

# WIRELESS WORLD ANNOUNCEMENT 

We apologise to readers for inserting an incorrect advertisement for the WIRELESS<br>WORLD ANNUAL on page a39 of this issue

## The correct advertisement appears below

## GETIT WHILE ITSGOING

This is the first ever Wireless World Annual. It's got 128 pages including features covering all aspects of electronics and communications - new and established techniques, some practical, some theoretical - all written to the high standard you'd expect from Wireless World. Contents include: A General Purpose Audio Oscillator by L. Neison Jones (a constructional project specially commissioned for the annual); Constructional Design for a Small Boat Echo Sounder by John French; Scientific Calculations with an Arithmetic Calculator by R. E. Schemel. There is also a reference section packed with useful information.
$£ 1$ from newsagents or $£ 1.35$ inclusive by post from the publishers.

## Wireless World Annual 1975

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To: General Sales Department, Room 11, Dorset House Stamford Street, London SE1 9LU.
Please send me copy/copies of Wireless World Annual 1975 at \(£ 1.35\) each inclusive. I enclose remittance value \(£\) (cheques payable to IPC Business Press Ltd).
Name (please print)
Address.
```


## wireless world annual 1975

COMMUNICATIONS • ELECTRONICS


## LOW COST RC OSCILLATORS <br> 

## PORTABLE INSTRUMENTS



FREQUENCY ACCURACY

SINE OUTPUT DISTORTION SQUARE OUTPUT SYNC. OUTPUT METER SCALES
SIZE \& WEIGHT

TG152D
Without meter.
£48

FREQUENCY

ACCURACY
SINE OUTPUT
DISTORTION
SQUARE OUTPUT
SYNC. OUTPUT
SYNC. INPUT
METER SCALES
SIZE \& WEIGHT

## ANALOGUE

3 Hz to 300 kHz in 5 decade ranges $\pm 2 \% \pm 0.1 \mathrm{~Hz}$ up to 100 kHz , increasing to $\pm 3 \%$ at 300 kHz .
2.5 V r.m.s. down to $<200 \mu \mathrm{~V}$.
$<0.2 \%$ from 50 Hz to 50 kHz .
2.5 V peak down to $<200 \mu \mathrm{~V}$.
2.5 V r.m.s. sine.
$0 / 2.5 \mathrm{~V}$ \& $-10 /+10 \mathrm{~dB}$ on TG152DM.
7 " high $\times 10 \frac{1}{4}{ }^{\prime \prime}$ wide $\times 5 \frac{1}{2}{ }^{\prime \prime}$ deep. 8 lbs .

TG152DM
With
meter.
f58

1 Hz to 1 MHz in 12 semi-decade ranges. 0 to $1 \%$ fine control included on TG200DMP
$\pm 2 \% \pm 0.03 \mathrm{~Hz}$
$7 V$ r.m.s. down to $<200 \mu \mathrm{~V}$ with Rs $=600 \Omega$
$<0.1 \%$ to $5 \mathrm{~V},<0.2 \%$ at 7 V from 10 Hz to 100 kHz TG200D, DM \& DMP only. 7V peak down to $<200 \mu \mathrm{~V}$. Rise time $<150 \mathrm{nS}$.
$>1 \mathrm{~V}$ r.m.s. sine in phase with output $\pm 1 \%$ freq. lock range per volt r.m.s TG200M. DM \& DMP only. $0 / 2 \mathrm{~V}$. $0 / 7 V \&-14 /+6 d B m$.
$7^{\prime \prime}$ high $\times 10 \frac{1^{\prime \prime}}{} \times 5 \frac{1}{2}{ }^{\text {" }}$ deep. 10 lbs .

TG200 TG200D TG200M TG200DM TG200DMP £57 f60 f67 f70 f74

## DIGITAL

FREQUENCY
ACCURACY

SINE OUTPUT
DISTORTION
METER SCALES
SIZE \& WEIGHT
TG66B
Battery
model 545

## SHSTEDODOD

## VORTEXION

A new range of sound equipment from Vortexion, System 2000 has been designed by our engineers to combine the aesthetics of design in the domestic equipment field with the near flexibility of a modular system. Like all our equipment Vortexion System 2000 is built to last.

No matter what your sound problem, whether hotel or local pop group, ask our Design Consultants how it can be solved with System 2000.

# Complete the coupon and well send you our new catalogue.Completely free. 

The new Heathkit catalogue is now out. Full as ever with exciting. new models. To make building a Heathkit even more interesting and satisfying.

And, naturally, being Heathkit, every kit is absolutely complete. Right down to the last nut and bolt. So you won't find yourself embarrassingly short of a vital component on a Saturday evening-when the shopsare shut.

You'll also get a very easy to understand instruction manual that takes you step by step through the assembly.

Clip the coupon now and we'll send you your free copy to browse through.

With the world's largest range of clectronic kits to choose from, there really is something for everyone.

Including our full range of test equipment, amateur radiogear, hi-ft equipment and many general interest kits.

So, when you receive your catalogue you should have hours of pleasant reading.

And, if you happen to be in London or Gloucester, call in and see us. The London Heathkit Centre is at 233
Tottenham Court Road. The Gloucester showroom is next to our factory in Bristol Road.

At either one you'll be able to see for yourself the one thing the catalogue can't show you.

Namely, how well a completed Heathkit performs.
Heath (Gloucester) Limited, Iept.WW-65,Bristol Road, Gloucester, Cil 26 FEE . Tel: Cloucester (0452) 29451.

A new oscilloscope from the Heathkit range.
Marine direction finderwith digital read-rut
Solid-state grid dip meter.


## The world's most universal audio bridges

Each of these bridges has ten decade ranges and can be used to measure any type of component or complex impedance. Transformer ratio-arms are used to cover a very wide range of measurement using a minimum number of standards which are set digitally. The three terminal facility provided by this type of bridge enables small values of capacitance or high values of resistance to be measured at the end of long lengths of cable. Components can also be effectively isolated electrically from a complex network allowing individual measurements to be made without disconnection from the circuit being necessary.

## Wayne Kerr's B224 and B642



The B224 is a manually operated bridge, the resistive and reactive terms being independently set to a null indicated on the meter. A rechargeable battery is fitted in order to make the instrument portable.


The B642 balances itself automatically. The meters read real and quadrature terms and highly stable analogue outputs are provided which are directly proportional to capacitance and conductance above $10 \Omega$ impedance and also to inductance and resistance below $10 \Omega$. One or two decades can be set to provide the first significant figures of the measurement, thereby increasing the meter sensitivity by 10 or 100 times. If a chart recorder is connected to the output of either term, drifts in component values to at least four significant figures can be observed.

For more information, telephone Bognor Regis on (02433) 25811 or write to the address below:

## WAYNE KERR

Durban Road, Bognor Regis, Sussex PO22 9R2
Telex: 86120. Cables: Waynkerr Bognor
A member of the Wilmot Breeden group


NOTE• $0.1 \%$ accuracy relates to parallel component measurements above $10 \Omega$ impedance $03 \%$ accuracy relates to series component measurements below $10 \Omega$
impedance

- Manualoperation only

DECADE BOXES
'Junior' Series-Resistance-1 \%


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R803 8
High Dissipation-Resistance- $1 \%$

|  | Decades | Ohms Range | Ohms Resolution | £ |
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| HD1 | 5 | 0-1.111.100 | 10 | 93.00 |
| HD1/L | 5 | $0-111.110$ | 0.2 Approx. | 98.00 |
| "Point One" Series-Inductance-5\% |  |  |  |  |
|  | Decades | mH Range | mH Resolution | £ |
| L1 | 3 | $0-1.110$ | 1 | 74.00 |
| L2 | 2 | $0-\quad 110$ | 1 | 55.40 |
| L3 | 2 | $0-1100$ | 10 | 61.60 |
| "Hundred" Series-Inductance-0.3\% |  |  |  |  |
|  | Decades | mH Range | mH Resolution | £ |
| 1300 | 3 | O- 1110 | 1 | 246.00 |
| L400 | 4 | $0-11.110$ | 1 | 320.00 |
| CAPACITANCE BOXES |  |  |  |  |

Decades
C3
PC3
C4
PC4

Decades
42.00
41.75
41.75
41.00
41.00
51.00
51.00
51.50
51.50
52.00
59.30
61.71
61.71
62.50
68.00
78.00
78.00
72.50
73.00
8850
88.50
85.00

Ohms Resolution

## $10 \quad 83.00$ <br> 87.00 88.00 <br> 88.00 $\mathbf{9 4 . 0 0}$ <br> 94.00 113.00 <br> 115.00 <br> 117.00 <br> 122.50 134.00 <br> 134.00 <br> 136.00 141.00 <br> 153.00

| Onms Resolution |  |
| :--- | ---: |
| 10 | $\mathbf{2 7 . 4 0}$ |
| 1 | $\mathbf{2 7 . 1 0}$ |
| 10 | $\mathbf{2 2 . 3 0}$ |
| 1 | $\mathbf{2 2 . 0 0}$ |
| 10 | $\mathbf{1 8 . 2 3}$ |
| 1 | $\mathbf{1 8 . 1 5}$ |
| 1 | $\mathbf{3 3 . 0 0}$ |
| 1 | $\mathbf{3 8 . 8 0}$ |

pF Resolution
100
22.20

20

|  | Decades | pF Range |  |  | Accuracy | £ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VC4 | 3 | 50- | 11.150 |  | $1 \%$ | 53.00 |
| VC5 | 4 | 50-1. | 11.150 |  | 1\% | 75.00 |
| PVC5 | 4 | 50-1. | 11.150 |  | 0 5\% | 112.00 |
| SVC5 | 4 | 50-1. | 11.150 |  | 0.1\% | 480.00 |
| C500 | 4 | 50-1. | 11.150 |  | 0.2\% | $212.00 \dagger$ |
| SVC5 special | Detals on | applicatio |  |  |  |  |
| Variables |  |  |  |  |  |  |
|  | pF Range |  |  |  | Accuracy | £ |
| VC1 |  | 10- | 260 |  | 1\% | 25.00 |
| PVC1 Mk 2 |  | 5- | 200 |  | 0 5\% | 88.00 |
| PVC Mk 2 |  | 20- | 1,120 |  | 0.5\% | 80.00 |
| VC2 |  | 20- | 1.130 |  | 9\% | 37.00 |
| PVC4 |  | 0- | 10 |  | 1\% | 61.00 |
| PVC1/S |  | 20- | 120 |  | $05 \%$ | 55.44 |
| Switched |  |  |  |  |  |  |
|  | uF Range |  |  | uF Resolution | Accuracy | $E$ |
| C140 |  | O- | 140 | 1.0 | 5\% | $130.00 \dagger$ |
| C100 |  | O- | 100 | 10 | 5\% | $110.00 \dagger$ |
| C60 |  | O- | 61 | 0.1 | 5\% | $98.00 \dagger$ |
| C60P |  | O- | 61 | 01 | 1\% | $199.00 \dagger$ |

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## D.J. Iloyd Instruments Itd

Brook Avenue, Warsash, Southampton SO3 6HP Tel: Locks Heath 4221
$\dagger$ Packing and Handling extra Prices do not include VAT

## The Dymar 1785 portable AM-FM modulation meter.



## No need to ask who's in control. It's you!

The Dymar Type 1785 is quickly and easily tuneable anywhere across the entire VHF band and into UHF to encompass the mobile 470 MHz band.

Designed to measure the depth of modulation or frequency deviation of today's demanding mobile and portable transmitters, the 1785 offers four ranges of both peak or trough percentage modulation ( 3 " $\%$ fsd to $100 \%$ ) and both positive and negative deviation $(3 \mathrm{kHz}$ to 100 kHz ).

The sensitivity over the entire frequency range is better than 2.5 mV into 50 ohms ( -40 dbm ),
which permits loose coupling to the transmitter under test. And internal noise is typically 44 db below 3 kHz .

Then, like most Dymar instruments, the 1785 is equally at home working from mains supply or in action in the field operating on its own rechargeable NiCd batteries.

With such value-for-money performance, you'll want to drive the 1785 to the limit - and that's why we emphasise that the 1785 is fully tuncable.

Want to know more? Use the Reader Reply Service or contact Dymar direct.

## DTMAS

the name in radiotelephones
DYMAR ELECTRONICS LIMITED, Colonial Way, Radlett Road, Watford, Herts. WD2 4LA, Telephone Watford 3732 I. Telex: 923035. Cables: Dymar Watford.

The Dymar range of instruments - designed for the mobile land, marine and air communications industry.

# Magnetic winner in the less-space race: the new Brimar M14-100. 



Thorn Radio Valves and Tubes LImited Mollison Avenue, Brimsdown, Enfield, Middlesex, EN3 7NS. $\frac{1}{\text { nomm }}$ Telephone: 01-804 1201.

## IP 1.L.P. (Electronics)Ltc

## SHEER SIMPLICITY!




The thes is a complete mono hybrid preamplifier. ideally suited tor both the device consists of two might qualily amplifiers the first contans freauency equalisation and gain correction, whue the second caters for tone control and
batance.
TECHNICAL SPECIFICATION
Inputs
Magnetic Pick-itp 3mV. FilaA Ceiamic Pick-up Microphone Tuner
Auxillary Auxillary
Input mpedince
Outputs
100 mV
Main outmut Odb ( 0.775 voits
Active Tone Control
Treble 12 ab at 10 KH ,
Distortion $\quad 0.0 \mathrm{db}$ at 100 bt lat
SignalNoise Ratio
Supply Voltage sensive input
PRICE $£ 4.50+0.36$ V.A.T. $P \& P$ free

## TWO YEARS GUARANTEE ON ALL OUR PRODUCTS

## I.L.P. Electronics Ltd, <br> Crossland House.

Nackington, Canterbury,
Kent CT4 7AD
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The HY50 is a complete solla state nybuld Hi-Fi amplifie incorporatimg its own high conductivity heatsink heimet cally sealed in black epoxy iesin. Only five comnec. tions are piovided: Input, output, power hnes and earth.
TECHNICAL SPECIFICATION
Output Power 25 walts KMS unto 8!? Load impedance 4-16?
Input Sensitivity Odb ( 0.775 volts RMS) Input Impedance $47 \mathrm{k} \Omega$
Distortion Less than $0.1^{\circ}$ at 25 watts typically 0.05
Signal/Noise Ratio Hetter thall 7bdb
Frequency Response $10 \mathrm{~Hz} \quad 50 \mathrm{kti} / 3 \mathrm{clb}$
Supply Voltage 25 volts
Size $105 \times 50 \times 25 \mathrm{~mm}$
PRICE $5.98+0.48$ V.A.T. P \& P free

Please Supply
Total Purchase Price
I Enclose Cheque $\square$ Postal Orders $\square$ Money Order $\square$
Please debit my Access account $\square$ Barclay card account $\square$
Account number
Name \& Address
Signature


The PSU50 incorporated a specially designed transformer and can be used for either mono or stereo systems

TECHNICAL SPECIFICATIONS
Output voltage 50 volts $(25-0-25)$
Input voltage $210-240$ volts
Size L.70.D.90. H. 60 mm
PRICE $£ 6.00+0.48$ V.A.T. P \& P free


## Cambridge Audio

for people who listen to music Cambridge Audio Limited

The River Mill
St. Ives
Huntingdon PE17 4EP
Telephone St. Ives 62901

## THE TUNER YOU CAN TRUST

This tuner has been designed for use with high quality audio equipment. It has therefore been designed so that only high quality audio signals may be heard. There are no interstation noises, distorted or mis-tuned stations, spurious tuning responses, or other unwanted effects. There are only clear stereo programmes set against a background of silence. When the tuning lamp is out - silence; tuning lamp on - one of a multitude of receivable stations, in perfect tune, and held by powerfula.f.c.


## FEATURES

- Solid wood cabinet
* Two-tone front panel
* Pre-select and manual tune
* "Intune" indicator lamp
$\star$ Stereo indicator lamp
* Frequency meter
* Foolproof tuning
* High sensitivity
* Anti-"Birdy" filter

OTHER ITEMS
LP1186 Filter Unit
TBA750 TBA750 TBA 625 C
$\mathrm{SL} 3045 / 6$ SL3045/6
SL301B SL301B
MC1310P
$£ 5.50$ $£ 5.50$
$£ 2.95$ $£ 2.95$
$£ 2.49$ £2.49
${ }^{£} 1.25$
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$€ 1.30$ £ 3.88

## COWIT'S TIE AMCROWM600

M600 POWER AMPLIFIER


Coupling two M600s together through a socket provided at the back of each amplifier produces a 140 Volt balanced output. This configuration is called an M2000, and produces 2 kilowatts into an 8 ohm load. A peak catching meter, and threshold lights provide convenient front panel output monitoring

## 1350 watts <br> DC-Coupled

The M600 amplifier is a new high-power amplifier capable of providing 1.350 watts RMS over a bandwidth of DC to 20 kHz . 70 volts RMS at the output terminals, very low noise and distortion. AC/DC selector switch, output terminals, very low noise and distortion. AC/DC selector switch,
plug-in front panel circuit board, built-in fan for cooling and the ability to plug-in front panel circuit board, built-in fan for cooling and the ability to
connect two M600s together to double the power and output voltage, are just some of the features which place the Amcron M600 in the forefront when considering power amplifiers
Driving shakers and vibrators, motors, and difficult speaker systems. providing power for material or components testing or used as a large distribution amplifier, the M600 is equally at home.

Brief specifications

RMS power out
DC output
Power bandwidth Phase response Siew rate
Damping factor (8s?) Hum \& noise THD
Dimensions

+ VAT
\& 15 p
P\&P ea.
45 p max.
33 aestrop view. purton wits sw 900
$\mathscr{g}_{\text {con }} \mathscr{D}_{\text {esign }}$
S.A.E. please for details to:

33 RESTROP VIEW, PURTON, WILTS SN5 9DG

MACINNES LABORATORIES LTD

An evaluation kit, with the MVAM 1 , the CA3123E radio IC, TOKO coils \& ceramic IF fillter, 150 mm Rivlin pot. and the IMI 6 button preset varicap controller is a wailable from Ambit Int., 37 High Street, Brentwood, Essex CM14 4RH for $£ 11.50$ ex vat (Includes a PCB for the construction of a MW electronically tuned radio)
 announcing

## The all electric wireless


#### Abstract

it had to happen a varicap diode to tune AM wireless, and at a price that opens new vistas to the design of radio at all frequencies, and at all levels of sophistication. And just so this momentous event does not go by unnoticed, four leading manufacturers have combined together to produce a complete package approach to incorporating this innovation.


Motorola make the diode. Which is only natural, since they have been producing varicaps for some time. The MVAM 1 is three 500 pF swing diodes, matched to $3 \%$ over a 25 v bias range. Use it to tune the antenna, RF and oscillator stages in high quality sets. And the MVAM 2 - two diodes of 300 pF swing each, again with $3 \%$ matching.
$\begin{array}{llll}\text { MVAM } 1 & \text { Cr 15:1 min. per section } & \ldots . . .100+£ 1.55 \\ \text { MVAM } 2 & \mathrm{Cr} 18: 1 \mathrm{~min} \text { per section } & 100+£ 0.45\end{array}$


TOKO Inc. make coils and filters for wireless. All electric or not, TOKO coils are the first choice of most radio design engineers. The range is enormous, and covers LF through MF, HF and VHF. Then there are ceramic and mechanical IF filters in a variety of bandwidths for AM/FM applications. For the MVAM project, a set of MW coils for antenna, RF and Oscillator is available; together with a ceramic filter and IF detector transformer.

Rivlin Instruments make a long slider potentiometer. When you have the versatility of electronic tuning, why complicate the issue with cord drives, pointers, pulleys etc. ? This new series (WS150) of wire wound precision potentiometers give direct scale resolution from their 150 mm track length. $100+£ 1.70$ each

IMI (Kynoch) Ltd. make preset push button potentiometer arrays. Preset FM and TV tuning ..and now AM radio tuning without cumbersome mechanical arrangements. Each button is a multiturn preset potentiometer with an interlock to the other buttons in the bank -..... $100+£ 1.90$ each.


Motorola Ltd. Semiconductor Division, York House, Empire Way, Wembley, Mx tel: (01) 9028836
t|x: 21740

## \% TOKO

TOKO (UK) Ltd., Shirley Lodge, 470 London Road, Slough,
Berks. SL3 8QY tel: (0753) 48444 tlx: 847185


Rivlin Instruments Ltd., Doman Road., Camberley, Surrey GU15 3DJ
tel: (0276) 21107


Imperial Metal Industries (Kynoch) Ltd.,
Components Division,
P.O. Box 216,

Witton, Birmingham B6 7BA.
tel: (021) 3564848
t|x: 336771

All initial enquiries to Ambit International, who will be supplying comprehensive data on the above products.
Ambit International, 37 High Street, Brentwood, Essex. CM14 4RH (0277) 216029

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If you have a sophisticated Ampex Recorder-Align it to the Manufacturers specification using our Alignment Units for F.M. Systems.

Speedy and inexpensive
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One more request item. We met it with a neat little transformer. Now, in two versions, it joins the list of useful Whiteley products, and everyone involved in communications system design will be interested in the protection they provide. Inserted in voice band circuits, they effectively isolate equipment from the hazards of adjacent high voltage power circuits on the 'line' side. High isolation level between line and equipment windings gives protection against voltage surges, lightning strikes and fault conditions. One version is designed for 17 Hz signalling circuits, the other with several voltage ratios also suits a 50 Hz ringing circuit. All are Post Office and C.E.G.B. approved and the second version is also approved with extra protection diodes added. Requests for data sheets welcome. Or if you want to request a product spec of your own - we're always interested!
Surprising how often you'll find


Whiteley Electrical Radio Co. Ltd
Mansfield, Notts NG18 5RW, England. Tel: 062324762

# Join the Digita Teach yourself the latest techniques of digital electronics <br> Computers and calculators are only the beginning of the 

 digital revolution in electronics Telephones, wristwatches, TV, automobile instrumentation - these will be just some of the application areas in the next few yearsAre you prepared to cope with these developments?
This four volume course - each volume measuring $11 \frac{3}{4}{ }^{\prime \prime} \times 8 \frac{1}{4}{ }^{\prime \prime}$ and containing 48 pages - guides you step-by-step with hundreds of diagrams and questions through number systems. Boolean algebra, truth tables, de Morgan's theorem, fhipflops, registers. counters and adders. All from first principles The only initial ability assumed is simple arithmetic

At the end of the course you will have broadened your horizons. career prospects and your fundamental understanding of the changing world around you
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These courses were written so that you could teach yourself the theory and application of digital logic. Learning by self-instruction has the advantages of being quicker and more thorough than classroom learning. You work at your own speed and must respond by answering questions on each new piece of information before proceeding to the nex.t.

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A continuously variable frequency laboratory oscillator with a range $10 \mathrm{~Hz}-100 \mathrm{kHz}$, having virtually zero distortion over the audio frequency band with a fast settling time.

Specification:
Frequency range:
Output voltage:
Output source resistance:

Output attenuation:
Output attenuation accuracy
Sine wave distortion:
$10 \mathrm{~Hz}-100 \mathrm{kHz}$ (4 bands)
10 volts r.m.s. max.
150 ohms unbalanced
(optional 150 ohms unbalanced plus 150/600 ohms balanced/ floating)
$0-100 \mathrm{~dB}$ (eight, 10 dB steps plus $0-20 \mathrm{~dB}$ variable)

Less than $0.002 \% 10 \mathrm{~Hz}-10 \mathrm{kHz}$ (typically below noise of measuring instrument)

Square wave rise and fall time: $40 / 60 \mathrm{n}$.secs.
Monitor output meter.
Scaled 0-3, 0-10, and dBV $110 \mathrm{~V} / 130 \mathrm{~V}, 220 \mathrm{~V} / 240 \mathrm{~V}$
$17^{\prime \prime}(43 \mathrm{~cm}) \times 7^{\prime \prime}(18 \mathrm{~cm})$ high $x$ 83/4"' $(22 \mathrm{~cm})$ deep

Price: 150 ohms unbalanced output: $£ 250$
150/600 unbalanced/balanced floating output. £300

## DISTORTION MEASURING SET, SERIES 3

(illustrated above)
A sensitive instrument with high input impedance for the measurement of total harmonic distortion. Designed for speedy and accurate use. Capable of measuring distortion products down to $0.001 \%$. Direct reading from calibrated meter scale.

## Specification

Frequency range:
Distortion range (f.s.d.):
Input voltage measurement
range:
input resistance:
High pass filter:
Power requirement: Size:
$5 \mathrm{~Hz}_{2}-50 \mathrm{kHz}$ (4 bands) $001 \%-100 \%$ ( 9 ranges)
$50 \mathrm{mv}-60 \mathrm{~V}$ (3 ranges)
47 K ohms on all ranges
$12 \mathrm{~dB} /$ octave below 500 Hz
$2 \times$ PP9, included
$17^{\prime \prime}(43 \mathrm{~cm}) \times 7^{\prime \prime}(18 \mathrm{~cm})$ high $\times$ $8^{3 / 4^{\prime \prime}}(22 \mathrm{~cm})$ deep £200

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the modern way to measure temperature
A Thermometer designed to operate.as an Electronic Test Meter. Will measure temperature of Air, Metals. Liquids. Machinery, etc., etc. Just plug-in the Probe. and read the temperature on the large open scale meter. Supplied in zippered vinyl case with transparent front and carrying loop. Probe, and internal $1 \frac{1}{2}$ volt standard size battery. Model "Mini-On $1^{\prime \prime}$ measures from $-40^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$, price f 17.50 Model "Mini-On Hi" measures from $+100^{\circ} \mathrm{C}$ to $+500^{\circ} \mathrm{C}$, price £20.00 (V.A.T. EXTRA)
Write for further detalls to
HARRIS ELECTRONICS (LONDON), 138 GRAY'S INN ROAD, LONDON. WC1X 8AX ('Phone 01-837 7937)

## The new MS PAGEANT



Mordaunt-Short Ltd. are proud to announce their new high performance loudspeaker system, the MS PAGEANT, incorporating the first transducer of their own formulation and development. By combining high power-handling capacity and exceptional efficiency, the MS PAGEANT achieves accurate reproduction of programme material at truly representative sound levels, while the new Mordaunt-Short bass- and mid-frequency transducer affords outstanding transient response and remarkably low distortion even at large cone excursions.
The MS PAGEANT is thus a full-frequency high-fidelity loudspeaker system to be used to advantage with compatible equipment of virtually any power rating.

Frequency response $60-20,000 \mathrm{~Hz} \pm 3 \mathrm{~dB}$. Sensitivity 6.5 V r.m.s. (5.3 Watts) for 96 dB at 1 metre. Maximum Sound Level 110 dB . Distortion Below $1 \%$ THD, $200 \mathrm{~Hz}-20,000 \mathrm{~Hz}$. Continuous Programme Rating 20 V r.m.s. ( $50 \mathrm{Watts} \mathrm{)}$ contoured noise. Amplifier Power Compatibility 15-100 Watts per channel. Dimensions 533 mm high $\times 330 \mathrm{~mm}$ wide $\times 230 \mathrm{~mm}$ deep.
Recommended Retail Price (U.K.) $£ 102.00$ per pair, plus V.A.T.

## Mordaunt-Short Ltd

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| 64 | 151 ${ }^{\prime \prime}$ | $7 \frac{1}{2}^{\prime \prime}$ | 121 ${ }^{\prime \prime}$ | - | 9.24 | - |
| 65 | 171 ${ }^{\prime \prime}$ | $8 \frac{1}{2}{ }^{\prime \prime}$ | 1212 ${ }^{\prime \prime}$ | - | 10.56 | - |
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Company founded by his lather in 1931. At school the sciences and the school jazz band were his two main interests. At home he was never happier than when designing - anything ir on crysial sets to a forge for melting lead. Following a spell in light engineering the joined Vitavox in 1961. at the age ol 19. Two years of prototype design and a period developing the Company's costing and production control system with his brother Neil. now Managing Director of Vitavox. during when he gained his Institution of Works Managers Certificate and Diploma in Works Management. preceded his appointment as Technical Director in 1969.

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# wireless world 

Electronics, Television, Radio, Audio
JUNE 1975 Vol 81 No 1474

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This month's front cover, showing the tape transport of the RacalThermionic ICR32 communications recorder, a $32 \cdot \mathrm{ch}$ annel machine, introduces the articles on magnetic recording technology in this issue.

## IN OUR NEXT ISSUE

## Digital wrist-watch

Constructional design, using a liquid-crystal display and c.m.o.s. circuitry, gives long battery life

## Active notch filters

Design theory for active circuits to remove single frequency interference such as whistles or hum

## Wireless World Dolby noise reducer

The final article will deal with calibration and use of the unit described in May and June

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## Off the record

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From the Egyptian ivory plaque of 4700 BC to the plastic video disc just on the German market in 1975 AD we have been getting cleverer and cleverer in devising cheap, small, durable media for recording our knowledge, ideas and visions. Passing on the culture is a permanent human obsession - sometimes a very profitable one - and the modern electronics engineer is as much caught up in it as the ancient cave painter or hieroglyphics writer. For several thousand years we have been able to get our information directly off the records simply by looking at them - or listening "live" to the bards. But with mechanical and electrical recording we have given ourselves problems. First of all the information is held on the medium in some special way that calls for reproducing apparatus to make it perceivable. Secondly, the records and reproducers have to be made compatible so that any record can be reproduced in any place it is wanted. Compatibility has become crucial and industrial fortunes can be made or lost on it.

With video records our main preoccupations in the matter of compatibility seem to be with the different recording methods and "standards" adopted by competing manufacturers and with the different television standards used for the reproducers. What everyone seems to have taken for granted is that video records should use television sets as reproducers. Obviously this makes sense in so far as millions of people already have television sets and in so far as we want to record and reproduce broadcast programmes. But the video disc, in particular, has an immensely wide range of possible applications for information storage apart from home entertainment. For example, we may want to use it for holding highly detailed stationary or slowly moving pictures or data - photographs, drawings, diagrams, charts, graphs, text and so on: The television broadcasting system, on the other hand, was designed for presenting moving pictures in "real time" and therefore requires fast scanning, a high information rate and a large bandwidth. To use this for displaying stationary pictures or text would be wasteful from several points of view and would not make the best use of the storage capacity of the video disc (which, for example, might use a whole disc to store one static or slowing moving illustration). As an alternative one could envisage a slow scanning or writing system (e.g. facsimile) with a very fine scanning structure on which two-dimensional information of much higher definition than that possible on the television screen could be presented. Perhaps the television set could be adapted to this requirement.

What of the future? Perhaps, for one thing, we could get rid of the crude necessity of having to mechanically move the recording medium past some transducer in order to obtain our information. What about scanning with light or electron beams, for example? Holography is a possibility. Or perhaps we can develop the idea of digital storage, as used in computers and now coming into sound and vision signal processing, to produce records consisting of binary cells. From these we could extract the information purely by electronic sequential read-out, if a sequential signal is needed, or complete and instantaneous, rather as visual memories come straight from our brain cells. Without doubt the video disc is not the end of the story.

# Digital techniques in recording and broadcasting 

## A summary of recent developments and future trends

by J. Dwyer

It has long been the prevailing view that a properly derived digital signal offers substantial advantages to the sound and television engineer over its analogue equivalent. The most important of these is that the signal to noise ratio of the signal depends on the number of steps into which the signal has been divided and is almost independent of the number of processes the signal is subjected to after the first analogue to digital conversion. Also, the level of the signal when it reaches its destination is not dependent on the gain stability of the circuits or channels through which it has passed, and there are no frequency-dependent phase shifts or other non-linearities during transmission. The signal can be delayed or stored for any length of time without damage. Digital equipment is less likely to need frequent adjustment and maintenance.

Against these advantages a greater bandwidth is needed to transmit a digital signal than its analogue equivalent; a fundamental rule, attributed to Nyquist, Hartley and others, is that the rate at which an analogue signal has to be sampled is twice the frequency of the highest frequency component in the analogue signal. The signal to noise ratio can be improved but only if each sample is defined by sufficient word length.

