ELECTRONIC DESIGN's Ninth Annual Transistor Data Chart (p 33) contains spe tions for 1,714 transistor types--last year only l,088 types were submitte publication by semiconductor manufacturers. With close to a 60 per cent in in the number of available iypes, the design engineer is now offered a gre selection of devices as well as increased sources of supply--but his searc for a transistor to do a certain job is likewise increased. Thus, ELECTRON SIGN's unique listing, specifically tailored for the design engineer, shou prove to be a handy time-saver. Contrary to existing lists which group tra tors by manufacturer or in numerical sequence (fine for salesmen, of limit to engineers), the 1961 Data Chart has transistors organized into six appl categories: AUDIO-mostly general purpose types, under l, listed in order creasing forward-current transfer ratio. HIGH FREQUENCY--including types $r$ up to and above the vhf range and tabulated in order of increasing alpha-c frequency. POWER DEVICES--transistors rated at 1 and above are listed in 0 of increasing collector power dissipation. HIGH-LEVEL AND LOW-LEVEL SWITCH devices intended for switching are listed in order of increasing alpha-cut frequency. SPECIAL TYPES--low noise, high power/high frequency and other $m$ laneous types are included. By this system of listing transistors, the des engineer is offered a rapid method of selecting a particular type based on meter value. In addition, close substitutes are apparent and multiple sour of supply are listed when applicable. Only U.S. manufactured types are giv One word of caution is included. Quite a few similar number types, made by eral companies, were submitted with different characteristics due to the n formity in test methods among manufacturers. The manufacturer whose data al used for each particular type is listed under "Mfg." Other suppliers of the types are found under "Remarks." Please take note that the company listed MICROWAVES. . . p 129 "Mfg." is not necessarily the prime supplier, a che source or the original EIA registrant. The final choice of supplier is obv: wo to the design engineer. I


CPPC's new 5 watt servo amplifier provides a unique combination of exceptional stability and miniature size. Built around a DC amplifier with high frequency cutoff above 30 acps, the SA 5601 provides uniform response over its full operating range. With a $10 \mathrm{k} \Omega$ input resistor the SA 5601 yields a voltage gain of $54 \pm 1 \mathrm{db}$ from $-55^{\circ}$ to $+125^{\circ} \mathrm{C}$ with all signal levels below saturation, and supply voltage of $56 \pm 3$ volts. Idling power is under 1 watt.
Designed to drive any size 8,10 or 11 servo motor with a 26 volt control-phase rating, the SA 5601 is available off the shelf with stud or screw mounting. A regulated supply of the 56 VDC power required for the SA 5601 operating from $115 \bigvee 400$ ~ and providing a 26 V AC tap for moto and synchro excitation is available in a similar package.

For information phone or write: Area 215 MAdison 2-1000 TWX LNSDWN, Pa. 1122(U)-or our Representatives.




##  <br> Home




## A New, Better ELECTRONIC DESIGN

We hope you noticed several physical improvements in the last issue of Electronic Design. There were three that we are particularly proud of: (a) the strongest binding available in printing-indeed, the same type of binding used in the better paperback books (thus, ED can be maintained in good condition for the many readers using each copy); (b) improved type faces and layouts; and (c) better reproduction of illustrations.
These changes came about as a result of our switching printing operations to the inidwest. Shifting printing to the central part of the country will also insure faster distribution of Electronic Design.

Advertisers als., get a new service coincident with our getting a new printer. A limited number of ads may be inserted only 12 days preceding the issue date, or three days before the magazine is mailed.

The late closing form will enable manufacturers to introduce new product advertising with minimum delay where such timing is critical.

The switchover is nol without its problems. The editorial department has to rely on airlines for daily messenger service. If a plane is grounded or "diverted (thats a neat term to describe o crisis) as we approach press time we hove to set copy and give make-up instructions via teletype. Fingers crossed, we hope we won' see crossed headlines.
The end result will be even more timely news reporting for design engineer readers.
Turn to page 6, for example, for a rundown on some of the top events at last weeks Fifth National Conference on Military Electronics in Washingion. On page 10 readers will find an even more timely report on two hardwareoriented developments discussed at an otherwise theoretically-oriented Joint Automatic Control Conference in Boulder, Col. This meeting was held last Wednesday through Friday, June 28 to 30.

As you read through the stories in the issue notice the easy readibility of the new type style used for text. We hope this will prove an added convenience to busy readers.

On the ground, or high in the sky, Raytheon's line of rugged diode rectifiers gives dependable arc-free operation.
Example: Raytheon 583, one of six Raytheon half-wave rectifier types. Operating as a clipper diode at altitudes to 36,000 fcet, maximum ratings are 15,000 volts PiV, 8 amperes peak plate current Arc-free clipping action makes sure a magnetron can be fired once without refiring automatically or uncontrollably!

The reliability of Raytheon diode rectifiers is the result of exceptional care in design and manufacture . . . with no compromise in quality control. Gold-plated plates and zirconium coatings assure reliable operation at high voltages. Cathodes are heliarc welded. Higher exhaust temperatures mean less gas and longer life. For more information on Raythcon's growing line of dependable diode rectifiers. please write: Raytheon, Industrial Cornponents Division. 55 Chapel Street, Newton 58, Massachusetts.

| PAYTHEON DIODE RECTIFIERS |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TVE | semvice | mater |  | max mare matums |  |  |
|  |  | veris | ames |  | $\begin{gathered} \text { purar } \\ \text { sumparion } \end{gathered}$ |  |
| 303* |  | $25$ $25$ | 4.9 <br> 4.9 | $11.000$ <br> 15.000 | $\begin{aligned} & 0850 \\ & 20 \end{aligned}$ | 0.063 <br> 0.240 |
| $\begin{gathered} 382010 . j \\ 3024 m a \cdot j \end{gathered}$ | H W. RECT (Malf fil.) (FULL (IL) | $\begin{aligned} & 28 \\ & 40 \end{aligned}$ | $\begin{aligned} & 30 \\ & 20 \end{aligned}$ | 20.000 20.000 | $\begin{aligned} & 0.150 \\ & 0.300 \end{aligned}$ | $\begin{aligned} & 0030 \\ & 0.060 \end{aligned}$ |
| 2028 | $\begin{aligned} & \text { Climen } \\ & \text { DIOOE } \end{aligned}$ | 2.5 | 4.75 | 13.000 | 8.0 | 0.020 |
| 3029 |  | 2.5 <br> 25 | 4.8 <br> 4.9 | $\begin{array}{r} 16.000 \\ 7.700 \\ 5.000 \\ 10.000 \end{array}$ | 0.250 0.300 0.300 8.0 |  |
| 48310 | n. W rect. Clippler OIOOE 0100 | 5.0 5.0 | S.0 | $\begin{aligned} & 16.000 \\ & 16.000 \end{aligned}$ | $\begin{gathered} 0.470 \\ 12.0 \end{gathered}$ | $\begin{aligned} & 0.150 \\ & 0.050 \end{aligned}$ |

-Mi-SIG-200E Prelerred Type

For Small Order or Prototype Requirements, See Your Local Franchised Raytheon Distributor


See how little difference can be noted between a nearly opaque original (left) and three fast, economical diazo copies (right) made with Post Super Vapo Black Paper.

## New Super Diazo Papers Make Prints From Prints

## More uses -

No longer limited to copying just thin, translucent originals, recent Posp progress in formulating superfast diazo compounds has added a new dimension to diazotype reproduction.

A selection of new Post direct positive papers can now handle, at reasonable speeds, such problems as making prints from discolored originals, letterhead correspondence, or even from old prints them-selves-in short, from subjects considered too opaque for conventional diazo copying.

In drafting rooms, for example, this ability to reproduce from nontranslucent originals provides a unique, low-cost way to copy present engineering forms that may be on inexpensive, semi-opaque, sulphite paper.

## More variety -

The convenience and versatility of the whiteprinting process takes on new meaning with these important Post developments. Available in sheets and rolls as Super VeriBlac (440-14) for semi-moist diazo
equipment, and as Super Vapo Blue (206M-14) and Super Vapo Black (208M-14) for dry, ammonia-process machines.
One of the most impressive features of these Post Super Diazo Papers is the extra speed in reproducing normal subjects, such as engineering tracings. There's no sacrifice of shelflife, image stability, development rate or clean backgrounds. The printing range is extremely wide.

## More economy -

Cost is a key word in the consideration of any new product. Post Super Diazo Papers cost no more. Further, both large and small users will be quick to note that the combination of speed and economy basic to these new diazotype papers make them practical for longer runs -even 50 copies-and, less expensive than other duplicating methods often selected for such quantities.

Ask your Post dealer or write Frederick Post Company, 3644 North Avondale Avenue, Chicago 18, Illinois, for Super Diazo Facts.

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## Coming Next Issue

The interest of the electronics industry will soon be centered on San Francisco's Cow Palace. For the duration of WESCON, Aug. 21 to Aug. 24, manufacturers will proudly display their wares for evaluation and approval.

To assist visiting engineers in making the all-important decision of what to see first, the WESCON, Aug. 2, issue of Electronic DEsign will feature the products to be introduced for the first time. For convenience in locating these items, booth numbers will ac. company the product descriptions.

A trend survey, conducted by the editors of Electronic Design, covering recent, present and future product developments will be a highlight of the issue. Don't miss it.


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 that

## Laminar Devices Key Superconductivity Push

Laminating Films to Control Transistion Temperature<br>Among Successes Reported at Top Research Meeting

Alan Corneretto
News Editor

RESEARCHERS trying to exploit superconductivity have developed a technique with high promise for designers: combining normally nonsuperconductive metallic thin filmes with superconductive ones and achieving superconductivity in the entire assembly.

Such devices have been made by superimposing thin films of superconductive lead and normally nonsuperconductive silver. Because the films become superconductive at temper-


Charateristics of combined superconducting and normal films are dependent on thickness of films, implying devices may be made that would become superconductive at predetermined cryogenic temperatures. Curves are for configurations shown under graph. Two curves af lower left resulied from a structure different from others shown. This work was done at Arthur D. Litile, Inc.
atures dependent on film thickness, multilayered devices are foreseen in which different layers would become superconductive at different predetermined cryogenic temperatures.

The development was among recent successes reported at a conference on fundamental research in superconductivity held June 15-17 at the International Business Machines research center, Yorktown Heights, N. Y. It reflected a growing interest in the field.

Two reasons are given for the spurt in interest. One is the discovery last year of tunneling in superconductive thin films ( $E D$, Dec. 7, 1960, p 4), and the other the recent development of materials that $r e m a i n$ superconductive in high magnetic fields.

Present superconductive thin-film devices are made either of naturally supercorductive metals, which are limited in number, or of difficult-to-process alloys. The $n \in w$ combina-


[^0]tion, or laminar, technique is expected to make it easier to tailor the transition temperatures of superconducting films than former methods permitted.
P. H. Smith of Arthur D. Little, Inc. ( ADL), Cambridge, Mass., delivered a jointly authored paper on the process at the Yorktown Heights conference. Substantially the same reports appear in the June 15,1961 , issue of Physical Review Letters, published by the American Physical Society. Similar work has been done by Dr. Hans Meissner at the Stevens Institute of Technology.

Both Dr. James Nicol, one of the authors of the ADL paper, and Dr. Meissner, report that the two films-normal and supercon-ducting-must be in intimate contact with each other before the effect can be achieved. At both organizations one film is deposited immediately after the other while the original vacuum is maintained. The reasons for the phenomenon are not completely understood at present.

ADL reports that it has constructed devices by superimposing a film of one material between two films of the other, and by depositing one film on the other in an opensandwich construction. It calls the resulting devices laminar superconductors. At the conference, Mr. Smith reported that the assembly of two metals in contact behaves as a unit having its own characteristic superconducting properties.

Films worked with at ADL measure from 500 to 10,000 A thick, he says. Typically they are made by superimposing along the length of a $10-$ by $-0.3-\mathrm{mm}$ silver film a longer lead film 0.15 mm wide. Electrical connections are soldered to the ends of the lead film. A glass substrate with lead, tin and normally nonsuperconductive gold and silver have been used.

Addition of the silver is said to reduce the transition temperature of the assembly below that of lead alone. In one sample, a tran-
sition temperature of 1.87 K was reportedly measured. Normally, lead has a transition temperature of 7.2 K , according to ADL.

Several samples can be deposited simultaneously on the same substrate. The superconductive effects appear to be unchanged by the type of construction ised or the sequence of deposition of metals, says ADL.

According to Dr. Nicol, the phenomenon apparently can be harnessed to tailor the temperature at which a device will become superconductive. Another advantage he cites for the technique is that the pure metals involved are easier to work with than alloys, which may be relatively hard to vacuumdeposit.

## Meeting Hears Evidence Backing Theories

## Of Bardeen, Cooper and Schrieffer

Many of the papers delivered at the conference reported work that supported the various thenries of Professors Bardeen, Cooper and Schrieffer on the nature of superconductivity. The existence of energy gaps in superconductors, the dependence of the gaps on temperature position and field strength, and the possibly paired nature of electrons in superconductive materials were all discussed at the meeting, which was attended by virtually all the top superconductivity experts in the Western countries.
One of the highlights of the conference was a report by Dr. Naebauer, of Herrsching, Germany, on the measurement, for the first time, of the flux quantization unit in a superconducting ring. The unit was given as $4 \times 10^{-7}$ gauss $\mathrm{cm}^{2}$. The measurement, which constitutes one of the few direct observations of a quantum effect, supports the theoretical prediction that flux in a superconducting ring occurs in discrete units. The fact that the units are discrete was said to raise the possibility that devices may be built eventually in which the quantized nature of flux in a superconducting ring may be harnessed to count or to transduce.
Also at the conference, J. E. Kunzler Bell Telephone Laboratories, reported that ductile alloys of niobium-zirconium appear to be the most promising superconductive materials for magnets with field strengths in the 80 -to- 100 -kilogauss range, while the characteristics of niobium-three tin in wire-like form appear to be suitable for fields of at least 200 kilogauss.
Dr. Kunzler added that the prospects for material with electrical and magnetic characteristics capable of still higher fields appear bright. - -

## Which AC/DC digital voltmeter should you buy?

...seven questions to help you decide

## 1. Is it rellable, dependable?

A rather general question, and one you often get rather general answers to. But with such an important consideration, you should get answers like these:

The stepping switches in the KIN TEL 502B AC/DC digital voltmeter are guaranteed for two years. KIN TEL can make this guarantee because it operates stepping switches conservatively, driving them with DC (as in telephone service) at a rate somewhat below their peak speed. This gentler drive gives the 502B a longer life, makes it capable of more sensitive measurements, eliminates the need for stepping switch adjustments or other maintenance, and greatly reduces down time.
When servicing is ultimately needed, KIN TEL-trained personnel in 22 different maintenance shops throughout the country are prepared to put your 502B in factory condition with minimum delay.

Each 502B is manufactured on a true production-line basis. KIN TEL has used this method in building over 10,000 "standard-cell-accuracy" instruments, instruments known for their consistent, trouble-free performance.
2. Does it have automatic range selection for AC and DC?

Auto-ranging is a convenience. It makes your job a little easier, a little surer. It permits unattended operation with \& printer to record voltages on the range giving the best resolution.
The KIN TEL 502B has it.

## 3. Does it have a single-plane readout?

A single-plane readout reduces reading errors. Each number is displayed individually. There are no super imposed outlines of "off" digits. You can read the num bers as easily from the side as from the front.
The KIN TEL 502B has a single plane readout.

## 4. Can you program it?

A programable instrument is a more useful instrument It can be used with a printer for unattended checkout of missile components, quality control of specific items, and other automated measurements.

You can program the 502B. It's the only standard off-theshelf digital voltmeter controllable by remote contact closures. With the AC converter control set to REMOTE, closures command any desired sequence of measurements at 10 -volt AC, 100 -volt AC, 1000 -volt AC, auto-range $A C$, or auto-range DC.

## 5. Will it over-range on both AC and DC?

A loaded question, perhaps, since the kin tel 502B is the only digital voltmeter on the market with AC and DC over-ranging. But this is an important feature, not just an extra one.
The 502B displays 4 complete digits plus a 5 th over ranging digit ( 0 or 1 ). This 5 th digit gives ten times more resolution at the often-measured decade points ( $1,10,100$ volts) than 4 -digit voltmeters that lose a digit changing from .9999 to 1.000 . This means you get the useful accuracy of a 5 -digit voltmeter over a large part of the measurement range while retaining the stability, reliability, and price advantage of a 4 -digit instrument

## 6. Does it offer the highest accuracy?

Of course, none of the features listed so far are worth a dime if you can't depend on what the instrument tells you. So let's be specific:
With the 502B, DC measurements are accurate to within $.01 \%$ of reading $\pm$ one digit. AC accuracy is the highest in the industry - within $0.1 \%$ of reading or $\pm 3$ digits ( $0.03 \%$ of full scale) for signals between 30 cps and 10 kc up to $10.000,100.00$, or 1000.0 volts on the respective range scales. With manual or programed ranging, this same accuracy is maintained up to 15.000 or 150.00 volts for signals between 50 cps and 7 kc .

This accuracy is maintained by a constant and automatic calibration of the metering circuit against an unsaturated mercury-cadmium standard cell.

## 7. Is it worth what it costs?

The KIN TEL 502B costs $\$ 4245$, and is delivered from stock. Compare it - what it does and what it costs - with any other AC/DC digital voltmeter. We think that when you do, the 502 B will rate the same answer on this question that it has on the other 6: yes.


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2. Cutrent Regulation: $\pm .02 \%$ or $\pm 50 \mu \mathrm{amp}$
3. Remote Voltage Programming: Full-range 0-40 v

Factory calibrated @ 100 ohms/volt $\pm .25 \%$
4. Remote Curvent Programming: Full range $15-500 \mathrm{ma}$ Factory calibrated @ 1 mho/ampere $\pm 1 \%$
5. Voltage Liminiting: Continuously adjustable 0-42 v
6. Current Limiting: Continuously adjustable $0-600 \mathrm{ma}$
7. Remote Voltage Sensing 8. Parallel Operation 9. Series Operation
10. Vernier Voltage Adjust: 5 mv resolution
11. Vernier Current Adjust: $50 \mu \mathrm{amp}$ resolution
12. Transicut-Free 13. Short-Circuit Proof
14. Extremely Fast Response: $25 \mu \mathrm{sec}$
15. Loz: Ripple: $500 \mu$ volts (voltage regulation mode)
$50 \mu$ amps (current regulation mode)
16. Conzection Cooling 17. Portable 18. Regulation Mode Sでitch
19. Master-Slacic Opcration 20. Excellent Long-Term Stability

Additional Specs ■ AC Input: 105-125 v, 1 $\varnothing, 47-420 \mathrm{cps}, 0.5 \mathrm{~A}$

- Max. Ambient Temp.: $45^{\circ} \mathrm{C}$ ■ Meters: Dual Scale 0-50 V.DC, 0-600 ma
- Dimensions: $51 / 9^{"} \mathrm{H}, 8^{\mu} \mathrm{W}, 9^{\prime \prime} \mathrm{D}$-adapter to mount two in $19^{\prime \prime}$ rack
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## NEWS

## 2.2-Gc Transmitter <br> Due for Telemetry

## Details Are Described at Mil-E-Con Along With Data on High-G System

DETAILS of one of the first transmitters under development for the new $2.2-\mathrm{Gc}$ telemetry band were disclosed last week in Washington, D. C., at the Fifth National Convention on Military Electronics (Mil-ECon). Also described were a high-g telemetry: system said to be capable of withstanding accelerative forces of more than $150,000 \mathrm{~g}$.

The transmitter, designed by Radiation, Inc., of Melbourne, Fla., will contain only solid-state components and a voltage-tunable magnetron. The device is intended for use in satellites, where it is to transmit simultaneously a number of phase-coherent carriers for a special measurement program.
Typical power output is to be 10 w for a 33 -w anode power input. The transmitter will weigh 40 lb and measure approximately $17-1 / 2$ by 8 by $5-3 / 4 \mathrm{in}$.

Because the magnetron must generate discrete, phase-coherent carriers, its anode voltage will be modulated by a vhf power amplifier. The frequency of this all-solid-state stage will determine the frequency separation between the carriers. Thus, says Radiation, Inc., modulation of the anode voltage will provide a frequency modulation of the magnetron center frequency. A phase-lock servo loop will provide frequency stabilization.

## Magnetron Amplifier to Have

## Efficiency of More Than 40 Per Cent

The amplifier that will provide power to modulate the magnetron will have an efficiency of more than 40 per cent, according to the company. It will be driven by a vhf crystal oscillator. Power will be supplied by a separate package in which magnetic amplifiers and regulating circuitry are to produce efficiencies ranging from 69 to 81 per cent for input voltages ranging from 30 to 22 v , respectively. The magnetron supply voltage of $2,000 \mathrm{v}$ is to be regulated over 0.2 per cent from 0 to 75 C .

Use of the 2.2-Gc telemetry band is expected to produce more stable frequencies for space communications than the $216-235-\mathrm{mc}$ band now being used.

High-G Telemetry System

## Projectile Speed Study

The high-g telemetry system described at the Mil-E-Con meeting is intended to aid study of the ionized shock layer generated by projectiles traveling at hyper velocities.

The airborne portion of the system is packaged as a $1.5-\mathrm{lb}$ projectile and is designed to be fired down an instrumented range into an oncoring narrow uhf beam transmitted at 8.5 and 11 Gc. A video crystal detector in the package receives the pulsed signal, which, after amplification frequency, modulates a $60-\mathrm{mc}$ oscillator in proportion to the amplitude of the incoming signal. A $60-\mathrm{mc}$ signal is then telemetered via diplexed antennas through the solid metal shell of the projectile to range receivers.

The project, described by Essad Tahan of Sylvania Electronics Systems, Waltham, Mass., is being conducted as a joint effort of Sylvania and the Canadian Armament Research and Development Establishment.

To withstand $150,000 \mathrm{~g}$ 's for several milliseconds, the telemetry package contains special components. Transistor cases were opened up and filled with an epoxy resin, a special microwave diode had to be developed, and the entire assembly had to be potted and reinforced in a glass-cloth laminate.

## Microminiature Timer for Arming Programs

 Uses Mirram Technique to Handle 370 WAmong the equipment on display was a 14oz digital arming program timer designed by Diamond Ordnance Fuze Laboratories, Washington, D.C. It was said to be the first operating device using the Micram microminiature packaging technique developed by Cleveland Metal Specialities Co., Cleveland, in cooperation with several large electronic companies. In this technique standard microminiature parts are densely packed on photoetched circuitry. The timer shown was said to be packed to a density equivalent to 300,000 components per cu ft.

The modularized unit, intended for use in missiles, includes a clock, timer, and readout and switching sections. It is said to have no moving parts. The clock uses a 24 point, 8-kc quartz-crystal oscillator having a 10 -cps output and an accuracy of 10 msec .

Aggregate power-handling capacity of the power-switching circuitry of the timer is 370 w says Cleveland Metal, which built the unit for DOFL. The company reports that the unit has been test flown successfully. It was developed under the Copperhead program. Cost of the unit is said to be in the $\$ 750-1,000$ range. -


Whenever you need voltage and power "regulation" for instrumentatiun purposes, especially transducer circuit:;, the new Bulova DC Reference Source assures maximum reliability.
In this Bulova double stage Zener model, regulation is accomplished by controlling the base voltage of a series power transisthe voltage chane first zener across input, are attenuated. The seond Zener source a voltage reference for feedback amplifier stage ( $\mathrm{Q}_{3}$ ).

Potentiometer connected to the base of the high beta transistor ( Q 3 ) allows the voltage on the arm of potentiometer to be compared with the reference voltage across reference Zener, and then the resulting voltage error being amplified and applied to the base of power cransistor $\left(Q_{1}\right)$.
A third transistor ( $Q_{2}$ ) is inserted to regula
A third transistor ( $Q_{2}$ ) is inserted to regulate the voltag of the input so that this is virtually non-existent (plus/minus


1 mv under all conditions).
In this circuit the output voltage follows the relation $V_{0}=V_{1}\left(\frac{R_{1}}{R_{2}}+1\right)$. It is evident that the circuit has to provide a voltage gain.
Obviously, looking to the equation, this supply can operate over a wide range of output voltage by changing the multiplier ratio $\frac{R_{1}}{R_{2}}$.
The Zener control current automatically changes with output voltage so that the ontrol voltage amplifier absorbs the difachieve optimum performance with high reliability using thoroughly silicon solid state devices. The small size $11 / h^{\prime \prime}$ square Ey $1^{3} 4^{\prime \prime}$, permits this unit to fit in any system which requires a DC reference source.

# RFI Studies Leading to Important Design Shifts 

New Requirements to Bar Square Pulse Modulation For Radar; Stiffen Other Equipment Requirements


#### Abstract

R ADICALLY new designs for radar and Rother military equipment will be demanded soon by the Defense Dept. in the light of its attack on radio frequency interference. The new specifications will eliminate in future equipment rectangular-pulse modulation of radar and many present antenna designs.


This was disclosed at the Third Annual Symposium on Radio Frequency Interference in Washington, D. C.

First set of specifications to near completion is a revised radar standard prepared by the Joint Frequency Allocation Board of the Joint Chiefs of Staff. Sufficient data for composing a tight, practical
standard have already been gathered. The requirements of the standard will reflect latest state-of-the-art techniques and component designs.

The standard will specify stricter control of radar fundamental frequencies and improved selectivity, dynamic range, sensitivity of radar receivers. It will also re-

## 'Thermal Circuit' Removes Heat in Miniature Modules

HINTS on how to design "thermal circuits" which represent solid-state (no fans) solutions to heat removal in miniature module packaging were given in a paper presented before the IRE Production Group, June 14 and 15 in Philadelphia.

The paper explained how miniature circuit modules had been mounted on a heatconductive ceramic board which provided an efficient heat removal path from the modules to a heat sink. The concept behind this type of packaging according to the paper is that with extreme miniaturization the designer may have to pay as much attention to the thermal "circuits" as he has in the past paid to the electrical ones

The authors, Gerald Kriss and Louis Po-


Beryllium oxide board 3 -in. square by 0.06 -in. thick was used for the thermal link between the modules and the heat sink which would be clamped on one edge. Kovar studs were weld points for the module leads of nickel-plated copper.
laski of General Electric Co.'s Space Vehicle Dept., Philadelphia, showed how their design used the thermally conductive but electrically insulating ceramic board to integrate the heat removal, circuit interconnection, and module support functions into one solution. In a space vehicle application they said that the board would be attached to the side of the vehicle.

A beryllium oxide ceramic board was chosen for its known combination of high thermal and low electrical conductivity. Kovar studs were inserted into the 0.06 -in thick board to transfer module lead heat and provide electrical connections from the module to the board's circuits. The board's circuits consisted of moly-manganese screened


Slice through module shows how two heat flow exit paths are provided out of module. The transistors are embedded in a high-thermal-conductivity silver-flakeloaded epoxy (lighter color) which is later epoxybonded to the ceramic board. Also, the leads are extra thick to conduct heat out to the Kovar studs.
on and fired then copper plated. Electrically oversized $0.06-\mathrm{in}$. module lead wires were used to carry out part of the heat.
The modules themselves were epoxy-potted in two stages. First, a high thermal conductivity silver-flake-loaded epoxy was used around the transistor cases (which were purposely located close to the board for shortest thermal exit path of their heat). Then a less thermally conductive but more electrically insulative alumina-loaded epoxy was used for the rest of the module.

The authors pointed out that ceramic boards of this type might be the only solution for rf or high-voltage microcircuits where proximity to conventional metallic heat removal surfaces cannot be tolerated. - -


Modules assombled on ceramic boord. Thermocouples at hot and cold spots of modules showed that the board provided as good a thermal conduction path between the modules and heat sink (not shown) as if the modules were attached directly to the heat sink. Transistor case-heat sink drops were 6 to 8 F .
quire reduction of out-of-band modulation components and will place limits or. frequency emissions.

To meet these requirements certain changes in design will have to be made. Thus, there will be a decrasing use of magnetrons, particularly at lower frequencies. It is anticipated that klystrons will be used in their place.
Rectangular pulses will no longer be permitted for radar modulation. Instead, there will be a shift to sine-cosine, $\cos ^{2}$ or gaussian pulses which do not cause emissions remote from the fundamental.
Antennas will have to be constructed with greater precision in order to limit off-frequency responses, spill-over, backside emission, etc. Also, there will be a need for high-power waveguide and transmission line filters to limit the transmitter emission to the tightly specified frequency bands, and in addition to limit receiver susceptibility:

Also disclosed at the Symposium was the progress made in the Department of Defense's Electromagnetic Compatibility Program. The major effort of the Program is currently devoted to establishing a Joint Analysis and Prediction Center in Annapolis, Md. This Center, being organized by the Armour Research Foundation, is charged with devising methods for predicting the electromagnetic environment at given geographic areas. To do this it will need data on environmental conditions and equipment emission characteristics (spectrum signatures).

A first test of the possibilities of prediction will be made in the San Diego area, one of the worst areas for electromagnetic interference in the country according to RFI specialists. Environmental data for the area have already been collected. Most of the spectrum signatures are, however, still to be gathered.

Armour is currently selecting a mathematical model for the project. Several models are being reviewed, including ones developed by Melpar, AMF, Georgia Tech, and Jansky and Bailey. Also yet to be chosen is the computer in which the information will be processed. Both the STRETCH and IBM 7090 units are said to be under consideration.

It is anticipated that data will be collected by February of 1962 , and the processing can begin. The Analysis and Prediction Center at Annapolis will be ready for occupancy by January of that year. - -

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## NEWS

## Two Advances Cited At Automation Parley

Digital Speed-Control System And Lightweight Motor Outlined

## Robert Cushman

Technical Editor
TWO PRACTICAL developments were described last week in Boulder, Colo., at the otherwise highly theoretical Joint Automatic Control Conference: a computercompatible digital speed servo and a very light, compact, powerful motor.

The digital speed-control system has been developed by Westinghouse Electric Corp. for large industrial process drives, such as those used in papermaking. It was explained that in papermaking not only is 0.1 per cent regulation desired for each drive but also, with the paper strips being driven through the mill at 3,000 ft per min by a $4,000-\mathrm{hp}$ system, it is important to be able to synchronize the speeds of all the drive motors along the process.

The digital speed servo has both position and speed loops. It includes all the features normally associated with analog servos, such as time-limit acceleration and vernier speed adjustment. Therefore it can be used directly in place of existing analog systems. Westinghouse says.
As might be expected, pulse rates from a master crystal reference are compared with feedback pulse rates from a digital tachometer connected to the output drive. A coincidence canceler had to be added to prevent ambiguity when pulses arrive at the same time.

Under steady operating conditions all of the control signal is provided by the position loop error. The position loop integrates the feedback and reference pulses from the coincidence pulse canceler by feeding them into the up and down lines of a high-speed reversible binary counter. The level of this counter is then determined by the respective pulse rates between reference and feedback, going up for one and down for the other. This level is then converted into an analog current level by a weighted decoder, and the level of this current is used to


Highly efficient de motor design is expected to produce $7-1 / 2 \mathrm{hp}$ inside a 5 -in. diam and with a weight of only 11 lb . Commutation would be by silicon-controlled rectifiers mounted in rotor and switched oplically by phototransistors.
drive the power amplifier.
The speed loop, on the other hand, operates on the difference of the pulse rates. Pulses from the reforence and feedback lines are made to cancel each other alternately.
Part of the significance of this type of system, according to Westinghouse, is that it facilitates digital computer control of large industrial processes.
The very lightweight, compact motor is a dc actuator, designed as a replacement for hydraulic actuators on missiles. The motor, said to be equally as efflicient but more reliable than its hydraulic counterpart, was described by Prof. George C. Neuton and R. W. Rasche of the Massachusetts Institute of Technology:

The design, which so far is only on paper, indicates a power rate of 550 kw per sec ( $7-1 / 2 \mathrm{hp}$ ) with a $\overline{5}$-in.-diam motor weighing only 11 lb . It will therefore be competitive with hydraulic actuators for missile applications, the authors contend. Hydraulic actuators have so far been much more powerful and efficient than any electric actuator, but they are less reliable because of their susceptibility to dirt.

The key to the MIT improvement is a highly efficient molded aluminum-epoxy-fiberglass rotor with integral conductors. It would be molded as a hollow shell and supported at one end, so that a ferromagnetic plug could be used inside the rotor to increase the flux. The rotor would be evaporatively cooled by a sprayed freon fog.

Other papers at the conference covered most of the topics of current interest to theoreticians in the automatic control field: optimization schemes including "cost" feedback loops, adaptive techniques, nonlinear control and statistical control.

The conference was held last Wednesday through Friday, June 28-30. - -

## Proven ultra-high-speed transistors by SPRAGUE



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- The well known slim-line Type 2N501A MicroAlloy Diffused-base Transistor, extensively used in critical military, industrial. and commercial applications, is now joined by the 2 N 1500 , in its low-height TO. 9 case.
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the advantages of direct-coupled circuitry with no loss in switching speed.
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- For prompt application engineering assistance, wrise Commercial Engineering Section, Sprague Electric Co. Concord, N.H.
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& \text { to } 3 \text { and } 3 \text { to } 10 \text {, each with } 10 \% \text { overlap; } 0 \text { to } 10 \mathrm{db} \\
& \text { scale Use as a sensitive null detector } 5 \mathrm{cps} \text { to } 30 \mathrm{Mc} \\
& \text { Use as a stable } 60 \mathrm{db} \text { wideband amplifier, } 2.5 \text { volts max. output Cathode follower } \\
& \text { probe has a voltage range of } 300 \mu \mathrm{~V} \text { to } 300 \mathrm{mV} \text {, and a high input impedance Instrument } \\
& \text { is average responding type. Effect of line transients nil } \text { Available in portable model } \\
& \text { shown or in } 19 \text { inch rack version. }
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## (D) Gil Gind UNa

VOLTAGE: $300 \mu \mathrm{~V}$ to 300 V .
FREQUENCY: 10 cps to 11 Mc (As a null detector, 5 cps to 30 Mc ).
ACCURACY: \% of reading anywhere on scale at any voltage. 20 cps to $2 \mathrm{Mc}-2 \% ; 10$ cps to $6 \mathrm{Mc}-4 \%$; 10 cps to $11 \mathrm{Mc}-6 \%$.
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# Hot TV Cooled Thermoelectrically 

Westinghouse Units Improve Operation of Vidicon Tube In Closed-Circuit System at Steel Plant Soaking Pits



Thermoelectrically cooled television camera (with front cover removed). At top are the heat-radiating fins of the cooling elements, which enclose the vidicon. Motors and pulleys af the bottom control the focus and aperture of the lens.


Cooling element consists of three Westinghouse WX-814 bismuth telluride units connected in series. Note common hot and cold plates and single set of input terminals.

THERMOELECTRIC coolers improve performance of the vidicon tube in a closedcircuit television system that monitors the operation of cranes at a steel mill.
Operating in a $140-\mathrm{F}$ ambient, three Westinghouse WX-814 coolers, with a total cooling capacity of 5 w , maintain the 7735 vidicon at 90 F and dissipate heat generated by filaments and deflection and focus coils. Without this cooling, operation of the tempera-ture-sensitive tube would be marginal.

The television system was built by General Precision Laboratory, Pleasantville, N.Y., for soaking pits at a large steel mill.

Because of the high ambient temperature and the camera's remote location (at the end of a traveling crane), thermoelectric elements were solected as the most practical cooling method.
"We couldn't use forced air at 140 F for cooling, and losses in long piping runs would have required about 250 w of mechanical refrigeration for the job," explained Murray Altman, designer of the camera. "Instead we provide the cooling directly at the point of use."

The three thermoelectric units, strapped together to provide common hot and cold junctions, draw about 16 amp and are 50 per cent efficient.

## Reliable Operation Is Essential <br> Because of Comera's Inaccessibility

The rest of the camera, however, is cooled by forced air at 140 F and operates at 160 F . Reliable operation despite elevated temperatures is particularly important because of the camera's relatively inaccessible location and a need for maintaining uninterrupted three-shift operation at the mill.

Much of the circuitry normally contained in a television camera was moved to more accessible boxes elsewhere on the crane. Only a $10-\mathrm{mc}$ video preamp strip was retained in the camera. Frame grid tubes, tantalum


Interior of camera. Left to right: aperture and focus controls, $10-\mathrm{mc}$ video preamp strip, and vidicon tube enclosed within the thermoelectric coolers.
capacitors and military components rated for 125 C service are used throughout. Modular construction is employed to speed maintenance.

The camera also includes motor-driven focusing and lens-aperture controls. The aperture controls respond automatically to the video signal level and adjust the lens diaphragm and vidicon target voltage to accommodate an illumination range of more than $2(0,0(0)$ to 1 . This readily covers the brightness range encountered between the white-hot soaking pit and the rest of the mill.

Other components of the television system, including the camera control unit, power supplies and voltage regulators are also designed for high-temperature operation. About one-third of the circuitry, including the synchronizing generator and portions of the power supply, are transistorized. Silicon units are specified.

The control unit is enclosed in a watertight case to exclude the ultrafine steel dust emanating from the soaking pits. Cooling is by means of a heat exchanger employing ambient air at 140 F .

Video signals are transmitted from the mobile crane to monitor viewers by slotted line and antenna probe arrangement.

Five of these television systems have been delivered by General Precision Laboratory. Initial units already installed are reported to be operating around the clock for several months between servicing. -


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[^2]

## Milestones in Engineering

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Soldiers whose very lives depended as much upon the quality of their weapons as upon their personal skill would settle for nothing less than the very best.

This first application of the principle of "Mil Spec" buying has been refined and tightened until, today, components intended for use in military equipment must be designed and built to meet the most exacting specifications, pass the most demanding tests, satisfy the most rigid requirements.


North Electric " 240 " 4 pole and " 260 " 6 pole sub-miniature sealed relays are precision designed and engineered to obtain maximum switching circuits in minimum space and meet specifications of MIL R-5757D at a breakthrough in price!
These heavy duty relays, which incorporate precision balanced rotary motors to withstand shock tests of 50 Gs and vibration tests of 1000 cps at 10 Gs , have a life expectancy in excess of 100,000 operations at rated load.
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## NEWS

## Foxboro Ends Exclusive Pact With RCA for Control Systems

Foxboro Co. of Foxboro, Mass., has severed its exclusive arrangement with Radio Corp. of America for joint development of industrial computer-control systems. The decision was announced in a statement that Foxboro has sent to its customers.

Foxboro, an instrumentation manufacturer, said it had become "sobered" by the many large technical and economic roadblocks to computer control of industrial processes. The company had been cooperating with RCA's Industrial Computer Div. in nearby Needham, Mass.

Now, Foxboro says, it will be freer to pursue more immediate, smaller-scale analog computer solutions to industrial automation.

Another reason for the Foxboro move, industry sources speculate, is that the company will now be in a position to sell its "sub-lomp" equipment to other digital process-control computer manufacturers.

## New National Group to Study Business Data Processing

A National Committee for Business DataProcessing is being formed under the sponsership of the Association for Computer Machinery. Its fields of interest will include business theory, operations research, management gaming, simulation and forecasting techniques, as well as the more usual business data-processing functions.

The association said that the formal organization of the committee would be completed at its September meeting in Los Angeles.

## Mobile Ground Surveillance Radar Will Be Modified AN/TPS-25

The Army's first mobile radar set for ground surveillance is under development by Hazeltine Corp. as $n$ modification of the shelter-housed AN/TPS-25 set now in operational use.

Conversion of the Hazeltine-built AN/ TPS-25 for use on tracked amphibious armored personnel carriers will involve three alterations: replacement of fixed antenna by a 25 -ft telescoping antenna mast for "quick look" capability at longer range; a smaller plotting board; and addition of an ac to de
converter for the $115-\mathrm{v}, 400$-cycle, gas-driven power unit.
The telescopic antenna will enable the set to detect moving targets at a range of more than 11 miles. At closer range, the set has the capability of distinguishing between the walk of a man and a woman up to a mile away.

## Device Measures Blood Volume With Improved Speed and Accuracy

A new instrument, the Volemetron, measures blood volume-or the volume of plasma or red cells-quickly and accurately. Regarded as a boon to surgeons, the instrument obviates the usual guess-work as well as the inaccurate method of weighing blood-soaked sponges (which does not account for blood on the patient or on the drapes).

Accurate to within 5 per cent, this transistorized product of Atomium Corp., a Waltham, Mass., affiliate of Perkin-Elmer Corp. uses well-known dilution-monitoring techniques. A measured amount of radioactive iodine is injected into the blood and allowed to circulate for a few minutes. After it is diluted in the blood stream, a sample of the isotope-diluted blood is placed in the Volemetron. A calibrated meter shows the blood volume in about a minute.

The instrument should help surgeons avoid the dangers of over or under-replacement of lost blood. While the Volemetron can be used by relatively unskilled personnel, earlier isotope-dilution measurements required highly skilled personnel with very complex instrumentation. The instruments were normally located in laboratories remote from operating rooms.


Transistorized digital circuitry counts oulput of scintillation counter which gives indication of radioactivity in patient's blood sample. Accurate measurements are first made of background radiation in patient's blood before he receives injection of measured dose of radioactive iodine.


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| Output | 115 volts. 400 CDS . single phase sinewave; voltage adiustable from 105 to 130 volts; 100 volt amp continuous duty. 150 volt amp intermittant duty |
| Output Regulation | $\pm 1 \%$ over full line or load change: response time 30 milliseconds inominal) |
| Harmonic Distortion | less than $2 \%$ under severest line and load conditions |
| Frequency Stability | $\pm \frac{1}{4} \%$ over mar. line and load change. or over ambient temperature range ( $0^{\prime}$ 10 $40^{\circ} \mathrm{C}$ ) |
| Frequency Setting | $400 \cos \pm 0.5{ }^{\circ}$ 。 |
| Synchronization | 25V RMS. 2000 ohms impedance: range 390 to 410 cps |
| Dimensions | $3 \frac{1}{2}{ }^{\circ} \times 19^{\circ} \times 10 \mathrm{t}^{\text {" }}$ max. depth (for standard rack mounting) |
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A new instrument, the Volemetron, measures blood volume-or the volume of plasma or red cells-quickly and accurately. Regarded as a boon to surgeons, the instrument obviates the usual guess-work as well as the inaccurate method of weighing blood-soaked sponges (which does not account for blood on the patient or on the drapes).

Accurate to within 5 per cent, this transistorized product of Atomium Corp., a Waltham, Mass., affiliate of Perkin-Elmer Corp. uses well-known dilution-monitoring techniques. A measured amount of radioactive iodine is injected into the blood and allowed to circulate for a few minutes. After it is diluted in the blond stream, a sample of the isotope-diluted blood is placed in the Volemetron. A calibrated meter shows the blood volume in about a minute.

The instrument should help surgens avoid the dangers of over or under-replacement of lost blood. While the Volemetron can be used by relatively unskilled personnel, earlier isotope-dilution measurements required highly skilled personnel with very complex instrumentation. The instruments ware normally located in laboratories remote from operating rooms.


Transistorized digital circuitry counts output of scintillation counter which gives indication of radioactivity in patient's blood sample. Accurate measurements are first made of background radiation in patient's blood before he receives injection of measured dose of radioactive iodine.


Whether you're developing an advanced servo system, verifying inertial guidance performance, checking out aircraft instrumentation or testing radar subassemblies - the chances are you need a convenient source of 400 cycle power. With MRC's portable frequency changer, 400 cycle service is within plug-in distance of the nearest 115 volt AC outlet. There 's no more need to depend on limited availability of built-in 400 cycle utility service - where troublesome line fluctuations can disrupt sensitive tests. The solid state converter weighs only 30 lbs ., yet provides 100 VA 's of well regulated sinewave power-free of distortion and unaffected by line or load changes. Its static, solid state design assures cool, efficient and silent operation. For added flexibility, it's packaged for either bench or rack mounting. Let this versatile unit assure you of dependable 400 cycle service . . . anywhere!


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Harmonic Distortion less than $2 \%$ under severest line and load conditions

| Harmonic Distortion | less than $2 \%$ under severest line and load conditions |
| :--- | :---: | :--- |
| Frequency Stability | $\pm y^{\prime}$ over max. line and load change. or over ambient temperature range $10^{\circ}$ to $40^{\circ} \mathrm{C}$ ) |
| Frequency Satting | $400 \mathrm{cDS} \pm 0.5 \sigma^{\circ}$ | Synchronization 25V RMS. 2000 ohms impadance: range 390 to 410 cDs Dimensions - $\quad 3 \mathrm{~s}^{\circ} \times 19^{\circ} \times 10 \mathfrak{x}^{-0}$ max depth (for standard rack mounting) Design Features automatic short circuit and overload protection; printed circuits.

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## NEWS

## Styrofoam Antenna Can Be Built on Site

## New Radar Dish Reported to Weigh

 Fifth as Much as Metal ParabolicsALIGHTWEIGHT radar antenna of styrofoam planks is designed to be machined and assembled directly at the radar site.

It is, its developer says, only one-fifth the weight of metal parabolic dishes. Transport ability and lightness are further enhanced by a novel antenna positioning device that employs a series of hydraulic jacks to steer the antenna.

The new dish was developed by Sylvania's Electronic Defense Laboratories of Mountain View, Calif. To construct it, one joins styrofoam planks into an egg-crate structure using urethane foamed-in-place seams. A computer-controlled milling machine, designed by Sylvania then automatically machines the reflector to the desired shape. For high-precision reflectors, a solid layer is first foamed-in-place over the cellular structure.

The reflective surface is then machined from this layer and is metalized by application of aluminum foil or copper mesh. A final layer of foam is then applied to protect the reflective surface and to receive the mounting plate.

## Milling Maching Also Shapes

Front End of the Antenno
The front of the antenna is also contoured by the milling machine. This provides a slight amount of beam focusing, but, more important, it streamlines the antenna to reduce wind drag by as much as two-thirds over conventional parabolic reflectors, the company says.

The feed system is buried in the foam for rigid support. The outer surface is then covered with a white fiber-glass skin for weath-er-proofing and to minimize solar heating.

The computer-controlled milling machine that shapes the antenna consists of light weight, readily disassemblable parts that can be conveniently transported to the fabrication site. Antennas up to 20 ft in diameter can be fabricated with the present machine Equipment and techniques to make antennas up to 50 ft across are being developed.


Foam antenna is examined by its developer, Mack Suliteanu, engineer at Sylvania's Electronic Defense Laboratories. Semi-transparent fiber-glass mesh covering the face of the antenna forms a base for a subsequently applied outer plastic coating. Note feed horn buried in the foam. The antenna is supported by a series of hydraulic jacks that can be programed to impart any desired tracking motion to the antenna.

The computer itself is an analog instrument, programed to fabricate a given contour by inserting pre-calculated constants into a series of potentiometers.

A hydraulic positioning system replaces the conventional system of mounting rings, bearings and driving motors. The antenna is supported by four tripods, each consisting of three hydraulic jacks. Programed changes in the length of each leg, controlled by at digital computer and hydraulic servo steer the antenna through any desired search or track pattern.

Operation of the positioning system has been confirmed by manual programing, but the computer required for automatic operation is still in development.

This arrangement results in an unusual antenna motion. In a $360-\mathrm{deg}$ horizon search, for example, the antenna rolls on its edge through a full circle. In overhead tracking the reflector merely flips over between opposite horizons.

The hydraulic positioner is "much faster" than conventional antenna drives, according to a Sylvania spokesman. This is due to the inherently fast response of the hydraulic system and to the reduced inertial and gyrating loads of the foam antenna with its unusual rolling motion.

The antenna and positioning system were developed under a contract from the Army Signal Corps. - -

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# Nationwide Data Loop Speeds Airline Work 

## 1,000-Station Centralized System

 Uses Both Fast and Slow Bit RatesANATIONWIDE data-processing loop linking all ticket agents of United Air Lines to a central computer has been put into operation.

The loop has:

- A main trunk in which the data are transmitted at 1,000 bits per sec.
- Secondary lines, which feed into the main trunk at 75 bits per sec. Once the information reaches the main trunk, however, it is speeded to 1,000 bits per sec.

The system handles flight reservations from 1,000 stations around the country to a central nrocessing terminal in Denver. Agents in najor cities-about 80 per cent of all the agents-are linked directly to the fast trunk, and those in smaller cities to the slower lines. Use of the slower lines permits a considerable savings in operating costs.

The loop, called Instamatic, was designed for United Air Lines by the Teleregister Corp. of Stamford, Conn. Data communication equipment was constructed by North American Philips Co., Inc., of New York City.

## Central Units Include Trunk

Terminal, Computer and Memory
The electronic equipment in the system includes a Central Trunk Terminal in Denver and a series of concentrators along two loops running east and west from Denver. Each loop is composed of two telephone trunk lines that carry traffic at the rate of 1,000 bits per sec in opposite directions.

A central processing computer and memory storage unit is also in Denver.

The central terminal links the trunk lines with the processor. Equipment at the terminal regulates information going into and out of the computer, handles the reception and transmission of traffic through the trunk lines, and detects errors in messages by applying horizontal and vertical parity checks.

Messages concerning such information as availability of space on a certain flight are generated and received at agent sets. These


Map of western portion of Instamatic flight-reservation network shows (1) Concentrator, (2) High-speed trunk line, (3) Low-speed line, (4) Distant Central Office Transceiver, (5) Keyset Multiple Selector, and (6) Agent set.
sets also contain printing units on which reservation confirmation information and cancellations are printed.

At the concentrators, messages are handled and operations carried out at the rate of 54,000 per hr, Philips says. The concentrators along the trunk lines continually read the addresses of all messages passing through the circuit, determining whether they are for agent sets under their control or are to be forwarded. And they check them for errors.

## 11 Switching to Spare Unit

Possible in Case of Failure
Concentrators also answer test and supervisory messages from the control center in Denver. Finally, if necessary, they can switch traffic to a spare unit should there be a mechanical or electrical failure.

Theoretically ticket agents can receive information about the availability of seats on a given flight up to a year in advance. The average elapsed time from the moment an agent on the main trunk sends the question until he receives an answer from the central terminal is 1 sec . Response time on the secondary lines is slightly longer, owing to the time lag in storage and retransmission. Here it is about $5-1 / 2$ sec.

Engineers have included in the system provisions for redesign and the addition of other services. These could include maintenance of passenger records, fare computations, flight-crew schedules, and anything else to insure a high operational speed. -

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## NEWS

## Twofold Rise Seen In Consumer Sales

## Executive Predicts an Industry Volume of $\$ 21$ Billion by 1970

C ONSUMER electronic sales will double in the next decade-from $\$ 10.2$ billion last year to $\$ 21$ billion by $1970-$ W. Walter Watts, chairman of RCA Sales Corp., told the June 19-20 Chicago Spring Conference on Broadcast and TV Receivers.

Among the new products to be offered in the near future, he said, are multiplex adapters to receive the newly approved fm stereo broadcasts. More than 75 per cent of present fm stations have indicated they will be broadcasting stereo within a year or two.

Color TV, in which RCA pioneered, for many years, Mr. Watts said, is now included in the marketing plans of almost all major TV manufacturers. Closed-circuit TV for industrial uses and educational TV offer additional sales areas for the TV'set supplier, he added.

Other prospects listed by the electronic executive included transistorized TV sets, electronic air-conditioners and home videotape recorders. These await clever ideas by design engineers, he said.

Various approaches to the design of multiplex adapters were discussed at the conference. Major manufacturers are ready to supply adapters that are either self-powered or obtain power from the basic fm tuner or amplifier chassis, it was indicated. Several one-tube and two-tube schemes have been devised, it was brought out, but most manufacturers prefer to field-test their units rather than risk consumer drop in interest following hasty, premature product delivery.
The radio-TV industry has long awaited
Table 1. Per Cent Tube Failures by Year and by Circuit Application

| Circuit | July to July Test |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & 1954 \\ & 1955 \end{aligned}$ | $\begin{aligned} & 1955 \\ & 1956 \end{aligned}$ | $1956$ | $\begin{aligned} & 1957 \\ & 1958 \end{aligned}$ | $\begin{aligned} & 1958 \\ & 1959 \end{aligned}$ | $\begin{aligned} & 1959 \\ & 1960 \end{aligned}$ |
| Horiz. Defl. | 25 | 34 | 17 | 10 | 10 | 5 |
| Amp. Defl. Vert. Del |  |  |  |  |  |  |
| Amp. | 25 | 29 | 16 | 3 | 5 | 1 |
| Damper | 33 | 17 | 9 | 15 | 9 | 5 |
| VHF Amp. | 22 | 18 | 7 | 12 | 10 | ${ }_{12}^{5}$ |

ELECTRONIC DESIGN • July 5, 1961

Table 2. Per Cent Tube Failure By Cause and Year

| Cause | 1955 | 1956 | $\frac{1957}{}$ | $\frac{1958}{}$ | 1959 | 1960 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Open <br> Heater | 1.86 | 1.775 | 1.025 | 1.17 | 0.73 | 0.725 |
| Shorts | 2.02 | 1.17 | 1.19 | 0.935 | 1.08 | 0.83 |
| Arcing | - | 0.72 | 0.22 | 0.56 | 0.34 | 0.76 |
| Gas | 1.50 | 0.82 | 0.29 | 0.14 | 0 | 0 |
| Other | 1.35 | 1.37 | 1.20 | 1.5 | 1.45 | 1.3 |

stereo fm approval as a boom to a saturated and dropping TV market, conferees said privately. Pessimists were wary of rushing into production and delivery with out adequate field experience.

Strides in receiving tube reliability were outlined by a company applications engineer, E. H. Boden. In 1954, he said, Sylvania began a reliability study TV receiver tubes. The tubes were operated in various manufacturers' sets under $130-v$ ac input for 50 min , turned off for 10 min and then turned on again. This cycle was repeated each hour for $1, j 00 \mathrm{hr}$. Mr. Boden noted that 59 per cent of the tube failures occurred in five circuits: horizontal-output, damper, vertical deflection-amplifier, rf-amplifier and uhfoscillator.

From 1950 to 1960 , he said, horizontalamplifier failure was reduced from 34 per cent to 5 ; vertical-amplifier from 29 per cent to 1, and rf-amplifier from 22 to 5 per cent (see Table 1 and 2). Tubes exhibiting no failure after 1500 hr at $130-\mathrm{v}$ ac cycling, increased from 38.5 to 72.5 per cent. From tests comparing the life of single and double-section tubes used in similar applications, Mr. Boden reported, Sylvania concluded that no serious difference in reliability was noted.

Pigeon Wired for VHF Tracking


Miniature vhf transmitter riding piggyback on this homing pigeon was used to track the bird for 25 miles. The $140-\mathrm{mc}$, crystal-controlled transmitter, powered by four mercury cells, delivers about 1 mw to a modified half-wave dipole antenna. The 5 -oz transmitter package was developed by American Electronics Laboratories for an animal homing instinct study of the Office of Naval Research


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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TVAE | $\begin{aligned} & \text { Vee } \\ & \text { velte } \end{aligned}$ | $\begin{aligned} & \text { vee } \\ & \text { vone } \end{aligned}$ | ${ }^{16}$ | 9] | $\begin{aligned} & \operatorname{mix} . \\ & \operatorname{losen} \\ & \ln 0 \end{aligned}$ | Hes | Ree |  |
| ${ }^{2 N 173 .}$ | -80 | -60 | ${ }^{18}$ | 100 | 8 | 82 | 10 | - |
| $2 \times 170^{\circ}$ | -70 | -80 | 18 | 100 | - | 87 | 10 | - |
| 2N174A | -70 | -80 | 18 | 100 | - | 97 | 10 | - |
| $2 \mathrm{2N277}$ | -40 |  | 188 | 100 100 | 8 | 62 | 10 10 | 8 |
| 2N270 2N441 | -480 | -80 | 188 | 100 100 | : | 82 | 10 | 8 |
| ${ }_{2} \mathbf{N 4 4} 4$ | -480 | -80 | 18 | 100 | : | 80 | 10 | - |
| 2 N 448 | -80 | -80 | 18 | 100 | - | so | 10 | . |
| 2 N 1089 | -90 | -00 | 18 | 100 | - | B2 | 10 | . |
| 2 21100 | -a | -100 | 18 | 100 | - | 87 | 10 | , |
| 201889 ${ }^{\text {a }}$ | -70 | -80 | 18 | 100 | - | 37 | 10 | . |
| 2 21412 | -80 | -100 | 18 | 100 | - | 17 | 10 | . |
| 2 m 1970 | -80 i1) | . 100 | 10 | 100 | 4 | 29 | 10 | . |

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## WASHINGTON REPORT

The proposed all-out acceleration of the National Space Program puts NASA in the market for a wide range of professional and technical skills. Of particular concern to the agency is its need for personnel to fill key professional and administrative posts, carrying responsibilities for which industry is willing to pay from 25 to 100 per cent higher salaries.

NASA is now seeking a bigger allotment of grades eligible for salaries above the ceiling for career Government service. Its present authorization is for 290 such positions at salaries up to $\$ 19,000$, with 17 of them earmarked for a special top bracket of $\$ 21,000$. The agency has requested Congress to authorize 135 more "excepted" positions for a total of $42 \overline{5}$, of which 30 would be in line for the $\$ 21,000$ maximum. In order to hold key personnel, NASA would reserve some of the new salary authorizations for its present staff. But, many of the new posts would have to be filled from the outside.

The agency is currently engaged in a recruiting drive to fill some 500 jobs ranging from technicians to experienced scientists. Its campaign has included the college campuses, where last year NASA representatives interviewed 3,000 grads in competition with industry's talent scouts. In fiscal '62 a 4,000 increase in personnel is projected.
Industry's Space Work Load will increase sharply along with NASA'S, if, as seems likely, Congress goes along with the President's recommendation that the nation mount a crash program to gain undisputed leadership in lunar and planetary exploration. It will be primarily an R\&D workload, with heavy demand for top-flight scientists.

Congress willing, the space agency's estimated expenditures in fiscal ' 62 will total an estimated $\$ 1.7$ billion for an increase of 43 per cent over the original budget submitted by the outgoing Eisenhower administration. Of this amount, almost $\$ 1.3$ billion is earmarked for R\&D, with the man-in-space program getting the overwhelming share.

Space agency procurement officials estimate that at least 80 per cent of NASA'S R\&D spending will be placed under contract with industry, the universities and other private organizations. These officials are now at work revising procedures in an effort to reduce time lags in selecting contractors and conducting contract negotiations.
AIR FORCE TO PUSH DATA AUTOMATION
Incentive type CPFF contracts have been used to a limited potential of data automation techniques is the Air Force decision to set up an office to coordinate and foster improvements in automated data-processing systems for both administrative and command and control functions.

The new activity, which will become operational Aug. 1 under the Air Force Comptroller's Office, will evaluate the data requirements and existing data-processing facilities of all administrative
more precisely, to foster development of new system design concepts and to seek improvements through the re-engineering of existing facilities.

## IN SEARCH OF COMPETITION

Top Defense Dept. officials have promised Congress an intensive new effort to curtail sole-source procurement, which is chiefly responsible for the fact that 60 per cent of military contracting is noncompetitive.

The growing complexity of military hardware and the frequent need for telescoping development and first-run production to shorten lead time inevitably have fostered single-source buying. But while award of first-run production to development contractors is considered a justifiable expedient in most cases, defense officials readily acknowledge that the services should seek competition for follow-on production.
Delayed Delivery of Technical Data and manufacturing drawings accounts for a good deal of the failure to shift promptly from singlesource to competitive buying. Thus the Pentagon intends to ride herd on procurement agencies to see that the Government gets the data to which it is entitled in time for competitive re-procurement. Contractors may be subject to financial penalties for failure to meet contract provisions on this score.

Such action, in turn, will require further steps to insure that the data ordered by the procurement agencies are adequate for re-procurement. Studies have indicated considerable laxity in specifying the Government's rights to data during contract negotiations.

In some cases, data are unavoidably incomplete because contractors withhold "proprietary" information. However, regulations defining such information are currently under review, and indications are that contractors will be subject to further restrictions on what they can claim as trade secrets.

Despite all efforts to correct deficiencies, some sole-source procurement will persist, even though adequate technical data and drawings are available, for the reason that quality cannot otherwise be assured.
NEW COST REDUCTION TACTICS
The Pentagon has instituted what amounts to an R\&D program on contracting techniques. It is investigating all sorts of schemes to achieve tighter control of costs under the controversial cost-plus-fixed-fee contracts, which now account for 42 per cent of military expenditures, compared with 24 per cent only five years ago.

CPFF contracts, like sole-source procurement, started as an expedient but rapidly became common practice owing to the difficulty of projecting costs for complex weapons systems and to the pressure for concurrent development and production.

Incentive type CPFF contracts have been used to a limited extent in an effort to capture the profit motivation and risk-taking inherent in fixed-price contracts. Defense officials now want to make greater use of incentive contracting. But they also want to provide a wider range of incentives and stiffer penalties, as well as more effective means of evaluating technical and cost performance.
Imaginative. If Nothing Else, is is proposed new form of incentive contract dubbed the "cost-plus-award-fee contract." It would provide that a board of assessors evaluate a contractor's technical and cost performance during the life of a contract and determine his exact fee on completion of the work.


## Sprague type 73Z1 core-transistor DECADE COUNTERS

Sprague's Special Products Division, the largest and most complete facility in the magnetics industry, offers a simple yet versatile, low-cost yet reliable component for counter applications. Counting to speeds of 10 kc , the 73 Zl decade counter provides an output signal for every 10 input pulses, then resets in preparation for the next cycle. For higher counting, two or more counters may be cascaded. Typical characteristics are shown in the following table:

| CHARACTERISTIC | INPUT | OUTPUT |
| :---: | :---: | :---: |
| Amplitude | 1.5 to 8 volts | 6.5 volts min. |
| Pulse Width | $1 \mu \mathrm{sec}$ min. | $50 \mu \mathrm{sec}$ nom. |
| Impedance | 100 ohms | 20 ohms |

Utilizing two rectangular hysteresis loop magnetic cores and two junction transistors to perform the counting operation, the $73 \mathrm{Z1}$ counter is encapsulated in epoxy resin for protection against adverse environmental conditions. It has five terminals-B+(12v $\pm 10 \%)$, input, output, ground, and manual reset.

The 73 Z 1 decade counter is available as a standard item. However, "customer engineered" designs can be supplied when other counting cycles, speeds, and package configurations are required for special applications.

Other Special Products Division components for the digital equipment industry include: LOGILINE $5 \mathrm{mc} / \mathrm{s}$ digital circuits; $1 \mu \mathrm{sec}$ access time memory; magnetic shift registers and logic components; computer pulse transformers; switching transformers; precision toroidal inductors.

For complete sechnical data or application assistance on the 7321 counter or other Sprague components, write to Special Products Division, Sprague Electric Co., 347 Marshall Street, Nortb Adams, Massachwsetts.
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- Single and Polycrystalline forms doped to your specifications
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## SPECIAL PACKAGING

To prevent in-transit da mage to electronic properties, ingots of Cominco Indium Antimonide are sealed in polyethylene and shipped in shockproof containers. Fabricated shapes are suspended in an inert liquid.

## plus

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## NEWS

## 400-Cps Phase-Shift Standard Useful from 0 to 180 Deg

Designers at the National Bureau of Standards, Washington, D. C., have designed a phase-angle master standard said to be capable of measuring phase shift to within 0.01 deg at 400 cps . It can do this reportedly from 0 to 180 deg .

The instrument consists of $12 \pi$-sections each of 14.6 deg , and three $4.3-\mathrm{deg} \pi \mathrm{sec}-$ tions, plus switching arrangements that permit any combination of sections to be connected as a delay line. It was considered desirable, the bureau reports, to provide several different phase-shift steps and a continuously variable fine control.

The input to the delay line is used as part of an RC network that incorporates 10 capacitor steps, each giving 0.44-deg of phase shift.

According to NBS, all $\pi_{\pi}$-sections must be exactly adjusted to have the same characteristic impedance in order to prevent reflections and to make the phase shift put in by the RC circuit independent of the number of $\pi$-sections connected.

Similar phase-angle standards could be made for higher audio frequencies, but the upper limit in frequency would probably be about 20 kc , the bureau believes. At higher frequencies, reportedly, stray capacitance introduced by connecting and switching leads might prove troublesome. However, it might be feasible to use the same master standard over a 2 -to- 1 frequency range by readjustments on the $\pi$-sections and termination for each frequency.


Phase-angle master standard designed by National Bureau of Standards operates continuously from 0 to 180 deg at 400 cps with 0.01 -deg accuracy. One of the designers, H. N. Cones, adjusts a mercury conlact for a portion of $\pi$-section used as delay line.

AMERICAN MACHINE \& FOUNDRY COMPANY
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* Wrife foday for further information
and spacifictions



## Contact Redundancy in New UNION Crystal Case Relays

The UNION 2-pole double throw General Purpose Crystal Case Relay is designed to consistently meet the requirements of Mil-R-5757D and Mil-R 5757 10. Its essential features . . . from mininıum size to optimum reliability
 rotary armature provides maximum resistance to severe shock and vibration.

This small 4-PDT-10-Ampere relay is currently available with II5VAC and various DC operating voltages. Various mounting styles are provided. Write for bulletin 1069.
permit it to be used in aircraft, guided missiles, shipboard and ground control electronic equipment.
A unique torsion-wire armature suspension system and a rugged all-welded frame construction provide a high level of vibration and shock immunity. Contact redundancy, which assures reliability in dry circuit and higher level contac loads, is provided through the use of bifurcated contacts.
Available with $0.2^{\prime \prime}$ grid-spaced header or "S" type header, with various mountings, terminals, and operating voltages. Write for Bulletin 1064.

## Why UNION Relays Are So Denendable

There's a good reason why our relays are the standard for reliability. For years, we ${ }^{\text {ve }}$ been building tough. reliable relays for use in airborne and guided missile electronic equipment and similar vital applications where perfect operation under severe environmental conditions is mandatory
Our engineers created a compact 6-PDT miniature relay with just three major assemblies . . . instead of a fistful of small parts. This was accomplished by using a balanced rotary-type armature that provided a maximum resistance to the severe shock and vibration environment of aircraft and guided missiles. The rotary principle of operation is utilized in all our relays.
We have a reputation for building reliable electronic components and we intend to maintain our tradition for building reliable relays. And we supply these quality relays in quantity. Stocks are now available for prototype requirements in New York, Pittsburgh, Dallas and Los Angeles

For additional information, write for Bulletin 1017 or call Churchill 2-5000 in Pitrsburgh.
MEMBER OF THE NATIOMAL ASSOCIATION OF RELAY MAMUFACTURERS
UN O N S W ITCH \& S G G NAL DIVISION OF WESTINGHOUSE AIR BRAKE COMPANY PITTSBURGH 1B, PENNSYLVANIA

## Space Center Awards $\$ 7$ Million In Work Contracts in a Month

More than $\$ 7$ million in contracts were awarded in April by the George C. Marshall Space Flight Center of the National Aeronautics and Space Administration, Huntsville, Ala. Manufacturers and Government agencies in 16 states and the District of Columbia shared in the awards.

Of the total, more than $\$ 2$ million in work went to industrial concerns in Texas; $\$ 2$ million to private and Federal groups in Alabama, Florida, Georgia and Tennessee; $\$ 800,000$ in California; more than $\$ 1 \mathrm{mil}$ lion in Connecticut, Massachusetts, New Jersey, New York, Pennsylvania and Washington, D. C., and more than $\$ 300,000$ in Indiana, Illinois, Michigan, Ohio and Wisconsin.

The contracts to manufacturers ranged from $\$ 2,083,832$ to the Chance Vought Corp. of Dallas, Tex. - the largest single award - for 70-in. fuel and oxidizer tanks for Saturn; to $\$ 5,065$ to the Interelectronics Corp. of New York City for transmitters.

Epsco, Inc., of Cambridge, Mass., has announced receipt of a $\$ 360,000$ contract from the Goddard Space Flight Center in Maryland for three pulse-code-modulation receiving stations.

## Million-Bit Computer Aids Navy



This real-time computer, designated AN/USQ-20V collects, processes and evaluates naval tactical data in combat and recommends courses of action. The memory section contains 1 million bits of information. Thirty-bits, comprising a single word, can be drawn from any location in the memory in $2.5 \mu \mathrm{sec}$. The com puters are being produced by Remington Rand Univac St, Paul, Minn., under a $\$ 5,534,526$ contract.
the raw materials of progress


## Big help in thinking small:

## 7 times more cooling power with FC-75 and FC-43!

For substantial space-saving, weight-saving reductions in the design of electronic equipment, look to 3M Brand Fluorochemical Liquids FC-75 and FC-43! Their heat transfer capabilities are outstanding. Since these fluids boil at $100^{\circ} \mathrm{C}$. (FC-75) and $180^{\circ} \mathrm{C}$. (FC-43), their heats of vaporization can be used to effect heat removal by at least seven times the rate of nonvolatile organic liquid coolants.

Getting down to cases: the heat removal capacity of FC-75 and FC-43 helped Hughes Aircraft designers to miniaturize the com-
munications power unit (shown above) by a factor of six. For Raytheon designers, a transformer was reduced by 4 to 1 in volume and by 2 to 1 in weight, without impairment of performance or power output.

If you are designing in the electrical, electronics, missile or jet aircraft fields, look into the miniaturization help that the dielectric strength, limited solubility, thermal stability, and low pour points of FC-75 and FC-43 can offer. After reading the "Properties Profile," write for further information

PROPERTIES PROFILE
on 3M Brand Inert Liquids FC-75 AND FC-43

These unique dielectric coolants possess unusual properties that can prove advantageous to the designer of electrical devices and instruments, as well as to the manufacturer. Increased range of operating temperatures, improved heat dissipa lion which permits miniaturization, and greatly increased protection from thermal or electrical overload are possible with their use.
FC. 75 and FC. 43 are non-explosive, non flammable, non-toxic, odorless and non-corrosive. They are stable up to $750^{\circ}$., and are completely compatible with most materiais . . . even above the maximum temperatures permissible with all other dielectric coolants. Both are selfhealing after repeated arcing in either the liquid or vapor state.

## ELECTRICAL PROPERTIES

|  | FC. 75 | FC-43 |
| :---: | :---: | :---: |
| Electrical Strength | 35kV | 40 KV |
| Dielectric Constant (1 to 40 KC (ct $75^{\circ} \mathrm{F}$.) | 1.86 | 1.86 |
| Dissipation Factor (1000 cycles) | 0.0005 | 0.0005 |

TYPICAL PHYSICAL PROPERTIES

|  | FC-75 | FC-43 |
| :---: | :---: | :---: |
| Pour Point | <-100 ${ }^{\circ} \mathrm{F}$. | $-58^{\circ} \mathrm{F}$. |
| Boling Point | $212^{\circ} \mathrm{F}$. | $340{ }^{\circ} \mathrm{F}$. |
| Density | 1.77 | 1.88 |
| Surface Tension ( $77^{\circ} \mathrm{F}$.) (dynes/cm) | 15 | 16 |
| Viscosity Centistokes | 0.65 min. | 2.74 |
| Thermal Stability | $750^{\circ} \mathrm{F}$. | $600^{\circ} \mathrm{F}$. |
| Chemical Stability | Inert | Inert |
| Radiation Resistance | $\begin{gathered} 25 \% \\ \text { change } \\ 1 \times 10^{(a)} \\ \text { rads } \end{gathered}$ | $\begin{gathered} 25 \% \\ \text { change } \\ 1 \times 10^{0} \\ \text { rads } \end{gathered}$ |

FC. 75 and FC. 43 have nearly equivalent heat capacities in the liquid and gaseous states.
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Repetition Rate 0.2 to 25 cps , Logarithmic and Linear

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Price \$895.00, Pob. factory. (\$985.00 F.A.S., N. Y.)
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Price $\$ 795.00$, f.o.b. factory. (\$875.00 FA.S., N. Y.)
50 kc to $20 \mathrm{mc} .$. Marka-SWeC户 model video For Flixed Band Video

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Price $\$ 795.00$, f.o.b. lactory. ( $\$ 875.00$ F.A.S., N. Y.)
1 mc 10260 mc ... Rada-Sweep Sr. For Production Alignmemt

- 6 Fixed Bands - Pulse Markers

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- Fundamental Frequonc
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## NEWS

## Doppler Navigator on Way For All Aircraft Types

A versatile navigation system applicable to all types of aircraft including fixed-wing rotary, vertical/short take-off and landing, drones and airships is under development.
Called the Ryanav IV, the completely selfcontained unit is undergoing air tests in a DC-3 of Ryan Electronics of San Diego, the system's developer. The system is reported to provide "all-weather, automatic navigation and hovering, without radio aids, wind estimates or true air speed data."

The Ryanav IV, the company says, accommodates all speed ranges from - 50 knots to $+2,000$ knots; all altitudes from 0 to 70,000 ft; drift velocities from 0 to $\pm 300$ knots; velocities from -50 knots to $+2,000$; ground track from 0 to 360 deg , and vertical velocities to $\mathbf{6 0 , 0 0 0} \mathrm{ft}$ per min.

Velocity error is less than $1 / 2$ per cent and navigation positional error 0.7 per cent of the distance traveled, Ryan says. The hovering threshold is put at $1 / 4$ knot. The use of pure continuous-wave techniques permits this accuracy to be achieved without altitude or attitude "holes," from take-off to landing, according to the company.

Ground Speed and Drift
Computed on Visual Displays
Its electrical outputs are: heading velocity, drift velocity, vertical velocity, ground speed, ground track, drift angle, true heading, and east-west, north-south distance traveled. Visual displays include a navigation indicator showing ground speed and ground track, or wind speed and wind heading; a hovering indicator showing heading velocity, drift velocity, vertical velocity and a control indicator with five switch positions: Off, Silence, Land, Sea and Test.

The receiver-transmitter in the Ryanav IV is designed as a space-duplexed, fixedantenna system with no moving parts and requiring no adjustments. Attitude capability is not limited by radome cutout area or the gimbals usually found in systems employing stabilized antennas. Supersonic speeds are accommodated simply by shift ing the receiver band. No change in antenna angles or other system parameters is necessary.

Outputs are provided for tie-in with plot-
ting boards and other position-indicating equipment, inertial navigation equipment, bomb-director sets, anti-submarine warfare sets, and terrain-clearance radar.

The Ryanav IV employs continuous-wave eletromagnetic energy at $13,300 \mathrm{mc}$. The set's antenna directs this energy toward the earth's surface in three narrow beams. The frequency of the energy back-scattered from the ground is "Doppler shifted" by an amount proportional to the aircraft's velocity along the individual beam. The three Doppler frequencies are measured and used to compute the aircraft's velocity components. This is accomplished in the converter/computer unit, which comprises a low-voltage power supply module, a frequency-tracker module, a frequency-converter and velocity-computer module, and a computer module.

The various configurations of the Ryanav IV family of Doppler ground-velocity indicators may omit, modify or add certain units to meet specific needs. Antennas can be provided to meet specialized aircraft structural or operational requirements.

## Maser Method Amplifies Sound



Direct amplification of sound waves using microwave radio energy has been achieved with this apparatus being assembled by Dr. E. B. Tucker of General Electric Research Laboratory. Amplification of the sound waves, or phonons, is accomplished by "stimulated emission" of energy by atoms as they change from higher to lower energy levels in a ruby crystal. The some mechanism is used in the maser (microwave am plification by stimulated emission of radiation) to am plify electromagnetic radiation.


## Said Isaac Newton:

"Every particle of matter attracts every other particle with a force directly proportional to the product of their masses and inversely proportional to the square of the distances between them."

Until recently, the thrust which propelled rocket vehicles into their coast stage, prior to orbiting, was provided by booster stages. The fuel carried by the satellite stage was used only to inject itself into orbit.

Now, however, a scientist at Lockheed Missiles and Space Division has evolved a Dual Burning Propulsion System which allows higher orbits and heavier payloads. With this system, the satellite vehicle fires immediately after the last booster stage burns out, thus augmenting the begin-coast speed. Later the satellite stage is re-started to provide orbit injection.

An even more recent development by Lockheed is a triple-burning satellite stage. This will permit a precise $\mathbf{2 4}$-hour equatorial orbit, even though the vehicle is launched a considerable distance from the equator.

These principles have made possible the early development of the midas satellite. Moreover, they substantially increase the altitude and payload of the DISCOVERER series. Lockheed, Systems Manager for these programs and for the polaris fbm, is pursuing even more advanced research and development projects. As a result, there are ever-widening opportunities for creative engineers and scientists in their chosen fields.

Why not investigate future possibilities at Lockheed? Write Research and Development Staff, Dept. M-15E, 962 West El Camino Real, Sunnyvale, Calif. U.S. citizenship or existing Department of Defense industrial security clearance required. All qualified applicents will receive consideration for employment without regard to race, creod, color or national origin,

## Lockheed/missiles and space division

Systems Manager for the Navy POLARIS FBM and the Air Force AGENA Satellite in the DISCOVERER and MIDAS Programs


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$\star 100$ Ohms to 200K Ohms Resistance . Ł Meet Full Range of Military Specifications...

## 4 NEW SINGLE-TURNS

Feel the fine construction by turning the shaft . . . action is smooth, continuous . . . a feel of jeweled precision. See the extra strong design in the one-piece aluminum housing and front bearing mount. Note the rear covers fit precisely into machined shoulders to seal out dirt, vapors, corrosive atmospheres according to applicable mil specs.
Color-coded terminals are gold-plated for perfect solderability, corrosion-free shelf life. Element ends and terminals are welded to prevent loosening during application. All models are wirewound and linear. Standard bushing mounts have life-time lubricated sleeve bearings; standard servo mounts have two precision ball bearings. Precious metal contact and collector surfaces minimize noise, contact resistance and thermal effects over a long, trouble-free life. Complete data is yours by return mail.

BORG EQUIPMENT DIVISION<br>Amphenol-Borg Electronles Corporation<br>Janesville, Wisconsin - Phone Pleasant 4-6616

## NEWS

## Space ‘Pointer’ Slated With 6-Sec Accuracy

Servoed System to Aim Spectrometer For Measuring UV Star Radiation

ASPECTROMETER to be rocketed more than 62 miles above the earth will be aimed by a fine-guidance system, being designed for accuracy of $\pm 6 \mathrm{sec}$ of arc over a $\pm 2$-deg field. The spectrometric system is intended to measure ultraviolet starlight in the $1,000-$ to- $3,000-\mathrm{A}$ range to a resolution of 2 A . It is planned for launching early in 1962 by Princeton University scientists working with the support of the National Aeronautics and Space Administration.

Coarse guidance will be provided by inertial gyroscopes, which are expected to stabilize the rocket to within $\pm 1 \mathrm{deg}$ of the desired pointing position. The fine-guidance system, being developed by Perkin-Elmer Corp., Norwalk, Conn., will actuate servo controls to point the spectrometer with the anticipated 6-sec accuracy.

This system will stabilize in two axes and use a rotating-image technique that is said to be relatively simple. Servos will signal two gimbal ring mounts to adjust their axes and position the spectrometer's stabilized diffraction grating. The servo signals will be gen-


Fine-guidance system to aim ultraviolet spectrometer from rocket depends on rotating image formed by optical system to actuate servos that adjust gimbal ring mounts. Spectrometer is to be rocketed above the atmosphere early next year to analyze radiation from bright stars.

ELECTRONIC DESIGN • July 5, 1961


Spectrometer portion of system will fit in 30 -in. long by 14 -in. diam volume. Before fine-guidance system takes over, coarse positioning will be provided by inertial gyroscopes.
erated when a star's light beam is picked up on a rotating, tilted mirror and directed through a reticle. The segmented reticle will modulate the beam passing through it according to the amount and direction of error. The system is designed to scan its portion of the UV spectrum in units of 30 A per sec.

The modulated beam, which is to contain information on the position of the star's image, will be focused on a phototube. The position data will be converted into error signals by an fm discriminator and resolver.

The $100-\mathrm{lb}$ spectrometer package is to be 35 in . long by $14-1 / 4 \mathrm{in}$. diam. Radiation from stars will enter through an opening in the nose section of the rocket and will arrive at the instrument already collimated. After being diffracted, the radiation is to be focused on a photomultiplier detector to generate photon-count signals for telemetering to ground-receiving equipment.

## Closed-Circuit TV System Used To Verify Check Signatures

A closed-circuit TV system used for verification of check signatures has been installed in the First Pennsylvania Banking and Trust Co. of Philadelphia.

The system, developed by John F. McCarthy, Inc., Philadelphia, uses cameras and components furnished by Philco Corp.

The teller phones the bank's Signature Dept., identifies his numbered station, and requests the specific account. The clerk at the other end pulls the card from its alphabetical file, places it face down on one of two cameras, and the reproduction appears on the monitor.


## SAVE SPACE WITH THIN, EXTRA-STRONG ELECTRICAL TAPES OF MYLAR ${ }^{\circ}$

Here's a pressure-sensitive tape that packs great strength into thinner gauges ( 20,000 psi for 1 mil). Tape of Mylar* polyester film saves space because manufacturers can use thinner gauges with no loss in performance... at lower cost per linear foot.

Want more? "Mylar" also provides -flexibility for snug wraps-high dielectric strength ( $4,000 \mathrm{v} / \mathrm{m} \dagger$ ) -dimensional stability at high humidities -moisture and chemical resistance -resistance to temperatures from $-60^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$. And "Mylar" lasts and lasts because there's no plasticizer to dry out with age.

Insulation of "Mylar" gives motors 50 to $100 \%$ longer service-free life. Gives capacitors longer-lasting stability, greater reliability. In a wide variety of electrical applications, the advantages of "Mylar" can improve the performance, lower costs. Evaluate "Mylar" for your product. Write for free booklet (SC) detailing properties.
Du Pont Co., Film Dept., Wilmington 98, Delaware.


General Electric slear LTV silicome componnd for potting and embedding

Transparent, resilient, self-supporting and easy to repair



LTV-s02 is easily appliod, flows freely in-and-LTV-602 is easily opplied, Hows freely in-andcosity in the uncured state. 800 . 1500 centipoise, LTV is ideal for potting and embedding of electronic assemblies. Unlike "gel-like" potting materials. I.TV-602 cures to a flexible solid. Oven rure is overnight, or from 6 to $B$ hours at is to $80^{\circ} \mathrm{C}$.


ITV-602 is cosy to work with and ceas to repair. To repair parts embedded in LTV, merely cut out and remove section of material, renair into opening and cure. Pot life, with catalyst added, is approximately $\%$ hours and may be extended with refrigeration. When desirable, LTV may also be cured at room temperature.


Rosilioncy offors oxcollont shock resistance. Rosilioncy offors oxcollont shock rosistance acribed in MIL-STD-202A test condition B which sperifies five temperature cycles from -65 to $125^{\circ} \mathrm{C}$. Tests indirate that ITV retains protective properties even after 1800 hours aging at $175^{\circ} \mathrm{C}$. Other tests confrm LTV's
resistance to moisture and water immersion.
1.TV-602 is the newest addition to the broad line of G.E silicone potting and encapsulating materials which also include the RTV silicone rublers. For more information, write to General Electric Company, Silicone Products Department, Section L740, Waterford, New York.

## GENERAL (6) ELECTRIC

## NEWS

## Soviet Hopes to View Venus And Mars With Color TV

A Soviet television scientist, Dr. Pavel V. Shmakov, predicts that "in the near future" his country will observe Venus and Mars by color tv.

The prediction was one of several made at the first International Festival of TV Arts and Sciences, held in Montreux, Switzerland. Dr. Shmakov declined to elaborate on his forecast, however.

The Soviet expert was questioned about TV equipment used in recent Russian space shots. He explained that although the moon rockets did not contain true TV apparatus, more recent vehicles, such as the one that carried Maj. Yuri Gagarin, did.

Dr. Leonard Jaffe, chief of the United States space agency's Operation Relay, pre-

Sonic 'Death' of a Light Bulb


When a 25,000 -w beam of sonic power-energy equivalent to a thousand symphony orchestras playing si-multaneously-is directed at a light bulb, this is what happens. Sequence shots show the actual separation of the bulb from the lamp base, the filament still glowing even though exposed to the air, and the final failure of the filament. The experiment, performed at facilities of Bolt, Beranek \& Newsman, acoustical consultants of Cambridge, Mass., was televised for the public by WBZ in Boston. The photos were taken by Jonathan Karas \& Associates of Durham, N. H.
dicted at the festival that a permanent translation TV link would be "bounced" from satellites within four to five years.

