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SIMPLE HOME PROJECTS No. 3

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Rec. Price RSC Price $£ 45 \cdot 40$ $£ 45.40 \quad £ 28.95$
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## TURNTABLES

 BSR Cover CartridgeCart.

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Simulated Teak finish.
Sizes approx.
Carr. 50p. per enc.

RSC G66 MKII GF6 WATT high quality STEREO AMPIFTER SEIO $25 \times 16 \times 9 \mathrm{in}$. E10.25

Controls: Bass. Treble, Vol. and Bal. 10 Transistors plus Diodes. Range 0-20,000 cos. Bass Control Range Treble Control $\pm 13 \mathrm{db}$. Selector switch for Crystal P.U. or Tape/Radio. 3-15 ohms. Attractive Black and Silver finished metal fascia plate. conirlitir EIT INO FULY WIRED PRINTED CLRCOIT EnA WIRING diagrays : Nisth Or factory bumi in teak veremed cabirit as illustrated $£ 19.50$. $\quad \mathbf{1 4 . 9 9} \begin{aligned} & \text { CnIr } \\ & 40 \mathrm{p}\end{aligned}$

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|  | Rec. Pr E105. |  |
| :---: | :---: | :---: |
| CS34D | $\pm 137 \cdot 50$ | 499.95 |
| GXC39D | £186.50 | ¢136.95 |
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GOLDRING GL75 with G800
As above but with Plinth and
PIONEER PL12D with Plinth
5

BSR MP60 with Plinth and
Cover plus G850 Goldring
GARRARD SP25 Mk. 1V with
Plinth and Cover plus G850

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ME8 $13 \times 9 \frac{1}{2} \times 6 \frac{1}{2}$ in. $E 4.50$
JE8 $\quad 16 \times 11 \times 9$ in. $\quad 66.95$
Both cut for 8 in. speaker. $\mathrm{Cu}^{+}$for 10 in . and Tweeter SEI2 $25 \times 16 \times 9$ in. $\quad \mathbf{E 1 0 \cdot 2 5}$ Cut for 12 in . and Tweeter
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Consisting of Twin Turntable Console with Pre-amp and built-in Power Output. Sep. vol. controls for each T/table H/phone monitoring facilities. Sep. Bass and Treble controls. Mic. Vol. control. Neon Mains Indicator. Plus Pair 12 25w
Rexine covered cabinets.
c99.99

Terms: Dep. $\mathbf{£ 1 5 . 9 9}$ and 18 fortnightly paymts. £5.38. (Total £112.83)
AS ABOVE LESS SPEAKERS Terms: Dep. 59.00 and 18 fort.
aightly payments 84.61
179.95

MOBILE DISCO CONSOLE


MIC., JACK, PHONE JACK, MONITOR VOL. CONTROL. MONITOR SELECTOR DECK (1) Vol. Control, DECK (2) Vol. control, Mic. Vol. Control, Treble Control, Bass Control and ON/ OFF Switch, Neon Indi- $\mathbb{5 0 . 0 5}$ cator, Twin Turntables.

Carr. £3
Terms: Dep, 57.95 and 18 fortnightly paymts. £3.33 Total $£ 67 \cdot 89$.
POWER (SLAVE)
AMPLIFIER 100 WATT


Suitable for use with above or other DISCOConsoles.
Also for increasing output $\pm 45.00$
of lower-powered Ampliof lower-powered Amplipayments of $£ 5.80$ (Total $£ 52.20$ ) mthly
 TITAN GROUP/DISCO SPKRS

| T12/35 12" 35w | Rec. Price $£ 13 \cdot 00$ | RBC Price $\mathbf{£ 1 0} 95$ |
| :---: | :---: | :---: |
| T12/60 12' ${ }^{\prime \prime}$ 60w | £20.00 | £14.95 |
| T12/100 12" 100 w | £35.00 | £27.95 |
| T15/70 15" 70 w | $£ 27 \cdot 00$ | £19.95 |
| T15/100 15" 100w | £38.50 | £27.95 |
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AUDIO FIDELITY MODEL 80 HIGH FIDELITY SPEAKER
A full range 8 in. 10 watt unit for excellent sound quality, in suitable enclosure. Roll P.V.C. cone surround and long throw voice coil to achieve very low fundamental resonance of 30 c.p.s. Tweeter cone is fitted to extend high note response. Frequency range 25 Hz to 15 KHz . Gauss 10,000. Impedance $8-15 \Omega$. 86.21 en. $\leq 9.25 \mathrm{pr}$.




250 v .60 mA 6.3 v . 2 a . $250-0-250 \mathrm{v} .60 \mathrm{~mA} 6.3 \mathrm{v}-2 \mathrm{a}$. FULLY SHROUDFD UPRICET MOUHTI $250-0.250 \mathrm{v}_{0} 60 \mathrm{~mA} \theta .9 \mathrm{~F}$. $250.0-950 \mathrm{v} .100 \mathrm{~m}$. 2 v . 28.60 | $250 \cdot 0-250 \mathrm{v} .100 \mathrm{~mA}$ |
| :--- |
| $300-0-300 \mathrm{v}$. |
| 130 mA |
| $6 \cdot 3 \mathrm{v} .4 \mathrm{a}$. | la. for Mullard 510 Amplifer

19. For Mulard 510 Amplifer 85.20

 425-0-425v. 200mA 6-3v. 4a. 6-3v. 4s. 6v. 3a
$450-0-450 \mathrm{v} .250 \mathrm{~mA} 6.3 \mathrm{v} .4 \mathrm{a}$. C.T. 5v. 3a. $210 \cdot 45$

## TOP 8HROUDED DROP-THROUGH TYPE

 $250-250 \mathrm{v} .70 \mathrm{~mA} 6-3 \mathrm{v}$. 2a. $0 \cdot 5 \cdot 6.3 \mathrm{v}$. 2 a . $250-0-250 \mathrm{v} .100 \mathrm{~mA} 6.8 \mathrm{v}$. 3.5 s $250-0-250 \mathrm{v} .100 \mathrm{~mA} 6.3 \mathrm{v} .2 \mathrm{a} .6 \cdot 3 \mathrm{v}$. 1 a . $350-0-350 \mathrm{v} .80 \mathrm{~mA} 6 \cdot 3 \mathrm{v} .2 \mathrm{~s} .0-5 \cdot 6 \cdot 3 \mathrm{v}$. 2 $250-0-250 \mathrm{v} .100 \mathrm{~mA} 6 \cdot 3 \mathrm{v}$. $4 \mathrm{a} .0-5 \cdot 6 \cdot 3 \mathrm{v}$. 3 a $300-0-300 \mathrm{v} .100 \mathrm{~mA}$$300-0-300 \mathrm{v} .3 \mathrm{v}$. 4 s . $0-5-6.3 \mathrm{~mA}$. 3 a a $300-0-300 \mathrm{v}$. $180 \mathrm{~mA} 6.3 v .4 \mathrm{a} .0-5-6$
sultable for Mullard $\delta 10$ anp

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\begin{aligned}
& \text { sultable for Mullard } 510 \mathrm{Amp} \text {. } \\
& 350-0.350 \mathrm{v} . ~ \\
& 100 \mathrm{~mA} 6 \cdot 3 \mathrm{v} .4 \mathrm{a} .0-5
\end{aligned}
$$ $350-0-360 \mathrm{v} .100 \mathrm{~mA} 6.3 \mathrm{v}$. 4 a . $0-5-6.3 \mathrm{v} .3 \mathrm{a}$ 85.8.

 Type: 12v. 1a si 10 6.3v 1 POWFR PACK


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| 6.20 | 1 |
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AUTO (ETKP UP/BTEP DOWN) TRAKEFORMERS $\begin{array}{llll}0-110 / 120 \% & 200-230-250 \% & 50-80 \mathrm{w} . & 22 \cdot 80 \quad 150\end{array}$ watts $8.80,250$ watts $86.37,500$ watts 80.84 CHARGRE TRAAGFORMERS
$0-9 \cdot 15 \mathrm{v} .1 \frac{1}{4} \mathrm{a}$. 6a. $88 \cdot 19,8 \mathrm{~s} .48 \cdot 48$
OUTPUT TRANGFORMRRS
Standard Pentode 5000 to 3
Standard Pentode 6000 to 3 ohra, or 7000 ohm to 3 ohm s1-18, Pugh Poll 8 watts EL84 to 3 ohm or ohm or 15 ohm ese.61; Push Pull 10-12 6 to 3 match 6v. 6 to 3, 5, 8 or 15 ohm 28:72; Pugh Pull EL84 to 3 or 15 ohm 10-12 watts 88.61 ; Push Pull Ultra Linear for Mullard 510 etc. 44.35 ;.


DISCOMASTER TWIN TURNTABLE POWER CONSOLE $£ 119.95$
W20 $\begin{aligned} & \text { Twin McDonald MP60 type turntables. Sonotone or Acos cartriges with } \\ & \text { dimmond styll. Fachlitles an TDI Console but with bullt-in } 100 \text { watt Power Am }\end{aligned}$ dimmond styll. F'aillties a.. TDI Console but with bullt-in 100 watt Power Am- $\quad 2.50$
plifier, complete with lid. Or Dep. A18.95 and 18 fortnightly pymts 26.78 (Total 5135.98 ) STEREO VERSION $\leq \mid 55$ or DEPOSIT 825 and 18 fortnightly
R.S.C. COLUMN SPEAKERS

IDEAL FOR VOCALISTS All types 15 Ohms covered in Vynide \& Vyair TYPE Cl32 40-50 WATTS 427.95 Incorporating two exceptionally efficient
 AND PUBLIC ADDRESS TYPE
$12^{\prime \prime}$
25
watt
Highly
Bensitive high flux $12 " 25$ watt Highly sonaitive high fiux
apeakers with high power volee colls. speakers with high power volce colle
Rizo approx. $\mathbf{\delta}^{\prime \prime} \times 14^{\prime \prime} \times 11^{\prime \prime}$. Dop. $85 \cdot 11$



INTEREST on Credit Purchases REFUNDED settled in 3 months
SUPER MINSTREL 10 W GUITAR AMP.
Incorporating Tremolo and 10 " Speaker. Outpat 10 wstts
R.M.S. Continuous. 3 Jsck Inputs for IIticrophone and Inatrument. Maing Neon Controls: Volume, Tont. Tromolo Bpoed, Tremolo Intensity.
Terms: DEPOSIT 57.78 and 8 monthly payments 83.40 (20tal 884.88 ) Carr. Iree
 For Lead Guitar. Mic, Gram, Radio, Tape (Not for une with Buas instrumenta) Inc. 3 Inputs and 2 vol coutrols plus Treble \& Bass, TREMOLO with asioociated controls. Attractively fintshed in black with silvor-anioned iancia. Compact size
Fitted carrying handie. Deponit 89.25 and 8 mithly paymenta 86.76 (Total 288.38)
PTA ATP夏 5 COMBINED AMPLIFIER
COMBINED AM
AND BPEAKER
£59.95
Rating 50 watts. 3 inputs, 2 vol. controls. Bas. Treble, Presence Carr. 81.50
Rating
Dep. $87 \cdot 95$ \& 8 mthly . pyints. $\$ 7 \cdot 48$ (Total $\AA 67 \cdot 79$ ).


## FAL PHASE 50-4 AMPLIFIER 50 WATT

solld state. 4 Sep. controlled inputs Flus master vol. control. Ind Bass and Treble Controls. Protection against serious o/p overlonding.


Units listed below
(a) DISCOMASTER TWIN TURNTABLE CONSOLE with integral l00W amplifier
(b) PAIR OF HIMFI HEAD PHONES
(c) MATCHING 'MIKE'
(d) PAIR 50 WATI SPEAKERS Black Rexine covered Cabinets Size approx

DEP. $119.99 \& 18$ fortnightly. payments of $£ 9 ; 75$ (Total $£ 195 \cdot 49$ ).

## STEREO VERSION

Or DEPOSYT 284.95 and $\mathbf{~} 209.95$ 18 fortnightly pymts.
e11.19 (Total 28888.87)

TDI DISCO CONSOLE
Incorporating twin BSR MP60 type turntables and Sonotone or Acos Cartridger with diemond styli. turntable. Also MOHITORING FACLIMIES, plus Treble and Bass Controls. Separate iupat for 'mike' with vol. control. Black Vynide covered
Cabinot with lid, Cabinot with lid,
Or DEP
18 fortiontly and 85.11 (Total 8101.98 )

TD2S STEREO VERSION OF ABOVE
Terine DEPO8IT \&20 $\leq 125 \cdot 00$ and 18 fortnightiy Carr. 21.60 payments 28.71 (Tutal 8140.78)
FANE ULTRA HIGH POWER SPEAKERS \& KITS ll power ratinge ars R.M.S. continuoun. \& Y EARg' GUARANTERE High flux ceramic magnets. ALL CARRIAGE FREE. $18^{\prime \prime} 100 \mathrm{Watt}$ 14,000 tauss $8 / 150$
638 $£ 38.95$
Dep: 88.95 and 8 mthly paymonts
60 (Total 848.75 ) TOR BAES GUITAR

'POP' $100 |$\begin{tabular}{l|l|l|}
\& <br>
\hline

 $15^{\prime \prime} 60$ Watt $12^{\prime \prime} 50 \mathrm{Watt}$ 

14,000 gauss \& 13,000 gaus: <br>
$8 / 15 \Omega$ \& $8 / 15$ <br>
\hline 14.95
\end{tabular} £ 22.95

Dop. 83.95 and 8 monthly payrnents.
$\mathbf{4 2 . 8 7}$ (Total 228.91 ) $\begin{aligned} & 8 / 15 \\ & \text { ohm }\end{aligned} \leq 14.95$ Dual Cone. Terms for pairs Dep. 88.90 $\& 8$ mthly pymts
84.24 . Total 887.82 84.24. Total $287 \cdot 82$
PAIR BUITABLR PALR BUTTABLE
ALI PURPOSE 8

## HIGH POWER

 TWEETER PH50 Response $3 \mathrm{KHz}-20 \mathrm{KZz}$ with 2 to 4 mid. Non elect. fliter available 5 p Rating50 Watt Imp 8 Q £6.65 'POP' 25/T 12" 25W Dual cone.
15 ohm Imp.
 Gultar use). Terms for Pairs: Deposit $\mathbf{5 3 . 0 8}$ and 8 mthly paymts of $82 \cdot 70$
(Total $825 \cdot 88$ ).

## CO KIT <br> D40 50 WATT DISCO KIT <br> ALL PURPOSE FULL RANGE

 Consisting of $12^{\prime \prime} 13,000$ Gauss Bass Unit. HPXI Cross over and PH50. Tweeter as above. Imp requires pair in one cabinet). Terms: Dep. £3 88 mthly.pyts. £2. 75 (Total £25)


HIGH QUALITY LOUDSPEAKER UNITS $\begin{array}{lll}\text { ALL } & \text { 2-TONE VYNIDE and } \\ \text { Lid } \\ \text { 50-WATT Fitted pair of } 12 / 2\end{array}$ 30 watt high flux speakers. Imp. 8-15 ohms. Car. £1-50.Terms: Dep. $85-11$ and 8 monthly payts. of $£ 5 \cdot 11$ T L12/50 $12^{\prime \prime} 50$ WAT' 13.000 lines 15 ohms. Terms: Dep. £3-95 and ${ }_{8}^{8}$ mthly pymts. $£ 3.37$ (Total £30-91) Сarr. 55p.
IINGLE MACHINES I.S.E. CAI 27
£25.95

DEPOSIT \& 8 and 18 fortnightlypayments $84 \cdot 61$. Total $191 \cdot 98$

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 PROLECTORS £29.95 'SOUND'TO LITE' SYSTEM PULSAR , patind mid ¢ 106.95 Dep. $\$ 14.96$ and 18 fortnightiy payts. $25 \cdot 93$. (Total \&121.69). Super 8L Unit. 1000 watt per channel. Manusal override buttons, 2 ppotbanks with 6 bulbs ( 3 sep. colours) 6 yd.and 10 yd. leads, fitted plugs. Units sold sep. FAL SOUND-TO-LITE UNIT E21.60
3-WAY SPOT BANK Excluding Bulba Each $\leq 16.20$ COMPLETE SYSTEM $\underset{\& 1.50 .255}{\text { Carr }}$ Incl, 2 spotbanks and bulbs. AIL ORDERS 2 EXPORT EAQULRI AUDIO HOUSE, HENOONNER LANE, LEEDS. 18. Tel: Pudrey (09785) 77881.
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solder dispenser


A coil of Ersin Multicore Savbit Solder in a dispenser 7 tt 6 in of 18 s.w.g. (2.2 metres of 1.22 mm ), The Solder that reduces the wear of soldering iron bits.

Size 5 32p

SAVBIT $_{\text {solder }}$
for general purpose work

A handyplastic reel of SAVBIT alloy. 63 tf of 18 s.w.g. ( 19.2 metres of 1.22 mm )

Size $12 £ 1.72$


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 soldering aluminiumNew Muiticore Alu-sol flux-cored solder in 16 s.w.g. No extra flux needed. Plastic reel holds 36 ft . Supplied with full instructions. Also available in solder dispenser.

Size $4 £ 2.32$


## Fine gauge solder

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For soldering fine joints Dispensers. of Ersin Multicore Solder make those small jobs easier. 21 ft of 22 s.wo 16.4 s.w.g. (6.4
metres of 0.71 mm ) 0.71 mm
solder, specially suitable for soldering fine wires, small components and for repairing printed circuits.
Size 15 36p
Or size 19A for kit wiring or Radio and T.V. repairs 7ft. (2.1 metres) of 18 S.w.g. ( 1.22 mm ) s.w.g. ( 1.22 mm )
Ersin Multicore Solder. Ersin Multicore Solder.
Size 19A $34 p$

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Prices showr are recommended retait excluding $V . \dot{A} T$.
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reith full er with full ication
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| AC12B | 13 |
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| AC155 | 18 |
| AC156 | 20 |
| AC176 | 22 |
| AC187 | 19 |
| AC187K | 24 |
| AC188 | 17 |
| AC188K | 26 |
| AD142 | 45 |
| AD149 | 40 |
| AD161 | 38 |
| AD162 | 38 |
| AF114 | 24 |
| AF115 | 21 |
| AF116 | 22 |
| AF117 | 19 |
| AF118 | 50 |
| AF139 | 35 |
| AF178 | 45 |
| AF180 | 45 |
| AF181 | 45 |
| AF239 | 40 |
| AF240 | 60 |
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AB16
AB17
AB18
AB1

|  | 10 | 4 | 3 | 1.08 |
| :--- | :--- | :--- | :--- | :--- |
| AB19 | 12 | 5 | 3 | 81.20 |
|  | 12 | 8 | 3 | 81.50 |

ABS PLASTIC BOXES $+8 \%$
Handy boxes for construction projects. Moulded extruston Handy boxes for construction projects. Moulded extrusion
rails for P.C. or chassis panels. Fitted with 1 mm front rails ior P.C. or chasais panels. Fitted with
panels.
$1005=105 \mathrm{~mm} \times 73 \mathrm{~mm} \times 45 \mathrm{~mm}=55 \mathrm{p}$
$1006=150 \mathrm{~mm} \times 75 \mathrm{~mm} \times 47 \mathrm{~mm}=72 \mathrm{p}$
$1006=150 \mathrm{~mm} \times 75 \mathrm{~mm} \times 47 \mathrm{~mm}=72 \%$
$1007=184 \mathrm{~mm} \times 124 \mathrm{~mm} \times 60 \mathrm{~mm}=81.28$
$1007=184 \mathrm{~mm} \times 124 \mathrm{~mm} \times 60 \mathrm{~mm}$ (sloping front) $=65 \mathrm{p}$ TELESCOPIC AERLAL
TELESCOPIC AERLAL
Nine section fully swivelling telescopic aerial with 4B
Nine section fully swivelling telescopic aeri
single bolt flxing or two hole fixing bracket.
single bolt fixing or tr
Fully extended $=43^{\prime \prime}$
Fully extended $=43^{\prime \prime}$
Fully closed $=7^{\prime \prime}$
Fully closed $=7^{\prime \prime}$
Our Price 50 p $+\mathbf{P} / \mathbf{P}+$ VAT @ $25 \%$

CLEAR PLASTIC PANEL METERS
Size $59 \mathrm{~mm} \times 46 \mathrm{~mm} \times 35 \mathrm{~mm}$ these metern require * 38 mm hole for mounting.
ME6 $=0$ to 50 micro amp Full Scale
ME7 $=0$ to 100 micro amp Full Scale
ME8 $=0$ to 500 micro amp Full Scale
$\begin{array}{ll}\text { MES } & =0 \text { to } 1 \mathrm{~m} / \mathrm{a} \text { Full Scale }\end{array}$
ME10 $=0$ to $5 \mathrm{~m} / \mathrm{a}$ Full Scale $\begin{aligned} M E 11 & =0 \text { to } 10 \mathrm{~m} / \mathrm{s} \text { Fulls } \\ & =0 \text { to } 50 \mathrm{~m} / \mathrm{g} \mathrm{F}_{11}\end{aligned}$ ME12 $=0$ Scale
ME13 $=0$ to $100 \mathrm{~m} / \mathrm{A}$ Full MEI: $\quad \begin{gathered}\text { Scale } \\ -0 \text { to } 500 \mathrm{~m} / \mathrm{a} \text { Full }\end{gathered}$
 $\begin{aligned} & \text { ME16 } \text { Scale } \\ &=0 \text { to } 50 \text { volte }\end{aligned}$
$\mathrm{MEIT}=0$ to 300 voits
ME18 $=$ "S" Meter
OUR PRICE 38
ME19 $=$ "VU" Meter
$\begin{array}{lll}\text { DECON DALO } & \text { B3PC } \\ \text { ETCH } & \text { RESIST } & \text { PEM }\end{array}$
The Decon Dalo 33PC in a unique instrument tor the protersional electronies en gineer; enabling him to prepare in minutes a perfect printed circ
board
OUP
$\xrightarrow{\text { OUR PRICE } 80 \mathrm{p}+8 \%}$
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$=\$ 1.30 .12 \times 4 \times 4 \mathrm{in} .=21.50$.

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$2 / 350 \mathrm{~V}$ \& 20 p \& $500 / 25 \mathrm{~V}$ \& 20 p \& $10+16+16 / 275 \mathrm{~V} 45 \mathrm{p}$ <br>
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$8 / 350 V$ \& 20 p \& $100 / 26$ \& $100 / 275 \mathrm{v} 85 \mathrm{D}$ \& $80+50 / 300 \mathrm{~V}$ <br>
$8 / 350 \mathrm{~V}$ \& 22 p \& $100+32 / 450 \mathrm{~V}$ \& 75 p
\end{tabular}

 \begin{tabular}{llll|l}
$18 / 500 V$ \& 50 D \& $8+8 / 450 \mathrm{~V}$ \& 50 p \& $100+50+50 / 850 \mathrm{~V} 85 \mathrm{p}$ <br>
$82 / 500 \mathrm{~V}$ \& 10 p \& $8+10 / 450 \mathrm{~V}$ \& 50 D \& $82+32+82 / 850$ <br>
$25 / 25 \mathrm{~V}$ \& 10 p \& 78

 

$25 / 85 V$ \& $10 \mathrm{D}, 8+10 / 450 \mathrm{~V}$ \& 50 D \& $82+32+32 / 850$ \& 75 D <br>
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$100 / 25 v$ \& 10 D \& $182+82 / 350 \mathrm{~V}$ \& 50 D \& 4700/68V \& 85D
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22, 25, 50, 68, $150,470,600,680,1500,2200,3800$, mid sil 6801 l 10 p .68.
$92,25,28,100,150,200,220,380,470, ~ 880,1000, ~$
2500. 2900 . mid all 10 voll 10 p 68.
$220,880,1000,4700$, mtd all 4 y .10 p at
$1,2,4,5,8,18,25,80,50,100,200 \mathrm{mF} 15 \mathrm{~V} 10 \mathrm{p}$.

 500 mF 50 V 68 p , 8000 mF : 80 V 67p; $4700 / 63 \mathrm{~V} 95 \mathrm{p}$
 $500 \mathrm{~V}-0.001$ to $0.054 \mathrm{p} ; 0.110 \mathrm{p} ; 0.2512 \mathrm{p} ; 0.4725 \mathrm{p}$. CERAMIC 10F to $001 \mathrm{mF}, 5 \mathrm{p}$. Silver Mica 2 to 8000 DF , 5p PAPER 850 80.1 Tp; 0.6 18p; 1 mF or 2 mF 150 V 16 p .基ICRO SWITCH angle pole changeover 20y
MICRO SWITCH aub min 86p
TWIN GAKG. "0-0" $208 \mathrm{pF}+176 \mathrm{pF}$, $81 \cdot 10$. s00pF atandard twin gang 75 p . 120 PF twin gang 80 p .

