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REDRESSED
FOR PEACE

Pertrix Batteries have emerged from the testing ground of war as more reliable, more efficient than ever before. You will soon see them in the smart new post-war pack shown above. It denotes the finest battery for radio use yet made.

* Holsun Batteries Limited
37 Victoria Street, London, S.W.I.
THE Radio Industry Council came into existence in 1944 as a unified body, co-ordinating four associations representing the radio industry. It was then realised that the post-war years would bring many technical problems which could better be solved by one parent body, rather than by four associations working independently. For this reason, a technical directive board was formed representing these four bodies, and the board acted in an advisory capacity to the Radio Industry Council. A technical executive committee was also set up to carry out the normal technical activities of the radio industry. Each constituent association elected two representatives to the board, which also had the services of two representatives of the technical executive committee for liaison purposes.

Nine meetings of the board have been held. Amongst the subjects dealt with may be mentioned a series of meetings to ensure adequate co-operation between those responsible for the preparation of Service Specification for radio components in industry, and this naturally led to general questions of technical co-operation between the Services and those in industry whose task it is to see that the country is supplied with up-to-date and reliable apparatus.

These meetings led up to the formation of the Standards Committee.

The discussion between Great Britain, U.S.A. and Canada on the standardisation of screw threads affords an example of the assistance which the board was able to put forward to enhance the viewpoint of the British radio industry.

The board has also done a great deal of work on the standardisation of valves.

Standardisation of radio apparatus in matters affecting the user have also received attention by the British Standards Institution and the board, acting in concert. Also in the field of international standardisation the board has made its views known to the International Standards Co-ordinating Association, and it has maintained close and cordial relations with the Institution of Electrical Engineers on the proposed regulations for the electrical equipment of ships, also in the preparation of a number of I.E.E. codes of practice, including those dealing with radio interference.

The board has taken a leading part in the work of the joint-committee on practical training in the electrical engineering industry and has helped in the preparation of the syllabus. In the important field of radar, the board has been able satisfactorily to clear up the question of official view as to the best wavelength for general purposes of navigation, and to eliminate doubts on the efficiency of the 3 cm. system.

Amongst its other activities, the board has dealt with industry representation at various conferences, such as the British Commonwealth Standards Conference and a number of electrical research association committees. It also co-operated with radio exhibits at the “Britain Can Make It” Exhibition.

The Technical and Scientific Register

The Technical and Scientific Register, which is a centralised branch of the Ministry of Labour Appointments Department, offers a valuable service to employers seeking professionally qualified technicians and scientists, and to technically and scientifically qualified people who are seeking employment or a change of employment.

The minimum qualification for enrolment on the register is, in general, a university degree or its equivalent in subjects appropriate to the profession or post concerned.

In the case of engineers, the Higher National Certificate or the professional examination of recognised engineering institutions or a regular training as a pupil or apprentice, followed by an executive position (normally for at least five years) above the rank of foreman are alternative qualifications necessary for enrolment.

The register is divided into sections, each in charge of technical officers with high professional qualifications and standing in the professions and subjects with which they deal.

Television Tests

Two further half-hourly test periods are now available as a result of a request from the British Radio Equipment Manufacturers' Association. These periods are from 2.30 to 3 and from 4 to 4.30 p.m.

Portable Transmitters

A special licence is now available for the use of portable transmitters. The additional fee is 10s. and allows the transmitter to be operated with a radius of 10 miles of the permanent address of the licensed amateur, or within a similar radius of another stipulated address. This licence does not include organised club field days, for which permission is granted free of charge. As in pre-war days, the transmitter will be operated under the licensee's ordinary call-sign prefixed by "/P." Maximum power is 25 watts on all bands except the 1.8-2.0 mc/s band, for which 10 watts is the maximum.

1947 R.C.M.F. Exhibition

The annual private exhibition of British Radio and Communications Components and Accessories will be held at the new Royal Horticultural Hall, Greycoat and Pimlico Streets, Westminster, S.W.1, during the period 10th to 13th March, 1947. The display is organised by the Radio Component Manufacturers' Federation and, as in former years, is intended to acquaint radio manufacturers and engineers with the most recent advances in the design and development of British radio components, accessories and materials. The exhibition will be open to visitors, by invitation only, from 10 a.m. to 6 p.m. daily during the four days Monday to Thursday inclusive, and it is hoped to attract a record attendance of overseas visitors. Further particulars will be announced in due course.

Ecko Engineering Appointment

EK. COLE, LTD., announce the appointment of Mr. H. L. Oura, M.B.E., B.Sc., M.I.E.E., to take charge of their Western Development Unit located at Malmsbury, Wiltshire. Mr. Oura, who will work directly under Mr. A. W. Martin, chief Engineer, took up his duties on Monday, October 7th. He has for many years been associated with the phonograph industry and has worked closely with the development of electrical recording both in this country and abroad. He has a distinguished war record, having been connected with radar development, in particular H.S.S. and G.I. equipment, and wide and varied work for the Admiralty. Immediately prior to his EKCO appointment, Mr. Oura was a director of E.M.I. Engineering and Development, Ltd.

Schools Broadcasting

It is announced by the Central Council for School Broadcasting that there are now more than 13,000 schools registered as listening to the B.B.C. schools broadcasts—an increase of 1,500 over last year's figure. Scotland reports 1,684 schools registered.

Broadcast Receiving Licences

The following statement shows the approximate numbers of licences issued during the year ended 30th September, 1946.

<table>
<thead>
<tr>
<th>Region</th>
<th>Number</th>
</tr>
</thead>
<tbody>
<tr>
<td>London Postal</td>
<td>2,810,000</td>
</tr>
<tr>
<td>Home Counties</td>
<td>1,360,000</td>
</tr>
<tr>
<td>Midland</td>
<td>1,543,000</td>
</tr>
<tr>
<td>North Eastern</td>
<td>1,045,000</td>
</tr>
<tr>
<td>North Western</td>
<td>1,413,000</td>
</tr>
<tr>
<td>South Western</td>
<td>590,000</td>
</tr>
<tr>
<td>Welsh and Border</td>
<td>617,000</td>
</tr>
<tr>
<td>Total England and Wales</td>
<td>9,527,000</td>
</tr>
<tr>
<td>Scotland</td>
<td>1,030,000</td>
</tr>
<tr>
<td>Northern Ireland</td>
<td>153,000</td>
</tr>
<tr>
<td>Grand Total</td>
<td>10,765,000</td>
</tr>
</tbody>
</table>

The total includes 2,370 television licences, but this figure does not represent the number of television sets in use, as viewers holding unexpired 10s. licences are not required to take out television licences until their 10s. licence expires.

Unlicensed Sets: Post Office Drive

The Post Office drive to detect unlicensed sets still continues, and many persons have been prosecuted in recent weeks for operating wireless receiving apparatus without a licence. The requirement that each householder using wireless apparatus should have a licence applies not only to householders operating their own sets, but also to those using sets which are rented or hired.

Motorists are again reminded that it is necessary for them to take out a separate broadcast receiving licence for a wireless set fitted in a motor-car.

Peter Brough devotes as much attention to making up his ventriloquist dolly, Archie Andrews, as to his own make-up. He is seen here preparing for a recent broadcast.
Philips’ X-ray Expert for U.S.A.

MR. S. W. WEST, of the X-ray Division, Philips Lamps, Ltd., a well-known figure in the industry, has left London by American Overseas Airways for the United States of America. It has been announced that he will join the North American Philips Company as Technical Manager X-ray Division, in the New York Office.

In conjunction with Philips Lamps, Ltd., Mr. West holds a number of patents in the field of X-ray science. He developed and perfected a Pedestal Bucky apparatus of particular value in obstetrical and general radiography, which has been adopted by hospitals in many parts of the world. In 1940, to meet the urgent need for X-ray inspection in war industries, he originated a system of factory-planned X-ray protection, by prefabricated units which could be erected rapidly without expert supervision, making use of a home-produced substitute for metallic lead. Likely to be of far-reaching importance in the new hospital service, the system was extensively employed throughout the war, and resulted in a saving of many tons of vitally needed material during a period of critical shortage.

Radio Teleprinter Link

As a first step to bringing all the Dominion's Air Forces into direct teleprinter communication with the R.A.F., a new radio teleprinter circuit was recently opened between this country and Canada. A similar link will be opened later between this country and Australia. The teleprinter link utilizes standard teleprinters at each end, the impulses from the various letters afterwards being transmitted by radio.

New Zealand Transmitters

THE Australian firm of Amalgamated Wireless, Ltd., which built most of New Zealand's original national radio transmitting stations, is the successful tenderer for a £200,000 New Zealand Government contract for the work of replacing the out-dated and worn out equipment of the Dominion’s radio network. Competition for the contract came from British and American concerns. Most of the work at present contemplated is deferred wartime replacement, but also includes the installation of new stations where coverage is so far inadequate. The major individual item will be replacing the 60-kilowatt transmitter at Wellington Station, 2YA, which gives Dominion-wide coverage.

Philo Presentation to Yorks Town

THE first Philco radio set produced in the new Airmec Ltd. factory at Ossett, Yorks, some time ago, was officially presented to the borough at a ball at the local town hall recently. Attended by nearly 700 people, the ball was organized jointly by Airmec Ltd. and Philco Radio to celebrate the establishment of the factory, which was opened in March last year. The set, an “A 535 B” all-wave table model, bearing a suitably inscribed silver plaque, was presented to the Mayor of Ossett, Alderman J. Gill, by Mr. I. D. Bennett, chairman of the Radio Tel Group of companies. Accepting the gift for the borough, the Mayor said he hoped Ossett would soon become known the world over. The Mayoress, Mrs. Gill, members and officials of the Ossett Council were present at the ceremony.
V.H.F. Receivers
Circuit and Constructional Details of Equipment for Use on 10 Metres and Below
By WM. NIMMONS

With the opening of the Alexandra Palace television service, the ultra-short waves (or, as they have come to be called, V.H.F. or very high frequencies) are coming once more within the province of the amateur constructor. Apart from the vision part of the transmission, which is useless except to those who have a vision receiver, there is the sound channel which gives very high quality. In addition, there is some agitation for the opening of a purely sound programme on V.H.F., which could give quality reproduction not attainable on the longer wavelengths. So we see that there is something to be said for the construction of a V.H.F. receiver.

The Straight Circuit
For wavelengths of the order of 7 metres, the ordinary simple regenerative receiver may be used; in fact, the ordinary triode valve may be employed down to about 3 metres, providing care is taken to achieve a symmetrical layout. In this connection the length of the leads often constitutes a considerable proportion of the circuit, and it is essential to mount the coils so that they are close up to their associated variable condensers.

The Colpitts Circuit
The ordinary straight circuit often behaves erratically, however, on frequencies as high as 50 mc/s. It may not oscillate at all, even with the greatest care in designing. A much more ready oscillator, such as the Colpitts circuit, may be used with advantage. The Colpitts circuit is shown in Fig. 2.

Self-quenching
As previously mentioned, this class of circuit requires a fairly high signal strength for satisfactory operation. The super-regenerative receiver, however, can operate with a much-reduced input and still give a satisfactory output. A two-valve super-regenerative set is indicated in Fig. 3. This is known as the self-quenched type, and the quench action depends upon the condenser C3, which has a capacity of 0.0005 mfd. It is not proposed to go into the theory of the quenching action, let it suffice to say that with the assistance of R4 (50,000 ohms, variable) the valve can be induced to work with far more regeneration than is commonly employed, with consequent increased amplification. The grid-leak, R1, also affects the performance, and various values should be tried, starting with 2 megohms; it is also an advantage to try a grid-leak of 10 megohms connected between grid and H.T. positive as some valves work better this way.

Fig. 1.—The straight circuit designed for V.H.F. work. Note the tapping down the coil to reduce damping.

Fig. 2.—This is the Colpitts circuit, which will be found a ready oscillator.
The grid condenser $C_z$ is a ceramic condenser of 50 m.mfd, while the variable condenser $C_i$ is a midget type of 15 m.mfd. $C_4$ and $C_6$ are both of 2 mfd., and $C_5$ is a by-pass condenser of about .0603 mfd.

The resistors $R_2$ and $R_3$ are for the purpose of preventing threshold howl, and should not be omitted. The value of $R_2$ should lie between 100,000 ohms and 500,000 ohms, depending upon the characteristics of the transformer; but 250,000 ohms is often a satisfactory value. $R_3$ is less critical, and 25,000 ohms is about right.

The operation of Fig. 3 is simple, but it should be noted that as both plates of $C_i$ are at high H.F. potential it is necessary to use an extension spindle if freedom from hand capacity effect is desired. The aerial coupling should be fairly tight, as the circuit is a ready oscillator, and movement of $R_4$ should be tried after the station has been tuned in. It should also be noted that this circuit is not suitable for quality reproduction.

The Superhet

The foregoing are only suitable for headphone use, and the gain is small. For high gain it is essential to employ the superheterodyne system, and commercial practice has settled down to some form of Colpitts or Ultraudion circuit for the oscillator section of the frequency-changer. This simply means a coil connected between the anode and grid, with a grid condenser and grid-leak interposed to prevent grid tick. The circuit of such a frequency-changer is shown in Fig. 4, and there are one or two points worthy of special mention. This circuit may be made up in the form of a converter, for joining to existing apparatus. The point of using such a circuit is that, with the customary oscillator, the conversion gain is very limited and a further difficulty is that the circuit is liable to generate parasitic oscillations; these render the whole circuit useless. This difficulty can be got over fairly successfully by employing the Colpitts oscillator.

Note also the condenser connected across the filament. This should have a value of round about .0005 mfd., and should be connected as close to the filament terminals as possible, with a length of lead not exceeding 1 in. The two 25 m.mfd. variable condensers are preferably not ganged, and the first will be found to give the broader tuning. The aerial coupling should be fairly loose, and should consist of one turn of thick wire, separated from the grid coil by about half an inch, the aerial itself being very short.

The I.F.T. follows usual practice, the transformer being designed for 465 kc. in the case of a complete superhet; or a higher value for a converter to follow.

Push-pull Operation

This circuit (Fig. 4) employs a triode-hexode, and this type of valve is recommended for V.H.F. operation. As far as heptodes are concerned, this type of valve works best in push-pull, and the symmetry with which the circuit can be arranged is a decided advantage. Each valve is tapped across half of the coil, and the total damping is reduced and increased gain is obtained. The method of making connection to the centre-tap of the coils may be by crocodile clip, but once the correct spot has been found it is recommended that a permanent soldered joint be made; this makes a better connection than the clip, which may give trouble owing to corrosion, etc., and as the clip may be made of ferrous metal this would absorb a great deal of power from the circuit, due to its being in the field of the coil.

As previously mentioned, it is essential in all practical receivers built from circuit diagrams that all wires be as short as possible, and careful placing of the components is necessary to ensure...
this. In particular, all earth return wires should be
taken to the actual filament terminal on the valve-
holder of the circuit concerned, and not to chassis as
is customary. Screening of each stage is not absolutely
necessary if careful layout is made beforehand, but
screening ensures stability and freedom from hand
capacity.

already been set forth in Practical Wireless, and it
is not proposed to enter into a discussion of the principles,
involved here. Suffice it to say that for 7-metre recep-
tion on a half-wave aerial, each of the arms should
be a quarter of a wavelength long; this is approximately
6 feet only, and an aerial of these dimensions will cover
6-8 metres, "peaking," of course, at 7 metres.