Another prediction, sent to the conference by David Sarnoff, president of the Radio Corp. of America, stated: "Ten years from now a billion people will watch the same TV show at the same time in color." Mr. Sarnoff added that simultaneous translation techniques would make the show understandable to all.

He suggested that new satellite television systems should be used by the heads of all nations for face-to-face discussions, and proposed that every TV set should have a special channel reserved for United Nations telecasts.
Dr. Jaffe was one of six recipients of a festival citation "in recognition of outstanding contributions to the advance of television." The others were Dr. Shmakov, of the Leningrad Technical Institute; Sir Noel Ashbridge of Great Britain, Prof. G. A. Boutry of France, Dr. Kenjiro Takayanagi of Japan, and Eric Esping of Sweden.
Thirty-two nations took part in the conference.

## Israel Seeks Electricity In Shallow Salt Waters

A group of Israeli scientists is experimenting with a principle that may make it possible to get electricity from small, shallow bodies of salt water. The principle, based on a natural phenomenon discovered in a lake in Hungary, where the bottom waters were found warmer than the top, can be explained by a difference in density.
In the heavy brine of a "dead sea," the water tends to form two distinct layers: a heavy dense layer underneath and a less dense layer on top. The top layer acts as a transparent cover over the bottom. When the water is shallow and the bottom is black, the lower layer gets hotter and hotter. The heat cannot escape because the nonmixing of the layers prevents convection. Heat thus retained could be transferred to general electricity.
Since arid countries with abundant sunshine usually have some waters too salty for human use, a curse can be turned to an advantage.

This idea, as well as many others, will be discussed at the United Nations Conference on New Sources of Energy, to be held in Rome, Italy, from Aug. 21 to 31.

## QUADRATURE-FREE AC SIGNALS!

## ...now possible with two entirely new AC pots -precision-built by Helipot!

Even though today's potentiometers are developed to a level of performance never before achieved, their use as AC voltage dividers introduces several problems not present under DC conditions. Most important of these are quadrature voltage and phase shift-the extraneous voltage $90 \%$ out of phase with the input signal, which results from capacitance between wire turns and metallic mandrel.
How do you eliminate quadrature? And the many other considerations associated with AC applications what about them? Helipot solves all these problems with two new AC potentiometer series.
Let's talk specifics.
YOU'LL WANT THE ANSWERS
TO THESE 5 QUESTIONS...

1. WHAT IS AN AC POTENTIOMETER?

Simply stated, a pot that's specifically designed for AC-excited circuits. It differs from ordinary wirewound pots in that quadrature effects are eliminated without the addition of elaborate compensating networks. At the same time, it provides lower output impedance, and improves linearity and reliability.
2. HOW DO AC POTS ELIMINATE QUADRATURE ERROR?
Helipot combines a multi-tapped pot with a multi-tapped autotransform

er. The voltage existing at each pot tap point is determined by the reference voltage at the corresponding
autotransformer tap. The pot resistance element is divided into a series of independent low-resistance ele-ments-hence a reduction in quadrature.
The figure shown plots quadrature error against rotation. It illustrates the difference in phase shift between ordinary wire-wound pots and a Helipot AC unit with 12 -segment autotransformer. You'll note that quadrature error is at its maximum near the midpoint between taps and is nearly zero at tap points. The result: negligible quadrature error and phase shift.
3. HOW ARE INPUT AND OUTPUT IMPEDANCE AFFECTED?
Input impedance remains high. Under AC applications, total pot resistance is paralleled by the AC impedance of the autotransformer. Since this impedance is 10 to 100 times greater than that of the pot, the addition of an autotransformer has a negligible effect on the input impedance.
Output impedance is much lower The addition of an autotransformer to the basic pot results in a maximum output impedance occurring midway between each set of adjacent taps. It follows that total output impedance is greatly reduced-any energy required by the load is fed from the nearest auto-transformer tap.

## 4. HOW DOES THE AC POT

IMPROVE LINEARITY?
The overall linearity of AC pots is dependent on the linearity of pot sections between taps - not total pot linearity.
An important feature of autotransformer application is the ability to easily adjust the voltage appearing at each pot tap - without affecting
the voltage ratio at any other tap. It is therefore possible to pull all tap points into the desired linearity band, regardless of basic pot linearity.
Another AC pot feature: It is capable of truly zero electrical "end coil."
5. ARE AC POTS MORE RELIABLE

THAN BASIC POTS?
Yes-much more so. That's because a pot winding or tap lead going open affects only that portion of the pot between taps adjacent to the open. Even the opening of CW or CCW terminals has no effect beyond the adjacent tap point. Or, simply stated - the more taps, the greater the inherent reliability. Models with up to 28 taps are available as special from Helipot.


Helipot offers two AC pot series and 26 standard models with frequency ranges from 20 to $20,000 \mathrm{cps}$. Choose your linear or non-linear version of either the $3^{\prime \prime}$ diameter single turn Series 5800 or the $2^{\prime \prime}$ diameter multiturn Series 7800. They're precisionbuilt by Helipot to meet unusual conformities and perform in most any desired function.
Any more questions? Detailed specs and additional product information are included in a new 32 -page potentiometer catalog. To get a copy, call your nearest Helipot Sales Engineer ing Representative...or write direct :

## Beckman

instruments. inc.
HELIPOT DIVISION
fullertion, Calif.
pots: moroes. Meres

Electron Products

BW and BWE High Voltage Capacitors

## 

## Newest-8mallest High Voltage Capacitorsi

Compact configuration, lighter weight and extremely low noise are festures deserved by design engineers seeking smaller, more reliable high voltage capacitors.

BWE Series epoxy tube capacitors are designed for applications as AC and DC power supply ripple filter capacitors, voltage doubler circuits and blocking capacitora. Basic construction is similar to the Mil-C-14157 Hi-Rel Spec and meets environmental test conditions of Mil-C-25. Rectangular shaped, non-metallic case eliminates need for large stand-off terminals. The BW wrap and fill version is available for similar applications in less stringent environmenta.

Up to $30,000 \mathrm{~V}$ operation with standard capacity from .001 to .2 mfd. Standard capacity tolerance $\pm 20 \%$ (also available to $\pm 1 \%$ ). Competitively priced against other less sophisticatod versions. Technical information and test data available upon request.

Specifications:
Operating Temperature: $\quad-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Insulation Resistance: $\quad 30,000 \mathrm{M} \Omega \mathrm{min}$. (a4 $25^{\circ} \mathrm{C}$
Dissipation Factor: $1.0 \%$ max. © $25^{\circ} \mathrm{C}$
Test Voltage: $200 \%$ of rated voltage

## ELECTRON PRODUCTS

430 North Halatead Street, Pasadena, California
T11 division of Marshall Induatries

## EDITORIAL

## Transistor Reliability Specs Well on Way

In last year's Transistor Data Chart issue our editorial called for reliability figures to be included with other important transistor characteristics contained in data sheets. Military specifications for components, including transistors, had been lax in reliability specifications due to lack of definitions and environmental standards. We cannot report this data this year, but progress is being made.

Since the release of the Darnell Report (Parts Specification Management for Reliability), improvement in component specifications has been in evidence. Perhaps the most significant in terms of semiconductor specifications is the use of LTPD (lot tolerance per cent defective) in newly prepared MIL-S-19500 documents in place of AQL (acceptable quality level) found in early MIL-STD105 specs. AQL is normally considered the quality level for which the producer takes a 5 per cent risk of having a good lot rejected while LTPD is generally defined as the quality level for which the customer takes a 10 per cont risk of accepting a defective lot. Therefore the manufacturer's risk is linked with AQL and LTPD is a measure of the customer's risk. Based on sample size, an AQL of 4 per cent can exist with LTPD figures ranging from 12 to 38 per cent. Thus, MIL-STD-105 clearly defines the manufacturer's obligation but offers rather a vague reliability promise to the customer responsible for producing reliable equipment from his incoming components.

With newer transistor specifications outlining specific LTPD values and environmental conditions, the customer is fully aware of the confidence he can place on his incoming devices. Manufacturers can determine their acceptance number from the charts included in the specs.

Other improvements in reliability specifications soon to be adopted include the listing of failure-rate figure for components placed on the Qualified Products List. In addition, products will remain on the QPL only as long as they meet specification requirements; failure to maintain a given quality level will result in deletion from QPL.

Based on the earnest efforts being applied by government personnel responsible for the preparation of components specifications, meaningful reliability will be contracted and delivered. Reliability figures may appear in next year's Transistor Data Chart if the rate of effort and enthusiasm generated by the Darnell Report is maintained by the military and industry.

Howarl Sirman

## PSI TRANSISTORS FOR EVERY COMPUTER, COMMUNICATION AND POWER NEED!

## NEWEST LOGIC SWITCH!

- Highly advanced version of 2N706
- $\mathrm{V}_{\text {cesar }}=.2 \mathrm{~V}$ Max at $\mathrm{I}_{\mathrm{c}}=10 \mathrm{~mA}, \mathrm{I}_{\mathrm{o}} \quad 1 \mathrm{~mA}$
- Broadest $h_{s \varepsilon}$ vs. $V_{c t}$ linearity ever offered

NEWEST VHF POWER AMPLIFIER!

- Even higher power-frequency
performance than 2N1506
- Five watt power output at $30 \mathrm{mc}, 12 \mathrm{db}$ power gain


NEWEST MEDIUM POWER SWITCH!

- Vesar - 1.0 V Max at $\mathrm{l}=1 \mathrm{Amp} . \mathrm{I}_{0}=100 \mathrm{~mA}$
- 13 watts at 25 C case temperature
- $l_{1} \quad 30 \mathrm{~m} \mu \mathrm{~s}$ typical at $\mathrm{I}_{\mathrm{c}} \quad 1 \mathrm{~A}, I_{\mathrm{s}_{1}}=\mathrm{I}_{\mathrm{h}}-100 \mathrm{~mA}$
$R=11$ ohms $V_{c c}=12 \mathrm{~V}$

NEWEST HIGH VOLTAGE POWER AMPLIFIER!

- 300 mW power output at 100 mc . 10 db power gain
- $\mathrm{V}_{\mathrm{Ci}}=150 \mathrm{~V}$ Min V cio -125 V Min



## SWITCHING TRANSISTORS

NPN TRIPLE DIFFUSED SILICON MESA
Wide Range of Types $\mu \mathrm{A}$ to 10 Amps .2 V to 140 V


DIMENSIONAL DRAWINGS
All dimensions shown in inches



FREQUENCY-POWER OUTPUT RANGE OF PSI COMMUNICATIONS TRANSISTORS

PSI TRIPLE DIFFUSED PROCESS


DIMENSIONAL DRAWINGS All dimensions shown in inches

PSI triple diffusion makes possible these outstanding performance characteristics: Low VCE saturation. small signal beta and broad VHF versatility. The triple diffusion process, above, provid acturing control unmatched by any other process.
OTHER MESA PROCESSES



COMMUNICATION TRANSISTORS NPN TRIPLE DIFFUSED SILICON MESA Wide Range of Types
$m W$ to Watts 10 to $100+$ Source Voltages


HF HIGH POWER TRANSISTORS
NPN TRIPLE DIFFUSED SILICON MESA
Wide Range of Types . . . for many new applications.

| TYPE | $\begin{aligned} & \mathbf{V} \text { Min. } \\ & \text { Min. } \end{aligned}$ | $\begin{aligned} & V_{\text {ce: }} \\ & \text { Min. } \end{aligned}$ | $\begin{aligned} & V_{\text {in }} \\ & \text { Min. } \end{aligned}$ | hot | 10 me | $\begin{aligned} & \text { per } \\ & \text { me } \end{aligned}$ | $\begin{array}{\|c\|} \hline 5 \mathrm{mc} \text { C } \\ \text { AMM } \\ \text { Powort } \\ \text { OUt } \end{array}$ | lass C Power Gawer | Package |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { 2N1899 } \\ & \text { Cormerly } \\ & \text { PT } 901 \end{aligned}$ | 140 | 100 | 5 | 10 min | 3 | 50 min | 125w | 10db | Single End |
| 2N1900 | 140 | 100 | 5 | 10-20 | 3 | 50 min | 125w | 1000 | Single End |
| 2N1801 | 140 | 100 | 5 | 15.40 | 3 | 50 min | 125w | 1000 | Single End |
| 2N1902 | 140 | 100 | 5 | 10 min | 3 | 50 min | 125w | 10db | Double End |
| 2N1903 | 140 | 100 | 5 | 10.20 | 3 | 50 min | 125w | 10db | Double End |
| 2N1909 | 140 | 100 | 5 | 15.40 | 3 | 50 min | 125w | 10db | Double End |
| PT900 | 80 | 50 | 5 | 10 min | 3 | 50 min | 125w | 10db | Single End |
| kilowatt megacycles amperes nanoseconos Now possible with PSI Load Tested Silicon Mesa Power Transistors. In a typical switching apopication the rate o? iurrent lise can be as high as 100 million Amperes per second. Selected Beta ranges now available. able. |  |  |  |  |  |  |  |  |  |
| Avalability Single Ended packages are avaliable in production quantities. Double Ended in Engineering quantities |  |  |  |  |  |  |  |  |  |

VERY HIGH FREQUENCY

| TYPE | TOTAL POWEA AT 25 C CASE Warts | $\begin{aligned} & \mathbf{v} \\ & \text { Min. } \end{aligned}$ | $\mathrm{V} .{ }^{2}$ Min. | V mio | POWER GAIN AT $\mathrm{I}=30 \mathrm{me}$ Tyo. | $\begin{aligned} & \text { POWER GAIN } \\ & \text { AT } \varphi=70 \mathrm{me} \\ & \text { Tyo. } \end{aligned}$ | POWER GAIN AT $\mathrm{f}=100 \mathrm{mc}$ Tyo. | PK |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2M1338 | 28 | 80 | so | 3 | db 0 | $10.500 \mathrm{P}=0.35 \mathrm{~W}$ | $7 \mathrm{db} \mathrm{P}_{7}=0.35 \mathrm{w}$ | 10.5 |
| 2N1342 | 28 | 150 | 125 | 5 |  | $1306 \mathrm{P}_{3}=0 \mathrm{AW}$ | $10 \mathrm{db} P=03 \mathrm{~W}$ | 10.5 |
| 2N1505 | 30 | 50 | 40 | 3 | $10 \mathrm{db} \mathrm{P}_{0}=18 \mathrm{w}$ | $800 \mathrm{P}=12 \mathrm{~W}$ | 600 P $=1 W$ | 10.5 |
| 2N1506 | 30 | 60 | 40 | 4 | $12 \mathrm{db} \mathrm{P}=18 \mathrm{w}$ | $108 \mathrm{~b} P=12 \mathrm{~W}$ | $850 \mathrm{dbP}=1 \mathrm{~W}$ | 10.5 |
| 2N1710 | 130 | 60 | 45 | 3 | $1080 \mathrm{P}, 5 \mathrm{FW}$ | $60 \mathrm{~b} \mathrm{P}_{0}=6 \mathrm{~W}$ | $500 P_{0}=6 \mathrm{~W}$ | 108 |
| 2N1709 | 130 | 75 | 60 | 4 | $12 \mathrm{db} P=5 \mathrm{~W}$ | 8db $P_{0}=1 \mathrm{w}$ | $6010 P_{0}=7 w$ | 10 |

[^3]perating current ima io several amos
OPERATING FREQUENCY UP TO SEVERAL HUNDRED ME (HIGHER WITH VARICAPE DOUBLING CIRCUITS) POWER OUTPUT MILLIWATIS TO NEARLY 10 WATIS
he 2 N1 338. 2N1 342, 2N1505. 2N1506 are avalable in production quantities
the 2N1709 and 2N1710 are avalable in protolyping quantities

## PICO-TRANSISTORS and MICRO-TRANSISTORS

PSI Pico and Micro transistors are ultra miniature triple diffused silicon mesa devices. They are designed for low level amplification and for low power, high speed switching applications. These unique transistors are extremely valuable where weight and size are prime design and operational factors.
The remarkable high reliability standards of PSI Micro-Diodes are the result of simplified construction and advanced surface passivation techniques. These same techniques are employed in the manufacture of PSI Micro Transistors.
The surface passivation process and coating materials provide pro tection from extreme environmental conditions of heat, moisture. thermal shock, mechanical stresses and electrical load.
After manufacture all devices are subjected to environmental testing to assure reliability and device parameters.

- Meet MIL-S-19500B and MIL-STD-202A
- $200 \mathrm{hr} .200^{\circ} \mathrm{C}$ Reliability Assurance
- $-65^{\circ} \mathrm{C}$ to $200^{\circ} \mathrm{C}$ temperature range
- 100 mW power dissipation
- Pico size $1 / 1000$ of TO-5 package
- Micro size $1 / 100$ of TO-5 package
- Companion components to PSI Micro-Diode



## (2ss. Pacific Semiconductors, Inc. <br> A a subsidiary of thompson ramo wooldridge inc

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NIC CENTERS COAST-TO-COAST


Electronic Design's Ninth Annual

## TRENSISTOR DERE CEART

Electronic Design's Ninth Annual Transistor Data Chart contains specifications for 1,714 transistor types-last year only 1,088 types were submitted for publication by semiconductor manufacturers. With close to a 60 per cent increase in the number of available types, the design engineer is now offered a greater selection of devices as well as increased sources of supply-but his search time for a transistor to do a certain job is likewise increased. Thus, Electronic Design's unique listing, specifically tailored for the design engineer, should prove to be a handy time-saver.
Contrary to existing lists which group transistors by manufacturer or in numerical sequence (fine for salesmen, of limited use to engineers), the 1961 Data Chart has transistors organized into six application categories:

Audio-mostly general purpose types, under 1 w , listed in order of increasing forward-current transfer ratio, ( $h_{1 e}$ or $h_{F E}$ ).

High frequency-including types ranging up to and above the vhf range and tabulated in order of increasing alpha-cut-off frequency, $\left(f_{c e}\right)$.

Power devices-transistors rated at 1 w and above are listed in order of increasing collector power dissipation.

Special types-low-noise, high-power/high-frequency and other miscellaneous types are included.

High-level and low-level switching-devices intended for switching are listed in order of increasing alpha-cut-off frequency, $\left(f_{a e}\right)$.

By this system of listing transistors, the design engineer is offered a rapid method of selecting a particular type based on a parameter value. In addition, close substitutes are apparent and multiple sources of supply are listed when applicable. Only U. S. manufactured types are given.
One word of caution is included. Quite a few similar number types, made by several companies, were submitted with different characteristics due to the nonconformity in test methods among manufacturers. The manufacturer whose data are used for each particular type is listed under "Mfg." Other suppliers of the same types are found under "Remarks." Please take note that the company listed under "Mfg." is not necessarily the prime supplier, a cheaper source or the original EIA registrant. The final choice of supplier is obviously up to the design engineer. It is thus advisable to use this listing as a guide to selection and then follow up with a detailed evaluation of specific test methods and data as outlined in each manufacturer's spec sheet.

A cross index is included to identify a type number with its listed category. The JEDEC type numbers are tabulated in numerical order and the category group is indicated.

## Audio

| $\begin{aligned} & \text { Type } \\ & \text { Ne. } \end{aligned}$ | mig. | Type | $\begin{gathered} \text { hfo } \\ 0, \\ \text { hFE } \end{gathered}$ | Moximum Rotinge |  |  |  |  | Chorectoristics |  |  |  | Remarts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \mathbf{w}_{c} \\ & (m w) \end{aligned}$ | $\begin{array}{\|l\|} \hline T_{i} \\ (c) \\ (c) \end{array}$ |  | $v_{c}$ | $\mathrm{ma}$ | $\begin{aligned} & I_{c 0} \\ & \mu \mathrm{a} \end{aligned}$ |  | $\begin{array}{\|c\|} \hline c_{c} \\ \mu \mu 4 \end{array}$ | $\begin{array}{\|l\|} \hline \mathrm{f}_{\mathrm{a}} \mathrm{e} \\ \mathrm{mc} \end{array}$ |  |
| 2 N 160 | RRD | nom.GJ, si | 0.93 | 150 | 175 | - | 40 | 25 | 0.2 | 25 | 7 | 4 |  |
| 215164 | RRD | nom, CJ, si, | 0.93 | ${ }^{150}$ | 175 | - | 40 | ${ }^{2}$ | 0.2 | 25 | 1 | 4 |  |
| ${ }^{213} 319$ | RRD | nm,G),sil | 0.95 | 50 <br> 150 <br> 150 |  |  | 125 | 10 |  | 7 |  |  |  |
| 21614 | RRD | nmo, $\mathrm{Cl}^{\text {j }, \text { si }}$ | 0.56 | 150 | 175 | = | 40 | 25 | 0.2 | ${ }_{25}$ | 7 | 5 |  |
| 21318 | RRD | $\mathrm{nm}, \mathrm{GJ}$ si | 0.9\% | so | 175 | - | 90 | 50 | 10 |  |  | 3 |  |
| 2 N 1038 | RRD | nno,GJ, si | 0.56 | 500 | 175 | - | 90 | 30 | 6 | - | - | 3 |  |
| 2n31) 21109s | RRD |  | 0.98 | 150 500 | 175 | = | 60 | 60 | 10 | 18 | 1 | 3 |  |
| 2 NI | RRD | nom, ${ }^{\text {jos,si }}$ | 0.98 | 150 | 175 | - | 40 | 25 | 0.2 | 25 | 1 | 6 |  |
| 2211634 | Rro | non, GJ, si | 0.99 | 150 | 175 | - | 40 | 25 | 02 | 25 | 7 | 6 |  |
| ${ }_{951}^{580}$ | TI | nop, (J),si | ${ }_{6}^{6}$ | 750 750 | 150 | 6 |  | S0 6 | 6 | - | = | 8 | ${ }_{2}^{2 N 1155}$ |
| $2 \mathrm{Ls63}$ | II | nom, $\mathrm{Gj}, \mathrm{si}$ |  | 750 | 150 | 6 | 120 | 40 | 8 | - | $=$ | 8 | ${ }_{2} 2 \mathrm{HL15} 5$ |
| 2 LH 154 | MA | nen,ou, si | 9 | 750 | 150 | 5 | ${ }_{50}$ | 60 | 5 | - | - | - |  |
| 2 N 1155 | Ma | nmo,0msi | 9 | 750 | 150 | 5 | 80 | 50 | 6 | - | - | - |  |
| 211156 | Ma | nno. OH , si | 4 | 750 | 150 | 5 | 120 | 40 | 8 | \% | - |  |  |
| ${ }_{21332}$ | TI |  | 9 | 150 | 175 |  | 4 | 25 | 2 | ${ }_{20}^{20}$ | - | $!$ | TR, USM |
| 22332A | HA | nmomesisi | 920 | 150 | 175 | 0.66 | 15 |  | 2 |  | 30 |  |  |
| 2313334 | MA | nom, 16 c, si | 920 | 500 | 175 | 2.8 | 45 | - | 0.5 |  | 15 | - |  |
| 221903 | II | nnom, $\mathrm{CJ}, \mathrm{si}$ | 9-20 | 150 | 175 | 1 | 45 | 25 | 2 | 25 |  | 4 | ${ }^{211149}$ |
| ${ }_{2}^{2 N 1169}$ | TR |  | 920 932 | 150 750 | 150 | - | 30 60 | 25 60 | 0.1 |  | 1 | 7 |  |
| 2W142A | TR | nmodidisi | 10.25 | 200 | 200 | - | 45 | 25 | 0.10 | 22 | 7 | 1 | 1008 meliztily as. |
|  |  | non. $\mathrm{C}, \mathrm{si}$ | 10.25 |  |  | - |  |  |  |  |  |  |  |
| $22 \times 71$ | TR | nop, ${ }_{\text {aj,si }}$ | 10.25 | 200 | 200 | - | 15 | 25 | O.CO | ${ }_{22}^{22}$ | 7 | 8 |  |
| $2 \mathrm{~N} / 2$ | TR | non,G1, si | $10-25$ | 200 | 200 | - | 45 | 25 | 0.02 | 22 | 7 | 8 |  |
| 2M10 | 5 | , Aj je |  |  | 75 | 20 | 30 | 1.53 | 5 ma |  |  |  |  |
| $2 \mathrm{~N} 10 / 13$ | Sr | non, $\mathrm{A}, \mathrm{se}$ | 10.5 | Im |  | 20 | 50 | 0.89 | 5 ma | - | - | - |  |
| 2 M45 | ${ }_{\text {G1 }}^{\text {M }}$ |  | 12 | 150 | 100 | 2 | 45 | - | 10 | 22 | 40 | - | -MIL |
| ${ }^{2} 21736$ | MA | non,oinisi | 12.20 | 500 | 220 | 2.5 | 45 | - | 0.21 |  | 25 | $\underline{1}$ | aucio |
| 2 Cl 756 |  | non.om,si | $12-20$ | 500 | 200 | 2.5 | 60 | - | 0.1 |  | - | - |  |
|  | RA |  | 13.5 | $\pi$ | 85 | 1.25 |  | 100 |  |  | - | - | Sub |
| $\xrightarrow{\text { CKGIC }}$ | $\begin{array}{\|l\|l} R A \\ \text { SSO } \end{array}$ | pmp,AJ.ge | $\begin{aligned} & 13.5 \\ & 14.5 \end{aligned}$ | $\begin{gathered} 76 \\ 305 \end{gathered}$ | $\left.\right\|_{160} 85$ | $\left\lvert\, \begin{aligned} & 1.25 \\ & 2.28 \end{aligned}\right.$ | $\left.\right\|_{40} ^{45}$ | $\left.\begin{array}{r} 100 \\ 50 \end{array} \right\rvert\,$ | 10 | 18 | 70 | $\overline{2}$ | ${ }_{\text {Scosem }}^{\text {Solin }}$ |
| ${ }_{2} 2129$ | amp |  | 15 | 125 | 125 | 2.5 | 30 | 125 | - | 18 | $\underline{2}$ | $\underline{-}$ |  |
| 2N33AA |  |  | 15 | 1200 | 200 | ${ }^{2.5}$ | ${ }_{55}$ | 1 | - | - | $=$ | - |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $2 \mathrm{S3} 10 \mathrm{~A}$ | TR |  | 15 | 1000 | 200 | 1 | 25 | 0.1 | 1 | - | - | - | Beta spees at 3 |
| 23314 | TR | nmm, $\mathrm{J}, \mathrm{si}$ | 15 | 1000 | 200 | 1 | 125 | 0.1 | 1 | - | - | - | ITment evels. |
| 2Ms |  |  |  |  |  |  |  |  |  |  |  |  | current bevels. |
| 2 2038 | SSD |  | 15 | 250 | 175 | 1.7 | 35 | 100 | 001 | $=$ | 7 | 2 |  |
| 2W1247 | MA | npm,0i,si | 15 | 30 | 150 | 0.2 | 6 | 5 | 1.5 |  | 12 |  | TR |
| ${ }^{211248}$ | TR | nom. GJ, si | 15 | 300 | 150 |  | 6 | 5 |  |  |  | 1 |  |
| ${ }_{2}^{2 N 14140}$ | $\left\lvert\, \begin{aligned} & M A \\ & R A \end{aligned}\right.$ | mp, Aj, si | 15 | 400 250 | 1200 | 2.28 | $\begin{aligned} & 50 \\ & 20 \end{aligned}$ | 180 | 0.00 | 12 | ${ }_{20}^{25}$ | 1 | astio/red. |
| 2 L 1655 | RA | mp,aj, si | 15 | 250 | 160 | 0.54 | 125 | 50 | . 005 | 18 | 70 |  |  |
| TR3 | IND | mp,AJ, se | 15 | 120 | 85 | 3 | 40 | 150 | 10 | 15 | 15 | 1.6 |  |
| ${ }_{2}^{24 \times 25}$ | $\begin{aligned} & M A \\ & 6.1 \end{aligned}$ | $\mathrm{mp}^{\mathrm{m}, \mathrm{A}, \text { sil }}$ | 16 | 150 | ${ }^{200}$ | ${ }_{2}^{2.5}$ | 50 | = | . 05 | - | 12 | . 8 |  |
| 21118 | Ti | nm, CR,si | 18.40 | 150 | 175 | 2 | 15 | $\bar{z}$ | 2 | ${ }_{20}^{16}$ | $\stackrel{18}{18}$ | 5 | TR Prace mpanam |
| $\begin{aligned} & 2 n 333 \\ & 2 \text { n33 } \end{aligned}$ | $\left.\right\|_{M A} ^{i n}$ | nom,CR,si | $\begin{aligned} & 1840 \\ & 18-36 \end{aligned}$ | $\begin{aligned} & 150 \\ & 500 \end{aligned}$ | 175 | ${ }_{2}^{18}$ | 15 | 25 | 0.5 | 120 | - | 8 | GE,TR,Ma,ra |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2nsia | ${ }_{\text {MA }}^{\text {MA }}$ |  | ${ }_{18,36}^{10.36}$ | 500 500 | $\begin{aligned} & 200 \\ & 200 \\ & 10 \end{aligned}$ | $\begin{aligned} & 2.5 \\ & 2.5 \end{aligned}$ | 45 60 | - | 0.2 |  | - | $\bar{\square}$ |  |
|  | $\left.\right\|_{M A} ^{I I}$ | nop,GR,si | cock | 150 150 | 175 | ${ }_{0}^{1}$ | 15 15 | 25 | 2 | 25 | , | 5 | 2N115 |
| 2N334 | TI | men, GR,si | 18.90 | 150 | 175 | $1{ }^{\text {d }}$ | 45 | 25 | 2 | 20 | - | 10 | GE,TR,M, RA |
|  | ma | non, 16, si | 18.90 |  |  |  |  | - |  | - | - | - |  |
| 2 2nsoun | $\left.\right\|_{\pi} ^{M}$ | nop, DM, ${ }^{\text {asi }}$ | ${ }_{\text {coser }}^{18.90}$ | $\begin{aligned} & 500 \\ & 150 \\ & \hline \end{aligned}$ | 200 | 2.5 | 150 | $\overline{2}$ | 0.1 | $\overline{25}$ | - | 1 |  |
| ${ }^{2} 2 \times 151$ | m | nmomionisi | 18. | 150 | 175 | 0.\% | 4 | ${ }_{25}^{25}$ | 2 | 25 | 7 | 8 | ${ }_{\text {RR }}^{2 M 1}$ |
| ${ }^{2 N 129}$ | SPR | mpo.a) se |  |  |  |  |  | 5 |  |  |  | 30 |  |
| 212923 201051 |  |  | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ |  |  |  |  |  | $.005$ |  |  |  |  |
| 2121670 | GI | mp, DR se | 20 | 120 |  | 2 | 100 |  | ${ }^{3}$ | - |  | , | Hivolt smich |
| $2 \mathrm{~L} / 58 \mathrm{~A}$ |  | npo,06,si | 20.50 |  |  |  |  | ${ }_{2}^{50}$ | 0. 10 | 20 | 7 | 10 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | srance procesed |

## Index of Manufacturers

Abbrev. Company

| AMP | Amperex Elec. tronic Co. | Hicksville, N. Y. |
| :---: | :---: | :---: |
| BE | The Bendix Corp. | Holmdel, N. J. |
| CBS | CBS-Hytron, Semicond. Operations | Lowell, Mass. |
| CL | Clevite Transistor | Waltham, Mass. |
| CT | Crystalonics, Inc. | Cambridge, Mas |
| DE | Delco Radio Div., GM Corp. | Kokomo, Ind. |
| EM | Electromation Co. | Venice, Calif. |
| FA | Fairchild Semicond. Corp. | Mountain View Calif. |
| GE | General Electric Co. | Syracuse, N. Y. |
| GI | General Instru. ment Corp. | Newark. N. J. |
| HO | Hoffman Semi cond. Div. | El Monte, Calif. |
| HU | Hughes Semicond. Div. | Newport Beach, Calif. |
| IND | Industro Transis. tor Corp. | Long Island City. N. Y. |
| KF | Kearfott Semi. cond. Corp. | West Newton, Mass. |
| MH | Minneapolis-Honeywell | Minneapolis, Minn. |
| MO | Motorola Semi. cond. Products Inc. | Phoenix, Ariz. |
| NA | National Semicond. Corp. | Danbury, Conn. |
| PH | Philco Corp. Lansdale Div. | Lansdale. Pa. |
| PSI | Pacific Semicond., Inc. | Cuiver City, Calif. |
| RCA | Radio Corp. of America | Somerville, N. J. |
| RRD | Radio Develop. ment and Re search Corp. | Paterson. N. J. |
| RA | Raytheon Co. Semicond. Div. | Newton, Mass. |
| RH | Rheem Semicond. Corp. | Mountain View, Calif. |
| SE | Secoa Electronic Corp. | Westbury, L. I.. N. Y. |
| STC | Silicon Transistor Corp. | Clare Place, L. I., N. Y. |
| SSD | Sperry Semicond. Div. | South Norwalk, Conn. |
| SPR | Sprague Electric Co. | North Adams, Mass. |
| SY | Sylvania Semicond. Div. | Woburn, Mass. |



Audio（continued）

| $\begin{aligned} & \text { Type } \\ & \text { Mo. } \end{aligned}$ | Mfg． | Type |  | Menimum Retings |  |  |  |  | Cherecterisulies |  |  |  | Romarts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{array}{\|c\|} \hline W_{c} \\ (m w) \\ (m) \\ \hline \end{array}$ | $\begin{aligned} & \mathbf{T}_{\mathrm{j}} \\ & (\mathrm{c}) \end{aligned}$ | mw＇d | $V_{c}$ | $\begin{aligned} & 1 \\ & l^{\prime} c \\ & \text { ma } \end{aligned}$ |  | $\begin{aligned} & \overline{N F} \\ & d b \end{aligned}$ | $\begin{gathered} C_{c} \\ \mu \mu! \end{gathered}$ | $\begin{aligned} & \text { lae } \\ & \mathrm{me} \end{aligned}$ |  |
| 2 M 06 | SY | pmp，AJ，${ }^{\text {a }}$ | 20－00 | 150 | 7 | 3 | 20 | 35 | 14 | － | － | 250 |  |
| 2 N 161 | MA | nmon，DM，si | 20－55 | 500 | 200 | 2.5 | 45 | － | 2 | － | － |  |  |
| $2 \mathrm{NS330}$ | GI | －，Dm， | $2{ }^{2}$ | 100 | 8 | 2 | 15 |  | $3^{2}$ | 14 | 3 | 25 | －matched pap，nan |
| TRT22 | IND | mponjs | 22 | 150 | 2.5 | 3 | 45 | $200$ | 10 | 15 | 20 | 2.5 |  |
| CK22A | RA | pnp，A， $\mathrm{sec}^{\circ}$ | 22.5 | 80 | 85 | － | 20 | 100 | 2 | 6.5 |  | 1.2 | aicromin |
| CK6EA | RA | mpp，AJ，ge | 22.5 | 80 | 85 | － | 29 | 100 | 2 | 7 | － | 0.8 | nicromin |
| CK54 | RA | Pmp，FA， | 23 | 80 | 8 | － | 29 | 100 | 2 | 2 | － | 0.8 | microm |
| 20185A | GE | mp， $\mathrm{N}, \mathrm{ge}$ | 24 | 200 | 85 | 1 | 25 | 200 | 16 | 15 | 40 | 0.8 |  |
| 21109 | GE | pmp，A， $\mathrm{se}^{\text {e }}$ | 24 | 75 | 85 | 2 | 25 | 50 | 16 | 15 | 40 | 0.8 |  |
| $2 N 1476$ | SS | pmp，AJ， 31 | 21 | 250 | 175 | 1.7 | 100 | 100 | 0.5 | － | 1 |  |  |
| 2 Cl 301 | SY | mpp，AJ，ge | 24－15 | 200 | 85 | 3.3 | 25 | 200 | 20 | － | － | 10 |  |
| $2 \mathrm{CH4}$ | GE | mpo，AJ，se | 25 | 240 | 100 | 1 | 45 | 300 | 16 | 6 | 40 | 1 | MIL，GI |
| 21229 | ${ }^{5}$ | $\mathrm{nm}, \mathrm{A}, \mathrm{ge}$ | 25 | 50 | 15 | 1 | 10 | － | 100 |  | － | 600 |  |
| 213300 A | SSO | pmpaj，${ }^{\text {a }}$ | 25 | 5 | 160 | 3 | 30 | 50 | 0.1 | 8 | － | 0.5 |  |
| 2 m 56 | TS |  | 25 | 200 | 100 | 0.3 | 45 | 400 | 15 | － | － | － |  |
| 2 L 564 | IMD | mPD，AJ， | 25 | 150 | ${ }^{6}$ | 2.5 | 30 | 300 | 3 | 12 | 20 | 0.8 | us |
| 24598 | GI | mpp，A］．sa | 25 | 150 | 100 | 0.2 | 20 | 50 | 5 | 116 | 35 | 0.4 | Bilateral |
| 24726 | T1 | omp，DM， 51 | 25 | 1 m | 175 | － | 25 | 50 | 000 | － | － |  |  |
| 21265 | SY | mp，a，${ }^{\text {ce }}$ | 25 | 50 | 85 | 0.9 | 10 | 100 | 100 | － | － | 600 |  |
| 2 L 1641 | MA | Mma，A，${ }^{\text {ai }}$ | 25 | 400 | 200 | 2.28 | 50 | 100 | 0.01 | 12 | 25 | 1 | audio／med．power |
| 2 L 1101 | SY | npo， 1 A，se | 25.50 | 180 | 75 | 3.6 | 20 | 100 | 50 | － | － | 0.01 | RCA |
| $2 \mathrm{Cl1102}$ | SY | npm，AA．ge | 25.50 | 180 | 75 | 3.6 | 40 | 100 | 50 | － | － | 0.01 |  |
| 2034 2035 | SY |  | $25-125$ | 150 | 75 | 3 | 40 | 100 | 50 | － | － | 0.01 | Driver，${ }^{\text {II }}$ |
| 2035 24306 | SY | npn，A」．se nomid． | 25－125 | 150 50 | 75 88 | ${ }_{0}^{3} 8.83$ | 40 | 100 100 | 50 100 | － | － | $\begin{aligned} & 0.01 \\ & 0.6 \end{aligned}$ | Driver， T |
| 2W064 | mo | mpo，Al．se | 26 | 200 | 100 | 2.5 | 45 | 100 | 6 | － | － | 0.1 | IMD，RA，US，GI |
| 2141474 | SSO | pna， $\mathrm{AJ}, \mathrm{si}$ | 25 | 250 | 175 | 1.7 | 60 | 100 | 005 | 1 | 7 | 1 |  |
| 215331 | GI |  | 27 | 100 | 85 | 2 | 15 | － | 3 | 14 | 14 | － | －matched pap，npm |
| $\begin{aligned} & \text { CKESB } \\ & \text { CKESC } \end{aligned}$ | $\begin{aligned} & \text { RA } \\ & \text { RA } \end{aligned}$ | mp，A〕， | $\begin{aligned} & 27 \\ & 27 \end{aligned}$ | $\begin{aligned} & 75 \\ & 75 \end{aligned}$ | ${\underset{\mathbb{E}}{\mathbf{E}}}^{2}$ | $\begin{aligned} & 1.25 \\ & 125 \end{aligned}$ | $\begin{aligned} & 45 \\ & 45 \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | 10 | － | － | － | Sutan |
| 2 N 24 | TI | mp， $\mathrm{A}, \mathrm{si}$ |  |  |  |  |  |  | ． 005 | 18 | 70 | 2.5 | T0－18 |
| 2N118 | 1 | npm，GR，si | 29 | 150 | 175 | 1 | 45 | 60 | 2 | $\overline{20}$ | － | ${ }_{5}^{8}$ |  |
| 24279 | AMP | pro．AJ．ge | 30 | 25 | 75 | 2.5 | 20 | 10 | 110 | 10 | － | 0.15 |  |
| 2M524 | SY | mp，AJ， | 30 | 225 | 100 | 3 | 45 | 500 | 10 |  | － | ， | GE，mo |
| $\begin{aligned} & 225594 \\ & 2 m 939 \end{aligned}$ | GI SSO | npm，AJge | 30 | 150 | ${ }_{175}^{85}$ | 1.67 | 20 | 10 | 2 | 16 | 15 | 2 | Bilateral |
| 2101406 | SSO | pmp，AJ，it | 30 | 250 | ${ }_{85}^{175}$ | 1.7 | 45 | 100 | ． 5 5 | $\bar{\square}$ | 20 | 2 |  |
| 2m1074a | SSO | pnanj，si | 30 | 250 | 175 | 1.7 | 60 | 100 | ．068 | － | ${ }_{7} 7$ | 2 |  |
| 2N1654 | RA | prp，AJ，si | 30 | 250 | 150 | 0.51 | 80 | 50 | ． 005 | 18 | 70 | 2 |  |
| 2 211656 | RA | Dnp，AJ，si | 30 | 250 | 160 | 0.54 | 125 | 50 | S | 11 | 70 | 2 |  |
| Cr25a | RA | onp，A，哭 | 30 | 80 | 85 | － | 20 | 400 | 2 | － | 14 | 4 | micromin RF switch |
| OC201 | AMP | mp，PAÁT， | 30 | 250 | 150 | － | 25 | 50 | 10 | 10 | 1 | 1 | micamin af smich |
| 2 n 331 | ${ }_{5}$ | mp，AJ，ge｜ | $30-70$ | 75 | ${ }^{8} 8$ | 1.2 | 30 | 5 | 1 | 20 | 50 | ． 1 |  |
| 211372 | 5 | mp，A，．ge | 30.50 | 150 | 100 | ， | 25 | 200 | 100 |  | － | － |  |
| 211373 | 5 | pmodJ．em | 30.50 | 150 | 100 | 1 | 45 | 200 | 100 | － | － | － |  |
| 2211432 | 5 | mpp．DD，ge | 30.120 | ${ }^{80}$ | ${ }^{85}$ | 1.3 | 35 | 10 | 15 | － | － | 250 |  |
| 2N1380 | 5 | mpa， $\mathrm{A}, \mathrm{ge}^{\text {c }}$ | 30.300 | 150 | 100 | 2 | 15 | 200 |  |  | － | 250 |  |
| ${ }_{2}^{2 N 1331}$ | Sy |  | $30-300$ | 150 | 100 |  | 25 | 200 | 100 | － | $\bar{T}$ | － |  |
| 21532 | G1 |  |  | 100 | 85 | 2 | 15 | － | 3 | 14 | 14 | － | －arched pmp，npn |
| 21319 | GE | DPQAJ．se | 34 | 225 | \＆ | 4 | 20 | 200 | 16 | － | 25 |  |  |
| 24065 24005 | RCA | pmp，AJ， | 35 35 | 150 150 150 | － | － | 20 | 70 | 14 | $\overline{-}$ | － | 0.25 | SY |
| 21598 | GI | monjs | 35 | 150 | 100 | $\bar{\square}$ | 35 |  | 5 | is | $\overline{35}$ |  |  |
| 21534 | II | npm，10．si | 35 | 1.0 | 175 | $\underline{-}$ | 80 | 50 | 5 | 20 | 35 | 50 | TO-18 TR, MA |
| ${ }_{2} 24738$ | 1 | $n \mathrm{~nm}, \mathrm{DM}, \mathrm{si}$ | 35 | 1. | 175 | － | 125 | 35 | 1 | － | － | － | TR |
| $2 \mathrm{2ms26}$ | ma | mp，N，si | 35 | 150 | 200 | 2.5 | 50 | － | ． 005 | － | 12 | 0.8 |  |
| 2 N 288 | MA | pap，$A$, ，si | 35 | 150 | 200 | 2.5 | 70 | － | ． 005 | － | 12 | 08 |  |
| 221010 | RCA | nmone | 35 | 20 | 55 | － | 10 | 2 | 10 | 5 | $\underline{5}$ |  |  |
| 2N1564 | 1 | nmen，M，si | 35 | 12 | 175 | － | 80 | 50 | 1 | 20 | 5 | 50 | TO－S TR，MA |
| 201572 | TI | non，om，si | 35 | 1200 | 175 | － | 125 | 50 | 1 | － | － | － | TR |
| OC53 | AMP | POp，PADT | ＋35 | 10 | 55 55 | 0.7 | $7$ | 10 | 1.5 | 10 | － | 1.4 |  |
| 21383 | SY | mpo．Aj，ge | 35.110 | 200 | 85 | 3.3 | 30 | 200 | 20 | 10 | － | $\begin{aligned} & 0.01 \\ & 10 \end{aligned}$ | Hearing Aid |
| ${ }^{2121874}$ | GE | anp．as | ${ }^{36}$ | 200 | 85 | 4 | 25 | 200 | 16 | － | 40 | ＋ |  |
| $2 \mathrm{2N119}$ | TI | Mpp，A］，Re |  | 25 150 | ${ }_{15}^{5}$ | 2 | 25 | 50 | 16 | 15 | 40 | 6 |  |
| 21335 | 1 | npm，GR，si | 36－90 | 150 | 175 | 1 | 45 | 25 | ${ }_{2}$ | 20 | － | i1 | TR，USN，MA，RA |
| 2M335A | MA | nmo，KS，si | 36－90 | 500 | 175 | 28 | 45 | 25 | 0.5 | 20 | － | is | GE，${ }^{\text {GE，M，}}$ |
| 2N759 | ma | nma，DM，si | 36－50 | 500 | 200 | 2.5 | 45 | － | 0.2 | － | － | － |  |
| 2M7594 | ma | npo，DM，si | 36.90 | 500 | 200 | 2.5 | 60 | － | 0.1 | － | － | － |  |
| 229505 | II | nma，GR，si | 36－90 | 150 | 175 | 1 | 45 | 25 | 2 | 25 | － | 5 | $2 \mathrm{N1152}$ |
| 221152 | m | ngan，DM， 81 | ${ }_{37}^{36-90}$ | 150 | 175 | 0.06 | 45 | 25 | 2 | － | 7 | 1 |  |
| 2 L 533 | GI |  | 37 | 100 | ES | 2 | 15 | － | 3 | 14 | 14 | － | －matctred pap，nen |


| Type Mo. | Mfs. | Type |  | Masimon Relins |  |  |  |  | Charectoriaties |  |  |  | Remark: |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} w_{c} \\ (m \omega) \end{gathered}$ | $\begin{aligned} & T_{j} \\ & (c) \end{aligned}$ | mem 6 | $v_{c}$ | $\begin{gathered} I_{c} \\ \text { ma } \end{gathered}$ | $\begin{array}{\|l\|} \hline \mathrm{I}_{\mathrm{co}} \\ \mu \mathrm{a} \end{array}$ | $\begin{aligned} & \mathrm{NF} \\ & d b \end{aligned}$ | $\boldsymbol{C}_{\mathrm{c}}^{\mathrm{c}} \mathrm{~m}!$ | $\begin{array}{\|l\|l\|} \text { 'ae } \\ \text { an } \end{array}$ |  |
| 20712 | MA | npm, MS.si | 40 |  | 200 | 1.7 | 60 | 100 | 0.1 | - | 5 | 200 | Switch |
| 211009 | S | DAPAJ80 | 40 | 150 | E5 | 25 | 25 | 20 | 1 | - | - | 0 |  |
| 211176 | BE | mp,A) ${ }^{\text {a }}$ | 40 | 300 | 85 | 6.6 | 15 | 300 | 10 | - | - | - |  |
| 2011764 | 㫙 | mpp,Al.se | 40 | 300 | ${ }^{85}$ | 6.6 | 40 | 300 | 10 | - | - | - |  |
| 2011768 | BE | mpa, N ge | 40 | 300 | 8 | 6.6 | 60 | 300 | 15 | - | - |  |  |
| 211191 | HO | pnp,AJ.se | 40 | 200 | 100 | 2.1 | 40 | 200 | 2 | 10 | - | 1.5 |  |
| 211670 | 61 | POP, DR, ${ }^{\text {ce }}$ | 40 | 120 | 85 | 2 | 60 | - | 3 | - | 3 | - | Trinie Drivem |
| 2 Ck 1730 | 11 | mpnomisi | 40 | 20 | 175 | - | 60 | 50 | 0.5 | - | - | - |  |
| CKı | RA | mpajge | 40 | 80 | 85 | - | 24 | 100 | ? | - | 14 | 6 | Submin RF swich |
| CKAA | RA | mponlse | 40 | 80 | 85 | - | 24 | 100 | 2 | - | 14 | 5 | micromin RF swich |
| Cr26a | RA | mpp,A1se | 40 | 80 | 85 | - | 18 | 400 | 2 |  | 11 | 6 | Micromin RF switch |
| TR.650 | NMO | map, AJ, | 40 | 150 | 8 | 2.5 | 45 | 400 | 1.0 | 10 | 20 | 2 | 2 moso |
| TR 653 | INO | mpp,A1.ge | 40 | 150 | 85 | 2.5 | 30 | 400 | 1.0 | 10 | 20 | 2 |  |
| 21382 | SY | mpajse | 10-7 | 200 | ${ }^{85}$ | 3.3 | 25 | 200 | 20 | - | $\stackrel{7}{7}$ | 10 |  |
| 2MSCOA | TR | npm, DG, 81 | 40-100 | 200 | 200 | - | 45 | 25 | 0.18 | 20 | 1 | 11 | 1006 reliability as. |
|  |  |  |  |  |  |  |  |  |  |  |  |  | sance prece |
| $2 \mathrm{2Na3}$ | GE | mpa.AJ $\mathrm{ge}^{\text {e }}$ | 42 | 240 | 100 | 4 | 45 | 300 | 15 | 6 | 40 | 1.3 |  |
| OC79 | AMP | map, PADT se | 42 | 550 | 75 | - | 25 | 300 | 10 | is | - | 12 |  |
| 2 LHO | RCA | pap, Al.se। | 4 | 150 | - | - | 30 | 50 | 10 | 12 | - | 0.7 |  |
| 2 L 215 | RCA | pnp, aj se | 41 | 150 | - | - | 30 | 50 | 10 | 12 | $=$ | 0.7 |  |
| 2M525 | GE | pno, Alse | 14 | 23 | 100 | 4 | 45 | 500 | 10 | S | \% | 2.5 | MO. S\% |
| 201924 | GE | mpDAJse | 14 | 225 | E5 | - | 10 | 500 | 1 | 7 | - | - |  |
| 21238 | II | pno, AJ se | 45 | 150 | ${ }^{6} 5$ | 0025 | 25 | 200 | 6 | 7.5 | - | 1.5 |  |
| $2 \mathrm{2N21}$ | TI | pnp, A jase | 45 | 180 | 85 | .003 | 25 | 200 | - | 7.5 | - | 1.5 |  |
| 20322 | GE | pmp, AJse | 45 | 140 | 85 | 1 | 16 | 100 | 16 |  | 25 | 2.0 | Driver |
| 2 W 465 | WD | OnP, AJ ge | 45 | 150 | 85 | 2.5 | 45 | 200 | 5 | 15 | 20 | 0.1 | MO, RA, US, GI, SY |
| 2N595 | G1 | npn.AJse | 45 | 150 | 15 | 1.67 | 20 | - | 2 | 16 | 15 | 4 | Bilateral |
| 2N1098 | GE | pmp,AJ, 81 $\mathrm{mmo}, \mathrm{AJ}$ ge | 45 | 150 | 200 | 2.5 | 40 | - | . 005 | - |  |  |  |
| ${ }^{211372}$ | TI | prp,AJ,se | 45 | 250 | 100 | 3.3 | 25 | 200 | 3 | $\overline{7}$ | $\stackrel{1}{2}$ | I's | Oris |
| 2 L 1373 | TI | map,AJse | 45 | 250 | 100 | 3.3 | 45 | 200 | 3 | 1 | - | 1.5 |  |
| 201442 | MA | pmp, AJ, si | 45 | 400 | 200 | 220 | 50 | 100 | 0.01 | 12 | 25 | 1 | audio/med. powel |
| 2011145 201447 | GE | mp,AJ.ge | 45 | 140 | 55 | 1 | 16 | 100 | 16 | $\stackrel{\rightharpoonup}{7}$ | 40 | - | Oriver |
| 2011441 2 N 1451 | ND | pmp, AJ. ${ }^{\text {e }}$ | 45 | 200 | Es | 3.3 | 45 | 400 |  | 6 | 20 | 3 |  |
| (2N1451 | INO | mp, A 1.5 ge | 45 | 200 | 05 | 3.3 | 45 | 400 | 7.5 | 9 | 20 | 1.5 |  |
| 2 L 1471 | 550 | Dnp, $\mathrm{N}, 81$ | 45 | 250 | 175 | 1.7 | 100 | 100 | 0.5 | - | 1 | 1. |  |
| Cress | RA | mpp,FA, re | 45 | 80 | \% | - | 21 | 100 | ? | 22 | - | 1 |  |
| Cruna | RA | Pap, AJ ¢ | 15 | 80 | 85 | - | 24 | 100 | 2 | 22 | - | 1.0 | macromin |
| TRT1 | IMD | mpp,Al.se | 45 | 150 | 2.5 | 3 | 30 | 200 | 10 | 15 | 20 | 3 |  |
|  | MAP | npn.DM, ${ }^{1}$ | 45.150 | 500 | 200 | 2.5 | ${ }^{4} 5$ | - | 0.2 | is | - |  |  |
| 20850 | AMP | pap,AJ, ${ }^{\text {ce }}$ | 41 | 25 | 75 | 2.5 | 20 | 10 | 150 | 10 | - | 0.1 |  |
| TR320 $2 m 050$ | IMO | mpa.AJ.se | 48 | 150 | 85 | 3 | 25 | 100 | 10 | - | 25 | 2.5 | 2 21320 |
| 2wnso | m0 | [mp, 1 ], | 49 | 200 | 100 | 2.1 | 45 | 500 |  |  |  | 1.5 |  |
| $20050 A$ 23053 | M0 | mpl, A . .ge | 49 | 200 | 100 | 2.1 | 45 | 500 | 10 | 15 | 25 | 1.5 | Mega lite |
| 20c53 | mo | papajage | 49 | 200 | 100 | 2.1 | 30 | 250 | 5 | 10 | 20 | 1.5 |  |
| 2N1185 | MO | pap,AJ.se | 49 | 200 | 100 | 2.1 | 60 | 500 | 5 | 5 | - | 1.5 |  |
|  | G1 | mpajse | 50 | 150 | 100 | 2 | 45 | - | 10 | 18 | 40 |  | -MIL, GE |
| $\left\lvert\, \begin{aligned} & 2 N 320 \\ & 2 N 331 \end{aligned}\right.$ | GE | pmp,As, | 50 | 225 | ${ }^{8}$ | 1 | 20 | 200 | 16 | - | 25 | 2.5 |  |
| 24363 | IMO | pmpajse | 50 | 200 | 8 | $\overline{2}$ | 30 | 200 | 16 | 9 | - | 1.16 | IMD, MO, GI |
| 20368 | II | mp,A1se | 50 | 150 | ${ }_{6}$ | 2.5 | 30 | 200 | 10 | - | 33 | - | RA, us |
| 24369 | TI | pap, A) | 50 | 150 | 6 | 2.5 | 30 |  | 7 |  | 33 |  |  |
| 29022 | RA | mp, FAs | 50 | 150 | 15 | - | 20 | 100 | 6 | 6.5 | 3 | 0.8 |  |
| 2 msM | ${ }_{5 S} 5$ | pmp, A 1 , 31 | 50 | 250 | 175 | 1.7 | 1 | 50 | 001 |  | 7 | 0. | T0-18 |
| 2 msp | 530 | MPP,AJ, $\mathrm{sin}^{1}$ | 50 | 250 | 175 | 1.7 | 11 | 50 | 000 | - | 7 | - | T0-16 |
| 21933 | SSO | Pma, AJ, \% | 50 | 250 | 175 | 1.7 | 18 | 50 | .003 | - | 1 | - | T0.18 |
| 2 W904 | SSO | pmo, AJ.si | 50 | 250 | 175 | 1.7 | 18 | 50 | 005 | - | 7 | - | T0.18 |
| 2095 | SSO | pmp,AJ, 31 | 50 | 250 | 175 | 1.7 | 50 | 50 | $?$ | - | 1 | - | T0-11 |
| $2 \mathrm{NO46}$ | SSD | ppp, AJ, 31 | 50 | 250 | 175 | 1.7 | 80 | 50 | ? | - | 1 | - | T0.16 |
| 211273 | II | mp, A A de | 50 | 150 | 18 | . 0005 | 15 | 150 | 3 | 6.5 | - | - |  |
| $2 \mathrm{2W1274}$ | TI |  | 50 | 150 | 85 | . 0025 | 25 | 150 | 3 | 6.5 | - | - |  |
| 201383 | 1 | Pap,A]se | 50 | 200 | 65 | - | 25 | 200 | . 001 | 7.0 | - | 1.5 |  |
| 201917 | 550 | pmp, AJ, 81 | 50 | 250 | 175 | 1.7 | 1 | 50 | 001 | - | 1 | . 5 | TO-S |
| 291910 | SSO | mpo.AJ.si | 50 | 250 | 175 | 1.7 | 11 | 50 | 003 | - | ; | - | TO-S |
| 201919 | SSD | pap.N.si | 50 | 250 | 175 | 1.7 | 18 | 50 | 003 | - | 1 | - | T0-5 |
| 2 Cl 280 | SSO | pmp,AJ, 31 | 50 | 250 | 175 | 1.7 | 18 | 50 | 06 | - | 1 | - | T0. 5 |
| 201991 | 550 |  | 50 | 250 | 175 | 1.7 | 50 | 50 | 2 | - | 1 | - | TO-S |
| 211922 | 550 | mon,A, si | 50 | 250 | 175 | 1.7 | 00 | 50 | ? | - | - | - | T0.5 |
| TR.320 | 110 | omp, AJe | 50 | 150 | 85 | 2.5 | 30 | 200 | 7.5 | - | 20 | 2.5 | 21320 |
| 21211 21028 | 5 |  | 50.100 | 180 | 85 | 3 | 40 | 100 | 50 | - | - | 0.01 | mecred |
| 21228 | S\% | non, AJse | 50.100 | so | 75 | 1 | 40 | 100 | 100 | - | - | 0.01 |  |
| 202114 | S | pmo.AJse | 50.100 | 200 | 65 | 3.3 | 30 | 200 | 16 | - | - | 10 |  |
| 21870 | Sy | pap, Aj, se | 50.100 | 150 | 85 | 2.5 | ${ }^{25}$ | 75 | 12 | - | - | 0.01 |  |
| 203321 | 5 | Dap, AJ ge- | 50.100 | 200 | 05 | 3.3 | 25 | 200 | 16 | $\square$ | - | 10 |  |
| 201059 | 5 | non,Ajse | 50.100 | 180 | 15 | 3.6 | 20 | 100 | 50 | - | - | 0.01 |  |
| 2wnos | ת | PRPAIS | $50-135$ | 150 | 85 | 2.5 | 20 | 70 | 14 | - | - | - |  |

DFTA CHERT
Audio（continued）

| $\begin{aligned} & \text { Type } \\ & \text { Ne. } \end{aligned}$ | Mfs． | Troe | $\mathrm{b}_{6}$ | Mastomen Retimy |  |  |  |  | Cravermiaties |  |  |  | Remante |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} \mathbf{w}_{c} \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{array}{\|l\|} \hline T_{j} \\ \text { (c) } \end{array}$ |  |  | $l_{\mathrm{e}}^{1}$ | $l_{180}^{1}$ |  |  | $\begin{aligned} & \text { 1at } \\ & \text { en } \end{aligned}$ |  |
| 2n109 | תy | onp.A. Aes | $50.150$ | 50 | \％ | 0.9 | ${ }_{25}^{25}$ | $\frac{17}{15}$ | 12 | Z | － |  |  |
| 2 Lm 23 | S | mondee | $\begin{aligned} & 50-150 \\ & 50-150 \end{aligned}$ | 140 | ${ }^{5}$ | 23 | ${ }_{2}^{25}$ | ${ }_{100}$ | 12 | ＝ | － | 10 |  |
| 29134 | Sr | map $A, 1$ | 50－150 | 150 | 100 | 2 | 25 | 200 | 100 | － | － | － | \％ |
| 2 L 133 | Sr |  | 50－150 | 150 | 100 | 2 | 15 | 200 | 100 | － |  |  | $\pi$ |
| 212004 | ${ }_{\text {GE }}^{\text {GE }}$ | mod．je | 54 | 200 | ¢ | ， | 25 | 200 | 16 | 1 | 40 | 12 |  |
| ${ }_{\text {C1223 }}$ | $\left\lvert\, \begin{aligned} & \text { GE } \\ & \text { RA } \end{aligned}\right.$ |  | 54 | 75 | $\left.\right\|_{65} ^{80}$ | ${ }_{125}$ | 25 | 150 | $1{ }_{10}^{18}$ | ${ }_{6}^{15}$ | 40 | 1.2 | Diven |
| CKG5 | RA |  | ${ }_{5}$ | 7 | ${ }_{6} 5$ | 1.25 | 35 | 100 | $\left\lvert\, \begin{aligned} & 10 \\ & 10 \end{aligned}\right.$ | $\stackrel{\square}{6}$ | － | こ | Sismin． |
| CKISC | R | ［m， 11.8 | ${ }_{54}$ | 15 | 85 | 125 | 35 | 100 | 10 |  |  |  | Smmin， |
|  | IMO | mpapajige | \＄5 | 150 | ${ }^{25}$ | 25 | 30 | 300 | ， | 12 | 20 | 1 |  |
| ${ }_{2014}^{2014}$ | $\left.\right\|_{\mathrm{GE}} ^{\mathrm{GE}}$ | mpad se | ${ }_{55}^{55}$ | 140 | ${ }_{8}^{185}$ | 1 | 16 | ${ }_{100}^{100}$ | 16 | － | 8 | － | Diva |
| C1／2］A | RA | pmatas | 55 | 80 | ${ }_{8}$ | － | 15 | ${ }_{100}^{100}$ | ${ }_{2}^{16}$ |  | ${ }_{10}$ | $\overline{11}$ | ${ }_{\text {der }}^{\text {Oiven }}$ |
| Ocs4 | AMP | madse | 5 | 10 | 55 | 0.1 | 3 |  | 0.1 | 10 |  | 0.01 | Howing oud |
| ${ }^{\text {OCS5 }}$ | $a_{p H}$ | AOT | 5 | 10 | S5 | － | 1 | 10 | 15 |  |  | 1.5 |  |
| ${ }_{2} 2155$ | $\mathrm{Cl}_{\mathrm{Cl}}^{\mathrm{PH}}$ | Mnp，A）se | ${ }_{60} 6$ | 250 150 | ${ }^{5}$ | 5.0 | 30 | 150 | $\frac{1}{2}$ | 16 | 115 | 0.4 |  |
| ${ }_{2} 2 \times 63$ | IMD |  | 60 | 150 | 8 | 2.5 | 3 | 200 | 10 |  |  | 0.1 | RA，us |
| 22937 | S50 | mp，AJ， $\mathrm{si}^{\text {a }}$ | 60 | 385 | 160 | 2.5 | 30 | 50 | ． 08 | 18 | 70 | 3 | T0．15 |
| 29940 | SS0 | ORPA」s， | ${ }_{60}$ | 250 | $1 / 15$ | 1.7 | 35 | 100 | 001 | － | 7 | 3 |  |
| ${ }^{2121475}$ | SSD |  |  | 250 10 | 175 | 1.7 | ${ }^{6}$ | 100 | ．00 |  | 1 | 1 |  |
| $2 \mathrm{Ls526}$ | Sr | mpa ${ }^{\text {a me }}$ | 0 | 225 | ${ }^{15}$ | 3.1 | 45 | 500 | $10^{\circ}$ |  | ： | 3 | GE，TS，mo |
| $2 \mathrm{2mises}$ | GE | mpas ${ }^{\text {ce }}$ | 61 | 225 | ${ }^{2} 5$ |  | 40 | 500 | 1 |  |  |  | ce，\％， |
| ${ }_{2}^{2 N 175}$ | ${ }_{\text {R }}^{\text {RCA }}$ | mop．A」se | ${ }_{65}^{65}$ | 50 | － | － | 10 | 2 | 12 | － | － | 0.85 |  |
| 233980 | RCA | （mon，Aj，ge | ${ }_{65}^{65}$ | $\begin{aligned} & 50 \\ & 150 \end{aligned}$ | $\overline{100}$ | 2 | 10 | ${ }_{200}$ | $\left\lvert\, \begin{aligned} & 12 \\ & 12 \end{aligned}\right.$ | 6 | － | ${ }_{1}^{0.15}$ |  |
| $2 \mathrm{mm07}$ | rca | mo，$A 1 . \mathrm{se}$ | 65 | 150 | － | 2 | 20 | 70 | 12 |  |  | $\underline{-}$ | sr |
| 2 L 088 | RCA | mo， 1.1 .8 | 65 | 150 | － | － | 20 | 70 | 14 | － |  | － |  |
| $2 \mathrm{Cm49}$ | RCA | nomAjse | 65 | 100 | － | 13 | 20 | 100 | 14 |  |  | － |  |
| ${ }_{2}^{2141488}{ }_{2}$ | IMO | mo，Al se | ${ }_{6}^{65}$ | ${ }_{200}^{200}$ | ${ }^{85}$ | 3．33 | 45 | 100 | 5 | 6 | 20 | 2 |  |
| Ocs | Amp | mo，$)^{\text {a }}$ | ${ }_{6}$ | 10 | 55 | 0.7 | 3 |  | 120 |  |  |  | Heatıng ald |
| 0 Cl 4 | AMP | DMD，PADT 28 |  | 550 | 5 | ． | 20 | 300 | 10 |  |  | is | － |
| ${ }_{20}^{212323}$ | GE |  | ${ }^{68}$ | 140 | ${ }_{75}^{\mathrm{Es}}$ | 1 | 16 | 100 | 16 | － | 25 | 25 | Oive |
| $2 \times 361$ | 1 mo | mp，A）de | 70 | 150 | 85 | 2.5 | 15 | 200 | $1{ }^{10}$ |  | Z |  |  |
| 2 L 591 | RCA | monofise | 70 | 100 | － | － | 3 | 40 | 1 | － |  | － |  |
| 2 m 517 | RCA | nomaj ge | 10 | 100 |  | － |  | 100 | 14 |  | － |  |  |
| $\xrightarrow{2 N 735}$ | T11 | apn，15，si | 70 | 1.0 | ${ }_{175}^{175}$ | － | 80 | 50 | 1 | 20 | 5 | 50 | Tolid，tr，ma |
| 2 L 1297 | TR | nnom， $\mathrm{OG}, 31$ | 10 | 30 | 150 | 0.24 | ${ }_{6}^{125}$ | － | 0.8 |  |  | 5 |  |
| 211332 211565 | Ti | mondse | 10 | 150 | 15 | 2.5 | 30 | 200 | 25 |  |  |  | Lom mint de ino． |
| 2 T 26s | $\pi$ |  | 70 | 1.2 | 13 |  | 80 | so |  | 20 |  | 50 | TR，M |
| $\xrightarrow{211513}$ | T1 ry | nen， $\mathrm{OH}, \mathrm{Sl}$ | ${ }_{0}^{70} 5$ | 120 | 175 |  | 125 | 50 | 1 | － |  |  | TR |
| ［ | $\xrightarrow{\text { sr }}$ | nponAlse <br> nponje | co－250 | 150 | ${ }_{\infty}^{\mathbb{E}}$ | $\begin{aligned} & 2.3 \\ & 2.5 \end{aligned}$ | $\begin{aligned} & 100 \\ & 20 \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ |  |  | ${ }_{0}^{0.01}$ |  |
| TR．313 | 1 mo | mondse |  | 200 | \％ | ${ }^{3} .33$ |  |  | 7.5 |  |  | 1.1 | $2{ }^{213} 3$ |
| 22241 | GE | modse | B | 100 | 15 | 3 | 8 | 200 | 16 |  | 10 | 13 | 2 |
| 2 M 109 | RCA | onp，Asse | 15 | 150 | － | － | 25 |  | 10 |  |  |  |  |
| ${ }_{2}^{212108}$ | $\left\lvert\, \begin{aligned} & G E \\ & R C A \\ & \hline \end{aligned}\right.$ | Mopalse | $\begin{aligned} & 75 \\ & 75 \end{aligned}$ | $\begin{aligned} & { }_{1} \\ & \text { is0 } \end{aligned}$ | ${ }^{18}$ | 2 | ${ }_{25}^{25}$ | 50 | 16 | 15 | 10 | 1.5 |  |
| 21118 | ${ }^{10} 0$ |  | 15 | 200 | 100 | 2.7 | 40 | 200 | 2 | 10 |  | $\overline{7}$ |  |
| 2 L 1412 | m | mpa 1.81 | 15 | 100 | 200 | 228 | so | 100 | 0.01 | 12 | 25 | 1 | audio mod．pomat |
| ${ }_{2}^{21162}$ | G1 | non，A，Ase | 15 | 120 |  | 0.5 | 10 | － | 5 | $\overline{5}$ | x | － | Tricieat |
| GT01 | $\left\lvert\, \begin{gathered} G 1 \\ G I \end{gathered}\right.$ | mpandse | $\frac{1}{5}$ | 150 150 | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ | $\begin{aligned} & 28 \\ & 25 \end{aligned}$ | － | 5 | ${ }_{6} 6$ | ${ }_{3}$ | － |  |
| ${ }_{\text {cher }}^{\text {TR．23 }}$ | ${ }_{50}{ }^{\text {mo }}$ | mp，Aise | ${ }^{7}$ | 150 | ${ }^{10} 5$ | 2.5 |  | 200 | 7.5 |  | 20 | 2.5 | 2N323 |
| 211316 | SY | monse | 万－150 | 150 | 100 | 2 | 25 | 200 | 100 |  |  |  | 213 |
| 2 L 1231 | ${ }^{51}$ | Menatice | ${ }_{5}^{5} .150$ | 180 | \％ | 3.6 | 25 | 100 | 50 | － | － | 10 |  |
| 2n181 | Ino | \％om， Om | 5 7.250 | 600 |  | － | 30 | － | 0.01 | 三－ | $=$ | \％ |  |
| $2 \mathrm{2ms5}$ | Ino． | mon．om，$\square^{1}$ | ${ }^{5} 5230$ | 600 | 175 | 1 | 40 |  | 0.01 | － | － |  |  |
| 21120 | 11 | nem，GR，31 | 6．333 | 150 | 175 | 1 | 15 | 25 | 2 | 20 | － | 1 | TR |
| $\underset{\substack{212336 \\ 213364}}{2}$ | $\begin{array}{l\|l\|} \hline 1{ }_{m a} \end{array}$ |  | ${ }_{\substack{16.333 \\ 0.333}}^{1}$ | 150 500 | $\begin{aligned} & 175 \\ & 175 \end{aligned}$ | $\frac{1}{2.1}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | ${ }^{25}$ | 2.5 |  | ＝ | 13 | Tr，GE，MA，RA |
| 217560 | m | mon． Oinis | ${ }_{76-333}$ | 500 | 200 | 2.5 | 15 | － | 0.2 | － | － | ： |  |
| 2n7son | ${ }_{T 1}^{m}$ | non． 01.31 | ${ }_{\substack{6 \\ 76.333}}^{\text {c－333 }}$ | 500 | 200 | 2.5 | 50 | $\bar{s}$ | 0.1 | － | － | ； |  |
| 2 zsio |  | nm，GR， 31 | ${ }^{76-333}$ | 150 | 175 | 1 | 45 | 25 | 2 | 20 | － | 1 | 2 Ll 15 |
| ${ }_{2}^{2121153}$ | $\left\lvert\, \begin{aligned} & \text { MA } \\ & I I \end{aligned}\right.$ |  | ${ }_{60} 16.333$ | 150 150 |  | 0．0．6 | ${ }_{2}$ |  | 2 | 5 | 1 | 1 | TR |
| 24321 | GE | mpaise | 80 | $\begin{aligned} & 125 \\ & 20\end{aligned}$ | 矿 | 0．029 | 20 | 1500 | 16 | 6.5 | \％ | 2 |  |
| （2N527 |  | Pop，Afs | 80 | 235 200 | ${ }_{100}^{5}$ | 3.7 | 45 45 | 500 500 | 10 |  | － | 3.3 |  |
|  |  | mpaje |  |  | 100 | 2.1 |  |  | 3 |  |  |  |  |


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$\square$ model NC-1 performs transistor tests up to 50 amps at 750W peak power!


Here's the only direct reading, variable duty cycle test set for non-destructive measure ment of medium and high power transistors The B A Model NC-1 applies suitable pulse then prak detects the resulting current pulse oo they have the same measuring value as ateady state DC same measuring value as agnal powerieconeiderably lowerthan puise steady state DC. lese stress is pue on the tran sistor. This permits power tests to be made at level meny times that of rated dissipation

- Minimizes heat sink requirements.
- Under optimum conditions, requires only 3 loths of 17. of the input power used in con ventional DC current tests
- Permits 750 watis max. power with max current of 50A or max $\omega$ oltage of 250 V

Gird-Atomic also offers the following equip ment for transistor testing
Beta Tester
Transistor Test Set Model KT• 1
Transistor Test Set Model GP-4
General Purpose Trankistor
Test Set
Model KP Series Curve Tracer Model KP Serie with Circuit Analyzer Model MW-1 rite today for nddreional information Write today for addionai information and name of your nearby Baird-Atomic representative.


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- Phileo
- RCA
- Rayeom Mrg.
- Radlo Dev. \& Research Corp


## DATA CHERT

(concluded)

| Charesteristict |  |  |  | Romoth | TypeNo. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 1_{\infty} \\ & \mu \end{aligned}$ | $\begin{aligned} & \text { MF } \\ & \text { © } \end{aligned}$ | $c_{c}$ unl | ${ }_{m}^{6}$ |  |  |
| 3 | 12 | 20 | 2 |  | 22550 |
| 500 | - | - | ${ }^{1.2}$ | ${ }_{\text {Re }}^{\mathrm{Ra}}$ |  |
| 2.5 | 10 | 18 | 5 |  | 2 m 1471 |
| 2 | 10 | - | 2.5 |  | 211188 |
| 6 | - | - |  | Ino. SY | 2 m 67. |
| 2 | 2 | - | 1.5 |  | $\mathrm{C}_{6} 167$ |
| \% | $\underline{2}$ | izs | - 2,5 | macomin |  |
| 10 | 16 | 10 | 0.5 | mo, RA, US | ${ }_{2966} 2116$ |
| 3 | 12 | 20 | 3 |  | 2 msn |
| 3 | 4 | 40 | 3 |  | 211378 |
| ${ }_{5}^{3}$ | 4 | 40 | 3 |  | $2{ }^{211379}$ |
| 5 | 5 | - | 3 |  | 2 2115 |
| ${ }_{3}^{2}$ | 10 | - |  |  |  |
| 135 | 20 | $=$ | 5.7 |  | OCP70 2461 |
|  |  |  |  |  |  |

## of Terms

## Si Silicon

SBT Surface Barrier
$\mathbf{C}_{\text {ion }}=$ Collector-to-emitter capacitance meas. ured across the output terminals with
the input ac open-circuited
$f_{\text {ar }}=$ Frequency at which the magnitude of the forward-current transfer ratio (small-signal) is 0.707 of its low-fre-(small-signal)
f. = Frequency at which common emitter gain is unity.
$\mathbf{h}_{\text {te }}=$ Common emitter-small signal forward current transfer ratio
$\mathbf{h}_{r n}=$ Common emitter-static value of short circuited forward current ratio
$\mathbf{I}_{\mathrm{co}}=$ Collector current when collector junc tion is reverse-biased and emitter is dc open-circuited.

