Most - Often - Needed

F. M.

and Television

Servicing Information



Compiled by M. N. BEITMAN

SUPREME PUBLICATIONS

Preface

This manual has a two-fold purpose. First, the material included will aid you in servicing and adjusting popular F.M. and Television receivers. Second, you can employ this material as a study-manual of factory instructions for carrying out tests, adjustments, and repairs of F.M. and Television equipment. The contents will give you the "know-how" to do F.M. and television servicing, and will guide you step-by-step if you are called to repair any of the popular models included.

As always, it is the object of SUPREME PUBLICATIONS to bring to servicemen needed books of practical nature and this volume is a worthy addition. The time spent in the study of this manual will be repaid handsomely when more and more F.M. and television service jobs will be coming your way. You have made a wise move in wanting to keep abreast of developments.

Our sincere thanks is extended to the many manufacturers whose receivers are described and whose cooperation was secured in this undertaking.

M. N. BEITMAN

February, 1948.

Copyright, 1948, by SUPREME PUBLICATIONS. Chicago, Ill.

All rights reserved, including the right to reproduce or quote the contents of this book, or any portion thereof, in any form.

647656

Table of Contents

Preface	2
Table of Contents	3
Admiral Corporation Chassis 9Al, Model 7C73 5-	12
Bendix Aviation Corp. Model 847-B 13-	17
Crosley Corporation Models 88TA, 88TC 18- 87CQ, & Revised 86CR, 86CS 21- Models 146CS, 146CS(V) 29-	28
Du Mont Laboratories, Allen B. Model RA-101	46
Emerson Radio & Phonograph Corp Model 528, Chassis 120038 47-3 Model 537, Chassis 120043 51-3	5Ò
Espey Manufacturing Co. Model 7-B	54
Farnsworth Television & Radio Series GK-140 to GK-144 55-5 Models GV-220,-240,-260 59-6 General Electric Co. Model 417A	52
Model 801 69-8 Howard Radio Company	
Model 474 89-8 Models 472AC, -AF, -C, -F 91-8	
Majestic Radio & Television Corp Model 8FM776, Chas. 8B07D 93-9 Models 12FM475, -778, -779, Chassis 41201, 12B26E 97-10	96
Meissner Manufacturing Co. Models 9-1091A, 9-1091B 10	
Midwest Radio Corp. Models R-12, RT-12, RGT-12, Chassis RGT-12 102-10)4
Montgomery Ward Co. Model 74BR-1812A 105-10	8

Mo	to	ro	1a	.,	I:	nc										
	Mo	de	19	1	95	F3	1	,	9	5 F :	33	, -	Β,	-M,		
	· (Ch	as	S	is	H	S	-3	8	, 1	HS	-3	9	109	-1	13
	Mod	de	ls	1 "	77	FM	[2]	1,	-2	22,	,	23,	,			
														114	1-1	20
	Mod	de	ls		77:	XM	12	1,	-2	22,	-	22	Β,			
	(Ch	as	S	is	H	S	-1	.02	S				121	1	24
	Mod	de)	ls	1	VT	-7	1,	, V	K.	-1(21	u	9 1 1	ng		
	(Ch	83	S	is	Т	S	-3)	٠	•	•	٠	125	5-1	34
01	ymj	pi	С	Ra	ad	io	8	ŝc	Te	e le	эv	is	io	n		
	Mod	le	ls	1	7-	92	5	,	7.	-9:	34	,				
		7-9	93	6	,	an	d	7	-9	939	Э		•	135	5-1	36
Pa	ck	are	a _	Re	-1	٦	C	0								
	Mod					-	0	••						137		z 0
	moc	10.	-	01	2		ľ	*	•		0	•	٠	101	÷Τ.	00
Pf	101	H 1	Ro	đf	10	C	01	nn								
	Mod							гp	•					139	1	10
								•	•	ę.	•	٠		100	- T	±0
к.	C.1	7 .	V .	10	3 C (or	-		~ -	0	10			7 4 9		
	MOC	10	13	t	510		Ţ.	,	6.	LO	12		•	141	-1	44
	Mod	10.	TS.	0	213	20	T	,	6.	121	13	٠	•	145) -	52
									٠					153	>=1	62
Sp	arl	٢S	-W	11	ch:	in	g	to	n	Co	om	par	ny			
]	Mod	le:	1	10)-'	76	-	PA		٠	٠	٠	٠	163	-10	68
St:	ron	nbe	э r	g-	-Ca	ar	1:	30	n	Te	1	. 1	Mf	g. C	0.	
1	Mod	le	1	ĭ	210	э.	-	Se	ri	les	3	10	-1	169	-1	70
	ewe														-	
~ ~	472	ν T T T	1	-2	<u>, , ,</u>	-3	•	_4	C	202	26.			171	- 7 '	71
Î	A72 Mod	ie.	1	Ψ.	7	וו	7	1	nt,	.9	.0.			175		
													•		- T	10
We	STE	r	<u>.</u>	AU	100	2	Sı	qد	۲d	-У	C	omp	bar			
1	Mod	10.	L .	נמ		22	9	T	rι	101	501	ne		177		
														181	-18	32
We																
F	I-1	.13	5,	-1	.14	1 ,	-]	11	6	to]	119)	183	-18	36
F	I-1	.6]	L,	H	[-]	16	8,	,	-A	L				187	-18	38
Zei	nit	h	R	ad	110		Cr	ייוכ	n.							
	Mod										09	94				
-		he												189	-19	91
Ind													•			

2,00



Servicing Notes on 1947-1948 F. M. and Television Receivers Admiral CHASSIS 9A1 MODEL 7C73

FM ALIGNMENT

The model 9A1 chassis should be aligned only with an AM signal generator and a vacuum tube voltmeter. Any standard brand vacuum tube voltmeter with a DC scale of not over 5 volts is suitable. A 3-volt zero center scale is desirable. A signal generator with a frequency range up to 110 MC. is desirable. It is possible however, to align the receiver with a signal generator going to 20 or 30 megacycles, by using the harmonics of these lower frequencies. To do this merely set the signal generator dial as follows and align exactly as explained in the alignment instructions.

Where alignment chart specifies 108.5 MC., set signal generator to highest available frequency of the following:

108.5	MC	27.13	MC
54.25	MC	21.7	MC
36.17	MC	18.08	MC

Where alignment chart specifies 102 MC., set signal generator to highest available frequency of the following:

102.	MC	25.5	MC
51.0	MC	20.4	MC
34.0	MC	17.0	MC

Signal generators which do not tune to 110 MC or whose harmonics are not strong enough, cannot be used for FM alignment.

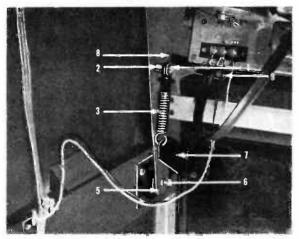


Fig. 5. Receiver Tilt-Out Mounting

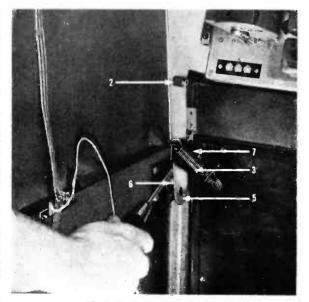


Fig. 6. Receiver Tilt-Out Mounting

POINTER SETTING

With the gang closed, the lower edge of the pointer should be set at the upper tip of the pear-shaped opening (in the dial scale) on the A.M. range (see "Stringing Diagram" Fig. 1).

TRI	MMER IDE	NTIFICATION CHART
TRIMMER	SYMBOL	FUNCTION
A,F		Ratio Detector
		2nd I.F. Transformer (FM)
		1st I.F. Transformer (FM)
		. FM Oscillator Trimmer
		FM Converter Trimmer (RF)
		FM-RF Trimmer
		FM Oscillator Coil
		FM Converter Coil (RF)
		FM-RF Coil
		2nd I.F. Transformer (AM)
0.P		1st I.F. Transformer (AM)
0	C21	. AM Oscillator Trimmer
Ř		. AM Converter Trimmer (RF)
S		.AM Antenna Trimmer
		AM Oscillator Coil
U	L6	AM Converter Coil (RF)
V	L3	AM Antenna Coil

REPLACING TUNING SLUG

If it becomes necessary to change a tuning slug proceed in the following manner: Set the gang to its wide open position, unsolder and remove the old slug. Set the slug adjusting screw about half way down. Place the new slug in such a position that $1\frac{1}{4}$ inches of its length is above the coil form (or 1'' above the chassis top). Solder it in this position making sure that it does not slip during the operation and that the slug wire is straight. Realign as directed.

CHASSIS REMOVAL (For Servicing)

Due to the type of chassis mounting used, removal of the entire tilt-out door assembly (with receiver chassis attached) simplifies removal of the receiver chassis. The receiver chassis can then be easily removed from its shock mountings. Removal is a little "tricky" but can be done most readily as described below:

Disconnect all cabinet wiring and cables from the chassis. Difficulty may be experienced in removing the phono pickup plug due to the tight fit in the socket shield. This plug can best be removed with long-nose pliers.

Remove the screw and washer (#1 in figure 5) from both tilt-out spring studs (2), one on each side of the tilt-out assembly. Slip the tilt-out springs (3) off their respective studs. Unscrew the ends of the tie-bar (4). The tie-bar then hangs free on the copper braid used to bond it to the classis.

Stand at the end of the cabinet (next to the radio compartment) and hold the tilt-out door open slightly with the left hand. Use a screwdriver to pry both tilt-out arms (#5 in figure 6) off their studs (#6). Then push the tilt-out arms toward the front of the cabinet (against bracket #7). The tilt-out assembly can now be removed from the front of the cabinet by tipping it forward and then pulling it straight out.

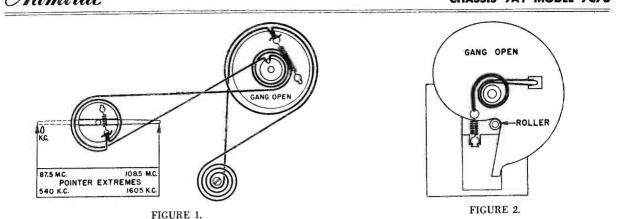
CHASSIS REPLACEMENT

Make sure the rubber numpers (#9, Fig. 5) and rubber strips (#8) are in place.

To replace the radio tilt-out door assembly in the cabinet, set the assembly in so that the tilt-out arms (#5) are in back of the studs (#6) they normally hinge on. Use your left hand to hold the assembly in the proper position in the same manner as was done in removing the tilt-out assembly. Use a screwdriver (in your right hand) to spring the tilt-out arm clear of its stud (#6). **Push it forward as far as possible (as shown in figure 6**). When both tilt-out arms are in this position, the assembly can be lifted up and the tilt-out arms slipped into place on their respective studs. The tilt-out assembly will now support itself (in the open position).

Replace the tie-bar (#4). Replace the tilt-out springs (#3. See figure 5). Reconnect the cabinet wiring and cables to the receiver chassis. Check to see that the rubber bumper (#9) and rubber strips (#8) are in place. The assembly should now appear as shown in figure 5.

Servicing Notes on 1947-1948 F. M. and Television Receivers Adminal. CHASSIS 9A1 MODEL 7C73



ADMIRAL FREQUENCY MODULATION CIRCUIT

An amplitude modulated (AM) signal varies in amplitude in accordance with the sound being transmitted. If the frequency of the sound increases, the amplitude variations in the transmitted carrier occur at a faster rate (at the new audio rate). If the volume of the sound increases, a greater amplitude variation takes place in the transmitted carrier.

In the case of frequency modulation (FM), the transmitted signal varies in frequency in accordance with the sound being transmitted. If the frequency of the sound increases, the variations in transmitter carrier trequency occur at a faster rate. If the volume of the sound increases, a wider frequency variation takes place in the transmitted carrier.

Due to the higher operating frequencies used for frequency modulation transmission, a higher intermediate frequency is also used in F.M. receivers. An IF of 10.7 Mc. is most frequently used. The converter in the receiver changes the original signal to this new frequency without changing the modulation characteristic.

The audio modulation is obtained from the carrier in an amplitude modulation receiver by the second detector. This function must be performed by a different type of circuit in a frequency modulation receiver since the type of modulation is different. This can be done by either a discriminator or a ratio detector.

Conventional Discriminator

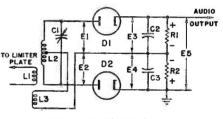
An elementary discriminator circuit is shown in figure 3. L1, L2 and L3 are all part of the discriminator transformer. L1 is the primary and signal input for the circuit. The voltages induced in L2 and L3 add vectorially and are applied to the plates of the two diodes, D1 and D2. When the LF. signal is exactly 10.7 Mc., E1 and E2 are equal. The diodes then pass equal currents through R1 and R2. Since R1 and R2 have the same resistance, equal voltages E3 and E4 will appear across them. Due to the polarity of E3 and E4 (as indicated in figure 3), output voltage E5 will be equal to their difference. When the LF, signal is exactly 10.7 Mc., E3 and E4 are equal and E5 is zero.

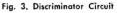
If the I.F. signal is below 10.7 Mc., E1 will be greater than E2, thus D1 will pass more current than D2. E3 will then be greater than E4. Since E5 is the difference between E3 and E4, E5 will be positive. If the I.F. signal is above 10.7 Mc., conditions will be reversed and E4 will be greater than E3. E5 will now be negative.

Since the I.F. signal varies above and below 10.7 Mc. at the audio modulation rate (it carries the same modulation as the original transmitter signal), the positive and negative output voltages from the discriminator will conform to the audio modulation wave form. E5 is then amplified and reproduced as sound.

Assuming the I.F. signal is below 10.7 Mc., E5 will be a positive voltage equal to the difference between E3 and E4. If the signal amplitude were to increase at this time (as it might due to a noise

pulse), E3 and E4 would increase in proportion. Since E5 is the difference between E3 and E4, it must also increase. An increase in signal amplitude causes an increase in output voltage under these conditions. This illustrates the fact that the discriminator is sensitive to amplitude variations as well as frequency deviation. Since noise is essentially an amplitude variation, all amplitude variations must be removed from the signal before it is fed to the discriminator. This is the function of the one or more limiter stages normally employed ahead of the discriminator circuit in an F.M. receiver.





Due to the function of a limiter (which is essentially a class "C" R.F. amplifier), a large input signal is required before it will remove amplitude variations from the F.M. signal. This requires the use of a high gain R.F. and l.F. amplifier system in an F.M. receiver using a discriminator type second detector. This type of circuit does not provide noise rejection on weak signals since the limiter must have a certain minimum signal in order to operate. The result is an expensive receiver that is noisy on weak signals.

The Ratio Detector

The ratio detector was developed to overcome the afore-mentioned limitations of the discriminator-limiter type F.M. second detector circuit. An elementary ratio detector circuit is shown in figure 4. Although a similar discriminator type transformer is used in the ratio detector, note that the connections of one diode are reversed as compared to the discriminator circuit in figure 3. As before, El and E2 are equal when the I.F. signal is 10.7 Mc. El will be greater than E2 when the I.F. signal is below 10.7 Mc. and E2 will be greater than E1 when the I.F. signal is higher than 10.7 Mc.

If the total signal voltage across L2 and C1 be considered, diodes D1 and D2 are connected in a series rectifier circuit. The load for this circuit consists of R1 and R2 in series. Load voltage E6 is developed across these two resistors and filtered by C4. Since C4 has a capacity of 4 or 5 Mfd., E6 is essentially a D.C. voltage. Since variations in amplitude are filtered out by C4, E6 is proportional to the average I.F. signal strength. Point "Y" is the electrical mid-point of this circuit and is grounded.

So far, the circuit from the center tap of L2, through L3 and to point "X", has been disregarded. This is permissible when considering a 10.7 Mc. input signal since the signal voltages E1 and E2 are equal only for this condition. The diodes then pass equal currents and current can flow from the bottom side of L2, through D2, through R2 and R1, through D1 and back through L2. No current flow will take place between center tap of L2 and point "X". C2 and C3 having equal capacity are connected in series across the load resistors R1 and K2. They will charge up to equal voltages, E3 and E4 respectively. The electrical mid-point of this capacitive circuit, point "X", will be at ground potential. (Resistive center tap "Y" is grounded. Therefore, capacitive center tap "X" must be at ground potential). Output voltage E5 is zero.

When the I.F. signal is below 10.7 Mc., El will be greater than E2. C2 will then charge through D1 to a higher voltage (this center connection now plays a vital part in the operation of the circuit). Since E2 is a smaller voltage, C3 will charge through D2 and assume a charge that is less than that of C2. Therefore, E3 and E4 are proportional to voltages E1 and E2, respectively. Although E3 is greater than E4, their sum is still equal to E6 (due to the parallel circuit arrangement), point "X" is negative with respect to point "Y" and ground. Output voltage E5 is negative. When the I.F. signal is above 10.7 Mc., E2 is greater than E1, E4 is greater than E3, and E5 is positive. E5 varies positive and negative in accordance with the I.F. signal modulation wave form.

Due to the unusual nature of some portions of the circuit, and the fact that their function may not be too apparent, examination of the circuit prior to servicing will simplify the task of locating trouble. This is the purpose of the following information on the function of various portions of the circuit.

Grounded-Grid R.F. Amplifier

The input signal is introduced between grid and cathode in any amplifier circuit. It is conventional to apply the signal between grid and ground. The cathode is then grounded at signal frequencies. If the grid is grounded, the signal can just as well be applied between cathode and ground. This is the circuit arrangement of a grounded-grid RF amplifier.

Since the cathode circuit of a vacuum tube has a low characteristic impedance, the grounded-grid amplifier has a low input impedance and provides a satisfactory match for a folded dipole antenna. This eliminates complicated antenna coupling devices.

Due to the low impedance and inverted nature of the input circuit of the grounded-grid amplifier, feedback which might result in oscillation, is unlikely. This permits the use of a triode tube. The use of a triode tube greatly reduces circuit noise in comparison to that present in a pentode amplifier stage. A triode RF amplifier circuit provides excellent circuit stability without the use of tricky circuits or adjustments.

Band-Switching

There is little that is unusual about the operation of the band switch in the FM position. Due to the fact that some of the FM components are not removed from the circuit in the AM setting of the switch, it is rather difficult to trace the operation of the circuit. For AM operation, C7 is still in the circuit. Due to a relatively low capacity, it does not bypass the signal around the RF amplifier grid (but acts as a small portion of the tuned circuit capacity). L4 is also left in the circuit and is in series with the feed to the RF grid. It, like C7, has no appreciable effect due to its low electrical value. A shunt feed system is used on the RF amplifier grid, R3 being the grid return resistor.

Cl3 and L5 remain in series across the signal grid of the converter stage for AM operation. They have no appreciable effect on the circuit since Cl3 has a very low capacity. Cl4 is also across this grid circuit but it is also a very small capacity. The effect of these circuit components is merely that of added capacity.

The band switch shorts the primary of the first IF transformer that is not in use (the FM first IF transformer primary is shorted out for AM operation). This prevents the production of undesired frequencies in the plate circuit of the converter. The unused IF transformer windings which remain in the circuit have The voltage at point "X" is determined by the ratio between E3 and E4. The ratio between E3 and E4 is determined by the frequency deviation of the I.F. signal input. The sum of E3 and E4 must be equal to E6 (series voltages E3 and E4 are paralleled ucross E6). Since E6 is proportional to average signal strength.

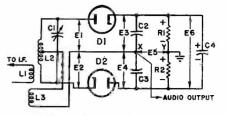


Fig. 4. Ratio Detector Circuit

amplitude variations being filtered out by C4, E3 and E4 will be unaffected by amplitude variations (such as might be caused by noise signals). Therefore, output voltages E5 is purely a function of input signal frequency. The ratio detector is, therefore, inherently insensitive to amplitude modulated noise signals and provides noise rejection without the use of a limiter.

Since noise rejection does not depend on limiter action, a ratio detector provides noise free reception of weak signals. For this same reason, the receiver is relatively quiet when tuning from one station to another. Due to the fact that a limiter is not used with a ratio detector, elaborate and expensive R.F. and I.F. amplifiers are unnecessary.

ADMIRAL 9A1 RECEIVER CIRCUIT

a very low impedance at the operating frequency since this frequency is far removed from the resonant frequency of the unused windings. Therefore, they have little effect on the operation of the circuit.

Although it does not cause difficulty in tracing the operation of the circuit, it is important to note that CH4 and Cl0 form a series resonant circuit at 10.7 Mc. Since this series resonant circuit is effectively connected from plate to ground on the RF amplifier, it acts as an IF wave trap for FM operation. This provides excellent rejection of any strong 10.7 Mc. signals which might be present in the input circuit of the receiver. (It is desirable to detune this trap for FM-IF alignment.)

FM Second IF Amplifier, AM Second Detector

A 6BA6 tube is used as a second IF amplifier for FM operation. Self-bias is developed in the grid resistor (R15 and R16 in series) of this stage. Since this DC bias voltage is dependent on signal strength, it is used for AVC purposes.

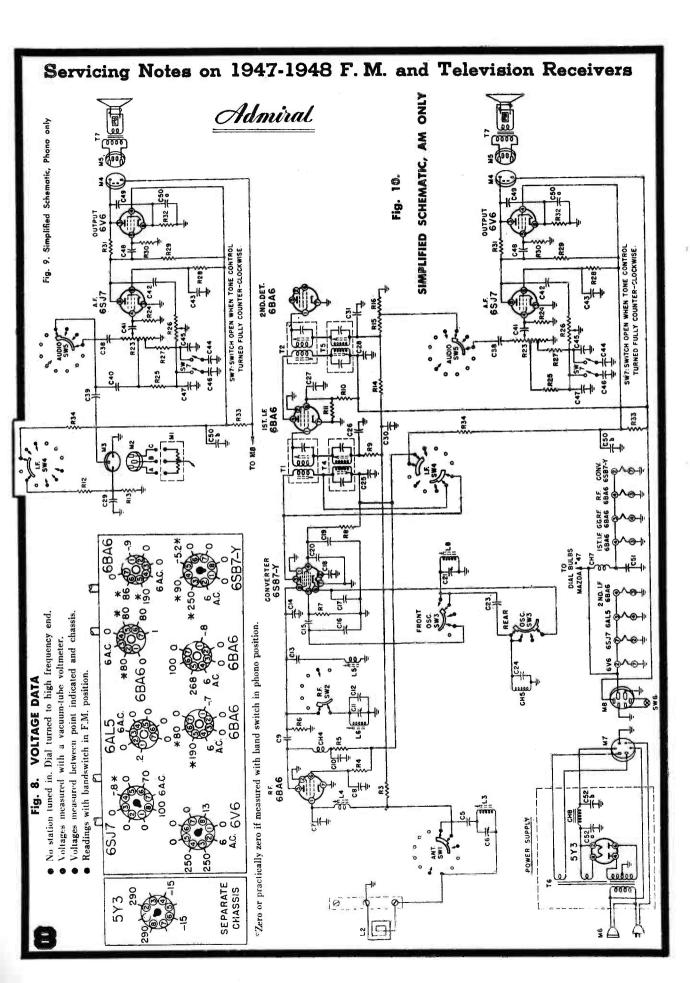
In the AM setting of the band switch, plate and screen voltages are removed from this tube. The grid and cathode of this tube then function as an AM second detector (diode) and AVC tube in a conventional manner.

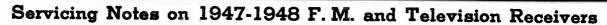
Ratio Detector

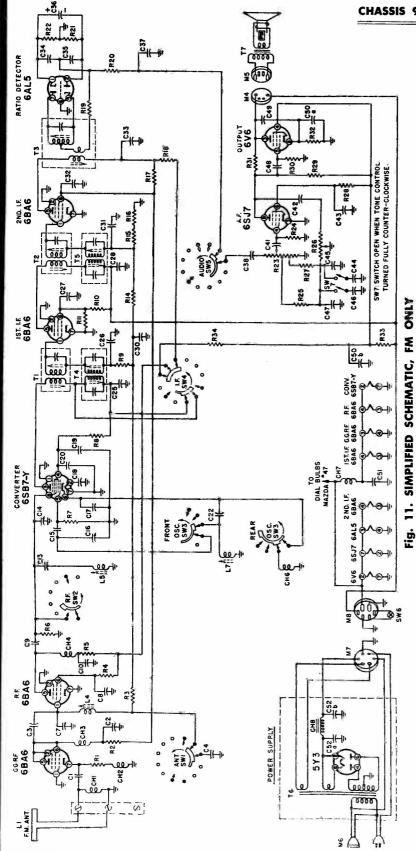
In AM reception, the transmitter signal varies in amplitude in accordance with the sound being transmitted. The second detector of the receiver converts these amplitude variations into an audio signal that is a duplicate of that used to modulate the transmitter. In the case of FM, the transmitter frequency is made to vary in accordance with the sound to be transmitted. These frequency variations are again converted into an audio signal by the discriminator or ratio detector in an FM receiver.

The conventional discriminator has the disadvantage of being sensitive to amplitude variations as well as to variations in frequency. Amplitude variations, such as might be introduced by noise signals, can be removed by the use of a limiter circuit ahead of the discriminator. However, the input signal to the limiter must exceed a certain minimum amplitude before limiter action takes place. Therefore, the limiter-discriminator type circuit does not provide noise rejection on weak signals.

Since the ratio detector is relatively insensitive to amplitude variations, it can be used without a limiter stage. It provides noise rejection on weak as well as strong signals. This is the reason for the use of the ratio detector in preference to the limiter-discriminator type circuit.







CHASSIS 9A1 MODEL 7C73

COILS, TRANSFORMERS, ETC.

	э, с	
CH1 Choke, F.M. Antenna	AR	103.33
CH2 Choke, Grounded Grid Cathod		103 35
		100 0.0
CH3 Choke, Grounded Grid Plate	. AB	103-35
CH4 Choke, R.F. Plate	.AB	103-36
CH5 Choke, A.M. Oscillator Cathod	e.AB	103-1
CH6 Choke, F.M. Oscilator Cathode	. AB	103-34
CH4. Choke, Crounded Grid Plate CH4. Choke, R.F. Plate CH5 Choke, A.M. Oscillator Cathoda CH6 Choke, F.M. Oscillator Cathoda CH7. Choke, R.F. FilomentCons of approximately 8 turns ⇒20 solid hookup wire woo around condenser C51	ists	
of approximately 8 turns	of	
=20 solid hookup wire wo	und	
around condenser C51		
CH8 Choke, Filter	744	•
CH8 Choke, Filter	AB	120
L2 Antenna, A.M. (13')	0.04	10 1
LZ Antenna, A.M. (13')		
L3 Coil, A.M. Antenna (less slug).	AL	105-2
L4 Coil, F.MR.F. (less slug)		122
L5 Coil, F.M. Canverter (less slug) L5 Coil, A.M. Converter (less slug) L6 Coil, A.M. Converter (less slug)	. 🗛 .	122
L6 Coil, A.M. Converter (less slug).AB	100-1
L8 Coil, A.M. Oscillator (less stua)	. AC	101-2
When Ordering Slugs Sperify Color Cor	-	
When Ordering Slugs Specify Color Coc Slug, Iron Core (F.MOsc., Conv.,	.e	
& P F	718	1.19
Shug Iron Core (A M. Ore Come)	718	1.20
& R.F. Slug, Iron Core (A.MOsc., Conv.) Slug, Iron Core (A.MAntenna)	710	1-20
Slug, Iron Core (A.MAntenna)	. /18	1-21
SW1 Switch, Antenna (Second from		
front). SW2 Switch, R.F. (Fourth from front)	.76C	11-3
SW2 Switch, R.F. (Fourth from front)	.76C	11-5
SW3 Switch, Oscillator (Third from		
SW3 Switch, Oscillator (Third from front)	.76C	11-4
SW4 Switch, I.F. (Farthest from front	1)76C	
	.,	., .
COILS, TRANS.,ETC.,	Cont	t.
Symbol Description	Part	
SW5 Switch, Audio (Closest to front)	ran	NQ.
JWJ., JWITCH, AUGIO (LIOSEST TO TRONT)	710	
Barrid Control Ch. fr. A. 11	.76C	11-2
SW5 Switch, Audio (Closest to front) Band-Switch Shaft Assembly.	.76C	11-2
Band-Switch Shaft Assembly Set Screw, #6-32 x ¼	.76C .76C .1A 5	11-2 11-1 -54
Band-Switch Shaft Assembly Set Screw, #6-32 x ¼ Spacers for Shaft Assembly	.76C .76C .1A 5 .29A	11-2 11-1 -54 4-4
Band-Switch Shaft Assembly. Set Screw, ±6-32 x ¼. Spacers for Shaft Assembly SW6, Switch (On-off)	.76C .76C .1A 5 .29A rt of I	11-2 11-1 -54 4-4 R23
Band-Switch Shaft Assembly. Set Srew, #6-32 x ¼. Spacers for Shaft Assembly SW6, Switch (On-off)	.76C .76C .1A 5 .29A rt of I rt of I	11-2 11-1 -54 4-4 R23 R26
Band-Switch Shaft Assembly. Set Screw, #6-32 x ½. Succers for Shaft Assembly SW6. Switch (On-off)Pa SW7. Switch (On-off)Pa 11. Transformer, 1st 1.F. (F.M.).	.76C .76C .1A 5 .29A rt of I rt of I .728	11-2 11-1 -54 4-4 R23 R26 24
Band-Switch Shaft Assembly. Set Screw, #6-32 x ½. Spacers for Shaft Assembly SW6, Switch (On-off)	.76C .76C .1A 5 .29A rt of 1 rt of 1 .728 .728	11-2 11-1 -54 4-4 R23 R26 24 26
Band-Switch Shaft Assembly. Set Screw, #6-32 x ¼. Spacers for Shaft Assembly SW6, Switch (On-off)	.76C .76C .1A 5 .29A rt of I rt of I .728 .728	11-2 11-1 -54 4-4 R23 R26 24 26 27
Band-Switch Shaft Assembly. Set Strew, #6-32 x ½. Succers for Shaft Assembly SW6. Switch (On-off)	.76C .76C .1A 5 .29A rt of I rt of I .728 .728 .728 .728	11-2 11-1 -54 4-4 R23 R26 24 26 27 25
Band-Switch Shaft Assembly. Set Screw, #6-32 x ¼. Spacers for Shaft Assembly SW6, Switch (On-off)	.76C .76C .1A 5 .29A rt of I rt of I .728 .728 .728 .728 .728 .728	11-2 11-1 -54 4.4 R23 R26 24 26 27 25 25
Band-Switch Shaft Assembly. Set Screw, #6-32 x ½. Switch (On-off)	.76C .76C .1A 5 .29A rt of 1 rt of 1 .728 .728 .728 .728 .728 .728 .728 .728	11-2 11-1 -54 4-4 R23 R26 24 26 27 25 25 1-22
Band-Switch Shaft Assembly. Set Strew, #6-32 x ¼. Spacers for Shaft Assembly Switch (On-off)	.76C .76C .1A 5 .29A rt of I rt of I .728 .728 .728 .728 .728 .728 .728 .728	11-2 11-1 -54 4.4 R23 R26 24 26 27 25 25 1-22 2 20
Band-Switch Shaft Assembly. Set Screw, #6-32 x ¼. Succers for Shaft Assembly SW6, Switch (On-off)	.76C .76C .1A 5 .29A rt of I rt of I .728 .728 .728 .728 .728 .728 .728 .728	11-2 11-1 -54 4.4 23 24 26 27 25 25 25 1-22 2 2 2 2 2 2 2 2
Band-Switch Shoft Assembly. Set Strew, ic-32 x Va. Spacers for Shaft Assembly Switch (On-off)	.76C .76C .1A 5 .29A rt of I .728 .728 .728 .728 .728 .728 .728 .728	11-2 11-1 -54 4.4 823 826 24 26 27 25 25 1-22 2 22 22
Band-Switch Shoft Assembly Set Strew, #6-32 x ¼ Spacers for Shaft Assembly SW6, Switch (On-off)	.76C .76C .1A 5 .29A rt of I rt of I .728 .728 .728 .728 .728 .728 .728 .728	11-2 11-1 -54 4.4 R23 R26 27 25 25 1-22 2 2 22 22 21
Band-Switch Shoft Assembly. Set Strew, #6-32 x ¼. Spacers for Shaft Assembly SW6, Switch (On-off)	.76C .76C .1A 5 .29A rt of I rt of I r728 .728 .728 .728 .728 .728 .728 .728	11-2 11-1 -54 4-4 823 826 24 26 27 25 25 25 1-22 2 2 22 21
TUNER PARTS		
TUNER PARTS	Part	No.
TUNER PARTS	Part	No.
TUNER PARTS Description Tuning Shaft	Part .28A	No. 17
TUNER PARTS Description Tuning Shaft. Slug Travel Bracket, Bushing and Roller Assy. (front).	Part 28A A139	No. 17 6
TUNER PARTS Description Tuning Shaft. Slug Travel Bracket, Bushing and Roller Assy. (front).	Part 28A A139	No. 17 6
TUNER PARTS Description Tuning Shaft. Slug Travel Bracket, Bushing and Roller Assy. (front).	Part 28A A139	No. 17 6
TUNER PARTS Description Tuning Shaft. Slug Travel Bracket, Bushing and Roller Assy. (front).	Part 28A A139	No. 17 6
TUNER PARTS Description Tuning Shaft. Slug Travel Bracket, Bushing and Roller Assy. (front).	Part 28A A139	No. 17 6
TUNER PARTS Description Tuning Shaft Slug Travel Bracket, Bushing and Roller Assv. (front). Slug Travel Bracket, Bushing and Roller Assy. (rear). Brass Guide Rod (Tuner). Speed Nut (for Guide Rod). Com and Hub for Tuner (front). Com gain with for Sumer (seen).	Part 28A A139 28A 28A 2A 1 A140	No. 17 6 8 7-2 0-1-59 0 7
TUNER PARTS Description Tuning Shaft Slug Travel Bracket, Bushing and Roller Assv. (front). Slug Travel Bracket, Bushing and Roller Assy. (rear). Brass Guide Rod (Tuner). Speed Nut (for Guide Rod). Com and Hub for Tuner (front). Com gain with for Sumer (seen).	Part 28A A139 28A 28A 2A 1 A140	No. 17 6 8 7-2 0-1-59 0 7
TUNER PARTS Description Tuning Shaft Slug Travel Bracket, Bushing and Roller Assv. (front). Slug Travel Bracket, Bushing and Roller Assy. (rear). Brass Guide Rod (Tuner). Speed Nut (for Guide Rod). Com and Hub for Tuner (front). Com gain with for Sumer (seen).	Part 28A A139 28A 28A 2A 1 A140	No. 17 6 8 7-2 0-1-59 0 7
TUNER PARTS Description Tuning Shaft Slug Travel Bracket, Bushing and Roller Assv. (front). Slug Travel Bracket, Bushing and Roller Assy. (rear). Brass Guide Rod (Tuner). Speed Nut (for Guide Rod). Com and Hub for Tuner (front). Com gain with for Sumer (seen).	Part 28A A139 28A 28A 2A 1 A140	No. 17 6 8 7-2 0-1-59 0 7
TUNER PARTS Description Tuning Shaft Slug Trevel Bracket, Bushing and Roller Assv. (front). Slug Trevel Bracket, Bushing and Roller Assy. (recr). Brass Guide Rod (Tuner). Speed Nut (for Guide Rod). Cam and Hub for Tuner (front). Spring, Bearing Takeup. Cable, Drive (for Cam and Hub). Spring, Gold (for Cam and Hub).	Part 28A A139 28A 2A 1 A140 A146 19A 95A 19B	No. 17 6 8 7-2 0-1-59 0 7 16 15-1 1-14
TUNER PARTS Description Tuning Shaft Slug Travel Bracket, Bushing and Roller Assv. (front) Slug Travel Bracket, Bushing and Roller Assy. (rear) Brass Guide Rod (Tuner) Speed Nut (for Guide Rod) Cam and Hub for Tuner (front) Spring, Bearing Takeup. Cable, Drive (for Cam and Hub) Spring, Bearing Takeup. Cable, Drive (for Cam and Hub) Breact (for Cam and Hub) Beveite Plate for slog mounting	Part 28A A139 28A 2A 1 A140 A146 19A 95A 198	No. 17 6 8 7-2 0-1-59 0 7 16 15-1 1-14
TUNER PARTS Description Tuning Shaft Slug Travel Bracket, Bushing and Roller Assv. (front) Slug Travel Bracket, Bushing and Roller Assy. (rear) Brass Guide Rod (Tuner) Speed Nut (for Guide Rod) Cam and Hub for Tuner (front) Spring, Bearing Takeup. Cable, Drive (for Cam and Hub) Spring, Bearing Takeup. Cable, Drive (for Cam and Hub) Breact (for Cam and Hub) Beveite Plate for slog mounting	Part 28A A139 28A 2A 1 A140 A146 19A 95A 198	No. 17 6 8 7-2 0-1-59 0 7 16 15-1 1-14
TUNER PARTS Description Tuning Shaft Slug Travel Bracket, Bushing and Roller Assv. (front) Slug Travel Bracket, Bushing and Roller Assy. (rear) Brass Guide Rod (Tuner) Speed Nut (for Guide Rod) Cam and Hub for Tuner (front) Spring, Bearing Takeup. Cable, Drive (for Cam and Hub) Spring, Bearing Takeup. Cable, Drive (for Cam and Hub) Breact (for Cam and Hub) Beveite Plate for slog mounting	Part 28A A139 28A 2A 1 A140 A146 19A 95A 198	No. 17 6 8 7-2 0-1-59 0 7 16 15-1 1-14
TUNER PARTS Description Tuning Shaft Slug Travel Bracket, Bushing and Roller Assv. (front) Slug Travel Bracket, Bushing and Roller Assy. (rear) Brass Guide Rod (Tuner) Speed Nut (for Guide Rod) Cam and Hub for Tuner (front) Spring, Bearing Takeup. Cable, Drive (for Cam and Hub) Spring, Bearing Takeup. Cable, Drive (for Cam and Hub) Breact (for Cam and Hub) Beveite Plate for slog mounting	Part 28A A139 28A 2A 1 A140 A146 19A 95A 198	No. 17 6 8 7-2 0-1-59 0 7 16 15-1 1-14
TUNER PARTS Description Tuning Shaft Slug Trevel Bracket, Bushing and Roller Assv. (front). Slug Trevel Bracket, Bushing and Roller Assy. (recr). Brass Guide Rod (Tuner). Speed Nut (for Guide Rod). Cam and Hub for Tuner (front). Spring, Bearing Takeup. Cable, Drive (for Cam and Hub). Spring, Gold (for Cam and Hub).	Part 28A A139 28A 2A 1 A140 A146 19A 95A 198	No. 17 6 8 7-2 0-1-59 0 7 16 15-1 1-14

Drum and Hub on Tuner Shaft (includes 1" drum and 311" drum). . A1401

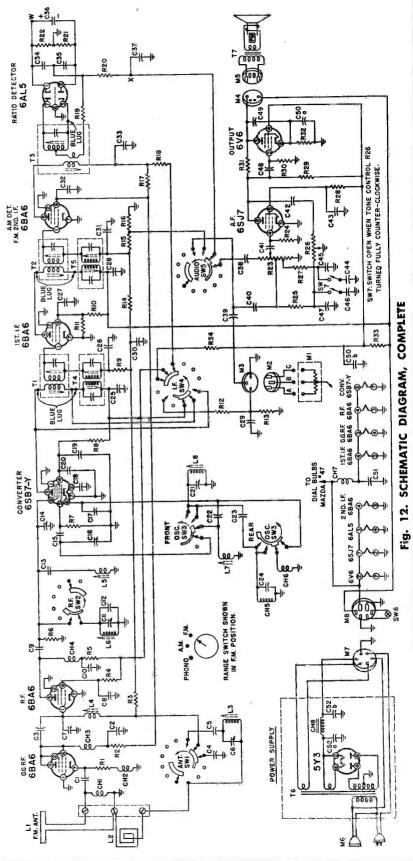
DIAL PARTS

28A 19	
.41388	
50A 1-	3
198 1-	š -
.41404	-
15A 17	6
	-
A1405	
81A 1-	8
82A 3-	õ.
A1477	
23E 20	
23C 25	į
	28A 19 A1388 50A 1- 19B 1- A1404 A1405 81A 1- 82A 3- A1477 23E 20 23C 25

C52a... 30 mfd., 350 Volts } C52b... 30 mfd., 350 Volts } Electrolytic.67C 6-22

	RESISTORS
Symbol	Description Part No.
R1 R2	100 Ohms, 1/2 Watt
R3	470,000 Ohms, 1/2 Watt 608 B-474
R4 R5	39,000 Ohms, 1 Watt
R6 R7 R8	33,000 Ohms, 1/2 Watt
R8	18,000 Ohms, 2 Wait
R9	120,000 Ohms, 1/2 Watt
R10 R11	18,000 Ohms, 1 Watt
R12 R13	100,000 Ohms, 1/2 Watt 60B 8-104
R14	470,000 Ohms, 1/2 Watt
R14 R15 R16 R17	82,000 Ohms, 1/2 Watt 60B 8-823 8 200 Ohms 2 Watt
R18	2,200 Ohms, 2 Watt
R19 R20	390 Ohms, ±5%, ½ Watt
R21	6,800 Ohms, ±5%, ½ Watt 608 7-682
R22 R23	6,800 Ohms, ±5%, ½ Watt608 7-662 1 Megohm Volume Control &
	on-off switch SW6. Tapped at
R24	4.7 Megohms, 1/2 Watt
R25 R26	47,000 Ohms, ½ Watt
	& D.P.S.T. switch SW7758 1-14
R27 R28 R29	470.000 Ohms, ½ Watt
R29	100,000 Ohms, 1/2 Watt
R30	2.2 Megohms, 1/2 Watt
R31 R32	390 Ohms, 1 Watt
R33 R34	100 Ohms, 1 Watt
	RESISTORS Description Part No. 100 Ohms, ½ Watt .608 8-101 330 Ohms, ½ Watt .608 8-331 470,000 Ohms, ½ Watt .608 8-431 370,000 Ohms, ½ Watt .608 8-433 470,000 Ohms, ½ Watt .608 8-433 470,000 Ohms, ½ Watt .608 8-473 18,000 Ohms, ½ Watt .608 8-473 18,000 Ohms, ½ Watt .608 8-473 18,000 Ohms, ½ Watt .608 8-473 120,000 Ohms, ½ Watt .608 8-124 18,000 Ohms, ½ Watt .608 8-124 120,000 Ohms, ½ Watt .608 8-124 20,000 Ohms, ½ Watt .608 8-124 20,000 Ohms, ½ Watt .608 8-224 20,000 Ohms, ½ Watt .608 8-224 20,000 Ohms, ±5%, ½ Watt .608 7-682 200 Ohms, ±5%, ½ Watt .608 7-682 2,000 Ohms, ½ Watt .608 8-473 2,000 Ohms, ½ Watt .608 8-474 2,000 Ohms, ½ Watt .608 8-474<
C1	1000 mmfd., Mica
C2 C3	35 mmfd. ±2%; 0 temp.
C4	35 mmfd. ±2%; 0 temp. 65B 6-14 27 mmfd. ±1 mmfd.; 0 temp. 65B 6-17 26 mmfd. ±1 mmfd.; 0 temp. 65B 6-17 500 mmfd. Mica 65B 5-27 3.40 mmfd. Trimmer 66A 12-5 3.12 mmfd. Trimmer 66A 22-1 200 mmfd. Trimmer 56B 5-21 30 mmfd. Trimmer 56A 5-21 31 mmfd. To temp. 56B 5-21
	coeff. ceramic
C5	3-40 mmfd., Trimmer
C7	3-12 mnifd., Trimmer
C8	35 mmfd. ±2%; 0 temp.
	600 0-14
C10	40 mmfd. ±2%; 0 temp. coeff; ceramic
C11	
C12	$25 \text{ mmfd} \pm 1 \text{ mmfd}; 0 \text{ temp}.$
	coeff coromic 65B 6-15
C14 C15	3-12 mmd., mmer
	coeff.; ceromic
C16	coeff; ceramic 658 654 22-1 30 mmfd. Timmer. 658 62-1 200 mmfd. ±3%;00033 658 6-20 .005 mfd. 600 Volts, Paper. 648 1-12 100 mmfd. ±10%;00075 temp. coeff; ceramic. 558 6-19 5000 d coeff; ceramic. 558 6-19
	coeff ; ceramic
C18	100 mmfd, ±10%;00075
	temp. coeff.; ceramic
C20	3-40 mmfd., Ceramic
C22	5000 mmfd., Ceramic
C23	coeff ; ceramic
	temp. coeff.; Ceramic
C24	2000 mmfd., Alica 01 mfd., 400 Volts, Paper
C25 C26 C27 C28	2000 mmfd., Mica
C27	10 mfd., 400 Volts, Paper
C29	2 mfd , 400 Volts, Paper
C31 .	05 mtd., 400 Voits, roper
C32	05 mfd., 200 Volts, Paper
C28 C29 C30 C31 C32 C33 C34	. 100 mmfd. ±10%;00075 temp_coeff : Ceramic
C35	100 mmfd. ±10%;00075
C36	4 - 4 J 150 Volte Floctrolytic 67A 4-7
C37	002 mfd., 600 Valts, Paper 64B 1-14 .005 mfd., 600 Valts, Paper 64B 1-12
C38 C38 C39	1 1002 mfd., 600 Valts, Paper. 648 1-14 002 mfd., 600 Valts, Paper. 648 1-12 1000 mmfd., Mica.
C40 C41	. 500 mmfd., Mica
C42	
C43	05 mfd., 200 Volts, Paper 64B 1-22
C45	01 mfd., 400 Volts, Paper
C46	000 mid., 000 volis, ruper 040 1-12
C47	
C49. C50a	
C50a	. 30 mtd., 330 volts)
C51.	

10



Servicing Notes on 1947-1948 F. M. and Television Receivers Admiral. PRELIMINARY ALIGNMENT STEPS

CHASSIS 9A1 MODEL 7C73

- With the gang closed, the lower edge of the pointer should be at the dotted position shown in Fig. 1. That is, the lower edge of the pointer should be at the upper tip of the AM pearshaped opening in the dial scale. If the pointer is in different position, move it by hand while keeping the gang closed.
- Check the set screws that hold the tuning drum to the shaft to see that they are tight and that the drum has not slipped on
- the shaft. See Fig. 1 for correct drum position.
- In the wide open position, the roller on the slug tuning platform must be as shown in dial stringing diagram, Fig. 2.
- With the gang wide open, all slugs should be 11/4 inches out of their coil forms. If there is any serious deviation or if there has been any tampering, turn the adjusting screws until this distance is corrected.

FM IF AND RATIO DETECTOR ALIGNMENT

- Solder output indicator leads in place and keep them well separated from signal generator leads and chassis wiring. ò
- While peaking IF's, keep reducing signal generator output so VTVM reading is approximately +1.5 volts DC with exception of Step #5.
- FM antenna disconnected during alignment
- Band switch in FM position (red signal at MC on dial)
- Speaker must be connected during alignment

I.F. SLUG INFORMATION

To avoid splitting the slotted head of the powdered iron core tuning slug in the I.F. transformers, use a screw-driver with a blade 1/8" wide for I.F. alignment.

Under normal operating conditions, mis-alignment of slug-tuned circuits with age is slight. Therefore, re-alignment of the I.F. transformers should be accomplished by only a slight adjustment of the slugs. Do not turn a slug in an extreme amount or it will fall into the center of the coil form. Always try to adjust hy first turning slug out. Should an I.F. tuning slug be turned in too far and fall into the center

of the coil form, it will be necessary to remove the other tuning slug on the opposite side of the I.F. can. Then, using a thin rod and screw-driver, "jockey" the dislocated slug until it re-engages the threads in the coil form. Since this is a difficult operation, care should be exercised as outlined above in paragraph and this difficulty will be avoided.

If the iron core slug should become stripped or if the slotted head should become rounded or cracked, it may be removed by removing the opposite slug and forcing the defective slug out with a thin screw-driver.

Steps 1 and 2 may be omitted if set is not badly out of alignment so signal comes through in Step 3 Before proceeding, be sure to follow all steps listed above. under "Important Preliminary Alignment Steps."

	Connect Signal Generator	Generator Frequency	Receiver Dial Setting	Output Indicator and Special Connections	Adjust as Follows (very carefully)
1	Thru .01 cond. to 2nd IF grid (Pin #1 of 6BA6 2nd I.F.).	10.7 MC unmodu- lated.	Tuning gang wide open	Connect 3300 ohm carbon resistor across second- aries of both FM-IF transformers. Connect VTVM (DC probe) from point "W" to ground. (See Figure 19.)	"A" (ratio detector primary) for maximum reading on VTVM.
2	Thru .01 cond. to 1st IF grid (Pin #1 of 6BA6 1st I.F.).	**		Same as above.	Iron cores "B" and "C" (2nd IF trans.) for maximum reading on VTVM.
3	To FM antenna terminals. (Do not feed signal into converter grid.)	FM antenna ninals. (Do feed signal Same as above. In addition, connect a 50 mmfd. condenser in parallel with Cl0 to detune the IF rejection trap consisting of CH4 and Cl0. (See note at bottom of page.) This condenser MUST			Iron cores D and E for maxi- mum on VTVM. Re-adjust A, B, C, D, E for maximum. (Keep reducing generator out- put to keep VTVM at 1.5 volts.)
4	72	b. Re c. Tun ger d. Tu ger e. Ad res f. Tun diff cu	duce output of ne generator f nerator frequer ne generator f d generator fr ult is the cent ne generator f terent frequen- ve. If you ha	n resistors from IF transformers. isignal generator until VTVM reads exactly $+1.5$ vor requency above 10.7 MC until VTVM reads exactly hey. Extreme care in reading this is essential. requency below 10.7 MC until VTVM reads exactly hey. Extreme care in reading this is essential. requency in step c to generator frequency in step d er frequency of the IF curve to be used in step 5. requency above and below 10.7 MC and note voltag cy points until you have a good impression of the twe two peaks as in Figures 17 or 18, note readings the that would require realignment is illustrated by Figure 19. 19. The state of the the state of the state	+1.0 volt. Note exact +1.0 volt. Note exact and divide by 2. The See example on page 10. ge reading on VTVM at shape of the selectivity (voltage) of both peaks.
5	27	Center of IF selectivity curve per step 4e above. See "EXAM- PLE" on p. 10	Set pointer to upper limit on dial.	Connect VTVM (DC probe) from point "X" to ground. (See Figure 19.)	Iron core "F" (detector sec- ondary) for zero voltage read- ing on VTVM. (The correct zero point is located between a positive and a negative maximum.)

If any adjustments were very far off, it is desirable to repeat steps 3, 4 and 5.

Note: Condenser C10 is mounted parallel to the chassis on the bakelite terminal board. Connect added 50 mmfd. condenser between the terminal board lug (junction of CH4 and R5) and pin #1 of the 6BA6 (GG RF stage). With the chassis in the position shown in figure 19, the correct terminal board lug is located on the corner nearest trimmer "G", and on the left side of the terminal board.

Servicing Notes on 1947-1948 F. M. and Television Receivers Admiral CHASSIS 9A1 MODEL 7C73

SETTING SIGNAL GENERATOR TO CENTER OF IF SELECTIVITY CURVE

CAUTION: Due to the difficulty of setting a signal generator to the accuracy required by this operation, extreme care must be exercised in making each setting. Otherwise improper alignment of the radio detector and consequent audio distortion will result.

EXAMPLE: (See Figs. 13 and 14)

Voltage reading in Step 4b is + 1.5 volts.

- Generator frequency on low side of 10.7 MC for a reading of +1 volt DC = 10.640 MC.
- Generator frequency on high side of 10.7 MC for a reading of +1 volt DC = 10.800 MC.
- Center frequency is obtained by adding 10.640 and 10.800, then dividing by 2. For these readings it will be 10.72 MC.
- Set generator frequency to 10.72 MC as this is center of selectivity curve as shown in Figure 14.

Note: Numerical vernier dial readings may be used instead of MC.

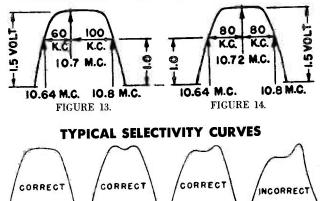


FIGURE 17.

signal

1300 KC

V

FIGURE 18.

FIGURE 16. FIGURE 15.

FM RF ALIGNMENT PROCEDURE

Alignment of FM RF section will require re-alignment of AM RF section

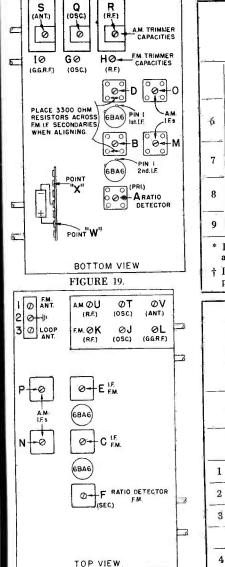


FIGURE 20.

	1	among thim	section will req mer capacities ned, however,	during AW	operation. 4	YINT INT			
, <u> </u>	Connect Signal Generator	Generator Frequency	Receiver Dial Setting	Output India and Connectio	Adj	ust as follows			
6	Thru 270 ohms to FM ant. terminal.	108.5 MC† (unmodu- lated).	Tuning gang wide open	Connect VT (DC probe) point "W" ground.	from "H" an	ity trimmers "G", ad "I" for maxi- eading on VTVM.			
7	75	102 MC [†] (unmodu- lated).	102 MC	13	and "	slugs "J", "K" L" for maximum eading on VTVM.			
8	25	108.5 MC ⁺ (uninodu- lated).	Tuning gang wide open	η		beat Step #6.			
9	Alignment section m	of the FM ust be realign	RF section w ned after the F	ill affect the M RF alignm	AM band als ent.	so so the AM RF			
4]	 * It is advisable that generator output be adjusted so that VTVM readings do not exceed approximately +1.5 volts DC after peaking. † If your signal generator does not reach this frequency, use harmonics as described in 								
	paragraph on "	FM Alignmer	nt'' .						
	 Be sure bo starting ali Turn receiv Use lowest on meter 	e output mete th the set an gnment. ver Volume O output setti		cross speaker enerator are t generator that	voice coil. horoughly war	med up before			
	Connect Signal	Dummy Between Signal	Antenna Radio and Generator	Signal Generator Frequency	Receiver Dial Setting	Adj. Trimmers in Following Order to Max.			
	Set Band Switch to Broadcast position (center) and be sure to follow instructions under heading "Important Preliminary Alignment Steps." (See page 9). Loop antenna can be disconnected from chassis in Steps 1, 2 and 3.								
1	65B7.Y J MED 455 KC Tuning gang M. N. O. P								
2	To loop ant	-	irect nection	1605 KC	Tuning gang wide open	Q, R			
3	To loop ant.	D	irect nection	1300 KC	1300 KC	T. U			
	Set Re Loop A	ceiver Chass ntenna to R	is on table r eceiver.	next to back		Connect			
4	To loop ant	10 MMFD	(Or wrap sev- of generator	1605 KC	Tune in signal	S			
			nd white loop	1000 VC	Tune in	v			

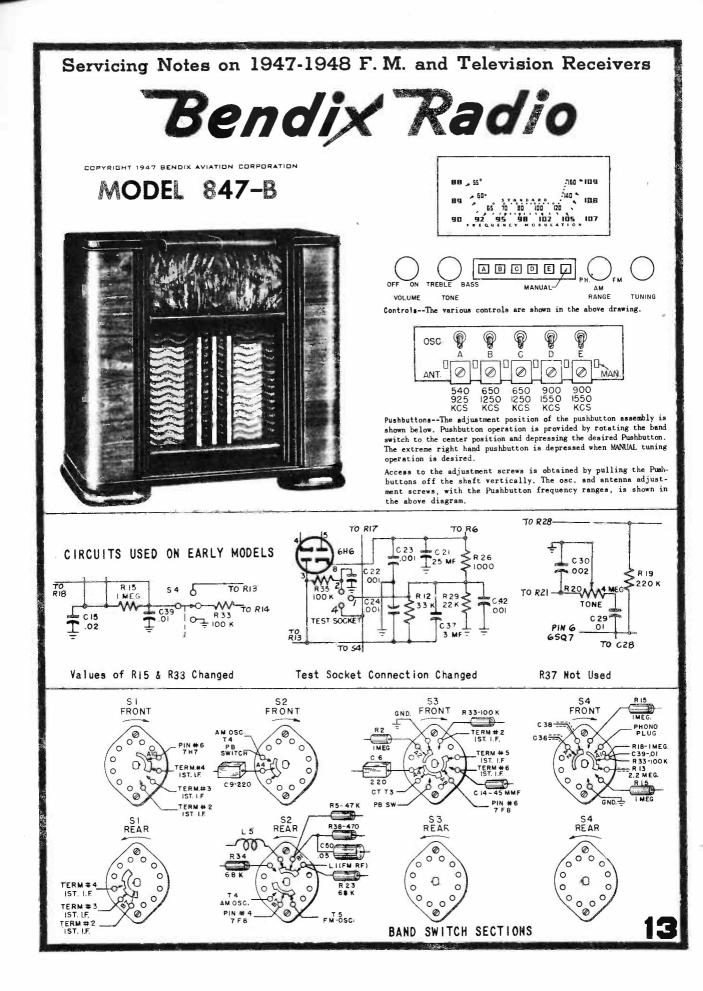
lead around white loop

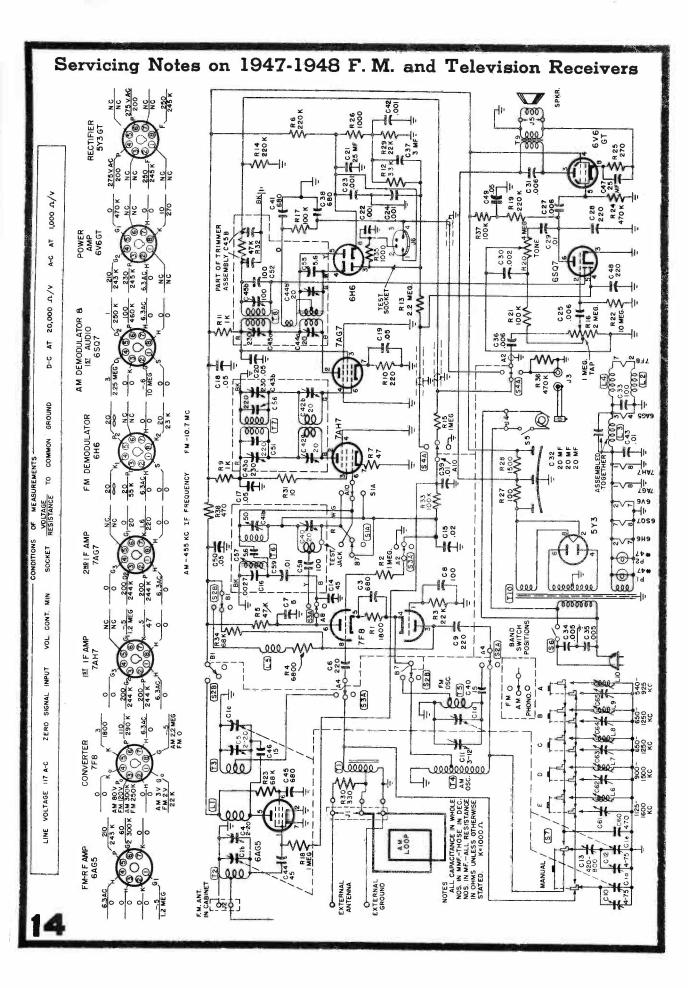
lead.)

To loop ant.

terminal #3

5





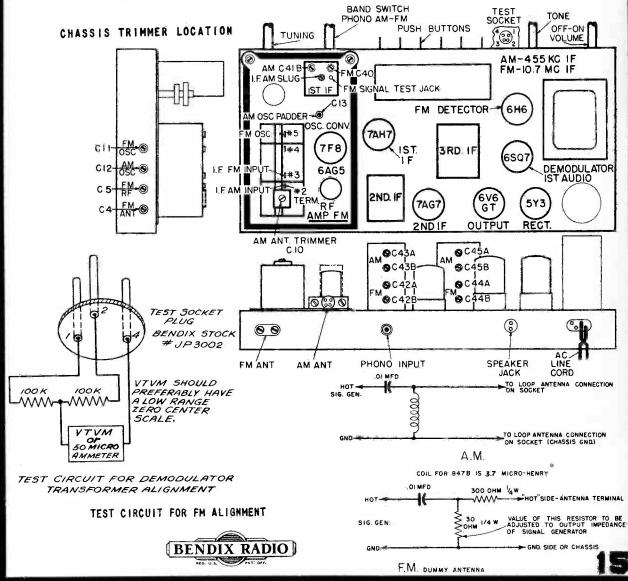
Servicing Notes on 1947-1948 F. M. and Television Receivers BROADCAST BAND ALIGNMENT

Rotate gang condenser until full closed. Set pointer to reference mark. Connect output meter across voice coil on lowest scale. Signal Generator amplitude modulated. Rotate volume control full ON. Keep generator output low as practical.

Thru	То	Band Switch Position	Dial Setting	Adjust
.05 mfd.	Term. #2 gang cond. & chassis	AM-mid- position	Gang cond. full open	IF slug, C41B, C43A, C43B, C45A, C45B for max output
Bendix dummy loop ADOLOO	Dummy loop plugged in AM ant. socket on rear of chassis	n	580 KC ref. mark	C13 for max. output
n	n	π		*CI2,CI0 for max. output
A	*	P	Approx. 580 KC ref. mark	CI3 for max. output "Rock" gang during adjustment
m	.	n	Approx. 965 KC ref. mark	**Check Calibration
m	37	N	Approx. 580 KC ref. mark	**Check Calibration
	.05 mfd. Bendîx dummy loop ADOLOO n	.05 mfd. Bendix dummy loop AD0L00 Term. #2 gang cond. & chassis Dummy loop plugged in AM ant. socket on rear of chassis " " " " " " " " " " " " " " " " " " "	Thru To Switch Position .05 mfd. Term. #2 gang cond. & chassis AM-mid- position Bendix dummy loop AD0L00 Dummy loop plugged in AM ant. socket on rear of chassis " n " " n " "	Inru Io Switch Position Setting .05 mfd. Term. #2 gang cond. & chassis AM-mid- position Gang cond. full open Bendix dummy loop ADOLOO Dummy loop plugged in AM ant. socket on rear of chassis " 580 KC ref. mark " " 1475 KC ref. mark " " Approx. 580 KC ref. mark " " Approx. 965 KC ref. mark " " "

* Repeat 1475 KC and following 580 KC adjustment in rotation several times until receiver is properly aligned.

** If calibration does not check within 10 KC, "knife" oscillator and antenna gang sections.



A - CW METER METHOD

For reference marks see Fig. Rotate gang condenser fully closed and set pointer to reference mark Trimming screwdriver must be 100% insulated Generator output - pure RF or amplitude modulated VTVM must not be AC-DC, or with GND. connected to AC line or through resistor

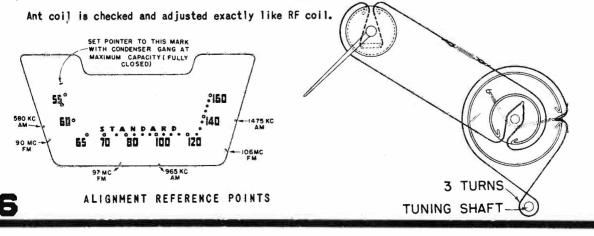
Gen. Freq.	Dummy Ant.	Gen. To	Band Sw. Position	Pointer Setting	Special Conditions	VTVM Connections	Adjust	Remarks
10.7 mc.	•01 mfd	Term⊾ #3 on gang & chassis	FM-Full counter- clock- wise		Short FM osc.term. #5 to chassis	Test socket pins #1 (+) & #2 (-) Low Scale		Realign several times to assure max. output Signal may be fed into "Test Jack" in 1st IF can for prel. align. of C444,C42A & C42B.
10.7 mc.	H	n	n		Ħ	*Center of jumper res- istors & test sock. Pin #4 - Fig. #2.	Srd. IF-C448 To zero reading on VTVM	**Alternate step #1 (C44A for max. output) & step #2 (C44B for zero) several times to assure correct alignment
106 mc.	Std. FM Fig. #4	FM ant input term's.	R	106 mc. refer. mark	Remove short from osc. term. #5	Test socket pins # (+) & #2 (-) Low scale	***OscCII RF -C5 Ant -C4 for max.out- put on VTVM	"Rock" tuning control during alignment
97 mc.	N	17	fi	Approx. 97 mc ref. mark	යා දා ආ ග යා දා දා යා යා යා	(m) M		****Check Calibra- tion
90 mc.	n		64	Approx. 90 mc. refer. mark	677 gal (2) gal (2) gal (2) (2) (2) (2) (2) (2) (2) (2) (2) (2)	W		****Check Calibra- tion

* See Fig. "Test Circuit for FM Alignment".

** A VTVM with a zero center scale is very convenient for use in this alignment step. A50 microammeter may be used in place of the VTVM, but is not as accurate.

- *** The oscillator circuit has been designed to operate on the high freq. side of the incoming signal. It is possible to adjust the trimmer (CII) at 106 MC such that the osc. is operating on the "image" or low freq. side of the signal. To check the osc. (CII) adjustment, set sig. gen. to 84.6 MC, freq. modulated, dial pointer at 106 MC. If signal is NOT heard, adjustment of CII is correct, but if signal <u>15</u> heard, osc. trimmer CII has been incorrectly adjusted on the "image" frequency. Readjust CII to other setting at 106 MC and recheck with gen. freq. at 84.6 MC. Signal <u>MUST</u> NOT be heard with pointer at 106 MC and sig. gen., freq. modulated, set at 84.6 MC.
- *** If calibration is not within reasonable tolerance at these points, the osc. coil inductance must be adjusted. If dial pointer reading is on low freq. side, inductance is too low, and turns must be compressed slightly. If pointer reading is on high freq. side, osc. coil is too high and coil turns must be spread slightly.

To check and adjust inductance of ant. and RF coils, tune receiver to 90 MC signal and observe AVC reading. Insert iron core end of "tuning wand" into RF coil, at same time rocking tuning control to max. AVC. If reading increases as wand is inserted, RF coil inductance is too low and turns must be compressed slightly. If reading decreases, reverse wand and insert metal end into coil, again rocking tuning control to max. AVC. If reading decreases, (after iron core check), inductance is properly adjusted. If reading increases, inductance is too high and turns must be spread slightly.



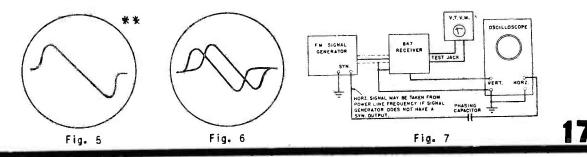
Servi	cing N	lotes	3 on 19	947-1	948 F.	M. ar	nd To	elevis	ion F	Receivers
	al Metho				ALIGNMEN					anga personan mana ana kana mana ang kana ang ka
Gen. Freq.	Gen. Mod.	Dummy Ant.	Generator to	Band SW. Position	Special Conditions	Dial Setting	VTVM Conn	Oscillo- scope	Adjust	Remarks
10.7 MC	Pure RF or Amplitude	.05 mfd	High side to Term. ∦3 Gang Cond. Low side to chassis	FM-Max. CCW.	Short Osc. Stator- Term.#5 to Chassis Gnd.		Socket Pins #I (+) & #2 (-) Low Scale		С40 2nd IF С42А, С42В 3rd IF С44А	Adjust for max- imum output on low range of VTVM - Realign each Cond. several times to assure max. out- put. Signal may be fed into "test jack" in 1st IF can for Prelim. Alignment of C44A.C42A & C42B.
Approx. 10.7 MC Adjust until Ratio Detector curve is cen- tered on Horiz Scope Sweep	Freq.Mod. 60 Cy- Sweep width max. possible (should be 200 KC Min)				H			Connect vert.in- put to Test Socket Pins #4 & Chass is Gnd.	3rd IF C44B	*Adjust for max. symmetrical "S" curve similar to Fig. 5. Alternate adjs. of C44A & C44B to obtain Max desired curve.
Line 106 MC	8	8td. FM Fig.4	FM Ant. Terms's thru dummy	*	Remove short from Term #5.		No con- nection	n	FM Osc. CII	**Adjust until "S" curve is centered on Horiz.Sweep scope line.
106 MC	13	Ŕ	Π	H		Π	71	97.	FM RF Trimmer C5. FM Ant. Trimmer C-4.	pattern-"rock" tuning control at same time to keep "S" curve centered on Scope.
97 MC	ж	.8	И.	π		Approx. 97 MC ref.mark	1	8		***Check Cal- ibration
90 MC	н	9	N.	в		Approx. 90 MC ref.mark	ĸ	n	*****	***Check Cal- ibration

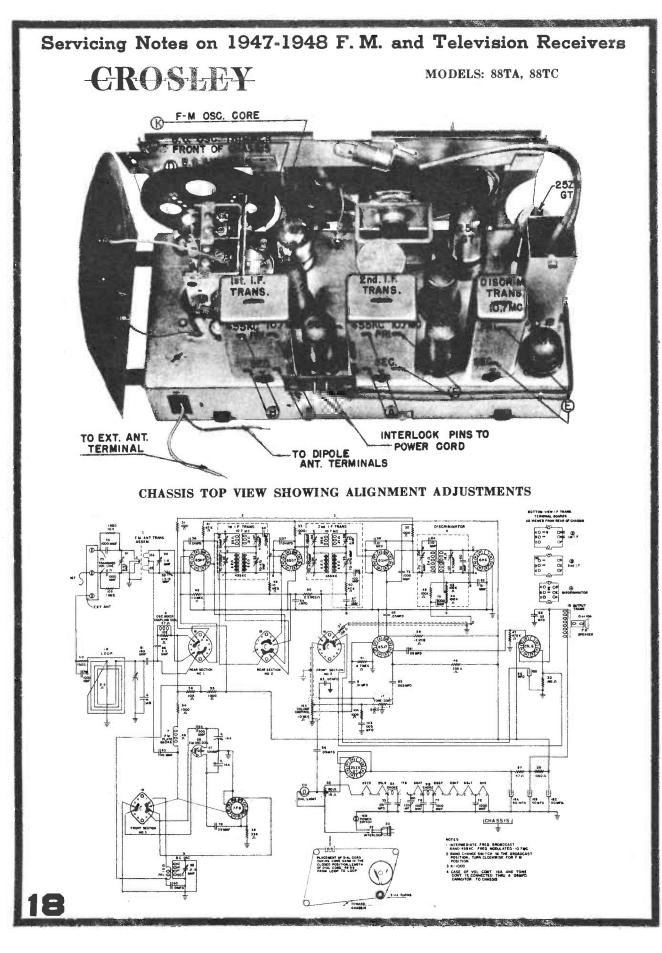
Some phase shift between the Signal Generator and the scope horizontal sweep may be encountered, resulting in a double trace pattern, shown in Fig. 6. In some Oscilloscopes, provision is made for connecting this phase shift directly in the oscilloscope circuit. If so, rotate the "phase shift" control until the curves coincide as in Fig. 5. If no provision is made in the scope, the connection might be accomplished by in-serting a condenser of suitable value in series with the signal generator "Synchronized Sweep Voltage" output. The condenser value will depend upon the amount of phase shift and the horizontal input impedance of the scope - approximate condenser range of the limit. of the scope - approximate condenser range .01 to .1 mfd. See Fig. 7 for instrument connection diagram.

See ** * #

If calibration is not within tolerance at these points, the inductance of local FM oscillator coil, RF and antenna coils must be adjusted. ***

NOTE: The latter operation is a very delicate and difficult procedure, and must be attempted only by tech-nicians of considerable high frequency experience.





Servicing Notes on 1947-1948 F. M. and Television Receivers ALIGNMENT CHART

	ľ	Sign	al Gener	ator Output	Por	sition of				Remark-
ment	Type Gen- erator	Fre- quency	In Series with	То	Range Switch	Dial Pointer or Var. Cond.	Adjust	Type of Selectivity Curve	Osc. Fre- quency	
1	AM	455 kc	100 mmf.	Mixer Grid 6SH7	AM	Open	A & B	Single Peak		See Note 1
2	AM	1400 kc.	100 mmf.	Stator Plates, Ant. Section of Var. Cond.	AM	1400 kc.	C	1.2.2.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.	Above	See Notes 1 and 2
3	AM	1400 kc.	220 mmf.	Loop Primary	AM	1400 kc.	D	• • • • • • • • • • • • • • • •	Above	See Note 1.
4	FM	10.7 mc.	30 mmf.	2nd I.F. Grid 6SH7	FM	Closed	E	~		See Notes 1, 3, 4. 5 & 6
5	FM	10.7 mc.	30 mmf.	1st I.F. Grid 6SG7	FM	Closed	F	2	5. 1. 10 p. p. 6 44	See Notes 3, 5 & 6.
6	FM	10.7 mc.	30 mmf.	F.M. Ant. Terminals	FM	Closed	G	N	43 - 4 4 4	See Notes 3, 5 & 6.
7	FM	98.0 mc.	*78 ohm Dummy	F.M. Ant. Terminals	FM	98 mc.	H & I	Single Peak	6 v p 2 6 5	See Notes 7 & 9
8	Disco		enerator ength Me	. Connect Field eter.*	FM	92 mc.	J		L., K. F. F. K.	Adjust for null point. See Note 8.
9	If Tri	mmer (J) in Ste	ep 8 is turned i	more the	an ¼ turn, rej	peat Step 7.			
10	Repe	at Step	8 if Ste	p 9 was necess	ary.					
11	FM	98.0 mc.	*78 ohm Dummy	F.M. Ant. Terminals	FM	98 mc.	K			Adjust for maximum out- put.

- 1. All Amplitude Modulated input signals are modulated 30% at 400 cycles with the High side of the signal generator connected to receiver as indicated in the alignment chart. Connect the low side of signal generator thru a 0.1 mfd condenser to the receiver chassis.
- 2. Receiver should tune thru peaks at 540 and 1600 kc.
- 3. Sweep generator alignment. (For 10.7 mc. I.F. alignment use approximately 450 kc. sweep width).
- 4. Sweep generator output 0.1 to 1 volt R. M. S.
- 5. Connect high side of scope to discriminator transformer terminal at shielded lead wire junction. Connect low side of scope to the receiver chassis.
- 6. Align for maximum peak amplitude. Peak separations should be 150 to 170 kc.
- 7. Disconnect scope. Connect output meter to voice coil (3.2 ohms).
- 8. It is important that the radiation balance trimmer be adjusted to the null point for proper operation of the Frequency Modulation band. To check the null point, connect a Field Strength Meter across the F.M. antenna primary trimmer.
- 9. (a) With the F.M. signal generator set to 98.0 megacycles, feed a signal, modulated with 400 cycles at 30% to the receiver as indicated in the alignment chart. Shunt the antenna primary trimmer with a 10 ohm carbon resistor and adjust trimmer (H) for maximum output.
 - (b) Place the 10 ohm carbon resistor across the F.M. antenna secondary trimmer and adjust trimmer (I) for maximum output. Remove 10 ohm carbon resistor from secondary trimmer.