With regard to Fig. 5, the I.F. stages and second
detector are not shown as they follow normal practice.
Commercial 405 kc. I.F. transformers are suitable, and
give a high gain; some of these are fitted with a means
of varying the selectivity by means of movable dust-
iron cores, and these will be found useful when amateur
activity starts up again. The method of varying the
selectivity by connecting a resistance across the coils
of the I.F. transformer is not recommended as the
damping reduces the gain.

If Figs. 4 and 3 are made up in the form of a converter
attached to an existing receiver, the lead from the
secondary of the I.F. transformer should be connected
to the aerial grid of the I.F. valve (in this case, the
first valve in a receiver of the 1-V-1 type), and not
to the aerial terminal. By careful placing of the two
sets a lead of not more than a foot can be arranged,
and this should not lead to trouble considering the
frequency.

It will be noted that a dipole aerial is used with all
circuits. This is recommended for all V.H.F. work.
It is usually of the half-wave type, connected to the
receiver through a suitable feeder, so that the actual
aerial may be placed as high as possible. There is
nothing against the direct connection, however, if the
receiver is on the first or second floor. The reason
for this is that the waves are liable to be more reflected
and deflected at earth level, and a signal may be inaudible
at ground level and of good strength 20 or 30 feet up.
The laws governing choice of aerial, length, etc., have

Fig. 5.—An efficient converter arranged around a couple of heptode valves in push-pull.

Varying Selectivity

A CONSIDERABLE development in the packaging
of cored solder wire is the production of the new
Size One carton of Eros multicore solder. This pack
has been particularly designed for service engineers and
firms undertaking maintenance. It possesses consider-
able advantages over the nominal 1 lb. reels previously
supplied. The wire is wound in a special way so that
it may be pulled out as required without becoming tanged from the carton. Windows are provided at one
side to enable the user to determine when the contents
are nearly exhausted.

The alloys and gauges now available are identical
with those previously supplied on nominal 1 lb. reels.
Multicore Solders, Ltd., of Mellor House, Alkermere
Street, London, W.1, state that these Size One cartons
are not sold as containing 1 lb. each of solder. They
contain a specified length which will enable sale prices
to be maintained equivalent to the nominal 1 lb. reels,
despite the recent very considerable increase in the
controlled price of tin.

Retail selling prices are as follows: 60/40 alloy
14 s.w.g. containing 56 ft., 6s. each; 60/40 alloy 18 s.w.g.
containing 35 ft., 6s. 6d. each; 40/60 alloy 13 s.w.g.
containing 36 ft., 4s. 6d. each; 40/60 alloy 16 s.w.g.
containing 83 ft., 5s. 3d. each.

Service engineers should be particularly interested in
these new cartons as they can be packed easily in service
engineers' kit and will not tend to become unwound, as
is the case when solder wire is supplied on reels.

Size Two cartons for the handyman retailing at 6d.,
of which several million have been sold since they were
introduced, are still available.
Frequency Modulation—5

Instructions for Lining-up a Receiver of the F-M. Type
By C. A. QUARRINGTON

It will be recalled that the previous article described how the amplitude limiter and frequency amplitude converter functioned, and provided an audio frequency output of a few volts amplitude. It now remains to consider the introduction of de-emphasis and any special requirements of the output stage and power pack, in order to complete the general principles of the frequency-modulated receiver. To complete the picture, however, some general information is included on alignment problems peculiar to this type of receiver.

Fig. 1 shows the complete circuit of a typical limiter, converter, audio frequency amplifier and output stages, which not only embodies all the necessary details to illustrate the points made in this article, but includes that part of a frequency-modulated receiver which differs from an amplitude-modulated receiver. Reference to Fig. 1 will show that the audio output from the frequency-amplitude converter is taken through a pair of triodes arranged for phase splitting, the resistance $R_3$ and condenser $C_4$ being arranged as a filter to attenuate, to negligible proportions, any radio frequency that might otherwise appear at troublesome amplitude in the audio-frequency stages. The values for this filter are not particularly critical as long as the higher audio frequencies are not attenuated, unless, of course, the filter is intended to perform the additional office of de-emphasis. Suitable values for these components are 100,000 ohms and 50 to 100 pfd., or if it is desired to introduce de-emphasis the value of the condenser would be increased as necessary to conform with a degree of pre-emphasis used in the transmitter. It will be noted that a push-pull amplifier is shown using negative feed-back; the circuit used for the audio-frequency section has, of course, no direct connection with frequency modulation except that some high-quality amplifier will presumably be used, as it would appear somewhat illogical to go to the trouble of wide-band frequency modulation and finish-up with easily avoidable distortion in the output stage.

Alternative Phase-splitter

It is possible to introduce an interesting variation by substituting the phase-splitting arrangement shown at Fig. 1 for a pair of triodes in ordinary push-pull and rearrange the discriminator circuit so that a symmetrical output is obtained. It is merely necessary to remove the earth tap from the outer end of $R_2$ and place it at the junction between $R_1$ and $R_2$; this rearrangement results in a symmetrical output that can be used to feed the push-pull triodes. If de-emphasis is used with this rearranged system, it will be desirable to place a filter in each grid lead. This alternative arrangement appears at first sight to be preferable to the arrangement at Fig. 1, and surprise may be evinced that it has been selected for illustration in preference to the alternative. Given perfectly matched components, and a perfectly-designed receiver, there is much to be said for the alternative arrangement, but under less favourable conditions the arrangement illustrated is probably more satisfactory. One advantage is a gain in stability which in practice appears when one or other of the diode cathodes is connected direct to the earth line, instead of via the condenser potentiometer $C_1$, $C_2$. A further advantage is readily apparent by reference to Fig. 1. The use of the centre-tap diode circuit may introduce undesirable lack of balance, if the increase of potential difference across one resistance is not sensibly equal to the decrease across the companion resistance under conditions of modulation; when the centre tap is not employed, the audio-frequency amplifier

![Fig. 1.—The complete circuit of a typical limiter, converter, A.F. and output stages.](image-url)
Power Pack

The power pack of a frequency-modulated receiver will be quite conventional and a single rectifier may be used for supplying high tension to all stages if so desired, particularly if a push-pull output stage is used; if, however, a push-pull output circuit is employed, it is sometimes desirable to arrange for a separate rectifier to supply the audio frequency and output stage, to avoid the difficulties that might otherwise arise in the oscillator stage due to audio-frequency feedback. The danger of this has been explained in a previous article, which also explained the need for keeping mains hum out of the frequency-changer stage. It is a matter of convenience whether the hum level in the frequency changer is kept down to acceptable limits by improvement of the smoothing as a whole, or whether by the provision of additional smoothing to the appropriate stage. The latter course is preferable on economic grounds but the pros and cons cannot be usefully discussed as the question is so influenced by the design of the receiver as a whole.

Special care is needed when aligning all tuned I.F. circuits in a frequency-modulated receiver. A good signal generator is essential and, in addition to having adequate accuracy, must be capable of variation over the required bandwidth without appreciable change in output amplitude. This is particularly important, as serious shortcomings of signal generator design will bring about unsymmetrical working of the frequency-amplitude converter, which is a serious matter from the point of view of the quality of reproduction.

The foregoing alignment instructions are given primarily for use without an oscilloscope, since those who are fortunate enough to possess this piece of equipment are best experienced in interpreting alignment instructions given for use with other equipment. Without an oscilloscope, however, the unquestionable advantages of the oscilloscope when used for gauging the normal receiver, using a voltmeter especially to describe this particular I.F. transformer, all others being referred to as I.F. transformers to earth. The frequency deviation against meter deflection. This figure is based on an average receiver and is, at best, very approximate.

(5) Assuming all I.F. transformer primaries and secondaries to be adjusted to resonance, as nearly as possible, attention can be given to the shape of the overall response curve. Starting from the unmodulated intermediate frequency, set the oscillator alternatively above and below this frequency by progressively equal small steps, noting that each deviation in one direction produces the same meter deflection in the opposite direction; continue this procedure until the bandwidth is covered. Unless abnormal luck is encountered the desired symmetry will not be obtained without further adjustment of the I.F. trimmers by trial and error methods. When such readjustment seems to be approaching finality, note that attenuation is not too rapid towards the edges of the bandwidth. Special care, a final check for symmetry can be made by plotting the response curve on squared paper and by setting frequency deviation against meter deflection.

(6) Should it be desired to carry out alignment as described in (4) and (5) above with more than average care, a final check for symmetry can be made by plotting the response curve on squared paper and by setting frequency deviation against meter deflection.

(7) Remove meter and re-connect limiter resistance to earth.

(8) Some form of output meter is now required which may be introduced into the audio frequency or output stage as convenient. If the available output meter happens to be an oscilloscope, or valve voltmeter, it can with advantage be coupled across the frequency-amplitude converter output. The set is now rigged to check the action of the amplitude limiter and align the converter transformer. It is necessary to bear in mind two rules:

(a) The symmetrical working of the frequency-amplitude converter is mainly achieved by tuning the converter transformer primary.

(b) Adjustment of the necessary zero output when receiving the unmodulated frequency is mainly achieved by tuning the converter transformer secondary.

(9) Set the signal generator conveniently between the unmodulated frequency and the edge of the bandwidth and note that the limiter action is correct by rocking the signal generator output control, when no deflection should be noted on the output meter. Obviously, the signal generator output must be varied over a range which, when duly amplified, will not overload the limiter or overload the I.F. amplifier.

(10) Set the signal generator exactly to the unmodulated frequency and adjust I.F. transformers to resonate in the usual way. Resonance will be shown by maximum reading of the meter connected in series with the limiter bias resistance. At all times the oscillator output must be kept low enough to ensure that the limiter is not saturated; check this frequently by noting that the milliammeter needle shows a marked increase if the signal generator output is experimentally increased. If a marked increase does not result, the signal generator output is too high. As resonance is obtained on various successive windings, the oscillator output will need to be reduced so that the limiter valve has a workable input. Where over-coupled I.F. transformers are employed, resonance will not be shown by maximum meter deflection, and the centre of the peaks must be "felt for" by swinging the trimmers until the mid-point of the peaks is found as accurately as possible; the presence of sharply-peaked single tuned circuits elsewhere in the circuit increases the difficulty of lining up the over-coupled tuned circuits.

(11) Set the signal generator to a frequency half-way between the unmodulated frequency and the bandwidth edge successively on either side and adjust I.F. transformers to resonate in the usual way. Resonance will be shown by maximum reading of the meter connected in series with the limiter bias resistance.
on the output meter. A closer approach to perfect symmetrical working can be obtained by checking at several values of deviation on each side of the unmodulated frequency.

(12) Re-check zero setting by repeating (10) above.

(13) Some converter transformers are provided with variable coupling between primary and secondary. This adjustment is best left alone unless experience and more advanced test gear are available. If for any reason readjustment is necessary—i.e., after unavoidably upsetting adjustment while effecting repair—manufacturers' alignment instructions should be obtained appropriate to the particular transformer and/or receiver.

(14) Remove output meter and signal generator and counteract steps taken to stop frequency changer oscillator from oscillating.

(i5) The R.F. tuned circuits will not require such frequent alignment as the I.F. amplifier and converter transformer, but, when necessary, it can be accomplished in the normal manner using unmodulated output from the signal generator, and employing an indicator meter in the limiter grid circuit as described for other purposes in (2) above.

Frequency modulation has been little used in this country. There is, therefore, no cut-and-dried alignment procedure that can be considered as standard for general purposes. The above procedure has been used successfully by the writer for lining up both narrow and wide-band frequency modulated receivers and was evolved in difficult circumstances after considerable trial-and-error experiment and will, it is hoped, act as a basis for individual requirements. The cathode-ray oscilloscope and special wide-band frequency modulated signal generator are ideal instruments for aligning this type of receiver, and it is presumed that the fortunate few who possess, or have access to, such equipment will have no difficulty in adapting the above notes.

Tone Compensation by Negative Feed-back

An Account of Some Practical and Simple Experiments, by G. T. Edwards

The high-fidelity reproduction of gramophone records and broadcast programmes often necessitates the provision of some form of tone corrector to compensate for deficiencies in the overall frequency response of the reproducing equipment used. These deficiencies are attributed to one or more of the following reasons:

(i) Non-linear response of the loudspeaker and pick-up.

(ii) Attenuation of the higher modulation frequencies due to sharply-tuned H.F. and/or I.F. amplifying circuits.

(iii) The falling frequency-amplitude characteristics of a gramophone record below the region of approximately 250 c.p.s.

A very attractive and effective method of compensation is available to the radio constructor in the use of negative feed-back, and this article is the outcome of a number of experiments carried out by the writer. No highly-specialised apparatus or expensive components are needed for the incorporation of the following systems in existing amplifiers and receivers. Further, with slight

Fig. 1.—Circuit diagram of basic amplifier.

<p>| COMPONENTS |</p>
<table>
<thead>
<tr>
<th>No.</th>
<th>Value</th>
<th>No.</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>R1</td>
<td>25 Meg 0 V.C.</td>
<td>R6</td>
<td>1,000</td>
</tr>
<tr>
<td>R2-R6</td>
<td>50,000</td>
<td>5 w. min.</td>
<td>R8</td>
</tr>
<tr>
<td>R7</td>
<td>2,000 ohm</td>
<td>C5</td>
<td>50 juF 12 v. wkg.</td>
</tr>
<tr>
<td>C1</td>
<td>3 Meg 0</td>
<td>C6</td>
<td>8 juF 450 v. wkg.</td>
</tr>
<tr>
<td>C2</td>
<td>3 Meg 0</td>
<td>C7</td>
<td>8 juF 500 v. wkg.</td>
</tr>
</tbody>
</table>
modifications, these circuits are easily applicable to battery-operated apparatus.

The circuit diagram of the simple amplifier used as a basis for these experiments is shown in Fig. 1. It consists of the triode section of a DH63 R-C coupled to a high sensitivity output tetrode (KT61). Power is derived from a conventional full-wave rectifier circuit.

From Anode

R7
RS

H T—

Fig. 2.—Tone control circuit No. 1.

In the maximum "treble-boost" position, where the .5 mfd. condenser is connected across the cathode circuit, the percentage feedback is reduced as the frequency increases, thus giving increased gain at the high frequency end of the audio scale. In the maximum "top-cut" position, the .002 mfd. condenser is connected across the input circuit of the output stage so that the high notes are by-passed to an extent which increases with frequency.

Circuit No. 3

This circuit (Fig. 4) was developed to provide two facilities: (a) A fixed degree of both treble and bass-boost for local radio reception of orchestral programmes, and (b) fixed bass-cut for speech reproduction. Facility (b) is particularly desirable to prevent "booming" on "speech" should the loudspeaker being used have a pronounced resonance in the region of 100 c.p.s.

With the D.P.D.T. switch in the "music" position the .01 mfd. condenser is included in the voltage feedback circuit from V2 anode to R7.
Wireless and Sunspots

Warnings are occasionally published that solar activity may momentarily interrupt telegraphic transmission overseas, thus causing anxiety to the Press about delays to their messages.

The effects of solar activity are so varied that it must be emphasized that such statements should be used only as warnings, not as forecasts.

From time to time radio transmission fades completely; much more rarely, submarine cables may be affected. But in order that all possible measures may be taken towards preventing delays in transmission, Cable and Wireless, with the cooperation of the Royal Observatory, Greenwich, have evolved a system by which the Central Telegraph Station in London and the outlying wireless stations are informed when solar activity may result in interference.

Sunspots

Sunspots (regarded only as a symptom of underlying activity) are related to disturbances in the ionosphere which interfere with the normal transmission of radio waves. In general, the larger the sunspot the greater the effect, but exceptions are frequent, and at times marked disturbances do occur when sunspots are absent. The Royal Observatory reports to Cable and Wireless all sunspots having an area greater than 500 millionths of the sun's visible hemisphere, i.e., 5.2/1,000,000 of this surface.

