devices, the numbers that follow the two letters start with 100, allowing registration of 899 similar devices.

FOR EXAMPLE: The designation BLY 80 means the device uses silicon ( $B$ ) is for high rf power use (L), and is used in industrial applications, $(\mathrm{Y})$; the 80 means that it is the 71st device of its type to be registered with Pro Electron.

CHARACTERISTICS OF INTEGRATED CIRCUIT LOGIC FAMILIES

|  | Typical <br> Circuit <br> Disgram | $\begin{aligned} & \text { Loger } \\ & \text { Type } \end{aligned}$ | Ralative Cosi Par Gste | Propagation Thme Par Gute (nstc) | $\begin{gathered} \text { Power } \\ \text { Disospation } \\ \text { Per Gati } \\ \text { (mow) } \end{gathered}$ | $\begin{array}{\|l\|} \hline \text { Typical } \\ \text { Nosase } \\ \text { Mergin } \\ \text { (V) } \end{array}$ | $\begin{aligned} & \text { Typical } \\ & \text { Tanin } \end{aligned}$ | $\left\lvert\, \begin{aligned} & \text { Typical } \\ & \text { fonout } \end{aligned}\right.$ | A Aomaks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RTL <br> Resistor:Couplied Transustor Logic |  | NOR | Low | 15 | 10 | 0.2 | 3 | 3 | Variations in input characteris tics result in base-current "hogging" problem. Proper operation not always guaranteed. More susceptible to noise because of low operating and signal voltages |
| ACTL <br> Ressistor-Capacitor Transistor Logic |  | NOR | Medium | 50 | 10 | 0.2 | 3 | 4 | Very sumilar to DCTL. Resistors resolve current "hogging" problem and reduce power dissipation. However, operating speed is riduced. |
| DCTL <br> Dract-Coupted <br> Trampstor Logic |  | NOR | Med high | 30 | 10 | 0.2 | 3 | 4 | Though capactors can increase speed capability, noise immunity is affected by capaci: tive coupling of noise signals. |
| OTL <br> Diode-Transistor <br> Loge |  | NAND | Medium | 25 | 15 | 07 | 8 | 8 | Use of pull-up resistor and charge control technique im. proves speed capabalities. Many variations of this circurt exist, each having specific advantages, |
| TTL <br> Transistor: <br> Transustor Loge |  | NAND | Medium | 10 | 20 | 1 | 8 | 12 | Very similar to DTL. Has lower parasitic capacity at uiputs. With the many existing varia. tions, this logic family is very popular. |
| CTL <br> Complimentary <br> Transistor Logic |  | OR/NOR | High | 5 | 50 | 0.4 | 5 | 25 | Sumilar to a differental ampir fier, the reference voltage sets the threshold voltage High speed, high fanout operation is possible with associated high power dissipation, Also known as emitter coupled logic (ECL). |
| CML <br> Current-Mode <br> Logic <br> IECL <br> Emuttar <br> Coupled Loget |  | AND/OR | High | 5 | 50 | 0.4 | 5 | 25 | More difficult manufacturny process results in compromises of active device characteristics and hrgher cost. |
| mosL <br> Matal-Oxida <br> Samiconductor <br> Logic | $\exists^{4}$ | NOR | Very lon | 250 | $<1$ | 2.5 | 10 | 5. | Limited in switching speed compared to bipolar transistor circuits because the MOS transis. tor is a high-impedance device and cannot charge the stray carcuit capacitance quickly. |

CHARACTERISTICS OF DISPLAYS USED IN ELECTRONIC EQUIPMENT

| Drspley Technoiogy | Averege Viewing Anglo | Typical Current Requirement | Typicel Voltege Requrement | Typicel Opereting Temperetures | Relative Brightness | Durebulity | Colors averieble (besic fight source) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Light emiting drodes | Med bright (washout in sunlight) | $150^{\circ}$ (magnifying lens cuts down angle) | 5 to 10 mA | 2 to 5 V | -40 to $85^{\circ} \mathrm{C}$ | Rugged, no breakable parts | Red, orenge yellow, green |
| Liquid crystal displays | Highcontrast. no juminance | 90 to $150^{\circ}$ | $50 \text { to } 500$ | 3 to 7V | $\begin{gathered} -10 \\ \text { to } 65^{\circ} \mathrm{C} \end{gathered}$ | Glass construction | Black on white (or reverse) |
| Gas discharge | Bright | $100^{\circ}$ | ${\underset{2 A}{150 \mathrm{~mA}} \text { to }}^{2}$ | 135 to 250 V | 0 to $70^{\circ} \mathrm{C}$ | Gas-filled glass construction | Orange |
| Incandescent | Very bright | $150^{\circ}$ | $\begin{gathered} 10 \text { to } 17 \\ \mathrm{~mA} \end{gathered}$ | 3 to 5 V | $\text { to }-55$ | Glass and filaments construction subject to shock | Whte. filterabie to most colors |
| Vacuum fluorescent | Bright | $100^{\circ}$ | $\begin{gathered} 400 \text { to } 650 \\ \mathrm{~mA} \end{gathered}$ | 30 to 50 V | $\begin{gathered} -10 \\ \text { to } 55^{\circ} \mathrm{C} \end{gathered}$ | Vacuum-tube device, glass construction | Bright-green filterable to many colors |
| (From Electronic Products, June, 1982, courtesy of Electronic Products.) |  |  |  |  |  |  |  |

## DEFINITIONS OF INTEGRATED CIRCUITS, LOGIC, AND MICROELECTRONICS TERMS

Abrading equipment This type of equipment fires a gas propelled stream of finely graded abrasive particles through a precise nozzle against the work surface. When linked to abrading equipment, it can cut intricate patterns in silicon semiconductors.
Abrasive trimming Trimming a film resistor to its nominal value by notching the resistor surface with a fine adjusted stream of abrasive material such as aluminum oxide.
Access time Time required in a computer to move information from memory to the computing mechanism.
Activating A treatment which renders nonconductive material receptive to electroless deposition.
Active elements Those components in a circuit which have gain or which direct current flow: diodes, transistors, SCR's, etc.
Active substrate A substrate for an integrated component in which parts display transistance. Examples are single crystals of semiconductor materials, within which transistors and diodes are formed.
A.D. converter Analog-to-digital converter; a circuit which accepts information in a continuously varying ac or dc current or voltage and whose output is the same information in digital form.
Adder Switching circuits which combine binary bits to generate the SUM and CARRY of these bits. Takes the bits from the two binary numbers to be added (ADDEND and AUGEND) plus the CARRY from the preceding less significant bit and generates the SUM and the CARRY.
Address Noun: a location, either name or number, where information is stored in a computer. Verb: to select or pick out the location of a stored information set for access.
Alloy junction A junction produced by alloying one or more impurity metals to a semiconductor. A small button of impurity metal is placed at each desired location on the semiconductor wafer, heated above its melting point, and cooled. The impurity metal alloys with the semiconductor material to form a $p$ or $n$ region, depending on the impurity used.
Alternate print In screen printing, one squeegee print stroke per substrate in alternate directions.
Alumina Aluminum oxide $\left(\mathrm{A1}_{2} \mathrm{O}_{3}\right)$ used as a ceramic substrate material.
Align To put into proper relative position, agreement, or coordination when placing parts of a photomask together or placing a photomask over an etched pattern in the oxide on a semiconductor wafer.
Alignment The accuracy of coordination or relative position of images on a semiconductor oxide coating and on the photomask, or any other images placed in relation to those.
"AND" A boolean logic expression used to identify the logic operation wherein given two or more variables, all must be logical " 1 " for the result to be logical "1." The AND function is graphically represented by the dot (*) symbol.
Angle of attack In screen printing, angle at which the squeegee blade attacks the screen surface.
Anticipated carry adder A parallel ADDER in which each stage is capable of looking back at all ADDEND and AUGEND bits of less significant stages and deciding whether the less significant bits provide a " 0 " or a " 1 " CARRY IN. Having determined the CARRY IN it combines it with its own ADDEND and AUGEND to give the SUM for that bit or stage. Also called FAST ADDER or look ahead CARRY ADDER.
Arrays Integrated circuits designed to perform near or actual subsystem operations. They are characterized by high complexity and component density. Each array package replaces a number of conventional I/Cs. Arrays are classified as medium-scale or larger-scale according to function performed. They can be monolithic or fabricated on a silicon wafer with interconnections between circuits.
Artwork The original pattem or configuration produced at an enlarged ratio, from which a circuit product is made, using a technique of photographic reduction to achieve microelectric scale; layouts and photographic films created to produce thick film screens and thin film masks.
As-fired Description of properties of ceramic substrates (smoothness) or thick film resistors (values) as they emerge from furnace processing, before any trimming or polishing.
Asynchronous inputs Those terminals in a flip-flop which can affect the output state of the flip-flop independent of the clock. Called Set, Preset, Reset or DC Set and Reset, or clear.
Back bonding Bonding active chips to the substrate using the back of the chip, leaving the face with its circuitry face up. The opposite is face down bonding.
Backfill Filling an evacuated hybrid circuit package with dry inert gas prior to hermetric sealing of the package.
Bake-out Elevated temperature process which evaporates unwanted gases and moisture before final sealing of a hybrid circuit package.
Ball bond Type of thermocompression bond wherein a ball shaped end interconnect wire is fiattened against a metallized pad.
Basic logic diagram A logic diagram that depicts logic functions with no reference to physical implementations. It consists primarily of logic symbols and is used to depict all logic relationships as simply and understandably as possible. Nonlogic functions are not normally shown.
Beam leads A generic term describing a system in which flat, metallic leads extend beyond the edges of a chip component, much the same as wooden beams extend from a root overhang. These are used to interconnect the component to film circuitry. Beryllia Beryllium oxide ceramics ( BeO ) significant in that they have high thermal conductivity characteristics.
Binders Substances added to unfired substrates and thick film compounds to add strength.

Binary coded decimal (BCD) A binary numbering system for coding decimal numbers in groups of 4 bits. The binary value of these 4 -bit groups ranges from 0000 to 1001 and codes the decimal digits " 0 " through 9 . To count to 9 takes 4 bits; to count to 99 takes two groups of 4 bits; to count to 999 takes three groups of 4 bits.
Binary logic Digital logic elements which operate with two distinct states. The two states are variously called true and false, high and low, on and off, or " 1 " and " 0 ." In computers they are represented by two different voltage levels. The level which is more positive (or less negative) than the other is called the high level, the other the low level. If the true (" 1 ") level is the most positive voltage, such logic is referred to as positive true or positive logic.
Bistable element Another name for flip-flop. A circuit in which the output has two stable states (output levels " 0 " or " 1 ") and can be caused to go to either of these states by input signals, but remains in that state permanently after the input signals are removed. This differentiates the bistable element from a gate also having two output states but which requires the retention of the input signals to stay in a given state. The characteristic of two stable states also differentiates it from a monostable element which keeps returning to a specific state, and an astable element which keeps changing from one state to the other.
Bit A synonym for binary numeral. Also refers to a single binary numeral in a binary word.
Bleeding In photomasking, poor edge definition or acuity caused by spread of image onto adjacent areas.
Blister A lump or raised section of a conductor or resistor caused by out-gassing of the binder or vehicle during firing. Boat A container for materials to be evaporated or fired.
Bond liftoff The failure mode whereby the bonded lead separates from the surface to which it was bonded.
Bond-to-bond distance The distance measured from the bonding site on the die to the bond impression on the post, substrate land, or fingers which must be bridged by a bonding wire or ribbon.
Bond-to-chip distance In beam lead bonding, the distance from the heel of the bond to the component.
Bonding pad A metallized area at the end of a thin metallic strip or on a semiconductor to which a connection is made. Also called Bonding Island.
Bonding ribbon and tape Bonding ribbon and tape are used in the manufacture of high-volume ICs such as memory devices and consumer products. Wire connections between I /O pads on the circuit die and the lead frame are replaced by a piece of tape with finely etched fingers that are patterned to fit exactly onto the pads.
Bonding wire Fine gold or aluminum wire for making electrical connections in hybrid circuits between various bonding pads on the semiconductor device substrate and device terminals or substrate lands.
Boolean algebra The mathematics of logic which uses alphabetic symbols to represent logical variables and " 1 " and " 0 " to represent states. There are three basic logic operations in this algebra: AND, OR, and NOT. (Also see NAND, NOR, Invert which are combinations of the three basic operations.)
Bubble memories In general, magnetic bubble memory systems consist of a film deposited on a gamet substrate. Data is stored in magnetic domains (bubbles) which are formed on the film by the application of a perpendicular magnetic field.
Buffer A circuit element, which is used to isolate between stages or handle a large fanout or to convert input and output circuits for signal level compatibility.
Bump chip A chip that has on its termination pads a bump of solder or other bonding material that is used to bond the chip to external contacts.
Bump contact A large area contact used for alloying directly to the substrate of a chip, for mounting or interconnecting purposes.
Buried layer A heavily doped ( $\mathrm{N}+$ ) region directly under the N doped epitaxial collector region of transistors in a monolithic integrated circuit used to lower the series collector resistance.
Bum-in Operation of electronic components often at elevated temperature, prior to their ultimate application in order to stabilize their characteristics and to identify their early failures.
Burn-in, dynamic High temp test with device(s) subject to actual or simulated operating conditions.
Bum-in, static High temp test with device(s) subjected to unvarying voltage rather than to operating conditions; either forward or reverse bias.
Camber In screen printing, a slight rise or curve in the surface of the substrate.
Carriage Mechanism on a screen printer to which the workholder is attached, which conveys the substrate to and from the print position.
Carriers Holders for electronic parts and devices which facilitate handling during processing, production, imprinting, or testing operations and protect such parts under transport.
Ceramic Non-metallic and inorganic material (e.g., alumina, beryllia, or steatite) used in microelectric substrates and component parts.
Cermet A combination of ceramic and metal powders used for thin and thick film resistors.
Chip A single substrate on which all the active and passive circuit elements have been fabricated using one or all of the semiconductor techniques of diffusion, passivation, masking, photoresist, and epitaxial growth. A chip is not ready for use until packaged and provided with extemal connectors. The term is also applied to discrete capacitors and resistors which are small enough to be bonded to substrates by hybrid techniques.
Chip and wire A hybrid technology exclusively employing face-up-bonded chip devices interconnected to the substrate conventionally, i.e., by flying wires.
Chip architecture The design or structure of an IC chip, incorporating arithmetic logic unit, registers, and control-bus pathway configuration.

Chip capacitors Discrete devices which introduce capacitance into an electronic circuit, made in tiny wedge or rectangular shapes to be fired onto hybrid circuits.
Chip component An unpackaged circuit element (active or passive) for use in hybrid microelectronics. Besides ICs, the term includes diodes, transistors, resistors, and capacitors.
Chip-outs Semiconductor die defects where fragments of silicon on the face have been chipped off in processing, leaving an active junction exposed.
Circuit The interconnection of a number of devices in one or more closed paths to perform a desired electrical or electronic function.
Clean room A work station or processing area in which steps are taken (e.g., air filtering) to protect incomplete circuits from dust and contamination.
Clear An asynchronous input. Also called Reset. To restore a memory elementor flip-flop to a "standard" state, forcing the Q terminal to logic " 0 ."
Clearance The shortest distance between the outer edges of images applied in sequence.
Clock A pulse generator which controls the timing of computer switching circuits and memory stages and regulates the speed at which the computer central processor operates. It serves to synchronize all operations in a digital system.
Clock input That terminal on a flip-flop whose condition or change of condition controls the admission of data into a flip-flop through the synchronous inputs and thereby controls the output state of the flip-flop. The clock signal performs two functions:
(1) It permits data signals to enter the flip-flop; (2) after entry, it directs the flip-flop to change state accordingly.

CML (Current Mode Logic) Logic in which transistors operate in the unsaturated mode as distinguished from most other logic types which operate in the saturation region. This logic has very fast switching speeds and low logic swings. Also called ECL or MECL.
CMOS Complementary metal-oxide semiconductor. Device formed by the combination of a PMOS and an NMOS (P-type and N -type channel semiconductors).
Co-fire To place circuits onto an unfired ceramic and fire both circuits and ceramic simultaneously.
Collector junction The semiconductor junction in a transistor between the collector and base regions.
Collocator Device used to collect substrates from a screen printer and deposit them, in rows, onto a conveyor/dryer or furnace belt.
Compliant bond A bond which uses an elastically and /or plastically deformable member to import the required energy to the lead.
Component A packaged functional unit consisting of one or more circuits made up of devices, which (in turn) may be part of an operating system or subsystem. A part of, or division of, the whole assembly or equipment.
Component part A term sometimes used to denote a passive device.
Component placement equipment Automatic systems for sorting and placing components onto hybrid circuit substrates: consisting of indexing-conveyor, sorter, placement heads, missing component detector, programmable electro-pneumatic control, and options to handle special requirements.
Con/dryer Process equipment designed to receive screen printed substrates and dry the ink on the substrate while conveying them away.
Contact printing Print mode in screen printing wherein entire substrate contacts bottom surface of screen during print cycle. Necessary when using metal masks.
Contaminant An impurity or foreign substance present in a material that affects one or more properties of the material.
Cosmetic defect A variation from the conventional appearance of an item, such as a slight change in color: not necessarily detrimental to performance.
Corrosion In semiconductors, a defect in or on the aluminum metallization, usually a white crystalline growth.
Counter A device capable of changing states in a specified sequence upon receiving appropriate input signals. The output of the counter indicates the number of pulses which have been applied. (See also Divider.) A counter is made from flip-flops and some gates. The output of all flip-flops are accessible to indicate the exact count at all times.
Counter, binary An interconnection of flip-flops having a signal input so arranged to enable binary counting. Each time a pulse appears at the input, the counter changes state and tabulates the number of input pulses for readout in binary form. It has a $2^{n}$ possible counts where $n$ is the number of flip-flops.
Counter, ring A special form of counter sometimes called a Johnson or shift counter which has very simple wiring and is fast. It forms a loop or circuits of interconnected flip-flops so arranged that only one is " 0 " and that as input signals are received, the positioning of the " 0 " state moved in sequence from one flip-flop to another around the loop until they are all " 0 ," then the first one goes to " 1 " and this moves in sequence from one flip-flop to another until all are " 1 . "It has $2 \times n$ possible counts where $n$ is the number of flip-flops.
Cover lay, cover coat Outer layer(s) of insulating material applied over the conductive pattern on the surface of the substrate.
Crazing Minute cracks on or near the surface of materials such as ceramic.
Data Term used to denote facts, numbers, letters, symbols, binary bits presented as voltage levels in a computer. In a binary system data can only be " 0 " or "1."
DCTL (Direct-Coupled Transistor Logic) Logic employing only transistors as active circuit elements.
Debug To remove malfunctions from a system or device.

Decimal A system of numerical representation which uses ten numerals $0,1,2,3, \ldots, 9$. Each numeral is called a digit. $A$ number system to the radix 10.
Defect Any deviation from the normally accepted characteristics of a product or component.
Delay The slowing up of the propagation of a pulse either intentionally, such as to prevent inputs from changing while clock pulses are present, or unintentionally as caused by transistor rise and fall time pulse response effects.
Detailed logic diagram A diagram that depicts all logic functions and also shows nonlogic functions, socket locations, pin numbers, test points, and other physical elements necessary to describe the physical and electrical aspects of the logic. The detailed logic diagram is used primarily to facilitate the rapid diagnosis and localization of equipment malfunctions. It also is used to verify the physical consistency of the logic and to prepare fabrication instructions. The symbols are connected by lines that represent signal paths.
Detritus Fragments of material produced during resistor trimming which remain in the trimmed area.
Device The physical realization of an individual electrical element in a physical independent body which cannot be further reduced or divided without destroying its stated function. This term is commonly applied to active devices. Examples are transistors, pnpn structures, tunnel diodes, resistors, capacitors, and inductors.
Diamond powders, grits, and compounds These materials are used mainly as abrasives for processes such as lapping and polishing, abrasives in abrasive trimming, or to create the cutting surface of slicing equipment.
Die A tiny piece of semiconductor material, broken from a semiconductor slice, on which one or more active electronic components are formed. (Sometimes called chip).
Die bonding Attaching the semiconductor chip to the substrate, with an epoxy, eutectic, or solder alloy.
Dielectric isolation The use of silicon dioxide barriers created during silicon IC processing to provide isolation between components on a chip.
Diffusion A process, used in the production of semiconductors, which introduces minute amounts of impurities into a substrate material such as silicon or germanium and permits the impurity to spread into the substrate. The process is very dependent on temperature and time.
Diffusion and oxidation systems Equipment in which non-conductive materials are made semiconductive by diffusing controlled amounts of selected impurities into the surface and the surface of silicon is oxidized selectively to provide a protective or insulative layer. Diffusion and oxidation are accomplished by exposing the silicon wafer to specific atmospheres in a high temperature fumace.
Diffusion depth testing A diffusion depth tester determines to what depth diffused impurities have been implanted into a wafer under ion implantation.
Digital circuit A circuit which operates in the manner of a switch, that is, it is either "on" or "off." More correctly should be called a binary circuit.
Diode A device permitting current to flow in one direction only. Diodes are used in logic circuits to control the passage or nonpassage of a signal from one element to another.
Discrete Having an individual identity. Fabricated prior to installation, and /or separately packaged, not part of an integrated circuit.
DIP Dual in-line package.
Discrete circuits Electronic circuits built of separate, individually manufactured, tested, and assembled diodes, resistors, transistors, capacitors, and other specific electronic components.
Discrete component A circuit component having an individual identity, such as a transistor, capacitor, or resistor.
Divider (frequency) A counter which has a gating structure added which provides an output pulse after receiving a specified number of input pulses. The outputs of all flip-flops are not accessible.
Dopants Selected impurities introduced into semiconductor substrates in controlled amounts, the atoms of which form negative ( $n$-type) and positive (p-type) conductive regions. Phosphorus, arsenic, and antimony are n-type dopants for silicon; boron, aluminum, gallium, and indium are p-type dopants for silicon.
Doping Addition of controlled impurities to a non-conductive material to achieve the desired semiconductor characteristic, accomplished through thermal diffusion or ion implantation.
Dot "AND" Externally connecting separate circuits or functions so that the combination of their outputs results in an "AND" function. The point at which the separate circuits are wired together will be a "1" if all circuits feeding into this point are " 1 " (also called WIRED "OR").
Dot "DR" Externally connecting separate circuits or functions, so that the combination of their outputs results in an "OR" function. The point at which the separate circuits are wired together will be a "1" if any of the circuits feeding into this point are "1."
Driver An element which is coupled to the output stage of a circuit in order to increase its power or current handling capability or fanout; for example, a clock driver is used to supply the current necessary for a clock line.
DTL (Diode-Transistor Logic) Logic employing diodes with transistors used only as inverting amplifiers.
Dual-in-line package (DIP)) Carrier in which a semiconductor integrated circuit is assembled and sealed. Package consists of a plastic or ceramic body with two rows of seven vertical leads which are inserted into a circuit board and secured by soldering.
Durometer An instrument for measuring the hardness of the squeegee material for screen printing.
ECL Emitter-coupled logic; a type of current mode logic in which the circuits are coupled with one another through emitter followers at the input or output of the logic circuit.

Ejection Wipe off or removal of the printed part from the workholder, in screen printing.
Electrical element The concept in uncombined form of the individual building blocks from which electric circuits are synthesized.
Electron beam bonding Process using a stream of electrons to heat and bond two conductors within a vacuum.
Electron beam lithography Lithography in which the radiation sensitive film or resist is placed in the vacuum chamber of a scanning beam electron microscope and exposed by an electron beam under digital computer control.
Electron heam welding Process in which welder generates a stream of electrons traveling at up to $60 \%$ of the speed of light, focuses it to a small, precisely controlled spot in a vacuum, and converts the kinetic energy into extremely high temperature on impact with the workpiece.
Emitter The region of transistor from which charge carriers (minority carriers in the base) are injected into the base.
Enable To permit an action or the acceptance or recognition of data by applying appropriate signals (generally a logic " 1 " in a positive logic) to the appropriate input. (See Inhibit.)
Encapsulate To embed electronic components or other entities in a protective coating, usually done when the plastic encapsulant is in fluid state so that it will set in solid form as an envelope around the work.
Entrapment The damaging admission and trapping of air, flux, and fumes, caused by contamination and plating process defects.
Epitaxial Pertaining to a single-crystal layer on a crystalline substrate, and having the same crystalline orientation as the substrate: e.g., silicon atoms condensed from vapor phase onto a silicon-wafer substrate.
Epitaxial growth A process of growing layers of material on a selected substrate. Usually silicon is grown in a silicon substrate. Silicon and other semiconductor materials may be grown on a substrate with compatible crystalography, such as sapphire (silicon-on-sapphire).
Epitaxial layer A precisely doped, thin layer of silicon grown on a p-doped thick wafer and into which $n$-type semiconductor junctions are diffused.
EPROM Electrically programmable read only memory.

## Etch factor

The ratio of depth of etch to the amount of undercut.
Exclusive " 0 " A logical function whose output is " 1 " if either of the two variables is " 1 " but whose output is " 0 " if both inputs are "1" or both are "0."
Exposure The act of subjecting photosensitive surfaces or matter to radiant energy such as light to produce an image.
Evaporation and sputtering materials Metals used for evaporation charges and sputtering targets, including: chromium and
its alloys, for (1) a thin adhesive layer on IC substrates to allow better deposition of gold or other metal, (2) resistor material, and
(3) vacuum deposition in mask production; aluminum and certain Al alloys, for first layer deposition in MOS technology; molybdenum, as a conductor or adhesive layer for IC fabrication; and titanium, as an intermediate adhesive layer for beam-lead interconnection.
Evaporation sources Boats and filaments used as heat sources for vacuum evaporation to form thin film layers on substrates. The process is frequently done by resistively heating the evaporant in a ceramic crucible or by self-heating or boats constructed of tungsten, molybdenum, or tantalium.
Extrinsic properties Properties introduced into a semiconductor by impurities with a crystal.
Extrinsic semiconductor The resulting semiconductor produced when impurities are introduced into an otherwise nonsemiconductor crystal. The electrical properties depend upon the impurities.
Face bonding Process of bonding semiconductor chip so that its circuitry side faces the substrate. Flipchip and beam lead bonding are two common methods. (Opposite of back bonding.)
Fall time A measure of the time required for the output voltage of a circuit to change from a high voltage level to a low voltage level once a level change has started. Current could also be used as the reference, that is, from a high current to a low current level.
Fanin The number of inputs available to a specific logic stage of function.
Fanout The number of input stages that can be driven by a circuit output.
Fast ADDER (See Anticipated CARRY ADDER.)
FEB (Functional Electronic Block) Another name for a monolithic integrated circuit of thick-film circuit.
Feedback When part of the output of a circuit is channeled back to an input, it is said to have feedback. When part of the output of an amplifier is routed back to augment the input signal, the amplifier has positive feedback or if this rechanneling is employed to diminish the input it is called negative feedback.
FET Field effect transistor; semiconductor device in which resistance between source and drain terminals is modulated by a field applied to the third (gate) terminal.
Film conductor Electrically conductive material formed by deposition on a substrate.
Film microcircuit Thin or thick film network forming an electrical interconnection of numerous devices.
Film resistor A device whose resistive material is a film on an insulator substrate; resistance value is determined by trimming.
Final seal The hybrid microelectronic packaging step which encloses the circuit so that further intemal processing cannot be performed without disassembly.
Flatpack Subassembly composed of two or more stages made up of integrated circuits and thin film components mounted
on a ceramic substrate. This semiconductor network is enclosed in a shallow rectangular package with the connecting leads projecting from edges of the package.
Flip-chip A generic term describing a semiconductor device having all terminations on one side of the form of bump contacts. After the surface of the chip has been passivated or otherwise treated, it is flipped over for attaching to a matching substrate.
Flip-flop (storage element) A circuit having two stable states and the capability of changing from one state to another with the application of a control signal and remaining in that state after removal of signals. (See Bistable element.)
Flip-flop, "D" D stands for delay. A flip-flop whose output is a function of the input which appeared one pulse earlier; for example, if a "1" appeared at the input, the output after the next clock pulse will be a "1."
Flip-flop, "J-K" A flip-flop having two inputs designated J and K . At the application of a clock pulse, a " 1 " on the " J " input and $a$ " 0 " on the " $K$ " input will set the flip-flop to the " 1 " state; $a$ " 1 " on the " $K$ " input and a " 0 " on the " J " input will reset it to the " 0 " state; and "1's" simultaneously on both inputs will cause it to change state regardless of the previous state. $\mathrm{J}=0$ and $\mathrm{K}=0$ will prevent change.
Flip-flop, "R-S" A flip-flop consisting of two cross-coupled NAND gates having two inputs designated "R" and "S." $A$ " 1 " on the " $S$ " input and " 0 " on the " $R$ " input will reset (clear) the flip-flop to the " 0 " state, and " 1 " on the " $R$ " input and " 0 " on the " S " input will set it to the "1." It is assumed that " 0 's" will never appear simultaneously at both inputs. If both inputs have " 1 ' $s$ " it will stay as it was. " 1 " is considered nonactivating. A similar circuit can be formed with NOR gates.
Flip-flop, "R-S-T" A flip-flop having three inputs, "R," "S," and "T." This unit works as the "R-S" flip-flop except that the "T" input is used to cause the flip-flop to change states.
Flip-flop, "T" A flip-flop having only one input. A pulse appearing on the input will cause the flip-flop to change states. Used in ripple counters.
Floating squeegee This squeegee, as opposed to a rigid squeegee, has the ability to produce a rocking movement on the horizontal plane in screen printing.
Flood stroke Return stroke of squeegee in screen printing which redistributes ink back over the pattern. Provides for proper ink control, and is especially useful for thixotropic inks. (See "Print Stroke".)
Fluid flow masking A gold electro-plating technique in which the work to be plated is the cathode and current flows through the fluid stream of plating material, allowing control of deposit at the point of contact between the stream and the workpiece.
Furnaces, diffusion and firing Systems designed for enclosed elevated temperature processing of solid state devices and systems, in gaseous atmospheres. Diffusion furnaces are operated at temperatures from 1,000 to $1300^{\circ} \mathrm{C}$ to achieve doping of semiconductor substrates, by one of a number of processes. Oxidation is a process that puts a protective layer of silicon oxide on the wafer and is used either as an insulator or to mask out certain areas when doping. Deposition systems, of which there are three (liquid, gaseous, solid), are used to deposit impurities on the silicon wafer. Other systems include a drive-in system used to diffuse impurities into the wafer to a specified level, and an alloy system which is used in a final step of the metallization process. Firing furnaces are used for the curing of multilayer ceramics for integrated electronics and for the firing of thick film materials on microcircuits.
Furnace, screen printing Process equipment designed to cure substrates after screen printing and drying.

## FULL ADDER See Adder.

Gate 1. A circuit having an output and a multiplicity of inputs designed so that the output is energized only when a certain combination of pulses is present at the inputs. An AND-gate delivers an output pulse only when every input is energized simultaneously in a specified manner. An OR-gate delivers an output pulse when any one or more of the pulses meet the specified conditions. 2. An electrode in a field effect transistor. 3. A circuit that admits and amplifies or passes a signal only when a gating (triggering) pulse is present. 4. A circuit in which one signal serves to switch another signal on and off.

## Gate definitions below assume positive logic

Gate, AND All inputs must have " 1 " level signals at the input to produce a " 1 " level output.
Gate, NAND All inputs must have " 1 " level signals at the input to produce a " 0 " level output.
Gate, NOR Any one input or more than one input having a "1" level signal will produce a "0" level output.
Gate, OR Any one input or more than one input having a " 1 " level signal will produce a " 1 " level output.
Gates (decision elements) A circuit having two or more inputs and one output. The output depends upon the combination of logic signals at the input.
Germanium polycrystalline A prime raw material for making crystal ingots.
Glassivation A deposited layer of glass on top of a metallized wafer or chip; primarily a protective layer.
Glazed substrate Ceramic substrate with a glass coating to effect a smooth and nonporous surface.
Green ceramic Unfired ceramic material.
Green substrate Unfired material in substrate form. Normally substrates are printed after firing. Under special circumstances, however, green (unfired) substrates are printed.
Half ADDER A switching circuit which combines binary bits to generate the SUM and the CARRY. It can only take in the two binary bits to be added and generate the SUM and CARRY (see also ADDER).
Half shift register Another name for certain types of flip-flops when used in a shift register. It takes two of these to make one stage in a shift register.

Header Base of a hybrid circuit package, holding the leads.
High See Binary logic.
High temperature reverse bias Burn-in type test of diodes and transistors conducted with the junctions reverse biased to effect any failure due to ion migration in bonds of dissimilar metals
Hole A mobile vacancy or electron deficiency in the valence structure of a semiconductor. It is equivalent to a positive charge.
HTRB High temperature reverse bias.
Hybrid A method of manufacturing integrated circuits by using a combination of monolithic, thin-film and thick-film techniques.
IC Integrated circuit.
IC socket Female contact which provides pluggable electrical engagement on its inner surface for integrated circuit components to achieve interfacing to a PCB.
Image/pattern The printed screen or design on the substrate after screen printing.
Inhibit To prevent an action, or acceptance of data, by applying an appropriate signal to the appropriate input (generally a logic " 0 " in positive logic). (See Enable.)
Ink In hybrid technology the conductive paste used on thick film materials to form the printed conductor pattern. Usually contains metals, metal oxide, glass frit, and solvent.
Input/output Interface circuits or devices offering access between external circuits and the central processing unit or memory.
Integrated circuit (EIA definition) (1) "The physical realization of a number of electrical elements inseparably associated on or within a continuous body of semiconductor material to perform the functions of a circuit." (See Slice and Chip.) (2) Electronic circuits or systems consisting of an interconnected array of extremely small active and passive elements, inseparably associated on or within a continuous substrate or body. Other names are integrated electronic circuit, integrated electronic system, and integrated microcircuit.
Integrated injection logic Integrated circuit logic which uses bipolar transistor gates. Makes possible large scale integration on silicon for logic arrays and other analog and digital applications.
Inverter A circuit whose output is always in the opposite state from the input. This is also called a NOT circuit. (A teeter-totter is a mechanical inverter.)
1/0 Input/output.
Ion implantation Precise and reproducible method of doping semiconductors to achieve a desired characteristic. lons of the particular dopant are energized and accelerated to the point where they can be driven in a focused beam directly into the silicon wafer. This technique assures uniform, accurately controlled depth of implantation and ionic diffusion in the wafer.
Ion milling Ion milling is a VLSI production technique that performs many of the same type of tasks that more traditional wet chemical and plasma etching processes do.
ISHM The International Society for Hybrid Microelectronics.
Isolation diffusion In MIC technology, the diffusion step which generates back-to-back junctions to isolate active devices from one another.
Josephson effect The tunneling of electron pairs through a thin insulating barrier between two superconducting materials.
Junction A joining of two different semiconductors or of semiconductor and metal. Alloy, diffused, electrochemical, and grown are the four junction types.
Kerf The slit or channel cut in a resistor during trimming by laser beam of abrasive jet.
Laminar flow A directed stream of filtered air moved constantly across a clean work station, usually parallel to the workbench surface.
Land area in image Closed spaces in the screen which result in open spaces on the printed image in screen printing.
Lapping Grinding and polishing such products as semiconductor blanks in order to obtain precise thicknesses or extremely smooth, flat, polishing surfaces.
Large-scale integration (LSI) Usually denotes arrays of integrated circuits on a single substrate that comprise 100 or more individual active circuit functions or gates.
Laser bonding A process which forms a metal-to-metal fastened union, using a laser heat source to join conductors.
Laser trim The adjustment (upward) of a film resistor value by applying heat from a focused laser source to remove material.
Laser welding Process in which thermal energy released by a laser impinging upon the surface of a metal is conducted into the bulk of the metal work-piece by thermal conduction, bonding component leads to highly conductive materials such as copper printed circuitry.
Lead frame The metal part of a solid state device package which achieves electrical connection between the die and other parts of the systems of which the IC is a component. Large scale integrated circuits are welded onto lead frames in such a way that leads are available to facilitate making connections to and from the various solid state devices to the packages.
Leadless inverted device (LID) A shaped, metallized ceramic form used as an intermediate carrier for the semiconductor chip devices, especially adapted for attachment to conductor lands of a thick or thin film network by reflow solder bonding.
Leak detectors Applied only to hermetic devices, fine leak detectors are used to detect defects in sealing that are too small to be detected by gross-leak methods. Devices are placed in a bomb pressurized with a mixture of gases.

LID Leadless inverted device.
Life aging Burn-in test which moderates the elevation of temperature and extends the time period in order to test overall device quality as opposed to infant mortality.
Linear circuit A circuit whose output is an amplified version of its input, or whose output is a predetermined variation of its input.
Logic A mathematical arrangement using symbols to represent relationships and quantities, handled in a microelectronic network of switching circuits or gates, which perform certain functions; also, the type of gate structure used in part of a data processing system.
Logic diagram A picture representation for the logical functions of AND, OR, NAND, NOR, NOT.
Logic function A combinational, storage, delay, or sequential function expressing a relationship between variable signal input(s) to a system or device and the resultant output(s).
Logic swing The voltage difference between the two logic levels "1" and "0."
Logic symbol The graphic representation of the aggregate of all the parts implementing a logic function.
Low See Binary logic.
LSI Large scale integration.
Magnetic integrated circuit The physical realization of one or more magnetic elements inseparably associated to perform all, or at least a major portion, of its intended function.
Masks, microelectronic Thin metals or other materials with an open pattern designed to mask off or shield selected portions of semiconductors or other surfaces during deposition processes. There also are photomasks or optical masks for contact or projection printing of wafers-these may use an extremely flat glass substrate with iron oxide, chrome, or emulsion coating. There also are thick film screen masks.
Medium scale integration (MSI) The physical realization of a microelectronic circuit fabricated from a single semiconductor integrated circuit having circuitry equivalent to more than 10 individual gates or active circuit functions.
Memory The semi-permanent storage of numbers, in digital form, in a circuit or system. With reference to computers, the term also describes the storage capability or location and which receives and holds information for later use. Also, the storage arrangement, such as RAM or other type.
Metallization The selective deposition of metal film on a substrate to form conductive interconnection between IC elements and points for connections with the outside world.
Metal-oxide-semiconductor (MOS) A metal over silicon oxide over silicon arrangement which produces circuit components such as transistors. Electrical characteristics are similar to vacuum tubes.
MIC Monolithic integrated circuit.
Microbond The realization of a very small fastened joint between conductors or between a conductor and a microelectronic chip device.
Microcircuit The physical realization of a hybrid or monolithic interconnected array of very small active and passive electronic elements.
Microelectronics The entire spectrum of electronic art dealing with the fabrication of sophisticated, practical systems using miniaturized electronic components. Microelectronics has developed along two basic technologies-monolithic integrated circuits and hybrid integrated circuits.
Microminiaturization The process of packaging an assembly of microminiature active and passive electronic elements, replacing an assembly of much larger and different parts.
Micromodule A microcircuit constructed of a number of components (e.g., microwafers) and encapsulated to form a block that is still only a fraction of an inch in any dimension.
Microprobe An extremely sharp and small exploring tool head attached to a positioning handle, used for testing microelectronic circuits by establishing ohmic contact.
Microprocessor An IC package incorporating logic, memory, control, computer, and/or interface circuits, the whole of which is designed to handle certain functions.
Microwave integrated circuit The physical realization of an electronic circuit operating at frequencies above one gigahertz and fabricated by microelectronic techniques. Either hybrid or monolithic integrated circuit technology may be utilized.
Minority carrier The less-predominant carrier in a semiconductor. Electrons are the minority in p-type; holes are the minority in n-type semiconductors.
Mobility. The ease with which charge carriers can move through a semiconductor. Generally electornics and holes do not have equal mobility in a given semiconductor. Mobility is higher in germanium than in silicon.
Module A packaging unit displaying regularity and separable repetition. It may or may not be separable from other modules after initial assembly. Usually all major dimensions are in accordance with a prescribed set of dimensions.
Molecular beam epitaxy equipment This equipment is used for growing epitaxial thin films under UHV conditions by directing beams of atoms or molecules created by thermal or electron beam evaporation onto clean, heated substrates.
Molecular electronics Simply, electronics on a molecular scale, dealing with the production of complex circuitry in semiconductor devices with integral elements processed by growing multi-zoned crystals in a furnace for the ultimate performance of electrical functions.
Monolithic Refers to the single silicon substrate in which an integrated circuit is constructed. (See Integrated circuit.)
Monolithic integrated circuit The physical realization of electronic circuits or sub-systems from a number of extremely small
circuit elements inseparably associated on or within a continuous body or a thin film of semiconductor material.
Morphology, integrated The structural characterization of an electronic component in which the identity of the current or signal modifying areas, patterns, or volumes has become lost in the integration of electronic materials, in contrast to an assembly of devices performing the same function.
Morphology, translational The structural characterization of an electronic component in which the areas or patterns of resistive, conductive, dielectric, and active materials in or on the surface of the structure can be identified in a one-to-one correspondence with devices assembled to perform an equivalent function.
MOS Metal-oxide-semiconductor. A technology for producing transistors that incorporates metal over oxide over silicon layers. Electrical characteristics are similar to vacuurn tubes.
MSI Medium scale integration.
MTNS Metal thick nitride semiconductor, which is similar to an MTOS device except that a thick silicon nitride or silicon nitride-oxide layer is used instead of just plain oxide.
MTOS Metal thick oxide semiconductor, where the oxide outside the desired active gate area is made much thicker in order to reduce problems with unwanted parasitic effects.
Multichip integrated circuit Hybrid integrated circuit which includes two or more SIC. MSI, or LSI chips.
Multilayer dielectric A compound including glass and ceramic which is applied as an insulating barrier between conductors for multi-layer and crossover work.
"NAND" A Boolean logic operation which yields a logic " 0 " output when all logic input signals are logic "1."
Negative logic Logic in which the more negative voltage represents the " 1 " state; the less negative voltage represents the "0" state. (See Binary logic.)
Network A collection of elements, such as resistors, coils, capacitors, and sources of energy, connected together to form several interrelated circuits.
NMOS N-channel MOS circuits, using currents made up of negative charges and producing devices at least twice as fast as PMOS.
Noble metal paste A soft, moist, smooth compound made up partially of precious metals such as gold, platinum, ruthenium, or others classed as noble metals, providing conductors in film circuitry.
Noble system Thick film system using conductors of gold, platinum, and possibly palladium silver, or certain alloys of these precious metals.
Noise immunity A measure of the insensitivity of a logic circuit to triggering or reaction to spurious or undesirable electrical signals or noise, largely determined by the signal swing of the logic. Noise can be either of two directions, positive or negative.
Non-noble system Thick film system using conductors of copper, tungsten, nickel, molybdenum, and other non-noble metals.
"NOR" A Boolean logic operation which yields a logic " 0 " output with one or more true " 1 " input signals.
"NOT" A Boolean logicoperation indicating negation, not " 1 ." Actually an inverter. If inputs is " 1 " output is NOT " 1 " but " 0 ." If the input is " 0 " output is NOT " 0 " but " 1 ." Graphically represented by a bar over a Boolean symbol such as A. A means "when A is not 1 ."
n -Region The zone in a semiconductor in which electron density is greater than hole density.
n-type Semiconductor material whose impurities produce free electrons in the compound, leading to conduction.
$n$-type semiconductor An extrinsic semiconductor in which electron density exceeds hole density. An electron donor type.
Off-contact printing Print mode wherein screen printer's squeegee stretches screen to touch the substrate and deposit ink. Usually $0.010^{\prime \prime}$ snap-off is used. Allows thicker ink deposition.
Offset The change in input voltage required to produce a zero output voltage in a linear amplifier circuit. In digital circuits it is the dc voltage on which a signal is impressed.
One ("1") See Binary Logic.
"OR" A Boolean logic operation used to identify the logic operation wherein two or more true " 1 " inputs only add to one true "1" output. Only one input needs to be "true" to produce a "true" output. The graphical symbol for "OR" is a plus sign ( + ).
Overglaze A glass compound in low-melting, vitreous form, used as a coating to passivate thick film resistors and offer mechanical protection.
Overlap The contact area between a film resistor and film conductor.
Packaging The process of physically locating, connecting, and protecting devices or components.
Packaging density The number of devices or equivalent devices per unit volume in a working system or subsystem.
Pad In IC technology, the bonding area.
Parallel gap welding Type of resistance welding wherein electrodes contact the work from one side only. Mechanism by which bonding occurs is virtually always fusion. Process is well suited to welding component leads to planar surfaces such as IC leads to PC conductors.
Parallelity Relationship of screento work-holder and print head in screen printing. Each should be parallel to one another in order to print accurately.
Parameter Any specific characteristic of a device. When considered together, all the parameters of a device describe its operational and physical characteristics.
Parallel This refers to the technique for handling a binary data word which has more than one bit. All bits are acted upon simultaneously. It is like the line of a football team. Upon a signal all line men act. (See also Serial.)

