# 75A-4 <br> AMATEUR-BAND RECEIVER INSTRUCTION BOOK 

COLLINS RADIO COMPANY<br>Cedar Rapids, Iowa

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## COLLINS AMATEUR EQUIPMENT GUARANTEE

The Collins Amateur equipment described herein is sold under the following guarantee:
Collins agrees to repair or replace, without charge, any equipment, parts, or accessories which are defective as to design, workmanship, or materials, and which are returned to Collins at its factory, transportation prepaid, provided:
(a) Buyer has completed and returned to Collins promptly following his purchase the Registration Card included in the Instruction Book furnished with the equipment.
(b) Notice of the claimed defect is given Collins within 90 days from the date of purchase and goods are returned in accordance with Collins' instructions.
(c) Equipment, accessories, tubes, and batteries not manufactured by Collins or from Collins' designs are subject to only such adjustments as Collins may obtain from the supplier thereof.
(d) No equipment or accessory shall be deemed to be defective if, due to exposure or excessive moisture in the atmosphere or otherwise after delivery, it shall fail to operate in a normal and proper manner.
(e) Any failure due to use of equipment in excess of that contemplated in normal amateur operations shall not be deemed a defect within the meaning of these provisions.
The guarantee of these paragraphs is void if equipment is altered or repaired by others than Collins or its authorized service center.

No other warranties, expressed or implied, shall be applicable to said equipment, and the foregoing shall constitute the Buyer's sole right and remedy under the agreements contained in these paragraphs. In no event shall Collins have any liability for consequential damages, or for loss, damage or expense directly or indirectly arising from the use of the products, or any inability to use them either separately or in combination with other equipment or materials or from any other cause.

IMPORTANT!
It is necessary that the business reply card included herewith be filled out and mailed to the Company promptly in order for this guarantee to be effective.

HOW TO RETURN MATERIAL OR EQUIPMENT. ${ }^{\text {II }}$, for any reason, yuu should wish to return guarantee or otherwise, you should notify us, giving full particulars including the details listed below insofar applicable. If the item is thought to be defective, such notice must give full information as to nature of defect and identification (including part number if possible) of part considered defective. (With respect to tubes we suggest that your adjustments can be speeded up if you give notice of defect directly to the tube manufacturer.) Upon receipt of such notice, Collins willpromptly advise you respecting the return. Failure to secure our advice prior to the forwarding of the goods or failure to provide full particulars may cause unnecessary delay in handling of your returned merchandise.

## ADDRESS:

Collins Radio Company Sales Service Department
Cedar Rapids, Iowa

## INFORMATION NEEDED:

(A) Type number, name, and serial number of equipment
(B) Date of delivery of equipment
(C) Date placed in service
(D) Number of hours of service
(E) Nature of trouble
(F) Cause of trouble if known
(G) Part number (9 or 10 digit number) and name of part thought to be causing trouble
(H) Item or symbol number of same obtained from parts list or schematic
(I) Collins' number ( and name) of unit sub-assemblies involved in trouble
(J) Remarks

HOW TO ORDER REPLACEMENT PARTS. your order as indicated below and furnish the following information insofar as applicable. To enable us to give you better replacement service, please be sure to give us complete information.

## ADDRESS:

Collins Radio Company Sales Service Department Cedar Rapids, Iowa

## INFORMATION NEEDED:

(A) Quantity required
(B) Collins' part number ( 9 or 10 digit number) and description
(C) Item or symbol number obtained from parts list or schematic
(D) Collins' type number, name, and serial number of principal equipment
(E) Unit sub-assembly number (where applicable)


Figure 1-1. 75A-4 Receiver and Block Diagram

## SECTION I DESCRIPTION

## 1. GENERAL.

The Collins 75A-4 receiver is designed primarily for amateur reception on the seven HF amateur bands. It retains many of the time-proven features of the earlier 75A series of receivers. These features include:
a. Double conversion, crystal controlled front end for high stability and good image rejection even on the 10 -meter bands.
b. Permeability tuned, sealed master oscillator for accurate dial calibration and long-term stability.
c. Mechanical filters in the IF circuits for the ultimate in selectivity.

## 2. NEW FEATURES.

Increased amateur activity on single sideband has revealed a need for a receiver designed especially for single sideband reception. The 75A-4 incorporates several new features which considerably improve the ease of reception of a SSSC signal. They include:
a. DETECTORS. Separate detectors for double or single sideband signals. The sideband detector is a mixer type detector, which greatly reduces the distortion which is generated when a conventional diode detector is used for detecting a SSSC signal. A diode detector is used for conventional double sideband signals.
b. A VC. A fast attack, slow release A VC system is fast enough to respond to the first few cycles of a sideband transmission and does not require the presence of a carrier for operation. A fast and slow release time are available on a panel switch. The "fast" is used normally for AM reception. The "slow" is used during sideband and CW reception and prevents the receiver from "opening up" between words and characters.
c. PASSBAND TUNING. A passband tuning system is used in the 75A-4. In this system the receiver BFO is mechanically ganged and tracked with the main tuning dial. Once a SSSC signal is tuned in, it can be moved relative to the passband of the receiver without losing intelligibility of the signal. This feature is especially useful for "switching" sidebands and for dodging interfering signals. In $\mathrm{CW}^{\prime}$ reception, the desired signal can be moved around in the passband without changing the pitch of the received beat note, and at the same time, interfering signals can be pushed off the edge of the passband.
d. "Q" MULTIPLIER. A combination "Q" multiplier and bridge T-filter are used in the 75A-4. This circuit replaces the conventional crystal filter and has several features which make it superior to the crystal filter. It has a deep, narrow notch which has equal effectiveness anywhere in the passband. Conventional crystal filters become inoperative at frequencies several hundred cycles on either side of the resonant frequency of the crystal. The " $Q$ " multiplier does not seriously distort the shape of the IF passband as does a crystal filter. This results in much less loss of intelligibility while still doing a superior job of eliminating heterodynes.
e. MECHANICAL FILTERS. Space has been provided for 3 mechanical filters. This allows the operator to tailor his set to his requirement. An 800cycle filter is available for $C W$ use and a $6 K C$ filter for double sideband AM reception. The 75A-4 is normally supplied with one 3 -KC filter as standard equipment.
f. NOISE LIMITER. A new noise limiter circuit which is effective on AM, CW or SSSC signals is used in the 75A-4. This limiter is designed to clip both the positive and negative peaks of the detected signal. By means of a panel control the operator can select the degree of clipping desired.
g. CRYSTAL CALIBRATOR. A crystal calibrator circuit is an integral part of the 75A-4. No adapters are needed. Calibration signals are present every 100 KC at the flip of a panel switch.


Figure 1-2. Type F-455J Plug-in Mechanical Filter.

## 3. SPECIFICATIONS.

| Frequency Range: - | $\begin{gathered} \text { Band } \\ \text { (meters) } \end{gathered}$ | Range $(\mathrm{mc})$ |
| :---: | :---: | :---: |
|  | 160 | 1.5 to 2.5 |
|  | 80 | 3.2 to 4.2 |
|  | 40 | 6.8 to 7.8 |
|  | 20 | 14.0 to 15.0 |
|  | 15 | 20.8 to 21.8 |
|  | 11 | 26.5 to 27.5 |
|  | 10 | 28.0 to 29.0 |
|  | 10 | 29.0 to 30.0 |

Size: - 10-1/2" high $\times 17-1 / 4^{\prime \prime}$ wide $\times 15-1 / 2^{\prime \prime}$ deep.
Weight: - 35 pounds.
Finish: - St. James gray wrinkle enamel.
Cabinet: - Table mounted with provision for relay rack mounting.

Power Input: $-105 \mathbf{- 1 2 5}$ volts AC, $50-60 \mathrm{cps}: 85$ watts.

Number of Tubes: - 22, including rectifier and voltage regulator tubes

Types of Reception: - AM, CW: SSB, MCW:
Sensitivity: - $\mathbf{1 . 0}$ microvolt for 6 db signal-tonoise ratio with 3 KC bandwidth.

Antenna Input: - Accommodates wide range of antenna impedances; designed for $50-150 \mathrm{ohms}$ terminal impedance; coax connector provided.

Selectivity: - The selectivity is determined entirely by the choice of mechanical filters. Provision is made for use of three filters. Filters are available in bandwidths of $0.8 \mathrm{KC}, 3.1 \mathrm{KC}$ and 6 KC . Use only the filters here listed; F-455J-08 (Part No. $\overline{522} 909000$ ) for $800 \mathrm{cps} ; \mathrm{F}-455 \mathrm{~J}-31$ (522 908900 ) for $3.1 \mathrm{KC} ; \mathrm{F}-455 \mathrm{~J}-60(522909100$ ) for 6 KC . Receiver supplied with 3.1 KC filter ( $\mathrm{F}-455 \mathrm{~J}-31$ ).


Figure 1-3. 75A-4 Selectivity Curves
A VC Characteristics: - Audio rise less than 3 db for inputs of 5 to $200,000 \mathrm{uv}$.

## AVC Time Constants: -

|  | Fast | Slow |
| :--- | ---: | ---: |
| Rise Time | .01 sec. | .01 sec. |
| Release Time | .1 sec. | 1 sec. |

IF and Image Rejection: - All greater than 50 db down.

## Audio Characteristics: -

Output - . 75 watts with a 3.0 uv signal, $30 \%$ modulated.

Output impedance - 500 ohms, 4 ohms.
Response of audio circuits $- \pm 3 \mathrm{db} 100 \mathrm{cps}$ to 5000 cps .

Distortion - Less than $10 \%$.

## Noise Limiter: -

AM - Adjustable clip point, automatic carrier reference.

CW-SSB - Adjustable clip point. Clip reference controlled by flat AVC.

Muting: - Provisions for muting the receiver during key-down operation is provided. A muting voltage of +20 volts must be supplied by the transmitter or a separate contact on a keying rel $y$ and a 20 volt " $B$ " battery.

Frequency Stability (at 14.5 mc ):
Temperature - Not more than 1200 cycles drift, from 0 degrees to +60 degrees centigrade.

Warmup - After 30 -minute warmup, drift during any 10 -minute period does not exceed 100 cps . Voltage - For line voltage changes of $\pm 10 \%$, the frequency does not change more than 100 cps . Humidity - For humidity changes of from 0 to $90 \%$, the frequency does not change more than 50 cps . Dial Accuracy - (After calibration) All Bands $- \pm 300 \mathrm{cps}$.

## 4. ACCESSORIES.

In addition to the mechanical filters listed in paragraph 3 above, the following accessories are available:

Speaker $-10^{\prime \prime}$ speaker in matching cabinet, speaker cabinet $15^{\prime \prime}$ wide, $11-1 / 8^{\prime \prime}$ high, $9-1 / 8^{\prime \prime}$ deep. Type No. $270 \mathrm{G}-3$. Part No. 522014900.

Rack Mounting Bracket Assembly: - To adapt the receiver for standard relay rack mounting. St. James Gray wrinkle finish. Part No. 540462800 .

## SECTION II INSTALLATION

## 1. UNPACKING.

Open packing cartons carefully to prevent damage to the equipment. Remove packing material and remove the equipment from the cartons. Search the packing material for small packages. Inspect the receiver for loose screws and bolts. Check all knobs, switches, etc., to see that they operate properly. Any claims for damage should be filed promptly with the transportation company. If a claim is to be filed, the original packing case must be preserved. See instructions on back of the bill of lading.

## 2. EXTERNAL CONNECTIONS (See figure 2-1).

a. ANTENNA AND GROUND. The antenna connector strip is located at the rear of the chassis on the right-hand side. Balanced antennas should be connected to terminals 1 and 2. When a balanced antenna is used, grounding terminal G may introduce noise. Therefore, to determine the more satisfactory arrangement, try the receiver both
with and without an external ground. A single-wire antenna should be connected to terminal 1 with terminals 2 and G connected together and grounded.
b. COAXIAL ANTENNA CONNECTION. The $75 \mathrm{~A}-4$ is provided with a UG-58/U receptacle and UG-21B/U plug for use with coaxial cable antenna input. Figure 5-6 shows the proper method for assembling plug RG-21B/U to RG-8/U cable.

$$
\text { N. } 527 A \text { flch CAUTION }
$$

Do not subject the antenna input to RF exceeding 50 volts. Excessive RF voltages may be encountered if the receiving antenna is not disconnected when the transmitter is operating. Excessive capacity coupling across contacts of the antenna change-over relay may also result in excessive $R F$ voltage when the transmitter is operating. If an RF voltmeter is not available, a small neon bulb connected at the receiver terminals will serve as an indicator of harmful RF voltage.


2-0
Figure 2-1. 75A-4 Receeiver, External Connections

c. OUTPUT CONNECTIONS.
(1) SPEAKER. The output connections are on the rear of the chassis at the left-hand side. Terminals $G$ and 4 are for connection to a speaker voice coil. This output is open circuited by the headphone jack on the front panel so that plugging in headphones disables the speaker.
(2) HEADPHONES. In addition to the frontpanel jack, a pair of terminals marked $G$ and $P$ is provided for rear-chassis headphone connection. This output is connected to the 4 -ohm tap on the output transformer and is not open circuited by the front-panel jack.
d. 500-OHM OUTPUT. These terminals may be used to feed a transmitter or telephone line for phone patch, or may be connected to a sidetone oscillator or monitor.
e. STANDBY. The standby terminals. marked 1 and 2, are located at the rear of the chassis on the center terminal strip. These terminals are across a blocking bias resistor and are in parallel with contacts on the OFF-STANDBY-ON CAl. switch. The terminals may be connected to contacts of a send-receive relay for external stamith control. With the OFF-STANDBY-ON CAl. switth in STANDBY position, closing the stamills elrcuit will allow the receiver to operate. (anening the atindthy circuit will disable the audio outinat tute and all sube: which are connected to the AVC line.
f. MUTING. Terminals $M$ and $G$ on the conter terminal strip at the rear of the chassis are brovided for connection to a source of muting voltage for break-in CW' operation. This source must ts. capable of delivering +20 volts to the terminals for key-down muting and 0 volts key-up. The Collins KWS-1, $32 \mathrm{~V}-1,32 \mathrm{~V}-2$, and $\mathrm{KW}-1$ transmitters provide a muting voltage.

The muting voltage may be obtained from the cathode resistor of a keyed stage which is biased to cutoff during key-down conditions, from a resistor in series with a cathode-keyed stage. or from a battery in series with auxiliary contacts on a keying relay. Terminal G must be connected to a point of ground potential and terminal M to the source of positive voltage.

## NOTE

Neither the disabling nor the muting circuits provide protection to the antenna input circuit. See part 2 of this section, paragraph b.
g. POWER. The receiver must be powered from a 115 -volt, $50 / 60 \mathrm{cps}$ source.
h. FUSE. The fuse is in an extractor-type fuse post located on the rear of the chassis near the lefthand corner. To remove the fuse, push in the fusepost cap, turn it counterclockwise, and pull straight out. Use only a 2 -ampere fuse.

## 3. INSTALLATION OF MECHANICAL FILTERS.

If the receiver was shipped with the mechanical filter (or filters) removed, open the receiver lid and loosen the filter clamp wing nut and remove the clamp. Plug the filter all the way in (very important to prevent feedthru) and replace the filter clamp. Shove the clamp down tightly and tighten the wing nut. Use socket B for 3 KC , socket A for 800 cps , and socket C for KC filters.