Operating digital equipment also needs entirely different skills if it is to be used to the best advantage. Some processes which are easy to carry out on analogue signals need more complicated and therefore more costly technology if they are to be used on digital signals, though this effect is mitigated to a large extent by the possibility of multiplexing a number of channels through the same equipment. It may be more convenient to change the signal to analogue form, process it and convert it back, in which case a number of analogue to digital and digital to analogue convertors may be needed in a system, resulting in increased costs.

Perhaps the most serious disadvantage of the digital signal is that poor transmission conditions which would merely deteriorate an analogue signal
may destroy its digital equivalent. A discontinuity in a digital signal may cause a more perceptible disturbance than would result in the analogue.
Nevertheless sound and vision engineers are working towards the day when signals are in digital form from the primary transducer, the microphone or camera, right up to the transmitter and even, in the distant future, up to the receiver ${ }^{2,3}$. In sound engineering much of. the impetus towards digital techniques has been provided by the knowledge that the analogue recorder has reached the theoretical limits of its development and is now proving an obstacle to the reproduction of the highest quality sound.
Perhaps the earliest application of digital techniques to sound engineering came with the realisation that analogue methods did not provide a satisfactory method of delaying a signal. For this reason delay units were built which converted the sound to digital form, delayed the signal, and then reconverted it to analogue form. In the Gotham Delta T101, for example ${ }^{1}$, a word length of ten bits was used to give a theoretical pk -to-pk signal to pk -to- pk noise ratio of 60 dB , which was quite adequate bearing in mind that it would almost certainly be used where its output would form a small part of the overall sound picture and its inherent noise would be masked by the other parts of the final sound signal.

## P.c.m. links

Possibly the best-known use of digital techniques in broadcasting has been the use of pulse code modulation of sound signals for distribution between studios and transmitters. The details of the system have been widely reported elsewhere ${ }^{4.5}$. There is nothing new about p.c.m. It was first described in 1938 by Alec Reeves of Standard Telephone Laboratories. But it was not until semiconductors became widely available that the principle could be applied to a practical system.

The BBC has been using p.c.m. links between Broadcasting House and the Wrotham transmitter since September

14, 1972. Sutton Coldfield was connected in November and Holme Moss in February, 1973. The system is now used for transmitters as far north as Kirk O'Shotts. A BBC engineer said, "The main spine is now complete as far as the length of the country and to the west. Without it," he said, "it's impossible to see how stereo could have reached the rest of the country." Indeed the greatest advantage of the system for stereo coverage is that channels can be decoded at the end much as they were encoded before transmission. It is almost impossible to use two analogue lines over long distances that will transmit the two channels without introducing phase and other changes between them which make the use of such lines for stereo impractical. BBC engineers hope that eventually television coverage can be improved by p.c.m. just as stereo radio has been.

The extension of the p.c.m. system has kept. step with the British Post Office's introduction of digital techniques for ordinary telephone lines and the gradual withdrawal of music lines. In early 1973 the GPO awarded contracts to STC, Plessey and GEC to produce pulse code modulation equipment for use over long distances; 24 -channel p.c.m. links had been used for exchanges up to 30 km apart since 1968. The Post Office installed a trial line between Guildford, Portsmouth and Southampton during 1973 and in December the following year they started field trials to initiate the 1,680 channel, $120 \mathrm{Mb} / \mathrm{s}$ line between Guildford and Portsmouth. The 24 -channel local lines had only been capable of $1.5 \mathrm{Mb} / \mathrm{s}$, and the Guildford line was the first highspeed p.c.m. line of a system that will one day cover the whole of Europe, hence its importance to the BBC and the IBA.

As used at present the p.c.m. radio distribution system uses a sampling frequency of 32 kHz , which happens to be four times the sampling frequency used by the Post Office on digitally coded telephone lines. There are 8,192 equally spaced quantizing levels in each of the thirteen channels, each of whose levels is defined by a 13 -bit binary word
plus a parity bit. To each group of 13 samples are added 11 synchronising bits and five auxiliary bits for transmitter remote control, mono-stereo switching and so on, making up a total "frame" of 198 bits. The total bit rate is thus 6.336 $\mathrm{Mb} / \mathrm{s}$.
These signals are sent down wideband s.h.f. links suitable for television transmission. The BBC have been developing ways to send p.c.m. signals down the $2.048 \mathrm{Mb} / \mathrm{s}$ links which the Post Office is currently developing for digital transmission. Normally only four sound channels could be accommodated on such a link, but the BBC is researching the means of reducing the bit-rate for each channel so that six channels may be transmitted down a link, with a consequent saving in costs. Engineers have estimated ${ }^{6}$ that the existing 13 channel links could carry 24 channels by the same process.
The accuracy with which an analogue waveform can be dismantled, p.c.m. encoded and then reassembled at the receiving end is determined by the sampling frequency and the number of levels into which the maximum value of that waveform has been divided. Each of those levels is assigned a number, and the level to which the amplitude of the waveform is nearest when the sampling instant arrives has its number transmitted. Thus in Fig. $1 Q_{2}$ will be transmitted at instant $t_{1}, Q_{1}$, at $t_{2}, Q_{1}$ at $t_{3}$ and $Q_{4}$ at $t_{4}$. Plainly, if distances $x$ and $y$ are reduced the waveform can be reproduced much more accurately.

It is a measure of the improvement that p.c.m. offers that the signal can actually be improved by adding noise to it. At very low signal levels the distance between quantizing levels becomes an appreciable proportion of the signal magnitude. There is a tendency for small changes in signal level to cause irregular jumps from one quantizing level to another. Since the quantizing jumps may be much larger than the changes in signal level that produced them, the effect can be audible, particularly as some sounds are dying away. The effect is called "crumbling" or "granular distortion".

To counteract it a dither signal is added to the signal which is a square wave, with a frequency of half the sampling rate and an amplitude of half a quantizing level, with a white noise signal superimposed on it. The dither worsens the signal to noise ratio by about 1.5 dB but the resulting noise, if audible, is more continuous and less obtrusive since the dither causes low level signals to cross and recross the quantizing levels at more frequent intervals. The theoretical signal to noise ratio after the dither signal has been added is 70 dB .

The coding error in the transmission can be as much as half a quantizing step, so the quantizing steps have to be made as small as possible. In order to define smaller quantizing steps the number of binary digits which are

transmitted to represent each level must be increased. Each addition of a binary digit to the word length giving the number signifies a doubling of the number of levels and a reduction in quantizing noise of 6 dB . But each addition of a bit to the binary word means an increase in the bandwidth needed to transmit the signal.
Therefore if the bit rate for each word is to be reduced a method has to be found to compress the signal so that changes in level, whether they occur at low level or high, use as many of the available quantization levels as possible. An opposing process has to be applied at the other end to restore the signal to its original proportions.

## Companding processes

Broadly there are two methods of companding: instantaneous and syllabic. The instantaneous method of companding alters the gain of the compressor according to the instantaneous amplitude of the signal. In order for the signal to be reconstructed perfectly the signal going into the expander at the receiving end has to be the same as that which left the compressor on transmission. Over an analogue line of any length this condition clearly cannot be met.

With the syllabic method the gain of the compressor is adjusted by a signal derived from the signal envelope by rectifiers with smoothing constants of some milliseconds, thus the control voltage is not critically dependent on the phase characteristics of the signal path. The BBC rejected analogue syllabic companding for stereo. Although they saved two bits per sample, "the elaborate analogue instrumentation was not attractive on the grounds of cost and reliability." ${ }^{6}$ The method had, in fact, been used for compressing the Sound in Syncs signal but was not considered suitable for stereo since two syllabic companders would have to be
used which had identically matched characteristics. The methods the BBC are developing were based on principles similar to the instantaneous discontinuous companders described by Bartlett and Greszc.7.uk?

The disadvantages already attributed to instantaneous companders do not arise in the case of digital transmission because there are no non-linear effects on the transmitted waveform. The only difficulty is to obtain a correct match between the non-linear characteristics of the compressor at the transmitting end and the expander at the receiving end. This can be overcome by introducing the non-linearity after the analogue to digital conversion. The basis of the method is to compress the quantizing steps for low level signals and to allow the quantizing steps to become larger for signals at higher volume. In effect this means that the quantizing steps in a low level signal correspond to a longer word length than is actually transmitted.

The compression curve normally used in telephony, and presently accepted by European broadcasters, is the seven-segment A companding law shown in Fig. 2. Systems have been built which use fewer segments but it has been found that dividing the signal into a greater number produces no substantial advantages. The slope of the curve indicates the number of bits transmitted, so that although the actual number transmitted, a constant, is represented by the dotted line, at low levels the signal is allowed to pass through that numbers of levels which, if the signal were a linear system, would correspond to a signal word length of $n$ bits. Half-way up the curve the slope is $n-4$, which happens to be the same slope as the dotted line, and therefore coincides with the actual number of bits transmitted. High level signals have to be transmitted at a bit-rate less than the actual number transmitted. The seven segment A law is a continuous companding law.

Bartlett and Greszczuk proposed a companding law that was discontinuous. The system has been described ${ }^{8}$ as similar to the operation of a digital voltmeter provided with automatic ranging. The curve is shown in Fig. 3. A signal that varies between zero and one eighth the maximum signal amplitude can use all the available quantizing levels, and the slope here is such that the bit rate is that of an $n$ bit per sample system. As the level increases the "range" is changed and the signal is allowed to occupy the top half of the available quantizing range. Additional information has to be transmitted to tell the receiving equipment which part of the curve the signal is working in.

All the signals in the proposed BBC system are transmitted with a word length of ten bits, but at low level the distance between quantizing levels is the same as would exist in a 13 -bit transmission system. There are four ranges in the system, corresponding to resolutions of $13,12,11$ and ten bits per sample. A scale factor is transmitted to tell the receiving equipment which of the four ranges of signal level the word is operating in. In truly instantaneous companding systems a scale factor is attached to every word, but the BBC have discovered that a factor is necessary only for about every 30 -word samples. The two-bit scale factor is thus transmitted at intervals of about a millisecond, and indicates the peak value of the word group that follows. For this reason the method has features in common with both the syllabic and instantaneous methods and so is called "near-instantaneous" companding. ${ }^{9}$
If ten bits are used per sample and a two-bit scale factor is transmitted every 30 words then the bit rate per channel at a sampling frequency of 32 kHz is $322.13333 \mathrm{~kb} / \mathrm{s}$. Six channels therefore require $1.9328 \mathrm{Mb} / \mathrm{s}$ which, in a $2.048 \mathrm{Mb} / \mathrm{s}$ link, leaves 115.2 $\mathrm{kb} / \mathrm{s}$ for synchronization, error protection and signalling.

Error protection will be considered
at greater length later on but it has become clear during research that while an error in the most significant bit in each word produces a loud click, an error in the least significant binary digit is imperceptible. Clearly, then, not all of the word needs to be protected against error. Errors in only the first five bits in a linearly coded signal need to be concealed. In a near instantaneous digitally companded signal, however, the most significant bits are only transmitted during a high frequency, high level signal, so there are fewer error-clicks, and only the two or three most significant bits plus the two bit scale factor need protection.

It should be noted that the pro-gramme-modulated noise of the BBC. near-instantaneous digital companding method is less than that of the continuous A law companding method which uses the same number of bits per sample. The BBC method was first described ${ }^{8}$ with the use of an analogue simulation which, when the prototype was built, proved substantially accurate. The prototype is still at the development stage but it is hoped that it will eventually augment existing 13 -bit linear p.c.m. links. A final point here is that there is no distorting interaction, it seems, between near instantaneous companding and any Dolby encoding which may have taken place elsewhere in the chain.

## Digital recorders

One of the most keenly awaited developments in sound engineering has been the arrival of a practical digital sound recorder. Although a commercial tape recorder hasn't yet arrived the BBC had built a prototype as long ago as 1972. The digital recorder needs no bias,

Fig. 2. Seven-segment A law currently in use for telephone communication. $Q$ represents the maximum number of digital codes available.

eliminates wow and flutter problems, has much lower noise and distortion and needs less maintenance than the analogue equivalent. In addition, the signal from such a machine can be delayed for whatever period the engineer wishes.

There is the problem that the recorder needs at least a track for each bit in the word length, so a channel reproducing or recording 13 -bit words needs at least 13 record and 13 replay heads -13 track recording in other words. This has meant that the record process and the replay process each need two heads, the tracks from one interleaving with the tracks from the other. There can, therefore, be difficulties when reading from one head and writing into the other because of the different combinations of head spacings.
The BBC digital recorder ${ }^{10}$ was built as a step along the road to making a digital television recorder, which they produced only two years later ${ }^{11}$ and which was shown at the Grosvenor House hotel 1974 IBC exhibition. When they started on the sound recorder, Howard Jones and Alan Bellis and their colleagues at Kingswood Warren decided that it would have to use ordinary instrumentation tape at a reasonably low speed; high energy tape is difficult to obtain and expensive.

Fig. 5 shows the arrangement. Each channel is sampled at 32 kHz and the two channels are interleaved at a clock rate of 64 kHz in the multiplexer. The levels of these signals are then converted into parallel digital 13 -bit codes to which two parity bits and a channel identification bit are added, making a 16 -bit word for each sample, alternate samples for each channel. The "stuffer" inserts framing pulses into the channel at regular intervals to enable timing correction to be carried out.

One of the most important contributions the digital tape recorder is likely to make to audio engineering is that of timing correction, the principle of which is amply demonstrated in the BBC prototype. There are two types of timing error that can occur in tape recording any type of signal. One is dynamic error of the wow and flutter type and the other is a static error produced by incorrect head alignment; it is not difficult to imagine the result of a small error in azimuth when you consider that the packing density on the prototype stereo recorder was 5,000 bits per inch. Computer tapes have typical packing densities of 1,600 bits per inch. The BBC have progressed since then to machines which use packing densities of 15,000 bits per inch, and it only needs a small error for the digit read at the top of the tape to be several clock periods away from the bit read at the bottom of the tape.

On the recording side, synchronizing pulses eight bits long are inserted into the data every 100 bits. This is done by reading the 100 bits into a store at the
correct rate but reading them out slightly faster. This leaves an eight-bit gap at the end of each 100 -bit sequence into which the eight-bit framing pulse can be inserted. This framing pulse is inserted simultaneously on all sixteen channels. Miller coded (or "delay modulated") data contains its own clock pulse and, on replay, this recorded pulse is used to clock the 108 bits of data into a 100 -bit shift register. The eight framing pulses are lost but by now they have fulfilled their function of steering the data stream through the information store. The record process of reading the data into the store slower than it leaves is reversed, so that although the data may have arrived at the replay store irregularly, as dictated by the speed of the clock pulses derived from the tape signal and misalignments between the top of the tape head and the bottom, they leave at a predetermined, regular rate fixed by the rate of the clock pulse which originally fed the information into the input store during record. Although each of the sixteen channels has a store into which the information is read at a rate determined by its own internal clocks, the information is read out at a rate independent of tape speed, determined by the accuracy of the record-read-in/replay-read-out clock. These circuits have been called stuffers and de-stuffers, for fairly obvious reasons. In the prototype, timing errors of $\pm 0.75 \mathrm{~ms}$ were allowed for and a low bandwidth capstan servo control kept the tape speed within these limits.

The machine had two interleaved eight-track record heads and two interleaved eight-track replay heads. The half-inch 3 M 951 instrumentation tape travelled past them at $15 \mathrm{in} / \mathrm{sec}$. The prototype performed with a signal to noise ratio of 72 dB and the crosstalk, mainly attributable to the analogue input and output circuits, was -45 dB . This machine needed improvement in one respect at least, which was that the inevitable errors produced by tape drop-outs caused gross disturbances to the digital signal which had to be papered over by an error concealment

technique. This meant that, if an error occurred, as indicated by the parity bit or bits, the previous correct word was inserted instead. This method is known as zero order interpolation, and although it was partially satisfactory, the treatment of errors needed further research.

For the next two years the $B B C$ Research Department worked on a digital television recorder, and later, with the lessons they had learned from that, they were able to apply more advanced techniques to the improvement of the sound recorder.

Meanwhile Japanese engineers at Nippon Columbia and the OKl Electric Industry Company ${ }^{12,13.14}$ were developing a p.c.m. sound recorder in co-operation with NHK Research Laboratories. They used serially multiplexed p.c.m. trains on two-inch videotape, which

Fig. 3. Four-range "automatic ranging code" companding law. Q represeuts the maximum number of digital codes available. A two-bit control word has to be transmitted in addition to the $n-3$. word length so that, in its basic form, only one binary digit can be saved per word.

Fig. 4. Block diagram of an experimental single-channel near-instantaneous digital compander: (a) pre-emphasis, (b) limiter, (c) linear 13-bit a/d converter, (d) digital delay, (e) compressor - variable length shift register, (f) multiplexer, ( $g$ ) dither generator, ( $h$ ) measure digital signal magnitude, (i) record and store magnitude, (j) de-multiplexer, ( $k$ ) expander-variable length shift register, (l) linear 13-bit d/a converter, $(m)$ de-emphasis, $(n)$ record and store scale factor.

meant that tape consumption was much higher and the tape more expensive. Although eight channels could be accommodated on the tape there might be difficulty in modifying the signal on one channel without affecting the others. This was one reason why the BBC rejected the vtr method of transverse recording. The use of a vtr also meant that the tape recorder would initially be more expensive. In addition, more parity checking might be necessary with serial pulse trains than parallel trains; errors in longitudinallyrecorded pårallel trains can be corrected by the adjacent tracks.

In the vtr system the sampling rate for each channel was 47.25 kHz and the word length was 13 bits plus a parity bit and a phase check bit. The bit rate was $5.67 \mathrm{Mb} / \mathrm{s}$. To make the signal compatible with those from other vtrs a horizontal scan of the tv signal corresponded with three samples of the eight channels. The clock frequency was 7.1825 Hz . It has to be said that this machine is well past the development stage and has been used particularly for "distortion-free" master disc-cutting. It can work at half speed and an advance head has been fitted to enable the groove to be altered automatically for pitch and depth.

The BBC digital television recorder, when it arrived, used one-inch instrumentation tape at $120 \mathrm{in} / \mathrm{sec}$. Two staggered non-adjustable heads, recorded 42 18-thou wide tracks simultaneously. The picture was of broadcast quality, in colour, and showed no timing or skew errors. At first the machine used error concealment throughout to average between the last and the next correct word, but later they improved it by using error correction techniques. Now two thirds of the errors which occur are concealed and one third are corrected. The first four bits of each eight-bit word must be correct but the other bits are not important in an error period. Another phenomenon which helped the development of the machine was that certain peculiarities of the PAL system enabled sampling to happen at less than the Nyquist theoretical minimum, twice the highest frequency
component of the signal ${ }^{15}$. Later the machine was refined so that repeated successive recordings of a signal could be made; on one occasion they recorded a signal 2,000 times, and it ended up both recognisable and in colour.

## Timing correction

Although error protection for television signals proved easier than that of sound signals, the timing correction of an analogue television signal is much more critical than correcting the timing of a sound signal. Digital timing correction of analogue-recorded television signals is now one of the main uses of digital techniques in television. Once the BBC had built the television recorder they returned to improving the timing and error correction of the sound recorder.

With the packing densities they were using tape drop-outs were potentially much more serious than in an alogue recorder since a single drop-out could eliminate 200 to 300 bits of information, and a drop-out of this kind is potentially much more damaging to a digital signal, as we have seen.

One concealment method was tased on the fact that concealment works fairly well on isolated errors but not on burst errors. They therefore tried to turn the burst errors into isolated errors by "shuffling the pack of signal samples before we record, and then reshuffling them again after." Thus the theory was that burst errors would be redistributed and picked off one by one. They spread the errors so that there would be ten good words between each error and tried zero-order interpolation on the error when it occurred. This technique

Fig. 5. Record and replay channels of a digital recorder ${ }^{10}$ (a) multiplexer, (b) a/d converter, (c) parity generator, (d) stuffer, (e) delay modulation (Miller) coder, (f) record amp., (g) replay amp., (h) differentiator and slicer, (i) clock regenerator, ( $j$ ) delay modulation (Miller) decoder, ( $k$ ) de-stuffer, (l) parity checker, ( $m$ ) concealment unit, ( $n$ ) converter, (o) de-multiplexer.
proved unsuccessful. Similar results' were achieved when first-order interpolation was used with the error redistribution technique, which in any case was based on the perhaps dubious assumption that errors would not be of more than a certain length.

They then decided that they would have to develop a full error correction technique instead of merely concealment. In doing so they made the assumption that although the burst errors could knock out 200 or maybe 300 bits, only one track would be affected at a time. To demonstrate this they recorded the signal among four tracks and on decoding disconnected one of them without any damage to the signal except when drop-outs occurred elsewhere in the other three tracks. They have used a cyclic error code, which works so that the signal word is divided by another number and, if the signal is correct, there is no remainder. If there is a remainder the magnitude of the remainder indicates where the error is, after which it can be corrected. No assumptions are necessary about the length of the error. If two tracks should drop out at once a muting circuit could be introduced for a millisecond.

They had learned enough about timing correction from their work on the television recorder to be able to use an asymmetrical idler wheel on the sound recorder and to remove the wow that it produced. This means that the servomechanism of a digital tape recorder need only be crude enough to keep the average speed of the tape fairly constant. As a result of the work the BBC say that an eight- or sixteen-track machine can now be made at competitive cost and tape consumption with an analogue machine. If the same number of tracks are used on a sound recorder as on the television recorder, ten sound channels can be accommodated on one-inch tape. Further, a drop-out can occur in each of the ten simultaneously as long as two drop-outs don't happen in the same channel at once.

There are still disadvantages. Editing is one of them. You cannot splice a

digitally-modulated tape as you can an analogue one, where the noise of the splice is masked by the signal on the fape. This is because the last code of the pre-edit section has to be married exactly to the first code of the after-edit section and with a packing density of 15,000 bits per inch this is impossible to do without causing a severe disruption of the binary information across the tape. Thus editing will have to be done electronically, just as videotape editing is done. There are also difficulties in simply rocking the tap back and forth over the heads to find an edit point. This, the standard method in analogue recording, cannot be easily done on a digital machine.

Nonetheless a master made on a digital machine is competitive with a 16-track Dolbyed master, and the information is easily updated. Synching with a video picture is simple. Masters can be stored in any number of ways (not necessarily on magnetic tape) such as plastic discs or laser-exposed photographic film, and such methods of storage will not introduce any deterioration in the quality of the master.
But the biggest advantage of all is the improved quality. A typical audio recorder produces second harmonic distortion at 50 dB below peak level and third harmonic at only 34 dB below peak level. The entire measured harmonic distortion of the BBC experimental machine was 68 dB below peak level. It is only when you hear this kind of quality from a tape machine that you realise how bad an analogue machine working at $15 \mathrm{in} / \mathrm{sec}$ on half-inch tape is.

## Digital future?

If the BBC have developed or are developing a digital mixer they're keeping very quiet about it. They have said that a digital recorder could be used in a studio by itself, but it would be far better to design it in conjunction with a digital mixing desk. Functions such as limiters, equalisers, faders have been built individually but putting them into a practical desk, with the necessity to clock all the different functions within it at exactly the same time and with pulses that are phase-coherent, needs serious thought.

There are some processes, such as equalization and panning, which are much more easily carried out on an analogue signal, and it may be better where only one signal is involved to convert to analogue, process and reconvert. Another of the difficulties of extending digital techniques to all parts of sound and television engineering is that experiments must not interfere with continued high-quality broadcasting. So at least in the introductory period there will be parts of the system that are digital and parts that are analogue, which means that there will need to be a lot of analogue-to-digital and digital-to-analogue conversion. This may be expensive and is bound to
degrade the signal. Therefore an estimate has to be made of how many conversions can be made before the degradation becomes unacceptable.
However, it is important to remember that although a digital circuit to carry out a comparatively simple function may be much more complicated and expensive than the analogue version, this does not mean that the digital mixing console will be much more expensive than the types currently in use, since a number of mixing channels can be multiplexed through the same piece of equipment; much of the expense of a modern mixing desk results from the duplication of the same simple function in each of two or three dozen channels. A memory could store each of the individual settings on each channel; modern automated mixing devices are merely crude memory aids for analogue mixing, and in any case no standard method of accomplishing even this has been agreed.
Another area of research is to devise codes that suit various applications and interfaces between the codes. One type of code, say 13-bit linear p.c.m. may be the best for fading, mixing, and signal processing whereas 10 -bit NIDC may be suited to transmission. Another type of modulation may be suitable for recording. Suitable digital-to-digital interfaces therefore have to be designed to convert from one to the other. The European Broadcasting Union is now engaged in trying to reach common standards for these codes.
It will be a long time, therefore, before digital mixing desks begin to appear. The BBC have set themselves a target of about six years or so to develop the necessary equipment, the life expectancy of their present mixing consoles.
A more likely use of digital technology in the near future may be the extension of satellite coverage to replace terrestrial transmitters. Next year the European Satellite Research Organisation will launch an orbital test satellite as a first step towards the international exchange of digital television programmes by satellite. Initially it was proposed that analogue links would be used for television and communications links but now it is possible that digital programme circuits may be used, and the BBC is engaged in examining the technical possibilities.

Anotner possibility is that s.h.f. frequencies might.in future be allocated to digital signals beamed directly to the home via satellite. Extending radio coverage to the last half per cent of the population is very expensive using ground transmitters. A satellite is much more democratic; it will reach anyone in its line of sight. For the BBC such a development might provide a welcome end to all those grumbles about coverage.

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4. Williamson, "The PCM Story," Hi Fi News \& Record Review, Jan. 1974, p.77, and Feb. 1974, p. 299. 6. Cross, Osborne \& Spicer, "Digital sound signals, the present BBC distribution system and a proposal for bit-rate reduction by digital companding." Collected papers of the IBC. 1974, IEE publication number 119, p. 952.
5. Bartlett \& Greszczuk, "Companding in a pcm system." Symposium on transmission aspects of communication networks, London IEE, 1964, pp.183-6.
6. Osborne, "Digital sound signals; further investigation of instantaneous and other rapid companding systems." BBC Engineering, no.96, November 1973, p. 18.
7. Croll, Moffat \& Osborne, "Near-instantaneous digital compander for transmitting six sound programme signals in a 2.048 M bits/s multiplex," Electronics Letters Vol. 9, no. 14, July 12, 1973.
8. Jones \& Bellis, "Digital stereo sound recorder," Wireless World, Vol. 78, no. 1443, September 1972, p. 432.
9. Digital television recording, Wireless World, Vol. 80, no. 1462, June 1974, p. 185.
10. Iwamura, Hayashi, Miyashita \& Anazawa, "Pulse-code-modulation recording system," AES Journal, vol. 21, no. 7, September 1973, p. 535 13. Sato, "PCM recorder, a new type of audio magnetic tape recorder," AES Journal, Vol. 21, no. 7, September 1973, p. 542.
11. Sound recorder uses PCM, Wireless World, vol. 79, no. 1457, November 1973, p. 548.
12. Digital equipment in broadcasting, BBC Designs Department Liaison Unit leaflet distributed at IBC 74.

## Additional sources and suggested reading

The following papers were presented at IBC 74 and are published in the collected papers, IEE Conference Publication Number I19:
16. Fenton \& Bradley, Special effects employing digital pattern generation, p.14.
17. Chambers, Use of digital techniques in television waveform generation, p. 40 .
18. Fletcher, Video analogue to digital converter, p.47.
19. Devereux and Phillips, Bit rate reduction of digital video signals using differential pcm techniques, p. 83.
20. Karuma et al. Digital fields store television standards converter, p. 104.
21. Jones \& Bellis, Experimental approach to digital television recording, p.114.
22. Kitson, Fletcher \& Spencer, Digital time base correction, p. 119.
23. Barnaby \& Crowther, Receiver design concepts for the receipt of digital data from the standard tv signal, p. 249.
24. Hausdorfer, Digital transmission of colourtelevision signals, p. 274.

## APRS 75

## Details for the Association of Professional Recording Studios exhibition

The eighth international exhibition of professional recording equipment is to be held at the Connaught Rooms, Great Queen Street, Kingsway, London WC2 on Thursday, June 19th (10.00-21.00 hrs) and Friday, June 20th (10.00-18.00 hrs). On the right is a list of exhibitors who will be seen at the show. Further information can be obtained from the association's secretary at 23 Chestnut Avenue, Chorleywood, Herts. As this is a trade exhibition, tickets are required and are available from the above address.


Exhibitors



## Ferrograph Professional <br> Studio 8Console



Full logic control. Tape motion sensing.Two speeds.Servo-controlled capstan. Constant tape tension. Directreading tape timer (minutes and seconds). Three editing modes. Provision for synchronisation, remote control and remote display panel. Available for line-in/line-out or with mixing and monitoring facilities.IEC or NAB equalisation. Full or
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# News of the Month 

## Optical stereo for cinema films using Dolby

Dolby Laboratories have now applied their noise reduction technique to stereo optical sound tracks for cinema playback. Previously, multichannel sound in the cinema has been achieved ky adding a magnetic track to film, with a reported cost penalty of $50 \%$. As first reported in the April 1972 issue of Wireless World News, page 171), the Dolby system was orıginally applied in the cinema to single-channel optical sound tracks, with a resultant A-system noise reduction of 10 dB up to 5 kHz , and rising to 15 dB at 15 kHz (if the medium allows). The new format known as the Dolby Stereo Variable Area (SVA) sound track makes possible high quality, low noise stereo theatre sound reproduction. For several years, engineers have been studying new methods of achieving high quality sound reproduction from optical sound tracks of the type now used in the motion picture industry. One result of the work under-
taken by Dolby Laboratories has been the development of an improved, fully compatible, wide-range monaural optical sound track used in a number of films already in circulation. Another has been the installation in more than 350 theatres of the equipment required to play these sound tracks.

The main characteristics of the Dolby SVA track are stated to be: it is fully compatible for projection in any theatre without adjustment, modification or additions, or in theatres equipped to play monaural Dolby optical sound tracks and in theatres equipped with Dolby A stereo playback decoder (the CP100 cinema processor). A special circuit provides secure centre-screen information requiring only two channels on the actual SVA track. Because conventional variable area techniques are used to make and project the stereo track, there is no premium print cost (as for magnetic stripe). The Dolby SVA track has a usable audio bandwidth of 10 kHz . Crosstalk between channels is better than 20 dB separation at all frequencies, being typically $25-30 \mathrm{~dB}$ and signal-to-noise ratio is $61 \mathrm{~dB}(20 \mathrm{~Hz}$ to 20 kHz , unweighted).

## Paging service for London

London is to have a radiopaging service operational in 1976 and the Post Office is now examining what form a national radiopaging service might take. The decision to bring radiopaging - a system in which people carrying pocket "bleepers" can be contacted while on the move - into London follows a successful trial covering 800 square miles of the Thames Valley (see

One of several new TV outside broadcast vehicles, being completed at the Reading plant of Ampex GB. The photograph shows a videotape recorder for colour, ready for installation in the vehicle and (inset) part of the sound mixer installed in the vehicle sound control booth.


News of the Month, February 1973, p.58). The London system will cover 900 square miles and will cater for 20,000 users initially, rising to a maximum of 100,000 . The Post Office is examining the possibility of providing pagers giving two clearly distinctive bleep tones. This would mean that a user would not be limited to phoning one contact point when his receiver "bleeped." To operate the system, eight transmitters will be used, located throughout London. The service will be controlled from a computer centre which will receive calls to pagers and activate the radio signals which set the pagers "bleeping."
A call to the radiopaging device is made by dialling a 10 -digit number. The first four digits are an STD type code common to all radiopagers and these route calls to computer-controlled terminal equipment. The remaining six digits identify individual paging devices. Calls can be made from any telephone in Britain. If the user does not wish to be disturbed, the bleeper can be switched off completely or, with some types of bleeper having a memory facility, incoming signals are stored until the pager is switched on again.
Example of another type of paging system now in operation and providing a useful service is that called overlay paging and which is working over the Glasgow Fire Service's existing radiotelephone network. Fire officers out on inspection or fire prevention duties can be called for operational duties either individually or in groups at the press of a button.