Parallel Adder A conventional technique for adding where the two multibit numbers are presented and added simultaneously (parallel). A ripple adder is still a parallel adder; the carry is rippled from the least significant to the most significant bit. Another type of parallel adder is the "Look Ahead," or "Anticipated Carry" adder. (See Ripple ADDER and Fast ADDER.)
Parallel operation The organization of data manipulation within computer circuitry where all the digits of a word are transmitted simultaneously on separate lines in order to speed up operation, as opposed to serial operation.
Particle impact noise detection (PIND) PIND testing equipment detects any loose foreign particles that may be present in a hermetic package. The package is placed on a shaker table where it is in intimate contact with an acoustic transducer that drives an ultrasonic amplifier.
Parts handling Devices used to load and unload substrates during screen printing and drying operations.
Passivation The growth of an insulating layer on the surface of a semiconductor to provide electrical stability by isolating the transistor surface from electrical and chemical conditions in the environment. It reduces reverse-current leakage, increases breakdown voltages, and improves the power-dissipation rating.
Passive elements Resistors, inductors, or capacitors, elements without gain.
Passive substrate A substrate for an integrated component which may serve as physical support and thermal link to a thickor thin-film integrated circuit, but which exhibits no transistance. Examples of passive substrates are glass, ceramic, and similar materials.
Paste Synonymous with "composition" and "ink" when relating to screenable, thick film materials.
Pattern/image The open area in the screen through which the ink penetrates to become the printed image on the substrate, in screen printing.
Photomask A square, flat glass substrate, coated with a photographic emulsion or a very thin layer of metal, on which appear several hundred circuit pattems (each containing thousands of images). The patterns are exposed onto semiconductor wafers.
Photoresists and processing materials These are light sensitive materials that are deposited as a uniform film on a wafer or substrate. The exposure of specific pattern is performed through masking operations.
Pinhole A minute hole through a layer or pattern.
Planar process Fabrication of MICs and semiconductor devices using silicon dioxide as a masking agent and producing components on a single plane.
Platen Plate which holds substrate during screen printing.
Plating The deposition of a metal layer on a substrate surface by electrolytical or certain chemical means. The materials include gold, copper, solder, etc. The functions of the metal plate vary, including corrosion protection, solderability enhancement, etch resist, bonding for lead frames, and electrical connection, among others.
PMOS P-channel MOS: refers to the oldest type of MOS circuit where the electrical current is a flow of positive charges.
Polishing A mechanical finishing operation conducted upon solid state substrates to achieve smoothness and desired surface qualities. See Lapping.
Porcelainize To coat and fire a metal with glass material, forming a hybrid circuit substrate.
Positive logic Logic in which the more positive voltage represents the "1" stage. (See Binary logic.)
Preset An input like the Set input and which works in parallel with the Set.
Probing A term used to describe electrical testing that employs very finely-tipped probes applied sequentially to each of the finished dice of a wafer.
PROM Programmable read-only memory; a ROM which requires a programming operation.
Propagation delay A measure of the time required for a change in logic level to be transmitted through an element or a chain of elements.
Propagation time The time necessary for a unit of binary information (high voltage or low) to be transmitted or passed from one physical point in a system or subsystem to another. For example, from input of a device to output.
p-type semiconductor An extrinsic semiconductor in which the hole density exceeds the conduction electron density. An electron acceptor type.
Print stroke Stroke of the squeegee in screen printing at which time ink is forced through the pattem on the screen.
Print-print Squeegee prints in both directions per substrate in screen printing process.
Printer Process unit designed to accept, hold, and screen print a substrate in order that ink may be applied with extremely accurate and repeatable registration.
Pulse A signal of very short duration.
Purple plague Defect-causing formation of gold-aluminum chemical compounds often produced when gold and aluminum are bonded. Purple in color, brittle, subject to degenerative failure, and sometimes compounded by inclusion of silicon.
Q output The reference output of a flip-flop. When this output is " 1 " the flip-flop is said to be in the " 1 " state; when it is " 0 " the output is said to be in the "0" state. (See also State and Set.)
$\overline{\mathrm{Q}}$ output The second output of a flip-flop. It is always opposite in logic level to the Q output.
RAM Random access memory; a type of memory which offers access to storage locations within it by means of $X$ and $Y$ coordinates.
RCTL (Resistor-Capacitor-Transistor-Logic) Same as RTL except that capacitors are used to enhance switching speed. Register A device which can store information, usually that contained in a small subset or word of the total within a digital computer system.

Registration The degree of proper alignment of a circuit pattern on the substrate.
Resist Material such as ink, paint, or metallic plating, used to protect the desired portions of the printed conductive pattern from the action of the etchant, solder, or plating.
Reset Also called clear. Similar to Set except it is the input through which the Q output can be made to go to "0."
Rigid squeegee Firm mounting of the screen printer squeegee blade and holder. Squeegee adjustment is more critical.
Ripple The transmission of data serially. It is a serial reaction analogous to a bucket brigade or a row of falling dominoes.
Ripple ADDER A binary adding system similar to the system most people used to add decimal numbers-that is, add the
"units" column, get the carry, add it to the " 10 's" column, get the carry, add it to the " 100 ' s " column, and so on. Again it is necessary to wait for the signal to propagate through all columns even though all columns are present at once (parallel). Note that the carry is rippled.
Ripple counter A binary counting system in which flip-flops are connected in series. When the first flip-flop changes it effects the second which effects the third and so on. If there are ten in a row, the signal must go sequentially from the first flip-flop to the tenth.
Risers In a multilayer substrate, the conductive paths that vertically connect various levels.
Rotary (theta) motion Angular (rotary) adjustment of image to substrate. Allows registration in angularity in addition to " X " and " $Y$ " in screen printing. (Also called Theta motion.)
Rise time A measure of the time required for the output voltage of a state to go from a low voltage level (" 0 ") to a high voltage level ("1") once a level change has been started.
ROM Read-only memory; a random access storage in which the data pattern is unchangeable after manufacture.
RTL (Resistor-Transistor-Logic) Logic is performed by resistors. Transistors are used to produce an inverted output.
Sapphire substrates Materials which provide a uniform dielectric constant, controlled orientation, thermal conductivity, and the single crystal surface desired for SOS, hybrid IC, and other microcircuit systems. The material may be grown directly in ribbons, tubes, filaments. and sheets.
Screen Tensioned mesh material with an open pattern through which ink penetrates to place an image on the substrate. Screen is above and parallel to the substrate during screen printing.
Screen printing, thick film The art of depositing conductive, resistive, and insulating materials on a dielectric base. This deposition is made through selected open areas in screens with inks or pastes forced through the open areas of the screen by squeegee motion onto the substrate base. In some cases, masks instead of conventional mesh screens may be used.
Scribing Scratching a tooled line or laser path on a brittle substrate to allow a wafer to be cleft or broken along the line, producing IC chips when all brakes are completed.
Scribing machines and tools Equipment used to separate wafers into individual devices, chips, or dice. This has been done by crude techniques similar to glass cutting, but is now accomplished by more efficient methods, using truncated pyramid diamond scribers, automated machines, conical tools, or lasers.
SEM Standard electronic module; a subassembly configuration format which meets a particular U.S. Navy set of specifications. This abbreviation is also used for scanning electron microscope.
Semiconductor The name applied to materials which exhibit relatively high resistance in a pure state but much lower resistance when minute amounts of impurities are added. The word is commonly used to describe electronic devices made from semiconductor materials.
Semiconductor devices Devices in which the characteristic distinguishing electron conduction takes place within a semiconductor, ranging from the single unit transistor to multiple unit devices such as the semiconductor rectifier. Other devices are diodes, photocells, thermistors, and thyristors.
Semiconductor integrated circuit (SIC) The physical realization of a number of electric elements inseparably associated on or within a continuous body of semiconductor material to perform the function of a circuit.
Serial The technique for handling a binary data word which has more than one bit. The bits are acted upon one at a time. It is like a parade going by a review point.
Serial operation The organization of data manipulation within computer circuitry where the digits of a word are transmitted one at a time along a single line. The serial mode of operation is slower than parallel operation, but utilizes less complex circuitry.
Set An input on a flip-flop not controlled by the clock (see Asynchronous inputs), and used to effect the Q output. It is this input through which signals can be entered to get the Q output to go to "1." Note it cannot get Q to go to "0."
Shear tester Shear testers are used to determine the integrity of a material or to test the adherance between two attached items. It is used for testing eutectic and epoxy die-bond strengths, and for adherance testing a gold-wire ball bonds, gold and solder chip bumps, external lead frames, coined and welded gold electrical contacts, thick film plating, and more.
Shift The process of moving data from one place to another. Generally many bits are moving at once. Shifting is done synchronously and by command of the clock. An 8 -bit word can be shifted sequentially (serially)-that is, the 1 st bit goes out, 2nd bit takes 1st bit's place, 3rd bit takes 2nd bit's place, and so on, in the manner of a bucket brigade. Generally referred to as shifting left or right. It takes 8 clock pulses to shift an 8 -bit word or all bits of a word can be shifted simultaneously. This is called parallel load or parallel shift.
Shift register An arrangement of circuits, specifically flip-flops, which is used to shift serially or in parallel. Binary words are generally parallel loaded and then held temporarily or serially shifted out.

SIC Semiconductor integrated circuit.
Silicon A brittle, gray, crystalline chemical element which, in its pure state, serves as a semiconductor substrate in microelectronics. It is naturally found in compounds such as silicon dioxide.
Silicon gate A type of MOS in which the gate is made of silicon instead of metal. It is faster and denser than the metal-gate MOS.
Silicon nitride A compound of silicon and nitrogen deposited on the surface of silicon monolithic ICs to impart greater stability.
Silicon oxide Silicon monoxide or dioxide or a mixture, the latter of which can be deposited on a silicon IC as insulation between metallization layers.
Single print One squeegee print stroke and flood return per substrate, in screen printing.
Skewing Refers to time delay or offset between any two signals in relation to each other.
Slewing rate Rate at which the output can be driven from limit to limit over the dynamic range.
Slice A single wafer cut from a silicon ingot forming a thin substrate on which all active and passive elements for multiple integrated circuits have been fabricated utilizing semiconductor epitaxial growth, diffusion, passivation, masking, photo resist, and metallization technologies. A completed slice generally contains hundreds of individual circuits. (see Chip.)
Small scale integration A circuit of under 10 gates, generally involving one metallization level implementing one circuit function in monolithic silicon.
Snap-off Distance from top of substrate in screen printing to bottom surface of screen. Squeegee must stretch screen this far to meet the substrate and deposit ink. Set by " $Z$ " motion adjustments.
Snapstrate Scored large area substrate which, after screen printing, may be snapped or broken apart into smaller sized substrates.
Snugger Device for automatically positioning and holding the substrate in proper position during the print cycle, in screen printing.
Solder systems for bonding and welding Processors for ceramic hybrid microcircuits, substrates, lead frames, microassemblies, flat packs, wire memory arrays, ceramic headers, and magnet wire, where solder normally has been pretinned on the substrate or individual components, or solder pastes provide solder without the need for pretinning operations. Temperature controlled preheat, reflow, and cooling stages are involved, with reflow being almost instantaneous.
Solid state The electronic properties of crystalline materials (usually semiconductor in type). The interaction of light, heat, magnetic fields, and electric currents in these crystalline materials are involved in solid state devices. Less power is required to operate solid state devices and a greater variety of effects can be obtained. (2) Technology utilizing solid semiconductors in place of vacuum tubes for amplification, rectification, and switching.
SOS Silicon-on-sapphire transistor device. Silicon is grown on a passive insulating base (sapphire) and then selectively etched away to form a solid state device.
Sputtering A method of depositing a thin film of material onto a substrate. The substrate is placed in a large demountable vacuum chamber having a cathode made of the metal or ceramic to be sputtered. The chamber is then operated so as to bombard the cathode with positive ions. As a result, small particles of the material fall uniformly on the substrate.
Sputtering targets These are usually in the form of simple circular or rectangular plates, comprised of a variety of materials, and bombarded by gas ions that transfer their momentum to particles of the target, ejecting them into the vacuum chamber that houses the operation. These particles are then deposited in a thin film on strategically located substrates.
SSI Small scale integration.
Squeegee Hard, flexible blade with a precision edge which, with applied pressure, forces or pushes ink through the screen in screen printing.
Squeegee pressure Downward force exerted upon the screen and substrate by the squeegee during screen printing. Squeegee speed Rate of speed at which the squeegee is driven across the screen during screen printing.
Stability The specific ability of electronic circuits or other devices to withstand use and environmental stresses without changing. Also continued operation according to specifications despite adverse conditions.
State This refers to the condition of an input or output of a circuit as to whether it is a logic " 1 " or a logic " 0 ." The state of a circuit (gate or flip-flop) refers to its output. The flip-flop is said to be in the "1" state when its Q output is "1." A gate is in the "1" state when its output is "1."
Static In burn-in, the quality of a test wherein the device is subject to either forward or reverse bias applied to appropriate terminals; voltages are unvarying throughout test.
Steatite Ceramic material composed mainly of a silicate of magnesium, used as a circuit substrate.
Step To use the step-and-repeat method.
Substrate The physical material upon which an electronic circuit is fabricated. Used primarily for mechanical support but may serve a useful thermal or electrical function. Also, a material on whose surface an adhesive substance is spread for bonding or coating, or any material which provides a supporting surface for other materials.
Subsystem A part or division of a system which in itself has the properties of a system.
Surface diffusion The high temperature injection of atoms into the surface layer of a semiconductor material to form the junctions. Usually a gaseous diffusion process.

Synchronous Operation of a switching network by a clock pulse generator. All circuits in the network switch simultaneously. All actions take place synchronously with the clock.
Synchronous inputs Those terminals on a flip-flop through which data can be entered but only upon command of the clock. These inputs do not have direct control of the output such as those of a gate but only when the clock permits and commands. Called JK inputs or ac set and reset inputs.
System A group of integrated circuits or other components interconnected to perform a single function or number of related functions. If further interconnected into a large system, the individual elements are referred to as subsystems.
Taper testers A taper tester is used to test one aspect of the dimensional integrity of wafers. Taper results when the two faces of the water under test are not parallel.
TCR Temperature coefficient of resistance.
Temperature coefficient of resistance The amount of change in the resistance of a material per degree of temperature rise. Thermal compression bonding Process of diflusion bonding in which two prepared surfaces are brought into intimate contact, and plastic deformation is induced by the combined effects of pressure and temperature, which in tum results in atom movement causing the development of a crystal lattice bridging the gap between facing surfaces and resulting in bonding.
Thermistor A semiconductor device, the electrical resistance of which varies with the temperature. Its temperature coefficient of resistance is high, nonlinear, and usually negative.
Thick film Conductive, resistive, and/or capacitive passive network deposited on a substrate using a metallic or resistive film which is more than five microns in thickness.
Thick film hybrid integrated circuits The physical realization of a hybrid integrated circuit fabrication on a thick film network.
Thick film resistor, conductor, and dielectric compositions The principle materials for making thick film circuits, available in paste form and consisting of mixtures of metal, oxide, and glass powders.
Thin film Conductive, resistive, and/or capacitive passive network deposited on a substrate using a metallic or resistive film which is less than five microns in thickness.
Thin film deposition, chemical vapor type The CVD technique involves a decomposition and reaction between gases on the surface of a heated substrate such that a solid layer is nucleated and grown. Metals are generally derived from the decomposition of the metal halides. Insulators may be formed by reacting metal halides with oxygen (oxides), ammonia (nitrides), diborane (borides), etc.
Thin film deposition, evaporation type Popular technique for depositing thin film in vacuum, accomplished by heating the source material in a low pressure chamber so that it vaporizes and then condenses onto all cooler surfaces in line-of-sight from the source.
Thin film deposition, sputtering type Evaporation produced by ion bombardment of the source material, known as cathodesputtering.
Thin film deposition materials, conductors and resistors Metals such as aluminum, gold, chromium, nickel, platinum, fungsten, alloys, and cermets deposited as electrical conductors and resistors on silicon or other substrates.
Thin film deposition materials, inorganic dielectrics Film compounds produced by various vacuum evaporation processes and deposited on substrates to perform electrical functions. Examples include silicon monoxide. $\mathrm{ZnS}, \mathrm{CaF}, \mathrm{SiO}_{2}, \mathrm{Al}_{2} \mathrm{O}_{3}$, $\mathrm{SI}_{3} \mathrm{~N}_{4}$, and other chemical compounds.
Thin film deposition materials, organic dielectrics Insulating film compounds produced when organic vapors are heated under conditions in which polymerization and deposition occur. Examples are parylene, butadene, acrolein, and divinyl benzene.
Thin film deposition materials, semiconductors Polycrystalline films deposited by vacuum or flash evaporation to produce high purity single crystal silicon or other semiconductor substances.
Thin film hybrid integrated circuits The physical realization of a hybrid integrated circuit fabricated on a thin film network. Thin film integrated circuit The physical realization of a number of electric elements entirely in the form of thin films deposited in a patterned relationship on a structural supporting material.
Toggle To switch between two states as in a flip-flop.
Tooling Vacuum holes, grooves, and locating pins on the tool plate surface dedicated to a certain size substrate in order to position and hold the substrate during the print cycle of screen printing.
TO package Can-type IC chip configuration, an outgrowth of the original TO transistor package. Most common are the TO-5, TO-18, and TO-47. The IC chip is mounted within the package, interconnected to terminals on the can, and then hermetically sealed. TO stands for transistor outline.
Transistance The characteristic of an electric element which controls voltages or current so as to accomplish gain or switching action in a circuit. Examples of the physical realization of transistance occur in transistors, diodes, saturable reactors, limitors, and relays.
Transistor An active semiconductor device having three or more electrodes, and capable of performing almost all the functions of tubes, including rectification and amplification. Germanium and silicon are the main materials used, with impurities introduced to determine the conductivity type ( $n$-type as an excess of free electrons, $p$-type, a deficiency).
Transistor testers Equipment and instruments which detect or measure leakage current, breakdown voltage, gain, or saturation voltage. Some testers are computer operated.
Trigger A timing pulse used to initiate the transmission of logic signals through the appropriate circuit signal paths.

Trimming Removal of film resistor material in order to increase the resistance to a certain value. Two types of equipment are used for this purpose. The air abrasive jet trimming system (AJT) depends on a precisely controlled stream of abrasive particles to carve away small portions of a thick film resistor. Laser systems are often used for both thick and thin films. With lasers, the material is burned away.
Truth table A chart which tabulates and summarizes all the combinations of possible states of the inputs and outputs of a circuit, It tabulates what will happen at the output for a given input combination.
ITL, T ${ }^{2}$ L (Transistor-Transistor-Logic) A logic system which evolved from DTL wherein the multiple diode cluster is replaced by a multiple-emitter transistor. A circuit which has a multiple emitter input and an active pullup network.
Tum-on time The time required for an output to turn on (sink current, to ground output, to go to $0-\mathrm{V}$ ). It is the propagation time of an appropriate input signal to cause the output to go to 0 V .
Turn-off time Same as Turn-on time except the output stops sinking current, goes off and/or goes to a high voltage level (logic "1").
Ultrasonic bond A contact area where two materials are joined by means of ultrasonic energy and pressure.
Ultrasonic wire bonder Equipment unit which fastens fine wire onto substrate by use of ultrasonic energy.
Unit under test (UUT) Any system, set subsystem, assembly, or subassembly undergoing testing.
UV curing Polymerizing, hardening, or cross linking a low molecular weight resinous material in a wet coating or ink, using ultraviolet light as an energy system.
VISI Very large scale integration.
Vacuum evaporation. The creation of thin films by vaporizing the film substance and allowing its deposition onto a substrate through mask openings.
Varistor A two-electrode semiconductor device with a voltage-dependent nonlinear resistance which falls significantly as the voltage is increased.
Via A vertical conductor or conductive path forming the interconnection between multi-layer hybrid circuit layers.
Wafer and die sorters. Equipment which automates the testing and sorting of semiconductor devices from wafer form.
Wafer handling equipment Equipment used for processing silicon wafers using methods which include batch processing in a common carrier, air bearing single wafer processing, and a combination of batch and single wafer processing.
Wafers Slices of semiconductor crystal materials used as substrates for monolithic ICs, diodes, and transistors.
Wet-process benches These are benches or stations used for water processing. Because of the hazardous materials (acids) that are used, they should be designed with personnel safety and contamination control foremost. Wire bond The fastened union point between a conductor or terminal and the semiconductor die.
Wire, semiconductor lead Fine wire used to connect semiconductor chips to substrate patterns, packages, other chips, etc. Usually made from an aluminum alloy or gold.
Wired "OR" Externally connected separate circuits or functions arranged so that the combination of their outputs results in an "AND" function. The point a which separate circuits are wired together will be an "O" It any one of the separate outputs is an "O." The same as a dot "AND."
Word A group of bits treated as an entity in a computer.
$X$ axis The horizontal or left-to-right direction in a two-dimensional system of coordinates.
$X-X \quad$ Signifies one direction followed in a step-and-repeat method.
" $X$ " motion Registration adjustment left and right of the screen pattern to the substrate, in screen printing.
$Y$ axis The vertical direction, perpendicular to the $X$ axis, in a two-dimensional system of coordinates. $\mathbf{Y}$ - $\mathbf{Y}$ signifies one direction followed in a step-and-repeat method.
" $Y$ " motion Registration adjustment front to rear of the screen pattern to the substrate, in screen printing.
Zener diode A p-n junction two-terminal, single junction semiconductor device reverse biased into the breakdown region and providing high impedances under less than breakdown voltage but conduction with no impedance above breakdown voltage level.
Zero (" $0^{\prime \prime}$ ) See Binary logic.
" ${ }^{\prime}$ ' motion Vertical adjustment of screen-substrate distance. Used for setting snap-off and leveling in screen printing.
(The glossary includes terms from Insulation/Circuits, May, 1982. Copyright Lake Publishing Corporation, Libertyville, IL 60048. Used with permission.)

## CLASSIFICATION OF AMPUFIERS

The definitions of class A, B, or C operation apply to vacuum tubes as well as to transistor circuits. Bias voltage on the emitter junction of a transistor determines collector current just as grid voltage determines plate current in a vacuum tube.

Class A allows for $360^{\circ}$ operation of a sine wave.
Class B operation is with zero bias (cutoff) and allows $180^{\circ}$ conduction.
Class C operation is with bias beyond cutoff which allows less than $180^{\circ}$ conduction.
Class $A B$ operation allows small-signal class $A$ operation, and large-signal class $B$ operation.
The above classes of operation are defined and illustrated for transistors and vacuum tubes.

| Class | Bias Setting | Input-signal Voltage Swing | Plate or Collector Current Flow | Performance Characteristic |
| :---: | :---: | :---: | :---: | :---: |
| $A_{1}$ | Center point of characteristic curve | Confined to linear portion of characteristic curve | Complete cycle | Undistorted output. High gain. Low power conversion efficiency. (25\% maximum) |
| $A_{2}$ | Above center point of characteristic curve | Extends into upper (saturation) bend of characteristic curve | Complete cycle | Almost undistorted output. Lower gain but higher efficiency than class $A_{1}$. |
| $A B_{1}$ | Below center point of characteristic curve | Extends into lower (cutoff) bend of characteristic curve | Cuts off for a small portion of negative half-cycle | In push-pull operation output is practically undistorted. Lower gain but higher efficiency than class $A_{2}$. |
| $\mathrm{AB}_{2}$ | Center point of characteristic curve | Extends into lower (cutoff) and upper (saturation) bends of characteristic curve | Cuts off for small portion of negative half-cycle | Slight harmonic distortion in push-pull operation. Lower gain but higher efficiency than class $A B_{1}$ |
| $B_{1}$ | Near lower bend of characteristic curve | Extends beyond lower (cutoff) bend of characteristic curve | Cuts off for greater part of negative half-cycle | Little harmonic distortion in push-pull operation. Gain less than class $A B_{2}$. Maximum efficiency $\mathbf{7 8 . 5 \%}$. |
| $\mathrm{B}_{2}$ | Near lower bend of characteristic curve | Extends into lower (cutoff) and upper (saturation) bend of characteristic curve | Cuts off for greater part of negative half-cycle and small portion of positive half-cycle | Some harmonic distortion in push-pull operation. Lower gain but higher efficiency than class $B_{1}$. |
| C | Beyond lower bend of characteristic curve | Extends well beyond lower (cutoff) and upper saturation) bends of characteristic curve | Cuts off all of negative and part of positive halfcycles | Considerable harmonic distortion. Low gain. High power conversion efficiency ( $80 \%$ maximum). |

Subscript 1 denotes that no grid current flows during any part of the cycle.
Subscript 2 denotes that grid current flows at least for a portion of the cycle.
In class C amplifiers, grid current always flows, and a subscript is therefore unnecessary.

TRANSISTORS


VACUUM TUBES


Two cascaded amplifying devices will have an overall risetime given by:

$$
T_{r_{t}}=\sqrt{T_{r_{1}}^{2}+T_{r_{2}}^{2}}
$$

where $T_{r_{1}}, T_{r_{2}}$, and $T_{r_{t}}$ are the first stage, second stage, and total risetimes respectively.
The above relation is presented in the accompanying graph.
FOR EXAMPLE: A system incorporating two cascaded amplifiers having risetimes of $100 \mu \mathrm{sec}$ and $25 \mu \mathrm{sec}$ (a ratio of 4:1), would have an overall risetime of $103 \mu \mathrm{sec}$.

NOTE: The Y -axis is the percentage increase in the risetime above the risetime of the slower of two cascaded devices.

Where $A_{1}, A_{2} \cdots A_{n}$ are amplifiers with zero output impedance and infinite input impedance

$$
e_{n}=\text { square wave of frequency } F
$$

Then for TILTS of $10 \%$ or less

$$
\% \text { TILT }_{1}=\pi \frac{F_{1}}{F} \times 100 \text { where } F_{1}=\frac{1}{2 \pi R_{1} C_{1}}
$$

TILTS of $10 \%$ magnitude or less are additive. Thus

$$
\% \text { TILT }_{2}=\pi\left(\frac{F_{1}}{F}+\frac{F_{2}}{F}\right) \times 100
$$

where

$$
F_{2}=\frac{1}{2 \pi R_{2} C_{2}}
$$

and

$$
\% \mathrm{TILT}_{n}=\pi\left(\frac{F_{1}}{F}+\frac{F_{2}}{F}+\cdots \frac{F_{n}}{F}\right) \times 100
$$

By definition

$$
\% \text { TILT }=\frac{V_{1}-V_{2}}{V / 2} \times 100 \approx \pi \frac{F_{1}}{F} \times 100
$$

where

$$
\begin{aligned}
& F=\text { Frequency of applied wave } e_{i n} \\
& F_{1}=\frac{1}{2 \pi \mathrm{RC}}-\text { cutoff of high pass network }(3 \mathrm{~dB}) \\
& \mathrm{C} \text { in farads } \mathrm{R} \text { in ohms }
\end{aligned}
$$



Square wave Thf Due To RC Coupang

(From Electronics and Communications, December, 1968.)

## NEGATIVE FEEDBACK NOMOGRAM

In negative-feedback amplifier considerations, $\beta$ (expressed as a percentage) has a negative value. A line across the $\beta$ and $\mu$ scales will intersect the center scale to indicate resulting change in gain. It also indicates amount (in decibels) by which input must be increased to maintain original output. Original amplification may be expressed as voltage ratio or in decibels by using appropriate scale at right.

FOR EXAMPLE: For a $\beta$ of $10 \%$ and an amplifier $\mu$ of 30 , the nomogram yields a change in $\mu$ of 0.25 .

(Reprinted with permission from International Telephone and Telegraph Corporation

This nomogram determines the available power from the output of class B vacuum tube or transistor push-pull stage operating under the following conditions: The output is a sine wave, the collector or plate swing is twice the supply voltage, and the available output power is determined by the formula

$$
P=\frac{(\sqrt{2} v)^{2}}{z}
$$

FOR EXAMPLE: A transistor amplifier with a 12-V supply and a collector-to-collector impedance of 400 ohms could produce 720 mW of undistorted output power.


## CATHODE FOLLOWER NOMOGRAM

A cathode follower is useful for properly terminating transmission lines and coaxial cables. It provides high $Z_{\text {in }}$ and low $Z_{\text {our }}$, good frequency and phase response, ground common to the input and output, reduced input capacitance, power gain and in-phase input and output. To match a transmission line, $R_{0}$ should equal the impedance of the line ( A ). If $R$ is less, add a series resistor ( B ), if $R_{o}$ is greater use a resistor ( C ) so that $R=R_{o} Z_{o} /\left(R_{o}-Z_{o}\right)$.

FOR EXAMPLE: To drive a 52 -ohm line using a tube with a $g_{m}$ of 5,000 requires an $R_{o}$ of 70 ohms . To provide proper cathode bias, determine the required cathode resistance from the tube manual or by calculation, and subtract $R_{o}$ to determine $R_{\kappa}$. Assuming that 220 ohms is required for proper bias, the $R_{K}$ is 150 ohms and $R_{o}$ is 70 ohms. If fixed bias is used, $R_{\kappa}$ is not needed.



## CATHODE FEEDBACK NOMOGRAM

This nomogram shows the reduction in the gain of an amplifier as a result of negative feedback that is introduced if the cathode resistor is not bypassed.

FOR EXAMPLE: What will be the gain of an amplifier that has an initial stage gain of 20 , a cathode resistor of 22 K , and a dynamic plate load resistor of 220 K if the cathode bypass capacitor is removed. The ratio of $R_{L}$ to $R_{K}$ is 10 , thus the resultant "actual" stage gain is 7.

The range of the nomogram can be extended by multiplying all three scales by the same power of 10 .


EUROPEAN TUBE NUMBERING SYSTEM

## Receiving and Amplifying Tubes

| First Letter | Second and Subsequent Letter | Numbers |
| :---: | :---: | :---: |
| Type of Filament or Heater | Electrode StructureClass of Tube | Type of Base |
| A 4 V ac (parallel) <br> C 200 mA heater <br> D $0.5-1.5 \mathrm{~V}$ dc <br> E 6.3 V ac (parallel) <br> G 5 V heater <br> H 12.6 V 150 mA heater <br> (parallel) <br> K 2 V dc (parallel) <br> M 2.5 V <br> O no filament <br> P 300 mA heater (series) <br> U 100 mA heater (series) <br> Z code cathode | A Single diode <br> B Dual diode <br> C Triode, small-signal <br> D Triode, large-signal <br> E Tetrode, small-signal <br> F Pentode, small-signal <br> H Hexode or heptode <br> K Octode, pentagrid converter <br> L Pentode or tetrode, large-signal <br> M Electron-beam indicator <br> N Thyratron <br> P Secondary emission tube <br> Q Nonode (9 electrodes) <br> T Miscellaneous <br> $X$ Gas-filled full-wave rectifier <br> Y Vacuum half-wave rectifier <br> Z Vacuum full-wave rectifier <br> Two or more of these letters may be combined. Thus ac indicates a diode and a triode in one envelope. | 1 Base indicated by second number <br> 2 Loctal <br> 3 Octal <br> 4 European rim-lock <br> 5 Miscellaneous special bases <br> 6,7 Subminiature tube <br> 8 Nine-pin miniature (noval) <br> 9 Seven-pin miniature <br> Second and third digits differentiate between tubes that have the same general description but different characteristics. If the first number is a 1 , then the second number indicates the type of base. |

## FOR EXAMPLE:

Type ECH81 Triode-heptode oscillator converter, with noval socket and 6.3 V heater
Type EL34 Power pentode with octal base and 6.3-V heater
Type GZ34 Full-wave rectifier with octal base and 5-V heater
NOTE: For special tubes (ruggedized, long-life, etc.), the numbers are placed between the letters. For example: E80F, E90CC, E80CF.

## Transmitting Tubes

| First Letter | Second Letter | Third Letter | Numbers |
| :---: | :---: | :---: | :---: |
| Tube Type | Filament | Cooling Type | Characteristic |
| D Rectifier | A Tungsten, directly heated | G Mercury filled | No uniform |
| M Triode | B Thoriated tungsten, directly heated | L Forced air | notation |
| P Pentode | C Oxide coated, directly heated | W Water cooled | used |
| Q Tetrode | E Heater/cathode | X Xenon filled |  |
| T Triode |  |  |  |

FOR EXAMPLE: Type QQE-04-20 Dual tetrode with indirectly heated cathode

SOLID-STATE SENSING TECHNOLOGIES
This table summarizes the characteristics of solid-state sensors of position, temperature, level, pressure, and speed.

| Sensing Technique | Actuation | Actuator | Construction | Advantages | Disadvantages |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hall effect | Proximity | Electromagnet or permanent magnet | Integrated circuit only | Not rate sensitive, fast signal conditioning, simple | Requires magnet actuator, cannot achieve fine resolution |
| Hall effect vane | Interrupted | Ferrous material | IC, permanent magnet | Integral design, not rate sensitive, low cost, signal conditioning | Magnet attraction mode of actuation, cannot achieve fine resolution |
| Eddy current olution | Proximity | Ferrous or | Coil, IC and nonferrous material ponents | All-metal detector, indiscrete comcontaminated, high frequency | Cannot achieve fine resdiscrete comtegral unit, not easily |
| Opt-electronic | Interrupted or reflective | Any opaque material | IC, LED, and components | Detects any opaque material, good resolution | Easily contaminated ambient light sensitive |
| Piezoelectric | Impact | Any hard material | Crystal | No stand-by power, potentially lowest cost device | Pulse output, requires impact |
| Piezo-resistance | Pressure or flexing | Gaseous or mechanical | IC | Detection without mechanical linkage | Complex, difficult construction, expensive for accuracy |
| Variable reluctance (Magnetic) pickup | Proximity | Ferrous | Coil, magnet, IC and discrete components | Fine resolution, integral unit, high speed detection | Cannot sense zero speed, hard signal conditioning, small operate point, complex |
| Capacitance | Touch or proximity | Any material | IC and sensing capacitor | Detects any low dielectric material | False triggering, moisture and temperature sensitive, complex |
| Sonic | Audio bearn interrupted or reflected | Any material | Transmitter, receiver, IC and discretes | Large sensing gap, detects any material | Triggered by random noise, not precise, nondirectional |

This family tree illustrates the interrelationship of the various types of volatile and nonvolatile semiconductor memories.


| CCD | Charge-coupled device |
| :--- | :--- |
| EEPROM | Electrically erasable programmable read-only memory |
| EPROM | Erasable programmable read-only memory |
| MOS | Metal-oxide semiconductor |
| NOVRAM | Nonvolatile random access memory |
| RAM | Random-access memory |
| ROM | Read-only memory |

## VOICE INPUT/OUTPUT FAMILY TREE

Electronic voice input/output capability endows machines with the human qualities of hearing (speech recognition) and speaking (speech output). This family tree highlights some of the current applications of voice input/output equipment.


The cascade noise figure of two noise sources is given by the equation

$$
F_{T}=F_{1}+\frac{\left(F_{2}-1\right)}{G_{1}}
$$

where $F_{1}, F_{2}$, and $F_{T}$ are the first-stage, second-stage, and overall noise figures respectively, and $G$ is the gain of the first stage-all expressed as power ratios. The nomogram has all scales calibrated in decibels. To use the nomogram connect $F_{2}$ and $G$ and note the intersect point on the turning scale. That point is then connected to $F_{T}$ or $F_{1}$ depending on which of these figures is given. Two ranges (high and low) are given for all three " $F$ " scales and they must be used together. Only one " $G$ " scale is necessary.

FOR EXAMPLE: A first-stage noise figure of 3 dB , a second-stage noise figure of 7 dB , and a first-stage gain of 8 dB , results in an overall noise figure of 4.2 dB .


## Section 5

# Mathematical Data, Formulas, Symbols 

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## RELIABILITY CHARTS

This chart relates system MTBF (Mean-Time-Between-Failures) with the number of components per system and the component MTBF.

FOR EXAMPLE: A system using 10,000 components with a component MTBF of 30 years will have a system MTBF of 1 day.


This chart relates system reliability in percent with the number of serial parts, that is, the critical partsthat must function in order for the system to perform its function.

FOR EXAMPLE: 10,000 critical parts with a $99.99 \%$ parts reliability provide a system reliability of only $37 \%$.


## RELABILITY NOMOGRAM

Reliability is a dependent function of operating time and failure rate. It is generally given as a percentage or a decimal that states the probability that an equipment will perform its function satisfactorily during a mission. Reliability is based on the formula

$$
P_{0}=e^{-t T}=e^{-\lambda t}
$$

where

$$
\begin{aligned}
T & =1 / \lambda & t & =\text { operating time in hours } \\
P_{0} & =\text { probability of success, i.e., reliability } & T & =\text { mean time between failures } \\
e & =\text { base of natural logarithm } & \lambda & =\text { failure rate (\% per } 1,000 \mathrm{hr})
\end{aligned}
$$

FOR EXAMPLE: A circuit that has a falure rate of $100 \% / 1,000 \mathrm{hr}$ (an hourly failure rate of 0.001 or an MTBF of 1,000 ) has a reliability of $99.8 \%$ when operated for 2 hr . That means that the circuit will not operate properly an average of 2 times out of 1,000 operations, or out of 1,000 circuits an average of 2 will fail in 2 hr .

NOTE: An equipment or circuit with an MTBF of one hour will have a reliability of only $33.788 \%$ (100/e) when operated for one hour.

NOTE: For more detailed treatment of MTBF see the latest edition of MIL-Handbook-217.

(From Electronics and Communications, March, 1965.)

## RELIABILITY-REDUNDANCY NOMOGRAM

For certain critical applications, such as manned space flights, the required reliability is often greater than what can be achieved with a single system. Under these conditions it is necessary to resort to redundancy where two or more identical systems are paralleled. The required redundancy is based on the following equation:

$$
P_{N}=1-\left(1-P_{0}\right)^{N}
$$

where
$P_{N}=$ probability of success of $N$ paralleled systems
$P_{\mathrm{o}}=$ probability of success of one system
$N=$ number of paralleled systems
FOR EXAMPLE: A subsystem for a two-week moon exploration flight has a special reliability of $99.99 \%$ and a MTBF of $2,000 \mathrm{hr}$. What is the required redundancy? On reliability nomogram (A) connect 2,000 on the $T$ scale with 336 ( 2 weeks) on the $t$ scale to determine subsystem reliability to be 0.845 . On redundancy nomogram connect 0.845 on the $P_{0}$ scale with 0.9999 on the $P_{N}$ scale to determine that a redundancy of five is required.


## CONFIDENCE LEVEL DETERMINATOR

This graph is used to determine the minimum MTBF for a given confidence level. To use the chart, determine the actual number of Operating Hours, the Observed Failures, and the required Confidence Level. Read across from "Observed Failures" to "Confidence Level" and then down to obtain the "Divisor." Divide the number of Operating Hours by the "Divisor." The result is the minimum MTBF for the stated Confidence Level.

FOR EXAMPLE: During 2,000 hours of operation there were 8 failures. What is MTBF stated with a confidence level of $90 \%$ ? Reading across 8 to the $90 \%$ curve shows the divisor to be 13 . Dividing 2,000 by 13 yields approximately 154. Thus, it can be said that the MTBF (minimum) is 154 hours with a confidence of $90 \%$. If, in the above example, a confidence level of $70 \%$ had been required, then it could be said that the MTBF was 194 hours with a confidence level of $70 \%$.


## ANGULAR RESOLUTION TABLE

The shaft angle corresponding to an integral binary fraction is required wherever shaft angle encoders are used. This resolution table aids in determining accurately the angle represented by a specific number of counts or conversely, the precise number of counts which equals a given angle.

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline \& \& \multirow[t]{2}{*}{$r^{-6}$} \& \multicolumn{4}{|l|}{Aspular Resiohetion Coresponding to inequal-Exponmex Biray Frizition} \& <br>
\hline \& 7 \& \& $1700000 / 7^{6}($ secends $)$ \& $21500 /{ }^{2}$ (minues) \& $36 / z^{\text {n }}$ (deyrees) \&  \& <br>
\hline - \& \& \& 1206000 \& 21500 \& 300.0 \&  \& 0 <br>
\hline \& 2 \& 5 \& 048000 \& 10000 \& 1000 \& 3. 411502051580078323848 \& ' <br>
\hline \& \& 8 \& 334000
162000 \& 5000
2700 \& - 400 \& (1) \& ${ }_{3}^{2}$ <br>
\hline \& $t$ \& 12 \& 162000 \& 2790 \& O \& \& <br>
\hline \& 1 \& $0 \times 2$ \& ${ }^{01000}$ \& 1330 \& 22.5 \& 202 2000001608724154.008 \& : <br>
\hline \& 32 \& 2018 \& 20 200 \& ${ }_{3}^{208}$ \& 11.28 \& 106 178 \& s <br>
\hline \& $\cdots$ \& 01568 \& 208 \& 39.3 \& \& \& <br>
\hline \& 128 \& 0078125 \& ${ }^{10} 128$ \& 10875 \& \& \& 8 <br>
\hline \& 812 \& ${ }^{003}$ \& 50025
2531

28 \& $$
{ }_{42}^{4.375}
$$ \&  \&  \& : <br>

\hline \& 1024 \&  \& 12058 \& 2100375 \& 1515023 \& 00613593 15154258597687 \& 10 <br>
\hline \& 204 \& 0004843125 \& 432175 \& 10 Se6 208 \& 11578125 \&  \& 11 <br>
\hline 12 \& 4096 \& 000 2441100428 \& 31640625 \& 5 mbay \& 00000025 \& 00153390076 \& <br>
\hline 13 \& 4192 \& $0001220 \% 3125$ \& 13480318 \& 2.63871875 \& .003904 12125 \&  \& 13 <br>
\hline \& 163 m \& 000 0510381568 \& 701015025 \& 1.31830 31085 \&  \& (ex \& 14 <br>
\hline 13 \& 32750 \& 000030 S1754 18 \& 558507818 \&  \& . 010985388 \& 000101747508 cts 7051131 715 \& 15 <br>
\hline \& ess 320 \& 000015 88 mow \& 19738008 \& . 3085080437 \& 0054091640025 \&  \& <br>
\hline \& 131072 \&  \& - 508053125 \& 104 784818185 \& ( \& (emo \& 18 <br>
\hline 14 \& 262144 \&  \& 4.90007045 \& 0413740095 \& . 01738101015 \& 000023968468810 773 144 2144 \& <br>
\hline \& 530 204 \&  \& 2.47102308818 \& 01198700480 \& Ooo se6 us soy 123 \& 000 011 va4 214 cos 3303721072 \& <br>
\hline 20 \& 104858 \&  \& 1235961914023 \&  \&  \& (1) \& 12 <br>
\hline 21 \& 2007152 \&  \& 41740085031838 \& \& \& \& <br>
\hline 2 \& 4104504 \&  \& 304000477 51508 \&  \&  \&  \& 22 <br>
\hline ${ }^{2}$ \& ${ }^{1} 304000$ \& 000000 116 20\% 200150 \& 154 mes 2302888125 \&  \&  \&  \& ${ }_{24}^{23}$ <br>
\hline \& 16716 \&  \&  \&  \& 00001072 ELS CSO 570312 S \& $00000018 \% 2335141461964017 \%$ \& 25 <br>
\hline
\end{tabular}






## Boolean Relationships

Idempoint:
$a+0=a \quad a 0=0$
$a+1=1 \quad a 1=a \quad 0 \equiv \bar{a}$
$a+a=a \quad a a=a$
Commutative: $a+b=b+a$

$$
a b=b a
$$

Associative: $(a+b)+c=a+(b+c)$

$$
(a b) c=a(b c)
$$

Distributive: $a b+a c=a(b+c)$

$$
a+b c=(a+b)(a+c)
$$

Absorption: $a(a+b) \equiv a+a b \equiv a$
DeMorgan Theorem: $\overline{\bar{a}}=a$

$$
\begin{aligned}
& (\overline{a b})=\bar{a}+\bar{b} \quad(\overline{\overline{a b}})=a+b \\
& \overline{a+b}=\overline{a b} \quad \overline{\bar{a}+\bar{b}}=a b
\end{aligned}
$$

## Basic Logic



Legend:
NOT: The line over a term indicates a false or not true state.
AND: Two terms directly adjacent to each other are called an "AND" function.
OR : Two terms separated by " + " are called an "OR" function.
Examples: $\quad a b$ reads as " $a$ and not $b$ " $\bar{a} b$ reads as "Not $a$ and $b$ " $\bar{a} b$ reads as "Not $a$ and Not $b$ " $a b$ reads as "Not $a$ or Not $b$ " (See DeMorgan)

Clocked Logic Elements


## CONVERSION CHART OF STANDARD METRIC PREFIXES

This chart shows, in their relative positions, symbols, multiples $\left(10^{2}\right)$, and abbreviations for all the international multiples and submultiples as recommended by the International Committee on Weights and Measures (1962) and adapted by the National Bureau of Standards.

This chart provides a fast and easy method of conversion from any metric notation to any other. "Unity" represents the basic unit of measurement such as volts, ohms, watts, amperes, grams, hertz, etc. The number of steps up or down between the two prefixes which are being compared is equal to the direction and the number of places in which the decimal point has to be moved to convert from one to the other.

FOR EXAMPLE: To convert 0.0032 milliampere to nanoampere-move six places down. Answer: $3,200 \mathrm{nA}$.
To convert 43,280 kilohertz to megahertz-move three places up. Answer: 43.28 MHz .
To convert 10.74 microns to millimeters-move three places up. Answer: 0.01074 mm .


## HARMONIC REJECTION NOMOGRAM

This scale relates the magnitude of harmonic distortion, expressed as a rejection ratio in decibels, to percentage of distortion.