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## to meet critical electronic manufacturing needs


'Baker Analyzed' Reagents

THE d . T. BAKER ELECTRONIC CHEMICALS listed below offer you the highest standards of purity in the industry-proved by the most informative labeling in the industry. Every 'Baker Analyzed' label provides an Actual Lot Analysis that deAnalyzed' label provides an Actual Lot Analysis that de-
fines purity to the decimal; many also provide an Actual fines purity to the decimal; many also provide an Actual
Lot Assay. Your variables are minimized... rejections are Lewer... product performance is improved.
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| Acefic Acid, Glacial | Cobal Carbonato | Mickelous Nirrote |
| :---: | :---: | :---: |
| Acelone | Cobolt Oxide | Nickolous Sulfote |
| Aluminum Nitrate | Cabalt Nitrate | Nitric Acid |
| Alvininum Sulfato | Emer, Anhydrous | Potroloum Eihor |
| Ammonium Carbonat | Hydrochloric Acid | Potasive Dichromat- |
| Ammonium Chloride | Hydrotworic Acid | Potassing Hydroxide |
| Ammonium Hydroxtde | Hydrogen Peroxide, | iso-Propyl Alcohot |
| Ammonivm Plosphote | 30\% and 3\% Solution | Redio Mixhure No. 3 |
| Antimony Triozide | Limivm Carbonato | Silicie Aeld |
| Barivin Acotate | Liminm Chloride | Sodivm Carbonate |
| Barium Carbonat | Limium Nitrate | Sodivm Chloride |
| Barium Fluoride | Limium Sulfate | Sodium Mydrozide |
| Barium Nitrate | Magnesium Carbonate | Sodiwm Phorphate Dibasic |
| Benzene | Magnesium Chloride | Strontium Corbonat- |
| Boric Acid | Mogneshum Oxide | Strontium Nitrate |
| Cadmium Chloride | Manganese Diozide | Sulturic Acid |
| Codminm Nitrote | Manganese Nirrate | Toluene |
| Codmium Sulfote | Manganese Sesquiozida | Trichloroamylene |
| Cokium Carbonate | Manganous Carbonate | Triple Corbenate |
| Colchum Chloride | Mothanol | Xylene |
| Caklum Fivoride | Nickel Carbonate | Zinc Chloride |
| Calchum Nitroto | Nickel Oxide, Black | Zine Nitrote |
| Colcium Phosphat- | Nikkel Oxido, Groen | Zinc Oxide |
| Carbon Tefrachloride | Niskolows Chloride |  |

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## High Frequency

| Type No. | Mfg. | Type | $f$ fre | Maximum Ratings |  |  |  |  | Charactoristics |  |  |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} W_{c} \\ (\mathrm{mw}) \end{gathered}$ | $\mathrm{T}_{\mathrm{i}}$ <br> (c) | mw/ c | $v_{c}$ | $\begin{aligned} & \text { Ic } \\ & \text { ma } \end{aligned}$ | ${ }^{6}$ le | $I_{\infty}$ <br> $\mu \mathrm{a}$ | $\begin{gathered} N F \\ \text { do } \end{gathered}$ | $C_{e}$ $1 \% \frac{1}{}$ |  |
| 2N44AA | G1 | nmm, A, ge | 1 | 150 | 100 | 2 | 40 | - | 25 | 2 | 12 | 14 |  |
| 2N1024 | SSD | pmp,A, Si | $1$ | 150 | 150 | 1.2 | 15 | 100 | 9 | 25 | $\underline{+}$ | 7 | NA |
| 2 N 1025 | SSS | pmp,A, si | $1$ | 150 | 150 | 1.2 | 35 | 100 | 922 | 25 | - | - | NA |
| $2 \mathrm{N94}$ | SY | npn,AJ,ge | 2 | 50 | 75 | 1 | $\pm$ | 50 | 50 | 50 | - | - |  |
| 2N139 | SY | pmp, A, ge | $2($ min. $)$ | 80 | 85 | . 75 | 20 | 15 | 22-110 | 50 | - |  |  |
| ${ }_{2}^{2 N 169 A}$ | SY | npm,AJ, ge | ? | 65 | 75 | . 8 | 25 | 20 | 36-220 | 5 | - | - |  |
| 2N193 | SY | npm, $\mathrm{N}, \mathrm{ge}$ | ? | 50 | 75 | 1 | 18 | 50 | 9 | 50 | - | - |  |
| 2 N 194 | SY | npn, $A 1.8 \mathrm{se}$ | $?$ | 50 | 75 | 1 | 18 | 50 | 10 | 50 | - | - |  |
| 2N194A | SY | npm, $A$, se | 2 | 50 | 75 | 1 | 18 | 50 | 10 | 50 | - | - | Converter |
| 2N211 | SY | $\mathrm{nm}, \mathrm{A}, \mathrm{ge}^{\text {e }}$ | 2 | 50 | 70 | 1.1 | 10 | 50 | 5-15 | 20 | - | - |  |
| $2 \mathrm{2N233}$ | $\mathrm{SY}_{5}$ | nm, A」, ge | 2 | 50 | 75 | 1 | 18 | 50 | 30 | 50 | - | - |  |
| ${ }^{\text {2N4I3A }}$ | SY | pop,A, ${ }^{\text {ce }}$ | 2 | 150 | 85 | 2.5 | 15 | 200 | - | 10 | - | $\overline{7}$ | GI |
| 2N515 | CBS | npm,AJ,ge | 2 | 100 | 8 | 1.67 | 15 | - |  | 5 | - | 12 |  |
| 2N516 | SY | npo, A, $\mathrm{g}^{\text {ene }}$ | 2 | 50 | 75 | 1 | 18 | 10 | -5.50 | 50 | - | - |  |
| ${ }_{2}^{2 N 517}$ | SY | npr, AN.ge | 2 | 50 150 | 75 | $\frac{1}{2}$ | ${ }_{2} 8$ | 10 | 10-60 | 50 |  |  |  |
| 2N1026 | GSO | Pmp, A, ge | 2 | 150 | 100 | 2 | 25 | - | 25 | 1 | 12 | 14 | IND, KF |
| 2N1469 | sso | pnp,AN,si | 2 | 150 | 150 | 1.2 | 35 35 | 100 | ${ }^{184}$ | 25 | - | 7 |  |
| 2N413 | RA | pmo, FA, ${ }^{\text {ge }}$ | 2.5 | 150 | 85 | 1.2 | 18 | 200 | 30 | 2.0 | 7 | 7 | IND, US, KF, GI |
| CK13 | RA | Pnp,FA, ${ }^{\text {ge }}$ | 2.5 | 80 | 85 | - | 18 | 200 | 30 | 20 | 7 | - | Wo. us, MF, G1 |
|  | RA CBS | Pmp,AJ, ge | 2.5 3 | ${ }_{100}^{80}$ | ${ }_{8} 8$ | 167 | 18 | 200 | 30 | 2.0 | 7 | $\overline{7}$ | Micronin |
| 2N438 | CBS | Pnp,AJ, 8 C | 3 | 100 | 88 | 1.67 | 20 | - | - | 5 | - | 12 | RCA, GI, SY |
| 2N438A | CBS | npn,AJ,ge | 3 | 150 | 85 | 2.5 | 30 | - | - | 10 | - | 12 |  |
| 2W445A | GI | npn,A,ge | , | 150 | 100 | 2.5 | 30 | - | 70 | 2 | 12 | 12 | GI, R |
| $\begin{aligned} & 2 \mathrm{~N} 481 \\ & 2 \mathrm{~N} 882 \end{aligned}$ | $\begin{aligned} & \text { RA } \\ & \text { iND } \end{aligned}$ | $\begin{aligned} & \text { pnp,AJ,ge } \\ & p n p, A, \varepsilon_{2} \end{aligned}$ | 3.5 | 200 150 | $\begin{aligned} & 85 \\ & { }_{ष} \end{aligned}$ | 2.5 | 30 11 | 200 | 50 50 | 3 | - | 14 |  |
| TR-482 | IND | Pnp,AJ, ge | 3.5 | 150 | 85 | 2.5 | 11 | 200 | 20 | 3 | - | 12 | RA, US |
| 2N212 | SY | npn, $A \cup, \mathrm{~g}^{\text {e }}$ | , | 50 | 15 | 1 | 18 | 50 | 20 | 50 | - | 12 | Converter |
| 2N385 | CBS | npm, $\mathrm{A}, \mathrm{s}$ ge | 4 | 150 | 100 | 2.0 | 25 | S |  | 35 | - | 4 | SY, GI |
| $\begin{aligned} & 2 \mathrm{Na14A} \\ & 2 N 528 \end{aligned}$ | ${ }^{S Y}$ | pnp, ${ }^{\text {d, ge }}$ | 4 | 150 | 8 | 2.5 | 15 | 20 | $\overline{-}$ | 20 | - | - | KF, GI |
| 2 L 1027 | SSO | $\mathrm{map}_{\mathrm{mp}, A J, s i}^{\text {mi }}$ | 1 | 150 | 150 | 1.2 | 15 | 100 | 25 | 10 | - | 7 | US, MIL only |
| 2 2N1058 | SY | npn,AJ, | 4 | 50 | 75 | 1 | 18 | ${ }^{100}$ | 15 | 25 50 | - | 7 | Converiter |
| 2 m 4 A A | SY | non, N , \% | 5 | 50 | 85 | . 8 | 20 | 50 | 19 | 50 | - | - | Convener |
| $\begin{aligned} & 2 \mathrm{~N} 168 \mathrm{~A} \\ & 2 \mathrm{~N} 292 \end{aligned}$ | $\begin{aligned} & S Y \\ & S Y \end{aligned}$ |  | 5 | $\begin{aligned} & 65 \\ & 65 \end{aligned}$ | 85 | 1.1 | 15 | 20 | 23-135 | 5 | - | - |  |
| ${ }_{2} \mathbf{N} 398$ | RA | npm,Aj, ge | 5 | 65 150 | 85 | . 9 | 15 25 | 20 | $6-14$ 40 | ${ }^{5}$ | - | $\overline{12}$ |  |
| 2M38 | RA | npm AJ, ge | 5 | 100 | 85 | - | 25 | 400 | 25 | 2.0 | - | 12 | T0-5 RF Smich |
| 2N139 | CBS | $\mathrm{nPn}, \mathrm{A}, \mathrm{ge}$ | 5 | 100 | 85 | 1.67 | 30 | +0 |  | 10 | - | 12 | GT, SY |
| $2 \mathrm{2N439A}$ | CBS | $n p n, A, g e$ | 5 | 150 | 85 | 2.5 | 30 | - | - | 10 | - | 12 | RA |
| 2N448 | CBS |  | 5 | 100 | 85 | 167 | 15 | 5 | 9 | 6 | - | 12 |  |
| 2 2N520A | GI | pnd,N, $z^{\text {che }}$ | 5 | 150 150 | 100 | ${ }_{2}$ | 15 25 | 2 | 100 | 5 | 12 | 2.4 |  |
| 2N634 | CBS | nm, $\mathrm{N}, \mathrm{se}$ | 5 | 150 | 85 | 25 | 20 | - | 100 | 5 | 12 | 14 12 | $\operatorname{lind}_{G,} \mathrm{KF}$ |
| 2N1090 | CBS | non, A.ge | 5 | 120 | ${ }_{10}^{85}$ | 2 | 25 | $\cdots$ | 75 | 8 | - | 12 |  |
| 2N1681 | $\left\lvert\, \begin{aligned} & \text { TS } \\ & \text { RA } \end{aligned}\right.$ |  | 5 | 180 | 100 | - | 30 | 200 | 75 | 3 | $=$ | - |  |
| 2N435 | CBA |  | 5.5 | 150 100 | \% 8 | 1.67 | 12 | 20 | 60 | 30 | - | $\overline{2}$ | IMD, US |
| 2 N 377 | CBS | npo, A, ${ }^{\text {a }}$ | 6 | $\begin{aligned} & 100 \\ & 150 \end{aligned}$ | 100 | $\begin{aligned} & 1,67 \\ & 20 \end{aligned}$ | 20 | - | - | 5 5 | - | 12 | ${ }_{C Y} \mathrm{RCA}, \mathrm{GI}, \mathrm{SY}$ |
| 2 L 465 A | GI | npm,AJ, pel | - | 150 | 100 | 2 | 30 | - | 120 | 2 |  | 14 |  |
| OCA5 ST4150 | ${ }_{\text {amp }}^{\text {TR }}$ | Pap, PADT, | 80 6 | 83 | 75 | 15 | 15 | 10 | 100 | 0.5 | $\underline{-}$ | $\square$ |  |
| $\begin{aligned} & 5 T 4150 \\ & \text { 2W139 } \end{aligned}$ | TR | n¢n, DJ, si | ${ }^{6}$ | 50 | 200 | 45 | 60 | - | 25 | 15 | - | 0 |  |
| 2 N 218 | RCA | DMP, A, ${ }^{\text {cee }}$ | 6.8 | 0 | 85 | 1 | 15 | 15 | 48 | 6 | 1 | - | SY |
|  | rca | PnP, N, ge | 6.8 | 8 | 85 | - | 16 | 15 | 4 | 5 | - | - |  |
| 2 N 409 2 M 410 | RCA | mpp,N, ${ }^{\text {cer }}$ | 6. 8.8 | 0 | 85 | - | 13 | 15 | 48 | 10 | - | - | SY |
| 2NSI4 | RA | momp, FA, | 6 | 150 | 8 | - | 13 | 15 | 75 | 10 | - | - |  |
|  |  | mplifne | 7 | 150 | ¢ | - | 15 | 200 | 60 | 2.0 | 6 | - | IND, US, TS, GE, RCA, |
| 2m30 | RA |  | 7 | 100 | 5 | - | 20 | 400 | 45 | 3 | - | 9 | TO'S RF Smitch GI |
| $\begin{aligned} & \text { 2N1090 } \\ & \text { CK14 } \end{aligned}$ | $\left\lvert\, \begin{aligned} & R A \\ & 0 A \end{aligned}\right.$ | npm,A, ${ }_{\text {apm }}$ | 7 | 150 | 8 | - | 18 | 100 | 50 | 3 | , | 9 | TO-S RF Swith |
| ST903 | TR |  | 7 | 80 | 5 | $\bar{\square}$ | 15 | 200 | 0 | 20 | 6 | - |  |
| 22485 | INO | npn, ,AR,si | 75 | 200 | 150 | ${ }^{1.0} 3$ | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | 2 | 16 50 | 0.1 | 2 | 7 |  |
| 2M160A | GE | npm, RG, ${ }^{\text {en }}$ | d | 6 | ${ }_{6}^{6}$ | 11 | 15 | 20 | 40 | 3 5 | - | 12 | RA, US |
| 21169 | CE | npm, RG, 8 e | 8 | ${ }_{0}$ | 85 | 1.1 | 15 | 20 | 12 |  | - |  |  |
| 21283 | GE |  | $!$ | 65 | 85 | 1.1 | 15 | 20 | 8 | 5 | - | 2.4 |  |
|  | CBS | mpran, e | 8 | 15 | 100 | 20 | 25 | $-$ | - | 5 | - | 12 |  |
| 213360 | RA |  | 8 | 150 | 85 | - | 20 | - | $\infty$ | 20 | - | 12 | TS |
|  | ck | MPR,RG, $0^{\text {co }}$ | 8 | 65 | 85 | 11 | 15 | 20 | 72 | 5 | - | 24 |  |
| $2 M 714$ | TR | mpa, Gl, si | 8 | 200 | 200 | - | 30 | 25 | 10.25 | . 02 | 22 | 7 |  |
| 24581 | $\begin{aligned} & \text { TR } \\ & \text { RA } \end{aligned}$ | mpp,G,N,si | 8 | 200 | 200 | - | 45 | 25 | $10-25$ | . 02 | 2 | 7 |  |
| 21085 | GE |  | 8 | 100 | 8 | $\square$ | 15 | 100 | 30 | 3 | - | 12 | T0-5 RF Switch |
| 2N1085 | GE | mpn,RG, | 8 | ${ }_{6}^{6}$ | 85 | $\begin{array}{ll} 2.1 \\ 2.1 \end{array}$ | 9 | $20$ | 40 | 3 | - | 24 |  |
|  |  |  |  |  |  |  |  |  | 4 |  |  |  |  |

High Frequency（continued）

| Troo | $\mu_{1}$ ． | Typo |  |  |  |  |  |  |  |  | Remokt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ${ }_{6 E}^{6 E}$ | monche | ： | ${ }^{65}$ |  | 1.12 | ${ }_{15}{ }_{2}^{2}$ | ${ }_{0}^{20}{ }_{n}^{0}$ | ${ }^{3}=$ | 220 |  |
| ， |  |  |  | ${ }_{10}^{10}$ | 12 | ${ }_{\substack{25 \\ 20}}^{20}$ | （25 | 10 | ${ }^{25}$ | 12 |  |
| 2ma | ${ }^{\text {ces }}$ | min |  | ${ }_{1 \infty}$ | ${ }^{\text {cos }}$ | 1．6］ 15 |  |  |  | 12 |  |
| stom | 1 |  |  |  | 150 |  |  |  | O | 14 |  |
|  | $\xrightarrow[\substack{\text { rich } \\ \text { RCA }}]{ }$ | mmanem | ， | ${ }_{\substack{150 \\ 80}}$ |  | L0 | ${ }_{16}{ }_{16}$ is | ${ }^{315}{ }^{0}$ | ${ }^{0.1}{ }^{0.1}$ | ！ | sr |
|  | ${ }_{\substack{\text { RCCA }}}^{\text {RCA }}$ |  | 10 |  | ${ }^{5}$ |  | ${ }^{15}$ | 15 |  | － |  |
|  | 1150 | mon N, | 10 | 20 | ${ }^{1} 85$ | 2.514 | 20 | 200 | 3 | in |  |
| con | ${ }_{\text {cose }}^{\text {Rea }}$ | mornem | 10 | ${ }_{\substack{150}}^{100}$ | I， | 2，6］${ }^{1}$ | ${ }_{30}{ }^{2} 20$ | 20.8 | ${ }^{20}{ }^{20}$ | 兂 | mo mis |
|  | ${ }_{\text {cose }}^{\text {cas }}$ | nm， | io |  | ${ }^{1050} 2.25$ |  | 10 |  | 2 |  |  |
| 2 mB |  |  | 10 |  |  |  |  | ${ }^{25}$ | 50． $0^{.02}$ |  |  |
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|  | ${ }_{\text {che }}^{\substack{\text { R } \\ \text { R }}}$ |  | 10 10 | 圱䞨 | （1） | 三15 | （120 | 230 ${ }^{235}$ | S00 |  |  |
| ， | ${ }_{\text {cas }}$ | moner | 10 |  | ${ }^{0} 5$ |  | 20 |  |  | 12 | ${ }_{68}^{\text {cx }}$ |
| ， |  |  |  |  |  |  | ${ }_{12} 20$ | 200 |  |  |  |
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|  | IR | momes | il | ${ }_{\substack{150 \\ 200}}$ | ${ }^{\circ} 1150$ | ＝ $\begin{aligned} & 30 \\ & 15 \\ & 15\end{aligned}$ | ${ }_{15}$ | 12080 | 2000．20 |  | Mn，Ti |
| ， |  | mome | 11 |  |  |  | 8 |  | （100 |  |  |
| 22012 |  | nmicas | ＂ |  | ${ }^{150}{ }^{50}$ |  | 15.25 |  | 2000.1 |  |  |
|  | ${ }_{\text {IR }}^{\text {IR }}$ |  | 11 | cois | ${ }^{0} 5150$ |  | ${ }_{30}^{30}$ |  | 1200 |  |  |
|  | $\sqrt{\frac{\mathrm{T}}{\mathrm{TR}} \underset{\mathrm{TR}}{ }}$ | coich | ${ }^{11}$ |  | （lll | － | （10） | 25 | H000．020 |  | ${ }^{2432}$ |
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|  | ${ }_{\substack{80 \\ 100}}^{\text {mid }}$ | mondic |  |  | （100 |  | ${ }^{15} 5$ | 20 ${ }^{1} 000$ | ${ }^{0}$ |  | Tras，Re sment ，kF |
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|  | $\stackrel{\text { TR }}{\text { TR }}$ | nimicts |  |  | 边 |  | （10） | ${ }^{25} 5$ | com |  |  |
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|  | ${ }_{\text {cosp }}^{18}$ | mentige |  |  | ${ }^{50}$ |  | $1{ }^{15} 120$ | 100 | ${ }^{5} / 2{ }^{3}$ |  | Tr－Sef smikn |
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| $\pm$ | ${ }_{\text {Pr }}^{\text {Pr }}$ | ${ }_{\text {mom }}$ |  | ciso | S0 | 1， 1.38 | co | （10） | 5 ${ }^{0}$ |  |  |
| ${ }_{2}^{2120}$ | ${ }_{\text {RH }}^{\text {PR }}$ |  |  | ${ }_{150}{ }^{\circ}$ | $9{ }^{5} 5$ | ${ }^{0.9} 9$ |  |  | ${ }^{10} 5$ | 4 6 | ${ }^{\text {Sime }}$ us，al， |
| $\underset{\substack{\text { and } \\ \text { cing }}}{\text { ckil }}$ | ${ }_{\text {cid }}^{\text {¢ }}$ |  |  |  | ${ }_{50}{ }^{5}$ | ${ }^{2} 20$ | 20 |  | － $0^{3}$ | ！ |  |
|  | ${ }_{\text {PN }}^{\text {P／}}$ |  | ${ }^{2}$ | \％ | ${ }^{\circ}$ |  | 20 | 2010 |  |  |  |
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| com | ${ }_{\text {Pr }}^{\text {Pr }}$ | momer |  | ${ }_{10}^{10}$ | S 120 | 0．0．56 | ¢ 6 | ${ }_{50}^{50} 80$ | 15．${ }^{501}$ |  |  |
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| $\cdots$ | $\xrightarrow[\substack{\text { raca } \\ \text { raca } \\ \text { R }}]{ }$ |  | － | ${ }_{\infty}^{\infty}$ | ${ }^{\circ}$ |  |  | ${ }^{10} 10$ | ${ }_{0} 8$ |  |  |
| ， | ${ }_{\text {cos }}^{\text {man }}$ | Mapere | 3 | ¢ | ${ }^{5}$ | \％ | ${ }_{28}{ }_{16}$ | ® | － | is |  |
|  | $\xrightarrow[\substack{\text { fica } \\ \text { nca }}]{ }$ | come | 3 | $\left.\begin{array}{\|l\|l\|} 1020 \\ 1000 \\ 100 \end{array} \right\rvert\,$ |  | （1．610 <br> 10 | （10 | 边 | （10 | こ |  |

ELECTRONIC DESIGN • July 5， 1961

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## SILICON CONTROLLED SWITCHES ... from SSPD

 to 10 amperes, in the miniature TO-18 package.
## High sensitivity

 $\ldots 20 \mu \mathrm{~A}$ firingClose firing control ... within $\pm .08 \mathrm{~V}$Voltage ratings to 200 VMIL-S-19500 capability

| Type | Maximum Anode Voltage (DC or Peak AC) $\pm$ Volts | Maximum Average Forward Current $75^{\circ} \mathrm{C}$ mA | Maximum Gato Current to "Fire" $\mu \mathrm{A}$ | Gate Voltage to Fire + Volts |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min. | Max. |
| 2N884 | 15 | 200 | 20 | . 44 | . 60 |
| 2N885 | 30 | 200 | 20 | . 44 | . 60 |
| 2N886 | 60 | 200 | 20 | 44 | . 60 |
| 2 N887 | 100 | 200 | 20 | . 44 | . 60 |
| 2N888 | 150 | 200 | 20 | . 44 | . 60 |
| 2N889 | 200 | 200 | 20 | . 44 | . 60 |

## ... Offering efficient switching in the 1-200 mA range and peak pulse current capability

Available for the first time in the miniature TO-18 case, these units offer the same high sensitivity and close characteristics control introduced by SSPI in pioneering PNPN devices for control and logic applications.

The precise firing characteristics of these devices make them ideal for timing and time delay circuits, voltage limit detectors, high gain static switching, logic circuits, and related applications.

With the high surge capability of this series, squib firing systems requiring pulse currents up to 5 amperes can be greatly miniaturized without sacrificing design margin. In addition, the low 1 mA holding current level is particularly useful in many programming, control and logic circuits.

Designed to meet the requirements of MIL-S19500, these units are subjected to extensive temperature storage and cycling, as well as $100 \%$ acceptance testing, as a regular part of the manufacturing procedure.

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## SOLid STATE $\left.\right|_{\text {rom }}$ roducts. Inc.

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| Type Ne. | Mfg. | Type | ${ }^{+}$a* | Maximum Rotiege |  |  |  |  | Charactoristies |  |  |  | Remark ${ }^{\text {a }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{array}{\|c\|} \hline W_{c} \\ (m w) \\ (m w) \end{array}$ | $\begin{aligned} & T_{j} \\ & \text { (c) } \end{aligned}$ | mw/c | $\left\lvert\, \begin{array}{ll} v_{e} \\ v \end{array}\right.$ | $\left\lvert\, \begin{array}{ll} 1 & c \\ \text { ma } \end{array}\right.$ | ${ }^{\text {h }}$ le | $\left\lvert\, \begin{aligned} & 1 \mathrm{co} \\ & \mu \mathrm{a} \end{aligned}\right.$ | $\begin{aligned} & N F \\ & d b \end{aligned}$ | $\left\lvert\, \begin{gathered} C_{c} \\ \mu \mu \end{gathered}\right.$ |  |
| 2 L 1395 | RCA | mpp, Di, ee | 30 | 120 | 85 | - | 40 | 10 | 90 | 16 | - | - |  |
| $2 \mathrm{NLT50}$ | PH | pmp,SBT, 180 | 30 | 15 | 7 | 0.5 | 14 | 5 | 50 | 2 | - | 6 |  |
| 221025 | RCA | Onp, $\mathrm{Dr}, \mathrm{E}^{2}$ | 33 | 80 | 71 | - | 24 | 10 | 50 | 12 |  | - |  |
| 2N1426 | RCA | Pmp, Di,se | 33 | 80 | 71 | - | 24 | 10 | 130 | 12 | - | - |  |
| 2N1524 | RCA | map,Di,ge | 33 | 80 | 71 | 0.4 | 24 | 10 | $\infty$ | 16 | - | 2 |  |
| 20155 | ACA | mp, Di,ge | 33 | 80 | 71 | 0.4 | 24 | 10 | 60 | 16 | - | 2 |  |
| 221526 | RCA | mmp, Di,ge | 33 | 80 | 71 | 0.4 | 24 | 10 | 130 | 16 | - | - |  |
| 2 21527 | RCA | pmp, Dr, ge | 33 | 80 | 71 | 0.4 | 24 | 10 | 130 | 16 | - | - |  |
| 2 N 1108 | TI | Pnp,GD,ge | 35 | 30 | 85 | 0.5 | 16 | 5 | - | 5 | - | 15 |  |
| 2 2 1110 | TI | Mm, $\mathrm{CDO}^{\text {cege }}$ | 35 | 30 | 85 | 0.5 | 16 | 5 | - | 5 | - | 1 |  |
| $2 \mathrm{2N1111}$ | TI | DMP, GD, ge $^{\text {ce }}$ | 35 | 30 | 85 | 0.5 | 20 | 5 | - | 5 | - | 15 |  |
| 2 21111A | TI | Mnp,GD,ge | 35 | 30 | 85 | 0.5 | 20 | 5 | - | 5 | - | 1.5 |  |
| 2 N 1111 B | T | pnp,GD, $\mathrm{se}^{\text {e }}$ | 35 | 30 | 85 | 0.5 | 20 | 5 | - | 5 | - | 15 |  |
| 24003 | GI | pop, $\mathrm{Of}, \mathrm{ge}$ | 40 | 120 | ${ }_{15}^{85}$ | 2 | 30 | $\overline{5}$ | - | 3 | 14 | 3 |  |
| 2N750 | RA | npn, $\mathrm{DJ}, \mathrm{si}$ | 40 | 150 | 1/5 | 0.7 | 50 | 50 | 7 | 10 | - | 5 |  |
| 2 Cl 107 | TI | mpagios | 40 | 330 | 185 | 0.5 | 16 | 5 | 7 | 5 | - | 1.5 |  |
| 2W1369 | RACA | npm, DJ , si | 40 | 300 | 175 | 0.5 | 50 | 50 | 75 | 10 | - | 6 |  |
| 201634 | RCA |  | 40 | 0 | 71 | 0.4 | 31 | 10 | 75 | 16 | - | - |  |
| 2N1638 | RCA | mpodrse | 40 | $\infty$ | 71 | 0.4 | 31 | 10 | $\frac{15}{5}$ | 7 | - | 2 |  |
| 2213746 | RCA | mp, Dr, ge | 40 | $\infty$ | $\pi$ | - | 31 | 20 | . 985 | 16 | - | 3.8 |  |
| 214640 | RCA | Pmp, Dr,ge | 42 | 80 | 85 | 0.75 | 34 | 10 | 60 | 5 | $-$ | - |  |
| $2 \mathrm{MGH1}$ | RCA | mp, Dise | 42 | 0 | 85 | 0.75 | 34 | 10 | 00 | 7 | - | - |  |
| $2 \mathrm{NGA2}$ | RCA | mp, Dr, | 42 | 80 | 85 | 0.75 | 31 | 10 | $\infty$ | 7 | - | - |  |
| 2Nな | TR | npn, $\mathrm{DJ}, \mathrm{si}$ | 44 | 300 | 1/5 | - | 60 | 50 | 20-00 | 1 | - | 8 |  |
| 2 N 75 | TR | npm, $D J$, si | 41 | 300 | 175 | - | 100 | 50 | 20-60 | 1 | - | 8 |  |
| $24 \times 39$ | TR | npm, DJ , si | 4 | 300 | 175 | - | 45 | 25 | 20-45 | 4.1 | 15 | - | TMTE3 ( 150 mm ) |
| 2 NSHO | TR | non, DJ, si | 4 | 300 | 175 | - | 45 | 25 | $0^{60} 90$ | 0.1 | 15 | 8 | TMT ${ }^{\text {a }}$ ( 150 mm ) |
| TMT812 | TR | mpon, DJ,s | 4 | 150 | 15 | - | 45 | 25 | 20 | 0.1 | - | 6 | - |
| 2 W1196 | HU | pnp,W0,si | 45 | 385 | 200 | 2 | 70 | 25 | - | , | - | 4 |  |
| 201631 | RCA | mp, $\mathrm{Dr}, 50$ | 45 | 80 | 71 | 0.4 | 34 | 10 | 80 | 16 | - | 2 |  |
| 27168 | RCA | MPD, Di, m | 45 | 80 | 71 | 0.4 | 34 | 10 | 80 | 16 | - | 2 |  |
| $2 N 1635$ | RCA |  | 45 | $\infty$ | 71 | 0.4 | 34 | 10 | 75 | 16 | - | 2 |  |
| 23163 | RCA | mpa, Dr, ${ }^{\text {a }}$ | 45 | 0 | 71 | 0.4 | 34 | 10 | 7 | 16 | - | - |  |
| $2{ }^{2} 1681$ | RCA | Pmp, Dis | 45 | 80 | 71 | 0.4 | 34 | 10 | 80 | 5 | - | - |  |
| 201169 | RCA | pmp, Orat | 45 | 0 |  |  |  |  |  |  | - |  |  |
| 21048 21364 | TI | Mmp, ciose | 50 | 30 80 | $\begin{aligned} & 75 \\ & 55 \\ & 55 \end{aligned}$ | $0.6$ | ${ }_{2} 2$ | 5 5 | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | 0.7 | - | $L_{3}$ |  |
| 27315 | PH | pmp,si,ge | 50 | 20 | 5 | 1.33 | 5 | 5 5 | $\stackrel{22}{38}$ | 0.7 | - | 3 3 | SPR |
| 20693 | PH | Pmp, Ma, ${ }^{\text {a }}$ | 50 | 2 | 100 | 0.63 | 6 | 50 | 155 | 5 | - | 2 | SPR,GI |
| 24E04 | G1 | mpp, Dr me | 50 | 120 | ${ }^{85}$ | 2 | 30 | - | - | 4 | 14 | 3 |  |
| $2 \times 189$ | PSI | mpn, DMaisi | 50 | 125 w | 150 | 1000 | 140 | 10a | 10 | Oma |  | 6 | hit Ieg., hi pur |
| 3306 | GE | npm, MB, $\mathrm{C}_{\text {ce }}$ | 50 | 30 | 86 | 0.5 | ${ }^{5}$ | 20 | 2.2 | 3 | - | $?$ | tetrode |
| PTs00 | PSI | non, $\mathrm{OM}, \mathrm{si}$ | 50 | 125 m | 150 | 1000 | ${ }^{80}$ | 102 | $3$ | homa | - | 1 | hi hequ hi pow. |
| PTSOI | PSI | npo,mbsis | 50 | 125w | 150 | 1000 | 140 | 10 a | 10 | $30$ | - |  | Mi frequancy. high powes |
| 201197 | nu | pap,mesi | 55 | 385 | 200 | 2 | $\pi$ | - | - | - | - | 4 |  |
| 2 N 128 | PH | Dmp,SB, | 60 | 25 | 85 | 0.1 | 10 | 5 | 40 | 0.6 | 10 | 2.5 | SPR |
| $2 \mathrm{N749}$ | RA | nom, $\mathrm{DO}, \mathrm{s}$ | 60 | 150 | 175 | 0.75 | 45 | 50 | 10 | 10 | - | 6 |  |
| 271388 | RA | npm, $\mathrm{D}, \mathrm{J}$ si | $\infty$ | 300 | 175 | 0.5 | 45 | 50 | 10 | 10 | - | 6 |  |
| 2N811 | TR | npm, $\mathrm{O}, \mathrm{si}$ | 6 | 300 | 175 | - | 45 | 25 | cobs30 | 0.1 | 15 | 8 | TMTM (150 mim) |
| กTル | TR | nmpodsi | ${ }_{6}^{6}$ | 150 | 173 | $\overline{7}$ | 45 | 25 | 40 | 0.1 | - | 6 |  |
| 2N1517a | AMP | Mmp,PADT, |  | 180 | - | 1.7 | 20 | 10 | 100 | - | - | - | *T, RF-IF |
| PADTzo | AMP | m, PADT, | $7^{\circ}$ | 8 | - | 1.7 | 20 | 10 | 150 | - | - | - | :it re |
| PADT21 | amp | pmo,PADT, 8 | $10^{\circ}$ | 83 | - | 1.7 | 20 | 10 | 150 | - | - | - | IT, Convener |
| PADTE | AMP | pmopadis | $70^{\circ}$ | ${ }^{83}$ | - | 1.7 | 20 | 20 | 150 | - | - | - | of T, IF $=$ mop |
| PADT23 | AMP | pro, PADT, | 70 $0^{\circ}$ | 100 | - | 1.7 | 35 | 10 | 150 | - | - | - | Ot, RF amp |
| PADT24 | AMP | Pmp, PADT, | $0^{\circ} 0^{\circ}$ | 100 | - | 1.7 | 35 | 10 | 150 | - | - | - | of, IF |
| PAOT\% | AMP | map, PADT ${ }^{\text {ma }}$ |  | - | - | =- | - | - | - | - | - | - | -15, IF amp |
| PADT27 | amp | map, PADT | $70^{\circ}$ | 100 | - |  |  |  | 150 | - |  | - | - T , ose |
| PADT31 | AMP | Pmp, PADT, | \% $0^{\circ}$ | 100 | - | 1.7 | 35 | 10 | - | - | - | - |  |
| 20336 | PH | pmp, SR, ${ }^{\text {m }}$ | 75 | 20 | 5 | 1.3 | 5 | 5 | 35 | 0.7 | - | 3 | SPR |
| 2N6\% | FA | nm, DP, si | $\infty$ | 2\% | $1 \%$ | 13.3 | 40 | 5 | 40 | 0.1 | - | 18 | RM, PSI, HO, TR, TI, IMO, SY, SSD, MA |
|  | FA | npa, $\mathrm{DP}_{1}$, si | 0 | 21 | 15 | 133 | 00 | - | 30 | 0.1 | - | 12 | RH, IMD, TR, MA |
|  | FA | $n \mathrm{~nm}, \mathrm{DP}, \mathrm{sin}$ | 0 | 20 | 15 | 13.3 | 80 | - | 6 | . 01 | - | 12 | RH\% M M M, Ma |
| 2105 | FA | $n \mathrm{nma,DP}$ si | 0 | 10 | 15 | 6.7 | 28 | - | $\frac{12}{38}$ | . 005 | - | 5 |  |
| 20127 | FA | nmp, DP, si | 0 | 20 | 175 | 133 | 20 | - | 35 | 0.1 |  | 30 | QH. TR |
| 2 man | TR | nen, DJ, $\mathrm{s}^{\text {i }}$ | 6 | 300 | 1\% |  | $\infty$ | 50 | 40-129 | . | - | 8 | -10. |
| $2{ }^{2105}$ | TR | ¢90, D J, \% | E | 300 | 175 | - |  | 50 |  | 1 | - |  |  |
| 3 M 37 | GE | men, 318 | 90 | 30 | 5 | 0.5 | 5 | 20 | 11 | 3 | - | 1.5 | tesom |
| $2{ }^{2098}$ | RCA | mom, Dip | 10 | 0 | 5 5 | - | 30 | 10 | 0 | 15 | - | - |  |
| 3 mm | FA | $n \mathrm{~nm}, \mathrm{DP}$ 2 ${ }^{\text {a }}$ | 100 | 210 | 175 | 113 | 40 | - | 5 | 01 | - | 18 | RM, PSI, TDO, TR, SSD, |

DATE CHERT
High Frequency (continued)

| Type No. | Mig. | Type | a | Meximum Reolinge |  |  |  |  | Charecteristics |  |  |  | Remerks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} w_{c} \\ (m w) \end{gathered}$ | $\begin{aligned} & T_{j} \\ & (c) \end{aligned}$ | mw/d | $\left\|\begin{array}{c} v_{c} \\ v \end{array}\right\|$ | $\begin{aligned} & 1 \mathrm{c} \\ & \mathrm{ma} \end{aligned}$ | ${ }^{\text {h }}$ te | $\begin{array}{\|l\|} \hline 1 \mathrm{co} \\ \mu \mathrm{a} \end{array}$ | $\begin{aligned} & \text { NF } \\ & d D \end{aligned}$ | $\begin{gathered} C_{c}^{c} \\ \mu \mu \mathrm{f} \end{gathered}$ |  |
| 2 N 1180 | RCA | $\mathrm{mpl}, \mathrm{D}, \mathrm{ge}$ | 100 | 80 | 71 | - | 30 | 10 | 80 | 12 | - | - |  |
| 221225 | RCA | pmo, $\mathrm{Drageg}^{\text {a }}$ | 100 | 120 | 85 |  | 80 | 10 | 8 | 12 | - | - |  |
| $2 \mathrm{NL253}$ | FA | npm, DP, si | 100 | 2 w | 175 | 13.3 | 20 | - | 45 | 0.1 | - | 30 | RH |
| 2 21396 | RCA | pnp, Dr, ge | 100 | 120 | 85 | - | 40 | 10 | 90 | 16 | - | $\square$ |  |
| 2 N 1420 | FA | npn,DP,si | 100 | 2w | 175 | 13.3 | 30 | - | 130 | 0.1 | - | 20 | RH, NA |
| 2 21613 | FA | non, DP, St | 100 | 3w | 200 | 17.2 | 50 | - | 80 | . 0004 | - | 18 | RH |
| 212178 | PH | Dnp,MD.ge | 100 | 60 | 100 | . 8 | 25 | - | 45 | 1.5 |  | 1.3 |  |
| 2N1778A | PH | pnp, MO.ge | 100 | 60 | 100 | . 8 | 25 | 50 | 70 | 1.5 | - | 1.3 |  |
| 2N1749 | PH | pmp,MD, ge | 100 | 75 | 100 | $i$ | 40 | 10 | 45 | 1.5 | - | 1.3 |  |
| 3N34 | TI | non,GD,si | 100 | 125 | 150 | 1 | 30 | 20 | 1 | 0.4 | 20 | . | terrode |
| 0 Cl 17 | AMP | pro, DJ.ge | 100 | 60 | 15 | 2 | 20 | 5 | - | 2 | - | - |  |
| $2 \times 152$ | PH | pnp,MD, | 100 | 60 | 100 | . 8 | 12 | 50 | 250 | 0.8 | - | 1 |  |
| 2 M97 | RH | npn, MS, si | 120 | 41 | 173 | 26.5 | 60 | 500 | 25 | 0.1 | - | 20 | MA, GE |
| 2 2N998 | RH | non,N0,si | 120 | am | 175 | 26.5 | 100 | 500 | 25 | 0.1 | - | 20 | MA, GE |
| 2N656 | RH | $\mathrm{nma}, \mathrm{MS}$, $\mathrm{si}_{1}$ | 120 | ${ }^{4}$ | 175 | 26.5 | ${ }_{0}$ | 500 | 60 | 0.1 | - | 20 | M. GE |
| 2 N 657 | RH | npn,MS, si | 120 | 4 | 175 | 26.5 | 100 | 500 | 60 | 0.1 | - | 20 | NA, GE |
| 211023 | RCA | pap, Dr,ge | 120 | 120 | 85 | - | 40 | 10 | 60 | 12 | - | $\underline{-}$ | W, ${ }^{\text {ce }}$ |
| 210066 | RCA | mpo, Or ,ge | 120 | 120 | 8 | - | 40 | 10 | 00 | 12 | - | - |  |
| 2 N 1397 | RCA | pmp,or,Ge | 120 | 120 | 85 | - | 40 | 10 | 90 | 16 | - | - |  |
| 2N1409 | RH | npm, $16, \mathrm{si}$ | 120 | 2.8w | 150 | 22.5 | 30 | 500 | 30 | 0.1 | - | 20 | PS |
| 221410 | RH | n@n,MS,S1 | 120 | 2.8w | 150 | 22.5 | 30 | 500 | 50 | 0.1 | - | 20 | PSI |
| 211420 | RH | non, DD, Si | 120 | 2 m | 175 | 13.2 | 0 | 500 | 200 | . 003 | - | 20 | PSI, TR, GI |
| 2 L 1507 | RH | n¢0,00,s | 120 | 2w | 175 | 13.2 | 60 | 500 | 200 | . 003 | - | 20 |  |
| PT600 | PSI | nom, $\mathrm{OM}, \mathrm{si}$ | 120 | 13m | 175 | 86.7 | 80 | - | 12 | 1 |  | 40 | hit frea, hi pwo. |
| PT601 | PSI | npm,DM,si | 120 | 13w | 175 | 66.7 | 60 | - | 14 | 1 | - | 40 | hitrea. hi pwis |
| RT5001 | RH | npo, M5, st | 120 | $3 \times$ | 175 | 20 | $\infty$ | 1000 | 0 | 0.1 | - | 30 |  |
| RT5002 | RH | non,ME,si | 120 | 3m | 175 | 20 | 60 | 1000 | 60 | 0.1 | - | 30 |  |
| RTS003 | RH | n¢0, MS, 51 | 120 | 3 m | 175 | 20 | 100 | 1000 | 40 | 0.1 | - | 30 |  |
| RTS000 | RH | npm, MS, St | 120 | 3 m | 175 | 20 | 100 | 1000 | 60 | 0.1 | - | 30 |  |
| 2N715 | TI | nom,10, si | 125 | 1.2 w | 175 | 8 | 50 | - | 1 | . 001 | - | 3 | ${ }^{n}$ FEE $10-50, \mathrm{Ma}$ |
| 20716 | TI | npm, MS, $\mathrm{sil}_{1}$ | 125 | 1.2 m | 175 | 75 | 70 | 50 | 1 | . 001 | - | 3 | nFE 10-50, MA |
| 2N1785 | PH | DROMD, ${ }^{\text {r }}$ | 125 | 45 | 85 | . 75 | 10 | 50 | - | $?$ | - | 1.5 |  |
| 211785 | PH | pap.MD.ge | 125 | 45 | 85 | . 75 | 10 | 50 | - | 2 | - | 17 |  |
| 2N1787 218184 | PH | map. 10.0 ge | 125 | 45 | 4 | . 75 | 15 | 50 |  | 1.5 | - | 1.5 |  |
| 2N1854 | PH | Dnp.Mo.ge | 125 | 60 | 100 | . 8 | 20 | 50 | 60 | 1.5 | - | 1.6 |  |
| 2 N 1177 | RCA | mp, DT, ge | 140 | 80 | $n$ | - | 30 | 10 | 100 | 12 | - | - |  |
| ${ }^{211178}$ | RCA | mop, Dise | 140 | 80 | 71 | - | 30 | 10 | 40 | 12 | - | - |  |
| 211179 | RCA | mod, Di,ge | 140 | 80 | 71 | - | 30 | 10 | 80 | 12 |  |  |  |
| $2 N 728$ | TR | npm, O , 51 | 150 | 300 | 175 | - | 15 | 25 | 20 | 25 | - | 8 |  |
| 21472 | TR | nmo, DJ, si | 150 | 300 | 175 | - | 30 | 25 | 20 | 25 | - | 8 |  |
| $\begin{aligned} & 2 N 1505 \\ & 2 N 127 \\ & 2 N \end{aligned}$ | PSI PH | non, 18.51 | 150 150 | $3{ }^{3}$ | 175 | 0.2 | 50 | 50 | 1 | - | - | 1.5 | high frea, high momer |
| 2 W 1727 | PH |  | 150 | 60 | 100 | 0.8 0.8 | 20 | 50 | - | 15 | - | 1.5 |  |
| 211788 | $P H$ | pop, 10.8 | 150 | 60 | 100 | 0.8 | 20 | 50 | - | 1.5 | - | 1.5 |  |
| 2 N 1788 | PH | pmp,M0,se | 150 | 60 | 100 | 0.8 | 35 | 50 | - | 1.5 | - | 1.5 |  |
| 2 1 1780 | PH | pno.mD,ge | 150 | 60 | 100 | 0.8 | 3 | 50 | - | 1.5 | - | 1.5 |  |
| 211790 | PM | pnp,MD, ${ }^{\text {che }}$ | 150 | 00 | 100 | 0.8 | 35 | 50 | - | 1.5 | - | 1.5 |  |
| 3135 | TI | npa,GD,si | 150 | 125 | 150 | 1 | 30 | 2 | 1 | 0.4 | 14 | - | Tetiode |
| 211335 | PSI | non, MS, si | 170 | 2.8 m | 150 | 24 | 120 | 75 | 13 | 8 | $\underline{-}$ | - | High freq, lugh power |
| 2N1336 | PSI | npo, WS, si | 170 | 2.8m | 150 | 24 | 120 | 15 | 13 | , | - | 4 | High freq, min power |
| $\left\lvert\, \begin{aligned} & 2 \text { 2N1337 } \\ & \text { PADT30 } \end{aligned}\right.$ | $\begin{aligned} & \text { PSI } \\ & \text { AMP } \end{aligned}$ | npm,10,sil | $\begin{aligned} & 170 \\ & 2^{200} \end{aligned}$ | $\underset{83}{2.8 \mathrm{~m}}$ | 150 | $\begin{aligned} & 24 \\ & 1.7 \end{aligned}$ | $\begin{gathered} 120 \\ 25 \end{gathered}$ | 7 10 | 13 | 8 | - | 1 | Hugh treq, high power |
| 2W1506 | PSI | npn,mS,si | 210 | ${ }^{3} \mathrm{~m}$ | 175 | 1.7 | 60 | 10 | - | - | - | 8 | High frequency, hish |
| 2W1339 | PSI | npn,MS, sı | 220 | 2.8 m | 150 | 24 | 120 | 75 | - | 8 | - | 4 | Afiphlireo., hoth powet |
| PADT 28 2N1746 | AMP | pnp,PADT.88 | $82220{ }^{\circ}$ | 100 | - | 1.7 | 35 | 10 | 120 | - | - | - | ${ }^{\text {- }} \mathrm{it}$, rf amp |
| 2N1746 | PH | Dnp.MD ${ }^{\text {de }}$ | 235 | 60 | 100 | . 8 | 20 | 50 | - | 2 | - | 3 |  |
| 221709 | PSI PSI | npm, DM, si | 240 240 | ${ }_{13}^{13 m}$ | 175 | 66.7 | 75 | 1.20 | - |  | - | 40 | Mi freq., hi pwt, |
| 2N588 | PH | npn,mome | 250 | 30 | 15 | 0.75 | 15 | 1.28 50 | - | $\begin{aligned} & 50 \\ & \text { L. } 8 \end{aligned}$ | 3.8 | 4 | Hi freq, in pwt. SPR,G |
|  | mos | Dnp, WS, ge | 250 | 300 | 100 | 1 | 15 | 50 | 40 |  | - | - |  |
| 221340 | PSI | nppomes, ${ }^{\text {a }}$ | 250 | 28m | 2.80w | 24 | 120 | 75 | $\square$ | 8 | - | - | High freq.on high power |
| 201491 | RCA | npm,10,s | 250 | 3 m | 175 | 20 |  | 50 | 50 | 10 | - |  | Wiskrea, his power |
| 201837 2018374 | PSI PSI |  | 250 | $2 w$ | 175 | 13.3 | 0 | 5 | 9 | 001 |  | 11 |  |
| 2N1837A | PSI | npm, DM, ${ }^{\text {a }}$ | 250 | 2.8 w | 17 | 18.6 | 80 | - | , | . 01 | - | 11 | HI freq., ho power |
| 2N1838 2M1639 |  | npm, DM, ${ }^{\text {a }}$ | 250 | 20 | $1 / 75$ | 18.3 | 45 | - | 9 | 0.1 | - |  |  |
| $\left\|\begin{array}{l} 2 \text { NO1838A } \\ 2 N 1839 \end{array}\right\|$ | $\begin{array}{\|l\|l\|} \hline \text { PSI } \\ \text { PSI } \end{array}$ | non, DM, ${ }^{\text {a }}$, | 250 | 2.0 | 175 | 18.5 | 45 | - | , | 0.1 | - | 9 | Mi froa., hi pur. |
| $\left\|\begin{array}{l\|l\|l\|l\|} 2 N 189 \\ 2 N 189 A \end{array}\right\|$ | $\begin{array}{\|l\|l\|} \text { PSII } \\ \text { PSI } \end{array}$ |  | $\begin{aligned} & 250 \\ & 250 \end{aligned}$ | 20.8m | $175$ | $13.3$ | 45 | - | 9 | 0.1 | - | 9 | $\mathrm{H}_{1} \text { freq, min pui }$ |
| 2H602A | PH |  | 200 | $\frac{15}{2.0}$ | 115 | 10.6 1.0 | 45 30 | - | g | 0.1 13 | 6 | $10^{9}$ | Hi feqo, in pwo |
|  | PH | prommper | 250 | 60 | 6 |  | 20 | - | - | 1 |  |  |  |
| 211492 | RCA |  | 275 | 30 | 175 | 20 | 60 | 50 | 50 | 10 | - | $\stackrel{-}{-}$ |  |
| 211341 | PSI | npm, MS, 31 | 280 | 2.80 | 150 | 24 | 120 | 5 | $-$ | 8 | - | , | High heq, hich somer |
| 21058 | mo | pmo, DM, me | 300 | 75 | 100 | 1. | 15 | 50 | 0 | 0.2 | - | 3.5 | CES |
| 2N1488 | RCA |  | 300 | 3 m | $1 / 5$ | 20 | 100 | 50 | 50 | 10 | - | 35 |  |



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| SWITCHING SERVICEManimum Ratinge, Aboluot Menimum Values 3907/2M4O4 |  |
| :---: | :---: |
| COLIECTORTO. case voltace | - 25 MAX |
| COHECTOR TO-EMITRE Voltage with VED $=-1 v$ | - 24 max |
| emitier to-mase voltage | -12 max |
| collector current | - 200 max |
| emitier current | 200 max |
| TRANSISTOR DISSIPATION: Al ambient lemporalure of: $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 55^{\circ} \mathrm{C} \\ & \hline 11^{\circ} \end{aligned}$ $71^{\circ} \mathrm{C}$ | $\begin{gathered} 150 \text { max } \\ \text { 7s max } \\ 35 \text { max } \\ \hline \end{gathered}$ |
| AMBIENT <br> temperature iange. Operating Storage | $\begin{aligned} & -0510+15 \mathrm{c} \\ & -0510+100^{\circ} \mathrm{c} \end{aligned}$ |
| LEAD temperature <br> For immorsion in molton solder for 10 secondi mar | 255 max ${ }^{\circ} \mathrm{C}$ |



| Type No. | Mis. | Trpe | las | Marimum Retinge |  |  |  |  | Charactoristics |  |  |  | Remarts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\underset{(m w)}{c}$ | $T_{j}$ <br> (c) | mw/ 6 | $V_{V}$ | ${ }^{1} \mathrm{c}$ | hfo | $\begin{aligned} & I_{\mathrm{CO}} \\ & \mu^{2} \end{aligned}$ | $\begin{aligned} & N F \\ & d b \end{aligned}$ | $\begin{gathered} \mathrm{C}_{\mathrm{C}} \\ \mu \mu \mathrm{l} \end{gathered}$ |  |
| 2N503 | PH |  | 320 | 25 | 85 | 0.63 | 20 | 50 | 4.2 | 3 | - | 1.0 |  |
| 2N499 | PH | Pnp,MD.ge | 340 | 30 | 85 | 0.75 | 30 | $50$ | 85 | 10 | - | 1.3 | 61 |
| 2M741 | $\cdots$ |  | 360 | 300 | 100 | 1 | 15 | 100 | 25 | 2 | 7 | 6 | And VFF |
| 2N71AA | Mo | PM, DM, ge | 300 | 300 | 100 | 1 | 20 | 100 | 25 | 0.2 | 7 | 6 |  |
| 2N1407 | TI | Mnp,MS, ge | 375 | 75 | 100 | 1 | 30 | 50 | 6 | 2 | 1 | - |  |
| $2 \times 19$ | PSI | npn, OM, si | 400 | 1.2w | 100 | 6.7 | 25 | 220 | 4 | . 005 | - | 5 |  |
| $2 \mathrm{mg20}$ | PSI | npo, Dm, si | 400 | 1.2 w | 200 | 67 | 25 | 220 | 4 | . 005 | - | 5 |  |
| $2 \mathrm{me21}$ | PSI | npo, OM, 31 | 400 | 1.2 m | 200 | 67 | 50 | 200 | 4 | . 005 | - | 1 |  |
| 2 N 922 | PSI | npm, DM, si | 100 | 1.2m | 200 | 6.7 | 50 | 200 | 4 | . 005 | - | 4 |  |
| 2 N 1405 | 11 | Mp, MN, ge | 450 | 75 | 100 | 1 | 30 | 50 | 8 | 2 | 5 | - |  |
| 2N1405 | TI | DAP, WS, | 450 | 75 | 100 | 1 | 30 | 50 |  | 2 | 6 | - |  |
| 2 2N1143 | TI | prip, DB, ${ }^{\text {ce }}$ | 400 | 750 | 100 | 10 | 25 | 100 | 8 | . 1 | - | 1.5 | PGe2cto 20mc |
| 2 N 1502 | mo | Pap, MS, ge | 500 | 3 m | 100 | 40 | 25 | 500 | 108b | 1.5 | - | 7 | Migh frequ, high powar |
| 2N1561 | MO |  | 500 | 3m | 100 | 40 | 25 | 500 | 10db | 1.5 | - | 7 | Higt freq, high power |
| $2 \times 1700$ | 10 | mp, DM | 600 | 75 | 100 | 1 | 25 | 50 | 100 | 0.4 | - | 11 | UMF Amp |
| 217004 | $\cdots$ | PAP, DM, | 600 | 75 | 100 | 1 | 2 | 505 | db200me | C0. 0 | 5 | 11 | MIL |
| $2 \times 1142$ | TI | mod, DB, | 600 | 750 | 100 | 10 | 30 | 100 | 10 | 0.7 |  | 15 | PGe26db e 200 me |
| 2N1645 | WE | pmp, DJ, | 700 | - | 100 | 12.5 | 35 | 0.3 | 50 | 0015 | - | 10 |  |
| 2 5 537 | WE | MAP, DG, | 750 | 250 | 100 | 3 | - | 100 | 10 | 2 | - | 28 | U.S. MIL only |
| 2N1094 | VE | mp, DM, ge | 750 | 150 | 100 | 0.3 | - | 4 | 13 | 1.2 | - | 4 | U.S., MIL only |
| 2 N 1111 | TI | MP, DB, ${ }^{\circ}$ | 750 | 750 | 100 | 10 | 35 | 100 | 12 | 0.1 | - | 1.5 | PGJod a 20 mc |
| 241195 | WE | Pmp, DMge | 750 | 250 | 100 | 0.3 | 30 | 40 | 13 | 1.2 | - | 4 | HO |
| 2M218 | SY | PAR,N,g | - | 80 | 85 | 1.3 | 20 | - | 22.110 | 50 | - | - |  |
| $2 \times 231$ | PH | Mnp,SBT.ge | - | 9 | 55 | 0.9 | 4.5 | 3 | 66 | 3 | - | - | SPR |
| 2N233 | SY | mpn,AJ.ge | - | 50 | 75 | 1 | 10 | 50 | 10 | 50 | - | - |  |
| 21217 | SY | PMP, Dr,ge | - | . 000 | 100 | 1 | 40 | 10 | 20-175 | 50 | - | - |  |
| 2 W312 | CES | npm, $\mathrm{N}^{\text {de }}$ | - | 75 | 8 | 1 | 15 | - | - | 60 | - | 12 | SY, GI |
| 2M10 | SY | pap, AJ, ${ }^{\text {Pe }}$ | - | 50 | 75 | 1 | 20 | - | 22-110 | 5 | - | - |  |
| 2nsor | SPR | pnomorse | - | 30 | 85 | - | 35 | 50 | 16 | 100 | - | - |  |
| 2W544 | SY | MPD, DJ, ${ }^{\text {ce }}$ | - | 80 | 65 | 13 | 18 | 10 | 20-175 | 4 | - | - |  |
| 20x ${ }^{2}$ | SY | PRD, DJ, \% | - | 100 | 100 | 1.3 | 20 | - | 20 | 30 | - | - |  |
| 201706C | SY | npn, DM, si | - | 300 | 200 | 2 | 40 | 50 | 20-60 | d25 | - | - |  |
| 2N743 | SY | npm, MS, ${ }^{\text {si }}$ | - | 300 | 175 | 2 | 20 | 200 | 20-60 | 1 | - | - | Epitaxial |
| 2N74 | SY | $n \mathrm{n}, \mathrm{N}_{1} \mathrm{~N}, \mathrm{si}$ | - | 300 | 175 | 2 | 20 | 200 | 10-120 | 1 | - | 5 | Epitaxial |
| 21753 | PSt |  | - | $1{ }^{16}$ | 175 | 6.7 | 25 | 50 | - | 0.5 | - | 5 | Epiral |
| 21768 | SPR | pnp,MD, ${ }^{\text {c }}$ | - | 35 | 100 | - | 12 | 100 | 40 | 1 | - | - | PH |
| 210769 | SPR | Pnp,MD. | - | 35 | 100 | - | 12 | 100 | 55 | 0.3 | - | - | PH |
| 20173 | PH | npor, $\mathrm{SA}, \mathrm{si}^{\text {si }}$ | - | 150 | 150 | 1.2 | 20 | 100 | 11 | 0.1 | - | 1.3 |  |
| 20174 | PH | mpm,SA, si | - | 150 | 150 | 12 | 20 | 100 | 20 | 0.1 | - | 1.3 |  |
| 20175 | PH | npm,SA, si | - | 150 | 150 | 12 | 20 | 100 | 50 | 0.1 | - | 1.3 |  |
| 2N776 | PH | npm, SA, si | - | 150 | 150 | 12 | 20 | 100 | 11 | 0.1 | - | 1.3 |  |
| 2477 | PH | $n \mathrm{Pn}, \mathrm{SA}, \mathrm{si}$ | - | 150 | 150 | 12 | 20 | 100 | 20 | 0.1 | - | 13 |  |
| 2N778 | PH | nmosh , si | - | 150 | 150 | 12 | 20 | 100 | 50 | 0.1 | - | 1.3 |  |
| 2.1781 | SY | OAP, M5, ${ }^{\circ}$ | - | 150 | 100 |  | 15 | 200 | 25 | 3 | - | - | Epitaxial |
| 21762 | SY | MPD,MS, \% | - | 150 | 100 | 2 | 12 | 200 | 20 | 3 | - | - | Epitaxial |
| 2178 | SY | npm, Ms, si | - | 300 | 15 | 2 | 40 | 210 | 20-60 | . 25 | - | - | Epitaxial |
| 20178 | SY | npm, MS, si | - | 300 | 175 | 2 | 30 | 200 | ${ }^{2}$ | . 25 | - | - |  |
| 20115 | PH | MaMDs | - | 0 | 100 | 0.8 | 20 | 100 | 50 | 5 | - | 3 |  |
| 2N1158A | PH | PATM M M | - | 75 | 100 | 1 | 20 | 100 | 50 | 5 | - | 2.8 |  |
| $2 N 1204$ | SPR | Pap,MD, | - | 200 | 100 | - | 20 | 500 | 40 | 7 | - | - | PH |
| 2W12\% | SY | Mando | - | 50 | 75 | 1 | 20 | 10 | 15 | 50 | - | - |  |
| 2 W 1205 | SY | Pmpad, | - | 0 | 65 | 13 | 10 | - | 10 | 100 | - | - |  |
| 2N1267 | PH | npa, SADT, si | - | 150 | 150 | 0.8 | 2.1 | 100 | 11 | 01 | - | 1.5 |  |
| 2N1258 | PH | npa, SADT, si | - | 150 | 150 | 0.8 | 20 | 100 | 20 | . 01 | - | 1.5 |  |
| 2012: | PH | TM, SADT, 3 | - | 150 | 150 | 0.8 | 20 | 100 | 50 | . 01 | - | 15 |  |
| 241270 | PH | MPnSNDT, si | - | 150 | 150 | a 1 | 20 | 100 | 11 | 10 | - | 15 |  |
| $2 \times 1271$ | PH | npm, MDT, el | - | 150 | 150 | 0.1 | 20 | 100 | 20 | . 01 | - | 1.5 |  |
| 2 W 1272 | PH | npasadis il | - | 150 | 150 | as | 20 | 100 | 50 | D1 | - | 1.5 |  |
| 2N1398 | $\pi$ | Danp MS, ${ }^{\text {cos }}$ | - | 50 | 85 | - | 30 | 10 | 2.3 | 10 | 5 | - |  |
| 241308 | TI | Pap, $\mathrm{S}_{5}$, sil | - | 50 | 6 | - | 30 | 10 | 23 | 10 | 5 | - |  |
| 201400 | $\pi$ |  | - | 50 | 85 | - | 30 | 10 | 1.5 | 10 | - | - |  |
| 271401 | $\pi$ | Pap ${ }^{\text {Nas, }}$ | - | 50 | 0 | - | 30 | 10 | 2 | 10 | - | - |  |
| 2N1401a | $\pi$ | Pra, ${ }^{\text {ces }}$ | - | 50 | \% | - | 30 | 10 | 2 | 10 | - | - |  |
| 241402 | $\pi$ |  | - | 50 | 6 | - | 30 | 10 | 22 | 10 | - | - |  |
| 201450 | 51 | DQA, ${ }^{\text {a }}$ | - | 12. | 100 | 16 | 30 | 100 | 20 | 10 | - | - |  |
| 201494 | SPR | DmpMD, | - | 400 | 100 | - | 20 | 500 | 5 | 7 | - | - | PH |
| 2 W 1515 | AMP | 日, PAOTa |  | 8 | 75 | - | 20 | 10 | 6 | - | - | - | 0C169 |
| 201636 | SY | E0, ${ }^{\text {asel }}$ | - | 150 | 100 | 2 | 15 | 50 | 20 | 3 | - | - |  |
| 20167 | PH | mansat, si | - | 100 | 140 | - | 4.5 | 50 | 2.5 | 001 | - | - |  |
| 21®7 | PH | MPD, SAT, si | - | 100 | 10 | - | 4.5 | 5 | 5 | +001 | - | - | SPR, chopper |
| 20104 | SY | Monda | - | 100 | 400 | 13 | 5 | 100 | - | 5 | - | - |  |
| 201742 | PH | Pand ${ }^{\text {a }}$, 1 | - | $\infty$ | 100 | 08 | 20 | - | - | 08 | 4.9 | - |  |
| 201773 | PH | Wupmose | - | 0 | 100 | 0.8 | 20 | - | - | al | 10 | - |  |

High Frequency (concluded)

| Typo No. | Mfs. | Trpe | $f^{\text {a }}$ | Maximum Ratings |  |  |  |  | Charaetoristles |  |  |  | Rement |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\left.\begin{array}{c} w_{c} \\ (\mathrm{~m} \end{array}\right)$ | $T_{j}$ <br> (c) | mw/c | $v_{c}$ | $\begin{aligned} & I_{c} \\ & \text { ma } \end{aligned}$ | H/0 | $\begin{array}{\|l\|} 1 \\ \hline \end{array}$ | $\begin{aligned} & \text { NF } \\ & \text { do } \end{aligned}$ | $\begin{aligned} & C_{e} \\ & \mu \mu! \end{aligned}$ |  |
| 20174 | PH |  | - | $\infty$ | 100 | 0.8 | ๗ | - | - | 1 | - | - |  |
| 221745 | PH | POp, 10.10 | - | $\infty$ | 100 | 08 | 20 | 50 | - | 2.5 | - | - |  |
| 201777 | PH | DND.MO ${ }^{\text {a }}$ | - | 0 | 100 | 0.1 | 20 | 50 |  | 2 | - | - |  |
| 21178 | SY | mp, $\mathrm{Nu}^{\text {a }}$ | - | 100 | 100 | 13 | 30 | 100 | 30-150 | 6 | - | - |  |
| 21173 | SY | mande | - | 100 | 100 | 13 | 30 | 100 | $30-50$ | 5 | - | - |  |
| 20178 | SY | mp, $\mathrm{N}_{1}$ \% | - | 100 | 100 | 1.3 | 30 | 100 | 20 | 4 | - | - |  |
| 211840 | PSI | npm, DM M, si | - | 200 | 175 | 13.3 | 24 | - | 9 | - | - | 11 | mi fieq, mi pum |
| 20140A | PSI | npen, $\mathrm{Dm}_{6}$, si | - | 28 | 175 | 18.6 | 25 | - | 9 |  | - | 11 | hiv meq, hi mum |
| 201818 | WE | nom, $\mathrm{Mm}, \mathrm{si}$ | - | 15.4 | 150 | 75 | 2 | 35 | . 005 | 100 mc | - | - |  |
| 2N1865 | PH | mp, Mose | - | 60 | 1100 | 0.8 | 20 | 50 |  | 2 | - | - |  |
| 2011865 | PH | mpp, 10.8 | - | 0 | 100 | 0.8 | 35 | 50 | - | 2 | - | - |  |
| 21185 | PH | ONPMD.8e | - | 0 | 100 | 0.8 | 35 | 50 | - | 2 | - | - |  |
| 20165 | PH | WP. D, \%e | - | $\infty$ | 100 | 0.8 | 20 | 50 | - | 2.5 | - | - |  |
| 2 N 1588 | SY | npn,MS,si | - | 600 | 175 | 1 | $\pm$ | 500 | 20.00 | 0.5 | - | 18 | Epitaxial |
| 21.1589 | SY |  | - | 600 | 175 | 4 | 60 | 500 | 40-120 | 0.5 | - | 11 | Epitaxial |
| 211590 21151 | SY | MP, 以, \% | - | 150 | 100 | 2 | 15 | 200 | 25 | 3 | - | - | Epitaxial |
| 2N1501 | SY | Onpusem | - | 150 | 100 | $2^{2}$ | 12 | 200 | 20 | 3 | - | - | Epitaxial |
| 2 N 1963 | SY |  | - | 400 | 175 | 2.8 2.6 | 30 | 200 | 2 | 25 | - | 3.5 | Epiraial |
| 2NISA | SY | mmoms, si | - | 400 | 175 | 2.6 | ${ }_{0}$ | 500 | 20-60 | 0.5 | - | 18 | Epitaxial |
| 201195 | 5 |  | - | 400 | 175 | 2.6 | $\omega$ | 500 | 40.120 | 0.5 | - | 18 | Epitaxial |
| 2 L 1969 | SY | Pap, $\mathrm{A}, 18$ | - | 150 | 100 | 2 | 30 | 400 | 50-200 | 5 | - | 20 |  |
| GT16\% | GI |  | - | 150 | 100 | 2 | 100 | - | 25 | 1 | - | - | Orift |
| Mal 1 | SPR | mp, MAT, ${ }^{\text {co }}$ | - | 25 | 75 | - | 6 | 50 | 40 | 10 | - | - |  |
| mat | SPR | mp,MAT, $\mathrm{Se}^{\text {e }}$ | - | 20 | 75 | - | , | 50 | 40 | 10 | - | - |  |
| PTE50 | P51 | npn, $\mathrm{OM}_{3}$ si | - | 2 w | 175 | 13.3 | 120 | - | 2 | 2 | - | - | his frea, mi gur. |
| PTB50A | PSI | nom, $\mathrm{OM}, \mathrm{si}$ | - | 2.0w | 175 | 18.6 | 120 | - | 2 | 2 | - | - | hi meg, in pum. |
| Sol | SPR | pmp, SBT, ge | - | 20 | ${ }_{6} 6$ | - | 5 | 5 | 10 | 10 | - | - |  |
| 50.2 | SPR | pmp.SBT. ${ }^{\text {e }}$ | - | 15 | ${ }^{6}$ | - | 3 | 5 | 10 | 10 | - | - |  |
| 50.3 | SPR | pmp, SBT, $0^{3}$ | - | 20 | 6 | - | 5 | 5 | 10 | 10 | - | - |  |
| ST3081 | IR | Pon, DJ ,si | - | 150 | 175 | $=$ | - | - | - | - | - | - |  |

## Abbreviation of Terms

Alloy Junction
Double Diffused
Grown Diffused
Diffused Junction
Diffused Mesa
Diftused Planar
Drift
Epitaxial
Fused Alloy

| FJ | Fused Junction |
| :--- | :--- |
| GD | Grown Diffused |
| Ge | Germanium |
| GJ | Grown Junction |
| GR | Grown Rate |
| MB | Meltback |
| MD | MADT |
| Ms | Mesa |
| RG | Rate Grown |

Si Silicon
SBT Surface Barrier
$\mathbf{C}_{0 。}=$ Collector-to-emitter capacitance meas. ured across the output terminals with the input ac open-circuited.
$f_{\mathrm{ar}}=$ Frequency at which the magnitude of the forward-current transfer ratio (small-signal) is 0.707 of its low-frequency value.
$f_{t}=$ Frequency at which com!non emitter gain is unity.
$\mathbf{h}_{\mathrm{f}}$ = Common emitter-small signal forward current transfer ratio
$\mathbf{h}_{\mathrm{PE}}=$ Common emitter-static value of short circuited forward current ratio.
$\mathbf{I}_{\mathrm{se}} \quad=$ Collector current when collector junction is reverse-biased and emitter is dc open-circuited.
 Specify the new Amperex: P•A•D•T 40 the 2 timesfaster PNP Germanium Switching Transistor * $\mathrm{U}=\frac{1}{\text { nanoseconds } \times \text { pennies }}$ Right from the sketch-pad stoge, plan your computer switching circuits with the new PADT-40. * The extrsme speed and efficient design of the PADT-40 gives more $U$ (usefulness factor) and lower cost $x$ switching time. This results in fower mansistors to buy, less complicated circuits to design, and the elimination of many costly components becouse of multifunction circuit usage. But speed, of course, is only one of the cost-and-production advanlages inherent in the PADT-40; RELIABILITY, as only the revolutionary Post Alloy Diffusion Technique con provide, is another; AVAILABiluty, os only the mass-production rech. niques employed of the new Amperex plant in Slatersville, R. I., can provide, is still another; LOW PRICES (no higher than for low-speed transistors)... plus INTERCHANGEABILITY with many conventional meso transistors, round oul our 'package'. Yes, the new Amperek PADT- 40 is truly worth spocifying . . . nowl

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | w/c | $\mathbf{T}_{\mathbf{j}}$ | $\underset{v}{v_{c}}$ | $\left[\begin{array}{ll} 1 & c \\ \text { amp } \end{array}\right]$ | ${ }^{\text {h fe }}$ | $I_{m 0}$ | $\begin{aligned} & \mathrm{f} \\ & \mathrm{ai} \\ & \mathrm{kc} \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { Powr. } \\ \text { Gain } \\ \text { in } \end{array}$ | Pown. Out. wit |  |
| 21333 | II | npm, CR,si | 1.0 | 0.008 | 150 | 55 | D6 | 9.90 | . 01 | 6 | 30 | - | TR |
| $2 \mathrm{N340}$ | TI | nm, GR,si | 1.0 | 0.008 | 150 | 85 | . 06 | 990 | . 001 | 6 | 30 | - | TR |
| $2 \mathrm{N341}$ | T1 | npR, GR, si | 10 | 0.008 | 150 | 125 | . 06 | 9.90 | . 001 | 6 | 30 | - | TR |
| 2 3 31 A | TR | $\mathrm{npn}, \mathrm{OJ}, \mathrm{si}$ | 1 | 0.008 | 200 | 125 | . 1 | 1590 | . 001 | - |  |  |  |
|  | II | npn,GR,si | 1.0 | 0.008 | 150 | 60 | . 06 | 932 | . 001 | 6 | 30 | - | IR |
| 213424 | II | npm, GR, si | 10 | 0.008 | 150 | 85 | . 06 | 939 | . 001 | 6 | 30 | - | TR |
| $2 \mathrm{N3M} 3$ | II | npm, GR,si | 1.0 | 0,008 | 150 | 60 | . 06 | 20.50 | . 001 | 8 | 30 | - | TR |
| 2N343A | IR | $\mathrm{nma}, \mathrm{OJ}, \mathrm{si}$ | 1 | . 008 | 150 | 85 | - | 29.90 | . 001 | - | - | - | TR |
| 231206 | TR | mpn, GR,si | 10 | 10 | 200 | 60 | - | 15-18 | 1 | - | - | - |  |
| 21207 | TR | nm, 6 R,si | 1.0 | 10 | 200 | 125 | - | 15-90 | 1 | - | - | - |  |
| 2011566 | II | npm, MS, si | 1.2 | - | 175 | 80 | 50 | 100 | 1 | 50 | - | - | TR,NA |
| 211335 | PSI | nom, M, sis | 28 | 0.024 | 150 | . 120 | . 075 | 13 | . 008 | 170 mc | - | - | high frea, high pwo. |
| 211336 | PSI | $\mathrm{ngm}, \mathrm{MS}, \mathrm{si}$ | 2.8 | 0.024 | 150 | 120 | 075 | 13 | -008 | 170.mic | - |  | high reqe, high pur. |
| 211339 | PS | npmMS.si | 28 | 0.024 | 150 | 120 | . 075 | - | 008 | 220 mc |  |  | high frea, high pwi. |
| 2N1340 | PSI | npn, स¢,si | 28 | Q. 24 | 150 | 120 | . 075 | - | . 008 | $250 \mathrm{mc}$ | - | - | high heq, higit pum. |
| 221341 | PSI | npon, MS, si | 2.8 | 0.024 | 150 | 120 | . 075 | - | . 000 |  |  |  |  |
| 211505 | PSI |  | 3 | 0.2 | 1775 | 50 | - | 7 | - | $150 \mathrm{mc}$ | - | - | high frequ, high pur. |
| 2 L 1506 | PSI | non, $1 \times 5,81$ | 3 | 0.2 | 175 | 60 | 25 | 9 | M15 | 210 mc | - | - | high frea, high pwr. |
| $2 N 1561$ | $\cdots$ | pnp,ME, si | 3 | 0 | 100 | 25 | . 25 | 10 | . 2015 | 500 mc | - | - | high trea, high pur. |
| 2N1552 | 40 | MnD,MS, | 3 | . 04 | 100 | 25 | . 25 | 10 | . 015 | 450 mc | - | - | hightrea., nigh pwo. |
| 2 N 1692 | Mo | mproms, | 3 | . 04 | 100 | 25 | 25 | 10 do | . 0015 | 500 mc | 6 | 0.5 |  |
| 2N1693 | MO | pmp,ws.er | 3 | . 04 | 100 | 25 | 25 | 10 db | 2015 |  | 6 | . 1 |  |
| 2 MOg | ${ }_{11}$ | mppopal, si | 3.6 | . Q $_{3}$ | 200 | 32 60 | 1.40 | ${ }_{12} 35$ | 012 10 | 9 nc | - | - |  |
|  |  |  |  | .es | 20 | 60 |  | $12 \cdot 36$ | 10 | 9 nc | - | - | RCA |
| 2 m 988 | TI | $\mathrm{nmm}, \mathrm{DJ}, \mathrm{si}$ | 4.0 | .033 | 200 | 100 | 200 | 12-36 | 10 | 9 mc | - | - |  |
| 24656 | II | $\mathrm{nm}, \mathrm{DJ}, 51$ | 4.0 | . Q3 | 200 | 60 | 200 | 30-90 | 10 | 8 mc | - | - | $T R, R H, F A, N A$, RCA G' |
| 2N®1 | II | npm, DJ,si | 4.0 | . 023 | 200 | 100 | 200 | 30-90 | 10 | 8 mc | - | - | TR, RH, FA, NA, GE |
| 201479 | RCA | npp, $\mathrm{DJ}, \mathrm{si}$ | 4 | - | 175 | 60 | 1.5 | 50 | 10 | 1.5 mc | - | - |  |
| 2 N 1400 | RCA | npo, DJ ${ }^{\text {si }}$ | 4 | - | 175 | 100 | 1.5 | 50 | 10 | 1.5 mc | - | - |  |
| 211481 | RCA | $\mathrm{nm}, \mathrm{D}, \mathrm{st}$ | 4 | - | 175 | 60 | 1.5 | 50 | 10 | L. 5 mc | - | - |  |
| 211468 | RCA | npm, DJ, si | 4 | - | 175 | 100 | 1.5 | 50 | 10 | 1.5 mc | - | - |  |
| 2N1067 | STC | non, $\mathrm{DJ}, \mathrm{si}$ | 5 | 28.6 | 175 | 60 | 0.5 | 35 | 5 | 1.5 | - | - | RCA |
| ${ }^{2121210}$ | SY | npn, AJ, ge | 6 | 0.1 | 85 | 15 | 2 | 40, 100 | 3 | 7 | - | - |  |
| 574201 | TR | $\mathrm{npn}, \mathrm{DJ}, \mathrm{si}$ | ${ }_{6}^{6}$ | . 03 | 200 | 45 | 0.5 | 12.36 | . 001 | - | - | - |  |
| 574202 | TR | $n \mathrm{~nm}, \mathrm{DS}, 31$ | 6 | 03 | 200 | 75 | 0.5 | 12.36 | . 001 | - | - | - |  |
| ST203 | TR | npo, $\mathrm{OJ}, 51$ | 5 | . 03 | 200 | 45 | 0.5 | $30-90$ | . 01 | - | - | - |  |
| STA20] | TR | npm, DJ, 31 | 6 | . 03 | 200 | 75 | 0.5 | 30-90 | . 001 | - | - | - |  |
| 218326 | SY | npn, $\mathrm{N}, \mathrm{se}$ | 7 | 0.11 | 85 | 35 | 2 | 45 | 3 | 150 | - | - |  |
| 221172 | DE | Pmp,N,ge | 7.5 | . 1 | 100 | 40 | 1.5 | 0 | 0.01 | 17 | 34 | - | driver |
| 2W1183A | RCA | pmp,A,ge | 7.5 | - | 100 | 45 | 3 | 20 | . 03 | 500 | - | - |  |
| 2W11838 | RCA | mp, AJ.ge | 7.5 | - | 100 | 80 | 3 | 20 | . 03 | 500 500 | - | - |  |
| 201184 | RCA | mp, A, ge | 7.5 | - | 100 | 45 |  | 40 | . 03 | 500 | - | - |  |
| $2 N 1184$ | RCA | mp, N, ge | 7.5 | - | 100 | 60 | 3 | 40 | 03 | 500 | - | - |  |
|  | RCA | mpp,A, ge | 7.5 |  | 100 | 80 | 3 | 40 | . 13 | 500 | - | - |  |
| 2 N 122 | TI | npm, GR,si | 8.75 | . 070 | 150 | 120 | 140 | 3 | 10 | 5 | 28 | - |  |
| 2W176 | SY | pmp,AJ.ge | 10 | 0.15 | 90 | 30 | , | 4.5 | 0.3 | - | 35.5 | - | RCA, MO, BE |
| $2 \times 350$ | SY | mp,AJ.ge | 10 | 0.13 | 100 | 40 | 3 | 40 | - | 5 | 32 | $\bar{\square}$ |  |
| 2N351 2N376 | RCA | Mm, A.ge | 10 | 1 | 90 | 40 | 3 | 65 | , | - | 33.5 | 4 | MO, 5 Y |
| 2N376 2N669 | $\begin{aligned} & \text { RCA } \\ & \text { ma } \end{aligned}$ | pra, A,ge pmp,N, ge | 10 10 | 1.5 | 90 | 40 | 3 | 78 | ${ }^{3}$ | $\overline{5}$ | 35 | 4 |  |
| 21.1058 | IND |  | 10 | $\left.\right\|_{0.133} ^{1.5}$ | 175 | 30 | ${ }^{3}$ | 90 | 03 | 5 | 40 | 2 |  |
| 2 L 1714 | II | npn, MS, si | 10 | . 134 | 175 | 60 | 1 | - | . 002 |  | - |  | , |
| 221715 | T1 | nom, ${ }^{\text {NS }}$, si | 10 | . 134 | 175 | 100 | , | - | . 002 | 20 mc | - | - |  |
| 2 2 1716 | TI | npm, M5, si | 10 | . 134 | 175 | 60 | , | - | .000 | 20 mc | - | - |  |
| $2 N 1717$ | TI | npa, M6, si | 10 | . 134 | 175 | 100 | 1 | - | . 002 | 20 mc | - | - |  |
| 2N1718 | 11 | non,MS.si | 10 | . 134 | 175 | 60 | 1 | - | . 002 | 20 mc | - | - |  |
| 2N1719 | II | npon 10.10 si | 10 | . 134 | 175 | 100 | 1 | - | . 002 | 20 mc | - | - |  |
| 2 L 1720 | II |  | 10 | . 134 | 175 | 60 | 1 | - | . 002 | 20 mc | - | - |  |
| 2 N 1721 | TI | npm,MS, si | 10 | . 134 | 175 | 100 | 1 | - |  | 20 mc | - | - |  |
| 221755 | CL | pmp, N, ge | 10 | 2.5 | 95 | 40 | 3 | - | $?$ | 15 | 30-75 | - |  |
| 2N1756 | CL | mpa, A, ge | 10 | 2.5 | 95 | 60 | 3 | - | 7 | 15 | 30.75 | - |  |
| 2 N 1757 | CL | mpp, N, pe | 10 | 2.5 | 95 | 80 | 3 | - | 7 | 8 | 30-75 | - |  |
| 2N1758 | CL | pmp, A, 8 ge | 10 | 25 | 95 | 100 | 3 | - | 7 | 8 | $30-75$ | - |  |
| 2 N 1758 | CL | pap, ${ }^{\text {a }}$, ge | 10 | 2.5 | 95 | 0 | 3 | - | 7 | 10 | 60.150 | - |  |
| 211760 | CL | mpp,N,ge | 10 | 2.5 | 8 | 60 | 3 | - | $?$ | 10 | 60.150 | - |  |
| 2N1761 | CL | mp,N, ${ }^{\text {ce }}$ | 10 | 2.5 | 95 | 80 | 3 | - | 7 | , | 60-150 | - |  |
| 2N11762 CDT1310 | CL | pnp, A. $\mathrm{ge}^{\text {ge }}$ | 10 | 2.5 | 95 | 100 | 3 | - | 7 | 5 | 60-150 | - |  |
| COT1310 | CL | pnp,N, 8 ce | 10 | 1.5 | 95 | 40 | 5 | - | 15 | 5 | 40.120 | - |  |
| COT1311 | CL | mpp, A, $\mathrm{E}^{\text {e }}$ | 10 | 1.5 | 9 | 60 | 5 | - | 15 | 5 | 40-120 | - |  |
| CDT1312 CDT1313 | CL | mp, N, ge | 10 | 1.5 | 8 | 80 |  | - | 15 | 5 | 40.120 | - |  |
| CDT1313 | CL | pmp, A, 8 ge | 10 | 1.5 | 95 | 100 | 5 | - | 15 | 5 | 40-120 | - |  |

Power (continued)



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| :---: | :---: | :---: |
|  |  |  |
| Pasen <br> 120CG TYPE <br> 4 TYPEs a silicon "Solaprid" cells-120CG-10 to 120CG-14 (Oata sheet No. 136) <br> 220C TYPE <br> 3 TrPEs E silicon solar colls-220C-8 to $2200-10$ (Dat sheat No 126) (Dreie sheat No. 126) |  |  |
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- Almost infinite power gain
- Extremely low noise figures ( 0.5 dB maximum)
- Negligible offset voltage (less than $1_{\mu} V$ )
- Unprecedented gain stability

The silicon field-effect transistors from Crystalonics combine almost all advantages of vacuum tubes and conventional transistors. They are silicon majority carrier devices presently available in the TO-5 package, and have three terminals; anode, cathode, and grid. The transistor action takes place entirely within the bulk of the silicon material and completely away from the surface, giving rise to an unprecedented gain stability of the unit. The radiation resistance of the fieldeffect transistors exceeds that of the conventional units approximately ten times.
The new devices are recommended as first stages to high input, low noise amplifiers, low level switching circuits such as choppers, analog multipliers, and electronically variable resistors.

Low Noise Amplifiers:
Field-effect transiteors are inherently low noise devices and have noise fíures considerably below that of the bert Ielected low noise transistors and tubes. sistor, the field-effect unit does not pacs any working current throukh the junctions, and it does not rely for its operation on minority carriers which eventually recombine to produce base current of the conventional unit. Both processes, the passink of current throukh emitter and collector junctions and carrier recombination are inher. ently noiay, and are completely elim. inated in the new device. The result io

- transiator series (C620) with maximum noise figures of 0.5 dB with 1 Ma senerator impedance. To obtain optimum performance for the low noise field-efiect transistors, the krid bins should he kept at zero and the anode potential at approximately 3 volts.

High Input Impedance A mplifiers:
The input impedence of the field. effect irantiator is effectively equiva. lent to a reverse biased silicon diode and is of the order of 1000 Mis. The output characteristics of the C613 fieldeffect transistor is shown below. They pentode. In wict the fold-effect tran sistor can be used in a manner analoRous to vacuum pentodes and. therefore. no new circuit techniques are required.