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$£ 3.45$
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 Ditto $5 \%$. Protorred valuan 10 ohme to 10 meg., ip. 10 D . WIRE-WOUND RESISTORS. 5 watt. 10 wift. 15 watt, 10 ohme to $100 \mathrm{x}, 12 \mathrm{p}$ ach; 2 w 0.5 ohm to 8.2 ohma 15 g .


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 $5,8,10,16$ च. $\frac{1}{2}$ A $£ 2.6-0-6$ v. 500 mA 90 p .9 च. $1 \mathrm{\varepsilon mp} .95 \mathrm{p}$. 0 v .2 smp . tapped 10 v . or 30 v . 82.50 .20 V 3 amp . 52 40 V 8 a. $£ 2.50$. 22V 4 s .48
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or 18y, outputs 1 i
MAINS ISOLATING TRANSFORMER
Primary 0-110-240v. siscondary 0-240v. s empa. 720 watta. Innulated torminalin. Varnigh improgneted. Fully nclosed in steel cene with fring ieot.
Famoun make. (Value s10) OUR PRICE $\{\mid 3.50$ Carr.
Euitable for ontride use.
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Complete with 12 ft . twin lesd flted with din spesker plug. Ready assembled with leads ior speakers, bass, mid and tweeter. Cronsover frequencies- 950 cps and
$3,000 \mathrm{cps}$. For aystems up to 25 watts.

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6 K. ohma to 2 Meg. LoG or BRITISH AERIALITE
 Edge 5K. 8.P. Trannistor 25p 40 yd . 22; 60 yd . 23. FRINGE LOW LOSS 10 p per
Ideal 625 and colour.

Wirowound controls 1 tin. diam. 3 watts. 10 ohms to 100 X Britith made with long apindlea tin. dia 85 pas.
DUAL CONCENTRIC POT 500k LOG + 600k LIN D.P. 5 witch. Inner apindle $3 \frac{1}{2} \mathrm{in}$; outer apindle 2iin. 75p.
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ALL PURPOSE AMPLIFIER
4 inputs 2-way mixing. 2 outputs separate treble

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QUALITY LOUDSPEAKER ENCLOSURE
Teak veneered in thick wood cabinet. Size $18 \frac{1}{2}$ in $\times 18$ tin $\times 8$ in. Weight 231 ha . Thin cabinet features a wide mesh Silver Grill covering a separate compartment for mounting Tweeters or Mid-Range Horn. The tully sealed bass compartment is cut out for 6inch Woofer. $£ 8.50$ Carr. 85p.
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 12 in 15 wattsEspecially designed to provide full ranga reprodaction at an economical cost. Suitable for ystem. Built-in concentric weeter cone.
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I2in. 25 watts
A high quality loudspeaker. resonance ensures clear reproduction of the deepest bass. Fitted with a specisil copper drive and concentric tweeter cone resalting in fuli range reproduction with
remarkable efficiency in the romarkable efficiency in the Baps Resonanco
Bass Resonanco $18,500 \mathrm{ganan}$ $\begin{array}{ll}\text { Flux Density } & 16,500 \mathrm{ganas} \\ \text { Useful responss } \\ 20-17,000 \mathrm{cps}\end{array}$ 8 or 15 ohms models.

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A full range reproducer for high power, Electric Guitara, public address, multi-speakar Ideal for Hi-Fi and Discotheques.
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A high wattage loudspeaker of oxceptional quality with a lovel response to above 8,000 cps. Ideal for Public Address, Discotheques. Electronic instrument and the ome Ri-FI.
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Practical Wireless, December 1975

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\hline 12 & 6 & 116 & 6.61 & 0.52 \\
\hline 16 & 8 & 17 & 7.90 & 0.80 \\
\hline 20 & 10 & 115 & \(10 \cdot 42\) & 0.88 \\
\hline 30 & 15 & 187 & 18.25 & 1.01 \\
\hline 40 & 20 & 282 & 14.85 & O.A. \\
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\hline \multicolumn{5}{|l|}{30 Volts} \\
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\hline Amp: & Re & & Price & Post \\
\hline & \(\stackrel{N}{11}\) & & \({ }^{5}\) & \({ }_{0}^{4}\) \\
\hline 0-5 & 11 & & 1-90 & \(0 \cdot 47\) \\
\hline , & 7 & & 2.40 & 0.56 \\
\hline 2 & & & 8-50 & 0-56 \\
\hline 3 & 2 & & 4.50 & \(0 \cdot 64\) \\
\hline 4 & 2 & & \(5-15\) & 0.72 \\
\hline 5 & 5 & & 6.40 & 0.72 \\
\hline , & 11 & & 7-16 & \(0 \cdot 88\) \\
\hline 8 & 8 & & 9.55 & 0.95 \\
\hline 10 & 8 & & \(9 \cdot 67\) & \(0 \cdot 95\) \\
\hline
\end{tabular}

\section*{50 Volts} Prim. 200-240V

\begin{tabular}{|c|c|c|c|}
\hline Ambe & \[
\begin{aligned}
& \text { Ret. } \\
& \text { No. }
\end{aligned}
\] & Pricif E & \[
\mathbf{f}_{6,0 \mathrm{~s}}
\] \\
\hline 0.3) & 102 & 2.58 & 0.47 \\
\hline \(]\) & 103 & 3.18 & \(0 \cdot 56\) \\
\hline \(\because\) & 104 & 5.08 & 0-64 \\
\hline 3 & 105 & 6.81 & 0.78 \\
\hline 4 & 100 & 788 & 0.88 \\
\hline 6 & 107 & 12.30 & 0.95 \\
\hline 8 & 118 & 13.20 & \(1 \cdot 13\) \\
\hline 10 & 119 & 17.02 & O.A. \\
\hline
\end{tabular}

\section*{60 Volts}

Prim. 230-240V.
Prim. 250-240V.
See. \(24,30,40,607\)
\begin{tabular}{|c|c|c|c|}
\hline Amps & Ref. & Price & Post \\
\hline & No. & + & \% \\
\hline 0.3 & 124 & \(2 \cdot 30\) & \(0 \cdot 5\) \\
\hline 1 & 126 & \(3 \cdot 11\) & \(0 \cdot 56\) \\
\hline 2 & 127 & 6.69 & 0.72 \\
\hline 3 & 125 & 7.92 & \(0 \cdot 80\) \\
\hline 4 & 123 & 8.75 & 0.95 \\
\hline 5 & 40 & 9.75 & 0.95 \\
\hline 6 & 120 & 11.20 & 1.01 \\
\hline \% & 121 & 15.00 & 1.18 \\
\hline 10 & 122 & 18.20 & O.A. \\
\hline 19 & 189 & 18.50 & O.A. \\
\hline
\end{tabular} O.A.

\section*{miniature and equipment}
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline \[
\text { Prim. } 240 \mathrm{~V} \text { Vilt. }
\] & creon. & \multicolumn{2}{|r|}{Miliatup*} & \multirow[b]{2}{*}{Het.
No.} & \multirow[b]{2}{*}{Brice} & Post \\
\hline Bec. 1 & Sec. \({ }^{\text {a }}\) & sec. 1 & Spe. 2 & & & 3 \\
\hline 3-0-2 & - & 200 & \(\cdots\) & 438 & 1.50 & 0.25 \\
\hline 0-6 & 0-6 & 500 & 500 & 234 & 1.38 & 0.25 \\
\hline 0-6 & 0-6 & 1000 & 1000 & 212 & 1.90 & \(0 \cdot 47\) \\
\hline 9-0-9 & - & 100 & - & 13 & 1.40 & \(0 \cdot 25\) \\
\hline 0-9 & 0-9 & 330 & 330 & 235 & \(1 \cdot 50\) & 0.25 \\
\hline 0-8-9 & 0-8-9 & 500 & -00 & 207 & \(1 \cdot 93\) & \(0 \cdot 34\) \\
\hline 0-8-9 & 0-8-9 & 1000 & 1000 & 208 & 2.76 & 0.47 \\
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\hline & Ref. & Caned & Plugs & Open & Powt \\
\hline \multicolumn{6}{|l|}{\multirow[b]{2}{*}{Tapped at 115, 290, 240 Yolts}} \\
\hline & & & & & \\
\hline 20 & 113 & \(4 \cdot 10\) & \(0 \cdot 20\) & 1.72 & 0.47 \\
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\hline 150 & 4 & 6.65 & 0.20 & \(4 \cdot 12\) & 0.86 \\
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\title{
Software Gobbledegook!
}

0NE of the most difficult things about publishing technical material is that one is never quite sure for whom one is writing. This is particularly so in the case of a magazine like ours. Our readership covers students, school teachers, laymen, electronics engineers and university professors. In order to avoid talking down or talking up we have to be very careful how we select our words. Regular readers will know that we are always careful to define words of an unusual nature and we always attempt to make our descriptions as simple as possible using plain language.

On the whole, manufacturers of elecironic components are only too well aware of the problems the potential user has in working within the specified ratings of his device and are careful to ensure that there is no doubt in the mind of the experimenter or development engineer. We would like to think that this ability has evolved by using practising engineers to write up the original instructions.

We only wish the same could be said of a new range of technical literature that is coming out on a new type of integrated circuit, the MICROPROCESSOR. Publicity material tells us that these devices are God's gift to the electronics industry; anything you can do with combinational logic you can do with a microprocessor, with a saving of space, time and money. Intuitively we believe what we are told but from the reams of descriptive material that are flooding our offices we have yet to find a document which tells us in simple terms exactly what the devices do, how they do it and how we can use them.

At first we thought that the problem was our own ignorance but on making enquiries in the electronics industry we find the complaint is very commonplace. These devices, like the computers they emulate, have brought into our sphere of the electronics business a new type of individual, the SOFTWARE SPECIALIST. It is unfortunate for us that most of the major microprocessor manufacturers seem to have recruited teams of these, so called, "WhizzKids" to pass on the facts of how to use and not abuse these exciting new components. In so doing they have now inflicted on us the "Buzz Word" technology in which these Whizz Kids specialise. Being cynics we are not impressed with sophisticated new words because, more often than not, we have found that with a little more thought on the part of the writer a meaningless new. word, which needs a glossary of terms to decode, could easily be replaced in descriptive text with a straightforward sentence written in simple English. We accept the fact that eventually one may have to resort to the shorthand of mnemonics and buzzwords when one is totally familiar with the subject but where on earth is the sense in presenting to the newcomer a document in which every fifth word is meaningless?

Come off it microprocessor manufacturers! We admire your technical achievement in developing these potentially revolutionary components but we are not impressed with the way in which you are trying to persuade us to use them. What we want is some well-written literature originated by engineers, for engineers, and this MUST be supplemented by a few simple applications reports. In our experience there is only one way to really get to understand a new component and that is by using it. How on earth do you expect us to start building these systems when you seem hell bent on disguising them behind a forest of "Gobbledegook"?

LIONEL E. HOWES-Editor

\section*{Disco Decks}

THE BSR McDonald BDS80 belt-drive turntables used in the Disco, illustrated on the front cover this month, were kindly supplied by BSR Limited.

\section*{Trio Catalogue}

BH. Mórris \& Company, United Kingdom distributors for Trio high-fidelity equipment, have produced a new, full-colour, illustrated catalogue detailing the Trio range.
Specifications and prices for the complete range of stereo receivers, tuners, amplifiers, turntables, cassette decks, loudspeakers, headphones and highfidelity systems are included.

Copies of the catalogue, which was designed and printed in Britain, are available free from Trio dealers or direct from B. H. Morris \& Company, Trio House, The Hyde, London NW9 6JP (Telephone 01-205 6441).

\section*{Leak 2000 series speakers}

ANEW and improved treble unit is being incorporated in the Leak 2000 series of loudspeakers.

Whilst the current treble unit has a wide and smooth response in the operating range of 4 kHz to 20 kHz and excellent power handling qualities it is now felt by some that it sounds slightly hard or brash.

The new unit, distinguished by the carefully designed phase-correcting assembly on the front, when compared with its predecessor produces smoother treble but shares the detailed response to beyond 20 kHz . The previous traces of hardness however have now been reduced to negligible proportions.
This new driver will be incorporated in the 2030, 2060 and 2075 enclosures in the Leak 2000 range.-Rank Audio Visual Limited, P.O. Box 70, Great West Road, Brentford, Middx.

\section*{Ambience Phones}

JAPANESE electronics giant Matsushita Electrical Industrial Co. Ltd. has introduced a new headphone system called "Ambience-phone". It will be sold in Japan this year and is to be available in other countries in 1976.

Listening with conventional headphones, the sound image localises inside the area of the listener's head-unlike the sound from a loudspeaker. Thus the feeling of distance with conventional headphones is nil.

Engineers at Matsushita found that indirect sound is a vital factor in giving a feeling of distance to the acoustic sense of human beings. It was also found that when the feeling of distance was greater, the sound localisation outside the area of the head was realised in a more idealistic manner.

To achieve the desired effect the company uses a delay element called a BBD-bucket brigade device. This device passes a signal charge along its elements from one to the other, rather like a chain of firemen passing buckets of water along from one to the other-hence the name. Passing these charges along takes a finite time from first to last element and thus a delay is introduced.
Further research at Matsushita showed that even in a system where the loudspeaker gives an "even" reproduction of sound, the

middle audio range is heard louder, and the higher sound weaker, due to the characteristics of the human head and hearing system.

The headphones used in the Ambience system are designed in such a way as to automatically modify the middle range sounds making them appear louder and to make the higher sounds weaker. The purpose is to simulate more exactly the characteristics of a loudspeaker system.

Applications for the new system are seen in almost every facet of audio, hi fi, portable radios, tape recorders, stereo receivers etc.

The system was shown this year at the "International Radio and TV Exhibition 1975" in Berlin. Already, some 20 patents have been taken out in Japan, and a further five are being sought in five other countries including Britain.-D.L.G.

\section*{Audio/Visual Show}

AUDIO/VISUAL in the Midlands" will be held on February 24th, 25th and 26th, 1976 and will feature a wide range of equipment within certain categories encapsulated by the Audio/Visual banner. This new exhibition will be staged in spacious exhibition halls at the National Agricultural Centre, Stoneleigh, Warwickshire. The show will run from 10.00 a.m. till 8.00 p.m. each day with trade visitors only during the morning sessions, the general public being admitted from 2.30 p.m. daily.

The show will be divided into
sections covering trade, education, security and equipment of domestic interest. The organisers are aiming to attract specialist audiences in each of these major categories by issuing invitations and directing an advertising campaign towards each sector.

Parking facilities are excellent, and there are plenty of good hotels within easy reach of the exhibition site.

For further information please contact the organisers: D. L. Ford Exhibitions (1968) Ltd., National Agricultural Centre, Stoneleigh, Warwickshire. Tel: Coventry 21784.

\section*{Short courses}

THE Engineering Technology Department of the Inner London Education Authority Paddington College is running the following short courses: "Electronics Practical" from February 25th for six weeks. This is a series of practical evenings for the construction of gadgets, projects etc. "Practical Electronics" will run for five weeks from 28th April, 1976. Students for this should have a basic knowledge of electronics and the course will cover such subjects as latest circuit designs and devices. Some of the devices will be demonstrated including a robot, HiFi unit and an electronic music maker.

Further details of the courses and application forms may be obtained by contacting the course organiser, G. D. Bishop on 01-402 6221 Ext. 55.

\section*{VHF station for Radio Tees}

THE Independent Broadcasting Authority's new VHF/ FM/Stereo transmitters at Bilsdale are now in operation on \(95 \cdot 0 \mathrm{MHz}\), carrying the programmes of Radio Tees.

Since the opening of Radio Tees on June 24 th, 1975, the programmes have been available on 257 metres ( 1169 kHz ) medium-wave. The predicted VHF service area, which covers about 680,000 people, extends from a little north of Hartlepool to about 'Shildon and Richmond in the west, southwards to a few districts of Ripon and then again northwards along the boundary of the Cleveland Hills to Redcar and including West Hartlepool, Billingham, Middlesbrough, Stockton-on-Tees, Darlington, Thornaby - on-Tees and Northallerton.

Listeners using stereo receivers are advised to use a good VHF roof or loft aerial, reasonably high, if reception is to be completely free of background hiss. It is usually well worthwhile to take extra care over an aerial intended for stereo reception.

\title{
DIITRL RERDOUT \\ 
}

The circuit shown in Fig. 8 gives regulated supplies of 5 V and 13 V . The two outputs from the trans former are full wave rectified and smoothed to give DC voltages of 8 V and 18 V . A voltage regulator, IC16, is used with transistor \(\operatorname{Tr} 5\) to drop the 18 V line to 13 V (V2). This IC has an internal reference diode and the output voltage can be adjusted with VR2. The 13 V output supplies the prescaler circuit and also the input buffer if there is no convenient supply in the tuner itself.

The 5V output (V1) uses \(\operatorname{Tr} 6\) and \(\operatorname{Tr} 7\) as a series regulator from the \(8 V\) line. The voltage reference is taken from the 13 V supply via R50 and R51. The IC has an internal current limiting circuit and R53 is used as a current sensing resistor.

Adjusting VR2 affects both the output voltages, but the supply for the prescaler is not critical and
* Formerly Texas Instruments \(\dagger\) Texas Instruments

VR2 is set to give exactly 5 V for the TTL logic circuits. Typical currents drawn by the circuits are 0.5 A at 5 V and 90 mA at 13 V .

The power supply, prescaler and display circuits are built on \(0 \cdot 1\) in pitch Veroboard. A Vero DIP board is used for the logic circuits.

\section*{POWER SUPPLY BOARD}

The power supply should be built first as it can be tested separately and then used to test the other circuits. Fig. 9 shows the layout of the Veroboard containing all the components except \(\operatorname{Tr} 7\) and the mains transformer. Tr7 is a plastic power transistor mounted on the back panel of the case and connected to the circuit board with flying leads. The layout of this board is not critical and can be changed if


Fig. 8: Circuit diagram of the power supply unit.


Fig. 9: Component layout on the power supply board. Transistor Tr7 is mounted on a heatsink.
necessary to allow for different sized components. The polarity of the electrolytic capacitors is important and should not be reversed.

When the board has been built and checked it can be tested by connecting the transformer and Tr7. For this initial test \(\operatorname{Tr} 7\) need not be mounted in the case as, under no-load conditions, it should not get hot. When connecting the transformer to the mains, the usual safety precautions should be observed and connectors to the mains side of TI should be insulated.

The outputs are checked with a multimeter and the 5 V line set by adjusting VR2. With V1 set to \(5 \cdot 0 \mathrm{~V}\), V2 should be \(13 \mathrm{~V} \pm 1 \cdot 5 \mathrm{~V}\). With this circuit working correctly the rest of the boards can be built.

\section*{components list}


\section*{DISPLAY BOARD}

The seven segment LED displays are mounted on \(0 \cdot 1\) in pitch Veroboard. Fig. 10 shows the layout. Care should be taken not to overheat the displays when soldering and a very small soldering iron is recommended. This also helps when soldering the input wires as it is very easy to bridge the tracks when a large iron is used.

\section*{LOGIC BOARD}

Because of the large number of ICs a Vero DIP board is used for the main logic board. This has supply and ground conductor tracks and also solder pads for making connections to the IC pins. Fig. 11 shows the underside of the board. Connections between the ICs are made on the top of the board with insulated wire and connections to ground or 5 V are made on the underside of the board.

The component layout is shown in Fig. 12. In the prototype IC sockets were used to make it easy to change devices. These are not essential but they do simplify fault finding.

The position of the wires is not critical, but they should be made as short as possible. The circuit is neater if the wires are all bent at right angles and routed between the ICs. To avoid wiring errors as many different colours as possible should be used.

All components should be soldered in first followed by the ground and 5 V connections (under-


Fig. 10: Component layout on the display panel. The board is viewed from the copper strip side. Note that to achieve close packing of the LEDs some of the breaks in the strips occur between holes. In the prototype 7-way ribbon cable was used to connect the LEDs to the prototype 7 -way ribbon cable was used to con
main logic board
side) and finally the component interconnections. The wiring should then be rechecked as it is very easy to make an error with so many connections. It is a good idea to mark pin 1 of all the ICs on the reverse side of the board before starting the wiring. Fig. 5 shows the pin arrangements for the ICs.

At this stage the data input pins of IC8 to 11 are connected to earth in order to facilitate testing of the board. The final setting of these inputs is determined when this circuit is connected to the tuner.

This board can be tested by connecting the displays and the power supply (V1 and GND). Tr7 must be mounted on the heatsink. With no input the displays should indicate
\[
100 \cdot 0=
\]

Note: V1 must be set to 5 V . If it is higher than \(5 \cdot 2 \mathrm{~V}\) the logic ICs may be damaged.

\section*{PRESCALER}

The prescaler circuit is also built on Veroboard, the layout is shown in Fig. 13. Because of the high frequency of operation, the components and layout are critical, in particular IC1 and \(\operatorname{Tr} 2-4\) should be the Texas devices specified. The board can be tested by connecting to the power supply (V2 and GND) and to the logic board.

The two connections to the logic board should be insulated wires twisted together and not more than 150 mm (6in) long.


A view of the internal layout of the unit showing the main logic board mounted on one side of the metal tray.


Fig. 11 : Layout of the components on the upper side of the Veroboard DIP board. In order to fit into the box the DIP board has to be cut down to the slze shown.


The reverse side of the metal tray showing the Veroboard panels holding the power supply and prescaler components.

The display should be set to 110 MHz by adjusting C9 which should vary the frequency about this point. VR1 should be set to mid position.
If a high frequency 'scope is available then a signal of between 3 and 5 V peak to peak at about 40 MHz should be seen at the emitter of Tr 4 .

\section*{INPUT BUFFER}

The construction of the input buffer will depend on the tuner. The most important consideration is to mount it as close as possible to the tuner's local oscillator circuitry. Fig. 14 shows the arrangement used with the Heathkit tuner (AJ-1214). The components are mounted on a small printed circuit board which is screwed to the top of the VHF oscillator tuning capacitor, copper side up. Components are soldered to the top of the board and the leads must be kept as short as possible.

Coupling capacitor Cl is formed by the capacitance between the copper of the PCB and the tuning capacitor. The value depends on the thickness of the PCB, the type used in the prototype giving a value of about 1 pF .
An earth connection is made by soldering a short length of tinned copper wire to the tuner metalwork as shown in Fig. 14. The 12V supply is taken from the tuner itself.
The output coaxial lead is soldered to the board and passes through a hole drilled in the back of the tuner. \(75 \Omega\) high frequency coax must be used, and a BNC type connector is soldered to the other end to connect to the display unit.


Fig. 12 : Underside wiring of the logic board. The programming pins are either connected to 5 V or GND lines according to the programming process. described in the text.


Fig. 13: Layout of the components on the prescaler board.

\section*{CHASSIS CONSTRUCTION}

The display unit is housed in an RS type 3 case. The four boards are mounted on a metal tray which also shields the prescaler circuit from the logic board. The tray is then screwed to the front panel of the case.
Assembly is quite straightforward as can be seen from the diagrams and photos. The front and back panels are supplied with the case, and the mounting tray is made from \(18 \mathrm{~s} . \mathrm{w} . \mathrm{g}\). aluminium.

Transistor \(\operatorname{Tr} 7\) is attached to the back panel as shown and the transformer is bolted to the bottom of the case. A fuse holder and coax socket are also mounted on the back panel.

Next make the interconnections between the boards. Wire lengths are not critical but the prescaler output wires should be kept as short as possible. Connections to the transformer and back panel should be long enough to let the circuitry be pulled out for adjustment while it is operating.

\section*{SETTING UP}

Assuming all the boards are operating correctly and the power supply output voltage has been set, the first adjustment is to set the free running frequency of the prescaler. This is done with the input buffer connected but the tuner switched off. C9 is adjusted until the display reads 109 MHz . VR1 is then set to give the correct input level to enable the 733 oscillator to lock over the whole of the range. The optimum level is about 250 mV peak to peak at pin 14 of IC1. If the signal is less than this the lock-in range will be reduced, and too much signal will stop the oscillator.

The simplest procedure is to switch on the tuner and set it to about 98 MHz . Starting with VR1 set fully clockwise slowly rotate the slider anticlockwise until the display locks to the tuner. When this happens the display becomes steady and will change when the tuner frequency is adjusted.

The tuner frequency is now reduced until the display indicates that lock has been lost, then VR1 is turned further anticlockwise until lock in is again achieved. This process is repeated until the display locks over the whole band. If the circuit will not lock at one end of the band, C9 can be reset so that the free running frequency is offset in that direction.

Note that although the display changes with the tuning control, the frequency displayed will not be correct as the IF offset has not been allowed for.

Although in most tuners the local oscillator is higher in frequency than the signal being received this is not always the case. If the display will not lock to the tuner at all in the above procedure then this is probably the reason. For a tuner with the local oscillator frequency lower than the signal, the frequency of the 733 oscillator must be reduced, and a 30 pF capacitor should be connected across C 9 . The above procedure should then be successful if C 9 is initially adjusted to give 87 MHz instead of 109 MHz .

\section*{COUNTER PROGRAMMING}

When the display locks satisfactorily across the band, the data inputs to the counters can be programmed.