FOR EXAMPLE: (1.) A design specifies that a given audio sine-wave oscillator should have its closest harminic at least 28 dB below the fundamental. The chart indicates that the closest harmonic must be less than $3.9 \%$ of the magnitude of the fundamental.
(2.) Find the harmonic content of a signal made up of the following:

| Fundamental frequency | 100 V rms |
| :--- | ---: |
| Second harmonic | 5 V rms |
| Third harmonic | 2 V rms |

Adding harmonics vectorially gives

$$
\sqrt{5^{2}+2^{2}}=5.39
$$

$\%$ distortion $=\frac{\text { harmonic voltage }}{\text { fundamental voltage }} \times 100=\frac{5.39}{100} \times 100$

Thus the distortion is $5.30 \%$, which means that the harmonic content of the signal is 25.2 dB below the fundamental.


n $2^{-n}$
10
05
0.25
0.125
0.0525
0.03125
0.015625
0.0078125
000390625
0.001953125
$0.000 \quad 976 \quad 5625$
$0.000488281 \quad 25$
0.000244140625
$0.000122 \quad 0703125$
$\begin{array}{lllll}0.0000 & 122 & 055 & 156 & 25\end{array}$
$0.000 \quad 030 \quad 517 \quad 578 \quad 125$
0.0000152587890625
0.00000762939453125
0.000003814697265625
0.0000019073486328125 $\begin{array}{lllllllll}0.000 & 000 & 953 & 674 & 316 & 406 & 25\end{array}$
$0.000 \quad 000 \quad 476837 \quad 158 \quad 203125$
$0.000 \quad 000 \quad 238418 \quad 579101.562 \quad 5$ $0.000 \quad 0001192092695501781 \quad 25$ $0.000 \quad 000 \quad 059604644775 \quad 390 \quad 625$ $\begin{array}{lllllllll}0.000 & 000 & 059 & 601 & 644 & 775 & 390 & 625 \\ 0.000 & 000 & 029 & 802 & 322 & 387 & 695 & 312 & 5\end{array}$
 $\begin{array}{llllllllllll}0.000 & 000 & 007 & 450 & 580 & 596 & 923 & 828 & 125\end{array}$ 0.000000003725290298461914062 S

| $n$ | $2{ }^{\text {n }}$ |
| :---: | :---: |
| 73 | 9444732965739290427392 |
| 74 | 18889465931478560854784 |
| 75 | 37778931862957181709568 |
| 76 | 75557863725914323419136 |
| 77 | 1511157274518286468838272 |
| 78 | 302231454903657293678544 |
| 79 | 604462909807314587353088 |
| 80 | 1208925819614629174706176 |
| 81 | 2417851639229258349412352 |
| 82 | 4835703278458518898824704 |
| 83 | 9671406558917033397849408 |
| 84 | 19342813113834086795298818 |
| 85 | 38585828227668133590197632 |
| 86 | $\begin{array}{ll}77371 & 25245 \\ 53362 & 87181 \\ 19526\end{array}$ |
| 87 | 154742504910672534362390588 |
| 86 | 309485009621345088724781056 |
| 89 | 618970019642690137449562112 |
| 90 | 1237940039285360274899124224 |
| 91 | 2475880078570780549795248448 |
| 92 | 4951760157141521099596496896 |
| 93 | 9903520314283042199192903792 |
| 94 | 19807040628586084398385967584 |
| 95 | 39814081257132168798771975168 |
| 96 | 79228182514264337593543950338 |
| 97 | 158456325028528875187087900872 |
| 96 | 318912650057057350374175801344 |
| 99 | 833825300114114700748351802888 |
| 100 | 1267850600228229401496703205378 | $0.000 \quad 000 \quad 001362646149 \quad 230957031 \quad 25$ $0.000 \quad 000 \quad 000931 \quad 322 \quad 574 \quad 615478 \quad 515 \quad 625$

 $\begin{array}{lllllllllll}0.000 & 000 & 000 & 232 & 830 & 643, & 653 & 869 & 628 & 906 & 25\end{array}$ $0.000 \quad 000 \quad 000116415321826934314453125$ 0.000000000 058 $207660913467407 \quad 2265625$
 $\begin{array}{llllllllllll}0.000 & 000 & 000 & 029 & 103 & 830 & 456 & 733 & 703 & 613 & 281 & 25 \\ 0.000 & 000 & 000 & 014 & 551 & 915 & 228 & 366 & 851 & 806 & 640 & 625\end{array}$ $\begin{array}{lllllllllll}0.000 & 000 & 000 & 014 & 551 & 915 & 228 & 366 & 851 & 806 & 640 \\ 0.000 & 000 & 000 & 007 & 275 & 957 & 614 & 183 & 425 & 903 & 320 \\ 312 & 5\end{array}$ $0.000 \quad 000000003637978 \quad 807091712951660156 \quad 25$ $0.000 \quad 000 \quad 000 \quad 001818989403545835475830078125$

 $\begin{array}{llllllllllllll}0.000 & 000 & 000 & 000 & 227 & 373 & 675 & 43 & 232 & 059 & 478 & 759 & 765 & 625\end{array}$
 0.00000000000005684341886080801486968994140525 0.000000000000028421709430404007434344970703125

 $0.000 \quad 000 \quad 000 \quad 000 \quad 003 \quad 582713678800500929 \quad 355 \quad 621 \quad 337 \quad 890 \quad 625$ 0.000000000000001776356839400250464677810868


 | 0.000 | 000 | 000 | 000 | 000 | 444 | 089 | 209 | 830 | 062 | 616 | 169 | 452 | 667 | 236 | 325 | 125 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0.000 | 000 | 000 | 000 | 000 | 222 | 044 | 604 | 925 | 031 | 308 | 084 | 725 | 333 | 618 | 184 | 052 | $\begin{array}{llllllllllllllll}0.000 & 000 & 000 & 000 & 000 & 222 & 044 & 604 & 925 & 031 & 308 & 084 & 725 & 333 & 618 & 184 \\ 0.052 & 5 \\ 0.000 & 000 & 000 & 000 & 00 d^{\prime} & 111 & 022 & 302 & 462 & 515 & 654 & 042 & 363 & 166 & 809 & 052\end{array} 03125$




















 590295 $\begin{array}{lllllllll}1 & 180 & 591 & 680 & 717 & 411 & 303 & 424\end{array}$ $\begin{array}{lllllllll}2 & 361 & 183 & 241 & 434 & 822 & 606 & 848\end{array}$ $4322366482869645 \quad 213 \quad 696$

| $n$ | $n^{2}$ | $\sqrt{n}$ | $\sqrt{10 n}$ | $n^{2}$ | $n$ | $\sqrt[3]{n}$ | $\sqrt[3]{10 n}$ | $\sqrt[3]{100 n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1.000000 | 3.162278 | 1 | 1 | 1.000000 | 2.154435 | 4.641589 |
| 2 | 4 | 1.414214 | 4.472136 | 8 | 2 | 1.259921 | 2.714418 | 5.848035 |
| 3 | 9 | 1.732051 | 5.477226 | 27 | 3 | 1.442250 | 3.107233 | 6.694330 |
| 4 | 16 | 2.000000 | 6.324555 | 64 | 4 | 1.587401 | 3.419952 | 7.368063 |
| 5 | 25 | 2.236068 | 7.071068 | 125 | 5 | 1.709976 | 3.684031 | 7.937005 |
| 6 | 36 | 2.449490 | 7.745967 | 216 | 6 | 1.817121 | 3.914868 | 8.434327 |
| 7 | 49 | 2.645751 | 8.366600 | 343 | 7 | 1.912931 | 4.121285 | 8.879040 |
| 8 | 64 | 2.828427 | 8.944272 | 512 | 8 | 2.000000 | 4.308869 | 9.283178 |
| 9 | 81 | 3.000000 | 9.486833 | 729 | 9 | 2.080084 | 4.481405 | 9.654894 |
| 10 | 100 | 3.162278 | 10.00000 | 1,000 | 10 | 2.154435 | 4.641589 | 10.00000 |
| 11 | 121 | 3.316625 | 10.48809 | 1,331 | 11 | 2.223980 | 4.791420 | 10.32280 |
| 12 | 144 | 3.464102 | 10.95445 | 1,728 | 12 | 2.289428 | 4.932424 | 10.62659 |
| 13 | 169 | 3.605551 | 11.40175 | 2,197 | 13 | 2.351335 | 5.065797 | 10.91393 |
| 14 | 196 | 3.741657 | 11.83216 | 2,744 | 14 | 2.410142 | 5.192494 | 11.18689 |
| 15 | 225 | 3.872983 | 12.24745 | 3,375 | 15 | 2.466212 | 5.313293 | 11.44714 |
| 16 | 256 | 4.000000 | 12.64911 | 4,096 | 16 | 2.519842 | 5.428835 | 11.69607 |
| 17 | 289 | 4.123106 | 13.03840 | 4,913 | 17 | 2.571282 | 5.539658 | 11.93483 |
| 18 | 324 | 4.242641 | 13.41641 | 5,832 | 18 | 2.620741 | 5.646216 | 12.16440 |
| 19 | 361 | 4.358899 | 13.78405 | 6,859 | 19 | 2.668402 | 5.748897 | 12.38562 |
| 20 | 400 | 4.472136 | 14.14214 | 8,000 | 20 | 2.714418 | 5.848035 | 12.59921 |
| 21 | 441 | 4.582576 | 14.49138 | 9,261 | 21 | 2.758924 | 5.943922 | 12.80579 |
| 22 | 484 | 4.690416 | 14.83240 | 10,648 | 22 | 2.802039 | 6.036811 | 13.00591 |
| 23 | 529 | 4.795832 | 15.16575 | 12,167 | 23 | 2.843867 | 6.126926 | 13.20006 |
| 24 | 576 | 4.898979 | 15.49193 | 13,824 | 24 | 2.884499 | 6.214465 | 13.38866 |
| 25 | 625 | 5.000000 | 15.81139 | 15,625 | 25 | 2.924018 | 6.299605 | 13.57209 |
| 26 | 676 | 5.099020 | 16.12452 | 17,576 | 26 | 2.962496 | 6.382504 | 13.75069 |
| 27 | 729 | 5.196152 | 16.43168 | 19,683 | 27 | 3.000000 | 6.463304 | 13.92477 |
| 28 | 784 | 5.291503 | 16.73320 | 21,952 | 28 | 3.036589 | 6.542133 | 14.09460 |
| 29 | 841 | 5.385165 | 17.02939 | 24,389 | 29 | 3.072317 | 6.619106 | 14.26043 |
| 30 | 900 | 5.477226 | 17.32051 | 27,000 | 30 | 3.107233 | 6.694330 | 14.42250 |
| 31 32 | 961 | 5.567764 | 17.60682 | 29,791 | 31 | 3.141381 | 6.767899 | 14.58100 |
| 32 | 1,024 | 5.656854 | 17.88854 | 32,768 | 32 | 3.174802 | 6.839904 | 14.73613 |
| 33 | 1,089 | 5.744563 | 18.16590 | 35,937 | 33 | 3.207534 | 6.910423 | 14.88806 |
| 34 | 1,156 | 5.830952 | 18.43909 | 39,304 | 34 | 3.239612 | 6.979532 | 15.03695 |
| 35 | 1,225 | 5.916080 | 18.70829 | 42,875 | 35 | 3.271066 | 7.047299 | 15.18294 |
| 36 | 1,296 | 6.000000 | 18.97367 | 46,656 | 36 | 3.301927 | 7.113787 | 15.32619 |
| 37 | 1,369 | 6.082763 | 19.23538 | 50,653 | 37 | 3.332222 | 7.179054 | 15.46680 |
| 38 | 1,444 | 6.164414 | 19.49359 | 54,872 | 38 | 3.361975 | 7.243156 | 15.60491 |
| 39 | 1,521 | 6.244998 | 19.74842 | 59,319 | 39 | 3.391211 | 7.306144 | 15.74061 |
| 40 | 1,600 | 6.324555 | 20.00000 | 64,000 | 40 | 3.419952 | 7.368063 | 15.87401 |
| 41 | 1,681 | 6.403124 | 20.24846 | 68,921 | 41 | 3.448217 | 7.428959 | 16.00521 |
| 42 | 1,764 | 6.480741 | 20.49390 | 74,088 | 42 | 3.476027 | 7.488872 | 16.13429 |
| 43 | 1,849 | 6.557439 | 20.73644 | 79,507 | 43 | 3.503398 | 7.547842 | 16.26133 |
| 44 | 1,936 | 6.633250 | 20.97618 | 85,184 | 44 | 3.530348 | 7.605905 | 16.38643 |
| 45 | 2,025 | 6.708204 | 21.21320 | 91,125 | 45 | 3.556893 | 7.663094 | 16.50964 |
| 46 | 2,116 | 6.782330 | 21.44761 | 97,336 | 46 | 3.583048 | 7.719443 | 16.63103 |
| 47 | 2,209 | 6.855655 | 21.67948 | 103,823 | 47 | 3.608826 | 7.774980 | 16.75069 |
| 48 | 2,304 | 6.928203 | 21.90890 | 110,592 | 48 | 3.634241 | 7.829735 | 16.86865 |
| 49 | 2,401 | 7.000000 | 22.13594 | 117,649 | 49 | 3.659306 | 7.883735 | 16.98499 |
| 50 | 2.500 | 7.071068 | 22.36068 | 125.000 | 50 | 3.684031 | 7.937005 | 17.09976 |


| $n$ | $n^{2}$ | $\sqrt{n}$ | $\sqrt{10 n}$ | $n^{3}$ | $n$ | $\sqrt[3]{n}$ | $\sqrt[3]{10 n}$ | $\sqrt[3]{100 n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 2,500 | 7.071068 | 22.36068 | 125,000 | 50 | 3.684031 | 7.937005 | 17.09976 |
| 51 | 2,601 | 7.141428 | 22.58318 | 132,651 | 51 | 3.708430 | 7.989570 | 17.21301 |
| 52 | 2,704 | 7.211103 | 22.80351 | 140,608 | 52 | 3.732511 | 8.041452 | 17.32478 |
| 53 | 2,809 | 7.280110 | 23.02173 | 148,877 | 53 | 3.756286 | 8.092672 | 17.43513 |
| 54 | 2,916 | 7.348469 | 23.23790 | 157,464 | 54 | 3.779763 | 8.143253 | 17.54411 |
| 55 | 3,025 | 7.416198 | 23.45208 | 166,375 | 55 | 3.802952 | 8.193213 | 17.65174 |
| 56 | 3,136 | 7.483315 | 23.66432 | 175,616 | 56 | 3.825862 | 8.242571 | 17.75808 |
| 57 | 3,249 | 7.549834 | 23.87467 | 185,193 | 57 | 3.848501 | 8.291344 | 17.86316 |
| 58 | 3,364 | 7.615773 | 24.08319 | 195,112 | 58 | 3.870877 | 8.339551 | 17.96702 |
| 59 | 3,481 | 7.681146 | 24.28992 | 205,379 | 59 | 3.892996 | 8.387207 | 18.06969 |
| 60 | 3,600 | 7.745967 | 24.49490 | 216,000 | 60 | 3.914868 | 8.434327 | 18.17121 |
| 61 | 3,721 | 7.810250 | 24.69818 | 226,981 | 61 | 3.936497 | 8.480926 |  |
| 62 | 3,844 | 7.874008 | 24.89980 | 238,328 | 62 | 3.957892 | 8.527019 | 18.37091 |
| 63 | 3,969 | 7.937254 | 25.09980 | 250,047 | 63 | 3.979057 | 8.572619 | 18.46915 |
| 64 | 4,096 | 8.000000 | 25.29822 | 262,144 | 64 | 4.000000 | 8.617739 | 18.56636 |
| 65 | 4,225 | 8.062258 | 25.49510 | 274,625 | 65 | 4.020726 | 8.662391 | 18.66256 |
| 66 | 4,356 | 8.124038 | 25.69047 | 287,496 | 66 | 4.041240 | 8.706588 | 18.75777 |
| 67 | 4,489 | 8.185353 | 25.88436 | 300,763 | 67 | 4.061548 | 8.750340 | 18.85204 |
| 68 | 4,624 | 8.246211 | 26.07681 | 314,432 | 68 | 4.081655 | 8.793659 | 18.94536 |
| 69 | 4,761 | 8.306624 | 26.26785 | 328,509 | 69 | 4.101566 | 8.836556 | 19.03778 |
| 70 | 4,900 | 8.366600 | 26.45751 | 343,000 | 70 | 4.121285 | 8.879040 | 19.12931 |
| 71 | 5,041 | 8.426150 | 26.64583 | 357,911 | 71 | 4.140818 | 8.921121 | 19.21997 |
| 72 | 5,184 | 8.485281 | 26.83282 | 373,248 | 72 | 4.160168 | 8.962809 | 19.30979 |
| 73 | 5,329 | 8.544004 | 27.01851 | 389,017 | 73 | 4.179339 | 9.004113 | 19.39877 |
| 74 | 5,476 | 8.602325 | 27.20294 | 405,224 | 74 | 4.198336 | 9.045042 | 19.48695 |
| 75 | 5,625 | 8.660254 | 27.38613 | 421,875 | 75 | 4.217163 | 9.085603 | 19.57434 |
| 76 | 5,776 | 8.717798 | 27.56810 |  | 76 | 4.235824 | 9.125805 | 19.66095 |
| 77 | 5,929 | 8.774964 | 27.74887 | 456,533 | 77 | 4.254321 | 9.165656 | 19.74681 |
| 78 | 6,084 | 8.831761 | 27.92848 | 474,552 | 78 | 4.272659 | 9.205164 | 19.83192 |
| 79 | 6,241 | 8.888194 | 28.10694 | 493,039 | 79 | 4.290840 | 9.244335 | 19.91632 |
| 80 | 6,400 | 8.944272 | 28.28427 | 512,000 | 80 | 4.308869 | 9.283178 | 20.00000 |
| 81 | 6,561 | 9.000000 | 28.46050 | 531,441 | 81 | 4.326749 | 9.321698 | 20.08299 |
| 82 | 6,724 | 9.055385 | 28.63564 | 551,368 | 82 | 4.344481 | 9.359902 | 20.16530 |
| 83 | 6,889 | 9.110434 | 28.80972 | 571,787 | 83 | 4.362071 | 9.397796 | 20.24694 |
| 84 | 7,056 | 9.165151 | 28.98275 | 592,704 | 84 | 4.379519 | 9.435388 | 20.32793 |
| 85 | 7,225 | 9.219544 | 29.15476 | 614,125 | 85 | 4.396830 | 9.472682 | 20.40828 |
| 86 | 7,396 | 9.273618 | 29.32576 | 636,056 | 86 | 4.414005 | 9.509685 | 20.48800 |
| 87 | 7,569 | 9.327379 | 29.49576 | 658,503 | 87 | 4.431048 | 9.546403 | 20.56710 |
| 88 | 7,744 | 9.380832 | 29.66479 | 681,472 | 88 | 4.447960 | 9.582840 | 20.64560 |
| 89 90 | 7,921 8,100 | 9.433981 | 29.83287 | 704,969 | 89 | 4.464745 | 9.619002 | 20.72351 |
| 90 | 8,100 | 9.486833 | 30.00000 | 729,000 | 90 | 4.481405 | 9.654894 | 20.80084 |
| 91 | 8,281 | 9.539392 | 30.16621 | 753,571 | 91 | 4.497941 | 9.690521 |  |
| 92 | 8,464 | 9.591663 | 30.33150 | 778,688 | 92 | 4.514357 | 9.725888 | 20.95379 |
| 93 | 8,649 | 9.643651 | 30.49590 | 804,357 | 93 | 4.530655 | 9.761000 | 21.02944 |
| 94 | 8,836 | 9.695360 | 30.65942 | 830,584 | 94 | 4.546836 | 9.795861 | 21.10454 |
| 95 | 9,025 | 9.746794 | 30.82207 | 857,375 | 95 | 4.562903 | 9.830476 | 21.17912 |
| 96 | 9,216 | 9.797959 | 30.98387 | 884,736 |  | 4.578857 |  |  |
| 97 | 9,409 | 9.848858 | 31.14482 | 912,673 | 97 | 4.594701 | 9.898983 | 21.32671 |
| 98 | 9,604 | 9.899495 | 31.30495 | 941,192 | 98 | 4.610436 | 9.932884 | 21.39975 |
| 99 | 9,801 | 9.949874 | 31.46427 | 970,299 | 99 | 4.626065 | 9.966555 | 21.47229 |
| 100 | 10,000 | 10.00000 | 31.62278 | 1,000,000 | 100 | 4.641589 | 10.00000 | 21.54435 |


Radix (base) point

- Logic multiplication symbol
$\infty \quad$ Infinity
+ Plus, positive, logic OR function
- Minus, negative
$\pm \quad$ Plus or minus, positive or negative
$\mp \quad$ Minus or plus, negative or positive
$\times$ Times, logic AND function
$\div \quad$ Divided by
/ Divided by (expressive of a ratio)
$=$ Equal to
$\equiv \quad$ Identical to, is defined by
$\cong$ Approximately equal to, congruent to
$\doteq$ Approximately equal to
$\neq \quad$ Not equal to
~ Similar to
$<\quad$ Less than
$<\quad$ Not less than
$\ll \quad$ Much less than
$>$ Greater than
$\ngtr \quad$ Not greater than
>> Much greater than
$\leqslant \quad$ Equal to or less than
$\geqslant \quad$ Equal to or greater than
$\propto \quad$ Proportional to, varies directly as
$\rightarrow \quad$ Approaches
: Is to, proportional to
.. Therefore
\# Number
\% Percent
@ At the rate of; at cost of
$\epsilon$ or $\theta \quad$ The natural number $=2.71828$
$\pi \quad \mathrm{Pi} \cong 3.14159 \ldots$
() Parentheses. Used to enclose a common group of terms.
[ ] Brackets. Used to enclose a common group of terms which includes one or moregroups in parentheses.
\{ \} Braces. Used to enclose a common group of terms which includes one of moregroups in brackets.
$\angle$ Angle
Degrees (arc or temperature)
Minutes, prime " Seconds, double prime
|| Parallel to
$\perp$ Perpendicular to
And beyond, ellipsis

| $x+y$ | $x$ added to $y, x$ OR $y$ |
| :---: | :---: |
| $x-y$ | $y$ subtracted from $x$ |
| $x \cdot y, x \times y$ or $x y$ | $x$ multiplied by $y, x$ AND $y$ |
| $x-y$ | $x$ divided by $y$ |
| $x / y$ or $\frac{x}{y}$ | $x$ divided by $y$ |
| $1 / x$ | Reciprocal of $x$ |
| $\sqrt{1}$ | $x$ raised to the indicated power of $n$ |
| $\sqrt[5]{x}$ | Indicated root ( $\sqrt{ }$ ) of $x$ |
| x:y | $x$ is to $y$ |
| 傢. | Absolute value of $x$, magnitude of $x$ |
| $\overline{\bar{X}}, \dot{X}$, or X | Vector $X$ |
| I | Average value of $x$ |
| $f(x)$ or $F(x)$ | Function of $x$ |
| $i$ | $\sqrt{-1}$ |
|  | Operator, equal to $\sqrt{-1}$ |
| $\Delta x$ | Increment of $x$ |
| dx | Differential of $x$ |
| $\partial x$ | Partial differential of $x$ |
| $\Delta x$ | Change in $x$ with respect to $y$ |
| $\Delta y$ | Change in $x$ with respect to $y$ |
| $\frac{\mathrm{d}}{\mathrm{d}}$ | Derivative of $x$ with respect to $y$ |
| dy |  |
| $\frac{\mathrm{d}}{\mathrm{~d} y}(x)$ | Derivative of $x$ with respect to $y$ |
| $\mathrm{D}_{\boldsymbol{r}} \boldsymbol{x}$ | Derivative of $x$ with respect to $y$ |
| $\partial x$ | Partial derivative of $x$ with respect to $y$ |
| $\frac{\partial y}{}$ | Partial derivalive of $x$ with respect toy |
| $\Sigma$ | Summation |
| $\Sigma_{6}^{0}$ | Summation between limits (from $a$ to $b$ ) |
| $\square$ | Product |
| Пٌ | Product between limits (from $a$ to $b$ ) |
| f | Integral |
| $\int_{0}^{\text {b }}$ | Integral between limits (from $a$ to $b$ ) |
| $\int x d y$ | Integral of $x$ with respect to $y$ |
| 10 | Evaluated at $a$ |
| 10 | Evaluated between limits (from $a$ to $b$ ) |

FACTORIALS
Numerical

| $n$ | $\frac{1}{n!}$ |  |  |  |  |  |  | $n!$ |  | $n$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1. |  |  |  |  |  |  |  | 1 | 1 |
| 2 | 0.5 |  |  |  |  |  |  |  | 2 | 2 |
| 3 | . 16666 | 66666 | 66666 | 66666 | 66667 |  |  |  | 6 | 3 |
| 4 | . 04166 | 66666 | 66666 | 66666 | 66667 |  |  |  | 24 | 4 |
| 5 | . 00833 | 33333 | 33333 | 33333 | 33333 |  |  |  | 120 | 5 |
| 6 | 0.00138 | 88888 | 88888 | 88888 | 88889 |  |  |  | 720 | 6 |
| 7 | . 00019 | 84126 | 98412 | 69841 | 26984 |  |  |  | 5040 | 7 |
| 8 | . 00002 | 48015 | 87301 | 58730 | 15873 |  |  |  | 40320 | 8 |
| 9 | . 00000 | 27557 | 31922 | 39858 | 90653 |  |  | 3 | 62880 | 9 |
| 10 | . 00000 | 02755 | 73192 | 23985 | 89065 |  |  | 36 | 28800 | 10 |
| 11 | 0.00000 | 00250 | 52108 | 38544 | 17188 |  |  | 399 | 16800 | 11 |
| 12 | . 000000 | 00020 | 87675 | 69878 | 68099 |  |  | 4790 | 01600 | 12 |
| 13 | . 00000 | 00001 | 60590 | 43836 | 82161 |  |  | 62270 | 20800 | 13 |
| 14 | . 00000 | 00000 | 11470 | 74559 | 77297 |  | 8 | 71782 | 91200 | 14 |
| 15 | . 00000 | 00000 | 00764 | 71637 | 31820 |  | 130 | 76743 | 68000 | 15 |
| 16 | 0.00000 | 00000 | 00047 | 79477 | 33239 |  | 2092 | 27898 | 88000 | 16 |
| 17 | . 000000 | 00000 | 00002 | 81145 | 72543 |  | 35568 | 74280 | 96000 | 17 |
| 18 | . 00000 | 00000 | 00000 | 15619 | 20697 | 6 | 40237 | 37057 | 28000 | 18 |
| 19 | . 00000 | 00000 | 00000 | 00822 | 06352 | 121 | 64510 | 04088 | 32000 | 19 |
| 20 | . 00000 | 00000 | 00000 | 00041 | 10318 | 2432 | 90200 | 81766 | 40000 | 20 |
|  |  |  |  | $1=1 \times 2$ | $\times 3 \times 4$ |  |  |  |  |  |

FOR EXAMPLE: For $n=7, n!=5040$.
$1 / n!=0.001984126984126984126984$,
$\log (n!)=3.702431$.

## Logarithmic

Logarithms of the products $1 \times 2 \times 3 \ldots n, n$ from 1 to 100 .

| $\boldsymbol{n}$ | $\log (n /)$ | $n$ | $\log (n) / 1$ | $n$ | $\log (n /)$ | $n$ | $\log (n))$ |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.000000 | 26 | 26.605619 | 51 | 66.190645 | 76 | 111.275425 |
| 2 | 0.301030 | 27 | 28.036983 | 52 | 67.906648 | 77 | 113.161916 |
| 3 | 0.778151 | 28 | 29.484141 | 53 | 69.630924 | 78 | 115.054011 |
| 4 | 1.380211 | 29 | 30.946539 | 54 | 71.363318 | 79 | 116.951638 |
| 5 | 2.079181 | 30 | 32.423660 | 55 | 73.103681 | 80 | 118.854728 |
| 6 | 2.857332 | 31 | 33.915022 | 56 | 74.851869 | 81 | 120.763213 |
| 7 | 3.702431 | 32 | 35.420172 | 57 | 76.607744 | 82 | 122.677027 |
| 8 | 4.605521 | 33 | 36.938686 | 58 | 78.371172 | 83 | 124.596105 |
| 9 | 5.559763 | 34 | 38.470165 | 59 | 80.142024 | 84 | 126.520384 |
| 10 | 6.559763 | 35 | 40.014233 | 60 | 81.920175 | 85 | 128.449803 |
| 11 | 7.601156 | 36 | 41.570535 | 61 | 83.705505 | 86 | 130.384301 |
| 12 | 8.680337 | 37 | 43.138737 | 62 | 85.497896 | 87 | 132.323821 |
| 13 | 9.794280 | 38 | 44.718520 | 63 | 87.297237 | 88 | 134.268303 |
| 14 | 10.940408 | 39 | 46.309585 | 64 | 89.103417 | 89 | 136.217693 |
| 15 | 12.116500 | 40 | 47.911645 | 65 | 90.916330 | 90 | 138.171936 |
| 16 | 13.320620 | 41 | 49.524429 | 66 | 92.735874 | 91 | 140.130977 |
| 17 | 14.551069 | 42 | 51.147678 | 67 | 94.561949 | 92 | 142.094765 |
| 18 | 15.806341 | 43 | 52.781147 | 68 | 96.394458 | 93 | 144.063248 |
| 19 | 17.085095 | 44 | 54.424599 | 69 | 98.233307 | 94 | 146.036376 |
| 20 | 18.386125 | 45 | 56.077812 | 70 | 100.078405 | 95 | 148.014099 |
| 21 | 19.708344 | 46 | 57.740570 | 71 | 101.929663 | 96 | 149.996371 |
| 22 | 21.050767 | 47 | 59.412668 | 72 | 103.786996 | 97 | 151.983142 |
| 23 | 22.412494 | 48 | 61.093909 | 73 | 105650319 | 98 | 153.974368 |
| 24 | 23.792706 | 49 | 62.784105 | 74 | 107.519550 | 99 | 155.970004 |
| 25 | 25.190646 | 50 | 64.483075 | 75 | 109.394612 | 100 | 157.970004 |

## RECTANGULAR-POLAR CONVERSION CHART

This chart quickly converts between cartesian (rectangular) and polar forms of notation. The horizontal (real) and the vertical (imaginary) coordinates are used for rectangular notations, and the angular (magnitude) and circular (angle) coordinates are used for polar notation. The same units of measurement are used for both systems. This makes conversion from one system to the other readily possible. The range of the chart can be extended by multiplying the horizontal and vertical axes by the same power of ten.

## FOR EXAMPLE:

1. $2+\beta$ is equivalent to $3.6 / 56^{\circ}$
2. $70 / 55^{\circ}$ is equivalent to $40+j 57$
3. $6-\beta$ is equivalent to $6.7<333^{\circ}$

$X^{2}+Y^{2}=a^{2}$
$\mathbf{X}=\mathrm{a} \cos \mu, \mathrm{Y}=\mathrm{a} \sin \mu$

$\mathrm{r}=2 \mathrm{a} \cos \mu$

$\mathrm{r}=\mathrm{a} \cos \mu+\mathrm{b} \sin \mu$


$$
\mathbf{r}=2 \mathrm{a} \sin \mu
$$



$$
\frac{x^{2}}{a^{2}}+\frac{y^{2}}{b^{2}}=1
$$

$$
\begin{gathered}
\mathrm{r}=\mathrm{a}+\mathrm{b} \cos \mu \\
\mathrm{a}>\mathrm{b}>0
\end{gathered}
$$

$$
\mathrm{X}=\mathrm{a} \cos \mu, \mathrm{Y}=\mathrm{b} \sin \mu
$$


$r=a(1+\cos \mu)$

Witch of Agnesi

$Y\left(X^{2}+4 a^{2}\right)=8 a^{3}$

$r=a \cos 3 \mu$


$\mathrm{r}=\mathrm{a} \cos 2 \mu$

$r=a \sin 2 \mu$

$Y^{2}(2 a-X)=X^{3}$

$Y^{2}=X^{2} \frac{a+X}{a-X}$

$Y=a^{x}$

$Y=\log _{a} X$

$Y=e^{-x^{2}}$

$\mathrm{X}=\mathrm{a}(\mu-\sin \mu)$
$Y=a(1-\cos \mu)$

$X^{3 / 4}+Y^{2 / 5}=a^{2 / 5} \quad Y=a\left(\cos H \frac{X}{a}-1\right)$

$$
\begin{aligned}
Y=a\left(\cos H \frac{X}{a}-1\right) & X= \\
& \pm\left(a \operatorname{sech}^{-1} \frac{Y}{a} \sqrt{a^{2}-Y^{2}}\right)
\end{aligned}
$$

Cube


Parallelopiped

Surface Area
$A=2(a b+h c+a c)$
Volume
$V=a b c$
Diagonal
$D=\sqrt{a^{2}+b^{2}+c^{2}}$

## Right Cireular Cylinder



Surlace Area
$A=1.5708 \mathrm{~d}(2 \mathrm{~h}+\mathrm{d})$
Volume
$V=.7854 d^{2} h$

Right Regular Pyramid


Surface Area
$\mathrm{A}={ }_{1}{ }_{2} \mathrm{nbl}+\mathrm{AB}$ (area of base)

Volume
$V=1 / \int A s h$

Right Regular Cone


Surface Area
$A=1.5708 d(.5 d+1)$

Volume
$V=.2618 \mathrm{~d}^{2} h$

Frustrum of Right Regular Pyramid


Surface Area

$$
\mathrm{A}=1 / \mathrm{/}\left|\mathrm{n}\left(\mathrm{~b}+\mathrm{b}_{1}\right)+\mathrm{AB}+\mathrm{AT}\right|
$$

Volume

$$
V=I / 3 h(A B+A T+\sqrt{A B A T})
$$

Frustrum of Right Regular Cone


Surface Area
$A=.3927\left[d^{2}+d^{2}+4\left|\left(d+d_{1}\right)\right|\right.$

## Volume

$V=.2618 h\left(d^{2}+d d_{1}+d_{1}{ }^{2}\right)$

Sphere


## Surface Area

$\mathrm{A}=3.1416 \mathrm{~d}^{2}$
Volume
$V=.5236 \mathrm{~d}^{3}$

## Surface Area <br> $\mathrm{A}=1.5708 \mathrm{r}(4 \mathrm{~h}+\mathrm{c})$

## Volume

$V=2.0944 r^{1} h$

Surface Area of Top Section $\mathrm{A}=6.2832 \mathrm{rh}$ or

$$
\mathrm{A}=.7854\left(4 \mathrm{~h}^{2}+\mathrm{c}^{2}\right)
$$

Total Surface Area $A=1.5708\left(2 h^{2}+c^{2}\right)$

## Volume

$\mathrm{V}=1.0472 \mathrm{~h}^{\mathbf{1}}(3 \mathrm{r}-\mathrm{h})$ or $V=, 1318 h\left(3 c^{2}+4 h^{3}\right)$

## Zone of Sphere


Area of Spherical Surface $\mathrm{A}=6.2832 \mathrm{rh}$

## Total Surface Area

 $A=.7854\left(8 r h+c^{2}+c,{ }^{1}\right)$Volume
$V=.1318 h\left(3 c^{2}+3 c^{2}+4 h^{2}\right)$
Torus


Surface Ares $\mathrm{A}=39.47 \mathrm{Brr}$

Volume
$\mathrm{V}=19.739 \mathrm{r}^{1} \mathrm{r}_{\mathrm{l}}$

Volume
$\mathrm{V}=.5236 \mathrm{abc}$

## Volume

$V=.3927 a b^{3}$


HALF ROUNDS
$A R E A=\frac{0.7854 d^{2}}{2}-d \longrightarrow d$


HALF OVALS
AREA $=0.7854 \mathrm{ab}$


OCTAGONS


HEXAGONS AREA $=3.464 \mathrm{r}$


SEGMENT OF ROUNDS
AREA $=\frac{\mathrm{rl}-\mathrm{c}(\mathrm{r}-\mathrm{h})}{2}$,


EQUILATERAL TRIANGLES
AREA $=0.433013 \mathrm{~b}^{2}$


KEYSTONES

$$
\text { AREA }=\frac{a(b+c)}{2}
$$


$1-b-1$

| Knewn | Find |  |
| :---: | :---: | :---: |
| 0,6 | A, B, b | $\sin A=\frac{a}{c}, \cos B=\frac{a}{c}, b=\sqrt{c^{2}-a^{2}}$ |
|  | Area | $\frac{a}{2} \sqrt{c^{2}-a^{2}}$ |
| a, b | A, B, e | $\tan A=\frac{a}{b}, \tan B=\frac{b}{a}, c=\sqrt{a^{2}+b^{2}}$ |
|  | Ares | $\frac{a b}{2}$ |
| A, 0 | B,b,c | $s=90^{\circ}-\mathrm{A}, \mathrm{b}=\operatorname{cet} \mathrm{A}, \mathrm{c}=\frac{\mathrm{a}}{\sin \mathrm{A}}$ |
|  | Arso | $\frac{a^{2} \cot A}{2}$ |
| A, b | B, e, c | $s=90^{\circ}-\mathrm{A}, \mathrm{a}=\mathrm{b} \tan \mathrm{~A}, \mathrm{c}=\frac{\mathrm{b}}{\cos \mathrm{~A}}$ |
|  | Arsa | $\frac{b^{2} \tan A}{2}$ |
| A, 6 | B, es,b | $B=90^{\circ}-A, a=c \sin A, b=c \cos A$ |
|  | Area | $\frac{c^{2} \sin A \cos A}{2}=\frac{t^{2} \sin 2 A}{4}$ |
| Known | Find |  |
|  |  | $\begin{aligned} & \sin \frac{1}{2} A=\sqrt{\frac{(s-b)(s-c)}{b c}}, \cos \frac{1}{2} A= \\ & \sqrt{\frac{s(b-a)}{b c}}, \operatorname{ten} \frac{1}{2} A=\sqrt{\frac{(s-b)(v-c)}{1(b-a)}} \end{aligned}$ |
|  | 3 | $\begin{aligned} & \sin \frac{1}{2} B=\sqrt{\frac{(1-a)(p-c)}{a \varepsilon}}, \sec \frac{1}{2} B= \\ & \sqrt{\frac{1(3-b)}{a c}}, \tan \frac{1}{2}=\sqrt{\frac{(s-a)(3-c)}{s(s-b)}} \end{aligned}$ |
|  | C | $\begin{aligned} & \sin \frac{1}{2} c=\sqrt{\frac{(b-a)(s-b)}{a b}}, \cos \frac{1}{2} c= \\ & \qquad \sqrt{\frac{s(s-c)}{a b}}, \operatorname{lan} \frac{1}{2} c=\sqrt{\frac{(b-a)(s-b)}{s(s-c)}} \end{aligned}$ |
|  | Aree | $\sqrt{s(s-a)(b-b)(b-c)}$ |
| $\star$ A, B, | $b, 6$ | $\mathrm{b}=\frac{0 \sin B}{\sin A}, c=\frac{a \sin C}{\sin A}=\frac{\sin (A+B)}{\sin A}$ |
|  | C | $C=180^{\circ}-(A+B)$ |
|  | Area | $\frac{1}{2} a b \sin C=\frac{\sigma^{2} \sin B \sin C}{2 \sin A}$ |
| $0, b, A$ | $\checkmark$ | $\sin B=\frac{b \sin A}{b}$ |
|  | C | $C=150^{\circ}-(A+B)$ |
|  | 6 | $c=\frac{a \sin C}{\sin A}=\frac{b \sin C}{\sin B}=\sqrt{a^{2}+b^{2}-2 a b \cos C}$ |
|  | Area | $\frac{1}{2} a b \sin C=\frac{1}{2} e c \sin s=\frac{1}{2} b \operatorname{cosin} A$ |
| a, b, C | A | $\tan A=\frac{a \sin c}{b-\cos c}$ |
|  | - | $s=180^{\circ}-(A+c), \tan \frac{1}{2}(a-b)=\frac{a-b}{a+b} \cot \frac{1}{2} c$ |
|  | C | $c=\frac{a \sin c}{\sin A}=\sqrt{a^{2}+b^{2}-2 \cdot b \cos C}$ |
|  | Area | $\frac{1}{2} a b \sin C$ |
| $\begin{gathered} a^{2}=b^{2}+c^{2}-2 b c \cos A, b^{2}=a^{2}+c^{2}-2 \cos \operatorname{sen}, \\ c^{2}=a^{2}+b^{2}-2 a b \cos C \\ \frac{a}{\sin A}=\frac{b}{\sin B}=\frac{c}{\sin C} . \end{gathered}$ |  |  |


| Angle deg. | Are | Sin | Cos | Tan | Cot | See | Cse | Chord. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | +1 | 0 | $\infty$ | +1 | $\infty$ | 0 |
| 30 | 1/6 \% | 1/2 | $1 / 2 \sqrt{3}$ | $1 / 3 \sqrt{3}$ | $\sqrt{3}$ | $2 / 3 \sqrt{3}$ | 2 | $\sqrt{2-\sqrt{3}}$ |
| 45 | 1/4 7 | $1 / 2 \sqrt{2}$ | $1 / 2 \sqrt{2}$ | +1 | +1 | $\sqrt{2}$ | $\sqrt{2}$ | $\sqrt{2-\sqrt{2}}$ |
| 60 | 1/3 | $1 / 2 \sqrt{3}$ | 1/2 | $\sqrt{3}$ | $1 / 3 \sqrt{3}$ | 2 | $2 / 3 \sqrt{3}$ | 1 |
| 90 | $1 / 2 \pi$ | $+1$ | 0 | $\infty$ | 0 | - | +1 | $\sqrt{2}$ |
| 120 | 2/3 \# | $1 / 2 \sqrt{3}$ | -1/2 | $-\sqrt{3}$ | $-1 / 3 \sqrt{3}$ | -2 | $2 / 3 \sqrt{3}$ | $\sqrt{3}$ |
| 135 | 3/4 $\pi$ | $1 / 2 \sqrt{2}$ | $-1 / 2 \sqrt{2}$ | -1 | -1 | $-\sqrt{2}$ | $\sqrt{2}$ | $\sqrt{2+\sqrt{2}}$ |
| 150 | 5/6 $\pi$ | 1/2 | $-1 / 2 \sqrt{3}$ | $-1 / 3 \sqrt{3}$ | $-\sqrt{3}$ | $-2 / 3 \sqrt{3}$ | 2 | $\sqrt{2+\sqrt{3}}$ |
| 180 | $\pi$ | 0 | -1 | 0 | $\infty$ | -1 | $\infty$ | 2 |
| 210 | 7/6 $\pi$ | -1/2 | -1/2 $\sqrt{3}$ | $1 / 3 \sqrt{3}$ | $\sqrt{3}$ | $-2 / 3 \sqrt{3}$ | -2 | $\sqrt{2+\sqrt{3}}$ |
| 225 | 5/4 7 | $-1 / 2 \sqrt{2}$ | $-1 / 2 \sqrt{2}$ | +1 | +1 | $-\sqrt{2}$ | $-\sqrt{2}$ | $\sqrt{2+\sqrt{2}}$ |
| 240 | 4/3 7 | $-1 / 2 \sqrt{3}$ | $-1 / 2$ | $\sqrt{3}$ | $1 / 3 \sqrt{3}$ | -2 | $-2 / 3 \sqrt{3}$ | $\sqrt{3}$ |
| 270 | 3/2 $\pi$ | -1 | 0 | $\infty$ | 0 | $\infty$ | -1 | $\sqrt{2}$ |
| 300 | 5/3 $\pi$ | $-1 / 2 \sqrt{3}$ | 1/2 | $-\sqrt{3}$ | $-1 / 3 \sqrt{3}$ | 2 | $-2 / 3 \sqrt{3}$ | 1 |
| 315 | 7/4 $\pi$ | $-1 / 2 \sqrt{2}$ | $1 / 2 \sqrt{2}$ | -1 | -1 | $\sqrt{2}$ | $-\sqrt{2}$ | $\sqrt{2-\sqrt{2}}$ |
| 330 | 11/6 \% | $-1 / 2$ | $1 / 2 \sqrt{3}$ | $-1 / 3 \sqrt{3}$ | $-\sqrt{3}$ | $2 / 3 \sqrt{3}$ | -2 | $\sqrt{2-\sqrt{2}}$ |
| 360 | $2 \pi$ | 0 | +1 | 0 | $\infty$ | +1 | $\infty$ | 0 |




Fundamental Trigonometric Functions

$$
\begin{array}{ll}
\sin A=\frac{a}{c} . & \csc A=\frac{c}{a} \\
\cos A=\frac{b}{c} & \sec A=\frac{c}{b} \\
\tan A=\frac{a}{b} & \cot A=\frac{b}{a}
\end{array}
$$

Functions of one angle

$$
\begin{aligned}
& \sin ^{2} A+\cos ^{2} A=1 \\
& \sec ^{2} A-\tan ^{2} A=1 \\
& \csc ^{3} A-\cot ^{2} A=1
\end{aligned}
$$

Functions of the sum of two angles
$\sin (A+B)=\sin A \cos B+\cos A \sin B$
$\cos (A+B)=\cos A \cos B-\sin A \sin B$
$\tan (A+B)=\frac{\tan A+\tan B}{1-\tan A \tan B}$
$\cot (A+B)=\frac{\cot A \cot B-1}{\cot B+\cot A}$

Functions of the difference of two angles
$\sin (A-B)=\sin A \cos B-\cos A \sin B$ $\cos (A-B)=\cos A \cos B+\sin A \sin B$ $\tan (A-B)=\frac{\tan A-\tan B}{1+\tan A \tan B}$ $\cot (A-B)=\frac{\cot A \cot B+1}{\cot B-\cot A}$

Functions of one-half an angle

$$
\begin{aligned}
& \sin 1 / 2 A=\frac{\sin A}{2 \cos 1 / 2 A}= \pm \sqrt{\frac{1-\cos A}{2}} \\
& \cos 1 / 2 A=\frac{\sin A}{2 \sin 1 / 2 A}= \pm \sqrt{\frac{1+\cos A}{2}} \\
& \tan 1 / 2 A=\frac{1-\cos A}{\sin A}= \pm \sqrt{\frac{1-\cos A}{1+\cos A}} \\
& \cot 1 / 2 A= \pm \sqrt{\frac{1-\cos A}{1+\cos A}}
\end{aligned}
$$

Functions of twice an angle

$$
\begin{aligned}
\sin 2 A & =2 \sin A \cos A=\frac{2 \tan A}{1+\tan ^{2} A} \\
\cos 2 A & =\cos ^{2} A-\sin ^{2} A=1-2 \sin ^{2} A \\
& =2 \cos ^{2} A-1=\frac{1-\tan ^{2} A}{1+\tan ^{2} A} \\
\tan 2 A & =\frac{2 \tan A}{1-\tan ^{2} A}=\frac{\sin 3 A-\sin A}{\cos 3 A+\cos A} \\
\cot 2 A & =\frac{\cot A-1}{2 \cot A}
\end{aligned}
$$

Functions of three times an angle
Functions of angles squared

$$
\begin{aligned}
& \sin 3 A=3 \sin A-4 \sin ^{2} A \\
& \cos 3 A=4 \cos ^{2} A-3 \cos A \\
& \tan 3 A=\frac{3 \tan A-\tan ^{2} A}{1-3 \tan ^{2} A} \\
& \cot 3 A=\frac{\cot ^{3} A-3 \cot A}{3 \cot ^{2}-1}
\end{aligned}
$$

$$
\sin ^{2} \mathrm{~A}=\frac{1-\cos 2 \mathrm{~A}}{2}
$$

$$
\cos ^{2} A=\frac{1+\cos 2 A}{2}
$$

$$
\tan ^{2} A=\frac{1-\cos 2 A}{1+\cos 2 A}
$$

$$
\cot ^{1} \mathrm{~A}=\frac{1+\cos 2 \mathrm{~A}}{1-\cos 2 \mathrm{~A}}
$$

$$
\sin ^{2} A-\sin ^{1} B=\sin (A+B) \sin (A-B)
$$

$$
\cos ^{2} A-\sin ^{2} B=\cos (A+B) \cos (A-B)
$$

Functions-Relationships

$$
\begin{aligned}
& \sin A=\frac{\cos A}{\cot A}=\frac{1}{\csc A}=\cos A \tan A=\sqrt{1-\cos ^{1} A} \\
& \cos A=\frac{\sin A}{\tan A}=\frac{1}{\sec A}=\sin A \cot A=\sqrt{1-\sin ^{2} A} \\
& \tan A=\frac{\sin A}{\cos A}=\frac{1}{\cot A}=\sin A \sec A \\
& \cot A=\frac{\cos A}{\sin A}=\frac{1}{\tan A}=\cos A \csc A \\
& \sec A=\frac{\tan A}{\sin A}=\frac{1}{\cos A} \\
& \csc A=\frac{\cot A}{\sin A}=\frac{1}{\sin A} \\
& \sin A+\sin B=2 \sin 1 / 2(A+B) \cos 1 / 2(A-B) \\
& \sin A-\sin B=2 \cos 1 / 2(A+B) \sin 1 / 2(A-B) \\
& \cos A+\cos B=2 \cos 1 / 2(A+B) \cos 1 / 2(A-B) \\
& \cos A-\cos B=-2 \sin 1 / 2(A+B) \sin 1 / 2(A-B) \\
& \tan A+\tan B=\frac{\sin (A+B)}{\cos A \cos B} \\
& \tan A-\tan B=\frac{\sin (A-B)}{\cos A \cos B} \\
& \cot A+\cot B=\frac{\sin (A+B)}{\sin A \sin B} \\
& \cot A-\cot B=\frac{\sin (B-A)}{\sin A \sin B}
\end{aligned}
$$

For two signals having the same frequency, the phase can be determined by measuring the majorand minor axes of the ellipse. The phase angle is equal to twice the angle whose tangent is the ratio of the major axis to the minor axis. The absolute accuracy of this method is dependent upon the phase in the horizontal and vertical amplifiers of the oscilloscope being equal and the care that is taken to make the horizontal and vertical amplitudes equal.