## 4. "S" METER ADJUSTMENT.

Set up the receiver for AM operation (section III, part 2), short the antenna input connections, and set the ZERO-ADJUST Control, located on top of the receiver chassis, for an " S " meter reading of 0 .

## NOTE

The METER SENSITIVITY Control is set at the factory by injecting a $100 \mathrm{uv}, 3.7 \mathrm{MC}$ signal into the ANT input and adjusting for an S-9 reading of the " S " meter.

## 5. ADJUSTMENT OF CALIBRATION OSCILLATOR.

Turn the set on and allow it to warm up for about 20 minutes. During this 20 -minute period, read Section III OPERATION and tune around the bands and get the "feel" of the set. After the set is warmed up, tune in a signal of known accuracy (WWV at $2.5,15$, or 30 MC is suggested). Turn the OFF-STANDBY-ON CAL Control to CAL, switch to AM and center the PASSBAND TUNING knob. If an audible beat note is heard, lift the receiver lid and locate the CAL adjusting capacitor in the left-hand, rear corner of the chassis. Be sure not to confuse the tone modulation, when present, on WW'V with the beat note. Turn this capacitor until zero beat is obtained. The calibrator is now adjusted. Check for a signal at several $100-\mathrm{KC}$ points on the tuning dial.

## 6. USE OF EXTERNAL SIDEBAND SELECTING DEVICES.

Do not use the 75A-4 with external sideband selecting devices. These arrangements which have become popular for single sideband reception with other types of receivers should not be employed
with the 75A-4. These devices were intended to provide rejection of an unwanted sideband, selection of either sideband, and carrier reinsertion. Each of these functions is performed by the normal circuitry of the 75A-4 and in a more convenient and effective manner than would be accomplished with such devices.


Figure 3-1. 75A-4 Oferating Controls

## SECTION III OPERATION

## 1. CONTROLS.

a. OFF-STANDBY-ON CAL. This switch turns the receiver power on and off and in STANDBY position allows filament and plate voltages to remain on but disables the receiver. In the CAL position, plate and filament power remain on and $\mathrm{B}+$ is applied to the calibration oscillator. In STANDBY position, a resistor, $\mathrm{R}-98$, is inserted in series with the bias load resistors to increase the bias voltage to cutoff on the output tube and the AVC controlled tubes. Standby terminals 1 and 2 on the rear of the chassis are connected across $\mathrm{R}-98$ to allow the use of an external send-receive switch or relay to control the standby function. This connection would be effective with S-6 in STD BY position.
b. BAND CHANGE. This switch is used to select the desired amateur band. Turning the control knob turns the shaft of the band switch and at the same time rotates the dial drum so that the scale in use is visible through the MEGACYCLES window. The 10-meter band occupies 2 positions of the switch; all other bands one position.
c. MEGACYCLES - KILOCYCLES. The main tuning dials are a slide-rule MEGACYCLES dial and circular KILOCYCLES dial. The MEGACYCLES dial is calibrated in $100-\mathrm{KC}$ divisions on each scale. The scale for each band is 1 megacycle wide. The KILOCYCLES dial is calibrated in $1-\mathrm{KC}$ divisions. The KILOCYCLES dial has two scales; the lower scale is black, and is calibrated in $1-\mathrm{KC}$ divisions for 80-10 meters; and the upper scale, also marked in 1-KC divisions, is red, and is used on 160 meters. The 160 -meter scale is separate from the black scale because kilocycle readings on this band run in the opposite direction from those on the other bands.

Scales on the MEGACYCLES dial are colored to correspond to the colors on the KILOCYCLES dial.

The frequency at which the receiver is set is determined by combining the readings of the two dials. For example, if the MEGACYCLES scale reads 3.8 plus and the KILOCYCLES scale reads 52 , the receiver is tuned to 3852 KC ; or if the MEGACYCLES dial reads 28.6 plus and the KILOCYCLES
dial reads 32 , the receiver is tuned to $28,632 \mathrm{KC}$. For frequency measuring procedures, refer to part 9 of this section, FREQUENCY MEASURING.
d. AM CW-SSB. In the CW-SSB position this switch turns on the BFO, selects the CW-SSB detector $\mathrm{V}-11$, and puts fixed operating bias on the noise limiter. In the AM position, this switch turns off theBFO, selects the AM-MCW detector, and removes the fixed bias from the noise limiter and connects the noise limiter to the carrier source of bias.
e. SELECTIVITY. This control selects the sockets into which the mechanical filters are inserted. It is suggested that the $3-\mathrm{KC}$ filter be inserted into socket B, socket A be reserved for an $800-\mathrm{cps}$ filter, and socket C be reserved for a 6 KC filter. The panel is marked to conform with the socket lettering.
f. RF GAIN. This control is used to set the maximum RF and IF gain of the receiver so that the AVC will not increase the gain excessively between characters in CW or between words and syllables in SSB reception. The 75A-4 should always be used with AVC for all types of signals. The AVC OFF position is provided merely for test and special purposes. The RF GAIN Control is normally set so that the S meter "kicks up" about three S points or 20 db during keying or SSB reception. Adjustment of the RF GAIN Control does not disturb the reading of the $S$ meter provided it is set so that the $S$ meter rises in the presence of a signal. For exact tuning and operating procedures, refer to parts 2-8 of this section.
g. AUDIO GAIN. This control is used to adjust the gain of the first audio stage. It should be employed to adjust the loudness or volume of the receiver. The RF GAIN Control should not be used for this purpose either on CW or voice reception.
h. PASSBAND TUNING. The shaft of this control is connected directly to the BFO tuning condenser and is connected by a belt drive to the frame of the master oscillator (KILOCYCLES tuning). Its function is explained in part 7.
i. ANT. TRIM. This control should be adjusted for maximum RF gain each time a different band is used. The control shaft is coupled to a trimmer capacitor across the RF coil for the band in use and is used to compensate for changes in antenna characteristics from one band to another.
j. NOISE LIMITER. The noise limiter functions for both AM and CW-SSB operation. The NOISE LIMITER is out of the circuit when the control is in the OFF position. When the control is advanced from the OFF position, the noise limiter is connected into the circuit. Advancing the control toward higher numbers increases the noise limiting action on both AM and CW-SSB. Use the noise limiter on phone only when the need arises because, as with all noise limiters, some distortion is introduced with its use.
k. AVC. The AVC Control can turn off the AVC altogether or it can select either fast release or slow release AVC characteristics. In both cases the AVC is fast attack, the release time being the selectable characteristic. The FAST position is used for AM operation. The SLOW is used for CW-SSB operation and for CWoperation because it prevents the receiver from "opening up" between words or CWcharacters.

1. REJECTION TUNING. This control takes the place of the usual crystal filter phasing control. In operation, it is much more effective than the crystal filter phasing control in reducing heterodyne interference. The control tunes the rejection filter through the entire receiver passband. To remove the filter from the circuit, turn the control to OFF. See part 8 for operational procedures.

> m. ZERO SET. Rotating the ZERO SET knob moves the indicator line on the KILOCYCLES dial This adjustment allows exact calibration of the KILOCYCLES dial on a signal of known frequency. Calibration procedures are described in part 9 of this section, FREQUENCY MEASURING.

## 2. TUNING AM SIGNALS.

The tuning techniques used with a 75A-4 receiver when employing the $3-\mathrm{KC}$ filter differ somewhat from those used in tuning a conventional receiver. Because of the flat top and almost vertical sides of the passband, it is possible to tune either sideband of an AM station and reject the opposite sideband. Tuning "on the nose" results in loss of the high frequency audio components with a loss of intelligibility. Select the sideband that contains the least
objectionable adjacent channel interference. Use the following procedure to tune AM signals.
a. Setup for AM reception. Power on. Operate BAND CHANGE switch to desired band. Select 3-KC mechanical filter. RF GAIN maximum. Use AUDIO GAIN for volume control. Set for FAST AVC. Set PASSBAND tuning for LOWER sideband as described below, after adjusting DIAL DRAG.
b. Tune in AM station for maximum $S$ meter reading.
c. Adjust antenna trim for maximum $S$ meter reading. (One setting for each new band usually sufficient.)
d. Tune the receiver clockwise (counterclockwise on 160 meters) or to high frequency side of the signal until the $S$ meter reading drops sharply. Then back up the tuning until the $S$ meter reading just regains its former value and the modulation is readable. The receiver is now tuned to accept the lower sideband and the carrier of the AM station. If interference is present it may be possible to avoid it by setting the PASSBAND TUNING to accept the carrier and the upper sideband. The same result can be obtained by adjustment of the main tuning control except that if the main tuning control is used for this purpose instead of the PASSBAND TUNING, the dial will no longer read the exact carrier frequency of the received signal.
e. If impulse noise is severe, advance the NOISE LIMITER Control from the OFF position far enough to reduce the impulse noise but not so far as to distort the modulation appreciably.
f. If heterodyne interference is bad on both sidebands, tune to the better sideband. Operate the REJECTION TUNING Control over its entire range ( $90^{\circ}$ either side of center position) to find the position at which the heterodyne is weakest.
g. If interference is not severe, some improvement in reception may be experienced by switching to the $6-\mathrm{KC}$ mechanical filter if one is available. W'hen the $6-K C$ mechanical filter is used, the PASSBAND TUNING should be centered and the receiver should be tuned to place the carrier in the center of the passband.

## 3. TUNING SINGLE-SIDEBAND SIGNALS.

a. Setup for CW-SSB reception. Operate BAND CHANGE switch to desired band. Select 3-KC
mechanical filter. RF GAIN 8 to 10. AUDIO GAIN for normal volume of about 2. AVC-SLOW. PASSBAND TUNING set for desired sideband. • Usual amateur practice is to employ the lower sideband on the 4 and 7 bands and the upper sideband on the 14 , 21 , and 28 mc bands. Occasionally amateurs do not follow this rule, in which case it will be necessary to switch sidebands by resetting the PASSBAND TUNING accordingly.
b. Tune in SSB station very slowly until signal is readable. Some care is necessary in the final adjustment of tuning in order to set the frequency sufficiently accurately to make the voice sound entirely natural.
c. If the signal cannot be made readable, turn PASSBAND TUNING to the other side of zero and repeat the tuning procedure.
d. Readjust the RF GAIN Control until the $S$ meter kicks up not to exceed three $S$ points or 20 db with the voice modulation. If the $S$ meter kicks much more than this with the modulation, a popping or pumping effect will be observed due to the necessary attack time of the AVC. The RF GAIN Control can be set so that the $S$ meter does not kick up, but if this is done a weaker station breaking in on the same frequency may not be received.
e. The PASSBAND TUNING can be displaced slightly from its normal setting from either the upper or lower sideband in order to minimize interference which may be present at the edges of the sideband. The NOISE LIMITER can also be used to reduce impulse noise interference.

## 4. TUNING CW SIGNALS.

The receiver is set up for $C W$ reception in exactly the same way as it is set for SSB reception. Namely, set switch for CW-SSB, power on. BAND CHANGE switch to desired band. Select 3 KC mechanical filter. RF GAIN 8-10. AVC-SLOW. AUDIO GAIN for desired headset or speaker volume.
a. Set PASSBAND TUNING in the normal position for either sideband (not centered).
b. Tune CW station to give a beat note of 1000 to 1500 cycles.
c. If the CWstation is being interfered with, turn PASSBAND TUNING one way or the other to drop off interfering station and to retain the wanted station (be sure the DIAL DRAG is engaged).
d. The REJECTION TUNING may also be used to eliminate an interfering station.
e. If an $800-$ cycle filter is available, it may be selected and the PASSBAND TUNING readjusted to place the signal in its narrow passband and to accomplish a further reduction of interference and noise.
f. The NOISE LIMITER can be advanced to reduce impulse noise interference.
g. The RF GAIN Control can be adjusted so that the $S$ meter kicks up only sufficiently to provide an $S$ meter reading during keying and so that the gain of the receiver does not recover excessively between characters. Some AVC action should be retained, however, in order to make sure that a weaker breaking station will be heard.

## 5. LOCALLY REINSERTED CARRIER.

Locally reinserted carrier technique can be employed to advantage where selective fading is causing difficulty in reading an AM signal. The tuning procedure eliminates the station's carrier and substitutes the 75A-4 BFO for use as steady source of carrier power. Combining the station's sideband with the BFO carrier in the 75A-4 receiver produces the intelligible signal. Proceed as follows:
a. Set receiver up for $\operatorname{SSB}$ reception and tune the signal for greatest intelligibility as in SSB reception. (See part 3 of this section.)

## 6. SINGLE-SIDEBAND AM RECEPTION.

Some AM transmitters emnloy only one sideband. This is accomplished with a single-sideband transmitter by reinserting carrier after phasing out or filtering out one of the sidebands. It has the advantage of permitting reception on an ordinary AM receiver and at the same time occupying only half the spectrum space of an "old-fashioned" doublesideband AM transmitter. The disadvantage, of course, is that the full power of the transmitter can not be employed in the voice sideband and also that a carrier, which may produce continuous interference, is transmitted. Single-sideband AM signals of this type can be received with the 75A-4 receiver set for $A M$, except that the receiver must be adjusted to correspond to the sideband being transmitted.

## 7. PASSBAND TUNING.

Previous receivers have been inconvenient to tune for $C W$ or SSB reception because there has been no
way of varying the position of the passband without at the same time disturbing the frequency of the beat note. It is, of course, necessary to have a BFO correctly positioned in respect to the passband in order to obtain proper voice reception in the case of SSB, and in order to obtain a suitable beat note in $C W$ reception while at the same time accepting the desired signal and rejecting others. This difficulty in tuning conventional receivers has been aggravated by the fact that the BFO tuning usually was not accurately calibrated and many BFO's were subject to drift and instability. The 75A-4 overcomes these difficulties through the use of a stable, temperaturecompensated and calibrated BFO arranged with a mechanical linkage to the VFO tuning. The PASSBAND TUNING Control varies the frequency of the $B F O$ and at the same time produces an equal and opposing change in the VFO frequency by rotating the case of the VFO. Since the tuning of both oscillators is linear, it is possible to make this tuning track closely at all points. The net effect, then, of turning the BFO tuning control is to maintain the reinserted carrier (BFO injection) frequency unchanged relative to the received signal, but at the same time to change the tuning of the receiver in respect to the IF passband. In this way it is possible to use the main tuning control to "zero in" on an SSB signal or to adjust a CW' beat note to the desired frequency and then to use the PASSBAND TUNING Control to select the desired sideband in the case of SSB or to dodge interference in the case of $C W$ without disturbing the beat frequency. In order to have the PASSBAND TUNING Control work in this way it is necessary to adjust the DIAL DRAG so that rotating the PASSBAND TUNING Control does not cause the main tuning dial to rotate. This adjustment is made most easily by rocking the PASSBAND TUNING Control back and forth and at the same time slowly tightening the DIA L DRAG knob until just sufficient drag is obtained to prevent the main tuning dial from rotating. Once this adjustment is set, it is still possible to use the main tuning control with negligible increase in friction.

Use of the PASSBAND TUNING Control has been described in the preceding sections. Once its purpose and method of operation is understood, its use will become second nature. It will be observed that the PASSBAND TUNING knob has a white sector which spans approximately 3 KC of the panel calibration. It thus forms a graphic representation of the passband displayed against the panel calibration with zero representing the position of the carrier frequency. The smaller black sector in the middle
of the white sector represents the width of an 800 cycle filter and thus the same picture is presented when this narrower filter is employed in CW reception.