## Electronics at 'A' level

The teaching of Electronic Systems at ' $A$ ' level has, with the approval of the Schools Council, been initiated at nine schools for a trial period of three years*. The trial represents the culmination of six years preparation by Professor G. B. B. Chaplin of the University of Essex with the backing of the National Electronics Council. For the past two years the subject has been taught in an Essex Grammar School and Diplomas have been awarded to successful pupils. In future the Associated Examining Board will assess the results. The syllabus for Electronic Systems comprises three main sections: computer, feedback and communication systems. The syllabus also includes a section on basic electronics. Each main section starts with the human aspects of the system under consideration and then goes on to discuss the fundamental principles involved. Further information can be obtained on both the teaching of Electronic Systems as an ' A ' level subject and the Electronics Link Scheme (concerned with providing technical expertise for those schools which are encouraging the development of project work, involving the use
of electronic techniques, see "National Electronics Council Link scheme," Wireless World, April 1975, p.192) from Professor G. B. B. Chaplin, Department of Electrical Engineering Science, University of Essex, Wivenhoe, Colchester, Essex CO4 3SQ.
*"Electronics in Schools," National Electronic, Review, published by the National Electronics Council, January-February 1975, pp.11, 12.

## High Fidelity 75 success

This year's Spring audio show at London's Heathrow Hotel brought forth a number of new products, most exhibitors having at least one new item to reveal for the first time. The show took place from Tuesday April 8 to Sunday April 13 and about 50 exhibitors represented over 80 brand names.

Several completely new ranges of loudspeaker systems were on demonstration, notably those from Celestion, Mordaunt-Short, Wharfedale, Marsden Hall and Lowther. Other new items included turntables from BSR, an amplifier from Cambridge Audio, a preview of a tuner amplifier with touch controls from Metrosound and a cassette deck with unusual styling from Yamaha. We will be publishing more detailed product information on a selection of items from the show in our next issue. A sentiment expressed by one or two major companies who were not exhibiting was that they were missing out at a well organized show and one at which dealers had shown a lot of interest. Rather a sad final note apparent from the show was a general feeling that the Japanese have a lead over British manufacturers of audio electronic equipment, both in styling and reliability - not necessarily a true state of affairs but one which should prevent any complacency from undermining the abilities and experience of the British audio industry.

## Gulf radar

Bahrein International, the most important airport in the Arabian Gulf and the centre of air traffic control in the region, is to be equipped with automatic secondary surveillance radar - the first to be ordered for a.t.c. in the Gulf area. Its primary radar is also to be up-dated with a 200 nautical mile equipment on 23 cm

The s.s.r. will be the Plessey Series 200, which, in addition to allowing the identity and height of any aircraft equipped with the transponder to be displayed, will show emergency codes, such as "HIJACK," "SOS" in flashing characters on the controller's screen. The primary radar is to be the Plessey AR-5, designed to work in conjunction with the s.s.r. to form a complete traffic control system. (The secondary radar is

These aerial parts (foreground) are produced by photo-developing their patterns on a sheet of brass, excess material being chemically etched away. The result is four identical parts which are assembled into an aerial array. This quick, economic and accurate method of fabrication has been developed by GTE Sylvania Inc.

so called because the returns are not reflections from the aircraft but are signals transmitted by the aircraft transponder when interrogated by the ground control radar.)

## Navel television

Colour telecine has found a new application in the teaching of transcendental meditation. The television production centre of the Students' International Meditation Society is to take delivery of a Marconi B3404 telecine and expect the new capability to play a fundamental part in their teaching programme.

The B3404, which is claimed to be the first machine of its type to have a projector system specifically designed for broadcast work, will produce pictures from 16 mm or 35 mm film or slides and possesses a true instant-start facility with a random-access film programmer for frame selection. The telecine is the second order received by Marconi from SIMS, the society having recently bought five Mk VIII colour cameras for use at Livingston Manor, New York and in a mobile function.

## Solid state radio transmitter

What is claimed to be the first fully transistorized a.m. broadcast transmitter for commercial radio stations has
been developed by Harris Corporation and authorized by the Federal Communications Commission for use by US broadcasters. Transistorized components have replaced the vacuum tubes used in conventional transmitters. The design also incorporates a new modulating technique called "progressive series modulation," on which Harris has applied for patents.

The transmitter is a 1,000 -watt model, the size used by half of the $4,446 \mathrm{a} . \mathrm{m}$. radio stations currently operating in the US and which are now more than ten years old, indicating a substantial replacement market.

## Quintophonic Tommy

Attending a preview at the Leicester Square Theatre, London, of "Tommy," Ken Russell's film based on the rock opera by Pete Townshend and The Who, we had our ears blasted by excessive sound levels in the auditorium and so were unable to assess the niceties of the Quintophonic Sound used for the sound tracks. Quintophonic Sound is so called because it uses five loudspeaker sound sources in the cinema auditorium - a pair at the front, a pair at the rear and a single "voice" speaker at the middle of the screen. At the Leicester Square Theatre there were in fact two pairs of speakers at the rear, and these pairs had corresponding sound outputs.

On the film the sound is recorded on three magnetic tracks. Two of these tracks are matrixed to provide fourchannel sound by the QS system.

# Wireless World Dolby noise reducer 

## 2 - Construction

by Geoffrey Shorter


#### Abstract

This noise reducer design is intended mainly for hiss reduction in magnetic-tape recording machines. The unit described can be switched to decode commercially available Dolby B-encoded cassette tapes, Dolby B-encoded f.m. radio transmissions (current in the USA), or to encode blank tapes from any source. As an alternative it can be used in trading some of the noise improvement for reduced distortion at peak recorded levels. Part 1 in the May issue gave background to the Dolby system and this part gives details of a design that can be built with or without the help of the Wireless World kit.


This Dolby B noise reduction unit can be used with both open-reel and cassette tape machines. It is intended for decoding Dolby B-encoded tapes and f.m. transmissions, and for encoding and decoding your own tapes.

The circuit diagram is split into three parts: the main signal path, Fig. 12 (top), the subsidiary or side path, Fig. 12 (bottom), and the circuitry used in setting up the unit.

The input signal to be processed from the auxiliary, tuner or tape inputs passes via the switching arrangement of Fig. 13 to point D in Fig. 12 (top). In addition to providing 12 dB of gain, $\mathrm{Tr}_{1}$ ensures a proper source impedance for the low-pass filter. Filter components $\mathrm{L}_{1}$ and $\mathrm{C}_{5}$ provide a gradual attenuation ( -3 dB at 28 kHz ), while the 19 kHz filter switch brings in additional components to give a response $\pm 1 \mathrm{~dB}$ at 15 kHz , -31 dB at 19 kHz and -22 dB at 38 kHz .

With high-quality open-reel machines whose response is flat up to 19 kHz , the additional filter may be out of circuit when the source is free from spurious signals. But because the bandwidth of signals into the record processor should be the same as that for signals entering the playback processor for proper matching, it is usually advisable to have the filter in, especially with cassette machines having a fastfalling response. If there is any risk of unwanted signals above audibility, for example from a stereo decoder or tape bias oscillator, the filter must be switched in. If such signals are above the compression threshold the noise reduction will not operate correctly.

The direct-coupled pair $\mathrm{Tr}_{2}$ and $\mathrm{Tr}_{3}$ have a low output impedance for driving the voltage-controlled filter and it is at this point that the signal path is split during encoding. The main signal
path continues via the summing junction following $\mathrm{R}_{14}$

The final directly-coupled amplifier pair $\mathrm{Tr}_{4}$ and $\mathrm{Tr}_{5}$ must be inverting because on decoding the subsidiary or side signal path is arranged to form a feedback path from its output to input via $R_{15}$ (See Fig. 9c May issue).

For encoding, the signal at point $A$ passes via a series of switches to point B in the side-path section, Fig. 12 (bottom), and is returned to point E after processing. Point $G$ feeds the meter amplifiers. The processed output is available at $C$, passing through the switching arrangement of Fig. 1,3 to the record output socket, Skt $_{1}$, pin 4.

In decoding, the signal is taken from a recorder via pin 5 of $\mathrm{Skt}_{1}$ to point D . The output from $\mathrm{Tr}_{4}, \mathrm{Tr}_{5}$ at point C is passed to the side path at $B$, through switch $\mathrm{Sw}_{1 \mathrm{~b}}$ in Fig. 13. Decoded output appears at $\mathrm{Skt}_{2}(\mathrm{pin} 5)$ via $\mathrm{Sw}_{1 \mathrm{c}}$.

From the side-path dynamic filter, whose operation was described in the May issue, the signal is amplified by 26 dB by $\mathrm{Tr}_{6}$ and $\mathrm{Tr}_{7}$, and extracted at the overshoot suppression diodes, $\mathrm{D}_{2}$ and $D_{3}$. When combined with the main path signal via $R_{15}$ this results in either a boost of up to 10 dB during encoding or a loss of up to 10 dB during decoding. (Diode $D_{1}$ forms part of a temperature compensation network for the f.e.t. bias.) The variable time-constant con-trol-voltage circuit, following $\mathrm{Tr}_{8}$ and described last month, also provides an a.c. signal of half the f.e.t. drain voltage. This signal, obtained by attenuating the $26-\mathrm{dB}$ amplified signal with $\mathrm{R}_{37}$ and $\mathrm{R}_{44}$, is passed through $C_{20}$ to linearize f.e.t. operation.

Setting-up circuitry (in kit version) Because this noise reduction unit can be used with a variety of tape recorders,
the side-path includes its own 400 Hz oscillator so that a standard-level tone can be recorded, played back and the processor calibrated for the particular tape used. The 400 Hz tone is obtained by switching the side-path circuit ( $\mathrm{Sw}_{3}$ ), to form a Wien-bridge oscillator with $\mathrm{R}_{46}, \mathrm{C}_{27}, \mathrm{C}_{26}$ and $\mathrm{R}_{45}$ around $\mathrm{Tr}_{106}{ }_{107}$ \& $\mathrm{Tr}_{108}$. Oscillator output is taken from point $E$ and applied via point $F$ to the processor input, D, by $\mathrm{Sw}_{3 \mathrm{c}}$ and $\mathrm{Sw}_{3 \mathrm{a}}$. Switch $\mathrm{Sw}_{3 f}$ alters the control time constant to prevent oscillator instability. Potentiometers P.V $\mathrm{V}_{3}$ and $\mathrm{RV}_{103}$ are used to set the level of the 400 Hz tone for both left and right channels respectively, but only the left-channel sidepath circuit is wired to oscillate. This adjustment, and that of $R V_{1}, 101$ and $R V_{2,102}$, are made with the aid of the right channel meter, calibrated in the kit design by a further oscillator (Fig. 14). This oscillator provides a well-defined output of 580 mV , whose accuracy is determined by the supply line regulation of $5 \%$.

For the kit design the oscillator of Fig. 14 , including the components shown by the broken lines and with its output feeding the attenuator of $\mathrm{R}_{60}$ and $\mathrm{R}_{61}(\mathrm{a})$, provides the 580 mV signal to calibrate the meter. After this calibration, $\mathrm{R}_{48}$ and $R_{57}$ are removed and the second network, (b), of Fig. 14 wired in to provide a 5 kHz sinewave source for aligning the circuit. The input filter coil $\mathrm{L}_{2}$ is used temporarily in this oscillator.
The two meter circuits of the kit design use two parts of an LM3900 Norton or current-differencing amplifier in a "perfect diode" arrangement, Fig. 15. Because the circuit is set-up at low levels, $\mathrm{R}_{55}$ is temporarily reduced in value to increase sensitivity for these measurements. Additional current gain is provided by $\mathrm{Tr}_{9}$. Only the right-chan-


Fig. 12. Circuit of one channel of the stereo Dolby B noise reduction unit. Upper circuit is of main signal path, input at $D$, output at $C$. Point $G$ feeds meter circuits of Fig. 15, while point A or point $C$ feeds the side-path input $B$ (bottom), according to whether encode
or decode is switched by the interface circuit of Fig. 13. Side-path output from $E$ is combined with main signal via $R_{15}$. Connection shown with broken line forms a Wien bridge oscillator to provide a $400-\mathrm{Hz}$ calibration tone. Output is via oscillator level controls
$R V_{3,103}$ and feeds point F in Fig. 13. This additional circuitry, including potentiometers and $S w_{3 b-e}$ is used on one channel only (the left channel in the kit design). Resistor $R_{33}$ is omitted in left channel if used as an oscillator.

## Components

Electrolytic capacitors are 16 -volt working (except $\mathrm{C}_{24}, \mathrm{C}_{14},{ }_{114}, \mathrm{C}_{29}$, and $\mathrm{C}_{31},{ }_{131}$. Polystyrene capacitors may be marked with a " $k$ " multiplier instead of " n ". (Polyester capacitors are colour coded.)

| $\mathrm{C}_{1,101}$ | $10 \mu$ electrolytic |
| :---: | :---: |
| $\mathrm{C}_{2,102}$ | 3n 5\% polystyrene |
| $\mathrm{C}_{3.103}$ | 3.9n $5 \%$ polystyrene |
| C. ${ }_{4} 104$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{5,105}$ | 2.2n $5 \%$ polystyrene |
| $\mathrm{C}_{6,106}$ | $5.6 \mathrm{n} 1 \%$ polystyrene |
| $\mathrm{C}_{7,107}$ | 27n 1\% polystyrene |
| $\mathrm{C}_{8,108}$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{9,109}$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{10.110}$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{11, \ldots 1}$ | 4.7n $1 \%$ polystyrene |
| $\mathrm{C}_{12,112}$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{13.113}$ | 100 n metallized polyester |
| $\mathrm{C}_{14.114}$ | 47 or $50 \mu 6$-volt electrolytic |
| $\widetilde{\mathrm{C}}_{15,1115}$ | 100 n metallized polyester |
| $\mathrm{C}_{16,116}$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{17,117}$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{18,118}$ | 100 n metallized polyester |
| $\mathrm{C}_{19.119}$ | 100 n metallized polyester |
| $\mathrm{C}_{20,120}$ | 330 n metallized polyester |
| $\mathrm{C}_{21,121}$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{22.122}$ | 22p polystyrene |
| $\mathrm{C}_{23.123}$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{24}$ | $1000 \mu 25$-volt electrolytic |
| $\mathrm{C}_{25}$ | $10 \mu$ electrolytic |
| $\mathrm{C}_{26}$ | 10 n metallized polyester |
| $\mathrm{C}_{27}$ | 47n metallized polyester |
| $\mathrm{C}_{28}$ | 100 n metallized polyester |
| $\mathrm{C}_{29}$ | $10 \mu 10$-volt electrolytic |
| $\mathrm{C}_{30}$ | 33n metallized polyester |
| $\mathrm{C}_{31,131}$ | $10 \mu 10$-volt electrolytic |
| $\mathrm{C}_{32,132}$ | 330n metallized polyester |
| $\mathrm{C}_{3}$ | 1.5 n disc ceramic |
| $\mathrm{C}_{\mathrm{x}}$ (two) | $2.7 \mathrm{n}^{*}$ polystyrene |

*Values for 50 to $25 \mu$ s change in time constant. For 75 to $25 \mu$ s change, as in USA, use 1.8 nF and $39 \mathrm{k} \Omega$.

Resistors $1 / 4$-watt, $5 \%$ tolerance unless otherwise stated.

| $\mathrm{R}_{1,101}$ | 470k | $\mathrm{R}_{33}{ }^{+}$ | 22k |
| :---: | :---: | :---: | :---: |
| $\mathrm{R}_{2.102}$ | 47k | $\mathrm{R}_{34,134}$ | 120k |
| $\mathrm{R}_{3,103}$ | 1 k | $\mathrm{R}_{35,135}$ | 47k |
| $\mathrm{R}_{4,104}$ | 470 | $\mathrm{R}_{36,136}$ | 2.7 k |
| $\mathrm{R}_{5,105}$ | 43k | $\mathrm{R}^{37,137}$ | 1k 2\% |
| $\mathrm{R}_{6.106}$ | 100 | $\mathrm{R}_{38,138}$ | 47 |
| $\mathrm{R}_{7,107}$ | 6.8 k | $\mathrm{R}_{39,139}$ | 15k |
| $\mathrm{R}_{8,108}$ | 2.2k | $\mathrm{R}_{40.140}$ | 270k |
| $\mathrm{R}_{9.109}$ | 820 | $\mathrm{R}_{41,141}$ | 270k |
| $\mathrm{R}_{10.110}$ | 180 | $\mathrm{R}_{42.142}$ | 220k |
| $\mathrm{R}_{11,111}$ | 270k | $\mathrm{R}_{43.143}$ | 8.2 k |
| $\mathrm{R}_{12,112}$ | 3.3k | $\mathrm{R}_{4 \text { 4, 144 }}$ | 33 |
| $\mathrm{R}_{13.113}$ | 33k | $\mathrm{R}_{45}$ | 27k |
| $\mathrm{R}_{14,114}$ | 150k 2\% | $\mathrm{R}_{46}$ | 6.8k |
| $\mathrm{R}_{15.115}$ | 180k $2 \%$ | $\mathrm{R}_{47}$ | 1M |
| $\mathrm{R}_{16,116}$ | 27k | $\mathrm{R}_{48}$ | 1 M |
| $\mathrm{R}_{17,117}$ | 22k | $\mathrm{R}_{49}$ | 4.7 k |
| $\mathrm{R}_{18 \mathrm{a} .118 \mathrm{a}}$ | 150k | $\mathrm{R}_{50}$ | 2.2 M |
| $\mathrm{R}_{18 \mathrm{~b}, 118 \mathrm{~b}}$ | 150k 2\% | $\mathrm{R}_{51}$ | 3.9M |
| $\mathrm{R}_{18 \mathrm{c}, 118 \mathrm{c}}$ | 10k | $\mathrm{R}_{52.152}$ | 560 |
| $\mathrm{R}_{19,119}$ | 1k | $\mathrm{R}_{53,153}$ | 150k |
| $\mathrm{R}_{20.120}$ | 33k | $\mathrm{R}_{54,154}$ | 150k |
| $\mathrm{R}_{21.121}$ | 3.3k 1\% | $\mathrm{R}_{55}$ | 330k 2\% |
| $\mathrm{R}_{22.122}$ | 47k | $\mathrm{R}_{155}$ | 330k |
| $\mathrm{R}_{23,123}$ | 2.2k | $\mathrm{R}_{56,156}$ | 330k |
| $\mathrm{R}_{24,124}$ | 6.8 k | $\mathrm{R}_{57,157}$ | 1 k |
| $\mathrm{R}_{25.125}$ | 2.7 k | $\mathrm{R}_{58}$ | 10k |
| $\mathrm{R}_{26.126}$ | 1 M | $\mathrm{R}_{59}$ | 3.9 M |
| $\mathrm{R}_{27,127}$ | 1.8 M | $\mathrm{R}_{60}$ | 110k 2\% |
| $\mathrm{R}_{28.128}$ | 1 k | $\mathrm{R}_{61}$ | 10k 2\% |
| $\mathrm{R}_{29,129}$ | 15k | $\mathrm{R}_{62}$ | 15k 2\% |
| $\mathrm{R}_{30,130}$ | 6.2 k | $\mathrm{R}_{63}$ | 6.8k |
| $\mathrm{R}_{31,131}$ | 8.2k | $\mathrm{R}_{64}$ | 82 |
| $\mathrm{R}_{32.132}$ | 10k | $\mathrm{R}_{\mathrm{x}}$ (two) | 18k* |
| $\dagger$ Two needed if cal. osc. not used. |  |  |  |
| Transistors |  |  |  |
| $\operatorname{Tr}_{1,101}, \operatorname{Tr}_{5},{ }_{105}$ 2TX109C, BC109C or equivalent |  |  |  |
| $\begin{aligned} & \operatorname{Tr}_{2,100} \operatorname{Tr}_{4,104} \operatorname{Tr}_{6.100} \operatorname{Tr}_{8,109} \operatorname{Tr}_{9} \text { ZTXAll } \\ & \text { or ZTX109, BC109, etc. } \end{aligned}$ |  |  |  |
| $\mathrm{Tr}_{3}$, ,103, $\mathrm{Tr}_{7},{ }_{107}$ ZTXA21, 2 N 4058 equivalent |  |  |  |
| f.e.ts (two) $\overline{2} N 5458$, MPF104, 2SK30D or GR specially selected. |  |  |  |

Diodes
$\mathrm{D}_{1.10 \mathrm{p}} \mathrm{D}_{4.104} \mathrm{D}_{10.11} \quad$ OA9
$D_{2,102} D_{3.103} D_{5.105}, D_{110.111} 1 \mathrm{~N} 914$
$\mathrm{D}_{6.9} 1 \mathrm{~N} 4001$ or 1 N 4002
ZD 1 , ${ }_{101} \mathrm{BZV19C} 8 \mathrm{~V} 2$ (8.2V zener E-line package)
$\mathrm{IC}_{1} \quad \mathrm{LM} 3900, \mathrm{MC} 3401$ or MC3311
IC $_{2}$. L131 or TDA1415

## Potentiometers

| RV ${ }_{1,101}$ | 5 k or 4.7 k lin. preset (law) |
| :---: | :---: |
| $\mathrm{RV}_{2.102}$ | 470 lin. preset (gain) |
| $\mathrm{RV}_{3,103}$ | 50 k or 47 k lin. preset ( $400-\mathrm{Hz}$ osc. level) |
| $\mathrm{RV}_{4.104}$ | 50 k or 47 k log. preset (play cal.) |
| RV ${ }_{5}$ | 5 k or 4.7 lin. preset ( 5 kHz osc. level) |
| $\mathrm{RV}_{6,106}$ | 20 k log. preset (record cal.) |
| $\mathrm{RV}_{7,107}$ | 5 k or 4.7 k log. preset (f.m.cal.) |
| $\mathrm{RV}_{8,108}$ | 1k lin. preset (meter cal.) |
| $\mathrm{RV}_{9}$ | 50k dual $\log$ /reverse $\log$ (record balance) |
| $R V_{10}$ | 50 k dual $\log$. (record level) |
| RV ${ }_{11}$ | $5 k$ dual log. (output level) |

## Inductors

$\mathrm{L}_{1.101} 36 \mathrm{mH} \pm 5 \%$ (Toko 30569 in kit)
$\mathrm{L}_{2,102} 23 \mathrm{mH}, \mathrm{Q} \geqslant 60$ (Toko 30568 in kit)
Transformer $240 / 17 \mathrm{~V}$ nominal
Other parts (all supplied in kit)
Dual $200-\mu \mathrm{A}$ meter, plastic foam wire-ended $14-\mathrm{V} 40-\mathrm{mA}$ lamp $\bullet$ fuse and holder - 7-button switch unit, 6 -pole switch $\left(\mathrm{Sw}_{3}\right)$, mains switch two printed boards o three knobs - three DIN sockets chassis, front panel, screws, tag strip, meter bracket labels, connecting wire, mains lead, strainrelief bush © cabinet.
nel meter is used to measure the low levels.

## Circuit options

The unit can of course be constructed without using the kit. Provided that normal good practice is followed in circuit construction, assembly on Lektrokit or Vero circuit boards should be no problem. But for those constructors unfamiliar with normal practice, we recommend using either the full kit or a smaller p.c. board. This smaller board is for a single-channel processor without the switching and setting-up circuitry of the full stereo board, and is available separately.
If similar functions to those of the kit are required the same switching arrangements of Fig. 13 can be used. Selected field-effect transistors are available separately through Wireless World (see panel).
The simplest possible circuit option is for playback of B-encoded cassettes. Designed for use as a noise reduction unit, the circuits have many more facilities than required for a playbackonly processor; nc vertheless, Fig. 12 can
be used in this application with an enormous simplification of the switching. The circuit can be permanently wired in the decode mode, and needs only the switch $\mathrm{Sw}_{4}$ in Fig. 13. Point C is permanently wired to point B via $\mathrm{Sw}_{4}$ and the signal from the head amplifier wired to point $D$ via the play cal. control. The filter components can be omitted if use is to be always limited to playback of recorded cassettes.

Inclusion of the facility for decoding B-type f.m. transmissions can be added to this basic design simply by retaining $\mathrm{Sw}_{2 \mathrm{a}}$ and $\mathrm{Sw}_{1 \mathrm{a}}$ and associated input circuitry. More simply, the two switches can be combined into one.
Maximum cost-effectiveness is clearly obtained with the encode/decode version, as almost all of the circuitry is common to both modes - see Fig. 9, May issue, page 204. The first basic simplification possible of this switchable family is omission of the f.m. facility. Switch $\mathrm{Sw}_{2}$ is eliminated, being permanently wired in the position shown in Fig. 13.
If a separate audio oscillator is available, the circuit of Fig. 14 version
(b), need not be used. If the unit is to be built into a tape machine you may wish to omit the meter circuits, and adopt a simpler switching scheme. But you would then need an a.c. millivoltmeter for setting up. The 400 Hz oscillator wiring, shown by the broken line in Fig. 12, could also be omitted if the same tape is always used. We recommend retention of this feature to take account of tapes with different sensitivities (see part three)

## Setting-up procedure

For proper operation, the encoding and decoding signal processors and the intervening signal channel must be matched at all frequencies of interest and all levels. Any errors in channel gain, on a wideband or frequency-selective basis, can produce a mismatch, or error, in overall response. But first, the circuit must be adjusted to provide the correct degree of low-level h.f. emphasis and de-emphasis (10dB at 5 kHz ), and the correct threshold level. Matching between encode and decode modes must be checked. Then the processor must be level-matched to the

equipment and media (tape of t.m. radio) it is to be used with; to be covered in part three.

If the circuit of Fig. 12 is constructed without using the kit, apply the following setting-up procedure (see part 3 for kit). You will need an a.c. millivoltmeter and an oscillator, unless you adopt the technique using the circuits of Fig. 14 \& 15 , as in the kit design.
Before starting, make sure that the f.e.t. gates are shorted to earth. Start in the record mode with the noise reduction switched out (also the cal. tone off and the filter out, if used).
-Set law control RV ${ }_{1}$ to produce maximum positive voltage on the f.e.t. source.
-Feed in 5 kHz signal at a level to give 17.5 mV at test point 1 and note signal level at test point 2.
-Switch in noise reduction and adjust gain control $R V_{2}$ to give a $10 \pm 0.25 \mathrm{~dB}$ rise at test point 2 . Note signal level*.
-Remote f.e.t. gate short and adjust law control $\mathrm{RV}_{1}$ for a $2 \pm 0.25 \mathrm{~dB}$ drop at test point 2.
-Replace gate short and check that level returns to that identified by*. Finally, remove gate short.

Encode/decode matching check. Without altering the control settings, switch to play mode.

Fig. 13. Switching interface for one channel of Dolby B processor allows decoding and encoding of tapes, recording and simultaneous decoding Dolby f.m. transmissions (current in the USA), encoding of normal f.m. transmissions, and a normal signal for monitoring during recording.
This arrangement is used in the kit design, but could be simplified in other constructions, for instance by omitting Dolby f.m. provision given by $S w_{z}$ Switch $S w_{3 a}$ appears in both channels, but remainder of $\mathrm{Sw}_{3}$ is used in one channel only. Pin numbers on kit DIN sockets are indicated for both channels (dashed boxes for left).
-Switch out noise reduction and short f.e.t. gate.
-Feed in 5 kHz signal at a level to give 44 mV at test point 2 .
-Check that signal drops by $10 \pm 0.5 \mathrm{~dB}$ when noise reduction is switched in.
-Remove gate short and switch in noise reduction. Check that signal at test point 2 is $17.5 \mathrm{mV} \pm 0.5 \mathrm{~dB}$.

Decode-only processor. As with the switchable encode/decode version, ensure that f.e.t. gates are shorted to earth, and switch noise reduction off.
-Set law control RV to pinch-off f.e.t. i.e. maximum positive voltage on source.
-Feed in 5 kHz signal to give a level of 44 mV at test point 2 .
-Switch in noise reduction and adjust gain control $\mathrm{RV}_{2}$ to give a fall of $10 \pm 0.25 \mathrm{~dB}$ at test point 2 . Note signal level*.
-Remove gate short and adjust law control $R V_{1}$ to give a rise of $2 \pm 0.25 \mathrm{~dB}$ at test point 2 (should be 17.5 mV ).
-Replace f.e.t. gate and check that level returns to that indicated by*
-Remove gate short.
Meter and oscillator calibration. If the meter circuits are to be fitted, calibrate them by applying a 580 mV tone and adjusting for a 0 dB reading. One of the meters can then be used to calibrate the 400 Hz oscillator level, if used. (The circuit of Fig. 14 from the kit design could be used if fed from a sufficiently well-regulated supply line; $5 \%$ in the circuit of Fig. 12.)
-Apply input signal to point $D$ to give 580 mV at point $G$.
-Adjust $\mathrm{RV}_{8}$ for 0 dB meter reading.
-Operate cal. tone switch (if oscillator fitted).
-Adjust $\mathrm{RV}_{3}$ to give 0 dB meter reading.
The unit is now rearly for use. But to

Fig. 14.Oscillator circuit used in kit for generating a $1-\mathrm{kHz}$ tone (a) for calibrating the meters. Though a square wave, the magnitude is chosen to give the same reading as a $580-m V$ sine wave. Circuit is subsequently used to provide a $5-\mathrm{kHz}$ circuit alignment tone at (b) by temporarily using $L_{z}$

Fig. 15. Meter circuits using "perfect" diode arrangement. Right-channel meter circuit at bottom includes extra gain to allow measurement of low signal levels during alignment.
ensure compatibility with commercial-ly-available Dolby tapes, and to ensure interchangeability of tapes from machine to machine, it must be calibrated using a level-setting tape, to be detailed in part three of this article.

## Kit construction

Successful operation of the unit depends on a number of factors. As well as proper matching of the unit, strict adherence to component tolerances and alignment procedure, use of selected f.e.ts, and a low ripple in the supply line are all essential to correct operation. For these reasons the parts for the unit are available as a complete kit.

The printed board of the kit is designed to keep wiring to an absolute minimum; it is for this reason that switches, calibration controls, and DIN sockets are board-mounted types. First thoughts indicated a double-sided board would be needed together with platedthrough holes, but this would make an expensive board. The same effect could be achieved with a larger single-sided board but would result in a large number of links. The relatively large number of controls finally decided the format. To keep board length down, some controls had to be mounted above others, and as there was to be a minimum of wiring, the top controls are mounted on to a separate board. The advantage of this sandwich board technique is a saving of about 24 links.

In the instructions, component numbers for the left-channel have 100 added to the number for the right channel: thus $\mathrm{R}_{121}$ is the left channel component corresponding to $\mathrm{R}_{21}$ in the right channel.

## Kit assembly instructions

A number of pins are supplied with each kit; in fitting them insert from the track side of the board, tap down lightly with a hammer and solder into place. Insert pins as follows

[^2]
close to $\mathrm{C}_{32}$ (see Fig. 16)
-three pins in the $L_{2}$ position, marked with broken lines, next to $\mathrm{IC}_{1}$
-one pin at the 5 kHz oscillator output point, marked "osc"
-six pins in the holes marked $E, R, L$; $E, r$ and 1 between socket $\mathrm{Skt}_{3}$ and $\mathrm{C}_{7}$
There are seven links to be inserted on the main board; two further links are used if a tuner is to be connected to the auxiliary input socket, rather than the tuner input. The two f.e.t.-gate links should be looped, to allow easy breaking and making of the gate during alignment. Close-tolerance components, i.e. resistors of $2 \%$ tolerance or
better and capacitors of $5 \%$ tolerance or better, are separately packed.
-Insert seven or nine links, as appropriate.

- Mount close-tolerance resistors $\mathrm{R}_{21,121}-\mathrm{R}_{14,114}-\mathrm{R}_{15,115}-\mathrm{R}_{18 \mathrm{~b} ; 118 \mathrm{~b}}$ $-R_{37,137}$.
-Follow with close-tolerance capacitors $\mathrm{C}_{2,102}-\mathrm{C}_{3,103}-\mathrm{C}_{6,106}-\mathrm{C}_{7,107}$ $-\mathrm{C}_{11,111}$.
-Mount the remaining fixed resistors and capacitors identified on board, excepting $\mathrm{C}_{30}, \mathrm{R}_{47}, \mathrm{R}_{55,155}$.
Make sure electrolytic capacitors are inserted the correct way round, that is, indented end to the hole marked + . Note that $R_{58}$ to $R_{64}, R_{x}$ and $C_{x}$ will be

left over, in addition to the four components already mentioned.
-Add pre-set potentiometers $\mathrm{RV}_{1,101}$ $-R V_{2,102}-\mathrm{RV}_{3,103}-\mathrm{RV}_{4,104}-$ $R V_{5}-R V_{8,108}$.