Capyright 1947. CROSLEY Division-AVCO Manufacturing Corporation

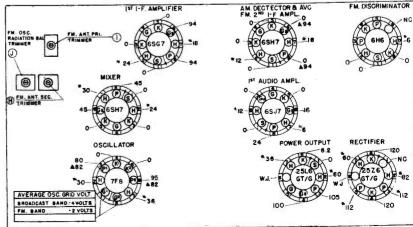
REPLACEMENT PARTS LIST-MODELS 88TA, 88TC

Figures in first column correspond to figures in Schematic Diagram

	F			00000 00	Deviator 1 marshim 1/ 11
Item	Dent No.	Description	49	39373-92	Resistor, 1 megohm, $\frac{1}{2}$ w. Resistor, 2.2 megohm, $\frac{1}{2}$ w.
No.	Part No.	The short a laboratory	50	39373-97 39373-102	Resistor, 4.7 megohm, ½ w.
			51		Resistor, 80 ohm (Wire Wound) Two
1	AC-137783	Transformer Assy., Antenna (F.M.)	52	W-139035	Resistor, 18 ohm (Wire Wound) Section
2	AC-138819	Transformer Assy., 1st I.F.	F 4	90001 17	Condenser, .05 mfd., 600 v., paper
3	AC-139094	Transformer Assy., 2nd I.F.	54	39001-17	Condenser, .05 mfd., 600 v., paper
4	AC-139077	Transformer Assy., Discriminator	55	39001-17	Condenser, .01 mfd., 600 v., paper
5	AW-138924	Coil Assy., Oscillator (Broadcast)	56	39001-13	Condenser, .01 mfd., 600 v., paper
6	AW-138950	Coil Assy., Oscillator Mixer Coupling	57	39001-13	Condenser, .01 mid., 600 v., paper
7	AW-138978	Choke Assv., Plate (F.M. Usc.)	58	39001-13	Condenser, .01 mfd., 600 v., paper
8	AW-139056	Condenser Assy01 mfd., 200 v., (shielded)	60	39001-13	Condenser, .01 mfd., 600 v., paper
9A	AW-136720	Choke, R.F. Heater Choke, R.F. Heater	61	39001-17	Condenser, .05 mfd., 600 v., paper
9B	1100120	Choke, R.F. Heater Assy.	62	39001-17	Condenser, .05 mfd., 600 v., paper
10	AB-139118	Loop and Support Assy., Antenna	63	39001-17	Condenser, .05 mfd., 600 v., paper
11	Part of Item 1	Coil Assy.	64	39001-19	Condenser, .1 mfd., 600 v., paper
12A	Part of Item 1	Coil)m	65	39001-76	Condenser, .003 mfd., 600 v., paper
12B	1 alt of 10cm 1	Coil Two Section Assy.	66	39001-80	Condenser, .02 mfd., 600 v., paper
13	AD-138246	Speaker	67	Part of Item 3	Condenser, 100 mmf., 300 v., ceramic
	C-139028	Condenser, Variable Two	68	Part of Item 3	Condenser, 100 mmf., 300 v., ceramic
14A	0-109020	Condenser, Variable) Section	69	Part of Item 2	Condenser, 100 mmf., 300 v., ceramic
14B	B-137364	Transformer Output	70	C-137727-8	Condenser, 1000 mmf., 300 v., ceramic
15		Control, Volume (1 megohm) Assy.	71	C-137727-8	Condenser, 1000 mmf., 300 v., ceramic
16A	B-137781	Switch, Power	72	C-137727-8	Condenser, 1000 mmf., 300 v., ceramic
16B	00000 19	Control, Volume	73	C-137727-8	Condenser, 1000 mmf., 300 v., ceramic
-	39368-18	Shaft, Plug, in	74	C-137727-8	Condenser, 1000 mmf., 300 v., ceramic
* {	39370-2		75	Part of Item 4	
1	39369-1	Switch, Power Control, Tone (2 megohm)	76	C-137727-8	Condenser, 1000 mmf., 300 v., ceramic
17	B-137782	Control, Tone (2 megonin)	77	C-137727-8	Condenser, 1000 mmf., 300 v., ceramic
	39368-11	Control, Tone Condenser, 50 mfd., 200 v. Four	78	Part of Item 1	
18A	B-137976	Condenser, 50 mfd., 200 v. Section	79	C-137727-19	Condenser, 39 mmf., 300 v., ceramic
18 B		Condenser, 50 mild., 200 v. Elect	80	Part of Item 4	
18C	1	Condenser, 50 mfd., 150 v. Elect.	81	C-137727-24	Condenser, 180 mmf., 500 v., ceramic
18 D		Condenser, 20 mfd., 25 v. Filter	82	C-137727-28	Condenser, 51 mmf., 500 v., ceramic
19	B-137986	Switch, Band Change	83	C-137727-37	Condenser, 10 mmf., 300 v., ceramic
20	W-48858	Bulb (Dial), Type 47, 6.3 v., .15 amp.	84	Part of Item 4	
21	39012-70	Iron Core, F.M. Oscillator Coil	85	B-137499-5	Condenser, 500 mmf., 300 v., silver mica
22	AB-138971	Interlock Assy.	86	Part of Item	
23	C-132300-6	Cable and Plug Assy., Power	87	W-139285	Condenser, 52 mmf., ceramic
25	W-137143	Transmission Line, 75 ohm	88	W-138268	Condenser, Trimmer
26	W-139286	Coil, Oscillator (F.M.)	89	C-136327-29	Condenser, Trimmer
27	39373-9	Resistor, 47 ohm, 1/2 w.	90	Part of Item	
28	39373-93	Resistor, 1.2 megohm, ¹ / ₂ w.	91	Part of Item	
29	39373-143	Resistor, 1000 ohm, 1 w.	92	Part of Item	
30	39373-16	Resistor, 150 ohm, ¹ / ₂ w.	93	Part of Item	
31	39373-33	Resistor, 1000 ohm, 1/2 w.	94	Part of Item	
32	39373-33	Resistor, 1000 ohm, $\frac{1}{2}$ w.	94	Part of Item	
33	39373-33	Resistor, 1000 ohm, 1/2 w.	96	Part of Item	
34	39373-33	Resistor, 1000 ohm, 1/2 w.		Part of Item	
35	39373-33	Resistor, 1000 ohm, ¹ / ₂ w.	97 98	Part of Item	
37	39373-54	Resistor, 10,000 ohm, 1/2 w.	98	Part of Item	
38	39373-54	Resistor, 10,000 ohm, ¹ / ₂ w.	100	Part of Item	
39	39373-64	Resistor, 33,000 ohm, 1/2 w.	100	Part of Item	
40	Part of Item 3	Resistor, 47,000 ohm, 1/2 w.		Part of Item	
41	39373-67	Resistor, 47,000 ohm, 1/2 w.	102		Condenser, .005 mfd., 600 v., paper
42	Part of Item 4	Resistor, 100,000 ohm, 1/2 w.	103	39001-11	Resistor, 100,000 ohm, 19 w.
43	Part of Item 4	Resistor, 100,000 ohm, 1/2 w.	104	39373-74	Condenser, 1000 mmf., 300 v., ceramic
44	Part of Item 4	Resistor, 100,000 ohm, ½ w.	105	C-137727-8	Resistor, 1 megohm, 1/2 w.
46	39373-84	Resistor, 330,000 ohm, 1/2 w.	107	39373-92	
47	39373-87	Resistor, 470,000 ohm, 1/2 w.	108	39373-92	Resistor, 1 megohm, 1/2 w.
48	39373-92	Resistor, 1 megohm, $\frac{1}{2}$ w.	109	Part of item	10 Resistor, 1 megohm, $\frac{1}{2}$ w.
					AM DECTECTOR & AVC FM. DISCRIMINATOR

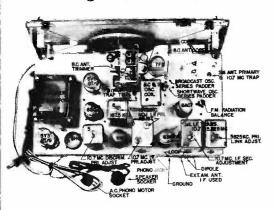
SOCKET VOLTAGE CHART

NOTES: 1 BOTION VIEW OF TUBE SOCKETS. 2 MEASURE VOLTAGE WITN AN ELECTRONIC VOLTMETER FROM BOCKET LUS TO CHARBIG. 3.ALL VOLTAEGS ARE THE BANE FOLDS. B FM EXCEPT WIRTE MARTED STITUE BANE FOLDS. B FM EXCEPT WIRTE BAND SWITCH IN THE FM. POSITION S.KC. NO CONSECTION 7.8 - AC VOLTAGE 8.SOCKET VOLTAGE TOLERANCE 10% DTES

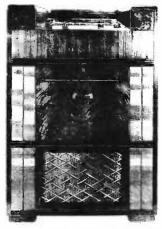


Model: 87CQ and Revised Models: 86CR, 86CS

Pages 21 to 28.



Model 87CQ



Model 86CR—Walnut Cabinet and Albums. Model 86CS—Mahogany Cabinet with doors. No albums.

TYPE: Eight-tube, three-band, Superheterodyne. **FREQUENCY RANGE:** Standard American Broadcast Band: 540 to 1600 kc. (Selector Switch to AM position).

Short-wave Band: 9.45 to 11.9 mc. (Selector switch at SW position).

Frequency Modulated Band: 88.1 to 107.9 mc., Channel 201 to 300 (Selector Switch at FM position).

INTERMEDIATE FREQUENCY: Standard American Broadcast Band and Short-wave Band: 5825 and 167.5 kc. Frequency Modulation Band: 10.7 mc.

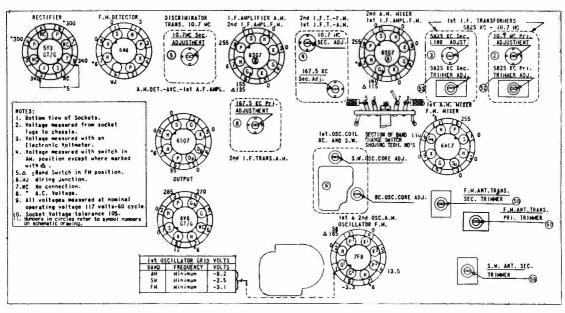
POWER SUPPLY: 60 cycle a.c. only.

VOLTAGE RATING: 105-125 volts.

POWER CONSUMPTION: 85 watts maximum at normal power supply voltage (117 volts), 20 watts additional for record changer.

POWER OUTPUT: 8 watts maximum at 3.2 ohm load.

NOTE: Models 87CQ, 86CR, 86CS, use the Model "K" Automatic Record Changer.



SOCKET VOLTAGE CHART SHOWING BOTTOM ALIGNMENT ADJUSTMENTS

Copyright 1947. CROSLEY Division-AVCO Manufacturing Corporation

Servicing Notes on 1947-1948 F. M. and Television Receivers ALIGNMENT EQUIPMENT

The following equipment is used as indicated in the alignment charts and alignment notes: Signal Generators:

- 1. Amplitude Modulated Signal Generator with 400 cycle modulated signal to cover 167.5 kc. to 108 mc.
- 2. Frequency Modulated Signal Generator to cover 87 to 108 mc., with sweep to cover 10 to 30 kc. on narrow band and 450 kc. on wide band (Scope alignment only).

Cathode Ray Oscillograph (Scope alignment only).

Meters:

- 1. Suitable Output Meter.
- 2. Field Strength Meter (Fig. 1). This meter may consist of a D.C. 100 microampere (full scale) meter, shunted by a 1000 mmf. mica by-pass condenser; a crystal

5 FOOT 75 OHM

TO DIPOLE ANT.

DIPOLE ANT.

TERMINALS

LOOP TERMINAL

GROUND

TERMINALS

TWISTED PAIR

RECTIFIER

IOQUA

1000 mmf

Fig. 1

www.

CARBON RESISTORS

www.www

Fig. 2

70 mm f 14.7

uh.

Fig. 3.

39 OHM

39 OHM

GERMANIUM

CRYSTAL

F. M. SIGNAL

GENERATOR

TERMINALS

HIGH SIDE OF GENERATOR THRU

GROUND SIDE OF

30 uuf GAP.

rectifier connected in series with the meter and a five foot, 75 ohm twisted, pair of leads. The open ends of the leads are connected to the dipole antenna terminals. Connect condenser directly across meter terminals, and crystal directly to one terminal of meter. Keep connecting leads as short as possible.

Dummy Antennas:

- 1. 78 ohm Dummy Antenna (Fig. 2).
- 2. Dummy Loop Antenna (Fig. 3) is used to replace "Signal Web" antenna, when chassis is removed from cabinet.

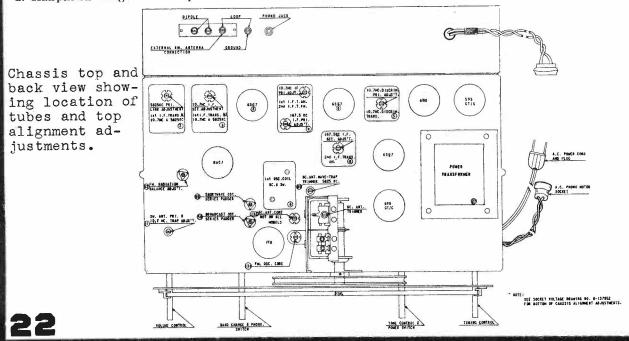
Condensers:

1. 0.1 mfd. Condenser.

2. 30 mmf. Condenser.

Shunts:

- 1. 5000 ohm carbon Resistor in series with a 0.1 mfd. Condenser.
- 2. Hairpin Shorting Shunt composed of two inches of No. 14 bare tinned copper wire.



Turn the tuning condenser to full mesh, against stop, and set the dial pointer to the reference point which is to the left of Channel 200 on the dial.

Set tone control knob to the treble position, (extreme right).

When output meter is used, connect across voice coil: (3.2 ohms).

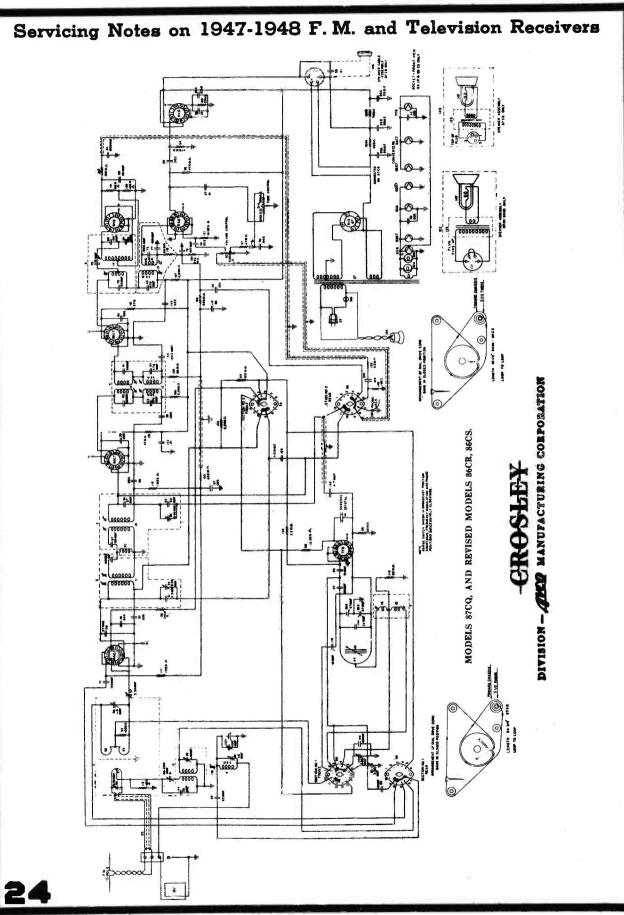
Feed an R. F. signal modulated 30% at 400 cycles to the receiver as indicated on the alignment chart

When F. M. signal generator is used, a 30% modulated signal is equal to 22.5 kilocycles deviation.

Turn volume control knob to maximum clockwise position and adjust signal generator output to produce a noticeable output meter reading, (approx. 500 mw.) Keep signal generator output as low as possible to prevent excessive AVC action in the receiver.

	A. M. S	ignal Gene	rator Output	Position of		ALIGNMENT	CHART	(Output Meter Method)
Align- ment equence	Frequency	In Series with	To	Range Switch	Dial Pointer or Var.Cond.	Adjust	Osc. Frequency	Remarks (Alignment notes begin on page 2
1	167.5 kc.	0,1 mfd.	2nd I. F. Grid 6SG7 (B)	SW	Open	2nd I. F. Trans. (8)		See Note 1
2	167.5 kc.	0.1 mfd.	1st I. F. Grid 6SG7 (A)	SW	Open	1st I. F. Trans. (4)		See Note 2
3	10.7 mc.	30 mmf.	2nd I. F. Grid 6SG7 (B)	FM	Open	Discriminator Trans. (5)		See Note 3
4	10.7 mc.	30 mmf.	1st I. F. Grid 6SG7 (A)	FM	Open	2nd I. F. 10.7 mc. Trans. (4)		See Note 4
5	10.7 mc.	30 mmf.	See Note 5	FM	Open	1st I. F. 10.7 mc. Trans. (2) & (3)		See Note 5
6	5825 kc.	30 mmf.	*Link Coupling on 10.7 mc. I. F. No. 2	sw	Open	5825 kc. I. F. Trans. (3)	167.5 kc. Above	See Note 6—*The short lea between Transformers No. 2 &
7	5825 kc.	30 mmf.	6AC7 Grid	SW	Open	5825 kc. I. F. Trans. (2)	167.5 kc. Above	See Note 7
8	100 mc.	*78 ohm Dummy	F. M. Dipole Terminals	FM	Channel 260.5	F. M. Osc. Core F. M. Ant. Trims. Sec. & Prim.	10.7 mc. Above	See Note 8—*See "Dummy Antennas (1)"
9	97.9 mc.	*78 ohm Dummy	F. M. Dipole Terminals	FM	Channel 250	F. M. Osc. Core	10.7 me. Above	See Note 9-*See "Dummy Antennas (1) "
10		isconnect (ect Field St	lenerator trength Meter	FM	Channel 215	Radiation Bal. Trimmer		*See Note 10—*See "Field Streng Meter"
11	*9.6 mc.	30 mmf.	One F. M. Ant. Term.	SW	9.6 mc.	S. W. Oscillator Series Padder	5825 kc. Above	*Disconnect Field Strength Met Connect Signal Generator. S Note 11
12	11.8 mc.	30 mmf.	One F. M. Ant. Term.	SW	11.8 mc.	S. W. Osc. Core	5825 kc. Above	See Note 12
13	10.7 me.	30 mmf.	One F. M. Ant. Term.	SW	10.7 mc.	S. W. Ant. Prim. & Sec. Padder		See Note 13
14	10.7 mc.	30 mmf.	One F. M. Ant. Term.	FM	10.7 mc.	S. W. Primary (10.7 mc. Trap)		See Note 14
15	535 kc.	30 mmf.	*HI. Side of Dummy Loop Ant.	AM	Closed	B. C. Oscillator Series Padder	5825 kc. Above	*See Note 15—See "Dummy Antennas (2)"
16	1620 kc.	30 mmf.	HI. Side of Dummy Loop Ant.	AM	Open	B. C. Osc. Core	5825 kc. Above	See Note 16
17	1400 kc.	30 mmf.	HI. Side of Dummy Loop Ant.	AM	1400 kc.	B. C. Antenna Trimmer		See Notę 17
18	600 kc.	30 mmf.	HI. Side of Dummy Loop Ant.	AM	600 kc.	B. C. Antenna Core•		See Nøte 18
19	5825 kc.	30 mmf.	HI. Side of Dummy Loop Ant.	AM	1400 kc.	B. C. Wave Trap Trim.		See Note 19
20	600 kc.	See Not	e 20					

*Refer to remarks (with corresponding asterisk) in last column.



ALIGNMENT NOTES (Output Meter Method)

Use the following notes in conjunction with ALIGNMENT CHART, TOP AND BACK VIEW, SOCKET VOLTAGE CHART, and SCHEMATIC DIAGRAM. Reference numbers of parts correspond to item numbers in Parts List.

- 1. (a) Place Shunt from link, between transformers (5) and (8), to ground See "Shunts (1)," Adjust secondary (top) for maximum output.
 - (b) Connect the Shunt from diode plate (pin No. 4) of 6SQ7 tube socket to the shielded lead junction on transformer (8). Adjust primary (bottom) for maximum output. Remove Shunt.
- 2. (a) Place Shunt from plate of the 6SG7 tube socket (A) to the transformer side of 2200 ohm resistor (106), See "Shunts (1)".
 Adjust secondary (bottom) for maximum output.
 - (b) Connect the Shunt from grid of the 6SG7 tube socket (B) to Transformer side of 68,000 ohm resistor (109). Adjust primary (top) for maximum output. Remove Shunt.
- 3. (a) Adjust secondary (bottom) core for null point.
 - (b) Tune Signal Generator for maximum Output Meter reading, approximately 75 to 100 kc. off the null point obtained in 3 (a), and note reading.
 - (c) Tune Signal Generator to the opposite side of the null point for maximum reading on the Output Meter. Note this reading. If the two readings are not equal, adjust primary (top) core until equal readings are obtained.
- 4. (a) Set Signal Generator to peak on high side of 10.7 mc. and adjust primary (top) and secondary (bottom) for maximum output. Note meter reading.
 - (b) Set Signal Generator to peak on low side of 10.7 mc. and note reading. If necessary, readjust primary (top) and secondary (bottom), slightly, until Output Meter readings and frequency spacing are equal on both sides of the 10.7 mc. null point.
- 5. (a) Connect Signal Generator output in series with a 30 mmf. condenser to either lug of the F. M. antenna transformer primary Trimmer (60). Connect Signal Generator ground to the receiver chassis at a point close to the trimmer. Keep lead lengths to a minimum and do not drape shielded cable, from Signal Generator output, near under side of chassis.
 - (b) Set Signal Generator to peak on high side of 10.7 mc. and adjust 10.7 mc. primary (bottom) of transformer (2). Adjust 10.7 mc. secondary (top) of transformer (3). These two adjustments should be adjusted for maximum output. Note reading on Output Meter.
 - (c) Set Signal Generator to peak on low side of 10.7 mc. and note Output Meter reading. If meter readings obtained on the peaks on both sides of 10.7 mc. are not equal, readjust the 10.7 mc. primary of transformer (2), and the 10.7 mc. secondary of transformer (3). The peaks should appear approximately 80 kc. on each side of 10.7 mc.
- 6. (a) Set Signal Generator frequency control for maximum output. Adjust 5825 kc. secondary Trimmer and secondary link adjustment, on bottom of transformer (3), for maximum output.
- 7. (a) Adjust 5825 kc. primary trimmer (bottom) and 5825 kc. primary link adjustment (top) of transformer (2) for maximum output.
- 8. (a) Adjust F. M. oscillator core (131), on top of chassis, to midway position.
 - (b) Preset F. M. radiation balance adjustment (57), on top of chassis, to approximately two turns from the closed position.
 - (c) Short circuit F. M. antenna primary trimmer (60), located on bottom of chassis, with Hairpin Shorting Shunt See "Shunts (2),"
 - (d) Adjust F. M. antenna secondary trimmer (58), on bottom of chassis, for maximum output.
 - (e) Transfer Shorting Shunt to F. M. antenna secondary Trimmer (58) and adjust F. M. antenna primary Trimmer (60) for maximum output.

- (f) Remove Shorting Shunt.
- 9. (a) Adjust F. M. oscillator core (131), slowly, until 97.9 mc. signal is tuned in. Receiver should tune thru 87.9 and 107.9 mc. signal (channel 200 and 300).
- 10. (a) Connect Field Strength Meter to dipole antenna terminals, on back of chassis.
 - (b) Adjust F. M. radiation balance trimmer (57), on top of chassis, to null point. If it is necessary to move this trimmer more than a quarter turn, repeat steps 8 and 10.

Alternate Method:—Connect a D.C. Vacumn Tube Voltmeter to No. 1 lug of 7F8 tube socket and adjust F. M. radiation balance trimmer for maximum grid volt reading.

- 11. (a) Set Signal Generator to 9.6 mc. modulated 30% at 400 cycles.
 - (b) Turn volume control to maximum.
 - (c) Adjust short-wave series padder (55), on top of chassis, for maximum output.
- 12. (a) Adjust short-wave oscillator core, on bottom of chassis, for maximum output. Repeat steps 11 and 12 until dial tracks at 9.6 and 11.8 mc.
- 13. (a) Shunt short-wave antenna primary padder (51), (lug connected to coil) to chassis with a Shorting Clip.
 - (b) Increase Signal Generator output if necessary.
 - (c) Adjust short-wave antenna secondary trimmer (59), for maximum output, while rocking variable condenser.
 - (d) Transfer the Shorting Clip to across the short-wave antenna secondary trimmer (59).
 - (e) Adjust short-wave antenna primary padder (51), for maximum output, while rocking variable condenser.
 - (f) Remove Shorting Clip.
- 14. (a) Connect Field Strength Meter from Signal Generator side of 30 mmf. condenser to chassis.
 - (b) Increase or decrease Signal Generator output until Field Strength Meter reads between 10 and 15 microamperes.
 - (c) Adjust short-wave antenna primary padder (51), for lowest reading on Field Strength Meter. Make this adjustment slowly, otherwise the dip may be passed unnoticed when a highly damped meter is used.
 - (d) Disconnect Field Strength Meter.

Alternate Method:—After the receiver is installed in cabinet, turn band switch to F. M. position and tune in an F. M. station. If a 10.7 kc. signal (indicated by a whistle or code) is heard in the speaker, adjust the short-wave antenna primary (51) until the interferring signal disappears or is minimized. Make this adjustment slowly.

- 15. (a) Connect Dummy Loop Antenna to Signal Web Antenna terminal and to ground terminal (See "Dummy Antennas (2)."
 - (b) Preset broadcast antenna wave trap (85), on top of chassis, to approximately two turns from the closed position.
 - (c) Adjust broadcast oscillator series padder (56), on top of chassis, for maximum output.
- 16. (a) Adjust broadcast oscillator core, on bottom of chassis, for maximum output.
 - (b) Repeat steps 15 to 16 until frequency shift stops.
- 17. (a) Adjust broadcast antenna trimmer, on top of variable condenser, for maximum output.
- 18. (a) Adjust broadcast antenna core (132), on top of chassis, for maximum output while rocking variable condenser.

- 19. (a) Set dial pointer to approximately 1400 kc. and retune Signal Generator to maximum output.
 - (b) Adjust Signal Generator output to approximately midscale reading on the Output Meter.
 - (c) Adjust broadcast antenna wave trap trimmer (85), for lowest reading on Output Meter.
 - (e) All Air Trimmers should be locked in position by applying a drop of household cement on the screw threads.
- 20. (a) After the receiver is placed in cabinet and all connections are made for normal operation, readjust the broadcast antenna core for maximum output at 600 kc.

		Signal Generator Output			Position of			Tune of	Osc.	
Align- ment Se- quence	ent Gen- le- erator Fre- In		То	Range Switch	Dial Pointer or Var. Cond.	Adjust	Type of Selectivity Curve	Osc. Fre- quency	Remarks	
1	F. M.	167.5 kc.	0.1 mfd.	2nd I. F. Grid 63G7 (B)	sw	Open	2nd I. F. Trans. (8), Top & Bottom	Flat or Double Peak		See Notes 1(a) & 2(a)
2	F. M.	167.5 kc.	0.1 mfd.	1st I. F. Grid 6SG7 (A)	sw	Open	1st I. F. Trans. (4), Bottom & Top	10% Double Peak		See Notes 1(a) & 2(a)
3	* A. M.	10.7 mc.	30 mmf.	1st I. F. Grid 6SG7 (A)	FM	Open	Discriminator Trans. (6), Bottom	Adjust for null point		*Disconnect F. M. Signal Generator and Scope See Note 5.
4	* F. M.	10.7 mc.	30 mmf.	1st I. F. Grid 6SG7 (A)	FM	Open	Discriminator Trans. (5), Top	~		*Disconnect A. M. Signal Generator and Output Meter See Notes 1(b), 2(b), & 3
5	F. M.	10.7 mc.	30 mmf.	1st I. F. Grid 6SG7 (A)	FM	Open	2nd I. F., 10.7 mc., Trans. (4), Top & Bottom	\sim		See Notes 1(b), 2(b), & 4 Readjust, slightly, dis- criminator primary (Top).
6	F. M.	10.7 mc.	30 mmf.	Grid.of 6AC7	FM	Open	lst I. F., 10.7 mc., Trans. (2) & (3)	\sim		See Notes 1(b), 2(b), & 4 Adjust Trans. (2) bottom. Adjust Trans. (3) Top
7	A. M.	Use Ali	ignmen	t Chart on pag	e 4. Beg	in with sequ	ence No. 6 and conti	nue thru to se	quence l	No. 19, inclusive.

ALIGNMENT CHART (Scope Method)

*Refer to Remarks (with corresponding asterisk) in last column.

1. (a) Sweep align (Use approximately 20 to 30 kc. to sweep).

(b) Sweep align (Use approximately 450 kc. to sweep).

- 2. (a) For 167.5 kc.; connect Scope to terminal No. 8 on the rear plate section of band change switch.
 - (b) For 10.7 mc.; connect Scope, thru a 100,000 ohm resistor, to lug No. 6 of 6H6 tube socket.
- 3. Sweep Generator output 100,000 to 200,000 microvolts.
- 4. Scope Adjustment remains. Reduce Sweep input.
- 5. Connect Output Meter across voice coil. Feed an R. F. signal, calibrated at 10.7 mc. and modulated 30% at 400 cycles, to the receiver as indicated.

Cross index between channel calibrations on the dial and frequency in megacycles follow:

Channel No.	Frequency in Megacycles	Channel No.	Frequency in Megacycles
200	87.9	255	98.9
205	88.9	260	99.9
210	89.9	265	100.9
215	90.9	270	101.9
220	91.9	275	102.9
225	92.9	280	103:9
230	93.9	285	104.9
235	94.9	290	105.9
240	95.9	295	106.9
245	96.9	300	107.9
250	97.9		_

T

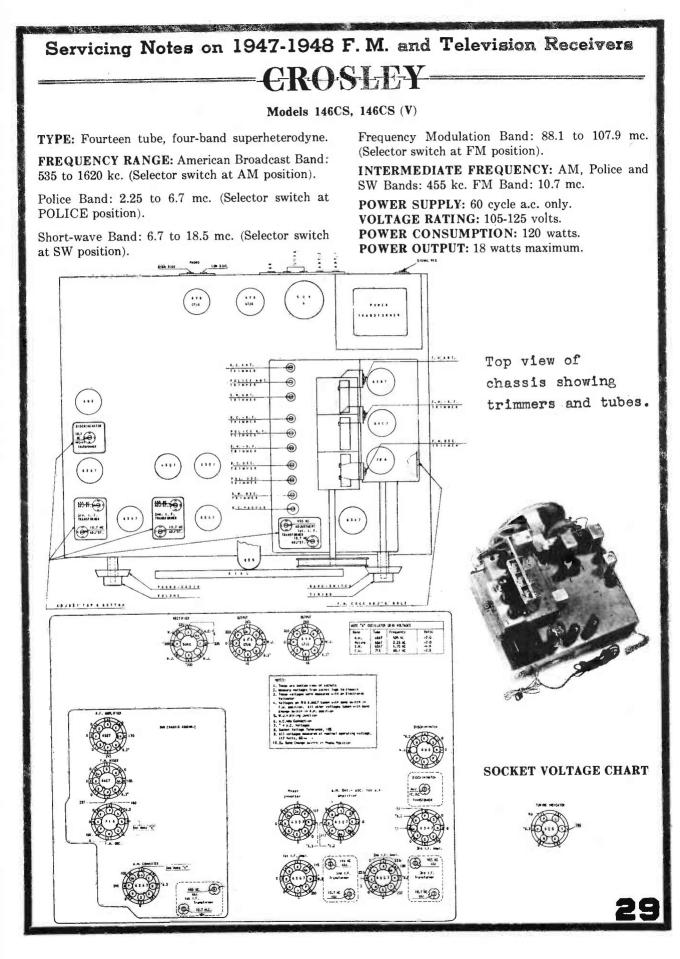
26

PARTS LIST-MODEL 87CQ AND REVISED MODELS 86CR, 86CS

Figures in first column correspond to figures in Schematic Diagram

Item No.	Part No.	Description	Item No.	Part No.	Description
1 2	AC-136171 AC-136264	Transformer Assy. (F. M. Antenna) Transformer, 10.7 mc. and 5.825 mc.	81 83 85	Part of Item #4 B-226638-49 C 197210 2	Condenser, 33 mmf., 500 v., ceramic Condenser, 10 mmf., 300 v., ceramic Condenser, Tommer, (B. C. Asti
3	AC-136081	1. F. (A) Transformer, 10.7 mc. and 5.825 mc.	86	C-137219-3 B-226638-27	Condenser, Trimmer (B. C. Ant. Wave Trap)
4 5 6 8 9	AC-136276 AC-136260 AC-136509 AC-136261 AW-136511	I. F. (B) Transformer, 10.7 mc. and 167.5 kc. I. F. Transformer, 10.7 mc. Discriminator Coil Assy., 1st Oscillator (B. C. & S. W.) Transformer, 167.5 kc., Diode Coil, Antenna (B. C.)	87 88 89 90 91	B-226638-51 B-226638-52 GC-210685-183 B-226638-35 Part of Item #3	Condenser, 82 mmf., 500 v., ceramic Condenser, 39 mmf., 300 v., ceramic Condenser, 91 mmf., 300 v., ceramic Condenser, 50 mmf., 500 v., mica Condenser, 27 mmf., 500 v., ceramic Condenser, 27 mmf., 500 v., ceramic
10 24 25	AB-136444 W-136179 39001-17	Coil Assy., Antenna (S. W.) Coil, F. M. Oscillator Condenser, .05 mfd., 600 v., paper	92 93 94	Part of Item #1 39373-87 39373-87	Resistor, 1000 ohm, ½ w. Resistor, 470,000 ohm, ½ w. Resistor, 470,000 ohm, ½ w.
26A 26B 26C	B-137028	Condenser, 20 mfd., 400 v.) Four Condenser, 30 mfd., 350 v. Section Condenser, 20 mfd., 300 v. (Elect.	95 96 97 98	39373-69 39373-94 39373-67 39373-75	Resistor, 56,000 ohm, ½ w. Resistor, 1.5 megohm, ½ w. Resistor, 47,000 ohm, ½ w. Resistor, 120,000 ohm, ½ w.
26D 27 28A 28B	B-135336 C-135946	Condenser, 20 mfd., 25 v.) Filter Transformer, Power Condenser, Variable\Two Condenser, Variable/Section	99 100 101	39373-75 39373-129 39373-74	Resistor, 120,000 ohm, ½ w. Resistor, 220 ohm, 1 w. Resistor, 100,000 ohm, ½ w.
29 30	C-136161 B-135783	Switch, Band Change Control, Volume (3 megohm, Tap 720,000 ohm)	102 103 104 105	39373-74 39373-74 39373-80 39373-40	Resistor, 100,000 ohm, ½ w. Resistor, 100,000 ohm, ½ w. Resistor, 220,000 ohm, ½ w. Resistor, 2,200 ohm, ½ w.
*{ 31A 31B	39368-22 39370-2 B-135784	Control (Volume) Shaft (Knurled Plug-in) Control, Tone) Switch, Power	106 107 108	39373-40 39373-40 39373-90	Resistor, 2,200 ohm, ½ w. Resistor, 2,200 ohm, ½ w. Resistor, 680,000 ohm, ½ w.
32A 32B 33	W-48858 W-48858 C-132300-2	Bulb (Dial), Type 47, 6.3 v., .15 amp. Bulb (Dial), Type 47, 6.3 v., .15 amp. Cable and Plug Assy., Power	109 110 111	39373-71 Part of Item #8 39373-92	Resistor, 68,000 ohm, ½ w. Resistor, 68,000 ohm, ½ w. Resistor, 1 megohm, ½ w.
34 35 36	39001-7 39001-13 39001-11	Condenser, .001 mfd., 600 v., paper Condenser, .01 mfd., 600 v., paper Condenser, .005 mfd., 600 v., paper Condenser, .005 mfd., 600 v., paper	112 113 114 115	39373-92 Part of Item #1 39001-17 39373-67	Resistor, 1 megohm, ½ w. Resistor, 1 megohm, ½ w. Condenser, .05 mfd., 600 v., paper Resistor, 47,000 ohm. ½ w.
37 38 39 40	39001-11 39001-11 39001-11 39001-11	Condenser, .005 mfd., 600 v., paper Condenser, .005 mfd., 600 v., paper Condenser, .005 mfd., 600 v., paper	116 118 119	39373-62 39373-60 B-226638-59	Resistor, 27,000 ohm, ½ w. Resistor, 22,000 ohm, ½ w. Condenser, 15 mmf., 500 v., ceramic
41 42 43	39001-11 39001-11 39001-11	Condenser, .005 mfd., 600 v., paper Condenser, .005 mfd., 600 v., paper Condenser, .005 mfd., 600 v., paper	120A 120B	W-137021	Resistor (Wire-wound), 400 ohm, 4 w. Resistor (Wire-wound), Section 700 ohm, 4 w.
44 45 46 47	39001-11 39001-11 39001-13 39001-13	Condenser, .005 mfd., 600 v., paper Condenser, .005 mfd., 600 v., paper Condenser, .01 mfd., 600 v., paper Condenser, .01 mfd., 600 v., paper	121 122	39373-107 C-135974	Resistor, 10 megohm, ½ w. Speaker & Transformer Assy. (86CR, 86CS)
48 49 50	39001-17 39001-17 39001-76	Condenser, .05 mfd., 600 v., paper Condenser, .05 mfd., 600 v., paper Condenser, .003 mfd., 600 v., paper	123 124 125 126	AW-136911 39019-3 W-137143 W-137143	Condenser, 1.3 mmf. (Transmission Line) Terminal Board Transmission Line (75 ohm)
51 52 53 55	C-137219-1 Part of Item #2 Part of Item #3 W-136964	Condenser, Trimmer (S. W. Ant. Prim.) Condenser, Trimmer (5.825 mc. Prim.) Condenser, Trimmer (5.825 mc. Sec.) Condenser, Air Trimmer (S. W. Osc.)	128 129 130	39001-17 39001-7 B-226638-49	Loop Antenna (Transmission Line) Condenser, .05 mfd., 600 v., paper Condenser, .001 mfd., 600 v., paper Condenser, .10 mmf., 300 v., ceramic
56	W-136964	Series Padder) Condenser, Air Trimmer (B. C. Osc. Series Padder)	131 132 133	39012-59 39012-60 W-136998	Iron Core (F. M. Osc.) Iron Core (B. C. Ant.) Connector, Phono Pickup
57	W-136964	Condenser, Air Trimmer (F. M. Radia- tion Balance)	135	W-137213 B-138131-2	Cable & Plug Assy., Phono Motor Transformer, Output
58 59 60 61	Part of Item #1 Part of Item #10 Part of Item #1 Part of Item #2	Condenser, Trimmer (F. M. Ant. Sec.) Condenser, Trimmer (S. W. Ant. Sec.) Condenser, Trimmer (F. M. Ant. Prim.) Condenser, 82 mmf., 300 v., ceramic	137 138 139 140	39001-11 39373-170 39373-60 W-138531	Condenser, .005 mfd., 600 v., paper Resistor, 22,000 ohm, 1 w. Resistor, 22,000 ohm, 1½ w. Condenser, 53 mmf., 500 v., ceramic
62 63 64	Part of Item #3 Part of Item #4 Part of Item #4	Condenser, 68 mmf., 300 v., ceramic Condenser, 470 mmf., 300 v., silver mica Condenser, 470 mmf., 300 v., silver mica	141 142 143 144	B-138774 W-137398-6 39373-92 Part of Item #1	Crystal, 5992.5 kc. Condenser, 4.7 mmf., 500v. Resistor, 1 megohm, ½ w. Condenser, 30 mmf., 500 v., mica
65 66 67 68	Part of Item #8 Part of Item #2 Part of Item #3 Part of Item #5	Condenser, 470 mmf., 300 v., silver mica Condenser, 150 mmf., 500 v., silver mica Condenser, 150 mmf., 500 v., silver mica Condenser, 150 mmf., 500 v., silver mica	145 146	C-138777 AB-138935 C-137173 C-137236	Speaker & Transformer Assy. (87CQ) Cable & Plug Assy., Speaker (87CQ) Album, 12" Record (86 CR) Album, 10" Record (86 CR)
69 70 71 75	Part of Item #5 Part of Item #5 B-226638-39 Part of Item #8	Condenser, 150 mmf., 500 v., silver mica Condenser, 62 mmf., 500 v., ceramic Condenser, 120 mmf., 300 v., ceramic Condenser, 1000 mmf., 500 v., silver mica		AC-136204 AC-139380 C-136222	Background, Dial (86CR, 86CS) Background, Dial (87CQ) Bracket, Variable condenser Mtg.
76 77 79	GC-210685-182 Part of Item #8 Part of Item #5 Part of Item #4	Condenser, 100 mmf., 500 v., mica Condenser, 100 mmf., 500 v., mica Condenser, 12 mmf., 300 v., ceramic		R-137010 R-138491 R-138569 W-136201	Cabinet (86CR) Cabinet (86CS) Cabinet (87CQ) Clip, Dial Glass
00	Tart of Item #4	1 Convenser, oo minin, ooo v., ceranne		W-131154-1	Cotter, External

There are also other parts.

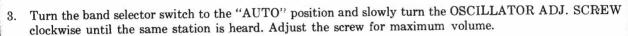


PUSH BUTTON ADJUSTMENT PROCEDURE

Each of the six push buttons, for automatic tuning, has two adjusting screws by which it may be set to any nearby American broadcast station whose frequency in kilocycles is within the kilocycle range covered by that button. To gain access to these screws, carefully pull off the

push button. To set No. 1 push button to a desired position, proceed as follows:

- Turn the ANTENNA ADJ. SCREW clockwise until moderately tight, then turn the OSCILLATOR ADJ. SCREW counterclockwise until the threaded portion extends approximately 3/4 inch. Use a small screw-driver and do not exert pressure.
- Turn the band selector switch to the "AM" position and manually 2. tune in the station to which the push button is to be set. The frequency of the station selected must be between 540 and 900 kilocycles. Carefully adjust the tuning control to the point of clearest reception.



- Adjust the ANTENNA ADJ. SCREW for maximum volume. 4.
- Turn the band selector switch from "AUTO" to "AM" and back again to check if the adjustment has 5. been correctly made. There should be no change in tone quality when switched from one to the other.
- Place the tab with the call letters of the station, to which the push button has been set, in a celluloid "V" 6. and slide it into the button from the side.
- The remaining push buttons may be set in a similar manner. No adjustment of master tone control push 7. buttons is required.

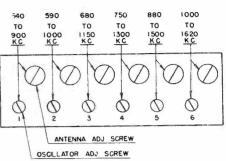
ALIGNMENT PROCEDURE NOTES

- 1. Sweep alignment (use approximately 500 kc. to sweep),
- 2. Sweep Generator Output .1 to 1 Volt RMS.
- 3. Scope connected to center terminal on phono switch.

4. Align for maximum peak amplitude. Peak separation should be 150 to 200 kc.

- 5. Scope connected to center terminal of 3rd I.F. through 200,000 ohms.
- 6. Repeat operations 8 and 9 until no change can be noted in sensitivity.
- 7. Rock gang.
- 8. Repeat operations 12, 13 and 14 for maximum sensitivity.
- 9.* C=Channel number.
- When aligning the shortwave oscillator trimmer, make certain the circuit is aligned at the correct frequency and not at the image 10. frequency which is 910 kilocycles lower in frequency as indicated on the receiver dial. To check, tune in signal generator frequency, then increase the generator output and tune in the image frequency which should be audible, but weaker than the fundamental frequency. If the image can not be tuned in, the oscillator trimmer is adjusted to the wrong peak. The correct peak is the second peak of the trimmer from the closed position.

The F.M. channel numbers run from 200 to 300, and correspond to frequencies from 87.9 to 107.9 megacycles. To find the frequency in megacycles for any channel number, multiply the channel number by 2/10, and add 47.9. For example, channel number 280 when multiplied by 2/10 equals 56.0 and plus 47.9 gives 103.9 megacycles as the frequency.



CIRCUIT

To Receiver

Ant. Terminals

and 2

50m mf.

37.5 Ohm

Carbon

Resistors

-MM

37.5 Ohm

FIG |

0

FIG. 2

16.6 00

uh.

Generator

TO SIGNAL WEB

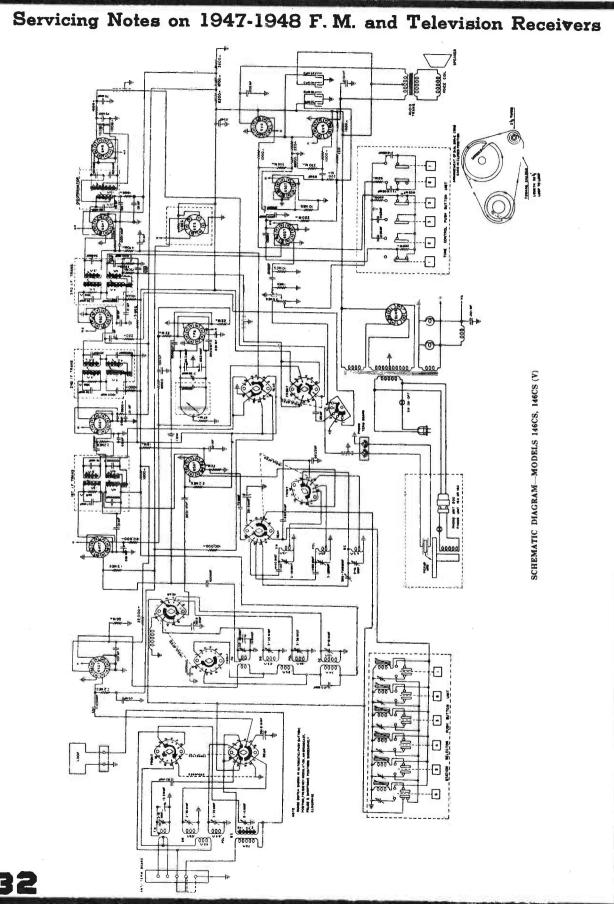
TERMINALS ON

CHASSIS

Servicing Notes on 1947-1948 F. M. and Television Receivers ALIGNMENT PROCEDURE CHART

Align-	Sig	mal Generator O	lutput	Po	sition of	Adjust for	Remarks
ment Sequence	Frequency	In Series with	To	Band Switch	Tuning Dial	Maximum Output	
1	455 kc.	.1 mfd.	2nd I.F. Grid	AM	Hi. Freq. stop	3rd I.F.	
2	455 kc.	.1 mfd.	1st I.F. Grid	AM	Hi. Freq. stop	2nd I.F.	
3	455 kc.	.1 mfd.	19 plate section of center gang	AM	Hi. Freq. stop	1st I.F.	Retouch 3rd, 2nd, 1st.
.4	10.7 mc.	.1 mfd.	3rd I.F. Grid	FM	Hi. Freq. stop	Discriminator	Notes 1, 2, 3, 4
5	10.7 mc.	.1 mfd.	2nd I.F. Grid	FM	Hi. Freq. stop	3rd I.F.	Notes 1 and 5
6	10.7 mc.	"1 mfd.	1st I.F. Grid	FM	Hi. Freq. stop	2nd I.F.	Retouch 3rd I.F.
7	7 10.7 mc1 mfd.		3 plate section of center gang	FM	Hi. Freq. stop	1st I.F.	Retouch 3rd, 2nd, 1st
8	1400 kc.	200 mmf.	Ant. 1	AM	1400 kc.	BCOscRF. & Ant. Trim	
ġ	600 kc.	200 mmf.	Ant. 1	ÅМ	600 kc.	Broadcast Osc. Padder	Notes 6 and 7
10	6.0 mc.	400 ohm	Ant. 1	Police	6.0 mc.	Police Osc., R.F. & Ant. Trimmers	
11	18 mc.	400 ohm	Ant. 1	SW	18 mc.	Sw. Osc., R.F., & Ant. Trimmers	Note 10
12	108.1 mc.	See Circuit Diag. Fig. 1	Ant. 1 & 2	FM	Hi. Freq. stop	FM-Osc. Trimmer	
13	87.9 mc.	See Circuit Diag. Fig. 1	Ant. 1 & 2	FM	Low Freq. stop	FM-Osc. Core	
14	105.9 mc.	See Circuit Diag.	Ant. 1 & 2	FM	*C-290	FM. R.F. & Ant. Trimmer	Notes 7,8 and 9*

To align, turn the tuning condenser to full mesh, against stop, and set dial pointer to the reference line at the end of the dial scale. Release all tone control buttons to the "out" position. Connect the output meter across the speaker voice coil (3.2 ohms). Feed an R.F. signal modulated 30% at 400 cycles to the receiver as indicated in the chart above. Connect signal generator ground terminal to the chassis of the receiver. When F.M. generator is used, a 30% modulated signal is equal to a deviation of 22.5 KC. Advance volume control to maximum clockwise position, adjust generator output to produce noticeable output meter reading. Keep generator output low to prevent excessive AVC action. The low impedance "Signal Web" antenna should remain connected at all times. If chassis is removed use dummy antenna Fig. 2, page 30. Link in "Ext. Ant."



Servicing Notes on 1947-1948 F. M. and Television Receivers DUNDOP Model RA-101 © 1947 Allen B. Du Mont Laboratories Passale, N. J.

The material presented on pages 33-46 has been supplied by Allen B. Du Mont Laboratories and is reproduced with the permission of this firm. While this information has direct reference to Du Mont Model RA-101 television receiver, it will prove helpful to television students and servicemen in servicing other sets since much of these data are of a general nature.

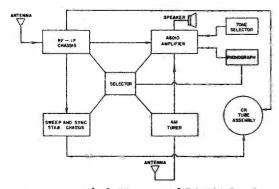


Figure 1. Block Diagram of RA-101 Receiver

DESCRIPTION OF SET.

The Model RA-101 is a complete home entertainment unit containing facilities for television, FM and AM reception. Included in the model is an automatic record changer.

All cabinet styles contain the following chassis and subassemblies:

1. Audio amplifier chassis (containing the audio amplifier and its power supply).

2. Sweep chassis (containing sweep circuits, a power supply for low voltage and bias voltage for the sweep and RF-IF chassis, and the high-voltage supply for the cathode-ray tube).

2a. Sync stabilizer chassis (containing automatic frequency control circuit).

3. The RF-IF chassis (containing both sound and video IF circuits, video amplifier, RF input system).

4. The AM tuner chassis (containing the tuning unit for AM reception).

5. The tuning meter assembly. (The Tele-FM tuning meter plus the cable connecting it to the RF-IF chassis.)

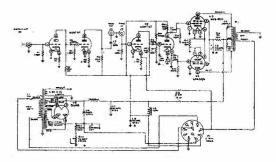
6. The tone selector assembly (consisting essentially of a push button switch and the tone control attenuators).

7. The service selector switch assembly (consisting of a push button switch system).

8. Record changer assembly (containing the complete assembly of motor, turntable, pick-up arm and changing mechanism).

9. Cathode-ray tube assembly (consisting of the cathode-ray tube socket, cabling, focusing coil and deflection yoke).

A block diagram of the set showing the relationship of the various circuits is given in Figure 1.



Audio Amplifier Schematic

AUDIO AMPLIFIER CHASSIS.

The audio amplifier assembly contains its own power supply furnishing sufficient output to operate the entire audio system and sound IF of the RF tuner. The amplifier section itself contains four tubes, namely: two tubes, Type 6SN7, V1 and V2, and two tubes, Type 6V6, V3 and V4. The audio amplifier is resistance coupled. V1 is a dual triode with both sections connected as voltage amplifiers in cascade. The sound volume control is in the input circuit of the first stage. The tone control is connected in the plate circuit of the second half of V1. The first half of V2 is another voltage ampli-

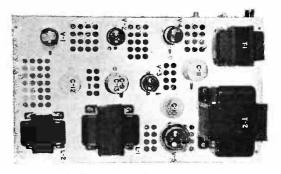


Figure 2. Audio Amplifier Chassis

fier which in turn feeds the second half of V2. The second half of V2 is the phase inverter containing balanced plate and cathode-loads from which the signal is derived to drive the two 6V6's, V3 and V4 in push-pull. The power supply on this chassis also furnishes B+ to the AM Tuner, the RF and Sound IF sections of the RF-IF chassis, and focusing current to the cathode-ray tube focusing coil. The Focus control is also on this chassis.

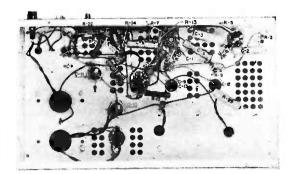


Figure 3. Audio Amplifier Chassis

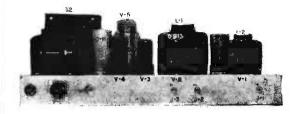


Figure 4. Audio Amplifier Chassis

SWEEP CHASSIS.

The sweep chassis contains the power supply which furnishes both B+ and bias voltages to the sweep chassis and also to the video IF amplifier and the video amplifier on the RF-IF chassis. A negative voltage is also derived from this same power supply to furnish a negative bias voltage for both the sweep and RF-IF chassis. This low voltage power supply



Figure 5. Sweep Chassis

contains two 5U4G rectifiers, V9 and V10, each of which is operated as a half wave rectifier to result in full wave rectification. A time delay relay in this power supply prevents B+ from being available for about 30 seconds.

The sweep chassis also contains the high voltage power supply. This power supply uses two Type 2X2 rectifiers, V11 and V12, which are connected to operate as a voltage doubler circuit. This voltage doubler furnishes high positive voltage to the anode of the cathode-ray tube. The sweep circuits on this chassis generate both the vertical and horizontal sweep voltages for the deflection yoke of the cathode-ray tube. A toggle switch on the chassis is available to shut off the high voltage at the convenience of the serviceman.

The sweep circuits are used to generate deflection voltages which when applied to the cathode-ray tube will cause the electron beam to scan across the face of the tube. The sweeps

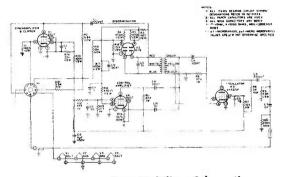
34

must be synchronized to those at the transmitter, and for that purpose, synchronizing pulses transmitted with the video signal are used.

The sync pulses are obtained from the video channel on the RF-IF chassis and fed to V2, the sync amplifier. The output from V2 drives the circuits in the sync stabilizer chassis.

SYNC STABILIZER CHASSIS

Four stages comprise the sync stabilizer chassis. The signal from the sync amplifier is clipped by V1, the clipper stage on the sync stabilizer. The three other stages on the sync stabilizer chassis comprise the "automatic frequency control" circuit The object of the "AFC" circuit is to obtain pulses for synchronization that are stable in frequency and phase and not affected by extraneous disturbances. The principle used is to originate the pulses by a local oscillator, whose frequency

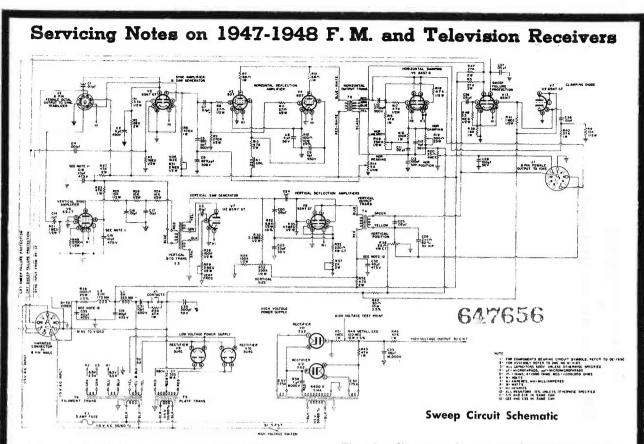


Sync Stabilizer Schematic

and phase are controlled by the incoming sync pulses. The oscillator output will then be used to pulse the sweep circuits.

The oscillator used is an electron coupled oscillator using a 6K6 tube. The oscillator is coupled to the phase discriminator by transformer coupling (T1). The sync pulses are fed to the center tap of the discriminator transformer from the clipper stage. With respect to the center tap, the sinusoidal oscillator output on the discriminator plates are 180 degrees out of phase. The pulse, being center fed, adds to both plates with the same polarity. When the oscillator frequency is in adjustment, the pulse rides the sine wave at the 180 degree point in its cycle. See Figure 7. During one-half the cycle, one section of the dual diode will conduct, and during the second half of the cycle, the other section of the diode will conduct. The output voltage across the diode load will be the same in magnitude throughout the cycle, since the magnitude of the voltage on each plate is equal during each diode's conduction period. If the oscillator frequency changes, the pulse will no longer ride the mid-point of the wave. See Figure 7. Now the pulse voltage adds to the sine wave voltage on one plate while it subtracts from the voltage on the other plate. Thus during the cycle, the magnitude of the output voltage will change. A bias of -1.5 volts is applied to the cathode circuit of the diode. Since this voltage supply has no d-c return path to ground in the diode cathode circuit, no current will flow and the 1.5 volts will be applied equally to both cathodes. The output voltage of the diode stage will add or subtract from the -1.5 volts. The -1.5 volts are used to bias the "reactance tube" V4 through the diode lead.

There is, therefore, a d-c voltage that is constant for proper oscillator frequency, but changes when the oscillator frequency is not correct. The voltage is fed to the grid of the "reactance tube" (V4). Output from the oscillator is fed to the cathode of the reactance tube through C10, a .01 μ f capacitor. This



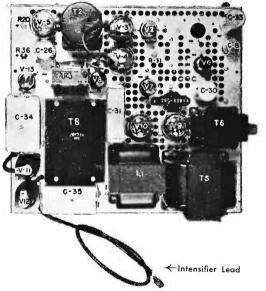


Figure 6. Sweep Chassis

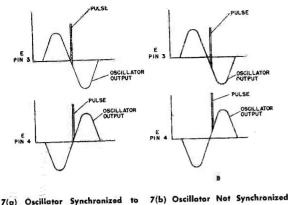
capacitor causes a phase shift of the signal. Depending upon the voltage on the grid of the reactance tube, the output impedance of the reactance tube will be of a certain inductive value. Changes in the oscillator frequency or phase with respect to the pulse frequency will cause different values of voltage on the reactance tube grid and therefore vary the inductive output impedance of the tube.

By coupling the reactance tube across the oscillator coil, the oscillator frequency will vary in such a manner as to correct its deviation from the proper value. The oscillator is thus synchronized to the pulse frequency. There is a filter circuit between the discriminator and the reactance tube (C12, R17 and C11). Any irratic pulses or disturbances are by-passed to ground by the filter, and therefore will not affect the operation of the sweeps. The oscillator output is a distorted sine wave which, when differentiated, will give a pulse output. The differentiating circuit used is C6, C7, R9 and R10.

The signal from the plate of the electron coupled oscillator is then fed to the second half of V2, a Type 6SN7, which is connected as a driven sweep generator (sometimes called a sawtooth wave generator). The signal from the sweep generator is then fed to the grids of the horizontal deflection amplifiers, two tubes Type 807. These tubes are V3 and V4, which operate in parallel to drive the horizontal output transformer T2. Because of the relatively high frequency components present in the horizontal sweep signal, it is necessary that the primary of this output transformer have relatively few turns compared to the vertical deflection amplifier in order to keep the distributed capacitance within the transformer to a minimum. Also, much more power must be delivered to the horizontal deflection coils due to greater energy losses. Thus it is necessary to supply more current and power to the horizontal output transformer than to the vertical.

The horizontal damping tube, V5, is a 6AS7. This tube is a dual triode which is connected across the output of the horizontal output transformer. The function of the horizontal damping tube is to eliminate the oscillation which occurs from an overshoot on the sawtooth voltage. The horizontal sweep signal is fed to the deflection yoke. Horizontal positioning is obtained by means of a potentiometer which injects a portion of the bias voltage into the secondary of the horizontal output transformer.

The vertical sync amplifier, V6, is a 6SJ7. This tube amplifies the vertical sync signal and transmits it to one of the windings of the vertical blocking oscillator transformer. The



7(a) Öscillator Synchronized to 7(b) Oscillator Not Synchronized Pulse Frequency to Pulse Frequency Figure 7. AFC Diagram

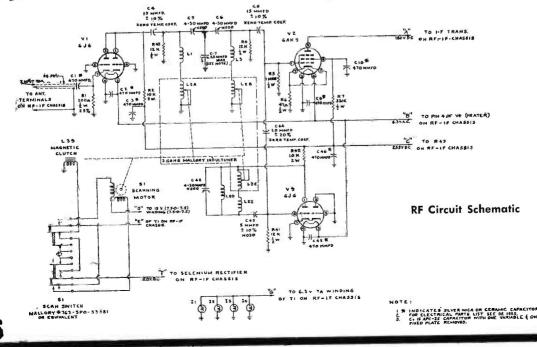
vertical blocking tube oscillator consists of one-half of V7, a Type 6SN7. This blocking tube oscillator triggers the sweep generator which is the second half of V7. The vertical sweep signal from the sweep generator is fed to the vertical deflection amplifier which consists of another 6SN7 with both halves operating in parallel. The vertical deflection amplifier drives the primary of T4, the vertical output transformer. Because the vertical sweep operates at a low frequency of 60 cycles (distributed capacitance has much less effect than at 15,750 cycles), it is possible to use more turns of wire in T4 and thus obtain the same number of ampere turns as used in the horizontal output transformer, and drive the primary of T4 with less current. Thus, a 6SN7, operated in parallel, will furnish sufficient current as a deflection amplifier to operate the vertical output transformer. Vertical positioning is obtained by means of a potentiometer, which injects a portion of the bias voltage into the secondary of the vertical output transformer.

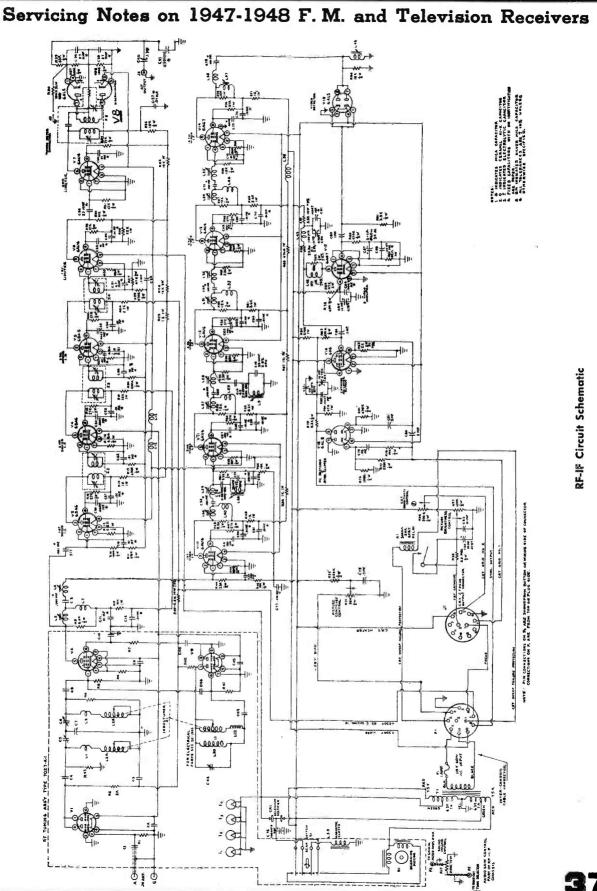
The beam control amplifier, V13, is also on the sweep chassis. This amplifier is a dual triode, Type 6SN7, which receives the signal from the vertical output transformer on one grid and a signal derived from the horizontal output on the other grid. One-half of this tube is normally conducting and the other half is normally cut off. If either of the sweeps fail, the half of the dual triode which is conducting becomes non-conducting. Since the solenoid of the relay is connected in series with the plate of the normally conducting half of the tube, the relay contacts are allowed to open. The opening of these relay contacts applies a positive voltage to the cathode of the cathode-ray tube, thus cutting off the beam of the cathode-ray tube, and preventing a stationary bright spot or line from appearing on the screen if the sweep should fail.

THE RF-IF CHASSIS.

The RF tuning assembly is the complete input system for the Du Mont Teleset. It consists of three separate variable inductors (the Du Mont Inputuner) which cover the range of 44 to 216 megacycles without band-switching. In the Du Mont input system are the tubes V1, V2, and V9. V1 and V9 are type 6J6 tubes and V2 is a Type 6AK5; V1 is an RF stage; V9 is the local oscillator, and V2 is the mixer.

The output of the RF section is the intermediate frequency of the Teleset. This intermediate frequency differs, however, from the normal AM receiver in that it is a band of frequencies which contains both video and sound signals. The video and sound IF signals can be separated because they occur at different frequencies due to the fact that they were transmitted on separate carriers, 4.5 megacycles apart. The sound IF is separated from the video signals by means of a sound trap and is impressed on the grid of the first sound IF stage. The sound IF amplifier is a three-stage amplifier consisting of V3, V4 and V5, which utilize Type 6BA6 tubes. After passing through the sound IF amplifiers, the sound IF signal passes through the two limiter stages, V6 and V7, which are connected in cascade. These tubes remove amplitude modulation from the FM signal. The output of the second limiter is coupled to the discriminator tube by means of the discriminator transformer. The discriminator, V8, is a 6AL5. This is a typical discriminator circuit for removing the modulation from the intermediate frequency and is so tuned that its output is zero volts, at exactly 21.9 megacyles. The voltage output of the discriminator is a varying DC voltage whose magnitude is dependent upon the deviation of fre-





quency of the sound IF signal from the center value of 21.9 megacycles. The FM teletuning meter is connected to one of the cathodes of the discriminator and registers zero when the FM or television station being received is properly tuned. The output of the discriminator is the audio signal which is fed to the audio amplifier, which in turn drives the speaker.

The tuned circuit in the plate of the mixer tube, V2, is tuned to have a band pass between 21.5 and 26.4 megacycles.

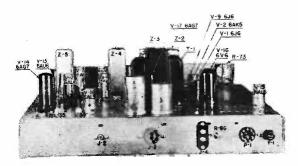


Figure 8. RF-IF Chassis

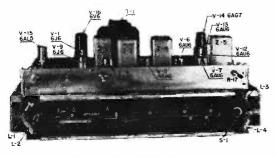


Figure 9. **RF-IF** Chassis

The sound IF frequency is picked off prior to the tuned circuit and the video IF frequency passes through to the grid of V10, the first video IF amplifier. Two sound traps are located, one between the first and second video IF stages and the other between the second and third video IF stages. These sound traps prevent the sound IF signals from passing through the video IF amplifier and causing interfering patterns in the picture. In all there are five video IF stages in the Model RA-101. These five stages consist of V10, V11, V12, V13, and V14. All of these stages employ the same tube type, a 6AU6, with the exception of V14, which uses a 6AG7. The video IF stages utilize special coupling circuits to provide a band pass of 4 megacycles. The output of the fifth viedo IF stage feeds V19, the video detector. V19 is a 6AL5 which is connected as a half wave diode detector. The output of the video detector feeds the first video amplifier, V17, a 6AG7. V17 in turn feeds V16, a 6V6, connected as a cathode follower output. The output of V16 is coupled directly to the control grid of the cathode-ray tube. However, V15, the DC restorer and sync clipper is connected across the output.

The DC restorer and sync clipper consists of a single tube, V15, a 6AL5. One-half of this tube operates as the DC restorer and the other half as the sync clipper. The signal is taken from the plate of the sync clipper and fed to the sweep chassis as composite sync.

There are a number of other components also located on this chassis. These items are enumerated below:

1. The Contrast Control, which effectively is the same control on the video signal as the volume control is on the audio signal, varies the output of the video IF amplifier by varying the negative bias voltage applied to the grids of the first two video IF amplifiers.

2. The Picture Brightness Control is located on this chassis. It is used to set the intensity level of the background of the picture.

3. Because the Picture Brightness Control is located on this chassis, it is also convenient to place the relays for the sweep failure protection circuit for the cathode-ray tube on this same chassis.

4. The Sound Volume Control is also located on this chassis to consolidate all controls on a single chassis, and is connected by cable to the audio chassis.

5. The motor for driving the pointer on the FM teletuning dial, the magnetic clutch, and the hand vernier tuning mechanism, all of which are used in conjunction with the inductuner, are also included on this chassis, thus consolidating all front panel controls on one chassis.

6. The Grid Drive Control-which adjusts the cathode-ray tube grid sensitivity.

2.4 THE AM TUNER CHASSIS.

AM tuner chassis, which is employed in the Model RA-101, consists essentially of four major sections. The RF amplifier is a tuned RF stage which feeds a 6SA7 converter. The 6SA7 serves the function of both oscillator and mixer to convert the RF signal to an intermediate frequency of 456 KC. This chassis contains one IF amplifier, a 6SK7, which in turn feeds a 6SN7. One-half of this tube acts as a diode detector and the other half as a cathode follower output. This chassis contains its own heater transformer but B+ is supplied to it from the audio chassis.

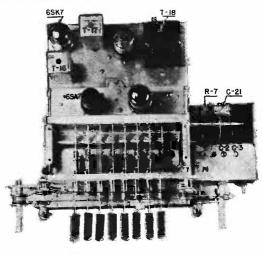


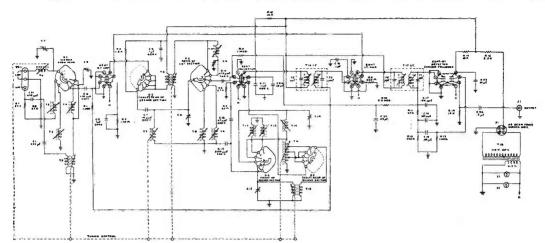
Figure 10. AM Tuner

THE TONE SELECTOR.

The Tone Selector is a separate assembly with five different RC circuits connected for varying the quality of the audio signal. This separate assembly is located directly behind the bezel for the teleset.

THE SERVICE SELECTOR.

The Service Selector is a push-button switch assembly which connects both AC and DC circuit voltages to the proper units



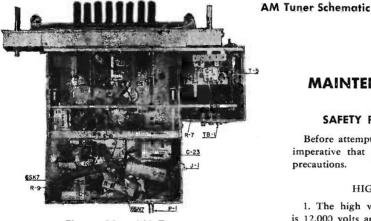
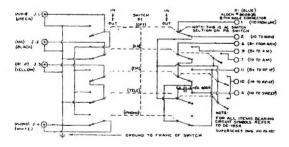
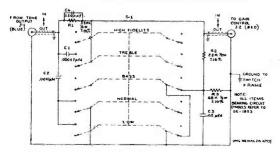


Figure 11. AM Tuner

depending upon the service selected, and switches the output of the three different chassis to the input of the audio amplifier.



Service Selector Schematic



Tone Selector Schematic

MAINTENANCE AND ADJUSTMENT

SAFETY PRECAUTIONS.

Before attempting any sort of servicing or adjustment it is imperative that the serviceman bear in mind certain safety precautions.

HIGH VOLTAGE PRECAUTIONS

1. The high voltage applied to the accelerating electrode is 12,000 volts and contact with it can cause severe burns or even DEATH.

2. Always turn OFF the high voltage switch on the sweep chassis before doing any work on this chassis.

3. Always turn OFF all power, and remove the power plug from wall receptacle before removing any chassis from the cabinet.

4. Always make adjustments with only one hand.

5. Always turn OFF all power before soldering or making connections.

CATHODE-RAY TUBE PRECAUTIONS

1. Do not bump the tube against hard objects.

2. Do not use tools near the tube.

3. Always wear safety goggles and gloves when handling the tube.

4. Always stand the tube on its face on a thick piece of felt in a protected place if it is removed from the cabinet.

5. Always replace a tube if it becomes scratched and return it to the factory for a pressure test.

4.2 ADJUSTMENT OF CONTROLS.

Normal operating procedure should be followed. See operating instruction manual. If satisfactory results are not acquired, then further adjustments should be made as outlined below. If required results are still not obtained, a diagnosis should be made to locate the trouble.



A. LOCATION OF CONTROLS

			Location on
Control	Chassis	Designation	Chassis
Sensitivity	RF-IF	R96 (Fig. 8)	Rear-Left
Focus	Audio	R22 (Fig. 3)	Rear-Left
Vert. Hold	Sweep	R29 (Fig. 5)	Rear-Left
Vert. Size	Sweep	R33 (Fig. 5)	Rear-Left
Vert. Linearity	Sweep	R37 (Fig. 5)	Rear-Center
Vert. Positioning	Sweep	R36 (Fig. 6)	Top Front
Hor. Peaking	Sweep	R14 (Fig. 5)	Rear-Center
Hor. Linearity	Sweep	R46 (Fig. 5)	Rear-Right
Hor. Size	Sweep	R31 (Fig. 6)	Top-Center
Hor. Positioning	Sweep	R20 (Fig. 6)	Top-Rear
Hor. Damping	Sweep	R19 (Fig. 5)	Top-Rear
Hor. Frequency	Sync. Stabilizer		Top of Phase Discriminator Transformer
Hor. Phase	Sync. Stabilizer		Bottom of Phase Discriminator Transformer

All other controls are on the control panel and are marked.

B. ADJUSTMENT OF CONTROLS

1. Sensitivity Control Adjustment (should not be touched except when cathode-ray tube is changed).

a. Press the "Tele" button on the service selector switch.

b. Increase brightness for raster appearance.

c. Decrease brightness until raster just fades out.

d. Check voltage on cathode of cathode-ray tube. If the voltage is less than 45 volts, this adjustment is correct. If the voltage is greater than 45 volts, turn sensitivity control full clockwise, increase brightness until 45 volts are obtained and then turn sensitivity control for disappearance of raster.

2. Turn up contrast control for image, and adjust the focus control for a clear picture.

3. If the picture is tilted, adjust the yoke on the neck of the cathode-ray tube. Loosen both top and bottom screws to turn yoke. Be certain that the set is turned off. Remember, contact with the high voltage may be lethal.

4. Increase brightness more than usual, and adjust vertical hold control if necessary.

5. When horizontal adjustment is necessary the following procedure should be followed:

a. Turn the screwdriver adjustment (horizontal frequency adjustment on phase discriminator transformer) until the test pattern or picture comes into sync.

b. Turn clockwise until the test pattern falls out of sync, then back off until it pulls in again. Note the position where "pull in" occurs.

c. Continue rotating counterclockwise until the test pattern falls out of sync again. Then turn clockwise until it pulls in. Note the position of the control for this second pull in point.

d. Set the adjustment half way between the two "pull in" points.

6. Adjust phase control for proper blanking and sync pulse, if necessary. Then readjust frequency as outlined above.

7. Set the vertical linearity, size and positioning controls for a good pattern.

8. Set the horizontal controls for good linearity, as well as for size and positioning.

EFFECTS OF CONTROLS ON LINEARITY

Control	Effect on Pattern					
Hor. linearity Hor. peaking	Flattens and expands pattern on right side. Flattens and expands both sides, but affects left side more.					
Hor. damping Vert. linearity	Flattens and expands left side of pattern. Flattens and expands top side of pattern.					

TROUBLESHOOTING PROCEDURE.

Although much information can be given for diagnosing trouble in the Telesets, the information is of a general nature. The nature, location and repair of troubles must be analyzed by the repairman. This necessitates a good working knowledge of the circuits of the sets, as well as an understanding of television principles. It behooves the repairman to study teleset circuits as well as outside information on television.

Before attempting to repair a set, a diagnosis should be made to determine in what channel or circuit there is trouble. Remember that in 99% of cases only one trouble develops at a time. It is only a waste of time and effort to indiscriminately test circuits of a set when trouble occurs. The method to follow is by use of logic and symptoms to localize the trouble before testing. When the troublesome circuit has been localized, a tube check should be made for faulty tubes. A few examples of proper reasoning are presented below.

Assume that the following trouble is evident: No picture can be obtained, but sound is operating. First of all, it can be assumed that the Inputuner is operating correctly. If it weren't, the sound channel would not be operating. Turn the brightness control clockwise. If a raster appears, the sweep circuits must be operative. The trouble has been localized to the video channel. The repairman can now test the video channel.

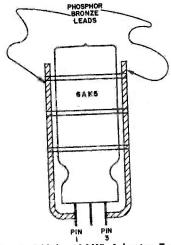


Figure 12(a). 6AK5 Adapter Tube

If when the brightness control is advanced, no raster appears, the difficulty can be in either the sweep circuits or the high voltage power supply. A failure of either sweep circuit will cause excessive bias on the cathode-ray tube and cut it off. Check the voltage on the cathode of the cathode-ray tube. If it is excessive, a failure of sweep is indicated. If it is normal, a failure of high voltage is indicated. Thus, the trouble has been localized to either the sweep or high voltage circuits.

Another condition is that there is picture, but no sound. Check the action of the tuning meter. If it is operating correctly, the trouble is in the audio amplifier. If it is not, the

trouble is in the sound IF channel. This assumption comes from the fact that the tuning meter operates from the sound discriminator. Again, it can be assumed that the Inputuner is operating correctly since the picture is being received.

If the receiver is completely dead (no picture, no sound), check the input power, input power cords and interlock (safety) switches. The antenna lead-in cable or the Inputuner may be bad. If these checks do not reveal the trouble, the low voltage power supply outputs should be checked. In case of Inputuner difficulties (aside from bad tubes), the entire unit should be removed and sent back to the factory.

If the sound channel is operating correctly, and the picture alone is distorted, an analysis can be made by merely viewing the screen of the cathode-ray tube. Such faults as too strong a signal, too weak a signal, outside interfering signals, excessive ripple, distortion and phase shift, can be viewed on the screen. Once recognized as specific faults, corrections can be made. The procedure to follow then is:

- 1. Analyze symptoms.
- 2. By reasoning, localize trouble to possible channels.
- 3. By tests, locate actual channel.
- 4. By further tests, find and correct trouble.

Normal signal tracing methods of testing is recommended for the audio amplifier and the sound channel. For the video channel, response curves can be checked by using a wobbulator and an oscillograph. For the sweep channel, waveforms can be viewed and checked against those given in section 4.5.

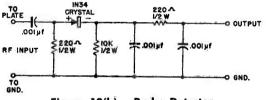


Figure 12(b). Probe Detector

REQUIRED TEST EQUIPMENT

- VACUUM TUBE VOLTMETER-20,000 ohms-per-volt voltmeter with ranges approximately 0 to 5 V, 0 to 10 V, 0 to 100 V, 0 to 500 V.
- CATHODE-RAY OSCILLOGRAPH—Du Mont Type 208-B recommended for RF-IF alignment, and audio amplifier servicing. Du Mont Type 224-A or Type 241 for troubleshooting sweep chassis.

SIGNAL GENERATORS-

- (1) FM Signal Generator—This is a wobbulator-type signal generator whose center frequency ranges from 20 to 30 megacycles with a sweep width of ±5 megacycles (adjustable). The voltage output of this generator should be 0.1 volts.
- (2) RF Signal Generator—With amplitude modulation available. RF range from 20 megacycles to a minimum of 60 megacycles. The RF signal must be adjustable to within 10 kc with a calibrated attenuator on the output.
- (3) Audio Signal Generator (for Checking Audio Amplifiers).
- TRAVELING DETECTOR-This is a crystal detector mounted in a probe assembly to enable IF stages to be aligned stage-by-stage. (See Figure 12b.)
- 6AK5 ADAPTER TUBE—See Figure 12a.

OPTIONAL TEST EQUIPMENT

- VIDEO SWEEP GENERATOR—Output varies from 0 to 6 megacycles.
- VOLTAGE CALIBRATOR—Du Mont Type 264-A recommended for use in measuring peak-to-peak voltages.
- SQUARE WAVE GENERATOR—For servicing audio and video amplifiers.

SWEEP WAVEFORMS.

Sweep waveforms are given in Figure 16. Waveforms were taken with the following control settings:

Line Voltage	-115 volts a-c
Horizontal Damping	Control-Full counterclockwise
Horizontal Linearity	Full clockwise
Horizontal Peaking	-Full clockwise
Vertical Linearity	-Full counterclockwise
Vertical Size	Full clockwise
Horizontal Size	-Full counterclockwise
Vertical Hold	Set to lock picture
Positioning Controls	-Normal setting

INSTALLATION

Installations, at the present state of the television art, are of the utmost importance. Customer satisfaction will depend entirely upon a well made installation. The best teleset manufactured is not capable of improving upon the signal presented to it by its antenna. The consumer is not technically educated enough to appreciate the difficulties involved in obtaining a clean picture in our urban areas. He will judge the television industry by the picture presented to him in his home. No amount of explanations or apologies will offset the unfavorable impression created by a noisy, blurry, jumpy picture.

Remember also, that a teleset purchaser will remain a teleset owner, only as long as he is able to enjoy the entertainment provided by the art. A rejected and returned teleset will not improve a dealer's net profit. It, therefore, is important for the service or installation man to bend every effort to make a good installation when a teleset is sold, not only for his own immediate profit, but also for the good of the art as a whole. The mortality will be high among servicemen attempting to profit from television installations. The field is complex and demanding of perfection. Only those who have firmly grasped and assimilated the necessary techniques and principles, will survive the competitive era now approaching. The following installation data is not complete. To be of value to a practicing serviceman it should be amplified by study and experimentation on his part.

Select a temporary position for the antenna, bearing in mind the requirements for a clean signal. Connect the antenna to the receiver and examine the resulting picture.

If the picture is satisfactory on all stations available, orient the antenna for maximum signal strength, and note the location so determined. A permanent installation may then be made.

Should the location prove to be poor, one or more picture defects will be evident. Various remedies should be applied until a clean picture results. A permanent installation can then be made. The advantages of the survey method should be self-evident. Trying out different antennas and antenna positions in permanent form is not only difficult but almost impossible.

The detailed alignment instructions presented below, and the resulting patterns illustrated on the next two pages, will not only assist you in carrying out necessary alignment of the Du Mont Model RA-101 television receiver, but will also serve as instructions for clearly understanding the effect of various adjustments on the response. In general, the same information can be applied to any modern television set. Please bear in mind that these patterns were obtained on a separate oscilloscope connected as instructed. To obtain the values of voltage A and B, a source of measureable and controlled voltage is applied with the controls of the test oscilloscope unchanged for the particular test, see page 45. For instructions of the connections see diagram on page 37.