Low Level Switching:
Unlike the conventional transitur which is armally "off" switch. the feld-effect unit is "normally "on" switch. In the "on condition. the unit, retistor without any "offset" voltale. The only equivalent of "offset voltake" in the field-eflect transistors is the noise senerated by this silicon resistor, and is of the order of $.1 \mu$ Volt. No matehink of units is therefore required. and only one device has to be used instead of the usual two.
FROM STOCK
Silicon Field-effect Transistors Crystalonics Inc. Types

| C610 | C611 | C612 | C613 | C614 |
| :--- | :--- | :--- | :--- | :--- |
| C615 | C650 | C651 | C652 | C653 |

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| $\begin{aligned} & \text { Typt } \\ & \text { No. } \end{aligned}$ | Mfy. | Type |  | Man. Rarlag: |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | w/c | $\begin{gathered} \mathrm{T}_{\mathrm{j}} \\ \mathrm{c} \end{gathered}$ | $V_{c}$ | $\mathrm{T}_{\mathrm{c}}$ |
| LT-12 | CBS | Dup, | 20 | 0.33 | 85 | 100 | 3 |
| LT-13 | CBS | $\mathrm{mp}, \mathrm{N}, \mathrm{C}$ | 20 | 0.33 | 5 | 120 | 3 |
| LT-14 | CBS | Pap, A, Pe | 20 | 0.33 | 85 | 150 | 3 |
| LT. 15 | C8s | pmp, $\mathrm{N}, \mathrm{ge}^{\text {c }}$ | 20 | 0.33 | \$ | 200 | 3 |
| 21234 | 8 BE | PWRANP | 25 | 1.2 | 50 | 30 | 3 |
| 21235A | BE | manNs: | 25 | 12 | 9 | 10 | 3 |
| 212358 | BE | pnp,N, ${ }^{\text {a }}$ | 25 | 12 | 90 | 10 | 3 |
| 212364 | BE | mp, 1.80 | 25 | 12 | 5 | 40 | 3 |
| 212051 | BE | mopango | 25 | 12 | \% | 40 | 3 |
| 2129 | SY | manice | 25 | 0.33 | 100 | $\infty$ | 2 |
| 27399 | BE | mp | 25 | 1.2 | S | 10 | 3 |
| 2900 | BE | mp, N, | 25 | 12 | 95 | 40 | 3 |
| 27146 | CL | pmp, N. ${ }^{\text {a }}$ | 25 | 0.7 | 5 | 40 | 5 |
| 20111450 | CL | mpande | 25 | 0.7 | 5 | 0 | 15 |
| 2111468 | CL | Pmanse | 25 | 0.7 | 5 | $\infty$ | 15 |
| 2N146C | CL | pmp,AN, ze | 25 | 0.1 | 9 | 100 | 5 |
| $2 N 147$ | CL | Pmp, | 2 | 0.7 | 5 | 0 | 15 |
| 211147 | CL | mpon, ${ }^{\text {P }}$ | \% |  | 95 | co | 15 |
| 2 W 11478 | CL | Pno,N, | 25 | - | 9 | 80 | 15 |
| $21137 C$ | CL | mpa,N, | 25 |  | 85 | 100 | 15 |
| 212205 | CBS | pn | 25 | 0.5 | ${ }^{6}$ | 25 | 3 |
| 211246 | C8S |  | 25 | 0.5 |  | 25 |  |
| 211463 | RCA | npm,01,si | 25 |  | 200 | 60 | 3 |
| 21104 | RCA | mpm, $\mathrm{OJ}, \mathrm{si}$ | 25 | - | 201 | 100 | 3 |
| 211485 | RCA | mpen, Oj , si | 25 | - | 200 | 60 | 3 |
| 20146 | RCA | npm, DJsi | 25 |  | 200 | 100 | 3 |
| $8-17$ | BE | mpana | 2 | 12 | 50 | 30 | 3 |
| ${ }^{8} .178$ | BE | mpan, | 25 | 12 | 9 | 30 | 3 |
| $8-179$ | BE | pmp,Nip | 25 | 12 | 0 | 40 | 3 |
| CTPISOX | CL | - np, ${ }^{\text {a }}$ | 25 | 10 | 95 | 100 | 15 |
| CTPI503 | CL | man | 25 | 20 | 5 | 0 | 15 |
| CTP1504 | CL | PMAN. $0^{\text {a }}$ | 25 | 10 | 95 | 0 | 5 |
| CTP 150 | CL | pmp,N, ise | 2 | 1.0 | 95 | 4 | 15 |
| CTP154 | CL | Map,Nus | 2 | 10 | 95 | 0 | 25 |
| CTPIS | CL | mpp, $\mathrm{N}_{30}$ | 2 | 10 | \% | 0 | 25 |
| CTP1552 | CL | mp, N, $\mathrm{S}_{5}$ | 25 | LO | 9 | 0 | 25 |
| CTPIS53 | CL | mapondse | 25 | 10 | 5 | 100 | 25 |
| 212368 | CBS | Mm, N, | 30 | - | ${ }^{5}$ | 40 | 3 |
| 21242 | SY |  | 30 | 0.33 | 100 | 45 | 20 |
| 21257 | BE | mpd | 30 | 2.0 | 9 | 40 | 3 |
| 21258 | BE | mpp,N, ${ }^{\text {ce }}$ | 30 | 2.0 | 0 | - | 3 |
| 2 L 338 | MH | MPD,AJ, ${ }^{\text {cem }}$ | 32 | Q, 15 | 5 | 80 | 3 |
| 21538 | M ${ }^{\text {H }}$ | pnpanje | 32 | Q/5 | \% | $\omega$ | 3.0 |
| 2 NS 40 | M ${ }_{\text {M }}$ | $\mathrm{mpp}, \mathrm{N}, \mathrm{g}^{8}$ | 32 | 0,45 | 95 |  | 3.0 |
| 2N120 | M H | mp, N, ge | 32 | 0.5 | 5 | 80 | 3 |
| 2 N 1200 | M | Pmp, N, se | 32 | 0,A5 | 95 | 120 | 3 |
| 211251 | M ${ }^{\text {M }}$ | mpp, $\mathrm{N}, \mathrm{se}$ | 32 | 0.45 | 95 | $\infty$ | 3 |
| 212262 | M ${ }_{\text {H }}$ | mp,N, ${ }^{\text {cem }}$ | 32 | 0.45 | 95 | 0 | , |
| 201208 | MH | pmp, $\mathrm{Na}^{\text {cee }}$ | 32 | 0.15 | 45 | 0 | 3 |
| 212501 | M | P9p, $\mathrm{N}_{\text {de }}$ | 32 | a/5 | 95 | 60 | 3 |
| 201508 | H | mp, $\mathrm{Na}_{\text {ce }}$ | 32 | 0.5 | 5 | 0 | 3 |
| 2 max | WE | momaje | 35 |  |  | $\infty$ | 5 |
| 211011 | BE | dapan, | 35 | 02 | 95 |  | , |
| 2 L 178 | 00 | mpang | 40 | 14 | 50 | 40 | 3 |
| 2 NW 5 | mo | Pmon, $\mathrm{c}^{\circ}$ | 4 | L4 | 50 | 15 | 3 |
| 21555 | mo |  | $\infty$ | 1.4 | 50 | 30 | 3 |
| 211007 | STC | mpad,y | 40 | $a_{2}$ | 200 | 80 |  |
| 2M1087a | $\pi$ | mpm MS, ${ }^{\text {a }}$ | 40 | . 278 | 200 | 80 | . 5 |
| 212088 | STC | apmod, DJi , | 4 | 02 | 200 | 120 | S |
| 2W1040A | TI |  | 40 | . 280 | 20 | 120 | 0.5 |
| 210201 | STC | npm, $0 \mathrm{~J}, \mathrm{~s}$ | 40 |  | 200 | 0 | 5 |
| 2 Cl 1099 A | TI |  | 4 | 228 | 200 | d | 5 |
| ${ }^{2 N 1050}$ | STC | npen, 01.15 | 40 | 02 | 200 | 120 |  |
| 2 2 11550 A | 1 | npm,16, si | 0 | 228 | 200 | 120 | 5 |
| 211458 | ces | mp,AJ.Es | 10 | 0.66 | 8 | 30 | 5 |
| $2 \mathrm{NL1454}$ | CBS | mpp, $\mathrm{N}, \mathrm{c}^{0}$ | 40 | 2.65 | 85 | 30 | 5 |
| 21145 | CBS | mplas, | 0 | 2.66 | 85 | 60 | , |
| $2 \times 1456$ | COS | omp, $\mathrm{N}, \mathrm{se}$ | 40 | 266 | 85 | $\infty$ | , |
| 211457 | C8S |  | 10 | 2 6 5 | 85 | 0 | 5 |
| 201458 | CES | mp,N, | $\omega$ | 265 | 85 | $\infty$ | 5 |
| 214661 | CES | pmonase | 40 | D.cs | 5 | 30 | 5 |
| 211462 | CES | mpa, $\mathrm{L}_{1} \mathrm{~g}$ e | 40 | 2666 | 5 | 30 | 5 |
| 211483 | CES | pmp, A , es | 40 | D. 65 | 85 | 0 | 5 |
| 201164 | CBS | pap, AN, es | 40 | 2.c5 | 85 | 0 | 5 |
| 20161 | TR | Monodjosil | 10 | 21 | 175 | 0 | 3 |


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| $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ | Mfg． | Type | $w_{c}$ | Mor．Rotings |  |  |  | Charectorlasics |  |  |  |  | Remarts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | w／c | $\begin{aligned} & T_{1} \\ & c \end{aligned}$ | ${ }_{v_{c}}$ | $\begin{gathered} { }^{1}{ }^{c}{ }^{c} \\ \text { amp } \end{gathered}$ | ${ }^{\prime}$ fe | $\begin{aligned} & 1 \\ & \infty \\ & m \end{aligned}$ | $\begin{aligned} & \hline \\ & \mathrm{cec} \\ & \mathrm{kc} \end{aligned}$ | $\begin{gathered} P o w r_{0} \\ \text { Gain } \\ \text { db } \end{gathered}$ | Pown． Out w |  |
| $2 N 1649$ | TR | npn，DJ，si | 40 | 27 | 17 | 120 | 3 | 15－45 | ．025 | 10 nc | － | － |  |
| $2 \mathrm{LLG9}$ | TR | npm， DJ, si | 40 | 27 | 17 | 80 | 3 | 30－90 | ．025 | 10 mc | － | － |  |
| $2 \times 1650$ | TR | npm， 0 J，si | 40 | 27 | 175 | 120 | 3 | 30－50 | ． 025 | 10 mc | － | － |  |
| 2N1885 | TR | npn， $\mathrm{DJ}, \mathrm{si}$ | 40 | 27 | 175 | 60 | 5 | 20－80 | ． 35 | 8 mc | － | － |  |
| 2 2 2018 | TR | npn，$D J$, si | 40 | 27 | 175 | 150 | － | $20-60$ | 01 | 10 mc | － | － |  |
| 2 2 2019 | TR | mpn， DJ, si | 40 | 27 | 175 | 200 | － | 20.60 | ． 01 | 10 me | － | － |  |
| 2N2020 | TR | npm， DJ, si | 40 | 27 | 175 | 150 | － | 40－120 | 01 | 10 mc | － | － |  |
| 2TECO1 | TR | npm， $\mathrm{D}, \mathrm{J}, 3 \mathrm{i}$ | 40 | ． 27 | 15 | 200 |  | 10.120 |  | to mc | － | － |  |
| 2W1120 | BE | onpoAJ，${ }^{\text {a }}$ | 45 | 10 | \％ | 0 | 15 | 20.50 | 15 | － | － | － | mo |
| 2N250 | It | PnD．A J， | 50 | 27 | 100 | 30 | 5 | 00 | 2 | － | 30 | － | CL |
| 21051 | TI | pmp，AJ， $0^{\text {a }}$ | 50 | 27 | 100 | $\infty$ | 5 | $\infty$ | 2 | － | 30 | － |  |
| 21553 | OE | Pnpaj」s | 50 | 15 | 100 | 80 | 5 | － | 202 | 25 | － | － |  |
| 2N655 | DE | pnp，$A$ Jes | 50 | 25 | 100 | 80 | 5 | $\square$ | 10 | 25 | － | － | Jan2Me65 |
| 2 N 1014 | RCA | pap，AN，ge | 50 | 10 | 100 | 100 | 10 | 7 | 2.1 | － | 26 | 30 |  |
| 2N1059 | STC | npn， $0 \mathrm{~J}, \mathrm{si}$ | 50 | ． 29 | 1／5 | © 0 | 4 | $\pm$ | 1 | 1 | － | － | RCA |
| 211070 | STC | npm， $\mathrm{DJ}, \mathrm{si}$ | 50 | 29 | 175 | 6 | 4 | 21 | 1 | 1 | － | － | RCA |
| 21172 | TI | npm，MS，si | 50 | ． 67 | $1 / 5$ | 80 | 7.5 | － | 1 | 20 nc | － | － |  |
| 211724 | TI | non，MS，si | 50 | ． 67 | 178 | 80 | 7.5 | － | 1 | 20 nc | － | － |  |
| 221505 | RCA | pnp， $\mathrm{Dr}_{1} \mathrm{sec}^{8}$ | 50 | 0.7 | － | $\infty$ | 10 | 90 | ． 15 | － | － | － |  |
| 2N1506 | RCA | pmo．Dr， $8^{\circ}$ | 50 | 0.7 | － | 100 | 10 | 125 | ． 15 | － | － | － |  |
| 2141470 201657 | RA | npm，DJ，si | 55 | 3.0 | 20 | 60 | 2 | 50 | 10 | 10 | － | － | Diamond Pack rex |
| 2 L 1657 | RA | ¢pn，DB，si | 55 | 33 | 200 | 60 | 2 | 50 | 10 | 10 mc | － | － |  |
| 2 M 19 | BE | pap，AJ， $\mathrm{gec}^{\text {c }}$ | 60 | 12 | 98 | 45 | 3 | － | 0.5 | － | － | 5 |  |
| $2 \mathrm{nc39}$ | BE | pnp，AJ，${ }^{\text {co }}$ | 80 | 1.2 | 100 | 40 | 5 | 15－30 | 20 | － | － | － |  |
| 2Wagh | BE | pmp，N，${ }^{\text {cem }}$ | 60 | 12 | 100 | 70 | 5 | 15－30 | 10 | － | － | － |  |
| 2 2 6398 | BE | p $p$ P，$A J_{1}$ ， | $\infty$ | 12 | 100 | 80 | 5 | 15－30 | 2.2 | － | － | － |  |
| 2W1073 | 8E | mppaj，${ }^{\text {ce }}$ | 0 | 10 | 100 | 40 | 10 | 20－6 | 20 | 15 | － | － |  |
| 2N1073A | BE | MP，AL， | © | 1.0 | 100 | 80 | 10 | 20.6 | 1.5 | － | － | － |  |
| 2N10738 | BE | mpp，AJ，${ }^{\text {ce }}$ | 60 | 1.0 | 100 | 120 | 10 | 206 | 20 | 1.5 | － |  |  |
| 2N1136 | BE | DMp，AJ，${ }^{\text {a }}$ | $\infty$ | 12 | 100 | 40 | － |  | 0.5 | － | － | － |  |
| $2 N 11364$ | 㔭 |  | $\infty$ | 1.2 | 100 | 7 | 6 | － | 2 | － | － | － |  |
| 2111368 | BE | 㗇，AJ，${ }^{\text {ce }}$ | 60 | 12 | 100 | 80 | 6 | － | 2 | － | － | － |  |
| 2 N 1137 | BE | pmp， $\mathrm{NJ}^{\text {，ge }}$ | $\infty$ | 12 | 100 | 40 | 5 | － | 0.5 | － | － | － |  |
| 2W1137A | BE | mpaj， | $\infty$ | 12 | 100 | 70 | 6 | － | 2 | － | － | － |  |
| 2 W 1378 | BE | mon，AJ， | $\infty$ | 12 | 100 | 80 | 6 | － | 2 | － | － | － |  |
| $2{ }^{2} 1238$ | BE | mpo， N ，\％ | 60 | 1.2 | 300 | 40 | 6 | － | 0.5 | － | － | － |  |
| 2W1139 | BE | PAD，AJ， | 60 | 12 | 100 | 70 |  | － | 20 | － | － | － |  |
| 2 W 13388 | BE |  | 60 | 12 | 100 | 00 | － | － | 2 | － | － | － |  |
| 2N120 | TR | mpan， $\mathrm{D}, \mathrm{y}$ ， $\mathrm{I}^{\text {a }}$ | 60 | 27 | 175 | $\infty$ | 5 | 15－75 | 50 | 15 mc | － | － | STC |
| 2 N 1211 | TR | nmon， D, si | 60 | 21 | 175 | 70 | 5 | 15－75 | 50 | 15 mc | － | － | STC |
| 201487 | RCA |  | 60 | － | 175 | 60 | 6 | 30 | 25 | 1 nc | － | － | STC，SE |
| 2141409 | rca | npm，$D J$, si | 60 | － | 175 | 100 | 6 | 30 | 25 | 1 mc | － | － | STC，SE |
| 2N1409 | RCA |  | 6 | － | 175 | 60 | 6 | 30 | ${ }^{2}$ | 1 mc | － | － | STC，SE |
| 2 L 1490 | RCA | npm， $\mathrm{DJ}, \mathrm{si}$ | 60 | － | 175 | 100 | 5 | 30 | 25 | 1.25 mc | － | － | STC，SE |
| 2N1616 | TR | npon， DJ, si | $\pm$ | 27 | 15 | 60 | 5 | 15－7 | 50 | 15 mc | － | － |  |
| 241617 | TR | npon， $\mathrm{O}, \mathrm{J}$, si | $\infty$ | 27 | 175 | 5 | 5 | 15－75 | 50 | 15 mc | － | ＊ |  |
| $2 N 1618$ | TR | npm，DJ，si | $\infty$ | 27 | 175 | 0 | 5 | 15－75 | 50 | 15 me | － | － |  |
| STALO | TR | npm， $\mathrm{DJ}, \mathrm{si}$ | © | 27 | 150 | $\omega$ | 5 | 10 | 1 | － | － | － | SE |
| STA50 | TR | n¢n， DJ, si | 0 | 21 | 150 | 60 | 5 | 10 | 1 | － | － | － |  |
| 2 N 1740 | TS | pmpalsse | 7 |  | \％ | 80 | 15 | 37 | 8 | 18 | － | － | $\cdots$ |
| 3M5 | M ${ }_{\text {M }}$ | pmpad．p | 75 | 1.0 | 100 | $\omega$ | 10 | 50 | 30 | 750 | － | － | Sat wilte． 15 v |
| 3 M 45 | M ${ }_{\text {H }}$ | mpaj， | 75 | 1.0 | 100 | 20 | 10 | 40 | 3.0 | 450 | － | － | Sat voll 0.15 |
| 3047 | 4 | app，AJ． | 7 | 10 | 200 | 40 | 10 | 50 | 3 | 750 | － | － | Sat voll 0 O． $15 v$ |
| 330 | ${ }^{4}$ | mpajam | 75 | 10 | 100 | 6 | 10 | 40 | 3 | 450 | － | － | Sat volt＝0．15v |
| 2068 | 7 | npm，DJ，${ }^{\text {a }}$ | 05 | ． 0 | 200 | 0 | ， | 12－40 | 10 | 7 mc | － | － | STC，RR，RA |
| 20121619 | TI | mpon， $\mathrm{DJ}, \underline{0}$ | 6 | ． 48 | 200 | 00 | 2 | $12-00$ | 10 | 6 me | － | － | STC，TR，MA SE |
| 2W1619 2W1ce0 | TR | Tpand ，\％il | 5 | 27 | 200 | 50 | 5 | 30 | 01 | 15 cc | － | － |  |
| 2 c 1 cos | RA | mpa， $08,3 i$ | 8 | 0.5 | 200 | 60 | 2 | 50 | 10 | 40 ac | － | － |  |
| 2 l （108 | RA | \％pa， 08 | \％ | 0.5 | 200 | 100 | 2 | 9 | 10 | 40 | － | － |  |
| 2W1894 | RA | mpan， DR ，¢ ${ }^{\text {di }}$ | 65 | 0.5 | 200 | 60 | 2 | 30 | ． 01 | － | － | － |  |
| ${ }^{211205}$ | Ra | apa， 08,41 | 65 | 0.5 | 200 | 20 | 2 | 30 | ． 01 | － | － | － |  |
| 2 W1155 | RA | пpm， 08, si | ${ }^{5}$ | 05 | 200 | $\infty$ | 2 | 9 | ． 01 | － | － | － |  |
| 211057 | Ra | mpn，D8，si | 6 | 0.5 | 200 | 00 | ， | 50 | ． 01 | － | － | － |  |
| 2 N 180 | RA | mpa， $\mathrm{DB}_{3}$ si | 85 | 0.5 | 20 | 100 | 2 | 9 | ． 01 | － | － | － |  |
| STCID | STC |  | \％ | － | 200 | 60 | f | 10－50 | ．025 |  |  |  |  |
| STC1102 | 5TK | mpa 0 D，si | 85 | － | 200 | 500 | 6 | 10.50 | ． 025 | 1 lac | － | $=$ |  |
| STCllue | STC | apan DJ S ${ }^{\text {a }}$ | 8 | － | 200 | 0 | 5 | 25.5 | des | $1 \times$ | － | － |  |
| STCILO | STC | －0，00，${ }^{\text {a }}$ | 85 | － | 200 | 100 | 6 | $25-15$ | 095 | isec | － | － |  |
| 20esia | $\pm 0$ | Dajome | 50 | 12 | 100 | 0 | 3 | 40－100 |  | 5 | － | － | DE，BE |
| 2 rasoa | $\square$ | pmp， $\mathrm{N}_{\text {ces }}$ | 50 | 1.4 | 100 | 50 | 3 | 3 | 3 | 5 | 33 |  |  |
| 220514 | 0 |  | 50 | 14 | 100 | 50 | 1 | 6 | 3 | 5 | 30 | － |  |
| $213 \pi \times 1$ | mo | －9，Ne | 90 | 14 | 100 | 50 | 5 | 0 | 3 | 5 | 38 | － |  |
| 2 c 1 | 10 | mal， | 0 | 12 | 100 | $\oplus$ | 10 | 10－30 | 4 | 5 | 36 | － |  |
| 2 m 20 | 0 | ma， | $\pm$ | 12 | 30 | 0 | ¢ | 10.30 | 1 | 5 | 38 | － |  |

Power (continued)

| Type | Mfg. | Typo | ${ }^{w}=$ | Max. Ratings |  |  |  | Chorectorisitica |  |  |  |  | Roment |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | W/6 | $\begin{array}{\|c} T_{1} \\ c \\ \hline \end{array}$ | $\begin{aligned} & v_{c} \\ & { }_{c} \end{aligned}$ | $\begin{aligned} & 1 \\ & c \\ & \text { cimp } \end{aligned}$ | ${ }^{1}$ | $\begin{aligned} & 1 \\ & \infty \\ & \infty \end{aligned}$ | $\begin{array}{\|l} \hline 1 \\ \mathrm{ce} \\ \mathrm{kc} \end{array}$ | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Pown } \\ \text { Gind } \\ 0 \end{array} \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline \text { Poun: } \\ \text { Oal } \\ \hline \end{array}$ |  |
| ${ }^{214629}$ | mo |  | 90 | 1.2 | 100 | 80 | 10 | 10.30 | 1 | 5 | 38 | - |  |
| ${ }_{21500}^{2 N 50}$ | mo | pmp,A, se | 90 | 1.2 | 100 | 100 | 10 | 10,30 | ' | 5 | 38 |  |  |
| ${ }_{2 \times 67}^{2 W 6}$ | ${ }_{\text {BE }}^{8 E}$ | prosi, ${ }^{\text {mom }}$ | 90 | 1.2 | 100 | 50 | 15 | 15 | 1 | - | - | - |  |
| $2 \mathrm{M6}$ 7 ${ }^{\text {a }}$ | ${ }^{\text {BE }}$ |  | ${ }_{90}$ | 12 | 100 | 90 | 15 | 15 | 1 | - | : | - |  |
| 2467 C | 恹 | Pmp,A, $8^{\circ}$ | 90 | 12 | 100 | 120 | 15 | 4 | 1 | - | - | - |  |
| ${ }_{2 \times 1475}$ | BE | pmpa, | 90 | L2 | 100 | 150 | 15 | 7 | 1 | - | - |  |  |
| ${ }_{2} 2 \mathrm{NG774}$ | 8 BE | pmande | \$0 | 1.2 | 100 | 60 | 15 | 15 | 1 | - | - | - |  |
| ${ }^{2 N 6788}$ | 8E | Pmpa, | \% | 1.2 | 1100 | 90 | 15 | 15 | 1 | $-$ | - | - |  |
| $2 \mathrm{C678C}$ | BE | pmpAJge | 90 | 12 | 100 | 100 | 15 | 75 | 1 | - | - | - |  |
| 211001 | 8 E | pmoAJ, ee | 90 | 0.8 | 100 | 30 | 5 | 20:60 | 1.0 | - | - | - |  |
| $2 \mathrm{2m10314}$ | BE |  | 90 | 0.8 | 1100 | 40 | 15 | 20.60 | 1.0 | - | - | - |  |
| $2 \mathrm{2N10318}$ | ${ }_{\text {BE }}^{8 E}$ | mpp,N, ${ }_{\text {max }}$ | 90 | Q. 8 | 100 100 | n | 15 | 20-60 | ${ }_{20}^{20}$ | - | - | - |  |
| 211038 | ${ }_{\text {BE }}$ | mponise | ${ }_{90}$ | Q ${ }^{8}$ | 100 | 30 | 15 | 50-100 | 10 | - | - | - |  |
| 2 2 1138 a | BE | mpon, ${ }^{\text {mos }}$ | 90 | 0.8 | 100 | 40 | 15 | 50-100 | 10 | - | - | - |  |
| 2710328 | BE | Prp,N, | 0 | 0.8 | 100 | n | 15 | 50-100 | 22 | - | - | - |  |
| ${ }_{2 N 112}^{2 N 123 C}$ | 8E | pronde | so | $0_{1}^{08}$ | 100 | \% | 15 | 50-100 | 2 | - | - | - |  |
| 2W1162A | mo |  | 90 | 12 | 100 | 50 | 25 | 15.6 | 15 | 1 | - | - |  |
| 2 21163 | mo | pmondice | 50 | 12 | 100 | 50 |  | 15-6 |  |  | - |  |  |
| 221163 | \% | mpp,AJ, | 90 | 1.2 | 100 | 50 | 25 | 15-E | 15 | , | - | - |  |
| ${ }_{2 N 1164}^{2 N 164}$ | mo | mop,N, ce | 90 | 1.2 | 100 100 | 8 |  | 15-65 | 3 | 4 | - | - |  |
| 2N116 | mo | mpan,se | 90 | $\stackrel{L}{2}^{2}$ | 100 | \$0 | 25 | 15.55 | ${ }_{3}$ | 1 | = | - |  |
| 2 2 11155 | mo | pmo,N.se | 90 | 12 | 100 | $\infty$ | 25 | 15-65 | 15 | 4 | - | - |  |
| 211165 | mo | mp,N, | 50 | 12 | 100 100 | 80 | 25 | ${ }^{1565}$ | 3 | 1 | - | - |  |
| ${ }_{2 N 167} 21165$ | mo |  | 90 | ${ }_{L} \mathrm{~L}_{2}$ | 1100 | 100 | 25 | ${ }_{15}^{1565}$ | 15 | ! | - | - |  |
| 2N1167a | 0 | Mp, N, | 9 | L2 | 100 | 100 | 25 | 150\% | 15 | 1 | = | - |  |
| 211335 | mo | mp,N.e | 90 | 1.2 | 100 | 50 | 3 | 35-90 | 3 | 7 | - | - |  |
| 211350 | mo | mp,Nom | 90 | 12 | 100 | 50 | 3 | 00-140 | 3 | 5 | - | - |  |
| 211362 | ${ }^{0} 0$ | mpanse | 90 | 1.2 | 100 | 100 | 3 | 3590 | 3 | 7 | - | - |  |
| ${ }_{2} 21131363$ | ${ }^{0} 0$ | mpande | ${ }_{90} 9$ | 12 | 100 | 100 | 3 | 60-100 | 3 | 5 | - | - |  |
|  |  |  |  |  | 100 | 120 | 3 | 35.90 | 3 | 1 | - | - |  |
|  | mo | PppN, ${ }^{\text {ce }}$ | 50 | L2 | : 20 | 120 | 3 | 60-100 | 3 | 5 | - |  |  |
| 2N1529A | mo | Pap, N, | 90 |  | 1000 | ${ }_{40}^{40}$ | 5 | ${ }_{20-40}^{20-40}$ | 2 | 10 10 | - | - |  |
| $2{ }^{2} 1530$ | mo | mpando | 90 | 1.2 | 100 | 40 | 5 | 2040 | 2 | 10 | = |  |  |
| 2W1530A | mo | mp,N, $\mathrm{m}^{8}$ | 50 | 1.2 | 100 | $\infty$ | 5 | $20-10$ | 2 | 10 | - | - |  |
| 201531 | mo | prpan, | 5 | 1.2 | 100 | 80 | 5 | 20-60 | 2 | 10 | - |  |  |
| ${ }_{20}^{2015354}$ | \% | pranje | 50 | 1.2 | 100 | ${ }^{80}$ | 5 | 2010 | 2 | 10 | $=$ | - |  |
| 2N1532A | mo | mpNo | 5 | 1.2 | 100 | 100 | 5 | $20=0$ | 2 | 10 |  |  |  |
| 201533 | $\pm 0$ | pmon, ${ }^{\text {a }}$ | 50 | 1.2 | 100 | 121 | 5 | 2040 | 2 | 10 | - | - | TR |
| ${ }_{2011534}^{20154}$ |  | mpanic | 90 | 1.2 | 100 | 40 | 5 | ${ }^{3}-20$ | 2 | 25 | - |  |  |
|  | M0 | pmpand, | \$0 | L.2 | 100 100 | - 0 | 5 | ${ }_{35-10}^{350}$ |  | 25 | = | - |  |
| 2215335 | \% | mpans | 50 | 12 | 100 | $\infty$ |  | ${ }^{35} 70$ |  | 0.5 | $=$ | - |  |
| 2N1536 | mo | mpan | 9 | 1.2 | 100 | $\infty$ | 5 | 35-10 | 2 | 25 | - | - |  |
| 221536 | mo | Prpane | so | 12 | 100 | $\infty$ | 5 | 35-0 | 2 | 2.5 | - |  |  |
| ${ }_{2}^{212153374}$ | mo | RoAND, | 0 | ${ }_{1.2}^{1.2}$ | 100 | 1300 | 5 | 3510 | 2 | 05 | - | - |  |
| $201533^{\circ}$ | mo | mp, $\mathrm{N}^{\text {a }}$ | 90 | ${ }_{2}^{2} 2$ | 100 | 120 | 5 | $35 / 10$ | 2 | 4.5 | - | $\square$ |  |
| 211538 | mo | mpans | so | 1.2 | 100 | $\omega_{0}$ | 5 | 50, 000 | 2 | 4 | - | - |  |
| 2215392 | mo | mand |  | 1.2 | 100 | 40 | 5 | 50.100 | 2 | 4 | - | $-$ |  |
| 2N1550 | \% | mpaje | 50 | ${ }_{1}^{1.2}$ | 100 100 | - | 5 | 50,100 | 2 | : | $=$ | : |  |
| $2 \mathrm{Lls41}$ | mo | $\square_{\text {apone }}$ | ${ }_{50}$ | ${ }_{2}{ }^{2}$ | 100 | $0_{0}$ | 5 | 80-100 |  | : | - |  |  |
| 2 zistia | mo | mpasios | 90 | 12 | 100 | 0 | 5 | 50-100 | 2 | 1 | - | - |  |
| 2015ce | mo | Pro, A), som | so | $1.2$ | $\begin{aligned} & 1000 \\ & 100 \end{aligned}$ | $\left\lvert\, \begin{aligned} & 100 \\ & 100 \end{aligned}\right.$ | 5 | $50.100$ |  | 4 | - | - |  |
| 2 L 1513 | $\pm 0$ | mpanio | 90 | $L^{2}$ | 100 | 120 | 5 | 50, 100 | 2 | 1 | - | - |  |
| $2 \mathrm{2mL54}$ | mo | mpanie | 9 | 12 | 100 | 0 | 5 | 15-150 | 2 | 4 | - | - |  |
| 2015444 | mo | mpancomem | 50 | 12 | 100 | 10 | 5 | \% 150 | 2 | 1 | - | - |  |
| 20125s | mo | mpande | 5 | 12 | 100 | ${ }_{0}^{0}$ | 5 | T-150 | 2 | ! | - | - |  |
| ${ }_{2} 21.546$ | mo |  | 80 | 1.2 | 100 | ${ }_{0}^{0}$ | 5 | cols | 2 | ! | - | - |  |
| 2misica | Mo | mpaic | 50 | 1.2 | 100 | 0 | 5 | 75-150 | 2 | 1 | - | - |  |
| 2 L 1317 | mo | mpa, | 5 | 12 | 100 | 10 | 5 | 7-150 | 2 | 1 | - |  |  |
|  |  | Nopem | ${ }_{80}$ | $\frac{12}{12}$ | 180 | $\left\lvert\, \begin{array}{l\|l\|} 1000 \end{array}\right.$ | 5 |  | 2 | $\stackrel{1}{4}$ | - | - |  |
| 20159 | m | Oma | 0 | 1.2 | 100 | 4 | 15 | 10.30 | 3 | 10 | - | - |  |
| $\left\|\begin{array}{l} 2 \pi 15 \operatorname{sen} \\ 2 \pi 150 \end{array}\right\|$ | $0$ | miNo | $5$ | $\sqrt{12}$ | $100$ | ${ }_{\infty}^{10}$ | $\begin{aligned} & 15 \\ & 15 \end{aligned}$ | $\left\|\begin{array}{c} 90.30 \\ 10.30 \end{array}\right\|$ | 3 | 10 | - | - |  |



| Type No. | Mrg. | Typo | ${ }_{w}{ }^{c}$ | Max. Ratings |  |  |  | Charactaristics |  |  |  |  | Remarks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | w/c | $T_{i}$ | $\begin{gathered} V_{c} \\ v^{\prime} \end{gathered}$ | $\mathrm{amp}$ | ${ }_{\text {fe }}$ | $\begin{aligned} & T_{\infty} \\ & \text { ma } \end{aligned}$ | $\begin{aligned} & \mathrm{f} \\ & \mathrm{cot} \\ & \mathrm{kc} \end{aligned}$ | Powh Gain db | Pown. Out. * |  |
| 2 21550A | mo | pnp,AJ, ge | 90 | 1.2 | 100 | 00 | 15 | 10-30 | 3 | 10 | - | - |  |
| 2N1551 | mo |  | 90 | 1.2 | 100 | 80 | 15 | 10.30 | 2 | 10 |  | - |  |
| 2 21551A | m0 | pnp, $A 1$. ge | 90 | 1.2 | 100 | 80 | 15 | 10-30 | 3 | 10 |  |  |  |
| 2N1552 | mo | pnp,A, ge | 50 | 1.2 | 100 | 100 | 15 | $10-30$ | 2 | 10 |  |  |  |
| 2N1552A | mo | Pnp,AJ.ge | 90 | 1.2 | 100 | 100 | 15 | 10-30 | 3 | 10 | - | - |  |
| ${ }_{2}^{2 N 1553}$ | no | pnp,ALse | 90 | 1.2 | 100 | 40 | 15 | 30-60 | 2 | 6 | - | - |  |
| 2N1553A | Mo | Pmp,A1,ge | 90 | 1.2 | 100 | 10 | 15 | 3060 | 3 | 6 |  | - |  |
| 2N1554 | MO | Pmp,AI,ge | 90 | 1.2 | 100 | 60 | 15 | 30-60 | $?$ | 6 | - | - |  |
| 2N1551A 2N1555 | Mo | mpadige | 90 | 1.2 | 100 | 60 | 15 | $30-60$ | 3 | 6 |  |  |  |
| 2N1555 | mo | pmp,A, $\mathrm{se}^{\text {e }}$ | 90 | 1.2 | 100 | 80 | 15 | $30-60$ | 3 | 6 | - | - |  |
| 2N1555A | mo | mpa,AJ,ge | 90 | 1.2 | 100 | 80 | 15 | 3060 | 3 | 6 | - | - |  |
| 2N1556 | M0 | pnp,AJıse | 90 | 1.2 | 100 | 100 | 15 | 30,60 |  | 6 | - |  |  |
| $\begin{aligned} & 2 N 1556 A \\ & 2 N 1557 \end{aligned}$ | Mo | MPD, $\mathrm{N}^{\text {deg }}$ | 90 | 1.2 | 100 | 100 | 15 | 30-60 | 3 | 6 | - | - |  |
| 2 N 1557 A | mo | mp,A, ge | 90 | 1.2 | 100 | 40 | 15 | $50-100$ | 3 | 6 | - | - |  |
| 2N 1558 | mo | pmp,AJ, | 90 | 12 | 100 |  |  |  |  |  |  |  |  |
| 2 2N1558A | mo | pmp, N, ge | 90 | 1.2 | 100 |  | 15 | 50-100 | 3 | 5 | - | - |  |
| 2N1559 | mo | pmp, $\mathrm{N}_{\text {a }} \mathrm{se}$ | 90 | 12 | 100 | 80 | 15 | 50.100 | 3 | 5 | - |  |  |
| 2N1559A | M0 | pap, $\mathrm{N}, \mathrm{ge}$ | 90 | 1.2 | 100 | 80 | 15 | 50.100 | 3 | 5 | - | - |  |
| 2N1560 | Mo | pmp,adge | 90 | 1.2 | 100 | 100 | 15 | 50-100 | 3 | 5 | - | - |  |
| $2 \mathrm{2N1560a}$ | MO | mapange | 90 | 1.2 | 100 | 100 | 15 | 50-102 | 3 | 5 |  | - |  |
| 2 N 392 | DE | Pnp,AN, ${ }^{\text {e }}$ | 91 | . 8 | 100 | 60 | 5 | - | 0.065 | 6 | - | - |  |
| 2N608 | DE | ppp, $A$, ge $^{\text {c }}$ | 9 | 1.2 | 100 | 40 | 3 | - | 1.065 | 10 | - | - |  |
| 2 N 1159 | DE | MnDAJ, ge | 94 | 0.8 | 100 | 80 | 5 | - | 0.0®6 | 10 | - | - |  |
| 2N1160 | DE | Pnp,A, ${ }^{\text {ce }}$ | 8 | 0.8 | 100 | 80 | 7 | - | 0.065 | 10 | - | - |  |
| 241168 | DE |  | 9 | 0.8 | 100 | 50 | 5 | - | 0.065 | 10 | - | - |  |
| 3 M 49 | M | Pmp,A, | 94 | 1.25 | 100 | 60 | 10 | 50 | 3 | 750 | - | - | Sal volt e $0.15 v$ |
| 3N50 | M ${ }_{\text {M }}$ | pmpanise | 91 | 1.25 | 100 | 80 | 10 | 40 | 3 | 450 | - | - | Sat. voll $=0.15 v$ |
| $\begin{aligned} & 3 N 51 \\ & 3 N 52 \end{aligned}$ | MH | Pmp,AJ, 8 e | 9 | 1.25 | 100 | 40 | 10 | 50 | 3 | 750 |  | - | Sab wolt $=0.15 \mathrm{v}$ |
|  |  | Pmp,AJ, ${ }_{\text {e }}$ | 94 | 1.25 | 100 | 80 | 10 | 40 | 3 | 450 | - | - | Sat volt = 0.15v |
| $\begin{aligned} & \text { 2N574 } \\ & 22574 A \end{aligned}$ |  | pnp, Nıse | 100 | 1.13 | 95 | 60 | 15 | 14 | 7 | 75 | - | - |  |
| 2 21575 | WH | Mmp,A, ${ }^{\text {che }}$ | 100 | 1.13 | 95 | 80 | 15 | 14 | 20 | 75 | - | - |  |
| 2N5/5A | M $\mathrm{HH}^{\text {che }}$ | Pmp, N, $\mathrm{Pmp}, \mathrm{N}, \mathrm{ge}$ | 100 | $\underline{L} 43$ | 95 | 6 | 30 | 25 | 7 | 75 | - | - |  |
| 2N1157 | MH | Pmp, Pmp, AJ, ge de | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | 1.43 1.43 | 95 | 80 60 | 30 | 25 | 20 | 75 | - | - |  |
| 2N1651 | BE | M, ${ }^{\text {d, }}$ |  | 1.4 | 95 | 80 | 30 | 50 | 20 | 15 | - | - |  |
| $2 N 1002$ | BE | Pmp,OJ,ge | 100 | 12 | 110 | 60 | 25 | 30 | 2.0 | - | - | - | Sat, volt $=1.0 \mathrm{v}$ |
| $2 \mathrm{2N1653}$ | ${ }^{\text {BE }}$ | Dmp,ojige | 100 | 1.2 | 110 | 1200 | 25 25 | 30 30 | 20 | - | - |  | Sat volt $=0.5 \mathrm{v}$ |
| 2N1936 | TI | npn,w,si | 100 | 134 | 175 | 120 | 15 | 30 | $\begin{aligned} & 2.0 \\ & 20 \end{aligned}$ | 7 me | - | - | Sat. voll $=0.5 v$ |
| 2 N 1987 | TI | nDPn,MS, Si | 100 | 1.34 | 175 | 80 | 15 | - | 20 | 1 mc |  |  |  |
| PT900 | PSI | non, im, si | 125 | 1 | 150 | 80 | 10 | 3 | 10 | 50 mc | 10 | 100 | hi req, hi power |
| Pr901 <br> 2N1899 | $\begin{array}{\|l\|} \hline \text { PS } \\ \text { PS } \end{array}$ |  | 125 | 1 | 150 | 140 | 10 | 10 | 30 | 50 mc | - | 0 | hi freq, hi power |
| 2N1900 | $\left\lvert\, \begin{array}{l\|l\|} \mathrm{PSS} \\ \mathrm{PSI} \end{array}\right.$ |  | 125 | 1 | 150 | 140 | 10 | 10 | 20 | 50 mc | 10 | 100 | tif freg, it power |
| 214800 |  | non,OM 31 | 125 | 1 | 150 | 140 | 5 | 10 | 20 | 2 mc | - | - | hi frequ, hi power |
| 2N1901 | PSI | nom, DM, $\mathrm{Si}_{1}$ | 125 | 1 | 150 | 140 | 5 | 10 | 20 | 25 mc | - | - |  |
| 2N173 $2 N 174$ | \|DE | pmpajse | 150 | 0.5 | 100 | 60 | 0.5 | - | 0.1 | 10 | - | 20 |  |
| $2 N 174$ $2 N 27$ | DE | mpaj, | 150 | 0.5 | 100 | 80 | 15 | - | 0.1 | 10 | - | 40 | TS, mo, Ti, RCA |
| 21278 | DE | $\begin{aligned} & \text { مnpA AJge } \\ & \text { PnpA } A, g e \end{aligned}$ | 150 | 0.5 0.5 | 100 100 | 40 50 | 15 | - | 0.1 | 10 | - | 20 | MO, TS. TL, RCA |
| $2 \mathrm{MH1}$ |  | mparis |  | 45 | 100 | 50 | 15 |  | 0,1 | 10 | - | 20 | MO, TS, TI, RCA |
| 2 MQ | DE | Pmp, ${ }^{\text {Paj }}$ | $\begin{aligned} & 150 \\ & 150 \end{aligned}$ | 0.5 | 100 | 40 | 15 | - | 0.1 | 10 | - | 20 | MO, TS, TI, RCA |
| 2 mm 3 | DE | pmp, ${ }^{\text {a }}$, $\mathrm{g}^{\circ}$ | 150 | 0.5 | 100 | 50 | 15 15 | - | 0.1 | 10 | - | 20 | MO, TS, TI, RCA |
| 2 LW 11 | TI | pmpA, ge | 150 | 2 | 100 | 40 | 25 | 20.00 | 0.1 | 10 | - | 20 | MO, TS, TI, RCA |
| 2N511A | TI | DMp, $\mathrm{N}_{\text {cese }}$ | 150 | 2 | 100 | 60 | 25 | 20.60 | $5$ | - | - | - | Sa, volt 0.2 LV |
| 2M5118 | TI | Papad ame | 150 | 2 | 100 | 80 | 25 | 20.60 | 5 |  | - |  | Quv |
| 24512 | TI | PMP, N ¢ | 150 | 2 | 100 | 40 | 25 | 20.00 | 5 | - | - | - |  |
| ${ }_{\text {2N5 }}^{2 \times 12 A}$ | T1 | pmpAls | 150 | 2 | 100 | $\infty$ | 25 | 20.0 | 5 | - | - | - |  |
| 225128 | T1 | mp, N, ${ }^{\text {a }}$ | 150 | 2 | 100 | 80 | 25 | $20-60$ | 5 | - | - | - |  |
| 2N513 | TI | mpp, N ,ge | 150 | 2 | 100 | 40 | 25 | 2000 | 5 | - | - | - | Six. volt $=0.4 v$ |
| 226134 | T1 | pepajem | 150 | 2 | 100 | 60 | 25 | $20-60$ | 5 | - |  | - |  |
| 2N5138 | TI | Pmp, Nige | 150 | 2 | 100 | 80 | 25 | 20-60 | 5 | - | - | - |  |
| ${ }_{2}^{21514}$ | TI | pmpajese | 150 | 2 | 100 | 40 | 25 | 20-60 | 5 | - | - | $=$ |  |
| 2M514A | TI | mandse | 150 | $?$ | 100 | $\infty$ | 25 | $20-60$ | 5 | - | - | - | Sak. woll - 0.5 v |
| 2N5148 | TI | pmpajse | 150 | 2 | 100 | 80 | 25 | 20-60 | 5 | - | - | - | Sat. volt = L. $5 v$ |
| 211021 | TI | pmp,adse | 150 | ? | 1200 | 100 | 10 | 30.50 | 2 | - |  | - |  |
| 2 L 1002 | T | Pmp, A, | 150 | 2 | 100 | 120 | 10 | 30-50 | 2 | - | - | - |  |
| 2N1025 2N1100 | DE | PPp, N. | 150 | 0.5 | 100 | 80 | 15 | - | 0.1 | 10 | - | 40 | TS, mo, TI, RCA |
| 2N1507 | TI | Pmanjo | 150 | 0.5 | 100 | 100 | 15 | $\square$ | 0.1 | 10 | - | 40 | TS, MO, RCA |
|  |  | PDPAD, ${ }^{\text {c }}$ |  | 2 | 100 | 100 | 20 | 10 | 10 |  |  | - |  |
| 2M1500 | T | Pap,AD, ${ }^{\text {Pa }}$ | 150 | 2 | 100 | 130 | 20 | 10 | 10 | - | - | - |  |
| 2 L 1981 | $\pi$ | Mp ${ }^{\text {a }}$ | 150 | ? | 100 | 50 | 15 | 50 | 6 | - | - | - |  |
| 24190 | II | рпp, $\mathrm{J}_{1}$ si | 150 | 2 | 100 | $\begin{aligned} & \text { D } \\ & \mathbf{D} \end{aligned}$ | 15 15 | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ | 6 | - | - | - |  |
| WX118ub | WH | пpp, F, si | 150 | 2 | 150 | 50 | 10 | 1000 | 10 | 11 |  | - |  |

## DATA CHERT

Power (concluded)


Special Types

| Typo No. | Mig. | Tyロ | $\cdots$ | Men. Refiegs |  |  |  |  | Cherectopistics |  |  |  | Remerte |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\mathrm{m}_{\mathrm{c}}{ }^{\text {c }}$ | Tij | menc | $V_{\text {c }}$ | $I_{e}$ $\square$ | He | ${ }^{1}$ | MF | Eto |  |
|  | GI GI |  | 1.8 mm | 50 | 100 | 0.83 | 20 | - | 7 | 5 | 16 | 30 | photo |
| 2 l 1312 | GI | npn, A, re | 1.5 mc | 120 | 100 | 1.5 | 75 50 | - | 25 | 3 | 10 | 11 | hist woltape |
| 201322 | GI | ¢п¢AN, | 2 mm 1 mm | 120 50 | 100 | 1.5 | 50 20 | - | 30 40 | 3 5 | 10 16 | 11 30 | lind waltare |
| 2W1310 | GI | mpnajie | 10 mo | 120 | 100 | 1.5 | 50 | - | 30 | 3 | 10 | 11 | photo migh waltere |
| 211393 | CI | PmoAJ, ${ }^{\text {ce }}$ | 3.4 mc | 50 | 85 | Q88 | 20 | - | 160 | 5 |  |  |  |
| 2M139 | GI | Pnp,AJ, er | 1 mc | 50 | ${ }^{6}$ | 0.6 | 10 | - | 50 | 5 | 16 | 30 | photo |
| GT124 | G1 | nppa, $\mathrm{N}, \mathrm{c}^{2}$ | 3 | 150 | 100 | 2 | 40 | - | 7 |  | $\square$ | - | hish volime |
| GT1200 | G1 |  | - | 120 | 15 | 2 | 50 | - | - | 1 | 20 | - | driver |
| 2 N 1408 | CI | pmp,AJ,ge | - | 150 | 100 | 2 | 50 | - | 20 | 3 | 10 | 35 | hit wolage |


| $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ | Mig. | Type | (mm) | T | mw.e | $v$ | I(ma) | 8 m | Rement |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C650 | CT | OMP, $\mathrm{N}, \mathrm{si}$ | 250 | 100 | 2 | 45 | 50 | - | field eftect |
| C681 | CT | PRD, $N$, si | 250 | 160 | 2 | 35 | 50 | - | field effloct |
| C65 | CT | Mnp, N, , s ${ }^{\text {a }}$ | 250 | 160 | 2 | 2 | 50 | - | held effect |
| C653 | CT | pmp, $N$, si | 250 | 160 | 2 | 15 | 50 | - | field effect |
| C610 | CT |  | 250 | 150 | , | 40 | 50 | 250 | field aflea |
| C611 | CT |  | 250 | 100 | 2 | 40 | 50 50 | $\begin{aligned} & 400 \\ & 650 \end{aligned}$ | field eftect fiod effect |
| C613 | CT | mp, N, si | 250 | 100 | 2 | 40 | 50 | 1000 | field eflect |
| C614 | CT | pap, $\mathrm{N}, \mathrm{si}^{\text {si }}$ | 250 | 100 | 2 | 40 | 50 | 250 | field ethect |
| C615 | CT |  | 250 | 100 | 2 | 40 | 50 | 750 | field efloct |
| 2N1671 | GE | Mm, ${ }^{\text {m }}$ | 150 | 140 | - | - | 5 | - | mijuation |
| 271714 | GE | m, si | 450 | 140 | - | - | - | - | mijunction |
| 2 L 15718 | GE | 0n, si | 450 | H0 | - | - | - | - | unijuction |
| 24510 | GE | nen, RU, $0^{\circ}$ | 15 | ${ }_{8}$ | - | 70 | 20 | - |  |

In-prosess festing of sillicon diodes with a Type 575
TEKTRONIX TRANSISTOR-CURVE TRACER

... in research and development
The Type 575 is a versatile precision tool for in-process testing of semiconductor diodes-as illustrated above in the Semiconductor-Device Development Lab of Tektronix. Research Division. Viewing the display on a Type 575, a technician can easily determine the forward conduction characteristics as well as the reverse breakdown-and-leakage of a semiconductor diode prior to sealing, during sealing, and after sealing.
NOTE: Double-exposure waveform photos of the case-sealing operation were taken with control settings at 1 ma/div ( $v$ ) and 0.2 vidiv ( h )-forward direction, upper right-and $20 \mu \mathrm{aldiv}(v)$ and $20 \mathrm{v} / \mathrm{div}(\mathrm{h})$-leverse direction, lower left.

- in other applications

The Type 575 provides 20 -ampere collector displays ( $10-$ ampere average supply current), two ranges of collector supply (0 to 20 volts, 0 to 200 volts), and 2.4 -ampere base supply (positive or negative base stepping).

With a Type 575 , you can plot and measure 7 different transistor characteristics. You can display 4 to 12 curves per family-with input current from 1 microampere/step to 200 200 millivolis/step-in repetitive or single-family presentations. You can select either common-emitter or common-base configurations.

Add a Type 175 Adapter and you extend the range of collector displays 10 times and the range of base supply 5 times.

## Type 575 Calibrated Displays

Vortical Axis-Collector Current, 16 steps from 0.01 ma/div to 1000 maldiv. Pushbuttons are provided for multiplying each current slep by 2 and dividing orizontal Axis-Collector Voir
Horizontal Axis-Collector Voltage, 11 steps from 0.01 v/div to 20 v/div.
oth Axes-Base Voltage, 6 steps from 0.01 v/div to $0.5 \mathrm{v} / \mathrm{dlv}$ Base Current, 17 steps from 0.001 ma/div to $200 \mathrm{ma} / \mathrm{div}$.

Type 573 Transister-Curve Tracer

standards, and speedily accept or reject the transistor under test.

- In production rune

The Type 575-used by itself or with a Type 175 Adapter for increased current capability-is a convenient Quality Control tool for production testing of both PNP and NPN transistors-a simple procedure with Test-Setup Charts of front-panel layout available from your Tektronix Field Enwith arrows, display limits drawn on the seraticule, other with arrows, display limits drawn on the graticule, other time-saving techniques devised by a QC Engineer clearly noted, a production worker can easily change from one test urves displayed on the s-inch crt of the Type 575 with charted

Tekironix, Inc.

- PC. P. Box 500 - Sooverton, Oregon - Thone Mirchell 4-0161 - TWX-BEAV 311 - Cable: TEKTRONIX


 CIRCLE SA ON READER-SERVICE CARD


## HIGH-CURRENT

## ADAPTER AVAILABLE

For measuring high-powered semiconductor devices which exceed the current capabilities of a Type ask, about the Type 175 High-Current Adap:er. Not intended for separate use, the Type 175 depends upon the circuitry and crt of a Type 575 to provide 200 -ampere collector displays, three ranges of collector supply, and 12-ampere base supply-for Current on the Vertical Axis and current on the Vertical Axis and Voltage on the Horizontal Axis.
Type 173 Translator-Curve Tracer High-Current Adapter

HIGH-VOLTAGE TYPE 575
AVAILABLE
Supplied on order from your Tektronix Field Engineer is a special model of the Type 575 Transistorthe Type 575 , the special model provides much higher diode breakdown test voltage (variable from zero to 1500 volis at a maximum current of I milliampere) and also much higher Collector Supply (up 10400 volts, at 0.5 ampere).

For complete specifications of this special model-call your Tektronix Field Engineer.
Type 575 Mod IzeC
.31175 (wicos (0.0. Iaction)
. . for more information about evaluating semiconductor devices with a Type 575 or orher Tekronix fesl Engineer. He will be glad so assist you.

CAREER OPPORTUNTIES NOw enizt of Tektronix in the following fields: Instru. ment dosign, Circuis dosion ond angineoring, Cothode-ray inbes, Electron dovices. For information write to Irving Smith, Profossional Plocement.


| $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ | Mfg． | Type | $\begin{aligned} & i_{0} \\ & \text { nct } \end{aligned}$ | Maximum Roflings |  |  |  |  | Charactoristic： |  |  |  | Swhethiag |  |  |  | Remerks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | （w） | $\begin{aligned} & T_{i} \\ & \text { (c) } \end{aligned}$ | W／c | $v_{c}$ |  | ${ }^{6} 10$ | $1_{\infty}$ | $\begin{gathered} \text { Powr. } \\ \text { Gain } \\ \text { (1) } \end{gathered}$ | Pown． Out w | $\begin{array}{\|l\|} \hline \text { Rise } \\ \text { Time } \\ \mu \mathrm{sec} \end{array}$ | $\begin{array}{\|l\|} \hline \text { Store } \\ \text { Time } \\ \mu \text { sec } \end{array}$ | $\begin{array}{l\|} \hline \text { Sat } \\ \text { Volt } \end{array}$ | $\begin{aligned} & \text { Lew } \\ & \text { Cur } \end{aligned}$ |  |
| 241238 | HU |  | 0．8 | 1.0 1.0 | $\begin{aligned} & 200 \\ & 200 \end{aligned}$ | － | $\begin{array}{\|l\|} \hline 15 \\ 15 \end{array}$ | $\begin{array}{\|l\|} \hline 0.5 \\ 0.5 \end{array}$ | $\begin{array}{\|c\|} \hline 14 \\ 32 \end{array}$ | $\begin{aligned} & 0.1 \\ & 0.1 \end{aligned}$ | Z | ＝ | $\bar{\square}$ | － | － | － |  |
| 201240 | HU | mpp，FJ，si | $1.0$ | 1.0 | 200 | － | $\begin{aligned} & 15 \\ & 35 \end{aligned}$ | $\begin{aligned} & 0.5 \\ & 0.5 \end{aligned}$ | $\left\lvert\, \begin{aligned} & 32 \\ & 16 \end{aligned}\right.$ | 0.1 | － | － | － | － | － | － |  |
| 211241 | HU | pmp，F J，si | 1.0 | 1.0 | 200 | － | 35 | 0.5 | 24 | 0.1 | － | － | － | － | － | － |  |
| 2 L 1242 | HU | Dop，F J，si | 1.0 | 1.0 | 200 | － | 65 | 0.5 | 14 | 0.1 | － | － | － | － | － | － |  |
| 211243 | nu | mpp，FJ，si | 1.0 | 1.0 | 200 | － | E5 | 0.5 | 21 | 0.1 | － | － | － | － |  |  |  |
| 21124 | HU | pmp，FJ，si | 12 | 1.0 | 200 | － | 110 | 0.5 | 14 | 0.1 | － | － | － | － | － | － |  |
| 201073 | 8E | pap， 01.80 | 1.5 | 35 | 100 | 1.5 | 40 | 10 | 206 | 2.0 | － | － | － | － | 1.0 | － |  |
| 2 L 1073 | BE | mp， 01.80 | 1.5 | 35 | 100 | 1.5 | 80 | 10 | 206 | 2.0 | － | － | － | － | 1.0 | － |  |
| 211073 | BE | mp， 01.8 | 1.5 | 35 | 100 | 1.5 | 120 | 10 | 20.6 | 2.0 | － | － | － | － | 1.0 | － |  |
| 8－1085 | BE | mp，DJfe | 1.5 | 60 | 100 | 1.0 | 120 | 10 | 5s | 2.0 | － | － | － | － | 0.75 | － |  |
| $0 \mathrm{CL2}$ | AMP | Pnp，PADT，${ }^{\text {Pe }}$ | 2.5 | 10 | 75 | － | 38 | 1 | 150 | 30 | － | － | － | － | 0. | － |  |
| ${ }_{0}^{0093}$ | AMP | mp，PADT，se | 25 | 10 | 75 | － | ${ }_{4}^{40}$ | 1 | 150 | 30 | － | － | － | － | － | － |  |
| $2 \mathrm{ML518}$ | ${ }_{\text {A }}$ DE | MPD，A，${ }^{\text {made }}$ | 4 | 70 | 15 100 | $\overline{12}$ | 50 | 25 | 150 | 30 100 | － | 40 | 20 | $\overline{7}$ | － | － |  |
| 201519 | DE | mp，AJse | 4 | 70 | 100 | 1.2 | 80 | 25 | － | 100 | － | 40 | 20 | 7 | 0.3 | － |  |
| 2 W1520 | DE | pmp，AJse | 4 | 70 | 100 | 12 | 50 | 35 | － | 100 | － | 40 | 20 |  |  | － |  |
| 2M1521 | DE | pnpAJse | 4 | 70 | 100 | 12 | 80 | 35 | － | 100 | － | 10 | 20 | 7 | 0.3 | － | 3a |
| 201522 | DE | mp， $\mathrm{AJsex}^{\text {d }}$ | 4 | 70 | 100 | 12 | 50 | 50 | － | 100 | － | 40 | 20 | 7 | 0.3 | － |  |
| 2N1523 | DE | mpa，AJse | 4 | 70 | 100 | 12 | 80 | 50 | － | 100 | － | 40 | 20 | 7 | 0.3 | － | 502 <br> Winn．gain of 12 m |
| 2N297 | BE | PRPAJ． | 5 | 35 | 90 |  |  |  |  | 3 | － | － |  | － |  |  |  |
| 20997A | ct | mpAAJe <br> pnp，A | $\frac{5}{5}$ | 12 | $\frac{95}{90}$ | 2.5 | 88 | 5 | － | $\frac{3}{3}$ | ＝ | Z | ＝ | － | 108 | 80 | BE，DE，MO |
| 21375 | CL | mpaje | 7 | － | 98 | 3. | 80 | 3 | － | 3 | － | － | － | － | 1.0 | 80 |  |
| 2M378 | TS | mpajse | 1 | 50 | 100 | 12 | 20 | 5 | 30 | 0.5 | － | － | － | － | 1.0 | － |  |
| 24377 | CL | ppodje | 7 | 5 | 85 | 0.3 | 80 | 3 | － | 5 | － | － | － | － | 1 | 15 | TS |
| 24360 24058 | TS | Pnp，A．se | 7 | 50 50 | 100 | 0.8 | 30 | 5 | － | 0.5 | － | － | － | $-$ | － | 50 |  |
| 2 M59 | TS | mpajage | 7 | 50 | 100 | 0.8 | 80 | 5 | － | 0.5 | － | － | 12 | 12.5 | 0.24 | 30 | CL |
| 210011 | DE | mpajse | 7 | 70 | 100 | 0.1 | 80 | 5 | － | 100 | － | － | 5 | 2 | 0.3 | 3 | 2m1011 Sig．C．，mo |
| 274568 | DE | mpo．AJse | 10 | 91 | 100 | 12 | 40 | 7 | － | 0.065 | － | － | 10 | 5 | － | － | II |
| 2 2M55A | DE | popaj，ec | 10 | 0 | 100 | 12 | 60 | 0.065 | － | 0.065 | － | － | 10 | 5 | － | － | TI |
| 2 L 558 A | DE | mpajse | 10 | 9 | 100 | 1.2 | 80 | 7 | 33 | 0.065 | － | － | 10 | 5 | － | － | TI |
| 211038 | T1 | Pmpajas | 10 | 20 | 100 | 0.21 | 40 | 3 | 33 | 50 | － | － | － | － | － |  |  |
| 2 N 1039 | TI | DnP，AJse | 10 | 20 | 100 | 0.27 | 60 | 3 | 33 | 50 | － | － | － | － | － |  |  |
| 2 W 1010 | TI | PMPAJse | 10 | 20 | 100 | 0.27 | 80 | 3 | 33 | 50 | － | － | － | － | $\square$ |  |  |
| 211358 | DE | mpajse | 10 | 150 | 100 | 2 | 80 | 15 | － | 0.1 | － | 40 |  | 5 | 0.3 | － | IS，TI，RCA，MO |
| 201412 201970 | DE | mpadice | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ | 150 150 | 100 | 2 | 100 100 | 15 | － | 100 | － | 40 | 15 | 5 | 0.3 |  | TS，RCA，MO |
| 214387 | ${ }_{\text {PH }}^{\text {PE }}$ | mapadse | $\left\lvert\, \begin{aligned} & 10 \\ & 12 \end{aligned}\right.$ | 150 | 100 | 2 | 100 | 15 | － | 0.1 | － | － | 10 | 5 |  | － |  |
| 2N3\％ | PH |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.35 |  |  |
| $2 \mathrm{~L} 10 \%$ | TI | MPD，A］${ }^{\text {cee }}$ | 15 | 12.5 | 100 | 0.5 | 60 | 3 | － | 0.1 | 33 | 5 | － | － | － | － |  |
| 2M1006a | II | mpadise | 15 | 150 | 100 | 2 | 100 | 10 | 40 20 | 10 | － | － | － | － | 1.0 | － |  |
| 2210468 | TI | mpados | 15 | 150 | 100 | 2 | 130 | 10 | 10 | 10 | － | － | － | － | － | － |  |
| 201600 | DE | papdja | 17 | 15 | 100 | 0.1 | 80 | 1.5 | 0 | 10 | － | 0.6 m | 3 | $i$ | 0.3 |  |  |
| 201610 | DE | mp，AJse | 17 | 15 | 100 | 0.1 | 80 | 1.5 | － | 10 | － | 0.4 m | 3 | 1 | 0.3 |  |  |
| 241611 | DE | pmpadse | 17 | 7.5 | 100 | 0.1 | 60 | 1.5 | － | 10 | － | 0.4 m | 3 | 1 | 0.3 | － |  |
| 201612 | DE | MPDAS | 17 | 75 | 100 | 0.1 | 60 | 15 | － | 10 | － | $0.4 m$ | 3 | 1 | 0.3 | － |  |
| 2 L 1015 | ${ }_{\text {DE }}^{\text {DE }}$ |  | 25 | 50 150 | 150 | 0.7 | 60 30 | 4.5 | － | $\begin{aligned} & 0.00 \\ & 10 \end{aligned}$ | － | － | 5 | 2 | is | $\square$ |  |
| $2 \mathrm{2m1005a}$ | UH | man，FJ，si |  | 150 | 150 | 1.4 | 60 | 7.5 | 8 | 10 |  |  |  |  |  |  |  |
| 2 L 1015 B | ［1］ | am， FJ ，si | 25 | 150 | 150 | 1.4 | 100 | 7.5 | 8 | 10 |  | － | 5 | 1 | 1.5 | 1 | SE |
| 2 21015C | UH | amm， Fl ，si | 25 | 150 | 150 | 1.4 | 150 | 75 | － | 10 | － | － | 5 | 1 | 1.5 | 8 |  |
| 2210150 | WH | nemorjsi | 25 | 150 | 150 | 1.1 | 200 | 75 | － | 10 | － | － | 5 | 1 | 1.5 | － |  |
| 201016 | UH | men，FJ，Si | 25 | 150 | 150 | 1.4 | 30 | 7.5 | 8 | 10 | － | － | 5 | ， | 25 | 1 | SE |
| 2710164 | WH | mpa，FJ，it | 25 | 150 | 150 | 1.4 | 60 | 7.5 | 1 | 10 | － | － | 5 | 1 | 2.5 | 1 | SE |
| 2010168 | VM | mpmof J，si | 25 | 150 | 150 | 1.4 | 100 | 7.5 | 8 | 10 | － | － | 5 |  | 25 | 1 |  |
| ${ }_{2}^{201 m} 2010$ | \％${ }^{\text {\％}}$ | Apm，F J，si | 25 | 150 | 158 | 1.4 | 150 | 7.5 | 8 | 10 | － | － | 5 | 1 | 2.5 | $!$ |  |
| 2m160 | AMP | aph，FJ，si ${ }_{\text {and }}$ | 200 | ${ }_{30} 150$ | 150 | 1.4 | 200 | ${ }^{7}$ | 8 | 10 0.1 | － | － | 5 | 1 | 2.5 | 8 |  |
| 221656 | AMP | mpo，PADT | 200 | 30 | 50 | － | － | 6 |  |  | － | － |  | － | － | － |  |
| 201669 | AMP | MP，PADT ${ }^{\text {P }}$ | 200 | 30 | 90 | － | － | $\overline{-}$ | 5 | 0.1 | － | － | ＝ | － | － | － |  |
| 0 CzS | AMP | Ma，PADT | 200 | 13 | 90 | － | 80 | 6 | 32 | －100 | － | － | － | $=$ | － | － |  |
| OC3s | AMP | Map，PADT ${ }^{\text {and }}$ | 200 | 13 | 50 | － | 60 | 5 | 50 | $\leqslant 100$ | － | － | － | － | － | － |  |
| 0035 |  | －a．mots | 20 | 13 | 90 | － | 60 | 6 | 50 | $\leqslant 100$ | － | － | － | － | － | － |  |
| 20118 | 㫙 | PMP，PADT | 200 | ${ }_{50}^{13}$ | 100 | 12 | $\infty$ | 6 | 70 | ＜100 | － | － | － | － | － | － |  |
| 2420 | BE | papajs | 400 | 60 | 100 | 12 | 100 | 1 | 60 | 1.0 1.0 | ＝ | － | 15 | $=$ | 0.5 | － |  |
| 2 mc 2 OA | 嫄 | pmode | 400 | 60 | 100 | 12 | 90 | 15 | 60 | 1.0 | － | － | is | － | 0.5 | － |  |
| 2 m 37 | BE | 昒A了 | 400 | 60 | 100 | 12 | 60 | d | 15 | 1.0 | － |  | － | － | 4.7 | － |  |

## reliability <br> in <br> volume...

## CLEVITE TRANSISTOR



# How to select power transistors 

by RICHARD F. MOREY, JR.<br>Monager, Applications Engineering, Clevife Transistor<br>Division of Clevite Corporation

A basic understanding of the interrelationship of transistor design parameters facilitates selection of the most advantageous unit for a given application.

Transistor characteristics depend upon each other. Consequently, a design change in the manufacture of a transistor directly affects a number of its electrical characteristics.
As a guide to users of power transistors, several of the important design elements and the electrical characteristics they influence have been summarized in chart form (fig. 1).

The curves (figs. 2-5), show typical characteristics for two power transistors of quite different design. Clevite's 2 N 1762 , for example, is a 3 ampere unit having the following design parameters: Small junction area; high resistivity germanium; moderate germanium lifetime; average wafer thickness and no emitter doping.

In contrast, Clevite's 2 N 1146 C is a 15 ampere power transistor which has several quite different parameters based upon a higher current and power requirement; large junction area several times the size of the 3 ampere unit; identical base width and resistivity but longer germanium lifetime and thicker wafer plus aluminum doping to increase emitter efficiency.

Working with the chart in figure 1 and the table, figure 6 , we see that the comparative design elements of


Effect of Transistor Design on Characteristics

| DESIGM PARAMETEA |  | Increase in Wafer Thictroess | heduction in GE matorial lifetime | Increase in Ce material resistivity | Retuction in Bese Widih | Incresse in Nunction Arse |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PMEGMAL MESISTAMCE R, | - | - | - | - | - | decrease |
| COLLECTO LEAKACE CURAENT laso $\qquad$ | - | tecrease | increasa | increaso | - | incresse |
| COLLECTOR <br> BASE <br> VOLTAGE <br> VCa <br> COI | - | - | - | incrasest | - | decresse slightly |
| COLLECTOA EMITIER VOLTAGE $V_{a}$ | decrease | - | increase | increase | decreasa | dacrease slightly |
|  | increase | - | decrease | - | increase | - |
| Linesitity of hes | better | - | - | - | - | better |
| SATURATION VOLTAGE Vesisat | decrease | decrease | increase | increase | decrase | encrease |
| beta cutorf FREOUENCY fos | dacrease | - | incrosso | - | incrosso | decresse |
| PUNCH <br> THROUGH <br> VOLTAGE <br> VPI | - | - | - | decresse | cocriase | - |
| SECONDATY <br> BREAKODWH <br> CURRENT <br> I | increase | increase | - | decrease | - | incosase |

Figure 1.
the two transistors result in the 15 ampere unit exhibiting: - lower thermal resistance and higher leakage currents because of its large junction area.

- slightly lower collector to base voltage.
- higher gain because of the emitter doping and higher lifetime.
- very linear current gain out to high currents because of its large area and special emitter doping.
- lower collector to emitter breakdown voltages because of its higher gain and lower collector to base voltage.
- much lower saturation voltage and base input voltage because of its high gain and thicker wafer and larger area.
- low common emitter frequency response because of its high gain and large area.
Comparison of Characteristics - Two different designs

| Characteristic | 2N1762 Typical Value 3 Amp. Device | 2N1146 <br> Typical $V$ <br> 15 Amp. D | Units |
| :---: | :---: | :---: | :---: |
| Thermal Resistance | 1.4 | 0.5 | ${ }^{\circ} \mathrm{C} /$ wall |
| levo at loov at $85^{\circ} \mathrm{C}$ | 3 | 15 | mA |
| leoo at 100 V at $25^{\circ} \mathrm{C}$ | 1 | 4 | mA |
| BVemo | 130 | 120 | Volts |
| $V_{\text {ciolme) }}$ | 70 | 50 | Volts |
| Current Gain at $I_{\mathrm{c}}=1$ Amp. | 60 | 220 |  |
| Current Gain at $1_{c}=5 \mathrm{Amps}$. | 15 | 140 |  |
| Current Gain at $l_{c}=15 \mathrm{Amps}$. | S. | 75 |  |
| Saturation Voltage at 3 Amps . | 0.3 | 0.2 | Volts |
| Saturation Voltage at 15 Amps. | . - | 0.4 | Volts |
| Saturation Resistance | 100 | 26 | Milliohms |
| Frequency Cutoff at 1 Amp. | 18 | 4 | kc. |

Figure 6
In order for circuit designers and users of power transistors to obtain the best combination of electrical characteristics, the requirements for the application must be well known and be matched to the transistors available on the market. Therefore, an elementary knowledge of the existing relationships between transistor characteristics is a useful design tool. A tabular summary of characteristics for Clevite's complete line of power transistors is available. Ask for Bulletin 61-A.

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## Abbreviation of Terms

AJ

DJ
DM

Epitaxial
Fused Alloy
Fused Junction
Grown Diffused
Germanium
Grown Junction
Grown Rate
Meltback
MADT
Mesa
Rate Grown
Silicon
SBT Surface Barrier
$\mathbf{C}^{\text {. }}=$ Collector-to-emitter capacitance meas ured across the output terminals with the input ac open-circuited.
$\mathbf{f}_{\mathrm{se}}=$ Frequency at which the magnitude of the forward-current transfer ratio (small-signal) is 0.707 of its low-frequency value
f = Frequency at which common emitter gain is unity
$\mathbf{h}_{\text {. }}=$ Common emitter-small signal forward current transfer ratio.
$\mathbf{h}_{v k}=$ Common emitter-static value of short circuited forward current ratio.

Ivu = Collector current when collector juncion is reverse-biased and emitter is dc open-circuited.

If you would like an additional copy of the Transistor Data Chart Section circle 251 on the Reader-Service Card (Quantity prices on request)

High Level (continued)

| $\begin{gathered} \text { Type } \\ \text { No. } \end{gathered}$ | Mis. | Typo | 1 | Man. Retings |  |  |  |  | Charactorititics |  |  |  | Swirehing |  |  |  | Remomin |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | ${ }^{c}$ <br> (w) | - ${ }^{1}$ | c w'e |  | $\begin{aligned} & 1_{c} \\ & 1 \end{aligned}$ | $\mathrm{n}_{\text {le }}$ | $\begin{aligned} & \hline 1_{c o} \\ & \text { ma } \end{aligned}$ | $\begin{aligned} & \text { Powra } \\ & \text { Gain } \\ & \text { in } \end{aligned}$ | $\begin{gathered} \text { Powto } \\ \text { oul } \\ w \end{gathered}$ | $\begin{aligned} & \hline \text { Rise } \\ & \text { Time } \\ & \text { Usec } \end{aligned}$ | $\left\lvert\, \begin{aligned} & \text { Sior } \\ & \text { Time } \\ & \mu \mathrm{sec} \end{aligned}\right.$ | $\left[\begin{array}{l} \mathrm{S}_{2} 2 \mathrm{~L} \end{array}\right.$ | $\left[\begin{array}{c} \text { Lisik } \\ \text { Out } \end{array}\right.$ |  |
| 2296374 | BE | pmo, AJ, ge | 400 | 60 | 100 | 1.2 | 90 | 6 | 45 | 1.0 | - | - | - | - | 0.7 | - |  |
| 2N637B | BE | pmp,A).g | 400 | 60 | 100 | 12 | 100 | 6 | 45 | 1.0 | - |  |  |  | 0.7 | - | CL |
| 2M638 | BE | map,Alse | 400 | 60 | 100 | 1.2 | 60 | 6 | 30 | 1.0 | - | - | - | - | 0.7 | - |  |
| 2m6384 | BE | mpalse | 400 | 60 | 100 | 12 | 90 | 6 | 30 | 1.0 | - | - | - | - | 0.7 | - |  |
| 206388 | BE | pmp,AJse | 400 | 60 | 100 | 1.2 | 100 | 6 | 30 | 1.0 | - | - | - | - | 0.7 | - |  |
| $2 \mathrm{NG75}$ | PH | pnp,A, ge | 400 | 1 | 85 | 16.7 | 75 | 2 | 40 | 100 | - | - | - | - | 0.35 | - | Infinite heat sink |
| 2 N456 | TI | pmp,AJse | 430 | 50 | 100 | 0.67 | 40 | 5 | 30-90 | 02 | - | $-$ | 12 | 12.5 | 0.24 | 30 | RCA |
| 2 M 55 | TI | pap A).ge | 430 | 50 | 100 | 0.67 | 60 | 5 | 30-90 | 0.6 | - | - | 12 | 12.5 | 0.21 | 30 | RCA |
| 2 Tm 71 | PH | Pap,AJ.ge | 700 | 1 | 8 | 0.017 | 40 | $?$ | 100 | 20 | - | - | $-$ | - | - | - | Infinite heat sink |
| STCLICS | STC | npa, DJ,si | 1 lic | 85 | 200 | 0.125 | 60 | 6 | 25-75 | 0.025 | - | - | - | - | - | - |  |
| STCIIOA | STC | npn, DJ,si | 1ma | 85 | 200 | 0.425 | 100 | 6 | 25.75 | 0.025 | - | - |  |  | - | - |  |
| ${ }_{2}^{20673}$ | PY | PDPAJ, | 1.1 mc | 0.3 | 85 | 5 | 75 | 2 | 160 | 40 | - | - | 0.5 | 0.4 | 0.2 | - | Infinite heat sink |
| 20124A | STC | non, DM, ${ }^{\text {ai }}$ | 2 ac | 85 | 200 | 0.4 | 60 | 3.5 2.5 | 12.60 20.80 | 10 | - | - | - | - | - | - | SE |
| 2N178 | STC |  |  | 25 7 | 200 | 0.125 0.375 | 60 | 2.5 5 | 20.80 15.60 | 0.1 0.2 | $=$ | 2 | - | - | $=$ | - |  |
| 211768 | STC | npon, DM, si | 2 | 40 | 200 | 0.2 | 80 | 3 | 35-100 | . 015 | - | - | - | - | - | - |  |
| 241769 | STC | npon,0M, ${ }^{\text {a }}$ | , | 40 | 200 | 0.2 | 100 | 3 | 35-100 | . 015 | - | - | $\square$ | - | - | - |  |
| 2 21620 | STC | npn,0m,si | 2 mc | 85 | 200 | 0.45 | 100 | 5 | 15.51 | 1 | $\square$ | - | - | - | - | - |  |
| 21551 | TR | npm,01.si | 3nc | 3 | 200 | 0.5 | 60 | - | 20-80 | 1.2 | - | - | 1.2 | 0.3 | 0.9 | - |  |
| 26552 | TR | npm, $0 \mathrm{O}, 31$ | 3 nc | 3 | 200 | 0.5 | 30 | - | 20-80 | 12 | $-$ | - | 1.2 | 0.3 | 0.9 | - |  |
| 201055 | TR | npm, $\mathrm{DJ}, \mathrm{si}$ | 3 | 3 | 200 | 0.015 | 100 | - | 20.80 | 0.001 | - | - | - | - | $\square$ | - |  |
| 24547 | TR | npon, DJ, 31 | 4 Am | 5 | 200 | 0.5 | 60 | $\cdots$ | 20-80 | 1.2 | - | - | 0.7 | 0.2 | 3.0 | - |  |
| $2 \mathrm{LS54}$ | TR | nom, DJ,si | anc | 5 | 200 | 0.5 | 30 | $=$ | 20.80 | 0.5 | $=$ | - | 0.7 | 0.2 | 2.0 | - |  |
| $2 \mathrm{TH549}$ | TR | nmm, $\mathrm{DJ}, \mathrm{si}$ | 4 frc | 5 | 200 | 0.5 | 60 | - | 20-80 | 0.5 | - |  | 0.7 | 0.2 | 1.5 |  |  |
| 2W550 | TR | npm, DJ,si | Inc | 5 | 200 | 0.5 | 30 | - | 20-80 | 0.5 | - | - | 0.1 | 0.2 | 1.5 | - |  |
| 241117 | TR | npm, $\mathrm{D}, \mathrm{si}$ | Anc | 5 | 200 | 0.5 | 60 | - | 10 | 0.04 | - | - | 0.7 | 0.2 | 1.5 |  |  |
| 241115 | TR | npm, DJ, si | 6 mac | 5 | 200 | 0.5 | 60 | 0 | 40 | 1.2 | - | - | 0.7 | 0.2 | 3.0 | - |  |
| 291173 | WE | npm, $, \mathrm{J}, \mathrm{se}$ | ${ }_{6}^{6 m c}$ | - | 100 | 3.33 | 35 | 0.2 | 80 | 0.001 | - | $=$ | $\overline{7}$ | - | - | - |  |
| ST40 | TR |  | 6 fax | 50 50 | 200 | 0.33 | 60 | 3 | 30 | 20 | - | $=$ | 0.25 | 0.5 | 6 |  |  |
| ST400 | TR | npm, $\mathrm{DJ}, \mathrm{si}$ | 6 mc | 50 | 200 | 0.33 | 45 | 3 | 30 | 20 | - | - | 0.25 | 0.5 | 5 | - |  |
| 211174 | WE | pnp,AJ,ge | 7 mc | - | 100 | 3.33 | 35 | 0.2 | 85 | 0.005 | - | - | - | - | - |  |  |
| $2 \mathrm{SH55}$ | TR | nonojosi | bac | 5 | 200 | 0.5 | 60 | - | 15 | 12 | - | - | 0.3 | 0.15 | 3.0 | 25 |  |
| 27546 2 21052 | TR | npn, $0 \mathrm{~J}, \mathrm{si}$ | 8 mc | 5 | 200 | 0.5 | 30 | - | 15 | 0.5 | - | - | 0.3 | 0.15 | 2.0 | - |  |
|  | TR | npa, DJ, ${ }^{\text {i }}$ | ima | 5 | 200 | . 012 | 60 | 500 | 15 | 0.001 | - | - | - | - | - | - |  |
| $2{ }^{2} 212$ | TR | non,0J, 31 | 10ac | 85 | 200 | 0.27 | 60 | 3000 | 12.60 | 1000 | - | - | - | - | 3.5 | - |  |
| 21251054 201208 | TR | npm, DJ, si | 12mc | \% | 200 | . 017 | 125 | - | 20-80 | . 0001 | - | - | - | - | \% | - |  |
| 211208 | TR | npm, DJ, si | 12 mc | 85 | 200 | 0.27 | 60 | 5 | 15 | 1.0 | , | - | 0.25 | - | 3 | - |  |
| 211209 2 L 1250 | TR | nmon, $\mathrm{DJ}, \mathrm{si}$ | 12 mc | 85 | 200 | 0.27 | 45 | 5 | 20 | 2.0 |  | - | 0.25 | - | 3 | - |  |
|  | TR | nma, 0 ¢ 51 | 12 mc | 85 | 200 | 0.21 | 45 | 5 | 20 | 2.0 | - | - | 0.25 | - | 3 | - |  |
| $\begin{aligned} & 2 \mathrm{~N} 1072 \\ & 2 \mathrm{~N} 101 \end{aligned}$ | WE | npn,DD,s1 non,A1.se | $\begin{aligned} & 30 \mathrm{mc} \\ & \hline \end{aligned}$ | $\begin{aligned} & 12 \\ & 20 \end{aligned}$ | $\begin{aligned} & 150 \\ & 100 \end{aligned}$ | $\begin{aligned} & 65 \\ & 0.27 \end{aligned}$ | $17$ | 3 | 13 33. | 0.1 50 | - | - | 0.05 | 0.05 | - | - | US, ML anly |
| RT 497M | RH | nponod, 01 | 50 | 3 | 175 | 0.0 | 60 | 0.5 | ${ }_{20}^{33 .}$ | So | - | - | - | - | - | - |  |
| RTAgem | RH | non,00,si | 50 | 3 | 175 | 0.0 | 100 | 0.5 | 20 |  |  | - | - | = | = | - | Miciobloc T0.46 |
| 2W92 | FA | men, DP, si | $60^{\circ}$ | 1.8 | 200 | 0.01 | 80 | - | 30 | 0.00518 | - | - | - | = | - | - |  |
| 2N1975 | FA | npm, $\mathrm{OP}, \mathrm{si}$ | $600^{\circ}$ | 3 | 200 | 0.017 | 80 | - | 30 | $0.005{ }^{103}$ | - | - | - | - | - | - |  |
| 211978 | FA | npmopesi | ${ }^{600}$ | 30 | 200 | 0.17 | 40 | $=$ | 40 | $0.001 / 10$ | - | - | = | = | - | - | -19 |
| 231585 | FA | npm, DM M,si | 600 | 2 | 150 | 0.0016 | 35 | - | 30 |  | - | - | - | - | - | - | ${ }^{19}$ |
| 2N1989 | FA | npon, DM, ${ }^{\text {a }}$ | $60^{\circ}$ | 2 | 150 | 0.001 | 60 | - | 40 |  | - | - | - | - |  | - |  |
|  | RH | npn,DD,s1 | 60 | 3 | 175 | Q.Q | 60 | 0.5 | 60 | - | - | - | - | - | - | - | Microbloc |
|  | $\begin{gathered} \text { RH } \\ R H \end{gathered}$ |  | 60 60 | 3 5 | 175 | 0.0 | 100 | 0.5 | 60 50 |  | - | - | $\pm$ | - | - | - | Miciobloc |
| RT5230 | RH |  | 60 | 2 | 175 | 0.003 | ${ }_{30} 17$ | 0.5 0.5 | 50 50 | 0.001 | $=$ | - | - | = | = | : |  |
| 2 N 21 | FA | mmp, $\mathrm{DPP}^{\text {a }}$, ${ }^{\text {a }}$ | $10^{\circ}$ | 1.5 | 175 | 0.01 | 50 | - | 35 | 0.044 | - | - | - | = | - | - |  |
| 211131 | FA | pmp,DP, 31 | $70^{\circ \mathrm{mc}}$ | 2 | 175 | 13.3 | 50 | - | 35 | 0.01 | - | - | 0.08 | = | - | 5 | OTTHU, TI, TR |
| 2011987 | FA | nmon, 01.81 |  | 2 | 150 | 0.0016 | 40 | - |  | - | - | - | - | - |  |  |  |
| ${ }_{2}^{24.69 \%}$ | FA | npn, DP, 3i | $80 / 7$ | ${ }^{2}$ | 175 | 13.3 | 40 | - | 40 |  |  | $\underline{-}$ | 0.00 | 0.03 | - |  | SSO, TR, SY, MA, TI. |
| 2469 | FA | n@m, DP, $\mathrm{si}^{1}$ | $80(1)$ |  | 175 | 13.3 | 80 | - | 30 | 0.01 | - | - | 0.08 | 0.05 | = | - | SH, TR,'MA, GI, SSO. |
| 21717 | FA | nmm, DP sil | 800(t) |  | 175 | 10 | 80 | - | 30 | 0.01 |  | - |  | - | - |  | GI. HO, PSI, RH, MA |
| 201719 | FA | npon, DP, si | $80(15)$ | 1.5 | 175 | 10 | 80 | - | 30 | 0.01 | $\pm$ | - | 0.08 | $\overline{=}$ | = | - | PSI, RM, GI RH, |
| 211252 | FA | npn,0Psi | $80(1)$ |  | 175 | 13.3 | 20 | - | 35 | 0.1 | - | - | 0.08 | 0.05 | - | - | $\begin{aligned} & \text { TR, GI, IND, PSI, TI, } \\ & \text { RH } \end{aligned}$ |
| 217190 | FA | npn, DP, si | ${ }^{80}$ | 1.8 | 200 | 0.01 | 80 | - | 45 | 0.0001, |  | - | - | - | - | - |  |
| 27870 | FA | npm, DP, si | ${ }^{80}$ | 1.8 | 200 | 0.01 | 80 | - | 80 | 0.0001 | - | - | - | - | - | - | ${ }^{4} \mathrm{~T}$ |
| 241613 | FA |  | ${ }_{80}^{80}$ | ${ }_{3}^{1.8}$ | 200 200 | 0.01 | 80 50 | - | 70 80 | ${ }^{0} 0005$ |  | Z | $0 \times$ | - | - | - |  |
| 210189 | FA | nma, DP , $\mathrm{sic}^{\text {a }}$ |  | ${ }^{3}$ | 200 | 0.017 | ${ }_{80}$ | - | 880 | 0.000 |  | - | 0.08 | - | - | - | OTRM |
| 2 L 1893 | FA | npm, DP, si | $80^{\circ}$ | 3 | 200 | 0.017 | 100 | - | 80 |  |  | - | - | - |  |  |  |
| 201974 | FA | non, DP, si | 80 |  | 200 | 0.017 | 180 | $=$ | 70 | 0.006 |  | Z | - | = | = | $=$ | -19 |
| 2N1984 | FA |  | $80^{\circ}$ | 1 | 150 | 0.0016 | 83 | - | 70 |  | - | - | - | - | - | - | -19 |
| 211991 | FA | MPD.OM, Si | $80{ }^{\circ}$ | 1 | 175 | 0.005 | 20 | $\overline{0}$ | 45 |  |  | - | - | - | - | 1 | ${ }^{\circ} 9$ |
| RT482 | RH | npm, DD,si | $\infty$ | 2 | 175 | 0.013 |  | 0.5 | 50 |  |  | - | - | - | - | - |  |
| RT483 | RH | nmo, DD,si | 80 | $?$ | 175 | 0.013 | 40 | 0.5 |  |  | - | - | - | - | - | - |  |
| RTAM | RH | nmm, DD, 31 | 80 | 2 | 175 | 0.013 | 10 | 0.5 | 70 | 0.0 | - | - | - | - | - | - |  |
| RTSSSM | RH | nom, DD, 3 | 80 | 3 | 175 | 0.12 | 50 | 0.5 | 40 | 0.008 |  |  | - | - | - | - | Macoblec |

High Level


For an additional copy

| (concluded) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IPharastarisics sminening |  |  |  |  |  |  |  | Romek |
| nh | $\begin{aligned} & I_{\infty} \\ & m 0 \end{aligned}$ | $\begin{array}{\|c} \begin{array}{c} \text { Pawn } \\ \text { Gain } \\ \infty \end{array} \end{array}$ | $\begin{array}{\|c\|} \hline \text { Pomer } \\ \text { Oot } \\ \hline \end{array}$ | $\begin{array}{\|l\|l} \hline \text { Rive } \\ \text { Time } \\ \text { usec } \end{array}$ | $\begin{array}{\|l\|} \hline \text { Stor } \\ \text { Time } \\ \mu \text { seec } \end{array}$ | $\begin{array}{\|c} \hline \text { Sat } \\ \text { Voll } \end{array}$ | $\left\|\begin{array}{c} \text { Leaw } \\ \text { Out } \end{array}\right\|$ |  |
| 40 | 0.01 | - | - | - |  | - |  | Micobloc |
| 60 | = | - | - | $=$ | Z | $z$ | = |  |
| 70 | = | - | - | - | = | - | : |  |
| 70 | - | - | - | - | - | - | - |  |
| 50 70 | 0.01 m | = | - | $=$ | - | $=$ | $=$ | ${ }_{4}{ }^{4}$ |
| 15 | - | 18 | 0.00 | 0.05 | - | - | - | TSD, SY, MA, 61 TI, INO, PSI, HO, |
| 65 | 0.01 | - | - | 0.08 | - | - | - | NA, TR, SSO, GI, <br> PSI, TI, RH |
| ${ }_{80}^{75}$ |  | - | - | 0.08 | - | - | - | M4. GI, MO, PJI, RH |
| 80 85 80 |  |  | - | 0.08 | - | $=$ | - |  |
| 80 30 |  | - | - | 0.11 | 0.14 | 0.9 | - |  |
| 60 | 0.01 | - | - | 0.11 | 0.14 | 0.9 |  |  |
| 130 150 | 0.000 | - | - | O.1. | O.1. | - | - | ${ }_{1}$ |
| 110 | 0.0081 | - | - | - | - | - | $=$ | \% ${ }_{4}$ |
| 10 | 0.001 m | - | - | - | - | - | $=$ | का |
| 50 45 | 0.01 | - | - | 0.08 |  | - | - | HU. TI, TR |
| 45 | 0.01 | - | - | 0.08 | 0.05 | - | - | Tr. Mid, GI, PSI, |
| ${ }_{25}^{130}$ | 0.01 | - | - | - | - | - | - |  |
| 138 130 | 0.0004 |  | $\bar{\square}$ | - | - | $\square$ | - | ${ }^{\text {9T }}$ |
| 130 | 0.0001 | - | - | - | - | - |  |  |
| 150 100 | 0.01 0.005 |  | = | $=$ | - | $=$ | $=$ | 41 |
| 110 |  |  | - | = | - | - |  | ${ }_{4}^{4}$ |
| 120 | - | - | - | - | - | $=$ | = | \% |
| 10 10 | 0.0003 | - | - | - | - |  |  |  |
| 10 70 | 0.000 | - | - | - | = | - | $=$ | Micabloc |
| 70 | 0.001 | - | - | $\overline{-}$ |  | - | - | Wicablox |
| 65 | 0.01 | - | - | - | - | - | - | Wrabloc |
| ${ }_{4} 4$ | 0.001 | - | - | $\bar{\square}$ | $\bar{\square}$ | - | - | Micrabloc |
| 60 | 0.1 | - | - | 0.1 | 0.0 | 1.3 | - |  |
| 40 60 | 0.1 | - | - | 0.1 | 0.15 | 13 | - |  |
|  |  |  |  |  | 0.2 | 13 | - |  |
| 15 | 0.000 |  | - | - | $\overline{-}$ | - | - | Marobloc <br> 4 |
| $\begin{aligned} & 30 \\ & 10 \end{aligned}$ | $\begin{aligned} & 10.05 \\ & 0.06 \end{aligned}$ | ${ }_{10}$ | 1 | 0.06 0.002 | $0.1$ | 0.8 | $=$ | Poumer gin Fa70mRH |
| 60 | 10 | 1 | 1 | 0.002 | 0.11 | 0.8 | - | RH |
| 6.5 50 |  |  | - | 0.0 | 0.17 | - | - |  |
| $\begin{aligned} & 50 \\ & 70 \end{aligned}$ | 0.0003 0.0003 |  |  | - |  | - | Z | ${ }_{6} \%_{1} 61$ |
| 80 50 | 0.00029 0.0000 |  | - | - |  | - | - |  |
| 5 |  |  | - | - | - | - | - | 4. Epilaxial |
| 12 | ${ }_{10}$ | Z | - | Z | $=$ | - | 50 | BE. 2M639 |
| ${ }_{30}^{12}$ | 10 | $=$ | - | - | $=$ | = | - |  |
| 30 | 10 | - | $\square$ | - | - | - | $=$ |  |
| ${ }^{0}$ | - | - | - | - | - | - | - |  |
| 50 | - | - | - |  |  | : | $=$ |  |

Pe Transistor Data Chart
ard and circle 251.
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## stluanla Pailcake tranisitoins

Increased packaging density! Mil-min .100" lead-to-lead spacing!
Now available in - Epitaxial Germanium Mesa - Epitaxial Silicon Mesa
Germanium Alloy-Junction - Germanium Drift-Field
$100^{\sim}$ lead-to-lead apacing for automatic and direct insertion in Mil-atandard 273A printed circuit without reforming leads - mechanically indexed for ponitive and
permanent lead identification- eliminate solder bridging problems. $070^{" \prime}$ max cane height - 255" max. cane diameter - power dixsipation in free air: 300 mw fur Mesa, 100 mw for Alloy and Drift-Field units - max. junction temperature: $100^{\circ} \mathrm{C}$ for Germanium and $175^{\circ} \mathrm{C}$ for Siticon eneet all environmental texts in
accordance with Mil-S-19500R . hermetic seal reliability ( leak rate lower than

Sylvania originated the "Pancake" package to provide a practicable solution to a vital engineering challenge-end-product miniaturization with high operational reliability. The tabulation of 15 types is a clear indicator of the industry's acceptance of the "Pancake" package
If you are working with microminiacurization to improve "payload factors" or to enable "redundancy for reliability," call in your Sylvania Sales Engineer now. to help you determine the best device for your specific requirements. He or your Sylvania franchised Semiconductor Distributor can provide you with "Pancake" transistors-fast!' For tech data on specific types, write Semiconductor Division, Sylvania Electric Producta Inc., Dept. 187, Woburn, Mass.