It is important when first placing the receiver in operation and at occasional intervals thereafter to check the calibration of the BFO to make sure that it is correctly set. The calibration adjustment can be accomplished most readily as follows:
a. Adjust DIAL DRAG.
b. Set PASSBAND TUNING on center.
c. Tune the receiver to a calibration check point on one of the higher frequency bands. Adjust for zero beat.
d. Rotate the PASSBAND TUNING each way until the $S$ meter drops about three $S$ points or 20 db and note the position of the center index mark on the PASSBAND TUNING knob at which this drop is obtained. A 20 db reduction in S meter reading should occur symmetrically on each side of zero and at about 15 KC as indicated by the line in the center of the white sector on the knob (using a 3 KC filter). If the drop off is not symmetrical, remove the plug from the top of the BFO can and make a small change in the setting of the adjustable slug. Retune the main tuning for zero beat and see if the drop off points are more symmetrical around zero than before. Repeat until the correct setting of the inductance slug is found. Ordinarily this adjustment would not be needed or, at most, very infrequently. Complete BFO alignment procedures are given in section $V$, part 7 .

The PASSBAND TUNING Control, of course, serves as a "sideband switch". Positioning the white sector either side of zero serves to select either the upper or lower sideband without retuning the receiver.

## 8. REJECTION TUNING.

This control is used to minimize interference caused by heterodynes. It is usually placed in the OFF position until a heterodyne is experienced. Tune the REJECTION TUNING very carefully until the most bothersome heterodyne is eliminated or greatly attenuated. When the UPPER sideband is being received, low frequency heterodynes will be attenuated in the region left of center mark. High frequency heterodynes will be attenuated in the
region right of the center mark. When the LOWER sideband is being received, low frequency heterodynes will be attenuated in the region right of center and high frequency heterodynes to the left of center. The null for any audio tone is very sharp so the knob must be moved very slowly.

## 9. FREQUENCY MEASURING.

The KILOCYCLES dial reads the true carrier frequency if the station is tuned to zero beat.

## NOTE

See part 5 of section II for calibration oscitlator adjustment.
a. Calibration: Frequency readings will be more accurate if the calibrator is used to calibrate the dial before frequency measurements are made. To use the calibrator, set up for CW reception (part 4 of this section), tune to the $100-\mathrm{KC}$ point nearest the frequency to be measured, set the PASSBAND TUNING Control to center position, and turn on the calibrator. Zero beat the calibrator signal, using the main tuning control. Adjust the ZERO SET knob so that the dial marker lines up with zero on the KILOCYCLES dial. Turn off the calibrator.
b. To measure the carrier frequency of an $A M$ station, select CW operation, set PASSBAND TUNING to 0 , tune the station for zero beat, and read the frequency on the tuning dial.
c. With the single-sideband station properly tuned in the suppressed carrier frequency is the KILOCYCLES dial reading.

## 10. SETTING DIAL DRAG.

a. Loosen DIAL DRAG.
b. Gently rock PASSBAND TUNING back and forth and gradually tighten DIAL DRAG.
c. Stop tightening DIAL DRAG at the point where the KILOCYCLES dial stops following the movement of the PASSBAND TUNING dial.
d. DIAL DRAG is now properly adjusted.
e. The KILOCYCLES dial can now be tuned with negligible additional friction due to the DIAL DRAG.

# SECTION IV <br> THEORY OF OPERATION 

## 1. GENERAL

Refer to the block diagram of figure 1-1. The 75A-4 amateur band receiver is a dual conversion receiver on all bands except 160 meters where single conversion is employed. The dual conversion scheme employs a fixed high frequency oscillator, crystal controlled, and a variable first intermediate frequency. The signal from a type $70 \mathrm{E}-24 \mathrm{VFO}$ is beat against the variable IF to produce a fixed 455 KC second intermediate frequency. One stage of RF amplification is employed in the receiver. The passband of the fixed IF ( 455 KC ) is shaped by a mechanical filter stage. A "Q" multiplier stage provides a tunable notch to minimize heterodyne interference. Two more 455 KC IF stages follow the "Q" multiplier. These feed separate detectors for AM or CW-SSB reception. The output of the detectors feed a combination AM and CW type adjustable noise limiter. Three stages of audio amplification follow. The output stage feeds a headset jack and a 500 -ohm load or a 4 -ohm speaker. A separate AVC amplifier and rectifier are used. Bias for the audio output tube and the RF gain control system is obtained from a separate rectifier. A built-in $100-\mathrm{KC}$ calibration oscillator is included in the set. The passband tuning feature is accomplished by gang tuning the BFO and variable frequency oscillator by means of a metal belt.

## 2. TUNING.

All variable tuned stages including the RF stage, the first mixer, the variable IF system and the variable frequency oscillator are operated by the KILOCYCLES dial. This dial is coupled directly to the shaft of the variable frequency oscillator. All other variable tuned circuits just mentioned are tuned by a common platform to which powdered iron slugs are attached. The platform is moved up and down at a linear rate by means of a mechanism which is coupled to the VFO shaft by a system of split gears and metal belts. The receiver uses a unique method of band switching in the RF stage in which only the 80 -meter (T-2) and the 160 -meter ( $\mathrm{T}-1$ ) coils are tuned by the main tuning mechanism, and coils for 40-10 meters are selected and connected across the 80 -meter coil. Varying the inductance of
the 80 -meter coil varies the total inductance, and therefore the resonant frequency of the tuned circuit in use.

## 3. RF CIRCUITS.

A simplified block diagram of the 75A-4 RF system is shown in figure 4-1. The RF stage V-2 feeds the mixer at the carrier frequency of the incoming signal. The coverage of each band is as follows:

$$
\begin{array}{r}
160 \text { meters }-1.5-2.5 \mathrm{MC} \\
80 \text { meters }-3.2-4.2 \mathrm{MC} \\
40 \text { meters }-6.8-7.8 \mathrm{MC} \\
20 \text { meters }-14.0-15.0 \mathrm{MC} \\
15 \text { meters }-20.8-21.8 \mathrm{MC} \\
11 \text { meters }-26.0-28.0 \mathrm{MC} \\
10 \text { meters }-28.0-29.0 \mathrm{MC} \\
29.0-30.0 \mathrm{MC}
\end{array}
$$

The first conversion circuit, consisting of a crystal controlled oscillator, V-4 and a mixer tube, $\mathrm{V}-3$, converts the incoming signal to the variable IF frequency of 2.5 to 1.5 MC for all bands from 80 meters thru 10 meters. The variable IF is mixed with a signal from the VFO, V-14 and V-15, in the second mixer $\mathrm{V}-5$ where it is converted to a fixed IF of 455 KC . See figure 5-7. A discussion of the individual circuits in the RF portion of the receiver follows:
a. RF STAGE. The RF stage uses a 6DC6 pentode. This tube was chosen because of its lownoise, remote-cutoff characteristics. This tube allows greater grid voltage swing without crossmodulation distortion. Individual variable slugtuned coils are switched into the grid circuit on 160 and 80 meters. On 40-10 meters the coil in use is switched across the 80 -meter coil, and varying the inductance of the 80 -meter coil tunes the coil for the band in use. The 80 -meter trimmer capacitors are not in the circuit on 40-10 meters.

One coil, T-7, is used for the 11 and 10 -meter bands. Manual tracking is used here employing the ANT TRIM capacitor, C-18. Separate antenna coils are employed on the $10-11$-meter coil, the 80 -meter coil, and the 160 -meter coil.


Figure 4-1. Tuning Elements of RF and Mixer Stages, Simplified Diagram

The 160 -meter band feeds on thru the first mixer, V-2, into the 2.5 to 1.5 MC variable IF coils, which track with the receiver front end, and on into the second mixer V-3. On $80,40,20,15$ and the highest frequency 10 -meter band the first mixer grid circuit is similar to the RF stage grid circuit with the higher frequency coils being
paralleled with the 80 -meter coil to produce the tuning for the band in use. On the low 10-meter band and the 11-meter band, capacitors $\mathrm{C}-32$ and $\mathrm{C}-31$ are individually selected to pad the 10 -meter coil to these bands. The following table shows the tuning components used in the various bands for each tube circuit.

| BAND (METERS) | $\begin{gathered} \text { ANT } \\ \text { L } \\ \hline \end{gathered}$ | $\begin{aligned} & \text { ANT } \\ & \text { C PAD } \end{aligned}$ | $\begin{gathered} \text { ANT } \\ \mathrm{C} \text { TRIM } \\ \hline \end{gathered}$ | $\begin{gathered} \text { RF } \\ \mathrm{L} \end{gathered}$ | $\begin{gathered} \mathrm{RF} \\ \mathrm{CPAD} \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{RF} \\ \mathrm{C} \text { TRIM } \\ \hline \end{gathered}$ | $\begin{gathered} \text { OSC } \\ \mathrm{L} \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{OSC} \\ & \mathrm{PAD} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 160 | T-1 | C-6 | $\begin{aligned} & \mathrm{C}-7 \\ & \mathrm{C}-18 \end{aligned}$ | - | - | - | - | - |
| 80 | T-2 | C-9 | $\begin{aligned} & \mathrm{C}-8 \\ & \mathrm{C}-18 \end{aligned}$ | L-6 | C-24 | C-23 | L-12 | C-40 |
| 40 | $\begin{gathered} \mathrm{L}-1 \\ (\mathrm{~T}-2) \end{gathered}$ | C-10 | $\begin{gathered} C-11 \\ (\mathrm{C}-18) \end{gathered}$ | $\begin{gathered} \mathrm{L}-7 \\ (\mathrm{~L}-6) \end{gathered}$ | C-25 | C-26 | L-13 | C-41 |
| 20 | $\begin{gathered} \mathrm{L}-2 \\ (\mathrm{~T}-2) \end{gathered}$ | C-12 | $\begin{gathered} \mathrm{C}-13 \\ (\mathrm{C}-18) \end{gathered}$ | $\begin{gathered} \mathrm{L}-8 \\ (\mathrm{~L}-6) \end{gathered}$ | C-27 | C-28 | L-14 | C-42 |
| 15 | $\begin{gathered} \mathrm{L}-3 \\ (\mathrm{~T}-2) \end{gathered}$ | C-14 | $\begin{gathered} \mathrm{C}-15 \\ (\mathrm{C}-18) \end{gathered}$ | $\begin{gathered} \mathrm{L}-9 \\ (\mathrm{~L}-6) \end{gathered}$ | C-29 | C-30 | L-15 | C-43 |
| 11 | $\begin{gathered} \mathrm{T}-7 \\ (\mathrm{~T}-2) \end{gathered}$ | C-22 | $\begin{gathered} C-16 \\ (\mathrm{C}-18) \end{gathered}$ | $\begin{array}{r} \mathrm{L}-10 \\ (\mathrm{~L}-6) \end{array}$ | C-50 | C-31 | L-16 | C-44 |
| 10 LO | $\begin{gathered} \mathrm{T}-7 \\ (\mathrm{~T}-2) \end{gathered}$ | C-22 | $\begin{gathered} \mathrm{C}-16 \\ (\mathrm{C}-18) \end{gathered}$ | $(\mathrm{L}-10)$ | C-50 | C-32 | L-17 | C-45 |
| 10 HI | $\begin{gathered} \mathrm{T}-7 \\ (\mathrm{~T}-2) \end{gathered}$ | C-22 | $\begin{gathered} C-16 \\ (\mathrm{C}-18) \\ \hline \end{gathered}$ | $\begin{aligned} & (\mathrm{L}-10) \\ & (\mathrm{L}-6) \\ & \hline \end{aligned}$ | C-50 | C-17 | L-11 | C-51 |

( ) Components used in a previous band

## b. CRYSTAL CONTROLLED OSCILLATOR AND FIRST MIXER.

The high frequency mixer stage employs a 12AT7 (V-4) in a crystal controlled oscillator circuit to provide a heterodyning signal. In this oscillator circuit the crystal is connected between the cathodes of a dual triode. One section (V-4 pins 6, 7, 8) is a cathode follower amplifier, the other section, a grounded grid amplifier. Feedback voltage is coupled from the plate of one section, which contains a tank circuit resonant at the crystal frequency, to the grid of the other section. The crystal, inserted between the cathodes, acts as a filter. The phase change through the loop is zero and oscillation takes place at the crystal frequency. Crystal oscillator output voltage is coupled to the injection grid of the 6BA7 first mixer. An individual crystal for each band is switched into the crystal oscillator circuit except for 160 meters, where the high frequency oscillator is not used. The crystal oscillator beats with the incoming carrier to produce the first, or variable, intermediate frequency. In this stage, because the crystal frequency is fixed and the incoming carrier frequency may be anywhere in the range of the band in use, the difference frequency produced in the mixer must be tuned by a variable IF system.
c. VARIABLE IF. The variable IF covers the range 2.5 to 1.5 MC . The system consists of two slug-tuned coils on the same frequency. The first of these coils is capacity coupled to the second which in turn is connected to the grid of the second mixer V-5. L-23, a 5.7 MC trap is connected between the two coils to remove a spurious response that occurs at 3.533 MC .

## d. VFO AND SECOND MLXER. A Type 70E-24

 permeability-tuned precision variable frequency oscillator provides the injection voltage to the second mixer V-5. The frequency range of the VFO is 1955 KC to 2955 KC . This frequency is mixed with the variable IF in V-5 to produce the fixed 455 KC difference frequency which is the frequency of the fixed IF amplifier.e. MECHANICAL FILTER. The functional diagram of the Collins Mechanical Filter is shown in figure 4-2. The mechanical filter uses the principle of magnetostriction to convert electrical energy to mechanical vibration. The magnetostriction transducer input coil is resonated at 455 KC . A nickel wire within this coil vibrates mechanically and transmits this mechanical energy to the first of a series of nickel alloy discs. The mechanical vibration of this first disc is coupled to succeeding
discs by means of nickel-wire coupling elements. Biasing magnets at either end of the mechanical filter polarize the filter elements to prevent frequency doubling, in much the same manner as biasing magnets in a headphone prevent the headphone diaphram from bending in the same direction for both halves of an AC cycle. The mechanical vibration of the last disc is coupled to a magnetostriction transducer element identical to the one used at the input of the filter. By a reverse principle of magnetostriction, the mechanical vibration of the nickel-wire transducer core is converted to electrical energy.

Each of the discs employed in the mechanical filter has a mechanically resonant $Q$ exceeding 2,000 . Six of these discs are overcoupled to produce a mechanically-shaped response curve with a flat top and straight, almost vertical sides. Thus, the filter passes a band of frequencies very little wider than the flat top of the selectivity curve. The mechanical filter furnished with the 75A-4 passes a band of frequencies approximately 3 KC wide and centered on 45 E KC , providing an IF selectivity curve ideal for the reception of AM and singlesideband signals. The $3-\mathrm{KC}$ filter is supplied as part of the 75A-4; however, a mechanical filter having similar selectivity characteristics but having a band pass of 800 cycles is available for use in CW reception. A $6-\mathrm{KC}$ filter is available for double-sideband reception of AM.