DATA FOR ALIGNMENT

SO	UND	CHAN	INEL

To Adjust	Type of Input Signal Required	Connect Generator Leads Across	Connect Output Leads Across	Feed Output Leads Directly Into Oscillograph or Into Oscillograph Via Probe Detector	Adjust Coils to Conform to Fig, No.	Remarks
Z2	Wobbulator, RF Signal Generator	Pin 1, V3 and Chassis	Pin 5, V4 and Chassis	Probe Detector	15-E	RF Signal Generator Set at 21.9 mc to give birdie
Z3	Wobbulator, RF Signal Generator	Pin 1, V4 and Chassis	Pin 5, V5 and Chassis	Probe Detector	15-E	RF Signal Generator Set at 21.9 mc to give birdie
Z4	Wobbulator, RF Signal Generator	Pin 1, V5 and Chassis	R27	Direct	15-F	Connect 100 k resistor in series with oscillograph
Z2, Z3, Z4	Wobbulator, RF Signal Generator	Pin 1, V3 and Chassis	R27	Direct	15-G	
Z5	Wobbulator, RF Signal Generator	Pin 1, V7 and Chassis	Pin 1, V8 and Chassis	Direct	15-L	Readjust Z4 and Z3 to obtain good response curve

VIDEO CHANNEL

	and the second se		where the party of the second s			
L37, L44	Wobbulator, RF Signal Generator	Pin 4, V14 and Chassis	Pin 8, V16 and Chassis	Direct	1 5-O	RF Signal Generator set at 26.4 mc
L34, L35	Wobbulator, RF Signal Generator	Pin 1, V13 and Chassis	Pin 8, V14 and Chassis	Probe Detector	15-S	
L31	Wobbulator, RF Signal Generator	Pin 1, V12 and Chassis	Pin 5, V13 and Chassis	Probe Detector	15-T	
19	Wobbulator, Signal Generator	Pin 1, V12 and Chassis	Pin 5, V13 and Chassis	Probe Detector	15- V	RF Signal Generator at 21.9 mc (Sound Trap Adjustment)
L27, L28	Wobbulator, RF Signal Generator	Pin 1, V11 and Chassis	Pin 5, V12 and Chassis	Probe Detector	15-X	
L26	Wobbulator	Pin 1, V11 and Chassis	Pin 5, V12 and Chassis	Probe Detector	15-Ż	Second sound trap adjustment. Remove RF Generator
L24, L25	Wobbulator, RF Signal Generator	Pin 1, V10 and Chassis	Pin 5, V11 and Chassis	Probe Detector	15-BB	2
L5, L6	Wobbulator, RF Signal Generator	Pin 1, 6AK5 Adapter (V2) and Chassis	Pin 5, V10 and Chassis	Probe Detector	15-CC	Remove V2 and replace with 6AK5 adapter tube. See Fig- ure 12(a)
42	Wobbulator Signal Generator	Pin 1, 6AK5 Adapter (V2) and Chassis	Pin 8, V16 and Chassis	Probe Detector	15-DD	Signal generator set at 26.4 mc.



Figure 15-A Oscillogram of the dual sound IF curve (untuned),



Figure 15-D Oscillogram showing the effect of too much birdie.



Figure 15-G Oscillogram of overall sound IF response. (The improper alignment is due to the different amplitude of the signal now being applied to the grids of each stage.) (Birdie at 21.9 mc.)

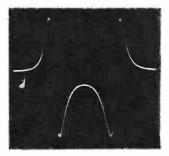


Figure 15-J Double discriminator curve.

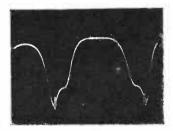


Figure 15-M Video IF response curve: Wobbulated signal generator at the grid of V14. Oscillograph at the cathode of V16. Birdie at 26.4 mc.



Figure 158 Oscillogram of the single sound IF curve (untuned). This is the response curve appearing on the right of Figure 15-A after it has been expanded.

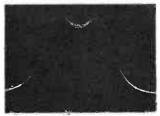


Figure 15-E Properly tuned sound IF curve with birdie at 21.9 mc.



Figure 15-H Oscillograph showing a slight amount of overload caused by too much signal from the wobbulated signal generator.



Figure 15-K Single discriminator curve (expanded from double curve). Birdie at 21.9 mc.

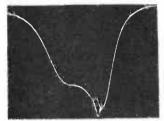


Figure 15-N Same as Figure 15-M except that the sweep of the oscillograph has been expanded to obtain a single curve.



Figure 15C Oscillogram of Figure 15-B with birdie at 21.9 mc.



Figure 15-F Sound IF curve obtained at the grid of the first limiter (properly adjusted), Birdie at 21.9 mc.



Figure 15-1 Oscillogram showing excessive overload caused by too much signal from the wobbulated signal generator.



Figure 15-L Properly aligned discriminator curve. Birdie at 21.9 mc.



Figure 15-0 Same as Figure 15-N with L37 and L44 properly tuned (birdie at 26.4 mc.).



Figure 15. Alignment Waveforms

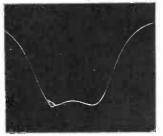


Figure 15-P Same as Figure 15-O except that the birdie is at 22.4 mc.

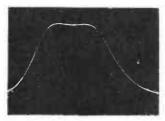


Figure 15-5 Video IF response curve: Wobbulator to the grid of V13 and the traveling detector to the oscillograph at the plate of V14. L34 and L35 properly tuned (birdie at 26.4 mc.).

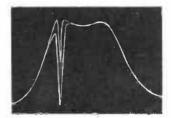
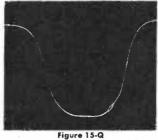


Figure 15-V Sound trap properly set. Birdie at 21.9 mc.



Video response curve showing excessive overloading due to too much signal applied to the stage from the wobbulated signal generator.

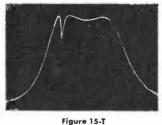


Figure 15-1 Video IF response curve: Wobbulator to the grid of V12 and the traveling detectar to the oscillograph at the plate af V13. L31 and L32 properly tuned (birdie at 26.4 mc.).



Figure 15-W Sound trap slightly too high.

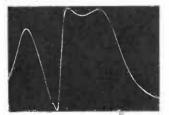


Figure 15-Y Sound trap too low .



Figure 15-BB Video IF response curve: Wobbulator to the grid of V10 and the traveling detector to the oscillograph at the plate of V11. L24 and L25 properly tuned (birdie at 26.4 mc.).

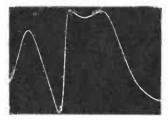


Figure 15-Z Sound trap properly adjusted.



Figure 15-CC Video IF response curve: Wobbulator to the grid of V2 and the traveling defector to the oscillograph at the plate of V10. L5 and L6 properly tuned (birdie at 26.4 mc.).

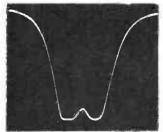


Figure 15-R Video IF response curve showing slight overloading due to too much signal applied to the stage from the wobbulated signal generator.

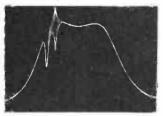


Figure 15-U Sound trap much too low. Birdie at 21.9 mc.

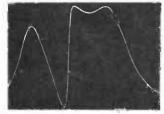


Figure 15-X Video IF response curve: Wobbulator to the grid of V11 and the traveling detector to the oscillograph at the plate of V12. L27 and L28 properly tuned (birdie at 26.4 mc.).

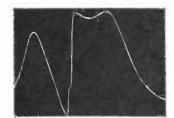


Figure 15-AA Sound trap too high.

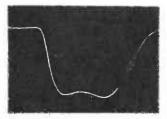
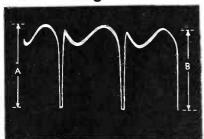
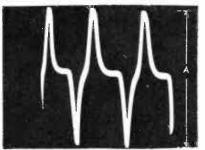


Figure 15-DD Overall video IF response curve: Wobbulator to the grid of V2 and the oscillograph to the cathode of V16. The birdie at 26,4 mc. is 50% down on the curve.

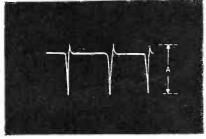
ALL AND AND A CONTRACTOR



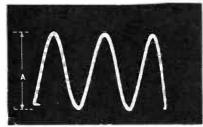
Cathode of Discriminator Tybe V2 Pin 8 Sync Stab A=22 volts B=20 volts



Horizontal Saw Gen Grid Tube V2 Pin 4 A=72 volts



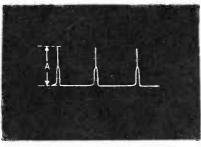
Sync Amplifier Grid Tube V2 Pin 1 A=4.5 volts



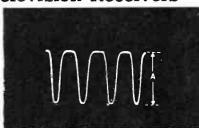
Oscillator Grid, Tube V3 Pin 5 Sync Stab A=35 volts



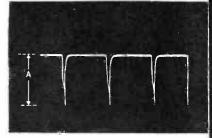
Horizontal Saw Gen Tube V2 Pin 5 A=50 volts



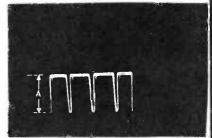
Sync Amplifier Plate Tube V2 Pin 2 A=17 volts



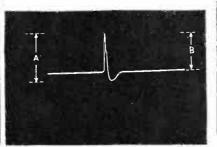
Oscillator Plate Tube V3 Pin 3 A=52 volts



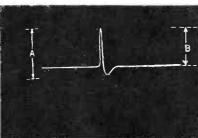
Damping Tube Plate Tube V5 Pin 2 A==450 volts



Vertical Sync Amp Grid Tube V6 Pin 4 A=35 volts



Vertical Sync Amp Plate Tube V6 Pin 8 A==55 volts B=50 volts



Vertical BTO Red Trans Lead A=60 volts B=50 volts



Vertical Saw Gen Grid Tube V7 Pin 4 A=25 volts B-105 volts



Vertical Saw Gen Plate Tube V7 Pin 5 A=25 volts B=125 volts

2001.00

100 M



Vertical Deflection Amp Grid Tube V8 Pin 4 A=60 volts B=85 volts Figure 16. Sweep Waveforms

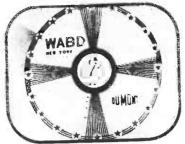


Vertical Amp Plate Tube V8 Pin 2 Sweep Non-Linear Due to Extreme Position of Controls A=125 volts

Test patterns presented by Allen B. Du Mont Laboratories in connection with their television receiver Model RA-101, but applicable to other modern television sets.



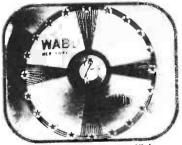
Normal Picture



Brightness Control Misadjusted



Focus Control Misadjusted*



Contrast Control Set Too High



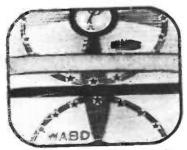
Contrast Control Set Much Too High*



Contrast Control Set Too Low



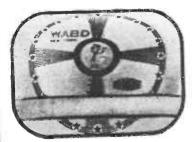
Horizontal Frequency Control Misadjusted*



Vertical Hold Control Misadjusted*



Horizontal Linearity Control Misadjusted*



Vertical Linearity and Size Controls Misadjusted*

* Test patterns taken with INS news tape.



Horizontal Size Control Misadjusted*

Figure 17. Test Patterns

Tre.



Outside Interference Caused By Diathermy

1

Emerson Radio

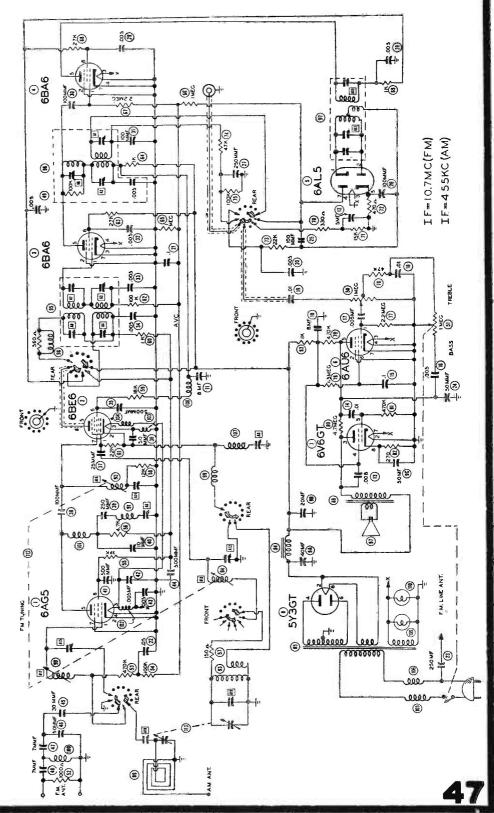
MODEL: 528

CHASSIS MODEL: 120038

An internal power line antenna is provided for FM operation in relatively strong signal areas. An external dipole antenna is recommended for maximum FM operation. To connect the dipole, remove the wire from the FM ANT, screw terminal "A," and connect the dipole leads to "A" and "G."

A ground connection is not required for AM or FM operation.

An external phonograph can be connected to the jack provided at the rear of the chassis base.



A self-contained loop antenna is provided for broadcast band reception. For permanent home installation, however, if it is desired to improve reception of weak stations, an additional outdoor antenna may be used. Connect the outdoor antenna to the single screw terminal on the loop terminal marked BCST. ANT. The loop antenna operates at maximum efficiency when its position is at right angles to the broadcasting source. Once the station is tured in, rotate the cabinet back and forth through a quarter of a circle, leaving it in the position where the station is received with maximum volume.



POWER SUPPLY: 60-cycle a.c.

VOLTAGE RATING: 105-125 volts.

POWER CONSUMPTION: 80 watts.

CURRENT DRAIN: 0.75 amp. at 117 volts a.c.

If replacements are made or the wiring disturbed in the r-f section of the circuit, the receiver should be carefully realigned.

The color coding of the i-f transformer leads is as follows:

Grid—green Grid return-black Plate-blue B+-red

INSTRUCTIONS FOR VOLTAGE AND RESISTANCE READINGS

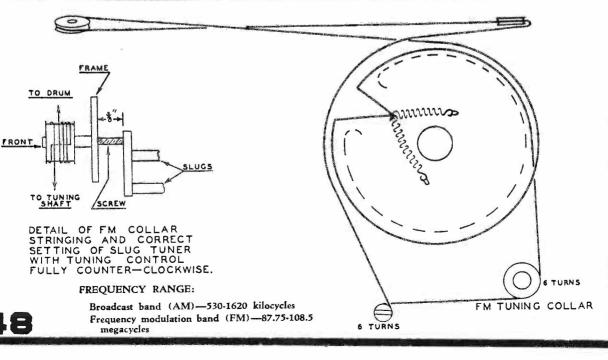
- All readings taken in broadcast position except those for item 4A, 6BA6 tube, which should be taken in FM position. Voltage readings are in volts and resistance readings in ohms unless otherwise specified. D-C voltage measurements are at 20,000 ohms per volt; a-c voltages measured at 1,000 ohms.
- 3.
- 4. 5. 6. 7. Socket connections are shown as bottom views.

2.

- Measured values are from socket pin to common negative.
- Line voltage maintained at 117 volts for voltage readings.
- Nominal tolerance on component values makes possible a variation of \pm 15% in voltage and resistance readings. Volume control at maximum, no signal applied for voltage measurements. Resistance readings in the B+ circuits may vary widely according to the condition of the filter capacitors. 8. ٥.

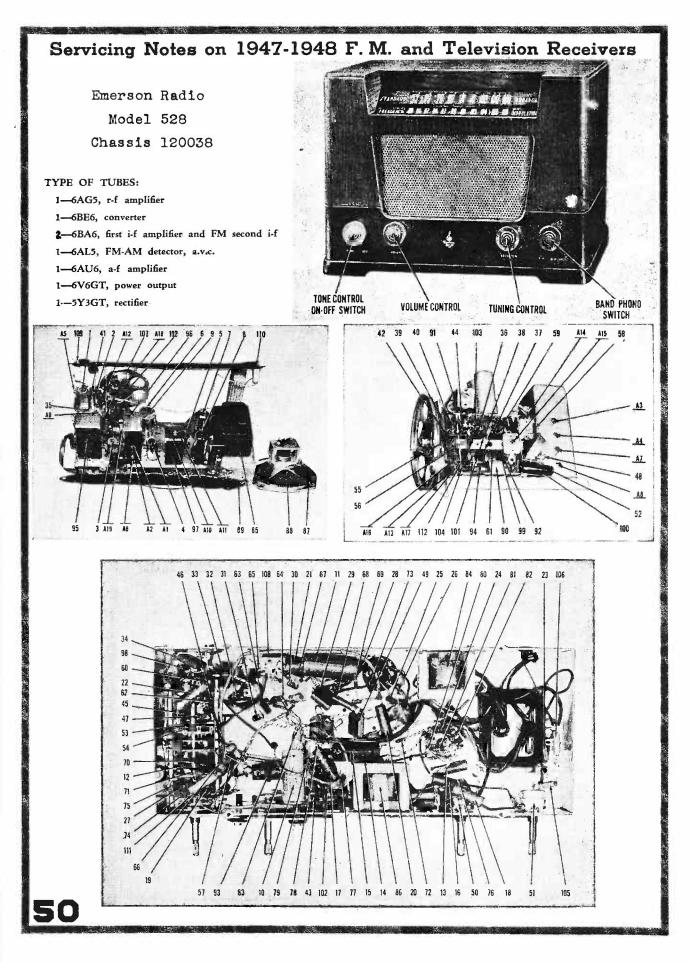
VOLTAGE READINGS

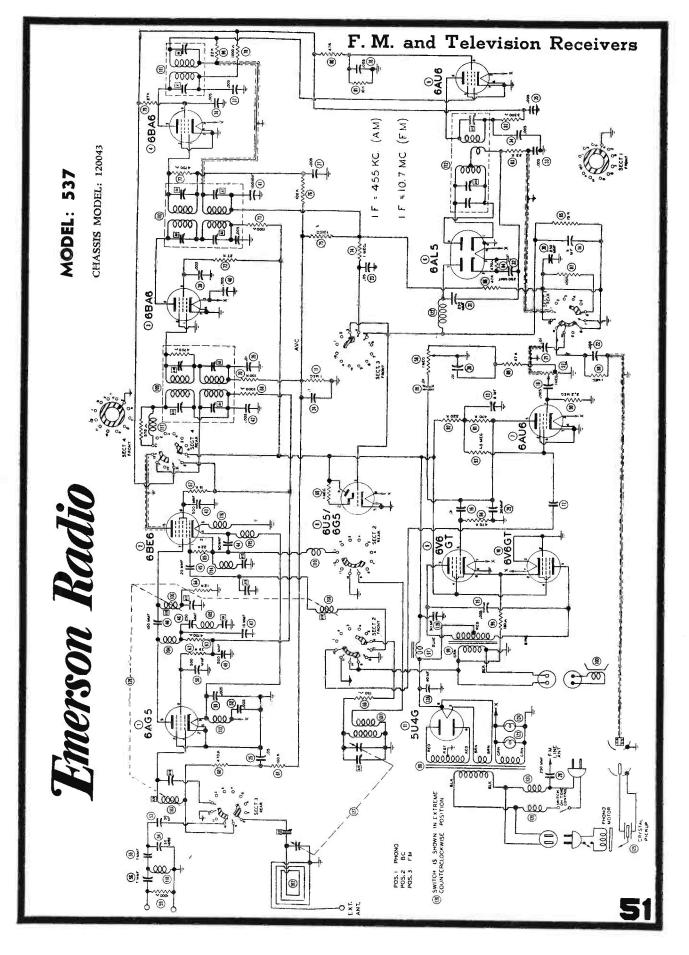
SYMBOL	TUBE	PIN 1	PIN 2	PIN 3	PIN 4	PIN 5	PIN 6	PIN 7	PIN 8
1	6AG5	-0.5 DC	0	6.5 AC	0	225 DC	137 DC	0	
2	6BE6	-0.3 DC	0	0	6.5 AC	270 DC	100 DC	0	
3	6 B A6	-0.1 DC	0	0	6.5 AC	260 DC	115 DC	0	
4	6BA6	-0.4 DC	0	6.5 AC	0	0	0	0	
4A	6BA6	-0.3 DC	0	6.5 AC	0	250 DC	110 DC	0	
5	6AL5	0	0	6.5 AC	0	0	0	-0.8 DC	
6	6AU6	-0.8 DC	0	6.5 AC	0	105 DC	32 DC	0	
7	6V6GT	0	0	260 DC	270 DC	0	105 DC	6.5 AC	13.5 DC
8	5Y3GT	0	300 DC	0	300 AC	0	300 AC	0	300 DC
	_		R	ESISTANC	E READIN	IGS			
SYMBOL	TUBE	PIN 1	PIN 2	PIN 3	PIN 4	PIN 5	PIN 6	PIN 7	PIN 8
1	6AG5	1.5 meg.	0	0.2	0	55,000	90,000	0	
2	6BE6	20,000	1	0.2	0.5	50,000	68,000	12,000	1
3	6BA6	680,000	0	0	0.1	50,000	77,000	0	
4	6BA6	3 meg.	0	0.1	0	inf.	inf.	0	
4A	6BA6	3 meg.	0	0.1	0	50,000	77,000	0	
5	6AL5	inf.	inf.	0.1	0	520	0	135,000	
6	6AU6	2.5 meg.	0	0.1	0	520,000	1.5 meg.	0	
7	6V6GT	0	0	50,000	50,000	470,000	520,000	0.1	250
8	5Y3GT	inf.	50,000	inf.	130	inf.	125	inf.	50,000



To set pointer turn variable condenser fully closed and set pointer to last reference mark at low-frequency end of dial. To inject signal in Steps 4, 5 and 6, remove tube and connect wire to pin 1. Replace tube, making certain that wire does not short to shield base. For Step 8, connect two 100,000 ohm resistors in series from pin 7 of 6AL5 to chassis. After Step 8, turn variable condenser fully counterclockwise and check adjustment of FM tuning unit per dial cord drawing. Volume control should be at maximum position; output of signal generator should be no higher than necessary to obtain an output reading. Use an alignment screwdriver for adjusting.

-						a state of the second second second	Constant of the second of the	warmen für für ihren mit determinen werten eine mit determinenten
	DUMMY ANTENNA	SIGNAL GENERATOR COUPLING	SIGNAL GENERATOR FREQUENCY	BAND SWITCH POSITION	RADIO DIAL SETTING	OUTPUT METER	ADJUST	REMARKS
1	0.1 mfd.	High side to stator of front section of the variable con- denser. Low side to chassis.	455 kc	BC (center position)	High fre- quency end of dial.	Across voice coil.	A1, A2, A3, A4	Adjust for maximum output.
2	0.1 mfd.	High side to stator of front section of the variable con- denser. Low side to chassis.	455 kc	BC (center position)	Low fre- quency end of dial.	Across voice coil.	A5	Adjust for minimum output.
3	0.05 mfd.	High side to pin 1 (grid) of 6BA6, 1st 1-f tube (3). Low side to chassis.	10.7 mc (unmodulated)	FM (fully clockwise)	High fre- quency end of dial.	7 of 6AL5 and chassis.	A6	Adjust for maximum deflection.
4	0.05 mfd.	High side to pin 1 (grid) of 6BE6. Low side to chassis.	10.6 mc (unmodulated)	FM (fully clockwise)	High fre- quency end of dial.	VTVM con- nected to pin 7 of 6AL5 and chassis.	A7	Adjust for maximum deflection.
5	0.05 mfd.	High side to pin 1 (grid) of 6BE6. Low side to chassis.	10.8 mc (unmodulated)	FM (fully clockwise)	High fre- quency end of dial.	VTVM con- nected to pin 7 of 6AL5 and chassis.	A8	Adjust for maximum deflection.
6	0.05 mfd.	High side to pin 1 (grid) of 6BE6. Low side to chassis.	10.7 mc (unmodulated)	FM (fully clockwise)	High fre- quency end of dial.	VTVM con- nected to pin 7 of 6AL5 and chassis.	A9	Adjust for maximum deflection.
7	0.05 mfd.	High side to pin 1 (grid) of 6BA6, 2nd 1-f tube (4). Low side to chassis.	10.7 mc (unmodulated)	FM (fully clockwise)	High fre- quency end of dial.	VTVM con- nected to pin 7 of 6AL5 and chassis.	A10	Adjust for maximum deflection.
8	0.05 mfd.	High side to pin 1 (grid) of 6BA6, 2nd 1-f tube (4). Low side to chassis.	10.7 mc (unmodulated)	FM (fully clockwise)	High fre- quency end of dial.	VTVM con- nected from junction of two 106,000 Ohm resistors and junction of condensers 25 and 26. (See prelimin- ary alignment notes.)	All	Adjust for zero deflection.
9	150 ohms in series with each lead.	High side to "A," low side to "Q" on FM antenna terminals. Dis- connect internal antenna.	108 mc (unmodulated)	FM (fully clockwise)	108 mc	VTVM con- nected to pin 7 of 6AL5 and chassis.	A 12	Adjust for maximum deflection,
10	150 ohms in series with each lead.	High side to "A," low side to "G" on FM antenna terminals. Dis- connect Internal antenna.	88 mc (unmodulated)	FM (fully clockwise)	88 mc	VTVM con- nected to pin 7 of 6AL5 and chassis.	A 13	Adjust iron core (hold brass in position) for maximum de- flection.
11	150 ohms in series with each lead.	High side to "A," low side to "G" on FM antenna terminals. Dis- connect internal antenna.	98 mc	FM (fully clockwise)	98 mč	VTVM con- nected to pin 7 of 6AL5 and chassis.	A 13	Adjust brass and from cores (one screw) for maximum deflection. Re- peat steps 9, 10 and 11 until no further improve- ment cau be made.
12	150 ohms in series with each lead.	High side to "A," low side to "G" on FM antenna terminals. Dis- connect internal antenna.	106 mc	FM (fully clockwise)	Tune for maximum deflection.	VTVM con- nected to pin 7 of 6AL5 and chassis.	A 14, A 15	Adjust for maximum deflection.
13	150 ohms in series with each lead.	High side to "A," low side to "G" on FM antenna terminals. Dis- connect internal antenna.	90 mc	FM (fully clockwise)	Tune for maximum deflection.	VTVM con- nected to pin 7 of 6AL5 and chassis.	A 16, A 17	Adjust iron cores (hold brass in place) for maximum deflection.
14	150 ohms in series with each lead.	High side to "A," low side to "G" on FM antenna terminals. Dis- connect internal antenna.	100 mc	FM (fully clockwise)	Tune for maximum deflection.	VTVM con- nected to pin 7 of 6AL5 and chassis.	A16, A17	Adjust both iron and brass cores for maximum deflection. Repeat steps 12, 13, and 14 until no further improvement can be made.
15	200 mmfd.	High side to "A," low side to "G" terminals of AM	1600 kc	BC	1600 kc	Across voice coil.	A18	Adjust for maximum output.
16	20 mmfd.	antenna terminals. High side to "A," low side to "G" terminals of AM autenna terminals.	1400 kc	BC	Tune for maximum output.	Across voice coil.	A19	Adjust for maximum output. 49





Servicing Notes on 1947-1948 F. M. and Television Receivers EMERSON RADIO & PHONOGRAPH CORPORATION

ALIGNMENT

To set pointer turn variable condenser fully closed and set pointer to last reference mark at low frequency end of dial. To inject signal in Steps 5, 6 and 7, remove 6BE6 and connect wire to pin 1. Replace tube, making certain that wire does not short to shield base. In Step 9, connect two 100,000 ohm resistors in series from pin 7 of 6AL5 to chassis. These resistors should be equal within 5%. After Step 9, turn variable condenser fully counterclockwise and check adjustment of FM tuning unit per dial cord drawing. Loop should be maintained in same relative position to chassis as when receiver is in cabinet. Volume control should be at maximum position; output of signal generator should be no higher than necessary to obtain an output reading. Use an insulated alignment screwdriver for adjusting.

0	npen reuting	g. Ose all insulated angl		DANTO	RADIO	The second se		
	DUMMY	SIGNAL GENERATOR COUPLING	SIGNAL GENERATOR FREQUENCY	BAND SWITCH POSITION	DIAL SETTING	OUTPUT METER	ADJUST	
1	0,1 mfd.	High side to front stator of variable condenser. Low side to chassis.	455 kc	BC (center position)	High fre- quency end of dial.	Across voice coil.	A3, A4	Adjust for maximum output.
2	0.1 mfd.	High side to front stator of variable condenser. Low side to chassis.	455 kc	BC (center position)	Low frequency end of dial.	Across voice coil.	A5	Adjust for minimum output.
3	0.05 mfd.	High side to pin 1 (grid) of 6BA6, 2nd i-f tube (4). Low side to chassis.	10.7 mc (un- modulated)	FM (fully clockwise)	High fre- quency end of dial.	VTVM con- nected from pin 7 of 6AL5 to chassis.	A6, A7	Adjust for maximum deflection.
4	0.05 mfd.	High side to pin 1 (grid) of 6BA6, 1st i-f tube (3). Low side to chassis.	10.7 mc (un- modulated)	FM (fully clockwise)	High frequency end of dial.	VTVM con- nected from pin 7 of 6AL5 to chassis.	A8, A9	Adjust for maximum deflection.
5	0.05 mfd.	High side to pin 1 (grid) of 6BE6. Low side to chassis.	10.6 mc un- modulated)	FM (fully clockwise)	High frequency end of dial.	VTVM con- nected from pir 7 of 6AL5 to chassis.	A10	Adjust for maximum deflection.
6	0.05 mfd.	High side to pin 1 (grid) of 6BE6. Low side to chassis.	10.8 mc (un - modulated)	FM (fully clockwise)	High frequency end of dial.	VTVM con- nected from pir 7 of 6AL5 to- chassis.	A11	Adjust for maximum deflection.
7	0.05 mfd.	High side to pin 1 (grid) of 6BE6. Low side to chassis.	10.7 mc (un- modulated)	FM (fully clockwise)	High frequency end of dial.		A12	Adjust for maximum deflection.
8	0.05 mfd.	High side to pin 1 (grid) 6AU6, 3rd i-f the (5). Low side to chassis.	10.7 mc (un- modulated)	FM (fully clockwise)	High frequency end of dial.		A13	Adjust for maximum deflection.
9	0.05 mfd.	High side to pin 1 (grid) 6AU6, 3rd 1-f tube (5). Low side to chassis.	10.7 mc (un- modulated)	FM (fully clockwise)	High frequency end of dial.		•	Adjust for zero deflection.
10	150 ohms i	High side to ungrounder	a 108 mc (un-	FM (fully clockwise)	108 mc	VTVM con- nected from	A15	Adjust for maximum deflection.
	series with each lead.		modulated)		88 · mc	pin 7 of 6AL5 to chassis. VTVM con-		Adjust iron core (hold
ī	150 ohms i series with each lead	Low side to chassis.	d 88 mc (un- modulated)	FM (fully clockwise)	00 · me	hected from pin 7 of 6AL5 to chassis.		brass in position) for maximum deflection.
ī	2 150 ohms i series with each lead	Low side to chassis.	d 98 mc (un- modulated)	FM (fully clockwise)	98 mc	VTVM con- nected from pin 7 of 6AL! to chassis.	A16	Adjust iron and brass cores (single screw) for maximum deflection. Re- pent steps 10, 11, 12 until no further im- provement can be made.
ī	3 150 ohms i series with each lead	1 Low side to chassis. (Disconnect internal	d 106 mc (un- modulated)	FM (fully clockwise)		VTVM con- nected from pin 7 of 6AL to chassis.		Adjust for maximum deflection.
ī	4 150 ohms i series with each lead	Low side to chassis. (Disconnect internal	ed 90 mc (un- modulated)	FM (fully clockwise)		VTVM con- nected from pin 7 of 6AL to chassis.	A19, A20	brass in position) for maximum deflection.
ī	5 150 ohms series with each lead	h FM antenna terminal.Lo	w modulated)	FM (fully clockwise)		VTVM con- nected from pin 7 of 6AL to chassis.		Adjust iron and brass cores (single serew) for maximum deflection. Re- peat steps 10, 11, 12 until no further 1m- provement can be made
Ĩ	.6 200 mmf	terminal strip. Low sid	na	BC	1600 kc	Across voice coil.	A21	Adjust for maximum output.
Ĩ	7 200 mmf	terminal strip. Low sid	na	BC	Tune for maximum output.	Across voice coil.	A22	Adjust for maximum output.
	36	to chassis.	.1.	1				

Servicing Notes on 1947-1948 F. M. and Television Receivers VOLTAGE READINGS

SYMBOL	TUBE	PIN 1	PIN 2	PIN 3	PIN 4	PIN 5	PIN 6	PIN 7	PIN :
1	6AG5	-0.4DC	0	6.2AC	0	225DC	137DC	0	
2	6BE6	-0.3DC	0	0	6.2AC	270DC	100DC	0	
3	6BA6	-0.3DC	0	6.2AC	0	270DC	122DC	0	1
4	6BA6	-0.5DC	0	6.2AC	0	260DC	110DC	Q	
5	6AU6	-0.6DC	0	6.2AC	0	280DC	48DC	0	4
6	6AL5	0	0	0	6.2AC	0.4DC	0	-11DC	1
7	6AU6	-0.7DC	0	6.2AC	0	59DC	29DC	0	1
9	6V6GT	0	0	320DC	290DC	0	59DC	6.2AC	15DC
10	6V6GT	0	0	320DC	290DC	0	0	6.2AC	15DC
11	5U4G	0	330DC	0	300AC	O	300AC	0	330DC

RESISTANCE READINGS

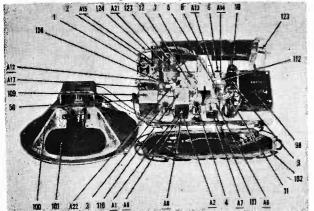
SYMBOL	TUBE	PIN 1	PIN 2	PIN 3	PIN 4	PIN 5	PIN 6	PIN 7	PIN 8
1	6AG5	1.1 meg.	0	0.2	0	85,000	120,000	0	
2	6BE6	22.000	0.7	0.2	014	80,000	98,000	12,000	
3	6BA6	650,000	0	0.1	0	80,000	110,000	0	
4	6BA6	650,000	0	0.1	0	45,000	70,000	0	
5.	6AU6	45.000	ō	0.1	0	45,000	10,000	0	·
6	6AL5	inf.	inf.	0	0.1	450	0	15,000	
7	6AU6	2.4 meg.	0	0.1	0	770,000	1.8 meg.	0	1
9	6V6GT	0	0	80,000	80.000	450,000	0.3	0.1	170
10	6V6GT	0	0	80.000	80,000	0	620,000	0.1	170
11	5U4G	inf.	80,000	inf.	69	inf.	72	inf.	80,000

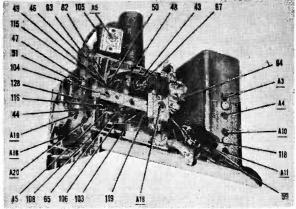
1. Voltage readings are in volts and resistance readings in ohms unless otherwise specified.

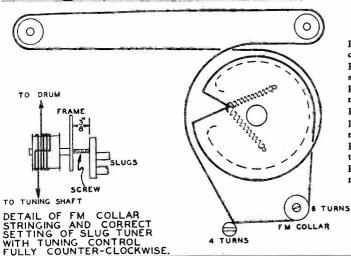
2. All readings taken in broadcast position except those for items 4, 5 and 6, which should be taken in FM position.

3. D-C voltage measurements are at 20,000 ohms per volt; a-c voltages measured at 1,000 ohms.

- 4. Socket connections are shown as bottom views.
- 5. Measured values are from socket pin to common negative.
- 6. Line voltage maintained at 117 volts for voltage readings.
- 7. Nominal tolerance on component values makes possible a variation of \pm 15% in voltage and resistance readings. 8. Volume control at maximum, no signal applied for voltage measurements.
- 9. Resistance readings in the B+ circuits may vary widely according to the condition of the filter capacitors.







DISASSEMBLY INSTRUCTIONS

Remove four push-on type control knobs from top of cabinet.

Remove phono motor plug, phono pickup plug, and two speaker plugs from chassis.

Remove two Phillips head screws holding antenna terminal strip to chassis.

Remove two nuts and washers fastening loop to cabinet. Remove two Phillips head bolts in phono compartment retaining chassis to cabinet.

Remove two hex head bolts and washers retaining chassis to cabinet. Remove loop and chassis from rear of cabinet. Remove four nuts fastening speaker to cabinet and remove speaker.

ALIGNMENT PROCEDURE FOR A.M.:

1. Connect generator to tuning condenser stator (BC Antenna) in series with .01 mfd.; tune generator to 455 Kc.; tune radio to quiet point on high frequency end of dial, and adjust 1st and 2nd IF transformers (455 Kc.) for maximum peak output.

2. Connect generator to antenna terminal in series with 200 mmf. Turn tuning control to extreme full mesh position of tuning condenser. Set pointer to line located just below 55 calibration on Bcst. Band. Tune receiver to 60 on dial; tune generator to 600 Kc. Adjust BC padder, BC Ant. Coil Inductance (%2 screw on rear of chassis) for maximum output.

3. Tune receiver to 160 on dial; tune generator to 1600 Kc. Adjust BC. Osc. and BC. Ant. trimmers for maximum output. Repeat 2 and 3 for best alignment.

ALIGNMENT PROCEDURE FOR F.M.:

Note: Points A, B, C, D, E, and F, are noted on circuit diagram.

1. Set Band Switch to FM.

69A6

2. Connect vacuum tube voltmeter (VTVM) across points B and C.

3. Connect 10.7 Mc. signal generator through .01 mfd. condenser to point A and ground.

4. Adjust primary of FM Detector Transformer for maximum VTVM reading.

5. Connect VTVM across points B and D

6. Adjust secondary of FM Detector Transformer for zero VTVM reading.

7. Connect 10.7 Mc. Signal Generator to point F and ground.

8. Connect VTVM across points B and C.

9. Rotate 10.7 Mc. adjustment screw of 2nd IF Transformer Secondary maximum number of turns counterclockwise. 10. Adjust primary of 2nd IF Transformer for maximum VTVM reading.

11. Adjust secondary of 2nd IF transformer, keeping reading between 2 and 3 volts.

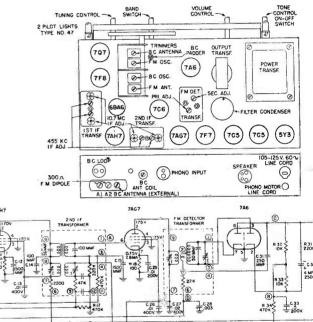
12. Connect 10.7 Mc generator to point E and ground. Rotate 10.7 Mc adjustment screw of 1st IF Transformer Secondary maximum number of turns counter clockwise. Adjust primary of 1st IF Transformer for maximum VTVM reading.

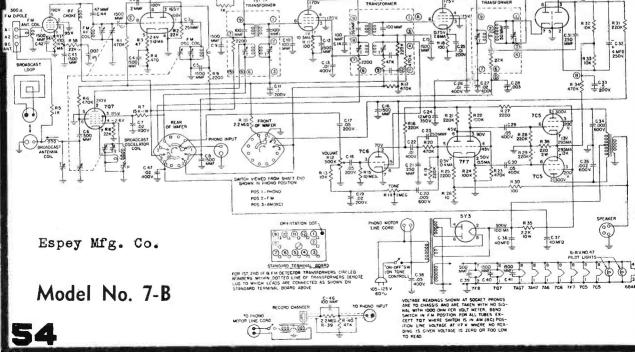
13. Adjust secondary of 1st IF Transformer for maximum VTVM reading, keeping the voltage between 2 and 3.

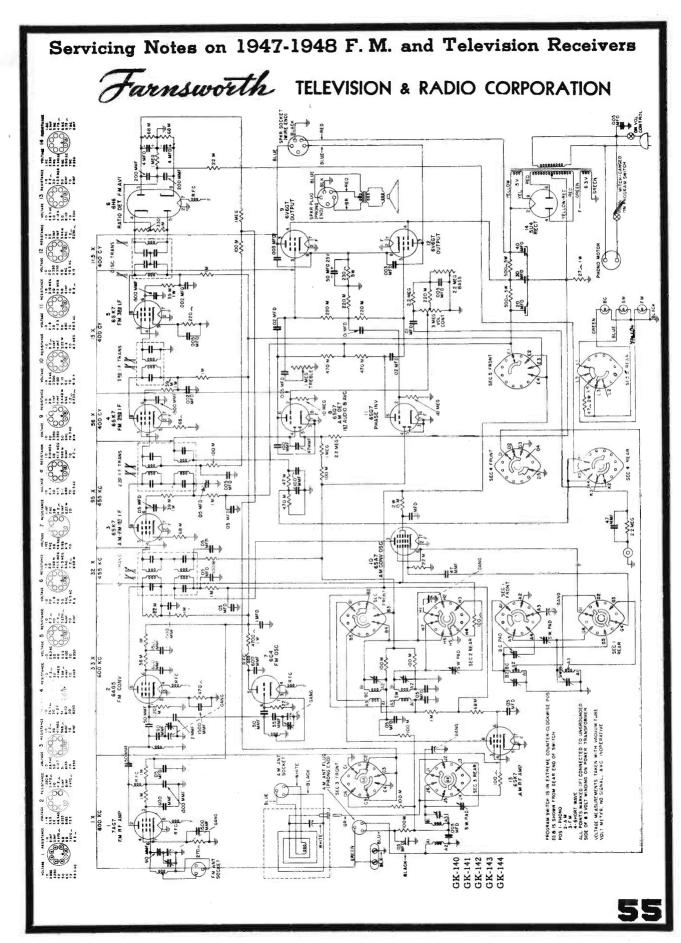
14. Connect 106 Mc. Signal Generator to FM antenna terminals. If generator impedance is low, put one 150-ohm carbon resistor in series with each of the generator leads. Tune receiver dial to 106 Mc.

15. Adjust FM Oscillator Trimmer for maximum VTVM reading.

16. Adjust FM Antenna Trimmer for maximum VTVM reading.







Farnsworth

GK-140 SERIES

TELEVISION & RADIO CORPORATION

TABULATION FOR AM ALIGNMENT

STEPS	CONNECT GENERATOR		SET GENERATOR AT	SET GANG AT	ADJUST	TO OBTAIN
1		S	Set Tone and Volum	ne Controls at M	aximum	
2	ngh Afd.		AFF Va	Quiet	2nd. I.F. Slugs	
3	Through .1 Mfd.	Grid Conv. tube 455 Kc Quiet Point	lst. I.F. Slugs	Ē		
4	Mfd.		1500 Kc	1500 Kc	BC Osc. Trimmer	MAXIMUM OUTPUT
5	ugh .1	RF of GANG	1500 Kt	1500 Ke	BC Mixer Trimmer	
6	Through		600 Kc	600 Kc	Osc. Padder *	IAXIM
7		Check dial calibratic adj	on at several frequen ust oscillator padder	cies. If not reaso . See Note 1	onably correct,	X
8	#	Ext. Ant. Binding Post	1500 Kc	1500 Kc	Loop Trimmer	

#Through RMA dummy antenna.

* This adjustment should be made while gang is rocked.

SHORT WAVE RF

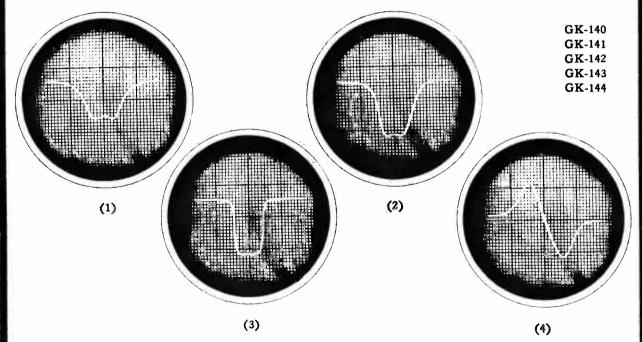
10				15 MC	SW Osc. Trimmer See Note 2	
11	esistor	тот tesise щи с External	15 MC	15 MC Image at 15.91 MC	SW Conv. Trimmer	OUTPUT
12	1				SW Ant. Trimmer	
13	gh 400	Antenna	9.4 MC	9.4 MC	SW Osc. Padder	
14	Through			Image at	SW Conv. Padder	MAXIMUM
15				10. 3 1 MC	SW Ant. Padder	M
16			Recheck Steps 10 to	5 15 inclusive.		

Servicing Notes on 1947-1948 F. M. and Television Receivers Oscilloscope Alignment FM Band

FM IF ALIGNMENT

- 1. Equipment Required: Oscilloscope. 10.7 MC sweep generator, voltomyst, and RF signal generator.
- 2. Set band switch in FM position.
- 3. Make connection from vertical deflection amplifier of oscilloscope to pin #3 of 6H6 discriminator tube. Make certain that the 4MFD electrolytic condenser is disconnected from this same circuit. It is necessary that the lead to the oscilloscope be shielded, of low total capacity, and connection to receiver isolated by means of a 1 meg. resistor.
- 4. Connect sweep generator to last FM IF grid through a .1 MFD coupling capacitor.
- 5. Load primary of discriminator transformer with resistor of approximately 39000 ohms. Back out secondary slug (top slug) as far as it will turn. Align primary (bottom slug) to obtain curve similar to figure 1. This does not constitute a final alignment of discriminator, but is a convenient expedient to assist in I.F. alignment.

- Shift connection of sweep signal generator to the grid of the second FM IF tube. NOTE: As alignment moves from stage to stage, reduce input instead of reducing oscilloscope gain.
- 7. Align third FM IF transformer for a symmetrical flat top pattern. (Fig. 2).
- 8. Shift signal generator to the grid of the first IF tube.
- 9. Align second IF transformer in same manner as described in Section 7. Note that the width of the nose of the curve is the same as before, but the sides have become steeper, as in Fig. 3.
- 10. Connect the signal generator to the grid of the converter tube grid in series with 10,000 ohm resistor and a .1MFD capacitor, or loosely couple by stray capacity of an insulated wire.
- 11. Align first FM IF transformer in the same manner as in Section 7. Note that the sides of the curve have further steepened, but that the nose of the curve has retained approximately the same width as in Fig. 3.



- 12. Connect 4 MFD electrolytic capacitor that was previously disconnected, and take off load resistor on discriminator primary.
- 13. Connect oscilloscope to audio output terminal of discriminator. There are several points where contact can be made and can be identified as the circuit connected to the terminal on the terminal board (nearest the discriminator transformer) to which the shielded lead is connected.
- 14. With sweep signal input to converter grid, align discriminator transformer for conventional discriminator pattern, as in Fig. 4.
- 15. Connect signal generator to converter tube grid through .1MFD capacitor. An unmodulated signal input of 65 microvolts at 10.7 Mc should develop .55 volt rise on the AVC line with voltohmyst connected to AVC line through 1 megohm resistor.



arnsworth

GK-140 SERIES

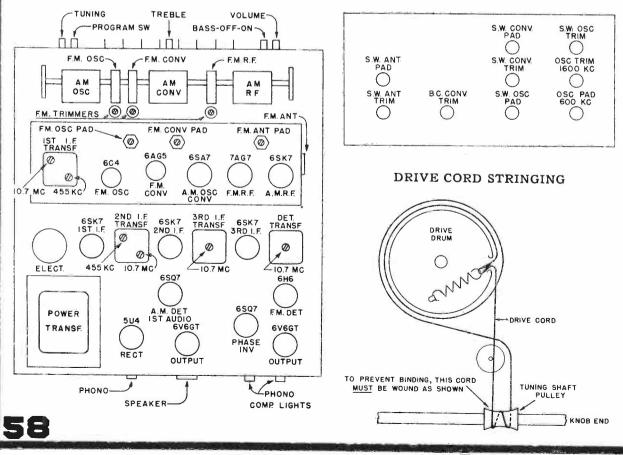
FM RF Alignment

- 1. Equipment Required:
 - a. RF Signal Generator. Range 88 to 108 MC.
 - b. Output Meter.
 - c. Insulated Screw Driver,
- 2. Connect RF signal generator in series with 400 ohm carbon resistor to "high" side of FM antenna socket. Connect output meter across voice coil of speaker.
- Set tuning control for pointer to calibrate at the equivalent of half way between channels 300 and 301.
- 4. Apply 108 MC Signal.
- 5. Set converter and antenna trimmers at minimum capacity.
- Adjust oscillator trimmer by tuning from maximum capacity to first signal that is heard, and peak for maximum output.
- 7. Adjust antenna and converter trimmers for maximum output.

CHASSIS LAYOUT

- 8. Set tuning controls so dial pointer calibrates at the equivalent of half way between channels 200 and 201.
- 9. Apply 88 MC signal.
- 10. Adjust oscillator, converter, and antenna slugs to maximum output.
- Repeat operations 3 to 10 inclusive. NOTE: The degree of adjustment required in the tuning of the oscillator slug will determine the number of times operations 3 to 10 must be repeated until no further gain in sensitivity is obtained.
- 12. Carefully tune across the entire FM band for the observance of the dead or weak spots that may be a resultant of improper alignment or defective components. This can be deternined by carefully noting the degree of receiver noise, that is, high noise generally is accompanied by good sensitivity.

FRONT OF CHASSIS



farnsworth

MODELS GV220, GV240

Model GV-260 is similar

The features described below will be of special interest to the serious student of television. By referring to the complete schematic diagram on this page, you will note that the control grid of the first tube is grounded, and that cathode injection of signals into the R.F. amplifier is used. This technique has the advantage of simplifying the input circuit and reducing tube noise.

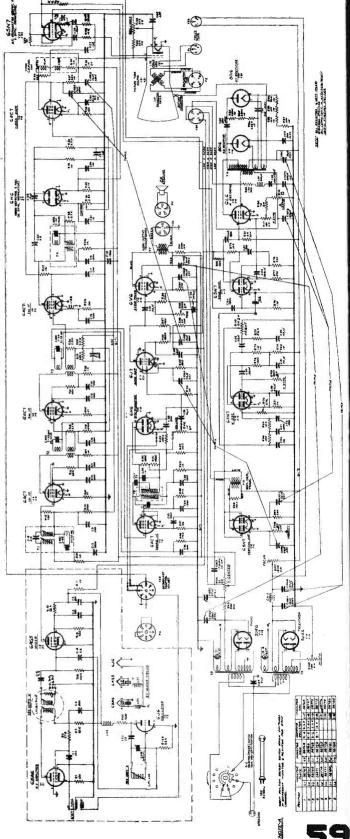
The R.F. section uses subchassis construction for better isolation of circuits. This is especially advantageous at frequencies above 100 MC.

A separate broadcast band adapter is avilable which can be plugged in and will permit the reception of both television and broadcast stations.

Band-switching is accomplished through a compact and stable turret assembly. This assembly carries all tuning inductances, slug-tuned, and the associated damping resistors. It is in three scetions, corresponding to plate coils of V1, grid coils of V2, and the oscillator tuning inductances.

In the video I.F. amplifier a wide pass-band is obtained through the use of loading resistors across the overcoupled transformer secondaries, while adjacent channel suppression is secured with trap circuits in each transformer.

Video detection, sync separation, automatic gain control action are accomplished with a single tube. Quite a complete explanation of such a circuit is given in "Advanced Radio Servicing" by Beitman.



In connection with the presentation of material on the Farnsworth television receiver, stress will be placed on detecting the existence of faults through observation of a test pattern. These are several different types of patterns and these are transmitted for short periods for use by servicemen. The Farnsworth Company pattern used in our illustrations embodies some special features, but in general the suggestions given can be applied to other patterns.

Refer to Figure 32a which shows this pattern. It consists of several sets of converging alternately black and white lines, a centrally-located series of concentric circles of graduated shading, certain lettering, and a series of horizontal and vertical lines. These shall be discussed in turn and their purpose explained.

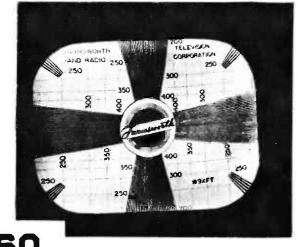
The converging lines constitute "resolution wedges" whose purpose is to indicate the amount of resolution which may be had in a picture. Those bars which are situated in a vertical direction measure the resolution in horizontal direction and those lying horizontally measure the vertical resolution.

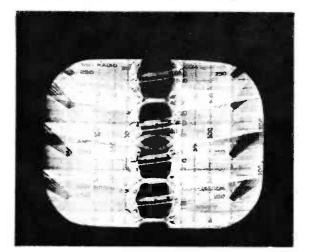
At the transmitter, the scanning of two lines, one black and one white, produces an electrical signal of one cycle (not one cycle per second). The scanning rate is a constant and it is evident that the more closely spaced these lines are placed, the greater the number of cycles are produced in a given lapse of time.

So may a known spacing of the lines represent a certain frequency of the video signal. It is also evident that, should the receiver be incapable of reproducing the high-frequency components in the reproduced image. The high-frequency portion of the resolution wedge will not be reproduced--the alternate black and white lines will not be distinct. Rather, they will merge into a single dark mass. Therefore, the point at which the lines merge into indistinction indicates the degree of frequency response of the system.

For example, the normally-functioning receiver should reproduce the lines approximately to the point marked 400--which means the equivalent of 400 alternately black and white lines between one side of the picture and the other. If the receiver is out of adjustment and the bandwidth is too narrow, it will not reproduce this many lines.

Next, we shall consider the concentric circles shown in the chart. Even as in photographic work, an improper gamma in reproduction will lead to a picture which is "washed out" or one which is "overly





32a Normal test pattern

32b Loss of vertical sync.

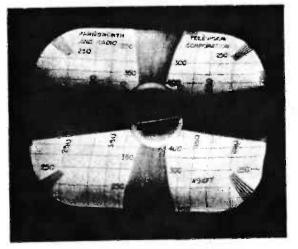
contrasty." If the proper gamma is present, the graduation of shading in these concentric circles will appear to be equally darker or lighter than adjacent circles. Misadjustment in the receiver may cause, for example, the two inner circles to be equally shaded - black - or the two circles may both be equally white. The first condition would produce an overly contrasty picture while the latter would produce a picture having a "washed out" appearance. Gamma is determined by the relative settings of the contrast control and the brilliance control.

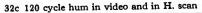
The circles must not become oval, for this indicates that there exists excessive sweep amplitude in the direction of the longer axis of the ellipse (or insufficient in the direction of the shorter axis which may also be shown by the fact that the raster is not filled). Non-linearity of sweep is shown by an improper relationship between the various portions of the test patterns and by an egg-shaped set of "circles."

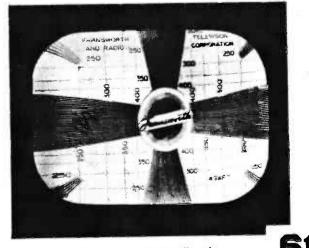
Some test patterns incorporate two large circles, one somewhat larger than the other. These may be used to obtain proper setting of the width and height controls, for the larger of the circles should just fill the screen in a horizontal direction, the smaller in the vertical direction. They, too, should be circles and not ellipses.

There are a few additional items to be observed in the use of the test chart. Its aspect ratio is 4.3, the proper ratio for a television picture. Therefore, it may be adjusted to just fill the screen by properly setting the height and width controls.

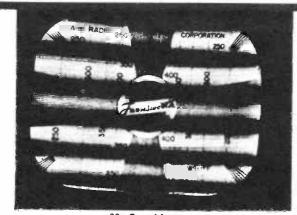
Should the frequency response of the receiver be peaked at any portion of the response curve, this will be indicated in the test pattern as an excessively dark portion of the resolution wedge. A dark portion across the screen may be the result of hum-modulation of the signal, such as the entrance of 60 cycle hum into the video portion of the receiver but this will be distinguished by a dark band extending from the left to the right extremities of the raster. Peaking in the video section will produce a darkened portion of the wedge alone and the frequency of this peak may be judged by the portion of the wedge which is dark (overly contrasty). If at the high frequency portion of the pass-band, the effect will be noted at the high-frequency portion of the wedge. The various figures illustrate the appearance of the pattern when defects in reception are present.



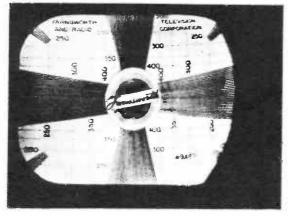




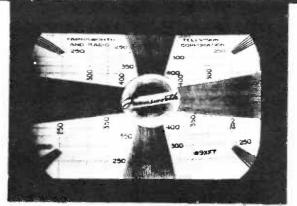
32d Faulty horizontal linearity



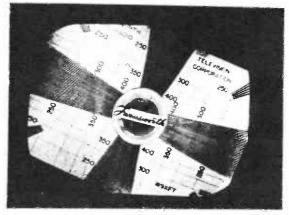




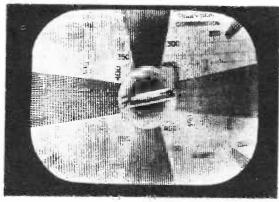
32g Corner cutting by focus coil



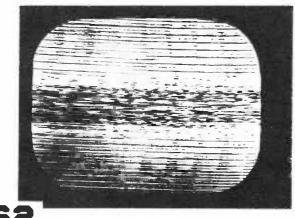
32f Height control too low



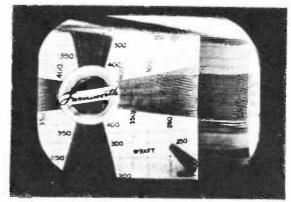
32h Deflection coil rotated



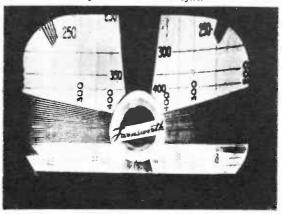
32i Beat frequency interference



32k Horizontal oscillator out of sync.



32j Loss of horizontal sync.



32L Improper vertical linearity

A CONTRACTOR



SERVICE DATA For MODEL 417A

SPECIFICATIONS

OPERATING FREQUENCIES:

Standard Band	540 to 1600 kc
Short Wave 1	9.4 to 9.9 mc
Short Wave 2	11.6 to 12.1 mc
Frequency Modulation 1	
Frequency Modulation 2	
AM I-F Frequency	
FM I-F Frequency	

POWER OUTPUT (117 volts line):

Undistorted.	 ts

ANTENNA INPUTS:

Broadcast and Short Wave—conventional antenna FM—300-ohm input for folded dipole

PHONOGRAPH PICK-UP:

Type	. Variable Reluctance
D-C Resistance	

GENERAL INFORMATION

INTRODUCTION

The information contained in this service note covers the Model 417A completely except for the record player. This receiver employs either the type P2 (two-post) or type P3 (single-post) record player which are covered in separate service notes.

THE TUNING SYSTEM

The "r-f end" of the receiver is unusual in a number of respects. Variable inductance tuning is employed instead of using a conventional tuning capacitor. This design makes possible two distinct advantages. First, it provides a high efficiency FM circuit in the 88 to 108 megacycle range which would not be possible with the more conventional methods of tuning. Second, it provides stable short-wave spread-bands which tune as easily as the broadcast band. Other advantages are also obtained but the two mentioned above are the most important. Tuning is accomplished by an "elevator" which consists of

Tuning is accomplished by an "elevator" which consists of a rigid plastic horizontal plate raised and lowered by means of a windlass controlled by the tuning knob at the panel. From this plate are suspended three powdered iron cores which tune the broadcast r-f, converter, and oscillator coils; and three tuning "vanes" which tune three low-inductance circuits. These latter circuits are employed in both FM bands and both short-wave bands with the exception of the antenna circuit for the short-wave spread-bands when a broad tuned antenna coil is used and the r-f guillotine tuner is switched out. They are called "guillotine" tuners because of their appearance.

FACTS ABOUT "GUILLOTINE" TUNING

The "guillotine" tuners are designed primarily for the 88-108 megacycle FM band where special technique is needed to realize high gain and circuit stability. Ordinary coils, tuned by a variable capacitor, are inefficient at these frequencies, first, because of the low inductances required to reach these frequencies when a variable tuning capacitor is employed and, second, because shunt capacity reduces the gain of the amplifier circuit; shunt capacity must be kept very low. Another disadvantage of standard tuning arrangements at these frequencies is that common coupling is obtained through the shaft of a ganged tuning capacitor unless insulated single sections are used (cumbersome and costly). Common coupling of this type tends to cause oscillation or general instability and precludes high gain per stage. The guillotines make possible short leads, completely isolated sections, stable tuning, high Q circuits, low shunt capacity, and location of each tuner in the best physical and electrical position in the assembly. Furthermore, since the shunt capacity is small and the inductance is consequently at its highest corresponding value, the additional unavoidable inductance introduced in the wiring, band switch, etc., produces a minimum of circuit losses and unbalance.

The guillotine tuner consists of a heavy, silver-plated, twoturn square coil, rigidly supported between two plastic posts. A flat, solid vane slides up and down between the two turns. It is guided in grooves in the plastic posts so that it passes between the two sections of the coil without touching them. The posts are so moulded and the coil so constructed that the whole assembly is held rigidly at a predetermined spacing. The tuning vane is raised and lowered by the tuning elevator. When the elevator is all the way up (set tuned to lowest frequency), the vane is completely above the coil which then acts as a simple two-turn coil. As the set is tuned toward the higher frequencies, the vane moves downward into the field of the coil until, finally, it is all the way in. The vane reduces the inductance of the coil through two principles. First, it acts as a shorted turn, and thus reduces inductance directly; second, it provides a barrier between the two turns of the coil which reduces the mutual coupling and thus also reduces inductance.

The tuners described above are identified as T2, T4, and T5, on the schematic diagram.

FM BANDS

Guillotine tuners T2, T5, and T4 are used as the tuned circuits for the r-f amplifier, converter, and local oscillator respectively, in both FM bands. In the higher frequency band, the tuner is used with only a small shunt trimmer for adjusting distributed capacity. In the lower band, a higher value shunt trimmer is used to reduce the frequency. The layout of band switch, tuners, and tube sockets is arranged to give the shortest possible leads when the FM bands are in use. The lead length in the other bands is not nearly so critical.

SHORT-WAVE SPREAD-BANDS

Bandspread tuning in the short-wave bands is obtained in the converter and oscillator circuits by inserting the guillotine tuners in series with a higher inductance so that the two inductances together form the "L" part of the short-wave tuned circuit. The small percentage change in inductance obtained in the tuner provides smooth, wide, and stable tuning. The "C" part of the tuned circuit consists primarily of a shunt trimmer. Switching from one short-wave band to the other is accomplished by selecting a different shunt trimmer.

The converter grid circuit, as an example, includes L7 and T5 in series in both the SW1 and SW2 bands. Tuner T5 is in the ground end of the circuit and the signal is fed into the grid and through C10. The shunt tuning capacity is either C56 or C57, depending upon which of the two short-wave bands is used. Additional oscillator coupling capacitors, C72 or C73, are also added to compensate for the lower coupling through C67 when the higher shunt capacitors are in the circuit.

In the r-f stage, a section of the loop is used as the grid circuit. It is tuned for resonance by a shunt capacitor (C54 and C55) and a shunt inductance (L20). Because a tuned circuit of this type is inherently broad, tuning through the relatively narrow spread-band offers little advantage and is not done.

STANDARD BROADCAST BAND

When manual tuning is employed (Band Switch in STD position), the receiver employs an r-f stage, a converter, and an oscillator, all of which are tuned by iron slugs suspended from the tuning elevator. In the automatic position (Band Switch in the AUTO position), the r-f stage is not used. Instead, a separate antenna coil is used which couples the antenna and loop directly into the converter. A separate coil is used in order to make the tuning circuit independent of the dial tuning mechanism so that it may be tuned by trimmers in the push-button assembly.

Switching from manual to automatic tuning is accomplished in the oscillator by using an oscillator coil which is tuned by a separate shunt inductance. In manual tuning, the inductance is one which is tuned by the tuning elevator. In automatic tuning, a fixed shunt capacity (C-76) plus one of a series of push-button selected coils tunes the oscillator.

I-F AMPLIFIER

The i-f amplifier consists of a composite 455 kc and 10.7 mc circuit. The electrical changes required to transfer between AM and FM service are made by the Band Switch. When the switch is in either the FM1 or FM2 position, the amplifier operates at 10.7 megacycles and delivers the i-f signal into an FM discriminator circuit. When the switch is in any of the other positions, the amplifier operates at 455 kc. Screen voltage is removed from the tube which acted as an FM limiter and this tube then acts as an AM diode detector. Thus, the AM audio signal appears across R16 while the FM audio signal appears across R22. A section of the Band Switch switches the audio input circuit from one to the other. The AVC bus is also shorted out for FM.

STAGE GAIN AND VOLTAGE CHECKS

Stage gain measurements by vacuum tube voltmeter or similar measuring devices may be used to check circuit performance and isolate trouble. The gain values listed may have tolerances of 20%. Readings taken with low signal so that AVC is not effective.

(1) R-F and I-F Stage Gains

Signal applied through IRE dummy antenna:Antenna post to V1 gridAntenna post to V1 grid2 @ 9.6 mcAntenna post to V1 grid2 @ 11.8 mcSignal applied through 300 ohms, including signalgenerator impedance:Dipole terminals to V1 grid1.5 @ 45 mcDipole terminals to V1 grid2 @ 98 mc

:
@ 1000 kc
@ 9.6 mc
@ 11.8 mc
@ 45 mc
@ 98 mc
:
@ 455 kc
@ 10.7 mc
@ 455 kc
@ 10.7 mc
@ 455 kc
@ 10.7 mc

(2) Audio Gain

.07 volts at 400 cps across volume control with control set at maximum will give approximately $\frac{1}{2}$ watt output across the speaker voice coil.

(3) Oscillator Grid Bias

D-c	voltage	develop	ed across	R5	(av	erage	e):	
		@ 1000						8 mc
	2.7 v.	@ 9.6				v. @	45	mc
			7 v. @	98 n	nc			

(4) Socket Pin Voltages

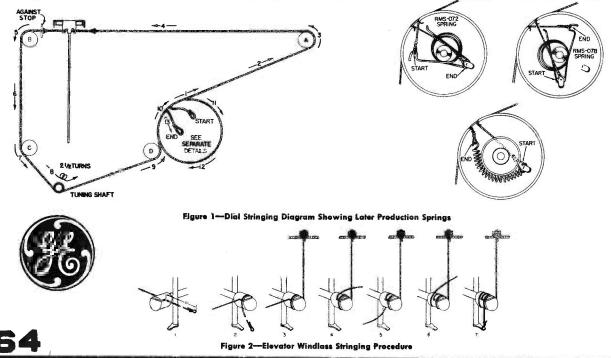
Fig. 8 shows typical tube pin voltages. All readings should be made from the pins to ground unless otherwise indicated.

REPLACEMENT OF DRIVE CORDS

DIAL STRINGING

Push the tuning elevator all the way down and string the dial as shown in Figure 1. This illustration shows the stringing as viewed from behind the dial scale, as you would see it when working on it. The numbers and arrows indicate the progression of the dial cord from start to finish. Notice that the dial cord, in progressive steps 9, 10, 11, and 12, is made to travel behind the start and end of cord stringing, as viewed in Figure 1. The procedure will be easier if pulley C is bypassed until the rest of the work is finished after which the cord can be pulled tight over that pulley. During the procedure, locate the two brass eyelets so that they fall between pulleys A and B. When finished, crimp the eyelets on the cord in the proper positions to act as minimum and maximum stops for the tuning mechanism and clip the pointer on the cable half-way between the eyelets.

Separate detail drawings are given to show the three different methods of attaching the ends of the cord. The arrangement with the standard helical spring was used in some earlier production receivers. If the cord and spring are to be replaced, the Type 1 spring should be used. It fits the same drum and is an improved type. The Type 2 spring should be used with the later type of drum (with two tabs).



When stringing the mechanism with either the Type 1 or Type 2 spring, load the spring by pulling the hook over the projection at the other end of the spring, string the dial and, as a final step, release the hook so that it pulls up the slack in the dial cord.

Elevator Stringing

The step-by-step procedure for stringing the elevator windlass is shown in Figure 2, a rear view of the mechanism. Start by inserting the metallic cord in slot as shown in Step 1. Observe that the cord is measured five inches from end of loop to where it enters the slot. Now bring the loop end around the pulley counterclockwise, as in Step 2. Next, thread loop through hole in elevator top plate, fastening it to the hoist cord tension spring, as viewed in Step 3. Steps 4, 5, 6, and 7 show how the free end of cord progresses on the pulley, going clockwise and that each turn is laid progressively one in back of the other and in back of the vertical section, going ito the tension spring in tuner plate. In Step 6, pass the free end of cord down through the hole in chassis, grasping its end with long-nosed pliers and drawing tension on cord while running elevator completely down to the bottom. Keeping the stord spring is compressed, complete Step 7 making a one turn loop of the cord's free end around the lug shown on end of elevator shaft and solder.

Concluding Comment

After replacing the dial cord or the elevator cord, it may be found that some correction in relative positioning is needed. This can be done by loosening the set screws in the large drive pulley directly behind the dial scale and re-positioning it on the shaft. The object, of course, is to permit the tuning control to drive the elevator through its full tuning range. Slight errors in final setting are not serious since leeway is provided in the location of the dial pointer itself.

WIRING OF BAND SWITCH

In order to facilitate repair, replacement, and circuit tracing, a table and diagrams are supplied with reference to the

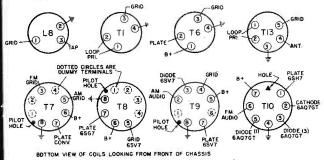
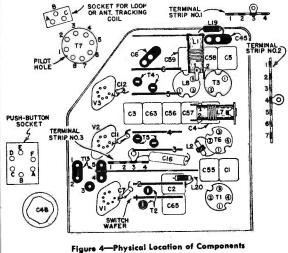


Figure 3—Terminal Identification of Coil Assemblies (Numbers correspond with schematic)

connections made in the band switch. If used properly, these will be of invaluable aid



Listed in Band Switch Wiring Table

The table is broken down into six parts, one for each switch wafer. Section 1 is nearest the front and section 6 is the rearmost wafer.

Individual lugs on each wafer are numbered from 1 to 12, depending upon their position on the wafer. The method of numbering is illustrated in Figure 5.

SECTION 1

At this lug—	connect this		-the other end of which is connected to this		
1		Insulated wire, 5" lg.	Antenna transformer T13, terminal 4		
2	a. b. c.	Insulated wire, 11 ½" lg. Insulated wire, 2" lg. Capacitor C50	Antenna terminal at rear of chassis Switch Section 1, lug 6 Switch Section 2, lug 1		
3		Capacitor C52	Switch Section 2, lug 3		
4	а. b. c.	Insulated wire, 1¼" lg. Insulated wire, 14" lg. Insulated wire, 5½" lg.	Antenna transformer T1, terminal 1 Beam-a-scope plug; terminal A Antenna transformer T13, terminal 2		
5	a. b.	Short bare bus Resistor R15	Ground lug on C65 Switch Section 1, lug 11		
6		See lug 2b, above			
7		Insulated wire, 11" lg.	Terminal strip 1, lug 4		
8		Capacitor C31	Front terminal of T2		
9	а. b.	Insulated wire, 9" lg. Insulated wire, 7" lg.	Terminal strip 2, lug 5 Filter capacitor, C46C		
11		See lug 5b, above			

SECTION 2

- <u>- 30 -</u> 1		
1	See Section 1, lug 2c	
3	a. Insulated wire, 21/2" lg. b. See Section 1, lug 3	Trimmer C1, lug nearer T1
4	Insulated wire, 11/2" lg.	Trimmer C55, lug nearer T1
5	Coil L20	Ground lug on trimmer C2
6	Short bare bus	Trimmer C65, left-hand terminal*
7	Short bare bus	Trimmer C2, left-hand terminal*
8	Capacitor C7	Tube socket V1, pin 1
9	Insulated wire, 4" lg.	Antenna transformer T13, terminal
10	Insulated wire, 31/2" lg.	Antenna transformer T1, terminal
11**	Insulated wire, 111/2" lg.	Beam-a-scope plug, terminal C

SECTION 3

	[
1	Shielded wire, 8%" lg.	Terminal strip 2, lug 6
2	Insulated wire, 11/2" lg.	Switch Section 3, lug 12
.3	a. Insulated wire, 2½" lg. b. Capacitor C16 c. Choke L3	Converter coil T6, terminal 1 Ground lug on terminal strip 3 Switch Section 3, lug 11
4	Insulated wire, 71/2" lg.	Terminal strip 2, lug 3
5	Insulated wire, 1 3/8" lg.	Converter coil T6, terminal 2
6	Short bus with spaghetti	Chassis
7	Short bare bus	Terminal strip 3, lug 4
10	Shielded wire, 101/2" lg.	Terminal strip 2, lug 2
11	a. See lug 3c, above b. Capacitor C10	Switch Section 4, lug 3
12	a. See lug 2, above b. Shielded wire, 7 ³ / ₄ " lg.	Push-button socket, terminal B

* Looking from front, chassis inverted. ** Double lug (front and rear) soldered together.

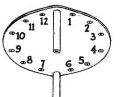
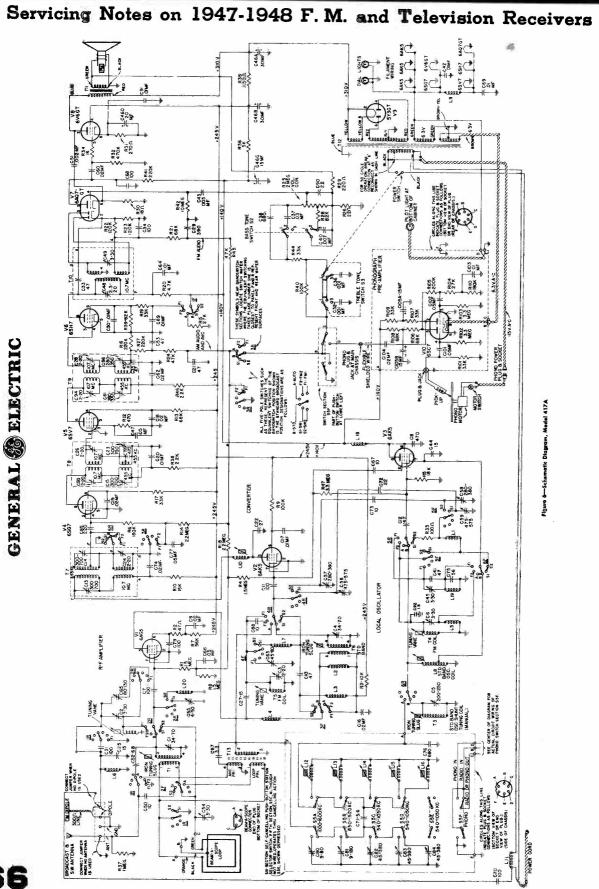


Figure 5—Identification of Switch Lugs —Set Inverted and Viewed from Panel



	Signal	Signal	Band	Dial		See	
Step	Generator Frequency	Input Point	Switch	Setting	Adjust	Note	Remarks
		and the Walt and and an an an and a state of the state of		FM IF ALIG	NMENT	<u>.</u>	
1	10.7 mc	6SH7 grid thru .01 mf	FM1		C49 for zero**	1, 2	Adjust C49 for zero meter reading Apply 1-volt signal input.
2	See last column	6SH7 grid thru .01 mf	FM1		Signal Generator	1, 2	Detune signal generator to point of maximum meter reading.
3	As in step 2	6SG7 grid thru .01 mf	FM1		Peak C48	1, 2	
4	10.7 mc	6SV7 grid thru .01 mf	FM1		Peak C28 & C94	1, 3	6AQ7GT tube removed from it socket.
5	10.7 mc	6SG7 grid thru .01 mf	FM1	and the African American	Peak C26 & C93	1, 3	6AQ7GT tube removed from it socket.
6	10.7 mc	Conv. grid directly	FM1	No P D J + 1 A MAR A	Peak C24 &	1, 3, 4	6AQ7GT tube removed from it socket.
	4			AM IF ALIG	NMENT		
7	455 kc	Conv. grid directly	STD		Peak C86 & C61	5,6	
8	455 kc	Conv. grid directly	STD	• • • • • • • • • • •	Peak C15 & C23	5, 6	
9	455 kc	Conv. grid directly	STD	••••••••••	Peak C13 & C14	5,6	
	l l	· · · · · · · · · · · · · · · · · · ·		FM RF ALIG		,	4
10	88 mc	DIPOLE terminals	FM2	88 mc—6.8 to 6.9 in.*	Peak C6**	1, 3, 7, 10	Set dial accurately—then adjust C(
11	98 mc	DIPOLE terminals	FM2	For max. out- put	Peak C3	1, 3, 8	Tune dial for maximum output, the peak C3 while rocking dial.
12	98 mc	DIPOLE terminals	FM2	Do not change	Peak C2	1, 3	
13	43 mc	DIPOLE terminals	FM1	43 mc—6 to 6.1 in.*	Peak C45**	1, 3, 7	Set dial accurately—then adjust C4
14	46 mc	DIPOLE terminals	FM1	For max. out- put	Peak C63	1, 3, 8	Tune dial for maximum output, the peak C63 while rocking dial.
15	46 mc	DIPOLE terminals	FM1	Do not change		1, 3	
16	11.8 mc	Antenna thru 400	SW2	SW RF ALIG	Peak C58	5, 6,	Set dial accurately-then adjust C5
10	11.8 mc	ohms	5w2	to 4.6 in.*	Frak Coo	5, 6, 7, 10	Set dial accurately—then adjust US
17	11.8 mc	Antenna thru 400 ohms	SW2	Do not change	Peak C57	5, 6, 8	Peak C57 while rocking dial.
18	11.8 mc	Antenna thru 400 ohms	SW2	Do not change	Peak C54	5, 6	C54 is located on back apron o chassis.
19	9.6 mc	Antenna thru 400 ohms	SW1	9.6 mc-4.5 to 4.6 in.*	Peak C59	5,6, 7,10	Set dial accurately—then adjust C5
20	9.6 mc	Antenna thru 400 ohms	SW1	Do not change	Peak C56	5, 6, 8	Peak C56 while rocking dial.
21	9.6 mc	Antenna thru 400 ohms	SWI	Do not change	Peak C55	5,6	
				BROADCAST RF			and the second
22	1620 kc	Antenna via 200 mmf	STD	Extreme right- hand position	Peak C5	5,6	
23	1620 kc	Antenna via 200 mmf		Extreme right- hand position	Peak C4	5, 6	· · · · · · · · · · · · · · · · · · ·
24	1620 kc	Antenna via 200 mmf	STD	Extreme right- hand position	Peak C1	5,6	
25	1500 kc	Antenna via 200 mmf	STD	1500 kc-1.4 to 1.5 in.*	Osc. Coil T3 iron slug	5, 6, 7, 9	T3 iron slug is the rear one on the left side. Adjust for peak.
26	1000 kc	Antenna via 200 mmf		For max. out- put	Conv. coil T6 iron slug	5, 6, 9	T6 iron slug is the center one on the left side. Adjust for peak.
27	1000 kc	Antenna via 200 mmf	STD	Do not change	R-F coil T1 iron slug	5, 6, 9	T1 iron slug is the front one on t left side. Adjust for peak.
28	580 kc	Antenna via 200 mmf	STD	For max. out- put	Peak L8	5, 6, 8	Peak L8 while rocking dial.
29							Repeat steps 22 to 28.