Experience by Cable and Wireless shows that any serious effect (if it occurs) on radio conditions starts during the period from the evening preceding to the second evening after the passage of the sunspot across the central meridian of the sun's disk. The disturbance lasts for about three days; exceptionally, effects may be observed two days before. The disturbing solar agency in this case takes only about eight minutes to reach the earth. The type of fading is different from that associated with the much longer periods (magnetic storms) referred to above. The flare type occurs only on routes which are very nearly, or nearly so, in the earth's day hemisphere, whereas the main effect of magnetic storms is felt of course at all times of day, especially on routes which pass nearest to the auroral zones.

Sunspots and solar flares vary in frequency in a well-marked 11-year cycle, the last minimum of which was in 1944 and the next expected maximum in about 1946. The solar cycle is not subject to exact prediction.
Analysis of the Television Receiver—6

This Month We Deal With Tube Sensitivity and Deflection Amplifiers

FIG. 35 makes clear the operation of Fig. 34 given last month. A free-running generator of the type described is of no value in the television receiver, however, for although it might be possible to obtain the required line and frame operating frequencies of 10,125 and 50 cycles per second respectively by critical adjustment of $R_3$ and $R_2$, these frequencies would not remain constant for long, due to small fluctuations in the H.T. supply and other unavoidable variations in operational conditions. In practice, therefore, the discharge of the generating condenser is controlled by the synchronising pulses.

The circuit then functions as follows: $V_1$ is cut off by the bias developed across $R_2$ as before and the generator discharges itself through the neutralised gas and the valve goes out when the condenser voltage has fallen to a value equal to the valve drop. $C$ then commences to re-charge, and the cycle repeats on the arrival of the following synch pulse. The circuit is now no longer free-running but generates a controlled saw-tooth waveform at a frequency determined by the frequency of the synchronising pulses. By using two separate discharger valves and feeding one with the line synch pulses and the other with the frame synch pulses, saw-tooth waveform of the desired 10,125 and 50 cycles per second are automatically secured.

The manner of feeding the saw-tooth waveforms to the respective deflector plates of the cathode-ray tube presents certain difficulties. Much depends upon the sensitivity of the tube, its anode voltage and the extent of the non-linearity of the sweep that can be tolerated. Nothing can be done on the part of the constructor regarding the construction of the tube; he has to take what the designer offers him, but care can be exercised in its choice, and the method adopted for feeding the deflector plates once he has bought his tube is entirely in his own hands for success or failure. For this reason a few notes will be made on the subject of tube sensitivity.

Tube Sensitivity

The actual movement of the spot on the screen of a cathode-ray tube depends upon various factors in the tube construction. The closer the deflection plates are located to the electron stream, the greater is their influence, and it is general to arrange each pair in a diverging position as shown in Fig. 36. This system of construction gives the advantages of closeness without allowing the beam to actually strike a plate due to excessive deflection.

With a given arrangement of deflector plates, a certain maximum angular movement of the electron stream is permissible; in the figure this angle is indicated by $\theta$. It is apparent at once that the longer the tube is made the greater will be the movement of the spot for a given value of $\theta$. Thus a long slender tube is generally more sensitive than a short fat one, the deflection angle $\theta$ being smaller for the same movement of the spot.

Yet another factor affecting the tube sensitivity is the final anode voltage. The velocity of the electron stream is directly proportional to the voltage on the final anode of the tube, and by doubling the anode voltage the sensitivity of the deflector plates will be approximately halved. Most readers will no doubt have noticed the lengthening effect on the time-base sweep of an oscilloscope when the tube anode supply is switched off and the tube anode voltage falls to zero. This is because the sensitivity of the plates is increased and the time-base voltage produces a longer sweep. The effect is quite common. The brilliance of the spot increases, of course, as the anode voltage is raised on any tube, as does the ability to obtain a sharp focus, and so a sensitive than a short fat one, the deflection angle $\theta$ being smaller for the same movement of the spot.

Fig. 36.—The sensitivity of a long tube is greater than that of a short one.

Fig. 37.—A simple push-pull deflection amplifier where the gas-discharger valve itself is one of the amplifiers.
compromise has to be drawn between these conflicting requirements of sensitivity and definition. The anode voltage is the only factor under the control of the user; the size of the screen, the shape and disposition of the deflector plates are all fixed by the manufacturers.

Most makers therefore express the sensitivity of a tube in terms of the final anode voltage, so:

$$\text{Sensitivity} = \frac{r}{V} \text{ mm. per volt.}$$

where \( k \) is a constant depending on the tube design and \( V \) is the final anode voltage. A maximum permissible anode voltage is also generally stated. Thus a tube may have a sensitivity of 1,000 \( \text{V mm. per volt} \), which means that for 3,000 volts on the final anode a voltage of \( r \) volt applied across the deflector plates will cause the spot to move \( r \) mm. across the screen. Taking the screen diameter to be 250 mm., then 750 volts must be applied across the deflector plates in order to move the spot completely across the screen.

It is general to obtain sensitivities in this way for both the horizontal and the vertical deflecting plates. Thus, a tube may be calibrated in this way:

- X-plate sensitivity = \( \frac{850}{r} \) mm./volt
- Y-plate sensitivity = \( \frac{800}{r} \) mm./volt

the plates situated nearest to the final anode having the greatest sensitivity, in this case the X plates. In television, since the ratio of picture width to height is 5:4, it obviously pays to use the most sensitive pair of plates for the horizontal deflection. (Fig. 37.)

A useful size of picture tube for the experimenter is one with an 8-in. round diameter screen, designed to work with a final anode voltage of 2,500 to 3,000 volts. Suppose the screen shown in Fig. 37 is 8-in. diameter, then for \( V/H = 3/4 \), the size of the maximum full rectangular image will be 5.6-in. x 4.2-in. In practice, it is general to ignore the corners of the picture and increase the central picture area accordingly. In the example under discussion 8-in. x 7-in. (\( 516 \times 178 \text{ mm.} \)) would be quite suitable for good viewing. Now the deflection voltages required to build up a raster of this size can be readily calculated as follows, assuming that the plate sensitivities are those quoted above, with a final anode voltage of 3,000 volts. Working with the X plates for the horizontal, or line deflection, we have:

Peak-to-peak deflecting volts = \( \frac{V}{k} \)

- horizontal: \( = \frac{216 \times 3,000}{850} = 762 \text{ volts.} \)
- vertical: \( = \frac{178 \times 3,000}{800} = 668 \text{ volts.} \)

Thus, for a tube of this nature, we must supply the horizontal plates with 762 volts peak-to-peak at a frequency of 10,125 cycles per second, and the vertical deflecting plates with 668 volts peak-to-peak at a frequency of 50 cycles per second.

Deflection Amplifiers

When using gas triodes for saw-tooth generation it is customary, in the interests of linearity, to arrange that the charging condenser only charges up to about 15 per cent of its full voltage before being discharged through the valve. If the tube deflector plates were fed directly from the discharger stage, this process would not be very practical, however, for the charging source would have to have a voltage six or seven times as high as the scanning stroke required, and this would mean a time-base H.T. supply of some 6,000 to 8,000 volts.

It is usual, then, to include deflection amplifiers in the television receiver, so that a small linear saw-tooth generated by the gas discharger is amplified to the required magnitude, without distortion, demanded by the cathode-ray tube. It is possible to use a straight-forward valve amplifier, feeding the output to one plate of a pair, the other plate being returned to final anode or earth, but in general this system is unsatisfactory since it leads to a form of picture distortion known as the trapezium effect. This is due to one or other of the deflector plates moving up or down in potential with respect to the final anode, thus affecting the tube sensitivity from instant to instant. This results in the edges of the picture being trapezium shaped instead of at right angles; in extreme cases the whole picture is badly "warped" right across the screen. In order to overcome this difficulty, a form of symmetrical deflection is almost invariably resorted to, one deflector plate of each pair being ceased to rise in potential as the scanning stroke required, and this would mean a time-base H.T. supply of some 6,000 to 8,000 volts.

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a capacity potentiometer consisting of C1 and C2. Only a portion of the saw-tooth generated across C1C2 is applied to the grid of V1, the gain of this stage being so chosen that the anode output voltage is exactly equal, but opposite in phase to the anode output voltage of V1. When the anode potential of V1 is rising, therefore, that on V2 is falling, so that the tube deflector plates receive scanning potentials in opposite directions. The deflection produced is proportional to the total voltage difference across them, but as they are both above and below the final anode by equal amounts, no distortion occurs. Linearity is likely to be bad with this type of circuit, however, owing to the necessity of having to charge C1C2 to a fairly high percentage of the total H.T. supply.

A better form of deflection amplifier is shown in Fig. 39. Both valves have the same characteristics and are Telf biased by the common cathode resistance Rj. R1 and R2 are so chosen that they are together equal to Rj, and the outputs of V1 and V2 are arranged to be equal by making their grid inputs equal. Since a large amplification of the saw-tooth waveform from the discharger is provided by V1, the input to V2 is taken from the centre point (not electrically) of R1 and R2 so that:

$$\frac{R_1 + R_2}{R_1}$$ = amplification of V2

assuming that R1 is very much larger than R1.

There is a reversal of phase in each valve so that the potential applied at any instant to a deflector plate is equal and opposite to that applied to the other, being symmetrical about the final anode. R1 and R2 may conveniently be an adjustable potentiometer of the correct total value.

The input of V2 need not be tapped along a portion of the anode resistance of V1 to secure the correct magnitude of input voltage, but may be taken from a point along its own grid resistance. Fig. 40 shows this part of the circuit. This system is preferable from the point of view of avoiding hum pickup, but it is not generally used in line amplifiers owing to the input capacity effect of V2 on the frequency response which must be high to avoid distortion. For frame amplifiers, however, it is quite useful.

Practical forms of the deflection amplifiers discussed above largely follow ordinary amplifier practice, but the requirements of frequency response and phase-shift effects cause the time-base amplifiers to differ from audio patterns in several important respects.

The frame amplifier must give negligible phase shift over a frequency-band of 50 to 500 cycles per second, while the line amplifier must deal adequately with the much greater range of 5,000 to 100,000 cycles per second. The frame amplifier is consequently far easier to construct than the line amplifier, the main difficulty in the latter being associated with the falling off in high-frequency response due to stray capacity. When the response is poor at high frequencies, the spot fly-back time is increased, with the result that the left-hand edge of the picture is missing altogether or appears "folded back upon itself.

The frame deflection amplifier of Fig. 41 consists of two power triodes, V14 and V15, with the line deflection amplifier using similar valves V17 and V18. Both stages are push-pull, and the only difference between them is that brought about by the higher frequency requirements of the line deflector plates. These differences will now be discussed; first, the frame amplifier, V14 and V15.

The saw-tooth voltage waveform is developed across C13 and C14, and a fraction of this is applied to the grid of V14 via C15 and R24. The output of V14 appears across R39 and R41 in the grid circuit of V15, and a tapping from R39 applies a fraction of the total voltage to the grid of the valve. The reason for taking the feed of V15 from a point on the grid resistance rather than from the anode load of V14 has been given previously; a smaller proportion of the hum voltage on V14 is transferred to the grid of V15 by adopting this method.

For the frame time-base amplifier, where a high-frequency response is not essential, the input capacity of V14 has no effect upon the performance and a low grid tapping point is permissible.

**Fig. 41.—Time Base and C-R. Tube arrangement, originally reproduced in our August issue last year.**
Business in Burma

Several radio firms in Burma have written to me complaining that whilst they are anxious to push British goods, they do not find British firms so accommodating. They either do not reply to letters or send circular replies. There are, of course, certain barriers, both artificial and conventional in connection with trade in Burma.

Perhaps we are unaware of Burma's isolation due to war, firms established in India, Ceylon, Malay and Singapore held the sole selling rights in certain goods as far as Burma was concerned. This has since been extended to the consumers in Burma, as well as to exporting British goods. They have not got their goods to be handled by agencies which are not in a position to study the tendencies of overseas markets, nor to control the trade in Burma.

I am informed that in the interests of both the Burmese and the countries with which the Burmese have to develop trade relations, intermediaries such as Indian firms in India who have been given the privilege of sole selling rights in Burma should be entirely eliminated. Burma has to-day more business contacts than pre-war, and are handling trade for their own welfare and rehabilitation. They ask British manufacturers to deal with them directly. Of course, only specialised receivers are saleable in that country, and they should cover a wave-range of from 13 to 500 metres with bandspread. If any English manufacturers are interested I shall be glad to put them into touch with reliable firms.

The Black Market in Servicing

I am always amazed when someone recounts to me his experiences at the hands of the thousands of private "service engineers," who are making a ready living and a handsome profit, cashing in on the shortage of really qualified service engineers. In very few cases is satisfaction given. These otherwise intelligent people will pass out to a comparatively unknown man a receiver which has cost £30 or so, and then wonder when they get it back why the set either does not function or is worse than before.

These black marketeers do not work cheaply. They know that the legitimate service stations have long waiting lists, and so they knock at doors posing as experts in the wireless and ask whether the receiver requires an overhaul. One of the tricks they play after an examination is to say that they will have to take it back to their "workshop." That is the last the owner sees of his wireless set. One or two of these common swindlers who successfully pit their Cambewell wits against those of Cambridge have been caught by the police and are doing long terms of imprisonment. But still the game goes on for the same to be played everywhere, and as the Americans put it "a sucker is born every minute."

Very few of my readers will be caught by these specious people, but one the other day wrote to me a pitious letter concerning the treatment he had had at the hands of one fly and shifty gentry. His set had been out of action for some weeks and the local repairer had cost £30 or so, and then wonder when they get it back why the set either does not function or is worse than before.

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The whole story is to say that they will have to take it back to their "workshop." That is the last the owner sees of his wireless set. One or two of these common swindlers who successfully pit their Cambewell wits against those of Cambridge have been caught by the police and are doing long terms of imprisonment. But still the game goes on for the same to be played everywhere, and as the Americans put it "a sucker is born every minute."

On Your Wavelength

By THERMIOM

January, 1947

PRACTICAL WIRELESS

59

Business in Burma

It was out of action for some weeks and the local repairer was sufficiently misguided to believe that this unknown man would be able to perform the necessary miracle and the man duly returned the receiver when only his wife was at home. That is a trick, of course, which they always play. The wife started with £3 and a half without displaying the necessary intelligence of asking to have the receiver demonstrated before she paid the money.

Not only had the receiver not been repaired but all of the valves had been removed as well as the loudspeaker and a number of other parts. The set is, of course, now worthless, and I have no doubt that in addition to the £3 the "expert" has made a further sum by the sale of the valves and other components.

Of course, the only thing to do in such circumstances is to report the matter to the police, but it is seldom that one of these lowest forms of tricksters from 'oxen, Petticoat Lane, or the gutters of the East End of London, is caught.

When they are I hope the magistrates make it really warm for them. My readers will be performing a service to the radio industry by warning their wives, sweethearts and friends not to deal in any case with door-knocking "experts." It is not only in the radio trade that these gentry operate. They call to buy up old gold, old clothes, and bric-a-brac. The unsuspecting housewife is easily cheated. You cannot expect her to know that a pound of gold is £100. Troy weight.

I am aware that there are similar frauds with business addresses, who trick their customers by charging for replacements which have not been made. I know that the radio industry has been concerned for years with purging the Angusan stables of these undesirables.

Deal only with recognised shops. Make quite certain if you are new to a district that the proprietor knows his business or employs someone who does.