## PULSE PARAMETER NOMOGRAM

This normalized nomogram relates pulse rise time, repetition frequency, and pulse width to data channel bandwidth. To use the nomogram, connect a horizontal line through the selected bandwidth. The intersection with the other columns gives maximum pulse repetition frequency, minimum pulse width, and minimum risetime. For a given bandwidth, any combination of factors below the line can be used.

FOR EXAMPLE: For a bandwidth of $10 \mathrm{MHz}\left(10 \times 10^{6} \mathrm{~Hz}\right)$ the fastest risetime is $0.035 \times 10^{-6} \mathrm{sec}$, the maximum pulse repetition frequency is $3.34 \times 10^{6}$ pulses per second, and the minimum pulse width is $0.15 \times 10^{-6} \mathrm{sec}$.



This scale is based on the formula $f=1 / T$ ．It converts between the frequency（ $f$ ）and the period（ $T$ ）of any recurrent waveform between 1 Hz and $10,00 \mathrm{GHz}$ ．It is useful where a large number of conversions are re－ quired as in the case when an oscilloscope with a time－calibrated sweep is used for frequency mea－ surements．

FOR EXAMPLE：（1）The period of a $40-\mathrm{MHz}$ sig－ nal is 25 nsec ．（2）The frequency of a signal with a period of $12.5 \mu \mathrm{sec}$ is 80 kHz ．

| FREQUENCY | PERIOD |
| :---: | :---: |
| $\mathrm{Hz}^{\longrightarrow}$ |  |
| $\mathrm{HHz}_{2}$ |  |
| $\mathrm{MH}_{2} \longrightarrow$ nsec |  |
| $\mathrm{CH}_{2}$ psec |  |
| $10000=0.1$ |  |
| $8000=$ |  |
| 6000－7 |  |
|  |  |
|  |  |
| $4000 \frac{z}{5=}$ |  |
| $3000 \frac{=}{=}=0.3$ |  |
|  |  |
| $2000=0.5$ |  |
| E |  |
|  |  |
| $1000 \frac{-5}{=-1}$ |  |
|  |  |
| $800=$ |  |
| $600-\frac{E}{E}$ |  |
| $500 \frac{\square}{\text { E }}^{2}$ |  |
|  |  |
| $400 \frac{\text { 者 }}{\text { 者 }}$ |  |
| $300=5$ |  |
| $200 \frac{\sum^{-E}}{\frac{E}{=1}} 5$ |  |
|  |  |
| ＝$=6$ |  |
| $=$ |  |
|  |  |
|  |  |
| $80=7$ |  |
| $60-5$ |  |
| $50 \frac{\text { F }}{\text { \＃}}$－ 20 |  |
| $40 \frac{\text { En }}{\frac{1}{2}}$ |  |
| $30 \frac{F}{E} 30$ |  |
| 三年 40 |  |
| 20－$=30$ |  |
| $\frac{\bar{E}}{=-} 60$ |  |
|  |  |
|  |  |
|  |  |
| $8=$ |  |
| $5 \frac{E}{=-} 200$ |  |
|  |  |
|  |  |
|  |  |
|  |  |
| $\begin{array}{r} 2=500 \\ \frac{y}{t}-600 \end{array}$ |  |
|  |  |
| I－800 |  |
| $1-1000$ |  |


| Letter |  | Name | Letter |  | Name |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Small | Capital |  | Small | Capital |  |
| $\begin{aligned} & \alpha \\ & \beta \\ & \gamma \\ & \delta \\ & \epsilon \\ & \zeta \\ & \eta \\ & \theta \\ & \iota \\ & \kappa \\ & \lambda \\ & \mu \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~B} \\ & \mathrm{r} \\ & \Delta \\ & \mathrm{E} \\ & \mathrm{Z} \\ & \mathrm{H} \\ & \Theta \\ & \mathrm{I} \\ & \mathrm{~K} \\ & \Lambda \\ & \mathrm{M} \end{aligned}$ | Alpha <br> Beta <br> Gamma <br> Delta <br> Epsilon <br> Zeta <br> Eta <br> Theta <br> lota <br> Kappa <br> Lambda <br> Mu | $\nu$ $\xi$ $o$ $\pi$ $\rho$ $\sigma$ $\tau$ $v$ $\phi$ $\chi$ $\psi$ $\omega$ | $\begin{aligned} & \mathrm{N} \\ & \Xi \\ & \mathrm{O} \\ & \Pi \\ & \mathrm{P} \\ & \mathrm{\Sigma} \\ & \mathrm{~T} \\ & \mathrm{Y} \\ & \Phi \\ & \mathrm{X} \\ & \Psi \\ & \Omega \end{aligned}$ | Nu <br> XI <br> Omicron <br> Pi <br> Rho <br> Sigma <br> Tau <br> Upsilon <br> Phi <br> Chi <br> Psi <br> Omega |

ROMAN NUMERALS
The chief symbols are $I=1 ; V=5 ; X=10 ; L=50 ; C=100 ; D=500$; and $M=1,000$. Note that $I V=4$, means 1 short of $5 ; I X=9$, means 1 short of ten; XL $=40$, means 10 short of 50 ; and $X C=90$, means 10 short of 100 . Any symbol following one of equal or greater value adds its value- $\|=2$. Any symbol preceding one of greater value subracts its value-IV $=4$. When a symbol stands between two of greater value its value is subtracted from the second and the remainder is added to the first-XIV = 14; LIX $=59$. Of two equivalent ways of representing a number, that in which the symbol of larger denomination preceded is preferred-XIV instead of VIX for 14.

| 1 | 1 | 8 | VIII |
| :---: | :---: | :---: | :---: |
| 2 | II | 9 | IX |
| 3 | III | 10 | X |
| 4 | IV | 50 | L |
| 5 | V | 100 | C |
| 6 | VI | 500 | D |
| 7 | VII | 1,000 | M |

Time delay, phase angle, and frequency are related by the following formula:

$$
t=\frac{10^{2} \theta}{36 f}
$$

where
$t$ is in milliseconds
$\theta$ is in degrees
$f$ is in hertz
FOR EXAMPLE: A phase angle of $90^{\circ}$ between two $60-\mathrm{Hz}$ wave shapes has a time interval of 4.16 msec .
NOTE: Corresponding right-hand frequency and time scales are used together as are left-hand frequency and time scales. The range of the nomogram can be extended by multiplying the frequency scale by any power of 10 and dividing the time scale by the same power of 10 .

| Description | Waveform | $E_{\text {mss }}$ | $E_{\text {ave }}$ |
| :---: | :---: | :---: | :---: |
| Alternating sine wave |  | $\frac{E_{\text {peak }}}{\sqrt{2}}$ | $\frac{2 E_{\text {peak }}}{\pi}$ |
| Sawtooth wave | $\text { ~レレ } \frac{1}{\varepsilon_{\text {peok }}}$ | $\frac{E_{\text {peak }}}{\sqrt{3}}$ | $\frac{E_{\text {pesk }}}{2}$ |
| Clipped sawtooth wave |  | $E_{\text {peak }} \sqrt{\frac{T_{0}}{3 T}}$ | $\frac{E_{\text {peak }} T_{0}}{2 T}$ |
| Square wave |  | $E_{\text {peok }} \sqrt{\frac{1}{2}}$ | $\frac{E_{\text {peok }}}{2}$ |
| Rectified sine wave | $\cdots \cdots \frac{1}{k_{p o o k}^{c}}$ | $\frac{E_{\text {patak }}}{\sqrt{2}}$ | $\frac{2 E_{\text {peak }}}{\pi}$ |
| Clipped sine wave | $\bigcap_{1-T \rightarrow 1}^{T_{0} \mid} \cap \frac{\frac{1}{E_{\text {peok }}}}{1}$ | $E_{\text {peak }} \sqrt{ } \begin{aligned} & \frac{T_{0}}{2 T} \\ & \frac{\text { if } T=T_{0}}{2} \\ & \frac{E_{\text {peak }}}{2} \end{aligned}$ | $\frac{E_{\text {peak }}}{\pi}$ |
| Alternating square wave |  | $E_{\text {peak }}$ | $E_{\text {peak }}$ |
| Rectangular wave | $\prod_{1-T \rightarrow+}^{160} \prod^{\frac{1}{E_{\text {peok }}}}$ | $E_{\text {peak }} \sqrt{\frac{T_{0}}{T}}$ | $\frac{E_{\text {peak }} T_{0}}{T}$ |
| Triangular wave |  | $\frac{E_{\text {peak }}}{\sqrt{3}}$ | $\frac{E_{\text {peak }}}{2}$ |

The Fourier content of five common periodic waveforms, out to the seventh harmonic, is given in this table. Magnitudes only are tabulated-not phase relationships. The magnitudes are those of the voltage waveform, followed by the corresponding percentage values in parentheses. If energy content is desired, these values must be squared. Note that there are no even harmonics present in any of the symmetrical waveforms.

| Waveform | Name | Harmonic Compotition (magnitude) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Fund. | 2nd | 3 rd | 4th | 5th | 6th | 7th |
|  | Squàre Wave | $\begin{gathered} \frac{4}{\pi} E \\ (127 \%) \end{gathered}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ | $\begin{aligned} & \frac{4}{3 \pi} \mathrm{E} \\ & (42.5 \%) \end{aligned}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ | $\begin{aligned} & \frac{4}{5 \pi} E \\ & (25.5 \%) \end{aligned}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ | $\begin{aligned} & \frac{4}{7 \pi} \mathrm{E} \\ & (18.2 \%) \end{aligned}$ |
|  | Triangular Wave | $\begin{aligned} & \frac{8}{\pi^{2}} \mathrm{E} \\ & (81 \%) \end{aligned}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ | $\begin{aligned} & \frac{8}{9 \pi^{2}} E \\ & (9 \%) \end{aligned}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ | $\begin{aligned} & \frac{8}{25 \pi^{2}} E \\ & (3.2 \%) \end{aligned}$ | 0 $(0 \%)$ | $\begin{aligned} & \frac{8}{49 \pi^{5}} E \\ & (1.6 \%) \end{aligned}$ |
|  | Sawtooth Wave | $\begin{aligned} & \frac{2}{\pi} E \\ & (63.6 \%) \end{aligned}$ | $\begin{gathered} \frac{1}{\pi} E \\ (31.8 \%) \end{gathered}$ | $\begin{aligned} & \frac{2}{3 \pi} E \\ & (21.2 \%) \end{aligned}$ | $\begin{gathered} \frac{1}{2 \pi} E \\ (15.9 \%) \end{gathered}$ | $\begin{aligned} & \frac{2}{5 \pi} E \\ & (12.7 \%) \end{aligned}$ | $\begin{aligned} & \frac{1}{3 \pi} E \\ & (10.6 \%) \end{aligned}$ | $\begin{aligned} & \frac{2}{7 \pi} \mathrm{E} \\ & (9.1 \%) \end{aligned}$ |
|  | Half-Wave Rectifier Output | $\begin{aligned} & \frac{1}{\pi} E \\ & (31.8 \%) \end{aligned}$ | $\begin{aligned} & \frac{2}{3 \pi} \mathrm{E} \\ & (21.2 \%) \end{aligned}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ | $\frac{2}{15 \pi} E$ <br> (4.2\%) | 0 <br> (0\%) | $\begin{aligned} & \frac{2}{35 \pi} \mathrm{E} \\ & (1.8 \%) \end{aligned}$ | 0 <br> (0\%) |
|  | Full-Wave Rectifler Output | $\begin{aligned} & \frac{2}{\pi} \mathrm{E} \\ & (63.6 \%) \end{aligned}$ | $\begin{gathered} \frac{4}{3 \pi} \mathrm{E} \\ (42.3 \%) \end{gathered}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ | $\begin{aligned} & \frac{4}{15 \pi} \mathrm{E} \\ & (8.5 \%) \end{aligned}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ | $\begin{aligned} & \frac{4}{35 \pi} \mathrm{E} \\ & (3.6 \%) \end{aligned}$ | $\begin{gathered} 0 \\ (0 \%) \end{gathered}$ |


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The nomogram below is based on the equation shown and makes possible rapid addition or subtraction of two or more dB levels.

For off-scale levels $1,2,5,10,20,30$, etc., can be added or subtracted, simultaneously, to all nomograph scale values. For more than two levels, add any two, and to the first sum add the third, etc.

FOR EXAMPLE: (1) What is the combined sound power level of 70,76 and 80.5 dB ? Align $(\mathrm{dB})=76$ with $(\mathrm{dB})_{\mathrm{b}}=70$ and read $(\mathrm{dB})_{\mathrm{t}}=77.0$; align $(\mathrm{dB})_{\mathrm{a}}=77.0$ with $(\mathrm{dB})_{\mathrm{b}}=80.5$ and read the answer as $(\mathrm{dB})_{\mathrm{t}}=82.1$ dB.
(2) When a fan is on, the sound pressure level equals 68 dB and 64 dB with the fan off. What is the sound pressure level of the fan? To extend the range of the nomogram, subtract 10 from all scale values; align $(\mathrm{dB})_{\mathrm{t}}=68=78-10$ with $(\mathrm{dB})_{a}=64=74-10$, and read $(\mathrm{dB})_{b}=75.8-10=65.8 \mathrm{~dB}=$ fan sound pressure level.

(From "Nomograph lets you add and subtract decibels," EDN, March 20, 1977, p. 149, courtesy of EDN.)

## DECIBEL NOMOGRAPHS

With the nomograph below and the one on the next page dB gain or loss of any equipment can be determined (even if input and output impedances differ) if input and output voltages and resistances can be measured. The nomograms cover a power range of 10,000 to 1 , a voltage range of 100 to 1 , and a decibel range from +40 to - 40 dB . Voltage and resistance scales of nomogram 1 bearing the same suffix are used together.


FOR EXAMPLE: Determine the gain of an amplifier that produces an output of 5 V across 8 ohms with a $10-\mathrm{V}$ signal applied to its 500 -ohm input. From nomogram 1 , the input power is 0.2 W and the output power is 3.1 W. Connecting input and output power on nomogram 11 shows the amplifier gain to be slightly less than 12 dB .


## LETTER SYMBOLS FDR QUANTITIES USED IN ELECTRICAL SCIENCE AND ELECTRICAL ENGINEERING

## Extracted from IEEE Standard No. 280

The tables that follow list quantities grouped in several categories, and give quantity symbols, units based on the International System,* and unit symbols.

Those quantity symbols that are separated by a comma are alternatives on equal standing. Where two symbols for a quantity are separated by three dots (...), the second is a reserve symbol, which is to be used only where there is specific need to avoid a conflict. As a rule the tables do not indicate the vectorial or tensorial character that some of the quantities may have.

The International System of Units (Systeme International d'Unités) is the coherent system of units based on the following units and quantities:

| Unit | Quantity |
| :--- | :--- |
| meter | length |
| kilogram | mass |
| second | time |
| ampere | electric current |
| kelvin | temperature |
| candela | luminous intensity |
| radian | plane angle |
| steradian | solid angle |

This system was named (and given the international designation SI) in 1960 by the Conférence Générale des Poids et Mesures (CGPM). The SI units include as subsystems the MKS system of units, which covers mechanics, and the MKSA or Giorgi system, which covers mechanics, electricity, and magnetism.
*The name of the unit is given as a further guide to the definition of the symbol. A quantity shall be represented by the standard letter symbol appearing in the table regardless of the system of units in which the quantity is expressed.


${ }^{3}$ Commas separate symbols on equal standing. Where two symbols are separated by three dots the second is a reserve symbol and is to be used only when there is specific need to avoid a conflict. See Introduction to the Tables.

| logerithmic decrement | $\wedge$ | (numeric) |  | then $\delta$ is the damping coefficient. <br> $\Lambda=T \delta$, where $T$ and 6 ere es given in tha equetion of 1.28 . |
| :---: | :---: | :---: | :---: | :---: |
| ettenuetion coefficient | * | neper per meter | $\mathrm{Np} / \mathrm{m}$ |  |
| phese coefficient | $\beta$ | redien per meter | $\mathrm{rad} / \mathrm{m}$ |  |
| propagation coefficient | $\boldsymbol{\gamma}$ | reciprocal meter | $m^{-1}$ | $\gamma=\alpha+j \beta$. |
| 2. Mechenics ${ }^{\text {b }}$ |  |  |  |  |
| mass | $m$ |  | $\mathbf{k g}$ |  |
| (mess) density | $\rho$ | kilogrem per cubic meter | $\mathrm{kg} / \mathrm{m}^{3}$ | Mess divided by volume. |
| momentum | $\rho$ | kilogram meter per second | $\mathrm{kg} \cdot \mathrm{m} / \mathrm{s}$ |  |
| momant of inertie | 1, J | kilogrem meter squared | $\mathrm{kg} \cdot \mathrm{m}^{2}$ |  |
| second (exiel) moment of erea | I, Ia | meter to the fourth power | $\mathrm{m}^{4}$ | Quentities 2.4a end 2.4 b should be distinguished from 2.4 |


| Itam Quantity | Quantity Symbo/a | Unit Based on International System | Unit Symbol | Remarks |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | They have often been given the nama "moment of inertie." |
| second (poler) moment of erea | $J, I_{p}$ | meter to the fourth power | $\mathrm{m}^{4}$ |  |
| force | $F$ | newton | N |  |
| weight | W | newton | N | Veries with eccelerstion of free fall. |
| weight density | ${ }^{\boldsymbol{\gamma}}$ | newton per cubic meter | $\mathrm{N} / \mathrm{m}^{3}$ | Weight divided by volume. |
| moment of force |  | newton meter | $N \cdot m$ |  |
| torque | $T \ldots M$ | newton meter | $N \cdot m$ |  |
|  |  | newton per squere meter | $\mathrm{N} / \mathrm{m}^{2}$ | The neme pasca/ hes been suggested for this unit. |
| normal stress | $\sigma$ | nowton per squere meter | $\mathrm{N} / \mathrm{m}^{2}$ |  |
| sheer stress | $\tau$ | newton per square meter | $\mathrm{N} / \mathrm{m}^{2}$ |  |
| stress tensor | $\sigma$ | newton per squere meter | $\mathrm{N} / \mathrm{m}^{2}$ |  |
| lineer strein | $\epsilon$ | (numeric) |  |  |
|  | $\boldsymbol{\gamma}$ | (numeric) |  |  |
| strein tensor | $\boldsymbol{E}$ | (numeric) |  |  |
| volume strain |  | (numeric) |  |  |
| Poisson's retio | $\mu, \nu$ $E$ | (numeric) |  | Lateral contrection divided by elongation. |
| Young's modulus modulus of elesticity | $E$ | newton per square meter | $\mathrm{N} / \mathrm{m}^{2}$ | $E=\sigma / \epsilon$ |
| sheer modulus modulus of rigidity | $G$ | newton per squere meter | $\mathrm{N} / \mathrm{m}^{2}$ | $G=\tau / \gamma$ |
| bulk modulus | $K$ | newton per squere meter | $\mathrm{N} / \mathrm{m}^{2}$ | $K=-p / \theta$ |
| work | $w$ | joule |  |  |
| energy | $E, W$ | joule |  | $U$ is recommended in thermodynemics for internal energy and for blackbody radiation. |

${ }^{\mathrm{b}}$ The units and corresponding unit symbois are included for use in electricel science and electrical engineering. In mechanics and mechanical engineering other units and corresponding unit symbols ere also used. (USAS Y 10.3 now being revised.)

| energy (volume) <br> density <br> power | $w$ | joule per cubic meter | $\mathrm{J} / \mathrm{m}^{3}$ |  |
| :---: | :--- | :--- | :--- | :--- |
| efficiency <br> 3. Heat <br> obsolute tempera- <br> ture <br> thermodynemic <br> temperature | $T \ldots \Theta$ | watt | W | Rete of energy trens- <br> fer, |
| $W=\mathrm{J} / \mathrm{s}$ |  |  |  |  |
| (numeric) |  |  |  |  |


${ }^{\text {CThe }}$ The units and corresponding unit symbols are included for use in electrical science end engineering. In mechenical engineering other units and corresponding unit symbols are also used. (Cf. USAS Y10.4.)

| tharmal conductivity | 入...k | wett per meter kelvin | W/(m-K) |  |
| :---: | :---: | :---: | :---: | :---: |
| thermel conductence | $G_{\theta}$ | wett per kelvin | W/K |  |
| thermal resistivity | $\stackrel{\rho}{0}_{R_{0}}$ | meter kelvin per wett | $\underset{K M}{m} \cdot K / W$ |  |
| thermel resistence | $R_{\theta}$ | kelvin per wett | K/W |  |
| thermel capecitance | $c_{\theta}$ | joule per keivin |  |  |
| heat capacity |  |  |  |  |
| thermal impedence | $Z_{\theta}$ | kelvin per watt | K/W |  |
| specif ic heet capscity | c | joule per kelvin kilogrem | J/(K.kg) | Heet capecity divided by mass. |









## LETTER SYMBOLS FOR UNITS USED IN ELECTRICAL SCIENCE AND ELECTRICAL ENGINEERING

## Extracted from IEEE Standard No. 260

The use of unit symbols, instead of the spelled-out names of the units, is frequently desirable where space is restricted. Their use presupposes that the reader will find them intelligible. If there is any doubt that the reader will understand a symbol, the name of the unit should be written in full. When an unfamiliar unit symbol is first used in text, it should be followed by its name in parentheses; only the symbol need be used thereafter. Explanatory notes or keys should be included where appropriate on drawings and in tabular matter.

The use of unit symbols is never mandatory, but when unit symbols are employed they must conform to those given in the Standard.

## List of Symbols

Symbols for units are listed alphabetically by name of unit below. The list is intended to be reasonably complete, but could not possibly include all units that might conceivably be used in modern electrical technology. Many compound symbols and many illustrations of the use of the metric prefixes are included. Other combined forms may easily be constructed.

Every effort should be made to maintain the distinction between upper- and lowercase letters shown in the list, wherever the symbols for units are used, even if the surrounding text uses uppercase style.

In the notes accompanying the symbols, some units are identified as SI units. These units belong to the Intemational System of Units (Système Intemational d'Unités), which is the name given in 1960 by the Conference Genérale des Poids et Mesures to the coherent system of units based on the following basic units and quantities:

| Unit | Quantity |
| :--- | :--- |
| meter | length |
| kilogram | mass |
| second | time |


| Unit | Quantity |
| :--- | :--- |
| ampere | electric current |
| kelvin | temperature |
| candela | luminous intensity |

The SI units include as subsystems the MKS system of units, which covers mechanics, and the MKSA or Giorgi system, which covers mechanics, electricity, and magnetism.

| Unit | Symbol | Remarks |
| :---: | :---: | :---: |
| ampere | A |  |
| ampere-hour | Ah |  |
| ampere-turn | At |  |
| angstrom | $\AA$ |  |
| atmosphere |  |  |
| normal atmosphere | atm | $1 \mathrm{~atm}=101325 \mathrm{~N} / \mathrm{m}^{2}$ |
| technical atmosphere | at | $1 \mathrm{at}=1 \mathrm{kgf} / \mathrm{cm}^{2}$ |
| atomic mass unit (unified) | u | The (unified) atomic mass unit is defined as one-twelfth of the mass of an atom of the ${ }^{12} \mathrm{C}$ nuclide. Use of the old atomic mass unit (amu), defined by reference to oxygen, is deprecated. |
| bar | bar | $1 \mathrm{bar}=100000 \mathrm{~N} / \mathrm{m}^{2}$ |
| barn | b | $1 \mathrm{~b}=10^{-28} \mathrm{~m}^{2}$ |
| bel | B |  |
| billion electronvolts | GeV | The name billion electronvolts is depre- |
| British thermal unit | Btu | cated; see gigaelectronvolt. |

## LETTER SYMBOLS FOR UNITS USEDIN ELECTRICAL SCIENCE AND ELECTRICAL ENGINEERING

| Unit | Symbol | Remarks |
| :---: | :---: | :---: |
| calorie (International Table calorie) | $\mathrm{cal}_{1 T}$ | $1 \mathrm{cal}_{!T}=4.1868 \mathrm{~J}$ <br> The 9th Conférénce Générale des Poids et Mesures has adopted the joule as the unit of heat, avoiding the use of the calorie as far as possible |
| calorie (thermochemical calorie) | $\mathrm{cal}_{\text {th }}$ | $1 \mathrm{cal}_{\mathrm{th}}=4.1840 \mathrm{~J}$ (See note for International Table calorie.) |
| candela | cd |  |
| candela per square foot | $\mathrm{cd} / \mathrm{ft}^{2}$ |  |
| candela per square meter | $\mathrm{cd} / \mathrm{m}^{2}$ | The name nit is sometimes used for this unit. |
| candle | cd | The unit of luminous intensity has been given the name candela; use of the name candle for this unit is deprecated. |
| centimeter | cm |  |
| circular mil | emil | $1 \mathrm{cmil}=(\pi / 4) \cdot 10^{-6} \mathrm{in}^{2}$ |
| coulomb | C |  |
| cubic centimeter | $\mathrm{cm}^{3}$ |  |
| cubic foot | $\mathrm{tt}^{3}$ |  |
| cubic foot per minute | $\mathrm{ft}^{3} / \mathrm{min}$ |  |
| cubic foot per second | $\mathrm{ft}^{3} / \mathrm{s}$ |  |
| cubic inch | $\mathrm{in}^{3}$ |  |
| cubic meter | $\mathrm{m}^{3}$ |  |
| cubic meter per second | $\mathrm{m}^{3} / \mathrm{s}$ |  |
| cubic yard | $\mathrm{yd}^{3}$ |  |
| curie | Ci | Unit of activity in the field of radiation dosimetry |
| cycle per second | $\mathrm{c} / \mathrm{s}$ | The name hertz $(\mathrm{Hz})$ is internationally accepted for this unit. |
| decibel | dB |  |
| decibel referred to one milliwatt degree (plane angle) | $\begin{gathered} \mathrm{dBm} \\ \ldots \end{gathered}$ |  |
| degree (temperature) degree Celsius degree Fahrenheit | ${ }^{\circ} \mathrm{C}$ | Note that there is no space between the symbol ${ }^{\circ}$ and the letter. The use of the word centigrade for the Celsius tempera- |
| kelvin | K | ture scale was abandoned by the Conférence Générale des Poids et Mesures in 1948. In 1967 the CGPM gave the name kelvin to the SI unit of temperature, which was formerly called degree Kelvin, and assigned it the symbol K (without the symbol ${ }^{\circ}$ ). |
| dyne | dyn |  |
| electronvolt | eV |  |
| erg | erg |  |
| farad | F |  |
| foot | ft |  |
| footcandle | fc | The name lumen per square foot $\left(1 \mathrm{~m} / \mathrm{ft}^{2}\right)$ is preferred for this unit. |



| Unit | Symbol | Remarks |
| :---: | :---: | :---: |
| kilovolt | kV |  |
| kilovoltampere | kVA |  |
| kilowatt | kW |  |
| kilowatthour | kWh |  |
| knot | knot |  |
| lambert | L | The lambert is the CGS unit of luminance. Use of the SI unit, the candela per square meter, is preferred. |
| liter | 1 |  |
| liter per second | 1/s |  |
| lumen | Im |  |
| lumen per square foot | $1 \mathrm{~m} / \mathrm{ft}^{2}$ |  |
| lumen per square meter | $1 \mathrm{~m} / \mathrm{m}^{2}$ |  |
| lumen per watt | $1 \mathrm{~m} / \mathrm{W}$ |  |
| lumen second | $1 \mathrm{~m} \cdot \mathrm{~s}$ |  |
| lux | IX | $1 \mathrm{~lx}=1 \mathrm{~lm} / \mathrm{m}^{2}$ |
| maxwell | Mx | The maxwell is the electromagnetic CGS unit of magnetic flux. Use of the SI unit, the weber, is preferred. |
| megacycle per second | $\mathrm{Mc} / \mathrm{s}$ | See note for cycle per second. |
| megaelectronvolt | MeV |  |
| megahertz | MHz |  |
| megavolt | MV |  |
| megawatt | MW |  |
| megohm | M $\Omega$ |  |
| meter | m |  |
| mho | mho | The IEC has adopted the name siemens (S) for this unit. |
| microampere | $\mu \mathrm{A}$ |  |
| microbar | $\mu \mathrm{bar}$ |  |
| microfarad | $\mu \mathrm{F}$ |  |
| microgram | $\mu \mathrm{g}$ |  |
| microhenry | $\mu \mathrm{H}$ |  |
| micrometer | $\mu \mathrm{m}$ |  |
| micromho | $\mu \mathrm{mho}$ | See note for mho. |
| micron | $\mu \mathrm{m}$ | The name micrometer is preferred. |
| microsecond | $\mu \mathrm{s}$ |  |
| microsiemens | $\mu \mathrm{S}$ |  |
| microwatt | $\mu \mathrm{W}$ |  |
| mil | mil | $1 \mathrm{mil}=0.001 \mathrm{in}$ |
| mile (statute) | mi |  |
| nautical mile | nmi |  |
| mile per hour | $\mathrm{mi} / \mathrm{h}$ |  |
| milliampere | mA |  |
| millibar | mbar |  |
| millibarn | mb |  |
| milligal | mGal |  |
| milligram | mg |  |
| millihenry | mH | - |


| Unit | Symbol | Remarks |
| :---: | :---: | :---: |
| milliliter | ml |  |
| millimeter | mm |  |
| conventional millimeter of mercury | mmHg | $1 \mathrm{mmHg}=133.322 \mathrm{~N} / \mathrm{m}^{2}$ |
| millimicron | nm | The name nanometer is preferred. |
| mill isecond | ms |  |
| millisiemens | mS |  |
| millivolt | mV |  |
| milliwatt | mW |  |
| minute (plane angle) | $\ldots$ |  |
| minute (time) | min | Time may be designated as in the following example: $9^{h} 46^{m} 30^{\text {t }}$ |
| nanoampere | nA |  |
| nanofarad | $n \mathrm{~F}$ |  |
| nanometer | nm |  |
| nanosecond | ns |  |
| nanowatt | nW |  |
| nautical mile | nmi |  |
| neper | Np |  |
| newton | N |  |
| newton meter | $N \cdot m$ |  |
| newton per square meter | $\mathrm{N} / \mathrm{m}^{2}$ |  |
| oersted | Oe | The oersted is the electromagnetic CGS unit of magnetic field strength. Use of the SI unit, the ampere per meter, is preferred. |
| ohm | $\Omega$ |  |
| ounce (avoirdupois) | O2 |  |
| picoampere | pA |  |
| picofarad | pF |  |
| picosecond | ps |  |
| picowatt | pW |  |
| pint | pt | The gallon, quart, and pint differ in the U.S. and the U.K., and their use is deprecated. |
| pound | lb |  |
| poundal | pdl |  |
| pound-force | Ibf |  |
| pound-force foot | lbf $\cdot \mathrm{ft}$ |  |
| pound-force per square inch | $\mathrm{lbf} / \mathrm{in}^{2}$ |  |
| pound per square inch |  | Although use of the abbreviation psi is common, it is not recommended. See pound-force per square inch. |
| quart | qt | The gallon, quart, and pint differ in the U.S. and the U.K., and their use is deprecated. |
|  | rd | Unit of absorbed dose in the field of radiation dosimetry. |
| radian | rad |  |
| rem | rem | Unit of dose equivalent in the field of radiation dosimetry. |


| Unit | Symbol | Remarks |
| :---: | :---: | :---: |
| revolution per minute | r/min | Although use of the abbreviation rpm is common, it is not recommended. |
| revolution per second | r/s |  |
| roentgen | R | Unit of exposure in the field of radiation dosimetry. |
| second (plane angle) | ..." |  |
| second (time) | $s$ | Time may be designated as in the following example: $9^{h} 46^{m} 30^{s}$. |
| siemens | S | $1 \mathrm{~S}=1 \Omega^{-1}$ |
| square foot | $\mathrm{ft}^{2}$ |  |
| square inch | in ${ }^{2}$ |  |
| square meter | $\mathrm{m}^{2}$ |  |
| square yard | $\mathrm{yd}^{2}$ |  |
| steradian | sr |  |
| tesla | -T | $1 \mathrm{~T}=1 \mathrm{~Wb} / \mathrm{m}^{2}$ |
| tonne | t | $1 \mathrm{t}=1000 \mathrm{~kg}$ |
| (unified) atomic mass unit | $u$ | The (unified) atomic mass unit is defined as one-twelfth of the mass of an atom of the ${ }^{12} \mathrm{C}$ nuclide. Use of the old atomic mass unit (amu), defined by reference to oxygen, is deprecated. |
| var | var | Unit of reactive power |
| volt | V |  |
| voltampere | VA | Unit of apparent power |
| watt | W |  |
| watthour | Wh |  |
| watt per steradian | W/sr |  |
| watt per steradian square meter | W/sr $\cdot \mathrm{m}^{2}$ ) |  |
| weber | Wb | $1 \mathrm{~Wb}=1 \mathrm{~V} \cdot \mathrm{~s}$ |
| yard | yd |  |

## CONVERSION OF ELECTROMAGNETIC UNITS

Three common systems of electromagnetic units are in universal employ. They are:

1. The absolute system of CGS electromagnetic system.
2. The practical CGS electromagnetic system.
3. The MKS system (Gaussian or Giorgi depending upon the choice of constants).

The chart allows rapid conversion from one system to another. In any one row, any quantity divided by any other quantity produces unity.

These Quantities Are Those Effected by Rationalization

| Quentity | Rotionolized |  |  | Unrotionolized |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MKS | CGS EM | CGS ES | MKS | CGS EM | ÇGS ES |
| Dielectric displocement <br> Units | 1 | $10^{-5}$ | $3 \times 10^{5}$ | 4\% | $4 \pi \times 10-5$ | $12 \pi \times 10^{5}$ |
|  | $10^{5}$ | 1 | $3 \times 10^{10}$ | $4 \times \times 10^{5}$ | 4\% | $12 \times \times 10^{10}$ |
|  | $1 / 3 \times 10^{-5}$ | $1 / 3 \times 10-10$ | 1 | $4 \mathrm{~m} / 3 \times 10-5$ | 4 $\times 13 \times 10^{-10}$ | 4\% |
|  | $1 / 4 m$ | $1 / 4 m \times 10^{-5}$ | $3 / 4 \pi \times 10^{5}$ | 1 | 10-5 | $3 \times 10-5$ |
|  | $1 / 4 \times 10^{5}$ | 1/4 | $3 / 4 \times 10^{10}$ | $10^{5}$ | 1 | $3 \times 10^{10}$ |
|  | $1 / 12 \times 10^{-5}$ | $1 / 12 \times \times 10^{-10}$ | 1/4m | $1 / 3 \times 10^{-5}$ | $1 / 3 \times 10-10$ | 1 |
|  | Coulomb/m ${ }^{2}$ | Abcoulomb/m ${ }^{2}$ | Stotcoulomb/cm ${ }^{2}$ | Coulomb/m ${ }^{2}$ | Abcoulomb/cm ${ }^{2}$ | Stotcoulomb/ $\mathrm{cm}^{2}$ |
| Mognefic field intensity | 1 | $10^{-3}$ | $3 \times 107$ | $4 \pi$ | $4 \pi \times 10^{-3}$ | $12 \pi \times 10^{7}$ |
|  | $10^{3}$ | 1 | $3 \times 10^{10}$ | $4 \pi \times 10^{3}$ | $4 \pi$ | $12 \pi \times 1010$ |
|  | $1 / 3 \times 10^{-7}$ | $1 / 3 \times 10^{-10}$ | 1 | $4 \pi / 3 \times 10^{-7}$ | $4 \pi / 3 \times 10^{-10}$ | 4\% |
|  | $1 / 4 \pi$ | $1 / 4 \pi \times 10^{-3}$ | $3 / 4 \pi \times 10^{7}$ | 1 | $10^{-3}$ | $3 \times 10^{7}$ |
|  | $1 / 4 \pi \times 10^{3}$ | $1 / 4 \pi$ | $3 / 4 \pi \times 10^{10}$ | $10^{3}$ | 1 | $3 \times 10^{10}$ |
|  | $1 / 12 \pi \times 10^{-7}$ | $1 / 12 \times \times 10^{-10}$ | $1 / 4 \pi$ | $1 / 3 \times 10^{-7}$ | $1 / 3 \times 10^{-10}$ | 1 |
| Units | Amp.fum/m | Oersted | ESU | Amp-fum/m | Oersted | ESU |
| Magnefometive force | 1 | 10-1 | $3 \times 10^{9}$ | 48 | $4_{17} \times 10-1$ | $12 \mathrm{~m} \times 109$ |
|  | 10 | 1 | $3 \times 10^{10}$ | 40. | $4 \pi$ | $12 . \times 10^{10}$ |
|  | $1 / 3 \times 10^{-9}$ | $1 / 3 \times 10-10$ | 1 | $4 \pi / 3 \times 10^{-9}$ | $4 \pi / 3 \times 10-10$ | $4 \pi$ |
|  | $1 / 4$ m | $1 / 4 \times \times 10^{-1}$ | $3 / 4 \times 10^{9}$ | 1 | $10-1$ | $3 \times 10^{9}$ |
|  | 10/4 | 1/4 | $3 / 4 \times 10^{10}$ | 10 | 1 | $3 \times 10^{10}$ |
|  | $1 / 12 \pi \times 10^{-9}$ | $1 / 12=10-10$ | 1/4\% | $1 / 3 \times 10^{-9}$ | $1 / 3 \times 10-10$ | 1 |
| Units | Amp-turn | Gilbert | ESU | Amp-turn | Gilbert | ESU |


|  | Practical Unit | Electromagnetic Unit | Electrostatic Unit |
| :---: | :---: | :---: | :---: |
| Quentity | MKS | CGS EM | CGS ES |
| 1. Cupocitence | 1 Farod | $10^{-9}$ Abfored | $9.100^{11}$ Starfored |
|  | $10^{9}$ Farod | 1 Ab fored | $9 \times 1020$ Siatiered |
|  | $1 / 9 \times 10^{-11}$ Forod | 1/9 = 10-20 Ablerod | 1 Stetferad |
| 2. Charge | 1 Coulomb | $10-1$ Absoulomb | $3 \times 109$ Statcoulamb |
|  | 10. Coulomb | 1 Abcoulomb | $3 \times 10^{10}$ Statcoulamb |
|  | $1 / 3=10^{-9}$ Coulamb | $1 / 3 \times 10-10$ Abcoulomb | 15 tatcoulomb |
| 3. Cherge denxity | 1 Coulamb/m ${ }^{3}$ | $10^{-7}$ Abcoulamb/ $/ \mathrm{cm}^{3}$ | $3 \times 10^{3}$ Statesulemb/ $/ \mathrm{cm}^{3}$ |
|  | $10^{7}$ Coulomb/m ${ }^{3}$ | $1 \mathrm{Abcoulomb/} / \mathrm{cm}^{3}$ | $3 \times 10^{10}$ Stotcoulomb/ $/ \mathrm{cm}^{3}$ |
|  | $1 / 3 \times 10^{-3}$ Coviomb/m ${ }^{3}$ | $1 / 3 \times 10^{-10}$ Abcoulomb/ $/ \mathrm{cm}^{2}$ ? | 1 Statceutomb/en ${ }^{3}$ |
| 4. Conduetivity | $1 \mathrm{mho} / \mathrm{m}$ | 10-11 Abmha/cm | $9 \times 10^{9}$ Statmherion |
|  | $10^{11}$ Wha m | 1 Abmho/cm | $9 \times 1020$ Statmhe/em |
|  | 1/9 = $10^{-9}$ Who/m | 1/9 $=10-20 \mathrm{Abmho} / \mathrm{cm}$ | 15 tatmbo/cm |
| 5. Current | 1 Ampere | $10^{-1}$ Abompero. | $3 \times 10^{9}$ Statampere |
|  | 10 Ampere | 1 Abempere | $3 \times 10^{10}$ Statampere |
|  | $1 / 3 \times 10-9$ Ampere | $1 / 3 \times 10^{-10}$ Abompere | 1 Stestampere |
| 6. Current den sity | 1 Ampare/m ${ }^{2}$ | 10-5 Abempere/cm ${ }^{\text {2 }}$ | $3 \times 10^{5}$ Statampere $/ \mathrm{cm}^{2}$ |
|  | $10^{5}$ Ampere/m $\mathrm{m}^{2}$ | 1 Abempere/ $/ \mathrm{cm}^{2}$ | $3 \times 10^{10}$ Statampera $/ \mathrm{cm}^{2}$ |
|  | $1 / 3 \times 10^{-5}$ Ampera/m ${ }^{2}$ | $1 / 3=10-10$ Abampera $/ \mathrm{cm}^{2}$ | 15 thempera/em ${ }^{2}$ |
| 7. Electric field intenxity | $1 \mathrm{Voli} / \mathrm{moter}$ | $10^{6} \mathrm{Abvalh} / \mathrm{cm}$ | $1 / 3=10-4$ Stativalt/em |
|  | 10-6 Volt/moter | 1 Abrolt/cm | $1 / 3 \times 10-10$ Statralt/sm |
|  | 3 $404 \mathrm{Valt} / \mathrm{meler}$ | $3 \times 10^{10} \mathrm{Abrolt} / \mathrm{cm}$ | 15 tatrolt/ $/ \mathrm{cm}$ |
| 8. Electrie potantial | 1 Velt | $10^{10}$ Abvolts | $1 / 3=10^{-2}$ Stetralts |
|  | 10-8 Valt | 1 Abvolt | $1 / 3 \pm 10-10$ Stetrolin |
|  | $3 \times 10^{2} \mathrm{Valt}$ | $3 \times 10^{10}$ Abvelts | 1 Statwolt |
| 9. Electric dipole moment | 1 Coulomb-meter | 10 Abcoulomb-cm | $3 \times 10^{11}$ Statcoulemb-cm |
|  | 10-1 Covlomb-meter | 1 Abesulomb-cm | 3* $10^{10}$ Stetceulemb-cm |
|  | $1 / 3 \times 10^{-11}$ Coulamb-mater | 1/3 $=10-10$ Abceulomb-cm | 1 Stelcoulemb-cm |
| 10. Eneryy | 1 Joule | $10^{7} \mathrm{Ect}$ | $10^{7} \mathrm{Ers}$ |
|  | $100^{-7}$ Joule | 1 Erg | 1 Ere |
|  | 10-7 Jouls | 1 Erg | 1 Erg |
| 11. Farce | 1 Newton | ${ }_{105}{ }^{5}$ Dyne | $10^{5}$ Oyne |
|  | 10-5 Nowton | 1 Dyne | 1 Dyne |
|  | 10-5 Neaton | 1 Dype | 1 Drne |
| 12. Flun density | 1 Weber m2 | $10^{4}$ Gouss | $1 / 3 \times 10-6$ an |
|  | $10^{-4}$ Wober'm ${ }^{2}$ | 1 Gevse | $13 \times 10^{-51700}$ |
|  | $3 \times 10^{\text {d }}$ Weber/m ${ }^{2}$ | $3 \times 10^{19}$ Geusa | 1 esu |
| 12. Induetence | 1 Manry | $10^{9}$ Abhenry | 1/9 = 10-11 stathenry |
|  | $10-9$ Henry | 1 Abhenry | $1 / 9.10-20$ Stathenry |
|  | 9 a $10^{11}$ Menry | $9 \times 10^{20}$ Athenty | 1 Stathenry |
| 14. Inductive copecity | 1 Forod/meter | $10-11 \mathrm{Ab}$ lorad/cm | $9=12^{9} 5$ tenfered. cm |
|  | $10^{11}$ Fared mater | 1 Ablered/cm | $9 \times 1020$ Statfored cm |
|  | 1/9 $\times 10-9$ Fored/meter | $1 / 9 \times 10-20 \mathrm{Abferad} / \mathrm{cm}$ | 1 statfered/em |
| 15. Magnetice flux | 1 Weber | $10^{8}$ mexwell | 1/3 $\times 10-2$ enu |
|  | 10-8 Weber | 1 Maswoll | $1 / 3 \times 10-10^{\text {ax }}$ |
|  | $3 \times 10^{2}$ Weber | $3 \times 10^{10}$ maxwell | 1.00 |
| 16. Mognutic dipelo mament | 1 Ampere-meter ${ }^{2}$ | $10^{3}$ Abomp-cm ${ }^{2}$ | $3 \times 10^{13}$ Stetemp-cm ${ }^{2}$ |
|  | 10-3 Ampere-mener ${ }^{2}$ | 1 Aboemp-cm ${ }^{2}$ | $3 \times 1010$ Stotomp- $\mathrm{cm}^{2}$ |
|  | $1 / 3 \times 10-12$ Ampere-menter ${ }^{2}$ | 1 $1.3 \times 10-10$ Abemp-cm ${ }^{2}$ | 15 tetamp-cm ${ }^{2}$ |
| 17. Permesbility | 1 Hency mater | $10^{7}$ Abhenry om | $1 / 20 \cdot 10^{-13}$ Stathenry cm |
|  | $10^{-7}$ Manry metar | 1 Abhenry cm | $1 / 9.10-20$ Siathenry - mm |
|  | $9 \times 10^{13} \mathrm{Hency}$ meter | $9 \times 10^{20}$ Alhenry cm | 1 Stothency cm |
| 18. Pawer | 1 Woll | $10^{7}$ erg/zec | $10^{7}$ era/uec |
|  | 10-7 Wett | 1 wi nec | 1 erg/ses |
|  | $10^{-7}$ wout | 1 erg sec | 1 ars/aec |
| 19. Resistence | 10 hm | $10^{9}$ Abehm | $19.10-11_{\text {stetahm }}$ |
|  | $10^{-9} 9 \mathrm{hm}$ | 1 Ahehm - | 1/9: $10-20$ Steratem |
|  | Q $\cdot 100^{11} 0 \mathrm{~mm}$ | $0=10^{20} \mathrm{Abohm}$ | 1 Statahm |