There are four types of diodes, easily identified by the quantities supplied. Zener diodes have the connections of the E-line package, the + lead corresponding to the collector position in Fig. 17. Of the others, the OA91 germanium diodes will be the largest and glass-encapsulated; the rectifier diodes will be the four plastics-encapsulated ones; and the 1 N 914 s should be the smallest, of either glass or plastics. The band-end is to correspond with + on the board. Base connections for the transistors are shown in Fig. 17. The field-effect transistors may have various markings but nevertheless will have been specially selected. Transistors $\mathrm{Tr}_{1,101}$ and $\mathrm{Tr}_{5,105}$ must be type ZTX109C, but the remaining n-p-n type may be supplied as either ZTXAll or 109 C . $\mathrm{IC}_{1}$ is located so that the end having the indent or other marking corresponds with the board marking. Solder next in place
- diodes $\mathrm{ZD}_{1,101},-\mathrm{D}_{1,101}$ to $\mathrm{D}_{5,105}, \mathrm{D}_{6}$
to $\mathrm{D}_{9}, \mathrm{D}_{10,10}$ and $\mathrm{D}_{1,111}$ to $\mathrm{D}_{9}, \mathrm{D}_{10,110}$ and $\mathrm{D}_{11,111}$
-transistors $\mathrm{Tr}_{1,101} \operatorname{Tr}_{5,105}$ (ZTX109C), $\mathrm{Tr}_{3,103}$ and $\mathrm{Tr}_{7,107}$ (ZTXA21), fieldeffect types, followed by remainder -integrated circuits $\mathrm{IC}_{1} \mathrm{IC}_{2}$.
When positioning the three DIN sockets make sure they are vertical and in line with each other, for appearance's sake. Check functioning of the push-button switches as they are difficult to remove once soldered. As the switch board markings will be covered by the

Fig. 16. Main board markings show seven essential links plus two optional links, for use if a tuner is to be applied to auxiliary socket. Some pin locations are shown. (Boards in kit have a slightly different track arrangement.)

Fig. 17. Socket connections, viewed from "holes". If E-line zener diode is used, as supplied in kit, the + sign on the board should correspond with the position of the collector lead in the E-line package shown right.
switches, identify them before assembly. Take care to push them fully into the board and ensure that they fit squarely: any skew will result in misalignment with the front panel. Fit and solder

> -three DIN sockets
> - switches $\mathrm{Sw}_{1}$ to $\mathrm{Sw}_{6}$
> -inductors $\mathrm{L}_{1}, \mathrm{~L}_{101}, \mathrm{~L}_{102}$, but not $\mathrm{L}_{2}$.

## Sub-printed board

Components are fitted on to the track side of the subsidiary printed board.
-Solder components $\mathrm{C}_{\mathrm{x}}, \mathrm{R}_{\mathrm{x}}$.
-Solder potentiometers $\mathrm{RV}_{6.106}$, $\mathrm{RV}_{7,107}$.
-Attach plastics adjuster inserts into $\mathrm{RV}_{6}, \mathrm{RV}_{7}$.
-Cut off potentiometer legs flush with the board.
The sub-board should be spaced about 0.09 in away from the top of the main switches to ensure potentiometer

centres line up with the front panel holes. Matchsticks form convenient spacers.
-Lay matchsticks on $\mathrm{Sw}_{2 \mathrm{a}}$ and $\mathrm{Sw}_{1}$
-Position sub-board, check alignment and solder

- Join areas on sub-board marked R, $\mathrm{L}, \mathrm{r}, \mathrm{I}$ to corresponding points on main board using twin-screened cable. Earth at one end only to points marked E.
-Connect link point on sub-board to link point on main board almost underneath.
-Insert links marked "Mpx" for use with $25-\mu \mathrm{S}$ B-Type f.m. transmissions.
Returning to the main board, be careful to align potentiometer spindles horizontally.

[^3]

Complete kits for the Wireless World Dolby B noise reducer are available through the address given below. The two-channel design features:

- a weighted noise reduction of 9 dB
- switching for both encoding (low-level h.f. compression) and decoding
- a switchable f.m. stereo multiplex and bias filter
- provision for decoding Dolby f.m. radio transmissions (as in USA)
- no equipment needed for alignment
- suitability for both open-reel and cassette tape machines

The kit includes:
-complete set of components for a stereo processor
-regulated power supply components
-board-mounted DIN sockets and push-button switches
-fibreglass board designed for minimum wiring
-solid mahogany cabinet, chassis, two meters, front panel, knobs, mounting screws and nuts.
Price is $£ 43$ inclusive.
A single-channel printed-circuit board, including components costs $£ 8.63$. inclusive (excluding edge connector, $£ 1.37$ extra). Selected
field-effect transistors cost 68p each inclusive, $£ 1.20$ for two and $£ 2.20$ for four.

Calibration tapes are available, costing $£ 1.94$ inclusive for $9.5 \mathrm{~cm} / \mathrm{s}$ open-reel use and for cassette (specify which).

Send cash with order, making cheques payable to IPC Business Press Ltd, to:

Wireless World noise reducer
General sales department
Room 11, Dorset House,
Stamford Street
London SE1 9LU
Allow three weeks for delivery.
shorting and dry joints.
-Crop leads to avoid touching chassis.
-Insert thin sheet of card between board and chassis.
-Fix board in position with 6BA screws.

Off-board assembly. Fix in position
-transformer
-fuseholder
-mains switch to meter/switch bracket
-bracket with tag strip under one screw.

At this point you can tape the meter to the bracket temporarily with the piece of foam plastic material between; normally the meter will be held in position by the front panel. Continue with off-board wiring
-transformer secondary to two points of tag strip (not earth tag)
-the two tags to $\mathrm{V}_{\text {in }}$ terminals on board
-meter illumination lamp, in series with $R_{64}$, to the two tags, the junction to a third tag (not earth tag)
-meter terminals to $\pm$ M.R. and $\pm$ M.L. on board (note + terminals on meter)
-mains cable brown lead to transformer primary via fuseholder and switch
-mains cable blue lead, via switch to transformer primary
-mains cable earth lead to earthed tag on strip
-insert strain-relief bush in hole and pass cable through
-stick on labels: one to identify sockets and play calibration potentiometers, the Dolby Laboratories label on the rear close to socket $\mathrm{Skt}_{3}$, and the third inside chassis close to transformer.
Setting-up procedure for the kit design together with calibration details will be given in part three of this article.

Correction to part 1: Readers of part 1 of this article will have noticed a discrepancy in referring to JVC's a.n.r.s. scheme. Being of the general class of Fig. 5(a), it is incorrect to refer to ". . . a fixed high-pass filter in the subsidiary signal path, as is done with the JVC a.n.r.s. system, ..." (page 203, column 2). It should be clear that the subsidiary signal path of Fig. $5(c)$ is a feature of the Dolby system, and not JVC's. The Dolby filter of course has a variable frequency characteristic, whereas the JVC circuit uses a fixed turnover frequency. In a.n.r.s., the filter is in the main signal path during encoding and the whole compressor is placed in a high-gain negative feedback loop during decoding. It is therefore incorrect to include the parenthetic reference to the JVC technique following the reference to Fig. 5(c) on page 202 (foot of column 3).

Dolby Laboratories tell us the amount of distortion introduced in the processor output as a result of the overshoot suppression diodes operating is a few times higher than the $1 \%$ figure quoted on page 205. As mentioned, this distortion is momentary of course, occurring when the causal (not casual, as misprinted!) programme transients mask the distortion. Dolby Laboratories also point out that the variable decay time mentioned in the following paragraph is a feature of the A system only; it is fixed at 100 ms in the $B$ system.

# Letters to the Editor <br> <br> CONFUSION ABOUT <br> <br> CONFUSION ABOUT NOISE 

 NOISE}

The March issue carried two articles about noise, one of them with the title "Noise - confusion in more ways than one". For this reader, alas, confusion was worse confounded by Fig. 1 of the article. The lower waveform looked like rectified noise, not band-limited noise as the caption said. Further, the probability density curve sketched and described as being of the Rayleigh type would only be correct for the envelope of narrow band noise. The noise itself has a Gaussian distribution. Perhaps the author meant to say that rectified narrow band noise has a Rayleigh distribution, and so it does, except when subjected to further band limiting whereupon its distribution reverts to Gaussian.
The other article "Low noise wideband amplifier" was reticent about the facts of life concerning the quiescent value of $I_{c}$ and the disturbing effect of base spreading resistance $r_{b}$ in circuits of this kind. If $r_{b}$ were zero, $R_{V}$ and $R_{I}$ values could be scaled to suit $R_{S}$ merely by adjusting $I_{c}$ for a single transistor, increasing $I_{c}$ for low values of $R_{S}$. This simple procedure is baulked by the presence of $r_{b}$ which provides the only reason for introducing parallel operation. To a good approximation $R_{V}=r_{b}$ $+r_{e} / 2$ and $R_{I}=2 \beta r_{e}$ for a single transistor, where $r_{e}$ is the characteristic slope impedance of the base emitter junction, given by $r_{e}=25 / I_{c}$ when $I_{c}$ is in mA. for $n$ transistors in parallel the effective values of $R_{V}$ and $R_{I}$ for the whole circuit are thus $r_{b} / n+12.5 /\left(n I_{c}\right)$ and $50 \beta /\left(n I_{c}\right)$ where $I_{c}$ is still the current of each individual transistor. The $I_{c}$ and $r_{b}$ values of the circuit described in the article were not given. It would be interesting to know them and check the circuit performance against this simplified theory.
H. Sutcliffe,

Department of Electronic Engineering, University of Salford.

## Dr Smith replies:

The point by Professor Sutcliffe concerning an error of omission in Fig. 1 of my article "Noise - confusion in more
ways than one", is quite correct. It also illustrates the interesting difference in intent by various people. Discussions about noise fall quite definitely into two camps. The first describes the statistical noise processes and involves a considerable depth of probability theory. The other effectively takes the stationary parameters characterising the noise (average value, root mean square value or power, and so on), and develops a measurement technique based on power ratios of signals to noise in actual systems. I wished to avoid the first approach, but thought to include Fig. 1 with the express purpose of showing that noise can have a distribution which differs from Gaussian. I find the assumption that noise is always Gaussian is an error often made in early stages of noise studies. (Even Professor Sutcliffe brought in "Gaussian" whenever he could!)
In Fig. 1 the words "envelope of" should be inserted before "band limited", although Professor Sutcliffe had the right idea when he surmised that I had intended to illustrate the detected envelope. My intention was to generate a picture of Rayleigh distributed noise and, as expected when I looked at my notes of the experiment to photograph the output of the detector, they read: "mention that the Rayleigh distribution is obtained after rectifying band limited noise, as follows . .." It is as well to mention that in practice all noise is ultimately band limited.
The output of a linear detector fed with Gaussian noise can be intuitively visualised as having a lop-sided peak at the average (or rectified d.c. output) value on one side of zero. It has zero probability of actually having the value zero, together with a decreasing probability after the peak, again towards zero as the output amplitude increases. This is just the one-sided Rayleigh distribution. Intuition is not a reliable guide to accurate concepts in probability - so do not take it too far! If there is a relatively large signal with the noise, then the output at the detector again tends to Gaussian, the more so as the signal amplitude increases. Also, further band limiting of the detector output will have the effect mentioned by Professor Sutcliffe. This discussion gives me the opportunity to offer a reference in case readers wish to follow up this interesting point ${ }^{1}$.
A small item: the commas in the last equation of the article (p.110) should be points or multiplication signs. The context should be obvious.

## Reference

1. J. A. Betts. "Signals processing, modification and noise," Chapter 4. E.U.P.

## Mr Grocock replies:

My reticence about the effects of varying the quiesent value of $I_{c}$ was due to the fact that this ground had already been covered by Mr P. J. Baxandall in his excellent article in Wireless World, December 1968. Indeed, this was the
first reference quoted in the first paragraph of my article and I did not feel justified in merely repeating what had already been said by Mr Baxandall.

I agree that parallel operation is only justified by the presence of $r_{b}$ and that $R_{V}$ and $R_{I}$ expressed in terms of individual transistor parameters are as stated by Professor Sutcliffe.

Unfortunately, I cannot quote the values of $I_{c}$ and $r_{b}$ for the circuit described since I no longer have access to the amplifier. However, I take the point made by Professor Sutcliffe; it would have been useful to compare the circuit performance against the values of $r_{b} I_{c}$ and $\beta$.

## CONTACTS REQUESTED

I am the Rehabilitation Officer for the Rhodesian Society for the Blind and Physically Handicapped. I am also a member of the Friends of the Lions, No. RH/4407/3/75.
I have a Mr Robert Harley on my books who is a registered blind person and whose great joy is in amateur radio communication. I write to enquire whether there is anything you could do to help this man by asking in your magazine for another amateur radio operator to contact Bob Harley (call sign ZEIDO), either from Wales or England, or both for that matter. If this were possible he would be overjoyed. He is an ex Air Force Battle of Britain pilot and besides being blind he has also lost a leg.
(Mrs) I. David,
Greendale, Salisbury,
Rhodesia.

## NAVIGATION BY SATELLITE'

I am surprised by the general way in which hyperbolic radio systems are treated in the article "Navigation by satellite" by W. Blanchard (February issue) In particular the Omega system does not suffer from many of the difficulties claimed, as they are not applicable to its mode of operation. The Omega system makes no attempt to "locate" (sic) the transmitters, as it uses a non-directional aerial and has no direction finding ability. The Omega system does not translate time intervals into distances, and it is not necessary to have an absolute time standard at the receiver. The system operates by phase comparison of sequentially transmitted signals, and the only accurate timing links required are between transmitters, a simple requirement.
No mention was made of the strategic implications of the satellite system. No armed force is likely to rely on the Omega system, as the transmitters could easily be silenced during hosti-
lities. It is much more difficult to knock down a satellite.

Finally the experience of Mr Blanchard's space-suited observer is only as stated if the satellite travels in a straight line. In a practical orbit the Doppler shift varies continuously from -D having just passed, and +D being about to pass.
J. R. Watkinson,

The University,
Southampton.

## Mr Blanchard replies:

I think Mr Watkinson's misgivings about my article stem partly from my rather idiomatic use of words.

Having used all the hyperbolic systems I mentioned, as well as satellite navigation, for many years, I am well aware of their shortcomings and strengths, and I can assure Mr Watkinson that Omega does indeed suffer from the troubles I mentioned. I don't think anyone would seriously claim that Omega possesses other than moderate accuracy, as I stated.

When I said that earth-bound systems usually have little trouble in locating their transmitters, I meant that measuring the exact site of such a transmitter in terms of some geographical co-ordinate system or other usually presents little difficulty, at least in the better-mapped areas of the world. It is of course very important to know these positions precisely, since all one is doing with any navigation system is to establish where one is by measuring difference of position from some other precisely known point or points. This difference can be expressed in many ways, but in the end they can all be boiled down to a range and a bearing, two ranges, or two bearings (or, of course, more than two).

So when Mr Watkinson says that Omega does not translate time intervals into distance, he is correct inasmuch as the receivers themelves present only time differences, but this information would be quite valueless to the navigator unless it could be turned into geographical co-ordinates. To do this needs a translation from time to distance, and this is done by many users by plotting the time differences on a suitable chart, the chart compilers making the assumption that radio waves travel at a known speed, and therefore that time can be turned into distance. This sort of chart is really a simple and very cheap analogue computer, and of course the same calculation can be performed more precisely by a small digital computer, at considerably higher cost.

I take his last point, and I should probably have stated that my remarks only applied strictly to a satellite travelling in a straight line and not in a quasi-elliptical earth orbit.
Since my article was written, another satellite has been launched and there are now six in orbit.

## EMERGENCY POWER GENERATOR

I was most interested in J. M. Caunter's article on generators (February issue) as for some time a colleague and I have been working along similar lines. We have used a heavy-duty dynamo, the normal 22 -amp car type being a little too small. By winding approximately 400 turns of 24 gauge wire over three slots we were able to get $240 \mathrm{~V}, 50 \mathrm{~Hz}$ direct. This requires a little more care in the winding but has several advantages. The lower current makes it possible to use the armature shaft bearings as one slip ring, the commutator segments being joined together form the other. It avoids the use of a heavy and expensive transformer and by using a small battery charger it is possible to excite the field. The use of a regulator is recommended. The residual magnetism is not enough to self-excite from start so a battery and "push to excite" switch is required.

I have achieved 350 watts with 6 amps excitation on a standard dynamo and 450 watts on a heavy-duty dynamo with 2.5 amps excitation. 450 watts is about the limit for this type of lawnmower engine, which, incidentally, I have converted to gas as this is much cheaper and the fumes are less unpleasant.
Maurice W. Garman,
Pinner,
Middlesex.

## PERIL OF PUBLISHING

It would be interesting to know how many people with bright ideas or circuits are put off submitting them to Wireless World, knowing that the following month they will be destructively attacked by some even brighter person with large resources behind him. Perhaps these wise guys might remember that good things come from small beginnings.
W. B. Henniker,

Henniker \& Kerr,
Edinburgh.

## SERIES AND PARALLEL FEEDBACK

Regarding the answers to my letter published in your February issue, I would like to make three short remarks.

1. I omitted to state the load impedance used in the distortion measurements on operational amplifiers. This was $5 \mathrm{k} \Omega$ in all cases. Below about $3 \mathrm{k} \Omega$ distortion increases rapidly; above that level no significant improvement in distortion was noted. Incidentally, Mr Linsley Hood's $1 \mathrm{k} \Omega$ is below the full output swing capability of the i.cs used.
2. Mr Sandman is correct in saying that his circuit does not suffer from the 'common-mode distortion I mentioned. I .mistook his circuit for a similar one, in which the non-inverting input of $A_{1}$ is used. In that case, the common-mode troubles I remarked upon will arise. My apologies to Mr Sandman.
3. Mr Sandman's remark about the Delft circuit is incorrect. It does have negative feedback around both amplifiers. The positive feedback around $A_{2}$ via $R_{1}$ is compensated by an equal amount of negative feedback through $A_{1}$ and $R_{2}$. The net result is no positive feedback but the only negative feedback applied to the inverting input of $\mathrm{A}_{2}$.
In my view this circuit is more elegant in so far as it does not require a floating load.
T. Magchielse,

Almelo,
Netherlands.

## CAPACITORS AS TRANSMISSION LINES

I found the letter by Mr Azelickis in the May issue most informative; I was aware that the equivalent circuit of the capacitor could be elaborated upon, and certainly to consider the capacitor as a transmission line is an excellent physical interpretation.

The transmission line analogy is the next step up from the simple $L C R$ circuit (resonant circuit) that I used for my description, and the reason that it was neglected was twofold. First, the resonant circuit is the standard equivalent circuit for capacitors, and as I thought the article covered a large amount of material in a rigorous as possible manner, the properties of transmission lines not being understood by everyone (including myself) who would read the article, such an equivalent circuit would be presumptuous on the part of the author. Secondly, manufacturers' information is developed along the lines of the LCR circuit; a transmission line circuit would have kept my typewriter busy making comparisons between the two.
I must confess a mention of the high frequency properties explained in terms of a lossy transmission line for capacitors would have been nice in the article. It is only when attention is drawn to a point that one realises just how much information one has left out. R. A. Fairs,

Mortlake,
London SW14.

## VAT new rates

In view of considerable confusion about the new rates of Value Added Tax which came into force on May 1, readers responding to advertisements in Wireless World are advised to check with the advertisers concerned before purchasing goods.

## A 50 MHz oscilloscope

## 2-Sweep and trigger circuits

by C. M. J. Little, B.A.
Department of Electronics, Southampton University

The sweep generator and associated circuitry provide a linear timebase with calibrated ranges from $1 \mathrm{~s} / \mathrm{cm}$ to $10 \mathrm{~ns} / \mathrm{cm}$. The timebase is triggered by the signal on the Y plates, unlike some timebases where the free-running sweep frequency is adjusted to syn-
chronize with the Y signal. A stability control adjusts the threshold of the sweep generator, allowing it to free run or to be triggered. The trigger generator is equipped with a level control and a positive/negative slope switch, which allows the triggering signal to be taken
off different parts of a waveform. This enables a stable display to be obtained from almost any input signal. The

Fig. 7. The sweep generator circuit diagram. Components $R_{T}, C_{T}$ and $C_{H}$ are selected by $\mathrm{S}_{8}$ in Fig. 8.

triggering signal may be selected from the $Y$ amplifier, with a choice of a.c. coupling or low frequency rejection (high pass filter), from the 50 Hz mains, or from an external socket. A facility is provided for single-shot operation either triggered or free running, depending on the position of the stability control. A push-button and neon indicator resets the sweep and provides an indication that the circuit is ready to be triggered.

A triggered timebase does not normally produce a trace on the screen in the absence of an input signal, and it is usual to provide an "auto" position on the trigger selector switch. The "auto". function triggers the sweep from an internal oscillator at a fairly low frequency when no triggering signal is present, and also disconnects the trigger level control. This provides a trace at all times and results in immediate lock when an input signal is applied. This facility has not been provided, partly for technical reasons, and partly because I have not found it necessary. I will give a suggestion for a circuit in the final part of the article.

The sweep generator in Fig. 7 will now be described in detail. The circuit is fairly complicated, so a step-by-step explanation of the circuit operation will be given.

## Circuit operation

Consider the circuit when the stability control is just off the point where the trace runs free. $\mathrm{Tr}_{50}$ is on, $\mathrm{Tr}_{52}$ is off, and the base-emitter junction of $\mathrm{Tr}_{52}$ is reverse-biased. The voltage at the collector of $\mathrm{Tr}_{52}$ is 18 V , and the voltage at the emitter of $\mathrm{Tr}_{53}$ is 5.4 V . This positive voltage holds $\mathrm{Tr}_{54}$ and $\mathrm{Tr}_{55}$ on via $D_{32}$ and $R_{137}$. The voltage at the junction of $D_{35}$ and $D_{41}$ will assume' a potential of about -2 V , diverting excess current from $\mathrm{R}_{137}$ through $\mathrm{D}_{33}$, $D_{41}$ and the resistor chain to the -50 V rail. The start of the sweep voltage is about -8 V at D . The loop $\mathrm{D}_{32}, \mathrm{Tr}_{55}, \mathrm{Tr}_{56}$, $D_{35}$ and $D_{33}$ forms a negative-feedback control loop which tends to hold the start voltage of the sweep constant in spite of the charging current through $\mathrm{R}_{\mathrm{T}}$, which varies from $0.6 \mu \mathrm{~A}$ to 2 mA . This control loop works very well, with almost no detectable change in start voltage over all the time $/ \mathrm{cm}$ ranges.

To continue, the emitter of $\mathrm{Tr}_{60}$ is at about -14 V . As the base voltage of $\mathrm{Tr}_{50}$ will be at $-10 \mathrm{~V}, \mathrm{D}_{39}$ is reverse-biased. The emitter voltage of $\mathrm{Tr}_{57}$ is controlled by the stability control, which is adjusted until $\mathrm{Tr}_{50}$ is only just on; $\mathrm{Tr}_{58}$ plays no part in the circuit operation as its collector is open circuit. Now a negative-going trigger pulse turns $\operatorname{Tr}_{50}$ off. $\mathrm{Tr}_{51}$ and $\mathrm{Tr}_{52}$ turn on and the voltage at the collector of $\mathrm{Tr}_{52}$ falls to 6.5 V . The voltage at the emitter of $\mathrm{Tr}_{53}$ is now at -6 V , which reverse-biases $\mathrm{D}_{32}$ and $\mathrm{D}_{33}$; The Miller run-up circuit $\mathrm{Tr}_{54}, \mathrm{Tr}_{55}, \mathrm{Tr}_{56}$ and $C_{T}$ is now disconnected and the gate of $\mathrm{Tr}_{54}$ tries to go negative. This is countered by the emitter of $\mathrm{Tr}_{56}$ going


Fig. 8. Sweep-time selector switch and fine sweep-time control. $\mathrm{C}_{\mathrm{H}}$ and $\mathrm{R}_{\mathrm{H}}$ are hold-off components to allow Ct time to discharge.
positive. The effect is that the gate voltage of $\mathrm{Tr}_{54}$ remains constant and a linear positive-going ramp is produced at the emitter of $\mathrm{Tr}_{56}$. The rate of the ramp is determined by the charging current through $\mathrm{R}_{\mathrm{T}}$ and the timing capacitor $\mathrm{C}_{\mathrm{T}}$. The collector load resistor is returned to the +115 V rail in order to use a high value load resistor, and thus to obtain a high loop gain.
The emitter of $\mathrm{Tr}_{60}$ follows the ramp voltage, forward biasing $\mathrm{D}_{39}$ and carrying the base of $\mathrm{Tr}_{50}$ at the same potential, $\mathrm{Tr}_{57}$ is reverse-biased. At a potential of about +3 V , the Schmitt trigger $\mathrm{Tr}_{50}, \mathrm{Tr}_{51}$ and $\mathrm{Tr}_{52}$ resets. $\mathrm{C}_{\mathrm{T}}$ now discharges via $R_{137}$ and $D_{32}$ on one side and $\mathrm{D}_{35}, \mathrm{D}_{34}$ and $\mathrm{Tr}_{55}$ on the other. The gate-voltage of $\operatorname{Tr}_{61}$ will follow the falling ramp voltage until $\mathrm{D}_{40}$ reverse biases. The hold off components, $\mathrm{C}_{85}, \mathrm{C}_{\mathrm{H}}$ and $\mathrm{R}_{159}$ maintain the emitter of $\mathrm{Tr}_{60}$ positive for an additional time period to allow $\mathrm{C}_{\mathrm{T}}$ to completely discharge. The hold-off capacitors discharge via $\mathrm{R}_{159}$
and the sweep is ready for another trigger pulse when $D_{39}$ reverse biases and the base voltage of $\mathrm{Tr}_{50}$ is again under the control of the stability control. This concludes the circuit operation under normal triggered use.
The single-shot facility takes effect when $S_{6}$ is operated. The rising voltage at the end of the sweep turns $\mathrm{Tr}_{57}$ off and $\mathrm{Tr}_{58}$ on. $\mathrm{Tr}_{58}$ holds the voltage at its emitter at a more positive value than that set by the stability control. This reverse biases $\mathrm{Tr}_{57}$ and inhibits the sweep. When $S_{7}$ is pressed, the positive pulse generated turns $\mathrm{Tr}_{57}$ on and $\mathrm{Tr}_{58}$ off, restoring the voltage at the base of $\mathrm{Tr}_{50}$ to its usual value. The sweep may now be triggered, and this is indicated by the neon.

There are a few points that have not been covered in this description. One section of the horizontal selector switch inhibits the sweep in the external $X$ position by shorting $R_{133} . C_{82}$ is shown connected to the +18 V rail, but could equally well be connected to earth. $D_{30}$, $\mathrm{D}_{34}, \mathrm{D}_{38}, \mathrm{D}_{37}$ and $\mathrm{D}_{36}$ protect against breakdown of base-emitter junctions. $\mathrm{R}_{160}$ adjusts the finish voltage of the ramp and is used to set the trace length.

The speed selector switch is shown in


Fig. 8, and hardly needs any comment. The hold off components, switched by $\mathrm{S}_{8 \mathrm{a}}$ increase the hold off time for some ranges, and decrease it on others by connecting additional resistors to the -50 V rail.

## Trigger generator

The trigger generator is shown in Fig. 9. The input stage is a differential amplifier similar to the Y pre-amplifier input, having the signal input applied to one gate, and the trigger level control voltage to the other. The positive/negative slope switch reverses the two gates. $\mathrm{Tr}_{73}$ produces a current output which drives the tunnel diode, $\mathrm{D}_{50}$.

The voltage divider chain $\mathrm{R}_{204}, \mathrm{R}_{205}$ and $\mathrm{R}_{206}$ biases the tunnel diode onto the
negative resistance part of its characteristic. $\mathrm{R}_{207}$ adjusts the slope of the load line so the tunnel diode just does not oscillate, as illustrated in Fig. 10. This adjustment minimises the hysteresis of the circuit. The current from $\mathrm{Tr}_{73}$ moves the load line so the tunnel diode switches alternately from its high voltage state to its low voltage state, and vice versa. The 300 mV step is amplified by $\mathrm{Tr}_{75}$ and differentiated by $T_{1}$. The positive spikes are suppressed by $D_{51}$, and the negative ones trigger the sweep generator.
When $\mathrm{S}_{9}$ is in the h.f. sync position, $\mathrm{S}_{9 b}$ shorts $\mathrm{R}_{207}$. The tunnel diode oscillates at about 10 MHz , providing trigger pulses. The input signal, which may be up to 100 MHz , synchronizes this oscillation and provides a locked trace.

## Aid for drivers

## Experimental German inductive-loop system to guide motor vehicle drivers to their destinations quickly and safely.

As the roads of the industrialized nations become more and more congested, getting to one's destination by motor vehicle becomes increasingly time-consuming, nerve-wracking and expensive. Electronics has already given some help in the form of the established German traffic information broadcasting system ARI (Autofahrer-Rundfunk-Information) described in the May 1973, p.238, and April 1974, p.95, issues of Wireless World. Even more assistance could come from Germany if a new electronic system giving drivers direct guidance to their destinations, taking account of road conditions, is generally adopted - though at present this does seem a long way off. Called ALI (Autofahrer Lenkungs-und Informations System, i.e. Drivers' Guidance and Information System), this scheme is the result of work by the Telecommunications Technology and Data Process-
ing Institute of the Aachen Institute of Technology, supported by development by the Robert Bosch Research Institute and the firm Blaupunkt-Werke which is a member of the Bosch group. Blaupunkt has been working on the ALI system for two years and recently Wireless World saw a demonstration of it on a test track built at their headquarters at Hildesheim, near Hanover.
The basic idea of ALI is' that the driver tells the system where he wants to go (e.g. a town or motorway exit) by pressing keys on a unit in his vehicle, and then, as he drives along, direction information (e.g. turn left, drive straight on) is automatically transmitted to the vehicle by roadside units just ahead of junctions, exits and so on and presented to the driver on a display unit. In addition to the directions to his destination, the driver receives information on road conditions, the presence of


Fig.1. Simplified schematic of the drivers'guidance and information system, showing a vehicle equipment and roadside equipment communicating with each other by magnetic induction.
obstacles such as traffic jams, and recommended average speeds for rapid progress. For example, on the vehicle display units we saw a Blaupunkt (see photo) there were arrows for direction instructions, the announcement words "icing", "fog" and "traffic jam" and numbers for the recommended average speeds - each of which was lit up as appropriate.
The information transmitted to the vehicles is stored in the roadside units, having been acquired by them mainly from the passing vehicles themselves (those fitted with ALI) and partly by telephone line from a central computer which itself is fed with accumulated information from a large number of the roadside units. (There would be one computer for each of 16 zones in W. Germany - see below.) Exchange of information between the roadside units and the vehicles takes place by means of $2 \mathrm{~m} \times 2.5 \mathrm{~m}$ inductive loops buried beneath the road surface and ferrite rod "aerials" fitted low down on the chassis of the vehicles.
A simplified block diagram of the vehicle and roadside equipments is shown in Fig.1. The "destination" keys which the driver presses in his vehicle have code letters and numbers which are used to give "four-symbol map references on a map of the German Federal Republic. This map is divided first of all into 16 main zones, labelled A to Q , and the first letter symbol keyed-in selects one of these. Each of these main zones is subdivided into 16 smaller zones, and the second keyed letter symbol selects one of these. Thus the first two keyed letter symbols, for example FB, select one of 256 small zones, each of which measures $31 \times$ 31 km . The third letter symbol keyed-in selects an even smaller subdivision area, of $8 \times 8 \mathrm{~km}$. The fourth keyed symbol can be one of nine letters and seven numerals: if a letter is keyed a final destination area, measuring $2.7 \times$ 2.7 km , is selected; while if a numeral is keyed a particular motorway exit is selected. This coding system allows more than 65,000 destinations to be defined.
In addition to the destination key-
board, the vehicle equipment comprises a small transmitter for sending out the pre-selected destination, a receiver which receives the direction instructions from the roadside equipment, and the display panel already mentioned. The "aerial" on the vehicle is a ferrite rod type about 20 cm long. The roadside equipment includes a transmitter and a receiver, the inductive loop in the road, and a programmable memory containing the instructions to be transmitted to the vehicles. This unit is buried close to the roadway.

The roadside equipment transmits call signals continuously. When a vehicle fitted with ALI travels over the loop, the call signal is identified by the vehicle's receiver. This identification serves to switch off the vehicle receiver and simultaneou sly switch on the vehicle transmitter, which then transmits the destination, pre-set on the vehicle's keyboard, to the roadside unit. The message begins with a start signal (coding identical with that of the call signal). Thereupon a 16 -bit destination message is transmitted, three times in succession, and in each case two successive messages are checked for identity.