The mechanical filters used in the 75A-4 are the plug-in type that plug into a 9 pin miniature tube socket. These are sealed units and must notbe tampered with. No external variable tuning is employed.
f. "Q" MULTIPLIER. (See figure 5-5.) The "Q" multiplier, as used in the 75A-4, is employed only as a rejection filter. In this capacity it performs the same function as the rejection notch of the crystal filter in earlier receivers but does it much better. It is capable of attenuating as much as 40 db , any single audio tone (heterodyne) which may be present within the receiver's passband. The " $Q$ " multiplier consists of a cathode follower amplifier coupled to a regenerative amplifier, the plate load of which is a bridge T -filter. The regenerative amplifier is kept just below the oscillating point by $\mathrm{R}-36$. At this point the plate circuit has a very high $Q$ and provides a very sharp null to frequencies within the receiver passband. REJECTION TUNING capacitor C-72 can shift the null around to any frequency within the passband. The " $Q$ " multiplier is removed from the circuit by turning the


Figure 4-2. A Collins Mechanical Filter, Functional Diagram

REJECTION TUNING Control clockwise to actuate a switch which short circuits inductor L-26.
g. 455 KC IF. AMPLIFIER. The 455 KC IF amplifier consists of V-6 which is associated with the mechanical filter and V-8 and V-9; the latter two are conventional IF amplifiers that contribute nothing to the passband wave shape, which is determined by the mechanical filter. All are 6BA6 tubes. AVC is applied to the grids of all three tubes.
h. AM DETECTOR. The AM detector is a conventional diode rectifier excited from IF transformer T-3 and having R-56 and R-57 as its load. The audio from the detector is applied to the noise limiter, V-12, when AM CW SSB selector switch $\mathrm{S}-3$ is operated to AM position.
i. CW-SSB DETECTOR. This detector, V-11 is designed especially for SSB reception. It is a mixer type circuit that takes the output of the BFO and mixes it with the output of the 455 KC IF. Tube elements 1,2 and 3 perform as a cathode follower amplifier. The remainder of the tube is a plate detector, the cathode of which is common with the cathode follower amplifier. The detector greatly reduces the distortion which is generated when a conventional diode detector is used for detecting SSSC signals. The audio from the detector is applied to the noise limiter $\mathrm{V}-12$ when $\mathrm{S}-3$ is operated to the CW-SSB position.
j. BFO. The BFO V-20, uses a 6 BA 6 in an electron coupled oscillator whose frequency range is approximately $453-457 \mathrm{KC}$. The BFO is tuned by means of the knob on the front panel labeled PASSBAND TUNING. The shaft of the PASSBAND TUNING Control is attached by a metal belt to the frame of the variable frequency oscillator which is mounted in a ball and oilite bearing equipped cradle. As the BFO is tuned through its range the VFO is also
tuned a like amount. (The shaft of the VFO is prevented from turning by the DIAL DRAG.) Because the actual intermediate frequency is changing, the passband is being shifted and an unwanted signal can be dropped off the edge of the passband while retaining the wanted signal in the passband without changing its pitch.

## 4. AUDIO CIRCUITS.

a. NOISE LIMITER. Noise limiter V-12, a 6 AL 5 tube, couples the audio from the detectors to the first audio stage. The function of the noise limiter is to minimize interference by removing noise peaks which exceed the amplitude of the modulation. It is effective on AM, CW and SSB.

Both diode sections of the 6AL5 are required in order to limit both the positive and the negative peaks. During AM reception, a negative voltage is derived across diode load resistors R-56 and R-57. NOISE LIMITER Control R-67 is connected to this source of supply. As a result the cathodes of V-12 assume a negative DC potential which is adjustable by means of the NOISE LIMITER Control, and direct current flows through the diodes (the plates being positive with respect to the cathodes). The AF signal voltage from the receiver is applied to the anode (pin 7) of one section of V-12 through coupling capacitor C-93. This AF signal modulates the DC flowing through this diode section and, as a result, the AF signal appears across cathode resistor R-65. This resistor is common to both diode circuits, therefore the AF signal is superimposed on the DC flowing through the second section of V-12 and appears across load resistor R-63. From this point, the signal is coupled through C-96 and AF GAIN Control R-62 to the audio amplifiers.

Any negative impulse that drives the anode of the input diode ( $p$ in 7) more negative than the cathode, will cut off the diode, and that impulse will be
limited to an amplitude equal to the threshold voltage (as set by the NOISE LIMITER Control). Similarly, any positive impulse that overcomes the threshold potential on the cathode of the second section (pin 5) will cut off that diode, and the positive impulse will be limited. As the NOISE LIMITER Control is turned toward 10, a less negative threshold voltage is applied to the diodes, and more severe limiting results. The threshold voltage at any given setting of the NOISE LIMITER Control varies with the average amplitude of the diode load signal, therefore limiting action automatically adjusts itself. C-97 and R-66 decouple the limiter circuit from the detector circuit.

During CW or SSB reception when the carrier is intermittent or absent, the reference voltage is supplied by connecting the NOISE LIMITER Control R-67 through switch S-3 to a value of bias obtained from the receiver bias rectifier. Because of the flat AVC characteristic of the receiver, frequent adjustment of the NOISE LIMITER Control is unnecessary.

The noise limiter is made inoperative by applying a value of $\mathrm{B}+$ to the diode plates through $\mathrm{R}-64$ and by grounding the cathodes of $\mathrm{V}-12$ thus insuring that the diode currents cannot be cut off on noise or high modulation peaks. This is done by a switch associated with the NOISE LIMITER Control. C-98 provides a ground path for the audio when $S-4$ is in the OFF position.
b. AUDIO AMPLIFIERS. The audio section consists of two stages of voltage amplification (both halves of the dual triode $V-13$, a 12AT7) and a 6AQ5 power amplifier. The AF GAIN Control is located in the grid circuit of the first stage. Fixed bias from the bias rectifier is applied to the grid of the power amplifier. The output transformer secondary consists of a 500 -ohm winding suitable for driving auxiliary apparatus and a four-ohm winding for use with loudspeaker voice coil and headphones. When a headphone is plugged into the headphone jack J-2, the speaker connection is interrupted and a 10 -ohm load resistor is connected in parallel with the headphone to keep the output transformer properly loaded.

## 5. RF GAIN CONTROL SYSTEM.

The RF gain control system in the 75A-4 works in conjunction with the AVC system. To control the sensitivity of the set, a source of fixed bias is added to the AVC voltage which is then applied to the A VC controlled tubes. This system maintains the gain distribution constant throughout all settings of
the gain control. A low impedance type AVC line is employed. In order to prevent the RF GAIN Control from affecting the characteristics of the line due to loading an RF gain gate is employed to decouple the RF GAIN Control from the AVC line. This gate is in the form of $1 / 2$ of a type 6AL5 twin diode, Y-19. The other half of the tube is employed as a bias rectifier.

Bias from this bias rectifier is connected to one end of the RF GAIN Control. The arm of the control is connected to the AVC line through the RF gain gate, V-19 (pins 1 and 7). Advancing the control adds negative bias to the AVC bias and reduces the gain of the tubes connected to the AVC line, namely, V-2, V-6, V-8 and V-9.

## 6. "S" METER.

The " S " meter is connected in a bridge circuit between the screen grids of $V-6$ and $V-8$ and the cathode of V-8. These are IF amplifier tubes that are furnished with AVC voltage. A reference voltage is developed at the negative terminal of the "S" meter by the cathode current flow of V-8. This reference voltage is adjusted under no-signal conditions to a value equal to that developed at the positive terminal of the "S" meter by the two IF amplifier screen-grid voltages. The presence of a signal in the IF strip causes an AVC voltage to be developed which reduces the screen grid current of the two IF amplifiers, causing the screen-grid voltage on these tubes to increase. This increase in voltage is applied to the positive terminal of the " S " meter to produce an " S " meter reading proportional to the strength of the incoming signal. R-41 adjusts the " S " meter sensitivity.

## 7. AVC SYSTEM.

A low impedance AVC line is employed to minimize blocking on strong signals. The RF amplifier V-2 and the 455 KC IF amplifiers V-6, V-8 and V-9 are all AVC controlled. A stage of IF amplification V-21, separate from the signal IF amplifier, is employed to amplify the IF signal for rectification for AVC voltage. The IF amplified IF voltage is rectified by $1 / 2$ of $\mathrm{V}-16$, a twin diode. The other half of $V-16$ is used as an AVC noise clipper. This tube clips sharp noise impulses from the AVC voltage and thus prevents the noise from desensitizing the AVC circuit. A small positive DC voltage is applied to the AVC rectifier through $R-86$ to produce an AVC delay so that the AVC is ineffective on weak signals. A network of load resistors is switched by switch S-5 to select either fast or
slow AVC characteristics. C-110 provides RF filtering for the AVC detector output, R-89, R-91 and R-92 are the detector loads. R-90 and C-112 provide the AVC time constant with R-92 and R-91 modifying the time constant for slow and fast AVC operation. AVC test point J-4 is provided for use in aligning the AVC IF amplifier transformer T-4. Each controlled stage is decoupled from the AVC line by suitable capacitors and resistors to prevent instability because of RF feedback.

## 8. CALIBRATOR CIRCUIT.

The calibrator employs a 6BA6 tube in a crystal controlled oscillator circuit. The fundamental frequency of the oscillator is 100 KC , therefore, a harmonic appears at each 100 KC point over the entire range of the receiver when the calibrator is turned on. C-1 is used to zero beat a calibrator harmonic with a 1500 KC or 1600 KC broadcast station or with WWV at $2.5,15$ or 30 MC . The calibrator output is coupled to the receiver input by $\mathrm{C}-5$. The calibrator is turned on wherever S-6 is in the CAL position.

## SECTION V MAINTENANCE

## 1. TROUBLE SHOOTING.

The table of voltage measurements located at the end of the alignment procedure will help in locating troubles which might arise in the 75A-4. Most normal receiver troubles such as burned-out tubes,
loose connections, noisy volume controls etc., are easily discovered and remedied. However, should more obscure troubles arise, only a trained and and competent repairman should be allowed to service the receiver. The following table gives a few possible causes for failure that might be associated with tubes having unusual functions.

| TUBE | FUNCTION | SYMPTOM | CAUSE AND REMEDY |
| :---: | :---: | :---: | :---: |
| V-7 | "Q" Mult. | Insufficient rejection notch. Notch not centered on dial when signal is centered in passband. | Realign L-26 and L-36 per part 6. Set panel control to midscale and adjust L-26 for notch. |
| V-10 | MUTING DIODE | Insufficient muting. | Check muting voltage; should be +20 volts for 40 db muting. |
| V-11 | $\begin{aligned} & \text { SSB-CW } \\ & \text { DET } \end{aligned}$ | Hum level high. | Heater-cathode leakage in V-11 or V-20. Replace tube. |
| V-12 | NOISE <br> LIMITER | Excessive hum. | Heater cathode leakage in V-12. Try new tube. |
| V-21 | AVC AMPLR | Insufficient AVC. | Bad tube or misalignment of $\mathrm{T}-4$. Leaky AVC by-pass. |
| V-19 | RF GAIN GATE | AVC action but no RF GAIN Control action. | Replace tube. |
| V-19 | $\begin{aligned} & \text { BLAS } \\ & \text { RECTIFIER } \end{aligned}$ | Excessive distortion. | Low bias voltage. Try new tube. |

## 2. FUSE.

The 75A-4 is supplied with a 2 ampere fuse. If the fuse blows, do not replace it until the trouble has been determined and remedied. Use only a type $3 A G$ fuse of 2 ampere capacity.

## 3. TEST EQUIPMENT REQUIRED FOR 75A-4 ALIGNMENT.

a. Signal generator.
b. Vacuum tube voltmeter.

## 4. PRELIMINARY CHECKS.

a. 2 ampere fuse in holder.
b. Output voltage of power supply at approximately $170-\mathrm{V}$. (Measure at $\mathrm{C}-94 \mathrm{~B}$ to ground.) Unless specifically changed in the following procedures, keep the following controls in the positions noted:

## PASSBAND TUNING to 0

NOISE LIMITER to OFF

## REJECTION TUNING to 0

## SELECTIVITY to 3 KC FILTER

OFF-STANDBY-ON CAL to ON

## 5. 455 KC IF ALIGNMENT.

a. Set the REJECTION TUNING Control to OFF, RF GAIN to maximum, the AM CW'-SSB switch to AM, the AVC switch to FAST and the OFF-STANDBY-ON CAL switch to ON.
b. Connect the lead from the signal generator to pin 1 of $\mathrm{V}-9$, and tune the signal generator to 455 KC .
c. Connect the VTVM to the AVC TEST POINT.
d. Increase the signal generator level until an increase above the static level is noted on the I'TVM.
e. Adjust tuning cores of T-4 for a m:ximum indication on the VTVM.
f. Connect VTVM to DIODE LOAD T\&:ST PONT and set AVC switch to OFF.
g. Adjust tuning cores of T-3 for a maximum indication on the VTVM.
h. Connect signal generator to pin 1 of $v \cdot a$.
i. Adjust L-27 for maximum indication on VTVM.

## 6. REJECTION TUNING ALIGNMENT.

a. BFO (PASSBAND TUNING) must be in good alignment (see paragraph 7. below).
b. Unlock DIAL DRAG and set up receiver for calibrate. set PASSBAND TUNING to " 0 ". and REJECTION TUNING to center mark.
c. Tune KILOCYCLE dial to zero beat with calibrate signal.
d. Tune L-26 slug to center of sharp dip in "S" meter, adjust R-36 for deepest dip then back off slightly.
e. Move KILOCYCLES dial exactly 1 KC and check with REJECTION TUNING knob to see that null occurs 1 KC to one side of center. Each small division of REJECTION TUNING scale is approximately 0.5 KC .

## 7. BFO ALIGNMENT.

There are several conditions that might cause a need for adjustment of the BFO.

The first is where a slight drift of frequency produces a need for resetting the BFO to frequency.

The second is where the front panel has been removed and where the BFO knob (BANDPASS TUNING) has been removed from the shaft.