To do this a station of known frequency is accurately tuned in and the resulting displayed frequency is noted. The difference between the displayed and actual frequency is equal to the IF frequency and will be about \(10 \cdot 7 \mathrm{MHz}\).
If the displayed frequency is below the correct value then the IF offset is equal to the IF frequency.


Transistor Tr7 is shown mounted on the inside of the rear panel (top) with the heatsink on the outside (bottom).


A wiew of the completed logic board and olisplay board fitted to the metal tray which is simply a piece of aluminium with a single bend cut to take the display board as shown.

If it is above then the IF frequency is subtracted from \(100 \cdot 00 \mathrm{MHz}\) to give the offset. In either case the number to be programmed is the IF offset frequency plus 50 kHz .


Fig. 14: The buffer board as used with the Heathkit Ad-1214 tuner. This is a small piece of printed circuit board which is screwed on top of the VHF oscillator as shown in the photograph. The shaded area indicates copper both sides of the board.

Number to be programmed \((\mathrm{D}+0 \cdot 05)=89 \cdot 35 \mathrm{MHz}\)
Each digit is converted into binary coded decimal ( BCD ) according to the following table
\begin{tabular}{ccccc} 
& D & C & B & A \\
\(\mathbf{0}\) & 0 & 0 & 0 & 0 \\
1 & 0 & 0 & 0 & 1 \\
2 & 0 & 0 & 1 & 0 \\
3 & 0 & 0 & 1 & 1 \\
4 & 0 & 1 & 0 & 0 \\
5 & 0 & 1 & 0 & 1 \\
6 & 0 & 1 & 1 & 0 \\
7 & 0 & 1 & 1 & 1 \\
8 & 1 & 0 & 0 & 0 \\
9 & 1 & 0 & 0 & 1
\end{tabular}

For the example above, the inputs to the display counters are as follows
\begin{tabular}{ccccc} 
& 8 & 9 & 3 & 5 \\
BCD & 1000 & 1001 & 0011 & 0101
\end{tabular}

Those inputs which are to be " 0 " are connected to GND and those which are to be " 1 " are connected to 5 V .

The circuit should now display the correct frequency for all stations. If the tuning indicator LED1 ( + or - ) is not quite accurate, the inputs to [C7 can be changed by one or two digits until it works correctly.

It will probably be noticed that the frequency scale on the tuner is now wrong by up to 1 MHz . This is due to the effect of the input buffer changing the local oscillator tuning. This can be cured by adjusting the trimmer on the local oscillator tuned circuit (C317 in the Heathkit tuner) until the stations return to their initial positions on the dial. It is best to choose a known station and mark its position accurately before the input buffer is connected.

\title{
PRODUCTION LINES colini riches
}

\section*{TEN-WATT PACKAGE}

Texas Instruments have announced the first of a new family of high power audio integrated circuits in a 'plastic power' package similar to the SOT 32 concept used for power transistors.


The new package has a single hole for easy attachment to the currently available standard power transistor heat sink, dramatically simplifying the awkward 'plumbing' required for comparable dual-in-line high power audios. The new format introduced by TI makes it possible to attach the audio I.C. to external metalwork of the equipment to get rid of heat outside the equipment, reducing ambient temperature in the cabinet and increasing reliability. This will be especially useful in applications where space is at a premium, for example in car radios and slim-line stereo equipment. Says Clive Hoggar, TI's Consumer I.C. Marketing Manager, "We've found the dual-in-line configuration inappropriate to the high power audio integrated circuits because of the plumbling you need to get the heat away. We'll be using this all-British 5 pin package for all our new audio circuits'.

Designated the SN76008, the new device is capable of delivering 10 watts into a \(4 \Omega\) speaker, with distortion significantly better than \(1 \%\) up to 7 watts. The circuit design incorporates on-chip frequency compensation in order to reduce stability problems, requiring only a single external capacitor for complete stability. A key feature of the design is the unique output transistors with greatly improved safe operating area for enhanced reliability under transient and overload conditions, compared with first generation audio integrated circuits.

The device was designed in the U.K. for world markets by Tl's Bed-ford-based design team, the same team who produced the U.K.'s most successful audio integrated circuitthe SN76013 series-over 5 million of which have been shipped since its introduction in 1972. Texas Instruments Ltd., Manton Lane, Bedford.

\section*{NEW C.K. PLIERS}

A new range of hand pliers has been launched by CeKa Works Ltd.

Carrying the company's 'C.K.' trade mark, the new 'Master' range of pliers comprises five individual tools: 7in. Electrician's combination plier, 6 in . Telephone plier, 6in. Wire Stripper, \(6 \frac{1}{2} \mathrm{in}\). Side cutter and an 8 in . Radio plier. Highly distinctive in appearance, the pliers have all exposed metal surfaces black phosphate anti-corrosion coated, and the handles are covered by a new design of bright yellow P.V.C. insulated safety grips.
The grips, extending the total length of the plier handles, incorporate extra large anti-slip horns, and, with a 'chunky' cross-sectional profile, enable the user to take a really positive hold of the tool.

Retail prices of the C.K. 'Master' range fall between \(£ 2.60\) for the combination plier and \(£ 3 \cdot 30\) for the side cutters.-Ceka Works Ltd., Gwynedd, Pwllheli, North Wales.

\section*{SFD WITH SM}

In case the title mystifies you, it refers to a new cassette tape from Agfa-Gevaert.

SFD cassettes are Super Ferro Dynamic, meaning they have a highly developed ferric-oxide coating, designed to give near absolute performance from recorders.
The ultra-fine iron-oxide consistency of SFD cassette tape is free from dentride particles and is of a very high density with excellent magnetic orientation.

Prices are: SFD C60: \(£ 1 \cdot 08\) RRP inc VAT. SFD C90: \(£ 1 \cdot 40\) RRP inc. VAT. SFD C120: \(£ 1 \cdot 94 \frac{1}{2}\) RRP inc. VAT. Agfa-Gevaert Limited, 27 Great West Road, Brentford, Middlesex. Tel. 01-560 2131.


\section*{RF POWER TRANSISTORS}

Intended for operation at 225 MHz , a new pair of transistors introduced by Motorola will produced 13W output and will provide a minimum gain of 9 dB with collector efficiencies of \(50 \%\). The new transistors are the MRF225 (driver) and the MRF226 (power output) and are designed for use with a 12.5 V collector supply.

A v.s.w.r. of up to \(20: 1\) at any phase angle will not damage MRF226. Motorola Ltd., Semiconductor Pro. ducts Division, York House, Empire Way, Wembley, Middlesex.

\section*{FREE SOLDERING IRONS}

A special Heath offer is aimed at first-time kit builders. The company has long felt that the one tool the first-time kit builder does not have is a soldering iron. Heath's offer gives that constructor a free soldering iron worth \(£ 3.50\) with his first kit purchase of \(£ 30\) or over. The offer is being made by sending to Heath and enclosing a voucher obtained from every enquiry catalogue they or their shop send out. Whilst this offer runs, every voucher will have a life of six to eight weeks. Don't forget also that the Heathkit organ is on show at the Tottenham Court Road shop. Heath (Gloucester) Limited, Gloucester, GL2 6EE.

\section*{NEW FROM UNI-COM}

Uni-Com Electronics Ltd., introduce the Weltron 2004 AM/FM stereo radio combined with a stereo cassette recorder.

This unit will operate on 240 mains or a 12 V battery supply. There is a power input socket to accept a supply from a battery in a car with a negative earth chassis. The radio has three wavebands, MW, LW and FM with stereo radio reception. There is a built-in aerial for LW and MW and a telescopic aerial for FM.

The full range of controls include push-button wave change and on/off; finger-tip tuning facility; slider controls for each speaker for stereo balance; fast forward/rewind; cassette eject button; cassette pause and record buttons; microphone volume control and a recording level indicator.

The 2004 weighs only 15 lbs and doubles as a portable unit with a flush fitting carrying handle. Finished in white this unit is also available with 8 -track cartridge in place of cassette. Price: \(£ 131 \cdot 50\) plus VAT. 36 Clarges Street, London W1.

\section*{EQUIPMENT HOUSINGS}

West Hyde Developments Limited are now offering a range of equipment housings in 28 different sizes.

This range is available ex-stock from Northwood. The fixing screws are inside the cabinet, but outside the enclosure, having the advantage that there are no ugly brackets for mounting.

In addition to the high impact strength of the blue/grey self-extinguishing polycarbonate, it also has a high temperature resistance up to \(140^{\circ} \mathrm{C}\). The cover retaining screws are captive and made of stainless steel. The insides of the case have pads for mouting chassis etc., with screws provided. The sealing gasket is recessed so giving protection whilst the lid is removed. The gaskets are oil, petrol and water resistant.


The smallest case is only \(35 \mathrm{~mm} \times\) \(55 \mathrm{~mm} \times 50 \mathrm{~mm}\) and the largest case is \(360 \mathrm{~mm} \times 200 \mathrm{~mm} \times 150 \mathrm{~mm}\) and two of the sizes are available with clear covers. (For quantity, all sizes are available with clear covers.) Prices vary from 75p up to \(£ 9 \cdot 00\) according to size and quantity. West Hyde Developments Ltd., Ryefield Crescent, NORTHWOOD, Middlesex, HA6 1NN.


\section*{VARIWIPE}

Scientronics announce their new car windscreen wiper delay timer kitthe Variwipe.

It consists of a single Printed Circuit Board, \(50 \mathrm{~mm} \times 63 \mathrm{~mm}\), with a maximum of four connections. It mounts by means of a single hole behind the car's dash.


Variwipe ST version


Variwipe \(D T\) version.
Once installed the Variwipe is controlled by a single knob. Turned fully anticlockwise this switches the Variwipe off. Turned clockwise the Variwipe switches on and the wiper gives an immediate wipe. The Variwipe is now set to maximum delayabout 50 seconds. Turning the control clockwise reduces the delay so that, at their fastest, the wipers pause for only a couple of seconds between wipes.
Construction is simple: the instructions give full pictorial layout diagrams and full circuit and installation details.

There are two versions: the "ST" for the older car which uses a single throw control switch (with two wires) for the motor. Price is \(£ 4 \cdot 98\) including V.A.T., postage and packing; The \(D T\) version for those cars which use a changeover switch, which has three wires. Priced at \(£ 5.98\) including V.A.T., postage and packing, this version is also suitable as a replacement for the ST version.

The Variwipe is covered by the customary one year free parts and labour guarantee, but Scientronics also offer an immediate refund on any kit should the user decide he does not wish to keep it. Scientronics also give a fixed, small charge service on units outside guarantee. Scientronics, 40 High Street, Somersham, Huntingdon, Cambridgeshire PE17 3JA. Telephone Somersham (048 74) 321


\section*{Elderly digit}

To celebrate my 72nd birthday I made a crystal-digital watch with press-button readout which I fitted into a silver pocket-watch case older than myself! It works perfectly, showing hours and minutes on one button and date and seconds on another. It keeps time to a second a day without final adjustment.

I wonder if \(I\) am the first amateur to make one of these watches as well as his own coherer and coils to receive ship's Morse signals in the earliest days of wireless?

The magic of making calculators has now faded with the construction of a CT7001 clock calendar and now this MK5031 watch, which incidentally, had to be fitted into a pocket-watch case because I had to use discrete transistors and a \(1_{8}\) in display which can be read easily without a magnifier.-E. W. Baigent (High Wycombe)

\section*{Armchair Tele-Tennis}

Last year I built a PW TeleTennis unit which has proved very popular with the family. However everyone agreed that it would be far better if the unit had remote bat and serve controls. In the original circuit each remote-control box would need a 6 -way connecting cable (5V, OV, S2a or S3a, 2 for S2b or S3b and one for batcontrol slider). I realised that greater neatness and economy would be achieved if 4-core screened cable could be used connected to 5 -pin DIN plugs. I therefore used the following circuitry which I thought might interest you. No extra IC's were needed as sufficient gates were left un-
used in the original circuit. This circuit allows only one lead to be used in an extension unit for S2 or S3b in addition to the four for \(5 \mathrm{~V}, \mathrm{OV}, \mathrm{S} 2 \mathrm{a}\) or S3a, and bat-control.

When neither serve button is pressed 1's appear at all inputs of gates A and B. Hence 0's appear

at both C's inputs and a 1 must appear at input 2 of gate \(D\). Therefore pulses from IC28, point 6 on board \(D\), having been inverted by gate \(E\) are again inverted by gate \(D\). These reach point 5 just as they would have done in the original circuit.

When a serve button is pressed, a 0 is forced to appear at input 2 of gate \(D\) thus preventing a 0 at point 5 (the whole point of the exercise). Gates A and B act as mixers to prevent shorting of the supply rails when one serve button is pressed and the other is not. In this way, common 4-way screened cable may now be used from the main unit to each of, say, two AB7 boxes each housing a batcontrol slider and a DPDT pushbutton switch connected thus:-


If the original controls on the main unit are to be kept, they must be switched with those on the extension unit through a 6 .
pole 2-way push-button switch (3 poles for each extension unit, the power rails being permanently connected to the DIN sockets).

This addition has proved very successful and means that we can now play Tele-Tennis from the comfort of our arm-chairs at a reasonable distance from the screen ( 3 m .) while the UHF lead to the TV remains short. Thank you for the excellent Tele-Tennis project.-Jeremy Lovell (Winchester).

\section*{Take your choice}

It's interesting to hear from fellow enthusiasts continued partisanship regarding valves and transistors. It reminds me of the 35 mm versus roll film camera controversy which raged some years ago in the correspondence columns of photographic magazines. Surely the simple answer must be to use whatever is most appropriate to the job in hand!

Unquestionably, transistors must be first choice when space is limited and available power restricted. Car radios and portable sets are two obvious examples. Turning to domestic equipment such as table nadios and televisions, ample power is available from the mains, and the overall size is likely to be governed by the dimensions: of the loudspeakers, record changers, picture tubes, etc., rather than the chassis. In this case the use of easily replaceable valves is surely better from the owner's point of view. There is, for instance, a well known make of unit audio languishing in my workshops for lack of an amplifier module. It has been there for a month already; had it been valved I could have had it repaired long ago. It's significant to note that the same manufacturer has reverted from transistors to the good old PCL82 in the sound output stage of his colour televisions! Speaking of which, my own fully transistorised set blew its line output transistor last week. Not only was the replacement dearer than the equivallent valve, it took a lot longer to fit! Nevertheless, I would hate to have valves in the umpteen portable radios used in my household. You pays your money and you takes your choice! -Charles Miller (Uttoxeter).


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\hline \(128{ }^{38} \mathrm{p}\) & AF173 & 25 p & BD115 & & GET & 18p & 0 & & AA1 & 14 p \\
\hline C128 20 p & AF239 & 45p & BD131 & & GET1 & 28p & & & & \\
\hline AC131 15 p & AD149 & & BD13 & & & & & & ba1 & \\
\hline AF118 35p & AD161/ & & BD & E1.05 & & 59p & OC169 & & & \\
\hline AF14 35 p & 162 & 98p & BF115 & 32p & & & OC200 & & OA & \\
\hline AF115 35p & ASY3 & 研 & BF159 & & OC26 & & 2N404 & & & \\
\hline AF116 32p & BC107 & 18p & BF195 & 23p & OC28 & & 2N706 & 48p & OA200 & \\
\hline AF117 32p & \({ }^{\text {c }}\) & 18p & BF197 & \({ }^{23} \mathrm{p}\) & & & 2N708 & & SXI/6 & \\
\hline AF124 55p & \(\mathrm{BC}^{\text {BC12 }}\) & 30 p & BF258 & 805 & - & & 2N1302 & & & \\
\hline AF126 \({ }^{\text {AFP }}\) & BC143
\(\mathrm{BC1} 47\) & 30p & \({ }^{\text {BFF194 }}\) & 30 p & - & & \(2 N 1090\)
2 & & & \\
\hline AF139 45 & BC148 & 18 p & BFi73 & \({ }_{28}{ }^{\text {p }}\) & OC46 & & 2N3054 & & DIOD & \\
\hline ACY17 30p & BC149 & 18p & BFY50 & 30 p & OC70 & & 2N3055 & & BY100 & 22 p \\
\hline ACY18 30p & BC157 & 20p & BFY51 & 30p & OC71 & & 2N3133 & & BY12 & \\
\hline ACY19 30p & BC158 & 20 p & BFY52 & 30 p & OC74 & 25p & 2N3773 & & IN4006 & \\
\hline CY20 30p & BCY32 & 28p & BSY84 & & OC81 & 20p & & & 40 & \\
\hline
\end{tabular}

\section*{Tele-Tennis- \\ more mods!}

I have just read the letters page and am prompted by a letter from A. O'Brien (Sunderland) describing how he has altered his PW Tele-Tennis.

I have altered mine in a similar manner, except, that I now have two extra games, one I call 'Holein the wall' and the other 'Squash'.

To play 'Hole-in-the-wall' I connected 'Right Bat Vertical Out' from Board C to pins 1 and 2 on ICI9 (SN7400) and to a new switch on the front panel as shown in Fig. 1. The output from pin 3 of ICI9 is also taken to the switch. The output from the switch is connected to pin 9 on board B (Right Bat Vertical In).

To play Squash though, required a further three sets of contacts. This is because we need to move the right bat from the right base to the left base, to prevent contact between ball and right base from blanking the ball out, and finally to make the ball change direction when it hits the right bat in its new position, Fig. 2.

To make the right bat appear on the left hand side I connected a wire from the link between ICIO pin 8 to ICI5 pin 4 , ie the \(o / p\) from the left bat width generator, to the third position of the switch. The \(o / p\) from the right bat width generator is connected to the first two connections, this is done by removing the link between ICI2 pins 1 and 2, and ICI5 pin 1, and replacing it with two pins. ICI2 pins 1 and 2 are connected to the first two connections of the switch, the \(o / p\) of the switch is connected to the other pin, ie ICI5 pin 1. So in fact what we have done is to use the left bat width generator as our right bat width generator when we are playing 'Squash'. This effectively moves the right bat over to the left hand side without affecting its vertical position.

To prevent the ball from being blanked when it hits the right base, the connection between IC26 pin 12, board D and IC28 pin 1 must have a switch in it. I did this by removing the link between these two points and replacing it with two pins. The pin connected to IC28 pin 1 is connected to the \(0 / p\) of \(S 5 C\) on the front panel. The other pin is then connected to the first two connections of S5C and the other is left continued on page 662


Fig. 1: top, modifications for playing 'Hole-in-the-Wall' while Fig. 2 : above, indicates alterations required for 'Squash'. Fig. 3: left, circuit to prevent ball blanking at right base. Fig. 4 : below, circuit to get the ball 'bounce' correct with 'Squash'.



ELECTRONICS-AN ELEMENTARY INTRODUCTION FOR BEGINNERS (SI Units)
By L. W, Owers, C.Eng.\& MIERE
Published by Publication Mailing Services, P.O. Box 6, Crawley, Sussex, RH10 6LH.
119 pages \(20.50 \mathrm{cms} \times 15 \mathrm{cms}\).
Price £1 45 (includes post \& packing)

ABASIC guide to electronics for those meeting the subject for the first time. It has an essentially nonmathematical approach and where possible, the information is given in diagrammatic form. Where simple formulae and units are mentioned SI units are used.
An easy-to-understand explanation is given of static electricity, the fundamental particles, atoms, energy, waves, the elementary physics of conductors, insulators and semiconductors, and the laws of current electricity. Types of conductors, resistors, capacitors and inductors and their applications are also dealt with. The concluding chapters are devoted to valves and semiconductor devices and their applications including radio, television, colour TV, etc.

\section*{TOWERS' INTERNATIONAL TRANSISTOR . SELECTOR}

By T. D. Towers
Published by W. Foulsham \& Co. Ltd., Yeovil Road, Slough, Bucks., SLi 4JH.
142 pages \(29.5 \mathrm{cms} \times 21 \cdot 5 \mathrm{cms}\).
Price \(£ 2.95\)

THE preface states, quite accurately that, if you deal with transistors-whether as a student, a hobbyist, circuit engineer, buyer, teacher or serviceman-you will often want data on a specific transistor of which you only know the type number. Specifications apart, you may want guidance on a readily available possible substitute. This transistor compendium, a comprehensive tabulation of basic specs. for over 10,000 transistors, offers gen on ratings, characteristics, case details, terminal identifications, applications use, manufacturers and substitution equivalents (both U.S. and European).

More than ten thousand transistors are covered in this compendium which comprises a selection of the more common current and widely used obsolete types.

\section*{110 OPERATIONAL AMPLIFIER PROJECTS FOR THE HOME CONSTRUCTOR}

\section*{By R. M. Marston}

Published by Newnes-Butterworths; The Butterworth Group, 88 Kingsway, London, WC2B 6AB.
123 pages \(21 \cdot 75 \mathrm{cms} \times 14 \mathrm{cms}\).
Price £2-80. Limp edition \(£ 1.80\)
F you have 1108 -pin D.I.L. 741 s then this is the book for you! Chapter 1 discusses the basic principles and applications of the 741 Op Amp. Chapter 2 contains 25 AC and DC amplifier projects, Chapter 3, 25 instrumentation projects, Chapter 4, 20 oscillator and multivib. projects and Chapter 5, gives 20 sound generator and alarm projects. The final chapter contains 20 relay-driving switching projects.

\section*{WTRODUCING ELECTRONIC SYSTEMS}

By lan R. Sinclait, B.Sc., MIEE, A. Inst. P
Published by Fountain Press, Argus Books Limited, Station Road, Kings Langley, Herts.
103 pages \(21.50 \mathrm{cms} \times 14 \mathrm{cms}\).
Price \(£ 1\) - 50

AS Mr. Sinclair says in his preface, this is a book for the beginner, and it deals, not with the theory of electronics nor with the nuts and bolts of circuits, but with 'systems'. It describes how electronic circuits are used to bring about the results which we see, and not with the details of the circuits which are used. It is as if the author were describing the action of a car-but not showing the construction of each component.

If you have ever wondered how radar works, what was involved in colour television, how electronic calculators can carry out their tasks; this book is meant for you. No previous knowledge of electronics or electricity is assumed but Chapter 7 on analogue computing does need some appreciation of algebraic equations. This is most certainly a book for those with an inquiring mind.

\section*{ELECTRONIC MUSICAL INSTRUMENTS By Norman Crowhurst \\ Published by Foulsham-Tab Limited, Yeovil Road, Slough, Berks. \\ 118 pages \(21 \cdot 5 \mathrm{cms} \times 14 \mathrm{cms}\). \\ Price £1-80}

THE first chapter of this book discusses the characteristics of orchestral and band instruments-strings, woodwind, brass etc., the types of sound produced and the part played by electronics in the musical world. The amplification of traditional instruments is discussed in Chapter 2 and other chapters are devoted to such items as electronic modifyers, fully electronic instruments, amplifiers and speaker systems, synthesisers, and troubleshooting.
If you contemplate purchasing this book, bear in mind that it was originally written for the U.S. market and some things may seem a bit strange to the English reader.

\section*{LETTERS}
-continued from page 661
open. See Fig. 3. Now when S5 is switched to its third position the right base signal is removed from IC28 pin 1, so preventing the ball being ball blanked on contact with the right base.

The only thing left to do now is to ensure that the ball will bounce off the right bat when the right bat is on the left hand side of the screen. To do this we have to connect the 'right bat in' to IC26 pin 1 when we are playing squash. Otherwise the signal from IC26
pin 8 will try to change the state of the flip-flop, IC27 A and B to that which causes the ball to travel from right to left across the screen. As the ball will already be travelling in this direction it will pass straight through the bat, and will be blanked out due to its contact with the left base. But by connecting it to IC26 pin 1 and removing it from IC26 pin 13 it will appear as a second left bat signal to IC26 and so the flip-flop will change its state causing the ball to go from left to right.
This is achieved by removing the link wire between pin 8 on
board \(B\) and pin 13 on board \(D\). A lead is then taken from pin 8 board \(B\) to the \(o / p\) of \(S 5 D\) and another lead is used to connect pin 13 on board \(D\) to the first two connections on S5D. Finally a lead is taken from pin 12 on board \(B\) to the third connection of S5D so that in the third switch position right bat is connected to IC26 pin 1. (See Fig. 4).

I hope you will be able to print this letter as I am sure someone else would be interested in modifying an already absorbing project.-P. J. Morris (Enfield).


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IN the past the most popular band for local contacts and the means whereby one began to learn about amateur radio, was Top Band. With the increasing proportion of \(\mathrm{G} 8+3\) callsigns 'two metres' has largely replaced the lower frequency. Readily available and easily modified commercial equipment has resulted in a new group of "black box" operators sufficiently knowledgeable to modify their equipment, erect an aerial and operate a micro phone. They don't experience however, the pleasure of making something from scratch, or getting the bugs out of their equipment with the help or other local amateurs. This transmitter is recommeded for bringing back some of the adventure of Top Band, and to give the beginner the same delight that the writer had when he made his first contact.