Whenever you take a receiver to be serviced see that you get a receipt which details the work done and the replacements made. Learn to know your set, so that you can spot on inspection whether replacements have been made or not. Preferably deal with the recognised agents for the particular receiver. Best of all, learn how to service the receiver yourself by studying a good handbook on the subject.

Readers who have had experiences such as those recounted earlier are invited to write to me in confidence so that I may warn other readers. The name and address of the reader concerned should be given, but not for publication unless it is desired.

"Snoopers"

(Press Note—A daily paper reporter (who may be misinformed) says in regard to police broadcasts on short waves that "the unauthorised amateur listener" will be prosecuted whenever sufficient evidence can be obtained.)

Shall modern crime detectors, with zeal their eyelids glinting, Fail like a thousand tons of stone? On amateurs caught listening? Won't someone kindly tell them They can't do that here, can't we? We think the actual facts might well Be made a bit more clear. Some danger here to liberty. Of that there is no doubt, The "crime" is set in "listening-in," But, later, "speaking out." To that, of course, we object, The Law we must support, But we must not have it misconstrued, And, blameless, haled to Court. Oh listen to, if so inclined, The Law permits you that, But insist that damage's picked up. Are kept inside your hat—" torch."
Generally speaking, television viewers are a dissatisfied set of people! The more technically minded ones are forever looking forward, striving after technical improvements rather than watching the progress of the artistic side or sitting back to enjoy the nightly entertainment. With a distant expression in their eyes, they talk easily about three-colour 1,000-line stereoscopic pictures as if these tremendous developments were just around the corner. They switch on their perfectly good pre-war television receivers as if they were make-shifts or stop-gaps, not to be taken too seriously. Others, not so technically minded, take innocent pleasure in the prestige which the possession of such instruments gives them in the eyes of their neighbours. Owing to the painfully slow deliveries of post-war television receivers, the vast public, which will in due course look upon television purely as a form of entertainment, is, as yet, untapped. I don't think I have yet come across a viewer who treats television in the same manner as most people look upon ordinary broadcast listening. Sound radio has now become an essential part of the equipment of a household, in the same category as the gas-stove or the plumbing, and, like the dripping tap, it is frequently allowed to become a mere musical background to the activities of the household.

Restricted Viewing

Television demands concentration on the part of the viewer. That is both its strength and its weakness. Considered as a form of home entertainment, it is all-absorbing, and in the natural course of events viewers are forced to restrict their periods of viewing and to select in advance those items in the programme which have the greatest personal appeal. These are points which must affect to a great extent the shape of things to come in television. But we must realise that the next steps will be big ones, involving major changes in receivers and transmitters, and such changes will not be embarked upon without experiments and tests which may cover a period of years. Therefore, I feel we can sit back and enjoy the entertainment offered, and persuade our friends to purchase a set and do likewise, safe in the conviction that the present standards will not be changed for a very long time. I know that at the transmitting end, the boys at the Alexandra Palace are getting things well under control, and the producers and directors are no longer the entire slaves of exacting technical limitations. We are approaching a period when we can contemplate the television picture without constantly thinking of the complicated chain of electrical wizardry which makes it possible.

Stereoscopy

Nevertheless, if it is possible to give viewers a foretaste of the technical marvels yet to come, without the disadvantages of scrapping the present receivers or of fumbling up elaborate “adaptors,” I feel sure such a step would be greatly appreciated. Take, for instance, stereoscopy. This has had a fascination for many in its various forms. First, there was the stereopticon, a simple home viewer which enabled the user to view pairs of still stereo photographs, with the right eye seeing only the picture which was taken through the right-hand lens of the stereo camera, and the left eye, restricted to the left-hand picture. It was a scientific novelty which had a long lease of life, and the third dimension continued to amuse and amuse for many years, whether presented in the form of remarkably solid views of Venice or in the more commercial penny-in-the-slot “What the Butler Saw” machines on seaside piers. Attempts to obtain the stereoscopic effect on the cinema screen were, at first, quite unsuccessful, owing to the fact that views of the right and left eye of a spectator could not be “insulated” from one another. Animated stereoscopic photographs were therefore restricted to instruments which would do this part of the job for one viewer only, and the “Kinora” took the place in the home of the old still stereopticon, while the seaside pier model, the Mutoscope, gave an animated version of the Butler’s recollections for the sum of one penny.

Colour Separation

Next came the idea of isolating the left and right eye views by means of colour separation. Stereo photographs, or special dual drawings were made with left and right pictures tinted red and green respectively, and the selection of the appropriate picture by the correct eye was made by observing the pictures through spectacles having glasses tinted red on one side and green on the other. With line drawings, it was possible to super-

(Continued on page 53)
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impose the two colour printings almost on top of one another, and still obtain excellent separation and stereoscopic effect. It will be readily appreciated that when viewed through the red spectacle, the red lines of the drawings could not be seen, but the green lines appeared solidly black. In the case of the green spectacle, the reverse was the case. This same principle was utilized later in several excellent cinematograph stereoscopic film systems, notably M.G.M.'s "Anchorscopes," and with a Lumière invention, both of which required the members of the audience to view the screen through green and red spectacles. For film purposes, the image photographed through the right-hand lens was taken through a red filter, and the left-hand picture through a blue-green filter. The resultant negatives were combined on one print, with alternate frames taken from "red" and "green" pictures, and the stereoscopic effect was most startling. When a figure on the screen held out a packet of chewing gum towards you and said "Have some gum, chum," he appeared almost to be putting a stick of that extraordinary compound right into your mouth. This system was by far the most effective stereoscopic arrangement for the cinema, but it could only be used as a special stunt, in view of the fact that every member of the audience had to be provided with a pair of simple cardboard-rum-gelatine spectacles.

Trade News

Mullard Valve and Service Guide

S\NPLIES of the Mullard Valve and Service Guide (published for use by the Trade only) are now available.

The Guide is divided into four sections. The first gives illustrations, in diagrammatic form, of the bases of the valves listed and their connections. The range of valves dealt with is as follows:

A.C./D.C. Mains types.
Battery types 2 volt. UX Base.
Battery types 1.4 volt. American Types.
Battery types 1.4 volt. A.C. Mains, 4 volt. Special Types.

The second section gives characteristics and operating data of the same range in tabulated form, while the third section gives equivalent tables.

The fourth and last section is devoted to a table of replacement and substitution types.

Wearite Ceramic Switches

THE demand for Ceramic Switches in various combinations that Messrs. Wright & Weaire, Ltd., of 749, High Road, Tottenham, London, N.17, have placed on the market through certain specialist retailers and distributors, is a measure of the quality of Ceramic Switch Components, so that the "Ham," the Student and the Constructor can readily obtain combinations to meet their every requirement. Everything is included in the kit to meet these requirements. Switch Wafers in assorted 1-pole 9 position, 2-pole 6 position, and 4-pole 3 position combinations.

The same method might be used in television, but would require provision at the receiving end of some kind of revolving shutter having red and green sectors, running at the correct synchronous speed, and phased for separating the superimposed pictures (transmitted alternately from two Emitron cameras, side by side, filtered respectively red and green). A simpler method would be to transmit two pictures side by side, from left- and right-hand Emitron cameras, so that they appeared on the home screen in more or less the same relation to one another as the original stereopticon photographs. No filters would be used, but the home viewer would see a bicolour picture on his set, and hold a piece of cardboard up in front of his face, so that the right eye could see only that picture picked up by the right-hand Emitron camera, and the left eye was confined to the left picture. After a few experiments, the idea of red and green sectors and the appropriate distance from the cathode-ray tube screen of your set, there should be no more "fiddling" required.

Colour Television

In order to enable them to cope with increased business, Messrs. Wright & Weaire, have moved into new offices. Their address is now ; 749, High Road, Tottenham, London, N.17. (Tel.; Tottenham 2384-7). Their North Country factory; Simenide Works, South Shields, Co. Durham. (Tel.; South Shields 2928-2-3).

Britannia Batteries

IN order to enable them to cope with increased business, Messrs. Britannia Batteries, Ltd., makers of Albium and Britannia Batteries, have moved into new offices. Their address is now: Britannia, Batteries, Ltd., Trafalgar House, 0, Great Newport Street, London, W.C.2. (Telephone : TEMple Bar 2336/7-9).

S. G. Brown's Headphones

AN illustrated leaflet is now available from Messrs. S. G. Brown relative to their standard range of headphones. A separate leaflet also includes details of the Type K moving-coil headphone which has recently been released. As far as is known, Messrs. S. G. Brown are the sole manufacturers of the moving-coil headphone in this country, and listeners who are anxious about the really sensitive high-quality headphone will no doubt be interested in the details. Special matching transformers are made for these phones, but they may be in short supply for some time yet. These headphones are 6, 8, or 16 ohms per pair, and have the following characteristics:

D.C. Resistance, 8 ohms per pair; Impedance, 10 ohms at 5000 c.p.s.; Sensitivity, 8 Dbs. above 1 microwatt per pair at 1000 c.p.s. The matching transformers are of two patterns of which are available at high and low resistance, and are designed to match loads of 5,000, 7,000, 20,000 and 1, 6 and 15 ohms.
Transmitting Circuits
Details of Some Standard and Unusual Circuits for the Beginner and the Old Hand
By W. J. DELANEY (G2FMY)

WHEN the newcomer enters the transmitting field he usually starts off with a one-valve circuit employing the Tritet arrangement. This is a more or less fool-proof circuit, provided that good components are employed and that care is taken in the initial wiring and setting up. As more experience is gained or more funds become free this is modified, at the same time rendering more power available. The usual jump from the single Tritet is to add a good P.A., for instance an 807 or equivalent. A further modification is sometimes carried out at this stage, the tuned circuit on the cathode side being shorted out and the original Tritet valve then employed as a simple C.O. The serious experimenter will find, however, that although such a two-stage transmitter will bring him good reports from most parts of the world it has a number of drawbacks. It is preferable, after some experience has been gained with this two-stage affair, to rebuild to include a further stage, a frequency-doubler.

A Three-stage Transmitter
For this purpose it is desirable to build each stage on a separate chassis, the C.O. on one, the doubler on another, and the P.A. on yet a further chassis. If the standard rack assembly is employed this will not make an untidy assembly, but will enable experiments to be carried out in each stage in a very simple manner without upsetting the remaining parts of the equipment. Coupling between the various stages is then ideally carried out by the link method and full flexibility is thereby obtained. When licenced for increased power it is then possible to build a complete new P.A. and utilise the original as a driver or replace it.

So far we have considered C.W. only, but the building of a modulator stage does not present much difficulty and this may easily be added to any type of circuit, using the method of modulation favoured by the builder.

Non-standard Circuits
So far the arrangements are standard and will be found to be those adopted by the majority of experimenters. Experiments with transmitting circuits are not so easily carried out as those with receivers, mainly on account of the fact that one hesitates to "go on the air" with an unknown performer, or because tests on an A.A. do not always show up to the best advantage just what takes place under open aerial conditions. There are, however, some very interesting circuits available to those who care to carry out serious experiments and take the usual precautions to see that they do not wander off the recognised bands or radiate harmonics which may interfere with broadcast receivers.

The crystal oscillator is the first stage in which one can find room for experiment. The Pierce oscillator is fairly well-known, but the Jones exciter is perhaps not quite so well-known as it deserves to be. It is a little fussy in regard to one fixed condenser, that labelled "C" in Fig. 2. This circuit is a two-stage, C.O. and P.A., using the Jones arrangement. The originator recommends a capacity of about 0.00035 to 0.00039, and one of the older type neutralising condensers of the tubular type, with a glass tube for the dielectric, will be found very useful in enabling adjustments to be made to obtain the optimum value for this particular arrangement. The remainder of the circuit is quite straightforward, although, if desired, the grid circuit of the P.A. may be tuned, and link coupling employed between the two stages. Keying may be carried out in either stage, and modulation applied as desired. The valve which has been found to work most satisfactorily as the C.O. by the writer in this particular scheme is a 6V6, and this valve is, of course, quite economical in its current demands.

Single-stage Push-pull
For those experimenters who are keen to see just what can be done with a minimum of equipment, the circuit of Fig. 3 offers good ground for many interesting hours of work. Here two 6L6's are employed in a push-pull scheme and it is highly probable that it will not work when first set up! The circuit has definitely got...
to be balanced on both sides and maximum performance will not be obtained until it is. But then, very often when a perfect balance has been obtained, in both components and wiring, the circuit will probably oscillate all over the load and not just at the crystal frequency. It will be found, however, that this can probably be cured by inserting a very small choke in one anode lead. This choke can be made by just twisting the actual lead from anode to tuned circuit round the finger to provide upwards of two turns. It may be found very critical but such a choke in one anode lead will definitely kill unwanted oscillation. This circuit may be used to cover two separate bands, using either plug-in coils for the P.A. side, or a coil tapped on each side of the centre and adjusted in that manner, with two crystals on the grid side, with a simple change-over switch to select the desired frequency. Alternatively, a large capacity split-stator condenser may be employed with a coil chosen to cover both of the desired ranges, although this is always a risky procedure in view of the probability of selecting the crystal frequency when changing bands. A closed-circuit jack is shown in the cathode circuit for keying, and modulation may be applied to the anode in the usual way for P.A. By using two 6L6's for both the crystal oscillator and for a push-pull modulation amplifier a very effective two-stage transmitter can be built, and such an arrangement will prove very useful as a "portable" for field days.

Other Schemes

The arrangements so far described are in the nature of complete transmitters, but they by no means exhaust the possible schemes which may be used. With all of these schemes, however, there is one point which is considered by many a drawback. That is, the restriction to one frequency which is governed by the crystal in use. Very often it is found that a really good P.A. transmitter is heard on a spot widely apart from your own crystal frequency, and most of the long distance boys seem to have a habit of searching only just around their own particular frequency, with the result that it would be hopeless to reply to his call. A number of crystals may be fitted into a transmitter and selected by means of a good rotary multi-point switch, but this is an expensive arrangement. A very good alternative is to build a variable-frequency oscillator, or V.F.O. Provided that care is taken to stabilise such a circuit it will give results which will always bring you a Tx., that it may be moved from stage to stage. This is quite satisfactory with a simple scheme, but there are adjustments which have to be made and which necessitate a balance between two or more separate currents. It is, therefore, worth while considering the inclusion of meters in all parts of the circuit where such readings are required, for instance, in all anode circuits and in the grid circuit of the P.A. at least.

Finally, we must point out that as our Query Service has been temporarily suspended it is not possible to deal with detailed queries regarding values or layouts for any of the circuits above described, but holders of transmitting licences should have no difficulty in constructing apparatus round the circuits given.

Star Sound Studios

We recently had the pleasure of visiting some of the studios of the above company, and were very impressed with the standard of equipment which is fitted. There are five studios in the West End area, each 175ft. long by 100ft. wide, in which various B.B.C. features (Music from the Movies, Dancing Through, Music While You Work, etc.) are often performed. From view points, view the main interest lay in the technical equipment provided for the making of records from any of the studio broadcasts or from any radio programme.

The equipment includes a high-fidelity amplifier, with a total of seven disc recording machines, five of which will cut up to 17½ in. discs at either 78 or 33⅓ r.p.m. These records may be counted to land lines linking various studios, including certain B.B.C. studies, or to radio receivers in the radio transcription studio. Provision is made for "hill and dale," recording, and when desired programmes on T.M. may also be recorded.