## SPACE-TIME-VELOCITY AND ACCELERATION FORMULAS

This tabulation presents all basic linear motion formulas with all their variations. Terms are defined and units of measurement are specified.
A = Acceleration or deceleration- $\mathrm{ft} / \mathrm{sec} / \mathrm{sec}$ ( 32.2 for gravity)
D = Distance-ft (may be used in lieu of "H" in vertical free fall)
E = Energy-ft-lbs
F = Force-lbs
$\mathrm{H}=$ Height- ft (may be used lieu of " D " with $\mathrm{A}-32.2$ )
$M=$ Mass $\quad \frac{W}{32.2}=\frac{\mathrm{lb}-\mathrm{sec}^{2}}{\mathrm{ft}}$
T = Time-sec
$\mathrm{V}_{\mathrm{a}}=$ Average velocity- $\mathrm{tt} / \mathrm{sec}$
$V_{t}=$ Final velocity- $\mathrm{Ht} / \mathrm{sec}$
$\mathrm{V}_{1}=$ Initial velocity- $\mathrm{t} / \mathrm{sec}$
$\mathrm{W}^{\prime}=$ Weight- bs


| To Convert | Into | Multiply By |
| :---: | :---: | :---: |
| ares | sq meters | 100.0 |
| Astronomical Unit | Kilometers | $1.495 \times 10^{8}$ |
| Atmospheres | Ton/sq. inch | . 007348 |
| etmospheres | cms of mercury | 76.0 |
| atmospheres | ft of water (et $4^{\circ} \mathrm{C}$ ) | 33.90 |
| atmospheres | in. of mercury (et $0^{\circ} \mathrm{C}$ ) | 29.92 |
| atmospheres | kgs/sq cm | 1.0333 |
| atmospheres | kgs/sq meter | 10,332. |
| etmospheres | pounds/sq.in. | 14.70 |
| etmospheres | tons/sq ft | 1.058 |
| B |  |  |
| Berrels (U.S., dry) | cu. inches | 7056. |
| Berrels (U.S., dry) | querts (dry) | 105.0 |
| Barrels (U.S., liquid) | gellons | 31.5 |
| berrels (oil) | gallons (oil) | 42.0 |
| bers | atmospheres | 0.9869 |
| bars | dynes/sq cm | $10^{6}$ |
| bars | kgs/sq meter | $1.020 \times 10^{4}$ |
| bars | pounds/sq ft | 2,089. |
| bars | pounds/sq in. | 14.50 |
| Beryl | Dyne/sq. cm. | 1.000 |
| Bolt (US Cloth) | Meters | 36.576 |
| BTU | Liter-Atmosphere | 10.409 |
| Btu | ergs | $1.0550 \times 10^{10}$ |
| Btu | foot-lbs | 778.3 |
| Btu | gram-celories | 252.0 |
| Btu | horsepower-hrs | $3.931 \times 10^{-4}$ |
| Btu | joules | 1,054.8 |
| Btu | kilogrem-calories | 0.2520 |
| Btu | kilogrem-meters | 107.5 |
| Btu | kilowatt-hrs | $2.928 \times 10^{-4}$ |
| Btu/hr | foot-pound/sec | 0.2162 |
| Btu/hr | grem-cel/sec | 0.0700 |
| Btu/hr | horsepower-hrs | $3.929 \times 10^{-4}$ |
| Btu/hr | wetts | 0.2931 |



To Convert
Abcoulomb䓘 는 는
$\stackrel{4}{4}$岕
 amperes/sq cm amperes/sq in.
 emperes/sq meter ampere-hours ampere-hours . ampere-turns/cm ampere-turns $/ \mathrm{cm}$ ampere-turns/cm ampere-turns/in. empere-turns/in. ampere-turns/in. ampere-turns/meter ampere-turns/meter ampere-turns/meter Angstrom unit Angstrom unit Angstrom unit



To Convert
cubic centimeters
cubic centimeters
cubic centimeters
cubic centimeters
cubic feet
cubic feet
cubic feet
cubic feet
cubic feet
cubic feet
cubic feet
cubic feet
cubic feet
cubic feet/min
cubic feet/min
cubic feet/min
cubic feet/min
cubic feet/sec
cubic feet/sec
cubic inches
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cubic inches
cubic inches
cubic meters
cubic meters
cubic meters
cubic meters
cubic meters
cubic meters
cubic meters
cubic metersMultiply By

12.96
0.02356
0.01757
17.57
0.1221
$1.818 \times 10^{4}$
1.2445
$2,150.4$
0.03524
35.24
4.0
64.0
32.0

| To Convert | Into |
| :---: | :---: |
| 8tu/min | foot-lbs/sec |
| 8tu/min | horsepower |
| 8tu/min | kilowatts |
| $8 \mathrm{tu} / \mathrm{min}$ | watts |
| $8 \mathrm{tu} / \mathrm{sq} \mathrm{ft} / \mathrm{min}$ | watts/sq in. |
| 8ucket (8r. dry) | Cubic Cm. |
| bushels | cu ft |
| bushels | cu in. |
| bushels | cu meters |
| bushels | liters |
| bushels | pecks |
| bushels | pints (dry) |
| bushels | quarts (dry) |
|  | C |
| Calories, gram (meen) centares (centiares) | B.T.U. (mean) sq meters |
| Centigrade (Celsius) | Fehrenheit |
| Centigrams | grams |
| Centiliter | Ounce fluid (US) |
| Centiliter | Cubic inch |
| Centiliter | drams |
| centiliters | liters |
| centimeters | feet |
| centimeters | inches |
| centimeters | kilometers |
| centimeters | meters |
| centimeters | miles |
| centimeters | millimeters |
| centimeters | mils |
| centimeters | yards |
| centimeter-dynes | cm-grams |
| centimeter-dynes | meter-kgs. |
| centimeter-dynes | pound-feet |
| centimeter-grams | cm-dynes |
| centimeter-grems | meter-kgs |






pound-feet
atmospheres
feet of water
$\mathrm{kgs} / \mathrm{sq}$ meter
pounds/sq ft
pounds/sq in.
feet/min
feet/sec
kilometers/hr
knots
meters/min
miles/hr
miles/min
feet/sec/sec
$\mathrm{kms} / \mathrm{hr} / \mathrm{sec}$
meters/sec/sec
miles/hr/sec
Inches
meters
yards
sq cms
sq mils
Radians
sq inches
cord feet
cu feet
Statcoulombs
faradays
coulombs/sq in.
coulombs $/ \mathrm{sq} \mathrm{meter}$
coulombs/sq cm
coulombs/sq meter
coulombs/sq cm
coulombs/sq in.
cu feet
cu inches
cu meters
cu yards


| To Convert | Into | Multiply By |
| :---: | :---: | :---: |
| foot－pounds | ergs | $1.356 \times 10^{7}$ |
| foot－pounds | gram－calories | 0.3238 |
| foot－pounds | hp－hrs | $5.050 \times 10^{-7}$ |
| foot－pounds | joules | 1.356 |
| foot－pounds | kg－calorias | $3.24 \times 10^{-4}$ |
| foot－pounds | kg－meters | 0.1383 |
| foot－pounds | kilowatt－hrs | $3.766 \times 10^{-7}$ |
| foot－pounds／min | Btu／min | $1.286 \times 10^{-3}$ |
| foot－pounds／min | foot－pounds／sec | 0.01667 |
| foot－pounds／min | horsepower | $3.030 \times 10^{-5}$ |
| foot－pounds／min | kg－calories／min | $3.24 \times 10^{-4}$ |
| foot－pounds／min | kilowatts | $2.260 \times 10^{-5}$ |
| foot－pounds／sec | Btu／hr | 4.6263 |
| foot－pounds／sec | Btu／min | 0.07717 |
| foot－pounds／sec | horsepower | $1.818 \times 10^{-3}$ |
| foot－pounds／sec | kg－celories／min | 0.01945 |
| foot－pounds／sec | kilowetts | $1.356 \times 10^{-3}$ |
| Furlongs | milas（U．S．） | 0.125 |
| furlongs | rods | 40.0 |
| furlongs | feet | 660.0 |
|  | G |  |
| gallons | cu cms | 3，785．0 |
| gallons | cu feet | 0.1337 |
| gellons | cu inches | 231.0 |
| gallons | cu metars | $3.785 \times 10^{-3}$ |
| gallons | cu yards | $4.951 \times 10^{-3}$ |
| gallons | liters | 3.785 |
| gallons（liq．Br．Imp．） | gellons（U．S．liq．） | 1.20095 |
| gellons（U．S．） | gallons（Imp．） | 0.83267 |
| gallons of water | pounds of water | 8.3453 |
| gellons／min | cu ft／sec | $2.228 \times 10^{-3}$ |
| gallons／min | liters／sec | 0.06308 |
| gallons／min | $\mathrm{cu} \mathrm{ft/hr}$ | 8.0208 |
| gausses | lines／sq in． | $6.452{ }^{-8}$ |
| gausses | wabers／sq cm | $10^{-8}$ |

## Multiply By



 Inch of Marcury at $0^{\circ} \mathrm{C}$ Inch of Marcury at $0^{\circ} \mathrm{C}$
Inch of Watar at $4^{\circ} \mathrm{C}$ grams grams
joules $/ \mathrm{cm}$ joulas／meter（newtons） kilograms poundals詋哙

E
 gram－csiories
gram－cms horsepower－hrs joules kg －calories kg－meters kilowatt－hrs watt－hours Btu／min ft － $\mathrm{lbs} /$ min $\mathrm{ft}-\mathrm{lbs} / \mathrm{sec}$ horsepower kg －calories／min kilowatts

To Convert Dyna／sq． cm ．
Dyne／sq． cm ．
dynes
dynes
dynes
dynes
dynes
dynnes
dynes／sq cm产 $\overline{\bar{w}}$ ：
范
世氾朢总 ${ }^{\circ}$苞总
 $\stackrel{8}{6}$㤐 ergs／sec ergs／sec ergsas sec ergs／sec args／sec