The transmitter to be described takes advantage of two facts. Firstly, two metres are remarkably penetrating, bearing in mind that on Top Band 10 W was essential to get across town in comfort, while on \(2 \mathrm{~m}^{1}{ }_{2} \mathrm{~W}\) will do the same job with greater efficiency. The second fact is that AM is expensive, consumes unnecessary power and goes through the front end of the average TV like a hot iron through solder. This transmitter employs FM to which TV sets and high-fi equipment is relatively insensitive, and has the additional advantage that VHF aerials can be physically small, or simple construction and can even be used inside the shack. Furthermore
they give considerable gain, for the six-over-six slot used by the writer multiplies the 1 W produced by this transmitter by over ten times.

A single watt on VHF gives all the contacts one made on Top Band, and the DX is there, for when tropospheric openings appear the Continent is wide open to the skilled operator. From the constructors point of view, VHF has many advantages. At low powers, transistors and small components can be used as no large power is involved and coils are equally small and easily made. Experience shows that for local working, up to 30 miles, this transmitter is fully the equal of a much more powerful 160 m one using ten watts.

This transmitter puts between a half and one watt into the aerial, runs off a 12 V battery, is FM, and can be operated with a crystal or VFO. Particular attention has been paid to the spectral purity of the signal and, correctly adjusted, harmonics should be better than 45 dB down. The input accepts both crystal and dynamic microphones and the output can be fed into a 50 to \(75 \Omega\) aerial with a very close match. Furthermore it can be operated into an infinite SWR load, that is short or open circuit, for a brief period without destroying the output transistor, also, being phase modulated converted to frequency modulation, over-deviation is unlikely.

FM can be achieved by two methods, the simplest being the use of a varicap diode across the crystal or VFO. This method calls for little additional circuitry but has the disadvantage of the possibility of overdeviation, that is more than the \(\pm 2.5 \mathrm{kHz}\) used in this country. Because the capacity variation with voltage is not linear the deviation can be asymmetrical resulting in more power in one set of sidebands. The second method is by the generation of a stable carrier frequency which is then phase modulated and converted into FM by trimming of the AF reponse. Phase modulation causes an increase in deviation not only with amplitude but also with rising AF so that audio amplifier has to have a falling characteristic. The advantages are that overdeviation is almost impossible, deviation is symmetrical and resolution on simple slope detection is a little easier than with pure FM. For these reasons phase modulation was adopted for this transmitter.

Phase modulation calls for a low fundamental frequency if adequate deviation is to be obtained at 144 to 146 MHz so \(8 \cdot 0\) to \(8 \cdot 1 \mathrm{MHz}\) was chosen requiring a \(\times 18\) multiplier chain to reach the operat-
ing frequency. Conventional transmitters employ bi-polar transistors operating in class \(C\) in the multiplier chains, but they have considerable disadvantages. The input impedance is very low, and they are driven by current rather than voltage. This absorbs power from the preceding circuit, so that careful matching into the preceding stage is required if the \(Q\) of the stage is to be maintained and the amplification of unwanted harmonics avoided. Though not as efficient, FET's overcome these difficulties, as they operate well in class \(C\) for harmonic generation at very low currents and because of the high input impedance, are voltage driven. Therefore the \(Q\) is maintained, unwanted harmonics suppressed, but giving selective amplification to the desired frequency.

The output from the multiplier is another FET and runs at 10 to 20 mA feeding a conventional driver and power amplifier.

\section*{MODULATOR CIRCUIT}

A high impedance input is provided by \(\operatorname{Tr} 1\) and Cl Fig. 1 though not essential, isolates the microphone while R1 and C2 constitute an RF filter, and the gate of Tr1 is earthed by R2. This resistor is not critical and any value over \(50 \mathrm{k} \Omega\) suffices. Trl is an impedance changer giving current amplification only,


Fig. 1: Circuit of the Modulator section. C5 trims the audio output while R6 and R7 decouples the audio amplifier from the phase modulator.
with a voltage loss of \(30 \%\) or more. VR1 in the source lead of Trl varies the audio output and thus the deviation, source following into the base of \(\operatorname{Tr} 2\) via C3. Tr2 supplies voltage gain, and by connecting the top of the bias chain to the collector, a measure of feedback is provided, limiting the gain to about 100 times. R8 and C5 decouple the modulator on the power supply side and R7 and C6 keep RF from the output of the modulator. R6 and C4 add the final tailoring to the circuit to provide the required falling characteristic to the audio response. The current consumption of the modulator is about \(500 \mu \mathrm{~A}\).

\section*{CRYSTAL OSC, VFO AMP AND PHASE MODULATOR}

These stages are voltage stabilized by D1 and R13 Fig. 2. The crystal oscillator is the Pierce configuration, the crystal being connected between gate and
components list
\begin{tabular}{|c|c|c|}
\hline \multicolumn{3}{|l|}{Resistors} \\
\hline R1 \(47 \mathrm{k} \Omega\) & R14. & 100k \(\Omega\) \\
\hline R2 50kR & R15. & \(2 \cdot 7 \mathrm{k} \Omega\) \\
\hline R3 820k & R16 & 1000 \\
\hline R4. 150 k ? & R17 & \(100 \mathrm{k} \Omega\) \\
\hline R5 . 47 k R & R18 & 3.3k \\
\hline R6 10k & R19 & 1005 \\
\hline R7 10k3 & R20 & \(2 \cdot 7 \mathrm{k} \Omega\) \\
\hline R8. 1500 & R21 & \(2 \cdot 2 \mathrm{k} \Omega\) \\
\hline \(\mathrm{R9}\). \(47 \mathrm{k} \Omega\) & R22 & \(100 \Omega\) \\
\hline R10:: 100k & R23 & 100kS \\
\hline RH1 2.7kS & R24 & 478. \\
\hline R12: 2.2 k Q & R25 & 1002 \\
\hline R13 330n & VR1 & \(10 \mathrm{k} \Omega\) veri. preset. \\
\hline All resistors \({ }^{\text {W }}\) W\% & & \\
\hline \multicolumn{3}{|l|}{Capacitors} \\
\hline C1 10 nF & C17 & 4.7 nF \\
\hline C2. 470pF & C18 & 4.7 nF \\
\hline C3 100 nF . & C19 & .10pF \\
\hline C4. 20 nF & C20 & 15 pF \\
\hline C5: 10aF (16v) & C21 & 4.7 nF \\
\hline C6 1nF & C22 & 4.7nF \\
\hline C7. 100 pF & C23 & 6.8 pF \\
\hline C8. 5.6 pF & C24 & 1.8 pF \\
\hline C9 - 4.7 nF & C25 & \(4 \cdot 7 \mathrm{nF}\) \\
\hline C10: 47pF & C26 & 22pF \\
\hline C11. 4.7 nF & C27 & 4.7 nF \\
\hline C12. 4.7 nF & C28 & 33 pF \\
\hline C13 \(4 \times 7 \mathrm{nF}\) & C29 & \(4 \cdot 7 \mathrm{nF}\) \\
\hline C14 82pF & C30. & 10 pF \\
\hline C15 : 4.7nF & C31 & 33 pF \\
\hline C16 100pF & & \\
\hline
\end{tabular}

Apart from \(\mathrm{C}_{5}\) all capacitors are high-K ceramics Erie ceramicons, or Mulatéd.
VC1, 3, 4and 5: 5 -60pF, plastic lnsulated Mullard
VC2
2-10pF, plastic insulated Mullard
Semiconductors
\begin{tabular}{|c|c|c|c|}
\hline Tı1 & 2N3819 & Tr10 & 2N4427 \\
\hline Tr2 & BC169C & & \\
\hline Tr 3, & 5,6,7,8 & D1 & 9.1 Volt \\
\hline & 2N3819 & & Zener \\
\hline Tr9 & BSX20 & D2 & 1N4000 \\
\hline
\end{tabular}

\section*{Inductors}

L1. 9 turns stretched to 10 mm
L2 . \(6 \frac{7}{2}\) furns stretched to 6 mm
L3. \(4 \frac{4}{2}\) turns stretched to 5 mm
These cofls wound on a No. 15 drill: mounted on 4 mm formers, using \(24 S W G\) enamelled copper wire.
44 and 45.5 tums stretched to 8 mm wound on a No: 13 drill using 22SWG enamelled copper wire.
16 and \(L 7,5\) turns stretched to 10 mm ; wound on a 6 mm drill, using 20SWG tinned copper wire.
RFCA \(33 a \mathrm{H}\) or higher
RFC2, 3, 5 and 6 2者 turns \(225 W G\) enamelled wire on FX115 ferrite bead
RFC4 5 turns closewound on a No. 13 drill using 22SWG enamelled wire (at a 2 N 4427 is used for Tho, fewer turns may be required).

\section*{Miscellaneous}

Tr9 heat sink, \(10 \times 22 \mathrm{~mm}\), one end rolled on a 5 mm dril. Trio heat sink, \(12.7 \times 14.3 \mathrm{~mm}\) star shaped type. Screens made from th-plate \(38 \times 13 \mathrm{~mm}\) bent into three sides of a square, and \(45 \times 13 \mathrm{~mm}\) bent approximately at the centre. Die-cast box \(114 \times 64\) \(x 30 \mathrm{~mm}\) Eddystone or Doram: \(1 \times 5 \mathrm{~mm}\) double sided copper clad fibre-glass board \(104 \times 49 \mathrm{~mm}\). Two coaxial sockets. Thiee 4 mm : stand-off bushes. HC6U crystal socket Two small inF feedthrough capacitors \(8 \times 0\) to 8.11 MHz crystal.


Fig. 2: Crystal oscillator/VFO amplifier, and phase modulator circuit. D1 and C11 are for voltage stabilization.
drain so that removal leaves the gate free for VFO input when Tr3 acts as an amplifier. VCl is used to pull a crystal to a specific frequency and makes little difference to the VFO. RFCl blocks the signal from Tr3, passing it via C7 to the gate of Tr4, the phase modulator, whose load is R12. The output goes through C10 to the multiplier chain, and feedback through C8 induces phase modulation, the audio signal being applied to the gate of \(\operatorname{Tr} 3\), IV \(\mathrm{p} / \mathrm{p}\) being required by the phase modulator.

\section*{MULTIPLIER CHAIN}

Transistors Tr5, Tr6 and Tr7, Fig. 3, are tripler, tripler and doubler respectively, with identical circuitry save for the necessary changes in coil and capacitor values required to resonate on the harmonic frequencies. All run quiescent currents of about \(500 \mu \mathrm{~A}\), increasing to \(1.5 \mathrm{~m} A\) when RF is applied, thus running in Class AB . Because of the high input impedance of the FETs, the output may be taken
from the drain, avoiding the need for taps on the coils, the loading being minimal. This keeps the circuit Q high so that tuning of the coils is fairly critical. The output tuning to the power amplifier is particularly sharp and VC2 requires very careful adjustment for the best results. A small screen is necessary around L4, to avoid feedback to L3 which causes spurious oscillation and reduces the efficiency of the stage. R24 provides a current limiter and voltage feedback to Tr8.

\section*{DRIVER AND POWER AMPLIFIER}

These stages operate in class C , the input to Tr 9 , Fig. 4, being tuned by L4, VC2 and C26, the two capacitors providing an impedance match into the base of Tr9, RFC2 being the DC return. The total dissipation of \(\operatorname{Tr} 9\) with a good multiplier chain and active crystal can rise to 300 mW so that a small heat sink is required. Tr10 is of overlay construction, the input impedance is very low and capacitative, while C28 and VC3, tune L5 and provide an impedance match into the base. RFC4 compensates for the input capacity and RFC5 is the DC return. As Tr10 dissipates up to \(2^{1}{ }_{2} \mathrm{~W}\), an efficient heat sink is required. RFC6 blocks RF' so that the collector load becomes the output circuit consisting of VC4, C30, L6, C31, L7 and VC5. The screen around L7 and VC5 considerably reduces the harmonic content of the output and should not be omitted.

\section*{CONSTRUCTION}

The circuit is constructed on double-sided copperclad board, Fig. 5. and it is recommended that the components and the instructions be followed precisely. Every earth point is taken to the top side of the board, all leads are made as short as possible, and the longer lead of coils and resistors being made earthy. The coils should be wound on the appropriate drill and then forced on the former after being correctly spaced, finally being held in place with a very light coat of epoxy resin adhesive.

wo 82
Fig. 3: Diagram of multipller chain and output to power amplifier. For Netting, power is applied to the junction R19/D2. D2 blocks this supply to the power stages.


Fig． 4 ：Circuit of the driver，power amplifier，and output sections．An efficient heat sink is required for Tr10，as up to \(2 \frac{1}{2} W\) needs to be dis－ sipated．

Coil slugs should be held in place with a dab of wax．

All holes on the topside should be countersunk except for the earth connections，using a suitable drill．Construction is started by clamping the board in the die－cast box and drilling the fixing holes through both．Then assemble the components，Fig． 6 ，from the long axis outwards，soldering the screens in place at an early stage before too many components accumulate around them．It is also wise to turn the board over，clamp it to the lid of the box and drill through the centre point of the variable capacitors and coils with a No． 60 drill．These should be enlarged to 6 mm to allow access to the com－ ponents for final tuning purposes when boxed up． The heatsink for \(\operatorname{Tr} 10\) is commercial，but that for Tr 9 is made by bending a 12 mm square of copper or tinplate around a 5 mm drill shaft and then forcing it on the transistor．

\section*{SETTING UP}

As usual，check the board very carefully for solder bridges and a scrub with an old toothbrush is worth while before applying power．It＇s a wise move now


Fig，bi Foil side view of the PCR shown fullstie．The holes for the 4 mm formers should he bored with；No； 2 otrin，whele those for the variable capacilors should be made with a bmm ormi．


Fig．6：Component side view of PCB drawn about 1⿳亠口冋⿱⿰㇒一乂⿳亠二口丿 times full size．All holes on the earthy side should be countersunk to provide an electrical ＇clearance＇for the components．

to get the transmitter working, before fixing it into the case, so temporary connections should be made to input, output and crystal connections. A suitable meter must be connected in the supply line, including a \(470 \Omega\) resistor to limit current flow should a short exist. Having taken these precautions the output is fed to a 50 to \(75 \Omega\) screened dummy load through a suitable power meter.

\section*{RF SNIFFER}

Without a crystal, apply 12 V and check that no more than 15 mA flows, to the audio stage, oscillator, phase modulator, zener and quiescent multiplier stage. More current indicates a faulty device, or just possibly that Tr8 is oscillating, best revealed by an RF 'sniffer' near L4, and cured by adjusting VC2. If all is well turn to the modulator and using a very high impedance meter, check that the voltage on \(\operatorname{Tr} 2\) collector is half the supply voltage as measured on the supply side of R19. If higher, increase the value of R 4 until the correct reading is reached, and vice versa. For perfection those with an audio generator and oscilloscope can change the value of C6 until there is a 3dB. drop in voltage output at 3 kHz compared with 1 kHz . This represents the optimum roll off for good frequency modulation, the measurement being made on the gate of Tr4.

Now plug in a crystal and check that there is a rise in current consumption, which, for the sake of the output transistor, should be optimised by adjusting VC4 and VC5. The multiplier chain should now be set up using an absorption wave meter to ensure that the circuits are on the correct harmonic frequency. Alternatively, tune the slugs for maximum output with a sniffer, or for maximum current consumption, as this still puts the circuits on the correct harmonic. VC2 should be adjusted with a sharpened plastic knitting needle, for maximum current consumption. Then adjust VC3 which will reflect on VC2 which will then require readjustment. VC4 and VC5 should now be adjusted, looking for maximum RF output and minimum total current consumption.

It is well worth while repeating all the adjustments for all reflect on one another. The final result should be between 0.75 and 1 W into the dummy load for a total current consumption of about 300 mA .

If an SWR meter is available the unit may now be connected to an aerial using a crystal on a clear frequency and final adjustments of VC4 and VC5 made to achieve optimum output for minimum SWR. No change in output should be seen when the transmitter is modulated. For those with a good absorption wavemeter, a loop pick-up from the output coil should show that all harmonics and spurii are better than 45 dB down on the fundamental, and further improvement on this figure can be made using such a wavemeter by readjustment of the variable capacitors. Once a satisfactory performance has been obtained the unit may be fixed in the diecast box and all the adjustments repeated until the same figures are obtained.

\section*{NOTES}

VR1 controls the audio amplification and thus the deviation and without very sophisticated equipment is best set by on-the-air testing. Any crystal between \(8 \cdot 0\) and \(8 \cdot 11 \mathrm{MHz}\) may be used, although if full coverage of the two metre band is envisaged, a compromise must be reached between output and band coverage. Because the \(Q\) of the multiplier chain is high, very careful adjustment of the coils is required. VC2 must be maximised to the centre of the band, but fall off of power is inevitable at the band edges if full coverage is to be achieved. The transmitter, frankly, is happiest when covering 1 MHz rather than the whole 2 MHz of the band. This proves to be no real disadvantage for all local operating and fits in with the band plan for 2 m . The crystal socket may be used as the input for a VFO, as it is high impedance and 2 V RMS is more than sufficient. For netting, power is applied to the earlier stages, blocking the supply to the output, but conducting on transmit passing a supply from the power to the earlier stages of the transmitter.

\section*{ON RECENT DEVELOPMENTS}

\section*{DIAL-A-COMPUTER}

Most people use the telephone in a social sense for talking with a friend located at a distant point. How about ringing up and having a chat with a computer? it hasn't quite reached that stage yet-but in the US a company has built a small viewing set which permits one to read out data which has been put into the computer. The subscriber with access to the computer uses a push-button type telephone and the viewing terminal (it's quite small, only weighing about 4.5 kg .) which stands next to the telephone completes the system. The user receives a special recognition tone to inform when the telephone is connected to the computer and data can then be entered into the computer using the ordinary numbered push-buttons which would otherwise be used for dialling. Data which is entered comes up on the viewing screen and will remain there until it is erased. The cost isn't too high, either. Initial rental is just \(\$ 30 /\) month in the US. It will probably be some time before anything like this gets established in the UK.

\section*{SAVE IT!}

1 confess to being impressed with the approach adopted by one large European electronics concern regarding the conservation of energy. Together with the German Federal Government the company has built an experimental house. The usual commercial electricity supply is used for lighting, cooking and the usual appliances such as washing machine, fridge and carpet sweeper, etc. All the energy for household heating, however, is supplied from the ever smiling sun. A mini-computer installed in the house simulates the electrical requirements of a family of four. It also controls the heating system and processes the data collected. The total energy supplied by the sun is 8300 kWh per year.
One obvious thing to emerge was that collecting energy from the sun is not difficult, the problem lies in storing that energy. Incident energy from the sun is collected via banks of solar cells which form part (not all) of one side of the roof. This energy is then converted into lowtemperature (up to \(95^{\circ} \mathrm{C}\) ) heat and is stored by a storage reservoir located
in the cellar. But the collection of "free" energy doesn't end with a few solar batteries on the roof-the surrounding ground offers a usefu supply also. The earth itself absorbs a certain amount of solar energy and this is collected from a soil heat exchanger and used for heating and cooling (it can work both ways).
For solar battery enthusiasts, the cells occupy an area of some 20 metres by 20 metres and they face south at an angle of \(48^{\circ}\). It has been claimed that the solar battery collects between 10,000 and \(12,000 \mathrm{~kW}\) hours of energy per year.

\section*{MAKE A DATE}

I note with interest that at least one UK importer is handling batteries from elsewhere in Europe for sale in this country. So what's new about that? Well, these batteries have small plastic caps over the terminals which prevents any possibility of shorting during transit and storage. More importantly, they have the date of manufacture printed on them. This allows anyone purchasing one of these batteries to know just how long it's been sitting on a stockist's shelf. Certain other manufacturers of batteries have decided not to follow suit, but if the public were educated to look for a date then this could become a trend.

\section*{TREASURE}

Treasure tracers of various types have been offered for sale on the British market for some time. Some boast the ability to locate or detect a single coin at anything up to 30 cms I note that a French company has developed and built something quite remarkable. A magnetometer is a device which will measure or detect very weak magnetic fields. The French company claim to have built a device which is called a double resonance magnetometer with a resolution of 0.01 gamma. This is something like 100 times more accurate than conventional detectors of magnetism. The company will not sell you one, but its team will travel to any part of the world and use it for you. So if you think you've located treasure and you really want to know, it may well pay you to hire someone to take a magnetic peep for yousaves all that fruitless digging if you're wrong.

\section*{ON THE DESK}

Talking computers, I see that the age of the desk-top unit is well and truly here. One of the latest desk-top computers weighs \(22 \cdot 5 \mathrm{~kg}\). and has a 100 mm . cathode ray tube screen which displays 16 lines of 64 characters each. This extremely useful little gadget employs a 48 kilobit MOS ROM (read-only memory), to interpret the high-level language which is fed into it from the self-contained keyboard. It looks just like a modern typewriter with a small television screen. If you're not impressed, the computer houses 25 of the ROM chips described above. To complete the story, the device also has a tape recorder inside it. The tape is used for mass storage of information. The cartridge of tape holds up to 204,000 characters. It's 90 km . long and 5 mm . wide.

\section*{DAB IT ON}

Those with future aspiration to get their " \(A\) " level in applied crime should remember the golden rulealways wear gloves. Laser holograms are now being employed to compare and sort finger prints. The "dabs" of the suspect are compared with prints on master cards to drastically reduce the number of cards which must be hunted through manually. One system can compare/sort finger prints at the rate of 144,000 per hour and can reduce the number of cards requiring manual searching by up to \(80 \%\).

\section*{GREEN STUFF!}

That green stuff which is so hard to come by these days-money, is in the news and coupled with computers. I hear that one prominent British bank network is to go on-line with a number of automatic tellers. These mechanical/electronic beasties will permit clients/customers (that's you and me) to deposit money (notes and cheques) and withdraw little heaps of cash up to a maximum of around \(£ 50\) per day. The initial set-up covers some 100 locations in banks, stores, and even factories.



THIS article describes the construction of a versatile stereo disco outfit comprising twin turntables, a five-input mixer and a pair of 100W slave amplifiers. An optional light display unit is also detailed which can be incorporated into the main console.
To ensure that this project can be given a professional finish a custom designed console has been prepared and will be available in kit form to constructors.

\section*{SYSTEM PERFORMANCE}

The ultimate performance of any system of this nature depends solely on the power amplifier. Attention to design details has resulted in an amplifier offering very high performance and reliability with sustained full power operation. The wide power bandwidth, low distortion and high stability ensure that the audible results are exceptional for this type of high power unit. Switch-on surges, which could damage loudspeakers, are eliminated by a slow switch-on circuit.
The mixer has input facilities for a pair of ceramic cartridges, dynamic microphone, tape recorder, and any auxiliary input in excess of 300 mV . The crossfade control is incorporated to provide a smooth changeover from one turntable to the other, and may also be used to mix the two.
Separate controls for each input allow effective mixing. The microphone input has a degree of bass cut to reduce any "boom" caused by speaking close to a dynamic microphone.
To compensate for the relatively high attenuation of the passive mixer, a high gain pre-amplifier circuit is used incorporating four transistors. Full tone control facilities are provided as well as an effective top cut filter. This is used to reduce record noise and to give a typical bass-heavy "disco sound".

By incorporating the light modulator into the console, advantage can be taken of the high output voltage available from the power amplifiers to drive the switching thyristors from a frequency selective network. Three coloured spot lamps are mounted in the front of the console to effect the display.

\section*{MIXER}

A circuit diagram of the mixer is shown in Fig. 1.
Provision is made for five inputs on each channel: AUX ( 300 mV ), TAPE ( 150 mV ), MTC ( 4 mV ), PU1 and PU2 \((20 \mathrm{mV})\).

To cater for two turntables a pair of ceramic inputs (PU1 and PU2) are provided with independent level controls, VR4 and VR5. Cross fading from one turntable to the other is accomplished by VR6.

A small capacitor, C1, in the microphone input serves to reduce the excessive bass produced when speaking close into a dynamic microphone.

Combination of the various inputs, from their respective level controls and attenuators, is carried out in a "star" network of 120 kilohm resistors feeding directly into the pre-amp input, which is a relatively low impedance.
Consideration of the simple mixing network will confirm the high insertion loss, requiring a sensitive pre-amp. It is as well to note at this point that the input sensitivity of the pre-amplifier is less than lmV.

\footnotetext{
*Consultant tW.F.K. Electronics
}


\section*{specification}

\section*{TURNTABLEB}

Two ESR BDS 80 turntables with Sonotone of AHC cersmic cartridges.

MIXER
Flua input with crossfade failfy betwaen pickup itpouts
Sensithities to give 800 my trom preamplifier (t.m.s.)
\begin{tabular}{lr} 
PU1, PU2 & \(20 \mathrm{mV}^{\circ}\) \\
MIC & 4 mV \\
TAPE & 150 mV \\
AUX & 300 mV
\end{tabular}

All inputs have independent level controls
PREAMPLIFIER
Raxandall tons controls \(\pm 15 \mathrm{~dB}\) at 50 Hz and 12 kHz . 800 mV maximum output.

