

NRBA proposes deregulation bill

Washington DC...The National Radio Broadcasters Association (NRBA) has announced it will immediately begin pressing for a radio deregulation bill now that H.R.-3333 is dead.

In the words of Senator Goldwater, the "deregulation of radio is no longer an issue. The only question is how and when."

NRBA believes that the time is now and will continue to press for legislation lifting the onerous and counterproductive regulatory burdens now borne by radio industry.

At this time it does not appear that the goal of the total deregulation of radio can be achieved through amendments to the Communications Act of 1934. If, however, the necessary changes are incorporated into the 1934 Act NRBA would in all likelihood be supportive.

"We are not so concerned with the vehicle for total radio deregulation as the achievement of our goal," NRBA Vice President Abe Voron commented. "We will not, however, sup-

port mere cosmetic alterations to the 1934 Act that will prove of little value in deregulating radio."

Points Made

Proposals were submitted to Congressmen Lionel Van Deerlin and James Broyhill following a meeting between NRBA representatives and the Congressmen to facilitate the development of radio deregulation legislation. The proposals will be shared with other members of the House Communications Subcommittee in the near future.

Highlights of the proposal include:

1. Radio licenses extended to 7 years.
2. Licensees will meet the public interest, convenience and necessity standard by broadcasting a certain percentage of non-entertainment programming. This percentage, to be determined by the FCC, shall

not exceed 8% for AM stations or 6% for FM stations.

3. License revocation only in cases of willful and intentional reporting of false information to the FCC, willful and repeated failure to operate as set forth in the license, violations of lottery, fraud and/or obscenity laws as outlined in the United States Criminal Code.
4. The FCC shall be prohibited from evaluating program content, format, presentation or topics covered in non-entertainment programming in renewal proceedings.
5. Section 317 of the Communications Act of 1934, sponsorship identification rules, will be

repealed.

6. In the event a renewal application is designated for hearing, competing applications will be entertained.
7. Ownership bill be limited to 10 AM and 10 FM stations. No restrictions on cross-ownership of AM and FM stations.
8. FCC required to set standards for petitions to deny or revoke, and to establish sanctions for abuse of these processes. Parameters for standards and sanctions to be set by statute.
9. Establish fund to make monies available to minority applicants qualified to own and operate a radio station. Fund to be administered by the FCC.

Ampro buys Scully Recording

Newtown PA...Ampro Broadcasting, a manufacturer of broadcasting

equipment, has purchased Scully Recording Instruments, formerly a division of Dictaphone Corporation. Scully manufactures recording instruments for the broadcast and recording industry.

"To reflect this new association, we have changed our name to Ampro/Scully", stated Tom Creighton, Vice President of Sales and Marketing. Ampro/Scully markets its products worldwide.

Ampro/Scully has added facilities in Newtown, Pa. for manufacturing and warehousing of Scully recorders. Executive offices have also been relocated to this new complex at 826 Newtown/Yardley Road, Newtown, Pa. 18940. Telephone: (215) 968-9000.

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Circle 104 on Action-gram

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Consultant's Corner:

The Howard AM sideband response method

by George P. Howard
Part I

Sarasota FL... (beaches, bikinis and a little engineering on cloudy days)...

In recent times there have been numerous articles on the importance of obtaining superior AM sideband response (bandwidth). This has become increasingly important due to the sideband response demands of AM stereo; and most are probably familiar with the articles of John H. Mullaney, Grant Bingeman, C.V. Clark, Harrison Klein, Harv Rees, and others.

Editor's Note: This month's Consultant's Corner features the Howard method for obtaining superior AM sideband response results.

George P. Howard is an R.F. network consultant (formerly vice president and director of the communications products division of Multronics, Inc.; from which he resigned in 1972 to engage in private consulting).

He is well-known for his designs of directional antenna phasing systems, bifilar filters, and his unique driving point impedance determination system. His most recent developments are the EOR impedance matching method (a constant phase network, requiring no R.F. bridging) and a special sideband rotation network.

This article takes issue with some of the things that have been written previously on this subject and it welcomes constructive criticism. The article would not have been possible without the helpful comments of such people as John Mullaney, Dr. Jerry Raines, Dr. Bob Hoover, Frank Colligan; and most especially the untiring computer programming efforts of Jack J. Mullaney and the field engineering assistance of Ed Osborne.

Point 1.

There are only two points in a broadcast system that are critical for obtaining good sideband response.

- (a) The plate tube of the transmitter
- (b) The antenna tuning unit

Point 2.

Sideband response is "generated" at the plate tube. If we do not start with a good condition there (by providing the optimum sideband loads) we will have nothing worthwhile to give to the antenna.

Point 3.

The antenna may be properly matched to the transmission line; but if the choice of the antenna network

provides poor sideband response at that point, it will not be making full use of whatever superior response we may have generated at the plate.

Point 4.

An improperly selected antenna network can make it more difficult to ultimately provide a good plate situation.

Point 5.

A transmission line is a "network" and the selection of its length affects the ease or difficulty of providing a good plate situation. It, of course, has different electrical lengths (and consequently, different "networks") at the various frequencies across the bandwidth spectrum of interest.

Point 6.

There is an optimum length of transmission line that can be used (in conjunction with the optimum antenna network). However, this length may be impractical and we usually must work with the time honored method of line length selection which is; "how do we get from here to there."

Point 7.

Even with a transmission line of a "poor length" it can be compensated by a proper network at its input.

Point 8.

The ultimate goal for obtaining superior sideband response is to achieve equal power sidebands, with that power being such that it is close to the optimum of carrier power/4. For a 10,000 watt carrier, this would be 2,500 watts in each sideband; giving a total bandwidth spectrum power of 15,000 watts. The equal sideband powers can be greater than carrier/4; but this depends upon the modulator being capable of producing the extra power that it would be called upon to deliver.

Point 9.

Smith Chart rotation of sideband impedances to obtain essentially symmetrical sideband loads (where the resistances are equal; and the reactances are equal but opposite in sign) is not the optimum method for obtaining good sideband response. A computer program is required to determine the power networks for a system, and those networks are not necessarily the ones that result from Smith Chart rotation, but rather are those that produce equal parallel resistances at the sideband; thereby producing equal power sidebands. In the process of accomplishing this they incidentally produce essentially symmetrical sidebands with the preferred horseshoe up condition and low VSWR's.

Point 10.

A few comments about parallel res-

istances. A load is a series circuit of $R + jX$. This can be the load that exists at the plate, the common point, the transmission line, the antenna; anywhere in the system. At any of these points the sideband frequencies have loads of different values, but still $R + jX$.

All of these series impedances have an "equivalent" parallel circuit. The equivalent for a series load of $20 - j200$ is a parallel circuit which has a resistance of $\cdot 2020$ paralleled by a capacitive reactance of $-j 202$. We call these parallel values R_p and X_p and they are easily obtained from:

$$R_p = R + \frac{(X)^2}{R}$$

$$X_p = \frac{R(R_p)}{X}$$

When the R_p values at the two sidebands being compared (like plus or minus 10KHz) are identical, you will have achieved equal power sidebands. The computer program selection of the proper system networks assures that those equal powers will be very close to the optimum of carrier power/4.

Smith Chart rotation does not do this. By now you must have guessed that I prefer calculators and computers to Smith Charts. They are often a useful tool, but probably not favored by the society for the prevention of blindness!

Point 11.

I have stated that points other than the plate tube and the antenna tuning unit are not critical for the sideband response condition. If they were, we would be in big trouble. Take a transmission line as an example. We might measure its input and output and find good sideband response conditions, but these are purely arbitrary measurement points and have no real meaning. There will be numerous points along that line that have very poor sideband response conditions; in fact the response is continually changing as we move from the output to the input.