##  <br> CIRCLE 58 ON READER-SERVICE CARD

## 6

## Low Level

| $\begin{gathered} \text { Type } \\ \text { No. } \end{gathered}$ | M/9. | Type | 'a. | Mailmum Ratinga |  |  |  |  | Charectaristics |  |  | Suirching |  |  |  | Romatk |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & w_{c} \\ & (\mathrm{~mm}) \end{aligned}$ | $\begin{array}{\|l\|} T_{i} \\ (c) \end{array}$ |  | $v_{c}$ | $\begin{aligned} & I_{c} \\ & m a \end{aligned}$ | $\begin{aligned} & m_{e} \\ & n_{F E} \end{aligned}$ | $\left.\right\|_{c o}$ | $\left\lvert\, \begin{aligned} & c_{c o e} \\ & \mu \mu 1 \end{aligned}\right.$ | $\begin{aligned} & \text { Rise } \\ & \text { Time } \end{aligned}$ | $\begin{aligned} & \text { Stor } \\ & \text { Time } \end{aligned}$ | $\begin{array}{\|c\|} \text { sal } \\ \text { voll } \end{array}$ | $\begin{aligned} & \text { Leak } \\ & \text { Cul } \end{aligned}$ |  |
| 21327 | CT | $\mathrm{mp}, \mathrm{A}, \mathrm{si}$ | 02 | 250 | 160 | 3 | 10 | 5 | , | . 005 | 70 |  | - |  | - |  |
| 210304 | RA | mi FA , | 0.2 | 250 | 1150 | - | 40 | 50 | 15 | ${ }^{5}$ | 70 | - | $=$ | - | $=$ | SSO |
| $\underset{\substack{211235}}{2125}$ | $\stackrel{\text { RA }}{\text { RA }}$ | Mmp.FA, si | 0.25 | ${ }_{250}^{250}$ | 160 180 | St | ${ }_{35} 8$ | 100 | ${ }_{30}$ | . 5 | ${ }_{70}$ | - | - | - | - | SSO. MA |
| 2331 | CT | mp, $\mathrm{N}, \mathrm{si}$ | 0.3 | 250 | 160 | 3 | 35 | 50 | 28 | . 05 | 0 | - | - | - |  |  |
| 21105 | RA | mp.FA, si | 0.3 | 250 | 160 |  | 35 | 50 | 30 | 5 | 0 | - | - | - | - | SSD, MA |
| 211006 | ${ }_{\text {RA }}^{\text {RT }}$ | mp.FA, ${ }^{\text {a }}$ | 0.4 | 250 | 160 |  | 30 | 50 | ${ }^{60}$ | 5 | 70 | - | $=$ |  |  | SSD. MA |
|  | CT | pmp.N, ${ }^{\text {a }}$ | 0.4 | 250 | 180 | $?$ | 20 | 50 | 11 | col | 5 | - | - |  |  |  |
| ${ }_{C} 101$ | CT CT | mpo | 0.4 | 250 250 | ${ }_{160}^{160}$ | ${ }_{2}^{2}$ | ${ }_{70}^{20}$ | 50 | 1 | 5 | 50 | - | $=$ | - | - |  |
| 2 N329 | cT |  | 0.5 | 250 |  |  |  |  | co |  |  |  |  |  |  |  |
| ${ }_{21329}$ | RA | mmo.fi,si | 0.5 | 385 | 160 | - | 30 | 50 | 60 | 005 | 0 | - | = | 5 | - |  |
| $2 \mathrm{mmos7}$ | GE | mmonj.se | 0.5 | 240 | 100 | 1 | 15 | 300 | is | 300 | 10 | - |  | 0.08 | 58 |  |
|  | ${ }_{\text {PH }}$ |  | 0.7 |  | 200 | 5.0 | ${ }_{4} 3$ | 200 | 15 | 100 | 70 | - | = | $\overline{0.3}$ |  | RA |
| $2 \mathrm{m670}$ | PH | DNO, AJ, Pe | 0.7 | 300 | 25 | 5.0 | 40 | 23 | 200 |  |  | - |  | 0.3 |  | Puls |
| ${ }_{21123}^{2124}$ | $\begin{gathered} \text { Hu } \\ \text { HU } \end{gathered}$ | m | $\begin{aligned} & 0.8 \\ & 0.8 \end{aligned}$ | 400 100 | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | ${ }^{3}$ | $110$ | $\begin{aligned} & 100 \\ & 200 \end{aligned}$ | $\begin{aligned} & 21 \\ & 20 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ | $\left\lvert\, \begin{aligned} & 95 \\ & 95 \end{aligned}\right.$ | - |  | - |  | TO.SP |
| 2 Ll 164 | CT |  | 0.8 | 250 | 160 | 2 | 10 | 50 | 15 | 001 |  | - |  |  |  |  |
| clie | CT | mp,a],sı | 0.8 | 250 | 160 | 2 | 15 | 50 | 15 |  | 50 | - |  | - |  |  |
| CSM | CT | DnP, A, si | 0.8 | 250 | 160 | 2 | 8 | 50 | 12 | . 2 | 50 |  |  |  |  |  |
| 243274 | HU | mp,N,si | 1.0 | 385 | 160 | 3 | 50 | 100 | 14 | 10 | 95 | - | - | - | - | RA. SSO |
| 21238284 | HU | mpajs | 1.0 | ${ }^{385}$ | 1150 |  | 50 | 100 | $25$ | 10 | ${ }_{9}^{95}$ | - |  |  |  | wT. RA SSO, Ja |
| $2{ }_{23393}$ | $\xrightarrow{\text { RUCA }}$ | pnp, $\mathrm{A}, 1,31$ | 1.0 | ${ }^{385}$ | 160 | 3 | 50 | 100 | $50$ | 10 | 9 | - |  |  |  | WT. RA SSO. MA |
| $\xrightarrow{2131053}$ | $\begin{array}{\|l\|l\|} \hline \text { RCA } \\ G E \end{array}$ | mpp.A.se | $\begin{aligned} & 1.0 \\ & 1.0 \end{aligned}$ | $\begin{gathered} 200 \\ 200 \end{gathered}$ | 105 | 4 | 30 50 | 300 | 25 | ${ }_{25}^{16}$ | $\stackrel{\square}{0}$ | - | - | 0.09 |  | BE, us. MO |
| 21067 | PH | monen, se | 1.1 | 300 |  | 5.0 |  |  |  |  |  |  | - |  |  | neon in |
|  | HU | DM,A, $\mathrm{A}, \mathrm{S}$ | 1.2 | 400 | 100 |  | 15 | 100 | 20 | 10 | 95 | - | - |  |  |  |
| ${ }^{211229}$ | HU | pmo, $\mathrm{N}, 8$ | 12 | 400 | 160 |  | 15 | 100 | 36 | 10 | 95 | - |  | - | - | MT.ma |
| 2 L 1230 | HU | map, | 12 | 250 | 200 | - | 35 | 500 | 14 | 50 | 100 |  |  |  |  | MA |
| 2 L 1231 | HU | mp.FJ, $\mathrm{Sl}^{1}$ | 1.2 | 250 | 200 | - | 35 | 500 | 24 | 50 | 100 |  |  |  |  | WT. MA |
| 2 L 123 | Hu | mop.ff | 12 | 250 | 200 | - | 65 | 500 | 14 | 50 | 100 | - | - | - | - | wT. ma |
| 2 m | HU | mpo.f., | ${ }^{12}$ | 250 250 | 200 200 | - | 110 | 500 500 | 24 | 50 | 100 | $=$ |  | - |  | MT. MA |
| $2 \mathrm{2N}$ | HU |  | 1.2 | $\underset{1}{250}$ | 200 160 | 1.4 | 110 | 200 | ${ }_{20}^{14}$ |  |  | - |  |  |  | ${ }_{\text {WTM Ma }}^{\text {coxal }}$ |
| 211239 | Hu | mp, 1 , $\mathrm{s}_{1}$ | 12 | 1* | 160 | 7.4 | 15 | 200 | 36 | 10 | 95 | - |  |  |  | Coxizal |
| 211239 | HU | m |  |  | 100 | - | 15 | - | 28.65 |  | - | - |  |  |  |  |
|  | H | mom | 12 | 1000 | 150 | 7.4 | 35 | 200 | , | 10 | 95 | - |  |  |  | Coaxal package |
| 201241 <br> 201221 | $\begin{array}{\|l\|l} \mathrm{Hu} \\ \mathrm{HU} \end{array}$ |  | 12 | 1000 | $1 \begin{aligned} & 160 \\ & 180\end{aligned}$ | 7.14 | ${ }_{65}^{35}$ | ${ }_{200}^{200}$ | ${ }_{20}^{36}$ | 10 | ${ }_{95}^{95}$ | - |  |  |  |  |
| 2 N 12 | HU | m, ${ }^{\text {m,sis }}$ | 1.2 | \% | 160 | 7.1 | ${ }_{65}$ | 200 | 36 | 10 | 9 | $=$ |  |  |  | coaxial pachage Coaial pachage |
| 2 N | CT | mo.n. |  |  |  |  |  |  |  | 005 |  |  |  |  |  |  |
|  | $\begin{aligned} & \mathrm{CT} \\ & \mathrm{CT} \end{aligned}$ | mpen. ${ }^{\text {and }}$ | 12 | 250 | 1160 | ${ }^{2}$ | 10 | 50 | 23 |  |  | - |  | - | - | eld |
| 2 K | $\begin{aligned} & \mathrm{Cr} \\ & \mathrm{SY} \end{aligned}$ | mpp.A.si ${ }_{\text {and }}$ | 1.5 | 250 100 | 1100 | ${ }_{1}^{1.65}$ | 10 | ${ }_{20} 20$ | 50 | 50 15 | 50 | 15 | , |  |  | , 10 |
| $2 \mathrm{NS5}$ | ino |  | 1.5 | 150 | ${ }_{5}$ | 2.5 | 15 | 200 | 25 | 15 | 14 |  |  |  | So | Us, KF |
|  | IND | mp.N. | 1.5 | 150 |  | 2.5 | 25 | 200 | 25 |  | 10 |  | 0.1 |  | 35 | US |
| B1ISAA | $\left.\right\|_{\text {\| }} ^{8 E}$ | Onp.A. ${ }^{\text {and }}$ | 1.5 | 100 | 100 | . 15 | 50 |  | - | $10$ |  | 1.5 |  | $\begin{aligned} & 25 \\ & 28 \end{aligned}$ | $=$ |  |
| ${ }^{2133294}$ | sso | mmp.fA,si | 2 | 385 | 160 | 2.85 | 40 | 50 | 14 |  | $\pi$ |  |  |  |  |  |
| 215336 | PH | DTP.A.E | 2.0 | 50 | ${ }_{*}$ | 0.18 | 20 | 30 |  | 4.0 | - | - |  | 0.07 | 150 |  |
| ${ }_{211125}^{21069}$ |  | non, A. ge | ? | 150 300 |  | 2.5 | 20 | 220 | - | 25 | - | 5 | 5 | 0.3 | 20 |  |
| 211125 211220 | $\begin{array}{\|l\|l\|} \hline \text { PS } \\ \text { SSO } \end{array}$ | mp.AJ.ge | ${ }_{2}^{2}$ | 300 150 | ${ }_{1}^{150}$ | 5.2 | 25 | 250 |  |  |  |  |  | 0.15 | 50 |  |
| 21123 | 550 | mpon, 31 | 2 | 150 | 150 | 1.2 | 10 |  | 6 | 0.1 | - | - |  |  | $\underline{\square}$ |  |
| 211146 | Imo | mponse | 2 | 200 | ${ }_{5}$ | 3.33 | 45 | 400 | 30 | 5 | - | - |  |  | - |  |
|  | $\begin{aligned} & \text { AMP } \\ & \text { AMP } \end{aligned}$ | DMP.PADT |  | $550$ |  | - |  | 600 |  | 10 |  |  |  |  |  |  |
| 2 NB 17 | RA |  | ${ }_{2.5}^{2.5}$ | 100 | ${ }_{6}$ | 1.6 | $\begin{aligned} & 30 \\ & 30 \end{aligned}$ | 100 |  | 10 |  | 0.7 | - | $=$ | 0.5 |  |
| 23618 | Ra | npm, $\mathrm{A}, \mathrm{se}$ | 2.5 | 75 | ${ }_{5} 5$ | 1.25 | 30 | 400 | 20 | 10 | 20 |  |  |  |  |  |
| $2 \times 356$ | 5 | apm, AJ, $\mathrm{se}^{\text {e }}$ | 3 | 100 | ${ }_{4}{ }^{\text {a }}$ | 1.6 | 20 | 500 | - | 25 | - | 1.0 | 0.3 | 0.6 | - | G1 |
|  | $\left\lvert\, \begin{aligned} & G 1 \\ & G F \end{aligned}\right.$ | Mo | $3$ | 150 | $\begin{aligned} & 100 \\ & 100 \end{aligned}$ | $\frac{2}{2}$ | $\begin{aligned} & 30 \\ & 20 \end{aligned}$ | 500 | ${ }^{60}$ | 3 | 14 | 1.5 | 0.3 | 0.18 | 35 | Sr |
| 2 m 201 | ${ }_{\text {RA }}$ | Mo, Aj se | 3 | 150 |  | ${ }^{2} 2$ |  | 400 | 20 man |  | 20 |  | Z |  | = |  |
| 212808 | Ra | mp.al | 3 | ${ }^{5}$ | ${ }^{65}$ | 1.25 | 30 | 40 | 30 | 4 | 20 | $=$ | - |  |  | Submin |
| 21147 | IMO | omp.AJ. $\mathrm{ce}^{\text {e }}$ | 3 | 200 | Es | 3.33 | 45 | 400 | 45 | 5 |  |  |  |  |  |  |
|  | $\begin{array}{\|l\|l\|} \text { ino } \end{array}$ | Mon, A.pe | $3.5$ | 200 | ${ }_{10}{ }^{\text {® }}$ | $3,33$ | $15$ | 200 | 70 | 2.5 | 12 | . 6 | 4 | 0.1 |  |  |
| 2 m 00 A | RCA | mpadis | , | 150 |  |  |  | 150 |  |  |  |  |  |  |  |  |
| 2 M 25 | SY | pRo.AJ. GE | 1 | 150 | 85 | 2.5 | 20 | 400 |  | 2.0 | 14 | 1.0 | 0.3 | 0.2 | 30 | RA, inots, us KF. GI |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ${ }^{2 \times 12000}$ | $\begin{aligned} & R M \\ & R A \end{aligned}$ | Pnop,AJ, ge |  |  | ${ }_{85}^{80}$ | $\begin{aligned} & 1.25 \\ & 125 \end{aligned}$ | $\begin{aligned} & 25 \\ & 25 \\ & 25 \end{aligned}$ | $\left\|\begin{array}{c} 150 \\ 100 \end{array}\right\|$ | $\begin{aligned} & 20 \\ & 10 \end{aligned}$ | 5 | 20 | - | $=$ | - | - |  |
| 2 Llig 7 | 50 |  |  | 150 |  |  | 15 | 100 |  |  |  |  |  | = |  |  |
| 2 N 1028 | SSO | mpp.A, 31 | 1 | 150 | 150 | , | 10 | 100 | 9 | 25 |  |  |  | 0.15 |  |  |

## Low Level (continued)

| Type Mo. | Mfg. | Typo | 4. | Maximum Ratings |  |  |  |  | Characteriatice |  |  | Smisching |  |  |  | Romerks |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} w_{c} \\ (m w) \end{gathered}$ | $T_{i}$ <br> (c) | mwic | $v_{c}$ | $\begin{aligned} & 1_{c} \\ & m a s \end{aligned}$ | $\begin{aligned} & \mathrm{h}_{\text {fe }} \\ & \mathrm{h}_{\mathrm{FE}} \end{aligned}$ | $\begin{aligned} & I_{\mathrm{CO}} \\ & \mu_{0} \end{aligned}$ | $\left\|\begin{array}{c} C_{\cos } \\ \mu \mu \mathrm{I} \end{array}\right\|$ | Rise Time | $\begin{aligned} & \text { Stor } \\ & \text { Tine } \end{aligned}$ | $\begin{aligned} & \text { Sat } \\ & \text { Volt } \end{aligned}$ | $\begin{array}{\|l\|l} \text { Leak } \\ \mathrm{CuI} \end{array}$ |  |
| 2N1448 | IND | pmp, $\mathbf{N}$, se | 1 | 200 | ${ }^{6}$ | 3.33 | 45 | 100 | 65 | 5 |  | - | - | - | - |  |
| 2N1605A | SY | npn,AJ, ge | 1 | 200 | 100 | 2.6 | 40 | 200 | 40 | 10 | 20 | - | - | - | - |  |
| 2N17E0 | SY | mpn,A,ge | 1 | 100 | 100 | 1.3 | 25 | 100 | 30-110 | 10 | 20 | - | - | - | - |  |
| $2 \mathrm{M1781}$ | SY | $\mathrm{npm}, \mathrm{A}, \mathrm{ge}$ | 1 | 100 | 100 | 1.3 | 25 | 100 | 40 | 5 | 20 | - | - | - | - |  |
| 2N2000 | TI | MMD, ${ }^{\text {N,fe }}$ | 1 | 300 | 100 | 4 | 50 | 750 |  | 8 | 30 | - | - | - | - |  |
| CK25 | RA | Pmp, FA,ge | 15 | 80 | \% | - | 20 | 400 | - | 2 | 14 | 0.5 | 0.3 | 0.25 | 30 |  |
| 21395 | GE | mp, Asge | 4.5 | 200 | 100 | 3.3 | 15 | 200 | $\square$ | 6 | 12 | 0.55 | 0.5 | 0.1 | $20$ | TI, KF |
| 2N520 | IND | map,AS, ge | 4.5 | 150 | 0 | 2.5 | 15 | 200 | 40 | 1 | 14 | - | 0.5 | 0.1 |  | US |
| 2N520A | IND | pmp,AJ.ge | 4.5 | 150 | \% | 2.5 | 25 | 200 | 100 | 1 | 14 | 0.9 | 0.7 | - | 75 | us |
| 2N1308 | TI | npn,A〕,ge | 4.5 | 150 | 85 | 2.5 | 25 | 300 | , | 5 | 11 | . 70 | . 50 | Iv | 7 | TO-S, SY, GI |
| 2 21303 | TI | Mnp,AJ.ge | 4.5 | 150 | 85 | 2.5 | 30 | 300 | - | 3 | 16 | . 40 | 90 | Iv | - | GI, MF |
| 2N1354 | IND | pnp,A, A,ge | 4.5 | 200 | 85 | 3.33 | 30 | 200 | 70 | 2.5 | 12 | . 55 | . 5 | 0.1 | - | GI, KF |
| 2N1169 | SY | mpn,AS.se | 4.5 | 120 | ¢ | 2 | 25 | 400 | 20 | 50 | 20 | . 5 | $\because$ | - | - | RCA |
| 2N1170 | SY | ¢pn, A. $\mathrm{ge}^{\text {c }}$ | 4.5 | 120 | ${ }^{5}$ | 2 | 25 | 400 | 20 | 50 | 20 | - | - | $\stackrel{\rightharpoonup}{7}$ | - | RCA |
| 2M123 | SY | mnp.AJ.ge | 5 | 100 | 85 | 1.65 | 15 | 125 | 30-150 | 0.6 |  | - | - | $\begin{aligned} & 9.2 \\ & r_{\text {max }} \end{aligned}$ | - |  |
| 2 K 315 | GI | pmp.A.se | 5 | 100 | $\pm$ | 2 | 20 | 500 | - | 1 | 14 | 1.0 | 0.2 | 0.12 | 20 | KF, IND, US |
| 2N315A | GI | Dnp, AJ, ge | 5 | 150 | 100 | 2 | 30 | 500 | 3 | 1 | 14 | 0.9 | 0.4 | 0.12 | 35 | WD, US, KF |
| 2 B 396 A | SY | Mmp, $\mathrm{N}, \mathrm{ge}$ | 5 | 150 | 100 | ? | 30 | 200 | 30-150 | 6 | - | - | . | - | - | TS,MF,GE,GI |
| 2M14 | SY | Omp,AJ.ge | 5 | 150 | 85 | 2.5 | 30 | 200 | 30-90 | 5 | - | - | - | - | - | KF, GI |
| 2M439 | SY | npn, AJ, ge | 5 | 100 | 85 | 1.66 | 20 | - | - | 10 | - | 0.5 | 0.1 | 0.25 | 30 |  |
| 2M150 | GE | PMp, $\mathrm{N}, \mathrm{ge}$ | 5 | 150 | 15 | 2.5 | 12 | 125 | - | 6 | 20 | - | - | 0.2 | 30 |  |
| 21576 | SY | npm,AJ.ge | 5 | 200 | 100 | 2.6 | 20 | 400 | $\checkmark$ | 20 | - | 2 | 1 | 0.4 | 40 |  |
| 2N578 | RCA | pmp,AJ.te | 5 | 120 | $n$ | - | 20 | 400 | 15 | 3 | - | 0.85 | 0.33 | 0.2 | 15 | TS,IND,US,KF,GI |
| 2 E 85 | RCA | npm,AJ.ge | 5 | 120 | 71 | - | 25 | 200 | 40 | 3 | $\bar{\square}$ | 0.35 | 0.25 | 0.1 | 40 | SY, GI |
| 2W658 | RA | DMO, FA,ge | 5 | 150 | 68 | - | 16 | la | - | 2.5 | 12 | - | . | 0.25 | 50 |  |
| 2 NOO 3 | RA | Dnp, Al, ge | 5 | 75 | \% | 1.25 | 30 | 400 | 40 | 4 | 20 | - | - | - | - | Submin |
| 2 N 004 | RA | pro, Ad, pe | 5 | 75 | 85 | 1.25 | 30 | 400 | 40 | 4 | 20 | - | - | - | - | Subinis |
| 2N815 | RA | npm,AJ.ge | 5 | 75 | 85 | 1.25 | 25 | 200 | 60 | 10 | 20 | - | - | - | - | Submin |
| $2 \mathrm{~N} 1{ }^{2} 16$ | RA | nom, N, ge | 5 | 15 | 85 | 1.25 | 25 | 200 | 60 | 10 | 20 | - | - | - | - | Submin |
| 2 M 19 | RA | npm,A..ge | 5 | 75 | 05 | 1.25 | 30 | 400 | 30 | 10 | 20 | - | - | - | - | Sitomin |
| 2N8O | RA | npm,A.ge | 5 | 75 | \% | 1.25 | 30 | 400 | 30 | 10 | 20 | - | - | - | - | Submis |
| 2M25 | RA | pnp, A.ge | 5 | 75 | ${ }_{5}$ | 125 | 30 | 200 | 30 | 6 | 20 | - | - | - | - | Sutam |
| 2M26 | RA | Onp, N, ge | 5 | 15 | 85 | 1.25 | 30 | 200 | 30 | 6 | 20 | - | - | - | - |  |
| 2N1012 | GI | npn, N , pe | 5 | 150 | 100 | ? | 40 | - |  | 5 | 10 | 0.1 | 0.1 | 0.1 | 50 |  |
| 2N1123 | PH | PAD, Anse | 5 | 150 | 100 | 10 | 45 | 500 | 3.5 | 10 | 15 | - | - | 0.005 | 70 |  |
| 2N1219 | SSD | pno.AJ, si | 5 | 250 | 175 | 1.1 | 25 | 100 | - | 001 | 15 | - | - | - | - |  |
| 2N1318 | IND | pnp,A」, ge | 5 | 200 | 25 | 3.33 | 40 | 400 | 98 | 5 | 12 | - | - | - | $=$ |  |
| 2N1449 | IND | mp,A, ge | 5 | 200 | ${ }^{5}$ | 3.33 | 45 | 400 | 80 | 5 | $\underline{-}$ | - | - | - | - |  |
| 2N1990 | TI | npm,A, es | 5 | 150 | 15 | 2.5 | 30 | 300 | - | 5 | 11 | 1.1 | 1.5 | - | - |  |
| GT1658 | GI | npo, $A \mathrm{~J}, \mathrm{ge}$ | 5 | 150 | 100 | 2 | 30 | 300 | 50 | 3 | 10 | 1.1 | 1.5 | - | - |  |
| KCS 1005 | KF | pmo, AJ, ge | 5 | 200 | \% | 5.2 | 30 | 400 | 40 | 12 | - | - |  | - |  |  |
| 2 N 271 | SV | non,AJ.ee | 6 | 150 | 100 | 2 | 20 | 200 | 0 | 10 | - | 2.5 | 0.7 | $\bar{\square}$ | 40 | GE, GI |
| 2 N 357 | SY | nom, A, ge | 6 | 100 | 18 | 1.6 | 15 | 500 | - | 25 | - | 12 | . 7 | . 20 | 1 |  |
| 21357 A | GI | npo,N, ge | 6 | 150 | 100 | 2 | 30 | 500 | 90 | 3 | 14 | 0.5 | 0.5 | 0.18 | 40 | ${ }_{5} \mathrm{SY}$ |
| 2M26 | SY | mp.AJ, ${ }^{\text {ce }}$ | 6 | 150 | \% | 2.5 | 20 | 400 | - | 2 | 14 | 1.0 | 0.3 | 0.22 | 0 | RA,TR,TS,GI,US. TI, KF |
| 2N799 | RA | npm,08,si | 6 | - | - | 1.4 | 45 | 25 | 15 | .008 | 5 | - | - | - |  |  |
| 2 NGO | RA | npn,D8.si | 6 | - | $\stackrel{\rightharpoonup}{1}$ | - | 45 | 25 | 15 | .002 | 5 | - | - | - | - |  |
| 2N1319 | RCA | pap.N.ge | 6 | 120 | 71 | - | 20 | 400 | 30 | 2.5 |  | 20 | - | - | = |  |
| 2N1343 | IND | mop.A, ie | 6 | 150 | 85 | 2.5 | 20 | 400 | 40 | 3 | 12 | 1.0 | - | - | - |  |
| 2N1997 | TI | non,A,se | 6 | 250 | 100 | 3.3 | 45 | - |  | 15 | 12 | 1.0 | - | - | - |  |
| CK26 | RA | map.FA,ge | 6 | 80 | \% | - | 18 | 400 | - | 2 | 14 | 0.5 | 0.3 | 0.25 | 40 |  |
| 2N100 | SY | npn,AJ.se | 7 | 150 | 100 | 2 | 40 | - | 25(min) | 15 | 1 | - | - | 0.25 | 0 |  |
| 2N1090 | RCA | npn,AJ, ze | 7 | 120 | 05 | - | 25 | 400 | 50 | 4 | - | 0.25 | 0.20 | - | 50 | GI |
| 2N1114 | SY | nom,AJ.ge | 7 | 150 | 100 | 2 | 15 | 200 |  | 30 | - |  | - | - | 80 | - |
| 2N198 | TI | npn,AJ.se | 7 | 150 | \% 15 | 2.5 | 25 | 300 | - | 5 | 11 | - | - | - | 0 |  |
| CT123 | GI | map.AJ.ge | , | 150 | 150 | 2 | 25 | I | 40 | 3 | 15 | 0.9 | 0.5 | 0.1 | 90 |  |
| 2N123 | GE | pap,AJ,ge | 8 | 150 | 0 | 2.5 | 15 | 125 | 0.981 | 6 | 15 | 0.45 | 0.90 | 0.15 | $\pm$ | SY |
| 21388 | GI | non,AJ.se | 8 | 150 | 100 | 2 | 25 | 500 | - | 5 | 10 | 0.6 | 0.4 | - | 120 | SY, GE, RA |
| 2N396 | GE | pnp,AJ.se | 8 | 200 | 100 | 3.3 | 20 | 200 | - | 6 | 12 | 0.4 | 0.6 | 0.08 | 30 | TI,GI,SY, TS |
| 219376A | SY | npn,AJ,ge | 8 | 200 | 100 | 2.6 | 40 | 400 | - | 40 | 12 | 2 | 0.6 | 0.4 | 40 | -1,olst,is |
| 2 2N579 | RCA | pro.AJ,ge | 8 | 120 | 11 | - | 20 | 400 | 30 | 3 | $\overline{-}$ | 0.36 | 0.33 | 0.2 | 30 |  |
| 2N581 | RCA | Dnp.AJ.se | 8 | 150 | 85 | - | 18 | 100 | 30 | 3 | 12 | 0.20 | 8.20 | 0.35 | 30 | US, IMO,GI,KF |
| 2N553 | RCA | pap,AJ, ee | 8 | 120 | 85 | - | 18 | 100 | 30 | 3 | 12 | 0.2 | 0.20 | 0.35 | 30 |  |
| 2N598 | PH | prip.AJ.ge | 8 | 250 | 100 | 3.3 | 35 | 500 | - | 3 | 15 | 0.2 | - | 0.085 | 8 |  |
| 2N6E2 | RA | pmp.FA.ge | 8 | 150 | 8 | - | 11 | 12 | - | 2.5 | 12 | - | - | 0.25 | co | KF |
| 2N714 | RCA | pmp, AJ,ge | 8 | 150 | 85 | $\square$ | 30 | 200 | 60 | 2 | 11 | - | - | - | - |  |
| 2N790 | RA | npn, DB, si | 8 | - | - | 1.4 | 45 | 25 | 30 | 002 | 8 | - | - | - | - |  |
| 2N792 | RA | npm, DB, ${ }^{\text {a }}$ | 8 | - | - | 1.1 | 45 | 25 | 60 | . 000 | 5 | - | - | - | - |  |
| 2NS03 | RA | npn,DB,sı | 8 | - | - |  | 45 | 25 | 30 | . 090 | 20 | - | - | - | - |  |
| 2NS05 | RA | non,OB,si | 8 | - | - |  | 45 | 25 | 80 | . 000 | 20 | - | - | - | - |  |
| 2N1280 | IND | pnp,AJ.ge | 8 | 200 | 85 | 3.33 | 16 | 400 | 60 | 5 | 10 | 10 |  |  |  |  |
| 2N1284 | IMD | pmp,AJ, ge | 8 | 150 | 85 | 2.5 | 20 | 400 | 90 | 2 | 15 | . 45 | . 9 | 15 | $\underline{\square}$ |  |
| 2N1304 | TI | mpn,A,ge | 8 | 150 | 6 | 2.5 | 25 | 300 | 110 | 5 | If | . 45 | . 50 | Iv | - | TO-S,GI,SY,GE |

## UNVARYING HIIHH-OUALITY PERFORMANGE



AT $120^{\circ} \mathrm{C}$, minnerime (5) =- =-

> Complete technical information is available from you Motorola district office: Motorola distributor: or write to tion Department. 5005 East McDoweli Road. Phoenix 10 Arizona.
> motorola distaict offices
> Chicago Chiton. N D Dallas $\begin{array}{ll}\text { Oarton Detroit } \\ \text { Silver Spring. Md. } & \text { Glenside. Pa. } \\ \text { Syracuse }\end{array}$ Hollywood Minneapolis Orlando. Fla

The parameter distribution shown in these 1000 hour $100^{\circ} \mathrm{C}$ and $120^{\circ} \mathrm{C}$ storage life tests exhibits a high degree of stability ... the key to product cliability and dependability in your circuits Even after extended life testing at an elevated emperature of $120^{\circ} \mathrm{C}\left(20^{\circ} \mathrm{C}\right.$ above the suggested maximum rating). these units continue to exhibit tight distribution within originally stated limits positive assurance of unvarying high-quality performance of Motorola power transistors.

This data. taken on random samples of produc ion lots of Motorola 2N174 transistors, is typical of the 100\% lot life-tests conducten on all Motorola power transistors. When you use Motorola power transistors you know you are obtaining outstanding product reliability.

## EVEN AT $20^{\circ} \mathrm{C}$ ABOVE $\mathrm{T}_{\mathrm{J}}$ MAX.

## MOTOROLA POWER TRANSISTORS

## MOTOROLA IS YOUR MOST COMPLETE POWER TRANSISTOR SOURCE

You'll find a standard power transistor that meets you specific design requirements from the wide selection of field-proven devices available from Motorola.

T0-36 "Doorknob" Package. 15 types in "low silhouette" case 150 watts power dissipation: $0.5^{\circ} \mathrm{C} / \mathrm{W}$ maximum thermal resistance: $100^{\circ} \mathrm{C}$ maximum junction temperature: 15 amps: 2 to 1 gain spread and voltage combinations to 100 volts; 3 Mil-type units.
T0.3 "Diamond" Package. 118 types in "low silhouette" case 90 watts power dissipation: $0.8^{\circ} \mathrm{C} / \mathrm{W}$ maximum thermal resistance: $100^{\circ} \mathrm{C}$ maximum junction temperature; 3. 5 . 10. 15 and 25 amps: narrow pain spread and voltage

4
MOTOROLA
Somiconductor Products Inc.


TRANSISTORS-1961
Low Level

| $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ | MFs. | Trpe | 'so | Maximen Ratings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} w_{c} \\ \left(\mathrm{~m}_{\mathrm{w}}\right) \end{gathered}$ | $T_{i}$ <br> (c) | w/c | $v_{c}$ | ${ }_{\text {I }}^{\text {c }}$ |
| 211305 | 11 | mp, N | 1 | 150 | ¢ | 2.5 | 30 | 300 |
| 2 L 347 | IND m | mpan | 8 | 150 | 8 | 2.5 | 20 | 200 |
| 2N1350 | IND | mom, $\mathrm{N}, \mathrm{se}$ | B | 200 | 85 | 3.33 | 50 | 0 |
| 201351 | Ind a | pen,AJ, | 1 | 200 | 85 | 3.33 | 10 | 400 |
| 2N1355 | IMO | mon, Nige | 8 | 200 | ${ }^{6}$ | 3.33 | 30 | 200 |
| 2N1356 | IND | mp,N, $\mathrm{m}^{\text {a }}$ | 1 | 200 | 100 | 2.66 | 30 | 200 |
| 2N16\% | SY | qpm, $\mathrm{N}_{\text {de }}$ | 8 | 100 | 100 | 1.3 | 25 | 200 |
| 212001 | TI | mp, AJ, | B | 300 | 100 | 1 | 30 | 150 |
| 2 L 167 | GE | mon. 6 J. | 9 | ${ }^{6}$ | 5 | 1.1 | 30 | 5 |
| 21358 | GI | non, $\mathrm{N}, \mathrm{s}$ | 9 | 100 | ¢ | 2 | 20 | 500 |
| 273580 | SY | apmAdso | 9 | 150 | 100 | 2 | 30 | 500 |
| 21090 | CE | Mp, AJ, | 9 | 150 | 65 | 2.5 | 10 | 200 |
| 2 meg | PA | npm, Ni, en | 9 | 75 | 6 | 125 | 25 | 100 |
| 2N1190 | GE | mpo,RG, ${ }_{\text {a }}$ | 9 | 6 | ¢ | 1.1 | 25 | 5 |
| OC141 | AMP | пpm,Padt. | 9 | 100 | 5 | - | 20 | 250 |
| 2 mmo | SY | mpa, AJ, | 10 | 100 | 4 | 1.66 | 15 |  |
| 20510 | GE | mp,A, | 10 | 150 |  | 2.5 | 12 | 125 |
| 2 L 521 | IND | [mp, A1, ge | 10 | 150 |  | 2.5 | 15 | 200 |
| 2 T 521 A | IMD |  | 10 | 150 | 8 | 2.5 | 25 | 200 |
| 2N600 | PH | mon, AJse | 10 | 730 | 100 | 10 | 35 | 500 |
| 2w6ss | RA | Ma.FA.Ex | 10 | 150 | ${ }^{\mathbf{5}}$ | - | 14 | 5 |
| 21775 | RA | npen, M6, si | 10 | 150 | 15 | 0.7 | 45 | 50 |
| 2 mes | RA |  | 10 | 75 | 5 | 1.25 | 30 | 100 |
| 2M005 | RA | PMP, N, | 10 | 75 | 4 | 1.25 | 30 | 100 |
| 2N21 | RA | ¢padse | 10 | 75 | 85 | 1.25 | 30 | 100 |
| 2 MOP | RA | mpo,N, se | 10 | 75 | ¢ | 1.25 | 30 | 100 |
| 211281 | 110 |  | 10 | 200 | E | 3.33 | 16 | 100 |
| 201349 | 190 | Pm, A1, | 10 | 200 | ${ }^{5}$ | 3.33 | 40 | 400 |
| 211998 | II | apon, $\mathrm{N}, \mathrm{le}$ | 10 | 150 | \% | 2.5 | 29 | 300 |
| 2 L 198 | 11 | mp,N, ${ }^{\text {co }}$ | 10 | 250 | 100 | 3.3 | 35 | 100 |
| 2 W 27 | GI | mpan, ${ }^{\text {ces }}$ | 11 | 150 | 100 | 2 | 30 |  |
| 2 7 791 | RA | am, $\mathrm{OB}, \mathrm{si}$ | 11 | - | - | 1.4 | 45 | 25 |
| $2 \mathrm{NsO4}$ | RA |  | 11 | - | - |  | 15 | 25 |
| C197 | RA | pap, FA, ${ }^{\text {a }}$ | 11 | $\infty$ | \% | - | 15 | 100 |
| 2 3 16 | GI | mpp, N, ge | 12 | 100 | 85 | 2 | 20 | 500 |
| 223164 | 61 | pmp,AJ.ge | 12 | 150 | 100 | 2 | 30 | 500 |
| 23037 | GE | Pap, AJ.ge | 12 | 200 | 100 | 3.3 | 15 | 200 |
| 2 4 404 | RCA | Pap, N, pe | 12 | 120 | 8 | - | 25 | 100 |
| $2 \mathrm{mb35}$ | GE | npo, AJ, $\mathrm{m}_{\text {ce }}$ | 12 | 150 | 区 | 2.5 | 20 | 300 |
| $2 \times 1300$ | II | np, A A | 12 | 150 | 85 | 2.5 | 25 | 300 |
| 2 N 1307 | II | mpp,A,ge | 12 | 150 | 85 | 2.5 | 30 | 300 |
| $2 N 1313$ | IMD | pmp, A, ce | 12 | 15 | ${ }^{\circ}$ |  | 30 | 400 |
| $2 \mathrm{N1344}$ | IMD | pap, AJ, | 12 | 150 | ${ }^{8} 5$ | 2.5 | 15 | 40 |
| $2 N 1345$ | IMD | pmp, N, , ${ }^{\text {ce }}$ | 12 | 150 | ${ }^{5}$ | 2.5 | 10 | 10 |
| 201346 | IND | pmp,A, ise | 12 | 150 | 85 | 2.5 | 12 |  |
| 211357 | INO | mpo, A, se | 12 | 200 | ${ }_{5}^{5}$ | 3.33 | 30 | 20 |
| 21269 | RCA | pmp,A].ge | 13 | 120 | 85 | 1 | 25 | 100 |
| 24798 | RA | mpn, DB, 51 | 13 | - | - | 1.4 | 45 | ${ }_{2} 2$ |
| 2NSO6 | RA | npm, 08, si | 13 |  |  |  | 45 | 2 |
| 2 L 1091 | RCA | mon, , ese | 13 | 120 | 85 |  | 25 |  |
| 2NSE | SY | pnp,AJ, ge | 14 | 120 | $\pi$ | 2.6 | 25 | a |
| $2 \mathrm{NB07}$ | RA | pmp,AJ, $\mathrm{pe}^{\text {e }}$ | 14 | 5 | あ | 1.25 | 25 | 10 |
| 2N800 | RA | pmp,AJ, ¢ | 14 | 15 | ${ }_{6}$ | 1.25 | 25 | 10 |
| 2 N 58 | PH | DPD.SP.si | 14 | 150 | 140 | 1.3 | 40 |  |
| 2N859 | PH | pmp.SP,si | 14 | 150 | 140 | 1.3 | 40 |  |
| 2N860 | PH | Pmp,SA, SI | 14 | 150 | 140 | 1.3 | 25 |  |
| 2 Mess | PH | DnD.SP, 31 | 14 | 150 | 140 | 1.3 | 15 |  |
| 215580 | RCA | pmp, Al.ge | 15 | 120 | 7 | - | 20 | 40 |
| $2 \mathrm{NG36A}$ | SY | mpa, AJ, ge | 15 | 150 | 100 | 2 | 25 | 30 |
| 2N660 | RA | $\mathrm{pmp}, \mathrm{FA}, 8 \mathrm{c}$ | 15 | 150 | * | - | 11 |  |
| 2N129 | IND | pro, AJ, ge | 15 | 200 | \% | 3.33 | 16 | 40 |
| 2N1316 | IND | pnp,AJ.se | 15 | 200 | 5 | 3.33 | 30 | 40 |
| 2 N 1317 | IND | pmp,AJ,ge | 15 | 200 | 15 | 3.33 | 20 |  |
| 2N1310 | IMD | mp, AJ, ge | 15 | 200 | 05 | 3.33 | 10 |  |
| 2N1999 | TI | pmp, A, ge | 15 | 250 | 100 | 3.33 | 30 |  |
| $2 \mathrm{NS59}$ | PH | $\mathrm{pmp}, \mathrm{AL}, \mathrm{ge}$ | 16 | 250 | 100 | 03.3 | 30 | 50 |
| 2 NGOL | PH | $\mathrm{pmp}, \mathrm{AJ}, \mathrm{pe}$ | 16 | 750 | 100 | 10.0 |  |  |
| $2 \mathrm{Na28}$ | GI | pmp,N, $\mathrm{ge}^{\text {e }}$ | 17 | 150 | 100 |  | 30 |  |
| 2N636 | GE | npn, AJ, ge | 17 | 150 | 8 | 2.5 | 20 |  |
| CK28 | RA | Pnp.FA.ge | 17 | 80 | \& | - | 12 | 40 |
| 2 N 522 | IMD | pnp.AJ, ge | 18 | 150 | 85 | 2.5 | 15 | 2 |
| 2 2552A | 1 ma | Pmp, AJ, ge | 18 | 150 | * | 2.5 | 25 | 2 |
| 2N582 | RCA | Dro.AJ,ge | 11 | 120 | d | - | 25 | 1 |
| 2N584 | RCA | Pmp,AJ,ge | 18 | 120 | 85 | 15 | 5 | 1 |

SILICON AND GERMANIUM DIODES AND TRANSISTORS - SILICON RECTIFIERS - CIRCUIT-PAKS
 ORLANDO, FLA, GArden 3.0518- PHILADELPHIA PA. Maddontield M 1), MAzet 8.1272- SAN FRANCISCO, CAL (Redwood City), EMerson 9.5566 - SYRACUSE. N Y howard 3.9141 - CANADA Waterloo. Ont. SWerwood 5.6831 - GOVERNMENT RELATIONS: Washington. D.C., MEtropolitan 8.5205 CIRCIE 60 ON READER-SERVICE CARD

DETE CHERT
(continued)


ELECTRONIC DESIGN • July 5, 1961


## higher temperature high vacuum oven

perature operate, migh vacuum bake oven. rn $1 \times 10^{-6} \mathrm{~mm} \mathrm{H}$
The 0.8 achieves temperature uniformity of $3^{\circ}$ at 0 to $800^{\circ} \mathrm{C}$ and is the low cost oven that functions perfectly temperatures above $250^{\circ} \mathrm{C}$ and pressures on the 6 th scale without custom modification.
Tri Metal's new oven not only saves you money at pur chase time, it is also extremely economical to operate and easy to maintain
No water-cooling of the door is required. Accepts bench or dry box mounting.
Tri metal Works has been engaged in the custom tabricafion of high vacuum components and equipment for leading manufacturers and users since 1946. You are invited to see a demonstration of 0.8 in our plant laboratory. Call or wite for appointment.
higher temperatures
UD to 800 C .
BETTER UNIFORMITY
Plus or minus 3 C.
LESS MAINTENANCE
Low.Cost. Neoprene " 0 " ring gaskets
guaranteed one year
FASTER HEAT UP
$500^{\circ} \mathrm{C}$ in 23 minutes.
CLOSER CONTROL
I C Thermocouple INSIDE the work zone.
HIGHER VACUUM
$1 \times 10.4$ Torr $=(\mathrm{mm} \mathrm{Hg}) @ 500 \mathrm{C}$
COOLER EXTERIOR
All surfaces cool to the touch

TRI METAL WORKS INC.

 or phone $893-2000$.

TRANSIETORS-1961

|  |  |
| :--- | :--- |
|  |  |
|  | Abbreviation of Terms |
| AJ | Alloy Junction |
| DD | Double Diffused |
| DG | Grown Diffused |
| DJ | Diffused Junction |
| DM | Diffused Mesa |
| DP | Diffused Planar |
| Dr | Dift |
| Ep | Epitaxial |
| FA | Fused Alloy |
| FJ | Fused Junction |
| GD | Grown Diffused |
| Ge | Germanium |
| GJ | Grown Junction |
| GR | Grown Rate |

For an additional copy of the Transistor Data Cha"t turn
phe Reader-Seruce Card and circle 251.

DATA CHERT

Low Level（continued）

| Typo Ne． | Mfg． | Type | Moximum Ratings |  |  |  |  |  | Charsectoristics |  |  | Swirching |  |  |  | Pamede |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | fa | $\begin{gathered} W_{c} \\ (\mathrm{mw}) \end{gathered}$ | $T_{j}$ <br> （c） | mw／c | $V_{c}$ | $\begin{array}{\|c} \hline \mathrm{c}_{\mathrm{c}} \\ \mathrm{ma} \end{array}$ | $\begin{aligned} & h_{f e} \\ & h_{F E} \end{aligned}$ | $\begin{aligned} & T_{C O} \\ & \mu_{0} \end{aligned}$ | $\begin{aligned} & C_{c o e} \\ & \mu \mu \mathrm{t} \end{aligned}$ | $\begin{aligned} & \text { Rise } \\ & \text { Time } \end{aligned}$ | Stor Time | $\begin{array}{\|l\|l} \text { Sat } \\ \text { Volt } \end{array}$ | $\begin{array}{\|l\|} \text { Leazt } \\ \text { Cur } \end{array}$ |  |
| $2 \mathrm{2N1300}$ | TI | npn，A，，ge | 18 | 150 | 8 | 2.5 | 25 | 300 | 200 | 5 | 15 | － | － | － | － | TO－S，SY，GE |
| 2N1309 | T1 | pmp，A，ge | 18 | 150 | 5 | 2.5 | 30 | 300 | 210 | 3 | 11 | － | － |  |  | T0－5，KF，GI |
| 2 2317 | GI | pmp，AJ．ge | 20 | 100 | 85 | ？ | 30 | 500 | － | 1 | 14 | 0.3 | 0.4 | 0.18 | 30 | US，IMD，KF |
| $2 \mathrm{2N317A}$ | GI | Pnp，A，ge | 20 | 150 | 100 | 2 | 30 | 500 | 180 | 1 | 14 | 0.3 | 0.4 | 0.18 | 40 | IMD，US，KF |
| 20337 | TI | npm，CD，si | 20 | 125 | 150 | ． 001 | 15 | 20 | 19 | 1 | － | 0.05 | 0.02 | 1.5 | 35 | TR，RA，GE |
| 2 M 17 | Ind | mp，AJ，ge | 20 | 200 | 85 | 3 | 30 | 200 | 140 | 25 | 12 | － | － | $-$ | － | KF |
| 20661 | RA | Pnp，FA．ge | 20 | 150 | 85 | － 7 | 9 | 1a | － | 2.5 | 12 | － | － | 0.25 | 120 | KF |
| 2 29746 | RA | npa，MS，${ }^{\text {si }}$ | 20 | 150 | 175 | 0.75 | 45 | 50 | 45 | 10 | 3 | － | － | 0.25 |  |  |
| 2 L 1008 | BE | pmp，N，re | 20 | 400 | 85 | 6.6 | 20 | 300 | 100 | 10 | － | － | － | 0.25 | － |  |
| 2 T 1008 A | BE | mp，AJ，ge | 20 | 400 | 85 | 6.6 | 40 | 300 | 100 | 10 | － | － | － | 0.25 | － |  |
| 2M10088 | 㫙 | pnp，AJ．ge | 20 | 400 | 85 | 6.6 | 60 | 300 | 100 | 10 | － | － | － | 0.25 | － |  |
| 2 L 1017 | RA | mpp，FA，ge | 20 | 150 | 8 | － | 10 | 400 | － | 2 | 12 | 0.25 | － | 0.25 | 100 | US，KF |
| CX419 | RA | npo，FA si | 20 | 385 | 160 | － | 40 | 50 | 15 | 005 | 35 | 0.25 | － | 0.2 | 100 | US，KF |
| CMM20 | RA | npn，FA．si | 20 | 385 | 160 | － | 35 | 50 | 30 | ． 005 | － | － | － | － | － |  |
| CK421 | RA | npn，FA，si | 20 | 385 | 160 | － | 30 | 50 | 60 | ． 05 | 20 | － | － | － | － |  |
| CKM74 | ra | non，08，si | 20 | 250 | 180 | 1.9 | 40 | 50 | 15 | ． 005 | 20 | － | － | － |  |  |
| CX475 | RA | npm，08，si | 20 | 250 | 180 | 1.9 | 35 | 50 | 30 | ． 005 | 20 | － | － | － | $=$ |  |
| CK476 | RA | npm．08，st | 20 | 250 | 180 | 1.9 | 30 | 50 | 60 | ． 005 | 20 | － | － | 5 | － |  |
| CK477 | RA | npn，OB，si | 20 | 250 | 180 | 1.9 | 30 | 50 | 65 | ． 005 | 20 | － | － | － | － |  |
| 2M861 | PH | pnp，SP，si | 22 | 150 | 110 | 1.3 | 25 | 50 | 65 | 0.1 | 5 |  |  |  |  |  |
| 24863 | PH PH | mpo，Sp，si | 22 | 150 | 140 | 1.3 | 15 | 50 | 65 | 1 | 5 | － | － | － | － |  |
| 20854 | PH | Dmp．SP．si | 22 | 150 | 140 | 1.3 | 6 | 50 | 65 | 1 | － | － | － | － | － |  |
| ${ }_{2}^{2 N 523}$ | IND | mop，A，ge | 24 | 150 | 成 | 2.5 | 15 | 200 | 200 | 1 | 11 | － | － | － | － | US．KF |
|  | IMO | pmp，A〕．ge | 24 | 150 | 65 | 2.5 | 20 | 200 | 300 | 1 | 14 | 0.1 | 0.4 | － | 200 | US，KF |
| 2 2747 | RA | npm，MS，si | 25 | 150 | 175 | 0.75 | 25 | 50 | 30 | 10 | － | － | － | － | － |  |
| $2 \mathrm{W748}$ | RA | nen，MS，si | 25 | 150 | 175 | 0.75 | 30 | 50 | 10 | 6 | － | － | － | － | － |  |
| 2N1386 | RA | npo，MEs，si | 25 | 300 | 175 | 0.5 | 25 | 50 | 30 | 10 | 6 | － | － | － | － |  |
| 2N1387 | RA | npa，M6，si | 25 | 300 | 175 | 0.5 | 30 | 50 | 20 | 10 | 6 | － | － | － | － |  |
| ${ }^{2 N 1205}$ | TR | npm，GR，si | 21 | 150 | 150 | － | 20 | － | 6 | 50 | 3.0 | － | － | － | 30 |  |
| 21338 | TI | npm，GD，si | 30 | 125 | 150 | 001 | 45 | 20 | 39 | 1 | － | 06 | 0 | 1.5 | 15 | TR，RA，MA，GE |
| 2N643 | RCA | Dmp．DR．se | $30^{\circ}$ | 120 | 71 | － | 30 | 100 | 45 | 3 | 2 | 0.03 | 0.005 | － | 45 | ＂gan－Danowioth |
| 2N907 | RA | npm，DB，sı | 30 | $\bigcirc$ | － | － | 45 | 25 | 35 | 002 | 20 |  | － | － | － |  |
| KCSI004 | KF | pmp．A．ge | 32 | 200 | 85 | 3 | 10 | 400 | 120 | 12 | － | － |  | － | － |  |
| 2NH2 | TR | npm，GJ， 81 | 4 | 300 | 175 | － | 45 | 25 | 20 | 0.1 | － | － | － | － | － |  |
| TMT812 | TR | npm，DJ，sı | 41 | 150 | 173 | － | 45 | 25 | 20 | 1 | 6 | － | － | － | － |  |
| $2 \mathrm{CsO88}$ | RA | non，DB，31 | 45 | － | － | － | 45 | 25 | 75 | 002 | 20 |  |  | － |  |  |
| 2NGA | RCA | pnp．DR．ge | $50^{\circ}$ | 120 | 71 | － | 30 | 100 | 45 | 3 | － | 0.015 | 0.009 | － | 45 | －gain bandmiatm product |
| 573030 | TR | npon， $\mathrm{DJ}, \mathrm{si}$ | 50 | 100 | 150 | 0.8 | 15 | 5 | － | 50 | 4 | ． 04 | 07 | 10 | － |  |
| 2N865 | PH | pnp，SP，si | 52 | 150 | 140 | 1.3 | 10 | 50 | ：50 | ． 1 | 5 | － | － | － | － |  |
| 2 L 1254 | HU | Dnp．MS．si | 55 | 250 | 100 | 1.8 | 15 | － | 25 | 30 | 8 | － | 015 | 015 | 0.28 | T0－5 package |
| $2 N 1256$ 2N1258 | HU | pmp．10，si | 55 | 250 | 100 | 1.8 | 30 | － | 25 | 30 | $\bigcirc$ | － | － |  | － | T0－5 package |
| $2 N 1258$ 201779 | HU | pmo．MS，si | 55 | 250 | 160 | 1.8 | 50 | $\overline{-}$ | 25 | 30 | 8 | － | － | － | － | T0．5 package |
| 2 L 1779 | SY | npm， $\mathrm{N}, \mathrm{ge}$ | 60 | 100 | 100 | 1.3 | 25 | 100 | 25 | 10 | 10 | － | － | － | － | ， |
| 2N803 | TR | npo，DJ， $\mathrm{sl}_{1}$ | 64 | 300 | 175 | － | 45 | 25 | 40 | 1 | － | － | － | － | － |  |
| TMT843 | TR | npm． DJ .81 | 64 | 150 | $1 / 5$ | － | 15 | 25 | 40 | 1 | 6 | － | － | － | － |  |
| 20560 | WE | npn，DD，si | 70 | 600 | 150 | ． 25 | 60 | 100 | 20 | ． 1 | 8 | ． 06 | ． 05 |  | － | US，MIL Lonly，MA |
| 2N615 | RCA | mp，Drise | 70 | 120 | \％ | － | 30 | 100 | 45 | ， | 2 | 0.01 | 0.002 | － | 45 | －gain bandwiclin |
| $0 C 46$ | AMF | Dnp．PADT，ge | 73 | 83 | $\pi$ | － | 20 | 125 | ＜ 80 | ＜ | － | － | － | － | － | product |
| OC139 | AMP | npn，PADT．ge | 73.5 | 100 | 75 | － | 20 | 250 | 15 | 0.8 | － | － | － | － | － |  |
| OC140 | AMP | npm，PADT．ge | 74.5 | 100 | 15 | － | 20 | 250 | 75 | 0.8 | － | － | － | － | ＝ |  |
| 2 L 1255 | H\％ | DMP．MS，SI | 75 | 250 | 160 | 1.8 | 15 | － | 55 | 30 | 8 | － | － | － | － | T0－5 Package |
| 2 N 1257 | MU | pnp．u5， 31 | 75 | 250 | 160 | 1.8 | 30 | － | 55 | 30 | 8 | － | － | － | － | T0－5 Package |
| 201259 | Hu | pap．MS，31 | 75 | 250 | 160 | 1.8 | 50 | － | 55 | 30 | 8 | － | － | \％ | － | T0－5 Package |
| $\begin{aligned} & \text { OCA7 } \\ & \text { 2NO6 } \end{aligned}$ | $\begin{aligned} & \text { AMP } \\ & F A \end{aligned}$ | $\begin{aligned} & \text { pap, PADT.ge } \\ & \text { npon,DP.si } \end{aligned}$ | $\begin{aligned} & 75.5 \\ & 180(\mathrm{fr}) \end{aligned}$ | $\begin{gathered} 83 \\ 1 w \end{gathered}$ | $\frac{15}{175}$ | 6.7 | $\begin{aligned} & 20 \\ & 20 \end{aligned}$ | 125 | $200$ | $<3$ |  |  | E | － | － |  |
|  |  |  |  | Iw | 15 | 6.7 | 2 | － | 45 |  | 5 | ． 02 | － | － | － | GI，TR．SSO，SY，MA． |
| 2N702 | T1 | $\mathrm{npn}, \mathrm{DJ}, 31$ | 100 | 150 | 175 | 002 | 20 | 50 | 15.45 | 5 | － | － | － | ． 6 | － | FA．MA |
| 2N1507 | RH |  | 120 | 1w | 15 | 13.2 | 60 | 500 | 200 | ． 003 | 20 | $\infty$ | 600 | ． 07 | $\bigcirc$ | TI |
| $2 \mathrm{NL139}$ | TR | npon，GR，si | 150 | 500 | 175 | － | 15 | 25 | 20 | 25 | 8 | 12 | 10 | 0.7 | 5 |  |
| 2 S 501 | PH | Pap．MD ge | 175 | 60 | 100 | 0.8 | 15 | 50 | － | 1.0 | 1.75 | 0.013 | 0.007 | 0.00 | 35 | SPR，GI |
| 2M501A | PH | pnp，Mo．ge | 175 | 175 | $\infty$ | 0.8 | 15 | 50 | － | －1．0 | 1.1 | 0.013 | 0.007 | 1.0 | 35 | SPR．GI |
| $2 N 705$ 20710 | TI | pno．AJ，ge | 300 | 300 | 100 | 1 | 15 | 50 | 6 | 3 | 5 | 0.03 | 0.075 | 0.2 | 40 | MO，SY，GE，RA |
| 2M710 | TI | pnp，WS，ge | 300 | 100 | 300 | 4 | 15 | 50 | 6 | ． 3 | 5 | ． 06 | ． 075 | 80 | － | SY，MO，RCA，GE，RA |
| 2 W 711 | TI | pnp，We，ere | 300 | 300 | 100 | 4 | 12 | 50 | 6 | 0.3 | 5 | ． 07 | 0.1 | 50 | － | MO．SY，RCA，GE，RA |
| 24707A | mo | npon，OM，si | 350 | Iv | 175 | 6.7 | 70 | － | 30 | ． 01 | 4 | － | － | meec | － | Epitaxal |
| 2N706A | MO | npo，DM，si | 400 | Iw | 175 | 6.1 | 25 | － | 4 | ． 005 | 4.5 | ． 018 | ． 016 | － | － | $\begin{aligned} & \text { (Epitaxalmo) SY, TI } \\ & \text { PSI,HU,MA,GI } \end{aligned}$ |
| 2N7068 | $\pm 0$ | npon，Om，st | 400 | 10 | 1／5 | 6.7 | 25 | － | 4 | ． 005 | 4.5 | ． 018 | ． 016 | － | 1 | （mo．Epitaxial）SY，PSI |
| 2 n 73 | Mo | mon， $\mathrm{OM}, 31$ | 400 | 10 | 1／5 | 6.7 | 25 | － | 4 | ． 005 | 4.5 | ． 018 | ． 019 | － | － | MA，HU，GI （MO，Epitaial）MU，SY |

Low Level (concluded)

| $\begin{aligned} & \text { Type } \\ & \text { No. } \end{aligned}$ | Wig. | Type | 'a. | Moximum Retings |  |  |  |  | Charecteristics |  |  | Switching |  |  |  | Remarts: |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} \mathbf{w}_{c} \\ \left(\mathbf{n W w}^{\prime}\right) \end{gathered}$ | $T_{1}$ <br> (c) | $\mathrm{mm} / \mathrm{c}$ | $\begin{gathered} v_{c} \\ v \end{gathered}$ | $\begin{aligned} & I_{c} \\ & m m \end{aligned}$ | $\begin{aligned} & \mathrm{H}_{\mathrm{fe}} \\ & \mathrm{~h} F \mathrm{E} \end{aligned}$ | $\left\lvert\, \begin{aligned} & I_{c o} \\ & \mu \mathrm{a} \end{aligned}\right.$ | $\left\|\begin{array}{l} c_{c o e} \\ \mu \mu 1 \end{array}\right\|$ | Rise Time | $\begin{array}{\|c\|} \hline \text { stor } \\ \text { Tine } \end{array}$ | $\begin{aligned} & \text { Sat } \\ & \text { Volt } \end{aligned}$ | $\begin{aligned} & \text { Leain } \\ & \text { CuIf } \end{aligned}$ |  |
| 2 N 228 | mo | Dnp, DM, sis | 100 | 500 | 175 | 1 | 15 | 200 | 1 | 4 | 3.5 |  |  |  |  |  |
| NS345 | NA | npn, DM, si | 100 | 500 | 175 | 2.8 | 30 |  | 80-200 |  | 5 | - | - | - | - | Epilaxial, SY |
| 2 2T79A | PH | mpomo ${ }^{\text {mose }}$ | 950 | 50 | 100 | ${ }^{8 .} 8$ | 15 | 50 | -20 | 1 | 1.9 | - | Z | - | = |  |
| 2 NBAEA | PH | pmp.mo.ge | 550 | 60 | 100 | 8 | 15 | 50 | - | 1 | 1.9 | - | - | - | - |  |
| 2N834 | mo | mpn,DM, si | 500 | 10 | 175 | 6.7 | 40 | 200 | 5 | . 01 | 2.8 | 015 | 016 | - | - | Epitaxial, SY |
| 2N559 | WE | pmp.DG, ge | 750 | 150 | 100 | . 5 | 15 | 50 | 25 | 5 | - | . 002 | 003 | - | - |  |
| 2N1305 | TI | mp, M6, ge | 750 | 750 | 100 | 8 | 25 | 100 | 30 | 5 | 1.3 | . 001 | 000 | 1 | - | TO-5, non saluiater |
| ${ }_{2}^{2 N 917}$ | FA | non, DP, si | $800^{\circ}$ | 300 | 200 | 1.71 | 20 | 7 | 50 | 05 | - | - | - | masec |  | 4T |
| 2N167A | GE | npn, AS,ge | - | 65 | 85 | 1. | 30 | 75 | 30 | 0.6 | - | - | - | - | - | T |
| 2N20 <br> 2N3356 | PH | mpo.SB, ge <br> non,GJ.s | - | 25 500 | 85 | 0.5 | 6 | 15 | 30 | 0.5 | 1 | - | - | 0.04 | 20 | SPR |
|  | $\begin{aligned} & \text { GE } \\ & \text { GE } \end{aligned}$ | npp,GJ,ss | - | 500 500 | 175 | - | 60 45 | 25 25 | 52 | 1 | II | - | - | - | - |  |
| 2 m 3774 | SY | npm,A」, ge | - | 150 | 100 | 2 | 40 | 200 | 20-60 | 40 | 11 |  |  |  |  |  |
| 2N388A | SY | npn,AJ, ef | - | 150 | 100 | ? | 25 | 200 | 20-180 | 40 | - |  |  | ${ }^{\text {CGC }}$ (ma |  | GI |
| $\begin{aligned} & \text { 2N398 } \\ & 2 N 399 A \end{aligned}$ | RCA | pnp.AJ, ge | - | 50 | 55 | - | 105 | 100 | $\infty$ | 6 | - | - | - | 0.3 | 60 | GI |
| 2M43BA | SY |  | - | 150 150 | 100 | -5 | 15 | 200 | N | 2 | - | 0 | - | - | - |  |
| 2N439A | SY | npo, $\mathrm{N}, \mathrm{se}$ | - | 150 | Q5 | 2.5 | 25 | 200 | 15(min) | 10 | - | 0.7 | - | - | - |  |
| 2NHCA | SY | non,N.se | - | 200 | 85 | 3.9 | 25 25 | 200 | $\begin{gathered} 30(\mathrm{man}) \\ 40 \end{gathered}$ | $\begin{aligned} & 10 \\ & 10 \end{aligned}$ | - | 0.5 0.3 | - | - | - |  |
| 2Mag6 | PH | pnp.SB, ${ }^{\text {I }}$ | - | 150 | 140 | 1.3 | 10 | 50 | 5.0 | 1 | 6 |  |  |  |  |  |
| 2MS56 | SY | npm,AJ.ge | - | 100 | 85 | 1.66 | 20 | 200 | 5.0 | 25 | $\stackrel{-}{-}$ | 3.5 | $\overline{2}$ | $0.08$ | $\begin{array}{\|l} 16 \\ 55 \end{array}$ | max |
| 2 T 557 | SY | non, AJ.se | - | 100 | 85 | 1.66 | 20 | 200 | - | 25 | - | 6.5 | 2.5 |  |  |  |
| 2N558 | SY | npo, A, ge | - | 100 | 5 | 1.66 | 15 | 200 | - | 15 | - | 3.5 | 2 | 0.75 | 20 |  |
| 2N586 | RCA | pnp,N.ge | - | 250 | \% |  | 45 | 250 | 55 |  |  |  |  | 0.25 | 55 |  |
| 2N587 2N597 | SY | npo,Ad.ge | - | 150 | ® | 2.5 | 40 | 200 | 28 | 10 | 30 | - | - |  | 20 |  |
| 225597 $2 N 634$ | PH | mpp,N.ge | - | 250 150 | 100 85 | 3.3 | 45 | 400 300 | $\stackrel{5}{5}$ | 5 | 15 | - | - | 0.005 | $\pi$ |  |
| 2 24635 | GE | npm,N. A ge | - | 150 150 | 85 | 85 | 20 | 300 | 55 100 | 6 | - | - | - | - | - |  |
| 2ME36A | GE | npm,N, se | - | 150 | \% | - | 15 | 300 | 190 | 6 | - | - | - | - | - |  |
| 24707 24725 | FA | npon,OP.si | - | $1{ }_{1} 150$ | 175 | 6.7 | 28 | 50 | 12 | .005 | 5 | Q | - | - | - | (Epitaxial, MO), GI |
| 2476 | PH |  | - | 150 | 100 | ${ }_{1}^{2} .2$ | 15 20 | ${ }^{50}$ | 20 | 3 | - | 0.1 | - | - |  |  |
| 20771 | PH | non.sh,s | - | 150 | 150 | 1.2 | 20 | 100 | 7.5 | 218 | 1.3 | - | - | - | - |  |
| 2W72 | PH | npn,SA,si | - | 150 | 150 | 1.2 | 25 | 100 | 5.5 | . 5 | $\begin{aligned} & 1.3 \\ & 1.3 \end{aligned}$ | - | - | - | - |  |
| 20790 | RCA | pnp.DM, ge | - | 150 |  | 2.5 | 13 | 100 | 50 | 1 | 8 | - | - | - | - |  |
| 20795 | ${ }_{\text {RCA }} \mathrm{PH}$ |  | - | 150 | ${ }_{10} 8$ | 2.5 | 13 | 100 | 50 | 1 | 8 | - | - | = | - |  |
| 221119 | PH | Dmp.SAT, si | - | 150 | 140 | 1.3 | 10 | 50 | 5.0 | . 001 | 6.0 | - | - | - | - |  |
| 221122 | PH | map.ma.se | - | 25 | 85 | 0.63 | 12 | 50 | 8 | 5.0 | 6.0 |  |  |  |  |  |
| 2W1122A | PH | onp.ma, ge | - | 25 | ${ }_{5}$ | 0.63 | 15 | 50 | 1 | 5.0 | 6.0 | - | - | 0.1 | $\begin{array}{\|l} 25 \\ 25 \end{array}$ | $\begin{aligned} & \text { BPR GI GI } \\ & \text { BPR } \end{aligned}$ |
| $\begin{aligned} & 2 \text { W117S } \\ & 2 N 11>A \end{aligned}$ | $\begin{aligned} & \text { GE } \\ & \text { GE } \end{aligned}$ | map, N, ce | - | 200 | \% | - | 25 | 200 | $\infty$ | 6 | - | - | - | - | - |  |
| 2 W 1213 | RCA | Pnp, A.ge | - | 200 | ${ }^{6}$ | - | 25 | 200 | 0 | 6 | - | - | - | - | $\square$ |  |
| 211214 | RCA | Mon, MESA.ge | - | 75 | \% | - | 25 25 | 100 | - | 3 | - | 015 | 05 | - | - |  |
| 2 W 212 | RCA | Dmp,Mesa, ${ }^{\text {me }}$ | - | 78 | ${ }_{85}$ | - | 25 25 | 100 | - | 3 | - | . 015 | . 05 | - | - |  |
| 241216 | RCA | map.LESA.ge | - | 15 |  | - | 25 | 100 |  |  |  |  |  |  |  |  |
| 211217 | GE | Opm, $\boldsymbol{N}$, \% | - | 75 | ${ }^{2} 5$ | - | 20 | 25 | 40 | ${ }^{3}$. |  | 015 | 0 | - | - |  |
| 2 L 1271 | GE | non,G1,si | - | 150 | 150 | - | 30 | 25 | 20 | .01 | - | - | - | : | - |  |
| 2 L 1278 | GE | nem, GI, es | - | 150 | 150 | - | 30 | 25 | 33 | -01 | - | - | - | - | - |  |
| 201278 | GE | npm, GJ, 31 | - | 150 | 150 | - | 30 | 25 | 0 | . 01 |  |  |  |  |  |  |
| 241280 | GE | non, ©G, ${ }^{\text {ce }}$ | - | 73 | 85 | - | 10 | 50 | 50 |  |  | - | - | - | - |  |
| 2 N 1200 | GE | npen, M8, | - | 75 | 8 | - | 15 | 100 | 50 | 2 | - |  |  |  |  |  |
| 261298 241300 | $\left\lvert\, \begin{aligned} & \text { SY } \\ & R C A \end{aligned}\right.$ | mpa, N.ge | - | 150 | 100 | 2 | 40 | 200 | 35-110 | 0.1 | - |  | Fal | In |  |  |
| 2 LH 301 | RCA |  | - | 150 | ${ }_{8}^{68}$ | $\begin{aligned} & 25 \\ & 25 \end{aligned}$ | 13 | ${ }_{100}^{100}$ | 50 | 1 | 8 |  |  |  | - |  |
| 201304 | RCA | pno. DR, ${ }^{\text {ce }}$ | - | 240 |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 L 1404 | TI | Pnp,A, ge | - | 150 | ¢5 | 2.5 | 30 25 | 300 | 50 | 3 | $16^{-}$ | - | - | - | - |  |
| 2 L 1413 | GE | mop. A, re | - | 200 | 85 | 2. | 25 | 200 | 36 | 8 | 16 | - | - | - | - |  |
| 2m1414 | REA | Dap,AJ. se | - | 200 | 85 | - | 25 | 200 | 52 | 8 | - | - | - | - |  |  |
| 2W1450 | RCA | Dap,DR, ¢e | - | 120 | \% | - | 30 | 100 | 20 | 10 | - | - |  | - |  |  |
| $\begin{aligned} & 2 N 1177 \\ & 2 N 1499 \end{aligned}$ | $\begin{array}{\|l\|} \hline S Y \\ P Y \end{array}$ | $\left\lvert\, \begin{aligned} & \text { nom, N, se } \\ & \text { pap, MD, } \end{aligned}\right.$ | - | 200 | 75 | 1 | 40 | 100 | 25.0 | 100 | - | - | - | - | - |  |
| 2 W 1614 | GE | pmp, N, ge | - | 230 | 85 | 0.60 | 20 | 50 | ${ }_{3}^{38}$ | 1 | 25 | - | 0.12 | - | - |  |
| 201663 | PH | mpn,SA, | - | 150 | 150 | $1 . \overline{2}$ | 20 | 1000 | 7.5 | 25 | - | - |  | - | - |  |
| 2 L 1608 | RCA | onp.DM, ge | - | 150 | \% | 2.5 | 13 | 100 | 7 7 | 1.5 | $\overline{7}$ | - | - | - | - |  |
| 23168 | GE | non, $\mathrm{N}, \mathrm{se}$ | - | 75 | \% | - | 20 | 25 | 30 | 0.6 | - |  | - | - | - |  |
| 218173 | PH | pap, Mo, er | - | 50 | * | 83 | 13 | 100 | 3 | 1.6 | 1.5 | - | - | - | - |  |
| 21.008 | TI | nom, $\mathrm{N}, \mathrm{ge}$ | - | 150 | \% | 2.5 | 25 | 300 | - | 5 | 11 | - | $=$ | - | = |  |
| 211984 | RA | papan N | - | 375 | 100 | 0.2 | 60 | 14 | 9 | 10 | 1 | - | - |  | - |  |
| 2W1958 | RA | pmop, N, | - | 375 | 100 | 0.2 | 60 | 1. | 100 | 10 | - | - | - |  |  |  |
| $\begin{aligned} & 2011856 \\ & 21157 \end{aligned}$ | RA | pmp, N, | - | 375 | 100 | 0.2 | 60 | 14 | 5 | $\overline{-}$ | - | - | - | - | - |  |
| 2 LH 200 | ra | mpo, N.se | - | 375 | 100 | 0.2 | 60 | 1. | 50 | 10 | 1 | - | - | - | - |  |
| 2veces | ma | Mav, $\mathrm{N}, \mathrm{si}$ | - | 250 250 | 175 | 1.67 | 30 | 100 |  | . 01 | 8 | - | - | - | - |  |
| 2meen | ma |  | - | 250 | 175 | 1.67 | 50 | 100 | - | . 001 | 8 | - | $=$ | - | $=$ |  |
| 20ess | ma | peo, N, , < | - | 250 | 173 | 1.67 | 50 | 100 | - |  |  | - | - | - | - |  |
| 2 cecos | M | Pap, ${ }^{\text {N, }} 31$ | - | 230 | 175 | 1.67 | 80 | 100 | - | . 02 | 8 | = | - | - | - |  |
| 2uecol | M | 202, $\mathrm{N}, 4$ | - | 250 | 175 | 1.67 | 60 | 100 | - | .05 |  |  |  |  |  |  |

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| 2N1654 |  | 2N1899 | P.HF | C652 |  | 53 | A |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2N1655 | A | 2N1900 | P. HF | C653 | SP | OC54 | A |
| 2N1656 | A | 2N1901 | P.HF | CF45017 | HL | OC5S | A |
| 2N1657 | P | 2N1905 |  | CK4 | A | OC56 | A |
| 2N1658 | P | 2N1906 | P | CK4A | A | OC57 | A |
| 2N1659 | P | 2N1917 | A | CK13 | HF | OC58 | A |
| 2N1660 | P | 2N1918 | A | CK14 |  | OC59 | A |
| 2N1661 |  | 2N1919 |  | CK16 | HF | OC60 | A |
| 2 N 1662 |  | 2N1920 | A | CK17 | HF | OC74 | A |
| 2 N1663 | 4 | 2N1921 |  | CK17A | A | OC79 | A |
| 2N1665 | HF | 2N1922 | A | CK22 | A | OC80 | 4 |
| 2 N1667 | HL | 2N1924 |  | CK22A | A | OC139 | Ll |
| 2N1668 | HL | 2N1925 | A | CK228 | A | OC140 | LL |
| 2N1669 | HL | 2N1926 |  | CK22C | A | OC141 | L |
| 2N1670 | A | 2N1936 |  | CK25 | 1 | OC170 | H |
| 2N1672 | $A$ | 2N1937 |  | CK25A | A | OC171 | HF |
| 2 N1676 | HF | 2N1944 | A | CK26 | - | OC:200 | A |
| 2 N 1677 | HF | 2N1945 |  | CK26A | A | OC201 | A |
| 2N1678 |  | 2N1946 | A | CK27 | 1 | OCP70 | A |
| 2N1681 | HF | 2N1947 |  | CK27A | A | PADT20 | HF |
| 2N1683 | 4 | 2N1948 |  | CK28 | 1 | PADT21 | HF |
| 2N1684 | HF | 2N1949 |  | CK28A | A | PADT22 | HF |
| 2N1692 |  | 2N1950 |  | CK64 | A | PADT23 | HF |
| 2 N 1693 | P | 2N1951 |  | CK64A | A | PADT24 | HF |
| 2N1701 | HL | 2N1952 |  | CK64B | A | PADT25 | HF |
| 2N1702 | HL | 2N1954 | 4 | CK64C | A | PADT26 | HF |
| 2N1705 | A | 2N1955 | 4. | CK65A | A | PADT27 | HF |
| 2N1706 | $A$ | 2N1956 | U | CK658 | A | PADT28 | HF |
| 2N1707 | A | 2N1957 | 4 | CK65C |  | PADT29 | HF |
| 2N1709 | P.HF | 2N1958 | HF | CK66 | A | Padt30 | HF |
| 2N1710 | P.HF | 2N1959 | HF | CK668 | A | PADT31 | HF |
| 2N1711 | Hi | 2N1960 | HF | CK66C | A | PAdT40 | LL |
| 2N1714 |  | 2N1961 | HF | CK67 | A | Padiso | HL |
| 2N1715 | P | 2N1962 | HF | CK67A | A | PADT51 | LL |
| 2N1716 |  | 2N1963 | HF | CK678 | A | PADTGO | SP |
| 2 N 1717 | P | 2N1964 | HF | CK67C | A | PT600 | HF |
| 2 N 1718 |  | 2N1965 | HF | CK261 | A | PT601 | Hf |
| 2N1719 |  | 2N1969 | HF | CK262 | A | PTE50 | HF |
| 2N1720 |  | 2N1970 | HL | CK419 | 4 | PT850A | Hf |
| 2N1721 |  | 2N1971 | HL | CK420 | 4 L | P1900 | P |
| 2N1722 |  | 2N1972 | HL | CK421 | 4 | RT409 | HL |
| 2 N 1723 |  | 2N1973 | HL | CK474 | 4 | RT482 | HL |
| 2N1724 | P | 2N1974 | HL | CK475 | 4 | RT483 | HL |
| 2N1726 | HF | 2N1975 | HL | CK476 | 4 | RT484 | HL |
| 2 N 1727 | HF | 2N1978 | HL | CK477 | L | RT497M | HL |
| $2 N 1728$ | HF | 2N1983 | HL | CDT1310 |  | RTA98m | HL |
| 2N1730 |  | 2N1984 | HL | CDT1311 |  | RT656M | HL |
| 2N1731 | A | 2N1985 | HL | CDT1312 |  | RT657M | HL |
| 2N1742 | HF | 2N1986 | HL | CDT1313 |  | RT696M | HL |
| 2N1743 | HF | 2N1987 | HL | CDT1319 | P | RT696AM | HL |
| 2N1744 | HF | 2N1988 | HL | CDT1320 |  | RT697M | HL |
| $2 N 1745$ | HF | 2N1989 | HL | CDT1321 |  | RT697AM | HL |
| 2N1746 | HF | 2N1990 | HL | CDT1322 |  | RT698M | HL |
| 2N1747 | HF | 2 N 1991 | HL | CST1739 |  | RT699m | HL |
| 2N1748 | HF | 2N1994 | LL | CST1740 |  | RT1420m | HL |
| 2N1749 | HF | 2N1995 | L1 | CST1741 |  | RT1613M | HL |
| 2N1750 | HF | 2N1996 | 4 | CST1742 |  | RT5151 | HL |
| 2N1752 | HF | 2N1997 | L1 | CST1743 |  | RTS151 RTS 152 | HL |
| 2 N 1754 | 4 | 2N1998 | L | CST1744 |  | RT5202 | HL |
| 2N1755 |  | 2N1999 | LL | CST1745 |  | RT5203 | HL |
| 2N1756 |  | 2N2000 | LL | CST1746 |  | RT5204 | HL |
| 2N1757 |  | 2N2001 | L | CTP1104 |  | RT5212 | HL |
| 2N1758 |  | 2N2002 | 11 | CTP1105 |  | RT5230 | L |
| 2 N 1759 |  | 2N2003 | 4 | CTP1108 |  |  | HF |
| 2N1760 |  | 2N2004 | L | CTP1109 |  | So-2 | HF |
| 2N1768 | HI. | 2N2005 | L | CTP1500 |  | S0.3 | HF |
| 2 N 1769 | Hi. | 2 N 2006 | 11 | CTP1503 |  | ST15 | HF |
| 2 N 1779 | 1 | 2N2007 | 4 | CTP1504 |  | ST35 |  |
| 2N1780 | 1. | 2N2018 |  | CTP1508 |  | ST45 | F |
| $2 N 1781$ 2 N 1782 | 4. | $\begin{aligned} & \text { 2N2019 } \\ & \text { 2N2020 } \end{aligned}$ |  | CTP 1544 CTP1552 |  | ST401 | L |
| 2N1783 | HF | 2N2021 |  | CTP1553 |  | ST440 | P |
| 2N1784 | HF | 3N34 | HF | CTP1728 |  | ST450 | P |
| 2N1785 | HF | 3N35 | MF | GK13A | ${ }_{\text {HF }}$ |  | P |
| 2N1786 | HF | 3N36 | HF | GK16A | HF | ST4203 ST4204 | P |
| 2N1787 | HF | 3 3N37 | HF | GT74 |  |  |  |
| 2N1788 | HF | 3N45 |  | GT81 | ${ }^{\text {a }}$ | STC1103 |  |
| 2N1789 | H2 | 3N46 |  | GT109 | A | TMTB39 |  |
| 2 N 1790 | HF | 3N47 |  | GT123 | LP | TMT839 | HF |
| 2N1837 | HF | 3 N 48 |  | GT1200 |  |  |  |
| 2N1837A | A HF | 3N49 |  | GT1624 | SP |  | HF |
| 2N1838 | HF | 3N50 |  | KGS1004 | $\frac{L}{4}$ | TMTEA2 H |  |
| ${ }^{2 N 1838 A}$ | A HF | 3N51 |  | KGS1005 |  | TMT843 ${ }^{\text {H }}$ |  |
|  | HF | 3N52 |  | LT11 |  | TMT843 |  |
| 2 N 1839 A | A HF | 3 N54 |  | LT12 |  | wxilsua |  |
| 2N1840 | HF | 8177 |  | LT13 |  | WX115UB |  |
| 2N1840A | A HF | 8178 |  | LT14 |  |  | P |
| 2N1841 |  | 8179 |  | P LT15 |  | WX115UD | P |
| 2N1864 | HF | 81085 | HL | MA. ${ }^{\text {ma }}$ | HF HF | Wx115UD | P |
| ${ }^{2 N 1865}$ | HF | 81154 | LL | MA.2 |  | W115WB | P |
| $2 N 1866$ | HF | 811544 | LL | NS345 | HL | W×115W8 | P |
| 2 N1867 | HF | C101 | $L$ | $\mathrm{OCl22}^{\text {O }}$ | ${ }_{\text {H2 }}$ | WX115WC | P |
| 2 N 1868 | HF | C102 | L | $\mathrm{OCl2}^{\text {O }}$ | HL | $\underset{W \times 115 \times A}{\text { Wxil }}$ | P |
| 2N1886 | P | C103 | LL | OC24 | HL | W×115×A | P |
| 2N1889 | HL | C106 | LL | OC28 | HL | W×115x8 | P |
| 2N1890 | HL | C301 | LL | OC29 | HL | WX115XC | P |
| 2N1893 | HL | C302 | LL | OC30 |  | W×115×0 | $P$ |
| 2N1894 | P | C611 | SP | OC35 | HL | wxilicua | $P$ |
| 2N1895 |  | C612 | SP | OC36 | HL | Wx118U8 | $P$ |
| 2N1896 |  | C613 | SP | P OC41 | HF | wx118UC | $P$ |
| 2N1897 |  | C614 | SP | P OC45 | HF | W×118×A | $P$ |
| 2N1898 |  | C650 | SP | P OC46 | 4 | W×118×8 | $P$ |
| 2N1899 |  | C651 | SP | P OC47 | LL | WX118xC | $P$ |

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There's a Better Way... to cool a transistor. The fish don't like this sort of briny nonsense, either. The one on the left is a rare species known as Pisces Lingua, or underwater talking fish. He's telling the rest of his buddies that some irate electronics engineer probably gave this transistor the deep six because of thermal runaway. Or maybe its derating curve was all wet. The other fish are mute on the matter. They could inform Pisces Lingua that the Birtcher Corporation makes a semiconductor heat radiator that would not only cool the transistor, but boost its efficiency $25 \%$ to $27 \%$. But they refrain from comment because there's a hungry gleam in his eye. If this makes you hungry to do business with me, write today for my catalog and other stuff. Don't ask me to send you any fish. But I'll send you an Honorary Membership Certificate to my Society. Write to: Charles F. Booher, Secretary, There's a Better Way Society of America, Inc., The Birtcher Corporation / Industrial Division, $74 \overline{5}$ S. Monterey Pass Rd., Monterey Park, California; phone ANgelus 8-8584, TWX LA 2177.