ALIGNMENT

EQUIPMENT REQUIRED:

- 1. Test Oscillator with tone modulation. (See Table.)
- 2. D-C Voltmeter or Microammeter. (See notes 2 and 3.)
- 3. A-C Voltmeter, 2 volts. (See note 6.)
- 4. Insulated hex wrench, $\frac{1}{4}$ ". (See steps 1, 10, 13.)
- 5. .01 MF Paper Capacitor. (See steps 1 to 5.)
- 6. 400-ohm, ¹/₂-watt resistor. (See steps 16 to 21.)
- 7. 200 mmf. mica capacitor. (See steps 22 to 28.)

Important detailed instructions and references in connection with the alignment table which follows are keyed in by means of column 7, headed "See Note." The notes are included in numerical order after the table. They are important —refer to them carefully.

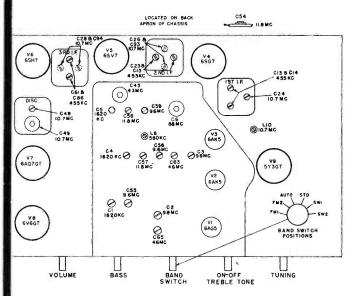
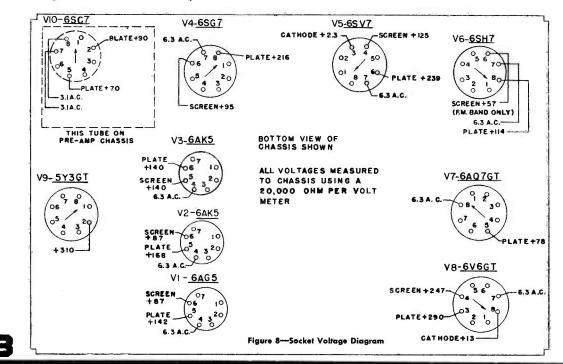


Figure 7-Location of Tubes and Adjusters

Notes in Connection with Alignment Table

- 1. Use unmodulated signal.
- Connect 20,000-ohm-per-volt meter from junction of R21 and C29 to chassis. Use ten-volt scale. (Steps 1-3.)
- 3. Connect 20,000-ohm-per-volt meter from grid pin 4 of 6SH7 to chassis with a 200,000-ohm resistor in series. The resistor must be connected directly to the grid so that capacity loading will be negligible and so that the meter is isolated from the i-f signal voltage. Keep signal generator output down so that the meter indicates not more than one volt at the grid (5 micro-amperes through 200,000 ohms). (Alignment steps 4 to 6, 10, to 15).
- 4. Connect signal generator directly to the converter grid at some convenient point. The generator lead must be shielded up to this connection so that not more than $\frac{1}{16}$ inch of exposed lead exists. Ground the shield solidly by clamping it firmly to the chassis or a shield as close to the connection as possible. (Steps 6-9.)
- 5. Use 400-cycle modulation. (Steps 7 to 9, 16 to 28.)
- Connect a standard output meter across speaker voice coil. Turn volume control fully on. Keep signal generator output down so that the meter indicates not more than ½-watt output (2 volts) during alignment. (Steps 7 to 9, 16 to 28.)
- 7. If dial scale is not available, index pointer as follows: Turn pointer to right-hand limit of travel. Mark the dial back plate at a reference edge of the pointer slider. Then set pointer by turning dial knob until the indicated dimension exists between the reference edge and the mark.
- "Rocking" consists of adjusting the indicated adjuster while turning the dial a small amount back and forth through peak output. The object is to find the maximum peak. Rocking is necessary and is permissible only when interlocking circuits are being adjusted.
- 9. The main tuning iron slugs are suspended from the left side of the tuning "elevator." They are individually adjustable by loosening the locknut and turning the supporting screw into which the suspending wire is soldered.
- 10. Two oscillator settings will give response. The higher frequency response point is the correct one; the other is the image. If in doubt, start with the trimmer screw loosened completely and adjust for the first response.





GENERAL 6 ELECTRIC

SERVICE DATA FOR **TELEVISION RECEIVER** MODEL 801

ELECTRICAL RATING:

Frequency	50/60 cps	60 cps
Voltage	105-125 v.	105-125 v.
Wattage (Radio)	85	85
Wattage (Television)	215	215

R-F FREQUENCY RANGE:

Selector Switch			Picture	Sound
Position	Fred.	Range	Carrier	Carrier
	particular in the local division of the loca	and the second second		Contraction of the Party of the
Radio			45.25	49.75
No. 1		50 mc 60 mc	45.25	49.75
No. 2		60 mc	61.25	65.75
No. 3		72 mc	67.25	71.75
No. 4		82 mc	77.25	81.75
No. 6		88 mc	83.25	87.75
No. 7		180 mc	175.25	179.75
No. 8.	180-	186 mc	181.25	185.75
No. 9.		192 mc	187.25	191.75
No. 10			193.25	197.75
No. 11		204 mc	199.25	203.75
No. 12			205.25	209.75
No. 13		216 mc	211.25	215.75
INTERMEDIATE FREQUENC				
Television Video (ca				
Television Audio				21.9 mc
Radio		£ + + + + + + + + +		455 kc
AUDIO POWER OUTPUT:				
Undistorted				
Maximum				.4.5 watts
TUBES: (24 including r	(arelificare)			
	-			Ture
Symbol	Purpo			Type 6AU6
(V 1) Television I (V 2) Television (7F8
(V 2) Television ((V 3) 1st Video I-				6AC7
(V 4) 2nd Video I				6AC7
(V 5) 3rd Video I				6AC7
(V 6) Video Deter				6H6
(V 7) Video Ampl				6AC7
(V 8) Picture Tub				10BP4
(V 9) Clipper-Hor	izontal S	Sync. Am	pli	6SN7GT
(V10) Horizontal				6SL7GT
(V11) Horizontal	Multivib	rator		6SN7GT
(V12) Horizontal				807
(V13) High Voltag	ge Rectif	ier		8016
(V14) Horizontal				6AS7G
(V15) Horiz, Disci				6SL7GT
(V16) Vertical Mu				6SN7GT
(V17) Vertical Ou				6V6GT
(V18) Radio Conv				6SA7
(V19) 1st Audio I				6SG7
(V20) 2nd Audio I				6SV7
(V21) Audio Discr				6AQ7GT 6V6GT
(V22) Audio Outp				5V4G*
(V23) Low Voltag				5U4G
(V24) Low Voltag				
* Changed to a Ty	pe 5Y3G	T in late	production	n receivers,

at approximately serial No. 2000.

LOUDSPEAKER:

Туре		Alnico	"PM" Dynamic
Voice Coil	Impedance (4)	00 cycles)	

MCTURE SIZE:

Height	 6 inches
Width	

ANTENNA REQUIREMENTS:

Type.....Folded Dipole

CAUTION NOTICE

THE REGULAR B + VOLTAGES ARE DANGEROUS AND PRE-CAUTIONS SHOULD BE OBSERVED WHEN THE CHASSIS IS RE-MOVED FROM THE CABINET FOR SERVICE PURPOSES. THE HIGH VOLTAGE SUPPLY (8000 v.) AT THE PICTURE TUBE ANODE WILL GIVE AN UNPLEASANT SHOCK BUT DOES NOT SUPPLY ENOUGH CURRENT TO GIVE A FATAL BURN OR SHOCK. HOWEVER, SECONDARY HUMAN REACTIONS TO OTHERWISE HARMLESS SHOCKS HAVE BEEN KNOWN TO CAUSE INJURY, SINCE THE HIGH VOLTAGE IS OBTAINED FROM THE B + VOLTAGE, CER-TAIN PORTIONS OF THE HIGH VOLTAGE GENERATING CIRCUIT ARE DANGEROUS AND EXTREME PRECAUTIONS SHOULD BE OBSERVED.

THE PICTURE TUBE IS HIGHLY EVACUATED AND IF BROKEN, GLASS FRAGMENTS WILL BE VIOLENTLY EXPELLED. IF IT IS NECESSARY TO CHANGE THE PICTURE TUBE, USE SAFETY GOGGLES AND GLOVES.

GENERAL INFORMATION

The General Electric Model 801 television receiver is a console type, 24 tube instrument providing reception of all 13 commercial television channels and radio reception in the standard broadcast band. The television picture is reproduced on a 10-inch electromagnetically deflected picture tube. All electrical components are mounted on a single chassis, permitting optimum case in adjustment and service.

Features of this television receiver include a constant input impedance r-f amplifier, ion trap, safe high voltage power supply, automatic frequency control for horizontal synchronization, ten-inch picture tube, and high fidelity FM audio system.

DESCRIPTION—TELEVISION CIRCUITS

The television receiver circuits are divided into the following sections:

- R-f amplifier, converter and oscillator 1.
- 2. Video and audio i-f amplifier
- Video detector and amplifier 3.
- 4. Sync pulse clipper-amplifier
- 5. Horizontal multivibrator and AFC sync.
- 6. Horizontal sweep output
- Vertical multivibrator and sweep output High voltage power supply (H.V. supply) Low voltage power supply (L.V. supply) 7.
- 8.
- Q.

A brief description of the operation of each section is described in the following paragraphs. This is supplemented by a comprehensive television training course in the publica-

tion, RSM-4-TV. A block diagram of the complete receiver is shown in block diagram of the complete receiver is shown in Figure 1 to assist in signal tracing and to better visualize the operation of the receiver as a whole.

1. R-F AMPLIFIER, CONVERTER & OSCILLATOR (See Figure 2)-The r-f amplifier makes use of a Type 6AU6 tube connected as a triode grounded-grid amplifier. The antenna is connected into the cathode circuit so as to provide a substantially constant input impedance of 300 ohms to the antenna at all frequencies. With a 300-ohm antenna and transmission line system, this coupling arrangement permits optimum transfer of signal from antenna to r-f amplifier for all 13 channels.

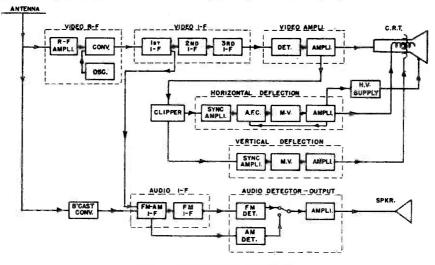


Fig. 1. Block Diagram, Model 801

R101 is the normal bias resistor. A choke, L_{K} , is placed in series with this cathode resistor to prevent the input impedance from being lowered by the shunting effect of the total stray capacity to ground of the cathode of the tube. The choke value is changed with frequency.

The r-f amplifier is coupled to the converter tube by a wide band transformer consisting of windings Lp and Ls.

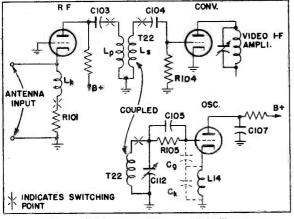


Fig. 2. R-f Amplifier, Converter & Oscillator

The windings are self-tuned by the distributed and tube capacities to provide optimum gain. On channels No. 1 and No. 2 the transformer is triple tuned to prevent the image frequencies of the 88-108 mc FM band from interfering with these two channels. The triode converter is one section of a Type 7F8 dual triode, V2A. Bias for this tube is provided by the oscillator voltage appearing in the grid of V2A causing grid rectification charging the grid resistorcondenser combination, R104 and C104.

The oscillator makes use of the remaining half of the Type 7F8 tube, V2B, and is inductively coupled to the converter grid by locating the oscillator grid coil, T22, on the same coil form as the converter grid coil, Ls. The oscillator is a modified Colpits oscillator, oscillation being produced by the cathode-to-grid, Cg, and cathode-to-plate, Ck, interelectrode capacities of the oscillator tube. The choke Lf provides a d-c ground to the cathode of the oscillator but maintains the cathode off-ground at the r-f frequencies. The oscillator operates on the high frequency side of the r-f signal on all bands.

The r-f amplifier, converter and oscillator is constructed as a complete unit sub-assembly which can readily be demounted from the main chassis. 2. VIDEO AND AUDIO 1-F AMPLIFIERS (See Figure 3)—The video i-f amplifier makes use of a three-stage band-pass amplifier using three Type 6AC7 tubes. The transformers, T1, T2, T3, and T4, are overcoupled and then loaded with resistance, RL, to give an adequate (approx. 4 mc).band-pass frequency characteristic. A third winding is added to each video transformer and tuned to trap out the adjacent audio and associated audio interference. The trap on T1 is tuned to 27.9 mc to provide rejection of the adjacent channel audio i-f, while the traps at T2, T3, and T4 are tuned to 21.9 mc to provide rejection of the same channel audio.

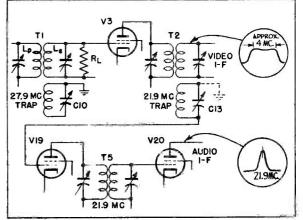


Fig. 3. Video & Audio I-f Amplifier

The audio i-f frequency is developed by taking the 21.9 mc signal from across the trap on T2 and applying it to the grid of the audio i-f amplifier tube V19. The ground return side of the trap is effectively connected to ground at 21.9 mc through the low impedance circuit offered by the capacitors C74 and C42. Since the audio channel of the television is frequency-modulated, the transformer T6 functions with the diode sections of V21 as the discriminator.

Bias voltage, derived by rectifying 6.3 volts a-c through the diode V6B, is applied to the grid circuits of the video i-f amplifier tubes, V3 and V4. A variable potentiometer contrast control, permits this voltage to be changed so as to vary the gain of the i-f amplifier.

3. VIDEO DETECTOR AND AMPLIFIER (See Figure 4)—The video if amplifier output is applied to a diode rectifier, V6, and the diode load, R14, is connected so as to develop a negativegoing signal voltage at this point. The signal is amplified by tube V7 and then applied directly to the cathode of the picture tube, V8. This provides direct coupling so that d-c reinsertion is unnecessary. The chokes L5 and L3 are series peaking chokes, while L4 is a shunt peaking choke. These are used to obtain good high frequency response. L5 also prevents harmonics of the i-f frequency from being passed through the video amplifier. R16 is the V7 tube plate load resistor.

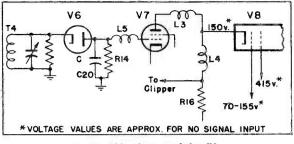


Fig. 4. Video Detector & Amplifier

With the cathode of V8 coupled directly into the plate circuit of V7, it is necessary to apply a variable positive voltage to the control grid of the picture tube in order to control the beam current and, therefore, the brightness of the picture. In late production receivers where the rectifier V23 is a Type 5Y3G tube, the cathode and control grid voltages of V8 will be approximately 25 volts less.

4. CLIPPER AND SYNC AMPLIFIER—The triode section, V9A, of a Type 6SN7GT tube is used to separate the sync pulses from the video signal taken off at the load resistor, R16, see Figure 4. This is accomplished by applying very low plate voltage to V9A, then the resulting grid rectification causes negative bias to be developed at the grid of V9A so that conduction occurs only during the sync pulse intervals which are the most positive component of the video signal. Tube V9B is a horizontal synchronizing amplifier which

Tube V9B is a horizontal synchronizing amplifier which rejects the vertical pulse at the transformer, TJ, by virtue of its low inductance to the vertical synchronizing pulse. The cathode impedance is required to raise the control grid to a positive voltage with respect to chassis for proper operation of V15B. The tube V15B is operated as a cathode follower vertical synchronizing amplifier. Integration of the vertical signal is provided in both the grid and cathode circuits.

5. HORIZONTAL MULTIVIBRATOR AND AFC SYNC (See Figure 5)— The horizontal sawtooth oscillator makes use of a Type 6SN7GT tube, V11, in a conventional cathode-coupled multivibrator circuit. Instead of its frequency being controlled directly by the horizontal sync pulses, it is controlled by a d-c voltage on its grid, which is the resultant of the phase error between the incoming sync signal and a sawtooth voltage derived from the output of the horizontal sweep amplifier. This voltage is called an automatic frequency control (AFC) voltage.

ampliner. This voltage is called an analysis of the diode-connected control (AFC) voltage is developed by the diode-connected triodes V10A and V15A by mixing the horizontal sync pulse at the secondary of transformer T7 with a sawtooth waveform derived at the output of the sweep amplifier. When the sync pulse occurs at the time "a" shown in the sawtooth waveform drawing in Figure 5, no voltage will be developed at the output of the filter. However if the multivibrator runs faster or slower so that the pulse falls at a point other than at "a," a positive or negative voltage will appear at the filter, which will be amplified by the d-c amplifier V10B and then

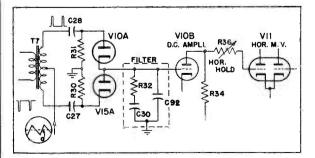


Fig. 5. Horizontal M.V. & Sync Circuit

applied to the grid of the multivibrator. This change in d-c voltage on the grid of the multivibrator will cause it to speed up or slow down so as to cause the sawtooth wave to combine with the incoming sync pulses until the correction voltage becomes zero. With the filter, consisting of C92, R32, and C30, the change is relatively slow in controlling the speed, permitting a synchronizing system which is relatively free from random noise triggering. The Horizontal Hold control, R36, controls the speed of the multivibrator, permitting the free-running speed of it to be set near the correct frequency during the time when no sync pulses are available.

6. HORIZONTAL SWEEP OUTPUT (See Figure 6)—The horizontal sawtooth voltage generated by the multivibrator, V11, is shaped and then amplified by a Type 807 tube, V12. The output of this tube is coupled to the horizontal deflection yoke through an impedance matching transformer, T9. An oscillatory voltage, as shown in the dotted line in the wave shape at the upper left of Figure 6, which results from the rapid retrace in transformer T9, is removed by the damping tube, V14. This tube is a triode Type 6AS7 and by its use the transient may be dampened, linearity controlled and the positive overshoot voltage retained for use in the high voltage supply. The linearity of the horizontal trace is controlled by varying the voltage wave shape applied to the grid of V14 by potentiometer R49. The horizontal size is varied by the adjustable iron core inductance, L7, which is in series with the output to the yoke.

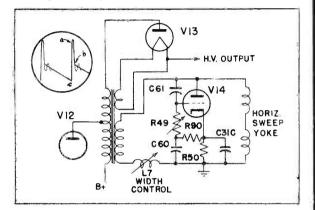
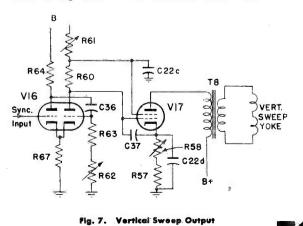


Fig. 6. Horizontal Sweep Output

7. VERTICAL MULTIVIBRATOR AND SWEEP OUTPUT (See Figure 7)— The vertical sawtooth voltage is generated by a Type 6SN7-GT tube, V16, connected as a multivibrator. This voltage is coupled directly to a Type 6V6G vertical sweep output tube, V17, and then to the vertical sweep yoke through the impedance matching transformer, T8. Vertical speed is controlled by changing the time constant of the multivibrator grid circuit by the potentiometer, R62. Sweep size is changed by the potentiometer, R61, which changes the B + voltage applied to the charging network of tube V16 simultaneously with the screen voltage on tube V17. Vertical linearity is controlled by feeding back voltage through C37 from the cathode to grid of the output tube. The amount of the voltage is varied by the variable cathode resistor, R58.

8. HIGH VOLTAGE SUPPLY (See Figure 6)—The high voltage is derived by making use of the inductive "kick" voltage produced during retrace in the horizontal output transformer



This "kick" voltage is shown in the wave shape shown as a-b in Figure 6. This voltage is generated in the primary winding and is further increased by an additional winding added to the transformer which connects to the rectifier tube plate of V13. The rectifier tube, V13, is a Type 8016 which derives its filament voltage from the horizontal sweep transformer T9 by a single turn around the transformer. Because of the high frequency which is rectified, a 500 mmf capacitor is more than sufficient for filtering purposes.

9. LOW VOLTAGE POWER SUPPLY-Two rectifiers are used to supply the required plate current for the television and radio receiver. A Type 5U4G tube, V24, supplies the bulk of the current and makes use of combination inductive and resistance type filter. A Type 5V4G or 5Y3G tube, V23, is used to supply higher voltage to the horizontal output, horizontal multivibrator, and the cathode ray tube 1st anode. This is followed by a choke filter. All filament supply leads except for tubes V19, V20, V21, V22 and the rectifier filaments pass through the band switch so that tubes may be switched ON or OFF when switching from radio to television.

CIRCUIT ALIGNMENT

GENERAL-A complete alignment of the Model 801 television receiver consists of the following individual alignment pro-cedures. These are listed below in the correct sequence of alignment. However, any one alignment may be performed without the necessity of realignment of any one of the other sectional alignments.

- Broadcast i-f amplifier 1.
- 2. Broadcast r-f amplifier
- 3. **Television** i-f traps
- Television sound i-f amplifier 4.
- 5. Video i-f amplifier
- Oscillator adjustments 6.
- Television r-f amplifier

The alignment procedure is in table form on pages 8 through 11. The following paragraphs are important suggestions to be followed when attempting alignment and should be read thoroughly before alignment is attempted.

TEST EQUIPMENT REQUIREMENTS-To provide the over-all alignment as outlined above, the following test equipment is required.

Cathode Ray Oscilloscope-This scope should preferably 1. have a 5-inch screen and should preferably have good high frequency response, which will be useful in making waveform voltage measurements on pages 20 and 21. 2. Signal Generator—This signal generator must have good

frequency stability and be accurately calibrated. It should be capable of covering the following frequency ranges with tone. modulation where desired.

- (a) 455 kc for broadcast
 (b) 550-1600 kc for broadcast
- 21.9 mc for video i-f trap (c)
- (d) 27.9 mc for video i-f trap
- 23.0 mc for video i-f marker (e)
- 25.65 mc for video i-f marker (f)
- 26.4 mc for video i-f marker (g)
- 44-110 mc and 174-238 mc for oscillator adjustment (h) and markers for the r-f channel bandwidth measurements.

R-F Sweep Generator-This should give approximately 3. 0.1 volt output with adjustable attenuation of the output. The output should be flat over wide frequency variations. The frequency coverage should be:

- a) 20 to 30 mc, with 10 mc sweep width
- (b) 40 to 90 mc, with 25 mc sweep width
- (c) 170 to 220 mc, with 25 mc sweep width

Output Meter-An output meter with a voltage range 0-2.5 volts a-c.

ALIGNMENT SUGGESTIONS—With the exception of the broad-cast i-f and r-f trimmers and the FM sound i-f discriminator trimmers, all alignment adjustments are performed from the underside of the chassis. Remove the chassis from the cabinet and turn it on its side with the power transformer down. This is the only safe position in which the chassis will rest and leave all adjustments accessible. The following suggestions apply to each individual alignment procedure.

1. Broadcast I-F Alignment-(a) Although the oscilloscope is recommended in the table for indicating the output voltage during alignment, an output meter may be connected across the speaker voice coil as an alternate output indicating device. When this is used, the volume control should be set for maximum volume and then attenuate the signal generator output so as not to cause audio overload.

(b) Use a 200 mmf mica capacitor or standard RMA dummy between the high side of the signal generator and the signal input point, as indicated in the Alignment Table. 2. Broadcast R-F Alignment—Apply signal generator input

to one of dipole input terminals through a 200 mmf mica capacitor as in (1) above. An output meter may be used in place of the oscilloscope for indicating output. First adjust oscillator trimmer by tuning gang condenser to minimum capacity and aligning oscillator trimmer for maximum with a 1620 kc input signal. Next with 1500 kc input signal, tune in signal, set pointer to 1500 kc calibration then align r-f trimmer for maximum output.

3. Video I-F Trap Alignment-The video i-f traps are used to attenuate the sound i-f of the same and adjacent channels from being detected and reproduced as sound bar interference on the picture tube. Misalignment of these traps results in the interference pattern, as shown in Figure 31.

Set the contrast control about half-way up. Turn the Station Selector to channel 13. Connect the oscilloscope through a 10,000-ohm resistor, to the top of the 3300-ohm video load resistor, R16.

Connect the output of an accurately calibrated signal generator with tone modulation to the grid of the converter tube, V2A, through a 200 mmf mica capacitor. The alignment frequencies are:

- T1 (C10)-27.9 mc T2 (C13)-21.9 mc T3 (C16)-21.9 mc T4 (C19)-21.9 mc

The trimmers should be aligned for minimum output, care being taken to get the lowest possible indication at the output. The input signal should be attenuated below saturation of the i-f amplifier tubes at start, then raised as signal is at-

the prime of the second For alignment, connect the oscilloscope through a 100,000 ohm isolating resistor across capacitor C49.

For store 1, insert a 21.9 mc marker signal from an un-modulated signal generator into the same point of input as the sweep generator. This input from the signal generator should be very loosely coupled by clipping the signal gen erator through insulation to the grid (4) of V3.

Keep the input of the sweep generator low enough so that the sound i-f amplifier does not overload. Check by increasing the output of the sweep; the response curve on the scope should increase in size proportionally. Set Contrast Control to half-advanced position.

The response curve of the amplifier at the grid return of V20 should appear as in Figure 8A.

For discriminator alignment the secondary trimmer, C78, of T6 is aligned by using a tone modulated 21.9 mc signal and listening to the tone at the loudspeaker. The trimmer is adjusted for minimum tone signal output. If the sweep is used for the secondary trimmer alignment, the cross-over should be symmetrical about a 21.9 mc marker and should be a straight line between the alternate peaks, as shown in Figure 8B. Reconnect oscilloscope across the top of the volume control.

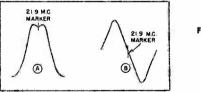


Fig. 8. T-V Audio I-F Curves

With the same sweep input as in step 1, adjust the primary trimmer, C84, of T6 for maximum peak-to-peak amplitude

5. Video I-F Alignment—The video i-f amplifier uses transformers which are coupled and loaded to give the proper band-pass characteristic. Before attempting alignment of the video i-f, the sound i-f traps should be aligned as in (3), then do not touch these trimmers when making the video i-f alignment.

Stage-by-stage alignment should be performed so as to duplicate the curves, as shown in Figures 9A, B, C, and D. The markers are used to establish the correct bandwidth and frequency limits.

The trap formed by L20 and C89 in the cathode of V4 is used to reduce the overshoot of the 21.9 mc traps. Adjust the spacing of turns comprising L20 by either pushing them together or separating them so as to give a minimum amplitude to the overshoot.

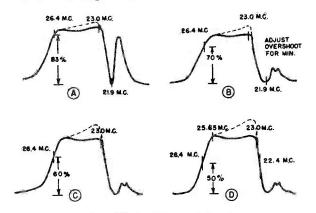


Fig. 9. Video I-F Alignment Curves

Connect the sweep generator to the tube grid preceding the transformer to be aligned. Adjust the sweep width for a minimum of 10 mc about the center frequency of the video i-f. The marker frequencies are supplied by a signal generator and sufficient marker signal may be supplied in most cases by merely connecting the high side of the signal generator to the television chassis.

The primary of the transformer preceding the grid where the signal is applied will act as a trap putting a hole in the alignment curves as viewed on the scope unless it is short circuited or detuned. It may be detuned readily by connecting a 100 to 200 mmf capacitor across the primary trimmer or place a temporary short circuit across the primary trimmer. Be sure to remove this capacitor after the stage is aligned.

Keep the input of the sweep generator low so as not to overload the video i-f amplifier.

The response curves shown are obtained on an oscilloscope at the junction of L4 and R16. Use a 10,000 resistor in series with the input lead to the oscilloscope.

The contrast control should be advanced approximately to its half-advanced position.

The Selector Switch should be turned to radio position and a temporary jumper put across filament switch wafer so as to keep the television tube filaments lit while in this radio position. If a television position is used, the i-f curve will be affected by the interaction from the r-f coil in the converter tube grid. NOTE—When jumper is used, remove B+ from r-f assembly by disconnecting external lead to terminal (2) of r-f assembly, see Fig. 12. 6. Oscillator Adjustment—The oscillator coil must be ad-

6. Oscillator Adjustment—The oscillator coil must be adjusted so that the Television Tuning Condenser, C112, will tune the sound carrier of the television signal at the middle of its range. Set the condenser, C112, to mid-position. Then adjust oscillator coil for channels No. 1 through No. 6 by spreading turns to raise frequency or compressing turns to lower frequency. For channels No. 7 through No. 13, the oscillator coil consists of a single turn. Adjust these coils by spreading the gap to lower frequency or closing the gap to raise frequency in the leads of the coil which run to the terminals.

Apply the signal generator with tone modulation to the antenna input terminals and set the generator to the sound carrier frequency for the channel under alignment. The signal generator must be very accurately calibrated. This can be done by beating its output against a known channel carrier or use a station operating on the channel and tune in the sound.

For output indication, advance the volume control about to mid-position so that the tone modulation or audio modulation on the channel station may be heard through the loudspeaker.

The oscillator coil is located on the coil form or assembly nearest to the front of the switch assembly and is wound of heavier wire than the other coils. This is shown in Figure 10. 7. R-F Coil Alignment—The r-f coil assembly is designed for stable, band-pass operation and under normal conditions will seldom require adjustment. In cases where it is definitely known that alignment is necessary (such as when the present coil is damaged and has been changed), do not attempt the adjustment unless suitable equipment is available. When tubes V1 or V2 are changed, alignment of r-f and oscillator may be necessary.

The minimum requirements for correct r-f alignment is to provide the correct band width, and for the response curve to be centered within the limit frequencies shown for each of the individual bands, as shown in Figure 11. It is also necessary that the curve be adjusted for maximum amplitude consistent with correct band width. To provide these minimum requirements, the r-f coils are overcoupled in a very similar manner to the video i-f transformers. However, instead of adjusting capacity to tune the coils, the inductance is varied by moving a few turns. Coupling is also adjustable by moving the entire coil either away from or toward the adjacent coil on the form.

The physical assembly of the coils in the band switch locates the r-f amplifier plate coil at the rear of the switch and the oscillator coil towards the front end. Two types of coils are used—the Channel No. 1 and No. 2 coils have an additional link circuit between the grid and plate coils to provide better image rejection of the FM band (88 to 108 mc) signals on these two channels. These links are tuned by means of two copper rings which are moved along the coil forms for adjustments.

The input sweep signal is applied to the antenna terminal board at the r-f unit. The 300-ohm cable between the antenna terminal board and r-f amplifier input must be disconnected at the r-f unit when making r-f alignment. The marker signal

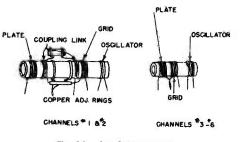


Fig. 10. R-F Coil Assembly.

generator may be coupled loosely to the antenna input terminals.

The output r-f response curve is taken off at the junction of R1 and C1. The Contrast Control should be set for minimum for all r-f alignment.

For channels No. 1 and No. 2, the r-f coil should be aligned to give approximately the curve shown in Figure 11A. The high frequency end of curve (at S marker) may be peaked slightly higher than the low frequency end of curve, but the 'ow frequency end should never be aligned with more amplitude than the high frequency end. The markers should be located on the inside of the humps of the curves, the video marker (P) preferably being inside slightly farther than the sound marker (S). Adjustment of the bandwidth is made by moving the plate coil closer to the grid coil or vice-versa. In most cases the sliding of the copper rings will give both the required bandwidth and frequency adjustment. Spread

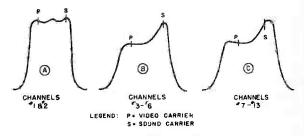


Fig. 11. R-F Alignment Curves

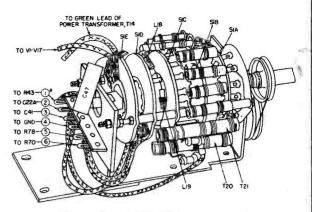
or squeeze turns in plate and grid coils if the frequency cannot be obtained by sliding the rings. Spreading turns results in a raising of the frequency; while squeezing turns lowers the frequency.

For the remainder of the channels, the adjustment of the plate coil in relation to the grid coil changes the bandwidth while the spreading or squeezing of the plate and grid coil turns results in the raising or lowering of frequency. Only when the plate and grid coils are tuned to the same frequency will the amplitude be greatest with the correct bandwidth. The outside peaks of the r-f response curve should be aligned to the carrier markers. In general it is desirable to have a slight rise on the high frequency (sound carrier) side of the curve, however the rise should not exceed approximately 30

per cent of the low frequency side. A low frequency rise in the response curve is not desirable and must be avoided, as a picture with poor definition will result if this is done.

The upper channel coils (No. 11, No. 12, and No. 13) may have the plate winding reversed from the winding direction of the plate coil of the other transformers. If this is the case, the bandwidth will be increased by separating the plate and grid coils and vice-versa. This condition can be determined by inspection or by the effect on the curve when mak ing the alignment.





* TERMINAL () NOT USED ON EARLY PRODUCTION RECEIVERS.

Fig. 12. R-F Coil & Switch Assembly

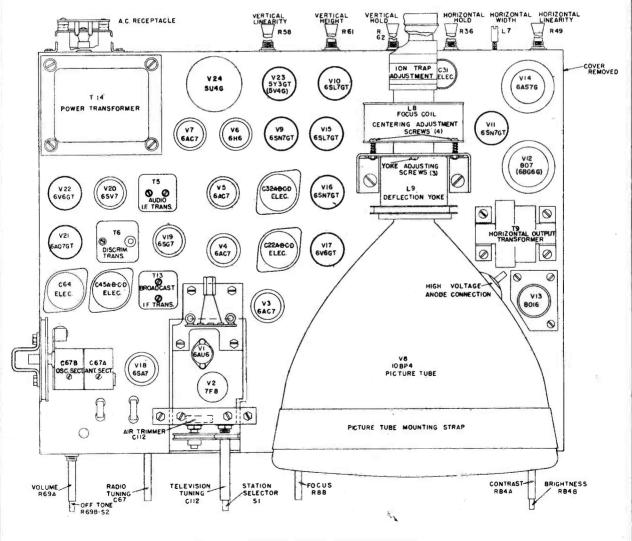
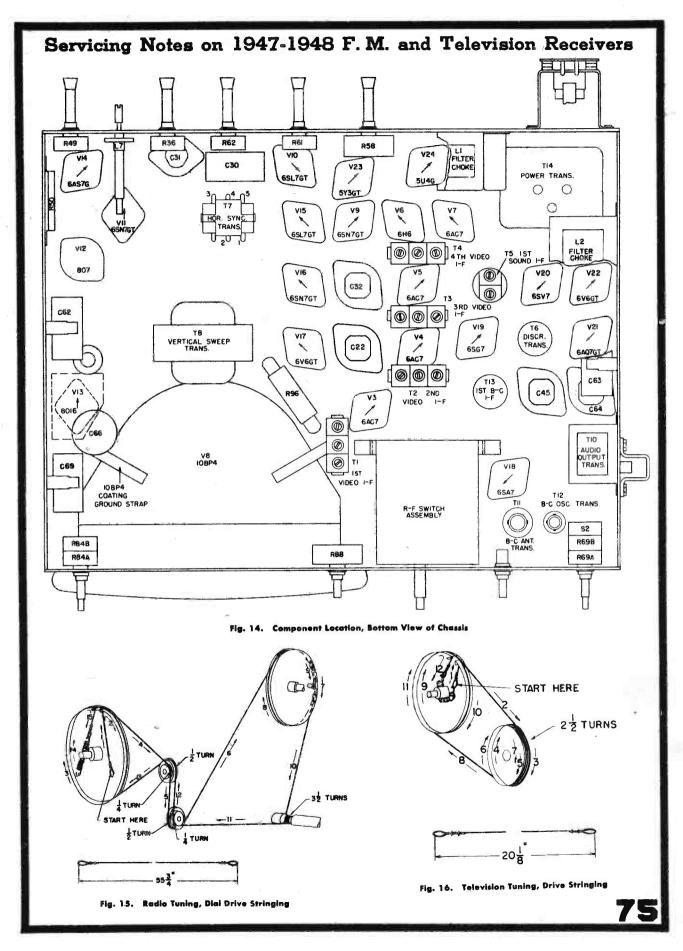


Fig. 13. Component Location, Top View of Chassis



Servicing Notes on 1947-1948 F. M. and Television Receivers ALIGNMENT TABLE

REMARKS	ADJUST	DIAL SET- TING	STATION SELECTOR SWITCH	CONNECT OSCILLO- SCOPE TO CHASSIS &	SIGNAL INPUT POINT	SWEEP GENERA- TOR FRE- QUENCY	SIGNAL GENERA- TOR FRE- QUENCY	STEP NO.
		MENT	AST I-F ALIGN	(1) BROAD				
Ē.	C75 & C76 for max. output	550 kc	Radio	Junction C41 & R69A	Grid (4) of V19 thru 200 mmf		455 kc with tone modulation	1
	C73 & C74 for max. output	550 kc	Radio	Junction C41 & R69A	Grid (5) of V18 thru 200 mmf		455 kc with tone modulation	2
n ann an transfer Chaine Arra	•	IMENT	AST R-F ALIGN	(2) BROADO			<u>1., </u>	- 40 - 16 - 1
* Tune gang condense minimum capacity settir	C67B osc. trimmer for maximum output	*	Radio	Junction C41 & R69A	Ant. terminal thru 200 mmf	·	1500 kc with tone modulation	1
** If pointer does not fa the 1500 kc calibration w 1500 kc signal is tuned slip pointer drum on cord until it does.	C67A r-f trimmer for maximum output	1500 kc**	Radio	Junction C41 & R69A	Ant. terminals thru 200 mmf		1500 kc with tone modulation	2
		GNMENT	I I-F TRAP ALI	(3) TELEVISIO			<u> </u>	a an an air an air an air an an air an
Connect 10,000 ohms series with oscilloscope in lead.	C19 on T4 for minimum output	i,	Channel #13	Junction L4 & R16	Grid (8) of V2A thru 200 mmf		21.9 mc with tone modulation	1
	C16 on T3 for minimum output	1 5	Channel #13	Junction L4 & R16	Grid (8) of V2A thru 200 mmf		21.9 mc with tone modulation	2
	C13 on T2 for minimum output		Channel #13	Junction L4 & R16	Grid (8) of V2A thru 200 mmf		21.9 mc with tone modulation	3
	C10 on T1 for minimum output		Channel #13	Junction L4 & R16	Grid (8) of V2A thru 200 mmf	Not Used	27.9 mc with tone modulation	4
	łT	ALIGNMEN	I-F AMPLIFIER	EVISION SOUNI	(4) TEL	<u>k</u>	anna an	<u>, 10</u>
Detune C84 on T6; then just trimmers C79 and Adjust for max. ampli and symmetry about mc marker as shown in 8A.	C79 & C80 for max. amplitude and symme- try at 21.9 mc		Channel #13	Junction of R77 & C49	Grid (4) of V3	21.9 mc with 2 mc sweep width	21.9 mc unmodulated	1
With volume control l way up and speaker nected, adjust C78 for n mum tone output.	C78 for mini- mum tone output		Channel #13		Grid (4) of V3		21.9 mc with tone modulation	2-
Peak trimmer so that positive and negative p have max. peak to p amplitude. See Fig. 8B.	C84 for max. peak to peak amplitude	-	Channel #13	Junction of C41 and R69A	Grid (4) of V3	21.9 mc with 2 mc sweep width	Not Used	3

4 Repeat steps 2 and 3.

75

				ALIGNMEN	TABLE				
TEP IO.	SIGNAL GENERA- TOR FRE- QUENCY	SWEEP GENERA- TOR FRE- QUENCY	SIGNAL INPUT POINT	CONNECT OSCILLO- SCOPE TO CHASSIS &	STATION SELECTO SWITCH	R	DIAL SET- TING	ADJUST	REMARKS
		<u> </u>	,,	(5) VIDEO 1-F	AMPLIFIER	ALIG	NMENT		
1	23.0 mc 8 26.4 mc marker	20-30 mc sweep	Grid (4) of V5	Junction of L4 and R16	Channel	#13		for max.	Shunt C14, T3 primary trim mer with a 100 mmf capaci tor. See Fig. 9A.
2	23.0 mc & 26.4 mc marker	20-30 mc sweep	Grid (4) of V4	Junction of L4 and R16	Channel	¥13		C14 and C15 for max. amplitude, bandwidth, and correct positioning of markers.	Remove 100 mmf capacito from C14, and shunt C11, T primary trimmer, with it See Fig. 9B.
3	23.0 mc 8 26.4 mc marker	20-30 mc sweep	Grid (4) of V4	Junction of L4 and R16	Channel	#13		Adjust L20 for minimum overshoot	See Fig. 9B. Either spread of squeeze turns together of give minimum aniplitude overshoot.
4	23.0 mc bs 26.4 mc	20-30 mc sweep	Grid (4) of V3	Junction of L4 and R16	Channel	#13	_	C11 and C12 for max. amplitude, bandwidth, and correct position of markers	Remove 100 mmf capacito from C11 and shunt C8, T primary trimmer, with See Fig. 9C.
5	23.0 mc & 26.4 mc	20-30 mc sweep	Grid (4) of V3	Junction of L4 and R16	Channel	#13		Readjust L20 for minimum overshoot	See Fig. 9 C. Repeat pr cedure as in step 3, exce for point of signal input.
6	23.0 mc, 26.4 mc, & 25.65 mc	20-30 mč swecp	Grid (8) of V2A	Junction of L4 and R16	Radio*			C8 and C9 for max. amplitude, bandwidth, and correct position of markers	Remove 100 mmf. capacit from C8. See Fig. 9D. * Jump filament wal switch with clip lead so th tube filaments will be lit. F move B+ from r-f assemb
			1	(6) OSCILL	ATOR COIL	ILDA	ISTMENT		

	-	the state of the second st				1			
~	49.75 mc with tone modulation		Antenna terminals		Channel	#1		coil. T20.	Make sure that C112 is at mid-position of travel. Use sound output as indicator.
	59.75 mc with tone		Antenna terminals		Channel	#2	dan stiller	Turns of osc. coil, T21.	Same as for Step #1.
3	modulation 65.75 mc with tone		Antenna terminals	<u>ii aa</u>	Channel	#3		Turns of osc. coil, T22.	Same as for Step #1.
4	modulation 71.75 mc with tone		Antenna terminals		Channel	#4	-	Turns of osc. coil, T23.	Same as for Step #1.
5	modulation 81.75 mc with tone	-	Antenna terminals	_	Channel	#5		Turns of osc. coil, T24.	Same as for Step' #1.
б	modulation 87.75 mc with tone		Antenna terminals	_	Channel	# 6		Turns of osc. coil, T25.	Same as for Step #1.
7	modulation 179.75 mc with tone modulation	-	Antenna terminals		Channel	# 7	-	Lead gap of oscillator coil, T26.	Same as for Step #1.
		3	L	1		- Alexandre			

TEP NO.	SIGNAL GENERA- TOR FRE- QUENCY	SWEEP GENERA- TOR FRE- QUENCY	SIGNAL INPUT POINT	CONNECT OSCILLO- SCOPE TO CHASSIS &	SELEC	TOR	DIAL SET- TING	ADJUST	REMARKS
				(6) OSCILLATO	R COIL AI	JUSTN	IENT (Con	t'd)	5
8	185.75 mc with tone modulation	-	Antenna terminals		Channel	#8		Lead gap of oscillator coil, T27.	Same as for Step #1.
9	191.75 mc with tone modulation	_	Antenna terminals	-	Channel	#9		Lead gap of oscillator coil, T28.	Same as for Step #1.
10	197.75 mc with tone modulation	-	Antenna terminals		Channel	#10	-	Lead gap of oscillator coil, T29.	Same as for Step #1.
	203.75 mc with tone modulation	-	Antenna terminals	-	Channel	#11	-	Lead gap of oscillator coil, T30	Same as for Step #1
	209.75 mc with tone modulation		Antenna terminals		Channel	#12	6	Lead gap of oscillator coil, T31.	Same as for Step #1
	215.75 mc with tone modulation		Antenna terminals		Channel	#13	:- <u>16</u> 00		Same as for Step #1
		1	<u> </u>	(7) R-F	COIL ALIG	3NMEN	17	1	L <u></u>
	Markers 45.25 mc & 49.75 mc	sweep		Junction R1 and C1	Channel	#1			See Fig. 11A for resultan alignment curve.
	Markers 55.25 mc & 59.75 mc	with 25 mc sweep	Antenna terminals at r-f amplifier	Junction R1 and C1	Channel	#2	-	For max.	See Fig. 11A for resultar alignment curve.
	Markers 61.25 mc 8 65.75 mc	sweep	Antenna terminals at r-f amplifier	Junction R1 and C1	Channel	#3	-	For max. amplitude and for recommended response	See Fig. 11B.
	Markers 67.25 mc & 71.75 mc	sweep	Antenna terminals at r-f amplifier		Channel	#4	-		See Fig. 11B for resultar alignment curve.
	Markers 77.25 mc & 81.75 mc	sweep		and C1	Channel	#5			See Fig. 11B for resultan alignment curve.
	Markers 83.25 mc 8s 87.75 mc				Channel	<i>#</i> 6			See Fig. 11B for resultan alignment curve.
	Markers 175.25 mc & 179.75 mc		Antenna terminals at r-f	Junction R1 and C1	Channel	#7			See Fig. 11C for resultan alignment curve.

				ALIGNMEN	TABLE	(CC	NT'D)		
STEP NO.	SIGNAL GENERA- TOR FRE- QUENCY	SWEEP GENERA- TOR FRE- QUENCY	SIGNAL INPUT POINT	CONNECT OSCILLO- SCOPE TO CHASSIS &	STATIC SELECT SWITC	OR	DIAL SET- TING	ADJUST	REMARKS
(<i>1</i> ,0),	, <u>1</u>	<u>, , , , , , , , , , , , , , , , , , , </u>		(7) R-F COI	L ALIGNME	NT (C	ont'd)		
8	Markers 181.25 mc & 185.75 mc	Channel #8 with 25 mc sweep	Antenna terminals at r-f amplifier	Junction R1 and C1	Channel	#8		For max. amplitude and for recommended response	See Fig. 11C for resultant alignment curve.
9	Markers 187.25 mc & 191.75 mc	Channel #9 with 25 mc sweep	Antenna terminals at r-f amplifier	Junction R1 and C1	Channel	#9		For max. amplitude and for recommended response	See Fig. 11C for resultan alignment curve.
10	Markers 193.25 mc & 197.75 mc	Channel #10 with 25 mc sweep	Antenna terminals at r-f amplifier	Junction R1 and C1	Channel	#10		For max. amplitude and for recommended response	See Fig. 11C for resultan alignment curve.
11	Markers 199.25 mc & 203.75 mc	Channel #11 with 25 mc sweep	Antenna terminals at r-f amplifier	Junction R1 and C1	Channel	#11		For max. amplitude and for recommended response	See Fig. 11C for resultan alignment curve.
12	Markers 205.25 mc 8 209.75 mc	Channel #12 with 25 mc sweep	Antenna terminals at r-f amplifier	Junction R1 and C1	Channel	#12	, manuar	For max. amplitude and for recommended response	See Fig. 11C for resultan alignment curve.
13	Markers 211.25 mc & 215.75 mc	Channel #13 with 25 mc sweep	Antenna terminals at r-f amplifier	Junction R1 and C1	Channel	#13	. Controller	For max. amplitude and for recommended response	See Fig. 11C for resultan alignment curve.

MISCELLANEOUS INSTALLATION AND SERVICE ADJUSTMENTS

REPLACEMENT OF PICTURE TUBE

To remove the picture tube from the television chassis, remove the picture tube socket and then untape and slide off the ion trap adjustment assembly. The ion trap can be removed readily, if the gap in the assembly is pulled apart slightly with the fingers while attempting to slide it. Loosen the two set screws partially that clamp the left side of the picture tube mounting strap, then slide the strap backward from the top-front rim of the picture tube until the rim of the tube is free from the strap. Carefully pull the tube out through the focus and deflection coils.

To replace a picture tube the reverse procedure should be followed, being careful never to force the picture tube if it sticks or fails to slip into place readily. Investigate and remove the source of the trouble. The picture tube should be oriented so that the anode cap is adjacent to the H.V. rectifier, V13, and the high voltage lead.

Wipe the screen surface of the tube to remove finger marks and dust. PRECAUTION-Do not handle, remove, or install a picture tube unless shatterproof goggles and heavy gloves are worn.

ION TRAP ADJUSTMENT

The ion trap may be approximately located as shown in Figure 17; however its final adjustment must be made with the television receiver operating.

The approximate adjustment requires that the gaps in the two magnets be lined up with the break in the rubber holder. NOTE—Some ion traps have been magnetized so that it is necessary to rotate the small magnet at 180 degrees to this normal position. Then slide the assembly onto the picture tube neck so that the ion trap assembly slit is at the bottom or top (dependent upon picture tube) and lines up with pin #12 or #6. Slide the assembly forward on the picture tube until it is about the position shown in the illustration. NOTE The wider of the two magnets should be located at the rear or the base end of the picture tube. The final following steps should be taken with the television receiver operating:

1. With Brilliance control advanced, turn ion trap assembly so that gap in rubber holder is faced up or down and lines up with either pin #6 or pin #12. Whichever way gives some illumination, is the correct approximate orientation of assembly. If the tube V16 is removed, it will be found much easier to adjust for maximum illumination since the resultant thin line will illuminate even though the magnets are considerably out of adjustment.

2. Move assembly back and forth and rotating it while viewing screen, adjust for maximum brightness.

3. If illuminated area gets very bright, reduce brightness with control and repeat step 2. If tube V16 was removed as suggested in Step 1, replace it before proceeding with step 4.

4. If any shadowing of the tube neck is present after completing step 3, rotate the small (front) magnet to correct shadow and repeat step 2 and 3. NOTE—Badly out-of-line focus coils can also cause neck shadowing. The focus coil should be symmetrical and straight before starting the ion trap adjustment.

CENTERING (FOCUS COIL) ADJUSTMENT

The four focus coil adjustment screws should all be tightened sufficiently so that the springs are always under tension. Too loose pressure on the springs will result in the picture centering being unstable. These adjustments are not readily available with the back cover in place unless a long screwdriver is used. Since each screw adjustment reacts in both the horizontal and vertical directions, a maladjustment in the centering may have to be corrected by the adjustment of one to four screws.

DEFLECTION YOKE ADJUSTMENT

Three set screws permit the deflection yoke to be loosened, permitting limited turning in either direction. If the picture does not line up horizontally or square with the picture tube mask, rotate the yoke until this condition is remedied, then tighten the set screws.

HORIZONTAL (HOLD) OSCILLATOR SPEED ADJUSTMENT

The horizontal hold control is a preset adjustment on the rear of the chassis which is used to adjust the speed. In late production receivers, a tuned circuit consisting of L21 and C91 was added to the horizontal oscillator cathode circuit to stabilize the horizontal hold operation. For complete alignment both controls must be adjusted. Check operation first as follows:

Check on Alignment—With a normal television signal being received, free from excessive noise, turn the horizontal hold control to the position where the picture locks in horizontally and passes the following tests:

1. With a picture being received, switch the Station Selector to a channel having no program and then back to the desired channel. The picture should immediately lock into position.

2. With a picture being received, turn the television receiver power "off" for two or three seconds and then turn it back "on" again. The picture should come into synchronization within ten seconds after the picture tube has been illuminated.

3. Turn the Station Selector to the "radio" position and allow the television receiver to transfer for two or three minutes to Broadcast reception, and then return to the television channel transmitting a picture. The picture should synchronize within ten seconds after the picture tube becomes illuminated with receivers not equipped with L21. Receivers with L21 should sync immediately upon showing raster.

4. Turn power off for three or four minutes and then turn "ON." The picture should lock-in horizontally within ten seconds after the raster becomes illuminated. Minor Adjustments—If the receiver does not have the tuned circuit consisting of L21 and C91 in the cathode of the horizontal multivibrator, V11, the horizontal hold control, R36, should be adjusted until the above checks can be satisfactorily accomplished. If attempted adjustment of the hold control will not permit all the above checks to be met when the tuned circuit is incorporated, then make the adjustment as outlined under "Complete Realignment."

Complete Realignment—Tune in a television signal for optimum sound and adjust for normal contrast.

1. Adjust the Horizontal Hold control to the center of its range.

2. Remove tube V9, and then adjust the iron core of L21 until the picture is approximately synchronized (held in frame) in the horizontal direction.

3. Replace tube V9 and then adjust the Horizontal Hold control until the picture passed all tests as outlined in "Check on Alignment."

VERTICAL (HOLD) OSCILLATOR SPEED ADJUSTMENT

This control, R62, is used to lock the picture in synchronism with the transmitted picture in the vertical direction. When the control is maladjusted the picture will slide vertically out-of-frame or lock out-of-frame, giving overlapping vertical images or even double images in the vertical direction. After the picture is locked in vertically on a normal picture, reduce the contrast control until the picture is barely visible, then readjust the control until the picture holds in frame.

HORIZONTAL LINEARITY AND WIDTH CONTROL

These controls react on each other so that when one control is adjusted the other may have to be. The adjustment of the linearity control should only be made on a test pattern signal. First, obtain the correct width by adjusting the width control, L7, until the picture extends approximately ½-inch outside the edge of the mask on both sides. Next, adjust the Horizontal Linearity control, R49, until the test pattern is symmetrical in the left and right direction. A slight readjustment of the Width control may now be necessary, as well as touching up of the centering adjusting screws.

VERTICAL LINEARITY AND HEIGHT CONTROL

The Height control, R61, is adjusted until the picture extends approximately $\frac{1}{2}$ inch outside the edge of the mask on both top_and bottom. Next, adjust the Vertical Linearity control, R58, until the test pattern is symmetrical from top to bottom. Readjustment of the Height and Vertical Hold controls as well as the centering adjustments may be necessary.

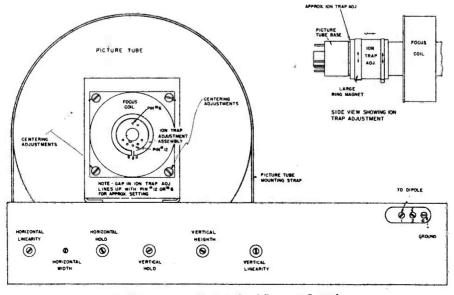


Fig. 17. Location of Installation Adjustment Controls

PRODUCTION CHANGES

The following production changes have taken place up to the time that this service data was compiled. In most cases the change can not be accurately identified with the serial number of the chassis. The order of listing below does not indicate the chronological order of the change.

1. Power Transformer, T14 and V23—The original transformer, T14, supplied, gave insufficient B+ voltage (385 volts) when using a Type 5Y3GT rectifier tube, V23. This resulted in a low anode voltage of 7500 volts for the picture tube. To increase this voltage, a Type 5V4G tube was substituted for the 5Y3G tube, V23. At approximately serial number 2500, a new transformer T14 having Stock No. RTP-040 was substituted, which gave the correct B + voltage of 415 volts when a Type 5Y3G tube was used as V23. This B + voltage gives an anode voltage to the picture tube of 8500 volts.

2. Television Tuning Trimmer C112—For approximately the first 2000 receivers, the tuning trimmer C112 did not quite have the correct tuning range, making it necessary to add a fixed 10 mmf. capacitor C114 in series with it. The shunt capacitor C102 had a value of 4.7 mmf. Later production trimmer, C114, has the correct range. With this new value of trimmer, the shunt capacitor C112 was changed to 6.0 mmf. This shunt capacitor in a few receivers was merely a 5.0 mmf., while in most it will consist of two capacitors; a 5 mmf. and a 1.0 mmf. capacitor in parallel. The early production trimmer has a $\frac{1}{4}$ -in. O.D. shaft, while the late production trimmer is slightly larger and has a $\frac{1}{16}$ -in. O.D. shaft.

3. Tone Control, R69B.—The tone control R69B, on early production receivers was connected in series between the Volume Control R69A, movable arm, and C39. C72 was a 680 mmf. capacitor from C39 to ground. Hum in the audio dependent upon the tone control setting necessitated a revision as shown in the schematic.

4. Tuned Circuit, L20 and C89—The capacitor, C89, was originally 240 mmf. and the coil, L20, was fixed-tuned and wound on a resistor form. This was later changed to 1000 mmf. and the coil turns were reduced and made variable, resulting in a higher Q circuit. This change permitted adjustment of the trap as described in the alignment procedure.

5. Resistor, R87—This resistor was changed from 100,000 ohms to 330,000 ohms to prevent excessive beam current in the picture tube, V8. This excessive beam current caused the high voltage to be reduced when the Brilliance control was advanced to maximum with the result that the control reduced brightness at end of its clockwise travel instead of increasing brightness.

6. Resistor, R47—This resistor has been changed from $\frac{1}{2}$ -watt to a 1-watt size. In some cases, the original $\frac{1}{2}$ -watt resistor dissipation is exceeded, especially if the Width control iron core is nearly all the way in the coil, resulting in a reduction in the resistance value. This reduced resistance changes the waveshape across G29 so much that the horizontal multivibrator may lock in at half frequency or not lock at all. It may also result in the resistor burning out.

7. Change in Horizontal Output Transformer, T9—A new design horizontal output transformer, T9, was used in late production receivers. This may be identified by the fact that it has two windings instead of the single winding design, as characterized the early production receivers. When the late production transformer is used, a 3900-ohm, 1-watt resistor, R47. Do not use a single I-wall resistor for this. The capacitor, C66, should be returned to ground when the new type transformer is used.

8. Horizontal Multivibrator Cathode Switching—After the first 150 receivers were built, a shorting contact was added to the filament wafer of the Station Selector switch so as to stop the horizontal multivibrator as soon as the Station Selector was switched to "Radio" position. This connects the multivibrator cathode to ground through the filament circuit when switching to "Radio" so that "birdies" are not heard on the broadcast band as the television tubes cool off after switching from television to radio reception.

9. Screen Resistor, R79—This resistor was changed from an original 47,000 ohms to 33,000 ohms. This reduces the operating d-c voltage on the plate of V7, and gives greater brightness.

10. Addition of C21—A fixed 10 mmf. mica capacitor, C21, was added across C10 so that the trimmer C10 would peak at the center of its range. 11. Change in R63—The 330,000 ohm resistor, R63, was changed to 220,000 ohms so that the Vertical Hold control will operate near its mid-adjustment position.

12. Removal of R95—To correct a transient which appeared in the vertical retrace as a white line at the top of the picture, the 2200 ohm resistor, R95, in series with capacitor, C37, was removed. The potentiometer, R58, was reconnected as a variable resistance as shown on the schematic.

13. Value Change of C52—The original capacity of C52 was 47 mmf. To improve vertical interlace, this capacitor was changed to 240 mmf.

14. Addition of Tuned Circuit, L21 and C91—A 15.75 kc tuned circuit was added to the cathode of the horizontal multivibrator, V11. This stabilizes the horizontal AFC circuit to the extent that it prevents picture wiggles on noise pulses and echoes. With this addition, the 240 $\mu\mu$ f capacitor, C56, should be changed to 150 mmf. and the 150,000 ohm resistor, R40, should be increased to 330,000 ohms. This prevents a white line at the left-center of the picture which may result with installation of L21-C91. With addition of L21, the capacitor, C30, was changed from a 40 mfd to a 1.0 mfd, and C92 was changed from 1.0 mfd to a .05 mfd.

15. Connection of Primary of T11—On early production receivers the primary of T11 was connected to a mid-tap on choke L10. This connection caused a resonant condition to develop which affected the lower television bands. This was corrected temporarily by shunting a 47 mmf. capacitor between the midtap of L10 and ground. Later the primary of T11 was connected to the junction of L10 and C101 as shown on the schematic.

50-CYCLE OPERATION

The supplement schematic diagram, Figure 18, shows the wiring of the power transformer, T14, through the special terminal board installed. Also, it shows the addition of capacitors C98 and C99 required for additional filtering. The changes involved in changing from 60-cycle to 50-cycle operation are listed below:

1. The 50-cycle power transformer, T14, is separated from the chassis and installed on a mounting plate at the base of the cabinet.

2. All filament and high voltage leads are extended on the transformer and terminated at the chassis proper in a terminal board. The connection of these leads through this terminal board is shown in Figure 18. All leads are twisted.

3. A 90 mfd. capacitor, C98, is shunted across C62. A 90 mfd. capacitor, C99, is shunted across C45-A.

4. The bias supply filter capacitor, C69, is changed to a 50 mfd. capacitor.

5. Filament leads to V6, V7, V9, V10, V11, V12, V14, V15, V16, and V17 are twisted. The ground connection is made at one point only for this series of tubes, and the high side is connected through the filament wafer of the band switch.

TROUBLE SHOOTING

The following is a listing of possible troubles and their cures. This is not intended as a comprehensive coverage of all possible failures but serves to point out some of the more difficult troubles that may be experienced. From time to time this information will be expanded as information becomes available.

I. NO RASTER ON PICTURE TUBE

(a) Ion trap adjustment incorrectly made. Assembly on backward or improperly oriented. See ion trap adjustment under "Miscellaneous Preset and Service Adjustments."

(b) Check for waveform at output of T9. If present, the trouble is probably in the Type 8016 rectifier tube or filter circuit. Check for open in high voltage winding of T9. If the V13 tube filament glows yellow, high-voltage is being generated and the trouble will possibly exist in the picture tube, V8.

(c) If there is no waveform at output of T9, check operation of 807, V12, V7, and multivibrator V11 by oscilloscope waveform measurement.

(d) Check that high voltage anode cap is contacting the anode terminal of V8.

NO RASTER ON PICTURE TUBE (Cont'd) ۲.

(e) Open Brightness control R84B, R87, or R85.

 (\mathbf{f}) No. B+ voltage at junction L4 and L3.

If only two or three thousand volts are generated, (g) check deflection yoke, L9, and Width control, L7, for continuity.

2. RASTER NORMAL, NO PICTURE OR SOUND

(a) Oscillator V2B defective, or oscillator coil resonates out of band.

(b) Defective antenna or lead-in.

Converter, r-f amplifier, or first video i-f amplifier (c) stage defective.

3. PICTURE NORMAL, NO SOUND

(a) 21.9 mc audio i-f amplifier, discriminator, or audio amplifier defective

(b) Oscillator V2B off frequency. (c) Defective speaker.

4. RASTER NORMAL, SOUND NORMAL, NO PICTURE

Video i-f amplifier (after 1st i-f) inoperative. (a)

(b) Resistor R83 in contrast control defective or open.

(c) Screen by-pass C32C open or shorted.

NORMAL PICTURE AND SOUND, NO HORIZONTAL OR VERTICAL 5. SYNC.

(a)Check for signal input waveform at grid (1) of V9A. Defective V9A or plate circuit components.

(b)

(c) Operation of receiver with Contrast control advanced too far.

6. PICTURE NORMAL, NO VERTICAL SYNC.

Check grid of V15B for normal waveform. (a)

Check speed of vertical multivibrator. Should be (b) capable of free running speed less than 60 cps. Check V15B circuit components. (c)

7. PICTURE NORMAL, NO HORIZONTAL SYNC.

- (\mathbf{a}) Check AFC transformer, T7.
- Check alignment of L21 and C91. (b)
- (c) Check socket voltages and waveforms of V10B and Viì.

(**d**) Check resistor R47 for correct value.

8. NO VERTICAL OR NO HORIZONTAL DEFLECTION

Check waveform and socket voltages of output and (a)multivibrator tubes of respective sweep circuits.

Check output transformer and yoke for continuity. (b)

9. ONE OR MORE HORIZONTAL WHITE LINES AT TOP OF PICTURE

Check for Production Change #12. (a)

10. RIPPLE ON EDGE OF PICTURE

Reflections on antenna lead-in. (a)

Instability of horizontal AFC circuit. See Production (h) Change #14.

(c) Defective capacitor, C30.

11. RASTER EDGE NOT STRAIGHT-KEYSTONING

- (a) Defective yoke.
- (b) Defective sweep transformer.
- (c) Improperly adjusted ion trap adjustment assembly.

12. PICTURE JUMPY

Operation at too high contrast control setting.

- (b) If picture moves at regular rate sideways, check capacitor C30, R32 and C92. Put in change #14.
 - If left of picture jitters, change 807 sweep tube, V12 (c)
 - Noisy sweep or sync circuit tubes. (d)

13. POOR INTERLACE OF VERTICAL SWEEP

(a) Check Production Change #13.

14. POOR PICTURE DETAIL

- Mismatch in antenna or lead-in. (\mathbf{a})
- Misalignment of i-f or r-f circuits. (b)
- Defective chokes L3, L4 or L5 in video amplifier, (c)
- Make sure that focus control operates on both sides (**b**) of proper focus point. (e) Overload of video amplifier, check contrast control

operation.

15. PICTURE CANNOT BE CENTERED

(a) Move focus coil back by loosening all four adjustment screws.

FOCUS CONTROL AT END OF TRAVEL 16.

- (a) Short out resistor R96. (b)
- Check for correct B+ voltages.

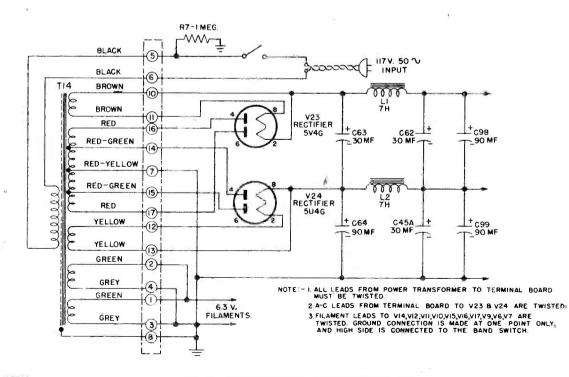
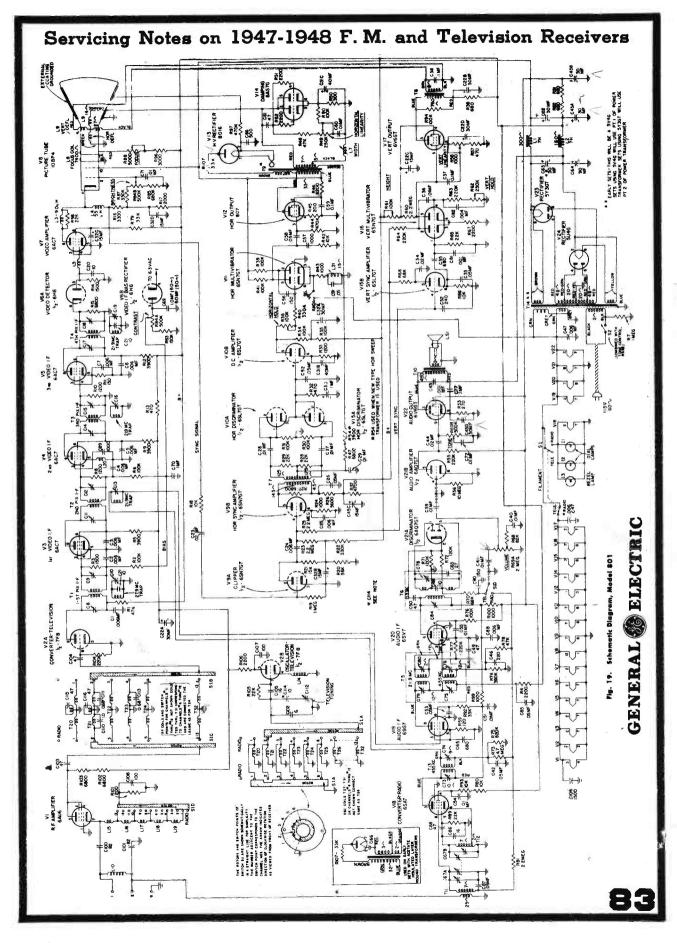


Fig. 18. Schematic Changes for 50-cycle Operation



Servicing Notes on 1947-1948 F. M. and Television Receivers SOCKET VOLTAGE CHART

.

NOTE—All d-c measurements taken by a 20,000 ohm/volt meter. Station selector switch at Channel No. 1 unless noted. Contrast control at maximum, Brilliance at minimum.

SYM-	TUBE	PL	ATE	SCI	REEN	CAT	HODE		RID	PLATE	SCREEN	NOTES
BOL	TYPE	PIN	VOLTS	PIN	VOLTS	PIN	VOLTS	PIN	VOLTS	M.A.	M.A.	
71	6AU6	5	140	6	140	7	1.3	1	0	7.2		
72A	7 F 8	6	115	_	<u> </u>	5	0	8	-4.5*	2.5		* Measured with V.T.V.M.
2 B		3	180	-		4	0	1	0	10	-	
73	6AC7	8	150	6	150	5	0	4	-2*	14	3	* Measured on 50 v scale
74	6AC7	8	160	6	160	5	0	4	-2*	15	3.2	* Measured on 50 v scale
75	6 AC 7	8	170	6	170	5	2	4	0	14 ,	3	
76A	6H6	5	0			8	0			4		
6 B		3	-8.5			4	6.3AC			0		
77	6AC7	8	150	6	125	5	0	4	0	15	3.7	
78	10 BP 4	CAP	8300*	10	415	n	150	2	90		-	* Use multiplier with 1000 scale
79A	6SN7GT	2	12.5	_	ž	3	0	1	-1	.2		
79B		5	110			6	11	4	6	10		
/10 A	6SL7GT	2	Dev_95			-3	0.5	1	-9.5	0		
710B		5	42.5	_	_	6	0.5	4	0.5	1	_	January and the second s
/11A	6 SN 7GT	5	170			6	ore	4	-25	2.5		
V11B		2	135	-		3	6	1	0	2.9	·	
V12	807	CAP	415	2	345e	4	22	3	-10	76	13	
V13	8016	CAP		-	-	2	8300*		-			* Use multiplier with 1000 scale
V 14	6AS7GT	2 86 5	0	-	_	3 86 6	5 10	1 86 4	-15	-		
V15A	6SL7GT	2	0.5	-	-	3	7.5	1	0.5	0	_	
V15 B	4	5	8 105	-		6	170	-4	904	1		
V16A	6SN7GT	2	8030	-	-	3	1.5	1	do	.7		
V16B		5	90 14.5			6	71.5	4	- <u>\$</u> 4.5	.1		
V17	6V6GT	3	195	180	135	8	23.5	5	914.5	20	1.85	
V18*	6 SA 7	3	200	4	80	8	0	6	0	3	8.5	
V19	6 S G7	8	200	6	110	5	1	4	0	10	4	
720	6 SV 7	6	195	4	88	2	-0.5	3	0	9.7	1.7	
V21A	6AQ7GT	1 85 3	3 0			2	0			0		
V21B		5	75			6	0	4	0	1		
V22	6V6GT	3	230	4	200	8	10	5	0	41.5	4.5	
V23	5Y3GT	4 86 (5 315AC			2	425	-		85*		* Cathode current
V24	5U4G	4 86 6	5 240AC	-		2	250		,	160*	<u> </u>	* Cathode current.

Servicing Notes on 1947-1948 F. M. and Television Receivers PICTURE MALADJUSTMENT OR INTERFERENCE

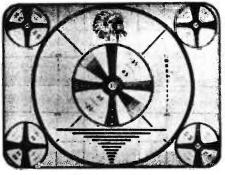


Fig. 20. Normal Picture

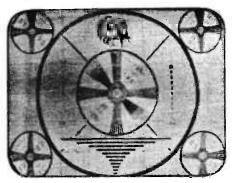


Fig. 22. Contrast Too Low, Brightness Too High

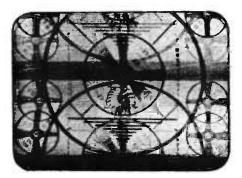


Fig. 24. Vertical Hold Control Misadjusted

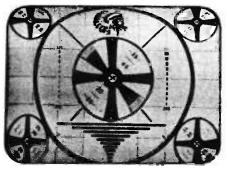


Fig. 26. Vertical Linearity Control Misadjusted

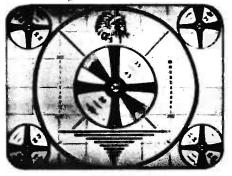


Fig. 21. Contrast Too High



Fig. 23. Focus Control Misadjusted



Fig. 25. Horizontal Hold Control Misadjusted

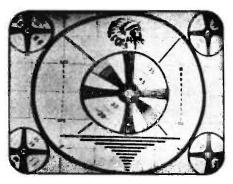


Fig. 27. Horizontal Linearity Control Misadjusted



Servicing Notes on 1947-1948 F. M. and Television Receivers PICTURE MALADJUSTMENT OR INTERFERENCE (Cont'd)

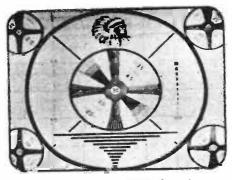


Fig. 28. Horizontal Width Control Misadjusted

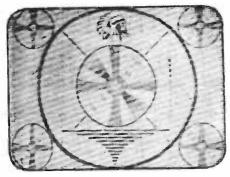


Fig. 30. R-F Interference Pickup on Antenna

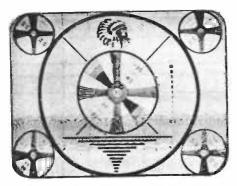


Fig. 32. Weak Diathermy Interference

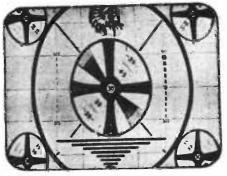


Fig. 29. Vertical Height Control Misadjusted

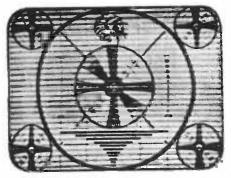


Fig. 31. Sound Bar Interference Such as Adjacent Channel or Microphonics

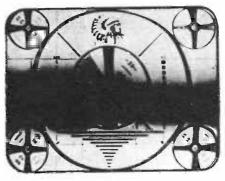


Fig. 33. Strong Diathermy or Hum in Video 1-F, Detector, or Video Output

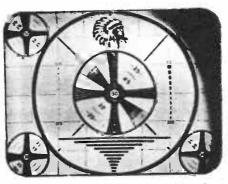
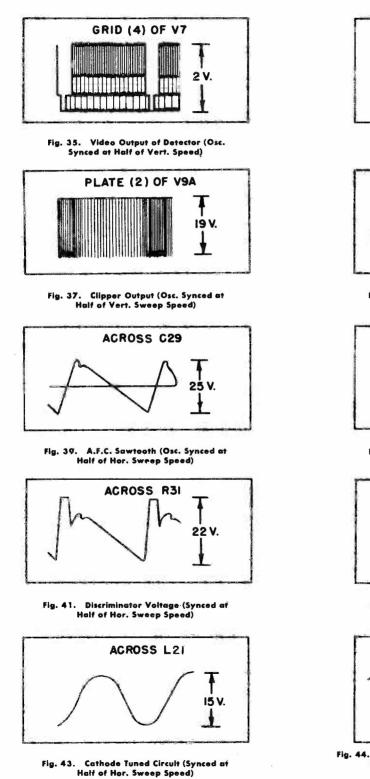


Fig. 34. Ion Trap or Focus Coll Not Properly Adjusted

WAVEFORM MEASUREMENTS

The waveforms shown in Figures 35 through 55 represent measurements on an average receiver wherein the controls have been adjusted for a normal picture with correct Contrast, Height, Width and Linearity. Most measurements must be made when a signal is being received. An oscilloscope where the vertical deflection amplifier has been pre-calibrated is used to take measurements at the point indicated in the waveform boxes. The oscilloscope sweep frequency is indicated in the waveform title.



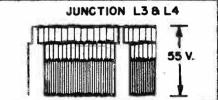


Fig. 36. Video Output of V7. (Osc. Synced at Half of Vert. Sweep Speed)

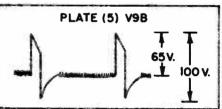


Fig. 38. Sync Amplifier Output (Osc. Synced at Half of Hor. Sweep Speed)

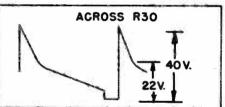


Fig. 40. Discriminator Voltage (Osc. Synced at Half of Hor. Sweep Speed)

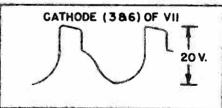


Fig. 42. Hor. M-V Cathode (Osc. Synced at Half of Hor. Sweep Speed)

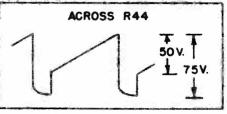
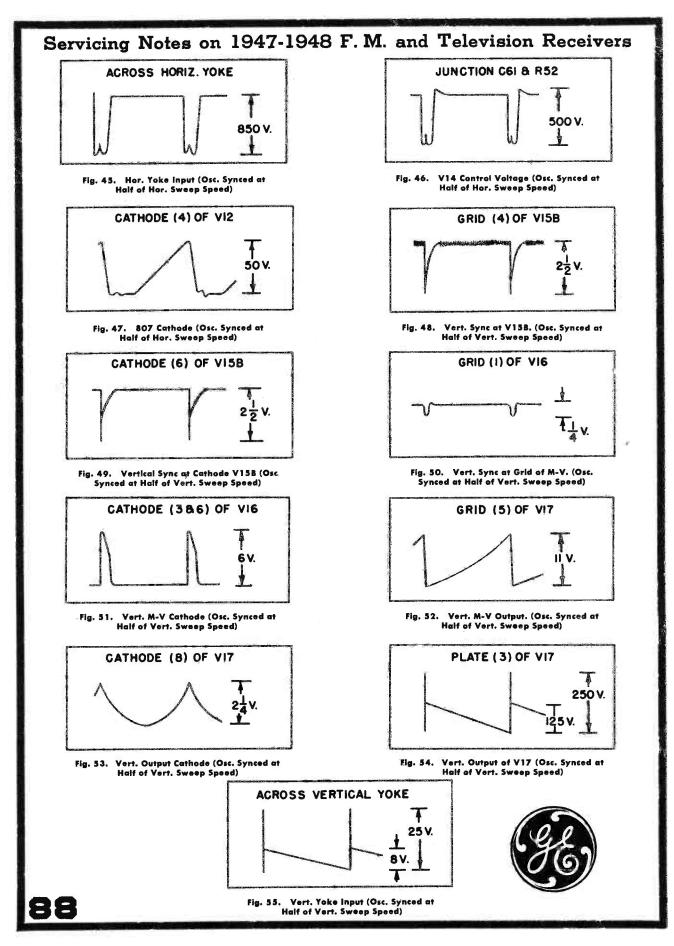
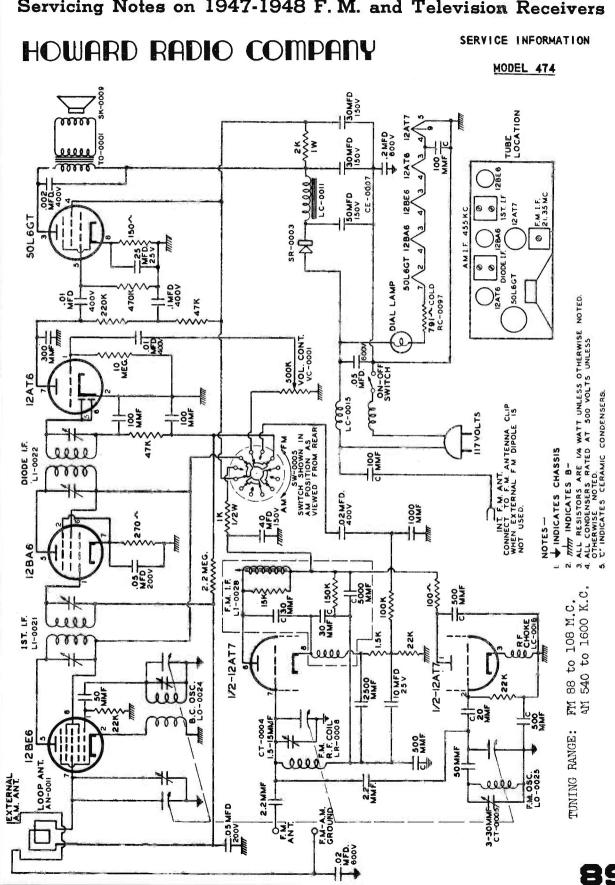


Fig. 44. Hor. M-V Output (Osc. Synced at Half of Hor. Sweep Speed)





12BE6



2

12AT6

50L6GT

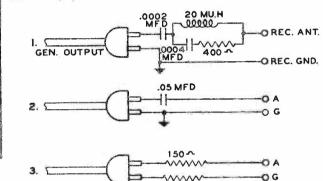
DIODE LE

IZAT7

JUKET TOETHOE MENDING									
Tube	Function	Screen Grid	Plate						
12BE6	Mixer	0	100	98					
12BA6	I.F. Amp.	1	100	98					
12AT7	FM Tube	Pin 8 14 V.	-	120					
12AT6	Det.	0	0	65					
50L6	Output	6.8	100	130					

SOCKET VOLTAGE READINGS

All voltages taken from the buss bar (B-) to the socket contacts, with a 20,000 Ohm per volt D.C. meter and the line voltage fixed at 117 Volts A.C.