\section*{PONER AMPLIFIER}

Power Output per channel 100 W continuous into 49 Frequency Response \(\quad 4512\) to \(25 k y z \leq 208\) Total Harmante Distortions. \(0.08 \%\) at 1 kHz 50 F Signal-to-notiso rado. sodB ret, foow moweighted


MGHT MODULATOR (OPTIONAL)
Three channel with crossover frecuencies of \(3 k \mathrm{~Hz}\) and zkHz . Up to 1000 W per channel.

\section*{}

\section*{SIMPIEROWEPROUEETS 8 PAGE SUPPLEMENT No. 3}


This simple project enables a microphone or record player pickup to be used through a radio that does not have auxiliary input connections. Access to the aerial of the radio is necessary but this is no problem because the
output signal of the link can be very loosely coupled to portable radios which do not have external aerial sockets simply by winding one or two turns of wire round the rod of the ferrite aerial.
The device was originally designed to fit inside a turntable and pickup enclosure with a coaxial output socket that could be coupled into any medium wave radio. The prototype system had a low output magnetic cartridge so it was necessary to bring the level up with the pre-amplifier stage of Tr3 before using the resulting signal to modulate the supply voltage feeding the RF oscillator, (Tr1). To

SUPPLEMENT TO PRACTICAL WIRELESS DECEMBER 1975


Top, circuit of the Radio-Pickup Link with, beiow, printed clrcuit board (actual size) and component layout. In the photograph, left, the 6.3 V supply is obtained from a \(6-0.6 \mathrm{~V}\) secondary, using one half only. The coil shown is not the one specified. It was used for later experiments with the Link on other frequencies.
run the unit from a 9 V battery by leaving out D1/4 and the transformer.

When built the unit should be housed in an aluminium case which is connected to the earth rail of the circuit. This is to prevent radiation which might interfere with other radio sets within a short range. Input and output connections should be made via screened coaxial cable.
When setting up you should adjust it so that signal is heard on a quiet part of the medium waveband of the radio.


All the components are mounted on one circuit board which forms the front panel. Leads run from the PCB to the internal battery. The cab/net can take any convenient form but the sloping front feature should be retained. The circuit of the Selector is shown below.

\section*{Bits and Pieces}

 anode display
S1, pushto make pust button swileh
52 Single 6010 0noon swleh
44 pIn DLL SOCkets 3 ) , 16 pin DIL Socket ( 1 )
Pinted Etcuit boan (WKP EEectonics)

This electronic dice uses a seven-segment light emitting diode LED1 to display the normal dice numbers, one to six. A conventional binary counter is modified to give a scale-of-six count and this is driven by a high frequency oscillator. The output from the counter feeds a binary to seven-segment code converter which drives the display.
Apart from the few discrete components used to set the speed of the oscillator, integrated circuits are used throughout. This, coupled with the printed circuit board design, make the project very straight-forward. It would be an ideal "starter" project for someone who has not yet used logic integrated circuits.

The two three-input NAND gates (IC1a/b) form the oscilfator which operates at a few kilohertz. The frequency is set by C1, C2 and R2 and R3. When the pushbutton switch \(\mathbf{S 1}\) is open R1 ensures that the logic level at pin 3 of IC1a is " 0 ". Under this condition the oscillator does not function. However, as soon as this pin is taken to logic level " 1 " (by pressing the button) the oscillator starts to work and makes the binary counter (IC2) start to cycle. The integrated circuit used here is a presettable four stage binary counter.

In this application only three stages are needed to give a count of six so the first stage of the SN74177 is bypassed. Under normal circumstances a binary counter would start counting from 000 to 111 (giving eight codes which would represent the denary numbers zero to seven). For a dice neither zero nor seven are wanted so steps have to be taken to suppress the codes 000 and 111. This is done



Top, circuit board layout shown actual size, with, below, layout of components on the board. Check carefully that the ICs are inserted the correct way round.
by making the counter reset to a pre-determined code immediately after the count six.
The start of the code 111 is detected by the NAND gate IC1C and this puts a signal on the reset input (1) of the integrated circuit. Being a programmable input counter it is possible to preset the code to the reset value, in this case 001. Thus IC2 counts sequentially from 001 to 110 (one to six). Because the oscillator operates at high speed. the count cycle occurs many hundreds of times a
second as long as the push button switch is pressed and it is impossible to predict at what number the counter will stop when the finger is removed from the button.
The binary coded numbers produced by IC2 are decoded by IC3 to seven-segment codes which are fed to th/ respective elements of the seven-segment display. When the button is pressed the LED appears to display the figure eight. This is because the segments are being switched on and off very rapidly as the counter is cycling round the sequence one to six, but as soon as the pushbutton is released a number between one and six will be displayed on the LED. This number stays until the device is switched off or until the button is pressed again.

Current consumption by the device is comparatively high being, on average, just over 100 mA . Therefore it is suggested that a reasonable capacity battery be used to power It; the prototype used a standard 4.5 V flat cycle lamp battery. Space has been left on the printed circuit board for the switch and pushbutton to be mounted on either side of the LED. However these could be mounted in remote positions. The cabinet style can be left to the individual as all the electronic components are mounted on the single board giving the constructor a wide variety of mounting options.


If you want to make a sound to light converter for domestic parties there is no simpler one than this. Although it comprises only the basic features it works remarkably well and has plenty of sensitivity so that it will work off the loudspeaker terminals of almost any amplifier.


\section*{Bits and Pieces}
\begin{tabular}{|c|c|c|}
\hline & 82 CLW & P6. 142 \\
\hline R2\% & \% k C & RJ. 392 \\
\hline R3 & thst & R8. 1 k 2 \\
\hline 84. & \$992 & R'0\% 302 \\
\hline R5: & 1kS , & R10. \(29 \sim 10 \mathrm{~W}\) \\
\hline
\end{tabular}


C1-0.047\%
\(\mathrm{C3}\) 0:022 \(\mu \mathrm{F}\)
\(\mathrm{C} 20047 \mathrm{\mu}\)
e4. \(00022 \mu \mathrm{~F}\)
AH 255 V
© 5 50 5120 V


4 Mains Lratistormet 240 V primary. 120012 V \(50 \mathrm{~m} A \mathrm{Seconday}\).
\(\operatorname{CSR} 22051 \%\) A 2280 Thac 400 pIV 5 A , with Jisulatug it Connecto blocks \(\$\) buay ando 6 way

 Wide somm bigh and somin deebor similat
 500 W per chanhet hopulse transfomers, maths
 Component Speciatisto. PEB WKY Etectronics)



18SWG aluminium heatsink
W099
Top, circuit of the Sound-to-Light Display. Above, details of the aluminlum heatsink for the three triacs, dimensions being given in mm. Insulating kit must be used with each triac. Check with ohmmeter that each is isolated from heatsink.

The audio signal is taken from across the loudspeaker terminals of the amplifier and fed to socket JK1. Note the \(82 \Omega\) resistor linking the earthy connection of the jack socket and the earth rail of the converter. This is to prevent damage if the amplifier output is earthed on one side and, inadvertently, the wires become crossed over. You MUST ensure that the earth of the amplifier corresponds to the earth of the input jack otherwise all signals will be shorted out. Fortunately no damage would result, because of R1, but the unit will not work if wrong in this detail.
The audio signal is fed to three separate transistor amplifier stages and simultaneously through frequency selective networks to pass bass frequencies to VR1, middle frequencies to VR2 and high frequencies to VR3. The transistors are operated without bias hence the input signal has to exceed a certain minimum amplitude before the transistors start to conduct. When this happens current pulses pass through the primary of the pulse transformers in the collector circuits and these pulses are coupled to the gate circuit of each triac, switching it on for the duration of that mains half cycle. Sensitivity to bass, middle and high frequencies is adjusted by VR1, VR2 and VR3 respectively. The lamps are standard 240 V coloured ones with a maximum load of 500 W per channel.
Construction is simplified by making use of a printed circuit board and there should be no problems with assembly. If the potentiometers having printed circuit tags are unobtainable ordinary potenfiometers can be used but use jumper wires to go into the board locations.


Lamp connector block
The printed circuit board, actual size, is given on the left with the parts layout at the top. Note that the heatsink is fitted at right-angles to the PCE.

When fixing the potentiometers make sure to insert them so that the spindle protrudes on the copper side of the board.
Care should be taken to insert the pulse transformers (T1, T2 and T3) the correct way round, noting the spot, and similarly insert the triacs in the right way. The best way of carrying out the latter stage is to bolt the triacs on to the aluminium heat sink, making sure to use the insulating plastic bush and mica sheet, and then offer up the triac pins to the circuit board so that the triacs are on the side of the heatsink opposite to that which faces the potentiometers. The leads for transistors Tr1 to Tr3 should be carefully formed before they are inserted into their respective holes.

Under no circumstances should the unit be operated without a fuse somewhere in the system. There is provision for a fuse on the circuit board but if difficulty is experienced in getting a suitable fuse holder then operate the unit with a fused plug but the rating should not exceed 3A. Connect a shorting link across the fuse contact pads.
Mains input connections are made to a three-terminal mains connector and the outputs to the three lights are made via similar connectors fixed to the rear of the cabinet. If you use the metal cabinet as specified make sure there is ample separation between the rear side of the front panel and the copper side of the circuit board. Preferably sandwich a thin layer of insulating material between the two, a piece of blank Veroboard or Formica would be ideal. Likewise ensure that the heatsink does not foul on the metalwork of the cabinet. As a final safety precaution the metal cabinet MUST be connected to the earth lead of the mains plug.

When operating, parts of the circuitry are Hive to mains voltages hence a soldering mistake or a finger in the wrong place when carrying out tests COULD prove very dangerous. If you are in doubt consult with a more experienced constructor before embarking on the project.


The output transistors of this amplifier are fitled to the backorop of the chassis which acts as a heatsink. The arrangement can be seen in the photograph at the right, with the PCB mounted on the bottom of the chassis with spacers.

Although this is a Public Address amplifier it is not a very powerful unit by normal public address standards. Nevertheless, when used with a directional re-entrant horn loudspeaker, it is very effective and would be ideal for amplifying the voice of a speaker at an average sized garden fête or it could be used as a mobile amplifier for advertising from a moving car. It provides an output of just over 2 watts RMS into an \(8 \Omega\) loudspeaker increasing to about 6 watts when used with a \(3 \Omega\) loudspeaker. Two alternative inputs are provided, one for a \(600 \Omega\) moving coil microphone and the other for, typically, a cassette tape recorder output. SK2 is the microphone input and, in the case of the prototype, maximum power output was obtained when using a Foster Low Impedance Microphone, type DF100.

Other microphones may be used but they MUST be moving coil (dynamic) types and should be of low impedance. SK1 is the phono input the sensitivity of which is set by the value of R1. A value of \(470 \mathrm{k} \Omega\) is suitable for a Philips cassette tape recorder allowing maximum output when VR1 is set at maximum, without any undue distortion. To obtain higher input sensitivity R1 should be reduced.
No great claims are made for the musical quality of the amplifier except to say that it is more than adequate when used with directional loudspeakers which, in themselves, leave much to be desired as far as frequency response is concerned. An LED is used as an on-off indicator.
The circuit is straight-forward and conventional. Tr1 serves as a pre-amplifier having fixed gain, the output level of which is manually adjusted by the volume control VR1. C3 is present to reduce the gain of this stage at high frequencies to prevent spurious high frequency oscillations. This component can be varied in value if a more mellow tone is required from the amplifier. Increasing its value to 1500 pF gives a more acceptable quality for music but makes speech a little muffled.
Tr2 provides the drive to the complementary output pair which operate in Class B thus lowering power con-

\section*{Bits and Pleces}

-1tor

C1 +46
2200022 \(\mu \mathrm{F}\)
© \(6.680 \%\)
C4 1640164
0420291
TO \& 8

PRSOt

e0 04105

e8, 500\%6 18 y
40 化 \(5005 . \circ \mathrm{GP}\)
40 285858










sumption. The quiescent current is set by adjusting VR2 from minimum resistance until the total current consumption is about 35 mA under no signal conditions. If you do not have a meter to check the current start with VR2 set to minimum resistance and play some music from a tape through the system with VR1 set about half way. It will sound very distorted, due to crossover distortion in the output stage. Slowly increase the value of VR2 until the distortion JUST disappears, the optimum setting of the control.

There are few problems to be encountered in assembly. Use mica spacers and insulating bushes when mounting Tr 3 and Tr 4 to the outside of the chassis and drill clearing holes for the leadouts. Ensure that all diodes, transistors and electrolytic capacitors are fitted to the circuit board with the correct polarity. When fixing the circuit board into the cabinet make sure that the spacers used do not short across between the earthed area of the PCB's foil and any other part of the PCB.



Fully drilled.epoxy glassfibre printed circuit boards which have been roller-tinned can be obtained for these projects from:-
WIK.F. Electronics, Welbeck Street, Whitwell, Worksop, Notts., S80 4TW.
Radio-Pickup Link, 12V PA System and Random Number Selector are each 98p plus 10p post and packing. The Sound-to-Light Display is \(£ 1 \cdot 15\) plus 10p post and packing.

\section*{IMPORTANT NOTE}

This circuit can only be used with negative earth vehicles if it is intended to mount the unit under the dashboard. With the same application in mind make sure that the loudspeaker leads do not make contact with the chassis of the vehicle and that the speech coil is isolated from the metal work of the loudspeaker. Remember that the car should be properly suppressed electrically to avoid interference when using the amplifier while moving.


\section*{A.C. AINSLIE* \(\&\) C. TOMS \({ }^{\dagger}\)}


Fig. 1 : Circuit diagram of the mixer.

Linear pots are used for the level controls' as, feeding into a relatively low impedance, they behave in a semi-logarithmic manner.

\section*{PRE-AMPLIFIER}

The power amplifier requires 800 mV r.m.s. from the pre-amp to deliver full power output. Due to the use of a simple passive mixer of low output the pre-amp is required to have higher gain than usual, and employs four transistors, see Fig. 2.

\section*{INPUT STAGE}

The input stage Trl has a medium input impedance and noise is kept to a minimum by operating at a low collector current and fairly low gain. Negative feedback is provided by R12 and R13, while C3 reduces the collector load to A.C.
\(\operatorname{Tr} 2\) and \(\operatorname{Tr} 3\) are a D.C. coupled pair with \(\operatorname{Tr} 2\) passing only a small collector current, again for minimum noise. Overall negative feedback round the pair is provided by R21 which stabilises the D.C. conditions, giving low D.C. gain to the pair. R20 and C6 apply a measure of positive A.C. feedback to Tr2 emitter, offsetting the effect of the negative feedback at signal frequencies. In effect the A.C. gain is defined by the difference between the positive and negative feedback. R24 and C7 stop any tendency towards high frequency instability.

\section*{TONE CONTROL}

Tone controls are incorporated into the final stage, Tr4. Bass and treble controls in the familiar Baxandall configuration are connected in the collec-tor-to-base feedback loop of the transistor. This feedback system gives a low collector impedance to Tr4 allowing the tone controls to be varied independently over a wide range. When the treble control is fully advanced, the gain of the final stage increases rapidly with frequency. To curtail this rise above 20 kHz a small capacitor (C14) applies high frequency negative feedback.

A "top cut" control is brought into operation by closing S1, connecting C23 across the signal to ground.

Balance and volume controls link the pre-amp to the power amplifier.

\section*{SUPPLY REGULATOR}

The pre-amp operates from a +30 V supply which is derived from the main amplifier supply. Rather than using simple resistance voltage dropping with capacitive decoupling, a single transistor, 30 V series stabiliser is used. This provides very effective decoupling of the main supply rail, which, in view of the high power output of the amplifier, is bound to fluctuate considerably under load.

Tr5 acts as the pre-amp supply regulator and is connected as a simple emitter follower with a constant 30 V on its base from D1. R33 provides the standing current for the Zener diode as well as base drive forTr5.


Fig. 2: Circuit diagram of the preamplifier.

\section*{POWER AMPLIFIER}

The amplifier is a class \(B\) design operating from an 80 V supply ( 65 V on full load). Feedback round the amplifier gives a constant voltage output so it follows that the output power is dependent on load impedance. Feeding 4 ohms the 20 V r.m.s. output develops 100 W of load power. Into 8 ohms and 15 ohms the theoretical output would be 50 W and 27 W respectively, but in practice will be considerably higher as the supply current at full output would not be so great, giving a higher supply voltage. The circuit is shown in Fig. 3.

\section*{SLOW SWITCH-ON}

A feature of this design is a "slow switch on" circuit which eliminates the output surge that occurs with conventional designs as the output capacitor charges when power is applied.

Tramsistors \(\operatorname{Tr} 9\) and \(\operatorname{Tr} 10\) are connected as a Darlington pair emitter follower in the emitter of the driver, Tr11. Initially on switch-on C22 is discharged and slowly charges to full supply voltage, bringing the emitter of Tr10 up to supply voltage. This slow turn-on of the driver gives a controlled rise to the D.C. voltage across the output capacitor, eliminating surges.


Fig. 3: Circuit diagram of the power amplifier. A 100 1 F smoothing capacitor (C29) is required between 80 V and GND.

The collector load of the driver Trll consists of Tr12, R46 and R47; Bootstrapping R47 increases its effective A.C. resistance giving Trll high A.C. gain.

\section*{BIAS STABILISER}

Tr12 acts as bias stabiliser for the quasi-complementary output stage, \(\operatorname{Tr} 13 / 14, \operatorname{Tr} 15 / 16\). It is connected as a "V be multiplier" whereby the voltage across emitter and collector is a multiple of its \(\mathrm{V}_{\mathrm{be}}\) determined by the setting of VR12. To just turn on the output stage a potential of three \(V_{b e}\) 's must be applied between \(\operatorname{Tr} 13\) and \(\operatorname{Tr} 14\) bases to overcome the \(\mathrm{V}_{\mathrm{be}}\) 's of \(\operatorname{Tr} 13, \operatorname{Tr} 14\) and \(\operatorname{Tr} 15\).

The \(\mathrm{V}_{\mathrm{be}}\) of Tr 12 varies with ambient temperature to maintain a constant standing current in the output stage.

The effect of too low a standing current is cross over distortion, more pronounced at high frequencies as the amplifier runs out of loop gain and feedback is consequently reduced. This amplifier has been designed for a standing current of 10 mA in \(\operatorname{Tr} 15\) with the transistors at working temperatures.

\section*{DIFFERENTIAL AMPLIFIER}

The front end of the power amplifier is a differential amplifier formed from Tr6 in one side of a "long tailed pair", with \(\operatorname{Tr} 7 / \mathrm{Tr} 8\) connected as a Darlington pair in the other side. Tr6 base is the non-inverting input, while \(\operatorname{Tr} 8\) base is the inverting input.

The audio input is fed to \(\operatorname{Tr} 6\) base while \(\operatorname{Tr} 8\) receives feedback from the output via R51. The emitter coupling between \(\operatorname{Tr} 6\) and \(\operatorname{Tr} 7\) (the common "longtail" connection) completes the A.C. feedback path round the amplifier.

Tr8 collector is decoupled to A.C. by C20 and D.C. feedback from this point to Tr6 base through R35 and R36 serves to stabilise the D.C. conditions of the amplifier overall.

For maximum output power and symmetrical clipping, the no-output D.C. voltage at the positive end of C25 should be one half of the supply voltage; this condition is set by adjustment of VR11.

\section*{STABILITY}

Apart from the input and output capacitors the amplifier is completely D.C. coupled, and the large feedback factor ensures high stability. C24 shunts Tr11 at high frequencies so that the gain of the


\section*{components lists}



\section*{POWER AMPPMEIER}

Resistors

capacitors
C19; C119 10 FF 25 V elect
C20, C120 \(22 \mu \mathrm{~F}\) 100V elect
C21, C121 4:7aF63V elect
C22, C122. \(100 \mu \mathrm{~F} 100 \mathrm{~V}\) elect
\(\mathrm{C} 23, \mathrm{C} 123 \cdots 1 \mu \mathrm{~F} 100 \mathrm{~V}\) polyester or tantalum
C24, C124 390pF 160V polystyrene
C25, C125: 2000 1 F 50 V elect (840mA A.C. nipple at 50 Hz )
C26, C126 0-1 1 F 100 V polyester
C29 100 \(\mathrm{\mu F} 100 \mathrm{~V}\)
Semiconductors
Tr6, Trio6 BC147
Tr7, Tr107 BC147
Tr8. Tr108 BC147
Tr9, Tr109 BC117.
Tr10, Tr110 BC117
Tr11, Tr111 BC461

\section*{Miscellaneous}

F1, F101 2A 20 mm fuse and p.c.b. clips
Heatsinks for M3055 transistors (R.S. type 180), heatsinks for Tri6, 18 and 19 (R.S. type 154). TO3 insulating kit for 7 T20 and 21 , terminal pins ( 00 off) p.c.b. (1 p.c.b. required for each channel)

\section*{POWER SUPPLY}

Capacitors
C27, C28 \(1000 \mu\) F 100 V elect (2 off)

\section*{Rectifier}

D2 200V 6.6A REC92 (R.S: Components)
Transformer
T1 55V 5A low flux leakage transformer ( \(B\). B. Atkin)
Miscellaneous
S3 S.P.S.T. onjof illuminated rocker switch
F2. 5A 20 mm fuse and holder
Note: Componenf numbers greater wan 100 refer to the second channel so two of these components are necessary for stereo system. For mono only one of each will be necessary.

\section*{MISCELLANEOUS}

BSR McDonald turntables (type MP60 or BDS80) (2 off)
Sonotone 9TAHC stereo ceramic cartridge (2 off) Mains plug and socket
Woodwork (see cutting list) A complete di.y. cabinet kif is available from Birch and Ridley (Cabinet makers) Watson Ra," Worksop, Notts.
The cabinet kit is supplied in pollshed teak veneer. The deck board has a cut out for either the BSR MP60 or BDS80 turntables-please specify when ordering. The price is \(£ 26.50+8 \%\) VAT and £3-20 p.\&p. Other deck board cut outs may be specified but a pattern plus an extra 51 must be sent with order.
Fully drilled and silk screen printed mixer and mains panels are avaliable fromW.K.F. Electronics, Welbeck St., Whitwell, Worksop, Notts, Prices are
 Amplifier and Light Modulator components are available from Worksop Electronics; 24 Vessy Rd;, Worksop, Notts. Send s.a.e. for price llst.
Transformers, inductors and accessories are avallable from B. B. Atkin Electronics, 1 Windsor Walk, \(\mathrm{S}_{\text {: }}\) Anston, \(\mathrm{N} \boldsymbol{r}\) Sheffield, Yorks. S.a.e. for price list.
Printed circuit boards for the amplifier and light modulator are available from W.K.F. Electronics. Prices are \(£ \mathbf{2} \times 40+18 \mathrm{p}\) patp (two required for stereo) and \(\mathbf{2} 270+18 \mathrm{p}\).p\&p respectively.
MP60 type turntables are available from R \& TVC, 323 Edgware Road, London W2, price £14 + £150 p.\&p. BDS80 type turntables are avallable from Maplin Electronic Supplies, PO Box 3, Rayleigh; Essex price £27-95 (VAT and postage included).
amplifier is reduced well before the output stage cut-off frequency is reached, ensuring good transient response with minimum transient distortion and overshoot.

The Zobel network C26 and R50 is connected across the output to compensate for the inductive nature of a loudspeaker load, further assisting stability.


Fig. 4 : Circ uit diagram of the power supply.

\section*{THE POWER SUPPLY}

Owing to the very high stability of the power amplifier and the series stabilisation of the preamplifier, there was no advantage to be gained by the use of a stabilised power supply. Another factor is that, owing to this very high stability large smoothing capacitors have also been unnecessary.

Transformer T1 is a low flux leakage transformer capable of delivering 55V D.C. at 5A. D2 is a full wave bridge rectifier. For full-wave circuits, the average current per rectifier is \(0.5 \times I_{\text {d.c. }}\) Each rectifier should have a \(V_{\text {rrm }}\) rating in excess of \(1.4 \times V_{\text {a.c. }}\). \(\mathrm{C} 27, \mathrm{C} 28\) is a \(2,000 \mu \mathrm{~F}\) capacitive filter rated at 100 VDC. No additional smoothing was found necessary.

As the \(V_{\text {d.c. }}=1.41 \times V_{\text {a.c. }}\), in this type of circuit and the \(I_{\mathrm{d} . \mathrm{c} .}=0.62 \times I_{\mathrm{a} . \mathrm{c} \text {. the supply voltage and }}\) current are adequate.

In Part 2 next month details of the Light Modulator and construction of the system will be described.

\section*{PRODUCT}

\section*{REPORT}

THE GD-348 De Luxe Metal Locator is designed to meet the needs of the more sophisticated treasure seeker. This instrument uses the induction balance method of operation and is typically capable of detecting the presence of a small coin at a distance of about 150 mm (6in.) in air.