Cool!
Write for my
non-fishy Transistor Radiator Catalog

## 웅

B
Sizes available for just about every commonly used transistor. So yours are different? Maybe I'll provide a radiator anyway - no hooks.

## Transistor Data Sheets-

# What They Mean and How to Use Them Properly 


#### Abstract

Electronic Design's Ninth Annual Transistor Data Chart (p 33) contains 1714 transistor types with abbreviated specifications. For complete details on the various transistor parameters and explanation of the test conditions used, reference to manufacturers' data sheets is necessary. Thus, the Transistor Data Chart is intended to guide the design engineer to several types; the specific selections is then based on complete device characteristics and price as obtained from the manufacturer. The relationship which exists between published characteristics and design requirements is discussed and a useful circuit design check list is included.


## Mitchell Baker, Jordan V. Sukert <br> Motorola Semiconductor Div., Inc. <br> Phoenix, Ariz.

AWELL-PREPARED transistor data sheet, properly interpreted by a circuit design engineer, is an extremely useful design aid. To meet the present demands for circuit and systems reliability, an understanding of transistor specifications and their relationship to design requirements is a valuable design asset.

Basic Structure of a
Transistor Data Sheet
A modern, well-prepared data sheet should provide the design engineer with all the necessary information for selecting a transistor capable of performing a particular job. To accomplish this, the data sheet is normally divided into six general sections. A description of the device is given first. followed by sections on absolute ratings, electrical and thermal characteristics, mechanical data and applications information.
The description of the device usually gives the broad general application which permits the designer to classify transistors ac-

If you would llike an additional copy of the Tranglator Data
Chart Seetlon circle 251 on the Reader-Service Card.
cording to his specific requirements. Thus. a typical power transistor description might indicate whether the unit was designed for audio work or switching applications. In addition, the power and/or current rating is specified, the polarity ( pnp or npn ) is given, and the type of material is indicated. At a glance, therefore, the engineer can determine if a particular transistor or group of transistors is suitable for using in a particular purpose.
From this point, however, the selection of a specific transistor for a particular project becomes more involved. The unit must be considered in terms of its various electrical ratings and characteristics to make sure that it fits the application from every conceivable standpoint. In addition, the engineer is responsible for selecting the least expensive transistor

## Distinction Between

Ratings and Characteristics
A rating is defined as a limiting value assigned by the manufacturer which, if exceeded, may result in permanent damage to the device. On the other hand, a characteristic is a measurable property of the device under specific operating conditions for
which the transistor will provide satisfactory and reliable performance

Absolute Maximum Ratings are those ratings beyond which degradation regarding the life and reliability of a transistor may be expected. These ratings are based on internal physical construction, semiconductor material and manufacturing processes. Because these are "ratings", most data sheets will not indicate test conditions under which these "ratings" are specified. Therefore, "ratings" are the extreme capabilities of a transistor and are not intended to be used as design conditions.

For example, under absolute maximum ratings, the letter $B$ placed before a characteristic symbol usually means breakdown. Therefore, $B V_{C B O}, B V_{C E O}, B V_{C E S}, B V_{C E S}$, and $B V_{\text {fв }}$ represent the breakdown ratings of the device; when these ratings are exceeded, an avalanche or breakdown condition may take place and destroy a transistor. Breakdown is dependent upon temperature and an


Fig. 1. Typical output characteristics of a Motorola 2N1530 power transistor.
arbitrary voltage and current condition，the combination of which can trigger the ava－ lanche effect．
As a practical example，the graph in Fig． 1 illustrates the typical output characteris－ tics of a 2N1530 power transistor．The ab－ solute maximum voltage $B V_{C E O}$ is shown as being 45 v ，the absolute maximum cur－ rent is shown as 5 amp ．

With an absolute maximum power rating of 90 w （as shown on the data sheet for this particular transistor），it is now possible for the design engineer to calculate and plot a maximum voltage－current relationship which must not be exceeded．
Thermal characteristics，listed with the absolute maximum ratings，are expressed in degrees $C$ per watt and define the dissipa－ tion capability of the transistor regarding the junction temperature in relation to the transistor case temperature．

## Electrical Characteristics <br> Indicate Design Centers

Whereas the absolute maximum specifica－ tions provide the limits beyond which reli－ able operation cannot be obtained，this sec－ tion of the data sheet contains the device design centers．When discussing any specific characteristics，the test conditions must be defined in order to achieve a common under－ standing between the user and the manu－ facturer of the transistor．Almost every pa－ rameter listed on a data sheet is subject to variation among manufacturers due to these test conditions．Motorola data sheets cover－ ing the power transistor series from 2N1539 through 2N1548 will be used to discuss each parameter in order．（See Fig．2）．
Collector－Base Leakage Currents：$I_{\text {CRO }}$ is a term initially used to signify the quality of a transistor．Actually，three very definite $I_{\text {ros }}$＇s are of importance to the designer． The first is the reading taken at some low collector－base voltage，in this case， $2 v$ with a maximum value of $I_{c k \prime}$ indicated at this voltage．This value，for all practical pur－ poses，represents the thermal component of the collector current which cannot be reduced by further decrease of $V_{\text {CR．}}$ ．As the ambient temperature increases，the leakage current increases．Using the arbitrary rule that the thermal component of current will double for every 10 C ，the design engineer can pin－ point the temperature component of the leakage current．
Collector－Base Voltage Characteristics：The second component of $I_{\text {rпо }}$ which is important in high－temperature usage is the current due to the collector－base voltage with the emitter

ELECTRICAL CHARACTERISTICS，GENERAL（AI $25^{\circ} \mathrm{C}$ Case Temperalure unless otherwise specified）

| Parsater | 8pmosi | Min | Tvp | Mas | Valk |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Iseo | 二 | 二 | $\begin{aligned} & 2.0 \\ & 2.0 \\ & 2.0 \\ & 2.0 \\ & 2.0 \\ & \hline \end{aligned}$ | mA |
| $\begin{aligned} & \text { Cllector-Base Cutof Current } \\ & \mathbf{V}_{C A}=-2 \mathbf{V} \text { (all eypes) } \end{aligned}$ | Iceor | － | － | 200 | ${ }^{4} \boldsymbol{\lambda}$ |
|  | $1{ }_{\text {raco }}$ | － | － | 20 | mA |
| $\begin{aligned} & \text { Emitter- Base Cuton Curpent } \\ & V_{\text {oin }}=12 \mathrm{~V} \text { (all types) } \end{aligned}$ | Ieao | － | － | 0.5 | mA |
|  | 80 | $\begin{aligned} & 30 \\ & 45 \\ & 60 \\ & 75 \\ & 70 \end{aligned}$ | 二 | 二 | volis |
|  | les | 二 | 二 | $\begin{aligned} & 20 \\ & 20 \\ & 20 \\ & 20 \\ & 20 \\ & \hline \end{aligned}$ | mA |
|  | BVicu | $\begin{aligned} & 20 \\ & 30 \\ & 40 \\ & 50 \\ & 60 \\ & \hline \end{aligned}$ | 二 | 二 | volts |
|  | $8 V_{\text {cmo }}$ | $\begin{aligned} & 90 \\ & 60 \\ & 80 \\ & 106 \\ & 120 \end{aligned}$ | 二 | 二 | volts |

ELECTRICAL CHARACTERISTICS，COMMON EMITTER（AI $25^{\circ} \mathrm{C}$ Case Temperature unless otherwise specified

| Currene Gain $\mathbf{V}_{\mathrm{co}}=-2 \mathbf{V}, 1 \mathrm{c}=3 \mathrm{~A}$ 2N1539．2M1540． 2 W15A1．2N15A2．2M1543 2N1544．2M154S．2N1546．2N1547．2N1548 | ho． | $\begin{aligned} & 50 \\ & 75 \end{aligned}$ | ＝ | $\begin{aligned} & 100 \\ & 150 \end{aligned}$ | － |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Ease－Emitter Drive Voltage $l_{1}=3 \mathrm{~A} .1 \mathrm{~m}=300 \mathrm{~mA}$ 2N1539．2N1540．2N1541．2W1542．2N1543 2W1544．2W1585．2M1546．2N1547．2N1548 | $\nabla \cdot$ | ＝ | ב | $\begin{aligned} & 0.7 \\ & 0.5 \end{aligned}$ | volts |
| Collector Saturation Voltage $1 .=3 \mathrm{~A} .1 \mathrm{n}=300 \mathrm{~mA}$ <br> 2N1539．2N1560，2N1541，2N1562．2W1543 <br> 2N1544，2N154S．2N1546，2W1547，2N1548 | $V_{\text {cra }}(\text { eat })^{\text {a }}$ | － | 0.2 0.1 | $\begin{aligned} & 0.6 \\ & 0.3 \end{aligned}$ | volts |
| Frequency Cutoff $\mathbf{V}_{10}=-2 \mathbf{V} .1=3 \mathbf{A}$ 2N1539．2N1540．2N1S41，2N1542 2N1543 2N1544．2N1545．2N（S46．2W154）．2N1548 | f．． |  | 4 |  | kc |
| Switching Characteristics <br> $I_{1}=3 \mathrm{~A}$ <br> Delay＋Rise Time <br> 2N1539，2N1540．2N1541，2N1542．2N1543 <br> 2W1S44．2W154S，2N1546，2W1547．2W1548 <br> Siorage Time <br> 2N1539．2N1540，2N1541，2N1542，2N1543 <br> 2N1544，2N1545．2N1546，2N1547，2N1548 <br> Fall Time <br> 2N1539．2N1540，2N154i，2N1542，2N1543 <br> 2M1544，2N1545．2N1546．2N1547，2M1548 | $1+6$ | － － ＝ | 1 5 5 3 5 5 8 | - | usec usec usex |
|  | 8 c ： | 3.0 <br> 5.0 | 6.0 7.5 | － | mhos |

Fig．2．Electrical characteristics contained in a transistor data sheet．
open．The data sheet indicates that $V_{\text {ch }}$ at 25 v on the 2 N 1539 power transistor pro－ duces a maximum leakage of 2 ma ．This volt－ age component is not temperature sensitive． Therefore，the design engineer wishing to determine his leakage value at some higher temperature（e．g．$T_{1}=75 \mathrm{C}$ ），can safely assume that the maximum increase in the thermal component of leakage current will be 32 times $200 \mu$ a（using the＂doubling－ every－10 C＂rule）．Adding to this the 2－ma
voltage component results in a value of 8.4 ma maximum leakage at 75 C with 25 v across the transistor．All future references to temperature will refer to the transistor case temperature and not the ambient tem－ perature．
High－Temperature Collector－Base Leakage Currents：Since there are many voltages and many applications to be considered，it is difficult for any manufacturer to specify leakage under all voltages at all tempera－


TRENSISTORS-1961


Fig. 5. Output characteristics of the 2 N351A with the saturation region indicated.
tures hence, the third $I_{\text {спо. }}$. Motorola specifies a guaranteed maximum leakage at 90 C at a voltage level well within reliable usage of any given transistor. The selection of the onehalf collector-emitter breakdown voltage ( $B V_{\text {ce:s }}$ ) rating for the high temperature test is an arbitrary one but is established at a point where the manufacturer knows the device will be in a reliable operating area.
Emitter-Base Cut-Off Current (IF, ${ }_{\text {Fis }}$ ): One of the least used parameters on a data sheet
 of any given junction within a transistor; therefore this limit is shown at a region where most design will be taking place. The emitter-base diode breakdown voltage rating is indicated by the $B V^{\prime}: m$, listed under the absolute maximum ratings.
Collector-Emitter Leakage Current (I, w): The $X$ in this symbol means that there is


Fig. 3. Collector characteristics of a power transistor in a common emitter connection.


Fig. 4. The current gain, $h_{\text {re }}$ of alloy transistors decreases with increased collector current.
some known back-bias voltage applied to the base-emitter diode. For each transistor, this back-bias must be specified as a test condition for any given $\boldsymbol{I}_{\text {cE, }}$ or $\boldsymbol{B} \boldsymbol{V}_{C E X}$ rating. This rating is very useful in designing power converters where one transistor is conducting while the other transistor is back-biased in the off condition waiting for transformer action to turn it back on. It is more convenient to apply a given voltage and guarantee that the current will not be above a certain maximum value than to apply a test current and see if the voltage will be above a certain minimum value. The latter test could be related to a second breakdown ${ }^{1}$ type of relationship. On many diodes, applying a given test current could show a voltage rating of many volts above the manufacturer's listed rating. The collectoremitter could, for example, possibly with-
stand 150 to 200 v ; however, power dissipation could be exceeded.
Collector-Emitter Breakdown ( $B V_{C E S}$ ): The most important rating that the engineer can consider when selecting the transistor for his circuit is $\boldsymbol{B} V_{\text {cES }}$, see Fig. 3.

Almost all power transistor applications require source voltages, collector-to-emitter, thus $V_{C E}$ ratings must be equal to or larger than the source voltage; inductive loads will make this requirement higher. For the design engineer, a useful rating would be $B V_{C E R}$ which falls between $B V_{C E B}$ and $B V_{\text {ceo }}$ in alloy transistors. On many test conditions, high dissipation can be experienced with the combination of test voltage and test current. Therefore, many tests are specified as sweep tests or pulse tests where the duty cycle is low enough that the maximum junction temperature is not exceeded. These tests should be performed with the transistor mounted on an adequate heat sink.
Collector-Emitter Breakdown Voltage with the Base Open ( $\boldsymbol{B} \boldsymbol{V}_{\text {ceo }}$ ): This test is related to $I_{C B O}$ and the gain characteristic $h_{F E}$. With the base open, a condition can be reached where $h_{F E}$ will multiply the $I_{\text {rao }}$ at a given voltage and start an avalanche condition as the junction temperature rises due to self-heating. This can quickly reach breakdown conditions if not carefully tested by the sweep method.

A possible cause of transistor failure is lack of $B V_{c E U}$, especially at high voltages; this condition is often encountered in application such as series-regulated power supplies and power amplifiers. In switching circuits, this condition can exist when the transistor is switched from on to off, thus passing a region where the base has infinite resistance or is essentially open.
Collector-Base Breakdown Voltage (BV $V_{\sigma_{1}}$ ): This rating will show the limitation of the collector-base junction, but is a rating which is only occasionally used in actual circuit considerations. Many engineers make the error of selecting a transistor based on this parameter putting themselves into a highpriced, low-availability category, when actually the true ratings could have been defined by $B V_{\sigma k}$. Circuits should be carefully analyzed to determine if $B V_{г}$ or some collector-to-emitter rating is the controlling factor under the worst conditions.
Current Gain ( $\boldsymbol{h}_{F E}$ ): This is the most arbitrary of all test conditions listed on a data sheet. For alloy transistors, current-gain is a function of collector current and in most
cases will decrease when $I_{c}$ increases, see Fig. 4.

It is best to design around data sheet limits. However, circuit requirements could dictate current gain spreads. Under these circumstances, it would be beneficial for the design engineer to work closely with the manufacturer to obtain a special device. This parameter is one that will vary to some degree with life, and is therefore used as an end-of-life characteristic.
Base to Emitter Voltage ( $V_{\text {HE }}$ ): This parameter denotes the input voltage at the specified test condition, required in the design of power converters and switching circuits. The test for this parameter is usually performed with the transistor in saturation. Saturation Voltage ( $V_{c \in, a l}$ ): Saturation voltage $V_{C E \text { vat }}$ (Fig. 5) is the minimum voltage necessary to maintain normal transistor action at a particular collector current. At collector voltages lower than $V_{V, \text { nat }}$ the base-collector diode is forward biased and the current-voltage relationship changes abruptly. Thus, the saturation voltage is the minimum collector-emitter voltage required to maintain full conduction when enough base drive is supplied; further applications of base drive will reduce $V_{r \text { : }}$ ot. Since the $V_{i, ~ s a l}-I_{c}$ curve is almost a straight line, some transistor manufacturers list the characteristic as saturation resistance ( $V_{(E, 01}$ ).

Transistor efficiency in converters is a function of switching speed and power dissipated in the fully-on condition. A very low saturation voltage is extremely desirable and is a function of the collector current and base current drive. Saturation voltage rises with an increase in collector current and is inversely related to the gain $\left(h_{r t}\right)$ of the transistor.
Common Emitter-C'ut-Of Frequency ( $f_{a f}$ ): Current gain frequency cut-off ( $f_{a}$ ) for the common emitter configuration, (also called the beta cut-off frequenc $y$ ) is the frequency where the small-signal, forward-current gain is 0.707 of the current gain value at a given reference frequency. The common base frequency cut-off $F_{a b}$. (generally not specified for power transistors) is appre nately equal to $h_{l e}$ times $F_{\text {ae }}$.
Power Transistor Circuit Design

## Check List

Without going into details of the external circuit requirements, the following questions should be considered during selection of a moper power transistor.
(comfinued on $p 80$ )


Four overlapping Beta Ranges - High meter resolution Direct reading with test circuit power off

SPECIFICATIONS
New Sierra 2198 4-range Transistor Tester reads Beta directly in the circuit; also measures lco, Beta out of circuit.
Less downtime and less danger of damage to transistors under test with this new Sierra instrument-battery-operated, light weight, portable, easy to use.
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In circuit: $\pm \begin{array}{ll} \pm 20 \% & \text { for external loads over } \\ 500 \text { ohms. }\end{array}$ Improved 1 mproved accuracy above
500 ohms, usable readings Sut of circuit: $\begin{aligned} & \text { below } 500 \text { ohms. } \\ & \pm 10 \%\end{aligned}$ Out of circuit: $\pm 10 \%$

Power: $\begin{aligned} & \text { Internal battery, mercury or } \\ & \text { zinc-carbon type, } 600 \mathrm{hrs} \text { av. } \\ & \text { life: }\end{aligned}$ zinc-carbon type, 600 hrs . av
life. output indicated on
front-panel meter. $\begin{aligned} & \text { Operating } \\ & \text { Temperature: } 32 \text { to } 149 \text { F }\end{aligned}$
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Temperature:
32 to $149 \quad$ F

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Higher power with cooler operation (coal transistors are reliable trausustorn)
Low input impedance (200 rus the veal 500 means more signal gets into the tramistor occumeme and wore current flow out !)
Lower saturation resistance (10) vo. the usual 25 means more power where you torus the unit on!)




Yoltanm Ratings ( $25^{\circ} \mathrm{C}$ ) Voltages
Collocser to Base
Collector to Emitter Collector to Emitter
Emitter to
to Temperatures Temperature i Storage
Operating Junction
 $25^{\circ} \mathrm{C}-5$ wats.* $\therefore$ - orate $5.72 \mathrm{mw} /{ }^{\circ} \mathrm{C}$ increase in ambient temperature above $25^{\circ} \mathrm{C}$
 Collector
(lc $=100$ bane Voltage ( $1 c=100 \mathrm{Ho}, 16=0$ )
Collector 10 E miner Voltage





 Cutoff Characteristics
Collector Current ( $\mathrm{I}_{\mathrm{B}}=0, \mathrm{~V}_{\mathrm{Ca}}=30 \mathrm{~V}$ ) Collector Current (High Tomparolura)
( $18=0, \mathrm{Vca}=30 \mathrm{~V}$, TA $=150^{\circ} \mathrm{C}$ ) -Pules Test: 300 uses. $2 \%$ Duty Cycle


## tested

## 98A, 2N656A, 57A...come from General Electric



Positive internal atmospheric control achieved through the use of General Electric's buffered-sieve encapsulation technique, higher power dissipation with lower saturation resistance and lower input impedance are important features of this line of top quality one to five watt audio switches. Especially well suited for either high level linear amplifier or switching applications, these are the industry's most thoroughly characterized and tested medium power silicon double diffused NPN transistors available today. Just take a look at the extended life test charts illustrated for convincing evidence of long term stability and reliability.
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Fig. 6. The relioble area of collector operation is contained within the shaded region shown.



Fig. 7. Curves used in determining peak power of $a$ power transistor.

1. What will the maximum load current requirement be?
2. What is the output voltage desired and what are the low and high line values of the source or input voltage?
3. What driving power is available? This factor is needed to determine the dc current gain required fo the maximum and minimum load currents.
4. What type of heat sink will be available?
j. What will the ambient temperature excursions be?
5. Are there any frequency requirements such as a response to a step function?
6. What are the cost limitations and availability requirements when considering large scale production?
In referring to the above questions, perhaps the most critical point is the collectoremitter voltage requirement for the specific design conditions. Knowing the voltage extremes and the maximum load current, the power dissipation must be considered in relationship to the heat sink available. With this knowledge, a search is then made for the thermal resistance or power dissipation capability of a suitable device. At this point, a decision might be required necessitating parallel operation for excessive load current requirements or series operation for highvoltage applications. ${ }^{2}$ Series or parallel operation is well worth considering because of the lower price and better availability of less-specialized types. If heat sink considerations limit single power transistor dissipation capability, series operation may be attractive. For a given heat sink size and a stated maximum dissipation, the individual junction temperature rise for two transistors in series will be one-half the rise of a single unit. The same advantage is offered with parallel operation.

Assume a condition of 80 C case temperature and power dissipation sufficient to raise the junction temperature of a single unit to 105 C . This would indicate a power dissipation of approximately 30 w if the thermal resistance junction to case was 0.8 C per watt. This 30 w would be divided between two transistors if series operation was used therefore dissipating 15 w per unit or a junction temperature rise of 12.5 C per transistor. The junction temperature will now be 92.5 C for both devices instead of the single unit at 105 C .

## Checkout for Reliable

## Circuit Design

A design is not complete until an examination is made of the reliability of the circuit.

It is of utmost importance to examine the safe area of operation and the load line characteristic of each power transistor used in any equipment.

Definite areas of reliable operation can be predicted in devices such as germanium pnp power transistors. In Fig. 6, the region indicated as "maximum reliability" denotes safe operation with little chance of device burnout. The cross-hatched area is $\Omega$ derated zone of operation which may be considered safe for momentary excursions but may result in a collector-to-emitter short. To evaluate line or load surges which instantaneously place the transistor into higher dissipation, a set of curves based upon the thermal time constant, pulse width, and duty-cycle is included on the data sheet as shown in Fig. 7. Determination of Peak Power: The peak allowable power is; from Fig. 7,

$$
P_{p}=\frac{\left(T_{1}-T_{A}-\theta_{A_{A}} P_{n a}\right)}{\theta_{l c}\left(\frac{1}{C_{e}^{\prime}}\right)+\theta_{C \cdot A}\left(t_{1} / t\right)}
$$

$C_{p}$ is a coefficient of power as obtained from the data chart. $T$, is junction temperature in $\mathrm{C} ; T_{1}$ is ambient temperature in C ; $\theta_{J e}+\theta_{C_{1}} ; t_{1}$ is pulse width; $t$ is the pulse period; $\left(t_{1} / t\right)$ is the duty cycle; $P_{0}$ is a constant power dissipation and $P_{p}$ is the additional allowable pulse power dissipation above the amount of $P_{0 s}$.

The above equation applies when a heat sink is used which has thermal capacity much larger than the transistors' thermal capacity

The chart in Fig. 7a is normalized with respect to the thermal time constant, which is on the order of 50 msec for these power transistors. Consider a typical example as follows:
$P_{0}=10 \mathrm{w} \quad T_{A}=40 \mathrm{C}$
Pulse width $\left(t_{1}\right)=1 \mathrm{msec}$
Duty Cycle $\mp 20 \sigma_{c}$
$\theta_{c .1}=3 \mathrm{C} / \mathbf{w}$ $\theta_{s c}=0.8 \mathrm{C} / \mathrm{w} \quad T_{/ m}=100 \mathrm{C}$
Solution: Enter the graph at $t_{1} \tau=1$ msec 50 msec , and duty cycle $20 c_{\%}$. Find $C_{p}=5$. Solve equation

$$
P_{p}=\frac{100-40-(3+0.8) 10}{\frac{0.8}{5}+3 \times 0.2}
$$

$P_{\mu}=29 \mathrm{w}$ in addition to the steady 10 wr resulting in 39 w peak. - -

## Reference

1. "How to Design Economical High-Voltage Circuits" Motorola Semiconductor Products, Inc., Phoenix. Ariz. 2. Motorola Power Transistor Handhook, First Edition, pg. 33-34.

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| :---: | :---: | :---: | :---: | :---: |
| Type | Minimum Peak Reverse Volt and Minimum Forward Breakover Voltage (volts) | Maximum Average Forward Current at $90^{\circ} \mathrm{C}$ case (amps) | Package Configuration | Package |
| TCR4050 | 400. | 50. | 1ko" hex | A |
| TCR3050 | 300. | 50. | 16/ ${ }^{\text {c }}$ hex | A |
| TCR2050 | 200. | 50. | 14." hex | A |
| TCR1050 | 100. | 50. | 1\%0* hex | A |
| TCR550 | 50. | 50. | 13, " her | A |

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Transitron continues to offer the broadest line of Silicon Controlled Rectifiers in the industry. Available in six different and versatile packages, these rugged devices offer greater reliability and efficiency while replacing thyratrons, magnetic amplifiers, and other switching devices in many varied applications.

|  | SILICON CONTROLLED RECTIFIERS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Type | Minimum Peak Reverse Voltage and <br> Minimum Forward Breahover Voltage (volts) | Maximum Forward (am at $25^{\circ} \mathrm{C}$ case | Average Current ps) at $100^{\circ}$ case | Package Configuration | Pach age |
| TCR1020 | 100. | 20. | 10. | "ha" hex | B |
| TCR2020 | 200. | 20. | 10. | "Ko" hex | 8 |
| $\begin{aligned} & \text { TCR3020 } \\ & \text { TCR } 4020 \end{aligned}$ | 300. | 20. | 10. | "Kos hex | 8 |
| TCR1010 | 100. | 10. | 5.0 | "ho" hex | B |
| TCR2010 | 200. | 10. | 5.0 | "Ka" her | B |
| TCR 3010 | 300. | 10. | 5.0 | "Ks* hex | 8 |
| TCR4010 | 400. | 10. | 5.0 | "has her | 8 |

## SILICON CONTROLLED RECTIFIERS - closely controlled electrical characteristics plus a high degree of mechanical ruggedness

## 11/6", $/ 16{ }^{"}$, $7 / 16^{"}$ HEX PACKAGES (B, C, D)

Transitron's Silicon Controlled Rectifiers are PNPN high power bistable controlled switching devices. They are analogous to a thyratron or ignitron, with far smaller triggering requirements and microsecond switching. The low conduction drop permits current ratings up to 20 amperes and provides high efficiency with low cooling requirements. Also, blocking voltages up to 500 volts permit the smallest packaging yet made possible for high power control. Operation at 125 C is permissible with derating.

## TO-5 PACKAGE (E)

The TO.5 package configuration also has a low conduction drop which permits operations from 25 ma to 1 ampere (types 2N1595-2N1599) and 5 ma to 1 ampere (Types TCR 251 - TCR 4001). Operating and storage temperature range is from -65 C to 150 C . Typical turn-on time is 0.2 to 0.3 microseconds; turn-off time is 1.0 to 1.2 microseconds.

## T0-18 PACKAGE (F)

Transitron's Silicon Controlled Switch is also a PNPN bistable unit featuring high gate sensitivity and low holding currents for low level switching from 1 ma to 200 ma. Further, these units are particularly useful in controlled rectifier trigger circuits as these switches offer precise and consistent control of the firing angle, Typical turnon time is 0.2 microseconds; turn-off time, 1.0 microseconds.
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| SILICON CONTROLLED RECTIFIERS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Type | Winimum Peák Reverse Voltage and <br> Minimum Forward Breakover Voltage (volts) | Maximum Average Forward Current (amps) at $25^{\circ} \mathrm{C}$ case at $100^{\circ}$ case |  | Pack. Config. uration | Package |
| 2N683 | 100. | 16. | 8. | Ko" hex | C |
| 2N685 | 200 | 16. | 8. | \% ${ }_{6}$ " hex | c |
| 2N687 | 300. | 16. | 8. | $\%_{0}{ }^{\prime \prime}$ hex | C |
| 2N688 | 400. | 16. | 8. | $Y_{0}{ }^{\prime \prime}$ hex | C |
| 2N689 | 500. | 16. | 8. | \%," hex | C |
| 2N1844 | 100. | 10. | 4. | Ko" hex | c |
| 2N1846 | 200. | 10. | 4. | \%o" hex | c |
| 2N1848 | 300. | 10. | 4.* | \%o" hex | C |
| 2N1849 | 400 | 10. | 4.0 | $\mathrm{K}_{0}{ }^{\text {a }}$ hex | C |
| 2N1850 | 500. | 10. | 4. | \% ${ }^{\prime \prime}$ hex | C |
| TCR1005 | 100. | 5.0 | 3.0 | \%o." hex | 0 |
| TCR2005 | 200. | 5.0 | 30 | \%/10" hex | D |
| TCR3005 | 300. | 5.0 | 3.0 | \%o" hex | 0 |
| TCR4005 | 400 | 5.0 | 3.0 | \%/8" hex | D |
| 2N1600 | 50. | 3.0 | $3.0{ }^{\circ}$ | hos hex | D |
| 2N1601 | 100 | 3.0 | $3.0{ }^{\circ}$ | 1/6" hex | D |
| 2N1602 | 200. | 3.0 | $3.0{ }^{\circ}$ | \%/6" hex | D |
| 2N1603 | 300 | 30 | $30^{\circ}$ | \%/6" hex | 0 |
| 2N1604 | 400. | 3.0 | $3.0{ }^{\circ}$ | \%/" hex | D |
| 2N1772A | 100. | 4.7 | 3. | hto hex | 0 |
| 2N1774A | 200 | 4.7 | 3. | \%/s" hex | D |
| 2N1776A | 300. | 4.7 | 3. | \%ho hex | D |
| 2N1777A | 400 | 4.7 | 3. | $h_{0}{ }^{\text {a }}$ hex | 0 |
| 2N1772 | 100 | 4.7 | 3. | 'how hex | D |
| 2N1774 | 200. | 4.7 | 3. | \%/s" hex | 0 |
| 2N1776 | 300. | 4.7 | 3. | \%o" hex | D |
| 2N1777 | 400. | 4.7 | 3. | \%/6" nex | D |
| 2N1595 | 50. | 0.6. | $10^{\circ}$ | T0.5 | E |
| 2N1596 | 100. | $0.6{ }^{\circ}$ | $10^{\circ}$ | T0.5 | E |
| 2N1597 | 200. | $0.6{ }^{\circ}$ | $1.0^{\circ}$ | 10.5 | E |
| 2N1598 | 300. | $0.6{ }^{\circ}$ | $1.0^{\circ}$ | T0.5 | E |
| 2N1599 | 400. | $0.6{ }^{\circ}$ | $1.0^{\circ}$ | T0.5 | $E$ |
| $\begin{aligned} & \text { 2N2011 } \\ & \text { (TCR1001) } \end{aligned}$ | 100. | $0.6{ }^{\circ}$ | $1.0^{\circ}$ | T0.5 | $E$ |
| 2N2012 <br> (TCR2001) | 200. | $0.6{ }^{\circ}$ | 1.0 * | T0.5 | E |
| 2N2013 (TCR3001) | 300. | $0.6{ }^{\circ}$ | $1.0^{\circ}$ | T0.5 | E |
| 2N2014 (TCR4001) | 400. | 0.6.0 | $1.0^{*}$ | 10.5 | E |
| SILICON CONTROLLED SWITCHES |  |  |  |  |  |
| 2N948 (TSW31S) | 30. | $0.2^{\bullet \bullet}$ | $0.2 \dagger$ | T0.18 | F |
| $\begin{aligned} & \text { 2N949 } \\ & \text { (TSW61S) } \end{aligned}$ | 60. | $0.2^{\circ}$ | $0.2 \dagger$ | T0-18 | $F$ |
| $\begin{aligned} & \text { 2N950 } \\ & \text { (TSW101S) } \\ & \hline \end{aligned}$ | 100. | 0.2** | $0.2 \dagger$ | T0-18 | $F$ |
| 2N951 (TSW201S) | 200. | $0.2^{\circ}$ | $0.2 \dagger$ | r0-18 | F |
| - At $80^{\circ} \mathrm{C}$ case |  | $25^{\circ} \mathrm{C}$ ambient $\quad \dagger$ At $75^{\circ}$ amblent |  |  |  |

## 

## SILICON DIODES - advanced techniques insure long-ferm mechanical and electrical stability

| COMPUTER TYPES |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Type |  | Maximum Average Current @ $25^{\circ} \mathrm{C}$ (mA) | $\begin{gathered} \text { Maximum } \\ \text { Recovery } \\ \text { TIme } \\ \text { (musec) } \end{gathered}$ | Maximum Capacitance at 0 Volts ( $\mu \mathrm{\mu}$ ) | Pactage |
| 10914* | 75. | 75. | 4. | 4. | $A$ |
| 1N916* | 75. | 75. | 4. | 2. | A |

"Alse avaMatie In miere pactage

| MICRO ZENER DIODES (SPECIFICATIONS AT 25 C ) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Iype | Mominal ${ }^{\circ}$ Voltage (volts) | $\begin{gathered} \text { Test } \\ \text { Current } \\ \text { (mA) } \end{gathered}$ | Maximum Resistance (0hmsi) | $\begin{gathered} \begin{array}{c} \text { Maximum } \\ \text { Inverse Current } \\ @ \\ =-1 \text { Volt } \\ (\mu A) \end{array} \\ E_{5} \end{gathered}$ | Typical Forward Voltage $@ 5.0 \mathrm{~mA}$ (volts) | $\begin{aligned} & \text { Pack- } \\ & \text { age } \end{aligned}$ |
| TMD. 01 | 5.1 | 5 | 15 | 1.0 | 0.75 | - |
| TMD. 02 | 5.6 | 5 | 15 | 1.0 | 0.75 | B |
| TMD. 03 | 6.2 | 5 | 15 | 1.0 | 0.75 | 8 |
| TMD. 04 | 6.8 | 5 | 15 | 1.0 | 0.75 | B |
| TMD-05 | 7.5 | 5 | 15 | 0.1 | 0.75 | - |
| TMO. 06 | 8.2 | 5 | 15 | 0.1 | 0.75 | - |
| TMD-07 | 9.1 | 5 | 15 | 0.1 | 0.75 | 8 |
| TMD-08 | 10.0 | 5 | 15 | 0.1 | 0.75 | B |
| TMD 09 | 11.0 | 5 | 20 | 0.1 | 0.75 | B |
| TMD 10 | 12.0 | 5 | 20 | 0.1 | 0.75 | B |
| - Voltage Tolerance $\pm 10 \%$. For $\pm 5 \%$ Voltage Tolerance use " $A$ " sulfix (i.e. TMMD-01A). |  |  |  |  |  |  |

FAST SWITCHING

|  | Maximum <br> Inverse <br> Operating <br> Voltage <br> (volts) | Maximum <br> Average <br> Forward <br> Current <br> @ $25^{\circ} \mathrm{C}$ <br> $(\mathrm{mA})$ | Maximum <br> Recovery <br> Time <br> $(\mu \mathrm{sec})$ | Pack- <br> age |
| :---: | :---: | :---: | :---: | :---: |
| TMD24 | 50. | 50. | 0.3 | - |
| TMD25 | 100. | 50. | 0.3 | $B$ |
| TMD27 | 200. | 50. | 0.3 | $B$ |

VERY FAST SWITCHING

| TMDSO | 60. | 20. | .004 | B |
| :--- | :---: | :---: | :---: | :---: |
| MEWI COMPUTER TVPE DIODES AVAILABLE IN MICRO PACKAGE |  |  |  |  |
| TMDS4 (1NO14) | 75. | 75. | .004 | B |
| TMO56 (1N916) | 75. | 75. | .004 | B |

HIGH CONDUCTANCE TYPES

| Type |  | Maximum average Forward Current $@ 25^{\circ} \mathrm{C}$ (mA) | Maximum Inverse Current <br> ( $\mu \mathrm{A}$ @ volts) | $\begin{aligned} & \text { Pact- } \\ & \text { age } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
| TMD-41 | 50. | 75. | 0.25 @ 50 | 8 |
| TMDD-42 | 100. | 75. | 0.25 @ 100 | - |
| TMD-45 | 200. | 75. | 0.25 @ 200 | 8 |

MICRO-STABISTORS

| Type | Forward Voltage <br> @ 1 mA DC (volts) | Maximum formard Voltage <br> © 20 mA DC (volts) | Maximum Dynamic Resistance <br> @ 1 mA <br> @ 1 KC (ohms) | Maximum Inverse Current <br> @ -2 volts DC <br> ( $\mu \mathrm{A}$ ) | Package |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TM020 | 0.64 $\pm 10 \%$ | 0.85 | 60 | 0.5 | - |
| TMD40 | $0.55 \pm 10 \%$ | 0.85 | 60 | 0.5 | B |

IN914 AND IN916 COMPUTER TYPE SILICON DIODES
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2N699
2N1252
2N1253
2N706
2N1420

| Tyoe |  |
| :---: | :---: |
| 2 21131 | 40 |
| 2N1132 | 40 |
| 2N696 | 60 |
| 2 N 697 | 60 |
| 2 N 698 | 100 |
| 2N699 | 100 |
| 2 L 1252 | 30. |
| 2 L 1253 | 30 |
| 2N706 | 25 |
| 2 N 1420 | 60 |

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Transitron now has available additional literature covering circuit design, operation, and application of various semiconductor types: -

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- THE SILICON CONTROLLED RECTIFIER Theory of Operation - Application Notes - Circuits (AN-1356A)
- THE BINISTOR - Circuir Design Informafion and Application Notes (AN-1360A)
- THE TRANSWITCH - Circuit Design Information and Application Notes (AN-1357A)


## PLUS <br> "25 Tips on How to Buy Semiconductors" FREE!

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## TEAR OUT AND SAVE

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Updated Transistor List
Contains Many Improved Types

Over 600 new types are included in this year's Transistor Data Chart. A high percentage of last year's types are upgraded in electrical characteristics such as power dissipation and cut-off frequency. Improvements in transistor fabrication techniques have resulted in the availability of high-power, highfrequency devices plus fastswitching epitaxial transistors.

The increasing quantity of types, of course, presents a growing problem to the design engineer in search of a particular one. Less than two dozen former types were abandoned. The addition of types bearing new JEDEC numbers, with marginal improvements (if any) over existing types, adds to the selection problem.

Electronic Design's organization of its Transistor Data Chart into basic types and its listing of types by the increasing value of a key characteristic make selection as straight-forward as possible.
If you would like a free reprint of this section, turn to the Reader-Service Card and circle 251.

## July 19-Case for Switching Speed

Due to space limitations, we were forced to postpone publication of a provocative argument posed by Charles Askanas, Engineering Project Manager al Luma. Iron Electronics. Titled "Optimum Test Limit for Transistor SwitchingCircuit Measurements," the article offers a iustification for the use of 20 and 80 per cent test points rather than 10 and 90 per cent points, presently used to characlerize switching devices. Be sure to read the analysis in the July 19 is. sue; your comments on the validity of the argument are invited.

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## Latest Listings of <br> Military Approved Transistors

To encourage the use of improved transistor types in the design of new military equipment, MIL-STD-701A has been updated, with Department of Defense approval, by MIL-STD-701B. New types have been added, some older types have been dropped and several "guidance" types have been upped to the "preferred" category. MIL-STD-701B types are grouped in a convenient application chart shown in Table 1. A list of the DOD, as well as single-service types with specification numbers and issue dates is in Table 2.

Table 1

|  |  |  | Germanium |  | Silicon |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | PNP | NPN | PNP | NPN |
| power | Audio ( $<300 \mathrm{mw}$ ) | Prelerred <br> Guidance | 2N526 2N652A 2N467 2N220 | [..... | 2N1026A | 2N335 |
|  | Medium frequency ( 3 to 30 mc ) | Preferred Guidance Preferred | 2N1309 | 2N1308 | 2N1118 | 2N338 |
|  | High írequency ( $>30 \mathrm{mc}$ ) | Guidance | $\begin{array}{\|l} \text { 2N384 } \\ \text { 2N700A } \\ \text { 2N1142 } \end{array}$ |  |  | $\begin{aligned} & 3 N 35 \\ & 2 N 1613 \end{aligned}$ |
| Switching | $\begin{array}{\|l\|} \hline \text { Low speed ( }>5 \\ \mu \mathrm{sec} \text { total time }) \end{array}$ | Preferred Guidance | 2N398 | $\cdots$ | 2N329A | (t) |
|  |  | Preferred | $\begin{array}{\|l\|} \hline \text { 2N404 } \\ \text { 2N428 } \end{array}$ | 2N358A |  |  |
|  | Medium speed ( 1 to $5 \mu \mathrm{sec}$ ) |  | $\begin{aligned} & \text { 2N428 } \\ & \text { 2N396A } \end{aligned}$ | 2N388 |  |  |
|  |  | Guidance | 2N599 |  | 2N491 | 2N337 |
|  |  |  | 2N705 | 2N1310 | 2N1119 |  |
|  |  | Preferred |  |  |  | 2N706 |
|  | Fast speed ( $<1 \mu \mathrm{sec}$ ) | Guidance | $\begin{aligned} & \text { 2N559 } \\ & \text { 2N1500 } \\ & \text { 2N695 } \\ & \text { 2N1195 } \end{aligned}$ |  | 2N1132 | 2N560 2N1893 |
|  | Bilateral switch (medium speed) | Preferred Guidance | …… | $\ldots$ | -787 | . ..... |
| Power |  | Preferred |  |  |  |  |
|  | 300 mw to 3 w | Guidance | 2N1039 2N1041 | , | 2N1234 | 2N341 |
|  | 31030 w | Prelerred | 2N539 | \% |  | 2N498 |
|  |  | Guidance | 2N1184B | 2N326 |  | 2N1485 |
|  |  | Preferred | $\begin{aligned} & \text { 2N297A } \\ & \text { 2N1358 } \end{aligned}$ |  |  | ...... |
|  | $>30 \mathrm{w}$ | Guidance | $\begin{aligned} & 2 \mathrm{~N} 1120 \\ & 2 \mathrm{~N} 1165 \\ & \text { 2N1046 } \end{aligned}$ | +..... |  | $\begin{aligned} & \text { 2N389 } \\ & 2 \mathrm{~N} 424 \\ & \text { 2N1050 } \\ & \text { 2N1016B } \\ & \hline \end{aligned}$ |


| Type | Specification | Date |
| :---: | :---: | :---: |
| 2N43A | MIL-T-19500/18(USAF) | Amend 2. 10 November 1958 |
| 2N44A | MIL-T-19500/6(USAF) | Amend 1.10 April 1958 |
| 2N78A | MIL S-19500/90(USAF) | 23 May 1960 |
| 2N117 | MIL-T-19500/35(NAWY) | 15 March 1958 |
| 2N118 | MIL T $19500 / 35$ (NAVY) | 15 March 1958 |
| 2N119 | MIL.T 19500/35(NAWY) | 15 March 1958 |
| 2N118 | MIL T 19500/2(JAN) | 12 December 1957 |
| 2N123 | MIL-T-19500/30(USAF) | 4 February 1959 |
| 2N128 | MIL T 19500/9A(JAN) | 12 June 1959 |
| 2N129 | MIL-T 19500/8(SigC) | 21 July 1958 |
| 2N144 | MIL-T-19500/29(USAF) | Dropped |
| 2N158 | MIL-S 19500/24A(JAN) | 27 November 1959 |
| 2N167A | MIL S. 19500/11A(USAF) | 23 May 1960 |
| 2N173 | MIL-T-19500/12(NAW) | Dropped |
| 2N174 | MIL-T-19500/13A(JAN) | 8 January 1953 |
| 2N200 | MIL T-19500/5 | Dropped |
| 2N220 | MIL- T 19500/1 | 14 June 1957 |
| 2N240 | MIL S. 19500/25A(JAN) | 5 November :959 |
| 2N243 | MIL T 19500/34(USAF) | Dropped |
| 2N244 | MIL T 19500/34(USAF) | Dropped |
| 2N245 | MIL T 19500/14(USAF) | Dropped |
| 2N246 | MIL T 19500/15(USAF) | Dropped |
| 2N274 | MIL-T 19500/26(SigC) | 3 October 1957 |
| 2N297A | MIL T 19500/36A(SigC) | 17 November 1953 |
| 2N299 | MIL T $19500 / 39(\mathrm{SigC})$ | Dropped |
| 2N300 | MIL- T. 19500/55(SigC) | 21 July 1958 |
| 2N325 | MIL S. 19500/40(JAN) | 29 February 1960 |
| 2N326 | MIL S 19500/40(JAN) | 29 Februan 1960 |
| 2N328A | MIL S $19500 / 110$ (SigC) | Amend 1 13 May 1960 |
| 2N329A | MIL-S 19500/111(SigC) | Amend 113 bilay 1960 |
| 2N331 | MIL T 19500/4A | 16 January 1958 |
| 2N332 | MIL.T 19500/37A(NAVY) | 18 June 1959 |
| 2N333 | MIL T 19500/37A(NAVY) | 18 June 1959 |
| 2N334 | MIL-T 19500/37A(NAVY) | 18 June 1959 |
| 2N335 | MIL T 19500/37A(NAVY) | 18 June 1959 |
| 2 N 337 | MIL S 19500/69C(NAVY) | 14 October 1950 |
| 2N338 | MIL S $19500 / 69$ (NAVV) | 14 October 1950 |
| 2N342 | MIL-S 19500/16B(JAN) | 24 February 1950 |
| 2N343 | MIL S 19500/16B(JAN) | 24 February 1950 |
| 2N358A | MIL S 19500/63B(JAN) | 23 May 1960 |
| 2N384 | MIL S-19500/27A(JAN) | 20 January 1960 |
| 2N388 | MIL T 19500/65(NAVY) | 20 March 1959 |
| 2 N 393 | MIL S 19500/77A(SigC) | 30 October 1957 |
| 2N396A | MIL S 19500/64A(NAVY) | 27 October 1959 |
| 2N404 | MIL T 19500/20(USAF) | Amend 23 March 1959 |
| 2N416 | MIL T 19500/56A(SIgC) | 3 February 1959 |
| 2N417 | MIL T- 19500/57A(SIgC) | 3 February 1959 |
| 2N422 | MIL T 19500/66A(NAVY) | 26 June 1959 |
| 2N425 | MIL T 19500/41A(SigC) | 26 January 1959 |
| 2N426 | MILT 19500/42A(SigC) | 26 January 1959 |
| 2 N 427 | MIL T $19500 / 43 \mathrm{~A}(\mathrm{SIgC})$ | 26 January 195\% |
| 2N428 | MIL S $19500 / 448($ SigC) |  |
| 2N431 | MIL T 19500/21(USAF) | Amend 110 sper 1958 |
| 2N432 | MIL. T 19500/22(USAF) | Amend 110 toril 1958 |
| 2N433 | MIL T 19500/23(USAF) | Amend 110 spril 1958 |
| 2N461 | MIL T 19500/45(USAF) | 7 July 1958 |
| 2N463 | MIL T 19500/70(NAVY) | 14 May 1959 |
| 2N464 | MIL T $19500 / 49 \mathrm{~B}(\mathrm{~S}, \mathrm{gC})$ | 3 February 1959 |
| 2N465 | MIL- $19500 / 50 \mathrm{~A}(\mathrm{SigC})$ | 3 February 1957 |
| 2N466 | MIL S 19500/51B(SigC) | 17 August 1950 |
| 2N467 | MIL T 19500/52B(SigC) | 3 February 1957 |
| 2N489 | MIL- T-19500/75(USAF) | 1 July 1959 |
| 2N490 | MIL. T-19500/75(USAF) | 1 July 1959 |
| 2N491 | MIL T 19500/75(USAF) | 1 July 1959 |
| 2N492 | MIL. 19500/75(USAF) | 1 July 1959 |
| 2N493 | MIL T 19500/75(USAF) | 1 July 1959 |
| 2N494 | MIL T 19500/75(USAF) | 1 July 1959 |
| 2N495 | MIL T 19500/54A(SigC) | 13 August 1959 |
| 2N496 | MIL S 19500/85(SigC) | Amend 122 March 1960 |
| 2N497 | MIL. T-19500/74(NAVY) | 30 June 1959 |
| 2N498 |  |  |
| 2N499 | MIL T-19500/72A(SigC) | 4 January 1960 |
| 2N501A | MILT. $19500 / 62(\mathrm{SigC})$ | 5 December 1953 |
| 2N502A | MIL S 19500/112(SigC) | 4 April 1960 |
| 2N526 | MIL-S-19500/60C(JAN) | 29 July 1960 |
| 2N537 | MIL S 19500/100(SigC) | 30 November 1959 |
| 2N539 | MIL. $19500 / 38$ (NAWY) | 28 May 1958 |
| 2N545 | MIL-S.19500/84(NAVY) | 24 February 1960 |
| 2N559 | MIL-S 19500/152(SIgC) | 7 December 1960 |
| 2N560 | MIL-S 19500/73A(JAN) | 29 July 1960 |
| 2N574 | MIL-T-19500/46(SigC) | 22 May 1960 |


| Type | Specitication | Date |
| :---: | :---: | :---: |
| 2N575 | MIL T. 19500/47(SigC) | 22 May 1960 |
| 2N599 | MIL-S.19500/66(NAWY) | 25 January 1961 |
| 2N624 | MIL.T 19500/82(SigC) | 10 August 1959 |
| 2N656 | MIL-T-19500/74(NAW) | 30 June 1959 |
| 2N657 | MIL- 19500/74(NAW) | 30 June 1959 |
| 2N665 | MIL-S-19500/588(JAN) | 12 July 1960 |
| 2N681 | MIL-S.19500/108(NAWY) Controlled Rectifiers | 22 March 1960 |
| 2N682 | MIL-S-19500/108(NAVY) | 22 March 1960 |
| 2N683 | Controlled Rectifiers MIL S 19500/108(NAVY) Controlled Rectıfiers | 22 March 1960 |
| 2N684 | MIL-S.19500/108(NAVY) Controlled Rectifiers | 22 March 1960 |
| 2N685 | MIL S 19500/108(NAVY) Controlled Rectifiers | 22 March 1960 |
| 2N686 | MIL S 19500/108(NAW) Controlled Rectifiers | 22 March 1960 |
| 2N687 | MIL S 19500/108(NAVY) | 22 March 1960 |
| 2N688 | Controlled Rectifiers MIL S. 19500/108(NAWY) Controlled Rectifiers | 22 March 1960 |
| 2N694 | MIL S 19500/160(SigC) | 9 December 1960 |
| 2N695 | MIL S 19500/135(NAWY) | 17 October 1960 |
| 2N696 | MIL S 19500/99A(SigC) | 1 April 1960 |
| 2N697 | MIL-S 19500/99A(SIgC) | 1 April 1960 |
| 2N700A | MIL S 19500/123(SigC) | 1 July 1960 |
| 2N702 | MIL S 19500/153(SIGC) | 7 December 1960 |
| 2N703 | MIL S 19500/153(SIgC) | 7 December 1960 |
| 2N705 | MIL S 19500/86(NAVY) | 6 June 1960 |
| 2N706 | MIL S 19500/120(SigC) | 2 June 1960 |
| 2N716 | MIL S 19500/154(SIEC) | 7 December 1960 |
| 2N1000 | MIL T-19500/79(SigC) | 22 June 1959 |
| 2N1001 | MIL S $19500 / 81(\mathrm{SigC})$ | 17 June 1959 |
| 2N1002 | MIL S 19500/83(SigC) | 10 August 1959 |
| 2N1011 | MIL T 19500/67(SigC) | 22 January 1959 |
| 2N1025 | MIL S 19500/78A(S,gC) | 7 December 1959 |
| 2N1026 | MIL S 19500/78A(S'gC) | 7 Decermber 1959 |
| 2N1026A | MIL S 19500/78AISIBC) | 7 December 1959 |
| 2N1039 | PAIL S 19500/89(NAVY) | 21 July 1960 |
| 2N1041 | MIL S 19500, '89(NAVY) | 21 July 1960 |
| 2 N 1042 | MIL S 19500/137(SigC) | 8 September 1960 |
| 2N1043 | MIL S $19500 / 137(S 18 C)$ | 8 Seplember 1960 |
| 2N1044 | MIL S 19500/137(SigC) | 8 September 1960 |
| 2N1045 | MIL S 19500/137(SigC) | 8 September 1960 |
| 2N1046 | MIL S 19500/88(NAVY) | 21 July 1960 |
| 2N1072 | MIL S $19500 / 1631$ SIGC) | 5 January 1961 |
| 2N1082 | MIL S $19500 / 103$ (SigC) | 18 December 1959 |
| 2N1094 | MIL S 19500/161(SigC) | 9 December 1960 |
| 2N1118 | MIL S 19500/138(SigC) | 9 September 1960 |
| 2N1119 | MIL S 19500/139(SigC) | 9 September 1960 |
| 2 N 1120 | MIL T 19500/68(SigC) | 10 February 1960 |
| 2 N 1142 | MIL S 19500/87(NAVY) | 15 August 1960 |
| 2N1158A | MIL S 19500/113(SigC) | 4 April 1960 |
| 2N1183 | MIL S 19500/143(SigC) | 10 October 1950 |
| 2N1183A | MIL S 19500/143(SigC) | 10 October 1950 |
| 2N11838 | MIL S 19500/143(SigC) | 10 October 1950 |
| 2N1184 | MIL S 19500/143(SIGC) | 10 October 1950 |
| 2N1184A | MIL S $19500 / 143(\mathrm{SigC})$ | 10 October 1950 |
| 2N1184B | MIL S $19500 / 143$ (SIGC) | 10 Oclober 1950 |
| 2N1195 | MIL S $19500 / 71$ B(JAN) | 29 July 1960 |
| 2N1196 | MIL S 19500/164(SigC) | 6 January 1961 |
| 2N1197 | MIL S 19500/165(SıgC) | 6 January 1961 |
| 2N1199A | MIL S 19500/131(SIgC) | 25 July 1960 |
| 2N1200 | MIL S $19500 / 105(\mathrm{SigC)}$ | 28 December 1959 |
| 2 N 1201 | MIL S $19500 / 101\left(S_{\text {S C }}\right.$ C) | 30 November 1960 |
| 2N1302 | MIL S 19500/126(NAVY) | 14 October 1960 |
| 2N1303 | MIL S 19500/126(NAVY) | 14 October 1960 |
| 2N1304 | MIL S 19500/126(NAVY) | 14 October 1960 |
| 2N1305 | MIL S 19500/126(NAVY) | 14 October 1960 |
| 2N1306 | MIL S 19500/126(NAW) | 14 October 1960 |
| 2N1307 | MIL S 19500/126(NAVY) | 14 October 1960 |
| 2N1308 | MIL S 19500/126(NAWY) | 14 Oclober 1960 |
| 2N1309 | MIL S 19500/126(NAVY) | 14 October 1960 |
| 2N1310 | MIL S 19500/136(NAVY) | 6 December 1960 |
| 2N1358 | MIL S 19500/122(SigC) | 20 June 1960 |
| 2N1411 | MIL S 19500/133(SigC) | 3 August 1960 |
| 2N1412 | MIL S 19500/76(NAVY) | 4 February 1960 |
| 2N1500 | MIL S 19500/125(SigC) | 11 July 1960 |
| 3N35 | MIL S $19500 / 80 \mathrm{~A}(\mathrm{SIGC})$ | 30 October 1959 |

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strength and dimensional accuracy. - For more information on Arnold iron powder cores, write for a copy of our new 36-page Bulletin PC-109A. The Arnold Engineering Company, Main Office and Plant, Marengo, Illinois. adoress otert. eo.


CIRCLE 71 ON READER-SERVICE CARD

## A BASIC GUIDE TO

## PRECISION POTENTIOMETERS



The Raytron Catalog of Precision Potentiometers describes, illustrates and provides electricai, mechanical and general specifications on most of our standard units. Drawings, temperature rating curves and general engineering data are also included to enable rapid, accurate selection of potentiometers which will meet all requirements, normal or special.

Whatever your specifications in single-turn, linear and non-linear units, the name Raytron guarantees high-precision, exact performance and environmental compliance...at minimum cost.

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INSTRUMENTS FOR INDUSTRY, INC.
101 NEW SOUTH ROAD, HICKSVILLE, L. J., N. Y. CIRCLE 72 ON READER-SERVICE CARD

## Transient Control Device

## Protects Rectifiers



## From Surge Overloads

HIGH-VOLTAGE transients, appearing across power supplies when an inductive load is suddenly turned off, can be effectively reduced by a newly developed gas-tube device. Conventional means to avoid rectifier burnout include the use of relatively expensive, high piv diodes or Zener devices.

## Low Cost Diodes Can Be Used

 With Transient ProtectorLow cost, 200-v piv rectifiers can be used with transient control, de-
veloped by Ledex, Inc., Dayton, Ohio. Transient peaks as high as $1,400 \mathrm{v}$ have been applied to rectifier and bridge arrangements using the transient control with no rectifier failures resulting. See Fig. 1. The heart of the device consists of a gas tube which ionizes at a critical voltage ( 200 v in present units) thus creating a low-impedance shunt for excessively large pulses. For most power-supply applications, the 200 -v ionization potential is adequate; higher voltage ratings and low-


Fig. 1. Oscilloscope trace across inductive load at output of a bridge rectifier. In (a) is shown a 1,400-v pulse (200-v/division) appearing across the de output while (b) shows the clipping action achieved by addition of the transient control.


Fig. 2. Basic rectifier bridge circuit showing current flow resulting from suddenly opening the inductive load circuit.
er voltage ratings can be supplied on a custom basis if required.

## Device Protects Against Line

## As Well As Load Surges

In the full-wave bridge circuit shown in Fig. :2, current $I$ would flow as indicated from an inductive load when the switch is opened. Without the transient control, a highvoltage pulse would appear across the four diodes and breakdown is possible: should one diode become shorted, the diode on the adjacent leg of the bridge would be destroved in at short time.

Should a transient occur at the ac input, the transient control permits current flow through the low impedance or conducting diodes rather thatl through the high-imperdance bridge arms. Thus, positive or negative spikes are clipped at the $200-v$ level.

In addition to the tramsient control. Ledex is packaging a protected bridge rectifier, incorporating four rectifiers plus a built-in control rated as follows: 115 v ace input, 100 v de output, maximum surge $\overline{\text { on }}$ amp for 8 msec.

Transient controls, part A-16800001 are packed 10 to a carton; prices per carton are $\$ 0(0)$ ) for one carton, $\$ 18.50$ ea for $2-9$ cartons and $\$ 16.00$ ea for 10-49 cartons. The protected bridge rectifier, part A-46501-()01, is $\$ x .1 \overline{5}$ ea in $1-9$ quantities, $\$ 7.40$ ea in $10-24$ lots and $\$ 6.80$ ea in $2 \overline{2}-99$ quantities. A value analysis kit RTC, containing one protected bridge rectifier and one transient control, is available at $\$ 11.00$ ea.

For further information on these devices, turn to the Reader-Service Card and circle 252.


Write for technical date on the complete line of "KEMET" Solid Tantalum CapacitorsI

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has the widest choice of High-Voltage

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.0047 to 330 MICROFARADS

## 111

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-55 to $+125^{\circ} \mathrm{C}$

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Temperature Range:
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J-Serles meets or exceeds MIL-C-26655A
KEMET offers you the only full line of high-voltage solid tantalum capacitors for a multitude of military/industrial applications. J-Series and N-Series are available in working voltages of 75 , $60,50,35,20,15,10$, and 6 -in standard E.I.A. values with $\pm 5 \%, \pm 10 \%$, and $\pm 20 \%$ tolerances. Low leakage characteristics are excellent. Four J.Series case sizes conform to MIL.C.26655A with or without insulating sleeve. Leads are solderable and weldable. All KEMET types have passed approved environmental tests. Whatever your solid tantalum capacitor needs, meet them with KEMET's complete line! Kemet Company. Division of Union Carbide Corporation, 12901 Madison Avenue, Cleveland 1, Ohio.

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More reliable electrical contact

- More secure mechanical grip
- Minimum electrical resistance

Each lead has individual strain relief because wire is doubled back through contact tab. Punch press contact design permits rapid heat transfer - eliminates unreliable cold solder joints as in screw machine contacts. Danger of insulation pull back is eliminated by bringing wire insulation right into molded clip pocket.

These unique Alden molding techniques in connector design drastically reduce the number of parts required and make possible multi-contact connectors of amazing basic simplicity and reliability.

Resilient Alden contacts can be included in any type of molded insulation for any combination of contacts. Hundreds of standard off-the-shelf designs are quickly available - with of without leads - of as part of unit-molded cables.

Our Customer Department will work closely with you on any connecting or cabling problems. A letter with description or sketch will enable us to provide recommendations or samples at once.


New, flamepraef. HIgh veltage First majer advance in connector standard assemblat connactors cennetars now available in high- roliatility since patting offers fool. in non-interchangeable layouts with from density flame-retardant polyethylone. proof tamper-proof connections for 2 to 11 contacts, miniature connectors. Light. compact connectors lor applica. trouble-free operation. Alden "IMI" plain or shielded, for carrying Dower or tions up to 30 KVDC and UD to $250^{\circ} \mathrm{F}$ connactors and cables (wies, contacts. signal, miniature plugs and sockefs;
without distertion.
or other inserts) are integraily molded signal connectors: and CRT connoctors in a single hot shot of insulation so that
material forming the connectors and maverias the wires forms a single con-
covering tinu ous, bonded insulation.

7139 North Main St., Brockion, Mass.
CIRCLE 74 ON READER-SERVICE CARD


## Coaxial Cavity Increases Magnetron Frequency Stability

THE USE of the coaxial cavity principle in magnetron design results in 5 to 10 times better frequency stability. Model SFD-303 magnetron, designed for X -band use, operates at 50 per cent efficiency, delivers minimum peak power of 1 megawatt and an average power of 1 kw . Its light weight of 45 lb makes it ideal for long-range airborne radar systems. Greater frequency stabilization makes steady state operation possible at the optimum impedance point.

The SFD-303 coaxial magnetron, manufactured by SFD Laboratories, 800 Rahway Ave., Union, N. J., employs a new concept in anode design which results in the significant improvements in frequency stability. Typically, side-lobe ratios are greater than 10 db , missing pulses less than 0.2 per cent and pulling factor is less than 6 mc at the megawatt level. At $2-\mu$ sec pulse lengths, the rf band-width is less than 0.7 mc.

The principle on which the model

303 is based allows for high-frequency magnetrons to be built with large interaction areas so that the power dissipated per unit area of the anode and cathode is very low. Normally, when such large interaction areas are used, serious problems of mode control exist. Control of the mode in which oscillations begin is lost as the voltage pulse rises on the magnetron.
The approach which has here-tofore been taken to the problem of mode control consists in designing the multi-cavity anode circuit to produce a relatively large frequency separation between the desired, or pi-mode, and its adjacent neighbors. Both strapped and rising-sun structures are based upon this philosophy. These techniques insure mode stability once the proper mode has been established, but do not insure its build-up in the presence of competing modes whose starting voltages fall in the same general range. To overcome the ease of starting such an unloaded mode the practice has
been to introduce some asymmetry into the anode block to orient both components of the doublet equally to the output slot.

In the coaxial structure, the design insures correctly phased rf currents at the normally short-circuited ends of the resonators.
The figure shown illustrates the main features of the anode. Alternate resonators are cut througi to the coaxial cavity which is dimensioned to resonate in the circular electric ( $T E_{011}$ ) mode. The circumferential currents associated with this mode have the same phase at all points around the periphery of the cylinders. Since the resonators present a low impedance at their back ends, they are well matched to the impedance of the coaxial cavity as seen from the inner cylinder wall cut through positions.

Operation of the large cavity in the $T E_{\text {w, }}$ mode insures currents and voltages of the same phase in alternate resonators. Mutual flux linkage between adjacent resonators is relied upon to excite the other half of the resonators with equal, but oppositely phased, currents giving rise to a pure pi-mode.

The higher $Q_{0}$ achieved by removing the straps in the resonator assembly yields higher efficiency in addition to greater frequency stability. It also raises the impedance of the anode so that less stored energy , accompanied by reduced power loss, is required to produce the same electric field in the interaction space.

In a conventional magnetron the anode surface can be increased only by increasing the anode height. This results in a long magnet with large magnet weight. With the new design the anode surface can be increased by increasing the number of resonators rather than increasing their height. This allows an extra degree of design freedom which results in weight reduction.

Model SFD-303 is available 120 days after receipt of order, with price dependent on quantity and delivery date.

For further information on this magnetron turn to the Reader-Service Card and Circle 253.
JUT ARRIVED! moos soce ramiy

ACompact-Versatile POWER SUPPLY
Constant Voltage / Constant Current Operation

- Auto-Series \& Auto-Parallel Operation
SPECIFICATIONS
Output: $0-40$ Volts, 0-0.5 Amps D.C. Load Regulation:
Constant Voltage: $0.01 \%$ or 4 mv . Constant Current: $0.05 \%$ or $250 \mu \mathrm{a}$ Line Regulation:
Constant Voltage: $0.01 \%$ or 4 mv .
Constant Current: $0.05 \%$ or $250 \mu$ a
Ripple and Noise:
Constant Voltage: $200 \mu \mathrm{~V}$.
Constant Current:
$200 \mu \mathrm{a}$ Transient Recovery Time: $50 \mu \mathrm{sec}$. Size: $51 / w^{\prime \prime} \mathrm{H} \times 712 / w^{\prime \prime}$ W X $81 / 2^{\prime \prime} \mathrm{D}$
Price: \$169.00
OThER PRECISE, VERSATILE AND COMPACT POWER SUPPLIES IMCLUDE:

| mesol | E Out | 1 Out | $\begin{aligned} & \text { Bench } \\ & \text { Model } \end{aligned}$ | Rack Moce | Continuously Varibula | Spectal Comments | Prics |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 52004 | 0.36 | 0.25 |  | $\times$ | Yes | Misht Efliciency | \$575.00 |
| $5 \mathrm{cos}-2$ | 0.36 | $0-1.5$ | x | X | Yes | Dual Outpul | 580.00 |
| 2000-2 | 0.36 | 0.2 .5 | $\times$ | $\times$ | Yes | Low Cost Madium | 339.00 |
| 2028 | 0.36 | 0.1 .5 |  | x | Yes | Dual Output Remote Sanzing | 380.00 |
| cesam | 0.20 | 0.2 .0 |  | x | Yes | Remote Sensing Remote Programmine | 350.00 |
| desa | 0.36 | 0.5 |  | $x$ | Yes | Constant Voltage/ Constant Current | 475.00 |
| 8108 | 0.60 | 0.7 .5 |  | $\times$ | Yes |  | 795.00 |
| 112 | 0.32 | 0.10 |  | X | No | Romote Sonsing | 550.00 |
| 814 | 0.36 | 0.25 |  | $x$ | Yes | Constant Voltage / Constant Curment | 775.00 |
| 1558 | 0.18 | 0.1 .5 | $x$ | $\times$ | Yes | Constant Voltage / Constant Current | 169.00 |
| 030 | 0.100 | 0.1 .0 | X | $x$ | Yes | wioe Voltage Span | 375.00 |
| 1814 | 0.100 | 0.1 .0 |  | $\times$ | Yes | Constant Voltage / Constant Current | 475.00 |
| B500 | 0.320 | 0.0 .6 |  | X | Yes | Remote Programming | 485.00 |

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## NEW PRODUCTS

Covering all new products generally specified by engineers designing electronic original equipment. Use the Reader-Service Card for more information on any product. Merely circle number corresponding to that appearing at the top of each description.


## System Records <br> 1,200 Bits Per In.

High-density recording system PHD-1200 can reliably read and write digital tapes at 1,200 bits per in., 100 ips . Transient error rates are fewer than one bit in $10^{5}$ and permanent error rates are less than one bit in $10^{10}$. More than 20,000 passes of the same tape can be made without losing information or increasing transient dropout rate. System includes a digital magnetic tape transport, a dual read/write head assembly, read/write amplifiers, de-skewing buffer, manual control unit, and power supplies, cabled and mounted in a rack cabinet.
Potter Instrument Co., Inc., Dept. ED, Sunnyside Blvd., Plainview, N. Y.
P\&A: 829,500 , evaluation sample; 4 months.


Line Voltage Regulator

## Provides $\mathbf{1 0 0 - D b}$ Isolation

Solid state ac line regulator series 700 provides $0.1 \%$ regulation and $100-\mathrm{db}$ line isolation. Harmonic attenuation and transient rejection are 40 db . Input harmonies of $10 \% \max$ are reduced to less than $0.25 \%$ in the output. Power rating is 1 kva . Response time is $100 \mu \mathrm{sec}$. Bench and rack models are made for use at 50,60 , and 400 cps . Both 115 and 230 v units are available.
Stevens-Evans, Inc., Dept. ED, 3801 Hicock St.. San Diego, Calif.
P\&A: 81,200 to 81,$500 ; 45$ to 60 days.


Silicon Controlled Rectifiers
Housed in a double-ended, studless package, silicon controlled rectifiers 2N1929 through 2N1935, handle up to 1.1 amp without heat sinks. Piv ratings range from 25 to 300 v : operating temperature range is -65 to +125 C . Maximum leakage current ranges from 4.0 to 0.9 ma .

General Electric Co., Rectifier Components Dept., Dept. ED, W. Genesee St., Auburn, N. Y.

P\&A: 2N1933, \$10 OEM; stock.


## PNPN Device

Has Alloyed Junction
The Dynaquad is a germanium, three-terminal, pmpn structure packaged in a standard TO-5 case. Alloyed juncrion design is used for economy and reliability. The device has a rise time of 10.1 usec, and provides an output voltage swing of 35 Applications include driver, flip-flop, counter shift register and other logic circuits. Type's 2N1966 through 2N1968 are in production.

Tung-Sol Electric Inc., Dept. EI). 1 Sumner Ave., Newark 4, N. J.
P\&A: From s.3.10: immediate


Voltage-Controlled

## Subcarrier Oscillator

Transistorized subcarrier oscillator type $516 / 2$. operating on IRIG channels 1 to 18 and A to E , measures $3 / 4 \times 3 / 4 \times 1-1 / 4 \mathrm{in}$. Input is 0 to 5 r or $=2.5 \mathrm{v}$. Input impedance is 30 ow K min, linearity $\pm 0.5 \%$ of bandwidth. Output is 1 v rms nominal. Unit requires 28 v unregulated de at 10 ma , and weighs 1.6 oz . Shock, acceleration and vibration tests are met.
Telemetering Corp. of America, Dept. ED. 8345 Hayvenhurst Ave.. Sepulveda, Calif. P\&A: On request.


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6. Silver plated copper leads.
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## NEW PRODUCTS

## Carbon Film Resistor

Designed for printed circuits, carbon film resistor EC 25 is $1 / 4 \mathrm{in}$. in diameter by $13 / 32$ in. long and mounts vertically. Rating is $1 / 4$ w at 70 C derated to 0 at 150 C . Resistances range from 5 ohms to 500 K with a tolerance of $1 \%$.

Mepco, Inc., Dept. ED, 37 Abbett Ave., Morristown, N. J.

## Electron Beam Systems



Guns, controls, and power supplies are available in ratings from 3 kw at 10 kv to 9 kw at 30 kv . Systems of the LB-100 series are complete, and provide magnetic deflection of beam over 3 in . square area, pulsing, regulation, and variable focus and focal length. Temperatures above 6,200 are readily attained.

GVC Electron Heating Corp., Dept. ED, 81 Hicks Ave., Medford 55, Mass.

Instrument Switch


With up to six banks. Instrument switch type PW is available in $1-, 2$-, 3 - and 4 -pole types and assemblies up to six banks. Maximum number of positions is 29 in one-pole versions, six in the four-pole version. Voltage rating is 250 v ac or dc, current rating 0.5 amp.

Interlab, Inc., Dept. ED, 116 Kraft Ave. Bronxville, N. Y.
Price: $\$ 6.96$ to $\$ 41.72$.

## Alternators



Semiconductor voltage regulation, holding the output to $\pm 2 \%$ from 1,000 to $12,000 \mathrm{rpm}$, is provided by these alternators. Two types are offered: 15 v dc, $1,000 \mathrm{w} ; 100 \mathrm{v}$ dc, $1,500 \mathrm{w}$. Construction features radially oriented ceramic magnets. in the rotor.

Syncro Corp., Dept. ED, Oxford, Mich.

## Transistor Testers

544
Automatic multi-parameter tester type 4 is one of a group of go no-go and absolute readout transistor testers. With automatic sorting and classification, it tests breakdown voltage, lower limiting voltage, dc pulse current gain, saturation voltage, and reverse current.
Fairchild Semiconductor Corp., Dept. ED, 545 Whisman Road, Mountain View, Calif.
P\&A: \$22,000; 90 to 120 days.

## Frequency Standard

551
Stable to 1 part in $10^{11}$ for one month, the Rubidium frequency standard is suitable for applications in the hf electromagnetic spectrum in communications, navigation and computational systems of aircraft and missiles. It weighs about 20 lb .
FMA, Inc.. Dept. ED, 142 Nevada St., El Segundo, Calif.

## Servo Motor

412


Designed for missile use, this 6 -pole, $400-\mathrm{cps}$, size 15 servo motor offers the following characteristics: theoretical acceleration at stall, 22,700 radians per $\sec ^{2}$; minimum power output, 1.151 w ; input power at stall, 6.1 w ; motor dampening, 130 dyne-cm per sec.

Wright Machinery Co., Div. of Sperry Rand Corp., Dept. ED, Durham, N. C.

Cuts balancing time 80\%. U'sed with a vibration analyzer, this computer determines location and amount of compensating weight to be added or removed. Used in single and twoplane balancing operations for both in-place or production balancing of rotating parts, the instrument saves up to $80 \%$ time.
International Research \& Development Corp., Dept. ED, Worthington, Ohio.

## Autotransformers

672


Handle 30 amp. Series W Variac autotransformers type W30, rated for 30 amp. provide continuous control of ac voltage from 0 v to $17 \%$ above line voltage. Available for $120-$ or $240-\mathrm{v}, 50$ - to $60-\mathrm{cps}$ operation, units withstand momentary overload of $1,000 \%$. Type W30M is fully enclosed.

General Radio Co., Dept. ED, West Concord, Mass.
Price: W:30, 875; W'30M, \$97.
Gear Heads


Precision gear heads and speed reducers are available in size 5 to 18 servo mounts. Units have Class 2 gearing, with ABEC Class 1.5 bearings. End play and radial play are low; backlash is 30 min maximum. Housing is anodized aluminum alloy.

EIm Instrument Corp., Dept. ED, 30 Chasner St., Hempstead, L. I., N. Y.

Volt-Ohm Meters


Accuracy is $0.01 \%$ for voltage and resistance measurements or $0.2 \%$ for ac measurements to 1.000 v and for 10 ohms to 10 meg . Model 600 voltohmmeters are five-digit precision differential instruments with in-line display readout. Reference voltage is provided by Zener diode supply stable to $0.001 \%$ for a $10 \%$ line change

Auto-Data. Dept. EII, 94:3 Turquoise, San Diego, Calif.
P\&A: $\$ 1,885$ to $\$ 3,450: 30$ t1) 45 dаук.

## Silicon Diodes

523
Diffused-junction silicon diodes in 53 types have high inverse voltages, high forward conductance, low leakage current. and high rectification efficiency. Operating from -65 to 175 C , the medium current rectifiers are welded and hermetically sealed in a glass and metal case.
Raytheon Co, Semiconductor Div., Dept. ED, 215 First Are., Needham, Mass.
P\&A: \$0.58 10 8.3 cn, 100 10 $999 ;$ immediate.

Glass Diodes


Mena diffused junction glass diodes 3G05 through 3G30 have rating ranging from 50 to 300 v . Forward conductance to 300 ma , voltage drop of 0.9 v at 25 C , and low leakage characteristics are other features. Temperature range is -55 to +150 C .

International Rectifier Corn., Dept. ED, 1521 E. Grand Ave., El Sexundo, Calif.
P\&A: $\$ 1.07$ to $\$ 2.80 \mathrm{ea}, 1$ to 99 ; stack.

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## $55 \times 10^{9}$ ANODE DISSIPATION FACTOR



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## Highest Registered Rating Now Available from G.E.

## In an Air-cooled Tube

The latest addition to General Electric's expanding line of hydrogen thyratrons is now available for pulse applications such as radar modulators and linear accelerators. Developed under U. S. Army Signal Corps contract, the GL-7890 achieves an anode dissipation factor of $55 \times 10^{9}$ and has a peak anode voltage rating of 40 kv . The tube can now be operated water-cooled or air-cooled at full ratings. COMING: increased current and voltage capactir
Now in the late stages of development, the Z-5212 will further increase voltage and current-carrying capacity in hydrogen thyratrons. Peak anode voltage rating for this tube will be 50 kv with an average current rating of 8 amp . General Electric's Power Tube Department will welcome your requests for technical data on the Z-5212.

## temperature indicating device on cl-7390a

The first high-power ceramic-metal hydrogen thyratron, General Electric's GL7390, is now being built to MIL specifications. A modified version of this tube, the GL7390 A , is equipped with an integral anode temperature indicator for convenient readings. Both the GL-7390 and the GL-7390A have ratings of $33-\mathrm{kv}$ peak anode voltage and 4 -amp average current.

61.7390A
hydrogen thyratron bulletin ayailable
For a comprehensive analysis of the theory and application of hydrogen thyratrons, write to the Power Tube Department, General Electric Company, Schenectady, N. Y. Ask for Bulletin PT-49. To order, or obtain more information on hydrogen thyratrons, contact your neareat Power Tube sales office. Phone numbers are listed below.


POWER TUBE DEPARTMENT
GENERAL ELECTRIC
TELEPHONE TODAY - Syracuse, OL 2-5102 . . caition, M. J., GR 3-6381 . Now York City, WI 7-4065 ... Wastiagtian, D. C., EX 3-3600 ... Cwicags. SP 7.1608 ... Darten, 8 A $3.7151 \ldots$ Orlanto, Fla., GA 4.62811. Los Angoles, CR 9-7785.