It is only at the carrier frequency that the line looks like Z_0 along its entire length (assuming a load of Z_0).

Point 12.

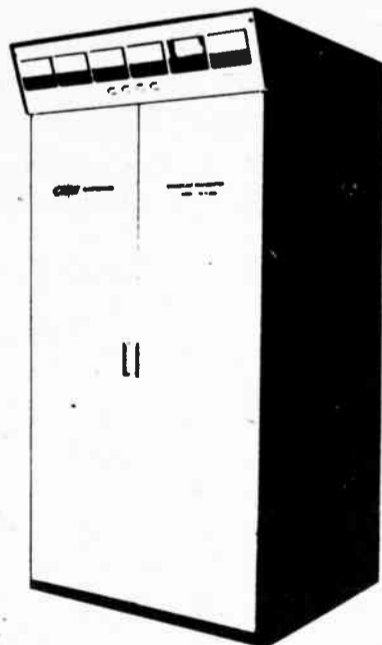
The "equivalent" network for a transmission line with a pure resistance characteristic impedance of Z_0 and a length in electrical degrees of θ (assuming no attenuation) is a Tee network consisting of:

$$X1 (\text{input arm}) = \left| Z_0 \tan \frac{\theta}{2} \right|$$

$$X2 (\text{output arm}) = \left| Z_0 \tan \frac{\theta}{2} \right|$$

$$X3 (\text{shunt leg}) = - \left| \frac{Z_0}{\sin \theta} \right|$$

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(Continued on page 9)

Gold plating a tin ear

by John Price
Radio Arts
PART III

Pasadena CA...Once our tin ears have been gold-plated (see BEE June and July, 1979) you may have found that your complacency has been lost forever. The little flaws in your station's sound used to be ignored or reasoned away. Now they demand fixing.

That's good. Just as your pd is constantly questioning his choice of currents and gold, you should be questioning the technical quality of your finished product.

The gold-plated ear will soon find that *cartridge sound* remains the root of most sound problems on the air. True, they are much better than they used to be. But the various machines that go to make up your cartridge audio often seem to have the poorest overall performance. You may have even bought various new pieces of equipment, or the latest version of the basic endless loop cartridge with little improvement.

Hot damn, you say. Another piece on cart machines. Right. But I dare you to do all that follows and admit that your cart performance has not improved.

Darers go first, you say. I have—and have made carts sound better than reel-to-reel equipment at stations from Daytona to Boise. Now it's your turn.

Tools and Supplies

Strange as it may seem, the first thing you'll need is a full track *reel-to-reel* machine. It doesn't have to be the world's greatest, so that old rusty one in the back room may do. Don't worry about performance unless it is really kaput—we won't record anything above 1KHz on it.

You'll also need an audio generator that is reasonably well calibrated. Hang a frequency counter on it if you have one.

And finally, a good *full track* 7½ ips test tape, a small supply of lubricated cartridge tape on a reel (with a *large* hub) and some empty cartridge

bodies. The carts should be of the same type as those you use on the air.

The recorder's bias should be close to optimum for your cartridge tape. This may need some adjusting if it has been set for a low-noise variety. Note where the "bias adjust" control is, feed 1KHz into the machine, and adjust the bias for maximum level on the *playback* meter. Close is good enough.

Now, thread the test tape and carefully set the *playback* meter for OVU while the 700Hz tone *at operating level* is heard. (Note: Now is a good time to "calibrate" the playback of your machine by marking the control set-

ting. Tapes made on this machine should peak OVU at this playback level.)

Next, thread the cartridge tape and record three lengths of 1KHz test tone, each about one minute long, using your audio generator (and frequency counter, if available). Record the first to *play back* at OVU, the second at -3VU, the third at -6VU.

Repeat this process using 150Hz. But first, go back to your test tape and set the playback meter to read -6VU while the 700Hz tone at operating level is heard. Cut three lengths of tape as before, but note that these will actually be six db hotter than the

1KHz set. (This is because 150Hz, or secondary, or "aux" tones are recorded six db hot by NAB standard. Evidently the "standard" was set up when cart machines had very poor bass response.)

You now have six cuts on your reel of cartridge tape: 1KHz at 0, -3 and -6VU; 150Hz at +6, +3 and OVU, except that you have lowered the playback level by 6db so that they read 0, -3, and -6VU.

If you really trust your reel machine, you may also want to cut three more tracks: they can be useful in trouble-shooting and routine

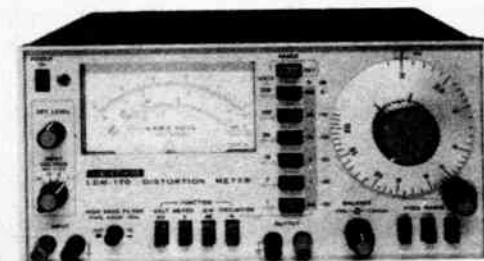
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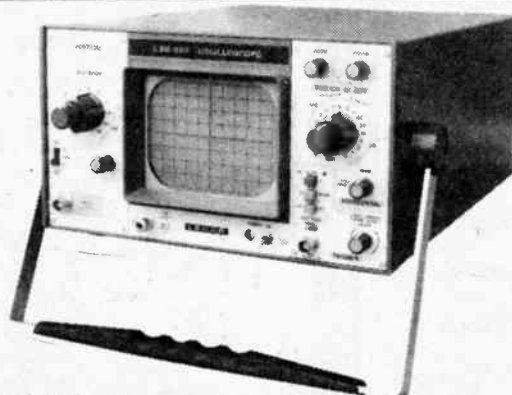
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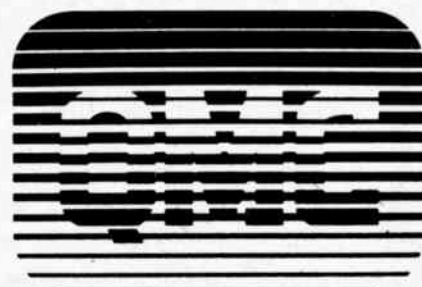
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Circle 116 on Action-gram

3M: Research of magnetic audio tape improvements

New York NY...Much of the improvement in the quality of magnetic tape recording in recent years results from basic research into the magnetic medium, generally oxides, that reproduce acoustical patterns. New magnetic particles developed by tape manufacturers have contributed greatly to improving the signal-to-noise ratios of tape recording systems.

The current generation of music mastering tapes exemplifies the contribution of this research to advances in sound reproduction. The oxide coating of 3M's "Scotch" 250 mastering tape, for example, increases its usable dynamic range by 4 dB over previous low noise, standard output tapes.

The significance of this improvement lies in the fact that it was achieved without trade-offs for undesirable print-through characteristics or a decline in high frequency sensitivity.

In explaining this achievement, 3M's engineers pointed out that improvements in signal-to-noise ratios can be accomplished in three

ways:

- Lowering biased tape noise.
- Increasing the maximum undistorted output of the tape.
- A combination of these two.

An obvious method to obtain higher maximum undistorted output is to increase the amount of magnetic material in each unit of coating. However, the use of this method prior to the present generation of commercial oxides produced two undesirable side effects. First, it resulted in greater print-through—the transfer of acoustical patterns from one layer of tape to another through the seepage of the magnetic field. Second, the consequent need for increased bias lessened high frequency sensitivity and contributed to high frequency saturation. Thus, the easy solution to the problem limited the dynamic range of the tape.

The Best Way

It appeared that a viable solution might lie in developing a new magnetic oxide with improved noise properties and improved print-

through characteristics. Clearly, these improvements would have to be achieved in a magnetic recording tape that would be compatible with current recording equipment.