The third condition is where the BFOcoil assembly has been replaced and a tracking problem exists.
a. SIMPLE ALIGNMENT. Where simple alignment of BFO frequency is concerned:
(1) Turn REJECTION TUNING to OFF, set AM CW-SSB to AM. Select 3-KC filter. Select FAST AVC.
(2) Set OFF-STANDBY-ON CAL switch to CAL.
(3) Tune in a calibration signal with KILOCYCLES DIAL to exact center of passband by watching "S" meter. (Refer to paragraph 3a. (2) in section III.)
(4) Set PASSBAND TUNING to 0.
(5) Remove plug from top of BFO can and adjust inductance slug for zero beat.
b. Where the front panel or BANDPASS TUNING knob has been removed and the calibration of the BANDPASS TUNING knob has been lost:
(1) If the tracking between the VFO and the BFO has not been disturbed, merely set the VFO frame so that the tubes are straight up, tune in a CAL signal to zero beat and put the BANDPASS TUNING knob on shaft with the marker on zera. Tighten the setscrews.
(2) If the tracking between the VFO and BFO has been disturbed, (BFO shaft out of track at the flexible coupler or at the metal belt pulley) see the paragraphs below.
c. Where the BFO coil assembly has been replaced and complete tracking is necessary:
(1) The new BFO coil is very nearly aligned when it is purchased i.e., the trimmer capacitor and coil slug are set to produce 455 KC at the correct position in the pitch control capacitor C-117 and a blue dot is painted at the root of the shaft of $\mathrm{C}-117$ to use in initially positioning $\mathrm{C}-117$.
(2) After the BFO coil is properly connected, connect up the metal belt but allow the pulley to remain free on the BFO shaft.
(3) Set the VFO frame with the tubes straight up and tune in a CAL signal to dead center on the KILOCYCLES dial and set the DIAL SET to 0 .
(4) Turn the AM CW-SSB Control to CW-SSB and turn the BFO shaft to zero beat with the blue dot upward.
(5) Set the PASSBAND knob to zero and tighten its setscrews.
(6) Tighten the setscrews in the pulley.
(7) Set DIAL DRAG.
(8) Turn the PASSBAND TUNING Control through its range and see if the BFO tone stays at reasonably close to zero beat throughout the ranf". If an error of over 50 cps is experienced. theBFO can be retracked as follows:

## NOTE

Because the following procedure is diffluall do not attempt it unless the BFO trackink error is really objectionable.
(9) Use 6 KC filter, setup for CW oper:ation. tune PASSBAND TUNING to 0 and tune in a CAl. signal to zero beat with KILOCYCLES diai on the. 160-meter band.
(10) Peer down in the BFO can and note thepositions of the two trimmer adjustment slots. Make a drawing if necessary.
(11) Turn the inductance trimmer ( $\mathrm{L}-31$ ) 10 degrees or so clockwise.
(12) Return to zero beat by turning the trimmer capacitor C-118.
(13) Now offset the KILOCYCLES dial on the low frequency side of 0 until a very low frequency tone is produced.
(14) Tune the PASSBAND TUNING Control through its range and see if the tone error is any better. (The change will be only in the order of a few cps so frequency measuring equipment should be used if available.)
(15) If the results are favorable return the KILOCYCLE dial to zero beat and repeat steps 11 through 14.
(16) If the error is greater, return the trimmers ( $\mathrm{L}-31$ and $\mathrm{C}-118$ ) to their original positions and repeat steps 12 through 14 except turn the inductance trimmer $\mathrm{L}-31$ in the other, or counterclockwise, direction.
(17) Repeat the alignment procedure until no better results can be obtained. The error should now be less than 50 cps .

## NOTE

An error produced by backlash is possible. This error must not be included when checking for alignment, therefore when the end stops of the PASSBAND TUNING knob are reached, back up the knob very slightly to take up the backlash.

## NOTE

It should be possible to swing the BANDPASS TUNING knob 2.5 KC each side of ( $\mathbf{W}$ nter without being stopped either by the VFO frame hitting the chassis or by the BFO shaft end stops. If either of these occur, reset the BFO end stops and BANDPASS TUNING knob as required and reset the BFO frequency to zero beat with $\mathrm{L}-31$.

## 8. VARIABLE IF AND 160-METER BAND ALIGNMENT.

a. Connect signal generator to antenna input through a 100 -ohm dummy antenna, and connect VTVM to DIODE LOAD test point.
b. Cunnect audio output meter to audio terminals 500 and $G$ and rear of receiver.
c. Set AM CW-SSB switch to AM, AUDIO GAIN to maximum, and RF GAIN to maximum. Select 3 KC mechanical filter.
d. Set receiver dial and signal generator to 1.6 MC. and adjust tuning slugs $\mathrm{L}-18, \mathrm{~L}-22$, and $\mathrm{T}-1$ for maximum output indication.
e. Set receiver dial and signal generator to 2.4 MC. and adjust capacitor $\mathrm{C}-7, \mathrm{C}-53$, and $\mathrm{C}-56$ for maximum output.
f. Repeat steps d. and e. until no further increase is noted in output.

## 9. ALIGNMENT OF CRYSTAL OSCILLATOR.

a. Connect VTVM through a 1 megohm resistor to pin 2 of $\mathrm{V}-3$. Turn $\mathrm{AM} \mathrm{CW}-\mathrm{SSB}$ to AM .
b. Set BAND switch to 80 and adjust L-12 for maximum output indication.
c. Successively change BAND switch to 40,20 , $15,11,10,10$ and adjust L-13, L-14, L-15, L-16, $\mathrm{L}-17$, and $\mathrm{L}-11$ in that order for a maximum output indication. Adjust L-13 core one-quarter turn into coil from peaked position.
d. The frequency of the crystals may be adjusted over a limited range by the adjustments of steps $b$. and c. After other alignment operations are completed, this method may be used to reduce the calibration error between bands.
e. Turn on the CAL oscillator ( 100 KC crystal standard) being sure it is on frequency. (See part 5 of section II for adjustment), and tune the receiver to zero beat at exactly 2.0 MC .

## NOTE

Do not turn tuning dial or PASSBAND TUNING during the remainder of this adjustment.
f. Turn BAND switch successively to the remaining bands, and adjust the receiver to zero beat by repeating steps $b$. and $c$. Be sure that the crystal oscillator does not stop oscillating or does not start oscillating at a spurious frequency.

## 10. RF ALIGNMENT.

a. Connect signal generator to antenna terminals on receiver, and VTVM to DIODE LOAD test point.
b. Rotate BAND switch to 160 , and tune signal generator and receiver to 1.6 MC .
c. Adjust tuning core in T-1 for maximum diode load voltage.

## NOTE

ANT TRIM shall be set to half capacity while aligning all bands.
d. Tune the signal generator and receiver to 2.4 MC, and adjust capacitor $\mathrm{C}-7$ for maximum diode load voltage.
e. Repeat steps c. and d. until no further increase in output is noted. If the 160 -meter coil was aligned along with the 1.5 to 2.5 MC IF, disregard the above and proceed with the remainder of the bands.
f. Repeat steps c., d., and e. for the other bands using the following table as a guide.

| BAND | RECEIVER AND <br> SIG. GEN. FREQ. <br> LOW END | RF <br> "L" | ANT <br> "L" | RECEIVERAND <br> SIG. GEN. FREQ. <br> HIGH END | RF <br> "C" | ANT <br> "C" |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 160 | 1.6 | - | $\mathrm{T}-1$ | 2.4 | - | $\mathrm{C}-7$ |
| 80 | 3.3 | $\mathrm{~L}-6$ | $\mathrm{~T}-2$ | 4.1 | $\mathrm{C}-23$ | $\mathrm{C}-8$ |
| 40 | 6.9 | $\mathrm{~L}-7$ | $\mathrm{~L}-1$ | 7.7 | $\mathrm{C}-26$ | $\mathrm{C}-11$ |
| 20 | 14.1 | $\mathrm{~L}-8$ | $\mathrm{~L}-2$ | 14.9 | $\mathrm{C}-28$ | $\mathrm{C}-13$ |
| 15 | 20.9 | $\mathrm{~L}-9$ | $\mathrm{~L}-3$ | 21.7 | $\mathrm{C}-30$ | $\mathrm{C}-15$ |
| $* 11$ | 27.1 | - | - |  | $\mathrm{C}-31$ | - |
| $* 10$ | 28.1 | $\mathrm{~L}-10$ | $\mathrm{~T}-7$ | 28.9 | $\mathrm{C}-32$ | $\mathrm{C}-16$ |
| $* 10$ | 29.5 |  |  |  | $\mathrm{C}-17$ |  |

*In performing the alignment of the 11 and the two 10 -meter bands, a specific sequence is necessary. First, align the 28 to 29 MC band in the normal manner with the ANT TRIM at midscale. The 26.5 to 27.5 MC band and the 29 to 30 MC bands are aligned at one point only by RF trimmers, $\mathrm{C}-31$ and $\mathrm{C}-17$. It is necessary to retune the ANT TRIM for resonance on these bands since no alignment trimmers are provided in the antenna circuit. Any retuning of L-10 after alignment will affect the tracking of bands 11,10 and 10 .

## 11. VFO ADJUSTMENT.

The VFO is calibrated at the factory and should require adjustment at only widely separated intervals. If the calibration error becomes excessive for operation or beyond the point where the vernier dial corrector (ZERO SET Control) can correct, the following procedure should be followed to make correcting adjustments:
a. Use the $100 \mathrm{KC} / \mathrm{s}$ calibrator. Allow the receiver to warm up from 1 to 2 hours.
b. Set the BAND CHANGE switch to the 160 -meter band. Tune KILOCYCLES dial to $1.5 \mathrm{MC} / \mathrm{s}$. Set up in accordance with paragraph 8 of OPERATION section to zero beat with calibrator signal. Note the dial reading if fiducial line cannot be set to 0 .
c. Rotate KILOCYCLES dial to $2.5 \mathrm{MC} / \mathrm{s}$ and exactly tune until zero beat is obtained. Do not readjust BFO or ZERO SET Control. The calibration error is then the number of dial divisions more or less than the 10 turns it should take to cover the range. Usually, the error tends to be toward more rotation of the KILOCYCLES dial than the 10 turns that should be required. To correct this error, proceed as follows:
(1) Rotate the KILOCYCLES dial towards and through dial zero until a total of 1.8 times the dial division error has been counted. Engage the trimmer adjusting stud with a strong thin wire and turn until zero beat is restored. The ZERO SET adjustment can now be rotated so that the ZERO SET is set to dial zero.
(2) To check the accuracy of the adjustment retune the KILOCYCLES dial to $1.5 \mathrm{MC} / \mathrm{s}$ and check the calibration error. If the adjustments have been done carefully less than $1 / 2$ division dial error will be found. The above procedure can be repeated until satisfactory results are obtained. This endpoint adjustment restores factory accuracy to the intermediate points, also.
(3) If it is desired to recenter the dial vernier pointer the following additional procedure should be followed. Set the ZERO SET Control to midscale. loosen the two setscrews of the VFO dial-shaft coupler and carefully turn the oscillator shaft until zero beat is obtained. During the VFO adjustment, best results in frequency readings will be obtained if the AVC is OFF and the RF GAIN Control is used at a low value.

## 12. TWEET TRAP ADJUSTMENT.

a. A third order tweet appears at 3.533 MC in the 80 -meter band caused by the 5.7 crystal beating with the second harmonic of the VFO at the mixer V-5.
b. Turn the AM CW-SSB switch to CW-SSB and tune in the tweet.
c. Adjust the core of $\mathrm{L}-23$ until the level of tweet is minimum.

## 13. AVC THRESHOLD (R-9).

a. Connect VTVM to A VC test point and ground and set range switch to 5 -volt range.
b. Set RF GAIN to maximum. Select FAST AVC.
c. Feed a 29.5 MC signal from a signal generator into the antenna terminals using a 100 -ohm resistor in series with the signal generator.
d. Tune in the signal "on the nose".
e. Increase the input signal until a definite increase in AVC voltage is noted and record the input.
f. Adjust R-9 so that the AVC threshold occurs with 3 uv input.

## 14. DIAL CORDS.

The front panel must be removed for replacement of the dial pointer cord or the drum rotator cord. Figure 5-1 shows both cords in place and the direction in which the restringing should proceed.
a. REMOVING FRONT PANEL. (See figure 5-4).
(1) Remove the six panel screws.
(2) Remove the following knobs:

## REJECTION TUNING

## SELECTIVITY

PASSBAND TUNING (see CAUTION below)

## ANT TRIM

BAND CHANGE

## KILOCYCLES TUNING



## CAUTION

Set the PASSBA ND TUNING Control knob on the index mark (straight up) and do not move the control after the knob has been removed. If the control has been accidently moved, see part 7 for instructions for adjusting the knob position.
b. POINTER CORD. Obtain a type 432101800 Collins Dial Cord.
(1) Scribe a mark on the VFO shaft and the KILOCYCLES dial hub to mark their relative positions and remove the KILOCYCLES dial.
(2) Turn the tuning knob to the clockwise stop.
(3) Start at point X in the drawing with the cord hooked to one end of the spring (part number of spring is 5031240001 ).
(4) Bring cord around pulley C to pulley B.
(5) Wrap around pulley B clockwise, through the deep slot, around the tab, and back through the shallow slot. Wrap around pulley B two times clockwise.
(6) Wrap cord around pulley A and loop the end on the free end of the spring.
(7) Fasten the pointer to the cord, tune in a station of known frequency and adjust the pointer to the correct setting.
(8) Replace the KILOCYCLES tuning dial. Match up the scribe marks (see step (1) and tighten setscrews.
(9) Replace the panel.
c. DRUM CORD. Obtain a 432102000 Collins Dial Cord.
(1) Turn the band switch to the $1.5-2.5 \mathrm{MC}$ band (pulley D at counterclockwise stop).
(2) Turn pulley E approximately one turn and hold the tension spring taut.
(3) Make approximately $3 / 4$ turn around pulley D and hook cord to tab.
(4) Extend the cord around pulley E and hook to the tab. Release the tension spring.
(5) Replace the panel.
(6) Loosen the setscrew in the drum hub opposite the coil tension spring, and align the dial calibration to the $1.5-2.5 \mathrm{MC}$ band. Then tighten the setscrew.

TABLE 5-1. VOLTAGE, AND RESISTANCE MEASUREMENTS
Pin Number

| TUBE |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | $\begin{gathered} \text { PLATE } \\ \text { CAP } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V-1 | $\begin{aligned} & \text { DC V. } \\ & \text { AC V. } \\ & \text { Ohms } \end{aligned}$ | $\mid-22.5$ <br> 680K | $\begin{array}{r} 7.5 \\ 4700 \end{array}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | 6.3 | 88 <br> 00 |  | 8 <br> 4700 |  |  |  |
| V-2 | $\left\lvert\, \begin{aligned} & \text { DC V. } \\ & \text { AC V. } \\ & \text { Ohms } \end{aligned}\right.$ | $\begin{gathered} -5.7 \\ 1.5 \\ \mathrm{meg} \end{gathered}$ | 0 <br> 0 | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | 6.3 | $190$ <br> 20K | $175$ <br> 50K | 0 <br> 0 |  |  |  |
| V-3 | $\begin{array}{\|l} \text { DC V. } \\ \text { AC V. } \\ \text { Ohms } \end{array}$ | $140$ $22 \mathrm{~K}$ | $\begin{aligned} & -2.7 \\ & 25 \mathrm{~K} \end{aligned}$ | $\begin{array}{r} 2.3 \\ 120 \end{array}$ | 6.3 | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $0$ $0$ | $\begin{gathered} 0 \\ 510 \mathrm{~K} \end{gathered}$ | $0$ $0$ | $190$ <br> 21K |  |
| V-4 | $\begin{aligned} & \text { DC V. } \\ & \text { AC V. } \\ & \text { Ohms } \end{aligned}$ | $\begin{aligned} & 175 \\ & 21 \mathrm{~K} \end{aligned}$ | $0$ $0$ | $\begin{array}{r} 1.5 \\ 330 \end{array}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $175$ $21 \mathrm{~K}$ | $-2.6$ <br> 10.5 K | $\begin{aligned} & 1.8 \\ & 330 \end{aligned}$ | 6.3 |  |
| V-5 | $\begin{array}{\|l} \text { DC V. } \\ \text { AC V. } \\ \text { Ohms } \end{array}$ | $\begin{array}{r} 105 \\ 27 \mathrm{~K} \end{array}$ | $\begin{aligned} & -3.8 \\ & 100 \mathrm{~K} \end{aligned}$ | $1$ $68$ | 6.3 | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | 0 <br> 0 | 0 <br> 0 | 0 <br> 0 | $190$ <br> 21K |  |