[^1]<1
msac
EMucentus livm 60 ta 70% is 10W sinet
Whth nem magnot matarilis, can dativer high palk
penver (herugomer a,gol)

``` & \begin{tabular}{l}
For fuli ranta of: inampensiva, qwed-performance Srive and cantrol applicolisas \\
Weth apprapiata anvusnmeatal precovtipas, saft. abie ter military/aersseact ase \\
Praterod as a hish performance, geneial.-gupese serve matore
\end{tabular} \\
\hline  & \begin{tabular}{l}
Wa commutater wear ar frictop \\
Ualimited lite \\
Intiesta masadotion. \\
Smoeth, cot-trey rolatish \\
No EW zeneration \\
Avilable is moter alemints or fally heused
\end{tabular} & \begin{tabular}{l}
Travel ramag typically ta \(120^{\circ}\) \\
Torese trom a low at-ut to \(>40 \mathrm{Ht}-\mathrm{Ht}\) \\
Mochanical tume comstaals trom it ta 50 mioc
\end{tabular} &  over a limitod angla \\
\hline  & \begin{tabular}{l}
Slow mpend. Miţh terque. \\
Redativily low powes estent \\
Availatie as pancale-shaped componesits. \\
Whice dyemic retga \\
Large samber of cowis give smoth aperation.
\end{tabular} & From 10's of ex-ia ta 100 's an M.llo Moderata machanical time constants Contred to secondis are. Elintively eqpomion & Fow durect couplag it loed Fex wry pacise contion Almastive to suted types \\
\hline  (invicess mitear & Similer to permasent-megart \&c sails Liment tow 4 we-spewd charectonstics Smeeth, sencergise rowation Handles wey migh, short-Antation peak loeds. Fast repansio \ll 10 mucl! & \begin{tabular}{l}
Outputs from <1W is tractional hersepower. \\
High efficiencies \\
Yey low mechanceal and alictrical tima comutants
\end{tabular} & \begin{tabular}{l}
Compoter penphersls melera smoch control and last ratponse are abeded \\
Conterif applicatiens needing bigh response band midh. last storting ond steppers
\end{tabular} \\
\hline  & \begin{tabular}{l}
Arusthess and rutted \\
High stapereef rita deppendent on drive cricesity \\
 \\
Pow interent damplet \\
Lom powe ellicients. \\
Con manibl resemance \\
Operates dem heep \\
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& \text { now be }
\end{aligned}
\] & ese motas usint newly dereleged. very hith aneety ia in compact integrat holsepower sulas with very high pa & th mapnets can verland ciegability \\
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\end{tabular} & Stiff bruct coupling to load gellored nwi ampi gerterid for high cominil power \\
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 moter fetiamiass respanase limets Oampang mended by divisif slectronics Sinple tow-cost atherastive to listsr peationers in positioning llopprwist masts \\
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Lsod inertis ratuctes performance \\
Fiction can improwe damping \\

\end{tabular} \\
\hline \begin{tabular}{l}
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Sandard drwess avaliable.
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\end{tabular} & Las athoedt thantrue brushle:12 motors using olectropic commutation Wora comples, apeniwe ant notsier than bevsh-hpe de meturs Lass surtable fer contred than ofther ac hass Very long Mfe with propecily designod inyeris & \begin{tabular}{l}
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\end{tabular} & \begin{tabular}{l}
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\end{tabular} & \begin{tabular}{l}
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dampang is unrelasble and networl damping difititutfle apply \\
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Wein field-capacifor phase shit anly canvenent in vary a mall motons \\
Wain field pewer heeps units hot even while ithing
\end{tabular} \\
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Less huming than efther types of synthronsus motors \\
Simpler than platilloch dives
\end{tabular} & \begin{tabular}{l}
High efficiencies important for cempule applications \\
Leo powe factors ined ta higb inpot courents \\
Hightr power facton swalable in singte-phase capactor werswas \\
Sensitive to input harmencics \\
Can eccelerate high-inetia isads \\
Does not have a preferted syachicemiation angle
\end{tabular} \\
\hline \multicolumn{3}{|c|}{These t, pes have low totoc theinal capacities To asuge ine hem nase if takes about 200w ts rase the temperature ci a I-18 armature ty I"C in in set Other values can be suitabiy prepettioned} \\
\hline
\end{tabular}
FAMILY TREE OF ELECTRIC MOTORS

Device Average Rating (Watts)
Air Cleaner ..... 50
Air Conditioner (room) ..... 1,500
Blender ..... 390
Broiler ..... 1,450
Carving Knife ..... 100
Clock ..... 2
Clothes Dryer ..... 4,850
Coffee Maker ..... 900
Deep Fryer ..... 1,450
Dehumidifier ..... 250
Dishwasher ..... 1,200
Electric Blanket ..... 175
Fan:
attic ..... 370
fumace ..... 290
window ..... 200
Floor Polisher ..... 300
Freezer:
( \(14 \mathrm{cu} . \mathrm{ft}\) ) ..... 340
(frostless - \(15 \mathrm{cu} . \mathrm{ft}\) ) ..... 440
Frying Pan ..... 1,200
Heater (portable) ..... 1,320
Heating Pad ..... 65
Hot Plate ..... 1,250
Humidifier ..... 175
Iron (Hand) ..... 1,000
Microwave Oven ..... 1,450
Mixer ..... 125
Oil Burner (stoker) ..... 265
Radio ..... 70
Radio/Record Player ..... 100
Range with oven ..... 12,200
Refrigerator:
300
( \(12 \mathrm{cu} . \mathrm{ft}\) )
390
(frostless, \(12 \mathrm{cu} . \mathrm{ft}\) )
Refrigerator /Freezer: ..... 
352 ..... 
352
( \(14 \mathrm{cu} . \mathrm{ft}\) )
( \(14 \mathrm{cu} . \mathrm{ft}\) )
600
600
Roaster ..... 1,300
Sandwich Grill ..... 1,150
Sewing Machine ..... 75
Television:
black and white:
tube type ..... 160
solid state ..... 55
color TV:
tube type ..... 300
solid state ..... 200
Toaster ..... 1,150
Trash Compactor ..... 400
Vacuum Cleaner ..... 630
Waffle Iron ..... 1,100
Washing Machine: automatic ..... 500
nonautomatic ..... 280
Waste Disposer ..... 440
Water Heater:
standard ..... 2,475
quick recovery ..... 4,475
Water Pump ..... 460

\section*{NOMOGRAM RELATING AMPLITUDE, FREQUENCY, AND ACCELERATION OF A BODY WITH SIMPLE HARMONIC MOTION}

This nomogram is based on the formula
\[
g=0.10225(d)(f)^{2}
\]
where
\(g=\) acceleration in g-units
\(f=\) frequency of vibration in cps
\(d=\) amplitude of vibration (peak displacement each side of resting point) in inches
FOR EXAMPLE: A vibrating body with a displacement of 0.01 in . each side of center at 200 Hz , has an acceleration of 40 g 's.

NOTE: To find the acceleration in a rotating body resulting from centrifugal force, substitute radius of rotation for amplitude (d), and revolutions per second for vibrations per second ( \(f\) ). \(g=32 \mathrm{ft} / \mathrm{sec} / \mathrm{sec}\) in the MKS system of units.


\section*{SHOCK DECELERATION NOMOGRAM}

This nomogram relates deceleration ( G load), stopping distance, and drop height as an aid to designers and engineers who must deal with problems of shock caused by violent or sudden deceleration.

The equation used to plot the nomograph is \(\log G=\log g+\log H-\log D\). Relating deceleration ( \(G\) load), stopping distance, and drop height, it is based on the following relationships:
\[
\begin{aligned}
& H=g t^{2} / 2 \\
& D=G T^{\prime 2} / 2 \\
& V_{t}=g t^{\prime \prime} \\
& V_{i}=G t^{\prime \prime}
\end{aligned}
\]
where:
\(H=\) free-fall distance
\(g=\) acceleration due to free fall
\(t=\) free-fall time
\(D=\) stopping or deflection distance
\(G=G\) load due to impact shock
\(t^{\prime}=\) deceleration time
\(V_{t}=\) terminal velocity due to free fall at instant of impact
\(V_{f}=\) initial deceleration velocity at instant of impact
Since at the moment of impact the terminal velocity \(\left(V_{t}\right)\) caused by acceleration is equal to the initial velocity \(\left(V_{1}\right)\), it follows that:
\[
g t=G t^{\prime}
\]

Combining the equations:
\[
H / D=\frac{g t^{2} / 2}{G t^{\prime} 2 / 2}=g t(t) / G t^{\prime}\left(t^{\prime}\right)
\]

Since \(g t=G t^{\prime} H / D=t / t^{\prime}\). Also, since \(G / g=t / t^{\prime}, H / D=G / g\). Transposing, \(G=g(H / D)\) or \(\log G=\log\) \(g+\log H-\log D\). This equation is based on a constant or uniformly decelerating force. For linear deceleration the equation for load distance relationship is: \(G=2 g H / D\).

Neither formula includes the stopping distance as part of the distance traveled because its effect is negligible for small values of stopping distance (D).

FOR EXAMPLE: 1. Find the \(G\) load on a shock-mounted case that endures a \(30-\mathrm{in}\). drop height with a maximum mount deflection of 0.4 in . Assume a rigid case and uniform deceleration in the mount.

ANSWER: Intersect impact shock \((\mathrm{G})\) scale with a line connecting the \(30-\mathrm{in}\). drop height with 0.4 in . on the absorber deflection scale. Read answer off impact shock scale. In this example, it is 73G.
2. Find the impact shock on a piece of equipment that is dropped 20 in . on expanded rubber foam gasket. The foam is compressed a total of 0.1 in . and is assumed to have a linear deceleration characteristic.

ANSWER: Intersect the impact shock \((G)\) scale with a line connecting the 20 -in. drop height with 0.1 in. on the absorber deflection scale. Since peak impact shock \((G)\) load due to linear deceleration is approximately twice as severe as that due to uniform deceleration, the value of 200 G obtained is multiplied by 2 for linear deflection. Answer is 400 G .


\section*{AIR-COOLING NOMOGRAM}

For a given power dissipation and air density, this nomogram solves for the air flow (cubic feet per minute) that is required to keep the temperature rise of an equipment at a specified value. At sea level ( 760 mm Hg ), \(0^{\circ} \mathrm{C}\), and an air density of \(0.079 \mathrm{lb} / \mathrm{ft}^{3}\), the temperature rise is approximately equal to \(3,000 P / Q\), where \(P\) is power dissipation in kilowatts and \(Q\) is the air flow in cubic feet per minute.

To use the nomogram first determine the ambient temperature and altitude at which the equipment must operate and note from the graph the applicable air density for these conditions. On the nomogram align the permissible temperature rise with the equipment's power dissipation and note the intersect point on the turning scale. Align this point with the applicable air density and read required air flow in cubic feet per minute on scale \(B\).

FOR EXAMPLE: To operate an equipment with a power consumption of 500 W at sea level, an ambient temperature of \(20^{\circ} \mathrm{C}\), and a permissible heat rise of \(15^{\circ} \mathrm{C}\), requires an air flow of \(50 \mathrm{ft}^{3} / \mathrm{min}\).


METALLIC ELEMENTS
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline Name and Symbol & Color & Atomic Weight & Specific Gravity or Density & Specific Heat & Meltingpoint ( \({ }^{\circ} \mathrm{Celsin}\) ) & Coefficient of Linear Expansion \\
\hline  &  &  &  &  &  & \begin{tabular}{l}
00000231 0000003105
0.0000055 \\
\(\overline{0000014}\) \\
\(\overline{0} 000087\) \\
-0000ess \\
\(\overline{0} 0000121\) \\
00000167 \\
\(]_{00000167}\) \\
00000136 \\
00000065
0.000118 \\
0000027 \\
\(\overline{0} 0000859\) \\
0.0000010 \\
-0000127 \\
00000085
00000117 \\
00000069
0000081 \\
-000000es \\
00000096 \\
00000192
0000071 \\
-00000079
00000187 \\
00000002 \\
\(\overline{00000 e 0 s}\) \\
\(=\)
\(=\)
\(\overline{0}\)
\(=0000874\)
\end{tabular} \\
\hline
\end{tabular}
(Reprinted from Master Handbook of Electronic Tables \& Formulas by Martin Clifford, courtesy TAB BOOKS, Inc.)

\section*{densities of solids and liquids in cubic centimeters and cubic feet}

\begin{tabular}{|c|c|}
\hline 21.50 g . per cub. cm . & \(1,342.2 \mathrm{lb}\). per cub. \\
\hline Sea Water....................... 1.025 g . per cub. cm . & 64.0 lb , per cub. f . \\
\hline Silver........................... 10.5 g . per cub. cm. & 655.5 lb . per cub. ft. \\
\hline Tin..............................7.18 g . per cub. cm . & 448. lb. per cub. it. \\
\hline Tungsten.....-............-... 16.6 g per cub. cm . & 1,161.2 ib. per cub. ft \\
\hline Uranlum ....-.......-............. 18.7 g . per cub. cm. & 1,167.4 lb. per cub. fi. \\
\hline  & 82.4 lb . per cub. ft. \\
\hline 19 g . per cuib. cm. & 448.6 lb . per cub. fl. \\
\hline
\end{tabular}

Zinc. \(\qquad\) 7.19 g . per cub. cm. 448.8 lb . per cub. it

\section*{SOLDER ALLOYS}

The term solder alloys covers a broad range of materials with greatest emphasis placed on compositions of tin and lead. The tin lead system of alloys has a general solidus temperature of \(361^{\circ} \mathrm{F}\). The eutectic composition, the alloy with a single sharp melting point and no plastic range, is \(63 \%\) tin, \(37 \%\) lead. This alloy is in widest use in the electronic industry.

The specific tin lead alloy selected is determined by the nature of the joining operation and the degree to which a plastic or "mushy" solder state can be tolerated or is desirable. Tin lead alloys with a tin content from 20\% up through and including \(97.5 \%\) have the same \(361^{\circ} \mathrm{F}\) solidus line. Alloys containing lower percentages of tin have an increased solidus temperature. This is also true of tin antimony, tin silver, and lead silver alloys. The higher solidus line permits operation of the soldered part in higher ambient temperatures. It also permits sequential or piggy-back soldering. Where two soldering connections are to be made in areas very close to each other, the first joint can be made with one of the high-temperature alloys. When the second joint is made with an alloy in the normal tin lead system, the first joint will not be disturbed.
\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline & & & & \multicolumn{2}{|l|}{Tempereture ot which Solder Becomes Plastic} & \multicolumn{2}{|l|}{Temperature et which Solder Becomes Liquid} \\
\hline Percent Tin & Parcent Lead & Percent Silver & Percent Antimony & \({ }^{\circ} \mathrm{C}\) & \({ }^{\circ} \mathrm{F}\) & \({ }^{\circ} \mathrm{C}\) & \({ }^{\circ} \mathrm{F}\) \\
\hline 0 & 100 & & & & & 327. & 621 \\
\hline 5 & 95 & & & 300 & 572 & 315 & 699 \\
\hline 10 & 90 & & & 267.5 & 514 & 300 & 572 \\
\hline 15 & 85 & & & 223 & 433 & 290 & 554 \\
\hline 20 & 80 & & & 183 & 361 & 280 & 536 \\
\hline 25 & 75 & & & 183 & 361 & 287 & 513 \\
\hline 30 & 70 & & & 183. & 361 & 255 & 491 \\
\hline 35 & 65 & & & 183 & 361 & 245 & 473 \\
\hline 40 & 60 & & & 183 & 361 & 235 & 456 \\
\hline 45 & 55 & & & 183 & 361 & 223 & 433 \\
\hline 50 & 50 & & & 183 & 361 & 212 & 414 \\
\hline 55 & 45 & & & 183 & 361 & 200 & 392 \\
\hline 60 & 40 & & & 183 & 361 & 189 & 372 \\
\hline 83 & 37 & & & *utectic & -170y \({ }^{3}\) & \({ }^{183}\) & 361 \\
\hline 65 & 35 & & & 183 & 361 & 186 & 367 \\
\hline 70 & 30 & & & 183 & 361 & 191 & 376 \\
\hline 75 & 25 & & & 183 & 361 & 195 & 383 \\
\hline 80 & 20 & & & 183 & 361 & 201 & 394 \\
\hline 85 & 15 & & & 183 & 361 & 207 & 404 \\
\hline 90 & 10 & & & 183 & 361 & 214 & 417 \\
\hline 95 & 5 & & & 183 & 361 & 222 & 432 \\
\hline 97.5 & 2.5 & & & 183 & 361 & 227 & 441 \\
\hline 100 & 0 & & & & & 232 & 460 \\
\hline 35 & 63 & & 2 & 187 & 389 & 237 & 459 \\
\hline 20 & 78.7 & 1.3 & & 181 & 358 & 276 & 529 \\
\hline 27 & 70 & \[
3
\] & & 178 & 352 & 263 & 487 \\
\hline & 95 & 5 & & 305 & 581 & 360 & 680 \\
\hline
\end{tabular}
\({ }^{8}\) A sutectic slloy is that composition of two or mors metals that hes one sherp melting point and no plastic range.


\section*{TRACK WIDTH OF PRINTED WIRING BOARDS}

The two graphs are used to determine the current-carrying capacity and sizes of etched copper conductors (tracks) for various temperature rises above ambient. To use the charts, enter the top chart from the left at the current value which is anticipated, to the point where it interrupts the applicable copper temperature-rise curve. Then, proceed vertically down to the second chart to the appropriate weight (the weight of one square foot of copper of a given thickness) slanted line, and proceed left to determine the minimum track width.

FOR EXAMPLE: To carry 10 amperes and not exceed a \(20^{\circ} \mathrm{C}\) rise above ambient requires a 0.100 -inch wide conduct of 2-ounce copper track.

*Based on \(1 / 16\) inch boards. For thicker boards, derate by \(15 \%\).

\section*{DEFINED VALUES AND PHYSICAL CONSTANTS}

A consistent set of physical values has been adapted by the National Bureau of Standards. The values presented below are at least as accurate as any others available, and have the advantage of being self-consistent, thus preventing the necessity of having to make a choice between different answers derived in different ways.

Fundamental Constants

Compiled by E. R. Cohen and B. N. Taylor under the auspices of the CODATA Task Group on Fundamental Constants. This set has been officially adopted by CODATA and is taken from J. Phys. Chem. Ref. Data, Vol. 2, No. 4, p. 663 (1973) and CODATA Bulletin No. 11 (December 1973).
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline Quenthy & Symbol & Numarical value* Un & Uncerth (ppm) & S1t & \(\leftarrow\) Units \(\rightarrow\) & cs: \(\ddagger\) \\
\hline Speed of light in vacuum & c & 299792458(1.2) & 0.004 & \(\mathrm{m} \cdot \mathrm{s}^{-1}\) & & \(10^{3} \mathrm{~cm} \cdot \mathrm{~s}^{-1}\) \\
\hline Permeability of vacuum & \(\mu_{0}\) & \[
\stackrel{4 \pi}{=} 12.5663706144
\] & & \[
\begin{aligned}
& 10^{-1} \mathrm{H} \cdot \mathrm{~m}^{-1} \\
& 10^{-7} \mathrm{H} \cdot \mathrm{~m}^{-1}
\end{aligned}
\] & & \\
\hline Permittivity of vacuum,
\[
1 / \mu_{0} c^{2}
\] & \(\epsilon_{0}\) & 8.854187818(71) & 0.008 & \(10^{-11} \mathrm{~F} \cdot \mathrm{~m}^{-1}\) & & \\
\hline Fine-structure constant, \(\left[\mu_{0} c^{2} / 4 \pi\right]\left(e^{3} \hbar c\right)\) & \({ }^{\text {a }}\) & \[
\begin{gathered}
7.2973506(60) \\
137.03604(11)
\end{gathered}
\] & \[
\begin{aligned}
& 0.82 \\
& 0.82
\end{aligned}
\] & \(10^{-1}\) & & \(10^{-2}\) \\
\hline Elementary charge & e & \[
\begin{aligned}
& 1.6021892(46) \\
& 4.803242(14)
\end{aligned}
\] & \[
\begin{aligned}
& 2.9 \\
& 2.9
\end{aligned}
\] & \(10^{-13} \mathrm{C}\) & & \[
\begin{aligned}
& 10^{-14} \text { emu } \\
& 10^{-16} \text { esu }
\end{aligned}
\] \\
\hline Planck constant & \[
\begin{aligned}
& n \\
& n=h / 2 \pi
\end{aligned}
\] & \[
\begin{aligned}
& 6.626176(36) \\
& 1.0545887(57)
\end{aligned}
\] & \[
\begin{aligned}
& 5.4 \\
& 5.4
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-24} \mathrm{~J} \cdot \mathrm{~s} \\
& 10^{-34} \mathrm{~J} .5
\end{aligned}
\] & & \[
\begin{aligned}
& 10^{-27} \mathrm{erg} \cdot \mathrm{~s} \\
& 10^{-27} \mathrm{erg} \cdot \mathrm{~s}
\end{aligned}
\] \\
\hline Avogadro constant & \(\mathrm{N}_{\text {A }}\) & \(6.022045(31)\) & 5.1 & \(10^{11} \mathrm{~mol}^{-1}\) & & \(10^{13} \mathrm{~mol}^{-1}\) \\
\hline Atomic mass unit, \(10^{-3} \mathrm{~kg} \cdot \mathrm{~mol}^{-1} \mathrm{~N}_{\mathrm{A}}{ }^{-1}\) & u & \(1.6605655(86)\) & 5.1 & \(10^{-27} \mathrm{~kg}\) & & \(10^{-24} \mathrm{~g}\) \\
\hline Electron rest mass & m 。 & \[
\begin{aligned}
& 9.109534(47) \\
& 5.4858026(21)
\end{aligned}
\] & \[
\begin{aligned}
& 5.1 \\
& 0.38
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-11} \mathrm{~kg} \\
& 10^{-4} \mathrm{u}
\end{aligned}
\] & & \[
\begin{aligned}
& 10^{-21} \mathrm{~g} \\
& 10^{-4} \mathrm{u}
\end{aligned}
\] \\
\hline Proton rest mass & \(m\), & \[
\begin{aligned}
& 1.6726485(86) \\
& 1.007276470(11)
\end{aligned}
\] & 5.1 & \[
u^{10^{-21} \mathrm{~kg}}
\] & & \[
{ }_{4}^{10-24} \mathrm{~g}
\] \\
\hline Ratio of proton mass to electron mass & \(m_{p} / m_{e}\) & 1836.15152(70) & 0.38 & & & \\
\hline Neutron rest mass & \(m_{n}\) & \[
\begin{aligned}
& 1.6749543(86) \\
& 1.008665012(37)
\end{aligned}
\] & \[
\begin{aligned}
& 5.1 \\
& 0.037
\end{aligned}
\] & \[
\mathrm{u}^{10^{-21} \mathrm{~kg}}
\] & & \[
{ }_{u}^{10^{-14} \mathrm{~g}}
\] \\
\hline Electron charge to mass ratio & \(e / m_{r}\) & \[
\begin{aligned}
& 1.7588047(49) \\
& 5.272764(15)
\end{aligned}
\] & \[
\begin{aligned}
& 2.8 \\
& 2.8
\end{aligned}
\] & \(10^{11} \mathrm{C} \cdot \mathrm{kg}{ }^{1}\) & &  \\
\hline Magnetic flux quantum, \([c]^{-1}(h c / 2 e)\) & \[
\Phi_{i n}{ }_{n}
\] & \[
\begin{aligned}
& 2.0678506(54) \\
& 4.135701(11) \\
& 1.3795215(36)
\end{aligned}
\] & \[
\begin{aligned}
& 2.6 \\
& 2.6 \\
& 2.6
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-16} \mathrm{~Wb} \\
& 10^{-11} \mathrm{~J} \cdot \mathrm{~s} \cdot \mathrm{C}^{-1}
\end{aligned}
\] & & \[
\begin{aligned}
& 10^{-1} \mathrm{G} \cdot \mathrm{~cm}^{2} \\
& 10^{-1} \mathrm{erg} \cdot{ }^{-1} \cdot{ }^{-1} \mathrm{erg} \cdot \mathrm{emu} \\
& 0^{-17} \mathrm{eg} \cdot \mathrm{~s} \cdot \mathrm{esu}{ }^{-1}
\end{aligned}
\] \\
\hline Josephson frequencyvoltage ratio & 2e/h & 4.835939(13) & 2.6 & \(10^{14} \mathrm{~Hz} \cdot \mathrm{~V}^{-1}\) & & \\
\hline Quantum of circulation & \[
\begin{aligned}
& h / 2 m_{\psi} \\
& h / m_{\psi}
\end{aligned}
\] & \[
\begin{aligned}
& 3.6369455(60) \\
& 7.273891(12)
\end{aligned}
\] & 1.6 & \[
\begin{aligned}
& 10^{-4} \mathrm{~J} \cdot \mathrm{~s} \cdot \mathrm{~kg}^{-1} \\
& 10^{-4} \mathrm{~J} \cdot 5 \cdot \mathrm{~kg}^{-1}
\end{aligned}
\] & & \[
\begin{aligned}
& \mathrm{erg} \cdot \mathrm{~s} \cdot \mathrm{~g}^{-1} \\
& \mathrm{erg} \cdot \mathrm{~s} \cdot \mathrm{~g}^{-1}
\end{aligned}
\] \\
\hline Faraday constant, \(\mathrm{N}_{\wedge} \mathrm{e}^{\text {e }}\) & F & \[
\begin{aligned}
& 9.648456(27) \\
& 2.8925342(82)
\end{aligned}
\] & \[
\begin{aligned}
& 2.8 \\
& 2.8
\end{aligned}
\] & \(10^{4} \mathrm{C}^{\mathrm{mol}}{ }^{-1}\) & & \(10^{2}\) emu \(\cdot \mathrm{mol}^{-1}\) \(10^{14}\) esu \(\cdot \mathrm{mol}^{-1}\) \\
\hline Rydberg constant,
\[
\left[\mu_{0} c^{2} / 4 \pi\right]^{2}\left(m_{e} e^{2} / 4 \pi n^{7} c\right)
\] & \(\mathrm{R}_{\boldsymbol{x}}\) & \(1.097373177(83)\) & 0.075 & \(10^{\prime} \mathrm{m}^{-1}\) & & \(10^{1} \mathrm{~cm}^{-1}\) \\
\hline Böhr radius,
\[
\left[\mu_{0} c^{1} / 4 \pi\right]^{-1}\left(n^{2} / m_{e} e^{2}\right)=a / 4 \pi R_{a}
\] & \({ }_{\text {a }}^{11}\) & \(5.2917706(44)\) & 0.82 & \(10^{-11} \mathrm{~m}\) & & \(10^{-2} \mathrm{~cm}\) \\
\hline Classical electron radius,
\[
\left[\mu_{0} c^{3} / 4 \pi\right]\left(e^{2} / m e c^{2}\right)=a^{3} / 4 \pi R_{\pi}
\] & \(r_{\text {c }}=a \lambda_{C}\) & \(2.8179380(70)\) & 2.5 & \(10^{-11} \mathrm{~m}\) & & \(10^{-13} \mathrm{~cm}\) \\
\hline Thomson cross section, \((8 / 3) \pi r_{e}{ }^{2}\) & \(\sigma_{\text {c }}\) & 0.6652448 (33) & 4.9 & \(10^{-11} \mathrm{~m}^{2}\) & & \(10^{-24} \mathrm{~cm}^{1}\) \\
\hline Free electron g -factor, or & \(\mathrm{g}_{4} / 2=\mu\) & \(1.0011596567(35)\) & 5) 0.0035 & & & \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|c|c|c|}
\hline Quantity & Symbol & Numerical Value * U & Uncert. (ppm) & SIt + - Units \(\rightarrow\) & - \(\cos 7\) \\
\hline Free muon g-factor, or muon magnetic moment in units of \([c]\left(e n / 2 m_{\mu} c\right)\) & \(\mathrm{g}_{\mu} / 2\) & \(1.00116616(31)\) & 0.31 & & \\
\hline \multirow[t]{2}{*}{Bohr magneton, \([\mathrm{c}](\mathrm{en} / 2 \mathrm{~m}, \mathrm{c}\) )
Electron magnetic moment} & \(\mu_{B}\) & \(9.274078(36)\) & 3.9 & \(10^{-34} \mathrm{~J} \cdot \mathrm{~T}^{-1}\) & \(10^{-11} \mathrm{erg} \cdot \mathrm{G}^{-1}\) \\
\hline & \(\mu_{*}\) & \(9.284832(36)\) & 3.9 & \(10^{-34} \mathrm{~J} \cdot \mathrm{~T}-1\) & \(10^{-31} \mathrm{erg} \cdot \mathrm{G}^{-1}\) \\
\hline Gyromagnetic ratio of protons in \(\mathrm{H}_{2} \mathrm{O}\) & \(\gamma^{\prime}\)
\(\gamma^{\prime} / 2 \pi\) & \[
\begin{aligned}
& 2.6751301(75) \\
& 4.257602(12)
\end{aligned}
\] & \[
\begin{aligned}
& 2.8 \\
& 2.8
\end{aligned}
\] & \[
\begin{array}{ll}
10^{2} & \mathrm{~s}^{-1} \cdot \mathrm{~T}^{-1} \\
10^{+} & \mathrm{Hz} \cdot \mathrm{~T}^{-1}
\end{array}
\] & \[
\begin{aligned}
& 10^{4} \mathrm{~s}^{-1} \cdot \mathrm{G}^{-1} \\
& 10^{1} \mathrm{~Hz} \cdot \mathrm{G}^{-1}
\end{aligned}
\] \\
\hline \(\gamma_{\text {, }}^{\prime}\), corrected for diamagnetism of \(\mathrm{H}_{2} \mathrm{O}\) & \(\gamma_{n} / 2 \pi\)
\(\gamma_{n} / 2 \pi\) & \[
\begin{aligned}
& 2.6751987(75) \\
& 4.257711(12)
\end{aligned}
\] & \[
\begin{aligned}
& 2.8 \\
& 2.8
\end{aligned}
\] & \[
\begin{aligned}
& 10^{3} \mathrm{~s}^{-1} \cdot \mathrm{~T}^{-1} \\
& 10^{+} \mathrm{Hz} \cdot \mathrm{~T}^{-1}
\end{aligned}
\] & \[
\begin{aligned}
& 10^{4} \mathrm{~s}^{-1} \cdot \mathrm{G}^{-1} \\
& 10^{4} \mathrm{~Hz} \cdot \mathrm{G}^{-1}
\end{aligned}
\] \\
\hline Magnetic moment of protons in \(\mathrm{H}_{2} \mathrm{O}\) in Bohr magnetons & \(\mu^{\prime} / \mu_{H}\) & \(1.52099322(10)\) & 0.066 & \(10^{-2}\) & \(10^{-3}\) \\
\hline Proton magnetic moment in Bohr magnetons & \(\mu_{s} / \mu_{1}\) & 1.521032209(16) & ) 0.011 & \(0^{-3}\) & \(10^{-1}\) \\
\hline Ratio of electron and proton magnetic moments & \(\mu_{s} / \mu_{\nu}\) & 658.2106880(66) & 0.010 & & \\
\hline \multirow[t]{2}{*}{Proton magnetic moment Magnetic moment of protons in \(\mathrm{H}_{2} \mathrm{O}\) In nuclear magnetons} & \(\mu_{2}\) & 1.4106171 (55) & 3.9 & \(10^{-12} \mathrm{~J} \cdot \mathrm{~T}^{-1}\) & \(10^{-11}\) erg. \({ }^{-1}\) \\
\hline & \(\mu^{\prime}{ }_{\nu} / \mu_{n}\) & 2.7927740 (11) & 0.38 & & \\
\hline \(\mu^{\prime}, / \mu_{\mathrm{N}}\) corrected for diamagnetism of \(\mathrm{H}_{2} \mathrm{O}\) & \(\mu_{v} / \mu_{0}\) & 2.7928456(11) & 0.38 & & \\
\hline Nuclear magneton, [c](en/2m,c) & \(\mu\) & \(5.050824(20)\) & 3.9 & \(10^{14} \mathrm{~J} \cdot \mathrm{~T}^{-1}\) & \(10^{-14}\) erg. \(\mathrm{G}^{-1}\) \\
\hline Ratio of muon and proton magnetic moments & \(\mu_{\mu} / \mu_{\nu}\) & \(3.1833402(72)\) & 2.3 & & \\
\hline Muon magnetlc moment & \({ }_{\mu}\) & 4.490474(18) & 3.9 & \(10^{-21} \mathrm{~J} \cdot \mathrm{~T}^{-1}\) & \(10^{-31}\) org. \(\mathrm{G}^{-1}\) \\
\hline Ratio of muon mass to electron mass & \(\mathrm{m}_{\mu} / \mathrm{m}_{\sim}\) & \(206.76865(47)\) & 2.3 & & \\
\hline Muon rest mass & \(\mathrm{m}_{\mu}\) & \[
\begin{aligned}
& 1.883566(11) \\
& 0.11342920(26)
\end{aligned}
\] & \[
\begin{aligned}
& 5.6 \\
& 2.3
\end{aligned}
\] & \[
\mathrm{u}^{10^{-23} \mathrm{~kg}}
\] & \[
l_{4}^{10^{-25}} \mathrm{~g}
\] \\
\hline Compton wavelength of the electron, \(h / m_{e} c=a^{2} / 2 R_{x}\) & \[
\begin{aligned}
& \lambda_{\mathrm{C}} \\
& \lambda_{\mathrm{C}}=\lambda_{\mathrm{C}} / 2 \pi=\alpha a_{0}
\end{aligned}
\] & \begin{tabular}{l}
\(2.4263089(40)\) \\
\(3.8615905(64)\)
\end{tabular} & \[
\begin{aligned}
& 1.6 \\
& 1.6
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-13} \mathrm{~m} \\
& 10^{-13} \mathrm{~m}
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-13} \mathrm{~cm} \\
& 10^{-11} \mathrm{~cm}
\end{aligned}
\] \\
\hline Compton wavefength of the proton, \(h / m_{e} \mathrm{c}\) & \[
\begin{aligned}
& \lambda_{\text {C, }} \\
& \pi_{C, r}=\lambda_{C, p} / 2 \pi
\end{aligned}
\] & \[
\begin{aligned}
& 1.3214099(22) \\
& 2.1030892(36)
\end{aligned}
\] & \[
\begin{aligned}
& 1.7 \\
& 1.7
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-15} \mathrm{~m} \\
& 10^{-18} \mathrm{~m}
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-11} \mathrm{~cm} \\
& 10^{-14} \mathrm{~cm}
\end{aligned}
\] \\
\hline Compton wavelength of the neutron, \(h / \mathrm{m}_{\mathrm{n}} \mathrm{c}\) & \[
\lambda_{\mathrm{C}, \mathrm{n}}{ }_{\mathrm{t}_{\mathrm{C}, \mathrm{n}}}=\lambda_{\mathrm{C}, \mathrm{n}} / 2 \pi
\] & \[
\begin{aligned}
& 1.3195909(22) \\
& 2.1001941(35)
\end{aligned}
\] & \[
\begin{aligned}
& 1.7 \\
& 1.7
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-15} \mathrm{~m} \\
& 10^{-13} \mathrm{~m}
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-11} \mathrm{~cm} \\
& 10^{-11} \mathrm{~cm}
\end{aligned}
\] \\
\hline Molar volume of ideal gas at s.t.p. & \(\mathrm{V}_{\mathrm{mb}}\) & \(22.41383(70)\) & 31 & \(10^{-2} \mathrm{~m}^{2} \cdot \mathrm{~mol}^{-1}\) & \(10^{3} \mathrm{~cm}^{1} \cdot \mathrm{~mol}^{-1}\) \\
\hline \multirow[t]{2}{*}{Molar gas constant, \(V_{m} p_{n} / T_{n}\) ( \(T_{0} \equiv 273.15 \mathrm{~K} ; p_{0} \equiv 101325\) \(\mathrm{Pa} \equiv 1 \mathrm{~atm})\)} & \(R\) & \(8.31441(26)\) & 31 & \(\mathrm{J} \cdot \mathrm{mol}^{-1}, \mathrm{~K}^{-1}\) & \(10^{+}\)erg. \(\mathrm{mol}^{-1} \cdot \mathrm{~K}^{-1}\) \\
\hline & & 8.20568(26) & 31 & \(10^{-5} \mathrm{~m}^{2} \cdot \mathrm{~atm} \cdot \mathrm{~mol}^{-1} \cdot \mathrm{~K}^{-1}\) & \(10 \mathrm{~cm}^{2} \cdot \mathrm{~atm} \cdot \mathrm{~mol}^{-1} \cdot \mathrm{~K}^{-1}\) \\
\hline \multirow[t]{2}{*}{\begin{tabular}{l}
Boltzmann constant, \(R / N_{A}\) \\
Stefan-Boltzmann constant,
\[
\pi^{2} k^{4} / 60 \hbar^{3} c^{2}
\]
\end{tabular}} & \(k\) & \(1.380662(44)\) & 32 & \(10^{-38} \mathrm{~J} \cdot \mathrm{~K}^{-1}\) & \(10^{-12}\) erg. \(\mathrm{K}^{-1}\) \\
\hline & \(\sigma\) & \(5.67032(71)\) & 125 & \(10^{-2} \mathrm{~W} \cdot \mathrm{~m}^{-8} \cdot \mathrm{~K}^{-4}\) & \(10^{-5} \mathrm{erg}^{-1} \mathrm{~s}^{-1} \cdot \mathrm{~cm}^{-8} \cdot \mathrm{~K}^{-4}\) \\
\hline First radiation constant, \(2 \pi h c^{2}\) & \(c_{1}\) & \(3.741832(20)\) & 5.4 & \(10^{-18} \mathrm{~W} \cdot \mathrm{~m}^{2}\) & \(10^{-3} \mathrm{erg} \cdot \mathrm{cm}^{2} \cdot \mathrm{~s}^{-1}\) \\
\hline Second radiation constant, hc/k & \(\mathrm{c}_{2}\) & \(1.438786(45)\) & 31 & \(10^{-3} \mathrm{~m} \cdot \mathrm{~K}\) & cm. K \\
\hline \multirow[t]{3}{*}{\begin{tabular}{l}
Gravitational constant Ratio, kx-unit to ângström, \(A=\lambda(A) / \lambda(k x u)\);
\[
\lambda\left(C u K a_{1}\right) \equiv 1.537400 \mathrm{kxu}
\] \\
Ratio, \(\mathrm{A}^{*}\) to ấngström,
\[
\begin{aligned}
& \lambda^{*}=\lambda(A) / \lambda\left(A^{*}\right): \\
& \lambda\left(W K_{a}\right) \equiv 0.2090100 A^{0}
\end{aligned}
\]
\end{tabular}} & G & 6.6720(41) & 615 & \(10^{-11} \mathrm{~m}^{3} \cdot \mathrm{~s}^{-3} \cdot \mathrm{~kg}^{-1}\) & \(10^{-3} \mathrm{~cm}^{3} \cdot \mathrm{~s}^{-3} \cdot \mathrm{~g}^{-1}\) \\
\hline & A & \(1.0020772(54)\) & 5.3 & & \\
\hline & A* & \(1.0000205(56)\) & 5.6 & & \\
\hline
\end{tabular}

\section*{ENERGY CONVERSION FACTORS AND EQUIVALENTS}
\begin{tabular}{|c|c|c|c|c|}
\hline Quantity & Symbol & Numarical Valua* & Units & Uncert. (ppm) \\
\hline 1 kilogram (kg* \({ }^{2}\) ) & & \[
\begin{aligned}
& 8.987551786(72) \\
& 5.609545(16)
\end{aligned}
\] & \[
\begin{aligned}
& 10^{18} \mathrm{~J} \\
& 10^{29} \mathrm{MeV}
\end{aligned}
\] & \[
\begin{aligned}
& 0.008 \\
& 2.9
\end{aligned}
\] \\
\hline 1 Atomic mass unit ( \(\mathrm{u}^{-\mathrm{c}^{2} \text { ) }}\) & & \[
\begin{aligned}
& 1.4924418(77) \\
& 931.5016(26)
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-10} \mathrm{~J} \\
& \mathrm{MeV}
\end{aligned}
\] & \[
\begin{aligned}
& 5.1 \\
& 2.8
\end{aligned}
\] \\
\hline 1 Electron mass m. \(\mathrm{m}^{\left(c^{2}\right)}\) & & \[
\begin{aligned}
& 8.187241(42) \\
& 0.5110034(14)
\end{aligned}
\] & \[
\begin{aligned}
& 10{ }^{H 1} \mathrm{~J} \\
& \mathrm{MeV}
\end{aligned}
\] & \[
\begin{aligned}
& 5.1 \\
& 2.8
\end{aligned}
\] \\
\hline 1 Muon mass ( \(m_{\mu} \cdot{ }^{*}{ }^{2}\) ) & & \[
\begin{gathered}
1.6928648(96) \\
105.65948(35)
\end{gathered}
\] & \[
\begin{aligned}
& 1011 \mathrm{~J} \\
& \mathrm{MeV}
\end{aligned}
\] & \[
\begin{aligned}
& 5.6 \\
& 3.3
\end{aligned}
\] \\
\hline 1 Proton mass ( \(m_{1} \cdot c^{4}\) ) & & \[
\begin{gathered}
1.5033015(77) \\
938.2796(27)
\end{gathered}
\] & \[
\begin{aligned}
& 10^{10} \mathrm{~J} \\
& \mathrm{MeV}
\end{aligned}
\] & \[
\begin{aligned}
& 5.1 \\
& 2.8
\end{aligned}
\] \\
\hline 1 Neutron mass ( \(\mathrm{m}_{\|}{ }^{*} \mathrm{c}^{\text {a }}\) ) & & \[
\begin{aligned}
& 1.5053738(78) \\
& 939.5731(27)
\end{aligned}
\] & \[
\begin{aligned}
& 10^{10} \mathrm{~J} \\
& \mathrm{MeV}
\end{aligned}
\] & \[
\begin{aligned}
& 5.1 \\
& 2.8
\end{aligned}
\] \\
\hline \multirow[t]{4}{*}{1 Electron volt} & & \(1.6021892(46)\) & \[
\begin{aligned}
& 10^{-11} \mathrm{~J} \\
& 10^{-15} \mathrm{erg}
\end{aligned}
\] & \[
\begin{aligned}
& 2.9 \\
& 2.9
\end{aligned}
\] \\
\hline & \(1 \mathrm{eV} / \mathrm{h}\) & 2.4179696 (63) & \(10^{14} \mathrm{~Hz}\) & 2.6 \\
\hline & \(1 \mathrm{eV} / \mathrm{hc}\) & 8,065479(21) & \[
\begin{aligned}
& 10^{5} \mathrm{~m}^{-1} \\
& 10^{3} \mathrm{~cm}^{-1}
\end{aligned}
\] & 2.6
2.6 \\
\hline & \(1 \mathrm{eV} / \mathrm{k}\) & \(1.160450(36)\) & \(10^{4} \mathrm{~K}\) & 31 \\
\hline Voltage wavelength conversion, he & & \[
\begin{aligned}
& 1.986478(11) \\
& 1.2398520(32)
\end{aligned}
\] & \[
\begin{aligned}
& 10^{25} \mathrm{~J} \cdot \mathrm{~m} \\
& 10^{-6} \mathrm{eV} \cdot \mathrm{~m} \\
& 10^{-4} \mathrm{eV} \cdot \mathrm{~cm}
\end{aligned}
\] & \[
\begin{aligned}
& 5.4 \\
& 2.6 \\
& 2.6
\end{aligned}
\] \\
\hline \multirow[t]{4}{*}{Rydberg constant} & \(\mathrm{R}_{\mathrm{x}} \mathrm{hc}\) & \(2.179907(12)\) & \[
\begin{aligned}
& 10^{-11} \mathrm{~J} \\
& 10^{-11} \mathrm{erg}
\end{aligned}
\] & \[
\begin{aligned}
& 5.4 \\
& 5.4
\end{aligned}
\] \\
\hline & & 13.605804(36) & \(\mathrm{eV}^{10^{15} \mathrm{~Hz}}\) & 2.6 \\
\hline & \(\mathrm{R}_{\mathrm{x}} \mathrm{c}\) & \(3.28984200(25)\) & \(10^{15} \mathrm{~Hz}\) & 0.075 \\
\hline & \(\mathrm{R}_{\mathrm{x}} h \mathrm{c} / \mathrm{k}\) & \(1.578885(49)\) & \(10^{5} \mathrm{~K}\) & 31 \\
\hline \multirow[t]{4}{*}{Bohr magneton} & \(\mu_{M}\) & \[
\begin{aligned}
& 9.274078(36) \\
& 5.7883785(95)
\end{aligned}
\] & \[
\begin{aligned}
& 10^{-24} \mathrm{~J} \cdot \mathrm{~T}^{\prime} \\
& 10^{-5}{\mathrm{eV} \cdot \mathrm{~T}^{-1}}^{\text {an }}
\end{aligned}
\] & 3.9
1.6 \\
\hline & & 1.3996123(39) & \(10^{18} \mathrm{~Hz} \cdot \mathrm{~T}^{-1}\) & 2.8 \\
\hline & \[
\mu_{\mathrm{B}} / h \mathrm{hc}
\] & \(46.68604(13)\) & \(\mathrm{m}^{-1 .} \mathrm{T}^{-1}\) & 2.8 \\
\hline & & \(0.671712(21)\) & \({ }_{K \cdot T^{-1}}^{10^{-1}} \mathrm{~cm}^{-1 \cdot \mathrm{~T}^{-1}}\) & 31. \\
\hline \multirow[t]{6}{*}{Nuclear magneton} & & \(5.505824(20)\) & \(10^{25} \mathrm{~J} \cdot \mathrm{~T}^{-1}\) & 3.9 \\
\hline & \(\mu\). & \(3.1524515(53)\) & \(10^{-8} \mathrm{eV} \cdot \mathrm{T}-1\) & 1.7 \\
\hline & \(\mu_{\mathrm{N}} / \mathrm{h}\) & 7.622532(22) & \(10^{\circ} \mathrm{Hz} \cdot \mathrm{T}-1\) & 2.8 \\
\hline & \(\mu, / h c\) & \(2.5426030(72)\) & \(10^{-2} \mathrm{~m}^{-1 . \mathrm{T}^{-1}}\) & 2.8 \\
\hline & & & \(10^{-4} \mathrm{~cm}^{-1} \cdot \mathrm{~T}^{-1}\) & 2.8 \\
\hline & \(\mu_{\mathrm{x}} / \mathrm{k}\) & 3.65826(12) & \(10^{-4} \mathrm{~K} \cdot \mathrm{~T}^{-1}\) & 31 \\
\hline
\end{tabular}
* Nota that tha numbers in paranthases are the one standerd-daviation uncartaintias in the last digits of the quoted value computed on the basis of intarnat consistancy. that tha unifiad atomic mass acala "C \(\leqslant 12\) has base used throughout, that u \(u\) atomic mass unit, \(\mathrm{C}=\mathrm{coulomb}\),
 T* \(\mathrm{m}^{1}\), and \(W=\) watt in casas where formulas for constants are givan (e.g., Re). the relations are written as the product of two factors. Tha eecond factor, in paranthases, is the axprassion to ba usad whan all quantities ara expressed in cgs units, with the alectron charge in aiectrostatic units. Tha first factor, in brackats, is to bo included only if all quantitias are exprassad in Si units. Wa remind the reader that with the arcaption of the auxilisry constants which hava base takan to be exact, tha uncertaintias of thase constants are correlated, and tharefore the ganaral taw of arror propagation must ba used in calculating additional quantitias requiring two or more of thesa constants.
+ Quantities given in \(u\) and atm ara for tha conveniance of tha reader, thass units are not part of the International Syatem of Units (SI).
If ordar to avoid saparata columns for "electromagnetic" and "alactrostatic" units, both are givan undar the single haeding "cge Units." When using these units. the elamantery chares a in the sacond column should be underatood to be replaced by ase or e, respectlvely.

\section*{APPROXIMATE CAPACITANCE OF CONDUCTORS (pf/inch)}
\begin{tabular}{|l|l|l|l|}
\hline Spacing (in.) & XXXP & \begin{tabular}{l} 
Material \\
Melamine
\end{tabular} & Teflon \\
\hline \(1 / 32\) & 1.05 & 1.25 & 0.33 \\
\(1 / 16\) & 0.85 & 1.10 & 0.26 \\
\(1 / 8\) & 0.72 & 0.90 & 0.22 \\
\hline
\end{tabular}

\section*{APPROXIMATE RESISTANCE OF CONDUCTORS (ohms/inch)}

Based on \(100 \%\) conductivity of copper at \(20^{\circ} \mathrm{C}\)
\[
\begin{aligned}
& R=\frac{0.000503}{w} \text { for } 1 \text { ounce copper } \\
& R=\frac{0.000226}{W} \text { for } 2 \text { ounce copper } \\
& R=\frac{0.000135}{W} \text { for } 3 \text { ounce copper } \\
& W=\text { conductor width in inches }
\end{aligned}
\]

VELOCITY OF SOUND IN SOLIDS, GASES, AND LIQUIDS


This is the letter code adapted by the American Standards Association and by the National Association of Relay Manufacturers to describe relay contacts.

Other standard contact symbols
\begin{tabular}{|c|c|c|}
\hline Form & IEC. JIC and NMTBA symbol & Other IEC symbols \\
\hline A & \(\frac{1}{T}\) & - OR O. \\
\hline  & \[
\frac{1}{7}
\] & \(\frac{1}{1}\) On \\
\hline c & \[
\frac{1}{4} \frac{1}{4}
\] & \[
\frac{1}{1} \text { OR }
\] \\
\hline D & \[
\frac{1}{\mathrm{~L}} \text { ст }
\] & \\
\hline
\end{tabular}
\begin{tabular}{|c|}
\hline - LETTER ABBREVIATIONS \\
\hline \multirow[t]{10}{*}{\begin{tabular}{l}
B: BREAK \\
C: CLOSED \\
D: OOUBLE \\
M. MAKE \\
N NORMALLY \\
O OPEN \\
P POLE \\
S. SINGLE \\
T. THROW \\
EXAMPLE: SP ST NC OB is reod as Single Pole, Single Throw, Narmolly Clased. Oouble Break
\end{tabular}} \\
\hline \\
\hline \\
\hline \\
\hline \\
\hline \\
\hline \\
\hline \\
\hline \\
\hline \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|c|c|c|}
\hline FORM & TERM & CONTACT CONFIGURATION & FORM & TERM & CONTACT CONFIGURATION \\
\hline A & MAKE & SP ST NO & J & MAKE MAKE BREAK &  \\
\hline B & break &  & K & \[
\begin{aligned}
& \text { SP DT } \\
& \text { CENTER } \\
& \text { OFF }
\end{aligned}
\] &  \\
\hline C & BREAK MAKE (transier) &  & 1 & BREAK MAKE MAKE &  \\
\hline D & \begin{tabular}{l}
MAKE-BEFORE \\
BREAK \\
(cantinuity transter)
\end{tabular} &  & U & double make CONTACT ON ARMATURE &  \\
\hline E & \begin{tabular}{l}
BREAK \\
MAKE-BEFORE \\
BREAK
\end{tabular} &  & V & DOUBLE BREAK CONTACT ON ARMATURE &  \\
\hline F & MAKE MAKE &  & W & DOUBLE 3REAK DOUBLE MAKE CONTACT ON ARmature &  \\
\hline G & BREAK BREAK &  & x & DOUBLE MAKE &  \\
\hline H & break BREAK MAKE &  & Y & OOUBLE BREAK &  \\
\hline I & MAKE BREAK MAKE &  & \(z\) & OOUBLE BREAK OOUBLE MAKE &  \\
\hline
\end{tabular}

Heat-sink thermal resistance can be determined with the accompanying chart. Values determined graphically are not as accurate as those found from thermal equations but are precise enough for most applications. To find thermal resistance, draw a vertical line from the scale for surface area to the scales for materials and read the corresponding thermal resistance. For example, a \(3 / 16\)-in.-thick piece of horizontally mounted copper with a surface area of \(15 \mathrm{in} .^{2}\) has a thermal resistance of approximately \(4.1^{\circ} \mathrm{C} / \mathrm{W}\). And a \(3 / 32\)-in.-thick piece of vertically mounted copper with a surface area of \(25 \mathrm{in}^{2}\) has a thermal resistance of approximately \(3.1^{\circ} \mathrm{C} / \mathrm{W}\). Note that vertical heatsinks have lower thermal resistances than horizontal sinks because convection provides increased heat dissipation.


\section*{FOREIGN VOLTAGE GUIDE}

Following is an up-to-date guide to predominant electric voltages in foreign countries. In general, all references to 110 V apply to the range from 110 V to 160 V . References to 220 V apply to the range from 200 V to 260 V . Where \(110 / 220 \mathrm{~V}\) is indicated, voltage varies within the country, depending on location.
\begin{tabular}{|c|c|c|c|}
\hline Aden & 220 V & Dominica & 220 V \\
\hline Atghanistan & 220 V & Dominican Rep. & \[
110 / 220 \mathrm{~V}
\] \\
\hline Algeria & \(110 / 220 \mathrm{~V}\) & Ecuador & \(110 / 220 \mathrm{~V}\) \\
\hline Angoia & 220 V & Egypt & \(110 / 220 \mathrm{~V}\) \\
\hline Anguilia & 220 V & El Salvador & 110 V \\
\hline - Antigua & \(110 / 220 \mathrm{~V}\) & Ethiopla & \(110 / 220 \mathrm{~V}\) \\
\hline + Argentina & 220 V & \(\ddagger\) Fijl & 220 V \\
\hline Aruba & 110 V & Finiand & 220 V \\
\hline \#+ Australia & 220 V & France & \(110 / 220 \mathrm{~V}\) \\
\hline - Austria & 220 V & French Guiana & \(110 / 220 \mathrm{~V}\) \\
\hline Azores & \(110 / 220 \mathrm{~V}\) & Gabon & 220 V \\
\hline Bahamas & \(110 / 220 \mathrm{~V}\) & Gambla & 220 V \\
\hline Bahrain & 220 V & ** Germany & \(110 / 220 \mathrm{~V}\) \\
\hline Bangladesh & 220 V & Ghana & 220 V \\
\hline Barbados & \(110 / 220 \mathrm{~V}\) & Gibraltar & 220 V \\
\hline Beiglum & \(110 / 220 \mathrm{~V}\) & - Greal Britain & 220V \\
\hline Bermuda & \(110 / 220 \mathrm{~V}\) & + Greece & \(110 / 220 \mathrm{~V}\) \\
\hline Bhutan & 220 V & Greenland & 220 V \\
\hline Bolivia & \(110 / 220 \mathrm{~V}\) & - Grenada & 220 V \\
\hline Bonaire & \(110 / 220 \mathrm{~V}\) & Grenadines & 220 V \\
\hline - Botswana & 220 V & - Guadeloupe & \(110 / 220 \mathrm{~V}\) \\
\hline +Brazil & \(110 / 220 \mathrm{~V}\) & Guatemala & \(110 / 220 \mathrm{~V}\) \\
\hline Brit. Honduras & \(110 / 220 \mathrm{~V}\) & Guinea & 220 V \\
\hline Brit. Virgin l. & \(110 / 220 \mathrm{~V}\) & Guyana & \(110 / 220 \mathrm{~V}\) \\
\hline Buigaria & \(110 / 220 \mathrm{~V}\) & Halti & \(110 / 220 \mathrm{~V}\) \\
\hline Burma & 220 V & Honduras & \(110 / 220 \mathrm{~V}\) \\
\hline Burundi & 220 V & - Hong Kong & 220 V \\
\hline Cambodia & \(110 / 220 \mathrm{~V}\) & Hungary & 220 V \\
\hline Cameroon & \(110 / 220 \mathrm{~V}\) & Iceiand & 220 V \\
\hline Canada & 110 V & tindia & 220 V \\
\hline Canal Zone & \(110 / 220 \mathrm{~V}\) & Indonesia & \(110 / 220 \mathrm{~V}\) \\
\hline Canaryl. & \(110 / 220 \mathrm{~V}\) & Iran & 220 V \\
\hline Caymani. & 110 V & Iraq & 220 V \\
\hline Cen. African Rep. & 220 V & - Ireiand & 220 V \\
\hline Chad & 220 V & isle of Man & 220 V \\
\hline +Channell. (Brit) & 220 V & israel & 220 V \\
\hline \({ }^{+}\)Chile & 220 V & Italy & 110 I 220 V \\
\hline \({ }^{\text {t }}\) China & 220 V & Ivory Coast & 220 V \\
\hline Cosombia Rica & 110 V
\(110 / 220 \mathrm{~V}\) & - Jamaica & \(110 / 220 \mathrm{~V}\) \\
\hline Costa Rica & \(110 / 220 \mathrm{~V}\) & Japan & 110 V \\
\hline Cuba & 110 V & Jordan & 220 V \\
\hline Curacao & 110 V & - Kenya & 220 V \\
\hline - Cyprus & 220 V & Korea & 110 V \\
\hline Czechosiovakia & \(110 / 220 \mathrm{~V}\) & Kuwait & 220 V \\
\hline Dahomey & 220 V & Laos & \(110 / 220 \mathrm{~V}\) \\
\hline Denmark & 220 V & Lebanon & \(110 / 220 \mathrm{~V}\) \\
\hline
\end{tabular}


\footnotetext{
Denotes countries in which plugs with 3 square pins are used (in whole or part)
\(\ddagger\) Requires plug with angled blades
}
tCountries using dc in certain areas -Countries with recessed outlets (Reprinted from "Foreign Electricity Is No Deep Dark Secret," couitesy of Franzus Company Inc.)


\section*{COORDINATES FOR EQUALLY SPACED HOLES}

It is sometimes necessary to determine the \(x\) and \(y\) coordinates of a circle divided into an equal number of parts. The following table can be used directly, or it can serve as a crosscheck against answers obtained by normal trigonometric methods.

FOR EXAMPLE: A circle that has a radius of 5.0 cm and contains 4 holes spaced at \(90^{\circ}\). Determine the distance between their centers. \(A=1.4142 R=1.4142(5.0)=7.07 \mathrm{~cm}\).
(

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[^0]:    The computer programming required for the Chebyshev and elliptic filter design tabulations was prepared by Mike Barge under the direction of Ed Wetherhold. The tables are made available for publication through the courtesy of the Signal Analysis Center of Honeywell Inc., Annapolis, MD.

[^1]:    gausses
    
    
    
    microferads
    Ampere（absolute） ampere－hours
    
    
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    | E． | miles／hr舞 $\mathrm{kms} / \mathrm{hr}$ knots

    meters／min $\stackrel{\stackrel{c}{c}}{\text { en }}$ miles／min
     $\mathrm{kms} / \mathrm{hr} / \mathrm{sec}$ meters／sec／sec miles／hr／sec per cent grade
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    | 0.1020 |
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    | 9.807 |
    | 70.93 |
    | 2.205 |
    | $9.842 \times 10^{-4}$ |
    | $1.102 \times 10^{-3}$ |
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    | 0.06243 |
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    | liters |
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    | cubic ft . |
    | gallons (U.S.) |
    | Btu/min |
    | foot-lbs/min |
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    | International Ampere | Ampere (absolute) |
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    | International volt | Joules (absolute) |
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    Watt
    Lumen／sq．meter
    foot－candles

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    | E | feet／min feet／sec kms／hr miles／hr feat／min feet／sec kilometers／hr

    
     liters／min liters／min lumens／sq ft Lumen Lumen／sq．ft． $\underset{\text { x }}{2}$
    maxwells maxwelis megalines megohms meters meters meters meters meters N
    E
    E
     meters meters／min meters／min meters／min meters／rnin

     들 | 4 |
    | :--- |
    | $\stackrel{y}{4}$ |
    | 5 |
    | E． |

     meters／sec meters／sec

    $$
    \begin{aligned}
    & \text { kilolines } \\
    & \text { webers } \\
    & \text { maxwells } \\
    & \text { microhms } \\
    & \text { ohms } \\
    & \text { centimeters }
    \end{aligned}
    $$

    
    

    | To Convert | Into |
    | :---: | :---: |
    |  | N |
    | nepers | decibels |
    | Newton | Dynes |
    |  | 0 |
    | OHM (International) | OHM (absolute) |
    | ohms | megohms |
    | ohms | microhms |
    | ounces | drams |
    | ounces | grains |
    | ounces | grams |
    | ounces | pounds |
    | ounces | ounces (troy) |
    | ounces | tons (long) |
    | ounces | tons (metric) |
    | ounces (fluid) | cu inches |
    | ounces (fluid) | liters |
    | ounces (troy) | grains |
    | ounces (troy) | grams |
    | ounces (troy) | ounces (avdp.) |
    | ounces (troy) | pennyweights (troy) |
    | ounces (troy) | pounds (troy) |
    | Ounce/sq. inch ounces/sq in. | Dynes/sq. cm. pounds/sq in. |
    |  | P |
    | Parsec | Miles |
    | Parsec | Kilometers |
    | parts/million | grains/U.S. gal |
    | parts/million | grains//mp.gal |
    | parts/million | pounds/million gal |
    | Pecks (British) | cubic inches |
    | Pecks (British) | liters |
    | Pecks (U.S.) | bushels |
    | Pecks (U.S.) | cubic inches |
    | Pecks (U.S.) | litters |

    

    | quadrants (angle) | radians |
    | :--- | :--- |
    | quadrants (angle) | seconds |
    | quarts (dry) | cu inches |
    | quarts (liq.) | cu cms |
    | quarts (liq.) | cu feet |
    | quarts (liq.) | cu inches |
    | quarts (liq.) | cu meters |
    | quarts (liq.) | cu yards |
    | quarts (liq.) | gallons |
    | quarts (liq.) | liters |
    |  |  |
    |  |  |
    | radians | degrees |
    | radians | minutes |
    | radians | quadrants |
    | radians | seconds |
    | radians $/ \mathrm{sec}$ | degrees $/ \mathrm{sec}$ |
    | radians $/ \mathrm{sec}$ | revolutions $/ \mathrm{min}$ |
    | radians $/ \mathrm{sec}$ | revolutions $/ \mathrm{sec}$ |
    | radians $/ \mathrm{sec} / \mathrm{sec}$ | revs $/ \mathrm{min} / \mathrm{min}$ |
    | radians $/ \mathrm{sec} / \mathrm{sec}$ | revs $/ \mathrm{min} / \mathrm{sec}$ |
    | radians $/ \mathrm{sec} / \mathrm{sec}$ | ravs $/ \mathrm{sec} / \mathrm{sec}$ |
    | revolutions | degrees |
    | revolutions | quadrants |
    | revolutions | radians |
    | revolutions $/ \mathrm{min}$ | degrees $/ \mathrm{sec}$ |
    | revolutions $/ \mathrm{min}$ | radians $/ \mathrm{sec}$ |
    | revolutions $/ \mathrm{min}$ | revs $/ \mathrm{sec}$ |
    | revolutions $/ \mathrm{min} / \mathrm{min}$ | radians $/ \mathrm{sec} / \mathrm{sec}$ |
    | revolutions $/ \mathrm{min} / \mathrm{min}$ | revs $/ \mathrm{min} / \mathrm{sec}$ |
    | revolutions $/ \mathrm{min} / \mathrm{min}$ | revs $/ \mathrm{sec} / \mathrm{sec}$ |
    | revolutions $/ \mathrm{sec}$ | degrees $/ \mathrm{sec}$ |
    | revolutions $/ \mathrm{sec}$ | radians $/ \mathrm{sec}$ |