At this point the vehicle equipment is automatically switched over to reception and the roadside unit to transmission. The roadside equipment transmits a start signal, followed by an 8-bit message of direction instructions, also three times in succession. This concludes the data transmission. The call signals of the roadside equipment which follow are no longer interpreted by the vehicle unit; this is an important teature, in cases where a driver has to stop over a loop.

When the information reaches the vehicle a short "pip" sounds inside the driving compartment and the display panel lights up with the appropriate message. The display brightness can be adjusted and the panel can be switched off by pressing a push-button.

The exchange of data described above takes place in about one hundredth of a second. Duration of transmission is so short that it would still be effective for vehicles travelling at $300 \mathrm{~km} / \mathrm{h}$ ( $180 \mathrm{~m} . \mathrm{p} . \mathrm{h}$.) for the size of inductive loop used. It is claimed that even at these high speeds the reliability of operation of the system is good because triplicate messages are being transmitted in both directions.

Information throughout the system is stored and processed in binary digital form, but for signalling purposes the binary data is converted into pulse duration modulation and then into frequency modulation for transmission via the loop or ferrite "aerial". Two frequencies are used, obtained in both the vehicle and roadside equipment from a quartz crystal oscillator via a frequency divider with a change-over switch. The crystal oscillator frequency of 4.433 MHz is divided by 40 and by 30 to give respectively the two frequencies


Fig. 2. Announcement display in the vehicle. This has arrows to give directions, warnings of road conditions and recommended speeds.

Fig. 3. Ferrite rod "aerial" for inductive transmission and reception on the chassis of a car.


111 kHz and 148 kHz . Binary data are then encoded as follows: "low" is represented by seven cycles of 148 kHz and 16 cycles of 111 kHz ; "high" is represented by 22 cycles of 148 kHz and six cycles of 111 kHz ; and the "start" signal consists of 30 cycles of 148 kHz and six cycles of 111 kHz . (This "start" signal is the one used for the beginning of the messages and for the call signals from the roadside equipment.)

As for the possible cost of putting the ALl system into operation, Blaupunkt were unwilling to commit themselves too definitely, but they thought that vehicle units could probably be manufactured for about 200DM each (about $£ 36.00$ ) and roadside equipments for about 1000DM each (about $£ 180.00$ ). For W. Germany possibly 20,000 road-
side equipments would be needed altogether. Total expenditure might be anything up to 1000 M DM (about £180M). The system has been presented to the Federal German transport ministry and has also been demonstrated to the Common Market scientific body COST (Co-operation Europeenne dans le domaine de la Recherche Scientifique et Technique). Our general impression is that Bosch and Blaupunkt are not themselves very convinced of the economic practicability of the scheme as at present proposed but are anxious to establish their technological lead in this general field of traffic information and guidance. ALI could for example be used for public transport systems within towns, and already several German bus operators have shown interest in it.


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# Paris components show 

## New semiconductor devices at the Porte de Versailles

Wireless World again made the annual pilgrimage to the Paris component show which, in the past, has been a favourite event for launching new products. This year, however, we were expecting the worst, having been constantly warned of impending doom and recession. Despite these "Job's comforters" the show was a success, with over 1100 exhibitors displaying their wares. In our report we have concentrated on semiconductor devices, in which most development is taking place.
Nippon Electric Company formally launched a microwave f.e.t. Designated the NE244, it is a gallium arsenide device suitable for low-noise amplifiers and oscillators operating between 9 and 12 GHz . The makers say that this device is the first reliable microwave f.e.t. on the market having a m.t.t.f. (mean time to failure), at $125^{\circ} \mathrm{C}$ junction temperature, of $10^{6}$ hours. Specifications of the f.e.t. are: drain-to-source voltage 10 V ; maximum power gain, at $8 \mathrm{GHz}, 11 \mathrm{~dB}$; typical noise figure, at $8 \mathrm{GHz}, 3 \mathrm{~dB}$. The device is available in several packages, including the stripline case, or the bare chip can be supplied which has a better frequency response because there is no parasitic package-capacitance. NEC tell us that a second-generation device is
under development and sample quantities should be available around July this year. The crux of a microwave f.e.t. is the channel thickness, which is one micron in the NE244. The development device, type NE388, has a channel width of $1 / 2$ micron and is intended for use at around 14 GHz although, say the makers, theoretically it could operate at 20 GHz .
Microprocessors were in evidence, with more companies entering the market, bringing the number of manufacturers to around a dozen. RCA announced the COSMAC - an eight-bit c.m.o.s. register-oriented microprocessor. The l.s.i. device is housed in one 40 -pin and one 28 -pin package and can be powered from an unregulated supply of 4 to 12 V . It is understood that the device will be available about October at a price of around $\$ 400$. Intersil launched the IM6100, a 12 -bit parallel microprocessor on a single chip. This is a silicon-gate c.m.o.s. device consisting of six 12 -bit registers, a programmable logic array to generate control signals, an arithmetic and logic unit, and timing circuitry. The IM6100 is t.t.I. compatible and requires a single 5 V supply.
Advanced Micro Devices also introduced a single-chip processor using m.o.s. technology. The Am8080, which


Development microwave f.e.t. from NEC showing $1 / 2$ micron channel.
is similar to the Intel device, has six 8 -bit registers, which may be used singly or in pairs for both 8 - and 16 -bit operations. The chip is housed in a 40 -pin package and samples should be available in July.
C.c.d. memories made their first commercial appearance at the show with the Fairchild CCD450 - a 1 -kilobyte serial memory using a bur-ied-channel, ion-implanted barrier structure in the registers combined with n-channel silicon-gate m.o.s. structures for timing, charge detection and level conversion circuitry. Nine bidirectional data lines are t.t.l.-compatible and have three-state output buffers for wired-OR application. The device is organized as 1,024 words of 9 bits: the nine c.c.d. registers are shifted in parallel to provide storage and retrieval of ninebit words. Power dissipation in the read and write modes is 250 mW and average random-byte access time is $200 \mu \mathrm{~s}$.
Intel also announced a c.c.d. memory called the 2416. This device is organised as 256 words of 64 bits with address register incorporated on the chip. Any one of the 64 registers can be accessed by applying an appropriate 6 -bit address input. The 2416 has maximum serialdata transfer rate of $2 \mathrm{megabits} / \mathrm{s}$, and an average latency time under $100 \mu$ s. Intel have indicated that they may be producing a 32 kbit device in the next year.
Advanced Micro Devices Inc are launching a t.t.l. family of low-power Schottky devices called the Am25LS range, which is expected to be available around July this year. These devices are faster, have improved noise margins and increased fan-out over their 54LS/74LS series. Circuits in the range include a one-of-eight or dual one-offour decoder/demultiplexer, a threestate quad two-input multiplexer inverting or non-inverting - and an eight-by-one serial/parallel two'scomplement multiplier.
The latest m.o.s. circuit from Siemens - a programmable counter module, type SAJ341 - was on display. The device is a continuation of the SAJ series of frequency dividers, and consists of a four-decade up-counter which is connected behind five divider stages

L.e.d.-array driver i.c. from Siemens.
to form an adjustable circuit, capable of comparing the coded timing of a process with the prescribed value. Four-digit quantities, minutes and hours can be counted, compared and displayed.
Another new i.c. from Siemens is the UAA180. Unlike the UAA170, which is a driver module for l.e.d. arrays, illuminating one l.e.d. at a time, the 180 drives up to 12 l.e.ds simultaneously to produce a strip of light of varying length, depending on an analogue quantity. This circuit, with an l.e.d. array, is intended to replace conventional meter movements for displaying quantity and rate of change.
Other new components seen were the 2708, an 8 k erasable m.o.s. programmable ROM, the 3604 , a 4 k bipolar PROM, and the 5101 , a 1 k c.m.o.s. RAM - all from Intel. AEG-Telefunken had a range of power semiconductors claimed to be the first manufactured from neutron-doped silicon. These were high-current diodes, D401 and D401R, with blocking capabilities of 4000 to 5000 V at 800 A r.m.s., and a high-current thyristor, T670N, which has a current capacity of 1500 A r.m.s. at an inverse voltage of 2000 to 2600 V . AEG say that thyristors with a peak inverse of 4000 to 5000 V are under development using n.d.s.

Consumer devices seem to be a popular area and SGS-Ates announced several new i.cs for electronic musical instruments. These m.s.i. and l.s.i. devices will cover the basic functions of an electronic organ and auxiliary functions (rhythm and automatic accompaniment). The new devices are the M081 and M082 m.o.s. circuits for tone generation, the HBF4727AE, a c.m.o.s. frequency divider, the M252 m.o.s. rhythm generator and the M251,
a m.o.s. circuit which automatically generates the accompaniment (bass notes, arpeggios and chords). Another device on show was the TDA1054, a monolithic level-control preamplifier for tape recorders, dictaphones, etc. It is also suitable for compressor-expander application in telephone equipment. The circuit incorporates a low-noise preamplifier, a.l.c. system, high-gain equalization amplifier and supply variation rejection facility all on one chip. SGS-Ates and AEG Telefunken have jointly developed a complete kit of integrated circuits and discrete devices for a PAL television receiver, which we understand is available now.
New from Mostek are the MKM70041 and MKM70042 modules for l.e.d.-display watches, which are 12 hr and 24 hr units respectively. Two gold plated switch contacts provide instant access to either hours and minutes or date and seconds. A third switch contact is used for setting the time. The module is designed to fit existing watch cases which contain three push switches in the bezel and where the back of the case makes contact to the positive terminal of one battery and the negative terminal of a second battery in series.


Digital watch module from Mostek.

## HF predictions

Ionspheric forecasting is very much the same in some respects as atmospheric weather forecasting. Seasonal trends are well established but day-to-day variations within a month can only be predicted on a statistical basis when forecasting a month or more in advance. Forecasts of conditions a day or two in advance and the progress of events once they have started meet with fair success. A good success rate is obtained by assuming that tomorrow will be the same as today and applying a measure of psuedo scientific folklore.




# Electronic circuit calculations simplified 

## 1 - Resistive circuits

by S. W. Amos, B.Sc., M.I.E.E.

Probably the problem most familiar to the experimenter in electronics, whether professional designer or interested amateur, is the determination of what value of component to use at a particular point in a circuit. Manufacturers' literature can provide useful information but often the designer has to solve the problem himself and in general there are two ways in which he can determine the optimum value for a component. He can make a working model of the circuit using preset components which can be adjusted to give the best performance: measurement of the values of the preset components then gives the required information. Alternatively, and this avoids the need to build a circuit, he can calculate the optimum values of the components. Many of the calculations are extremely simple and it is the aim of this series of articles to show that much circuit design is possible using elementary mathematics. Indeed many calculations require nothing more complicated than Ohm's law: others use formulae which are just as easy to handle. All the numerical examples which illustrate the articles stem from typical practical circuits.
We shall begin with calculations concerning a single resistor and will then consider those on circuits consisting of two resistors in parallel or in series.

Single resistors. In general problems concerning a single resistor are of two types:
(a) those in which the circuit requires for its proper operation a resistor of a particular, value and it is desired to calculate that value.
(b) those in which the resistor value is fixed and the operating conditions in the circuit containing the resistor must be chosen to suit the resistor value. It is desired to determine these optimum operating conditions.

Decoupling resistor. A simple example of calculating a resistor value is provided by Fig. 1 which illustrates an RC combination used to decouple the early stages of a receiver or amplifier
from the final stage. The problem is to calculate the value of the decoupling resistor $R$. Ideally the resistor should be as large as possible consistent with providing the early stages with an adequate supply voltage. If the final stages have a $9-\mathrm{V}$ supply (likely in a transistor portable receiver) then the early stages will require, say, 6 V so that 3 V can be lost across the decoupling resistor. The mean current taken by the early stages (at 6 V ) must be known: let this be 5 mA . We can now determine the decoupling resistor value from a simple application of Ohm's law thus:
Value of decoupling resistor is


Fig.1. A decoupling resistor.


Fig.2. Essential features of the automatic cathode biasing circuit.


Fig.3. One method of biasing a depletion-type f.e.t. using a resistor in the source circuit.
$=\frac{\text { voltage lost across decoupling resistor }}{\text { current taken by early stages }}$
$=\frac{3}{5 \times 10^{-3}}$ ohms
$=600 \mathrm{ohms}$.
The calculation of the value of the decoupling capacitor is dealt with in Part 4.

Biasing circuit. Another example of a calculation of a resistor value is provided by the bias circuit for a valve or f.e.t. class-A amplifying stage in which a resistor is included in the cathode or source circuit. A typical circuit diagram is given in Fig. 2: the grid is returned to h.t. negative via $R_{g}$ and the grid-cathode bias is equal to the voltage generated across $R_{k}$ by the cathode current of the valve. The value of $R_{k}$ is thus determined by the grid bias voltage and the mean cathode current. These values are likely to be given in the literature supplied by the manufacturer or can be determined by examination of the characteristic curves. For an a.f. output pentode, for example, the grid bias may be -8 V and the mean cathode current 40 mA . The required value of $R_{k}$ is given by Ohm's law thus:
value of cathode bias resistor

$$
\begin{aligned}
& =\frac{\text { grid bias voltage }}{\text { mean cathode current }} \\
& =\frac{8}{40 \times \frac{8}{10^{-3}} \text { ohms }} \\
& =200 \mathrm{ohms} .
\end{aligned}
$$

Fig. 3 shows a corresponding f.e.t. circuit. Here the mean source current may be 1.5 mA and the gate-source bias voltage -2 V . Again applying Ohm's law:
value of source bias resistor

$$
\begin{aligned}
& =\frac{\text { gate bias voltage }}{\text { mean source current }} \\
& =\frac{2}{1.5 \times 10^{-3}} \text { ohms } \\
& =1.3 \text { kilohms approximately. }
\end{aligned}
$$

One of the significant features of the circuits of Figs. 2 and 3 is that there is no voltage drop across $R_{g}$ due to grid (or gate) current: the bias voltage required is that developed across $\mathrm{R}_{\mathrm{k}}$ or $\mathrm{R}_{\mathrm{s}}$. Bipolar transistors, on the other hand, have a significant base current and it may be necessary to allow for this in biasing circuits as shown in a later numerical example.

Screen-grid resistor. A good illustration of a simple application of Ohm's law is provided by Fig. 4, which shows the circuit diagram of a class-A voltage amplifier using a pentode valve. For satisfactory operation of such a stage the mean screen-grid potential should be approximately equal to the mean anode potential, and this leads to a simple method of calculating the value of the screen-grid dropping resistor $\mathrm{R}_{\mathrm{sg}}$. Over a wide range of operating conditions the screen-grid current of a pentode is a fixed fraction, commonly between one quarter and one third, of the anode current. Because the voltage, across $R_{s g}$ must be approximately equal to that across $R_{a}$, it follows that $R_{s g}$ should be between $3 R_{a}$ and $4 R_{a}$. $A$ commonly-used value for $R_{a}$ is 100 kilohms and $\mathrm{R}_{\text {sg }}$ should therefore lie between 300 kilohms and 400 kilohms. 330 kilohms is often used.

Load resistor (directly-connected). A problem frequently encountered in electronics is that of obtaining the maximum output power of which a valve or transistor is capable in class-A operation. There is a particular value of load resistance (the optimum load) for which the output power is a maximum and its value depends on the operating conditions of the valve or transistor. The optimum load resistance can readily be calculated from Ohm's law as follows:
optimum load resistance
maximum undistorted anode (collector) voltage swing
maximum undistorted anode (collector) current swing

If the load resistor is connected directly in the collector circuit, as shown in Fig. 5 , then the collector voltage swing is limited in the positive-going direction by the supply voltage and in the nega-tive-going direction by the emitter voltage. If the collector voltage attempts to go below the emitter voltage the collec-tor-base junction becomes conductive and applies a low-resistance shunt across the load resistance. Some typical practical values are shown in Fig. 6, which also shows the maximum undistorted sinusoidal collector voltage swing of which the transistor is capable. The quiescent collector voltage (i.e. its value for no input signal to the transistor) is 7.5 V and the maximum voltage swing is of 4.5 V peak value. Let us


Fig.4. Method of applying positive bias to the screen-grid of a pentode.


Fig.5. A load resistor $R_{c}$ connected directly into the collector circuit of a biopolar transistor.


Fig.6. Representing operating conditions in the collector circuit of a bipolar transistor with a directly-connected load.


Fig.7. A load resistor connected to the collector circuit of a bipolar transistor by a transformer.
suppose that the mean collector current is 0.5 A : then this is also the peak collector current swing and the optimum load resistance is given by:
optimum load resistance
$=\frac{\text { maximum collector voltage swing }}{\text { maximum collector current swing }}$
$=\frac{4.5}{0.5} \mathrm{ohms}$
$=9 \mathrm{ohms}$.
The power delivered into this load is given by $V_{r m s} I_{r m s}$ but it is more convenient to use the equivalent expression $V_{p k} I_{p k} / 2$. Substituting for $V_{p k}$ and $I_{p k}$ we have
output power $=\frac{4.5 \times 0.5}{2}$ watts
$=1.25 \mathrm{~W}$ approximately.
Load resistor (transformer-coupled). It was assumed in the above example that the load resistor was connected directly into the collector circuit. Very often, however, load resistors are connected into the output circuits of valves or transistors by transformers as shown in Fig. 7. This affects the collector or anode voltage swing considerably because the quiescent voltage is now the positive supply voltage, there being no steady voltage drop across the primary winding of the transformer, which is assumed to have negligible resistance. The voltage swings are now above and below the positive supply voltage as shown in Fig. 8.

As a numerical example consider a pentode valve with $250-\mathrm{V}$ h.t. supply and a mean anode current of 35 mA . The anode voltage swing is unlimited in the positive direction but is limited in the negative direction by the curvature of the characteristics. To minimise distortion from this cause the anode voltage should not go lower than say 40 V . Thus the maximum downward anode voltage swing is 210 V and the maximum anode current swing is 35 mA . Thus the optimum load resistance is given by
optimum load resistance

$$
=\frac{\text { maximum anode voltage swing }}{\text { maximum ande }}
$$

$$
=\text { maximum anode current swing }
$$

$$
\begin{aligned}
& =\frac{210}{35 \times 10^{-3}} \text { ohms } \\
& =6 \text { kilohms } .
\end{aligned}
$$

The load into which the power is required may be a loudspeaker of 3 ohms resistance. The turns ratio of the transformer can be chosen to match the optimum load to 3 ohms so that the valve is effectively presented with a resistance equal to the optimum load value. The turns ratio required to effect such a match is $n$ : 1 where

$$
n=\int\left(\frac{\text { optimum load resistance }}{\text { loudspeaker resistance }}\right)
$$

Substituting the appropriate values we have:

$$
n=\sqrt{\left(\frac{6000}{3}\right)}
$$

## $=45$ approximately

Thus a transformer with a primary-tosecondary turns ratio of $45: 1$ is required to secure maximum power transfer from the valve to the loudspeaker.

Voltage and current amplifiers. In the previous examples we have been concerned with obtaining the maximum power output from a valve or transistor. This is not always the aim in circuits in which a resistor is included in the output circuit of an active device. Bipolar transistors, for example, are cur-rent-operated devices and in a cascade of transistors the aim of each intertransistor circuit is to transfer current from the output of each transistor to theinput of the next. In Fig. 9 the current output from $\mathrm{Tr}_{1}$ splits between $\mathrm{R}_{\mathrm{c}}$ and the input of $\mathrm{Tr}_{2}$ and $\mathrm{R}_{\mathrm{c}}$ should clearly be as large as possible to deflect maximum current into $\mathrm{Tr}_{2}$. By making $\mathrm{R}_{\mathrm{c}}$ large the collector potential of $\mathrm{Tr}_{1}$ becomes low, almost equal to the emitter potential in fact. $R_{c}$ then determines the collector current of $\mathrm{Tr}_{1}$ and if it is made too large $\mathrm{Tr}_{1}$ collector current becomes very small so that the current gain of $\mathrm{Tr}_{1}$ (which depends on collector current) may become too small. As a compromise we can decide that $\mathrm{Tr}_{1}$ mean collector current is 1 mA (giving good current gain) and, if the supply voltage is, say, 18 V then a simple application of Ohm's law gives $R_{c}$ as 18 kilohms. This is large compared with the likely value of the input resistance of $\mathrm{Tr}_{2}$ so that the correct conditions for a current amplifier are achieved.

There are occasions when a bipolar transistor is required to feed into a device with a very high input resistance such as a valve: It is impractical to attempt to drive' a current into such a high resistance and the output circuit of the transistor is instead designed to deliver an undistorted output voltage, valves being voltage-operated devices. What should be the value of the load resistor $R_{c}$ when the transistor is required to give an output voltage?

The voltage gain of the transistor is directly proportional to $R_{c}$ and this resistor should therefore be as large as possible provided that the transistor can deliver the required voltage output without distortion. Suppose that an output of IV peak value is required, that the mean emitter voltage is 3 and the supply voltage 15 . Then the quiescent collector voltage could be made 4.5 so that swings down to 3.5 (within 0.5 V of the emitter potential) and up to 5.5 occur during operation. The quiescent voltage drop across $R_{c}$ is $15-4.5=10.5$ and if the mean collector current is $1 \mathrm{~mA}, \mathrm{R}_{\mathrm{c}}$ should, from Ohm's law, be 10.5 kilohms.


Fig.9. In a cascade of bipolar transistors, current must be transferred from $\mathrm{Tr}_{1}$ output to $\mathrm{Tr}_{2}$ input.

Fig.8. Representing operating conditions in the anode circuit of a pentode with a transformer-connected load.


Fig.10. Basic form of an electronic voltmeter circuit.

Fig. 11. First step simplifying the circuit of Fig. 10.

Meter series resistor. In the circuits so far discussed it was possible to apply Ohm's law immediately to solve the problem. Sometimes, however, some simplification of the circuit is necessary before Ohm's law can be applied. The next circuit to be discussed is such an example.

Fig. 10 shows the essential features of a circuit used in electronic voltmeters. M is a measuring instrument connected between the cathodes of valves $V_{1}$ and $\mathrm{V}_{2}$. The steady voltage to be measured is applied to the grid of $V_{1} . V_{2}$ is included to minimise drift in meter readings and plays no direct part in the measuring process. The problem is to determine the value of the meter series resistor R . To do this we can replace the valves by equivalent circuits. A cathode follower can be regarded as a generator with an internal resistance of $1 / g_{m}$ and with a signal voltage equal to that applied to the valve grid. Thus Fig. 11 is equivalent to Fig. 10. Now in a practical circuit $\mathrm{R}_{\mathrm{k} 1}$ and $R_{k 2}$ are likely to be large compared


Fig.12. Final step in simplifying the circuit of Fig. 10.
with $1 / g_{m}$ and can thus be omitted from the equivalent circuit. If we combine the two resistors $1 / g_{m}$ the circuit takes the simple form shown in Fig. 12, to which we can apply Ohm's law. Suppose the meter requires $100 \mu \mathrm{~A}$ for full-scale deflection and has a resistance of 50 , ohms. Suppose that the mutual conductance of the valves is $2 \mathrm{~mA} / \mathrm{V}$ and that full-scale deflection is required for
a signal of 1 V . The total resistance in the circuit must be $1 /\left(100 \times 10^{-6}\right)$ i.e. 10,000 ohms. To this the valves contribute 1,000 ohms ( 500 ohms each) and the meter 50 ohms. The balance, i.e. the required value of $R$, is thus $10,000-1,050=8,950 \mathrm{nhms}$.

Earphone problem. We now turn to problems of the type where the resistor value is fixed and the circuit feeding it has to be adjusted to provide the required performance. An example of such a problem occurs when the load is an earphone of say 2,000 ohms resistance and it is desired to drive it directly from the collector circuit of a transistor. How can we ensure maximum power into the earphone?

We have already discussed directlyconnected loads and Fig. 6 represents the conditions in the circuit. Let us suppose that the supply voltage and emitter voltage have the values indicated in Fig. 6. The quiescent collector voltage is hence 7.5 and the maximum voltage which can be developed across the earphone has $4.5-\mathrm{V}$ peak value. To generate this voltage across a resistance of 2,000 ohms requires a peak current swing, from Ohm's law, given by:

$$
\begin{aligned}
I_{p k} & =\frac{4.5}{2,000} \mathrm{~A} \\
& =2.25 \mathrm{~mA}
\end{aligned}
$$

We thus need to bias the transistor to take a mean collector current of precisely this value. If a smaller mean current is used, the power output will be less than the maximum achievable: if a larger mean current is used, the quiescent collector voltage will be too low and there will be severe distortion of the negative-going collector-voltage halfcycles. One method of obtaining a desired mean collector current is described later in this article. When the transistor delivers its maximum output the collector voltage swings between 12 V and 3 V and the collector current swings between 0 and 4.5 mA . The power delivered into the earphone is given by $V_{r m s} I_{r m s}$ but it is more convenient to use the equivalent expression $V_{p k} I_{p k} / 2$. Substituting for $V_{p k}$ and $I_{p k}$ we have:
power into earphone

$$
\begin{aligned}
& =\frac{4.5 \times 2.25 \times 10^{-3}}{2} \text { watts } \\
& =5 \mathrm{~mW} \text { approximately }
\end{aligned}
$$

which is sufficient to give adequate sound output.

Feeding coaxial cables. Another example of a circuit in which a transistor has to work into a fixed-value load resistor is illustrated in simplified form in Fig. 13, which shows an emitter follower stage used to feed video signals into a coaxial cable. The characteristic resistance of the cable is commonly 75 ohms and if the cable is correctly terminated


Fig.13. An emitter follower used to feed video signals into a coaxial cable.


Fig.14. S is a stereo-mono switch which could lead to severe distortion.


Fig.15. Essential features of the circuit of Fig. 14 with $S$ closed and for the left-hand signal.
at the receiving end this is also the value of the load for $\mathrm{Tr}_{1}$. Suppose it is required to feed a signal of 1 V peak-to-peak value into the cable. A simple application of Ohm's law shows that the current required to generate a $1-V$ signal across a 75 -ohm resistance is approximately 13.5 mA . The transistor must therefore be capable of supplying a peak-to-peak current swing of 13.5 mA .

If the signal fed to the cable were a.f. or any other type with a waveform symmetrical about the time axis the transistor could be biased to take a mean emitter current of 7 mA : a peak-
to-peak current excursion of 14 mA would then be possible. However, video signals are not symmetrical and it is not possible to solve the problem so simply. One way of operating the emitter follower is to arrange for the negative-going extreme of the input signal (sync level, say) to be clamped at 0 V . For zero voltage input the emitter follower would give zero emitter current output. The positive-going extreme of the input signal (white level) will then be at 1 V which will drive the transistor into conduction, the 75 -ohm load ensuring that the emitter current is 13.5 mA .

Stereo-mono switch. Fig. 13 is an example of a circuit where the load is of low resistance and care must be taken to see that the transistor feeding it can supply sufficient current to produce the required voltage output. Sometimes it is not immediately obvious that the load is of low resistance: Fig. 14 is an example of such a circuit.
$\mathrm{Tr}_{1}$ is an emitter-follower stage in the left-hand signal chain of a stereo equipment and $\mathrm{Tr}_{2}$ is the corresponding emitter follower in the right-hand channel. $S$ is a switch which connects the two channels in parallel for monophonic reproduction. This circuit can produce very unsatisfactory results because the switch drastically alters the operating conditions of the emitter followers. When $S$ is closed $\mathrm{Tr}_{1}$ has as its load $R_{e 1}, R_{e 2}$ and the emitter input resistance of $\mathrm{Tr}_{2}$ all in parallel. The smallest of these resistances and the one which therefore determines the value of the effective load resistance is the emitter input resistance of $\mathrm{Tr}_{2}$. Thus the essential features of the circuit are as shown in Fig. 15: a significant feature of this circuit is that the effective generator resistance of $\mathrm{Tr}_{1}$ and the effective load resistance of $\mathrm{Tr}_{2}$ are both equal to $1 / g_{m}$ approximately. Now $1 / g_{m}$ can be as low as 15 ohms if the transistor has a mean emitter current of 2 mA . For such an emitter current, the greatest emitter-current swing possible from $\mathrm{Tr}_{1}$ is 2 mA and this, in flowing through the effective load resistance of 15 ohms, generates a signal of 30 mV peak value. This is the greatest output voltage swing which $\operatorname{Tr}_{1}$ can deliver without distortion. It is clear from Fig. 15 that if the signal voltage across $\operatorname{Tr}_{1}$ load resistance is 30 mV , then the generator voltage is 60 mV and this is therefore the greatest signal input which $\operatorname{Tr}_{1}$ can accept without overloading and consequent distortion. From the symmetry of the circuit $\mathrm{Tr}_{2}$ similarly overloads for input signals greater than 60 mV peak value.
It would be better to connect the stereo-mono switch between the bases of $\mathrm{Tr}_{1}$ and $\mathrm{Tr}_{2}$.

# A digital clock synchronized to a broadcast atomic time standard 

by D. A. Bateman, B.Sc.

By combining an electric digital clock with a suitable radio receiver and a pulse discriminating circuit, it is possible to synchronize the clock to a selected time signal. The clock described here is designed to synchronize every minute to the signals broadcast from MSF Rugby, enabling it to be economically "slaved" to an atomic clock and display the nationally defined time scale to an accuracy of 1 ms . Without the radio signals, the clock will run on its own internal quartz oscillator for several weeks before errors of a few seconds accumulate.

An independent and accurate clock (excluding portable atomic clocks) will usually depend on a quartz crystal which is chosen to suit the application. For example, a low frequency crystal $(<100 \mathrm{kHz})$ in a domestic situation should be stable to several parts per million, whereas a selected high frequency crystal operating at a closely controlled temperature can be stable, at no little cost, to parts in $10^{7}$ per year. The frequency of oscillation of such crystals may in turn be checked directly against atomic clocks, or indirectly via the national and international frequency standards which are broadcast from various radio stations.

Although the rate of the crystal may be suitably uniform, it does not necessarily mean that the clock which it is driving is telling the correct time as this depends on the accuracy or manner with which the clock is set in motion. An example of this frequency checking approach has recently been given ${ }^{1}$ where the temperature-controlled crystal was checked against the BBC 200 kHz transmissions (the frequency of which is controlled by an atomic clock), but even so, it was acknowledged to be difficult to maintain the clock to with in 3 seconds per year.

The alternative approach is to synchronize to specific impulses, a technique which has already been exploited with electromechanical clocks, but electronic clocks synchronized by "wireless" methods have advantages, including accuracy and portability.

The transmissions from MSF Rugby contain time markers, at 60 kHz , taking the form of interruptions of the carrier as in Fig 1. The call sign is given twice in Morse code just before the hour, and corrections for the difference between UTCC and GMT are given each minute in the form of double breaks between
seconds $01^{\prime}$ and 15, the position and number of "emphasized" markers indicating the sign and magnitude of the correction in tenths of a second. The minute mark - of 500 ms duration -- is identifiably different in the signals and may be detected electronically for synchronization purposes.

## Circuit operation

Briefly, the operation of the complete clock, shown in Fig. 2, is as follows. Assuming that the clock is already working, has been set manually to the nearest minute and is receiving the time signals, a special logic circuit detects the minute mark and "primes" the clock for synchronization at 01 seconds. At the instant this event is detected, the seconds display and part of the crystal dividing chain is set to zero and then restarted, and a subsidiary circuit restores the display to 01 seconds. If the clock was running up to 20 seconds slow then the synchronizing pulse would bring it forward; conversely, if up to 40 seconds fast it would be brought back to

Fig. 1. The form of time signals on 60 kHz from MSF Rugby, prior to September 1974.
the correct time. Precautions are taken which ensure that any electrical interference cancels the process, and the clock continues uninterrupted and will synchronize after the next minute mark.

The central timekeeping element of the clock is a 2.097152 MHz quartz crystal divided by $2^{21}$ to give 1 Hz pulses. An output at 32 Hz is also taken for the minute-mark detecting logic. C.m.o.s. integrated circuits are used to maintain the oscillator and carry out the division for a total dissipation of 3 mW . The final 14-stage binary divider has a reset facility so that the counters may be set to zero and then released, the count being sufficiently far back so that the maximum error is about 0.06 ms from the moment of release.