## NEW PRODUCTS

Storage Tube


Double-ended scan converter readout storage tube type K 2070 provides resolution in excess of 1 , 000 lines at $50 \%$ modulation. Simultaneous or sequential reading and writing is possible; retention. erasure, and decay rate are controlled.

Electronic Tube Sales Dept., Allen B. Dumont Laboratories, Div. of Fairchild Camera and Instrument Corp., Dept. ED, 750 Bloomfield Ave., Clifton, N. J.
Multiplier-Modulator
583


Miniature analog multipliermodulator model 100 provides $2 \%$ accuracy in case size of $1 \times 1-1 / 2 \times$ 3 in . Inputs are de to $20 \mathrm{kc}, \pm 1.5 \mathrm{v}$, output 100 to $20,000 \mathrm{cps}$, zero to 1.4 $v \mathrm{rms}$. Distortion is less than $1 \%$ : response time as a modulator is less than 1 msec .

Transmagnetics Inc., Dept. ED, 40-66 Lawrence St., Flushing 54, N. Y.

Ratio Computer 586


Output is 1 ma or 10 mv suitable for driving pen writing or stripchart recorders. Model 557-2B ratio computer accepts two independent dc signals as low as 10 mv . Accuracy of computed ratio is $1 \%$. Uses include measurement of ratios from strain-gage type transducers, thermocouples, resistance bulbs.
Magnetic Instruments Co., Inc., Dept. ED, Thornwood, N. Y.
Dept. ED,

Encapsulated variable inductors. with single or bifilar windings meet MIL-C-15305. Coils are tuned by a powdered iron core. Inductance variation is $\pm 20 \%$ from nominal, with temperature coefficient of $\mathbf{- 5 0}$ to 100 ppm per deg C. Distributed capacity is 1.5 pf max.

Vanquard Electronics Co., Iept. ED, 3384 Motor Ave.. Los Angeles 34, Calif.

## Angle Repeater



Accurate within 6 min. Panelmounted model PPR-20 displays the angular position of remote unit to within 6 min of arc. Range is 0 to 360 deg, slewing rate 180 deg per sec. Unit has solid-state construction and rapid response. Panel size is $1-3 / 4 \mathrm{in}$. OD by 1-1/2 in. long

Theta Instrument Corp., Dept. ED, 520 Victor St., Saddle Brook, N. J.

P\&A: \$1,500; \& weeks.

Vane-Axial Blower
575


Delivers 140 cfm of air against a static pressure of 5 in . of water at $25,000 \mathrm{ft}$. Sea level output is 77 cfm against 5 in . of water. No pressure-sensing or speed-regulating switches are needed in the system. Motor is wound for 200 vac 400 cps , three phase.
Globe Industries, Inc., Dept. ED 1784 Stanley Ave., Dayton 4, Ohio

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Designers who count on CLARE stepping switches as components for complex counting, totalizing and sequencecontrol equipment know that from the wide CLARE line they can select the exact switch their application requires. If necessary, CLARE engineering will provide special switch designs.
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C. P. Clare Canada Lld., 840 Caledonia Road

Toronto 19, Ont. Cable address: Clarelar.

## NEW PRODUCTS

Pressure Transducer


High-range absolute pressure transducer $7: 37$ meets oovernment specs in miniature size. Ranges from 0 to 4,000 up to 0 to 10,000 psi are made, with resolution to $0.2 \%$, resistances 1 K to $10 \mathrm{~K} \pm 5 \%$
Bourns, Inc., Dept. ED, 6135 Magnolia Ave., Riverside, Calif.

Shaft Extensions


Available in $1 / 8,3 / 16$, and $1 / 4 \mathrm{in}$. shaft sizes, these precision shaft extensions have male and female ends in the same or any combination of these sizes. Length of extension is 1-5/8 in. Diameters are concentric to 0.0005 in .
PIC Design Corp., Dept. ED, 477 Atlantic Ave., East Rockaway, L. I.. N. Y. PRA: S!5 to 75.00; from stock.

Wide Band-Pass Filters


Typen NB-1 and NB-1B are four-crystal networks contained in at hermetically sealed package less than $1 \mathrm{cu}-\mathrm{in}$. and $2.5 \mathrm{cu}-\mathrm{in}$. respectively. The center frequency of both types is 10.7 mc $\pm 3 \mathrm{kc}$ with a 6 db bandwidth of $200 \mathrm{kc}+10 \mathrm{kc}$, -0 kc and an ultimate rejection of 100 db min. Singly they provide a 60 to 6 db bandwidth ratio of $\mathbf{2 . 2 5}$ to 1 .
Midland Manufacturing Co., Dept. ED. 3155 Fiberglas Road, Kansas City 15, Kan. Availability: From stock.


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ELECTRONIC DESIGN • July 5, 1961

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Use Atomex gold immersion solution for more perma. nent, less expensive coating of printed circuits, metallized plastics, etc. with complete assurance of tarnish resistance and electrical resistivity, In a simplified immersion process, 24 K gold is deposited by ionic displacement in a thin, dense, uniform protective layer. - Atomex is the first practical gold immersion solution containing no free cyanide. It eliminates need for costly analytical controls. Write for technical data.

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Providing $6 \mathbf{l b}$ of linear force from a few watts of power, the firm's model 11 torque motor operates in high humidity and temperature. Unit can operate while immersed in fluids,resists shock to 67 g , and operates from -66 to +400 F . Device weighs 12 oz and meets MIL specs.
Midwestern Instruments, Inc., Dept. ED, P. O. Box 7509. Tulsa 18, Okla.

## Potentiometer Tester



Plots results on X-Y recorder. This potentiometer tester, type 2398, supplies necessary signals to plot resistance vs shaft rotation on an $\mathrm{X}-\mathrm{Y}$ recorder. It operates in two ranges, from 1 ohm to 1 meg and from 10 ohms to 10 meg . and provides 120 db resistance measurement capability.
F. L. Moseley Co., Dept. ED, 409 N. Fair Oaks Ave., Pasadena, Calif.

Ceramic Bases
539


For mounting components. Alumina ceramic bases are said to be extremely rugged, useful at temperatures as high as $1,000 \mathrm{C}$. Parts are custom fabricated. Complete subassemblies with metalized ceramic bases brazed into metal parts are available.
Metalizing Industries, Inc., Dept. ED, 338 Hudson St., Hackensack, N. J.


Of course-but they are much broader than you might think. The illustrated units are just a few of the difficult and unusual switches that Centralab has been called upon to design.
What kind of special switch do you need? Centralab engineers can modify an existing type, or design an entirely new switch to solve your problems.
For immediate attention, write directly to Centrabab's Switch Sales Manager, outlining your problem.

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a. 3 pole 18 pos
-. 3 pole 18 position unit with 6 positions on each section.

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ELECTRONIC SWITCHES • VARIABLE RESISTORS - CERAMIC CAPACITORS • PACKAGED ELECTRONIC CIRCUITS • ENGINEERED CERAMICS circle su on reader.service card

## NEW PRODUCTS

Shock and vibration resistant. Shock tests in excess of 200 g resulted in no visible shifting of components. Peak acceleration at 500 cps vibration is 200 g ; and at $2,000 \mathrm{cps}, 90 \mathrm{~g} ; 487 \mathrm{de}$ signs are available.

Masterite Industries, Dept. ED. 851 W. Olive St., Inglewond, Calif.
Availability: from stock.
Curve Follower


Function generator converts manual set-point control to automatic program control. The DataTrak curve follower can drive ganged pots to provide up to 12 control signals. Dust-tight case is 19 in . wide.
Research. Inc., Dept. ED, Box 6164, Minne. apolis 24, Minn.

## Proportional Solenoid

Occupying less than 1-1/2 cu in., and weighing less than $4-1 / 2 \mathrm{oz}$, this proportional solenoid, model 15, provides relatively small, highforce displacements proportional to input signals. Unit operates in temperatures to 400 F , is submersible in fluid or gas, and can be mounted to provide force in any direction.

Midwestern Instruments, Inc., Dept. ED, P. O Box 7509, Tulsa 18, Okla.

ELECTRONIC DESIGN • July 5, 1961

## Oscilloscope

Sensitivity is $50 \mu v$ per $\mathbf{c m}$; low noise level permits resolution of signals down to $10 \mu \mathrm{v}$. Model 403-B commercial oscilloscope permits display of nonamplified outputs from strain Lages, pressure pickups, accelerometers and other transducers. Its 21 sweeps range from $1 \mu$ sec to 5 sec per cm

Allen B. Du Mont Laboratories, Dept. ED -50) Bloomfield Ave., Clifton, N. J.

## Current Recorder



Five-ampere current recorder has better thatl -2 over-all accuracy, and a frequency response ण1 25 to 5011 cps. Safe working voltage is 750 rnss. iuput resistance is 0.112 ohm . At standard chart speed of $1 \mathrm{i} n$. per hr, paper supply lasts 31 days.
Rustrak Instrument (o.. Dept. ED, 1330 Silver St., Manchester. N. H.
Price: $\$ 105$.

## Volt-Ohm-Milliammeter



Models 267 and 268 are designed for general laboratory work and production line testing. Sensitivity is 5,000 ohms per volt for both models. Microampere ranges are 0 to 50 for model 267 and 0 to 60 for model 268.
Simpson Electric Co., Dept. ED, 5200 W. Kinzie St., Chicago 44, III.
Availability: Immediate from distributors.

## High-Performance

Commercial Potentiometer-Under \$1

Now-solve the quality-price dilemma with Bourns E. $\mathbf{Z}$ Trim * commercial potentiometers. These subminiature thoroughbreds are direct descendants of the time-proven Trimpot \& potentiometer, and their performance shows it. They stand up to steady-state humidity and fully satisfy the requirements for such demanding applications as industrial controls.
Settings you make with E.Z Trim units are pinpoint-sharp. thanks to the superior angular resolution afforded by the 15 -turn shaft. They stay that way, too, because the shaft is self-locking. Adiustments are fast and simple-an ordinary CIRCIE 84 ON READER-SERVICE CARD

Take your choice of wirewound or Resiston carbon units. Wirewound Model 3067 handles a hefty $1 / 2$ watt at room temperature, is available with resistances of 100 ohms to 20K. Carbon Model 3068 offers resistances of 20K to 1 Meg. Both units have either printed circuit pins or solder lug terminals.
Order in production quantities of 1000 or more, and these exceptional potentiometers are yours for under $\$ 1$ each. Tell us you're in a hurry, and you'll have them within 48 hours -they're on the shelf from coast to coast. Write now for complete data and list of stocking distributors.



## 8036 SMALL, RUGGED CERAMIC <br> HYDROGEN THYRATRON SAVES VALUABLE SPACE

Tung-Sol leads the way with a ceramic Hydrogen Thyratron that fills an important design need. An electrical equivalent of the popular Tung. Sol 5949A - only one third tube volume is required by this new member of the family.
Tung-Sol ceramic Ilydrogen Thyratron 8036 has rugged environmental ratings. It is designed for flange mounting with flexible connecturs to achieve a solid mounting with lossfree terminations. Grid connection is made to the flange through the grid ring clamp.

For full technical data, consult your Tung-Sol representative or write: Tung-Sol Electric Inc., Newark 4, N.J. TwX:Nk 193.


HYDROGEN THYRATRON GEBTA 6587A, a glass thyratron, is a direct plug. in replacement for Tung-Sol overall height are saved by means of the ring disk type of construction, which also provides the advantages of external (cool) anode and lower lead inductance. It is rated for higher voltages
with higher currents than prototype tubes. Grid connection can be made through the grid ring or through the tube base pin. An internally-connected hydrogen reservoir promotes long life.

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| Overall melogh, max | $3.75{ }^{\circ}$ | 6. | 8.75 |
| Peak forwera voltage | 25. KV | 18. | 16. |
| peazeurront | 500. Amps | 365. | 325. |
| Peak Pulse Power (Delivered is ino losa) | 6.25 Mw | 3.25 | 2.6 |

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## (4) TUNG-SOL

## NEW PRODUCTS

## Time-Delay Relay



Solid-state time-delay relay SI-01-TD, weighing less than 3 oz , has no moving parts. Supply voltage is 18 to 30 v dc; delay is $30 \pm 6 \mathrm{sec}$. Equivalent contact rating is $40 \mathrm{v}, 10 \mathrm{ma}$. Operating temperature range is -55 to +125 C .

Espey Manufacturing \& Electronics Corp., Saratoga Industries Div., Dept. ED, Saratoga Springs, N. Y.

## Oven Assembly

547
Three-vacuum oven assembly model 8435 is for bake-out of semiconductors and other devices at 200 or 300 C. A single pump evaluates to $1 \times 10^{-3} \mathrm{~mm} \mathrm{Hg}$. Control is sensitive to within $\pm 1 / 2 \mathrm{C}$. Each oven has individual controls. Work chamber is $18 \times 18 \times 18$ in.

Electric Hotpack Co., Inc., Dept. ED, Cottman Ave. at Melrose St., Philadelphia 35, Pa.

## Navigation Gyro

548
For missile applications and other high performance uses, type C70 2527-001 floated-rate integrating gyro has an angular momentum of inertia of $500,000 \mathrm{sm}-\mathrm{cm}^{2}$ per sec. Vertical drift is 0.003 and aximuth drift is 0.015 deg per hr , short term
General Precision, Inc., Kearfott Div., Dept. ED, 1150 McBride Ave., Little Falls, N. J.

Pulse Counter


Differential pulse counter F 160 has separate coils for addition and subtraction. Simultaneous add and subtract commands are accepted without error. Count rate is $\mathbf{2 5}$ per sec max. Front plate size of the five-digit counter is $2 \times 3-3 / 4$ in.
Presin Co., Inc., Dept. ED, 2014 Broadway, Santa Monica, Calif.
P\&A: \$62.50; stock.

## Potentiometer Transducer

587

Miniature. low-pressure transducer, madel L-96, has less than $1 \%$ error at vibration levels exceeding 35 g . Available in 0 to 10 to 0 to 350 psi absolute or gage pressure ranges. Performance is said to be unaffected by temperature variations. The unit weighs 4 oz and measures 1 in . in diameter and 2 in . long.
Servonic Instruments, Inc., Dept. ED, 1644 Whittier Ave., Costa Mesa, Calif.

## Medium-Power Relay

550
Rated at 15 amp . the GF series relay is for motor loads of up to $1 / 2 \mathrm{hp}$ and can be used in a wide range of ac and dc applications. Contacts are spst to 4 pdt. Standard relays with $1 / 4-\mathrm{in}$. diameter silver contacts are rated at 15 amp at 115 v ac or 28 v dc.

American Machine \& Foundry Co., Potter \& Brumfield Div., Dept. ED, Princeton, Ind. P\&A: $\$ 3.30$ to \$7.10: from stock.

## Integrating Gyro

549
Floated-rate integrating gyro type C70 2516 010 is suitable for missiles. Angular momentum is $101.000 \mathrm{gm}-\mathrm{cm}^{-}$per sec ; short term vertical drift is 0.02 deg per hr; short term azimuth drift is 0.03 deg per hr ; mass unbalance shift is 0.5 deg per hr
General Precision. Inc., Kearfott Dis., Dept. FII, 1150 McBride Ave.. Little Falls, N. J.

Drive Regulators


Variable-speed drive regulators and exciters use silicon controlled rectifiers and diodes to provide $0.1 \%$ regulation at base speed, with response times up to twice that of tube-typhe regulaturs. Drives range from 1 to 350 hp .

Reliance Electric \& Engineering Co., Dept. ED, $247(11$ Euclid Are., Cleveland 17, Ohio.

the first economical, space saving, vertically mounted resistor for printed circuit
applications

| MEPCO | MEPCO |
| :---: | :---: |
| EC 254 | EC254 |
| 500k 1\% | 500K $1=$ |

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importance in solving today's tough design problems. MEPCD's new miniature $1 / 4$ W Carbon Film resistors were specifically
designed to break the cost and space barrier in printed circuit applications.
Having both leads extending from one end and available in three different lead spacing arrangements, these Carbon Film Resistors for vertical mounting offer advantages never before available.

Write or call today for samples and literature.
SPECIFICATIONS


## Resistance Values up to 100,000,000 Megohms

Model RX-1 Hi-Mcg Resistor

Victoreen Hi-Meg Resistors -
Standard of the Industry for Over 18 Years

Available tolerances
1\% 2\% 5\% 10\%

For longer life, Victoreen Hi-Meg Resistors are in a class by themselves, especially for all high-impedance, low-current applications. Hi-Meg Resistors have a carbon-coated glass rod element with silver-banded ends for best electrical contact . . . are vacuum sealed in a glass envelope treated with special silicone varnish that minimizes moisture effects. Always specify Victoreen Hi-Meg Resistors for the ultimate in long-term stability.


## NEW PRJDUCTS

## Booster Amplifier



This dual-channel booster amplifier is able to drive both stators of a precision size $11,40(0)$ eps resolser. Known as model 1012, the device has unity gain, an accuracy of $0.05 \%$, and less than 5 min phase shift. The unit occupies 1 cu in., weighs 1 oz , and operates from -55 to 12 is C. Iifferent mounting configurations are available.

Melcor Electronics ('orp), Dept. EL), 48 Toledo St., South Farminydale, L. I., N. Y.
P\&.A: \$250-280 ench: 30 days.

## Germanium Transistor

545
For critical computer switching applications. Type 3917/2N4(1) germanium transistor meets mechanical and environmental stability requirements of MLL-S-19500B. Specifications are: col-lector-to-base voltase, -25 v max: collector-toemitte rvoltage. -24 v max with $\mathrm{V}_{\mathrm{var}}$ at -1 v ; operating ambient temperature, -65 to +85 C

Radio Corporation of America. Dept. EI), Somerville, N. J.
Availability: Immediuto.

## Magnetic-Tape Rewinder



Spools 10.5 -in. reel in 90 sec. Average rewind speed is 500 ips. The TR- 300 magnetictape rewinder has a universal hub variable from 3 to $3-3 / 4 \mathrm{in}$. which accepts NAB or IBM tape reels without adapters. Tape guides handle tapes $1 / 2$ or 1 in . wide.

Electronic Engineering Co. of Calif., Automation Div., Dept. ED, 1601 E. Chestnut Ave., Santa Ana, Calif.
P\&A: $\$ 690$; 6 weeks.


## Gamewell made a pot that will trip a microswitch

This $7 / \mathbf{s}^{\prime \prime}, 100,000$ ohm pot has a microswitch attached. The camshaped shaft can actuate the switch precisely at the chosen point A simple solution - yes. but the answer to a special problem.
Gamewell's YES service

- Your Engineered

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is amazingly capable at
designing simple
answers to special pot
problems. Why not put
it to the test? Write
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Specials service

the gamewell company, potentiometer division, 1421 Chestnut street, newton upper falls 64 , mass. A SUBSIDIARY OF E. W. BlISS COMPANY.

CIRCLE 88 ON READER-SERVICE CARD
ELECTRONIC DESIGN • July 5, 1961


For up to 3,000-psi oil pressure two-way solenoid valves are available in normally open and normall.: closed types. Both are pilot operated poppet valves in cartridge form and can adapt to any type of manifold or sub-plate. The poppet and plunger are the only moving parts.
Fluid Power Accessories, Inc. Dept. EI). Box 64. Glenview, III

Plugs and Receptacles 572


Phenolic molding compounds are used in the manufacture of these multiple plugs and receptacles, available in a variety of shapes and terminal arrangements. Applications include appliances. electronic equipment and other industries.

Hooker Chemical Corp., I)urez Plastics Div., Dept. ED. Niagara Falls, …

Multivibrators

## 11

One-shot multivibrators are offered in two types: the T-166 contains a built-in noise rejection cirtains a built-in noise rejection cir-
cuit and the $\mathrm{T}-167$ is designed to have a pulse-width variation of $5 \%$ max from -45 to 65 C. A pulse width of $2 \mu \mathrm{sec}$ to 1 sec can be generated by either unit.
Engineered Electronics Co., Dept. ED. 1441 E. Chestnut Ave., Santa Ana, Calif. P\&A: \$38.40: \$64.50: 2 weeks.

## General Instrument Planar Tranisistors

## At last! A truly passivated planar! New 2Nroe silibon ssitch

For high speed logic switching with assured reliability, the General Instrument 2 N708 npn silicon planar switch features the unique Molecular Shield"M surface-passivation process. Here's a planar that is stable, reliable and uniform...lot by lot... with excellent gain characteristics as well as extremely low leakage current. Designed for switching applications, this type, as well as others in the popular 2 N 706 class, utilizes the latest planar techniques. Extensive tests have proved that this type of transistor construction offers definite circuit advantages. Life tests, for example, indicate little degradation as a result of operation and storage at high temperatures. The immediate availability of the 2 N 706 series in production quantities should be of interest to designers now using our silicon mesa transistors. The 2N708 is also available in limited quantities. For microtransistors, pancake•package transistors...for all your silicon planar and mesa transistors, call the sales office or franchised distributor nearest you. Or write for complete details to General Instrument Semiconductor Division, 65 Gouverneur St., Newark 4, N.J.
Abbreviated Specifications-General Instrument NPN Silicon Planar Transistors

| Type | $\mathbf{V}_{\text {cio }}$ | $\mathbf{V}_{\text {CER }}$ | $\mathbf{h}_{\mathbf{4}}$ | $\boldsymbol{T}_{\mathbf{s}}$ |
| :---: | :---: | :---: | :---: | :---: |
| 2N706 | $25 v$ | 20 v | 20 | 60 nsec |
| 2N706A | 25 v | 20 v | 20 | 25 nsec |
| 2N706B | 25 v | 20 v | 20 | 25 nsec |
| 2N708 | 40 v | 20 v | 30 | 25 nsec |

GENERALINSTRUMENT SEMICONDUCTOR DIVISION geverallustrument corporatoh

## NEW PRODUCTS



Any 17-bit time code containing three binary words for seconds, minutes or hours can be generated. Model 6202 time-code generator, for ground or airborne use, has a stability of $10^{7}$ per day. One code format can be supplied as an amplitude-width-modulated code on a $1,000-\mathrm{cps}$ sine wave and as a dc level shift.

Epsco-West, Dept. ED, 240 E. Palais Road, A naheim, Calif.

## Five-Digit Voltmeter



Accuracy is $\mathbf{0 . 0 1 \%}$. This five-digit voltmeter has a range of $\pm 0.0001$ to $\pm 999.99 \mathrm{v}$ dc. Speed is 20 readings per sec avg; outputs are BCD and 10 -line decimal; all switching is electronic ; dimensions are 5-1/4 $\times 19 \times 20 \mathrm{in}$.

Electro Instruments, Inc., Dept. ED, 8611 Balboa Ave., San Diego 11, Calif.

## Power Inductor



Variable power inductor is designed for complex load banks, accurate voltage control for tuning and phase-angle control circuits and breadboard filter circuits. It is available in two overlapping ranges from 10 to 40 and 40 to 160 mh . Dc resistance in either range is less than 5 ohms with dc and rms current of 0.5 amp max. Servomechanisms/Inc., Dept. ED, 200 N. Aviation Blvd., El Segundo, Calif.

## Design with <br> MALLORY MERCURY BATTERIES for new sales appeal in your products



PERSONAL RADIATION MONITOR, developed at Oak Ridge National Laboratory, warns of radiation levels by flashing a neon lamp and sounding a tone in a hearing aid earphone. The transistorized circuit operates 24 hours a day for 30 days at a time, from power by a single Mallory TR-133R mercury battery.
Photo courtesy Oak Ridge National Laboratory
Operated by Union Carbide Corporation
For the U. S. Atomic Energy Commission


PORTABLE TRANSISTOR TEST SET is made by Metronix, Inc., a subsidiary of Assembly Products, Inc. Used as the DC power source, Mallory Mercury Batteries assure stable voltage over long periods of time, are undamaged by momentary short circuits, and provide long shelf life.


MICROMINIATURE TRANSMITTER, used for monitoring tooth wear and pressures and for other biomedical applications, is made by Varo, Inc. Small enough to be fitted into a dental bridge, it transmits information over short distances to a pickup/preamp, utilizing an RM-312 Mallory Mercury Battery smaller than an aspirin tablet.


A DUAL INSTRUMENT FOR REACTOR MONITORING, the $\log n$ Period Amplifier made by Keithley Instruments, Inc. gives extremely accurate low-level DC measurements. The constant voltage source used for calibrating this sensitive instrument is a Mallory Mercury Battery . . . chosen for its steady voltage and an accuracy within $\pm 1 / 2 \%$. Stable, long-lived Mallory Mercury Batteries are used as the power supply for several other Keithley instruments.

Miniaturize your new product . . . make it more portable . . . give it extra long service between battery changes . . . with Mallory Mercury Batteries. Pioneered by Mallory, these unusual batteries last 3 to 7 times longer than conventional batteries, depending on drain. They provide the highest watthours per pound of any commercially available primary battery. Sizes smaller than an aspirin tablet deliver ample energy for many miniature circuits.

Mallory Mercury Batteries have the unique characteristic of staying at constant voltage throughout their long life. This property is ideal for transistor circuitry . . . also proves useful in applying these cells as a highly stable source of voltage for reference or calibration. Voltage of cells coming from production varies no more than a few millivolts.

As for shelf life, we've tested mercury batteries held in storage for over six years: capacity loss was minimum. Steel case construction with molded grommet seal makes them free from leakage.

Choose from a broad line of standard single or multiple voltage cells . . . or let us develop a custom power pack or you. Write us for consultation and engineering data.

Mallory Battery Co., North Tarrytown. N. Y. a division of P. R. Mallory \& Co. Inc.

## Mallory

[^4]In Europe: Mallory Rulleries, Lid., Dagcnham, Eingland


Have no moving parts. Six types of PowerMax integral horsepower, position servo amplifiers are available. Positioning accuracy is typically better than $0.3 \%$. Dc inputs include analog programer output, positioning potentiometers, selector switch and fixed-resistor networks, electromagnetic flow-meters and static switching circuits.
Electromation Co., Dept. ED, 4254 Glencoe Ave., Venice, Calif. Availability: stock.

Resistor Networks
589


Lug-type resistor networks are made in lengths to 6 in., with up to 13 resistors. Values can be matched to $0.005 \%$; individual tolerances are $0.01 \%$. Values range from 1 ohm to 2 meg , with ratings to 3 w and 1 kv .

Reon Resistor Corp., Dept. E[), 155 Saw Mill River Road, Yonkers, N. Y.

Photoelectric Reader


Sorts by color. Photoelectric reader model 150 provides a resistance range of about 25 K to 250 K from white to black surfaces at a distance of $1 / 8 \mathrm{in}$. from the lens. Volume is $2 / 3 \mathrm{cu} \mathrm{in}$. Range is flush to $1-1 / 2 \mathrm{in}$.; weight is 1 oz .

Melpar, Inc., Dept. ED, 3000 Arling. ton Blvd., Falls Church, Va.

[^5]
circle ol on reader-service card

## NEW PRODUCTS

Vertical Sensing Element 580


Two-axis, proportionally damped, bubble-type A 1800-01A-A vertical sensing element drives gyro torque motors. Vertical accuracy is $\mathbf{+ 1 5}$ min of arc, repeatability is 5 min and tilt angle is 0.75 deg nominal at full-scale output.

General Precision, Inc., Kearfott Div., Dept ED, 1150 McBride Ave., Little Falls, N. J.

## Power Supply Cabinet

542


Shock and vibration, category D per MIL-E4970A, are withstood by this power supply cabinet. Designated model 2C, the cabinet is weath-er-proof and suitable for outdoor use. The cabinet is offered on nine of the firm's standard power supply models providing de currents up to $1,500 \mathrm{amp}$ from 15 to 135 v .

Christie Electric Corp., Dept. ED, 3410 W 67th St., Los Angeles 43, Calif.

## Bellows Couplings



Allow 5-deg misalignment. Solid, split-hub, and combination miniature bellows couplings transmit 200 oz-in. max torque. The phosphor bronze units have zero backlash, permit 5 -deg max misalignment, and $3,000 \mathrm{rpm}$ max speed. Surface is palladium flash-plated.

FAE Instrument Corp., Dept. ED, 16 Norden Lane. Huntington Station, L. I., N. Y.

674

## when

conditions

## are

 critical...
here's why
HOLDWE POWER - atlee clips are specially contoured to flex under tension. Their grip actually increases as shock and vibration increases. PROVEN RESULTS - no visible shift. ing or twisting - no lead-breaking resonance - holding power un. changed by heat or constant use.
COOLING EFFICIENCY - atlee clips, acting as heat sinks, approach within $10 \%$ of "infinity". PROVEN RESULTS - operation of transistor at maximum ratings without life shortage.
ELECTRICAL INSULATION-atlee clips are available with Dalcoal B coating. an enamel combining twice the dielectric stength of Teflon with equal heat conductivity of mica. PROVEN RESULTS - proper electrical insulation from chassis and proper thermal behavior.

SEND FOR TRANSISTOR APPLICAXION
TABLE - A comprehensive listing of attee clips for specific transistor application.


CIRCLE 92 ON READER-SERVICE CARD ELECTRONIC DESIGN • July 5, 1961

This variable-voltage power sup ply has an output from 0 to 140 v ac with regulation of $=6 \%$ at 75 w. Maximum no-load output is 142 v rms. Front panel meter reads 0 to $150 v$ with $1 \%$ full scale accuracy. Unit measures 9-3/8 x 4-7/8 x 5-1/2 in.

Lafavette Radio Corp. Dept. ED. 165-08 Liberty Ave.. Jamaica 33, N. Y'
Price: $\$ 19.75$.

## Miniature Pentode

Improved linear deflection is featured in the 6 HB , a T 6-1/2 miniature pentode. Designed for receiver applications, the tube has a transconductance of $25.000 \mu \mathrm{mhos}$.

Raytheon Co., Industrial Components Div., Dept. ED. 55 Chapel St., Newton 58, Mass.
P\&A: $\$ 0.72$ en, 100 or mary; immedinte.

## Recycling Timer

 516

This compact recycling timer designated series Dual-Trol, produces a series of on-off electrical pulses. It consists of two timing modules. one for the on and the other for the off signal, which can be adjusted to vary the timing interval. Ten replaceable modules are available with timing ranges from 6 sec to 3 hr . Units are rated at 10 amp and measure $7-1 / 2 \times 5-1 / 8 \times 5-9 / 16 \mathrm{in}$.
Industrial Timer Corp., Dept. ED, 1407 McCarter Highway, Newark 4, N. J. P\&A: $\$ 77.50$; sir to pight weeks.

CIRCLE OJ ON READER-SERVICE CARD $\rightarrow$

## New Transfilter ${ }^{\circ}$ Combinations

## Greater selectivity in a miniature package

. . . and increased stability at a decreased cost. Further, magnetic shielding can be eliminated as well as the necessity for factory and field alignment. That's why CLEVITE'S ceramic i-f filters are rapidly replacing conventional components in today's mobile or high quality commercial receivers. Basic component of these rugged fixed-tuned devices is the CLEVITE piezoelectric "Transfilter" developed especially for great stability of resonant frequency with respect to time and temperature. Cascading and coupling these resonators provide excellent selectivity at desired bandwidths. Size, $1^{1 / 2^{\prime \prime}} \times 3 / 4^{\prime \prime} \times 2.0^{\prime \prime}$ high; Center Frequency, 455 kc ; Shape Factor ( $60 / 6 \mathrm{db}$ ), 3:1 to 6:1; Bandwidth, 4 to 20 kc ; Insertion Loss, 6 to 12 db max. (depending on bandwidth); Impedance, 2700 ohms in and out; Temperature Range, $-20^{\circ} \mathrm{C}$ to $+90^{\circ} \mathrm{C}$. Call, write or wire for complete details.
CLEVITE ELECTRONIC COMPONENTS
232 Forbes Road, Bedford, Ohio / Division of ELEEITE Corporation


## NEW PRODUCTS

## Angular Accelerometers



Resolution is $0.01 \%$ of full scale. The AA series angular accelerometers for sensing roll. pitch and yaw cover from 0.5 to 500 radians per $\sec ^{2}$ in five models. They can be used with carrier amplifiers or $400-\mathrm{cps}$ power systems and are suitable for missile instrumentation and control.
Dynamic Measurements Co., Dept. ED, 106 Terwood Road, Willow Grove, Pa.

## Image Orthicon

428
With rugged construction as well as high sensitivity, type GI-7409 image orthicon is designed for military applications such as in missiles, satellites, fire control and drone guidance.
General Electric Co., Cathode Ray Tube Dept., Dept. ED, Syracuse, N. Y.

## Infrared Bolometer

426
Mosaic infrared bolometer permits imaging or photographing extensive areas at one time through the use of passive heat emission. A complete image can be provided in a fraction of a second.
Barnes Engineering Co., Dept. ED, 40 Com mercial Road, Stamford, Conn.

## Program Drill



Drills up to 200 holes in any pattern through a load of one or more printed-circuit boards, up to $8 \times 12 \mathrm{in}$. Model 120 automatic program drill, having a repeat accuracy of 0.002 in ., is a high-speed electric drill with a pneumatically operated spindle and movable work tablr controlled by paired stop-pins set in a revelving control disk.
Develop-Amatic Engineering, Dept. ED, 923 Industrial Ave., Palo Alto, Calif.

## SILICONE NEWS from Dow Corning

## Engineer for Value



## New Dielectric Gel Assures Protection Plus Easy Repairs

If value engineering is important to $\boldsymbol{z o u}$. so is Dielectric Gel. Tnis nen "see-through" potting material offers all the advantages of other materials plus visual inspection and instrument testing . . . plus easy repair . plus fool-proof repotting.
A water white, medium viscosity liquid, Dielectric Gel readily surrounds components. It cures in place, forming a resilient mass with outstanding dielectric properties, good thermal stability and moisture resistance. No significant stresses are developed during or after cure. Serviceable from -60 to 200 C, Dielectric Gel protects potted components and circuits from
shock and vibration. wher entironmental extreme- . . . is excellent for filling and impreqnating caparitors. maynetic amplifiers. similar components and devices.
Circuit- and components potted in Dielec. tric (iel can le checked both visually and by instrument. When probes are removed. Dielectric Gel heals itself. To replace a defective part you simply cut anay the Dielectric Gel with a knife or scissors. replace the defective component and pour fresh Gel around the part. Result: Original high quality protection:

CIRCIE 800 ON READER SERVICE CARD

Dow Corning

# ...Specify Silicones 

## No Heat-loosened Terminals Here

Repeated soldering dores not loosen terminals mounted on silicone-glass laminate made nith Dow Corning resins. lightweight and rugged, silicome-qlass laminates provide greater strenyth at elevated temperatures than many metals
keep, their excellent dielectric properties despite sturage, environmental aying. rapidly changing ambients. vibratory shock and high humidity. These are the reasons why Lear, Inc., Grand Rapids, Michigan selected siliconeglass laminate for the capacitor muunting board in their Stable Platform Model 2013J.


CIRCIE SOI ON READER SERVICE CARD
Easy Way to Repair Encapsulations
It's eass to replace defertive parts encapsulated in Silastic ${ }^{\text {® }}$ RTV. the fluid silicone rubber that cures without heat. First. you cut a slit in the Silastic RTV jacket; second, replace the component: third. patch the cut by pouring fresh silastic RTV over the repair . . . there's no measur. able lose in dielectric propertien or physical strength. Encap-ulation with Silastir RTV offers theve advantages. (on): resistance to muisture. fungus. corrosive atmospheres. corona and ozone. excerlent dielectric properties. good heat dissipation and all operating temperature range of $-(0)$ (o) 2.50 C . Silastic RTV assures top value protection.


CIRCIE 802 ON READER SERVICE CARD

## Heat-sink Sealant Ups Performance

When transistors and diodes are mounted with Dow Corning compound as the heat-sink sealant. heat dissipation improves up to $50 \%$. That's because this greaselike silicone compound doesn't dry out, harden, melt or lose its initial properties from - 50 to 200 C . . . even after long time expusure. Duw Corning silicone cumpound has excellent thermal conductisity and increases the heat transfer between diode-and-washer and washer-and-chassis
improves device performance. Applied to lead terminals and connector pins after soldering, Dow Corning compound protects against corrusion, corona and shorts.


ClRCIE 303 on reader service card

## CORPORATION MIDLAND, MICHIGAN

$\qquad$

ELECTRONIC DESIGN • July 5, 1961

## $\left\{\begin{array}{l}\text { 白 } \\ 0\end{array}\right.$

## The Right Formula

 For Your Career Your Ability + Cadillac
## = A Better Position For You

It's an easy formula to remember and it's one that has stood the test of 30 years of service. Cadillac is the nation's largest electronic placement service and is retained by over 520 top electroni firms-both large and small-from coast to coast. Cadillac's service is COMPLETELY CONFIDENTIAL and available to you ABSOLUTELY FREE OF CHARGE.

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If you wish to receive a monthly bulletin of the finest available electronics opportunities, simply send us your name and home address (and, if you wish, a review of your qualifications). Our services are without cost to you through our Chicago office and our Los Angeles subeidiary, Lon Barton Associates.


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Where More Electronic Executives Find Their Positions han Anywhere Else in the World

CIRCLE 072 ON READER-SERVICE CARD

## Class 1, Nikrothal L

Kanthal's Standard Nickel-based Alloy for resistors and potentiometers

## Now better gwalley and at a lower price!

Thanks to new aging equipment and more efficient processing, Kanthal now offers Class 1, Nikrothal $L$ with a maximum temperature coefficient of resistance of $\pm 5$ ppm per ${ }^{\circ} \mathrm{C}$ from $-50^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ (was $10 \mathrm{ppm})$ and at a five per cent reduction in bare wire price. Prices have been correspondingly lowered for insulated Class 1 , Nikrothal L.
Don't forget Class 2, Nikrothal L, and Classes 1 and 2, Kanthal DR - no change in quality or price.
$W$ riso loday for Kambal's now Precision Resistenco Alioys Bulletion describing physical properties, sizes, spocificastions, design and

## NEW PRODUCTS

High-Low Temperature Chamber


Range is -100 F to +600 F . Temperature can be lowered from 70 F to -100 F in 5 min , and raised to 600 F in 45 min . Heating unit is electric resistance type, operating on 15 amp , 115 v ac. Refrigerant is liquid $\mathrm{CO}_{2}$. Sealed construction is said to permit continuous operation at -100 F without condensation. Unit measures $21-1 / 2 \times 14 \times 18 \mathrm{in}$. Test space measures $9 \times 11 \times 10 \mathrm{in}$.
Bemco, Inc., Dept. ED, 11631 Vanowen St. North Hollywood, Calif.
P\&A: \$440.00 FOB Nurth Hollywood; from stock

## Controlled Switches

527
Fast recovery silicon controlled switches operate from 50 to 800 ma average, 10 amp peak Complete recovery occurs in $2 \mu \mathrm{sec}$; rise time is $0.1 \mu \mathrm{sec}$. Voltage ratings of the pnpn devices range from 30 to 200.

Solid State Products, Inc., Dept. ED, 1 Pingree St., Salem, Mass.
P\&A: $\$ 10$ to $\$ 29$ ea, 100 to 999; stock.
Delay Lines


Lumped-constant electromagnetic delay lines are designed for microminiature circuit applications. Delay is $0.35 \mu \mathrm{sec} \pm 5 \%$; risetime is 0.03 $\mu$ sec max ; impedance is 1,500 ohms; temperature range is -55 to +125 C. Unit shown occupies 0.3 cu in . Requirements of MIL-STD-202-B are met.

Andersen Laboratories, Inc., Dept. ED, 501 New Park Ave., W. Hartford 10, Conn.

## $+500^{\circ} \mathrm{Fro}$ - $100^{\circ} \mathrm{F}$ in SIX minutes Withnew delta TEMPERATURE CHAMBER

Rapid tomperature cycling without sacrificing preciso conirol $\left( \pm 1 / 2^{\circ} F\right.$ ) is achieved with the Delia 1060F fempera fure chamber.
This convenient bench model can make the complete cycle berween $-100^{\circ} \mathrm{F}$ and $+500^{\circ} \mathrm{F}$ in less than melve minutes.
An auxiliary timer Dolta MR-1 is available for use in tost work whore automatic cycling is dosired.
For further information on the 1060 F and other Delfa remperature chambers, confact your local Delta represen. tative or write


CIRCLE 97 ON READER-SERVICE CARD


ELECTRONIC DESIGN • July 5, 1961


Solid-state device is designed to switch input signals of up to $1 v$ with a resolution of $5 \mu \mathrm{v}$. Designated type SW-101, the unit switches up to 1,000 times per sec. Switching transient is less than 4 mv ; gating power is less than 2.5 mw , and error is less than $50 \mu \mathrm{v}$. No external transformer is required. The unit occupies less than $1 / 2 \mathrm{cu}$ in. and weighs 8 g .
Alpha-Tronics Corp., Dept. ED, 1033 Engracia, Torrance, Calif.
Availability: 80 duys.

## Multicoder

432
For all IRIG channels with sampling rates for PDM systems. Transducer-source resistances up to 5 meg may be used. Other features of the multicoder are: input of 28 v at $1-1 / 4 \mathrm{w}$. input resistance greater than 100 meg at 70 C . input impedance at $1,000 \mathrm{cps}$ of 150 K .

Applied Electronics Corp. of N. J., Dept. EI), 22 Center St., P. O. Box 4:3, Metuchen, N. J.

Absolute Pressure Transducer
485


Designed for use with corrosive media, the model 723 absolute pressure transducer is a bourdon-tube, potentiometer-type instrument with a stainless steel isolation bellows. Range is from 0 to 350 , to 0 to 3,500 psia. Typical static error band is $\pm 1 \%$. Resistance is 1 K to 10 K . Nominal resolution is 0.25 to $0.45 \%$. Power rating is 1.5 w continuous at 165 F . Units are $1-3 / 8 \mathrm{in}$. in diameter and 3 in . long. Weight is 7 oz.
Bourns, Inc., Instrument Div., Dept. ED, 6135 Magnolia Ave., Riverside, Calif.

# New Pangiescent 

## Iamp by Sylvania

## puts a dramatic idea in appliance design

Now you can design exciting new sales appeal into almost any appliance with Panelescent ${ }^{\text {² }}$ (electroluminescent) lamps.
For example, in the control panel of a room air conditioner. This startling new form of light glows beautifully in the dark, makes a control panel clearly visible in dim rooms or during the night.
Not a bulb, not a tube, but a sheet of metal with an electrified coating, the Panelescent lamp is virtually indestructible, gives off no heat, either. Installation by mass assembly is simple. No sockets,
bulbs, fragile parts, or complicated assemblies. Panelescent lamps use a minute amount of current, glow for years without ever needing to be switched on or off.
See your Sylvania representative for more information about how Panelescent lamps can be used to improve a new product you're planning. Or write now to Special Products Division, Sylvania Electric Products Inc., 60 Boston St., Salem, Mass.
With 6000 different kinds of lamps
8YLVANIA LIOHTS THE WAY


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GENERAL TELEPHONE \& ELECTRONICS

# NEW! solid State time/delay/relays 



## ...with traditional AGASTAT* reliability!

Now available . . . solid state time/delay/relays with the accuracy essential for critical missile and computer applications! These new AGASTAT relays are the result of over 25 years' time delay engineering and manufacturing experience . . . specialized experience which has made AGASTAT the standard of reliability throughout industry.
Advanced design combines specially selected semiconductors and other components in a "modular-sandwich" configuration. Result: the standard modules mean flexibility; uniformity; and rapid delivery of "custom" produced prototypes. The solid state AGASTAT is hermetically sealed . . . resistant to vibration and shock. Special circuitry protects against input polarity reversal, provides immunity to voltage transients and continuously modified inputs.
What are your requirements? These solid state relays are only $1-5 / 16^{\prime \prime}$ sq. ... available in six standard types, with delay on pull-in or drop-out; timing ranges from 0.01 sec . to 10 hours, fixed or adjustable. Operation $-18-32$ vdc; -55 c to 125 c; load capacity to 5 amperes. Write Dept. SI-47 for data sheet. Or ask for a quotation on your special application requirements.

## NEW PRODUCTS

Brakes and Clutches


Size 5 brakes and clutches have torque ratings of $6 \mathrm{oz}-\mathrm{in}$. min engaged and $0.05 \mathrm{oz}-\mathrm{in}$. max disengaged at 28 v dc. Brake torque is 2 oz-in. Units consume 1.16 w and have a 2.8 msec response time at 28 v . Minimum engagement voltage is 6 v dc. Designed for use in analog navigation computers, units weigh 0.97 oz and meet MIL specs.

Clifton Precision Products Co., Inc., Dept. ED, 5050 State Road, Drexel Hill, Pa. Availability: Off-shelf delivery.

## Hermetic Sealing Glass

532
Precision electronic components can be hermetically sealed in this glass, Kovex 50. The glass is said to provide a matched seal with metal. Annealing point is 502 C ; softening point, 700 C ; thermal expansion coefficient, 48 x $10^{7}$; density, 2.27 ; power factor, 0.25 ; dielectric constant, 4.98 ; loss factor, 1.24 .

Mansol Ceramics Co., Dept. ED, Belleville, N. J.

## Static Relay



Sensitivity is $0.5 \mu \mathbf{w}$. The ultRelay static relay with meter-movement sensitivity handles up to $750-\mathrm{w}, 650-\mathrm{cps}$ loads, and is virtually unaffected by shock and vibration. Power amplification ratios are 90 to 100 db . Operating temperature range is -40 to +160 F .

Airborne Accessories Corp., Industrionic Div., Dept. ED, 5456 W. Washington Blve., Los Angeles 16, Calif.
Price: $\$ 85$.


It's a fact! Only a specially designed indicator can exactly meer the precise circuitry requirements of computers, data proceming and control systems.
Only Tec. Litiss can be tailored exacely to meet your demands-at comperitive prioes - by engineers who conceived and developed the concept of self-contained transistorized indicator devices.
Every Tec-LuTe-a complex transitorized indicator or a simple lite-is manufactured under risid quality assurance programs to surpaces military and commercial quality standards.

Write for detailed information on TEC-LTRS. . . custom designed to exoced your most exacting demands.
orioimator of patentio
TRANSISTORIZEO INDICATORS


Transistor Electronics Corporation
3357 Ropublic Ave. - Minneopolis 26, Minn TWX MP 331 • WE 9-6754

CIRCLE 100 ON READER-SERVICE CARD


For TO-18 package. Heat sinks for mesa transistors in the TO-18 package use a threaded nut for secure contact with transistor weld flange. The two-piece, stud-mounted sinks are of aluminum having high thermal efficiency. No. 1107 is anodized, No. 1106 has caustic etch finish
Thermolloy Co.. Dept. ED, 2130 Irving Blvd.. Dallas 8. Tex.

Silicon Controlled Rectifiers


Rated at 25 amp at 100 C, diffused silicon controlled rectifiers of the TI-150 series are housed in stud package. Rated breakover voltages, both forward and reverse, are 50, 100, 200, 300, and 400 w respectively for the TI-150. 151, 152, 153 , and 154.
Texas Instruments Inc., Dept. ED, P. O. Box 5012. Dallas 22, Tex. Arailability: Immerdiatr.

## Silicon Transistors

502


In TO-18 case, phy alloy junction silicon transistors 2 N935 through 2 N 946 are electrically equivalent to TO-5 types such as 2 N 1917 through 2N1922, 2N1025, and others. They are suited for switching. communications, and instrumentation uses.
Sperry Semiconductor Div., Sperry Rand Corp., Dept. ED, Norwalk, Conn

## New Improved CBS PNP Power Transistors <br> 2N538(A) • $2 \mathrm{~N} 539(\mathrm{~A}) \cdot 2 \mathrm{~N} 540(\mathrm{~A})$ FEATURE MORE POWER, LESS WEIGHT, LESS SPACE

The CBS 2N538(A), 2N539(A) and 2N540(A) have a maximum dissipation of 30 watts at a base mounting temperature of 25 deg. Centigrade. Yet, each transistor weighs less than 5 grams and requires only $1 / 3$ square inch of chassis space.

Compact and rugged, these hermetically-sealed CBS PNP Germanium Power Transistors are ideal for military and industrial power applications demanding high reliability. They are especially suited for servo motor controls, power amplifiers, converters, power supply regulators and low-speed power switches.
Note the major characteristics and advantages. Call or write today for complete technical data and delivery information from your local sales office or Manufacturer's Warehousing Distributor.


## CBS semiconductors

More Reliable Products through Advanced Engineering


CBS ELECTRONICS, Semiconductor Operations, Lowell, Massachusetts
A Division of Columbia Broadcasting System, Inc. - Semiconductors • tubes - audio components - microelectronics
Sales Offices: Lowell, Mass., 900 Chelmsford St., GLenview 2-8961 • Newark, N. J., 231 Johnson Ave., TAlbert 4-2450 Melrose Park, Ill., 1990 N. Mannheim Rd., EStebrook 9-2100 • Los Angeles, Calif., 2120 S. Garfield Ave., RAymond 3-9081 Toronto, Ont., Canadian General Electric Co., Lid., LEnnox 4-6311.


FIELD PROVEN!
3240
WITH Q日 ROBOTEC overload and hort protectio
and M4.11 heatran electronic dissipotion
control \$34950
FOB FACTORY Other Modet Available. Write
for Catalog d solid state DC power supply with $05 \%$ regulation. 1 millivolpripple. 01 ohm source im. pedance, 50 microsec pedonce, 50 microsec and response time, 55 440 cycle input. 440 cycle input.
I MMEDIATE DELIVERY EOgewad 3.5200 (LD Aroa Cale 316)
CIRCLE 103 ON READER-SERVICE CARD

1708 SMAMES ORIVE, WESTBURY, MEW YORE

## NoW!

CONTINUOUS PRODUCTION
 SEMICONDUCTORIZED POWER SUPPLY $-5015$

## Ar Puner Devigus inc.

Y 170 SMAMES DRIVE, WESTBURY, MEW YOAK FDrewnad 36200 (LD Area Cove 516) CIRCLE 104 ON READER-SERVICE CARD

## NEW PRODUCTS

Bulkhead Connector


This compression-sealed unit has a normal leakage rate of less than $10^{-7}$ cc per sec, with rates of $10^{-4}$ cc per sec available on special order. Bodies and pins are fused with glass, meeting MIL-C-5015 specifications. Various contact arrangements with 12 to 32 pins are available. Unit mates with any standard MS socket
Escon, Inc.. 735 Branch Ale., Providence. R. I.

## Module Cage

507
Instrumentation module cage holds up to 24 printed circuit cards, or up to 12 modules 1.375 in. wide. Standard 22 -pin or 24 -pin connectors mount at rear. Modules are available ior strain sage, telemetry, and recorder uses.
Wiley Electronic Products Co., Dept. ED. 2045 W. Cheryl Drive, Phoenix, Ariz.

CONTROL DATA


High Speed Punched Paper Tape Reader

- Unsurpassed Reliability
- Advanced Mechanical Design
- 350 Char/Sec Read Rate
- Start-Stop or Continuous Mode
- 5, 7, or 8 Level Tape
- Tape Widths: $11 / 10^{\prime \prime}, 7 / 6^{\prime \prime}, 1^{\prime \prime}$
- Instantaneous tape width selection
- Reads all punched tape Paper-Plastic Colored-Plain
Oiled or Non-oiled
- Complete freedom from programming limitations
The Control Data Model 350 Paper Tape Reader employs the most advanced tape controls and reading techniques. Multi-colored tapes can be read interchangeably without the need of bias adjustments, and new specially designed light guides in the reading head eliminate dirt collecting holes. The precise control system eliminates troublesome resonances and provides complete freedom from programming limitations. These and other features combined with careful attention to details and quality, result in a paper tape reader which provides new high standards of reliability and versatility.
rer provides new hish and
CONTROL DATA CORPORATION


## CEDAR ENGINEERING DIVISION

 CIRCLE 105 ON READER-SERVICE CARD

## Connector Cables

506
Color-coded connector cables are made for in terconnection of audio equipment. Plugs are provided. Basic colors of white, green, yellow red and blue are available. Colored marking strips and color dots may be easily applied.
Zoron, Inc., Dept. ED. 512 W. Monroe St., Chicago, Ill.

Time Delay Relay


Of almost crystal can size, this time delay relay, Model M-100, has spdt output contacts rated at 0.25 amp . Input voltage is 24 to 32 v dc. Adjustable time ranges are from 5 msec to 30 $\mathrm{sec}, \pm 5 \%$ under 10 sec and $\pm 10 \%$ over 10 sec . Units are hermetically sealed, rated at one million operations, and available in a variety of mounting styles.

Electronic Products Corp., Dept. ED, 4642 Belair Road, Baltimore 6. Md.

Designed to cool digital modules, particularly the firm's S-PAC series, the model CU-30 cooling unit utilizes three axial-flow fan units mounted in parallel within the chassis. It has a removable dust filter. The airduct may be adjusted to draw air from either the front or rear of the cabinet. Unit measures $19 \times 5 \times 8 \mathrm{in}$.

Computer Control Co., Inc., Dept. ED, 983
Concord St., Framingham, Mass.
P\&A: \$12\%.00; delivery from stork,

## Differential Mv Commutator

459


Range is dc to 20 kc for the differential millivolt commutator, packaged for missile and ground support applications. Specifications include: nower, 1 w at 28 v : input impedance. 100 K : sensitivity, 10 mv full-scale input: resolution, better than $20 \mu \mathrm{v}$ : linearity, better than $11.25 \%$.
Applied Electronic: Corp. of … J., Dept. EI), 22 Center St.. P. O. Box 43. Metuchen, N. J.

## Leak Detector



For testing hermetically sealed components. Leaks in the $10^{-11}$ cc-per-sec range can be detected with the type 24-510 leak detector. Up to 10,000 transistors can be tested in each cycle, requiring less than an hour. Components are soaked in a nontoxic radioactive gas, are air washed. then are tested for traces of radioactivity.

Consolidated Electrodynamics Corp., Dept EI), 360 Sierra Madre Villa, Pasadena, Calif.

## EVERYONE TALKS

## IIN HERMETICALLY SEALED CONNECTORS

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TERMINATING AND CHECKOUT - RELIABILITY ASSURANCE SUBSTANTIALLY REDUCES THE NEED FOR USER'S VERIFICATION TESTING These are only a few of tne many reasons why you should consult the world's most experienced manufacturer of electrical connectors for your hermetic sealing needs. For immediate delivery and quotations write, phone, or wire Customer Services Manager, PHOENIX DIVISION, 2801 AIRLANE, PHOENIX, ARIZONA. Phone BRidge 5-4792. Test report and complete KPT Catalog available upon request from:

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The Cannon KPT Hermetic line is designed to, and far sur passes all requirements of MIL-C-26482 ... has proven sta. tistically reliable in leakage tests 200 times as severe as that required by MIL-C-26482. Cannon offers you hermetic seals with a reliability coefficient of .999 at a confidence level of $95 \%$. Our rigid manufacturing controls and continued testing guarantee reliability at no added cost-and, in many instances, at lower prices than ordinary hermetic seals. Available for off-the-shelf delivery from Cannon stocking points and CAPS Distributors throughout the United States. LEADFREE COMPRESSION GLASS EXCEPTIONALLY LEGIBLE CONTACT IDENTIFICATION FOR FASTER

CANNON ELECTRIC COMPANY, 3208 Humboldt Street, Los Angeles 31. California.


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## NEW PRODUCTS

Sea-Water Depth Transducer


Range is $\mathbf{3 5 0}$ to $\mathbf{1 , 0 0 0}$ psia for model 734 seawater depth transducer. Other features include : resistances of 5 to $10 \mathrm{~K} \pm 5 \%$, resolution of as low as $0.15 \%$; vibration limit of 35 g at 2,000 cps, static error band of $\pm 0.5 \%$. dimensions of 2 in . in diameter by 1.44 in ., and weight of 16 oz .

Bourns, Inc., Dept. ED, 6135 Magnolia Ave., Riverside, Calif.

## Appliance Wire

528
Tefion TFE and FEP insulation is 10 mils to $1 / 32$ in. thick on appliance wire AWG 16 to 26. Temperature ratings are 105 to 200 C max. with voltage ratings to 600 v . Wire is $\mathrm{U} / \mathrm{L}$ approved.

Tensolite Insulated Wire Co., Inc., Dept. ED, W. Main St., Tarrytown, N. Y.

## Ultrasonic Delay Lines

531
Almost temperature-independent. These delay lines are manufactured of Code 8875 glass. This material has a nominal time delay temperature coefficient of zero $\pm 0.75 \mathrm{ppm}$ per C. Attenuation coefficient is low enough to permit time delays of $350 \mu \mathrm{sec}$ or higher at frequencies below 10 mc .

Corning Glass Works, Dept. ED, Corning, N. Y.

## Frequency Standard

461


For 360 to $1,300 \mathrm{cps}$ with accuracies of $0.002 \%$. Type 27 frequency standard measures $11 / 16 \mathrm{in}$. in diameter and $2-15 / 16 \mathrm{in}$. long. It weighs $1-3 / 4 \mathrm{oz}$, requires 20 to 30 v dc at 5 ma and operates over a temperature range of -65 to +125 C. Vibration conditions of MIL-E-5272B Procedure II are met.

American Time Products, Div. of The Bulova Watch Co., Inc., Dept. ED, 61-20 Woodside Ave., Woodside 77, N. Y.


BLOWERS


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Rated at 15 w at 25 C with maximum operating temperature of 265 C. Model 3030 wirewound potentiometer offers resistances of 10 ohms to 10 K and nominal resolution of as low as $0.6 \%$. Weight is 0.9 oz ; size is $1.07 \times 0.52 \times 1.27 \mathrm{in}$. Applications include in power supplies.
Bourns, Inc., Dept. ED, 6135 Magnolia Ave., Riverside, Calif.
Price: $\$ 8$ to $\$ 10$.

## Synchros

Bu/Weps specification MIL-S-20708A are met by this series of synchros over a temperature range of -55 to +85 C . The series is designed for use in fire control, radar, navigation, missile functions, and similar applications.
Kearfott Div., General Precision, Inc., Dept. ED, Little Falls, N. J.

## Image Orthicon

433
For near infrared use, type Z5395 image orthicon is suitable for both military and industrial applications. It can be used to penetrate hazy atmospheres for mapping and surveillance, as well as in passive detection systems.
General Electric Co., Cathode Ray Tube Dept., Dept. ED, Syracuse, N. Y.

Static Inverter
462


Rated at 175 va, model 143-101-171 static inverter has an output of 115 v ac, 400 cps , single phase from an input of 25 to 30 vdc . Output voltage and frequency are maintained within $\pm 1 \%$ from no load to full load; harmonic distortion is held to within $\mathbf{4 \%}$. Uses include missile and aircraft ground support equipment.

American Electronics, Inc., Precision Power Div., Dept. ED, 1598 E. Ross Ave., Fullerton, Calif.


CIRCLE 109 ON READER-SERVICE CARD

## NEW PRODUCTS

Inductance Bridge


Designed for 400 to $20,000 \mathrm{cps}$ operation. this inductance bridge is basically a calibrated variable frequency oscillator coupled to a modified Maxwell bridge. The bridge, model 63B, provides direct-reading calibration of both the inductance and resistance dials, with a resolution of $0.01 \%$. Inductance range is $0.02 \mu \mathrm{~h}$ to 11 h : resistance range, 0.002 ohm to 110 K . Accuracy is about $0.25 \%$.
Boonton Electronics Corp., Dept. ED, Morris Plains, N. J.

## Image Orthicon

With ultraviolet sensitivity, type GL 7969 image orthicon is suited for missile detection systems, spectrographic detection and medical instruments. Light-level capacity can be as low as $10^{-5} \mathrm{ft}-\mathrm{c}$. Resolution is high
General Electric Co., Cathode Ray Tube Dept. Dept. ED. Syracuse, N. Y

## Fast-Responding Pico-ammeter

431
For nuclear applications, this pico-ammeter has a dynamic range of $10^{-12}$ to $10^{-3} \mathrm{amp}$ in 19 ranges and an accuracy of better than $3 \%$ of full scale at all outputs. Speed of response is less than 1 msec to $64 \%$ of final value at $10^{-3}$ to $10^{-3} \mathrm{amp}$.
General Electric Co., Dept. ED, Schenectady 5. N. Y.

## Variable Inductor



For low audio range. Miniature saturablecore reactor model EL-215 operates at 1 w from 30 to 450 cps min , and 250 to $3,750 \mathrm{cps}$ max. Used to determine frequencies in filter and oscillator circuits, it is effective as a lowfrequency sweeping device. The potted unit operates in temperatures from -55 to +85 C .
Vari-L Co., Inc., Dept. ED, 207 Greenwich Ave., Dept. ED, Stamford, Conn.

## HOW TO GET THE POWER TRANSISTORS YOU NEED?



JUST ASK DELCO. For even though our catalog lists only a handful of germanium power transistors, there is only a handful out of all those ever catalogued that we don't make. And those only because nobody ever asked for them.
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You get Delco transistors fast. You get Delco transistors in any quantity. And for all their high reliability, you get them reasonably priced. All you have to do is contact our nearest sales office-and ask for them.

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CAG ELECTRONICS COMPANY 2021 Third Avenue, Seattle 1, Washington MA 4-4354

## Ask for a complete catalog

 DELCO RadoCIRCIE 111 ON READER-SERVICE CARD

## Voltage Reference



Solid-state, shielded voltage reference standards of series 220 provide $5.7,8.5$, or 10.5 v dc at 10 ma . Operating from $115 \mathrm{v}, 60 \mathrm{cps}$ line. regulation is $\pm 0.001 \%$ for $\pm 10 \%$ line variations Capacitance from line to output is less than 1 pf.

Viking Industries, Inc., Dept. ED, 21343 Roscoe Blvd., Canoga Park, Calif.
P\&A: 150 ; \& weeks.

## Timing and Control Systems

434
Programed timing and control systems provide initiation and termination of various switching functions at preselected times. Programing is from punched tape, punched cards, magnetic tape, hard wire, patch panels or thumbwheel switches. Digital design and modular construction are used.

Curtiss-Wright Corp., Electronics Div., Dept. ED. P. O. Box 10044, Albuquerque, N. M.

## Size 11 Resolvers

529
Small. light weight size 11 resolves are intended for such applications as computation, angle data transmission and automatic control. Models CR4-0987-001 through CR4-0987-005. have a $0.1 \%$ function error, $\pm 3 \mathrm{~min}$ inter-axis error, and $0.1 \tilde{c}_{c}$ transformation ratio unbalance.

Kearfott Div.. General Precision, Inc., Dept. ED, Little Falls, N. J.

Submersible Pan-Tilt
489


Operating to $1,000 \mathrm{ft}$ depth, model 3003.2 submersible pan and tilt mechanism permits remotely controlled underwater positioning with 360 deg of pan and 90 deg of tilt. Remote readout of pan and tilt position is available.

Ward Associates, Dept. ED, P. O. Box 9067. San Diego 9. Calif.
P\&A: $\$ 8,000$ : 60 days.

## MICRO-MINIATURE RELAY STYLE 6A

For Printed Circuits

Less Space
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Conform to 0.2" Grid Spacing

For reliable switching of low-level as well as power loads. Style 6A will operate at coil power levels below most larger current-sensitive relays in its general class, yet easily switches load currents of 2 amps resistive and higher at 26.5 VDC or 115 VAC. Contact arrangement to DPDT.

Unique construction permits flexible wiring and a variety of schematics. Withstands 50 G shock and 20 G vibration to 2000 cycles.

Meets applicable portions of specifications MIL-R-5757D and MIL-R-25018 (USAF) Class B, Type II, Grade 3.

Call Or Write For Additional Information

## PRICE ELECTRIC CORPORATION

302 E. Church Street - Frederick, Maryland MOnument 3-5141 • TWX: Fred 565-U CIRCLE 112 ON READER-SERVICE CARD


New design capabilities unfold as RC,A's amazing nuvistor tube family grows in number. You now have at your fingertips five commercial nuvistor types which permit you to nuvistorize your critical equipment designs for greater efficiency and extreme compactness.
RCA-7587 general-purpose sharp-cutoff industrial tetrode RCA-7580 general-purpose medium-mu industrial triode RCA-7895 high-mu industrial triode ( $\mu=64$ )
RCA-ECW4 TV and FM tuner triode
RCA-2CW4 TV and FM tuner triode
Design features responsible for the fast-growing popularity of nuvistor tubes include:

- Low heater drain - Very high transconductance at low plate current and voltage - Exceptional mechanical ruggedness from ceramic-and-metal construction - Exceptional uniformity of characteristics from tube to tube - Operation at full ratings at any altitude - Extremely low interelectrode leakage - High sensitivity and stability • Very small size and light weight

Nuvistorized circuits are currently in use or under de. velopment for:

- Jet engine wave and vibration analyzers
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- Pulse-width discriminators, frequency multipliers
- IF amplifiers in airborne weather radars
- Cascode amplifiers in radar beacon IF strips . and literally scores of other applications.

Discover for yourself what nuvistor tubes can do in your own critical circuils. For information, contact your RCA Field Representative, or write: Commercial Engineering, Section G-18-DE-1, RCAElectron Tube Division, Harrison, New Jersey.

5-3900 - MIDWEST: Chicago 54, III., Suite 1154, Merchandise Mort Plozo. Whitehall 4-2900 - WEST, Los Angeles 22. Calif., 6801 E. Washington Blvd., RAymond 3-8361• Burlingame, Calif., 1838 EI Camino Real, OXIord $7-1620$

## NEW PRODUCTS

Thermoelectric Generator


Eight-watt thermoelectric power generator is designed for operation of remote, unattended industria field instrumentation. Fuel is natural gas, propane or butane. Rugged, reliable unit may be continually exposed to weather. Weight is 65 lb , width 12 in ., height 17 in

Texas Instruments Inc., Dept. ED, P. O. Box 6027, Houston 6 Tex.

## Ultrasonic Probe

Operating to 100 kc , with useful response to 1 mc , probe VP-10 provides an inexpensive means of measuring ultrasonic levels. The probe will stand a static pressure of 100 psi , and is unaffected by high temperatures. Output at cavitation is several volts, permitting use with simple equipment for waveform and level display

Vibrasonics, Inc., Dept. ED, 10 High St., Boston, Mass.

Low-Noise Preamplifier
501


For radiation detectors. Preamplifier model 100 A , featuring charge-sensitive feedback, is used with semiconductor radiation detectors. Charge sensitivity variation is less than $10 \%$ from 0 to $1,-$ 000 pf . Noise is equivalent to 600 electrons rms, rise time less than $0.1 \mu \mathrm{sec}$.

Nuclear Industries, Inc. Dept. ED, 10 Holland Court, Valley Stream, N. Y.
Price: \$295

This $100-\mathrm{w}$ broadband amplifier can provide a cw signal from 200 kc to 275 mc . Input and output imepdances of 50 and 90 ohms, respectively, are compatible with standard transmission lines and fittings. Broadband rf transformers for different impedance levels can be supplied. The cabinet measures $21 \times 22 \times 47 \mathrm{in}$., and has recessed casters

Instruments for Industry, Inc. 101 New South Road, Hicksville, N. Y.

P\&A: \$6.500: about 8 weeks.

## Power Transistors

Silicon power transistors 2N2015 and 2 N2016 have saturation resistance of 0.25 ohm max, power dissipation up to 150 w . Beta is 15 to 50 at $5 \mathrm{amp}, 7.5 \mathrm{~min}$ at 10 amp . The devices operate at case temperatures from -65 to +200 C

Radio Corp. of America, Semiconductor and Materials Dis., Dept. EI, Somerville, N. J.

Silicon Chopper

One-gram silicon chopper oper. ates from less than 1 mv to $\neq 20 \mathrm{v}$. Driving voltage is a square wave with amplitude of 5 to 25 v , peak to peak. Signal Current is 10 ma max, linearity less than $\pm 0.5 \%$ deviation from best straight line. Operating temperature is -55 to +150 C .
Solid State Electronics Co., Dept. ED, 15321 Rayen St., Sepulveda, Calif.
P\&A: \$88; stock.
CIRCLE 114 ON READER-SERVICE CARO

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Q. Why did BTU Engineering Corporation switch 10 a stepless
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Difusion furnace used in semiconuy BTU Enkineering Corporation Watham. Mass. The Stepless Control designed around th
General Eleciric SCR has no moviny parts. doses not deteriorate
with ake. It is also fail sale he absence of a signal it shuts

## Advantages of the

 BTU Stepless Control include:- No costly contactor failures
- Rellability of a solid state rectifier as the heart of the system.
- It operates "full-on." "full of" or any point in between with infinitesimally precise control.
- Nearly linear throughout ange.
- No matching of imposed land to size of control unit required.

Now lower-priced than ever be fore, the SCR opens new areas for engineering development. Can you afford 80 w'ais any longer? Write today for applica tion information. Rectifier Components Department. Section pany, Auburn, New York.


GENERAL ELECTRIC

## Light Flasher Users:

 Why does the Aero-Space Divi-
sion of the Walter Kidde Co. sion of the Walter Kidde Co. Controlled Rectifiers tatic light Reshers?

A."General Electric SCR's have made possible solid state cir-
cuits that optimize long. maintenance free life in our static flashers. They easily wuthstand the high inrush currents of incandescent lamp loads and the severtal conditions associated with commercial and military airborne equipment."


Solid state light flashers, developed by the Aero-
Space Div. of the Walter Kidde Co., Belleville, N.J. eliminate all rotating elements. nothing to wear out. vanced equipment design made possible by the use of the General Electric SCR.

Advantages of the static Ilgh flasher Includ
Withstands Inrush currents tem times normal.

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Now lower-priced than ever he ore, the SCR opens new area for ensineering development. Can you afford $t 0$ wait any onRer? Write today for appli cation information. Section 23618, Rectifier Component pany, Auburn, N. Y.

GENERAL ELECTRIC

## NEW PRODUCTS

High-Power Transmitter
415

Output is 1 to 2 kw at 200 to 400 mc . De signed for missile and space applications, the transmitter withstands temperatures of 400 or 500 F as well as severe shock and vibration. The rf circuitry is broad-banded for operation over a $10-\mathrm{mc}$ range around a selected nominal frequency.

Space Electronics Corp., Dept. ED, 930 Air Way, Glendale, Calif.

## Electroluminescent Panels

508
Metal, glass and plastic e-1 panels are now available in quantity. Metal panels can be made up to 2 sq ft , glass panels 30 in . square; plastic panels are made in a wide variety of shapes and forms. Metal panel life is about $\mathbf{1 5 , 0 0 0}$ hours. Light output is about $10 \mathrm{ft}-\mathrm{I}$ at 600 v , 60 cps .
Westinghouse Electric Corp., Dept. ED, Box 2278, Pittsburgh 30, Pa.

## Temperature Chamber

427
Range is -100 to $+350 \mathbf{F}$ for the Mark II temperature chamber. Features include: internal working dimensions of $11 \times 12 \times 5 \mathrm{in}$., liquid carbon dioxide refrigeration, resistance element heater, aluminum liner and fan with external blower motor
Associated Testing Laboratories, Inc., Dept ED, Wayne, N. J.
Price: \$285.
Decade Resistance
490


Five-dial decade resistance box has ranges from 0.0 to $9,999.9$ to 999,990 ohms in steps of 0.1 to 10.0 ohms. Temperature coefficient is less than $0.002 \%$ per deg C. Current rating ranges from 10 ma to 0.5 amp .

Voltron Products, Inc., Dept. ED, 1020 S. Arroyo Parkway, Pasadena, Calif.
Price: \$115 to \$1s0.

Super processing aids Tucor TR tubes' power-handling ability


One stage in Tucor's exclusive electronic ionization processing technique is illustrated in the highpower TR tube shown at the exhaust station. Model T48U15 is a cuuart\%, folded-cylinder tube operating at UHF and L-band frequencies with a multi-megawatt power input. This tube was designed to provide short recovery time without the disadvantages of the contaminants usually added for this purpose that shorten tube life. The addition of a newlydeveloped uranium getter maintains purity of the gas fill indefinitely.

Following the duplexer stage in which such a tube would be used. a lower-powered post-TR tube circuit is ustially required. Such tubes as the Tucor T48U9 and T48U10. which have been developed for this purpose as well as for use in medi-um-powered duplexers, provide lower leakage powers and long-life performance.

Why do Tucor tubes perform better? A combined microwave circuit and plasma physics design results in an optimum configuration and gas fill for any application.

Whether shelf items or custom designs for your specific application, Tucor tubes provide advantages in reliability. Why not investigate further by asking for our latest tube catalog?


CIRCLE 197 ON DONH Roced (Roun R, Witon, Commeticu ELECTRONIC DESIGN • July 5, 1961

## Trimmer Potentiometer



The 25-turn, $3 / 4$-in. sq model 51 trimmer potentiometer is available in ranges from 50 ohms to 200 K . It dissipates 3 w without external heat sink or other hardware. Military specs for altitude, humidity and other environmental conditions are met. Weight is 5 g .
Spectrol Electronics Corp., Dept. ED, 1074 S. Del Mar Ave., San Gabriel, Calif.

## Camera Tube

429
With tri-alkali photocathode, type 7967 camera tube is claimed to provide 50 times more sensitivity than standard image orthicons. It operates with an illumination of up to $10^{-6} \mathrm{ft}-\mathrm{c}$. The magnesium-oxide semiconductive target has almost no lateral leakage. Resolution is better than 300 TV lines at low light levels or 1,200 lines at higher levels.

General Electric Co., Cathode Ray Tube Dept. Dept. ED, Syracuse, N. Y.

## Miniature Humistor

435
Over-all length is $1 / 4 \mathrm{in}$. and header diameter is $5 / 32$ in. Model H-160-3 humistor detects and measures vapor or gases exhibiting an electric di-pole movement. Readout is through as megohmmeter or a megohm bridge. The device can be completely immersed in water and withstands temperatures from 0 to 100 C

Conrad-Carson Electronics. Inc., Dept. EI), El Cajon, Calif.
P\&A: \$10: from stock in small quantities.

## Remote Alarm



A solid-state remote alarm monitor, model 901, samples and encodes any number of data points and keys a single channel of any transmission medium. The signal is decoded and displayed at the receiver. Operation is continuous. Compact plug-in construction is employed, 17 points occupying a $3-1 / 2 \times 5-3 / 16 \times 6-15 / 16$ in. package. Units resist moisture, fungus, and high temperature.

Compudyne Corp., Dept. ED, Hatboro, Pa.


The 6 most inmportant things in your working life are your five skilled fingers and your A.W.Faber *9800 SG Locktite Tel-A-Grade Lead Holder.
Lockitite becomes a part of your creative process. The no-slip functional grip gives you smooth ess. The no-slip functional grip gives you smooth Gun-rifted cluch practically banishes finger fatigue. bull dos. Unique indicator reveals the degree in use at alance. Carries ironclad 2 -year guar nice. A FAbrg will replace the entire holder at no charge if any part wears out in normal
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Cartell Drawing leeds \#9030, ore of the identica quality and groding as world-fomous Costoll wood peneil - Usable in all standard holders, but a perfect mote for Lockrite Drows parlectly on all surfoces, includine Cronor and Mylar bose films Available in all degrees from 781010 H , and in a koleidoscope of colors -

A.W.FABER-CASTEIL

Poncil Co., Inc., Newark 3, 1. J.
 which can be readily engaged with a minimum angular error to a servomechanisms gear train when energized by an external command signal. The transducer must accurately return to a specified null position when the command signal is removed


## A SOLUTION:

Provide an electro-magnetic clusch, spring return mechanism and rotary potentiometer. Assemble these parts into the required package with the resultant difficulties brought about by the mounting and coupling problems with a consequent increase in cost.


## THE OPTIMUM SOLUTION:

Technology Instrument Corporation's west coast engineering facilities developed and offer a unitized package consist. ing of an electro-magnetic clutch, spring return mechanism and rotary potentiometer as one compact assembly. The clutch will transmit high torque without slippage and has negligible angular engagement error. TIC's unique spring return mech-
unitized package

GENERAL INFORMATION:

Shaft Position Transducers can be linear or nonlinear potentiometers, synchros. inear transformers or digitizers. Spring return mechanism can be supplied designed to return to any desired point, A built-in slip clucch can also be furnished if the input torque can exceed the rating of the clutch. anism will accurately return the output transclucer to the desired null, yet requires low driving torque. TIC's unitized assembly replaces three (3) individual components with their inherent assembly difficulties.

## TIC UNITIZED PACKAGE HAS MANY APPLICATIONS,

SUCH AS: Auto pilots, altitude controllers, machine controllers,
measurement and control problems, speed control, process
control of temperature and flow, differential measurement,
expanded scale servos, or any other problem requiring an output, commencing at some specified servo position determined by an external command signal.

## TNE

TECHNOLOGY INSTRUMENT CORPORATION

## NEW PRODUCTS

In-Wall Amplifier

For flush-mounting in frame or masonry walls, model 2030 in-wall amplifier requires a depth of 4 in . A 30-w, all-transistor unit, the amplifier includes a voltage-regulated power supply and has four microphone inputs. All 12 transistors are accessible through removable front plate.

Rauland-Borg Corp., Dept. ED, 3535 W. Addison St., Chicago 18, 111.

## Storage Tube

510
Writing speed of $\mathbf{1 0 0 , 0 0 0} \mathbf{i p s}$ and a brightness in excess of $200 \mathrm{ft-1}$ is obtained with a potential of 5 kv in the WL 7682 storage tube. One writing gun and one flood gun are used in the electrostatically focussed and deflected tube. Storage time is 30 sec to 30 min . Display area is 4 in . with an OD of $5-1 / 4 \mathrm{in}$. max.

Westinghouse Electronic Tube Div.. Dept. ED, P. O. Box 284, Elmira, N. Y.

## Multichannel Digital System



Low-level data signals are displayed and recorded on paper tape by this multichannel digital system, model ER-3295. Consisting of five separate units, the instrument scans consecutively 98 three-wire inputs from various transducers. Resolution is $\pm 1 \mu \mathrm{v}$. A digital voltmeter provides visual readout. A slave scanner can be added to increase input capacity.

Kin Tel Division, Cohu Electronics, Dept. ED, Box 623, San Diego, Calif.
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Cicoil Corp., Dept. ED. 3833 Saticoy St., Van Nuys. Calif.

## Voltage Divider

511
Decade voltage divider has total resistance of $1 \mathrm{~K}, 10 \mathrm{~K}$ and 100 K . Linearity of the five-dial unit is $0.01 \%$. temperature coefficient $0.001 \%$. The Kelvin Varley circuit is used. Box measures $3-3 / 4 \times 4 \times$ 5 in . and weighs 1 lb .
Voltron Products, Inc., Dept. ED 1020 S. Arroyo Parkway, Pasadena. Calif
P\&A: \$150: 30 daye
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Associated Research. Inc., Dept. ED, 3777 W. Belmont Ave., Chicago 18, III.


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405


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Princeton Machine and Development Co., Dept. ED, P. O. Box 187, Princeton Junction, N. J.

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417


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H. H. Scott, Inc., Dept. ED. 111 Powdermill Road, Maynard, Mass.
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Bendix Corp., Dept. ED. Red Bank Div., Holmdel, N. J.

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Consolidated Electrodynamics Corp., Dept. ED, 36ㅇ Sierra Madre Villa, Pasadena, Calif.

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Arnold Magnetics Corp., Dept. ED, 6050 W. Jefferson Blvd., Los Angeles 16, Calif.
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## REPORT



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Aero Electronics Corp., Dept. ED, 1745 W. 134th St., Gardena, Calif. Availability: 1 to 2 weeks.

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Computer Control Co., Inc., Dept. ED, 2251 Barry Ave., Los Angeles 64, Calif.

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Braincon Corp., Dept. ED, 312, Marion, Mass.

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Pioneer Electric \& Research Corp., Dept. ED, 743 Circle Ave., Forest Park, III.
Price: $\$ 9.5$

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Curtiss-Wright Corp., Electronics Div., Dept ED, P. O. Box 10044, Albuquerque, N. M.
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## NEW PRODUCTS

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Perkin Electronics Corp., Dept. ED, 345 Kansas St., El Segundo, Calif.

## IF Preamplifiers



For low-noise operation, series H modular if preamplifiers can be furnished with balanced or unbalanced input. Output impedance is 50 ohms. Tube units operate from -55 to +85 C and germanium transistor units, from -20 to +50 C. Silicon types can also be furnished. Design is miniature.

Orion Electronic Corp., Dept. ED, 108 Columbus Ave., Tuckahoe, N. Y.
P\&A: $\$ 200$ to $\$ 250$; 2 to 8 week.
Plotting Board


Vertical-horizontal plotting board type 1587 provides two simultaneous plots of any four independent voltages against time. Plotting surface is $30 \times 30 \mathrm{in}$. The unit operates with analog and digital computers, coordinate converters, radars and other analog devices.

Milgo Electronic Corp., Dept. ED, 7620 N. W. 36th Ave., Miami 47, Fla.

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## Direct Microwaves-to-Electricity Power Seen Near



Inverse magnetron converter developed by Raytheon. Left to right: cathode, anode-cavity structure, coaxial if input and cover. Final version of this device may approach 60 per cent efficiency and generate up to 1 kw cw in the 1. to 2-Gc range. Wright Air Development Div. is presenily emphasizing development of this type of microwave power converter over other possible inversely operated tubes. The weight of the final version, including magnet, will be approximately 35 lb .

## Manfred Meisels <br> Technical Editor

0FF-THE-SHELF hardware for direct conversion of microwaves into electrical power may be a reality within two years, according to scientists at the Wright Air Development Div., which is now sponsoring two research projects in this area.
Raytheon's Spencer Laboratory, Burlington, Mass., is investigating the inverse operation of magnetron-type tubes, while at Purdue University, West Lafayette, Ind.. the emphasis is on inverse operation of klystrons, and both vacuum and semiconductor diodes. Efficiencies of 60 per cent are believed possible with the inverse magnetron and semiconductor diode approaches.

Power requirements for such converters are fairly modest- 1 kw cw for the magnetron and perhaps 75 w for the semiconductor diodes. Proposed applications include powering electronic gear aboard satellites and transmitting power to unmanned equipment atop mountains and in other remote areas.
These applications and the proposed conversion methods differ markedly from those for the microwave powered helicopter (also a Raytheon project) in which heat exchangers and gas turbines would achieve power conversion. Power requirements here are measured in megawatts, though Raytheon is reportedly looking into thermionic and thermoelectric generators as an alternative to the mechanical conversion cycle. Regardless of the application and ultimate conversion scheme used, ultra-high-power microwave tubes such as Raytheon's Amplitron or General Electric's multiple-beam


## NO STEPPING SWITCHES IN THIS

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Cubic manufactures a complete line of quality digital instruments, including a-c and d-c voltmeters, ohmmeters, ratiometers, scanners and printer controls.

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INDUSTRIAL DIVISION EAN DIEGO, CALIF., U.EA. ROME, ITALY
klystron and Orthotron would be employed at the transmitter.

The direct conversion methods now being actively studied fall into three categories. - Inverse operation of conventional microwave tubes

- Vacuum diodes
- Semiconductor diode arrays

Of these, inverse operation of microwave tubes appears most likely to yield moderateorder powers (approximately 1 kw ) with acceptable efficiency. For low power, semiconductor diode arrays look promising. Light weight and small size would make them attractive for many satellite applications.

The inverse magnetron tube being developed by Raytheon as an outgrowth of earlier work with the backward-wave type Microfier has already shown efficiencies of 32 per cent. In tests at 1.28 Gc , pulsed outputs of 4 kw were obtained over a 0.1 per cent duty cycle. WADD scientists feel that cw operation at 60 per cent efficiency will eventually be obtained.

The tube consists of 30 radial vanes which form 29 anode cavities. Microwave fields applied to the tube accelerate the electrons from cathode to anode. Current is drawn to the anode when the rf interaction voltage exceeds the dc potential of the tube and Hartree threshhold voltage.