The engineers went to work. They created a new oxide comprising harder particles that permitted a thicker oxide coating. In their terms, they developed a "higher coercivity" oxide that permits an improvement in "remanence." In fact, the new oxide permits a 33% increase in remanence with significantly less increase in print-through than could be obtained with previous oxides.

The result is a tape capable of delivering higher output, lower tape noise and less harmonic distortion. The increase achieved in remanence enables the tape to produce a 3 dB higher maximum output at peak bias than the best of its predecessors.

Tests show the new tape to be lower in noise across the audio spectrum than any of its forerunners. When measured through a NAB standard noise weighting network, the new tape's noise was found to be 1 dB lower at both short and long wave lengths.

The low frequency signal-to-noise ratio of the new tape improved by 4 dB; 1 dB attributable to noise improvement and 3 dB attributable to maximum signal increase over older standard output, low-noise products.

The new tape requires about 2 dB, or approximately 25%, more bias to reach its peak output. However, if the machine is equalized to accommodate the tape's most popular predecessors, no equalization readjustment is necessary when switching to the new tape.

In addition to an improved oxide, the new tape incorporates technical innovations in surface finishing and durability. Since short wave-length signals are predominantly recorded at the oxide coating's surface, a

smooth surface is critical to high frequency sensitivity and saturation level.

Accelerated wear tests, as well as use under actual studio conditions, have shown the new tape to be equal to its predecessors in durability.

Set Up

When moving up from conventional recording tapes to the new music mastering series, a knowledge of machine adjustments is important. To obtain the best results, bias should be set for peak 15 mil output. No equalization adjustment is required for "Scotch" 250 tape if the machine has been set up for "Scotch" 206 or 207 recording tape.

After adjusting bias, three options are available:

- Improve signal-to-noise ratio by 4 dB, while maintaining the same overload margin (commonly called head room) as for "Scotch" 206 or 207. This is accomplished by decreasing the play meter calibrate or play level by 3 dB; increasing record drive by 2 dB and decreasing the record meter calibrate by 2 dB.

- Improve signal-to-noise ratio 1 dB, while increasing head room 3 dB across the audio spectrum. This is accomplished by reducing record drive 1 dB and increasing the record meter calibrate 1 dB.

- Improve signal-to-noise ratio 2 dB and head room 2 dB. This is accomplished by decreasing the play meter calibrate or play level by 1 dB.

What does the future hold? Most tape manufacturers are constantly working to improve the current state of the art. Digital recording tapes, metal particle pigments and new binder systems are some of the new advances the industry will see. All are designed to improve the quality of tape recording systems, whether for broadcast or recording studio use.

TIN EAR

continued from page 4

alignment work. Cut one minute of 700Hz at operating level (make the playback meter match the same tone on your test tape), plus 10KHz and 15KHz at -10VU. Cut the last two only if your machine is in good alignment. They will serve as rough-adjustment alignment tapes. The 700Hz gives you a good operating level reference.

Now, mark each cut's beginning and end with a grease pencil, and wind each onto a cartridge. When splicing, cut away enough tape so you are splicing audio to audio—this will give you continuous-tone carts.

When you are done, you should have either carts 1-6 or 1-9 on Table

1. Label them clearly, store them carefully, and never use them on a machine whose heads may be magnetized.

The same storage shelf should contain some "store-bought" items: A standard alignment cartridge, preferably full-track; a precision head-height gauge; a head demagnetizer and all the common tapemachine cleaning stuff.

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(Continued on page 6)

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Report on July FCC developments

by **B. Jay Baraff**
Baraff, Koerner & Olender, P.C.

The FCC has denied two petitions seeking reconsideration of its fee refunds challenging the FCC's requirement that applicants accept the refund as full payment of any claim and waive their rights to further litigation. Petitioners felt that they should be allowed to receive the allowed refunds but not waive their rights to seeking further refunds in court. However, FCC felt that there should be some finality to the 10 year old fee refund issue.

Fairness Doctrine and Personal Attack Rule Changed

The FCC has amended its Rules to exempt from the personal attack rule all uses of a broadcast station's facilities by a legally-qualified candidate. This means if a candidate attacks a non-candidate, the personal attack rules do not apply. It also eliminates the applicability of the Fairness Doctrine to Section 315 uses which means that if a candidate speaks out in favor of a controversial issue, the

licensee does not have to provide contrasting points of view.

FCC Has Revised Its Public Interest Notice

Section 73.1202 of the Commission's Rules pertaining to licensee public notice obligations has been simplified. The notice should include the date of the last renewal grant, expiration date and a statement that a list of problems and needs are available for public inspection. The notice suggests the public should send comments about the station's operation.

Format Changes To Be Considered By FCC

The U.S. Court of Appeals has ordered the FCC to hold hearings when a broadcast station changes a unique entertainment format. The Court feels that this affects diversity of programming. However, the Court held that no public interest question would be raised in the following areas if there is another station providing an adequate substitute for the lost programming; there is no public protest of the change in format; there are too few stations to

provide the format to the small number of supporters of the lost format; and the station cannot make a profit under the existing format.

New EEO Policy.

In a major policy change concerning FCC's affirmative action EEO requirements, the Commission announced that upgrading in this area after a license term will not mitigate a deficient record during the

license term. In short, if your EEO record is not good at the time that your renewal application is filed, later upgrading will not soften the blow of any sanctions.

Multiple Ownership Proposal.

The NAACP has requested that the FCC amend its Multiple Ownership Rules to require divestiture of existing AM/FM combinations and to prevent the common ownership of future acquisitions.

TIN EAR

continued from page 4

work backward.

First, *clean* each machine. More good equipment is replaced just because it is dirty than because it is worn out. Scrape and wipe and clean, then do it again. That blob of glup on the belt pulley will cause flutter no matter what fancy cartridge you shove into the deck. Cast your eye over the deck, and eliminate the dirt with swabs, a vacuum cleaner, alcohol and elbow grease.

Second, use your head height gauge. This is intense territory, for most false-cuing problems are caused by playback heads that are too high—the cue track of the head is hearing audio as well as cue tones. If your decks have pieces of metal on the deckplate that support the underside of carts, **DO NOT** rest the gauge on

these. It should measure height from the deck plate *only*.

Next comes the alignment cartridge. You may want to use the 10KHz and 15KHz carts as a rough guide before you wade through the whole alignment/frequency response run on that three-minute cartridge.

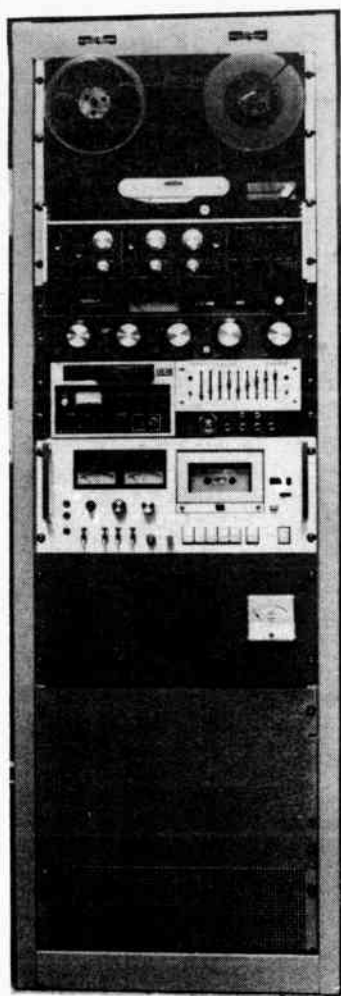
If you are working on stereo equipment, it is imperative that you listen to the summed mono signal from both left and right channels. In stereo, align for maximum *summed* highs—that is *minimum* summed phase shift, and that's the worst offender in stereo carts. An invaluable tool is a momentary A+B pushbutton next to the monitor control on every console. If your ears can hear alignment tones at 15KHz, you can ear-align any cart deck for perfect phasing in a matter of minutes while the button is depressed. Make sure it is installed behind enough isolation so that it can't destroy separation on the program busses while it is pressed. Make it momentary so it can't get left in the 'on' position.