Records may be made of items from programmes originating from the majority of European stations and the main overseas short-wave broadcasting stations, and artists may have a record made at any time for personal criticism, for auditions, etc. The quality of records made on this equipment is of a very high order, and the frequency range is far wider than one normally associates with gramophone discs. Fuller details of the equipment will be given at a later date, but readers desiring particulars can obtain a leaflet from the company on application to their offices at 17, Cavendish Square, London, W.1.
This is a five-valve T.R.F. short-wave receiver intended for the constructor who has had some experience and favours the "straight" circuit. It gives sufficient amplification for loudspeaker reception of many stations and the use of bandspreading, with separate bandsetting condensers for tuning both R.F. and detector stages, ensures maximum efficiency without any ganging troubles, or losses through misalignment on various parts of the tuning ranges. Plug-in coils are used as these give good results, simplify wiring, and allow any desired short-wave range to be tuned.

Construction
Although reference to Figs. 3 and 4 will show there is very little wiring for a 5-valve receiver, it is recommended that the theoretical circuit be kept in view when wiring to avoid errors. A metal chassis 12 in. by 9 in. of suitable depth is used. Both the coil holders and the R.F. and detector valve holders are mounted above the chassis by bolts to facilitate wiring. L.F. and output holders are bolted to the chassis as shown.

The Circuit
At Fig. 5 shows, the first R.F. stage is untuned. This greatly simplifies construction and enables the second R.F. stage to function without the damping of the aerial-earth system. Both R.F. stages are controlled by a single V.M. potentiometer. The use of transformer coupling, followed by tuned-grid coupling, enables 4-pin coils to be used and gives good selectivity and gain.

The detector is an ordinary triode, and is followed by a triode L.F. amplifier transformer coupled to the penultimate output valve. A top-cut control is added to reduce hiss and background. The result is a circuit which will put up a good performance, and as there are no auto-bias or voltage-dropping networks the circuit may also be built up in 3- or 4-valve form by omitting one R.F. stage, and the triode L.F. stage. Consequently the set may be built as a 3- or 4-valve, and the additional valves added later without interfering with the original constructional work.

Construction Details of a Short-wave 5-valve Receiver
Receiver Described by F. G. RAYER

To begin construction, mount the two bandspreading condensers, coupled with an extension spindle, allowing sufficient space near the panel for a concentric reduction drive of about 6:1 ratio. The detector bandset condenser should now be mounted beside the detector bandspreader as shown, a further extension spindle being added. Reaction and R.F. bandset condensers are then fixed in the position shown, noting the latter also has a concentric reduction drive. The panel should now be bolted to the front runner, when the potentiometer and variable resistor may be added to complete the panel controls. If flexible couplings are used on the extension spindles, this will ensure smooth action even if the spindles are not quite correctly aligned. Fig. 6 shows the panel layout.

The valve and coil holders should now be mounted, placing the sockets in the position shown. The only other part on the top of the chassis (excluding the screen, which should be left to last) is the small stand-off insulator for the aerial connection. Resistors, etc., are suspended in the wiring. All the connections shown in Figs. 3 and 4 may now be added, keeping coil and condenser leads well away from the chassis and using insulated wire for battery and other leads which require to pass through the chassis.

Note that the coil connections are numbered to agree with Fig. 5. Other makes of coils may be used (Premier coils being suitable) provided the coil holders are suitably wired. Reference to the numbers in Fig. 5 will make the connections for other coils clear.

Sub-chassis Wiring

It is now necessary to fix in position the L.F. transformer, 3-point on-off switch, large condensers, fuseholder and speaker terminals. Note the components and wiring are grouped in sections which should be kept apart as in Figs. 3 and 4. In particular it is essential the three R.F. chokes be well apart, and they may be arranged at different angles to reduce any chance of interaction.

The connections of the V.M. bias circuit (near the
20,000 ohm variable resistor) will become clear if Figs. 3 and 4 are compared. Similarly the two .1 mfd. condensers with their 20,000 ohm resistors used to decouple the R.F. screen grids. All other connections are also shown in the diagrams.

The R.F. choke used to couple the second R.F. stage, and its associated .0001 mfd. pre-set condenser, should be well clear of the chassis. It is important this choke be of good quality and capable of efficient operation over all the ranges tuned, or some loss of volume will result.

**Valve and Coil Types**

The output valve should be a high-gain pentode, such as the Cossor 220HPT, Osram FT2 or Mullard PM23A. For the L.F. stage, an Osram H1L may be used, or a valve such as the Mullard PM101F or Osram 11L10 if more power is to be handled at maximum speaker volume. In the detector stage an Osram H1L, Cossor 210H1E or Mullard PM22E may be used. The R.F. stages may use either pentode or tetrode valves of V.M. characteristics. Pentode types are Cossor 220PT, Osram VP11. Tetrode types Osram VS22, Mazda V5XV. Adjust the bias to a value suitable for the L.F. stages when the receiver is in use.

Coils must be used in pairs, and two pairs will cover the most-used ranges from 12 to 50 metres. For initial trials, coils for the 19-, 25- and 31-metre bands will prove most suitable.

**The Screen**

This is erected as shown in Fig. 3 to separate the tuned circuits, and isolate the detector and A.F. stages from the R.F. stages. If a metal sheet (aluminium, brass or copper) can be obtained it may be used. Otherwise foil glued to cardboard will have to be employed. Zinc is quite good, if clean, of fairly stout gauge, and extended for sufficient height. In any case, the screen must make good connection with the chassis at several points.

**Method of Operation**

When the way of adjusting the controls has been understood it will be found easy to achieve immediately correct alignment and best results. The tuning, or bandspread control, should have a dial marked in 0-100 or 0-180 degrees. The R.F. bandset control and detector bandset control should have dials with similar markings, although they will obviously be of different sizes. The detector bandset should have a fine pointer, or a locator arranged to give exact settings, if possible. Ordinary knobs for reaction and tone-control are suitable.

When listening, the detector bandset should be set to the appropriate point for the wavelength desired. The R.F. bandset should now be rotated to an approximately similar setting as shown on the dial, then adjusted slightly each side this setting until the receiver becomes fully alive, showing that both bandset condensers are set to resonance on the same wavelength. All tuning is now carried out with the ganged bandspread control. For other wavelengths, the detector bandset is adjusted again, and then the R.F. bandset tuned to such a setting (corresponding approximately to the detector bandset dial reading) as cancels stray capacities, etc., and brings the two tuned circuits in line.
Practical Hints

Chassis Handles

RECENTLY I constructed some radio equipment in a rack, and I quickly found that it was not very easy to remove the chassis rapidly for adjustments. To overcome this difficulty I made a pair of handles in the following manner.

An old cycle pedal was obtained from a friendly cycle dealer, and from this pedal I removed the two spindles which support the rubber blocks. First, the spindles must be annealed to prevent cracking when they are bent. This is effected by heating until they are red hot, and then cooling slowly. Next, loose rust is removed with a file, and when an even surface has been formed one end of the rod is fixed about half an inch deep in the vice. A few sharp taps with a hammer will bend the rod over to form a right-angle. When the other end has been similarly treated a rough handle will be formed.

A smooth polish can be obtained by rubbing with fine emery cloth and if a thin coat of clear varnish is applied a rustless silver handle will be obtained.

The finished handles are fixed to the panel by means of the nuts obtained from the original cycle pedal. A bracket between the panel and chassies is, however, desirable to prevent bending the panel when the set is held by the handles. — J. D. T. Davis (Beachill-on-Sea).

Battery Holder

FOR those who use 1.5 volt filament supply, I have devised a useful method of housing the cell.

An old 3-pin valve base is cleaned out, and the centre hole is used to hold a compression spring, connection from this being made to the grid pin. A partial recess is filed in the side of the valve-holder adjacent to the anode pin, similar connection being made here to a thin brass strip, the length of which allows its bent end to clip over the end of the cell, and so keep it secured in the valve-holder.

The assembly is then placed in the appropriate valve socket in the apparatus being used. The cell can easily be changed by pulling aside the spring clip and inserting a new cell.

In making the valve-pin connections, the old wire must be un-soldered and removed. Fresh wires being inserted and resoldered. — R. A. Bernard (London, N.W.6).

Aerial Erection

I SUCCESSFULLY used the following method to erect an aerial at the top of a tall and rather unsteady clothes pole, no ladder being available.

An old piece of chest expander spring, about 4 in. long, was used, an eye being bent around at both ends. This is laid against the back of the clothes pole and a length of stout wire (twisted in the middle to connect to insulator) is held around front of pole and the ends put through the eyes of the spring. The ends of the wire are then pulled back and secured, thus extending spring and making a tight fit around pole.

A ponderer as shown in sketch is used to push the assembly upwards, odd lengths of batten or broomsticks being successively nailed on until the necessary height is obtained. — M. Westlake (Plymouth).

SPECIAL NOTICE

All hints must be accompanied by the coupon cut from page iii of cover.
On the Amateur Bands

By "KAYAK"

The aim of this column is to bring to you up-to-the-minute happenings on the amateur short-wave bands. Never before in the history of amateur radio has there been such activity in our hobby; and never before have there been such opportunities to thrill to the reception from remote places. This is your column, and your DX settings are wanted for inclusion!

The 14 mc/s band has continued to be the most consistent as regards DX, and most of this month's column will be devoted to this band. Ten metres has been "wide open" on a few occasions and has well paid attention. The 7 mc/s band continues out of favour with DX addicts and this band will not regain favour until the broadcast stations are removed. We have heard nothing on this band other than east coast Americans.

During the month of November, stations on 14 mc/s have been K7CE, Puerto Rico, T2Q, Costa Rica, T27, El3B, Nigeria, and DX2M1, Greenland. The operator of this latter station is an American working with the American Overseas Airways Corporation. QSL cards should go to his home address, 293, Graham Street, Brooklyn, New York.

South Americans, both on phone and C.W. have been prolific. Consistent phone signals have been PY64O, Bahia; HK2AB, P.O. Box 1728, Bogota, Colombia; while Mexico produced XG21Z, 14,200 kc/s. On "key" we came across U41K, OK1Y, HI1SA, all around 14,200 kc/s; YQ2Z, Newfoundland, 14,050 kc/s; XE1A, and W5GKG/3. Cards for the latter station go to Mr. I. Simpson, A.P.O. 912, c/o Postmaster, U.S. Army, China.

A "late session" on one recent occasion rewarded us with YQR6B, Mauritius; VQ3JHP, Tanganjika; KL7BP, Alaska, all on C.W. South Africa produced ZS2X (14,073 kc/s) and ZS6DW (14,082 kc/s); and KL7BP, Alaska, all on C.W. South Africa produced ZS2X, ZS6DW ('phone), ZS5BZ and ZS2X, the last two on "key". These stations were heard at a most unusual time, between 04.00 and 05.00, with very good signal strength. Mention should also be made of ZB1AB, Malta, who came up during the same period and was the loudest signal on the band. All these stations were working to Pacific coast or east coast Americans.

The DX contest organised by the Wireless Institute of Australia over the first two weeks in November produced a large crop of signals from the Antipodes. All Australian districts, including Tasmania, were well received. A full list of all calls heard would run into many pages!

From Wing-Commander Waldie, G6W/2, comes an interesting letter full of DX topics. On 28 mc/s phone G6W has worked ZL7XY Rangoon Signal Centre, R.A.F. South-east Asia Command, VO8DD, P.O. Box 166, Dar es Salaam, Tanganyika; VO7GM, P.O. Box 167, Dar es Salaam; ZL2BE, 311, Queen Street, Hastings, New Zealand; and G6W/2, P.O. Box 207, Jadotville, Belgian Congo. From the latter station, G6W/2 received not only a QSL card by air mail but also confirmation by way of a telegram! Best on 28 mc/s was ZLSAC, British Legation, Amman, Paragway. G6W also tells us that he is running 28 mc/s schedules with VS9AB (ex G6VK), who is station engineer at R.A.F., Kanmanakea, Aden. Spot frequency for VS9AB is 28,600 kc/s. For your information G6W/2 has a world-wide reputation as a 'phone DX man. To date he has worked 155 countries on 'phone and has received confirmation from 99. One more confirmation will entitle G6W/2 to that much coveted award, the DX Century Club Certificate.

Mr. Leslye, Ilford, sends along a list of 14 mc/s C.W. DX, including HG1OE, Quito, Ecuador (14,086 kc/s); VE8NW (14,082 kc/s); W7PP (14,084 kc/s); and TaeBA, Turkey. We look upon all "TA" calls with suspicion! Recent information received from Turkey stresses the fact that the Turkish authorities will not issue amateur licences, but that the matter will be considered next time the country's radio regulations come up for revision. A few months ago there were one or two American Airlines operators working on 14 mc/s from Southern Turkey, using "X" call signs, but it is believed that they have now closed down. Mr. Leslye asks us what country is represented by the prefix "UB." The country is Ukraine. Normal Russian prefixes are "UA," while that for White Russia is "UC." John Brookes, North London, reports OQ5LL, Box 16, Stanleyville; SY6J, Athens; CO9CN, Cuba; and EL1B. EL1B is a good 'phone signal on 14 mc/s. Can any reader supply the QRA of EL1B? We have come across this station many times giving QRA as "Nigeria, West Africa," but that is hardly enough to guarantee safe delivery of a letter! John also reports KL7DP, Alaska, and VE8NW, which he believes to be in the Yukon.

John brings up the question of "XA" prefixes and
wonders whether they are pirates. The answer is that they are quite genuine and the prefix that officially
granted to military personnel operating from enemy
occupied territories. Call signs consist of the prefix
letters "XA" followed by two further letters. We
understand that cards for "XA" stations may be
sent to Captain Peter Keller, XADZ, British Army,
A/S, G.H.Q., C.I.F., Italy, who will forward. On
7 me's John reports the usual state of East Coast
Americans and Canadians and one or two weak
Australians. DX hunters on this band should look
out for signals from Oceania from about 0600 onwards.
There is plenty of good DX to be heard on this band
if only one gives it a try!

We are glad to have been able to contact Dennis
Tylor, a pre-war contributor to one of our short-wave
columns. Dennis never uses other than a two-valve
battery receiver, and his results, as you will see, are
excellent. Which only goes to prove that it is careful
listening what counts, and not the size of the set.

Dennis reports the following: AGVY, Lhasa, Tibet;
ZBRA, Ascension Island; OXLY, Box 16, Stanleyville;
VSYES, Colombo; VESAW, Yukon; VP2MY, Mont-
serrat; TF2AX, Yniska Observation, R.O. Box 1247,
Caracas, Venezuela, and OAMJ, Box 849, Lima.
Dennis also reports XUYY, Tientsin, China, and
XUBY. Both these stations were 87 and were working
a few kilocycles away from each other. The time
was around mid-day and the band 14 mc/s. XUYY
was working traffic to the U.S.A., and was heard to say
that his input was 3 kilowatts! Some Chinese
stations are using the prefix "XU" while others would
appear to be using the single letter "C."

28 me's Band

Apart from occasional dead periods due to sunspot
activity this band is settling down and producing
consistent DX. The charm of this band lies in its
un-predictable happenings. Conditions on this band
should continue good apart from temporary sunspot
upsets.

Phone stations from the Antipodes have been peaking
at around 1700 hours, while Pacific coast Americans
and Canadians come through early evenings. Unfor-
tunately space at our disposal does not permit of a
long commentary on this band this month. We shall
have much more to say about "ten" next month.