150 ~



EM. LE

12 BA6

1ST LE

DUMMY GENERATOR CHART

See Dummy Antenna Chart	Sig. Gen. Connection To	Gen. Freq.	Band Position	Dial Setting	Order of Trimmer Adj.	FUNCTION	See Note
2	Grid of 12BE6	455 K.C.	B,C.	Off Station	0034	I.F.Peak to Max.Output	
1	A.M.Ant. Clip	1400 K.C.	B.C.	1400 K.C.	56	B.C.Osc. and R.F.	A
2	F.M.Ant. Clip	21.35 M.C.	F.M.	Off Station	Ø	F.M1.F.	В
3	F.M.Ant. Clip	105 M.C.	F.M.	105 M.C.	89	F.M.Osc. Peak to Max.Output	C

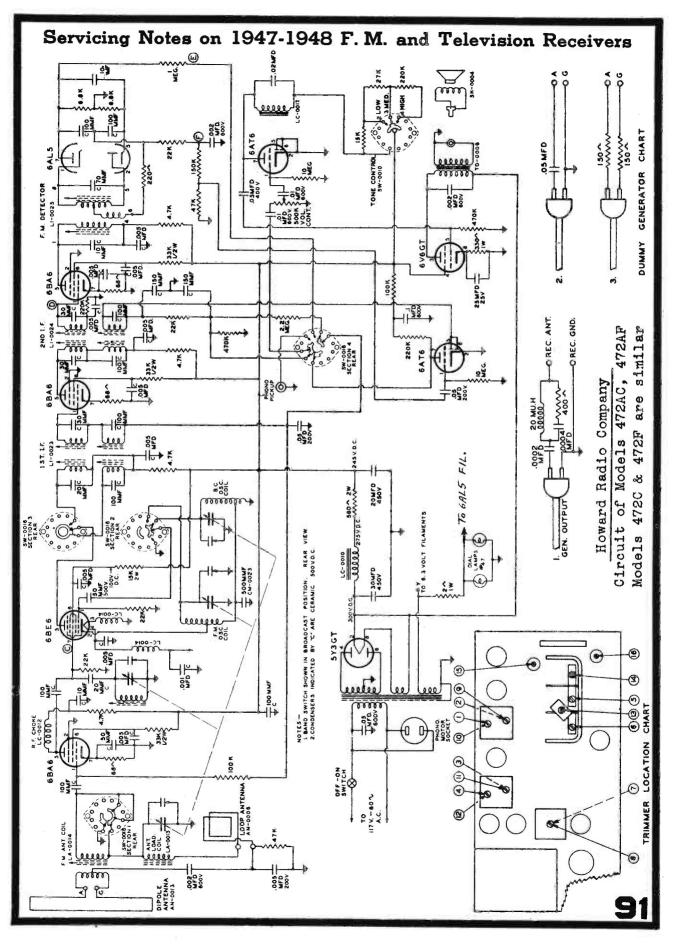
Set pointer in horizontal position with condenser gang closed. Note A.

Adjust for minimum noise with modulation off. Note B.

Note C.

Adjust (8) to 105 M.C.- Oscillator section.

While adjusting Q, rock condenser gang slowly back and forth for point of optimum. Check tracking of R.F. at 90 to 100 M.C.

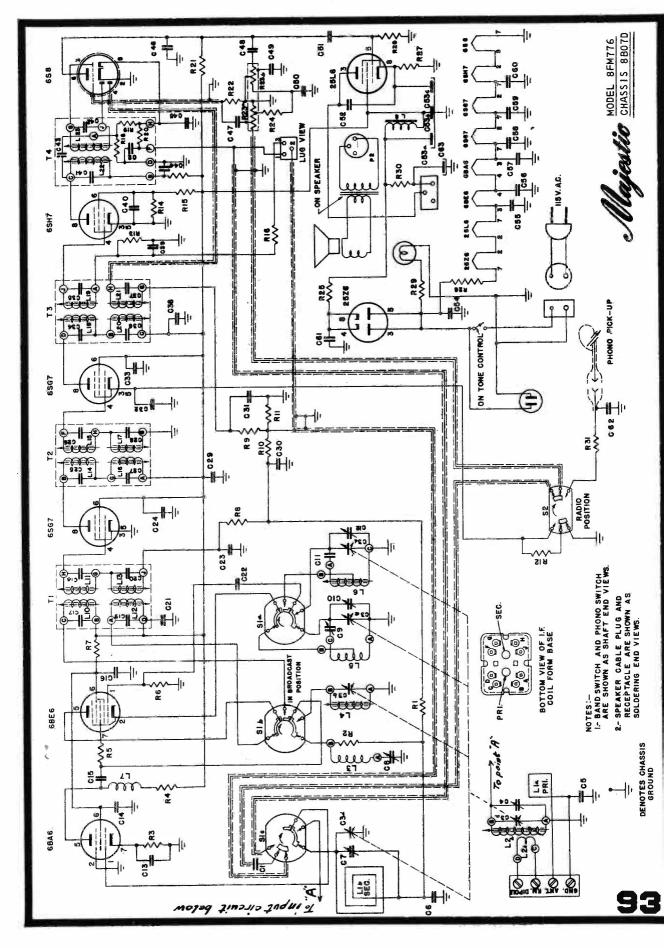


Servicing Notes on 1947-1948 F. M. and Television Receivers Howard Radio Company ** Models 472C - 472F - 472AC - 472AF ALIGNMENT CHART USING MODULATED GENERATOR Order of Trimmer See Dial Band Sig. Gen. Gen. See Slug and or Slug Notes Setting Dummy Connection Freq. Sw. Function Below Trimmer Gen. Adjust. Chart 1234 AM I.F. A & B Gang 455 KC AM 2 Point C on Closed Green D. Diagram 1 Ant. post, 66 AM - Osc. C & D 1400 KC AM rear of ch. 1.4 MC & RF Trm. loop conn. E & F $\overline{7}$ FM Det. Gang Point D on 10.7 MC FM 2 Closed Adj. Diagram 11 11 G 19 99 BAdj. As above 2 to 0 v. 11 91011 FM H 11 28 Point C on 2 I.F. 12 & (7)Diagram T & J Osc. & (14)(13)Ant and Gr 3 RF FM 105 MC 105 MC FM Back of Ch. FM - RF(15) 90 MC As above 90 MC FM 3 Ind. Adj. K & L FM Ind. M (16)101 MC FM 101 MC As above 3 Adj. A.Low voltage AC voltmeter across voice coil. B. Repeat operation until no further improvement can be found. C. Before adjusting set pointer on heavy gold line below 560 KC. with gang closed. D.Check complete dial for sensitivity.and calibration. E.Signal generator modulation off and turned up to about 100,000 microvolts. F.Connect electronic volt meter (equivalent to voltohmist) at point E on the wiring diagram and turn slug (7) on trimmer location chart to extreme counter clockwise position. Turn clockwise to 1st peak and adjust to maximum., G. Turn slug (8) to extreme counter clockwise position. Connect electronic voltmeter to Point F on wiring diagram and turn slug (8) until voltmeter is to zero voltage. Repeat adjustments given in notes F & G until no further improvement can be made. H.Connect voltmeter to point E and generator at point C. Adjust (9) (10) (11) (12) then retrin (7). Move voltmeter to post F and recheck zero voltage (retrim if necessary). These adjustments should be made with input signal necessary to produce approximately .7 volts at point E. I.Change generator dummy as shown on dummy antenna chart picture 3, and modulation on. J.Use meter across voice coil if using RF generator, but use AVC voltage if working with AM generator. K.Should 90 MC. signal not fall in at 90 MC. on the dial, adjust F.M. Osc. Coil to correct

K.Should 90 MC. signal not fall in at 90 MC. on the dial, adjust F.M. Osc. Coil to correct calibration. It is only necessary to slightly press together or open spacing on one turn to do so. Now adjust slug (15).

L.Repeat adjustments (13) (14) and then (15) until no further improvement can be made.



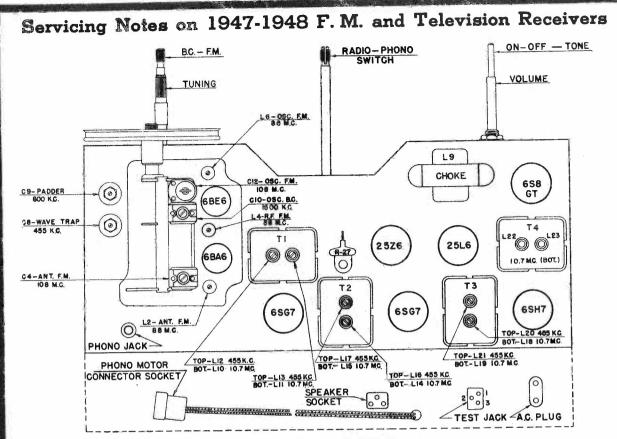


PARTS LIST

MODEL 8FM776 CHASSIS 8B07D

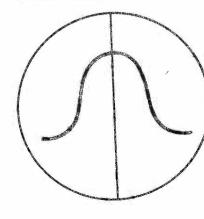
And the second	and the second	PARTS LIST CHASSI	S 8807D
ITEM	PART NO.	DESCRIPTION	L2.
C1,C48 C2,C14,C15,C16, C55,C56,C57 C3 C4,C10 C5,C23,C30,C32	017-4 6-230 7-25 8-35	.005 mfd, 600V	
C49,C50 C6,C62 C7 C8 C9 C11 C12 C13,C22 C17,C41 C18,C25,C26,C34,C35 C19,C20,C27,C28,	$\begin{array}{c} 015-5\\ 015-8\\ 8-59\\ 8-63\\ 8+65\\ 6-218\\ 8-38\\ -6-159\\ 6-247\\ 6-246\end{array}$.01 mfd, 200V	
C36,C37 C21,C29,C38,C44,C51	6-250 016 - 5	750 mmf Mica Special	
C24,C33,C40,C58, C59,C60 C31,C46,C61 C39,C45 C42 C43 C47 C52 C53	6-259 6-151 6-232 6-249 6-248 017-2 017-5 19-37	.005 mfd minimum disk-type Ceramic 220 mmf, 500V Mica 100 mmf, 500V Mica 62 mmf, Ceramic, Special 15 mmf, Ceramic, Special .002 mfd, 600V .01 mfd, 600V 100 mfd 150V, 200 mfd - 150B, 200 mfd	rd - 10V.
C54 C63	016-8 19-32	Electrolytic	
R1, R8, R11, R16 R21, R28 R2, R13, R17, R20 R3, R12 R4, R14 R5 R6, R9 R7 R10, R31 R15 R18, R19 R22 R23 R24 R25 R26 R27 R29 R30 L1 L2 L3 L4 L5 L6 L7 L8 T1 T2 T3 T4	$\begin{array}{c} 01-199\\ 01-157\\ 01-37\\ 02-108\\ 01-3\\ 01-143\\ 01-143\\ 01-143\\ 01-143\\ 01-227\\ 02-132\\ 01-174\\ 01-255\\ 03-32\\ 01-132\\ 02-52\\ 04-69\\ 01-45\\ S1400\\ S-142\\ 02-52\\ 04-69\\ 01-45\\ S1400\\ S-1410\\ S-1408\\ S-1411\\ S-1409\\ S-1384\\ 2-32\\ S-1389\\ S-1389\\ S-1390\\ S-1391\\ S-1392\\ \end{array}$	470K ohm, 1/4 watt	
			O Calegory
94		DIAL STRING	2 TURNS

1	Servi	cin	g No	otes	5 01	n 1	94	7-1	94	8 F	`. M	l. a	nd	Te	lev	is	ion R	ecei	vers
	PURPOSE	Align if channel for maximum output.	Adjust wave trap for maximum output.	Set oscillator to dial scale.	Align antenna for maximum output.	Rock gang to track BC padder	Align Primary of discriminator for maximum reading.	Adjust secondary of discriminator for zero reading.	Align 3rd IF Transformer for maximum reading.	Align 2nd IF Transformer for maximum reading.	Align 1st IF Transformer for maximum reading.	Set oscillator to dial scale.	Align anterna stage for maximum reading.	Set Oscillator to dial scale.	Align Antenna and RF stages for maximum reading.		or is replaced or the adjustment has meter connected across the primary or ignal generator output should be kept	tor load).	<pre>>tained by using a 10.7 MC signal generator, frequency modulated An oscilloscope should be connected to test jack pin 3 and all See Fig. 1. For discriminator alignment, connect oscilloscope ittern. See Fig. 2.</pre>
۲T	ADJUST TRIMMERS	L12, L13, L16, L17, L20, L21		CIO	C7	CO	L22 Coil Slug Primary Discriminator	L23 Coil Slug Secondary Discriminator	L18 and L19, Pr1. and Sec. 3rd IF Coll	L14 and L15 Pr1. and Sec. 2nd IF Co11	L10 and L11 Pr1. and Sec. 1st IF Co11	Cl2 Oscillator Trimmer	C4 Antenna Trimmer	L6 Oscillator Slug	14, L2 Slugs	tracking is perfect at 88 and	it cases be unnecessary unless an IF or RF transformer is timeter must be used for FM alignment. An AC output meter fill be satisfactory for all AM adjustments. The signal on the meter.	<pre>[!scriminator transformer to chassis (half discriminator load). st jack to chassis (full discriminator load). st jack to chassis (limiter grid load).</pre>	minator alignment may be obtained by using a 10.7 MC signal cimately 600 KC (±300 KC). An oscilloscope should be connectern of highest amptitude. See Fig. 1. For discriminator a lighest linear symetrical pattern. See Fig. 2.
ALIGNMENT	SET DIAL TO	600 KC	600 KC	1500 KC	1500 KC	600 KC			مراجع المراجع			106 MC	106. MC	88 MC	88 MC	14 until tra	cessary unl sed for FM cory for al	insformer to Is full dis Is limiter	nt may be ob (±300 KC). amptitude. ymetrical pa
A	BAND	BC	BG	BC	BC	ß	W	НИ	E	Η	MH	ЫŅ	μų	FIM	FM	and	e unne ist be tisfac	tor trachass chass chass	llignme 500 KC ghest near s
	INPUT SIGNAL FREQUENCY	455 KC	455 KC Modulated	1500 KC Modulated	1500 KC Modulated	600 KC Modulated	10.7 MC; Unmodulated	10.7 MC Unmodulated	10.7 MC Unmodulated	10.7 MC Unmodulated	10.7 MC Unmodulated	106 MC Unmodulated	106 MC Unmodulated	88 MC Unmodulated	88 MC Unmodulated	ps 11, 12, 13,	most cases be unnecessary voltmeter must be used fo er will be satisfactory f ion on the meter.	on discrimina test jack to test jack to	scriminator a proximately (pattern of hi or highest li
	DUMM Y ANTENNA	.OSmfd.	.05mfd.				⊳05mfd.	.05mfd.	.05mfd.	.05mfd.	.O5mfd.	300ohm Resistorr	300ohm Resistor	300ohm Resistor	300ohm Resistor	Repeat steps	chassis will in most A vacuum tube volt tput transformer wil get an indication or	er pin "A" er pin 1 of er pin 3 of	Y IF and d1 ind swept ap symetrical adjust T4 f
	CONNECT TEST OSCILLATOR TO	Stator Plates of C3d	Stator Plates of C3d	A TURNS	8" DIAMETER COUPLED LOOSELY	TO LOOP ANTENNA	Pin 4 (Grid) on 6SH7 Limiter Socket	Pin 4 (Grid) on 6SH7 Limiter Socket	Pin 4 (Grid) on 68G7 2nd IF Socket	Pin 4 (Grid) on 68G7 lst IF Socket	Lug "B" on Coll 14	Antenna Terminals	Antenna Terminals	Antenna Terminals	Antenna Terminals	Antenna Terminals	Allgrment of this chassis will in most cases been tampered with. A vacuum tube voltmeter secondary of the output transformer will be just high enough to get an indication on the	(a) Vacuum tube voltmeter pin "A" on di (b) Vacuum tube voltmeter pin 1 of test (c) Vacuum tube voltmeter pin 3 of test	A much more satisfactory IF and discriminator alignment may be obtained at an audio frequency and swept approximately $600 \text{ KC} (\pm 300 \text{ KC})$. An osci IF slugs adjusted for a symetrical pattern of highest amptitude. See Fit to test jack pin 1 and adjust T4 for highest linear symetrical pattern.
	OPERAT ION	T	02	3	4	ല	6(a)	(q)L	8(c)	(°)6	10(c)	11(c)	12(c)	13(c)	14(c)	15(c)	INPORTANT:	NOTES:	95



VOLTAGE TABLE

TUBE	FUNCTION	PLATE	CATHODE	SCREEN	GRID	
6BA6	RF Amplifier	80	0.5	78		
6BE6	Converter	100	0	78		
6SG7	lst IF Amplifier	100	0	100	-0.6	
6\$G7	2nd IF Amplifier	100	.7	100		
6SH7	Limiter Amplifier	70	0	21	-0.4	
6S8GT	Discriminator, Det., AVC	50	θ			
25L6	Power Amplifier	105	7	100		
2525	Rectifier	117AC	105			



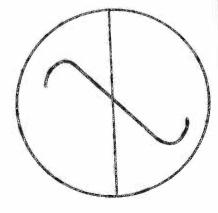
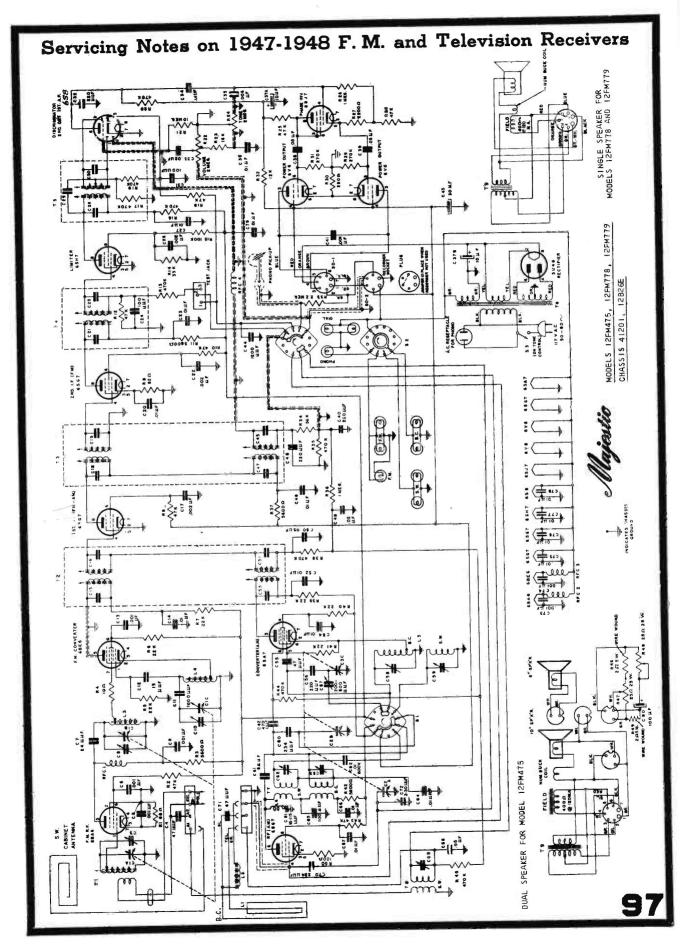


FIGURE 2

FIGURE 1



Servicing No	otes on	1947-1948 F. M. and Television Receivers
ITEM	PART NO.	DESCRIPTION Ganged Tuning Condenser.
C1,C2	7-17	Ganged Tuning Condenser.
C3,C8,C10	8-38	
C4,C55,C71	6-159	47 mmf, 500V, ceramic.
C5,C6,C9		
C13,C73,C74	6-230	.001 mfd., 400V. ceramic PARTS LIST
C7	6-143	24 mmf, 500V ceramic
C11	6-218	1000 mmf. 500V Ceramic MODELS 12FM475, 12FM778, 12FM779 15 mmf. 500V ceramic
	6199	15 mmf. 500V milea MODELS 12FM475, 12FM778, 12FM779 15 mmf. 500V ceramic
C14,C23,C27,C34, C48,C52,C54,C66,C67		
C79,C82	5-74	.01 mfd 600V
C15,C16,C51	0.14	
C53		Part of 1st. IF transformer, T2
C17,C22,C26	6-231	.002 mfd. 400V Ceramic
C18,C19,C45,C47		Part of 2nd IF transformer, T3
C21,C24,C25		Part of 3rd. IF transformer, T4
C28,C29,C30		Part of discriminator transformer, T5
C31	6-232	100 mmf. 500V Mica
C32,C40,C46	6-86	220 mmf. 500V. Mica
C33,C49	5-63	.02 mfd. 500V
C35	5-69	.006 mfd. 600V
C37A,C37B	19-34	10-10 mfd. 450V Electrolytic
C38,C39	5-77	.05 mfd. 600V
C41	5-84	.001 mfd. 1600 V
C42	6-102	470 mmf. Mica 500V
C43	19-35	30 mfd. 450 V. Electrolytic.
C44	6-234 5-64	1200 mmf. 500V
C50,C68 C56	6-207	.05 mfd. 400V
C57	8-65	200-600 Podder
C58,C59		Part of coll assembly L5
C61,C62,C63,C65		Part of coil assembly T7
C69	b	Part of coil assembly T8
C72	835	Trimmer 22 30 mmf. ceramic FIGURE 1
C75,C76,C77,C78	6-182	.0lmfd. 500V Mica
C81	8-63	15-115 mmf. Trimmer (Wave Trap)
Ll	20-27	Broadcast Loop Antenna
L2		Loading Coil, Part of Loop 20-27.
L3	3-184	F1 RF Co11
14	3189	FM Oscillator Coil
L5	3-171	AM Oscillator Coil Assembly.
L6	S-1468	Wave Trap Coll Assembly.
R1.	9-294	68 ohmes 1/4 watt
R2	9-293	47,000 ohms, 1 watt.
R3,R11,R37,R42	9-130	5600 ohmas 1 watt
R4	01-2 9-222	
R5,R41		22,000 ohms 1/4 watt
R6,R40	.9-209	22,000 ohms 2 watt
R7,R39 R8,R10,R25,R28,	9-253	22,000 homs 1/2 watt .
R43	9-235	47,000 ohms 1/2 watt
R9	9-283	82 ohms 1/2 watt
RI2	5 200	47,000 ohms (Part of T4)
R13,R20,R35,		
R38,R44,R45	9-223	470,000 ohms 1/4 watt.
R14	9-256	33,000 ohms 1/2 watt
R15	98	100,000 ohms 1/2 watt
R16	9-211	470,000 ohms 1/2 watt.
R17,R19		470,000 ohms (part of T5).
R18	9-121	47,000 ohms 1/4 watt
R21 R22	9-213	10 megohms 1/4 watt.
R23	13 - 25 9-225	Volume Control, 2 megohms
R24	9-225	18,000 ohms 1/4 watt
R26,R36	9-255	1 megohm 1/4 watt.
R27	9-7	2200 ohms 1/2 watt
R29,R31	9-295	270,000 ohms 1/4 watt.
R30	9-290	250 ohms 5 watt, wire wound.
R32	9-264	12,000 ohms 1/2 watt
R33	9-240	2.2 megohms 1/2 watt
R34	01-160	56K ohms 1/4 watt.
R50	01-44	100 ohm 1/4 watt
C80	Î	19-36 100 MF 10V electrolytic Model 12FM475
R46	[9-297 2 ohm 5 watt wirewound, Model 12FM475
R47,R48		13-23 Potentiometer, 25 ohm, 25 watt, Model 12FM475.

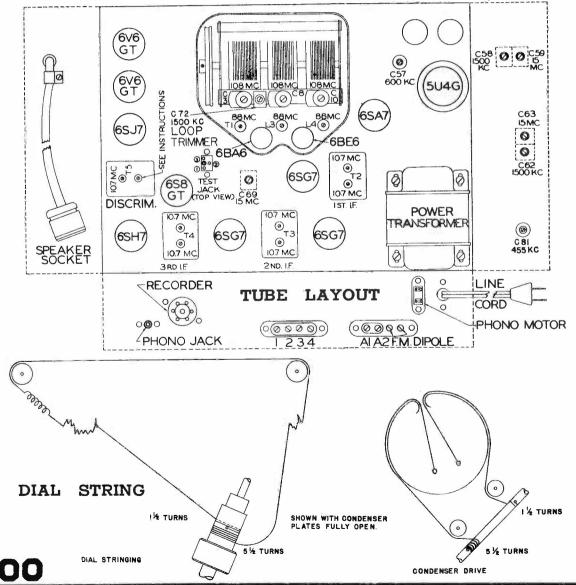
5	Servi	ci	ng	N	ot	es		n	1942	7-194	8 F. M	. an	d T	elev	<i>r</i> isi	or	Re	ceiver	s								
	PURPOSE	Align I.F.'s	I.F. trap adjustment for minimum I.F. signal	Set BC osc. to scale at 1500 KC	Align BC RF. and Loop	Rock Gang to track BC padder	Scale osc. at 15 MC	Align SW RF and Ant.	Align for max, voltage at test jack pin 3 Rock gen, over 10.7 MC to check for symmetrical I.F. response.	Align for max, voltage at test jack pin 3 Rock gen, over 10.7 MC to check for symmetrical I.F. response.	Align for max, voltage at text jack pin 3 Rock gen. over 10.7 MC to check for symmetrical 1.F. response. Re-check peaking of T4, and T3.	Align for max. voltage across 4 discriminator Load (un-used Lug bottom of T5 to ground)	Align for zero voltage across full discriminator load (Test jack pin 1 to ground)	Scale OSC at 108 MC (max. voltage Test jack pin 3.	Align FM RF and Ant. (max. voltage Test jack pin 3.	Scale osc. at 88 MC.	Align RF and Ant. at 88 MC repeat steps 13, 14, 15, 16 as necessary.	a 10.7 MC Signal generator frequency modulated should be commected to Test jack pin 3 and all For discriminator alignment, connect scope to	In all FM alignment calling for a voltage measurement at Test jack pin 3 (limiter grid resistor) keep signal generator output to such a value as will result in approximately 2 volts measured with a vacuum Tube voltmeter such as the Voltohmyst, Vomax or equiv.								
ALIGNMENT	TR IMMERS	T2,T3 Bottom	CBI	C58	C63,C72	C57	C59	C62,C69	T4 top	T3 top	T2 top	T5 primary	T5 secondary	CIO	C8,C3	14	L3, T1	tained by using a 10.7 M An oscilloscope should See Fig. 1. For dis e Fig. 2.	3 (limiter grid re m Tube voltmeter								
	SET DIAL AT	600 KC	GOOKKC	1500 KC	1500 KC	600 KC	15 MC	15 MC	BB MC	88 MC	88 MC	88 MC	88 MC	108 MC	108 MC	88 MC	88 MC	may be obtained 500 KC). An osc aptitude. See tern. See Fig.	Test jack pin 3 ured with a vacuu								
ALI	BAND	BO	BC	BC	BC	BC	MS	R	Ш	W	Wd	JUA	W	E	W	W	E	ulignment 100 KC (I 3 highest a rical pat	urement al volts meas								
	INPUT S IGNAL FREQUENCY	455 KC	455 KC	T500 KC	1500 KC	600 KC	15 MC	15 MC	10.7 MG	10.7 MC	10.7 MG	10.7 MC	10.7 MC	IO8 MC	108 MC	88 MC	88 MC	scriminator a pproximately (al pattern of highest symmet	voltage measu roximately 2 v								
	DUMMY ANTENNA	,01mfd	JRN 7. Litmu	ONE TURN LOOP MADE WITH GENERATOR LEADS		NN WITH JR		AN DR UTH	HLIN	NN WITH OR	NTH WITH OR	RN WITH OR	NN WITH OR	RN WITH OR	400 o hn	400 o hn	.01mfd.	, Olmfd.	.Olmfd.	.01mfd.	.Olmfd.	direct	direct	direct	direct	ory IF and d1 and swept a r a symmetric djust T5 for	alling for a result in app
	CONNECT OSCILLATOR TO	Conv. Grid	ONE TURN	GENERAL	LEAD	L	. bn9-lA	Al-Gnd.	68G7 2nd I.F. Grid	68G7 lst. I.F. Grid	Converter	Converter grid 6BE6	Converter grid 6B6E	FM ant.term.	FM ant.term.	FM ant.term.	FM ant.term.	A much more satisfactory IF and discriminator alignment may be obtained at an audio frequency and swept approximately 600 KC (#300 KC). An os IF screws adjusted for a symmetrical pattern of highest amptitude. See Test jack pin 1 and adjust 75 for highest symmetrical pattern. See Fig.	l FM alignment c 1 value as will								
	OPERAT ION	T	Q3	ю	4	ى	6	4	σ	Ø	10	11	12	13	14	15	16	NOTE: 1. A much at an IF scr Test	C 2. In all such a								

Servicing Notes on 1947-1948 F. M. and Television Receivers VOLTAGE TABLE MODELS 12FM475, 12FM778, 12FM779 CHASSIS 41201, 12B26E

Measurements made at 117 volts line; volume control at minimum; zero signal input. Measurements made to chassis ground with vacuum tube voltmeter.

FUNCTION	TYPE	EF	٤p	Es	Eĸ	EG
FM RF AMP.	6BA.6	6.3	210	90	1	0
FM CONVERTER	6BE6	6.3	210	1.00	0	0
AM RF AMP.	6SG7	6,3	260	180	1	~1
AM CONVERTER	65A7	6.3	250	90	0	
1ST IF AMP.	68G7	6.3	240	125	0	-1
2ND IF AMP.	6 3 G7	6.3	240	125	1	0
LIMITER	6SH7	6.3	3	60	0	6
DISC.; 2ND AMDET: AUDIO	6S8GT	6.3	80		0	8
PHASE INVERTER	6SJ7	6.3	160		80	0
POWER AMP.	6V6GT	6.3	260	270	15	
POWER AMP.	6V6GT	6.3	260	270	15	
RECTIFIER	5V4G	5			300	

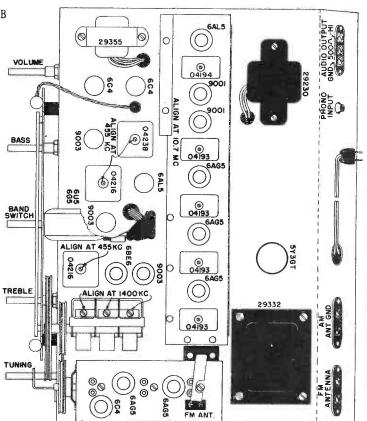
TOTAL B CURRENT FROM RECTIFIER 120 MA.

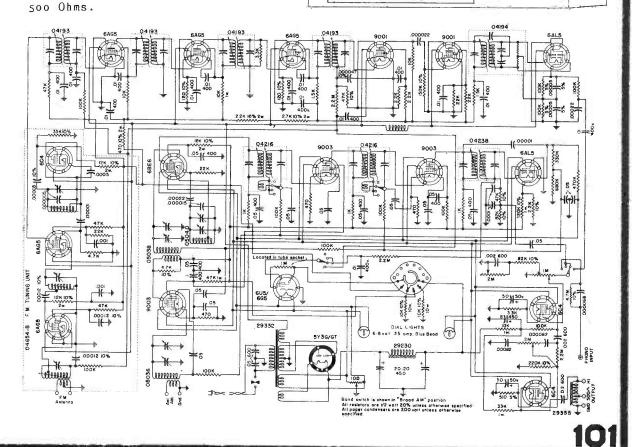


MEISSNER MODELS 9-1091A, 9-1091B

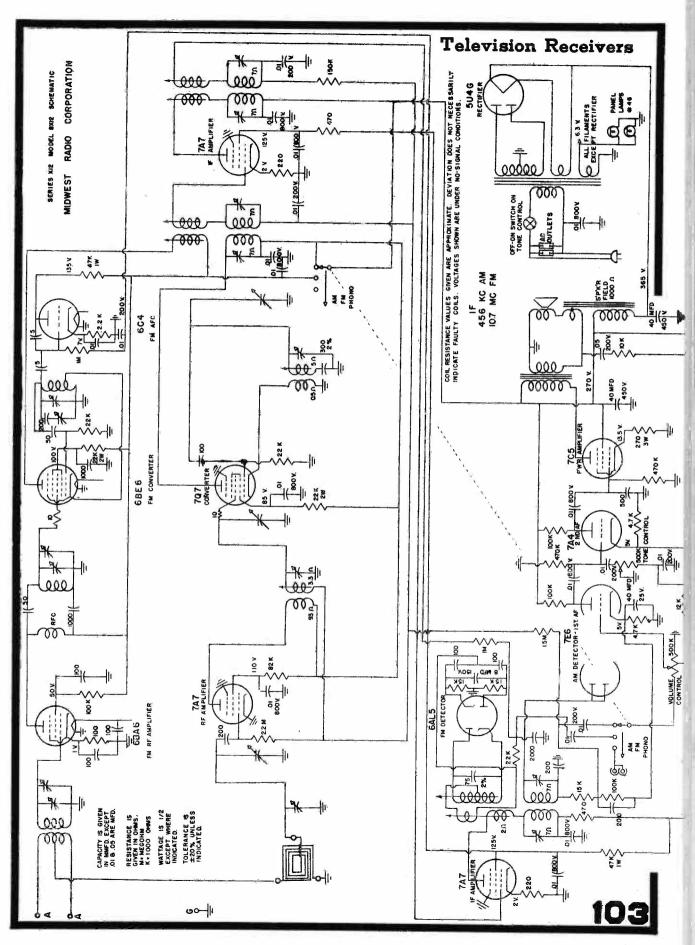
A. M. - F. M. TUNER

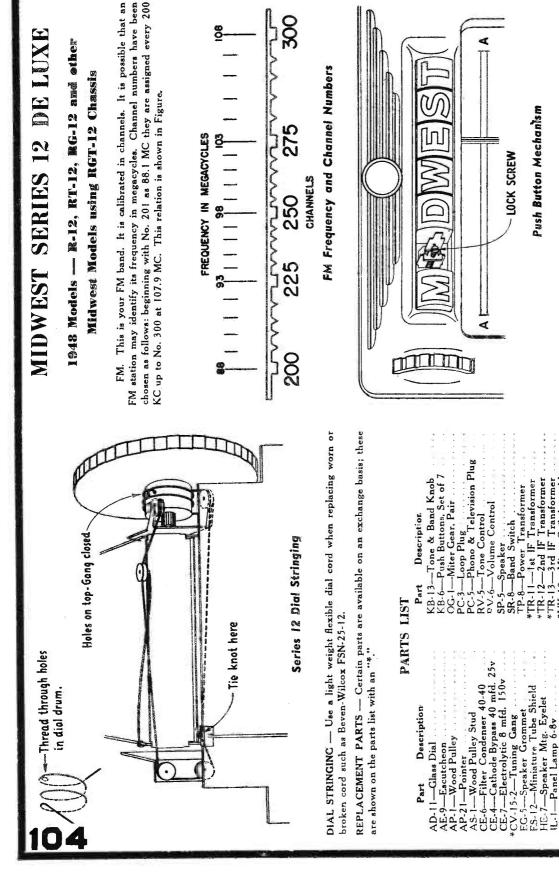
- Power Supply 105-125 Volts, 50-60 Cycles. Power Consumption - 80 Watts.
- Type of Circuit Superheterodyne.
- Tuning Range 527-1620 Kc. *88-108 Mc. Intermediate Frequency -
- 455 Kc. 10.7 Mc.
- Audio Fidelity Flat within $\neq 2$ d.b. from 30 to 15,000 cycles.
- Band Width at 1,000 Kc. -Sharp 7.5 Kc. Broad 18.5 Kc.
- Hum 60 d.b. below rated output.
- Distortion Less than 5%. Output - 8 Volts at High Impedance - 0.75 Volts at





RT-12, RG-12 and other sing R&T-12 Chassis	ALIGNMENT — Refer to the alignment chart for step by step procedure. It is preferable to align the FM IF stages with an AM or CW Signal. It should be noted that all adjustment are made for peak ave reading except the secondary of the third transformer. At this point, if you use an AM signal, it may be tuned for minimum audio signal; or the discriminator voltage may be used, reading it with a VTVM, and the secondary may be adjusted to the zero voltage. There may be some discrepancy between these methods, and if it is not excessive, is of no importance.	The FM RF alignment should be made using an FM signal and either ave or audio for peaking. In doing this alignment, or when feeding the IF signal into the FM mixer grid, care must be taken not to move the wiring. If the wiring is dis- placed so as to affect the inductance of the RF circuits it is difficult to re-establish the RF-Oscillator-tracking.	The AM, RF and IF alignment should be done with a VTVM across the avc. The recommended signal value is one which will generate 10 volts of avc. When aligning(the "AM" band the loop must be plugged in and you need not adjust the RF padder core. The RF padder is very broad and can be aligned only if the con- verter grid lead is connected to an RF type VTVM as indicator; this will usually involve a signal level greater than is normally available.	Band Dial Adjustment	1000 KC	AM 1609 KC Peak RP, converter and oscillator trimmers marked "B".	AM 550 KC Peak converter and oscillator padder cores marked "B". Loop mut be plugged in. Do not adjust RF.	FM 100 MC Peak core adjustments for avc (around 3 volts) at 1st, 2nd and primary of 3rd IF. Adjust secondary of 3rd IF for audio hull from 30% amplitude modulated 10.7 MC IF signal.	FM 105 MC Peak RF mixer and oscillator trimmers for avc or audio.	ament.
1948 Models R-12, RT-12, RG-12 and a Midwest Models using RGT-12 Chassis	ALIGNMENT — Refer to the alignment chart for step by preferable to align the FM IF stages with an AM or be noted that all adjustment are made for peak ave reading the third transformer. At this point, if you use an AM sign minimum audio signal; or the discriminator voltage may be a VTVM, and the secondary may be adjusted to the zei be some discrepancy between these methods, and if it is importance.	The FM RF alignment should be m audio for peaking. In doing this alignme FM mixer grid, care must be taken not placed so as to affect the inductance of th RF-Oscillator-tracking.	The AM, RF and IF alignment should be done w The recommended signal value is one which will gene aligning(the "AM" band the loop must be plugged in RF padder core. The RF padder is very broad and ca verter grid lead is connected to an RF type VTVM a involve a signal level greater than is normally available.	Coupling Signal Sw	27 converter grid 456 KC igh .05 mfd. capa-	To "A" on antenna 1600 KC A ground terminal atrip AM	550 KC AM	To 6BE6 mixer grid AMor CW direct.	To "A" and "A on 105 MC F doublet terminal strip through a pair 150 ohm resistors.	*Read text for use of UW for FM-IF alignment.
KB-I2 AP-I CV-J5-2 RY-6 KB-4	Z TER	B-J-J-V-J-V-J-V-J-V-J-V-J-V-J-V-J-V-J-V-	TR-I2 TR-I2 TOP View of Series 12 Chassis		AE-9 AD-I1 KB-6 KB-13		St-9	E3	xp-1 UK-11 xc-4 UK-13 UK-13	L Bottom View of Series 12 Chassis





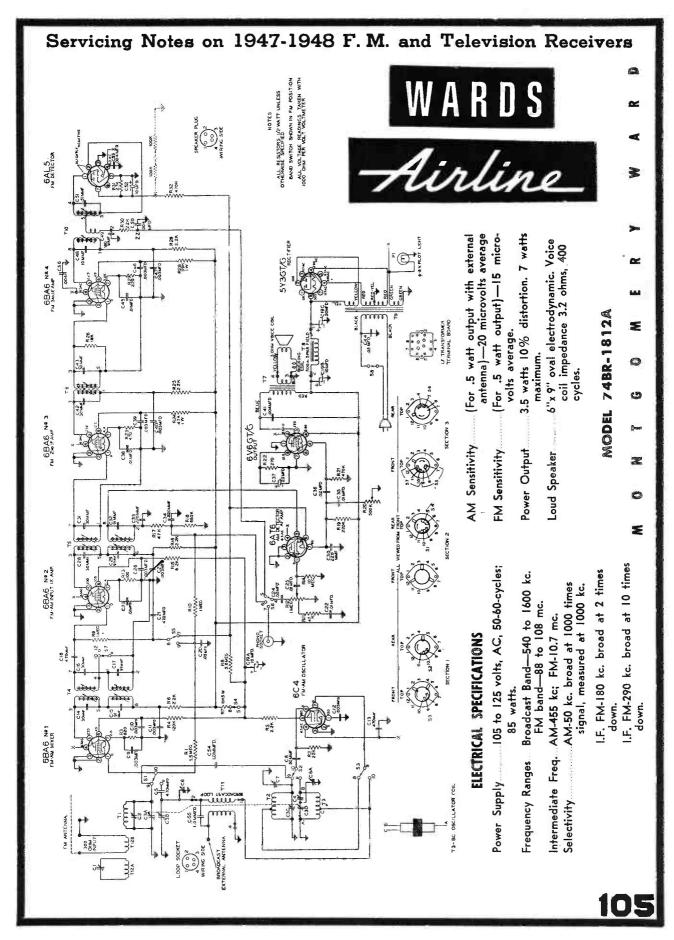
PUSH BUTTONS — The push buttons are for your convenience in selecting stations without the bother of making the exact tuning adjustments necessary for best reception. There are seven buttons and each button may be set for a station. The station may be at any point on the dial.

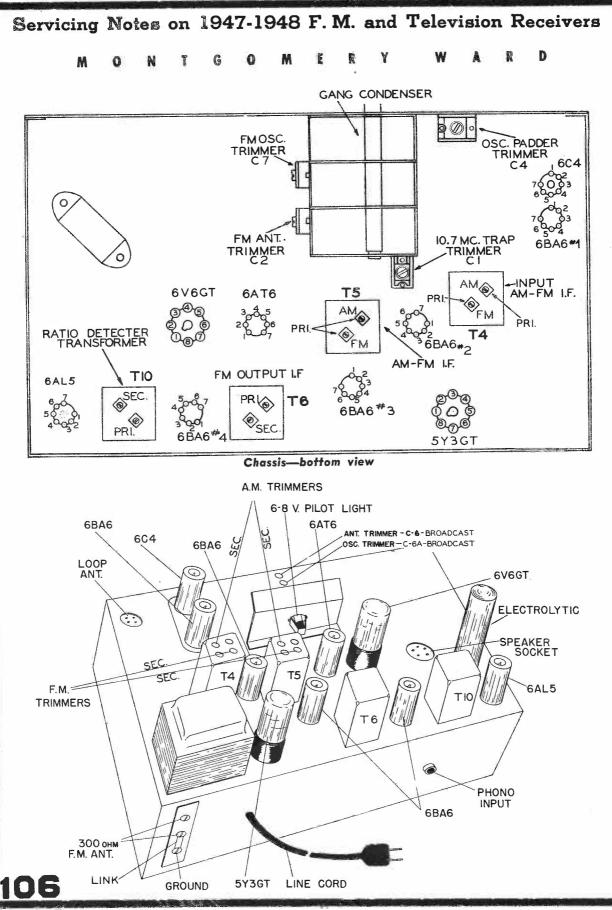
> Note: Order resistors and condensers by value, tolerance and wattage or vokage. Note: When ordering include serial number of chassis, since Midwest records of changes in parts specifications are kept by that number.

*UK-12-Mixer Coil Assembly *UK-13--Oscillator Coil Assembly

> KB-4--Volume Knob KB-12---Tuning Knob

Servicing Notes on 1947-1948 F. M. and Television Receivers





1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -

Montgomery Ward Model 74BR-1812A

ALIGNMENT PROCEDURE

Broadcast Band Section I.F. and R. F.

The alignment procedure below includes the sensitivities at the inputs of various stages. All signal input values are based on an output of 1/2 watt. This may be measured by disconnecting the speaker voice coil and substituting a 3.2-ohm resistor across the usecondary winding of the output transformer. A reading of 1.3 volts AC across this resistor will be approximately equivalent to a 1/2-watt output with the speaker connected. The volume control must be set at maximum. The tone control must be set for maximum treble.

The signal source must be an accurately calibrated signal generator capable of supplying the frequencies designated, modulated 30 % with a 400-cycles audio signal. A 400 cycle audio signal is required for the audio measurement. Variations in sensitivities of plus or minus 25 % are usually permissible.

AM - I. F. ALIGNMENT

Band Switch in AM Position. Tune Set to 1400 Kc. Dummy Antenna .1 Mfd.

SIGNAL GENERATOR FREQUENCY	CONNECTION TO RADIO	ADJUST FOR		
455 Kc. Use 2100 microvolts	Pin No. I of 6BA6 No. 2 and ground	Primary and Secondary of T5 AM windings. See top and bottom views	Maximum output Should be 1/2 watt	
455 Kc. Use 64 microvolts	Pin No. I of 6BA6 No. I and ground	Primary and Secondary of T4 AM windings. See top and bottom views	Maximum output Should be $1/2$ watt	
100 cycles. Use 63 millivolts	Pin No. 1 of 6AT6 and ground	None	Maximum output Should be 1/2 watt	

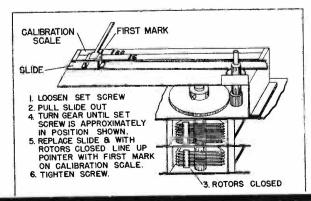
BROADCAST BAND - R. F. ALIGNMENT

Check Pointer so that it is Exactly Over Calibration Marker to the Extreme Left When Gang is Fully Closed. For Adjustment Loosen Set Screw on Large Gear. (see dial mechanism illustration.)

SIGNAL GENERATOR FREQUENCY	CONNECTION TO RADIO	DUMMY ANTENNA	ADJUST
1400 Kc. Use 15 microvolts	Antenna and Ground	200 mmf.	C6A for maximum 1/2 watt
600 Kc. Use 25 microvolts	Antenna and Ground	200 mmf.	C4 for maximum 1/2 watt
1400 Kc.	Antenna and Ground	200 mmf.	C6 See Note

NOTE: Recheck first two adjustments after this adjustment because of inter-locking effects.

Procedure for disassembly and assembly of dial mechanism



Servicing Notes on 1947-1948 F. M. and Television Receivers ALIGNMENT PROCEDURE

FM Band Section. I.F. and R.F.

IMPORTANT

No alignment of the FM section of this radio should be attempted unless you are positive that the circuits are in need of adjustment and you have the necessary equipment.

All components used in this radio are extremely stable and the tuned circuits should require no adjustment over long periods of time. NOTE

The following alignment is based on the use of the new Simpson vacuum tube voltmeter which has a "floating ground". In other words, the meter, when used as a vacuum tube voltmeter, can have both the positive and negative sides connected to points above ground and still give true readings.

A standard AM signal generator is required.

FM - I. F. ALIGNMENT

SIGNAL GENERATOR FREQUENCY	CONNECTION TO RADIO	VACUUM TUBE VOLT METER CONNECTION TO RADIO	ADJUSTMENT TO BE MADE	ADJUST FOR		
10.7 Mc. Use about .1 volt	Pin No.1 of 6BA6 no.4 and ground	Pin no. 7 of 6AL5 and ground	Primary of TIO	Resonance should be about 3 volts		
10.7 Mc. Use about .1 volt	Pin No.1 of 6BA6 no.4 and ground	See note "A"	Secondary of TIO	Zero. Use zero center scale See note "B"		
10.7 Mc. Use about 4000 microvolts	Pin No.1 of 6BA6 no.3 and ground	Pin no. 7 of 6AL5 and ground	Primary and Secondary of T6	Resonance should be about 3 volts		
10.7 Mc. Use about 150 microvolts	Pin No.1 of 6BA6 no.2 and ground	Pin no. 7 of 6AL5 and ground	Primary and Secondary of 10.7 mc. windings of T5. See top and bottom views	Resonance should be about 3 volts		
10.7 Mc. Use 3000 microvolts	FM Antenna input and ground	Pin no. 7 of 6AL5 and ground	Primary and Secondary of 10.7 mc. windings of T4. See top and bottom views	Resonance should be about 3 volts See Note "C"		
10.7 Mc.	FM Antenna input and ground	Pin no. 7 of 6AL5 and ground	CI	Minimum reponse. This is a trap circuit		

Band Switch in FM Position. Dummy Antenna .1 Mfd.

NOTES ON FM-I.F. ALIGNMENT:

NOTE "A" Connect two resistors, 100K OHMS each, from Pin No. 7 of 6AL5 to ground. These resistors must be matched within 5%. Connect as shown in dotted lines on schematic diagram. Connect vacuum tube voltmeter between the mid point of the resistors and point zz.

NOTE "B" If TIO has been tampered with, it is possible that no

crossover point will be found at first. Careful adjustment of both primary and secondary is necessary.

GENERAL: Input signals should be adjusted to give approximately 3 volts. The ratio detector is operating at a reasonable level at this point and will give the truest indication of correct alignment with the procedure specified.

NOTE "C" The input microvolts specified is based on the trap circuits being adjusted.

FM - R. F. ALIGNMENT

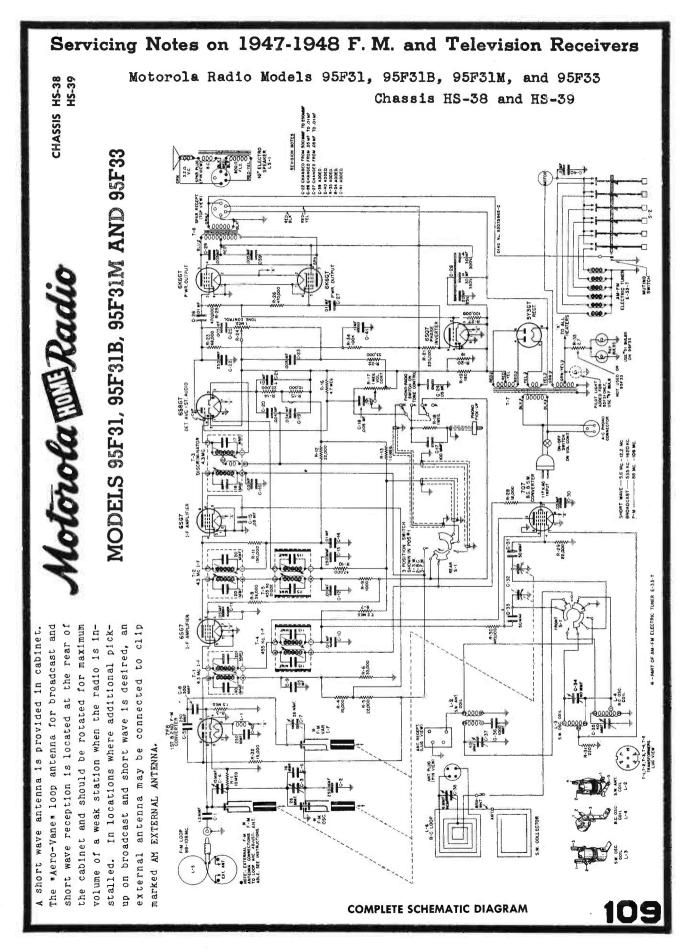
Check Pointer so that it is Exactly Over Calibration Marker to the Extreme Left When Gang is Fully Closed. For Adjustment Loosen Set Screw on Large Gear. (see dial mechanism illustration.)

SIGNAL GENERATOR FREQUENCY	CONNECTION TO RADIO	DUMMY ANTENNA	ADJŲST	VACUUM TUBE VOLT METER CONNECTION TO RADIO	ADJUST TO
100 Mc. Use about 15 microvolts	FM Antenna lead	300 ohms	C7 Osc. C2 Ant.	Pin No. 7 of 6AL5 and Ground	Resonance about 3 volts

NOTE: If a signal generator with the above fundamental frequency is not available, it is sometimes possible to use harmonics. Use extreme care in picking harmonics. An alternate procedure is.

1

to use a local station carrier of known frequency to align the FM Band and to use the vacuum tube volt meter as above for resonance indication. A weak carrier, however will not produce 3 volts.



MODELS 95F31, 95F31B, 95F31M AND 95F33 CHASSIS H5-38

HS-39

CHART I. ALIGNMENT PROCEDURE WHEN USING AM MODULATED SIGNAL

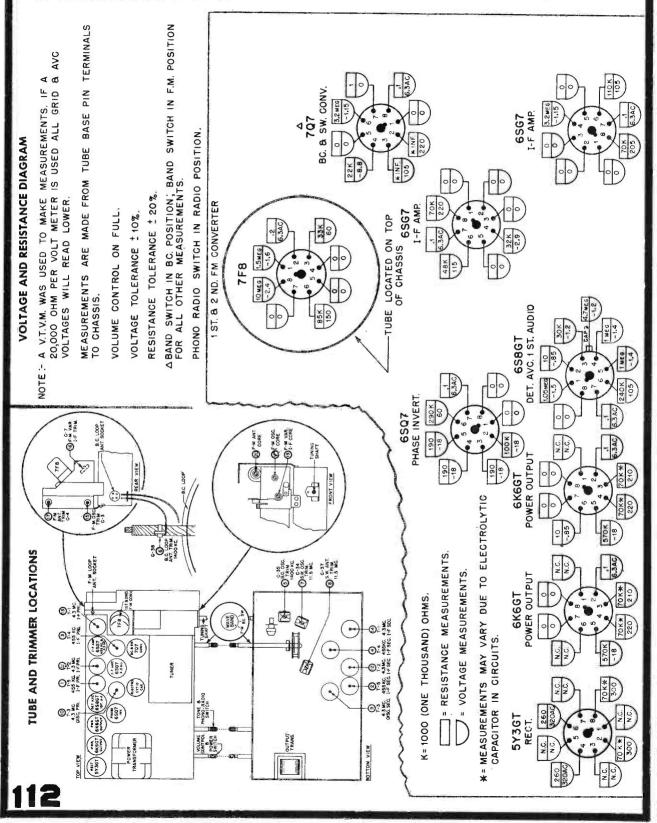
GENERATOR AND STANDARD OUTPUT METER FOR COMPLETE RECEIVER ALIGNMENT.

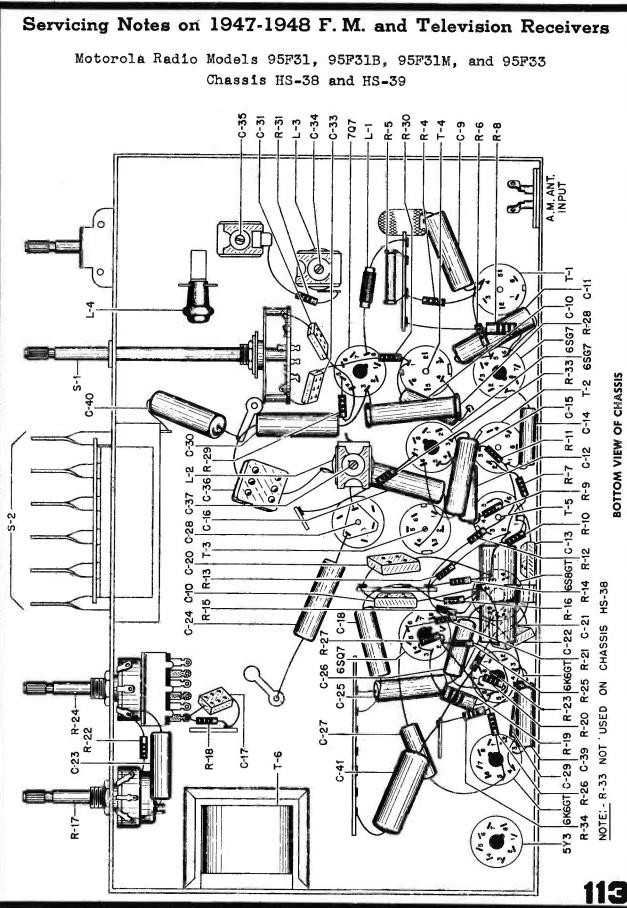
DIAL BAND SET SW. STEP TO SET TO	DUMMY	SIGNAL GENERATOR CONNECTED TO	SIGNAL GENERATOR SET AT	ADJUST TRIMMER OR CORE	<u>REMARKS</u>
455 Kc I.F. CHANNEL	ALI GNME	 <u> NT</u>			
1, 1620 КС В.С.	,1 MF.	707 B.C. & S.W. CONV. GRID (PIN #4) & CHASSIS	455 KC	1, 2, 3 & 4	ADJUST FOR MAXIMUM OUTPUT
I I BROADCAST BAND ALIG	NMENT		4	2) 	
2, 1400 KC B.C.	.1 MF.	707 B.C. & S.W. CONV. GRID (PIN #4) & CHASSIS	1400 KC	5(B.C. OSC. TRIM)	SET O SCILLATOR TO DIAL. (ON CHASSIS HS. 38, MOUNT OR HOLD DIAL SCALE TEMPORARILY ON CHASSIS WITH GANG FULLY MESHED, POINTER SHOULD BE AT LAST MARK ON DIAL. THEN SET TO 1400 KC. AND SET OSCILLATOR.)
3, 1400 КС В.С.	NONE	RADIATION-1.00P .	1400 KC	6(B.C. LOOP ANTENNA TRIM.)	ADJUST FOR MAXIMUM OUTPUT
SW. BAND ALIGNMENT					
4. 11.5 MC S.W.	.1 MF	707 B.C. & S.W. CONV. GRID (PIN #4) & CHASSIS	11-, 5 MC	7(S.W. OSC. TRIM)	SET OSC. TO DIAL. MAKE SURE OSC. IS HIGHER IN FREQUENCY THAN THE SIGNAL BY CHECKING IMAGE RESPONSE WHICH SHOULD OCCUR WITH THE INPUT SIGNAL AT 12.41 MC.
5. 11.5 MC S.W.	50 MMF	S.W. ANT. TERMINAL AND CHASSIS.	11.5 MC	8(S.W. ANT. COIL TRIM)	B.C. LOOP PLUG SHOULD BE DIS- CONNECTED. ADJ. FOR MAXIMUM OUTPUT
4.3 Mc I.F. CHANNEL	ALI GNME	NT			
6. 10				9(DISC. SEC.)	DETUNE DISCRIMINATOR SECONDARY BY SCREWING CORE OUT AS FAR AS IT WILL GO.

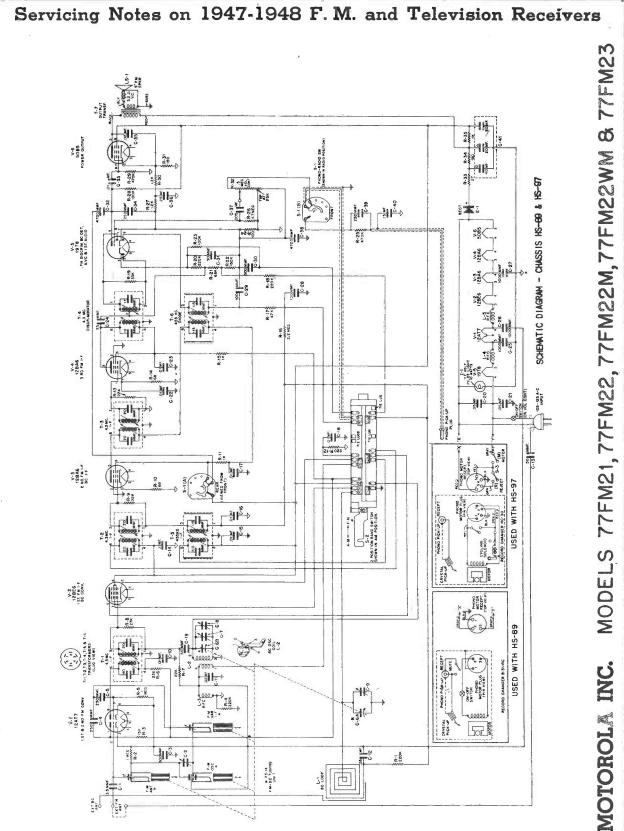
Ser	vicin	g No	tes o	n 1947-19	48 F. N	I. and	Television Receivers
STEP	DI AL SET TO	BAND SWL SET TO	DUMMY	SIGNAL GENERATOR CONNECTED TO	SIGNAL GENERATOR SETAT	ADJUST TRIMMER OR CORE	REMARKS
7.	112 MC	FM	.001 MF	7E8 2ND FM CONVERTOR GRID (#1 PIN) & CHASSIS	4.3 MC	10, 11, 12, 13 & 14 (4,3 MC 1.F.)	ADJUST FOR MAXIMUM OUTPUT
FM BAN	ND ALIG	NMENT					
8.						18 (FM OSC. CORE)	CHECK THE POSITION OF THE FM OSC. TUNING CORE 18. SET SPACING BE- TWEEN THE CORE AND BAKELITE PIECE TO WHICH IT IS MOUNTED. TO 1/32" BY TURNING TUNING CORE SLOTTED NUT.
9,	90 MC	FM	NONE	FM LOOP ANTENNA RECEPTACLE & CHASSIS RE- MOVE FM LOOP.	90 MC	15, 16 & 17 (FM OSC., ANT, & VARI- ABLE I.F. TRIM)	ADJUST FOR MAXIMUM OUTPUT
10 .	105 MC	FM	NONE	FM LOOP ANTENNA RECEPTACLE & CHASSIS RE- MOVE FM LOOP.	105 MC	18, 19 & 20 (FM OSC., ANT. & VARI- ABLE I.F. CORES)	ADJUST FOR MAXIMUM OUTPUT
11,							REPEAT STEPS 9 AND 10 SEVERAL TIMES UNTIL FURTHER ADJUSTMENT DOES NOT INCREASE THE OUTPUT. MAKE THE FINAL TRIMMER ADJUSTMENT AT 105 MC. (I.E., TRIMMERS 15, 16 AND 17 AT 105 MC).
12.	105 мС	FM	NONE	RADIATION LOOP *	105 MC	17 (FM ANT. TRIMMER)	ADJUST FOR MAXIMUM OUTPUT WITH FM LOOP ANTENNA CONNECTED.
ALIGN	DISCR	I MINATOR	I SECONDA	 <u>RY</u>	2		
13.		FM	.001 MF	CONVERTOR GRID (#1 PIN) & CHASSIS	4.3 MC	9(DISC. SEC.)	ADJUST DISCRIMINATOR SECONDARY FOR MINIMUM RESPONSE. THE CORRECT ADJUSTMENT IS THE SHARPLY DEFINED MINIMUM RESPONSE POINT BETWEEN THE TWO PEAKS.
	IMUM DIS	TANCE BE	TWEEN LOO	ERATOR TO A 5" D PS SHOULD NEVER	BE LESS THAN	12".	ADIATE SIGNAL INTO RECEIVER LOOP.

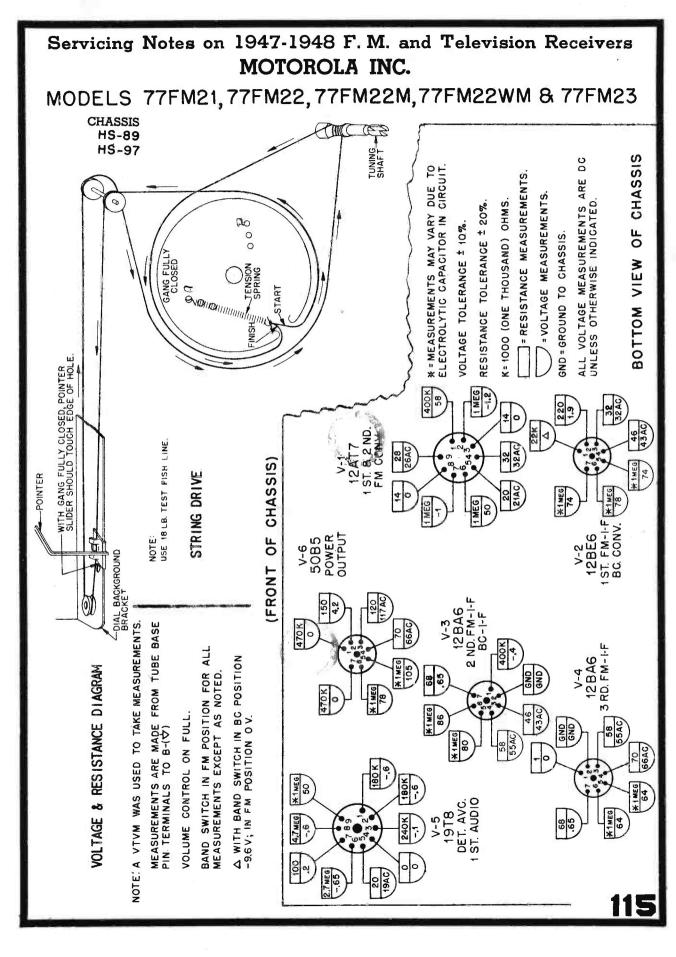
Motorola MERadio

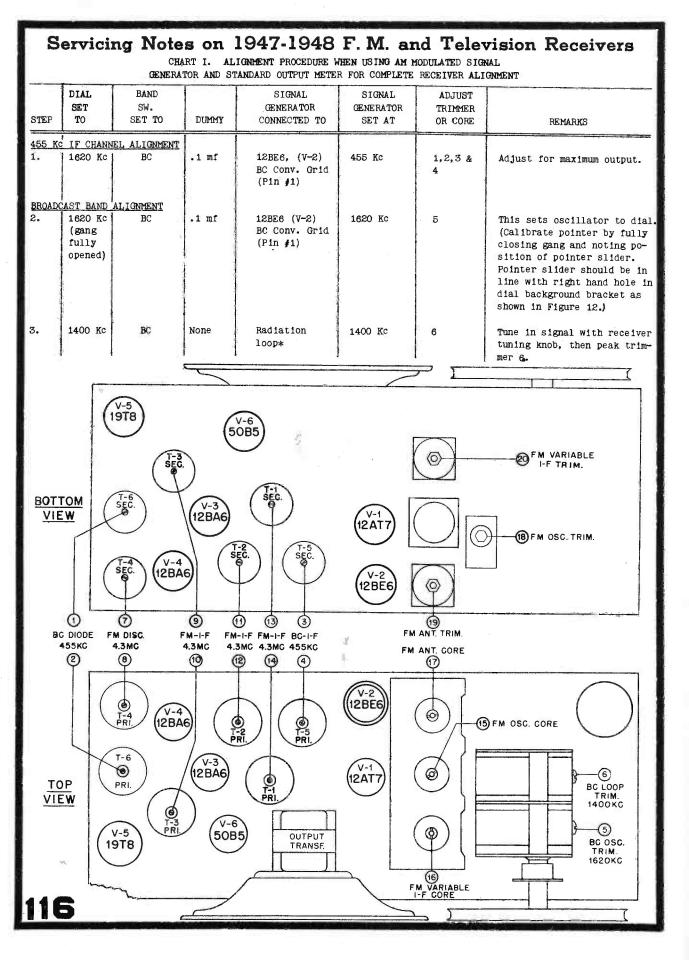
Models 95F31, -B, -M, & 95F33 Chassis HS-38, HS-39





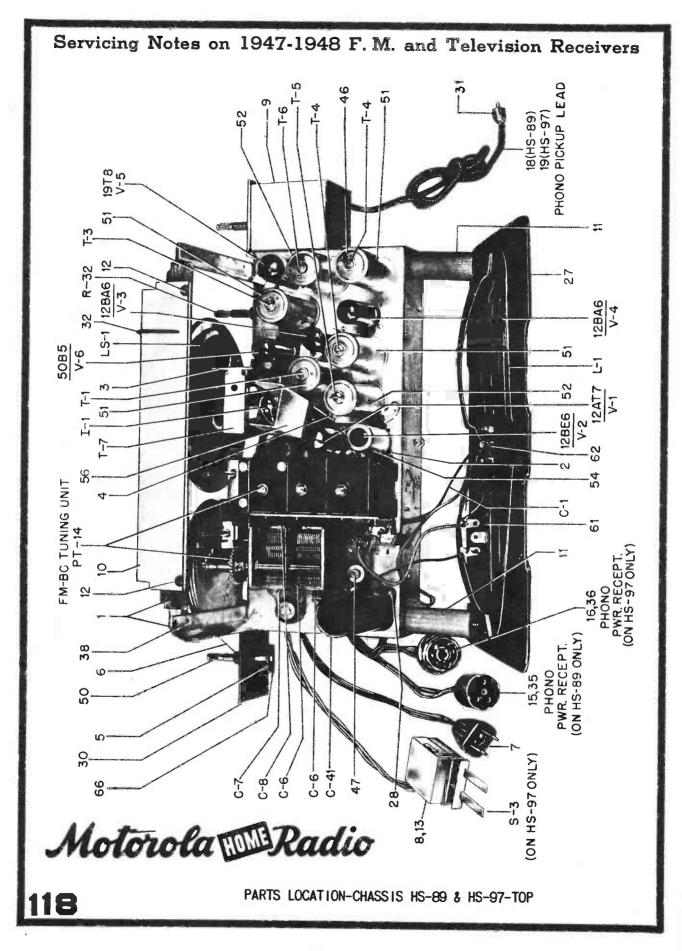


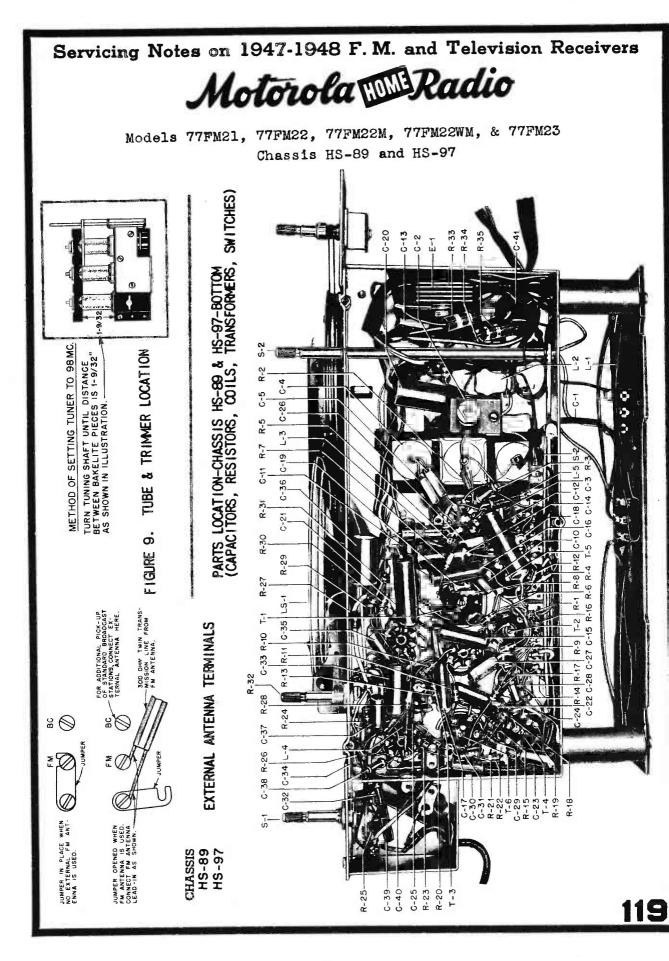




S	Servicing Notes on 1947-1948 F. M. and Television Receivers							
	(Alignment continued)							
STEP	DIAL SET TO	BAND SW. SET TO	DUMMY	SIGNAL GENERATOR CONNECTED TO	SIGNAL GENERATOR SET AT	ADJUST TRIMMER OR CORE	REMARKS	
	c IF CHANNEL	the second se	-	-	4	7	Detune discriminator secon- dary by screwing core out as far as it will go.	
5.	(extreme high fre- quency end)	FM	>001 mf	12AT7 (V-1) 2nd FM Con- verter Grid -(#7 pin)	4.3 MC.	8,9,10, 11, 12, 13 & 14	ädjust for maximum output.	
FM 8/	and alignment _	_	-	-	-	15	Check the position of the FM Osc. tuning core 15. Set spacing between the core and bakelite piece to which it is mounted, to two turns from tight by turning tuning core slotted nut.	
7.	98 MC	FM	None	FM Ant. ter- minal	.98 Mc	18	Tuner is set to 98 MC by moving cores out with tuning shaft until spac- ing between bakelite pieces is 1-9/32". See Figure 9. Peak 18 for maximum output.	
8.	90 Mc.	FM	None	FM Ant. ter- minal	90 MC	19 & 20	Tune in signal with re- ceiver tuning knob, then adjust 19 & 20 for maxi- mum output.	
9.	105 MC	FM	None	FM Ant. tér- minal	105 Mc	16 & 17	Tune in signal with re- ceiver tuning knob, then adjust 16 & 17 for maxi- mum output.	
10.	-	-	-	-			Repeat Steps 8 & 9 sev- eral times until further adjustment does not in- crease the output. Make the final <u>trimmer</u> adjust- ment at <u>105</u> Mc. (1.e., trimmers 19 & 20 at <u>105</u> <u>Mc</u>).	
11.	105 Mc	FM	None	Radiate sig- nal (or use station after performing Step 12)	105 Mc	19	Adjust for maximum out- put with built-in an- tenna connected.	
ALI 12.	GN DISCRIMINA	ITOR SECOND	.001 mf	12AT7 (V-1) 2nd FM Con- verter Grid (Pin #7)	4.3 Mc	7	Adjust discriminator secon- dary for minimum response. The correct adjustment is sharply defined minimum response point between the two peaks.	

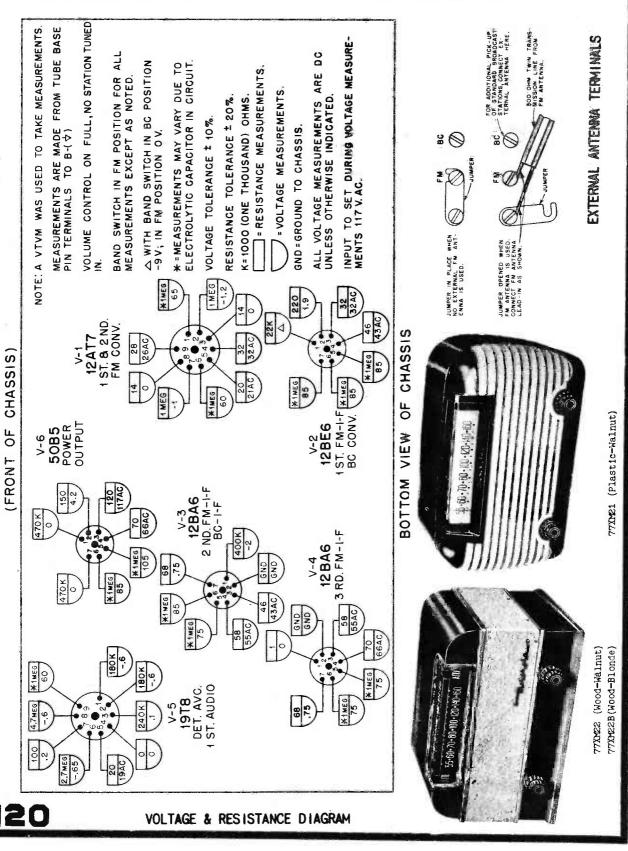
* Connect output of signal generator to a 5" diameter, 3 turn loop and radiate signal into receiver loop. Minimum distance between loops should never be less than 12".

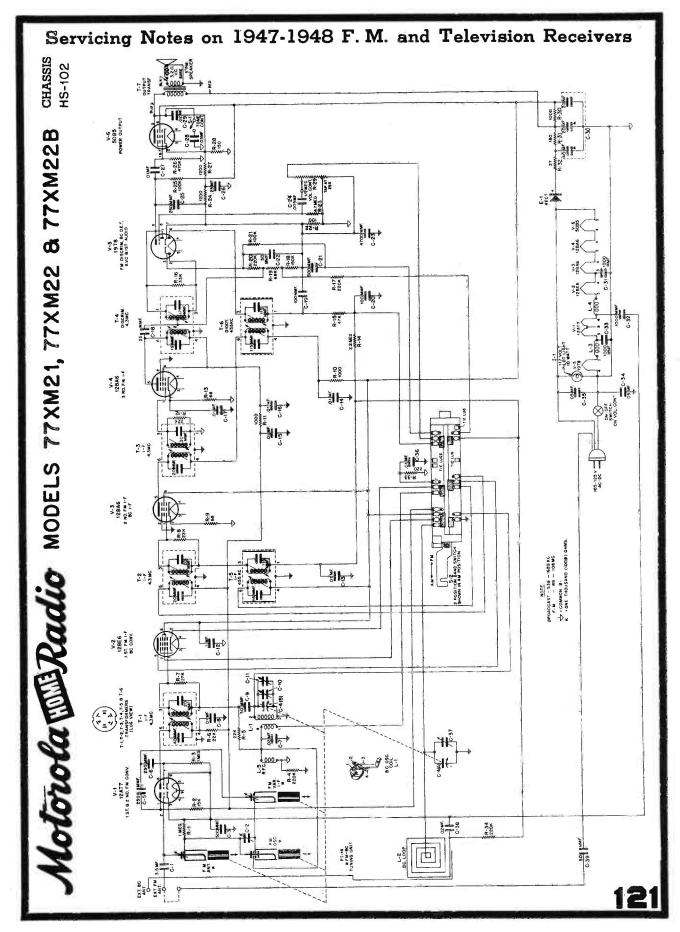




MOTOROLA INC.