\section*{CIRCUIT DESCRIPTION}

Transistors Q101, Q102 form an audio relaxation oscillator, Fig. 1, operating at about 500 Hz , whose output is applied to the search coil L301 which is tuned to resonate at 100 kHz . A modulated RF field thus surrounds the coil. The search coil and the pickup coil, L302, are so designed that there is virtually no magnetic coupling between them. The Null control R301 allows the signal due to the residual coupling to be balanced out in the absence of any metallic object.

When the search coil is passed over a metal object, a current is induced in the object, which sets up its own magnetic field. This field in turn induces a current in the pickup coil which provides the signal used for detection. This signal is passed through an active filter and amplifier formed by transistors Q103, Q104 whose output is detected by diode D101 to recover the 500 Hz audio signal.

A fixed-gain amplifier Q201, Q202 raises this signal to a suitable amplitude to operate the level detector Q203. This transistor's bias is adjusted by the Sensitivity control R302 (the second operator control) to be just in saturation when only noise and residual audio are present. As soon as a small audio signal arrives, indicating the proximity of metal, Q203 plus the output amplifier Q204, Q205 amplify it to a level sufficient to drive the built-in loudspeaker or optional headphones. The output also feeds the output meter M301. This is protected by a shunt transistor Q206 which is brought into conduction by very large signals.

\section*{CONSTRUCTION}

The majority of the circuitry is mounted on two small printed circuit boards, one of which is fitted in the search coil housing and the other in the handle housing. Construction begins with the assembly of these boards, which is straightforward and well documented in the usual Heathkit fashion. Assembly of the rest of the parts mounted in the

handle housing similarly presents no headaches. The same, unfortunately, cannot be said of the assembly of the telescopic shaft and the wiring which runs through it, which took well over one third of your reviewer's total assembly time.

The interconnecting wiring requires five cores and Heath get round this by using part of a coiled four-core telephone handset-style lead, plus a single wire which the constructor has to form into a coil and feed down the centre of the four-core cable. Because only a part length of a coiled

lead is used, it means that at least one end of the cable will be from the "curly" part. I have never had to try to strip one of these before, but I can assure you that it is not an exercise to be recommended unless you are both patient and dexterous. The same comment applies to the operation of threading the concentric coils of wire safely through the shaft and the various obstacles at each end.

The final stage of construction, assembly of the search coll housing, poses no problems. If initial tests prove satisfactory, the application of waterproof sealant to all the housing joints completes assembly. The whole process, from unpacking the parts to final testing, took your reviewer just six hours.

\section*{OPERATION}

The two controls, Null and Sensitivity, allow very sensitive adjustment of the instrument, which proved during tests to be capable of detecting the heads of floorboard nails and would even register the presence or absence of carpet over those floorboards. By offisetting the Null control from its optimum position, the locator can differentiate between ferrous and non-ferrous metals; very useful to the treasure hunter.

The whole instrument is powered from a 9 V battery which has a life of about 50 hours. The telescopic handle allows the overall height to be adjusted between 710 and 915 mm ( 28 and 36 in .). The search coil housing is waterproof and is submersible to a depth of 610 mm (24in.). It folds flat against the shaft for transit or storage. The whole instrument weighs \(1 \cdot 6 \mathrm{~kg}\) ( \(3 \frac{1}{2} \mathrm{lbs}\).)
Heath offer two optional accessories. The first, headphones, proved very useful in noisy locations and, indeed, in very quiet ones where the 500 Hz tone from the loudspeaker can be a bit shattering, there being no volume control. The
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second accessory is a zippered plastic carrying case, rather reminiscent of a golfing bag.
Price of the GD-348 kit is \(£ 58 \cdot \mathbf{2 0}\). The headphones, Model GD-396 cost \(£ 5 \cdot 70\) and the carrying case, Model GDA-348-1 \(\mathbf{£ 5} \cdot \mathbf{5 0}\). All prices are inclusive of VAT and delivery within the United Kingdom.

Further details are available from Heath (Gloucester) Limited, Bristol Road, Gloucester GL2 6EE (telephone 045229451) or from the London Heathkit Centre, 233 Tottenham Court Road, London W.1.

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More from E, Trundie on the ITI CVC5-CVC9 series colour chassis while Les Lawry-dolins deals with arimposted set, the indesili Model T24EGB, which has been widely distributed in the UK

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\section*{TRACKING}

While it is a matter more of maintenance than "improvements", I feel that a few words on tracking are not out of place. All the work on the gram side already described will be largely spoiled if the stylus and arm track badly and produce serious harmonic distortion. Budget stereo almost always comes with one of the well-known and quite excellent budget decks. Lateral tracking will have been taken care of in the design so we have no need to worry about that for it is very unlikely to deteriorate with wear and tear. However, there are some other points which should be examined carefully from time to time or sound quality may slowly deteriorate.

The first is that budget decks require to be level, more so than the expensive sophisticated ones. So arm yourself with a spirit level, check that the instrument is level on whatever piece of furniture it stands. This check, by the way, sometimes produces unpleasant surprises! Next check that the cartridge shell is also level, that is, parallel with the turntable. The vertical tracking angle, the angle the stylus arm trails in the groove when playing, is most important. Unfortunately it is almost impossible to measure it so we have to get at it another way.

See that the flat part of the cartridge underside is perfectly parallel with the record surface and this will ensure that the vertical angle is within limits. Some budget decks (the Garrard SP25 is one) have the pickup arm tilting downward towards the record; a small plastic wedge is supplied to fix between the cartridge and the shell to counteract this: make sure there is one fitted and that it is fitted the right way round.

My last point concerns wear and tear on the Garrard deck. The pickup arm rests in a cradle at its pivot end and is held in place by two small screws which go into the metal tube from the underside. After a lot of use these screws can work loose with the result that the arm, and therefore the cartridge, can rock about the arm axis. This will cause the stylus to meet the record groove at some angle very different from \(90^{\circ}\) which can cause horrible distortion and loss of output on one channel. The arm is easily removed by unscrewing the two large screws which provide pivots for the vertical arm movement, one on each side of the assembly, and gently lifting it out of its cradle. The holding screws for the arm are then easily accessible and can be tightened.

\section*{MORE REFINEMENTS}

In previous articles I described the various modifications that I have carried out to a budget stereo outfit, costing £80 cash-and-carry, which brought it,
in my opinion and that of many visitors who have heard it, into at least the \(£ 250\) class. I feel more than ever that it can hold its own against many very much more expensive systems in the hi-fi category. I doubt if the cost of the modifications exceeded \(£ 20\) provided, of course, we ignore completely the hours of planning and labour that went into them. The next step is to upgrade the appearance and functions as much as possible so that what is good, looks good.

Having fitted a tuning meter I cast around for other uses for the meter, to monitor and test certain vital points in the total circuitry. Of the many possibilities that occurred to me, I decided that the resistors in the emitter circuits of the output transistors were the most useful and promising.


Fig. 1: Typical arrangement of output stage transistors, the test meter being switched across each emitter resistor in turn.

Figure 1 shows a circuit of four output transistors for both left- and right-hand amplifiers and is typical. The currents through R1, 2, 3 and 4 under no-signal conditions are the quiescent conditions and are of the highest importance where crossover distortion is concerned. In addition to this, if a small constant
amplitude signal is applied to each amplifier in turn, measurement of these currents will monitor the behaviour of each output transistor and check that all are giving the correct and equal AC output. Obviously we cannot keep breaking into the circuit to measure these currents but we can, by some reasonably simple switching, connect the 50 mV meter across each resistor in turn.
These emitter resistors are usually between 0.5 and \(1.5 \Omega\) and in this particular circuit they are \(1 \Omega\) each which is very fortunate as it means the meter reads directly, volts for milliamps, that is a reading of 15 mV means 15 mA . If the resistance values are different from this, the calculations to obtain equivalent currents to scale readings are quite simple or one can simply mark on the meter scale a normal reading and work to that. Our tuning meter on the front panel in this way becomes a multi-purpose instrument which carries out useful tests.

\section*{SWITCHING THE METER}

Two single-pole, 6-way break-before-make switch wafers are required, Fig. 2. Only five positions are required with position 2 blank to give some obvious separation between the functions of "Tune" and "Test". Normally the switch is left in the "Tune" position and it must be remembered that the volume control must be turned to zero before moving the switch to "'Test", as a strong signal driving the output stages will probably swing the meter needle off the scale .


Fig.2: Switch wiring for test meter measuring the quiescent current of each transistor in the output stage.

Photographs show the meter switch and its wiring. For clarity the playing deck has been removed and only the motor board together with the main body of the instrument is shown. In models like this where the motor board is hinged, there are obvious advantages in mounting the switch as near the hinge line as possible as this reduces the length of the necessary connections and reduces the movement of them


In this view the playing deck has been removed leaving the hinged motor board. The added meter switch and wiring can also be seen.
every time the motor board has to be lifted. The switch has been fitted in the position shown. It is mounted on a small aluminium plate which is screwed to the fancy woodwork that surrounds the playing deck. I had to cut away some of the wood underneath to make room for the switch assembly but this did not spoil the appearance of the cabinet. The leads from the switch are cleated to the back of the motor board and then emerge in loose loops to be soldered to the ends of the respective emitter resistors. The meter leads are cleated to the woodwork close to the switch and then loosely towards the AFC switch and meter. With this arrangement, the leads fall neatly and safely into position when the motor board is lowered as can be seen in the photograph. The small loops going to the power board and the one larger loop of the meter leads are no hazard to the circuit provided the cleating. and the soldering are thoroughly sound.

It is essential that the wire used for this work is lightweight and fully flexible. The tags on switch wafers are not usually very strong and if one should break off sometime after the job is done it is an annoying job repairing it. Connect all the wires to the switch before mounting it; making them overlong and establish a colour code for the meter pair and for the four pairs going to the emitter resistors.

I have already found and located one elusive fault that had bothered me for a long time, an intermittent slight reduction of output on one channel which completely upset the stereo image. I thought it must be my imagination but the meter in the "test" position with a constant amplitude signal from my audio generator and the volume control just "on" confirmed the drop was real. With this factual confirmation, it was a matter of twenty minutes or so to find the offending dry joint and put it right. It is worth remembering that with an input signal driving the meter within its scale limits, we are not only monitoring the output circuit behaviour but the drive levels as well.

\section*{ILLUMINATION REFINEMENTS}

No doubt because of its low price, the dial illumination was sparse and consisted of two 12 V pilot lamps edge-lighting the tuning scale, glowing brightly but not very prettily whatever service was in use, and there were no separate lamp indicators to show when "Gram" or "Aux" were in use. I therefore decided to look around the circuit and mechanical arrangements to see if it was possible to fit

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View of the budget stereo system after all the modifications described in this series have been added.
indicator lamps on the panel to light when "Gram" or "Aux" were selected. This really meant searching for spare, unused switch contacts. For good measure I decided to fit a neon mains indicator lamp but this is simple and straightforward.

Luckily spare contacts with 12 V DC were ready and waiting for both services. Many models have push-button switches, usually two-pole changeover, requiring only one position, to break the DC supply to the radio section in order to kill it on gram or auxiliary. Figure 3 shows the arrangement showing only the DC contacts concerned.


Fig. 3 : Additional contacts were found for this switching arrangement for indicating LED's on Aux and Gram.

I decided to use LEDs as they are neat and tidy and I like the even, soft glow. The resistor marked " \(R\) " is put in the original design presumably to present a dummy load to the supply when the radio circuits are switched out. As LEDs take up to 50 mA it seems sensible to remove " \(R\) " when they are fitted. But check with a voltmeter that the supply stays constant and correct on "Radio", "Gram" and "Aux" without " \(R\) " in circuit.

\section*{HANDLING LED's}

There is a space between the facia and the main chassis from which the connecting wires must emerge and a first attempt to connect flexible wires from chassis to the LED wires merely proved that the LED leads are fragile and break off very easily!

Eventually I soldered the LED leads to a thin strip of Veroboard, pressing the diode itself closely and safely against the strip. The flex leads can then be connected to the ends of the Veroboard conductors and taken away to the appropriate switch contacts on the main chassis. The LEDs on their respective Veroboard strips can then be safely offered to the panel clips which will have already been fitted to the front panel. For 12 V supplies, each LED must be connected through about \(1 \mathrm{k} \Omega\) but in the circuit shown they share the same resistor.

\section*{SWITCHED LIGHTING}

But the tuning scale light still glows and glows on all services! Hardly daring to hope, I made a further search for spare contacts on the "Gram" and "Aux" switches which would be open when either was selected but would be closed on radio. And I found them. True they had been soldered together in parallel with the contacts feeding DC to the radio chassis so as to share the load but as the radio load was well within the specification of the average push-button switch I decided I could safely separate them.


Fig. 4: On Aux or Gram the tuning scale lights are dimmed using this circuit.

The 24 V AC for the pilot lamps (the 12 V bulbs are in series) was now fed through these contacts so that the scale lamps on "Gram" and "Aux" are extinguished but come back on again as soon as both these buttons are disengaged by the latch action whenever any of the radio buttons is pressed. Unfortunately, edge-illuminated scales look even worse unlit, the scale shows up too clearly in black and white so I had to think again. I decided that the most pleasing arrangement would be if the scale was dimmed on "Gram" and "Aux" but went back to full brilliance on radio. This accounts for the two \(300 \Omega\) resistors included in Fig. 4 across the switch contacts. They reduce the pilot lamp current when "Gram" or "Aux" is selected and so dim the lamps. The value of these resistors is a matter for experiment depending on the wattage of the lamps and a personal decision as to the degree of "dim-out" that is acceptable.

The colour of the scale illumination was originally a pale pink which I did not find very pleasant and is decided by transparent plastic stuck to the edges of the scale. I changed mine to a dark green by the simple expedient of changing the plastic to one of this colour.


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MOST power supplies to date are variations on two basic themes-the shunt stabiliser, in its simplest form shown in Fig. 1, and the series stabiliser, which is the same circuit with a transistor added (Fig. 2) which acts as a variable resistor controlled by the Zener and the current drawn by the load.

If one considers a bench supply where sooner or later inadvertent overloads or shorts are almost bound to occur the shunt system has something to recommend it in that it is inherently current limited and therefore short-proof. However, at load currents of more than a few milliamps it becomes very inefficient, since the Zener is called on to carry all the current that the load does not need, and therefore may need to be a high dissipation device.

The series system is the more common, probably because it is far more efficient, since apart from a relatively small loss in the Zener and feed resistor, loss only occurs in the series transistor when it is passing current. The one drawback of the series system is that it is not short-circuit proof (or even resistant), and under fault conditions the transistor can pass a large current with usually disastrous consequences to itself, and probably to the equipment under test.

It is not necessary to have a complicated circuit to achieve the best of the two sorts of regulating systems, and the circuit about to be described is one way of combining the advantages of each system.

The bench supply to be described has a maximum short circuit current of 1 A , with the output voltage controllable between 24 V and 5 V , which should cover most needs except high power amplifiers.

\section*{FEEDBACK CONTROL}

The simplest way of varying the output voltage is to connect the base of the transistor to a potentiometer placed across the Zener diode in Fig. 2, but this form of control does not give very good regulation at the lower voltages, so a feedback type control will be used, shown in basic form in Fig. 3. Here, the base voltage of \(\operatorname{Tr} A\), and hence output voltage, is controlled by the voltage drop across RA due largely to the current drawn by TrB, which in turn is a function of its emitter voltage, set by DA, and the fraction of output voltage applied to its base by VRA.

With the slider at the earthy end of VRA, \(\operatorname{TrB}\) will be cut off, and the only voltage drop across RA will be due to the base current of TrA, and the output voltage will be nearly equal to the collector voltage.

At the other extreme \(\operatorname{Tr} B\) will be turned hard on when the slider is at the positive end of VRA, so that RA and the base of TrA will be almost shorted to DA, giving the minimum output voltage, with intermediates between these extremes.

This feedback action helps to maintain the output voltage set by VRA because if the output voltage drops due to an increasing load, the proportion applied to \(\operatorname{TrB}\) base also falls, lowering its current demand, so reducing the voltage drop across RA, which therefore increases TrA's base volts, so tending to restore the output to its pre-set value.

If the output tends to rise, the action is reversed. The same effect applies to any ripple left at the output, since this is inverted and fed back to the TrA base so tending to cancel the original variation.

Up to now RB and TrC have been ignored, since they play no part in the proceedings until the current through RB causes a potential difference that exceeds the 'turn-on' voltage of TrC. If RB is, say, 0.5 ohms, a current of 1 A through it will cause a base emitter difference of 0.5 V across \(\operatorname{Tr} C\), which will begin to conduct, drawing extra current through RA and diverting it via the load to the negative


Fig. 1 : (left) The simplest shunt stabiliser using a Zener diode. Fig. 2 : (right) A simple series stabiliser, which is Fig. 1 with a transistor across the resistor.


Fig. 3: A more complicated voltage stabiliser using a feedback control system.


Fig. 4 : Complete circuit diagram of the Stabilised Power Supply.
rail. The voltage drop across \(R A\) will be increased, lowering the base voltage of \(\operatorname{Tr} A\), which of course reduces the voltage driving the current through the load such that it will only maintain a maximum current of 1A through any load, even a short circuit.

\section*{PRACTICAL CIRCUIT}

So, from abstract theorising to a practical circunt (Fig. 4). Tl, D1-D4 and Cl perform the obvious conversion of 240 V A.C. to about 36 V D.C. The main responsibility for smoothing rests on R1, C2 and the series transistors, so Cl need not be as large as might be expected for an unregulated supply, though there is no reason why a larger one could not be used.

To get the extra benefit of the feedback ripple reduction, RA of Fig. 3 has to be split, (into R1 and R2) and C2 connected to the junction rather than at \(\operatorname{Tr} 2\) base, where it would actually decrease the overall smoothing.

Resistor R1 + R2 in total could be as high as \(6 \mathrm{k} \Omega\) but to avoid any risk of Tr3 being starved of current and to ensure that the current taken by Tr2 base is a relatively small fraction of the total current through R1, it should be much less, but this would tend to restore the conditions that \(\operatorname{Tr} 2\) was added to avoid, so a value of around \(4 \mathrm{k} \Omega\) was chosen.

Obviously the larger the proportion of this that R1 can be, the smaller C2 can be for equivalent smoothing, therefore R2 should be as small as possible. In this case it will be made about ten times the minimum expected base impedance of \(\operatorname{Tr} 2\), say \(470 \Omega\), leaving \(3 \cdot 9 \mathrm{k} \Omega\) for R1. With C2 at \(100 \mu \mathrm{~F}\), this will give a ripple at \(\operatorname{Tr} 2\) base of less than nne per cent of that at its collector.
Zener diode D5 needs to be less than the minimum required output voltage, since this, together with the collector to emitter saturation voltage of Tr3, sets the minimum possible output voltage, so to allow for tolerances, D5 was chosen to be \(3 \cdot 9 \mathrm{~V}\). R3 is included as an attempt to keep the variation of current through D5 reasonably stable despite varying output voltages and currents.

The current limit resistors (R4-7) can now be chosen to limit the output current to whatever the constructor feels to be a safe value for a particular purpose, providing that they are never less than \(0 \cdot 47 \Omega\), which gives a maximum current of about 1 A . \(1 \Omega\) will give about \(500 \mathrm{~mA}, 5 \Omega\) about 100 mA and so on. It must be pointed out however, that the 'usable' current before the output voltage pre-set begins to fall significantly is less than the 'short-circuit current.
Capacitor C3 is included to reduce the tendency of amplifiers to oscillate, but constructors should beware of putting any large value capacitor after the output, because while the supply itself can be made to give no more than a safe current, a few hundred microfarad fully charged can easily supply enough current to destroy a transistor which has inadvertently been caused to pass more than its rated current.

\section*{CONSTRUCTION}

The prototype was made up in an aluminium box with the controls mounted on the lid. The meter can be regarded as an optional extra, and is not essential,



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but it does give an indication of overload conditions. S3 is included as a means of switching off the D:C. from a circuit without switching off the powersupply, and could also be ignored.
The transformer is mounted on one long side of the box, which becomes the bottom. The output terminals were put at the side partly for preference, but also because the transformer makes it difficult to put them on the front panel in a convenient position.

Transistor \(\operatorname{Tr} 1\) is bolted to the rear of the box with the leads towards the inside, taking care that it is properly insulated with a mica washer from the case, and if possible, with a smear of heatsink compound or silicone grease on both sides of the mica to aid heat transference. The collector is the case, and connection is best made to this by passing a 6BA screw through the transistor then through the plastic bush which should be pushed through the box from the inside, and then putting a solder tag on before the securing nut. The other end of the transistor is treated in the same way, except that a washer should be substituted for the solder tag.

The other regulator components can be mounted on a piece of Veroboard. It is much easier to drill the 6BA clearance holes and make the breaks in the copper strips at the appropriate points before soldering any components in. It is probably better also to use the Veroboard as a template for drilling the mounting holes in the box rather than measure them out separately, since this should ensure that they line up.

Allowance has been made for four different values of resistor to be selected by S2. As long as the minimum value is not less than \(0.47 \Omega\), the other values may be almost any required value. Those shown give nominal values of \(1 \mathrm{~A}, 300 \mathrm{~mA}, 80 \mathrm{~mA}\) and 30 mA . Only R7 need be of 1 W rating, but small value resistors are not so easily available in carbon film, so 1 W wirewound should be used for values less than 10 ohms.
\(\star\) components list



FIg. 5: Layout of the components on the 0.15 in pitch Veroboard panel, and connections to the other components. Only one pole of S2 is shown though it is probably easier to use a 3 pole 4 way type.

The board should be stood off from the box by insulating spacers-4BA nylon nuts serve the purpose well.

Leave the interconnecting wires long enough from the board to allow them to reach the appropriate points on the front panel when this is removed from the box.

\section*{TESTING}

It makes sense to do the initial tests before the board is mounted in the box, as it saves the possibility of having to remove it again if anything is amiss. Check carefully that there are no solder splashes or copper whiskers bridging any of the strips. If all seems well, apply mains volts, and with no load applied, check that the output voltage varies in the correct direction as VR1 is rotated. If not recheck the circuit and component placings, then check that the voltage at the slider of VR1 varies as it is rotated. If the output remains high ( \(24-36 \mathrm{~V}\) ) although that at the slider varies, it could be due to a short in \(\operatorname{Tr} 1\) or \(\operatorname{Tr} 2\), or open circuit in \(\operatorname{Tr} 3\), D5, or \(\operatorname{Tr} 4\). If it is low, then the reverse is probably true, but make sure that there is about 36 V at the top of Cl before replacing transistors. When this part of the circuit seems to be working as it should. the next step is to check the current limiting section.

It is prudent to try it with a modest load first, rather than short the output terminals together and


The Veroboard panel showing the heatsink on Tr2.


Internal view of the completed Stabilised Power Supply.
hope that all is. well! Set the current limit switch to 300 mA , then find a load that will draw about 300 mA , say \(81 \Omega\), with VR1 set to give 24 V out. Check then that with the load applied the output voltage remains at 24 V . Remove the load and switch to the 80 mA and then 30 mA positions, then re-apply the load while monitoring the output voltage. If the current limiting is working correctly, the voltage should drop to around 6 V to 9 V , and if this is so, the output can then be shorted through a milliameter to see how far it is from the nominal 30 mA (or whatever value was aimed at). Each position of S2 can then be checked in the same way, by first choosing a value of load that would exceed the set current limit, but not enough to damage the regulator transistors in event of an error somewhere.

If all is well, the unit can be finally assembled and should then be ready for use by the constructor confident in the knowledge that used intelligently, it can provide a safe source of variable volts for test or experimental purposes.
..issue of P.W. containing Digitronic Solid State Digital Clock-A. A. Dyksman, 38 Harsley Road, Hartburn, Stockton-on-Tees, Teesside, TS18 5DJ.
..January 1971 issue of P.W.-J. Little, 1 Wellington Court, Wellington Road, Wanstead, London, E,11.
.P.W. for October and December 1973, January 1974.R. Cole, 54 Thorpe Place, Tattershall, Lincoln.
. Practical Television for August, September and October 1959, November 1955 and December 1956.-A. Cornish, 'Elsinore', Landscore Road, Teignmouth, Devon.
.P.W. June 1965. Also buy or borrow any issues containing information on or mods. to, the R1155.-M. Turner, 13 Churchill Way, Faversham, Kent, ME13 7RF.
. P.W. December 1972 with details of the Reverb Unit.Kjell Bergkvist, Vretgatan 25, S-781 00 Borlange, Sweden.
..June 1965 issue of P.W. with gen on the Hawaiian Guiter (including blueprint).-N. A. Danlel, 36 Hillcrest Drive, Little Sutton, Wirral, Merseyside, L66 4QD.
..issues of P.W. containing the \(10+10 \mathrm{~W}\) Amplifier (January 1973 onwards).-M. Cole, 4 Eastbourne Street, Lincoln, Lincs.