The digital clock part is conventional, using t.t.1. for further division, and non-multiplexed driving of seven segment l.e.d.-type displays. An input is available for zeroing the seconds and tens of seconds counters, and unless a synchronizing pulse is received at this input, or the dividing chain, the clock behaves as a normal digital clock with a crystal oscillator.
To receive the time signals, a straight t.r.f. receiver with a ferrite rod aerial is

used. The rectified signal is inverted to give output pulses as in Fig. 1, and the bandwidth is made wide enough, together with a suitable gain setting, to ensure that the output follows the "r.f. off" transition to within 1 ms . A.g.c. is not incorporated, because the received signal level is fairly constant, and also because an increase in gain when the transmitter is off would increase the sensitivity to noise.
A block diagram of the minute-mark detecting logic is shown in Fig. 3, and the method of operation is as follows. The output from the MSF receiver is applied to monostable A and gates B and $C$, the monostable having a period $t_{1}$, where $t_{1}<1 \mathrm{~ms}$ for a synchronizing accuracy of better than 1 ms . On arrival of the minute mark at 00 seconds, the monostable is triggered and in turn resets the binary counters and the RS flip-flops D and E as shown; for the remainder of the pulse (period $T_{1}$, Fig. 1) the gate $B$ is opened, passing the 32 Hz pulses to the four-stage binary counter F, flip-flop D being set after a count of 15 has accumulated. (Any interference detected during this period causes a reset and the process is abandoned.) The output from flip-flop D, together with gates $C$ and $G$, pass the 32 Hz pulses to counter H when period $T_{2}$ (Fig. 1) commences. As before, flip-flop $E$ is set when a count of 15 has accumulated, and again any interference during the count will cause a reset.
The system is now "primed" and ready to pass a reset pulse to the counters at 01 seconds. This is achieved by passing the reset pulse through gate I, which is possible only when both flip-flop $E$ is in the required state and the third input is set to logical 1 , either manually or automatically, by the


Fig. 2. Block diagram of the complete instrument. Standby battery powers the oscillator and counters only, as shown by dotted line.
clock. In order to reduce further the risk of setting the clock to a burst of interference after initial synchronization, this latter facility may be used so that the clock itself will only permit synchronization between seconds 58 and 02.
ln the "primed" state the circuit now awaits the arrival of time marker 01, and when this occurs a reset pulse is transmitted to the oscillator dividing circuit and the seconds counting stages of the clock, causing the clock to display 00 seconds, and monostable J changes
state. This monostable has a period $t_{2}>t_{1}$, and at the end of $t_{2}$ the output of gate K returns to logical 0 causing the display to read the correct time, i.e. 01 seconds; $t_{2}$ is sufficiently brief so that any flicker in the display is undetectable. The output of the monostable also resets the separate display indicating that synchronization has taken place.

The operation is such that the system is "primed" after counting 15 of the 32 Hz pulses during period $T_{2}$ and therefore exposed to the radio signals for a waiting period of about 30 ms . Anyinterference before the seconds marker could put the clock in error by up to 30 ms , but this risk could be reduced by changing the 32 Hz pulse train to some higher frequency and using more counters to count up to say 495 ms ,

when the "prime" interval would be about 5 ms .
As far as can be determined the clock works perfectly in a domestic environment, but a further refinement to ensure foolproof minute-mark detection could take the form of another counter stage following the first four-stage binary. This could be arranged to cause a cancel if a count of 17 were accumulated, indicating that period $T_{1}$ was longer than 500 ms and therefore not genuine.
The performance of the clock may be summarized in the following remarks. After initial setting it will detect the minute mark and synchronize at 01 seconds to an accuracy of 1 ms ; it will similarly synchronize at each successive minute; positive or negative leap seconds are automatically followed; a light shows that the clock is in the synchronized condition; any radio interference detected during the minute mark and the next 470 ms causes the synchronizing process to be abandoned for that minute; once synchronized, the clock may be set so that synchronization is possible only between seconds 58 and 02 ; if the clock is so set, the quartz crystal will enable the clock to be without the radio signals for about 2 weeks before drifting "out of lock"; a battery standby maintains the oscillator and dividing circuits if disconnected from the mains, and on reconnexion the correct time is displayed and synchronized after the next minute mark.
It is quite feasible to synchronize a clock by similar means to other time signals, either from other low frequency transmitters, such as Switzerland's HBG ( 75 kHz ) or Germany's DCF 77 ( 77.5 kHz ), or the "six pips" in domestic


Fig. 4. Pulse-stretching logic to maintain independence from the new NPL time code.
services ${ }^{2}$, all of which have different but identifiable components in their signals.
The clock had been operating satisfactorily since October, 1973, until mid-September 1974 when the National Physical Laboratory introduced a modification to the time signals. The purpose of this change is to broadcast a time code of GMT hours and minutes, so that each minute may be electronically identified without the use of a separate clock or counting from the hourly call sign. The code consists of a number of 10 ms pulses containing the time information in b.c.d. form within the first 200 ms of the originally blank part of the minute marker ${ }^{3}$ (period $T_{1}$, Fig. 1). Unfortunately, as a consequence of the design, my clock rejected this information as interference! However, by using a pulse stretcher as in Fig. 4, and inserting this between the radio and the minute mark detecting logic, the time code may be blanked out so that the clock synchronizes each minute as before.

Fig. 5. Digital clock circuit diagram.

It is worth emphasising the differences between these two schemes. The NPL time code enables one to have a radio with a decoder which (assuming no problems with interference) gives the nationally defined time, and the ability to switch the "clock" off say, in the evening, and then obtain the correct time within a minute of switching on the next morning. Conversely, if the transmitter goes off the air, as it does for 4 hours per month, the time is not available. The system described here, on the other hand, is a clock which is able to synchronize by radio the seconds and part of the oscillator dividing chain to within 1 ms of the time scale. This method has a greater degree of independence, in that it will continue to give the time without the radio signals. Clearly, a future system could combine the advantages of the two separate approaches.

## Construction

These notes and accompanying circuit diagrams represent the clock in its finished form, and as such contain a partial record of its development. The clock is capable of further refinement, either in design or by the use of bought out items, and these notes are intended to give general information, rather than give a detailed circuit description and act as a practical or constructional guide.

Digital clock. This circuit, shown in Fig. 5 , was constructed on a $5 \times 33 / 4 \mathrm{in}$ Veroboard, permitting reasonable spacing between the integrated circuits. The displays were mounted at right angles

to the plane of the board along one edge by wiring the sockets in a wire frame and bridging the 150 current-limiting resistors directly from the 7447 s , this resistor value being as given in a Hewlett Packard data sheet for a current of about 22 mA per segment. Setting of the clock is achieved with a three-position switch on the rear panel by routing to the minute count, either 1 Hz or 32 Hz pulses, enabling a fairly rapid run through of the hours $(32 \mathrm{~Hz})$, to be followed by a slower minute advance, and normal operation. Using this size of board and layout and components as shown in the diagram, no problems were due to interference were experienced. Some power supply connexions have been omitted in the diagram to avoid repetition.

Pulse detecting logic. A $5 \times 33 / 4$ in Veroboard was also used for the circuit of Fig. 6 and the board was bolted to metal strips attached to the clock board, so that all the digital circuitry was in
effect on one large panel, $71 / 2 \times 6$ inches in size.

In order to permit synchronization at any time during the minute, a switch on the rear panel may be put open circuit ( $=1$ input to the triple-input gate 7410 ); with the switch closed a 1 is available only during seconds $58-02$, restricting synchronization to this time slot. Note that the "synchronized" l.e.d. goes on at 58 s and off if synchronized, but remains on if synchronization does not take place.

Crystal oscillator. The 2.097152 MHz crystal was purchased from the McKnight Crystal Co., Southampton, and the oscillator circuit in Fig. 7 is based on the data given in the RCA Application Note ICAN 6086 - "Timekeeping advances through COS/MOS technology." Frequency setting was achieved by monitoring at pin 12 of the seven-stage binary, CD4024AE, thereby avoiding loading of the oscillator. The $18 \mathrm{k} \Omega$ and $6.8 \mathrm{k} \Omega$ resistors in the $\mathrm{V}_{\mathrm{DD}}$
leads were left in the circuit after current/voltage experiments. A $33 / 4 \times$ 2in Veroboard was used for the oscillator and divider chain, the whole being mounted in a metal box. The reset control could be operated manually to stop the oscillator and clock, for either releasing the clock near a given time signal, or demonstrating the synchronizing abilities of the clock after having been set wrongly for $a$ number of seconds.

Radio receiver. The 60 kHz radio waves are picked up on an external tuned ferrite-rod aerial, the stepped down output being fed down a 2 m length of coaxial cable to the receiver. The length of cable is not critical, 50 m having been used with only a slight effect on the tuning. Aerial dimensions, number of turns, and value of tuning capacitor are also not critical, but a signal generator is useful in initially finding resonance. Similarly, situation is not critical, a safe and convenient place being floor or

Fig. 6. Pulse detector circuit. L.e.ds are H.P. 5082/4850.

ground level, providing the aerial is not too near a ring main, or other source of switching transients, etc.
A straightforward t.r.f. amplifier, followed by a diode rectifier, d.c. amplifier and Schmitt trigger, comprises the complete receiver as shown in Fig. 8. The r.f. stages are not conventional, and damping resistors were used at an early stage in the design to ensure wide bandwidth; indeed, in the presence of strong signals the tuned amplification could be dispensed with. The circuit shown has a bandwidth of about 400 Hz and, with a low gain setting, gives a 1
output within 1 ms of the r.f. off transition. Constructionally, care had to be taken to prevent oscillation by earthing unused strips on the Veroboard, and mounting in an aluminium box.

Audio oscillator. An LC oscillator was chosen to give a reasonably stable 1 kHz sinusoidal waveform. Although the "modulator" gives a slight click for each "on," this system gives quite adequate pips. Fig. 9 shows the circuit diagram.

Pulse stretcher. In order to maintain
independence from the new NPL time code (introduced in September, 1974) a pulse stretcher is necessary to override the code which ocurrs during the first 200 ms of the originally blank part of the minute mark. Fig. 10 shows the relatively simple modification, which was included on the same board as the pulse detecting logic, together with some additional power supply decoupling, and consists of a monostable and gates interposed between the MSF input buffer transistor and the pulse detecting logic; the monostable timing resistor is about $14 \mathrm{k} \Omega$ for $C=25 \mu \mathrm{~F}$.


Fig. 8.60 kHz radio receiver and pulse shaper. $T_{1}$ is 200 and 33 turns 36 g ; $T_{2}$ is 340 and 57 turns 38 g ; both in



Fig. 9. The 1 kHz oscillator is in Siemens N28/400A pot core.

Fig. 10. Pulse-stretcher circuit.

Fig. 11. Power supply with battery standby. Rectifier and diodes are Electrovalue types.

Power supply. This was developed specifically to give battery standby to the "heart" of the clock, i.e. the crystal oscillator and the clock divider chain, and it is very satisfying to move the clock from one location to another and display the correct time as soon as it is plugged into the mains! The circuit is that of Fig. 10.
Originally, the supply was designed for the relatively heavy current consumption of 1A for l.e.d. displays requiring 22 mA per segment, but the more efficient type finally used was set for about 12 mA per segment by simply lowering the output volts and inserting a series resistor to avoid changing all the $150 \Omega$ resistors. When the mains supply is turned off the l.e.d.s and drivers go off without affecting the timing.

The clock logic is driven from a separate 5 V supply with a battery standby, a PP9 giving nearly an hour of continuous reserve: an external socket gives extended capability from a 12 V lead-acid battery if required. The crystal oscillator also has its own battery standby - a PP7 - but this is partly for historical reasons, as when finished at an early stage, the oscillator was left running continuously.

Case. For the case, the attractive Vero D series was used, type 81CD-1U-3 and 8FP-1U-19 front panel. A particular advantage of this (large) case was that the lower panel on which the various circuits and boxes could be generously spaced out, could be unscrewed. A minimum number of items were included in the front panel - an aperture with a red plastic filter to improve the contrast of the displays, the two l.e.d.s showing the presence of MSF and state of synchronization, and pip volume control - the remaining switches and sockets being mounted on a specially included rear panel.

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# 75 years of magnetic recording 

4 - The boom years, 1946 to . . .

by Basil Lane<br>Assistant Editor, Wireless World

Subsequent to World War II the development of magnetic recording was to proceed at a rapid pace. Applications originally seen for it but unexploited because of the lack of a high state of technology came into being, and totally new applications were found such that today we are hardly able to do anything without coming into contact with some aspect of magnetic recording.

The immediate post war period saw a slight hiatus in the progressive development of magnetic recording, since the tape recorder, as produced by AEG, was a totally new form of machine which was unknown outside Germany.A few paper tape machines had appeared in America in the late 'forties, one of which was the Brush Soundmirror. But what was to influence design from this point in time was the dissemination of a vast amount of intelligence information gleaned from the prostrate German industry by teams of Allied Forces engineers and technicians. The resulting reports were made available to anyone interested and were directly responsible for the eventual production of close copies of the Magnetophone such as the. RGD domestic console machine and its portable professional version.

In America Col. Richara Ranger had retired from his Forces post and set up a company devoted to the manufacture of the Rangertone recorder - looking remarkably like a K4 Magnetophone. ${ }^{52}$. John Mullin, also retired from Armed Service, had managed to send two dismantled machines and 50 reels of tape back to his home where he re-assembled and modified them to an a.c. biased version. ${ }^{53}$ These he used in a series of lectures that opened two remarkable new avenues of commercial development. The first of these was the decision of the directors of Ampex to go in for the manufacture of tape machines, this resulting in the appearance of the first Ampex studio recorder (the model 200) in 1948. So successful were these machines, that twelve were bought by the ABC Network at $\$ 5,200$ each and installed for broadcast purposes.
The second line of development resulting from Mullin's early lecture tour came from the interest shown in the machines by Crosby Enterprises.

Headed by that grand old master of popular ballads, Bing Crosby, this company was probably most directly responsible for the early introduction of magnetic tape into American broadcast studios.

## Crosby interest in tape

Briefly, the story is told that Mullin was approached by representatives of Crosby Enterprises who told him that the Philco sponsored radio put out by Bing Crosby was losing its audience quite rapidly. The show was entirely recorded before broadcast and since the only quality medium available for this purpose was disc, the problem of editing the original performance into a slick
series of sound cameos was $\mathrm{f}_{\mathrm{r}}$ aught with technical difficulties. Many disc to disc transfers had to be made, all of which resulted in a deterioration of quality which was, apparently, responsible for the declining audience. Tape, they felt, might prove to be the solution, and accordingly a demonstration was mounted to test the merits, not only of Mullin's Magnetophones, but also those of an optical system developed by RCA and two machines manufactured by Colonel Ranger as copies of the original Magnetophone. As it turned out the original Magnetophones owned by Mullin won the day hands down and the whole of the 1947-48 season of Crosby shows were recorded using these

Fig. I. Recordon paper disc dictating machine produced by Thermionic Products. (Courtesy of Racal Thermionics Ltd.)

machines and the original 50 reels of German tape. It was not until 1948 that 3 M were to produce a suitable tape for use on the machine (Type 111). ${ }^{13}$

With the success of Mullin's tape machines assured, he spurred on Ampex to complete their first design, the Ampex 200, which represented a real improvement over the Magnetophones. At the same time Col. Ranger was able to improve his own machines, but these were rather smaller and more suited to the domestic market.

Over succeeding years Crosby Enterprises were to employ John Mullin as their chief engineer, the company at first distributing Ampex machines. Subsequently they were to relinquish the Ampex franchise and he bought into the 3 M Company as their Mincom division. However, they appear again later in our story with product developments of their own, before this takeover was to occur.

Here in the UK, EMI had launched its first professional studio machine, the BTR1, in 1947 and had installed it in their own Abbey Road Studios. Like the Ampex 200, the EMI machine was an improvement on the Magnetophone design although the high tape speed of 30 i.p.s. was still in use, due to the rather poor quality of the tape then available. Since the EMI tape factory had not yet gone into full production, initial recordings were made on a Continental tape called Genotone, that clearly owed its origins to the I.G. Farben methods, since it was a homogeneous tape. Shortly after, improved tapes began to appear and the BTRI was converted to offer both 30 i.p.s. and 15 i.p.s.

Although it may appear that Rangertone, Ampex and 3M were clear leaders in the production of post-war professional tape recorders, this was not strictly true, for apart from the slowly reviving AEG Telefunken Company, there were several other companies in America such as Magnecord, which switched from wire to tape machines in 1948, Stancil Hoffman with a multitrack recorder and Brush with their Soundmirror paper tape recorder.

However, it was in the domestic consumer market that the greatest interest was to be created. Never before had there been the technology available to make home recordings which could be edited with the ease of tape, and the first models available in the UK were met with considerable enthusiasm. Just about the first product on the market was the Wright and Weaire deck made by an old established manufacturer of radio components. This came on the market in March 1949, followed closely by a tape recorder from Scophony-Baird for use with film as a sound-track machine, together with the "Sound Magnet" from General Lamination Products and the Brush Soundmirror, imported by Thermionic Products Ltd.

The performance of the Wearite tape deck was modest, giving two-track mono on 0.25 in tape running at 7.5 i.p.s.
and 3.75 i.p.s., and at this stage, with the only tapes available being paper, or imported Continental types of relatively low quality, the frequency response at the slowest speed made it suitable only for speech. In America, tape recording as a hobby got off to a very good start. There had already been quite a wide range of wire recorders available from such companies as Pierce, Brush, Pentron and the Electronic Sound Engineering Company from 1946. By 1947 the Brush Soundmirror tape recorder had been joined by the Ekotape from Webster, already established as a wire reçorder manufacturer and an odd paper disc machine from Brush called the Mail-a-Voice. This machine was later to be re-designed by Thermionic Products Ltd and marketed here under the name of the Recordon. Intended as a dictating machine, the Recordon had the head mounted in the end of a curved arm which was guided in a spiral pattern by a stylus riding in the grooves of a solid disc fitted on the turntable spindle. A special version of this disc was made and marketed in pairs, where the spiral groove would have a random lateral wobble thus "scrambling" the spiral track to prevent replaying on a standard machine. Thermionic made these machines to a UK design but under licence from Brush from 1948 until about 1956, just before its take-over by Controls and Communications Ltd. The UK version of the Soundmirror was also developed into a different unit and marketed under the same licencing agreement.

From 1949 the number of machines
and manufacturers proliferated with such names as Ferrograph from Wright and Weaire, Simon, Reflectograph appearing in the UK and in America Berlant Concertone, Magnecord, Crestwood and Fairchild all appearing on the domestic or business scene. At this stage, all of these were single channel, either single track or two (half) track machines. The industry was poised for the advent of stereophonic recordings.

## The birth of stereo tape recorders

The earliest stereo, or rather two channel recording, made by magnetic recording appears to have been that by Bell Laboratories in 1939 , ${ }^{14}$ followed by the Magnetophone recordings of the War years. However, subsequent to this there were some experiments made in 1948, by Marvin Camras, using a three channel staggered head machine recording on wide tape. ${ }^{54}$ Interestingly, Camras made the distinction between binaural and stereo recordings.

The former were made with two microphones placed close together, as if they were a pair of ears; stereo recordings were made with two, widely spaced microphones. However, it was to be some little time more before stereophonic tape recording really became fully developed.

Part of the problem was to design a vertically stacked, multiple track recording and replay head. All of the earliest recordings were made with staggered heads. However, by 1954, EMI had reached the stage of making regular stereo recordings at their Abbey Road studios and in April 1955 the Stereoson-

Fig. 2. The BBC video recorder code-named VERA.

ic tape record was first demonstrated to members of the Press. ${ }^{55}$ This was a two track stereo recording initially mastered at 15 i.p.s. and then duplicated down to 7.5 i.p.s. for domestic consumption.

RCA were not long in following this lead, since in June 1954 they marketed, at first mono tape recordings, and then followed this with two-track stereo recordings in September of the same year. The main disadvantage suffered by RCA was the need to use heads staggered apart by 1.25 in. ${ }^{56}$

Domestic machines to replay these commercial recordings were few and far between and at first the system was encouraged by the sale of stereo heads, such as that offered by Truvox in 1955 or a conversion kit containing the additional heads and amplifiers as marketed in the US by V-M. Recorded tape seemed to become quite popular in America and to a lesser degree over here in the UK American companies such as Omegatape, Ameritape, Bel Canto and Livingstone appear during the early 'fifties, some of these being imported into the UK. Due to the precipitous jump into marketing staggered head recordings, in-line machines were much later on the market in America, some conversion kits and machines appearing in 1957.

All this was rather surprising since both RCA and Ampex had developed in-line heads by 1954 and in fact Ampex had a three-core head in vertical alignment by 1956 which was used for several spectacular public demonstrations. ${ }^{44}$ This Ampex machine was the precursor to the multi-track machines now in regular use in recording studios. One of the earliest machines in use at Abbey Road, after the introduction of the two track BTR3, was a modified Telefunken T9U which was installed about 1958. From this date, the available number of tracks on professional machines was to multiply and tape widths up to two inches employed to accommodate the remarkable maximum of 24 tracks used today.

## Video recording

Magnetic recording of pictures seems to have arisen at times in the most unlikely places. Some of the earliest mentions have been already remarked upon, but perhaps the most detailed is contained with a British Patent of 1928, registered by one Boris Rtcheouloff ${ }^{57}$ of 179 Cromwell Road, London! Based on the Poulsen recorder the system used'many ideas developed in later years and is a model of ingenuity.

In practical terms it was to be quite some years before a commercially viable system was to be evolved and by 1953 at least three companies in America and the BBC here were working on early examples.

December 1953 saw the announcement by RCA of one of the earliest machines, capable of not only recording and reproducing black and white pic-
tures, but also colour. This was a linear machine based on established audio methods of recording with the three basic colour signals, red, blue and green being recorded on three tracks with a bandwidth of 1.5 MHz , synchronising signals on a fourth track, a fifth track taking the signal "highs" from 1.5 MHz to 3.5 MHz and finally two audio tracks. This machine consumed tape at a rate of 20ft per second. ${ }^{58}$

Amazingly, 3M claim an earlier experimental video machine developed in 1948 using spinning heads and wide tape to produce transverse recorded tracks and go on to say that Ampex were to adopt these principles in their later machine. However, this remark appeared in an internal publicity document and 1 have found no other references. Certainly Crosby Enterprises developed a working video machine, which appeared briefly in 1954, but this and all other developments were to be overshadowed by the Ampex quad recording system. Mullin claims in his article on the history of American tape recording, that a patent was filed in November 1950, after first recording crude video pictures of aircraft landing and taking off. ${ }^{53}$

The first demonstration of video recording from Crosby Enterprises, now intimately linked with 3 M , was in 1951 and by 1955 when Ampex first demonstrated their machine several models had been made and installed. Here in the U.K. the BBC were busy developing their own short-lived video recorder called VERA, ${ }^{59}$ using the longitudinal recording methods adopted by RCA and Crosby Enterprises. The use of an Ampex quad machine by the commercial television stations precipitated the fall of this monster machine and soon the Ampex standard became standard. The first sight of the latter development was at the NARTB show in May 1956. The remarkable feature of this design was the vertically rotated head coupled with a relatively low tape speed of 15 i.p.s. ${ }^{60}$ This reduction in tade consumption, coupled with remarkable quality, spelled the doom of longitudinal systems which completely disappeared until recently. They were to re-appear in a slightly different context with p.c.m. encoding. (See article on digital recording in this issue.)

Domestic video machines followed six years later after several false starts, with the Toshiba helical scan system ${ }^{61}$ being an early example described in 1961. However, even this type of machine and its competitors were not to establish a really domestic market to this day, although it would seem that the Philips VCR has re-awakened interest on this front.

## Cassette and cartridge systems

The tremendous public interest in tape recording was probably one of the principle motivations for the development of cassettes and cartridge. Those


Fig. 3. The first compact cassette recorder marketed by Philips in 1963.
who are old enough and were really interested, may well remember the tremendous confusion caused by one system after another appearing on the market. One of the earliest patents for a cassette (this term is applied to reel-to-reel tape containers), utilising mul-ti-track recording on tape is that secured by Herman S. Heller ${ }^{62}$ in 1949. The cassette was clumsy, using $0.25 i n$ wide tape, but was unusual in that an eight-track record-replay head was proposed, this having been drawn from an earlier patent ${ }^{63}$ secured in 1940.

However, this particular invention did not see the light of day and it was not until George Eash, an American, patented the first commercial endless loop cartridge ${ }^{64}$ in 1957 that the system arrived to stay. This particular machine and system was developed principally for use as a background music source in stores. The first domestic tape magazine to appear was in 1954 and was the 24 track cartridge for use on a machine designed for the blind. ${ }^{65}$

In America, Marvin Camras introduced, in 1959, a tape spool loaded with tape having a special clip on the leader, and a machine which would automatically grab this clip and thread the machine. This, however, had been preceded by a large cassette type of magazine by Cousins, made in 1957. There then followed a series of cassettes and cartridges by RCA, Bell Sound, Fidelipac Echomatic and 3M, the latter being to the RCA design. ${ }^{66}$

An echo of the tape cassette format was seen in the brief appearance of a laboratory prototype machine jointly developed by 3M and CBS in 1960. The tape was 0.125 in wide and was driven at 1.875 i.p.s., the speed later to be adopted by Philips in their compact cassette system. This machine disappeared, but 3M's interest in magazine loading re-emerged in 1962 with a new cartridge and a machine manufactured by Revere, a company they had acquired in 1960.

However, the battle for supremacy was soon to be settled when Nortronics introduced first an eight-track head in 1965 and then followed it with an endless-loop cartridge machine in the same year. The Nortronics head was to be the key that RCA and Lear Jet required to complete the development of their cartridge which appeared later in that same year. The battle entered its final stages when large car manufacturess offered the RCA/Lear Jet system as an optional extra in 1965.
Here in Europe a similar battle was being fought with various formats offered by Grundig, Garrard and BSR, but stealing in under the shadow of all of these was Philips who, in 1963 introduced the first cassette recorder and the compact cassette system.

The survivors of this remarkable "systems war" are to be seen today, but with the possibility of a similar format war developing over video recording.

## Digital and other systems

An early application of magnetic recording for systems other than audio or video, was noise and vibration analysis, by Chrysler and General Motors: however even these machines were just used to record audio signals.

Storage of digital signals for computers was effected in the late 1940s and has now developed into a variety of formats including magnetic drum, reel-to-reel tape and cassettes.

Early p.c.m. recordings are described elsewhere in this issue, but one effort worthy of mention is the system used by Rudman in 1954 for the recording of signals in the frequency range $0-150 \mathrm{~Hz}$. ${ }^{67}$
One company still wholly involved in some of the more unusual applications of magnetic recording is Racal Thermionic, which grew out of the old Thermionic Products Ltd. Starting with multi-channel speech recorders for recording air traffic control communications, they have developed from their first crude effort of 1950 to the sophisticated version seen on the front cover.
In the concluding part of this series the latest developments in magnetic recording are discussed together with the history of tape from 1947 to the present day. Also included will be details of some of the more unusual applications for magnetic recording.

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ACTIVE DEVICES
Three leaflets from Microwave Associates give complete specifications on low-cost P1N diodes (bulletin 4306 A ), r.f.-burnout-tested mixer diodes (4125A) and high-power Gunn diodes (4507). The leaflets can be obtained from Microwave Associates Inc., Burlington, Mass., U.S.A.

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Motorola have published an eight-page cross-reference chart of linear i.cs, listing equivalents or near equivalents made by the major semiconductor companies. The chart is available from GDS Sales Ltd, Michaelmas House, Salt Hill, Bath Road, Slough, Bucks

Plessey has produced a data book, which gives details of its range of silicon integrated circuits linear and digital types, including the high-speed divider i.cs. The book is available at $£ 1$ from Plessey Semiconductors Ltd, Publicity services, Cheney Manor, Swindon, Wilts SN2 2QW.

A colour brochure from GEC is an attempt to cut through the confusion which tends to obscure the areas of choice when deciding on whether to use t.t.l. or m.o.s. large-scale logic in a system. The booklet is effectively a description of several types of m.o.s. transistor and complementary transistors and the methods used in custom integrated circuit manufacture, using both m.o.s. and bipolar devices. The publication can be obtained from GEC Semiconductors Ltd, East Lane, Wembley, Middlesex HA9 7PP

WW406

APPLICATION NOTES
The 1975 IEEE (American) Standards Catalogue, covering standards used in electronic and electrical engineering, is now available. The list includes the American National Standards published by the IEEE and those developed by the Institute. Single copies of the catalogue are obtainable free from IEEE Standards Department, 345 East 47th Street, New York, N.Y. 10017, USA

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A code of practice on the identification, prevention and avoidance of the effects of electrical interference on electronic equipment has been published by the Electrical Research Association Ltd. Mechanisms of propagation and coupling, layout of equipment and methods of testing equipment are described. The price is $£ 10$ to members of the Association - $£ 15$ for non-members - and the report is obtainable from the ERA Publication Sales Department, Cleeve Road, Leatherhead, Surrey KT22 7SA.

Search, Vol. 10, No. 1, published by General Motors, contains a description of recent research in the field of zinc/nickel-oxide batteries, with particular reference to the reduction in manufacturing costs and their eventual use in cars. The publication is published by General Motors Ltd, Stag Lane, London NW9 OEH
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## EQUIPMENT

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A comprehensive catalogue from Magnetic Tech nology (a division of the American Vernitron company) presents performance and mechanical information on over 250 servo and d.c. motors tachometers and torque motors. The catalogue is obtainable from Servodata Ltd, Highclere, New bury, Berkshire RG15 9PU at $£ 1$ by post.

National Sound Reproducers Ltd, have produced the new edition of their hire rate card for professional sound reproduction equipment. Equipment newly available for hire includes the

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WW410
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## GENERAL

The series of eurolec guides now include a 338-page publication, entitled "Electronic Manufacturers Alphabetical Listing/UK 1975", or Eurolec 46 for short. It is a listing of 850 UK manufacturers of a wide variety of electronic equipment and components, with information on activities, number of employees, contacts and related companies. The price is $£ 11$ by post and it is obtainable from eurolec. Little Waltham, Chelmsford CM3 3NU.

Airwork Services have sent us a 32 -page, four-colour brochure, describing the activities of their group of companies in the field of aviation and avionics. The booklet, which is in English, French, Spanish and Arabic can be obtained from Airwork Services Ltd, Bournemouth Hurn Airport, Christchurch, Dorset BH26 6EB

Zaar Colour Video Ltd have sent us their list of video services, which include film-to-cassette transfer, slide-to-cassette transfer, editing, recording and viewing facilities and insert filming. The address of Zaar is 339 Clifton Drive South, Lytham St. Annes, Lancashire FY8 ILP .. WW419

## PASSIVE DEVICES

Ceramic and polyester capacitors, in various forms, are the subject of a catalogue from ITW Electronics, which includes construction information, application notes, performance and mechanical information. The catalogue is produced by ITW Ltd, Electronics Division, 263 Farnham Road, Slough, Bucks

WW420

# Amplitude modulators 

# Set 22 of Circards, available now, gives circuits for various kinds of modulators, this article providing introductory background 

by J. Carruthers, J. H. Evans, J. Kinsler and P. Williams

Paisley College of Technology

If the amplitude of a high-frequency sinusoidal carrier, $c(t)=A$ cos $\omega_{0} t$ is made to vary in sympathy with the instantaneous value of a low-frequency signal $x(t)$ an amplitude-modulated signal is generated which has a spectrum concentrated in the vicinity of the unmodulated carrier frequency, $f_{0}$. The effect is to shift, or frequency-translate, the spectrum of the modulating signal to produce a pair of sidebands symmetrically disposed with respect to $f_{0}$ as shown in Fig. 1. The resulting wave may be described by: $y(t)=[A+x(t)] \cos \omega_{1} t$, so if, for example, $x(t)$ is a pure tone modulating signal represented by $x(t)=A_{1} \cos \omega \cdot t$ the a.m. output becomes $y(t)=\left[A+A_{1} \cos (\omega, t] \cos \left(\omega_{1} t\right.\right.$ which may be written as $y(t)=A[1+m \cos (1), t] \cos (1)_{0} t$ where $m=A_{1} / A$ is the modulation index, or modulation depth, and has a value $\leqslant 1$ if over-modulation is to be avoided.