Models 77FM21, 77FM22, -M, -WM, & 77FM23 Chassis HS-89 and HS-97





MOTOROLA INC. MODELS 77XM21, 77XM22 & 77XM22B

CHASSIS

HS-102

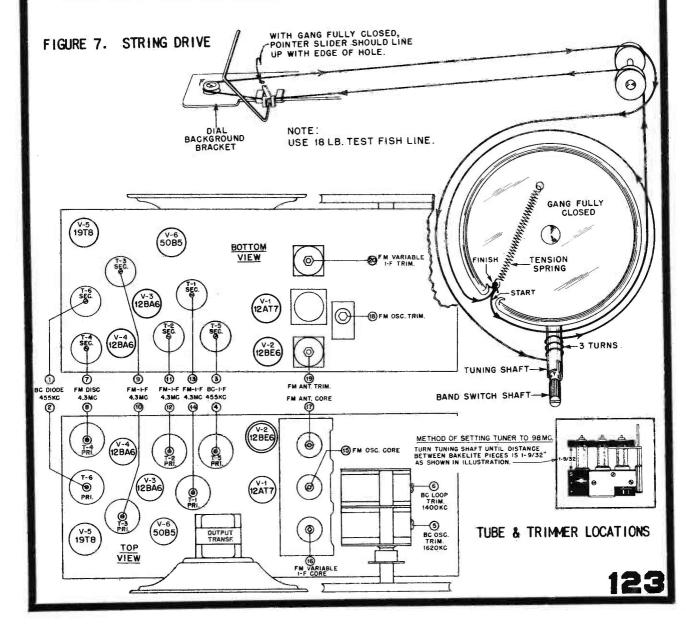
CHART I. ALIGNMENT PROCEDURE WHEN USING AM MODULATED SIGNAL GENERATOR AND STANDARD OUTPUT METER FOR COMPLETE RECEIVER ALIGNMENT

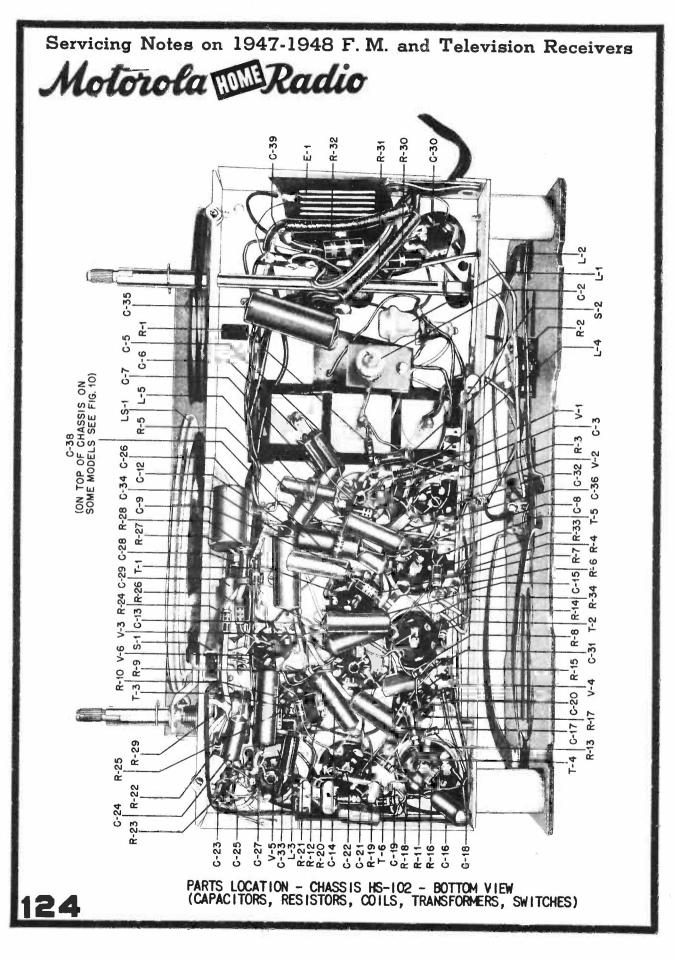
	GENERATOR AND STANDARD OUTPUT METER FOR COMPLETE RECEIVER ALIGNMENT						
STEP	DIAL SET TO	BAND SW. SET TO	DUMMY	SIGNAL GENERATOR CONNECTED TO	SIGNAL GENERATOR SET AT	ADJUST TRIMMER OR CORE	REMARKS
<u>455</u> 1.	KC IF CHAN 1620 KC	NEL ALIGNMEN BC	1 <u>7</u> .1 mf	128E6 (V-2) BC Conv. Grid (Pin #1)	455 Kc	1,2,3 & 4	Adjust for meximum output.
Broal 2.	CAST BAND 1620 Kc (gang fully opened)	ALIGNMENT BC	"1 mf	12BE6(V-2) BC Conv. Grid (Pin #1)	1620 Kc	5	This sets oscillator to dial. (Calibrate pointer by fully closing gang and noting po- sition of pointer slider. Pointer slider should be in line with right hand, hole in dial background bracket as shown in Figure 7.)
3,	1400 Kc	BC	None	Radiation loop*	1400 Kc	6	Tune in signal with receiver tuning knob, then peak trim- mer 6.
4.3 1	C IF. CHANN	EL ALIGNMEN	TT I				
4.		-	-	ano,	-	7	Detune discriminator secon- dary by screwing core out as far as it will go.
5.	(extreme high fre quency e		.001 mf	12AT7 (V-1) 2nd FM Converter Grid (#7 Pin)	4.3 Mc	8,9,10,11, 12, 13 & 14	Adjust för maximum output.
EM <u>Ba</u> 6.	ND ALIGNME -	<u>.</u>	-	*	-	15	Check the position of the FM Osc. tuning core 15. Set spacing between the core and bakelite piece to which it is mounted, to two turns from tight by turning tuning core slotted nut.
7.	98 Mc	Fht	None	FM Ant. terminal	98 Mc	18	Tuner is set to 98 Mc by moving cores out with tuning shaft until spacing between bakelite pieces is 1-9/32". See illustration. Peak 18 for maximum output
8.	90 Mc	FM	None	FM Ant. terminal	90 Mc	19 & 20	Tune in signal with receiver tuning knob, then adjust 19 and 20 for maximum output.
9.	105 Mc	FM	None	FM Ant. terminal	105 Mc	16 & 17	Tune in signal with receiver tuning knob, then adjust 16 and 17 for maximum output.
10. 12	2	-	-	-	-	-	Repeat steps 8 & 9 several times until further adjust- ment does not increase the output. Make the final <u>trimmer</u> adjustment at <u>105</u> Mc. (1.e., trimmers 19 & 20 at <u>105 Mc.</u>)

ALIGNMENT (cont'd)

STEP	DIAL SET TO	BAND SW. SET TO	DUMMY	SIGNAL GENERATOR CONNECTED TO	SIGNAL GENERATOR SET AT	ADJUST TRIMMER OR CORE	REMARKS
11.	105 Mc	FM	None	Radiate signal (or use station after performing Step 12)	105 Mc	19	Adjust for maximum output with built-in antenna con- nected.
ALIGN 12.	DISCRIM	INATOR SECC FM	0001 mf	12AT7 (V-1) 2nd FM Converter Grid (Pin ∦7)	4.3 Mc	7	Adjust discriminator secon- dary for minimum response. The correct adjustment is sharply defined minimum response point between the two peaks.

* Connect output of signal generator to a 5" diameter, 3 turn loop and radiate signal into receiver loop. Minimum distance between loops should never be less than 12".





Motorola Television Receivers VT-71 and VK-101 Chassis TS-3

Motorola Models VT-71 and VK-101 Television receivers use 29 tubes including a 10" picture tube. Antenna receptacle is provided for either a 75 ohm unbalanced or 300 ohm balanced line. The picture I.F. is 26.4 MC. and sound I.F. is 21.9 MC. The description of the receiver will be divided into sections and reference should be made to the complete circuit diagram or to other illustrations as instructed. The material presented here is supplied through the courtesy of Motorola, Inc., and is of preliminary nature. A great deal of knowledge of modern television design can be obtained by the serviceman in carefully studying this material.

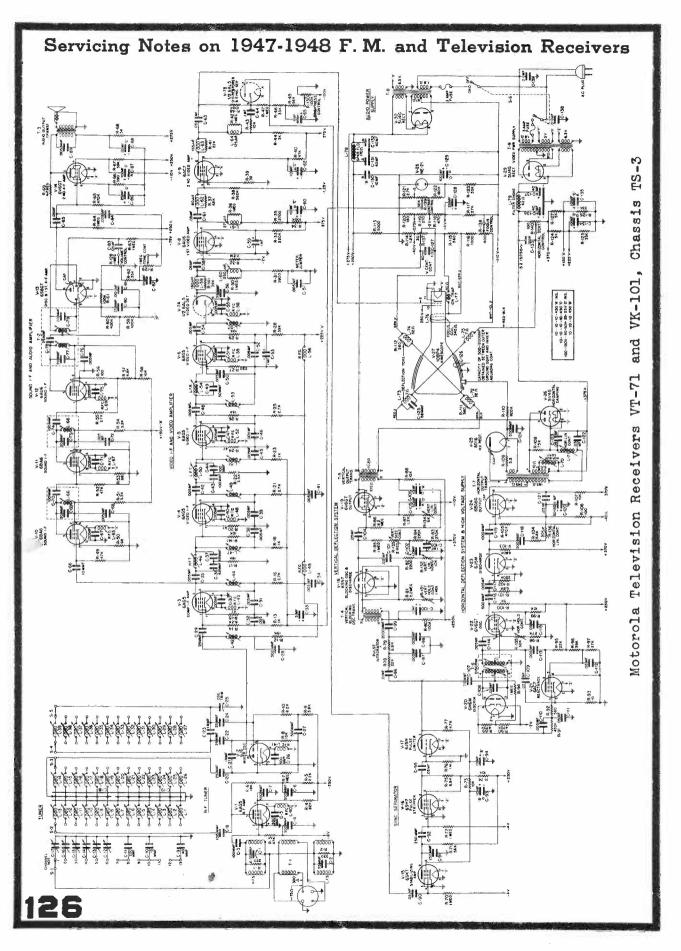
The R.F. tuner permits the selection of any one channel of the 13 television channels existing between 44-88 and 174-216 MC. A waveband switch is used. The resonant circuits involved are designed to pass a band of about 4.5 MC. The overall receiver band pass is about 3.5 MC. as it is reduced by that of the I.F. system. See the upper left hand corner of schematic diagram.

The secondary consists of a high and low frequency winding in series to provide more constant impedance over the entire television band and to avoid reflections which would produce ghost images in the picture. Channels one through six are tuned by connecting capacitors C17, C16, C15, C14, C13, C12, respectively, across the low frequency winding L.F.S. These are trimmer condensers and each is pre-tuned at the factory to a specific frequency in each channel. The high frequency winding (H.F.S.) being a very small inductance has negligible effect on the tuning of the low channels.

For channels seven through thirteen, the low frequency winding is effectively shorted out of the resonant circuit by means of connecting capacitors Cll, ClO, and C9, respectively, across this winding. Capacitor C2 which is permanently connected across the low frequency coil, resonates the coil above channel six and serves to short the coil more effectively in the upper channels because of the series inductance present in the wave-band switch. Resistors Rl and R2 are used to secure a more constant input impedance.

The R.F. amplifier employs a critically coupled double tuned circuit. The mutual coupling is provided by capacitors Cl8 and Cl9. Each pair of coils, such as Ll3-Ll4 of the coils numbered from Ll to L26, is pre-tuned at the factory to the same frequency in each channel by means of a brass slug.

This type of double tuned circuit is similar in performance to that of the double tuned I.F. transformer of the average broadcast receiver. The difference is that a capacitive mutual impedance rather than an inductive mutual impedance is used. The degree of coupling which determines the bandwidth of the pass band is controlled by the size of the capacities of C18 and C19. The smaller the size of this capacity, the greater will be the mutual impedance and the greater will be the bandwidth; however, if coupling exceeds critical coupling, a double hump will occur in the response. In these receivers, C18 and C19 are so chosen that critical coupling is obtained in each channel, and provides a pass band of approximately 4.5 MC. measured between frequencies for which the output is 3 DB. down or .7 of the output at the resonant frequency.



The double capacitor C18 and C19 is composed of two large circular plates with a third circular plate sandwiched between them and insulated from the two outer plates by mica sheets. The two outer plates are grounded and represent one side of the capacitor. The inner plate represents the other side of the capacitor. The coupling condensers C8 and C20 are used to keep D.C. off the exposed coils.

The oscillator circuit (the right hand section of the diagrammed 6J6, V2), is a Colpitts circuit in which the voltage developed across the grid-cathode capacity provides the feed-back voltage necessary to maintain oscillation. Capacitor C25 is a small variable condenser which is provided for the operator to permit fine tuning of the receiver to the sound carrier. The major change in frequency required in channel selection is obtained through selection of the proper oscillator coil of which there are thirteen. These coils are adjusted at the factory. Capacitors C22 and C24 keep the D.C. plate voltage off the exposed coils. The very small capacity provided by C23 has a temperature compensating characteristic and is used to reduce oscillator frequency drift.

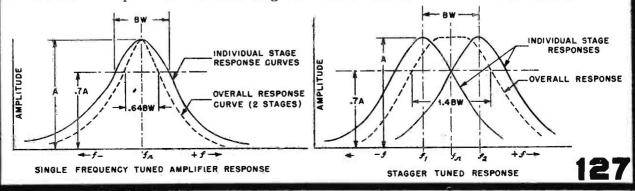
The mixer circuit employs a triode tube (the other section of the 6J6) V2. Some oscillator voltage injection occurs through the common cathode lead inductance; however, coupling capacitor C21 provides the principle source of injection voltage. The plate circuit of the mixer is resonated by Video I.F. coil L42 to a frequency of 23.5 MC.

The sound I.F. amplifier has three stages of amplification and a limiter. The first stage using V3, is actually the first amplifier stage of the video I.F. amplifier system. The second and third stages (V10 and V11) are single iron-slug tuned coils which resonate a fixed capacitor of 20 mmfd. and the tube capacities to the operating frequency of 21.9 MC.

The limiter grid resistor R55 is kept small so that the time constant of it and the capacitor C74 will be small; hence, when ignition interference is present and tends to drive the limiter grid positive, the capacitor C74 will not store the energy very long and the interference will be reduced.

The discriminator circuit is conventional as used in F.M. receivers. The circuit uses a novel method for introducing the primary voltage into the secondary circuit and does away with the R.F. choke usually placed between the center tap of the secondary and center of the load. Resistor R61 and capacitor C81 produce audio frequency de-emphasis necessary because in the F.M. transmitter the "highs" are over emphasized.

The audio amplifier is conventional and consists of a triode voltage amplifier 6S8, V13 driving a 6V6, V14 in the power stage. Resistor R69 provides audio degeneration which reduces distortion.

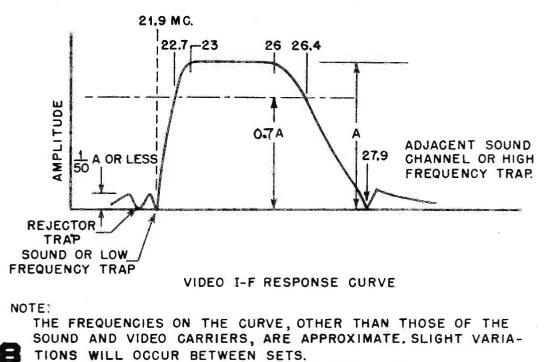


The video I.F. amplifier, sometimes referred to as the wide-band amplifier, is designed to provide gain and a bandwidth of approximately 4 MC. (at .5 down) to the picture I.F. frequencies. It must also reject the sound I.F. frequencies so as not to cause sound interference in the picture. Wide-band response and gain are accomplished by means of a 5-stage stagger-tuned system, four amplifiers and the mixer. Basically, a stagger-tuned amplifier is one in which each single tuned stage resonates at a different frequency in the pass band. The overall response of all the stages is then considerably wider than would be achieved with all the stages tuned to the same frequency, and the overall gain is still as high. See figure on page 127.

To vary the gain of the video I.F. amplifier the bias of the first three stages is changed, and is accomplished by means of the CONTRAST control. This nomenclature is used, as varying the amount of video signal reaching the kinescope grid determines the amount of black and white appearing in the picture.

It is necessary to prevent the sound I.F. frequencies from reaching the video detector and the sound from getting into the picture. This is accomplished by means of the Low Frequency Trap (L.F.T.) L50 in the video I.F. amplifier which reduces the response to the sound I.F. frequencies to 1/50 or less than that of the video I.F. frequencies. This causes the low frequency skirt of the video I.F. response to become very steep, see figure.

The trap is made up of components L50, C43, C44, and R22 and is located in the 2nd Video I.F. amplifier stage. By resonating this trap to the sound I.F. carrier frequency 21.9 MC., a negative resistance is produced which equals the value of R22 and results in a short to ground at this frequency. This results in high attenuation of the sound carrier and its side bands. In alignment the signal generator is set at the sound I.F. carrier and L50 is adjusted for minimum current in the video detector circuit.



As the sound I.F. trap does not reduce the response sufficiently to frequencies below the sound carrier, which could result in interference from any stations operating at these frequencies, a low frequency rejector trap has also been included. This rejector trap composed of L54 and C49 resonates to 21 MC.

To eliminate interference in the picture resulting from the sound I.F. carrier of the adjacent television channel which is 27.9 MC., a trap has been included to attenuate this frequency to 1/50 or more of the frequencies in the pass band. This trap is of the same type as that used for eliminating the sound I.F. frequencies and is located in the 1st I.F. amplifier stage. It is composed of L46, C36, C37 and R17. In alignment it is tuned for minimum current in the detector circuit at 27.9 MC.

Please notice that the first and second I.F. stages which contain the high and low frequency traps, have two shunt tuning coils. In each of these stages, both coils are effectively in parallel and determine the net tuning inductance; the reason for two is that they improve the performance of the traps. Two shunt coils were found unnecessary for the third stage containing the low frequency rejector trap.

The video detector uses one section of the 6AL5, V7A which is a double diode tube. The signal voltage is applied to the cathode producing a negative polarity video voltage across the diode load R31. This load is only 3900 ohms in order to prevent the shunting tube capacities from affecting the high frequency video response. A video response of approximately 4.5 MC. is desired. The inductances L59 and L60 are peaking inductances which resonate with the tube capacities and C56 and extend the frequency response.

The video amplifier is a two stage resistance coupled system. It is similar in operation to that used for audio amplification except that the frequency response is much greater being approximately 4 MC. This high frequency response is achieved by using small plate loads and peaking L59 to L64 coils which resonate the tube capacities.

One other aspect of video amplifiers is the ability to pass the signal without introducing phase shift. Phase shift causes distortion due to improper displacement of picture elements. Phase shift at low frequencies is caused by the reactance of the plate to grid coupling capacitors. To compensate for this phase shift, the resistor-capacitor network R34 and C60 is used. This network introduces compensation by increasing the effective plate load at low frequencies.

To limit the amplitude of noise bursts and auto ignition type of interference which would smear the picture and upset the synchronization, the D.C. plate and screen voltages of the 4th video I.F. tube and 1st video amplifier have been lowered. The use of a two stage video amplifier system also aids in reducing trouble from noise in that large noise amplitudes out of the detector operate in the cut-off region of the 1st video grid. Stabilizing the 4th I.F. amplifier plate return with a large capacitor C53 also helps reduce noise streaks in the picture.

D.C. restoration is necessary because the video amplifiers are not directly coupled and cannot pass the D.C. component present in the video signal received from the detector. The D.C. component is that which determines the average brightness of the picture and its magnitude is dependent on whether a light or dark picture is being televised at the station being received. Since the video stages are **1**

capacitively coupled, the D.C. component is not passed; but only the A.C. component which is the variation about the D.C. component. This subject receives detailed treatment in the lecture on Television in "Advanced Radio Servicing" by M. N. Beitman.

In the Motorola television sets, the D.C. restorer consists of the second section of the 6AL5 double diode V7B used in the video detector circuit and is connected into the grid circuit of the kinescope. The D.C. restorer load is R47 across which a positive voltage is developed when the video signal is applied. The positive restorer voltage reduces the negative voltage applied by the Brightness Control R130 and determines the average brightness. Since the diode is connected with its plate below its cathode on the resistor string, it will conduct only on the negative amplitude of the video signal. This means that the D.C. restorer voltage produced across R47 will be nearly that of the negative amplitude. The D.C. restorer voltage is maintained for a time approximately a frame period, because during the period that the restorer diode is conductive, condenser C64 is charged to the D.C. voltage developed across R47; and when the tube is non-conductive, this charge must leak through a resistive path made up of R47, R46, R44 and Since R47 is particularly high, it takes a comparatively long R43. time for the D.C. voltage on C64 to change.

In order to synchronize the sweep voltages of the horizontal and vertical deflection systems, it is necessary to first separate the synchronizing pulses from the video component. By taking the Sync. Amplifier input voltage from a point in the kinescope grid circuit below the D.C. Restorer, the D.C. Restorer tube aids in the Sync. sep-This action comes about from the difference in Sync. Ampliaration. fier input voltage when the tube is conducting as compared to when it is not. To understand this action, consider the method of obtaining the Sync. Amplifier input voltage. It is seen to be the voltage developed across R46, R45, and R130 are by passed by capacitor C65. the positive half of the video signal applied to the D.C. Restorer, On the Restorer tube V7B does not conduct as its plate is then negative with respect to its cathode. The Sync. Amplifier input voltage is then the fraction 33/1043 of the kinescope grid voltage or voltage across R44 and, as can be seen, is quite small. On the negative half of the video signal, the Restorer tube conducts and presents a series impedance of several hundred ohms. This effectively shunts R47 and makes the Sync. Amplifier input voltage 33/43 of the kinescope grid voltage. This means that approximately 24 times as much Sync. signal is applied to the Sync. Amplifier on the negative half of the video signal which contains the Sync. pulses and some video than on the positive half which contains mainly the video component. Because of the presence of some video component on the negative half of the composite signal, the Sync. input voltage still contains an appreciable amount of video and further stripping is necessary.

The Sync. Separator removes the synchronizing pulses from the composite video signal. It also stabilizes and limits the amplitude of the synchronizing pulses so that a constant pulse amplitude is applied to the deflection systems for a weak or strong video signal. It is a three-stage system containing a pulse stabilizing amplifier, a pulse stripper, and a pulse limiter.

The purpose of the pulse stabilizing amplifier is to amplify the "Sync" pulses and also stabilize the output so that the output will tend to remain constant for a wide range of input voltages. This

stabilization or compression is accomplished by operation over non-linear portion of the plate current-grid voltage curve.

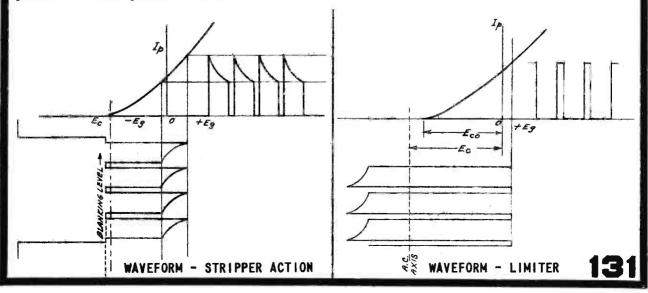
V-15 is a 6SK7 tube and has a remote plate current cut-off characteristic. The signal received from the kinescope is of negative polarity and tends to drive the tube toward plate current cut-off. With a weak signal, the "Sync" pulse operates over the relatively high gain portion of the curve, while on large signals, the "Sync" pulse operates over a lower gain portion of the curve. The result is a more constant "Sync" pulse amplitude.

The pulse stripper stage of the Sync. Separator V16 clips the signal at just above the blanking level and removes all of the video comonent from the "Sync" pulses. This is accomplished by driving the grid of the Stripper positive. A negative bias voltage proportional to the "Sync" signal is developed across grid resistor R72 and this bias is of such value that plate current flows only during the peak portion of the signal received from the stabilizing amplifier.

The shunt capacitor C91 serves to reduce the high frequency components of the video signal reaching the grid of the stripper. The coupling capacitor C92 is made small to discriminate against low frequency voltage changes that would cause the "Sync" pulses to move up and down and cause the picture to jitter. However, the use of a small coupling capacitor causes differentiation of the vertical pulse group, that is, the grid coupling condenser C92 charges up rapidly on the wide vertical pulses which causes the pulse at the grid to have a saw-tooth shaped top, as shown in the left hand figure at the bottom of the page.

The pulse limiter stage flattens the top of the vertical pulses received from the clipper so that a good square shaped pulse is applied to the integrating circuit which provides the resultant vertical pulse that "Syncs" the vertical blocking oscillator. It also helps provide a more constant pulse amplitude for change of signal input level.

A 6J5 triode V17 is used and is operated at zero bias. The "Sync" pulse applied is negative going but the coupling condenser C95 produces an A.C. axis which because of the width of the pulses and the short interval between pulses is located close to the top of the "Sync" pulses. The positive component is then very large and drives the grid positive producing a bias voltage across R76 which is quite large, see figure at right below on this page. This bias voltage is represented by E_c . The top part of the pulse which as the saw-tooth shape then falls beyond the cut-off point and is, therefore, clipped producing a square pulse in the plate circuit.



The vertical deflection system generates the 60 cycle saw-tooth voltage. It is a four circuit arrangement involving three tubes. It consists of a pulse integrator, a blocking oscillator, a discharge tube, and an output amplifier. The pulse integrating circuit generates one large pulse from the vertical group of six pulses contained in the composite video signal. This integrated pulse is then used to synchronize the blocking oscillator. The blocking oscillator generates a large positive pulse which is applied to the discharge tube grid and makes it conductive. This tube then discharges a capacitor across which the saw-tooth sweep voltage is developed. The output amplifier converts this sweep voltage into the sweep current that is used to deflect the kinescope beam.

The pulse integrator circuit consists of a double RC filter in the grid return circuit of the vertical blocking oscillator. It is composed of resistors R78 and R79 and capacitors C97 and C98, see the schematic diagram. The vertical group of pulses consisting of six equalizing followed by six field pulses and then six more equalizing pulses is applied to the integrator through capacitor C96. The time constants of R78 and C97, R79 and C98 are so large that capacitors C97 and C98 charge very little during each equalizing pulse period. As the interval between equalizing pulses is larger than the pulse period, any charge due to the equalizing pulses leaks off. During the periods of the six field pulses, however, capacitors C97 and C98 are charged appreciably since the field pulses are quite wide, further since the interval between field pulses is very short, very little of the charge can leak off before the next pulse is applied. The result is the charge builds up on each field pulse creating a pulse of sufficient size to reduce the negative voltage on the grid of the blocking oscillator tube to a value less than cut-off and starts the oscillator cycle. The vertical "sync" pulse built up in the integrator leaks off in the long interval between vertical pulse groups.

The blocking oscillator is a regenerative arrangement. The oscillator tube which is one section of a 6SN7, V18 has its plate circuit coupled to its grid circuit by means of the transformer T4. This oscillator produces a varying voltage on the grid that is used to control the discharge tube. The circuit arrangement produces a very sharp positive grid voltage rise. The peak value is limited by grid saturation. The positive grid voltage gradually drops from the peak until a reversed action takes place and the grid voltage drop through negative values to cause plate current cut-off. The negative charge on C99 prevents immediate reversal of the action. The action would reverse in time and continue even without the "sync" pulse, but this pulse triggers the action and produces these oscillations, at the same frequency as the vertical synchronizing pulses.

The discharge tube is the second section of the 6SN7, V18, used as the blocking oscillator. Its grid is tied directly to that of the blocking oscillator grid so that during the non-conduction period of the oscillator it is also cut-off. Capacitor C101 then charges through resistors R133, R85, R82 and R132. Capacitor C101 continues to charge until the positive pulse produced by the blocking oscillator causes the discharge tube to conduct which discharges capacitor C101 quickly through the tube plate resistance and resistors R82 and R132. Resistor R82 and the variable resistor R132 are placed in series with capacitor C101 in order to produce a saw-tooth voltage of the shape

necessary to produce a linear change of current in deflection coils which contain both resistance and inductance.

The variable resistance R133 serves to control the size of the sweep voltage since it determines the time constant or rate at which the capacitor charges. The variable resistance R132 is a linearity control as it determines the amplitude of the square pulse component which produces linear current through the inductance of the deflection coil. Indirectly it also affects the size so a readjustment of the size control is usually necessary when the linearity control is changed.

The output amplifier V19 is a power stage and serves to convert the voltage wave into a current wave of the same shape. This is done by means of the output transformer in the plate which is a step down transformer of approximately 8/1. The second linearity control R134 affects the bias of the 6V6 output tube and, therefore, controls the linear operating characteristic of the output stage. It tends to correct for any non-linearity in the sweep voltage applied to the grid or any non-linear deflection characteristic of the kinescope.

Resistances Rlll and Rll2 shunted across the vertical deflection coils serve to dampen any oscillation which might occur in these coils as a result of the distributed capacity resonating with the coil inductance. The Vertical Centering Control is the potentiometer Rl37 and controls the amount of D.C. current through the vertical deflection coils L72 and L74.

The horizontal deflection system generates the horizontal sweep current. The shape of this current is similar to that in the vertical deflection coils, but its frequency is much higher being 15,750 c.p.s. It also incorporates an automatic frequency control system (AFC) for synchronizing the generated sweep voltage to the frequency of the line "Sync" pulses. It differs from the vertical "Sync" method in that horizontal synchronization is not determined by each consecutive line pulse but rather by the frequency of the line pulses, thereby, reducing considerably the interference caused by noise pulses which tend to upset synchronization.

The deflection system also contains a discharge tube V23 for generating the desired shape of sweep voltage and an output amplifier V24 to convert the voltage wave into a current wave in the deflection coils. The output amplifier performs one other function and that is to generate a high pulse voltage which is rectified and used on the anode of the kinescope.

A very high voltage results in the transformer T-7 winding from the rapid change in plate current when the discharge tube is cut-off during the retrace time. By using an auto-transformer arrangement in the primary, a very high pulse voltage of approximately 10,000 volts is developed, which is rectified by tube V25 and is applied to the kinescope anode. Capacitor Cl24, Resistor Rl10 and the capacity between the inner and outer Aquadag coating on the kinescope glass, Cl26, provide a filter circuit that eliminates the 15,750 c.p.s. ripple voltage which would otherwise exist.

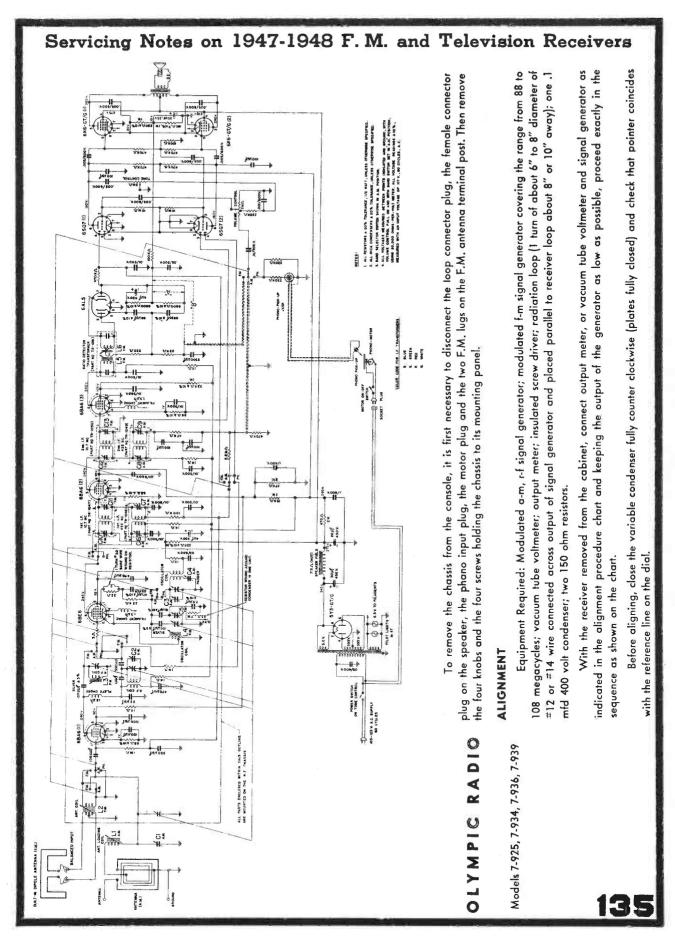
Cathode ray tubes using magnetic deflection present the problem of burning the screen by the negative ions existing in the beam. These ions are thousands of times heavier than the electrons and though charged are little affected by the magnetic field. In an electrostatic deflection system the ions are also acted on by the electron fields, so this problem does not exist. To prevent the dark spot resulting from the burning of the screen by the ions, the electron gun of the 10BP4 magnetic type cathode ray tube used in this receiver is located in the tube at a slight angle to the axis of the tube. This causes the beam to strike the side of the tube rather than the face. By using the Ion Trap which is a small double coil arrangement mounted

on the neck of the tube, a magnetic field is set up that acts on the electrons in the beam and bends them so that they strike the tube face.

The alignment procedure is not included in this text since our main objective in this instance was to give the general theory of operation. Because stagger-tuned I.F. system is used, the alignment frequencies and procedure is critical.

Faults in a television receiver can be localized by examining various raster distortions, or limitations in the quality of the picture obtained. The hints given below are suggestive and can be applied to other television receivers. It is recommended that you study these possible faults by referring to the diagram on page 126.

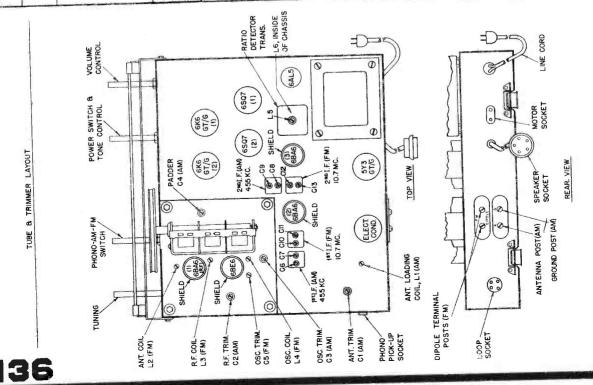
No Raster on Kinescope	Signal at Kinescope Grid, But No Syr
Ion trap out of adjustment V22, V23, V24, or V25 defective No high voltage T7 defective	Too much video I.F. gain Open C90 Defective V15, V16, V17
(open or shorted primary, open V25 fil. winding)	Raster, but No Sound, Pict. or Sync
Defective V26 or 10BP4	Defective R.F. Amplifier R.F. oscillator dead
Small Raster	Defective V3, open C29
Low V24 or V29	Ant. coil pri. shorted to ground
Partial short in T7 Shorted C122 or C123	Picture Stable but Poor Resolution
Low B voltage	Open L59, L62, L63, or L60 Video I.F. out of alignment
Open ClO5 or ClO6 Low line voltage	R.F. tuner much out of alignment
now line volvage	Picture Smeared
Trapezoidal Raster	Video I.F. bandwidth excessive
Improper Ion Trap adjustment Poor focus coil adjustment Defective yoke	Video stages overloaded Low bias voltage on V8 & V9 Condensers C61 or C63 leaky
No Horizontal Deflection, Vert. 0.K	Low Video Sensitivity
Open 173 or L75 Open secondary T7	Weak tubes in R.F., video I.F. Improper video I.F. & R.F. align.
No Vertical Deflection, Horiz. O.K.	Shorted Ant. coil pri. to ground
Open L72, L74, C100 Open or shorted T5	Sound "Bars" in Picture
Defective V18 or V19	Fine tuning control improperly set Low freq. trap L50 adjustment
Open or shorted T4	L50 open or shorted
Poor Horizontal Linearity	C43 or C44 shorted or open
Improper adjustment of R136, L70 Defective V24 or V26	Low Screen Intensity
Defective V24 or V26	Weak V24 or V23 tube
Defective V24 or V26 No Sound, Picture O.K.	Weak V24 or V23 tube Partially shorted T7
Defective V24 or V26 No Sound, Picture O.K. Open speaker voice coil Defective V14, V13, V12, V11, V10	Weak V24 or V23 tube Partially shorted T7 Improper Ion Trap adjustment Defective V26 or V25 tube
Defective V24 or V26 No Sound, Picture O.K. Open speaker voice coil Defective V14, V13, V12, V11, V10 Improper R.F. osc. frequency	Weak V24 or V23 tube Partially shorted T7 Improper Ion Trap adjustment Defective V26 or V25 tube Open Cl21 or Cl20 condenser
Defective V24 or V26 No Sound, Picture O.K. Open speaker voice coil Defective V14, V13, V12, V11, V10	Weak V24 or V23 tube Partially shorted T7 Improper Ion Trap adjustment Defective V26 or V25 tube



Servicing Notes on 1947-1948 F. M. and Television Receivers OLYMPIC TRU-BASE RADIO

Models 7-925, 7-934, 7-936, 7-939

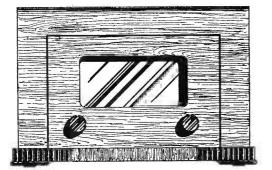
				ALIGNMENT PROCED	URE CHART		
	SET BAND SWITCH	CONNECT HIGH SIDE OF SIGNAL GENERATOR TO-	SET SIGNAL GENERATOR TO-	TURN POINTER TO-	READ OUTPUT ON-	ADJUST THE FOLLOWING- (KEEP SIGNAL FROM SIGNAL GENERATOR AS LOW AS POSSIBLE).	
	ON-				VACUUM TUBE VOLTMETER ACROSS 6800 OHM RESISTOR (SEE "A" ON CIRCUIT DIAGRAM).	L5 (RATIO DETECTOR) FOR MAXIMUM READING.	
١	F.M.	PIN 1 OF 6BA6 (3) TUBE FOR 1 VOLT SIGNAL.	IO.7 M.C.		VACUUM TUBE VOLTMETER ACROSS "B" ON CIRCUIT DIAGRAM.	L6 (RATIO DETECTOR) FOR ZERO READING.	
2	F. M.	PIN 7 OF 6BE6 TUBE	SIGNAL.	EXTREME RIGHT HAND POSITION, (CONDENSER	VACUUM TUBE VOLTMETER	C13 AND C12 (2mm LE TRANSFORMER) FOR MAXIMUM READING.	
		IN SERIES WITH A IMFD., 400 VOLT CONDENSER.		PLATES FULLY OPEN).	ACROSS 6800 OHM RESISTOR (SEE "A" ON CIRCUIT DIAGRAM).	C11 AND C10 (1 at. I.F. TRANSFORMER) FOR MAXIMUM READING.	
3	F.M.	R.E SECTION OF VARIABLE				C9 AND C8 (2mm. LE TRANSFORMER) FOR MAXIMUM OUTPUT.	
4	A.M. A.M.	CONDENSER OR PIN 7 OF THE 6BE6 TUBE IN SERIES WITH A 1 MFD.,400 VOLT	455 KG.		OUTPUT METER ACROSS SPEAKER VOICE COIL.	C7 AND C6 (1 m. I.E. TRANSFORMER) FOR MAXIMUM OUTPUT.	
ů.,		CONDENSER.		REPEAT STEPS 2 AND	3.		
6	F.M.	ANTENNA SECTION OF	1700 KG.	1700 KC. ON DIAL.		C2 (OSCILLATOR TRIMMER) FOR MAXIMUM OUTPUT.	
7	A.M.	VARIABLE CONDENSER	1500 KG.	RESONANCE, APPROXIMATELY	OUTPUT METER ACROSS	C2 (R.F. TRIMMER) FOR MAXIMUM OUTPUT.	
8	A.M.	TUBE IN SERIES WITH A IMFD., 400 VOLT	500 KG.	1500 KC. ON DIAL. RESONANCE, APPROXIMATELY 600 KC. ON DIAL.		C4 (PADDER) ROCK VARIABLE FOR MAXIMUM SIGNAL	
9	A. 16.	CONDENSER.	1	REPEAT STEPS 7,8	AND 9.		
10	A.M.			RESONANCE, APPROXIMATELY		LI (ANTENNA LOADING COIL)	
11	A.M.	USE RADIATED SIGNAL (CONNECT BOTH SIDES	600 KG.	600 KC. ON DIAL.	OUTPUT METER ACROSS	ROCK VARIABLE FOR MAXIMUM SIGNAL	
12	A.M.	OF SIGNAL GENERATOR	1500 KG.	RESONANCE, APPROXIMATELY 1500 KC. ON DIAL.	SPEAKER VOICE COIL.	CI (ANTENNA TRIMMER) FOR MAXIMUM OUTPUT.	
		10 1000011011	1	REPEAT STEPS 11 A	ND 12.	and the second se	
13 14	A.M.		108 MC.	108 MC: ON DIAL.	OUTPUT METER ACROSS	C5 (OSCILLATOR TRIMMER) FOR MAXIMUM OUTPUT.	
15		CONNECT F.M. SIGNAL GENERATOR TO DIPOLE		88 MC. ON DIAL. (CHECK IMAGE AT 109.4 MC.)	SPEAKER VOICE COIL.	L4 (OSCILLATOR COIL) FOR MAXIMUM OUTPUT.	
10		TERMINAL POSTS WITH	·	REPEAT STEPS 14 A			
16	F. M.	A 150 OHM RESISTOR			OUTPUT METER ACROSS	L3 (R.F. GOIL) FOR MAXIMUM OUTPUT.	
17	F. M.	SIDE. 30% MODULATE		102 MC. ON DIAL.	SPEAKER VOICE COIL.	L2 (ANTENNA COL) FOR MAXIMUM OUTPUT	



TUBE & TRIMMER LAYOUT

Packard-Bell

SERVICE DATA - MODEL 872 - FM TUNER



SPECIFICATIONS

Overall Dimensions:

							weight	
Height							Chassis 7 lk	
Width							Cabinet 4 lk	
Depth .		•	•	•	•	9"	Total 11 lk).
Dissinguitant I	m		4.2-					

*** * * *

Electrical Rating:

Line Voltage . . . 110-120 volts 50-60 cycle A.C. Power Consumption . . 52 watts

Tuning Frequency Range:

Frequency Modulation Band . . 88-108Mc Intermediate Frequency:

10.7 Mc

Electrical Power Output: This tuner is designed to operate into the amplifier of any regular broadcast receiver.

The output voltage is comparable to that of the crystal pickup used on the phonograph. A signal from an average strong station will give an audio output of 1 to 3 volts.

Loudspeaker:

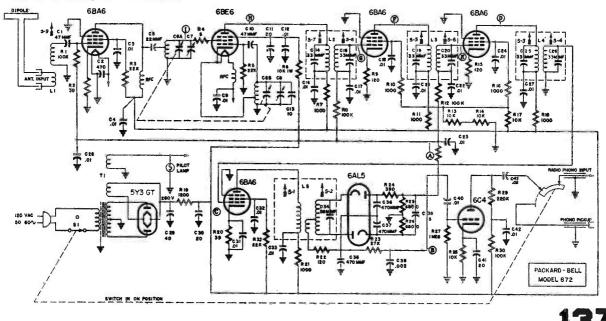
The speaker will be that of the receiver into which the tuner is operating.

Tubes:	
Tube	Function
6BA6	R. F. Amplifier
6BE6	Converter Oscillator
6BA6	1st. I. F. Amplifier
6BA6	2nd. I. F. Amplifier
6BA6	Driver Tube
6AL5	Ratio Detector
6C4	Audio
5Y3	Rectifier
	OFINED AT INTODICAM

GENERAL INFORMATION

Model 872 is a tuner designed to receive frequency-modulation signals in the Frequency-Modulation Band which extends from 88 to 108 megacycles. It may be fastened inside the record compartment of any Packard-Bell console type radio phonograph. If it is not practical to incorporate the tuner and regular broadcast receiver, the tuner can be purchased complete with its own cabinet.

- **Outstanding Features of the 872 Tuner are:**
 - 1. Ratio Type Detector which is more sensitive to desired FM signals and less sensitive to undesirable noise than types of detectors previously used.
 - 2. Two I.F. Stages assuring adequate sensitivity, and permitting the reception of weak (distant) FM stations with good volume.
 - 3. Miniature Type Tubes, advantageous to FM because of their size.
 - 4. Folded Doublet Antenna giving good pickup when located on back of radio cabinet and maximum pickup when located as high as possible above surrounding terrain.



Cackard. Roll MODEL 872

SPECIAL SERVICE INFORMATION

Stage Gain Measurements:

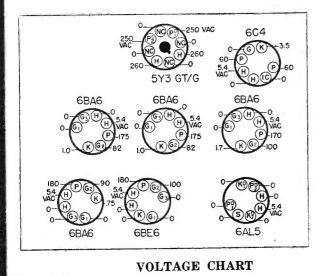
Stage gains are measured by connecting the VTVM to AVC (point A) and proceeding backwards stage by stage and calculating gain of desired stage.

- Audio Gain . . . 10X at 400 cycles
- Ratio Detector Sensitivity . . . 100,00 microvolts on driver grid results in approximately 3.0 volts as measured at AVC point.
- Second I.F. Gain . . . 20X at 10.7 Mc
- First I.F. Gain . . . 20X at 10.7 Mc Converter Gain . . . This measurement can not be made accurately. The gain is approximately 5X at 100 Mc
- R.F. Gain . . . 5X at 100 Mc

Antenna Gain . . . 1.2X at 100 Mc

MODEL 872 ALIGNMENT CHART

	ONNECT EST OSC. TO	TEST OSC. SETTING	METER CONNEC. TO	ADJUST- MENT
1	"C" Driver Grid	10.7 Mc	A	Slug S-1 Max. Output
2	"C" Driver Grid	10.7 Mc	В	*Slug S-2 Zero Center Output
3	"E" 2nd I.F. Grid	10.7 Mc	A	**Slugs S-3 S-4 Max. Output
4	"G" 1st I.F. Grid	10.7 Mc	A	Slugs S-5, S-6 Max. Output
5	"I" Conv. Grid	10.7 Mc	A	Slugs S-7, S-8 Max. Output
6	Antenna	108. Mc	A	Trimmer C-8 Max. Output
7	Antenna	105 Mc	A	Trimmer C-7 Max. Output
8	Antenna	96 Mc	A	Slug S-9 Max. Output



Oscillator Cathode Voltages:

This measurement should not be made as it is impossible to connect a meter to the cathode without disturbing the proper functioning of the oscillator circuit. Fortunately, oscillators either operate or do not function at all at these frequencies. Make usual overall sensitivity measurements to determine if oscillator is functioning.

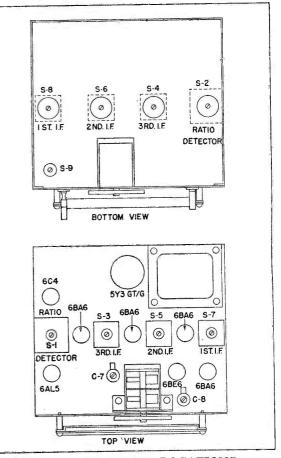
D.C. Resistance Measurements.

All three I.F. Coils are identical

Primary . 0.6 ohms Secondary 0.6 ohms **Ratio Detector Coil**

Secondary 0.2 ohms Primary . 1.2 ohms R. F. Coils

These coils are wound with heavy wire and have only a few turns. Their resistances are extremely low and will read zero on any ohmmeter test.



TRIMMER LOCATIONS

NOTE: * As slug S-2 (Bottom of Ratio Detector Coil) NUTE: - As sug S-2 (Bottom of Ratio Detector Coll) is turned back and forth, a direct-current voltage of posi-tive or negative polarity should be observed if detector is functioning properly. Adjust for zero (center) output. ** A resistive shunt consisting of 1000 ohms in series with 100 mmf should be used. Connect shunt from point (CQU (or generative) to crowned and adjust alter S.² More

"C" (on schematic) to ground and adjust slug S-3. Move shunt from point "C" to point "D" and adjust slug S-4. Same procedure for 1st LF, and converter.

For steps 6, 7, and 8, the tuner should be set to the required frequency.

LOTUN

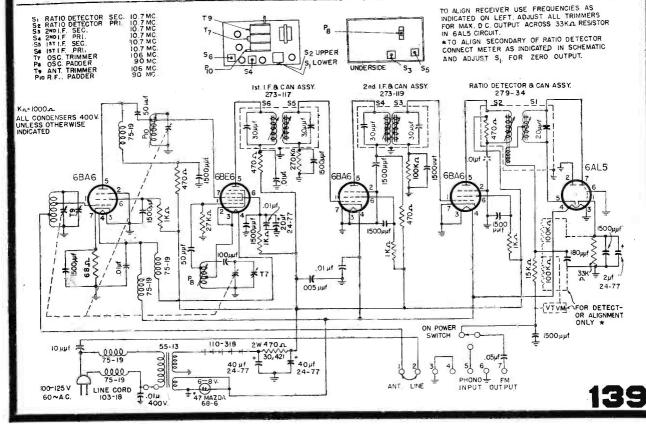
PILOT RADIO - MODEL T-601

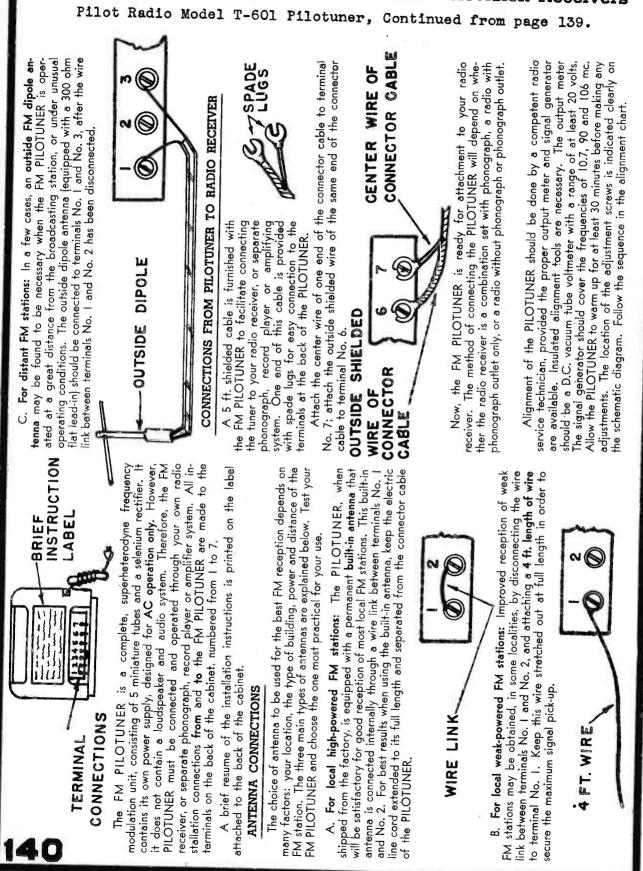
Tuning Range 88-108 Mc.

ALIGNMENT CHART

(Follow sequence as indicated)

					-				
	STEP	RCVR. DIAL POINTER	SI FREQ.	GNAL GEN. CONNECTIONS	METER	METER CONNECTIONS	TRIMN SLUG AD	IER OR JUSTMENT	PROCEDURE
ĬF	l	.88 mc	10.7 mc	Through .01 mfd. cap. to grid of 6BE6	VTVM	Across two 100K resistors —indicated by dotted lines in schematic	S2, S1, S4, S3, S6, S5	Adjust put	for maximum out-
	2	- <u> </u>	Repe	at Step No I					
Ratio Detector	3	88 mc	10.7 mc	Same as No. 1	VTVM	From: Junction of two 100K resistors TO: Audio output of ratio detector. Connec- tions indicated by dot- ted lines in schematic	51	(Check Meter s verse p	meter to zero proper zero set) hould register re- olarity when slug ed through zero
Oscil- lator	4	90 mc	90 mc	Through carbon 300 ohm resistor to Ant. Terminal	VTVM	Same as Step No. 1	P8	Same	as Step No. I
	5	106 mc	106 mc	Same as No. 4	VTVM	Same as No. 1	77	Sa	me as No. I
	6)	Repeat	Steps No. 4 & 5					
	7	90 mc	90 mc	Same as No. 4	V TVM	Same as No. I	P10	Sa	me as No. I
RF	8	106 mc	106 mc	Same as No. 4	VTVM	Same as No. I	T9	Sa	ame as No. I







AM-FM Radio-Phonograph Combination

Circuit Description

Models 610V1 and 610V2 have individual built-in antennas for FM and AM coupled to individual 1st Det.-Osc. tubes (68E6 V1 and V2). The outputs of these two tubes are connected to sepa-rate IF transformers (T1 and T2) whose secondaries are in series and connected to the IF amplifier tube (68A6 V3). The output of V3 is connected to separate IF transformers (T3 and T4) whose primaries are in series. The secondary of T3 (FM IF) is connected to the driver tube (6AU6 V4). The secondary of T3 (AM IF) is connected to the AM second detector (6SQ7 V6). The output of the driver tube (V4) is coupled thru the driver transformer (T5) and ratio detector transformer (T6) to the FM ratio detector tube (6AL5 V5). [In 610V1 the functions of both T5 and T6 are combined in one unit (T5).]

The audio outputs of the AM second detector and the FM ratio detector are connected thru a section of the range switch to the volume control input.

The B+ supply (+245 V) to the plates and screen grids of V1 and V2 is controlled thru a section of the range switch.

Simple AVC is used on AM and is applied to both the IF amplifier (V3) and the AM lat detector (V2). Delayed AVC is used on FM and is applied only to the IF amplifier (V3). The AVC distribution is controlled thru a section of the range switch.

Alignment Procedure

Alignment Indicators:

An RCA VoltOhmyst or equivalent meter is necessary for meas-uring developed d-c voltage during FM alignment. Connections are specified in the alignment tabulation below. An output meter is also necessary to indicate minimum audio output during FM Ratio Detector alignment. Connect the output meter across the enceder voire coil speaker voice coil.

The RCA VoltOhmyst can also be used as an AM alignment indicator, either to measure audio output or to measure a-v-c voltage.

When audio output is being measured the volume control should be turned to maximum.

Signal Generator:

For all alignment operations, except FM IF-RF, connect the low side of the signal generator to the receiver chassis. The output should be adjusted to provide accurate resonance indica-tion at all times. If output measurement is used for AM align-ment the output of the signal generator should be kept as low as possible to avoid a-v-c action.

Calibration Scale,-The dial scale printed in this service note may be temporarily attached to the chassis for quick reference during alignment.

Using Printed Dial Scale.-

- Cut out the printed dial scale, or, better still, make a tracing 1. of the scale.
- 2. With gang at full mesh the pointer should be set to the first reference mark from the left hand end of the dial backing plate.
- Place the printed dial scale or the tracing under the pointer so that the extreme left scale graduations coincide with the pointer. Use scotch tape to hold the dial scale in place.

610V1 (RC-610C) FM Ratio Detector Alignment RANGE SWITCH IN FM POSITION-VOL. CONT. MAXIMUM

Stops	Connect high side of sig. gen. to-	output	Adjustments and indications				
1	Connect the d-c I lead of the 5 min the VoltOhmyst to	d. capacitor, C20, t	yst to the negative he common lead of				
2	Pin 1 of driver tube 6AU6 in series with .01 mfd.	10.7 mc. modu- lated 30% 400 cycles AM (Approx1 volt)	Top core T5 for max. d-c across C20 (Approx. 4 volts) Bottom core T5 for minimum audio output				
3	Repeat Step 2 un alignment.	til further adjustme	ent does not improve				

610V2 (RC-610) FM Ratio Detector Alignment

RANGE SWITCH IN FM POSITION-VOL. CONT. MAXIMUM

Steps	Connect high side of sig. gen. to—	Signal gen- erator output	Adjustments and indications			
1	Connect a 680 ohr the ratio detector a VoltOhmyst to th itcr, C20, te comm	ube 6AL5. Conne	the 5 mfd. capac-			
2	Pin l of driver tube 6AU6 in series with .01 mfd.	10.7 mc. modu- lated 30% 400 cycles AM (Approx25 volt)	Driver trans. T5, for max. d-c across C20 (Approx. 14.5 volts)			
and the second second	Disconnect the Vo	HOhmyst and the	680 ohm resistor			
3	from the 6AL5. Con from the 6AL5. Con 1% of each other) sistor R17. Connec to the center point d.c probe to term. T6. Use 30 volt s lower scale as req	in series across t the common lead of the 68,000 ohr inal "A" of the r cale of VoltOhmys	the 22,000 ohm re- of the VoltOhmys' n resistors and the stic detector trans			
3	from the 6AL5. Col 1% of each other) sistor R17. Connec to the center point d.c probe to term T6. Use 30 volt s	in series across t the common lead of the 68,000 ohr inal "A" of the r cale of VoltOhmys	the 22,000 ohm re- of the VoltOhmyst n resistors and the stic detector trans			
	from the 6ALS. Coi 2% of each other) isistor R17. Connec to the center point d.c probe to fermin T6. Use 30 volt s lower scale as req Same as Step 2	in series across the common lead of the 68,000 ohr ingl "A" of the r cale of VoltOhmys uired. Same as Step 2	 in resistor of the VoltOhmys's n resistors and the detector transst first, reducing to the first reducing the first reduc			
4	from the 6ALS. Coi 2% of each other) bistor R17. Connec to the center point d.c probe to term T6. Use 30 volt s lower scale as req Same as Step 2 Reconnect VoltOhr	in series across the common lead of the 68,000 ohr ingl "A" of the r cale of VoltOhmys uired. Same as Step 2	 in resistor of the VoltOhmys n resistors and the date ctor trans st first, reducing to first, reducing to first reducing to first response of the transmission of transmission of the transmission of transmissio			

† Near the correct core position the zero point is approached rapidly and continued adjustment causes the indicated polarity to reverse. A slow approach to the zero point is an indication of severe detuning, and the bottom core should be turned in the opposite direction.

opposite direction. The zero dc balance and the minimum a-f output should oc-cur at the same point. If such is not the case, the two cores should be adjusted until both occur with no further adjustment of either core. It may be advantageous to adjust both cores simul-taneously, watching the VolKOhmyst, and an output meter, hooked across the voice coil for the point at which both zero d-c and minimum a-f output occur.

FM IF-RF Alignment

(FM Ratio Detector must be aligned first.) SWITCH IN FM POSITION

Steps	Connect sig. gen.	Sig. gen. output	Turn radio dial to—	Adjustment for peak output	
1	Connect the d-c probe of a VoltOhmyst to the negative lead of the 5 mfd. capacitor C20 and the common lead to chassis. Turn gang condenser to max. capacity (fully meshed).				
2	High side to one FM ant. term. in series with 01 mfd. Low side to the other FM ant. term.	10.7 mc 30% modu- lation, 400 cycles AM. Adjust to pxovide 2 to 3 volts indi- cation on VoltOhmyst during alignment.	Max. ca- pacity (fully meshed)	(pri.) Tl bottom core (sec.) Tl top core (pri.) C54 osc. C52 ant.	
3	High side to one FM ant. term. in series with a 120 ohm resistor. Low side to the other FM ant. term in series with a 120 ohm resistor.	106 mč.	106 me		
4	4 Same as 90 mc		90 mc	L3 osc. L2 ant.	
5	Repeat Steps improve cal	3 and 4 unti ibration.	l further adju	istment does n	

* Alternate loading involves the use of a 680 ohm resistor to load the plate winding while the grid winding of the SAME TRANSFORMER is being peaked. Then the grid winding is loaded with the resistor while the plate winding is peaked. Only one winding is loaded at any one time. Remove the 680 ohm resistor after T3 and T1 have been aligned.

AM Alignment

(Correct alignment of the 455 kc. IF requires that the 10.7 mc. IF be aligned previously.) RANGE SWITCH IN BC POSITION

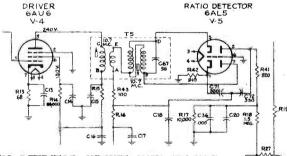
Steps	Connect high side of sig. gen. to—	Sig. gen. output	Turn radio dial to—	Adjust for peak output
1	AM conver- ter grid 6BE6 V-2	455 1	Quiet point at low freq. end.	*T4 top cor (sec.) *T4 bottom core (pri.)
2	in series with .01 mfd.	455 kc		*T2 bottom core (sec.) *T2 top core (pri.)
3	"A" termi- nal of ter- minal board at rear of	1400 kc	1400 kc	C57 osc. C58 ant. (loop)
4	chassis in series with 200 mmf. (link open)	600 kc	600 kc	L5 osc. (Rock gang)
5	Repeat Step 3	3.		
6	After chassis adjust C58 fo 1400 kc.	and loop ha or max, outp	ve been instal ut on a wea	led in cabinet, k station near

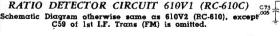
*Align T4 and T2 by means of alternate loading as explained ader FM IF-RF alignment. Use a 47,000 ohm resistor instead under of a 680 ohm resistor.

Oscillator frequency is above signal frequency on both AM and FM.



Front Panel Controls





MODEL 610V2 ONLY (RC 610)

GAU6

(GALS)

Va

EKSGT

DRIVER TRAIS.

15 F.M.

TE RATIO

0 TOP 10.7 MC BOT. 10.7 MC

6597

TS IN MODEL GIOV

C50A C50B

та

VIC

5Y361

v٤

SK6GT

Critical Lead Dress

- 1. Dress capacitor Cl near chassis base.
- Dress lead from pin 5, V-1, to terminal C, of transformer T1, as near bottom of FM shelf as possible. 2.
- The lead from capacitor C23 to the high side of the volume control must be dressed next to chassis along front apron. 3.
- 4. Dress resistor R20 near chassis base.
- 5. Dress all A.C. leads away from volume control.
- 6.
- Solder FM antenna coil primary leads to terminal board with as short a lead length as is practical. 7. Make all FM leads as short as possible.
- The lead from pin 2, V-3, to chassis ground must be dressed as close to base and as near to the back apron as possible. This lead provides degeneration for the IF stage and neither 8. its length nor the point at which it is grounded to the chassis should be changed.
- 9. Dress all leads away from the 3300 ohm resistors R28 and B29

Push Button Adjustment

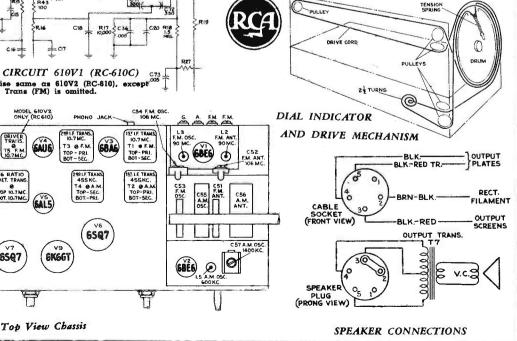
	880-T0 1600 KC	740 TO 1430 KC		610 TO 1250		540 TO 1030 KC
SCREWS	0	\oslash	\oslash	\oslash	\oslash	$ \emptyset$
CORE	6	5	4	3	2	1
RODS		Ø	Ø	Ø	Ø	Ø

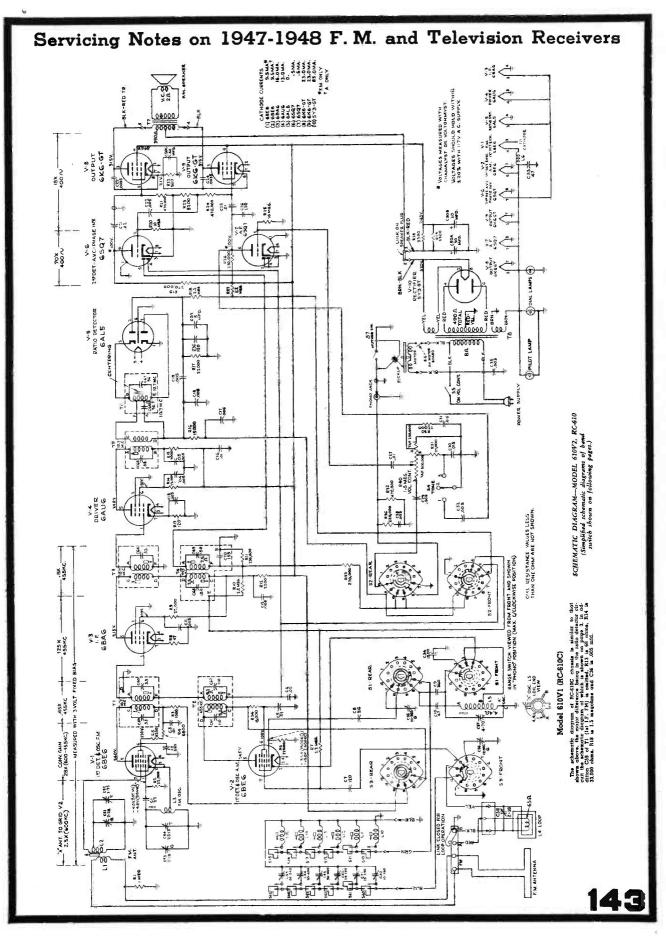
The push buttons connect to separate magnetite-core oscillator coils and separate loop circuit trimmers which must be adjusted for the desired stations. Use an insulated screwdriver or align-ment tool such as RCA Stock No. 31031. Allow about five minutes warm-up period before making adjustments.

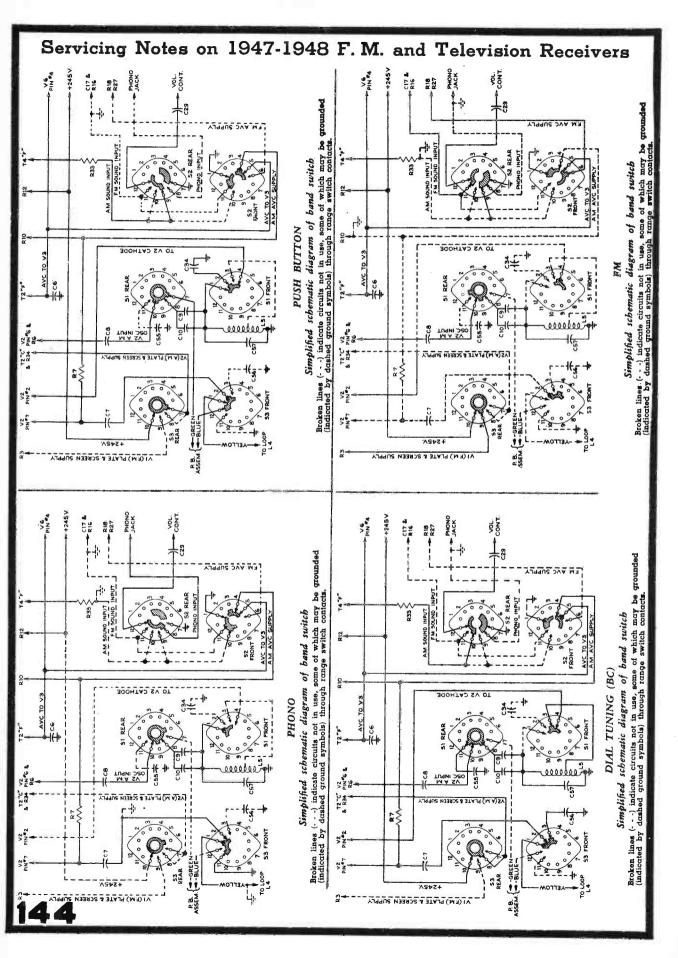
- The procedure is as follows:
- Make a list of the desired stations, arranged in order from low to high frequencies.
- Turn the range switch to the broadcast position and manually tune in the first station on the list. 2.
- Turn range switch to push-button position and press in the 3. left-hand button.
- Adjust core rod No. 1 to receive the first station. To secure Adjust core rod No. 1 to receive the mist statistic to secure the best adjustment, rotate the loop for least pickup, and ad-just core rod No. 1 for peak output.
- Adjust trimmer screw No. 1 for peak output on the first sta-5. tion.
- 6. Proceed in the same manner to adjust for the remaining stations.
- 7. Repeat adjustments for best results.

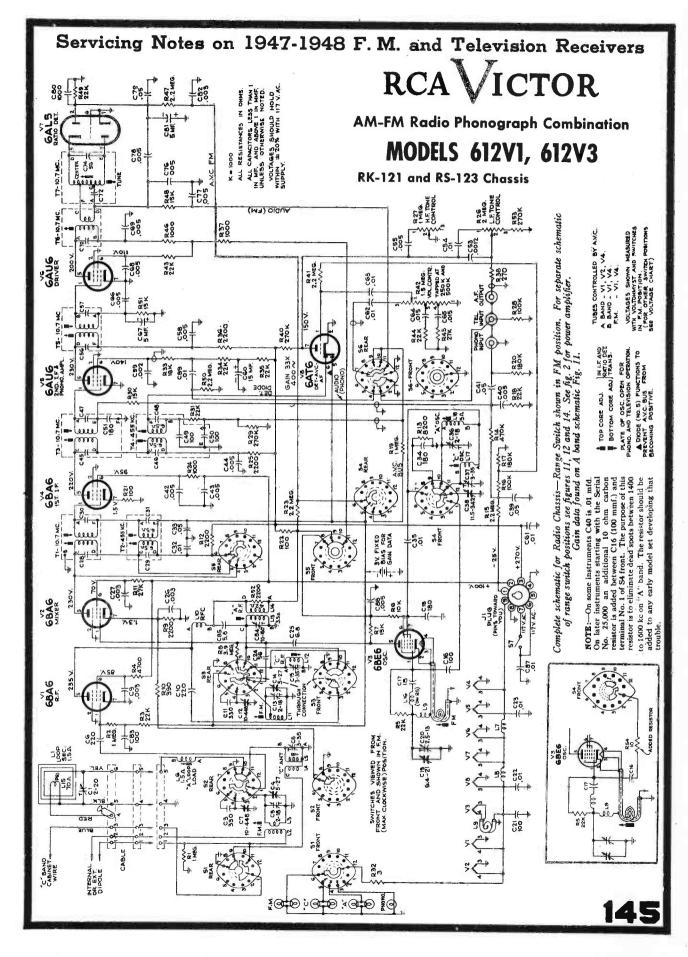
On the 880 to 1,600 kc push-button, the higher frequency stations may be received with core rol No. 6 either in or out (oscillator frequency either 455 kc below or 455 kc above the station fre-quency). The adjustment with this core in its out position (oscil-lator frequency 455 kc above the station frequency) is the correct one.

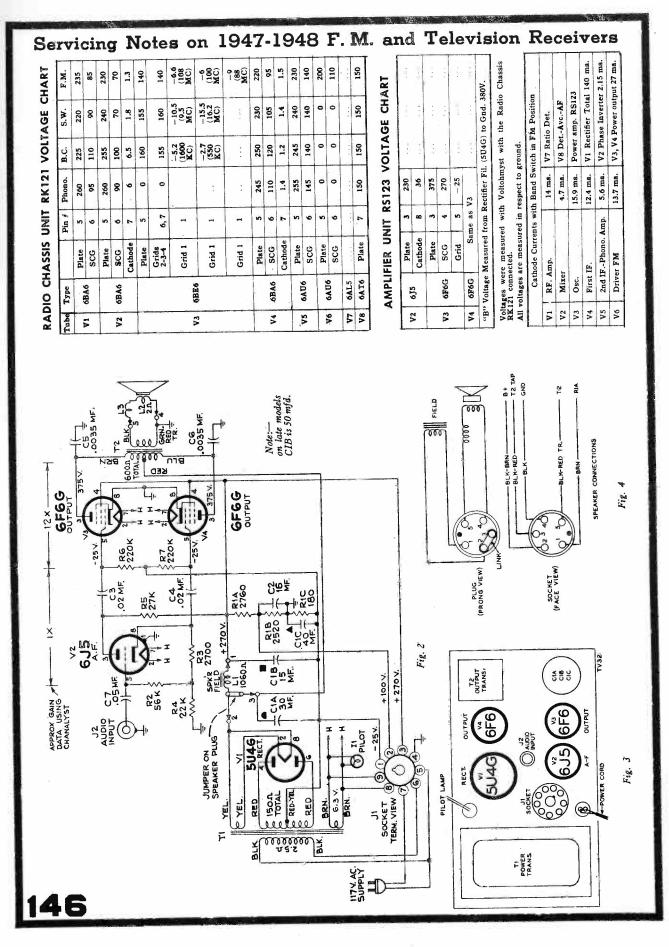
NOTE: Clockwise adjustment of cores and trimmers tunes the circuits to lower frequencies.











ALIGNMENT PROCEDURE

Before aligning set, completely mesh the gang and set the dial pointer on the mechanical maximum calibration point at the extreme left hand end of the dial.

When making a complete alignment follow in proper sequence the tabulated form below.

If only a portion of the circuit is to be aligned select the portion required, followed by the remaining steps in the chart. Any adjustments made on the FM 10.7 mc. IF's make it necessary to realign the AM 455 kc. IF's.

For "A" and "C" band alignment use output meter across voice coil keeping Test Oscillator output as low as possible to prevent AVC action.

Equipment Required for Alignment

Two 68,000 ohm Resistors within 1% of each other (Carbon) 200 mmf. Capacitor 20-30 mmf. Capacitor .01 mfd. Capacitor

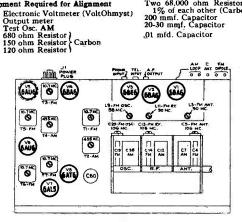


Fig. 5

FM RATIO DETECTOR ALIGNMENT

SET RANGE SWITCH TO FM POSITION

Steps	Connect High Side of Test Osc. To	Tune the Osc. To-		
1.		ansformer T7 negative lead	of the 5	
2.	Driver grid pin 1, of 6AU6 (V6) in series with a .01 MFD capacitor.	10.7 MC 30% Mod. 400 Cycles AM	Maximum Volume	Driver transformer T6 for maximum DC voltage across C-81
	Remove Meter from D and E	Leads and d on T7. Con	isconnect th	e 680 ohm resistor
3.	(within 1% of e the common lea	ach other) is d of the Vol resistors and	a series, act tohmyst to the DC pro	oss C81. Connect the center point of be to contact No. 7
3. 4.	(within 1% of e the common lea the 68,000 ohm	ach other) is d of the Vol resistors and	a series, act tohmyst to the DC pro	oss C81. Connect the center point of be to contact No. 7
	(within 1% of e the common lea the 68,000 ohm ; on rear of Switc) Same as Step 2	ach other) ii d of the Vol resistors and h wafer S6. Same as Step 2	a series, act tohmyst to the DC pro Use the 30 v Volume Control Maximum	oss C81. Connect the center point of be to contact No. 7 olt scale. †T7 Bottom core foi Zero DC Balance on Voltohmyst †T7 top core for minimum audio output. (Output meter across voice
4.	(within 1% of e the common lea the 68,000 ohm ; on rear of Switc) Same as Step 2	ach other) is d of the Vol resistors and h wafer S6. Same as Step 2 myst as in step	a series, act tohmyst to the DC pro Use the 30 v Volume Control Maximum	oss C81. Connect the center point of be to contact No. 7 olt scale. †T7 Bottom core foi Zero DC Balance on Voltohmyst †T7 top core for minimum audio output. (Output meter across voice coil)

[†]Near the correct core position the zero point is approached rapidly and continued adjustment causes the indicated polarity to reverse. A slow approach to the zero point is an indication of severe detuning, and the bottom core should **be** turned in the opposite direction.

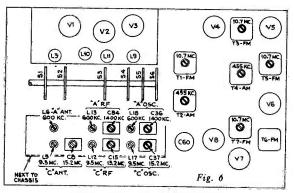
TThe zero DC balance and the minimum AF output should occur at the same point: if such is not the case, the two cores should be adjusted until both occur with no further adjustment of either core. It may be advantageous to adjust both cores simultaneously, watching the volt-ohmyst, and an output meter connected across the voice coil for the point at which both zero DC and minimum output occurs.

Note:—Two or more points may be found which will satisfy the condition required in step 4. T7 top core should be correctly adjusted when approxi-mately ½, inch of threads extend above the can, therefore, it is desirable to start adjustment with the top core in its furthest "in" position and turn out, while adjusting the bottom core, until the first point of minimum AF and minimum DC is reached.

CRITICAL LEAD DRESS (Make lead dress before alignment)

- 1. Lead from pin 5, tube V2, to terminal "C" on transformer T1 should be dressed close to chassis.
- Leads to terminals "C" and "D" on transformer T2 should 2. be dressed close together.
- The following capacitors must be dressed close to the chassis with leads kept as short as possible: C32, C33, C66, C69, C79, and C80.
- 4. All FM coil connections must be soldered in exact place as the original. (One-sixteenth inch difference in length may be excessive).
- Lead from pin 7, tube V8, must be dressed away from lead to terminal "D" of transformer T7.
- б. ALL wiring in the receiver is critical as to length and placement. It is therefore important when servicing, that extreme care should be taken so as not to disturb more of the wiring than absolutely necessary.

Note: Keep tuning capacitor rotor grounding brushes clean and making good contact.



ANT.--RF.--IF. ALIGNMENT

Steps	Connect the High Side of the Test Occ. to-		Tune the Osc. To—	Radio Dial Tuned to	AGjust
-------	---	--	----------------------	------------------------------	--------

"FM" IF Alignment

1.	of the 5 MF lead of the m	D electrolyti	c capacitor	C 81, and	negative lead the common
2.	Mixer grid pin #1 of 6BA6, (V2) in series with a .01 MFD capacitor (Adjust test osc. output for 6-10 volts developed across C81) (Range switch in FM position) (Uss very short lead)	Tube shelf ground near mixer tube(use very short	10.7 MC 30% modulated at 400 cycles AM.	Max. cap. (Fully meshed)	*T5, T3, T1 top and bot- tom cores al- ternately load secondary of each trans- former with 680 ohms while the op- posite side of the same transformer ij being ad- justed. Adjus all trans- formers for maximum voltage across C81.

"AM" IF Alignment

3.	Mixer grid pin #1 of (V2) in series with a .01 MFD Capacitor. (Turn band switch to "A" or "C" band)	To chassis ground	455KC	High Freq. end of Dial	**Top and bottom Cores of T2 and T4. (For maximum voltage across voice coil)
----	--	----------------------	-------	------------------------------	---

ANT-RF-IF-ALIGNMENT (Continued)

Connect the High Side of the Test Osc. Connect Ground Side of the Test Osc.	ne the Dial c. To
--	----------------------

"C" Band OSC.-RF.-ANT. Alignment

4.	"C" Band Ant. Terminal 43 Through a dummy Ant. comprising a 150 ohm re-	To Chassis	15.5 MC	15.5 MC	Osc.—C37*** RF.—C15 Ant.—C8 (For maximum voltage across voice coil)
5,	sistor in series with a 25 to 30 mmf capacitor	ground	9.5 MC	9.5 MC	Osc.—L17*** RFL12 Ant.—L5 (For maximum voltage across voice coil)

"A" Band OSC.—RF.—ANT.