Shorts

Cards in bulk for American and Canadian stations
may be sent to American Radio Relay League, West
Hartford, Connecticut. The British amateurs were
heard complaining of ignition QRM due to miniature
car race in progress. QRA is on top of coot, hill
overlooking Bay of Naples. Cards should be go to
Technical Unit, 15, Forces Broadcast Service, Central
Mediterranean Forces. Australian amateurs now have
the whole of the ten-metre band back. QTH for
TF2AX is Box 284, Reykjavik, Iceland. Several
British amateurs were lucky enough to work the
American Super-fortress "Panasonic Dreamboat" on
its recent flight. G8KP worked the "Dreamboat" while
it was over Iceland while GJ9K contacted it over
Alexandria. Reports are wanted by VPSD, J. A. Main,
R.N. W/T Station, Bermuda, on his 14 mc/s trans-
missions. Spot frequencies of VP/2D are 14018, 14290
and 14045 kc/s. Dutch amateurs are complaining
about the large number of QSL cards reaching them
from this country bearing insufficient postage. Check
mail rates before posting!

Which brings us to the end of this month's news.
Suggestions and contributions to this feature will be
welcomed. In submitting DX reports please give as
many details as possible, and send them to "Kayak,"
care of this magazine.

Air Traffic Control

THE Ministry of Civil Aviation makes the following
announcement:

A number of misleading statements have been made
recently about air traffic control in the London area.
The facts are that the system of air traffic control
in force at the London and Northolt Airports is in line
with the latest up-to-date techniques in the world today.
Although no one can say of airports, any more than
railways, that accidents will not happen, the public
must remember that the London area has one of the
by the utmost possible safety is tolerated in the London
area or, indeed, at any British commercial airport.

Co-ordination of the control at the London and
Northolt Airports has been developed steadily during
the past year. Further improvements in the traffic
pattern are about to be made as a result of consultations
during recent months with the operators and the British
Airways Pilots Association. The fact that closely
situated airports can be operated with perfect safety
and without interference has long been demonstrated
in the United States. Further, the number of aircraft
movements per day in the London area is not allowed
to build up beyond that which can be handled safely
in the weather prevailing.

At present an average of only 50 arrivals and de-
partures per day is being maintained at the London
and Northolt Airports, giving a total of 200 movements
per week for the two airports together. This figure compares
with more than 1,000 movements per week which have
been handled successfully at Croydon for long past. It
contrasts also with more than 250 scheduled move-
ments per week at such airports as New York and
Washington in the U.S.A.

War-time Aid

Statements have been made that war-time radar aids
have not been applied to civil airport control—to the
disadvantage of Civil Aviation. Although there can be
no doubt that development in the field of radar and
radio will materially improve air-traffic handling methods
in the future and will make possible a greater number of
arrivals and departures in worse weather than can be
handled to-day; nevertheless, methods evolved directly
for wartime needs, where the high standards of safety
demanded for Civil Aviation had to take second place
to operational requirements, cannot be applied to Civil
Aviation without much development.

There is much public misunderstanding about the
meaning of radar and about the ways in which different
radar techniques can serve Civil Aviation. Although
some radar aids to instrument approach already exist at
the London and Northolt Airports, and others are in
process of installation, radar for air traffic control is
just emerging from the experimental stage and as yet is
installed at no civil airport in the world. The United
Kingdom is well ahead in its preparations for such use
of radar in the future.

A demonstration of projected British radar aids for
civil use was held in England in September.

The London and Northolt Airports are being equipped
with suitably modified military radar aids as an
additional safety check on standard radio navigational
aids. The problem is largely that of getting supplies of
new equipment, much of which has had to be specifically
designed to serve the needs of Civil Aviation. Until
radar and other devices are available to make possible
landings in lower visibility than at present, the British
policy remains that aircraft will be diverted to other
airports when safety demands it. Diversions and cancellations that are likely have, however,
been greatly over-estimated in some quarters.

The British Airways Corporation, as the record shows,
make the safety of passengers their prime consideration. Air traffic controllers are instructed that diversions
should be made whenever the weather is such as to
create any doubts on safety.
Thermionic Insulation Tester
A Useful Aid for the Serviceman and Constructor.
By J. C. THWAITES

INSULATION test meters of the type that incorporate a small hand-driven generator are expensive. The instrument about to be described was designed to take the place of this usual type, be simple in operation and construction, and yet to have fair accuracy. It relies on a valve to convert small changes of voltage between its grid and cathode into changes of current which are indicated on a milliammeter in the valve anode circuit.

Rx

How It Operates

The valve $V$ (Fig. 1) is biased negatively on its grid by a voltage drop in its cathode circuit (represented in the diagram by a battery). The resistor $R_1$ is connected between grid and H.T. negative and a meter in the anode circuit of the valve reads the anode current. The electrical components or circuit of which it is required to find the leakage resistance $R_x$ is connected between H.T. positive and the grid. The voltage which is developed across $R_1$ and applied to the grid is dependent upon the resistance of $R_x$.

Let us suppose, for example, that $R_1$ has a value of one megohm. If $R_x$ is 30 megohms then the voltage developed across $R_1$ is $\frac{1}{30}$ of the total voltage across the potentiometer, which is the H.T. voltage—say 60 volts, then the voltage across the grid resistance $R_1$ is $\frac{1}{30} \times 60$ volts. If the mutual conductance of the valve is 1.5 milli-amps per volt then this voltage will give a change in anode current of $60 \times \frac{1}{30} \times 1.5 = 2.9$ mA.

When the resistance $R_x$ is below a certain value the voltage on the grid rises above that of the cathode. It is not able to rise much, however, because of the flow of grid current. To prevent the grid current flow being excessive should the leakage be zero ohms, a resistor $R_a$ (Fig. 2) is connected in series with the item under test. Its value is not critical, about one megohm will do.

To bias the valve a potentiometer circuit is used. It consists of $R_2$ between the cathode of the valve and H.T. negative, resistor $R_4$, and variable resistor $V_{R_6}$, which is adjusted so that voltage developed across $R_4$ is nearly the cut-off voltage of the valve.

The variable resistor $V_{R_6}$ is to prevent more than full-scale deflection current flowing through the milliammeter.

To increase the range of the instrument $R_1$ is made larger, to reduce it $R_1$ is made of lower value. A dual range meter could be made by arranging that a resistor could be switched in parallel with $R_1$.

Constructional Details

The chassis is made from 20 gauge aluminium sheet and the layout is as shown in Fig. 3. The front panel is made from 3/16in. sheet ebonite (see Fig. 4). The wiring is straightforward and the positioning of the wire is not critical, although the insulation between the grid and other parts should be particularly good.

**Fig. 1—Basic circuit of the insulation tester described in this article.**

**Fig. 2—Complete circuit of the tester.**

**Fig. 3—Drilling details for the chassis.**
There are moving coil 0-40 volt meters on sale by Practical Wireless advertisers which may be used in this test meter. They are five milliamp full-scale deflection, and are suitable for use as a milliammeter if the series resistor has been removed or short-circuited.

The valve used is a low-impedance triode—a 220PA with 60 volts high tension. With other types of triode it may be necessary to increase the high tension to 90 volts.

Calibration

To set up the equipment for calibration or for use it is necessary to carry out the following steps:
1. Turn off switch.
2. Connect up L.T. and H.T. batteries.
3. Adjust VR₁ for maximum resistance and VR₂ for maximum resistance, both fully clockwise.
4. Set zero adjuster so that the needle is set correctly to zero.
5. Turn on switch (when all is correct the meter will read between 1 and 5 milliamps).
6. Turn VR₃ anti-clockwise until the meter reads one-quarter of a milliamp.
7. Short test terminals.
8. Turn VR₄ anti-clockwise until the meter reads 5 milliamps.
9. Remove short from test terminals.

The instrument is most easily calibrated against known resistors. Resistors of the carbon-rod type are placed across the test terminals and the meter readings noticed. The higher resistances are made up by connecting a number of resistors in series. The values may be checked on a Megger although 10 per cent, or 5 per cent.

**LIST OF COMPONENTS**

- R₁—1 megohm resistor.
- R₂—1 megohm resistor.
- R₃—5,000 ohms.
- VR₁—10,000 ohms.
- VR₂—10,000 ohms.
- One valve, 220PA.
- One 0.5 mA meter.
- One British valve socket, 4-pin.
- One double-pole toggle switch.

Two terminals
- One sheet brass, 6in. x 5in. x 3/16in.
- One sheet aluminium, 6in. x 5in. x 3/16in.
- One sheet brass, 8in. x 5in. x 3/16in. (20 gauge).
- Nuts, bolts, wire, etc.

**Fig. 4.—Drilling details for the panel.**

**Fig. 5.—Complete wiring of the chassis and panel section of the tester.**

**Fig. 6.—How to prepare a calibration graph for the tester.**
Fan-mail for Philco Workers

T HE avidity with which English technical publications are sought and scrutinised in all parts of the world has been brought to our notice on several occasions recently.

Two Philco workers, Miss Joyce Oughton and Mrs. Gladys Pernam, of the Perivale factory, have both been in the news of late and both have received letters from students and technicians in countries as far apart as Nigeria and Malaya.

These native correspondents show their interest in the latest radio and electrical developments, or maybe an article in the latest issue of the journal to reach them, and then comes a polite request for further information and catalogues.

Miss Oughton, who is this year's "Miss Philco," has herself quite a fan-mail, which she takes considerable pleasure in answering. A short time ago a Flight-Sergeant serving in the Middle East wrote her and exchanged a pair of Nylons for a pin-up photograph.

Both of these Philco workers received their fan-mail from readers of Practical Wireless, and the following is a copy of one of the letters received by Mrs. Pernam:

"Dear Mrs. Pernam,

Greetings to you in our dear Lord's Name Jesus who died on the Cross for us to be saved.

"Dear Mrs. Pernam,

Greetings to you in our dear Lord's Name Jesus who died on the Cross for us to be saved.

You may wonder how do I manage to know you, and why am I so much interested in you. Yes, I will answer both questions. (1) I saw your name and address in a newspaper called Practical Wireless of April issue this year. (2) I was at the same time interested in you, because I am interested in Radio Engineers, because I think you are one, so I therefore wish to befriend you whether you are a Radio Engineer or not. Oh, I have much interest in you, so I beg you not to let me down by refusing this offer.

I am presently taking a course in England for Radio Service Engineering, and I am taking the practical side of it here. So when you reply to my letter, I will be able to give you more details about myself.

I have written you a letter before, which I posted by ordinary mail, but the messenger I gave it to, to buy 3d. stamp and post it, posted it with a 1s. stamp and brought back to me 1s. change. Because this will bring taxation on you, I therefore write this by air, to meet you before that, and to tell you not to take that, because it is the same content in this, you will find there. I beg of you not to be annoyed.

I'm eagerly waiting your reply.

I am, Your sincere friend,

S. A. Oshokova."

Television School Looks Ahead

E. K. COLE'S television courses for dealers are now well under way, with a mounting waiting list of "pupils." The school is part of the service organisation under E. W. Shepherd, and takes place at the Service Headquarters, Somerton Works, Southend-on-Sea. Each course runs for one week—Monday to Friday—and up to 12 students are invited per course. Every effort is made to maintain a friendly team spirit and accommodation has been arranged for all under one roof.

On the final Friday afternoon, the students are conducted on a tour round the EKCO Works, including the Development and Engineering Department, drawing offices, assembles lines, lighting division and plastics plant. There is a tea-break in the Lecture Room both morning and afternoon, and lunch is taken in the Executive Canteen at the Main Works near by.

The very latest Test Gear, including the EKCO Television Pattern Generator, has been installed and a feature is a permanent display of various types of aerials mounted on a dummy chimney stack.

Mr. A. W. Stephen is proving a popular instructor. He has 25 years in the company's service and has only recently returned from radio and signal work in the Royal Navy, including a period with the British Mission in Murmansk.

Dealers wishing to attend or to send a representative are invited to contact Radio Sales Division, E. K. Cole, Ltd. Already there are no vacancies till early 1947.

The course has been found by dealers to have a valuable secondary function in enabling them to point out problems arising from their day-to-day business to a sales executive who is always available.

Fig. 7.—Suggested mains-operated version of the tester.
A 5-valve Radiogram

Details of a Reader's Equipment Employing a 5-valve TRF Circuit With Double Diode
Triode as Detector and A.V.C.

By J. L. HALL

As far as I know, there is nothing original about this circuit, but it certainly fulfils my need for a first-class radiogram.

It is built into an old-fashioned H.M.V. acoustic gramophone cabinet. All the old works were removed, and the doors of the record cupboard at the bottom were joined into one piece to form the baffle board for the speaker—a R.G.D. 20 in. ebonised. Behind this, on the same floor, is the power pack, a 350-0-350 at 200 mA with four r.f. windings and rectifier winding, a massive component but serviceable and silent.

The sound doors above this old record cupboard hide the control panel, with the main radio works behind. The layout is a dead straight line, with the first R.F. stage, and the D.D.T., completely screened, lids as well (because of the gramophone electric motor up above). A cable (each pair of heater wires screened) with an eight-pin octal plug connects the radio to the power pack. The output transformer is mounted by the Pen 45, and the speaker leads plug into the sockets of the radio chassis. The field leads plug into sockets on the power pack. Another screened cable carries the mains to the D.P. switch on the front panel and up to the motor. The aerial is 6 ft. of covered wire laid out round the back of the cabinet.

The Controls

In London, for Home and Light programmes, the volume control has no need to go beyond three of ten divisions, the Third Programme requires about five. The radiogram Vaxley switch is mounted by the grid of the H.L.4/DD in the vertical screen. The pick-up is immediately above this valve, so pick-up leads to switch are only 6 in. Tuning is by my own idea, three ball-bearings and springs select Home, Light and Third programmes, there is no slow-motion drive or lighted dial, just a pointer. I have extension speakers, and a two-bank Vaxley switch selects either internal, external or both. When the internal speaker is off the set is dead silent. (The third position shown on the radiogram switch is for a 1-v short-wave unit).

The tone control, a simple top-cut affair, remains untouched, without any cut, even for the gramophone (only thorn needles used). The A.V.C. regulation is perfect (but has to be disconnected for trimming). The condensers across the mains and H.T. are i,ooo v. working and were necessary to cure slight modulation hum. The Pen 45 is an excellent output valve but

(Continued on page 81).

COMPONENTS.

R1,3—25 megohms; R2—75,000 ohms; R3—450 ohms; R4,6—58,000 ohms; R7—250 ohms; R8—10,000 ohms; R9—25 megohm pot.; R11—2,000 ohms; R12—1,000 ohms; R13—30,000 ohms; R14—.25 megohm; R15—5 megohm; R16—50 megohms; R17—3,000 ohms; R18—175 ohms; R19—5,000 pot.; R21—As fitted to P.U. C1,5,6,11,12,13,15,16,27—1 mfd. mica; C2,4—.01 mfd. mica; C3,7—.005 mfd. mica; C8,9,10,11,13,14—.005 mfd. mica; L1,2—Wearite P.A.2; L3,4,5,6—Wearite P.182.
Programme Pointers

MAURICE REEVE Here Continues His Comments on the Adaptations of Music to Various Instruments and Combinations

In arriving at the modern perversion, maltreatment, and travesties of the classics which burst upon our over-patient ears these days, and which scream out at us from all points of the compass in all places and at all times, we are up against many acute problems of modern life and "new age" trends of thoughts and actions. Such of it has probably, and most regretfully, come to stay with much other degrading of art and quality in living. But in order to prove the contention I am not out to solve, I will describe for you what I might call a "tour of the classics" I made recently. I pretended I had no knowledge of them in their original forms; I decided to make a list of all the numbers I heard during my tour, and find out afterwards through what mediums they were given to the world and to hear them when I returned home in their original versions or settings.

I began by turning on my wireless during breakfast, when a famous regimental band gave a programme of what the B.B.C. term light classics. Two numbers were particularly famous: a selection from "Carmen," and "O Star of Eve," from "Trumnhuizer."