The amplitude modulated waveform is shown in Fig. 2, and if this is displayed on an oscilloscope the modulation index may be found from $m=(B-C) /(B+C)$. As well as measuring the modulation index, the oscilloscope may be used to examine the linearity of the modulation process if it has an $\mathrm{X}-\mathrm{Y}$ facility. If the amplitude modulated wave is applied to the Y-amplifier and the low-frequency modulating signal applied to the $X$-amplifier a Lissajous figure of $y(t) / x(t)$ is obtained as shown in Fig. 3.

The above process is what is generally accepted as understood when referring to a.m. However a family of processes may together be considered as amplitude modulation techniques which include

- a pair of sidebands with carrier (a.m.)
- a pair of sidebands without carrier (d.s.b. or d.s.b.s.c.) or with diminished carrier (d.s.b.d.c.)
- an upper or lower sideband without carrier (s.s.b.) or with diminished carrier (s.s.b.d.c.)
- à pair of single sidebands with independent modulation (i.s.b.)
- one sideband, carrier and a vestige of the other sideband (v.s.b.)

In general, the above systems depend in some way on the use of four basic


Fig. 2,
methods of producing amplitude modulation.

- analogue multiplication
- chopper modulation
- non-linear-device modulation
- direct tuned-circuit modulation

Except for the last method listed, modulation is normally performed at low power levels and the required output power obtained by class-B amplification of the modulated signal.

Analogue modulation, or multiplication, is obtained by applying the modulating signal and the carrier to a circuit providing an output which is a function of the product of its inputs. Output from the multiplier or balanced modulator is ideally a d.s.b.s.c. signal. This arrangement is often convenient for producing an s.s.b.s.c. signal by removing the unwanted sideband and any residual carrier by means of band-pass sideband filter.

Many multipliers or balanced modulators are available in the form of purpose-designed integrated circuits for operation at carrier frequencies of at least 100 MHz . Depending on the nature of the modulating signal, the carrier


Fig. 3.
frequency and the required degree of unwanted-sideband and carrier suppression, the filter can be realized using L-C networks, quartz crystal lattice networks, ceramic disc resonators or mechanical filters. If the same signal is applied to both inputs of a multiplier it acts as a squarer and it, or any other square-law device, may be used to produce an a.m. output as shown in Fig. 4 if $v_{1}(t)=A+x(t)$ and $v_{2}(t)=V \cos (1,1, t$.

Chopper modulation is obtained by chopping the modulating signal at the carrier rate, using either a sinusoidal or a square-wave carrier, and then passing the resulting wave through a band-pass filter centred on the carrier frequency.

The bandpass filter will normally remove the component at the modulating frequency as well as the sidebands centred on the harmonics of the carrier frequency. To ease the requirements of the band-pass filter a balanced chopper modulator removes the low-frequency modulating signal component. The carrier-driven switches are normally realized using diode bridges or field-effect transistors.

Modulation using a non-linear device is achieved by adding the modulatingand carrier-frequency components and then passing the resultant through a bandpass filter centred on the carrier frequency to extract the a.m. signal. The non-linear device should have non-linearity not exceeding second-order and the highest significant modulation frequency should not exceed one-third of the carrier frequency.

Direct tuned-circuit modulation is achieved by controlling the voltage across a parallel-tuned circuit, tuned to the carrier frequency, by means of the modulating signal and pulsing the tuned circuit at the carrier rate with a highpower, class-C amplified carrier pulse. If modulating frequency is too high its rate of increase can be such as to cause the envelope of the a.m. wave to become distorted due to the failure to follow the modulation.

The modulation techniques discussed above which use band-pass filters must provide a filter bandwidth suited to the transmission of the desired signal whilst rejecting all unwanted components. For a.m. and d.s.b. this bandwidth must be


Fig. 4.
twice the highest modulating frequency and for s.s.b. it must be equal to the bandwidth of the modulating signal. In virtually all these cases the sharp cut-off required from the bandpass filter is only obtainable if the centre frequency of the filter is relatively low. Normally the filtration is achieved in the region of 50 Hz to about 1 MHz and the resulting modulated wave heterodyned, or frequency translated, to the required carrier frequency for transmission.

Another way is the phasing method of generating an s.s.b. signal which avoids the problems associated with filter design, but replaces them with the problem of designing a pair of networks ( $A$ and $B$ ) which are required to maintain a constant $90^{\circ}$ phase difference between their outputs whilst their output amplitudes are held constant over the bandwidth of the modulating signal. Selection of either sideband is achieyed by reversing the output from one of the balanced modulators or
by reversing the phase of either the carrier or the modulation to one balanced modulator. Because of the relative ease of inverting an audio signal, the modulating signal reversal is normally the simplest to accomplish in practice.

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Each card normally describes operation of a selected circuit, gives measured performance data and graphs, component values and ranges, circuit limitations and modifications to alter performance. Suggestions for further reading are included together with cross references to related circuits. The Circard concept was outlined more fully in the October 1972 issue of Wireless World, pp.469/70.

## New circuit book

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 cards" brings together the first ten sets of Circards, introductory articles to each of the subjects, and ten pages of additional circuits. The hardback A4book contains 168 pages, in which 120 cards are rearranged so that each is laid out on one page. A brief introduction precedes the articles, which were previously published in Wireless World, and each of the ten subjects is followed by an up-dating page. Corrections have been incorporated where appropriate.
"Circuit designs" is obtainable through leading bookstalls at $£ 10$ per copy. In case of difficulty order direct by sending remittance for $£ 10.40$ (includes postage and packing) to the address given later, making cheques payable to IPC Business Press Ltd. Advertisement appears on page 27 .

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21 voltage to frequency converters
22 amplitude modulators.

# Radio telescope project at Frensham Heights School 

by J. H. Duncan, M.Sc., Senior Science Master

During 1970 to 1972, as part of an M.Sc. Astrophysics Course at Queen Mary College, London University, it was decided to construct, and operate, a radio telescope of the radiometer type for examining solar radiation at 200 MHz , and at 450 MHz . Thanks are due to the Governors of Frensham Heights for a grant, and to the Royal Society for financial assistance. Also to the Staffs at Queen Mary College and Frensham Heights for advice and assistance. Several senior pupils of the School assisted in various aspects of the work. A parent also generously gave a quantity of very low-cost coaxial cable for the antennae.
I am not going to write a discourse on radio astronomy, as there are many books at all levels of understanding on the subject. Probably the best books, of moderate mathematical difficulty, are "Radio Astronomy" by J. D. Kraus (McGraw Hill), and ${ }^{\circ}$ Cosmic Radio Waves" by I. S. Shklovsky (Haryard University Press). However, there is a great shortage of articles with practical details of equipment. Probably the best available are two articles by J. R. Smith in the Journal of the British Astronomical Association Vol. 75, No. 2, 1965, and Vol. 80, Nos. 5 and 6, 197(). There was also a series of articles by F. W. Hyde in Practical Electronics, June 1971 to March 1972. There is also a book by F.
W. Hyde, "Amateur Radio Astronomy," which is now out of print, and somewhat dated, but which is well worth perusal if a copy can be obtained from your local library service. 1 owe a lot to these authors in the design of the equipment described.

This article is an account of the equipment constructed and operated at Frensham Heights. It was decided to construct phase-switched receivers, as these reduce internal noise levels to a fairly low level. The basic block diagram is shown in Fig. 1. When used in the phase switched interferometer mode, two antennae are used, with a half-wave phasing loop connected to the input as shown in Fig. 2. When used in the Dicke mode, one antenna is connected to one input, and a 75 ohm restive standard load connected to the other input, with no phasing link, as shown in Fig. 3.

The signal picked up by the antenna is immediately amplified at the antenna, and passed by coaxial feeder to the receiver antenna switching unit. For interferometric use, the two antennae should be separated as far as possible, and set out on an East-West baseline so as to get good fringe separation. For the Dicke mode, the greater the area of the antenna collecting surface, the better the signal
The output from the antenna is then

Fig. I. Block diagram of receiver.
amplified further in the receiver r.f. amplifier, and then converted to the i.f. broadband amplifier. This was at 40 MHz , and hàs a bandwidth of about 8 MHz . The signal is now rectified by a full-wave rectifier, and passed through a selective a.f. amplifier tuned to the switching frequency. The signal then passes to the phase.sensitive detector. The minimum


Fig. 2. Aerial and phasing loop connections.



Fig. 3. Dicke mode connection.


Fig. 5.


Eig. 6.


Figs. 4-8. Received signals using 12 Yagi aerials for 450 MHz .


Fig. 8.


Fig. 7.
detectable signal is proportional to $\checkmark$ bandwidth $\times$ time constant. Since the bandwidth is constant at about 8 MHz , several time constants were available at 0.5 secs., 2.5 secs. and 80 secs. This latter gave very smooth traces but the loss of detail was considerable. In this connection, very good quality paper dielectric capacitors must be used, or leakage will give an unknown time constant. The signal now passes to a d.c. amplifier and thence to the pen recorder.

The gain of the receiver must be kept at a constant value and stabilized power supply units must be used. The "markspace" ratio of the switch wave form generator must be adjusted with the aid, of an oscilloscope so that they are equal, or excess noise will appear in the output from the p.s.d.

Initial alignment was carried out using a signal generator, but final adjustment was made with the aid of a noise generator. All this equipment was constructed in the school, and valves were used because first, we were offered several TV sets for dismantling for components, and secondly, the author, being somewhat aged, felt more at home with valves than with transis-
tors. However, attempts are now being made to up-date the receivers by reconstruction using transistors. The pen recorders were also constructed to a design by D. Bollen given in Practical Electronics, October, 1971. There was some trouble with slip in the paper feed device, which occasionally gave distortion in the traces. On one memorable occasion, I had access to 12 Yagi antennae for 450 MHz , and these were strung out along the drive, with what seemed to be miles of cable. There were considerable problems in phasing these correctly, but the traces obtained were excellent (Figs. 4 to 8 ).

Finally, I would warn anyone attempting to build this type of equipment that it took some two years to get a workable trace, and I am not yet satisfied with the performance. I hope to improve the equipment considerably so that Fourier analysis can be performed on the traces, and also that some galactic, and extra-galacțic sources can be observed. I am also working on a receiver for observing radiation from the planet Jupiter on 20 MHz , using a $4 \frac{1}{2}$ ft . diameter directional-discontinuity ring-antenna.


## First African Landsat station

Zaire is to build the first ground station in Africa designed to receive Earth resources data directly from NASA's Landsat satellites. Landsat was originally called the Earth Resources Technology Satellite.

The new ground station to be built near Kinshasa will be able to obtain data from Landsats 1 and 2 as they pass within $3,000 \mathrm{~km}$ of Zaire's capital city. Data from the area which includes most of the African, continent from the northern border of Chad to South Africa and from Kenya to the Ivory Coast must currently be stored on Landsat 2 magnetic tape recorders for transmission to ground stations in the United States. Although Zaire is the first African nation to plan its own Landsat station, 13 African nations and two international organizations have undertaken Earth resources investigations using data of Africa provided by NASA from the two Landsats.

Zaire's new station will be able to produce both computer tapes and photographic imagery using received data. ERTS-Zaire will make copies of data available to scientists and others requesting data of the region. Ground stations are already in operation outside the US at Prince Albert, Canada, and Cuiaba, Brazil. Italy and Iran have agreed in the past year to build their own Landsat stations able to provide coverage of several African nations along the Mediterranean and Red Seas. Canada has also announced plans to build a second station near St. Johns, Newfoundland. Developing nations have found satellite data particularly valuable in learning about their natural resources, mapping geological and man-made features and conducting agricultural research.

## Crystals grown in space

Experiments designed to study growing large crystals in space will be conducted during the joint United States-Russian manned space flight during the summer. The experiment, called MA-028 Crystal Growth in Zero Gravity by

NASA, is designed to find out if large, defect-free crystals of value on Earth to the semiconductor industry, can be grown in space. American astronauts and Soviet cosmonauts plan to demonstrate to the world during July that spacecraft manufactured and launched by two different nations can rendezvous and dock in space and their crews can communicate using each other's language to successfully complete the joint mission. The crystal-growing experiments are designed to demonstrate a technique that holds promise in improving communications on the ground.

The experiment consists of six transparent tubes each of which contains three compartments. The outer two compartments will contain different salt solutions which, when mixed, form an insoluble compound which will grow into a crystal. The centre compartment contains pure water and, depending on the crystal to be grown, possibly a small seed crystal.

## Future of satellite communications

The key address given in April at the Institution of Electrical Engineers international conference entitled "Satellite Communication Systems Technology" was on the subject "Expanding horizons for satellite communications," given by Mr J. K. S. Jowett, Deputy Director of Engineering at the British Post Office, responsible for radio development. His subject included the discussion of: competition between satellite and terrestrial communications media, the types of service that satellite communication serves best, newlyemerging satellite services, desirable institutional arrangements, major technical and operational features, optimization of traffic capacity and the technological breakthroughs needed for further major advances in this field.
Mr Jowett summarized the answer to the question "To make further major advances in using this new medium what are the areas in which technological breakthroughs should be sought?" in the following areas:

- Frequency re-use within an individual satellite employing either multiple
spot beams and aerial discrimination or dual polarization.
- Frequency re-use within a total system by employing either multiple spot beams and aerial discrimination or dual polarization.
- Commercial use of frequency bands above 10 GHz , more especially between 11 and 14 GHz and subsequently a round 20 and 30 GHz . Very soon engineers will be gaining much-needed practical experience with experimental satellite systems operating in the bands around 11 and 14 GHz .
- Limitation of the freedom of normal movement of satellites by more efficient position control methods, thus permitting a closer spacing of satellites in the geostationary orbit.
- Employment of improved means to control side-lobe radiation of earth station antennas - and of satellite antennas using spot-beams.


## Jovian magnetic influences

Data returned by Pioneer 11 suggests that Jupiter's magnetic field, unlike Earth's, may be created by several "ring currents" deep within the liquid planet. Such a complex field close to the planet would be required to explain the field's high-energy particle pattern as well as the bursts of intense radio energy long-observed to emanate from Jupiter at long wavelengths. Planetary magnetic fields are believed to be produced by motions of the liquid material in planets' interiors, through mechanisms similar to those of electric dynamos. Earth and Jupiter are the only known planets with a substantial magnetic field.
Wobbling and tilting like a plate on top of a juggler's stick, Jupiter's field sometimes stretches across nine million miles of space and at other times shrinks in volume by three-quarters or more. Inside this pulsating field are the belts of intense radiation.

## Conference on spacecraft antennas

An international conference on "Antennas for Aircraft and Spacecraft" is to be held from June 3 to 5,1975 , at the Institution of Electrical Engineers. The sessions which will take place are: airborne radar antennas; radomes environment; calculation of antenna performance; ESRO studies of antennas for space systems; airborne antennas for satellite links; antennas for spacecraft; antennas for helicopters and light aircraft; h.f. antennas for aircraft; and integrated antennas for antenna rationalization. Enquiries concerning the conference should be addressed to The Manager, Conference Department, Institution of Electrical Engineers, Savoy Place, London WC2R 0BL.


## The amateur production line

Group constructional projects usually organised by local clubs and societies have become increasingly popular in recent years but a novel feature of one undertaken recently by six Dutch amateurs at Leiden, Holland, is that each of the six contributed one particular skill to the work, performing the same operation on each of six 144 MHz n.b.f.m. portable/mobile transceivers. One of the group was responsible for the electronic design; another the printed circuit layout; a third the mechanical work and so on. In effect a small "production line" was set up and resulted in six identical equipments. While most group projects tend to adopt well-tried, conventional circuịtry and design features, this was by no means the case for these transceivers, as an outline sent me recently by Dick Rollema, PAoSE, makes clear.
For example the five crystal-controlled receive and transmit channels are derived from five crystals by using in the transmitter section a voltage-controlled-oscillator operating directly on 144 MHz with a control voltage derived from an unusual form of phased-lock-loop n.b.f.m. detector in the single-conversion receiver. The detector, based on a TBA120 i.c., is arranged to provide high a.f. output on signals of about 3 kHz deviation at the 10.7 MHz i.f.

Another feature is a 25 -watt amplifier module with Philips BLY37 output transistor that exactly replaces the battery module when the equipment is operated in a car.

## Preparing for 1979

The various amateur groups who are engaged in drawing up plans and proposals for the ITU World Administrative Radio Conference in 1979 have so far come up with six main proposals: ! return to amateurs of the 1.8 MHz band (not available at present in many countries); elimination of "sharing" of the 3.5 MHz band; expansion of the 7 MHz band and elimınation of "sharing" broadcasting; expansion of the 14 MHz band and elimination of sharing
with fixed services (fixed services are presently permitted in the USSR in some parts of the band); expansion of the 21 MHz band by 100 kHz ; establishment of new amateur bands at around $10.1,18.1$ and 24.0 MHz .

While this list may seem unduly optimistic to amateurs who recall how in the past these World Conferences have progressively eaten into the original " 200 metres and down" allocation to amateurs, it is felt that the increasing use of communications satellites for commercial circuits may make such proposals not unrealistic. But as a start it would be extremely welcome if the intrusion of non-amateur stations into exclusive amateur allocations could be reduced, particularly broadcasting between $\overline{7} 000$ and 7100 kHz .

The Union of Swiss Short Wave Amateurs is expected to participate in the ITU's Telecom 75 exhibition at Geneva next October 2 to 8 and an international amateur conference is to be held there on October 4 to 5 .

## Using the London repeater

To assist amateurs using the new London $145 \mathrm{MHz}(145.175 / 145.775 \mathrm{MHz})$ repeater the UK FM Group (London) has published a detailed information sheet: "GB3LO without tears - a guide to the proper use of the repeater". This gives essential details of the operation of the 55 -second "time out" arrangement and the "break" facility between overs, both designed to prevent stations from monopolising the repeater for long periods; the excessive deviation inhibitor which chops signals that deviate by more than $\pm 6 \mathrm{kHz}$; and full details of the 1750 Hz tonebursts needed to gain access. The sheet is available from Richard Street, G3TJA, 3 White Ledges, Ealing, London W13 8JB (7p in stamps plus large stamped-addressed envelope, preferably 12 in long).
With the aerials about 750 ft above sea level on the BBC Crystal Palace mast the theoretical line of sight range of GB3LO is about 50 miles.

## Powers low and high

A group of British amateurs (G-QRP Club) interested in low power radio communication, preferably under 5 watts, now has a membership of over 60 and publishes a newsletter under the title Sprat. Details can' be obtained from Rev G. C. Dobbs, G3RJV, 61 Park Street, Cleethorpes, South Humberside Among recent suggestions made by club members are the improvement of short aerials for 1.8 and 3.5 MHz , modifications for the Heath HW7 low-power transceiver, aerial tuning units and r.f. meters. The club is supporting the American suggestion of encouraging QRP operation around certain spot frequencies: 3540, 7040 (Europe 7030), 14065, 21040 and 28040 $\mathrm{kHz}( \pm 5 \mathrm{kHz})$ for c.w. and 3640, 7140,

14260,21300 and 28600 kHz for phone.
At the other end of the power scale one notes the increasing number of broadcasting stations now using over a megawatt. For example, Radio Monte Carlo on 218 kHz now uses 1400 kW and the United States Information Agency is reported to be contemplating the construction of 2500 kW transmitters for "Voice of America".

## Across the Channel

French authorities have recently re-introduced permits for 405 -line and 625 -line amateur television transmissions between 434.5 and 440 MHz and 1250 and 1260 MHz . These permits are restricted to persons already holding normal amateur licences.

To mark the 50th anniversary of the formation of REF and IARU, French amateurs have been allowed to use the special prefix TK instead of $F$ during May. Among the events of the 50th anniversary meetings of REF in Paris on May 9 to 10 was a mark of homage to the French pioneer General Ferrie at the monument to him which is some 50 metres from the Eiffel Tower, where he established the first transmitter, and an address by General P. Revirieux, F80L, on technical developments in amateur transmission since 1925 ..

French amateurs F8DO, F1AVY and FICVJ have made contacts using lasers and infra-red light-emitting diodes over distances of about 1 km and have reported laser transmissions of about 9 km .

FAV22 radiates standard band-edge frequencies on Sunday mornings as follows: 3500 kHz (1000-1005 GMT); $3800 \mathrm{kHz} \quad(1010-1015) ; \quad 7000 \mathrm{kHz}$ (1020-1025); 7100 kHz (1030-1035); $14000 \mathrm{kHz} \quad(1040-1045) ; \quad 14350 \mathrm{kHz}$ (1050-1055).

## In brief

As a result of a clerical error two new amateurs, one in Reading, the other in East Anglia, were both issued with the callsign G8IOR which they used for several months (the Reading claimant is now re-mustered as G8IOJ) . . . The 1975 Convention of the British Amateur Radio Teleprinter Group is being held on Saturday, May 24, at the village hall, Meopham, near Gravesend, Kent (lectures this year start at 1.30 p.m.)... The Maidstone YMCA ARS Mobile Rally is being held on May 25 at the Y Sportscentre, Maidstone, Kent (details from A. S. Walter, G3WXL, 4 Oak Farm Gardens, Headcorn, Ashford, Kent) . . . The prefixes C6A to C6Z have been allotted by the ITU to the Bahamas...A special amateur radio station is expected to operate during the 1976 Summer Olympics from the Montreal, Canada, stadium . . A cross-band duplex r.t.t.y. contact is reported between Alan Hobbs, G8GOJ in South Croydon ( 144.6 MHz transmit) and G8IDZ in Edenbridge. Kent ( 432.88 MHz transmit).

PAT HAWKER, G3VA

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There are times, too, when - as a result of free-ranging, exploratory probing - they come up with a revolutionary instrument that was not o-iginally on the agenda at all. An example? The $X-Y$ Memory, a definitive solution to the irritating problem of clear oscilloscope display of very low frequency waveforms.

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# M: THE INNOVATORS 

## New Products

## Digital panel meter

Computing Techniques has announced what is claimed to be the first digital panel meter in the U.K. to provide the IEC-standard general-purpose bus interface. The meter, which can be connected directly to other instruments such as printers and computers, provides an accuracy to within $0.05 \%$ of reading $\pm 1$ digit. Computing Technigues Ltd, Brookers Road, Billingshurst, Sussex.
WW307 for further details

## Television tubes

Thorn has introduced the first in a new range of precision in-line colour tube assemblies. These tubes are marketed with the scanning coils and static convergence magnet assembly permanently fixed to the neck. Static and dynamic convergence, and purity adjustments are accurately set during manufacture, resulting in only minor adjustments by service engineers.


WW305

Thorn Colour Tubes Ltd, Mollison Avenue, Brimsdown, Enfield, Middx. WW305 for further details

## Wire-wrapping board

A new type of p.c.b.consists of a board with an etched copper pattern on both sides to provide a rail voltage and ground plane. The board has groups of discrete socket-pins or i.c. sockets, in the $14 / 16$ lead configuration, mounted on it which enables i.cs or header units containing discrete components to be plugged in.
Interconnexion on the pin side of the board can be made by wire wrapping. The boards are provided with rows of in/out pins for the interconnexion of complete boards. Vero Electronics Ltd, Industrial Estate, Chandler's Ford, Eastleigh, Hants.
WW312 for further details

## Helical filters

Polyplate helical-filters are constructed by electro-depositing a conductor on to a p.t.f.e. dielectric rod. Using these filters in local oscillator circuits, Q values of about 400 at 600 MHz are possible. Polyflon Resine, Via Mezzago, 20050 Sulbiate, Milan, Italy.
WW 318 for further details

## Digital integrator

The TS100A is a digital integrator and d.c. millivoltmeter having an input range from 1 mV to 300 V f.s.d. and switched integrator count rates of 30,3 or 0.3 c.p.s. The input level is displayed by a meter while the time integral is shown on a six-digit counter which can be switched to display fractional parts
of a count. Time Electronics Ltd, Botany Industrial Estate, Tonbridge, Kent. WW 316 for further details

## Calculators

Three models - the 100, 200 and 300 form the new Oxford range of mains/ battery calculators from Sinclair. The 100 and 200 are both four-function instruments, the latter having a percentage key and memory. The 300 is a scientific calculator. All the units are powered from a PP3 battery or a mains adaptor, and are priced at $£ 12.95, £ 19.95$ and $£ 29.92$ plus v.a.t. respectively. Sinclair Radionics Ltd, London Road, St. Ives, Huntingdon, Cambs PE174HJ. WW 306 for further details

## Resistors

A resistor set containing $2,725 \quad 1 / 4 \mathrm{~W}$ carbon film pieces in 170 values from $0.51 \Omega$ to $5.6 \mathrm{M} \Omega$ is available from EEP.

The quantity of resistors varies for each value so, theoretically, you run out of all the values at the same time. Energy Electronic Products Corp, 6060 Manchester Avenue, Los Angeles, California 90045, U.S.A.
WW 323 for further details

## Capacitors

ITT Components have introduced a range of metallized plastic capacitors using a polypropylene dielectric which gives a low-loss. This range has been designed for application where both pulse and r.m.s. current values are high, such as thyristor time-base circuits. ITT Components Group Europe, STC Ltd, Edinburgh Way, Harlow, Essex. WW313 for further details


WW316

## Wire stripper

The Scotchlok TH213 wire stripper will strip wires with conductor areas from 0.75 to $6 \mathrm{~mm}^{*}$. The tool has a pliers-type movement with a spring-loaded return action. 3 M UK Ltd, 380 Harrow Road, London W9 2HU.
WW 321 for further details

## Digital comparator

The model 1715 digital comparator has been designed for use with the model 1700 digital ohmmeter to provide simplified testing of resistances. The comparator has three panel l.e.d.s to indicate whether a resistance is below, within or above a selected range. Relay contact closures and d.t.1. outputs are available for operating peripheral equipment. Tranchant Electronics (UK) Ltd, Tranchant House, 100a High Street, Hampton, Middx.
WW301 for further details

## Spectrum analyzer

A microwave spectrum analyzer, model 4809 , which operates from 10 MHz to 40 GHz , has been announced by Sys-tron-Donner. The c.r.t. display can be standard or variable-persistence with frequency spans ranging from 10 kHz to 8 GHz and resolution bandwidths of 300 Hz to 1 MHz . The 4809 features an inbuilt digital frequency counter which displays frequency span and centre frequencies. Systron-Donner Ltd, St. Mary's Road, Leamington Spa, Warwicks.
WW303 for further details

## Microprocessor-'scope

Hewlett-Packard has combined a 275 MHz oscilloscope, a microprocessor and a $3 \frac{1}{2}$ digit l.e.d. display. This megalomaniac's dream will, say the makers, put an end to graticule counting, mental calculations and conventional 'scope errors. Basically, the instrument is a conventional 'scope in which a microprocessor keeps track of dial settings, computes time intervals and voltage levels to give a digital reading of a measurement in seconds, Hz , volts or percent. The microprocessor will also (to let you know it's working for a living) signal if an erroneous setting is made. HewlettPackard, King Street Lane, Winnersh, Wokingham, RGl1 5AR.
WW 319 for further details

## Re-usable circuit board

A re-usable circuit board with a 0.1 in matrix of holes uses pre-tinned solder pins, which are pushed into the matrix in the desired format. Components are then soldered to the pins which may be removed to produce another circuit. A kit comprises five $43 / 4 \times 4$ in boards and 500 pins, and costs $£ 4$ plus v.a.t. Lektrokit Ltd, 3 Trafford Road, Reading, Berks RGl 8JR.
WW302 for further details

## Gunn power supply

The type 703B power supply is a stable ripple-free voltage source suitable for energizing a variety of Gunn-diode oscillators. Output range covers 3 to 15 V at up to 2 A , the values being


WW303
indicated on a front panel meter. Current limiting can be set from 100 mA to 3 A and when the limit is reached the supply changes from the constant-voltage mode to constant-current working. A square-wave modulator circuit is included which is suitable for driving p.i.n. diode modulators. Microtest Ltd, 18 Normandy Way, Bodmin, Cornwall. WW 322 for further details

## Flat heat pipes

The SK133P and SK166P will accept two T03 or T066 packages respectively. The heat pipes are hollow and flat so the component is bolted through the pipe for maximum heat transfer. Thermal resistance of the pipes is $1.59^{\circ} \mathrm{C} / \mathrm{W}$ at 50 W reducing to $0.43^{\circ} \mathrm{C} / \mathrm{W}$ at 150 W when forced cooled. Solek Ltd, 16 Hollybush Lane, Sevenoaks, Kent.
WW309 for further details

## Reference-voltage tubes

The new $Z D$ range of cold-cathode voltage reference and regulator tubes from Hivac is available with voltages from 82 to 139 V . Several versions can be supplied, giving tolerances on the reference voltage from $\pm 1 \%$ to $\pm 20 \%$. Temperature coefficients range from $2 \mathrm{mV} /{ }^{\circ} \mathrm{C}$. Hivac Ltd, Asheridge Road, Chesham, Bucks.
WW308 for further details

## Sweep oscillator

The 6700 A sweep oscillator has a frequency range from 400 MHz to 18 GHz . An optional facility provides


WW309


WW308
remote digital programming via a 12 line b.c.d. input.
Plug-in YIG-tuned oscillators are used which can be supplied with a manual $10 \mathrm{~dB} /$ step attenuator or, for the remote version, a 0 to 70 dB binary step attenuator. Marconi Instruments Ltd, Sanders Division, Gunnels Wood Road, Stevenage, Herts.
WW 315 for further details

## Power amplifier

The Crown DC300A has now acquired a big brother -- the M600. This new amplifier, while retaining a high performance, will deliver 600 W into an eight ohm load or I KW into four ohms. Built-in cooling and protection circuitry allow continuous high power levels to be maintained. Two M600's can be connected together to deliver 2 kW into eight ohms. Macinnes Laboratories Ltd, Carlton Park Industrial Estate, Saxmundham, Suffolk.
WW304 for further details

## Kits

Recent additions to the Heathkit range of instruments are a single-trace 10 MHz oscilloscope and a digital multimeter. The'scope offers a vertical sensitivity of $10 \mathrm{mV} / \mathrm{cm}$, two input channels, and a triggered sweep. The multimeter is a portable unit including rechargeable cells and charging circuit. The meter, which has 26 ranges, will measure direct and alternating voltages from $100 \mu \mathrm{~V}$ to 1000 V and 750 V respectively, direct and alternating currents from 100 nA to 1000 mA , and resistances up to $1000 \mathrm{k} \Omega$. A $100 \%$ overrange capability allows measurement up to 1.999 on all ranges except 1000 V d.c. and 750 V a.c. Heathkit (Gloucester) Ltd, Gloucester GL2 6EE. WW3 14 for further details

## Dust caps

Lemo are now supplying sprung dustcaps for their range of panel sockets. A moulded disc which has a rubber washer provides a dust-proof seal whenever the plug is withdrawn. Lemo (UK) L.td, 6 South Street, Worthing, Sussex BNll 3AE.
WW3 10 for further details

## Cassette winder

A useful accessory for audiophiles is the Bib cassette-tape winder. The gadget is simply located into the spigot holes of the cassette and a handle is turned which, through appropriate gearing, rewinds the tape. A C90 cassette can be wound in about 60 seconds, which is faster than many cassette recorders. The unit is priced at $£ 1.34$ plus v.a.t. and is available from Bib Accessories, P.O. Box 78, Hemel Hempstead, Herts. WW 320 for further details


WW315


WW304


## WW314



WW310


I've always felt sorry for William McGonagall, poet and tragedian, whose poetic gems have achieved immortality for all the wrong reasons. In short, as Punch has truly said, McGonagall was the greatest Bad Verse writer of his age

Now he has serious competition, for a distant relative, Vector McGonagall, has submitted the following. As you will see, it has the same sublime disregard of scansion that was typical of our illustrious forebear:

## ODE TO COLOUR TELEVISION

Beautiful colour television set so fair Standing so blank in the corner there Awaiting the installation engineer
In the Dun Cow quaffing his lunchtime beer
While the rigger up on the roof does bellow
"Dear me, what a nuisance!" as the clumsy fellow
Drives a nail through his thumb, so sad to be seen
In fixing the antenna on our rooftop green.
Beautiful colour set with your twenty-six inch screen
By far the biggest our road has yet seen
No more from the Joneses shall we have to scrounge a view
Of Trooping the Colour on their mere twenty-two
We can now tell the world fearlessly and without dismay
That Messrs McTavish and Goldstein are installing it today
With a cracking down-payment and a lifetime of rental
And three hundred green stamps as a prized incidental.