    | revolutions $/ \mathrm{sec}$ | revs $/ \mathrm{min}$ |
    | revolutions $/ \mathrm{sec} / \mathrm{sec}$ | radians $/ \mathrm{sec} / \mathrm{sec}$ |
    | revolutions $/ \mathrm{sec} / \mathrm{sec}$ | revs $/ \mathrm{min} / \mathrm{min}$ |
    | revolutions $/ \mathrm{sec} / \mathrm{sec}$ | revs $/ \mathrm{min} / \mathrm{sec}$ |
    | Rod | Chain (Gunters) |
    | Rod | Meters |
    | Rod (Surveyors' meas.) | yards |

    
    
    pennyweights (troy) pennyweights (troy) pennyweights (troy) pennyweights (troy)
    pints (dry) pints (liq.)
    pints (liq.)
    흘
    훌
    흧
    흘
    亲
    pints (liq.)
    Planck's quantum Poise
     poundals poundals poundals poundals
    poundals poundals pounds $n$
    5
    5
    8
    8 $n$
    8
    8
    8 pounds n
    8
    8
    8 $n$
    $\frac{n}{5}$
    8 pounds pounds pounds pounds
    pounds (troy) pounds (troy)
     pounds (troy)

    | To Convert | Into M | Multiply By |
    | :---: | :---: | :---: |
    |  | T |  |
    | temperatura $\left({ }^{\circ} \mathrm{C}\right)+273$ | absoluta tamperature $\left({ }^{\circ} \mathrm{C}\right.$ | C) 1.0 |
    | tamperatura $\left({ }^{\circ} \mathrm{C}\right)+17.78$ | tamperetura ${ }^{\circ} \mathrm{F}$ ) | 1.8 |
    | tamperature $\left({ }^{\circ} F\right)+460$ | absolute temperetura ( ${ }^{\circ} \mathrm{F}$ ) | F) 1.0 |
    | temperaturs ( ${ }^{\circ} \mathrm{F}$ ) $\mathbf{- 3 2}$ | tempereture ( ${ }^{\circ} \mathrm{C}$ ) | 5/9 |
    | tons (long) | kilograms | 1,016. |
    | tons (long) | pounds | 2,240. |
    | tons (long) | tons (short) | 1.120 |
    | tons (matric) | kilograms | 1,000. |
    | tons (matric) | pounds | 2,205. |
    | tons (short) | kilograms | 907.1848 |
    | tons (short) | ounces 32 | 32,000. |
    | tons (short) | ounces (troy) 29 | 29,166.66 |
    | tons (short) | pounds | 2,000. |
    | tons (short) | pounds (troy) | 2,430.56 |
    | tons (short) | tons (long) | 0.89287 |
    | tons (short) | tons (metric) | 0.9078 |
    | tons (short/sq ft | kgs/sq meter 9 | 9,765. |
    | tons (short)/sq ft | pounds/sq in. | 2,000. |
    | tons of weter $/ 24 \mathrm{hrs}$ | pounds of water $/ \mathrm{hr}$ | 83.333 |
    | tons of water/24 hrs | gallons/min | 0.16643 |
    | tons of weter/24 hrs | cu ft/hr | 1.3349 |
    |  | V |  |
    | Volt/inch | Volt/cm. | . 39370 |
    | Volt (absoluta) | Statvolts | . 003336 |
    |  | W |  |
    | wetts | Btu/hr | 3.4129 |
    | watts | Btu/min | 0.05688 |
    | wetts | ergs/sec | $10^{7}$ |
    | wetts | foot-lbs/min | 44.27 |

    Multiply By
    16.5

    20
    $2.778 \times 10^{-4}$
    0.01667
    $3.087 \times 10^{-6}$
    $4.848 \times 10^{-6}$
    14.59
    32.17
    12.57
    $1.973 \times 10^{5}$
    $1.076 \times 10^{-3}$
    0.1550
    0.0001
    $3.861 \times 10^{-11}$
    100.0
    $1.196 \times 10^{-4}$
    $2.296 \times 10^{-5}$
    $1.833 \times 10^{8}$
    929.0
    144.0
    0.09290
    $3.587 \times 10^{-8}$
    $9.290 \times 10^{4}$
    0.1111
    $1.273 \times 10^{6}$
    6.452
    $6.944 \times 10^{-3}$
    645.2
    $10^{6}$
    $7.716 \times 10^{-4}$
    
    To Convert
    $\stackrel{\square}{8}$
    $\frac{\square}{8}$

    
    
    
    
    
    squere kilometers
    squere kilometers squere kilometers square kilometers squere kilometers square kilometers ssesewoIㅈ s senbs
    
     n
    है
    8
    $\frac{8}{8}$ equere meters
     square meters square meters quare miles quere miles
     quare miles squere millimeters squere millimeters square millimeters squere millimeters square mils square mils squere mils square yords quere yerds n
    $\frac{8}{8}$
    8
    0
    
     squere yards

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    This nomogram is used to estimate the safe range at which an object may be illuminated directly. It incorporates a scale for the introduction of loss factors including losses in the eye, optical surfaces external to the laser mirror, and optical losses.

    FOR EXAMPLE: Assume system losses of $50 \%$, a pupil diameter of 4 mm , a laser output of 0.05 J , and a laser beamwidth of 1 mrad. Connect loss factor and pupil size to turning scale (1), from that point to laser output of 0.05
    J to turning scale (2), then through safety threshold point to turning scale 3 and finally through J to turning scale (2), then through safety threshold point to turning scale (3), and finally through laser beamwidth (4) to distance line. In this case the safe range is approximately 4.0 km or 2.6 statute miles.

    NOTE: "Safe" threshold levels are a subject of some controversy and the figures specified in the nomogram should be interpreted in the light of most recent information.
    

    This nomogram relates laser radiation terms, which may be given as photon energy, wave number, frequency, or wavelength. Any of these terms can be converted to the others by a horizontal line across the nomogram.

    FOR EXAMPLE: 1. Light at a wavelength of $0.5 \mu$ can also be described as having (1) A wavelength of 5000 $\AA$, (2) a frequency of 600 THz or $6 \times 10^{14} \mathrm{~Hz}$, (3) a wavenumber of $20,000 \mathrm{~cm}^{-1}$, and (4) a photon energy of 2.48 eV.
    2. Electrons when falling through 4 V will radiate at $3100 \AA$.
    3. Light at 200 THz will produce conduction in semiconductors with band-gaps up to 0.83 V .
    

    ## SPECTRAL CHARACTERISTICS OF PHOTORECEPTORS AND LIGHT SOURCES

    This figure shows spectral sensitivity of various photoreceptors. Response of cadmium sulfide cells is similar to that of the human eye, but other commonly used receptors perform best at wavelengths invisible to the eye.
    

    This nomogram solves the light intensity equation:

    $$
    \text { foot-candles }=\frac{\text { candlepower }}{(\text { distance in feet })^{2}}
    $$

    which assumes a point source (distance greater than five times maximum lamp dimension).
    Most lamps are classified according to wattage, and the following approximate relations apply:

    1. The shorter the rated life of the lamp, the higher the efficiency ( $\mathrm{op} / \mathrm{watt}$ ) and the higher the color temperature of the light.
    2. For standard $120-\mathrm{V}$ inside-frosted incandescent lamps rated for $1,000 \mathrm{hr}$, the following hold true:
    a. Efficiency increases with increasing wattage.
    b. A $25-\mathrm{W}$ lamp is approximately 19 cp, a $60-\mathrm{W}$ lamp about 60 cp , and a $150-\mathrm{W}$ lamp is near 200 cp .
    c. Color temperature increases with increasing wattage ( $150-\mathrm{W}$ lamp is near $2,900 \mathrm{~K}$ ).
    d. When lamps are operated at constant voltage, light output falls with time, rapidly during the first 50 hrs and more slowly thereafter.
    e. When lamps are operated at constant current, light output rises with time, slowly at first, then accelerating to catastrophic failure.
    FOR EXAMPLE: A 6 -cp lamp will produce a light intensity of 100 fc , at a distance of 2.94 in . $(0.245 \mathrm{ft})$ from the lamp filament. The same lamp will provide 1 fc at 29.4 in . and 0.01 fc at 294 in .

    ## Several Useful Definitions

    A foot-candle is the illumination produced when the light from one candle falls normally on a surface at a distance of one foot.

    A lux (commonly used in Europe) is the illumination produced when the light from one candle falls normally on a surface at a distance of one meter.

    A point source emitting light uniformly in all directions radiates $4 \pi$ lumens/candle.
    A lambert is the brightness of a perfectly diffusing surface emitting or reflecting one lumen per square centimeter.

    A foot lambert $1 / \pi$ candles $/ \mathrm{ft}^{2}$.
    (Reod correspondingly headed columns, i.e., $A, A^{\prime}, A^{\prime \prime}$, efc.)
    
    

    SUGGESTED VALUES OF ILLUMINANCE

    Auditorium
    Lecture room-library
    Classroom
    Dratting room
    Low-contrast work inspection
    Hospital operating room

    10 fc
    30 fc
    30 fc
    30 fc
    250 fc
    $500-1,000$ fc

    This nomogram relates candles/square foot, footcandles, lumens/square foot, lamberts, foot-lamberts, lumens/square centimeter, candles/square centimeter, candles/square inch, end lux, and it is based on the following relationships:
    foot-lamberts $=$ lumens $/$ square foot $=$ foot-candles $=10.764$ lux
    lambets $=$ lumens/square centimeter $=295.72$ candles/square foot $=929.03$ lumens/square foot
    lux $=$ lumens/square centimeter and candles/square centimeter $=3.14159$ lambert
    A line from any known value through the index point intersects all other scales at corresponding values.
    FOR EXAMPLE:

    $$
    \begin{aligned}
    4 \mathrm{~L} & =8.2 \mathrm{~cd} / \mathrm{in.}^{2} & & =3,715 \mathrm{lM} / \mathrm{ft}^{2} \\
    & =4,400 \mathrm{fc} & & =1,183 \mathrm{~cd} / \mathrm{ft}^{2}
    \end{aligned}
    $$

    NOTE: the ranges can be extended by multiplying all scales by the same power of 10 .
    

    Measurements of Sources (as Seen by Observer)
    (Examples: Lamps, Stars, T.V., Lighthouse)

    | Measurement | Radiometric (Wide Band Receiver) | Photometric <br> (Eye will be the Receiver) | Where Used |
    | :---: | :---: | :---: | :---: |
    | Total emission | Power: watts | : Lumens | Lamps light standards |
    | Emissions into a solid angle from a point source | Intensity: watts/steradian | Luminous Intensity $\text { Candela }=\frac{\text { Lumen }}{\text { Steradian }}$ | Stars |
    | Emissions into a solid angle from a large source | Radiance watts $/ \mathrm{m}^{2} /$ steradian | Luminance <br> (Brighness) $\begin{aligned} & : \frac{\text { Candle }}{\mathrm{ft}^{2}}=\pi \text { foot lamberts } \\ & : \frac{\text { Candle }}{\mathrm{m}^{2}}=1 \text { nit } \\ & : \frac{\text { Candle }}{\mathrm{cm}^{2}}=1 \text { stilb }=\pi \text { lamberts } \end{aligned}$ <br> also: 1 foot lambert $=.0010764 \text { lamberts }$ $=3.426 \text { nits }$ | Lamps <br> T.V. Screen <br> L.E.D. |
    | Emission into all angles point source | Emittance watts/m ${ }^{2}$ | Luminous Emittance <br> : Lumen/ft ${ }^{2}$ <br> : Lumen/m ${ }^{2}$ <br> : Lumen/ $\mathrm{cm}^{2}$ | Flourescent lamps |

    Measurements of Sources (as Seen by Observer)
    (Examples: Lamps, Stars, T.V., Lighthouse)

    | Measurement | Radiometric (Wide Band Receiver) | Photometric <br> (Eye will be the Receiver) | Where Used |
    | :---: | :---: | :---: | :---: |
    | Total emissions received | Power: watts | : Lumens | Detectors |
    | Emissions per unit area | $\begin{aligned} & \text { Irradiance } \\ & \mathrm{W} / \mathrm{m}^{2} \end{aligned}$ | Hluminance $\begin{aligned} & : \frac{\text { Lumen }}{\mathrm{ft}^{2}}=\text { foot candle } \\ & : \frac{\text { Lumen }}{\mathrm{m}^{2}}=\text { lux }=\text { meter candle } \\ & : \frac{\text { Lumen }}{\mathrm{cm}^{2}}=\text { phot } \\ & \text { also: } \\ & 1 \text { foot candle }=10.764 \text { lux } \end{aligned}$ |  |

    ## Typical Measurements and Values

    | Source | Total Emissions |  | Luminance <br> Photometric Foot Lamberts | Illuminance |  |
    | :---: | :---: | :---: | :---: | :---: | :---: |
    |  | Photometric Lumens | Radiometric Watts |  | Photometric <br> Lumens/m ${ }^{2}$ | Radiometric $\mathrm{W} / \mathrm{m}^{2}$ |
    | Sun (noon) Lightning Flash |  |  | $\begin{array}{r} 4.7 \times 10^{8} \\ 2 \times 10^{10} \end{array}$ | $10^{5}$ | . 1 |
    | 100W Lamp | 1630 | 30 | $2.6 \times 10^{6}$ |  |  |
    | 40W Flourescent Lamp | 2560 | 16 | 2000 |  |  |
    | Moon |  |  | 730 | . 27 |  |
    | Twilight |  |  |  | 10 |  |
    | Starlight (Total) (zero magnitude) |  |  |  | $\begin{gathered} .001 \\ 2.6 \times 10^{-6} \end{gathered}$ |  |

    ## ILLUMINATION POWER CONVERSION NOMOGRAM

    This nomogram relates international lumens, watts, and candlepower. Select the known value. A line from that point through the index point intersects other scales at corresponding values.

    FOR EXAMPLE:

    $$
    \begin{aligned}
    5 \mathrm{Im} & =0.0074 \mathrm{~W} \\
    50 \mathrm{Im} & =3.98 \mathrm{cp}
    \end{aligned}
    $$

    NOTE: the ranges can be extended by multiplying all scales by the same power of 10 . The nomogram is based on the following:

    $$
    \begin{aligned}
    & 1 \mathrm{cp}=12.566 \mathrm{Im} \\
    & 1 \mathrm{Im}=0.001496 \mathrm{~W}
    \end{aligned}
    $$

    
    LUMINANCE SPECTRUM
    

    ## TABULATION OF SOUND INTENSITY LEVELS

    This tabulation extends from the barely audible to the unbearable and/or damaging sound intensity levels. The various levels are given in terms of sound pressure in dynes per square centimeter, sound intensity (at the eardrum) in watts per square centimeter, and intensity level in decibels above $10^{-16} \mathrm{~W} / \mathrm{cm}^{2}$ and related to familiar sound situations.

    FOR EXAMPLE: A faint to moderate sound such as can be found in an average residence is equal to a sound pressure of $0.024 \mathrm{dyn} / \mathrm{cm}^{2}$, which produces a sound intensity at the eardrum of $10^{-12} \mathrm{~W} / \mathrm{cm}^{2}\left(1 \mathrm{pW} / \mathrm{cm}^{2}\right)$ and is equal to an intensity level of 40 dB above $10^{-16} \mathrm{~W} / \mathrm{cm}^{2}$.
    
    

    ## EQUAL LOUDNESS CURVES OF THE AVERAGE HUMAN EAR

    The curves show that the frequency response characteristic of the human ear varies with the loudness of the sound. At low sound levels the ear is relatively insensitive to the lower frequencies, which must be at least 60 dB to be heard. Higher sound levels are heard nearly equally well at the high and low frequencies. Therefore, for llstening at low volume levels, the low frequencies must be boosted considerably to produce the effect of equal loudness and to avoid an apparent lack of low frequency tones. The ear is most sensitive to sounds in the 2,000 to $4,000 \mathrm{~Hz}$ range.
    (20- to 29-year old subjects)
    

    ## REVERBERATION TIME

    These graphs determine the optimum recommended reverberation time as a function of room volume and usage. The optimum times for speech rooms, motion picture theaters, and school auditoriums are given by a single line, whereas the optimum time for music is a broad band. Furthermore, the optimum reverberation time is not the same for all kinds of music. For example, slow organ and choral music require more reverberation than does a brilliant allegro composition played on woodwinds or a harpischord.

    The first chart is used to find the optimum reverberation time for frequencies above 512 Hz . For lower frequencies that value must be multiplied by the appropriate factor in the second graph. For small rooms the lower part of the shaded portion (closer to 1.0 should be used.)
    

    Optimum reverberetion time es efunction of volume of rooms for verious types of sound for efrequency of about 512 Hz .
    


    ## PHYSIOLOGICAL EFFECTS OF ELECTRIC CURRENT ON THE HUMAN BODY

    The chart shows the physiological effect of various current densities on the human body. Voltage is not the prime consideration, though it takes voltage to produce the current flow. The amount of shock current depends on the body resistance between the points of contact and the skin condition, (that is, moist or dry). For example, the internal resistance between the ears is only 100 ohms (less the skin resistance), while from hand to foot it is close to 500 ohms. Skin resistance may vary from about 1,000 ohms for wet skin to over $1 / 2$ Mohm for dry skin, and is even lower for ac.

    The chart shows that shock becomes more severe as current rises. At values as low as 20 mA breathing becomes labored, and as the current approaches 100 mA , ventricular fibrillation of the heart occurs. Above 200 mA , the muscular contractions are so severe that the heart is forcibly clamped during the shock. This clamping protects the heart from going into ventricular fibrillation and the victim's chances for survival are good if the victim is given immediate attention. Resuscitation, consisting of artificial respiration, will usually revive the victim.
    

    This graph relates light output, current, and life of incandescent lamps with rated (design) voltage. The curves show that the light output varies directly as the applied voltage raised to the 3.4 th power, while life is inversely proportional to applied voltage raised to the 12th power.

    FOR EXAMPLE: At $110 \%$ of rated voltage, the current will increase by $5 \%$, light output increases by $40 \%$, and life will be reduced to nearly $35 \%$ of that at design voltage.

    At $80 \%$ of rated voltage, current decreases by $10 \%$, light output drops by more than $50 \%$, but lamp life is increased to 18 times normal.
    
    COLOR COOES FOR ELECTRONIC COMPONENTS

    |  | 感 |  |  | $\begin{array}{\|l} \hline \frac{\pi}{6} \\ \hline \frac{\overline{4}}{3} \\ \hline \end{array}$ |  |  | － | （\％） |  |
    | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
    |  | \％ | 皆 | 号 | 宫 |  | E． | 皆喜 |  |  |
    | $\begin{aligned} & \frac{\pi}{3} \pi \\ & n \\ & \text { n } \\ & \text { 준 } \end{aligned}$ |  |  |  |  | 咢 |  |  | \％ | 皆 |
    |  |  | T | $\bigcirc$ | 8 | － | － | 7 | $\frac{2}{7}$ | 8 |
    |  |  | 앙 |  | $\bigcirc$ | $\stackrel{\sim}{\square}$ | N | m | $\stackrel{ }{*}$ | $\stackrel{10}{\sim}$ |
    |  | 諹言 | $\bigcirc$ | \％ | $\stackrel{N}{n}$ | $\stackrel{\bigcirc}{0}$ | 끅 | － | $\bigcirc$ | 응 |
    |  | 䉼 ${ }^{\text {aby }}$ | $\sim$ | $\stackrel{\square}{0}$ |  |  |  | $\stackrel{\circ}{\circ}$ |  |  |
    |  |  | － | － | － | $\stackrel{\sim}{\sim}$ |  | $\sim$ |  |  |
    |  | 言音 | $\rightarrow$ | $\bigcirc$ | － | 8 | $\begin{aligned} & 8 \\ & \hline 0 \\ & 0 \\ & \hline \end{aligned}$ |  |  |  |
    |  | 気遂 | $\bigcirc$ | $\rightarrow$ | $\sim$ | m | ＊ | $\sim$ | 6 | N |
    |  | － | 1 | $\cdots$ | $\sim$ | । | 1 | $\stackrel{\sim}{\circ}$ | $\begin{array}{\|c} n \\ 0 \\ \hline 0 \end{array}$ | $\bigcirc$ |
    |  | 立 | \％ | \％ | $\stackrel{\square}{\square}$ | \％ | －¢ | $\stackrel{\square}{\circ}$ | $\stackrel{\square}{7}$ | － |
    |  | 咅定 | － | － | $\sim$ | m | $\checkmark$ | $\sim$ | 6 | － |
    |  |  | ＋ | $\stackrel{-}{+1}$ | $\begin{gathered} N \\ +1 \\ \hline \end{gathered}$ | $\begin{array}{\|c} m \\ +1 \\ \hline \end{array}$ | $\sum_{0}^{n}$ |  | $\begin{aligned} & 0 \\ & +1 \\ & \hline \end{aligned}$ | － |
    |  |  | \％ | －\％ | 3 | O－ | － | $0^{\circ}$ | \％ | 5 |
    |  |  | \％ | －\％ | $\stackrel{\square}{\square}$ | 3 | － | 앙 | $\stackrel{\square}{7}$ | $\stackrel{\square}{\circ}$ |
    |  | 砏家 0 | － | $\cdots$ | $\sim$ | m | $\checkmark$ | $\sim$ | $\bullet$ | $\wedge$ |
    |  |  |  | \| | \％ | 訔 |  | 풇퉁 | 岂 | 产 |

    
    ${ }^{1}$ IFor components such as resistors, capacitors. and wires. Also, for identification of torange body identifies elements used principally for modulation purposes or beam
    

    $$
    \begin{aligned}
    & \text { In Value. have ext. leads, the body } \\
    & \text { intertally connetted element. } \\
    & \text { (b) } \\
    & \text { STANOARD-6-DOT }
    \end{aligned}
    $$ (E)ements used to control beam current. Deam norse ete

    i. Elements are numbered according to their relative position from cathoce-lowest

    $$
    \begin{aligned}
    & \text { digwhement } \mathrm{s}_{9} \text { (Yeillow) } \\
    & \text { Seceand } \\
    & \text { Equilikent fle }
    \end{aligned}
    $$

    $$
    \begin{aligned}
    & \text { Fivst } \\
    & \text { WigNheent } \mathrm{K}_{9} \text { (Yollow) }
    \end{aligned}
    $$

    (t)
    
    FUM RESISTORS
    
    i For components such as resistors, capacitors. and wires. Also, for identification of
    terminals and circuit functions.
    I GMy $=-0$ - $100 \%$ tolerance or Cuaranteed Minimum Value.
    If heater-cathode elements are internally conaected, but have ext. leads, the body
    color gives the major element and the tracer is the internally connected element.
    (a) COMPOSITION RESISTORS
    Seosed
    
    
    

    ## EIA AND MILTARY DESIGNATIONS OF TEMPERATURE

    CHARACTERISTICS AND TOLERANCES FOR CERAMIC DIELECTRIC CAPACITORS
    ## General Application and High-K Capacitors

    EIA
    

    Example: X7R means a max. cap. change of $\pm 15 \%$ over the temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.

    ## Military

    

    Example: BX means a max. cap. change of $\pm 15 \%$ with no applied voltage or $-25 \%,+15 \%$ with applied voltage over the temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.

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    Temperature Stable and Temperature Compensating Capacitors
    EIA

    | $\mathrm{C} 0 \mathrm{G}$ |  |  |  |
    | :---: | :---: | :---: | :---: |
    | Temp. Coeff. in ppm/ ${ }^{\circ} \mathrm{C}$ |  | Tolerance <br> in ppm/ ${ }^{\circ} \mathrm{C}$ |  |
    | Significant Figures | Multiplier |  |  |
    | C 0.0 | $\begin{array}{ll}0 & -1 \\ 1 & -10\end{array}$ | G |  |
    | M 1.0 | $2-100$ | H | $\pm 60$ |
    | $\begin{array}{ll}\mathrm{P} & 1.5\end{array}$ | $3-1000$ | J | $\pm 120$ |
    | R 2.2 | $5+1$ | K | $\pm 250$ |
    | S $\quad 3.3$ | $6+10$ | L | $\pm 500$ |
    | T 4.7 | $7+100$ | M | $\pm 1000$ |
    | $\begin{array}{ll}U & 7.5\end{array}$ | $8+1000$ | $N$ | $\pm 2500$ |

    Example: characteristic COG is $0 \pm 30 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. For many years these capacitors were known by the trade designation NPO , which stood for Negative-Positive Zero.
    Exceptions: $\mathrm{S} 2 \mathrm{~L}=$ any temp. coeff. between +100 and $-750 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
    U2M $=$ any temp. coeff. between +150 and $-1500 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
    S3 $\mathrm{N}=$ any temp. coeff. between -1000 and $-5200 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$

    ## Military

    

    Example: characteristic CG is $0 \pm 30 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ (NPO).

    ## Capacitance Tolerance Codes

    | EIA and Military | Tolerance | Sprague | EIA and Military | Tolerance | Sprague |
    | :---: | :---: | :---: | :---: | :---: | :---: |
    | A | $\pm 0.05 \mathrm{pF}$ | - | K | $\pm 10 \%$ | X9 |
    | B | $\pm 0.1 \mathrm{pF}$ | F1 | L | $\pm 15 \%$ | $\times 8$ |
    | C | $\pm 0.25 \mathrm{pF}$ | F1 | M | $\pm 20 \%$ | $\times 0$ |
    | D | $\pm 0.5 \mathrm{pF}$ | F2 | N | $\pm 30 \%$ | G3 |
    | F | $\pm 1 \%$ or $\pm \mathrm{lpF}$ | $\times 1$ | r | GMV or $-0 \%$, $+100 \%$ | A8 |
    | G | $\pm 2 \%$ or $\pm 2 \mathrm{pF}$ | $\times 2$ | $\checkmark$ | $-20 \%,+40 \%$ | D4 |
    | H | $\pm 2.5 \%$ | $\times 7$ $\times 5$ | Y | $-20 \%,+50 \%$ | D5 |
    | 1 | $\pm 5 \%$ | $\times 5$ | 2 | -20\%. $+80 \%$ | D8 |

    Knowing the isotope half-life, its original activity at some particular time, it is an easy matter, using the chart, to determine the residual activity at some subsequent time

    FOR EXAMPLE: A sample of radioactive iodine -131 has an activity of $10 \mu \mathrm{C}$, find the remaining strength 20 days later.

    ANSWER: From an appropriate source determine the half-life of the isotope. For radioactive iodine-131, the half-life is 8.1 days.

    Calculate how many "half-lives"" there are corresponding to the time interval in question, that is, divide the time interval by the half-life: in this case 20/8.1 = 2.47.

    Enter this value on the horizontal axis of the chart and read the "fraction remaining" on the vertical axis as shown by the broken lines. In the case under consideration the value is 0.177 .

    Multiply this value by the original activity thus giving a final value of $1.77 \mu \mathrm{C}$.
    

    CATHODE-RAY TUBE PHOSPHOR CHARACTERISTICS

    |  | Color |  | Spectral |
    | :--- | :--- | :--- | :--- | :--- | :--- |
    | Type | Fluorescence | Phosphorescence | Range A |


    | P11 | Blue | Blue | $4000-5500$ | Medium short | Oscillographic recording |
    | :--- | :--- | :--- | :--- | :--- | :--- |
    | P12 | Orange | Orange | $5450-6800$ | Long | Radar |
    | P13 | Red-Orange | Red-Orange |  | Medium | No longer in general use |
    | P14 | Purple-Blue | Yellow-Orange | $3900-7100$ | One, medium short, <br> One, medium | Radar |
    | P15 | Green | Green | $3700-6050$ | Visible, short; <br> Ultraviolet, very short | Flying spot scanning <br> systems; photographic |
    | P16 | Blue-Purple and <br> near UV | Blue-Purple and <br> near UV | $3450-4450$ | Very short | Flying spot scanning <br> systems; photographic |
    | P17 | Yellow-White to <br> Blue-White | Yellow | $3800-6400$ | One, short; One, long | Radar |
    | P18 | White | White | $3260-7040$ | Medium to <br> medium short | Television |
    | P19 | Orange | Orange | $5450-6750$ | Long | Radar |
    | P20 | Yellow-Green | Yellow-Green | $4850-6700$ | Medium to <br> medium short | Radar |
    | P21 | Red-Orange <br> Tri-color | Red-Orange | $5540-6500$ | Medium <br> Medium short | Radar |
    | P23 | White | White | $4000-7200$ |  |  |

    ## GUIOE TO CRYSTAL SELECTION

    Important operating parameters are listed for various crystal cuts. The impedance of a crystal is close to zero at the resonant frequency $\left(f_{s}\right)$ and rises to a peak at the antiresonant frequency $\left(f_{d}\right)$. The practical parallel resonant operating frequency ranges between $f_{s}$ and $f_{s}$ and may include these two limiting values. The operating frequency is expressed as

    $$
    f_{p}=f_{s} \sqrt{1+\frac{C_{1}}{C_{0}}}
    $$

    The steep slope of the curve and the corresponding large differential between the impedances at $f_{s}$ and $f_{p}$ indicate that the $Q$ of the crystal is high. Also, the frequency separation between $f_{s}$ and $f_{p}$ is determined by the capacitance ratio $C_{o} / C_{1}$. For example, the $45^{\circ}$ cut is a favorite choice in crystal filters because of its low $C_{0} / C_{1}$ ratio. Thus a larger filter bandwidth is achieved with fewer crystals.
    

    The orientation of the better known crystal cuts shows the difference among the types.
    

    Equivalent circuit of a crystal includes the capacitances contributed by the wire leads and the holder in $C_{0}$. ratio of $C_{0}$ and $C_{1}$ indicates the frequency separation between the resonant and antiresonant frequencies of the crystal.
    

    The impedance of a crystal is near zero at the series resonant frequency, $f$ and reaches its peak at the antiresonant frequency, $F_{A}$. Steep slope between these two frequencies indicates a high $Q$.
    

    Temperature characteristics of four popular crystal cuts show the extremely stable behavior of the GT cut. Its frequency change is about 1 part per million over a $100^{\circ} \mathrm{C}$ range.

    | Cut | Designation | Mode of vibration | Frequency range in kHz | $\mathrm{C}_{0} / \mathrm{C}_{1}$ | Max. <br> drive <br> level | Remarks |
    | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
    | Duplex $5^{\circ} \mathrm{X}$ | J | Length, | 0.800-10 | 190-250 | 0.20 | Used in frequency and oscillator applications. Zerotemperature coefficient occurs at approximately room temperature; therefore the crystal is limited to oven operation and to rigid temperature-control conditions. |
    | XY | Custommade | Length, width | 3-50 | 600-900 | 0.1 | Suited for oven-control applications, especially in its optimum frequency range. |
    | NT | N | Length, | 4-150 | 800-1500 | 0.1 | Preferred in low-frequency oscillators and filters. It operates over large temperature ranges. Stability of $\pm 5$ ppm can be obtained over $\pm 5^{\circ} \mathrm{C}$, if ovencontrolled in the frequency range. Rugged, if properly mounted. <br> Can obtain frequency stability within $\pm 0.0025 \%$ over the normal roon-temperature range, withoul temperature control. |
    | $+5^{\circ} \mathrm{X}$ | H | Flexure | 5-140 | 225 | 0.1 | A relatively large frequency deviation over temperature range restricts filter applications to controlled environments. Low temperature coefficient and large ratio of stored mechanical energy to electrical energy are the characteristic features. <br> Used in wideband filters, below the range of practical size E plates, and in transistor oscillators, where LC circuits are not stable enough, or where there is a space problem. <br> Disadvantages: Fabrication difficulties. The crystal must be made in the form of a long, thin bar to fit in a special holder, to avoid jumping between modes. |
    | BT | B | Thickness | 1.75 | - | - | Thicker crystal possible at higher frequencies. Disadvantages: Too thick for low frequency. Also, difficult to fabricate and has zero-temperature coefficient over only a very small temperature range. Not as active as the AT. |
    | $-18-1 / 2^{\circ} \mathrm{X}$ | F | Extensional | 50-250 | 200 | - | Used principally in filters where low temperature coefficient is sacrificed for freedom from certain sputious responses. Suitable for multi-electrodes. |
    | $+5^{\circ} \mathrm{X}$ | E | Extensional | 50-250 | 130-160 | 2.0 | Mostly applicable in low-frequency filters, because of low $\mathrm{C}_{0} / \mathrm{C}_{1}$ and good temperature coefficient. |
    | DT | D | Face sheat | 80-500 | 450 | 2.0 | Suitable for oven and non-oven applications. Its low capacity ratıo permits many useful filter applications. Used as calibrator crystal and time base for frequency counters. Also used in FM and TV transmitters. <br> Disadvantage: Does not perform well over 500 kHz . |


    | Cut | Designation | Mode of vibration | Frequency range in kHz | $C_{0} / C_{1}$ | Max. <br> drive <br> level | Remarks |
    | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
    | MT | M | Extensional | 50-250 | 250 | 2.0 | Its low temperature coefficient makes it useful for oscillator control and for filters where low $C_{0} / C_{1}$ ratio is required along with low inductance and good temperature coefficient. However, this crystal is seldom used, because more compact units have replaced it. |
    | GT | G | Extensional | 85-400 | 375 | 0.1 | Has the greatest stability yet attained within a cut. Does not vary more than 1 part per million over a range of $100^{\circ} \mathrm{C}$. <br> Offiers a low temperature coefficient over a wide frequency range, by coupling any desired mode with another of nearly equal amplitude at a frequency equal to 0.86 times its natural frequency. <br> Used in frequency standards and when stability without temperature control or low impedance is essential. <br> Disadvantages: Most expensive of all types, because of painstaking labor required to obtain exact orientation in dimension. |
    | CT | C | Face shear | 300-1100 | $350-400$ | 2.0 | Provides a zero temperature coefficient in the shear mode for low frequencies. <br> Widely used in low-frequency osciliators and filters and does not require constant temperature control over normal operating conditions. Useful in filters because of low $\mathrm{C}_{0} / \mathrm{C}_{1}$ ratio. Popular in oscillators because of its low series resistance, especially above 400 kHz . <br> Disadvantages: Large face dimensions make it difficult to fabricate for the very low frequencies. |
    | X | Custommade | Extensional | 350-20,000 | - | - | Mechanically stable and an economic type of cut. Disadvantages: Large temperature coefficient, with the tendency to jump from one mode to another. |
    | SL | Custommade | Face shear, coupled to flexure | 300-800 | 450 | - | Electrical characteristics similar to DT, but it is larger, has better $Q$ and uniformity of characteristics above 300 kHz . Its various characteristics make it desirable for some filter applications. |
    | $Y$ | Y | Thickness, shear | 500-20,000 | - | - | Most active. Ratio of stored mechanical to electrical energy is large. is strong mechanically. Disadvantages: Large temperature coefficient and poor frequency spectrum. |
    | AT | A | Thickness | 550-20,000 fundamental $10,000-60,000$ (3rd overtone) 100,000 (5th overtone) | 10-100,000 | 1.0-8.0 | Excellent temperature and frequency characteristics. Its overtones are used in cases where the frequency should not change with oscillator reactance variations. <br> Designs provide suitable capabilities for satisfying $70-80 \%$ of all crystal requirements. Preferred for high-frequency oscillator-control wherever wide variation of temperature is encountered. Because of small size, it can be readily mounted to meet stringent vibration specifications. <br> Disadvantage: Difficult to fabricate for optimum operation without coupling between modes. |

    ## MILITARY NOMENCLATURE SYSTEM

    The AN nomenclature designation is assigned to:

    1. Complete sets of equipment and major components of military design.
    2. Groups of articles of commercial or military design which are grouped for a military purpose.
    3. Major articles of military design which are not part of, or used with, a set.
    4. Commercial articles where nomenclature facilitates identification and /or procedures.

    As applied to complete sets, the nomenclature consists of the two letters $A N$ followed by a slash and three indicator letters which indicate installation, type of equipment, and purpose. The number that may follow the letters indicates model number, and a subsequent letter refers to modification.

    FOR EXAMPLE: AN/APN-10B airborne-radar-navigational aid 10th model-second modification
    As applied to components, the AN nomenclature consists of one or two designator letters substituted for AN.
    FOR EXAMPLE: An indicator model 42 for use with APQ-13 is designated as ID-42 /APQ-13. Modifications are indicated by letters, for example, ID-42B /APQ-13
    Component Indicator Letters

    | AB-Support, antenna | HC-Crystal holder |
    | :---: | :---: |
    | AM-Amplifier | HD-Air conditioning apparatus |
    | AS-Antenna assembly | ID-Indicating device |
    | AT-Antenna | IL-Insulator |
    | BA - Battery, primary type | IM-Intensity measuring device |
    | BB-Battery, secondary type | IP-Indicator, cathode-ray tube |
    | BZ-Signal device, audible | $J$-Junction device |
    | C-Control article | KY-Keying device |
    | CA-Commutator assembly. sonar | LC-Tool, line construction LS-Loudspeaker |
    | CB Capacitor bank | M-Microphone |
    | CG-Cable and transmission | MD - Modulator |
    | CK line.rf | ME-Meter, portable |
    | CK Crystal kit | MK - Maintenance kit or equip |
    | CM-Comparator | ment |
    | CN -Compensator | ML-Meterological device |
    | CP-Computer | MT Mounting |
    | CR-Crystal | MX Miscellaneous |
    | CU-Coupling device | O Oscillator |
    | CV -Converter (electronic) | OA-Operating assembly |
    | CW Cover | OS-Oscilloscope, test |
    | CX -Cord | PD-Prime driver |
    | CY. Case | PF-Fitting, pole |
    | DA Antenna, dummy | PG-Pigeon article |
    | DT Detecting head | PH-Photographic article |
    | DY- Dynamotor | PP-Power supply ${ }^{\text {P }}$ |
    | E-Hoist assembly | PT-Plotting equipment |
    | F-Filter | PU-Power equipment |
    | FN-Furniture | R-Radio and radar receiver |
    | FR-Frequency measuring device | RD Recorder and reproducer RE-Relay assembly |
    | G-Generator | RF - Radio frequency com- |
    | GO-Goniometer | ponent |
    | GP. Ground rod H -Head, hand, and chest set | RG-Cable and transmission line, bulk r.f. |

    RL-Reel assembly
    RP-Rope and twine
    RR-Reflector
    RT - Receiver and transmitter
    S-Shel ter
    SA-Switching device
    SB-Switchboard
    SG-Generator, signal
    SM-Simulator
    SN-Synchronizer
    ST Strap
    T-Radio and radar transmitter
    TA-Telephone apparatus
    TD - Timing device
    TF. Transformer
    TG Positioning device
    TH - Telegraph apparatus
    TK-Tool kit or equipment
    TL-Tool
    TN- - Tuning unit
    TS-Test equipment
    TT - Teletypewriter and fac. simile apparatus
    TV - Tester, tube
    U-Connector, audio and power
    UG-Connector, r.f.
    $V$-Vehicle
    VS Signaling equipment, visual
    WD-Cable, two-conductor
    WF -Cable, two conductor
    WM - Cable, multuple conductor
    WS-Cable, single-conductor
    WT Cable, three conductor
    ZM - Impedance measuring device

    |  | Ist larter Dengeed Instationion Clasmes |  | $20 /$ lat ter <br> Trpe of Equipment |  | $3 d$ lerrer Purpose | Model Na . | Modif: carion lerter |  | Miscenlaneous Idantification |
    | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
    | A | Airborna (installed and opereted in aircraft). | A | Invisible light, hat radiation. | A | Auxiliary assemblies (not complete operating sets used with, or part of, two or more sets or sets serias). | $\begin{aligned} & 1 \\ & 2 \\ & 3 \\ & 4 \end{aligned}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~B} \\ & \mathrm{C} \\ & \mathrm{D} \end{aligned}$ | $\left.\begin{array}{l} x \\ y \\ z \\ T \end{array}\right\}$ | Chenges in voltage, phase, or frequency. <br> Treining. |
    | 8 | Underwater mobile, submarine. | $B$ | Pigeon. | B | Bombing. | etc. | etc. | (V) | Variabla grouping. |
    | C | Air trensportable finactrvatad, do not use). | c | Carrier. | C | Communications (recerving and transmitting). |  |  |  | , |
    | D | Plotlass Carrie. | D | Radiac. | D | Direction finder, reconnals: sance, end/or survaillance. |  |  |  |  |
    |  |  | E | Nupec. | E | Ejection and/or release. |  |  |  |  |
    | F | Fixed. | F | Photographic. |  |  |  |  |  |  |
    | G | Ground, general ground use (include two or more groundtype installetoons). | G | Telegraph or taletype. | G | Fire-control or searchlight directing. |  |  |  |  |
    |  |  |  |  | H | Racording end/or reproduc ing (grephic meteorological end sound). |  |  |  |  |
    |  |  | J | Intarphona and public eddress. <br> Electromechanical or inertial wire covered. |  |  |  |  |  |  |
    | K | Amphibious. | $K$ | Talemetering. | K | Computing |  |  |  |  |
    |  |  | L | Countarmaesures. | 1 | Searchlight control (Inactivated, use G). |  |  |  |  |
    | M | Ground, mobila (installed es opereting unut in a vahicla which hes no function othar then trensporting tha aquip. mant). | M | Meteorological. | M | Meintenanca and tast assemblias (including tools). |  |  |  |  |
    |  |  | N | Sound in arr. | N | Navigational ards fincluding eltimaters, baacons, compasses, racons, dapth sounding, epproach and landingl. |  |  |  |  |
    | P | Pack or portabla (animel or men). | P | Rader. | P | Reproducing finectiveted, do not use). |  |  |  |  |
    |  |  | 0 | Sonar and underwater sound. | 0 | Special, or combinetion of purposes. |  |  |  |  |
    |  |  | R | Radio. | R | Racaiving, passiva datecung |  |  |  |  |
    | 5 | Water surface craft. | S | Special types, megnetic, atc., or combinations of typas. | 5 | Datecting end/or renge and baaring, search. |  |  |  |  |
    | T | Ground, trensportabla. | T | Talephona (wira). | T | Trensmitting |  |  |  |  |
    | U | Genaral utility (includes two or mora generel installetion classes, errborne, shipboard, end ground). |  |  |  |  |  |  |  |  |
    | V | Ground, vahicular (installed in vahicle designed for functions other then carrying alactronic equipment, atc., such as tanks). | V | Visual and visible light. |  |  |  |  |  |  |
    | W | Water surfaca and underweter | W | Armamant (peculeer to armament, not otherwise covered). Fecsimile or talevision. Data processang. | W | Autometic flight or remota control. <br> Identification and recognition |  |  |  |  |

    This nomogram solves for the magnetic field strength, surrounding a power line, as a function of current in the line and the distance from it. Electronic equipment is susceptible to magnetic field interference, and this nomogram helps in determining the magnitude of the problem. For convenience the distance scale is calibrated in inches and centimeters.

    FOR EXAMPLE: The magnetic field strength at a point 5 cm from a line that carries 100 A is 4.2 gauss.

    ## Derivation of the Field-Strength Equation

    The field at point $P$ resulting from the current in segment $d l$ is given by

    $$
    d B=\mu_{0} \frac{l}{r^{2}} \cos \alpha d l
    $$

    If $d l$ is small, then

    $$
    \begin{aligned}
    d l \cos \alpha & =r d \alpha \\
    r & =R / \cos \alpha
    \end{aligned}
    $$

    and

    $$
    \therefore d B=\mu_{\circ} \frac{I}{R} \cos \alpha d \alpha
    $$

    If the line is very long with respect to $R$,

    $$
    B=\int_{-\pi / 2}^{\pi / 2} \mu_{0} \frac{l}{R} \cos \alpha d \alpha=\mu_{0} \frac{2 l}{R}
    $$

    If $B$ is in gauss, $l$ in amperes, and $R$ in centimeters, $\mu_{0}$ is equal to 0.1 .
    

    $$
    B=\mu_{0} \frac{2 I}{R}
    $$

    R
    (inches) (centimeters)
    
    
    INTERNATIONAL TIME MAP
    This map shows the number of hours to add or subtract from Eastern Standard Time to determine the time anywhere on earth.
    

    05648 060

    06590
    070
    07647
    

    ## PPM/ ${ }^{\circ} \mathrm{C}$ VS \% CHANGE CONVERSION CHART

    This chart is used to determine the \% change over a certain temperature range when the $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ characteristic is known or to determine the desired $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ for a maximum change over a given temperature range.

    FOR EXAMPLE: 1. What will be the change in capacitance of a capacitor with a TC of 750 ppm when used over a $60^{\circ}$ temperature range? Answer: $4.5 \%$
    2. What is the required stability in $\mathrm{ppm} /{ }^{\circ} \mathrm{C}$ of an oscillator that should not change in frequency by more than $1 \%$ when used between 10 to $90^{\circ} \mathrm{C}$ (i.e., temp. change $=80^{\circ} \mathrm{C}$ )? Answer: $125 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
    
    (Reprinted courtesy TRW Capacitor Division, Ogallala, Nebraska.)

    Troposphere, Stratosphere and Ionosphere
    

    WIND DESIGNATIDNS

    | Designation | Wind Speed $(\mathrm{mph})$ | Designation | Wind Speed (mph) |
    | :--- | :--- | :--- | :---: |
    | Calm | Less than 1 | Moderate gale | 32 to 38 |
    | Light air | 1 to 3 | Fresh gale | 39 to 46 |
    | Light breeze | 4 to 7 | Strong gale | 47 to 54 |
    | Gentle breeze | 8 to 12 | Whole gale | 55 to 63 |
    | Moderate breeze | 13 to 18 | Storm | 64 to 72 |
    | Fresh breeze | 19 to 24 | Hurnicane | Above 72 |

    Based on U.S. Weather Bureau data, this map shows the number of lightning storms occurring over a 20 -year period.
    

    This chart shows the "windchill" and state of comfort under varying conditions of temperature and wind velocity.
    

    ## WIND MAP OF THE U.S.

    This map shows the annual wind extremes in miles/hour, 30 feet above ground, 50 year mean recurrence interval.
    

    Wind map-annual extreme in miles per hour, 30 feet above ground, 50 year mean recurrence interval. From Thom "New Distribution of Winds in the United States". ASCE Proceedings, 1968.

    ## Steady Wind - miles/hour (as shown on map)

    6070 70 80 85 85 90 100 110 120

    ## Gusting Wind - equivalent miles/hour

    (using standard 1.3 gust factor)78 91 104 110 117 130 143 156
    (Reprinted from "SBC Square Beam Cutoff," Kim Lighting publication A5, page A5-10, courtesy Kim Lighting.)
    GROUND CONDUCTIVITY
    This map shows the effective ground conductivity in the United States in millimhos/meter. The conductivity of seawater (not shown) is assumed to be 5,000 millimhos/meter.
    

    ## THE TRIBOELECTRIC (OR ELECTROSTATIC) SERIES

    The table below is so arranged that any material becomes positively charged (that is, it gives up electrons) when rubbed with any material lower on the list. The farther apart the materials are on the list, the higher the charge will be. Surface conditions and variations in characteristics of some materials may alter some positions slightly.

    ```
    Positive polarity (+)
    Asbestos
    Rabbit's fur
    Glass
    Mica
    Nylon
    Wool
    Cat's fur
    Silk
    Paper
    Cotton
    Wood
    Lucite
    Sealing wax
    Amber
    Polystyrene
    Polyethylene
    Rubber balloon
    Sulphur
    Celluloid
    Hard rubber
    Vinylite
    Saran wrap
    Negative polarity (-)
    ```

    FOR EXAMPLE: A rubber balloon rubbed with nylon will produce a negative charge on the balloon and leave the nylon positively charged.

    ## CORROSION

    Galvanic corrosion occurs when two dissimilar metals are in contact, in a liquid capable of carrying an electric current. Under these conditions the least noble metal (the anode) corrodes, while the more noble metal (the cathode) is not attacked.

    In general, galvanic corrosion may be avoided by uniformity in the types of metals used. If uniformity is not practical, then metals should be used that are as close as possible to each other in the galvanic table, which lists metals in order of increasing nobility.

    Stainless steel is "active" when chemicals present do not allow the formation of an oxide film on the surface of the metal. The treatment of stainless steel in a passivating solution accelerates the formation of the oxide film, thus making it "passive" and thereby increasing its resistance to galvanic corrosion.
    

    | Material and Major Applicetion Considerations | Common Availeble Forms | Representetive Tradenames and Suppliers |
    | :---: | :---: | :---: |
    | Acetals <br> Good alectrical proparties at most frequancies, which ere little changed in humid environmants to $125^{\circ} \mathrm{C}$. Dutstanding machanical strength, stiffness, toughness, and dimensional stability. | Extrusions, injection moldings, stock shapas. | Dalrin (DuPont); Calcon (Calanese Corp.) |
    | Acrylics <br> Excellent resistance to arcing and elactrical tracking. Excellant clarity and resistance to outdoor waatharing. | Castings, ektrusions, injection moldings, tharmoformed parts, stock shapes, film, fiber. | Lucita (DuPont); Plaxiglas (Rohm and Hass Co.) |
    | Cellulosics <br> Good electrical properties and toughness. Used more for general-purpose applications than for ultimate in any electrical requiremant. Saveral types evailable. | Blow moldings, axtrusions, injection moldings, tharmoformed parts, film, fiber, stock shapas. | Tanite (Eastman Chamical Co.): Ethocal-EC (Dow Chamical Co.): Fortical-CAP (Celanese Corp.) |
    | Chlorineted Polyathars <br> Good alectrically, but most outstanding propartias ara corrosion resstance and physicel and thermal stability. | Extrusions, injaction moldings, stock shapas, film. | Panton (Harculas Powder Co.) |
    | Fluorocarbans <br> TFE. Electrically one of the most outstanding thermoplastic meterials. Vary low alectrical losses: very high electrical resistivity. Usaful from $-300^{\circ}$ to over $500^{\circ} \mathrm{F}$ Excellent high frequency dielectric. Hes excellent combinetion of mechanical and alectrical properties but is relatively weak in cold.flow properties Nearly inert chemically, as ara most fluorocarbons. Very low coefficient of friction. Nonflammabla | Compression moldings, stock shapes, film. | Tsflon TFE (DuPont); Halon TFE (Allied Chamical Corp.) |
    | FEP: Similar to TFE, except uselul temparatura limitad to ebout $400^{\circ} \mathrm{F}$ Easier to mold than TFE. <br> CTFE: Excellent electrical proparties and relatively good mechanicel properties. Stiffar than TFE and FEP, but does have some cold flow Useful to about $400^{\circ} \mathrm{F}$ | Extrusions, injection moldings, laminatas, film. <br> Extrusions, isostatic moldings, injection moldings, film, stock shapas. | Teflon FEP (DüPont) <br> Kal-F (3M Co.); Plaskon CTFE (Allied Chemical Corp.) |
    | PVF $_{2}$ Dne of the easiest of the flugrocarbons to process Stiffer and more resistant to cold flow than TFE Good electrically Useful to ebout $300^{\circ} \mathrm{F}$. Major electrical application is wire jacketing. | Extrusions, injaction moldings, Ieminatas, film. | Kynar (Pannsalt Chamicals Corp.) |
    | Nylons <br> Conventionel: Good general-purpose electrical proparties Eesily processed Good mechanical strangth and abrasion resistance and low coefficient of friction. Commonly used types of nylon era nylon 6 , nylon $6 / 6$ and nylon $6 / 10$. Some hava limited use in electrical applications beceuse of moistursabsorption properties. Nylon $6 / 10$ is best hera. | Extrusions, injection moldings, laminates, rotational moldings, stock shapas, film, fiber. | Zytel (DuPont); Plaskon (Allied Chamical Co.); Bakalite (Union Carbida Corp.) |