Now, recheck head height. Your alignment work may have disturbed this.

With the audio section peaked, our new test cartridges go to work. Insert #3—1KHz at -6VU. Adjust the *primary* tone sensor so it will just *barely* catch this tone. You have just given yourself an honest 6db of headroom at playback. It may be the first time you knew just how sensitive that sensor was. If you can't get it to cue on a tone 6db low, you may be headed for trouble on that machine, and the circuit should be checked. Any deck should have that much headroom built into its electronics.

Repeat the procedure with cartridge #6—15KHz at 6db below normal 15KHz levels. This will give you that much forgiveness for secondary (or "aux") tones if you use them for automation or warning cues.

Once this procedure is applied to all of your playbacks, you will have established a group of calibrated machines—all with the same head height and alignment, all with six db of headroom for cue tones recorded at standard levels. (Cont. on page 12)



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Table 1
RECOMMENDED TEST CARTRIDGES

Required

- | | |
|----|--|
| #1 | 1 KHz at 0db
Primary tone record level |
| #2 | 1 KHz at -3db
Primary tone sensor set: cartridge recorder |
| #3 | 1KHz at -6db
Primary tone sensor set: cartridge playbacks |
| #4 | 150Hz at +6db
Secondary tone record level |
| #5 | 150Hz at +3db
Secondary tone sensor set: cartridge recorder |
| #6 | 150Hz at 0db
Secondary tone sensor set: cartridge playbacks |

Optional

- | | |
|----|--|
| #7 | 700Hz at OVU reference NAB operating level:
Operating level set |
| #8 | 10KHz at -10db
Rough azimuth adjust |
| #9 | 15KHz at -10db
Medium azimuth adjust |

Each cartridge is fully described in text. #8 and #9 should never be used for final azimuth adjustments, but only as preliminary rough adjustments before a professional alignment cartridge is used.

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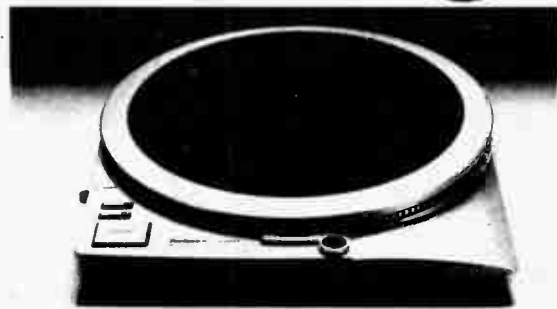
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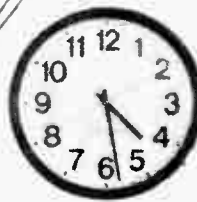
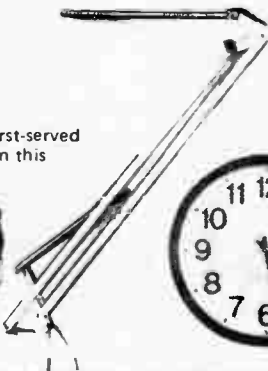
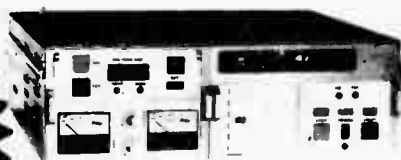
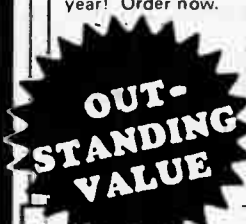
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5.5 minutes	3.10	3.30
7.5 minutes	3.40	3.50
10.5 minutes	3.70	3.90

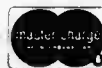
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Clint Free on VTR's:

Some notes on the VR-2000

Fargo ND...Last month I worked on an interesting editing problem on an Ampex VR-2000. There was a "click" in the audio of approximately -5db from program level at the edit time. In this machine, the audio, cue erase and bias amplifier are turned on with either audio or cue record. Also, when editing, cue record is not separated from master record as audio is. Consequently, when record is activated at the beginning of an edit, the bias and erase amplifier is turned on immediately. Then, when audio is turned on by the editor, approximately 1/2 second later, erase and bias are at full amplitude. Applying this drive to the erase and record heads at full amplitude produces a "click," one of life's problems!

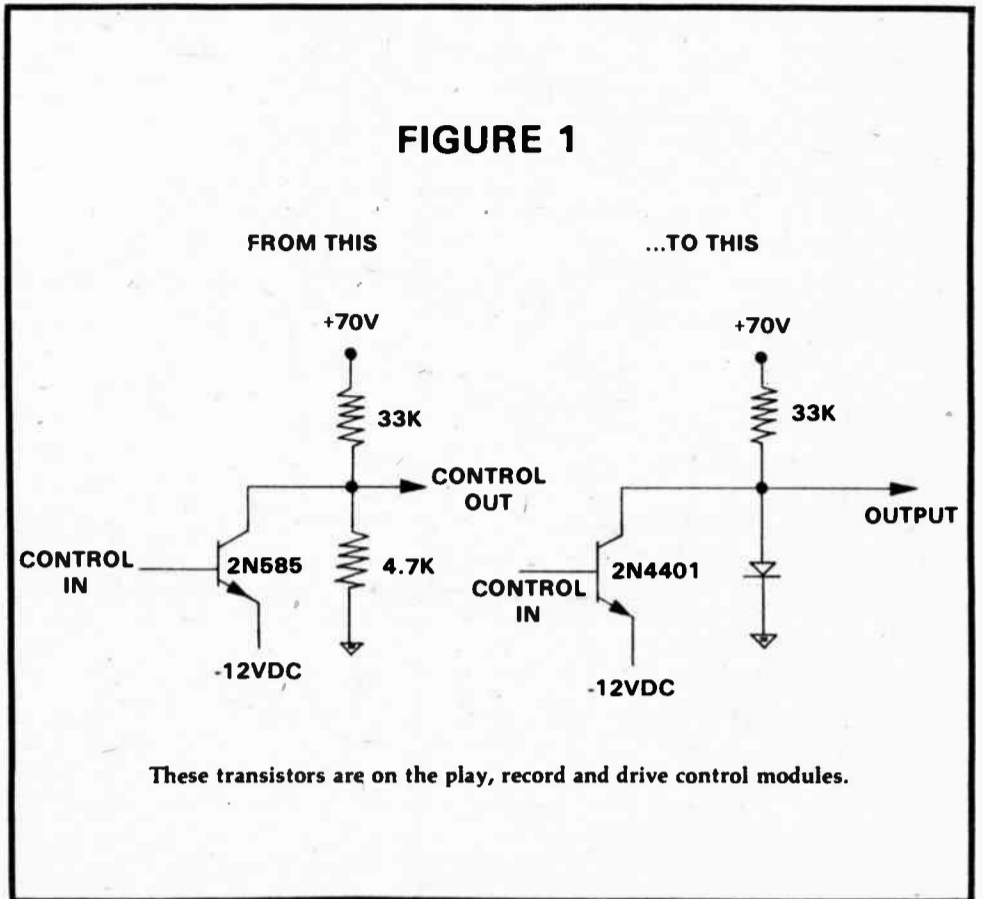
In this machine the cue channel was never used and everyone was happy just to remove the cue control connector to correct the problem. However, for machines where the cue channel is used, this would be a poor solution. For most VR-2000 machines using a relay to disconnect cue control of the bias and erase amplifier when the editor is on, and audio is not off, would be a suitable

solution. Slightly more involved would be to edit the cue channel with audio edit record logic.