Beautiful colour set with your twenty-six inch screen.
And your cathode ray tube so fine to be seen With its shadow-mask invented by Dr Goldsmith some experts do say
With its millions of holes which serve to display
The Rt. Hon. Harold Wilson our Prime Minister so true
In appropriate shades of red and blue
Whene'er he has something of import to state
Or even on nothing he'll profoundly orate.
Meanwhile up on the roof the Storm Fiend doth bray
And the rigger zooms down the unorthodox way

The Dun Cow closes its doors with a clang And the engineer on our front door he doth bang
With unsteady fingers he adjusts all the knobs
While the screen starts to glow with indeterminate blobs
Of colour, so grand and so fine to be seen
On our wonderful, marvellous twenty-six inch screen.

For a toast now to Nipkow, Rosing and Baird let us call,
Campbell Swinton and Zworykin and Shoenberg et al
NTSC, SECAM and PAL who worked like the deuce
To display Fanny Cradock in glorious puce
Our skies may be green and our grass fiery red
With fringing and rainbows around every head
And dot-structures crawling all over the place
Like ants wandering aimless on Dimbleby's face
No matter! The Joneses with envy are green At our opulent set with its twenty-six inch screen.

## TUPPENCE COLOURED

Traditionally, what the United States does today, Britain, for better or for worse, gets around to doing four or five years hence. As a case in point you may or may not know that for some time past it has been a common custom in American zoos to provide the gorillas and chimpanzees with colour television sets; the objective, as in human circles, is to ameliorate to some extent the sheer boredom of civilized livìng

Now comes news that at least three British zoos have done the same. For this piece of information I'm indebted to (appropriately enough) the Spectrum column in The Sunday Times. The apes, I'm told, have definite preferences. Michael Parkinson and Russell Harty leave their simian viewers cold; no - it's football, horse opera with plenty of redskins biting the dust, all-in wrestling and Kojak that really gets the old adrenalin pulsating around in the cages.

I don't know whether you agree, but to me that's really interesting for these are precisely the items which are accorded top ratings by the apes' human counterparts on both sides of the Atlantic. It points strongly toward a parity in intelligence between the two factions; indeed, it seems that the apes don't dig girl singers or blue movies, which might, appear to give them something of an edge in the matter of I.Q. In view of this, the question which every thinking person will ask himself is - are we being fair to the gorillas in our midst? Shouldn't they, for instance, be accorded the right to vote? This, is no idle academic question. It's a matter which the Liberal Party in particular would do well to ponder

You, sir, and you, madam, no doubt suppose that the gorilla population of Britain is insignificant and so it is in comparison with that of the United

States, where the whole thing started. But I'm now in a position to reveal exclusively that for some years past, gorilla-smuggling across' the Channel has been rife and on a scale that makes the Pakistani forays seem chickfeed. And if this news has triggered the raised eyebrow, then stand by to hoist the other one also, for a startling announcement is imminent. Here it comes. I can state unequivocably that the sinister, secret organization behind this illegal mass-immigration is not the Mafia but our own electronics industry, no less.

Naturally, you require evidence of this, and evidence you shall have. As every retail service department in this country, and indeed, every buyer, will confirm - in any given piece of electronic apparatus which arrives from the manufacturers, half the main components will be found to be falling off the chassis while the other half are immovably clamped (these, in the very nature of things, are the ones which turn out to be faulty and need replacement). You may have wondered why, and I can now tell you. The manufacturers are using trained anthropoids on their assembly lines. The bits which are falling off represent the immature efforts of young apes; tyros who haven't yet quite got the hang of tightening self-tapping screws. The ones you can't shift at all are those tightened by adults in the prime of lusty gorillahood.

This secret work-force is housed in spartan quarters within factory precincts and, at the cost of a few colour sets, a handful of bananas and the defoliation of Epping Forest, is Britain's answer to the Hong-Kong menace. So successful has this enterprise become that disturbing new moves seem probable; no less a project than to give the anthropoids the status of British citizenship with full integration into our society as the eventual target. Incredible as this may seem, proof is not lacking. The BBC and IBA are already in cahoots with the electronics manufacturers; the former's surfeit of animal programmes and the latter's chimpanzee-orientated advertisements are not, as you have supposed, primarily directed at the human viewership. No - their main purpose, like the Pakistani programmes, is to keep our simian immigrants in touch with the dear old homeland.

Needless to add, the concept of gorilla-labour is no longer a monopoly of the electronics industry. Car users are also experiencing the symptoms and the expression "the engine's missing" has taken on a new connotation. Neither is the practice confined to industry. I can personally attest to the employment of gorillas as bouncers in many Soho strip-clubs and discos, a matter about which I feel particularly sore. It was clearly my patriotic duty to acquaint the British Public with the sinister facts, even though my body may be discovered up some dark alley riddled with Impatt diodes. FOR P.A., STUDIO AND PROFESSIONAL AUDIO EQUIPMENT


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| AC194k | 0.32 | 日C157 | 0.15 | 80×32 | 2.55 |  | 0.30 | MPSA05 | 0.47 | ${ }^{2} 1307$ | 0.22 | 2N4286 | 0.19 | Bax Bx72 | INTEGRATED | CIRCUITS |  |  |
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| AD 142 | 0.52 | BC1 $1678^{\text {c }}$ | 0.15 | 8F115 | 0.20 | BFx86 | 0.26 | MPSU | ${ }^{0.76}$ |  | 0．45 | ${ }^{\text {2N4291 }}$ | － 0.18 | $\begin{array}{\|cc\|}\text { Br100 } & 0.15 \\ \text { Vr1 }\end{array}$ | $\begin{array}{ll}\text { Ca3046 } & 0.70 \\ \text { CA3065 } & 1.90 \\ \end{array}$ |  | 11 DII． 8 |  |
| AD 143 AD 149 | 0.51 0.48 |  | 0.13 0.13 | ${ }^{8 F 1} 178$ | 0．45 |  | 0.28 0.24 0.28 | MPSU55 | ${ }^{1.26}$ | 2N18 | 0.48 | 2N4871 | 0.24 0.30 |  | MC 1307 P 1.19 | a |  |  |
| ${ }_{\text {AD }} 161$ | 0.48 | ${ }_{\text {RCC }}$ | 0．15 | ${ }_{\text {8F } 121}^{8 F 123}$ | ${ }_{0}^{0.25}$ | BFY ${ }^{\text {BFY } 40}$ | 0.53 0.40 | OC26 OC 28 O－ | ${ }_{0}^{0.38}$ |  | 0.51 0.36 | 2N4902 | 1.30 1.05 |  | MC1310P 2.94 | ${ }^{4.18}$ | £105 | 500 |
|  | 0.48 0.25 | ${ }_{\text {BC1714 }}^{\text {BC17 }}$ | O．15 | ${ }_{\text {BF }}^{8 \times 123}$ | 0.28 0.25 | 8F | （0．40 0 | OC28 | 0.65 0.59 | 2N2218 | 0.36 0.60 | 2N5960 | 0.32 |  | 1.01 | 18 | 5 Timers |  |
| AF115 | 0.25 | ${ }^{\text {BCI } 173}$ | 0.20 0.22 | ${ }^{8 F 127}$ | 0.30 0.25 |  | 0 | ${ }^{\text {OC36 }}$ | 0.64 |  |  | ${ }^{\text {2N5061 }}$ | 0．35 | E8164 0.55 | MC1 133PP 0.76 <br> $M C 1351 P$ <br> 185 | TAA 700 4.18 <br> TAAB 40 2.02 | £55 | 00 |
| Aft AF | 0.25 0.25 | ${ }_{\text {BCI }}{ }_{\text {BC7 }}$ | 0 | ${ }_{\text {BF }}{ }^{859}$ | 0.27 | BFY52 | 0.23 | ${ }_{\text {OC4a }}$ | 0.25 | 2 N 2 | 0.50 | 2N5087 | 0.32 | $\left\lvert\, \begin{array}{\|cc\|}\text { Er176 } \\ \text { 8179 }\end{array}\right.$ | MC1352P 0.82 | tals6ia | £205 | 500 |
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| AF124 | 0.25 | ${ }_{\text {BC179 }}$ | 0.20 | ${ }_{\text {BF／} / 62}$ | 0.45 | BFY72 | 0.31 | OC71 | 0.32 | 2N2484 | 0.41 | 2N5298 | 0.58 |  | MC1496L 0.87 | TBA120S |  |  |
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| 2N3703 | 0.13 | AC187K | 0.35 | 8CY70 | 0.17 | MJE340 | 0.48 | OA47 | 0.06 |
| 2N3704 | 0.15 | AC 188K | 0.40 | BCY7 | 0.22 | MJE370 | 0.65 | OA81 | 0.18 |
| 2N3706 | 0.15 | AD143 | 0.68 | 8 CY 72 | 0.15 | MJE371 | 0.75 | 0490 | 0.06 |
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| 2N3773 | 2.65 | AF 115 | 0.35 | BD132 | 0.50 | MPB113 | 0.47 | 40669. | 1.0 |
| 2N3789 | 2.06 | AF116 | 0.35 | 80135 | 0.43 | MPF 102 | 0.39 | T/C44 | 0.29 |
| 2N3819 | 0.37 | AF:17 | 0.35 | 80136 | 0.47 | MPSAO5 | 0.25 | C1060 | 0.85 |
| 2N3820 | 0.64 | AF 118 | 0.35 | 8D137 | 0.55 | MPPSA06 | 0.31 | RP12 | . 6 |
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Hi-Fi News Linsley-Hood 75W/Channel Amplifier
Mk III Version (modifications as per Hi.fi News April 1974)

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## FINAL ACCEPTANCE ENGINEERS SALARIES UP T0 $£ 3,000$ CAMBRIDGE

Our client, Cambridge Scientific Instruments Ltd, is a world leader in the manufacture of high resolution scanning electron microscopes. They have an urgent requirement for a number of Electronics Test Engineers who will initially work on fault finding on modules. After a short induction period they will move on to complete systems. Further career development could involve a move into $R / D$ or Sales. These vacancies have come about because of internal promotions to other areas - it is the

Company's practise to develop staff into positions of more responsibility.
For these jobs experience is more important than paper qualifications, although an HNC could be useful. Candidates should have a good basic knowledge of I.C.'s and be familiar with modern Test Equipment.
If you would like to work with a Company you can grow with, write or 'phone, quoting Ref CSI/WW to

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Cambridge Recruitment Consultants,
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## ThePolytechnic

of NorthLondon

## Laboratory Technician

## Grade 4

Applications are invited for the appointment of an experienced Technician in the Department of Electronics and Communications Engineering.
The work is interesting and involves the operation and maintenance of high grade test equipment in an Audio Engineering Laboratory, which has its own Anechoic Chamber participation in Research and Development, and the general responsibility for the efficient running of the day-to-day requirements of the laboratory for students' experiments and project work. Normal background experience: at least 7 years (including training period); normal education level, with ONC or OND in appropriate subjects and/or specialist qualifications in the field of Audio/Acoustics.
Salary Scale: £2247-£2628 per annum plus £411 London Allowance.
Application forms obtainable from the Establishment Officer, The Polytechnic of North London, Holloway Road, N7 8DB.
Further details obtainable from Mr . S. A. Elliott (01-607 6767 extn. 289).

## RADIO TECHNICIANS

Are you a Radio Technician with a City and Guilds Intermediate Telecommunications Certificate or equivalent, plus 1 year's practical workshop experience? If so, then why not join the Home Office. There are vacancies in Central London (near Waterloo Station) and the Home Office Laboratory at Canons Park, Stanmore.

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is $£ 1695$ at 19 , rising to $£ 2575$ *plus a cost of living supplement which is at present $£ 19.14$ a month. In addition, London Weighting Allow ances of $£ 410$ a year in Central London and £260 at Stanmore are payable.
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## A Secure Future

with a non-contributory pension scheme. prospects of promotion and a generous leave allowance. Five day week of 41 hours

## Interested?

Then telephone or write for an application form to Mr J. J. Willis, Directorate of Radio Technology, Room 514, Waterloo Bridge House, Waterloo Road, LONDON SE1 8UA Telephone 01-2753006.

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Engineers! If you are interested in electronics, data transmission, digital systems, this could be of great importance to you.

How does Jeoff Samson, STC's Director, Switching, approach the problems of techno logical change? How does he see the mix between pure research and the practicalities of the telecommunications business? How far can an engineer be encouraged to experiment while working with current technologies?

STC - one of the world's leading companies in telecommunications and a pioneer of the new British Telephone Switching System, TXE4 -- is looking for professional and technical engineers at all levels of experience for Advanced Systems Development, Application Engineering, Systems Design and Integration, and Circuit and Logic Design.

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To answer some of the questions you might be expected to ask about us, Ken Corfield, STC's Managing Director, and three of his colleagues Jeoff Samson, Jock Marsh, Neville Cooper - have chosen to make a record, each explaining the thinking behind the tasks and challenges of his own specific area of responsibility, and outlining the opportunities within STC. In this way, you can build up a picture of the company as a whole: its attitudes, approach to business, present and long-term views.

You can have a free copy of this record now. Send for it. Play it. Listen to it. Consider whether you like the sound of us. It could mean a lot to you. your future -and ours!


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The work is just as
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Starting pay for a man of 25 or over is $£ 2,270$, plus cost of living allowance with further

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Do you have PMG I, PMG II. MPT 2 years operating experience?

Possession of one of these qualifies you for consideration for a Radio Officer post with composite signals organisation.

On satisfactory completion of a 7 -month specialist training course, successful applicants are paid on a scale rising to $£ 3,242$. pa: commencing salary according to age-25 years and over $£ 2.383 \mathrm{pa}$. During training salary also by age, 25 and over $£ 1.724$ pa with free accommodation.

The future holds good opportunities for established status, service overseas and promotion.

Training courses commence at intervals throughout the year. Earliest possible application advised.

Applications only from British-born UK residents up to 35 years of age ( 40 years if exceptionally well qualified) will be considered.

Full details from:

## Recruitment Officer,

Government Communications Headquarters, Room A/1105, Priors Road, Oakley, Cheltenham, Glos GL52 5AJ
Telephone Cheltenham 21491 Ext 2270


## UNIVERSITY OF SURREY ELECTRONIC ENGINEER

Applications are invited for the above position in the Electronic Workshop of the Psychics Department. The person appointed will work, together with two other members of the technical staff, under the general direction of a Chief Technician.
Applicants should have a good electronics background, a sound theoretical knowledge and should have experience in the development and construction of computer interfacing and be familiar with nucleonic instrumentation Qualification: HNC or equivalent. Salary scale: $£ 2,844-£ 3,450$.
For further details and application forms please apply to the Staff Officer, University of Surrey, Guildford, Surrey GU2 5XH or Tel: Guildford 71281, Ext. 452.

THE ROYAL NATIONAL THROAT, NOSE \& EAR HOSPITAL
Gray's Inn Road, London WC1X 8DA

## PHYSICIST <br> (BASIC GRADE)

Applications are invited for a newly established post of Physicist (Basic Grade) for work in the field of hearing disorders and the applications of hearing aids. Suitable candidates will have a degree in Physics and should have experience in electronics and acoustics. He /she will be based in a new elec-tronic-acoustics laboratory and in the Hearing Aid Centre.
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Applications giving details and names of two referees to Senior Administrative Assistant.

Kensington and Chelsea and Westminster Area Health Authority

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Applications are invited for the post of Medical Physics Technician Grade IV at the Middlesex Hospital. Salary according to Whitley Council 'B' Scales. Duttes will involve a wide variety of work in Physiological measurement including work in the Department of Cardiolog.y Day work in the Department of release faclities for study at approved release facilites for st
Colleges can be arranged

Applications, with fu'l details of career to date and quoting two referees, should be sent to Establishment Officer. The Middlesex Hospital. London. W1N 8AA. Closing date for applications 2nd June. 1975

## Electronics Development Engineersdevelop in Cambridge

Develop your career in an expanding industry where increasing worldwide demand for our radio-communications equipment provides a career path limited only by personal ability. Develop your quality of living in an area that has all you need - a university city with plenty of amenities, attractive reasonably-priced housing, enjoyable countryside and only 50 miles from London and the coast.

Engineers will be involved in design/development on portable, mobile, fixed station and digital equipment. BSc is preferred, but lower qualifications with sufficient RF experience and interest may be acceptable. Age range is $21-30$ and you will preferably have up to 5 years relevant experience of radio-communication equipment. It's a pleasant, small-team working atmosphere, using the very latest $R F$ technology.

Generous assistance with relocation expenses is just one part of an attractive salary and benefits package. For more information phone or write to Richard Turner at:


## ELECTROSONIC LTD.

## S.E. LONDON

## MANAGER ELECTRONIC TEST DEPARTMENT

Electrosonic Ltd. are seeking a candidate, having wide experience in a production test shop. Technical ability in analogue and digital circuitry is essential together with experience of supervising the work of others and a commercial awareness.

Duties will include the organisation and day-to-day running of the test shop with technical assistance, training of junior engineers, the introduction and programming of automatic test equipment and supervision of quality control.

The Company is leader in the rapidly expanding fields of lighting control, audio and audio visual systems and offers a wide range of interesting work in an attractive environment and excellent conditions of employment

Apply: Personnel Director, Electrosonic Ltd., 815 Greenwich Road, Charlton, SE7 8LT. Tel: 01-855 1101

## APPOINTMENTS

## Electronics Test Engineers: career openings that affect all sorts of people...


. you most of all, naturally. Mainly because, by joining the world's largest exporter of radio-telephone equipment you will inevitably open up for yourself career advantages that very few companies can provide. Pye Telecom is growing at an ever-increasing rate - and the potential for its products has as yet been only fractionally utilised.
But the work you do will also be vital to an incredible number of others. Very frequently, life itself depends on the efficiency of the UHF and VHF equipment you'll be working on. Police, firemen and ambulance staff are a small sample of the extensive range of users. Which explains the exacting specifications of the test procedures in operation - and why previous fault-finding and testing experience is an essential requirement. If it relates to communications equipment, so much the better, but this is not absolutely essential. More important is practical proficiency, which may well have been gained in the armed forces. Find out more right now by phoning or writing to Mrs Audrey Darkin at:

## Pye Telecommunications Ltd

Cambridge Works. Elizabeth Way. Cambridge CB4 1 DW Tel: Cambridge 58985


Opportunities in the ELECTRONICS FIELD
Men with analogue or digital qualifications/ experience seeking higher paid posts in: TEST - SERVICE - DESIGN - SALES Phone Mike Gernat. Ref. WW.

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for District Medical Physics Department. Salary scale from £1773 p.a. rising by annual increments to £2463 plus £312 London Weighting Allowance.
Further details can be obtained from Chief Technical Officer - 01-644 4343, Ext. 375.
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UNIVERSITY OF LEEDS DEPARTMENT OF PHYSIOLOGY cardiovascular unit
Applications are invited for the post of

## EXPERIMENTAL OFFICER <br> mes

A degree is required, Responsibilities include PDP12 and PDP8 computers, electronic equipment in three physiological laboratories and three hospital catheter laboratories, and the supervision of four electronics technicians. Preliminary enquiries may be made to the Director of the Cardiovascular Unit, Department of Physiology. The University, Leeds LS
9 JT . Form
Forms of application and further particulars may be obtained from the Registrar. The University of Leeds, Leeds LS2 9 JT quoting reference number $105 / 1 / \mathrm{Cl}$, to whom applications
should be returned as soon as possible.

## RADIO TECHNICIAN FOR CENTRAL AMERICA

Needed to work in Guatemala with the Radio Schools Movement, training a team of Guatemalans in the maintenance and repair of station equipment. A British Volunteer Programme post.
Information
Paddy Coulter, Overseas Volunteers/C11R 41 Holland Park, London W. 11

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For our London based Service Department (Near Marylebone Station) to maintain a range of Professional audio equipment (Nagra, Sennheiser. etc.)
An attractive salary and four weeks' holiday will be offered to the right man. Interviews to be carried out in London.

Please apply in writing marked confidential to:

The Managing Director<br>Hayden Laboratories Limited<br>Hayden House<br>17 Chesham Road<br>Amersham BUCKS.

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## O TO TOLOTOROIOLOL Design/ Development Engineers

## Is your future in Cambridge?

To a Design/Development Engineer, Cambridge means Pye. And Pye means a better future. Labgear is one of the Pye Group and manufactures cable TV systems and TV service equipment. We have a vacancy in a team engaged in the design and development of M.A.T.V. and C.A.T.V. distribution equipment, associated test gear and filter networks ranging from single channel band width to wide band applications covering from $40-860 \mathrm{mHz}$. Candidates will have at least 2 years' experience in high frequency circuit techniques, and keen to develop with the job. Education to HNC (Electronics) or equivalent standard is preferred.
We offer an attractive starting salary, which is negotiable, assistance with relocation expenses, and considerable company benefits.
Please write or telephone for an appointment to:
Mr. C. G. Houghton Personnel Manager

## $(1) / 2$ Labgear Ltd

Abbey Walk Cambridge
CB1 2RQ Tel: Cambridge 66521
(4683)
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## ERA <br> HF COMMUNICATIONS PROBLEMS

Within the Materials Sciences Division of ERA Ltd., a leading contract research organisation, work has been proceeding for a number of years on non-linear problems associated with materials used in radio communications systems.

We need an experienced person to undertake a major role in this research, which will be mainly of an experimental nature with scope for theoretical development, concentrating on the HF band. As this work has not yet commenced, the person appointed will be able to influence its direction from an early stage. Liaison with clients, designing, building and operating laboratory equipment will also be involved.

Age and paper qualifications are not so important as relevant experience (from radio "ham" upwards) and this will be reflected in the salary offered.

The person appointed will be encouraged to submit ideas on the direction of future research.

ERA laboratories and offices are located in pleasant surroundings and are within easy reach of London. There is a contributory Pension Fund and entitlement to relocation expenses, if relevant. Amenities include full canteen facilities and an active Sports and Social Club.

Please submit curriculum vitae to, or ask for Application Form from, Miss E. Cox, Personnel Officer, Electrical Research Association Ltd., Cleeve Road, Leatherhead, Surrey KT22 7SA. Leatherhead 74151.

# PRODUCTION MANAGER 

for small quartz crystal manufacturing plant
in

## NEW ZEALAND

An opportunity exists for a Production Manager familiar with all aspects of quartz crystal manufacturing for the communications market. Past experience should encompass grinding, vacuum plating and finishing to frequency. The company, Hatfield Crystals Ltd., has recently entered the field of quartz crystal filter manufacture thus, although not an essential, it would be useful if the applicant has knowledge of quartz crystal design, particularly monolithic crystal filters in the 10.7 MHz band.
The successful applicant must be prepared to reside permanently in New Zealand and will be sponsored through the Migration Department of the New Zealand High Commission. The company is located at Napier, North Island, in a temperate climate not unlike the South of France. An attractive salary together with the usual fringe benefits will be offered.

Applicants to write in the first instance to:
The Managing Director
HATFIELD INSTRUMENTS LTD.
Burrington Way
Plymouth, PL5 3LZ
Devon

## Electronics

## Technicians

career opportunities in Yorkshire

Holset Engineering is the world's largest manufacturer and technical leader in the field of sophisticated original equipment for the diesel engine industry and other automotive applications. We employ over 1,600 people and occupy modern, well-equipped premises close to the centre of Huddersfield.

Opportunities exist for experienced electronics/instrument technicians to work in our development department. You should be experienced in the operation and maintenance of electronic and electro-mechanical measuring devices. A technical qualification would be an advantage.

An attractive salary, excellent working conditions, company pension and free life insurance schemes, plus 32 days holiday per annum will be provided. We will also pay removal expenses to the West Riding, which abounds in reasonably priced housing, pleasant countryside and excellent civil, social, educational and recreational facilities.

Please write or telephone for an application form to: P. G. Phipps, Personnel Development Manager

Holset Engineering Co. Ltd., PO Box A9, Turnbridge, Huddersfield, HD1 6RD.

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Fully experienced broadcasting engineers are needed to help the growth of Pye TVT as a leading international designer and nanufacturer of TV broadcasting systems and equipment.
The applicants appointed as Project Engineers (Commercial) will closely liaise with all relevant departments in defining and design of Studio, Outside Broadcast and sometimes radio schemes to meet customers' specific requirements or Transmitters. They will be responsible for the preparation of tenders and will assist in their.negotiation. which will involve some travel overseas. They should be qualified to at least HNC level and fully experienced in either design, installation or operation of TV Studio and / or Outside Broadcast vehicles, or Transmitters.

The appointments are based in Cambridge, and relocation expenses will be paid where applicable. There is a good starting salary, with a pension and other company benefits.
Please apply, with brief details of experience, to:
Mrs. J. A. Macnab, Personnel Manager,

## DEVON AREA HEALTH AUTHORITY

 (PLYMOUTH HEALTH DISTRICT)
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Medical Physics Department, Plymouth General Hospital, Freedom Fields

## ELECTRONICS TECHNICIAN

required for further expansion of the electronics service. The person appointed will join a small team in a well-equipped laboratory. He will be responsible to a graduate electronics engineer for maintenance of a wide range of patient-orientated electronic equipment. Development of special-purpose systems is undertaken, and safety and purchase decisions are made on new equipment. Minimum qualifications: ONC or HNC. Some travel in S. Devon and Cornwall necessitates a current driving licence. The appointment will be in either of the following grades depending on experience:-

Medical Physics Technician III
(£2,190-£2.817
Medical Physics Technician IV

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(£ 1,773-£ 2,463)
$$

Further details of the work may be obtained by telephoning Mr. L. R. Jenkin, Plymouth 68080, ext. 369. Application 'forms are available from the Sector Administrator, North Friary House, Greenbank Terrace, Plymouth PL4 8QQ.

## ELECTRONICS DEVELOPMENT ENGINEER

A new opening has been created in the Ealing area for a highly skilled Electronics Engineer to join a new team within a newly created small research and development laboratory within a new small production and prototype unit.

The Engineer required will have strong innovative abilities as well as sound modern technical skills to design. develop and prove advanced circuitry. He will work with two highly skilled industrial Designers and other support skills to bring an idea through to a full production item.

While the area of electronic interest ranges over all aspects of advanced security devices, the prime ability of the man required will be in the RF field. Transmitters. receivers, scanners, RF detection systems and associated audio

The interests of the C.D.I. group of companies covers military, paramilitary electronics: police support electronics; technical intelligence retrieval devices and systems; pulse induction metal detectors; night vision systems and body armour.

The group is relatively new having been formed in June 1972 and to date has concentrated on building a marketing capability to support its already existing strong innovative abilities. It is now filling in the centre sections thereby creating a very good opportunity for a young man of outstanding ability to grow with the group. Profit sharing, health and pension schemes are operated

Please write to the Managing Director giving complete and thorough details of your qualifications in relation to our needs and your expected salary requirements. All replies will be held in strict confidence.

## FREELANCE CONTRACT ELECTRONIC DESIGN AND DEVELOPMENT ENGINEERS

In addition to the staff Development Engineer required we are also seeking very high calibre Design and Development Engineers to work on specific projects on a freelance contract basis.
We are also interested in purchasing outright or on a royalty basis fully developed devices which fall within our armas of interest.
We are open to discuss sound ideas which we can develop. manufacture and market or any combination which makes sound commercial sense.
If any of this interests you then please write to the Managing Director clearly stating what you have to offer.

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Technical Security Ltd, Pulse Induction Ltd, Night Vision Systems Ltd, Body Armour Ltd.

## SITUATIONS VACANT

HI-FI AUDIO ENGINEERS. We require experienced Junior and Seniors and will pay top rates to get them. Tell us about your abilities. 01-437 4607.

MEDICAL RESEARCH COUNCIL CYCLOTRON UNIT, requires an Electronics Technician to work in a small igroup concerned with the construction, development and servicing of solid state equipment used in the biological sections of the Unit. ONC or equivalent is a minimum requirement and relevant practical experience an advantage. Salary, according to age and experience, in the range $£ 2,214-£ 3,375$ particulars to The 'Director, MRC Cyclotron particulars to The Drector, Mrc cyclotron London W12 oHS.

UNIVERSITY OF LEEDS. Electronics Technician
UNIVERSITY OF LEEDS. Electronics Technician 1 Grade 3 required in the department of Physiology. The person appointed would be responsible, under the head of the department the construction, modification and maintenance of electronic equipment associated with research and teaching of biological studies. Must search and teaching of biological studies. Must tions, circuit diagrams, sketches and manuals. Applicants should hold ONC or equivalent qualifications in relevant subjects. Salary is in the range of $£ 2,013$ - $£ 2,343$ according to qualifications and experience. Applications stating age, qualifications and full experience, logether with the names and addresses of two referees should be addressed to Mr. E. French, Repartmental Superintendent Department of Physiology, Medical Multipurpose Building. Mount Preston Street, Leeds LS. 2

ELECTRONICS TECHNICIAN required in Department of Psychology. University of Reading Should have or be completing final $C$ \& $G$ in Electronics Servicing or equivalent. Salary in scale E 2439 -f2895 p.a. (Grade 5). Apply with names of 2 referees and full details, quoting Ref. T.ZZ.23A, to Assistant Bursar (Personnel), UGiversity of Reading, Whiteknights, Reading

RADIO OP/TECH, 8 years marine experience, requires demanding shore post outside UK. Coms net/point to point experience. Weldon, 1 Fendon Road, Cambridge. (4707


## Telecommunications Technicians

London Transport's technology is constantly developing to meet ever increasing demands. - especially in the vital area of telecommunications.
The maintenance of existing telephone switching and transmission equipment must therefore be carried out to the highest standards. We are accordingly looking for men with a good knowledge of telecommunications to assume responsibility for maintaining, testing and fault finding on -Automatic Telephone Exchanges and associated equipment (including electronic exchange intercom. systems) as well as PCM and Carrier Transmission Systems. The work involves shift duties.
You should have a sound knowledge and experience of one of these job categories, preferably with City and Guilds Certificates (or equivalent) in telecommunications subjects. The basic rate of pay, including bonus, is $£ 54$ for a 5 day ( 40 hour) week. Additional payments are made for overtime, night work and rostered Saturday and Sunday duties.
Weekly earnings average $£ 76$ which include payment for rostered overtime at weekends, London Weighting and the current threshold payments.
In addition, you will enjoy valuable FREE TRAVEL on London Transport bus and train services at all times with special reductions on British Rail. There are also special concessions for your wife and family on London Transport trains and British Rail.
A good pension fund and sick pay arrangements are provided. Please telephone Mr Crowder on 01-748 9564 or apply in writing to:- London Transport (Ref: ATL),
ChiefSignal Engineer's Dept,270Bolio Lane, A cton, London W3.

## © LONDON TRANSPORT

## NEW HEBRIDES <br> SENIOR RADIO TECHNICIAN <br> (TWO POSTS)

* Tour 2 years
* Gratuity $25 \%$ of basic salary
* Free Family passages
* Furnished quarters at reasonable rental
* Children's education allowances and holiday visit passages
* Appointment grant up to $£ 300$ payable
* Interest free car loan of £600
* Outfit allowance
* No income tax payable in the New Hebrides at present

Required by the Condominium Radio Department to maintain transmitting and receiving equipment for postal services, local and overseas shipping, aircraft and the broadcasting studio, both that housed in the Radio Station and equipment at outstations. Some touring will be needed.

Candidates, preferably over 25 years of age MUST have an HNC or a City and Guilds Fina Certificate with at least 5 years' experience relevant to at least three of the following relevant to at least three of the following categories:-1) H.F. transmitter and receivers
using SSB. ISB and AM modulation; 2) VHF using SSB. ISB and AM modulation; 2) VH
radio telephone systems; 3) Telex systems radio telephone systems; 3) Telex Systems Broadcasting transmitters; 5) LF Beacons A knowledge of French would be an advantage.

Salary in scale $£ 3,725$ to $£ 5,390$ p.a. which includes an allowance, normally tax-free, in scale $£ 462$ to £1,662 p.a. according to qualifications, experience and marital status.

The post described is partly financed by Britain's programme of aid to the developing countries administered by the Ministry of Overseas Development.

For further particulars you should apply. giving brief details of experience to: CROWN AGENTS, M Division, 4 Millbank, London SW1P 3JD, quoting reference number M2K/750304/WF

## Avery-Hardoll

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