7.	High Side (Red Lead) of Loop Primary with link open through a	To Chassis	1400 KC	1400 KC	Osc.—C36 RF.—C84 Ant.—C1 (For maximum voltage across voice coil)
8.	Dummy Ant. comprising a 200 mmf. Capacitor	ground	600 KC	600 KC	OscL18 RF-L13 AntL6 (For maximum voltage across voice coil)
9.	Repeat steps	7 and 8 for 1	ax. output	•	L

"FM" Band OSC.-RF.-ANT. Alignment

10.	FM antenna terminal #1 in series with a 120 ohm	To FM antenna terminal #2 in series with a 120	106 MC	106 MC	Osc.—C20 for maximum voltage across C81.
11.	* resistor	ohm resistor	88 MC	-88 MC	**** Osc.—L9 for maximum voltage across C81.
12.	Repeat steps	10 and 11 for	exact calib	oration.	
13.	Remove	or turn		106 MC No Carrier	***** RF, C13 for maximum voltage across C81 (Noise Voltage)
14.	test oscilla	ator off.		90 MC No Carrier	**** RF, L11 for maximum voltage across C81. (Noise Voltage)
15.	Repeat steps	13 and 14 for	maximum	output.	
16.	Same as step 10	Same as step 10	106 MC	106 MC	Ant. C5 for maximum voltage across C81.
17.	Same as step 10	Same as step 10	90 MC	90 MC	Ant. L3 for maximum voltage across C81.
18.	Repeat steps	16 and 17 fo	r maximum	qutput.	• · · · · · · · · · · · · · · · · · · ·
19.	Disconnect d loop when set	ummy anten t is installed	na and adj in cabinet.	ust Ant. th	rimmer C1 on

*This method is known as alternate loading which involves the use of a 680 ohm resistor to load the plate winding while the grid winding of the same transformer is being peaked. Then the grid winding is loaded with 680 ohm resistor while the plate winding is being peaked.

When the windings are loaded, it is necessary to increase the 10.7 MC input since the gain will decrease and the voltage across C81 will be less.

**It is necessary to alternately load the primary and secondary of each 455 KC I. F. transformer with 10,000 ohms while the opposite side of the same transformer is being adjusted.

***To guard against the possibility of alignment of L17 and C37 to image frequencies, tune the test oscillator to 15.5 MC and turn the radio dial to 15.5 MC. Then adjust the test oscillator to 16.41 MC (image frequency). By increasing the test oscillator output, a signal should be heard.

Tune the test oscillator to 9.5 MC and turn the radio dial to 9.5 MC, then adjust the test oscillator to 10.41 MC (image frequency). By increasing the test oscillator output, a signal should be heard. (If these image frequencies cannot be heard, the set is incorrectly aligned, therefore repeat-steps 4 and 5)).

****Two points may be found to fulfill the requirements. Use the one with the longest threaded end extending out of the transformer.

***** Two points can be found having the greatest noise voltage developed. Use the one with the greater capacity (tighter adjustment).

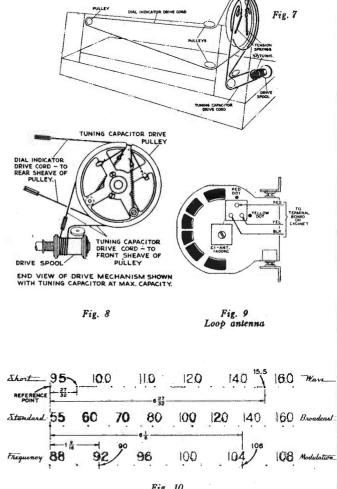


Fig. 10 Dial scale drawing

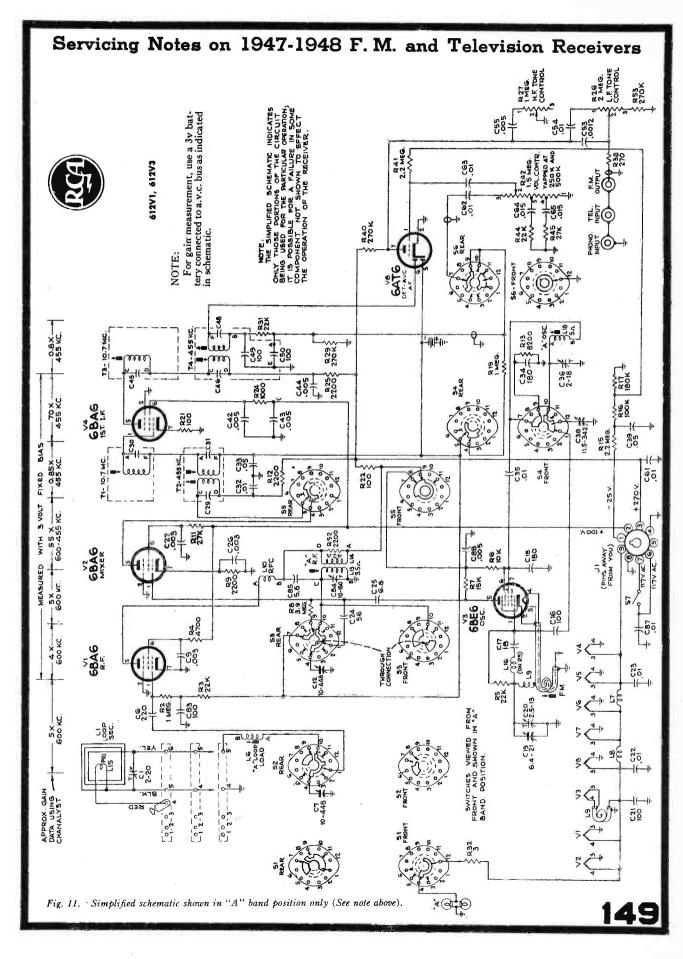
Circuit diagram breakdown description

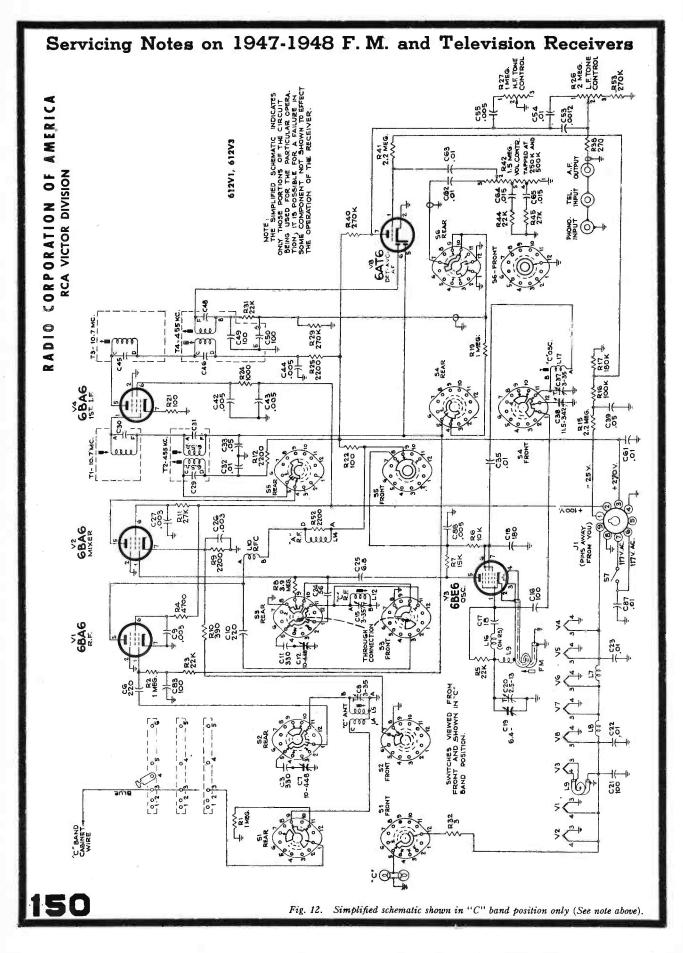
In order to have the instrument function in all of the positions of the band switch, a number of extra tubes and parts are required. We have attempted to simplify the circuits by including simplified schematics showing only the parts actually required for the instrument to operate in the position to which the switch is turned.

It can be noted by examining the different simplified schematics, that a few of the circuits deviate from the conventional form.

Tube V8 performs the function of 2nd Det., AVC and AF amp. in "A" and "C" bands only. Diode #5 of V8 functions as a device to prevent the AVC bus from becoming positive.

Tubes V6 and V7 are used only in the FM positions; V6 as a driver and V7 as an FM demodulator,





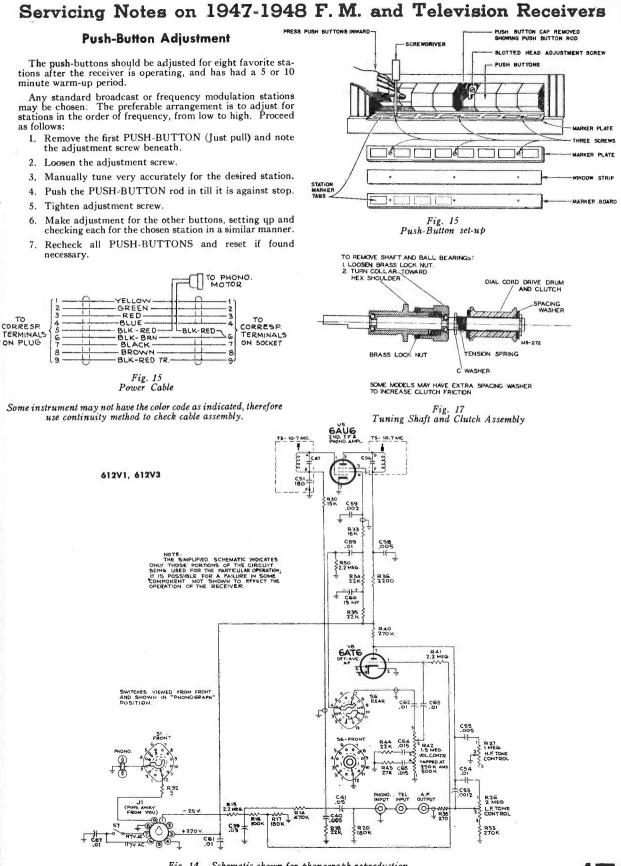
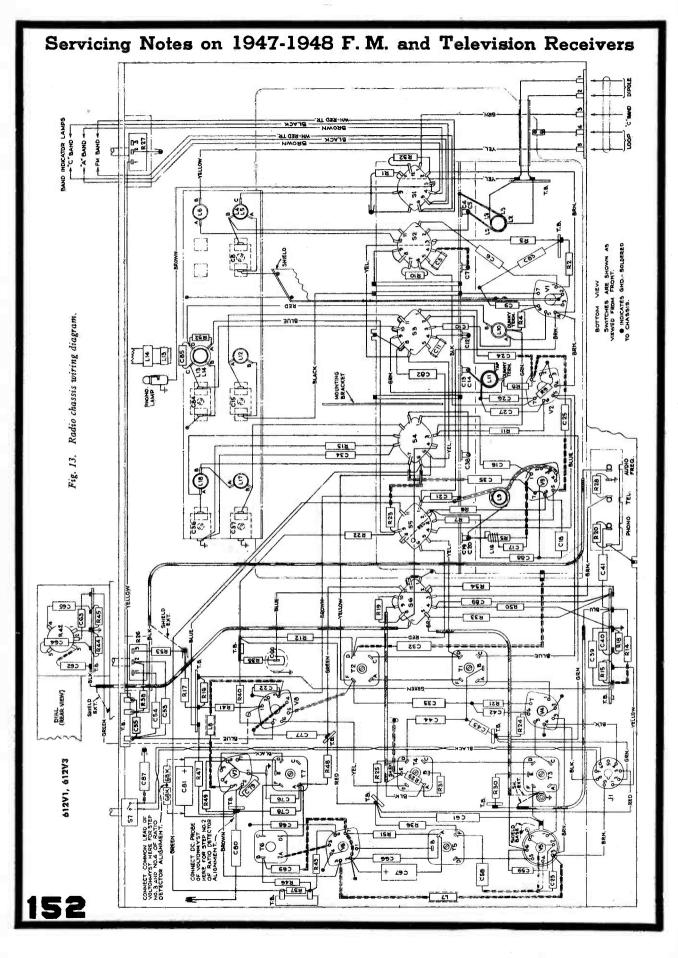
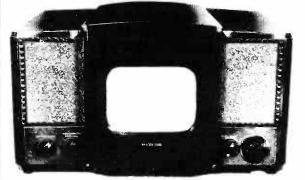


Fig. 14. Schematic shown for phonograph reproduction. Note: Oscillator plate voltage is removed when operating phonograph. 151





RCAVICTOR

TELEVISION RECEIVER MODEL 630TS

Chassis No. KCS 20A (60 cycles) and KCS 20C-2 (50 cycles)—Mfr. No. 274

Important information on the operation, adjustment, and repair on RCA Victor Model 630TS television receiver is presented on pages 153 to 162. The RCA Victor Division of Radio Corporation of America, through its Home Instrument Department, has made these service notes available to the trade for the development of television and as an information medium to the service fraternity.

GENERAL DESCRIPTION

Model 630TS is a thirty-tube, direct-viewing, 10" table model. Television Receiver. The receiver is complete in one unit and is operated by the use of seven front-panel controls. Features of the receiver include: Full thirteen channel coverage; F.M. sound system; Improved picture brilliance; A.F.C horizontal hold; Stabilized vertical hold; Two stages of video amplification; Noise saturation circuits; Three stage sync separator and clipper; Four mc. band width for picture channel, and Reduced hazard high voltage supply.

RECEIVER OPERATING INSTRUCTIONS

The following adjustments are necessary when turning the receiver on for the first time.

 Turn the receiver "ON" and advance the SOUND VOL-UME control to approximately mid-position.

2. Set the STATION SELECTOR to the desired channel.

3. Turn the PICTURE control fully counterclockwise.

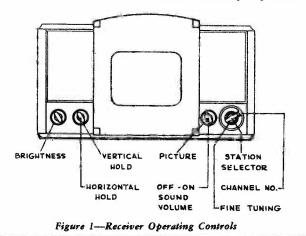
 Turn the BRIGHTNESS control clockwise, until a glow appears on the screen then counterclockwise until the glow just disappears.

5. Turn the PICTURE control clockwise until a glow or pattern appears on the screen.

6. Adjust the FINE TUNING control for best sound fidelity and SOUND VOLUME for suitable volume.

7. Adjust the VERTI-CAL hold control until the pattern stops vertical movement.

 Adjust the HORI-ZONTAL hold control until a picture is obtained and centered.



9. Adjust the PICTURE control for suitable picture contrast.

 After the receiver has been on for some time, it may be necessary to readjust the FINE TUNING control slightly for improved sound fidelity.

11. In switching from one station to another, it may be necessary to repeat steps number 6 and 9.

12. When the set is turned on again after an idle period, it should not be necessary to repeat the adjustments if the positions of the controls have not been changed. If any adjustment is necessary, step number 6 is generally sufficient.

> 13. If the position of the controls has been changed, it may be necessary to repeat steps number 1 through 9.

> NOTE: If any difficulty is experienced with steps number 7 or 8, turn the PICTURE control ¼ turn counterclockwise and repeat those adjustments.

CIRCUIT DESCRIPTION

It is advisable that the reader be familiar with a recent standard textbook of television principles in order to properly understand the receiver circuits and their functions. Such a knowledge is assumed for the purpose of this publication. The discussions which follow will not dwell on the operation of conventional circuits used which have been used in previous receivers and which should be well known. In general, the circuits discussed will be only those that are new to the field.

For ease of understanding the basic operation of the receiver, a 15 unit block diagram of it is shown in Figure 2. The circuit description will follow the numerical order of these blocks in order to logically follow a signal through the set.

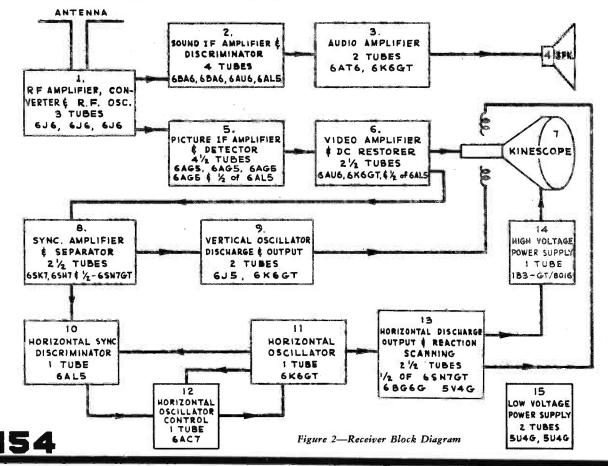
R-F UNIT (block # 1)—The r-f unit is a separate subchassis of the receiver. On this subchassis are the r-f amplifier, converter, oscillator, fine tuning control, channel switch, converter transformer, r-f, converter and oscillator coils and all their tuning adjustments. The unit provides operation on all thirteen of the present television channels. It functions to select the desired picture and sound carriers, amplifies and converts to provide at the converter plate, a picture i-f carrier frequency of 25.75 mc. and a sound i-f carrier of 21.25 mc.

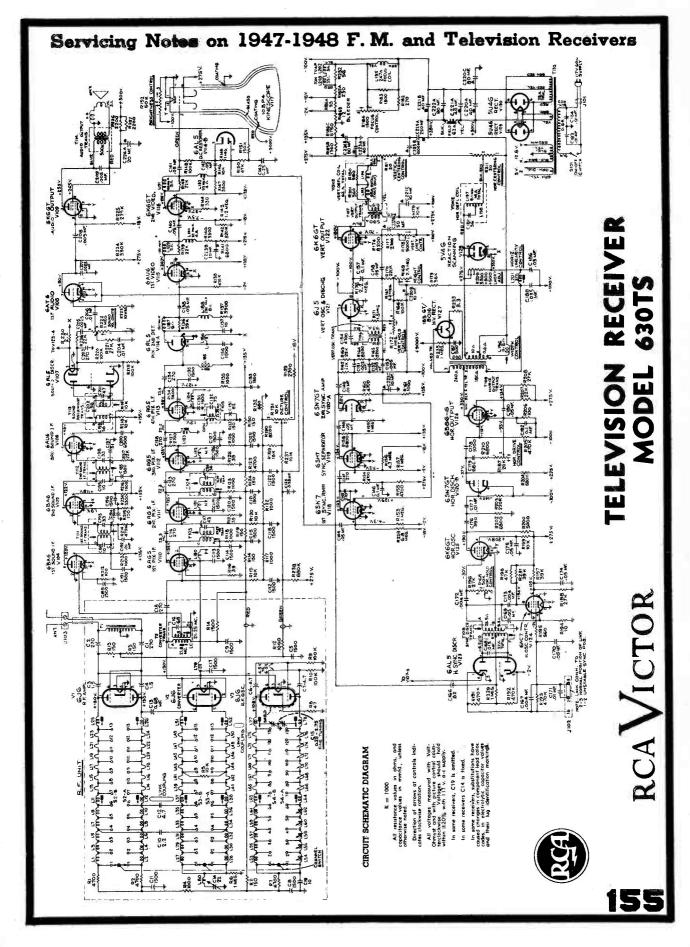
R-F Amplifier—Referring to the Schematic Diagram T1 is a center tapped coil used for the short circuiting of low frequency signals picked up by the antenna which would otherwise be airectly applied to the control grids of the 6J6 rf amplifier, V1. C1 and C2 are antenna isolating capacitors. The d-c return for the grids of V1 is through R3 and R13 which also properly terminate the 300 ohm antenna transmission line. C3 and C4 are neutralizing capacitors necessary to counteract the grid to plate capacitance of the triode rf amplifier.

In the plate circuit of the r-f amplifier are a series of inductances L1 to L25 and L2 to L26 inclusive. These inductances may be considered as a quarter wave section of a balanced transmission line which can be tuned over a band of frequencies by moving a shorting bar along the parallel conductors.

Adjustable coils L25 and L26 provide the correct length of line for the thirteenth channel, 210-216 mc. L13 to L23 and L14 to L24 are fixed sections of line which are added to L25 and L26 as the shorting bar is moved progressively down the line. The physical construction of each one of these inductances is a small non-adjustable silver strap between the switch contacts. Each strap is cut to represent a six-megacycle change

in frequency. In order to make the jump between the lowest high frequency channel (174-180 mc) and the highest low frequency channel (82-88 mc), adjustable coils L11 and L12 are inserted. To provide for the remaining five low frequency channels, L1 to L9 and L2 to L10 are progressively switched in to add the necessary additional inductance.





Coils L1 to L9 and L2 to L10 are unusual in that they are wound in figure 8 fashion on fingers protruding from the switch wafer. This winding form produces a relatively noncritical coil since the coupling between turns is minimized. A maximum amount of wire is used for the small inductance which is required, thus permitting greater accuracy in manufacturing.

Converter—The converter grid line operates in a similar manner and is so arranged on the switch to provide coupling between it and the r-f line. C10, C12, C13 and a link, provide additional coupling which is arranged to produce at least a 4.5 megacycle band pass on each of the channels.

L80 and C14 form a series resonant circuit used to prevent i-f feedback in the converter by grounding its grids for i-f frequency. They also act as a trap to reject short-wave signals of i-f frequency which arrive at the converter grids in a push push manner.

A 676 twin triode is used as converter. Since the grids are fed in push pull by both the signal and the oscillator, the heterodyne products (i-f signals) are in phase on the converter plates so the two plates are connected in parallel. Unwanted signals of i-f frequency that arrive at the converter grid in a push pull manner are out of phase on the converter plates. Since the plates are tied together, these signals tend to cancel thus reducing the possibility of interference from this source.

R-F Oscillator—The oscillator line is similar except that trimmer adjustments are provided for each channel and the low frequency coils are not figure 8 windings. For tuning each channel, brass screws are used in close proximity to the high frequency tuning straps L66 to L76, and brass cores are adjusted through coils L54 to L62. It is obvious that the high frequency adjustments should be made before each lower frequency one.

C15 is a fine tuning adjustment which provides approximately plus or minus 300 kc. variation of oscillator frequency on channel 1 and approximately plus or minus 750 kc. on channel 13. On a few early production units, slightly less range is available.

The physical location of the oscillator line with respect to the converter grid line is such as to provide some coupling to the converter grids. This coupling is augmented by the link shown on the schematic and provides a reasonably uniform oscillator voltage at the converter grids over the entire tuning range of the unit.

The converter transformer T2 is a combination picture if transformer, sound trap, and sound if transformer. The converter plate coil is assembled within the structure of a high Q resonant circuit tuned to the sound if frequency. This high Q coil absorbs the sound if component from the primary. Thus on the T2 primary (from which the picture if is fed), the sound carrier is attenuated with relation to the picture channel.

SOUND 1-F AMPLIFIER AND DISCRIMINATOR (block #2)—A portion of the energy absorbed by the T2 trap circuit is fed to the first sound i-f amplifier. Three stages of amplification are used to provide adequate sensitivity. A conventional discriminator is used to demodulate the signal. The discriminator band width is approximately 350 kc. between peaks.

AUDIO AMPLIFIER AND SPEAKER (block #3 and 4)—The audio amplifier is a conventional system employing a 6AT6 high mu. triode amplifier and a 6K6GT power output tube feeding a 5-inch E.M. dynamic speaker.

PICTURE I-F AMPLIFIER AND DETECTOR (block #5)—The picture i-f amplifier departs considerably from the conventional coupled amplifier. To obtain the necessary wide band characteristic with adequate gain, four stages of i-f amplification are employed. The converter plate and each successive i-f transformer utilizes only one tuned circuit and each is tuned to a different frequency. The effective Q of each coil is fixed by the shunt plate load or grid resistor so that the response product of the total number of stages produces the desired overall response curve. Figure 3 shows the relative gains and selectivities of each coil and the shape of the curve of the quintuple combination.

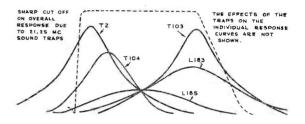


Figure 3-Stagger Tuned I-F Response

In order to obtain this band pass characteristic, the picture if transformers are 'uned as follows:

Converter transformer
First pix i-f transformer 25.3 mc. (T103 primary)
Second pix i-f transformer 22.3 mc (T104 primary)
Third pix i-f coil
Fourth pix i-f coil 23.4 mc. (L185)

In such a stagger tuned system variations of individual i-f amplifier tube gain do not affect the shape of the overall i-f response curve if the Q and center frequency of the stages remain unchanged. This means that the i-f amplifier tubes are The converter transformer T2 is a combination picture i-f transformer, sound trap, and sound i-f transformer. The converter To align the i-f system, the transformers are peaked to the specified frequencies with a signal generator. The overall i-f response is then observed by use of a sweep generator and oscilloscope. Slight deviations from standard circuit Q are compensated for with slight shifts in transformer center frequency until the desired response curve is obtained. If this response cannot be obtained, the difficulty is likely to be in a location that affects either the frequency or Q of one or more of the i-f transformers.

The response curve does shift slightly as the picture control is varied due to the Miller effect. This effect is the change in tube input capacitance as its gain is varied by grid bias changes. The change of input capacitance causes a slight detuning of the preceding i-f transformer and a small shift in response shape. This effect is slight, however, and when the receiver is aligned with the specified grid bias, no difficulty from this source should be encountered.

For familiarization with the frequencies which are important in the receiver's operation, Figure 4 shows the relative position of the picture and sound carriers for channels 2, 3 and 4. If a station on channel 3 is transmitting a picture with video frequencies up to 4 mc., the picture carrier will have side band frequencies up to 65.25 mc. The lower side bands are suppressed at the transmitter.

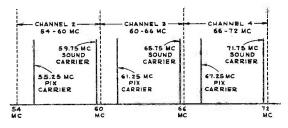


Figure 4-Television Channel Frequencies

With the receiver r-f oscillator operating at a higher frequency than the received channel, the i-f frequency relation of picture to sound carrier is reversed as shown in Figure 5.

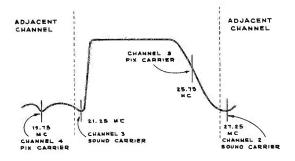


Figure 5-Overall Picture I-F Response

Traps—Since it is necessary for the picture i.f to pass frequencies quite close to the sound carrier frequency, the sound carrier would produce interference in the picture. In order to prevent this interference, traps must be added to the picture i-f amplifier to attenuate the sound carrier. If the receiver should be operating on channel 3, it is possible that interference would be experienced from the channel 2 sound carrier and the channel 4 picture carrier. The adjacent channel traps are provided to attenuate these unwanted frequencies.

The first three traps are absorption circuits. The first trap (T2 secondary) is tuned to the accompanying sound i-f frequency, the second trap (T103 secondary) is tuned to the adjacent channel sound frequency, and the third trap (T104 secondary)

tuned to the adjacent channel picture carrier frequency. The fourth trap (T105 secondary) is in the cathode circuit of the fourth picture i-f amplifier V113 and is tuned to the accompanying sound carrier i-f frequency. The primary of T105 in series with C181 forms a series resonant circuit at the frequency to which L185 is tuned (23.4 mc.). This provides a low impedance in the cathode circuit at this frequency and permits the tube to operate with a gain. However, at the resonant frequency of the secondary (21.25 mc.), a high impedance is reflected into the cathode circuit, and the gain of the tube for this frequency is reduced by degeneration. The rejection with this circuit is limited to the gain of the tube.

Picture Control—The picture (or contrast) control varies the bias on the r-f amplifier and the first, second and third i-f amplifier control grids. It is a manual sensitivity control, and is operated to prevent overloading of the i-f stages and to provide the correct video output level from the second detector. A novel arrangement is used in conjunction with the control. The object of this system is to provide optimum signal to noise ratio from the receiver. This is achieved by allowing the r-f amplifier to run essentially at full gain over a considerable range of the picture control. The gain in the r-f stage is reduced only when it becomes necessary to do so in order to prevent overloading of the first i-f stage. The circuit shown in Figure 6 is used to provide the non-proportional r-f and i-f bias from a single control.

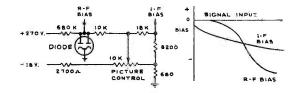


Figure 6-Picture Control Circuit

When the picture control is in the maximum gain position, the i-f bias is approximately minus one volt. The r-f bias is taken from a tap up the control network which would be several volts positive except for relatively heavy conduction of the diode. Diode conduction holds the voltage at this point to approximately ground potential.

As the picture control gain setting is reduced slightly, the i-f bias begins to go more negative. At the r-f bias junction, diode conduction is reduced but the voltage remains essentially constant. When the picture control setting is reduced still further, diode conduction is stopped and the r-f bias voltage changes rapidly to assume a more negative potential than the i-f grid.

This high value of bias on the r-f amplifier is necessary to reduce the triode nearly to cut-off. Although triodes are not generally considered to be remote cut-off tubes, sufficient curvature is present in the grid control characteristic to provide approximately α ten to one reduction in gain when the bias approaches the cut-off point.

VIDEO AMPLIFIER AND D-C RESTORER (block #6)—The function of this section of the receiver is to amplify the video output of the second detector. Two amplifier stages are employed. The gain from the first video grid to output plate is 30X and the frequency response extends to 4 mc.

D-C Restorer—Since the video amplifier is an a-c amplifier, the d-c component of the video signal that represents the average illumination of the original scene will not be passed. Unless this d-c component is restored, difficulty will be experienced in maintaining proper scene illumination. For any given scene, this average illumination could be set properly by the brightness control. However, a change of scene would probably necessitate resetting this control. The d-c restorer accomplishes this setting automatically thus assuring proper picture illumination at all times.

KINESCOPE (block #7)—The Kinescope is a 10" tube employing a new type screen material which provides considerably improved picture brilliance. The tube employs magnetic deflection and magnetic focus. An ion trap is employed to prevent the ion beam from producing a brown spot on the picture screen. The inside and outside of the flaring portion of the bulb are given a metallic coating. The inner coating, which is the second anode, is connected to the high voltage supply. The outer coating is grounded by means of two small springs on the deflection yoke support. The capacity between the two coatings is approximately 500 mmf and is used as a high voltage filter condenser.

SYNC AMPLIFIER AND SEPARATOR (block #8)—The function of this system is to amplify the sync signal and effect separation of sync from the video.

Sync Amplifier—The first sync amplifier V118 is a 6SK7 which has a remote cut-off characteristic. The signal from the d-c restorer is fed into this amplifier with the polarity such that the sync is in the negative direction. Noise pulses above sync that remain after the limiting action of the first video grid are thus further compressed and the sync to noise ratio is again improved.

Sync Separator—The sync at the sync separator grid is positive in polarity. The operating voltages applied to the grid, screen and plate, are such that the negative portion of the applied signal is cut off. Thus, the video and blanking pulses are removed and only the sync pulses appear at the sync separator plate.

Second Sync Amplifier—The sync pulses appearing at the second sync amplifier, (V120Å), grid are negative in polarity and must be inverted before they can be injected into the sweep oscillators. The signal at the V120Å grid is sufficient to drive the tube beyond cut-off and the signal is again clipped. This final clipping removes all amplitude variations between sync pulses due to noise, hum, etc., and it appears with the correct polarity at the plate.



Integrating Network—The purpose of this network is to separate the horizontal from the vertical sync and to pass the vertical to the vertical oscillator.

Since the horizontal sync pulse is of short duration (5 microseconds) and the vertical pulse is of much longer duration (190 microseconds), they can be separated by an r-c filter which is responsive to wave shape. The integrating network which is such a filter is composed of R163, R164, R165, C151, C152 and C153. In operation it can be considered as a low-pass filter which by-passes the narrow or high frequency horizontal sync but passes the broad or low frequency vertical sync.

VERTICAL OSCILLATOR DISCHARGE AND OUTPUT (block #9)—The function of these circuits is to provide a sawtooth of current of the proper frequency and phase to perform the vertical scanning for the Kinescope. To produce such a current in the vertical deflection coil, a somewhat different shaped voltage wave is required.

Since the vertical trace is slow, requiring approximately 16,000 microseconds, and the vertical deflection coil inductance is small, approximately 50 millihenries, the majority of the voltage across the coil during trace is across its resistive component. In order to produce a linear change of current through a resistance, a linear change of voltage is necessary. Retrace, however, must be accomplished within the 666 microsecond vertical blanking time and therefore requires a much faster rate of change of current through the coil. During this time, the effect of its inductance becomes appreciable because of the required fast rate of change of current. It is therefore necessary to apply a large pulse of voltage across the coil in order to obtain rapid retrace. The composite waveform required to produce a sawtooth of current in the coil is a sawtooth of voltage with α sharp pulse as shown in Figure 7. V121 and V122 supply such a voltage.

Vertical Oscillator and Discharge—A single 6J5 triode, V121, with its associated components form a blocking oscillator and discharge circuit. The wave form of the voltage at the control grid of this tube with respect to time, is a small, positive surge followed by a large negative drop which returns to the positive condition at a relatively slow rate. During the negative part of the cycle, the grid is beyond cut-off and the discharge capacitor, C158, charges through resistors **R**169 and **R**170.

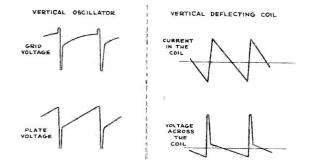


Figure 7-Vertical Sweep Waveforms

When the grid reaches a voltage that permits plate to cathode conduction, C158 discharges through T106 secondary and V121. The discharge current of C158 builds up a magnetic field in T106 that in turn induces a positive voltage at the grid of V121. This positive voltage on the V121 grid lowers the plate resistance of the tube and allows C158 to discharge more rapidly. This process builds up very rapidly until C158 is nearly discharged. The magnetic field in T106 then collapses and drives the V121 grid negative. The charge placed on C154 due to grid conduction during the positive pulse now holds the grid negative. As the charge on C154 leaks off through R171, R172, etc., the grid slowly becomes less negotive and approaches the point which will allow plate to cathode conduction. Just before the conduction point is reached, the 60 cycle vertical synchronizing pulse from the integrating network is applied to the V121 grid. This pulse is sufficient to drive the tube to conduction and the process is repeated. In this manner, the incoming sync maintains control of vertical scanning.

On the plate of V121, a sawtooth of voltage appears due to the slow charging and rapid discharging of C158. A sharp negative pulse also occurs during the discharge period. See Figure 7. This pulse appears because of the action of R174 and C158, an action which is known as peaking. When V121 is conducting, the plate voltage drops nearly to cathode potential. C158 discharges during this time. However, since the conduction time is short, C158 cannot be completely discharged due to the time constant of R174 in series with C158. When V121 becomes non-conducting, the plate voltage does not have to rise slowly from cathode potential but instead rises immediately to an appreciable value due to the charge that remains on C158. The plate voltage then slowly rises from this value as C158 charges through R170 and R169. Adjustment of the height control R169 varies the amplitude of the sawtooth voltage on V121 plate by controlling the rate at which C158 can charge.

The voltage present on the V121 plate is of the shape required to produce a sawtooth of current in the vertical deflection coil. It is now necessary to amplify it in a tube capable of supplying a sufficient amount of power.

Vertical Output—A 6K6GT is connected as a triode for the output stage, V122. The vertical output transformer T106 matches the resistance of the vertical deflection coils to the plate impedance of the 6K6GT.

R178 is provided as a vertical sweep linearity control. Since the grid control characteristic curve of V122 is not a straight line over its entire range, the effect of adjustments of R178 is to produce slight variations in shape of the sawtooth by shifting the operating point of the tube.

Since the slope of the curve varies at these different points and thus varies the effective gain of the tube, it is apparent that adjustments of linearity effect picture height and that such adjustments must be accompanied by readjustments of the height control R169. Adjustments of the height control affect the shape of the sawtooth voltage on V121 plate so that adjustments of height must be accompanied by readjustments of linearity. HORIZONTAL SYNC DISCRIMINATOR, HORIZONTAL OSCIL-LATOR AND OSCILLATOR CONTROL (block #10, 11 and 12) —These circuits are a radical departure from the conventional systems used for framing the picture in the horizontal direction. Their features are ease of operation, stability and good noise immunity.

HORIZONTAL OSCILLATOR (block #11)—The horizontal oscillator is an extremely stable Hartley oscillator operating at the scanning frequency 15,750 cps. The primary of T108 (terminals A, B and C) is the oscillator coil. This coil is closely coupled to the secondary winding (terminals D, E and F) and thus feeds a sine wave voltage to V123.

HORIZONTAL SYNC DISCRIMINATOR (block #10)—The sync discriminator, V123, is a 6AL5 dual diode in a circuit which produces a d-c output voltage proportional to the phase displacement between two input voltages.

The sine wave oscillator voltages applied to the plates of V123 are equal in amplitude and opposite in phase. The synchronizing pulses from the second sync amplifier are fed through a differentiating network to attenuate the vertical sync and then applied to the center tap of T108. The horizontal sync pulses thus appear in phase and of equal amplitude on the diode plates as shown in Figure 8. When the pulse and sine wave are properly phased as in (A), both diodes will produce equal voltage across their load resistances, R191 and R192. However, these voltages are of opposing polarity and therefore the sum of the voltages across these two load resistors will be zero. If the phase of the pulse changes with respect to the sine wave as in (B), the top diode will produce more voltage across R191 than the bottom diode produces across R192. Thus, the voltage across the two will be positive. In (C) the reverse condition exists. It is obvious that the output of the discriminator can swing from positive through zero to negative dependent upon the phase relation of the synchronizing signal and the oscillator. This d-c output is applied to the grid of V124.

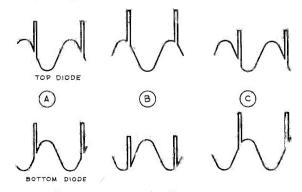


Figure 8-Sync Discriminator Waveforms

HORIZONTAL OSCILLATOR CONTROL (block # 12)—V124 the oscillator control is a 6AC7 connected as a reactance tube across the V125 oscillator coil. A change in the d-c output of the discriminator produces a change in Gm of V124 which

159

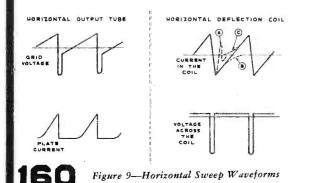
in turn changes the frequency of the oscillator. If the phase of the oscillator shifts with respect to the synchronizing pulse, the corresponding change in d-c from the discriminator brings the oscillator back into correct phase. C167 and C170 form a voltage divider to attenuate rapid changes in d-c from the sync discriminator such as are produced by vertical sync or bursts of noise.

HORIZONTAL DISCHARGE, OUTPUT AND REACTION SCAN-

NING (block # 13)—The purpose of these circuits is to produce a sawtooth of current in the deflection coils to provide horizontal scanning. One-half of a 6SN7GT is employed for the discharge tube V120B.

The oscillation in V125 takes place between screen-grid and cathode. Since the peak to peak voltage on its grid is approximately 130 volts, a square wave is produced on its plate. This wave is differentiated by C176 and R202, and the pulse so obtained is applied to the grid of the discharge tube V120B. The discharge tube is normally cut off due to bias produced by grid rectification of these incoming pulses. The pulse from V125 overcomes this bias and drives the tube into heavy momentary conduction. During this period the plate voltage falls nearly to cathode potential and C179 discharges rapidly. However, since the period of conduction is quite short, C179 is not completely discharged due to the time constant introduced by R187 and R210 in series with C179. Then when V120B again becomes non conducting, the plate voltage rises quickly to a value determined by the charge remaining on C179. From this point the plate voltage rises slowly and approximately linearly as C179 charges through R204.

Horizontal Output and Reaction Scanning—The operation of these two circuits is so interconnected that it will be necessary to discuss them simultaneously. The function of the output tube V126 is to supply sufficient current of the proper wave form to the horizontal deflection coil in order to provide horizontal scanning for the Kinescope. The function of the reaction scanning tube V128 is to stop oscillation of certain components at certain times and thus help provide a linear trace. Other functions of these circuits include the utilization of energy stored in the horizontal deflection coil to furnish retrace and Kinescope high voltage. The reaction scanning circuit also recovers some of the energy from the yoke kickback and uses it to help supply the plate power requirements of the output tube.



In operation, the visible portion of the horizontal trace is approximately 53 microseconds in duration. Although the inductance of the horizontal deflection coil is in the order of 8 millihenries, at the horizontal scanning frequency, the reactance of the coil predominates over its resistance. This is a different case than that encountered in the vertical deflection system and so a different method of operation must be employed.

Horizontal blanking is approximately 10 microseconds in duration. During this time, the Kinescope beam must be returned to the left side of the tube, the trace started and made linear. In order that all this be accomplished within the horizontal blanking time, only 7 microseconds can be allowed for the return trace. In order to obtain such rapid retrace, the horizontal deflection coil, output transformer and associated circuits are designed to resonate at a frequency such that one half cycle of oscillation at this frequency will occur in the 7 microseconds retrace time limit.

During the latter part of the horizontal trace, the output tube conducts very heavily and builds up a strong magnetic field in the deflection coil and output transformer. When the negative pulse from the horizontal tube is applied to the output tube grid, its plate current is suddenly cut off and the magnetic field in the transformer and deflection coil begins to collapse at a rate determined by the resonant frequency of the system. Actually the system is shock excited into oscillation. Since the output tube is cut off and since the voltage generated by the collapsing field is negative on the reaction scanning tube plate so that it is non-conductive, there is essentially no load on the circuit and it oscillates vigorously for one half cycle. If the reaction scanning tube were not present, the circuit would continue to oscillate as shown in Figure 9 (A). This condition, however, is not permitted. One half cycle of oscillation is permitted because at the end of such a time the current in the deflection coil has reached a maximum in the opposite direction to which it was flowing at the end of the trace period. This reversal of the direction of flow of current was the requirement for retrace and it was accomplished in the allotted 7 microseconds.

Now that retrace has been completed, it is necessary to start the next trace. The energy which was placed in the deflection coil by the output tube in the later part of the last trace has not been dissipated. During the one-half cycle of oscillation retrace was accomplished with very little loss of energy. The field in the coil was merely reversed in polarity. So, at this point, a strong field exists in the deflection coil.

As mentioned previously, if the coil were not damped, it would continue to oscillate at its natural frequency as shown in Figure 9 (A). To prevent such an oscillation the reaction scanning tube is brought into action. This tube is in a modified damper circuit which is effectively connected across the deflecting coil.

In the oscillating circuit, the current in the deflection coil lags the voltage by approximately 90 degrees and when the current has reached its maximum negative value, the voltage across the coil being 90 degrees ahead, has begun to swing positive. When the voltage on the reaction scanning tube

plate becomes positive with respect to its cathode, it begins to conduct heavily. This places such a load across the deflection coil that it cannot oscillate. Instead the field begins to decay at a rate permitted by the load which the reaction scanning tube placed on the coil. The circuit constants are such that this decay is linear and at a rate suitable for the visible trace.

If no additional energy were fed into the coil, the field would fall to zero and the Kinescope beam would come to rest in the center of the tube. In such an r-l circuit, as the current approaches its final value, it does not do so linearly but asymptotically as indicated in Figure 9 (B). It is therefore necessary to have the output tube begin to supply power to the deflection coil before the energy in the coil is completely dissipated. Figure 9 (C) shows the shape of the current supplied by the output tube. Although the currents supplied by the output tube and by the decaying field are curved at the cross over point, together they produce a coil current that is linear.

By the time the beam has reached the right side of the Kinescope, the output tube is conducting heavily and has built up a strong field in the transformer and coil. At this point, the output tube is again suddenly cut off and the process is repeated.

The 6BG6G plate voltage is supplied through the 5V4G which is conducting over the major portion of the trace. Capacitors C186 and C188 are charged during this period and this charge is sufficient to supply the 6BG6G plate when the 5V4G is not conducting.

The charge is placed on these capacitors by the receiver d-c supply and by the current from the collapse of the field in the horizontal deflecting coil. The a-c axis of the sweep voltage is 275 volts above ground since the T109 secondary is connected to the receiver 275 volt bus. The charge placed on these capacitors by the coil kick-back is therefore in addition to that from the d-c supply and thus the capacitors are charged to a voltage greater than the d-c supply. This permits operation of the 6BG6G at a higher voltage than is obtainable from the receiver power supply and produces an increase in the system efficiency by salvaging energy that would otherwise have been wasted.

HIGH VOLTAGE POWER SUPPLY (block # 14)—The Kinescope high voltage supply is unusual in that the power is obtained from the energy stored in the deflection inductances during each horizontal scan. When the 6BG6G plate current is cut off by the incoming signal, a positive pulse appears on the T109 primary due to the collapsing field in the deflection coil. This pulse of voltage is stepped up, rectified, filtered and applied to the second anode of the Kinescope. Since the frequency of the supply voltage is high, (15,750 cps), relatively little filter capacity is necessary. Since the filter capacity is small, the stored energy is small, and the high voltage supply is made less dangerous.

LOW VOLTAGE POWER SUPPLY (block #15)—The low voltages for the receiver. The unit is conventional, and employs two 5U4G rectifier tubes in parallel to supply 400 volts d-c at approximately 290 ma.

SERVICE SUGGESTIONS

Following is a list of symptoms of possible failures and an indication of some of the possible faults.

NO RASTER ON KINESCOPE:

- Incorrect adjustment of ion trap--Coils reversed either front to back or top to bottom, ion trap coil open.
- (2) V126 or V127 inoperative—check voltage and waveform on grids and plates.
- (3) No high voltage—If horizontal deflection is operating as evidenced by the correct waveform on terminal 4 of horizontal output transformer, the trouble can be isolated to the 8016 circuit. Either the T109 high voltage winding is open, (points 2 to 3), the 8016 tube is defective, its filament circuit is open, C187 is shorted or R239 open.
- (4) V125 and V120-B circuits inoperative—check for sine wave on V125 grid, pulse on V120-B grid, and sawtooth on V126 grid. Refer to schematic.
- (5) Reaction scanning tube (V128) inoperative.
- (6) Defective Kinescope.
- (7) R152 open, (terminal 3 to ground).
- (8) No receiver plate voltage—filter capacitor or speaker field shorted—negative bleeder or speaker field open.
- NO VERTICAL DEFLECTION:
- V121 or V122 inoperative. Check voltage and wave forms on grids and plates.
- (2) T107 open.
- (3) Vertical deflection coils open.
- NO HORIZONTAL DEFLECTION:
- (1) V125, V120B, V126 or V128 inoperative-check voltage and wave forms on grids and plate.
- (2) T109 open.

(3) Horizontal deflection coil open.

POOR VERTICAL LINEARITY:

- (1) If adjustments cannot correct, change V122.
- (2) Vertical output transformer defective.
- (3) V121 inoperative—check voltage and wave forms on grid and plate.
- (4) R174, C158, C221-C or C222-B defective.
- (5) Low bias or plate voltage—check rectifiers and capacitors in supply circuits.

SIGNAL AT KINESCOPE GRID BUT NO SYNC:

(1) Picture control advanced too far:

- (2) V114-B, V118, V119, or V120-A inoperative. Check voltage and waveforms at their grids and plates.
- (3) C142 defective.

SIGNAL ON KINESCOPE GRID BUT NO VERTICAL SYNC:

- (1) Check V121 and associated circuit-C154, T106, etc.
- (2) Integrating network inoperative—Check C149, C151, C152, C153, R162, R163, R164 and R165.

SIGNAL ON KINESCOPE GRID BUT NO HORIZONTAL SYNC:

- (1) T108 misadjusted
- (2) V123 or V124 inoperative—check socket voltages and waveforms.
- (3) T108 defective.
- (4) C166, C167, C170 or C171 defective.
- (5) If horizontal speed is completely off and cannot be adjusted check C168, C169, R168 and R196.

SOUND & RASTER BUT NO PICTURE OR SYNC:

- Picture i-f, detector or video amplifier inoperative—check V110, V111, V112, V113, V114, V115 and V116—check socket voltages.
- (2) Bad contact to Kinescope grid.

PICTURE STABLE BUT POOR RESOLUTION:

- (1) V114, V115 or V116 defective.
- (2) Peaking coils defective---check for specified resistance.
- (3) C138, C140, C141 or C142 defective.
- (4) Make sure that the focus control operates on both sides of proper focus.
- (5) R-F and I-F circuits misaligned.

PICTURE SMEAR:

- Video amplifier overloaded by excessive input—reduce picture control setting.
- (2) Insufficient bias on V115 and V116 resulting in grid current on video signal. Check bias and possible grid current.
- (3) Defective coupling condenser or grid load resistor—check C138, C140, C141, C223B, R138, R142, R143, R148, etc.
- (4) This trouble can originate at the transmitter—check on another station.

PICTURE JITTER:

- (1) Picture control operated at excessive level.
- If regular sections at the left picture are displaced change V126.
- (3) Vertical instability may be due to loose connections or noise.
- (4) Horizontal instability may be due to unstable transmitted sync. Connect sync link to terminal 1 and 2.

RASTER BUT NO SOUND, PICTURE OR SYNC:

- (1) Defective antenna or transmission line.
- (2) R-F oscillator off frequency.
- (3) R-F unit inoperative—Check V1, V2, V3 and their socket voltages.
- DARK VERTICAL LINE ON LEFT OF PICTURE:
- (1) Reduce horizontal drive and readjust width and horizontal linearity.
- (2) Replace V126.

LIGHT VERTICAL LINE ON LEFT OF PICTURE:

- (1) C181 defective.
- (2) V128 defective.
- (3) Change tap on R209.

POOR HORIZONTAL LINEARITY:

- (1) If adjustments do not correct, change V128 or V126.
- (2) T109 or L201 defective.
- (3) C186 or C188 or R209 defective.
- (4) C179, R187 or R210 defective.

WRINKLES ON LEFT SIDE OF RASTER:

- (1) R180, R201 or C181 defective.
- (2) Defective yoke.

PICTURE OUT OF PHASE HORIZONTALLY:

- T108 winding D to F incorrectly tuned or connected in reverse.
- (2) R200 or R202 defective.

RASTER & SIGNAL ON KINESCOPE BUT NO SOUND:

- (1) R-F oscillator off frequency.
- (2) Sound i-f, discriminator or audio amplifier inoperative check V104, V105, V106, V107, V108, V109 and their socket voltages.
- (3) T114 or C209 defective.
- (4) Speaker defective.

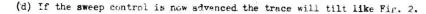
Servicing Notes on 1947-1948 F. M. and Television Receivers Sparton Superheterodyne Model 10-76-PA

F.M. I.F. ALIGNMENT

In that the alignment of the I.F. stages of an F.M. receiver is inherently far more critical than is the case in the conventional A.M. receiver the visual method using an oscilloscope and frequency modulated signal generator should be used where such equipment is available. In case this equipment is not available any good signal generator providing a stable signal at 10.7 Mc. may be used providing a vacuum tube voltmeter and zero center voltmeter are used in place of the output meter. Both methods are outlined below.

Visual Alignment of F.M.-I.F. Transformers and Discriminators.

- 1. Equipment required.
 - (a) Cathode ray oscilloscope with both vertical and horizontal amplifiers and preferably with calibrated screen.
 - (b) Frequency modulated signal generator providing sweep width up to approximately 400 Kc., preferably variable. The modulation voltage should be available at terminals to syncronize the oscilloscope sweep.
 - (c) Insulated alignment tools and shielded leads for the scope and signal generator,
- 2. Preliminary adjustments.
 - (a) Set the signal generator for a center frequency of 10.7 Mc. and allow sufficient warm up time for the generator to stabilize. It is very important that the frequency remain at exactly 10.7 Mc. throughout the entire alignment procedure. A shift in frequency during alignment might result in stagger tuning with consequent impairments of receiver performance.
 - (b) Turn the oscilloscope on and after focusing the beam for the smallest spot of desired brilliance, center the spot exectly.
 - (c) Connect syncronize or sweep terminals of signal generator to the horizontal input post on the oscilloscope.
- 3. Alignment of plate reactor and discriminator.
 - (a) Connect output from signal generator to pin #4 of 1st limiter tube (ASJ7GT).
 - (b) Connect output cable from pin #5 of 6S8GT tube to the vertical input terminals on the scope.
 - (c) With the sweep or modulation control off advance the R.F. control on the signal generator to give a trace approximating Fig. 1.



(e) Adjust core in L15 plate reactor for maximum vertical deflection. Note that the length of trace increases as Fig. 3.



(f) Align discriminator transformer by adjusting primary C60A for maximum vertical deflection,

meanwhile keeping the trace in the exact center of the screen by adjusting secondary C6OB.







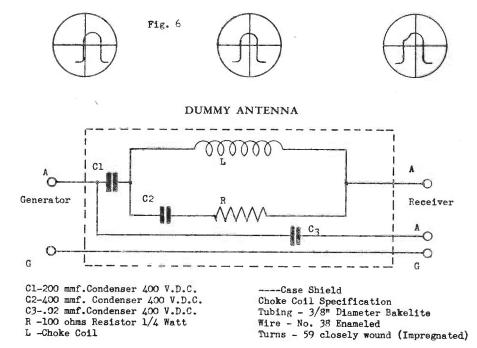
When the discriminator has been properly aligned and the generator sweep increased to about 400 Kc. the conventional shaped discriminator curve will be presented on the screen.

See Fig. 5.



This presentation will be helpful for final alignment and balance of the discriminator transformer. Make sure that the straight center position crosses the exact center of the screen and that the distance from the pertical center line to each peak is approximately equal.

- 4. Alignment of #3 I.F. Transformer
 - (a) Connect input from signal generator to pin #4 on No. 2 I.F. amplifier tube (6SK7GT).
 - (b) Connect output cable from AVC terminal on #3 I.F. transformer to the vertical terminals on the scope using a 50 K ohm isolating resistor at the set end of the cable.
 - (c) With generator sweep width set for approximately 400 Kc. increase R.F. output until a convenient pattern is presented on the screen.
 - (d) Adjust C42A and C42B for maximum vertical deflection with a symmetrical curve. See Fig. 6.



Note: When using this dummy antenna the generator output impedance should be 10 ohms or lower.

- 5. Alignment of No. 2 I.F. Transformer
 - (a) Connect input from signal generator to pin #4 of No. 1 I.F. tube (6SK7GT). The output connection remains at the AVC terminal of the 3rd I.F. transformer.
 - (b) Align C33A and C33B per instructions and diagram in (c) and (d) above.
- 6. Alignment of No. 1 I.F. Transformer
 - (a) Connect input from signal generator to Pin #6 on the converter tube (7Q7). (Note: There will be an apparent reduction in gain here due to the short circuiting effect of the F.M. detector coil but this may be compensated for by increasing the generator output. If the generator output is still too low the lead from 7Q7 pin #6 to the wave band switch may be unsoldered thus removing the short circuit).
 - (b) Align C27A and C27B per instructions in (c) and (d) Par. 4. See Fig. 6.
- 7. Caution: Do not try to "touch up" or worse yet completly align the I.F. channel by applying the signal to the converter grid. To do so will almost certainly result in misalignment of one stage to compensate for the poor alignment of another.
- 8. For alignment of the A.M.-I.F. transformers see alignment chart. Operation #2

Sparton Superheterodyne Model 10-76-PA

ine Volta	age: 117 Volts AC	Position Position								nnel.
			Ve				to Grou chematic			
TUBE	FUNCTION	No. 1	No. 2		No. 4			No. 7	No. 8	Grid Cap
6SG7	R. F. Amplifier	0	0	2.20	.10	2.20	155	6.0*	270	
707	Osc. & Convt.	6.05*	270	110	-9.8	0	**	0	0	
6SK7GT	No. 1 I. F. Amp.	0	0	3.0	**	3.0	95	6.05*	270	
6SK7GT	No. 2 I. F. Amp. ***	0	0	3.0	**	3.0	***	6.05*	270	
6SJ7GT	lst Limiter	0	0	0	3	0	46	6.05*	270	
6SJ7GT	2nd Limiter	0	0	0	42	0	47	6.05*	207	
658GT	F.MA.M.Det. 1st Audio	20	0	20	30	**	95	6.05	0	27
6V6G	Power Amp.	0	0	260	270	**	****	6.05*	12.5	
5Y3GT	Rectifier	0	375	0	360*	0	360*	360	375	
6E5	Viso-Glo	5.95*	23	-4.4	270					

VOLTAGE CHART

NOTES: Voltage readings are for schematic diagram on back of sheet. Allow 15% / or - on all measurements. Always use meter scale which will give greatest deflection within scale limits. All DC measurements made with 20,000 ohms per volt voltmeter. All AC voltages made with rectifier type voltmeter. Unless designated otherwise, voltages in table are / DC voltages.

* AC volts.

Cannot be measured with 20,000 ohms per volt voltmeter.

** Band switch in F.M. position.

**** Zero volts or 237 volts. (Tie point only on some receivers).

THE SPARKS-WITHINGTON COMPANY

Sparton Superheterodyne Model 10-76-PA

ALIGNMENT CHART

OPER- ATION	ALIGNMENT OF	GENERATOR CONNECTED TO		GENERATOR FREQUENCY	BAND Switch Setting	TUNNING COND. SETTING	TRIMMER	REMARKS
1	Set dial poir	nter even with lef	t-hand st	op line wi	th condens	er closed.		
2	A.MI.F.	Pin #6 of 7Q7 Convt. Tube	.02 MFD Cond.	456 KC.	BC.	Open	C34A & B C28A & B	Peak Accurately
3		1		1600 KC.		1600 KC.	C24B Osc.T.	11 11
	BC.	BC.			BC.	1500 KC.	C3B R.F.TR.	-11 11
4	R.F.	ANT.	*	1500 KC.			C2A Ant.TR.	11 17
5	1		o	600 KC.		600 KC.	C24A Osc. P.	**
6	Repeat opera	tions 3, 4, & 5.	•		λ		▲	
7		ations at 600 KC.,	1000 KC.	, and 1500	KC.			
	1	T	1				C25 Osc.Tr.	Peak Accurately
				1			C2B R.F.Tr.	**
8	S.W.	F.M. ANT.	*	18 MC.	S.W.	18 MC.	C3A Ant.Tr.	**
	BAND	to GND.			BAND		C26 Osc. P.	See Oper. #9
9	C26 Osc. Pade	der is precision s	et at the	factory a	nd should	not be mov	red.	
	Repeat opera							and a start of the second s
10	Check calibra	ation at 6 MC. and		daval alta	mont inst	metions		and 5 of this
	Check calibra SPECIAL NOTE	ation at 6 MC. and : For complete F. n alternate F.MI	MI.F. v .F. align					
11	Check calibra SPECIAL NOTE bulletin. An	ation at 6 MC. and : For complete F. n alternate F.MI elow.	MI.F. v .F. align	ment using				
11 12	Check calibra SPECIAL NOTE bulletin. An 17, and 18 bo	ation at 6 MC. and For complete F. n alternate F.MI elow. Pin No. 4 on 1st	MI.F. v .F. align .02 MFD. Cond.	IO.7 MC. Unmod. 10.7 MC.	a V.T.V.M	l. is shown	in operation	is 13, 14, 15, 16
11 12 13	Check calibra SPECIAL NOTE: bulletin. An 17, and 18 bulletin. LIMITER Disc. Stage	ation at 6 MC. and For complete F. n alternate F.MI elow. Pin No. 4 on 1st Lim. Tube. Pin #4 on 1st	MI.F. v .F. align .02 MFD. Cond.	io.7 NC. Unmod.	a V.T.V.M F.M.	. is shown Optional	L15 Slug C60A Disc.	s 13, 14, 15, 16
11 12 13 14	Check calibra SPECIAL NOTE: bulletin. An LIMITER Disc. Stage Pri. Disc. Stage	ation at 6 MC. and For complete F. n alternate F.MI elow. Pin No. 4 on 1st Lim. Tube. Pin #4 on 1st limiter to Gnd. Pin #4 on 1st	MI.F. v .F. align .02 MFD. Cond.	IO.7 MC. Unmod. 10.7 MC.	a V.T.V.M F.M.	. is shown Optional	L15 Slug C60A Disc. Prim. C60B Disc.	8 13, 14, 15, 16
11 12 13 14 15	Check calibra SPECIAL NOTE: bulletin. An 17, and 18 bu LIMITER Disc. Stage Pri. Disc. Stage Stage Stage	ation at 6 MC. and For complete F. n alternate F.MI elow. Pin No. 4 on 1st Lim. Tube. Pin #4 on 1st limiter to Gnd. Pin #4 on 1st Limiter to Gnd.	MI.F. v. .F. align .O2 MFD. Cond. .O2 MFD. Cond.	IO.7 MC. Unmod. 10.7 MC. Unmod. 10.7 MC.	a V.T.V.M F.M.	. is shown Optional	L15 Slug C60A Disc. Prim. C60B Disc. Sec. C42A & B No. 3. I.F. C33A & B No. 2 I.F.	s 13, 14, 15, 16
11 12 13 14 15 16	Check calibra SPECIAL NOTE: bulletin. An 17, and 18 bu LIMITER Disc. Stage Pri. Disc. Stage Stage Stage	ation at 6 MC. and For complete F. n alternate F.MI elow. Pin No. 4 on 1st Lim. Tube. Pin #4 on 1st limiter to Gnd. Pin #4 on 1st Limiter to Gnd. Note "A"	MI.F. v .F. align .O2 MFD. Cond. .O2 MFD. Cond.	IO.7 MC. Unmod. 10.7 MC. Unmod.	a V.T.V.M F.M. F.M.	Optional	L15 Slug C60A Disc. Prim. C60B Disc. Sec. C42A & B No. 3. I.F. C33A & B	s 13, 14, 15, 16
11 12 13 14 15 16 17	Check calibra SPECIAL NOTE: bulletin. An 17, and 18 bu LIMITER Disc. Stage Pri. Disc. Stage Stage Stage	ation at 6 MC. and For complete F. n alternate F.MI elow. Pin No. 4 on 1st limiter to Gnd. Pin #4 on 1st Limiter to Gnd. Note "A" Note "B"	MI.F. v. .F. align .O2 MFD. Cond. .O2 MFD. Cond.	IO.7 MC. Unmod. 10.7 MC. Unmod. 10.7 MC.	a V.T.V.M F.M. F.M.	Optional Optional	L15 Slug C60A D1sc. Prim. C60B D1sc. Sec. C42A & B No. 3. I.F. C33A & B No. 2. I.F. C27A & B	s 13, 14, 15, 16
11 12 13 14 15 16 17 18	Check calibra SPECIAL NOTE: bulletin. An 17, and 18 bu LIMITER Disc. Stage Pri. Disc. Stage Sec. F.MI.F.	ation at 6 MC. and For complete F. n alternate F.MI elow. Pin No. 4 on 1st limiter to Gnd. Pin #4 on 1st Limiter to Gnd. Note "A" Note "B"	MI.F. v .F. align .O2 MFD. Cond. .O2 MFD. Cond. .O2 MFD. Cond.	IO.7 MC. Unmod. IO.7 MC. Unmod. IO.7 MC. Unmod. IO8 MC.	a V.T.V.M F.M. F.M.	Optional	L15 Slug C60A Disc. Prim. C60B Disc. Sec. C42A & B No. 3. I.F. C33A & B No. 2 I.F. C27A & B No. 1 I.F.	<pre>s 13, 14, 15, 16 **** **** See Note 1. See Note 2. </pre>
11 12 13 14 15 16 17	Check calibra SPECIAL NOTE: bulletin. An 17, and 18 bu LIMITER Disc. Stage Pri. Disc. Stage Stage Stage	ation at 6 MC. and For complete F. n alternate F.MI elow. Pin No. 4 on 1st limiter to Gnd. Pin #4 on 1st Limiter to Gnd. Note "A" Note "B" Note "C"	MI.F. v .F. align .02 MFD. Cond. .02 MFD. Cond.	10.7 MC. Unmod. 10.7 MC. Unmod.	a V.T.V.M F.M. F.M.	Optional Optional i0.7 MC.	L15 Slug C60A Disc. Prim. C60B Disc. Sec. C42A & B No. 3. I.F. C33A & B No. 2 I.F. C27A & B No. 1 I.F. C22 Osc.Tr.	<pre>s 13, 14, 15, 16 *** *** See Note 1. See Note 2. n n n n n n n</pre>
11 12 13 14 15 16 17 18	Check calibra SPECIAL NOTE: bulletin. An 17, and 18 bu LIMITER Disc. Stage Pri. Disc. Stage Sec. F.MI.F.	ation at 6 MC. and For complete F. n alternate F.MI elow. Pin No. 4 on 1st limiter to Gnd. Pin #4 on 1st Limiter to Gnd. Note "A" Note "B" Note "C" F.M. Ant.	MI.F. v .F. align .O2 MFD. Cond. .O2 MFD. Cond. .O2 MFD. Cond.	IO.7 MC. Unmod. IO.7 MC. Unmod. IO.7 MC. Unmod. IO8 MC.	a V.T.V.M F.M. F.M.	Optional Optional i0.7 MC.	L15 Slug C60A Disc. Prim. C60B Disc. Sec. C42A & B No. 3. I.F. C33A & B No. 2 I.F. C27A & B No. 1 I.F. C22 Osc.Tr. C13 R.F.TR.	s 13, 14, 15, 16

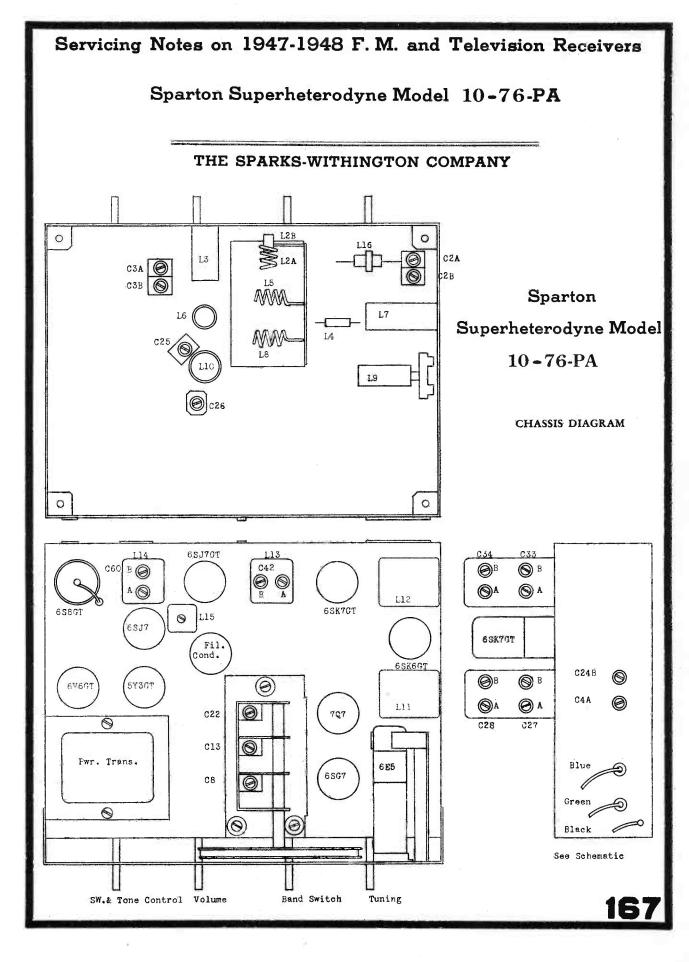
Use dummy antenna as described on page 1 of Rock dial while adjusting for maximum output. **

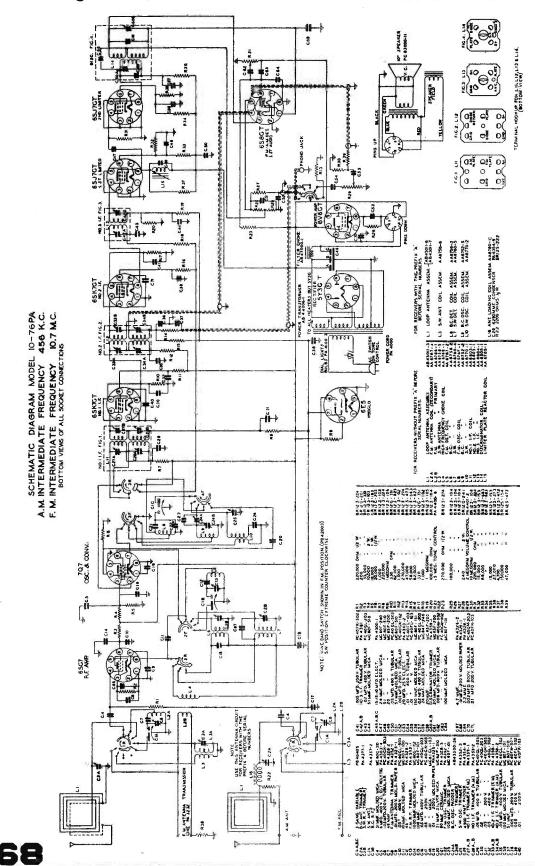
*** Connect V.T.V.M. from C.T. of discriminator coil to chassis gnd. using lowest scale on D.C. NOTE 1: Connect V.T.V.M. from pin #5 of 6S8CT tube to gnd. adjust for zero reading on V.T.V.M.
 NOTE 2: Connect V.T.V.M. between A.V.C. terminal on #3 I.F. Trans. to gnd. Tune for maximum response

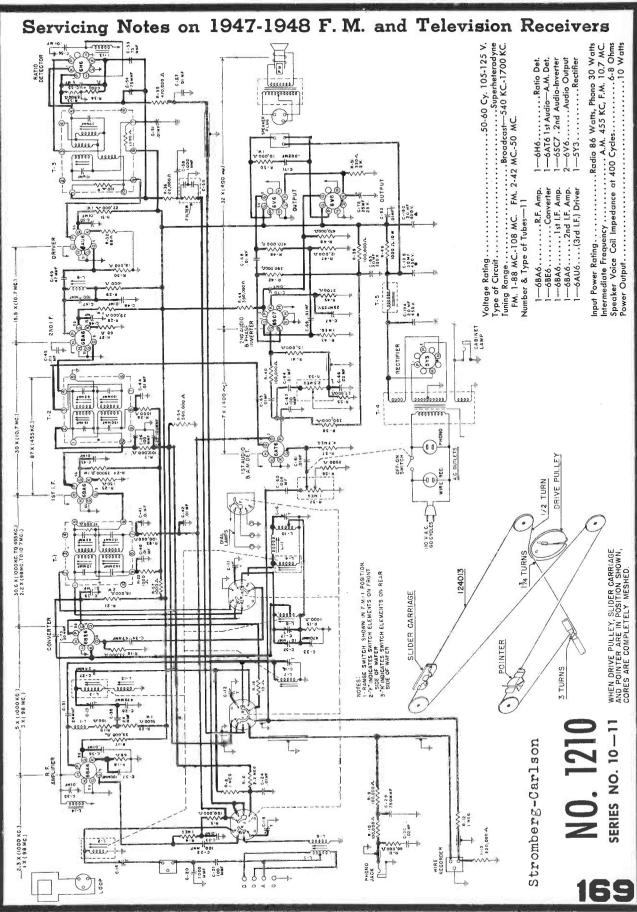
on lowest scale D.C. range.

66

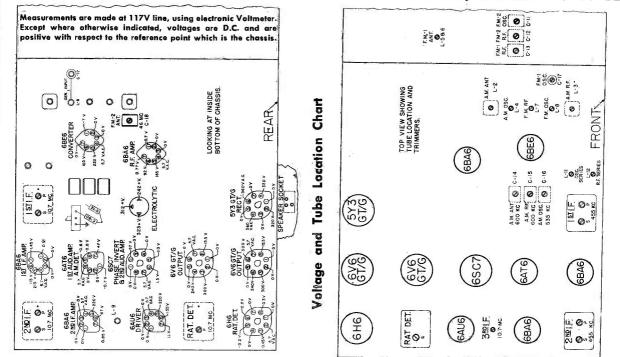
"A" Connect signal generator between pin #4 on No. 2 I.F. tube and gnd. "B" Connect signal generator between pin #4 on No. 1 I.F. tube and Gnd. "C" Connect signal generator between pin #6 on 727 converter tube and gnd.





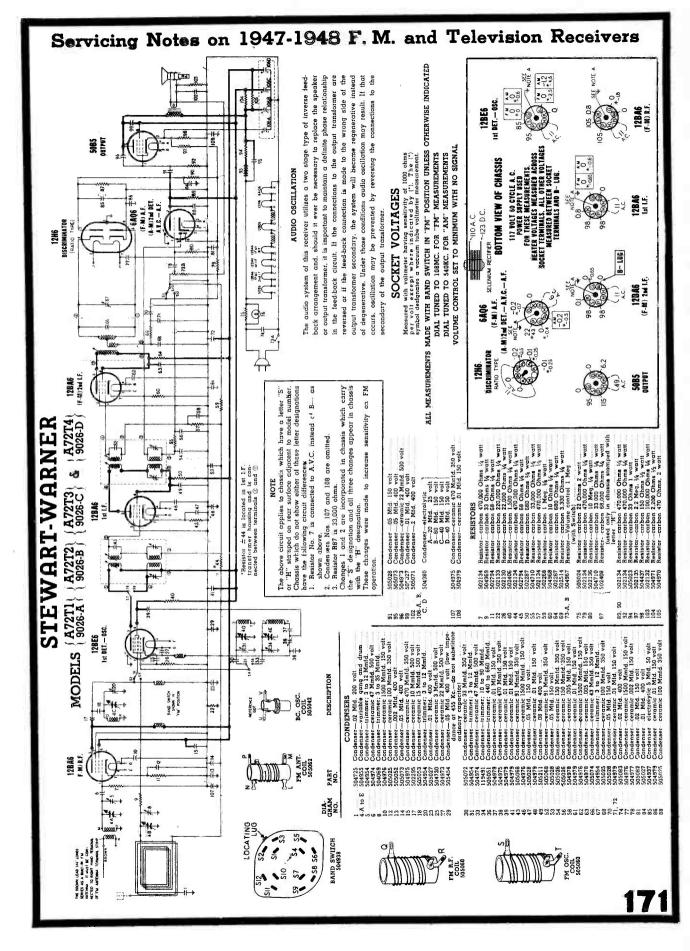


Servicing Notes on 1947-1948 F. M. and Television Receivers STROMBERG - CARLSON Model 1210, Series No. 10-11



ALIGNMENT PROCEDURE 1210

Bond and Pointer Settin	ng Input Generator Setting	Input and Dummy	VTM and Scope Input	Trimmer Adj. and Notes
		A.M. I.F. ALIGN	MENT	
1 AM Low end of dial	455 kc. 400 cy. mod.	Junction C-17 and L-8. See location chart. 100 mmf. dummy	Junction R-12 and C-60 (See location chart)	Adj. Pri. and Sec. 1st and 2nd I.F. (To of Chassis) for highest voltage on -3 DC Scale
2 1	455 kc. swept 15 kc.	**	i)	Adj. same cores as above for be over-lapping curve on scope.
		F.M. I.F. ALIG	NMENT	
FM (1) Low end of dial	10.7 mc. 400 cyc. mod.	Junction C-17 and L-8. See location chart. 100 mmf. dummy	AVC buss (Green and White Wire)	Detune Sec. Ratio Det. (Top of Cha sis). Adj. Pri. and Sec. 1st and 2nd L. Pri. Ratio Det. (Bottom of Chassis) an 3rd l.F. (L-9 Top of Chassis) an -3 VD Scale for max. AVC voltage.
* 13 VIL 10 VIL	10.7 mc. swept 150 kc.		Pin No. 6 Driver tube (screen) thru .01 capac.	Adj. same cores (as in step 1) for bes overlapping curve on scope.
*Repeat 2 and 3 if ne	n Ressarý	ı) ²¹ 2.	Junction R-12 and C-60	Adj. Sec. of Ratio Det. for zero volt age. (Top of Chassis),
		A.M. R.F. ALIG	MATNE	and the second
Broadcast Extreme	535 Kc.	Ant. term.	AVC Buss	
Low Freq.	400 cyc. mod.	200 mmf. dummy	Green and White Wire	Adj. C-16 for max. AVC voltage
Extreme Hi Freq.	1700 Kc. 400 cyc. mod.	17	"	Adj. L-11 for max. AVC voltage
Repeat 1 and 2			· · · · · · · · · · · · · · · · · · ·	Add, corr for max. Ave voltage
600 Kc	600 Kc. 400 cyc. mod.	11	17	Adj, C-15 for max, AVC voltage
1500 Kc	1500 Kc. 400 cyc, mod.	· · · · · · · · · · · · · · · · · · ·	ŋ	Adj. L-12 for max. AVC voltage
Repeot 4 and 5				ridi. E-12 for max. Ave volidge
600 Kc	600 Kc. 400 cyc. mod.	0		Adj. C-14 for max. AVC voltage
		F.M. R.F. ALIG	NMENT	Aul: C-14 for mux. AVC volidge
FM 1 Channel 260	100 Mc	Ant. term. (DD) 150 ohm series with each side of Gen.	AVC Buss Green and White Wire	CAUTION: Align FM-1 1st. 1. C-17 2. C-13 3. L-5 and 6 Voltage. (All Trimmers)
FM 2 Channel 60	46 Mc.	υ	nt to avoid overloading.	1. C-11 2. C-12 3. C-12 Voltage (All Trimmers)



Servicing Notes on 1947-1948 F. M. and Television Receivers FREQUENCY MODULATION -

INSTRUMENTS: Alignment of the FM circuits in this receiver may be accomplished with either a conventional AM type signal generator or an FM signal generator. The output indicator should be an oscilloscope or a vacuum tube voltmeter.

Although it is preferable to use an FM generator and an oscilloscope, reasonably accurate alignment is obtainable when using a conventional » AM generator and a vacuum tube voltmeter providing proper care is exercised in adjusting the discriminator circuit trimmer condenser.

IMPORTANT: If an AM signal generator is used, it should be capable of producing fundamental frequencies of 10.7 and 88 to 108 MC. Avoid using an AM generator which produces signals in the 88 to 108 MC range by using harmonics higher than the second. Generators which are dependent upon third, fourth or fifth harmonics for frequencies of 88 to 108 MC will generally produce undesireable spurious beat signals with the local oscillator in the receiver and alignment will be exceedingly difficult.

The following procedure is adaptable for use with either an AM or FM generator and oscilloscope or vacuum tube voltmeter-merely follow the instructions that are applicable to the instruments that are used.