After that, a well-known radio orchestra included Debussy's "Girl with the Flaxen Hair"—one of the 24 Preludes for piano solo—and Mendelssohn's "Song Without Words," popularly known as "La Chine," and also written originally for piano solo.

The third programme I heard, before proceeding on my inquiries elsewhere, was in the feature called "Keyboard Cavalcade." This particular keyboard—organ, belonged to a cinema organ, and the classics played were "Melodies" from the "Swan Lake Ballet," by Tschaikowsky, "Tunes" from Sullivan's "Mikado," played were "Melodies" from the "Swan Lake Ballet," by Tschaikowsky, "Tunes" from Sullivan's "Mikado," and the Overture to Mozart's "Magic Flute."

I then switched off and, softly humming to myself one of these "tunes" or "melodies," proceeded into town and took lunch in a popular restaurant which provided music through the skill of a five piece orchestra, plus a harmonium—an instrument whose presence in an orchestra always affects me like a hair would in a plate of soup—rather de trop and out of place.

I entered this palace of the gastronomic arts and started, as I say, with some of the songs of Schubert, Schumann's "Devotion" and Tschaikowsky's "None but the Weary Heart," finishing with love songs and operatic airs.

Back home once more, the wireless brought me some of the famous two piano combination playing Grieg's "Peer Gynt" suite and a medley of Strauss waltzes.

Now what had I heard? When I returned home and mused over this question before reticiting, it didn't take me very long to realise that I had heard it all hundreds of times before. Also that I had heard things like the Schubert "Serenade" and the "Peer Gynt" suite in so many different instros and combinations of instruments as well as those I had heard this day. Which fact naturally prompted me to ponder on for what instruments they had originally been intended.

The Original Settings

To ascertain this I thought the catalogues of the famous gramophone companies might enlighten me. But, oh dear! This put me into the greatest confusion as everything seemed to have been recorded on everything and by everybody! But there ends fantasy; as the reader knows I only pretended I knew nothing of these works. The question is, what did I lose, and what do you lose, by their transference to these media? The answer can only be given in one word; "everything," with, perhaps, one small qualification. The "tunes" remained—those things which the whole human race whistles and hums to itself.

The Melody Only

I'm afraid it was only the tunes, or melodies, which received any serious attention on either side. The public wanted to be entertained with them in the various places I resorted to, and the entertainers knew this full well. Harmony, nuance, tone colour, atmosphere; all these and many other components of the original meant little.

One reply to these charges I can already hear. "It is impossible to get symphony orchestras, opera companies, first-class pianists, singers, etc., etc., to restaurants or cinemas. It is the melodies we like to hear. Many of us know the originals very well, but we are satisfied with the nostalgia that 'One Fine Day' or the 'Serenade' creates in us, no matter on what it is played, and we are grateful for it."

Well, well! to that hypothetical answer I say, "did the chicken rissole you had in that restaurant where I heard 'Tosca,' etc., create a nostalgia of roast chicken?"

I played over all the numbers I heard that day, on records. First there was a famous soprano singing the "Serenade." Then another of "Tosca," with full symphony orchestra for background. Rachmaninov himself played his "Melodie" on another; and on yet another an equally great pianist played the haunting Debussy Preludes. And so on and so on. Orchestral, vocal, piano, tone colour and nuance, the tender passion of the soprano, the amazing palette of the orchestra and the percussive brilliance of the piano. All gone in the name of compromise, nostalgia, light entertainment.

What had I lost? Everything.

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It is our duty to you (and in fairness to our registered Dealers) to be frank regarding the present supply position of Eddystone Components. In view of to-day’s manufacturing difficulties (common to all) we are not finding it easy to meet the demand as quickly as we would wish. We must, in the Nation’s interest, maintain our Export Drive thus leaving only a portion of our output for the Home Market. To avoid disappointment, order your Eddystone Components well in advance. Don’t blame your dealer if he cannot fulfil your entire requirements over the counter—he is doing his best for you and we are doing our best for him. You may be sure that we, the manufacturers, are doing everything possible to increase output. Distribution of our products is being made evenly throughout the country—you may not have to wait, but if you do, please be patient.

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Published by

STRATTON & Co. Ltd.
WEST HEATH, B’HAM, 31
In another series of articles in *Practical Wireless*, I have recently dealt with the alleged difficulties of vectorising valve circuits.

Considering the "noise" that has been made on the question of conventions, etc., I did not expect my treatment to escape criticism, but it appears no objections have been recorded so far! Needless to add, such criticism is welcomed, or if there are still any difficulties I shall be glad to deal with them in these columns.

The vector rules themselves are extremely easy.

The shift is 180 deg. If there is inductive reactance and a phase angle $\phi$ in an anticlockwise direction, where $\tan \phi = X/R$, for capacitive reactance and resistance, change this to clockwise direction.

Figure 1 shows these three cases. It will be seen that the 180 deg. angle of (a) becomes (180 deg.) in (b), and (180 deg.) in (c). In (b), the phase-shift may, of course, be stated as the smaller angle between $Eg$ and $Vo$. Thus if $\phi = 60^\circ$ (180 deg.) a phase-shift of 120 deg. however, in these Notes I would like to tell you something of a "history" behind ray deliberations on the vector conventions in valve circuits. It will explain why the whole subject has been made to look so abstruse.

A "Technical Argument"

I had been aware for some years of lack of agreement and contradictory views among authorities interested in the problems.

Looking over some correspondence, I find that I questioned certain statements made by writers on vector relationships in oscillators as far back as 1939. It became important to obtain authoritative opinion upon a particular text-book account.

With all due respect and thanks to the authorities whom I consulted, I found a complete lack of agreement on fundamental issues—ways of looking at things which led to unnecessarily difficult conventions. The main point at issue was the phase-reversed output voltage, $Vo$, of an ordinary resistance amplifying stage, Fig. 2(a).

I submitted what has been put forward in my recent articles, namely: that there is an applied voltage component across $R$, from the H.T. source, equal to but opposite in phase to $Eg$—experienced by $V$, in Fig. 2(a).

In course of the discussion, I pointed out that the phase of $Vo$ represents the load reaction—a term borrowed from "The Principles of Radio-Communication" by Morecroft, though this eminent authority did not discuss specific applications to valve networks.

After all, a valve amplifier is simply a device for converting D.C. power from a battery or mains unit into A.C. power in an anode load. By a current "swing," a proportion of the H.T. E.M.F. is developed as an A.C. "supply voltage" across the load, which is the voltage $V$. At the same time, because one end of the load is at the fixed potential of H.T., the valve voltage $Vo$ (anode-to-cathode) falls, and so is of opposite phase to $V$. But not one of the authorities consulted would even agree that $V$ existed! In justice to them, let me add that there are some pretty cogent arguments against $V$. As far as I know, there is but one textbook which shows a supply voltage in some vector diagrams, taking its existence for granted in the actual text.

The objection is this: it is impossible to find any alternative potential of a phase opposite to the input valve stage where the load is in the anode circuit. For example, an oscilloscope test will always show $Vo$.

That certainly seems conclusive. $Vo$ is the output voltage, and if experiment fails to demonstrate any other, then $V$ and $Vo$ must be one and the same as regards magnitude and phase.

Fig. 1.—Vectors showing phase-shift with (a) pure resistance load; (b) inductive reactance and resistance load, and (c) capacitative reactance and resistance load.

Course, be stated as the smaller angle between $Eg$ and $Vo$. Thus if $\phi = 60^\circ$ (180 deg.) a phase-shift of 120 deg. for capacitive reactance and resistance, change this to clockwise direction.

That is, as long as we say the alternating current $Ia$ is of "positive sign." The authorities got over this by giving $Ia$ also a reversed phase. Perfect agreement with A.C. theory then results. $Vo$ and $Ia$ are in phase, but both are phase-reversed in relation to the grid input E.M.F. $Eg$.

Here all the difficulties and confusions begin. Conventions had to be devised to explain how $Ia$ and $Eg$ could be regarded as being at 180 deg. to one another, whereas common-sense demands they should be exactly in-phase! Let us consider this point in a little more detail.

$Eg$ and $Ia$ at 180 Deg.?

When the grid potential is varying in a positive sense—an E.M.F. acting towards the grid, or away from cathode, see arrow Fig. 2 (a)—the anode current $Ia$ will be increasing, above its mean value $I_0$.

At all ordinary frequencies the current will reach its peak at the same instant as $Eg$, and the obvious statement is that the two things are exactly in phase—like the flux and magnetising current of a transformer.

But to try to get consistent results by ignoring $V$, this oblique convention was invented by putting $Eg$ and $Ia$ 180 deg. out of phase. Our current increase ("positive" change) then becomes "negative," whilst to turn things topsy-turvy properly, a decrease below the mean datum line is treated as a "positive" change.

It contradicts mathematical conventions and plain commonsense. We need not go into certain A.C.-D.C. conditions which might be postulated to justify such
Inversions of straightforward ideas, because simple recognition of the applied voltage V gets rid of all difficulties at one stroke.

Note, again, that all the confusions arise because Vo was said to be the only alternating voltage component existing in the anode circuit.

The "Supply Voltage" Again

At the risk of repetition of what has been said in this and previous articles, let me state once again why we must consider a supply component itself at 18 deg. to Vo.

Still keeping to a load resistance R, we have, by elementary A.C. theory, a "p.d.," "drop," or "voltage" across the resistance given by \( V = I \times R \), or, strictly, a voltage-drop, since there is also a steady drop of 103 volts.

In any ordinary A.C. circuit we would simply regard this as the supply voltage, in-phase with the current. There is nothing in valve circuits that demands violation of this basic A.C. principle. The current and "voltage" in a resistance are necessarily in-phase, whether the resistance is that of a wire, a lamp, a heater, or one inserted in the anode circuit.

Therefore, we say the alternating current I develops a "drop" across R—or, if you like, "more volts" are developed across the resistance, from the H.T., in a negative sense, thereby tacitly admitting there must be an applied voltage V, at 180 deg. to E., or some other E.M.F.

But, at the same time that V rises to a maximum, the valve anode-to-cathode, or output voltage Vo, falls by exactly the same amount as V increases. After all, "volts" are derived from the H.T., and it is simply a case of

\[ V = V_o \text { volts as before.} \]

Let Eg change in a "positive sense," as before—from zero to maximum. The current I will be increasing exactly in step with Eg, and the magnetic field around L will be increasing.

By the laws of electromagnetic induction, a back E.M.F. will be induced in the coil opposing the current increase. What direction of E.M.F. will do that?

We need not consider this 90 deg. shift for the moment.

Across the valve, exactly the same happens as in Fig. 3—forgetting the 90 deg. angle in Fig. 3. An increase in the volts dropped across the inductance is accompanied by an equal fall in the volts across the valve. The total increase (peak) across L is V volts.

Therefore Vo—V volts as before.

Thus V and Vo are still at 180 deg. This is true whatever the nature of the anode load—resistance, inductive, or capacitive—without application of "supply volts"! In every valve circuit there must be an equivalent voltage, even though at 180 deg. to some other E.M.F.

If, as in Fig. 3(a), we substitute for R a pure inductance L, we cannot get away from the facts: (a) that there is a back E.M.F. of self-induction E in the coil turns, and (b) that there must be an applied voltage V, at 180 deg. to E.

Both these E.M.F.s must be accounted for in any and every inductive circuit, and Fig. 3 is no exception. Let us again consider the detailed action.

While the facts we have emphasised seem perfectly obvious even on superficial examination, the authorities would have none of it. All maintained that my "supply voltage V" was non-existent, and subsequent writings and correspondence on the subject in the technical press prove that they actually believed this right.

True, some did note that "Vo at the load voltage in a negative sense," thereby tacitly admitting there must be an opposite component of "positive sense" somewhere!

At the time we were discussing the pure resistance case, Fig. 2. But very often, if a point or principle can be conclusively established for one particular case, there is more than a reasonable presumption that it must be true generally.

For example: we cannot imagine a current flowing or changing in any sort of circuit—resistive, inductive, or capacitive—without application of "supply volts"! In every valve circuit there must be an equivalent voltage, even though at 180 deg. to some other E.M.F. Only one answer is possible. E will be directed against H.T. (and H.T.), as indicated by the dotted arrow in Fig. 2. The H.T. is acting positively around the circuit anti-clockwise (from + to —), whilst the back E.M.F. is directed the opposite way.

We would be quite correct in saying: the counter E.M.F. has a positive direction opposite to that of the H.T. But the standard electrical convention is to treat such a direction as negative (mathematically, \( E = -LdI/dt \)), the negative sign merely denoting the fact of phase-opposition to an applied voltage of positive direction.

Therefore we have two E.M.F.s in mutual opposition. What happens? Ia will go on increasing to its peak, whilst the back E.M.F. retards the growth. The effect will be to throw the current quater of a cycle (90 deg.) out of phase with both E.M.F.s—1a leading 90 deg. on E, and lagging 90 deg. on V.

We need not consider this 90 deg. shift for the moment. Since E is in direct opposition to the H.T., a proportion of the H.T. volts will be thrown across L, equal but opposite to the counter E.M.F. This is our applied voltage V again. Any further argument necessary to demonstrate its existence

But, once more, we are up against that paradoxical quantity, the Output Voltage Vo. Will this have the same phase as E, or V, or some other E.M.F.?

Across the valve, exactly the same happens as in Fig. 2—forgetting the 90 deg. angle in Fig. 3. An increase in the volts dropped across the inductance is accompanied by an equal fall in the volts across the valve. The total increase (peak) across L is V volts. Therefore Vo becomes the same as V volts as before.

Thus V and Vo are still at 180 deg. This is true whatever the nature of the anode load—resistance, inductive, or mixed impedance. The anode-to-cathode volts fall by exactly the same amount as the volts dropped across the load rise. Or, conversely, during a negative half-cycle, the valve volts rise.

Because they are at 180 deg., Vo still has a "negative sign" relative to V. Since E also has a negative sign
A 5-VALVE RADIOGRAM

January, 1947

PRACTICAL WIRELESS

relative to V, it follows by elementary logic that E and Vo are in-phase. The output voltage taken off the anode has the phase of the back E.M.F. in the inductive load.

By a rather longer route, we arrive back at the same conclusion as in Fig. 2—that V and Vo are 180 deg. out of phase. In Fig. 3, the total phase-shift between Vo and E will not be 180 deg., but 90 deg., because V is turned round anti-clockwise to lead on la by a quarter-cycle—instead of being in-phase with la as in the resistance case (see Figs. 2 (b) and 2 (c), comparing with 3 (b) and 3 (c)).

"Load Reaction"

Here was a pretty conclusive argument. But, it was argued, it is all very well to take an inductive case where the conditions are entirely different. What about a load resistance? You have no "back E.M.F." there!

The back E.M.F. in an inductance is one form of a load reaction. In electrical circuits it denotes an E.M.F. or potential-difference of opposite sign, and therefore phase-opposing the applied voltage. Is there such a voltage in a resistance? In inductive circuits we have a tangible counter-E.M.F. self-induced by the magnetic field. But surely, nothing of this kind applies to a pure resistance, i.e., a non-inductive resistance?

True, there is no back E.M.F. of "induction." Nevertheless, there is a very definite load reaction, which takes the form of a potential-difference opposing the applied E.M.F. It differs from a back E.M.F. of self-induction in being at 180 deg. instead of 90 deg. to the current.

When you say that volts are "dropped" in a resistance you really imply they are cancelled-out by some equal and opposite potential. What is "lost," of course, is energy—electrical energy converted into heat. But the very fact that volts are lost means that they set up an internal potential-difference of opposite sign to the applied E.M.F.