TABLE 5-1. VOLTAGE, AND RESISTANCE MEASUREMENTS (Cont.)
Pin Number

| TUBE |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | PLATE <br> CAP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V-6 | DC V. <br> AC V. <br> Ohms | -2.8 | 0 | 1.8 | 0 | 0 | 6.3 | 20 | 100 | $* 4$ |  |

TABLE 5-1. VOLTAGE, AND RESISTANCE MEASUREMENTS (Cont.)
Pin Number

| TUBE |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | $\begin{gathered} \text { PLATE } \\ \text { CAP } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| V-18 | $\begin{aligned} & \text { DC V. } \\ & \text { AC V. } \\ & \text { Ohms } \end{aligned}$ | $0$ $00$ | $0$ $0$ | $\begin{array}{r} 0 \\ 00 \end{array}$ | $\begin{array}{r} 0 \\ 00 \end{array}$ | $\begin{aligned} & 160 \\ & 23 \mathrm{~K} \end{aligned}$ | 0 <br> 00 | 0 <br> 00 |  |  |  |
| V-19 | $\begin{aligned} & \text { DC V. } \\ & \text { AC V. } \\ & \text { Ohms } \end{aligned}$ | $\begin{aligned} & \hline * * * * \\ & -38.5 \\ & 600 \end{aligned}$ | $-135$ <br> 30K | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | 6.3 | $\begin{gathered} 120 \mathrm{AC} \\ 0 \end{gathered}$ | $0$ $00$ | $\begin{aligned} & -38.5 \\ & 300 \mathrm{~K} \end{aligned}$ |  |  |  |
| V-20 | $\begin{aligned} & \text { DC V. } \\ & \text { AC V. } \\ & \text { Ohms } \end{aligned}$ | $\begin{array}{\|c\|} \hline-5 \\ 150 \mathrm{~K} \end{array}$ |  | 6.3 | $\begin{aligned} & 0 \\ & 0 \\ & 0 \end{aligned}$ | 14 <br> 10K | $\begin{aligned} & 42.5 \\ & 00 \end{aligned}$ | 0 <br> 0 |  |  |  |
| V-21 | $\left.\begin{array}{\|c} \text { DC V. } \\ \text { AC V. } \\ \text { Ohms } \end{array} \right\rvert\,$ | $\begin{gathered} 0 \\ 1 \\ \text { meg } \end{gathered}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | $6.3$ | $185$ <br> 22 K | 75 <br> 82K | $\begin{aligned} & 1.3 \\ & 150 \end{aligned}$ |  |  |  |
| V-22 | $\begin{array}{\|l} \mathrm{DC} \text { V. } \\ \text { AC V. } \\ \text { Ohms } \end{array}$ | $\begin{array}{\|l\|} -11 \\ 168 \mathrm{~K} \end{array}$ | $0$ $0$ | $\begin{aligned} & 0 \\ & 0 \end{aligned}$ | 6.3 | $220$ $21 \mathrm{~K}$ | $205$ $20 \mathrm{~K}$ | $\begin{aligned} & -11 \\ & 168 \mathrm{~K} \end{aligned}$ |  |  |  |

NOTES:

1. AVC in OFF position.
2. Unless otherwise indicated RF GAIN adjusted until "S" meter needle rests at S-9 with no signal input.

* Depends upon setting of R-9.
** Depends upon setting of R-67.
*** AM CW-SSB at CW-SSB; NOISE LIMITER (R-67) at 1.
**** RF GAIN to 0 .


Figure 5-1. Dial Cord Replacement


Figure 5-2. 75A-4, Top View


Figure 5-3. 75A-4, Bottom View, Page 1


Figure 5-3. 75A-4, Bottom View, Page 2


Figure 5-4. 75A-4, Front Panel Lowered



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WITH CLAMP IN PLACE, TRIM BRAID AS SHOWN

FOLD COPPEF BRAID BACK ON CLAMP TIN CENTER CONDUCTOR. USING MINIMUM AMOUNT OF HEAT.

HOLDING CONTACT WITH PLIERS SOFT SOLDER CONTACT TO CENTER CONDUCTOR. IT IS /MPERATIVE THAT BACK END OF CONTACT BE FLUSH WITH POLYETHYLENE DIELECTRIC. DO NOT USE EXCESS SOLDER WIPE CLEAN-SEE THAT END OF CABLE INSULATOR IS CLEAN AND FREE OF SOLDER. ROSIN AND FOREIGN MATERIAL

SLIDE BODY INTO PLACE CAREFULLY SO THAT CENTER CONDUCTOR ENTERS HOLE IN INSULATOR FACE OF CABLE DIELECTRIC MUST FIT FLUSH AGAINST INSULATOR, PROPERLY TIGHTEN BODY AND NUT WITH WRENCHES