Headwheel problems


In another VR-1200 editing problem, I found that there was a lurch of headwheel at the edit time caused by temporary loading of the plus and minus 12 volt regulator by the record RF amplifiers. The regulated power is common to the servo and the phase of the headwheel changed by about 200 nanoseconds for a new head (more RF drive) and 1.5 microseconds for a worn head (less RF drive). The problem was corrected by installing a 1.8 amp plus and minus regulator for the RF record drive electronics, and removing the switched loading resistors on the RF chassis.

In RCA TR-4 machines there are some unlatch and inhibit stages in the control system which become unstable as temperatures rise. Germanium transistors (2N585) develop leakage causing modes to drop out, change, etc. I installed some 2N4401 transistors and changed the circuit as shown in Figure 1 to correct the problem.



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4½ Minute	3.22
5½ Minute	3.39
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HOWARD METHOD

continued from page 2

The equations above assume that the line is equal to or less than 180°. If it is greater than 180°, simply subtract increments of 180° until the answer is a phase less than 180°. That will be the proper θ value to use.

The Zo value is the same for all frequencies, but remember that the θ value is different for different frequencies.

$$\theta = \frac{(ft.) (MHz)}{2.734 (VP)}$$

Where: VP = the velocity of propagation of the particular line (like .81 for 7/8" foam).

Once you have determined the "equivalent" networks you can find the resulting input impedances for any given load at a specific frequency (using of course the proper network for the frequency involved).

This can be done by letting:

$$R_a = \text{load resistance}$$

$$X_a = \text{load reactance}$$

Then for the resulting input impedance of Rs jXs.

$$A = \tan^{-1} \left(\frac{(X_a) + (X_2) + (X_3)}{R_a} \right)$$

$$R_s = \frac{(X_3)^2 (\cos A)^2}{R_a}$$

$$X_s = -(R_s \tan(A) - (X_3) - (X_1))$$

The above applies to any R.F. network where the values of X1, X2 and X3 are known.

It does not have to be a so-called Tee network, because all networks are essentially Tee networks.

a. An L network is a Tee network where either X1 or X2 of the equivalent Tee is 0 reactance.

b. A shunt reactance is a Tee network where both the X1 and X2 of the equivalent Tee are 0 reactance.

c. A series reactance is a Tee network where X1 = 0 and X3 = infinity for the equivalent Tee.

d. A Pi network is 2 Tee networks in series, where the input Tee has X1 = 0; with the output Tee having X2 = 0 and X1 = the series arm of the Pi.

Often it is helpful to view all networks or strings of networks as being Tees in the manner described above. Your transmitter networks can be analyzed by this method.

Point 13.

To truly obtain superior sideband response it may be advisable or necessary to modify some of the transmitter networks by changing their settings or adding components. This is to be done without lessening the harmonic suppression quality of the signal.

Transmitters are designed to work into a non-reactive dummy load; and even for this condition the sideband response at the plate tube is not as good as it is capable of being.

For most transmitters to produce good sideband response at the plate tube, they do not want to see symmetrical sideband loads at the transmitter output point (common point)!

As an example, assume that your transmitter's plate is designed for wanting to see a load of 3200 jO.

Now, if you were to put a 3200 ohm resistor across the plate tube (disconnecting from that point all other circuitry except the R.F. output network/s; and at the same time being sure to leave the plate tube "in" as part of the total circuit) you could:

a. Use an R.F. bridge and signal generator/receiver at the transmitter output.

b. Carefully make a bridge measurement of the impedance existing at the carrier frequency (with all networks set to their factory specified reactances or actual tuned settings). You should find that impedance to be 50 jO. Like the dummy load that you normally tune your transmitter into.

c. Next put the generator on the sideband frequency that is 10KHz above carrier and make another bridge measurement to get an impedance for that sideband.

d. Do the same for 10KHz below carrier.

e. For all measurements use a frequency counter and correct the bridge dial X reading appropriately to get the actual reactance for the frequency involved.

f. These impedance measurements will be the values that the network/s want to see as a load at the different frequencies to produce the 3200 jO at the plate tube for each of those frequencies.

g. Those loads will not be symmetrical at the sidebands, nor will the sideband powers be equal at the transmitter output with those loads. Again, this is not one of the critical points for equal sideband powers; but providing loads of those or similar values at the transmitter output can be quite difficult, if not impossible.

Point 14.

The Howard sideband method produces equal sideband powers at the transmitter output; and then by transmitter network/s adjustment carries that equal power condition over to the plate tube.

Point 15.

The optimum situation would be to have a transmitter specifically designed for sideband response. An example of such a transmitter will be given.

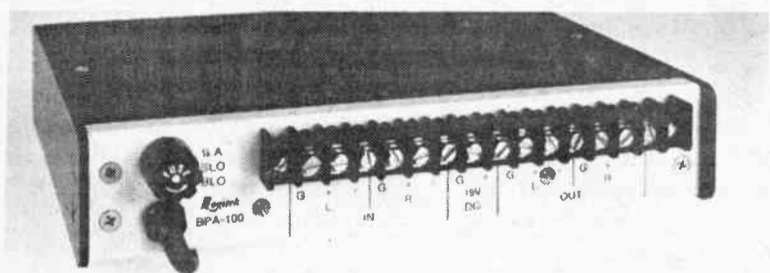
Point 16.

There is a network that is especially
(Continued on page 10)

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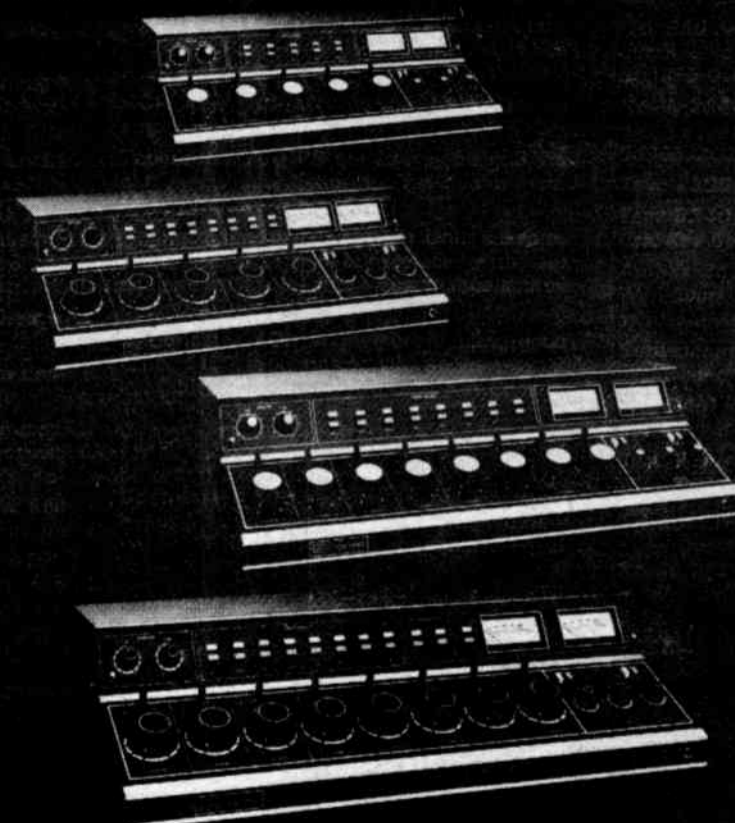
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HOWARD METHOD