SIGNAL	GENERATOR CONNECT	IONS	V-T VOLTMETER OR OSCILLO	SCOPE CONNECTIONS	1	•
CONNECT HIGH SIDE OF SIGNAL GENERATOR TO	CONNECT GROUND LEAD OF SIGNAL GENERATOR TO	The second se	IF A V-T VOLTMETER IS USED, CONNECT IT AS FOLLOWS:	IF AN OSCILLOSCOPE IS USED, CONNECT IT AS FOLLOWS:	BAND SWITCH POSITION	
Pin #1 of 12BA6 (FM) 2nd I.F. use a .01 MFD. condenser in series with generator lead.	B— in vicinity of 12BA6 (FM) 2nd LF. tube.	10.7 MC AM signal may be 400 cycle modu lated or FM signal should preferably be mod- ulated ±300 KC.	Connect common (or ground) ter- mind of meter to B, D.C. probe lead of meter is then connected to pin #3 of the 12H6 tube.	Connect vertical amplifier "high" lead in series with an 0.1 MFD. condenser to pin #7 of 6ÅQ6 tube. Con- nect scope ground lead to B	FM Maximum clockwise position	Read across two pares.
Same as above Same as above		Same as above	Before connecting V-T voltmeter, it is necessary to connect two 58,000 ohm resistors (resistance of both units must compare within 1%) in series from pin $\#3$ of the 12H6 tube to B—. Then connect common (or ground) terminal of V-T volt- meter to the junction of these two resistors. D.C. probe lead of meter is now connected to junction of re- sistor $\#59$ (3300 ohms) and con- denser $\#70$ (.05 MFD.) which are in the discriminator output circuit.	Same as above	Same as above	le next page.
Recheck the two preced	ing adjustments to be sur	e that both trimmers a	re set as accurately as possible to o	bain the specified output ind	cation on vacuum	3
Pin #1 of 12BA6 (FM) 1st I.F. tube; use a .01 MFD. condenser in se- ries with generator lead. IFM) 1st I.F. tube.		Same as above	Connect common (or ground) ter- minal of meter to B, D.C. probe lead of meter is then connected to Pin #3 of the 12H6 tube.	Same as above	Same as above	d on
Pin #7 of 12BE6 tube; use a .01 MFD, con- denser in series with generator lead.	B— in vicinity of 12BE6 tube.	Same as above	Şame as above	Same as above	Same as above	sinue
Generator output leads the two "External FM back of antenna loop f lead to one terminal in resistor and connect g to the other terminal in resistor.	series with a 120 ohm renerator ground lead	98 MC AM signal may be 400 cycle modu- lated or FM signal should preferably be mod- ulated ±300 KC.	Same as above	Same as above	Same as above	t is conti
Same as	above	Same as above	Same as above	Same as above	Same as above	chart
Same as	above	Same as above	Same as above	Same as above	Same as above	This o
179 Check	c calibration and tracking	of receiver with input	signals of 88 and 108 MC.			

"If your signal generator has an AC-DC type power supply, insert a .25 MFD, condenser in series with the ground lead before making the connections

Servicing Notes on 1947-1948 F. M. and Television Receivers "FM" — ALIGNMENT PROCEDURE

- 1. If alignment of both AM and FM channels is required it is necessary to align the AM channel first, then align the FM channel as instructed in the following chart
- 2. Before removing the chassis from the cabinet, turn the tuning control until dial pointer is at 98 MC. Then remove chassis and place a pencil mark on dial frame so as to indicate the 98 MC calibration point.
- 3. Do not attempt to reposition pointer by releasing it from clip on dial card as this is done only during AM alignment.
- 4. Set the receiver volume control to the maximum volume position.
- 5. Dress FM circuit leads as short and straight as possible, particularly those in the oscillator circuit. I.F. plate and grid leads should also be kept short and straight.
- 6. Alignment of receiver circuits may now be accomplished by using the procedure in the chart below.

BEC	EIVER		TYPE OF ADJUSTMENT AND OUTPUT INDICATION					
DIAL	TRIMMER OR SLUG NUMBER	TRIMMER DESCRIPTION	ADJUSTMENT AND OUTPUT INDICATION WHEN USING A V-T VOLTMETER	ADJUSTMENT AND OUTPUT INDICATION WHEN USING AN OSCILLOSCOPE				
Any position where it does not affect the signal.	8	Discriminator Primary	Set meter to a low D.C. voltage range and adjust trimmer #8 for maximum meter reading. (This voltage will be negative.)	Set vertical emplifier of scope for maximum emplification. Where FM signal generator provides an output voltage for synchronization, connect this voltage to "sync" terminals of the scope. Then adjust setting of trimmer $\#3$, before attempting to adjust trimmer $\#8$, until a pattern similar to the following appears on the screen. Il pattern does not remain stationary, operate sweep frequency control on scope and also "sync" control until desired result is obtained. A A B C C C C This double "S" curve pattern results when "scope uses "Sawtoch" This single "S" curve pattern results when "scope uses "Sawtoch"				
,				Adjust trimmer #8 for maximum amplitude and steepness of that portion of the curve between "A"				
Same as above 9		Discriminator Secondary Use an insulated phas- ing tool to adjust this trimmer.	Set meter for operation on its lowest D.C. voltage range. Note that as trimmer #9 is rotated a point will be found where voltmeter will swing rather sharply from a positive to a negative reading or vice versa. Correct setting of trimmer #9 is obtained when meter reads zero as trim- mer is moved through this point. The ad- justment is somewhat critical and con- siderable care must be exercised to set the trimmer for a zero meter indication.	With the 'scope set up as described above, adjust trimmer #9 until the cross-over point "B" is cen- trally located in both the horizontal and vertical directions; in addition, the portion of the curve be- tween "A" and "C" should be as linear (straight) as possible.				
whe weltmotor or org	l	connect and remove the t	wo 68,000 ohm resistors that were used for the	ne vacuum tube voltmeter connection in the 2nd step.				
Same as above	10 and 11	2nd I.F.	Adjust trimmers #10 and #11 for maxi- mum meter reading.	With scope set up as described above. Galas and mers #10 and #11 for maximum amplitude and steepness of that portion of the pattern between "A" and "C".				
Same as above	12 and 13	lst I.F.	Adjust trimmers #12 and #13 for maxi- mum meter reading.	Adjust trimmers #12 and #13 for maximum ampli- tude and steepness of pattern as described above. If the enlarged pattern now indicates a lack of sym- metry, readjust trimmer #9 for correct cross-over point.				
98 MC	14	Oscillator Trimmer	Set trimmer #14 to receive 98 MC. signal and adjust for maximum meter reading.	Adjust trimmer #14 to obtain the symmetrical pattern shown above. Correct setting of trimmer #14 is obtained when cross-over point in pattern is centrally located.				
, and the second se	15	R.F. Trimmer	Adjust trimmer #15 for maximum meter reading.	Adjust trimmer #15 for maximum amplitude of pattern.				
98 MC	12 and 13 lst LF.		Recheck adjustment of these trimmers for maximum meter reading.	Recheck adjustment of these trimmers for maximum amplitude and symmetry of pattern.				
98 MC	16	Antenna Trimmer	Adjust trimmer #16 for maximum meter reading.	Adjust trimmer #16 for maximum amplitude of pattern.				
al (Marconstant) - and your a file of your strain of the second strain o	1		1	and the second se				

Servicing Notes on 1947-1948 F. M. and Television Receivers A72T2 A72T3 A72T4

Stewart-Warner Models A72T1 9026A 9026B

BROADCAST BAND - "AM" - ALIGNMENT PROCEDURE

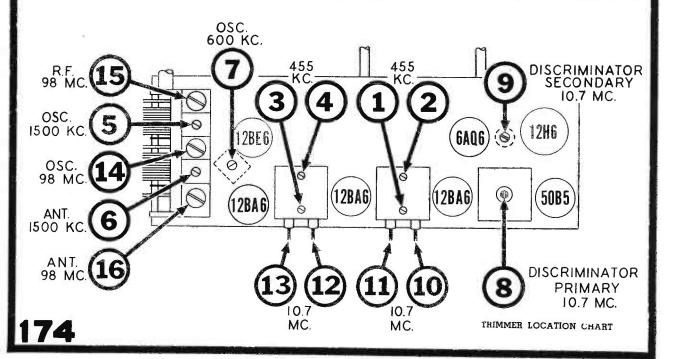
9026C

9026D

1. Remove chassis and loop antenna from cabinet.

- 2. With the gang fully meshed, the dial pointer should be in the position indicated by the last mark below 55 on the dial. If it is set incorrectly, release the pointer clip on the dial cord and reposition pointer.
- 3. During the alignment of this receiver, it will be necessary to set the dial pointer to the following frequencies: 1500 Kc., and 600 Kc. In order to avoid replacing the chassis in the cabinet each time a dial setting is required, it will be found more convenient to mark the required frequency points on the white dial background before starting the alignment.
- 4. Connect an output meter across speaker voice coil or from plate of the 50B5 tube to B— through a 0.1 Mfd. condenser (see voltage chart for convenient B- connection).
- 5. Connect ground lead of signal generator to B-- lug. CAUTION: If your signal generator is designed with an AC-DC type power supply, connect ground lead of signal generator to B- lug through a .25 Mfd. condenser.
- 6. Set volume control to the maximum volume position and use a weak signal from the signal generator.
- 7. If alignment of both AM and FM channels is required, it is necessary to align the AM channel first; then align the FM channel as instructed in the preceding section.

DUMMY ANT. IN SERIES WITH SIGNAL GENERATOR	CONNECT HIGH SIDE OF SIGNAL GENERATOR TO	SIGNAL GENERATOR FREQUENCY	BAND SWITCH POSITION	RECEIVER DIAL SETTING	TRIMMER NUMBER	TRIMMER DESCRIPTION	TYPE OF ADJUSTMENT
0.1 MFD. Condenser	Pin #7 of 12BE6 tube.	455 KC	Broadcast (counter- clockwise)	Any point where it does not affect the signal.	1-2	2nd I.F.	Adjust for maximum output. Then repeat adjustment.
200 MMFD. Mica Condenser	External Anten- na Terminal (AM) on Loop Antenna	1500 KC	Broadcast (counter- clockwise)	1500 KC	5	Broadcast Oscillator	Adjust for maximum output.
200 MMFD. Mica Condenser	External Anten- na Terminal (AM) on Loop Antenna	1500 KC	Broadcast (counter- clockwise)	Tune to 1500 KC Generator Signal	6	Broadcast Antenna	Adjust for maximum output.
200 MMFD. Mica Condenser	External Anten- na Terminal (AM) on Loop Antenna	600 KC	Broadcast (counter- clockwise)	Tune to 600 KC Generator Signal	7	Broadcast Oscillator (Series Pad)	Adjust for maximum output. Try to increase output by de- tuning trimmer and retuning receiver dial until maximum output is obtained.
200 MMFD. Mica Condenser	External Anten- na Terminal (AM) on Loop Antenna	Repeat o	rdjuštment of tr	immers 5 and 6 at 15	500 Kc. Then re	e-chëck adjustment	of trimmer 7 at 600 Kc.



These helpful notes on adjustment and detection of external faults in television receivers is taken from Stewart-Warner T-711 Manual.

CONTRAST—The receiver has now been properly tuned to the selected Television Station and the picture may be made visible by turning the "Contrast" knob on the front panel in a clockwise direction. As the name suggests, the "Contrast" control adjusts the black and white contrast between the various picture elements. This control should be turned clockwise until the picture remains stationary on

the screen but not so high that the gradation between black and white is lost. In the event that the picture does not reremain stationary on the screen, proceed to the next step.

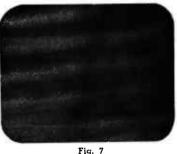
-Should the picture on the screen appear to move horizontally or completely break up as shown in Figure 7, adjustment of the "Horizontal Hold" control on the rear of the chassis is necessary. This control locks the horizontal picture elements in synchronism with the transmitted picture, and although it has a relatively wide control range, care should be taken to set it correctly so as to insure optimum performance. As a check for proper setting of this control, turn the set off for a few seconds and then turn it on again. If the control is properly set, the picture should lock into position within a reasonable interval after the picture tube becomes illuminated.

In the event that strong reflections or "ghosts" occur, which are displaced approximately ¼ raster width from the true picture, then the "Horizontal Hold" control may not lock the picture into synchronism. It will therefore be necessary to orient the antenna so as to minimize reflected signal response.

VERTICAL HOLD— Should the picture appear to roll by in a vertical direction or cause multiple overlaping vertical images, as shown in Figure 8, it is



Sound Interference Caused by Incorrect Tuning



Horizontal Movement



Fig. 8 Vertical Movement



Fig. 9 Reduce Contrast—Increase Brightness

necessary to adjust the "Vertical Hold" control on the rear of the chassis. After the adjustment is made, reduce the setting of the contrast control until the picture is barely visible, then readjust the "Vertical Hold" control to "lock" the picture in position.

READJUST BRIGHTNESS AND CONTRAST—The "Brightness" and "Contrast" controls must be adjusted simultaneously to strike a proper balance of picture quality. Too much contrast and too little brightness is apparent when the picture is lacking in gradation between black and white or if the picture loses form as shown in Figure 9. Too little contrast and too much brightness causes the picture to appear faded so that it seems composed entirely of grays, as illustrated in Figure 10.

FOCUS --- If the pic-

ture has a fuzy or cloudy appearance as illustrated in Figure 11, the "Focus" control should be readjusted to a position which gives sharpest definition.

HORIZONTAL LINE-ARITY - Adjustment of picture linearity, both horizontal and vertical, must be made while receiving some form of circular test patten on the receiver screen. Broadcasting stations usually transmit a pattern of that type before their regular entertainment programs. Improper horizontal linecrity will cause the circular pattern to appear condensed on one side of the screen and extended on the other side as shown in Figure 12. Proper horizontal balance can be obtained by adjusting the "Horizontal Linearity" control on the rear of the chassis. It may be necessary to readjust the "Width" control if an appreciable change was made in the linearity control setting.

VERTICAL LINEAR-ITY --- Improper vertical linearity will cause the circular test pattern to appear condensed on the upper edge of the screen and extended on the lower edge or vice versa. The effect of incorrect setting of the "Vertical Linearity" control is shown in Figure 13. Proper linearity is obtained by adjusting the "Vertical Linearity" control on the rear of the chassis. It may be necessary to readjust the "Height" control if an appreciable change was

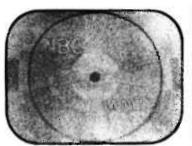


Fig. 10 Increase Contrast—Reduce Brightness



Fig. 11 Adjust Focus

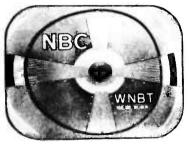


Fig. 12 Adjust Horizontal Linearity

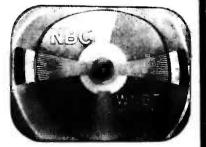


Fig. 13 Adjust Vertical Linearity

made in the linearity control setting.



The quality of the picture that is reproduced on the screen of a modern television receiver is dependent upon many factors, some of which are beyond the control of the receiver. The information presented in the following paragraphs is therefore intended to aid the installation and serviceman in becoming acquainted with the way a perfectly normal television receiver will perform when it receives transmitted picture signals which have been affected by some unfavorable external condition.

The strength of the transmitted picture signal that reaches the receiver is a vitally important factor in determining the quality of the picture that is reproduced on the screen. A very weak signal will produce a picture similar in appearance to that shown in Figure 15. In cases where the signal is exceedingly weak the picture has a "milky" appearance which is usually accompanied by a "speckled" or "snow" effect.

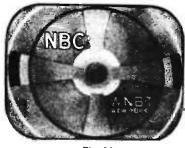


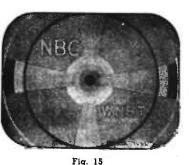
Fig. 14 Correctly Adjusted Picture

The very high frequency waves used for the trans-

mission of television picture signals act quite similarly to rays of light in that they do not bend around corners and are reflected by obstacles in their path. It should therefore be appreciated that television waves do not follow the curvature of the earth and reliable reception should only be anticipated in the region determined by the "line of sight" to the horizon in all directions from the antenna tower of the transmitting station. This region and the strength of signals encountered within that area is usually found to be adequate.

Since signal strength decreases rapidly when the "line of sight" distance is exceeded it is not possible to reliably predict conditions which might prevail at greater distances away from the transmitter. The technician who installs the television receiver must always carefully check to determine if signals at a particular location are of satisfactory strength.

The characteristic of high frequency television signals which permit them to be reflected from the walls of nearby buildings or other objects may, under certain conditions, create "multiple transmission paths." This would permit the reflected signal to arrive at the antenna a short interval of time later than the signal traveling in a direct path from the transmitter and the effect produced on the picture of the television receiver is illustrated in Figure 16. These multiple images,



Weak Signal

known as "echoes" or "ghosts," may generally be prevented by careful installation and orientation of the antenna.

Aircraft in the vicinity may also produce a temporary "multiple transmission path" as the surfaces of a plane are capable of reflecting television signals. Although this source of interference is usually rare, its effect would be recognized by a temporary fluctuation in picture brightness and sound volume as well as the existence of a "ghost" image. In areas of relatively low signal strength, aircraft interference may cause the picture to temporarily lose synchronization or "tear out."



Severe static, or man-made electrical interference, which is audible in a conventional receiver may be both audible and visible in a television receiver. For example, interference from automobile ignition systems, inadequately filtered electrical appliances, arcing electrical contacts, elevators, street cars, or electric signs may cause white streaks in the picture as shown in Figure 17. If the interference is particularly severe, the picture may lose synchronization and effects similar to those shown in Figures 7 or 8 will prevail.

A "herring bone" pattern in a television picture indicates the existence of interference from electrically operated medical equipment such as diathermy machines. When such equipment is in relatively close proximity to a television receiver, the resulting interference may either partially or completely obliterate the picture as indicated in Figure 18.

Interference created by signals coming from a short wave transmitter that may be close to the receiver or operating on the wrong frequency will produce the type of pattern shown in Figure 19. This bar pattern appears to ripple or move across the screen diagonally and should not be confused with the horizontal pattern produced by incorrect tuning. The type of interference described here should be rarely encountered and is only included in this section in the interest of furnishing complete information on the subject of interference phenomenon.

If the quality of the television picture is unsatisfactory, the fault may not lie in the antenna system or the receiver, but may be due to temporary operating difficulty at the transmitting station. Keep in mind that television picture quality is heavily dependent upon the lighting conditions of the actual scene. Where the "telecast" originates in the studio of the transmitting station, excellent results may be expected since lighting conditions can be closely controlled; however, where the "telecast" originates from locations outside of the studio, lighting conditions may occasionally be inadequate for highest quality picture reproduction.

Should you find that poor quality is noted when observing a "telecast" of a motion picture film, this may be due to the quality of the film—wait until the motion picture program is finished and observe whether picture quality improves when the next studio program begins. If there is more than one television station in the locality it is always desirable to tune in on another station and obtain a quick check on picture quality whenever some transmission fault is suspected.



Fig. 16 Multiple Images



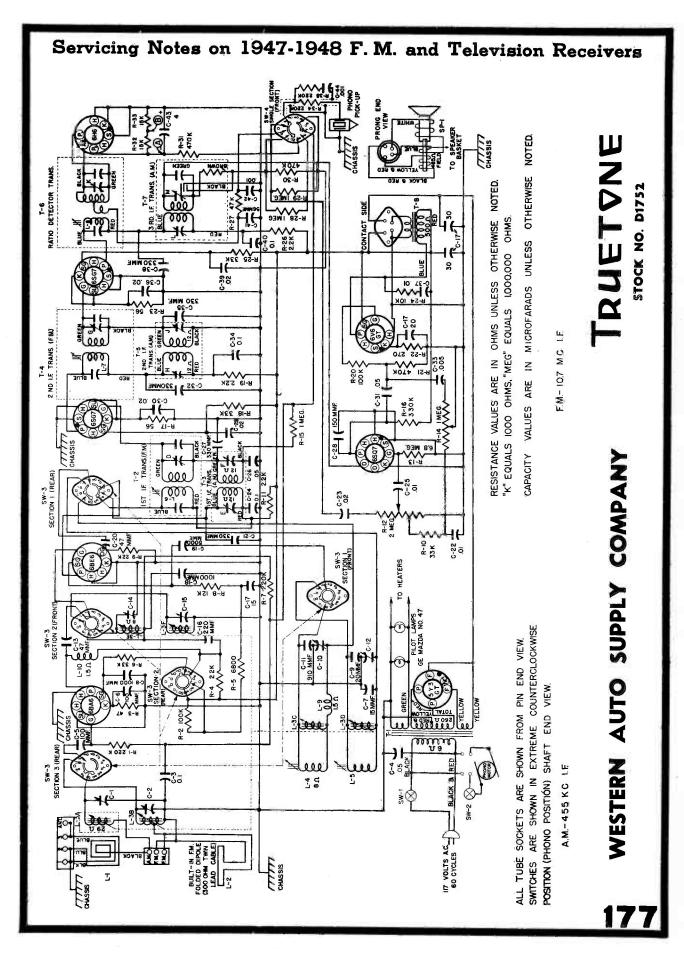
Fig. 17 Auto Ignition Interference



Fig. 18 Diathermy Interference



Fig. 19 Interference from Radio Transmitters



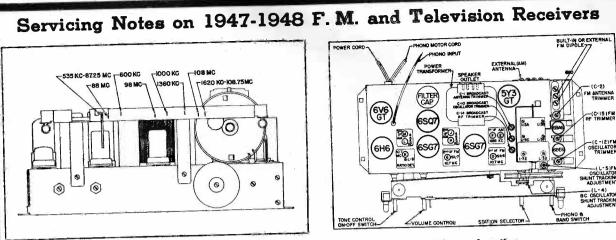
Servicing Notes on 1947-1948 F. M. and Television Receivers ALIGNMENT CHART

The following equipment is necessary to properly align this receiver:

- from 455 kc. to 1700 kc.
- 2. FM or CW signal generator covering the FM band from 87.25 mc. to 108.75 mc. and the 10.7 mc. frequency for FM IF alignment.
- Vacuum Tube Voltmeter (VTVM). 3.
- 4. Output meter-to match 4 ohms, 5 watts maximum.
- Insulated alignment screwdriver. 5.
- Dummy antenna-0.1 mfd. capacitor, 300 ohm 6. carbon resistor and inductive loop (fashioned from several turns of wire).
- 1. AM signal generator with frequency coverage NOTE: Oscilloscope equipment not required if aligned according to the following procedure:

The accuracy of the AM RF and AM antenna slug adjustments may be determined by noting the trimmer adjustment at each end of the band when the oscillator is set for proper coverage. The proper setting of the AM or FM oscillator slugs is indicated by proper tracking of the receiver at the center of the respective band. The FM RF and FM antenna slugs must be adjusted to dimensions given in the permeability tuner illustration.

Step No.	Band Switch Position	Signal Generator	Connection at Receiver	Dummy Anten na	Dial Setting	Adjust Tr imm er	Remarks	
1	AM	455 kc.	6BE6 Con- verter Grid Pin No. 7	0.1 mfd,	HF end	E, F, H, J, L, M, AM IF Trimmers	Adjust for Maximum Output.	
2	AM	535 kc.	6BA6 Grid Pin No. 1	0.1 mf d .	LF end	C-10 AM Osc. Trimmer	Adjust for Maximum Output.	
3	AM	1620 kc.	6BA6 Grid Pin No. 1	0.1 mfd.	HF end	L-4 AM Osc. Shunt Tracking Adjustment. (Remove Fly- wheel from Shaft of Tuning Control.)	Adjust for Band Coverage. (See Note 1.)	
4	AM	535 kc.	6BA6 Grid Pin No. 1	0.1 mfd.	LF end	C-14 AM RF Trimmer	Adjust for Maximum Output.	
5	AM	1400 kc.	Thru Loop (With Re- ceiver Loop Connected to Set.)	Inductive Loop	1400 kc.	C-1 AM Antenna Trimmer	Adjust for Maximum Output.	
6	FM	10.7 mc. (CW Sig- nal)	6SG7 Driver Grid Pin No. 4	0.1 mfd.	HF end	L-8 Ratio Detector Primary	Adjust for Maximum AVC between Point "A" on Wiring Diagram and Chassis using Electronic Voltme- ter. See Notes 2 and 3.	
7	FM	10.7 mc. (CW Sig- nal)	6SG7 Driver Grid Pin No. 4	0.1 mfd.	HF end	K Ratio Detector Secondary	See Note 2. Adjust for Zero Posi- tion (Using Electronic Voltmeter) from No. 12 Position on Single Sec- tion Switch and Point "B" on Wir- ing Diagram.	
8A	FM	10.7 mc. (CW Sig- nal)	6BE6 Con- verter Grid Pin No. 7	0.1 mfd.	HF end	L-6, D, L-7, G 1st and 2nd FM IF	See Note 2. Adjust for Maximum AVC.	
8B	FM	10.7 mc. (CW Sig- nal)	6BE6 Con- verter Grid Pin No. 7	0.1 mfd.	HF end	L-6, D, L-7, G 1st and 2nd FM IF	See Note 3. Adjust for Maximum Output.	
9	FM	87.25 mc. (FM Sig- nal)	6BA6 Grid Pin No. 1	0.1 mfd.	LF end	C-12 FM Osc. Trimmer	Adjust for Maximum Output.	
,10	FM	108.75 mc. (FM Sig- nal)	6BA6 Grid Pin No. 1	0.1 mfd.	HF end	L-5 FM Osc. Shunt Tracking Adjustment	Adjust for Band Coverage. (See Note 4.)	
11	FM	87.25 mc. (FM Sig- nal)	6BA6 Grid Pin No. 1	0.1 mfd.	LF end	C-15 FM RF Trimmer Adjust for Maximum Outpu		
12 7	FM	87.25 mc. (FM Sig- 'nal)	Thru 300 ohm Carbon Re- sistor to End FM Antenna Terminal and Center FM Antenna Terminal.	300 ohm Carbon Resistor	87.25 mc.	C-2 FM Antenna Trimmer	Adjust for Maximum Output.	



Calibration Points



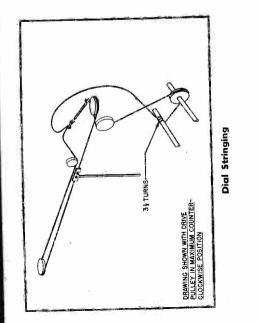
Reference Notes to Alignment Chart on Page 178.

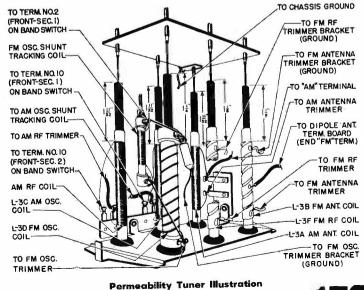
- Note 1—If 1620 kc. signal is received lower in frequency than the 1620 kc. dial calibration, turn BC oscillator shunt tracking adjustment (L-4) outward. Retrack at 535 kc. (Step 2). If higher than the 1620 kc. dial calibration, screw adjustment inward and retrack at 535 kc. Repeat until 535 kc. and 1620 kc. signals coincide with their respective dial calibrations.
- Note 2-Adjust input voltage to give approximately 5 volts AVC before final adjustment is made.

For STEPS 6 and 8A—Voltmeter "common" lead to chassis.

For STEP 7—Voltmeter "common" lead to point "B" on wiring diagram. The desired zero position is at the point where the meter indicates a polarity change from plus to minus or vice-versa.

- Note 3—For all tests requiring an FM signal, the generator output (22.5 kc. deviation, 400 cycles) must be adjusted to give approximately onehalf watt receiver output before final adjustments are made. Either STEP 8A or 8B may be used depending on equipment available.
- Note 4—If 108.75 mc. signal is received lower, in frequency than the 108.75 mc. dial calibration, turn FM oscillator shunt tracking adjustment (L-5) outward. Retrack at 87.25 mc. (STEP 9). If higher than the 108.75 mc. dial calibration, screw adjustment inward and retrack at 87.25 mc. Repeat until 87.25 mc. and 108.75 mc. signals coincide with their respective dial calibrations.





Western Auto Supply Company

STOCK NO. D1752

IRUETVNE

		- SOCKET	VOLTAGES -					and the second	and the product of the second
TUBE	POSITION	1	2	3	4	5	6	7	8
6BA6	RF Amplifier	0	0	6.3 AC	0	250	100	.6	
6BE6	Oscillator-Converter	0	0	6.3 AC	0	250	90	0	
6SG7	1st IF Amplifier	0	0	.6	0	.6	125	6.3 AC	250
6SG7	2nd IF Amplifier	0	0	.6	0	.6	125	6.3 AC	250
6SQ7	AM Detector—AVC— 1st Audio (AM-FM)	0	0	0	0	0	90	6.3 AC	0
6H6	FM Detector	0	6.3 AC	0	0	0	0	0	0
6V6GT	Power Output	NC	0	240	26 0	0	269	6.3 AC	14
5Y3GT	Rectifier	NC	325	NC	325 AC	NC	325	NC	325

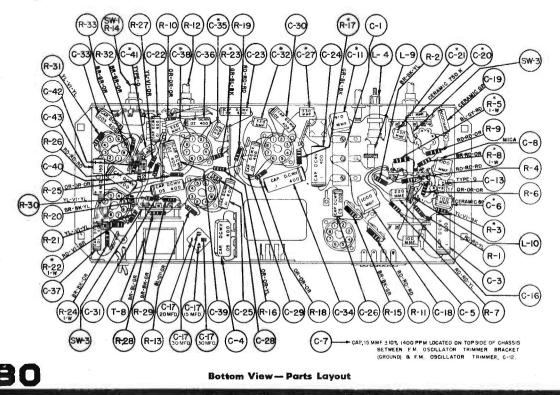
NOTE: All DC voltages measured with a 1000 ohm-per-volt meter from B— to socket contact indicated. All voltages are positive DC unless otherwise marked. Volume control full on. Zero signal input.

CHASSIS REMOVAL – Remove the receiver power cord from the electrical outlet before starting to remove chassis.

- 1. Turn the tuning control so that the dial pointer is in the extreme left-hand position (low frequency end).
- 2. Unhook the dial cable from dial pointer and slide the pointer to center of cutout in the pointer track. The dial pointer may be removed, if necessary, by turning it clockwise and clearing it through the cutout.

Tone control in clockwise position. Band switch in "AM" position. Line voltage 117 volts, 60 cycle AC.

- 3. Remove the loop and dipole antennae leads from their respective terminals.
- 4. Detach the phono-motor cord (plug and socket connection).
- 5. Remove the phono input leads at the terminal board on the chassis shelf and remove the speaker plug from receptacle at back of chassis.
- 6. Remove knobs and the four chassis mounting screws. The chassis can now be removed from the cabinet.



Servicing Notes on 1947-1948 F. M. and Television Receivers Jruetone Model D1846

ALIGNMENT PROCEDURES

AM STAGES

Volume Control Maximum all Adjustments,

Connect Radio Chassis to Ground Post of Signal Generator with a Short Heavy Lead.

The following is required for aligning:

An All Wave Signal Generator Which Will Provide an Accurately Calibrated Signal at the Test Frequencies as Listed.

Allow Chassis and Minutes.	Signal Generator to "Heat U	o" for Several		g Meter, Non-Metallic mf, and 50 mmf.	Screwdriver, Dummy An
FREQUENCY SETTING	SIGNAL GENERATOR CONNECTION AT RADIO	GROUND CONNECTION	DUMMY	GANG CONDENSER SETTING	ADJUST TUNING SLUGS (I-F ONLY) TRIMMERS (OSC. & ANT.)
455 KC	Control Grid 1st 6BA6 Pin No. 1	Chassis Base	.1 mf	Turn Rotor to Full Open	2nd J.F. Pri. & Sec,
455 KC	Control Grid 6BE6 Pin No. 7 1st Det.	Same as above	,ĭmf	Turn Rotor to Full Open	ist I.F. Pri. & Sec.
1620 KC	Control Grid 6BE6 Pin No. 7	Same as above	.1 mf	Turn Rotor to Full Open	Oscillator C-39
1400 KC	External Antenna Lead	Same as above	50 mmf	Turn Dial to 1400 KC. See Note A	Antenna C-35

NOTE A-Set pointer at the 1400 KC mark on the dial scale. Attach pointer to drive cord.

FM STAGES

Allow chassis and signal generator to warm up for several minutes. The following equipment is required for aligning:

An accurately calibrated signal generator providing unmodulated signals at the test frequencies listed below.

Non-metallic screwdriver.

Dummy Antennas and 1-F Loading Resistor-01 mf, 300 ohms and 100 K ohms.

Zero center scale DC vaccum tube voltmeter having a range of approximately 3 volts.

(If a zero center scale meter is not available, a standard scale vacuum tube voltmeter may be used by reversing the meter connections for negative readings.)

	SIGN	AL GENERATOR			BAND		ADJUSTMENT
Discriminator	FREQUENCY	CONNECTION AT RADIO	DUN ANTE		SWITCH	CONDENSER SETTING	FOR MAX. METI DEFLECTION
	10.7 MC	6BA6 2nd I-F Pin 1 & Chassis	.01 mi		FM	Rotor to Full Open	Disc. Pri. Note A
	10.7 MC	Same as above	.01 mf		FM	Same as above	Disc. Sec. Note B
	10.7 MC	Same as above	.01 mf		FM	Same as above	Disc. Pri.
	10.7 MC	Same as above	.01 mf		FM	Same as above	Disc. Sec. Note B
I⊧F	10.7 MC	6BA6 1st IF Pin 1 & Chassis	.01 mf		FM	Same as above	2nd I-F Pri. 2nd I-F Sec. Note C
	10.7 MC	Unsolder lead from Pin 7 to band switch. Insert 100K ohm resistor between Pin 7 & Ground and feed sig- nal into Pin 7 of 68E6	.01 mf		FM	Same as above	îst I-F Pri₂ Note C
	10.7 MC	Same as above	.01 mf		FM	Same as above	1st I-F Sec. Note C
		RECHECK I-F AL	DJUSTMEN	S IN ORD	ER GIVEN		
Ant. & Osc.	108.4 Note D	Disconnect dipole and con- nect generator to dipole terminals with resistor in series.	300 ohr	15	FM	Rotor to Full Open	Osc. C-38
	104.5	Same as obové	300 ohn	15	FM	Tune rotor for max. AVC voltage	Ant, C-37

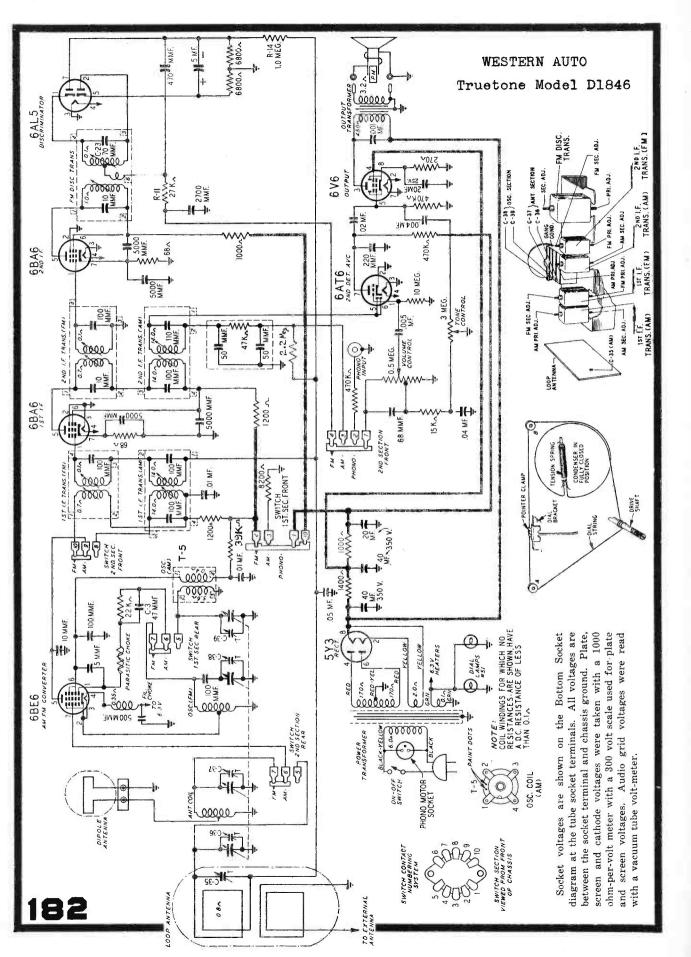
FM ALIGNMENT NOTES

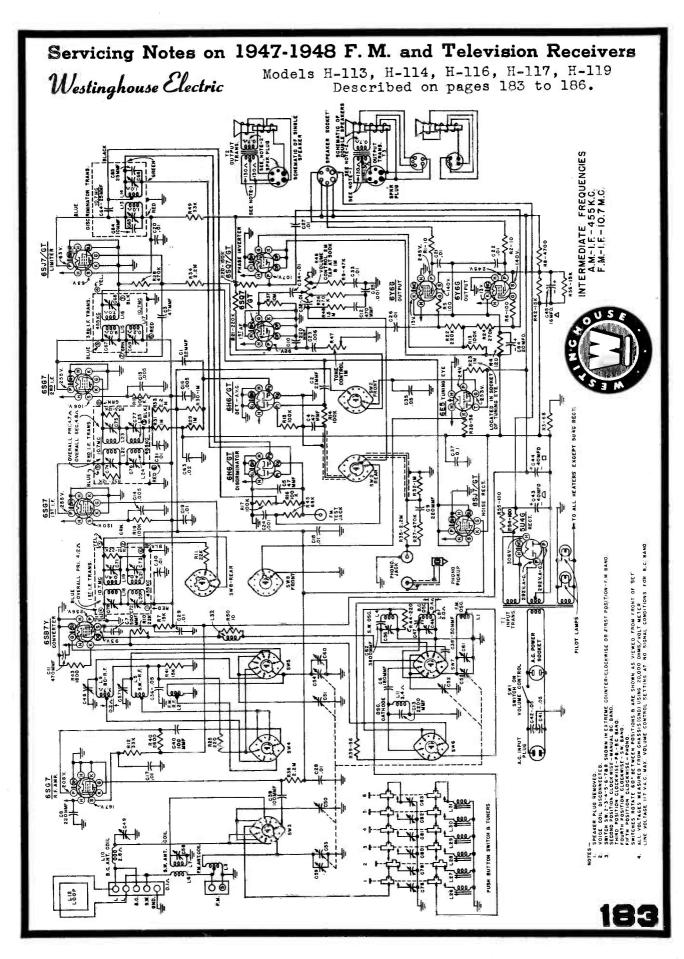
NOTE A-The zero center scale DC vacuum tube voltmeter is to be connected between chassis ground and the A.V.C. line at the 27 K. ohm resistor (R-11) and its junction with terminal strip. A signal of .1 volt must be fed into the receiver for this adjustment. Note output voltage on the zero center DC vacuum

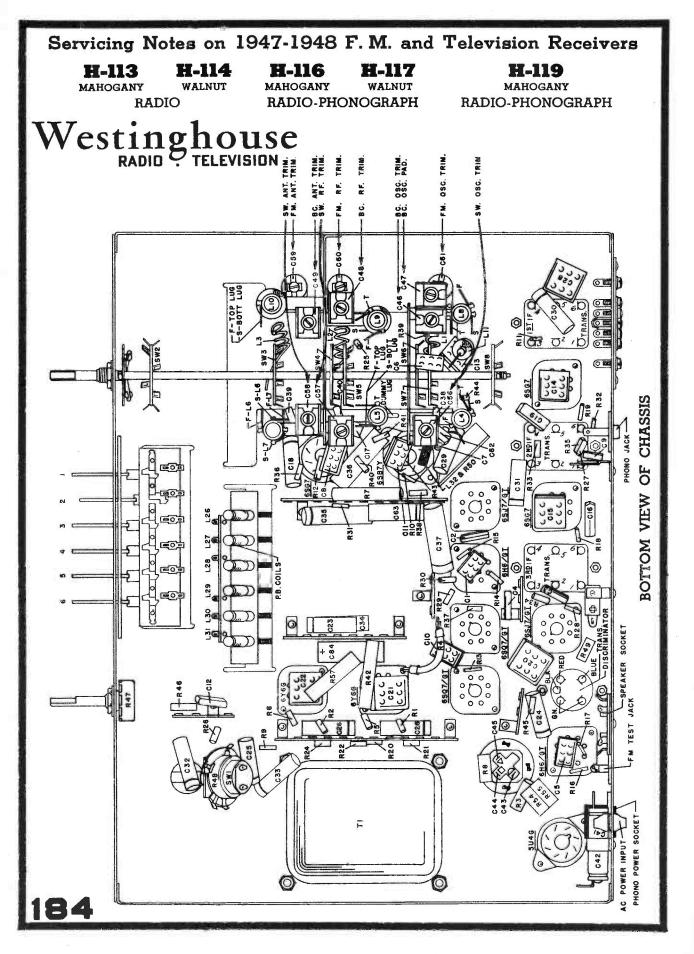
tube voltmeter.

NOTE B-Disconnect zero center DC vacuum tube voltmeter from A.V.C. and connect it to the audio takeoff point at the 1 megohim resistor (R-14) and its junction with the terminal strip. Adjust for zero voltage indication.

- NOTE C-Cannect zero center DC vacuum tube voltmeter as in Note A. Adjust input to give same output on the zero center DC vacuum tube voltmeter as in Note A.
- NOTE D-Remove the 100 K ohm load resistor and solder the lead from pin 7 of 6BE6 tube to the band switch before attempting to check the antenna and oscillator coil adjustments.







Westinghouse RADIO TELEVISION

FREQUENCY RANGES:

Standard Broadcast	to	1700 kc.
International Short Wave	to	18.0 mc.
Frequency Modulation	to to	108 mc.
Ilequency modulation		

ALIGNMENT

POWER OUTPUT:

Undistorted														•	٠	٠	•	•	•	•	•	ź	•	•	. 14	watt	3
Maximum	1.	. 5	2	:	12	2	ż	,	6		•		•		•	•	•	•	÷	•	í4		•	•	.25	watt	5

...

POWER SUPPLY RATING: 105-120 volts, 50-60 cycles A-C POWER CONSUMPTION (radio sect. only);175 watts

BROADCAST AND SHORT WAVE BANDS AMPLITUDE MODULATION

Connect an output meter across the speaker voice coil.

.

With the volume control set for maximum output and the signal from the generator attenuated to avoid A.V.C. action, proceed as follows:

Step	Connect Signal Generator to	Signal Generator Frequency	Radio Dial Setting	Adjust
1	Set Phono-Band switch to "	BC"		
2	6SG7, 2nd I-F, control grid through a 0.1 mfd capac- itor	455 kc	550 kc	455 kc secondary and primary trimmers of 3rd I-F transformer for maximum output.
3	6SG7, 1st I-F, control grid through a 0.1 mfd. capac- itor	455 kc	550 kc	455 kc secondary and primary trimmers of 2nd I-F transformer for maximum output.
4	6SB7Y, converter, control grid through a 0.1 mfd ca- pacitor	455 kc	550 kc	455 kc secondary and primary trimmers of 1st I-F transformer for maximum output.
5	6SB7Y, converter, control grid through a 0.1 mfd ca- pacitor	455 kc	550 kc	carefully "peak" all 455 kc I-F trans- former trimmers for maximum output.
6	BC antenna terminal through a 200 mmf capac- itor	`600 kc	600 kc	BC oscillator padder for maximum output
2	BC antenna terminal through a 200 mmf capac- itor	1600 kc	1600 kc	BC oscillator trimmer for maximum output
8	Re-check steps 6 and 7			
9	Radiated signal (no con- nection)	1400 kc	1400 kc	BC R-F and ANT trimmers for maximum output.
10	Set Phono-Band switch to "	S.W."		
11	SW antenna terminal through a 400 ohm resistor	18.0 mc	18.0 mc	SW oscillator trimmer for maximum out put. NOTE: If the signal is heard at two dif ferent trimmer settings, the one neares minimum capacity is correct—the other is the image.
12	Radiated signal (no con- nection)	16.0 mc	16.0 mc	SW R-F and ANT trimmers for maximum output.

CHASSIS LAYOUT C82 C83 NC NO.44 PILOT LAM -053 - 650 - 054 -051 6SE C52 - 055 RD, 2 HD IST LE 6567 6SJ7 TRAN 5040 RANS 0 DISCRIMINATOR

455 K C

10.716

TEST JACKS

AC. PHONO.

O LINE CORO

155 KG

0.7140

58

0"0

000000

455 KG

10.7 MC



H-116 MAHOGANY

H-117 WALNUT

18

Westinghouse Electric

MODELS H-113, H-114, H-116, H-117 AND H-119

F. M. BAND

FREQUENCY MODULATION

Connect a 20,000 ohms-per-volt or Vacuum Tube Voltmeter between the Discriminator Test Jack and the chassis.

With the volume control set for maximum output and the signal from the generator attenuated to avoid A.V.C. action, proceed as follows:

Step	Connect Signal Generator to—	Signal Generator Frequency	Radio Dial Setting	Adjust
1	Set Phono-Band switch to "			
2	Detune secondary trimmer o	f discriminator trans	sformer.	
3	6SG7, 2nd I-F, control grid through a .01 mfd mica capacitor	UNMODULATED 10.7 mc	88 mc	10.7 mc primary trimmer of 3rd I-F trans for maximum voltage.
4	6SG7, 1st I-F, control grid through a .01 mfd mica ca- pacitor	UNMODULATED 10.7 mc	88 mc	10.7 mc secondary and primary trimmer of 2nd I-F trans. for maximum voltage.
5	Fixed plates of the FM converter tuning capacitor through a .01 mfd mica ca- pacitor	UNMODULATED 10.7 mc	88 mc	10.7 mc secondary and primary trimmer of 1st I-F transformer for maximum volt age.
6	Fixed plates of the FM converter tuning capacitor through a .01 mfd mica capacitor	UNMODULATED 10.7 mc	88 mc	carefully "peak" all 10.7 mc I-F trimmer for maximum voltage.
7	FM antenna terminal through a non-inductive 300 ohm resistor	UNMODULATED 105 mc	105 mc	FM oscillator trimmer for maximum voltage.
8	FM antenna terminal through a non-inductive 300 ohm resistor	UNMODULATED 105 mc	105 mc	FM R-F and ANT trimmers for maximum voltage.
9	Fixed plates of the FM converter tuning capacitor through a .01 mfd mica ca- pacitor	UNMODULATED 10.7 mc	88 mc	Primary trimmer of discriminator trans former for maximum voltage.
10	Fixed plates of the FM converter tuning capacitor through a .01 mfd mica ca- pacitor	UNMODULATED 10.7 mc	88 mc	Secondary trimmer of discriminator trans former for zero voltage. The voltage wil change polarity as the trimmer is tuned through resonance. Tune carefully fo zero voltage.

PUSH BUTTONS

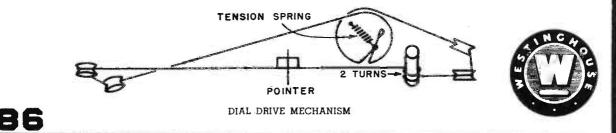
Push buttons 1 to 3 are designed to receive stations from 900 to 1600 kc; push buttons 4 to 6 are designed to receive stations from 540 to 900 kc.

Refer to CHASSIS LAYOUT drawing for location of push button adjusters, and then proceed as follows:

- 1. Turn on radio and allow it to warm up for five minutes.
- 2. Set the Phono-Band switch on "BC," and tune in the desired station in the frequency range 900 to 1600 kc.
- 3. Re-set the Phono-Band switch on "P.B.", and depress the first push button (right button viewed from the front).
- 4. Adjust C78 for maximum receiver output (either a station or static will be heard depending on the setting of L26). Now adjust L26 until the desired station is heard. It will be necessary to re-adjust C78 at intervals to maintain maximum output.
- 5. Make a final adjustment of L26 for proper tuning and C78 for maximum output.

 Return the band switch to "B.C." to make certain that the push button has been set to the desired station.

7. Adjust the remaining push buttons in the same manner.



Westinghouse RADIO TELEVISION

H-161

H-168 and H-168A MAHOGANY AND BLONDE

MAHOGANY AND BLONDE

ALIGNMENT

BROADCAST BAND AMPLITUDE MODULATION

Connect an output meter across the speaker voice coil.

While making the following adjustments, keep the volume control set for maximum output, the tone control set on treble, and the signal generator output attenuated to avoid AVC action.

Step	Connect Signal Generator to—	Signal Gen. Freq.	Radio Dial	Adjust for Maximum Output
1.	Set Phono-Band Switch to "AM"			
2.	6BA6, 2nd I-F, control grid through a 0.1 mfd capacitor	455 kc	540 kc	455 kc primary trimmer of 3rd I-F transformer
3.	6BA6, 1st I-F, control grid through a 0.1 mfd capacitor	455 kc	540 kc	455 kc primary and secondary trimmers of 2nd I-F trans.
4,	6J6, converter, control grid through a 0.1 mfd capacitor	455 kc	540 kc	455 kc primary and secondary trimmers of 1s I-F trans.
5	6]6, converter, control grid through a 0.1 mfd capacitor	455 kc	540 kc	Peak all 455 kc I-F transformer trimmers.
6.	Radiated signal (no actual connection)	1600 kc	1600 kc	AM oscillator trimmer.
7	Radiated signal	600 kc	600 kc	AM antenna padder.
1.		1400 kc	1400 kc	AM antenna trimmer.
8.	Radiated signal	"D1" +11		r while adjusting AM antenna trimmer
9.	Recheck steps 7 and 8 in order of	given. nock tu	ining capacito	I wine adjusting the second second

FM BAND-FREQUENCY MODULATION

Do not align the 10.7 mc I-F circuits until all 455 kc I-F adjustments have been completed.

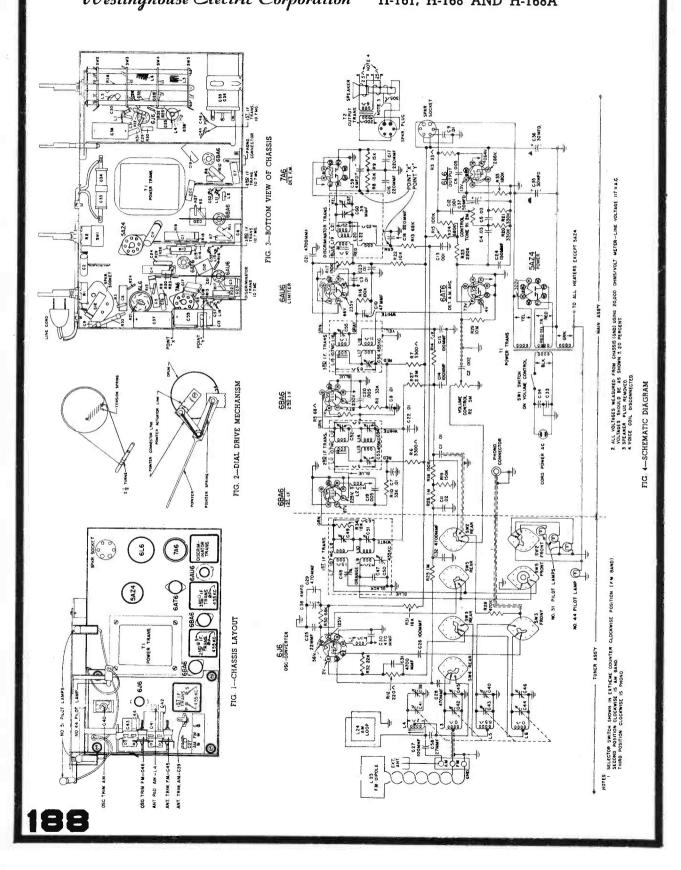
Connect Signal Generator to—	Signal Gen. Freq.	Radio Dial	Adjust—
Set Phono-Band switch to "FM."	p		
Connect a vacuum tube voltmete	r between point X	(see Figs. 3	and 4) and ground (chassis).
6BA6, 2nd I-F, control grid through a .001 mfd mica	Unmodulated 10.7 mc	88 mc	trans. and primary of discriminator trans. for max, voltage.
6BA6, 1st 1-F, control grid through a .001 mfd mica	Unmodulated 10.7 mc	88 mc	10.7 mc primary and secondary of 2nd 1-1 trans. for max. voltage,
Stator of FM tuning capacitor (C42) through a .01 mfd mica	Unmodulated 10.7 mc	88 mc	10.7 mc primary and secondary of 1st I- trans. for max. voltage.
Connect the vacuum tube voltme	ter between point	Y (Figs. 3 c	and 4) and chassis.
Stator of FM tuning capacitor (C42) through a .01 mfd mica capacitor	Unmodulated 10.7 mc	88 mc	Secondary of discriminator trans. for zer voltage. The voltage will change polarity a the trimmer is tuned through resonance. Tun carefully for zero voltage.
Connect the vacuum tube voltme	eter between point	X and chas	ssis.
Stator of FM tuning capacitor (C42) through a .01 mfd mica	Unmodulated 10.7 mc	88 mc	age.
FM antenna terminal through a 72 ohm non-inductive re-	Unmodulated 105 mc	105 mc	FM oscillator trimmer for max. voltage.*
FM antenna terminal through a 72 ohm non-inductive re-	Unmodulated 105 mc	105 mc	FM antenna trimmer for max, voltage *- "rock" tuning capacitor while adjusting.
	Generator to- Set Phono-Band switch to "FM." Connect a vacuum tube voltmete 6BA6, 2nd I-F, control grid through a .001 mfd mica capacitor 6BA6, 1st I-F, control grid through a' .001 mfd mica capacitor Stator of FM tuning capacitor (C42) through a .01 mfd mica capacitor Connect the vacuum tube voltme Stator of FM tuning capacitor (C42) through a .01 mfd mica capacitor Connect the vacuum tube voltme Stator of FM tuning capacitor (C42) through a .01 mfd mica capacitor Connect the vacuum tube voltme Stator of FM tuning capacitor (C42) through a .01 mfd mica capacitor FM antenna terminal through a 72 ohm non-inductive re- sistor FM antenna terminal through	Generator io—Gen. Freq.Generator io—Gen. Freq.Set Phono-Band switch to "FM."Connect a vacuum tube voltmeter between point X6BA6, 2nd I-F, control grid through a .001 mfd micaUnmodulated 10.7 mc6BA6, 1st I-F, control grid through a .001 mfd micaUnmodulated 10.7 mcCapacitorUnmodulated 10.7 mcCapacitorUnmodulated 10.7 mcConnect the vacuum tube voltmeter between pointStator of FM tuning capacitor (C42) through a .01 mfd mica capacitorUnmodulated 10.7 mcConnect the vacuum tube voltmeter between pointStator of FM tuning capacitor (C42) through a .01 mfd mica capacitorUnmodulated 10.7 mcConnect the vacuum tube voltmeter between pointStator of FM tuning capacitor (C42) through a .01 mfd mica capacitorUnmodulated 10.7 mcConnect the vacuum tube voltmeter between pointStator of FM tuning capacitor (C42) through a .01 mfd mica capacitorUnmodulated 10.7 mcConnect the vacuum tube voltmeter between pointStator of FM tuning capacitor (C42) through a .01 mfd mica capacitorUnmodulated 10.7 mcFM antenna terminal through a 72 ohm non-inductive re- sistorUnmodulated 105 mcFM antenna terminal through 	Connect SignalDignalGenerator ioGen. Freq.DialSet Phono-Band switch to "FM."Connect a vacuum tube voltmeter between point X (see Figs. 36BA6, 2nd I-F, control gridUnmodulated88 mcthrough a .001 mfd mica10.7 mccapacitor6BA6, 1st I-F, control gridUnmodulated88 mcthrough a' .001 mfd mica10.7 mccapacitorUnmodulated88 mc(C42) through a .01 mfd mica10.7 mc88 mc(C42) through a .01 mfd mica10.7 mc10.5 mcFM antenna terminal throughUnmodulated105 mcsistorFM antenna terminal throughUnmodulated105 mcFM antenna terminal throughUnmodulated105 mc

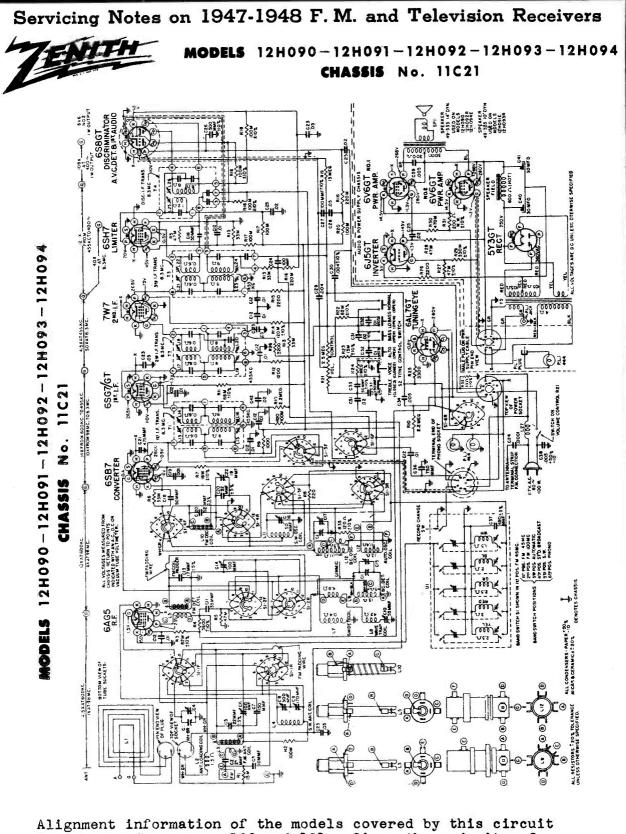
* The FM oscillator and antenna trimmers can be adjusted by using the thumb and forefinger to rotate the outside drum of the capacitor. Hand capacity effects may be reduced by holding the heel of the hand against the 1st I-F trans. can.

** After the radio has been aligned at 105 mc., check calibration by tuning to a 90 mc. signal from the generator. If the dial pointer indicates 90 mc., no further adjustments are necessary. If the pointer is on the high frequency side of 90 mc., slightly compress the length of oscillator coil (L6) and repeat steps 10, 11, and 12 above until dial calibration is correct. If the pointer is on the low frequency side of 90 mc., slightly expand the length of oscillator coil (L6) and repeat steps 10, 11, and 12 above until dial calibration is correct.

After calibration has been checked and the antenna circuit has been "peaked" at 105 mc., check the antenna circuit tracking by tuning to a 90 mc. signal and rotating the FM antenna trimmer. If the "peak" setting is the same at 90 mc. as it was at 105 mc., no further adjustments are necessary. If the trimmer capacitance must be increased to obtain maximum output at 90 mc., slightly compress the length of antenna coil (L3) and repeat steps 11 and 12 until correct tracking is obtained. If the trimmer capacitance must be decreased to obtain maximum output at 90 mc., slightly expand the length of antenna coil (L3) and repeat steps 11 and 12 until correct tracking is obtained.

Servicing Notes on 1947-1948 F. M. and Television Receivers Westinghouse Electric Corporation H-161, H-168 AND H-168A





Arignment information of the models covered by this circuit is presented on pages 190 and 191. Since the majority of Zenith post-war F.M. receivers use similar R.F. and I.F. sections, the same alignment information will apply to many other models.

189

ZENITH RADIO CORPORATION

12H090-12H091-12H092-12H093-12H094 No. 11C21 **CHASSIS** MODELS

3-GANG VARIABLE 25 MMFD, CER, 500 V 10 MMFD, CER, 500 V BROADCAST ANT, TRIM

22-1504 1 22-1507

DESCRIPTION

DIAG PART

ZZMMFD CER. 500 V FM ANTENNA TRIM.

22-M9X S.W. ANT. TR

22-1503 150 MMFD

The llC21 chassis incorporates a superheterodyne circuit two stages of IF, and one stags of RF amplification on all hands. with

the coil forms. The slugs are slotted for a small size fiber screw driver. Do not press hard on the aligning tool (fiber The alignment of this chassis on the short The alignment slugs in the IF transformers are threaded and screw into or the threads in the coil forms will strip and wave and standard broadcast band is conventional. adjustment will be impossible. AM Alignment: screw driver)

and padding wires in series with the 100 MC coils. The tuning FM RF Alignment: The same coil slug arrangement which tunes the 100 MC FM band also tunes the $45~{\rm MC}$ band. However, on in parallel slugs are attached to threaded shafts and the slugs are varied counter-clockwise. After adjustments the shafts must be securin the field of the coils by turning the shafts clockwise or 45 MC the band switch connects trimmer condensers ed with a drop of speaker cement.

ed with an unmodulated signal, the stage must be loaded. A 300 Observe FM IF Alignment: The same type of tuning slugs for align-The second 8.3 Overcoupling gives a wide band pass with good sensitivity. When an overcoupled stage is alignohm carbon resistor soldered across the secondary of the second transformer provides a satisfactory load for this circuit. The resistor leads must be kept short to reduce the distributing the AM IF Amplifier are used for the FM I.F.'s. same precautions when making adjustments. IF stage is overcoupled. ed capacity of the circuit. the Ŵ h

When allgning a loaded stage, it will be found that considerable signal from the generator will be required, and that it will tune broadly. THE LOAD RESISTOR MUST BE REMOVED AFTER ALIGNMENT.

If the signal generator used does not have sufficient outto overcome the temporary loss caused by the load resistor, the load resistance may be increased or the signal fed into the preceding stage. put

of the discriminator is aligned (operation 9) use sufficient signal before A center zero indicating meter is recommended for this adjustment, but is not absolutely observing closely when this meter starts to go to the left Reversing the leads of a non-zero center meter, or input to get a good positive and negative indication FM Discriminator Alignment: When the secondary negative) of zero will give the same results. setting the slug for zero reading. necessary.

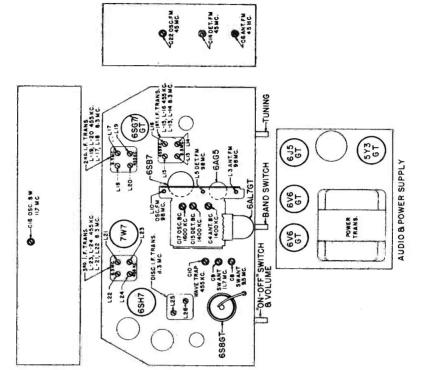
470 М ОНЫ 14W

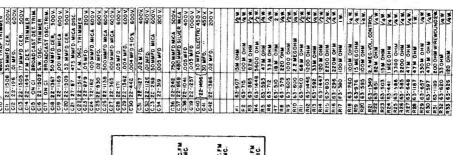
AW.

TRIMMER LOCATION

AND

UBE





400V 400V 600V

1947-1948 F. M. and Television Receivers Servicing Notes on

12 W

Zenith Radio Chassis No. 11C21, Models 12H090 to 12H094

For improving F.M. reception from console receivers, a cabinet F.M. antenna may be added in addition to the line This new antenna is made up of two 28 inch antenna. One wire is connected to the F.M. anlengths of wire. tenna post, the other to chassis. These two wires then are tacked in the cabinet in opposite directions, and should not come in contact with ground.

Current Construction Automate Autom			-	Tamt of mail		Cat Dial		
1 Tube 66 1 Tube 66 2 2 4 2 5 5 6 2 7 2 7 2 8 3 7 2 8 3 9 1 7 2 7 2 8 3 9 1 10 1 11 4 11 4 11 4 11 4 11 4 11 4 11 4 11 4 11 4 11 4 11 4 11 4 11 4 11 4 11 4 12 6 13 4 14 6 14 6 15 6 14 6 15 6 14 7 15 6 14 7 15 6 16 1 17	opera-	Connect Oscillator to	Antenna		Band	To To	Ad. Trimere	Purpose
1 Tube 65 2 7 tube 65 3 2 4 2 5 Autenna 5 Autenna 6 Autenna 6 Autenna 6 Autenna 7 Autenna 6 Autenna 7 Autenna 6 Autenna 7 Autenna 7 Pin 4 1 (c) 11 (c) 7 Pin 4 11 (c) 12 (c) 13 (c) 14 (c) 15 (c) 14 (c) 15 Mutenna 15 Mutenna 15 Mutenna 15 Mutenna 16 Mutenna 17 Autenna 18 Nore 19 10	2 + Mit	Pin 8 on Converter					L15,16,19,20,23	Align I.F. channel for
2 Fin 1 2 2 turnio 4 2 turnio 5 5 6 Antenno 6 Antenno 6 Antenno 6 Antenno 6 Antenno 6 Antenno 7 Antenno 6 Antenno 7 Antenno 7 Antenno 7 Pin 4 7 Pin 4 11 (c) 7 Pin 4 11 (c) 12 6 13 6 14 (c) 14 (c) 15 Covert 14 Antenno 15 Moven 16 Moven 15 Moven 15 Moven 16 Moven 17 Poven	-	Tube 6SB7 Bocket	.05 Mfd.	Modulated	_	600 Kc.	and 24	maximum output
2 6465 e. 3 2 4 2 5 5 6 4 6 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 8 8 9 11mite 11 11 11 11 12 6 12 6 13 11 14 8 13 9 14 10 13 10 14 10 15 9 14 10 15 10 14 10 15 10 14 10 15 10 14 10 15 10 14 10 15 10 10 10 10 10 10 10 11 10 12 10 13 10 <t< td=""><th>1</th><td>Pin 1 on R.F. tube</td><td></td><td>455 Kc.</td><td></td><td>Press any but-</td><td></td><td>Adjust wavetrap to</td></t<>	1	Pin 1 on R.F. tube		455 Kc.		Press any but-		Adjust wavetrap to
3 2 7 4 2 couplet 5 Antenna 5 Antenna 6 Antenna 6 Antenna 6 Antenna 7 Pin 4 7 Pin 4 9 1 1 9 7 7 7 8 8 6 14 6 14 6 14 6 14 6 14 6 15 6 16 6 17 7 16 1 17 <	¢,	6AG5 Bocket	.05 Mfd.			ton on Auto.	C10	minimum
3 couple 4 couple 5 Antenn 5 Antenn 6 Antenn 6 Antenn 6 Antenn 7 Antenn 6 Antenn 7 Antenn 7 Antenn 7 Antenn 7 Antenn 7 Antenn 1 4 1 1 1 4 1 Antenn 13 6 14 6 15 6 14 6 15 Antenn 15 6 14 6 15 6 15 Antenn 15 6 15 0 15 0 15 0 15 0		2 Turns loosely		1600 Kc.	_			Set oscillator to dial
k2 turn k Antenni 5 Antenni 6 Antenni 6 Antenni 6 Antenni 7 $11m 4$ 7 $11m 4$ $7 m 2n$ $11m 4$ $11 (c)$ $6000 c$ $12 (c)$ $8000 c$ $12 (c)$ $800 c$ $12 (c$	N'S	coupled to wavemag.		Modulated		1600 Kc.	C17	<u>šcale</u>
4 couple 5 Anternul 5 Anternul 6 Anternul 6 Anternul 7 Pln 4 9 11mite 11 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 8 8000000000000000000000000000000000000		2 turns loosely		1400 Xc.				
5 Antenna 5 move 1 6 move 1 7 move 1 7 move 1 7 move 1 7 move 1 9 9 11 (e) 11 (e) 11 (e) 11 (e) 11 (e) 11 (e) 12 (e) 13 (e) 14 (e) 15 (e) 14 (e) 15 (e) 14 (e) 15 (e) 15 (e) 15 (e) 15 (e)		coupled to wavemag.		Modulated		1400 Kc.	C15 & C4	Align det. and ant. stages.
5 move 1 6 move 1 6 move 1 7 11 11 (c) 11 (c) 11 (c) 12 60 12 60 14 (c) 14 (c) 14 (c) 14 (c) 14 (c) 15 move 1 15 move 1 15 move 1 15 move 1		Antenna Post (Re-	00	11.7 Mc.	_	-		Set oscillator to dial
6 Antennation 7 move 1 7 move 1 8 11mite 9 11mite 9 11mite 9 11mite 11 11mite 11 11mite 11 11 11 11 12 60 12 60 12 60 13 60 14 10 15 0 14 0 15 0 14 10 15 10 14 10 15 0 14 10 15 10 15 10 15 10 15 10 15 10	5	move line ant.)	ohms	Modulated		11.7 Mc.	C16	60 81 6
6 move 1 7 7 9 1 <th></th> <td>Antenna Post (Re-</td> <td>004</td> <td>11.7 Mc.</td> <td></td> <td></td> <td>1</td> <td></td>		Antenna Post (Re-	004	11.7 Mc.			1	
7Antenn7 $Pin 4$ 911m149911m149911m141067W7 2m11(c)65G7 112(c)65G7 113(c)80000114(c)80000115(c)move 115(c)move 115(c)move 115(c)move 115(c)move 115(c)move 115(c)move 115(c)move 115(c)move 115(c)90.8815(c)90.88	10	move line ant.)	ohme	Modulated	MS	11.7 Ma.	69	Align ant. stage
7 mare 1 8 (a) 11mlte 4 7 7 7 7 9 (b) 11mlte 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 11 (c) 8 9 9 9 12 (c) 11 8 6 11 11 13 (c) 11 8 9 8 1		Antenna Post (Re-	001	9.7 Mc.	it			Align ant. stage Repeat
Pin 4 8 (a) Pin 4 9 (b) Pin 4 7 10 (c) Pin 6 7 7 W7 2n Pin 6 1 (c) 800 ket 1 (c) Mntenn 1 (c) Mntenn 1 (c) Mntenn 1 (c) 90 ket 1 (c) 90 ket 1 (c) 90 ket	[move line ant.)	ohme	Modulated	MO	9.7 Mc.	C8	Oper. 6 for maximum output
8 (a) 11mite 9 (b) 11mite 9 (c) 1 mite 7 7 2n 7 m 7 2n 7 7 2n 7 m 7 2n 11 (c) 6 SG7 1 12 (c) 8 socket 13 (c) 8 socket 14 (c) Antenn 15 (c) more 1		Pin 4 arid on 6SE/		8.3 Mc.	W		I25 coil slug	Allen primary of disorimin-
9 (b) Pin 4 7 Pin 6 Pin 6 Pin 6 Pin 6 Pin 8(11 (c) 6567 1 12 (c) 6567 1 13 (c) 900000 14 (c) Antenn 15 (c) Motenn 15 (c) Motenn 15 (c) Motenn 10 (c) 14 (c) 11 (c) 14 (c) 12 (c) Motenn 12 (c) Motenn 12 (c) Motenn 13 (c) Motenn 14 (c) Motenn 10 move 1	8 (a)	limiter socket	.05 Mfd.	Unmodulated	45		primery disc.	ator for maximum reading
9 (b) 11mite 7w7 2m 7w7 2m 7w7 2m 11 (c) socket 12 (c) socket 12 (c) Pin 8(12 (c) Pin 8(13 (c) Pin 8(14 (c) Antenn 15 (c) move 1 15 (c) bo sa		Pin 4 artia on 6887		8.3 Mc.	M		126 coil slug sec.	Adjust secondary of discr.
10 (e) Pin 4 Pin 4 Pin 4 Pin 4 (s) 800 ket 11 (c) 6567 1 12 (c) 800 ket 1 13 (c) 800 ket 1 14 (c) Antenn 1 15 (c) Moren 1 15 (c) More 1	(4) 0	limiter socket	. 05 Mfd.	Unmodulated	45		of disor.	for zero reading
10 (c) 7W7 2m 11 (c) 90cket 11 (c) 90cket 12 (c) 90cket 13 (c) Antenn 14 (c) Antenn 15 (c) Antenn 15 (c) Antenn 15 (c) Mutenn 15 (c) Antenn 15 (c) Antenn 16 (c) Antenn 19 Berve Berve		Pin 6 (artic) an					L21 & L22 prim. &	
10 (c) 80cket 11 (c) 80cket 12 (c) 80cket 13 (c) 80cket 14 (c) Antenn 15 (c) Move 15 (c) Move 14 (c) Antenn 15 (c) Move 15 (c) Move 15 (c) Move 15 (c) Berve 15 (c) Berve		TWT 2nd Th tube		8.3 Mc.	FM			Align 3rd Dr transformer
11 (c) Fin 4 12 (c) 65G7 1 12 (c) 55G7 1 13 (c) 500/er 6 14 (c) Antenn 15 (c) Matenn 16 (c) Matenn 16 0 Matenn 19 0 Berve	10 (e)	anokat	.05 Mfd .	Unmodulated	45		transformer	for maximum reading
11 (c) 657 1 (1) 800 ket 12 (c) 800 ket (1) 800 ket 13 (c) Antenn 14 (c) Antenn 15 (c) Antenn 15 (c) Move 1 16 (c) Antenn 17 (c) Antenn 18 (c) Antenn 19 (c) Antenn 10 (c) Antenn 11 (c) Move 1 12 (c) Antenn 14 (c) Antenn 15 (c) Move 1 16 (c) Berve							L17 & L18 prim. &	
(1) 90.05.484 (2) 12.00 80.05.484 (3) 80.05.464 80.05.64 (3) 80.05.61 14.00 15 (0) Morenn 15 (1) move 15 (2) Mutenn 16 (2) 90.98 15 90.88		6SG7 let IF tube		8.3 Mc.	M		Bec. of 2nd Dr	Align 2nd IF transformer
12 (c) Fin 8(13 (c) socket 14 (c) Antenn 15 (c) Antenn 15 (c) Antenn 15 (c) Mutenn 15 (c) Antenn 16 (c) Antenn 16 (c) Berve		Bocket	.05 Mfd.	Unmodulated	45		transformer	for maximum reading
12 (c) conver (d) socket Antenn Antenn 15 (c) move 1 Antenn Antenn 15 (c) move 1 aerve be sa		Pin 8(grid)on 6SB7			Z		L13 & L14 prim. &	
(d) Bocket 13 (c) Antenn 14 (c) Move 1 15 (c) Move 1 16 (c) Move 1 15 (c) Berve		converter tube		8.3 Mc.	E U		sec. of lat IF	Align let D' transformer
13 (c) Antenn 14 (c) Antenn 15 (c) Antenn 15 (c) Antenn 15 (c) Move 1 16 0 Berve		Bocket	.05 Mfd.	Unmodulated	f		transformer	for maximum reading
13 (c) more 1 14 (c) Antenn 15 (c) Antenn 15 (c) Mutenn 16 (e) move 1 16 (e) move 1		Antenna Post (re-	270	98 Mo.	æ	98 Mc.	LIO OHC. COIL	Set oscillator to
14 (c) Antenn 15 (c) Antenn 15 (c) Mutenn 16 (c) move 16 (c) be	13 (o)	move line ant.)	ohme	Unmodulated	100		Slug	dial scale
14 (c) move 1 15 (c) Antenn Antenn Antenn move 1 15 (c) be sa		~	270	98 Mc.	W	98 Mc.	L5 and L3 Det.	Allen det. and Ant.
14 (c) Antenn 15 (c) Antenn 15 (c) move 1 16 (c) move 1		move line ant.)	ohme	Unmodulated	100		and RF coil	stage to maximum
15 (c) Antenn Antenn 26 (c) move 1 Berve be sa	14 (C)						BANTE	LOGUTUR
15 (c) Antenn Antenn Besre besa	15 (a)	Antenna Post (re-	270 chime	45 Mc.	M L	. OM C#	CZ2	Set oscillator to diminanti
15 (c) move 1 Berve		Ant anna Doat (wa	010	LE No	2	LE MA	An and An	Alian Astector and
15 (c) Berve		move line ant.)	Chme	Unmodul sted	5 LC 4 -4			ant. stages for
0 88 170 9 0 0	36 (e)				<u>`</u>			maximum reading
B B P P P P P P P P P P P P P P P P P P	121 24							
0 0 8 14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		A vacuum tube	voltmete	r with an 180]	Lation	a	00,000 ohms in serie	of 200,000 ohms in series with the not lead will
8 9 0		BBFVB IOF FM BUJUB An Andinery A	C outmut.	meter connecte	ad acr	ces the primer	v or secondary of th	e output transformer vill
E C C E		be satisfactory fo	w all AM	adjustments.				
8207 8		The signal ge	merator c	utput should h	be ker	pt just high en	ough to get an indic	ation on the meter.
202 202		(a) Vacuum Tu	ibe Voltme	ter pin 5 on d	discri	Iminator transf	ormer to chassis (he	lf discriminator losd.)
(c) (g)			the Voltme	ter pin 7 on c	discri	Iminator transf	ormer to chassis (fu	(11 discriminator load).
(P)	4		ibe Voltme	ter 6SH7 limit	ter g	rid (pin 4 to c	bassis).	
	F		F watt cer	bon resistor i	solder	red across the	secondary L15 (pin 2	18 (pin 2 and 3 of 2nd LF trans.).

ALIGNMENT PROCEDURE

300 ohm ½ watt carbon resistor soldered across the secondary L18 (pin 2 and 3 of 2nd IF trans.). The leads to the resistor must be as short as possible and the resistor removed before operation 13 1s started

INDEX

Reference is made to the first page where material for the particular model begins.

Admiral Corp. 7C73	5 5	Majestic Radio 8B07D	93	R.C.A. Victor KCS 20A	153
9Al	5	8FM776	93	RK-121	145
Airline		12B26E	97 97	RS-123	145
74BR-1812A	105	12FM475 12FM778	97	610V1 610V2	141 141
74DA=1012A	100	12FM779	97	RC-610C	141 141
Bendix Aviation		41201	97	612V1	145
847-B	13	41201	57	612V3	145
011 5	10	Meissner Mfg. Co	.	630TS	153
Crosley Corp.		9-1091A, -B	101	00010	100
86CR	21	, .		Sparks-Withingto	n
86CS	21	Midwest Radio		see Sparton	
87CQ	21	R-12	102		
88TA	18	RGT-12	102	Sparton	
88TC	18	RT-12	102	10-76-PA	163
146CS	29			Stewart-Warner	
		Montgomery Ward		A72T1	171
Du Mont Laborato		74BR-1812A	105	A72T2	171
RA-101	33		1	A72T3	171
		Motorola, Inc.		A72T4	171
Emerson Radio		TS-3	125	T-711	175
528	47	HS-38	109	9026A to-D	171
537	51	HS-39	109		
120038	47	VT-71	125	Stromberg-Carlso	'n
120043	51	77FM21	114 114	1210	169
Fanor Mfa Co		77FM22	114	1010	200
Espey Mfg. Co. 7-B	5.4	77FM23 77XM21	121	Truetone	
/=D	0,2	77XM22, -B	121	see Western Au	ito
Farnsworth Telev	ision	HS-89	114		
GK-140 to 144	55	95F31, -B, -M	109	Western Auto	
GV-220	59	95F33	109	D1752	177
GV-240	59	HS-97	114	D1846	181
GV-260	59	VK-101	125		
		HS-102	121	Westinghouse Ele	
Galvin				H-113	183
see Motorola		Olympic Radio		H-114	183
		7-925	135	H-116	183
General Electric		7-934	135	H-117	183
417A	63	7-936	135	H-118	183
801	69	7-939	135	H-119	193
001	00	Packard-Bell		H-161	187
Howard Radio		872	137	H-168,-A	187
472AC, -AF	91	<u> </u>	101	Zenith Radio	
472C, -F	91	Pilot Radio		11C21	189
474	89	T-601	139	12H090 to -094	
		e		1211090 00 -094	; 109