\section*{NEW MULLARD \& MAZDA VALVES}

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Each additional Valve add \(2 p\) in UK application.
\begin{tabular}{ll|l} 
DM70 & 0.69 & EF88 \\
DY86/7 & 0.58 & EF83 \\
DY802 & 0.53 & EF88 \\
EABC80 & 1.16 & EF86 \\
EB91 & 0.78 & EF89 \\
EBC81 & 0.89 & EF91 \\
EBF80 & 0.68 & EF92 \\
EBF83 & 0.66 & EF95 \\
EBF89 & 0.50 & EF183 \\
EGC86 & 0.82 & EF154 \\
EC88 & 0.86 & EH90 \\
EC90 & 0.94 & EL34 \\
EC97 & 0.69 & EL36 \\
ECC81 & 0.64 & EL84 \\
ECC82 & 0.53 & EL86 \\
ECC83 & 0.53 & EL95 \\
ECC84 & 0.68 & ELL80 \\
ECC85 & 0.78 & EM81 \\
ECC88 & 0.91 & EM84 \\
ECC189 & 0.77 & EM87 \\
ECF80 & 0.68 & EY51 \\
ECF82 & 0.90 & EY86/87 \\
ECF86 & 0.78 & EY88 \\
ECH81 & 1.29 & EZ80 \\
ECH83 & 1.06 & EZ81 \\
ECH84 & 1.17 & GY501 \\
ECL80 & 0.78 & GZ34 \\
ECL82 & 0.69 & PC86 \\
ECL83 & 0.72 & PC88 \\
ECL86 & 0.73 & PC97
\end{tabular}
\begin{tabular}{l|lr}
0.53 & PC900 & 0.65 \\
1.10 & PCC84 & 0.68 \\
0.58 & PCC85 & 090 \\
1.30 & PCC88 & 0.98 \\
1.30 & PCC89 & 0.73 \\
1.35 & PCC189 & 0.91 \\
1.51 & PCF80 & 0.63 \\
1.83 & PCF88 & 1.37 \\
0.69 & PCF86 & 0.73 \\
0.69 & PCF200 & 1.13 \\
0.91 & PCF 201 & 1.13 \\
1.06 & PCF801 & 0.73 \\
1.15 & PCF802 & 0.78 \\
0.68 & PCF806 & 0.78 \\
1.06 & PCE200 & 1.30 \\
0.78 & PCL82 & 0.63 \\
2.81 & PCL83 & 0.73 \\
1.24 & POL84 & 0.69 \\
1.34 & PCL85 & 0.72 \\
1.25 & PCL83 & 0.73 \\
0.89 & PCL805/850.78 \\
0.53 & PD500 & 2.11 \\
0.81 & PFL200 & 0.91 \\
0.68 & PL36 & 1.06 \\
0.53 & PL81 & 0.91 \\
1.30 & PL81A & 1.08 \\
0.91 & PL82 & 0.48 \\
1.05 & PL83 & 1.29 \\
1.05 & PL84 & 0.78 \\
0.68 & PL500 & 1.02
\end{tabular}

\(\qquad\)

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\begin{tabular}{|c|c|c|c|c|c|}
\hline AZ1 & 0.75 & EF39 & 1.25 & KTW61 & 1.50 \\
\hline AZ31 & 0.60 & EF80 & 0.85 & MU14 & 1.00 \\
\hline CBL31 & 140 & EF85 & 0.45 & N78 & 8.50 \\
\hline CL33 & 1.50 & EF86 & 0.60 & OA2 & 0.45 \\
\hline CY31 & 0.60 & EF889 & 0.85 & OB2 & 0.46 \\
\hline DAF91 & 0.40 & EF91 & 0.40 & PC86 & 0.65 \\
\hline DAF96 & 0.60 & EF92 & 0.50 & PC88 & 0.65 \\
\hline DCC90 & 1.85 & EF95 & 0.45 & PC97 & 0.55 \\
\hline DF91 & 0.40 & EF98 & 0.80 & PC900 & 0.65 \\
\hline DF96 & 0.60 & EF183 & 0.40 & PCC84 & 0.45 \\
\hline DK91 & 0.60 & EF184 & 0.40 & PCO88 & 0.68 \\
\hline DK92 & 1.00 & EL32 & 0.60 & \({ }^{\text {PCC89 }}\) & 0.65 \\
\hline DK96 & 0.75
0.50 & EL33 & 2.50 & PCCI89 & 0.85 \\
\hline DL92 & 0.50
0.48 & EL34 & 0.70 & PCF80 & 0.40 \\
\hline DL94 & 0.48
0.65 & EL36 & 0.60 & PCF82 & 0.48 \\
\hline DY86 & 0.45 & EL37 & 2.60
0.90 & PCF86 & 0.65 \\
\hline DY87 & 0.45 & EL41 & 0.80
1.65 & PCF801 & 0.60 \\
\hline DY802 & 0.47 & EL84 & 1.65 & PCF802. & 0.55 \\
\hline EABC80 & 0.88 & EL85 & 0.85 & PCF806 & 0.90 \\
\hline EAF42 & \(0 \cdot 70\) & EL95 & 0.60 & PCF806 & \(0 \cdot 80\) \\
\hline EB91 & 0.30 & ELL80 & 8.00 & PCF808 & 1.00 \\
\hline EBC33 & 1.00 & EM80 & 0.55 & PCL82 & 0.45 \\
\hline EBC41 & 0.75 & EM84 & 0.60
0.40 & PCL83 & 0.70 \\
\hline EBC81 & 0.40 & EM85 & 0 & PCL84 & 0.50 \\
\hline EBF80 & 0.40 & EM87 & 1 & PCL85 & \(0 \cdot 60\) \\
\hline EBF83 & 0.40 & EM8 & 1.00 & PCL86 & 0.60 \\
\hline EBF89 & 0.82 & \({ }_{\text {E Y }} \times 15\) & 0.45
0.45 & PCL805/8 & \\
\hline EBL31 & 2.00 & EY86 & 0.45 & & 0.60 \\
\hline ECC81 & 0.45 & EZ40 & 0.60 & PD500 & 1.60 \\
\hline E0C82 & 0.88 & EZ41 & 0.75 & PEN45 & 0.85 \\
\hline EC083 & 0.88 & Ez80 & 0.30 & PL36 & \(0 \cdot 68\) \\
\hline ECC84 & 0.85 & Ez81 & 0.81 & PL81 & 0.55 \\
\hline ECC85 & 0.45 & GY501 & 0.90 & PL82 & 0.50 \\
\hline ECC88 & 0.60 & GZ30 & 0.65 & PL83 & 0.50 \\
\hline ECH35 & 1.50 & GZ32 & 0.65 & PL84 & 0.50 \\
\hline ECH42 & 0.85 & GZ34 & 0.75 & PL500 & 0.85 \\
\hline ECH81 & 0.85 & QZ37 & 1.25 & PL504 & 0.85 \\
\hline ECH83 & 0.50 & HN309 & 1.50 & PL508 & 0.80 \\
\hline ECL 80 & \(0 \cdot 60\) & KT61 & 2.50 & PL509 & 1.55 \\
\hline ECL82 & 0.42 & KT66 & 2.95 & PL802 & 1.25 \\
\hline ECL83 & 0.75 & KT81 & & PX25 & \(3 \cdot 50\) \\
\hline ECL86 & 0.55 & & 1.30 & PY33 & 0.68 \\
\hline ECLL800 & 8.50 & KT81 & 1.75 & PY81 & 0.50 \\
\hline EFP37A & 1.20 & KT88 & \(3 \cdot 25\) & PY82 & 0.45 \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|c|}
\hline PY83 & 0.50 & 6 F 28 & 0.75 \\
\hline PY88 & 0.63 & 6J5M & 0.65 \\
\hline PY500 & 110 & 6J5G & 0.45 \\
\hline PY81/800 & 0.50 & \({ }^{85} 6\) & 0.85 \\
\hline PY801 & 0.55 & 8.J7G & 0.30 \\
\hline 8P41 & 3.00 & 6J7M & 0.65 \\
\hline SP61 & 0.85 & 8K6GT & 0.80 \\
\hline T41 & 1.00 & 8K7G & 0.85 \\
\hline U14 & 0.75 & 6K7M & 0.45 \\
\hline U25 & 1.00 & 6K8G & 0.45 \\
\hline U26 & 0.85 & 6 K 8 M & 0.70 \\
\hline U191 & 0.75 & 6K. 25 & 1.00 \\
\hline UABC80 & \(0 \cdot 40\) & 6.L6G & 1.25 \\
\hline UAF42 & 0.75 & 6Q7G & 0.40 \\
\hline UBC4I & 0.60 & 6Q7M & 0.60 \\
\hline UBC81 & 0.50 & 6SL7GT & 0.65 \\
\hline UBF80 & 0.50 & 68N7GT & 0.55 \\
\hline UBF89 & 0.50 & 68Q7GT & 0.40 \\
\hline UCC85 & 0.50 & 6U5G & 1.50 \\
\hline UCH42 & 0.80 & 6V8G & 0.80 \\
\hline UCH81 & 0.80 & 6V6GT & 0.60 \\
\hline UCL82 & 0.40 & 6X4 & 0.45 \\
\hline UCL83 & 0.70 & 6X5G & 0.45 \\
\hline UF41 & 0.75 & 6X5GT & 0.65 \\
\hline UF89 & 0.50 & 7B6 & 0.80 \\
\hline UL41 & 0.85 & 7B7 & 0.80 \\
\hline UL84 & 0.50 & 7C6 & 1.80 \\
\hline UY41 & 0.55 & 7 C 6 & 1.00 \\
\hline UY85 & 0.45 & 7H7 & \\
\hline VR105/30 & 0.40 & 7R7 & 0.80 \\
\hline VR150/30 & 0.45 & 787 & 8.25 \\
\hline 1RS & 0.50 & 7Y4 & 0.80 \\
\hline 185 & 0.40 & 12AT6 & 0.45 \\
\hline 1T4 & 0.40 & 12AT7 & 0.45 \\
\hline 384 & 0.60 & 12AU6 & 0.50 \\
\hline 3V4 & 0.85 & 12AU7 & 0.88 \\
\hline 5R4GY & 1.00 & \(12 \mathrm{AX7}\) & 0.88 \\
\hline 5U4G & 0.65 & 12BA8 & 0.50 \\
\hline \({ }^{\text {6Y3GT }}\) & 0.65 & 12BE6 & 0.80 \\
\hline 5Z4G & 0.65 & 30C1 & 0.40 \\
\hline 6/30L2 & 0.90 & 30 Cl 5 & 1.00 \\
\hline 6AK5 & 0.45 & 30 Cl 7 & 1.00 \\
\hline 6AM5 & 1.00 & 30 Cl 8 & 0.90 \\
\hline 6AQ5 & 0.60 & \(30 \mathrm{F5}\) & 1.00 \\
\hline 6AS7G & 1.00 & 30 FL 1 & 1.00 \\
\hline 6AT6 & 0.60 & 30FL2 & 1.00 \\
\hline 6AU6 & 0.40 & 30FL14 & 1.00 \\
\hline 6BA6 & 0.38 & \(30 \mathrm{Ll5}\) & 0.95 \\
\hline 6BE6 & 0.45 & \(30 \mathrm{L17}\) & 0.85 \\
\hline 6BH6 & 0.75 & 30P4MR & 1.80 \\
\hline 6BJ6 & 0.76 & \(30 \mathrm{P12}\) & 1.00 \\
\hline 6BQ7A & 0.65 & 30P19 & 0.85 \\
\hline 6BR7 & \(1 \cdot 20\) & 30 PL 1 & 0.95 \\
\hline 6BS7 & 1.40 & 30PL13 & \(1 \cdot 10\) \\
\hline 6BW6 & 1.00 & 30 FLIL 4. & 1.10 \\
\hline 6BW7 & 1.00 & 35 W4 & 0.60 \\
\hline 6C4 & 0.40 & 35Z4GT & 0.70 \\
\hline 6CD6G & 1.60 & 50CD6 & 1.20 \\
\hline 6CH6 & 1.50 & 807 & 1.00 \\
\hline 6CW4 & 1.00 & \(8131 T T\) & 14.00 \\
\hline 6F23 & 0.90 & 813 USSR & 8.00 \\
\hline 6 F 25 & 1.00 & 866A & 1.20 \\
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\end{tabular}

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4

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\begin{tabular}{l} 
EXPRESS \\
POSTAGE \\
12p per order in UE \\
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\end{tabular}
\begin{tabular}{ll|ll} 
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AAZ13 & 0.12 & BD131 & 0.4
\end{tabular}

全


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\[
\begin{aligned}
& \text { OAP1 } \\
& \text { OA200 } \\
& \text { OA209 }
\end{aligned}
\]
\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline SN7400 & \(0 \cdot 16\) & SN7428 & 0.40 & EN7486 & 0.47 & SN74145 & 1.26 & & \\
\hline 8N7401 & 0.16 & 8N7430 & 0.16 & SN7490 & 0.55 & SN74150 & 1.75 & SN74182 & \[
\begin{aligned}
& 2.00 \\
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\] \\
\hline SN7402 & 0.16 & SN7433 & 0.37 & 8N7491AN & & SN74161 & 1.00 & SN74194 & 2.00
1.30 \\
\hline SN7403 & 0.16 & SN7437 & 0.37 & & 1.00 & SN74154 & 8.00 & SN74198 & 1.10 \\
\hline 8N7404 & 0.26 & GN7438 & 0.37 & SN7492 & 0.70 & SN74155 & 2.00 & SN74196 & 1.10
1.20 \\
\hline SN7405 & 0.22 & 8N7440 & 0.22 & SN7493 & 0.70 & 8N74156 & 1.00 & SN74197 & 1.20 \\
\hline SN7408
SN7407 & 0.42 & AN7441AN & & SN7494 & 0.80 & 8N74157 & 0.95 & SN74198 & 2.77 \\
\hline SN7407
SN7408 & 0.42
0.28 & & 0.82 & SN7495 & 0.80 & gN74170 & \(2 \cdot 62\) & SN74199. & \(2 \cdot 52\) \\
\hline SN7408 & 0.28
0.28 & 8N7442
SN7450 & 0.79
0.16 & SN7496 & 0.85 & SN74174 & 1.57 & & \\
\hline SN7410 & 0.16 & GN7451 & 0.16 & SN74100 & 8.87
1.89 & SN74176 & 1.10
1.28 & & \\
\hline GN7411 & 0.25 & SN7453 & 0.16 & SN74107 & 0.45 & SN74176
SN74190 & 1.26
8.00 & & \\
\hline 8N7412 & 0.30 & gN7454 & 0.16 & 8N74110 & 0.68 & 8N74191 & 2.00
8.00 & & \\
\hline SN7413 & \(0 \cdot 36\) & SN7460 & 0.18 & GN74118 & 0.90 & SN7491 & & & \\
\hline SN7417 & 0.36 & AN7470 & 0.88
0.41 & SN74119 & 1.68
0.50 & D & & & \\
\hline SN7420 & \(0 \cdot 16\) & gN7474 & 0.42 & 8N74122 & 0.70 & D & & 14 pin & \\
\hline SN7422 & 0.25 & SN7480 & 0.60 & SN74123 & 1.00 & & & & \\
\hline SN7423 & \(0 \cdot 37\) & SN7483 & 1.10 & SN74141 & 0.90 & SOCK & & 6 pin & \\
\hline
\end{tabular}

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Electrolytics. \(32 / 32 / 32 / u \mathrm{~F}, 325 \mathrm{v}, 2^{\prime \prime} \times\)
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Ferguson Stereogram Chassis. MW/ LW: VHF with tuning scale ( \(5+5\) watts sine wave) 15 ohms \(\mathbf{£ 2 6} \mathbf{- 2 5}\). Post paid 15 ASSORTED SWITCHES \(81 \cdot 90\) + post. \(50-3\) way to 7 way TAG STRIPS, \(£ 1 \cdot 15+\) post, ALMA REPANCO \& DENCO COILS. NEW BOXED OUR SELECTION-. 5 FOR £1-15 + post.
Please add \(10 \%\) post and packing. Add \(25 \%\) VAT to total order. Gram Chassis free postage. No goods despatched outside U.K.

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"H.A.C." SHORT-WAVE PRODUCTS P.O. BOX NO. 16, EAST GRINSTEAD, NO. 18, EAST GRIN
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\section*{Gamages of 嘖olborn}

TERE is a name which still brings many memories of the good old daysGamages of Holborn. How many of you remember the adverts in the popular radio magazines of the early twenties where Gamages used to advertise, "Valve or crystal, complete set or smallest accessory, you cannot go wrong at Gamages. Stocks are so complete, prices for warranted apparatus so keen, and the firm's desire to help the Amateur so genuine, that it would seem almost folly to go elsewhere".

Alas, the site where Gamages of Holborn stood until a couple of years ago is now a great gaping hole filled with men, machinery and dust preparing the area for, I suspect one of those concrete architect's nightmares which abound in such great profusion in London today.

So, with a little bit of imagination and a few pictures, let's try to conjure up a bit of the magic of 1923 by seeing what A. W. Gamage had to sell in March of that year.
The Gamage Crystal Receiving


Set, fully licensed by the Post Master General had the Reg. No. 226. The tuning coil was said to be wound with the best quality wire and tapped in four places. This, when used in conjunction with the variable condenser, which was of the 'best possible workmanship', gave a good variation of tuning. The crystal detector, designed to prevent dust from deteriorating the sensitivity of the crystal, contained

Gamage's famous 'Permanite' crystal 'which had given such excellent results'. The task of finding a sensitive spot on the crystal was minimised by means of a buzzer. The adverts used to read, 'This set will receive telephony for 30 miles and signals from spark stations, using a wavelength of \(300-500\) metres for \(150-200\) miles. Complete in polished mahogany cabinet, with instruments mounted on polished Ebonite, also with phones, aerial wire and the insulators, this set costs \(£ 4\) 19s 6d.'

The 'Sonus' two-valve Broadcast Receiver consisted of one high frequency , and one detecting valve. Telephony from broadcasting stations up to 100 miles away could be satisfactorily received on 'telephones' and low frequency amplifying valves could be added to increase the volume of music for the purposes of operating a loudspeaker or several pairs of 'phones. The number of low frequency valves required, depended
on the distance of the set from


Above: the Gamages "Sonus" two-valve receiver.
Left : Gamages Crystal Receiving Set, complete with accessories.
the transmitting station.
Music and speech were claimed by Gamages to be exceptionally clear on this broadcast receiver, which was designed to work on an 'average' aerial and had a wave range of 300 to 3,000 metres which enabled the owner to receive the well known time signals from Paris. The range of reception of spark transmissions was said to be between 150 and 2,000 miles. Price, complete as shown was £21.



\section*{by Eric Dowdeswell G4AR}

AFEW words this month on something that has worried me for some time past. Extracts from readers' logs are published in all good faith but my credulity is rather stretched when someone reports a real bit of weak DX received on a onetransistor receiver and a bit of wet string! I am exaggerating a bit, but not much!

It is obvious to me that this situation arises when a reader sits on the frequency of a powerful European station, logging the DX stations as he works them. The listener no doubt does hear something of the DX too and so he logs it. No trouble with the callsign of the DX because the European is using it! The problem arises when the listener can't hear the DX but logs it nevertheless!
So next time you begin to \(\log\) a juicy bit of DX ask yourself if you can really hear him well enough to get his callsign, at least, without the assistance of that European,' and don't log him if you can't! Self-deception is a futile pastime and brings no satisfaction.

Those of you who live in Surrey should watch out for CATS! The newly-formed Coulsdon Amateur Transmitting Society meets the first Thursday of each month at the 10th Purley Scout Group Hut. This is opposite Rickman Hill on the Chipstead Valley Road, Coulsdon. First in the queue to join ranged from 11 to 72 apparently so that ought to cover most of our readers in Surrey. For more info send an SAE to Nick Moyes G8KMJ, 23 Ellenbridge Way, Sanderstead, Surrey CR2 OEW.

Mark Hill (Birmingham) deserted the HF bands to log some interesting stuff on 2 m aided by a halo, all via Oscar 7. Mark who lives at 114 Green Lane, Castle Bromwich, Birmingham would appreciate information on a design for a mobile whip covering the 80 and 160 m bands. Jeremy Hinton (Newcastle, Staffs) took his Trio 9R59DS on holiday but had to be content with a metal door frame for an aerial! He's swotting for the RAE in December and getting on well with the code. He is very rightly annoyed to find the local radio club night clashes with the RAE course at the local college. Looks like a lack of communication to me!
T. H. Bithell (Chester) for many years an ardent reader of PW plucked up enough courage to drop me a line on his doings. In the last three years he
has built up 19 kits by you-know-who and has nine tape recorders! He did at last get round to the Heathkit (I've said it!) HR-10B which led to his interest in this column. He's logged over 2000 stations in a few weeks, mainly on 20 and 80 m . However, as I have told him, I hope diplomatically, it's the quality and not the quantity that counts!

Shaun O'Sullivan (Bristol) has just managed to get his 11th ' \(O\) ' level and has at last turned to amateur radio. About time, too! He's pleased with the PW Microtune plus 80ft of wire. Martin Kessel (Stoke) copies SSB the hard way with an old HMV 5 -valve superhet plus a 1 -valve superregen as the BFO! Oh-er! Concentrates on 20 and 80 m but it must be very hard work. Stephen Terry (Banbury) stuck to 15 m with his FR50B and dipole for that band, an unusual one being VK9XK on Christmas Island, the one in the Indian Ocean if I remember aright. I still have a QSL from him when worked from ST2AR years ago.

Michael Bennett (Slough) spread his effort over 10 to 80 m albeit all on SSB. I particularly liked KH6INV on KS6 on 20m and CM6AI on 10m. Regular Alan Rae (Glasgow) has done it! Apart from succeeding in his Higher level exams he is madly waving his GM8KRO ticket around. Caught without any gear he persuaded friend GM4DHJ to bring round some 2 m gear to make his first QSO from home. Wisely the code is now receiving attention and feelers are out for an HF bands transceiver. Glad you didn't forget us, Alan!
Anent Peter Walton A9002 in the last issue he rebukes me because his full QTH is 55 letters long! He'd just quoted the abbreviated form! It's that one that starts at one end of the railway platform and goes on to the other! His 359X, dipole and PR30 preselector worked mainly on 20m. 'Dick' Dickens writes from 'Steptoe' land, Shepherds Bush, London, about his 'PCR4' being his rebuilt version of the PCR3, preceded by a PW preselector and ATU. The aerial goes out with the washing line! Peter Allen A8677 (Taunton) is very happy with his PR30 preselector which has made a great difference to all signals. Andrew Swiffin A8603 (Cheadle) is another who cannot be parted from his rig, taking a solid state receiver and loaded whip to GM land.

\section*{Log extracts (All SSB)}
A. Swiffin:- 20m FP0YY (QSL K90TB) KG6KD/ KB6 KB6BU KC6MW WA8VYV/KL7 VP2MCT5T5BJ C9MIC
P. Allen:- 80m ZL3GS 20m 9Y4RH 15m CE7BDW VP2MCT ZS1EZ ZP5AO ZS4BU JA5EUQ

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MEDIUM WAVE DX by CHARLES MOLLOY

THE DX season for Asiatics extends from November until February and, during this period, medium wave reception of India, Pakistan, China and parts of the Far East becomes possible in the UK. There are two times of the day to listen for these stations-in the afternoon during the hour before sunset and again between midnight and 0300 GMT when many broadcasters sign-on for the day as local sunrise approaches. The Voice of America outlet at Ban Pachi in Thailand on 1580 kHz is often audible between 1600 and 1700 GMT. Hofei in China has been heard recently on 940 kHz while Kabul in Afghanistan on 1280 kHz is logged regularly until it becomes submerged in European QRM as darkness approaches. The period between midnight and 0300 can be very rewarding. Two Chinese stations, Urumchi on 740 kHz and an unknown outlet on 1310 kHz , are heard frequently between midnight and 0100. All India Radio signs-on after 0100. Listen for Indore on 650 kHz , Jullunder on 710 kHz , Rajkot on 1070 kHz and Calcutta on 1130 kHz . Pakistan is well represented with Quetta on 750 kHz , Multan on 1030 kHz and Hyderabad on 1010 kHz . All of these stations can be heard in the UK with a communications receiver such as the CR100 or the AR88 and a medium wave loop or an outdoor longwire antenna.

Malcolm Laugharne writes from Witney to ask if it is possible to purchase a MW loop aerial. So far as the writer knows this type of aerial is not available commercially and the DXer will have to follow the example of A. B. G. Hall (Daventry) who is
building a loop for himself. Steve Howell (Bristol) wonders if the World Medium Wave Guide is still available. This handy list of medium wave stations is now published as part of the World Radio TV Handbook, which comes out annually, usually in January.

The winter season on the medium waves is now in full swing. Conditions, which are better now than they have been for several years, will continue to improve as we approach the minimum of the current sunspot cycle. North American medium wave stations should become prominent from 2330 until 0300 GMT, when QRM from Eastern Europe starts to build up. North American medium wave stations are allocated callsigns which they use frequently, followed by the name of the city or town where the studios are located, so identification is seldom a problem. Nearly all North Americans are good verifiers and will answer a correct reception report with a QSL card or a letter. Reports should give the date and time of reception along with programme details such as station slogans, commercials, weather reports, announcers' names. Return postage in the form of an International Reply Coupon should always be sent as the DXer is well outside the station's normal coverage area.