"Potential-difference," and "Applied E.M.F." are in mutual opposition, as you will see if you consider the relative value of each. The + and — signs attached at any ends A and B of a resistance denote an applied E.M.F. resulting in the direction A—B. They also denote the potential-difference acting B—A. Because terminal A is at a higher + potential than B, this difference acts as an "opposition," or "counter-potential," to the applied E.M.F.

It takes a little thinking to see the point. In general, of course, when we refer to "voltage drop" we simply mean loss of applied volts. With the single exception of the American work, Principles of Radio-Communication, by Morecroft, I know of no textbook that even mentions the principles outlined in Practical Wireless.

In most circuits the direction of the internal potential-difference is relatively unimportant—except perhaps when you consider the internal loss of volts in a battery. But, remember, what we had to show was something equivalent to a "back" E.M.F. in an anode load resistance.

Fig. 3—An amplifying stage in which the load resistance of Fig. 2 is replaced by a pure inductance.

The negative sign of the output voltage in Fig. 5 should thus be clear. It takes the sign of the load reaction, just the same as it did in Fig. 4, where we had a

more tangible counter E.M.F. Otherwise, what has been said before should make it abundantly clear that the load voltage V exists, not across the valve, but directly across the load impedance in the anode circuit, and that in all cases it is at 180 deg. to the output voltage.

Conclusions

It appears from an article I recently read in another periodical that this subject of the load reaction has received much learned attention in some of the more academic technical journals.

As far as I am aware, the correct term, load reaction, was not employed. If it had, there would not be much room left for argument. I pointed it out to the authorities who took part in my "argument" in 1939-40. I claim no particular originality in doing so, since Morecroft had published his explanation even at that time.

The writer of the article I read recently sets a problem for his readers on the question we have just been discussing—the relative directions of applied E.M.F. and potential-difference. It appears, too, from the article, that the subject gave rise to involved controversy in two or three of the leading technical journals.

Considering that Morecroft had elucidated the point years ago, whilst I tried to get authorities to see it was the real explanation of phase-reversal in a resistance stage, one wonders whether radio technicians will ever reach agreement on anything! It is about time radio engineers should agree on their vectors, as electrical engineers have done ages ago.

Teachers of radio, in particular, should have the student's interests at heart, and I am always open to discuss in these columns any criticisms or objections to the principles outlined in Practical Wireless.

I think I can claim to have demonstrated conclusively the root cause of disagreements. I will go so far as to ask the Editor to invite more authoritative opinions if it can be shown my reasoning is faulty or inadmissible on any point.

That is a fair enough offer. If objections are still not forthcoming, shall we take the issue as settled once and for all time?

A 5-VALVE RADIOGRAM

(Concluded from page 75)
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Hon. Sec.: L. Bingley, 39, Fountain Street, Sowerby, Halifax, Yorks.

to encourage newcomers into the movement, and to increase the 
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 impressions on the Wax
Review of the Latest
Gramophone Records

Goethe's tragedy "Egmont" is not more famous than the brilliant overture Beethoven wrote for it. This piece was written when the composer was at the height of his fame, and shows him in dramatic mood, master of every orchestral resource. The heavy chords for strings at the opening are dark with meaning and the downward plunge at the commencement of the allegro is as thrilling as anything in orchestral music. At the end of the overture is one of those massive climaxes Beethoven knows so well how to produce, not unlike the coda of the finale in the C minor Symphony. Beethoven, unlike some of his contemporaries, had a fine literary taste; the books in his collection at his death showed a high standard of reading, and evidently Goethe's tragedy inspired him enough to draw forth one of the finest overtures in the orchestral repertory. "Egmont" is a scope that provides ample opportunities for individual interpretations, and this latest recording on Columbia DX1373 by the Philharmonia Orchestra, conducted by Malcolm Sargent, is sure to find many warm admirers.

Another interesting release this month is a recording of "Overture No. 6 in E Minor, Op. 85" on four 12-inch records. It has been recorded by the B.B.C. Symphony Orchestra, under the able baton of Sir Adrian Boult with Pau Casals playing the 'cello.

Benedetto Gigli is one of the finest tenors in the ranks of Italian artists, with an extensive repertory in both opera and art-song. His recent debut at Covent Garden was a tremendous success. He has recorded this month "Amari" and "O del mio amato ben," both of which are sung in Italian on H.M.V. DB5176.

Tchaikovsky's \"Rondelle\" music from the \"Sleeping Beauty\" is another highlight in the latest releases, and it has been recorded by the Royal Opera House Orchestra, Covent Garden, conducted by Constant Lambert on two 12-inch records—Columbia DX1381-2.

H.M.V. Album Series

Beethoven's \"Symphony No. 6 in F Major\" (\"Pastoral\") is featured in the above series and consists of a set of five 12-inch records—Columbia LX63-5-9. The recording is made by the Philharmonia Orchestra, conducted by Bruno Walter. Other interesting recordings are \"Die Meuttrinzinger\" and \"Jedermann\" by the well-known baritone, Herbert Janssen, on Columbia LX947, \"Reverie and Caprice\" played by the Philharmonia Orchestra, conducted by Constant Lambert, on Columbia LX446, with Joseph Szigeti (violin), \"Fantasia on a Theme of Tallis\" by the Halle Orchestra, conducted by John Barbirolli, on H.M.V. C1597-8 and \"Addio del Passato\" and \"Si, Mi Chiamano\" sung by Margherita Carosio, soprano, on H.M.V. DB67.

New Tempo Record

Richard Tauber's repertory of songs of various schools is indeed amazing. He seems to have the power of identifying himself completely with the nationality and characteristics of the composer whose song he sings, and his fine tone never fails him. This month he has included two Tschaikovsky pieces: \"Filidnola\" is a love song in the Florentine tradition, in which Tschaikovsky skillfully reproduces the Italian style. Companion to it is the very beautiful \"In the Ballroom\"—Parlophone F3549.

Other releases are \"Strange Love\" and \"Ono More Tomorrow\" by Tex Beneke with the Glenn Miller Orchestra on H.M.V. BD5943. "London Town" is devoted to the House of Commons, while the Sullivan opera had more to do with Lords. The new production is on a grand scale, beautifully dressed and organized in the true Cochran tradition. This month Vivian Ellis himself plays six pieces from the show in piano solos on H.M.V. BB500. "London Town" is one of the finest of them, a rousing piece given to the King's Bargeman and his jolly watermen. The three walkers are jollifications and happy, and in them Vivian Ellis has epitomised the gaiety and elegance of this attractive rye.

Glancing through the vocal recordings I noticed records by most of the popular English singers. On H.M.V. BD507, for instance, we have Webster Booth singing \"Aazareth\", and \"O Come all ye Faithful\" in his own inimitable style, whilst Joan Hammond sings "The Donkey" and "Magadan at Michael's Gate\" on H.M.V. BB503. Also Jennette MacDonald, the popular film star has recorded a very old favourite, "Smoke gets in your Eyes", on H.M.V. BB510. On the reverse side she sings \"Sweetheart Waltz\". The evergreen \"Rondlette\" turns up again on Columbia BB259, sung by Luigi Infantino, tenor, and another old favourite \"The Vagabond\" has been recorded by Robert Irwin on H.M.V. BB504.

As a coupling to this record he sings \"Bright is the Ring of Words\" from \"Songs of Travel, No. 2\".

Dance Music

Finally, I come to the dance music which seems to cater for all tastes. All the latest popular hits have been recorded by well-known dance bands.

The latest Irving Berlin number from his film \"Blue Skies\", \"You keep Coming back like a Song\", has been recorded by the Skyrockets Dance Orchestra, conducted by Paul Feniouhet on H.M.V. BD5945. The coupling is \"Let It Be Soon.\"

Other releases are \"Strange Love\" and \"One More Tomorrow\", by Tex Beneke with the Glenn Miller Orchestra on H.M.V. BD5943. "As Long as I Live" and \"It's a Beautiful Day\", by Carroll Gibbons and the Savoy Hotel Orchestra on Columbia FB1237, and finally \"Sunrise Serenade\" and \"Missouri Waltz\", by Frank Carle and his Orchestra on Columbia FB3339. This is the first Columbia recording featuring this orchestra.

Our Cover Subject.

Our cover illustration this week shows the B.B.C. television cameras at work during the Remembrance Day ceremony at the Cenotaph. It will be noted that the vantage point is the same as that used by the Cinema News cameras.
Open to Discussion

The Editor does not necessarily agree with the opinions expressed by his correspondents. All letters must be accompanied by the name and address of the sender (not necessarily for publication).

An Amateur's Views

SIR,—I heartily endorse G. C. Eagley's letter re DX listening.

Perhaps it has not occurred to your readers that logging stations of commercial concerns, whose power of several kilowatts is beamcd more often than not towards this country, can hardly be called or rated an achievement. After all, where is there anything outstanding in listening to stations which are listened to achievement. After all, where is there anything

several kilowatts is beamed more often than not towards

logging stations of commercial concerns, whose power of

(a) I always understood a differential reaction con-

denser did not affect tuning.

(b) There was no traces of the "Jei Londres" announce-
er except at just below the oscillation point, and no sug-
gestion of the Light Programme when in this position.

Neither programme appeared to butt in on the other,

were all that was changed to produce separate programmes

was the movement of the reaction condenser, which is

supposed not to affect tuning.

Is the answer that "Jei Londres" is a harmonic of a

B.B.C. short-wave station, or is the effect due to the

more layout of my set, which is different from any other

I've ever seen?

I've been experimenting with battery sets for some

years on ideas culled from Practical Wireless, but

this is the first set I've ever made completely from my

own design and from old and odd components stripped

from junk sets.

With many thanks for all your help over the years

to constructors in the enjoyment of the best indoor

hobby in the world.—R. G. Richman (Glasgow).

Short-wave Results

SIR,—I have been a reader of your excellent journal

for a long time, but I have not written before. Since

being demobbed from the Forces I have received

my pre-war DX listening. Until recently I have had a

DX Economy Three, and very good results were obtained.

Last month I purchased a Philips P.C.R. communi-
cations receiver. I would very much like to hear from

any reader who has one of these jobs, so as to compare
reports, etc. At present I am using a golf, indoor

aerial, but in the near future I will be trying out a few
different types of aerials so as to obtain best results.

So if any DX enthusiasts care to write I would be

only too pleased to hear from them.

Here are a few stations logged recently, mainly on

7 and 13 metres:

<table>
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<tr>
<th>Callsign</th>
<th>Frequency</th>
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<tbody>
<tr>
<td>4BH</td>
<td>4820 kHz</td>
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<td>G4PT</td>
<td>6400 kHz</td>
</tr>
</tbody>
</table>


A.C. versus D.C. Receivers

SIR,—If you will allow me to enter the camp and

smoke a peace pipe with the "Experimenter" of

Cheilley, I would very much like to settle up one or two
points arising out of his letter in your December issue.

I am well aware that the "Experimenter" did not

include the word "impossible" in his letter of September.

I concluded my first paragraph with that word, maybe

ill-chosen. However, the object of using it was to
convey to the reader that it is not beyond the technical resources of radio engineering to voltage double with a D.C. supply.

I would like readers to note that any description of a piece of apparatus to convert D.C. into A.C. was the inverter.

The use of the term "D.C. transformer" was employed because it conveys more readily what an inverter does. Care was taken to put this term between inverted commas. I feared that it would be confused with the rotating machine, apparently with justification.

The fact that I appear to have fallen into a trap just shows that one must not jump too readily to conclusions. What was the trap? The 'Experimenteur' quite rightly maintains that the voltage doubler is essentially a circuit for A.C. input.

The " D.C. transformer " referred to in Mr. J. Copley-May's letter.

The careful reading of a letter before replying is an essential these days, as it is so easy to "trigger off" a mass of technically capable people who may each have a different interpretation of the subject.

I did not suggest that voltage doubling could be achieved with a D.C. "input" to the circuit. My contention is that a voltage doubler can be made to function from a D.C. "supply." That was made clear in my first letter.

I attach a circuit of an inverter—"D.C. transformer"—the functioning of which is almost self-explanatory.

The transformer on the left, which supplies a small A.C. voltage fluctuation (obtained by feedback through C1) drives the grids of the two valves alternately less and conducts, draws current and charges C. The top A.C., voltage doubler for the use of.

I endorse the last paragraph of Mr. G. W. House's March 16th, letter, and most of the contents.—J. Copley-May (Richmond).

Correspondent Wanted

SIR,—Taking up DX listening again after a lapse of six years, for the past month, I have been listening for about eight hours weekly, I have logged 163 Hands on 20 metres in 16 different countries. The set I am using is a 5-valve superhet (commercial) with a 50ft. 6in. aerial indoors, and all were heard on the middlewave. Included in the log are : CEFAR, LUXZ, W7MRE, W7AK, W7FM, W5GAC portable in Iceland, VE7-DD, etc.

Through the medium of your current journal I would like to contact any readers who may have built or operated a 25-watt transmitter, battery operated, described in this paper before the war.—Lionel V. Lawe ( Stonewall, Balfourborough, Co. Cavan, Eire).

Hints to Manufacturers

SIR,—Why do not the manufacturers of radio parts and accessories cater more for the amateur here in England?

I have yet to see Fahnstock clips on sale. They are surely one of the greatest time-savers for an experimenter yet invented. We also require:

Small plastic boxes for meters, etc.

Plastic cabinets for radio sets, midget size upwards.

Metal speaker cabinets to match the metal set type.

Escutcheons, round and square, from about 1—1/2ins. upwards. (These are badly needed for speakers and dial openings.)

Telescopic aerials for fixing in side of set from 6ins. upwards, i.e., as in the "Handle-Talkie."

Books of service sheets such as those issued by the "Rider Manuals" in the U.S.A.; or is it that the circuits of some British sets are so shambled that the makers do not dare to publish them? These are a few of the things we require—what about it, manufacturers?

A. W. J. Marsh (Newport, I.W.).

News from Jerusalem

SIR,—Your readers may be interested in the following:

ZC1AR/6EZ. This infamous station operated jointly by the writer and two other Servicemen was located in Palestine near Jerusalem. As no licences were granted in Palestine at that time, we very stupidly used a ZC1 call. All cards to be sent to Box 360, Cairo, Egypt, for forwarding to the respective operators. SWL reports will be welcomed, provided they are detailed and suitable. QSLs will be sent to those of this nature.

ZC6F was genuine at R.A.F. Station, Agir, Palestine. JX calls are shortly to be issued to Servicemen in Palestine for 10, 5 and 2J metres with maximum input of 90 watts. The calls shall have no figure, i.e., similar to XA calls. I expect to be JXJC.—"Jack" (Jerusalem).

Television Results in Norfhants

SIR,—The enclosed photograph, which is an enlargement of a 35mm. "snap," may interest those readers who are following television trends outside the Alexandra Palace service area. The receiver is operated at Wellingborough in an extremely busy part of the town where car interference is at its worst. The receiver consists of a two-stage pre-amplifier tuned to the vision and sound frequencies, frequency changer common to vision and sound, four vision L.F.s and anode-bend rectifier feeding the tube, a 6in. electro-magnetic.

The amount of interference which can be tolerated on the picture without becoming too annoying is very much greater than that on sound. On the screen, car interference appears generally as white blobs and dashes, sometimes upsetting the frame synchronising, but the noise from the speaker is ear-splitting. Television has little opportunity of development from the viewers' point of view (no pun intended) until some form of compulsory car suppression is brought into force. Everything depends on the activities of those readers whose reception areas lie outside the range adequately covered by Alexandra Palace and who are plagued by cars, cinemas, fans and other forms of television interference.—S. A. Knight (Wellingborough).

[The photograph was not suitable for reproduction, but should have a remarkably "clear" screen.—Ed.]

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