Figure 5-6. Assembling Plug UG-21B/U to Cable RG-8/U


PRE-SELECTION COILS ON I6OMC
BAND

## SECTION VI PARTS LIST FOR 75A-4 RECEIVER

TABLE 6-1

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS <br> PART NUMBER |
| :---: | :---: | :---: | :---: |
| C-1 | Calibration Oscillator frequency adjuster | CAPACITOR, variable: ceramic; $\mathbf{5 - 2 5} \mathrm{mmf}$; 350 wv | 917107300 |
| C-2 | V-1 Cathode bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$; 500 wv | 913118800 |
| C-3 | V-1 Screen bypass | CAPACITOR: mica; $200 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912051900 |
| C-4 | V-1 plate decoupling | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-5 | Calibration signal coupling | CAPACITOR: ceramic; $1 \mathrm{mmf}, \pm 1 / 4 \mathrm{mmf}$, 500 wv | 916007000 |
| C-6 | Padder for T-1 | C.\PACTTOR: mica; $390 \mathrm{mmf}, \pm 2 \%, 500 \mathrm{wv}$ | 912053500 |
| C-7 | Trimmer for T-1 | C゚PACITOR, variable: ceramic; $\mathbf{8 - 5 0} \mathbf{m m f}$; 3', w. | 917107500 |
| C-8 | Trimmer for T-2 | C...PACITOR, variable: ceramic; $8 \mathbf{- 5 0} \mathbf{m m f}$; $3: 10 \mathrm{wv}$ | 917107500 |
| C-9 | Padder for T-2 | CAPACITOR: mica; $650 \mathrm{mmf}, \pm 2 \%, 500 \mathrm{wv}$ | 912054800 |
| C-10 | Padder for L-1 | CAPACITOR: mica; $300 \mathrm{mmf}, \pm 5 \%, 500 \mathrm{wv}$ | 912052700 |
| C-11 | Trimmer for L-1 | CAPACITOR, variable: ceramic; $8 \mathbf{- 5 0} \mathbf{m m f}$, 350 wv | 917107500 |
| C-12 | Padder for L-2 | CAPACITOR: mica; $120 \mathrm{mmf}, \pm 10 \%$; 500 wv | 912050100 |
| C-13 | Trimmer for L-2 | CAPACITOR, variable: ceramic; $8 \mathbf{- 5 0} \mathbf{m m f}$, 350 wv | 917107500 |
| C-14 | Padder for L-3 | CAPACITOR: mica; $68 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912048300 |
| C-15 | Trimmer for L-3 | CAPACITOR, variable: ceramic; 8-50 mmf, 350 wv | 917107500 |
| C-16 | Trimmer for T-7 | CAPACITOR, variable: ceramic; $\mathbf{5 - 2 5} \mathbf{~ m m f}$, 350 wv | 917107300 |
| C-17 | Trimmer for L-10 | CAPACITOR, variable: ceramic; 5-25 mmf, 350 wv | 917107300 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS <br> PART NUMBER |
| :---: | :---: | :---: | :---: |
| C-18 | Antenna Trimmer | CAPACITOR, variable: air; 2.6-19.7 mmf | 922003300 |
| C-19 | V-2 grid blocking | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 10 \%$, 500 wv | 912049500 |
| C-20 | V-2 grid decoupling | CAPACITOR: paper; . $1 \mathrm{mmf}, \pm 10 \%$, 400 wv | 931029900 |
| C-21 | V-2 screen bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-22 | Padder for T-7 | CAPACITOR: mica; $24 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912045000 |
| C-23 | Trimmer for L-6 | CAPACITOR, variable: ceramic; $8-50 \mathrm{mmf}$, 350 w | 917107500 |
| C-24 | Padder for L-6 | CAPACITOR: mica; $650 \mathrm{mmf}, \pm 20 \%$, 501 w | 912054800 |
| C-25 | Padder for L-7 | CAPACITOR: mica; $270 \mathrm{mmf}, \pm 5 \%$, :OW: W | 912052400 |
| C-26 | Trimmer for L-7 | C\VけrПいH. variable: ceramic; $8-50 \mathrm{mmf}$, 3:\% w | 917107500 |
| C-27 | Padder for L-8 | CAPACTINH mica; $130 \mathrm{mmf}, \pm 2 \%, 500 \mathrm{wv}$ | 912050200 |
| C-28 | Trimmer for L-8 | CAMACITON. variable: ceramic; $8-50 \mathrm{mmf}$, 3:" | 917107500 |
| C-29 | Padder for L-9 | CAPACITOR: mica; $68 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912048300 |
| C-30 | Trimmer for L-9 | CAPACITUR, variable: ceramic; $8-50 \mathrm{mmf}$, 350 wv | 917107500 |
| C-31 | Trimmer for L-10 | CAPACTTOR, variable: ceramic; $5-25 \mathrm{mmf}$, 350 wv | 917107300 |
| C-32 | Trimmer for L-10 | CAPACITOR, variable: ceramic; $5 \mathbf{- 2 5} \mathbf{~ m m f}$, 350 wv | 917107300 |
| C-33 | V-2 plate decoupling | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$. 500 wv | 913118800 |
| C-34 | V-3 grid blocking | CAPACTTOR: mica; $100 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912049500 |
| C-35 | V-3 cathode bypass | CAPACITOR: ceramic; $.01 \mathrm{mf},+100-20 \%$. 500 wv | 913118800 |
| C-36 | V-3 screen bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$. 500 wv | 913118800 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS <br> PART NUMBER |
| :---: | :---: | :---: | :---: |
| C-37 | V-3 injection coupling | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912049500 |
| C-38 | V-4 plate feedback | CAPACITOR: mica; $220 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912051900 |
| C-39 | Padder for L-18 | CAPACITOR: mica; $47 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912047100 |
| C-40 | Padder for L-12 | CAPACITOR: mica; $220 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912051900 |
| C-41 | Padder for L-13 | CAPACITOR: mica; $120 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912050100 |
| C-42 | Padder for L-14 | CAPACITOR: mica; $120 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912050100 |
| C-43 | Padder for L-15 | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912049500 |
| C-44 | Padder for L-16 | CAPACITOR: mica; $56 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912047700 |
| C-45 | Padder for L-17 | CAPACITOR: mica; $47 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912047100 |
| C-46 | V-4 plate decoupler | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-47 | Padder for L-18 | CAPACITOR: mica; $330 \mathrm{mmf}, \pm 5 \%, 500 \mathrm{wv}$ | 912053000 |
| C-48 | V-3 plate decoupler | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-50 | Padder for L-10 | CAPACITOR: mica; $39 \mathrm{mmf}, \pm 10 \%$, 500 wv | 912046500 |
| C-51 | Padder for L-11 | CAPACITOR: mica; $47 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912047100 |
| C-52 | Coupler for L-18 and $\mathrm{L}-22$ | CAPACITOR: ceramic; $4 \mathrm{mmf}, \pm 1 / 2 \mathrm{mmf}$, 500 wv | 916011400 |
| C-53 | Trimmer for L-18 | CAPACITOR, variable: ceramic; $8 \mathbf{- 5 0} \mathbf{~ m m f}$, 350 wv | 917107500 |
| C-54 | V-6 cathode bypass | CAPACITOR: paper; $.1 \mathrm{mf}, \pm 10 \%$, 150-200 wv | 931033300 |
| C-55 | Padder for L-22 | CAPACITOR: mica; $330 \mathrm{mmf}, \pm 5 \%, 500 \mathrm{wv}$ | 912053000 |
| C-56 | Trimmer for L-22 | CAPACITOR, variable: ceramic; $8 \mathbf{- 5 0} \mathrm{mmf}$, 350 wv | 917107500 |
| C-57 | Padder for L-22 | CAPACITOR: mica; $56 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912047700 |
| C-58 | Tweet trap series | CAPACITOR: mica; $270 \mathrm{mmf}, \pm 5 \%, 500 \mathrm{wv}$ | 912052400 |
| C-59 | V-5 cathode bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS PART NUMBER |
| :---: | :---: | :---: | :---: |
| C-60 | V-5 screen bypass | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$, 500 wv (p/o L-27) | 913118800 |
| C-61 | Mechanical filter padder | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 2 \%, 500 \mathrm{wv}$ | 912049300 |
| C-62 | V-5 plate decoupling | CAPACITOR: paper; . $1 \mathrm{mmf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-63 | B+ bypass | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-64 | Mechanical filter padder | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 2 \%, 500 \mathrm{wv}$ | 912049300 |
| C-65 | V-6 grid decoupler | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-66 | V-6 screen bypass | CAPACITOR: ceramic; $.01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-67 | V-6 plate decoupling | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-68 | V-6 plate to V-7 grid coupler | CAPACITOR: mica; $470 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912054300 |
| C-69 | External padder for L-27 | CAPACITOR: mica; $33 \mathrm{mmf}, \pm 20 \%$, 500 wv | 912045700 |
| C-70 | V-7 plate bypass | CAPACITOR: paper; $.1 \mathrm{mf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-71 | V-7 plate blocking | CAPACITOR: mica; $1000 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 935506700 |
| C-72 | Rejection filter tuning | CAPACITOR, variable: air; 2.6-19.7 mmf | 922003300 |
| C-73 | Padder for L-26 | CAPACITOR: mica; $1000 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 935506700 |
| C-74 | Padder for L-26 | CAPACITOR: mica, $1000 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 935506700 |
| C-75 | V-8 grid coupling | CAPACITOR: mica; $470 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912054300 |
| C-76 | V-8 grid decoupling | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-77 | V-8 cathode bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-78 | V-8 screen bypass | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-79 | V-8 plate decoupling | CAPACITOR: ceramic; $.01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-80 | Padder for L-27 | CAPACITOR: 100 mmf , part of L-27 |  |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS PART NUMBER |
| :---: | :---: | :---: | :---: |
| C-81 | V-9 grid coupling | CAPACITOR: mica; $470 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912054300 |
| C-82 | V-9 grid decoupling | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-83 | V-9 screen bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-84 | V-9 plate decoupling | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-85 | T-3 primary padder | CAPACITOR: 500 mmf , part of T-3 |  |
| C-86 | T-3 secondary padder | CAPACITOR: mica; $510 \mathrm{mmf}, \pm 5 \%, 300 \mathrm{wv}$ | 912054500 |
| C-87 | V-11 grid coupler | CAPACITOR: mica; $10 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912043200 |
| C-88 | T-3 secondary bypass | CAPACITOR: mica; $330 \mathrm{mmf}, \pm 5 \%, 500 \mathrm{wv}$ | 912053000 |
| C-89 | V-11 plate bypass | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-90 | V-11 load filter | CAPACITOR: mica; $220 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912051900 |
| C-91 | V-11 load filter | CAPACITOR: mica; $220 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912051900 |
| C-92 | V-11 grid coupler from BFO | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912049500 |
| C-93 | AM detector audio output coupler | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-94 ABC | C-94A-Plate supply filter C-94B-Plate supply filter C-94C-V-11 plate decoupling | CAPACITOR: electrolytic; $40 \mathrm{mmf},-15 \%$ $+100 \%, 300 \mathrm{wv}$ | 183111500 |
| C-95 | CW detector audio output coupler | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-96 | Noise limiter audio output coupler | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-97 | V-12 cathode bypass | CAPACITOR: paper; $.1 \mathrm{mmf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-98 | V-12 plate decoupler | CAPACITOR: paper; . $1 \mathrm{mmf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-99 | V-11 grid divider | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912049500 |
| C-100 | V-13 grid coupling | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS PART NUMBER |
| :---: | :---: | :---: | :---: |
| C-101 | V-22 grid coupling | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-102 | V-22 grid decoupling | CAPACITOR: paper; $1 \mathrm{mmf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-103 | V-22 plate stabilizing | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-104 | V-21 grid coupling | CAPACITOR: mica; $470 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912054300 |
| C-105 | V -21 cathode bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-106 | V-21 screen bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-107 | V-21 plate decoupling | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-108 | V-16 cathode filter | CAPACITOR: paper; . $1 \mathrm{mf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-109 | T-4 secondary tuning | CAPACITOR: mica; $510 \mathrm{mmf}, \pm 5 \%, 300 \mathrm{wv}$ | 912054500 |
| C-110 | V-16 cathode filter | CAPACITOR: mica; $330 \mathrm{mmf}, \pm 5 \%, 500 \mathrm{wv}$ | 912053000 |
| C-111 | V-16 plate bypass | CAPACITOR: paper; . $1 \mathrm{mf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-112 | AVC time constant | CAPACITOR: paper; . $1 \mathrm{mf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-113 | Bias supply filter | CAPACITOR: electrolytic; 50 mf , $+100-10 \%$, 150 wv | 183104500 |
| C-114 | V-9 cathode | CAPACITOR: ceramic; $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-115 | Bias bypass | CAPACITOR: paper; . $1 \mathrm{mmf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-116 | V -18 anode bypass | CAPACITOR: paper; $1 \mathrm{mmf}, \pm 10 \%, 400 \mathrm{wv}$ | 931029900 |
| C-117 | BFO tuning | CAPACITOR, variable: air; 6-75 mmf | 922015500 |
| C-118 | Trimmer for BFO | CAPACITOR, variable: air; 6-75 mmf | 922420000 |
| C-119 | Padder for BFO | CAPACITOR: mica; $1600 \mathrm{mmf}, \pm 1 \%, 250 \mathrm{wv}$ | 912128300 |
| C-120 | Padder for BFO | (p/o L-31) |  |
| C-121 | V-20 grid blocking | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 10 \%, 500 \mathrm{wv}$ | 912049500 |
| C-122 | V-20 plate decoupling | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS PART NUMBER |
| :---: | :---: | :---: | :---: |
| C-123 | V-20 screen bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-124 | B+ bypass | CAPACITOR: paper; $5 \mathrm{mmf},+20 \%,-10 \%$, 200 wv | 931016900 |
| C-125 | T-4 primary tuning | CAPACITOR: 500 mmf , part of T-4 |  |
| C-126 | 115-V line bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-127 | 115-V line bypass | CAPACITOR: ceramic; . $01 \mathrm{mf},+100-20 \%$, 500 wv | 913118800 |
| C-128 | V-20 feedback | CAPACITOR: ceramic; $4 \mathrm{mmf}, \pm 1 / 2 \mathrm{mmf}$, 500 wv | 916011400 |
| C-130 | Mech. filter primary tuning | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 2 \%, 500 \mathrm{wv}$ | 912049300 |
| C-131 | Mech. filter secondary tuning | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 2 \%, 500 \mathrm{wv}$ | 912049300 |
| C-132 | Mech. filter primary tuning | CAPACITOR: mica, $100 \mathrm{mmf}, \pm 2 \%, 500 \mathrm{wv}$ | 912049300 |
| C-133 | Mech. filter secondary tuning | CAPACITOR: mica; $100 \mathrm{mmf}, \pm 2 \%, 500 \mathrm{wv}$ | 912049300 |
| C-134 |  | Not Used |  |
| C-135 |  | (p/o L-31) |  |
| C-136 |  | (p/o L-31) |  |
| C-137 | Bias supply filter | CAPACITOR: electrolytic; $50 \mathrm{mf},+100 \%$, $-10 \%, 150 \mathrm{wv}$ | 183104500 |
| C-138 | Padder for C-31 | CAPACITOR: mica; $10 \mathrm{mmf}, \pm 5 \%, 500 \mathrm{wv}$ | 912043100 |
| C-139 | V-8 grid shunt | CAPACITOR: mica; $56 \mathrm{mmf}, \pm 5 \%, 500 \mathrm{wv}$ | 912047600 |
| C-140 | Tweet trap tuning | CAPACITOR: ceramic; $18 \mathrm{mmf}, \pm 5 \%, 500 \mathrm{wv}$ | 916418400 |
| E-1 | Antenna input connector | STRIP: terminal; 3 screw term on bakelite board | 306003300 |
| E-2 | V-2 grid suppressor | PARASITIC SUPPRESSOR: 47 ohm; \#24 bus wire | 504706400 |
| E-3 | Muting-standby connector | STRIP: terminal; 4 screw term on bakelite board | 306003400 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS PART NUMBER |
| :---: | :---: | :---: | :---: |
| E-4 | Audio output connector | STRIP: terminal; 4 screw term on bakelite board | 306003400 |
| F-1 | Primary fuse | FUSE: cartridge; $2 \mathrm{amp}, 250 \mathrm{v}$ | 264407000 |
| I-1 | Meter lamp | LAMP: part of M-1 |  |
| I-2 | KILOCYCLE dial bulb | LAMP: pilot light bulb w/ miniature bayonet base | 262324000 |
| I-3 | Megacycle dial bulb | LAMP: pilot light bulb w/ miniature bayonet base | 262026400 |
| I-4 | Megacycle dial bulb | LAMP: pilot light bulb w/ miniature bayonet base | 262026400 |
| J-1 | Antenna Coaxial input | CONNECTOR, receptacle: single round female contacts | 357900300 |
| J-2 | Headphone connector | JACK: phone; 2 circuit for 1/4" diam plug | 360002500 |
| J-3 | Diode load test | CONNECTOR, receptacle: single round female contact | 360006200 |
| J-4 | AVC test | CONNECTOR, receptacle: single round female contact | 360006400 |
| L-1 | 40 meter RF | COIL, RF: single wnd, single layer wnd, 18 turrs \#2\& AWG DS wire | 5047001001 |
| L-2 | 20 meter RF | COIL, RF: single wnd, single layer wnd, 9 turns \#28 AWG DS wire | 5046999001 |
| L-3 | 15 meter RF | COIL, RF: single wnd, single layer wnd, 7 turns \#28 AWG DS wire | 5046997001 |
| L-6 | 80 meter mixer | COIL, RF: single wnd, single layer wnd, 16 turns \#26 AWG DS wire | 5047037002 |
| L-7 | 40 meter mixer | COIL, RF: single wnd, single layer wnd, 18 turns \#28 AWG DS wire | 5047000001 |
| L-8 | 20 meter mixer | COIL, RF: single wnd, single layer wnd, 9 turns \#28 AWG DS wire | 5046999001 |
| L-9 | 15 meter mixer | COIL, RF: single wnd, single layer wnd, 7 turns \#28 AWG DS wire | 5046997001 |
| L-10 | 11-10-10 meter mixer | COIL, RF: single layer wnd, 6 turns @19 turns per inch | 540460800 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS <br> PART NUMBER |
| :---: | :---: | :---: | :---: |
| L-11 | 10 meter crystal (high freq.) | COIL, RF: 23, $31,33 \mathrm{mc}$; single wnd, single layer wnd, 5 turns \# 28 AWG DS wire | 5047001001 |
| L-12 | 80 meter crystal | COIL, RF: 5.7 mc , single wnd, single layer wnd, 16 turns \#28 AWG E wire | 5047004001 |
| L-13 | 40 meter crystal | COIL, RF: single wnd, single layer wnd, 12 turns \#28 AWG DS wire | 5046998001 |
| L-14 | 20 meter crystal | COIL, RF: single wnd, single layer wnd, 7 turns \#28 AWG DS wire | 5046997001 |
| L-15 | 15 meter crystal | COIL, RF: 23, $31,33 \mathrm{mc}$; single wnd, single layer wnd, 5 turns \#28 AWG DS wire | 5047001001 |
| L-16 | 11 meter crystal | COIL, RF: 23, $31,33 \mathrm{mc}$; single wnd, single layer wnd, 5 turns \#28 AWG DS wire | 5047001001 |
| L-17 | 10 meter crystal (low) | COIL, RF: $23,31,33 \mathrm{mc}$; single wnd, single layer wnd, 5 turns \#28 AWG DS wire | 5047001001 |
| L-18 | Variable IF. primary | COIL, RF: $1.5-2.5 \mathrm{mc}$, single wnd, single layer wnd, 52 turns \#32 AWG E wire | 5047005001 |
| L-20 | Tweet trap inductor | COIL, RF: single wnd, 3 pie universal wnd, $500 \mathrm{uh} \mathrm{p} / \mathrm{m} 10 \%$, at 1000 kc | 240007300 |
| L-22 | Variable IF. secondary | COIL, RF: $1.5-2.5 \mathrm{mc}$, single wnd, single layer wnd, 52 turns \#32 AWG E wire | 5047005001 |
| L-23 | 5.7 mc tweet trap | COIL, RF: single pie, duo lat wnd, 124 turns litz wire | 5407017002 |
| L-24 | V-16 plate | COIL, RF: 2 mh | 240008400 |
| L-25 | V-7 plate choke | COIL, RF: 2 mh | 240008400 |
| L-26 | Bridge T filter coil | COIL, IF. and Audio Assy. | 540463500 |
| L-27 | V-8 plate coil | COIL, RF: crystal filter grid; freq. range $440-470 \mathrm{kc}$ (incl. C-60, C-80) | 278008500 |
| L-28 | V-11 detector output filter | COIL, RF: 2 mh | 240008400 |
| L. 29 | Power supply filter | REACTOR: filter; 3.0 hy at 0.120 amp | 668002000 |
| L-30 | Power supply filter | REACTOR: filter; 5.0 hy at 0.080 amp | 668001900 |
| L-31 | BFO coil | COIL, RF: 70 turns (incl C-120, C-135, C-136) | 540378500 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS PART NUMBER |
| :---: | :---: | :---: | :---: |
| M-1 | "S" meter | METER: single level; 1 ma DC, 50 ohm $\pm 20 \%$, DC resistance, illuminated dial (incl. I-1) | 458004400 |
| P-1 | Antenna coaxial | CONNECTOR: male coax, UG-21B/U | 357904000 |
| P-2 | Power connector | CONNECTOR: two conductor flexible AC cord | 426100300 |
| R-1 | V-1 grid | RESISTOR: 680,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745147100 |
| R-2 | V-1 cathode | RESISTOR: 4,700 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745138000 |
| R-3 | V-1 screen | RESISTOR: $100,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745143600 |
| R-4 | V-1 plate | RESISTOR: $220,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745145000 |
| R-5 | V -1 plate decoupling | RESISTOR: 10,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745139400 |
| R-6 | L-6 series | RESISTOR: 4, 700 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745138000 |
| R-7 | V-2 grid | RESISTOR: 1.0 megohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745147800 |
| R-8 | V-2 grid decoupling | RESISTOR: 100,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745143600 |
| R-9 | V-6 cathode | RESISTOR: 2, 500 ohms $\pm 20 \%, 1 / 4 \mathrm{w}$ | 376420500 |
| R-10 | V-2 plate series | RESISTOR: 47 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745129600 |
| R-11 | V-2 screen | RESISTOR: 33,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745141500 |
| R-12 | V-2 plate decoupling | RESISTOR: 2, 200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |
| R-13 | V-3 grid | RESISTOR: 470, 000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745146400 |
| R-14 | V-3 cathode | RESISTOR: 120 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745131400 |
| R-15 | V-3 screen | RESISTOR: 4, 700 ohm $\pm 10 \%, 2 \mathrm{w}$ | 745568000 |
| R-16 | V-3 injection grid | RESISTOR: 22,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745140800 |
| R-17 | V-4 cathode | RESISTOR: 330 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745133100 |
| R-18 | V-4 cathode | RESISTOR: 330 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745133100 |
| R-19 | V-4 plate series | RESISTOR: 47 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745129600 |
| R-20 | V-4 grid | RESISTOR: 10,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745139400 |
| R-21 | $\mathrm{V}-4$ plate decoupling | RESISTOR: 2200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS <br> PART NUMBER |
| :---: | :---: | :---: | :---: |
| R-22 | V-3 plate decoupling | RESISTOR: 2200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |
| R-23 | V-5 grid | RESISTOR: 100,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745143600 |
| R-24 | V-5 cathode | RESISTOR: 68 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745130300 |
| R-25 | V-5 screen | RESISTOR: 8200 ohm $\pm 10 \%$, 2 w | 745569100 |
| R-26 | V-5 plate decoupling | RESISTOR: 2200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |
| R-27 | V-6 grid decoupling | RESISTOR: 3.3 megohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745149900 |
| R-28 | V-6 "S" meter dropping | RESISTOR: $68,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745142900 |
| R-29 | L-24 shunt | RESISTOR: 47,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-30 | V-6 screen | RESISTOR: $47,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-31 | V-6 plate decoupling | RESISTOR: 2200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |
| R-32 | V-7 cathode | RESISTOR: 470 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745133800 |
| R-34 | V-7 plate load | RESISTOR: 330,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745145700 |
| R-35 | Bridge T adjustor series | RESISTOR: 33,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745141500 |
| R-36 | Bridge T regeneration adjuster | RESISTOR: 10,000 ohm $\pm 20 \%, 1 / 4 \mathrm{w}$ | 376420700 |
| R-37 | V-8 grid | RESISTOR: 1.0 megohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745147800 |
| R-38 | V-8 grid decoupling | RESISTOR: 22,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745140800 |
| R-39 | "S" meter bridge | RESISTOR: 150 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745131700 |
| R-40 | "S" meter bridge | RESISTOR: 220 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745132400 |
| R-41 | 'S' meter SENS adjust | RESISTOR: 100 ohm $\pm 10 \%, 1 \mathrm{w}$ | 377012100 |
| R-42 | V-8 cathode | RESISTOR: 150 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745131700 |
| R-43 | "S' meter zero | RESISTOR: 100 ohm $\pm 10 \%, 1 \mathrm{w}$ | 377012200 |
| R-44 | V-8 "S" meter dropping | RESISTOR: 68,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745142900 |
| R-45 | V -8 screen | RESISTOR: 47, 000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-46 | L-27 shunt | RESISTOR: 22,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745140800 |
| R-47 | V-8 plate decoupling | RESISTOR: 2200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS PART NUMBER |
| :---: | :---: | :---: | :---: |
| R-48 | V-9 grid | RESISTOR: 3.3 megohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745149900 |
| V-49 | V-9 grid decoupling | RESISTOR: $22,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745140800 |
| R-50 | T-3 primary shunt | RESISTOR: $4700 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-51 | V-9 screen | RESISTOR: 4700 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-52 | V-9 plate decoupling | RESISTOR: 2200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |
| R-53 | V-9 grid bleeder | RESISTOR: $68,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745142900 |
| R-54 | V-11 grid | RESISTOR: 100,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745143600 |
| R-55 | V-9 cathode | RESISTOR: 150 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745131700 |
| R-56 | V-10A diode load | RESISTOR: $\quad 22,000$ ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745140800 |
| R-57 | V-10A diode load | RESISTOR: 4700 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-58 | V-11 cathode | RESISTOR: 820 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745134900 |
| R-59 | V-11 grid | RESISTOR: 100,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745143600 |
| R-60 | V-11 plate load | RESISTOR: $47,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-61 | V-11 plate decoupling | RESISTOR: $15,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745140100 |
| R-62 | AF gain control | RESISTOR: 500,000 ohm $\pm 20 \%, 1 / 4 \mathrm{w}$ | 376449900 |
| R-63 | V-12 plate load | RESISTOR: 470,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745146400 |
| R-64 | V-12 plate dropping | RESISTOR: 680,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745147100 |
| R-65 | V-12 cathode | RESISTOR: 220,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745145000 |
| R-66 | V-12 cathode | RESISTOR: 47,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-67 | Noise limiter adjust | RESISTOR: (Incl. S-4) | 376570100 |
| R-68 | V-12 plate load | RESISTOR: 220,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745145000 |
| R-69 | V-13 cathode | RESISTOR: 3300 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745137300 |
| R-70 | V-9 grid bleeder | RESISTOR: 470,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745146400 |
| R-71 | V-9 feedback | RESISTOR: 33,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745141500 |
| R-72 | V-13 plate load | RESISTOR: 270,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745145400 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS <br> PART NUMBER |
| :---: | :---: | :---: | :---: |
| R-73 | V-13 plate load | RESISTOR: 270,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745145400 |
| R-74 | V-13 cathode | RESISTOR: 3300 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745137300 |
| R-75 | V-13 grid | RESISTOR: 470,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745146400 |
| R-76 | V-22 grid | RESISTOR: 100,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745143600 |
| R-77 | V-22 grid bias series | RESISTOR: 180, 000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745144700 |
| R-78 | Audio load | RESISTOR: 10 ohm $\pm 10 \%, 2 \mathrm{w}$ | 745901300 |
| R-81 | V-21 grid | RESISTOR: 1.0 megohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745147800 |
| R-82 | V-21 cathode | RESISTOR: 150 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745131700 |
| R-83 | V-21 screen | RESISTOR: 47,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-84 | V-21 plate decoupling | RESISTOR: 2200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |
| R-85 | T-4 primary shunt | RESISTOR: $47,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745142200 |
| R-86 | V-16 diode load | RESISTOR: $39,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745141900 |
| R-87 | V-16 diode load | RESISTOR: $3300 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745137300 |
| R-88 | V-16 plate load | RESISTOR: 2.2 megohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745149200 |
| R-89 | V-16 diode load | RESISTOR: $10,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745139400 |
| R-90 | AVC time constant | RESISTOR: 2200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |
| R-91 | AVC time constant "fast" | RESISTOR: 330,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745145700 |
| R-92 | A VC time constant "slow" | RESISTOR: 3.3 megohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745149900 |
| R-93 | RF gain bleeder | RESISTOR: 330,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745145700 |
| R-94 | Voltage regulator dropping | RESISTOR: 2500 ohm $\pm 10 \%, 10 \mathrm{w}$ | 710003000 |
| R-95 | V-19 plate series | RESISTOR: 1000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745135200 |
| R-96 | Bias rectifier filter | RESISTOR: $4700 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745138000 |
| R-97 | Bias rectifier filter | RESISTOR: $15,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745140100 |
| R-98 | Standby bias divider | RESISTOR: $22,000 \mathrm{ohm} \pm 10 \%, 1 / 2 \mathrm{w}$ | 745140800 |
| R-99 | RF gain control | RESISTOR: $10,000 \mathrm{ohm} \pm 20 \%, 1 / 2 \mathrm{w}$ | 376352200 |
| R-100 | V-20 plate decoupling | RESISTOR: 2200 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745136600 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS PART NUMBER |
| :---: | :---: | :---: | :---: |
| R-101 | V-20 grid | RESISTOR: 150,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745144300 |
| R-102 | V-20 plate | RESISTOR: 100,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745143600 |
| R-103 | V-20 screen | RESISTOR: 150,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745144300 |
| R-104 | RF gain series | RESISTOR: 270 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745132800 |
| R-105 | V-7 grid | RESISTOR: 100,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745143600 |
| R-106 | V-20 $\mathrm{B}+$ divider | RESISTOR: 10,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745139400 |
| R-107 | V-12 filament dropping | RESISTOR: 10 ohm $\pm 10 \%, 2 \mathrm{w}$ | 745556800 |
| R-108 | AVC bleeder | RESISTOR: 3.3 megohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745149900 |
| R-109 | Audio feedback | RESISTOR: 390,000 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745146100 |
| R-110 | V-7 grid | RESISTOR: 47 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745129600 |
| R-111 | V-20 grid series | RESISTOR: 47 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745129600 |
| R-112 | V-22 screen | RESISTOR: 3300 ohm $\pm 10 \%$, 1 w | 745337300 |
| R-113 | V-7 Parasitic suppressor | RESISTOR: 120 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745131400 |
| R-114 | V-5 Parasitic suppressor | RESISTOR: 47 ohm $\pm 10 \%, 1 / 2 \mathrm{w}$ | 745129600 |
| S-1A | Band switch, ant coil sel. | SWITCH SECTION, rotary: 2 circuit, 12 position, shorting | 269168900 |
| S-1B | Band switch, RF coil sel. | SWITCH SECTION, rotary: 2 circuit, 12 position, shorting | 269169000 |
| S-1C | Band switch, mixer coil sel. | SWITCH SECTION, rotary: 2 circuit, 12 position, shorting | 269169000 |
| S-1D | Band switch, crystal sel. | SWITCH SECTION, rotary: 1 circuit, 12 position, shorting | 269168800 |
| S-1E | Band switch, crystal coil sel. | SWITCH SECTION, rotary: 1 circuit, 12 position, shorting | 269168800 |
| S-1F | Band switch, 10-10-11 meter padder selector | SWITCH SECTION, rotary: 1 circuit, 12 position, shorting | 269169100 |
| S-2 | S-2A, S-2B | SWITCH, rotary: detent, 3 position, $30^{\circ}$ angle of detent | 269143500 |
| S-2A | Mechanical filter primary selector | SWITCH SECTION, rotary: 1 circuit, 12 position, shorting | 269166600 |