    | High-Tempereture. Hes excellent combination of thermel andurence ( to $200^{\circ} \mathrm{C}$ ) end electrical propertias Exhibits relatively low dialectric constant, high volume resistivity, and good dielectric strangth. Has high tensile strength and wear resistance. | Fiber, sheet, tape, paper, fabric. | Normex (DuPont) |
    | Polysulfones |  |  |
    | Good combination of thermal endurance to ovar $300^{\circ} \mathrm{F}$ ) end dielectric propertes. Ralativaly low dielecticic constant end dissipation factor, and high volume resistivity Elactrical properties are maintanad at $90 \%$ of initual valuas after ona yaar at $300^{\circ} \mathrm{F}$ Good dimansional stability and high ertep rasistanca Flama rasistant, and good charnical resistanca | Extrusions, injection moldings, tharmoformed parts, stock shapes, ffilm, sheet. | Polysulfona (Union Carbida Corp.) |


    | Mareriel end Mejor Application Consideretions |
    | :--- |
    | Parylenes |
    | Excellent low-loss dielectric properties end good |
    | dimensional stebility. Low permeebility to gases end |
    | moisture. Produced as a film on a substrete, from e |
    | vapor phese. Used primerily as thin films in capeci- |
    | tors and dielectric coetings. |

    Polycarbonetes
    Relatively low electrical losses and high voluma resistivity. Loss properties ere steble to ebout $150^{\circ} \mathrm{C}$. Excellent dimensional stebility, low weter absorption, low creep, end outstending impect resistence.

    ## Polyestars

    Outstending dielectric strength end tear strength. Widely usad for mechine-applied tepe insuletion. Hes high volume resistivity end low moisture ebsorption.

    Polyethylenes, Polypropylanes, Polyallomars
    Excellent electrical properties, especially low electricel losses. Tough end chamicelly resistant, but weak to varying degrees in creep end thermal resistence. Thermal stebility generelly increeses with density clesses of polyethylene. Polypropylenes are generally similer to polyethylenes, but offer ebout $50^{\circ} \mathrm{F}$ highar heat resistance. Polyallomers are electricelly similar to polyethylene and polypropylene but have better stress-creck resistanca and surfece hardness. Crosslinked polyethylanes provide improved thermal enduranca.

    Polyimides and Polyamida-imides
    Among the highest-temperature thermoplastics aveileble, heving useful operating tamperatures to about $700^{\circ} \mathrm{F}$ or higher. Excellent electrical proparties, good rigidity, end excellent thermel stebility.

    ## Polyphenylene Oxides (PPO)

    Excellant electrical properties, especielly loss propertias to above $350^{\circ} \mathrm{F}$, and over a wide frequency range. Good mechenicel strength end toughness. A lower-cost grode, Noryl, hes similer properties to PPO, but with e $75^{\circ}$ to $100^{\circ} \mathrm{F}$ reduction in heat resistence.

    ## Polystyranes

    Genaral-Purpose: Excellent electricel properties, especially loss properties. Conventionel polystyrans is temperaturs-limited, but high-temperature modifications such as Rexalite or Polypenco crosslinked polystyrene ere widely used, especielly for highfrequency epplications.
    ABS: Good general electricel properties but not outstending for eny spacific electric applicetion. Extremely tough, with high impect resistence. Can be formuleted over a wide renge of herdness and toughness properties. Special gredes avarleble for pleted surfeces.

    ## Vinyls

    Good low-cost, generel-purpose thermoplestic meteriels, but electrical properties ere not outstending. Properties are graetly influenced by plesticizers. Meny verietions aveilable, including flexibie and rigid types. Flexible vinyls, especielly PVC, ere widaly used for wire insuletion.
    Common Aveileb/a Forms
    Film coatings.

    Extrusions, injection mold-
    ings, thermoformed parts, ings, thermoformed parts, stock shepes, film.

    Films and tapes.

    Blow moldings, extrusions, injection molding, thermoformed parts, stock shapes, film, fiber, foam.

    Films, coetings, molded end mechined perts, resin solutions.

    Extrusions, injection moldings, thermoformed parts, stock shepes, film.

    Blow moldings, extrusions, injection moldings, rotetionel moldings, thermoformed perts, foam.

    Extrusions, injection moldings, thermoformed parts, leminetes, stock shepes, foem.

    Blow moldings, extrusions, injaction moldings, rotetionel moldings, film, sheet.

    | Representative Tradenames |
    | :---: |
    | and Suppliars |

    Parylene (Union Carbide Corp.)

    Lexen (G. E. Co.); Marlon (Mabay Chemical Co.)

    Mylar (OuPont); Scotchper (3M Co.): Celenar (Celanese Corp.)

    Alathon Polyethylene (OuPont); Petrothene Polyethylene IUSI Chamical Co.); Grax H. O. Polyethylene (Allied Chemical Corp.); Hi-Fax H. D. Polyethylane, ProFax Polypropylene (Hercules Powder Co.l; Tenite Polyethylene, Polypropylene, end Polyallomer (Eestman Chemical Co.)

    Vespal perts end shapes, Kapton film, and PyreM.L. resin (DuPont); Al (Amoco); Skybond (Monsanto Co.)

    PPO and Noryl (G. E. Co.)

    Styron (Dow Chernical Co.); Lustrex (Monsanto Co.); Rexolite (American Enka Corp.); Polypanco $0-200.5$ (Polymer Corp.)

    Marbon Cycolec (BorgWarner Corp.): Lustren (Monsanto Co.): Abson (Goodrich Chemical Co.)

    Oiemond PVC (Diamond Alkalı Co.): Pliovic (Goodyear Chemical Co.1; Seran (Oow Chamicel Co.)

    | Matarial and Major Application Considerations | Common Available Forms | Reprasentative Tradenames and Suppliers |
    | :---: | :---: | :---: |
    | Alkyds <br> Excaliant dialectric strangth, arc rasistance, and dry insulation rasistanca. Low dialactric constant and dissipation factor. Good dimansional stability. Easily molded. | Compression and transfar moldings. | Plaskon (Allied Chemical Corp.); Glaskyd (American Cyanamid Co.) |
    | Aminos (Matamina and Uraa) <br> Good general alectrical propertias, but not outstanding except for glass-filled malaminas whose hardnass and arc rasistanca maka them useful for molded conneectors. | Comprassion and transter moldings, extrusions, laminatas | Plaskon (Allied Chamical Corp.); Resimena (Monsanto Co.); Cymel malamine, Beatla urse (American Cyanamid Co.) |
    | Diallyl Phthalates (Allylics) <br> Unsurpassed ernong tharmosets in ratantion of alactrical propertias in high-humidity environmants. Also, thay have among the highast volume and surface resistivitus in tharmosets. Low dissipation fector and haat resistenca to $400^{\circ} \mathrm{F}$ or highar. Excallant dimansional stability. Easily molded. | Comprassion, injection, and transfer moldings; axtrusiona; laminatas. | Dapon (FMC Corp.); Diall (Allied Chemical Corp.l |
    | Epoxies <br> Good alactrical propartias, low shrinkage, axcallant dimansional stability, and good to axcallant adhesion. Eesy to compound, using nonpressura processes, for e variaty of and proparties. Usaful ovar e wida range of anvironments. | Castings; comprassion, injection, and transfer moldings; extrusions; Iaminatas; matched-dia moldings: filamant windings; foam. | Epon (Shall Chamical Co.); EpiRez (Jones-Dabney Co.); D.E.R. (Dow Chamical Co.l: Araldita (Ciba Products Co.); ERL (Union Carbida Corp.); Scotchcast (3M Co. 1 |
    | Phanolics <br> Good genaral alectrical propartias, laeding to wide use for genaral-purpose molded parts. Not outstanding in any specific electric property, but soma formulations have axcalient thermal stability above $300^{\circ} \mathrm{F}$. | Castings; compression, injection, and transfar moldings; axtrusions; laminatas; matched-die moldings: stock shapas; foam. | Bakelita (Union Carbide Corp.): Duraz (Hookar Chamical Corp.) |
    | Polyesters <br> Very low dissipation factor. Low-cost and extremaly aasy to compound using nonprassura procasses. Lika epoxias, they can be formulated for arthar room tamparature or alevated tamperatura use. Not equivalent to apoxias in anvironmental rasistanca. | Compression, injection, and transfar moldings: axtrusions; leminates; matched-dia moldings; filamant windings; stock shapas. | Selactron (Pittsburgh Plate Glass Co.l: Laminec (Amarican Cyanamid Co.); Paraplex (Rohm \& Hass Co. 1 |
    | Silicones (rigid) <br> Excallent alactrical proparties, espacially low dielectric constant and dissipation factor, which change little to $400^{\circ} \mathrm{F}$. | Castings, comprassion and transfar moldings, laminates. | DC Rasins (Dow Corning Corp.) |

    ## SIGNIFICANCE OF PROPERTIES OF ELECTRICAL INSULATING MATERIALS

    | Property end Definition |
    | :--- |
    | Dialectric Strangth |
    | All insuleting meteriels feil et some level of epplied voltege for a given set of |
    | opereting conditions. The dielectric strength is the voltege an insuleting |
    | materiel cen withstand before dielectric braekdown occurs. Dielectric |
    | strength is normally exprassed in voltege gradient terms, such es volts per |
    | mil. In testing for dielectric strength, two methods of epplying the voltege |
    | (gradual or by steps) ere used. Type of voltege, tamperature, and any pre- |
    | conditioning of the test pert must be noted. Also, thickness of the piece |
    | being tested must be recorded because the voltage per mil at which break- |
    | down occurs veries with thickness of test piece. Normally, breakdown occurs |
    | at a much higher volt-per-mil value in very thin test pieces (e few mils thick) |
    | than In thickar sections ( $1 / 3$ in. thick, for exemple). |

    ## Resistanca and Resistivity

    Resistance of en insuleting meteriel, like that of e conductor, is the resistence offered by the conducting peth to pessage of electricel current. Resistance is expressed in ohms. Insuleting meteriels are very poor conductors, offering high resistence. For insulating materials, the term volume resistivity is more commonly applied. Volume resistivity is the electrical resistence between opposite faces of e unit cube for a given metarial end et a given tempereture. The reletionship between resistance end resistivity is expressed by the equation $\rho=R, A / /$ where $\rho=$ volume resistivity in ohm-cm, $R=$ resistance in ohms between feces; $A=$ area of tha faces, and $/ \mathrm{m}$ distance between facas of the piece on which meesurement is made. This is not resistence per unit volume, which would ba ohm/ $\mathrm{cm}^{3}$-elthough this term is sometimes erroneously used. Other terms are sometimes used to describe a specific epplication or condition. One such term is surface resistivity, which is the resistence between two opposite edges of a surface film 1 cm squere. Since the length and width of the path are the same, the centimeter terms cencel. Thus, units of surface resistivity are actuelly ohms. However, to avoid confusion with usual resistance velues, surface resistivity is normally given in ohms/sq. Another broadly used term is insulation resistance, which, again, is a measurement of ohmic resistence for a given condition, rather than e stendardized resistivity test. For both surface resistivity and insulation resistence, standardized comperetive tests are normelly used. Such tests can provide dete such as effects of humidity on a given insuleting matarial configuretion.

    ## Dialectric Constant

    The dielectric constant of an insuleting meterial is the ratio of the cepacitance of a capacitor containing thet perticular material to the capacitance of the same electroda system with eir replacing the insuletion as the dielectric medium. The dielectric constant is also sometimes defined as the proparty of an insulation which determines the electrostatic energy stored within the solid material. The dielectric constent of most commarcial insulating materials varies from about 2 to 10 , eir heving the value 1 .

    ## Powar Factor and Dissipation Factor

    Power factor is the ratio of the power dissipated (watts) in en insulating materiel to the product of the effective voltage and current (volt-ampere input) end is a meesure of the relative dielectric loss in the insulation when the system acts as a capacitor. Power factor is nondimensionel and is a commonly used measure of insuletion quality. It is of perticular interest at high levels of frequency and power in such applications as microwave equipment, trensformers, and other inductive devices.

    Dissipetion factor is the tangent of the dielectric loss angle. Hence, the term tan defta (tangent of the angle) is also sometimes usad. For the low values ordinarily encountered in insulation, dissipation factor is prectically the equivalent of powar fector, and the terms are used interchangeably.

    ## Arc Resistanca

    Arc resistance is a meesure of an electrical breakdown condition along an insulating surfece, caused by the formation of a conductive path on the surface. It is a common ASTM measurement, especielly used with plastic materiels because of the veriations among plastics in the extent to which a surfaca breakdown occurs. Arc resistance is measured as the time, in seconds, required for breakdown along the surface of the material being measured. Surfaca breakdown (arcing or electrical tracking along the surface) is also affected by surface cleenliness and dryness.

    The highar the value, the better for a good insulating material. The resistence value for e given material depends upon e number of fectors. It veries inversaly with temperatura, end is affacted by humidity, moisture contant of the test part, level of the epplied voltage, and time during which the voltage is epplied. When tests are mada on epieca that has been subjected to moist or humid conditions, it is important that meesurements be made at controlled time intervals during or after the test condition has been applied, since dry-out and resistance increese occur rapidly. Comparing or interpreting deta is difficult unless the test period is controlled end dafined.

    Low values are best for high-frequancy or power epplications, to minimize electrical power losses. Higher values are best for capacitance applications. For most insulating materials, dialactric constent increases with temparature, es pecielly above a critical temparature region which is unique for each material. Dielectric constant velues are also affected (usually to a lesser dagree) by fraquency. This variation is also unique for each material.

    Low values ara favoreble, indicating a more afficient system, with lowar power losses.

    The higher the valua, the better. Higher valuas indicate greatar resistence to break. down along the surface due to arcing or trackıng conditions.

    To convert from Fahrenheit to Celsius*-locate temperature ( ${ }^{\circ} \mathrm{F}$ ) in center column and read ${ }^{\circ} \mathrm{C}$ in left column.
    To convert from Celsius* to Fahrenheit-locate temperature ( ${ }^{\circ} \mathrm{C}$ ) in center column and read ${ }^{\circ} \mathrm{F}$ in right column.
    
    

    | Interpolation Factors |  |  |  |  |  |  |  | Interpolation Factors |  |  |
    | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
    | $C$ | $F$ | $C$ | $F$ |  |  |  |  |  |  |  |
    | 0.56 | 1 | 1.8 | 3.33 | 6 | 10.8 |  |  |  |  |  |
    | 1.11 | 2 | 3.6 | 3.9 | 7 | 12.6 |  |  |  |  |  |
    | 1.67 | 3 | 5.4 | 4.44 | 8 | 14.4 |  |  |  |  |  |
    | 2.22 | 4 | 7.2 | 5.00 | 9 | 16.2 |  |  |  |  |  |
    | 2.78 | 5 | 9.0 | 5.56 | 10 | 18.0 |  |  |  |  |  |

    *The term Centigrade was officially changed to Celsius by international agreement in 1948. The Celsius scale uses the triple phase point of water, at $0^{\circ}$ Centigrade, in place of the ice point as a reference, but for all practical purposes the two terms are interchangeable.

    | ${ }_{0}^{5}$ | Temperature Conversion |  |  |  |  |
    | :---: | :---: | :---: | :---: | :---: | :---: |
    |  | Colsius | Fahrenheit | Kelvin | Reaumur | Rankine |
    | Cels. | - | $\left(\frac{9}{5} c\right)+32$ | $C+273.16$ | $\frac{4}{5} \mathrm{C}$ | $1.8(C+273.16)$ |
    | Fahr. | $\frac{5}{9}(F-32)$ | - | $\left[\frac{5}{9}(F-32)\right]+273.16$ | $\frac{4}{9}(F-32)$ | $F+459.7$ |
    | Kelvin | K-273.16 | $\left[\frac{9}{5}(K-273.16)\right]+32$ | - | $\frac{4}{5}(K-273.16)$ | K $\times 1.8$ |
    | Reau. | $\operatorname{Re} \times \frac{5}{4}$ | $\left(\frac{9}{4} \mathrm{Re}\right)+32$ | $\left(\frac{5}{4} R e\right)+273.16$ | - | $\left(\frac{9}{4} \mathrm{Re}\right)+491.7$ |
    | Rank. | $\frac{R a}{1.8}-273.16$ | Ra-459.7 | $\frac{R a}{1.8}$ | $\frac{4}{9}(R a-491.7)$ | - - |

    Five major temperature scales are in use at present. They are: Fahrenheit, Celsius, Kelvin (Absolute), Rankine, and Reaumur. The interrelationship among the scales is shown here.
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    
    

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    | 名ちな号 | －5\％\％\％ | ¢¢8×8 | 283xa |  |  |
    | 9\％8538 | 9\％8：8 | SRERER | 9\％Ex | 8\％ 2788 | 年 |

    To determine relative humidity from wet and dry bulb temperature readings，subtract the wet－bulb temperature from the dry－bulb temperature and find the number representing this difference in the top row．Follow that column vertically to find the relative humidity at the intersection of the horizontal column representing the dry－bulb reading． Tables are given for Celsius and Fahrenheit readings at sea level．
    FOR EXAMPLE：A dry－bulb reading of $88^{\circ} \mathrm{F}$ and a wet－bulb reading of $80^{\circ} \mathrm{F}$（difference $8^{\circ} \mathrm{F}$ ）indicates a relative humidity of $70^{\circ}$ ．

    The United States Weather Bureau developed the formula for temperature-humidity index. It is based on temperature and relative humidity.

    $$
    \mathrm{THI}=15+0.4\left(T_{\text {dry bulb }}+T_{\text {wet buib }}\right)
    $$

    where temperatures are in degrees Fahrenheit. It has been determined that when the THI reaches 72, some people are uncomfortable; when it reaches 76 most everyone is uncomfortable.

    Actually it is the combination of both high temperature and high humidity which causes discomfort. Lowering either one will increase comfort. On the other hand, lower temperature plus low humidity can cause discomfort on the cool side. Thus, in the wintertime, when the humidity in heated buildings is low, a higher temperature is needed for comfort than is required during other seasons when the humidity is higher.

    FOR EXAMPLE: At a dry-bulb temperature of $75^{\circ} \mathrm{F}$ and a relative humidity of $60 \%$, the THI is 71 .
    

    Commonly used terms to describe the color of heat are related to the approximate range of temperature.

    |  |  |  |  |
    | :--- | :--- | :--- | ---: |
    | Incipient red heat | $500-550$ | Yellow heat | 1050-1150 |
    | Dark red heat | $650-750$ | Incipient white heat | $1250-1350$ |
    | Bright red heat | $800-900$ | White heat | Above 1450 |
    | Orange-red heat | $900-1000$ |  |  |

    ## THERMAL SPECTRUM

    

    | AWG <br> B A S <br> Gauge | Dam. aver in Mils | Cross Section |  | Ohms/ <br> 1000 Ft <br> at $20^{\circ} \mathrm{C}$ <br> $168^{\circ} \mathrm{Fi}$ | $\stackrel{20}{1000} \mathrm{Ft}$ | Fi/Lb | Fi/Ohm at $20^{\circ} \mathrm{C}$ $168^{\circ} \mathrm{F} 1$ | Ohms/b <br> at $20^{\circ} \mathrm{C}$ <br> $158^{\circ} \mathrm{F}$ ) | $\begin{aligned} & \mathrm{Lb} / O \mathrm{Am} \\ & \text { \& } 20^{\circ} \mathrm{C} \\ & \left(=68^{\circ} \mathrm{F}\right) \end{aligned}$ |
    | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
    |  |  | Circular Mils | Square Incher |  |  |  |  |  |  |
    | 0000 | 4600 | 211,600 | 0.1662 | 0.04901 | 6405 | 1561 | 20,400 |  |  |
    | 000 | 4096 | 167.800 | 01318 | 006180 | 507.9 | 1968 | 16,180 | 000007652 00001217 | 13.070 8.219 |
    | 00 | 364.8 | 133,100 | 0.1045 | 007793 | 402.8 | 2482 | 12.830 | 00001935 | $\begin{aligned} & 8,219 \\ & 5,169 \end{aligned}$ |
    | 0 | 324.9 | 105.500 | 0.08289 | 009827 | 3195 | 3130 | 10,180 | 00003076 | 3.251 |
    | 1 | 2893 | 83,690 | 0.06573 | 0.1239 | 2533 | 3947 | 8.070 | 00004891 | 2.044 |
    | 2 | 257.6 | 66,370 | 0.05213 | 01563 | 2009 | 4977 | 6.400 | 00007778 | 1.286 |
    | 3 | 2294 | 52,640 | 004134 | 0.1970 | 159.3 | 6276 | 5,075 | 0001237 | 1.286 8086 |
    | 4 | 204.3 | 41.740 | 0.03278 | 0.2485 | 1264 | 7.914 | 4,025 | 0001966 | 5085 |
    | 5 | 181.9 | 33,100 | 002600 | 0.3133 | 100.2 | 9980 | 3,192 | 0003127 | 3198 |
    | 6 | 1620 | 26.250 | 002062 | 03951 | 7946 | 1258 | 2,531 | 0004972 | 2011 |
    | 7 | 1443 | 20,820 | 0.01635 | 04982 | 6302 | 1587 | 2,007 | 0007905 | 1265 |
    | 8 | 1285 | 16,510 | 0.01297 | 0.6282 | 4998 | 2001 | 1,592 | 001257 | 1265 7955 |
    | 9 | 1144 | 13,090 | 0.01028 | 0.7921 | 39.63 | 2523 | 1.262 | 001999 | 5003 |
    | 10 | 1019 | 10.380 | 0008155 | 09989 | 3143 | 3182 | 1,001 | 003178 | 3147 |
    | 11 | 90.74 | 8,234 | 0006467 | 1260 | 2492 | 4012 | 794 | 005053 | 1979 |
    | 12 | 8081 | 6,530 | 0005129 | 1.588 | 1977 | 50.59 | 629 | 008035 | 1245 |
    | 13 | 71.96 | 5,178 | 0004067 | 2.003 | 1568 | 6380 | 499.3 | 01278 | 7827 |
    | 14 | 6408 | 4,107 | 0003225 | 2.525 | -12.43 | 8044 | 396.0 | 02032 | 4922 |
    | 15 | 5707 | 3,257 | 0002558 | 3.184 | 9858 | 101.4 | 314.0 | 03230 | 4922 |
    | 16 | 5082 | 2,583 | 0002028 | 4016 | 7818 | 1279 | 249.0 | 05136 | 1947 |
    | 17 | 45.26 | 2.048 | 0001609 | 5064 | 6200 | 161.3 | 197.5 | 08167 | 1224 |
    | 18 | 40.30 | 1624 | 0001276 | 6385 | 4917 | 2034 | 156.6 | 1299 | 07700 |
    | 19 | 3589 | 1,288 | 0001012 | 8051 | 3899 | 2565 | 124.2 | 2065 | 4843 |
    | 20 | 3196 | 1,022 | 00008023 | 1015 | 3092 | 3234 | 98.50 | 3283 | 3843 |
    | 21 | 28.46 | 8101 | 0.0006363 | 12.80 | 2452 | 4078 | 78.11 | 5221 | 3046 1915 |
    | 22 | 25.35 | 6424 | 0.0005046 | 16.14 | 1945 | 5142 |  |  | 1205 |
    | 23 | 22.57 | 5095 | 00004002 | 2036 | 1542 | 6484 | 61.95 49.13 | 8301 1320 | 1205 07576 |
    | 24 | 20.10 | 4040 | 00003173 | 2567 | 1223 | 8177 | 38.96 | 2099 | 04765 |
    | 25 | 17.90 | 3204 | 00002517 | 3237 | 09699 | 1,0310 | 30.90 | 3337 | 02997 |
    | 26 | 1594 | 2541 | 00001996 | 4081 | 0.7692 | 1,300 | 24.50 | $5306$ | 02997 01885 |
    | 27 | 1420 | 201.5 | 00001583 | 51.47 | 06100 | 1.639 | 19.43 | 8437 | 01185 |
    | 28 | 1264 | 1598 | 00001255 | 6490 | 04837 | 2,067 | 1943 | 1342 | 01185 |
    | 29 | 1126 | 1267 | 000009953 | 8183 | 03836 | 2.607 | 1541 12.22 | 2133 | 007454 004688 |
    | 30 | 1003 | 1005 | 000007894 | 1032 | 03042 | 3.287 | 9691 | 3392 | $002948$ |
    | 31 | 8928 | 7970 | 000006260 | 1301 | 02413 | 4.145 | 7.685 | 5393 | 001854 |
    | 32 | 7950 | 6321 | 000004964 | 1641 | 01913 | 5,227 | 6.095 | 8576 | $001166$ |
    | 33 | 7080 | 5013 | 000003937 | 2069 | 01517 | 6,591 | 4.833 | 1,364 | 0007333 |
    | 34 | 6305 | 3975 | 000003122 | 2609 | 01203 | 8,310 | 3.833 | 2,168 | 0007333 |
    | 35 | 5615 | 3152 | 000002476 | 3290 | 009542 | 10.480 | 3.040 | 2,168 3,448 | 0004612 |
    | 36 | 5000 | 2500 | 000001964 | 4148 | 007568 | 13.210 | 2411 | 5.482 | $0001824$ |
    | 37 | 4453 | 1983 | 000001557 | 5231 | 006001 | 16.660 | 1912 | 8.717 | $0001147$ |
    | 38 | 3965 | 1572 | 000001235 | 6596 | 004759 | 21,010 | 1516 | 13,860 | $00007215$ |
    | 39 | 3531 | 1247 | 0000009793 | 8318 | 003774 | 26.500 | 1.202 | 13,860 22,040 | $\begin{aligned} & 00007215 \\ & 00004538 \end{aligned}$ |
    | 40 | 3145 | 9888 | 0000007766 | 10490 | 002993 | 33,410 | 095.34 | 35,040 | $00002854$ |

    Temperature coefficient of resistance: The resistance of a conductor at temperature $t$ in degrees Celsius is given by

    $$
    R_{1}=R_{20}\left[1+a_{20}(t-20)\right]
    $$

    where $R_{20}$ is the resistance at $20^{\circ} \mathrm{C}$ and $\mathrm{a}_{20}$ is the temperature coefficient of resistance at $20^{\circ} \mathrm{C}$. For copper, $a_{20}$ $=0.00393$. That is, the resistance of a copper conductor increases approximately $0.4 \%$ per degree celsius rise in
    temperature.

    PROPERTIES OF COMMON WIRE ANO CABLE INSULATIONS

    | Insulation Material | Breakdown Voltage | R. $F$. <br> Losses | Operating <br> Temp. ( $\left.{ }^{\circ} \mathrm{C}\right)$ | Weather Resistance | Flexibility | Suggested Use |
    | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
    | Standard PVC | High | Medium | -20 to +80 | Good | Fair | General purpose |
    | Premium PVC | High | Medium | -55 to +105 | Good | Fair | General purpose |
    | Polyethylene | High | Low | -60 to +80 | Good | Good | R. f. cables |
    | Natural rubber | High | High | -40 to +70 | Poor | Good | Light duty |
    | Neoprene | Low | High | -30 to +90 | Good | Good | Rough service |
    | Waxed cotton | Low | High |  | Poor | Good | Experimenting |
    | Teflon | High | Low | -70 to +260 | Good | Fair | High temperature |

    ## WIRE STRANDING CHART

    A stranded conductor is made up of a number of smaller wire strands. This chart shows the size of each strand, when the number of strands in the finished wire size is known. Also, the number of strands for each given strand size may be determined for a finished wire gauge size.

    Locate the conductar's desired AWG size an the chart and trace it vertically. The number and size af strands needed ta make the stranded canductar will be indicated by the harizantal line (strand number) and diaganal line (strand size), respectively.

    ## For example:

    A \#22 AWG stranded conductor can be made with 4 strands of \#28 AWG wire or 10 strands of \#32 AWG wire, etc.
    

    | Class | Definition |  |
    | :---: | :---: | :---: |
    | 0 | Materials or combinations of materials such as cotton, silk, and paper without impregnation. Other materials or combinations of materials may be included in this class if by experience or accepted tests they can be shown to be capable of operation at | 90 C |
    | A | Materials or combinations of materials such as cotton, silk, and paper when suitably impregnated or coated or when immersed in a dielectric liquid such as oil. Other materials or combinations of materials may be included in this class if by experience or accepted tests they can be shown to be capable of operation at | 105C |
    | B | Materials or combinations of materials such as mica, glass fiber, asbestos, etc., with suitable bonding substances. Other materials or combinations of materials, not necessarily inorganic, may be included in this class if by experience or accepted tests they can be shown to be capable of operation at | 130C |
    | F | Materials or combinations of materials such as mica, glass fiber, asbestos, etc., with suitable bonding substances. Other materials or combinations of materials, not necessarily inorganic, may be included in this class if by experience or accepted tests they can be shown to be capable of operation at | 155C |
    | H | Materials or combinations of materials such as silicone elastomer, mica, glass fiber, asbestos, etc., with suitable bonding substances such as appropriate silicone resins. Other materials or combinations of materials may be included in this class if by experience or accepted tests they can be shown to be capable of operation at | 180C |
    | 220C | Materials or combinations of materials which by experience or accepted tests can be shown to be capable of operation at | 220 C |
    | Over <br> 220 C (class C) | Insulation that consists entirely of mica, porcelain, glass, quartz, and similar inorganic materials. Other materials or combinations of materials may be included in this class if by experience or accepted tests they can be shown to be capable of operation at temperatures over | 220 C |

    ## NOTES:

    1. Insulation is considered to be "impregnated" when a suitable substance provides a bond between components of the structure and also a degree of filling and surface coverage sufficient to give adequate performance under the extremes of temperature, surface contamination (moisture, dirt, etc.), and mechanical stress expected in service. The impregnant must not flow or deteriorate enough at operating temperature so as to seriously affect performance in service.
    2. The electrical and mechanical properties of the insulation must not be impaired by the prolonged application of the limiting insulation temperature permitted for the specific insulation class. The word "impaired" is here used in the sense of causing any change which could disqualify the insulating material for continuously performing its intended function whether creepage spacing, mechanical support, or dielectric barrier action.
    3. In the above definitions the words "accepted tests" are intended to refer to recognized Test Procedures established for the thermal evaluation of materials by themselves or in simple combinations. Experience or test data, used in classifying insulating materials are distinct from the experience or test data derived for the use of materials in complete insulation systems. The thermal endurance of complete systems may be determined by Test Procedures specified by the responsible Technical Committees. A material that is classified as suitable for a given temperature may be found suitable for a different temperature, either higher or lower, by an insulation system Test Procedure. For example, it has been found that some materials suitable for operation at one temperature in air may be suitable for a higher temperature when used in a system operated in an inert gas atmosphere.
    4. It is important to recognize that other characteristics, in addition to thermal endurance, such as mechanical strength, moisture resistance and corona endurance, are required in varying degrees in different applications for the successful use of insulating materials.

    This nomogram can be used to determine:

    1. The minimum wire size for any given load current and voltage drop;
    2. the mV drop/foot for any given wire size and load current;
    3. the maximum recommended* current for any given size wire.

    FOR EXAMPLE: 1 . With a permissible voltage drop of $5 \mathrm{mV} / \mathrm{ft}$, the minimum wire size in a 3-A circuit is \#12 AWG.
    2. At 300 mA the voltage drop across \#22 AWG wire is $4.5 \mathrm{mV} / \mathrm{ft}$.
    3. The maximum recommended current for \#18 AWG wire is 3.5 A . (This is found by connecting point A on the IR drop scale with the wire gauge scale, and reading the intersect point on the Current scale).
    
    *Based on an arbitrary minimum 500 circular mils per ampere. High-temperature class insulation will safely allow higher current.

    ## FUSING CURRENTS OF WIRES

    This table gives the fusing currents in amperes for five commonly used types of wires. The current l in amperes at which a wire will melt can be calculated from $I=K d^{3 / 2}$ where $d$ is the wire diameter in inches and $K$ is a constant that depends on the metal concerned. A wide variety of factors influence the rate of heat loss, and these figures must be considered approximations.
    

    ## SUGGESTED AMPACITIES FOR APPLIANCE WIRING MATERIAL—ALL TYPES OF INSULATION

    | Copper Temperature |  |  |  |  |  |  |
    | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
    | Amperes per Conductor |  |  |  |  |  |  |
    | 30 | 3 | 3 | 3 | 4 | 4 | CURRENT RATING FOR DIFFERENT CONDUCTOR MATERIALS MAY BE CALCULATED BY MULTIPLYING THE APPROPRIATE COPPER CONDUCTOR RATING BY THE FOLLOWING FACTORS: |
    | 28 | 4 | 4 | 5 | 6 | 6 |  |
    | 26 | 5 | 5 | 6 | 7 | 8 |  |
    | 24 | 7 | 7 | 8 | 10 | 11 |  |
    | 22 | 9 | 10 | 11 | 13 | 14 |  |
    | 20 | 12 | 13 | 14 | 17 | 19 | Nickel - clad copper 0.87 |
    | 18 | 25 | 20 | 22 | 26 | 29 | Nickel 0.43 |
    | 16 | 27 | 28 | 30 | 36 | 38 | Note: The ultimate temperature an appliance wire reaches is |
    | Correction Factors For Various Air Temperatures |  |  |  |  |  | influenced more by its proximity to heat sources (resistors, motors, etc.), within the appliance than by the |
    | 30 C | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | current flowing in the wire itself. The ratings, therefore, |
    | 40 | 0.91 | 0.93 | 0.95 | 0.97 | 0.98 | should only be used as a guide. In no case should the |
    | 50 | 0.82 | 0.85 | 0.89 | 0.94 | 0.95 | wire be used in a manner that will cause it to exceed its |
    | 60 | 0.71 | 0.77 | 0.83 | 0.91 | 0.93 | maximum temperature rating. |
    | 70 | 0.58 | 0.68 | 0.76 | 0.87 | 0.91 |  |
    | 80 | 0.41 | 0.57 | 0.69 | 0.84 | 0.87 |  |
    | 90 | ... | 0.44 | 0.61 | 0.80 | 0.83 |  |
    | 100 |  | 0.25 | 0.51 | 0.77 | 0.80 |  |
    | 125 |  | ... | ... | 0.66 | 0.69 |  |
    | 150 |  |  |  | 0.54 | 0.56 |  |
    | 200 | ... | . . | $\ldots$ |  | 0.43 |  |

    ## AUDIO LINE TABLE

    This chart shows the maximum length of line that can be used between an amplifier and speaker(s) that would assure that the power loss does not exceed $15 \%$ in low-impedance circuits, and $5 \%$ in high-impedance circuits.

    When several speaker lines are brought separately to an amplifier, calculations must be made for each line independently.

    FOR EXAMPLE: Four 16 -ohm speakers are connected in parallel to the 4 -ohm tap for perfect impedance match. Line losses are calculated for each line on the basis of the 16 -ohm impedance rather than the combined 4 -ohm impedance.

    | Wire Size (B and S) | 4 ahms | Load Impedance 8 ohms | 16 ohms |
    | :---: | :---: | :---: | :---: |
    | 14 | 125 ft | 250 ft | 450 ft |
    | 16 | 75 ft | 150 ft | 300 ft |
    | 18 | 50 ft | 100 ft | 200 ft |
    | 20 | 25 ft | 50 ft | 100 ft |
    | Maximum Length of Line for 5\%-Power Loss-High Impedance Lines |  |  |  |
    | Wire Size ( $B$ and $S$ ) | 100 ohms | Load Impedance 250 ohms | 500 ohms |
    | 14 | 1000 ft | 2500 ft | 5000 ft |
    | 16 | 750 ft | 1500 ft | 3000 ft |
    | 18 | 400 ft | 1000 ft | 2000.ft |
    | 20 | 250 ft | 750 ft | 1500 ft |

    ## SPARK-GAP BREAKDOWN VOLTAGES

    The curves are for a voltage that is continuous or at a frequency low enough to permit complete deionization between cycles, between needle points, or clean, smooth, spherical surfaces (electrodes ungrounded) in dust-free clean air. Temperature is $25^{\circ} \mathrm{C}$ and pressure is 760 mm ( 29.9 in .) of mercury. Peak kilovolts shown in the graph should be multiplied by the factors given in the table for other atmospheric conditions.

    An approximate rule for uniform fields at all frequencies up to at least 300 MHz is that the voltage breakdown gradient of air is 30 peak $\mathrm{kV} / \mathrm{cm}$ or 75 peak $\mathrm{kV} / \mathrm{in}$. at sea level ( 760 mm of mercury) and normaltemperature ( $25^{\circ}$ C). The breakdown voltage is approximately equal to pressure and inversely proportional to absolute ( ${ }^{\circ} \mathrm{Kelvin}$ ) temperature.
    

    Spark-gap breakdown voltages.
    Table of Multiplying Factors

    | Pressure |  |  |  |  |  |  |  |  |
    | ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
    | (in. <br> $\mathrm{Hg})$ | $(\mathrm{mm})$ |  |  |  |  |  |  |  |
    | $\mathrm{Hg})$ | -40 | -20 | 0 | 20 | 40 | 60 |  |  |
    | 5 | 127 | 0.26 | 0.24 | 0.23 | 0.21 | 0.20 | 0.19 |  |
    | 10 | 254 | 0.47 | 0.44 | 0.42 | 0.39 | 0.37 | 0.34 |  |
    | 15 | 381 | 0.68 | 0.64 | 0.60 | 0.56 | 0.53 | 0.50 |  |
    | 20 | 508 | 0.87 | 0.82 | 0.77 | 0.72 | 0.68 | 0.64 |  |
    | 25 | 635 | 1.07 | 0.99 | 0.93 | 0.87 | 0.82 | 0.77 |  |
    | 30 | 762 | 1.25 | 1.17 | 1.10 | 1.03 | 0.97 | 0.91 |  |
    | 35 | 889 | 1.43 | 1.34 | 1.26 | 1.19 | 1.12 | 1.05 |  |
    | 40 | 1016 | 1.61 | 1.51 | 1.42 | 1.33 | 1.25 | 1.17 |  |
    | 45 | 1143 | 1.79 | 1.68 | 1.58 | 1.49 | 1.40 | 1.31 |  |
    | 50 | 1270 | 1.96 | 1.84 | 1.73 | 1.63 | 1.53 | 1.44 |  |
    | 55 | 1397 | 2.13 | 2.01 | 1.89 | 1.78 | 1.67 | 1.57 |  |
    | 60 | 1524 | 2.30 | 2.17 | 2.04 | 1.92 | 1.80 | 1.69 |  |

    ## PRINTERS

    The family trees show the various types of serial and parallel printers and how they relate.
    

    The American Standard Code for Information Interchange (ASCII code) is used extensively in computer data transmission. The ASCII Code produced by most computer keyboards is shown here.
    

    | NUL | Null, or all zeros |
    | :--- | :--- |
    | SOH | Start of heading |
    | STX | Start of text |
    | ETX | End of text |
    | EOT | End of transmission |
    | ENQ | Enquiry |
    | ACK | Acknowledge |
    | BEL | Bell, or alarm |
    | BS | Backspace |
    | HT | Horizontal tabulation |
    | LF | Line feed |
    | VT | Vertical tabulation |
    | FF | Form feed |
    | CR | Carriage return |
    | SO | Shift out |
    | SI | Shift in |
    | DLE | Data link escape |

    DC1
    DC2
    DC3
    DC4
    NAK
    SYN
    ETB
    CAN
    EM
    SUB
    ESC
    FS
    GS
    RS
    US
    SP
    DEL

    Device control 1
    Device control 2
    Device control 3
    Device control 4
    Negative acknowledge
    Synchronous idle
    End of transmission block
    Cancel
    End of medium
    Substitute
    Escape
    File separator
    Group separator
    Record separator
    Unit separator
    Space
    Delete

    BAUDOT CODE
    The Baudot Code is a 5 -bit code suitable for punched paper tape and standard teletypewriter operation. In addition to the five bits per character, each character is preceded by a start bit, which is a space, followed by a stop bit, which is a mark, approximately $11 / 2$ times longer than the regular data mark.

    | CHARACTER | IMPULSE POSITION |  |  |  |  |
    | :---: | :---: | :---: | :---: | :---: | :---: |
    | LOWER UPPER CASE CASE |  | 2 | 3 | 4 | 5 |
    | A - | - | - |  |  |  |
    | B ? | - |  |  | - | - |
    | C |  | - | - | - |  |
    | D 3 | - |  |  | - |  |
    | E 3 | - |  |  |  |  |
    | F ! | - |  | - | - |  |
    | G a |  | - |  | - | - |
    | H |  |  | - |  | - |
    | 18 |  | - | - |  |  |
    | $\checkmark$, | - | - |  | - |  |
    | K | - | 0 | - | - |  |
    | L ) |  | - |  |  | - |
    | M |  |  | - | - | - |
    | N |  |  | - | - |  |
    | $0 \quad 9$ |  |  |  | - | - |
    | $P \quad 0$ |  | - | - |  | $\bullet$ |
    | $0 \quad 1$ | - | - | - |  | - |
    | R 4 |  | - |  | - |  |
    | 5 Boll | - |  | - |  |  |
    | $T$ 5 |  |  |  |  | - |
    | U 7 | - | - | - |  |  |
    | $V$ i |  | - | - | - | $\bigcirc$ |
    | W 2 | - | $\bigcirc$ |  |  | - |
    | $x \quad 1$ | - |  | $\bigcirc$ | - | - |
    | $Y$ \% | - |  | - |  | $\bigcirc$ |
    | 2 " | - |  |  |  | $\bigcirc$ |
    | LETTERS Lower Case | - | - | - | - | - |
    | FIGURES Upper Cose. | $\bigcirc$ | - |  | $\bigcirc$ | - |
    | SPACE |  |  | - |  |  |
    | CARRIAGE RETURN |  |  |  | - |  |
    | LINE FEED |  | - |  |  |  |
    | BLANK |  |  |  |  |  |

    NOTE: PRESENCE OF INDICATES MARKING IMPULSE

    ABSENCE OF - INDICATES SPACING IMPULSE

    ## GRAPHIC SYMBOLS FOR ELECTRONIC DIAGRAMS

    ## Semiconductors

    

    ## Optoelectronic Devices

    FIELD-EFFECT TRANSISTORS (FETs)
    
    three-terminal depletion-type
    insulated-gate (IGFET)
    
    threeterminal depletion-type IGFET, substrate tred to source
    
    four-terminal depletion-type IGFET
    
    four-terminal enhancement-type IGFET
    
    five-terminal dual gate depletion-type IGFET
    
    five-terminal dual-gate enhancement-type IGFET
    
    

    OIODES
    light-emittung drode (LED)
     00
    photodiode
    
    npn bedirectional photodiode (photo-duo diode)
    
    pnp bidirectional photodiode (photo-duo-diode)
    
    pnp two-segment photodiode. mip two-segment phomon cathode
    
    pno four-quadrant photodiode, with common cathode
    

    ## TRANSISTORS

    npn phototransistor, no base connection
    
    npn phototransistor, npn photorransustor.
    

    OPTICALLY COUPLED ISOLATORS
    with photodiode output
    
    with phototransistor output. no bese connection
    
    with phototransestor output, and base connection
    
    with photo-Darlington output, no base
    
    with photo Darlington output, and base
    
    with photodiode and amplifiertransistor output
    
    with NAND-gate-photodetector output
    

    ## Two-State Logic Devices

    Fundamental Circuit Components
    

    ## Contacts, Switches, and Relays

    

    Transmission Path
    CABLE
    twoconductor cable
    with grounded shield
    coaxial cable with
    grounded shield

    Microwave Circuits
    COUPLING
    coupling by loop to space
    DIRECTIONAL
    COUPLERS
    dual directional coupler

    | coupling by loop to |
    | :--- |
    | guided transmassion |
    | path |
    | coupling by loop from |
    | coaxial to circular |
    | grounds connected |


    |  | css-Esu | Multiply by to get CGS-Emu |  | Mnitiply by to get Rationalized MKs |  |
    | :---: | :---: | :---: | :---: | :---: | :---: |
    | 1. Length | Centimeter | 1 | Centimeter | $10^{-2}$ | Meter |
    | 2. Mass | Gram | 1 | Gram | $10^{-3}$ | Kilogram |
    | 3. Force | Dyne | 1 | Dyne | $10^{-5}$ | Newton, Dyne-five |
    | 4. Energy, Work | Erg | 1 | Erg | $10^{-7}$ | Joule |
    | 5. Power | Erg/second | 1 | Erg/second | $10^{-7}$ | Watt |
    | 6. Electric Charge | Statcoulomb | $3.335 \times 10^{-11}$ | Abcoulomb | 10 | Coulomb |
    | 7. Linear Charge Density | Statcoulomb/cm. | $3.335 \times 10^{-11}$ | Abcoulomb/cm. | $10^{3}$ | Coulomb/m. |
    | 8. Surface Charge Density | Statcoulomb/cm. ${ }^{2}$ | $3.335 \times 10^{-11}$ | Abcoulomb/cm. ${ }^{2}$ | $10^{5}$ | Coulomb/m. ${ }^{2}$ |
    | 9. Volume Charge Density | Statcoulomb/cm. ${ }^{2}$ | $3.335 \times 10^{-11}$ | Abcoulomb/cm. ${ }^{3}$ | $10^{7}$ | Coulomb/m. ${ }^{2}$ |
    | 10. Electric Flux | Statcoulomb | $3.335 \times 10^{-11}$ | Abcoulomb | 10 | Coulomb |
    | 11. Displacement, Electric Flux Density | Statcoulomb/cm. ${ }^{2}$ | $3.335 \times 10^{-11}$ | Abcoulomb/cm. ${ }^{2}$ | $10^{5}$ | Coulomb/m. ${ }^{2}$ |
    | 12. Polarization | Statcoulomb/cm. ${ }^{2}$ | $3.335 \times 10^{-11}$ | Abcoulomb/cm. ${ }^{2}$ | $10^{5}$ | Coulomb/m. ${ }^{2}$ |
    | 13. Electric Dipole Moment | Statcoulomb-cm. | $3.335 \times 10^{-11}$ | Abcoulomb-cm. | $10^{-1}$ | Coulomb-m. |
    | 14. Potential | Statvolt | $2.998 \times 10^{10}$ | Abvolt | $10^{-8}$ | Volt |
    | 15. Electric Field Intensity | Statvolt/cm. | $2.998 \times 10^{10}$ | Abvolt/cm. | $10^{-6}$ | Volt/m. |
    | 16. Current | Statampere | $3.335 \times 10^{-11}$ | Abampere | 10 | Ampere |
    | 17. Surface Current Density | Statampere/cm. | $3.335 \times 10^{-11}$ | Abampere $/ \mathrm{cm}$. | $10^{3}$ | Ampere/m. |
    | 18. Volume Current Density | Statampere/cm. ${ }^{2}$ | $3.335 \times 10^{-11}$ | Abampere/cm. ${ }^{2}$ | $10^{3}$ | Ampere/m. ${ }^{2}$ |
    | 19. Resistance | Statohm | $8.988 \times 10^{20}$ | Abohm | $10^{-9}$ | Ohm |
    | 20. Resistivity | Statohm-cm. | $8.988 \times 10^{20}$ | Abohm-cm. | $10^{-11}$ | Ohm-m, |
    | 21. Conductance | Statmho | $1.113 \times 10^{-21}$ | Abmho | $10^{9}$ | Mho |
    | 22. Conductivity | Statmho/cm. | $1.113 \times 10^{-21}$ | Abmho/cm. | $10^{\prime \prime}$ | Mho/m, |
    | 23. Capacity | Statfarad, Cm. | $1.113 \times 10^{-81}$ | Abfarad | $10^{9}$ | Farad |
    | 24. Elastance | Statdaraf | $8.988 \times 10^{20}$ | Abdaraf | $10^{-9}$ | Daraf |
    | 25. Dielectric Constant, Permittivity | - | $1.113 \times 10^{-21}$ | - | . $7958 \times 10^{10}$ | Farad/m. |
    | 26. Inductance | Stathenry | $8.988 \times 10^{20}$ | Abhenry (Centimeter) | $10^{-9}$ | Henry |
    | 27. Permeability | - | $8.988 \times 10^{20}$ | Gauss/0ersted | $1.257 \times 10^{-6}$ | Henry/m. |
    | 28. Reluctivity | - | $1.113 \times 10^{-21}$ | Oersted/Gauss | $10^{7}$ | - |
    | 29. Magnetic Charge | - | $2.998 \times 10^{10}$ | Unit Pole | $1.257 \times 10^{-7}$ | Weber |
    | 30. Magnetic Flux | - | $2.998 \times 10^{10}$ | Maxwell (Line) | $10^{-8}$ | Weber |
    | 31. Magnetic Flux Density, Magnetic Induction | - | $2.998 \times 10^{10}$ | $\begin{gathered} \text { Gauss, }{ }^{2} \\ \text { Lines } / \mathrm{cm}^{2}{ }^{2} \end{gathered}$ | $10^{-4}$ | Weber/m. ${ }^{2}$ |
    | 32. Magnetization | - | $2.998 \times 10^{10}$ | Pole/cm. ${ }^{2}$ | $1.257 \times 10^{-2}$ | Weber/m. ${ }^{2}$ |
    | 33. Magnetic Dipole Moment | - | $2.998 \times 10^{10}$ | Pole-cm, | $1.257 \times 10^{-9}$ | Weber-m, |
    | 34. Magnetic Field Intensity Magnetizing Force | - | $3.335 \times 10^{-11}$ | Oersted (Gilbert/cm.) (Gauss) | $.7958 \times 10^{102}$ | $\begin{gathered} \text { Praoersted } \\ \text { Ampere-turn/m. } \end{gathered}$ |
    | 35. Magnetomotive Force | - | $3.335 \times 10^{-11}$ | Gilbert | $\begin{gathered} .10 \\ .7958 \\ \hline \end{gathered}$ | Pragilbert Ampere-turn |
    | 36. Reluctance | - | $1.113 \times 10^{-21}$ | $\begin{array}{\|c} \hline \begin{array}{c} \text { Gilbert/Maxwell } \\ \text { (Oersted) } \end{array} \\ \hline \end{array}$ | $.7958 \times 10^{10}$ | Pragilbert/Weber Ampere-turn/Weber |
    | 37. Permeance | - | $8.988 \times 10^{20}$ | Maxwell/Gilbert | $1.257 \times 10^{10-1}$ | Weber/Ampere-turn |

    Practical System: Incomplete system similar to MKS, but using centimeters and grams.
    For all Systems: Temperature is in ${ }^{\circ} \mathrm{C}$. Time is in seconds.
    For MKS System: Space Permittivity $8.854 \times 10^{-12} \mathrm{~F} / \mathrm{m}$. Space permeability $1.257 \times 10^{-6} \mathrm{H} / \mathrm{m}$.
    Older or obsolete names are shown in parentheses.
    To convert CGS-ESU to Rationalized MKS, multiply by both factors.

    ## Radio-Phono

    

    ## Television

    
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    ## TORQUE-POWER-SPEED NOMOGRAM

    This nomogram relates power, torque, and speed.
    FOR EXAMPLE: 200 oz-in. at 500 rpm is 0.1 hp , which equals approximately 75 W . The nomogram is based on the formula:

    $$
    \text { Horsepower }=9.92 \times \text { torque } \times \text { speed } \times 10^{-7}
    $$

    where torque is in ounce-inches and speed in revolutions per minute.
    

    | Direct-Current Motors <br> (Amperes at <br> (Aull Load) |  |  |  |
    | :---: | :---: | :---: | :---: |
    | $H P$ | 115 V | 230 V | 550 V |
    | $1 / 2$ | 4.6 | 2.3 |  |
    | $3 / 4$ | 6.6 | 3.3 | 1.4 |
    | 1 | 8.6 | 4.3 | 1.8 |
    |  |  |  |  |
    | $1 \frac{1}{2}$ | 12.6 | 6.3 | 2.6 |
    | 2 | 16.4 | 8.2 | 3.4 |
    | 3 | 24 | 12 | 5.0 |
    |  |  |  |  |
    | 5 | 40 | 20 | 8.3 |
    | $7 \frac{1}{2}$ | 58 | 29 | 12.0 |
    | 10 | 76 | 38 | 16.0 |
    |  |  |  |  |
    | 15 | 112 | 56 | 23.0 |
    | 20 | 148 | 74 | 31 |
    | 25 | 184 | 92 | 38 |
    |  |  |  |  |
    | 30 | 220 | 110 | 46 |
    | 40 | 292 | 146 | 61 |
    | 50 | 360 | 180 | 75 |
    |  |  |  |  |
    | 70 | 430 | 215 | 90 |
    | 75 | 536 | 268 | 111 |
    | 100 |  | 355 | 148 |
    | 125 |  | 443 | 184 |
    | 150 |  | 534 | 220 |
    | 200 |  | 712 | 295 |

    Single-Phase, Alternating-Current Motors ${ }^{\text {b }}$ (Amperes at Full Load)

    | $H P$ | 115 V | 230 V | 440 V |
    | :---: | :---: | :---: | :---: |
    | $1 / 6$ | 3.2 | 1.6 |  |
    | $1 / 4$ | 4.6 | 2.3 |  |
    | $1 / 2$ | 7.4 | 3.7 |  |
    | $3 / 4$ | 10.2 | 5.1 |  |
    | 1 | 13 | 6.5 |  |
    |  |  |  |  |
    | $1 \frac{1}{2}$ | 18.4 | 9.2 |  |
    | 2 | 24 | 12 |  |
    | 3 | 34 | 17 |  |
    |  |  |  |  |
    | 5 | 56 | 28 |  |
    | $7 \frac{1}{2}$ | 80 | 40 | 21 |
    | 10 | 100 | 50 | 26 |

    For fuli-load currents of 208 - and $200-\mathrm{V}$ motors, increase corresponding $230-\mathrm{V}$ motor full-load current by $10 \%$ and $15 \%$, respectively.
    ${ }^{\text {a }}$ These values for full-load current are average for all speeds.
    bThese values of full-load current are for motors running at speeds usual for belted motors and motors with normal torque characteristics. Motors built for especially low speeds or high torques may require more running current, in which case the name plate current rating should be used.

    ## CHARACTERISTICS OF SELECTED MOTOR TYPES

    \begin{tabular}{|c|c|c|c|}
    \hline Motor Type \& Basic Characteristics \& Performance Ranges \& Application Areas <br>
    \hline cawbriomu Penmuiri-hacmer \& a smaple allewnstive to wownd-fale sheel. Pu finte ples movend asastura Lunear lareat-speed rolationships is small enis Lta limited by brostas in high-speos er sewert applications Eadily controlled by lransisters or SCR : \& ```
    Oetpet from IW to a laction of o horsspower
    Time constants to 63 6% \&f m-lowd upedita