Raytheon has built nine progressively improved tubes of this type for WADD. In its ultimate version, a $1-\mathrm{kw}$ tube is expected to weigh about 35 lb . including the magnet. Continuous heating of the cathode would


Inverse klystron microwave power converter. Electron beam between cathode and collector is accelerated by microwave input. Efficiency is reduced by need to divert some of the input to the pre-bunching cavity. A separately heated cathode is required.
not be required as operation is sustained by secondary electron emission resulting from back bombardment.
Inverse operation of klystrons for direct conversion is also considered feasible. Recently initiated work at Purdue University has been confined to inverse operation of commercially available tubes. Preliminary tests at 3 Gc are inconclusive as the emphasis has been on gathering data for design of a special-purpose tube rather than on extracting power from a commercial version.
A proposed inverse klystron, illustrated here, has been theoretically analyzed by WADD with mixed conclusions. Such a unit could be designed for high powers and frequencies. However, a separate heater supply is necessary. Spreading of the electron beam and entrance angle, as well as the need to supply power to both cavities of the tube would result in low efficiency and degraded performance.
An inversely operated traveling-wave-tube converter has also been analyzed at WADD. The electron beam in this device would gain energy from the microwave field rather than surrendering it as is the case in normal twt operation. By gradually increasing phase velocity of the rf traveling wave to account for increasing beam velocity, the electrons can be accelerated while continuing to be phase locked with the traveling wave. This can be accomplished with a tapered helix of gradually increasing pitch.
Limitations of the inverse twt include need for a separate heater supply and limited power handling capability of the slow wave structure. Efficiency of such a device might approach 40 per cent.

## Cyclotron and Plasma Convertors

Believad Theoratically Possible
A cyclotron resonance converter has also been analyzed at WADD. In the basic design, electrons emitted from a central anode are spiraled outward by the cyclotron action of the rf input and a suitably adjusted magnetic field. The electrons thus gain energy from the field and strike properly oriented collector plates. By placing the collectors at a low velocity point of the electron trajectory, efficiencies of up to 60 per cent could


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ELECTRONIC DESIGN • July 5, 1961

## 200 watts paak power 20 watts CW



TYPICAL OPERATING PARAMETERS

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result, as there would be little power dissipated via electron bombardment. Back bombardment of the cathode, however, could enable heaterless operation.

Prospects for plasma converters have also been analyzed by WADD. One approach would be to create a plasma by using the microwave input and then apply a magnetic gradient to cause ion and electron drift in opposite directions. The electrons would be connected to an external load and the positive ions used to bombard a cathode to cause electron emission.

While a plasma converter would be small and easy to fabricate, the wide distribution of electron energies in the plasma would probably result in efficiencies no greater than 25 per cent.

Having analyzed these approaches to medium-power direct conversion, WADI) has settled on the inverse magnetron as the most feasible-at least for the immediate future.

## Multiple-Diode Arrays

In Development of Purdue
Equall: imaginative designs for low power converters have also been proposed. The obvious approach of vacuum diode rectification may prove useful despite electron transit time limitations. It has been shown that rectification can take place even when the cathode-to-anode spacing is equal to several hundred periods. Realistically, a spacing equal to a few periods could achieve


Inverse fraveling-wave-fube microwave power converter. Electron beam is accelerated by absorbing energy from if wave in the helix. The gradually increasing pitch of the helix keeps the traveling wave in phase with the accelerating electrons. A separate heater is required for the cathode.

COLLECTOR


Proposed cyclotron resonance microwave power converter. Rf input, in conjunction with magnetic field (perpendicular to plane of drawing), accelerates electrons to the collector plates. Studies indicate that the device could approach 60 per cent efficiency. Back bombard ment of cathode would eliminate need for heater
efficiencies of up to 25 per cent. In this mode of operation, out-of-phase electrons would absorb energy from the rf input and be returned to the cathode. The resulting secondary emission could allow heaterless operation of the diode.
Experiments at Purdue with lighthouse tubes operating as diodes have shown efficiencies of up to 20 per cent at 3 Gc . Maximum output was approximately 1 w .

Much higher efficiency and power output are anticipated for arrays of semiconductor diodes wired as full-wave rectifiers. The yroup at Purdue has operated arrays of 64 diodes placed directly in the waveguide. A 360 -diode array employing 1 N830 silicon point-contact diodes is now being assembled for testing. The diodes will be mounted in a flared section of $10-\mathrm{cm}$ guide. Outputs of between 10 and 15 w at 2.5 Gc with perhaps 75 per cent efficiency are hoped for.

Future plans call for even larger arrays developing up to 100 w . These could be distributed among several parallel sections of guide joined by a magic T or similar device.

Theoretical studies of large junction diodes as possible microwave rectifiers are also under way. In addition, nonlinear effects in bulk semiconductor materials in strong rf fields have been noted at Purdue. It has been suggested that an understanding of these effects could lead to a rectifier consisting of a large semiconductor crystal properly oriented within a waveguide. - -


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# Designing the "Parant" 



Instead of worrying about noise temperature and noise pickup in antenna leads, authors Frost and Clark circumvented these problems by integrating the parametric amplifier within the antenna structure. The resulting parant, designed for Doppler tracking of satellites, eliminates open connecting lines between antenna and amplifier. Input to the parametric amplifier is applied directly from the signal-induced potentials at the ends of the antenna. Dipole parants have been built for 54-, 108-, and 220-mc operation. Etched circuit antennas for 500 mc and slotted antennas useful at 2 Gc are being designed.


Fig. 2. Construction details of the half-wave parant. Two matched varactor diodes provide parametric amplification in conjunction with the coaxial cavity formed by the addition of the hollow center conductor. Higher order TEM modes provide resonant storage for the pump and ider frequencies

Albert D. Frost, Ronald R. Clark
University of New Hampshire,
Durham, N. H.

WHEN the need for low-noise reception warrants the use of parametric amplifiers, noise pickup in the leads between the antenna and receiver can significantly degrade system performance. Since reducing the distance between antenna and receiver is only a partial solution, it was decided to eliminate this source of noise altogether by integrating the parametric amplifier with the antenna.
Experiments were performed with halfwave and quarter-wave dipoles because the antenna elements could be most conveniently adapted to serve as the network elements of a parametric amplifier. This was accomplished by adding a concentric inner conductor to the dipole, thus forming a coaxial cavity. Units operating at 108 mc and 54 mc are illustrated in Figs. 1 through 4.
Coupling between the inner region and the outer cylindrical surface of the antenna occurs through incidental fringing capacitance and through shunt varactor diodes. The inner region, through its spectrum of TEM resonances provides the resonant storage necessary for parametric amplification.

## Parant Operates as

## A Degenerate Amplifier

The parant is operated in the degenerate amplification mode (input frequency $=$ output frequency). The fundamental TEM mode provides the signal frequency; the fifth order mode provides idler storage; and the sixth order mode matches the pumping frequency. A high order even TEM coaxial mode was chosen for pumping to minimize parasitic self-oscillations at or near the signal frequency.
The output signal is extracted from the coaxial region by a rectangular loop appropriately oriented in a radial plane. Coupling to the idler frequency is minimized by


Fig. 3. Quarter-wave dipole parant designed for 54 -mc operation. Design is similar to the half-wave unit, but note use of a ground plane. Bottom view shows internal construction and varactor diode connected be tween the inner and outer elements.
cutting loop length to a half-wavelength of the idler. The position of the loop with respect to the standing-wave current pattern in the center conductor also reduces coupling to this mode.

The diode is pumped through the center conductor, which also provides a dc path for the diode reverse bias.

Suitable external circuitry associated with the parant was designed to provide the following:

- Tuning of the idler, pump, and signal modes
- Pump input
- De bias

Networks for the half-wave, 108 -mc parant and for the quarter-wave, $54-\mathrm{mc}$ parant are shown in Figs. 5 and 6, respectively. Circuit values were chosen to match the characteristics of the 1 N894 varactor diodes used in the antennas described here.

Both the half-wave and quarter-wave parants provide stable gains of up to 15 db over passive dipoles. (See gain-frequency curves in Figs. 7 and 8).

## Antenna Can Be Electronically

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Fig. 4. Construction details of the quarter-wave parant. The antenna is single-ended and uses only one diode. However, additional diodes can be wired in parallel with the first, if desired. Construction of the quarter-wave antenna is simpler than that of the half-wave parant


Fig. 5. Tuning networks and bias blocking circuits for the half-wave, 108 -me parant. Length L represents the distributed impedance of the leads and connectors between the antenna and the circuit. Capacitors C, and $C_{N}$ fune the idler and signal frequencies, respectively.


Fig. 6. Tuning networks for the quarterwave, 54 -me parant. Single-ended characteristic of the antenno eliminates circuit balancing problems inherent in the half-wave design. Only one capacitor is required for tuning the idler or signal frequencies.


Fig. 7. Gain-frequency characteristic of the half-wave parant. Pump frequency was 600 mc


Fig. 8. Gain-frequency characteristic of the quarter-wave parant. Pump frequency was 302 mc .


Fig. 9. Tuning network for the halfwave, 108 -me parant. Unit is conveniently mounted at center section of the antenna.


Fig. 10. Etched circuit, half-wave parant. This design approach should prove useful for antenncs operating up to 500 mc . The etched circuit board replaces inner conductor of the lower-frequency parants. Resonant region is achieved by the stripline construction. Distributed elements would be used for tuning.

This change is due to the inhibition of para metric amplification and the combined effect of detuning and resistive shunting of the interior coaxial cavity. By pulsing the bias, an unmodulated signal can thus be conveniently chopped at rates up to 200 kc with $50-\mathrm{db}$ isolations. This ease of switching makes the parant a versatile beginning for many complex types of receiving systems.

The half-wave parant of Fig. 1 was constructed of 1.75 in . square aluminum pipe with a wall thickness of 0.125 in . The flat side walls and increased wall thickness as compared to earlier models built of circular pipes permit convenient use of stripline fittings and more effective support of the inner
conductor. The circular pipe was, however retained for the inner conductor. Length was calculated by the equation

$$
\begin{equation*}
L=0.48 \lambda \frac{L \cdot D}{L / D+1} \tag{1}
\end{equation*}
$$

where
$L=$ antenna length for half-wave dipole
$D=$ antenna diameter
$\lambda=$ free-space signal-wave length.
This expression was found empirically valid for conventional dipoles in which the signal is derived across a mid-point gap of negligible width and coupled to a matched resistive load. The gap in the inner conductor as shown in Fig. 2 provides the necessary dc isolation between the two diodes of the half-

## MicroWares

wave parant, but it is also an important factor in the design of tuning circuits for the signal, idler and pump frequencies.

The effect of this gap on the resonance of the inner region is dependent on the relative magnitude of its susceptance, though generally it shifts the resonant frequencies upwards.

## Distributed Impedance Is

A Factor in Design
Also across this gap are the composite impedances of the radial connections from sap to plug, connectors, leads (see Fig. 5) and internal wiring as far as capacitor $C_{t}$ in the tuning network. These act as an irregular transmission line to provide, together with $C_{1}$, a series resonance as viewed from the gap. Their detuning effect is relatively minor at the $108-\mathrm{mc}$ signal frequency of the antenna, but quite important at the $490-\mathrm{mc}$ idler frequency.

The gap is physically located at a point where the longitudinal current density and voltage gradient are high for the odd order modes. Its location with respect to the oven order modes is at a low-current, highimpedance point.

Tuning of the idler and signal frequencies, occuring at odd TEM modes, is accomplished by adjustment of series resonant branches composed of lumped and/or distributed impedance elements. With a signal frequency of 108 mc and a consequent pump frequency near 600 mc , the circuit elements are largely distributed.

The pump signal coupling loops provide an in-phase voltage across the center conductor gap. Thus, any out of phase excitation arising from signal or idler frequency components will not produce a net output along the pumping signal line. Loading and signal loss are thereby avoided.

A tuning network assembled for the halfwave parant is shown in Fig. 9. Early models of the parant were tuned by the insertion of dielectric strips into the coaxial region. It was felt that the adjustable tuning network described here is more suitable for a developmental model, but the use of dielectrics for fixed tuning may be attractive when assembling a large number of

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parants designed for constant-frequency operation at a single frequency.

Matched-diode selection for the half-wave parant emphasized voltage sensitivity and static capacity. These two characteristics were matched as closely as possible within the tolerances obtainable with the lowpriced diodes employed. Matching of reverse resistance and forward conduction point was performed less critically.

Quarter-Wave Parant Considered Simpler to Design and Fabricate

The quarter-wave parant is a more workable design from the standpoint of simplicity in construction and operation. It is essentially a half-section of the half-wave parant with the outer conductor welded to 』 conducting ground plane.
Its singled-ended configuration, as compared to a symmetrical half-wave dipole. permits more freedom of design for external circuitry and better control of cavity resonances. There is no balancing problem, either of external circuitry or diodes. Cir cuitry can be placed under the ground plane and there adjusted without affecting fields within the antenna itself.
The quarter-wave parant shown in Figs. 8 and 4 was designed for a $54-\mathrm{mc}$ signal thus allowing lumped circuit elements to be used. Tuning networks for the signal and idler resonances (see Fig. 6) are connected across the base of the cavity, as are the dc bias and pumping inputs. In designing these networks, the following precautions should be observed.

- Dc bias must be applied between the center conductor and the dipole cylinder without shorting out the pump signal.
- The bias circuit must not lower the Q of the idler and signal-tuned circuits.
- Idler and signal power must not be dissipated in the pump and bias circuits.


## Etched-Circuit and Slot Parants

 Being Designed for Higher FrequenciesParants for use at higher frequencies are now being developed at the Antensa Sys-


Fig. 11. Dual slot parant for use up to 2 Gc. Cavities behind slots in ground plane provide resonant storage for parametric amplification. Initial model of this design is undergoing operational tests.
tems Laboratory of the University of New Hampshire. In the region between 200 and 500 mc , an etched circuit antenna using essentially distributed elements for tuning appears feasible. The design shown in Fig. 10 is now being fabricated. A slot antenna, such as illustrated in Fig. 11 would operate at frequencies in the $1.5-$ to 2 -Gc range. An initial model of this type has been completed and development is being continued.

As a simple dipole, the parant can be employed alone or together with Yagi arrays. parabolas, corner reflectors, etc. Multiple units with in-phase pumping and adjusted for equal gain merit consideration in high speed electronically-scanned arrays or in direction finding systems using a Wullenweber antenna or Luneberg lens. - -

## Acknowledgment

The parant concept was evolved in connection with Doppler tracking at the University of New Hampshire of early U. S. and Soviet satellites and is being developed under the sponsorship of the Electronics Research Directorate, Air Force Cambridge Research Labora-
tories.


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# New Definitions Of Receiver Noise Performance 


#### Abstract

Shortly before the 1961 National Symposium of the IRE's Professional Group on Microwave Theory and Techniques, five authorities in the field of noise measurement undertook to agree on a workable set of definitions of receiver noise. Whether Messrs. William Mumford and Rudolf Engelbrecht of Bell Telephone Laboratories, Hermann Haus, Massachusetts Institute of Technology, Robert Adler, Zenith Radio Corp., and Matthew Lebenbaum, Airborne Instruments Laboratory, have indeed said the last word in this long-standing controversy remains to be seen. Their significant report to the symposium, abstracted here, is nevertheless strongly commended to the interest of microwave designers.


THE noise performance of a system is evaluated in terms of its output signal-to-noise power ratio under operating conditions, $S_{0} / N_{0}$. Output power is expressed as the signal power at the input multiplied by the signal gain, $G_{6}$.

The output noise power can be expressed in terms of the signal gain, $G_{s}$, input signal power, $S_{i}$, output signal bandwidth, $B_{o}$, and an operating noise temperature, $T_{o p}$. Hence, the output signal-to-noise ratio is:

$$
\begin{equation*}
\frac{S_{o}}{N_{o}}=\frac{G_{n} S_{i}}{G_{0} k T_{o p} E_{o}}=\frac{S_{i}}{k T_{o p} B_{o}} \tag{1}
\end{equation*}
$$

Two receiving systems have the same output signal-to-noise ratio if they have the same $S_{i} / k T_{\text {on }} B_{o}$ ratio.

In a single response receiver (in which one frequency at the input corresponds to a single output frequency, regardless of the complexity of the gain-frequency characteristic) the output noise power, $N_{o}$, is defined as

$$
N_{o}=G_{s} k B_{o}\left(T_{\theta}+T_{e}\right)
$$

(2)

The term $T_{0}$ is the input generator noise temperature. T. is called the "Effective Input Noise Temperature." For a two-port transducer, this is the temperature which, when
the input is connected to a noise-free equivalent of the transducer, would result in the same output noise power as that of the actual transducer connected to a noise-free input source.

To measure $T_{e}$, the designer can observe the output noise power for two different temperatures of the generator. If the ratio of the two output noise powers is $Y$,

$$
\begin{equation*}
T_{t}=\frac{T_{\rho}(h o t)-Y T_{g}(\text { cold })}{Y-1} \tag{3}
\end{equation*}
$$

The term $T_{\text {up }}$, occurring in Eq. 1 can be expressed as

$$
\begin{equation*}
T_{o p}=T_{g}+T_{e} \tag{4}
\end{equation*}
$$

An alternative definition of receiver noise, that of the Noise Figure, remains useful. Since, however, the literature contains several conflicting definitions of Noise Figure, the authors recommend the definition in the IRE standards on electron tubes. ${ }^{1}$ In terms of Noise Figure, $F$, the operating noise temperature can be written as

$$
\begin{equation*}
T_{o,}=T_{g}+290(F-1) \tag{5}
\end{equation*}
$$

In a multiple response receiver, such as a superheterodyne receiver with response at the image frequency or a parametric amplifier with response at the idler frequency,
there are two distinct contributions to moise:
$N_{00}$ - output noise due to the noise power available from the impedance connected to the amplifier input.
$V_{s}$ - All other contributions to the input noise power. These are due to noise generated within the receiver components and noise resulting from any frequency conversions within the receiver.
Letting $B_{s}$ be the limiting noise bandwidth common to all responses
$\boldsymbol{N}_{g o}=k B_{N}\left(\boldsymbol{T}_{v 1} \boldsymbol{G}_{1}+\boldsymbol{T}_{92} \boldsymbol{G}_{2}+\right.$ $\qquad$ $+T_{u n} \boldsymbol{G}_{n}$ ) (6) where $G_{n}$ is the transducer gain of the $n^{\text {'h }}$ response. That is, the ratio of output power to the corresponding input power available to the $\boldsymbol{n}^{\text {th }}$ input response.
$N_{n}$ can be characterized by a temperature, $T_{b}$, common to all responses, so that
$N_{n}=k B_{s} T_{b}\left(G_{1}+G_{2}+\ldots .+G_{n}\right) \quad$ (7)
The total output noise is then
$N_{o}=k E_{\checkmark}\left[G_{1}\left(T_{g 1}+T_{b}\right)+G_{i}\left(T_{g=}+T_{i,}\right)\right.$

$$
\begin{equation*}
\left.+\ldots \cdots+G_{n}\left(T_{g n}+T_{n}\right)\right] \tag{8}
\end{equation*}
$$

$T_{b}$ is obtained from Eq. 3.
The operating noise temperature is given by

$$
\begin{equation*}
T_{o \omega}=\frac{N_{0}}{k B_{0} G_{0}} \tag{9}
\end{equation*}
$$

Since most modern noise generators provide broadband noise, their use in direct measurement of noise injects the noise equal1 y into all responses. That is,
$\boldsymbol{T}_{o}=\boldsymbol{T}_{g 1}=\boldsymbol{T}_{g \mathrm{t}}=\ldots \ldots=\boldsymbol{T}_{\theta n} \quad$ (10)
Eq. 8 thus reduces to
$N_{i}=k B_{1}\left(T_{y}+T_{b}\right)\left(G_{1}+G_{2}+\ldots .+G_{n}\right) \quad$ (11)
To measure $T_{b}$ in terms of Noise Figure, use $T_{b}=290\left(F_{b}-1\right) \quad$ (12) where $F_{l}$, is the multiple channel or "broadband" Noise Figure.
To evaluate $F_{l}$, use

$$
F_{b}=\left[\frac{T_{g}(\text { hot })}{290}-1\right]-Y\left[\frac{T_{g}(\text { cold })}{290}-1\right]
$$

When the input signal occupies only one
response, $G_{d}=G_{1}$. If the system is designed for lowest operating noise temperature, i.e., noise bandwidth $B_{s}$ matches signal bandwidth $\boldsymbol{B}_{0}$, the operating noise temperature is given by

$$
\begin{align*}
T_{o p}= & T_{p 1}+T_{b}+\frac{G_{2}}{G_{1}}\left(T_{g z}+T_{b}\right) \\
& +\frac{G_{3}}{G_{1}}\left(T_{p z}+T_{b}\right) \\
& +\ldots+\frac{G_{n}}{G_{1}}\left(T_{p n}+T_{b}\right) \tag{14}
\end{align*}
$$

For the special case when, under operating conditions, the generator noise temperatures applied to all input responses are equal, Eq. 14 reduces to

$$
T_{o \triangleright}=\left(T_{\theta}+T_{0}\right)\left(1+\frac{G_{2}}{G_{2}}+\ldots \ldots+\frac{G_{n}}{G_{2}}\right)(15)
$$

When the received input signal is distributed over more than one input response, only the term $G_{8}$ of Eq. 9 is affected. When the portions of the input signal are uncorrelated, with powers of $S_{11}, S_{i n}, \ldots, S_{1 n}$
$G .=\frac{S_{11} G_{1}+S_{12} G_{2}+\ldots . .+S_{1 n} G_{n}}{S_{11}+S_{i 2}+\ldots+S_{i n}}=\frac{S_{o}^{(16)}}{S_{i}(\text { total })}$ Substituting $G$, into Eqs. 8 and 9 yields
$T_{*}=\frac{N_{0}}{k B_{0} G_{0}}$

$$
\frac{B_{N}\left[G_{1}\left(T_{g 1}+T_{b}\right)+\ldots+G_{n}\left(T_{g n}+T_{6}\right)\right]}{B_{n}\left[\frac{S_{i 1} G_{1}+S_{12} G_{2}+\ldots .+S_{i n} G_{n}}{S_{i 1}+S_{i 2}+\ldots .+S_{i n}}\right]}
$$

It is concluded that to evaluate the signal-to-noise ratio of any receiving system, the designer must know $T_{o p}, B_{o}$, and the total input signal power $S_{i}$ (having the same distribution over the various input responses assumed in the evaluation of $T_{o p}$ ).

The multiple-channel effective input noise temperature, $T_{b}$, (i.e., $T_{e}$ for a single response receiver) is computed by Eq. 3, the gains of the various responses, and the noise bandwidth, $B_{N}$.

With these terms, the designer can calculate his particular system's operating noise temperature, $T_{o p}$ by inserting them in the general Eq. 17, or an appropriate simpler form. - -

Reference

1. Proceedings of the IRE, July, 1957, Vol. 45, p 1000.

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| COAXIAL TYPES |  |  |  |  |  |  |
| NA10A | 1.00-4.00 | 0.10 | 3000 | $12 / 2^{\text {c }}$ Cosx | Type N) | \$495.00 |
| NSIAA | 3.85-11.0 | 0.10 | 500101500 | 13/8- ${ }^{\text {cose }}$ | Typen) | 485.00 |
| WAVEGUIDE TYPES |  |  |  |  |  |  |
| -hal08 | 3.95-5.85 | 0.08 | 8000 | 49 | 149A | 250.00 |
| ${ }^{4}$ Calos | 5.85-8.20 | 0.08 | 8000 | 50 | 344 | 180.00 |
| -W4108 | 7.05-10.00 | 0.08 | 8000 | 51 | 51 | 165.00 |
| $0 \times 4108$ | 8.20-12.40 | 0.08 | 8000 | 52 | 39 | 150.00 |
| Y410A | 12.40-18.00 | 0.10 | 4500 | 91 | 419 | 210.00 |
| KA10A | 18.00-26.50 | 0.10 | 4000 | 53 | 425 | 230.00 |
| UAIOA | 26.50.39.50 | 0.10 | 3000 | 96 | 381 | 250.00 |
| Ci02A | 5.85-8.20 | 0.03 | 8000 | 50 | 344 | 1275.00 |
| X402A | 8.20.12.40 | 0.03 | 8000 | 52 | 39 | 1275.00 |

DELIVERY FROM STOCK

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Amphanol-Aorg Electronits Corparation


PRECISION MICROWAVE EQUIPMEWT - HIEH-POWER PULSE MODULATORS - HICH-VOLTAGE POWER SUPPLIES - ELECTRONIC TEST EQUIPMENT CIRCLE 137 ON READER-SERVICE CARD

## VARIAN Potentiometer RECORDERS

More performance in less space


G-22 FOUR CHANNELS IN 14"; DEPTH ONLY $111 / 2^{\prime \prime}$ BEHIND FRONT PANEL

6. 11 TWO CHANNELS IN $101 / 2^{\circ}$. DEPTH ONLY $55^{\circ}$ EEMIND FRONT PANEL


## G. 10 ONE CHANNEL <1/2 CU. FT

## THIREE COMPAC'I CHOICE:S

Using one quarter the space of many comparable potentiometer recorders, the Varian family packs exceptional function into very little space. Interchangeable input chassis accommodate full-scale signal voltages from 10 mv to 500 v d.c., temperatures from $-200^{\circ} \mathrm{C}$ to $+1500^{\circ} \mathrm{C}$, and 1 mA current recording. The Varian recorders have $1 \%$ accuracy, $\frac{1 / 4 \%}{6}$-of span sensitivity, 1 or $2 / \frac{1}{5}$ second balancing time, full-span zero adjust, Zener diode or mercury cell reference. A selection of chart speeds from \%//hour to $16^{\prime \prime} /$ minute lets you pick the time resolution you need.
In addition to being rack-mountable, the G- 22 and G-11A are portable for use in many locations. A wide range of accessories - such as retransmitting slidewires, alarm contacts and event markers - helps broaden the outstanding functional versatility outlined above. Chances are a Varian recorder can serve your need. Write Instrument Division for detailed specifications.

mma B EPA SPECTROMETERS, MAGNETS. FLUXMETERS GRAPMIC RECORDEQS MAGNETOMETERS MICROWAVE TUBES MICROWAVE SYSTEM COMPONENTS. MIGG VACUUM COUIPMENT. LINEAR ACCELERATORS. RESEARCH AMD DEVELOPMENT SERVICES


## MICROWAVE PRODUCTS

## Reflex Klystron

Operates to 120 Gc. Reflex klystron QKK971 operates from 100 to 120 (ic with power output of 10 mw min , and a minimum life of 250 h . Anode voltage is 1.700 v , current 50 ma . Heater requires 2.5 v at 1.5 amp , and reflector voltage is -100 to $300 \%$. The integral-cavity tube has vernier tuning.

Raytheon Co., Microwave and Power Tube Div., Dept. ED, Foundry Ave., Waltham 54, Mass. P\&A: 83.500: 90 days.

## Optical Maser Head 703

Precision positioning of optical maser head model TO2000 provides aiming accuracy within 10 sec of arc. Operating from 150 to 400 K . the head handles up to 4,000 J , and will accommodate rods up to 0.2 in . diameter. Included are three pink ruby rods, sighting telescope, tube and rod cooling, sync output, and manual and automatic triggering. Power supply is available.

Trion Instruments, Inc. Dept. ED, 7300 Huron River Drive, Dexter, Mich.
P\&A: \$s,695; so days.


ELECTRONIC DESIGN • July 5, 1961



## ONE METER TO FOUR MILLIMETERS

## New Litton Electron Tubes for Advanced Applications

A. L-3403 KLYSTRON TUBE: One of our super power line, a long pulse, power amplifier klystron for the Ballistic Missile Early Warning System, delivering 1.25 megawatts peak power output.
B. L-3270 BRoadband KLystron: A 2 megawatt L-band klystron offering long life, high peak power, 8 percent bandwidth. Other broadband klystrons, using the exclusive Litton Skirtron techniques, are available with higher power in the L through S-band region with .002-.004 duty cycles.
c. L-3455 HICH POWER MAGNETROM: A new magnetron delivering a minimum of 2 megawatts peak power at $406-450 \mathrm{mc}$. with a .002 duty cycle.
D. L-3450 HIGH TEMPERATURE PULSE MAGMETRON: Provides long life operation at ambient temperatures in excess of $662^{\circ} \mathrm{F}$. Many hours of $900^{\circ} \mathrm{F}$. operation have been achieved in X-band tests.
E. L-3629 floatimg drift fube klystron: High power, water-cooled klystron oscillator fixed tuned at $33,000-37,000 \mathrm{mc}$. Power output: 15 watts CW minimum. Other tubes available for immediate delivery from $12-4 \mathrm{~mm}$. wavelength.
f. L-3472 TWT: PPM focused traveling wave tube offers higher CW power - 10 watts minimum and wider bandwidth in a compact $3-\mathrm{lb}$. size. Operates in the range of $\mathbf{7 , 0 0 0 - 1 1 , 0 0 0 ~ m c . ~ O n e ~ o f ~}$ a line of TWT's including a 1000 -watt X-band pulse tube.
G. MICROTRON: The L-3189, one-kilowatt CW magnetron, is accompanied in package form by an electromagnet and filter assembly, high voltage and filament and isolation transformers. Only 6 -second warm-up. Two year warranty for domestic microwave cooking.
H. L-3H30 CUBE MINIATURE MAGNETRON: A one-kilowatt miniature magnetron, fixed tuned at $9300 \pm 30 \mathrm{mc}$, weighing less than 9 ounces and no bigger than a normal X-band waveguide flange. Developments at other power levels and frequencies are planned.
I. L-3408 SWITCH TUBE: Provides switching at relatively low control voltage levels with an efficiency of 95 percent. Features high voltage holdoff, high current handling. Collector ratings: 150 Kv ; $20 \mathrm{Amps} ; 10 \mathrm{KW}$ dissipation.


For information on our tube line, exclusive of classified types, send for the 1961 Electron Tube Condensed Catalog. Write to: Marketing Dept., Electron Tube Division, 960 Industrial Road, San Carlos, California

## [8 <br> LITTON INDU8TRIE8 Eleotron Tube Division

CIRCLE 139 ON READER-SERVICE CARD

One of a series EXPLORING THERMISTOR APPLICATIONS


## makes a big difference in a

## time delay circuit

Circuits like the one above are often used where variable or fixed delay are required. Circuit ingredients: a thermistor and a variable resistor, in series with a battery and a relay.

With the switch closed, current flow is limited by the high resistance of the thermistor. The thermistor then heats up. permitting sufficient current flow to close the relay. Delay time can be increased or decreased by increasing or decreasing series resistance.

This is just one example of putting the thermistor to work. There are hundreds more - including temperature control, liquid level measurement, remote control, switching, power measurement, voltage control or you name it.

There are Just two kinds of thermistors, really: ordinary, which are good; and FENWAL ELECTRONICS', which are a little bit better. One reason is that FENWAL ELECTRONICS has the edge in experience. We pioneered in this field. Another reason is that we can suit your application exactly - FENWAL ELECTRONICS has the most complete line of thermistors available

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| ance, and new Thermistor |
| Catalog EMC 4, writo: |

## AUGAT <br> HEAT DISSIPATORS FOR <br> POWER TRANSISTORS



Augat's new Heat Dissipators utilize a minimum of space and still offer the large radiating surfaces needed for maximum transfer of heat. All Augat dissipators feature a parallel, open-fin construction assuring low thermal resistance. They are readily adaptable to forced air cooling for even lower resistance.

Augat Heat Dissipators are manufactured in three styles to accommodate the TO-3, TO-36 and 2N-1015 transistors or their equivalent.

Write for Bulletin No. HD-261 which describes this new line in full detail.

AUGAT BROS., INC.
31 Perry Avenue, Aitleboro, Mass. CIRCLE 141 ON READER-SERVICE CARD ELECTRONIC DESIGN • July 5, 1961


Broad-band ferrite coaxial isolator C992-100-409 operates from 2 to 4 Gc . Bandwidth isolation is 15 db . insertion loss 1 db , vswr less than 1.25:1. The 2-lb isolator is 6.16 in . long. Type N female coaxial connectors are standard, with other types optional
General Precision, Inc., Kearfott Div., Microwave Products, Dept. ED, 14844 Oxnard St., Van Nuys. Calif.

## Microwave Garnet

404
Low-loss, microwave garnet. MCL-300 is intended for use in the uhf and L-band regions. This material is available in bars, cylinder: and disk form. Typical applications include 3- or 4-port low-loss circulators, either in full waveguide or coaxial. Curie temperature is 125 C .
Microwave Chemicals Laboratory. Inc., Dept. ED, 282 Seventh Ave., New York 1, N.Y.

## Traveling-Wave Tube



A periodic-permanent, magnetfocused, low-noise traveling-wave tube, the HA-54 is for operation in the S-band. When operated from 2.4 to 3.4 Gc the tube has a noise figure of 13 db max, small signal gain of 25 db min and saturation power output of 5 dbm min . It measures 18 in . long with a 2 in . OD and weighs $3-1 / 2 \mathrm{lb}$.
Huggins Laboratories, Inc Dept. ED, 999 E. Arques Ave., Sunnyvale, Calif.
P\&A: $\$ 2,500$ ea; 8 to 10 weeks.
CIRCLE 142 ON READER-SERVICE CARD $\rightarrow$


ELECTROLYTIC CAPACITORS—Reliability is our first ingredient


## The "case" for 300-volt Tantalytic* capacitors

The best capacitor case for 300 -volt oper ation is General Electric's High Voltage Tantalytic* Capacitor. Its single-cell construction is the smallest and lightest for its rating. It weighs 0.1 ounce and measures only 0.875 inch in length.

Performance of this G.E unit distinguishes it as quickly as its size. -Rog. Trade-mart ol Genoral Electrie Co.

Capacitance stays within $10 \%$ of original value even after 2000 hours testing at rated voltage and temperature. Impedance is lower at -55 C than that of any other high-voltage tantalum capacitor.
These same features characterize the full line of ratings from 200 V (. 15 uf ) to 300 V ( 25 uf ). Polar or non-polar designs
are available from stock for 85 C and 125C applications.

Data on G.E High Voltage Tantalytic Capacitors is found in Bulletin GEA7065. Ask your G-E Sales Engineer for a copy today. Or write to General Electric Co., Schenectady, N. Y. Capacitor Department, Irmo, South Caroline.

## Progress /s Our Most Important Product GENERAL ELECTRIC

General Electric also offers these reliable Tantalytic capacitors



## Measures every Characteristic

 of Semiconductor Devices from 25 to 1500 Mc> TRANSISTORS - $h_{f b}, h_{f e}, h_{s b}, h_{i b}, h_{o b}, h_{s e}-$ all short-circuit admittance and open-circuit impedance parameters.
> TUNNEL DIODES - equivalent circuit parameters: series $\mathbf{L}$, series $\mathbf{R}$, shunt $\mathbf{C}_{\boldsymbol{*}}$ negative $\mathbf{R} .$. resistive cut-off frequency, self-resonant frequency.
> * measures vacuum-tube transadmittances
> as well, under high frequency, dynamic conditions
> . 7-pin miniature, grounded-cathode Tube Mount available (Type 1607-P201, \$75.)
> * TRANSISTOR TEST MOUNTS AVAILABLE:
> * Type 1607-P101
> (0.200-in.-pin-circle
> common base, 860. )
> Type 1607-P111
> (0.100-in.-pin-circle.
> common base, \$65.)
> - Type 1607-P102
> (0.200-in.-pin-circle. common emitter, 560 .)
> - Type 1607-P401
> (0.200-in.-pin-circle,
> tetrode, S65.)

This Instrument Takes In Stride Advances In Solid-State Devices -
it can measure all theoretical two-, three-, and four-terminal characteristics


## Monitoring Diode

RF power monitoring diode MA462 is for measurement applications in the X -band region. It is housed in a hermetically sealed, reversible polarity cartridge and is guaranteed for operation to 150 C . It meets the environmental conditions of MIL-S-19500B. A rectified output voltage with controlled variation is provided for input power levels between $10 \mu \mathrm{w}$ and 10 mw cw .

Microwave Associates, Inc., Dept. ED, Burlington, Mass.
Availability: Immediate

## Y-Circulator

For the 2-Gc region, this Y-Circulator is 2 in . in diameter. It can be magnetically tuned with electromagnets or permanent magnets which become an integral part of the package. Standard configuration is with TNC connectors at 120 deg spacing. A $6 \%$ bandwidth is obtained across a frequency range of 2 to 4 Gc . Insertion losses are less than 0.4 db with an isolation of $-20 \mathrm{db}\left(-30 \mathrm{db}\right.$ at $\left.f_{0}\right)$ and vswr of 1.3 ( 1.1 at $f_{0}$ ).

Hycon Manufacturing Co., Dept. ED, 700 Royal Oaks Drive, Monrovia, Calif.
Availability: Immediate.

## Coaxial Mixer Diode <br> 403

The MA-445 series of coaxial silicon mixer diodes are rated conservatively at 1 -erg burnout. Primary applications include use in single-ended or balanced hybrid mixers and communication and radar applications in the 10 - to 18 -Gc frequency range. Specifications for the MA-445 are: conversion loss, 7.5 db max; output noise ration, 2.5 max ; if impedance, 325 to 625 ohms.

Microwave Associates, Inc., Semiconductor Div., Dept. ED, Burlington, Mass. Availability: Immediate.

- CIRCLE 143 ON READER-SERVICE CARD

ANOTHER ADVANCED MICROWAVE TUBE DEVELOPMENT FROM RAYTHEON'S SPENCER LABORATORY

## Crystal Detectors

## Microwavis

For $K$ and $R$ band waveguide systems, models K422A and R422A have sensitivity of 0.05 v per mw and flat response within 2 db Maximum vswr is 2.5. Both models have feed-through terminations which may be removed when great er sensitivity is required. Model K 422 A is for 18 to 26.5 Gc and the R422A is for 26.5 to 40 Gc .
Hewlett Packard Co., Dept. ED, 1501 Page Mill Road. Palo Alto Calif.
P\&A: Single units are $\$ 200$ nintched pairs are $\$ 820$.

## C-Band Oscillator


i microminiature, C-band oscillator $3 / 4$-in. in diameter and $3 / 8$ in. long, model 9180 is for both plate pulse and cw service. The plate pulse service unit can be built in the 4 to 6 Gc spectrum with a tuning range of any 300 mc segment of that section. Peek pulse power is 50 to 100 w . The cw version can tune any 100 mc segment of the 4.0 tp 5.5 Gc spectrum. Power output is approximately 5 mw . Trak Microwave Corp.. Dept. F,D. Tampa, Fla.

## Pulse Modulator

360
The PM-87 pulse moderator is designed to test, for life and performance, super power klystrons, continuous-duty radar transmitters and similar equipment. Peak power is 64 megawatts continuous average power is 75 kw . Continu ously adjustable pulse range is 75 kv to 250 kv with pulse current of 260 amp at 250 kv . Frequency is 30 to 360 pps; pulse height deviates from flatness $\pm 2 \%$. Rise time at 10 to $90 \%$ voltage is $0.8 \mu$ sed ; decal time is $1.5 \mu \mathrm{sec}$ at the same voltag es.
Ling-Temco Electronics, Inc., Dept. ED, 1515 S. Manchester Ave., A naheim, Calif. Availability: so to 60 days.

## How new Raytheon "BEAM MISER" boosts efficiency in crossed field devices

Unique depressed collector greatly improves efficiency of "M" BWO's and crossed field amplifiers.
"Beam Miser" is Raytheon's newest advance in crossed field oscillator and amplifier design. With it are opened many new design possibilities for applications requiring voltage tunability or bandwidth plus high reliability and efficiency.

Incorporating the "Beam Miser" into, existing crosised field tubes will yield improved performance and will not require any mechanical or electricul changes in equipment.

Write for further information on Raytheon develupments in crossed field devices. Microwave \& Puwer Tube Division, Raytheon Company. Waltham 54, Massachusetts. In Canada: Waterloo, Ontario.

"BEAM MISER" consists of an additional electrode in the crossed field device which collects a portion of the spent beam at cathode potential and returns it to the cathode by means of an internal conductor.

RAYTHEON COMPANY

## FERRITE ISOLATORS by $D-B$

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a full range of sizes. 30-day deliveries


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CIRCIE 145 ON READER-SERVICE CARD


Communications System


Operates at $6 \mathbf{G c}$. The 50 series is a solidstate microwave package including rf, multiplex, telegraph carrier and alarm equipment. Modular construction and circuit cards are used throughout. Klystron provides 1 w output, is rated for $20,000 \mathrm{hr}$ of continuous operation. Up to 600 voice channels may be used, with 18 frequency-shift channels per voice circuit. Monitoring equipment can serve 22 stations with 8 points continuously scanned at each station.

Motorola Inc., Communications Div., Dept. ED, 4501 W. Augusta Blvd., Chicago 51, Ill.

## Mixer Diode

467
Noise figure is 7 db . Glass packaged diode type 1N831A, useful in strip-line circuits, can be conveniently mounted in coaxial circuits for broad-band, low-noise mixer applications. Operating from 1 mc to 4 Gc , burn-out rating is 250 mw cw . The device exhibits a noise figure of 7.0 db max for a $30-\mathrm{mc}$ if noise figure of 1.5 db at $3,060 \mathrm{Gc}$.

Microwave Associates, Inc., Dept. ED, Burlington, Mass,
P\&A: On request; stock.
Delay Line


For X-band. Waveguide line lengths of 13 to $1,228 \mathrm{ft}$ are contained in a mobile unit. The step-variable line is composed of coiled, rigid waveguide. Improved bending techniques result in minimum distortion of the waveguide and reduction of discontinuities. Length is changed quickly and accurately through use of highisolation waveguide switches.

Turbo Machine Co., Dept. ED, Lansdale, Pa.

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S. E. D. Memaries, Inc.

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WEbster 3-5958


## CIRCIE IAS ON READER-SEVVICE CARO

ELECTRONIC DESIGN - July 5, 1961


Model XD-6A rf detector consists of two separate detection circuits in a single package. Each section has an operating range of 100 kc to 1 Gc . Input impedance is 5) ohms for each section: vswr rating is 1.2 to $1 \mathbf{m a x}$ at $1 \mathbf{G c}$. U'nit comes complete with BNC connections on both inputs and both outbuts. TNC and N-type connector: are also available.
Telonic Industries. Inc., Dept. f:I). Beech Grove. Ind

## Shielded Grid Triode

402
Designed as a switch tube in hard-pulse modulations. the ML7845 delivers more than 4 megawatts pulse power output for radar. communications and similar applications. The cathode is unipotential and oxide-coated. When cooled by forced air the anode is capable of dissipating 3 kw with capable of dissipating 3 kw with
15! cfm air flow. When the tube is immersed in a suitable dielectric was such as sulfur hexafluoride, its maximum ratings are 75 kv de and 80 kv peak.

Machlett Laboratories. Inc.. Dept. ED, Springdale, Conin.
P\&A: \$2.415; so drys.

## Junction Circulator

Broad-band junction circulator model SL-43-3, operating at 2.2 to 2.7 Gc , is one of a line covering 1 to 35 Gc . The devices have better than 20 db isolation, less than 0.5 db insertion loss, and vswr less than $1.2: 1$ over a 15 to $20 \%$ frequency band. S, X, and SL band models with insertion loss of 0.15 db or less are available.
Cascade Research Div., Lewis and Kaufman Electronics Corp., Dept ED, 5245 San Fernando Road West, Los Angeles 39, Calif. Availability: 2 weeks.


Scientific-Allanta antenna pattern recording console at Boeing Airplane Company. Wichita, Kansas, with Scientific-Allanta model range tower in oachground-

## Advancing the Art of Aircraft Antennas

## Boeing uses versatile Scientific-Atlanta equipment to design and evaluate antennas for $B-52 H$ bombers

1A Boeing B-52H global bomber packs more total firepower than that expended by all the Allied and Axis bombers in World War II. Each B-52H will carry four Skybolt missiles plus a potent assortment of other weapons. Equipped with penetration aids. including electronic countermeasures (ECM) and decoys. the B-52H can strike as many as five military targets on a single mission. It is produced for the Air Force's Strategic Air Command at the Wichita. Kansas, Division of Boeing.
Obviously, the design of antennas for such an aircraft demanded nothing short of "state of the art." As it turned out. Boeing engineers advanced the state of the art in the design of ECM antennas for B-52Hs and B-47s. They were aided significantly by a new antenna test facility, consisting predominately of Scientific-Atlanta equipment-including pattern recorders, wide range receivers, signal sources, and a model range tower.
The foremost advantage of Scientific-Atlanta instrumentation is versatility. Complete frequency coverage is provided with recordings proportional to voltage. power, or db in

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betwer:n mounting hole
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## PROBING THE "TRANSPROBE" Wavegulde switch



The only moving parts of the "Transprobe" are solenoid plunger and a light weight, dielectrically supported metal probe. Result ... greater fexibility, longer life, ability to switch under full waveguide power. The design can be applied to any waveguide size. Unit shown is a single-pole-double-throw, X-band switch The design is equally successful for adaptation to SPDT, SP3T, transfer switch or special configurations. Typical specifications: Frequency. 8.2-12.4 KMC, VSWR ... 1.20, Insertion Loss ... 0.2 db , Crosstalk... 35 db , Life . . 2,000,000 operations. To probe more thoroughly the unusual advantages in this new approach to waveguide switching write Transco Products. Inc., 12210 Nebraska Avenue, Los Angeles 25, California.


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## world's shortest short-form catalog on BWOS

 rely gold-plated and designed for heat sink type mounting and operation. Frequency range covered is 215 to $2,325 \mathrm{mc}$. All units can be used as building blocks stacked side by side on 4 surfaces.Resdel Engineering Corp., Dept. ED, 330 S Fair Oaks Ave., Pasadena, Calif.
Availability: 20 days.

## Waveguide Fittings



Broached or unbroached waveguide fitting are manufactured to MIL-F-3922 from forgings castings or bar stock for microwave applications Magnesium and oxygen free copper flanges are available
Pem Machine Tool Co., Inc., Dept. ED, 1456 Chestnut Ave., Hillside, N. J
Availability: From stock.

## Variable Attenuator



For field equipment. Type $\mathbf{1 7 0}$ series of panelmounting attenuators is made for operation over full waveguide bandwidth, or with direct-reading dials for narrow-band use. Frequency range of type X170 is 8.5 to 10.5 Gc , with accuracy $\pm 2$ db from 0 to 50 db . Insertion loss is 0.75 db max, vswr 1.15:1 max. Average power handling capability is 1 w , peak lower 1 kw .
General Microwave Corp., Dept. ED, 47 Gazza Blvd., Farmingdale, N. Y.

You don't have to send for it This is it!

| TYPE \# | fREQ. RANGE kmc | POWER ต\| |
| :---: | :---: | :---: |
| 001.2 | 1-2 | 50-200 |
| 002.4 | 2.4 | 30-120 |
| 00 3.7-5.9 | 3.7-5.9 | 30-45 |
| 004.8 | 4.8 | 10.70 |
| 005.2 .8 .3 | 5.2-8.3 | 10.40 |
| 006 -11 | 7.11 | $10-40$ |
| 006 -12 | 6-12 | 10-30 |
| 007.13 | 8.2-12.4 | 10.15 |
| $0010-15$ | 10.15.5 | 10.20 |
| OD 12.18 | 12.4-18 | 10.25 |
| OD 15-22 | 15-22 | $10-20$ |

But don't give up if the tube you need isn't listed here these are just the BWOs we usually keep on the shelf in quantity, ready to ship today. We also produce, in either experimental or production quantities, oscillators covering partial, octave, and even greater-thanoctave bandwidths.
Would you like a copy of our honest-to-goodness catalog, with complete periormance curves, specifications, and operating data? Just drop us curves, on the Type $0015-22$ back. ward wave oscillator


## $\Longrightarrow \rightarrow$ -

We'd also like to hear from you if you're interested in permanent-magnet-focused tubes or traveling wave amplifiers.

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For bulletins and more information contact the nearest Sales Branch affice: Allanta-750 Ponce de Leon Place N.E.; Chicago-564 W. Adams Street; Kansas City (Mo.)-2017 Grand Avenue; Rochester-1040 University Avenue; San Francisco1805 Rollins Road.

CBNCDAL OYNAMICES /BLBCTMONICE

CIRCLE 153 ON READER-SERVICE CARD
ELECTRONIC DESIGN • July

## Micnowaves

## Hybrid Mixer

Compact hybrid mixer V-8306C performs without adjustment over 7.0 to 8.0 Gc . It is designed for waveguide coupling in both local oscillator and signal arms. Typical noise figure of 8.0 db includes a $3-\mathrm{db}$ image and 1.5 db if strip contribution. Maximum vswr in both signal and local oscillator arms is 2.0 . Isolation is 20 db min . Made of aluminum it weighs 6 oz .

Varian Associates, Dept. ED, 611 Hansen Way, Palo Alto, Calif.
Price: $\$ 495$ fob Palo Alto.

## Waveguide Isolator



X-band waveguide isolator C994-100-932 provides isolation greater than 70 db . Insertion loss is 1.0 db max, vswr 1.2:1 max. Center frequency is $\pm 100 \mathrm{mc}$, power handling capability 1 w avg. The $9-\mathrm{oz}$ isolator is 3 in . long.

General Precision, Inc., Kearfott Div., Microwave Products, Dept. ED, 14844 Oxnard St., Van Nuys, Calif.

Ceramic Seals


Coaxial ceramic seals for traveling-wave tubes consist of dense alumina insulator sealed to a monel inner conductor and surrounded by a nickel outer conductor. Metallization process results in good rf match characteristics.

Ceramics International Corp, Dept. ED. 39 Siding Place, Mahwah, N. J

## DIRECT READING

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Four seales with the following frll seale ceflections: 1 milliveth, 10 millimatts, 10 milliwatts, 1000 millimets.
Acearsey: $1 \%$-areapt in the 1 millimath range.
DC-10 KMC - Input Impedaace: 51.5 ohms

In this Calorimeter the R.F. power to be measured is compared to an accurately known D.C. power, by means of a null indicator and 260 thermocouples in 2 differential thermopiles, which sense the very low temperature rise of .0015 degrees $C$ per milliwatt of the circulating fluid. This fluid is flowing at the rate of $2 / 3$ of an ounce per minute.
Since R.F. power is compared to

MODEL CE-31

D.C. power, both of which will depend to an equal extent on the ambient temperature, the effect of the ambient temperature on this power measurement is cancelled out. The R.F. power is then read directly on a $1 / 4 \%$ D.C. milliameter, calibrated in milliwatts. The null indicator pointer is deflected $1 / 4$ " by a power difference of 100 microwatts.

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For detailed technical bulletins, call the American Bosch Arma marketing offices in Washington, Dayton or Los Angeles. Or write or call Tele-Dynamics Division, American Bosch Arma Corporation, 5000 Parkside Avenue, Philadelphia 31, Pa. Telephone TRinity 8-3000.

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Inquiries invited. Write to Rome Cable Division of Alcoa, Dept. 11-71, Rome. N. Y.


## NEW LITERATURE

## Planar Semiconductors

261
Reliability, performance, cost and adaptability of planar diodes and transistors are discussed in this 12-page color brochure. Technical data, including performance curves and electrical specifications, are included. Planar transistors, manufactured with a protective oxide coating, are compared with their mesa equivalents. Fairchild Semiconductor Corp., 545 Whisman Road, Mountain View, Calif.

## RF Interference Filters

262
Radio-frequency interference filters designed to reduce conducted interference in shielded-enclosure test activities and groundsupport equipment applications are described in this eight-page publication. Entitled "Shielded Room and Ground Support Equipment Filters", the booklet covers the firm's complete line. Genistron, Inc., Sales Dept., 6320 W. Arizona Circle. Los Angeles 4ì, Calif.

## Environmental Data

263
Common conversion factors, formulas, and data on vibration, shock, pressure and other dynamic phenomena are given in this pocket folder. It is intended primarily for the environmental engineer. The folder has 27 sections, each devoted to a particular topic from the basic trigonometric formulas to a graph of piezuelectric transducer response. Endevco Corp., 161 E. California Blvd., Pasadena, Calif.

## Electroplating

264
A method of electroplating without requiring immersion tanks is described in this eight-page brochure. Localized areas, it is said, can be plated, with little masking required. Sifco Metachemical, Inc., 935 E. 63rd St., Cleveland 3, Ohio.

## Plugs, Connectors and Switches 265

Banana plugs, phone jacks, alligator clips, test leads, cable connectors, toggle switches and miscellaneous related items are described and illustrated in this 32-page catalog. Physical and electrical specifications and prices are included. GC Electronics Co.. Rockford, III.

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## NEW LITERATURE

## Measuring Instruments

In 96 pages, Catalog $S$ describes over 250 instruments, counting systems, radionucleides and nuclear accessories. Much of the catalog is devoted to new products. Illustrations and technical data are included for each device. Nuclear-Chicago Corp., 359 E. Howard Ave., Des Plaines, Ill.

## Toroidal Cores

Basic design information tips and formulas for toroidal cores are given in this 14page handbook. Included are temperature curves, analysis of core loss, dc resistance, eddy current loss resistance, hysteresis loss resistance and self-capacitance. Request on company letterhead from Connolly and Co.. Dept. ED, P. O. Box 295, Menlo Park, Calif.

## Silicon Diodes

267
Eighty-six glass silicon diodes are cataloged in this four-page brochure, as well as 35 general purpose and 51 computer types. Technical specifications are given. Computer Diode Corp., 250 Garibaldi Ave., Lodi, N. J.

## Long-Life Vacuum Tubes

268
Specifications, descriptions and dimensional drawings for the firm's vacuum tubes are given in this 26-page handbook. Manufacturing techniques and quality control procedures are also described. State Labs, Inc. 215 Park Ave. S., New York 3, N. Y.

## Low-Pressure and Flow Switches <br> 269

Complete specifications, details and prices on low-pressure switches and velocity-actuated flow switches are described in this 30 page catalog. Design information and dimensional diagrams are included. The Henry G. Dietz Co., Inc., 12-16 Astoria Blvd., Long Island City 2, N. Y.

## Flashtubes for LASERS

270
Flashtubes capable of driving LASERS are described in this four-page booklet. Information on operation and application is included. Data on power requirements and capabilities of three assemblies are given. General Electric Co., Dept. LP-15, Nela Park, Cleveland 12, Ohio.

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## DC Power Supplies

The firm's model CVQ transistorized power supply is described in this eight-page brochure. Theory of operation of the $100-\mathrm{w}$, regulated supply is discussed. Specifications are included. Sola Electric Co., Busse Road at Lunt, Elk Grove Village, IIl.

## Clutches and Brakes

Electromagnetic clutches and brakes, mechanical clutches, torque indicators, torque standards and multi-speed transmissions are described in 40-page manual No. 361. Engineering and applications information is included. Autotronics, Inc., Dept. 30, Florissant, Mo.

## Photoelectric Systems

273
Applications of photoelectric systems in automation are described in this 20-page bulletin, No. 611. Light sources, photo units, electronic controls and timers are discussed. with electrical and physical specifications included. Photomation, Inc., 96 S. Washington Ave., Bergenfield, N. J.

## Temperature-Measuring Paints

 274Paints and crayons which can be used to measure surface temperatures are described in this folder. Pigments change color at specified temperatures, indicating whether surface is hotter or colder than desired Princeton Div., Curtis-Wright Corp., Princeton, N. J.

## Semiconductor Technical Bulletins 275

A series of technical bulletins on semiconductors are available. No. 60S17-1, "Index of Technical Bulletins", lists technical data sheets on the firms semiconductor products. No. ICE-235, "RCA 2N404 Family", gives data on six transistors. No. ST-1945, "Reliability of the RCA-USAF-2N404 at High Stress Levels", presents test data on the 2 N 404 transistor. No. ICE-229, RCA Silicon Rectifier Interchangeability Guide", lists available silicon rectifiers. No. ICE-228, "Application Guide-RCA VHF Silicon Transistors", includes information on transistor design, construction and circuitry. No. ST2106, "Micromodule Reliability Status Report", presents reliability information on the firm's micromodules. Radio Corp. of America, Semiconductor and Materials Div., Somerville, N. J.

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## IDEAS FOR DESIGN

## Vote for Ideas Valuable to You

Vote for the Ideas which are valuable to you. Other engineers will vote for the Ideas which are most valuable to them. The Idea which receives the most "Valuable" votes will be judged "Most Valuable of Issue." Its author will receive a $\$ 50$ award.
Choose the Ideas which suggest a solution to a problem of your own or stimulate your thinking or which you think are clever.

The Ideas chosen as the most valuable in each issue will be eligible for the $\$ 1,000$ Idea of the Year award.
So vote for the Ideas you find most valuable. And, after you've voted, why not send in an Idea of your own?

## Simple Circuit Halves <br> 20-Mc Supply Frequency

A simple circuit was required to supply a $10-\mathrm{mc}$ signal from a $20-\mathrm{mc}$ source. The circuit shown fulfilled the requirement quite adequately.
Transformer $T_{1}$ is resonant at the $20-\mathrm{mc}$ input frequency. Transformer $T_{2}$ is resonant at 10 mc , with a portion of the $10-\mathrm{mc}$ energy coupled back into the transistor. The loop gain is low enough to keep the circuit from oscillating with the drive removed.


Frequency divider has two resonant circuits-the input circuit at 20 mc , the output at 10 mc .

Herbert F. Verse, Jr., Research Engineer. Jet Propulsion Laboratory, Pasadena, Calif.

If this Idea is valuable to you, give it a vote by circling Reader-Service number 734.

## Power Gain Plot Can Be

When plotting the large current gain of power transistors the plot can be made rather quickly by eliminating the division step.

Current gain is given by $\boldsymbol{H}_{F B}=\boldsymbol{I}_{c} / \mathrm{b}$. The graph paper is used as shown in the figure, with base current values laid out beforehand on the graph. The intersection of the measured base current line and the collector current abscissa yields a correct point on the $H_{r \varepsilon}$ vs $I_{\text {, curve. }}$


Current gain $H_{F B}$ is plotted directly from $I_{b}$ and $I$. measurements by laying out base current "guidelines beforehand.

John T. Lamb, Research Enyineer, Th, Tappan Co., Mansfield, Ohio.

If this Idea is valuable to you, give it a vote by circling Reader-Service number 733.

## Fourth $\$ 50$

"Most Valuable of Issue" Award For Curve-Tracing Attachment
Chester B. Shapero, self-employed research engineer of Cupertino, Calif., has won Electronic Design's fourth \$50 Most Valuable of Issue Award.
Mr. Shapero receives the award for his Idea for Design, "Low-Cost Scope Traces Transistor Characteristic Curves," which appeared in the April 12 issue. The idea described a circuit which enabled a lowcost oscilloscope to be used for displaying transistor characteristic curves.

## IDEAS-FOR-DESIGN

## How You Can Participate

## Rules For Awards

Here's how you can participate in Ideas for Designs Seventh Anniversary Awards:
All engineer readers of Electronic DeSIGN are eligible.
Entries must be accompanied by filled-out Official Entry Blank or facsimile. Ideas submitted must be original with the author, and must not have been previously published (publication in internal company magazines and literature excepted).

Ideas suitable for publication should deal with:

1. new cirevits or circuir modifications
2. new design techniques
3. designs for new production methods
4. clever use of new materials or new components in design
5. design or drafting aids
6. new methods of packaging
7. design short cuts
8. cost saving tips

Awards:

1. Each Idea published will receive an honorarium of $\$ 20$
2 The Idea selected as the most valuable in the issue in which it appears will receive $\$ 50$.
2. The Idea selected as the Idea of the Year will receive a Grand Prize of $\$ 1,000$ in cash.
The Idea of the Year will be selected from those entries chosen Most Valuable of the Issue.

Most Valuable of the Issue and Idea of the Year selections will be made by the readers of Electronic Design. The readers will select the outstanding Ideas by circling keyed numbers on the Reader-Service cards. Payment will be made eight weeks after Ideas are published.
Exclusive publishing rights for all Ideas will remain with the Hayden Publishing Co.

Ideas-for-Design Editor
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8.50 Third Ave.

New York 22, N. Y.
Idea (State the problem and then give your solution. Include sketches or photos that will help get the idea across.)

> (Use separate sheet if necessary)

I submit my Idea for Design for publication in Electronic Desigs. I understand it will be eligible for the Seventh Anniversary Awards- $\$ 20$ if published, $\$ 50$ if chosen Most Valuable of Issue, $\$ 1,000$ if chosen Idea of the Year.

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## IDEAS FOR DESIGN

Long Period Multivibrator 748

## Reduces Timing Capacitor Size

Building a transistorized monostable multivibrator for pulse widths of 10 msec or more can be a problem if space is at a premium. The problem arises because the finite $\beta$ of $Q_{1}$ (circuit a in the figure) places an upper limit on resistor $R$. This, in turn, means that $C$ must be large, both electrically and physically, to yield the large $R C$ product required for long pulse widths.

The maximum permissible value of $R$ is given approximately by:

$$
R=\frac{V_{1}-1.3}{V_{1} / R_{t} \cdot \frac{1}{\beta}}
$$

The quantity 1.3 accounts for the drop across $C R_{1}$ and the base-to-emitter junction of $Q_{1}$ when the transistor is on. $V_{1} R_{1}$ is the collector current of $Q_{1}$ when $Q_{1}$ is on. Not considered is the effect of the collector-toemitter drop of $Q_{1}$ when it is on, and the bleeder current required to hold $Q_{2}$ off.

As an example, consider the typical values below:

$$
\begin{aligned}
V_{1} & =30 \mathbf{v} \\
R_{b} & =3.3 \mathrm{~K} \\
\beta & =40
\end{aligned}
$$

Then,

$$
R=\frac{30-1.3}{\frac{30}{3.3} \cdot \frac{1}{40}}=126.3 \mathrm{~K}
$$

If a pulse width of 20 msec is required, the time constant is derived from:

$$
t \approx 0.68 R C
$$

Choosing a standard value for $R$ of 120 K , we have

$$
C=\frac{20 \times 10^{-3}}{0.68 \times 120 \times 10^{2}}=0.245 \mu \mathrm{f}
$$


(a)
(a) Maximum value of $R$ in this monostable multivibrator is limited by the value of $\beta$ for transistor $Q_{1}$. Thus, for long pulse widths, capacitor $C$ must be large.

(b)
(b) Replacing $Q_{1}$ with two-transistor Darlington connection effectively squares the value of $\beta$. This allows a iarger $R$, and reduces both the value and size of $C$.

Compared to the other components in the circuit, this capacitor is physically very large. This is especially true if the capacitor must be both accurate and stable.

However, the size of the capacitor can be considerably reduced if transistor $Q_{1}$ is replaced by the two-transistor Darlington connection. The over-all $\beta$ is now $40 \times 40=$ 1.600 , and $R$ can be 40 times larger than before. Hence, $C$ can be 40 times smaller. Using a practical value of $R=1 \mathrm{meg}$, we have

$$
C=\frac{20 \times 10^{-1}}{0.68 \times 1 \times 10^{i}}=0.0294 \mu \mathrm{f}
$$

Obviously, a much smaller capacitor will be required.
W. E. Zrubek. Design Engineer. Westinghouse Electric Corp., Baltimore, Md.
If this Idea is valuable to you, give it a vote by circling Reader-Service number 748.

One-Shot Pulse Output Has 746 Greater Than 100\% Duty Cycle

Greater than 100 per cent duty cycle pulse generators can be designed by connecting two one-shot multivibrators in series.

Such a generator was needed to produce display pulses variable from microseconds to seconds. The pulses were to be triggered by a four-decade, preset counter when the counter reached a preselected number. The maximum frequency of the display was 100 kc .
At the end of the display pulse time, the counters were to be reset, ready to be triggered again, within $10 \mu \mathrm{sec}$. Thus, if the preset selector is set to a low number such as 0002 , and if the counter receives pulses at a 100 -kc rate, coincidence is again reached 20 to $30 \mu \mathrm{sec}$ after the counter is reset to zero
Thus, if the output display pulse time is 1 sec, the pulse generator has to operate with


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## IDEAS FOR DESIGN

a duty cycle of 99.998 per cent or better. That is, it must be retriggered within $20 \mu \mathrm{sec}$ after the elapse of the 1 -sec pulse.

A single one-shot multi was ruled out because of duty cycle limitations. However, the problem was simply solved by connecting two ordinary one-shots in series.

The first multi triggered the second, with the output of the second multi initiating the zero set of the counters. The display pulse time was the sum of the periods of the two multivibrators.

By the time the period of the second multi is over, the first multi is ready to accept a trigger. The duty cycle of this combination is better than 100 per cent.

Arpad Somlyody, Circuit Design Analyst. Burroughs Corp., Electronic Components Div., Plainfield. N. J.


Pulse output with greater than 100 per cent duty cycle can be obtained by connecting two one-shot multivibrators in series.
If this Idea is valuable to you, give it a vote by circling Reader-Service number 746.

## Servo Circuit Compared <br> Antenna Pattern Nulls, Peaks

 735In developing an automatic antenna pattern computer н simple and reliable method was required to compare the pattern nulls with the lobe peaks. In addition, not only was the greatest magnitude lobe peak to be selected, but also the "deepest" null.

The maximum lobe peak is easily measured and selected for greatest amplitude with a simple voltage memory device, such as a capacitor. Locating the "deepest" null, how-


Automatic readout supplies lobe peak to null depth ratios of antenna pattern.
ever, presents circuitry problems which can set complex.

This problem was solved by using a simple servo bridge balancing circuit with a high back-resistance silicon diode. The servo used with this diode is able to proceed in the direction of the greatest ratio of lobe peak to null depth. When the diode is properly oriented, the servo direction cannot be reversed. To regain the original $1: 1$ ratio, it is only necessary to short out the diode momentarily. The servo then swings back to its unity ratio.

Eduin S. Osner. Sr. Enginepr, Varian Associates, Radiation Div., Palo Alto, Calif.
If this Idea is valuable to you, give it a vote by circling Reader-Service number 735.

## Tunnel Diode Trigger <br> Circuit Can Reset Itself

The tunnel diode trigger circuit, Fig. 1, resets itself without the need for a clipping line or additional reset pulses. A trigger applied as shown switches the tunnel diode from the low state (state 1) to the high state (state 2). The diode now presents a higher impedance than in the original state, and its current decreases to $I_{2}$, Fig. 2. The original current through the tunnel diode is

$$
\boldsymbol{I}_{1}=\frac{\mathbf{V}_{1}-\boldsymbol{V}_{1}}{\boldsymbol{R}^{\prime}+\boldsymbol{R}}
$$

If capacitor $C$ were sufficient to maintain the voltage across $R^{\prime}$, the current through the tunnel diode immediately after switching to state ? would be

$$
I_{7}=\frac{\boldsymbol{V}^{\circ}-V_{x}-V_{K}^{\prime}}{R}
$$

Since the voltage across capacitor $C$ changes with the time constant of $C, R$, and $R^{\prime}$ in parallel, the current through the tunnel diode will decrease toward


Fig. 1. Presence of voltage holding capacitor C allows tunnel diode trigger circuit to reset itself.

## .tough going ahead!

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## IDEAS FOR DESIGN



Fig. 2. After being switched to stote 2 by trigger pulse, capacitor $C$ causes current to decrease to $I$, and the diode switches back to its original state.

Thus the voltage across the tunnel diode will decrease exponentially, moving from point 2 to point 3.

When the current through the tunnel diode reaches $I_{1}$ (the valley current), the diode will switch back to its original state.
The conditions for the tunnel diode to reset to state 1 are:

$$
I^{\prime}<I_{+} \text {where } I^{\prime}=\frac{V_{*}-V_{2}}{R^{\prime}+R}
$$

Since $V$, and $K$ are chosen by normal circuit considerations, and $I_{v}$ and $V_{z}$ are obtained from the tunnel diode specifications, the value of $R^{\prime}$ is determined as:

$$
R^{\prime}=\frac{V_{t}-V_{2}-I_{t} R}{I_{v}}
$$

The "on-time" of the tunnel diode is determined by the time constant $T$ where:

$$
T=\frac{R^{\prime} R C}{R^{\prime}+R}
$$

Since the values of $R^{\prime}$ and $R$ are determined by the previous considerations, the on-time of the trigger circuit is fixed by the choice of the value of $C$.

Robert N. Larsen, Assist. Electrical Enyineer, Argonne National Laboratory, Argonne, Ill.
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High frequency sine-to-square converter is made up of transistorized emitter-coupled lihiteds.
the rise time of the square wave then depends on the magnitude of the input sine wave. Thus, the ratio of the peak-to-peak values of the input to the output should be at least 3 .

However, an emitter-coupled limiter not only needs a much smaller input voltage, but its rise-time is limited only by the switching times of the transistors. These can be reduced by driving the switching transistors out of a common collector stage.
The circuit shown produces, once the potentiometer is adjusted, a fast rise time, symmetrical square wave. A 5 -mc sine wave with 2 v peak-to-peak at the input gives a $2 \cdot \mathrm{v}$ peak-to-peak square wave with a rise time of approximately 20 nsec . For an input voltage of 6 v peak-to-peak, the rise time reduces to less than 10 nsec with a slight overshont.

Harald Hahn. Assist. Electrical Engineer. Brookhaven National Laboratory, Upton. L.I., N.Y.

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## REPORT BRIEFS

## Tem Diode Switching

The theory and technique for the design of a broadband ( $100-$ to- 1 frequency range) TEM microwave diode switch are presented. A coaxial transmission line switch has been constructed that provides 26 db or greater isolation and insertion loss ranging from 1.6 db to less than 1 db from 40 mc to $\mathbf{4 0 0 0}$ mc. An analysis is given of the switching action of one and of two or more diodes. Also discussed is the biasing of the center conductor of a TEM transmission line over broad frequency bandwidths so as not to interact with the rf signal. Theory of TEM Diode Switching, Robert V. Garver, Diamond Ordnance Fuze Laboratories, Washington, D. C., Oct., 1960, 56 pp , Microflm \$3.60, Photocopy 89.30. Order PB 153579 from Library of Congress, Washington 25, D. C.

## RFI-Duplexer Tubes

An investigation was conducted on several types of TR duplexer tubes and a waveguide filter commonly used in systems, to determine their effectiveness in rejecting spurious microwave radiation. The devices studied were all designed for operation in the $2.8-\mathrm{Gc}$ frequency band. The low power level characteristics of these devices were checked over a frequency range of 2.6 to 35 Gc . Results of the investigation showed that neither the TR tube nor the waveguide filter can provide adequate protection against unwanted signals at frequencies higher than the system frequency. Characteristics of Microwave Duplexer Tubes Under Spurious Radiation Conditions, Irving Reingold, Army Signal Research and Development Labs., Fort Monmouth, N. J., March 31, 1959, 27 pp, Microfilm \$2.70, Photocopy \$4.80. Order PB 147821 from Library of Congress, Washington 25, D. C.

## Waveguide Components

Presents the design and development of components for use in a circular waveguide system employing the low-loss $\mathrm{TE}_{01}$ circular electric wave mode. Components were investigated with regard to direct scaling for use with $2.710-\mathrm{in}$. ID and $0.725-\mathrm{in}$. ID circular waveguide at 9.375 Gc and 35 Gc , respectively.

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## Printed Antennas

Discusses several types of printed antenna arrays and related feeds and baluns. Detailed consideration is given to the Franklin array, Chireix-Mesny array, and the capacitively coupled collinear array. Experimental techniques, such as probing the magnitude and phase distribution of the current along a printed array and measuring the impedance and phase velocity that characterize printed balanced lines are described. The antenna performance characteristics for the types of arrays that were studied are given including gain, loss, impedance, size, side-lobe levels, and half-power beamwidths. Study of Printed Antennas, J. A. McDonough, R. G. Malech. J. Kowalshy, Airborne Instruments Lab., Inc., Mineola. N. Y., Aug., 1955. 57 pp , Microfilm \$3.60, Photocopy \$9.30. Order PR 150667 from Library of Congress, Washin!gton 25, D. C.

## Transistors

A hybrid parameter equivalent circuit for the common emitter connection is developed. The basic circuit is modified for high-frequency use in such a way that the parameters of the equivalent circuit are independent of frequencies. Methods of measuring these various parameters are discussed in detail and circuit diagrams are provided for each such measurement. The proposed transistor equivalent circuit is then used in the analytical development of circuit design equations and criteria for low-pass, highpass, and band-pass amplifiers. Transistor Equivalent Circuit Criteria, Thomas L. Martin Jr., David J. Sakrison, et al. Arizonn University, Tucson, Ariz., Aug. 30, 1.956, 83 pp. Microfilm \$4.80, Photocopy \$1.3.80. Order $\boldsymbol{P} \boldsymbol{E} 147539$ from Library of Congرress, Washington 25, D. C.

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## REPORT BRIEFS

## Radiation Damage in Semiconductors

A diode resistant to nuclear radiation damage was constructed as a result of extensive studies of nuclear irradiation effects on semiconducting materials. The diode uses p-type germanium with resistivity of about $0.20 \mathrm{ohm}-\mathrm{cm}$ as the base material. Principal object of the study was to determine the mechanisms by which radiation degrades semiconductor devices. The researchers state that one of the most significant accomplishments of the program was the development of the instrumentation and techniques of measurement used with the General Atomic electron linear accelerator. Resrarch in Radiation Damage in Semiconductors, J. W. Harrity and nthers, General Dynamies Corp. for U. S. Air Force. Feb. 1960, 157 pp, $\$ 3.00$. Order PB 16167.3 from OTS, Washington 25, D. C.

## Ground Support Functions

This study was conducted to determine the relations between automation and personnel requirements for guided missile ground support functions. Three systemsSnark, Bomarc, Mace-were investigated in regard to organization-level maintenance of electronic equipment. The study shows that automatic equipment, itself, is not the cause of increased personnel requirements, but rather the use to which automation is put within the over-all support organization. Automation and Personnel Requirements for (inided Missile Ground Support Functions, General Electric Co. for Wright Air Development Center, May 1959, pp 49, \$1.25. Order PB 151978 from U. S. Department of Commerce Field Office, 10.31 S. Broadway, Los Angeles 15. Calif.

## Ceramic Tubes

This Air Force "phasing-in" study reports on the results of a survey to facilitate the prompt use of newly developed high-temperature ceramic tubes and components in aviation electronic equipment. Many of the supporting components investigated were still in the research and development stages. Various materials and construction methods were tested in a search for simple, efficient, and economical means of installation and servicing. Adaptation of Ceramic Tube Types.

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Aerovox Corp. for Wright Air Development Center, June 1959, 166 pp, \$3.00. Order PB 151922 from U.S. Department of Commerce Field Office, 1031 S. Broadway, Los An!seles 15, Calif.

## Sampled-Data Systems

Theory of the operational analysis of the finite, pulse-width system is developed. The closed-form expression of the response of such a system is described by several wellknown operators such as the z-transform, the modified $z$-transform and the simple form of the p-transform. Finding the incremental responses and their superposition is the basic principle of the theory. It is applied to two-sampler systems as well as multirate sampling systems. Operational Analysis of Finite Pulsed Sampled-Data Systems, T. Nishimura, Electronics Research Laboratory, University of California, Berkeley, Calif., May 1960, 39 pp, Microfilm \$3.00, Photocopy \$6.30. Order PB 149092 from Library of Congress, Washington 25, D. C.

## Reliability

A specific mathematical model is formulated for improving system reliability with a minimum of effort. Also shown is how to determine the allocation of effort among subsystems which yields the desired system reliability at minimum total expenditure of effort. Increased Reliability With Minimum Effort, Arthur Albert, Frank Proschan, Applied Mathematics and Statistics Labs., Stanford University, Calif., Oct. 9, 1959, 29 pp, Microfilm \$2.70. Photocopy \$4.80. Order PB 14994.3 from Library of Congress. Washington 2:5, D. C.

## Speech Statistics

At a symposium co-sponsored by the Leningrad State University and the Speech Section of the Commission on Acoustics, USSR Academy of Sciences, papers were presented by Soviet scientists on the investigation of speech, linguistics, telephonic acoustics, physiology, mathematics, and related subjects. Fourteen of these research reports on statistical methods have been translated and compiled in this publication. Problems of Speech Statistics, translated from 12 Russianlanguage publication of the Leningrad State University, 1958, $137 \mathrm{pp}, \$ 2.75$. Order 6111792 from OTS, Washington 25, D. C.

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The do-it-yourself tests put out by the General Electric Company's Light Military Electronics Department, Utica, N. Y., have proved surprisingly successful. LMED says 8,695 "self-tests" have been sent out in answer to requests.

These tests were originated by LMED as a recruiting "gimmick." They have been publicized in LMED's employment ads during the past year. The result, according to GE recruiter Ron Bach is that about 10 times as many names have come into LMED as might otherwise have been expected. The number and quality of the "hires" resulting from this greater number of "contacts" has been encouraging, Mr. Bach said.

The self-tests are made up of multiplechoice questions and each test averages about six pages in length. They cover the technical specialties of interest to LMED, ranging from electronic packaging to radar and digital computer design. Sample questions from two of the most recent of these tests, the one on digital computers and the sole nontechnical test of the series, are included here to show the nature of the questions. Using the answers given at the back of each test, an engineer can score himself and then, by comparing his score with the norms developed by LMED through testing its own engineers, he can see how he "stacks up" with engineers presently at LMED.

## GE Doesn't Use Test

## Results in Its Own Recruiting

GE recruiters themselves do not pay any particular attention to what a man says his score was on one of these self-tests. GE does hope of course that the tests create the right "image" of attitudes and opportunities at LMED and that the tests serve to help applicants voluntarily pre-screen themselves. But the recruiters at LMED still believe that their personal interviews "in depth" are best for determining which men to make offers to.

Mr. Bach says he has found one particular line of questioning the most productive in separating out the better engineers. He first asks the engineer he is interviewing to describe the engineering organizations he has been with. Then, most important, he asks the man to describe in detail his functional relationship with those organizations. What were his individual responsibilities? A man

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IBM scientists have developed a process of falbricating cryogenic memory planes in a single, automatic cycle. Aithough still experimental, such work could result in larger, more reliable cryogenic computer memories.
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The IBMI engineering group that developed this new method of automatically fabricating experimental memory planes found it had to move back and forth across
technical boundaries to achieve its results. Circuit design engineers, for example. worked closely with physicists and mathematicians to develop special circuits that would operate within the limits imposed by film characteristics and control techniques. This integrated approach to systems development has helped make possible many of the adrances that IBM has made recently in such fields as semiconductors, microwaves, optics and magnetics. If imaginative problem-solving in any of these areas interests you-and you have a degree and experience in engincering. mathematics, or one of the sciences - wed like to hear from you.

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:vhe can't describe his responsibilities on past engineering jobs (and a great many can not, apparently) would probably not receive an offer through Mr. Bach.

## Nontechnical Test Has

## Uncovered Good Administrators

An example of the self-screening potential of these tests has been the number of good men for nonengineering, administrative posts within LMED which the one nontechnical test in the group has helped uncover, Mr. Bach said. Nonengineers also read the ads for engineers, he said, and when they see that a nontechnical test is also available, they are encouraged to write to what they would have otherwise considered a hopelessly technical organization like LMED to inquire about the test and employment. Some of these nonengineering applicants have been employed in businesses as far removed from engineering as advertising agencies.

## What Do the

## Tests Mean?

Since most of the tests are technical, engineers will have little trouble in understanding the right or wrongness of the answers. They may however question the relative meaning of their scores as compared to the norms given for the GE engineers. For example, one Electronic Design editor who did not think himself a match for a LMED computer designer was surprised to find that he self-scored in the second to highest (there were five) group which according to GE indicated he "shows probability of excellent performance in intermediate to high-level computer research, design and development." It was this editor's conclusion that multiplechoice questions favor the widely read person but possibly disfavor the working designer who must concentrate in a certain area.
Nevertheless the tests make for a pleasant evening's exercise and with intelligent selfinterpretation can be a quasi-quantitative indication of one's strengths and weaknesses.

## Management Aptitude <br> \section*{Test More Subtle}

At first sight the answers to the questions in the "Human Relations Quiz" look obvious. "This is what any company would expect you to say." Obviously a manager-type should "want to play cards with a neighbor and his
wife" rather than "build some new furniture in the workshop" (question 5). Obviously he should "tend to identify more with his company than with a profession" (question 29)

Less obvious is question 27 which says that a good manager should not want his subordinates to run to him whenever they had a question but to work out their problems for themselves. Also less obvious is question 12 which says that a good manager ought to be able to readily allay other people's suspicions.

The weighing values given for the answers to the questions help to understand the logic )ehind the test (actually as GE explains, the tests were developed by the empirical procedure of relating responses of GE managers and individual worker types. A top weight of six points is given the answer to question 38 which indicates that a good manager type should not respect people who seem uncertain about things. But only two points are given for the answer to question 23 which indicates that a good manager thinks that people should try to behave ethically even when it means personal sacrifice.

## Interested Engineers

## Should Obtain Complete Tests

These sample questions and answers will give some idea of the tests. However, engineers who are seriously interested should obtain the complete tests by writing: Technical Recruiting, Light Military Electronics Dept. French Road, Utica, N. Y.

## Sample Questions From GE Self-Test

## Logic Circuits and Digital Computers

1. In a junction transistor the base-to-collector current amplification factor is in the range of:
a. $10^{-3}$ to $10^{-8}$
b. 0.9 to 1.0
c. 20 to 100
d. 700 to 900
2. In the Venn diagram below, areas correspond to Boolean functions of the variables A, B, and C. How many of these represent MINTERMS?

b. 2
c. 3
d. 7
e. 8
3. With reference to the schematic circuit diagram below (if $\mathbf{A}=$ positive voltage and $\overline{\mathbf{A}}=$ no voltage) the Boolean func-


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Your equations together with Newton's Laws serve as a basis for explaining classical electromagnetic phenomena. Most important among the outgrowths of your theory are radio and its allied invention, radar. At AC, we are using techniques for the generation and propagation of electromagnetic waves to increase the total capabilities of the B-52 weapons system.
If you are interested in applying yesterday's theories, like Maxwell's, to today's Mach 2 and 3 aircraft, and if you have a BS, MS or PhD in EE, ME, Physics or Math, please contact Mr. G. F. Raasch, Director of Scientific and Professional Employment, Dept. G, 7929 South Howell, Milwaukee 1, Wisconsin.

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tion $f$ is:
a. $A B+C D$
b. $(A+B) C D$
c. $(A B+C) D$
d. $(A+B)(C+D)$

ค. $A B C D$
9. The monostable multivibrator below

a. Is used in counters.
b. Generates a gating pulse.
c. Is free running.
d. Will not work as drawn.
89. Circuits employing NOR logic
a. Are found in superspeed computers.
b. Were first used in the NORC computer.
c. Are based upon negative resistances.
d. Contain blocks which expcute the negative $-O R$ operation.
e. Contain transistors and resisturs.

## Professional Inventory on Human Relations

1. If you had to choose an occupation other than the one you now have, which would you rather be:
a. Physician
b. Explorer
2. How would you rather spend an evening:
a. Building some new furniture in the workshop
b. Playing cards with a neighbor and his wife
3. Which would you least like to do:
a. Add several columns of figures
b. Be interviewed for a new job
4. You are usually able to "put yourself in someone else's shoes" in order to understand his point of view:
a. True
b. Not true
5. Are you a keen judge of other people's motives:
a. Yes
b. $N o$
6. Opportunity to contribute to basic scien-

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tific knowledge is highly important to me:
a. Agree
b. Disagree
12. Can you readily allay other people's suspicions:
a. Yes
b. No
14. It's more important that a man we hire can do his work well than that he makes friends rapidly among his work associates:
a. Agree
b. Disagree
23. People should try to behave ethically, even when it means some personal sacrifice:
a. Agree
b. Disayree
24. When internal tensions occur, do you give full attention to their resolution:
a. Yes
b. No
27. I would rather that a man who works under my supervision:
a. Consults me whenever he had a doubt
b. Tries to work out problems for himself
29. I tend to identify more with my profession and work than with any one company:
a. True
b. Not true
38. Do people who seem unsure and uncertain about things lose your respect:
a. Yes
b. No

Ansucers to Sample Questions
Computer Quiz:

1. $c$
2. 
3. $b$
4. b
5. $d$

Human Relations Quiz:
Weighing Factor

| 1. $a$ | 4 |
| :---: | :---: |
| 5. $b$ | 6 |
| 7. $a$ | 4 |
| 9. $a$ | 2 |
| 10. $a$ | 4 |
| 11. $b$ | 6 |
| 12. $a$ | 4 |
| 14. $a$ | 4 |
| 23. $a$ | 2 |
| 24. $b$ | 4 |
| 27. $b$ | 4 |
| 29. $b$ | 4 |
| 38. $a$ | 6 |



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| 10 mm min. into 50 ohm load | 1 watt min. into 50 ohm lood | 20 mw min. into 50 ohm lood | 20 mw min. into 50 ohm lood |
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