continued from page 9

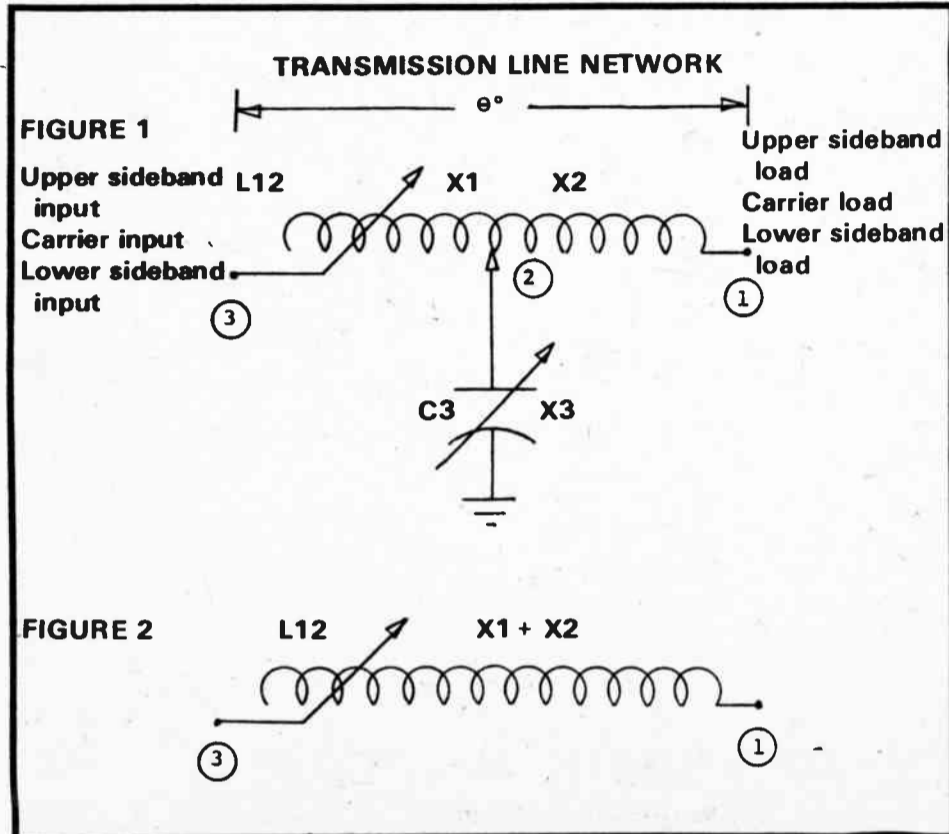
useful for giving equal sideband powers at the input when the carrier load is $R + jO$. It is not a cure-all, because it does not automatically produce powers of carrier/4 if the sideband loads presented to it are very badly "out of balance;" but in many instances it does a good job.

Most importantly its method for tuning is easy and logical. It is a "transmission line network" with

values as previously described in Point 12 and as shown in Figures 1 and 2.

Using the computer value determined for θ degrees and the resulting $X1$, $X2$, $X3$ reactance values:

a. (Fig. 2) Tune L12 to give the total reactance required by $X1 + X2$. (This would be done by R.F. bridge measurement for the carrier frequency.)



b. (Fig. 2) Accurately count the total number of turns required.

c. (Fig. 2) Now locate the point on L12 that is exactly 1/2 that number of turns.

d. (Fig. 1) Clip the X3 shunt leg on at that point (which will be point 2).

e. (Fig. 1) Now there will be a position within the tuning range of C3 that produces that desired carrier pure resistance input, point 3, and gives equal power sidebands there. That will be the position that produces the pure resistance as the result of having the calculated X3 value.

f. Calling the load resistance R_a and the desired input resistance R_s : the resulting requirement for the X3 reactance value will never be less than, $-[(R_a)(R_s)]^{1/2}$. This determines the maximum capacity requirement for C3.

g. L12 will have a wide range of inductance requirements, because the network is technically capable of going from $0 = 0^\circ$ to $0 = -180^\circ$. The input portion of L12 will have a different amperage requirement than the output portion of L12 (if $R_s = R_a$). Consequently, the coil must be selected for the higher of the two amperage requirements.

n. Most often the total reactance requirement for L12, ($X1 + X2$), will be that which results from a 0 value of plus or minus $90^\circ + 20^\circ$.

i. L12 does not have to be a variable type coil, but it is more convenient if it is.

j. C3 does not have to be a variable capacitor. It can be a coil and capacitor in series, but then the capacitor should be of only slightly lesser capacity value than the computer calculated value.

k. Sometimes computer values are not necessarily essential. The requirements for the network can be computed for the range of θ shown in (h) above. Then following the tuning procedure a range of network conditions can be tried by simply starting with L12 at its full number of turns (with C3 attached at the mid-point); checking the input sideband results, then moving one turn towards the output simultaneously with both the coil roller (or tap) and the C3 clip position. Each time retuning C3 for a pure resistance input and then once again checking the sideband results. As those sideband R_p values approach equality you are approaching power equality.

This is a time consuming process in that it requires many measurements and frequency changes for the generator being used, but it will accomplish the job. Thank the "main man" for computers.

Point 17.

The equations for sideband response conditions will be given next month at the conclusion of this article with a sug-

gested format for listing their results.

Point 18.

The antenna network was one of our two critical points for achieving good sideband response. Let's see what happens by our selection of different networks for a given load situation.

For the sideband response of the antenna we are told to take its impedances for the carrier; and upper and lower sidebands.

Like: 1010 KHz $70 + j 177$
1000 KHz $67 + j 170$
990 KHz $63 + j 162$

Then we take the resonated condition of the carrier by cancelling out its reactance (in this case with a capacitor of $-j 170$). That capacitor looks like $-j 168.317$ at 1010 KHz and $-j 171.717$ at 990 KHz.

Therefore, for the resonated carrier condition we now have:

1010 KHz $70 + j 8.683$
1000 KHz $67 + j 0$
990 KHz $63 - j 9.717$

Then we are told to calculate the sideband response conditions based upon these new impedance values.

But wait a minute, this assumes that we have an antenna network, part of which is a capacitor of $-j 170$ (or greater) in series with the carrier load. I say "or greater;" because if it were, the resonated condition would still be obtained but it would occur at a point somewhere "along the capacitor" rather than at its input.

If we do this we would get the sideband response conditions listed for Example #1 (all examples will be shown next month at the conclusion of the article).

Now, what happens if our particular network does not have a series capacitor of that size in its output arm (because a different reactance is needed due to the requirements of the network that we have chosen to make the match to the transmission line)?

We then have simply given the generator "a new pure resistance load to look at" by now having produced the pure resistance condition at the input of the antenna network.

If we look at the sideband response conditions there, we will see that we have obtained equal power sidebands that are very close to the optimum of carrier/4 by having used the optimum network.

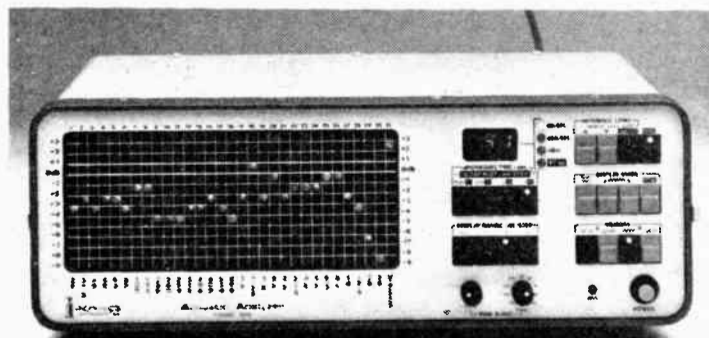
Point 19.