The more prominent North Americans heard in the UK include WABC on 770 kHz , WCBS on 880 kHz , WINS on 1010 kHz and WNEW on 1130 kHz , all in New York City; WHDH on 850 kFz and WBZ on 1030 kHz both in Boston, WCAU on 1210 in Philadelphia, WBAL on 1090 kHz in Baltimore, KDKA 1020 kHz in Pittsburg and WKBW 1520 in Buffalo. Many Canadians can be heard. Search for CBN 640 kHz and CJON 930 kHz from St. John's in Newfoundland, CHER 950 kHz in Sydney N.S. CHNS 960 kHz in Halifax, CBA 1070 kHz in Moncton and CBI 1140 in Sydney.

\section*{SHORT WAVE BROADCASTS} by Derek Bell

THERE'S a pub in Kent that is worthy of a pilgrimage according to R. I. Macmillan of Deal. Standing on the bar of this hostelry is a 1934 HMV radio that is in working order and a contestant for this column's "oldest working short wave set" title! Mr. Macmillan (sorry, no other names given) recently repaired this \(R X\) and describes it as a five valve straight set. When the dust was removed from the interior, the chassis and all the valve "cans" were found to have been painted matt black by the maker.

Having repaired it R.I. hooked on a six metre longwire and pulled in Voice of Turkey on 31 m at 2300 and VOA (Tangiers on \(31 \cdot 8 \mathrm{~m}\) at 2255 and something described as National Public Radio at 2231. This latter is something of a puzzle to me and I would be interested in more details. The Voice of Turkey logging is in fact the relay of the Turkish home service on 1061 kHz transmitting from Diyarbakir with 300 kilowatts. Thus, having shall we say, "knocked out" Dr. Brodribb's set recently featured in the column, its "any advance" on 1934 for the oldest set in use!

Several questions are asked by Brian Buckley from County Tyrone, Northern Ireland. First, the transmission times of NHK Radio Japan are listed in WRTV Handbook as 0100 to 0130,0200 to 0230 , 0300 to 0330 and so on with half-hourly gaps for

the whole 24 hours on \(9585,15105,17880,15195\), 9505, 17855 and 5990, the frequencies altering and rotating as the target area is altered. The best times for the UK are generally thought to be from 0600 to 1000 depending on propagation conditions. So the thing to do is to try all the frequencies mentioned above until you strike gold, then write for the QSL to Radio Japan NHK 2-2-1 Jinnan Shibuya-Ku Tokyo, which deals with the second question.

Brian says that he has fitted a socket to his Bush VTR178 to take a TV aerial, presumably the one on his chimney and can pull in Radio Australia, Pekin, Kuwait and WYFR. The Radio Australia service mentioned is the South-East Asia one on 9770 and Brian logs it from 1600 to the sign-off at 1730 . I personally feel that the TV aerial would only be effective for the TV bands and that it might be better to use the socket for a long wire provided the aerial input circuitry is not overloaded.

As to the final question Brian I don't think it would be ethical for me to say which sets I use since I see this column as a medium for the exchange of tips, ideas and news and I would not want to influence anyone or perhaps I should say inflict anyone with my personal likes and dislikes.

Bad news is in the air in more ways than one lately. Anthony Street from Braintree writes that he heard Radio Canada announce that as from November they were "having to stop the Short Wave Club" but they would merge it with the Mailbag Show. Anthony is another reporter of Voice of Turkey, this time on 11880, the overseas service and is a 250 kW station from either Izmir or Erzurum. The QSL address is TRT Turkiye Radyo Televizyon Kurumu, Genel Mudurlugu, Ankara.

For those who have wondered exactly what is put
on a QSL card Paul Cowburn from Leyland, Lancs, can fill us in. He is the proud possessor of a Radio Nacional de Brasil card and sends the details which, in brief, are that the transmitter power is 250 kW and that the aerials are 31,25 and 19 metre rhombics, situated 55 km northwest of Brasilia. The trans: mitting equipment is made by Brown Boveri of Switzerland and puts out a signal on 9605,11780 and 15245 at 2200. When not in use for the overseas service the transmitter puts out a domestic service "Avoz da Brazil" Paul gives the address as Radio Nacional de Brasillia, International Service, PO Box 07/0173, Brasillia Federal District, Brazil.

Next we hear from Nicholas Try from Gerrards Cross who mentions hearing Radio Nacional de Espania on 9515 at 1900; not in itself great DX but how many QSL collectors I wonder bother with the Europeans? For those of us that are pop fans, for instance, AFRTS puts out the American top-of-thepops every Saturday night over their German transmitters and there is a "night owl" show that I am told is of a very free and easy nature from RAI in Italy. While these are local it must be remembered that in certain propagational circumstances even Radio Nederland cannot be heard here in the UK.

Speaking of B. Nederland I recently heard a jingle put out by the BBC stating that Radio One was "The Happy Station" I wonder what RN will reply to that!

Its time to draw stumps for this month alas so all I can say is good DX and 73s to you and yours

\section*{BROADCAST EANOS}

Short Wrve 1 egots by the \(15 t h\) of he manth to Derek Belf cho Rraxtical Whreless. Feetway House Fazing den Street London, EC4A 4AD. Medium Wave Logs to Charles Molloy, 132 Sogars KHe, Southpot PR835S

\section*{AMATEUR BANDS}
stogis covelina any, watebr band/s in bandi
 Eric Dovdeswell G4AR, Silver Firs, Leatherhead Fiosid, s3ntead. Surfey KCT \(212 T \mathrm{~W}\).

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& \text { (watts) }
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Complete with crossover Components and circuit diagram

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Complete with crossover Components and circuit diagram


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250V: \(0.05 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 6 \mathrm{p} .0 \cdot 25,6 \mathrm{p}_{7} 0 \cdot 5 \mu \mathrm{~F}, 7 \frac{1}{2} \mathrm{p} .1 \mu \mathrm{~F}, 9 \mathrm{p} .500 \mathrm{~V}\) :


\section*{LEIGHTON ELECTRONICS CENTRE}

Our new Electronics Centre is now open in Leighton Buzzard and all callers are welcome. As well as our normal stock of over 3000 product Jines, we have a large range of surplus equipment, Bargains, Calculators, etc. OPEN 6 DAYS 9 to 5 (sh ut
12.30 to 1.30 ).

20

ASSORTED RESISTORS. Carbon and Carbon Film Types. 4 Watt to 3 Watts ( 25 different valves). \(\quad 300\) for only \(\mathbf{E} 1 \cdot 50\) FIRST GRADE TRANSISTORS all Branded.
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also
\(\mathrm{BCI47}, \mathrm{BCI48}, \mathrm{BCl} 49, \mathrm{BCI57}, \mathrm{BCI58}, \mathrm{BCI59}, \mathrm{BF194}, \mathrm{BF195}\), BF196, BF197

Bp each or 100 for \(\mathbf{E 6} 50\) IN4148 Diodes \(\quad 50\) for only \(\mathbf{E I} \cdot 25\) A Amp Diodes. IN4001, IN4002, IN4003, IN4004, IN4005, IN4006 6p each, 30 for \(\mathbf{E 1} \cdot 50\) Assorted Polyester Capacitors by Mullard, Erie, etc.

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NEW T AMEAICAN TYPE CRADLE TELEPHONE AMPLIFIER


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Everest Instruments Ltd.
34, Shakespeare St., Nottingham. Tel. (0602) 45466
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\hline Mid. & Volts & Pence \\
\hline 47 & 4 & 7 \\
\hline 330 & 4 & 7 \\
\hline 68 & 6.3 & 7 \\
\hline 470 & \(6 \cdot 3\) & 9 \\
\hline 1000 & 6 & 11 single end p/c ftting \\
\hline 25 & 10 & 7 \\
\hline 47 & 10 & 7 \\
\hline 220 & 10 & 7 \\
\hline 330 & 10 & \(\$\) \\
\hline 15 & 16 & 7 \\
\hline 33 & 16 & 7 \\
\hline 68 & 46 & 7 \\
\hline 220 & 16 & 9 \\
\hline 220 & 16 & 9 single end p/c fiting \\
\hline 330 & 16 & 12 \\
\hline 1000 & 16 & 29 \\
\hline 10 & 25 & 7 \\
\hline 22 & 25 & 7 \\
\hline 47 & 25 & 7 \\
\hline 100 & 25 & 7 \\
\hline 150 & 25 & 9 \\
\hline 200 & 25 & 11 \\
\hline 1250 & 25 & 24 single end can \\
\hline 5000 & 25 & 55 single end can \\
\hline \(1000+1000\) & 30 & 32 single end can \\
\hline 2500 & 30 & 40 single end can \\
\hline \(6 \cdot 8\) & 40 & 7 \\
\hline 16 & 40 & 7 \\
\hline 100 & 40 & 9 \\
\hline 1000 & 50 & 35 single end can \\
\hline 4 & 63 & 7 \\
\hline \(4 \cdot 7\) & 63 & 7 \\
\hline 10 & 63 & 7 \\
\hline 32 & 63 & 7 \\
\hline 800 & 63 & 32 single end can \\
\hline 4700 & 63 & 140 single end can \\
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\hline \multicolumn{10}{|l|}{35 PARK AVENUE, POTTERS BAR, HERTS. O1-882 4355} \\
\hline \multicolumn{5}{|l|}{MAIL ORDER ONLY} & & \multicolumn{4}{|l|}{CASH WITH ORDER, OR PHONE US} \\
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\hline \({ }^{\text {AC126 }}\) & & BCY & 27 p & 2N697 & 14p & 2N2926 & & R.C.A. & \\
\hline \({ }_{\text {ACl2 }}\) & \({ }_{1}^{15 p}\) & \({ }_{\text {BCY }}{ }^{\text {B }} 8\) & 25 p & 2N698 & & 2 N 3053 & & \({ }_{40309}\) & 30p \\
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119 & 2N3054 & 42p & 40310 & 80p \\
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\hline ACY17 & 28p & \({ }_{\text {BF183 }}\) & 33p & 2N916 & \({ }_{30}^{240}\) & \({ }^{2} \mathbf{N} 3614\) & 60 p & 40315 & ( \\
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19 p & \({ }^{2 N} 1131\) & \({ }_{20 \mathrm{p}}^{20 \mathrm{p}}\) & 2N3704 & 110 & \({ }_{T T I P 335}\) & \({ }^{80 \mathrm{p}}\) \\
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18 & \({ }_{\text {BFX }}\) & 30 p & \({ }^{2} \mathrm{~N} 1305\) & 23p & 2N3710 & 111 & \({ }_{6} \mathrm{Amp}\) & 28p \\
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\hline AF139 & 32 p & BFY11 & 20 p & 2N1308 & 27 y & 2N3771 & £1.10 & & \\
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\hline \({ }_{\text {BC108 }}\) & 10 p & BFY51 & 19 p & 2N1671B & 21.00 & 2N3819 & 25 p
70 p & \({ }^{2 A}, 600 \mathrm{~V}\) & V 48 p \\
\hline \({ }^{\mathrm{BC}} \mathbf{0} 109\) & \({ }^{10 p}\) & BFY64 & \({ }^{2}\) & 2N2217 & \(21 p\) & \({ }_{2}^{2 N 3866}\) & & 4 AA,
\(6 \mathrm{~A}, 100 \mathrm{~V}\) & \({ }^{655 p}\) \\
\hline \({ }_{\text {BC113 }}\) & \(11 p\)
\(13 p\) & BFY90 & 72 p
150 & 2N2218 & 20p & \({ }_{2} \mathbf{2 N} 39004\) & 14p & 6A, 10 & 65 \\
\hline BC114 & 148 & BSX 26 & 22p & 2N2290 & 18p & \({ }^{2 N} 3905\) & 15p & S.C.R.s & \\
\hline \({ }_{\text {BC115 }}\) & 13p & \({ }_{\text {BXX }}^{\text {B }}\) (27 & 26 p & 2N2303 & 75 & \({ }_{2}^{2 N} 4066\) & 12p & 1/05 & 80 p \\
\hline \({ }_{\text {BC116A }}\) & 14 p & \({ }^{\text {B }}\) BU108 & \({ }^{12} \mathbf{2}\) 25 & \({ }_{2}^{2 N 2369} 23 \mathrm{~A}\) & 13p & 2N545 & 27p & 1/20 & (1) \\
\hline BC117 & 18 p & MEF103 & 325 & 2N2369A & 15p & OA81 & 15p & 16/400 & 0, \\
\hline BCI18 & 10p & MJ480 & 750 & & 44p & OC20 & 21.00 & 16/600 & 21.20 \\
\hline BC119 & 22p & MJ481 & 95p & \({ }_{\text {2N2846 }}\) & 70p & \({ }^{0} \mathbf{C} 28\) & 58 p & & \\
\hline BC134 & 12p & MJ490 & 855 & 2N2894 & 35 p & OC85 & 50p & Triacs & \\
\hline - \({ }_{\text {BC136 }}\) & 16 p
160 & MJE371 & 60 D & \({ }^{2 N} 2904 \mathrm{~A}\) & 45p & OC35 & 48 p
50 p & SC40D & 21.05
21.80 \\
\hline BC138 & 16 p & & 15 & 2N2905 & 22 D & OC71 & 30p & SC45E & 21.45 \\
\hline BC153 & 17 p & MJE2955 & & 2N2906 & 14 p & 0 C 83 & 20p & SC50D & 21.50 \\
\hline \({ }_{\text {BC167R }}\) & 17 p & & 81.00 & 2N2906A & 16p & OCP71 & 75p & & \\
\hline \({ }_{\text {BC183L }}^{\text {BC1 }}\) & \(12 p\)
\(10 p\) & MJE3055 & 65p
30 p &  & 16p & PTX 107 & 8y &  & 250 \\
\hline \multicolumn{10}{|c|}{Mullard Hi-Stab 4 watt resistors, \(2 \frac{1}{2} \mathrm{p}\) each} \\
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each; \(2 \cdot 5 \mathrm{Ah}\), \(1 \cdot 2 \mathrm{~V}\), \(£ 3 \cdot 49\) each. Ultra each; \(2 \cdot 5 \mathrm{Ah}, 1 \cdot 2 \mathrm{~V}, ~ £ 3 \cdot 49\) each. Ultra
heavy duty, \(6 \mathrm{Ah}, 1 \cdot 2 \mathrm{~V}\) ( 60 amps for heavy duty, 6Ah, \(1 \cdot 2 \mathrm{~V}\) (60 amps for
5 mins.) \(\mathrm{t} 5 \cdot 71\) each. Special 9 V tran5 mins.), t5-71 each. Special 9V tranf3. 60 each. Current limiting chargers from eas.09. Further information and sales from Sandwell Plant Ltd., I Denholm Road, Sutton Coldfield, West Midlands. 0213549764.


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Chesterfield Road, Sheffield 58 .

\footnotetext{
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Polystyrene \(3 p . ~ T a n t a l u m ~ 11 p . ~ Z e n e r s ~\)
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MULTIBAND RADIOS. Grundig Satellit, 13 band, £158. BF8 Unit, £15. Koyo marine, aircraft, PSB, FM, SW1/2, MW, LW, E55. Multi 5 (MW, FM, SW, aircraft, PSB), £17. Sharp' (MW/aircraft), £13.. Langtons, High Street, Rowester, Staffs. Sae lists.
brand New, Inclusive Prices, SAE for lists. 562 PLL \(£ 2 \cdot 90,500112\) digit calc. £4.10, 53146 digit clock \(£ 6 \cdot 15\), MAN7 7 seg . LED fle00, Mail order, MELLOW ELECTRONFICS, 5 Sheepcot Mrive, Watford, Herts.

Practical Wireless, December 1975

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For Black and White TV, Radios, Record Players and Tape Recorders 50p Please send large Stamped Addressed Envelope. COLOUR MANUALS
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Mail order or phone 01-458 4882
no overseas mail please

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250V: \(0.01,0.015,0.022,0.033\) \begin{tabular}{l} 
250V: 0.01, 0.015, 0.022, 0.033 3p; 0.047, 0.068, 0.14p;0.156p; \\
\(0.22,0.337 \mathrm{p} ; 0.479 \mathrm{p} ; 0.6810 \mathrm{p} ; 1.014 \mathrm{p} ; 1.522 \mathrm{p} ; 2.224 \mathrm{p}\). \\
\hline
\end{tabular} ELECTROLYTIC CAPACITORS. Axlal lead type (Values ate In \(\mu\) i)
\(63 V: 0 \cdot 47,1 \cdot 0,1 \cdot 5,2 \cdot 2,3 \cdot 3,4 \cdot 7,6 \cdot 8,40.15,20,22,47,6 p: 68,10 p: 10042 p\)
 \(840,78 p ; 1000,24 \mathrm{p}\); 2200, 34p. 3000, 39p; 4700, 47p; 18V: \(40,125,250,6 \mathrm{p}\); 1000,1500, 18p; 10V:4,100,5p;640, 10p; 1000, 14p; 2200, 18p.


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Dlelectric 80 s
\begin{tabular}{lr|l} 
lopp & 80p & 45 \\
300 pF & \(88 p\) & 00 \\
500 pF & 95 p & 00 \\
DHemin & & C \\
300 pF & 125 p & C
\end{tabular}

6:1 Ball Drive
4511/DAF \(500 \mathrm{pF} \quad 88 \mathrm{p}\) \begin{tabular}{ll|} 
& \\
300 pF & 125 p \\
500 pF & 195 p
\end{tabular} \(\begin{array}{ll}00-365 & 240 \mathrm{p} \\ 00-208 / 176 & 240 \mathrm{p} \\ \mathrm{CBO4-15pF} & 118 \mathrm{p} \\ \text { C804 }\end{array}\) \(\begin{array}{ll}\text { C804-25pF } & \text { 118p } \\ \text { 118p }\end{array}\)
CERAMIC TRIMMER
CAPACITORS
\(2-7\) PF \(_{4-15 p F ;}^{6-25 p F}\) 2-7pF: \(4-15 p F ; 6\)
\(8-30 \mathrm{pF} 17 \mathrm{peach}\) MINIA TURE 2-10pF: 3-30pF; 10-40p F COMPRESSION TRIMMERS
\(3-40 \mathrm{DF}\) \(3-40 \mathrm{pF}\)
\(20-250 \mathrm{pF}\) \(20-250 \mathrm{pF}\)
\(100-500 \mathrm{pF}\) DAU TRIMBERS minlature \(5-25 \mathrm{pF} \quad 20\) With Cord and Jack Plug Magnetic
2.5 mm 2.5 mm plug
3.5 mm plug Crystal
3.5 mm plug 45p
15p
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline \multicolumn{3}{|r|}{JACK PLUGS} & \multicolumn{2}{|l|}{SOCKETS} & \multicolumn{2}{|l|}{\multirow[t]{2}{*}{CERAMIC TRIMMER CAPACITORS
\[
2-7 \mathrm{pF} ; 4-15 \mathrm{pF} ; 6-25 \mathrm{pF} ;
\]
\[
8-30 \mathrm{pF} 17 \mathrm{p} \text { each }
\]}} \\
\hline \multirow[b]{2}{*}{2.5 mm} & \multicolumn{2}{|l|}{Screened Plastic} & Open & Moulded & & \\
\hline & 10p & 8p & metal & break & \multicolumn{2}{|l|}{MINIATURE} \\
\hline 3.5 mm & 14p & 10 p & 8p & contacts & \multicolumn{2}{|l|}{2-10pF: 3-30pF; 10-40pF} \\
\hline \multirow[t]{2}{*}{Standard Mono Standard Stere} & \(\bigcirc 19 p\) & 3p & 13p & \(17 \mathrm{\rho}\) & \multicolumn{2}{|l|}{\multirow[t]{2}{*}{COMPRESSION}} \\
\hline & eo 32p & 18p & 15p & 17p & & \\
\hline TRIA & \multicolumn{2}{|l|}{OIN} & ugs & Sockets & \multirow[t]{4}{*}{\[
\begin{aligned}
& 3-40 \mathrm{pF} \\
& 20-250 \mathrm{pF} \\
& 100-500 \mathrm{pF} \\
& \text { DAt TRIMBERS } \\
& \text { mlnlature } 5-25 \mathrm{pF}
\end{aligned}
\]} & \(18 p\)
27p \\
\hline \multirow[t]{4}{*}{3 A 400 V 100 p 6A 400V120p 6 A 500 V 150 D 10A 500V 165p} & \multicolumn{2}{|l|}{\multirow[t]{3}{*}{\begin{tabular}{l}
2 pIn Loudspeaker \\
\(3,4,5\) ( \(180^{\circ} \& 240^{\circ}\) ) \\
6pln Audlo type
\end{tabular}}} & & & & 32 p \\
\hline & & & & & & \\
\hline & & & & P & & 20p \\
\hline & \multicolumn{2}{|l|}{CO-AXIAL (TV)} & p & 8p & \multicolumn{2}{|l|}{\multirow[t]{2}{*}{EARPHONES With Cord and Jack Plug Magnetlc}} \\
\hline & \multicolumn{2}{|l|}{PHONO} & & & & \\
\hline \multirow[t]{3}{*}{TERMINAL POST 4 mm 20p each} & \multicolumn{2}{|l|}{\multirow[t]{2}{*}{assorted colours Metal screened}} & & 7p (dbli) & \multirow[t]{3}{*}{\begin{tabular}{l}
2.5 mm plug 3.5 mm plug Crystal \\
3.5 mm plug
\end{tabular}} & 45p \\
\hline & & & & 10p (trpl.) & & \\
\hline & \multicolumn{2}{|l|}{BANANA} & & 7p & & 30p \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|}
\hline TOGGLE: SPST20p & Push on/Push off, spring loaded 44p Miniature Non Locking & \[
\begin{aligned}
& \text { DIL SOCKI } \\
& \text { Low profile } \\
& 8 \text { pin }
\end{aligned}
\] \\
\hline SUB-MIN TOGGLE & Push to Make \({ }^{\text {f5p }}\) & 14 pln 13p \\
\hline SP changeover 45p & Push to Break \({ }^{\text {OCKER }}\) (white) 104 250V 25p & 16 pln 14p \\
\hline SPST on/oft 40p & SP cheng (white): 10A 250 V & \\
\hline DPDT \({ }^{\text {S Tag }}\) ( \({ }^{\text {64p }}\) & SP changeover centre off & HO5/5F \\
\hline DPDT Centre off 80p & ROCKER: (black) on/off 10A 250V 20p & TO18/18F \\
\hline SLIDE: & FOCKER: Illuminated (white) & TV2 15p \\
\hline 1A DP 250V 10p & lights when on, 3A 240V 46p & TO3/TV3 15p \\
\hline 1 A DP 250 V C/O 12p & ROTARY: \(1 \mathrm{p} / 2 \mathrm{w}, 2 \mathrm{p} / 6 \mathrm{w}, 2 \mathrm{p} / 2 \mathrm{w}, 2 \mathrm{p} / 4 \mathrm{w}_{\text {\% }}\) & Insulation Kit 8p \\
\hline 4A DP 250V 9p & 3p/3w 3p/4w, 4p/2w, 4p/3w 24p & (MIca \& 2 washers) \\
\hline
\end{tabular}

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6.3viA Heater/Cathode Short LT44 Minl. Drik. Pri 20K S LI700 Mini. Output, Pri 1-2K Sec \(5 \Omega 54 \mathrm{p}\) VEROBOARD*

\begin{tabular}{|l|} 
LAMP HOLDERS AND LAMPS* \\
LES HOLDER Dome shaped, Red, Blue,
\end{tabular} LES HOLDER Dome shaped, Red, Blue, LES BULES \(6 v\) and \(12 v\)
MES HOLDERS Chrome cover, Red or Amber, Jewelled top cover, Red or Amber, Jowelled top
MES BULBS 3.5 V 6 V 12 V
NEON: square top, red, green, Req. : \({ }^{7}\) hole

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calibrated \(0-10.37 \mathrm{~mm}\) dia. PK2 as K5 with pointer on skirt K7 Black, knurled, tapered. Metal top \& skint. Calib. \(0-10,30 \mathrm{~mm}\)


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HI-5344 Six MM5314 chid digit basic ciock, \(12 / 24\) hour HI-5025. Six digit alarm clock, Snooze, MK50 chip.
Hll-7004. Six digit Time/Date/Alarm/Timer, can be used as electronic imes-switch in adon to other functions.
MHI-D797. Four or six digit dispiay kit, \(0 \cdot 3^{\prime \prime \prime}\) digit Supplled with PCE
MHI-D727. Four or six digits, 0.5" 6 Dig- 69.5 Supplied with a digit PCB 4 Dig-E © 50 HHID747 Four ar six digits, \(0 \cdot 6^{\prime \prime}\) bigh digite Supplled with PCS for 6 digits 6 Dig-Ets.70 ERMS: CWO, Access, Barclaycard fsimply quote your number and sign). Credit facilities to Accredited account holders.




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