TABLE 6-1 (Cont.)

| I'SEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS <br> PART NUMBER |
| :---: | :---: | :---: | :---: |
| S-2B | Mechanical filter secondary selector | SWITCH SECTION, rotary: 1 circuit, 12 position, shorting | 269166700 |
| S-3 | AM-CW-SSB selector switch | SW'ITCH, rotary: 4 circuit, 2 position, non-skorting | 259065500 |
| S-4 | Noise limiter on-off | SWITCH: part of R-67 |  |
| S-5 | AVC selector switch | SWITCH, rotary: 2 circuit, 3 position, non-st.orting | 259041700 |
| S-6 | OFF-STANDBY-ON-CAL selector switch | SWITCH, rotary: 3 circuit, 4 position, positive shorting | 259065600 |
| T-1 | 160 meter RF coil | COIL, RF: two wnd, single layer wnd, one und w/51 turns, other wnd w/4 turns | 5047038002 |
| T-2 | 80 meter RF coil | COIL, RF: two wnd, single layer wnd, one und w/16 turns, other wnd w/3 turns | 5047039002 |
| T-3 | 455 KC IF. coil | TIRANSFORMER: intermediate freq. 455; treq. range $440-470 \mathrm{KC}$ (incl. $\mathrm{C}-85$ ) | 278019700 |
| T-4 | AVC 455 KC IF. ( $\quad$, 1 | 1R.N.SSFORMER: intermediate freq. 455; tre.. range 440-470 KC | 278019700 |
| T-5 | Audio output transformer | IRA SSFORMER: audio output; pri 5000 ohm; secd 500 ohm tapped at 4 ohm, 2:00 TV | 667001800 |
| T-6 | Power transformer | $\begin{aligned} & \text { TRANSFORMER, power: pri } 115 \mathrm{v} \text {, secd \#1; } \\ & 100 \mathrm{v} \mathrm{CT}, \text { secd } \# 2 ; 5.0 \mathrm{v} \text { secd } \# 3 ; 6.3 \mathrm{v} \\ & 1500 \mathrm{TV}, 50 / 60 \mathrm{cps} \end{aligned}$ | 662014500 |
| T-7 | 11-10-10 meter RF coil | COIL ASSY: 6 turns @ 19 turns per inch | 540460900 |
| V-1 | Calibrator | TUBE: type 6BA6; pentode | ${ }_{2} 55018500$ |
| V-2 | RF amplifier | TUBE: type 6DC6; pentode | 255022600 |
| V-3 | First mixer | TUBE: type 6BA7; pentagrid | 255020900 |
| V-4 | HF crystal osc. | TUBE: type 12AT7; double triode | 255020500 |
| V-5 | Second mixer | TUBE: type 6BA7; pentagrid | 255020900 |
| V-6 | Mechanical filter 455 IF . amplifier | TUBE: type 6BA6; pentode | 255018500 |
| V-7 | "Q" multiplier | TUBE: type 12AT7; double triode | 255020500 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS <br> PART NUMBER |
| :---: | :---: | :---: | :---: |
| V-8 | 455 KC IF. amplifier | TUBE: type 6BA6; pentode | 255018500 |
| V-9 | 455 KC IF . amplifier | TUBE: type 6BA6; pentode | 255018500 |
| V-10 | AM detector muting diode | TUBE: type 6AL5; double diode | 257001800 |
| V-11 | CW-SSB detector | TUBE: type 12AU7; twin triode | 255019900 |
| V-12 | Noise limiter | TUBE: type 6AL5; double diode | 257001800 |
| V-13 | Audio amplifier | TUBE: type 12AT7; double triode | 255020500 |
| V-14 | VFO oscillator | TUBE: type 6BA6; pentode | 255025000 |
| V-15 | VFO amplifier | TLBr:: type 6BA6; pentode | 255025000 |
| V-16 | A VC Det-noise clipper | TCBE trie 6AL5; double diode | 257001800 |
| V-17 | Power rectifier | Tl'BE: tym 5 Y 3 GT ; full wave rectifier | 255015700 |
| V-18 | Voltage regulator | TIMF: IVtm (1at | 257005200 |
| V-19 | RF gain gate - Bias rectificr | TIMt. Nime i.al.5; double diode | 257001800 |
| V-20 | BFO | TIME. IItm Mibat pentode | 255018500 |
| V-21 | A VC amplifier | TIBE: twe fight pentode | 255018500 |
| V-22 | Audio output | TL'BF. trre GiAQ5; beam pentode | 255019500 |
| XF-1 | Holder for F-1 | FLSE Hollder : extractor post for 3AG fuse | 265100200 |
| XFL-1 | Socket for Mechanical filter | SOCKET, tube: 9 contact miniature | 220121600 |
| XFL-2 | Socket for Mechanical filter | SOCKET, tube: 9 contact miniature | 220121600 |
| XFL-3 | Socket for Mechanical filter | SOCKET, tube: 9 contact miniature | 220121600 |
| XI-3 | Socket for I-3 | LAMP HOLDER: bracket for miniature bayonet base bulb | 262121000 |
| XI-4 | Socket for I-4 | LAMP HOLDER: bracket for miniature bayonet base bulb | 262121000 |
| XV-1 | Socket for V-1 | SOCKET, tube: 7 contact miniature | 220103400 |
| XV-2 | Socket for V-2 | SOCKET, tube: 7 contact miniature | 220103400 |
| XV-3 | Socket for V-3 | SOCKET, tube: 9 contact miniature | 220106200 |
| XV-4 | Socket for V-4 | SOCKET, tube: 9 contact miniature | 220106200 |

TABLE 6-1 (Cont.)

| ITEM | CIRCUIT FUNCTION | DESCRIPTION | COLLINS PART NUMBER |
| :---: | :---: | :---: | :---: |
| XV-5 | Socket for V-5 | SOCKET, tube: 9 contact miniature | 220106200 |
| XV-6 | Socket for V-6 | SOCKET, tube: 7 contact miniature | 220103400 |
| XV-7 | Socket for V-7 | SOCKET, tube: 9 contact miniature | 220106200 |
| $\mathrm{XV}-8$, <br> XV-9, <br> XV-10 | Socket for V-8, V-9, V-10 | SOCKET, tube: 7 contact miniature | 220103400 |
| XV-11 | Socket for V-11 | SOCKET, tube: 9 contact miniature | 220106200 |
| XV-12 | Socket for V-12 | SOCKET, tube: 7 contact miniature | 220103400 |
| XV-13 | Socket for V-13 | SOCKET, tube: 9 contact miniature | 220105300 |
| XV-16 | Socket for V-16 | SOCKET, tube: 7 contact miniature | 220103400 |
| XV-17 | Socket for V-17 | SOCKET, tube: 8 contact miniature | 220115700 |
| $\begin{aligned} & \mathrm{XV}-18, \\ & \mathrm{XV}-19 \end{aligned}$ | Socket for V-18, V-19 | SOCKET, tube: 7 contact miniature | 220104500 |
| $\begin{aligned} & X V-20 \\ & \text { XV-21 } \end{aligned}$ | Socket for V-20, V-21 | SOCKET, tube: 7 contact miniature | 220103400 |
| XV-22 | Socket for V-22 | SOCKET, tube: 7 contact miniature | 220104500 |
| XY-1 | Socket for Y-1 | SOCKET, crystal: crystal holders with .094 dia. pins spaced 500 | 292005500 |
| Y-1 | Calibrator crystal | CRYSTAL: 100 KC | 291595400 |
| Y-2 | 80 meter crystal | CRYSTAL: 5.7 mc | 291807000 |
| Y-3 | 40 meter crystal | CRYSTAL: 9.3 mc | 291807100 |
| Y-4 | 20 meter crystal | CRYSTAL: 16.5 mc | 291807200 |
| Y-5 | 15 meter crystal | CRYSTAL: 23.3 mc | 291807300 |
| Y-6 | 11 meter crystal | CRYSTAL: 29 mc | 291807600 |
| Y-7 | 10 meter crystal | CRYSTAL: 30.5 mc | 291807700 |
| Y-8 | 10 meter crystal | CRYSTAL: 31.5 mc | 291807800 |
| 70E-24 | OSCILLA TOR (VFO) | This unit has been dehydrated and hermetically sealed, and should be returned to the Collins Radio Company if servicing is required. |  |
| $455 \mathrm{~J}-08$ <br> ( 800 cps ) <br> $455 \mathrm{~J}-31$ <br> (3.1 kc) <br> $455 \mathrm{~J}-60$ <br> ( 6.0 kc ) | MECHANICAL FILTER | This unit has been dehydrated and hermetically sealed, and should be returned to the Collins Radio Company if servicing is required. | $\begin{aligned} & 5229090002 \\ & 5229089002 \\ & 5229091002 \end{aligned}$ |