If you think that you may be having a problem with the sideband response of your system (and consequently the strength and quality of your audio), a computer analysis of your system might be advisable. This would let you know what could be done through changes of network settings and/or addition of components or networks to improve your situation.

Next month: Final discussion, equations and examples.

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AT's Ham Brosious and Manhattan's Howard Schwartz flank Mack Emerman, owner of Miami's famed Criteria Studios, during a Biscayne Bay sail on Mack's 52-foot ketch. Occasion was Howie's trip to MCI to finalize custom requirements for his new 56 input automated console, said to be MCI's most expensive ever. The large number of inputs on the new board, scheduled for delivery in April, is required to provide capability for the planned dual 24 and 32 track operation. Emerman's new Criteria West, another all-MCI twin 32 track operation, and the new Schwartz facility were both designed by Sugarloaf View, NYC.

Greg Hanks named Technical Services Manager

Audiotechniques is pleased to announce the appointment of Greg Hanks to the position of Technical Services Manager. Greg was formerly Chief Engineer for Heider-Filmways in Hollywood, CA. Other engineering positions included ABC and Western United Sound Labs, both Hollywood, and Longview Farm in MA. Welcome, Greg!

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Ludwig #935 Timpani (29"-26")
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20" Zildjian Ride Cymbal
Tambourine w/head
Tambourine w/o head
Maracas
Claves
LP Bongos
Gourd & Scraper
Cowbell w/beater
Cabasa
Tubos Shaker
Triangle w/beater & clip
Castinettes
Woodblock
Ratchet
Police Whistle
Slide Whistle
Bird Whistle
Slapstick
Vibraslap
Finger Cymbals
Sleigh Bells
MXR 100
2-MXR Envelope Filters
2-Mutron Biphase
DeArmond Vol. Pedal
Cry Baby Wah Wah
Small Stone Phaser
2-Echoplex
MXR 90
Helpinstill 110

More Automation

It's another MCI automation system for Manhattan as A & R Recording adds the JH-50 system to their 500 console at the A-2 studio on 7th Avenue.

SHORT TAKES

24 track studio for the Tallyman

Perennial recording super star, Harry Belafonte, recently took delivery of MCI 24 track equipment for his new studio at Belafonte Productions in NYC. Audiotechniques' Mike Salafia took care of the arrangements.

New Studio for Ace Frehley

Kiss recording star, Ace Frehley, has contracted with Audiotechniques to supply and install all equipment for his new 24-track studio at his home in Connecticut. The all-MCI studio has been designed by Sugarloaf View.

New Recorders for Generation

Generation Sound Studios (NYC) took delivery of a new MCI 24-track recorder and the first of three new MCI two-track units with mono-stereo capability for advertising requirements. Owner Alan Mirchin also reports that his new John Storyk designed 24-track studio at Aura Recording will open this month.

Speaking of Storyk Designs

Audiotechniques' new demo room in Stamford is a John Storyk design, featuring the latest technology in control room acoustics. We'll have all the newest of outboard goodies on demo as well as consoles, recorders, monitors and mikes (Faulkner and Salafia, that is!).

Hottest Outboard Gear?

Last month's article on outboard brought plugs for favorites by users and many requests for demonstrations. Most requested . . . toss up between A & D's Compex Limiter and Lexicon's Prime Time. (Solution: try 'em both!)

New Studio Activity

Looks like another big year for studio expansions and new studios as our proposal writers turned out a record number of project presentations during January-February. Give us a call for an individually tailored, computerized proposal. If you're even thinking about a project, we should be talking.

Check Audiotechniques first . . . for WEST PENN WIRE!

We recommend West Penn as the best studio wire made. Reason? We've sold nearly 5 million feet of #291 two conductor shielded to studios all over the world without one complaint! Always in stock, in a blinding array of colors!

Rumor Mill . . .

Digital 2 tracks to hit market with affordable prices? (Sooner than you think, reports our overseas spy!)

New "Super Tape" to dominate studio market within 2 years? (Don't ask us, ask our midwest secret agent.)

Caribbean 24 track studio on huge barge to be backed by industry's biggest stars as tax shelter? (Why not?)

Two offers on that Manhattan studio biggie, but has anyone come close to the asking price? (Not according to our N.Y.C. correspondent.)

NEW . . . FROM MCI!

JH-600 Series Automated Consoles

Response to MCI's new 600 console at the AES convention was overwhelming! In the month following the show, orders for 60 units with a sales value of over \$2.6 million have been received by MCI! Recording engineers were impressed with the thoroughness of design considerations of multi-track recording, the simplicity of the automation system and the attractive price. We can safely say that the MCI 600 is the outstanding console value in the world today! We know that's pretty strong, but when you consider the features, we know you'll agree, too.

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TIN EAR

continued from page 6

Cartridge Recorders

Now it's time to get at the machine that cuts all those cartridges. Precision here will be reflected all over the station, so make it good. Do all the things we've listed for playbacks, with particular emphasis on cleaning, since your recorder probably gets very heavy use.

The one major change is for the tone sensor levels: Set them to just barely detect tones from cartridges #2 and #5. Those have tones just 3db below standard level, while your playbacks are set for 6db of headroom. The purpose is to make your recorder the quality-control machine. A cart with a bad tone will fail to recue here, before it gets on the air. You will occasionally find a note that "carts won't recue in Production, but they're OK on the air." That's just your safety factor at work. You know that those carts have tones between 3 and 6db low, and you'd

better start trouble-shooting the recorder.

It is no secret that the record section of your cart recorder is the most important of all. Before we go through the routine, let's pause to reflect on just why we use cartridges in broadcasting.

The original endless-loop cartridge was what we call a "C" size today—the great big ones. They were loaded full of double-coated tape, and ran at 3 3/4 ips. At the splice, the tape was twisted 1/2 turn, and two programs of background music were recorded on the tape—one on each side. Each time the splice passed by the heads, the alternate program was played.

Along came radio in 1958. We doubled the cartridge speed, shrunk it to "B" and "A" sizes, and put it in a start-stop-start-stop mode of operation, all the while requiring broadcast audio quality and, later, stereo broadcast quality. No wonder some problems developed.

The biggest problem remaining is the variations in the corner post at the left front corner of the cartridge. The different heights from cart to cart cause the tape to pass across the first opening of the cartridge at different angles. This was no problem when the carts were used only to play back tapes recorded on open-reel duplicators, then wound onto the cartridge turntables. It wasn't even a problem when combination record-play heads were used in the second opening.

Then came NAB standards, which put the separate record head out in that first hole. Much energy, time and money has been spent selling various forms of cartridges that propose better quality-control of the all-important corner post. My experience shows that the problem is still the cause of most bad cartridge sound.

But by following a few key steps, not stressed enough in most manuals and articles, we can minimize the "floating corner post syndrome" so that your carts will meet all but the very best reel-to-reel standards.

1. Adjust the record head height very carefully, using your gauge, but don't take that as a final answer. Recording a continuous 1KHz tone on a cart, raise and lower the record head slightly until you obtain maximum playback level. This shows that the recorded tracks exactly match the sections of the playback head—and all other playback heads if you've been meticulous with your height gauge.

2. Align the record head very carefully while looking at the playback of the machine—of the summed playback if it's a stereo one. Remember that this record section will cast the die for every playback in the place, so take your time. See how close OVU equals NAB operating level out. If it is more than 2db off in either direction, suspect the recording bias and adjust it for peak output level. See if the various types of lube tape in use require different bias settings. If so, peak the bias for the tape requiring the most, and let other types be somewhat over-biased.

Check the overall record-play frequency response, but remember that high frequencies get turned up inside the record amp, then turned down in playback (pre- and de-emphasis). Your machine, fed 15KHz at -10VU, is really putting it on tape at OVU, so keep all tones for a frequency run at -10VU. Boost playback so -10VU in equals OVU out for accurate meter readings.

So now you have perfect bias, frequency response, alignment and head height—for the one cartridge you've been playing all this time. Now comes the most important part!

Select as many cartridges as your patience will stand. One dozen is the minimum. Erase each one, and record 15KHz on it while watching the (summed) playback signals. Rock the record head azimuth adjustment back and forth until you get a perfect maximum reading. You will soon start to notice that the maximum occurs somewhere between a range of settings—usually about 90 degrees

(Continued on page 22)

BEE Employment Service

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Any company or station can run technical Help Wanted ads at the flat rate of \$12 per month, per insert (for each 50 word increment). Payment is preferred with insert, but if invoice is necessary, there will be an extra \$1.00 charge. Blind box numbers can be provided at an extra charge of \$10.00 per insert, and the responses will be forwarded to the listee, unopened, upon receipt.

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1st Class. Experience includes: 2 years directional, 6 years with non-commercial stations, fund raising, management, programming, instruction, complete design, operation and installation of 2 stations, CCTV experience. Prefer school station position but will look at others and will re-locate. Box PW 6-1.

Chief Engineer at Midwest AM/FM (stereo) automation station looking for advancement from a small-market facility to medium or large-market station. Love the station/work but I have to eat. Send replies to Box PW 6-2 for mutual exchange of information.

For listings with Box numbers, reply to Box _____, c/o BEE, PO Box 1238, Arlington VA 22210

TIN EAR

continued from page 22

Now we're recording perfect cartridge audio, but we're not quite through. You also need perfect cue tones.

Arrange some way for the cue section of the playback head to drive a program playback channel. On machines with pin plugs behind the head, simply transpose two plugs behind the head. Insert cartridge #1, and set the level on any convenient meter. If you have one, hang the frequency counter on the output, too. (If not, just hum along with the 1KHz tone. You may want to do this late at night when you're alone in the place to protect your reputation.)

Now insert a blank cartridge and tone. Is it the same frequency? NAB specs allow a plus or minus 10% tolerance, so anywhere between 900-1100Hz is OK, but the closer the better. Now, how about the level? If it is more than plus or minus 1db from your standard cart's level, better adjust it. Remember, those playback sensors on your quality-control machine have only 3db of forgiveness.

Now do the same thing with cartridge #4 and the 150 Hz secondary or "aux" tone. Remember, it should be 6db "hot" compared to the primary tone. For some reason, cart recorders have a tendency to let their secondary tones drift off-frequency. I've seen more than one automation system bravely trying to figure out what to do with 120Hz secondary tones. Often, its decision was the wrong one. While specs allow it to range from 135-165Hz, keep it as close as possible, and check it once in a while. There's nothing worse than having to re-dub dozens of carts because the aux tones are bad.

Admire Your Results

You now have a cartridge record-play chain with minimum phase shift, maximum tone reliability and the best durn sound you've ever heard off of carts. If there are still problems, it has to be external to this chain.

Which it well could be: hundreds of pieces of equipment are replaced with "a better model" each year, only to connected up with the same bad wiring, to the same cheap mikes feeding distorted mixers, thereby improving nothing.

As a final step, make sure anyone recording carts can easily "A-B" what's going in against what's coming out. First, lock the input level control on the recorder so that OVU on your console equals OVU during playback of the cartridge 700Hz tone, when compared to a known standard (cartridge #7, for example). If the recorder's VU reads other than zero in the record position at this point, it could mean a) the VU is out of calibration (adjust the "record calibration" control); b) the bias setting is not correct for the tape you are using (adjust

the bias as above); or c) it was just never set right, and you have been recording carts at the wrong level all these years. In any case, correct it, but leave the meter switch on playback. Instruct your staff to read the console VU to see what's going in, and the recorder's VU to see what's coming out a split-second later. Now they can A-B input versus output levels.

Go one step farther: A-B audio checks. Balance the program and audition levels in your console, and keep the recorder's output on the audition buss. Now, by switching the monitor from program to audition during cart dubbing, you can easily hear the difference between input

and output. Activate the A+B push-button, and you add a check for stereo-mono phasing as you dub each cartridge.

If you possess a dual-channel console, you may even try a version of the above with identical speakers for each channel, so you can constantly hear both input and the recorded output, if you can stand the delay between the two. (It tends to offset one ear about six inches to the rear of your head).

Carts Can Sound Good

The final result of all this will be cartridge sound that will amaze you.

You have the tools with which to keep the sound that way, and the checkpoints for cart-by-cart monitoring as you dub the lifeblood of your station's sound.

Of course, good cart sound can be self-defeating. You may find yourself carting music, which formerly had to come from discs to sound decent. Your pleas for new equipment may be for naught, since the old stuff sounds so great (ask for a raise instead). Other stations may attempt to spy on your new gear, which doesn't exist.

The real secret will be your gold-plated ears, which can hear the difference between the good, the bad and the ugly.

DISTRIBUTOR DIRECTORY

The following is a listing of distributors that serve the broadcast industry and who would be glad to help you with any of your equipment needs. Contact any of them directly, or circle the appropriate number(s) on the Reader Inquiry Card and send it to IMAS today. We will forward your request to the distributors, and they will send you their literature or line cards.

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70 sec	2.19	2.25	3.27
100 sec	2.25	2.32	3.38
2.5 min	2.48	2.56	3.51
3.5 min	2.59	2.67	3.66
4.5 min	2.72	2.75	3.81
5.5 min	2.89	2.96	3.97
7.5 min	3.06	3.14	4.21
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Shintron 315 sync generator w/ power supply and burst generator.
Shintron 361 switcher.
Shure M-64 phone stereo preamplifier.

For Sale

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Sony AV-3200 camera w/ viewfinder.
Sony AV-3600 1/2" VCR.
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Telemation TSG-2000 sync generator.
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TRI Sun III time code encoder.
Viscount SG-2 sync generator.
2 Viscount 7V3FER switchers.
Viscount 5V2FE video mixer.
RCA TR-3 black and white VTR
RCA TR-4 B & W VTR rec./play.
Tektronix 525 waveform monitor, needs some work.
McMartin TBM-3000 FM frequency monitor 92.7.
RCA BW-73 FM multiplex monitor.
Hewlett-Packard 335B frequency monitor.
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H.P. 650A oscillator frequency range 10Hz to 10mhz metered output.
Polarad FIM-2 field intensity meter.
Marconi OA-1094 spectrum analyzer.
Ampex VR-1100 VTR.
Ampex 5800 VTR.
Ampex 5200 VTR.
Ampex 7500, 7100, 5100 and 7000 VTR's.
Ikegami ITC-7001 3 tube self contained high resolution, 6 X 1 zoom lens rear control color camera, good cond.
Ikegami VR-624 camera w/ silicon or vidicon tube option, good cond.
Panasonic mobile w/ 3 cameras, 2 WV-350, 1 WV-220, 1 switcher WV-600 audio mixer/monitor, etc., good cond.
Sanyo 2000C VTR rec./play., good cond.
Sanyo 2000 VTR rec./play., good cond.
ITC VF-2020 B&W camera w/ 5" viewfinder, remote panel, 50' cable and 2 1 sync generator, good cond.
ITE VF-301 camera w/ 5" viewfinder, 2-1' remote panel, 50' cable, option of self-contained., Good cond.
Audiotronics camera w/ 4" viewfinder, 12V DC/110V AC int. Ext.
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For Sale

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